Appendix "A"

Preliminary Hydrology Study Tentative Tract 39011

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Preliminary Hydrology Study

Tentative Tract Map No. 39011

JN: 10615
CLIENT: Green Willow Ranch, LLC
DATE PREPARED
12/17/2024
05/05/2025

PRELIMINARY HYDROLOGY STUDY

Tentative Tract Map No. 39011

Located in the County of Riverside, CA

Prepared by:

adkan ENGINEERS
CIVIL ENGINEERING · SURVEYING · PLANNING
www.adkan.com

6879 Airport Drive
Riverside, CA 92504
Tel. (951) 688-0241
Fax (951) 688-0599

Job No. 10615
December 17, 2024
May 5, 2025

Mitchell J Adkison, R.C.E. NO. 75731 DATE SEAL
Exp. 06/30/2026

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Section 1 - Introduction

1. Introduction

This report provides a for an analysis of proposed storm water infrastructure, detention facilities and the development of Tentative Tract Map No. 39011. This report provides information on proposed and existing storm flows rates, storm volumes, existing facilities, recommended facilities, and the necessary basin storage and water quality sizing criteria associated with managing the projects storm water run-off while effectively treating the quality of the storm water.

Tentative Tract Map No. 39011 is located in the unincorporated area of Riverside County. The project is located on the north side of Lake Matthews, north of El Sobrante Road and East of McAllister Street. Figure 1.1 provides a location map for the project.

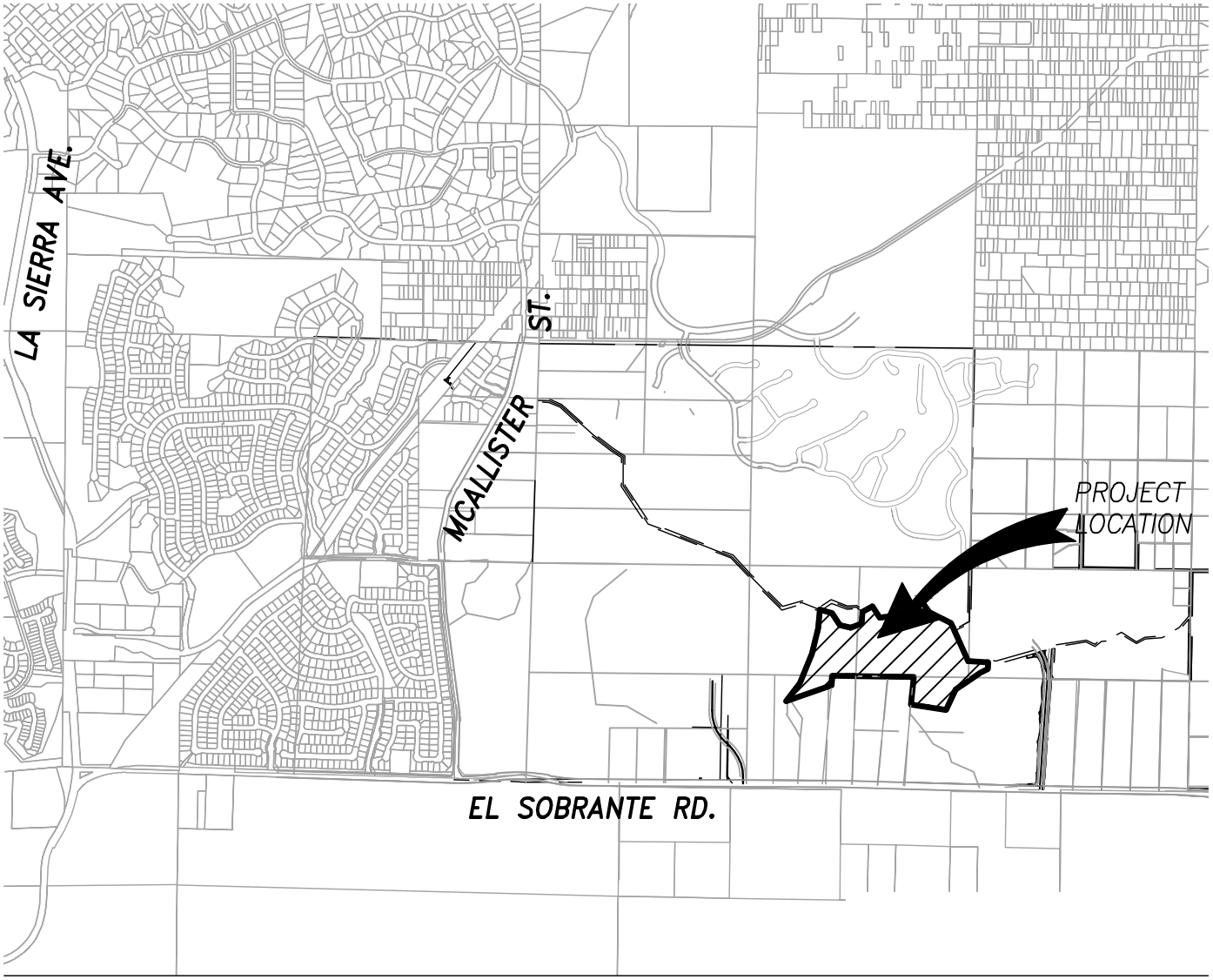
2. Land Use Plan

Tentative Tract Map No. 39011 encompasses a total of approximately 38.56 acres. Figure 1.2 provides the development plan for the project. The proposed project consists of the development of 73 detached single family dwelling units located within the unincorporated area of Riverside County known as the Lake Matthews Area. The Lake Mathew Area Plan was developed as part of the Riverside County General Plan 2025, prepared in 2003 as part of the General Plan Update. The project is located with the El Sobrante Policy Area of the Lake Matthews Area, which encourages the clustering of parcel sizes to a minimum of 10,000 square feet for the purposes of conserving open space and sensitive habitat while not exceeding the underlying housing densities identified by the general plan's designation of LDR-Low Density Residential (2 units/acre) and VLDR-Very Low Density Residentials (1 unit/acre). As part of the clustering efforts the project will be proposing a zone change to incorporate development standards that are consistent with the reduced lot sizes. It should be noted that although the project is clustering the units to a smaller overall parcel size, the total number of units is consistent with the existing land use designation.

3. Purpose of Study

The purpose of this study is to substantiate the hydrology and hydraulic design of the residential development known as Tentative Tract Map No. 39011. This study will analyze the pre-development and post-development storm water run-on and run-off values and propose storm water design recommendations to ensure the adequate size, volumes, and proper operation of drainage facilities for the proposed project while not adversely affecting downstream facilities and maintaining the conveyance of 100-year storm flows for on-site facilities. Along with the standard analysis of a typical report, this report outlines the specific analysis and back-up calculations necessary for determining the hydrology and hydraulics of the development such that the post-developed condition is equal to or improved when compared to pre-developed condition.

4. Figure 1.1 Location Map - Tract No. 39011



0 2000 6000

1000 4000 8000

SCALE: 1" = 2000'

PREPARATION DATE: DEC 2024

adkan ENGINEERS
Civil Engineering • Surveying • Planning
6879 AIRPORT DRIVE RIVERSIDE, CA 92504
TEL:(951) 688-0241 · FAX:(951) 688-0599

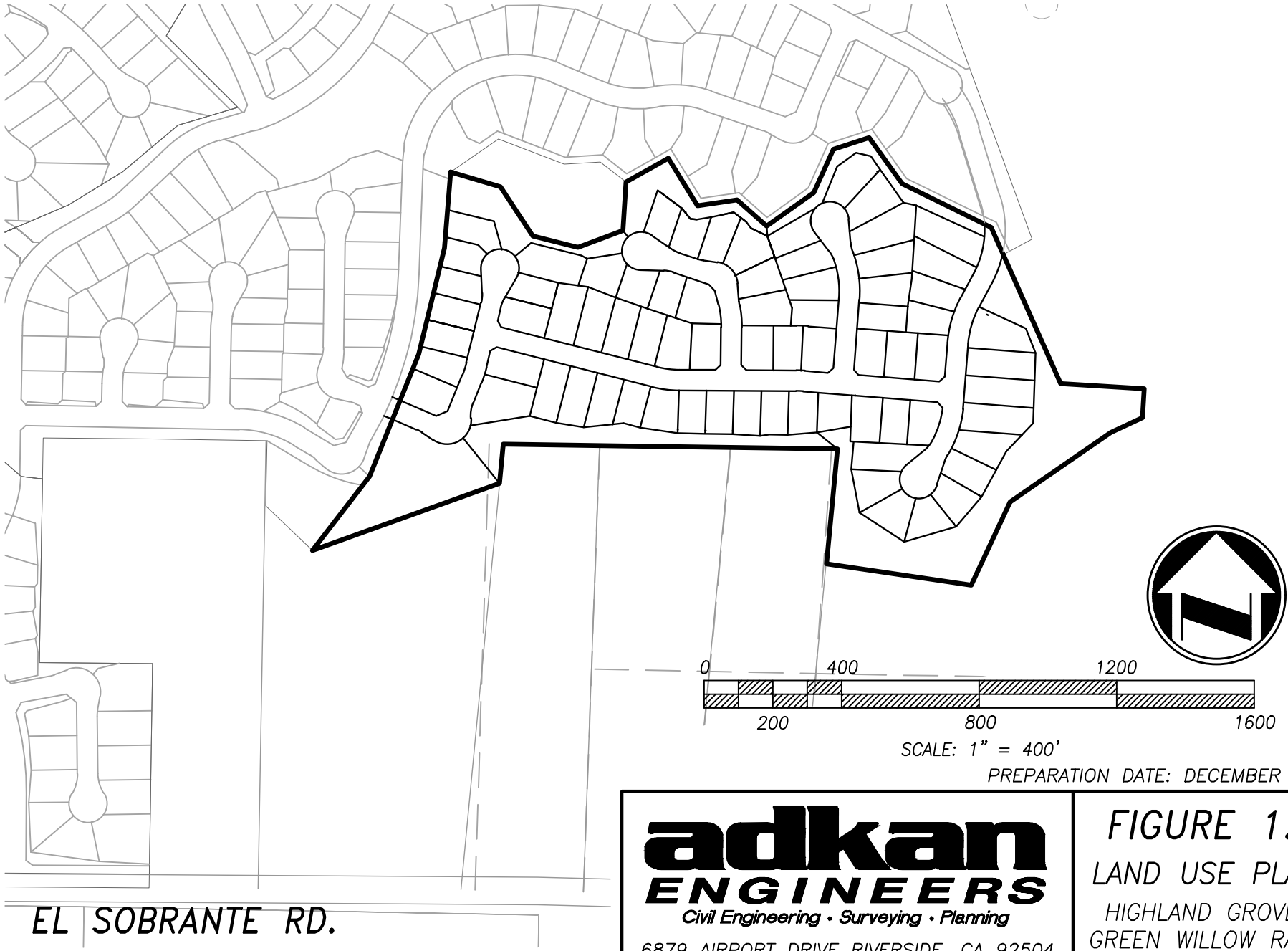
FIGURE 1.1

PROJECT SPECIFIC LOCATION

HG5

TTM 39011

5. Figure 1.2 Land Use Map - Tentative Tract No. 39011



SCALE: 1" = 400'

PREPARATION DATE: DECEMBER 2024

adkan ENGINEERS
Civil Engineering • Surveying • Planning
6879 AIRPORT DRIVE RIVERSIDE, CA 92504
TEL:(951) 688-0241 FAX:(951) 688-0599

FIGURE 1.2

LAND USE PLAN

HIGHLAND GROVE V
GREEN WILLOW RANCH
TTM 39011

\\OST COMMUNITIES\8794\Waddell\10615 - HG5\EXHIBITS\GREEN WILLOW LAND USE FIGURE 1.2.dwg

Section 2 –Rational Method Hydrology Analysis

The Rational Method is commonly used for determining park discharge from relatively small drainage areas. The rational method is based on the following equation Q = CIA, where Q is the peak discharge, C is the coefficient of runoff, I is the rainfall intensity, and A is the area of the watershed. Values of these variables necessary to calculate the park discharge are found utilizing the various plates located within the Riverside County Flood Control Hydrology Manual. The Rational Method Hydrology is calculated for the 10-year and 100-year storm events. The criteria for the protection of storm flow are determined by containing the 10-year storm event with in the tops of street curbs, and the 100-year storm event within the public right of way. Storm drains and/or channels should be considered when either condition is exceeded.

1. Existing Rational Method Hydrology

The existing site is an irregular shaped property consisting of rolling hills previously utilized for the cultivation of citrus fruit. The existing citrus trees have since been removed leaving the remanent of citrus furrows and overgrown earthen irrigation trenches. The project site consists of a ridgeline along the northerly boundary of the site. The ridgeline can also be defined by an unpaved road seen within aerial imagery providing a means of maintenance access for an existing reservoir owned by Western Municipal Water District (WMWD) directly north of the Project site. From the ridge line, the existing flows travel south into a natural drainage course that bounds the south edges of the project site. The natural drainage course flows from east to west along the southerly project boundary, continues westerly and ultimately conveys flows northwesterly before being conveyed northerly beyond the project through a development to the northwest of the project site, known as Tramonte, and finally into the Harrison Dam facility. The existing drainage course has been deeply incised and defined throughout time, and in many locations exhibit exposed bedrock limiting the potential for future erosion.

The Harrison Dam was constructed based on the development of the upstream tributaries to protect the downstream properties located in the City of Riverside. The Dam was designed to detain the watershed of the proposed project, including the upstream properties, to a maximum discharge of 150 CFS. Based on the projects clustering efforts it was determined through discussion with RCFC that additional post development increased storm water runoff mitigation would be necessary beyond the normally required 2-, 5-, and 10-year storm events, and therefore detention basins are required for the project to be designed with the capacity to mitigate the 100-year storm events. This is further discussed within Section 3 of this report.

From the Harrison Dam facility existing storm flows are conveyed through the City of Riverside and ultimately into the Arizona Channel owned and maintained by RCFC. The Arizona Channel is part of a drainage system funded by Area Drainage Plan fees known at the Southwest Area Drainage Plan.

2. Proposed Rational Method Hydrology

The proposed project consists of 73 single family detached single family residences. The project site has been designed in such a manner to respect the existing drainage pattern from north to south. The project maintains one distinct drainage tributary on the southwesterly portion of the site. The entire project site is conveyed into one extended detention basin on the southwest side of the project. This southwest location is the projects single point of flows leaving from the project site. All preliminary storm drainage facilities and catch basins have been proposed within the proposed project to limit the spread of the 100 year on-site flows to be contained within tops of the street curbs.

As discussed within the Existing Rational Method Hydrology section, it was determined through discussion with RCFC that additional post development increased storm water runoff mitigation would be necessary beyond the 2-, 5-, and 10-year storm events, and therefore the extended detention basins are required for the project to be designed with the capacity to mitigate the 100-year storm events. These calculations were performed utilizing the Synthetic Unit Hydrograph Method and a summary of the results are included within Section 3 of this report.

It should be noted the Proposed Rational Method Hydrology flow rates are utilized to size the storm drain facilities to provide a level of storm protection to adequately convey the 100-year storm flow rates. This information is utilized to analyze the hydraulics of the storm facilities for the purposes of sizing storm drain lines, inlets and outlets, spillways, street capacities and culverts for the ultimate experienced flow rates.

The results of the Proposed Rational Method Hydrology can be found in Appendix “B” of this report.

Table 2-2
Tract 39011– Proposed Rational Method Flow Rates

Drainage Area	Node No.	10-Year Flow Rate	100-Year Flow Rate
Extended Detention Basin	25	35.88 CFS	58.73 CFS

Section 3 – Synthetic Unit Method Hydrology Analysis

The Synthetic Unit Method Hydrology is utilized to analyze the entire are of a proposed development that will be routed through a detention facility for mitigation of the post construction incremental increased runoff when compared to the existing condition.

Storms to be studied will include the 1-hour, 3-hour, 6-hour and 24-hour duration for the 2-year, 5-year, and 10-year return frequencies. Detention basins and outlet sizing's will ensure that none of these storm events will have up to a 10% increase in peak storm discharge of the post development condition than in the pre-development conditions. As previously discussed, peak flow storm mitigation would be necessary beyond the 2-, 5-, and 10-year storm events, however with the added level of storm protection needed for the Harrison Dam, RCFC has required the extended detention basin to be designed with the capacity to mitigate the 100-year storm events.

The project is proposing the utilization of a detention basin for the mitigation of the post construction incremental increased runoff. The proposed extended basin effectively mitigate the post development flow rates ensuring none of the storm events will have up to a 10% increase in peak storm discharge of the post development condition than in the pre-development conditions.

A summary of the extended detention basins existing, proposed, and routed peak flows for all storm events and frequencies are shown in Table below. Existing Synthetic Unit Method Hydrology calculations can be found in Appendix C of this report, Proposed Synthetic Unit Method Hydrology calculations can be found in Appendix D of this report, and Basin Routing Hydrographs along with respective Outflow Calculations can be found in Appendix E of this report.

It should be noted, although the impervious fraction of the project site increased, the developed flow rate when compared to the existing flow rates generally decreased without basin mitigation. The typically does not occur, however because of the topography of the existing watershed the lag time has an extremely short duration and in the proposed condition the lag time is increased by creating a longer flow path lengthening the duration of the hydrograph. By lengthening the duration of the hydrograph, although the volume of the storm has increased, the peak flow is reduced over a longer duration and ultimately decreases without utilizing a basin for mitigation. Simply stated, the time of concentration of the proposed watershed is longer when compared to the time of concentration of the existing watershed, therefore although the imperviousness has increased to the proposed flow rates decrease.

The basin was also analyzed to confirm a maximum of a 72-hour drawdown time. The outflow basin was analyzed to experience being filled by the depth of the volume of a 100-year storm passing through the primary outlet structure for a duration of a 100-year storm. The basin was emptied to a depth of les than 3" after 72 hours and considered to be negligible as the volume would be contained by the low flow trenches. Calculations for the basin drawdown can be found within Appendix "H".

1. Extended Detention Basin

UNIT HYDROGRAPH SUMMARY							
Storm Event	Existing Condition		Developed Condition		Routed Basin		
	Flow (cfs)	Volume (ac.ft.)	Flow (cfs)	Volume (ac.ft.)	Routed Basin Out Flow (cfs)	Storage Volume (ac.ft.)	Depth (ft)
2 Year - 1 Hour	26.924	0.6278	25.921	0.7357	0.452	0.719	2.51
2 Year - 3 Hour	13.297	0.5661	11.612	0.9719	0.723	0.915	3.09
2 Year - 6 Hour	11.651	0.6045	10.033	1.3136	0.888	1.182	3.80
2 Year - 24 Hour	0.942	0.4342	3.509	2.1321	1.020	1.457	4.48
5 Year - 1 Hour	39.661	1.0447	38.649	1.0675	0.805	1.037	3.42
5 Year - 3 Hour	20.450	1.0214	18.702	1.3939	0.953	1.310	4.12
5 Year - 6 Hour	19.222	1.1974	17.368	1.9210	8.813	1.623	4.86
5 Year - 24 Hour	3.864	0.9101	4.970	3.0199	3.986	1.593	4.79
10 Year - 1 Hour	53.004	1.6866	51.576	1.4893	1.016	1.448	4.46
10 Year - 3 Hour	29.569	2.2396	27.216	1.9110	11.093	1.638	4.90
10 Year - 6 Hour	28.658	2.8266	26.296	2.6439	25.151	1.698	5.03
10 Year - 24 Hour	9.264	3.2965	7.094	3.7320	7.052	1.612	4.84
100 Year - 1 Hour	85.010	2.8019	84.206	2.5933	57.187	1.762	5.17
100 Year - 3 Hour	47.544	3.9062	45.284	3.3629	44.090	1.736	5.11
100 Year - 6 Hour	47.683	5.4579	45.417	4.7524	43.321	1.734	5.11
100 Year - 24 Hour	16.607	6.7703	14.437	6.7447	14.384	1.659	4.94

Section 4 – Analytical Approach

The site hydrology was performed utilizing Riverside County Flood Control and Water Conversation District Hydrology Manual, from which pertinent soil and rainfall information was obtained. See Appendix G of this report for the referenced Plates within the Riverside County Flood Control Hydrology Manual.

Rational Method storm flow rates were analyzed by using the "RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM", Riverside County Flood Control & Water Conservation District 1978 Hydrology Manual, produced by Bondamin Engineering.

Existing and Proposed detention basin flow rates were analyzed by utilizing the "SYNTHETIC UNIT HYDROLOGY METHOD COMPUTER PROGRAM", Riverside County Flood Control & Water Conservation District 1978 Hydrology Manual, produced by Bondamin Engineering.

Detention basin routing flow rates were analyzed by utilizing the "FLOOD HYDROGRAPH ROUTING PROGRAM", produced by CIVIL CADD/CIVIL DESIGN.

Basin Outflow Curves were calculated by utilizing a Microsoft Excel Spreadsheet developed by Adkan Engineers based on fundamental fluid mechanics by determining the pressure drop across the orifice allowing for a calculation of flow rate. The fundamental formula used for flow rate in an orifice flow scenario is shown below:

$$Q=C_d \times A \times 2gH$$

"Q" denotes the flow rate
"C_d" is the discharge coefficient
"A" is the Area of the orifice
"g" is the acceleration due to gravity
"H" is the height to the orifice centroid

Hydraulic computations for catch basin sizing, street flow capacities, and sharp/broad crested weir flow rates were performed utilizing software known as "FlowMaster" produced by Haestad Methods and/or "Hydraflow Express" produced by Autodesk Civil 3D.

Section 5 – Conclusion

The hydrologic calculations provided within this report substantiate the preliminary hydrology and hydraulic design of the proposed project, Tentative Tract Map No. 39011, and indicate the following:

- The proposed storm drain facilities demonstrate the ability to convey the Rational Hydrology Method 10 and 100 year storm events as required by the Riverside County Flood Control Hydrology Manual.

- The proposed extended detention basin provides mitigation for post development peak storm discharge for the 1-hour, 3-hour, 6-hour and 24-hour duration for the 2-year, 5-year, 10-year, and 100-year return frequencies to the pre-development condition.

Therefore, it is our conclusion this project **does not** negatively impact the local community or watershed goals of the Santa Ana River and does not adversely affect downstream facilities while maintaining the adequate conveyance of storm flows for on-site facilities to the criteria for the protection of storm flow as determined by the Riverside County Flood Control Hydrology Manual.

Appendix A – Existing Rational Hydrology Method

```
                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
        Rational Hydrology Study        Date: 05/05/25  File:ex10.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

------------------------------------------------------------------------
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =   10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year =  10.0
Calculated rainfall intensity data:
1 hour intensity =  0.829(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   914.000(Ft.)
Top (of initial area) elevation =  1620.000(Ft.)
Bottom (of initial area) elevation =  1572.000(Ft.)
Difference in elevation =    48.000(Ft.)
Slope =    0.05252  s(percent)=       5.25
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.608 min.
Rainfall intensity =      1.680(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.791
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.900
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  85.20
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     12.746(CFS)
Total initial stream area =        9.590(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        2.000 to Point/Station        3.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of natural channel elevation =   1572.000(Ft.)
End of natural channel elevation =   1444.000(Ft.)
Length of natural channel  =  4065.000(Ft.)
Estimated mean flow rate at midpoint of channel =     72.191(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.64(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0315
Corrected/adjusted channel slope =  0.0315
Travel time =    8.86 min.     TC =   23.47  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.764
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.600
```

```
Decimal fraction soil group D = 0.200
RI index for soil(AMC 2)  =  85.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.326(In/Hr) for a    10.0 year storm
Subarea runoff =     90.636(CFS) for     89.450(Ac.)
Total runoff =    103.382(CFS)       Total area =      99.040(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
----------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     99.040(Ac.)
Runoff from this stream =    103.382(CFS)
Time of concentration =   23.47 min.
Rainfall intensity =     1.326(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        4.000 to Point/Station        5.000
**** INITIAL AREA EVALUATION ****
----------------------------------------------------------------------------
Initial area flow distance =   952.000(Ft.)
Top (of initial area) elevation =  1572.000(Ft.)
Bottom (of initial area) elevation =  1532.000(Ft.)
Difference in elevation =    40.000(Ft.)
Slope =    0.04202  s(percent)=       4.20
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   15.526 min.
Rainfall intensity =      1.630(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.794
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      9.748(CFS)
Total initial stream area =        7.530(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        5.000 to Point/Station        3.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1532.000(Ft.)
End of natural channel elevation =   1444.000(Ft.)
Length of natural channel  =  2338.000(Ft.)
Estimated mean flow rate at midpoint of channel =     46.889(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.37(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0376
Corrected/adjusted channel slope =  0.0376
Travel time =    5.29 min.     TC =   20.81  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.780
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.408(In/Hr) for a    10.0 year storm
Subarea runoff =     62.990(CFS) for     57.380(Ac.)
Total runoff =     72.738(CFS)       Total area =      64.910(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
----------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     64.910(Ac.)
Runoff from this stream =     72.738(CFS)
```

```
Time of concentration =   20.81 min.
Rainfall intensity =     1.408(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      103.382     23.47                 1.326
2       72.738     20.81                 1.408
Largest stream flow has longer time of concentration
Qp =    103.382 + sum of
          Qb         Ia/Ib
          72.738 *    0.942 =     68.494
Qp =    171.876

Total of 2 streams to confluence:
Flow rates before confluence point:
     103.382      72.738
Area of streams before confluence:
       99.040       64.910
Results of confluence:
Total flow rate =    171.876(CFS)
Time of concentration =    23.471 min.
Effective stream area after confluence =    163.950(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        6.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1444.000(Ft.)
End of natural channel elevation =   1369.000(Ft.)
Length of natural channel  =  2816.000(Ft.)
Estimated mean flow rate at midpoint of channel =    206.860(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.67(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0266
Corrected/adjusted channel slope =  0.0266
Travel time =    4.85 min.     TC =   28.32  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.758
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  85.50
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.207(In/Hr) for a    10.0 year storm
Subarea runoff =     61.047(CFS) for     66.740(Ac.)
Total runoff =    232.924(CFS)       Total area =     230.690(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        6.000 to Point/Station        6.000
**** CONFLUENCE OF MINOR STREAMS ****
________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    230.690(Ac.)
Runoff from this stream =    232.924(CFS)
Time of concentration =   28.32 min.
Rainfall intensity =     1.207(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        7.000 to Point/Station        8.000
**** INITIAL AREA EVALUATION ****
________________________________________________________________________
Initial area flow distance =   901.000(Ft.)
Top (of initial area) elevation =  1592.000(Ft.)
Bottom (of initial area) elevation =  1516.000(Ft.)
Difference in elevation =    76.000(Ft.)
Slope =    0.08435  s(percent)=       8.44
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.211 min.
Rainfall intensity =      1.767(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
```

```
Runoff Coefficient = 0.802
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      6.189(CFS)
Total initial stream area =        4.370(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        8.000 to Point/Station        6.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1516.000(Ft.)
End of natural channel elevation =   1369.000(Ft.)
Length of natural channel  =  4248.000(Ft.)
Estimated mean flow rate at midpoint of channel =     90.528(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.57(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0346
Corrected/adjusted channel slope =  0.0346
Travel time =    8.26 min.     TC =   21.47  min.


 Adding area flow to channel
UNDEVELOPED (fair cover) subarea
Runoff Coefficient = 0.717
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  79.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.386(In/Hr) for a    10.0 year storm
Subarea runoff =    118.309(CFS) for    119.100(Ac.)
Total runoff =    124.498(CFS)       Total area =     123.470(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        6.000 to Point/Station        6.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =    123.470(Ac.)
Runoff from this stream =    124.498(CFS)
Time of concentration =   21.47 min.
Rainfall intensity =     1.386(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      232.924     28.32                 1.207
2      124.498     21.47                 1.386
Largest stream flow has longer time of concentration
Qp =    232.924 + sum of
          Qb          Ia/Ib
         124.498 *    0.871 =    108.400
Qp =    341.324

Total of 2 streams to confluence:
Flow rates before confluence point:
     232.924     124.498
Area of streams before confluence:
      230.690      123.470
Results of confluence:
Total flow rate =    341.324(CFS)
Time of concentration =    28.323 min.
Effective stream area after confluence =    354.160(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        6.000 to Point/Station        9.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1369.000(Ft.)
```

```
End of natural channel elevation =   1286.000(Ft.)
Length of natural channel  =  2452.000(Ft.)
Estimated mean flow rate at midpoint of channel =    376.328(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  13.16(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0338
Corrected/adjusted channel slope =  0.0338
Travel time =    3.11 min.     TC =   31.43  min.


 Adding area flow to channel
UNDEVELOPED (fair cover) subarea
Runoff Coefficient = 0.668
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  77.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.146(In/Hr) for a    10.0 year storm
Subarea runoff =     55.574(CFS) for     72.640(Ac.)
Total runoff =    396.898(CFS)       Total area =     426.800(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        9.000 to Point/Station       10.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1288.000(Ft.)
End of natural channel elevation =   1221.000(Ft.)
Length of natural channel  =  2462.000(Ft.)
Estimated mean flow rate at midpoint of channel =    433.947(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  12.35(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0272
Corrected/adjusted channel slope =  0.0272
Travel time =    3.32 min.     TC =   34.75  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.754
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.900
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  86.30
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.089(In/Hr) for a    10.0 year storm
Subarea runoff =     65.416(CFS) for     79.680(Ac.)
Total runoff =    462.314(CFS)       Total area =     506.480(Ac.)


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Process from Point/Station       10.000 to Point/Station       10.250
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1221.000(Ft.)
End of natural channel elevation =   1207.000(Ft.)
Length of natural channel  =   710.000(Ft.)
Estimated mean flow rate at midpoint of channel =    464.532(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  10.74(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0197
Corrected/adjusted channel slope =  0.0197
Travel time =    1.10 min.     TC =   35.85  min.
```

```
 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.750
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2)  =  86.10
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.073(In/Hr) for a    10.0 year storm
Subarea runoff =      3.907(CFS) for      4.860(Ac.)
Total runoff =    466.222(CFS)       Total area =     511.340(Ac.)


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Process from Point/Station       10.250 to Point/Station       10.250
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    511.340(Ac.)
Runoff from this stream =    466.222(CFS)
Time of concentration =   35.85 min.
Rainfall intensity =     1.073(In/Hr)


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Process from Point/Station       10.500 to Point/Station       10.500
**** USER DEFINED FLOW INFORMATION AT A POINT ****
______________________________________________________________________________
Rainfall intensity =      1.520(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.773
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
User specified values are as follows:
TC =  17.86 min.  Rain intensity =       1.52(In/Hr)
Total area =        33.20(Ac.)  Total runoff =     67.24(CFS)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       10.500 to Point/Station       10.250
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1249.000(Ft.)
End of natural channel elevation =   1207.000(Ft.)
Length of natural channel  =   932.000(Ft.)
Estimated mean flow rate at midpoint of channel =     72.303(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.15(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0451
Corrected/adjusted channel slope =  0.0451
Travel time =    1.70 min.     TC =   19.56  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.784
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2)  =  86.10
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.452(In/Hr) for a    10.0 year storm
Subarea runoff =      5.691(CFS) for      5.000(Ac.)
Total runoff =     72.931(CFS)       Total area =      38.200(Ac.)


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Process from Point/Station       10.250 to Point/Station       10.250
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     38.200(Ac.)
Runoff from this stream =     72.931(CFS)
Time of concentration =   19.56 min.
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Rainfall intensity =     1.452(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                (In/Hr)


1      466.222     35.85                 1.073
2       72.931     19.56                 1.452
Largest stream flow has longer time of concentration
Qp =    466.222 + sum of
          Qb         Ia/Ib
          72.931 *    0.739 =     53.865
Qp =    520.086

Total of 2 streams to confluence:
Flow rates before confluence point:
     466.222      72.931
Area of streams before confluence:
      511.340       38.200
Results of confluence:
Total flow rate =    520.086(CFS)
Time of concentration =    35.854 min.
Effective stream area after confluence =    549.540(Ac.)


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Process from Point/Station       10.250 to Point/Station       11.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1207.000(Ft.)
End of natural channel elevation =   1169.000(Ft.)
Length of natural channel  =   839.000(Ft.)
Estimated mean flow rate at midpoint of channel =    572.195(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  17.40(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0453
Corrected/adjusted channel slope =  0.0453
Travel time =    0.80 min.     TC =   36.66  min.


 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.873
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2)  =  75.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      1.061(In/Hr) for a    10.0 year storm
Subarea runoff =    102.024(CFS) for    110.120(Ac.)
Total runoff =    622.111(CFS)       Total area =     659.660(Ac.)


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Process from Point/Station       11.000 to Point/Station       12.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1169.000(Ft.)
End of natural channel elevation =   1139.000(Ft.)
Length of natural channel  =   933.000(Ft.)
Estimated mean flow rate at midpoint of channel =    636.587(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  15.18(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0322
Corrected/adjusted channel slope =  0.0322
Travel time =    1.02 min.     TC =   37.68  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.741
Decimal fraction soil group A = 0.000
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Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.400
Decimal fraction soil group D = 0.400
RI index for soil(AMC 2)  =  85.60
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.046(In/Hr) for a    10.0 year storm
Subarea runoff =     23.804(CFS) for     30.700(Ac.)
Total runoff =    645.915(CFS)       Total area =     690.360(Ac.)


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Process from Point/Station       12.000 to Point/Station       12.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =    690.360(Ac.)
Runoff from this stream =    645.915(CFS)
Time of concentration =   37.68 min.
Rainfall intensity =     1.046(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station       16.000 to Point/Station       17.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   972.000(Ft.)
Top (of initial area) elevation =  1518.000(Ft.)
Bottom (of initial area) elevation =  1451.000(Ft.)
Difference in elevation =    67.000(Ft.)
Slope =    0.06893  s(percent)=       6.89
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.179 min.
Rainfall intensity =      1.706(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.810
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.500
Decimal fraction soil group D = 0.500
RI index for soil(AMC 2)  =  87.50
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     11.847(CFS)
Total initial stream area =        8.580(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station       17.000 to Point/Station       17.100
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1451.000(Ft.)
End of natural channel elevation =   1371.000(Ft.)
Length of natural channel  =  1350.000(Ft.)
Estimated mean flow rate at midpoint of channel =     21.899(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.48(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0593
Corrected/adjusted channel slope =  0.0593
Travel time =    3.01 min.     TC =   17.19  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.779
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.700
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  84.70
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.549(In/Hr) for a    10.0 year storm
Subarea runoff =     17.567(CFS) for     14.560(Ac.)
Total runoff =     29.415(CFS)       Total area =      23.140(Ac.)


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Process from Point/Station       17.100 to Point/Station       17.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
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```
Upstream point/station elevation =  1371.000(Ft.)
Downstream point/station elevation =  1360.000(Ft.)
Pipe length  =   473.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    29.415(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    29.415(CFS)
Normal flow depth in pipe =   17.04(In.)
Flow top width inside pipe =   21.78(In.)
Critical Depth =   22.24(In.)
Pipe flow velocity =     12.33(Ft/s)
Travel time through pipe =    0.64 min.
Time of concentration (TC) =    17.83 min.


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Process from Point/Station       17.200 to Point/Station       18.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1360.000(Ft.)
End of natural channel elevation =   1347.000(Ft.)
Length of natural channel  =   166.000(Ft.)
Estimated mean flow rate at midpoint of channel =     29.771(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.35(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0783
Corrected/adjusted channel slope =  0.0783
Travel time =    0.30 min.     TC =   18.12  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.787
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.509(In/Hr) for a    10.0 year storm
Subarea runoff =      0.665(CFS) for      0.560(Ac.)
Total runoff =     30.079(CFS)       Total area =      23.700(Ac.)


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Process from Point/Station       18.000 to Point/Station       18.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     23.700(Ac.)
Runoff from this stream =     30.079(CFS)
Time of concentration =   18.12 min.
Rainfall intensity =     1.509(In/Hr)


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Process from Point/Station       19.000 to Point/Station       20.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   687.000(Ft.)
Top (of initial area) elevation =  1478.000(Ft.)
Bottom (of initial area) elevation =  1430.000(Ft.)
Difference in elevation =    48.000(Ft.)
Slope =    0.06987  s(percent)=       6.99
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.308 min.
Rainfall intensity =      1.831(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.805
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      7.291(CFS)
Total initial stream area =       4.950(Ac.)
Pervious area fraction = 1.000
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Process from Point/Station       20.000 to Point/Station       21.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1430.000(Ft.)
End of natural channel elevation =   1400.000(Ft.)
Length of natural channel  =   583.000(Ft.)
Estimated mean flow rate at midpoint of channel =     13.212(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.09(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0515
Corrected/adjusted channel slope =  0.0515
Travel time =    1.60 min.     TC =   13.90  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.799
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.722(In/Hr) for a    10.0 year storm
Subarea runoff =     11.068(CFS) for      8.040(Ac.)
Total runoff =     18.359(CFS)       Total area =      12.990(Ac.)


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Process from Point/Station       21.000 to Point/Station       18.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1400.000(Ft.)
End of natural channel elevation =   1347.000(Ft.)
Length of natural channel  =  1004.000(Ft.)
Estimated mean flow rate at midpoint of channel =     29.998(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.69(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0528
Corrected/adjusted channel slope =  0.0528
Travel time =    2.17 min.     TC =   16.08  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.793
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.602(In/Hr) for a    10.0 year storm
Subarea runoff =     20.908(CFS) for     16.470(Ac.)
Total runoff =     39.267(CFS)       Total area =      29.460(Ac.)


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Process from Point/Station       18.000 to Point/Station       18.000
**** CONFLUENCE OF MINOR STREAMS ****
----------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     29.460(Ac.)
Runoff from this stream =     39.267(CFS)
Time of concentration =   16.08 min.
Rainfall intensity =     1.602(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                (In/Hr)


1       30.079     18.12                1.509
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```
2       39.267     16.08                 1.602
Largest stream flow has longer or shorter time of concentration
Qp =     39.267 + sum of
          Qa          Tb/Ta
          30.079 *    0.887 =     26.685
Qp =     65.952

Total of 2 streams to confluence:
Flow rates before confluence point:
      30.079      39.267
Area of streams before confluence:
       23.700       29.460
Results of confluence:
Total flow rate =     65.952(CFS)
Time of concentration =    16.079 min.
Effective stream area after confluence =     53.160(Ac.)


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Process from Point/Station       18.000 to Point/Station       15.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1347.000(Ft.)
End of natural channel elevation =   1299.000(Ft.)
Length of natural channel  =  1128.000(Ft.)
Estimated mean flow rate at midpoint of channel =     74.462(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.97(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0426
Corrected/adjusted channel slope =  0.0426
Travel time =    2.10 min.     TC =   18.18  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.787
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.506(In/Hr) for a    10.0 year storm
Subarea runoff =     16.259(CFS) for     13.720(Ac.)
Total runoff =     82.211(CFS)       Total area =      66.880(Ac.)


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Process from Point/Station       15.000 to Point/Station       15.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     66.880(Ac.)
Runoff from this stream =     82.211(CFS)
Time of concentration =   18.18 min.
Rainfall intensity =     1.506(In/Hr)


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Process from Point/Station       13.000 to Point/Station       14.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   930.000(Ft.)
Top (of initial area) elevation =  1522.000(Ft.)
Bottom (of initial area) elevation =  1448.000(Ft.)
Difference in elevation =    74.000(Ft.)
Slope =    0.07957  s(percent)=       7.96
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.537 min.
Rainfall intensity =      1.746(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.800
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      9.529(CFS)
Total initial stream area =        6.820(Ac.)
```

```
Pervious area fraction = 1.000

++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.000 to Point/Station       14.100
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1448.000(Ft.)
End of natural channel elevation =   1363.000(Ft.)
Length of natural channel  =  1674.000(Ft.)
Estimated mean flow rate at midpoint of channel =     24.236(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.11(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0508
Corrected/adjusted channel slope =  0.0508
Travel time =    3.92 min.     TC =   17.46  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.778
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.700
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  84.70
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.537(In/Hr) for a    10.0 year storm
Subarea runoff =     25.175(CFS) for     21.050(Ac.)
Total runoff =     34.704(CFS)       Total area =      27.870(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.100 to Point/Station       14.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1363.000(Ft.)
Downstream point/station elevation =  1359.000(Ft.)
Pipe length  =    86.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    34.704(CFS)
Nearest computed pipe diameter  =     21.00(In.)
Calculated individual pipe flow  =    34.704(CFS)
Normal flow depth in pipe =   17.53(In.)
Flow top width inside pipe =   15.60(In.)
Critical depth could not be calculated.
Pipe flow velocity =     16.18(Ft/s)
Travel time through pipe =    0.09 min.
Time of concentration (TC) =    17.55 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.300 to Point/Station       14.400
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.788
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    17.55 min.
Rainfall intensity =      1.533(In/Hr) for a    10.0 year storm
Subarea runoff =     10.818(CFS) for      8.950(Ac.)
Total runoff =     45.522(CFS)       Total area =      36.820(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.400 to Point/Station       14.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1377.000(Ft.)
Downstream point/station elevation =  1359.000(Ft.)
Pipe length  =   366.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    45.522(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    45.522(CFS)
Normal flow depth in pipe =   17.93(In.)
Flow top width inside pipe =   20.87(In.)
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Critical depth could not be calculated.
Pipe flow velocity =     18.09(Ft/s)
Travel time through pipe =    0.34 min.
Time of concentration (TC) =    17.88 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.200 to Point/Station       14.500
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1359.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =    75.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    45.522(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    45.522(CFS)
Normal flow depth in pipe =   17.34(In.)
Flow top width inside pipe =   21.49(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.74(Ft/s)
Travel time through pipe =    0.07 min.
Time of concentration (TC) =    17.95 min.


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Process from Point/Station       14.500 to Point/Station       14.600
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1355.000(Ft.)
End of natural channel elevation =   1329.000(Ft.)
Length of natural channel  =   406.000(Ft.)
Estimated mean flow rate at midpoint of channel =     47.729(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.66(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0640
Corrected/adjusted channel slope =  0.0640
Travel time =    0.70 min.     TC =   18.65  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.785
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.487(In/Hr) for a    10.0 year storm
Subarea runoff =      4.169(CFS) for      3.570(Ac.)
Total runoff =     49.692(CFS)       Total area =      40.390(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.600 to Point/Station       14.700
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1329.000(Ft.)
Downstream point/station elevation =  1319.000(Ft.)
Pipe length  =   258.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    49.692(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    49.692(CFS)
Normal flow depth in pipe =   18.52(In.)
Flow top width inside pipe =   25.07(In.)
Critical depth could not be calculated.
Pipe flow velocity =     17.09(Ft/s)
Travel time through pipe =    0.25 min.
Time of concentration (TC) =    18.90 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.700 to Point/Station       15.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1319.000(Ft.)
End of natural channel elevation =   1299.000(Ft.)
Length of natural channel  =   333.000(Ft.)
Estimated mean flow rate at midpoint of channel =     50.307(CFS)
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Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.50(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0601
Corrected/adjusted channel slope =  0.0601
Travel time =    0.58 min.     TC =   19.49  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.783
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.455(In/Hr) for a    10.0 year storm
Subarea runoff =      1.139(CFS) for      1.000(Ac.)
Total runoff =     50.831(CFS)       Total area =      41.390(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       15.000 to Point/Station       15.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     41.390(Ac.)
Runoff from this stream =     50.831(CFS)
Time of concentration =   19.49 min.
Rainfall intensity =     1.455(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       82.211     18.18                 1.506
2       50.831     19.49                 1.455
Largest stream flow has longer or shorter time of concentration
Qp =     82.211 + sum of
          Qa          Tb/Ta
          50.831 *    0.933 =     47.409
Qp =    129.620

Total of 2 streams to confluence:
Flow rates before confluence point:
      82.211      50.831
Area of streams before confluence:
       66.880       41.390
Results of confluence:
Total flow rate =    129.620(CFS)
Time of concentration =    18.175 min.
Effective stream area after confluence =    108.270(Ac.)


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Process from Point/Station       15.000 to Point/Station       22.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1299.000(Ft.)
End of natural channel elevation =   1215.000(Ft.)
Length of natural channel  =  1781.000(Ft.)
Estimated mean flow rate at midpoint of channel =    173.246(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  12.18(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0472
Corrected/adjusted channel slope =  0.0472
Travel time =    2.44 min.     TC =   20.61  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.766
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
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Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.415(In/Hr) for a    10.0 year storm
Subarea runoff =     79.022(CFS) for     72.880(Ac.)
Total runoff =    208.642(CFS)       Total area =     181.150(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       22.000 to Point/Station       23.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1215.000(Ft.)
End of natural channel elevation =   1170.000(Ft.)
Length of natural channel  =  1218.000(Ft.)
Estimated mean flow rate at midpoint of channel =    218.415(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  11.59(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0369
Corrected/adjusted channel slope =  0.0369
Travel time =    1.75 min.     TC =   22.36  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.748
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.400
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  82.80
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.358(In/Hr) for a    10.0 year storm
Subarea runoff =     17.228(CFS) for     16.970(Ac.)
Total runoff =    225.870(CFS)       Total area =     198.120(Ac.)


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Process from Point/Station       23.000 to Point/Station       23.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.762
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Time of concentration =    22.36 min.
Rainfall intensity =      1.358(In/Hr) for a    10.0 year storm
Subarea runoff =     88.024(CFS) for     85.030(Ac.)
Total runoff =    313.895(CFS)       Total area =     283.150(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       23.000 to Point/Station       12.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1170.000(Ft.)
End of natural channel elevation =   1139.000(Ft.)
Length of natural channel  =   692.000(Ft.)
Estimated mean flow rate at midpoint of channel =    317.331(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  14.34(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0448
Corrected/adjusted channel slope =  0.0448
Travel time =    0.80 min.     TC =   23.17  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.702
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Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  78.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.334(In/Hr) for a    10.0 year storm
Subarea runoff =      5.808(CFS) for      6.200(Ac.)
Total runoff =    319.703(CFS)       Total area =     289.350(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       12.000 to Point/Station       12.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =    289.350(Ac.)
Runoff from this stream =    319.703(CFS)
Time of concentration =   23.17 min.
Rainfall intensity =     1.334(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      645.915     37.68               1.046
2      319.703     23.17               1.334
Largest stream flow has longer time of concentration
Qp =    645.915 + sum of
          Qb         Ia/Ib
         319.703 *    0.784 =    250.679
Qp =    896.594

Total of 2 main streams to confluence:
Flow rates before confluence point:
     645.915     319.703
Area of streams before confluence:
      690.360      289.350


Results of confluence:
Total flow rate =    896.594(CFS)
Time of concentration =    37.683 min.
Effective stream area after confluence  =    979.710(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       12.000 to Point/Station       24.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1139.000(Ft.)
End of natural channel elevation =   1136.000(Ft.)
Length of natural channel  =   119.000(Ft.)
Estimated mean flow rate at midpoint of channel =    897.015(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  15.02(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0252
Corrected/adjusted channel slope =  0.0252
Travel time =    0.13 min.     TC =   37.81  min.

 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.662
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  78.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.044(In/Hr) for a    10.0 year storm
Subarea runoff =      0.636(CFS) for      0.920(Ac.)
Total runoff =    897.230(CFS)       Total area =     980.630(Ac.)
End of computations, total study area =          980.63 (Ac.)
The following figures maybe used for a unit hydrograph study of the same area.
Area averaged pervious area fraction(Ap) = 0.839
Area averaged RI index number =  80.8
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
        Rational Hydrology Study        Date: 05/05/25  File:mcs10.out
--------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

--------------------------------------------------------------------------


Program License Serial Number 5006

--------------------------------------------------------------------------
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =   10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year =  10.0
Calculated rainfall intensity data:
1 hour intensity =  0.829(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       25.000 to Point/Station       26.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =  1000.000(Ft.)
Top (of initial area) elevation =  1296.000(Ft.)
Bottom (of initial area) elevation =  1238.000(Ft.)
Difference in elevation =    58.000(Ft.)
Slope =    0.05800  s(percent)=       5.80
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.845 min.
Rainfall intensity =      1.667(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.784
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      8.260(CFS)
Total initial stream area =        6.320(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       26.000 to Point/Station       26.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      6.320(Ac.)
Runoff from this stream =      8.260(CFS)
Time of concentration =   14.85 min.
Rainfall intensity =     1.667(In/Hr)


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Process from Point/Station       27.000 to Point/Station       26.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   446.000(Ft.)
Top (of initial area) elevation =  1289.000(Ft.)
Bottom (of initial area) elevation =  1238.000(Ft.)
Difference in elevation =    51.000(Ft.)
Slope =    0.11435  s(percent)=      11.43
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    9.383 min.
Rainfall intensity =      2.097(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.805
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
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Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      1.773(CFS)
Total initial stream area =        1.050(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       26.000 to Point/Station       26.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      1.050(Ac.)
Runoff from this stream =      1.773(CFS)
Time of concentration =    9.38 min.
Rainfall intensity =     2.097(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        8.260     14.85                  1.667
2        1.773      9.38                  2.097
Largest stream flow has longer time of concentration
Qp =      8.260 + sum of
          Qb         Ia/Ib
           1.773 *    0.795 =      1.410
Qp =      9.669

Total of 2 streams to confluence:
Flow rates before confluence point:
       8.260       1.773
Area of streams before confluence:
        6.320        1.050
Results of confluence:
Total flow rate =      9.669(CFS)
Time of concentration =    14.845 min.
Effective stream area after confluence =      7.370(Ac.)
End of computations, total study area =            7.37 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number =  84.4
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
        Rational Hydrology Study        Date: 05/05/25  File:ex100.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

------------------------------------------------------------------------
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =  100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity =  1.300(In/Hr)
Slope of intensity duration curve = 0.5000




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Process from Point/Station        1.000 to Point/Station        2.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   914.000(Ft.)
Top (of initial area) elevation =  1620.000(Ft.)
Bottom (of initial area) elevation =  1572.000(Ft.)
Difference in elevation =    48.000(Ft.)
Slope =    0.05252  s(percent)=       5.25
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.608 min.
Rainfall intensity =      2.635(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.827
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.900
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  85.20
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     20.902(CFS)
Total initial stream area =        9.590(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station        2.000 to Point/Station        3.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of natural channel elevation =   1572.000(Ft.)
End of natural channel elevation =   1444.000(Ft.)
Length of natural channel  =  4065.000(Ft.)
Estimated mean flow rate at midpoint of channel =    118.383(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.86(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0315
Corrected/adjusted channel slope =  0.0315
Travel time =    7.64 min.     TC =   22.25  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.811
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.600
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```
Decimal fraction soil group D = 0.200
RI index for soil(AMC 2)  =  85.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.135(In/Hr) for a   100.0 year storm
Subarea runoff =    154.788(CFS) for     89.450(Ac.)
Total runoff =    175.690(CFS)       Total area =      99.040(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     99.040(Ac.)
Runoff from this stream =    175.690(CFS)
Time of concentration =   22.25 min.
Rainfall intensity =     2.135(In/Hr)


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Process from Point/Station        4.000 to Point/Station        5.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   952.000(Ft.)
Top (of initial area) elevation =  1572.000(Ft.)
Bottom (of initial area) elevation =  1532.000(Ft.)
Difference in elevation =    40.000(Ft.)
Slope =    0.04202  s(percent)=       4.20
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   15.526 min.
Rainfall intensity =      2.556(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.830
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     15.964(CFS)
Total initial stream area =        7.530(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station        5.000 to Point/Station        3.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1532.000(Ft.)
End of natural channel elevation =   1444.000(Ft.)
Length of natural channel  =  2338.000(Ft.)
Estimated mean flow rate at midpoint of channel =     76.786(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.51(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0376
Corrected/adjusted channel slope =  0.0376
Travel time =    4.58 min.     TC =   20.10  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.821
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.246(In/Hr) for a   100.0 year storm
Subarea runoff =    105.760(CFS) for     57.380(Ac.)
Total runoff =    121.723(CFS)       Total area =      64.910(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     64.910(Ac.)
Runoff from this stream =    121.723(CFS)
```

```
Time of concentration =   20.10 min.
Rainfall intensity =     2.246(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      175.690     22.25                 2.135
2      121.723     20.10                 2.246
Largest stream flow has longer time of concentration
Qp =    175.690 + sum of
          Qb         Ia/Ib
         121.723 *    0.950 =    115.695
Qp =    291.385

Total of 2 streams to confluence:
Flow rates before confluence point:
     175.690     121.723
Area of streams before confluence:
       99.040       64.910
Results of confluence:
Total flow rate =    291.385(CFS)
Time of concentration =    22.253 min.
Effective stream area after confluence =    163.950(Ac.)


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Process from Point/Station        3.000 to Point/Station        6.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1444.000(Ft.)
End of natural channel elevation =   1369.000(Ft.)
Length of natural channel  =  2816.000(Ft.)
Estimated mean flow rate at midpoint of channel =    350.693(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  11.41(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0266
Corrected/adjusted channel slope =  0.0266
Travel time =    4.11 min.     TC =   26.36  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.807
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  85.50
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.961(In/Hr) for a   100.0 year storm
Subarea runoff =    105.619(CFS) for     66.740(Ac.)
Total runoff =    397.004(CFS)       Total area =     230.690(Ac.)


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Process from Point/Station        6.000 to Point/Station        6.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    230.690(Ac.)
Runoff from this stream =    397.004(CFS)
Time of concentration =   26.36 min.
Rainfall intensity =     1.961(In/Hr)


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Process from Point/Station        7.000 to Point/Station        8.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   901.000(Ft.)
Top (of initial area) elevation =  1592.000(Ft.)
Bottom (of initial area) elevation =  1516.000(Ft.)
Difference in elevation =    76.000(Ft.)
Slope =    0.08435  s(percent)=       8.44
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.211 min.
Rainfall intensity =      2.770(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
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```
Runoff Coefficient = 0.835
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     10.104(CFS)
Total initial stream area =        4.370(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station        8.000 to Point/Station        6.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1516.000(Ft.)
End of natural channel elevation =   1369.000(Ft.)
Length of natural channel  =  4248.000(Ft.)
Estimated mean flow rate at midpoint of channel =    147.797(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.94(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0346
Corrected/adjusted channel slope =  0.0346
Travel time =    7.12 min.     TC =   20.33  min.


 Adding area flow to channel
UNDEVELOPED (fair cover) subarea
Runoff Coefficient = 0.777
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  79.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.233(In/Hr) for a   100.0 year storm
Subarea runoff =    206.575(CFS) for    119.100(Ac.)
Total runoff =    216.680(CFS)       Total area =     123.470(Ac.)


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Process from Point/Station        6.000 to Point/Station        6.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =    123.470(Ac.)
Runoff from this stream =    216.680(CFS)
Time of concentration =   20.33 min.
Rainfall intensity =     2.233(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      397.004     26.36                 1.961
2      216.680     20.33                 2.233
Largest stream flow has longer time of concentration
Qp =    397.004 + sum of
          Qb         Ia/Ib
         216.680 *    0.878 =    190.292
Qp =    587.296

Total of 2 streams to confluence:
Flow rates before confluence point:
     397.004     216.680
Area of streams before confluence:
      230.690      123.470
Results of confluence:
Total flow rate =    587.296(CFS)
Time of concentration =    26.365 min.
Effective stream area after confluence =    354.160(Ac.)


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Process from Point/Station        6.000 to Point/Station        9.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1369.000(Ft.)
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End of natural channel elevation =   1286.000(Ft.)
Length of natural channel  =  2452.000(Ft.)
Estimated mean flow rate at midpoint of channel =    647.525(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  15.66(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0338
Corrected/adjusted channel slope =  0.0338
Travel time =    2.61 min.     TC =   28.98  min.


 Adding area flow to channel
UNDEVELOPED (fair cover) subarea
Runoff Coefficient = 0.742
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  77.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.871(In/Hr) for a   100.0 year storm
Subarea runoff =    100.833(CFS) for     72.640(Ac.)
Total runoff =    688.129(CFS)       Total area =     426.800(Ac.)


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Process from Point/Station        9.000 to Point/Station       10.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1288.000(Ft.)
End of natural channel elevation =   1221.000(Ft.)
Length of natural channel  =  2462.000(Ft.)
Estimated mean flow rate at midpoint of channel =    752.363(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  14.74(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0272
Corrected/adjusted channel slope =  0.0272
Travel time =    2.78 min.     TC =   31.76  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.805
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.900
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  86.30
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.787(In/Hr) for a   100.0 year storm
Subarea runoff =    114.566(CFS) for     79.680(Ac.)
Total runoff =    802.695(CFS)       Total area =     506.480(Ac.)


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Process from Point/Station       10.000 to Point/Station       10.250
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1221.000(Ft.)
End of natural channel elevation =   1207.000(Ft.)
Length of natural channel  =   710.000(Ft.)
Estimated mean flow rate at midpoint of channel =    806.546(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  12.83(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0197
Corrected/adjusted channel slope =  0.0197
Travel time =    0.92 min.     TC =   32.68  min.
```

```
 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.802
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2)  =  86.10
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.761(In/Hr) for a   100.0 year storm
Subarea runoff =      6.866(CFS) for      4.860(Ac.)
Total runoff =    809.560(CFS)       Total area =     511.340(Ac.)


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Process from Point/Station       10.250 to Point/Station       10.250
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    511.340(Ac.)
Runoff from this stream =    809.560(CFS)
Time of concentration =   32.68 min.
Rainfall intensity =     1.761(In/Hr)


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Process from Point/Station       10.500 to Point/Station       10.500
**** USER DEFINED FLOW INFORMATION AT A POINT ****
______________________________________________________________________________
Rainfall intensity =      2.383(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.810
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
User specified values are as follows:
TC =  17.86 min.  Rain intensity =       2.38(In/Hr)
Total area =        33.20(Ac.)  Total runoff =     67.24(CFS)


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Process from Point/Station       10.500 to Point/Station       10.250
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1249.000(Ft.)
End of natural channel elevation =   1207.000(Ft.)
Length of natural channel  =   932.000(Ft.)
Estimated mean flow rate at midpoint of channel =     72.303(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.15(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0451
Corrected/adjusted channel slope =  0.0451
Travel time =    1.70 min.     TC =   19.56  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.822
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2)  =  86.10
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.277(In/Hr) for a   100.0 year storm
Subarea runoff =      9.361(CFS) for      5.000(Ac.)
Total runoff =     76.601(CFS)       Total area =      38.200(Ac.)


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Process from Point/Station       10.250 to Point/Station       10.250
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     38.200(Ac.)
Runoff from this stream =     76.601(CFS)
Time of concentration =   19.56 min.
```

```
Rainfall intensity =     2.277(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                (In/Hr)


1      809.560     32.68                 1.761
2       76.601     19.56                 2.277
Largest stream flow has longer time of concentration
Qp =    809.560 + sum of
          Qb         Ia/Ib
          76.601 *    0.774 =     59.258
Qp =    868.818

Total of 2 streams to confluence:
Flow rates before confluence point:
     809.560      76.601
Area of streams before confluence:
      511.340       38.200
Results of confluence:
Total flow rate =    868.818(CFS)
Time of concentration =    32.682 min.
Effective stream area after confluence =    549.540(Ac.)


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Process from Point/Station       10.250 to Point/Station       11.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1207.000(Ft.)
End of natural channel elevation =   1169.000(Ft.)
Length of natural channel  =   839.000(Ft.)
Estimated mean flow rate at midpoint of channel =    955.867(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  20.55(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0453
Corrected/adjusted channel slope =  0.0453
Travel time =    0.68 min.     TC =   33.36  min.


 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.882
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2)  =  75.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      1.743(In/Hr) for a   100.0 year storm
Subarea runoff =    169.273(CFS) for    110.120(Ac.)
Total runoff =   1038.091(CFS)       Total area =     659.660(Ac.)


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Process from Point/Station       11.000 to Point/Station       12.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1169.000(Ft.)
End of natural channel elevation =   1139.000(Ft.)
Length of natural channel  =   933.000(Ft.)
Estimated mean flow rate at midpoint of channel =   1062.247(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  17.93(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0322
Corrected/adjusted channel slope =  0.0322
Travel time =    0.87 min.     TC =   34.23  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.796
Decimal fraction soil group A = 0.000
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Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.400
Decimal fraction soil group D = 0.400
RI index for soil(AMC 2)  =  85.60
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.721(In/Hr) for a   100.0 year storm
Subarea runoff =     42.073(CFS) for     30.700(Ac.)
Total runoff =   1080.164(CFS)       Total area =     690.360(Ac.)


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Process from Point/Station       12.000 to Point/Station       12.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =    690.360(Ac.)
Runoff from this stream =   1080.164(CFS)
Time of concentration =   34.23 min.
Rainfall intensity =     1.721(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station       16.000 to Point/Station       17.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   972.000(Ft.)
Top (of initial area) elevation =  1518.000(Ft.)
Bottom (of initial area) elevation =  1451.000(Ft.)
Difference in elevation =    67.000(Ft.)
Slope =    0.06893  s(percent)=       6.89
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.179 min.
Rainfall intensity =      2.674(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.840
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.500
Decimal fraction soil group D = 0.500
RI index for soil(AMC 2)  =  87.50
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     19.277(CFS)
Total initial stream area =        8.580(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station       17.000 to Point/Station       17.100
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1451.000(Ft.)
End of natural channel elevation =   1371.000(Ft.)
Length of natural channel  =  1350.000(Ft.)
Estimated mean flow rate at midpoint of channel =     35.633(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.55(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0593
Corrected/adjusted channel slope =  0.0593
Travel time =    2.63 min.     TC =   16.81  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.820
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.700
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  84.70
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.456(In/Hr) for a   100.0 year storm
Subarea runoff =     29.310(CFS) for     14.560(Ac.)
Total runoff =     48.587(CFS)       Total area =      23.140(Ac.)


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Process from Point/Station       17.100 to Point/Station       17.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
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Upstream point/station elevation =  1371.000(Ft.)
Downstream point/station elevation =  1360.000(Ft.)
Pipe length  =   473.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    48.587(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    48.587(CFS)
Normal flow depth in pipe =   22.88(In.)
Flow top width inside pipe =   19.43(In.)
Critical depth could not be calculated.
Pipe flow velocity =     13.52(Ft/s)
Travel time through pipe =    0.58 min.
Time of concentration (TC) =    17.39 min.


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Process from Point/Station       17.200 to Point/Station       18.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1360.000(Ft.)
End of natural channel elevation =   1347.000(Ft.)
Length of natural channel  =   166.000(Ft.)
Estimated mean flow rate at midpoint of channel =     49.175(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  10.78(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0783
Corrected/adjusted channel slope =  0.0783
Travel time =    0.26 min.     TC =   17.65  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.825
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.397(In/Hr) for a   100.0 year storm
Subarea runoff =      1.108(CFS) for      0.560(Ac.)
Total runoff =     49.695(CFS)       Total area =      23.700(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       18.000 to Point/Station       18.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     23.700(Ac.)
Runoff from this stream =     49.695(CFS)
Time of concentration =   17.65 min.
Rainfall intensity =     2.397(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       19.000 to Point/Station       20.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   687.000(Ft.)
Top (of initial area) elevation =  1478.000(Ft.)
Bottom (of initial area) elevation =  1430.000(Ft.)
Difference in elevation =    48.000(Ft.)
Slope =    0.06987  s(percent)=       6.99
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.308 min.
Rainfall intensity =      2.870(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.837
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     11.888(CFS)
Total initial stream area =        4.950(Ac.)
Pervious area fraction = 1.000
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Process from Point/Station       20.000 to Point/Station       21.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1430.000(Ft.)
End of natural channel elevation =   1400.000(Ft.)
Length of natural channel  =   583.000(Ft.)
Estimated mean flow rate at midpoint of channel =     21.542(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.94(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0515
Corrected/adjusted channel slope =  0.0515
Travel time =    1.40 min.     TC =   13.71  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.833
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.720(In/Hr) for a   100.0 year storm
Subarea runoff =     18.225(CFS) for      8.040(Ac.)
Total runoff =     30.113(CFS)       Total area =      12.990(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       21.000 to Point/Station       18.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1400.000(Ft.)
End of natural channel elevation =   1347.000(Ft.)
Length of natural channel  =  1004.000(Ft.)
Estimated mean flow rate at midpoint of channel =     49.202(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.85(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0528
Corrected/adjusted channel slope =  0.0528
Travel time =    1.89 min.     TC =   15.60  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.829
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.550(In/Hr) for a   100.0 year storm
Subarea runoff =     34.827(CFS) for     16.470(Ac.)
Total runoff =     64.939(CFS)       Total area =      29.460(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       18.000 to Point/Station       18.000
**** CONFLUENCE OF MINOR STREAMS ****
----------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     29.460(Ac.)
Runoff from this stream =     64.939(CFS)
Time of concentration =   15.60 min.
Rainfall intensity =     2.550(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                (In/Hr)


1       49.695     17.65                2.397
```

```
2       64.939     15.60                 2.550
Largest stream flow has longer or shorter time of concentration
Qp =     64.939 + sum of
          Qa          Tb/Ta
          49.695 *    0.884 =     43.923
Qp =    108.862

Total of 2 streams to confluence:
Flow rates before confluence point:
      49.695      64.939
Area of streams before confluence:
       23.700       29.460
Results of confluence:
Total flow rate =    108.862(CFS)
Time of concentration =    15.600 min.
Effective stream area after confluence =     53.160(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       18.000 to Point/Station       15.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1347.000(Ft.)
End of natural channel elevation =   1299.000(Ft.)
Length of natural channel  =  1128.000(Ft.)
Estimated mean flow rate at midpoint of channel =    122.910(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  10.42(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0426
Corrected/adjusted channel slope =  0.0426
Travel time =    1.80 min.     TC =   17.40  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.826
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.414(In/Hr) for a   100.0 year storm
Subarea runoff =     27.346(CFS) for     13.720(Ac.)
Total runoff =    136.208(CFS)       Total area =      66.880(Ac.)


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Process from Point/Station       15.000 to Point/Station       15.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     66.880(Ac.)
Runoff from this stream =    136.208(CFS)
Time of concentration =   17.40 min.
Rainfall intensity =     2.414(In/Hr)


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Process from Point/Station       13.000 to Point/Station       14.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   930.000(Ft.)
Top (of initial area) elevation =  1522.000(Ft.)
Bottom (of initial area) elevation =  1448.000(Ft.)
Difference in elevation =    74.000(Ft.)
Slope =    0.07957  s(percent)=       7.96
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.537 min.
Rainfall intensity =      2.737(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.834
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     15.565(CFS)
Total initial stream area =        6.820(Ac.)
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Pervious area fraction = 1.000

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Process from Point/Station       14.000 to Point/Station       14.100
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1448.000(Ft.)
End of natural channel elevation =   1363.000(Ft.)
Length of natural channel  =  1674.000(Ft.)
Estimated mean flow rate at midpoint of channel =     39.585(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.16(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0508
Corrected/adjusted channel slope =  0.0508
Travel time =    3.42 min.     TC =   16.96  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.819
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.700
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  84.70
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.445(In/Hr) for a   100.0 year storm
Subarea runoff =     42.174(CFS) for     21.050(Ac.)
Total runoff =     57.739(CFS)       Total area =      27.870(Ac.)


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Process from Point/Station       14.100 to Point/Station       14.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1363.000(Ft.)
Downstream point/station elevation =  1359.000(Ft.)
Pipe length  =    86.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    57.739(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    57.739(CFS)
Normal flow depth in pipe =   19.38(In.)
Flow top width inside pipe =   24.30(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.91(Ft/s)
Travel time through pipe =    0.08 min.
Time of concentration (TC) =    17.03 min.


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Process from Point/Station       14.300 to Point/Station       14.400
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.826
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    17.03 min.
Rainfall intensity =      2.440(In/Hr) for a   100.0 year storm
Subarea runoff =     18.048(CFS) for      8.950(Ac.)
Total runoff =     75.787(CFS)       Total area =      36.820(Ac.)


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Process from Point/Station       14.400 to Point/Station       14.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1377.000(Ft.)
Downstream point/station elevation =  1359.000(Ft.)
Pipe length  =   366.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    75.787(CFS)
Nearest computed pipe diameter  =     30.00(In.)
Calculated individual pipe flow  =    75.787(CFS)
Normal flow depth in pipe =   20.91(In.)
Flow top width inside pipe =   27.58(In.)
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Critical depth could not be calculated.
Pipe flow velocity =     20.73(Ft/s)
Travel time through pipe =    0.29 min.
Time of concentration (TC) =    17.33 min.


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Process from Point/Station       14.200 to Point/Station       14.500
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1359.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =    75.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    75.787(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    75.787(CFS)
Normal flow depth in pipe =   24.00(In.)
Flow top width inside pipe =   16.97(In.)
Critical depth could not be calculated.
Pipe flow velocity =     20.30(Ft/s)
Travel time through pipe =    0.06 min.
Time of concentration (TC) =    17.39 min.


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Process from Point/Station       14.500 to Point/Station       14.600
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1355.000(Ft.)
End of natural channel elevation =   1329.000(Ft.)
Length of natural channel  =   406.000(Ft.)
Estimated mean flow rate at midpoint of channel =     79.461(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  11.22(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0640
Corrected/adjusted channel slope =  0.0640
Travel time =    0.60 min.     TC =   17.99  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.825
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.374(In/Hr) for a   100.0 year storm
Subarea runoff =      6.989(CFS) for      3.570(Ac.)
Total runoff =     82.775(CFS)       Total area =      40.390(Ac.)


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Process from Point/Station       14.600 to Point/Station       14.700
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1329.000(Ft.)
Downstream point/station elevation =  1319.000(Ft.)
Pipe length  =   258.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    82.775(CFS)
Nearest computed pipe diameter  =     30.00(In.)
Calculated individual pipe flow  =    82.775(CFS)
Normal flow depth in pipe =   25.31(In.)
Flow top width inside pipe =   21.79(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.72(Ft/s)
Travel time through pipe =    0.23 min.
Time of concentration (TC) =    18.22 min.


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Process from Point/Station       14.700 to Point/Station       15.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1319.000(Ft.)
End of natural channel elevation =   1299.000(Ft.)
Length of natural channel  =   333.000(Ft.)
Estimated mean flow rate at midpoint of channel =     83.800(CFS)
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Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  11.03(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0601
Corrected/adjusted channel slope =  0.0601
Travel time =    0.50 min.     TC =   18.72  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.823
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.327(In/Hr) for a   100.0 year storm
Subarea runoff =      1.916(CFS) for      1.000(Ac.)
Total runoff =     84.691(CFS)       Total area =      41.390(Ac.)


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Process from Point/Station       15.000 to Point/Station       15.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     41.390(Ac.)
Runoff from this stream =     84.691(CFS)
Time of concentration =   18.72 min.
Rainfall intensity =     2.327(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      136.208     17.40                 2.414
2       84.691     18.72                 2.327
Largest stream flow has longer or shorter time of concentration
Qp =    136.208 + sum of
          Qa          Tb/Ta
          84.691 *    0.929 =     78.718
Qp =    214.927

Total of 2 streams to confluence:
Flow rates before confluence point:
     136.208      84.691
Area of streams before confluence:
       66.880       41.390
Results of confluence:
Total flow rate =    214.927(CFS)
Time of concentration =    17.404 min.
Effective stream area after confluence =    108.270(Ac.)


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Process from Point/Station       15.000 to Point/Station       22.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1299.000(Ft.)
End of natural channel elevation =   1215.000(Ft.)
Length of natural channel  =  1781.000(Ft.)
Estimated mean flow rate at midpoint of channel =    287.264(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  14.26(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0472
Corrected/adjusted channel slope =  0.0472
Travel time =    2.08 min.     TC =   19.49  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.812
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
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Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.281(In/Hr) for a   100.0 year storm
Subarea runoff =    135.040(CFS) for     72.880(Ac.)
Total runoff =    349.967(CFS)       Total area =     181.150(Ac.)


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Process from Point/Station       22.000 to Point/Station       23.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1215.000(Ft.)
End of natural channel elevation =   1170.000(Ft.)
Length of natural channel  =  1218.000(Ft.)
Estimated mean flow rate at midpoint of channel =    366.359(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  13.63(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0369
Corrected/adjusted channel slope =  0.0369
Travel time =    1.49 min.     TC =   20.97  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.799
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.400
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  82.80
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.199(In/Hr) for a   100.0 year storm
Subarea runoff =     29.824(CFS) for     16.970(Ac.)
Total runoff =    379.791(CFS)       Total area =     198.120(Ac.)


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Process from Point/Station       23.000 to Point/Station       23.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.804
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Time of concentration =    20.97 min.
Rainfall intensity =      2.199(In/Hr) for a   100.0 year storm
Subarea runoff =    150.248(CFS) for     85.030(Ac.)
Total runoff =    530.039(CFS)       Total area =     283.150(Ac.)


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Process from Point/Station       23.000 to Point/Station       12.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1170.000(Ft.)
End of natural channel elevation =   1139.000(Ft.)
Length of natural channel  =   692.000(Ft.)
Estimated mean flow rate at midpoint of channel =    535.842(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  16.95(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0448
Corrected/adjusted channel slope =  0.0448
Travel time =    0.68 min.     TC =   21.66  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.767
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Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  78.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.164(In/Hr) for a   100.0 year storm
Subarea runoff =     10.287(CFS) for      6.200(Ac.)
Total runoff =    540.326(CFS)       Total area =     289.350(Ac.)


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Process from Point/Station       12.000 to Point/Station       12.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =    289.350(Ac.)
Runoff from this stream =    540.326(CFS)
Time of concentration =   21.66 min.
Rainfall intensity =     2.164(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1     1080.164     34.23               1.721
2      540.326     21.66               2.164
Largest stream flow has longer time of concentration
Qp =   1080.164 + sum of
         Qb          Ia/Ib
        540.326 *    0.795 =    429.772
Qp =   1509.936

Total of 2 main streams to confluence:
Flow rates before confluence point:
    1080.164     540.326
Area of streams before confluence:
      690.360      289.350


Results of confluence:
Total flow rate =   1509.936(CFS)
Time of concentration =    34.229 min.
Effective stream area after confluence  =    979.710(Ac.)


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Process from Point/Station       12.000 to Point/Station       24.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1139.000(Ft.)
End of natural channel elevation =   1136.000(Ft.)
Length of natural channel  =   119.000(Ft.)
Estimated mean flow rate at midpoint of channel =   1510.645(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  17.82(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0252
Corrected/adjusted channel slope =  0.0252
Travel time =    0.11 min.     TC =   34.34  min.
 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.738
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  78.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.718(In/Hr) for a   100.0 year storm
Subarea runoff =      1.167(CFS) for      0.920(Ac.)
Total runoff =   1511.103(CFS)       Total area =     980.630(Ac.)
End of computations, total study area =          980.63 (Ac.)
The following figures maybe used for a unit hydrograph study of the same area.
Area averaged pervious area fraction(Ap) = 0.839
Area averaged RI index number =  80.8
```

```
                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
        Rational Hydrology Study        Date: 05/05/25  File:mcs100.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

------------------------------------------------------------------------
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =  100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity =  1.300(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       25.000 to Point/Station       26.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =  1000.000(Ft.)
Top (of initial area) elevation =  1296.000(Ft.)
Bottom (of initial area) elevation =  1238.000(Ft.)
Difference in elevation =    58.000(Ft.)
Slope =    0.05800  s(percent)=       5.80
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.845 min.
Rainfall intensity =      2.614(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.822
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     13.585(CFS)
Total initial stream area =        6.320(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       26.000 to Point/Station       26.000
**** CONFLUENCE OF MINOR STREAMS ****
____________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      6.320(Ac.)
Runoff from this stream =     13.585(CFS)
Time of concentration =   14.85 min.
Rainfall intensity =     2.614(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       27.000 to Point/Station       26.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   446.000(Ft.)
Top (of initial area) elevation =  1289.000(Ft.)
Bottom (of initial area) elevation =  1238.000(Ft.)
Difference in elevation =    51.000(Ft.)
Slope =    0.11435  s(percent)=      11.43
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    9.383 min.
Rainfall intensity =      3.287(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.837
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
```

```
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      2.890(CFS)
Total initial stream area =        1.050(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       26.000 to Point/Station       26.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      1.050(Ac.)
Runoff from this stream =      2.890(CFS)
Time of concentration =    9.38 min.
Rainfall intensity =     3.287(In/Hr)
Summary of stream data:

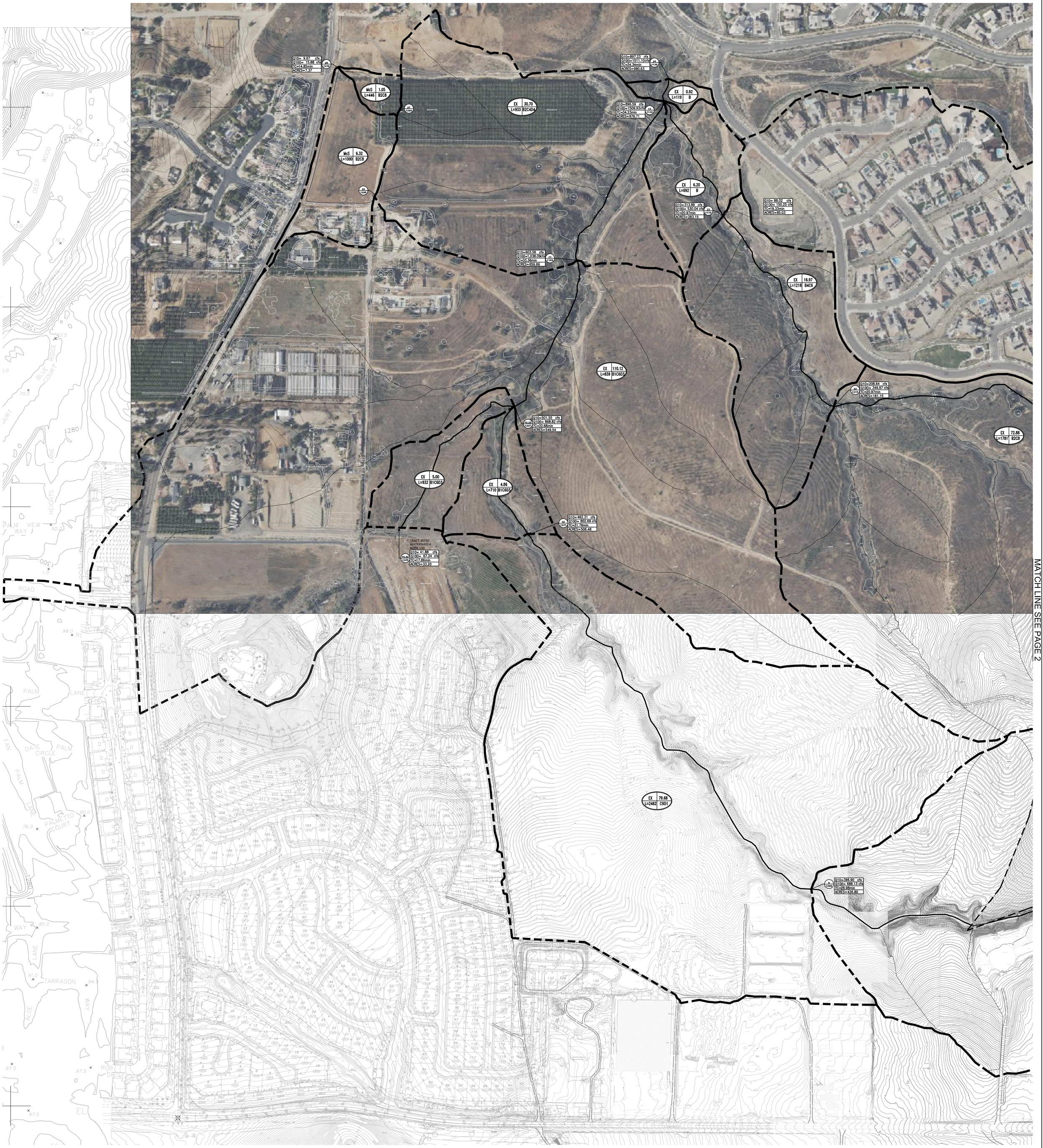
Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       13.585     14.85                 2.614
2        2.890      9.38                 3.287
Largest stream flow has longer time of concentration
Qp =     13.585 + sum of
          Qb         Ia/Ib
           2.890 *    0.795 =      2.298
Qp =     15.882

Total of 2 streams to confluence:
Flow rates before confluence point:
      13.585       2.890
Area of streams before confluence:
        6.320        1.050
Results of confluence:
Total flow rate =     15.882(CFS)
Time of concentration =    14.845 min.
Effective stream area after confluence =      7.370(Ac.)
End of computations, total study area =            7.37 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number =  84.4
```

EXISTING HYDROLOGY MAP



LEGEND

AREA	ACRES
LENGTH	SOIL

NODE / ELEV

Q10=_____ cfs
Q100=_____ cfs
TC=_____min
ACRES=

WATERSHED BOUNDARY

FLOW PATH

0 150 450
75 300 600
SCALE: 1" = 150'

EXISTING HYDROLOGY MAP
PREPARATION DATE : MAY 2016
REVISION DATE : MAY 2025

PLAN PREPARED BY:
adkan ENGINEERS
Civil Engineering • Surveying • Planning
6879 Airport Drive, Riverside, CA 92504
Tel:(951) 688-0241 · Fax:(951) 688-0599

EXISTING HYDROLOGY MAP

MATCH LINE SEE PAGE 1

MATCH LINE ABOVE

MATCH LINE BELOW

EXISTING SITE

LAKE MATHEWS

BLACKBURN ROAD

VISTA DEL LAGO DRIVE

EL SOBRANTE ROAD

ML-90

LEGEND

AREA | ACRES
LENGTH | SOIL

NODE | Q10= cfs
ELEV | Q100= cfs
TC= min
ACRES=

WATERSHED BOUNDARY

FLOW PATH

EXISTING HYDROLOGY MAP
PREPARATION DATE : MAY 2016
REVISION DATE : MAY 2022

SCALE: 1" = 150'

PLAN PREPARED BY:
adkan ENGINEERS
Civil Engineering • Surveying • Planning
6879 Airport Drive, Riverside, CA. 92504
Tel:(951) 688-0241 Fax:(951) 688-0599

Appendix B – Proposed Rational Hydrology Method

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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
        Rational Hydrology Study        Date: 04/30/25  File:pro10.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

------------------------------------------------------------------------
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =   10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year =  10.0
Calculated rainfall intensity data:
1 hour intensity =  0.829(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =  1000.000(Ft.)
Top (of initial area) elevation =  1411.000(Ft.)
Bottom (of initial area) elevation =  1397.000(Ft.)
Difference in elevation =    14.000(Ft.)
Slope =    0.01400  s(percent)=       1.40
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.516 min.
Rainfall intensity =      1.686(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.782
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      9.729(CFS)
Total initial stream area =        7.380(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        2.000 to Point/Station        3.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
____________________________________________________________________________
Upstream point/station elevation =  1397.000(Ft.)
Downstream point/station elevation =  1378.000(Ft.)
Pipe length  =   640.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     9.729(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     9.729(CFS)
Normal flow depth in pipe =   10.86(In.)
Flow top width inside pipe =   13.41(In.)
Critical Depth =   14.12(In.)
Pipe flow velocity =     10.22(Ft/s)
Travel time through pipe =    1.04 min.
Time of concentration (TC) =    15.56 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
____________________________________________________________________________
```

```
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      7.380(Ac.)
Runoff from this stream =      9.729(CFS)
Time of concentration =   15.56 min.
Rainfall intensity =     1.628(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        4.000 to Point/Station        5.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   518.000(Ft.)
Top (of initial area) elevation =  1411.000(Ft.)
Bottom (of initial area) elevation =  1408.500(Ft.)
Difference in elevation =     2.500(Ft.)
Slope =    0.00483  s(percent)=       0.48
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.806 min.
Rainfall intensity =      1.728(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.784
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      6.059(CFS)
Total initial stream area =        4.470(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        5.000 to Point/Station        6.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of street segment elevation =  1408.500(Ft.)
End of street segment elevation =  1384.000(Ft.)
Length of street segment  =  1265.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      8.586(CFS)
Depth of flow =   0.416(Ft.), Average velocity =   3.874(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  14.456(Ft.)
Flow velocity =   3.87(Ft/s)
Travel time =    5.44 min.     TC =   19.25  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.769
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      1.464(In/Hr) for a    10.0 year storm
Subarea runoff =      4.989(CFS) for      4.430(Ac.)
Total runoff =     11.048(CFS)        Total area =       8.900(Ac.)
Street flow at end of street =     11.048(CFS)
Half street flow at end of street =     11.048(CFS)
Depth of flow =   0.446(Ft.), Average velocity =   4.117(Ft/s)
Flow width (from curb towards crown)=  15.990(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        6.000 to Point/Station        3.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1384.000(Ft.)
```

```
Downstream point/station elevation =  1378.000(Ft.)
Pipe length  =    20.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    11.048(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =    11.048(CFS)
Normal flow depth in pipe =    6.46(In.)
Flow top width inside pipe =   11.96(In.)
Critical depth could not be calculated.
Pipe flow velocity =     25.61(Ft/s)
Travel time through pipe =    0.01 min.
Time of concentration (TC) =    19.26 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      8.900(Ac.)
Runoff from this stream =     11.048(CFS)
Time of concentration =   19.26 min.
Rainfall intensity =     1.463(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        2.000 to Point/Station        7.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   702.000(Ft.)
Top (of initial area) elevation =  1397.000(Ft.)
Bottom (of initial area) elevation =  1384.000(Ft.)
Difference in elevation =    13.000(Ft.)
Slope =    0.01852  s(percent)=       1.85
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   11.915 min.
Rainfall intensity =      1.861(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.790
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      8.986(CFS)
Total initial stream area =        6.110(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        7.000 to Point/Station        3.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1384.000(Ft.)
Downstream point/station elevation =  1378.000(Ft.)
Pipe length  =    36.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     8.986(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     8.986(CFS)
Normal flow depth in pipe =    6.82(In.)
Flow top width inside pipe =   11.89(In.)
Critical depth could not be calculated.
Pipe flow velocity =     19.49(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    11.95 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 3
Stream flow area =      6.110(Ac.)
Runoff from this stream =      8.986(CFS)
Time of concentration =   11.95 min.
Rainfall intensity =     1.858(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)
```

```
1        9.729     15.56                 1.628
2       11.048     19.26                 1.463
3        8.986     11.95                 1.858
Largest stream flow has longer time of concentration
Qp =     11.048 + sum of
          Qb         Ia/Ib
           9.729 *    0.899 =      8.744
          Qb         Ia/Ib
           8.986 *    0.788 =      7.076
Qp =     26.868

Total of 3 streams to confluence:
Flow rates before confluence point:
       9.729      11.048       8.986
Area of streams before confluence:
        7.380        8.900        6.110
Results of confluence:
Total flow rate =     26.868(CFS)
Time of concentration =    19.262 min.
Effective stream area after confluence =     22.390(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        8.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1378.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =   334.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    26.868(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =    26.868(CFS)
Normal flow depth in pipe =   14.37(In.)
Flow top width inside pipe =   14.45(In.)
Critical depth could not be calculated.
Pipe flow velocity =     17.78(Ft/s)
Travel time through pipe =    0.31 min.
Time of concentration (TC) =    19.57 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        8.000 to Point/Station        8.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     22.390(Ac.)
Runoff from this stream =     26.868(CFS)
Time of concentration =   19.57 min.
Rainfall intensity =     1.452(In/Hr)
Program is now starting with Main Stream No. 2


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        9.000 to Point/Station       10.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   688.000(Ft.)
Top (of initial area) elevation =  1395.500(Ft.)
Bottom (of initial area) elevation =  1362.000(Ft.)
Difference in elevation =    33.500(Ft.)
Slope =    0.04869  s(percent)=       4.87
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    9.741 min.
Rainfall intensity =      2.058(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.799
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      4.272(CFS)
Total initial stream area =        2.600(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       10.000 to Point/Station       11.000
```

```
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
_____________________________________________________________________
Upstream point/station elevation =  1362.000(Ft.)
Downstream point/station elevation =  1357.000(Ft.)
Pipe length  =    26.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     4.272(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     4.272(CFS)
Normal flow depth in pipe =    4.97(In.)
Flow top width inside pipe =    8.95(In.)
Critical depth could not be calculated.
Pipe flow velocity =     17.09(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =     9.77 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       11.000 to Point/Station       11.000
**** CONFLUENCE OF MINOR STREAMS ****
_____________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      2.600(Ac.)
Runoff from this stream =      4.272(CFS)
Time of concentration =    9.77 min.
Rainfall intensity =     2.055(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        9.000 to Point/Station       12.000
**** INITIAL AREA EVALUATION ****
_____________________________________________________________________
Initial area flow distance =   764.000(Ft.)
Top (of initial area) elevation =  1395.500(Ft.)
Bottom (of initial area) elevation =  1362.000(Ft.)
Difference in elevation =    33.500(Ft.)
Slope =    0.04385  s(percent)=       4.38
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.373 min.
Rainfall intensity =      1.994(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.796
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      3.968(CFS)
Total initial stream area =        2.500(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       12.000 to Point/Station       11.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
_____________________________________________________________________
Upstream point/station elevation =  1362.000(Ft.)
Downstream point/station elevation =  1357.000(Ft.)
Pipe length  =    34.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.968(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     3.968(CFS)
Normal flow depth in pipe =    5.16(In.)
Flow top width inside pipe =    8.90(In.)
Critical depth could not be calculated.
Pipe flow velocity =     15.15(Ft/s)
Travel time through pipe =    0.04 min.
Time of concentration (TC) =    10.41 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       11.000 to Point/Station       11.000
**** CONFLUENCE OF MINOR STREAMS ****
_____________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      2.500(Ac.)
Runoff from this stream =      3.968(CFS)
Time of concentration =   10.41 min.
Rainfall intensity =     1.990(In/Hr)
Summary of stream data:
```

```
Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        4.272      9.77                2.055
2        3.968     10.41                1.990
Largest stream flow has longer or shorter time of concentration
Qp =      4.272 + sum of
          Qa          Tb/Ta
           3.968 *    0.938 =      3.723
Qp =      7.995

Total of 2 streams to confluence:
Flow rates before confluence point:
       4.272       3.968
Area of streams before confluence:
        2.600        2.500
Results of confluence:
Total flow rate =      7.995(CFS)
Time of concentration =     9.766 min.
Effective stream area after confluence =      5.100(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       11.000 to Point/Station        8.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1357.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =   133.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     7.995(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     7.995(CFS)
Normal flow depth in pipe =   10.27(In.)
Flow top width inside pipe =   17.82(In.)
Critical Depth =   13.15(In.)
Pipe flow velocity =      7.68(Ft/s)
Travel time through pipe =    0.29 min.
Time of concentration (TC) =    10.06 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        8.000 to Point/Station        8.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      5.100(Ac.)
Runoff from this stream =      7.995(CFS)
Time of concentration =   10.06 min.
Rainfall intensity =     2.025(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       26.868     19.57                1.452
2        7.995     10.06                2.025
Largest stream flow has longer time of concentration
Qp =     26.868 + sum of
          Qb          Ia/Ib
           7.995 *    0.717 =      5.730
Qp =     32.598

Total of 2 main streams to confluence:
Flow rates before confluence point:
      26.868       7.995
Area of streams before confluence:
       22.390        5.100


Results of confluence:
Total flow rate =     32.598(CFS)
Time of concentration =    19.575 min.
Effective stream area after confluence  =     27.490(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        8.000 to Point/Station       13.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
```

```
Upstream point/station elevation =  1355.000(Ft.)
Downstream point/station elevation =  1350.000(Ft.)
Pipe length  =    77.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    32.598(CFS)
Nearest computed pipe diameter  =     21.00(In.)
Calculated individual pipe flow  =    32.598(CFS)
Normal flow depth in pipe =   14.30(In.)
Flow top width inside pipe =   19.58(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.68(Ft/s)
Travel time through pipe =    0.07 min.
Time of concentration (TC) =    19.64 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       13.000 to Point/Station       14.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.680
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  74.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    19.64 min.
Rainfall intensity =      1.449(In/Hr) for a    10.0 year storm
Subarea runoff =      0.926(CFS) for      0.940(Ac.)
Total runoff =     33.524(CFS)       Total area =      28.430(Ac.)
End of computations, total study area =           28.43 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.517
Area averaged RI index number =  69.2
```

```
                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
        Rational Hydrology Study        Date: 04/30/25  File:pro.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

------------------------------------------------------------------------
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =  100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity =  1.300(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =  1000.000(Ft.)
Top (of initial area) elevation =  1411.000(Ft.)
Bottom (of initial area) elevation =  1397.000(Ft.)
Difference in elevation =    14.000(Ft.)
Slope =    0.01400  s(percent)=       1.40
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.516 min.
Rainfall intensity =      2.643(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.817
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =     15.933(CFS)
Total initial stream area =        7.380(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        2.000 to Point/Station        3.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
____________________________________________________________________________
Upstream point/station elevation =  1397.000(Ft.)
Downstream point/station elevation =  1378.000(Ft.)
Pipe length  =   640.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    15.933(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =    15.933(CFS)
Normal flow depth in pipe =   13.10(In.)
Flow top width inside pipe =   16.02(In.)
Critical Depth =   17.08(In.)
Pipe flow velocity =     11.56(Ft/s)
Travel time through pipe =    0.92 min.
Time of concentration (TC) =    15.44 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
____________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      7.380(Ac.)
Runoff from this stream =     15.933(CFS)
Time of concentration =   15.44 min.
Rainfall intensity =     2.563(In/Hr)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        4.000 to Point/Station        5.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   518.000(Ft.)
Top (of initial area) elevation =  1411.000(Ft.)
Bottom (of initial area) elevation =  1408.500(Ft.)
Difference in elevation =     2.500(Ft.)
Slope =    0.00483  s(percent)=       0.48
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.806 min.
Rainfall intensity =      2.710(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.819
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      9.916(CFS)
Total initial stream area =        4.470(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        5.000 to Point/Station        6.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of street segment elevation =  1408.500(Ft.)
End of street segment elevation =  1384.000(Ft.)
Length of street segment  =  1265.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =     14.139(CFS)
Depth of flow =   0.479(Ft.), Average velocity =   4.371(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  17.629(Ft.)
Flow velocity =   4.37(Ft/s)
Travel time =    4.82 min.     TC =   18.63  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.808
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      2.333(In/Hr) for a   100.0 year storm
Subarea runoff =      8.352(CFS) for      4.430(Ac.)
Total runoff =     18.267(CFS)        Total area =       8.900(Ac.)
Street flow at end of street =     18.267(CFS)
Half street flow at end of street =     18.267(CFS)
Depth of flow =   0.514(Ft.), Average velocity =   4.732(Ft/s)
Warning: depth of flow exceeds top of curb
Note:  depth of flow exceeds top of street crown.
Distance that curb overflow reaches into property =    0.69(Ft.)
Flow width (from curb towards crown)=  18.000(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        6.000 to Point/Station        3.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1384.000(Ft.)
Downstream point/station elevation =  1378.000(Ft.)
Pipe length  =    20.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    18.267(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =    18.267(CFS)
Normal flow depth in pipe =    9.21(In.)
Flow top width inside pipe =   10.14(In.)
```

```
Critical depth could not be calculated.
Pipe flow velocity =     28.24(Ft/s)
Travel time through pipe =    0.01 min.
Time of concentration (TC) =    18.64 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
----------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      8.900(Ac.)
Runoff from this stream =     18.267(CFS)
Time of concentration =   18.64 min.
Rainfall intensity =     2.332(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        2.000 to Point/Station        7.000
**** INITIAL AREA EVALUATION ****
----------------------------------------------------------------------------
Initial area flow distance =   702.000(Ft.)
Top (of initial area) elevation =  1397.000(Ft.)
Bottom (of initial area) elevation =  1384.000(Ft.)
Difference in elevation =    13.000(Ft.)
Slope =    0.01852  s(percent)=       1.85
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   11.915 min.
Rainfall intensity =      2.917(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.823
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =     14.676(CFS)
Total initial stream area =        6.110(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        7.000 to Point/Station        3.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
----------------------------------------------------------------------------
Upstream point/station elevation =  1384.000(Ft.)
Downstream point/station elevation =  1378.000(Ft.)
Pipe length  =    36.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    14.676(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =    14.676(CFS)
Normal flow depth in pipe =    7.99(In.)
Flow top width inside pipe =   14.97(In.)
Critical depth could not be calculated.
Pipe flow velocity =     22.06(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    11.94 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
----------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 3
Stream flow area =      6.110(Ac.)
Runoff from this stream =     14.676(CFS)
Time of concentration =   11.94 min.
Rainfall intensity =     2.914(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       15.933     15.44                 2.563
2       18.267     18.64                 2.332
3       14.676     11.94                 2.914
Largest stream flow has longer time of concentration
Qp =     18.267 + sum of
          Qb         Ia/Ib
          15.933 *    0.910 =     14.500
          Qb         Ia/Ib
          14.676 *    0.800 =     11.746
Qp =     44.514
```

```
Total of 3 streams to confluence:
Flow rates before confluence point:
      15.933      18.267      14.676
Area of streams before confluence:
        7.380       8.900       6.110
Results of confluence:
Total flow rate =     44.514(CFS)
Time of concentration =    18.641 min.
Effective stream area after confluence =     22.390(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        8.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1378.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =   334.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    44.514(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    44.514(CFS)
Normal flow depth in pipe =   15.52(In.)
Flow top width inside pipe =   22.95(In.)
Critical depth could not be calculated.
Pipe flow velocity =     20.74(Ft/s)
Travel time through pipe =    0.27 min.
Time of concentration (TC) =    18.91 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        8.000 to Point/Station        8.000
**** CONFLUENCE OF MAIN STREAMS ****
------------------------------------------------------------------------------
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     22.390(Ac.)
Runoff from this stream =     44.514(CFS)
Time of concentration =   18.91 min.
Rainfall intensity =     2.316(In/Hr)
Program is now starting with Main Stream No. 2


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        9.000 to Point/Station       10.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   688.000(Ft.)
Top (of initial area) elevation =  1395.500(Ft.)
Bottom (of initial area) elevation =  1362.000(Ft.)
Difference in elevation =    33.500(Ft.)
Slope =    0.04869  s(percent)=       4.87
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    9.741 min.
Rainfall intensity =      3.226(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.830
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      6.959(CFS)
Total initial stream area =        2.600(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       10.000 to Point/Station       11.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1362.000(Ft.)
Downstream point/station elevation =  1357.000(Ft.)
Pipe length  =    26.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     6.959(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     6.959(CFS)
Normal flow depth in pipe =    7.07(In.)
Flow top width inside pipe =    7.39(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.70(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =     9.76 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
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```
Process from Point/Station       11.000 to Point/Station       11.000
**** CONFLUENCE OF MINOR STREAMS ****
____________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      2.600(Ac.)
Runoff from this stream =      6.959(CFS)
Time of concentration =    9.76 min.
Rainfall intensity =     3.223(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        9.000 to Point/Station       12.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   764.000(Ft.)
Top (of initial area) elevation =  1395.500(Ft.)
Bottom (of initial area) elevation =  1362.000(Ft.)
Difference in elevation =    33.500(Ft.)
Slope =    0.04385  s(percent)=       4.38
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.373 min.
Rainfall intensity =      3.127(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.828
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      6.469(CFS)
Total initial stream area =        2.500(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       12.000 to Point/Station       11.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
____________________________________________________________________________
Upstream point/station elevation =  1362.000(Ft.)
Downstream point/station elevation =  1357.000(Ft.)
Pipe length  =    34.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     6.469(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     6.469(CFS)
Normal flow depth in pipe =    5.81(In.)
Flow top width inside pipe =   11.99(In.)
Critical depth could not be calculated.
Pipe flow velocity =     17.16(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    10.41 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       11.000 to Point/Station       11.000
**** CONFLUENCE OF MINOR STREAMS ****
____________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      2.500(Ac.)
Runoff from this stream =      6.469(CFS)
Time of concentration =   10.41 min.
Rainfall intensity =     3.122(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        6.959      9.76                 3.223
2        6.469     10.41                 3.122
Largest stream flow has longer or shorter time of concentration
Qp =      6.959 + sum of
          Qa          Tb/Ta
           6.469 *    0.938 =      6.070
Qp =     13.029

Total of 2 streams to confluence:
Flow rates before confluence point:
       6.959       6.469
Area of streams before confluence:
        2.600        2.500
Results of confluence:
Total flow rate =     13.029(CFS)
Time of concentration =     9.764 min.
Effective stream area after confluence =      5.100(Ac.)
```

```
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       11.000 to Point/Station        8.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1357.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =   133.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    13.029(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =    13.029(CFS)
Normal flow depth in pipe =   14.95(In.)
Flow top width inside pipe =   13.50(In.)
Critical Depth =   16.21(In.)
Pipe flow velocity =      8.31(Ft/s)
Travel time through pipe =    0.27 min.
Time of concentration (TC) =    10.03 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        8.000 to Point/Station        8.000
**** CONFLUENCE OF MAIN STREAMS ****
------------------------------------------------------------------------------
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      5.100(Ac.)
Runoff from this stream =     13.029(CFS)
Time of concentration =   10.03 min.
Rainfall intensity =     3.179(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       44.514     18.91               2.316
2       13.029     10.03               3.179
Largest stream flow has longer time of concentration
Qp =     44.514 + sum of
          Qb          Ia/Ib
          13.029 *    0.728 =      9.489
Qp =     54.003

Total of 2 main streams to confluence:
Flow rates before confluence point:
      44.514      13.029
Area of streams before confluence:
       22.390        5.100


Results of confluence:
Total flow rate =     54.003(CFS)
Time of concentration =    18.910 min.
Effective stream area after confluence  =     27.490(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        8.000 to Point/Station       13.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1355.000(Ft.)
Downstream point/station elevation =  1350.000(Ft.)
Pipe length  =    77.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    54.003(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    54.003(CFS)
Normal flow depth in pipe =   18.42(In.)
Flow top width inside pipe =   20.27(In.)
Critical depth could not be calculated.
Pipe flow velocity =     20.86(Ft/s)
Travel time through pipe =    0.06 min.
Time of concentration (TC) =    18.97 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       13.000 to Point/Station       14.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.748
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  74.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
```

```
Time of concentration =    18.97 min.
Rainfall intensity =      2.312(In/Hr) for a   100.0 year storm
Subarea runoff =      1.626(CFS) for      0.940(Ac.)
Total runoff =     55.629(CFS)       Total area =      28.430(Ac.)
End of computations, total study area =           28.43 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.517
Area averaged RI index number =  69.2
```

PROPOSED RATIONAL HYDROLOGY MAP



0 100 300
50 200 400
SCALE: 1" = 100'

LEGEND

NODE / ELEV

AREA | ACRES
LENGTH | SOIL

WATERSHED BOUNDARY

FLOW PATH

PROPOSED RATIONAL HYDROLOGY MAP
PREPARATION DATE: SEPTEMBER 2024
REVISION DATE: DECEMBER 2024
JOB NUMBER: 10615

PLAN PREPARED BY:
adkan ENGINEERS
Civil Engineering • Surveying • Planning
6879 Airport Drive, Riverside, CA 92504
Tel:(951) 688-0241 Fax:(951) 688-0599

Appendix C – Existing Synthetic Unit Hydrograph Method

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2008, Version 8.1
Study date 04/30/25 File: ex212.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.50	14.22

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.30	36.96

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.300(In)

Point rain (area averaged) = 0.500(In)
Areal adjustment factor = 99.97 %
Adjusted average point rain = 0.500(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

Slope of intensity-duration curve for a 1 hour storm =0.5500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time		Pattern	Storm Rain	Loss rate(In./Hr)		Effective
	(Hr.)	Percent	(In/Hr)	Max	Low	(In/Hr)
1	0.08	3.30	0.198	(0.246)	0.178	0.020
2	0.17	4.20	0.252	(0.246)	0.227	0.025
3	0.25	4.40	0.264	(0.246)	0.238	0.026
4	0.33	4.80	0.288	0.246	(0.259)	0.042
5	0.42	5.20	0.312	0.246	(0.281)	0.066
6	0.50	6.20	0.372	0.246	(0.335)	0.126
7	0.58	6.80	0.408	0.246	(0.367)	0.162
8	0.67	8.80	0.528	0.246	(0.475)	0.282
9	0.75	13.90	0.834	0.246	(0.750)	0.587
10	0.83	31.40	1.884	0.246	(1.695)	1.637
11	0.92	7.20	0.432	0.246	(0.389)	0.186
12	1.00	3.80	0.228	(0.246)	0.205	0.023
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	3.2

Flood volume = Effective rainfall 0.26(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 0.6(Ac.Ft)
Total soil loss = 0.23(In)
Total soil loss = 0.556(Ac.Ft)
Total rainfall = 0.50(In)
Flood volume = 27348.2 Cubic Feet
Total soil loss = 24239.0 Cubic Feet

Peak flow rate of this hydrograph = 26.924(CFS)

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0015	0.22	Q				
0+10	0.0052	0.54	Q				
0+15	0.0099	0.68	Q				
0+20	0.0161	0.90	|Q				
0+25	0.0256	1.38	|Q				
0+30	0.0422	2.41	| VQ				
0+35	0.0675	3.67	| Q				
0+40	0.1067	5.69	| VQ				
0+45	0.1813	10.84	|	V Q			
0+50	0.3667	26.92	|	|	V	Q	
0+55	0.5410	25.31	|	|	|	QV	
1+ 0	0.5970	8.12	|	Q	|		V |
1+ 5	0.6182	3.08	| Q	|	|		V|
1+10	0.6268	1.25	|Q	|	|		V|
1+15	0.6277	0.14	Q	|	|		V|
1+20	0.6278	0.01	Q	|	|		V

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex232.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.80	22.74

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	2.00	56.86

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 0.800(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 0.800(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.125	(0.246)	0.112	0.012
2	0.17	1.30	0.125	(0.246)	0.112	0.012
3	0.25	1.10	0.106	(0.246)	0.095	0.011
4	0.33	1.50	0.144	(0.246)	0.130	0.014
5	0.42	1.50	0.144	(0.246)	0.130	0.014
6	0.50	1.80	0.173	(0.246)	0.156	0.017
7	0.58	1.50	0.144	(0.246)	0.130	0.014
8	0.67	1.80	0.173	(0.246)	0.156	0.017
9	0.75	1.80	0.173	(0.246)	0.156	0.017
10	0.83	1.50	0.144	(0.246)	0.130	0.014
11	0.92	1.60	0.154	(0.246)	0.138	0.015
12	1.00	1.80	0.173	(0.246)	0.156	0.017
13	1.08	2.20	0.211	(0.246)	0.190	0.021
14	1.17	2.20	0.211	(0.246)	0.190	0.021
15	1.25	2.20	0.211	(0.246)	0.190	0.021
16	1.33	2.00	0.192	(0.246)	0.173	0.019
17	1.42	2.60	0.250	(0.246)	0.225	0.025
18	1.50	2.70	0.259	(0.246)	0.233	0.026
19	1.58	2.40	0.230	(0.246)	0.207	0.023
20	1.67	2.70	0.259	(0.246)	0.233	0.026
21	1.75	3.30	0.317	0.246	(0.285)	0.070
22	1.83	3.10	0.298	0.246	(0.268)	0.051
23	1.92	2.90	0.278	0.246	(0.251)	0.032
24	2.00	3.00	0.288	0.246	(0.259)	0.042
25	2.08	3.10	0.298	0.246	(0.268)	0.051
26	2.17	4.20	0.403	0.246	(0.363)	0.157
27	2.25	5.00	0.480	0.246	(0.432)	0.234
28	2.33	3.50	0.336	0.246	(0.302)	0.090
29	2.42	6.80	0.653	0.246	(0.587)	0.406
30	2.50	7.30	0.701	0.246	(0.631)	0.454
31	2.58	8.20	0.787	0.246	(0.708)	0.541
32	2.67	5.90	0.566	0.246	(0.510)	0.320
33	2.75	2.00	0.192	(0.246)	0.173	0.019
34	2.83	1.80	0.173	(0.246)	0.156	0.017
35	2.92	1.80	0.173	(0.246)	0.156	0.017
36	3.00	0.60	0.058	(0.246)	0.052	0.006
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	2.9

Flood volume = Effective rainfall 0.24(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 0.6(Ac.Ft)
Total soil loss = 0.56(In)
Total soil loss = 1.329(Ac.Ft)
Total rainfall = 0.80(In)
Flood volume = 24658.8 Cubic Feet
Total soil loss = 57891.7 Cubic Feet

Peak flow rate of this hydrograph = 13.297(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0010	0.14	Q				
0+10	0.0030	0.30	Q				
0+15	0.0052	0.31	Q				
0+20	0.0076	0.35	Q				
0+25	0.0103	0.40	Q				
0+30	0.0134	0.44	Q				
0+35	0.0164	0.45	QV				
0+40	0.0196	0.45	QV				
0+45	0.0229	0.49	QV				
0+50	0.0261	0.46	QV				
0+55	0.0291	0.43	Q V				
1+ 0	0.0322	0.46	Q V				
1+ 5	0.0359	0.53	|QV				
1+10	0.0399	0.58	|QV				

```
    1+15       0.0440      0.60  |Q V      |          |          |          |
    1+20       0.0480      0.58  |Q V      |          |          |          |
    1+25       0.0523      0.62  |Q V      |          |          |          |
    1+30       0.0572      0.70  |Q  V     |          |          |          |
    1+35       0.0620      0.70  |Q  V     |          |          |          |
    1+40       0.0668      0.70  |Q  V     |          |          |          |
    1+45       0.0753      1.23  | Q  V    |          |          |          |
    1+50       0.0863      1.60  |   Q  V  |          |          |          |
    1+55       0.0950      1.26  | Q   V   |          |          |          |
    2+ 0       0.1027      1.12  | Q    V  |          |          |          |
    2+ 5       0.1116      1.30  | Q    V  |          |          |          |
    2+10       0.1295      2.60  |    Q   V|          |          |          |
    2+15       0.1629      4.85  |         Q|V         |          |          |
    2+20       0.1942      4.55  |          Q|  V       |          |          |
    2+25       0.2394      6.57  |           |  Q  V    |          |          |
    2+30       0.3148     10.94  |           |          |QV        |          |
    2+35       0.4063     13.30  |           |          |     Q V  |          |
    2+40       0.4915     12.37  |           |          |   Q      |   V      |
    2+45       0.5373      6.65  |           |  Q       |          |      V   |
    2+50       0.5528      2.24  |   Q       |          |          |        V |
    2+55       0.5608      1.16  | Q         |          |          |        V |
    3+ 0       0.5646      0.55  |Q          |          |          |        V |
    3+ 5       0.5656      0.15  Q           |          |          |        V |
    3+10       0.5659      0.05  Q           |          |          |        V |
    3+15       0.5661      0.02  Q           |          |          |        V |
    3+20       0.5661      0.00  Q           |          |          |         V
-------------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex262.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.10	31.27

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	3.00	85.29

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.100(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.100(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.066	(0.246)	0.059	0.007
2	0.17	0.60	0.079	(0.246)	0.071	0.008
3	0.25	0.60	0.079	(0.246)	0.071	0.008
4	0.33	0.60	0.079	(0.246)	0.071	0.008
5	0.42	0.60	0.079	(0.246)	0.071	0.008
6	0.50	0.70	0.092	(0.246)	0.083	0.009
7	0.58	0.70	0.092	(0.246)	0.083	0.009
8	0.67	0.70	0.092	(0.246)	0.083	0.009
9	0.75	0.70	0.092	(0.246)	0.083	0.009
10	0.83	0.70	0.092	(0.246)	0.083	0.009
11	0.92	0.70	0.092	(0.246)	0.083	0.009
12	1.00	0.80	0.106	(0.246)	0.095	0.011
13	1.08	0.80	0.106	(0.246)	0.095	0.011
14	1.17	0.80	0.106	(0.246)	0.095	0.011
15	1.25	0.80	0.106	(0.246)	0.095	0.011
16	1.33	0.80	0.106	(0.246)	0.095	0.011
17	1.42	0.80	0.106	(0.246)	0.095	0.011
18	1.50	0.80	0.106	(0.246)	0.095	0.011
19	1.58	0.80	0.106	(0.246)	0.095	0.011
20	1.67	0.80	0.106	(0.246)	0.095	0.011
21	1.75	0.80	0.106	(0.246)	0.095	0.011
22	1.83	0.80	0.106	(0.246)	0.095	0.011
23	1.92	0.80	0.106	(0.246)	0.095	0.011
24	2.00	0.90	0.119	(0.246)	0.107	0.012
25	2.08	0.80	0.106	(0.246)	0.095	0.011
26	2.17	0.90	0.119	(0.246)	0.107	0.012
27	2.25	0.90	0.119	(0.246)	0.107	0.012
28	2.33	0.90	0.119	(0.246)	0.107	0.012
29	2.42	0.90	0.119	(0.246)	0.107	0.012
30	2.50	0.90	0.119	(0.246)	0.107	0.012
31	2.58	0.90	0.119	(0.246)	0.107	0.012
32	2.67	0.90	0.119	(0.246)	0.107	0.012
33	2.75	1.00	0.132	(0.246)	0.119	0.013
34	2.83	1.00	0.132	(0.246)	0.119	0.013
35	2.92	1.00	0.132	(0.246)	0.119	0.013
36	3.00	1.00	0.132	(0.246)	0.119	0.013
37	3.08	1.00	0.132	(0.246)	0.119	0.013
38	3.17	1.10	0.145	(0.246)	0.131	0.015
39	3.25	1.10	0.145	(0.246)	0.131	0.015
40	3.33	1.10	0.145	(0.246)	0.131	0.015
41	3.42	1.20	0.158	(0.246)	0.143	0.016
42	3.50	1.30	0.172	(0.246)	0.154	0.017
43	3.58	1.40	0.185	(0.246)	0.166	0.018
44	3.67	1.40	0.185	(0.246)	0.166	0.018
45	3.75	1.50	0.198	(0.246)	0.178	0.020
46	3.83	1.50	0.198	(0.246)	0.178	0.020
47	3.92	1.60	0.211	(0.246)	0.190	0.021
48	4.00	1.60	0.211	(0.246)	0.190	0.021
49	4.08	1.70	0.224	(0.246)	0.202	0.022
50	4.17	1.80	0.238	(0.246)	0.214	0.024
51	4.25	1.90	0.251	(0.246)	0.226	0.025
52	4.33	2.00	0.264	(0.246)	0.238	0.026
53	4.42	2.10	0.277	0.246	(0.249)	0.031
54	4.50	2.10	0.277	0.246	(0.249)	0.031
55	4.58	2.20	0.290	0.246	(0.261)	0.044
56	4.67	2.30	0.304	0.246	(0.273)	0.057
57	4.75	2.40	0.317	0.246	(0.285)	0.070
58	4.83	2.40	0.317	0.246	(0.285)	0.070
59	4.92	2.50	0.330	0.246	(0.297)	0.084
60	5.00	2.60	0.343	0.246	(0.309)	0.097
61	5.08	3.10	0.409	0.246	(0.368)	0.163
62	5.17	3.60	0.475	0.246	(0.428)	0.229
63	5.25	3.90	0.515	0.246	(0.463)	0.268
64	5.33	4.20	0.554	0.246	(0.499)	0.308
65	5.42	4.70	0.620	0.246	(0.558)	0.374
66	5.50	5.60	0.739	0.246	(0.665)	0.493
67	5.58	1.90	0.251	(0.246)	0.226	0.025
68	5.67	0.90	0.119	(0.246)	0.107	0.012
69	5.75	0.60	0.079	(0.246)	0.071	0.008
70	5.83	0.50	0.066	(0.246)	0.059	0.007
71	5.92	0.30	0.040	(0.246)	0.036	0.004

```
72   6.00     0.20      0.026       (  0.246)       0.024        0.003
            (Loss Rate Not Used)
   Sum =     100.0                                    Sum =     3.1
      Flood volume = Effective rainfall      0.26(In)
       times area      28.4(Ac.)/[(In)/(Ft.)] =       0.6(Ac.Ft)
      Total soil loss =      0.84(In)
      Total soil loss =     2.001(Ac.Ft)
      Total rainfall =      1.10(In)
      Flood volume =       26332.4 Cubic Feet
      Total soil loss =       87177.5 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     11.651(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
-------------------------------------------------------------------------
  0+ 5       0.0005      0.07  Q          |          |          |          |
  0+10       0.0017      0.17  Q          |          |          |          |
  0+15       0.0031      0.21  Q          |          |          |          |
  0+20       0.0047      0.22  Q          |          |          |          |
  0+25       0.0062      0.23  Q          |          |          |          |
  0+30       0.0079      0.24  Q          |          |          |          |
  0+35       0.0097      0.26  Q          |          |          |          |
  0+40       0.0115      0.26  Q          |          |          |          |
  0+45       0.0133      0.26  Q          |          |          |          |
  0+50       0.0151      0.26  QV         |          |          |          |
  0+55       0.0169      0.26  QV         |          |          |          |
  1+ 0       0.0189      0.28  QV         |          |          |          |
  1+ 5       0.0209      0.30  QV         |          |          |          |
  1+10       0.0230      0.30  QV         |          |          |          |
  1+15       0.0251      0.30  QV         |          |          |          |
  1+20       0.0271      0.30  QV         |          |          |          |
  1+25       0.0292      0.30  QV         |          |          |          |
  1+30       0.0313      0.30  Q V        |          |          |          |
  1+35       0.0334      0.30  Q V        |          |          |          |
  1+40       0.0355      0.30  Q V        |          |          |          |
  1+45       0.0376      0.30  Q V        |          |          |          |
  1+50       0.0397      0.30  Q V        |          |          |          |
  1+55       0.0417      0.30  Q V        |          |          |          |
  2+ 0       0.0439      0.32  Q V        |          |          |          |
  2+ 5       0.0461      0.32  Q  V       |          |          |          |
  2+10       0.0483      0.32  Q  V       |          |          |          |
  2+15       0.0507      0.34  Q  V       |          |          |          |
  2+20       0.0530      0.34  Q  V       |          |          |          |
  2+25       0.0553      0.34  Q  V       |          |          |          |
  2+30       0.0577      0.34  Q  V       |          |          |          |
  2+35       0.0600      0.34  Q  V       |          |          |          |
  2+40       0.0624      0.34  Q   V      |          |          |          |
  2+45       0.0648      0.36  Q   V      |          |          |          |
  2+50       0.0674      0.37  Q   V      |          |          |          |
  2+55       0.0700      0.38  Q   V      |          |          |          |
  3+ 0       0.0726      0.38  Q   V      |          |          |          |
  3+ 5       0.0752      0.38  Q   V      |          |          |          |
  3+10       0.0779      0.39  Q    V     |          |          |          |
  3+15       0.0807      0.41  Q    V     |          |          |          |
  3+20       0.0836      0.41  Q    V     |          |          |          |
  3+25       0.0865      0.43  Q    V     |          |          |          |
  3+30       0.0897      0.46  Q    V     |          |          |          |
  3+35       0.0931      0.50  Q     V    |          |          |          |
  3+40       0.0967      0.52  |Q    V     |          |          |          |
  3+45       0.1004      0.54  |Q    V     |          |          |          |
  3+50       0.1043      0.56  |Q    V     |          |          |          |
  3+55       0.1083      0.58  |Q     V    |          |          |          |
  4+ 0       0.1124      0.60  |Q     V    |          |          |          |
  4+ 5       0.1167      0.62  |Q     V    |          |          |          |
  4+10       0.1212      0.65  |Q      V   |          |          |          |
  4+15       0.1259      0.69  |Q      V   |          |          |          |
  4+20       0.1309      0.72  |Q      V   |          |          |          |
  4+25       0.1364      0.80  |Q       V  |          |          |          |
  4+30       0.1423      0.86  |Q       V  |          |          |          |
  4+35       0.1493      1.02  | Q      V  |          |          |          |
  4+40       0.1586      1.35  | Q       V |          |          |          |
  4+45       0.1703      1.70  |  Q      |V          |          |          |
  4+50       0.1836      1.93  |  Q      | V         |          |          |
  4+55       0.1983      2.13  |   Q     |  V        |          |          |
  5+ 0       0.2154      2.48  |   Q     |   V       |          |          |
  5+ 5       0.2390      3.43  |     Q   |    V      |          |          |
  5+10       0.2739      5.07  |         Q       V   |          |          |
  5+15       0.3192      6.57  |         |  Q       |V         |          |
  5+20       0.3729      7.80  |         |    Q     |   V      |          |
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    5+25       0.4368      9.28  |          |        Q |        V |          |
    5+30       0.5170     11.65  |          |          |  Q       |   V      |
    5+35       0.5736      8.22  |          |      Q   |          |      V   |
    5+40       0.5906      2.47  |    Q     |          |          |        V |
    5+45       0.5983      1.11  |  Q       |          |          |        V |
    5+50       0.6019      0.53  | Q        |          |          |        V |
    5+55       0.6032      0.18  Q          |          |          |        V |
    6+ 0       0.6040      0.12  Q          |          |          |        V |
    6+ 5       0.6044      0.06  Q          |          |          |        V |
    6+10       0.6045      0.02  Q          |          |          |        V |
    6+15       0.6045      0.01  Q          |          |          |        V |
    6+20       0.6045      0.00  Q          |          |          |         V
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex2242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.80	51.17

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	5.00	142.15

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 1.800(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.800(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.014	(0.437)	0.013	0.001
2	0.17	0.07	0.014	(0.435)	0.013	0.001
3	0.25	0.07	0.014	(0.433)	0.013	0.001
4	0.33	0.10	0.022	(0.432)	0.019	0.002
5	0.42	0.10	0.022	(0.430)	0.019	0.002
6	0.50	0.10	0.022	(0.428)	0.019	0.002
7	0.58	0.10	0.022	(0.427)	0.019	0.002
8	0.67	0.10	0.022	(0.425)	0.019	0.002
9	0.75	0.10	0.022	(0.423)	0.019	0.002
10	0.83	0.13	0.029	(0.422)	0.026	0.003
11	0.92	0.13	0.029	(0.420)	0.026	0.003
12	1.00	0.13	0.029	(0.418)	0.026	0.003
13	1.08	0.10	0.022	(0.417)	0.019	0.002
14	1.17	0.10	0.022	(0.415)	0.019	0.002
15	1.25	0.10	0.022	(0.413)	0.019	0.002
16	1.33	0.10	0.022	(0.412)	0.019	0.002
17	1.42	0.10	0.022	(0.410)	0.019	0.002
18	1.50	0.10	0.022	(0.408)	0.019	0.002
19	1.58	0.10	0.022	(0.407)	0.019	0.002
20	1.67	0.10	0.022	(0.405)	0.019	0.002
21	1.75	0.10	0.022	(0.404)	0.019	0.002
22	1.83	0.13	0.029	(0.402)	0.026	0.003
23	1.92	0.13	0.029	(0.400)	0.026	0.003
24	2.00	0.13	0.029	(0.399)	0.026	0.003
25	2.08	0.13	0.029	(0.397)	0.026	0.003
26	2.17	0.13	0.029	(0.395)	0.026	0.003
27	2.25	0.13	0.029	(0.394)	0.026	0.003
28	2.33	0.13	0.029	(0.392)	0.026	0.003
29	2.42	0.13	0.029	(0.391)	0.026	0.003
30	2.50	0.13	0.029	(0.389)	0.026	0.003
31	2.58	0.17	0.036	(0.387)	0.032	0.004
32	2.67	0.17	0.036	(0.386)	0.032	0.004
33	2.75	0.17	0.036	(0.384)	0.032	0.004
34	2.83	0.17	0.036	(0.383)	0.032	0.004
35	2.92	0.17	0.036	(0.381)	0.032	0.004
36	3.00	0.17	0.036	(0.380)	0.032	0.004
37	3.08	0.17	0.036	(0.378)	0.032	0.004
38	3.17	0.17	0.036	(0.376)	0.032	0.004
39	3.25	0.17	0.036	(0.375)	0.032	0.004
40	3.33	0.17	0.036	(0.373)	0.032	0.004
41	3.42	0.17	0.036	(0.372)	0.032	0.004
42	3.50	0.17	0.036	(0.370)	0.032	0.004
43	3.58	0.17	0.036	(0.369)	0.032	0.004
44	3.67	0.17	0.036	(0.367)	0.032	0.004
45	3.75	0.17	0.036	(0.366)	0.032	0.004
46	3.83	0.20	0.043	(0.364)	0.039	0.004
47	3.92	0.20	0.043	(0.362)	0.039	0.004
48	4.00	0.20	0.043	(0.361)	0.039	0.004
49	4.08	0.20	0.043	(0.359)	0.039	0.004
50	4.17	0.20	0.043	(0.358)	0.039	0.004
51	4.25	0.20	0.043	(0.356)	0.039	0.004
52	4.33	0.23	0.050	(0.355)	0.045	0.005
53	4.42	0.23	0.050	(0.353)	0.045	0.005
54	4.50	0.23	0.050	(0.352)	0.045	0.005
55	4.58	0.23	0.050	(0.350)	0.045	0.005
56	4.67	0.23	0.050	(0.349)	0.045	0.005
57	4.75	0.23	0.050	(0.347)	0.045	0.005
58	4.83	0.27	0.058	(0.346)	0.052	0.006
59	4.92	0.27	0.058	(0.344)	0.052	0.006
60	5.00	0.27	0.058	(0.343)	0.052	0.006
61	5.08	0.20	0.043	(0.341)	0.039	0.004
62	5.17	0.20	0.043	(0.340)	0.039	0.004
63	5.25	0.20	0.043	(0.338)	0.039	0.004
64	5.33	0.23	0.050	(0.337)	0.045	0.005
65	5.42	0.23	0.050	(0.335)	0.045	0.005
66	5.50	0.23	0.050	(0.334)	0.045	0.005
67	5.58	0.27	0.058	(0.332)	0.052	0.006
68	5.67	0.27	0.058	(0.331)	0.052	0.006
69	5.75	0.27	0.058	(0.330)	0.052	0.006
70	5.83	0.27	0.058	(0.328)	0.052	0.006
71	5.92	0.27	0.058	(0.327)	0.052	0.006

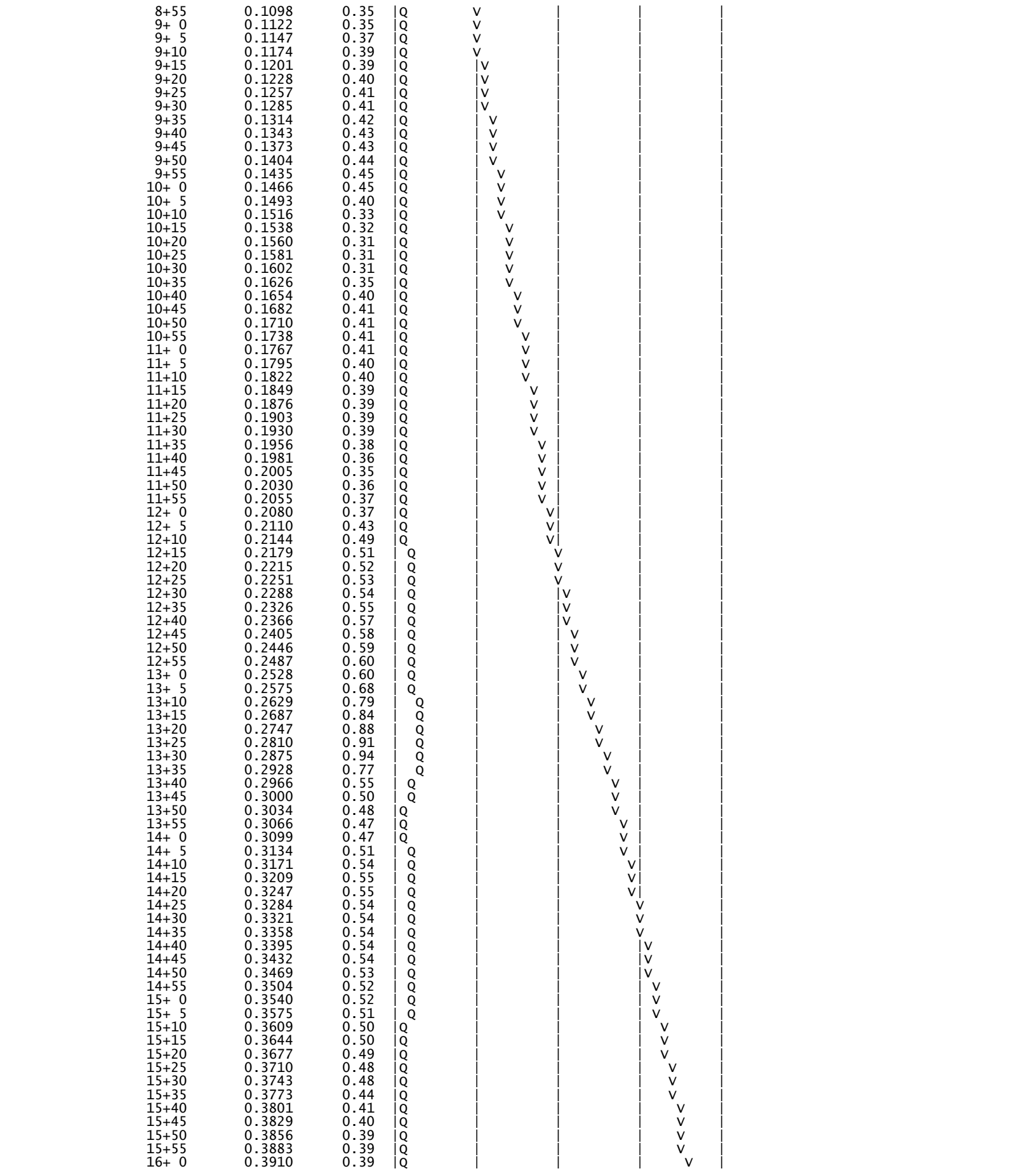
72	6.00	0.27	0.058	(0.325)	0.052	0.006
73	6.08	0.30	0.065	(0.324)	0.058	0.006
74	6.17	0.30	0.065	(0.322)	0.058	0.006
75	6.25	0.30	0.065	(0.321)	0.058	0.006
76	6.33	0.30	0.065	(0.319)	0.058	0.006
77	6.42	0.30	0.065	(0.318)	0.058	0.006
78	6.50	0.30	0.065	(0.317)	0.058	0.006
79	6.58	0.33	0.072	(0.315)	0.065	0.007
80	6.67	0.33	0.072	(0.314)	0.065	0.007
81	6.75	0.33	0.072	(0.312)	0.065	0.007
82	6.83	0.33	0.072	(0.311)	0.065	0.007
83	6.92	0.33	0.072	(0.310)	0.065	0.007
84	7.00	0.33	0.072	(0.308)	0.065	0.007
85	7.08	0.33	0.072	(0.307)	0.065	0.007
86	7.17	0.33	0.072	(0.305)	0.065	0.007
87	7.25	0.33	0.072	(0.304)	0.065	0.007
88	7.33	0.37	0.079	(0.303)	0.071	0.008
89	7.42	0.37	0.079	(0.301)	0.071	0.008
90	7.50	0.37	0.079	(0.300)	0.071	0.008
91	7.58	0.40	0.086	(0.298)	0.078	0.009
92	7.67	0.40	0.086	(0.297)	0.078	0.009
93	7.75	0.40	0.086	(0.296)	0.078	0.009
94	7.83	0.43	0.094	(0.294)	0.084	0.009
95	7.92	0.43	0.094	(0.293)	0.084	0.009
96	8.00	0.43	0.094	(0.292)	0.084	0.009
97	8.08	0.50	0.108	(0.290)	0.097	0.011
98	8.17	0.50	0.108	(0.289)	0.097	0.011
99	8.25	0.50	0.108	(0.288)	0.097	0.011
100	8.33	0.50	0.108	(0.286)	0.097	0.011
101	8.42	0.50	0.108	(0.285)	0.097	0.011
102	8.50	0.50	0.108	(0.283)	0.097	0.011
103	8.58	0.53	0.115	(0.282)	0.104	0.012
104	8.67	0.53	0.115	(0.281)	0.104	0.012
105	8.75	0.53	0.115	(0.280)	0.104	0.012
106	8.83	0.57	0.122	(0.278)	0.110	0.012
107	8.92	0.57	0.122	(0.277)	0.110	0.012
108	9.00	0.57	0.122	(0.276)	0.110	0.012
109	9.08	0.63	0.137	(0.274)	0.123	0.014
110	9.17	0.63	0.137	(0.273)	0.123	0.014
111	9.25	0.63	0.137	(0.272)	0.123	0.014
112	9.33	0.67	0.144	(0.270)	0.130	0.014
113	9.42	0.67	0.144	(0.269)	0.130	0.014
114	9.50	0.67	0.144	(0.268)	0.130	0.014
115	9.58	0.70	0.151	(0.267)	0.136	0.015
116	9.67	0.70	0.151	(0.265)	0.136	0.015
117	9.75	0.70	0.151	(0.264)	0.136	0.015
118	9.83	0.73	0.158	(0.263)	0.143	0.016
119	9.92	0.73	0.158	(0.261)	0.143	0.016
120	10.00	0.73	0.158	(0.260)	0.143	0.016
121	10.08	0.50	0.108	(0.259)	0.097	0.011
122	10.17	0.50	0.108	(0.258)	0.097	0.011
123	10.25	0.50	0.108	(0.256)	0.097	0.011
124	10.33	0.50	0.108	(0.255)	0.097	0.011
125	10.42	0.50	0.108	(0.254)	0.097	0.011
126	10.50	0.50	0.108	(0.253)	0.097	0.011
127	10.58	0.67	0.144	(0.251)	0.130	0.014
128	10.67	0.67	0.144	(0.250)	0.130	0.014
129	10.75	0.67	0.144	(0.249)	0.130	0.014
130	10.83	0.67	0.144	(0.248)	0.130	0.014
131	10.92	0.67	0.144	(0.247)	0.130	0.014
132	11.00	0.67	0.144	(0.245)	0.130	0.014
133	11.08	0.63	0.137	(0.244)	0.123	0.014
134	11.17	0.63	0.137	(0.243)	0.123	0.014
135	11.25	0.63	0.137	(0.242)	0.123	0.014
136	11.33	0.63	0.137	(0.241)	0.123	0.014
137	11.42	0.63	0.137	(0.239)	0.123	0.014
138	11.50	0.63	0.137	(0.238)	0.123	0.014
139	11.58	0.57	0.122	(0.237)	0.110	0.012
140	11.67	0.57	0.122	(0.236)	0.110	0.012
141	11.75	0.57	0.122	(0.235)	0.110	0.012
142	11.83	0.60	0.130	(0.233)	0.117	0.013
143	11.92	0.60	0.130	(0.232)	0.117	0.013
144	12.00	0.60	0.130	(0.231)	0.117	0.013
145	12.08	0.83	0.180	(0.230)	0.162	0.018
146	12.17	0.83	0.180	(0.229)	0.162	0.018
147	12.25	0.83	0.180	(0.228)	0.162	0.018
148	12.33	0.87	0.187	(0.227)	0.168	0.019
149	12.42	0.87	0.187	(0.225)	0.168	0.019
150	12.50	0.87	0.187	(0.224)	0.168	0.019
151	12.58	0.93	0.202	(0.223)	0.181	0.020
152	12.67	0.93	0.202	(0.222)	0.181	0.020
153	12.75	0.93	0.202	(0.221)	0.181	0.020
154	12.83	0.97	0.209	(0.220)	0.188	0.021
155	12.92	0.97	0.209	(0.219)	0.188	0.021
156	13.00	0.97	0.209	(0.218)	0.188	0.021
157	13.08	1.13	0.245	0.216	(0.220)	0.028

158	13.17	1.13	0.245	0.215	(0.220)	0.029
159	13.25	1.13	0.245	0.214	(0.220)	0.031
160	13.33	1.13	0.245	0.213	(0.220)	0.032
161	13.42	1.13	0.245	0.212	(0.220)	0.033
162	13.50	1.13	0.245	0.211	(0.220)	0.034
163	13.58	0.77	0.166	(0.210)	0.149	0.017
164	13.67	0.77	0.166	(0.209)	0.149	0.017
165	13.75	0.77	0.166	(0.208)	0.149	0.017
166	13.83	0.77	0.166	(0.207)	0.149	0.017
167	13.92	0.77	0.166	(0.206)	0.149	0.017
168	14.00	0.77	0.166	(0.205)	0.149	0.017
169	14.08	0.90	0.194	(0.204)	0.175	0.019
170	14.17	0.90	0.194	(0.203)	0.175	0.019
171	14.25	0.90	0.194	(0.202)	0.175	0.019
172	14.33	0.87	0.187	(0.200)	0.168	0.019
173	14.42	0.87	0.187	(0.199)	0.168	0.019
174	14.50	0.87	0.187	(0.198)	0.168	0.019
175	14.58	0.87	0.187	(0.197)	0.168	0.019
176	14.67	0.87	0.187	(0.196)	0.168	0.019
177	14.75	0.87	0.187	(0.195)	0.168	0.019
178	14.83	0.83	0.180	(0.194)	0.162	0.018
179	14.92	0.83	0.180	(0.193)	0.162	0.018
180	15.00	0.83	0.180	(0.192)	0.162	0.018
181	15.08	0.80	0.173	(0.191)	0.156	0.017
182	15.17	0.80	0.173	(0.190)	0.156	0.017
183	15.25	0.80	0.173	(0.189)	0.156	0.017
184	15.33	0.77	0.166	(0.188)	0.149	0.017
185	15.42	0.77	0.166	(0.188)	0.149	0.017
186	15.50	0.77	0.166	(0.187)	0.149	0.017
187	15.58	0.63	0.137	(0.186)	0.123	0.014
188	15.67	0.63	0.137	(0.185)	0.123	0.014
189	15.75	0.63	0.137	(0.184)	0.123	0.014
190	15.83	0.63	0.137	(0.183)	0.123	0.014
191	15.92	0.63	0.137	(0.182)	0.123	0.014
192	16.00	0.63	0.137	(0.181)	0.123	0.014
193	16.08	0.13	0.029	(0.180)	0.026	0.003
194	16.17	0.13	0.029	(0.179)	0.026	0.003
195	16.25	0.13	0.029	(0.178)	0.026	0.003
196	16.33	0.13	0.029	(0.177)	0.026	0.003
197	16.42	0.13	0.029	(0.176)	0.026	0.003
198	16.50	0.13	0.029	(0.175)	0.026	0.003
199	16.58	0.10	0.022	(0.175)	0.019	0.002
200	16.67	0.10	0.022	(0.174)	0.019	0.002
201	16.75	0.10	0.022	(0.173)	0.019	0.002
202	16.83	0.10	0.022	(0.172)	0.019	0.002
203	16.92	0.10	0.022	(0.171)	0.019	0.002
204	17.00	0.10	0.022	(0.170)	0.019	0.002
205	17.08	0.17	0.036	(0.169)	0.032	0.004
206	17.17	0.17	0.036	(0.168)	0.032	0.004
207	17.25	0.17	0.036	(0.168)	0.032	0.004
208	17.33	0.17	0.036	(0.167)	0.032	0.004
209	17.42	0.17	0.036	(0.166)	0.032	0.004
210	17.50	0.17	0.036	(0.165)	0.032	0.004
211	17.58	0.17	0.036	(0.164)	0.032	0.004
212	17.67	0.17	0.036	(0.163)	0.032	0.004
213	17.75	0.17	0.036	(0.163)	0.032	0.004
214	17.83	0.13	0.029	(0.162)	0.026	0.003
215	17.92	0.13	0.029	(0.161)	0.026	0.003
216	18.00	0.13	0.029	(0.160)	0.026	0.003
217	18.08	0.13	0.029	(0.159)	0.026	0.003
218	18.17	0.13	0.029	(0.159)	0.026	0.003
219	18.25	0.13	0.029	(0.158)	0.026	0.003
220	18.33	0.13	0.029	(0.157)	0.026	0.003
221	18.42	0.13	0.029	(0.156)	0.026	0.003
222	18.50	0.13	0.029	(0.156)	0.026	0.003
223	18.58	0.10	0.022	(0.155)	0.019	0.002
224	18.67	0.10	0.022	(0.154)	0.019	0.002
225	18.75	0.10	0.022	(0.153)	0.019	0.002
226	18.83	0.07	0.014	(0.153)	0.013	0.001
227	18.92	0.07	0.014	(0.152)	0.013	0.001
228	19.00	0.07	0.014	(0.151)	0.013	0.001
229	19.08	0.10	0.022	(0.150)	0.019	0.002
230	19.17	0.10	0.022	(0.150)	0.019	0.002
231	19.25	0.10	0.022	(0.149)	0.019	0.002
232	19.33	0.13	0.029	(0.148)	0.026	0.003
233	19.42	0.13	0.029	(0.148)	0.026	0.003
234	19.50	0.13	0.029	(0.147)	0.026	0.003
235	19.58	0.10	0.022	(0.146)	0.019	0.002
236	19.67	0.10	0.022	(0.146)	0.019	0.002
237	19.75	0.10	0.022	(0.145)	0.019	0.002
238	19.83	0.07	0.014	(0.144)	0.013	0.001
239	19.92	0.07	0.014	(0.144)	0.013	0.001
240	20.00	0.07	0.014	(0.143)	0.013	0.001
241	20.08	0.10	0.022	(0.142)	0.019	0.002
242	20.17	0.10	0.022	(0.142)	0.019	0.002
243	20.25	0.10	0.022	(0.141)	0.019	0.002

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244  20.33     0.10      0.022       (  0.141)       0.019        0.002
245  20.42     0.10      0.022       (  0.140)       0.019        0.002
246  20.50     0.10      0.022       (  0.139)       0.019        0.002
247  20.58     0.10      0.022       (  0.139)       0.019        0.002
248  20.67     0.10      0.022       (  0.138)       0.019        0.002
249  20.75     0.10      0.022       (  0.138)       0.019        0.002
250  20.83     0.07      0.014       (  0.137)       0.013        0.001
251  20.92     0.07      0.014       (  0.137)       0.013        0.001
252  21.00     0.07      0.014       (  0.136)       0.013        0.001
253  21.08     0.10      0.022       (  0.135)       0.019        0.002
254  21.17     0.10      0.022       (  0.135)       0.019        0.002
255  21.25     0.10      0.022       (  0.134)       0.019        0.002
256  21.33     0.07      0.014       (  0.134)       0.013        0.001
257  21.42     0.07      0.014       (  0.133)       0.013        0.001
258  21.50     0.07      0.014       (  0.133)       0.013        0.001
259  21.58     0.10      0.022       (  0.132)       0.019        0.002
260  21.67     0.10      0.022       (  0.132)       0.019        0.002
261  21.75     0.10      0.022       (  0.131)       0.019        0.002
262  21.83     0.07      0.014       (  0.131)       0.013        0.001
263  21.92     0.07      0.014       (  0.131)       0.013        0.001
264  22.00     0.07      0.014       (  0.130)       0.013        0.001
265  22.08     0.10      0.022       (  0.130)       0.019        0.002
266  22.17     0.10      0.022       (  0.129)       0.019        0.002
267  22.25     0.10      0.022       (  0.129)       0.019        0.002
268  22.33     0.07      0.014       (  0.128)       0.013        0.001
269  22.42     0.07      0.014       (  0.128)       0.013        0.001
270  22.50     0.07      0.014       (  0.128)       0.013        0.001
271  22.58     0.07      0.014       (  0.127)       0.013        0.001
272  22.67     0.07      0.014       (  0.127)       0.013        0.001
273  22.75     0.07      0.014       (  0.127)       0.013        0.001
274  22.83     0.07      0.014       (  0.126)       0.013        0.001
275  22.92     0.07      0.014       (  0.126)       0.013        0.001
276  23.00     0.07      0.014       (  0.126)       0.013        0.001
277  23.08     0.07      0.014       (  0.125)       0.013        0.001
278  23.17     0.07      0.014       (  0.125)       0.013        0.001
279  23.25     0.07      0.014       (  0.125)       0.013        0.001
280  23.33     0.07      0.014       (  0.125)       0.013        0.001
281  23.42     0.07      0.014       (  0.124)       0.013        0.001
282  23.50     0.07      0.014       (  0.124)       0.013        0.001
283  23.58     0.07      0.014       (  0.124)       0.013        0.001
284  23.67     0.07      0.014       (  0.124)       0.013        0.001
285  23.75     0.07      0.014       (  0.124)       0.013        0.001
286  23.83     0.07      0.014       (  0.123)       0.013        0.001
287  23.92     0.07      0.014       (  0.123)       0.013        0.001
288  24.00     0.07      0.014       (  0.123)       0.013        0.001
              (Loss Rate Not Used)
    Sum =     100.0                                  Sum =     2.2
      Flood volume = Effective rainfall      0.18(In)
       times area      28.4(Ac.)/[(In)/(Ft.)] =       0.4(Ac.Ft)
      Total soil loss =      1.62(In)
      Total soil loss =     3.830(Ac.Ft)
      Total rainfall =      1.80(In)
      Flood volume =       18914.8 Cubic Feet
      Total soil loss =      166836.5 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.942(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
---------------------------------------------------------------------------
  0+ 5       0.0001      0.02  Q         |         |         |         |
  0+10       0.0003      0.03  Q         |         |         |         |
  0+15       0.0006      0.04  Q         |         |         |         |
  0+20       0.0010      0.05  Q         |         |         |         |
  0+25       0.0014      0.06  Q         |         |         |         |
  0+30       0.0018      0.06  Q         |         |         |         |
  0+35       0.0022      0.06  Q         |         |         |         |
  0+40       0.0026      0.06  Q         |         |         |         |
  0+45       0.0030      0.06  Q         |         |         |         |
  0+50       0.0035      0.07  Q         |         |         |         |
  0+55       0.0041      0.08  Q         |         |         |         |
  1+ 0       0.0046      0.08  Q         |         |         |         |
  1+ 5       0.0051      0.07  Q         |         |         |         |
  1+10       0.0056      0.07  Q         |         |         |         |
  1+15       0.0060      0.06  Q         |         |         |         |
  1+20       0.0065      0.06  Q         |         |         |         |
  1+25       0.0069      0.06  Q         |         |         |         |
  1+30       0.0073      0.06  Q         |         |         |         |
  1+35       0.0077      0.06  Q         |         |         |         |
  1+40       0.0082      0.06  Q         |         |         |         |
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1+45      0.0086      0.06  Q          |          |          |          |
1+50      0.0091      0.07  Q          |          |          |          |
1+55      0.0096      0.08  Q          |          |          |          |
2+ 0      0.0102      0.08  Q          |          |          |          |
2+ 5      0.0107      0.08  Q          |          |          |          |
2+10      0.0113      0.08  QV         |          |          |          |
2+15      0.0119      0.08  QV         |          |          |          |
2+20      0.0125      0.08  QV         |          |          |          |
2+25      0.0130      0.08  QV         |          |          |          |
2+30      0.0136      0.08  QV         |          |          |          |
2+35      0.0142      0.09  QV         |          |          |          |
2+40      0.0149      0.10  QV         |          |          |          |
2+45      0.0156      0.10  QV         |          |          |          |
2+50      0.0163      0.10  QV         |          |          |          |
2+55      0.0170      0.10  QV         |          |          |          |
3+ 0      0.0177      0.10  QV         |          |          |          |
3+ 5      0.0184      0.10  QV         |          |          |          |
3+10      0.0192      0.10  QV         |          |          |          |
3+15      0.0199      0.10  QV         |          |          |          |
3+20      0.0206      0.10  QV         |          |          |          |
3+25      0.0213      0.10  QV         |          |          |          |
3+30      0.0220      0.10  Q V        |          |          |          |
3+35      0.0227      0.10  Q V        |          |          |          |
3+40      0.0234      0.10  Q V        |          |          |          |
3+45      0.0241      0.10  Q V        |          |          |          |
3+50      0.0249      0.11  Q V        |          |          |          |
3+55      0.0257      0.12  Q V        |          |          |          |
4+ 0      0.0266      0.12  Q V        |          |          |          |
4+ 5      0.0274      0.12  Q V        |          |          |          |
4+10      0.0283      0.12  Q V        |          |          |          |
4+15      0.0291      0.12  Q V        |          |          |          |
4+20      0.0300      0.13  Q V        |          |          |          |
4+25      0.0310      0.14  Q V        |          |          |          |
4+30      0.0320      0.14  Q V        |          |          |          |
4+35      0.0330      0.14  Q  V       |          |          |          |
4+40      0.0340      0.14  Q  V       |          |          |          |
4+45      0.0350      0.14  Q  V       |          |          |          |
4+50      0.0360      0.15  Q  V       |          |          |          |
4+55      0.0371      0.16  Q  V       |          |          |          |
5+ 0      0.0383      0.16  Q  V       |          |          |          |
5+ 5      0.0393      0.15  Q  V       |          |          |          |
5+10      0.0402      0.13  Q  V       |          |          |          |
5+15      0.0411      0.13  Q  V       |          |          |          |
5+20      0.0420      0.13  Q  V       |          |          |          |
5+25      0.0429      0.14  Q  V       |          |          |          |
5+30      0.0439      0.14  Q   V      |          |          |          |
5+35      0.0450      0.15  Q   V      |          |          |          |
5+40      0.0461      0.16  Q   V      |          |          |          |
5+45      0.0472      0.16  Q   V      |          |          |          |
5+50      0.0484      0.16  Q   V      |          |          |          |
5+55      0.0495      0.17  Q   V      |          |          |          |
6+ 0      0.0506      0.17  Q   V      |          |          |          |
6+ 5      0.0518      0.17  Q   V      |          |          |          |
6+10      0.0531      0.18  Q   V      |          |          |          |
6+15      0.0543      0.18  Q    V     |          |          |          |
6+20      0.0556      0.19  Q    V     |          |          |          |
6+25      0.0569      0.19  Q    V     |          |          |          |
6+30      0.0582      0.19  Q    V     |          |          |          |
6+35      0.0595      0.19  Q    V     |          |          |          |
6+40      0.0609      0.20  Q    V     |          |          |          |
6+45      0.0623      0.21  Q    V     |          |          |          |
6+50      0.0637      0.21  Q    V     |          |          |          |
6+55      0.0652      0.21  Q     V    |          |          |          |
7+ 0      0.0666      0.21  Q     V    |          |          |          |
7+ 5      0.0680      0.21  Q     V    |          |          |          |
7+10      0.0694      0.21  Q     V    |          |          |          |
7+15      0.0709      0.21  Q     V    |          |          |          |
7+20      0.0723      0.21  Q     V    |          |          |          |
7+25      0.0739      0.22  Q     V    |          |          |          |
7+30      0.0754      0.23  Q     V    |          |          |          |
7+35      0.0770      0.23  Q      V   |          |          |          |
7+40      0.0787      0.24  Q      V   |          |          |          |
7+45      0.0804      0.25  Q      V   |          |          |          |
7+50      0.0822      0.26  |Q     V   |          |          |          |
7+55      0.0840      0.27  |Q     V   |          |          |          |
8+ 0      0.0858      0.27  |Q     V   |          |          |          |
8+ 5      0.0878      0.28  |Q      V  |          |          |          |
8+10      0.0899      0.30  |Q      V  |          |          |          |
8+15      0.0920      0.31  |Q      V  |          |          |          |
8+20      0.0941      0.31  |Q      V  |          |          |          |
8+25      0.0963      0.31  |Q      V  |          |          |          |
8+30      0.0984      0.31  |Q       V |          |          |          |
8+35      0.1006      0.32  |Q       V |          |          |          |
8+40      0.1028      0.33  |Q       V |          |          |          |
8+45      0.1051      0.33  |Q       V |          |          |          |
8+50      0.1074      0.34  |Q       V |          |          |          |
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8+55	0.1098	0.35	
9+ 0	0.1122	0.35	
9+ 5	0.1147	0.37	
9+10	0.1174	0.39	
9+15	0.1201	0.39	
9+20	0.1228	0.40	
9+25	0.1257	0.41	
9+30	0.1285	0.41	
9+35	0.1314	0.42	
9+40	0.1343	0.43	
9+45	0.1373	0.43	
9+50	0.1404	0.44	
9+55	0.1435	0.45	
10+ 0	0.1466	0.45	
10+ 5	0.1493	0.40	
10+10	0.1516	0.33	
10+15	0.1538	0.32	
10+20	0.1560	0.31	
10+25	0.1581	0.31	
10+30	0.1602	0.31	
10+35	0.1626	0.35	
10+40	0.1654	0.40	
10+45	0.1682	0.41	
10+50	0.1710	0.41	
10+55	0.1738	0.41	
11+ 0	0.1767	0.41	
11+ 5	0.1795	0.40	
11+10	0.1822	0.40	
11+15	0.1849	0.39	
11+20	0.1876	0.39	
11+25	0.1903	0.39	
11+30	0.1930	0.39	
11+35	0.1956	0.38	
11+40	0.1981	0.36	
11+45	0.2005	0.35	
11+50	0.2030	0.36	
11+55	0.2055	0.37	
12+ 0	0.2080	0.37	
12+ 5	0.2110	0.43	
12+10	0.2144	0.49	
12+15	0.2179	0.51	
12+20	0.2215	0.52	
12+25	0.2251	0.53	
12+30	0.2288	0.54	
12+35	0.2326	0.55	
12+40	0.2366	0.57	
12+45	0.2405	0.58	
12+50	0.2446	0.59	
12+55	0.2487	0.60	
13+ 0	0.2528	0.60	
13+ 5	0.2575	0.68	
13+10	0.2629	0.79	
13+15	0.2687	0.84	
13+20	0.2747	0.88	
13+25	0.2810	0.91	
13+30	0.2875	0.94	
13+35	0.2928	0.77	
13+40	0.2966	0.55	
13+45	0.3000	0.50	
13+50	0.3034	0.48	
13+55	0.3066	0.47	
14+ 0	0.3099	0.47	
14+ 5	0.3134	0.51	
14+10	0.3171	0.54	
14+15	0.3209	0.55	
14+20	0.3247	0.55	
14+25	0.3284	0.54	
14+30	0.3321	0.54	
14+35	0.3358	0.54	
14+40	0.3395	0.54	
14+45	0.3432	0.54	
14+50	0.3469	0.53	
14+55	0.3504	0.52	
15+ 0	0.3540	0.52	
15+ 5	0.3575	0.51	
15+10	0.3609	0.50	
15+15	0.3644	0.50	
15+20	0.3677	0.49	
15+25	0.3710	0.48	
15+30	0.3743	0.48	
15+35	0.3773	0.44	
15+40	0.3801	0.41	
15+45	0.3829	0.40	
15+50	0.3856	0.39	
15+55	0.3883	0.39	
16+ 0	0.3910	0.39	

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16+ 5       0.3929      0.27  |Q       |         |         |     V   |
16+10       0.3938      0.13  Q        |         |         |     V   |
16+15       0.3945      0.10  Q        |         |         |     V   |
16+20       0.3951      0.09  Q        |         |         |     V   |
16+25       0.3956      0.08  Q        |         |         |     V   |
16+30       0.3962      0.08  Q        |         |         |     V   |
16+35       0.3967      0.07  Q        |         |         |     V   |
16+40       0.3972      0.07  Q        |         |         |     V   |
16+45       0.3976      0.06  Q        |         |         |     V   |
16+50       0.3980      0.06  Q        |         |         |     V   |
16+55       0.3985      0.06  Q        |         |         |     V   |
17+ 0       0.3989      0.06  Q        |         |         |     V   |
17+ 5       0.3994      0.08  Q        |         |         |     V   |
17+10       0.4001      0.10  Q        |         |         |     V   |
17+15       0.4008      0.10  Q        |         |         |     V   |
17+20       0.4015      0.10  Q        |         |         |     V   |
17+25       0.4022      0.10  Q        |         |         |      V  |
17+30       0.4029      0.10  Q        |         |         |      V  |
17+35       0.4036      0.10  Q        |         |         |      V  |
17+40       0.4043      0.10  Q        |         |         |      V  |
17+45       0.4050      0.10  Q        |         |         |      V  |
17+50       0.4057      0.10  Q        |         |         |      V  |
17+55       0.4063      0.09  Q        |         |         |      V  |
18+ 0       0.4069      0.08  Q        |         |         |      V  |
18+ 5       0.4074      0.08  Q        |         |         |      V  |
18+10       0.4080      0.08  Q        |         |         |      V  |
18+15       0.4086      0.08  Q        |         |         |      V  |
18+20       0.4091      0.08  Q        |         |         |      V  |
18+25       0.4097      0.08  Q        |         |         |      V  |
18+30       0.4103      0.08  Q        |         |         |      V  |
18+35       0.4108      0.07  Q        |         |         |      V  |
18+40       0.4112      0.07  Q        |         |         |      V  |
18+45       0.4117      0.06  Q        |         |         |      V  |
18+50       0.4121      0.05  Q        |         |         |      V  |
18+55       0.4124      0.04  Q        |         |         |      V  |
19+ 0       0.4127      0.04  Q        |         |         |       V |
19+ 5       0.4130      0.05  Q        |         |         |       V |
19+10       0.4134      0.06  Q        |         |         |       V |
19+15       0.4138      0.06  Q        |         |         |       V |
19+20       0.4143      0.07  Q        |         |         |       V |
19+25       0.4148      0.08  Q        |         |         |       V |
19+30       0.4154      0.08  Q        |         |         |       V |
19+35       0.4159      0.07  Q        |         |         |       V |
19+40       0.4164      0.07  Q        |         |         |       V |
19+45       0.4168      0.06  Q        |         |         |       V |
19+50       0.4172      0.05  Q        |         |         |       V |
19+55       0.4175      0.04  Q        |         |         |       V |
20+ 0       0.4178      0.04  Q        |         |         |       V |
20+ 5       0.4181      0.05  Q        |         |         |       V |
20+10       0.4185      0.06  Q        |         |         |       V |
20+15       0.4189      0.06  Q        |         |         |       V |
20+20       0.4194      0.06  Q        |         |         |       V |
20+25       0.4198      0.06  Q        |         |         |       V |
20+30       0.4202      0.06  Q        |         |         |       V |
20+35       0.4206      0.06  Q        |         |         |       V |
20+40       0.4211      0.06  Q        |         |         |       V |
20+45       0.4215      0.06  Q        |         |         |       V |
20+50       0.4219      0.05  Q        |         |         |       V |
20+55       0.4222      0.04  Q        |         |         |       V |
21+ 0       0.4225      0.04  Q        |         |         |       V |
21+ 5       0.4228      0.05  Q        |         |         |       V |
21+10       0.4232      0.06  Q        |         |         |       V |
21+15       0.4236      0.06  Q        |         |         |        V|
21+20       0.4240      0.05  Q        |         |         |        V|
21+25       0.4243      0.04  Q        |         |         |        V|
21+30       0.4246      0.04  Q        |         |         |        V|
21+35       0.4249      0.05  Q        |         |         |        V|
21+40       0.4253      0.06  Q        |         |         |        V|
21+45       0.4258      0.06  Q        |         |         |        V|
21+50       0.4261      0.05  Q        |         |         |        V|
21+55       0.4264      0.04  Q        |         |         |        V|
22+ 0       0.4267      0.04  Q        |         |         |        V|
22+ 5       0.4271      0.05  Q        |         |         |        V|
22+10       0.4275      0.06  Q        |         |         |        V|
22+15       0.4279      0.06  Q        |         |         |        V|
22+20       0.4283      0.05  Q        |         |         |        V|
22+25       0.4286      0.04  Q        |         |         |        V|
22+30       0.4289      0.04  Q        |         |         |        V|
22+35       0.4291      0.04  Q        |         |         |        V|
22+40       0.4294      0.04  Q        |         |         |        V|
22+45       0.4297      0.04  Q        |         |         |        V|
22+50       0.4300      0.04  Q        |         |         |        V|
22+55       0.4303      0.04  Q        |         |         |        V|
23+ 0       0.4306      0.04  Q        |         |         |        V|
23+ 5       0.4309      0.04  Q        |         |         |        V|
23+10       0.4311      0.04  Q        |         |         |        V|
```

```
   23+15       0.4314      0.04  Q          |          |          |         v|
   23+20       0.4317      0.04  Q          |          |          |         v|
   23+25       0.4320      0.04  Q          |          |          |         v|
   23+30       0.4323      0.04  Q          |          |          |         v|
   23+35       0.4326      0.04  Q          |          |          |         v|
   23+40       0.4328      0.04  Q          |          |          |         v|
   23+45       0.4331      0.04  Q          |          |          |         v|
   23+50       0.4334      0.04  Q          |          |          |         v|
   23+55       0.4337      0.04  Q          |          |          |         v|
   24+ 0       0.4340      0.04  Q          |          |          |         v|
   24+ 5       0.4342      0.03  Q          |          |          |         v|
   24+10       0.4342      0.01  Q          |          |          |         v|
   24+15       0.4342      0.00  Q          |          |          |         v|
   24+20       0.4342      0.00  Q          |          |          |          v
-------------------------------------------------------------------------------
```

```
        U n i t   H y d r o g r a p h   A n a l y s i s

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      28.43(Ac.)  =      0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      28.43(Ac.)  =      0.044 Sq. Mi.
Length along longest watercourse =     691.00(Ft.)
Length along longest watercourse measured to centroid =     346.00(Ft.)
Length along longest watercourse =      0.131 Mi.
Length along longest watercourse measured to centroid =      0.066 Mi.
Difference in elevation =      73.00(Ft.)
Slope along watercourse =    557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time =    0.047 Hr.
Lag time =     2.84 Min.
25% of lag time =     0.71 Min.
40% of lag time =     1.14 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       28.43           0.50                 14.22

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       28.43           1.30                 36.96

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.687(In)
Areal adjustment factor =   99.97 %
Adjusted average point rain =    0.687(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    28.430           91.00         0.000
 Total Area Entered =     28.43(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

```
       Unit time period   Time % of lag   Distribution   Unit Hydrograph
           (hrs)                          Graph %           (CFS)
       ------------------------------------------------------------------------
           1   0.083        176.088         38.943             11.158
           2   0.167        352.176         45.069             12.913
           3   0.250        528.264          9.844              2.820
           4   0.333        704.352          4.075              1.168
           5   0.417        880.440          2.069              0.593
                                    Sum = 100.000   Sum=      28.652
------------------------------------------------------------------------
```

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

```
 Unit Time   Pattern   Storm Rain     Loss rate(In./Hr)     Effective
      (Hr.)  Percent   (In/Hr)         Max    |   Low        (In/Hr)
  1   0.08     3.30      0.272       (  0.246)       0.245        0.027
  2   0.17     4.20      0.346          0.246    (  0.312)        0.100
  3   0.25     4.40      0.363          0.246    (  0.327)        0.116
  4   0.33     4.80      0.396          0.246    (  0.356)        0.149
  5   0.42     5.20      0.429          0.246    (  0.386)        0.182
  6   0.50     6.20      0.511          0.246    (  0.460)        0.265
  7   0.58     6.80      0.561          0.246    (  0.505)        0.314
  8   0.67     8.80      0.726          0.246    (  0.653)        0.479
  9   0.75    13.90      1.146          0.246    (  1.032)        0.900
 10   0.83    31.40      2.589          0.246    (  2.330)        2.343
 11   0.92     7.20      0.594          0.246    (  0.534)        0.347
 12   1.00     3.80      0.313          0.246    (  0.282)        0.067
              (Loss Rate Not Used)
    Sum =     100.0                                  Sum =      5.3
       Flood volume = Effective rainfall      0.44(In)
        times area      28.4(Ac.)/[(In)/(Ft.)] =       1.0(Ac.Ft)
       Total soil loss =      0.25(In)
       Total soil loss =     0.583(Ac.Ft)
       Total rainfall =      0.69(In)
       Flood volume =       45507.7 Cubic Feet
       Total soil loss =       25412.2 Cubic Feet
       ---------------------------------------------------------------------
        Peak flow rate of this hydrograph =     39.661(CFS)
       ---------------------------------------------------------------------
       +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                           1 - H O U R    S T O R M
                      R u n o f f      H y d r o g r a p h
       ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

       ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0       10.0      20.0      30.0      40.0
 ------------------------------------------------------------------------
   0+ 5       0.0021      0.30  Q         |         |         |         |
   0+10       0.0122      1.47  VQ        |         |         |         |
   0+15       0.0306      2.67  |VQ       |         |         |         |
   0+20       0.0546      3.49  | VQ      |         |         |         |
   0+25       0.0851      4.43  |  VQ     |         |         |         |
   0+30       0.1260      5.93  |   VQ    |         |         |         |
   0+35       0.1789      7.69  |     VQ  |         |         |         |
   0+40       0.2510     10.46  |        VQ         |         |         |
   0+45       0.3718     17.54  |          |  V  Q  |         |         |
   0+50       0.6450     39.66  |          |        |   V     |        Q|
   0+55       0.9028     37.44  |          |        |         |   V  Q  |
   1+ 0       0.9936     13.18  |          |  Q     |         |      V  |
   1+ 5       1.0288      5.12  |    Q     |        |         |        V|
   1+10       1.0425      1.98  |Q         |        |         |        V|
   1+15       1.0444      0.28  Q          |        |         |        V|
   1+20       1.0447      0.04  Q          |        |         |         V
------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex535.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.80	22.74

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	2.00	56.86

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 1.081(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.081(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

```
      ----------------------------------------------------------------------
          1   0.083        176.088          38.943             11.158
          2   0.167        352.176          45.069             12.913
          3   0.250        528.264           9.844              2.820
          4   0.333        704.352           4.075              1.168
          5   0.417        880.440           2.069              0.593
                                   Sum = 100.000    Sum=       28.652
----------------------------------------------------------------------


 The following loss rate calculations reflect use of the minimum calculated loss
 rate subtracted from the Storm Rain to produce the maximum Effective Rain value

  Unit Time   Pattern   Storm Rain     Loss rate(In./Hr)     Effective
       (Hr.)  Percent   (In/Hr)          Max    |   Low         (In/Hr)
   1   0.08     1.30      0.169       (  0.246)       0.152         0.017
   2   0.17     1.30      0.169       (  0.246)       0.152         0.017
   3   0.25     1.10      0.143       (  0.246)       0.128         0.014
   4   0.33     1.50      0.195       (  0.246)       0.175         0.019
   5   0.42     1.50      0.195       (  0.246)       0.175         0.019
   6   0.50     1.80      0.233       (  0.246)       0.210         0.023
   7   0.58     1.50      0.195       (  0.246)       0.175         0.019
   8   0.67     1.80      0.233       (  0.246)       0.210         0.023
   9   0.75     1.80      0.233       (  0.246)       0.210         0.023
  10   0.83     1.50      0.195       (  0.246)       0.175         0.019
  11   0.92     1.60      0.208       (  0.246)       0.187         0.021
  12   1.00     1.80      0.233       (  0.246)       0.210         0.023
  13   1.08     2.20      0.285          0.246    (  0.257)         0.039
  14   1.17     2.20      0.285          0.246    (  0.257)         0.039
  15   1.25     2.20      0.285          0.246    (  0.257)         0.039
  16   1.33     2.00      0.259       (  0.246)       0.233         0.026
  17   1.42     2.60      0.337          0.246    (  0.304)         0.091
  18   1.50     2.70      0.350          0.246    (  0.315)         0.104
  19   1.58     2.40      0.311          0.246    (  0.280)         0.065
  20   1.67     2.70      0.350          0.246    (  0.315)         0.104
  21   1.75     3.30      0.428          0.246    (  0.385)         0.182
  22   1.83     3.10      0.402          0.246    (  0.362)         0.156
  23   1.92     2.90      0.376          0.246    (  0.339)         0.130
  24   2.00     3.00      0.389          0.246    (  0.350)         0.143
  25   2.08     3.10      0.402          0.246    (  0.362)         0.156
  26   2.17     4.20      0.545          0.246    (  0.490)         0.298
  27   2.25     5.00      0.649          0.246    (  0.584)         0.402
  28   2.33     3.50      0.454          0.246    (  0.409)         0.208
  29   2.42     6.80      0.882          0.246    (  0.794)         0.636
  30   2.50     7.30      0.947          0.246    (  0.852)         0.701
  31   2.58     8.20      1.064          0.246    (  0.957)         0.817
  32   2.67     5.90      0.765          0.246    (  0.689)         0.519
  33   2.75     2.00      0.259       (  0.246)       0.233         0.026
  34   2.83     1.80      0.233       (  0.246)       0.210         0.023
  35   2.92     1.80      0.233       (  0.246)       0.210         0.023
  36   3.00     0.60      0.078       (  0.246)       0.070         0.008
               (Loss Rate Not Used)
     Sum =     100.0                                   Sum =      5.2
       Flood volume = Effective rainfall      0.43(In)
        times area      28.4(Ac.)/[(In)/(Ft.)] =       1.0(Ac.Ft)
       Total soil loss =      0.65(In)
       Total soil loss =     1.540(Ac.Ft)
       Total rainfall =      1.08(In)
       Flood volume =       44491.6 Cubic Feet
       Total soil loss =       67061.9 Cubic Feet
       ---------------------------------------------------------------------
        Peak flow rate of this hydrograph =     20.450(CFS)
       ---------------------------------------------------------------------
       +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          3 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
       ---------------------------------------------------------------------
                   Hydrograph in   5   Minute intervals ((CFS))

       ---------------------------------------------------------------------
  Time(h+m) Volume Ac.Ft   Q(CFS)  0        7.5      15.0      22.5      30.0
  ----------------------------------------------------------------------------
    0+ 5       0.0013      0.19  Q         |         |         |         |
    0+10       0.0041      0.41  Q         |         |         |         |
    0+15       0.0070      0.42  Q         |         |         |         |
    0+20       0.0102      0.47  Q         |         |         |         |
    0+25       0.0140      0.54  Q         |         |         |         |
    0+30       0.0180      0.59  Q         |         |         |         |
    0+35       0.0222      0.60  Q         |         |         |         |
    0+40       0.0264      0.61  QV        |         |         |         |
    0+45       0.0309      0.66  QV        |         |         |         |
    0+50       0.0352      0.62  QV        |         |         |         |
    0+55       0.0393      0.59  QV        |         |         |         |
    1+ 0       0.0436      0.62  QV        |         |         |         |
    1+ 5       0.0493      0.83  |Q        |         |         |         |
    1+10       0.0565      1.04  |QV       |         |         |         |
```

```
    1+15       0.0640      1.09  |QV       |          |          |          |
    1+20       0.0706      0.96  |QV       |          |          |          |
    1+25       0.0811      1.53  | QV      |          |          |          |
    1+30       0.0982      2.48  |  Q      |          |          |          |
    1+35       0.1146      2.38  |  QV     |          |          |          |
    1+40       0.1312      2.41  |  Q V    |          |          |          |
    1+45       0.1569      3.73  |   Q V   |          |          |          |
    1+50       0.1880      4.52  |     QV  |          |          |          |
    1+55       0.2164      4.13  |    Q  V |          |          |          |
    2+ 0       0.2439      3.98  |    Q   V|          |          |          |
    2+ 5       0.2731      4.24  |    Q    V          |          |          |
    2+10       0.3143      5.99  |      Q  | V        |          |          |
    2+15       0.3765      9.03  |         | Q V      |          |          |
    2+20       0.4359      8.62  |         |Q     V   |          |          |
    2+25       0.5141     11.36  |         |    Q    V          |          |
    2+30       0.6330     17.27  |         |         |  QV      |          |
    2+35       0.7739     20.45  |         |         |     Q  V            |
    2+40       0.9061     19.20  |         |         |    Q     |    V     |
    2+45       0.9783     10.50  |         |  Q      |          |       V  |
    2+50       1.0020      3.43  |   Q     |         |          |         V|
    2+55       1.0139      1.73  | Q       |         |          |         V|
    3+ 0       1.0193      0.79  |Q        |         |          |         V|
    3+ 5       1.0208      0.21  Q         |         |          |         V|
    3+10       1.0212      0.06  Q         |         |          |         V|
    3+15       1.0214      0.02  Q         |         |          |         V|
    3+20       1.0214      0.00  Q         |         |          |         V|
-------------------------------------------------------------------------- |
```

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.10	31.27

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	3.00	85.29

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.545(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.545(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.093	(0.246)	0.083	0.009
2	0.17	0.60	0.111	(0.246)	0.100	0.011
3	0.25	0.60	0.111	(0.246)	0.100	0.011
4	0.33	0.60	0.111	(0.246)	0.100	0.011
5	0.42	0.60	0.111	(0.246)	0.100	0.011
6	0.50	0.70	0.130	(0.246)	0.117	0.013
7	0.58	0.70	0.130	(0.246)	0.117	0.013
8	0.67	0.70	0.130	(0.246)	0.117	0.013
9	0.75	0.70	0.130	(0.246)	0.117	0.013
10	0.83	0.70	0.130	(0.246)	0.117	0.013
11	0.92	0.70	0.130	(0.246)	0.117	0.013
12	1.00	0.80	0.148	(0.246)	0.133	0.015
13	1.08	0.80	0.148	(0.246)	0.133	0.015
14	1.17	0.80	0.148	(0.246)	0.133	0.015
15	1.25	0.80	0.148	(0.246)	0.133	0.015
16	1.33	0.80	0.148	(0.246)	0.133	0.015
17	1.42	0.80	0.148	(0.246)	0.133	0.015
18	1.50	0.80	0.148	(0.246)	0.133	0.015
19	1.58	0.80	0.148	(0.246)	0.133	0.015
20	1.67	0.80	0.148	(0.246)	0.133	0.015
21	1.75	0.80	0.148	(0.246)	0.133	0.015
22	1.83	0.80	0.148	(0.246)	0.133	0.015
23	1.92	0.80	0.148	(0.246)	0.133	0.015
24	2.00	0.90	0.167	(0.246)	0.150	0.017
25	2.08	0.80	0.148	(0.246)	0.133	0.015
26	2.17	0.90	0.167	(0.246)	0.150	0.017
27	2.25	0.90	0.167	(0.246)	0.150	0.017
28	2.33	0.90	0.167	(0.246)	0.150	0.017
29	2.42	0.90	0.167	(0.246)	0.150	0.017
30	2.50	0.90	0.167	(0.246)	0.150	0.017
31	2.58	0.90	0.167	(0.246)	0.150	0.017
32	2.67	0.90	0.167	(0.246)	0.150	0.017
33	2.75	1.00	0.185	(0.246)	0.167	0.019
34	2.83	1.00	0.185	(0.246)	0.167	0.019
35	2.92	1.00	0.185	(0.246)	0.167	0.019
36	3.00	1.00	0.185	(0.246)	0.167	0.019
37	3.08	1.00	0.185	(0.246)	0.167	0.019
38	3.17	1.10	0.204	(0.246)	0.184	0.020
39	3.25	1.10	0.204	(0.246)	0.184	0.020
40	3.33	1.10	0.204	(0.246)	0.184	0.020
41	3.42	1.20	0.222	(0.246)	0.200	0.022
42	3.50	1.30	0.241	(0.246)	0.217	0.024
43	3.58	1.40	0.260	(0.246)	0.234	0.026
44	3.67	1.40	0.260	(0.246)	0.234	0.026
45	3.75	1.50	0.278	0.246	(0.250)	0.032
46	3.83	1.50	0.278	0.246	(0.250)	0.032
47	3.92	1.60	0.297	0.246	(0.267)	0.050
48	4.00	1.60	0.297	0.246	(0.267)	0.050
49	4.08	1.70	0.315	0.246	(0.284)	0.069
50	4.17	1.80	0.334	0.246	(0.300)	0.087
51	4.25	1.90	0.352	0.246	(0.317)	0.106
52	4.33	2.00	0.371	0.246	(0.334)	0.124
53	4.42	2.10	0.389	0.246	(0.350)	0.143
54	4.50	2.10	0.389	0.246	(0.350)	0.143
55	4.58	2.20	0.408	0.246	(0.367)	0.161
56	4.67	2.30	0.426	0.246	(0.384)	0.180
57	4.75	2.40	0.445	0.246	(0.400)	0.199
58	4.83	2.40	0.445	0.246	(0.400)	0.199
59	4.92	2.50	0.463	0.246	(0.417)	0.217
60	5.00	2.60	0.482	0.246	(0.434)	0.236
61	5.08	3.10	0.575	0.246	(0.517)	0.328
62	5.17	3.60	0.667	0.246	(0.601)	0.421
63	5.25	3.90	0.723	0.246	(0.651)	0.477
64	5.33	4.20	0.779	0.246	(0.701)	0.532
65	5.42	4.70	0.871	0.246	(0.784)	0.625
66	5.50	5.60	1.038	0.246	(0.934)	0.792
67	5.58	1.90	0.352	0.246	(0.317)	0.106
68	5.67	0.90	0.167	(0.246)	0.150	0.017
69	5.75	0.60	0.111	(0.246)	0.100	0.011
70	5.83	0.50	0.093	(0.246)	0.083	0.009
71	5.92	0.30	0.056	(0.246)	0.050	0.006

```
72   6.00     0.20      0.037       (  0.246)       0.033        0.004
              (Loss Rate Not Used)
   Sum =     100.0                                    Sum =     6.1
      Flood volume = Effective rainfall      0.51(In)
       times area      28.4(Ac.)/[(In)/(Ft.)] =       1.2(Ac.Ft)
      Total soil loss =      1.04(In)
      Total soil loss =     2.463(Ac.Ft)
      Total rainfall =      1.54(In)
      Flood volume =       52158.5 Cubic Feet
      Total soil loss =      107274.0 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     19.222(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
-------------------------------------------------------------------------
  0+ 5       0.0007      0.10  Q          |          |          |          |
  0+10       0.0024      0.24  Q          |          |          |          |
  0+15       0.0044      0.29  Q          |          |          |          |
  0+20       0.0066      0.31  Q          |          |          |          |
  0+25       0.0087      0.32  Q          |          |          |          |
  0+30       0.0111      0.34  Q          |          |          |          |
  0+35       0.0136      0.36  Q          |          |          |          |
  0+40       0.0161      0.37  Q          |          |          |          |
  0+45       0.0187      0.37  Q          |          |          |          |
  0+50       0.0212      0.37  Q          |          |          |          |
  0+55       0.0238      0.37  Q          |          |          |          |
  1+ 0       0.0265      0.39  Q          |          |          |          |
  1+ 5       0.0294      0.42  Q          |          |          |          |
  1+10       0.0323      0.42  QV         |          |          |          |
  1+15       0.0352      0.42  QV         |          |          |          |
  1+20       0.0381      0.43  QV         |          |          |          |
  1+25       0.0411      0.43  QV         |          |          |          |
  1+30       0.0440      0.43  QV         |          |          |          |
  1+35       0.0469      0.43  QV         |          |          |          |
  1+40       0.0498      0.43  QV         |          |          |          |
  1+45       0.0528      0.43  QV         |          |          |          |
  1+50       0.0557      0.43  QV         |          |          |          |
  1+55       0.0586      0.43  QV         |          |          |          |
  2+ 0       0.0617      0.45  Q V        |          |          |          |
  2+ 5       0.0648      0.45  Q V        |          |          |          |
  2+10       0.0679      0.45  Q V        |          |          |          |
  2+15       0.0711      0.47  Q V        |          |          |          |
  2+20       0.0744      0.48  Q V        |          |          |          |
  2+25       0.0777      0.48  Q V        |          |          |          |
  2+30       0.0810      0.48  Q V        |          |          |          |
  2+35       0.0843      0.48  Q V        |          |          |          |
  2+40       0.0876      0.48  Q V        |          |          |          |
  2+45       0.0910      0.50  Q  V       |          |          |          |
  2+50       0.0946      0.52  |Q V       |          |          |          |
  2+55       0.0983      0.53  |Q V       |          |          |          |
  3+ 0       0.1019      0.53  |Q V       |          |          |          |
  3+ 5       0.1056      0.53  |Q V       |          |          |          |
  3+10       0.1094      0.55  |Q V       |          |          |          |
  3+15       0.1134      0.58  |Q V       |          |          |          |
  3+20       0.1174      0.58  |Q V       |          |          |          |
  3+25       0.1215      0.60  |Q  V       |          |          |          |
  3+30       0.1260      0.65  |Q  V       |          |          |          |
  3+35       0.1308      0.70  |Q  V       |          |          |          |
  3+40       0.1358      0.73  |Q  V       |          |          |          |
  3+45       0.1414      0.80  |Q  V       |          |          |          |
  3+50       0.1475      0.88  |Q  V       |          |          |          |
  3+55       0.1551      1.11  | Q  V      |          |          |          |
  4+ 0       0.1644      1.35  | Q  V      |          |          |          |
  4+ 5       0.1755      1.61  |  Q V      |          |          |          |
  4+10       0.1899      2.08  |   Q V     |          |          |          |
  4+15       0.2077      2.59  |    QV     |          |          |          |
  4+20       0.2292      3.11  |     QV    |          |          |          |
  4+25       0.2543      3.64  |      QV   |          |          |          |
  4+30       0.2816      3.97  |      Q V  |          |          |          |
  4+35       0.3109      4.26  |       Q V |          |          |          |
  4+40       0.3436      4.74  |        Q|V |          |          |          |
  4+45       0.3797      5.25  |         Q V|          |          |          |
  4+50       0.4181      5.56  |          |Q V        |          |          |
  4+55       0.4584      5.86  |          |Q   V      |          |          |
  5+ 0       0.5020      6.33  |          | Q   V     |          |          |
  5+ 5       0.5549      7.67  |          |    Q  V   |          |          |
  5+10       0.6236      9.98  |          |        QV |          |          |
  5+15       0.7069     12.09  |          |          | VQ       |          |
  5+20       0.8020     13.81  |          |          |    VQ    |          |
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    5+25       0.9114     15.89  |          |          |          VQ          |
    5+30       1.0438     19.22  |          |          |          |   V   Q   |
    5+35       1.1407     14.08  |          |          |       Q  |       V   |
    5+40       1.1740      4.83  |          Q|         |          |         V |
    5+45       1.1873      1.93  |   Q       |         |          |         V |
    5+50       1.1935      0.89  |Q          |         |          |         V |
    5+55       1.1955      0.30  Q           |         |          |         V |
    6+ 0       1.1966      0.16  Q           |         |          |         V |
    6+ 5       1.1972      0.08  Q           |         |          |         V |
    6+10       1.1973      0.02  Q           |         |          |         V |
    6+15       1.1974      0.01  Q           |         |          |         V |
    6+20       1.1974      0.00  Q           |         |          |          V
-------------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex5245.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.80	51.17

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	5.00	142.15

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 2.550(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 2.549(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.020	(0.437)	0.018	0.002
2	0.17	0.07	0.020	(0.435)	0.018	0.002
3	0.25	0.07	0.020	(0.433)	0.018	0.002
4	0.33	0.10	0.031	(0.432)	0.028	0.003
5	0.42	0.10	0.031	(0.430)	0.028	0.003
6	0.50	0.10	0.031	(0.428)	0.028	0.003
7	0.58	0.10	0.031	(0.427)	0.028	0.003
8	0.67	0.10	0.031	(0.425)	0.028	0.003
9	0.75	0.10	0.031	(0.423)	0.028	0.003
10	0.83	0.13	0.041	(0.422)	0.037	0.004
11	0.92	0.13	0.041	(0.420)	0.037	0.004
12	1.00	0.13	0.041	(0.418)	0.037	0.004
13	1.08	0.10	0.031	(0.417)	0.028	0.003
14	1.17	0.10	0.031	(0.415)	0.028	0.003
15	1.25	0.10	0.031	(0.413)	0.028	0.003
16	1.33	0.10	0.031	(0.412)	0.028	0.003
17	1.42	0.10	0.031	(0.410)	0.028	0.003
18	1.50	0.10	0.031	(0.408)	0.028	0.003
19	1.58	0.10	0.031	(0.407)	0.028	0.003
20	1.67	0.10	0.031	(0.405)	0.028	0.003
21	1.75	0.10	0.031	(0.404)	0.028	0.003
22	1.83	0.13	0.041	(0.402)	0.037	0.004
23	1.92	0.13	0.041	(0.400)	0.037	0.004
24	2.00	0.13	0.041	(0.399)	0.037	0.004
25	2.08	0.13	0.041	(0.397)	0.037	0.004
26	2.17	0.13	0.041	(0.395)	0.037	0.004
27	2.25	0.13	0.041	(0.394)	0.037	0.004
28	2.33	0.13	0.041	(0.392)	0.037	0.004
29	2.42	0.13	0.041	(0.391)	0.037	0.004
30	2.50	0.13	0.041	(0.389)	0.037	0.004
31	2.58	0.17	0.051	(0.387)	0.046	0.005
32	2.67	0.17	0.051	(0.386)	0.046	0.005
33	2.75	0.17	0.051	(0.384)	0.046	0.005
34	2.83	0.17	0.051	(0.383)	0.046	0.005
35	2.92	0.17	0.051	(0.381)	0.046	0.005
36	3.00	0.17	0.051	(0.380)	0.046	0.005
37	3.08	0.17	0.051	(0.378)	0.046	0.005
38	3.17	0.17	0.051	(0.376)	0.046	0.005
39	3.25	0.17	0.051	(0.375)	0.046	0.005
40	3.33	0.17	0.051	(0.373)	0.046	0.005
41	3.42	0.17	0.051	(0.372)	0.046	0.005
42	3.50	0.17	0.051	(0.370)	0.046	0.005
43	3.58	0.17	0.051	(0.369)	0.046	0.005
44	3.67	0.17	0.051	(0.367)	0.046	0.005
45	3.75	0.17	0.051	(0.366)	0.046	0.005
46	3.83	0.20	0.061	(0.364)	0.055	0.006
47	3.92	0.20	0.061	(0.362)	0.055	0.006
48	4.00	0.20	0.061	(0.361)	0.055	0.006
49	4.08	0.20	0.061	(0.359)	0.055	0.006
50	4.17	0.20	0.061	(0.358)	0.055	0.006
51	4.25	0.20	0.061	(0.356)	0.055	0.006
52	4.33	0.23	0.071	(0.355)	0.064	0.007
53	4.42	0.23	0.071	(0.353)	0.064	0.007
54	4.50	0.23	0.071	(0.352)	0.064	0.007
55	4.58	0.23	0.071	(0.350)	0.064	0.007
56	4.67	0.23	0.071	(0.349)	0.064	0.007
57	4.75	0.23	0.071	(0.347)	0.064	0.007
58	4.83	0.27	0.082	(0.346)	0.073	0.008
59	4.92	0.27	0.082	(0.344)	0.073	0.008
60	5.00	0.27	0.082	(0.343)	0.073	0.008
61	5.08	0.20	0.061	(0.341)	0.055	0.006
62	5.17	0.20	0.061	(0.340)	0.055	0.006
63	5.25	0.20	0.061	(0.338)	0.055	0.006
64	5.33	0.23	0.071	(0.337)	0.064	0.007
65	5.42	0.23	0.071	(0.335)	0.064	0.007
66	5.50	0.23	0.071	(0.334)	0.064	0.007
67	5.58	0.27	0.082	(0.332)	0.073	0.008
68	5.67	0.27	0.082	(0.331)	0.073	0.008
69	5.75	0.27	0.082	(0.330)	0.073	0.008
70	5.83	0.27	0.082	(0.328)	0.073	0.008
71	5.92	0.27	0.082	(0.327)	0.073	0.008

72	6.00	0.27	0.082	(0.325)	0.073	0.008
73	6.08	0.30	0.092	(0.324)	0.083	0.009
74	6.17	0.30	0.092	(0.322)	0.083	0.009
75	6.25	0.30	0.092	(0.321)	0.083	0.009
76	6.33	0.30	0.092	(0.319)	0.083	0.009
77	6.42	0.30	0.092	(0.318)	0.083	0.009
78	6.50	0.30	0.092	(0.317)	0.083	0.009
79	6.58	0.33	0.102	(0.315)	0.092	0.010
80	6.67	0.33	0.102	(0.314)	0.092	0.010
81	6.75	0.33	0.102	(0.312)	0.092	0.010
82	6.83	0.33	0.102	(0.311)	0.092	0.010
83	6.92	0.33	0.102	(0.310)	0.092	0.010
84	7.00	0.33	0.102	(0.308)	0.092	0.010
85	7.08	0.33	0.102	(0.307)	0.092	0.010
86	7.17	0.33	0.102	(0.305)	0.092	0.010
87	7.25	0.33	0.102	(0.304)	0.092	0.010
88	7.33	0.37	0.112	(0.303)	0.101	0.011
89	7.42	0.37	0.112	(0.301)	0.101	0.011
90	7.50	0.37	0.112	(0.300)	0.101	0.011
91	7.58	0.40	0.122	(0.298)	0.110	0.012
92	7.67	0.40	0.122	(0.297)	0.110	0.012
93	7.75	0.40	0.122	(0.296)	0.110	0.012
94	7.83	0.43	0.133	(0.294)	0.119	0.013
95	7.92	0.43	0.133	(0.293)	0.119	0.013
96	8.00	0.43	0.133	(0.292)	0.119	0.013
97	8.08	0.50	0.153	(0.290)	0.138	0.015
98	8.17	0.50	0.153	(0.289)	0.138	0.015
99	8.25	0.50	0.153	(0.288)	0.138	0.015
100	8.33	0.50	0.153	(0.286)	0.138	0.015
101	8.42	0.50	0.153	(0.285)	0.138	0.015
102	8.50	0.50	0.153	(0.283)	0.138	0.015
103	8.58	0.53	0.163	(0.282)	0.147	0.016
104	8.67	0.53	0.163	(0.281)	0.147	0.016
105	8.75	0.53	0.163	(0.280)	0.147	0.016
106	8.83	0.57	0.173	(0.278)	0.156	0.017
107	8.92	0.57	0.173	(0.277)	0.156	0.017
108	9.00	0.57	0.173	(0.276)	0.156	0.017
109	9.08	0.63	0.194	(0.274)	0.174	0.019
110	9.17	0.63	0.194	(0.273)	0.174	0.019
111	9.25	0.63	0.194	(0.272)	0.174	0.019
112	9.33	0.67	0.204	(0.270)	0.184	0.020
113	9.42	0.67	0.204	(0.269)	0.184	0.020
114	9.50	0.67	0.204	(0.268)	0.184	0.020
115	9.58	0.70	0.214	(0.267)	0.193	0.021
116	9.67	0.70	0.214	(0.265)	0.193	0.021
117	9.75	0.70	0.214	(0.264)	0.193	0.021
118	9.83	0.73	0.224	(0.263)	0.202	0.022
119	9.92	0.73	0.224	(0.261)	0.202	0.022
120	10.00	0.73	0.224	(0.260)	0.202	0.022
121	10.08	0.50	0.153	(0.259)	0.138	0.015
122	10.17	0.50	0.153	(0.258)	0.138	0.015
123	10.25	0.50	0.153	(0.256)	0.138	0.015
124	10.33	0.50	0.153	(0.255)	0.138	0.015
125	10.42	0.50	0.153	(0.254)	0.138	0.015
126	10.50	0.50	0.153	(0.253)	0.138	0.015
127	10.58	0.67	0.204	(0.251)	0.184	0.020
128	10.67	0.67	0.204	(0.250)	0.184	0.020
129	10.75	0.67	0.204	(0.249)	0.184	0.020
130	10.83	0.67	0.204	(0.248)	0.184	0.020
131	10.92	0.67	0.204	(0.247)	0.184	0.020
132	11.00	0.67	0.204	(0.245)	0.184	0.020
133	11.08	0.63	0.194	(0.244)	0.174	0.019
134	11.17	0.63	0.194	(0.243)	0.174	0.019
135	11.25	0.63	0.194	(0.242)	0.174	0.019
136	11.33	0.63	0.194	(0.241)	0.174	0.019
137	11.42	0.63	0.194	(0.239)	0.174	0.019
138	11.50	0.63	0.194	(0.238)	0.174	0.019
139	11.58	0.57	0.173	(0.237)	0.156	0.017
140	11.67	0.57	0.173	(0.236)	0.156	0.017
141	11.75	0.57	0.173	(0.235)	0.156	0.017
142	11.83	0.60	0.184	(0.233)	0.165	0.018
143	11.92	0.60	0.184	(0.232)	0.165	0.018
144	12.00	0.60	0.184	(0.231)	0.165	0.018
145	12.08	0.83	0.255	(0.230)	0.229	0.025
146	12.17	0.83	0.255	0.229	(0.229)	0.026
147	12.25	0.83	0.255	0.228	(0.229)	0.027
148	12.33	0.87	0.265	0.227	(0.239)	0.039
149	12.42	0.87	0.265	0.225	(0.239)	0.040
150	12.50	0.87	0.265	0.224	(0.239)	0.041
151	12.58	0.93	0.286	0.223	(0.257)	0.062
152	12.67	0.93	0.286	0.222	(0.257)	0.064
153	12.75	0.93	0.286	0.221	(0.257)	0.065
154	12.83	0.97	0.296	0.220	(0.266)	0.076
155	12.92	0.97	0.296	0.219	(0.266)	0.077
156	13.00	0.97	0.296	0.218	(0.266)	0.078
157	13.08	1.13	0.347	0.216	(0.312)	0.130

158	13.17	1.13	0.347		0.215	(0.312)	0.131
159	13.25	1.13	0.347		0.214	(0.312)	0.132
160	13.33	1.13	0.347		0.213	(0.312)	0.134
161	13.42	1.13	0.347		0.212	(0.312)	0.135
162	13.50	1.13	0.347		0.211	(0.312)	0.136
163	13.58	0.77	0.235		0.210	(0.211)	0.025
164	13.67	0.77	0.235		0.209	(0.211)	0.026
165	13.75	0.77	0.235		0.208	(0.211)	0.027
166	13.83	0.77	0.235		0.207	(0.211)	0.028
167	13.92	0.77	0.235		0.206	(0.211)	0.029
168	14.00	0.77	0.235		0.205	(0.211)	0.030
169	14.08	0.90	0.275		0.204	(0.248)	0.072
170	14.17	0.90	0.275		0.203	(0.248)	0.073
171	14.25	0.90	0.275		0.202	(0.248)	0.074
172	14.33	0.87	0.265		0.200	(0.239)	0.065
173	14.42	0.87	0.265		0.199	(0.239)	0.066
174	14.50	0.87	0.265		0.198	(0.239)	0.067
175	14.58	0.87	0.265		0.197	(0.239)	0.068
176	14.67	0.87	0.265		0.196	(0.239)	0.069
177	14.75	0.87	0.265		0.195	(0.239)	0.070
178	14.83	0.83	0.255		0.194	(0.229)	0.061
179	14.92	0.83	0.255		0.193	(0.229)	0.062
180	15.00	0.83	0.255		0.192	(0.229)	0.063
181	15.08	0.80	0.245		0.191	(0.220)	0.053
182	15.17	0.80	0.245		0.190	(0.220)	0.054
183	15.25	0.80	0.245		0.189	(0.220)	0.055
184	15.33	0.77	0.235		0.188	(0.211)	0.046
185	15.42	0.77	0.235		0.188	(0.211)	0.047
186	15.50	0.77	0.235		0.187	(0.211)	0.048
187	15.58	0.63	0.194	(0.186)		0.174	0.019
188	15.67	0.63	0.194	(0.185)		0.174	0.019
189	15.75	0.63	0.194	(0.184)		0.174	0.019
190	15.83	0.63	0.194	(0.183)		0.174	0.019
191	15.92	0.63	0.194	(0.182)		0.174	0.019
192	16.00	0.63	0.194	(0.181)		0.174	0.019
193	16.08	0.13	0.041	(0.180)		0.037	0.004
194	16.17	0.13	0.041	(0.179)		0.037	0.004
195	16.25	0.13	0.041	(0.178)		0.037	0.004
196	16.33	0.13	0.041	(0.177)		0.037	0.004
197	16.42	0.13	0.041	(0.176)		0.037	0.004
198	16.50	0.13	0.041	(0.175)		0.037	0.004
199	16.58	0.10	0.031	(0.175)		0.028	0.003
200	16.67	0.10	0.031	(0.174)		0.028	0.003
201	16.75	0.10	0.031	(0.173)		0.028	0.003
202	16.83	0.10	0.031	(0.172)		0.028	0.003
203	16.92	0.10	0.031	(0.171)		0.028	0.003
204	17.00	0.10	0.031	(0.170)		0.028	0.003
205	17.08	0.17	0.051	(0.169)		0.046	0.005
206	17.17	0.17	0.051	(0.168)		0.046	0.005
207	17.25	0.17	0.051	(0.168)		0.046	0.005
208	17.33	0.17	0.051	(0.167)		0.046	0.005
209	17.42	0.17	0.051	(0.166)		0.046	0.005
210	17.50	0.17	0.051	(0.165)		0.046	0.005
211	17.58	0.17	0.051	(0.164)		0.046	0.005
212	17.67	0.17	0.051	(0.163)		0.046	0.005
213	17.75	0.17	0.051	(0.163)		0.046	0.005
214	17.83	0.13	0.041	(0.162)		0.037	0.004
215	17.92	0.13	0.041	(0.161)		0.037	0.004
216	18.00	0.13	0.041	(0.160)		0.037	0.004
217	18.08	0.13	0.041	(0.159)		0.037	0.004
218	18.17	0.13	0.041	(0.159)		0.037	0.004
219	18.25	0.13	0.041	(0.158)		0.037	0.004
220	18.33	0.13	0.041	(0.157)		0.037	0.004
221	18.42	0.13	0.041	(0.156)		0.037	0.004
222	18.50	0.13	0.041	(0.156)		0.037	0.004
223	18.58	0.10	0.031	(0.155)		0.028	0.003
224	18.67	0.10	0.031	(0.154)		0.028	0.003
225	18.75	0.10	0.031	(0.153)		0.028	0.003
226	18.83	0.07	0.020	(0.153)		0.018	0.002
227	18.92	0.07	0.020	(0.152)		0.018	0.002
228	19.00	0.07	0.020	(0.151)		0.018	0.002
229	19.08	0.10	0.031	(0.150)		0.028	0.003
230	19.17	0.10	0.031	(0.150)		0.028	0.003
231	19.25	0.10	0.031	(0.149)		0.028	0.003
232	19.33	0.13	0.041	(0.148)		0.037	0.004
233	19.42	0.13	0.041	(0.148)		0.037	0.004
234	19.50	0.13	0.041	(0.147)		0.037	0.004
235	19.58	0.10	0.031	(0.146)		0.028	0.003
236	19.67	0.10	0.031	(0.146)		0.028	0.003
237	19.75	0.10	0.031	(0.145)		0.028	0.003
238	19.83	0.07	0.020	(0.144)		0.018	0.002
239	19.92	0.07	0.020	(0.144)		0.018	0.002
240	20.00	0.07	0.020	(0.143)		0.018	0.002
241	20.08	0.10	0.031	(0.142)		0.028	0.003
242	20.17	0.10	0.031	(0.142)		0.028	0.003
243	20.25	0.10	0.031	(0.141)		0.028	0.003

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244  20.33     0.10      0.031       (  0.141)       0.028        0.003
245  20.42     0.10      0.031       (  0.140)       0.028        0.003
246  20.50     0.10      0.031       (  0.139)       0.028        0.003
247  20.58     0.10      0.031       (  0.139)       0.028        0.003
248  20.67     0.10      0.031       (  0.138)       0.028        0.003
249  20.75     0.10      0.031       (  0.138)       0.028        0.003
250  20.83     0.07      0.020       (  0.137)       0.018        0.002
251  20.92     0.07      0.020       (  0.137)       0.018        0.002
252  21.00     0.07      0.020       (  0.136)       0.018        0.002
253  21.08     0.10      0.031       (  0.135)       0.028        0.003
254  21.17     0.10      0.031       (  0.135)       0.028        0.003
255  21.25     0.10      0.031       (  0.134)       0.028        0.003
256  21.33     0.07      0.020       (  0.134)       0.018        0.002
257  21.42     0.07      0.020       (  0.133)       0.018        0.002
258  21.50     0.07      0.020       (  0.133)       0.018        0.002
259  21.58     0.10      0.031       (  0.132)       0.028        0.003
260  21.67     0.10      0.031       (  0.132)       0.028        0.003
261  21.75     0.10      0.031       (  0.131)       0.028        0.003
262  21.83     0.07      0.020       (  0.131)       0.018        0.002
263  21.92     0.07      0.020       (  0.131)       0.018        0.002
264  22.00     0.07      0.020       (  0.130)       0.018        0.002
265  22.08     0.10      0.031       (  0.130)       0.028        0.003
266  22.17     0.10      0.031       (  0.129)       0.028        0.003
267  22.25     0.10      0.031       (  0.129)       0.028        0.003
268  22.33     0.07      0.020       (  0.128)       0.018        0.002
269  22.42     0.07      0.020       (  0.128)       0.018        0.002
270  22.50     0.07      0.020       (  0.128)       0.018        0.002
271  22.58     0.07      0.020       (  0.127)       0.018        0.002
272  22.67     0.07      0.020       (  0.127)       0.018        0.002
273  22.75     0.07      0.020       (  0.127)       0.018        0.002
274  22.83     0.07      0.020       (  0.126)       0.018        0.002
275  22.92     0.07      0.020       (  0.126)       0.018        0.002
276  23.00     0.07      0.020       (  0.126)       0.018        0.002
277  23.08     0.07      0.020       (  0.125)       0.018        0.002
278  23.17     0.07      0.020       (  0.125)       0.018        0.002
279  23.25     0.07      0.020       (  0.125)       0.018        0.002
280  23.33     0.07      0.020       (  0.125)       0.018        0.002
281  23.42     0.07      0.020       (  0.124)       0.018        0.002
282  23.50     0.07      0.020       (  0.124)       0.018        0.002
283  23.58     0.07      0.020       (  0.124)       0.018        0.002
284  23.67     0.07      0.020       (  0.124)       0.018        0.002
285  23.75     0.07      0.020       (  0.124)       0.018        0.002
286  23.83     0.07      0.020       (  0.123)       0.018        0.002
287  23.92     0.07      0.020       (  0.123)       0.018        0.002
288  24.00     0.07      0.020       (  0.123)       0.018        0.002
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =     4.6
      Flood volume = Effective rainfall      0.38(In)
       times area      28.4(Ac.)/[(In)/(Ft.)] =       0.9(Ac.Ft)
      Total soil loss =      2.17(In)
      Total soil loss =     5.130(Ac.Ft)
      Total rainfall =      2.55(In)
      Flood volume =       39642.2 Cubic Feet
      Total soil loss =      223455.7 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      3.864(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
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   0+ 5       0.0002      0.02  Q         |         |         |         |
   0+10       0.0005      0.05  Q         |         |         |         |
   0+15       0.0009      0.05  Q         |         |         |         |
   0+20       0.0013      0.07  Q         |         |         |         |
   0+25       0.0019      0.08  Q         |         |         |         |
   0+30       0.0025      0.09  Q         |         |         |         |
   0+35       0.0031      0.09  Q         |         |         |         |
   0+40       0.0037      0.09  Q         |         |         |         |
   0+45       0.0043      0.09  Q         |         |         |         |
   0+50       0.0050      0.10  Q         |         |         |         |
   0+55       0.0058      0.11  Q         |         |         |         |
   1+ 0       0.0066      0.12  Q         |         |         |         |
   1+ 5       0.0073      0.10  Q         |         |         |         |
   1+10       0.0079      0.09  Q         |         |         |         |
   1+15       0.0085      0.09  Q         |         |         |         |
   1+20       0.0091      0.09  Q         |         |         |         |
   1+25       0.0098      0.09  Q         |         |         |         |
   1+30       0.0104      0.09  Q         |         |         |         |
   1+35       0.0110      0.09  Q         |         |         |         |
   1+40       0.0116      0.09  Q         |         |         |         |
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1+45      0.0122      0.09  Q          |          |          |          |
1+50      0.0129      0.10  Q          |          |          |          |
1+55      0.0136      0.11  Q          |          |          |          |
2+ 0      0.0144      0.12  Q          |          |          |          |
2+ 5      0.0152      0.12  Q          |          |          |          |
2+10      0.0160      0.12  Q          |          |          |          |
2+15      0.0168      0.12  Q          |          |          |          |
2+20      0.0176      0.12  Q          |          |          |          |
2+25      0.0184      0.12  Q          |          |          |          |
2+30      0.0192      0.12  Q          |          |          |          |
2+35      0.0201      0.13  Q          |          |          |          |
2+40      0.0211      0.14  Q          |          |          |          |
2+45      0.0221      0.14  Q          |          |          |          |
2+50      0.0231      0.15  QV         |          |          |          |
2+55      0.0241      0.15  QV         |          |          |          |
3+ 0      0.0251      0.15  QV         |          |          |          |
3+ 5      0.0261      0.15  QV         |          |          |          |
3+10      0.0271      0.15  QV         |          |          |          |
3+15      0.0281      0.15  QV         |          |          |          |
3+20      0.0291      0.15  QV         |          |          |          |
3+25      0.0301      0.15  QV         |          |          |          |
3+30      0.0312      0.15  QV         |          |          |          |
3+35      0.0322      0.15  QV         |          |          |          |
3+40      0.0332      0.15  QV         |          |          |          |
3+45      0.0342      0.15  QV         |          |          |          |
3+50      0.0353      0.16  QV         |          |          |          |
3+55      0.0364      0.17  QV         |          |          |          |
4+ 0      0.0376      0.17  QV         |          |          |          |
4+ 5      0.0388      0.17  QV         |          |          |          |
4+10      0.0400      0.18  QV         |          |          |          |
4+15      0.0412      0.18  QV         |          |          |          |
4+20      0.0425      0.19  QV         |          |          |          |
4+25      0.0439      0.20  QV         |          |          |          |
4+30      0.0453      0.20  QV         |          |          |          |
4+35      0.0467      0.20  Q V        |          |          |          |
4+40      0.0481      0.20  Q V        |          |          |          |
4+45      0.0495      0.20  Q V        |          |          |          |
4+50      0.0510      0.22  Q V        |          |          |          |
4+55      0.0526      0.23  Q V        |          |          |          |
5+ 0      0.0542      0.23  Q V        |          |          |          |
5+ 5      0.0556      0.21  Q V        |          |          |          |
5+10      0.0569      0.18  Q V        |          |          |          |
5+15      0.0582      0.18  Q V        |          |          |          |
5+20      0.0594      0.19  Q V        |          |          |          |
5+25      0.0608      0.20  Q V        |          |          |          |
5+30      0.0622      0.20  Q V        |          |          |          |
5+35      0.0637      0.22  Q V        |          |          |          |
5+40      0.0653      0.23  Q V        |          |          |          |
5+45      0.0669      0.23  Q V        |          |          |          |
5+50      0.0685      0.23  Q  V       |          |          |          |
5+55      0.0701      0.23  Q  V       |          |          |          |
6+ 0      0.0717      0.23  Q  V       |          |          |          |
6+ 5      0.0734      0.25  Q  V       |          |          |          |
6+10      0.0752      0.26  |Q V       |          |          |          |
6+15      0.0770      0.26  |Q V       |          |          |          |
6+20      0.0788      0.26  |Q V       |          |          |          |
6+25      0.0806      0.26  |Q V       |          |          |          |
6+30      0.0824      0.26  |Q V       |          |          |          |
6+35      0.0843      0.27  |Q V       |          |          |          |
6+40      0.0863      0.29  |Q V       |          |          |          |
6+45      0.0883      0.29  |Q V       |          |          |          |
6+50      0.0903      0.29  |Q V       |          |          |          |
6+55      0.0923      0.29  |Q  V      |          |          |          |
7+ 0      0.0943      0.29  |Q  V      |          |          |          |
7+ 5      0.0963      0.29  |Q  V      |          |          |          |
7+10      0.0983      0.29  |Q  V      |          |          |          |
7+15      0.1004      0.29  |Q  V      |          |          |          |
7+20      0.1024      0.30  |Q  V      |          |          |          |
7+25      0.1046      0.32  |Q  V      |          |          |          |
7+30      0.1068      0.32  |Q  V      |          |          |          |
7+35      0.1091      0.33  |Q  V      |          |          |          |
7+40      0.1115      0.35  |Q  V      |          |          |          |
7+45      0.1139      0.35  |Q   V     |          |          |          |
7+50      0.1164      0.36  |Q   V     |          |          |          |
7+55      0.1190      0.38  |Q   V     |          |          |          |
8+ 0      0.1216      0.38  |Q   V     |          |          |          |
8+ 5      0.1244      0.40  |Q   V     |          |          |          |
8+10      0.1273      0.43  |Q   V     |          |          |          |
8+15      0.1303      0.43  |Q   V     |          |          |          |
8+20      0.1333      0.44  |Q   V     |          |          |          |
8+25      0.1363      0.44  |Q   V     |          |          |          |
8+30      0.1394      0.44  |Q    V    |          |          |          |
8+35      0.1425      0.45  |Q    V    |          |          |          |
8+40      0.1457      0.46  |Q    V    |          |          |          |
8+45      0.1489      0.47  |Q    V    |          |          |          |
8+50      0.1522      0.48  |Q    V    |          |          |          |
```

8+55	0.1555	0.49	
9+ 0	0.1590	0.50	
9+ 5	0.1625	0.52	
9+10	0.1663	0.55	
9+15	0.1701	0.55	
9+20	0.1740	0.57	
9+25	0.1780	0.58	
9+30	0.1820	0.58	
9+35	0.1861	0.60	
9+40	0.1903	0.61	
9+45	0.1945	0.61	
9+50	0.1988	0.62	
9+55	0.2032	0.64	
10+ 0	0.2076	0.64	
10+ 5	0.2115	0.56	
10+10	0.2147	0.47	
10+15	0.2179	0.45	
10+20	0.2209	0.44	
10+25	0.2239	0.44	
10+30	0.2269	0.44	
10+35	0.2304	0.50	
10+40	0.2342	0.56	
10+45	0.2382	0.58	
10+50	0.2422	0.58	
10+55	0.2462	0.58	
11+ 0	0.2502	0.58	
11+ 5	0.2542	0.57	
11+10	0.2580	0.56	
11+15	0.2619	0.56	
11+20	0.2657	0.56	
11+25	0.2695	0.56	
11+30	0.2734	0.56	
11+35	0.2770	0.53	
11+40	0.2805	0.51	
11+45	0.2840	0.50	
11+50	0.2875	0.51	
11+55	0.2911	0.52	
12+ 0	0.2947	0.52	
12+ 5	0.2989	0.61	
12+10	0.3037	0.71	
12+15	0.3088	0.75	
12+20	0.3150	0.90	
12+25	0.3224	1.07	
12+30	0.3301	1.13	
12+35	0.3397	1.40	
12+40	0.3515	1.70	
12+45	0.3638	1.79	
12+50	0.3773	1.96	
12+55	0.3920	2.14	
13+ 0	0.4071	2.20	
13+ 5	0.4264	2.81	
13+10	0.4506	3.51	
13+15	0.4759	3.68	
13+20	0.5019	3.77	
13+25	0.5283	3.83	
13+30	0.5549	3.86	
13+35	0.5731	2.64	
13+40	0.5815	1.22	
13+45	0.5880	0.94	
13+50	0.5938	0.84	
13+55	0.5993	0.80	
14+ 0	0.6050	0.83	
14+ 5	0.6141	1.32	
14+10	0.6270	1.87	
14+15	0.6409	2.02	
14+20	0.6545	1.98	
14+25	0.6677	1.90	
14+30	0.6808	1.90	
14+35	0.6940	1.92	
14+40	0.7074	1.95	
14+45	0.7210	1.97	
14+50	0.7340	1.89	
14+55	0.7463	1.79	
15+ 0	0.7586	1.79	
15+ 5	0.7703	1.69	
15+10	0.7811	1.58	
15+15	0.7920	1.58	
15+20	0.8022	1.48	
15+25	0.8116	1.37	
15+30	0.8211	1.37	
15+35	0.8283	1.06	
15+40	0.8331	0.68	
15+45	0.8372	0.61	
15+50	0.8412	0.57	
15+55	0.8450	0.56	
16+ 0	0.8488	0.56	

```
16+ 5       0.8515      0.38  |Q        |         |         |       V  |
16+10       0.8528      0.19  Q        |         |         |       V  |
16+15       0.8537      0.14  Q        |         |         |       V  |
16+20       0.8546      0.13  Q        |         |         |       V  |
16+25       0.8554      0.12  Q        |         |         |       V  |
16+30       0.8562      0.12  Q        |         |         |       V  |
16+35       0.8569      0.11  Q        |         |         |       V  |
16+40       0.8576      0.09  Q        |         |         |       V  |
16+45       0.8582      0.09  Q        |         |         |       V  |
16+50       0.8588      0.09  Q        |         |         |       V  |
16+55       0.8594      0.09  Q        |         |         |       V  |
17+ 0       0.8600      0.09  Q        |         |         |       V  |
17+ 5       0.8608      0.11  Q        |         |         |       V  |
17+10       0.8617      0.14  Q        |         |         |       V  |
17+15       0.8627      0.14  Q        |         |         |       V  |
17+20       0.8637      0.14  Q        |         |         |       V  |
17+25       0.8647      0.15  Q        |         |         |        V |
17+30       0.8657      0.15  Q        |         |         |        V |
17+35       0.8667      0.15  Q        |         |         |        V |
17+40       0.8677      0.15  Q        |         |         |        V |
17+45       0.8687      0.15  Q        |         |         |        V |
17+50       0.8697      0.13  Q        |         |         |        V |
17+55       0.8705      0.12  Q        |         |         |        V |
18+ 0       0.8713      0.12  Q        |         |         |        V |
18+ 5       0.8721      0.12  Q        |         |         |        V |
18+10       0.8729      0.12  Q        |         |         |        V |
18+15       0.8737      0.12  Q        |         |         |        V |
18+20       0.8745      0.12  Q        |         |         |        V |
18+25       0.8753      0.12  Q        |         |         |        V |
18+30       0.8762      0.12  Q        |         |         |        V |
18+35       0.8769      0.11  Q        |         |         |        V |
18+40       0.8775      0.09  Q        |         |         |        V |
18+45       0.8781      0.09  Q        |         |         |        V |
18+50       0.8787      0.08  Q        |         |         |        V |
18+55       0.8791      0.06  Q        |         |         |        V |
19+ 0       0.8795      0.06  Q        |         |         |        V |
19+ 5       0.8800      0.07  Q        |         |         |        V |
19+10       0.8806      0.08  Q        |         |         |        V |
19+15       0.8812      0.09  Q        |         |         |        V |
19+20       0.8818      0.10  Q        |         |         |        V |
19+25       0.8826      0.11  Q        |         |         |        V |
19+30       0.8834      0.12  Q        |         |         |        V |
19+35       0.8841      0.10  Q        |         |         |        V |
19+40       0.8848      0.09  Q        |         |         |        V |
19+45       0.8854      0.09  Q        |         |         |        V |
19+50       0.8859      0.08  Q        |         |         |        V |
19+55       0.8863      0.06  Q        |         |         |        V |
20+ 0       0.8868      0.06  Q        |         |         |        V |
20+ 5       0.8872      0.07  Q        |         |         |        V |
20+10       0.8878      0.08  Q        |         |         |         V|
20+15       0.8884      0.09  Q        |         |         |         V|
20+20       0.8890      0.09  Q        |         |         |         V|
20+25       0.8896      0.09  Q        |         |         |         V|
20+30       0.8902      0.09  Q        |         |         |         V|
20+35       0.8908      0.09  Q        |         |         |         V|
20+40       0.8914      0.09  Q        |         |         |         V|
20+45       0.8920      0.09  Q        |         |         |         V|
20+50       0.8926      0.08  Q        |         |         |         V|
20+55       0.8930      0.06  Q        |         |         |         V|
21+ 0       0.8934      0.06  Q        |         |         |         V|
21+ 5       0.8939      0.07  Q        |         |         |         V|
21+10       0.8945      0.08  Q        |         |         |         V|
21+15       0.8951      0.09  Q        |         |         |         V|
21+20       0.8956      0.08  Q        |         |         |         V|
21+25       0.8960      0.06  Q        |         |         |         V|
21+30       0.8964      0.06  Q        |         |         |         V|
21+35       0.8969      0.07  Q        |         |         |         V|
21+40       0.8975      0.08  Q        |         |         |         V|
21+45       0.8981      0.09  Q        |         |         |         V|
21+50       0.8986      0.08  Q        |         |         |         V|
21+55       0.8990      0.06  Q        |         |         |         V|
22+ 0       0.8994      0.06  Q        |         |         |         V|
22+ 5       0.8999      0.07  Q        |         |         |         V|
22+10       0.9005      0.08  Q        |         |         |         V|
22+15       0.9011      0.09  Q        |         |         |         V|
22+20       0.9016      0.08  Q        |         |         |         V|
22+25       0.9020      0.06  Q        |         |         |         V|
22+30       0.9025      0.06  Q        |         |         |         V|
22+35       0.9029      0.06  Q        |         |         |         V|
22+40       0.9033      0.06  Q        |         |         |         V|
22+45       0.9037      0.06  Q        |         |         |         V|
22+50       0.9041      0.06  Q        |         |         |         V|
22+55       0.9045      0.06  Q        |         |         |         V|
23+ 0       0.9049      0.06  Q        |         |         |         V|
23+ 5       0.9053      0.06  Q        |         |         |         V|
23+10       0.9057      0.06  Q        |         |         |         V|
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   23+15       0.9061      0.06  Q          |          |          |         v|
   23+20       0.9065      0.06  Q          |          |          |         v|
   23+25       0.9069      0.06  Q          |          |          |         v|
   23+30       0.9073      0.06  Q          |          |          |         v|
   23+35       0.9077      0.06  Q          |          |          |         v|
   23+40       0.9081      0.06  Q          |          |          |         v|
   23+45       0.9085      0.06  Q          |          |          |         v|
   23+50       0.9089      0.06  Q          |          |          |         v|
   23+55       0.9093      0.06  Q          |          |          |         v|
   24+ 0       0.9097      0.06  Q          |          |          |         v|
   24+ 5       0.9100      0.04  Q          |          |          |         v|
   24+10       0.9100      0.01  Q          |          |          |         v|
   24+15       0.9101      0.00  Q          |          |          |         v|
   24+20       0.9101      0.00  Q          |          |          |          v
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U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.50	14.22

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.30	36.96

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.300(In)

Point rain (area averaged) = 0.829(In)
Areal adjustment factor = 99.97 %
Adjusted average point rain = 0.829(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

Slope of intensity-duration curve for a 1 hour storm =0.5500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time		Pattern	Storm Rain	Loss rate(In./Hr)			Effective
	(Hr.)	Percent	(In/Hr)	Max		Low	(In/Hr)
1	0.08	3.30	0.328	0.117	(	0.295)	0.211
2	0.17	4.20	0.418	0.117	(	0.376)	0.301
3	0.25	4.40	0.438	0.117	(	0.394)	0.321
4	0.33	4.80	0.477	0.117	(	0.430)	0.360
5	0.42	5.20	0.517	0.117	(	0.466)	0.400
6	0.50	6.20	0.617	0.117	(	0.555)	0.500
7	0.58	6.80	0.676	0.117	(	0.609)	0.559
8	0.67	8.80	0.875	0.117	(	0.788)	0.758
9	0.75	13.90	1.383	0.117	(	1.244)	1.266
10	0.83	31.40	3.123	0.117	(	2.811)	3.006
11	0.92	7.20	0.716	0.117	(	0.645)	0.599
12	1.00	3.80	0.378	0.117	(	0.340)	0.261
		(Loss Rate Not Used)					
Sum =		100.0				Sum =	8.5

Flood volume = Effective rainfall 0.71(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 1.7(Ac.Ft)
Total soil loss = 0.12(In)
Total soil loss = 0.277(Ac.Ft)
Total rainfall = 0.83(In)
Flood volume = 73470.0 Cubic Feet
Total soil loss = 12074.5 Cubic Feet

Peak flow rate of this hydrograph = 53.004(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	15.0	30.0	45.0	60.0
0+ 5	0.0162	2.36	VQ				
0+10	0.0582	6.09	V Q				
0+15	0.1137	8.06	V Q				
0+20	0.1775	9.26	V Q				
0+25	0.2498	10.51	V Q				
0+30	0.3347	12.32	VQ				
0+35	0.4341	14.44	QV				
0+40	0.5566	17.78	Q V				
0+45	0.7379	26.33	Q				
0+50	1.1030	53.00			V	Q	
0+55	1.4495	50.32				QV	
1+ 0	1.5946	21.07		Q		V	
1+ 5	1.6589	9.33	Q				V
1+10	1.6810	3.22	Q				V
1+15	1.6856	0.66	Q				V
1+20	1.6866	0.15	Q				V

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex10310.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

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Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
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Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.80	22.74

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	2.00	56.86

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 1.294(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.294(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.202	0.117	(0.182)	0.085
2	0.17	1.30	0.202	0.117	(0.182)	0.085
3	0.25	1.10	0.171	0.117	(0.154)	0.054
4	0.33	1.50	0.233	0.117	(0.210)	0.116
5	0.42	1.50	0.233	0.117	(0.210)	0.116
6	0.50	1.80	0.279	0.117	(0.251)	0.162
7	0.58	1.50	0.233	0.117	(0.210)	0.116
8	0.67	1.80	0.279	0.117	(0.251)	0.162
9	0.75	1.80	0.279	0.117	(0.251)	0.162
10	0.83	1.50	0.233	0.117	(0.210)	0.116
11	0.92	1.60	0.248	0.117	(0.224)	0.131
12	1.00	1.80	0.279	0.117	(0.251)	0.162
13	1.08	2.20	0.341	0.117	(0.307)	0.224
14	1.17	2.20	0.341	0.117	(0.307)	0.224
15	1.25	2.20	0.341	0.117	(0.307)	0.224
16	1.33	2.00	0.310	0.117	(0.279)	0.193
17	1.42	2.60	0.404	0.117	(0.363)	0.287
18	1.50	2.70	0.419	0.117	(0.377)	0.302
19	1.58	2.40	0.373	0.117	(0.335)	0.256
20	1.67	2.70	0.419	0.117	(0.377)	0.302
21	1.75	3.30	0.512	0.117	(0.461)	0.395
22	1.83	3.10	0.481	0.117	(0.433)	0.364
23	1.92	2.90	0.450	0.117	(0.405)	0.333
24	2.00	3.00	0.466	0.117	(0.419)	0.349
25	2.08	3.10	0.481	0.117	(0.433)	0.364
26	2.17	4.20	0.652	0.117	(0.587)	0.535
27	2.25	5.00	0.776	0.117	(0.699)	0.659
28	2.33	3.50	0.543	0.117	(0.489)	0.426
29	2.42	6.80	1.056	0.117	(0.950)	0.939
30	2.50	7.30	1.133	0.117	(1.020)	1.016
31	2.58	8.20	1.273	0.117	(1.146)	1.156
32	2.67	5.90	0.916	0.117	(0.824)	0.799
33	2.75	2.00	0.310	0.117	(0.279)	0.193
34	2.83	1.80	0.279	0.117	(0.251)	0.162
35	2.92	1.80	0.279	0.117	(0.251)	0.162
36	3.00	0.60	0.093	(0.117)	0.084	0.009
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	11.3

Flood volume = Effective rainfall 0.95(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 2.2(Ac.Ft)
Total soil loss = 0.35(In)
Total soil loss = 0.825(Ac.Ft)
Total rainfall = 1.29(In)
Flood volume = 97555.2 Cubic Feet
Total soil loss = 35938.2 Cubic Feet

Peak flow rate of this hydrograph = 29.569(CFS)

++

3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0065	0.95	VQ	|	|	|	|
0+10	0.0206	2.04	V Q	|	|	|	|
0+15	0.0339	1.93	V Q	|	|	|	|
0+20	0.0499	2.33	V Q	|	|	|	|
0+25	0.0712	3.09	|V Q	|	|	|	|
0+30	0.0970	3.75	|V Q	|	|	|	|
0+35	0.1238	3.89	| V Q	|	|	|	|
0+40	0.1512	3.97	| V Q	|	|	|	|
0+45	0.1821	4.50	| V Q	|	|	|	|
0+50	0.2102	4.08	| V Q	|	|	|	|
0+55	0.2356	3.68	| Q	|	|	|	|
1+ 0	0.2640	4.12	| VQ	|	|	|	|
1+ 5	0.2998	5.21	| VQ	|	|	|	|
1+10	0.3417	6.09	| V Q	|	|	|	|

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    1+15       0.3852      6.31  |      V Q |          |          |          |
    1+20       0.4269      6.05  |       VQ |          |          |          |
    1+25       0.4732      6.73  |        Q |          |          |          |
    1+30       0.5284      8.02  |         VQ          |          |          |
    1+35       0.5830      7.92  |          Q          |          |          |
    1+40       0.6379      7.98  |          QV         |          |          |
    1+45       0.7038      9.56  |          | Q        |          |          |
    1+50       0.7761     10.50  |          |  VQ      |          |          |
    1+55       0.8453     10.04  |          |  Q V     |          |          |
    2+ 0       0.9132      9.87  |          |  Q  V    |          |          |
    2+ 5       0.9832     10.17  |          |  Q   V   |          |          |
    2+10       1.0677     12.27  |          |     Q  V |          |          |
    2+15       1.1772     15.90  |          |          |Q         |          |
    2+20       1.2834     15.42  |          |          Q V        |          |
    2+25       1.4121     18.69  |          |          |   QV     |          |
    2+30       1.5895     25.76  |          |          |       V  |   Q      |
    2+35       1.7932     29.57  |          |          |          | V       Q|
    2+40       1.9865     28.07  |          |          |          |    V Q   |
    2+45       2.1069     17.49  |          |          |  Q       |      V   |
    2+50       2.1656      8.52  |          |Q         |          |       V  |
    2+55       2.2074      6.08  |        Q |          |          |         V|
    3+ 0       2.2305      3.36  |    Q     |          |          |         V|
    3+ 5       2.2366      0.88  |Q         |          |          |         V|
    3+10       2.2388      0.31  Q          |          |          |         V|
    3+15       2.2395      0.11  Q          |          |          |         V|
    3+20       2.2396      0.01  Q          |          |          |         V|
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex10610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.10	31.27

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	3.00	85.29

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.882(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.881(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.113	(0.117)	0.102	0.011
2	0.17	0.60	0.135	0.117	(0.122)	0.018
3	0.25	0.60	0.135	0.117	(0.122)	0.018
4	0.33	0.60	0.135	0.117	(0.122)	0.018
5	0.42	0.60	0.135	0.117	(0.122)	0.018
6	0.50	0.70	0.158	0.117	(0.142)	0.041
7	0.58	0.70	0.158	0.117	(0.142)	0.041
8	0.67	0.70	0.158	0.117	(0.142)	0.041
9	0.75	0.70	0.158	0.117	(0.142)	0.041
10	0.83	0.70	0.158	0.117	(0.142)	0.041
11	0.92	0.70	0.158	0.117	(0.142)	0.041
12	1.00	0.80	0.181	0.117	(0.163)	0.064
13	1.08	0.80	0.181	0.117	(0.163)	0.064
14	1.17	0.80	0.181	0.117	(0.163)	0.064
15	1.25	0.80	0.181	0.117	(0.163)	0.064
16	1.33	0.80	0.181	0.117	(0.163)	0.064
17	1.42	0.80	0.181	0.117	(0.163)	0.064
18	1.50	0.80	0.181	0.117	(0.163)	0.064
19	1.58	0.80	0.181	0.117	(0.163)	0.064
20	1.67	0.80	0.181	0.117	(0.163)	0.064
21	1.75	0.80	0.181	0.117	(0.163)	0.064
22	1.83	0.80	0.181	0.117	(0.163)	0.064
23	1.92	0.80	0.181	0.117	(0.163)	0.064
24	2.00	0.90	0.203	0.117	(0.183)	0.086
25	2.08	0.80	0.181	0.117	(0.163)	0.064
26	2.17	0.90	0.203	0.117	(0.183)	0.086
27	2.25	0.90	0.203	0.117	(0.183)	0.086
28	2.33	0.90	0.203	0.117	(0.183)	0.086
29	2.42	0.90	0.203	0.117	(0.183)	0.086
30	2.50	0.90	0.203	0.117	(0.183)	0.086
31	2.58	0.90	0.203	0.117	(0.183)	0.086
32	2.67	0.90	0.203	0.117	(0.183)	0.086
33	2.75	1.00	0.226	0.117	(0.203)	0.109
34	2.83	1.00	0.226	0.117	(0.203)	0.109
35	2.92	1.00	0.226	0.117	(0.203)	0.109
36	3.00	1.00	0.226	0.117	(0.203)	0.109
37	3.08	1.00	0.226	0.117	(0.203)	0.109
38	3.17	1.10	0.248	0.117	(0.224)	0.131
39	3.25	1.10	0.248	0.117	(0.224)	0.131
40	3.33	1.10	0.248	0.117	(0.224)	0.131
41	3.42	1.20	0.271	0.117	(0.244)	0.154
42	3.50	1.30	0.294	0.117	(0.264)	0.177
43	3.58	1.40	0.316	0.117	(0.284)	0.199
44	3.67	1.40	0.316	0.117	(0.284)	0.199
45	3.75	1.50	0.339	0.117	(0.305)	0.222
46	3.83	1.50	0.339	0.117	(0.305)	0.222
47	3.92	1.60	0.361	0.117	(0.325)	0.244
48	4.00	1.60	0.361	0.117	(0.325)	0.244
49	4.08	1.70	0.384	0.117	(0.345)	0.267
50	4.17	1.80	0.406	0.117	(0.366)	0.289
51	4.25	1.90	0.429	0.117	(0.386)	0.312
52	4.33	2.00	0.452	0.117	(0.406)	0.335
53	4.42	2.10	0.474	0.117	(0.427)	0.357
54	4.50	2.10	0.474	0.117	(0.427)	0.357
55	4.58	2.20	0.497	0.117	(0.447)	0.380
56	4.67	2.30	0.519	0.117	(0.467)	0.402
57	4.75	2.40	0.542	0.117	(0.488)	0.425
58	4.83	2.40	0.542	0.117	(0.488)	0.425
59	4.92	2.50	0.564	0.117	(0.508)	0.447
60	5.00	2.60	0.587	0.117	(0.528)	0.470
61	5.08	3.10	0.700	0.117	(0.630)	0.583
62	5.17	3.60	0.813	0.117	(0.732)	0.696
63	5.25	3.90	0.881	0.117	(0.792)	0.764
64	5.33	4.20	0.948	0.117	(0.853)	0.831
65	5.42	4.70	1.061	0.117	(0.955)	0.944
66	5.50	5.60	1.264	0.117	(1.138)	1.147
67	5.58	1.90	0.429	0.117	(0.386)	0.312
68	5.67	0.90	0.203	0.117	(0.183)	0.086
69	5.75	0.60	0.135	0.117	(0.122)	0.018
70	5.83	0.50	0.113	(0.117)	0.102	0.011
71	5.92	0.30	0.068	(0.117)	0.061	0.007

```
72   6.00     0.20      0.045       (  0.117)       0.041        0.005
              (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    14.3
       Flood volume = Effective rainfall      1.19(In)
        times area      28.4(Ac.)/[(In)/(Ft.)] =       2.8(Ac.Ft)
       Total soil loss =      0.69(In)
       Total soil loss =     1.631(Ac.Ft)
       Total rainfall =      1.88(In)
       Flood volume =      123128.1 Cubic Feet
       Total soil loss =       71043.5 Cubic Feet
       ---------------------------------------------------------------------
        Peak flow rate of this hydrograph =     28.658(CFS)
       ---------------------------------------------------------------------
       +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
       ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

       ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        7.5      15.0      22.5      30.0
-------------------------------------------------------------------------
  0+ 5       0.0009      0.13  Q          |          |          |          |
  0+10       0.0033      0.35  Q          |          |          |          |
  0+15       0.0066      0.48  Q          |          |          |          |
  0+20       0.0101      0.51  Q          |          |          |          |
  0+25       0.0137      0.53  Q          |          |          |          |
  0+30       0.0191      0.78  VQ         |          |          |          |
  0+35       0.0265      1.07  VQ         |          |          |          |
  0+40       0.0343      1.14  VQ         |          |          |          |
  0+45       0.0423      1.16  VQ         |          |          |          |
  0+50       0.0504      1.18  VQ         |          |          |          |
  0+55       0.0585      1.18  VQ         |          |          |          |
  1+ 0       0.0684      1.43  VQ         |          |          |          |
  1+ 5       0.0802      1.72  |VQ        |          |          |          |
  1+10       0.0925      1.78  |VQ        |          |          |          |
  1+15       0.1050      1.81  |VQ        |          |          |          |
  1+20       0.1175      1.82  |VQ        |          |          |          |
  1+25       0.1301      1.82  |VQ        |          |          |          |
  1+30       0.1427      1.82  | Q        |          |          |          |
  1+35       0.1552      1.82  | Q        |          |          |          |
  1+40       0.1678      1.82  | Q        |          |          |          |
  1+45       0.1803      1.82  | Q        |          |          |          |
  1+50       0.1929      1.82  | Q        |          |          |          |
  1+55       0.2055      1.82  | Q        |          |          |          |
  2+ 0       0.2198      2.08  | QV       |          |          |          |
  2+ 5       0.2343      2.12  | QV       |          |          |          |
  2+10       0.2491      2.14  | QV       |          |          |          |
  2+15       0.2655      2.39  |  Q       |          |          |          |
  2+20       0.2824      2.44  |  Q       |          |          |          |
  2+25       0.2993      2.46  |  QV      |          |          |          |
  2+30       0.3163      2.47  |  QV      |          |          |          |
  2+35       0.3334      2.47  |  QV      |          |          |          |
  2+40       0.3504      2.47  |  QV      |          |          |          |
  2+45       0.3691      2.72  |  Q V     |          |          |          |
  2+50       0.3899      3.01  |   QV     |          |          |          |
  2+55       0.4111      3.08  |   QV     |          |          |          |
  3+ 0       0.4325      3.10  |   Q V    |          |          |          |
  3+ 5       0.4540      3.12  |   Q V    |          |          |          |
  3+10       0.4772      3.37  |   Q V    |          |          |          |
  3+15       0.5024      3.66  |   Q  V   |          |          |          |
  3+20       0.5280      3.73  |   Q  V   |          |          |          |
  3+25       0.5556      4.00  |    Q V   |          |          |          |
  3+30       0.5870      4.56  |     Q V  |          |          |          |
  3+35       0.6226      5.17  |     Q V  |          |          |          |
  3+40       0.6609      5.55  |      Q V |          |          |          |
  3+45       0.7015      5.91  |      Q V |          |          |          |
  3+50       0.7445      6.24  |       Q V|          |          |          |
  3+55       0.7897      6.57  |       Q  |V         |          |          |
  4+ 0       0.8371      6.88  |        Q |V         |          |          |
  4+ 5       0.8868      7.21  |        Q | V        |          |          |
  4+10       0.9404      7.78  |          Q  V       |          |          |
  4+15       0.9983      8.41  |          |Q  V      |          |          |
  4+20       1.0606      9.04  |          | Q  V     |          |          |
  4+25       1.1273      9.69  |          | Q  V     |          |          |
  4+30       1.1967     10.08  |          |  Q  V    |          |          |
  4+35       1.2686     10.44  |          |  Q   V   |          |          |
  4+40       1.3445     11.02  |          |   Q    V |          |          |
  4+45       1.4247     11.64  |          |    Q    V|          |          |
  4+50       1.5075     12.02  |          |     Q   |V          |          |
  4+55       1.5927     12.38  |          |     Q   | V         |          |
  5+ 0       1.6820     12.96  |          |      Q  |  V        |          |
  5+ 5       1.7825     14.59  |          |       Q |    V      |          |
  5+10       1.9023     17.40  |          |         |  Q  V     |          |
  5+15       2.0399     19.97  |          |         |     Q V   |          |
  5+20       2.1919     22.07  |          |         |        Q|V         |
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    5+25       2.3612     24.59  |          |          |          | QV        |
    5+30       2.5586     28.66  |          |          |          |     V Q   |
    5+35       2.7128     22.40  |          |          |        Q|       V   |
    5+40       2.7805      9.83  |          |  Q       |          |         V|
    5+45       2.8088      4.10  |     Q    |          |          |         V|
    5+50       2.8201      1.65  |  Q       |          |          |         V|
    5+55       2.8240      0.56  Q          |          |          |         V|
    6+ 0       2.8257      0.24  Q          |          |          |         V|
    6+ 5       2.8264      0.10  Q          |          |          |         V|
    6+10       2.8265      0.03  Q          |          |          |         V|
    6+15       2.8266      0.01  Q          |          |          |         V|
    6+20       2.8266      0.00  Q          |          |          |          V
-------------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex102410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

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Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.80	51.17

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	5.00	142.15

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 3.117(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 3.116(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.025	(0.207)	0.022	0.002
2	0.17	0.07	0.025	(0.207)	0.022	0.002
3	0.25	0.07	0.025	(0.206)	0.022	0.002
4	0.33	0.10	0.037	(0.205)	0.034	0.004
5	0.42	0.10	0.037	(0.204)	0.034	0.004
6	0.50	0.10	0.037	(0.203)	0.034	0.004
7	0.58	0.10	0.037	(0.203)	0.034	0.004
8	0.67	0.10	0.037	(0.202)	0.034	0.004
9	0.75	0.10	0.037	(0.201)	0.034	0.004
10	0.83	0.13	0.050	(0.200)	0.045	0.005
11	0.92	0.13	0.050	(0.199)	0.045	0.005
12	1.00	0.13	0.050	(0.199)	0.045	0.005
13	1.08	0.10	0.037	(0.198)	0.034	0.004
14	1.17	0.10	0.037	(0.197)	0.034	0.004
15	1.25	0.10	0.037	(0.196)	0.034	0.004
16	1.33	0.10	0.037	(0.196)	0.034	0.004
17	1.42	0.10	0.037	(0.195)	0.034	0.004
18	1.50	0.10	0.037	(0.194)	0.034	0.004
19	1.58	0.10	0.037	(0.193)	0.034	0.004
20	1.67	0.10	0.037	(0.192)	0.034	0.004
21	1.75	0.10	0.037	(0.192)	0.034	0.004
22	1.83	0.13	0.050	(0.191)	0.045	0.005
23	1.92	0.13	0.050	(0.190)	0.045	0.005
24	2.00	0.13	0.050	(0.189)	0.045	0.005
25	2.08	0.13	0.050	(0.189)	0.045	0.005
26	2.17	0.13	0.050	(0.188)	0.045	0.005
27	2.25	0.13	0.050	(0.187)	0.045	0.005
28	2.33	0.13	0.050	(0.186)	0.045	0.005
29	2.42	0.13	0.050	(0.186)	0.045	0.005
30	2.50	0.13	0.050	(0.185)	0.045	0.005
31	2.58	0.17	0.062	(0.184)	0.056	0.006
32	2.67	0.17	0.062	(0.183)	0.056	0.006
33	2.75	0.17	0.062	(0.183)	0.056	0.006
34	2.83	0.17	0.062	(0.182)	0.056	0.006
35	2.92	0.17	0.062	(0.181)	0.056	0.006
36	3.00	0.17	0.062	(0.180)	0.056	0.006
37	3.08	0.17	0.062	(0.180)	0.056	0.006
38	3.17	0.17	0.062	(0.179)	0.056	0.006
39	3.25	0.17	0.062	(0.178)	0.056	0.006
40	3.33	0.17	0.062	(0.177)	0.056	0.006
41	3.42	0.17	0.062	(0.177)	0.056	0.006
42	3.50	0.17	0.062	(0.176)	0.056	0.006
43	3.58	0.17	0.062	(0.175)	0.056	0.006
44	3.67	0.17	0.062	(0.174)	0.056	0.006
45	3.75	0.17	0.062	(0.174)	0.056	0.006
46	3.83	0.20	0.075	(0.173)	0.067	0.007
47	3.92	0.20	0.075	(0.172)	0.067	0.007
48	4.00	0.20	0.075	(0.171)	0.067	0.007
49	4.08	0.20	0.075	(0.171)	0.067	0.007
50	4.17	0.20	0.075	(0.170)	0.067	0.007
51	4.25	0.20	0.075	(0.169)	0.067	0.007
52	4.33	0.23	0.087	(0.169)	0.079	0.009
53	4.42	0.23	0.087	(0.168)	0.079	0.009
54	4.50	0.23	0.087	(0.167)	0.079	0.009
55	4.58	0.23	0.087	(0.166)	0.079	0.009
56	4.67	0.23	0.087	(0.166)	0.079	0.009
57	4.75	0.23	0.087	(0.165)	0.079	0.009
58	4.83	0.27	0.100	(0.164)	0.090	0.010
59	4.92	0.27	0.100	(0.164)	0.090	0.010
60	5.00	0.27	0.100	(0.163)	0.090	0.010
61	5.08	0.20	0.075	(0.162)	0.067	0.007
62	5.17	0.20	0.075	(0.161)	0.067	0.007
63	5.25	0.20	0.075	(0.161)	0.067	0.007
64	5.33	0.23	0.087	(0.160)	0.079	0.009
65	5.42	0.23	0.087	(0.159)	0.079	0.009
66	5.50	0.23	0.087	(0.159)	0.079	0.009
67	5.58	0.27	0.100	(0.158)	0.090	0.010
68	5.67	0.27	0.100	(0.157)	0.090	0.010
69	5.75	0.27	0.100	(0.157)	0.090	0.010
70	5.83	0.27	0.100	(0.156)	0.090	0.010
71	5.92	0.27	0.100	(0.155)	0.090	0.010

72	6.00	0.27	0.100	(	0.154)	0.090		0.010
73	6.08	0.30	0.112	(	0.154)	0.101		0.011
74	6.17	0.30	0.112	(	0.153)	0.101		0.011
75	6.25	0.30	0.112	(	0.152)	0.101		0.011
76	6.33	0.30	0.112	(	0.152)	0.101		0.011
77	6.42	0.30	0.112	(	0.151)	0.101		0.011
78	6.50	0.30	0.112	(	0.150)	0.101		0.011
79	6.58	0.33	0.125	(	0.150)	0.112		0.012
80	6.67	0.33	0.125	(	0.149)	0.112		0.012
81	6.75	0.33	0.125	(	0.148)	0.112		0.012
82	6.83	0.33	0.125	(	0.148)	0.112		0.012
83	6.92	0.33	0.125	(	0.147)	0.112		0.012
84	7.00	0.33	0.125	(	0.146)	0.112		0.012
85	7.08	0.33	0.125	(	0.146)	0.112		0.012
86	7.17	0.33	0.125	(	0.145)	0.112		0.012
87	7.25	0.33	0.125	(	0.144)	0.112		0.012
88	7.33	0.37	0.137	(	0.144)	0.123		0.014
89	7.42	0.37	0.137	(	0.143)	0.123		0.014
90	7.50	0.37	0.137	(	0.142)	0.123		0.014
91	7.58	0.40	0.150	(	0.142)	0.135		0.015
92	7.67	0.40	0.150	(	0.141)	0.135		0.015
93	7.75	0.40	0.150	(	0.140)	0.135		0.015
94	7.83	0.43	0.162		0.140	(0.146)		0.022
95	7.92	0.43	0.162		0.139	(0.146)		0.023
96	8.00	0.43	0.162		0.138	(0.146)		0.024
97	8.08	0.50	0.187		0.138	(0.168)		0.049
98	8.17	0.50	0.187		0.137	(0.168)		0.050
99	8.25	0.50	0.187		0.137	(0.168)		0.050
100	8.33	0.50	0.187		0.136	(0.168)		0.051
101	8.42	0.50	0.187		0.135	(0.168)		0.052
102	8.50	0.50	0.187		0.135	(0.168)		0.052
103	8.58	0.53	0.199		0.134	(0.180)		0.065
104	8.67	0.53	0.199		0.133	(0.180)		0.066
105	8.75	0.53	0.199		0.133	(0.180)		0.067
106	8.83	0.57	0.212		0.132	(0.191)		0.080
107	8.92	0.57	0.212		0.131	(0.191)		0.080
108	9.00	0.57	0.212		0.131	(0.191)		0.081
109	9.08	0.63	0.237		0.130	(0.213)		0.107
110	9.17	0.63	0.237		0.130	(0.213)		0.107
111	9.25	0.63	0.237		0.129	(0.213)		0.108
112	9.33	0.67	0.249		0.128	(0.224)		0.121
113	9.42	0.67	0.249		0.128	(0.224)		0.122
114	9.50	0.67	0.249		0.127	(0.224)		0.122
115	9.58	0.70	0.262		0.127	(0.236)		0.135
116	9.67	0.70	0.262		0.126	(0.236)		0.136
117	9.75	0.70	0.262		0.125	(0.236)		0.136
118	9.83	0.73	0.274		0.125	(0.247)		0.149
119	9.92	0.73	0.274		0.124	(0.247)		0.150
120	10.00	0.73	0.274		0.124	(0.247)		0.151
121	10.08	0.50	0.187		0.123	(0.168)		0.064
122	10.17	0.50	0.187		0.122	(0.168)		0.065
123	10.25	0.50	0.187		0.122	(0.168)		0.065
124	10.33	0.50	0.187		0.121	(0.168)		0.066
125	10.42	0.50	0.187		0.121	(0.168)		0.066
126	10.50	0.50	0.187		0.120	(0.168)		0.067
127	10.58	0.67	0.249		0.119	(0.224)		0.130
128	10.67	0.67	0.249		0.119	(0.224)		0.130
129	10.75	0.67	0.249		0.118	(0.224)		0.131
130	10.83	0.67	0.249		0.118	(0.224)		0.132
131	10.92	0.67	0.249		0.117	(0.224)		0.132
132	11.00	0.67	0.249		0.117	(0.224)		0.133
133	11.08	0.63	0.237		0.116	(0.213)		0.121
134	11.17	0.63	0.237		0.115	(0.213)		0.121
135	11.25	0.63	0.237		0.115	(0.213)		0.122
136	11.33	0.63	0.237		0.114	(0.213)		0.123
137	11.42	0.63	0.237		0.114	(0.213)		0.123
138	11.50	0.63	0.237		0.113	(0.213)		0.124
139	11.58	0.57	0.212		0.113	(0.191)		0.099
140	11.67	0.57	0.212		0.112	(0.191)		0.100
141	11.75	0.57	0.212		0.111	(0.191)		0.100
142	11.83	0.60	0.224		0.111	(0.202)		0.114
143	11.92	0.60	0.224		0.110	(0.202)		0.114
144	12.00	0.60	0.224		0.110	(0.202)		0.115
145	12.08	0.83	0.312		0.109	(0.280)		0.202
146	12.17	0.83	0.312		0.109	(0.280)		0.203
147	12.25	0.83	0.312		0.108	(0.280)		0.204
148	12.33	0.87	0.324		0.108	(0.292)		0.217
149	12.42	0.87	0.324		0.107	(0.292)		0.217
150	12.50	0.87	0.324		0.107	(0.292)		0.218
151	12.58	0.93	0.349		0.106	(0.314)		0.243
152	12.67	0.93	0.349		0.105	(0.314)		0.244
153	12.75	0.93	0.349		0.105	(0.314)		0.244
154	12.83	0.97	0.361		0.104	(0.325)		0.257
155	12.92	0.97	0.361		0.104	(0.325)		0.258
156	13.00	0.97	0.361		0.103	(0.325)		0.258
157	13.08	1.13	0.424		0.103	(0.381)		0.321

158	13.17	1.13	0.424		0.102	(0.381)	0.322
159	13.25	1.13	0.424		0.102	(0.381)	0.322
160	13.33	1.13	0.424		0.101	(0.381)	0.323
161	13.42	1.13	0.424		0.101	(0.381)	0.323
162	13.50	1.13	0.424		0.100	(0.381)	0.324
163	13.58	0.77	0.287		0.100	(0.258)	0.187
164	13.67	0.77	0.287		0.099	(0.258)	0.188
165	13.75	0.77	0.287		0.099	(0.258)	0.188
166	13.83	0.77	0.287		0.098	(0.258)	0.189
167	13.92	0.77	0.287		0.098	(0.258)	0.189
168	14.00	0.77	0.287		0.097	(0.258)	0.190
169	14.08	0.90	0.337		0.097	(0.303)	0.240
170	14.17	0.90	0.337		0.096	(0.303)	0.240
171	14.25	0.90	0.337		0.096	(0.303)	0.241
172	14.33	0.87	0.324		0.095	(0.292)	0.229
173	14.42	0.87	0.324		0.095	(0.292)	0.229
174	14.50	0.87	0.324		0.094	(0.292)	0.230
175	14.58	0.87	0.324		0.094	(0.292)	0.230
176	14.67	0.87	0.324		0.093	(0.292)	0.231
177	14.75	0.87	0.324		0.093	(0.292)	0.231
178	14.83	0.83	0.312		0.092	(0.280)	0.219
179	14.92	0.83	0.312		0.092	(0.280)	0.220
180	15.00	0.83	0.312		0.091	(0.280)	0.220
181	15.08	0.80	0.299		0.091	(0.269)	0.208
182	15.17	0.80	0.299		0.090	(0.269)	0.209
183	15.25	0.80	0.299		0.090	(0.269)	0.209
184	15.33	0.77	0.287		0.090	(0.258)	0.197
185	15.42	0.77	0.287		0.089	(0.258)	0.198
186	15.50	0.77	0.287		0.089	(0.258)	0.198
187	15.58	0.63	0.237		0.088	(0.213)	0.149
188	15.67	0.63	0.237		0.088	(0.213)	0.149
189	15.75	0.63	0.237		0.087	(0.213)	0.150
190	15.83	0.63	0.237		0.087	(0.213)	0.150
191	15.92	0.63	0.237		0.086	(0.213)	0.150
192	16.00	0.63	0.237		0.086	(0.213)	0.151
193	16.08	0.13	0.050	(0.085)		0.045	0.005
194	16.17	0.13	0.050	(0.085)		0.045	0.005
195	16.25	0.13	0.050	(0.085)		0.045	0.005
196	16.33	0.13	0.050	(0.084)		0.045	0.005
197	16.42	0.13	0.050	(0.084)		0.045	0.005
198	16.50	0.13	0.050	(0.083)		0.045	0.005
199	16.58	0.10	0.037	(0.083)		0.034	0.004
200	16.67	0.10	0.037	(0.082)		0.034	0.004
201	16.75	0.10	0.037	(0.082)		0.034	0.004
202	16.83	0.10	0.037	(0.082)		0.034	0.004
203	16.92	0.10	0.037	(0.081)		0.034	0.004
204	17.00	0.10	0.037	(0.081)		0.034	0.004
205	17.08	0.17	0.062	(0.080)		0.056	0.006
206	17.17	0.17	0.062	(0.080)		0.056	0.006
207	17.25	0.17	0.062	(0.080)		0.056	0.006
208	17.33	0.17	0.062	(0.079)		0.056	0.006
209	17.42	0.17	0.062	(0.079)		0.056	0.006
210	17.50	0.17	0.062	(0.078)		0.056	0.006
211	17.58	0.17	0.062	(0.078)		0.056	0.006
212	17.67	0.17	0.062	(0.078)		0.056	0.006
213	17.75	0.17	0.062	(0.077)		0.056	0.006
214	17.83	0.13	0.050	(0.077)		0.045	0.005
215	17.92	0.13	0.050	(0.076)		0.045	0.005
216	18.00	0.13	0.050	(0.076)		0.045	0.005
217	18.08	0.13	0.050	(0.076)		0.045	0.005
218	18.17	0.13	0.050	(0.075)		0.045	0.005
219	18.25	0.13	0.050	(0.075)		0.045	0.005
220	18.33	0.13	0.050	(0.075)		0.045	0.005
221	18.42	0.13	0.050	(0.074)		0.045	0.005
222	18.50	0.13	0.050	(0.074)		0.045	0.005
223	18.58	0.10	0.037	(0.074)		0.034	0.004
224	18.67	0.10	0.037	(0.073)		0.034	0.004
225	18.75	0.10	0.037	(0.073)		0.034	0.004
226	18.83	0.07	0.025	(0.072)		0.022	0.002
227	18.92	0.07	0.025	(0.072)		0.022	0.002
228	19.00	0.07	0.025	(0.072)		0.022	0.002
229	19.08	0.10	0.037	(0.071)		0.034	0.004
230	19.17	0.10	0.037	(0.071)		0.034	0.004
231	19.25	0.10	0.037	(0.071)		0.034	0.004
232	19.33	0.13	0.050	(0.070)		0.045	0.005
233	19.42	0.13	0.050	(0.070)		0.045	0.005
234	19.50	0.13	0.050	(0.070)		0.045	0.005
235	19.58	0.10	0.037	(0.069)		0.034	0.004
236	19.67	0.10	0.037	(0.069)		0.034	0.004
237	19.75	0.10	0.037	(0.069)		0.034	0.004
238	19.83	0.07	0.025	(0.069)		0.022	0.002
239	19.92	0.07	0.025	(0.068)		0.022	0.002
240	20.00	0.07	0.025	(0.068)		0.022	0.002
241	20.08	0.10	0.037	(0.068)		0.034	0.004
242	20.17	0.10	0.037	(0.067)		0.034	0.004
243	20.25	0.10	0.037	(0.067)		0.034	0.004

244	20.33	0.10	0.037	(0.067)	0.034	0.004
245	20.42	0.10	0.037	(0.066)	0.034	0.004
246	20.50	0.10	0.037	(0.066)	0.034	0.004
247	20.58	0.10	0.037	(0.066)	0.034	0.004
248	20.67	0.10	0.037	(0.066)	0.034	0.004
249	20.75	0.10	0.037	(0.065)	0.034	0.004
250	20.83	0.07	0.025	(0.065)	0.022	0.002
251	20.92	0.07	0.025	(0.065)	0.022	0.002
252	21.00	0.07	0.025	(0.065)	0.022	0.002
253	21.08	0.10	0.037	(0.064)	0.034	0.004
254	21.17	0.10	0.037	(0.064)	0.034	0.004
255	21.25	0.10	0.037	(0.064)	0.034	0.004
256	21.33	0.07	0.025	(0.064)	0.022	0.002
257	21.42	0.07	0.025	(0.063)	0.022	0.002
258	21.50	0.07	0.025	(0.063)	0.022	0.002
259	21.58	0.10	0.037	(0.063)	0.034	0.004
260	21.67	0.10	0.037	(0.063)	0.034	0.004
261	21.75	0.10	0.037	(0.062)	0.034	0.004
262	21.83	0.07	0.025	(0.062)	0.022	0.002
263	21.92	0.07	0.025	(0.062)	0.022	0.002
264	22.00	0.07	0.025	(0.062)	0.022	0.002
265	22.08	0.10	0.037	(0.062)	0.034	0.004
266	22.17	0.10	0.037	(0.061)	0.034	0.004
267	22.25	0.10	0.037	(0.061)	0.034	0.004
268	22.33	0.07	0.025	(0.061)	0.022	0.002
269	22.42	0.07	0.025	(0.061)	0.022	0.002
270	22.50	0.07	0.025	(0.061)	0.022	0.002
271	22.58	0.07	0.025	(0.060)	0.022	0.002
272	22.67	0.07	0.025	(0.060)	0.022	0.002
273	22.75	0.07	0.025	(0.060)	0.022	0.002
274	22.83	0.07	0.025	(0.060)	0.022	0.002
275	22.92	0.07	0.025	(0.060)	0.022	0.002
276	23.00	0.07	0.025	(0.060)	0.022	0.002
277	23.08	0.07	0.025	(0.060)	0.022	0.002
278	23.17	0.07	0.025	(0.059)	0.022	0.002
279	23.25	0.07	0.025	(0.059)	0.022	0.002
280	23.33	0.07	0.025	(0.059)	0.022	0.002
281	23.42	0.07	0.025	(0.059)	0.022	0.002
282	23.50	0.07	0.025	(0.059)	0.022	0.002
283	23.58	0.07	0.025	(0.059)	0.022	0.002
284	23.67	0.07	0.025	(0.059)	0.022	0.002
285	23.75	0.07	0.025	(0.059)	0.022	0.002
286	23.83	0.07	0.025	(0.059)	0.022	0.002
287	23.92	0.07	0.025	(0.059)	0.022	0.002
288	24.00	0.07	0.025	(0.059)	0.022	0.002

(Loss Rate Not Used)

Sum = 100.0 Sum = 16.7

Flood volume = Effective rainfall 1.39(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 3.3(Ac.Ft)
Total soil loss = 1.72(In)
Total soil loss = 4.087(Ac.Ft)
Total rainfall = 3.12(In)
Flood volume = 143594.9 Cubic Feet
Total soil loss = 178013.5 Cubic Feet

Peak flow rate of this hydrograph = 9.264(CFS)

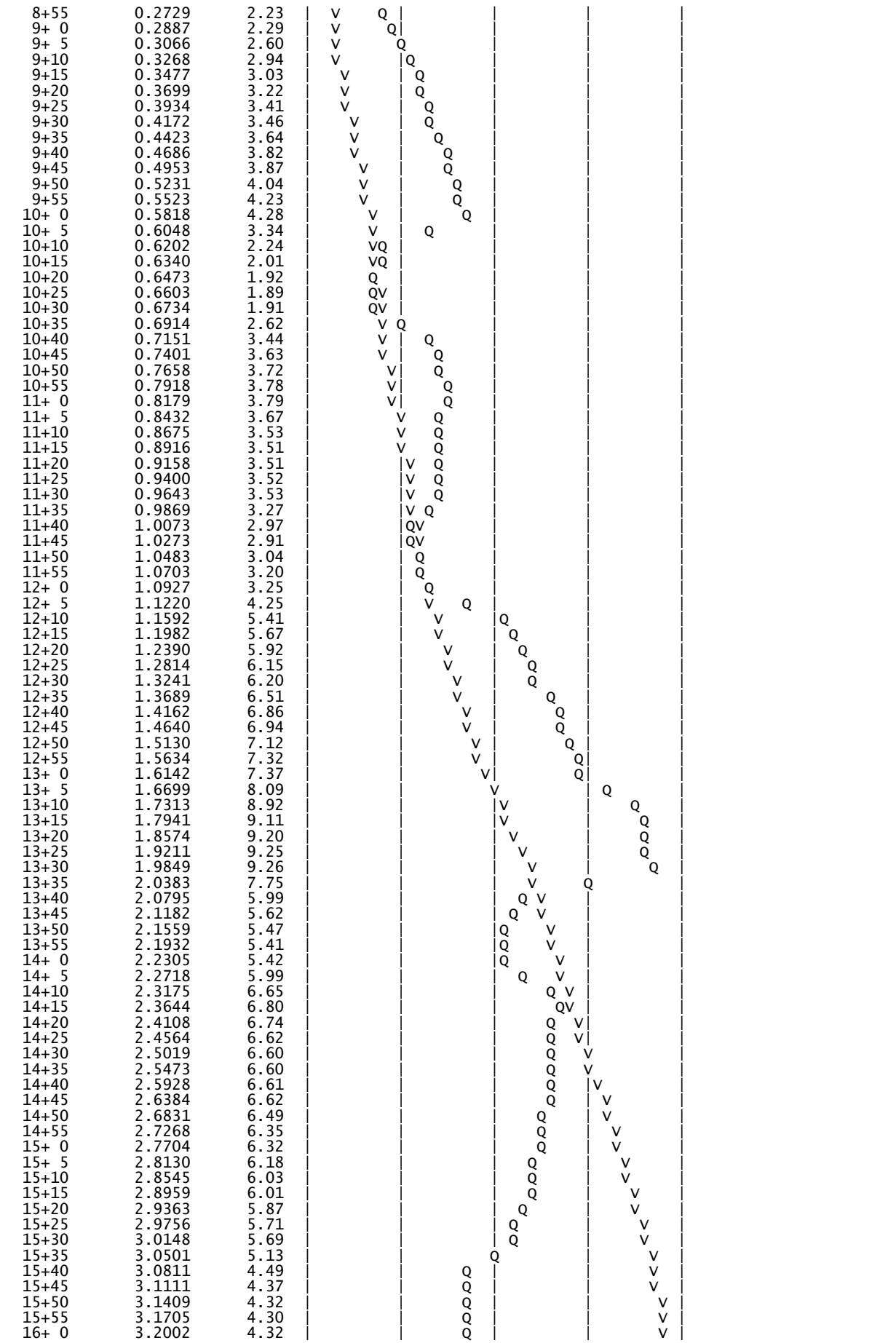
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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0002	0.03	Q				
0+10	0.0006	0.06	Q				
0+15	0.0011	0.07	Q				
0+20	0.0016	0.08	Q				
0+25	0.0023	0.10	Q				
0+30	0.0031	0.11	Q				
0+35	0.0038	0.11	Q				
0+40	0.0045	0.11	Q				
0+45	0.0053	0.11	Q				
0+50	0.0061	0.12	Q				
0+55	0.0071	0.14	Q				
1+ 0	0.0080	0.14	Q				
1+ 5	0.0089	0.13	Q				
1+10	0.0097	0.11	Q				
1+15	0.0104	0.11	Q				
1+20	0.0112	0.11	Q				
1+25	0.0119	0.11	Q				
1+30	0.0127	0.11	Q				
1+35	0.0134	0.11	Q				
1+40	0.0141	0.11	Q				

1+45	0.0149	0.11	Q	|	|	|	|
1+50	0.0157	0.12	Q	|	|	|	|
1+55	0.0167	0.14	Q	|	|	|	|
2+ 0	0.0176	0.14	Q	|	|	|	|
2+ 5	0.0186	0.14	Q	|	|	|	|
2+10	0.0196	0.14	Q	|	|	|	|
2+15	0.0206	0.14	Q	|	|	|	|
2+20	0.0216	0.14	Q	|	|	|	|
2+25	0.0225	0.14	Q	|	|	|	|
2+30	0.0235	0.14	Q	|	|	|	|
2+35	0.0246	0.16	Q	|	|	|	|
2+40	0.0258	0.17	Q	|	|	|	|
2+45	0.0270	0.18	Q	|	|	|	|
2+50	0.0282	0.18	Q	|	|	|	|
2+55	0.0295	0.18	Q	|	|	|	|
3+ 0	0.0307	0.18	Q	|	|	|	|
3+ 5	0.0319	0.18	Q	|	|	|	|
3+10	0.0332	0.18	Q	|	|	|	|
3+15	0.0344	0.18	Q	|	|	|	|
3+20	0.0356	0.18	Q	|	|	|	|
3+25	0.0369	0.18	Q	|	|	|	|
3+30	0.0381	0.18	Q	|	|	|	|
3+35	0.0393	0.18	Q	|	|	|	|
3+40	0.0405	0.18	Q	|	|	|	|
3+45	0.0418	0.18	Q	|	|	|	|
3+50	0.0431	0.19	Q	|	|	|	|
3+55	0.0445	0.21	Q	|	|	|	|
4+ 0	0.0460	0.21	Q	|	|	|	|
4+ 5	0.0475	0.21	Q	|	|	|	|
4+10	0.0489	0.21	Q	|	|	|	|
4+15	0.0504	0.21	Q	|	|	|	|
4+20	0.0520	0.23	Q	|	|	|	|
4+25	0.0537	0.24	Q	|	|	|	|
4+30	0.0554	0.25	Q	|	|	|	|
4+35	0.0571	0.25	Q	|	|	|	|
4+40	0.0588	0.25	VQ	|	|	|	|
4+45	0.0605	0.25	VQ	|	|	|	|
4+50	0.0624	0.26	VQ	|	|	|	|
4+55	0.0643	0.28	VQ	|	|	|	|
5+ 0	0.0663	0.28	VQ	|	|	|	|
5+ 5	0.0680	0.26	VQ	|	|	|	|
5+10	0.0696	0.23	Q	|	|	|	|
5+15	0.0711	0.22	Q	|	|	|	|
5+20	0.0727	0.23	Q	|	|	|	|
5+25	0.0744	0.24	Q	|	|	|	|
5+30	0.0761	0.25	Q	|	|	|	|
5+35	0.0779	0.26	VQ	|	|	|	|
5+40	0.0798	0.28	VQ	|	|	|	|
5+45	0.0818	0.28	VQ	|	|	|	|
5+50	0.0837	0.29	|Q	|	|	|	|
5+55	0.0857	0.29	|Q	|	|	|	|
6+ 0	0.0877	0.29	|Q	|	|	|	|
6+ 5	0.0897	0.30	|Q	|	|	|	|
6+10	0.0919	0.32	|Q	|	|	|	|
6+15	0.0941	0.32	|Q	|	|	|	|
6+20	0.0963	0.32	|Q	|	|	|	|
6+25	0.0985	0.32	|Q	|	|	|	|
6+30	0.1007	0.32	|Q	|	|	|	|
6+35	0.1030	0.34	|Q	|	|	|	|
6+40	0.1055	0.35	|Q	|	|	|	|
6+45	0.1079	0.36	|Q	|	|	|	|
6+50	0.1104	0.36	|Q	|	|	|	|
6+55	0.1128	0.36	|Q	|	|	|	|
7+ 0	0.1153	0.36	|Q	|	|	|	|
7+ 5	0.1178	0.36	|Q	|	|	|	|
7+10	0.1202	0.36	|Q	|	|	|	|
7+15	0.1227	0.36	|Q	|	|	|	|
7+20	0.1252	0.37	|Q	|	|	|	|
7+25	0.1279	0.39	|Q	|	|	|	|
7+30	0.1306	0.39	|Q	|	|	|	|
7+35	0.1334	0.41	|Q	|	|	|	|
7+40	0.1363	0.42	|Q	|	|	|	|
7+45	0.1392	0.43	|Q	|	|	|	|
7+50	0.1428	0.51	|VQ	|	|	|	|
7+55	0.1470	0.61	|VQ	|	|	|	|
8+ 0	0.1514	0.65	|VQ	|	|	|	|
8+ 5	0.1580	0.95	|V Q	|	|	|	|
8+10	0.1669	1.30	| V Q	|	|	|	|
8+15	0.1765	1.39	| V Q	|	|	|	|
8+20	0.1864	1.43	| V Q	|	|	|	|
8+25	0.1965	1.47	| V Q	|	|	|	|
8+30	0.2067	1.49	| V Q	|	|	|	|
8+35	0.2180	1.64	| V Q	|	|	|	|
8+40	0.2306	1.82	| V Q	|	|	|	|
8+45	0.2435	1.87	| V Q	|	|	|	|
8+50	0.2576	2.05	| V Q	|	|	|	|



8+55	0.2729	2.23	
9+ 0	0.2887	2.29	
9+ 5	0.3066	2.60	
9+10	0.3268	2.94	
9+15	0.3477	3.03	
9+20	0.3699	3.22	
9+25	0.3934	3.41	
9+30	0.4172	3.46	
9+35	0.4423	3.64	
9+40	0.4686	3.82	
9+45	0.4953	3.87	
9+50	0.5231	4.04	
9+55	0.5523	4.23	
10+ 0	0.5818	4.28	
10+ 5	0.6048	3.34	
10+10	0.6202	2.24	
10+15	0.6340	2.01	
10+20	0.6473	1.92	
10+25	0.6603	1.89	
10+30	0.6734	1.91	
10+35	0.6914	2.62	
10+40	0.7151	3.44	
10+45	0.7401	3.63	
10+50	0.7658	3.72	
10+55	0.7918	3.78	
11+ 0	0.8179	3.79	
11+ 5	0.8432	3.67	
11+10	0.8675	3.53	
11+15	0.8916	3.51	
11+20	0.9158	3.51	
11+25	0.9400	3.52	
11+30	0.9643	3.53	
11+35	0.9869	3.27	
11+40	1.0073	2.97	
11+45	1.0273	2.91	
11+50	1.0483	3.04	
11+55	1.0703	3.20	
12+ 0	1.0927	3.25	
12+ 5	1.1220	4.25	
12+10	1.1592	5.41	
12+15	1.1982	5.67	
12+20	1.2390	5.92	
12+25	1.2814	6.15	
12+30	1.3241	6.20	
12+35	1.3689	6.51	
12+40	1.4162	6.86	
12+45	1.4640	6.94	
12+50	1.5130	7.12	
12+55	1.5634	7.32	
13+ 0	1.6142	7.37	
13+ 5	1.6699	8.09	
13+10	1.7313	8.92	
13+15	1.7941	9.11	
13+20	1.8574	9.20	
13+25	1.9211	9.25	
13+30	1.9849	9.26	
13+35	2.0383	7.75	
13+40	2.0795	5.99	
13+45	2.1182	5.62	
13+50	2.1559	5.47	
13+55	2.1932	5.41	
14+ 0	2.2305	5.42	
14+ 5	2.2718	5.99	
14+10	2.3175	6.65	
14+15	2.3644	6.80	
14+20	2.4108	6.74	
14+25	2.4564	6.62	
14+30	2.5019	6.60	
14+35	2.5473	6.60	
14+40	2.5928	6.61	
14+45	2.6384	6.62	
14+50	2.6831	6.49	
14+55	2.7268	6.35	
15+ 0	2.7704	6.32	
15+ 5	2.8130	6.18	
15+10	2.8545	6.03	
15+15	2.8959	6.01	
15+20	2.9363	5.87	
15+25	2.9756	5.71	
15+30	3.0148	5.69	
15+35	3.0501	5.13	
15+40	3.0811	4.49	
15+45	3.1111	4.37	
15+50	3.1409	4.32	
15+55	3.1705	4.30	
16+ 0	3.2002	4.32	

16+ 5	3.2188	2.69	|	Q	|	|	V|
16+10	3.2244	0.81	| Q	|	|	|	V|
16+15	3.2271	0.40	|Q	|	|	|	V|
16+20	3.2287	0.23	Q	|	|	|	V|
16+25	3.2297	0.14	Q	|	|	|	V|
16+30	3.2307	0.14	Q	|	|	|	V|
16+35	3.2316	0.13	Q	|	|	|	V|
16+40	3.2323	0.11	Q	|	|	|	V|
16+45	3.2331	0.11	Q	|	|	|	V|
16+50	3.2338	0.11	Q	|	|	|	V|
16+55	3.2346	0.11	Q	|	|	|	V|
17+ 0	3.2353	0.11	Q	|	|	|	V|
17+ 5	3.2362	0.14	Q	|	|	|	V|
17+10	3.2374	0.17	Q	|	|	|	V|
17+15	3.2386	0.17	Q	|	|	|	V|
17+20	3.2398	0.18	Q	|	|	|	V|
17+25	3.2410	0.18	Q	|	|	|	V|
17+30	3.2423	0.18	Q	|	|	|	V|
17+35	3.2435	0.18	Q	|	|	|	V|
17+40	3.2447	0.18	Q	|	|	|	V|
17+45	3.2460	0.18	Q	|	|	|	V|
17+50	3.2471	0.16	Q	|	|	|	V|
17+55	3.2481	0.15	Q	|	|	|	V|
18+ 0	3.2491	0.15	Q	|	|	|	V|
18+ 5	3.2501	0.14	Q	|	|	|	V|
18+10	3.2511	0.14	Q	|	|	|	V|
18+15	3.2521	0.14	Q	|	|	|	V|
18+20	3.2531	0.14	Q	|	|	|	V|
18+25	3.2541	0.14	Q	|	|	|	V|
18+30	3.2550	0.14	Q	|	|	|	V|
18+35	3.2559	0.13	Q	|	|	|	V|
18+40	3.2567	0.11	Q	|	|	|	V|
18+45	3.2575	0.11	Q	|	|	|	V|
18+50	3.2581	0.09	Q	|	|	|	V|
18+55	3.2586	0.08	Q	|	|	|	V|
19+ 0	3.2591	0.07	Q	|	|	|	V|
19+ 5	3.2597	0.09	Q	|	|	|	V|
19+10	3.2604	0.10	Q	|	|	|	V|
19+15	3.2612	0.11	Q	|	|	|	V|
19+20	3.2620	0.12	Q	|	|	|	V|
19+25	3.2629	0.14	Q	|	|	|	V|
19+30	3.2639	0.14	Q	|	|	|	V|
19+35	3.2648	0.13	Q	|	|	|	V|
19+40	3.2656	0.11	Q	|	|	|	V|
19+45	3.2663	0.11	Q	|	|	|	V|
19+50	3.2670	0.09	Q	|	|	|	V|
19+55	3.2675	0.08	Q	|	|	|	V|
20+ 0	3.2680	0.07	Q	|	|	|	V|
20+ 5	3.2686	0.09	Q	|	|	|	V|
20+10	3.2693	0.10	Q	|	|	|	V|
20+15	3.2700	0.11	Q	|	|	|	V|
20+20	3.2708	0.11	Q	|	|	|	V|
20+25	3.2715	0.11	Q	|	|	|	V|
20+30	3.2722	0.11	Q	|	|	|	V|
20+35	3.2730	0.11	Q	|	|	|	V|
20+40	3.2737	0.11	Q	|	|	|	V|
20+45	3.2744	0.11	Q	|	|	|	V|
20+50	3.2751	0.09	Q	|	|	|	V|
20+55	3.2756	0.08	Q	|	|	|	V|
21+ 0	3.2761	0.07	Q	|	|	|	V|
21+ 5	3.2767	0.09	Q	|	|	|	V|
21+10	3.2774	0.10	Q	|	|	|	V|
21+15	3.2781	0.11	Q	|	|	|	V|
21+20	3.2788	0.09	Q	|	|	|	V|
21+25	3.2793	0.08	Q	|	|	|	V|
21+30	3.2798	0.07	Q	|	|	|	V|
21+35	3.2804	0.09	Q	|	|	|	V|
21+40	3.2811	0.10	Q	|	|	|	V|
21+45	3.2818	0.11	Q	|	|	|	V|
21+50	3.2825	0.09	Q	|	|	|	V|
21+55	3.2830	0.08	Q	|	|	|	V|
22+ 0	3.2835	0.07	Q	|	|	|	V|
22+ 5	3.2841	0.09	Q	|	|	|	V|
22+10	3.2848	0.10	Q	|	|	|	V|
22+15	3.2855	0.11	Q	|	|	|	V|
22+20	3.2862	0.09	Q	|	|	|	V|
22+25	3.2867	0.08	Q	|	|	|	V|
22+30	3.2872	0.07	Q	|	|	|	V|
22+35	3.2877	0.07	Q	|	|	|	V|
22+40	3.2882	0.07	Q	|	|	|	V|
22+45	3.2887	0.07	Q	|	|	|	V|
22+50	3.2892	0.07	Q	|	|	|	V|
22+55	3.2897	0.07	Q	|	|	|	V|
23+ 0	3.2902	0.07	Q	|	|	|	V|
23+ 5	3.2907	0.07	Q	|	|	|	V|
23+10	3.2911	0.07	Q	|	|	|	V|

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   23+15       3.2916      0.07  Q          |          |          |         v|
   23+20       3.2921      0.07  Q          |          |          |         v|
   23+25       3.2926      0.07  Q          |          |          |         v|
   23+30       3.2931      0.07  Q          |          |          |         v|
   23+35       3.2936      0.07  Q          |          |          |         v|
   23+40       3.2941      0.07  Q          |          |          |         v|
   23+45       3.2946      0.07  Q          |          |          |         v|
   23+50       3.2951      0.07  Q          |          |          |         v|
   23+55       3.2956      0.07  Q          |          |          |         v|
   24+ 0       3.2961      0.07  Q          |          |          |         v|
   24+ 5       3.2964      0.04  Q          |          |          |         v|
   24+10       3.2964      0.01  Q          |          |          |         v|
   24+15       3.2965      0.00  Q          |          |          |         v|
   24+20       3.2965      0.00  Q          |          |          |          v
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex1001100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.50	14.22

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.30	36.96

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.300(In)

Point rain (area averaged) = 1.300(In)
Areal adjustment factor = 99.97 %
Adjusted average point rain = 1.300(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

Slope of intensity-duration curve for a 1 hour storm =0.5500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
		Sum = 100.000	Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time		Pattern	Storm Rain	Loss rate(In./Hr)			Effective
	(Hr.)	Percent	(In/Hr)	Max		Low	(In/Hr)
1	0.08	3.30	0.515	0.117	(	0.463)	0.398
2	0.17	4.20	0.655	0.117	(	0.590)	0.538
3	0.25	4.40	0.686	0.117	(	0.618)	0.569
4	0.33	4.80	0.749	0.117	(	0.674)	0.632
5	0.42	5.20	0.811	0.117	(	0.730)	0.694
6	0.50	6.20	0.967	0.117	(	0.870)	0.850
7	0.58	6.80	1.061	0.117	(	0.954)	0.944
8	0.67	8.80	1.372	0.117	(	1.235)	1.255
9	0.75	13.90	2.168	0.117	(	1.951)	2.051
10	0.83	31.40	4.897	0.117	(	4.407)	4.780
11	0.92	7.20	1.123	0.117	(	1.011)	1.006
12	1.00	3.80	0.593	0.117	(	0.533)	0.476
		(Loss Rate Not Used)					
Sum =		100.0				Sum =	14.2

Flood volume = Effective rainfall 1.18(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 2.8(Ac.Ft)
Total soil loss = 0.12(In)
Total soil loss = 0.277(Ac.Ft)
Total rainfall = 1.30(In)
Flood volume = 122052.1 Cubic Feet
Total soil loss = 12074.5 Cubic Feet

Peak flow rate of this hydrograph = 85.010(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	22.5	45.0	67.5	90.0
0+ 5	0.0306	4.44	VQ				
0+10	0.1073	11.14	V Q				
0+15	0.2067	14.43	V Q				
0+20	0.3196	16.39	V Q				
0+25	0.4461	18.38	V Q				
0+30	0.5923	21.22	VQ				
0+35	0.7614	24.55	Q				
0+40	0.9665	29.79	Q				
0+45	1.2639	43.18	VQ				
0+50	1.8494	85.01	V		Q		
0+55	2.4059	80.80	VQ				
1+ 0	2.6465	34.94	Q		V		
1+ 5	2.7552	15.78	Q		V		
1+10	2.7921	5.35	Q		V		
1+15	2.8000	1.15	Q		V		
1+20	2.8019	0.28	Q		V		

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex1003100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.80	22.74

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	2.00	56.86

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 2.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 2.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.312	0.117	(0.281)	0.195
2	0.17	1.30	0.312	0.117	(0.281)	0.195
3	0.25	1.10	0.264	0.117	(0.238)	0.147
4	0.33	1.50	0.360	0.117	(0.324)	0.243
5	0.42	1.50	0.360	0.117	(0.324)	0.243
6	0.50	1.80	0.432	0.117	(0.389)	0.315
7	0.58	1.50	0.360	0.117	(0.324)	0.243
8	0.67	1.80	0.432	0.117	(0.389)	0.315
9	0.75	1.80	0.432	0.117	(0.389)	0.315
10	0.83	1.50	0.360	0.117	(0.324)	0.243
11	0.92	1.60	0.384	0.117	(0.346)	0.267
12	1.00	1.80	0.432	0.117	(0.389)	0.315
13	1.08	2.20	0.528	0.117	(0.475)	0.411
14	1.17	2.20	0.528	0.117	(0.475)	0.411
15	1.25	2.20	0.528	0.117	(0.475)	0.411
16	1.33	2.00	0.480	0.117	(0.432)	0.363
17	1.42	2.60	0.624	0.117	(0.562)	0.507
18	1.50	2.70	0.648	0.117	(0.583)	0.531
19	1.58	2.40	0.576	0.117	(0.518)	0.459
20	1.67	2.70	0.648	0.117	(0.583)	0.531
21	1.75	3.30	0.792	0.117	(0.713)	0.675
22	1.83	3.10	0.744	0.117	(0.670)	0.627
23	1.92	2.90	0.696	0.117	(0.626)	0.579
24	2.00	3.00	0.720	0.117	(0.648)	0.603
25	2.08	3.10	0.744	0.117	(0.670)	0.627
26	2.17	4.20	1.008	0.117	(0.907)	0.891
27	2.25	5.00	1.200	0.117	(1.080)	1.083
28	2.33	3.50	0.840	0.117	(0.756)	0.723
29	2.42	6.80	1.632	0.117	(1.469)	1.515
30	2.50	7.30	1.752	0.117	(1.577)	1.635
31	2.58	8.20	1.968	0.117	(1.771)	1.851
32	2.67	5.90	1.416	0.117	(1.274)	1.299
33	2.75	2.00	0.480	0.117	(0.432)	0.363
34	2.83	1.80	0.432	0.117	(0.389)	0.315
35	2.92	1.80	0.432	0.117	(0.389)	0.315
36	3.00	0.60	0.144	0.117	(0.130)	0.027
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	19.8

Flood volume = Effective rainfall 1.65(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 3.9(Ac.Ft)
Total soil loss = 0.35(In)
Total soil loss = 0.832(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 170152.6 Cubic Feet
Total soil loss = 36223.5 Cubic Feet

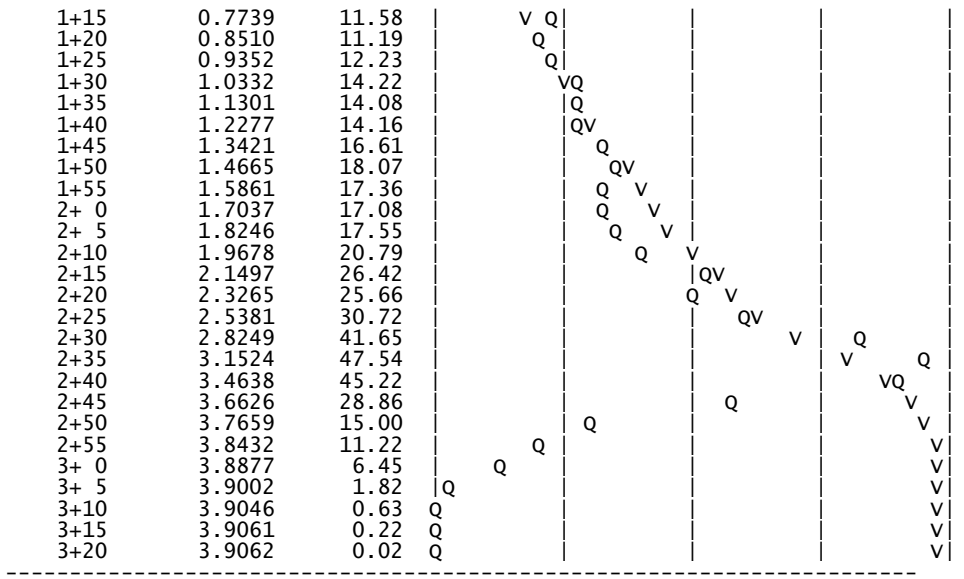
Peak flow rate of this hydrograph = 47.544(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	12.5	25.0	37.5	50.0
0+ 5	0.0150	2.18	VQ				
0+10	0.0473	4.70	V Q				
0+15	0.0798	4.71	V Q				
0+20	0.1169	5.39	V Q				
0+25	0.1624	6.61	V Q				
0+30	0.2149	7.63	V Q				
0+35	0.2689	7.84	V Q				
0+40	0.3238	7.97	V Q				
0+45	0.3843	8.78	V Q				
0+50	0.4404	8.14	V Q				
0+55	0.4922	7.52	VQ				
1+ 0	0.5487	8.21	VQ				
1+ 5	0.6167	9.88	VQ				
1+10	0.6941	11.24	VQ				



1+15	0.7739	11.58	V Q
1+20	0.8510	11.19	Q
1+25	0.9352	12.23	Q
1+30	1.0332	14.22	VQ
1+35	1.1301	14.08	Q
1+40	1.2277	14.16	QV
1+45	1.3421	16.61	Q
1+50	1.4665	18.07	QV
1+55	1.5861	17.36	Q V
2+ 0	1.7037	17.08	Q V
2+ 5	1.8246	17.55	Q V
2+10	1.9678	20.79	Q V
2+15	2.1497	26.42	QV
2+20	2.3265	25.66	Q V
2+25	2.5381	30.72	QV
2+30	2.8249	41.65	V Q
2+35	3.1524	47.54	V Q
2+40	3.4638	45.22	VQ
2+45	3.6626	28.86	Q V
2+50	3.7659	15.00	Q V
2+55	3.8432	11.22	Q V
3+ 0	3.8877	6.45	Q V
3+ 5	3.9002	1.82	Q V
3+10	3.9046	0.63	Q V
3+15	3.9061	0.22	Q V
3+20	3.9062	0.02	Q V

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex1006100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.10	31.27

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	3.00	85.29

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 3.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 3.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.180	0.117	(0.162)	0.063
2	0.17	0.60	0.216	0.117	(0.194)	0.099
3	0.25	0.60	0.216	0.117	(0.194)	0.099
4	0.33	0.60	0.216	0.117	(0.194)	0.099
5	0.42	0.60	0.216	0.117	(0.194)	0.099
6	0.50	0.70	0.252	0.117	(0.227)	0.135
7	0.58	0.70	0.252	0.117	(0.227)	0.135
8	0.67	0.70	0.252	0.117	(0.227)	0.135
9	0.75	0.70	0.252	0.117	(0.227)	0.135
10	0.83	0.70	0.252	0.117	(0.227)	0.135
11	0.92	0.70	0.252	0.117	(0.227)	0.135
12	1.00	0.80	0.288	0.117	(0.259)	0.171
13	1.08	0.80	0.288	0.117	(0.259)	0.171
14	1.17	0.80	0.288	0.117	(0.259)	0.171
15	1.25	0.80	0.288	0.117	(0.259)	0.171
16	1.33	0.80	0.288	0.117	(0.259)	0.171
17	1.42	0.80	0.288	0.117	(0.259)	0.171
18	1.50	0.80	0.288	0.117	(0.259)	0.171
19	1.58	0.80	0.288	0.117	(0.259)	0.171
20	1.67	0.80	0.288	0.117	(0.259)	0.171
21	1.75	0.80	0.288	0.117	(0.259)	0.171
22	1.83	0.80	0.288	0.117	(0.259)	0.171
23	1.92	0.80	0.288	0.117	(0.259)	0.171
24	2.00	0.90	0.324	0.117	(0.292)	0.207
25	2.08	0.80	0.288	0.117	(0.259)	0.171
26	2.17	0.90	0.324	0.117	(0.292)	0.207
27	2.25	0.90	0.324	0.117	(0.292)	0.207
28	2.33	0.90	0.324	0.117	(0.292)	0.207
29	2.42	0.90	0.324	0.117	(0.292)	0.207
30	2.50	0.90	0.324	0.117	(0.292)	0.207
31	2.58	0.90	0.324	0.117	(0.292)	0.207
32	2.67	0.90	0.324	0.117	(0.292)	0.207
33	2.75	1.00	0.360	0.117	(0.324)	0.243
34	2.83	1.00	0.360	0.117	(0.324)	0.243
35	2.92	1.00	0.360	0.117	(0.324)	0.243
36	3.00	1.00	0.360	0.117	(0.324)	0.243
37	3.08	1.00	0.360	0.117	(0.324)	0.243
38	3.17	1.10	0.396	0.117	(0.356)	0.279
39	3.25	1.10	0.396	0.117	(0.356)	0.279
40	3.33	1.10	0.396	0.117	(0.356)	0.279
41	3.42	1.20	0.432	0.117	(0.389)	0.315
42	3.50	1.30	0.468	0.117	(0.421)	0.351
43	3.58	1.40	0.504	0.117	(0.454)	0.387
44	3.67	1.40	0.504	0.117	(0.454)	0.387
45	3.75	1.50	0.540	0.117	(0.486)	0.423
46	3.83	1.50	0.540	0.117	(0.486)	0.423
47	3.92	1.60	0.576	0.117	(0.518)	0.459
48	4.00	1.60	0.576	0.117	(0.518)	0.459
49	4.08	1.70	0.612	0.117	(0.551)	0.495
50	4.17	1.80	0.648	0.117	(0.583)	0.531
51	4.25	1.90	0.684	0.117	(0.616)	0.567
52	4.33	2.00	0.720	0.117	(0.648)	0.603
53	4.42	2.10	0.756	0.117	(0.680)	0.639
54	4.50	2.10	0.756	0.117	(0.680)	0.639
55	4.58	2.20	0.792	0.117	(0.713)	0.675
56	4.67	2.30	0.828	0.117	(0.745)	0.711
57	4.75	2.40	0.864	0.117	(0.778)	0.747
58	4.83	2.40	0.864	0.117	(0.778)	0.747
59	4.92	2.50	0.900	0.117	(0.810)	0.783
60	5.00	2.60	0.936	0.117	(0.842)	0.819
61	5.08	3.10	1.116	0.117	(1.004)	0.999
62	5.17	3.60	1.296	0.117	(1.166)	1.179
63	5.25	3.90	1.404	0.117	(1.263)	1.287
64	5.33	4.20	1.512	0.117	(1.361)	1.395
65	5.42	4.70	1.692	0.117	(1.523)	1.575
66	5.50	5.60	2.016	0.117	(1.814)	1.899
67	5.58	1.90	0.684	0.117	(0.616)	0.567
68	5.67	0.90	0.324	0.117	(0.292)	0.207
69	5.75	0.60	0.216	0.117	(0.194)	0.099
70	5.83	0.50	0.180	0.117	(0.162)	0.063
71	5.92	0.30	0.108	(0.117)	0.097	0.011

```
72   6.00     0.20      0.072       (  0.117)       0.065        0.007
            (Loss Rate Not Used)
   Sum =     100.0                                    Sum =    27.6
      Flood volume = Effective rainfall      2.30(In)
       times area      28.4(Ac.)/[(In)/(Ft.)] =       5.5(Ac.Ft)
      Total soil loss =      0.70(In)
      Total soil loss =     1.649(Ac.Ft)
      Total rainfall =      3.00(In)
      Flood volume =      237744.8 Cubic Feet
      Total soil loss =       71827.7 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     47.683(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0       12.5      25.0      37.5      50.0
-------------------------------------------------------------------------
  0+ 5       0.0048      0.70  Q         |         |         |         |
  0+10       0.0181      1.92  VQ        |         |         |         |
  0+15       0.0357      2.56  V Q       |         |         |         |
  0+20       0.0545      2.74  V Q       |         |         |         |
  0+25       0.0739      2.82  V Q       |         |         |         |
  0+30       0.0962      3.24  V Q       |         |         |         |
  0+35       0.1218      3.70  V Q       |         |         |         |
  0+40       0.1480      3.81  |V Q       |         |         |         |
  0+45       0.1745      3.85  |V Q       |         |         |         |
  0+50       0.2011      3.87  |V Q       |         |         |         |
  0+55       0.2278      3.87  |V Q       |         |         |         |
  1+ 0       0.2572      4.27  |V Q       |         |         |         |
  1+ 5       0.2898      4.74  | VQ       |         |         |         |
  1+10       0.3231      4.84  | VQ       |         |         |         |
  1+15       0.3567      4.88  | VQ       |         |         |         |
  1+20       0.3905      4.90  | VQ       |         |         |         |
  1+25       0.4242      4.90  |  Q       |         |         |         |
  1+30       0.4580      4.90  |  Q       |         |         |         |
  1+35       0.4918      4.90  |  Q       |         |         |         |
  1+40       0.5255      4.90  |  Q       |         |         |         |
  1+45       0.5593      4.90  |  QV      |         |         |         |
  1+50       0.5930      4.90  |  QV      |         |         |         |
  1+55       0.6268      4.90  |  QV      |         |         |         |
  2+ 0       0.6633      5.30  |   Q      |         |         |         |
  2+ 5       0.7003      5.37  |   QV     |         |         |         |
  2+10       0.7375      5.40  |   QV     |         |         |         |
  2+15       0.7775      5.81  |   QV     |         |         |         |
  2+20       0.8181      5.89  |   QV     |         |         |         |
  2+25       0.8588      5.91  |   Q V    |         |         |         |
  2+30       0.8996      5.93  |   Q V    |         |         |         |
  2+35       0.9405      5.93  |   Q V    |         |         |         |
  2+40       0.9814      5.93  |   Q  V   |         |         |         |
  2+45       1.0250      6.34  |    Q V   |         |         |         |
  2+50       1.0718      6.80  |    Q V   |         |         |         |
  2+55       1.1194      6.90  |    Q  V  |         |         |         |
  3+ 0       1.1672      6.94  |    Q  V  |         |         |         |
  3+ 5       1.2151      6.97  |    Q  V  |         |         |         |
  3+10       1.2659      7.37  |    Q   V|         |         |         |
  3+15       1.3198      7.83  |     Q  V|         |         |         |
  3+20       1.3745      7.93  |     Q   V         |         |         |
  3+25       1.4322      8.38  |     Q   V         |         |         |
  3+30       1.4960      9.27  |      Q  V         |         |         |
  3+35       1.5665     10.23  |       Q |V        |         |         |
  3+40       1.6411     10.84  |       Q | V       |         |         |
  3+45       1.7197     11.41  |        Q| V       |         |         |
  3+50       1.8019     11.94  |        Q|  V      |         |         |
  3+55       1.8878     12.46  |        Q|  V      |         |         |
  4+ 0       1.9771     12.97  |         Q   V     |         |         |
  4+ 5       2.0700     13.49  |         Q    V    |         |         |
  4+10       2.1692     14.40  |         |Q   V    |         |         |
  4+15       2.2753     15.39  |         | Q   V   |         |         |
  4+20       2.3882     16.40  |         |  Q   V  |         |         |
  4+25       2.5083     17.44  |         |  Q    V |         |         |
  4+30       2.6327     18.07  |         |   Q    V|         |         |
  4+35       2.7611     18.63  |         |   Q     V         |         |
  4+40       2.8958     19.56  |         |    Q    |V        |         |
  4+45       3.0374     20.55  |         |     Q   | V       |         |
  4+50       3.1831     21.16  |         |     Q   |  V      |         |
  4+55       3.3327     21.73  |         |      Q  |   V     |         |
  5+ 0       3.4888     22.66  |         |       Q |    V    |         |
  5+ 5       3.6627     25.26  |         |         Q     V   |         |
  5+10       3.8675     29.73  |         |         |  Q    V |         |
  5+15       4.1006     33.84  |         |         |      Q  V         |
  5+20       4.3566     37.18  |         |         |        Q|V        |
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    5+25       4.6404     41.20  |          |          |          | Q V      |
    5+30       4.9688     47.68  |          |          |          |     V Q  |
    5+35       5.2284     37.70  |          |          |          Q       V  |
    5+40       5.3500     17.66  |          |    Q     |          |        V|
    5+45       5.4088      8.53  |      Q   |          |          |        V|
    5+50       5.4388      4.35  |   Q      |          |          |        V|
    5+55       5.4511      1.79  |Q         |          |          |        V|
    6+ 0       5.4555      0.64  Q          |          |          |        V|
    6+ 5       5.4573      0.26  Q          |          |          |        V|
    6+10       5.4577      0.07  Q          |          |          |        V|
    6+15       5.4578      0.01  Q          |          |          |        V|
    6+20       5.4579      0.00  Q          |          |          |        V|
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: ex10024100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 691.00(Ft.)
Length along longest watercourse measured to centroid = 346.00(Ft.)
Length along longest watercourse = 0.131 Mi.
Length along longest watercourse measured to centroid = 0.066 Mi.
Difference in elevation = 73.00(Ft.)
Slope along watercourse = 557.8003 Ft./Mi.
Average Manning's 'N' = 0.040
Lag time = 0.047 Hr.
Lag time = 2.84 Min.
25% of lag time = 0.71 Min.
40% of lag time = 1.14 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.80	51.17

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	5.00	142.15

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 5.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 5.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	91.00	0.000

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	176.088	38.943	11.158
2	0.167	352.176	45.069	12.913
3	0.250	528.264	9.844	2.820
4	0.333	704.352	4.075	1.168
5	0.417	880.440	2.069	0.593
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.040	(0.207)	0.036	0.004
2	0.17	0.07	0.040	(0.207)	0.036	0.004
3	0.25	0.07	0.040	(0.206)	0.036	0.004
4	0.33	0.10	0.060	(0.205)	0.054	0.006
5	0.42	0.10	0.060	(0.204)	0.054	0.006
6	0.50	0.10	0.060	(0.203)	0.054	0.006
7	0.58	0.10	0.060	(0.203)	0.054	0.006
8	0.67	0.10	0.060	(0.202)	0.054	0.006
9	0.75	0.10	0.060	(0.201)	0.054	0.006
10	0.83	0.13	0.080	(0.200)	0.072	0.008
11	0.92	0.13	0.080	(0.199)	0.072	0.008
12	1.00	0.13	0.080	(0.199)	0.072	0.008
13	1.08	0.10	0.060	(0.198)	0.054	0.006
14	1.17	0.10	0.060	(0.197)	0.054	0.006
15	1.25	0.10	0.060	(0.196)	0.054	0.006
16	1.33	0.10	0.060	(0.196)	0.054	0.006
17	1.42	0.10	0.060	(0.195)	0.054	0.006
18	1.50	0.10	0.060	(0.194)	0.054	0.006
19	1.58	0.10	0.060	(0.193)	0.054	0.006
20	1.67	0.10	0.060	(0.192)	0.054	0.006
21	1.75	0.10	0.060	(0.192)	0.054	0.006
22	1.83	0.13	0.080	(0.191)	0.072	0.008
23	1.92	0.13	0.080	(0.190)	0.072	0.008
24	2.00	0.13	0.080	(0.189)	0.072	0.008
25	2.08	0.13	0.080	(0.189)	0.072	0.008
26	2.17	0.13	0.080	(0.188)	0.072	0.008
27	2.25	0.13	0.080	(0.187)	0.072	0.008
28	2.33	0.13	0.080	(0.186)	0.072	0.008
29	2.42	0.13	0.080	(0.186)	0.072	0.008
30	2.50	0.13	0.080	(0.185)	0.072	0.008
31	2.58	0.17	0.100	(0.184)	0.090	0.010
32	2.67	0.17	0.100	(0.183)	0.090	0.010
33	2.75	0.17	0.100	(0.183)	0.090	0.010
34	2.83	0.17	0.100	(0.182)	0.090	0.010
35	2.92	0.17	0.100	(0.181)	0.090	0.010
36	3.00	0.17	0.100	(0.180)	0.090	0.010
37	3.08	0.17	0.100	(0.180)	0.090	0.010
38	3.17	0.17	0.100	(0.179)	0.090	0.010
39	3.25	0.17	0.100	(0.178)	0.090	0.010
40	3.33	0.17	0.100	(0.177)	0.090	0.010
41	3.42	0.17	0.100	(0.177)	0.090	0.010
42	3.50	0.17	0.100	(0.176)	0.090	0.010
43	3.58	0.17	0.100	(0.175)	0.090	0.010
44	3.67	0.17	0.100	(0.174)	0.090	0.010
45	3.75	0.17	0.100	(0.174)	0.090	0.010
46	3.83	0.20	0.120	(0.173)	0.108	0.012
47	3.92	0.20	0.120	(0.172)	0.108	0.012
48	4.00	0.20	0.120	(0.171)	0.108	0.012
49	4.08	0.20	0.120	(0.171)	0.108	0.012
50	4.17	0.20	0.120	(0.170)	0.108	0.012
51	4.25	0.20	0.120	(0.169)	0.108	0.012
52	4.33	0.23	0.140	(0.169)	0.126	0.014
53	4.42	0.23	0.140	(0.168)	0.126	0.014
54	4.50	0.23	0.140	(0.167)	0.126	0.014
55	4.58	0.23	0.140	(0.166)	0.126	0.014
56	4.67	0.23	0.140	(0.166)	0.126	0.014
57	4.75	0.23	0.140	(0.165)	0.126	0.014
58	4.83	0.27	0.160	(0.164)	0.144	0.016
59	4.92	0.27	0.160	(0.164)	0.144	0.016
60	5.00	0.27	0.160	(0.163)	0.144	0.016
61	5.08	0.20	0.120	(0.162)	0.108	0.012
62	5.17	0.20	0.120	(0.161)	0.108	0.012
63	5.25	0.20	0.120	(0.161)	0.108	0.012
64	5.33	0.23	0.140	(0.160)	0.126	0.014
65	5.42	0.23	0.140	(0.159)	0.126	0.014
66	5.50	0.23	0.140	(0.159)	0.126	0.014
67	5.58	0.27	0.160	(0.158)	0.144	0.016
68	5.67	0.27	0.160	(0.157)	0.144	0.016
69	5.75	0.27	0.160	(0.157)	0.144	0.016
70	5.83	0.27	0.160	(0.156)	0.144	0.016
71	5.92	0.27	0.160	(0.155)	0.144	0.016

72	6.00	0.27	0.160	(0.154)	0.144	0.016
73	6.08	0.30	0.180	0.154	(0.162)	0.026
74	6.17	0.30	0.180	0.153	(0.162)	0.027
75	6.25	0.30	0.180	0.152	(0.162)	0.028
76	6.33	0.30	0.180	0.152	(0.162)	0.028
77	6.42	0.30	0.180	0.151	(0.162)	0.029
78	6.50	0.30	0.180	0.150	(0.162)	0.030
79	6.58	0.33	0.200	0.150	(0.180)	0.050
80	6.67	0.33	0.200	0.149	(0.180)	0.051
81	6.75	0.33	0.200	0.148	(0.180)	0.052
82	6.83	0.33	0.200	0.148	(0.180)	0.052
83	6.92	0.33	0.200	0.147	(0.180)	0.053
84	7.00	0.33	0.200	0.146	(0.180)	0.054
85	7.08	0.33	0.200	0.146	(0.180)	0.054
86	7.17	0.33	0.200	0.145	(0.180)	0.055
87	7.25	0.33	0.200	0.144	(0.180)	0.056
88	7.33	0.37	0.220	0.144	(0.198)	0.076
89	7.42	0.37	0.220	0.143	(0.198)	0.077
90	7.50	0.37	0.220	0.142	(0.198)	0.078
91	7.58	0.40	0.240	0.142	(0.216)	0.098
92	7.67	0.40	0.240	0.141	(0.216)	0.099
93	7.75	0.40	0.240	0.140	(0.216)	0.100
94	7.83	0.43	0.260	0.140	(0.234)	0.120
95	7.92	0.43	0.260	0.139	(0.234)	0.121
96	8.00	0.43	0.260	0.138	(0.234)	0.122
97	8.08	0.50	0.300	0.138	(0.270)	0.162
98	8.17	0.50	0.300	0.137	(0.270)	0.163
99	8.25	0.50	0.300	0.137	(0.270)	0.163
100	8.33	0.50	0.300	0.136	(0.270)	0.164
101	8.42	0.50	0.300	0.135	(0.270)	0.165
102	8.50	0.50	0.300	0.135	(0.270)	0.165
103	8.58	0.53	0.320	0.134	(0.288)	0.186
104	8.67	0.53	0.320	0.133	(0.288)	0.187
105	8.75	0.53	0.320	0.133	(0.288)	0.187
106	8.83	0.57	0.340	0.132	(0.306)	0.208
107	8.92	0.57	0.340	0.131	(0.306)	0.208
108	9.00	0.57	0.340	0.131	(0.306)	0.209
109	9.08	0.63	0.380	0.130	(0.342)	0.250
110	9.17	0.63	0.380	0.130	(0.342)	0.250
111	9.25	0.63	0.380	0.129	(0.342)	0.251
112	9.33	0.67	0.400	0.128	(0.360)	0.272
113	9.42	0.67	0.400	0.128	(0.360)	0.272
114	9.50	0.67	0.400	0.127	(0.360)	0.273
115	9.58	0.70	0.420	0.127	(0.378)	0.293
116	9.67	0.70	0.420	0.126	(0.378)	0.294
117	9.75	0.70	0.420	0.125	(0.378)	0.295
118	9.83	0.73	0.440	0.125	(0.396)	0.315
119	9.92	0.73	0.440	0.124	(0.396)	0.316
120	10.00	0.73	0.440	0.124	(0.396)	0.316
121	10.08	0.50	0.300	0.123	(0.270)	0.177
122	10.17	0.50	0.300	0.122	(0.270)	0.178
123	10.25	0.50	0.300	0.122	(0.270)	0.178
124	10.33	0.50	0.300	0.121	(0.270)	0.179
125	10.42	0.50	0.300	0.121	(0.270)	0.179
126	10.50	0.50	0.300	0.120	(0.270)	0.180
127	10.58	0.67	0.400	0.119	(0.360)	0.281
128	10.67	0.67	0.400	0.119	(0.360)	0.281
129	10.75	0.67	0.400	0.118	(0.360)	0.282
130	10.83	0.67	0.400	0.118	(0.360)	0.282
131	10.92	0.67	0.400	0.117	(0.360)	0.283
132	11.00	0.67	0.400	0.117	(0.360)	0.283
133	11.08	0.63	0.380	0.116	(0.342)	0.264
134	11.17	0.63	0.380	0.115	(0.342)	0.265
135	11.25	0.63	0.380	0.115	(0.342)	0.265
136	11.33	0.63	0.380	0.114	(0.342)	0.266
137	11.42	0.63	0.380	0.114	(0.342)	0.266
138	11.50	0.63	0.380	0.113	(0.342)	0.267
139	11.58	0.57	0.340	0.113	(0.306)	0.227
140	11.67	0.57	0.340	0.112	(0.306)	0.228
141	11.75	0.57	0.340	0.111	(0.306)	0.229
142	11.83	0.60	0.360	0.111	(0.324)	0.249
143	11.92	0.60	0.360	0.110	(0.324)	0.250
144	12.00	0.60	0.360	0.110	(0.324)	0.250
145	12.08	0.83	0.500	0.109	(0.450)	0.391
146	12.17	0.83	0.500	0.109	(0.450)	0.391
147	12.25	0.83	0.500	0.108	(0.450)	0.392
148	12.33	0.87	0.520	0.108	(0.468)	0.412
149	12.42	0.87	0.520	0.107	(0.468)	0.413
150	12.50	0.87	0.520	0.107	(0.468)	0.413
151	12.58	0.93	0.560	0.106	(0.504)	0.454
152	12.67	0.93	0.560	0.105	(0.504)	0.455
153	12.75	0.93	0.560	0.105	(0.504)	0.455
154	12.83	0.97	0.580	0.104	(0.522)	0.476
155	12.92	0.97	0.580	0.104	(0.522)	0.476
156	13.00	0.97	0.580	0.103	(0.522)	0.477
157	13.08	1.13	0.680	0.103	(0.612)	0.577

158	13.17	1.13	0.680		0.102	(0.612)	0.578
159	13.25	1.13	0.680		0.102	(0.612)	0.578
160	13.33	1.13	0.680		0.101	(0.612)	0.579
161	13.42	1.13	0.680		0.101	(0.612)	0.579
162	13.50	1.13	0.680		0.100	(0.612)	0.580
163	13.58	0.77	0.460		0.100	(0.414)	0.360
164	13.67	0.77	0.460		0.099	(0.414)	0.361
165	13.75	0.77	0.460		0.099	(0.414)	0.361
166	13.83	0.77	0.460		0.098	(0.414)	0.362
167	13.92	0.77	0.460		0.098	(0.414)	0.362
168	14.00	0.77	0.460		0.097	(0.414)	0.363
169	14.08	0.90	0.540		0.097	(0.486)	0.443
170	14.17	0.90	0.540		0.096	(0.486)	0.444
171	14.25	0.90	0.540		0.096	(0.486)	0.444
172	14.33	0.87	0.520		0.095	(0.468)	0.425
173	14.42	0.87	0.520		0.095	(0.468)	0.425
174	14.50	0.87	0.520		0.094	(0.468)	0.426
175	14.58	0.87	0.520		0.094	(0.468)	0.426
176	14.67	0.87	0.520		0.093	(0.468)	0.427
177	14.75	0.87	0.520		0.093	(0.468)	0.427
178	14.83	0.83	0.500		0.092	(0.450)	0.408
179	14.92	0.83	0.500		0.092	(0.450)	0.408
180	15.00	0.83	0.500		0.091	(0.450)	0.409
181	15.08	0.80	0.480		0.091	(0.432)	0.389
182	15.17	0.80	0.480		0.090	(0.432)	0.390
183	15.25	0.80	0.480		0.090	(0.432)	0.390
184	15.33	0.77	0.460		0.090	(0.414)	0.370
185	15.42	0.77	0.460		0.089	(0.414)	0.371
186	15.50	0.77	0.460		0.089	(0.414)	0.371
187	15.58	0.63	0.380		0.088	(0.342)	0.292
188	15.67	0.63	0.380		0.088	(0.342)	0.292
189	15.75	0.63	0.380		0.087	(0.342)	0.293
190	15.83	0.63	0.380		0.087	(0.342)	0.293
191	15.92	0.63	0.380		0.086	(0.342)	0.294
192	16.00	0.63	0.380		0.086	(0.342)	0.294
193	16.08	0.13	0.080	(0.085)		0.072	0.008
194	16.17	0.13	0.080	(0.085)		0.072	0.008
195	16.25	0.13	0.080	(0.085)		0.072	0.008
196	16.33	0.13	0.080	(0.084)		0.072	0.008
197	16.42	0.13	0.080	(0.084)		0.072	0.008
198	16.50	0.13	0.080	(0.083)		0.072	0.008
199	16.58	0.10	0.060	(0.083)		0.054	0.006
200	16.67	0.10	0.060	(0.082)		0.054	0.006
201	16.75	0.10	0.060	(0.082)		0.054	0.006
202	16.83	0.10	0.060	(0.082)		0.054	0.006
203	16.92	0.10	0.060	(0.081)		0.054	0.006
204	17.00	0.10	0.060	(0.081)		0.054	0.006
205	17.08	0.17	0.100		0.080	(0.090)	0.020
206	17.17	0.17	0.100		0.080	(0.090)	0.020
207	17.25	0.17	0.100		0.080	(0.090)	0.020
208	17.33	0.17	0.100		0.079	(0.090)	0.021
209	17.42	0.17	0.100		0.079	(0.090)	0.021
210	17.50	0.17	0.100		0.078	(0.090)	0.022
211	17.58	0.17	0.100		0.078	(0.090)	0.022
212	17.67	0.17	0.100		0.078	(0.090)	0.022
213	17.75	0.17	0.100		0.077	(0.090)	0.023
214	17.83	0.13	0.080	(0.077)		0.072	0.008
215	17.92	0.13	0.080	(0.076)		0.072	0.008
216	18.00	0.13	0.080	(0.076)		0.072	0.008
217	18.08	0.13	0.080	(0.076)		0.072	0.008
218	18.17	0.13	0.080	(0.075)		0.072	0.008
219	18.25	0.13	0.080	(0.075)		0.072	0.008
220	18.33	0.13	0.080	(0.075)		0.072	0.008
221	18.42	0.13	0.080	(0.074)		0.072	0.008
222	18.50	0.13	0.080	(0.074)		0.072	0.008
223	18.58	0.10	0.060	(0.074)		0.054	0.006
224	18.67	0.10	0.060	(0.073)		0.054	0.006
225	18.75	0.10	0.060	(0.073)		0.054	0.006
226	18.83	0.07	0.040	(0.072)		0.036	0.004
227	18.92	0.07	0.040	(0.072)		0.036	0.004
228	19.00	0.07	0.040	(0.072)		0.036	0.004
229	19.08	0.10	0.060	(0.071)		0.054	0.006
230	19.17	0.10	0.060	(0.071)		0.054	0.006
231	19.25	0.10	0.060	(0.071)		0.054	0.006
232	19.33	0.13	0.080		0.070	(0.072)	0.010
233	19.42	0.13	0.080		0.070	(0.072)	0.010
234	19.50	0.13	0.080		0.070	(0.072)	0.010
235	19.58	0.10	0.060	(0.069)		0.054	0.006
236	19.67	0.10	0.060	(0.069)		0.054	0.006
237	19.75	0.10	0.060	(0.069)		0.054	0.006
238	19.83	0.07	0.040	(0.069)		0.036	0.004
239	19.92	0.07	0.040	(0.068)		0.036	0.004
240	20.00	0.07	0.040	(0.068)		0.036	0.004
241	20.08	0.10	0.060	(0.068)		0.054	0.006
242	20.17	0.10	0.060	(0.067)		0.054	0.006
243	20.25	0.10	0.060	(0.067)		0.054	0.006

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244  20.33     0.10      0.060       (  0.067)       0.054        0.006
245  20.42     0.10      0.060       (  0.066)       0.054        0.006
246  20.50     0.10      0.060       (  0.066)       0.054        0.006
247  20.58     0.10      0.060       (  0.066)       0.054        0.006
248  20.67     0.10      0.060       (  0.066)       0.054        0.006
249  20.75     0.10      0.060       (  0.065)       0.054        0.006
250  20.83     0.07      0.040       (  0.065)       0.036        0.004
251  20.92     0.07      0.040       (  0.065)       0.036        0.004
252  21.00     0.07      0.040       (  0.065)       0.036        0.004
253  21.08     0.10      0.060       (  0.064)       0.054        0.006
254  21.17     0.10      0.060       (  0.064)       0.054        0.006
255  21.25     0.10      0.060       (  0.064)       0.054        0.006
256  21.33     0.07      0.040       (  0.064)       0.036        0.004
257  21.42     0.07      0.040       (  0.063)       0.036        0.004
258  21.50     0.07      0.040       (  0.063)       0.036        0.004
259  21.58     0.10      0.060       (  0.063)       0.054        0.006
260  21.67     0.10      0.060       (  0.063)       0.054        0.006
261  21.75     0.10      0.060       (  0.062)       0.054        0.006
262  21.83     0.07      0.040       (  0.062)       0.036        0.004
263  21.92     0.07      0.040       (  0.062)       0.036        0.004
264  22.00     0.07      0.040       (  0.062)       0.036        0.004
265  22.08     0.10      0.060       (  0.062)       0.054        0.006
266  22.17     0.10      0.060       (  0.061)       0.054        0.006
267  22.25     0.10      0.060       (  0.061)       0.054        0.006
268  22.33     0.07      0.040       (  0.061)       0.036        0.004
269  22.42     0.07      0.040       (  0.061)       0.036        0.004
270  22.50     0.07      0.040       (  0.061)       0.036        0.004
271  22.58     0.07      0.040       (  0.060)       0.036        0.004
272  22.67     0.07      0.040       (  0.060)       0.036        0.004
273  22.75     0.07      0.040       (  0.060)       0.036        0.004
274  22.83     0.07      0.040       (  0.060)       0.036        0.004
275  22.92     0.07      0.040       (  0.060)       0.036        0.004
276  23.00     0.07      0.040       (  0.060)       0.036        0.004
277  23.08     0.07      0.040       (  0.060)       0.036        0.004
278  23.17     0.07      0.040       (  0.059)       0.036        0.004
279  23.25     0.07      0.040       (  0.059)       0.036        0.004
280  23.33     0.07      0.040       (  0.059)       0.036        0.004
281  23.42     0.07      0.040       (  0.059)       0.036        0.004
282  23.50     0.07      0.040       (  0.059)       0.036        0.004
283  23.58     0.07      0.040       (  0.059)       0.036        0.004
284  23.67     0.07      0.040       (  0.059)       0.036        0.004
285  23.75     0.07      0.040       (  0.059)       0.036        0.004
286  23.83     0.07      0.040       (  0.059)       0.036        0.004
287  23.92     0.07      0.040       (  0.059)       0.036        0.004
288  24.00     0.07      0.040       (  0.059)       0.036        0.004
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    34.3
      Flood volume = Effective rainfall      2.86(In)
       times area      28.4(Ac.)/[(In)/(Ft.)] =       6.8(Ac.Ft)
      Total soil loss =      2.14(In)
      Total soil loss =     5.075(Ac.Ft)
      Total rainfall =      5.00(In)
      Flood volume =      294914.3 Cubic Feet
      Total soil loss =      221061.6 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     16.607(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
 ---------------------------------------------------------------------------
   0+ 5       0.0003      0.04  Q          |          |          |          |
   0+10       0.0010      0.10  Q          |          |          |          |
   0+15       0.0017      0.11  Q          |          |          |          |
   0+20       0.0026      0.13  Q          |          |          |          |
   0+25       0.0038      0.16  Q          |          |          |          |
   0+30       0.0049      0.17  Q          |          |          |          |
   0+35       0.0061      0.17  Q          |          |          |          |
   0+40       0.0073      0.17  Q          |          |          |          |
   0+45       0.0085      0.17  Q          |          |          |          |
   0+50       0.0098      0.19  Q          |          |          |          |
   0+55       0.0113      0.22  Q          |          |          |          |
   1+ 0       0.0129      0.23  Q          |          |          |          |
   1+ 5       0.0143      0.21  Q          |          |          |          |
   1+10       0.0155      0.18  Q          |          |          |          |
   1+15       0.0167      0.18  Q          |          |          |          |
   1+20       0.0179      0.17  Q          |          |          |          |
   1+25       0.0191      0.17  Q          |          |          |          |
   1+30       0.0203      0.17  Q          |          |          |          |
   1+35       0.0215      0.17  Q          |          |          |          |
   1+40       0.0227      0.17  Q          |          |          |          |
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1+45       0.0239      0.17  Q          |          |          |          |
1+50       0.0252      0.19  Q          |          |          |          |
1+55       0.0267      0.22  Q          |          |          |          |
2+ 0       0.0283      0.23  Q          |          |          |          |
2+ 5       0.0298      0.23  Q          |          |          |          |
2+10       0.0314      0.23  Q          |          |          |          |
2+15       0.0330      0.23  Q          |          |          |          |
2+20       0.0346      0.23  Q          |          |          |          |
2+25       0.0362      0.23  Q          |          |          |          |
2+30       0.0377      0.23  Q          |          |          |          |
2+35       0.0395      0.25  Q          |          |          |          |
2+40       0.0414      0.28  Q          |          |          |          |
2+45       0.0433      0.28  Q          |          |          |          |
2+50       0.0453      0.29  Q          |          |          |          |
2+55       0.0473      0.29  Q          |          |          |          |
3+ 0       0.0493      0.29  Q          |          |          |          |
3+ 5       0.0512      0.29  Q          |          |          |          |
3+10       0.0532      0.29  Q          |          |          |          |
3+15       0.0552      0.29  Q          |          |          |          |
3+20       0.0571      0.29  Q          |          |          |          |
3+25       0.0591      0.29  Q          |          |          |          |
3+30       0.0611      0.29  Q          |          |          |          |
3+35       0.0631      0.29  Q          |          |          |          |
3+40       0.0650      0.29  Q          |          |          |          |
3+45       0.0670      0.29  Q          |          |          |          |
3+50       0.0691      0.31  Q          |          |          |          |
3+55       0.0715      0.33  Q          |          |          |          |
4+ 0       0.0738      0.34  Q          |          |          |          |
4+ 5       0.0762      0.34  Q          |          |          |          |
4+10       0.0785      0.34  Q          |          |          |          |
4+15       0.0809      0.34  Q          |          |          |          |
4+20       0.0834      0.37  Q          |          |          |          |
4+25       0.0861      0.39  Q          |          |          |          |
4+30       0.0889      0.40  Q          |          |          |          |
4+35       0.0916      0.40  Q          |          |          |          |
4+40       0.0944      0.40  Q          |          |          |          |
4+45       0.0971      0.40  Q          |          |          |          |
4+50       0.1001      0.42  Q          |          |          |          |
4+55       0.1032      0.45  Q          |          |          |          |
5+ 0       0.1063      0.46  Q          |          |          |          |
5+ 5       0.1091      0.41  Q          |          |          |          |
5+10       0.1116      0.36  Q          |          |          |          |
5+15       0.1140      0.35  Q          |          |          |          |
5+20       0.1166      0.37  Q          |          |          |          |
5+25       0.1193      0.39  Q          |          |          |          |
5+30       0.1220      0.40  Q          |          |          |          |
5+35       0.1249      0.42  Q          |          |          |          |
5+40       0.1280      0.45  Q          |          |          |          |
5+45       0.1312      0.46  Q          |          |          |          |
5+50       0.1343      0.46  Q          |          |          |          |
5+55       0.1375      0.46  Q          |          |          |          |
6+ 0       0.1406      0.46  Q          |          |          |          |
6+ 5       0.1446      0.57  VQ         |          |          |          |
6+10       0.1495      0.71  VQ         |          |          |          |
6+15       0.1547      0.76  VQ         |          |          |          |
6+20       0.1601      0.79  VQ         |          |          |          |
6+25       0.1657      0.81  VQ         |          |          |          |
6+30       0.1715      0.83  |Q         |          |          |          |
6+35       0.1789      1.08  |VQ        |          |          |          |
6+40       0.1882      1.35  |VQ        |          |          |          |
6+45       0.1981      1.43  |VQ        |          |          |          |
6+50       0.2082      1.47  |VQ        |          |          |          |
6+55       0.2185      1.50  |V Q       |          |          |          |
7+ 0       0.2290      1.52  |V Q       |          |          |          |
7+ 5       0.2396      1.54  |V Q       |          |          |          |
7+10       0.2504      1.56  |V Q       |          |          |          |
7+15       0.2613      1.58  |V Q       |          |          |          |
7+20       0.2738      1.82  |V Q       |          |          |          |
7+25       0.2883      2.10  |V  Q      |          |          |          |
7+30       0.3032      2.17  |V  Q      |          |          |          |
7+35       0.3200      2.44  |V  Q      |          |          |          |
7+40       0.3388      2.73  | V  Q     |          |          |          |
7+45       0.3581      2.80  | V  Q     |          |          |          |
7+50       0.3793      3.07  | V   Q    |          |          |          |
7+55       0.4024      3.36  | V   Q    |          |          |          |
8+ 0       0.4260      3.43  | V   Q    |          |          |          |
8+ 5       0.4530      3.92  | V    Q   |          |          |          |
8+10       0.4838      4.47  | V     Q  |          |          |          |
8+15       0.5155      4.60  |  V     Q |          |          |          |
8+20       0.5476      4.66  |  V     Q |          |          |          |
8+25       0.5800      4.71  |  V     Q |          |          |          |
8+30       0.6126      4.72  |  V     Q |          |          |          |
8+35       0.6468      4.97  |  V     Q |          |          |          |
8+40       0.6829      5.24  |   V     Q          |          |          |
8+45       0.7195      5.32  |   V     Q          |          |          |
8+50       0.7579      5.58  |   V     |Q         |          |          |
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8+55	0.7984	5.87	
9+ 0	0.8393	5.94	
9+ 5	0.8836	6.43	
9+10	0.9316	6.98	
9+15	0.9806	7.11	
9+20	1.0315	7.40	
9+25	1.0845	7.70	
9+30	1.1381	7.77	
9+35	1.1934	8.03	
9+40	1.2507	8.32	
9+45	1.3085	8.40	
9+50	1.3682	8.66	
9+55	1.4298	8.95	
10+ 0	1.4919	9.02	
10+ 5	1.5436	7.50	
10+10	1.5830	5.72	
10+15	1.6197	5.34	
10+20	1.6555	5.19	
10+25	1.6908	5.13	
10+30	1.7263	5.15	
10+35	1.7695	6.28	
10+40	1.8218	7.59	
10+45	1.8761	7.89	
10+50	1.9313	8.02	
10+55	1.9871	8.10	
11+ 0	2.0429	8.11	
11+ 5	2.0974	7.91	
11+10	2.1501	7.66	
11+15	2.2026	7.62	
11+20	2.2551	7.62	
11+25	2.3076	7.62	
11+30	2.3602	7.64	
11+35	2.4098	7.21	
11+40	2.4560	6.71	
11+45	2.5015	6.61	
11+50	2.5483	6.80	
11+55	2.5969	7.05	
12+ 0	2.6460	7.12	
12+ 5	2.7061	8.73	
12+10	2.7788	10.56	
12+15	2.8544	10.97	
12+20	2.9327	11.38	
12+25	3.0135	11.73	
12+30	3.0948	11.80	
12+35	3.1795	12.29	
12+40	3.2679	12.83	
12+45	3.3571	12.96	
12+50	3.4484	13.25	
12+55	3.5416	13.54	
13+ 0	3.6354	13.62	
13+ 5	3.7371	14.77	
13+10	3.8480	16.09	
13+15	3.9608	16.39	
13+20	4.0746	16.52	
13+25	4.1888	16.59	
13+30	4.3032	16.61	
13+35	4.4008	14.17	
13+40	4.4789	11.34	
13+45	4.5528	10.73	
13+50	4.6250	10.49	
13+55	4.6965	10.37	
14+ 0	4.7680	10.39	
14+ 5	4.8458	11.30	
14+10	4.9308	12.34	
14+15	5.0175	12.58	
14+20	5.1033	12.47	
14+25	5.1878	12.27	
14+30	5.2720	12.23	
14+35	5.3562	12.22	
14+40	5.4403	12.22	
14+45	5.5246	12.23	
14+50	5.6074	12.02	
14+55	5.6885	11.78	
15+ 0	5.7694	11.74	
15+ 5	5.8486	11.50	
15+10	5.9261	11.25	
15+15	6.0032	11.20	
15+20	6.0788	10.97	
15+25	6.1525	10.71	
15+30	6.2260	10.67	
15+35	6.2933	9.77	
15+40	6.3535	8.73	
15+45	6.4121	8.52	
15+50	6.4703	8.44	
15+55	6.5282	8.41	
16+ 0	6.5861	8.42	

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16+ 5       6.6222      5.23  |          Q          |          |          V|
16+10       6.6328      1.54  |   Q         |          |          |          V|
16+15       6.6378      0.73  |Q            |          |          |          V|
16+20       6.6406      0.40  Q             |          |          |          V|
16+25       6.6422      0.23  Q             |          |          |          V|
16+30       6.6437      0.23  Q             |          |          |          V|
16+35       6.6452      0.21  Q             |          |          |          V|
16+40       6.6464      0.18  Q             |          |          |          V|
16+45       6.6476      0.18  Q             |          |          |          V|
16+50       6.6488      0.17  Q             |          |          |          V|
16+55       6.6500      0.17  Q             |          |          |          V|
17+ 0       6.6512      0.17  Q             |          |          |          V|
17+ 5       6.6534      0.32  Q             |          |          |          V|
17+10       6.6569      0.50  |Q            |          |          |          V|
17+15       6.6607      0.55  |Q            |          |          |          V|
17+20       6.6647      0.58  |Q            |          |          |          V|
17+25       6.6688      0.60  |Q            |          |          |          V|
17+30       6.6730      0.61  |Q            |          |          |          V|
17+35       6.6773      0.62  |Q            |          |          |          V|
17+40       6.6816      0.63  |Q            |          |          |          V|
17+45       6.6860      0.64  |Q            |          |          |          V|
17+50       6.6894      0.48  Q             |          |          |          V|
17+55       6.6914      0.30  Q             |          |          |          V|
18+ 0       6.6932      0.26  Q             |          |          |          V|
18+ 5       6.6948      0.24  Q             |          |          |          V|
18+10       6.6964      0.23  Q             |          |          |          V|
18+15       6.6980      0.23  Q             |          |          |          V|
18+20       6.6995      0.23  Q             |          |          |          V|
18+25       6.7011      0.23  Q             |          |          |          V|
18+30       6.7027      0.23  Q             |          |          |          V|
18+35       6.7041      0.21  Q             |          |          |          V|
18+40       6.7054      0.18  Q             |          |          |          V|
18+45       6.7066      0.18  Q             |          |          |          V|
18+50       6.7076      0.15  Q             |          |          |          V|
18+55       6.7085      0.12  Q             |          |          |          V|
19+ 0       6.7093      0.12  Q             |          |          |          V|
19+ 5       6.7102      0.14  Q             |          |          |          V|
19+10       6.7114      0.16  Q             |          |          |          V|
19+15       6.7125      0.17  Q             |          |          |          V|
19+20       6.7140      0.21  Q             |          |          |          V|
19+25       6.7158      0.26  Q             |          |          |          V|
19+30       6.7177      0.28  Q             |          |          |          V|
19+35       6.7193      0.24  Q             |          |          |          V|
19+40       6.7207      0.19  Q             |          |          |          V|
19+45       6.7219      0.18  Q             |          |          |          V|
19+50       6.7229      0.15  Q             |          |          |          V|
19+55       6.7238      0.12  Q             |          |          |          V|
20+ 0       6.7246      0.12  Q             |          |          |          V|
20+ 5       6.7256      0.14  Q             |          |          |          V|
20+10       6.7267      0.16  Q             |          |          |          V|
20+15       6.7278      0.17  Q             |          |          |          V|
20+20       6.7290      0.17  Q             |          |          |          V|
20+25       6.7302      0.17  Q             |          |          |          V|
20+30       6.7314      0.17  Q             |          |          |          V|
20+35       6.7326      0.17  Q             |          |          |          V|
20+40       6.7338      0.17  Q             |          |          |          V|
20+45       6.7349      0.17  Q             |          |          |          V|
20+50       6.7360      0.15  Q             |          |          |          V|
20+55       6.7368      0.12  Q             |          |          |          V|
21+ 0       6.7376      0.12  Q             |          |          |          V|
21+ 5       6.7386      0.14  Q             |          |          |          V|
21+10       6.7397      0.16  Q             |          |          |          V|
21+15       6.7409      0.17  Q             |          |          |          V|
21+20       6.7419      0.15  Q             |          |          |          V|
21+25       6.7427      0.12  Q             |          |          |          V|
21+30       6.7436      0.12  Q             |          |          |          V|
21+35       6.7445      0.14  Q             |          |          |          V|
21+40       6.7456      0.16  Q             |          |          |          V|
21+45       6.7468      0.17  Q             |          |          |          V|
21+50       6.7478      0.15  Q             |          |          |          V|
21+55       6.7487      0.12  Q             |          |          |          V|
22+ 0       6.7495      0.12  Q             |          |          |          V|
22+ 5       6.7504      0.14  Q             |          |          |          V|
22+10       6.7516      0.16  Q             |          |          |          V|
22+15       6.7527      0.17  Q             |          |          |          V|
22+20       6.7537      0.15  Q             |          |          |          V|
22+25       6.7546      0.12  Q             |          |          |          V|
22+30       6.7554      0.12  Q             |          |          |          V|
22+35       6.7562      0.12  Q             |          |          |          V|
22+40       6.7570      0.11  Q             |          |          |          V|
22+45       6.7578      0.11  Q             |          |          |          V|
22+50       6.7586      0.11  Q             |          |          |          V|
22+55       6.7594      0.11  Q             |          |          |          V|
23+ 0       6.7602      0.11  Q             |          |          |          V|
23+ 5       6.7609      0.11  Q             |          |          |          V|
23+10       6.7617      0.11  Q             |          |          |          V|
```

```
   23+15       6.7625      0.11  Q          |          |          |         v|
   23+20       6.7633      0.11  Q          |          |          |         v|
   23+25       6.7641      0.11  Q          |          |          |         v|
   23+30       6.7649      0.11  Q          |          |          |         v|
   23+35       6.7657      0.11  Q          |          |          |         v|
   23+40       6.7665      0.11  Q          |          |          |         v|
   23+45       6.7673      0.11  Q          |          |          |         v|
   23+50       6.7680      0.11  Q          |          |          |         v|
   23+55       6.7688      0.11  Q          |          |          |         v|
   24+ 0       6.7696      0.11  Q          |          |          |         v|
   24+ 5       6.7701      0.07  Q          |          |          |         v|
   24+10       6.7702      0.02  Q          |          |          |         v|
   24+15       6.7703      0.01  Q          |          |          |         v|
   24+20       6.7703      0.00  Q          |          |          |         v|
-------------------------------------------------------------------------
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EXISTING UNIT HYDROGRAPH MAP



LEGEND

NODE / ELEV

AREA | ACRES
LENGTH | SOIL

WATERSHED BOUNDARY

FLOW PATH

EXISTING UNIT HYDROGRAPH MAP
PREPARATION DATE: SEPTEMBER 2024
REVISION DATE: DECEMBER 2024
JOB NUMBER: 10615

PLAN PREPARED BY:
adkan ENGINEERS
Civil Engineering • Surveying • Planning
6879 Airport Drive, Riverside, CA 92504
Tel:(951) 688-0241 • Fax:(951) 688-0599

Appendix D – Proposed Synthetic Unit Hydrograph Method

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: pro212.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 1871.00(Ft.)
Length along longest watercourse measured to centroid = 935.00(Ft.)
Length along longest watercourse = 0.354 Mi.
Length along longest watercourse measured to centroid = 0.177 Mi.
Difference in elevation = 79.00(Ft.)
Slope along watercourse = 222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.045 Hr.
Lag time = 2.70 Min.
25% of lag time = 0.68 Min.
40% of lag time = 1.08 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.50	14.22

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.30	36.96

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.300(In)

Point rain (area averaged) = 0.500(In)
Areal adjustment factor = 99.97 %
Adjusted average point rain = 0.500(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	69.00	0.500

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

Slope of intensity-duration curve for a 1 hour storm =0.5500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time		Pattern	Storm Rain	Loss rate(In./Hr)			Effective
	(Hr.)	Percent	(In/Hr)	Max		Low	(In/Hr)
1	0.08	3.30	0.198	(0.316)		0.099	0.099
2	0.17	4.20	0.252	(0.316)		0.126	0.126
3	0.25	4.40	0.264	(0.316)		0.132	0.132
4	0.33	4.80	0.288	(0.316)		0.144	0.144
5	0.42	5.20	0.312	(0.316)		0.156	0.156
6	0.50	6.20	0.372	(0.316)		0.186	0.186
7	0.58	6.80	0.408	(0.316)		0.204	0.204
8	0.67	8.80	0.528	(0.316)		0.264	0.264
9	0.75	13.90	0.834	0.316	(	0.417)	0.518
10	0.83	31.40	1.884	0.316	(	0.942)	1.568
11	0.92	7.20	0.432	(0.316)		0.216	0.216
12	1.00	3.80	0.228	(0.316)		0.114	0.114
		(Loss Rate Not Used)					
Sum =		100.0				Sum =	3.7

Flood volume = Effective rainfall 0.31(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 0.7(Ac.Ft)
Total soil loss = 0.19(In)
Total soil loss = 0.449(Ac.Ft)
Total rainfall = 0.50(In)
Flood volume = 32048.4 Cubic Feet
Total soil loss = 19538.8 Cubic Feet

Peak flow rate of this hydrograph = 25.921(CFS)

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0080	1.16	VQ				
0+10	0.0268	2.73	V Q				
0+15	0.0503	3.41	V Q				
0+20	0.0765	3.81	VQ				
0+25	0.1054	4.19	Q				
0+30	0.1381	4.75	QV				
0+35	0.1752	5.39	Q V				
0+40	0.2194	6.42	Q	V			
0+45	0.2899	10.24		Q V			
0+50	0.4684	25.92			V	Q	
0+55	0.6355	24.27				Q V	
1+ 0	0.6975	9.00		Q		V	
1+ 5	0.7250	3.99	Q				V
1+10	0.7338	1.28	Q				V
1+15	0.7354	0.23	Q				V
1+20	0.7357	0.05	Q				V

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: pro232.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 1871.00(Ft.)
Length along longest watercourse measured to centroid = 935.00(Ft.)
Length along longest watercourse = 0.354 Mi.
Length along longest watercourse measured to centroid = 0.177 Mi.
Difference in elevation = 79.00(Ft.)
Slope along watercourse = 222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.045 Hr.
Lag time = 2.70 Min.
25% of lag time = 0.68 Min.
40% of lag time = 1.08 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.80	22.74

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	2.00	56.86

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 0.800(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 0.800(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	69.00	0.500

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.125	(0.316)	0.062	0.062
2	0.17	1.30	0.125	(0.316)	0.062	0.062
3	0.25	1.10	0.106	(0.316)	0.053	0.053
4	0.33	1.50	0.144	(0.316)	0.072	0.072
5	0.42	1.50	0.144	(0.316)	0.072	0.072
6	0.50	1.80	0.173	(0.316)	0.086	0.086
7	0.58	1.50	0.144	(0.316)	0.072	0.072
8	0.67	1.80	0.173	(0.316)	0.086	0.086
9	0.75	1.80	0.173	(0.316)	0.086	0.086
10	0.83	1.50	0.144	(0.316)	0.072	0.072
11	0.92	1.60	0.154	(0.316)	0.077	0.077
12	1.00	1.80	0.173	(0.316)	0.086	0.086
13	1.08	2.20	0.211	(0.316)	0.106	0.106
14	1.17	2.20	0.211	(0.316)	0.106	0.106
15	1.25	2.20	0.211	(0.316)	0.106	0.106
16	1.33	2.00	0.192	(0.316)	0.096	0.096
17	1.42	2.60	0.250	(0.316)	0.125	0.125
18	1.50	2.70	0.259	(0.316)	0.130	0.130
19	1.58	2.40	0.230	(0.316)	0.115	0.115
20	1.67	2.70	0.259	(0.316)	0.130	0.130
21	1.75	3.30	0.317	(0.316)	0.158	0.158
22	1.83	3.10	0.298	(0.316)	0.149	0.149
23	1.92	2.90	0.278	(0.316)	0.139	0.139
24	2.00	3.00	0.288	(0.316)	0.144	0.144
25	2.08	3.10	0.298	(0.316)	0.149	0.149
26	2.17	4.20	0.403	(0.316)	0.202	0.202
27	2.25	5.00	0.480	(0.316)	0.240	0.240
28	2.33	3.50	0.336	(0.316)	0.168	0.168
29	2.42	6.80	0.653	0.316	(0.326)	0.337
30	2.50	7.30	0.701	0.316	(0.350)	0.385
31	2.58	8.20	0.787	0.316	(0.394)	0.471
32	2.67	5.90	0.566	(0.316)	0.283	0.283
33	2.75	2.00	0.192	(0.316)	0.096	0.096
34	2.83	1.80	0.173	(0.316)	0.086	0.086
35	2.92	1.80	0.173	(0.316)	0.086	0.086
36	3.00	0.60	0.058	(0.316)	0.029	0.029
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	4.9

Flood volume = Effective rainfall 0.41(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 1.0(Ac.Ft)
Total soil loss = 0.39(In)
Total soil loss = 0.923(Ac.Ft)
Total rainfall = 0.80(In)
Flood volume = 42335.0 Cubic Feet
Total soil loss = 40215.4 Cubic Feet

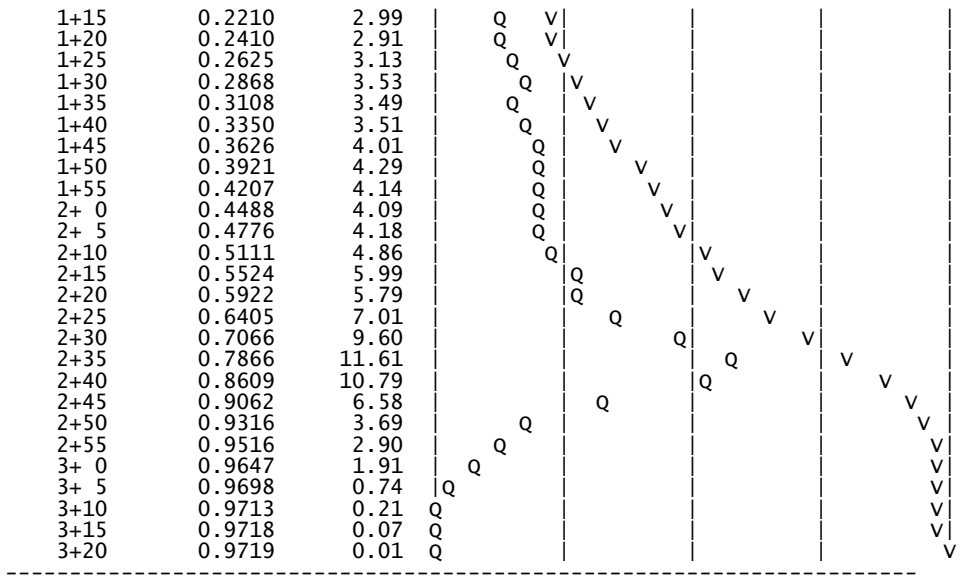
Peak flow rate of this hydrograph = 11.612(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0050	0.73	VQ				
0+10	0.0155	1.52	V Q				
0+15	0.0264	1.58	|V Q				
0+20	0.0384	1.75	|V Q				
0+25	0.0522	2.00	| VQ				
0+30	0.0674	2.21	| V Q				
0+35	0.0828	2.24	| VQ				
0+40	0.0984	2.27	| Q				
0+45	0.1152	2.43	| Q				
0+50	0.1310	2.29	| QV				
0+55	0.1459	2.17	| Q V				
1+ 0	0.1619	2.32	| Q V				
1+ 5	0.1802	2.66	| Q V				
1+10	0.2004	2.93	| Q V				



1+15	0.2210	2.99	
1+20	0.2410	2.91	
1+25	0.2625	3.13	
1+30	0.2868	3.53	
1+35	0.3108	3.49	
1+40	0.3350	3.51	
1+45	0.3626	4.01	
1+50	0.3921	4.29	
1+55	0.4207	4.14	
2+ 0	0.4488	4.09	
2+ 5	0.4776	4.18	
2+10	0.5111	4.86	
2+15	0.5524	5.99	
2+20	0.5922	5.79	
2+25	0.6405	7.01	
2+30	0.7066	9.60	
2+35	0.7866	11.61	
2+40	0.8609	10.79	
2+45	0.9062	6.58	
2+50	0.9316	3.69	
2+55	0.9516	2.90	
3+ 0	0.9647	1.91	
3+ 5	0.9698	0.74	
3+10	0.9713	0.21	
3+15	0.9718	0.07	
3+20	0.9719	0.01	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: pro262.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 1871.00(Ft.)
Length along longest watercourse measured to centroid = 935.00(Ft.)
Length along longest watercourse = 0.354 Mi.
Length along longest watercourse measured to centroid = 0.177 Mi.
Difference in elevation = 79.00(Ft.)
Slope along watercourse = 222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.045 Hr.
Lag time = 2.70 Min.
25% of lag time = 0.68 Min.
40% of lag time = 1.08 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.10	31.27

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	3.00	85.29

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.100(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.100(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	69.00	0.500

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.066	(0.316)	0.033	0.033
2	0.17	0.60	0.079	(0.316)	0.040	0.040
3	0.25	0.60	0.079	(0.316)	0.040	0.040
4	0.33	0.60	0.079	(0.316)	0.040	0.040
5	0.42	0.60	0.079	(0.316)	0.040	0.040
6	0.50	0.70	0.092	(0.316)	0.046	0.046
7	0.58	0.70	0.092	(0.316)	0.046	0.046
8	0.67	0.70	0.092	(0.316)	0.046	0.046
9	0.75	0.70	0.092	(0.316)	0.046	0.046
10	0.83	0.70	0.092	(0.316)	0.046	0.046
11	0.92	0.70	0.092	(0.316)	0.046	0.046
12	1.00	0.80	0.106	(0.316)	0.053	0.053
13	1.08	0.80	0.106	(0.316)	0.053	0.053
14	1.17	0.80	0.106	(0.316)	0.053	0.053
15	1.25	0.80	0.106	(0.316)	0.053	0.053
16	1.33	0.80	0.106	(0.316)	0.053	0.053
17	1.42	0.80	0.106	(0.316)	0.053	0.053
18	1.50	0.80	0.106	(0.316)	0.053	0.053
19	1.58	0.80	0.106	(0.316)	0.053	0.053
20	1.67	0.80	0.106	(0.316)	0.053	0.053
21	1.75	0.80	0.106	(0.316)	0.053	0.053
22	1.83	0.80	0.106	(0.316)	0.053	0.053
23	1.92	0.80	0.106	(0.316)	0.053	0.053
24	2.00	0.90	0.119	(0.316)	0.059	0.059
25	2.08	0.80	0.106	(0.316)	0.053	0.053
26	2.17	0.90	0.119	(0.316)	0.059	0.059
27	2.25	0.90	0.119	(0.316)	0.059	0.059
28	2.33	0.90	0.119	(0.316)	0.059	0.059
29	2.42	0.90	0.119	(0.316)	0.059	0.059
30	2.50	0.90	0.119	(0.316)	0.059	0.059
31	2.58	0.90	0.119	(0.316)	0.059	0.059
32	2.67	0.90	0.119	(0.316)	0.059	0.059
33	2.75	1.00	0.132	(0.316)	0.066	0.066
34	2.83	1.00	0.132	(0.316)	0.066	0.066
35	2.92	1.00	0.132	(0.316)	0.066	0.066
36	3.00	1.00	0.132	(0.316)	0.066	0.066
37	3.08	1.00	0.132	(0.316)	0.066	0.066
38	3.17	1.10	0.145	(0.316)	0.073	0.073
39	3.25	1.10	0.145	(0.316)	0.073	0.073
40	3.33	1.10	0.145	(0.316)	0.073	0.073
41	3.42	1.20	0.158	(0.316)	0.079	0.079
42	3.50	1.30	0.172	(0.316)	0.086	0.086
43	3.58	1.40	0.185	(0.316)	0.092	0.092
44	3.67	1.40	0.185	(0.316)	0.092	0.092
45	3.75	1.50	0.198	(0.316)	0.099	0.099
46	3.83	1.50	0.198	(0.316)	0.099	0.099
47	3.92	1.60	0.211	(0.316)	0.106	0.106
48	4.00	1.60	0.211	(0.316)	0.106	0.106
49	4.08	1.70	0.224	(0.316)	0.112	0.112
50	4.17	1.80	0.238	(0.316)	0.119	0.119
51	4.25	1.90	0.251	(0.316)	0.125	0.125
52	4.33	2.00	0.264	(0.316)	0.132	0.132
53	4.42	2.10	0.277	(0.316)	0.139	0.139
54	4.50	2.10	0.277	(0.316)	0.139	0.139
55	4.58	2.20	0.290	(0.316)	0.145	0.145
56	4.67	2.30	0.304	(0.316)	0.152	0.152
57	4.75	2.40	0.317	(0.316)	0.158	0.158
58	4.83	2.40	0.317	(0.316)	0.158	0.158
59	4.92	2.50	0.330	(0.316)	0.165	0.165
60	5.00	2.60	0.343	(0.316)	0.172	0.172
61	5.08	3.10	0.409	(0.316)	0.205	0.205
62	5.17	3.60	0.475	(0.316)	0.238	0.238
63	5.25	3.90	0.515	(0.316)	0.257	0.257
64	5.33	4.20	0.554	(0.316)	0.277	0.277
65	5.42	4.70	0.620	(0.316)	0.310	0.310
66	5.50	5.60	0.739	0.316	(0.370)	0.423
67	5.58	1.90	0.251	(0.316)	0.125	0.125
68	5.67	0.90	0.119	(0.316)	0.059	0.059
69	5.75	0.60	0.079	(0.316)	0.040	0.040
70	5.83	0.50	0.066	(0.316)	0.033	0.033
71	5.92	0.30	0.040	(0.316)	0.020	0.020

```
72   6.00     0.20      0.026       (  0.316)       0.013        0.013
            (Loss Rate Not Used)
   Sum =     100.0                                   Sum =     6.7
      Flood volume = Effective rainfall      0.55(In)
       times area      28.4(Ac.)/[(In)/(Ft.)] =       1.3(Ac.Ft)
      Total soil loss =      0.55(In)
      Total soil loss =     1.292(Ac.Ft)
      Total rainfall =      1.10(In)
      Flood volume =       57218.4 Cubic Feet
      Total soil loss =       56291.5 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     10.033(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
-------------------------------------------------------------------------
  0+ 5       0.0027      0.39  Q         |         |         |         |
  0+10       0.0087      0.88  VQ        |         |         |         |
  0+15       0.0160      1.06  V Q       |         |         |         |
  0+20       0.0236      1.11  V Q       |         |         |         |
  0+25       0.0314      1.13  V Q       |         |         |         |
  0+30       0.0398      1.21  |VQ       |         |         |         |
  0+35       0.0487      1.30  |VQ       |         |         |         |
  0+40       0.0578      1.31  |VQ       |         |         |         |
  0+45       0.0669      1.32  | Q       |         |         |         |
  0+50       0.0760      1.32  | Q       |         |         |         |
  0+55       0.0851      1.32  | Q       |         |         |         |
  1+ 0       0.0947      1.40  | Q       |         |         |         |
  1+ 5       0.1050      1.49  | QV      |         |         |         |
  1+10       0.1153      1.50  |  Q      |         |         |         |
  1+15       0.1257      1.51  |  Q      |         |         |         |
  1+20       0.1362      1.51  |  QV     |         |         |         |
  1+25       0.1466      1.51  |  QV     |         |         |         |
  1+30       0.1570      1.51  |  QV     |         |         |         |
  1+35       0.1674      1.51  |  Q V    |         |         |         |
  1+40       0.1779      1.51  |  Q V    |         |         |         |
  1+45       0.1883      1.51  |  Q V    |         |         |         |
  1+50       0.1987      1.51  |  Q  V   |         |         |         |
  1+55       0.2091      1.51  |  Q  V   |         |         |         |
  2+ 0       0.2201      1.59  |  Q  V   |         |         |         |
  2+ 5       0.2311      1.60  |  Q   V  |         |         |         |
  2+10       0.2422      1.61  |  Q   V  |         |         |         |
  2+15       0.2537      1.68  |  Q   V  |         |         |         |
  2+20       0.2654      1.70  |  Q    V |         |         |         |
  2+25       0.2771      1.70  |  Q    V |         |         |         |
  2+30       0.2888      1.70  |  Q    V |         |         |         |
  2+35       0.3006      1.70  |  Q     V|         |         |         |
  2+40       0.3123      1.70  |  Q     V|         |         |         |
  2+45       0.3246      1.78  |  Q     V|         |         |         |
  2+50       0.3374      1.86  |  Q      V         |         |         |
  2+55       0.3503      1.88  |  Q      V         |         |         |
  3+ 0       0.3634      1.89  |  Q      |V        |         |         |
  3+ 5       0.3764      1.89  |  Q      |V        |         |         |
  3+10       0.3899      1.97  |  Q      |V        |         |         |
  3+15       0.4041      2.05  |   Q     | V       |         |         |
  3+20       0.4183      2.07  |   Q     | V       |         |         |
  3+25       0.4332      2.15  |   Q     |  V      |         |         |
  3+30       0.4492      2.32  |   Q     |  V      |         |         |
  3+35       0.4664      2.50  |   Q     |   V     |         |         |
  3+40       0.4843      2.61  |    Q    |   V     |         |         |
  3+45       0.5030      2.71  |    Q    |    V    |         |         |
  3+50       0.5223      2.81  |    Q    |    V    |         |         |
  3+55       0.5423      2.90  |    Q    |     V   |         |         |
  4+ 0       0.5630      3.00  |    Q    |      V  |         |         |
  4+ 5       0.5843      3.09  |     Q   |      V  |         |         |
  4+10       0.6067      3.26  |     Q   |       V |         |         |
  4+15       0.6304      3.44  |     Q   |        V|         |         |
  4+20       0.6554      3.63  |      Q  |        V|         |         |
  4+25       0.6817      3.82  |      Q  |         V         |         |
  4+30       0.7088      3.93  |      Q  |         |V        |         |
  4+35       0.7366      4.04  |       Q |         | V       |         |
  4+40       0.7656      4.21  |       Q |         |  V      |         |
  4+45       0.7958      4.39  |       Q |         |   V     |         |
  4+50       0.8268      4.50  |       Q |         |    V    |         |
  4+55       0.8585      4.60  |        Q|         |     V   |         |
  5+ 0       0.8914      4.78  |        Q|         |      V  |         |
  5+ 5       0.9277      5.27  |         Q         |       V |         |
  5+10       0.9697      6.10  |         | Q       |        V|         |
  5+15       1.0168      6.85  |         |  Q      |         V         |
  5+20       1.0682      7.46  |         |   Q     |         | V       |
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    5+25       1.1247      8.20  |          |      Q   |          |   V      |
    5+30       1.1938     10.03  |          |          Q          |      V   |
    5+35       1.2496      8.12  |          |      Q   |          |        V |
    5+40       1.2765      3.90  |          Q          |          |        V |
    5+45       1.2914      2.16  |     Q               |          |          V|
    5+50       1.3010      1.39  |  Q                  |          |          V|
    5+55       1.3070      0.88  |Q                    |          |          V|
    6+ 0       1.3109      0.57  |Q                    |          |          V|
    6+ 5       1.3128      0.28  Q                     |          |          V|
    6+10       1.3133      0.07  Q                     |          |          V|
    6+15       1.3135      0.02  Q                     |          |          V|
    6+20       1.3136      0.01  Q                     |          |           V
-------------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: pro2242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 1871.00(Ft.)
Length along longest watercourse measured to centroid = 935.00(Ft.)
Length along longest watercourse = 0.354 Mi.
Length along longest watercourse measured to centroid = 0.177 Mi.
Difference in elevation = 79.00(Ft.)
Slope along watercourse = 222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.045 Hr.
Lag time = 2.70 Min.
25% of lag time = 0.68 Min.
40% of lag time = 1.08 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.80	51.17

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	5.00	142.15

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 1.800(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.800(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	69.00	0.500

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.014	(0.560)	0.007	0.007
2	0.17	0.07	0.014	(0.557)	0.007	0.007
3	0.25	0.07	0.014	(0.555)	0.007	0.007
4	0.33	0.10	0.022	(0.553)	0.011	0.011
5	0.42	0.10	0.022	(0.551)	0.011	0.011
6	0.50	0.10	0.022	(0.549)	0.011	0.011
7	0.58	0.10	0.022	(0.547)	0.011	0.011
8	0.67	0.10	0.022	(0.545)	0.011	0.011
9	0.75	0.10	0.022	(0.542)	0.011	0.011
10	0.83	0.13	0.029	(0.540)	0.014	0.014
11	0.92	0.13	0.029	(0.538)	0.014	0.014
12	1.00	0.13	0.029	(0.536)	0.014	0.014
13	1.08	0.10	0.022	(0.534)	0.011	0.011
14	1.17	0.10	0.022	(0.532)	0.011	0.011
15	1.25	0.10	0.022	(0.530)	0.011	0.011
16	1.33	0.10	0.022	(0.528)	0.011	0.011
17	1.42	0.10	0.022	(0.525)	0.011	0.011
18	1.50	0.10	0.022	(0.523)	0.011	0.011
19	1.58	0.10	0.022	(0.521)	0.011	0.011
20	1.67	0.10	0.022	(0.519)	0.011	0.011
21	1.75	0.10	0.022	(0.517)	0.011	0.011
22	1.83	0.13	0.029	(0.515)	0.014	0.014
23	1.92	0.13	0.029	(0.513)	0.014	0.014
24	2.00	0.13	0.029	(0.511)	0.014	0.014
25	2.08	0.13	0.029	(0.509)	0.014	0.014
26	2.17	0.13	0.029	(0.507)	0.014	0.014
27	2.25	0.13	0.029	(0.505)	0.014	0.014
28	2.33	0.13	0.029	(0.503)	0.014	0.014
29	2.42	0.13	0.029	(0.501)	0.014	0.014
30	2.50	0.13	0.029	(0.499)	0.014	0.014
31	2.58	0.17	0.036	(0.497)	0.018	0.018
32	2.67	0.17	0.036	(0.494)	0.018	0.018
33	2.75	0.17	0.036	(0.492)	0.018	0.018
34	2.83	0.17	0.036	(0.490)	0.018	0.018
35	2.92	0.17	0.036	(0.488)	0.018	0.018
36	3.00	0.17	0.036	(0.486)	0.018	0.018
37	3.08	0.17	0.036	(0.484)	0.018	0.018
38	3.17	0.17	0.036	(0.482)	0.018	0.018
39	3.25	0.17	0.036	(0.480)	0.018	0.018
40	3.33	0.17	0.036	(0.478)	0.018	0.018
41	3.42	0.17	0.036	(0.476)	0.018	0.018
42	3.50	0.17	0.036	(0.474)	0.018	0.018
43	3.58	0.17	0.036	(0.472)	0.018	0.018
44	3.67	0.17	0.036	(0.470)	0.018	0.018
45	3.75	0.17	0.036	(0.468)	0.018	0.018
46	3.83	0.20	0.043	(0.466)	0.022	0.022
47	3.92	0.20	0.043	(0.464)	0.022	0.022
48	4.00	0.20	0.043	(0.463)	0.022	0.022
49	4.08	0.20	0.043	(0.461)	0.022	0.022
50	4.17	0.20	0.043	(0.459)	0.022	0.022
51	4.25	0.20	0.043	(0.457)	0.022	0.022
52	4.33	0.23	0.050	(0.455)	0.025	0.025
53	4.42	0.23	0.050	(0.453)	0.025	0.025
54	4.50	0.23	0.050	(0.451)	0.025	0.025
55	4.58	0.23	0.050	(0.449)	0.025	0.025
56	4.67	0.23	0.050	(0.447)	0.025	0.025
57	4.75	0.23	0.050	(0.445)	0.025	0.025
58	4.83	0.27	0.058	(0.443)	0.029	0.029
59	4.92	0.27	0.058	(0.441)	0.029	0.029
60	5.00	0.27	0.058	(0.439)	0.029	0.029
61	5.08	0.20	0.043	(0.437)	0.022	0.022
62	5.17	0.20	0.043	(0.435)	0.022	0.022
63	5.25	0.20	0.043	(0.434)	0.022	0.022
64	5.33	0.23	0.050	(0.432)	0.025	0.025
65	5.42	0.23	0.050	(0.430)	0.025	0.025
66	5.50	0.23	0.050	(0.428)	0.025	0.025
67	5.58	0.27	0.058	(0.426)	0.029	0.029
68	5.67	0.27	0.058	(0.424)	0.029	0.029
69	5.75	0.27	0.058	(0.422)	0.029	0.029
70	5.83	0.27	0.058	(0.420)	0.029	0.029
71	5.92	0.27	0.058	(0.419)	0.029	0.029

72	6.00	0.27	0.058	(0.417)	0.029	0.029
73	6.08	0.30	0.065	(0.415)	0.032	0.032
74	6.17	0.30	0.065	(0.413)	0.032	0.032
75	6.25	0.30	0.065	(0.411)	0.032	0.032
76	6.33	0.30	0.065	(0.409)	0.032	0.032
77	6.42	0.30	0.065	(0.407)	0.032	0.032
78	6.50	0.30	0.065	(0.406)	0.032	0.032
79	6.58	0.33	0.072	(0.404)	0.036	0.036
80	6.67	0.33	0.072	(0.402)	0.036	0.036
81	6.75	0.33	0.072	(0.400)	0.036	0.036
82	6.83	0.33	0.072	(0.398)	0.036	0.036
83	6.92	0.33	0.072	(0.397)	0.036	0.036
84	7.00	0.33	0.072	(0.395)	0.036	0.036
85	7.08	0.33	0.072	(0.393)	0.036	0.036
86	7.17	0.33	0.072	(0.391)	0.036	0.036
87	7.25	0.33	0.072	(0.389)	0.036	0.036
88	7.33	0.37	0.079	(0.388)	0.040	0.040
89	7.42	0.37	0.079	(0.386)	0.040	0.040
90	7.50	0.37	0.079	(0.384)	0.040	0.040
91	7.58	0.40	0.086	(0.382)	0.043	0.043
92	7.67	0.40	0.086	(0.381)	0.043	0.043
93	7.75	0.40	0.086	(0.379)	0.043	0.043
94	7.83	0.43	0.094	(0.377)	0.047	0.047
95	7.92	0.43	0.094	(0.375)	0.047	0.047
96	8.00	0.43	0.094	(0.374)	0.047	0.047
97	8.08	0.50	0.108	(0.372)	0.054	0.054
98	8.17	0.50	0.108	(0.370)	0.054	0.054
99	8.25	0.50	0.108	(0.368)	0.054	0.054
100	8.33	0.50	0.108	(0.367)	0.054	0.054
101	8.42	0.50	0.108	(0.365)	0.054	0.054
102	8.50	0.50	0.108	(0.363)	0.054	0.054
103	8.58	0.53	0.115	(0.362)	0.058	0.058
104	8.67	0.53	0.115	(0.360)	0.058	0.058
105	8.75	0.53	0.115	(0.358)	0.058	0.058
106	8.83	0.57	0.122	(0.356)	0.061	0.061
107	8.92	0.57	0.122	(0.355)	0.061	0.061
108	9.00	0.57	0.122	(0.353)	0.061	0.061
109	9.08	0.63	0.137	(0.351)	0.068	0.068
110	9.17	0.63	0.137	(0.350)	0.068	0.068
111	9.25	0.63	0.137	(0.348)	0.068	0.068
112	9.33	0.67	0.144	(0.346)	0.072	0.072
113	9.42	0.67	0.144	(0.345)	0.072	0.072
114	9.50	0.67	0.144	(0.343)	0.072	0.072
115	9.58	0.70	0.151	(0.341)	0.076	0.076
116	9.67	0.70	0.151	(0.340)	0.076	0.076
117	9.75	0.70	0.151	(0.338)	0.076	0.076
118	9.83	0.73	0.158	(0.337)	0.079	0.079
119	9.92	0.73	0.158	(0.335)	0.079	0.079
120	10.00	0.73	0.158	(0.333)	0.079	0.079
121	10.08	0.50	0.108	(0.332)	0.054	0.054
122	10.17	0.50	0.108	(0.330)	0.054	0.054
123	10.25	0.50	0.108	(0.329)	0.054	0.054
124	10.33	0.50	0.108	(0.327)	0.054	0.054
125	10.42	0.50	0.108	(0.325)	0.054	0.054
126	10.50	0.50	0.108	(0.324)	0.054	0.054
127	10.58	0.67	0.144	(0.322)	0.072	0.072
128	10.67	0.67	0.144	(0.321)	0.072	0.072
129	10.75	0.67	0.144	(0.319)	0.072	0.072
130	10.83	0.67	0.144	(0.317)	0.072	0.072
131	10.92	0.67	0.144	(0.316)	0.072	0.072
132	11.00	0.67	0.144	(0.314)	0.072	0.072
133	11.08	0.63	0.137	(0.313)	0.068	0.068
134	11.17	0.63	0.137	(0.311)	0.068	0.068
135	11.25	0.63	0.137	(0.310)	0.068	0.068
136	11.33	0.63	0.137	(0.308)	0.068	0.068
137	11.42	0.63	0.137	(0.307)	0.068	0.068
138	11.50	0.63	0.137	(0.305)	0.068	0.068
139	11.58	0.57	0.122	(0.304)	0.061	0.061
140	11.67	0.57	0.122	(0.302)	0.061	0.061
141	11.75	0.57	0.122	(0.301)	0.061	0.061
142	11.83	0.60	0.130	(0.299)	0.065	0.065
143	11.92	0.60	0.130	(0.298)	0.065	0.065
144	12.00	0.60	0.130	(0.296)	0.065	0.065
145	12.08	0.83	0.180	(0.295)	0.090	0.090
146	12.17	0.83	0.180	(0.293)	0.090	0.090
147	12.25	0.83	0.180	(0.292)	0.090	0.090
148	12.33	0.87	0.187	(0.290)	0.094	0.094
149	12.42	0.87	0.187	(0.289)	0.094	0.094
150	12.50	0.87	0.187	(0.287)	0.094	0.094
151	12.58	0.93	0.202	(0.286)	0.101	0.101
152	12.67	0.93	0.202	(0.284)	0.101	0.101
153	12.75	0.93	0.202	(0.283)	0.101	0.101
154	12.83	0.97	0.209	(0.282)	0.104	0.104
155	12.92	0.97	0.209	(0.280)	0.104	0.104
156	13.00	0.97	0.209	(0.279)	0.104	0.104
157	13.08	1.13	0.245	(0.277)	0.122	0.122

158	13.17	1.13	0.245	(0.276)	0.122	0.122
159	13.25	1.13	0.245	(0.275)	0.122	0.122
160	13.33	1.13	0.245	(0.273)	0.122	0.122
161	13.42	1.13	0.245	(0.272)	0.122	0.122
162	13.50	1.13	0.245	(0.270)	0.122	0.122
163	13.58	0.77	0.166	(0.269)	0.083	0.083
164	13.67	0.77	0.166	(0.268)	0.083	0.083
165	13.75	0.77	0.166	(0.266)	0.083	0.083
166	13.83	0.77	0.166	(0.265)	0.083	0.083
167	13.92	0.77	0.166	(0.264)	0.083	0.083
168	14.00	0.77	0.166	(0.262)	0.083	0.083
169	14.08	0.90	0.194	(0.261)	0.097	0.097
170	14.17	0.90	0.194	(0.260)	0.097	0.097
171	14.25	0.90	0.194	(0.258)	0.097	0.097
172	14.33	0.87	0.187	(0.257)	0.094	0.094
173	14.42	0.87	0.187	(0.256)	0.094	0.094
174	14.50	0.87	0.187	(0.254)	0.094	0.094
175	14.58	0.87	0.187	(0.253)	0.094	0.094
176	14.67	0.87	0.187	(0.252)	0.094	0.094
177	14.75	0.87	0.187	(0.250)	0.094	0.094
178	14.83	0.83	0.180	(0.249)	0.090	0.090
179	14.92	0.83	0.180	(0.248)	0.090	0.090
180	15.00	0.83	0.180	(0.247)	0.090	0.090
181	15.08	0.80	0.173	(0.245)	0.086	0.086
182	15.17	0.80	0.173	(0.244)	0.086	0.086
183	15.25	0.80	0.173	(0.243)	0.086	0.086
184	15.33	0.77	0.166	(0.242)	0.083	0.083
185	15.42	0.77	0.166	(0.240)	0.083	0.083
186	15.50	0.77	0.166	(0.239)	0.083	0.083
187	15.58	0.63	0.137	(0.238)	0.068	0.068
188	15.67	0.63	0.137	(0.237)	0.068	0.068
189	15.75	0.63	0.137	(0.235)	0.068	0.068
190	15.83	0.63	0.137	(0.234)	0.068	0.068
191	15.92	0.63	0.137	(0.233)	0.068	0.068
192	16.00	0.63	0.137	(0.232)	0.068	0.068
193	16.08	0.13	0.029	(0.231)	0.014	0.014
194	16.17	0.13	0.029	(0.229)	0.014	0.014
195	16.25	0.13	0.029	(0.228)	0.014	0.014
196	16.33	0.13	0.029	(0.227)	0.014	0.014
197	16.42	0.13	0.029	(0.226)	0.014	0.014
198	16.50	0.13	0.029	(0.225)	0.014	0.014
199	16.58	0.10	0.022	(0.224)	0.011	0.011
200	16.67	0.10	0.022	(0.223)	0.011	0.011
201	16.75	0.10	0.022	(0.221)	0.011	0.011
202	16.83	0.10	0.022	(0.220)	0.011	0.011
203	16.92	0.10	0.022	(0.219)	0.011	0.011
204	17.00	0.10	0.022	(0.218)	0.011	0.011
205	17.08	0.17	0.036	(0.217)	0.018	0.018
206	17.17	0.17	0.036	(0.216)	0.018	0.018
207	17.25	0.17	0.036	(0.215)	0.018	0.018
208	17.33	0.17	0.036	(0.214)	0.018	0.018
209	17.42	0.17	0.036	(0.213)	0.018	0.018
210	17.50	0.17	0.036	(0.212)	0.018	0.018
211	17.58	0.17	0.036	(0.211)	0.018	0.018
212	17.67	0.17	0.036	(0.209)	0.018	0.018
213	17.75	0.17	0.036	(0.208)	0.018	0.018
214	17.83	0.13	0.029	(0.207)	0.014	0.014
215	17.92	0.13	0.029	(0.206)	0.014	0.014
216	18.00	0.13	0.029	(0.205)	0.014	0.014
217	18.08	0.13	0.029	(0.204)	0.014	0.014
218	18.17	0.13	0.029	(0.203)	0.014	0.014
219	18.25	0.13	0.029	(0.202)	0.014	0.014
220	18.33	0.13	0.029	(0.201)	0.014	0.014
221	18.42	0.13	0.029	(0.200)	0.014	0.014
222	18.50	0.13	0.029	(0.199)	0.014	0.014
223	18.58	0.10	0.022	(0.198)	0.011	0.011
224	18.67	0.10	0.022	(0.197)	0.011	0.011
225	18.75	0.10	0.022	(0.197)	0.011	0.011
226	18.83	0.07	0.014	(0.196)	0.007	0.007
227	18.92	0.07	0.014	(0.195)	0.007	0.007
228	19.00	0.07	0.014	(0.194)	0.007	0.007
229	19.08	0.10	0.022	(0.193)	0.011	0.011
230	19.17	0.10	0.022	(0.192)	0.011	0.011
231	19.25	0.10	0.022	(0.191)	0.011	0.011
232	19.33	0.13	0.029	(0.190)	0.014	0.014
233	19.42	0.13	0.029	(0.189)	0.014	0.014
234	19.50	0.13	0.029	(0.188)	0.014	0.014
235	19.58	0.10	0.022	(0.187)	0.011	0.011
236	19.67	0.10	0.022	(0.187)	0.011	0.011
237	19.75	0.10	0.022	(0.186)	0.011	0.011
238	19.83	0.07	0.014	(0.185)	0.007	0.007
239	19.92	0.07	0.014	(0.184)	0.007	0.007
240	20.00	0.07	0.014	(0.183)	0.007	0.007
241	20.08	0.10	0.022	(0.182)	0.011	0.011
242	20.17	0.10	0.022	(0.182)	0.011	0.011
243	20.25	0.10	0.022	(0.181)	0.011	0.011

244	20.33	0.10	0.022	(0.180)	0.011	0.011
245	20.42	0.10	0.022	(0.179)	0.011	0.011
246	20.50	0.10	0.022	(0.179)	0.011	0.011
247	20.58	0.10	0.022	(0.178)	0.011	0.011
248	20.67	0.10	0.022	(0.177)	0.011	0.011
249	20.75	0.10	0.022	(0.176)	0.011	0.011
250	20.83	0.07	0.014	(0.176)	0.007	0.007
251	20.92	0.07	0.014	(0.175)	0.007	0.007
252	21.00	0.07	0.014	(0.174)	0.007	0.007
253	21.08	0.10	0.022	(0.174)	0.011	0.011
254	21.17	0.10	0.022	(0.173)	0.011	0.011
255	21.25	0.10	0.022	(0.172)	0.011	0.011
256	21.33	0.07	0.014	(0.172)	0.007	0.007
257	21.42	0.07	0.014	(0.171)	0.007	0.007
258	21.50	0.07	0.014	(0.170)	0.007	0.007
259	21.58	0.10	0.022	(0.170)	0.011	0.011
260	21.67	0.10	0.022	(0.169)	0.011	0.011
261	21.75	0.10	0.022	(0.168)	0.011	0.011
262	21.83	0.07	0.014	(0.168)	0.007	0.007
263	21.92	0.07	0.014	(0.167)	0.007	0.007
264	22.00	0.07	0.014	(0.167)	0.007	0.007
265	22.08	0.10	0.022	(0.166)	0.011	0.011
266	22.17	0.10	0.022	(0.166)	0.011	0.011
267	22.25	0.10	0.022	(0.165)	0.011	0.011
268	22.33	0.07	0.014	(0.165)	0.007	0.007
269	22.42	0.07	0.014	(0.164)	0.007	0.007
270	22.50	0.07	0.014	(0.164)	0.007	0.007
271	22.58	0.07	0.014	(0.163)	0.007	0.007
272	22.67	0.07	0.014	(0.163)	0.007	0.007
273	22.75	0.07	0.014	(0.162)	0.007	0.007
274	22.83	0.07	0.014	(0.162)	0.007	0.007
275	22.92	0.07	0.014	(0.161)	0.007	0.007
276	23.00	0.07	0.014	(0.161)	0.007	0.007
277	23.08	0.07	0.014	(0.161)	0.007	0.007
278	23.17	0.07	0.014	(0.160)	0.007	0.007
279	23.25	0.07	0.014	(0.160)	0.007	0.007
280	23.33	0.07	0.014	(0.160)	0.007	0.007
281	23.42	0.07	0.014	(0.159)	0.007	0.007
282	23.50	0.07	0.014	(0.159)	0.007	0.007
283	23.58	0.07	0.014	(0.159)	0.007	0.007
284	23.67	0.07	0.014	(0.158)	0.007	0.007
285	23.75	0.07	0.014	(0.158)	0.007	0.007
286	23.83	0.07	0.014	(0.158)	0.007	0.007
287	23.92	0.07	0.014	(0.158)	0.007	0.007
288	24.00	0.07	0.014	(0.158)	0.007	0.007

(Loss Rate Not Used)

Sum = 100.0 Sum = 10.8

Flood volume = Effective rainfall 0.90(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 2.1(Ac.Ft)
Total soil loss = 0.90(In)
Total soil loss = 2.132(Ac.Ft)
Total rainfall = 1.80(In)
Flood volume = 92875.7 Cubic Feet
Total soil loss = 92875.7 Cubic Feet

Peak flow rate of this hydrograph = 3.509(CFS)

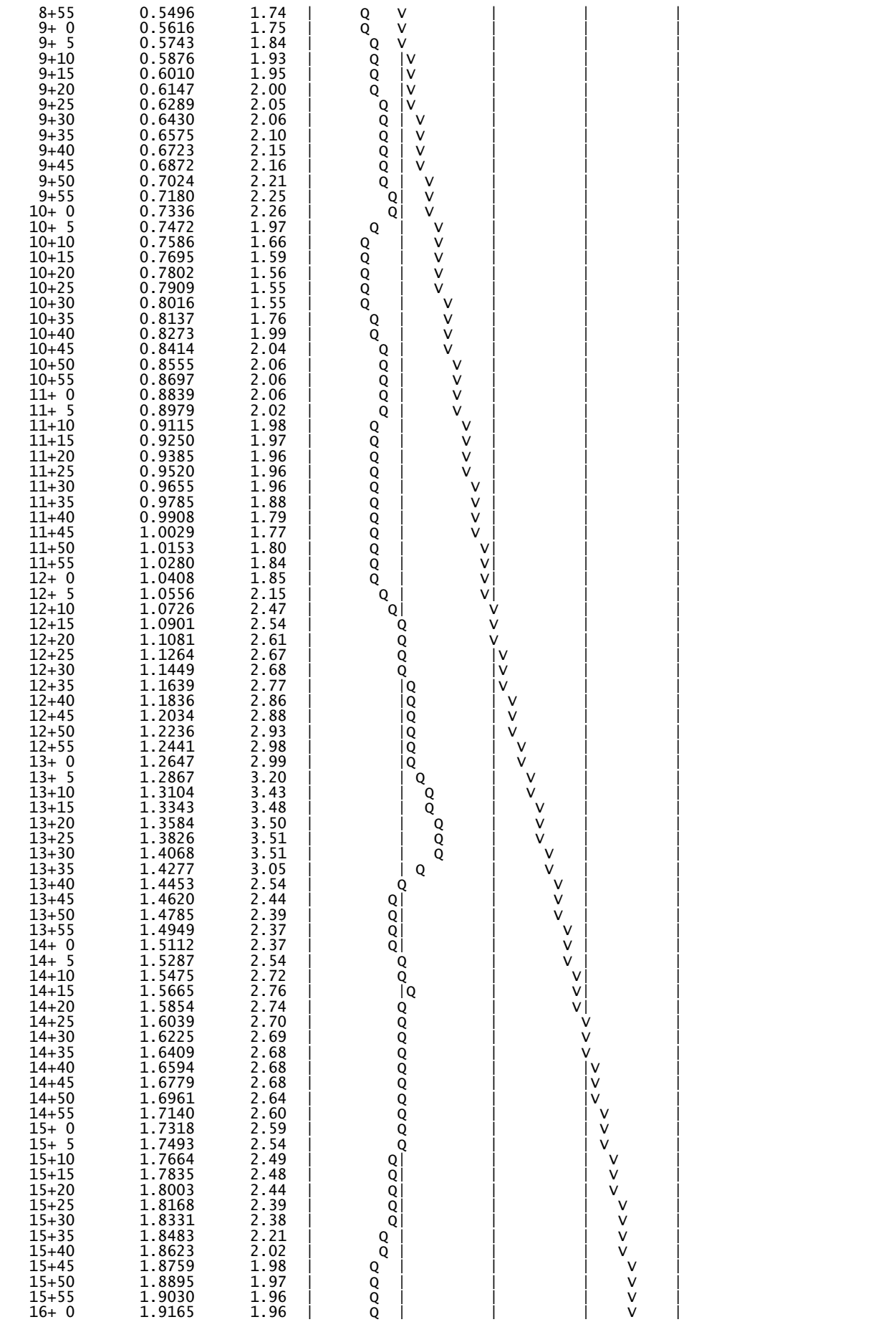
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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0006	0.08	Q				
0+10	0.0018	0.18	Q				
0+15	0.0031	0.20	Q				
0+20	0.0048	0.25	Q				
0+25	0.0068	0.29	VQ				
0+30	0.0089	0.30	VQ				
0+35	0.0111	0.31	VQ				
0+40	0.0132	0.31	VQ				
0+45	0.0153	0.31	VQ				
0+50	0.0177	0.35	VQ				
0+55	0.0205	0.40	VQ				
1+ 0	0.0233	0.41	VQ				
1+ 5	0.0258	0.37	VQ				
1+10	0.0281	0.32	VQ				
1+15	0.0302	0.32	VQ				
1+20	0.0324	0.31	VQ				
1+25	0.0345	0.31	VQ				
1+30	0.0366	0.31	VQ				
1+35	0.0388	0.31	VQ				
1+40	0.0409	0.31	VQ				

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1+45      0.0430      0.31  VQ        |         |         |         |
1+50      0.0455      0.35  VQ        |         |         |         |
1+55      0.0482      0.40  VQ        |         |         |         |
2+ 0      0.0510      0.41  VQ        |         |         |         |
2+ 5      0.0538      0.41  |Q        |         |         |         |
2+10      0.0567      0.41  |Q        |         |         |         |
2+15      0.0595      0.41  |Q        |         |         |         |
2+20      0.0624      0.41  |Q        |         |         |         |
2+25      0.0652      0.41  |Q        |         |         |         |
2+30      0.0681      0.41  |Q        |         |         |         |
2+35      0.0712      0.45  |Q        |         |         |         |
2+40      0.0746      0.50  |VQ       |         |         |         |
2+45      0.0781      0.51  |VQ       |         |         |         |
2+50      0.0817      0.51  |VQ       |         |         |         |
2+55      0.0852      0.52  |VQ       |         |         |         |
3+ 0      0.0888      0.52  |VQ       |         |         |         |
3+ 5      0.0923      0.52  |VQ       |         |         |         |
3+10      0.0959      0.52  |VQ       |         |         |         |
3+15      0.0995      0.52  |VQ       |         |         |         |
3+20      0.1030      0.52  |VQ       |         |         |         |
3+25      0.1066      0.52  |VQ       |         |         |         |
3+30      0.1101      0.52  | Q       |         |         |         |
3+35      0.1137      0.52  | Q       |         |         |         |
3+40      0.1172      0.52  | Q       |         |         |         |
3+45      0.1208      0.52  | Q       |         |         |         |
3+50      0.1246      0.56  | Q       |         |         |         |
3+55      0.1288      0.60  | Q       |         |         |         |
4+ 0      0.1330      0.61  | Q       |         |         |         |
4+ 5      0.1373      0.62  | Q       |         |         |         |
4+10      0.1415      0.62  | Q       |         |         |         |
4+15      0.1458      0.62  | Q       |         |         |         |
4+20      0.1503      0.66  | Q       |         |         |         |
4+25      0.1552      0.71  | Q       |         |         |         |
4+30      0.1601      0.72  | QV      |         |         |         |
4+35      0.1651      0.72  | QV      |         |         |         |
4+40      0.1701      0.72  | QV      |         |         |         |
4+45      0.1751      0.72  | QV      |         |         |         |
4+50      0.1803      0.76  |  Q      |         |         |         |
4+55      0.1859      0.81  |  Q      |         |         |         |
5+ 0      0.1915      0.82  |  Q      |         |         |         |
5+ 5      0.1966      0.74  | QV      |         |         |         |
5+10      0.2011      0.65  | QV      |         |         |         |
5+15      0.2055      0.63  | QV      |         |         |         |
5+20      0.2100      0.66  | QV      |         |         |         |
5+25      0.2149      0.71  | Q V     |         |         |         |
5+30      0.2198      0.72  | Q V     |         |         |         |
5+35      0.2251      0.76  |  QV     |         |         |         |
5+40      0.2307      0.81  |  QV     |         |         |         |
5+45      0.2363      0.82  |  QV     |         |         |         |
5+50      0.2420      0.82  |  QV     |         |         |         |
5+55      0.2477      0.83  |  QV     |         |         |         |
6+ 0      0.2534      0.83  |  QV     |         |         |         |
6+ 5      0.2593      0.87  |  QV     |         |         |         |
6+10      0.2656      0.91  |  QV     |         |         |         |
6+15      0.2720      0.92  |  Q V    |         |         |         |
6+20      0.2784      0.93  |  Q V    |         |         |         |
6+25      0.2848      0.93  |  Q V    |         |         |         |
6+30      0.2912      0.93  |  Q V    |         |         |         |
6+35      0.2979      0.97  |  Q V    |         |         |         |
6+40      0.3049      1.02  |   QV    |         |         |         |
6+45      0.3119      1.03  |   QV    |         |         |         |
6+50      0.3190      1.03  |   QV    |         |         |         |
6+55      0.3261      1.03  |   Q V   |         |         |         |
7+ 0      0.3332      1.03  |   Q V   |         |         |         |
7+ 5      0.3403      1.03  |   Q V   |         |         |         |
7+10      0.3475      1.03  |   Q V   |         |         |         |
7+15      0.3546      1.03  |   Q V   |         |         |         |
7+20      0.3620      1.07  |   Q V   |         |         |         |
7+25      0.3697      1.12  |   Q V   |         |         |         |
7+30      0.3774      1.13  |   Q  V  |         |         |         |
7+35      0.3855      1.18  |   Q  V  |         |         |         |
7+40      0.3940      1.22  |   Q  V  |         |         |         |
7+45      0.4025      1.23  |   Q  V  |         |         |         |
7+50      0.4113      1.28  |    Q V  |         |         |         |
7+55      0.4204      1.33  |    Q V  |         |         |         |
8+ 0      0.4296      1.34  |    Q  V |         |         |         |
8+ 5      0.4394      1.42  |    Q  V |         |         |         |
8+10      0.4498      1.52  |     Q V |         |         |         |
8+15      0.4604      1.54  |     Q V |         |         |         |
8+20      0.4711      1.54  |     Q V |         |         |         |
8+25      0.4817      1.55  |     Q  V|         |         |         |
8+30      0.4924      1.55  |     Q  V|         |         |         |
8+35      0.5033      1.59  |     Q  V|         |         |         |
8+40      0.5146      1.64  |     Q  V|         |         |         |
8+45      0.5259      1.65  |     Q  V|         |         |         |
8+50      0.5376      1.69  |     Q   V         |         |         |
```



8+55	0.5496	1.74	
9+ 0	0.5616	1.75	
9+ 5	0.5743	1.84	
9+10	0.5876	1.93	
9+15	0.6010	1.95	
9+20	0.6147	2.00	
9+25	0.6289	2.05	
9+30	0.6430	2.06	
9+35	0.6575	2.10	
9+40	0.6723	2.15	
9+45	0.6872	2.16	
9+50	0.7024	2.21	
9+55	0.7180	2.25	
10+ 0	0.7336	2.26	
10+ 5	0.7472	1.97	
10+10	0.7586	1.66	
10+15	0.7695	1.59	
10+20	0.7802	1.56	
10+25	0.7909	1.55	
10+30	0.8016	1.55	
10+35	0.8137	1.76	
10+40	0.8273	1.99	
10+45	0.8414	2.04	
10+50	0.8555	2.06	
10+55	0.8697	2.06	
11+ 0	0.8839	2.06	
11+ 5	0.8979	2.02	
11+10	0.9115	1.98	
11+15	0.9250	1.97	
11+20	0.9385	1.96	
11+25	0.9520	1.96	
11+30	0.9655	1.96	
11+35	0.9785	1.88	
11+40	0.9908	1.79	
11+45	1.0029	1.77	
11+50	1.0153	1.80	
11+55	1.0280	1.84	
12+ 0	1.0408	1.85	
12+ 5	1.0556	2.15	
12+10	1.0726	2.47	
12+15	1.0901	2.54	
12+20	1.1081	2.61	
12+25	1.1264	2.67	
12+30	1.1449	2.68	
12+35	1.1639	2.77	
12+40	1.1836	2.86	
12+45	1.2034	2.88	
12+50	1.2236	2.93	
12+55	1.2441	2.98	
13+ 0	1.2647	2.99	
13+ 5	1.2867	3.20	
13+10	1.3104	3.43	
13+15	1.3343	3.48	
13+20	1.3584	3.50	
13+25	1.3826	3.51	
13+30	1.4068	3.51	
13+35	1.4277	3.05	
13+40	1.4453	2.54	
13+45	1.4620	2.44	
13+50	1.4785	2.39	
13+55	1.4949	2.37	
14+ 0	1.5112	2.37	
14+ 5	1.5287	2.54	
14+10	1.5475	2.72	
14+15	1.5665	2.76	
14+20	1.5854	2.74	
14+25	1.6039	2.70	
14+30	1.6225	2.69	
14+35	1.6409	2.68	
14+40	1.6594	2.68	
14+45	1.6779	2.68	
14+50	1.6961	2.64	
14+55	1.7140	2.60	
15+ 0	1.7318	2.59	
15+ 5	1.7493	2.54	
15+10	1.7664	2.49	
15+15	1.7835	2.48	
15+20	1.8003	2.44	
15+25	1.8168	2.39	
15+30	1.8331	2.38	
15+35	1.8483	2.21	
15+40	1.8623	2.02	
15+45	1.8759	1.98	
15+50	1.8895	1.97	
15+55	1.9030	1.96	
16+ 0	1.9165	1.96	

```
16+ 5       1.9256      1.33  |    Q    |         |         |     V   |
16+10       1.9301      0.64  | Q       |         |         |     V   |
16+15       1.9335      0.50  |Q        |         |         |     V   |
16+20       1.9365      0.44  |Q        |         |         |     V   |
16+25       1.9394      0.41  |Q        |         |         |     V   |
16+30       1.9422      0.41  |Q        |         |         |     V   |
16+35       1.9447      0.37  |Q        |         |         |     V   |
16+40       1.9470      0.32  |Q        |         |         |     V   |
16+45       1.9492      0.32  |Q        |         |         |     V   |
16+50       1.9513      0.31  |Q        |         |         |     V   |
16+55       1.9534      0.31  |Q        |         |         |     V   |
17+ 0       1.9556      0.31  |Q        |         |         |     V   |
17+ 5       1.9583      0.39  |Q        |         |         |     V   |
17+10       1.9616      0.49  |Q        |         |         |     V   |
17+15       1.9651      0.50  | Q       |         |         |     V   |
17+20       1.9686      0.51  | Q       |         |         |     V   |
17+25       1.9722      0.52  | Q       |         |         |     V   |
17+30       1.9757      0.52  | Q       |         |         |      V  |
17+35       1.9793      0.52  | Q       |         |         |      V  |
17+40       1.9828      0.52  | Q       |         |         |      V  |
17+45       1.9864      0.52  | Q       |         |         |      V  |
17+50       1.9897      0.47  |Q        |         |         |      V  |
17+55       1.9926      0.43  |Q        |         |         |      V  |
18+ 0       1.9955      0.42  |Q        |         |         |      V  |
18+ 5       1.9983      0.41  |Q        |         |         |      V  |
18+10       2.0012      0.41  |Q        |         |         |      V  |
18+15       2.0040      0.41  |Q        |         |         |      V  |
18+20       2.0069      0.41  |Q        |         |         |      V  |
18+25       2.0097      0.41  |Q        |         |         |      V  |
18+30       2.0126      0.41  |Q        |         |         |      V  |
18+35       2.0151      0.37  |Q        |         |         |      V  |
18+40       2.0173      0.32  |Q        |         |         |      V  |
18+45       2.0195      0.32  |Q        |         |         |      V  |
18+50       2.0214      0.27  |Q        |         |         |      V  |
18+55       2.0229      0.22  Q         |         |         |      V  |
19+ 0       2.0244      0.21  Q         |         |         |      V  |
19+ 5       2.0261      0.25  |Q        |         |         |       V |
19+10       2.0281      0.29  |Q        |         |         |       V |
19+15       2.0302      0.30  |Q        |         |         |       V |
19+20       2.0326      0.35  |Q        |         |         |       V |
19+25       2.0353      0.40  |Q        |         |         |       V |
19+30       2.0382      0.41  |Q        |         |         |       V |
19+35       2.0407      0.37  |Q        |         |         |       V |
19+40       2.0429      0.32  |Q        |         |         |       V |
19+45       2.0451      0.32  |Q        |         |         |       V |
19+50       2.0470      0.27  |Q        |         |         |       V |
19+55       2.0485      0.22  Q         |         |         |       V |
20+ 0       2.0499      0.21  Q         |         |         |       V |
20+ 5       2.0517      0.25  |Q        |         |         |       V |
20+10       2.0537      0.29  |Q        |         |         |       V |
20+15       2.0558      0.30  |Q        |         |         |       V |
20+20       2.0579      0.31  |Q        |         |         |       V |
20+25       2.0600      0.31  |Q        |         |         |       V |
20+30       2.0622      0.31  |Q        |         |         |       V |
20+35       2.0643      0.31  |Q        |         |         |       V |
20+40       2.0664      0.31  |Q        |         |         |       V |
20+45       2.0686      0.31  |Q        |         |         |       V |
20+50       2.0704      0.27  |Q        |         |         |       V |
20+55       2.0719      0.22  Q         |         |         |       V |
21+ 0       2.0734      0.21  Q         |         |         |       V |
21+ 5       2.0751      0.25  |Q        |         |         |       V |
21+10       2.0771      0.29  |Q        |         |         |       V |
21+15       2.0792      0.30  |Q        |         |         |        V|
21+20       2.0811      0.27  |Q        |         |         |        V|
21+25       2.0826      0.22  Q         |         |         |        V|
21+30       2.0841      0.21  Q         |         |         |        V|
21+35       2.0858      0.25  |Q        |         |         |        V|
21+40       2.0878      0.29  |Q        |         |         |        V|
21+45       2.0899      0.30  |Q        |         |         |        V|
21+50       2.0917      0.27  |Q        |         |         |        V|
21+55       2.0933      0.22  Q         |         |         |        V|
22+ 0       2.0947      0.21  Q         |         |         |        V|
22+ 5       2.0964      0.25  |Q        |         |         |        V|
22+10       2.0985      0.29  |Q        |         |         |        V|
22+15       2.1006      0.30  |Q        |         |         |        V|
22+20       2.1024      0.27  |Q        |         |         |        V|
22+25       2.1039      0.22  Q         |         |         |        V|
22+30       2.1054      0.21  Q         |         |         |        V|
22+35       2.1068      0.21  Q         |         |         |        V|
22+40       2.1082      0.21  Q         |         |         |        V|
22+45       2.1097      0.21  Q         |         |         |        V|
22+50       2.1111      0.21  Q         |         |         |        V|
22+55       2.1125      0.21  Q         |         |         |        V|
23+ 0       2.1139      0.21  Q         |         |         |        V|
23+ 5       2.1153      0.21  Q         |         |         |        V|
23+10       2.1168      0.21  Q         |         |         |        V|
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   23+15       2.1182      0.21  Q          |          |          |         v|
   23+20       2.1196      0.21  Q          |          |          |         v|
   23+25       2.1210      0.21  Q          |          |          |         v|
   23+30       2.1224      0.21  Q          |          |          |         v|
   23+35       2.1239      0.21  Q          |          |          |         v|
   23+40       2.1253      0.21  Q          |          |          |         v|
   23+45       2.1267      0.21  Q          |          |          |         v|
   23+50       2.1281      0.21  Q          |          |          |         v|
   23+55       2.1296      0.21  Q          |          |          |         v|
   24+ 0       2.1310      0.21  Q          |          |          |         v|
   24+ 5       2.1318      0.12  Q          |          |          |         v|
   24+10       2.1320      0.03  Q          |          |          |         v|
   24+15       2.1321      0.01  Q          |          |          |         v|
   24+20       2.1321      0.00  Q          |          |          |         v|
-------------------------------------------------------------------------------
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       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/30/25 File: pro515.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      28.43(Ac.)  =      0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      28.43(Ac.)  =      0.044 Sq. Mi.
Length along longest watercourse =    1871.00(Ft.)
Length along longest watercourse measured to centroid =     935.00(Ft.)
Length along longest watercourse =      0.354 Mi.
Length along longest watercourse measured to centroid =      0.177 Mi.
Difference in elevation =      79.00(Ft.)
Slope along watercourse =    222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.045 Hr.
Lag time =     2.70 Min.
25% of lag time =     0.68 Min.
40% of lag time =     1.08 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       28.43           0.50                 14.22

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       28.43           1.30                 36.96

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.687(In)
Areal adjustment factor =   99.97 %
Adjusted average point rain =    0.687(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    28.430           69.00         0.500
 Total Area Entered =     28.43(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  49.8      0.574     0.500        0.316       1.000      0.316
                                                 Sum (F) =   0.316
Area averaged mean soil loss (F) (In/Hr) =  0.316
Minimum soil loss rate ((In/Hr)) =  0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time		Pattern	Storm Rain	Loss rate(In./Hr)		Effective
	(Hr.)	Percent	(In/Hr)	Max	Low	(In/Hr)
1	0.08	3.30	0.272	(0.316)	0.136	0.136
2	0.17	4.20	0.346	(0.316)	0.173	0.173
3	0.25	4.40	0.363	(0.316)	0.181	0.181
4	0.33	4.80	0.396	(0.316)	0.198	0.198
5	0.42	5.20	0.429	(0.316)	0.214	0.214
6	0.50	6.20	0.511	(0.316)	0.256	0.256
7	0.58	6.80	0.561	(0.316)	0.280	0.280
8	0.67	8.80	0.726	0.316	(0.363)	0.410
9	0.75	13.90	1.146	0.316	(0.573)	0.831
10	0.83	31.40	2.589	0.316	(1.295)	2.274
11	0.92	7.20	0.594	(0.316)	0.297	0.297
12	1.00	3.80	0.313	(0.316)	0.157	0.157
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.4

Flood volume = Effective rainfall 0.45(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 1.1(Ac.Ft)
Total soil loss = 0.24(In)
Total soil loss = 0.561(Ac.Ft)
Total rainfall = 0.69(In)
Flood volume = 46499.2 Cubic Feet
Total soil loss = 24420.7 Cubic Feet

Peak flow rate of this hydrograph = 38.649(CFS)

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	10.0	20.0	30.0	40.0
0+ 5	0.0109	1.59	VQ				
0+10	0.0368	3.75	V Q				
0+15	0.0691	4.69	V Q				
0+20	0.1052	5.24	V Q				
0+25	0.1449	5.77	Q				
0+30	0.1898	6.53	QV				
0+35	0.2408	7.41	Q V				
0+40	0.3054	9.37	Q V				
0+45	0.4159	16.05	VQ				
0+50	0.6821	38.65			V	Q	
0+55	0.9248	35.24				VQ	
1+ 0	1.0133	12.85	Q			V	
1+ 5	1.0523	5.67	Q				V
1+10	1.0648	1.81	Q				V
1+15	1.0670	0.31	Q				V
1+20	1.0675	0.07	Q				V

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: pro535.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 1871.00(Ft.)
Length along longest watercourse measured to centroid = 935.00(Ft.)
Length along longest watercourse = 0.354 Mi.
Length along longest watercourse measured to centroid = 0.177 Mi.
Difference in elevation = 79.00(Ft.)
Slope along watercourse = 222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.045 Hr.
Lag time = 2.70 Min.
25% of lag time = 0.68 Min.
40% of lag time = 1.08 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.80	22.74

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	2.00	56.86

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 1.081(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.081(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	69.00	0.500

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.169	(0.316)	0.084	0.084
2	0.17	1.30	0.169	(0.316)	0.084	0.084
3	0.25	1.10	0.143	(0.316)	0.071	0.071
4	0.33	1.50	0.195	(0.316)	0.097	0.097
5	0.42	1.50	0.195	(0.316)	0.097	0.097
6	0.50	1.80	0.233	(0.316)	0.117	0.117
7	0.58	1.50	0.195	(0.316)	0.097	0.097
8	0.67	1.80	0.233	(0.316)	0.117	0.117
9	0.75	1.80	0.233	(0.316)	0.117	0.117
10	0.83	1.50	0.195	(0.316)	0.097	0.097
11	0.92	1.60	0.208	(0.316)	0.104	0.104
12	1.00	1.80	0.233	(0.316)	0.117	0.117
13	1.08	2.20	0.285	(0.316)	0.143	0.143
14	1.17	2.20	0.285	(0.316)	0.143	0.143
15	1.25	2.20	0.285	(0.316)	0.143	0.143
16	1.33	2.00	0.259	(0.316)	0.130	0.130
17	1.42	2.60	0.337	(0.316)	0.169	0.169
18	1.50	2.70	0.350	(0.316)	0.175	0.175
19	1.58	2.40	0.311	(0.316)	0.156	0.156
20	1.67	2.70	0.350	(0.316)	0.175	0.175
21	1.75	3.30	0.428	(0.316)	0.214	0.214
22	1.83	3.10	0.402	(0.316)	0.201	0.201
23	1.92	2.90	0.376	(0.316)	0.188	0.188
24	2.00	3.00	0.389	(0.316)	0.195	0.195
25	2.08	3.10	0.402	(0.316)	0.201	0.201
26	2.17	4.20	0.545	(0.316)	0.272	0.272
27	2.25	5.00	0.649	0.316	(0.324)	0.333
28	2.33	3.50	0.454	(0.316)	0.227	0.227
29	2.42	6.80	0.882	0.316	(0.441)	0.566
30	2.50	7.30	0.947	0.316	(0.473)	0.631
31	2.58	8.20	1.064	0.316	(0.532)	0.748
32	2.67	5.90	0.765	0.316	(0.383)	0.450
33	2.75	2.00	0.259	(0.316)	0.130	0.130
34	2.83	1.80	0.233	(0.316)	0.117	0.117
35	2.92	1.80	0.233	(0.316)	0.117	0.117
36	3.00	0.60	0.078	(0.316)	0.039	0.039
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	7.1

Flood volume = Effective rainfall 0.59(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 1.4(Ac.Ft)
Total soil loss = 0.49(In)
Total soil loss = 1.167(Ac.Ft)
Total rainfall = 1.08(In)
Flood volume = 60720.3 Cubic Feet
Total soil loss = 50833.1 Cubic Feet

Peak flow rate of this hydrograph = 18.702(CFS)

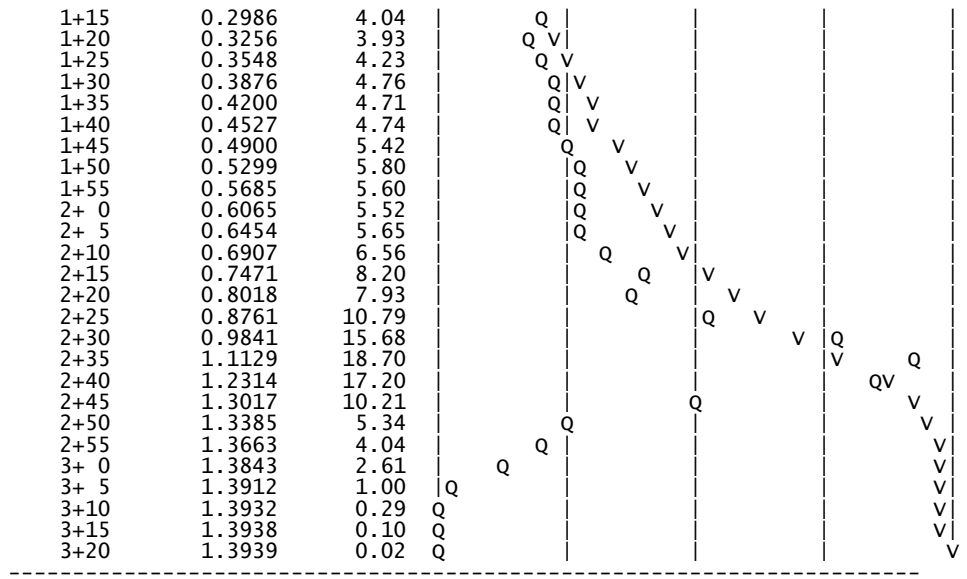
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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0068	0.98	VQ				
0+10	0.0209	2.06	V Q				
0+15	0.0356	2.13	V Q				
0+20	0.0519	2.36	V Q				
0+25	0.0705	2.70	V Q				
0+30	0.0910	2.98	V Q				
0+35	0.1119	3.02	V Q				
0+40	0.1330	3.07	V Q				
0+45	0.1556	3.28	V Q				
0+50	0.1770	3.10	VQ				
0+55	0.1972	2.94	Q				
1+ 0	0.2188	3.13	Q				
1+ 5	0.2435	3.59	VQ				
1+10	0.2707	3.96	Q				

1+15	0.2986	4.04	
1+20	0.3256	3.93	
1+25	0.3548	4.23	
1+30	0.3876	4.76	
1+35	0.4200	4.71	
1+40	0.4527	4.74	
1+45	0.4900	5.42	
1+50	0.5299	5.80	
1+55	0.5685	5.60	
2+ 0	0.6065	5.52	
2+ 5	0.6454	5.65	
2+10	0.6907	6.56	
2+15	0.7471	8.20	
2+20	0.8018	7.93	
2+25	0.8761	10.79	
2+30	0.9841	15.68	
2+35	1.1129	18.70	
2+40	1.2314	17.20	
2+45	1.3017	10.21	
2+50	1.3385	5.34	
2+55	1.3663	4.04	
3+ 0	1.3843	2.61	
3+ 5	1.3912	1.00	
3+10	1.3932	0.29	
3+15	1.3938	0.10	
3+20	1.3939	0.02	



U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: pro565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 1871.00(Ft.)
Length along longest watercourse measured to centroid = 935.00(Ft.)
Length along longest watercourse = 0.354 Mi.
Length along longest watercourse measured to centroid = 0.177 Mi.
Difference in elevation = 79.00(Ft.)
Slope along watercourse = 222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.045 Hr.
Lag time = 2.70 Min.
25% of lag time = 0.68 Min.
40% of lag time = 1.08 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.10	31.27

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	3.00	85.29

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.545(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.545(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	69.00	0.500

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.093	(0.316)	0.046	0.046
2	0.17	0.60	0.111	(0.316)	0.056	0.056
3	0.25	0.60	0.111	(0.316)	0.056	0.056
4	0.33	0.60	0.111	(0.316)	0.056	0.056
5	0.42	0.60	0.111	(0.316)	0.056	0.056
6	0.50	0.70	0.130	(0.316)	0.065	0.065
7	0.58	0.70	0.130	(0.316)	0.065	0.065
8	0.67	0.70	0.130	(0.316)	0.065	0.065
9	0.75	0.70	0.130	(0.316)	0.065	0.065
10	0.83	0.70	0.130	(0.316)	0.065	0.065
11	0.92	0.70	0.130	(0.316)	0.065	0.065
12	1.00	0.80	0.148	(0.316)	0.074	0.074
13	1.08	0.80	0.148	(0.316)	0.074	0.074
14	1.17	0.80	0.148	(0.316)	0.074	0.074
15	1.25	0.80	0.148	(0.316)	0.074	0.074
16	1.33	0.80	0.148	(0.316)	0.074	0.074
17	1.42	0.80	0.148	(0.316)	0.074	0.074
18	1.50	0.80	0.148	(0.316)	0.074	0.074
19	1.58	0.80	0.148	(0.316)	0.074	0.074
20	1.67	0.80	0.148	(0.316)	0.074	0.074
21	1.75	0.80	0.148	(0.316)	0.074	0.074
22	1.83	0.80	0.148	(0.316)	0.074	0.074
23	1.92	0.80	0.148	(0.316)	0.074	0.074
24	2.00	0.90	0.167	(0.316)	0.083	0.083
25	2.08	0.80	0.148	(0.316)	0.074	0.074
26	2.17	0.90	0.167	(0.316)	0.083	0.083
27	2.25	0.90	0.167	(0.316)	0.083	0.083
28	2.33	0.90	0.167	(0.316)	0.083	0.083
29	2.42	0.90	0.167	(0.316)	0.083	0.083
30	2.50	0.90	0.167	(0.316)	0.083	0.083
31	2.58	0.90	0.167	(0.316)	0.083	0.083
32	2.67	0.90	0.167	(0.316)	0.083	0.083
33	2.75	1.00	0.185	(0.316)	0.093	0.093
34	2.83	1.00	0.185	(0.316)	0.093	0.093
35	2.92	1.00	0.185	(0.316)	0.093	0.093
36	3.00	1.00	0.185	(0.316)	0.093	0.093
37	3.08	1.00	0.185	(0.316)	0.093	0.093
38	3.17	1.10	0.204	(0.316)	0.102	0.102
39	3.25	1.10	0.204	(0.316)	0.102	0.102
40	3.33	1.10	0.204	(0.316)	0.102	0.102
41	3.42	1.20	0.222	(0.316)	0.111	0.111
42	3.50	1.30	0.241	(0.316)	0.121	0.121
43	3.58	1.40	0.260	(0.316)	0.130	0.130
44	3.67	1.40	0.260	(0.316)	0.130	0.130
45	3.75	1.50	0.278	(0.316)	0.139	0.139
46	3.83	1.50	0.278	(0.316)	0.139	0.139
47	3.92	1.60	0.297	(0.316)	0.148	0.148
48	4.00	1.60	0.297	(0.316)	0.148	0.148
49	4.08	1.70	0.315	(0.316)	0.158	0.158
50	4.17	1.80	0.334	(0.316)	0.167	0.167
51	4.25	1.90	0.352	(0.316)	0.176	0.176
52	4.33	2.00	0.371	(0.316)	0.185	0.185
53	4.42	2.10	0.389	(0.316)	0.195	0.195
54	4.50	2.10	0.389	(0.316)	0.195	0.195
55	4.58	2.20	0.408	(0.316)	0.204	0.204
56	4.67	2.30	0.426	(0.316)	0.213	0.213
57	4.75	2.40	0.445	(0.316)	0.222	0.222
58	4.83	2.40	0.445	(0.316)	0.222	0.222
59	4.92	2.50	0.463	(0.316)	0.232	0.232
60	5.00	2.60	0.482	(0.316)	0.241	0.241
61	5.08	3.10	0.575	(0.316)	0.287	0.287
62	5.17	3.60	0.667	0.316	(0.334)	0.352
63	5.25	3.90	0.723	0.316	(0.362)	0.407
64	5.33	4.20	0.779	0.316	(0.389)	0.463
65	5.42	4.70	0.871	0.316	(0.436)	0.556
66	5.50	5.60	1.038	0.316	(0.519)	0.722
67	5.58	1.90	0.352	(0.316)	0.176	0.176
68	5.67	0.90	0.167	(0.316)	0.083	0.083
69	5.75	0.60	0.111	(0.316)	0.056	0.056
70	5.83	0.50	0.093	(0.316)	0.046	0.046
71	5.92	0.30	0.056	(0.316)	0.028	0.028

```
72   6.00     0.20      0.037       (  0.316)       0.019        0.019
            (Loss Rate Not Used)
   Sum =     100.0                                    Sum =     9.7
      Flood volume = Effective rainfall      0.81(In)
       times area      28.4(Ac.)/[(In)/(Ft.)] =       1.9(Ac.Ft)
      Total soil loss =      0.73(In)
      Total soil loss =     1.739(Ac.Ft)
      Total rainfall =      1.54(In)
      Flood volume =       83679.6 Cubic Feet
      Total soil loss =       75752.9 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     17.368(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                        6 - H O U R    S T O R M
                    R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                 Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
-------------------------------------------------------------------------
  0+ 5       0.0037      0.54  VQ        |         |         |         |
  0+10       0.0123      1.24  V Q       |         |         |         |
  0+15       0.0225      1.48  V Q       |         |         |         |
  0+20       0.0332      1.56  V  Q      |         |         |         |
  0+25       0.0442      1.59  V  Q      |         |         |         |
  0+30       0.0559      1.70  |V Q      |         |         |         |
  0+35       0.0684      1.82  |V Q      |         |         |         |
  0+40       0.0811      1.85  |V Q      |         |         |         |
  0+45       0.0939      1.86  |V Q      |         |         |         |
  0+50       0.1067      1.86  | VQ      |         |         |         |
  0+55       0.1195      1.86  | VQ      |         |         |         |
  1+ 0       0.1331      1.97  | VQ      |         |         |         |
  1+ 5       0.1475      2.09  |  VQ     |         |         |         |
  1+10       0.1620      2.11  |  VQ     |         |         |         |
  1+15       0.1766      2.12  |  VQ     |         |         |         |
  1+20       0.1912      2.13  |  VQ     |         |         |         |
  1+25       0.2059      2.13  |   Q     |         |         |         |
  1+30       0.2205      2.13  |   Q     |         |         |         |
  1+35       0.2352      2.13  |   Q     |         |         |         |
  1+40       0.2498      2.13  |   QV    |         |         |         |
  1+45       0.2644      2.13  |   QV    |         |         |         |
  1+50       0.2791      2.13  |   QV    |         |         |         |
  1+55       0.2937      2.13  |   Q V   |         |         |         |
  2+ 0       0.3091      2.23  |   Q V   |         |         |         |
  2+ 5       0.3246      2.24  |   Q V   |         |         |         |
  2+10       0.3401      2.26  |   Q  V  |         |         |         |
  2+15       0.3564      2.36  |   Q  V  |         |         |         |
  2+20       0.3728      2.38  |   Q  V  |         |         |         |
  2+25       0.3892      2.39  |   Q   V |         |         |         |
  2+30       0.4057      2.39  |   Q   V |         |         |         |
  2+35       0.4222      2.39  |   Q   V |         |         |         |
  2+40       0.4386      2.39  |   Q    V|         |         |         |
  2+45       0.4559      2.50  |   Q    V|         |         |         |
  2+50       0.4739      2.62  |    Q   V|         |         |         |
  2+55       0.4921      2.64  |    Q    V         |         |         |
  3+ 0       0.5104      2.65  |    Q    V         |         |         |
  3+ 5       0.5287      2.66  |    Q    |V        |         |         |
  3+10       0.5477      2.77  |    Q    |V        |         |         |
  3+15       0.5676      2.88  |    Q    |V        |         |         |
  3+20       0.5876      2.91  |    Q    | V       |         |         |
  3+25       0.6084      3.03  |     Q   | V       |         |         |
  3+30       0.6309      3.26  |     Q   |  V      |         |         |
  3+35       0.6550      3.51  |      Q  |  V      |         |         |
  3+40       0.6803      3.66  |      Q  |   V     |         |         |
  3+45       0.7065      3.81  |      Q  |   V     |         |         |
  3+50       0.7336      3.94  |      Q  |    V    |         |         |
  3+55       0.7617      4.08  |       Q |    V    |         |         |
  4+ 0       0.7907      4.21  |       Q |     V   |         |         |
  4+ 5       0.8206      4.35  |       Q |      V  |         |         |
  4+10       0.8522      4.58  |        Q|      V  |         |         |
  4+15       0.8855      4.84  |        Q|       V |         |         |
  4+20       0.9206      5.10  |         Q        V|         |         |
  4+25       0.9576      5.36  |         Q        V|         |         |
  4+30       0.9956      5.52  |         |Q        V         |         |
  4+35       1.0346      5.67  |         |Q        |V        |         |
  4+40       1.0753      5.91  |         |Q        | V       |         |
  4+45       1.1178      6.17  |         | Q       |  V      |         |
  4+50       1.1613      6.32  |         | Q       |   V     |         |
  4+55       1.2059      6.47  |         | Q       |    V    |         |
  5+ 0       1.2521      6.71  |         |  Q      |     V   |         |
  5+ 5       1.3030      7.40  |         |   Q     |      V  |         |
  5+10       1.3634      8.77  |         |      Q  |       V |         |
  5+15       1.4349     10.38  |         |         Q        V|         |
  5+20       1.5173     11.97  |         |         |  Q      |V        |
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    5+25       1.6137     14.00  |          |          |       Q  |  V       |
    5+30       1.7333     17.37  |          |          |          |   Q V    |
    5+35       1.8260     13.45  |          |          |     Q    |       V  |
    5+40       1.8672      5.99  |          |Q         |          |       V  |
    5+45       1.8895      3.24  |      Q   |          |          |        V |
    5+50       1.9033      2.01  |    Q     |          |          |        V |
    5+55       1.9119      1.24  |  Q       |          |          |        V |
    6+ 0       1.9174      0.80  |Q         |          |          |        V |
    6+ 5       1.9200      0.39  Q          |          |          |        V |
    6+10       1.9207      0.10  Q          |          |          |        V |
    6+15       1.9210      0.03  Q          |          |          |        V |
    6+20       1.9210      0.01  Q          |          |          |         V
-------------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: pro5245.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 1871.00(Ft.)
Length along longest watercourse measured to centroid = 935.00(Ft.)
Length along longest watercourse = 0.354 Mi.
Length along longest watercourse measured to centroid = 0.177 Mi.
Difference in elevation = 79.00(Ft.)
Slope along watercourse = 222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.045 Hr.
Lag time = 2.70 Min.
25% of lag time = 0.68 Min.
40% of lag time = 1.08 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.80	51.17

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	5.00	142.15

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 2.550(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 2.549(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	69.00	0.500

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.020	(0.560)	0.010	0.010
2	0.17	0.07	0.020	(0.557)	0.010	0.010
3	0.25	0.07	0.020	(0.555)	0.010	0.010
4	0.33	0.10	0.031	(0.553)	0.015	0.015
5	0.42	0.10	0.031	(0.551)	0.015	0.015
6	0.50	0.10	0.031	(0.549)	0.015	0.015
7	0.58	0.10	0.031	(0.547)	0.015	0.015
8	0.67	0.10	0.031	(0.545)	0.015	0.015
9	0.75	0.10	0.031	(0.542)	0.015	0.015
10	0.83	0.13	0.041	(0.540)	0.020	0.020
11	0.92	0.13	0.041	(0.538)	0.020	0.020
12	1.00	0.13	0.041	(0.536)	0.020	0.020
13	1.08	0.10	0.031	(0.534)	0.015	0.015
14	1.17	0.10	0.031	(0.532)	0.015	0.015
15	1.25	0.10	0.031	(0.530)	0.015	0.015
16	1.33	0.10	0.031	(0.528)	0.015	0.015
17	1.42	0.10	0.031	(0.525)	0.015	0.015
18	1.50	0.10	0.031	(0.523)	0.015	0.015
19	1.58	0.10	0.031	(0.521)	0.015	0.015
20	1.67	0.10	0.031	(0.519)	0.015	0.015
21	1.75	0.10	0.031	(0.517)	0.015	0.015
22	1.83	0.13	0.041	(0.515)	0.020	0.020
23	1.92	0.13	0.041	(0.513)	0.020	0.020
24	2.00	0.13	0.041	(0.511)	0.020	0.020
25	2.08	0.13	0.041	(0.509)	0.020	0.020
26	2.17	0.13	0.041	(0.507)	0.020	0.020
27	2.25	0.13	0.041	(0.505)	0.020	0.020
28	2.33	0.13	0.041	(0.503)	0.020	0.020
29	2.42	0.13	0.041	(0.501)	0.020	0.020
30	2.50	0.13	0.041	(0.499)	0.020	0.020
31	2.58	0.17	0.051	(0.497)	0.025	0.025
32	2.67	0.17	0.051	(0.494)	0.025	0.025
33	2.75	0.17	0.051	(0.492)	0.025	0.025
34	2.83	0.17	0.051	(0.490)	0.025	0.025
35	2.92	0.17	0.051	(0.488)	0.025	0.025
36	3.00	0.17	0.051	(0.486)	0.025	0.025
37	3.08	0.17	0.051	(0.484)	0.025	0.025
38	3.17	0.17	0.051	(0.482)	0.025	0.025
39	3.25	0.17	0.051	(0.480)	0.025	0.025
40	3.33	0.17	0.051	(0.478)	0.025	0.025
41	3.42	0.17	0.051	(0.476)	0.025	0.025
42	3.50	0.17	0.051	(0.474)	0.025	0.025
43	3.58	0.17	0.051	(0.472)	0.025	0.025
44	3.67	0.17	0.051	(0.470)	0.025	0.025
45	3.75	0.17	0.051	(0.468)	0.025	0.025
46	3.83	0.20	0.061	(0.466)	0.031	0.031
47	3.92	0.20	0.061	(0.464)	0.031	0.031
48	4.00	0.20	0.061	(0.463)	0.031	0.031
49	4.08	0.20	0.061	(0.461)	0.031	0.031
50	4.17	0.20	0.061	(0.459)	0.031	0.031
51	4.25	0.20	0.061	(0.457)	0.031	0.031
52	4.33	0.23	0.071	(0.455)	0.036	0.036
53	4.42	0.23	0.071	(0.453)	0.036	0.036
54	4.50	0.23	0.071	(0.451)	0.036	0.036
55	4.58	0.23	0.071	(0.449)	0.036	0.036
56	4.67	0.23	0.071	(0.447)	0.036	0.036
57	4.75	0.23	0.071	(0.445)	0.036	0.036
58	4.83	0.27	0.082	(0.443)	0.041	0.041
59	4.92	0.27	0.082	(0.441)	0.041	0.041
60	5.00	0.27	0.082	(0.439)	0.041	0.041
61	5.08	0.20	0.061	(0.437)	0.031	0.031
62	5.17	0.20	0.061	(0.435)	0.031	0.031
63	5.25	0.20	0.061	(0.434)	0.031	0.031
64	5.33	0.23	0.071	(0.432)	0.036	0.036
65	5.42	0.23	0.071	(0.430)	0.036	0.036
66	5.50	0.23	0.071	(0.428)	0.036	0.036
67	5.58	0.27	0.082	(0.426)	0.041	0.041
68	5.67	0.27	0.082	(0.424)	0.041	0.041
69	5.75	0.27	0.082	(0.422)	0.041	0.041
70	5.83	0.27	0.082	(0.420)	0.041	0.041
71	5.92	0.27	0.082	(0.419)	0.041	0.041

72	6.00	0.27	0.082	(0.417)	0.041	0.041
73	6.08	0.30	0.092	(0.415)	0.046	0.046
74	6.17	0.30	0.092	(0.413)	0.046	0.046
75	6.25	0.30	0.092	(0.411)	0.046	0.046
76	6.33	0.30	0.092	(0.409)	0.046	0.046
77	6.42	0.30	0.092	(0.407)	0.046	0.046
78	6.50	0.30	0.092	(0.406)	0.046	0.046
79	6.58	0.33	0.102	(0.404)	0.051	0.051
80	6.67	0.33	0.102	(0.402)	0.051	0.051
81	6.75	0.33	0.102	(0.400)	0.051	0.051
82	6.83	0.33	0.102	(0.398)	0.051	0.051
83	6.92	0.33	0.102	(0.397)	0.051	0.051
84	7.00	0.33	0.102	(0.395)	0.051	0.051
85	7.08	0.33	0.102	(0.393)	0.051	0.051
86	7.17	0.33	0.102	(0.391)	0.051	0.051
87	7.25	0.33	0.102	(0.389)	0.051	0.051
88	7.33	0.37	0.112	(0.388)	0.056	0.056
89	7.42	0.37	0.112	(0.386)	0.056	0.056
90	7.50	0.37	0.112	(0.384)	0.056	0.056
91	7.58	0.40	0.122	(0.382)	0.061	0.061
92	7.67	0.40	0.122	(0.381)	0.061	0.061
93	7.75	0.40	0.122	(0.379)	0.061	0.061
94	7.83	0.43	0.133	(0.377)	0.066	0.066
95	7.92	0.43	0.133	(0.375)	0.066	0.066
96	8.00	0.43	0.133	(0.374)	0.066	0.066
97	8.08	0.50	0.153	(0.372)	0.076	0.076
98	8.17	0.50	0.153	(0.370)	0.076	0.076
99	8.25	0.50	0.153	(0.368)	0.076	0.076
100	8.33	0.50	0.153	(0.367)	0.076	0.076
101	8.42	0.50	0.153	(0.365)	0.076	0.076
102	8.50	0.50	0.153	(0.363)	0.076	0.076
103	8.58	0.53	0.163	(0.362)	0.082	0.082
104	8.67	0.53	0.163	(0.360)	0.082	0.082
105	8.75	0.53	0.163	(0.358)	0.082	0.082
106	8.83	0.57	0.173	(0.356)	0.087	0.087
107	8.92	0.57	0.173	(0.355)	0.087	0.087
108	9.00	0.57	0.173	(0.353)	0.087	0.087
109	9.08	0.63	0.194	(0.351)	0.097	0.097
110	9.17	0.63	0.194	(0.350)	0.097	0.097
111	9.25	0.63	0.194	(0.348)	0.097	0.097
112	9.33	0.67	0.204	(0.346)	0.102	0.102
113	9.42	0.67	0.204	(0.345)	0.102	0.102
114	9.50	0.67	0.204	(0.343)	0.102	0.102
115	9.58	0.70	0.214	(0.341)	0.107	0.107
116	9.67	0.70	0.214	(0.340)	0.107	0.107
117	9.75	0.70	0.214	(0.338)	0.107	0.107
118	9.83	0.73	0.224	(0.337)	0.112	0.112
119	9.92	0.73	0.224	(0.335)	0.112	0.112
120	10.00	0.73	0.224	(0.333)	0.112	0.112
121	10.08	0.50	0.153	(0.332)	0.076	0.076
122	10.17	0.50	0.153	(0.330)	0.076	0.076
123	10.25	0.50	0.153	(0.329)	0.076	0.076
124	10.33	0.50	0.153	(0.327)	0.076	0.076
125	10.42	0.50	0.153	(0.325)	0.076	0.076
126	10.50	0.50	0.153	(0.324)	0.076	0.076
127	10.58	0.67	0.204	(0.322)	0.102	0.102
128	10.67	0.67	0.204	(0.321)	0.102	0.102
129	10.75	0.67	0.204	(0.319)	0.102	0.102
130	10.83	0.67	0.204	(0.317)	0.102	0.102
131	10.92	0.67	0.204	(0.316)	0.102	0.102
132	11.00	0.67	0.204	(0.314)	0.102	0.102
133	11.08	0.63	0.194	(0.313)	0.097	0.097
134	11.17	0.63	0.194	(0.311)	0.097	0.097
135	11.25	0.63	0.194	(0.310)	0.097	0.097
136	11.33	0.63	0.194	(0.308)	0.097	0.097
137	11.42	0.63	0.194	(0.307)	0.097	0.097
138	11.50	0.63	0.194	(0.305)	0.097	0.097
139	11.58	0.57	0.173	(0.304)	0.087	0.087
140	11.67	0.57	0.173	(0.302)	0.087	0.087
141	11.75	0.57	0.173	(0.301)	0.087	0.087
142	11.83	0.60	0.184	(0.299)	0.092	0.092
143	11.92	0.60	0.184	(0.298)	0.092	0.092
144	12.00	0.60	0.184	(0.296)	0.092	0.092
145	12.08	0.83	0.255	(0.295)	0.127	0.127
146	12.17	0.83	0.255	(0.293)	0.127	0.127
147	12.25	0.83	0.255	(0.292)	0.127	0.127
148	12.33	0.87	0.265	(0.290)	0.133	0.133
149	12.42	0.87	0.265	(0.289)	0.133	0.133
150	12.50	0.87	0.265	(0.287)	0.133	0.133
151	12.58	0.93	0.286	(0.286)	0.143	0.143
152	12.67	0.93	0.286	(0.284)	0.143	0.143
153	12.75	0.93	0.286	(0.283)	0.143	0.143
154	12.83	0.97	0.296	(0.282)	0.148	0.148
155	12.92	0.97	0.296	(0.280)	0.148	0.148
156	13.00	0.97	0.296	(0.279)	0.148	0.148
157	13.08	1.13	0.347	(0.277)	0.173	0.173

158	13.17	1.13	0.347	(0.276)	0.173	0.173
159	13.25	1.13	0.347	(0.275)	0.173	0.173
160	13.33	1.13	0.347	(0.273)	0.173	0.173
161	13.42	1.13	0.347	(0.272)	0.173	0.173
162	13.50	1.13	0.347	(0.270)	0.173	0.173
163	13.58	0.77	0.235	(0.269)	0.117	0.117
164	13.67	0.77	0.235	(0.268)	0.117	0.117
165	13.75	0.77	0.235	(0.266)	0.117	0.117
166	13.83	0.77	0.235	(0.265)	0.117	0.117
167	13.92	0.77	0.235	(0.264)	0.117	0.117
168	14.00	0.77	0.235	(0.262)	0.117	0.117
169	14.08	0.90	0.275	(0.261)	0.138	0.138
170	14.17	0.90	0.275	(0.260)	0.138	0.138
171	14.25	0.90	0.275	(0.258)	0.138	0.138
172	14.33	0.87	0.265	(0.257)	0.133	0.133
173	14.42	0.87	0.265	(0.256)	0.133	0.133
174	14.50	0.87	0.265	(0.254)	0.133	0.133
175	14.58	0.87	0.265	(0.253)	0.133	0.133
176	14.67	0.87	0.265	(0.252)	0.133	0.133
177	14.75	0.87	0.265	(0.250)	0.133	0.133
178	14.83	0.83	0.255	(0.249)	0.127	0.127
179	14.92	0.83	0.255	(0.248)	0.127	0.127
180	15.00	0.83	0.255	(0.247)	0.127	0.127
181	15.08	0.80	0.245	(0.245)	0.122	0.122
182	15.17	0.80	0.245	(0.244)	0.122	0.122
183	15.25	0.80	0.245	(0.243)	0.122	0.122
184	15.33	0.77	0.235	(0.242)	0.117	0.117
185	15.42	0.77	0.235	(0.240)	0.117	0.117
186	15.50	0.77	0.235	(0.239)	0.117	0.117
187	15.58	0.63	0.194	(0.238)	0.097	0.097
188	15.67	0.63	0.194	(0.237)	0.097	0.097
189	15.75	0.63	0.194	(0.235)	0.097	0.097
190	15.83	0.63	0.194	(0.234)	0.097	0.097
191	15.92	0.63	0.194	(0.233)	0.097	0.097
192	16.00	0.63	0.194	(0.232)	0.097	0.097
193	16.08	0.13	0.041	(0.231)	0.020	0.020
194	16.17	0.13	0.041	(0.229)	0.020	0.020
195	16.25	0.13	0.041	(0.228)	0.020	0.020
196	16.33	0.13	0.041	(0.227)	0.020	0.020
197	16.42	0.13	0.041	(0.226)	0.020	0.020
198	16.50	0.13	0.041	(0.225)	0.020	0.020
199	16.58	0.10	0.031	(0.224)	0.015	0.015
200	16.67	0.10	0.031	(0.223)	0.015	0.015
201	16.75	0.10	0.031	(0.221)	0.015	0.015
202	16.83	0.10	0.031	(0.220)	0.015	0.015
203	16.92	0.10	0.031	(0.219)	0.015	0.015
204	17.00	0.10	0.031	(0.218)	0.015	0.015
205	17.08	0.17	0.051	(0.217)	0.025	0.025
206	17.17	0.17	0.051	(0.216)	0.025	0.025
207	17.25	0.17	0.051	(0.215)	0.025	0.025
208	17.33	0.17	0.051	(0.214)	0.025	0.025
209	17.42	0.17	0.051	(0.213)	0.025	0.025
210	17.50	0.17	0.051	(0.212)	0.025	0.025
211	17.58	0.17	0.051	(0.211)	0.025	0.025
212	17.67	0.17	0.051	(0.209)	0.025	0.025
213	17.75	0.17	0.051	(0.208)	0.025	0.025
214	17.83	0.13	0.041	(0.207)	0.020	0.020
215	17.92	0.13	0.041	(0.206)	0.020	0.020
216	18.00	0.13	0.041	(0.205)	0.020	0.020
217	18.08	0.13	0.041	(0.204)	0.020	0.020
218	18.17	0.13	0.041	(0.203)	0.020	0.020
219	18.25	0.13	0.041	(0.202)	0.020	0.020
220	18.33	0.13	0.041	(0.201)	0.020	0.020
221	18.42	0.13	0.041	(0.200)	0.020	0.020
222	18.50	0.13	0.041	(0.199)	0.020	0.020
223	18.58	0.10	0.031	(0.198)	0.015	0.015
224	18.67	0.10	0.031	(0.197)	0.015	0.015
225	18.75	0.10	0.031	(0.197)	0.015	0.015
226	18.83	0.07	0.020	(0.196)	0.010	0.010
227	18.92	0.07	0.020	(0.195)	0.010	0.010
228	19.00	0.07	0.020	(0.194)	0.010	0.010
229	19.08	0.10	0.031	(0.193)	0.015	0.015
230	19.17	0.10	0.031	(0.192)	0.015	0.015
231	19.25	0.10	0.031	(0.191)	0.015	0.015
232	19.33	0.13	0.041	(0.190)	0.020	0.020
233	19.42	0.13	0.041	(0.189)	0.020	0.020
234	19.50	0.13	0.041	(0.188)	0.020	0.020
235	19.58	0.10	0.031	(0.187)	0.015	0.015
236	19.67	0.10	0.031	(0.187)	0.015	0.015
237	19.75	0.10	0.031	(0.186)	0.015	0.015
238	19.83	0.07	0.020	(0.185)	0.010	0.010
239	19.92	0.07	0.020	(0.184)	0.010	0.010
240	20.00	0.07	0.020	(0.183)	0.010	0.010
241	20.08	0.10	0.031	(0.182)	0.015	0.015
242	20.17	0.10	0.031	(0.182)	0.015	0.015
243	20.25	0.10	0.031	(0.181)	0.015	0.015

244	20.33	0.10	0.031	(0.180)	0.015	0.015
245	20.42	0.10	0.031	(0.179)	0.015	0.015
246	20.50	0.10	0.031	(0.179)	0.015	0.015
247	20.58	0.10	0.031	(0.178)	0.015	0.015
248	20.67	0.10	0.031	(0.177)	0.015	0.015
249	20.75	0.10	0.031	(0.176)	0.015	0.015
250	20.83	0.07	0.020	(0.176)	0.010	0.010
251	20.92	0.07	0.020	(0.175)	0.010	0.010
252	21.00	0.07	0.020	(0.174)	0.010	0.010
253	21.08	0.10	0.031	(0.174)	0.015	0.015
254	21.17	0.10	0.031	(0.173)	0.015	0.015
255	21.25	0.10	0.031	(0.172)	0.015	0.015
256	21.33	0.07	0.020	(0.172)	0.010	0.010
257	21.42	0.07	0.020	(0.171)	0.010	0.010
258	21.50	0.07	0.020	(0.170)	0.010	0.010
259	21.58	0.10	0.031	(0.170)	0.015	0.015
260	21.67	0.10	0.031	(0.169)	0.015	0.015
261	21.75	0.10	0.031	(0.168)	0.015	0.015
262	21.83	0.07	0.020	(0.168)	0.010	0.010
263	21.92	0.07	0.020	(0.167)	0.010	0.010
264	22.00	0.07	0.020	(0.167)	0.010	0.010
265	22.08	0.10	0.031	(0.166)	0.015	0.015
266	22.17	0.10	0.031	(0.166)	0.015	0.015
267	22.25	0.10	0.031	(0.165)	0.015	0.015
268	22.33	0.07	0.020	(0.165)	0.010	0.010
269	22.42	0.07	0.020	(0.164)	0.010	0.010
270	22.50	0.07	0.020	(0.164)	0.010	0.010
271	22.58	0.07	0.020	(0.163)	0.010	0.010
272	22.67	0.07	0.020	(0.163)	0.010	0.010
273	22.75	0.07	0.020	(0.162)	0.010	0.010
274	22.83	0.07	0.020	(0.162)	0.010	0.010
275	22.92	0.07	0.020	(0.161)	0.010	0.010
276	23.00	0.07	0.020	(0.161)	0.010	0.010
277	23.08	0.07	0.020	(0.161)	0.010	0.010
278	23.17	0.07	0.020	(0.160)	0.010	0.010
279	23.25	0.07	0.020	(0.160)	0.010	0.010
280	23.33	0.07	0.020	(0.160)	0.010	0.010
281	23.42	0.07	0.020	(0.159)	0.010	0.010
282	23.50	0.07	0.020	(0.159)	0.010	0.010
283	23.58	0.07	0.020	(0.159)	0.010	0.010
284	23.67	0.07	0.020	(0.158)	0.010	0.010
285	23.75	0.07	0.020	(0.158)	0.010	0.010
286	23.83	0.07	0.020	(0.158)	0.010	0.010
287	23.92	0.07	0.020	(0.158)	0.010	0.010
288	24.00	0.07	0.020	(0.158)	0.010	0.010

(Loss Rate Not Used)

Sum = 100.0 Sum = 15.3

Flood volume = Effective rainfall 1.27(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 3.0(Ac.Ft)
Total soil loss = 1.27(In)
Total soil loss = 3.020(Ac.Ft)
Total rainfall = 2.55(In)
Flood volume = 131549.0 Cubic Feet
Total soil loss = 131549.0 Cubic Feet

Peak flow rate of this hydrograph = 4.970(CFS)

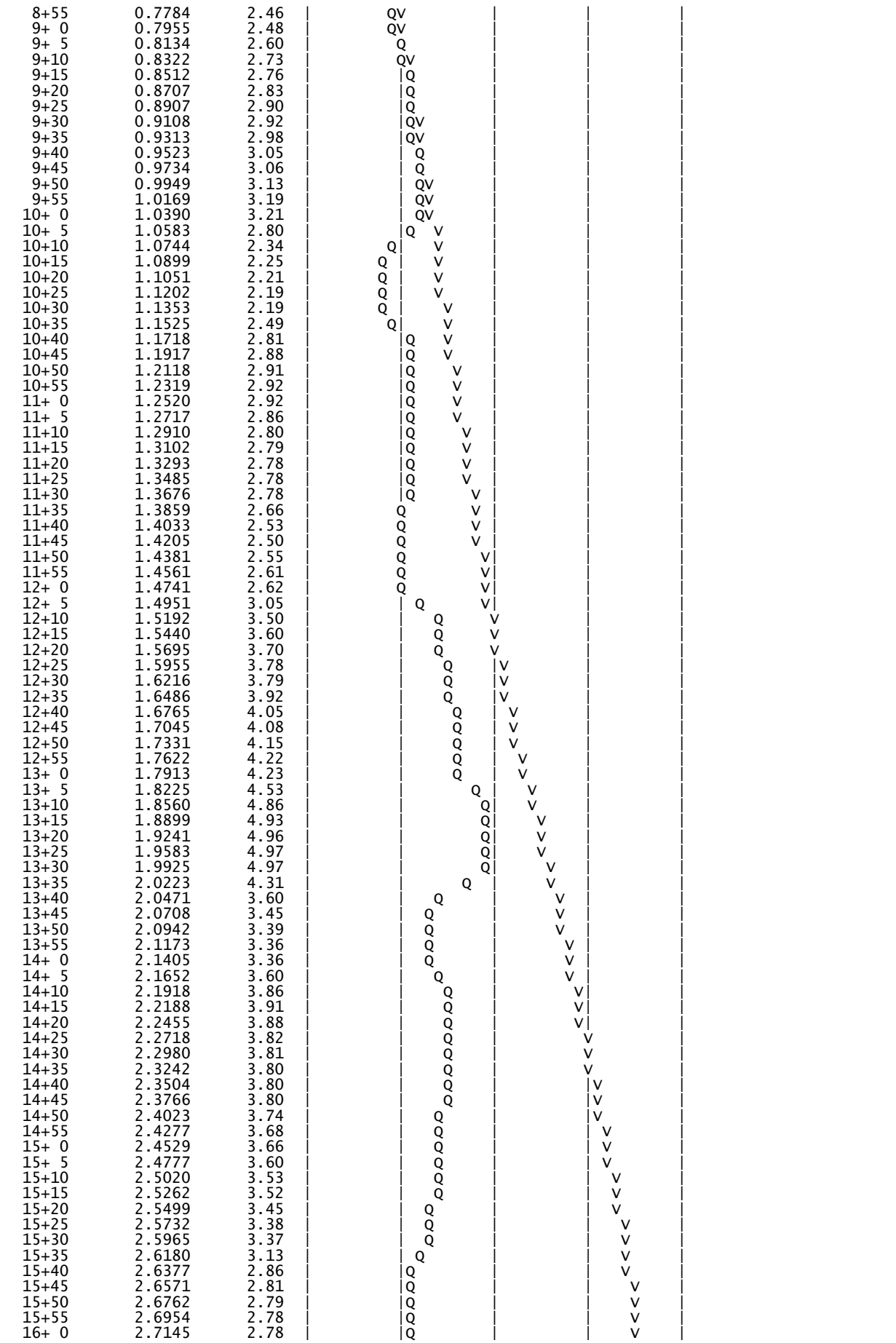
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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0008	0.12	Q				
0+10	0.0025	0.25	Q				
0+15	0.0044	0.28	VQ				
0+20	0.0068	0.35	VQ				
0+25	0.0097	0.42	VQ				
0+30	0.0127	0.43	VQ				
0+35	0.0157	0.44	VQ				
0+40	0.0187	0.44	VQ				
0+45	0.0217	0.44	VQ				
0+50	0.0251	0.50	VQ				
0+55	0.0290	0.56	V Q				
1+ 0	0.0330	0.58	V Q				
1+ 5	0.0366	0.52	V Q				
1+10	0.0398	0.46	VQ				
1+15	0.0428	0.45	VQ				
1+20	0.0459	0.44	VQ				
1+25	0.0489	0.44	VQ				
1+30	0.0519	0.44	VQ				
1+35	0.0549	0.44	VQ				
1+40	0.0579	0.44	VQ				

1+45	0.0610	0.44	VQ	|	|	|	|
1+50	0.0644	0.50	VQ	|	|	|	|
1+55	0.0683	0.56	V Q	|	|	|	|
2+ 0	0.0722	0.58	V Q	|	|	|	|
2+ 5	0.0763	0.58	|VQ	|	|	|	|
2+10	0.0803	0.58	|VQ	|	|	|	|
2+15	0.0843	0.58	|VQ	|	|	|	|
2+20	0.0883	0.58	|VQ	|	|	|	|
2+25	0.0924	0.58	|VQ	|	|	|	|
2+30	0.0964	0.58	|VQ	|	|	|	|
2+35	0.1008	0.64	|VQ	|	|	|	|
2+40	0.1057	0.71	|VQ	|	|	|	|
2+45	0.1107	0.72	|VQ	|	|	|	|
2+50	0.1157	0.73	|VQ	|	|	|	|
2+55	0.1207	0.73	|VQ	|	|	|	|
3+ 0	0.1258	0.73	|VQ	|	|	|	|
3+ 5	0.1308	0.73	|VQ	|	|	|	|
3+10	0.1358	0.73	|VQ	|	|	|	|
3+15	0.1409	0.73	|VQ	|	|	|	|
3+20	0.1459	0.73	|VQ	|	|	|	|
3+25	0.1509	0.73	|VQ	|	|	|	|
3+30	0.1560	0.73	| Q	|	|	|	|
3+35	0.1610	0.73	| Q	|	|	|	|
3+40	0.1660	0.73	| Q	|	|	|	|
3+45	0.1711	0.73	| Q	|	|	|	|
3+50	0.1765	0.79	| VQ	|	|	|	|
3+55	0.1824	0.86	| VQ	|	|	|	|
4+ 0	0.1884	0.87	| VQ	|	|	|	|
4+ 5	0.1944	0.87	| VQ	|	|	|	|
4+10	0.2005	0.88	| VQ	|	|	|	|
4+15	0.2065	0.88	| VQ	|	|	|	|
4+20	0.2129	0.94	| VQ	|	|	|	|
4+25	0.2198	1.00	| V Q	|	|	|	|
4+30	0.2268	1.02	| VQ	|	|	|	|
4+35	0.2339	1.02	| VQ	|	|	|	|
4+40	0.2409	1.02	| VQ	|	|	|	|
4+45	0.2480	1.02	| VQ	|	|	|	|
4+50	0.2554	1.08	| VQ	|	|	|	|
4+55	0.2633	1.15	| VQ	|	|	|	|
5+ 0	0.2713	1.16	| VQ	|	|	|	|
5+ 5	0.2785	1.05	| VQ	|	|	|	|
5+10	0.2849	0.92	| Q	|	|	|	|
5+15	0.2910	0.89	| Q	|	|	|	|
5+20	0.2975	0.94	| Q	|	|	|	|
5+25	0.3044	1.00	| Q	|	|	|	|
5+30	0.3114	1.02	| Q	|	|	|	|
5+35	0.3188	1.08	| Q	|	|	|	|
5+40	0.3267	1.15	| Q	|	|	|	|
5+45	0.3347	1.16	| Q	|	|	|	|
5+50	0.3428	1.17	| Q	|	|	|	|
5+55	0.3508	1.17	| Q	|	|	|	|
6+ 0	0.3589	1.17	| Q	|	|	|	|
6+ 5	0.3673	1.23	| Q	|	|	|	|
6+10	0.3762	1.29	| VQ	|	|	|	|
6+15	0.3853	1.31	| Q	|	|	|	|
6+20	0.3943	1.31	| Q	|	|	|	|
6+25	0.4034	1.32	| Q	|	|	|	|
6+30	0.4124	1.32	| Q	|	|	|	|
6+35	0.4219	1.38	| Q	|	|	|	|
6+40	0.4318	1.44	| Q	|	|	|	|
6+45	0.4418	1.45	| Q	|	|	|	|
6+50	0.4519	1.46	| Q	|	|	|	|
6+55	0.4619	1.46	| QV	|	|	|	|
7+ 0	0.4720	1.46	| QV	|	|	|	|
7+ 5	0.4821	1.46	| QV	|	|	|	|
7+10	0.4921	1.46	| QV	|	|	|	|
7+15	0.5022	1.46	| QV	|	|	|	|
7+20	0.5127	1.52	| Q	|	|	|	|
7+25	0.5236	1.59	| Q	|	|	|	|
7+30	0.5346	1.60	| QV	|	|	|	|
7+35	0.5461	1.66	| QV	|	|	|	|
7+40	0.5580	1.73	| QV	|	|	|	|
7+45	0.5700	1.75	| QV	|	|	|	|
7+50	0.5825	1.81	| Q	|	|	|	|
7+55	0.5954	1.88	| Q	|	|	|	|
8+ 0	0.6085	1.89	| QV	|	|	|	|
8+ 5	0.6224	2.02	| Q	|	|	|	|
8+10	0.6372	2.15	| Q	|	|	|	|
8+15	0.6522	2.18	| Q	|	|	|	|
8+20	0.6672	2.19	| Q	|	|	|	|
8+25	0.6823	2.19	| QV	|	|	|	|
8+30	0.6974	2.19	| QV	|	|	|	|
8+35	0.7129	2.25	| Q	|	|	|	|
8+40	0.7289	2.32	| Q	|	|	|	|
8+45	0.7449	2.33	| Q	|	|	|	|
8+50	0.7614	2.40	| QV	|	|	|	|



8+55	0.7784	2.46	
9+ 0	0.7955	2.48	
9+ 5	0.8134	2.60	
9+10	0.8322	2.73	
9+15	0.8512	2.76	
9+20	0.8707	2.83	
9+25	0.8907	2.90	
9+30	0.9108	2.92	
9+35	0.9313	2.98	
9+40	0.9523	3.05	
9+45	0.9734	3.06	
9+50	0.9949	3.13	
9+55	1.0169	3.19	
10+ 0	1.0390	3.21	
10+ 5	1.0583	2.80	
10+10	1.0744	2.34	
10+15	1.0899	2.25	
10+20	1.1051	2.21	
10+25	1.1202	2.19	
10+30	1.1353	2.19	
10+35	1.1525	2.49	
10+40	1.1718	2.81	
10+45	1.1917	2.88	
10+50	1.2118	2.91	
10+55	1.2319	2.92	
11+ 0	1.2520	2.92	
11+ 5	1.2717	2.86	
11+10	1.2910	2.80	
11+15	1.3102	2.79	
11+20	1.3293	2.78	
11+25	1.3485	2.78	
11+30	1.3676	2.78	
11+35	1.3859	2.66	
11+40	1.4033	2.53	
11+45	1.4205	2.50	
11+50	1.4381	2.55	
11+55	1.4561	2.61	
12+ 0	1.4741	2.62	
12+ 5	1.4951	3.05	
12+10	1.5192	3.50	
12+15	1.5440	3.60	
12+20	1.5695	3.70	
12+25	1.5955	3.78	
12+30	1.6216	3.79	
12+35	1.6486	3.92	
12+40	1.6765	4.05	
12+45	1.7045	4.08	
12+50	1.7331	4.15	
12+55	1.7622	4.22	
13+ 0	1.7913	4.23	
13+ 5	1.8225	4.53	
13+10	1.8560	4.86	
13+15	1.8899	4.93	
13+20	1.9241	4.96	
13+25	1.9583	4.97	
13+30	1.9925	4.97	
13+35	2.0223	4.31	
13+40	2.0471	3.60	
13+45	2.0708	3.45	
13+50	2.0942	3.39	
13+55	2.1173	3.36	
14+ 0	2.1405	3.36	
14+ 5	2.1652	3.60	
14+10	2.1918	3.86	
14+15	2.2188	3.91	
14+20	2.2455	3.88	
14+25	2.2718	3.82	
14+30	2.2980	3.81	
14+35	2.3242	3.80	
14+40	2.3504	3.80	
14+45	2.3766	3.80	
14+50	2.4023	3.74	
14+55	2.4277	3.68	
15+ 0	2.4529	3.66	
15+ 5	2.4777	3.60	
15+10	2.5020	3.53	
15+15	2.5262	3.52	
15+20	2.5499	3.45	
15+25	2.5732	3.38	
15+30	2.5965	3.37	
15+35	2.6180	3.13	
15+40	2.6377	2.86	
15+45	2.6571	2.81	
15+50	2.6762	2.79	
15+55	2.6954	2.78	
16+ 0	2.7145	2.78	

```
16+ 5       2.7275      1.88  |        Q  |           |           |      V    |
16+10       2.7337      0.91  |   Q       |           |           |      V    |
16+15       2.7386      0.70  |  Q        |           |           |      V    |
16+20       2.7429      0.62  |  Q        |           |           |      V    |
16+25       2.7469      0.58  |  Q        |           |           |      V    |
16+30       2.7509      0.58  |  Q        |           |           |      V    |
16+35       2.7545      0.53  |  Q        |           |           |      V    |
16+40       2.7577      0.46  |Q          |           |           |      V    |
16+45       2.7608      0.45  |Q          |           |           |      V    |
16+50       2.7638      0.44  |Q          |           |           |      V    |
16+55       2.7668      0.44  |Q          |           |           |      V    |
17+ 0       2.7699      0.44  |Q          |           |           |      V    |
17+ 5       2.7737      0.56  |  Q        |           |           |      V    |
17+10       2.7784      0.69  |  Q        |           |           |      V    |
17+15       2.7834      0.71  |  Q        |           |           |      V    |
17+20       2.7884      0.73  |  Q        |           |           |      V    |
17+25       2.7934      0.73  |  Q        |           |           |      V    |
17+30       2.7984      0.73  |  Q        |           |           |       V   |
17+35       2.8035      0.73  |  Q        |           |           |       V   |
17+40       2.8085      0.73  |  Q        |           |           |       V   |
17+45       2.8135      0.73  |  Q        |           |           |       V   |
17+50       2.8181      0.67  |  Q        |           |           |       V   |
17+55       2.8223      0.61  |  Q        |           |           |       V   |
18+ 0       2.8264      0.59  |  Q        |           |           |       V   |
18+ 5       2.8304      0.59  |  Q        |           |           |       V   |
18+10       2.8345      0.58  |  Q        |           |           |       V   |
18+15       2.8385      0.58  |  Q        |           |           |       V   |
18+20       2.8425      0.58  |  Q        |           |           |       V   |
18+25       2.8466      0.58  |  Q        |           |           |       V   |
18+30       2.8506      0.58  |  Q        |           |           |       V   |
18+35       2.8542      0.53  |  Q        |           |           |       V   |
18+40       2.8574      0.46  |Q          |           |           |       V   |
18+45       2.8604      0.45  |Q          |           |           |       V   |
18+50       2.8631      0.38  |Q          |           |           |       V   |
18+55       2.8652      0.31  |Q          |           |           |       V   |
19+ 0       2.8673      0.30  |Q          |           |           |       V   |
19+ 5       2.8697      0.35  |Q          |           |           |        V  |
19+10       2.8726      0.42  |Q          |           |           |        V  |
19+15       2.8756      0.43  |Q          |           |           |        V  |
19+20       2.8790      0.50  |Q          |           |           |        V  |
19+25       2.8829      0.56  |  Q        |           |           |        V  |
19+30       2.8868      0.58  |  Q        |           |           |        V  |
19+35       2.8904      0.52  |  Q        |           |           |        V  |
19+40       2.8936      0.46  |Q          |           |           |        V  |
19+45       2.8967      0.45  |Q          |           |           |        V  |
19+50       2.8993      0.38  |Q          |           |           |        V  |
19+55       2.9015      0.31  |Q          |           |           |        V  |
20+ 0       2.9035      0.30  |Q          |           |           |        V  |
20+ 5       2.9060      0.35  |Q          |           |           |        V  |
20+10       2.9088      0.42  |Q          |           |           |        V  |
20+15       2.9118      0.43  |Q          |           |           |        V  |
20+20       2.9148      0.44  |Q          |           |           |        V  |
20+25       2.9178      0.44  |Q          |           |           |        V  |
20+30       2.9209      0.44  |Q          |           |           |        V  |
20+35       2.9239      0.44  |Q          |           |           |        V  |
20+40       2.9269      0.44  |Q          |           |           |        V  |
20+45       2.9299      0.44  |Q          |           |           |        V  |
20+50       2.9325      0.38  |Q          |           |           |        V  |
20+55       2.9347      0.31  |Q          |           |           |        V  |
21+ 0       2.9368      0.30  |Q          |           |           |        V  |
21+ 5       2.9392      0.35  |Q          |           |           |        V  |
21+10       2.9421      0.42  |Q          |           |           |        V  |
21+15       2.9450      0.43  |Q          |           |           |         V |
21+20       2.9476      0.38  |Q          |           |           |         V |
21+25       2.9498      0.31  |Q          |           |           |         V |
21+30       2.9519      0.30  |Q          |           |           |         V |
21+35       2.9543      0.35  |Q          |           |           |         V |
21+40       2.9572      0.42  |Q          |           |           |         V |
21+45       2.9601      0.43  |Q          |           |           |         V |
21+50       2.9627      0.38  |Q          |           |           |         V |
21+55       2.9649      0.31  |Q          |           |           |         V |
22+ 0       2.9670      0.30  |Q          |           |           |         V |
22+ 5       2.9694      0.35  |Q          |           |           |         V |
22+10       2.9723      0.42  |Q          |           |           |         V |
22+15       2.9752      0.43  |Q          |           |           |         V |
22+20       2.9778      0.38  |Q          |           |           |         V |
22+25       2.9800      0.31  |Q          |           |           |         V |
22+30       2.9821      0.30  |Q          |           |           |         V |
22+35       2.9841      0.29  |Q          |           |           |         V |
22+40       2.9861      0.29  |Q          |           |           |         V |
22+45       2.9881      0.29  |Q          |           |           |         V |
22+50       2.9901      0.29  |Q          |           |           |         V |
22+55       2.9921      0.29  |Q          |           |           |         V |
23+ 0       2.9942      0.29  |Q          |           |           |         V |
23+ 5       2.9962      0.29  |Q          |           |           |         V |
23+10       2.9982      0.29  |Q          |           |           |         V |
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   23+15       3.0002      0.29  |Q        |         |         |        v|
   23+20       3.0022      0.29  |Q        |         |         |        v|
   23+25       3.0042      0.29  |Q        |         |         |        v|
   23+30       3.0062      0.29  |Q        |         |         |        v|
   23+35       3.0082      0.29  |Q        |         |         |        v|
   23+40       3.0103      0.29  |Q        |         |         |        v|
   23+45       3.0123      0.29  |Q        |         |         |        v|
   23+50       3.0143      0.29  |Q        |         |         |        v|
   23+55       3.0163      0.29  |Q        |         |         |        v|
   24+ 0       3.0183      0.29  |Q        |         |         |        v|
   24+ 5       3.0195      0.17  Q         |         |         |        v|
   24+10       3.0198      0.04  Q         |         |         |        v|
   24+15       3.0199      0.02  Q         |         |         |        v|
   24+20       3.0199      0.00  Q         |         |         |        v|
-------------------------------------------------------------------------
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       U n i t   H y d r o g r a p h   A n a l y s i s

       Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2008, Version 8.1
              Study date  04/30/25 File: pro10110.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      28.43(Ac.)  =      0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      28.43(Ac.)  =      0.044 Sq. Mi.
Length along longest watercourse =    1871.00(Ft.)
Length along longest watercourse measured to centroid =     935.00(Ft.)
Length along longest watercourse =      0.354 Mi.
Length along longest watercourse measured to centroid =      0.177 Mi.
Difference in elevation =      79.00(Ft.)
Slope along watercourse =    222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.045 Hr.
Lag time =     2.70 Min.
25% of lag time =     0.68 Min.
40% of lag time =     1.08 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       28.43           0.50                 14.22

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       28.43           1.30                 36.96

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.829(In)
Areal adjustment factor =   99.97 %
Adjusted average point rain =    0.829(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    28.430           69.00         0.500
 Total Area Entered =     28.43(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  69.0      0.373     0.500        0.205       1.000      0.205
                                                 Sum (F) =   0.205
Area averaged mean soil loss (F) (In/Hr) =  0.205
Minimum soil loss rate ((In/Hr)) =  0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time		Pattern	Storm Rain	Loss rate(In./Hr)			Effective
	(Hr.)	Percent	(In/Hr)	Max		Low	(In/Hr)
1	0.08	3.30	0.328	(0.205)		0.164	0.164
2	0.17	4.20	0.418	0.205	(	0.209)	0.213
3	0.25	4.40	0.438	0.205	(	0.219)	0.233
4	0.33	4.80	0.477	0.205	(	0.239)	0.272
5	0.42	5.20	0.517	0.205	(	0.259)	0.312
6	0.50	6.20	0.617	0.205	(	0.308)	0.412
7	0.58	6.80	0.676	0.205	(	0.338)	0.471
8	0.67	8.80	0.875	0.205	(	0.438)	0.670
9	0.75	13.90	1.383	0.205	(	0.691)	1.178
10	0.83	31.40	3.123	0.205	(	1.562)	2.918
11	0.92	7.20	0.716	0.205	(	0.358)	0.511
12	1.00	3.80	0.378	(0.205)		0.189	0.189
		(Loss Rate Not Used)					
Sum =		100.0				Sum =	7.5

Flood volume = Effective rainfall 0.63(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 1.5(Ac.Ft)
Total soil loss = 0.20(In)
Total soil loss = 0.475(Ac.Ft)
Total rainfall = 0.83(In)
Flood volume = 64874.1 Cubic Feet
Total soil loss = 20670.4 Cubic Feet

Peak flow rate of this hydrograph = 51.576(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	15.0	30.0	45.0	60.0
0+ 5	0.0132	1.92	VQ				
0+10	0.0447	4.57	V Q				
0+15	0.0851	5.87	VQ				
0+20	0.1326	6.90	VQ				
0+25	0.1880	8.05	Q				
0+30	0.2560	9.87	Q				
0+35	0.3386	11.99	Q V				
0+40	0.4447	15.41	QV				
0+45	0.6110	24.15	Q				
0+50	0.9662	51.58			V	Q	
0+55	1.2917	47.26				Q V	
1+ 0	1.4170	18.20	Q			V	
1+ 5	1.4688	7.52	Q			V	
1+10	1.4856	2.44	Q			V	
1+15	1.4887	0.45	Q			V	
1+20	1.4893	0.09	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: pro10310.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 1871.00(Ft.)
Length along longest watercourse measured to centroid = 935.00(Ft.)
Length along longest watercourse = 0.354 Mi.
Length along longest watercourse measured to centroid = 0.177 Mi.
Difference in elevation = 79.00(Ft.)
Slope along watercourse = 222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.045 Hr.
Lag time = 2.70 Min.
25% of lag time = 0.68 Min.
40% of lag time = 1.08 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.80	22.74

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	2.00	56.86

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 1.294(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.294(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	69.00	0.500

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.202	(0.205)	0.101	0.101
2	0.17	1.30	0.202	(0.205)	0.101	0.101
3	0.25	1.10	0.171	(0.205)	0.085	0.085
4	0.33	1.50	0.233	(0.205)	0.116	0.116
5	0.42	1.50	0.233	(0.205)	0.116	0.116
6	0.50	1.80	0.279	(0.205)	0.140	0.140
7	0.58	1.50	0.233	(0.205)	0.116	0.116
8	0.67	1.80	0.279	(0.205)	0.140	0.140
9	0.75	1.80	0.279	(0.205)	0.140	0.140
10	0.83	1.50	0.233	(0.205)	0.116	0.116
11	0.92	1.60	0.248	(0.205)	0.124	0.124
12	1.00	1.80	0.279	(0.205)	0.140	0.140
13	1.08	2.20	0.341	(0.205)	0.171	0.171
14	1.17	2.20	0.341	(0.205)	0.171	0.171
15	1.25	2.20	0.341	(0.205)	0.171	0.171
16	1.33	2.00	0.310	(0.205)	0.155	0.155
17	1.42	2.60	0.404	(0.205)	0.202	0.202
18	1.50	2.70	0.419	0.205	(0.210)	0.214
19	1.58	2.40	0.373	(0.205)	0.186	0.186
20	1.67	2.70	0.419	0.205	(0.210)	0.214
21	1.75	3.30	0.512	0.205	(0.256)	0.307
22	1.83	3.10	0.481	0.205	(0.241)	0.276
23	1.92	2.90	0.450	0.205	(0.225)	0.245
24	2.00	3.00	0.466	0.205	(0.233)	0.261
25	2.08	3.10	0.481	0.205	(0.241)	0.276
26	2.17	4.20	0.652	0.205	(0.326)	0.447
27	2.25	5.00	0.776	0.205	(0.388)	0.571
28	2.33	3.50	0.543	0.205	(0.272)	0.338
29	2.42	6.80	1.056	0.205	(0.528)	0.850
30	2.50	7.30	1.133	0.205	(0.567)	0.928
31	2.58	8.20	1.273	0.205	(0.636)	1.068
32	2.67	5.90	0.916	0.205	(0.458)	0.711
33	2.75	2.00	0.310	(0.205)	0.155	0.155
34	2.83	1.80	0.279	(0.205)	0.140	0.140
35	2.92	1.80	0.279	(0.205)	0.140	0.140
36	3.00	0.60	0.093	(0.205)	0.047	0.047
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	9.7

Flood volume = Effective rainfall 0.81(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 1.9(Ac.Ft)
Total soil loss = 0.49(In)
Total soil loss = 1.154(Ac.Ft)
Total rainfall = 1.29(In)
Flood volume = 83242.3 Cubic Feet
Total soil loss = 50251.0 Cubic Feet

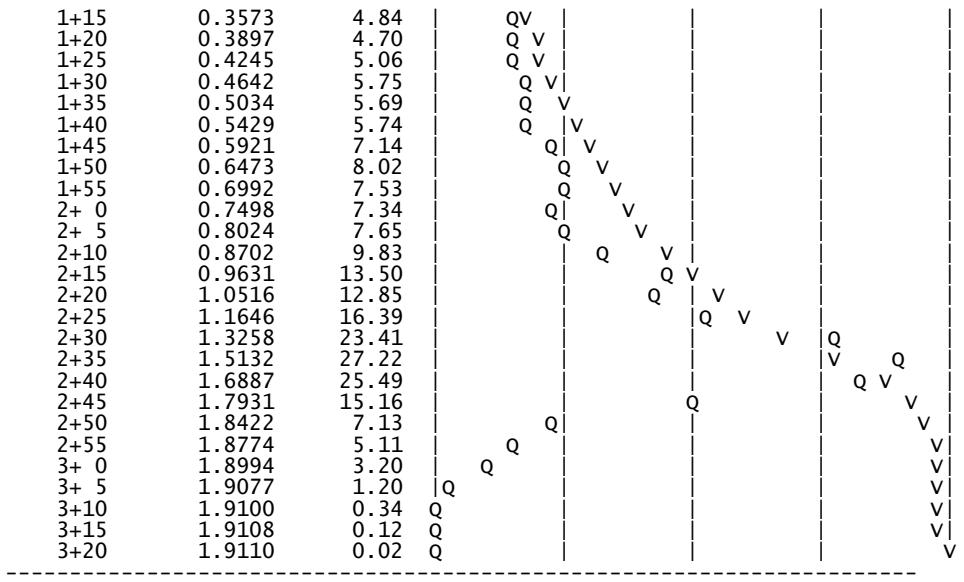
Peak flow rate of this hydrograph = 27.216(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0081	1.18	VQ				
0+10	0.0251	2.46	V Q				
0+15	0.0427	2.55	V Q				
0+20	0.0621	2.83	V Q				
0+25	0.0844	3.23	V Q				
0+30	0.1090	3.57	V Q				
0+35	0.1339	3.62	V Q				
0+40	0.1592	3.67	VQ				
0+45	0.1862	3.93	V Q				
0+50	0.2118	3.71	Q				
0+55	0.2360	3.52	Q				
1+ 0	0.2618	3.74	QV				
1+ 5	0.2914	4.30	QV				
1+10	0.3240	4.73	Q				



1+15	0.3573	4.84	
1+20	0.3897	4.70	
1+25	0.4245	5.06	
1+30	0.4642	5.75	
1+35	0.5034	5.69	
1+40	0.5429	5.74	
1+45	0.5921	7.14	
1+50	0.6473	8.02	
1+55	0.6992	7.53	
2+ 0	0.7498	7.34	
2+ 5	0.8024	7.65	
2+10	0.8702	9.83	
2+15	0.9631	13.50	
2+20	1.0516	12.85	
2+25	1.1646	16.39	
2+30	1.3258	23.41	
2+35	1.5132	27.22	
2+40	1.6887	25.49	
2+45	1.7931	15.16	
2+50	1.8422	7.13	
2+55	1.8774	5.11	
3+ 0	1.8994	3.20	
3+ 5	1.9077	1.20	
3+10	1.9100	0.34	
3+15	1.9108	0.12	
3+20	1.9110	0.02	

```
       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/30/25 File: pro10610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      28.43(Ac.)  =      0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      28.43(Ac.)  =      0.044 Sq. Mi.
Length along longest watercourse =    1871.00(Ft.)
Length along longest watercourse measured to centroid =     935.00(Ft.)
Length along longest watercourse =      0.354 Mi.
Length along longest watercourse measured to centroid =      0.177 Mi.
Difference in elevation =      79.00(Ft.)
Slope along watercourse =    222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.045 Hr.
Lag time =     2.70 Min.
25% of lag time =     0.68 Min.
40% of lag time =     1.08 Min.
Unit time =     5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       28.43           1.10                 31.27

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       28.43           3.00                 85.29

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    1.100(In)
Area Averaged 100-Year Rainfall =    3.000(In)

Point rain (area averaged) =    1.882(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    1.881(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    28.430           69.00         0.500
 Total Area Entered =     28.43(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  69.0      0.373     0.500        0.205       1.000      0.205
                                                 Sum (F) =   0.205
Area averaged mean soil loss (F) (In/Hr) =  0.205
Minimum soil loss rate ((In/Hr)) =  0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.113	(0.205)	0.056	0.056
2	0.17	0.60	0.135	(0.205)	0.068	0.068
3	0.25	0.60	0.135	(0.205)	0.068	0.068
4	0.33	0.60	0.135	(0.205)	0.068	0.068
5	0.42	0.60	0.135	(0.205)	0.068	0.068
6	0.50	0.70	0.158	(0.205)	0.079	0.079
7	0.58	0.70	0.158	(0.205)	0.079	0.079
8	0.67	0.70	0.158	(0.205)	0.079	0.079
9	0.75	0.70	0.158	(0.205)	0.079	0.079
10	0.83	0.70	0.158	(0.205)	0.079	0.079
11	0.92	0.70	0.158	(0.205)	0.079	0.079
12	1.00	0.80	0.181	(0.205)	0.090	0.090
13	1.08	0.80	0.181	(0.205)	0.090	0.090
14	1.17	0.80	0.181	(0.205)	0.090	0.090
15	1.25	0.80	0.181	(0.205)	0.090	0.090
16	1.33	0.80	0.181	(0.205)	0.090	0.090
17	1.42	0.80	0.181	(0.205)	0.090	0.090
18	1.50	0.80	0.181	(0.205)	0.090	0.090
19	1.58	0.80	0.181	(0.205)	0.090	0.090
20	1.67	0.80	0.181	(0.205)	0.090	0.090
21	1.75	0.80	0.181	(0.205)	0.090	0.090
22	1.83	0.80	0.181	(0.205)	0.090	0.090
23	1.92	0.80	0.181	(0.205)	0.090	0.090
24	2.00	0.90	0.203	(0.205)	0.102	0.102
25	2.08	0.80	0.181	(0.205)	0.090	0.090
26	2.17	0.90	0.203	(0.205)	0.102	0.102
27	2.25	0.90	0.203	(0.205)	0.102	0.102
28	2.33	0.90	0.203	(0.205)	0.102	0.102
29	2.42	0.90	0.203	(0.205)	0.102	0.102
30	2.50	0.90	0.203	(0.205)	0.102	0.102
31	2.58	0.90	0.203	(0.205)	0.102	0.102
32	2.67	0.90	0.203	(0.205)	0.102	0.102
33	2.75	1.00	0.226	(0.205)	0.113	0.113
34	2.83	1.00	0.226	(0.205)	0.113	0.113
35	2.92	1.00	0.226	(0.205)	0.113	0.113
36	3.00	1.00	0.226	(0.205)	0.113	0.113
37	3.08	1.00	0.226	(0.205)	0.113	0.113
38	3.17	1.10	0.248	(0.205)	0.124	0.124
39	3.25	1.10	0.248	(0.205)	0.124	0.124
40	3.33	1.10	0.248	(0.205)	0.124	0.124
41	3.42	1.20	0.271	(0.205)	0.135	0.135
42	3.50	1.30	0.294	(0.205)	0.147	0.147
43	3.58	1.40	0.316	(0.205)	0.158	0.158
44	3.67	1.40	0.316	(0.205)	0.158	0.158
45	3.75	1.50	0.339	(0.205)	0.169	0.169
46	3.83	1.50	0.339	(0.205)	0.169	0.169
47	3.92	1.60	0.361	(0.205)	0.181	0.181
48	4.00	1.60	0.361	(0.205)	0.181	0.181
49	4.08	1.70	0.384	(0.205)	0.192	0.192
50	4.17	1.80	0.406	(0.205)	0.203	0.203
51	4.25	1.90	0.429	0.205	(0.214)	0.224
52	4.33	2.00	0.452	0.205	(0.226)	0.247
53	4.42	2.10	0.474	0.205	(0.237)	0.269
54	4.50	2.10	0.474	0.205	(0.237)	0.269
55	4.58	2.20	0.497	0.205	(0.248)	0.292
56	4.67	2.30	0.519	0.205	(0.260)	0.314
57	4.75	2.40	0.542	0.205	(0.271)	0.337
58	4.83	2.40	0.542	0.205	(0.271)	0.337
59	4.92	2.50	0.564	0.205	(0.282)	0.359
60	5.00	2.60	0.587	0.205	(0.294)	0.382
61	5.08	3.10	0.700	0.205	(0.350)	0.495
62	5.17	3.60	0.813	0.205	(0.406)	0.608
63	5.25	3.90	0.881	0.205	(0.440)	0.675
64	5.33	4.20	0.948	0.205	(0.474)	0.743
65	5.42	4.70	1.061	0.205	(0.531)	0.856
66	5.50	5.60	1.264	0.205	(0.632)	1.059
67	5.58	1.90	0.429	0.205	(0.214)	0.224
68	5.67	0.90	0.203	(0.205)	0.102	0.102
69	5.75	0.60	0.135	(0.205)	0.068	0.068
70	5.83	0.50	0.113	(0.205)	0.056	0.056
71	5.92	0.30	0.068	(0.205)	0.034	0.034

```
72   6.00     0.20      0.045       (  0.205)       0.023        0.023
            (Loss Rate Not Used)
   Sum =     100.0                                    Sum =    13.4
      Flood volume = Effective rainfall      1.12(In)
       times area      28.4(Ac.)/[(In)/(Ft.)] =       2.6(Ac.Ft)
      Total soil loss =      0.77(In)
      Total soil loss =     1.814(Ac.Ft)
      Total rainfall =      1.88(In)
      Flood volume =      115166.2 Cubic Feet
      Total soil loss =       79005.4 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     26.296(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        7.5       15.0       22.5       30.0
-------------------------------------------------------------------------------
  0+ 5       0.0045      0.66  Q          |          |          |          |
  0+10       0.0149      1.51  V Q        |          |          |          |
  0+15       0.0274      1.81  V Q        |          |          |          |
  0+20       0.0404      1.90  V Q        |          |          |          |
  0+25       0.0538      1.94  V Q        |          |          |          |
  0+30       0.0681      2.07  |VQ        |          |          |          |
  0+35       0.0833      2.22  |VQ        |          |          |          |
  0+40       0.0988      2.25  |VQ        |          |          |          |
  0+45       0.1144      2.26  |V Q       |          |          |          |
  0+50       0.1300      2.27  |V Q       |          |          |          |
  0+55       0.1456      2.27  | VQ       |          |          |          |
  1+ 0       0.1621      2.40  | VQ       |          |          |          |
  1+ 5       0.1796      2.54  | VQ       |          |          |          |
  1+10       0.1973      2.57  | VQ       |          |          |          |
  1+15       0.2151      2.58  |  Q       |          |          |          |
  1+20       0.2329      2.59  |  Q       |          |          |          |
  1+25       0.2507      2.59  |  Q       |          |          |          |
  1+30       0.2686      2.59  |  QV      |          |          |          |
  1+35       0.2864      2.59  |  QV      |          |          |          |
  1+40       0.3042      2.59  |  QV      |          |          |          |
  1+45       0.3221      2.59  |  QV      |          |          |          |
  1+50       0.3399      2.59  |  Q V     |          |          |          |
  1+55       0.3577      2.59  |  Q V     |          |          |          |
  2+ 0       0.3765      2.72  |  Q V     |          |          |          |
  2+ 5       0.3953      2.73  |  Q V     |          |          |          |
  2+10       0.4142      2.75  |  Q  V    |          |          |          |
  2+15       0.4340      2.88  |  Q  V    |          |          |          |
  2+20       0.4540      2.90  |  Q  V    |          |          |          |
  2+25       0.4740      2.91  |  Q   V   |          |          |          |
  2+30       0.4941      2.91  |  Q   V   |          |          |          |
  2+35       0.5142      2.91  |  Q   V   |          |          |          |
  2+40       0.5342      2.91  |  Q    V  |          |          |          |
  2+45       0.5552      3.04  |   Q   V  |          |          |          |
  2+50       0.5771      3.19  |   Q   V  |          |          |          |
  2+55       0.5993      3.22  |   Q    V |          |          |          |
  3+ 0       0.6216      3.23  |   Q    V |          |          |          |
  3+ 5       0.6438      3.24  |   Q    V |          |          |          |
  3+10       0.6670      3.37  |   Q     V          |          |          |
  3+15       0.6912      3.51  |   Q     V          |          |          |
  3+20       0.7156      3.54  |   Q     V          |          |          |
  3+25       0.7410      3.69  |   Q     |V         |          |          |
  3+30       0.7683      3.97  |    Q    |V         |          |          |
  3+35       0.7978      4.27  |    Q    | V        |          |          |
  3+40       0.8285      4.46  |    Q    | V        |          |          |
  3+45       0.8604      4.64  |     Q   |  V       |          |          |
  3+50       0.8935      4.80  |     Q   |  V       |          |          |
  3+55       0.9277      4.97  |     Q   |   V      |          |          |
  4+ 0       0.9630      5.12  |     Q   |   V      |          |          |
  4+ 5       0.9994      5.29  |      Q  |    V     |          |          |
  4+10       1.0379      5.58  |      Q  |    V     |          |          |
  4+15       1.0792      6.00  |       Q |     V    |          |          |
  4+20       1.1245      6.57  |       Q |      V   |          |          |
  4+25       1.1740      7.20  |        Q|      V   |          |          |
  4+30       1.2262      7.57  |         Q       V  |          |          |
  4+35       1.2808      7.93  |         Q        V|          |          |
  4+40       1.3395      8.52  |         |Q        V          |          |
  4+45       1.4024      9.14  |         | Q       |V         |          |
  4+50       1.4680      9.51  |         | Q       | V        |          |
  4+55       1.5360      9.87  |         |  Q      |  V       |          |
  5+ 0       1.6080     10.46  |         |  Q      |   V      |          |
  5+ 5       1.6916     12.14  |         |    Q    |    V     |          |
  5+10       1.7947     14.98  |         |       Q |      V   |          |
  5+15       1.9156     17.55  |         |         |  Q    V  |          |
  5+20       2.0508     19.64  |         |         |     Q   |V         |
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    5+25       2.2035     22.18  |          |          |         Q|  V       |
    5+30       2.3846     26.30  |          |          |          |    QV    |
    5+35       2.5192     19.54  |          |          |     Q    |       V  |
    5+40       2.5756      8.18  |          Q          |          |       V  |
    5+45       2.6048      4.25  |     Q    |          |          |        V |
    5+50       2.6223      2.54  |   Q      |          |          |        V |
    5+55       2.6327      1.51  | Q        |          |          |        V |
    6+ 0       2.6394      0.97  |Q         |          |          |        V |
    6+ 5       2.6426      0.47  Q          |          |          |        V |
    6+10       2.6435      0.12  Q          |          |          |        V |
    6+15       2.6438      0.04  Q          |          |          |        V |
    6+20       2.6439      0.01  Q          |          |          |        V |
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: pro102410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 1871.00(Ft.)
Length along longest watercourse measured to centroid = 935.00(Ft.)
Length along longest watercourse = 0.354 Mi.
Length along longest watercourse measured to centroid = 0.177 Mi.
Difference in elevation = 79.00(Ft.)
Slope along watercourse = 222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.045 Hr.
Lag time = 2.70 Min.
25% of lag time = 0.68 Min.
40% of lag time = 1.08 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.80	51.17

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	5.00	142.15

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 3.117(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 3.116(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	69.00	0.500

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.025	(0.363)	0.012	0.012
2	0.17	0.07	0.025	(0.362)	0.012	0.012
3	0.25	0.07	0.025	(0.361)	0.012	0.012
4	0.33	0.10	0.037	(0.359)	0.019	0.019
5	0.42	0.10	0.037	(0.358)	0.019	0.019
6	0.50	0.10	0.037	(0.356)	0.019	0.019
7	0.58	0.10	0.037	(0.355)	0.019	0.019
8	0.67	0.10	0.037	(0.354)	0.019	0.019
9	0.75	0.10	0.037	(0.352)	0.019	0.019
10	0.83	0.13	0.050	(0.351)	0.025	0.025
11	0.92	0.13	0.050	(0.350)	0.025	0.025
12	1.00	0.13	0.050	(0.348)	0.025	0.025
13	1.08	0.10	0.037	(0.347)	0.019	0.019
14	1.17	0.10	0.037	(0.345)	0.019	0.019
15	1.25	0.10	0.037	(0.344)	0.019	0.019
16	1.33	0.10	0.037	(0.343)	0.019	0.019
17	1.42	0.10	0.037	(0.341)	0.019	0.019
18	1.50	0.10	0.037	(0.340)	0.019	0.019
19	1.58	0.10	0.037	(0.339)	0.019	0.019
20	1.67	0.10	0.037	(0.337)	0.019	0.019
21	1.75	0.10	0.037	(0.336)	0.019	0.019
22	1.83	0.13	0.050	(0.335)	0.025	0.025
23	1.92	0.13	0.050	(0.333)	0.025	0.025
24	2.00	0.13	0.050	(0.332)	0.025	0.025
25	2.08	0.13	0.050	(0.330)	0.025	0.025
26	2.17	0.13	0.050	(0.329)	0.025	0.025
27	2.25	0.13	0.050	(0.328)	0.025	0.025
28	2.33	0.13	0.050	(0.326)	0.025	0.025
29	2.42	0.13	0.050	(0.325)	0.025	0.025
30	2.50	0.13	0.050	(0.324)	0.025	0.025
31	2.58	0.17	0.062	(0.323)	0.031	0.031
32	2.67	0.17	0.062	(0.321)	0.031	0.031
33	2.75	0.17	0.062	(0.320)	0.031	0.031
34	2.83	0.17	0.062	(0.319)	0.031	0.031
35	2.92	0.17	0.062	(0.317)	0.031	0.031
36	3.00	0.17	0.062	(0.316)	0.031	0.031
37	3.08	0.17	0.062	(0.315)	0.031	0.031
38	3.17	0.17	0.062	(0.313)	0.031	0.031
39	3.25	0.17	0.062	(0.312)	0.031	0.031
40	3.33	0.17	0.062	(0.311)	0.031	0.031
41	3.42	0.17	0.062	(0.309)	0.031	0.031
42	3.50	0.17	0.062	(0.308)	0.031	0.031
43	3.58	0.17	0.062	(0.307)	0.031	0.031
44	3.67	0.17	0.062	(0.306)	0.031	0.031
45	3.75	0.17	0.062	(0.304)	0.031	0.031
46	3.83	0.20	0.075	(0.303)	0.037	0.037
47	3.92	0.20	0.075	(0.302)	0.037	0.037
48	4.00	0.20	0.075	(0.300)	0.037	0.037
49	4.08	0.20	0.075	(0.299)	0.037	0.037
50	4.17	0.20	0.075	(0.298)	0.037	0.037
51	4.25	0.20	0.075	(0.297)	0.037	0.037
52	4.33	0.23	0.087	(0.295)	0.044	0.044
53	4.42	0.23	0.087	(0.294)	0.044	0.044
54	4.50	0.23	0.087	(0.293)	0.044	0.044
55	4.58	0.23	0.087	(0.292)	0.044	0.044
56	4.67	0.23	0.087	(0.290)	0.044	0.044
57	4.75	0.23	0.087	(0.289)	0.044	0.044
58	4.83	0.27	0.100	(0.288)	0.050	0.050
59	4.92	0.27	0.100	(0.287)	0.050	0.050
60	5.00	0.27	0.100	(0.285)	0.050	0.050
61	5.08	0.20	0.075	(0.284)	0.037	0.037
62	5.17	0.20	0.075	(0.283)	0.037	0.037
63	5.25	0.20	0.075	(0.282)	0.037	0.037
64	5.33	0.23	0.087	(0.280)	0.044	0.044
65	5.42	0.23	0.087	(0.279)	0.044	0.044
66	5.50	0.23	0.087	(0.278)	0.044	0.044
67	5.58	0.27	0.100	(0.277)	0.050	0.050
68	5.67	0.27	0.100	(0.275)	0.050	0.050
69	5.75	0.27	0.100	(0.274)	0.050	0.050
70	5.83	0.27	0.100	(0.273)	0.050	0.050
71	5.92	0.27	0.100	(0.272)	0.050	0.050

72	6.00	0.27	0.100	(0.271)	0.050	0.050
73	6.08	0.30	0.112	(0.269)	0.056	0.056
74	6.17	0.30	0.112	(0.268)	0.056	0.056
75	6.25	0.30	0.112	(0.267)	0.056	0.056
76	6.33	0.30	0.112	(0.266)	0.056	0.056
77	6.42	0.30	0.112	(0.265)	0.056	0.056
78	6.50	0.30	0.112	(0.263)	0.056	0.056
79	6.58	0.33	0.125	(0.262)	0.062	0.062
80	6.67	0.33	0.125	(0.261)	0.062	0.062
81	6.75	0.33	0.125	(0.260)	0.062	0.062
82	6.83	0.33	0.125	(0.259)	0.062	0.062
83	6.92	0.33	0.125	(0.258)	0.062	0.062
84	7.00	0.33	0.125	(0.256)	0.062	0.062
85	7.08	0.33	0.125	(0.255)	0.062	0.062
86	7.17	0.33	0.125	(0.254)	0.062	0.062
87	7.25	0.33	0.125	(0.253)	0.062	0.062
88	7.33	0.37	0.137	(0.252)	0.069	0.069
89	7.42	0.37	0.137	(0.251)	0.069	0.069
90	7.50	0.37	0.137	(0.249)	0.069	0.069
91	7.58	0.40	0.150	(0.248)	0.075	0.075
92	7.67	0.40	0.150	(0.247)	0.075	0.075
93	7.75	0.40	0.150	(0.246)	0.075	0.075
94	7.83	0.43	0.162	(0.245)	0.081	0.081
95	7.92	0.43	0.162	(0.244)	0.081	0.081
96	8.00	0.43	0.162	(0.243)	0.081	0.081
97	8.08	0.50	0.187	(0.242)	0.093	0.093
98	8.17	0.50	0.187	(0.240)	0.093	0.093
99	8.25	0.50	0.187	(0.239)	0.093	0.093
100	8.33	0.50	0.187	(0.238)	0.093	0.093
101	8.42	0.50	0.187	(0.237)	0.093	0.093
102	8.50	0.50	0.187	(0.236)	0.093	0.093
103	8.58	0.53	0.199	(0.235)	0.100	0.100
104	8.67	0.53	0.199	(0.234)	0.100	0.100
105	8.75	0.53	0.199	(0.233)	0.100	0.100
106	8.83	0.57	0.212	(0.232)	0.106	0.106
107	8.92	0.57	0.212	(0.230)	0.106	0.106
108	9.00	0.57	0.212	(0.229)	0.106	0.106
109	9.08	0.63	0.237	(0.228)	0.118	0.118
110	9.17	0.63	0.237	(0.227)	0.118	0.118
111	9.25	0.63	0.237	(0.226)	0.118	0.118
112	9.33	0.67	0.249	(0.225)	0.125	0.125
113	9.42	0.67	0.249	(0.224)	0.125	0.125
114	9.50	0.67	0.249	(0.223)	0.125	0.125
115	9.58	0.70	0.262	(0.222)	0.131	0.131
116	9.67	0.70	0.262	(0.221)	0.131	0.131
117	9.75	0.70	0.262	(0.220)	0.131	0.131
118	9.83	0.73	0.274	(0.219)	0.137	0.137
119	9.92	0.73	0.274	(0.218)	0.137	0.137
120	10.00	0.73	0.274	(0.217)	0.137	0.137
121	10.08	0.50	0.187	(0.215)	0.093	0.093
122	10.17	0.50	0.187	(0.214)	0.093	0.093
123	10.25	0.50	0.187	(0.213)	0.093	0.093
124	10.33	0.50	0.187	(0.212)	0.093	0.093
125	10.42	0.50	0.187	(0.211)	0.093	0.093
126	10.50	0.50	0.187	(0.210)	0.093	0.093
127	10.58	0.67	0.249	(0.209)	0.125	0.125
128	10.67	0.67	0.249	(0.208)	0.125	0.125
129	10.75	0.67	0.249	(0.207)	0.125	0.125
130	10.83	0.67	0.249	(0.206)	0.125	0.125
131	10.92	0.67	0.249	(0.205)	0.125	0.125
132	11.00	0.67	0.249	(0.204)	0.125	0.125
133	11.08	0.63	0.237	(0.203)	0.118	0.118
134	11.17	0.63	0.237	(0.202)	0.118	0.118
135	11.25	0.63	0.237	(0.201)	0.118	0.118
136	11.33	0.63	0.237	(0.200)	0.118	0.118
137	11.42	0.63	0.237	(0.199)	0.118	0.118
138	11.50	0.63	0.237	(0.198)	0.118	0.118
139	11.58	0.57	0.212	(0.197)	0.106	0.106
140	11.67	0.57	0.212	(0.196)	0.106	0.106
141	11.75	0.57	0.212	(0.195)	0.106	0.106
142	11.83	0.60	0.224	(0.194)	0.112	0.112
143	11.92	0.60	0.224	(0.193)	0.112	0.112
144	12.00	0.60	0.224	(0.192)	0.112	0.112
145	12.08	0.83	0.312	(0.191)	0.156	0.156
146	12.17	0.83	0.312	(0.190)	0.156	0.156
147	12.25	0.83	0.312	(0.189)	0.156	0.156
148	12.33	0.87	0.324	(0.189)	0.162	0.162
149	12.42	0.87	0.324	(0.188)	0.162	0.162
150	12.50	0.87	0.324	(0.187)	0.162	0.162
151	12.58	0.93	0.349	(0.186)	0.175	0.175
152	12.67	0.93	0.349	(0.185)	0.175	0.175
153	12.75	0.93	0.349	(0.184)	0.175	0.175
154	12.83	0.97	0.361	(0.183)	0.181	0.181
155	12.92	0.97	0.361	(0.182)	0.181	0.181
156	13.00	0.97	0.361	(0.181)	0.181	0.181
157	13.08	1.13	0.424	0.180	(0.212)	0.244

158	13.17	1.13	0.424	0.179	(0.212)	0.245
159	13.25	1.13	0.424	0.178	(0.212)	0.245
160	13.33	1.13	0.424	0.177	(0.212)	0.246
161	13.42	1.13	0.424	0.177	(0.212)	0.247
162	13.50	1.13	0.424	0.176	(0.212)	0.248
163	13.58	0.77	0.287	(0.175)	0.143	0.143
164	13.67	0.77	0.287	(0.174)	0.143	0.143
165	13.75	0.77	0.287	(0.173)	0.143	0.143
166	13.83	0.77	0.287	(0.172)	0.143	0.143
167	13.92	0.77	0.287	(0.171)	0.143	0.143
168	14.00	0.77	0.287	(0.170)	0.143	0.143
169	14.08	0.90	0.337	(0.169)	0.168	0.168
170	14.17	0.90	0.337	(0.169)	0.168	0.168
171	14.25	0.90	0.337	0.168	(0.168)	0.169
172	14.33	0.87	0.324	(0.167)	0.162	0.162
173	14.42	0.87	0.324	(0.166)	0.162	0.162
174	14.50	0.87	0.324	(0.165)	0.162	0.162
175	14.58	0.87	0.324	(0.164)	0.162	0.162
176	14.67	0.87	0.324	(0.163)	0.162	0.162
177	14.75	0.87	0.324	(0.163)	0.162	0.162
178	14.83	0.83	0.312	(0.162)	0.156	0.156
179	14.92	0.83	0.312	(0.161)	0.156	0.156
180	15.00	0.83	0.312	(0.160)	0.156	0.156
181	15.08	0.80	0.299	(0.159)	0.150	0.150
182	15.17	0.80	0.299	(0.159)	0.150	0.150
183	15.25	0.80	0.299	(0.158)	0.150	0.150
184	15.33	0.77	0.287	(0.157)	0.143	0.143
185	15.42	0.77	0.287	(0.156)	0.143	0.143
186	15.50	0.77	0.287	(0.155)	0.143	0.143
187	15.58	0.63	0.237	(0.154)	0.118	0.118
188	15.67	0.63	0.237	(0.154)	0.118	0.118
189	15.75	0.63	0.237	(0.153)	0.118	0.118
190	15.83	0.63	0.237	(0.152)	0.118	0.118
191	15.92	0.63	0.237	(0.151)	0.118	0.118
192	16.00	0.63	0.237	(0.151)	0.118	0.118
193	16.08	0.13	0.050	(0.150)	0.025	0.025
194	16.17	0.13	0.050	(0.149)	0.025	0.025
195	16.25	0.13	0.050	(0.148)	0.025	0.025
196	16.33	0.13	0.050	(0.148)	0.025	0.025
197	16.42	0.13	0.050	(0.147)	0.025	0.025
198	16.50	0.13	0.050	(0.146)	0.025	0.025
199	16.58	0.10	0.037	(0.145)	0.019	0.019
200	16.67	0.10	0.037	(0.145)	0.019	0.019
201	16.75	0.10	0.037	(0.144)	0.019	0.019
202	16.83	0.10	0.037	(0.143)	0.019	0.019
203	16.92	0.10	0.037	(0.142)	0.019	0.019
204	17.00	0.10	0.037	(0.142)	0.019	0.019
205	17.08	0.17	0.062	(0.141)	0.031	0.031
206	17.17	0.17	0.062	(0.140)	0.031	0.031
207	17.25	0.17	0.062	(0.140)	0.031	0.031
208	17.33	0.17	0.062	(0.139)	0.031	0.031
209	17.42	0.17	0.062	(0.138)	0.031	0.031
210	17.50	0.17	0.062	(0.137)	0.031	0.031
211	17.58	0.17	0.062	(0.137)	0.031	0.031
212	17.67	0.17	0.062	(0.136)	0.031	0.031
213	17.75	0.17	0.062	(0.135)	0.031	0.031
214	17.83	0.13	0.050	(0.135)	0.025	0.025
215	17.92	0.13	0.050	(0.134)	0.025	0.025
216	18.00	0.13	0.050	(0.133)	0.025	0.025
217	18.08	0.13	0.050	(0.133)	0.025	0.025
218	18.17	0.13	0.050	(0.132)	0.025	0.025
219	18.25	0.13	0.050	(0.131)	0.025	0.025
220	18.33	0.13	0.050	(0.131)	0.025	0.025
221	18.42	0.13	0.050	(0.130)	0.025	0.025
222	18.50	0.13	0.050	(0.130)	0.025	0.025
223	18.58	0.10	0.037	(0.129)	0.019	0.019
224	18.67	0.10	0.037	(0.128)	0.019	0.019
225	18.75	0.10	0.037	(0.128)	0.019	0.019
226	18.83	0.07	0.025	(0.127)	0.012	0.012
227	18.92	0.07	0.025	(0.126)	0.012	0.012
228	19.00	0.07	0.025	(0.126)	0.012	0.012
229	19.08	0.10	0.037	(0.125)	0.019	0.019
230	19.17	0.10	0.037	(0.125)	0.019	0.019
231	19.25	0.10	0.037	(0.124)	0.019	0.019
232	19.33	0.13	0.050	(0.123)	0.025	0.025
233	19.42	0.13	0.050	(0.123)	0.025	0.025
234	19.50	0.13	0.050	(0.122)	0.025	0.025
235	19.58	0.10	0.037	(0.122)	0.019	0.019
236	19.67	0.10	0.037	(0.121)	0.019	0.019
237	19.75	0.10	0.037	(0.121)	0.019	0.019
238	19.83	0.07	0.025	(0.120)	0.012	0.012
239	19.92	0.07	0.025	(0.120)	0.012	0.012
240	20.00	0.07	0.025	(0.119)	0.012	0.012
241	20.08	0.10	0.037	(0.119)	0.019	0.019
242	20.17	0.10	0.037	(0.118)	0.019	0.019
243	20.25	0.10	0.037	(0.118)	0.019	0.019

244	20.33	0.10	0.037	(0.117)	0.019	0.019
245	20.42	0.10	0.037	(0.116)	0.019	0.019
246	20.50	0.10	0.037	(0.116)	0.019	0.019
247	20.58	0.10	0.037	(0.116)	0.019	0.019
248	20.67	0.10	0.037	(0.115)	0.019	0.019
249	20.75	0.10	0.037	(0.115)	0.019	0.019
250	20.83	0.07	0.025	(0.114)	0.012	0.012
251	20.92	0.07	0.025	(0.114)	0.012	0.012
252	21.00	0.07	0.025	(0.113)	0.012	0.012
253	21.08	0.10	0.037	(0.113)	0.019	0.019
254	21.17	0.10	0.037	(0.112)	0.019	0.019
255	21.25	0.10	0.037	(0.112)	0.019	0.019
256	21.33	0.07	0.025	(0.111)	0.012	0.012
257	21.42	0.07	0.025	(0.111)	0.012	0.012
258	21.50	0.07	0.025	(0.111)	0.012	0.012
259	21.58	0.10	0.037	(0.110)	0.019	0.019
260	21.67	0.10	0.037	(0.110)	0.019	0.019
261	21.75	0.10	0.037	(0.109)	0.019	0.019
262	21.83	0.07	0.025	(0.109)	0.012	0.012
263	21.92	0.07	0.025	(0.109)	0.012	0.012
264	22.00	0.07	0.025	(0.108)	0.012	0.012
265	22.08	0.10	0.037	(0.108)	0.019	0.019
266	22.17	0.10	0.037	(0.108)	0.019	0.019
267	22.25	0.10	0.037	(0.107)	0.019	0.019
268	22.33	0.07	0.025	(0.107)	0.012	0.012
269	22.42	0.07	0.025	(0.107)	0.012	0.012
270	22.50	0.07	0.025	(0.106)	0.012	0.012
271	22.58	0.07	0.025	(0.106)	0.012	0.012
272	22.67	0.07	0.025	(0.106)	0.012	0.012
273	22.75	0.07	0.025	(0.105)	0.012	0.012
274	22.83	0.07	0.025	(0.105)	0.012	0.012
275	22.92	0.07	0.025	(0.105)	0.012	0.012
276	23.00	0.07	0.025	(0.105)	0.012	0.012
277	23.08	0.07	0.025	(0.104)	0.012	0.012
278	23.17	0.07	0.025	(0.104)	0.012	0.012
279	23.25	0.07	0.025	(0.104)	0.012	0.012
280	23.33	0.07	0.025	(0.104)	0.012	0.012
281	23.42	0.07	0.025	(0.103)	0.012	0.012
282	23.50	0.07	0.025	(0.103)	0.012	0.012
283	23.58	0.07	0.025	(0.103)	0.012	0.012
284	23.67	0.07	0.025	(0.103)	0.012	0.012
285	23.75	0.07	0.025	(0.103)	0.012	0.012
286	23.83	0.07	0.025	(0.103)	0.012	0.012
287	23.92	0.07	0.025	(0.103)	0.012	0.012
288	24.00	0.07	0.025	(0.103)	0.012	0.012

(Loss Rate Not Used)

Sum = 100.0 Sum = 18.9

Flood volume = Effective rainfall 1.58(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 3.7(Ac.Ft)
Total soil loss = 1.54(In)
Total soil loss = 3.651(Ac.Ft)
Total rainfall = 3.12(In)
Flood volume = 162565.1 Cubic Feet
Total soil loss = 159043.2 Cubic Feet

Peak flow rate of this hydrograph = 7.094(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0010	0.15	Q				
0+10	0.0031	0.30	VQ				
0+15	0.0054	0.34	VQ				
0+20	0.0083	0.42	VQ				
0+25	0.0119	0.51	V Q				
0+30	0.0155	0.53	V Q				
0+35	0.0192	0.53	V Q				
0+40	0.0228	0.54	V Q				
0+45	0.0265	0.54	V Q				
0+50	0.0307	0.61	V Q				
0+55	0.0355	0.69	V Q				
1+ 0	0.0403	0.70	V Q				
1+ 5	0.0447	0.64	V Q				
1+10	0.0486	0.56	V Q				
1+15	0.0524	0.55	V Q				
1+20	0.0561	0.54	V Q				
1+25	0.0598	0.54	V Q				
1+30	0.0634	0.54	V Q				
1+35	0.0671	0.54	V Q				
1+40	0.0708	0.54	V Q				

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1+45    0.0745    0.54  V Q       |         |         |         |
1+50    0.0787    0.61  V Q       |         |         |         |
1+55    0.0835    0.69  V Q       |         |         |         |
2+ 0    0.0883    0.70  V Q       |         |         |         |
2+ 5    0.0932    0.71  V Q       |         |         |         |
2+10    0.0981    0.71  |VQ       |         |         |         |
2+15    0.1031    0.71  |VQ       |         |         |         |
2+20    0.1080    0.71  |VQ       |         |         |         |
2+25    0.1129    0.71  |VQ       |         |         |         |
2+30    0.1178    0.71  |VQ       |         |         |         |
2+35    0.1232    0.79  |V Q      |         |         |         |
2+40    0.1292    0.87  |V Q      |         |         |         |
2+45    0.1353    0.88  |V Q      |         |         |         |
2+50    0.1414    0.89  |V Q      |         |         |         |
2+55    0.1476    0.89  |V Q      |         |         |         |
3+ 0    0.1537    0.89  |V Q      |         |         |         |
3+ 5    0.1599    0.89  |V Q      |         |         |         |
3+10    0.1660    0.89  |V Q      |         |         |         |
3+15    0.1722    0.89  |V Q      |         |         |         |
3+20    0.1783    0.89  |V Q      |         |         |         |
3+25    0.1845    0.89  |V Q      |         |         |         |
3+30    0.1907    0.89  | VQ      |         |         |         |
3+35    0.1968    0.89  | VQ      |         |         |         |
3+40    0.2030    0.89  | VQ      |         |         |         |
3+45    0.2091    0.89  | VQ      |         |         |         |
3+50    0.2158    0.97  | VQ      |         |         |         |
3+55    0.2230    1.05  | V Q     |         |         |         |
4+ 0    0.2303    1.06  | V Q     |         |         |         |
4+ 5    0.2376    1.07  | V Q     |         |         |         |
4+10    0.2450    1.07  | V Q     |         |         |         |
4+15    0.2524    1.07  | V Q     |         |         |         |
4+20    0.2603    1.14  | V Q     |         |         |         |
4+25    0.2687    1.22  | V Q     |         |         |         |
4+30    0.2773    1.24  | V Q     |         |         |         |
4+35    0.2859    1.25  |  VQ     |         |         |         |
4+40    0.2945    1.25  |  V Q    |         |         |         |
4+45    0.3031    1.25  |  V Q    |         |         |         |
4+50    0.3122    1.32  |  V Q    |         |         |         |
4+55    0.3219    1.40  |  V Q    |         |         |         |
5+ 0    0.3316    1.42  |  V Q    |         |         |         |
5+ 5    0.3405    1.28  |  V Q    |         |         |         |
5+10    0.3482    1.13  |  VQ     |         |         |         |
5+15    0.3557    1.09  |  VQ     |         |         |         |
5+20    0.3637    1.15  |  VQ     |         |         |         |
5+25    0.3721    1.22  |  VQ     |         |         |         |
5+30    0.3806    1.24  |   Q     |         |         |         |
5+35    0.3897    1.32  |   VQ    |         |         |         |
5+40    0.3994    1.40  |   VQ    |         |         |         |
5+45    0.4092    1.42  |   VQ    |         |         |         |
5+50    0.4190    1.43  |   VQ    |         |         |         |
5+55    0.4288    1.43  |   VQ    |         |         |         |
6+ 0    0.4387    1.43  |   VQ    |         |         |         |
6+ 5    0.4490    1.50  |   V Q   |         |         |         |
6+10    0.4599    1.58  |   V Q   |         |         |         |
6+15    0.4709    1.60  |    VQ   |         |         |         |
6+20    0.4820    1.61  |    VQ   |         |         |         |
6+25    0.4931    1.61  |    VQ   |         |         |         |
6+30    0.5041    1.61  |    VQ   |         |         |         |
6+35    0.5157    1.68  |    VQ   |         |         |         |
6+40    0.5278    1.76  |    V Q  |         |         |         |
6+45    0.5401    1.78  |    V Q  |         |         |         |
6+50    0.5524    1.78  |    V Q  |         |         |         |
6+55    0.5647    1.79  |     VQ  |         |         |         |
7+ 0    0.5770    1.79  |     VQ  |         |         |         |
7+ 5    0.5893    1.79  |     VQ  |         |         |         |
7+10    0.6016    1.79  |     VQ  |         |         |         |
7+15    0.6139    1.79  |     VQ  |         |         |         |
7+20    0.6267    1.86  |     VQ  |         |         |         |
7+25    0.6400    1.94  |     VQ  |         |         |         |
7+30    0.6535    1.96  |      Q  |         |         |         |
7+35    0.6675    2.04  |     VQ  |         |         |         |
7+40    0.6821    2.12  |     VQ  |         |         |         |
7+45    0.6968    2.13  |     VQ  |         |         |         |
7+50    0.7121    2.21  |     VQ  |         |         |         |
7+55    0.7279    2.30  |     V Q|         |         |         |
8+ 0    0.7438    2.31  |     V Q|         |         |         |
8+ 5    0.7608    2.47  |      VQ|         |         |         |
8+10    0.7789    2.63  |      V Q|         |         |         |
8+15    0.7972    2.66  |      V Q|         |         |         |
8+20    0.8156    2.67  |      V Q|         |         |         |
8+25    0.8341    2.68  |      V Q|         |         |         |
8+30    0.8525    2.68  |       VQ|         |         |         |
8+35    0.8715    2.75  |       V|Q         |         |         |
8+40    0.8910    2.83  |       V|Q         |         |         |
8+45    0.9106    2.85  |       V|Q         |         |         |
8+50    0.9308    2.93  |       V|Q         |         |         |
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8+55	0.9515	3.01	V Q			
9+ 0	0.9724	3.03	V Q			
9+ 5	0.9943	3.18	V Q			
9+10	1.0173	3.34	V Q			
9+15	1.0405	3.38	V Q			
9+20	1.0644	3.46	V Q			
9+25	1.0888	3.55	V Q			
9+30	1.1133	3.56	V Q			
9+35	1.1384	3.64	V Q			
9+40	1.1641	3.73	V Q			
9+45	1.1899	3.74	V Q			
9+50	1.2162	3.82	V Q			
9+55	1.2431	3.90	V Q			
10+ 0	1.2701	3.92	V Q			
10+ 5	1.2936	3.42	Q			
10+10	1.3134	2.87	Q V			
10+15	1.3323	2.75	Q V			
10+20	1.3509	2.70	Q V			
10+25	1.3693	2.68	Q V			
10+30	1.3878	2.68	Q V			
10+35	1.4088	3.04	Q V			
10+40	1.4325	3.44	Q V			
10+45	1.4567	3.52	QV			
10+50	1.4812	3.56	QV			
10+55	1.5059	3.57	Q V			
11+ 0	1.5305	3.57	Q V			
11+ 5	1.5546	3.50	Q V			
11+10	1.5781	3.42	Q V			
11+15	1.6016	3.40	Q V			
11+20	1.6250	3.40	Q V			
11+25	1.6484	3.39	Q V			
11+30	1.6717	3.39	Q V			
11+35	1.6941	3.25	Q V			
11+40	1.7154	3.09	Q V			
11+45	1.7365	3.06	Q V			
11+50	1.7579	3.12	Q V			
11+55	1.7799	3.19	Q V			
12+ 0	1.8020	3.21	Q V			
12+ 5	1.8276	3.72	Q V			
12+10	1.8571	4.28	Q V			
12+15	1.8874	4.40	Q V			
12+20	1.9185	4.52	Q V			
12+25	1.9503	4.62	Q V			
12+30	1.9822	4.64	Q V			
12+35	2.0152	4.79	Q V			
12+40	2.0493	4.95	Q V			
12+45	2.0836	4.98	Q V			
12+50	2.1185	5.07	Q V			
12+55	2.1540	5.15	Q V			
13+ 0	2.1897	5.17	Q V			
13+ 5	2.2304	5.91	Q			
13+10	2.2767	6.73	V Q			
13+15	2.3244	6.92	V Q			
13+20	2.3727	7.01	V Q			
13+25	2.4214	7.07	V Q			
13+30	2.4702	7.09	V Q			
13+35	2.5108	5.89	Q V			
13+40	2.5421	4.55	Q V			
13+45	2.5715	4.27	Q V			
13+50	2.6002	4.16	Q V			
13+55	2.6285	4.11	Q V			
14+ 0	2.6568	4.11	Q V			
14+ 5	2.6871	4.40	Q V			
14+10	2.7196	4.72	Q V			
14+15	2.7526	4.79	Q V			
14+20	2.7853	4.75	Q V			
14+25	2.8175	4.67	Q V			
14+30	2.8495	4.66	Q V			
14+35	2.8815	4.65	Q V			
14+40	2.9135	4.65	Q V			
14+45	2.9455	4.65	Q V			
14+50	2.9770	4.57	Q V			
14+55	3.0080	4.49	Q V			
15+ 0	3.0388	4.48	Q V			
15+ 5	3.0691	4.40	Q V			
15+10	3.0988	4.31	Q V			
15+15	3.1284	4.30	Q V			
15+20	3.1575	4.22	Q V			
15+25	3.1859	4.14	Q V			
15+30	3.2143	4.12	Q V			
15+35	3.2406	3.82	Q V			
15+40	3.2647	3.50	Q V			
15+45	3.2884	3.43	Q V			
15+50	3.3118	3.41	Q V			
15+55	3.3352	3.39	Q V			
16+ 0	3.3586	3.39	Q V			

16+ 5	3.3745	2.30		Q			V
16+10	3.3821	1.11		Q			V
16+15	3.3881	0.86		Q			V
16+20	3.3933	0.76		Q			V
16+25	3.3982	0.71	Q				V
16+30	3.4031	0.71	Q				V
16+35	3.4075	0.64	Q				V
16+40	3.4114	0.56	Q				V
16+45	3.4152	0.55	Q				V
16+50	3.4189	0.54	Q				V
16+55	3.4226	0.54	Q				V
17+ 0	3.4263	0.54	Q				V
17+ 5	3.4310	0.68	Q				V
17+10	3.4368	0.84		Q			V
17+15	3.4428	0.87		Q			V
17+20	3.4489	0.89		Q			V
17+25	3.4550	0.89		Q			V
17+30	3.4612	0.89		Q			V
17+35	3.4673	0.89		Q			V
17+40	3.4735	0.89		Q			V
17+45	3.4796	0.89		Q			V
17+50	3.4853	0.82		Q			V
17+55	3.4904	0.74	Q				V
18+ 0	3.4954	0.72	Q				V
18+ 5	3.5003	0.72	Q				V
18+10	3.5053	0.71	Q				V
18+15	3.5102	0.71	Q				V
18+20	3.5151	0.71	Q				V
18+25	3.5200	0.71	Q				V
18+30	3.5249	0.71	Q				V
18+35	3.5294	0.64	Q				V
18+40	3.5332	0.56	Q				V
18+45	3.5370	0.55	Q				V
18+50	3.5402	0.47	Q				V
18+55	3.5429	0.38	Q				V
19+ 0	3.5454	0.37	Q				V
19+ 5	3.5484	0.43	Q				V
19+10	3.5519	0.51	Q				V
19+15	3.5555	0.53	Q				V
19+20	3.5597	0.61	Q				V
19+25	3.5644	0.69	Q				V
19+30	3.5693	0.70	Q				V
19+35	3.5737	0.64	Q				V
19+40	3.5775	0.56	Q				V
19+45	3.5813	0.55	Q				V
19+50	3.5845	0.47	Q				V
19+55	3.5872	0.38	Q				V
20+ 0	3.5897	0.37	Q				V
20+ 5	3.5927	0.43	Q				V
20+10	3.5962	0.51	Q				V
20+15	3.5998	0.53	Q				V
20+20	3.6035	0.53	Q				V
20+25	3.6072	0.54	Q				V
20+30	3.6109	0.54	Q				V
20+35	3.6145	0.54	Q				V
20+40	3.6182	0.54	Q				V
20+45	3.6219	0.54	Q				V
20+50	3.6251	0.46	Q				V
20+55	3.6278	0.38	Q				V
21+ 0	3.6303	0.37	Q				V
21+ 5	3.6333	0.43	Q				V
21+10	3.6368	0.51	Q				V
21+15	3.6404	0.53	Q				V
21+20	3.6436	0.46	Q				V
21+25	3.6462	0.38	Q				V
21+30	3.6487	0.37	Q				V
21+35	3.6517	0.43	Q				V
21+40	3.6552	0.51	Q				V
21+45	3.6589	0.53	Q				V
21+50	3.6620	0.46	Q				V
21+55	3.6647	0.38	Q				V
22+ 0	3.6672	0.37	Q				V
22+ 5	3.6702	0.43	Q				V
22+10	3.6737	0.51	Q				V
22+15	3.6773	0.53	Q				V
22+20	3.6805	0.46	Q				V
22+25	3.6831	0.38	Q				V
22+30	3.6857	0.37	Q				V
22+35	3.6881	0.36	Q				V
22+40	3.6906	0.36	Q				V
22+45	3.6931	0.36	Q				V
22+50	3.6955	0.36	Q				V
22+55	3.6980	0.36	Q				V
23+ 0	3.7004	0.36	Q				V
23+ 5	3.7029	0.36	Q				V
23+10	3.7054	0.36	Q				V

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   23+15       3.7078      0.36  |Q        |         |         |        v|
   23+20       3.7103      0.36  |Q        |         |         |        v|
   23+25       3.7128      0.36  |Q        |         |         |        v|
   23+30       3.7152      0.36  |Q        |         |         |        v|
   23+35       3.7177      0.36  |Q        |         |         |        v|
   23+40       3.7201      0.36  |Q        |         |         |        v|
   23+45       3.7226      0.36  |Q        |         |         |        v|
   23+50       3.7251      0.36  |Q        |         |         |        v|
   23+55       3.7275      0.36  |Q        |         |         |        v|
   24+ 0       3.7300      0.36  |Q        |         |         |        v|
   24+ 5       3.7314      0.21  Q         |         |         |        v|
   24+10       3.7318      0.05  Q         |         |         |        v|
   24+15       3.7319      0.02  Q         |         |         |        v|
   24+20       3.7320      0.01  Q         |         |         |         v
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U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 1871.00(Ft.)
Length along longest watercourse measured to centroid = 935.00(Ft.)
Length along longest watercourse = 0.354 Mi.
Length along longest watercourse measured to centroid = 0.177 Mi.
Difference in elevation = 79.00(Ft.)
Slope along watercourse = 222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.045 Hr.
Lag time = 2.70 Min.
25% of lag time = 0.68 Min.
40% of lag time = 1.08 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.50	14.22

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.30	36.96

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.300(In)

Point rain (area averaged) = 1.300(In)
Areal adjustment factor = 99.97 %
Adjusted average point rain = 1.300(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	69.00	0.500

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

Slope of intensity-duration curve for a 1 hour storm =0.5500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time		Pattern	Storm Rain	Loss rate(In./Hr)			Effective
	(Hr.)	Percent	(In/Hr)	Max		Low	(In/Hr)
1	0.08	3.30	0.515	0.205	(	0.257)	0.310
2	0.17	4.20	0.655	0.205	(	0.328)	0.450
3	0.25	4.40	0.686	0.205	(	0.343)	0.481
4	0.33	4.80	0.749	0.205	(	0.374)	0.544
5	0.42	5.20	0.811	0.205	(	0.405)	0.606
6	0.50	6.20	0.967	0.205	(	0.483)	0.762
7	0.58	6.80	1.061	0.205	(	0.530)	0.855
8	0.67	8.80	1.372	0.205	(	0.686)	1.167
9	0.75	13.90	2.168	0.205	(	1.084)	1.963
10	0.83	31.40	4.897	0.205	(	2.449)	4.692
11	0.92	7.20	1.123	0.205	(	0.561)	0.918
12	1.00	3.80	0.593	0.205	(	0.296)	0.388
		(Loss Rate Not Used)					
Sum =		100.0				Sum =	13.1

Flood volume = Effective rainfall 1.09(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 2.6(Ac.Ft)
Total soil loss = 0.21(In)
Total soil loss = 0.486(Ac.Ft)
Total rainfall = 1.30(In)
Flood volume = 112966.3 Cubic Feet
Total soil loss = 21160.3 Cubic Feet

Peak flow rate of this hydrograph = 84.206(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	22.5	45.0	67.5	90.0
0+ 5	0.0249	3.61	VQ				
0+10	0.0882	9.19	V Q				
0+15	0.1721	12.18	V Q				
0+20	0.2687	14.03	V Q				
0+25	0.3784	15.93	V Q				
0+30	0.5080	18.81	VQ				
0+35	0.6605	22.14	QV				
0+40	0.8498	27.49	Q V				
0+45	1.1336	41.20	VQ				
0+50	1.7135	84.21			V	Q	
0+55	2.2468	77.43				Q	
1+ 0	2.4643	31.58		Q		V	
1+ 5	2.5569	13.45	Q			V	
1+10	2.5862	4.25	Q			V	
1+15	2.5921	0.85	Q			V	
1+20	2.5933	0.18	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/30/25 File: pro1003100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 1871.00(Ft.)
Length along longest watercourse measured to centroid = 935.00(Ft.)
Length along longest watercourse = 0.354 Mi.
Length along longest watercourse measured to centroid = 0.177 Mi.
Difference in elevation = 79.00(Ft.)
Slope along watercourse = 222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.045 Hr.
Lag time = 2.70 Min.
25% of lag time = 0.68 Min.
40% of lag time = 1.08 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	0.80	22.74

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	2.00	56.86

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 2.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 2.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	69.00	0.500

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.312	(0.205)	0.156	0.156
2	0.17	1.30	0.312	(0.205)	0.156	0.156
3	0.25	1.10	0.264	(0.205)	0.132	0.132
4	0.33	1.50	0.360	(0.205)	0.180	0.180
5	0.42	1.50	0.360	(0.205)	0.180	0.180
6	0.50	1.80	0.432	0.205	(0.216)	0.227
7	0.58	1.50	0.360	(0.205)	0.180	0.180
8	0.67	1.80	0.432	0.205	(0.216)	0.227
9	0.75	1.80	0.432	0.205	(0.216)	0.227
10	0.83	1.50	0.360	(0.205)	0.180	0.180
11	0.92	1.60	0.384	(0.205)	0.192	0.192
12	1.00	1.80	0.432	0.205	(0.216)	0.227
13	1.08	2.20	0.528	0.205	(0.264)	0.323
14	1.17	2.20	0.528	0.205	(0.264)	0.323
15	1.25	2.20	0.528	0.205	(0.264)	0.323
16	1.33	2.00	0.480	0.205	(0.240)	0.275
17	1.42	2.60	0.624	0.205	(0.312)	0.419
18	1.50	2.70	0.648	0.205	(0.324)	0.443
19	1.58	2.40	0.576	0.205	(0.288)	0.371
20	1.67	2.70	0.648	0.205	(0.324)	0.443
21	1.75	3.30	0.792	0.205	(0.396)	0.587
22	1.83	3.10	0.744	0.205	(0.372)	0.539
23	1.92	2.90	0.696	0.205	(0.348)	0.491
24	2.00	3.00	0.720	0.205	(0.360)	0.515
25	2.08	3.10	0.744	0.205	(0.372)	0.539
26	2.17	4.20	1.008	0.205	(0.504)	0.803
27	2.25	5.00	1.200	0.205	(0.600)	0.995
28	2.33	3.50	0.840	0.205	(0.420)	0.635
29	2.42	6.80	1.632	0.205	(0.816)	1.427
30	2.50	7.30	1.752	0.205	(0.876)	1.547
31	2.58	8.20	1.968	0.205	(0.984)	1.763
32	2.67	5.90	1.416	0.205	(0.708)	1.211
33	2.75	2.00	0.480	0.205	(0.240)	0.275
34	2.83	1.80	0.432	0.205	(0.216)	0.227
35	2.92	1.80	0.432	0.205	(0.216)	0.227
36	3.00	0.60	0.144	(0.205)	0.072	0.072
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	17.0

Flood volume = Effective rainfall 1.42(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 3.4(Ac.Ft)
Total soil loss = 0.58(In)
Total soil loss = 1.375(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 146486.0 Cubic Feet
Total soil loss = 59890.1 Cubic Feet

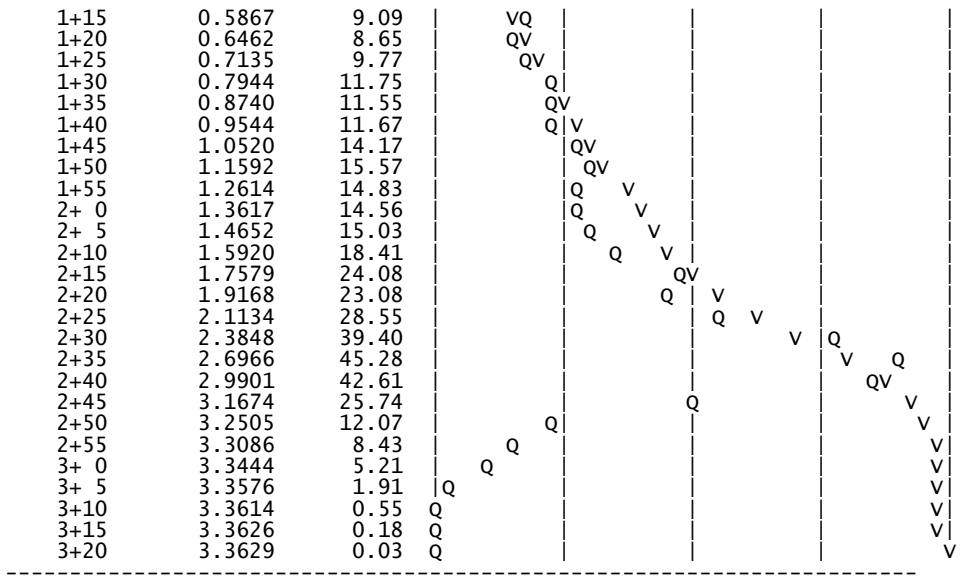
Peak flow rate of this hydrograph = 45.284(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	12.5	25.0	37.5	50.0
0+ 5	0.0125	1.82	VQ				
0+10	0.0388	3.81	V Q				
0+15	0.0659	3.95	V Q				
0+20	0.0961	4.37	V Q				
0+25	0.1304	4.99	V Q				
0+30	0.1693	5.64	V Q				
0+35	0.2088	5.73	V Q				
0+40	0.2490	5.83	V Q				
0+45	0.2928	6.36	V Q				
0+50	0.3334	5.91	VQ				
0+55	0.3712	5.48	Q				
1+ 0	0.4120	5.93	Q				
1+ 5	0.4635	7.48	Q				
1+10	0.5240	8.79	VQ				



1+15	0.5867	9.09	
1+20	0.6462	8.65	
1+25	0.7135	9.77	
1+30	0.7944	11.75	
1+35	0.8740	11.55	
1+40	0.9544	11.67	
1+45	1.0520	14.17	
1+50	1.1592	15.57	
1+55	1.2614	14.83	
2+ 0	1.3617	14.56	
2+ 5	1.4652	15.03	
2+10	1.5920	18.41	
2+15	1.7579	24.08	
2+20	1.9168	23.08	
2+25	2.1134	28.55	
2+30	2.3848	39.40	
2+35	2.6966	45.28	
2+40	2.9901	42.61	
2+45	3.1674	25.74	
2+50	3.2505	12.07	
2+55	3.3086	8.43	
3+ 0	3.3444	5.21	
3+ 5	3.3576	1.91	
3+10	3.3614	0.55	
3+15	3.3626	0.18	
3+20	3.3629	0.03	

U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 28.43(Ac.) = 0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 28.43(Ac.) = 0.044 Sq. Mi.
Length along longest watercourse = 1871.00(Ft.)
Length along longest watercourse measured to centroid = 935.00(Ft.)
Length along longest watercourse = 0.354 Mi.
Length along longest watercourse measured to centroid = 0.177 Mi.
Difference in elevation = 79.00(Ft.)
Slope along watercourse = 222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.045 Hr.
Lag time = 2.70 Min.
25% of lag time = 0.68 Min.
40% of lag time = 1.08 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	1.10	31.27

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
28.43	3.00	85.29

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 3.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 3.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
28.430	69.00	0.500

Total Area Entered = 28.43(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000	Sum= 28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.180	(0.205)	0.090	0.090
2	0.17	0.60	0.216	(0.205)	0.108	0.108
3	0.25	0.60	0.216	(0.205)	0.108	0.108
4	0.33	0.60	0.216	(0.205)	0.108	0.108
5	0.42	0.60	0.216	(0.205)	0.108	0.108
6	0.50	0.70	0.252	(0.205)	0.126	0.126
7	0.58	0.70	0.252	(0.205)	0.126	0.126
8	0.67	0.70	0.252	(0.205)	0.126	0.126
9	0.75	0.70	0.252	(0.205)	0.126	0.126
10	0.83	0.70	0.252	(0.205)	0.126	0.126
11	0.92	0.70	0.252	(0.205)	0.126	0.126
12	1.00	0.80	0.288	(0.205)	0.144	0.144
13	1.08	0.80	0.288	(0.205)	0.144	0.144
14	1.17	0.80	0.288	(0.205)	0.144	0.144
15	1.25	0.80	0.288	(0.205)	0.144	0.144
16	1.33	0.80	0.288	(0.205)	0.144	0.144
17	1.42	0.80	0.288	(0.205)	0.144	0.144
18	1.50	0.80	0.288	(0.205)	0.144	0.144
19	1.58	0.80	0.288	(0.205)	0.144	0.144
20	1.67	0.80	0.288	(0.205)	0.144	0.144
21	1.75	0.80	0.288	(0.205)	0.144	0.144
22	1.83	0.80	0.288	(0.205)	0.144	0.144
23	1.92	0.80	0.288	(0.205)	0.144	0.144
24	2.00	0.90	0.324	(0.205)	0.162	0.162
25	2.08	0.80	0.288	(0.205)	0.144	0.144
26	2.17	0.90	0.324	(0.205)	0.162	0.162
27	2.25	0.90	0.324	(0.205)	0.162	0.162
28	2.33	0.90	0.324	(0.205)	0.162	0.162
29	2.42	0.90	0.324	(0.205)	0.162	0.162
30	2.50	0.90	0.324	(0.205)	0.162	0.162
31	2.58	0.90	0.324	(0.205)	0.162	0.162
32	2.67	0.90	0.324	(0.205)	0.162	0.162
33	2.75	1.00	0.360	(0.205)	0.180	0.180
34	2.83	1.00	0.360	(0.205)	0.180	0.180
35	2.92	1.00	0.360	(0.205)	0.180	0.180
36	3.00	1.00	0.360	(0.205)	0.180	0.180
37	3.08	1.00	0.360	(0.205)	0.180	0.180
38	3.17	1.10	0.396	(0.205)	0.198	0.198
39	3.25	1.10	0.396	(0.205)	0.198	0.198
40	3.33	1.10	0.396	(0.205)	0.198	0.198
41	3.42	1.20	0.432	0.205	(0.216)	0.227
42	3.50	1.30	0.468	0.205	(0.234)	0.263
43	3.58	1.40	0.504	0.205	(0.252)	0.299
44	3.67	1.40	0.504	0.205	(0.252)	0.299
45	3.75	1.50	0.540	0.205	(0.270)	0.335
46	3.83	1.50	0.540	0.205	(0.270)	0.335
47	3.92	1.60	0.576	0.205	(0.288)	0.371
48	4.00	1.60	0.576	0.205	(0.288)	0.371
49	4.08	1.70	0.612	0.205	(0.306)	0.407
50	4.17	1.80	0.648	0.205	(0.324)	0.443
51	4.25	1.90	0.684	0.205	(0.342)	0.479
52	4.33	2.00	0.720	0.205	(0.360)	0.515
53	4.42	2.10	0.756	0.205	(0.378)	0.551
54	4.50	2.10	0.756	0.205	(0.378)	0.551
55	4.58	2.20	0.792	0.205	(0.396)	0.587
56	4.67	2.30	0.828	0.205	(0.414)	0.623
57	4.75	2.40	0.864	0.205	(0.432)	0.659
58	4.83	2.40	0.864	0.205	(0.432)	0.659
59	4.92	2.50	0.900	0.205	(0.450)	0.695
60	5.00	2.60	0.936	0.205	(0.468)	0.731
61	5.08	3.10	1.116	0.205	(0.558)	0.911
62	5.17	3.60	1.296	0.205	(0.648)	1.091
63	5.25	3.90	1.404	0.205	(0.702)	1.199
64	5.33	4.20	1.512	0.205	(0.756)	1.307
65	5.42	4.70	1.692	0.205	(0.846)	1.487
66	5.50	5.60	2.016	0.205	(1.008)	1.811
67	5.58	1.90	0.684	0.205	(0.342)	0.479
68	5.67	0.90	0.324	(0.205)	0.162	0.162
69	5.75	0.60	0.216	(0.205)	0.108	0.108
70	5.83	0.50	0.180	(0.205)	0.090	0.090
71	5.92	0.30	0.108	(0.205)	0.054	0.054

```
72   6.00     0.20      0.072       (  0.205)       0.036        0.036
            (Loss Rate Not Used)
   Sum =     100.0                                    Sum =    24.1
      Flood volume = Effective rainfall      2.01(In)
       times area      28.4(Ac.)/[(In)/(Ft.)] =       4.8(Ac.Ft)
      Total soil loss =      0.99(In)
      Total soil loss =     2.354(Ac.Ft)
      Total rainfall =      3.00(In)
      Flood volume =      207012.6 Cubic Feet
      Total soil loss =      102559.8 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     45.417(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0       12.5      25.0      37.5      50.0
-------------------------------------------------------------------------
  0+ 5       0.0072      1.05  Q         |         |         |         |
  0+10       0.0238      2.41  VQ        |         |         |         |
  0+15       0.0436      2.88  V Q       |         |         |         |
  0+20       0.0645      3.03  V Q       |         |         |         |
  0+25       0.0857      3.09  V Q       |         |         |         |
  0+30       0.1085      3.31  V Q       |         |         |         |
  0+35       0.1328      3.53  |VQ       |         |         |         |
  0+40       0.1575      3.58  |VQ       |         |         |         |
  0+45       0.1823      3.60  |VQ       |         |         |         |
  0+50       0.2072      3.61  |VQ       |         |         |         |
  0+55       0.2321      3.61  |VQ       |         |         |         |
  1+ 0       0.2584      3.82  | VQ      |         |         |         |
  1+ 5       0.2863      4.05  | VQ      |         |         |         |
  1+10       0.3145      4.10  | VQ      |         |         |         |
  1+15       0.3429      4.12  | VQ      |         |         |         |
  1+20       0.3713      4.13  |  Q      |         |         |         |
  1+25       0.3998      4.13  |  Q      |         |         |         |
  1+30       0.4282      4.13  |  Q      |         |         |         |
  1+35       0.4566      4.13  |  Q      |         |         |         |
  1+40       0.4850      4.13  |  QV     |         |         |         |
  1+45       0.5135      4.13  |  QV     |         |         |         |
  1+50       0.5419      4.13  |  QV     |         |         |         |
  1+55       0.5703      4.13  |  QV     |         |         |         |
  2+ 0       0.6002      4.34  |  Q V    |         |         |         |
  2+ 5       0.6302      4.36  |  Q V    |         |         |         |
  2+10       0.6604      4.39  |  Q V    |         |         |         |
  2+15       0.6920      4.59  |  Q V    |         |         |         |
  2+20       0.7238      4.62  |  Q  V   |         |         |         |
  2+25       0.7558      4.64  |  Q  V   |         |         |         |
  2+30       0.7878      4.64  |  Q  V   |         |         |         |
  2+35       0.8197      4.64  |  Q  V   |         |         |         |
  2+40       0.8517      4.64  |  Q   V  |         |         |         |
  2+45       0.8851      4.85  |  Q   V  |         |         |         |
  2+50       0.9201      5.08  |   Q  V  |         |         |         |
  2+55       0.9555      5.13  |   Q   V |         |         |         |
  3+ 0       0.9910      5.15  |   Q   V |         |         |         |
  3+ 5       1.0265      5.16  |   Q   V |         |         |         |
  3+10       1.0635      5.37  |   Q   V |         |         |         |
  3+15       1.1020      5.60  |   Q    V|         |         |         |
  3+20       1.1409      5.65  |   Q    V|         |         |         |
  3+25       1.1823      6.00  |   Q    V|         |         |         |
  3+30       1.2291      6.80  |    Q    V         |         |         |
  3+35       1.2826      7.76  |     Q   V         |         |         |
  3+40       1.3400      8.35  |     Q   |V        |         |         |
  3+45       1.4014      8.92  |      Q  |V        |         |         |
  3+50       1.4664      9.43  |      Q  | V       |         |         |
  3+55       1.5350      9.96  |      Q  | V       |         |         |
  4+ 0       1.6071     10.46  |       Q |  V      |         |         |
  4+ 5       1.6828     11.00  |       Q |   V     |         |         |
  4+10       1.7649     11.91  |        Q|   V     |         |         |
  4+15       1.8538     12.91  |         Q    V    |         |         |
  4+20       1.9496     13.92  |         |Q    V   |         |         |
  4+25       2.0526     14.95  |         |Q     V  |         |         |
  4+30       2.1598     15.57  |         | Q     V |         |         |
  4+35       2.2710     16.14  |         | Q      V|         |         |
  4+40       2.3886     17.07  |         |  Q      V         |         |
  4+45       2.5130     18.07  |         |   Q     |V        |         |
  4+50       2.6415     18.66  |         |   Q     | V       |         |
  4+55       2.7740     19.24  |         |    Q    |  V      |         |
  5+ 0       2.9129     20.17  |         |     Q   |   V     |         |
  5+ 5       3.0702     22.84  |         |      Q  |    V    |         |
  5+10       3.2587     27.37  |         |         |Q     V  |         |
  5+15       3.4755     31.47  |         |         |    Q   V|         |
  5+20       3.7151     34.80  |         |         |      Q  |V        |
```

```
    5+25       3.9827     38.85  |          |          |          |Q V       |
    5+30       4.2955     45.42  |          |          |          |     Q    |
    5+35       4.5341     34.65  |          |          |      Q   |       V  |
    5+40       4.6382     15.12  |          |  Q       |          |         V|
    5+45       4.6884      7.29  |     Q    |          |          |         V|
    5+50       4.7176      4.24  |   Q      |          |          |         V|
    5+55       4.7346      2.47  |Q         |          |          |         V|
    6+ 0       4.7452      1.54  |Q         |          |          |         V|
    6+ 5       4.7504      0.75  Q          |          |          |         V|
    6+10       4.7518      0.20  Q          |          |          |         V|
    6+15       4.7522      0.06  Q          |          |          |         V|
    6+20       4.7524      0.02  Q          |          |          |         V|
-------------------------------------------------------------------------------
```

```
       U n i t   H y d r o g r a p h   A n a l y s i s

       Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2008, Version 8.1
              Study date  04/30/25 File: pro10024100.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      28.43(Ac.)  =      0.044 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      28.43(Ac.)  =      0.044 Sq. Mi.
Length along longest watercourse =    1871.00(Ft.)
Length along longest watercourse measured to centroid =     935.00(Ft.)
Length along longest watercourse =      0.354 Mi.
Length along longest watercourse measured to centroid =      0.177 Mi.
Difference in elevation =      79.00(Ft.)
Slope along watercourse =    222.9396 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.045 Hr.
Lag time =     2.70 Min.
25% of lag time =     0.68 Min.
40% of lag time =     1.08 Min.
Unit time =     5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       28.43           1.80                 51.17

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       28.43           5.00                142.15

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    1.800(In)
Area Averaged 100-Year Rainfall =    5.000(In)

Point rain (area averaged) =    5.000(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    5.000(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    28.430           69.00         0.500
 Total Area Entered =     28.43(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  69.0      0.373     0.500        0.205       1.000      0.205
                                                 Sum (F) =   0.205
Area averaged mean soil loss (F) (In/Hr) =  0.205
Minimum soil loss rate ((In/Hr)) =  0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	185.173	40.719	11.667
2	0.167	370.346	44.415	12.726
3	0.250	555.518	9.425	2.700
4	0.333	740.691	3.805	1.090
5	0.417	925.864	1.637	0.469
			Sum = 100.000 Sum=	28.652

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.040	(0.363)	0.020	0.020
2	0.17	0.07	0.040	(0.362)	0.020	0.020
3	0.25	0.07	0.040	(0.361)	0.020	0.020
4	0.33	0.10	0.060	(0.359)	0.030	0.030
5	0.42	0.10	0.060	(0.358)	0.030	0.030
6	0.50	0.10	0.060	(0.356)	0.030	0.030
7	0.58	0.10	0.060	(0.355)	0.030	0.030
8	0.67	0.10	0.060	(0.354)	0.030	0.030
9	0.75	0.10	0.060	(0.352)	0.030	0.030
10	0.83	0.13	0.080	(0.351)	0.040	0.040
11	0.92	0.13	0.080	(0.350)	0.040	0.040
12	1.00	0.13	0.080	(0.348)	0.040	0.040
13	1.08	0.10	0.060	(0.347)	0.030	0.030
14	1.17	0.10	0.060	(0.345)	0.030	0.030
15	1.25	0.10	0.060	(0.344)	0.030	0.030
16	1.33	0.10	0.060	(0.343)	0.030	0.030
17	1.42	0.10	0.060	(0.341)	0.030	0.030
18	1.50	0.10	0.060	(0.340)	0.030	0.030
19	1.58	0.10	0.060	(0.339)	0.030	0.030
20	1.67	0.10	0.060	(0.337)	0.030	0.030
21	1.75	0.10	0.060	(0.336)	0.030	0.030
22	1.83	0.13	0.080	(0.335)	0.040	0.040
23	1.92	0.13	0.080	(0.333)	0.040	0.040
24	2.00	0.13	0.080	(0.332)	0.040	0.040
25	2.08	0.13	0.080	(0.330)	0.040	0.040
26	2.17	0.13	0.080	(0.329)	0.040	0.040
27	2.25	0.13	0.080	(0.328)	0.040	0.040
28	2.33	0.13	0.080	(0.326)	0.040	0.040
29	2.42	0.13	0.080	(0.325)	0.040	0.040
30	2.50	0.13	0.080	(0.324)	0.040	0.040
31	2.58	0.17	0.100	(0.323)	0.050	0.050
32	2.67	0.17	0.100	(0.321)	0.050	0.050
33	2.75	0.17	0.100	(0.320)	0.050	0.050
34	2.83	0.17	0.100	(0.319)	0.050	0.050
35	2.92	0.17	0.100	(0.317)	0.050	0.050
36	3.00	0.17	0.100	(0.316)	0.050	0.050
37	3.08	0.17	0.100	(0.315)	0.050	0.050
38	3.17	0.17	0.100	(0.313)	0.050	0.050
39	3.25	0.17	0.100	(0.312)	0.050	0.050
40	3.33	0.17	0.100	(0.311)	0.050	0.050
41	3.42	0.17	0.100	(0.309)	0.050	0.050
42	3.50	0.17	0.100	(0.308)	0.050	0.050
43	3.58	0.17	0.100	(0.307)	0.050	0.050
44	3.67	0.17	0.100	(0.306)	0.050	0.050
45	3.75	0.17	0.100	(0.304)	0.050	0.050
46	3.83	0.20	0.120	(0.303)	0.060	0.060
47	3.92	0.20	0.120	(0.302)	0.060	0.060
48	4.00	0.20	0.120	(0.300)	0.060	0.060
49	4.08	0.20	0.120	(0.299)	0.060	0.060
50	4.17	0.20	0.120	(0.298)	0.060	0.060
51	4.25	0.20	0.120	(0.297)	0.060	0.060
52	4.33	0.23	0.140	(0.295)	0.070	0.070
53	4.42	0.23	0.140	(0.294)	0.070	0.070
54	4.50	0.23	0.140	(0.293)	0.070	0.070
55	4.58	0.23	0.140	(0.292)	0.070	0.070
56	4.67	0.23	0.140	(0.290)	0.070	0.070
57	4.75	0.23	0.140	(0.289)	0.070	0.070
58	4.83	0.27	0.160	(0.288)	0.080	0.080
59	4.92	0.27	0.160	(0.287)	0.080	0.080
60	5.00	0.27	0.160	(0.285)	0.080	0.080
61	5.08	0.20	0.120	(0.284)	0.060	0.060
62	5.17	0.20	0.120	(0.283)	0.060	0.060
63	5.25	0.20	0.120	(0.282)	0.060	0.060
64	5.33	0.23	0.140	(0.280)	0.070	0.070
65	5.42	0.23	0.140	(0.279)	0.070	0.070
66	5.50	0.23	0.140	(0.278)	0.070	0.070
67	5.58	0.27	0.160	(0.277)	0.080	0.080
68	5.67	0.27	0.160	(0.275)	0.080	0.080
69	5.75	0.27	0.160	(0.274)	0.080	0.080
70	5.83	0.27	0.160	(0.273)	0.080	0.080
71	5.92	0.27	0.160	(0.272)	0.080	0.080

72	6.00	0.27	0.160	(0.271)	0.080	0.080
73	6.08	0.30	0.180	(0.269)	0.090	0.090
74	6.17	0.30	0.180	(0.268)	0.090	0.090
75	6.25	0.30	0.180	(0.267)	0.090	0.090
76	6.33	0.30	0.180	(0.266)	0.090	0.090
77	6.42	0.30	0.180	(0.265)	0.090	0.090
78	6.50	0.30	0.180	(0.263)	0.090	0.090
79	6.58	0.33	0.200	(0.262)	0.100	0.100
80	6.67	0.33	0.200	(0.261)	0.100	0.100
81	6.75	0.33	0.200	(0.260)	0.100	0.100
82	6.83	0.33	0.200	(0.259)	0.100	0.100
83	6.92	0.33	0.200	(0.258)	0.100	0.100
84	7.00	0.33	0.200	(0.256)	0.100	0.100
85	7.08	0.33	0.200	(0.255)	0.100	0.100
86	7.17	0.33	0.200	(0.254)	0.100	0.100
87	7.25	0.33	0.200	(0.253)	0.100	0.100
88	7.33	0.37	0.220	(0.252)	0.110	0.110
89	7.42	0.37	0.220	(0.251)	0.110	0.110
90	7.50	0.37	0.220	(0.249)	0.110	0.110
91	7.58	0.40	0.240	(0.248)	0.120	0.120
92	7.67	0.40	0.240	(0.247)	0.120	0.120
93	7.75	0.40	0.240	(0.246)	0.120	0.120
94	7.83	0.43	0.260	(0.245)	0.130	0.130
95	7.92	0.43	0.260	(0.244)	0.130	0.130
96	8.00	0.43	0.260	(0.243)	0.130	0.130
97	8.08	0.50	0.300	(0.242)	0.150	0.150
98	8.17	0.50	0.300	(0.240)	0.150	0.150
99	8.25	0.50	0.300	(0.239)	0.150	0.150
100	8.33	0.50	0.300	(0.238)	0.150	0.150
101	8.42	0.50	0.300	(0.237)	0.150	0.150
102	8.50	0.50	0.300	(0.236)	0.150	0.150
103	8.58	0.53	0.320	(0.235)	0.160	0.160
104	8.67	0.53	0.320	(0.234)	0.160	0.160
105	8.75	0.53	0.320	(0.233)	0.160	0.160
106	8.83	0.57	0.340	(0.232)	0.170	0.170
107	8.92	0.57	0.340	(0.230)	0.170	0.170
108	9.00	0.57	0.340	(0.229)	0.170	0.170
109	9.08	0.63	0.380	(0.228)	0.190	0.190
110	9.17	0.63	0.380	(0.227)	0.190	0.190
111	9.25	0.63	0.380	(0.226)	0.190	0.190
112	9.33	0.67	0.400	(0.225)	0.200	0.200
113	9.42	0.67	0.400	(0.224)	0.200	0.200
114	9.50	0.67	0.400	(0.223)	0.200	0.200
115	9.58	0.70	0.420	(0.222)	0.210	0.210
116	9.67	0.70	0.420	(0.221)	0.210	0.210
117	9.75	0.70	0.420	(0.220)	0.210	0.210
118	9.83	0.73	0.440	0.219	(0.220)	0.221
119	9.92	0.73	0.440	0.218	(0.220)	0.222
120	10.00	0.73	0.440	0.217	(0.220)	0.223
121	10.08	0.50	0.300	(0.215)	0.150	0.150
122	10.17	0.50	0.300	(0.214)	0.150	0.150
123	10.25	0.50	0.300	(0.213)	0.150	0.150
124	10.33	0.50	0.300	(0.212)	0.150	0.150
125	10.42	0.50	0.300	(0.211)	0.150	0.150
126	10.50	0.50	0.300	(0.210)	0.150	0.150
127	10.58	0.67	0.400	(0.209)	0.200	0.200
128	10.67	0.67	0.400	(0.208)	0.200	0.200
129	10.75	0.67	0.400	(0.207)	0.200	0.200
130	10.83	0.67	0.400	(0.206)	0.200	0.200
131	10.92	0.67	0.400	(0.205)	0.200	0.200
132	11.00	0.67	0.400	(0.204)	0.200	0.200
133	11.08	0.63	0.380	(0.203)	0.190	0.190
134	11.17	0.63	0.380	(0.202)	0.190	0.190
135	11.25	0.63	0.380	(0.201)	0.190	0.190
136	11.33	0.63	0.380	(0.200)	0.190	0.190
137	11.42	0.63	0.380	(0.199)	0.190	0.190
138	11.50	0.63	0.380	(0.198)	0.190	0.190
139	11.58	0.57	0.340	(0.197)	0.170	0.170
140	11.67	0.57	0.340	(0.196)	0.170	0.170
141	11.75	0.57	0.340	(0.195)	0.170	0.170
142	11.83	0.60	0.360	(0.194)	0.180	0.180
143	11.92	0.60	0.360	(0.193)	0.180	0.180
144	12.00	0.60	0.360	(0.192)	0.180	0.180
145	12.08	0.83	0.500	0.191	(0.250)	0.309
146	12.17	0.83	0.500	0.190	(0.250)	0.310
147	12.25	0.83	0.500	0.189	(0.250)	0.310
148	12.33	0.87	0.520	0.189	(0.260)	0.331
149	12.42	0.87	0.520	0.188	(0.260)	0.332
150	12.50	0.87	0.520	0.187	(0.260)	0.333
151	12.58	0.93	0.560	0.186	(0.280)	0.374
152	12.67	0.93	0.560	0.185	(0.280)	0.375
153	12.75	0.93	0.560	0.184	(0.280)	0.376
154	12.83	0.97	0.580	0.183	(0.290)	0.397
155	12.92	0.97	0.580	0.182	(0.290)	0.398
156	13.00	0.97	0.580	0.181	(0.290)	0.399
157	13.08	1.13	0.680	0.180	(0.340)	0.500

158	13.17	1.13	0.680		0.179	(0.340)	0.501
159	13.25	1.13	0.680		0.178	(0.340)	0.502
160	13.33	1.13	0.680		0.177	(0.340)	0.503
161	13.42	1.13	0.680		0.177	(0.340)	0.503
162	13.50	1.13	0.680		0.176	(0.340)	0.504
163	13.58	0.77	0.460		0.175	(0.230)	0.285
164	13.67	0.77	0.460		0.174	(0.230)	0.286
165	13.75	0.77	0.460		0.173	(0.230)	0.287
166	13.83	0.77	0.460		0.172	(0.230)	0.288
167	13.92	0.77	0.460		0.171	(0.230)	0.289
168	14.00	0.77	0.460		0.170	(0.230)	0.290
169	14.08	0.90	0.540		0.169	(0.270)	0.371
170	14.17	0.90	0.540		0.169	(0.270)	0.371
171	14.25	0.90	0.540		0.168	(0.270)	0.372
172	14.33	0.87	0.520		0.167	(0.260)	0.353
173	14.42	0.87	0.520		0.166	(0.260)	0.354
174	14.50	0.87	0.520		0.165	(0.260)	0.355
175	14.58	0.87	0.520		0.164	(0.260)	0.356
176	14.67	0.87	0.520		0.163	(0.260)	0.357
177	14.75	0.87	0.520		0.163	(0.260)	0.357
178	14.83	0.83	0.500		0.162	(0.250)	0.338
179	14.92	0.83	0.500		0.161	(0.250)	0.339
180	15.00	0.83	0.500		0.160	(0.250)	0.340
181	15.08	0.80	0.480		0.159	(0.240)	0.321
182	15.17	0.80	0.480		0.159	(0.240)	0.321
183	15.25	0.80	0.480		0.158	(0.240)	0.322
184	15.33	0.77	0.460		0.157	(0.230)	0.303
185	15.42	0.77	0.460		0.156	(0.230)	0.304
186	15.50	0.77	0.460		0.155	(0.230)	0.305
187	15.58	0.63	0.380		0.154	(0.190)	0.225
188	15.67	0.63	0.380		0.154	(0.190)	0.226
189	15.75	0.63	0.380		0.153	(0.190)	0.227
190	15.83	0.63	0.380		0.152	(0.190)	0.228
191	15.92	0.63	0.380		0.151	(0.190)	0.229
192	16.00	0.63	0.380		0.151	(0.190)	0.229
193	16.08	0.13	0.080	(0.150)		0.040	0.040
194	16.17	0.13	0.080	(0.149)		0.040	0.040
195	16.25	0.13	0.080	(0.148)		0.040	0.040
196	16.33	0.13	0.080	(0.148)		0.040	0.040
197	16.42	0.13	0.080	(0.147)		0.040	0.040
198	16.50	0.13	0.080	(0.146)		0.040	0.040
199	16.58	0.10	0.060	(0.145)		0.030	0.030
200	16.67	0.10	0.060	(0.145)		0.030	0.030
201	16.75	0.10	0.060	(0.144)		0.030	0.030
202	16.83	0.10	0.060	(0.143)		0.030	0.030
203	16.92	0.10	0.060	(0.142)		0.030	0.030
204	17.00	0.10	0.060	(0.142)		0.030	0.030
205	17.08	0.17	0.100	(0.141)		0.050	0.050
206	17.17	0.17	0.100	(0.140)		0.050	0.050
207	17.25	0.17	0.100	(0.140)		0.050	0.050
208	17.33	0.17	0.100	(0.139)		0.050	0.050
209	17.42	0.17	0.100	(0.138)		0.050	0.050
210	17.50	0.17	0.100	(0.137)		0.050	0.050
211	17.58	0.17	0.100	(0.137)		0.050	0.050
212	17.67	0.17	0.100	(0.136)		0.050	0.050
213	17.75	0.17	0.100	(0.135)		0.050	0.050
214	17.83	0.13	0.080	(0.135)		0.040	0.040
215	17.92	0.13	0.080	(0.134)		0.040	0.040
216	18.00	0.13	0.080	(0.133)		0.040	0.040
217	18.08	0.13	0.080	(0.133)		0.040	0.040
218	18.17	0.13	0.080	(0.132)		0.040	0.040
219	18.25	0.13	0.080	(0.131)		0.040	0.040
220	18.33	0.13	0.080	(0.131)		0.040	0.040
221	18.42	0.13	0.080	(0.130)		0.040	0.040
222	18.50	0.13	0.080	(0.130)		0.040	0.040
223	18.58	0.10	0.060	(0.129)		0.030	0.030
224	18.67	0.10	0.060	(0.128)		0.030	0.030
225	18.75	0.10	0.060	(0.128)		0.030	0.030
226	18.83	0.07	0.040	(0.127)		0.020	0.020
227	18.92	0.07	0.040	(0.126)		0.020	0.020
228	19.00	0.07	0.040	(0.126)		0.020	0.020
229	19.08	0.10	0.060	(0.125)		0.030	0.030
230	19.17	0.10	0.060	(0.125)		0.030	0.030
231	19.25	0.10	0.060	(0.124)		0.030	0.030
232	19.33	0.13	0.080	(0.123)		0.040	0.040
233	19.42	0.13	0.080	(0.123)		0.040	0.040
234	19.50	0.13	0.080	(0.122)		0.040	0.040
235	19.58	0.10	0.060	(0.122)		0.030	0.030
236	19.67	0.10	0.060	(0.121)		0.030	0.030
237	19.75	0.10	0.060	(0.121)		0.030	0.030
238	19.83	0.07	0.040	(0.120)		0.020	0.020
239	19.92	0.07	0.040	(0.120)		0.020	0.020
240	20.00	0.07	0.040	(0.119)		0.020	0.020
241	20.08	0.10	0.060	(0.119)		0.030	0.030
242	20.17	0.10	0.060	(0.118)		0.030	0.030
243	20.25	0.10	0.060	(0.118)		0.030	0.030

244	20.33	0.10	0.060	(0.117)	0.030	0.030
245	20.42	0.10	0.060	(0.116)	0.030	0.030
246	20.50	0.10	0.060	(0.116)	0.030	0.030
247	20.58	0.10	0.060	(0.116)	0.030	0.030
248	20.67	0.10	0.060	(0.115)	0.030	0.030
249	20.75	0.10	0.060	(0.115)	0.030	0.030
250	20.83	0.07	0.040	(0.114)	0.020	0.020
251	20.92	0.07	0.040	(0.114)	0.020	0.020
252	21.00	0.07	0.040	(0.113)	0.020	0.020
253	21.08	0.10	0.060	(0.113)	0.030	0.030
254	21.17	0.10	0.060	(0.112)	0.030	0.030
255	21.25	0.10	0.060	(0.112)	0.030	0.030
256	21.33	0.07	0.040	(0.111)	0.020	0.020
257	21.42	0.07	0.040	(0.111)	0.020	0.020
258	21.50	0.07	0.040	(0.111)	0.020	0.020
259	21.58	0.10	0.060	(0.110)	0.030	0.030
260	21.67	0.10	0.060	(0.110)	0.030	0.030
261	21.75	0.10	0.060	(0.109)	0.030	0.030
262	21.83	0.07	0.040	(0.109)	0.020	0.020
263	21.92	0.07	0.040	(0.109)	0.020	0.020
264	22.00	0.07	0.040	(0.108)	0.020	0.020
265	22.08	0.10	0.060	(0.108)	0.030	0.030
266	22.17	0.10	0.060	(0.108)	0.030	0.030
267	22.25	0.10	0.060	(0.107)	0.030	0.030
268	22.33	0.07	0.040	(0.107)	0.020	0.020
269	22.42	0.07	0.040	(0.107)	0.020	0.020
270	22.50	0.07	0.040	(0.106)	0.020	0.020
271	22.58	0.07	0.040	(0.106)	0.020	0.020
272	22.67	0.07	0.040	(0.106)	0.020	0.020
273	22.75	0.07	0.040	(0.105)	0.020	0.020
274	22.83	0.07	0.040	(0.105)	0.020	0.020
275	22.92	0.07	0.040	(0.105)	0.020	0.020
276	23.00	0.07	0.040	(0.105)	0.020	0.020
277	23.08	0.07	0.040	(0.104)	0.020	0.020
278	23.17	0.07	0.040	(0.104)	0.020	0.020
279	23.25	0.07	0.040	(0.104)	0.020	0.020
280	23.33	0.07	0.040	(0.104)	0.020	0.020
281	23.42	0.07	0.040	(0.103)	0.020	0.020
282	23.50	0.07	0.040	(0.103)	0.020	0.020
283	23.58	0.07	0.040	(0.103)	0.020	0.020
284	23.67	0.07	0.040	(0.103)	0.020	0.020
285	23.75	0.07	0.040	(0.103)	0.020	0.020
286	23.83	0.07	0.040	(0.103)	0.020	0.020
287	23.92	0.07	0.040	(0.103)	0.020	0.020
288	24.00	0.07	0.040	(0.103)	0.020	0.020

(Loss Rate Not Used)

Sum = 100.0 Sum = 34.2

Flood volume = Effective rainfall 2.85(In)
times area 28.4(Ac.)/[(In)/(Ft.)] = 6.7(Ac.Ft)
Total soil loss = 2.15(In)
Total soil loss = 5.101(Ac.Ft)
Total rainfall = 5.00(In)
Flood volume = 293797.2 Cubic Feet
Total soil loss = 222178.7 Cubic Feet

Peak flow rate of this hydrograph = 14.437(CFS)

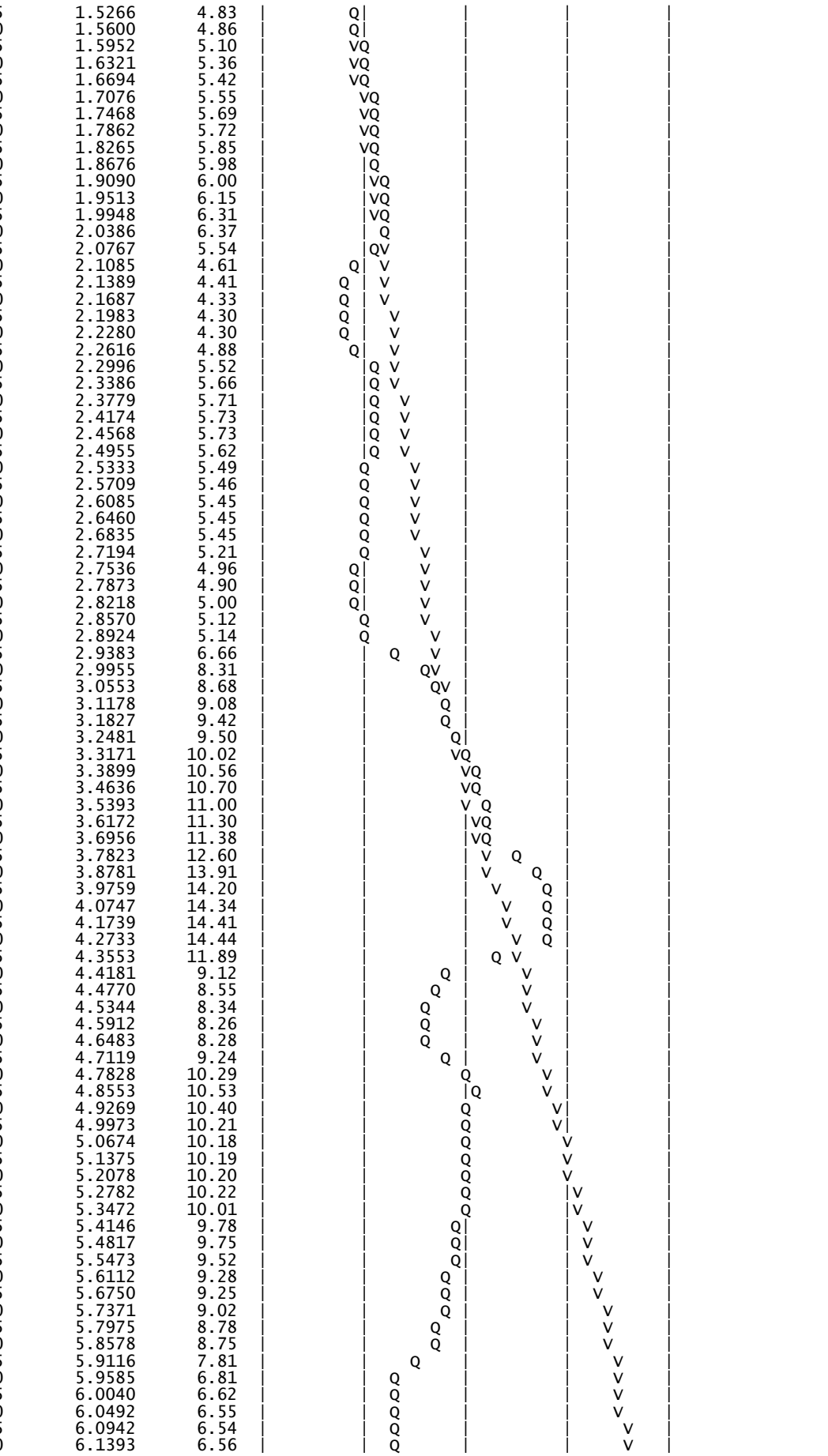
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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0016	0.23	Q				
0+10	0.0050	0.49	Q				
0+15	0.0087	0.54	VQ				
0+20	0.0134	0.68	VQ				
0+25	0.0190	0.82	VQ				
0+30	0.0248	0.84	VQ				
0+35	0.0307	0.86	VQ				
0+40	0.0366	0.86	VQ				
0+45	0.0426	0.86	VQ				
0+50	0.0493	0.98	VQ				
0+55	0.0569	1.10	V Q				
1+ 0	0.0647	1.13	V Q				
1+ 5	0.0717	1.03	V Q				
1+10	0.0780	0.90	VQ				
1+15	0.0840	0.88	VQ				
1+20	0.0900	0.86	VQ				
1+25	0.0959	0.86	VQ				
1+30	0.1018	0.86	VQ				
1+35	0.1077	0.86	VQ				
1+40	0.1136	0.86	VQ				

1+45	0.1196	0.86	VQ	|	|	|	|
1+50	0.1263	0.98	VQ	|	|	|	|
1+55	0.1339	1.10	V Q	|	|	|	|
2+ 0	0.1417	1.13	V Q	|	|	|	|
2+ 5	0.1495	1.14	V Q	|	|	|	|
2+10	0.1574	1.15	V Q	|	|	|	|
2+15	0.1653	1.15	V Q	|	|	|	|
2+20	0.1732	1.15	|VQ	|	|	|	|
2+25	0.1811	1.15	|VQ	|	|	|	|
2+30	0.1890	1.15	|VQ	|	|	|	|
2+35	0.1977	1.26	|VQ	|	|	|	|
2+40	0.2073	1.39	|VQ	|	|	|	|
2+45	0.2171	1.42	|VQ	|	|	|	|
2+50	0.2269	1.43	|VQ	|	|	|	|
2+55	0.2368	1.43	|VQ	|	|	|	|
3+ 0	0.2467	1.43	|VQ	|	|	|	|
3+ 5	0.2565	1.43	|VQ	|	|	|	|
3+10	0.2664	1.43	|VQ	|	|	|	|
3+15	0.2763	1.43	|VQ	|	|	|	|
3+20	0.2861	1.43	|VQ	|	|	|	|
3+25	0.2960	1.43	|VQ	|	|	|	|
3+30	0.3059	1.43	|VQ	|	|	|	|
3+35	0.3158	1.43	|VQ	|	|	|	|
3+40	0.3256	1.43	|VQ	|	|	|	|
3+45	0.3355	1.43	|VQ	|	|	|	|
3+50	0.3462	1.55	| VQ	|	|	|	|
3+55	0.3577	1.68	| VQ	|	|	|	|
4+ 0	0.3695	1.70	| VQ	|	|	|	|
4+ 5	0.3813	1.72	| VQ	|	|	|	|
4+10	0.3931	1.72	| VQ	|	|	|	|
4+15	0.4050	1.72	| VQ	|	|	|	|
4+20	0.4176	1.84	| VQ	|	|	|	|
4+25	0.4311	1.96	| VQ	|	|	|	|
4+30	0.4448	1.99	| VQ	|	|	|	|
4+35	0.4586	2.00	| V Q	|	|	|	|
4+40	0.4725	2.01	| V Q	|	|	|	|
4+45	0.4863	2.01	| V Q	|	|	|	|
4+50	0.5009	2.12	| V Q	|	|	|	|
4+55	0.5164	2.25	| VQ	|	|	|	|
5+ 0	0.5321	2.28	| VQ	|	|	|	|
5+ 5	0.5462	2.06	| VQ	|	|	|	|
5+10	0.5587	1.81	| Q	|	|	|	|
5+15	0.5707	1.75	| Q	|	|	|	|
5+20	0.5834	1.85	| Q	|	|	|	|
5+25	0.5970	1.96	| Q	|	|	|	|
5+30	0.6107	1.99	| Q	|	|	|	|
5+35	0.6253	2.12	| VQ	|	|	|	|
5+40	0.6408	2.25	| VQ	|	|	|	|
5+45	0.6565	2.28	| VQ	|	|	|	|
5+50	0.6722	2.29	| VQ	|	|	|	|
5+55	0.6880	2.29	| Q	|	|	|	|
6+ 0	0.7038	2.29	| Q	|	|	|	|
6+ 5	0.7204	2.41	| Q	|	|	|	|
6+10	0.7379	2.54	| VQ	|	|	|	|
6+15	0.7555	2.56	| VQ	|	|	|	|
6+20	0.7733	2.58	| VQ	|	|	|	|
6+25	0.7910	2.58	| VQ	|	|	|	|
6+30	0.8088	2.58	| VQ	|	|	|	|
6+35	0.8274	2.70	| VQ	|	|	|	|
6+40	0.8468	2.82	| Q	|	|	|	|
6+45	0.8665	2.85	| Q	|	|	|	|
6+50	0.8862	2.86	| Q	|	|	|	|
6+55	0.9059	2.87	| Q	|	|	|	|
7+ 0	0.9257	2.87	| Q	|	|	|	|
7+ 5	0.9454	2.87	| Q	|	|	|	|
7+10	0.9651	2.87	| Q	|	|	|	|
7+15	0.9849	2.87	| Q	|	|	|	|
7+20	1.0054	2.98	| Q	|	|	|	|
7+25	1.0269	3.11	| Q	|	|	|	|
7+30	1.0485	3.14	| Q	|	|	|	|
7+35	1.0709	3.27	| Q	|	|	|	|
7+40	1.0943	3.40	| Q	|	|	|	|
7+45	1.1179	3.42	| Q	|	|	|	|
7+50	1.1424	3.55	| VQ	|	|	|	|
7+55	1.1678	3.68	| VQ	|	|	|	|
8+ 0	1.1933	3.71	| Q	|	|	|	|
8+ 5	1.2206	3.96	| Q	|	|	|	|
8+10	1.2496	4.21	| VQ	|	|	|	|
8+15	1.2790	4.27	| VQ	|	|	|	|
8+20	1.3085	4.29	| VQ	|	|	|	|
8+25	1.3381	4.30	| VQ	|	|	|	|
8+30	1.3678	4.30	| Q	|	|	|	|
8+35	1.3982	4.42	| Q	|	|	|	|
8+40	1.4295	4.54	| VQ	|	|	|	|
8+45	1.4609	4.57	| VQ	|	|	|	|
8+50	1.4933	4.70	| VQ	|	|	|	|

8+55	1.5266	4.83	
9+ 0	1.5600	4.86	
9+ 5	1.5952	5.10	
9+10	1.6321	5.36	
9+15	1.6694	5.42	
9+20	1.7076	5.55	
9+25	1.7468	5.69	
9+30	1.7862	5.72	
9+35	1.8265	5.85	
9+40	1.8676	5.98	
9+45	1.9090	6.00	
9+50	1.9513	6.15	
9+55	1.9948	6.31	
10+ 0	2.0386	6.37	
10+ 5	2.0767	5.54	
10+10	2.1085	4.61	
10+15	2.1389	4.41	
10+20	2.1687	4.33	
10+25	2.1983	4.30	
10+30	2.2280	4.30	
10+35	2.2616	4.88	
10+40	2.2996	5.52	
10+45	2.3386	5.66	
10+50	2.3779	5.71	
10+55	2.4174	5.73	
11+ 0	2.4568	5.73	
11+ 5	2.4955	5.62	
11+10	2.5333	5.49	
11+15	2.5709	5.46	
11+20	2.6085	5.45	
11+25	2.6460	5.45	
11+30	2.6835	5.45	
11+35	2.7194	5.21	
11+40	2.7536	4.96	
11+45	2.7873	4.90	
11+50	2.8218	5.00	
11+55	2.8570	5.12	
12+ 0	2.8924	5.14	
12+ 5	2.9383	6.66	
12+10	2.9955	8.31	
12+15	3.0553	8.68	
12+20	3.1178	9.08	
12+25	3.1827	9.42	
12+30	3.2481	9.50	
12+35	3.3171	10.02	
12+40	3.3899	10.56	
12+45	3.4636	10.70	
12+50	3.5393	11.00	
12+55	3.6172	11.30	
13+ 0	3.6956	11.38	
13+ 5	3.7823	12.60	
13+10	3.8781	13.91	
13+15	3.9759	14.20	
13+20	4.0747	14.34	
13+25	4.1739	14.41	
13+30	4.2733	14.44	
13+35	4.3553	11.89	
13+40	4.4181	9.12	
13+45	4.4770	8.55	
13+50	4.5344	8.34	
13+55	4.5912	8.26	
14+ 0	4.6483	8.28	
14+ 5	4.7119	9.24	
14+10	4.7828	10.29	
14+15	4.8553	10.53	
14+20	4.9269	10.40	
14+25	4.9973	10.21	
14+30	5.0674	10.18	
14+35	5.1375	10.19	
14+40	5.2078	10.20	
14+45	5.2782	10.22	
14+50	5.3472	10.01	
14+55	5.4146	9.78	
15+ 0	5.4817	9.75	
15+ 5	5.5473	9.52	
15+10	5.6112	9.28	
15+15	5.6750	9.25	
15+20	5.7371	9.02	
15+25	5.7975	8.78	
15+30	5.8578	8.75	
15+35	5.9116	7.81	
15+40	5.9585	6.81	
15+45	6.0040	6.62	
15+50	6.0492	6.55	
15+55	6.0942	6.54	
16+ 0	6.1393	6.56	

16+ 5	6.1694	4.36	Q	|	|	|	V |
16+10	6.1828	1.95	Q	|	|	|	V |
16+15	6.1928	1.44	Q	|	|	|	V |
16+20	6.2013	1.24	Q	|	|	|	V |
16+25	6.2092	1.15	Q	|	|	|	V |
16+30	6.2171	1.15	Q	|	|	|	V |
16+35	6.2241	1.03	Q	|	|	|	V |
16+40	6.2304	0.90	Q	|	|	|	V |
16+45	6.2364	0.88	Q	|	|	|	V |
16+50	6.2423	0.86	Q	|	|	|	V |
16+55	6.2483	0.86	Q	|	|	|	V |
17+ 0	6.2542	0.86	Q	|	|	|	V |
17+ 5	6.2617	1.09	Q	|	|	|	V |
17+10	6.2710	1.35	Q	|	|	|	V |
17+15	6.2807	1.40	Q	|	|	|	V |
17+20	6.2905	1.42	Q	|	|	|	V |
17+25	6.3003	1.43	Q	|	|	|	V |
17+30	6.3102	1.43	Q	|	|	|	V |
17+35	6.3201	1.43	Q	|	|	|	V |
17+40	6.3300	1.43	Q	|	|	|	V |
17+45	6.3398	1.43	Q	|	|	|	V |
17+50	6.3489	1.32	Q	|	|	|	V |
17+55	6.3571	1.19	Q	|	|	|	V |
18+ 0	6.3651	1.16	Q	|	|	|	V |
18+ 5	6.3730	1.15	Q	|	|	|	V |
18+10	6.3809	1.15	Q	|	|	|	V |
18+15	6.3888	1.15	Q	|	|	|	V |
18+20	6.3967	1.15	Q	|	|	|	V |
18+25	6.4046	1.15	Q	|	|	|	V |
18+30	6.4125	1.15	Q	|	|	|	V |
18+35	6.4196	1.03	Q	|	|	|	V |
18+40	6.4258	0.90	Q	|	|	|	V |
18+45	6.4318	0.88	Q	|	|	|	V |
18+50	6.4370	0.75	Q	|	|	|	V |
18+55	6.4412	0.62	Q	|	|	|	V |
19+ 0	6.4453	0.59	Q	|	|	|	V |
19+ 5	6.4501	0.69	Q	|	|	|	V |
19+10	6.4557	0.82	Q	|	|	|	V |
19+15	6.4615	0.84	Q	|	|	|	V |
19+20	6.4682	0.97	Q	|	|	|	V |
19+25	6.4758	1.10	Q	|	|	|	V |
19+30	6.4836	1.13	Q	|	|	|	V |
19+35	6.4907	1.03	Q	|	|	|	V |
19+40	6.4969	0.90	Q	|	|	|	V |
19+45	6.5029	0.88	Q	|	|	|	V |
19+50	6.5081	0.75	Q	|	|	|	V |
19+55	6.5123	0.62	Q	|	|	|	V |
20+ 0	6.5164	0.59	Q	|	|	|	V |
20+ 5	6.5211	0.69	Q	|	|	|	V |
20+10	6.5268	0.82	Q	|	|	|	V |
20+15	6.5326	0.84	Q	|	|	|	V |
20+20	6.5385	0.86	Q	|	|	|	V |
20+25	6.5444	0.86	Q	|	|	|	V |
20+30	6.5503	0.86	Q	|	|	|	V |
20+35	6.5562	0.86	Q	|	|	|	V |
20+40	6.5622	0.86	Q	|	|	|	V |
20+45	6.5681	0.86	Q	|	|	|	V |
20+50	6.5732	0.74	Q	|	|	|	V |
20+55	6.5774	0.62	Q	|	|	|	V|
21+ 0	6.5815	0.59	Q	|	|	|	V|
21+ 5	6.5863	0.69	Q	|	|	|	V|
21+10	6.5919	0.82	Q	|	|	|	V|
21+15	6.5977	0.84	Q	|	|	|	V|
21+20	6.6028	0.74	Q	|	|	|	V|
21+25	6.6071	0.62	Q	|	|	|	V|
21+30	6.6111	0.59	Q	|	|	|	V|
21+35	6.6159	0.69	Q	|	|	|	V|
21+40	6.6215	0.82	Q	|	|	|	V|
21+45	6.6273	0.84	Q	|	|	|	V|
21+50	6.6324	0.74	Q	|	|	|	V|
21+55	6.6367	0.62	Q	|	|	|	V|
22+ 0	6.6407	0.59	Q	|	|	|	V|
22+ 5	6.6455	0.69	Q	|	|	|	V|
22+10	6.6511	0.82	Q	|	|	|	V|
22+15	6.6570	0.84	Q	|	|	|	V|
22+20	6.6620	0.74	Q	|	|	|	V|
22+25	6.6663	0.62	Q	|	|	|	V|
22+30	6.6703	0.59	Q	|	|	|	V|
22+35	6.6743	0.58	Q	|	|	|	V|
22+40	6.6783	0.57	Q	|	|	|	V|
22+45	6.6822	0.57	Q	|	|	|	V|
22+50	6.6862	0.57	Q	|	|	|	V|
22+55	6.6901	0.57	Q	|	|	|	V|
23+ 0	6.6941	0.57	Q	|	|	|	V|
23+ 5	6.6980	0.57	Q	|	|	|	V|
23+10	6.7020	0.57	Q	|	|	|	V|

```
   23+15       6.7059      0.57  |Q        |         |         |        v|
   23+20       6.7099      0.57  |Q        |         |         |        v|
   23+25       6.7138      0.57  |Q        |         |         |        v|
   23+30       6.7178      0.57  |Q        |         |         |        v|
   23+35       6.7217      0.57  |Q        |         |         |        v|
   23+40       6.7257      0.57  |Q        |         |         |        v|
   23+45       6.7296      0.57  |Q        |         |         |        v|
   23+50       6.7336      0.57  |Q        |         |         |        v|
   23+55       6.7375      0.57  |Q        |         |         |        v|
   24+ 0       6.7414      0.57  |Q        |         |         |        v|
   24+ 5       6.7438      0.34  Q         |         |         |        v|
   24+10       6.7444      0.09  Q         |         |         |        v|
   24+15       6.7446      0.03  Q         |         |         |        v|
   24+20       6.7447      0.01  Q         |         |         |         v
-------------------------------------------------------------------------
```

PROPOSED UNIT HYDROGRAPH MAP


PRO
L=1871
28.43
C
100
1428
101
1349
LOT 78
O.S.
LOT=31,419 SF
LOT 79
O.S.
LOT=35,434 SF
LOT 74
WQ EDB
LOT=81,423 SF
LOW FLOW TRENCH
FOREBAY
Q10=34.71CFS
Q100=56.71CFS
BOTTOM STAGE
SPILLWAY
LOT 76
O.S.
LOT=184,327 SF
LOT 75
O.S.
LOT=60,591 SF
20' WMWD EASEMENT
STREET A
STREET B
STREET C
STREET D
STREET E
STREET F
STREET G
Q10=4.70CFS
Q100=7.66CFS
Q10=5.83CFS
Q100=9.42CFS
Q10=12.39CFS
Q100=20.35CFS
Q10=7.48CFS
Q100=12.26CFS
Q10=17.27CFS
Q100=27.27CFS
Q10=11.27CFS
Q100=21.27CFS
1 LOT=11,200 SF PAD=10,065 SF PE=1385
2 LOT=11,079 SF PAD=9,456 SF PE=1380
3 LOT=11,200 SF PAD=9,902 SF PE=1388
4 LOT=11,209 SF PAD=9,902 SF PE=1388
5 LOT=10,869 SF PAD=9,624 SF PE=1392
6 LOT=10,102 SF PAD=9,290 SF PE=1396
7 LOT=12,532 SF PAD=11,335 SF PE=1399
8 LOT=17,983SF PAD=8,617 SF PE=1401
9 LOT=10,027SF PAD=8,727 SF PE=1395
10 LOT=12,533 SF PAD=9,163 SF PE=1390
11 LOT=14,905 SF PAD=9,163 SF PE=1392
12 LOT=14,287 SF PAD=8,179 SF PE=1392
13 LOT=12,804 SF PAD=8,110 SF PE=1394
14 LOT=12,460 SF PAD=8,114 SF PE=1395
15 LOT=13,208 SF PAD=9,097 SF PE=1397
16 LOT=12,275 SF PAD=9,203 SF PE=1399
17 LOT=12,008 SF PAD=9,268 SF PE=1414
18 LOT=10,301 SF PAD=9,469 SF PE=1416
19 LOT=10,486 SF PAD=9,777 SF PE=1419
20 LOT=12,887 SF PAD=13,105 SF PE=1422
21 LOT=10,007 SF PAD=9,386 SF PE=1419
22 LOT=10,010 SF PAD=8,864 SF PE=1416
23 LOT=11,095 SF PAD=10,233 SF PE=1414
24 LOT=13,737 SF PAD=12,574 SF PE=1412
25 LOT=11,120 SF PAD=10,032 SF PE=1409
26 LOT=13,406 SF PAD=11,054 SF PE=1404
27 LOT=10,848 SF PAD=9,175 SF PE=1401
28 LOT=12,256 SF PAD=10,521 SF PE=1403
29 LOT=10,454 SF PAD=9,963 SF PE=1407
30 LOT=12,108 SF PAD=11,122 SF PE=1408
31 LOT=11,822 SF PAD=11,131 SF PE=1410
32 LOT=10,782 SF PAD=10,816 SF PE=1412
33 LOT=10,782 SF PAD=10,816 SF PE=1412
34 LOT=14,251 SF PAD=14,668 SF PE=1412
35 LOT=14,631 SF PAD=14,263 SF PE=1411
36 LOT=18,080 SF PAD=15,424 SF PE=1410
37 LOT=13,627 SF PAD=11,315 SF PE=1409
38 LOT=12,340 SF PAD=10,117 SF PE=1408
39 LOT=10,693 SF PAD=8,417 SF PE=1407
40 LOT=11,880 SF PAD=9,482 SF PE=1406
41 LOT=11,997 SF PAD=10,157 SF PE=1408
42 LOT=11,757 SF PAD=10,192 SF PE=1410
43 LOT=10,690 SF PAD=10,052 SF PE=1415
44 LOT=11,503 SF PAD=10,654 SF PE=1416
45 LOT=15,210 SF PAD=14,228 SF PE=1417
46 LOT=19,274 SF PAD=18,014 SF PE=1418
47 LOT=16,975 SF PAD=13,265 SF PE=1415
48 LOT=15,909 SF PAD=13,106 SF PE=1414
49 LOT=16,190 SF PAD=15,041 SF PE=1413
50 LOT=16,103 SF PAD=15,485 SF PE=1414
51 LOT=13,562 SF PAD=13,679 SF PE=1414.5
52 LOT=11,868 SF PAD=11,137 SF PE=1415
53 LOT=11,208 SF PAD=10,350 SF PE=1416
54 LOT=11,102 SF PAD=11,063 SF PE=1416
55 LOT=12,623 SF PAD=12,643 SF PE=1415
56 LOT=12,093 SF PAD=11,629 SF PE=1414
57 LOT=14,449 SF PAD=13,003 SF PE=1411
58 LOT=10,848 SF PAD=10,053 SF PE=1409
59 LOT=10,459 SF PAD=8,720 SF PE=1407
60 LOT=11,685 SF PAD=9,358 SF PE=1405
61 LOT=11,758 SF PAD=11,126 SF PE=1404
62 LOT=10,334 SF PAD=9,763 SF PE=1403
63 LOT=10,185 SF PAD=9,494 SF PE=1400
64 LOT=10,284 SF PAD=9,667 SF PE=1399
65 LOT=10,065 SF PAD=9,429 SF PE=1397
66 LOT=10,005 SF PAD=9,706 SF PE=1396
67 LOT=11,712 SF PAD=11,453 SF PE=1395
68 LOT=10,008 SF PAD=9,578 SF PE=1394.5
69 LOT=11,874 SF PAD=11,340 SF PE=1393.5
70 LOT=13,317 SF PAD=12,623 SF PE=1392.5
71 LOT=13,600 SF PAD=13,169 SF PE=1391.5
72 LOT=13,265 SF PAD=11,135 SF PE=1383
73 LOT=19,796 SF PAD=15,214 SF PE=1380
74 LOT=13,678 SF PAD=9,505 SF PE=1374
N68°59'03"W 204.63'
N86°30'12"E 105.69'
N55°00'04"E 263.76'
N68°38'42"E 168.87'
N63°54'46"W 94.16'
N63°54'46"W 68.06'
N63°54'46"W 68.06'
N63°54'46"W 68.06

Appendix E – Basin Routing and Outflow Calculations

Basin Size and Flow Calculations

BASIN

Horiz. : Vert.

4 : 1 = Basin Side Slope

	BASIN PARAMETERS					OUTLET								
Basin Elevation	Depth	Area S.F.	Volume C.F.	Volume AC-FT	Effective Volume AC-FT	Q1 Orifice Plate (cfs)	Q2 Orifice Plate (cfs)	Q3 Orifice Plate (cfs)	Q4 Orifice Plate (cfs)	Q5Orifice Plate (cfs)	Q6 Orifice Plate (cfs)	Q7Orifice Plate (cfs)	Q Weir 1 (cfs)	Q Total (cfs)
1349.00	0.00	11,304.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1350.00	1.00	12,705.00	12,004.50	0.276	0.276	0.133	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.133
1351.00	2.00	14,154.00	25,458.00	0.584	0.584	0.193	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.193
1352.00	3.00	15,701.00	40,507.50	0.930	0.930	0.238	0.000	0.462	0.000	0.000	0.000	0.000	0.000	0.700
1352.50	3.50	16,531.50	48,712.13	1.118	1.118	0.258	0.000	0.566	0.000	0.000	0.000	0.000	0.000	0.824
1353.00	4.00	17,362.00	57,332.00	1.316	1.316	0.276	0.000	0.654	0.000	0.000	0.000	0.000	0.000	0.930
1353.50	4.50	18,270.50	66,542.63	1.528	1.528	0.293	0.000	0.731	0.000	0.000	0.000	0.000	0.000	1.024
1353.75	4.75	18,724.75	71,318.28	1.637	1.637	0.301	0.000	0.766	0.000	0.000	0.000	0.000	0.000	1.068
1354.00	5.00	19,179.00	76,207.50	1.749	1.749	0.309	0.000	0.801	0.000	0.000	0.000	0.000	17.173	18.283
1355.00	6.00	21,093.00	97,191.00	2.231	2.231	0.340	0.000	0.924	0.000	0.000	0.000	0.000	252.391	253.655

SUPPORTING DESIGN PARAMETERS

Orifice Coefficient	0.66	Dia of Orifice	2.20		4.00					
Gravimetric Constant	32.2 ft/s^2	Eff Dia of Orifice	0.1833	0.0000	0.3333	0.0000	0.0000	0.0000	0.0000	
Number of Rows		Area of Orifice	0.0264	0.0000	0.0873	0.0000	0.0000	0.0000	0.0000	
Minimum Orifice Plate Height		Number of Orifeces	1	1	1	1	1	1	1	
Minimum Orifice Plate Width		Elev	1349.1		1351	1352	1352			

Weir	Sharp Crest Weir Coefficient	4	
	Length of Weir	48.00	
	Elev. at Crest of Weir	1353.8	

Q100 Elevation Weir Calc		
Basin Weir Calc		
Crest Wier Elev.	1353.80	
Q100	55.63	cfs
Weir Length	48	
Weir Coeff.	4	
H Weir	0.43786	
Q100 Elevation	**1354.24**	

Q100 Elevation Weir Calc		
Emergency Spillway Weir Calc		
Crest Wier Elev.	1354.25	
Q100	55.63	cfs
Weir Length	85	
Weir Coeff.	4	
H Weir	0.29915	
Q100 Elevation	**1354.55**	

UNIT HYDROGRAPH SUMMARY							
Storm Event	Existing Condition		Developed		Routed Basin		
	Flow (cfs)	Volume (ac.ft.)	Flow (cfs)	Volume (ac.ft.)	Routed Basin Out Flow (cfs)	Storage Volume (ac.ft.)	Depth (ft)
2 Year - 1 Hour	26.924	0.6278	25.921	0.7357	0.393	0.720	2.39
2 Year - 3 Hour	13.297	0.5661	11.612	0.9719	0.685	0.919	2.97
2 Year - 6 Hour	11.651	0.6045	10.033	1.3136	0.862	1.190	3.68
2 Year - 24 Hour	0.942	0.4342	3.509	2.1321	1.002	1.477	4.38
5 Year - 1 Hour	39.661	1.0447	38.649	1.0675	0.772	1.039	3.29
5 Year - 3 Hour	20.450	1.0214	18.702	1.3939	0.929	1.315	4.00
5 Year - 6 Hour	19.222	1.1974	17.368	1.9210	7.086	1.676	4.84
5 Year - 24 Hour	3.864	0.9101	4.970	3.0199	3.870	1.655	4.79
10 Year - 1 Hour	53.004	1.6866	51.576	1.4893	0.989	1.450	4.31
10 Year - 3 Hour	29.569	2.2396	27.216	1.9110	9.236	1.690	4.87
10 Year - 6 Hour	28.658	2.8266	26.296	2.6439	25.327	1.763	5.03
10 Year - 24 Hour	9.264	3.2965	7.094	3.7320	7.051	1.676	4.84
100 Year - 1 Hour	85.010	2.8019	84.206	2.5933	56.831	1.828	5.16
100 Year - 3 Hour	47.544	3.9062	45.284	3.3629	43.957	1.802	5.11
100 Year - 6 Hour	47.683	5.4579	45.417	4.7524	43.291	1.800	5.11
100 Year - 24 Hour	16.607	6.7703	14.437	6.7447	14.381	1.724	4.94

```
                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 05/07/25

------------------------------------------------------------------------



Program License Serial Number 5006

------------------------------------------------------------------------
********************* HYDROGRAPH INFORMATION **********************

               From study/file name: PRO212.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    16
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       25.921 (CFS)
               Total volume =       0.736 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
____________________________________________________________________________

User entry of depth-outflow-storage data
------------------------------------------------------------------------
Total number of inflow hydrograph intervals = 16
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
------------------------------------------------------------------------
------------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
------------------------------------------------------------------------
------------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
------------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.276      0.133      0.276        0.276
   2.000      0.584      0.193      0.583        0.585
   3.000      0.930      0.700      0.928        0.932
   3.500      1.118      0.824      1.115        1.121
   4.000      1.316      0.930      1.313        1.319
   4.500      1.528      1.024      1.524        1.532
   4.750      1.637      1.068      1.633        1.641
   5.000      1.749     18.283      1.686        1.812
   6.000      2.231    253.655      1.358        3.104
------------------------------------------------------------------------
               Hydrograph Detention Basin Routing
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Graph values: 'I'= unit inflow; 'O'=outflow at time shown
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 Time   Inflow  Outflow    Storage                                    Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0       6.5   12.96   19.44   25.92 (Ft.)
 0.083    1.16    0.00      0.004  OI      |      |      |      |      0.01
 0.167    2.73    0.01      0.017  O  I    |      |      |      |      0.06
 0.250    3.41    0.02      0.038  O   I   |      |      |      |      0.14
 0.333    3.81    0.03      0.063  O   I   |      |      |      |      0.23
 0.417    4.19    0.04      0.090  O    I  |      |      |      |      0.33
 0.500    4.75    0.06      0.121  O    I  |      |      |      |      0.44
 0.583    5.39    0.07      0.155  O     I |      |      |      |      0.56
 0.667    6.42    0.09      0.195  O      I|      |      |      |      0.71
 0.750   10.24    0.12      0.252  O       |   I  |      |      |      0.91
 0.833   25.92    0.15      0.376  O       |      |      |      I      1.32
 0.917   24.27    0.19      0.547  O       |      |      |    I |      1.88
 1.000    9.00    0.30      0.660  O       |  I   |      |      |      2.22
 1.083    3.99    0.37      0.702  O   I   |      |      |      |      2.34
 1.167    1.28    0.39      0.718  OI      |      |      |      |      2.39
 1.250    0.23    0.39      0.720  O       |      |      |      |      2.39
 1.333    0.05    0.39      0.719  O       |      |      |      |      2.39
 1.417    0.00    0.39      0.716  O       |      |      |      |      2.38
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1.500	0.00	0.38	0.714	o	|	|	|	2.37
1.583	0.00	0.38	0.711	o	|	|	|	2.37
1.667	0.00	0.38	0.708	o	|	|	|	2.36
1.750	0.00	0.37	0.706	o	|	|	|	2.35
1.833	0.00	0.37	0.703	o	|	|	|	2.34
1.917	0.00	0.36	0.701	o	|	|	|	2.34
2.000	0.00	0.36	0.698	o	|	|	|	2.33
2.083	0.00	0.36	0.696	o	|	|	|	2.32
2.167	0.00	0.35	0.693	o	|	|	|	2.32
2.250	0.00	0.35	0.691	o	|	|	|	2.31
2.333	0.00	0.35	0.689	o	|	|	|	2.30
2.417	0.00	0.34	0.686	o	|	|	|	2.30
2.500	0.00	0.34	0.684	o	|	|	|	2.29
2.583	0.00	0.34	0.681	o	|	|	|	2.28
2.667	0.00	0.33	0.679	o	|	|	|	2.28
2.750	0.00	0.33	0.677	o	|	|	|	2.27
2.833	0.00	0.33	0.675	o	|	|	|	2.26
2.917	0.00	0.32	0.672	o	|	|	|	2.26
3.000	0.00	0.32	0.670	o	|	|	|	2.25
3.083	0.00	0.32	0.668	o	|	|	|	2.24
3.167	0.00	0.31	0.666	o	|	|	|	2.24
3.250	0.00	0.31	0.664	o	|	|	|	2.23
3.333	0.00	0.31	0.662	o	|	|	|	2.22
3.417	0.00	0.30	0.659	o	|	|	|	2.22
3.500	0.00	0.30	0.657	o	|	|	|	2.21
3.583	0.00	0.30	0.655	o	|	|	|	2.21
3.667	0.00	0.29	0.653	o	|	|	|	2.20
3.750	0.00	0.29	0.651	o	|	|	|	2.19
3.833	0.00	0.29	0.649	o	|	|	|	2.19
3.917	0.00	0.29	0.647	o	|	|	|	2.18
4.000	0.00	0.28	0.645	o	|	|	|	2.18
4.083	0.00	0.28	0.643	o	|	|	|	2.17
4.167	0.00	0.28	0.641	o	|	|	|	2.17
4.250	0.00	0.27	0.640	o	|	|	|	2.16
4.333	0.00	0.27	0.638	o	|	|	|	2.16
4.417	0.00	0.27	0.636	o	|	|	|	2.15
4.500	0.00	0.27	0.634	o	|	|	|	2.14
4.583	0.00	0.26	0.632	o	|	|	|	2.14
4.667	0.00	0.26	0.630	o	|	|	|	2.13
4.750	0.00	0.26	0.629	o	|	|	|	2.13
4.833	0.00	0.26	0.627	o	|	|	|	2.12
4.917	0.00	0.25	0.625	o	|	|	|	2.12
5.000	0.00	0.25	0.623	o	|	|	|	2.11
5.083	0.00	0.25	0.622	o	|	|	|	2.11
5.167	0.00	0.25	0.620	o	|	|	|	2.10
5.250	0.00	0.24	0.618	o	|	|	|	2.10
5.333	0.00	0.24	0.617	o	|	|	|	2.09
5.417	0.00	0.24	0.615	o	|	|	|	2.09
5.500	0.00	0.24	0.613	o	|	|	|	2.08
5.583	0.00	0.23	0.612	o	|	|	|	2.08
5.667	0.00	0.23	0.610	o	|	|	|	2.08
5.750	0.00	0.23	0.608	o	|	|	|	2.07
5.833	0.00	0.23	0.607	o	|	|	|	2.07
5.917	0.00	0.22	0.605	o	|	|	|	2.06
6.000	0.00	0.22	0.604	o	|	|	|	2.06
6.083	0.00	0.22	0.602	o	|	|	|	2.05
6.167	0.00	0.22	0.601	o	|	|	|	2.05
6.250	0.00	0.22	0.599	o	|	|	|	2.04
6.333	0.00	0.21	0.598	o	|	|	|	2.04
6.417	0.00	0.21	0.596	o	|	|	|	2.04
6.500	0.00	0.21	0.595	o	|	|	|	2.03
6.583	0.00	0.21	0.593	o	|	|	|	2.03
6.667	0.00	0.20	0.592	o	|	|	|	2.02
6.750	0.00	0.20	0.591	o	|	|	|	2.02
6.833	0.00	0.20	0.589	o	|	|	|	2.02
6.917	0.00	0.20	0.588	o	|	|	|	2.01
7.000	0.00	0.20	0.587	o	|	|	|	2.01
7.083	0.00	0.19	0.585	o	|	|	|	2.00
7.167	0.00	0.19	0.584	o	|	|	|	2.00
7.250	0.00	0.19	0.583	o	|	|	|	2.00
7.333	0.00	0.19	0.581	o	|	|	|	1.99
7.417	0.00	0.19	0.580	o	|	|	|	1.99
7.500	0.00	0.19	0.579	o	|	|	|	1.98
7.583	0.00	0.19	0.577	o	|	|	|	1.98
7.667	0.00	0.19	0.576	o	|	|	|	1.97
7.750	0.00	0.19	0.575	o	|	|	|	1.97
7.833	0.00	0.19	0.573	o	|	|	|	1.97
7.917	0.00	0.19	0.572	o	|	|	|	1.96
8.000	0.00	0.19	0.571	o	|	|	|	1.96
8.083	0.00	0.19	0.569	o	|	|	|	1.95
8.167	0.00	0.19	0.568	o	|	|	|	1.95
8.250	0.00	0.19	0.567	o	|	|	|	1.94
8.333	0.00	0.19	0.565	o	|	|	|	1.94
8.417	0.00	0.19	0.564	o	|	|	|	1.94
8.500	0.00	0.19	0.563	o	|	|	|	1.93
8.583	0.00	0.19	0.562	o	|	|	|	1.93

8.667	0.00	0.19	0.560	o	|	|	|	|	1.92
8.750	0.00	0.19	0.559	o	|	|	|	|	1.92
8.833	0.00	0.19	0.558	o	|	|	|	|	1.91
8.917	0.00	0.19	0.556	o	|	|	|	|	1.91
9.000	0.00	0.19	0.555	o	|	|	|	|	1.91
9.083	0.00	0.19	0.554	o	|	|	|	|	1.90
9.167	0.00	0.19	0.552	o	|	|	|	|	1.90
9.250	0.00	0.19	0.551	o	|	|	|	|	1.89
9.333	0.00	0.19	0.550	o	|	|	|	|	1.89
9.417	0.00	0.19	0.549	o	|	|	|	|	1.89
9.500	0.00	0.19	0.547	o	|	|	|	|	1.88
9.583	0.00	0.19	0.546	o	|	|	|	|	1.88
9.667	0.00	0.19	0.545	o	|	|	|	|	1.87
9.750	0.00	0.19	0.543	o	|	|	|	|	1.87
9.833	0.00	0.18	0.542	o	|	|	|	|	1.86
9.917	0.00	0.18	0.541	o	|	|	|	|	1.86
10.000	0.00	0.18	0.540	o	|	|	|	|	1.86
10.083	0.00	0.18	0.538	o	|	|	|	|	1.85
10.167	0.00	0.18	0.537	o	|	|	|	|	1.85
10.250	0.00	0.18	0.536	o	|	|	|	|	1.84
10.333	0.00	0.18	0.535	o	|	|	|	|	1.84
10.417	0.00	0.18	0.533	o	|	|	|	|	1.84
10.500	0.00	0.18	0.532	o	|	|	|	|	1.83
10.583	0.00	0.18	0.531	o	|	|	|	|	1.83
10.667	0.00	0.18	0.530	o	|	|	|	|	1.82
10.750	0.00	0.18	0.528	o	|	|	|	|	1.82
10.833	0.00	0.18	0.527	o	|	|	|	|	1.82
10.917	0.00	0.18	0.526	o	|	|	|	|	1.81
11.000	0.00	0.18	0.525	o	|	|	|	|	1.81
11.083	0.00	0.18	0.523	o	|	|	|	|	1.80
11.167	0.00	0.18	0.522	o	|	|	|	|	1.80
11.250	0.00	0.18	0.521	o	|	|	|	|	1.79
11.333	0.00	0.18	0.520	o	|	|	|	|	1.79
11.417	0.00	0.18	0.518	o	|	|	|	|	1.79
11.500	0.00	0.18	0.517	o	|	|	|	|	1.78
11.583	0.00	0.18	0.516	o	|	|	|	|	1.78
11.667	0.00	0.18	0.515	o	|	|	|	|	1.77
11.750	0.00	0.18	0.513	o	|	|	|	|	1.77
11.833	0.00	0.18	0.512	o	|	|	|	|	1.77
11.917	0.00	0.18	0.511	o	|	|	|	|	1.76
12.000	0.00	0.18	0.510	o	|	|	|	|	1.76
12.083	0.00	0.18	0.508	o	|	|	|	|	1.75
12.167	0.00	0.18	0.507	o	|	|	|	|	1.75
12.250	0.00	0.18	0.506	o	|	|	|	|	1.75
12.333	0.00	0.18	0.505	o	|	|	|	|	1.74
12.417	0.00	0.18	0.504	o	|	|	|	|	1.74
12.500	0.00	0.18	0.502	o	|	|	|	|	1.73
12.583	0.00	0.18	0.501	o	|	|	|	|	1.73
12.667	0.00	0.18	0.500	o	|	|	|	|	1.73
12.750	0.00	0.18	0.499	o	|	|	|	|	1.72
12.833	0.00	0.18	0.497	o	|	|	|	|	1.72
12.917	0.00	0.18	0.496	o	|	|	|	|	1.72
13.000	0.00	0.18	0.495	o	|	|	|	|	1.71
13.083	0.00	0.18	0.494	o	|	|	|	|	1.71
13.167	0.00	0.18	0.493	o	|	|	|	|	1.70
13.250	0.00	0.17	0.491	o	|	|	|	|	1.70
13.333	0.00	0.17	0.490	o	|	|	|	|	1.70
13.417	0.00	0.17	0.489	o	|	|	|	|	1.69
13.500	0.00	0.17	0.488	o	|	|	|	|	1.69
13.583	0.00	0.17	0.487	o	|	|	|	|	1.68
13.667	0.00	0.17	0.485	o	|	|	|	|	1.68
13.750	0.00	0.17	0.484	o	|	|	|	|	1.68
13.833	0.00	0.17	0.483	o	|	|	|	|	1.67
13.917	0.00	0.17	0.482	o	|	|	|	|	1.67
14.000	0.00	0.17	0.481	o	|	|	|	|	1.66
14.083	0.00	0.17	0.479	o	|	|	|	|	1.66
14.167	0.00	0.17	0.478	o	|	|	|	|	1.66
14.250	0.00	0.17	0.477	o	|	|	|	|	1.65
14.333	0.00	0.17	0.476	o	|	|	|	|	1.65
14.417	0.00	0.17	0.475	o	|	|	|	|	1.65
14.500	0.00	0.17	0.474	o	|	|	|	|	1.64
14.583	0.00	0.17	0.472	o	|	|	|	|	1.64
14.667	0.00	0.17	0.471	o	|	|	|	|	1.63
14.750	0.00	0.17	0.470	o	|	|	|	|	1.63
14.833	0.00	0.17	0.469	o	|	|	|	|	1.63
14.917	0.00	0.17	0.468	o	|	|	|	|	1.62
15.000	0.00	0.17	0.466	o	|	|	|	|	1.62
15.083	0.00	0.17	0.465	o	|	|	|	|	1.61
15.167	0.00	0.17	0.464	o	|	|	|	|	1.61
15.250	0.00	0.17	0.463	o	|	|	|	|	1.61
15.333	0.00	0.17	0.462	o	|	|	|	|	1.60
15.417	0.00	0.17	0.461	o	|	|	|	|	1.60
15.500	0.00	0.17	0.459	o	|	|	|	|	1.60
15.583	0.00	0.17	0.458	o	|	|	|	|	1.59
15.667	0.00	0.17	0.457	o	|	|	|	|	1.59
15.750	0.00	0.17	0.456	o	|	|	|	|	1.58

15.833	0.00	0.17	0.455	o	|	|	|	|	1.58
15.917	0.00	0.17	0.454	o	|	|	|	|	1.58
16.000	0.00	0.17	0.453	o	|	|	|	|	1.57
16.083	0.00	0.17	0.451	o	|	|	|	|	1.57
16.167	0.00	0.17	0.450	o	|	|	|	|	1.57
16.250	0.00	0.17	0.449	o	|	|	|	|	1.56
16.333	0.00	0.17	0.448	o	|	|	|	|	1.56
16.417	0.00	0.17	0.447	o	|	|	|	|	1.55
16.500	0.00	0.17	0.446	o	|	|	|	|	1.55
16.583	0.00	0.17	0.445	o	|	|	|	|	1.55
16.667	0.00	0.17	0.443	o	|	|	|	|	1.54
16.750	0.00	0.17	0.442	o	|	|	|	|	1.54
16.833	0.00	0.17	0.441	o	|	|	|	|	1.54
16.917	0.00	0.16	0.440	o	|	|	|	|	1.53
17.000	0.00	0.16	0.439	o	|	|	|	|	1.53
17.083	0.00	0.16	0.438	o	|	|	|	|	1.52
17.167	0.00	0.16	0.437	o	|	|	|	|	1.52
17.250	0.00	0.16	0.435	o	|	|	|	|	1.52
17.333	0.00	0.16	0.434	o	|	|	|	|	1.51
17.417	0.00	0.16	0.433	o	|	|	|	|	1.51
17.500	0.00	0.16	0.432	o	|	|	|	|	1.51
17.583	0.00	0.16	0.431	o	|	|	|	|	1.50
17.667	0.00	0.16	0.430	o	|	|	|	|	1.50
17.750	0.00	0.16	0.429	o	|	|	|	|	1.50
17.833	0.00	0.16	0.428	o	|	|	|	|	1.49
17.917	0.00	0.16	0.426	o	|	|	|	|	1.49
18.000	0.00	0.16	0.425	o	|	|	|	|	1.48
18.083	0.00	0.16	0.424	o	|	|	|	|	1.48
18.167	0.00	0.16	0.423	o	|	|	|	|	1.48
18.250	0.00	0.16	0.422	o	|	|	|	|	1.47
18.333	0.00	0.16	0.421	o	|	|	|	|	1.47
18.417	0.00	0.16	0.420	o	|	|	|	|	1.47
18.500	0.00	0.16	0.419	o	|	|	|	|	1.46
18.583	0.00	0.16	0.418	o	|	|	|	|	1.46
18.667	0.00	0.16	0.416	o	|	|	|	|	1.46
18.750	0.00	0.16	0.415	o	|	|	|	|	1.45
18.833	0.00	0.16	0.414	o	|	|	|	|	1.45
18.917	0.00	0.16	0.413	o	|	|	|	|	1.45
19.000	0.00	0.16	0.412	o	|	|	|	|	1.44
19.083	0.00	0.16	0.411	o	|	|	|	|	1.44
19.167	0.00	0.16	0.410	o	|	|	|	|	1.43
19.250	0.00	0.16	0.409	o	|	|	|	|	1.43
19.333	0.00	0.16	0.408	o	|	|	|	|	1.43
19.417	0.00	0.16	0.407	o	|	|	|	|	1.42
19.500	0.00	0.16	0.405	o	|	|	|	|	1.42
19.583	0.00	0.16	0.404	o	|	|	|	|	1.42
19.667	0.00	0.16	0.403	o	|	|	|	|	1.41
19.750	0.00	0.16	0.402	o	|	|	|	|	1.41
19.833	0.00	0.16	0.401	o	|	|	|	|	1.41
19.917	0.00	0.16	0.400	o	|	|	|	|	1.40
20.000	0.00	0.16	0.399	o	|	|	|	|	1.40
20.083	0.00	0.16	0.398	o	|	|	|	|	1.40
20.167	0.00	0.16	0.397	o	|	|	|	|	1.39
20.250	0.00	0.16	0.396	o	|	|	|	|	1.39
20.333	0.00	0.16	0.395	o	|	|	|	|	1.39
20.417	0.00	0.16	0.394	o	|	|	|	|	1.38
20.500	0.00	0.16	0.392	o	|	|	|	|	1.38
20.583	0.00	0.16	0.391	o	|	|	|	|	1.37
20.667	0.00	0.16	0.390	o	|	|	|	|	1.37
20.750	0.00	0.16	0.389	o	|	|	|	|	1.37
20.833	0.00	0.15	0.388	o	|	|	|	|	1.36
20.917	0.00	0.15	0.387	o	|	|	|	|	1.36
21.000	0.00	0.15	0.386	o	|	|	|	|	1.36
21.083	0.00	0.15	0.385	o	|	|	|	|	1.35
21.167	0.00	0.15	0.384	o	|	|	|	|	1.35
21.250	0.00	0.15	0.383	o	|	|	|	|	1.35
21.333	0.00	0.15	0.382	o	|	|	|	|	1.34
21.417	0.00	0.15	0.381	o	|	|	|	|	1.34
21.500	0.00	0.15	0.380	o	|	|	|	|	1.34
21.583	0.00	0.15	0.379	o	|	|	|	|	1.33
21.667	0.00	0.15	0.378	o	|	|	|	|	1.33
21.750	0.00	0.15	0.377	o	|	|	|	|	1.33
21.833	0.00	0.15	0.376	o	|	|	|	|	1.32
21.917	0.00	0.15	0.374	o	|	|	|	|	1.32
22.000	0.00	0.15	0.373	o	|	|	|	|	1.32
22.083	0.00	0.15	0.372	o	|	|	|	|	1.31
22.167	0.00	0.15	0.371	o	|	|	|	|	1.31
22.250	0.00	0.15	0.370	o	|	|	|	|	1.31
22.333	0.00	0.15	0.369	o	|	|	|	|	1.30
22.417	0.00	0.15	0.368	o	|	|	|	|	1.30
22.500	0.00	0.15	0.367	o	|	|	|	|	1.30
22.583	0.00	0.15	0.366	o	|	|	|	|	1.29
22.667	0.00	0.15	0.365	o	|	|	|	|	1.29
22.750	0.00	0.15	0.364	o	|	|	|	|	1.29
22.833	0.00	0.15	0.363	o	|	|	|	|	1.28
22.917	0.00	0.15	0.362	o	|	|	|	|	1.28

23.000	0.00	0.15	0.361	o	|	|	|	1.28
23.083	0.00	0.15	0.360	o	|	|	|	1.27
23.167	0.00	0.15	0.359	o	|	|	|	1.27
23.250	0.00	0.15	0.358	o	|	|	|	1.27
23.333	0.00	0.15	0.357	o	|	|	|	1.26
23.417	0.00	0.15	0.356	o	|	|	|	1.26
23.500	0.00	0.15	0.355	o	|	|	|	1.26
23.583	0.00	0.15	0.354	o	|	|	|	1.25
23.667	0.00	0.15	0.353	o	|	|	|	1.25
23.750	0.00	0.15	0.352	o	|	|	|	1.25
23.833	0.00	0.15	0.351	o	|	|	|	1.24
23.917	0.00	0.15	0.350	o	|	|	|	1.24
24.000	0.00	0.15	0.349	o	|	|	|	1.24
24.083	0.00	0.15	0.348	o	|	|	|	1.23
24.167	0.00	0.15	0.347	o	|	|	|	1.23
24.250	0.00	0.15	0.346	o	|	|	|	1.23
24.333	0.00	0.15	0.345	o	|	|	|	1.22
24.417	0.00	0.15	0.344	o	|	|	|	1.22
24.500	0.00	0.15	0.343	o	|	|	|	1.22
24.583	0.00	0.15	0.342	o	|	|	|	1.21
24.667	0.00	0.15	0.341	o	|	|	|	1.21
24.750	0.00	0.15	0.340	o	|	|	|	1.21
24.833	0.00	0.15	0.339	o	|	|	|	1.20
24.917	0.00	0.15	0.338	o	|	|	|	1.20
25.000	0.00	0.14	0.337	o	|	|	|	1.20
25.083	0.00	0.14	0.336	o	|	|	|	1.19
25.167	0.00	0.14	0.335	o	|	|	|	1.19
25.250	0.00	0.14	0.334	o	|	|	|	1.19
25.333	0.00	0.14	0.333	o	|	|	|	1.18
25.417	0.00	0.14	0.332	o	|	|	|	1.18
25.500	0.00	0.14	0.331	o	|	|	|	1.18
25.583	0.00	0.14	0.330	o	|	|	|	1.17
25.667	0.00	0.14	0.329	o	|	|	|	1.17
25.750	0.00	0.14	0.328	o	|	|	|	1.17
25.833	0.00	0.14	0.327	o	|	|	|	1.16
25.917	0.00	0.14	0.326	o	|	|	|	1.16
26.000	0.00	0.14	0.325	o	|	|	|	1.16
26.083	0.00	0.14	0.324	o	|	|	|	1.16
26.167	0.00	0.14	0.323	o	|	|	|	1.15
26.250	0.00	0.14	0.322	o	|	|	|	1.15
26.333	0.00	0.14	0.321	o	|	|	|	1.15
26.417	0.00	0.14	0.320	o	|	|	|	1.14
26.500	0.00	0.14	0.319	o	|	|	|	1.14
26.583	0.00	0.14	0.318	o	|	|	|	1.14
26.667	0.00	0.14	0.317	o	|	|	|	1.13
26.750	0.00	0.14	0.316	o	|	|	|	1.13
26.833	0.00	0.14	0.315	o	|	|	|	1.13
26.917	0.00	0.14	0.314	o	|	|	|	1.12
27.000	0.00	0.14	0.313	o	|	|	|	1.12
27.083	0.00	0.14	0.312	o	|	|	|	1.12
27.167	0.00	0.14	0.311	o	|	|	|	1.11
27.250	0.00	0.14	0.310	o	|	|	|	1.11
27.333	0.00	0.14	0.309	o	|	|	|	1.11
27.417	0.00	0.14	0.308	o	|	|	|	1.10
27.500	0.00	0.14	0.307	o	|	|	|	1.10
27.583	0.00	0.14	0.306	o	|	|	|	1.10
27.667	0.00	0.14	0.305	o	|	|	|	1.10
27.750	0.00	0.14	0.304	o	|	|	|	1.09
27.833	0.00	0.14	0.303	o	|	|	|	1.09
27.917	0.00	0.14	0.303	o	|	|	|	1.09
28.000	0.00	0.14	0.302	o	|	|	|	1.08
28.083	0.00	0.14	0.301	o	|	|	|	1.08
28.167	0.00	0.14	0.300	o	|	|	|	1.08
28.250	0.00	0.14	0.299	o	|	|	|	1.07
28.333	0.00	0.14	0.298	o	|	|	|	1.07
28.417	0.00	0.14	0.297	o	|	|	|	1.07
28.500	0.00	0.14	0.296	o	|	|	|	1.06
28.583	0.00	0.14	0.295	o	|	|	|	1.06
28.667	0.00	0.14	0.294	o	|	|	|	1.06
28.750	0.00	0.14	0.293	o	|	|	|	1.06
28.833	0.00	0.14	0.292	o	|	|	|	1.05
28.917	0.00	0.14	0.291	o	|	|	|	1.05
29.000	0.00	0.14	0.290	o	|	|	|	1.05
29.083	0.00	0.14	0.289	o	|	|	|	1.04
29.167	0.00	0.14	0.288	o	|	|	|	1.04
29.250	0.00	0.14	0.287	o	|	|	|	1.04
29.333	0.00	0.14	0.287	o	|	|	|	1.03
29.417	0.00	0.13	0.286	o	|	|	|	1.03
29.500	0.00	0.13	0.285	o	|	|	|	1.03
29.583	0.00	0.13	0.284	o	|	|	|	1.03
29.667	0.00	0.13	0.283	o	|	|	|	1.02
29.750	0.00	0.13	0.282	o	|	|	|	1.02
29.833	0.00	0.13	0.281	o	|	|	|	1.02
29.917	0.00	0.13	0.280	o	|	|	|	1.01
30.000	0.00	0.13	0.279	o	|	|	|	1.01
30.083	0.00	0.13	0.278	o	|	|	|	1.01

30.167	0.00	0.13	0.277	o	|	|	|	1.00
30.250	0.00	0.13	0.276	o	|	|	|	1.00
30.333	0.00	0.13	0.275	o	|	|	|	1.00
30.417	0.00	0.13	0.275	o	|	|	|	0.99
30.500	0.00	0.13	0.274	o	|	|	|	0.99
30.583	0.00	0.13	0.273	o	|	|	|	0.99
30.667	0.00	0.13	0.272	o	|	|	|	0.98
30.750	0.00	0.13	0.271	o	|	|	|	0.98
30.833	0.00	0.13	0.270	o	|	|	|	0.98
30.917	0.00	0.13	0.269	o	|	|	|	0.98
31.000	0.00	0.13	0.268	o	|	|	|	0.97
31.083	0.00	0.13	0.267	o	|	|	|	0.97
31.167	0.00	0.13	0.266	o	|	|	|	0.97
31.250	0.00	0.13	0.266	o	|	|	|	0.96
31.333	0.00	0.13	0.265	o	|	|	|	0.96
31.417	0.00	0.13	0.264	o	|	|	|	0.96
31.500	0.00	0.13	0.263	o	|	|	|	0.95
31.583	0.00	0.13	0.262	o	|	|	|	0.95
31.667	0.00	0.13	0.261	o	|	|	|	0.95
31.750	0.00	0.13	0.260	o	|	|	|	0.94
31.833	0.00	0.13	0.259	o	|	|	|	0.94
31.917	0.00	0.12	0.259	o	|	|	|	0.94
32.000	0.00	0.12	0.258	o	|	|	|	0.93
32.083	0.00	0.12	0.257	o	|	|	|	0.93
32.167	0.00	0.12	0.256	o	|	|	|	0.93
32.250	0.00	0.12	0.255	o	|	|	|	0.92
32.333	0.00	0.12	0.254	o	|	|	|	0.92
32.417	0.00	0.12	0.254	o	|	|	|	0.92
32.500	0.00	0.12	0.253	o	|	|	|	0.92
32.583	0.00	0.12	0.252	o	|	|	|	0.91
32.667	0.00	0.12	0.251	o	|	|	|	0.91
32.750	0.00	0.12	0.250	o	|	|	|	0.91
32.833	0.00	0.12	0.249	o	|	|	|	0.90
32.917	0.00	0.12	0.249	o	|	|	|	0.90
33.000	0.00	0.12	0.248	o	|	|	|	0.90
33.083	0.00	0.12	0.247	o	|	|	|	0.89
33.167	0.00	0.12	0.246	o	|	|	|	0.89
33.250	0.00	0.12	0.245	o	|	|	|	0.89
33.333	0.00	0.12	0.244	o	|	|	|	0.89
33.417	0.00	0.12	0.244	o	|	|	|	0.88
33.500	0.00	0.12	0.243	o	|	|	|	0.88
33.583	0.00	0.12	0.242	o	|	|	|	0.88
33.667	0.00	0.12	0.241	o	|	|	|	0.87
33.750	0.00	0.12	0.240	o	|	|	|	0.87
33.833	0.00	0.12	0.240	o	|	|	|	0.87
33.917	0.00	0.12	0.239	o	|	|	|	0.87
34.000	0.00	0.11	0.238	o	|	|	|	0.86
34.083	0.00	0.11	0.237	o	|	|	|	0.86
34.167	0.00	0.11	0.236	o	|	|	|	0.86
34.250	0.00	0.11	0.236	o	|	|	|	0.85
34.333	0.00	0.11	0.235	o	|	|	|	0.85
34.417	0.00	0.11	0.234	o	|	|	|	0.85
34.500	0.00	0.11	0.233	o	|	|	|	0.85
34.583	0.00	0.11	0.233	o	|	|	|	0.84
34.667	0.00	0.11	0.232	o	|	|	|	0.84
34.750	0.00	0.11	0.231	o	|	|	|	0.84
34.833	0.00	0.11	0.230	o	|	|	|	0.83
34.917	0.00	0.11	0.230	o	|	|	|	0.83
35.000	0.00	0.11	0.229	o	|	|	|	0.83
35.083	0.00	0.11	0.228	o	|	|	|	0.83
35.167	0.00	0.11	0.227	o	|	|	|	0.82
35.250	0.00	0.11	0.226	o	|	|	|	0.82
35.333	0.00	0.11	0.226	o	|	|	|	0.82
35.417	0.00	0.11	0.225	o	|	|	|	0.82
35.500	0.00	0.11	0.224	o	|	|	|	0.81
35.583	0.00	0.11	0.223	o	|	|	|	0.81
35.667	0.00	0.11	0.223	o	|	|	|	0.81
35.750	0.00	0.11	0.222	o	|	|	|	0.80
35.833	0.00	0.11	0.221	o	|	|	|	0.80
35.917	0.00	0.11	0.221	o	|	|	|	0.80
36.000	0.00	0.11	0.220	o	|	|	|	0.80
36.083	0.00	0.11	0.219	o	|	|	|	0.79
36.167	0.00	0.11	0.218	o	|	|	|	0.79
36.250	0.00	0.10	0.218	o	|	|	|	0.79
36.333	0.00	0.10	0.217	o	|	|	|	0.79
36.417	0.00	0.10	0.216	o	|	|	|	0.78
36.500	0.00	0.10	0.215	o	|	|	|	0.78
36.583	0.00	0.10	0.215	o	|	|	|	0.78
36.667	0.00	0.10	0.214	o	|	|	|	0.78
36.750	0.00	0.10	0.213	o	|	|	|	0.77
36.833	0.00	0.10	0.213	o	|	|	|	0.77
36.917	0.00	0.10	0.212	o	|	|	|	0.77
37.000	0.00	0.10	0.211	o	|	|	|	0.77
37.083	0.00	0.10	0.211	o	|	|	|	0.76
37.167	0.00	0.10	0.210	o	|	|	|	0.76
37.250	0.00	0.10	0.209	o	|	|	|	0.76

```
37.333    0.00    0.10      0.208  O       |       |       |       |     0.76
37.417    0.00    0.10      0.208  O       |       |       |       |     0.75
37.500    0.00    0.10      0.207  O       |       |       |       |     0.75

       Remaining water in basin =    0.21 (Ac.Ft)


       ****************************HYDROGRAPH DATA****************************
                     Number of intervals =   450
                     Time interval =    5.0 (Min.)
                     Maximum/Peak flow rate =        0.393 (CFS)
                     Total volume =       0.529 (Ac.Ft)
              Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
       ***********************************************************************

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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 05/07/25

 ------------------------------------------------------------------------
 Program License Serial Number 5006
 ------------------------------------------------------------------------
 ********************* HYDROGRAPH INFORMATION **********************
                From study/file name: PRO232.rte
 ****************************HYDROGRAPH DATA*****************************
                Number of intervals =    40
                Time interval =    5.0 (Min.)
                Maximum/Peak flow rate =       11.612 (CFS)
                Total volume =       0.972 (Ac.Ft)
         Status of hydrographs being held in storage
                   Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
         Peak (CFS)      0.000     0.000     0.000     0.000     0.000
         Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
 ************************************************************************
 ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
 Process from Point/Station        1.000 to Point/Station        2.000
 **** RETARDING BASIN ROUTING ****
 ________________________________________________________________________

 User entry of depth-outflow-storage data
 ------------------------------------------------------------------------
 Total number of inflow hydrograph intervals = 40
 Hydrograph time unit =  5.000 (Min.)
 Initial depth in storage basin =   0.00(Ft.)
 ------------------------------------------------------------------------
 ------------------------------------------------------------------------
 Initial basin depth =   0.00 (Ft.)
 Initial basin storage =      0.00 (Ac.Ft)
 Initial basin outflow =   0.00 (CFS)
 ------------------------------------------------------------------------
 ------------------------------------------------------------------------
 Depth vs. Storage and Depth vs. Discharge data:
  Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
      (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
 ------------------------------------------------------------------------
    0.000      0.000      0.000      0.000        0.000
    1.000      0.276      0.133      0.276        0.276
    2.000      0.584      0.193      0.583        0.585
    3.000      0.930      0.700      0.928        0.932
    3.500      1.118      0.824      1.115        1.121
    4.000      1.316      0.930      1.313        1.319
    4.500      1.528      1.024      1.524        1.532
    4.750      1.637      1.068      1.633        1.641
    5.000      1.749     18.283      1.686        1.812
    6.000      2.231    253.655      1.358        3.104
 ------------------------------------------------------------------------
                Hydrograph Detention Basin Routing
 ------------------------------------------------------------------------

 Graph values: 'I'= unit inflow; 'O'=outflow at time shown
 ------------------------------------------------------------------------
  Time   Inflow  Outflow    Storage                                  Depth
 (Hours)  (CFS)   (CFS)     (Ac.Ft) .0       2.9    5.81    8.71   11.61 (Ft.)
 0.083    0.73    0.00      0.003  o I      |       |       |       |     0.01
 0.167    1.52    0.00      0.010  o   I    |       |       |       |     0.04
 0.250    1.58    0.01      0.021  o   I    |       |       |       |     0.08
 0.333    1.75    0.02      0.032  o   I    |       |       |       |     0.12
 0.417    2.00    0.02      0.045  o    I   |       |       |       |     0.16
 0.500    2.21    0.03      0.059  o     I  |       |       |       |     0.21
 0.583    2.24    0.04      0.074  o     I  |       |       |       |     0.27
 0.667    2.27    0.04      0.090  o     I  |       |       |       |     0.32
 0.750    2.43    0.05      0.106  o     I  |       |       |       |     0.38
 0.833    2.29    0.06      0.121  o     I  |       |       |       |     0.44
 0.917    2.17    0.07      0.136  o    I   |       |       |       |     0.49
 1.000    2.32    0.07      0.151  o     I  |       |       |       |     0.55
 1.083    2.66    0.08      0.168  o      I |       |       |       |     0.61
 1.167    2.93    0.09      0.187  o       I       |       |       |     0.68
 1.250    2.99    0.10      0.206  o       I       |       |       |     0.75
 1.333    2.91    0.11      0.226  o       I       |       |       |     0.82
 1.417    3.13    0.12      0.246  o       I       |       |       |     0.89
 1.500    3.53    0.13      0.268  o       |I      |       |       |     0.97
 1.583    3.49    0.14      0.291  o       |I      |       |       |     1.05
 1.667    3.51    0.14      0.314  o       |I      |       |       |     1.12
 1.750    4.01    0.15      0.339  o       |  I    |       |       |     1.21
 1.833    4.29    0.15      0.367  o       |  I    |       |       |     1.29
 1.917    4.14    0.16      0.395  o       |  I    |       |       |     1.39
 2.000    4.09    0.16      0.422  o       |  I    |       |       |     1.47
 2.083    4.18    0.17      0.449  o       |  I    |       |       |     1.56
 2.167    4.86    0.17      0.479  o       |    I  |       |       |     1.66
 2.250    5.99    0.18      0.516  o       |       I       |       |     1.78
 2.333    5.79    0.19      0.555  o       |      I|       |       |     1.91
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2.417	7.01	0.21	0.598	O	|	| I	|	|	2.04
2.500	9.60	0.29	0.653	O	|	|	| I	|	2.20
2.583	11.61	0.40	0.724	|O	|	|	| I	2.40
2.667	10.79	0.51	0.798	|O	|	|	I |	2.62
2.750	6.58	0.59	0.854	|O	|	I |	|	2.78
2.833	3.69	0.63	0.885	|O	I |	|	|	2.87
2.917	2.90	0.66	0.903	|O	I |	|	|	2.92
3.000	1.91	0.68	0.915	|O	I |	|	|	2.96
3.083	0.74	0.68	0.919	|OI	|	|	|	2.97
3.167	0.21	0.68	0.918	IO	|	|	|	2.97
3.250	0.07	0.68	0.914	IO	|	|	|	2.95
3.333	0.01	0.67	0.910	IO	|	|	|	2.94
3.417	0.00	0.66	0.905	IO	|	|	|	2.93
3.500	0.00	0.66	0.901	IO	|	|	|	2.92
3.583	0.00	0.65	0.896	IO	|	|	|	2.90
3.667	0.00	0.64	0.892	IO	|	|	|	2.89
3.750	0.00	0.64	0.887	IO	|	|	|	2.88
3.833	0.00	0.63	0.883	IO	|	|	|	2.86
3.917	0.00	0.62	0.879	IO	|	|	|	2.85
4.000	0.00	0.62	0.875	IO	|	|	|	2.84
4.083	0.00	0.61	0.870	IO	|	|	|	2.83
4.167	0.00	0.61	0.866	IO	|	|	|	2.82
4.250	0.00	0.60	0.862	IO	|	|	|	2.80
4.333	0.00	0.59	0.858	IO	|	|	|	2.79
4.417	0.00	0.59	0.854	IO	|	|	|	2.78
4.500	0.00	0.58	0.850	IO	|	|	|	2.77
4.583	0.00	0.58	0.846	IO	|	|	|	2.76
4.667	0.00	0.57	0.842	IO	|	|	|	2.74
4.750	0.00	0.56	0.838	IO	|	|	|	2.73
4.833	0.00	0.56	0.834	IO	|	|	|	2.72
4.917	0.00	0.55	0.830	IO	|	|	|	2.71
5.000	0.00	0.55	0.826	IO	|	|	|	2.70
5.083	0.00	0.54	0.823	IO	|	|	|	2.69
5.167	0.00	0.54	0.819	IO	|	|	|	2.68
5.250	0.00	0.53	0.815	IO	|	|	|	2.67
5.333	0.00	0.53	0.812	IO	|	|	|	2.66
5.417	0.00	0.52	0.808	IO	|	|	|	2.65
5.500	0.00	0.52	0.804	IO	|	|	|	2.64
5.583	0.00	0.51	0.801	IO	|	|	|	2.63
5.667	0.00	0.51	0.797	IO	|	|	|	2.62
5.750	0.00	0.50	0.794	IO	|	|	|	2.61
5.833	0.00	0.50	0.790	IO	|	|	|	2.60
5.917	0.00	0.49	0.787	IO	|	|	|	2.59
6.000	0.00	0.49	0.784	IO	|	|	|	2.58
6.083	0.00	0.48	0.780	IO	|	|	|	2.57
6.167	0.00	0.48	0.777	IO	|	|	|	2.56
6.250	0.00	0.47	0.774	IO	|	|	|	2.55
6.333	0.00	0.47	0.771	IO	|	|	|	2.54
6.417	0.00	0.46	0.767	IO	|	|	|	2.53
6.500	0.00	0.46	0.764	IO	|	|	|	2.52
6.583	0.00	0.45	0.761	IO	|	|	|	2.51
6.667	0.00	0.45	0.758	IO	|	|	|	2.50
6.750	0.00	0.44	0.755	IO	|	|	|	2.49
6.833	0.00	0.44	0.752	IO	|	|	|	2.49
6.917	0.00	0.43	0.749	IO	|	|	|	2.48
7.000	0.00	0.43	0.746	IO	|	|	|	2.47
7.083	0.00	0.43	0.743	IO	|	|	|	2.46
7.167	0.00	0.42	0.740	IO	|	|	|	2.45
7.250	0.00	0.42	0.737	IO	|	|	|	2.44
7.333	0.00	0.41	0.734	IO	|	|	|	2.43
7.417	0.00	0.41	0.731	IO	|	|	|	2.43
7.500	0.00	0.40	0.729	IO	|	|	|	2.42
7.583	0.00	0.40	0.726	IO	|	|	|	2.41
7.667	0.00	0.40	0.723	IO	|	|	|	2.40
7.750	0.00	0.39	0.720	IO	|	|	|	2.39
7.833	0.00	0.39	0.718	IO	|	|	|	2.39
7.917	0.00	0.39	0.715	IO	|	|	|	2.38
8.000	0.00	0.38	0.712	IO	|	|	|	2.37
8.083	0.00	0.38	0.710	IO	|	|	|	2.36
8.167	0.00	0.37	0.707	IO	|	|	|	2.36
8.250	0.00	0.37	0.705	IO	|	|	|	2.35
8.333	0.00	0.37	0.702	IO	|	|	|	2.34
8.417	0.00	0.36	0.700	O	|	|	|	2.33
8.500	0.00	0.36	0.697	O	|	|	|	2.33
8.583	0.00	0.36	0.695	O	|	|	|	2.32
8.667	0.00	0.35	0.692	O	|	|	|	2.31
8.750	0.00	0.35	0.690	O	|	|	|	2.31
8.833	0.00	0.34	0.687	O	|	|	|	2.30
8.917	0.00	0.34	0.685	O	|	|	|	2.29
9.000	0.00	0.34	0.683	O	|	|	|	2.29
9.083	0.00	0.33	0.680	O	|	|	|	2.28
9.167	0.00	0.33	0.678	O	|	|	|	2.27
9.250	0.00	0.33	0.676	O	|	|	|	2.27
9.333	0.00	0.32	0.674	O	|	|	|	2.26
9.417	0.00	0.32	0.671	O	|	|	|	2.25
9.500	0.00	0.32	0.669	O	|	|	|	2.25
9.583	0.00	0.31	0.667	O	|	|	|	2.24
9.667	0.00	0.31	0.665	O	|	|	|	2.23

9.750	0.00	0.31	0.663	o	|	|	|	|	2.23
9.833	0.00	0.31	0.661	o	|	|	|	|	2.22
9.917	0.00	0.30	0.659	o	|	|	|	|	2.22
10.000	0.00	0.30	0.656	o	|	|	|	|	2.21
10.083	0.00	0.30	0.654	o	|	|	|	|	2.20
10.167	0.00	0.29	0.652	o	|	|	|	|	2.20
10.250	0.00	0.29	0.650	o	|	|	|	|	2.19
10.333	0.00	0.29	0.648	o	|	|	|	|	2.19
10.417	0.00	0.28	0.646	o	|	|	|	|	2.18
10.500	0.00	0.28	0.644	o	|	|	|	|	2.17
10.583	0.00	0.28	0.643	o	|	|	|	|	2.17
10.667	0.00	0.28	0.641	o	|	|	|	|	2.16
10.750	0.00	0.27	0.639	o	|	|	|	|	2.16
10.833	0.00	0.27	0.637	o	|	|	|	|	2.15
10.917	0.00	0.27	0.635	o	|	|	|	|	2.15
11.000	0.00	0.27	0.633	o	|	|	|	|	2.14
11.083	0.00	0.26	0.631	o	|	|	|	|	2.14
11.167	0.00	0.26	0.630	o	|	|	|	|	2.13
11.250	0.00	0.26	0.628	o	|	|	|	|	2.13
11.333	0.00	0.25	0.626	o	|	|	|	|	2.12
11.417	0.00	0.25	0.624	o	|	|	|	|	2.12
11.500	0.00	0.25	0.623	o	|	|	|	|	2.11
11.583	0.00	0.25	0.621	o	|	|	|	|	2.11
11.667	0.00	0.24	0.619	o	|	|	|	|	2.10
11.750	0.00	0.24	0.617	o	|	|	|	|	2.10
11.833	0.00	0.24	0.616	o	|	|	|	|	2.09
11.917	0.00	0.24	0.614	o	|	|	|	|	2.09
12.000	0.00	0.23	0.613	o	|	|	|	|	2.08
12.083	0.00	0.23	0.611	o	|	|	|	|	2.08
12.167	0.00	0.23	0.609	o	|	|	|	|	2.07
12.250	0.00	0.23	0.608	o	|	|	|	|	2.07
12.333	0.00	0.23	0.606	o	|	|	|	|	2.06
12.417	0.00	0.22	0.605	o	|	|	|	|	2.06
12.500	0.00	0.22	0.603	o	|	|	|	|	2.06
12.583	0.00	0.22	0.602	o	|	|	|	|	2.05
12.667	0.00	0.22	0.600	o	|	|	|	|	2.05
12.750	0.00	0.21	0.599	o	|	|	|	|	2.04
12.833	0.00	0.21	0.597	o	|	|	|	|	2.04
12.917	0.00	0.21	0.596	o	|	|	|	|	2.03
13.000	0.00	0.21	0.594	o	|	|	|	|	2.03
13.083	0.00	0.21	0.593	o	|	|	|	|	2.03
13.167	0.00	0.20	0.591	o	|	|	|	|	2.02
13.250	0.00	0.20	0.590	o	|	|	|	|	2.02
13.333	0.00	0.20	0.589	o	|	|	|	|	2.01
13.417	0.00	0.20	0.587	o	|	|	|	|	2.01
13.500	0.00	0.20	0.586	o	|	|	|	|	2.01
13.583	0.00	0.19	0.585	o	|	|	|	|	2.00
13.667	0.00	0.19	0.583	o	|	|	|	|	2.00
13.750	0.00	0.19	0.582	o	|	|	|	|	1.99
13.833	0.00	0.19	0.581	o	|	|	|	|	1.99
13.917	0.00	0.19	0.579	o	|	|	|	|	1.98
14.000	0.00	0.19	0.578	o	|	|	|	|	1.98
14.083	0.00	0.19	0.577	o	|	|	|	|	1.98
14.167	0.00	0.19	0.575	o	|	|	|	|	1.97
14.250	0.00	0.19	0.574	o	|	|	|	|	1.97
14.333	0.00	0.19	0.573	o	|	|	|	|	1.96
14.417	0.00	0.19	0.571	o	|	|	|	|	1.96
14.500	0.00	0.19	0.570	o	|	|	|	|	1.95
14.583	0.00	0.19	0.569	o	|	|	|	|	1.95
14.667	0.00	0.19	0.567	o	|	|	|	|	1.95
14.750	0.00	0.19	0.566	o	|	|	|	|	1.94
14.833	0.00	0.19	0.565	o	|	|	|	|	1.94
14.917	0.00	0.19	0.564	o	|	|	|	|	1.93
15.000	0.00	0.19	0.562	o	|	|	|	|	1.93
15.083	0.00	0.19	0.561	o	|	|	|	|	1.93
15.167	0.00	0.19	0.560	o	|	|	|	|	1.92
15.250	0.00	0.19	0.558	o	|	|	|	|	1.92
15.333	0.00	0.19	0.557	o	|	|	|	|	1.91
15.417	0.00	0.19	0.556	o	|	|	|	|	1.91
15.500	0.00	0.19	0.554	o	|	|	|	|	1.90
15.583	0.00	0.19	0.553	o	|	|	|	|	1.90
15.667	0.00	0.19	0.552	o	|	|	|	|	1.90
15.750	0.00	0.19	0.551	o	|	|	|	|	1.89
15.833	0.00	0.19	0.549	o	|	|	|	|	1.89
15.917	0.00	0.19	0.548	o	|	|	|	|	1.88
16.000	0.00	0.19	0.547	o	|	|	|	|	1.88
16.083	0.00	0.19	0.545	o	|	|	|	|	1.87
16.167	0.00	0.19	0.544	o	|	|	|	|	1.87
16.250	0.00	0.18	0.543	o	|	|	|	|	1.87
16.333	0.00	0.18	0.542	o	|	|	|	|	1.86
16.417	0.00	0.18	0.540	o	|	|	|	|	1.86
16.500	0.00	0.18	0.539	o	|	|	|	|	1.85
16.583	0.00	0.18	0.538	o	|	|	|	|	1.85
16.667	0.00	0.18	0.537	o	|	|	|	|	1.85
16.750	0.00	0.18	0.535	o	|	|	|	|	1.84
16.833	0.00	0.18	0.534	o	|	|	|	|	1.84
16.917	0.00	0.18	0.533	o	|	|	|	|	1.83
17.000	0.00	0.18	0.532	o	|	|	|	|	1.83

17.083	0.00	0.18	0.530	o	|	|	|	1.83
17.167	0.00	0.18	0.529	o	|	|	|	1.82
17.250	0.00	0.18	0.528	o	|	|	|	1.82
17.333	0.00	0.18	0.526	o	|	|	|	1.81
17.417	0.00	0.18	0.525	o	|	|	|	1.81
17.500	0.00	0.18	0.524	o	|	|	|	1.81
17.583	0.00	0.18	0.523	o	|	|	|	1.80
17.667	0.00	0.18	0.522	o	|	|	|	1.80
17.750	0.00	0.18	0.520	o	|	|	|	1.79
17.833	0.00	0.18	0.519	o	|	|	|	1.79
17.917	0.00	0.18	0.518	o	|	|	|	1.78
18.000	0.00	0.18	0.517	o	|	|	|	1.78
18.083	0.00	0.18	0.515	o	|	|	|	1.78
18.167	0.00	0.18	0.514	o	|	|	|	1.77
18.250	0.00	0.18	0.513	o	|	|	|	1.77
18.333	0.00	0.18	0.512	o	|	|	|	1.76
18.417	0.00	0.18	0.510	o	|	|	|	1.76
18.500	0.00	0.18	0.509	o	|	|	|	1.76
18.583	0.00	0.18	0.508	o	|	|	|	1.75
18.667	0.00	0.18	0.507	o	|	|	|	1.75
18.750	0.00	0.18	0.505	o	|	|	|	1.74
18.833	0.00	0.18	0.504	o	|	|	|	1.74
18.917	0.00	0.18	0.503	o	|	|	|	1.74
19.000	0.00	0.18	0.502	o	|	|	|	1.73
19.083	0.00	0.18	0.501	o	|	|	|	1.73
19.167	0.00	0.18	0.499	o	|	|	|	1.73
19.250	0.00	0.18	0.498	o	|	|	|	1.72
19.333	0.00	0.18	0.497	o	|	|	|	1.72
19.417	0.00	0.18	0.496	o	|	|	|	1.71
19.500	0.00	0.18	0.495	o	|	|	|	1.71
19.583	0.00	0.18	0.493	o	|	|	|	1.71
19.667	0.00	0.18	0.492	o	|	|	|	1.70
19.750	0.00	0.17	0.491	o	|	|	|	1.70
19.833	0.00	0.17	0.490	o	|	|	|	1.69
19.917	0.00	0.17	0.488	o	|	|	|	1.69
20.000	0.00	0.17	0.487	o	|	|	|	1.69
20.083	0.00	0.17	0.486	o	|	|	|	1.68
20.167	0.00	0.17	0.485	o	|	|	|	1.68
20.250	0.00	0.17	0.484	o	|	|	|	1.67
20.333	0.00	0.17	0.482	o	|	|	|	1.67
20.417	0.00	0.17	0.481	o	|	|	|	1.67
20.500	0.00	0.17	0.480	o	|	|	|	1.66
20.583	0.00	0.17	0.479	o	|	|	|	1.66
20.667	0.00	0.17	0.478	o	|	|	|	1.65
20.750	0.00	0.17	0.477	o	|	|	|	1.65
20.833	0.00	0.17	0.475	o	|	|	|	1.65
20.917	0.00	0.17	0.474	o	|	|	|	1.64
21.000	0.00	0.17	0.473	o	|	|	|	1.64
21.083	0.00	0.17	0.472	o	|	|	|	1.64
21.167	0.00	0.17	0.471	o	|	|	|	1.63
21.250	0.00	0.17	0.469	o	|	|	|	1.63
21.333	0.00	0.17	0.468	o	|	|	|	1.62
21.417	0.00	0.17	0.467	o	|	|	|	1.62
21.500	0.00	0.17	0.466	o	|	|	|	1.62
21.583	0.00	0.17	0.465	o	|	|	|	1.61
21.667	0.00	0.17	0.464	o	|	|	|	1.61
21.750	0.00	0.17	0.462	o	|	|	|	1.61
21.833	0.00	0.17	0.461	o	|	|	|	1.60
21.917	0.00	0.17	0.460	o	|	|	|	1.60
22.000	0.00	0.17	0.459	o	|	|	|	1.59
22.083	0.00	0.17	0.458	o	|	|	|	1.59
22.167	0.00	0.17	0.457	o	|	|	|	1.59
22.250	0.00	0.17	0.455	o	|	|	|	1.58
22.333	0.00	0.17	0.454	o	|	|	|	1.58
22.417	0.00	0.17	0.453	o	|	|	|	1.58
22.500	0.00	0.17	0.452	o	|	|	|	1.57
22.583	0.00	0.17	0.451	o	|	|	|	1.57
22.667	0.00	0.17	0.450	o	|	|	|	1.56
22.750	0.00	0.17	0.449	o	|	|	|	1.56
22.833	0.00	0.17	0.447	o	|	|	|	1.56
22.917	0.00	0.17	0.446	o	|	|	|	1.55
23.000	0.00	0.17	0.445	o	|	|	|	1.55
23.083	0.00	0.17	0.444	o	|	|	|	1.55
23.167	0.00	0.17	0.443	o	|	|	|	1.54
23.250	0.00	0.17	0.442	o	|	|	|	1.54
23.333	0.00	0.17	0.441	o	|	|	|	1.53
23.417	0.00	0.16	0.439	o	|	|	|	1.53
23.500	0.00	0.16	0.438	o	|	|	|	1.53
23.583	0.00	0.16	0.437	o	|	|	|	1.52
23.667	0.00	0.16	0.436	o	|	|	|	1.52
23.750	0.00	0.16	0.435	o	|	|	|	1.52
23.833	0.00	0.16	0.434	o	|	|	|	1.51
23.917	0.00	0.16	0.433	o	|	|	|	1.51
24.000	0.00	0.16	0.432	o	|	|	|	1.50
24.083	0.00	0.16	0.430	o	|	|	|	1.50
24.167	0.00	0.16	0.429	o	|	|	|	1.50
24.250	0.00	0.16	0.428	o	|	|	|	1.49
24.333	0.00	0.16	0.427	o	|	|	|	1.49

24.417	0.00	0.16	0.426	o	|	|	|	1.49
24.500	0.00	0.16	0.425	o	|	|	|	1.48
24.583	0.00	0.16	0.424	o	|	|	|	1.48
24.667	0.00	0.16	0.423	o	|	|	|	1.48
24.750	0.00	0.16	0.421	o	|	|	|	1.47
24.833	0.00	0.16	0.420	o	|	|	|	1.47
24.917	0.00	0.16	0.419	o	|	|	|	1.47
25.000	0.00	0.16	0.418	o	|	|	|	1.46
25.083	0.00	0.16	0.417	o	|	|	|	1.46
25.167	0.00	0.16	0.416	o	|	|	|	1.45
25.250	0.00	0.16	0.415	o	|	|	|	1.45
25.333	0.00	0.16	0.414	o	|	|	|	1.45
25.417	0.00	0.16	0.413	o	|	|	|	1.44
25.500	0.00	0.16	0.412	o	|	|	|	1.44
25.583	0.00	0.16	0.410	o	|	|	|	1.44
25.667	0.00	0.16	0.409	o	|	|	|	1.43
25.750	0.00	0.16	0.408	o	|	|	|	1.43
25.833	0.00	0.16	0.407	o	|	|	|	1.43
25.917	0.00	0.16	0.406	o	|	|	|	1.42
26.000	0.00	0.16	0.405	o	|	|	|	1.42
26.083	0.00	0.16	0.404	o	|	|	|	1.42
26.167	0.00	0.16	0.403	o	|	|	|	1.41
26.250	0.00	0.16	0.402	o	|	|	|	1.41
26.333	0.00	0.16	0.401	o	|	|	|	1.40
26.417	0.00	0.16	0.400	o	|	|	|	1.40
26.500	0.00	0.16	0.398	o	|	|	|	1.40
26.583	0.00	0.16	0.397	o	|	|	|	1.39
26.667	0.00	0.16	0.396	o	|	|	|	1.39
26.750	0.00	0.16	0.395	o	|	|	|	1.39
26.833	0.00	0.16	0.394	o	|	|	|	1.38
26.917	0.00	0.16	0.393	o	|	|	|	1.38
27.000	0.00	0.16	0.392	o	|	|	|	1.38
27.083	0.00	0.16	0.391	o	|	|	|	1.37
27.167	0.00	0.16	0.390	o	|	|	|	1.37
27.250	0.00	0.15	0.389	o	|	|	|	1.37
27.333	0.00	0.15	0.388	o	|	|	|	1.36
27.417	0.00	0.15	0.387	o	|	|	|	1.36
27.500	0.00	0.15	0.386	o	|	|	|	1.36
27.583	0.00	0.15	0.385	o	|	|	|	1.35
27.667	0.00	0.15	0.383	o	|	|	|	1.35
27.750	0.00	0.15	0.382	o	|	|	|	1.35
27.833	0.00	0.15	0.381	o	|	|	|	1.34
27.917	0.00	0.15	0.380	o	|	|	|	1.34
28.000	0.00	0.15	0.379	o	|	|	|	1.34
28.083	0.00	0.15	0.378	o	|	|	|	1.33
28.167	0.00	0.15	0.377	o	|	|	|	1.33
28.250	0.00	0.15	0.376	o	|	|	|	1.32
28.333	0.00	0.15	0.375	o	|	|	|	1.32
28.417	0.00	0.15	0.374	o	|	|	|	1.32
28.500	0.00	0.15	0.373	o	|	|	|	1.31
28.583	0.00	0.15	0.372	o	|	|	|	1.31
28.667	0.00	0.15	0.371	o	|	|	|	1.31
28.750	0.00	0.15	0.370	o	|	|	|	1.30
28.833	0.00	0.15	0.369	o	|	|	|	1.30
28.917	0.00	0.15	0.368	o	|	|	|	1.30
29.000	0.00	0.15	0.367	o	|	|	|	1.29
29.083	0.00	0.15	0.366	o	|	|	|	1.29
29.167	0.00	0.15	0.365	o	|	|	|	1.29
29.250	0.00	0.15	0.364	o	|	|	|	1.28
29.333	0.00	0.15	0.363	o	|	|	|	1.28
29.417	0.00	0.15	0.362	o	|	|	|	1.28
29.500	0.00	0.15	0.360	o	|	|	|	1.27
29.583	0.00	0.15	0.359	o	|	|	|	1.27
29.667	0.00	0.15	0.358	o	|	|	|	1.27
29.750	0.00	0.15	0.357	o	|	|	|	1.26
29.833	0.00	0.15	0.356	o	|	|	|	1.26
29.917	0.00	0.15	0.355	o	|	|	|	1.26
30.000	0.00	0.15	0.354	o	|	|	|	1.25
30.083	0.00	0.15	0.353	o	|	|	|	1.25
30.167	0.00	0.15	0.352	o	|	|	|	1.25
30.250	0.00	0.15	0.351	o	|	|	|	1.24
30.333	0.00	0.15	0.350	o	|	|	|	1.24
30.417	0.00	0.15	0.349	o	|	|	|	1.24
30.500	0.00	0.15	0.348	o	|	|	|	1.23
30.583	0.00	0.15	0.347	o	|	|	|	1.23
30.667	0.00	0.15	0.346	o	|	|	|	1.23
30.750	0.00	0.15	0.345	o	|	|	|	1.22
30.833	0.00	0.15	0.344	o	|	|	|	1.22
30.917	0.00	0.15	0.343	o	|	|	|	1.22
31.000	0.00	0.15	0.342	o	|	|	|	1.21
31.083	0.00	0.15	0.341	o	|	|	|	1.21
31.167	0.00	0.15	0.340	o	|	|	|	1.21
31.250	0.00	0.15	0.339	o	|	|	|	1.21
31.333	0.00	0.15	0.338	o	|	|	|	1.20
31.417	0.00	0.14	0.337	o	|	|	|	1.20
31.500	0.00	0.14	0.336	o	|	|	|	1.20
31.583	0.00	0.14	0.335	o	|	|	|	1.19
31.667	0.00	0.14	0.334	o	|	|	|	1.19

31.750	0.00	0.14	0.333	o	|	|	|	|	1.19
31.833	0.00	0.14	0.332	o	|	|	|	|	1.18
31.917	0.00	0.14	0.331	o	|	|	|	|	1.18
32.000	0.00	0.14	0.330	o	|	|	|	|	1.18
32.083	0.00	0.14	0.329	o	|	|	|	|	1.17
32.167	0.00	0.14	0.328	o	|	|	|	|	1.17
32.250	0.00	0.14	0.327	o	|	|	|	|	1.17
32.333	0.00	0.14	0.326	o	|	|	|	|	1.16
32.417	0.00	0.14	0.325	o	|	|	|	|	1.16
32.500	0.00	0.14	0.324	o	|	|	|	|	1.16
32.583	0.00	0.14	0.323	o	|	|	|	|	1.15
32.667	0.00	0.14	0.322	o	|	|	|	|	1.15
32.750	0.00	0.14	0.321	o	|	|	|	|	1.15
32.833	0.00	0.14	0.320	o	|	|	|	|	1.14
32.917	0.00	0.14	0.319	o	|	|	|	|	1.14
33.000	0.00	0.14	0.318	o	|	|	|	|	1.14
33.083	0.00	0.14	0.317	o	|	|	|	|	1.13
33.167	0.00	0.14	0.317	o	|	|	|	|	1.13
33.250	0.00	0.14	0.316	o	|	|	|	|	1.13
33.333	0.00	0.14	0.315	o	|	|	|	|	1.13
33.417	0.00	0.14	0.314	o	|	|	|	|	1.12
33.500	0.00	0.14	0.313	o	|	|	|	|	1.12
33.583	0.00	0.14	0.312	o	|	|	|	|	1.12
33.667	0.00	0.14	0.311	o	|	|	|	|	1.11
33.750	0.00	0.14	0.310	o	|	|	|	|	1.11
33.833	0.00	0.14	0.309	o	|	|	|	|	1.11
33.917	0.00	0.14	0.308	o	|	|	|	|	1.10
34.000	0.00	0.14	0.307	o	|	|	|	|	1.10
34.083	0.00	0.14	0.306	o	|	|	|	|	1.10
34.167	0.00	0.14	0.305	o	|	|	|	|	1.09
34.250	0.00	0.14	0.304	o	|	|	|	|	1.09
34.333	0.00	0.14	0.303	o	|	|	|	|	1.09
34.417	0.00	0.14	0.302	o	|	|	|	|	1.08
34.500	0.00	0.14	0.301	o	|	|	|	|	1.08
34.583	0.00	0.14	0.300	o	|	|	|	|	1.08
34.667	0.00	0.14	0.299	o	|	|	|	|	1.08
34.750	0.00	0.14	0.298	o	|	|	|	|	1.07
34.833	0.00	0.14	0.297	o	|	|	|	|	1.07
34.917	0.00	0.14	0.296	o	|	|	|	|	1.07
35.000	0.00	0.14	0.295	o	|	|	|	|	1.06
35.083	0.00	0.14	0.295	o	|	|	|	|	1.06
35.167	0.00	0.14	0.294	o	|	|	|	|	1.06
35.250	0.00	0.14	0.293	o	|	|	|	|	1.05
35.333	0.00	0.14	0.292	o	|	|	|	|	1.05
35.417	0.00	0.14	0.291	o	|	|	|	|	1.05
35.500	0.00	0.14	0.290	o	|	|	|	|	1.04
35.583	0.00	0.14	0.289	o	|	|	|	|	1.04
35.667	0.00	0.14	0.288	o	|	|	|	|	1.04
35.750	0.00	0.14	0.287	o	|	|	|	|	1.04
35.833	0.00	0.13	0.286	o	|	|	|	|	1.03
35.917	0.00	0.13	0.285	o	|	|	|	|	1.03
36.000	0.00	0.13	0.284	o	|	|	|	|	1.03
36.083	0.00	0.13	0.283	o	|	|	|	|	1.02
36.167	0.00	0.13	0.282	o	|	|	|	|	1.02
36.250	0.00	0.13	0.281	o	|	|	|	|	1.02
36.333	0.00	0.13	0.281	o	|	|	|	|	1.01
36.417	0.00	0.13	0.280	o	|	|	|	|	1.01
36.500	0.00	0.13	0.279	o	|	|	|	|	1.01
36.583	0.00	0.13	0.278	o	|	|	|	|	1.01
36.667	0.00	0.13	0.277	o	|	|	|	|	1.00
36.750	0.00	0.13	0.276	o	|	|	|	|	1.00
36.833	0.00	0.13	0.275	o	|	|	|	|	1.00
36.917	0.00	0.13	0.274	o	|	|	|	|	0.99
37.000	0.00	0.13	0.273	o	|	|	|	|	0.99
37.083	0.00	0.13	0.272	o	|	|	|	|	0.99
37.167	0.00	0.13	0.271	o	|	|	|	|	0.98
37.250	0.00	0.13	0.271	o	|	|	|	|	0.98
37.333	0.00	0.13	0.270	o	|	|	|	|	0.98
37.417	0.00	0.13	0.269	o	|	|	|	|	0.97
37.500	0.00	0.13	0.268	o	|	|	|	|	0.97
37.583	0.00	0.13	0.267	o	|	|	|	|	0.97
37.667	0.00	0.13	0.266	o	|	|	|	|	0.96
37.750	0.00	0.13	0.265	o	|	|	|	|	0.96
37.833	0.00	0.13	0.264	o	|	|	|	|	0.96
37.917	0.00	0.13	0.263	o	|	|	|	|	0.95
38.000	0.00	0.13	0.263	o	|	|	|	|	0.95
38.083	0.00	0.13	0.262	o	|	|	|	|	0.95
38.167	0.00	0.13	0.261	o	|	|	|	|	0.95
38.250	0.00	0.13	0.260	o	|	|	|	|	0.94
38.333	0.00	0.12	0.259	o	|	|	|	|	0.94
38.417	0.00	0.12	0.258	o	|	|	|	|	0.94
38.500	0.00	0.12	0.257	o	|	|	|	|	0.93
38.583	0.00	0.12	0.257	o	|	|	|	|	0.93
38.667	0.00	0.12	0.256	o	|	|	|	|	0.93
38.750	0.00	0.12	0.255	o	|	|	|	|	0.92
38.833	0.00	0.12	0.254	o	|	|	|	|	0.92
38.917	0.00	0.12	0.253	o	|	|	|	|	0.92
39.000	0.00	0.12	0.252	o	|	|	|	|	0.91

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39.083    0.00    0.12      0.251  o       |       |       |       |      0.91
39.167    0.00    0.12      0.251  o       |       |       |       |      0.91
39.250    0.00    0.12      0.250  o       |       |       |       |      0.91
39.333    0.00    0.12      0.249  o       |       |       |       |      0.90
39.417    0.00    0.12      0.248  o       |       |       |       |      0.90
39.500    0.00    0.12      0.247  o       |       |       |       |      0.90
39.583    0.00    0.12      0.247  o       |       |       |       |      0.89
39.667    0.00    0.12      0.246  o       |       |       |       |      0.89
39.750    0.00    0.12      0.245  o       |       |       |       |      0.89
39.833    0.00    0.12      0.244  o       |       |       |       |      0.88
39.917    0.00    0.12      0.243  o       |       |       |       |      0.88
40.000    0.00    0.12      0.242  o       |       |       |       |      0.88
40.083    0.00    0.12      0.242  o       |       |       |       |      0.88
40.167    0.00    0.12      0.241  o       |       |       |       |      0.87
40.250    0.00    0.12      0.240  o       |       |       |       |      0.87
40.333    0.00    0.12      0.239  o       |       |       |       |      0.87
40.417    0.00    0.11      0.238  o       |       |       |       |      0.86
40.500    0.00    0.11      0.238  o       |       |       |       |      0.86
40.583    0.00    0.11      0.237  o       |       |       |       |      0.86
40.667    0.00    0.11      0.236  o       |       |       |       |      0.86
40.750    0.00    0.11      0.235  o       |       |       |       |      0.85
40.833    0.00    0.11      0.235  o       |       |       |       |      0.85
40.917    0.00    0.11      0.234  o       |       |       |       |      0.85
41.000    0.00    0.11      0.233  o       |       |       |       |      0.84
41.083    0.00    0.11      0.232  o       |       |       |       |      0.84
41.167    0.00    0.11      0.231  o       |       |       |       |      0.84
41.250    0.00    0.11      0.231  o       |       |       |       |      0.84
41.333    0.00    0.11      0.230  o       |       |       |       |      0.83
41.417    0.00    0.11      0.229  o       |       |       |       |      0.83
41.500    0.00    0.11      0.228  o       |       |       |       |      0.83
41.583    0.00    0.11      0.228  o       |       |       |       |      0.82
41.667    0.00    0.11      0.227  o       |       |       |       |      0.82
41.750    0.00    0.11      0.226  o       |       |       |       |      0.82
41.833    0.00    0.11      0.225  o       |       |       |       |      0.82
41.917    0.00    0.11      0.225  o       |       |       |       |      0.81
42.000    0.00    0.11      0.224  o       |       |       |       |      0.81
42.083    0.00    0.11      0.223  o       |       |       |       |      0.81
42.167    0.00    0.11      0.222  o       |       |       |       |      0.81
42.250    0.00    0.11      0.222  o       |       |       |       |      0.80
42.333    0.00    0.11      0.221  o       |       |       |       |      0.80
42.417    0.00    0.11      0.220  o       |       |       |       |      0.80
42.500    0.00    0.11      0.219  o       |       |       |       |      0.80
42.583    0.00    0.11      0.219  o       |       |       |       |      0.79
42.667    0.00    0.11      0.218  o       |       |       |       |      0.79
42.750    0.00    0.10      0.217  o       |       |       |       |      0.79
42.833    0.00    0.10      0.217  o       |       |       |       |      0.78
42.917    0.00    0.10      0.216  o       |       |       |       |      0.78
43.000    0.00    0.10      0.215  o       |       |       |       |      0.78
43.083    0.00    0.10      0.214  o       |       |       |       |      0.78
43.167    0.00    0.10      0.214  o       |       |       |       |      0.77
43.250    0.00    0.10      0.213  o       |       |       |       |      0.77
43.333    0.00    0.10      0.212  o       |       |       |       |      0.77
43.417    0.00    0.10      0.212  o       |       |       |       |      0.77
43.500    0.00    0.10      0.211  o       |       |       |       |      0.76
43.583    0.00    0.10      0.210  o       |       |       |       |      0.76
43.667    0.00    0.10      0.210  o       |       |       |       |      0.76
43.750    0.00    0.10      0.209  o       |       |       |       |      0.76
43.833    0.00    0.10      0.208  o       |       |       |       |      0.75
43.917    0.00    0.10      0.207  o       |       |       |       |      0.75
      Remaining water in basin =    0.21 (Ac.Ft)
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =   527
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =        0.685 (CFS)
                  Total volume =       0.765 (Ac.Ft)
            Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
      ******************************************************************************
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                    FLOOD HYDROGRAPH ROUTING PROGRAM
                Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                            Study date: 05/07/25

      ---------------------------------------------------------------------

      Program License Serial Number 5006

      ---------------------------------------------------------------------
      ********************* HYDROGRAPH INFORMATION **********************
                    From study/file name: PRO262.rte
      ****************************HYDROGRAPH DATA****************************
                    Number of intervals =    76
                    Time interval =    5.0 (Min.)
                    Maximum/Peak flow rate =       10.033 (CFS)
                    Total volume =       1.314 (Ac.Ft)
             Status of hydrographs being held in storage
                       Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
             Peak (CFS)      0.000     0.000     0.000     0.000     0.000
             Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      ***********************************************************************
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
      Process from Point/Station        1.000 to Point/Station        2.000
      **** RETARDING BASIN ROUTING ****
      _______________________________________________________________________
      User entry of depth-outflow-storage data
      ---------------------------------------------------------------------
      Total number of inflow hydrograph intervals = 76
      Hydrograph time unit =  5.000 (Min.)
      Initial depth in storage basin =   0.00(Ft.)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Initial basin depth =   0.00 (Ft.)
      Initial basin storage =      0.00 (Ac.Ft)
      Initial basin outflow =   0.00 (CFS)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Depth vs. Storage and Depth vs. Discharge data:
       Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
            (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
      ---------------------------------------------------------------------
        0.000      0.000      0.000      0.000        0.000
        1.000      0.276      0.133      0.276        0.276
        2.000      0.584      0.193      0.583        0.585
        3.000      0.930      0.700      0.928        0.932
        3.500      1.118      0.824      1.115        1.121
        4.000      1.316      0.930      1.313        1.319
        4.500      1.528      1.024      1.524        1.532
        4.750      1.637      1.068      1.633        1.641
        5.000      1.749     18.283      1.686        1.812
        6.000      2.231    253.655      1.358        3.104
      ---------------------------------------------------------------------
                     Hydrograph Detention Basin Routing
      ---------------------------------------------------------------------
      Graph values: 'I'= unit inflow; 'O'=outflow at time shown
      ---------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                      Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0       2.5    5.02    7.52   10.03 (Ft.)
 0.083    0.39    0.00      0.001  OI      |       |       |       |     0.00
 0.167    0.88    0.00      0.006  O I     |       |       |       |     0.02
 0.250    1.06    0.01      0.012  O  I    |       |       |       |     0.04
 0.333    1.11    0.01      0.020  O  I    |       |       |       |     0.07
 0.417    1.13    0.01      0.027  O  I    |       |       |       |     0.10
 0.500    1.21    0.02      0.035  O  I    |       |       |       |     0.13
 0.583    1.30    0.02      0.044  O   I   |       |       |       |     0.16
 0.667    1.31    0.03      0.053  O   I   |       |       |       |     0.19
 0.750    1.32    0.03      0.062  O   I   |       |       |       |     0.22
 0.833    1.32    0.03      0.070  O   I   |       |       |       |     0.26
 0.917    1.32    0.04      0.079  O   I   |       |       |       |     0.29
 1.000    1.40    0.04      0.088  O   I   |       |       |       |     0.32
 1.083    1.49    0.05      0.098  O   I   |       |       |       |     0.36
 1.167    1.50    0.05      0.108  O   I   |       |       |       |     0.39
 1.250    1.51    0.06      0.118  O   I   |       |       |       |     0.43
 1.333    1.51    0.06      0.128  O   I   |       |       |       |     0.46
 1.417    1.51    0.07      0.138  O   I   |       |       |       |     0.50
 1.500    1.51    0.07      0.148  O   I   |       |       |       |     0.54
 1.583    1.51    0.08      0.158  O   I   |       |       |       |     0.57
 1.667    1.51    0.08      0.168  O   I   |       |       |       |     0.61
 1.750    1.51    0.09      0.178  O   I   |       |       |       |     0.64
 1.833    1.51    0.09      0.187  O   I   |       |       |       |     0.68
 1.917    1.51    0.10      0.197  O   I   |       |       |       |     0.71
 2.000    1.59    0.10      0.207  O    I  |       |       |       |     0.75
 2.083    1.60    0.10      0.217  O    I  |       |       |       |     0.79
 2.167    1.61    0.11      0.228  O    I  |       |       |       |     0.83
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2.250	1.68	0.11	0.238	O	I	|	|	|	0.86
2.333	1.70	0.12	0.249	O	I	|	|	|	0.90
2.417	1.70	0.13	0.260	O	I	|	|	|	0.94
2.500	1.70	0.13	0.271	O	I	|	|	|	0.98
2.583	1.70	0.13	0.282	O	I	|	|	|	1.02
2.667	1.70	0.14	0.292	O	I	|	|	|	1.05
2.750	1.78	0.14	0.303	O	I	|	|	|	1.09
2.833	1.86	0.14	0.315	O	I	|	|	|	1.13
2.917	1.88	0.14	0.327	O	I	|	|	|	1.17
3.000	1.89	0.15	0.339	O	I	|	|	|	1.20
3.083	1.89	0.15	0.351	O	I	|	|	|	1.24
3.167	1.97	0.15	0.363	O	I	|	|	|	1.28
3.250	2.05	0.15	0.376	O	I	|	|	|	1.32
3.333	2.07	0.16	0.389	O	I	|	|	|	1.37
3.417	2.15	0.16	0.403	O	I	|	|	|	1.41
3.500	2.32	0.16	0.417	O	I|	|	|	|	1.46
3.583	2.50	0.16	0.432	O	I|	|	|	|	1.51
3.667	2.61	0.17	0.449	O	I	|	|	|	1.56
3.750	2.71	0.17	0.466	O	I	|	|	|	1.62
3.833	2.81	0.17	0.484	O	I	|	|	|	1.67
3.917	2.90	0.18	0.502	O	|I	|	|	|	1.73
4.000	3.00	0.18	0.521	O	|I	|	|	|	1.80
4.083	3.09	0.18	0.541	O	|I	|	|	|	1.86
4.167	3.26	0.19	0.562	O	| I	|	|	|	1.93
4.250	3.44	0.19	0.584	O	| I	|	|	|	2.00
4.333	3.63	0.23	0.606	O	| I	|	|	|	2.06
4.417	3.82	0.26	0.630	O	| I	|	|	|	2.13
4.500	3.93	0.30	0.655	O	| I	|	|	|	2.21
4.583	4.04	0.33	0.680	|O	| I	|	|	|	2.28
4.667	4.21	0.37	0.706	|O	| I	|	|	|	2.35
4.750	4.39	0.41	0.733	|O	| I	|	|	|	2.43
4.833	4.50	0.45	0.761	|O	| I	|	|	|	2.51
4.917	4.60	0.49	0.789	|O	| I	|	|	|	2.59
5.000	4.78	0.54	0.818	|O	| I|	|	|	|	2.68
5.083	5.27	0.58	0.849	|O	| I	|	|	|	2.76
5.167	6.10	0.63	0.883	| O	| |	I	|	|	2.87
5.250	6.85	0.69	0.923	| O	| |	I	|	|	2.98
5.333	7.46	0.72	0.968	| O	| |	I	|	|	3.10
5.417	8.20	0.76	1.017	| O	| |	| I	|	3.23
5.500	10.03	0.80	1.074	| O	| |	|	I	3.38
5.583	8.12	0.83	1.131	| O	| |	I|	|	3.53
5.667	3.90	0.85	1.167	| O	| I	|	|	|	3.62
5.750	2.16	0.86	1.182	| O	I |	|	|	|	3.66
5.833	1.39	0.86	1.188	| O	I |	|	|	|	3.68
5.917	0.88	0.86	1.190	| O	|	|	|	|	3.68
6.000	0.57	0.86	1.189	|IO	|	|	|	|	3.68
6.083	0.28	0.86	1.186	I O	|	|	|	|	3.67
6.167	0.07	0.86	1.181	I O	|	|	|	|	3.66
6.250	0.02	0.85	1.176	I O	|	|	|	|	3.65
6.333	0.01	0.85	1.170	I O	|	|	|	|	3.63
6.417	0.00	0.85	1.164	I O	|	|	|	|	3.62
6.500	0.00	0.85	1.158	I O	|	|	|	|	3.60
6.583	0.00	0.84	1.152	I O	|	|	|	|	3.59
6.667	0.00	0.84	1.146	I O	|	|	|	|	3.57
6.750	0.00	0.84	1.141	I O	|	|	|	|	3.56
6.833	0.00	0.83	1.135	I O	|	|	|	|	3.54
6.917	0.00	0.83	1.129	I O	|	|	|	|	3.53
7.000	0.00	0.83	1.124	I O	|	|	|	|	3.51
7.083	0.00	0.82	1.118	I O	|	|	|	|	3.50
7.167	0.00	0.82	1.112	I O	|	|	|	|	3.48
7.250	0.00	0.82	1.107	I O	|	|	|	|	3.47
7.333	0.00	0.81	1.101	I O	|	|	|	|	3.45
7.417	0.00	0.81	1.095	I O	|	|	|	|	3.44
7.500	0.00	0.81	1.090	I O	|	|	|	|	3.43
7.583	0.00	0.80	1.084	I O	|	|	|	|	3.41
7.667	0.00	0.80	1.079	I O	|	|	|	|	3.40
7.750	0.00	0.79	1.073	I O	|	|	|	|	3.38
7.833	0.00	0.79	1.068	I O	|	|	|	|	3.37
7.917	0.00	0.79	1.062	I O	|	|	|	|	3.35
8.000	0.00	0.78	1.057	I O	|	|	|	|	3.34
8.083	0.00	0.78	1.052	I O	|	|	|	|	3.32
8.167	0.00	0.78	1.046	I O	|	|	|	|	3.31
8.250	0.00	0.77	1.041	I O	|	|	|	|	3.29
8.333	0.00	0.77	1.036	I O	|	|	|	|	3.28
8.417	0.00	0.77	1.030	I O	|	|	|	|	3.27
8.500	0.00	0.76	1.025	I O	|	|	|	|	3.25
8.583	0.00	0.76	1.020	I O	|	|	|	|	3.24
8.667	0.00	0.76	1.015	I O	|	|	|	|	3.22
8.750	0.00	0.75	1.009	I O	|	|	|	|	3.21
8.833	0.00	0.75	1.004	I O	|	|	|	|	3.20
8.917	0.00	0.75	0.999	I O	|	|	|	|	3.18
9.000	0.00	0.74	0.994	I O	|	|	|	|	3.17
9.083	0.00	0.74	0.989	I O	|	|	|	|	3.16
9.167	0.00	0.74	0.984	I O	|	|	|	|	3.14
9.250	0.00	0.73	0.979	I O	|	|	|	|	3.13
9.333	0.00	0.73	0.974	I O	|	|	|	|	3.12

9.417	0.00	0.73	0.969	I O					3.10
9.500	0.00	0.72	0.964	I O					3.09
9.583	0.00	0.72	0.959	I O					3.08
9.667	0.00	0.72	0.954	I O					3.06
9.750	0.00	0.71	0.949	I O					3.05
9.833	0.00	0.71	0.944	I O					3.04
9.917	0.00	0.71	0.939	I O					3.02
10.000	0.00	0.70	0.934	I O					3.01
10.083	0.00	0.70	0.929	I O					3.00
10.167	0.00	0.69	0.925	I O					2.98
10.250	0.00	0.69	0.920	I O					2.97
10.333	0.00	0.68	0.915	I O					2.96
10.417	0.00	0.67	0.911	I O					2.94
10.500	0.00	0.66	0.906	I O					2.93
10.583	0.00	0.66	0.901	I O					2.92
10.667	0.00	0.65	0.897	I O					2.90
10.750	0.00	0.64	0.892	I O					2.89
10.833	0.00	0.64	0.888	I O					2.88
10.917	0.00	0.63	0.884	I O					2.87
11.000	0.00	0.63	0.879	IO					2.85
11.083	0.00	0.62	0.875	IO					2.84
11.167	0.00	0.61	0.871	IO					2.83
11.250	0.00	0.61	0.867	IO					2.82
11.333	0.00	0.60	0.862	IO					2.80
11.417	0.00	0.59	0.858	IO					2.79
11.500	0.00	0.59	0.854	IO					2.78
11.583	0.00	0.58	0.850	IO					2.77
11.667	0.00	0.58	0.846	IO					2.76
11.750	0.00	0.57	0.842	IO					2.75
11.833	0.00	0.57	0.838	IO					2.73
11.917	0.00	0.56	0.834	IO					2.72
12.000	0.00	0.55	0.831	IO					2.71
12.083	0.00	0.55	0.827	IO					2.70
12.167	0.00	0.54	0.823	IO					2.69
12.250	0.00	0.54	0.819	IO					2.68
12.333	0.00	0.53	0.816	IO					2.67
12.417	0.00	0.53	0.812	IO					2.66
12.500	0.00	0.52	0.808	IO					2.65
12.583	0.00	0.52	0.805	IO					2.64
12.667	0.00	0.51	0.801	IO					2.63
12.750	0.00	0.51	0.798	IO					2.62
12.833	0.00	0.50	0.794	IO					2.61
12.917	0.00	0.50	0.791	IO					2.60
13.000	0.00	0.49	0.787	IO					2.59
13.083	0.00	0.49	0.784	IO					2.58
13.167	0.00	0.48	0.781	IO					2.57
13.250	0.00	0.48	0.777	IO					2.56
13.333	0.00	0.47	0.774	IO					2.55
13.417	0.00	0.47	0.771	IO					2.54
13.500	0.00	0.46	0.768	IO					2.53
13.583	0.00	0.46	0.765	IO					2.52
13.667	0.00	0.45	0.761	IO					2.51
13.750	0.00	0.45	0.758	IO					2.50
13.833	0.00	0.44	0.755	IO					2.49
13.917	0.00	0.44	0.752	IO					2.49
14.000	0.00	0.44	0.749	IO					2.48
14.083	0.00	0.43	0.746	IO					2.47
14.167	0.00	0.43	0.743	IO					2.46
14.250	0.00	0.42	0.740	IO					2.45
14.333	0.00	0.42	0.737	IO					2.44
14.417	0.00	0.41	0.735	IO					2.44
14.500	0.00	0.41	0.732	IO					2.43
14.583	0.00	0.41	0.729	IO					2.42
14.667	0.00	0.40	0.726	IO					2.41
14.750	0.00	0.40	0.723	IO					2.40
14.833	0.00	0.39	0.721	IO					2.40
14.917	0.00	0.39	0.718	IO					2.39
15.000	0.00	0.39	0.715	IO					2.38
15.083	0.00	0.38	0.713	IO					2.37
15.167	0.00	0.38	0.710	IO					2.36
15.250	0.00	0.37	0.707	IO					2.36
15.333	0.00	0.37	0.705	IO					2.35
15.417	0.00	0.37	0.702	IO					2.34
15.500	0.00	0.36	0.700	IO					2.33
15.583	0.00	0.36	0.697	IO					2.33
15.667	0.00	0.36	0.695	IO					2.32
15.750	0.00	0.35	0.693	IO					2.31
15.833	0.00	0.35	0.690	IO					2.31
15.917	0.00	0.34	0.688	IO					2.30
16.000	0.00	0.34	0.685	IO					2.29
16.083	0.00	0.34	0.683	IO					2.29
16.167	0.00	0.33	0.681	IO					2.28
16.250	0.00	0.33	0.678	IO					2.27
16.333	0.00	0.33	0.676	IO					2.27
16.417	0.00	0.32	0.674	IO					2.26
16.500	0.00	0.32	0.672	IO					2.25

16.583	0.00	0.32	0.669	IO	|	|	|	|	2.25
16.667	0.00	0.32	0.667	IO	|	|	|	|	2.24
16.750	0.00	0.31	0.665	O	|	|	|	|	2.23
16.833	0.00	0.31	0.663	O	|	|	|	|	2.23
16.917	0.00	0.31	0.661	O	|	|	|	|	2.22
17.000	0.00	0.30	0.659	O	|	|	|	|	2.22
17.083	0.00	0.30	0.657	O	|	|	|	|	2.21
17.167	0.00	0.30	0.655	O	|	|	|	|	2.20
17.250	0.00	0.29	0.653	O	|	|	|	|	2.20
17.333	0.00	0.29	0.651	O	|	|	|	|	2.19
17.417	0.00	0.29	0.649	O	|	|	|	|	2.19
17.500	0.00	0.28	0.647	O	|	|	|	|	2.18
17.583	0.00	0.28	0.645	O	|	|	|	|	2.18
17.667	0.00	0.28	0.643	O	|	|	|	|	2.17
17.750	0.00	0.28	0.641	O	|	|	|	|	2.16
17.833	0.00	0.27	0.639	O	|	|	|	|	2.16
17.917	0.00	0.27	0.637	O	|	|	|	|	2.15
18.000	0.00	0.27	0.635	O	|	|	|	|	2.15
18.083	0.00	0.27	0.633	O	|	|	|	|	2.14
18.167	0.00	0.26	0.632	O	|	|	|	|	2.14
18.250	0.00	0.26	0.630	O	|	|	|	|	2.13
18.333	0.00	0.26	0.628	O	|	|	|	|	2.13
18.417	0.00	0.25	0.626	O	|	|	|	|	2.12
18.500	0.00	0.25	0.624	O	|	|	|	|	2.12
18.583	0.00	0.25	0.623	O	|	|	|	|	2.11
18.667	0.00	0.25	0.621	O	|	|	|	|	2.11
18.750	0.00	0.24	0.619	O	|	|	|	|	2.10
18.833	0.00	0.24	0.618	O	|	|	|	|	2.10
18.917	0.00	0.24	0.616	O	|	|	|	|	2.09
19.000	0.00	0.24	0.614	O	|	|	|	|	2.09
19.083	0.00	0.24	0.613	O	|	|	|	|	2.08
19.167	0.00	0.23	0.611	O	|	|	|	|	2.08
19.250	0.00	0.23	0.610	O	|	|	|	|	2.07
19.333	0.00	0.23	0.608	O	|	|	|	|	2.07
19.417	0.00	0.23	0.606	O	|	|	|	|	2.06
19.500	0.00	0.22	0.605	O	|	|	|	|	2.06
19.583	0.00	0.22	0.603	O	|	|	|	|	2.06
19.667	0.00	0.22	0.602	O	|	|	|	|	2.05
19.750	0.00	0.22	0.600	O	|	|	|	|	2.05
19.833	0.00	0.21	0.599	O	|	|	|	|	2.04
19.917	0.00	0.21	0.597	O	|	|	|	|	2.04
20.000	0.00	0.21	0.596	O	|	|	|	|	2.03
20.083	0.00	0.21	0.594	O	|	|	|	|	2.03
20.167	0.00	0.21	0.593	O	|	|	|	|	2.03
20.250	0.00	0.20	0.592	O	|	|	|	|	2.02
20.333	0.00	0.20	0.590	O	|	|	|	|	2.02
20.417	0.00	0.20	0.589	O	|	|	|	|	2.01
20.500	0.00	0.20	0.587	O	|	|	|	|	2.01
20.583	0.00	0.20	0.586	O	|	|	|	|	2.01
20.667	0.00	0.19	0.585	O	|	|	|	|	2.00
20.750	0.00	0.19	0.583	O	|	|	|	|	2.00
20.833	0.00	0.19	0.582	O	|	|	|	|	1.99
20.917	0.00	0.19	0.581	O	|	|	|	|	1.99
21.000	0.00	0.19	0.579	O	|	|	|	|	1.99
21.083	0.00	0.19	0.578	O	|	|	|	|	1.98
21.167	0.00	0.19	0.577	O	|	|	|	|	1.98
21.250	0.00	0.19	0.575	O	|	|	|	|	1.97
21.333	0.00	0.19	0.574	O	|	|	|	|	1.97
21.417	0.00	0.19	0.573	O	|	|	|	|	1.96
21.500	0.00	0.19	0.572	O	|	|	|	|	1.96
21.583	0.00	0.19	0.570	O	|	|	|	|	1.96
21.667	0.00	0.19	0.569	O	|	|	|	|	1.95
21.750	0.00	0.19	0.568	O	|	|	|	|	1.95
21.833	0.00	0.19	0.566	O	|	|	|	|	1.94
21.917	0.00	0.19	0.565	O	|	|	|	|	1.94
22.000	0.00	0.19	0.564	O	|	|	|	|	1.93
22.083	0.00	0.19	0.562	O	|	|	|	|	1.93
22.167	0.00	0.19	0.561	O	|	|	|	|	1.93
22.250	0.00	0.19	0.560	O	|	|	|	|	1.92
22.333	0.00	0.19	0.558	O	|	|	|	|	1.92
22.417	0.00	0.19	0.557	O	|	|	|	|	1.91
22.500	0.00	0.19	0.556	O	|	|	|	|	1.91
22.583	0.00	0.19	0.555	O	|	|	|	|	1.90
22.667	0.00	0.19	0.553	O	|	|	|	|	1.90
22.750	0.00	0.19	0.552	O	|	|	|	|	1.90
22.833	0.00	0.19	0.551	O	|	|	|	|	1.89
22.917	0.00	0.19	0.549	O	|	|	|	|	1.89
23.000	0.00	0.19	0.548	O	|	|	|	|	1.88
23.083	0.00	0.19	0.547	O	|	|	|	|	1.88
23.167	0.00	0.19	0.546	O	|	|	|	|	1.88
23.250	0.00	0.19	0.544	O	|	|	|	|	1.87
23.333	0.00	0.19	0.543	O	|	|	|	|	1.87
23.417	0.00	0.18	0.542	O	|	|	|	|	1.86
23.500	0.00	0.18	0.541	O	|	|	|	|	1.86
23.583	0.00	0.18	0.539	O	|	|	|	|	1.85
23.667	0.00	0.18	0.538	O	|	|	|	|	1.85

23.750	0.00	0.18	0.537	o	|	|	|	1.85
23.833	0.00	0.18	0.535	o	|	|	|	1.84
23.917	0.00	0.18	0.534	o	|	|	|	1.84
24.000	0.00	0.18	0.533	o	|	|	|	1.83
24.083	0.00	0.18	0.532	o	|	|	|	1.83
24.167	0.00	0.18	0.530	o	|	|	|	1.83
24.250	0.00	0.18	0.529	o	|	|	|	1.82
24.333	0.00	0.18	0.528	o	|	|	|	1.82
24.417	0.00	0.18	0.527	o	|	|	|	1.81
24.500	0.00	0.18	0.525	o	|	|	|	1.81
24.583	0.00	0.18	0.524	o	|	|	|	1.81
24.667	0.00	0.18	0.523	o	|	|	|	1.80
24.750	0.00	0.18	0.522	o	|	|	|	1.80
24.833	0.00	0.18	0.520	o	|	|	|	1.79
24.917	0.00	0.18	0.519	o	|	|	|	1.79
25.000	0.00	0.18	0.518	o	|	|	|	1.79
25.083	0.00	0.18	0.517	o	|	|	|	1.78
25.167	0.00	0.18	0.515	o	|	|	|	1.78
25.250	0.00	0.18	0.514	o	|	|	|	1.77
25.333	0.00	0.18	0.513	o	|	|	|	1.77
25.417	0.00	0.18	0.512	o	|	|	|	1.77
25.500	0.00	0.18	0.510	o	|	|	|	1.76
25.583	0.00	0.18	0.509	o	|	|	|	1.76
25.667	0.00	0.18	0.508	o	|	|	|	1.75
25.750	0.00	0.18	0.507	o	|	|	|	1.75
25.833	0.00	0.18	0.506	o	|	|	|	1.75
25.917	0.00	0.18	0.504	o	|	|	|	1.74
26.000	0.00	0.18	0.503	o	|	|	|	1.74
26.083	0.00	0.18	0.502	o	|	|	|	1.73
26.167	0.00	0.18	0.501	o	|	|	|	1.73
26.250	0.00	0.18	0.499	o	|	|	|	1.73
26.333	0.00	0.18	0.498	o	|	|	|	1.72
26.417	0.00	0.18	0.497	o	|	|	|	1.72
26.500	0.00	0.18	0.496	o	|	|	|	1.71
26.583	0.00	0.18	0.495	o	|	|	|	1.71
26.667	0.00	0.18	0.493	o	|	|	|	1.71
26.750	0.00	0.18	0.492	o	|	|	|	1.70
26.833	0.00	0.17	0.491	o	|	|	|	1.70
26.917	0.00	0.17	0.490	o	|	|	|	1.69
27.000	0.00	0.17	0.489	o	|	|	|	1.69
27.083	0.00	0.17	0.487	o	|	|	|	1.69
27.167	0.00	0.17	0.486	o	|	|	|	1.68
27.250	0.00	0.17	0.485	o	|	|	|	1.68
27.333	0.00	0.17	0.484	o	|	|	|	1.67
27.417	0.00	0.17	0.483	o	|	|	|	1.67
27.500	0.00	0.17	0.481	o	|	|	|	1.67
27.583	0.00	0.17	0.480	o	|	|	|	1.66
27.667	0.00	0.17	0.479	o	|	|	|	1.66
27.750	0.00	0.17	0.478	o	|	|	|	1.66
27.833	0.00	0.17	0.477	o	|	|	|	1.65
27.917	0.00	0.17	0.475	o	|	|	|	1.65
28.000	0.00	0.17	0.474	o	|	|	|	1.64
28.083	0.00	0.17	0.473	o	|	|	|	1.64
28.167	0.00	0.17	0.472	o	|	|	|	1.64
28.250	0.00	0.17	0.471	o	|	|	|	1.63
28.333	0.00	0.17	0.470	o	|	|	|	1.63
28.417	0.00	0.17	0.468	o	|	|	|	1.62
28.500	0.00	0.17	0.467	o	|	|	|	1.62
28.583	0.00	0.17	0.466	o	|	|	|	1.62
28.667	0.00	0.17	0.465	o	|	|	|	1.61
28.750	0.00	0.17	0.464	o	|	|	|	1.61
28.833	0.00	0.17	0.463	o	|	|	|	1.61
28.917	0.00	0.17	0.461	o	|	|	|	1.60
29.000	0.00	0.17	0.460	o	|	|	|	1.60
29.083	0.00	0.17	0.459	o	|	|	|	1.59
29.167	0.00	0.17	0.458	o	|	|	|	1.59
29.250	0.00	0.17	0.457	o	|	|	|	1.59
29.333	0.00	0.17	0.456	o	|	|	|	1.58
29.417	0.00	0.17	0.454	o	|	|	|	1.58
29.500	0.00	0.17	0.453	o	|	|	|	1.58
29.583	0.00	0.17	0.452	o	|	|	|	1.57
29.667	0.00	0.17	0.451	o	|	|	|	1.57
29.750	0.00	0.17	0.450	o	|	|	|	1.56
29.833	0.00	0.17	0.449	o	|	|	|	1.56
29.917	0.00	0.17	0.448	o	|	|	|	1.56
30.000	0.00	0.17	0.446	o	|	|	|	1.55
30.083	0.00	0.17	0.445	o	|	|	|	1.55
30.167	0.00	0.17	0.444	o	|	|	|	1.55
30.250	0.00	0.17	0.443	o	|	|	|	1.54
30.333	0.00	0.17	0.442	o	|	|	|	1.54
30.417	0.00	0.17	0.441	o	|	|	|	1.53
30.500	0.00	0.16	0.440	o	|	|	|	1.53
30.583	0.00	0.16	0.438	o	|	|	|	1.53
30.667	0.00	0.16	0.437	o	|	|	|	1.52
30.750	0.00	0.16	0.436	o	|	|	|	1.52
30.833	0.00	0.16	0.435	o	|	|	|	1.52

30.917	0.00	0.16	0.434	o	|	|	|	|	1.51
31.000	0.00	0.16	0.433	o	|	|	|	|	1.51
31.083	0.00	0.16	0.432	o	|	|	|	|	1.51
31.167	0.00	0.16	0.431	o	|	|	|	|	1.50
31.250	0.00	0.16	0.429	o	|	|	|	|	1.50
31.333	0.00	0.16	0.428	o	|	|	|	|	1.49
31.417	0.00	0.16	0.427	o	|	|	|	|	1.49
31.500	0.00	0.16	0.426	o	|	|	|	|	1.49
31.583	0.00	0.16	0.425	o	|	|	|	|	1.48
31.667	0.00	0.16	0.424	o	|	|	|	|	1.48
31.750	0.00	0.16	0.423	o	|	|	|	|	1.48
31.833	0.00	0.16	0.422	o	|	|	|	|	1.47
31.917	0.00	0.16	0.420	o	|	|	|	|	1.47
32.000	0.00	0.16	0.419	o	|	|	|	|	1.47
32.083	0.00	0.16	0.418	o	|	|	|	|	1.46
32.167	0.00	0.16	0.417	o	|	|	|	|	1.46
32.250	0.00	0.16	0.416	o	|	|	|	|	1.45
32.333	0.00	0.16	0.415	o	|	|	|	|	1.45
32.417	0.00	0.16	0.414	o	|	|	|	|	1.45
32.500	0.00	0.16	0.413	o	|	|	|	|	1.44
32.583	0.00	0.16	0.412	o	|	|	|	|	1.44
32.667	0.00	0.16	0.411	o	|	|	|	|	1.44
32.750	0.00	0.16	0.409	o	|	|	|	|	1.43
32.833	0.00	0.16	0.408	o	|	|	|	|	1.43
32.917	0.00	0.16	0.407	o	|	|	|	|	1.43
33.000	0.00	0.16	0.406	o	|	|	|	|	1.42
33.083	0.00	0.16	0.405	o	|	|	|	|	1.42
33.167	0.00	0.16	0.404	o	|	|	|	|	1.42
33.250	0.00	0.16	0.403	o	|	|	|	|	1.41
33.333	0.00	0.16	0.402	o	|	|	|	|	1.41
33.417	0.00	0.16	0.401	o	|	|	|	|	1.40
33.500	0.00	0.16	0.400	o	|	|	|	|	1.40
33.583	0.00	0.16	0.399	o	|	|	|	|	1.40
33.667	0.00	0.16	0.397	o	|	|	|	|	1.39
33.750	0.00	0.16	0.396	o	|	|	|	|	1.39
33.833	0.00	0.16	0.395	o	|	|	|	|	1.39
33.917	0.00	0.16	0.394	o	|	|	|	|	1.38
34.000	0.00	0.16	0.393	o	|	|	|	|	1.38
34.083	0.00	0.16	0.392	o	|	|	|	|	1.38
34.167	0.00	0.16	0.391	o	|	|	|	|	1.37
34.250	0.00	0.16	0.390	o	|	|	|	|	1.37
34.333	0.00	0.15	0.389	o	|	|	|	|	1.37
34.417	0.00	0.15	0.388	o	|	|	|	|	1.36
34.500	0.00	0.15	0.387	o	|	|	|	|	1.36
34.583	0.00	0.15	0.386	o	|	|	|	|	1.36
34.667	0.00	0.15	0.385	o	|	|	|	|	1.35
34.750	0.00	0.15	0.384	o	|	|	|	|	1.35
34.833	0.00	0.15	0.383	o	|	|	|	|	1.35
34.917	0.00	0.15	0.381	o	|	|	|	|	1.34
35.000	0.00	0.15	0.380	o	|	|	|	|	1.34
35.083	0.00	0.15	0.379	o	|	|	|	|	1.34
35.167	0.00	0.15	0.378	o	|	|	|	|	1.33
35.250	0.00	0.15	0.377	o	|	|	|	|	1.33
35.333	0.00	0.15	0.376	o	|	|	|	|	1.33
35.417	0.00	0.15	0.375	o	|	|	|	|	1.32
35.500	0.00	0.15	0.374	o	|	|	|	|	1.32
35.583	0.00	0.15	0.373	o	|	|	|	|	1.32
35.667	0.00	0.15	0.372	o	|	|	|	|	1.31
35.750	0.00	0.15	0.371	o	|	|	|	|	1.31
35.833	0.00	0.15	0.370	o	|	|	|	|	1.30
35.917	0.00	0.15	0.369	o	|	|	|	|	1.30
36.000	0.00	0.15	0.368	o	|	|	|	|	1.30
36.083	0.00	0.15	0.367	o	|	|	|	|	1.29
36.167	0.00	0.15	0.366	o	|	|	|	|	1.29
36.250	0.00	0.15	0.365	o	|	|	|	|	1.29
36.333	0.00	0.15	0.364	o	|	|	|	|	1.28
36.417	0.00	0.15	0.363	o	|	|	|	|	1.28
36.500	0.00	0.15	0.362	o	|	|	|	|	1.28
36.583	0.00	0.15	0.361	o	|	|	|	|	1.27
36.667	0.00	0.15	0.360	o	|	|	|	|	1.27
36.750	0.00	0.15	0.359	o	|	|	|	|	1.27
36.833	0.00	0.15	0.358	o	|	|	|	|	1.26
36.917	0.00	0.15	0.356	o	|	|	|	|	1.26
37.000	0.00	0.15	0.355	o	|	|	|	|	1.26
37.083	0.00	0.15	0.354	o	|	|	|	|	1.25
37.167	0.00	0.15	0.353	o	|	|	|	|	1.25
37.250	0.00	0.15	0.352	o	|	|	|	|	1.25
37.333	0.00	0.15	0.351	o	|	|	|	|	1.24
37.417	0.00	0.15	0.350	o	|	|	|	|	1.24
37.500	0.00	0.15	0.349	o	|	|	|	|	1.24
37.583	0.00	0.15	0.348	o	|	|	|	|	1.23
37.667	0.00	0.15	0.347	o	|	|	|	|	1.23
37.750	0.00	0.15	0.346	o	|	|	|	|	1.23
37.833	0.00	0.15	0.345	o	|	|	|	|	1.23
37.917	0.00	0.15	0.344	o	|	|	|	|	1.22
38.000	0.00	0.15	0.343	o	|	|	|	|	1.22

38.083	0.00	0.15	0.342	o	|	|	|	|	1.22
38.167	0.00	0.15	0.341	o	|	|	|	|	1.21
38.250	0.00	0.15	0.340	o	|	|	|	|	1.21
38.333	0.00	0.15	0.339	o	|	|	|	|	1.21
38.417	0.00	0.15	0.338	o	|	|	|	|	1.20
38.500	0.00	0.14	0.337	o	|	|	|	|	1.20
38.583	0.00	0.14	0.336	o	|	|	|	|	1.20
38.667	0.00	0.14	0.335	o	|	|	|	|	1.19
38.750	0.00	0.14	0.334	o	|	|	|	|	1.19
38.833	0.00	0.14	0.333	o	|	|	|	|	1.19
38.917	0.00	0.14	0.332	o	|	|	|	|	1.18
39.000	0.00	0.14	0.331	o	|	|	|	|	1.18
39.083	0.00	0.14	0.330	o	|	|	|	|	1.18
39.167	0.00	0.14	0.329	o	|	|	|	|	1.17
39.250	0.00	0.14	0.328	o	|	|	|	|	1.17
39.333	0.00	0.14	0.327	o	|	|	|	|	1.17
39.417	0.00	0.14	0.326	o	|	|	|	|	1.16
39.500	0.00	0.14	0.325	o	|	|	|	|	1.16
39.583	0.00	0.14	0.324	o	|	|	|	|	1.16
39.667	0.00	0.14	0.323	o	|	|	|	|	1.15
39.750	0.00	0.14	0.322	o	|	|	|	|	1.15
39.833	0.00	0.14	0.321	o	|	|	|	|	1.15
39.917	0.00	0.14	0.321	o	|	|	|	|	1.14
40.000	0.00	0.14	0.320	o	|	|	|	|	1.14
40.083	0.00	0.14	0.319	o	|	|	|	|	1.14
40.167	0.00	0.14	0.318	o	|	|	|	|	1.14
40.250	0.00	0.14	0.317	o	|	|	|	|	1.13
40.333	0.00	0.14	0.316	o	|	|	|	|	1.13
40.417	0.00	0.14	0.315	o	|	|	|	|	1.13
40.500	0.00	0.14	0.314	o	|	|	|	|	1.12
40.583	0.00	0.14	0.313	o	|	|	|	|	1.12
40.667	0.00	0.14	0.312	o	|	|	|	|	1.12
40.750	0.00	0.14	0.311	o	|	|	|	|	1.11
40.833	0.00	0.14	0.310	o	|	|	|	|	1.11
40.917	0.00	0.14	0.309	o	|	|	|	|	1.11
41.000	0.00	0.14	0.308	o	|	|	|	|	1.10
41.083	0.00	0.14	0.307	o	|	|	|	|	1.10
41.167	0.00	0.14	0.306	o	|	|	|	|	1.10
41.250	0.00	0.14	0.305	o	|	|	|	|	1.09
41.333	0.00	0.14	0.304	o	|	|	|	|	1.09
41.417	0.00	0.14	0.303	o	|	|	|	|	1.09
41.500	0.00	0.14	0.302	o	|	|	|	|	1.09
41.583	0.00	0.14	0.301	o	|	|	|	|	1.08
41.667	0.00	0.14	0.300	o	|	|	|	|	1.08
41.750	0.00	0.14	0.299	o	|	|	|	|	1.08
41.833	0.00	0.14	0.298	o	|	|	|	|	1.07
41.917	0.00	0.14	0.297	o	|	|	|	|	1.07
42.000	0.00	0.14	0.297	o	|	|	|	|	1.07
42.083	0.00	0.14	0.296	o	|	|	|	|	1.06
42.167	0.00	0.14	0.295	o	|	|	|	|	1.06
42.250	0.00	0.14	0.294	o	|	|	|	|	1.06
42.333	0.00	0.14	0.293	o	|	|	|	|	1.05
42.417	0.00	0.14	0.292	o	|	|	|	|	1.05
42.500	0.00	0.14	0.291	o	|	|	|	|	1.05
42.583	0.00	0.14	0.290	o	|	|	|	|	1.05
42.667	0.00	0.14	0.289	o	|	|	|	|	1.04
42.750	0.00	0.14	0.288	o	|	|	|	|	1.04
42.833	0.00	0.14	0.287	o	|	|	|	|	1.04
42.917	0.00	0.13	0.286	o	|	|	|	|	1.03
43.000	0.00	0.13	0.285	o	|	|	|	|	1.03
43.083	0.00	0.13	0.284	o	|	|	|	|	1.03
43.167	0.00	0.13	0.283	o	|	|	|	|	1.02
43.250	0.00	0.13	0.283	o	|	|	|	|	1.02
43.333	0.00	0.13	0.282	o	|	|	|	|	1.02
43.417	0.00	0.13	0.281	o	|	|	|	|	1.02
43.500	0.00	0.13	0.280	o	|	|	|	|	1.01
43.583	0.00	0.13	0.279	o	|	|	|	|	1.01
43.667	0.00	0.13	0.278	o	|	|	|	|	1.01
43.750	0.00	0.13	0.277	o	|	|	|	|	1.00
43.833	0.00	0.13	0.276	o	|	|	|	|	1.00
43.917	0.00	0.13	0.275	o	|	|	|	|	1.00
44.000	0.00	0.13	0.274	o	|	|	|	|	0.99
44.083	0.00	0.13	0.273	o	|	|	|	|	0.99
44.167	0.00	0.13	0.272	o	|	|	|	|	0.99
44.250	0.00	0.13	0.272	o	|	|	|	|	0.98
44.333	0.00	0.13	0.271	o	|	|	|	|	0.98
44.417	0.00	0.13	0.270	o	|	|	|	|	0.98
44.500	0.00	0.13	0.269	o	|	|	|	|	0.97
44.583	0.00	0.13	0.268	o	|	|	|	|	0.97
44.667	0.00	0.13	0.267	o	|	|	|	|	0.97
44.750	0.00	0.13	0.266	o	|	|	|	|	0.96
44.833	0.00	0.13	0.265	o	|	|	|	|	0.96
44.917	0.00	0.13	0.264	o	|	|	|	|	0.96
45.000	0.00	0.13	0.264	o	|	|	|	|	0.95
45.083	0.00	0.13	0.263	o	|	|	|	|	0.95
45.167	0.00	0.13	0.262	o	|	|	|	|	0.95

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45.250    0.00    0.13      0.261  o       |       |       |       |      0.95
45.333    0.00    0.13      0.260  o       |       |       |       |      0.94
45.417    0.00    0.12      0.259  o       |       |       |       |      0.94
45.500    0.00    0.12      0.258  o       |       |       |       |      0.94
45.583    0.00    0.12      0.257  o       |       |       |       |      0.93
45.667    0.00    0.12      0.257  o       |       |       |       |      0.93
45.750    0.00    0.12      0.256  o       |       |       |       |      0.93
45.833    0.00    0.12      0.255  o       |       |       |       |      0.92
45.917    0.00    0.12      0.254  o       |       |       |       |      0.92
46.000    0.00    0.12      0.253  o       |       |       |       |      0.92
46.083    0.00    0.12      0.252  o       |       |       |       |      0.91
46.167    0.00    0.12      0.252  o       |       |       |       |      0.91
46.250    0.00    0.12      0.251  o       |       |       |       |      0.91
46.333    0.00    0.12      0.250  o       |       |       |       |      0.91
46.417    0.00    0.12      0.249  o       |       |       |       |      0.90
46.500    0.00    0.12      0.248  o       |       |       |       |      0.90
46.583    0.00    0.12      0.247  o       |       |       |       |      0.90
46.667    0.00    0.12      0.247  o       |       |       |       |      0.89
46.750    0.00    0.12      0.246  o       |       |       |       |      0.89
46.833    0.00    0.12      0.245  o       |       |       |       |      0.89
46.917    0.00    0.12      0.244  o       |       |       |       |      0.88
47.000    0.00    0.12      0.243  o       |       |       |       |      0.88
47.083    0.00    0.12      0.243  o       |       |       |       |      0.88
47.167    0.00    0.12      0.242  o       |       |       |       |      0.88
47.250    0.00    0.12      0.241  o       |       |       |       |      0.87
47.333    0.00    0.12      0.240  o       |       |       |       |      0.87
47.417    0.00    0.12      0.239  o       |       |       |       |      0.87
47.500    0.00    0.11      0.239  o       |       |       |       |      0.86
47.583    0.00    0.11      0.238  o       |       |       |       |      0.86
47.667    0.00    0.11      0.237  o       |       |       |       |      0.86
47.750    0.00    0.11      0.236  o       |       |       |       |      0.86
47.833    0.00    0.11      0.235  o       |       |       |       |      0.85
47.917    0.00    0.11      0.235  o       |       |       |       |      0.85
48.000    0.00    0.11      0.234  o       |       |       |       |      0.85
48.083    0.00    0.11      0.233  o       |       |       |       |      0.84
48.167    0.00    0.11      0.232  o       |       |       |       |      0.84
48.250    0.00    0.11      0.232  o       |       |       |       |      0.84
48.333    0.00    0.11      0.231  o       |       |       |       |      0.84
48.417    0.00    0.11      0.230  o       |       |       |       |      0.83
48.500    0.00    0.11      0.229  o       |       |       |       |      0.83
48.583    0.00    0.11      0.228  o       |       |       |       |      0.83
48.667    0.00    0.11      0.228  o       |       |       |       |      0.83
48.750    0.00    0.11      0.227  o       |       |       |       |      0.82
48.833    0.00    0.11      0.226  o       |       |       |       |      0.82
48.917    0.00    0.11      0.225  o       |       |       |       |      0.82
49.000    0.00    0.11      0.225  o       |       |       |       |      0.81
49.083    0.00    0.11      0.224  o       |       |       |       |      0.81
49.167    0.00    0.11      0.223  o       |       |       |       |      0.81
49.250    0.00    0.11      0.222  o       |       |       |       |      0.81
49.333    0.00    0.11      0.222  o       |       |       |       |      0.80
49.417    0.00    0.11      0.221  o       |       |       |       |      0.80
49.500    0.00    0.11      0.220  o       |       |       |       |      0.80
49.583    0.00    0.11      0.220  o       |       |       |       |      0.80
49.667    0.00    0.11      0.219  o       |       |       |       |      0.79
49.750    0.00    0.11      0.218  o       |       |       |       |      0.79
49.833    0.00    0.10      0.217  o       |       |       |       |      0.79
49.917    0.00    0.10      0.217  o       |       |       |       |      0.79
50.000    0.00    0.10      0.216  o       |       |       |       |      0.78
50.083    0.00    0.10      0.215  o       |       |       |       |      0.78
50.167    0.00    0.10      0.215  o       |       |       |       |      0.78
50.250    0.00    0.10      0.214  o       |       |       |       |      0.77
50.333    0.00    0.10      0.213  o       |       |       |       |      0.77
50.417    0.00    0.10      0.212  o       |       |       |       |      0.77
50.500    0.00    0.10      0.212  o       |       |       |       |      0.77
50.583    0.00    0.10      0.211  o       |       |       |       |      0.76
50.667    0.00    0.10      0.210  o       |       |       |       |      0.76
50.750    0.00    0.10      0.210  o       |       |       |       |      0.76
50.833    0.00    0.10      0.209  o       |       |       |       |      0.76
50.917    0.00    0.10      0.208  o       |       |       |       |      0.75
51.000    0.00    0.10      0.208  o       |       |       |       |      0.75
51.083    0.00    0.10      0.207  o       |       |       |       |      0.75
      Remaining water in basin =    0.21 (Ac.Ft)
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =   613
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =        0.862 (CFS)
                  Total volume =       1.107 (Ac.Ft)
            Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
      ************************************************************************
      ------------------------------------------------------------------------
```

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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 05/07/25

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: pro2242.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =   292
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =        3.509 (CFS)
               Total volume =       2.132 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
________________________________________________________________________

User entry of depth-outflow-storage data
------------------------------------------------------------------------
Total number of inflow hydrograph intervals = 292
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
------------------------------------------------------------------------
------------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
------------------------------------------------------------------------
------------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
------------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.276      0.133      0.276        0.276
   2.000      0.584      0.193      0.583        0.585
   3.000      0.930      0.700      0.928        0.932
   3.500      1.118      0.824      1.115        1.121
   4.000      1.316      0.930      1.313        1.319
   4.500      1.528      1.024      1.524        1.532
   4.750      1.637      1.068      1.633        1.641
   5.000      1.749     18.283      1.686        1.812
   6.000      2.231    253.655      1.358        3.104
------------------------------------------------------------------------
               Hydrograph Detention Basin Routing
------------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
------------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                  Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0       0.9    1.75    2.63    3.51 (Ft.)
 0.083    0.08    0.00      0.000  O      |       |       |       |     0.00
 0.167    0.18    0.00      0.001  OI     |       |       |       |     0.00
 0.250    0.20    0.00      0.002  OI     |       |       |       |     0.01
 0.333    0.25    0.00      0.004  O I    |       |       |       |     0.01
 0.417    0.29    0.00      0.006  O I    |       |       |       |     0.02
 0.500    0.30    0.00      0.008  O I    |       |       |       |     0.03
 0.583    0.31    0.00      0.010  O I    |       |       |       |     0.04
 0.667    0.31    0.01      0.012  O I    |       |       |       |     0.04
 0.750    0.31    0.01      0.014  O I    |       |       |       |     0.05
 0.833    0.35    0.01      0.016  O  I   |       |       |       |     0.06
 0.917    0.40    0.01      0.019  O  I   |       |       |       |     0.07
 1.000    0.41    0.01      0.022  O  I   |       |       |       |     0.08
 1.083    0.37    0.01      0.024  O  I   |       |       |       |     0.09
 1.167    0.32    0.01      0.026  O I    |       |       |       |     0.10
 1.250    0.32    0.01      0.029  O I    |       |       |       |     0.10
 1.333    0.31    0.01      0.031  O I    |       |       |       |     0.11
 1.417    0.31    0.02      0.033  O I    |       |       |       |     0.12
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1.500    0.31    0.02      0.035  o I     |       |       |       |     0.13
1.583    0.31    0.02      0.037  o I     |       |       |       |     0.13
1.667    0.31    0.02      0.039  o I     |       |       |       |     0.14
1.750    0.31    0.02      0.041  o I     |       |       |       |     0.15
1.833    0.35    0.02      0.043  o  I    |       |       |       |     0.16
1.917    0.40    0.02      0.045  o  I    |       |       |       |     0.16
2.000    0.41    0.02      0.048  o  I    |       |       |       |     0.17
2.083    0.41    0.02      0.051  o  I    |       |       |       |     0.18
2.167    0.41    0.03      0.053  o  I    |       |       |       |     0.19
2.250    0.41    0.03      0.056  o  I    |       |       |       |     0.20
2.333    0.41    0.03      0.059  o  I    |       |       |       |     0.21
2.417    0.41    0.03      0.061  o  I    |       |       |       |     0.22
2.500    0.41    0.03      0.064  o  I    |       |       |       |     0.23
2.583    0.45    0.03      0.067  o   I   |       |       |       |     0.24
2.667    0.50    0.03      0.070  o   I   |       |       |       |     0.25
2.750    0.51    0.04      0.073  o   I   |       |       |       |     0.26
2.833    0.51    0.04      0.076  o   I   |       |       |       |     0.28
2.917    0.52    0.04      0.079  o   I   |       |       |       |     0.29
3.000    0.52    0.04      0.083  o   I   |       |       |       |     0.30
3.083    0.52    0.04      0.086  o   I   |       |       |       |     0.31
3.167    0.52    0.04      0.089  o   I   |       |       |       |     0.32
3.250    0.52    0.04      0.093  o   I   |       |       |       |     0.34
3.333    0.52    0.05      0.096  o   I   |       |       |       |     0.35
3.417    0.52    0.05      0.099  o   I   |       |       |       |     0.36
3.500    0.52    0.05      0.102  o   I   |       |       |       |     0.37
3.583    0.52    0.05      0.105  o   I   |       |       |       |     0.38
3.667    0.52    0.05      0.109  o   I   |       |       |       |     0.39
3.750    0.52    0.05      0.112  o   I   |       |       |       |     0.41
3.833    0.56    0.06      0.115  o    I  |       |       |       |     0.42
3.917    0.60    0.06      0.119  o    I  |       |       |       |     0.43
4.000    0.61    0.06      0.123  o    I  |       |       |       |     0.44
4.083    0.62    0.06      0.126  o    I  |       |       |       |     0.46
4.167    0.62    0.06      0.130  o    I  |       |       |       |     0.47
4.250    0.62    0.06      0.134  o    I  |       |       |       |     0.49
4.333    0.66    0.07      0.138  o     I |       |       |       |     0.50
4.417    0.71    0.07      0.142  o     I |       |       |       |     0.52
4.500    0.72    0.07      0.147  o     I |       |       |       |     0.53
4.583    0.72    0.07      0.151  o     I |       |       |       |     0.55
4.667    0.72    0.07      0.156  o     I |       |       |       |     0.56
4.750    0.72    0.08      0.160  o     I |       |       |       |     0.58
4.833    0.76    0.08      0.165  o     I |       |       |       |     0.60
4.917    0.81    0.08      0.169  o      I|       |       |       |     0.61
5.000    0.82    0.08      0.175  o      I|       |       |       |     0.63
5.083    0.74    0.09      0.179  o     I |       |       |       |     0.65
5.167    0.65    0.09      0.183  o    I  |       |       |       |     0.66
5.250    0.63    0.09      0.187  o    I  |       |       |       |     0.68
5.333    0.66    0.09      0.191  o     I |       |       |       |     0.69
5.417    0.71    0.09      0.195  o     I |       |       |       |     0.71
5.500    0.72    0.10      0.199  o     I |       |       |       |     0.72
5.583    0.76    0.10      0.204  o     I |       |       |       |     0.74
5.667    0.81    0.10      0.209  o      I|       |       |       |     0.76
5.750    0.82    0.10      0.213  o      I|       |       |       |     0.77
5.833    0.82    0.11      0.218  o      I|       |       |       |     0.79
5.917    0.83    0.11      0.223  o      I|       |       |       |     0.81
6.000    0.83    0.11      0.228  |o     I|       |       |       |     0.83
6.083    0.87    0.11      0.233  |o     I|       |       |       |     0.85
6.167    0.91    0.12      0.239  |o      I       |       |       |     0.86
6.250    0.92    0.12      0.244  |o      I       |       |       |     0.88
6.333    0.93    0.12      0.250  |o      I       |       |       |     0.91
6.417    0.93    0.12      0.255  |o      I       |       |       |     0.93
6.500    0.93    0.13      0.261  |o      I       |       |       |     0.95
6.583    0.97    0.13      0.267  |o      I       |       |       |     0.97
6.667    1.02    0.13      0.273  |o      |I      |       |       |     0.99
6.750    1.03    0.13      0.279  |o      |I      |       |       |     1.01
6.833    1.03    0.13      0.285  |o      |I      |       |       |     1.03
6.917    1.03    0.14      0.291  |o      |I      |       |       |     1.05
7.000    1.03    0.14      0.297  |o      |I      |       |       |     1.07
7.083    1.03    0.14      0.303  |o      |I      |       |       |     1.09
7.167    1.03    0.14      0.309  |o      |I      |       |       |     1.11
7.250    1.03    0.14      0.316  |o      |I      |       |       |     1.13
7.333    1.07    0.14      0.322  |o      |I      |       |       |     1.15
7.417    1.12    0.14      0.328  |o      | I     |       |       |     1.17
7.500    1.13    0.14      0.335  |o      | I     |       |       |     1.19
7.583    1.18    0.15      0.342  |o      | I     |       |       |     1.21
7.667    1.22    0.15      0.349  |o      |  I    |       |       |     1.24
7.750    1.23    0.15      0.357  |o      |  I    |       |       |     1.26
7.833    1.28    0.15      0.364  |o      |  I    |       |       |     1.29
7.917    1.33    0.15      0.372  |o      |   I   |       |       |     1.31
8.000    1.34    0.15      0.380  |o      |   I   |       |       |     1.34
8.083    1.42    0.15      0.389  |o      |   I   |       |       |     1.37
8.167    1.52    0.16      0.398  |o      |    I  |       |       |     1.40
8.250    1.54    0.16      0.407  |o      |     I |       |       |     1.43
8.333    1.54    0.16      0.417  |o      |     I |       |       |     1.46
8.417    1.55    0.16      0.426  |o      |     I |       |       |     1.49
8.500    1.55    0.16      0.436  |o      |     I |       |       |     1.52
8.583    1.59    0.17      0.446  |o      |     I |       |       |     1.55
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 8.667    1.64    0.17      0.456  |O      |     I |       |       |     1.58
 8.750    1.65    0.17      0.466  |O      |      I|       |       |     1.62
 8.833    1.69    0.17      0.476  |O      |      I|       |       |     1.65
 8.917    1.74    0.17      0.487  |O      |      I|       |       |     1.68
 9.000    1.75    0.18      0.497  |O      |      I|       |       |     1.72
 9.083    1.84    0.18      0.509  |O      |       I       |       |     1.76
 9.167    1.93    0.18      0.520  |O      |       |I      |       |     1.79
 9.250    1.95    0.18      0.532  |O      |       |I      |       |     1.83
 9.333    2.00    0.19      0.545  |O      |       | I     |       |     1.87
 9.417    2.05    0.19      0.557  |O      |       | I     |       |     1.91
 9.500    2.06    0.19      0.570  |O      |       | I     |       |     1.96
 9.583    2.10    0.19      0.583  |O      |       |  I    |       |     2.00
 9.667    2.15    0.21      0.597  |O      |       |  I    |       |     2.04
 9.750    2.16    0.23      0.610  | O     |       |  I    |       |     2.07
 9.833    2.21    0.25      0.623  | O     |       |   I   |       |     2.11
 9.917    2.25    0.27      0.637  | O     |       |   I   |       |     2.15
10.000    2.26    0.29      0.650  | O     |       |   I   |       |     2.19
10.083    1.97    0.31      0.663  | O     |       | I     |       |     2.23
10.167    1.66    0.32      0.673  | O     |       I|      |       |     2.26
10.250    1.59    0.34      0.682  |  O    |      I |      |       |     2.28
10.333    1.56    0.35      0.691  |  O    |      I |      |       |     2.31
10.417    1.55    0.36      0.699  |  O    |      I |      |       |     2.33
10.500    1.55    0.37      0.707  |  O    |      I |      |       |     2.36
10.583    1.76    0.39      0.716  |  O    |       I       |       |     2.38
10.667    1.99    0.40      0.726  |  O    |       | I     |       |     2.41
10.750    2.04    0.42      0.737  |  O    |       | I     |       |     2.44
10.833    2.06    0.43      0.748  |  O    |       | I     |       |     2.47
10.917    2.06    0.45      0.759  |   O   |       | I     |       |     2.51
11.000    2.06    0.47      0.770  |   O   |       | I     |       |     2.54
11.083    2.02    0.48      0.781  |   O   |       | I     |       |     2.57
11.167    1.98    0.50      0.792  |   O   |       | I     |       |     2.60
11.250    1.97    0.51      0.802  |   O   |       |I      |       |     2.63
11.333    1.96    0.53      0.812  |   O   |       |I      |       |     2.66
11.417    1.96    0.54      0.822  |   O   |       |I      |       |     2.69
11.500    1.96    0.56      0.831  |    O  |       |I      |       |     2.71
11.583    1.88    0.57      0.841  |    O  |       |I      |       |     2.74
11.667    1.79    0.58      0.849  |    O  |       I       |       |     2.77
11.750    1.77    0.59      0.857  |    O  |       I       |       |     2.79
11.833    1.80    0.61      0.866  |    O  |       I       |       |     2.81
11.917    1.84    0.62      0.874  |    O  |       I       |       |     2.84
12.000    1.85    0.63      0.882  |    O  |       I       |       |     2.86
12.083    2.15    0.64      0.892  |    O  |       |  I    |       |     2.89
12.167    2.47    0.66      0.903  |     O |       |    I  |       |     2.92
12.250    2.54    0.68      0.916  |     O |       |     I |       |     2.96
12.333    2.61    0.70      0.929  |     O |       |     I |       |     3.00
12.417    2.67    0.71      0.942  |     O |       |      I|       |     3.03
12.500    2.68    0.72      0.956  |     O |       |      I|       |     3.07
12.583    2.77    0.73      0.969  |     O |       |       |I      |     3.10
12.667    2.86    0.74      0.984  |     O |       |       | I     |     3.14
12.750    2.88    0.75      0.998  |     O |       |       | I     |     3.18
12.833    2.93    0.75      1.013  |     O |       |       | I     |     3.22
12.917    2.98    0.76      1.028  |     O |       |       |  I    |     3.26
13.000    2.99    0.77      1.044  |      O|       |       |  I    |     3.30
13.083    3.20    0.79      1.059  |      O|       |       |    I  |     3.34
13.167    3.43    0.80      1.077  |      O|       |       |     I |     3.39
13.250    3.48    0.81      1.095  |      O|       |       |     I |     3.44
13.333    3.50    0.82      1.114  |      O|       |       |     I |     3.49
13.417    3.51    0.83      1.132  |      O|       |       |     I |     3.54
13.500    3.51    0.84      1.150  |      O|       |       |     I |     3.58
13.583    3.05    0.85      1.167  |      O|       |       |  I    |     3.62
13.667    2.54    0.86      1.181  |      O|       |     I |       |     3.66
13.750    2.44    0.86      1.192  |      O|       |    I  |       |     3.69
13.833    2.39    0.87      1.202  |      O|       |   I   |       |     3.71
13.917    2.37    0.87      1.213  |      O|       |   I   |       |     3.74
14.000    2.37    0.88      1.223  |       O       |   I   |       |     3.77
14.083    2.54    0.89      1.234  |       O       |     I |       |     3.79
14.167    2.72    0.89      1.246  |       O       |      I|       |     3.82
14.250    2.76    0.90      1.259  |       O       |       |I      |     3.86
14.333    2.74    0.91      1.271  |       O       |       I       |     3.89
14.417    2.70    0.91      1.284  |       O       |       I       |     3.92
14.500    2.69    0.92      1.296  |       O       |       I       |     3.95
14.583    2.68    0.93      1.308  |       O       |       I       |     3.98
14.667    2.68    0.93      1.320  |       O       |       I       |     4.01
14.750    2.68    0.94      1.332  |       O       |       I       |     4.04
14.833    2.64    0.94      1.344  |       O       |       I       |     4.07
14.917    2.60    0.95      1.356  |       O       |      I|       |     4.09
15.000    2.59    0.95      1.367  |       O       |      I|       |     4.12
15.083    2.54    0.96      1.378  |       O       |      I|       |     4.15
15.167    2.49    0.96      1.389  |       O       |     I |       |     4.17
15.250    2.48    0.97      1.399  |       O       |     I |       |     4.20
15.333    2.44    0.97      1.410  |       O       |     I |       |     4.22
15.417    2.39    0.98      1.420  |       O       |    I  |       |     4.24
15.500    2.38    0.98      1.429  |       O       |    I  |       |     4.27
15.583    2.21    0.98      1.438  |       O       |   I   |       |     4.29
15.667    2.02    0.99      1.446  |       |O      | I     |       |     4.31
15.750    1.98    0.99      1.453  |       |O      | I     |       |     4.32
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15.833    1.97    0.99      1.460 |        |O       |I       |        |      4.34
15.917    1.96    1.00      1.466 |        |O       |I       |        |      4.35
16.000    1.96    1.00      1.473 |        |O       |I       |        |      4.37
16.083    1.33    1.00      1.477 |        |O  I    |        |        |      4.38
16.167    0.64    1.00      1.477 |    I   |O       |        |        |      4.38
16.250    0.50    1.00      1.474 |   I    |O       |        |        |      4.37
16.333    0.44    1.00      1.471 |  I     |O       |        |        |      4.36
16.417    0.41    1.00      1.467 |  I     |O       |        |        |      4.36
16.500    0.41    1.00      1.463 |  I     |O       |        |        |      4.35
16.583    0.37    0.99      1.459 |  I     |O       |        |        |      4.34
16.667    0.32    0.99      1.454 | I      |O       |        |        |      4.33
16.750    0.32    0.99      1.450 | I      |O       |        |        |      4.32
16.833    0.31    0.99      1.445 | I      |O       |        |        |      4.30
16.917    0.31    0.99      1.440 | I      O        |        |        |      4.29
17.000    0.31    0.98      1.436 | I      O        |        |        |      4.28
17.083    0.39    0.98      1.431 |  I     O        |        |        |      4.27
17.167    0.49    0.98      1.428 |   I    O        |        |        |      4.26
17.250    0.50    0.98      1.424 |   I    O        |        |        |      4.26
17.333    0.51    0.98      1.421 |   I    O        |        |        |      4.25
17.417    0.52    0.98      1.418 |   I    O        |        |        |      4.24
17.500    0.52    0.97      1.415 |   I    O        |        |        |      4.23
17.583    0.52    0.97      1.412 |   I    O        |        |        |      4.23
17.667    0.52    0.97      1.408 |   I    O        |        |        |      4.22
17.750    0.52    0.97      1.405 |   I    O        |        |        |      4.21
17.833    0.47    0.97      1.402 |   I    O        |        |        |      4.20
17.917    0.43    0.97      1.398 |  I     O        |        |        |      4.19
18.000    0.42    0.96      1.395 |  I     O        |        |        |      4.19
18.083    0.41    0.96      1.391 |  I     O        |        |        |      4.18
18.167    0.41    0.96      1.387 |  I     O        |        |        |      4.17
18.250    0.41    0.96      1.383 |  I     O        |        |        |      4.16
18.333    0.41    0.96      1.380 |  I     O        |        |        |      4.15
18.417    0.41    0.96      1.376 |  I     O        |        |        |      4.14
18.500    0.41    0.95      1.372 |  I     O        |        |        |      4.13
18.583    0.37    0.95      1.368 |  I     O        |        |        |      4.12
18.667    0.32    0.95      1.364 | I      O        |        |        |      4.11
18.750    0.32    0.95      1.360 | I      O        |        |        |      4.10
18.833    0.27    0.95      1.355 | I      O        |        |        |      4.09
18.917    0.22    0.95      1.350 | I      O        |        |        |      4.08
19.000    0.21    0.94      1.345 |I       O        |        |        |      4.07
19.083    0.25    0.94      1.341 | I      O        |        |        |      4.06
19.167    0.29    0.94      1.336 | I      O        |        |        |      4.05
19.250    0.30    0.94      1.332 | I      O        |        |        |      4.04
19.333    0.35    0.94      1.327 |  I     O        |        |        |      4.03
19.417    0.40    0.93      1.323 |  I     O        |        |        |      4.02
19.500    0.41    0.93      1.320 |  I     O        |        |        |      4.01
19.583    0.37    0.93      1.316 |  I     O        |        |        |      4.00
19.667    0.32    0.93      1.312 | I      O        |        |        |      3.99
19.750    0.32    0.93      1.308 | I      O        |        |        |      3.98
19.833    0.27    0.92      1.304 | I      O        |        |        |      3.97
19.917    0.22    0.92      1.299 | I      O        |        |        |      3.96
20.000    0.21    0.92      1.294 |I       O        |        |        |      3.94
20.083    0.25    0.92      1.289 | I      O        |        |        |      3.93
20.167    0.29    0.91      1.285 | I      O        |        |        |      3.92
20.250    0.30    0.91      1.281 | I      O        |        |        |      3.91
20.333    0.31    0.91      1.277 | I      O        |        |        |      3.90
20.417    0.31    0.91      1.272 | I      O        |        |        |      3.89
20.500    0.31    0.90      1.268 | I      O        |        |        |      3.88
20.583    0.31    0.90      1.264 | I      O        |        |        |      3.87
20.667    0.31    0.90      1.260 | I      O        |        |        |      3.86
20.750    0.31    0.90      1.256 | I      O        |        |        |      3.85
20.833    0.27    0.90      1.252 | I      O        |        |        |      3.84
20.917    0.22    0.89      1.247 | I      O        |        |        |      3.83
21.000    0.21    0.89      1.243 |I       O        |        |        |      3.81
21.083    0.25    0.89      1.238 | I      O        |        |        |      3.80
21.167    0.29    0.89      1.234 | I      O        |        |        |      3.79
21.250    0.30    0.88      1.230 | I      O        |        |        |      3.78
21.333    0.27    0.88      1.226 | I      O        |        |        |      3.77
21.417    0.22    0.88      1.221 | I      O        |        |        |      3.76
21.500    0.21    0.88      1.217 |I       O|       |        |        |      3.75
21.583    0.25    0.87      1.212 | I      O|       |        |        |      3.74
21.667    0.29    0.87      1.208 | I      O|       |        |        |      3.73
21.750    0.30    0.87      1.204 | I      O|       |        |        |      3.72
21.833    0.27    0.87      1.200 | I      O|       |        |        |      3.71
21.917    0.22    0.87      1.196 | I      O|       |        |        |      3.70
22.000    0.21    0.86      1.192 |I       O|       |        |        |      3.69
22.083    0.25    0.86      1.187 | I      O|       |        |        |      3.67
22.167    0.29    0.86      1.183 | I      O|       |        |        |      3.66
22.250    0.30    0.86      1.179 | I      O|       |        |        |      3.65
22.333    0.27    0.85      1.175 | I      O|       |        |        |      3.64
22.417    0.22    0.85      1.171 | I      O|       |        |        |      3.63
22.500    0.21    0.85      1.167 |I       O|       |        |        |      3.62
22.583    0.21    0.85      1.162 |I       O|       |        |        |      3.61
22.667    0.21    0.85      1.158 |I       O|       |        |        |      3.60
22.750    0.21    0.84      1.154 |I       O|       |        |        |      3.59
22.833    0.21    0.84      1.149 |I       O|       |        |        |      3.58
22.917    0.21    0.84      1.145 |I       O|       |        |        |      3.57
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23.000    0.21    0.84      1.141  |I     o|       |       |       |      3.56
23.083    0.21    0.83      1.136  |I     o|       |       |       |      3.55
23.167    0.21    0.83      1.132  |I     o|       |       |       |      3.54
23.250    0.21    0.83      1.128  |I     o|       |       |       |      3.52
23.333    0.21    0.83      1.123  |I     o|       |       |       |      3.51
23.417    0.21    0.82      1.119  |I     o|       |       |       |      3.50
23.500    0.21    0.82      1.115  |I     o|       |       |       |      3.49
23.583    0.21    0.82      1.111  |I     o|       |       |       |      3.48
23.667    0.21    0.82      1.106  |I     o|       |       |       |      3.47
23.750    0.21    0.81      1.102  |I     o|       |       |       |      3.46
23.833    0.21    0.81      1.098  |I     o|       |       |       |      3.45
23.917    0.21    0.81      1.094  |I     o|       |       |       |      3.44
24.000    0.21    0.81      1.090  |I     o|       |       |       |      3.42
24.083    0.12    0.80      1.085  |I     o|       |       |       |      3.41
24.167    0.03    0.80      1.080  I      o|       |       |       |      3.40
24.250    0.01    0.80      1.075  I      o|       |       |       |      3.39
24.333    0.00    0.79      1.070  I      o|       |       |       |      3.37
24.417    0.00    0.79      1.064  I      o|       |       |       |      3.36
24.500    0.00    0.78      1.059  I      o|       |       |       |      3.34
24.583    0.00    0.78      1.053  I      o|       |       |       |      3.33
24.667    0.00    0.78      1.048  I      o|       |       |       |      3.31
24.750    0.00    0.77      1.043  I      o|       |       |       |      3.30
24.833    0.00    0.77      1.037  I      o|       |       |       |      3.29
24.917    0.00    0.77      1.032  I     o |       |       |       |      3.27
25.000    0.00    0.76      1.027  I     o |       |       |       |      3.26
25.083    0.00    0.76      1.021  I     o |       |       |       |      3.24
25.167    0.00    0.76      1.016  I     o |       |       |       |      3.23
25.250    0.00    0.75      1.011  I     o |       |       |       |      3.22
25.333    0.00    0.75      1.006  I     o |       |       |       |      3.20
25.417    0.00    0.75      1.001  I     o |       |       |       |      3.19
25.500    0.00    0.74      0.996  I     o |       |       |       |      3.17
25.583    0.00    0.74      0.990  I     o |       |       |       |      3.16
25.667    0.00    0.74      0.985  I     o |       |       |       |      3.15
25.750    0.00    0.73      0.980  I     o |       |       |       |      3.13
25.833    0.00    0.73      0.975  I     o |       |       |       |      3.12
25.917    0.00    0.73      0.970  I     o |       |       |       |      3.11
26.000    0.00    0.72      0.965  I     o |       |       |       |      3.09
26.083    0.00    0.72      0.960  I     o |       |       |       |      3.08
26.167    0.00    0.72      0.955  I     o |       |       |       |      3.07
26.250    0.00    0.71      0.950  I     o |       |       |       |      3.05
26.333    0.00    0.71      0.946  I     o |       |       |       |      3.04
26.417    0.00    0.71      0.941  I     o |       |       |       |      3.03
26.500    0.00    0.70      0.936  I     o |       |       |       |      3.02
26.583    0.00    0.70      0.931  I     o |       |       |       |      3.00
26.667    0.00    0.69      0.926  I     o |       |       |       |      2.99
26.750    0.00    0.69      0.921  I     o |       |       |       |      2.98
26.833    0.00    0.68      0.917  I     o |       |       |       |      2.96
26.917    0.00    0.67      0.912  I     o |       |       |       |      2.95
27.000    0.00    0.67      0.907  I     o |       |       |       |      2.93
27.083    0.00    0.66      0.903  I     o |       |       |       |      2.92
27.167    0.00    0.65      0.898  I    o  |       |       |       |      2.91
27.250    0.00    0.65      0.894  I    o  |       |       |       |      2.90
27.333    0.00    0.64      0.889  I    o  |       |       |       |      2.88
27.417    0.00    0.63      0.885  I    o  |       |       |       |      2.87
27.500    0.00    0.63      0.881  I    o  |       |       |       |      2.86
27.583    0.00    0.62      0.876  I    o  |       |       |       |      2.85
27.667    0.00    0.62      0.872  I    o  |       |       |       |      2.83
27.750    0.00    0.61      0.868  I    o  |       |       |       |      2.82
27.833    0.00    0.60      0.864  I    o  |       |       |       |      2.81
27.917    0.00    0.60      0.860  I    o  |       |       |       |      2.80
28.000    0.00    0.59      0.856  I    o  |       |       |       |      2.78
28.083    0.00    0.58      0.851  I    o  |       |       |       |      2.77
28.167    0.00    0.58      0.847  I    o  |       |       |       |      2.76
28.250    0.00    0.57      0.843  I    o  |       |       |       |      2.75
28.333    0.00    0.57      0.840  I    o  |       |       |       |      2.74
28.417    0.00    0.56      0.836  I    o  |       |       |       |      2.73
28.500    0.00    0.56      0.832  I    o  |       |       |       |      2.72
28.583    0.00    0.55      0.828  I    o  |       |       |       |      2.71
28.667    0.00    0.55      0.824  I   o   |       |       |       |      2.69
28.750    0.00    0.54      0.820  I   o   |       |       |       |      2.68
28.833    0.00    0.53      0.817  I   o   |       |       |       |      2.67
28.917    0.00    0.53      0.813  I   o   |       |       |       |      2.66
29.000    0.00    0.52      0.810  I   o   |       |       |       |      2.65
29.083    0.00    0.52      0.806  I   o   |       |       |       |      2.64
29.167    0.00    0.51      0.802  I   o   |       |       |       |      2.63
29.250    0.00    0.51      0.799  I   o   |       |       |       |      2.62
29.333    0.00    0.50      0.795  I   o   |       |       |       |      2.61
29.417    0.00    0.50      0.792  I   o   |       |       |       |      2.60
29.500    0.00    0.49      0.789  I   o   |       |       |       |      2.59
29.583    0.00    0.49      0.785  I   o   |       |       |       |      2.58
29.667    0.00    0.48      0.782  I   o   |       |       |       |      2.57
29.750    0.00    0.48      0.779  I   o   |       |       |       |      2.56
29.833    0.00    0.47      0.775  I   o   |       |       |       |      2.55
29.917    0.00    0.47      0.772  I   o   |       |       |       |      2.54
30.000    0.00    0.46      0.769  I   o   |       |       |       |      2.53
30.083    0.00    0.46      0.766  I   o   |       |       |       |      2.52
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30.167	0.00	0.45	0.762	I o	|	|	|	2.52
30.250	0.00	0.45	0.759	I o	|	|	|	2.51
30.333	0.00	0.45	0.756	I o	|	|	|	2.50
30.417	0.00	0.44	0.753	I o	|	|	|	2.49
30.500	0.00	0.44	0.750	I o	|	|	|	2.48
30.583	0.00	0.43	0.747	I o	|	|	|	2.47
30.667	0.00	0.43	0.744	I o	|	|	|	2.46
30.750	0.00	0.42	0.741	I o	|	|	|	2.45
30.833	0.00	0.42	0.738	I o	|	|	|	2.45
30.917	0.00	0.42	0.736	I o	|	|	|	2.44
31.000	0.00	0.41	0.733	I o	|	|	|	2.43
31.083	0.00	0.41	0.730	I o	|	|	|	2.42
31.167	0.00	0.40	0.727	I o	|	|	|	2.41
31.250	0.00	0.40	0.724	I o	|	|	|	2.41
31.333	0.00	0.39	0.722	I o	|	|	|	2.40
31.417	0.00	0.39	0.719	I o	|	|	|	2.39
31.500	0.00	0.39	0.716	I o	|	|	|	2.38
31.583	0.00	0.38	0.714	I o	|	|	|	2.37
31.667	0.00	0.38	0.711	I o	|	|	|	2.37
31.750	0.00	0.38	0.708	I o	|	|	|	2.36
31.833	0.00	0.37	0.706	I o	|	|	|	2.35
31.917	0.00	0.37	0.703	I o	|	|	|	2.34
32.000	0.00	0.36	0.701	I o	|	|	|	2.34
32.083	0.00	0.36	0.698	I o	|	|	|	2.33
32.167	0.00	0.36	0.696	I o	|	|	|	2.32
32.250	0.00	0.35	0.693	I o	|	|	|	2.32
32.333	0.00	0.35	0.691	I o	|	|	|	2.31
32.417	0.00	0.35	0.688	I o	|	|	|	2.30
32.500	0.00	0.34	0.686	I o	|	|	|	2.30
32.583	0.00	0.34	0.684	I o	|	|	|	2.29
32.667	0.00	0.34	0.681	I o	|	|	|	2.28
32.750	0.00	0.33	0.679	I o	|	|	|	2.27
32.833	0.00	0.33	0.677	I o	|	|	|	2.27
32.917	0.00	0.33	0.675	I o	|	|	|	2.26
33.000	0.00	0.32	0.672	I o	|	|	|	2.26
33.083	0.00	0.32	0.670	I o	|	|	|	2.25
33.167	0.00	0.32	0.668	I o	|	|	|	2.24
33.250	0.00	0.31	0.666	I o	|	|	|	2.24
33.333	0.00	0.31	0.664	I o	|	|	|	2.23
33.417	0.00	0.31	0.662	I o	|	|	|	2.22
33.500	0.00	0.30	0.659	I o	|	|	|	2.22
33.583	0.00	0.30	0.657	I o	|	|	|	2.21
33.667	0.00	0.30	0.655	I o	|	|	|	2.21
33.750	0.00	0.29	0.653	I o	|	|	|	2.20
33.833	0.00	0.29	0.651	I o	|	|	|	2.19
33.917	0.00	0.29	0.649	I o	|	|	|	2.19
34.000	0.00	0.29	0.647	I o	|	|	|	2.18
34.083	0.00	0.28	0.645	I o	|	|	|	2.18
34.167	0.00	0.28	0.643	I o	|	|	|	2.17
34.250	0.00	0.28	0.641	I o	|	|	|	2.17
34.333	0.00	0.27	0.640	I o	|	|	|	2.16
34.417	0.00	0.27	0.638	I o	|	|	|	2.16
34.500	0.00	0.27	0.636	I o	|	|	|	2.15
34.583	0.00	0.27	0.634	I o	|	|	|	2.14
34.667	0.00	0.26	0.632	I o	|	|	|	2.14
34.750	0.00	0.26	0.630	I o	|	|	|	2.13
34.833	0.00	0.26	0.629	I o	|	|	|	2.13
34.917	0.00	0.26	0.627	I o	|	|	|	2.12
35.000	0.00	0.25	0.625	I o	|	|	|	2.12
35.083	0.00	0.25	0.623	I o	|	|	|	2.11
35.167	0.00	0.25	0.622	I o	|	|	|	2.11
35.250	0.00	0.25	0.620	I o	|	|	|	2.10
35.333	0.00	0.24	0.618	I o	|	|	|	2.10
35.417	0.00	0.24	0.617	I o	|	|	|	2.09
35.500	0.00	0.24	0.615	I o	|	|	|	2.09
35.583	0.00	0.24	0.613	I o	|	|	|	2.08
35.667	0.00	0.23	0.612	I o	|	|	|	2.08
35.750	0.00	0.23	0.610	I o	|	|	|	2.08
35.833	0.00	0.23	0.608	I o	|	|	|	2.07
35.917	0.00	0.23	0.607	I o	|	|	|	2.07
36.000	0.00	0.22	0.605	I o	|	|	|	2.06
36.083	0.00	0.22	0.604	I o	|	|	|	2.06
36.167	0.00	0.22	0.602	I o	|	|	|	2.05
36.250	0.00	0.22	0.601	IO	|	|	|	2.05
36.333	0.00	0.22	0.599	IO	|	|	|	2.04
36.417	0.00	0.21	0.598	IO	|	|	|	2.04
36.500	0.00	0.21	0.596	IO	|	|	|	2.04
36.583	0.00	0.21	0.595	IO	|	|	|	2.03
36.667	0.00	0.21	0.593	IO	|	|	|	2.03
36.750	0.00	0.20	0.592	IO	|	|	|	2.02
36.833	0.00	0.20	0.591	IO	|	|	|	2.02
36.917	0.00	0.20	0.589	IO	|	|	|	2.02
37.000	0.00	0.20	0.588	IO	|	|	|	2.01
37.083	0.00	0.20	0.587	IO	|	|	|	2.01
37.167	0.00	0.19	0.585	IO	|	|	|	2.00
37.250	0.00	0.19	0.584	IO	|	|	|	2.00

37.333	0.00	0.19	0.582	IO					2.00
37.417	0.00	0.19	0.581	IO					1.99
37.500	0.00	0.19	0.580	IO					1.99
37.583	0.00	0.19	0.579	IO					1.98
37.667	0.00	0.19	0.577	IO					1.98
37.750	0.00	0.19	0.576	IO					1.97
37.833	0.00	0.19	0.575	IO					1.97
37.917	0.00	0.19	0.573	IO					1.97
38.000	0.00	0.19	0.572	IO					1.96
38.083	0.00	0.19	0.571	IO					1.96
38.167	0.00	0.19	0.569	IO					1.95
38.250	0.00	0.19	0.568	IO					1.95
38.333	0.00	0.19	0.567	IO					1.94
38.417	0.00	0.19	0.565	IO					1.94
38.500	0.00	0.19	0.564	IO					1.94
38.583	0.00	0.19	0.563	IO					1.93
38.667	0.00	0.19	0.561	IO					1.93
38.750	0.00	0.19	0.560	IO					1.92
38.833	0.00	0.19	0.559	IO					1.92
38.917	0.00	0.19	0.558	IO					1.91
39.000	0.00	0.19	0.556	IO					1.91
39.083	0.00	0.19	0.555	IO					1.91
39.167	0.00	0.19	0.554	IO					1.90
39.250	0.00	0.19	0.552	IO					1.90
39.333	0.00	0.19	0.551	IO					1.89
39.417	0.00	0.19	0.550	IO					1.89
39.500	0.00	0.19	0.549	IO					1.89
39.583	0.00	0.19	0.547	IO					1.88
39.667	0.00	0.19	0.546	IO					1.88
39.750	0.00	0.19	0.545	IO					1.87
39.833	0.00	0.19	0.543	IO					1.87
39.917	0.00	0.18	0.542	IO					1.86
40.000	0.00	0.18	0.541	IO					1.86
40.083	0.00	0.18	0.540	IO					1.86
40.167	0.00	0.18	0.538	IO					1.85
40.250	0.00	0.18	0.537	IO					1.85
40.333	0.00	0.18	0.536	IO					1.84
40.417	0.00	0.18	0.535	IO					1.84
40.500	0.00	0.18	0.533	IO					1.84
40.583	0.00	0.18	0.532	IO					1.83
40.667	0.00	0.18	0.531	IO					1.83
40.750	0.00	0.18	0.530	IO					1.82
40.833	0.00	0.18	0.528	IO					1.82
40.917	0.00	0.18	0.527	IO					1.82
41.000	0.00	0.18	0.526	IO					1.81
41.083	0.00	0.18	0.525	IO					1.81
41.167	0.00	0.18	0.523	IO					1.80
41.250	0.00	0.18	0.522	IO					1.80
41.333	0.00	0.18	0.521	IO					1.79
41.417	0.00	0.18	0.520	IO					1.79
41.500	0.00	0.18	0.518	IO					1.79
41.583	0.00	0.18	0.517	IO					1.78
41.667	0.00	0.18	0.516	IO					1.78
41.750	0.00	0.18	0.515	IO					1.77
41.833	0.00	0.18	0.513	IO					1.77
41.917	0.00	0.18	0.512	IO					1.77
42.000	0.00	0.18	0.511	IO					1.76
42.083	0.00	0.18	0.510	IO					1.76
42.167	0.00	0.18	0.508	IO					1.75
42.250	0.00	0.18	0.507	IO					1.75
42.333	0.00	0.18	0.506	IO					1.75
42.417	0.00	0.18	0.505	IO					1.74
42.500	0.00	0.18	0.504	IO					1.74
42.583	0.00	0.18	0.502	IO					1.73
42.667	0.00	0.18	0.501	IO					1.73
42.750	0.00	0.18	0.500	IO					1.73
42.833	0.00	0.18	0.499	IO					1.72
42.917	0.00	0.18	0.497	IO					1.72
43.000	0.00	0.18	0.496	IO					1.72
43.083	0.00	0.18	0.495	IO					1.71
43.167	0.00	0.18	0.494	IO					1.71
43.250	0.00	0.18	0.493	IO					1.70
43.333	0.00	0.17	0.491	IO					1.70
43.417	0.00	0.17	0.490	IO					1.70
43.500	0.00	0.17	0.489	IO					1.69
43.583	0.00	0.17	0.488	IO					1.69
43.667	0.00	0.17	0.487	IO					1.68
43.750	0.00	0.17	0.485	IO					1.68
43.833	0.00	0.17	0.484	IO					1.68
43.917	0.00	0.17	0.483	IO					1.67
44.000	0.00	0.17	0.482	IO					1.67
44.083	0.00	0.17	0.481	IO					1.66
44.167	0.00	0.17	0.479	IO					1.66
44.250	0.00	0.17	0.478	IO					1.66
44.333	0.00	0.17	0.477	IO					1.65
44.417	0.00	0.17	0.476	IO					1.65

44.500	0.00	0.17	0.475	IO					1.65
44.583	0.00	0.17	0.474	IO					1.64
44.667	0.00	0.17	0.472	IO					1.64
44.750	0.00	0.17	0.471	IO					1.63
44.833	0.00	0.17	0.470	IO					1.63
44.917	0.00	0.17	0.469	IO					1.63
45.000	0.00	0.17	0.468	IO					1.62
45.083	0.00	0.17	0.466	IO					1.62
45.167	0.00	0.17	0.465	IO					1.61
45.250	0.00	0.17	0.464	IO					1.61
45.333	0.00	0.17	0.463	IO					1.61
45.417	0.00	0.17	0.462	IO					1.60
45.500	0.00	0.17	0.461	IO					1.60
45.583	0.00	0.17	0.459	IO					1.60
45.667	0.00	0.17	0.458	IO					1.59
45.750	0.00	0.17	0.457	IO					1.59
45.833	0.00	0.17	0.456	IO					1.58
45.917	0.00	0.17	0.455	IO					1.58
46.000	0.00	0.17	0.454	IO					1.58
46.083	0.00	0.17	0.453	IO					1.57
46.167	0.00	0.17	0.451	IO					1.57
46.250	0.00	0.17	0.450	IO					1.57
46.333	0.00	0.17	0.449	IO					1.56
46.417	0.00	0.17	0.448	IO					1.56
46.500	0.00	0.17	0.447	IO					1.55
46.583	0.00	0.17	0.446	IO					1.55
46.667	0.00	0.17	0.444	IO					1.55
46.750	0.00	0.17	0.443	IO					1.54
46.833	0.00	0.17	0.442	IO					1.54
46.917	0.00	0.17	0.441	IO					1.54
47.000	0.00	0.16	0.440	IO					1.53
47.083	0.00	0.16	0.439	IO					1.53
47.167	0.00	0.16	0.438	IO					1.52
47.250	0.00	0.16	0.437	IO					1.52
47.333	0.00	0.16	0.435	IO					1.52
47.417	0.00	0.16	0.434	IO					1.51
47.500	0.00	0.16	0.433	IO					1.51
47.583	0.00	0.16	0.432	IO					1.51
47.667	0.00	0.16	0.431	IO					1.50
47.750	0.00	0.16	0.430	IO					1.50
47.833	0.00	0.16	0.429	IO					1.50
47.917	0.00	0.16	0.428	IO					1.49
48.000	0.00	0.16	0.426	IO					1.49
48.083	0.00	0.16	0.425	IO					1.48
48.167	0.00	0.16	0.424	IO					1.48
48.250	0.00	0.16	0.423	IO					1.48
48.333	0.00	0.16	0.422	IO					1.47
48.417	0.00	0.16	0.421	IO					1.47
48.500	0.00	0.16	0.420	IO					1.47
48.583	0.00	0.16	0.419	IO					1.46
48.667	0.00	0.16	0.418	IO					1.46
48.750	0.00	0.16	0.416	IO					1.46
48.833	0.00	0.16	0.415	IO					1.45
48.917	0.00	0.16	0.414	IO					1.45
49.000	0.00	0.16	0.413	IO					1.45
49.083	0.00	0.16	0.412	IO					1.44
49.167	0.00	0.16	0.411	IO					1.44
49.250	0.00	0.16	0.410	IO					1.43
49.333	0.00	0.16	0.409	IO					1.43
49.417	0.00	0.16	0.408	IO					1.43
49.500	0.00	0.16	0.407	IO					1.42
49.583	0.00	0.16	0.405	IO					1.42
49.667	0.00	0.16	0.404	IO					1.42
49.750	0.00	0.16	0.403	IO					1.41
49.833	0.00	0.16	0.402	IO					1.41
49.917	0.00	0.16	0.401	IO					1.41
50.000	0.00	0.16	0.400	IO					1.40
50.083	0.00	0.16	0.399	IO					1.40
50.167	0.00	0.16	0.398	IO					1.40
50.250	0.00	0.16	0.397	IO					1.39
50.333	0.00	0.16	0.396	IO					1.39
50.417	0.00	0.16	0.395	IO					1.39
50.500	0.00	0.16	0.394	IO					1.38
50.583	0.00	0.16	0.392	IO					1.38
50.667	0.00	0.16	0.391	IO					1.37
50.750	0.00	0.16	0.390	IO					1.37
50.833	0.00	0.16	0.389	IO					1.37
50.917	0.00	0.15	0.388	IO					1.36
51.000	0.00	0.15	0.387	IO					1.36
51.083	0.00	0.15	0.386	IO					1.36
51.167	0.00	0.15	0.385	IO					1.35
51.250	0.00	0.15	0.384	IO					1.35
51.333	0.00	0.15	0.383	IO					1.35
51.417	0.00	0.15	0.382	IO					1.34
51.500	0.00	0.15	0.381	IO					1.34
51.583	0.00	0.15	0.380	IO					1.34

51.667	0.00	0.15	0.379	IO					1.33
51.750	0.00	0.15	0.378	IO					1.33
51.833	0.00	0.15	0.377	IO					1.33
51.917	0.00	0.15	0.375	IO					1.32
52.000	0.00	0.15	0.374	IO					1.32
52.083	0.00	0.15	0.373	IO					1.32
52.167	0.00	0.15	0.372	IO					1.31
52.250	0.00	0.15	0.371	IO					1.31
52.333	0.00	0.15	0.370	IO					1.31
52.417	0.00	0.15	0.369	IO					1.30
52.500	0.00	0.15	0.368	IO					1.30
52.583	0.00	0.15	0.367	IO					1.30
52.667	0.00	0.15	0.366	IO					1.29
52.750	0.00	0.15	0.365	IO					1.29
52.833	0.00	0.15	0.364	IO					1.29
52.917	0.00	0.15	0.363	IO					1.28
53.000	0.00	0.15	0.362	IO					1.28
53.083	0.00	0.15	0.361	IO					1.28
53.167	0.00	0.15	0.360	IO					1.27
53.250	0.00	0.15	0.359	IO					1.27
53.333	0.00	0.15	0.358	IO					1.27
53.417	0.00	0.15	0.357	IO					1.26
53.500	0.00	0.15	0.356	IO					1.26
53.583	0.00	0.15	0.355	IO					1.26
53.667	0.00	0.15	0.354	IO					1.25
53.750	0.00	0.15	0.353	IO					1.25
53.833	0.00	0.15	0.352	IO					1.25
53.917	0.00	0.15	0.351	IO					1.24
54.000	0.00	0.15	0.350	IO					1.24
54.083	0.00	0.15	0.349	IO					1.24
54.167	0.00	0.15	0.348	IO					1.23
54.250	0.00	0.15	0.347	IO					1.23
54.333	0.00	0.15	0.346	IO					1.23
54.417	0.00	0.15	0.345	IO					1.22
54.500	0.00	0.15	0.344	IO					1.22
54.583	0.00	0.15	0.343	IO					1.22
54.667	0.00	0.15	0.342	IO					1.21
54.750	0.00	0.15	0.341	IO					1.21
54.833	0.00	0.15	0.340	IO					1.21
54.917	0.00	0.15	0.339	IO					1.20
55.000	0.00	0.15	0.338	IO					1.20
55.083	0.00	0.14	0.337	IO					1.20
55.167	0.00	0.14	0.336	IO					1.19
55.250	0.00	0.14	0.335	IO					1.19
55.333	0.00	0.14	0.334	IO					1.19
55.417	0.00	0.14	0.333	IO					1.18
55.500	0.00	0.14	0.332	IO					1.18
55.583	0.00	0.14	0.331	IO					1.18
55.667	0.00	0.14	0.330	IO					1.17
55.750	0.00	0.14	0.329	IO					1.17
55.833	0.00	0.14	0.328	IO					1.17
55.917	0.00	0.14	0.327	IO					1.16
56.000	0.00	0.14	0.326	IO					1.16
56.083	0.00	0.14	0.325	IO					1.16
56.167	0.00	0.14	0.324	IO					1.16
56.250	0.00	0.14	0.323	IO					1.15
56.333	0.00	0.14	0.322	IO					1.15
56.417	0.00	0.14	0.321	IO					1.15
56.500	0.00	0.14	0.320	IO					1.14
56.583	0.00	0.14	0.319	IO					1.14
56.667	0.00	0.14	0.318	IO					1.14
56.750	0.00	0.14	0.317	IO					1.13
56.833	0.00	0.14	0.316	IO					1.13
56.917	0.00	0.14	0.315	IO					1.13
57.000	0.00	0.14	0.314	IO					1.12
57.083	0.00	0.14	0.313	IO					1.12
57.167	0.00	0.14	0.312	IO					1.12
57.250	0.00	0.14	0.311	IO					1.11
57.333	0.00	0.14	0.310	IO					1.11
57.417	0.00	0.14	0.309	IO					1.11
57.500	0.00	0.14	0.308	IO					1.10
57.583	0.00	0.14	0.307	IO					1.10
57.667	0.00	0.14	0.306	IO					1.10
57.750	0.00	0.14	0.305	IO					1.10
57.833	0.00	0.14	0.304	IO					1.09
57.917	0.00	0.14	0.303	IO					1.09
58.000	0.00	0.14	0.303	IO					1.09
58.083	0.00	0.14	0.302	IO					1.08
58.167	0.00	0.14	0.301	IO					1.08
58.250	0.00	0.14	0.300	IO					1.08
58.333	0.00	0.14	0.299	IO					1.07
58.417	0.00	0.14	0.298	IO					1.07
58.500	0.00	0.14	0.297	IO					1.07
58.583	0.00	0.14	0.296	IO					1.06
58.667	0.00	0.14	0.295	IO					1.06
58.750	0.00	0.14	0.294	IO					1.06

58.833	0.00	0.14	0.293	IO				1.06
58.917	0.00	0.14	0.292	IO				1.05
59.000	0.00	0.14	0.291	IO				1.05
59.083	0.00	0.14	0.290	IO				1.05
59.167	0.00	0.14	0.289	IO				1.04
59.250	0.00	0.14	0.288	IO				1.04
59.333	0.00	0.14	0.287	IO				1.04
59.417	0.00	0.14	0.287	IO				1.03
59.500	0.00	0.13	0.286	IO				1.03
59.583	0.00	0.13	0.285	IO				1.03
59.667	0.00	0.13	0.284	IO				1.03
59.750	0.00	0.13	0.283	IO				1.02
59.833	0.00	0.13	0.282	IO				1.02
59.917	0.00	0.13	0.281	IO				1.02
60.000	0.00	0.13	0.280	IO				1.01
60.083	0.00	0.13	0.279	IO				1.01
60.167	0.00	0.13	0.278	IO				1.01
60.250	0.00	0.13	0.277	IO				1.00
60.333	0.00	0.13	0.276	IO				1.00
60.417	0.00	0.13	0.275	IO				1.00
60.500	0.00	0.13	0.275	IO				0.99
60.583	0.00	0.13	0.274	IO				0.99
60.667	0.00	0.13	0.273	IO				0.99
60.750	0.00	0.13	0.272	IO				0.98
60.833	0.00	0.13	0.271	IO				0.98
60.917	0.00	0.13	0.270	IO				0.98
61.000	0.00	0.13	0.269	IO				0.98
61.083	0.00	0.13	0.268	IO				0.97
61.167	0.00	0.13	0.267	IO				0.97
61.250	0.00	0.13	0.266	IO				0.97
61.333	0.00	0.13	0.266	IO				0.96
61.417	0.00	0.13	0.265	IO				0.96
61.500	0.00	0.13	0.264	IO				0.96
61.583	0.00	0.13	0.263	IO				0.95
61.667	0.00	0.13	0.262	IO				0.95
61.750	0.00	0.13	0.261	IO				0.95
61.833	0.00	0.13	0.260	IO				0.94
61.917	0.00	0.13	0.259	IO				0.94
62.000	0.00	0.12	0.259	IO				0.94
62.083	0.00	0.12	0.258	IO				0.93
62.167	0.00	0.12	0.257	IO				0.93
62.250	0.00	0.12	0.256	IO				0.93
62.333	0.00	0.12	0.255	IO				0.92
62.417	0.00	0.12	0.254	IO				0.92
62.500	0.00	0.12	0.254	IO				0.92
62.583	0.00	0.12	0.253	IO				0.92
62.667	0.00	0.12	0.252	IO				0.91
62.750	0.00	0.12	0.251	IO				0.91
62.833	0.00	0.12	0.250	IO				0.91
62.917	0.00	0.12	0.249	IO				0.90
63.000	0.00	0.12	0.249	IO				0.90
63.083	0.00	0.12	0.248	IO				0.90
63.167	0.00	0.12	0.247	IO				0.89
63.250	0.00	0.12	0.246	IO				0.89
63.333	0.00	0.12	0.245	IO				0.89
63.417	0.00	0.12	0.244	IO				0.89
63.500	0.00	0.12	0.244	IO				0.88
63.583	0.00	0.12	0.243	IO				0.88
63.667	0.00	0.12	0.242	IO				0.88
63.750	0.00	0.12	0.241	IO				0.87
63.833	0.00	0.12	0.240	IO				0.87
63.917	0.00	0.12	0.240	IO				0.87
64.000	0.00	0.12	0.239	IO				0.87
64.083	0.00	0.11	0.238	IO				0.86
64.167	0.00	0.11	0.237	IO				0.86
64.250	0.00	0.11	0.236	IO				0.86
64.333	0.00	0.11	0.236	IO				0.85
64.417	0.00	0.11	0.235	IO				0.85
64.500	0.00	0.11	0.234	IO				0.85
64.583	0.00	0.11	0.233	IO				0.85
64.667	0.00	0.11	0.233	IO				0.84
64.750	0.00	0.11	0.232	IO				0.84
64.833	0.00	0.11	0.231	IO				0.84
64.917	0.00	0.11	0.230	IO				0.83
65.000	0.00	0.11	0.229	IO				0.83
65.083	0.00	0.11	0.229	IO				0.83
65.167	0.00	0.11	0.228	IO				0.83
65.250	0.00	0.11	0.227	O				0.82
65.333	0.00	0.11	0.226	O				0.82
65.417	0.00	0.11	0.226	O				0.82
65.500	0.00	0.11	0.225	O				0.82
65.583	0.00	0.11	0.224	O				0.81
65.667	0.00	0.11	0.223	O				0.81
65.750	0.00	0.11	0.223	O				0.81
65.833	0.00	0.11	0.222	O				0.80
65.917	0.00	0.11	0.221	O				0.80

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66.000    0.00    0.11      0.221  o       |       |       |       |     0.80
66.083    0.00    0.11      0.220  o       |       |       |       |     0.80
66.167    0.00    0.11      0.219  o       |       |       |       |     0.79
66.250    0.00    0.11      0.218  o       |       |       |       |     0.79
66.333    0.00    0.10      0.218  o       |       |       |       |     0.79
66.417    0.00    0.10      0.217  o       |       |       |       |     0.79
66.500    0.00    0.10      0.216  o       |       |       |       |     0.78
66.583    0.00    0.10      0.215  o       |       |       |       |     0.78
66.667    0.00    0.10      0.215  o       |       |       |       |     0.78
66.750    0.00    0.10      0.214  o       |       |       |       |     0.78
66.833    0.00    0.10      0.213  o       |       |       |       |     0.77
66.917    0.00    0.10      0.213  o       |       |       |       |     0.77
67.000    0.00    0.10      0.212  o       |       |       |       |     0.77
67.083    0.00    0.10      0.211  o       |       |       |       |     0.77
67.167    0.00    0.10      0.211  o       |       |       |       |     0.76
67.250    0.00    0.10      0.210  o       |       |       |       |     0.76
67.333    0.00    0.10      0.209  o       |       |       |       |     0.76
67.417    0.00    0.10      0.208  o       |       |       |       |     0.76
67.500    0.00    0.10      0.208  o       |       |       |       |     0.75
67.583    0.00    0.10      0.207  o       |       |       |       |     0.75

      Remaining water in basin =    0.21 (Ac.Ft)


      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =   811
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =        1.002 (CFS)
                  Total volume =       1.925 (Ac.Ft)
            Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      ***********************************************************************

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                    FLOOD HYDROGRAPH ROUTING PROGRAM
                Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                            Study date: 05/07/25

      ---------------------------------------------------------------------

      Program License Serial Number 5006

      ---------------------------------------------------------------------
      ********************* HYDROGRAPH INFORMATION **********************
                    From study/file name: PRO515.rte
      ****************************HYDROGRAPH DATA****************************
                    Number of intervals =    16
                    Time interval =    5.0 (Min.)
                    Maximum/Peak flow rate =       38.649 (CFS)
                    Total volume =       1.067 (Ac.Ft)
             Status of hydrographs being held in storage
                       Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
             Peak (CFS)      0.000     0.000     0.000     0.000     0.000
             Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
      ************************************************************************
      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
      Process from Point/Station        1.000 to Point/Station        2.000
      **** RETARDING BASIN ROUTING ****
      ________________________________________________________________________
      User entry of depth-outflow-storage data
      ---------------------------------------------------------------------
      Total number of inflow hydrograph intervals = 16
      Hydrograph time unit =  5.000 (Min.)
      Initial depth in storage basin =   0.00(Ft.)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Initial basin depth =   0.00 (Ft.)
      Initial basin storage =      0.00 (Ac.Ft)
      Initial basin outflow =   0.00 (CFS)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Depth vs. Storage and Depth vs. Discharge data:
       Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
            (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
      ---------------------------------------------------------------------
        0.000      0.000      0.000      0.000        0.000
        1.000      0.276      0.133      0.276        0.276
        2.000      0.584      0.193      0.583        0.585
        3.000      0.930      0.700      0.928        0.932
        3.500      1.118      0.824      1.115        1.121
        4.000      1.316      0.930      1.313        1.319
        4.500      1.528      1.024      1.524        1.532
        4.750      1.637      1.068      1.633        1.641
        5.000      1.749     18.283      1.686        1.812
        6.000      2.231    253.655      1.358        3.104
      ---------------------------------------------------------------------
                     Hydrograph Detention Basin Routing
      ---------------------------------------------------------------------
      Graph values: 'I'= unit inflow; 'O'=outflow at time shown
      ---------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                        Depth
(Hours) (CFS)   (CFS)     (Ac.Ft) .0       9.7   19.32   28.99   38.65 (Ft.)
 0.083    1.59    0.00      0.005  OI      |       |       |       |      0.02
 0.167    3.75    0.01      0.024  O  I    |       |       |       |      0.09
 0.250    4.69    0.03      0.053  O  I    |       |       |       |      0.19
 0.333    5.24    0.04      0.087  O   I   |       |       |       |      0.31
 0.417    5.77    0.06      0.124  O   I   |       |       |       |      0.45
 0.500    6.53    0.08      0.166  O    I  |       |       |       |      0.60
 0.583    7.41    0.10      0.213  O     I |       |       |       |      0.77
 0.667    9.37    0.13      0.270  O      I|       |       |       |      0.98
 0.750   16.05    0.15      0.357  O       |   I   |       |       |      1.26
 0.833   38.65    0.19      0.544  O       |       |       |      I|      1.87
 0.917   35.24    0.50      0.796  O       |       |       |   I   |      2.61
 1.000   12.85    0.72      0.958  O       | I     |       |       |      3.07
 1.083    5.67    0.76      1.016  O   I   |       |       |       |      3.23
 1.167    1.81    0.77      1.037  OI      |       |       |       |      3.28
 1.250    0.31    0.77      1.039  O       |       |       |       |      3.29
 1.333    0.07    0.77      1.035  O       |       |       |       |      3.28
 1.417    0.00    0.77      1.030  O       |       |       |       |      3.27
 1.500    0.00    0.76      1.025  O       |       |       |       |      3.25
 1.583    0.00    0.76      1.019  O       |       |       |       |      3.24
 1.667    0.00    0.76      1.014  O       |       |       |       |      3.22
 1.750    0.00    0.75      1.009  O       |       |       |       |      3.21
 1.833    0.00    0.75      1.004  O       |       |       |       |      3.20
 1.917    0.00    0.75      0.999  O       |       |       |       |      3.18
 2.000    0.00    0.74      0.994  O       |       |       |       |      3.17
 2.083    0.00    0.74      0.988  O       |       |       |       |      3.16
 2.167    0.00    0.74      0.983  O       |       |       |       |      3.14
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2.250	0.00	0.73	0.978	o	|	|	|	3.13
2.333	0.00	0.73	0.973	o	|	|	|	3.12
2.417	0.00	0.73	0.968	o	|	|	|	3.10
2.500	0.00	0.72	0.963	o	|	|	|	3.09
2.583	0.00	0.72	0.958	o	|	|	|	3.08
2.667	0.00	0.72	0.953	o	|	|	|	3.06
2.750	0.00	0.71	0.948	o	|	|	|	3.05
2.833	0.00	0.71	0.944	o	|	|	|	3.04
2.917	0.00	0.71	0.939	o	|	|	|	3.02
3.000	0.00	0.70	0.934	o	|	|	|	3.01
3.083	0.00	0.70	0.929	o	|	|	|	3.00
3.167	0.00	0.69	0.924	o	|	|	|	2.98
3.250	0.00	0.68	0.919	o	|	|	|	2.97
3.333	0.00	0.68	0.915	o	|	|	|	2.96
3.417	0.00	0.67	0.910	o	|	|	|	2.94
3.500	0.00	0.66	0.906	o	|	|	|	2.93
3.583	0.00	0.66	0.901	o	|	|	|	2.92
3.667	0.00	0.65	0.897	o	|	|	|	2.90
3.750	0.00	0.64	0.892	o	|	|	|	2.89
3.833	0.00	0.64	0.888	o	|	|	|	2.88
3.917	0.00	0.63	0.883	o	|	|	|	2.86
4.000	0.00	0.63	0.879	o	|	|	|	2.85
4.083	0.00	0.62	0.875	o	|	|	|	2.84
4.167	0.00	0.61	0.870	o	|	|	|	2.83
4.250	0.00	0.61	0.866	o	|	|	|	2.82
4.333	0.00	0.60	0.862	o	|	|	|	2.80
4.417	0.00	0.59	0.858	o	|	|	|	2.79
4.500	0.00	0.59	0.854	o	|	|	|	2.78
4.583	0.00	0.58	0.850	o	|	|	|	2.77
4.667	0.00	0.58	0.846	o	|	|	|	2.76
4.750	0.00	0.57	0.842	o	|	|	|	2.75
4.833	0.00	0.57	0.838	o	|	|	|	2.73
4.917	0.00	0.56	0.834	o	|	|	|	2.72
5.000	0.00	0.55	0.830	o	|	|	|	2.71
5.083	0.00	0.55	0.826	o	|	|	|	2.70
5.167	0.00	0.54	0.823	o	|	|	|	2.69
5.250	0.00	0.54	0.819	o	|	|	|	2.68
5.333	0.00	0.53	0.815	o	|	|	|	2.67
5.417	0.00	0.53	0.812	o	|	|	|	2.66
5.500	0.00	0.52	0.808	o	|	|	|	2.65
5.583	0.00	0.52	0.804	o	|	|	|	2.64
5.667	0.00	0.51	0.801	o	|	|	|	2.63
5.750	0.00	0.51	0.797	o	|	|	|	2.62
5.833	0.00	0.50	0.794	o	|	|	|	2.61
5.917	0.00	0.50	0.791	o	|	|	|	2.60
6.000	0.00	0.49	0.787	o	|	|	|	2.59
6.083	0.00	0.49	0.784	o	|	|	|	2.58
6.167	0.00	0.48	0.780	o	|	|	|	2.57
6.250	0.00	0.48	0.777	o	|	|	|	2.56
6.333	0.00	0.47	0.774	o	|	|	|	2.55
6.417	0.00	0.47	0.771	o	|	|	|	2.54
6.500	0.00	0.46	0.767	o	|	|	|	2.53
6.583	0.00	0.46	0.764	o	|	|	|	2.52
6.667	0.00	0.45	0.761	o	|	|	|	2.51
6.750	0.00	0.45	0.758	o	|	|	|	2.50
6.833	0.00	0.44	0.755	o	|	|	|	2.49
6.917	0.00	0.44	0.752	o	|	|	|	2.49
7.000	0.00	0.43	0.749	o	|	|	|	2.48
7.083	0.00	0.43	0.746	o	|	|	|	2.47
7.167	0.00	0.43	0.743	o	|	|	|	2.46
7.250	0.00	0.42	0.740	o	|	|	|	2.45
7.333	0.00	0.42	0.737	o	|	|	|	2.44
7.417	0.00	0.41	0.734	o	|	|	|	2.43
7.500	0.00	0.41	0.732	o	|	|	|	2.43
7.583	0.00	0.41	0.729	o	|	|	|	2.42
7.667	0.00	0.40	0.726	o	|	|	|	2.41
7.750	0.00	0.40	0.723	o	|	|	|	2.40
7.833	0.00	0.39	0.720	o	|	|	|	2.39
7.917	0.00	0.39	0.718	o	|	|	|	2.39
8.000	0.00	0.39	0.715	o	|	|	|	2.38
8.083	0.00	0.38	0.712	o	|	|	|	2.37
8.167	0.00	0.38	0.710	o	|	|	|	2.36
8.250	0.00	0.37	0.707	o	|	|	|	2.36
8.333	0.00	0.37	0.705	o	|	|	|	2.35
8.417	0.00	0.37	0.702	o	|	|	|	2.34
8.500	0.00	0.36	0.700	o	|	|	|	2.33
8.583	0.00	0.36	0.697	o	|	|	|	2.33
8.667	0.00	0.36	0.695	o	|	|	|	2.32
8.750	0.00	0.35	0.692	o	|	|	|	2.31
8.833	0.00	0.35	0.690	o	|	|	|	2.31
8.917	0.00	0.34	0.688	o	|	|	|	2.30
9.000	0.00	0.34	0.685	o	|	|	|	2.29
9.083	0.00	0.34	0.683	o	|	|	|	2.29
9.167	0.00	0.33	0.680	o	|	|	|	2.28
9.250	0.00	0.33	0.678	o	|	|	|	2.27
9.333	0.00	0.33	0.676	o	|	|	|	2.27

9.417	0.00	0.32	0.674	o	|	|	|	2.26
9.500	0.00	0.32	0.671	o	|	|	|	2.25
9.583	0.00	0.32	0.669	o	|	|	|	2.25
9.667	0.00	0.31	0.667	o	|	|	|	2.24
9.750	0.00	0.31	0.665	o	|	|	|	2.23
9.833	0.00	0.31	0.663	o	|	|	|	2.23
9.917	0.00	0.31	0.661	o	|	|	|	2.22
10.000	0.00	0.30	0.659	o	|	|	|	2.22
10.083	0.00	0.30	0.657	o	|	|	|	2.21
10.167	0.00	0.30	0.654	o	|	|	|	2.20
10.250	0.00	0.29	0.652	o	|	|	|	2.20
10.333	0.00	0.29	0.650	o	|	|	|	2.19
10.417	0.00	0.29	0.648	o	|	|	|	2.19
10.500	0.00	0.28	0.646	o	|	|	|	2.18
10.583	0.00	0.28	0.645	o	|	|	|	2.17
10.667	0.00	0.28	0.643	o	|	|	|	2.17
10.750	0.00	0.28	0.641	o	|	|	|	2.16
10.833	0.00	0.27	0.639	o	|	|	|	2.16
10.917	0.00	0.27	0.637	o	|	|	|	2.15
11.000	0.00	0.27	0.635	o	|	|	|	2.15
11.083	0.00	0.27	0.633	o	|	|	|	2.14
11.167	0.00	0.26	0.631	o	|	|	|	2.14
11.250	0.00	0.26	0.630	o	|	|	|	2.13
11.333	0.00	0.26	0.628	o	|	|	|	2.13
11.417	0.00	0.25	0.626	o	|	|	|	2.12
11.500	0.00	0.25	0.624	o	|	|	|	2.12
11.583	0.00	0.25	0.623	o	|	|	|	2.11
11.667	0.00	0.25	0.621	o	|	|	|	2.11
11.750	0.00	0.24	0.619	o	|	|	|	2.10
11.833	0.00	0.24	0.618	o	|	|	|	2.10
11.917	0.00	0.24	0.616	o	|	|	|	2.09
12.000	0.00	0.24	0.614	o	|	|	|	2.09
12.083	0.00	0.23	0.613	o	|	|	|	2.08
12.167	0.00	0.23	0.611	o	|	|	|	2.08
12.250	0.00	0.23	0.609	o	|	|	|	2.07
12.333	0.00	0.23	0.608	o	|	|	|	2.07
12.417	0.00	0.23	0.606	o	|	|	|	2.06
12.500	0.00	0.22	0.605	o	|	|	|	2.06
12.583	0.00	0.22	0.603	o	|	|	|	2.06
12.667	0.00	0.22	0.602	o	|	|	|	2.05
12.750	0.00	0.22	0.600	o	|	|	|	2.05
12.833	0.00	0.21	0.599	o	|	|	|	2.04
12.917	0.00	0.21	0.597	o	|	|	|	2.04
13.000	0.00	0.21	0.596	o	|	|	|	2.03
13.083	0.00	0.21	0.594	o	|	|	|	2.03
13.167	0.00	0.21	0.593	o	|	|	|	2.03
13.250	0.00	0.20	0.591	o	|	|	|	2.02
13.333	0.00	0.20	0.590	o	|	|	|	2.02
13.417	0.00	0.20	0.589	o	|	|	|	2.01
13.500	0.00	0.20	0.587	o	|	|	|	2.01
13.583	0.00	0.20	0.586	o	|	|	|	2.01
13.667	0.00	0.19	0.585	o	|	|	|	2.00
13.750	0.00	0.19	0.583	o	|	|	|	2.00
13.833	0.00	0.19	0.582	o	|	|	|	1.99
13.917	0.00	0.19	0.581	o	|	|	|	1.99
14.000	0.00	0.19	0.579	o	|	|	|	1.98
14.083	0.00	0.19	0.578	o	|	|	|	1.98
14.167	0.00	0.19	0.577	o	|	|	|	1.98
14.250	0.00	0.19	0.575	o	|	|	|	1.97
14.333	0.00	0.19	0.574	o	|	|	|	1.97
14.417	0.00	0.19	0.573	o	|	|	|	1.96
14.500	0.00	0.19	0.571	o	|	|	|	1.96
14.583	0.00	0.19	0.570	o	|	|	|	1.95
14.667	0.00	0.19	0.569	o	|	|	|	1.95
14.750	0.00	0.19	0.567	o	|	|	|	1.95
14.833	0.00	0.19	0.566	o	|	|	|	1.94
14.917	0.00	0.19	0.565	o	|	|	|	1.94
15.000	0.00	0.19	0.564	o	|	|	|	1.93
15.083	0.00	0.19	0.562	o	|	|	|	1.93
15.167	0.00	0.19	0.561	o	|	|	|	1.93
15.250	0.00	0.19	0.560	o	|	|	|	1.92
15.333	0.00	0.19	0.558	o	|	|	|	1.92
15.417	0.00	0.19	0.557	o	|	|	|	1.91
15.500	0.00	0.19	0.556	o	|	|	|	1.91
15.583	0.00	0.19	0.554	o	|	|	|	1.90
15.667	0.00	0.19	0.553	o	|	|	|	1.90
15.750	0.00	0.19	0.552	o	|	|	|	1.90
15.833	0.00	0.19	0.551	o	|	|	|	1.89
15.917	0.00	0.19	0.549	o	|	|	|	1.89
16.000	0.00	0.19	0.548	o	|	|	|	1.88
16.083	0.00	0.19	0.547	o	|	|	|	1.88
16.167	0.00	0.19	0.546	o	|	|	|	1.88
16.250	0.00	0.19	0.544	o	|	|	|	1.87
16.333	0.00	0.19	0.543	o	|	|	|	1.87
16.417	0.00	0.18	0.542	o	|	|	|	1.86
16.500	0.00	0.18	0.540	o	|	|	|	1.86

16.583	0.00	0.18	0.539	o	|	|	|	1.85
16.667	0.00	0.18	0.538	o	|	|	|	1.85
16.750	0.00	0.18	0.537	o	|	|	|	1.85
16.833	0.00	0.18	0.535	o	|	|	|	1.84
16.917	0.00	0.18	0.534	o	|	|	|	1.84
17.000	0.00	0.18	0.533	o	|	|	|	1.83
17.083	0.00	0.18	0.532	o	|	|	|	1.83
17.167	0.00	0.18	0.530	o	|	|	|	1.83
17.250	0.00	0.18	0.529	o	|	|	|	1.82
17.333	0.00	0.18	0.528	o	|	|	|	1.82
17.417	0.00	0.18	0.527	o	|	|	|	1.81
17.500	0.00	0.18	0.525	o	|	|	|	1.81
17.583	0.00	0.18	0.524	o	|	|	|	1.81
17.667	0.00	0.18	0.523	o	|	|	|	1.80
17.750	0.00	0.18	0.522	o	|	|	|	1.80
17.833	0.00	0.18	0.520	o	|	|	|	1.79
17.917	0.00	0.18	0.519	o	|	|	|	1.79
18.000	0.00	0.18	0.518	o	|	|	|	1.79
18.083	0.00	0.18	0.517	o	|	|	|	1.78
18.167	0.00	0.18	0.515	o	|	|	|	1.78
18.250	0.00	0.18	0.514	o	|	|	|	1.77
18.333	0.00	0.18	0.513	o	|	|	|	1.77
18.417	0.00	0.18	0.512	o	|	|	|	1.77
18.500	0.00	0.18	0.510	o	|	|	|	1.76
18.583	0.00	0.18	0.509	o	|	|	|	1.76
18.667	0.00	0.18	0.508	o	|	|	|	1.75
18.750	0.00	0.18	0.507	o	|	|	|	1.75
18.833	0.00	0.18	0.505	o	|	|	|	1.75
18.917	0.00	0.18	0.504	o	|	|	|	1.74
19.000	0.00	0.18	0.503	o	|	|	|	1.74
19.083	0.00	0.18	0.502	o	|	|	|	1.73
19.167	0.00	0.18	0.501	o	|	|	|	1.73
19.250	0.00	0.18	0.499	o	|	|	|	1.73
19.333	0.00	0.18	0.498	o	|	|	|	1.72
19.417	0.00	0.18	0.497	o	|	|	|	1.72
19.500	0.00	0.18	0.496	o	|	|	|	1.71
19.583	0.00	0.18	0.495	o	|	|	|	1.71
19.667	0.00	0.18	0.493	o	|	|	|	1.71
19.750	0.00	0.18	0.492	o	|	|	|	1.70
19.833	0.00	0.17	0.491	o	|	|	|	1.70
19.917	0.00	0.17	0.490	o	|	|	|	1.69
20.000	0.00	0.17	0.489	o	|	|	|	1.69
20.083	0.00	0.17	0.487	o	|	|	|	1.69
20.167	0.00	0.17	0.486	o	|	|	|	1.68
20.250	0.00	0.17	0.485	o	|	|	|	1.68
20.333	0.00	0.17	0.484	o	|	|	|	1.67
20.417	0.00	0.17	0.483	o	|	|	|	1.67
20.500	0.00	0.17	0.481	o	|	|	|	1.67
20.583	0.00	0.17	0.480	o	|	|	|	1.66
20.667	0.00	0.17	0.479	o	|	|	|	1.66
20.750	0.00	0.17	0.478	o	|	|	|	1.66
20.833	0.00	0.17	0.477	o	|	|	|	1.65
20.917	0.00	0.17	0.475	o	|	|	|	1.65
21.000	0.00	0.17	0.474	o	|	|	|	1.64
21.083	0.00	0.17	0.473	o	|	|	|	1.64
21.167	0.00	0.17	0.472	o	|	|	|	1.64
21.250	0.00	0.17	0.471	o	|	|	|	1.63
21.333	0.00	0.17	0.470	o	|	|	|	1.63
21.417	0.00	0.17	0.468	o	|	|	|	1.62
21.500	0.00	0.17	0.467	o	|	|	|	1.62
21.583	0.00	0.17	0.466	o	|	|	|	1.62
21.667	0.00	0.17	0.465	o	|	|	|	1.61
21.750	0.00	0.17	0.464	o	|	|	|	1.61
21.833	0.00	0.17	0.462	o	|	|	|	1.61
21.917	0.00	0.17	0.461	o	|	|	|	1.60
22.000	0.00	0.17	0.460	o	|	|	|	1.60
22.083	0.00	0.17	0.459	o	|	|	|	1.59
22.167	0.00	0.17	0.458	o	|	|	|	1.59
22.250	0.00	0.17	0.457	o	|	|	|	1.59
22.333	0.00	0.17	0.456	o	|	|	|	1.58
22.417	0.00	0.17	0.454	o	|	|	|	1.58
22.500	0.00	0.17	0.453	o	|	|	|	1.58
22.583	0.00	0.17	0.452	o	|	|	|	1.57
22.667	0.00	0.17	0.451	o	|	|	|	1.57
22.750	0.00	0.17	0.450	o	|	|	|	1.56
22.833	0.00	0.17	0.449	o	|	|	|	1.56
22.917	0.00	0.17	0.447	o	|	|	|	1.56
23.000	0.00	0.17	0.446	o	|	|	|	1.55
23.083	0.00	0.17	0.445	o	|	|	|	1.55
23.167	0.00	0.17	0.444	o	|	|	|	1.55
23.250	0.00	0.17	0.443	o	|	|	|	1.54
23.333	0.00	0.17	0.442	o	|	|	|	1.54
23.417	0.00	0.17	0.441	o	|	|	|	1.53
23.500	0.00	0.16	0.439	o	|	|	|	1.53
23.583	0.00	0.16	0.438	o	|	|	|	1.53
23.667	0.00	0.16	0.437	o	|	|	|	1.52

23.750	0.00	0.16	0.436	o	|	|	|	|	1.52
23.833	0.00	0.16	0.435	o	|	|	|	|	1.52
23.917	0.00	0.16	0.434	o	|	|	|	|	1.51
24.000	0.00	0.16	0.433	o	|	|	|	|	1.51
24.083	0.00	0.16	0.432	o	|	|	|	|	1.51
24.167	0.00	0.16	0.430	o	|	|	|	|	1.50
24.250	0.00	0.16	0.429	o	|	|	|	|	1.50
24.333	0.00	0.16	0.428	o	|	|	|	|	1.49
24.417	0.00	0.16	0.427	o	|	|	|	|	1.49
24.500	0.00	0.16	0.426	o	|	|	|	|	1.49
24.583	0.00	0.16	0.425	o	|	|	|	|	1.48
24.667	0.00	0.16	0.424	o	|	|	|	|	1.48
24.750	0.00	0.16	0.423	o	|	|	|	|	1.48
24.833	0.00	0.16	0.421	o	|	|	|	|	1.47
24.917	0.00	0.16	0.420	o	|	|	|	|	1.47
25.000	0.00	0.16	0.419	o	|	|	|	|	1.47
25.083	0.00	0.16	0.418	o	|	|	|	|	1.46
25.167	0.00	0.16	0.417	o	|	|	|	|	1.46
25.250	0.00	0.16	0.416	o	|	|	|	|	1.45
25.333	0.00	0.16	0.415	o	|	|	|	|	1.45
25.417	0.00	0.16	0.414	o	|	|	|	|	1.45
25.500	0.00	0.16	0.413	o	|	|	|	|	1.44
25.583	0.00	0.16	0.412	o	|	|	|	|	1.44
25.667	0.00	0.16	0.410	o	|	|	|	|	1.44
25.750	0.00	0.16	0.409	o	|	|	|	|	1.43
25.833	0.00	0.16	0.408	o	|	|	|	|	1.43
25.917	0.00	0.16	0.407	o	|	|	|	|	1.43
26.000	0.00	0.16	0.406	o	|	|	|	|	1.42
26.083	0.00	0.16	0.405	o	|	|	|	|	1.42
26.167	0.00	0.16	0.404	o	|	|	|	|	1.42
26.250	0.00	0.16	0.403	o	|	|	|	|	1.41
26.333	0.00	0.16	0.402	o	|	|	|	|	1.41
26.417	0.00	0.16	0.401	o	|	|	|	|	1.40
26.500	0.00	0.16	0.400	o	|	|	|	|	1.40
26.583	0.00	0.16	0.398	o	|	|	|	|	1.40
26.667	0.00	0.16	0.397	o	|	|	|	|	1.39
26.750	0.00	0.16	0.396	o	|	|	|	|	1.39
26.833	0.00	0.16	0.395	o	|	|	|	|	1.39
26.917	0.00	0.16	0.394	o	|	|	|	|	1.38
27.000	0.00	0.16	0.393	o	|	|	|	|	1.38
27.083	0.00	0.16	0.392	o	|	|	|	|	1.38
27.167	0.00	0.16	0.391	o	|	|	|	|	1.37
27.250	0.00	0.16	0.390	o	|	|	|	|	1.37
27.333	0.00	0.15	0.389	o	|	|	|	|	1.37
27.417	0.00	0.15	0.388	o	|	|	|	|	1.36
27.500	0.00	0.15	0.387	o	|	|	|	|	1.36
27.583	0.00	0.15	0.386	o	|	|	|	|	1.36
27.667	0.00	0.15	0.385	o	|	|	|	|	1.35
27.750	0.00	0.15	0.384	o	|	|	|	|	1.35
27.833	0.00	0.15	0.382	o	|	|	|	|	1.35
27.917	0.00	0.15	0.381	o	|	|	|	|	1.34
28.000	0.00	0.15	0.380	o	|	|	|	|	1.34
28.083	0.00	0.15	0.379	o	|	|	|	|	1.34
28.167	0.00	0.15	0.378	o	|	|	|	|	1.33
28.250	0.00	0.15	0.377	o	|	|	|	|	1.33
28.333	0.00	0.15	0.376	o	|	|	|	|	1.33
28.417	0.00	0.15	0.375	o	|	|	|	|	1.32
28.500	0.00	0.15	0.374	o	|	|	|	|	1.32
28.583	0.00	0.15	0.373	o	|	|	|	|	1.31
28.667	0.00	0.15	0.372	o	|	|	|	|	1.31
28.750	0.00	0.15	0.371	o	|	|	|	|	1.31
28.833	0.00	0.15	0.370	o	|	|	|	|	1.30
28.917	0.00	0.15	0.369	o	|	|	|	|	1.30
29.000	0.00	0.15	0.368	o	|	|	|	|	1.30
29.083	0.00	0.15	0.367	o	|	|	|	|	1.29
29.167	0.00	0.15	0.366	o	|	|	|	|	1.29
29.250	0.00	0.15	0.365	o	|	|	|	|	1.29
29.333	0.00	0.15	0.364	o	|	|	|	|	1.28
29.417	0.00	0.15	0.363	o	|	|	|	|	1.28
29.500	0.00	0.15	0.362	o	|	|	|	|	1.28
29.583	0.00	0.15	0.361	o	|	|	|	|	1.27
29.667	0.00	0.15	0.359	o	|	|	|	|	1.27
29.750	0.00	0.15	0.358	o	|	|	|	|	1.27
29.833	0.00	0.15	0.357	o	|	|	|	|	1.26
29.917	0.00	0.15	0.356	o	|	|	|	|	1.26
30.000	0.00	0.15	0.355	o	|	|	|	|	1.26
30.083	0.00	0.15	0.354	o	|	|	|	|	1.25
30.167	0.00	0.15	0.353	o	|	|	|	|	1.25
30.250	0.00	0.15	0.352	o	|	|	|	|	1.25
30.333	0.00	0.15	0.351	o	|	|	|	|	1.24
30.417	0.00	0.15	0.350	o	|	|	|	|	1.24
30.500	0.00	0.15	0.349	o	|	|	|	|	1.24
30.583	0.00	0.15	0.348	o	|	|	|	|	1.23
30.667	0.00	0.15	0.347	o	|	|	|	|	1.23
30.750	0.00	0.15	0.346	o	|	|	|	|	1.23
30.833	0.00	0.15	0.345	o	|	|	|	|	1.22

30.917	0.00	0.15	0.344	o	|	|	|	1.22
31.000	0.00	0.15	0.343	o	|	|	|	1.22
31.083	0.00	0.15	0.342	o	|	|	|	1.21
31.167	0.00	0.15	0.341	o	|	|	|	1.21
31.250	0.00	0.15	0.340	o	|	|	|	1.21
31.333	0.00	0.15	0.339	o	|	|	|	1.21
31.417	0.00	0.15	0.338	o	|	|	|	1.20
31.500	0.00	0.14	0.337	o	|	|	|	1.20
31.583	0.00	0.14	0.336	o	|	|	|	1.20
31.667	0.00	0.14	0.335	o	|	|	|	1.19
31.750	0.00	0.14	0.334	o	|	|	|	1.19
31.833	0.00	0.14	0.333	o	|	|	|	1.19
31.917	0.00	0.14	0.332	o	|	|	|	1.18
32.000	0.00	0.14	0.331	o	|	|	|	1.18
32.083	0.00	0.14	0.330	o	|	|	|	1.18
32.167	0.00	0.14	0.329	o	|	|	|	1.17
32.250	0.00	0.14	0.328	o	|	|	|	1.17
32.333	0.00	0.14	0.327	o	|	|	|	1.17
32.417	0.00	0.14	0.326	o	|	|	|	1.16
32.500	0.00	0.14	0.325	o	|	|	|	1.16
32.583	0.00	0.14	0.324	o	|	|	|	1.16
32.667	0.00	0.14	0.323	o	|	|	|	1.15
32.750	0.00	0.14	0.322	o	|	|	|	1.15
32.833	0.00	0.14	0.321	o	|	|	|	1.15
32.917	0.00	0.14	0.320	o	|	|	|	1.14
33.000	0.00	0.14	0.319	o	|	|	|	1.14
33.083	0.00	0.14	0.318	o	|	|	|	1.14
33.167	0.00	0.14	0.318	o	|	|	|	1.13
33.250	0.00	0.14	0.317	o	|	|	|	1.13
33.333	0.00	0.14	0.316	o	|	|	|	1.13
33.417	0.00	0.14	0.315	o	|	|	|	1.13
33.500	0.00	0.14	0.314	o	|	|	|	1.12
33.583	0.00	0.14	0.313	o	|	|	|	1.12
33.667	0.00	0.14	0.312	o	|	|	|	1.12
33.750	0.00	0.14	0.311	o	|	|	|	1.11
33.833	0.00	0.14	0.310	o	|	|	|	1.11
33.917	0.00	0.14	0.309	o	|	|	|	1.11
34.000	0.00	0.14	0.308	o	|	|	|	1.10
34.083	0.00	0.14	0.307	o	|	|	|	1.10
34.167	0.00	0.14	0.306	o	|	|	|	1.10
34.250	0.00	0.14	0.305	o	|	|	|	1.09
34.333	0.00	0.14	0.304	o	|	|	|	1.09
34.417	0.00	0.14	0.303	o	|	|	|	1.09
34.500	0.00	0.14	0.302	o	|	|	|	1.08
34.583	0.00	0.14	0.301	o	|	|	|	1.08
34.667	0.00	0.14	0.300	o	|	|	|	1.08
34.750	0.00	0.14	0.299	o	|	|	|	1.08
34.833	0.00	0.14	0.298	o	|	|	|	1.07
34.917	0.00	0.14	0.297	o	|	|	|	1.07
35.000	0.00	0.14	0.296	o	|	|	|	1.07
35.083	0.00	0.14	0.295	o	|	|	|	1.06
35.167	0.00	0.14	0.295	o	|	|	|	1.06
35.250	0.00	0.14	0.294	o	|	|	|	1.06
35.333	0.00	0.14	0.293	o	|	|	|	1.05
35.417	0.00	0.14	0.292	o	|	|	|	1.05
35.500	0.00	0.14	0.291	o	|	|	|	1.05
35.583	0.00	0.14	0.290	o	|	|	|	1.05
35.667	0.00	0.14	0.289	o	|	|	|	1.04
35.750	0.00	0.14	0.288	o	|	|	|	1.04
35.833	0.00	0.14	0.287	o	|	|	|	1.04
35.917	0.00	0.13	0.286	o	|	|	|	1.03
36.000	0.00	0.13	0.285	o	|	|	|	1.03
36.083	0.00	0.13	0.284	o	|	|	|	1.03
36.167	0.00	0.13	0.283	o	|	|	|	1.02
36.250	0.00	0.13	0.282	o	|	|	|	1.02
36.333	0.00	0.13	0.282	o	|	|	|	1.02
36.417	0.00	0.13	0.281	o	|	|	|	1.01
36.500	0.00	0.13	0.280	o	|	|	|	1.01
36.583	0.00	0.13	0.279	o	|	|	|	1.01
36.667	0.00	0.13	0.278	o	|	|	|	1.01
36.750	0.00	0.13	0.277	o	|	|	|	1.00
36.833	0.00	0.13	0.276	o	|	|	|	1.00
36.917	0.00	0.13	0.275	o	|	|	|	1.00
37.000	0.00	0.13	0.274	o	|	|	|	0.99
37.083	0.00	0.13	0.273	o	|	|	|	0.99
37.167	0.00	0.13	0.272	o	|	|	|	0.99
37.250	0.00	0.13	0.271	o	|	|	|	0.98
37.333	0.00	0.13	0.271	o	|	|	|	0.98
37.417	0.00	0.13	0.270	o	|	|	|	0.98
37.500	0.00	0.13	0.269	o	|	|	|	0.97
37.583	0.00	0.13	0.268	o	|	|	|	0.97
37.667	0.00	0.13	0.267	o	|	|	|	0.97
37.750	0.00	0.13	0.266	o	|	|	|	0.96
37.833	0.00	0.13	0.265	o	|	|	|	0.96
37.917	0.00	0.13	0.264	o	|	|	|	0.96
38.000	0.00	0.13	0.263	o	|	|	|	0.95

```
38.083    0.00    0.13      0.263  o       |       |       |       |      0.95
38.167    0.00    0.13      0.262  o       |       |       |       |      0.95
38.250    0.00    0.13      0.261  o       |       |       |       |      0.95
38.333    0.00    0.13      0.260  o       |       |       |       |      0.94
38.417    0.00    0.12      0.259  o       |       |       |       |      0.94
38.500    0.00    0.12      0.258  o       |       |       |       |      0.94
38.583    0.00    0.12      0.257  o       |       |       |       |      0.93
38.667    0.00    0.12      0.257  o       |       |       |       |      0.93
38.750    0.00    0.12      0.256  o       |       |       |       |      0.93
38.833    0.00    0.12      0.255  o       |       |       |       |      0.92
38.917    0.00    0.12      0.254  o       |       |       |       |      0.92
39.000    0.00    0.12      0.253  o       |       |       |       |      0.92
39.083    0.00    0.12      0.252  o       |       |       |       |      0.91
39.167    0.00    0.12      0.251  o       |       |       |       |      0.91
39.250    0.00    0.12      0.251  o       |       |       |       |      0.91
39.333    0.00    0.12      0.250  o       |       |       |       |      0.91
39.417    0.00    0.12      0.249  o       |       |       |       |      0.90
39.500    0.00    0.12      0.248  o       |       |       |       |      0.90
39.583    0.00    0.12      0.247  o       |       |       |       |      0.90
39.667    0.00    0.12      0.247  o       |       |       |       |      0.89
39.750    0.00    0.12      0.246  o       |       |       |       |      0.89
39.833    0.00    0.12      0.245  o       |       |       |       |      0.89
39.917    0.00    0.12      0.244  o       |       |       |       |      0.88
40.000    0.00    0.12      0.243  o       |       |       |       |      0.88
40.083    0.00    0.12      0.242  o       |       |       |       |      0.88
40.167    0.00    0.12      0.242  o       |       |       |       |      0.88
40.250    0.00    0.12      0.241  o       |       |       |       |      0.87
40.333    0.00    0.12      0.240  o       |       |       |       |      0.87
40.417    0.00    0.12      0.239  o       |       |       |       |      0.87
40.500    0.00    0.11      0.238  o       |       |       |       |      0.86
40.583    0.00    0.11      0.238  o       |       |       |       |      0.86
40.667    0.00    0.11      0.237  o       |       |       |       |      0.86
40.750    0.00    0.11      0.236  o       |       |       |       |      0.86
40.833    0.00    0.11      0.235  o       |       |       |       |      0.85
40.917    0.00    0.11      0.235  o       |       |       |       |      0.85
41.000    0.00    0.11      0.234  o       |       |       |       |      0.85
41.083    0.00    0.11      0.233  o       |       |       |       |      0.84
41.167    0.00    0.11      0.232  o       |       |       |       |      0.84
41.250    0.00    0.11      0.231  o       |       |       |       |      0.84
41.333    0.00    0.11      0.231  o       |       |       |       |      0.84
41.417    0.00    0.11      0.230  o       |       |       |       |      0.83
41.500    0.00    0.11      0.229  o       |       |       |       |      0.83
41.583    0.00    0.11      0.228  o       |       |       |       |      0.83
41.667    0.00    0.11      0.228  o       |       |       |       |      0.82
41.750    0.00    0.11      0.227  o       |       |       |       |      0.82
41.833    0.00    0.11      0.226  o       |       |       |       |      0.82
41.917    0.00    0.11      0.225  o       |       |       |       |      0.82
42.000    0.00    0.11      0.225  o       |       |       |       |      0.81
42.083    0.00    0.11      0.224  o       |       |       |       |      0.81
42.167    0.00    0.11      0.223  o       |       |       |       |      0.81
42.250    0.00    0.11      0.222  o       |       |       |       |      0.81
42.333    0.00    0.11      0.222  o       |       |       |       |      0.80
42.417    0.00    0.11      0.221  o       |       |       |       |      0.80
42.500    0.00    0.11      0.220  o       |       |       |       |      0.80
42.583    0.00    0.11      0.220  o       |       |       |       |      0.80
42.667    0.00    0.11      0.219  o       |       |       |       |      0.79
42.750    0.00    0.11      0.218  o       |       |       |       |      0.79
42.833    0.00    0.10      0.217  o       |       |       |       |      0.79
42.917    0.00    0.10      0.217  o       |       |       |       |      0.78
43.000    0.00    0.10      0.216  o       |       |       |       |      0.78
43.083    0.00    0.10      0.215  o       |       |       |       |      0.78
43.167    0.00    0.10      0.214  o       |       |       |       |      0.78
43.250    0.00    0.10      0.214  o       |       |       |       |      0.77
43.333    0.00    0.10      0.213  o       |       |       |       |      0.77
43.417    0.00    0.10      0.212  o       |       |       |       |      0.77
43.500    0.00    0.10      0.212  o       |       |       |       |      0.77
43.583    0.00    0.10      0.211  o       |       |       |       |      0.76
43.667    0.00    0.10      0.210  o       |       |       |       |      0.76
43.750    0.00    0.10      0.210  o       |       |       |       |      0.76
43.833    0.00    0.10      0.209  o       |       |       |       |      0.76
43.917    0.00    0.10      0.208  o       |       |       |       |      0.75
44.000    0.00    0.10      0.207  o       |       |       |       |      0.75
      Remaining water in basin =    0.21 (Ac.Ft)
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =   528
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =        0.772 (CFS)
                  Total volume =       0.860 (Ac.Ft)
            Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
      ************************************************************************
      ------------------------------------------------------------------------
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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 05/07/25

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: PRO535.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    40
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       18.702 (CFS)
               Total volume =       1.394 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
________________________________________________________________________

User entry of depth-outflow-storage data
------------------------------------------------------------------------
Total number of inflow hydrograph intervals = 40
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
------------------------------------------------------------------------
------------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
------------------------------------------------------------------------
------------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
------------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.276      0.133      0.276        0.276
   2.000      0.584      0.193      0.583        0.585
   3.000      0.930      0.700      0.928        0.932
   3.500      1.118      0.824      1.115        1.121
   4.000      1.316      0.930      1.313        1.319
   4.500      1.528      1.024      1.524        1.532
   4.750      1.637      1.068      1.633        1.641
   5.000      1.749     18.283      1.686        1.812
   6.000      2.231    253.655      1.358        3.104
------------------------------------------------------------------------
               Hydrograph Detention Basin Routing
------------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
------------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                    Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0       4.7    9.35   14.03   18.70 (Ft.)
 0.083    0.98    0.00      0.003  OI      |       |       |       |     0.01
 0.167    2.06    0.01      0.014  O  I    |       |       |       |     0.05
 0.250    2.13    0.01      0.028  O  I    |       |       |       |     0.10
 0.333    2.36    0.02      0.044  O   I   |       |       |       |     0.16
 0.417    2.70    0.03      0.061  O   I   |       |       |       |     0.22
 0.500    2.98    0.04      0.080  O    I  |       |       |       |     0.29
 0.583    3.02    0.05      0.101  O    I  |       |       |       |     0.36
 0.667    3.07    0.06      0.121  O    I  |       |       |       |     0.44
 0.750    3.28    0.07      0.143  O    I  |       |       |       |     0.52
 0.833    3.10    0.08      0.164  O    I  |       |       |       |     0.59
 0.917    2.94    0.09      0.184  O    I  |       |       |       |     0.67
 1.000    3.13    0.10      0.205  O    I  |       |       |       |     0.74
 1.083    3.59    0.11      0.227  O     I |       |       |       |     0.82
 1.167    3.96    0.12      0.252  O     I |       |       |       |     0.91
 1.250    4.04    0.13      0.279  O     I |       |       |       |     1.01
 1.333    3.93    0.14      0.305  O     I |       |       |       |     1.10
 1.417    4.23    0.14      0.332  O      I|       |       |       |     1.18
```

1.500	4.76	0.15	0.362	O	I	|	|	|	1.28
1.583	4.71	0.16	0.394	O	I	|	|	|	1.38
1.667	4.74	0.16	0.425	O	I	|	|	|	1.49
1.750	5.42	0.17	0.459	O	|I	|	|	|	1.60
1.833	5.80	0.18	0.497	O	|I	|	|	|	1.72
1.917	5.60	0.18	0.535	O	|I	|	|	|	1.84
2.000	5.52	0.19	0.572	O	|I	|	|	|	1.96
2.083	5.65	0.23	0.609	O	|I	|	|	|	2.07
2.167	6.56	0.29	0.649	O	| I	|	|	|	2.19
2.250	8.20	0.36	0.698	O	| I	|	|	|	2.33
2.333	7.93	0.44	0.750	O	| I	|	|	|	2.48
2.417	10.79	0.53	0.812	O	| I	|	|	|	2.66
2.500	15.68	0.65	0.899	|O	|	| I	|	|	2.91
2.583	18.70	0.75	1.012	|O	|	|	| I	|	3.22
2.667	17.20	0.83	1.130	|O	|	|	| I	|	3.53
2.750	10.21	0.88	1.219	|O	|	|I	|	|	3.76
2.833	5.34	0.90	1.266	|O	|I	|	|	|	3.87
2.917	4.04	0.92	1.292	|O	I |	|	|	|	3.94
3.000	2.61	0.93	1.309	|O	I |	|	|	|	3.98
3.083	1.00	0.93	1.315	|O	|	|	|	|	4.00
3.167	0.29	0.93	1.313	IO	|	|	|	|	3.99
3.250	0.10	0.93	1.308	IO	|	|	|	|	3.98
3.333	0.02	0.92	1.302	IO	|	|	|	|	3.96
3.417	0.00	0.92	1.296	IO	|	|	|	|	3.95
3.500	0.00	0.92	1.289	IO	|	|	|	|	3.93
3.583	0.00	0.91	1.283	IO	|	|	|	|	3.92
3.667	0.00	0.91	1.277	IO	|	|	|	|	3.90
3.750	0.00	0.91	1.271	IO	|	|	|	|	3.89
3.833	0.00	0.90	1.264	IO	|	|	|	|	3.87
3.917	0.00	0.90	1.258	IO	|	|	|	|	3.85
4.000	0.00	0.90	1.252	IO	|	|	|	|	3.84
4.083	0.00	0.89	1.246	IO	|	|	|	|	3.82
4.167	0.00	0.89	1.240	IO	|	|	|	|	3.81
4.250	0.00	0.89	1.234	IO	|	|	|	|	3.79
4.333	0.00	0.88	1.228	IO	|	|	|	|	3.78
4.417	0.00	0.88	1.221	IO	|	|	|	|	3.76
4.500	0.00	0.88	1.215	IO	|	|	|	|	3.75
4.583	0.00	0.87	1.209	IO	|	|	|	|	3.73
4.667	0.00	0.87	1.203	IO	|	|	|	|	3.72
4.750	0.00	0.87	1.197	IO	|	|	|	|	3.70
4.833	0.00	0.86	1.191	IO	|	|	|	|	3.69
4.917	0.00	0.86	1.186	IO	|	|	|	|	3.67
5.000	0.00	0.86	1.180	IO	|	|	|	|	3.66
5.083	0.00	0.85	1.174	IO	|	|	|	|	3.64
5.167	0.00	0.85	1.168	IO	|	|	|	|	3.63
5.250	0.00	0.85	1.162	IO	|	|	|	|	3.61
5.333	0.00	0.84	1.156	IO	|	|	|	|	3.60
5.417	0.00	0.84	1.150	IO	|	|	|	|	3.58
5.500	0.00	0.84	1.145	IO	|	|	|	|	3.57
5.583	0.00	0.84	1.139	IO	|	|	|	|	3.55
5.667	0.00	0.83	1.133	IO	|	|	|	|	3.54
5.750	0.00	0.83	1.127	IO	|	|	|	|	3.52
5.833	0.00	0.83	1.122	IO	|	|	|	|	3.51
5.917	0.00	0.82	1.116	IO	|	|	|	|	3.49
6.000	0.00	0.82	1.110	IO	|	|	|	|	3.48
6.083	0.00	0.82	1.105	IO	|	|	|	|	3.46
6.167	0.00	0.81	1.099	IO	|	|	|	|	3.45
6.250	0.00	0.81	1.094	IO	|	|	|	|	3.43
6.333	0.00	0.80	1.088	IO	|	|	|	|	3.42
6.417	0.00	0.80	1.082	IO	|	|	|	|	3.41
6.500	0.00	0.80	1.077	IO	|	|	|	|	3.39
6.583	0.00	0.79	1.071	IO	|	|	|	|	3.38
6.667	0.00	0.79	1.066	IO	|	|	|	|	3.36
6.750	0.00	0.79	1.061	IO	|	|	|	|	3.35
6.833	0.00	0.78	1.055	IO	|	|	|	|	3.33
6.917	0.00	0.78	1.050	IO	|	|	|	|	3.32
7.000	0.00	0.78	1.044	IO	|	|	|	|	3.30
7.083	0.00	0.77	1.039	IO	|	|	|	|	3.29
7.167	0.00	0.77	1.034	IO	|	|	|	|	3.28
7.250	0.00	0.76	1.029	IO	|	|	|	|	3.26
7.333	0.00	0.76	1.023	IO	|	|	|	|	3.25
7.417	0.00	0.76	1.018	IO	|	|	|	|	3.23
7.500	0.00	0.75	1.013	IO	|	|	|	|	3.22
7.583	0.00	0.75	1.008	IO	|	|	|	|	3.21
7.667	0.00	0.75	1.002	IO	|	|	|	|	3.19
7.750	0.00	0.74	0.997	IO	|	|	|	|	3.18
7.833	0.00	0.74	0.992	IO	|	|	|	|	3.17
7.917	0.00	0.74	0.987	IO	|	|	|	|	3.15
8.000	0.00	0.73	0.982	IO	|	|	|	|	3.14
8.083	0.00	0.73	0.977	IO	|	|	|	|	3.13
8.167	0.00	0.73	0.972	IO	|	|	|	|	3.11
8.250	0.00	0.72	0.967	IO	|	|	|	|	3.10
8.333	0.00	0.72	0.962	IO	|	|	|	|	3.09
8.417	0.00	0.72	0.957	IO	|	|	|	|	3.07
8.500	0.00	0.71	0.952	IO	|	|	|	|	3.06
8.583	0.00	0.71	0.947	IO	|	|	|	|	3.05

8.667	0.00	0.71	0.942	IO				3.03
8.750	0.00	0.70	0.937	IO				3.02
8.833	0.00	0.70	0.933	IO				3.01
8.917	0.00	0.70	0.928	IO				2.99
9.000	0.00	0.69	0.923	IO				2.98
9.083	0.00	0.68	0.918	IO				2.97
9.167	0.00	0.68	0.914	IO				2.95
9.250	0.00	0.67	0.909	IO				2.94
9.333	0.00	0.66	0.904	IO				2.93
9.417	0.00	0.66	0.900	IO				2.91
9.500	0.00	0.65	0.895	IO				2.90
9.583	0.00	0.64	0.891	IO				2.89
9.667	0.00	0.64	0.887	IO				2.87
9.750	0.00	0.63	0.882	IO				2.86
9.833	0.00	0.62	0.878	IO				2.85
9.917	0.00	0.62	0.874	IO				2.84
10.000	0.00	0.61	0.869	IO				2.82
10.083	0.00	0.60	0.865	IO				2.81
10.167	0.00	0.60	0.861	IO				2.80
10.250	0.00	0.59	0.857	IO				2.79
10.333	0.00	0.59	0.853	IO				2.78
10.417	0.00	0.58	0.849	O				2.77
10.500	0.00	0.58	0.845	O				2.75
10.583	0.00	0.57	0.841	O				2.74
10.667	0.00	0.56	0.837	O				2.73
10.750	0.00	0.56	0.833	O				2.72
10.833	0.00	0.55	0.829	O				2.71
10.917	0.00	0.55	0.826	O				2.70
11.000	0.00	0.54	0.822	O				2.69
11.083	0.00	0.54	0.818	O				2.68
11.167	0.00	0.53	0.814	O				2.67
11.250	0.00	0.53	0.811	O				2.66
11.333	0.00	0.52	0.807	O				2.64
11.417	0.00	0.51	0.804	O				2.63
11.500	0.00	0.51	0.800	O				2.62
11.583	0.00	0.50	0.797	O				2.61
11.667	0.00	0.50	0.793	O				2.60
11.750	0.00	0.49	0.790	O				2.59
11.833	0.00	0.49	0.786	O				2.58
11.917	0.00	0.48	0.783	O				2.58
12.000	0.00	0.48	0.780	O				2.57
12.083	0.00	0.47	0.776	O				2.56
12.167	0.00	0.47	0.773	O				2.55
12.250	0.00	0.47	0.770	O				2.54
12.333	0.00	0.46	0.767	O				2.53
12.417	0.00	0.46	0.764	O				2.52
12.500	0.00	0.45	0.760	O				2.51
12.583	0.00	0.45	0.757	O				2.50
12.667	0.00	0.44	0.754	O				2.49
12.750	0.00	0.44	0.751	O				2.48
12.833	0.00	0.43	0.748	O				2.47
12.917	0.00	0.43	0.745	O				2.47
13.000	0.00	0.42	0.742	O				2.46
13.083	0.00	0.42	0.739	O				2.45
13.167	0.00	0.42	0.737	O				2.44
13.250	0.00	0.41	0.734	O				2.43
13.333	0.00	0.41	0.731	O				2.42
13.417	0.00	0.40	0.728	O				2.42
13.500	0.00	0.40	0.725	O				2.41
13.583	0.00	0.40	0.723	O				2.40
13.667	0.00	0.39	0.720	O				2.39
13.750	0.00	0.39	0.717	O				2.38
13.833	0.00	0.38	0.714	O				2.38
13.917	0.00	0.38	0.712	O				2.37
14.000	0.00	0.38	0.709	O				2.36
14.083	0.00	0.37	0.707	O				2.35
14.167	0.00	0.37	0.704	O				2.35
14.250	0.00	0.37	0.702	O				2.34
14.333	0.00	0.36	0.699	O				2.33
14.417	0.00	0.36	0.697	O				2.33
14.500	0.00	0.35	0.694	O				2.32
14.583	0.00	0.35	0.692	O				2.31
14.667	0.00	0.35	0.689	O				2.30
14.750	0.00	0.34	0.687	O				2.30
14.833	0.00	0.34	0.685	O				2.29
14.917	0.00	0.34	0.682	O				2.28
15.000	0.00	0.33	0.680	O				2.28
15.083	0.00	0.33	0.678	O				2.27
15.167	0.00	0.33	0.675	O				2.26
15.250	0.00	0.32	0.673	O				2.26
15.333	0.00	0.32	0.671	O				2.25
15.417	0.00	0.32	0.669	O				2.24
15.500	0.00	0.31	0.667	O				2.24
15.583	0.00	0.31	0.664	O				2.23
15.667	0.00	0.31	0.662	O				2.23
15.750	0.00	0.30	0.660	O				2.22

15.833	0.00	0.30	0.658	o	|	|	|	|	2.21
15.917	0.00	0.30	0.656	o	|	|	|	|	2.21
16.000	0.00	0.30	0.654	o	|	|	|	|	2.20
16.083	0.00	0.29	0.652	o	|	|	|	|	2.20
16.167	0.00	0.29	0.650	o	|	|	|	|	2.19
16.250	0.00	0.29	0.648	o	|	|	|	|	2.18
16.333	0.00	0.28	0.646	o	|	|	|	|	2.18
16.417	0.00	0.28	0.644	o	|	|	|	|	2.17
16.500	0.00	0.28	0.642	o	|	|	|	|	2.17
16.583	0.00	0.28	0.640	o	|	|	|	|	2.16
16.667	0.00	0.27	0.638	o	|	|	|	|	2.16
16.750	0.00	0.27	0.636	o	|	|	|	|	2.15
16.833	0.00	0.27	0.635	o	|	|	|	|	2.15
16.917	0.00	0.26	0.633	o	|	|	|	|	2.14
17.000	0.00	0.26	0.631	o	|	|	|	|	2.14
17.083	0.00	0.26	0.629	o	|	|	|	|	2.13
17.167	0.00	0.26	0.627	o	|	|	|	|	2.13
17.250	0.00	0.25	0.626	o	|	|	|	|	2.12
17.333	0.00	0.25	0.624	o	|	|	|	|	2.12
17.417	0.00	0.25	0.622	o	|	|	|	|	2.11
17.500	0.00	0.25	0.620	o	|	|	|	|	2.11
17.583	0.00	0.24	0.619	o	|	|	|	|	2.10
17.667	0.00	0.24	0.617	o	|	|	|	|	2.10
17.750	0.00	0.24	0.615	o	|	|	|	|	2.09
17.833	0.00	0.24	0.614	o	|	|	|	|	2.09
17.917	0.00	0.23	0.612	o	|	|	|	|	2.08
18.000	0.00	0.23	0.611	o	|	|	|	|	2.08
18.083	0.00	0.23	0.609	o	|	|	|	|	2.07
18.167	0.00	0.23	0.607	o	|	|	|	|	2.07
18.250	0.00	0.23	0.606	o	|	|	|	|	2.06
18.333	0.00	0.22	0.604	o	|	|	|	|	2.06
18.417	0.00	0.22	0.603	o	|	|	|	|	2.05
18.500	0.00	0.22	0.601	o	|	|	|	|	2.05
18.583	0.00	0.22	0.600	o	|	|	|	|	2.05
18.667	0.00	0.21	0.598	o	|	|	|	|	2.04
18.750	0.00	0.21	0.597	o	|	|	|	|	2.04
18.833	0.00	0.21	0.595	o	|	|	|	|	2.03
18.917	0.00	0.21	0.594	o	|	|	|	|	2.03
19.000	0.00	0.21	0.593	o	|	|	|	|	2.02
19.083	0.00	0.20	0.591	o	|	|	|	|	2.02
19.167	0.00	0.20	0.590	o	|	|	|	|	2.02
19.250	0.00	0.20	0.588	o	|	|	|	|	2.01
19.333	0.00	0.20	0.587	o	|	|	|	|	2.01
19.417	0.00	0.20	0.586	o	|	|	|	|	2.00
19.500	0.00	0.19	0.584	o	|	|	|	|	2.00
19.583	0.00	0.19	0.583	o	|	|	|	|	2.00
19.667	0.00	0.19	0.582	o	|	|	|	|	1.99
19.750	0.00	0.19	0.580	o	|	|	|	|	1.99
19.833	0.00	0.19	0.579	o	|	|	|	|	1.98
19.917	0.00	0.19	0.578	o	|	|	|	|	1.98
20.000	0.00	0.19	0.576	o	|	|	|	|	1.98
20.083	0.00	0.19	0.575	o	|	|	|	|	1.97
20.167	0.00	0.19	0.574	o	|	|	|	|	1.97
20.250	0.00	0.19	0.572	o	|	|	|	|	1.96
20.333	0.00	0.19	0.571	o	|	|	|	|	1.96
20.417	0.00	0.19	0.570	o	|	|	|	|	1.95
20.500	0.00	0.19	0.568	o	|	|	|	|	1.95
20.583	0.00	0.19	0.567	o	|	|	|	|	1.95
20.667	0.00	0.19	0.566	o	|	|	|	|	1.94
20.750	0.00	0.19	0.565	o	|	|	|	|	1.94
20.833	0.00	0.19	0.563	o	|	|	|	|	1.93
20.917	0.00	0.19	0.562	o	|	|	|	|	1.93
21.000	0.00	0.19	0.561	o	|	|	|	|	1.92
21.083	0.00	0.19	0.559	o	|	|	|	|	1.92
21.167	0.00	0.19	0.558	o	|	|	|	|	1.92
21.250	0.00	0.19	0.557	o	|	|	|	|	1.91
21.333	0.00	0.19	0.555	o	|	|	|	|	1.91
21.417	0.00	0.19	0.554	o	|	|	|	|	1.90
21.500	0.00	0.19	0.553	o	|	|	|	|	1.90
21.583	0.00	0.19	0.552	o	|	|	|	|	1.89
21.667	0.00	0.19	0.550	o	|	|	|	|	1.89
21.750	0.00	0.19	0.549	o	|	|	|	|	1.89
21.833	0.00	0.19	0.548	o	|	|	|	|	1.88
21.917	0.00	0.19	0.546	o	|	|	|	|	1.88
22.000	0.00	0.19	0.545	o	|	|	|	|	1.87
22.083	0.00	0.19	0.544	o	|	|	|	|	1.87
22.167	0.00	0.18	0.543	o	|	|	|	|	1.87
22.250	0.00	0.18	0.541	o	|	|	|	|	1.86
22.333	0.00	0.18	0.540	o	|	|	|	|	1.86
22.417	0.00	0.18	0.539	o	|	|	|	|	1.85
22.500	0.00	0.18	0.538	o	|	|	|	|	1.85
22.583	0.00	0.18	0.536	o	|	|	|	|	1.85
22.667	0.00	0.18	0.535	o	|	|	|	|	1.84
22.750	0.00	0.18	0.534	o	|	|	|	|	1.84
22.833	0.00	0.18	0.533	o	|	|	|	|	1.83
22.917	0.00	0.18	0.531	o	|	|	|	|	1.83

23.000	0.00	0.18	0.530	o	|	|	|	|	1.82
23.083	0.00	0.18	0.529	o	|	|	|	|	1.82
23.167	0.00	0.18	0.527	o	|	|	|	|	1.82
23.250	0.00	0.18	0.526	o	|	|	|	|	1.81
23.333	0.00	0.18	0.525	o	|	|	|	|	1.81
23.417	0.00	0.18	0.524	o	|	|	|	|	1.80
23.500	0.00	0.18	0.522	o	|	|	|	|	1.80
23.583	0.00	0.18	0.521	o	|	|	|	|	1.80
23.667	0.00	0.18	0.520	o	|	|	|	|	1.79
23.750	0.00	0.18	0.519	o	|	|	|	|	1.79
23.833	0.00	0.18	0.518	o	|	|	|	|	1.78
23.917	0.00	0.18	0.516	o	|	|	|	|	1.78
24.000	0.00	0.18	0.515	o	|	|	|	|	1.78
24.083	0.00	0.18	0.514	o	|	|	|	|	1.77
24.167	0.00	0.18	0.513	o	|	|	|	|	1.77
24.250	0.00	0.18	0.511	o	|	|	|	|	1.76
24.333	0.00	0.18	0.510	o	|	|	|	|	1.76
24.417	0.00	0.18	0.509	o	|	|	|	|	1.76
24.500	0.00	0.18	0.508	o	|	|	|	|	1.75
24.583	0.00	0.18	0.506	o	|	|	|	|	1.75
24.667	0.00	0.18	0.505	o	|	|	|	|	1.74
24.750	0.00	0.18	0.504	o	|	|	|	|	1.74
24.833	0.00	0.18	0.503	o	|	|	|	|	1.74
24.917	0.00	0.18	0.502	o	|	|	|	|	1.73
25.000	0.00	0.18	0.500	o	|	|	|	|	1.73
25.083	0.00	0.18	0.499	o	|	|	|	|	1.72
25.167	0.00	0.18	0.498	o	|	|	|	|	1.72
25.250	0.00	0.18	0.497	o	|	|	|	|	1.72
25.333	0.00	0.18	0.495	o	|	|	|	|	1.71
25.417	0.00	0.18	0.494	o	|	|	|	|	1.71
25.500	0.00	0.18	0.493	o	|	|	|	|	1.70
25.583	0.00	0.18	0.492	o	|	|	|	|	1.70
25.667	0.00	0.17	0.491	o	|	|	|	|	1.70
25.750	0.00	0.17	0.489	o	|	|	|	|	1.69
25.833	0.00	0.17	0.488	o	|	|	|	|	1.69
25.917	0.00	0.17	0.487	o	|	|	|	|	1.69
26.000	0.00	0.17	0.486	o	|	|	|	|	1.68
26.083	0.00	0.17	0.485	o	|	|	|	|	1.68
26.167	0.00	0.17	0.483	o	|	|	|	|	1.67
26.250	0.00	0.17	0.482	o	|	|	|	|	1.67
26.333	0.00	0.17	0.481	o	|	|	|	|	1.67
26.417	0.00	0.17	0.480	o	|	|	|	|	1.66
26.500	0.00	0.17	0.479	o	|	|	|	|	1.66
26.583	0.00	0.17	0.477	o	|	|	|	|	1.65
26.667	0.00	0.17	0.476	o	|	|	|	|	1.65
26.750	0.00	0.17	0.475	o	|	|	|	|	1.65
26.833	0.00	0.17	0.474	o	|	|	|	|	1.64
26.917	0.00	0.17	0.473	o	|	|	|	|	1.64
27.000	0.00	0.17	0.472	o	|	|	|	|	1.63
27.083	0.00	0.17	0.470	o	|	|	|	|	1.63
27.167	0.00	0.17	0.469	o	|	|	|	|	1.63
27.250	0.00	0.17	0.468	o	|	|	|	|	1.62
27.333	0.00	0.17	0.467	o	|	|	|	|	1.62
27.417	0.00	0.17	0.466	o	|	|	|	|	1.62
27.500	0.00	0.17	0.465	o	|	|	|	|	1.61
27.583	0.00	0.17	0.463	o	|	|	|	|	1.61
27.667	0.00	0.17	0.462	o	|	|	|	|	1.60
27.750	0.00	0.17	0.461	o	|	|	|	|	1.60
27.833	0.00	0.17	0.460	o	|	|	|	|	1.60
27.917	0.00	0.17	0.459	o	|	|	|	|	1.59
28.000	0.00	0.17	0.458	o	|	|	|	|	1.59
28.083	0.00	0.17	0.456	o	|	|	|	|	1.59
28.167	0.00	0.17	0.455	o	|	|	|	|	1.58
28.250	0.00	0.17	0.454	o	|	|	|	|	1.58
28.333	0.00	0.17	0.453	o	|	|	|	|	1.57
28.417	0.00	0.17	0.452	o	|	|	|	|	1.57
28.500	0.00	0.17	0.451	o	|	|	|	|	1.57
28.583	0.00	0.17	0.449	o	|	|	|	|	1.56
28.667	0.00	0.17	0.448	o	|	|	|	|	1.56
28.750	0.00	0.17	0.447	o	|	|	|	|	1.56
28.833	0.00	0.17	0.446	o	|	|	|	|	1.55
28.917	0.00	0.17	0.445	o	|	|	|	|	1.55
29.000	0.00	0.17	0.444	o	|	|	|	|	1.54
29.083	0.00	0.17	0.443	o	|	|	|	|	1.54
29.167	0.00	0.17	0.441	o	|	|	|	|	1.54
29.250	0.00	0.17	0.440	o	|	|	|	|	1.53
29.333	0.00	0.16	0.439	o	|	|	|	|	1.53
29.417	0.00	0.16	0.438	o	|	|	|	|	1.53
29.500	0.00	0.16	0.437	o	|	|	|	|	1.52
29.583	0.00	0.16	0.436	o	|	|	|	|	1.52
29.667	0.00	0.16	0.435	o	|	|	|	|	1.52
29.750	0.00	0.16	0.434	o	|	|	|	|	1.51
29.833	0.00	0.16	0.432	o	|	|	|	|	1.51
29.917	0.00	0.16	0.431	o	|	|	|	|	1.50
30.000	0.00	0.16	0.430	o	|	|	|	|	1.50
30.083	0.00	0.16	0.429	o	|	|	|	|	1.50

30.167	0.00	0.16	0.428	o	|	|	|	|	1.49
30.250	0.00	0.16	0.427	o	|	|	|	|	1.49
30.333	0.00	0.16	0.426	o	|	|	|	|	1.49
30.417	0.00	0.16	0.425	o	|	|	|	|	1.48
30.500	0.00	0.16	0.423	o	|	|	|	|	1.48
30.583	0.00	0.16	0.422	o	|	|	|	|	1.48
30.667	0.00	0.16	0.421	o	|	|	|	|	1.47
30.750	0.00	0.16	0.420	o	|	|	|	|	1.47
30.833	0.00	0.16	0.419	o	|	|	|	|	1.46
30.917	0.00	0.16	0.418	o	|	|	|	|	1.46
31.000	0.00	0.16	0.417	o	|	|	|	|	1.46
31.083	0.00	0.16	0.416	o	|	|	|	|	1.45
31.167	0.00	0.16	0.415	o	|	|	|	|	1.45
31.250	0.00	0.16	0.413	o	|	|	|	|	1.45
31.333	0.00	0.16	0.412	o	|	|	|	|	1.44
31.417	0.00	0.16	0.411	o	|	|	|	|	1.44
31.500	0.00	0.16	0.410	o	|	|	|	|	1.44
31.583	0.00	0.16	0.409	o	|	|	|	|	1.43
31.667	0.00	0.16	0.408	o	|	|	|	|	1.43
31.750	0.00	0.16	0.407	o	|	|	|	|	1.43
31.833	0.00	0.16	0.406	o	|	|	|	|	1.42
31.917	0.00	0.16	0.405	o	|	|	|	|	1.42
32.000	0.00	0.16	0.404	o	|	|	|	|	1.41
32.083	0.00	0.16	0.403	o	|	|	|	|	1.41
32.167	0.00	0.16	0.401	o	|	|	|	|	1.41
32.250	0.00	0.16	0.400	o	|	|	|	|	1.40
32.333	0.00	0.16	0.399	o	|	|	|	|	1.40
32.417	0.00	0.16	0.398	o	|	|	|	|	1.40
32.500	0.00	0.16	0.397	o	|	|	|	|	1.39
32.583	0.00	0.16	0.396	o	|	|	|	|	1.39
32.667	0.00	0.16	0.395	o	|	|	|	|	1.39
32.750	0.00	0.16	0.394	o	|	|	|	|	1.38
32.833	0.00	0.16	0.393	o	|	|	|	|	1.38
32.917	0.00	0.16	0.392	o	|	|	|	|	1.38
33.000	0.00	0.16	0.391	o	|	|	|	|	1.37
33.083	0.00	0.16	0.390	o	|	|	|	|	1.37
33.167	0.00	0.15	0.389	o	|	|	|	|	1.37
33.250	0.00	0.15	0.387	o	|	|	|	|	1.36
33.333	0.00	0.15	0.386	o	|	|	|	|	1.36
33.417	0.00	0.15	0.385	o	|	|	|	|	1.36
33.500	0.00	0.15	0.384	o	|	|	|	|	1.35
33.583	0.00	0.15	0.383	o	|	|	|	|	1.35
33.667	0.00	0.15	0.382	o	|	|	|	|	1.34
33.750	0.00	0.15	0.381	o	|	|	|	|	1.34
33.833	0.00	0.15	0.380	o	|	|	|	|	1.34
33.917	0.00	0.15	0.379	o	|	|	|	|	1.33
34.000	0.00	0.15	0.378	o	|	|	|	|	1.33
34.083	0.00	0.15	0.377	o	|	|	|	|	1.33
34.167	0.00	0.15	0.376	o	|	|	|	|	1.32
34.250	0.00	0.15	0.375	o	|	|	|	|	1.32
34.333	0.00	0.15	0.374	o	|	|	|	|	1.32
34.417	0.00	0.15	0.373	o	|	|	|	|	1.31
34.500	0.00	0.15	0.372	o	|	|	|	|	1.31
34.583	0.00	0.15	0.371	o	|	|	|	|	1.31
34.667	0.00	0.15	0.370	o	|	|	|	|	1.30
34.750	0.00	0.15	0.369	o	|	|	|	|	1.30
34.833	0.00	0.15	0.367	o	|	|	|	|	1.30
34.917	0.00	0.15	0.366	o	|	|	|	|	1.29
35.000	0.00	0.15	0.365	o	|	|	|	|	1.29
35.083	0.00	0.15	0.364	o	|	|	|	|	1.29
35.167	0.00	0.15	0.363	o	|	|	|	|	1.28
35.250	0.00	0.15	0.362	o	|	|	|	|	1.28
35.333	0.00	0.15	0.361	o	|	|	|	|	1.28
35.417	0.00	0.15	0.360	o	|	|	|	|	1.27
35.500	0.00	0.15	0.359	o	|	|	|	|	1.27
35.583	0.00	0.15	0.358	o	|	|	|	|	1.27
35.667	0.00	0.15	0.357	o	|	|	|	|	1.26
35.750	0.00	0.15	0.356	o	|	|	|	|	1.26
35.833	0.00	0.15	0.355	o	|	|	|	|	1.26
35.917	0.00	0.15	0.354	o	|	|	|	|	1.25
36.000	0.00	0.15	0.353	o	|	|	|	|	1.25
36.083	0.00	0.15	0.352	o	|	|	|	|	1.25
36.167	0.00	0.15	0.351	o	|	|	|	|	1.24
36.250	0.00	0.15	0.350	o	|	|	|	|	1.24
36.333	0.00	0.15	0.349	o	|	|	|	|	1.24
36.417	0.00	0.15	0.348	o	|	|	|	|	1.23
36.500	0.00	0.15	0.347	o	|	|	|	|	1.23
36.583	0.00	0.15	0.346	o	|	|	|	|	1.23
36.667	0.00	0.15	0.345	o	|	|	|	|	1.22
36.750	0.00	0.15	0.344	o	|	|	|	|	1.22
36.833	0.00	0.15	0.343	o	|	|	|	|	1.22
36.917	0.00	0.15	0.342	o	|	|	|	|	1.21
37.000	0.00	0.15	0.341	o	|	|	|	|	1.21
37.083	0.00	0.15	0.340	o	|	|	|	|	1.21
37.167	0.00	0.15	0.339	o	|	|	|	|	1.20
37.250	0.00	0.15	0.338	o	|	|	|	|	1.20

37.333	0.00	0.14	0.337	o	|	|	|	|	1.20
37.417	0.00	0.14	0.336	o	|	|	|	|	1.19
37.500	0.00	0.14	0.335	o	|	|	|	|	1.19
37.583	0.00	0.14	0.334	o	|	|	|	|	1.19
37.667	0.00	0.14	0.333	o	|	|	|	|	1.18
37.750	0.00	0.14	0.332	o	|	|	|	|	1.18
37.833	0.00	0.14	0.331	o	|	|	|	|	1.18
37.917	0.00	0.14	0.330	o	|	|	|	|	1.18
38.000	0.00	0.14	0.329	o	|	|	|	|	1.17
38.083	0.00	0.14	0.328	o	|	|	|	|	1.17
38.167	0.00	0.14	0.327	o	|	|	|	|	1.17
38.250	0.00	0.14	0.326	o	|	|	|	|	1.16
38.333	0.00	0.14	0.325	o	|	|	|	|	1.16
38.417	0.00	0.14	0.324	o	|	|	|	|	1.16
38.500	0.00	0.14	0.323	o	|	|	|	|	1.15
38.583	0.00	0.14	0.322	o	|	|	|	|	1.15
38.667	0.00	0.14	0.321	o	|	|	|	|	1.15
38.750	0.00	0.14	0.320	o	|	|	|	|	1.14
38.833	0.00	0.14	0.319	o	|	|	|	|	1.14
38.917	0.00	0.14	0.318	o	|	|	|	|	1.14
39.000	0.00	0.14	0.317	o	|	|	|	|	1.13
39.083	0.00	0.14	0.316	o	|	|	|	|	1.13
39.167	0.00	0.14	0.315	o	|	|	|	|	1.13
39.250	0.00	0.14	0.314	o	|	|	|	|	1.12
39.333	0.00	0.14	0.313	o	|	|	|	|	1.12
39.417	0.00	0.14	0.312	o	|	|	|	|	1.12
39.500	0.00	0.14	0.311	o	|	|	|	|	1.12
39.583	0.00	0.14	0.310	o	|	|	|	|	1.11
39.667	0.00	0.14	0.310	o	|	|	|	|	1.11
39.750	0.00	0.14	0.309	o	|	|	|	|	1.11
39.833	0.00	0.14	0.308	o	|	|	|	|	1.10
39.917	0.00	0.14	0.307	o	|	|	|	|	1.10
40.000	0.00	0.14	0.306	o	|	|	|	|	1.10
40.083	0.00	0.14	0.305	o	|	|	|	|	1.09
40.167	0.00	0.14	0.304	o	|	|	|	|	1.09
40.250	0.00	0.14	0.303	o	|	|	|	|	1.09
40.333	0.00	0.14	0.302	o	|	|	|	|	1.08
40.417	0.00	0.14	0.301	o	|	|	|	|	1.08
40.500	0.00	0.14	0.300	o	|	|	|	|	1.08
40.583	0.00	0.14	0.299	o	|	|	|	|	1.07
40.667	0.00	0.14	0.298	o	|	|	|	|	1.07
40.750	0.00	0.14	0.297	o	|	|	|	|	1.07
40.833	0.00	0.14	0.296	o	|	|	|	|	1.07
40.917	0.00	0.14	0.295	o	|	|	|	|	1.06
41.000	0.00	0.14	0.294	o	|	|	|	|	1.06
41.083	0.00	0.14	0.293	o	|	|	|	|	1.06
41.167	0.00	0.14	0.292	o	|	|	|	|	1.05
41.250	0.00	0.14	0.292	o	|	|	|	|	1.05
41.333	0.00	0.14	0.291	o	|	|	|	|	1.05
41.417	0.00	0.14	0.290	o	|	|	|	|	1.04
41.500	0.00	0.14	0.289	o	|	|	|	|	1.04
41.583	0.00	0.14	0.288	o	|	|	|	|	1.04
41.667	0.00	0.14	0.287	o	|	|	|	|	1.04
41.750	0.00	0.13	0.286	o	|	|	|	|	1.03
41.833	0.00	0.13	0.285	o	|	|	|	|	1.03
41.917	0.00	0.13	0.284	o	|	|	|	|	1.03
42.000	0.00	0.13	0.283	o	|	|	|	|	1.02
42.083	0.00	0.13	0.282	o	|	|	|	|	1.02
42.167	0.00	0.13	0.281	o	|	|	|	|	1.02
42.250	0.00	0.13	0.280	o	|	|	|	|	1.01
42.333	0.00	0.13	0.279	o	|	|	|	|	1.01
42.417	0.00	0.13	0.279	o	|	|	|	|	1.01
42.500	0.00	0.13	0.278	o	|	|	|	|	1.01
42.583	0.00	0.13	0.277	o	|	|	|	|	1.00
42.667	0.00	0.13	0.276	o	|	|	|	|	1.00
42.750	0.00	0.13	0.275	o	|	|	|	|	1.00
42.833	0.00	0.13	0.274	o	|	|	|	|	0.99
42.917	0.00	0.13	0.273	o	|	|	|	|	0.99
43.000	0.00	0.13	0.272	o	|	|	|	|	0.99
43.083	0.00	0.13	0.271	o	|	|	|	|	0.98
43.167	0.00	0.13	0.270	o	|	|	|	|	0.98
43.250	0.00	0.13	0.269	o	|	|	|	|	0.98
43.333	0.00	0.13	0.269	o	|	|	|	|	0.97
43.417	0.00	0.13	0.268	o	|	|	|	|	0.97
43.500	0.00	0.13	0.267	o	|	|	|	|	0.97
43.583	0.00	0.13	0.266	o	|	|	|	|	0.96
43.667	0.00	0.13	0.265	o	|	|	|	|	0.96
43.750	0.00	0.13	0.264	o	|	|	|	|	0.96
43.833	0.00	0.13	0.263	o	|	|	|	|	0.95
43.917	0.00	0.13	0.262	o	|	|	|	|	0.95
44.000	0.00	0.13	0.262	o	|	|	|	|	0.95
44.083	0.00	0.13	0.261	o	|	|	|	|	0.94
44.167	0.00	0.13	0.260	o	|	|	|	|	0.94
44.250	0.00	0.12	0.259	o	|	|	|	|	0.94
44.333	0.00	0.12	0.258	o	|	|	|	|	0.93
44.417	0.00	0.12	0.257	o	|	|	|	|	0.93

44.500	0.00	0.12	0.256	o	|	|	|	|	0.93
44.583	0.00	0.12	0.255	o	|	|	|	|	0.93
44.667	0.00	0.12	0.255	o	|	|	|	|	0.92
44.750	0.00	0.12	0.254	o	|	|	|	|	0.92
44.833	0.00	0.12	0.253	o	|	|	|	|	0.92
44.917	0.00	0.12	0.252	o	|	|	|	|	0.91
45.000	0.00	0.12	0.251	o	|	|	|	|	0.91
45.083	0.00	0.12	0.250	o	|	|	|	|	0.91
45.167	0.00	0.12	0.250	o	|	|	|	|	0.90
45.250	0.00	0.12	0.249	o	|	|	|	|	0.90
45.333	0.00	0.12	0.248	o	|	|	|	|	0.90
45.417	0.00	0.12	0.247	o	|	|	|	|	0.90
45.500	0.00	0.12	0.246	o	|	|	|	|	0.89
45.583	0.00	0.12	0.246	o	|	|	|	|	0.89
45.667	0.00	0.12	0.245	o	|	|	|	|	0.89
45.750	0.00	0.12	0.244	o	|	|	|	|	0.88
45.833	0.00	0.12	0.243	o	|	|	|	|	0.88
45.917	0.00	0.12	0.242	o	|	|	|	|	0.88
46.000	0.00	0.12	0.241	o	|	|	|	|	0.87
46.083	0.00	0.12	0.241	o	|	|	|	|	0.87
46.167	0.00	0.12	0.240	o	|	|	|	|	0.87
46.250	0.00	0.12	0.239	o	|	|	|	|	0.87
46.333	0.00	0.11	0.238	o	|	|	|	|	0.86
46.417	0.00	0.11	0.238	o	|	|	|	|	0.86
46.500	0.00	0.11	0.237	o	|	|	|	|	0.86
46.583	0.00	0.11	0.236	o	|	|	|	|	0.85
46.667	0.00	0.11	0.235	o	|	|	|	|	0.85
46.750	0.00	0.11	0.234	o	|	|	|	|	0.85
46.833	0.00	0.11	0.234	o	|	|	|	|	0.85
46.917	0.00	0.11	0.233	o	|	|	|	|	0.84
47.000	0.00	0.11	0.232	o	|	|	|	|	0.84
47.083	0.00	0.11	0.231	o	|	|	|	|	0.84
47.167	0.00	0.11	0.231	o	|	|	|	|	0.84
47.250	0.00	0.11	0.230	o	|	|	|	|	0.83
47.333	0.00	0.11	0.229	o	|	|	|	|	0.83
47.417	0.00	0.11	0.228	o	|	|	|	|	0.83
47.500	0.00	0.11	0.227	o	|	|	|	|	0.82
47.583	0.00	0.11	0.227	o	|	|	|	|	0.82
47.667	0.00	0.11	0.226	o	|	|	|	|	0.82
47.750	0.00	0.11	0.225	o	|	|	|	|	0.82
47.833	0.00	0.11	0.224	o	|	|	|	|	0.81
47.917	0.00	0.11	0.224	o	|	|	|	|	0.81
48.000	0.00	0.11	0.223	o	|	|	|	|	0.81
48.083	0.00	0.11	0.222	o	|	|	|	|	0.81
48.167	0.00	0.11	0.222	o	|	|	|	|	0.80
48.250	0.00	0.11	0.221	o	|	|	|	|	0.80
48.333	0.00	0.11	0.220	o	|	|	|	|	0.80
48.417	0.00	0.11	0.219	o	|	|	|	|	0.79
48.500	0.00	0.11	0.219	o	|	|	|	|	0.79
48.583	0.00	0.10	0.218	o	|	|	|	|	0.79
48.667	0.00	0.10	0.217	o	|	|	|	|	0.79
48.750	0.00	0.10	0.216	o	|	|	|	|	0.78
48.833	0.00	0.10	0.216	o	|	|	|	|	0.78
48.917	0.00	0.10	0.215	o	|	|	|	|	0.78
49.000	0.00	0.10	0.214	o	|	|	|	|	0.78
49.083	0.00	0.10	0.214	o	|	|	|	|	0.77
49.167	0.00	0.10	0.213	o	|	|	|	|	0.77
49.250	0.00	0.10	0.212	o	|	|	|	|	0.77
49.333	0.00	0.10	0.211	o	|	|	|	|	0.77
49.417	0.00	0.10	0.211	o	|	|	|	|	0.76
49.500	0.00	0.10	0.210	o	|	|	|	|	0.76
49.583	0.00	0.10	0.209	o	|	|	|	|	0.76
49.667	0.00	0.10	0.209	o	|	|	|	|	0.76
49.750	0.00	0.10	0.208	o	|	|	|	|	0.75
49.833	0.00	0.10	0.207	o	|	|	|	|	0.75

Remaining water in basin = 0.21 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 598
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.929 (CFS)
Total volume = 1.187 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/07/25

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: PRO565.rte
**********HYDROGRAPH DATA**********
Number of intervals = 76
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 17.368 (CFS)
Total volume = 1.921 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 76
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.276	0.133	0.276	0.276
2.000	0.584	0.193	0.583	0.585
3.000	0.930	0.700	0.928	0.932
3.500	1.118	0.824	1.115	1.121
4.000	1.316	0.930	1.313	1.319
4.500	1.528	1.024	1.524	1.532
4.750	1.637	1.068	1.633	1.641
5.000	1.749	18.283	1.686	1.812
6.000	2.231	253.655	1.358	3.104

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	4.3	8.68	13.03	17.37	Depth (Ft.)
0.083	0.54	0.00	0.002	O	|	|	|	|	0.01
0.167	1.24	0.00	0.008	O I	|	|	|	|	0.03
0.250	1.48	0.01	0.017	O I	|	|	|	|	0.06
0.333	1.56	0.01	0.028	O I	|	|	|	|	0.10
0.417	1.59	0.02	0.038	O I	|	|	|	|	0.14
0.500	1.70	0.02	0.050	O I	|	|	|	|	0.18
0.583	1.82	0.03	0.062	O I	|	|	|	|	0.22
0.667	1.85	0.04	0.074	O I	|	|	|	|	0.27
0.750	1.86	0.04	0.086	O I	|	|	|	|	0.31
0.833	1.86	0.05	0.099	O I	|	|	|	|	0.36
0.917	1.86	0.05	0.111	O I	|	|	|	|	0.40
1.000	1.97	0.06	0.124	O I	|	|	|	|	0.45
1.083	2.09	0.07	0.138	O I	|	|	|	|	0.50
1.167	2.11	0.07	0.152	O I	|	|	|	|	0.55
1.250	2.12	0.08	0.166	O I	|	|	|	|	0.60
1.333	2.13	0.09	0.180	O I	|	|	|	|	0.65
1.417	2.13	0.09	0.194	O I	|	|	|	|	0.70

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1.500    2.13    0.10      0.208  o  I    |        |        |        |     0.75
1.583    2.13    0.11      0.222  o  I    |        |        |        |     0.80
1.667    2.13    0.11      0.236  o  I    |        |        |        |     0.85
1.750    2.13    0.12      0.249  o  I    |        |        |        |     0.90
1.833    2.13    0.13      0.263  o  I    |        |        |        |     0.95
1.917    2.13    0.13      0.277  o  I    |        |        |        |     1.00
2.000    2.23    0.14      0.291  o   I   |        |        |        |     1.05
2.083    2.24    0.14      0.306  o   I   |        |        |        |     1.10
2.167    2.26    0.14      0.320  o   I   |        |        |        |     1.14
2.250    2.36    0.14      0.335  o   I   |        |        |        |     1.19
2.333    2.38    0.15      0.350  o   I   |        |        |        |     1.24
2.417    2.39    0.15      0.366  o   I   |        |        |        |     1.29
2.500    2.39    0.15      0.381  o   I   |        |        |        |     1.34
2.583    2.39    0.16      0.397  o   I   |        |        |        |     1.39
2.667    2.39    0.16      0.412  o   I   |        |        |        |     1.44
2.750    2.50    0.16      0.428  o   I   |        |        |        |     1.49
2.833    2.62    0.17      0.444  o   I   |        |        |        |     1.55
2.917    2.64    0.17      0.461  o   I   |        |        |        |     1.60
3.000    2.65    0.17      0.478  o   I   |        |        |        |     1.66
3.083    2.66    0.18      0.495  o   I   |        |        |        |     1.71
3.167    2.77    0.18      0.513  o    I  |        |        |        |     1.77
3.250    2.88    0.18      0.531  o    I  |        |        |        |     1.83
3.333    2.91    0.19      0.550  o    I  |        |        |        |     1.89
3.417    3.03    0.19      0.569  o    I  |        |        |        |     1.95
3.500    3.26    0.20      0.589  o     I |        |        |        |     2.01
3.583    3.51    0.23      0.611  o     I |        |        |        |     2.08
3.667    3.66    0.27      0.634  o     I |        |        |        |     2.14
3.750    3.81    0.30      0.658  o      I|        |        |        |     2.21
3.833    3.94    0.34      0.682  o      I|        |        |        |     2.28
3.917    4.08    0.37      0.707  o      I|        |        |        |     2.36
4.000    4.21    0.41      0.733  o      I|        |        |        |     2.43
4.083    4.35    0.45      0.760  o       I        |        |        |     2.51
4.167    4.58    0.49      0.787  o       I        |        |        |     2.59
4.250    4.84    0.53      0.816  o       I        |        |        |     2.67
4.333    5.10    0.58      0.846  |o      |I        |        |        |     2.76
4.417    5.36    0.62      0.878  |o      |I        |        |        |     2.85
4.500    5.52    0.67      0.911  |o       I       |        |        |     2.95
4.583    5.67    0.71      0.945  |o       I       |        |        |     3.04
4.667    5.91    0.73      0.980  |o       I       |        |        |     3.13
4.750    6.17    0.76      1.016  |o        I      |        |        |     3.23
4.833    6.32    0.78      1.054  |o        I      |        |        |     3.33
4.917    6.47    0.81      1.093  |o        I      |        |        |     3.43
5.000    6.71    0.83      1.132  |o         I     |        |        |     3.54
5.083    7.40    0.85      1.175  |o          I    |        |        |     3.64
5.167    8.77    0.88      1.225  |o           I   |        |        |     3.77
5.250   10.38    0.91      1.285  |o            | I |        |        |     3.92
5.333   11.97    0.95      1.355  |o            |    I     |        |     4.09
5.417   14.00    0.98      1.438  |o            |       |I     |        |     4.29
5.500   17.37    1.03      1.539  |o            |       |      |      I |     4.53
5.583   13.45    1.16      1.638  | o           |       I      |        |     4.75
5.667    5.99    7.09      1.676  |          I O |      |       |        |     4.84
5.750    3.24    5.37      1.665  |     I  |O    |      |       |        |     4.81
5.833    2.01    3.47      1.653  |  I  O  |     |      |       |        |     4.78
5.917    1.24    2.19      1.644  | I O    |     |      |       |        |     4.77
6.000    0.80    1.38      1.639  |IO      |     |      |       |        |     4.75
6.083    0.39    1.07      1.635  IO       |     |      |       |        |     4.74
6.167    0.10    1.06      1.629  IO       |     |      |       |        |     4.73
6.250    0.03    1.06      1.622  IO       |     |      |       |        |     4.72
6.333    0.01    1.06      1.615  IO       |     |      |       |        |     4.70
6.417    0.00    1.06      1.608  IO       |     |      |       |        |     4.68
6.500    0.00    1.05      1.600  IO       |     |      |       |        |     4.67
6.583    0.00    1.05      1.593  IO       |     |      |       |        |     4.65
6.667    0.00    1.05      1.586  IO       |     |      |       |        |     4.63
6.750    0.00    1.04      1.579  IO       |     |      |       |        |     4.62
6.833    0.00    1.04      1.572  IO       |     |      |       |        |     4.60
6.917    0.00    1.04      1.564  IO       |     |      |       |        |     4.58
7.000    0.00    1.04      1.557  IO       |     |      |       |        |     4.57
7.083    0.00    1.03      1.550  IO       |     |      |       |        |     4.55
7.167    0.00    1.03      1.543  IO       |     |      |       |        |     4.53
7.250    0.00    1.03      1.536  IO       |     |      |       |        |     4.52
7.333    0.00    1.02      1.529  IO       |     |      |       |        |     4.50
7.417    0.00    1.02      1.522  IO       |     |      |       |        |     4.49
7.500    0.00    1.02      1.515  IO       |     |      |       |        |     4.47
7.583    0.00    1.02      1.508  IO       |     |      |       |        |     4.45
7.667    0.00    1.01      1.501  IO       |     |      |       |        |     4.44
7.750    0.00    1.01      1.494  IO       |     |      |       |        |     4.42
7.833    0.00    1.01      1.487  IO       |     |      |       |        |     4.40
7.917    0.00    1.00      1.480  IO       |     |      |       |        |     4.39
8.000    0.00    1.00      1.473  IO       |     |      |       |        |     4.37
8.083    0.00    1.00      1.466  IO       |     |      |       |        |     4.35
8.167    0.00    0.99      1.459  IO       |     |      |       |        |     4.34
8.250    0.00    0.99      1.453  IO       |     |      |       |        |     4.32
8.333    0.00    0.99      1.446  IO       |     |      |       |        |     4.31
8.417    0.00    0.98      1.439  IO       |     |      |       |        |     4.29
8.500    0.00    0.98      1.432  IO       |     |      |       |        |     4.27
8.583    0.00    0.98      1.426  IO       |     |      |       |        |     4.26
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8.667	0.00	0.98	1.419	IO				4.24
8.750	0.00	0.97	1.412	IO				4.23
8.833	0.00	0.97	1.405	IO				4.21
8.917	0.00	0.97	1.399	IO				4.20
9.000	0.00	0.96	1.392	IO				4.18
9.083	0.00	0.96	1.385	IO				4.16
9.167	0.00	0.96	1.379	IO				4.15
9.250	0.00	0.95	1.372	IO				4.13
9.333	0.00	0.95	1.366	IO				4.12
9.417	0.00	0.95	1.359	IO				4.10
9.500	0.00	0.95	1.353	IO				4.09
9.583	0.00	0.94	1.346	IO				4.07
9.667	0.00	0.94	1.340	IO				4.06
9.750	0.00	0.94	1.333	IO				4.04
9.833	0.00	0.93	1.327	IO				4.03
9.917	0.00	0.93	1.320	IO				4.01
10.000	0.00	0.93	1.314	IO				3.99
10.083	0.00	0.93	1.307	IO				3.98
10.167	0.00	0.92	1.301	IO				3.96
10.250	0.00	0.92	1.295	IO				3.95
10.333	0.00	0.92	1.288	IO				3.93
10.417	0.00	0.91	1.282	IO				3.91
10.500	0.00	0.91	1.276	IO				3.90
10.583	0.00	0.91	1.270	IO				3.88
10.667	0.00	0.90	1.263	IO				3.87
10.750	0.00	0.90	1.257	IO				3.85
10.833	0.00	0.90	1.251	IO				3.84
10.917	0.00	0.89	1.245	IO				3.82
11.000	0.00	0.89	1.239	IO				3.80
11.083	0.00	0.89	1.233	IO				3.79
11.167	0.00	0.88	1.227	IO				3.77
11.250	0.00	0.88	1.221	IO				3.76
11.333	0.00	0.88	1.214	IO				3.74
11.417	0.00	0.87	1.208	IO				3.73
11.500	0.00	0.87	1.202	IO				3.71
11.583	0.00	0.87	1.196	IO				3.70
11.667	0.00	0.86	1.191	IO				3.68
11.750	0.00	0.86	1.185	IO				3.67
11.833	0.00	0.86	1.179	IO				3.65
11.917	0.00	0.85	1.173	IO				3.64
12.000	0.00	0.85	1.167	IO				3.62
12.083	0.00	0.85	1.161	IO				3.61
12.167	0.00	0.84	1.155	IO				3.59
12.250	0.00	0.84	1.149	IO				3.58
12.333	0.00	0.84	1.144	IO				3.56
12.417	0.00	0.83	1.138	IO				3.55
12.500	0.00	0.83	1.132	IO				3.54
12.583	0.00	0.83	1.126	IO				3.52
12.667	0.00	0.83	1.121	IO				3.51
12.750	0.00	0.82	1.115	IO				3.49
12.833	0.00	0.82	1.109	IO				3.48
12.917	0.00	0.81	1.104	IO				3.46
13.000	0.00	0.81	1.098	IO				3.45
13.083	0.00	0.81	1.093	IO				3.43
13.167	0.00	0.80	1.087	IO				3.42
13.250	0.00	0.80	1.082	IO				3.40
13.333	0.00	0.80	1.076	IO				3.39
13.417	0.00	0.79	1.071	IO				3.37
13.500	0.00	0.79	1.065	IO				3.36
13.583	0.00	0.79	1.060	IO				3.35
13.667	0.00	0.78	1.054	IO				3.33
13.750	0.00	0.78	1.049	IO				3.32
13.833	0.00	0.77	1.044	IO				3.30
13.917	0.00	0.77	1.038	IO				3.29
14.000	0.00	0.77	1.033	IO				3.27
14.083	0.00	0.76	1.028	IO				3.26
14.167	0.00	0.76	1.022	IO				3.25
14.250	0.00	0.76	1.017	IO				3.23
14.333	0.00	0.75	1.012	IO				3.22
14.417	0.00	0.75	1.007	IO				3.20
14.500	0.00	0.75	1.002	IO				3.19
14.583	0.00	0.74	0.997	IO				3.18
14.667	0.00	0.74	0.991	IO				3.16
14.750	0.00	0.74	0.986	IO				3.15
14.833	0.00	0.73	0.981	IO				3.14
14.917	0.00	0.73	0.976	IO				3.12
15.000	0.00	0.73	0.971	IO				3.11
15.083	0.00	0.72	0.966	IO				3.10
15.167	0.00	0.72	0.961	IO				3.08
15.250	0.00	0.72	0.956	IO				3.07
15.333	0.00	0.71	0.951	IO				3.06
15.417	0.00	0.71	0.946	IO				3.04
15.500	0.00	0.71	0.942	IO				3.03
15.583	0.00	0.70	0.937	IO				3.02
15.667	0.00	0.70	0.932	IO				3.01
15.750	0.00	0.70	0.927	IO				2.99

15.833	0.00	0.69	0.922	IO					2.98
15.917	0.00	0.68	0.918	IO					2.96
16.000	0.00	0.67	0.913	IO					2.95
16.083	0.00	0.67	0.908	IO					2.94
16.167	0.00	0.66	0.904	IO					2.92
16.250	0.00	0.65	0.899	IO					2.91
16.333	0.00	0.65	0.895	IO					2.90
16.417	0.00	0.64	0.890	IO					2.89
16.500	0.00	0.64	0.886	IO					2.87
16.583	0.00	0.63	0.881	IO					2.86
16.667	0.00	0.62	0.877	IO					2.85
16.750	0.00	0.62	0.873	IO					2.84
16.833	0.00	0.61	0.869	IO					2.82
16.917	0.00	0.60	0.865	IO					2.81
17.000	0.00	0.60	0.860	IO					2.80
17.083	0.00	0.59	0.856	IO					2.79
17.167	0.00	0.59	0.852	IO					2.78
17.250	0.00	0.58	0.848	IO					2.76
17.333	0.00	0.57	0.844	IO					2.75
17.417	0.00	0.57	0.840	IO					2.74
17.500	0.00	0.56	0.836	IO					2.73
17.583	0.00	0.56	0.833	IO					2.72
17.667	0.00	0.55	0.829	IO					2.71
17.750	0.00	0.55	0.825	IO					2.70
17.833	0.00	0.54	0.821	O					2.69
17.917	0.00	0.54	0.817	O					2.67
18.000	0.00	0.53	0.814	O					2.66
18.083	0.00	0.52	0.810	O					2.65
18.167	0.00	0.52	0.807	O					2.64
18.250	0.00	0.51	0.803	O					2.63
18.333	0.00	0.51	0.800	O					2.62
18.417	0.00	0.50	0.796	O					2.61
18.500	0.00	0.50	0.793	O					2.60
18.583	0.00	0.49	0.789	O					2.59
18.667	0.00	0.49	0.786	O					2.58
18.750	0.00	0.48	0.782	O					2.57
18.833	0.00	0.48	0.779	O					2.56
18.917	0.00	0.47	0.776	O					2.55
19.000	0.00	0.47	0.773	O					2.55
19.083	0.00	0.46	0.769	O					2.54
19.167	0.00	0.46	0.766	O					2.53
19.250	0.00	0.46	0.763	O					2.52
19.333	0.00	0.45	0.760	O					2.51
19.417	0.00	0.45	0.757	O					2.50
19.500	0.00	0.44	0.754	O					2.49
19.583	0.00	0.44	0.751	O					2.48
19.667	0.00	0.43	0.748	O					2.47
19.750	0.00	0.43	0.745	O					2.46
19.833	0.00	0.42	0.742	O					2.46
19.917	0.00	0.42	0.739	O					2.45
20.000	0.00	0.42	0.736	O					2.44
20.083	0.00	0.41	0.733	O					2.43
20.167	0.00	0.41	0.730	O					2.42
20.250	0.00	0.40	0.728	O					2.42
20.333	0.00	0.40	0.725	O					2.41
20.417	0.00	0.40	0.722	O					2.40
20.500	0.00	0.39	0.719	O					2.39
20.583	0.00	0.39	0.717	O					2.38
20.667	0.00	0.38	0.714	O					2.38
20.750	0.00	0.38	0.711	O					2.37
20.833	0.00	0.38	0.709	O					2.36
20.917	0.00	0.37	0.706	O					2.35
21.000	0.00	0.37	0.704	O					2.35
21.083	0.00	0.36	0.701	O					2.34
21.167	0.00	0.36	0.699	O					2.33
21.250	0.00	0.36	0.696	O					2.32
21.333	0.00	0.35	0.694	O					2.32
21.417	0.00	0.35	0.691	O					2.31
21.500	0.00	0.35	0.689	O					2.30
21.583	0.00	0.34	0.687	O					2.30
21.667	0.00	0.34	0.684	O					2.29
21.750	0.00	0.34	0.682	O					2.28
21.833	0.00	0.33	0.680	O					2.28
21.917	0.00	0.33	0.677	O					2.27
22.000	0.00	0.33	0.675	O					2.26
22.083	0.00	0.32	0.673	O					2.26
22.167	0.00	0.32	0.671	O					2.25
22.250	0.00	0.32	0.668	O					2.24
22.333	0.00	0.31	0.666	O					2.24
22.417	0.00	0.31	0.664	O					2.23
22.500	0.00	0.31	0.662	O					2.23
22.583	0.00	0.30	0.660	O					2.22
22.667	0.00	0.30	0.658	O					2.21
22.750	0.00	0.30	0.656	O					2.21
22.833	0.00	0.30	0.654	O					2.20
22.917	0.00	0.29	0.652	O					2.20

23.000	0.00	0.29	0.650	o	|	|	|	|	2.19
23.083	0.00	0.29	0.648	o	|	|	|	|	2.18
23.167	0.00	0.28	0.646	o	|	|	|	|	2.18
23.250	0.00	0.28	0.644	o	|	|	|	|	2.17
23.333	0.00	0.28	0.642	o	|	|	|	|	2.17
23.417	0.00	0.27	0.640	o	|	|	|	|	2.16
23.500	0.00	0.27	0.638	o	|	|	|	|	2.16
23.583	0.00	0.27	0.636	o	|	|	|	|	2.15
23.667	0.00	0.27	0.634	o	|	|	|	|	2.15
23.750	0.00	0.26	0.632	o	|	|	|	|	2.14
23.833	0.00	0.26	0.631	o	|	|	|	|	2.13
23.917	0.00	0.26	0.629	o	|	|	|	|	2.13
24.000	0.00	0.26	0.627	o	|	|	|	|	2.12
24.083	0.00	0.25	0.625	o	|	|	|	|	2.12
24.167	0.00	0.25	0.624	o	|	|	|	|	2.11
24.250	0.00	0.25	0.622	o	|	|	|	|	2.11
24.333	0.00	0.25	0.620	o	|	|	|	|	2.10
24.417	0.00	0.24	0.619	o	|	|	|	|	2.10
24.500	0.00	0.24	0.617	o	|	|	|	|	2.09
24.583	0.00	0.24	0.615	o	|	|	|	|	2.09
24.667	0.00	0.24	0.614	o	|	|	|	|	2.09
24.750	0.00	0.23	0.612	o	|	|	|	|	2.08
24.833	0.00	0.23	0.610	o	|	|	|	|	2.08
24.917	0.00	0.23	0.609	o	|	|	|	|	2.07
25.000	0.00	0.23	0.607	o	|	|	|	|	2.07
25.083	0.00	0.22	0.606	o	|	|	|	|	2.06
25.167	0.00	0.22	0.604	o	|	|	|	|	2.06
25.250	0.00	0.22	0.603	o	|	|	|	|	2.05
25.333	0.00	0.22	0.601	o	|	|	|	|	2.05
25.417	0.00	0.22	0.600	o	|	|	|	|	2.04
25.500	0.00	0.21	0.598	o	|	|	|	|	2.04
25.583	0.00	0.21	0.597	o	|	|	|	|	2.04
25.667	0.00	0.21	0.595	o	|	|	|	|	2.03
25.750	0.00	0.21	0.594	o	|	|	|	|	2.03
25.833	0.00	0.21	0.592	o	|	|	|	|	2.02
25.917	0.00	0.20	0.591	o	|	|	|	|	2.02
26.000	0.00	0.20	0.590	o	|	|	|	|	2.02
26.083	0.00	0.20	0.588	o	|	|	|	|	2.01
26.167	0.00	0.20	0.587	o	|	|	|	|	2.01
26.250	0.00	0.20	0.585	o	|	|	|	|	2.00
26.333	0.00	0.19	0.584	o	|	|	|	|	2.00
26.417	0.00	0.19	0.583	o	|	|	|	|	2.00
26.500	0.00	0.19	0.581	o	|	|	|	|	1.99
26.583	0.00	0.19	0.580	o	|	|	|	|	1.99
26.667	0.00	0.19	0.579	o	|	|	|	|	1.98
26.750	0.00	0.19	0.577	o	|	|	|	|	1.98
26.833	0.00	0.19	0.576	o	|	|	|	|	1.97
26.917	0.00	0.19	0.575	o	|	|	|	|	1.97
27.000	0.00	0.19	0.573	o	|	|	|	|	1.97
27.083	0.00	0.19	0.572	o	|	|	|	|	1.96
27.167	0.00	0.19	0.571	o	|	|	|	|	1.96
27.250	0.00	0.19	0.570	o	|	|	|	|	1.95
27.333	0.00	0.19	0.568	o	|	|	|	|	1.95
27.417	0.00	0.19	0.567	o	|	|	|	|	1.94
27.500	0.00	0.19	0.566	o	|	|	|	|	1.94
27.583	0.00	0.19	0.564	o	|	|	|	|	1.94
27.667	0.00	0.19	0.563	o	|	|	|	|	1.93
27.750	0.00	0.19	0.562	o	|	|	|	|	1.93
27.833	0.00	0.19	0.560	o	|	|	|	|	1.92
27.917	0.00	0.19	0.559	o	|	|	|	|	1.92
28.000	0.00	0.19	0.558	o	|	|	|	|	1.92
28.083	0.00	0.19	0.557	o	|	|	|	|	1.91
28.167	0.00	0.19	0.555	o	|	|	|	|	1.91
28.250	0.00	0.19	0.554	o	|	|	|	|	1.90
28.333	0.00	0.19	0.553	o	|	|	|	|	1.90
28.417	0.00	0.19	0.551	o	|	|	|	|	1.89
28.500	0.00	0.19	0.550	o	|	|	|	|	1.89
28.583	0.00	0.19	0.549	o	|	|	|	|	1.89
28.667	0.00	0.19	0.548	o	|	|	|	|	1.88
28.750	0.00	0.19	0.546	o	|	|	|	|	1.88
28.833	0.00	0.19	0.545	o	|	|	|	|	1.87
28.917	0.00	0.19	0.544	o	|	|	|	|	1.87
29.000	0.00	0.18	0.542	o	|	|	|	|	1.87
29.083	0.00	0.18	0.541	o	|	|	|	|	1.86
29.167	0.00	0.18	0.540	o	|	|	|	|	1.86
29.250	0.00	0.18	0.539	o	|	|	|	|	1.85
29.333	0.00	0.18	0.537	o	|	|	|	|	1.85
29.417	0.00	0.18	0.536	o	|	|	|	|	1.84
29.500	0.00	0.18	0.535	o	|	|	|	|	1.84
29.583	0.00	0.18	0.534	o	|	|	|	|	1.84
29.667	0.00	0.18	0.532	o	|	|	|	|	1.83
29.750	0.00	0.18	0.531	o	|	|	|	|	1.83
29.833	0.00	0.18	0.530	o	|	|	|	|	1.82
29.917	0.00	0.18	0.529	o	|	|	|	|	1.82
30.000	0.00	0.18	0.527	o	|	|	|	|	1.82
30.083	0.00	0.18	0.526	o	|	|	|	|	1.81

30.167	0.00	0.18	0.525	o	|	|	|	|	1.81
30.250	0.00	0.18	0.524	o	|	|	|	|	1.80
30.333	0.00	0.18	0.522	o	|	|	|	|	1.80
30.417	0.00	0.18	0.521	o	|	|	|	|	1.80
30.500	0.00	0.18	0.520	o	|	|	|	|	1.79
30.583	0.00	0.18	0.519	o	|	|	|	|	1.79
30.667	0.00	0.18	0.517	o	|	|	|	|	1.78
30.750	0.00	0.18	0.516	o	|	|	|	|	1.78
30.833	0.00	0.18	0.515	o	|	|	|	|	1.78
30.917	0.00	0.18	0.514	o	|	|	|	|	1.77
31.000	0.00	0.18	0.512	o	|	|	|	|	1.77
31.083	0.00	0.18	0.511	o	|	|	|	|	1.76
31.167	0.00	0.18	0.510	o	|	|	|	|	1.76
31.250	0.00	0.18	0.509	o	|	|	|	|	1.76
31.333	0.00	0.18	0.507	o	|	|	|	|	1.75
31.417	0.00	0.18	0.506	o	|	|	|	|	1.75
31.500	0.00	0.18	0.505	o	|	|	|	|	1.74
31.583	0.00	0.18	0.504	o	|	|	|	|	1.74
31.667	0.00	0.18	0.503	o	|	|	|	|	1.74
31.750	0.00	0.18	0.501	o	|	|	|	|	1.73
31.833	0.00	0.18	0.500	o	|	|	|	|	1.73
31.917	0.00	0.18	0.499	o	|	|	|	|	1.72
32.000	0.00	0.18	0.498	o	|	|	|	|	1.72
32.083	0.00	0.18	0.496	o	|	|	|	|	1.72
32.167	0.00	0.18	0.495	o	|	|	|	|	1.71
32.250	0.00	0.18	0.494	o	|	|	|	|	1.71
32.333	0.00	0.18	0.493	o	|	|	|	|	1.70
32.417	0.00	0.18	0.492	o	|	|	|	|	1.70
32.500	0.00	0.17	0.490	o	|	|	|	|	1.70
32.583	0.00	0.17	0.489	o	|	|	|	|	1.69
32.667	0.00	0.17	0.488	o	|	|	|	|	1.69
32.750	0.00	0.17	0.487	o	|	|	|	|	1.68
32.833	0.00	0.17	0.486	o	|	|	|	|	1.68
32.917	0.00	0.17	0.484	o	|	|	|	|	1.68
33.000	0.00	0.17	0.483	o	|	|	|	|	1.67
33.083	0.00	0.17	0.482	o	|	|	|	|	1.67
33.167	0.00	0.17	0.481	o	|	|	|	|	1.67
33.250	0.00	0.17	0.480	o	|	|	|	|	1.66
33.333	0.00	0.17	0.478	o	|	|	|	|	1.66
33.417	0.00	0.17	0.477	o	|	|	|	|	1.65
33.500	0.00	0.17	0.476	o	|	|	|	|	1.65
33.583	0.00	0.17	0.475	o	|	|	|	|	1.65
33.667	0.00	0.17	0.474	o	|	|	|	|	1.64
33.750	0.00	0.17	0.473	o	|	|	|	|	1.64
33.833	0.00	0.17	0.471	o	|	|	|	|	1.63
33.917	0.00	0.17	0.470	o	|	|	|	|	1.63
34.000	0.00	0.17	0.469	o	|	|	|	|	1.63
34.083	0.00	0.17	0.468	o	|	|	|	|	1.62
34.167	0.00	0.17	0.467	o	|	|	|	|	1.62
34.250	0.00	0.17	0.466	o	|	|	|	|	1.62
34.333	0.00	0.17	0.464	o	|	|	|	|	1.61
34.417	0.00	0.17	0.463	o	|	|	|	|	1.61
34.500	0.00	0.17	0.462	o	|	|	|	|	1.60
34.583	0.00	0.17	0.461	o	|	|	|	|	1.60
34.667	0.00	0.17	0.460	o	|	|	|	|	1.60
34.750	0.00	0.17	0.459	o	|	|	|	|	1.59
34.833	0.00	0.17	0.457	o	|	|	|	|	1.59
34.917	0.00	0.17	0.456	o	|	|	|	|	1.59
35.000	0.00	0.17	0.455	o	|	|	|	|	1.58
35.083	0.00	0.17	0.454	o	|	|	|	|	1.58
35.167	0.00	0.17	0.453	o	|	|	|	|	1.57
35.250	0.00	0.17	0.452	o	|	|	|	|	1.57
35.333	0.00	0.17	0.450	o	|	|	|	|	1.57
35.417	0.00	0.17	0.449	o	|	|	|	|	1.56
35.500	0.00	0.17	0.448	o	|	|	|	|	1.56
35.583	0.00	0.17	0.447	o	|	|	|	|	1.56
35.667	0.00	0.17	0.446	o	|	|	|	|	1.55
35.750	0.00	0.17	0.445	o	|	|	|	|	1.55
35.833	0.00	0.17	0.444	o	|	|	|	|	1.54
35.917	0.00	0.17	0.442	o	|	|	|	|	1.54
36.000	0.00	0.17	0.441	o	|	|	|	|	1.54
36.083	0.00	0.16	0.440	o	|	|	|	|	1.53
36.167	0.00	0.16	0.439	o	|	|	|	|	1.53
36.250	0.00	0.16	0.438	o	|	|	|	|	1.53
36.333	0.00	0.16	0.437	o	|	|	|	|	1.52
36.417	0.00	0.16	0.436	o	|	|	|	|	1.52
36.500	0.00	0.16	0.434	o	|	|	|	|	1.51
36.583	0.00	0.16	0.433	o	|	|	|	|	1.51
36.667	0.00	0.16	0.432	o	|	|	|	|	1.51
36.750	0.00	0.16	0.431	o	|	|	|	|	1.50
36.833	0.00	0.16	0.430	o	|	|	|	|	1.50
36.917	0.00	0.16	0.429	o	|	|	|	|	1.50
37.000	0.00	0.16	0.428	o	|	|	|	|	1.49
37.083	0.00	0.16	0.427	o	|	|	|	|	1.49
37.167	0.00	0.16	0.425	o	|	|	|	|	1.49
37.250	0.00	0.16	0.424	o	|	|	|	|	1.48

37.333	0.00	0.16	0.423	o	|	|	|	|	1.48
37.417	0.00	0.16	0.422	o	|	|	|	|	1.47
37.500	0.00	0.16	0.421	o	|	|	|	|	1.47
37.583	0.00	0.16	0.420	o	|	|	|	|	1.47
37.667	0.00	0.16	0.419	o	|	|	|	|	1.46
37.750	0.00	0.16	0.418	o	|	|	|	|	1.46
37.833	0.00	0.16	0.417	o	|	|	|	|	1.46
37.917	0.00	0.16	0.416	o	|	|	|	|	1.45
38.000	0.00	0.16	0.414	o	|	|	|	|	1.45
38.083	0.00	0.16	0.413	o	|	|	|	|	1.45
38.167	0.00	0.16	0.412	o	|	|	|	|	1.44
38.250	0.00	0.16	0.411	o	|	|	|	|	1.44
38.333	0.00	0.16	0.410	o	|	|	|	|	1.44
38.417	0.00	0.16	0.409	o	|	|	|	|	1.43
38.500	0.00	0.16	0.408	o	|	|	|	|	1.43
38.583	0.00	0.16	0.407	o	|	|	|	|	1.42
38.667	0.00	0.16	0.406	o	|	|	|	|	1.42
38.750	0.00	0.16	0.405	o	|	|	|	|	1.42
38.833	0.00	0.16	0.403	o	|	|	|	|	1.41
38.917	0.00	0.16	0.402	o	|	|	|	|	1.41
39.000	0.00	0.16	0.401	o	|	|	|	|	1.41
39.083	0.00	0.16	0.400	o	|	|	|	|	1.40
39.167	0.00	0.16	0.399	o	|	|	|	|	1.40
39.250	0.00	0.16	0.398	o	|	|	|	|	1.40
39.333	0.00	0.16	0.397	o	|	|	|	|	1.39
39.417	0.00	0.16	0.396	o	|	|	|	|	1.39
39.500	0.00	0.16	0.395	o	|	|	|	|	1.39
39.583	0.00	0.16	0.394	o	|	|	|	|	1.38
39.667	0.00	0.16	0.393	o	|	|	|	|	1.38
39.750	0.00	0.16	0.392	o	|	|	|	|	1.38
39.833	0.00	0.16	0.391	o	|	|	|	|	1.37
39.917	0.00	0.16	0.389	o	|	|	|	|	1.37
40.000	0.00	0.15	0.388	o	|	|	|	|	1.36
40.083	0.00	0.15	0.387	o	|	|	|	|	1.36
40.167	0.00	0.15	0.386	o	|	|	|	|	1.36
40.250	0.00	0.15	0.385	o	|	|	|	|	1.35
40.333	0.00	0.15	0.384	o	|	|	|	|	1.35
40.417	0.00	0.15	0.383	o	|	|	|	|	1.35
40.500	0.00	0.15	0.382	o	|	|	|	|	1.34
40.583	0.00	0.15	0.381	o	|	|	|	|	1.34
40.667	0.00	0.15	0.380	o	|	|	|	|	1.34
40.750	0.00	0.15	0.379	o	|	|	|	|	1.33
40.833	0.00	0.15	0.378	o	|	|	|	|	1.33
40.917	0.00	0.15	0.377	o	|	|	|	|	1.33
41.000	0.00	0.15	0.376	o	|	|	|	|	1.32
41.083	0.00	0.15	0.375	o	|	|	|	|	1.32
41.167	0.00	0.15	0.374	o	|	|	|	|	1.32
41.250	0.00	0.15	0.373	o	|	|	|	|	1.31
41.333	0.00	0.15	0.372	o	|	|	|	|	1.31
41.417	0.00	0.15	0.370	o	|	|	|	|	1.31
41.500	0.00	0.15	0.369	o	|	|	|	|	1.30
41.583	0.00	0.15	0.368	o	|	|	|	|	1.30
41.667	0.00	0.15	0.367	o	|	|	|	|	1.30
41.750	0.00	0.15	0.366	o	|	|	|	|	1.29
41.833	0.00	0.15	0.365	o	|	|	|	|	1.29
41.917	0.00	0.15	0.364	o	|	|	|	|	1.29
42.000	0.00	0.15	0.363	o	|	|	|	|	1.28
42.083	0.00	0.15	0.362	o	|	|	|	|	1.28
42.167	0.00	0.15	0.361	o	|	|	|	|	1.28
42.250	0.00	0.15	0.360	o	|	|	|	|	1.27
42.333	0.00	0.15	0.359	o	|	|	|	|	1.27
42.417	0.00	0.15	0.358	o	|	|	|	|	1.27
42.500	0.00	0.15	0.357	o	|	|	|	|	1.26
42.583	0.00	0.15	0.356	o	|	|	|	|	1.26
42.667	0.00	0.15	0.355	o	|	|	|	|	1.26
42.750	0.00	0.15	0.354	o	|	|	|	|	1.25
42.833	0.00	0.15	0.353	o	|	|	|	|	1.25
42.917	0.00	0.15	0.352	o	|	|	|	|	1.25
43.000	0.00	0.15	0.351	o	|	|	|	|	1.24
43.083	0.00	0.15	0.350	o	|	|	|	|	1.24
43.167	0.00	0.15	0.349	o	|	|	|	|	1.24
43.250	0.00	0.15	0.348	o	|	|	|	|	1.23
43.333	0.00	0.15	0.347	o	|	|	|	|	1.23
43.417	0.00	0.15	0.346	o	|	|	|	|	1.23
43.500	0.00	0.15	0.345	o	|	|	|	|	1.22
43.583	0.00	0.15	0.344	o	|	|	|	|	1.22
43.667	0.00	0.15	0.343	o	|	|	|	|	1.22
43.750	0.00	0.15	0.342	o	|	|	|	|	1.21
43.833	0.00	0.15	0.341	o	|	|	|	|	1.21
43.917	0.00	0.15	0.340	o	|	|	|	|	1.21
44.000	0.00	0.15	0.339	o	|	|	|	|	1.20
44.083	0.00	0.15	0.338	o	|	|	|	|	1.20
44.167	0.00	0.14	0.337	o	|	|	|	|	1.20
44.250	0.00	0.14	0.336	o	|	|	|	|	1.19
44.333	0.00	0.14	0.335	o	|	|	|	|	1.19
44.417	0.00	0.14	0.334	o	|	|	|	|	1.19

44.500	0.00	0.14	0.333	o	|	|	|	1.18
44.583	0.00	0.14	0.332	o	|	|	|	1.18
44.667	0.00	0.14	0.331	o	|	|	|	1.18
44.750	0.00	0.14	0.330	o	|	|	|	1.17
44.833	0.00	0.14	0.329	o	|	|	|	1.17
44.917	0.00	0.14	0.328	o	|	|	|	1.17
45.000	0.00	0.14	0.327	o	|	|	|	1.17
45.083	0.00	0.14	0.326	o	|	|	|	1.16
45.167	0.00	0.14	0.325	o	|	|	|	1.16
45.250	0.00	0.14	0.324	o	|	|	|	1.16
45.333	0.00	0.14	0.323	o	|	|	|	1.15
45.417	0.00	0.14	0.322	o	|	|	|	1.15
45.500	0.00	0.14	0.321	o	|	|	|	1.15
45.583	0.00	0.14	0.320	o	|	|	|	1.14
45.667	0.00	0.14	0.319	o	|	|	|	1.14
45.750	0.00	0.14	0.318	o	|	|	|	1.14
45.833	0.00	0.14	0.317	o	|	|	|	1.13
45.917	0.00	0.14	0.316	o	|	|	|	1.13
46.000	0.00	0.14	0.315	o	|	|	|	1.13
46.083	0.00	0.14	0.314	o	|	|	|	1.12
46.167	0.00	0.14	0.313	o	|	|	|	1.12
46.250	0.00	0.14	0.312	o	|	|	|	1.12
46.333	0.00	0.14	0.311	o	|	|	|	1.11
46.417	0.00	0.14	0.310	o	|	|	|	1.11
46.500	0.00	0.14	0.309	o	|	|	|	1.11
46.583	0.00	0.14	0.308	o	|	|	|	1.11
46.667	0.00	0.14	0.307	o	|	|	|	1.10
46.750	0.00	0.14	0.307	o	|	|	|	1.10
46.833	0.00	0.14	0.306	o	|	|	|	1.10
46.917	0.00	0.14	0.305	o	|	|	|	1.09
47.000	0.00	0.14	0.304	o	|	|	|	1.09
47.083	0.00	0.14	0.303	o	|	|	|	1.09
47.167	0.00	0.14	0.302	o	|	|	|	1.08
47.250	0.00	0.14	0.301	o	|	|	|	1.08
47.333	0.00	0.14	0.300	o	|	|	|	1.08
47.417	0.00	0.14	0.299	o	|	|	|	1.07
47.500	0.00	0.14	0.298	o	|	|	|	1.07
47.583	0.00	0.14	0.297	o	|	|	|	1.07
47.667	0.00	0.14	0.296	o	|	|	|	1.07
47.750	0.00	0.14	0.295	o	|	|	|	1.06
47.833	0.00	0.14	0.294	o	|	|	|	1.06
47.917	0.00	0.14	0.293	o	|	|	|	1.06
48.000	0.00	0.14	0.292	o	|	|	|	1.05
48.083	0.00	0.14	0.291	o	|	|	|	1.05
48.167	0.00	0.14	0.290	o	|	|	|	1.05
48.250	0.00	0.14	0.289	o	|	|	|	1.04
48.333	0.00	0.14	0.289	o	|	|	|	1.04
48.417	0.00	0.14	0.288	o	|	|	|	1.04
48.500	0.00	0.14	0.287	o	|	|	|	1.03
48.583	0.00	0.13	0.286	o	|	|	|	1.03
48.667	0.00	0.13	0.285	o	|	|	|	1.03
48.750	0.00	0.13	0.284	o	|	|	|	1.03
48.833	0.00	0.13	0.283	o	|	|	|	1.02
48.917	0.00	0.13	0.282	o	|	|	|	1.02
49.000	0.00	0.13	0.281	o	|	|	|	1.02
49.083	0.00	0.13	0.280	o	|	|	|	1.01
49.167	0.00	0.13	0.279	o	|	|	|	1.01
49.250	0.00	0.13	0.278	o	|	|	|	1.01
49.333	0.00	0.13	0.277	o	|	|	|	1.00
49.417	0.00	0.13	0.277	o	|	|	|	1.00
49.500	0.00	0.13	0.276	o	|	|	|	1.00
49.583	0.00	0.13	0.275	o	|	|	|	1.00
49.667	0.00	0.13	0.274	o	|	|	|	0.99
49.750	0.00	0.13	0.273	o	|	|	|	0.99
49.833	0.00	0.13	0.272	o	|	|	|	0.99
49.917	0.00	0.13	0.271	o	|	|	|	0.98
50.000	0.00	0.13	0.270	o	|	|	|	0.98
50.083	0.00	0.13	0.269	o	|	|	|	0.98
50.167	0.00	0.13	0.268	o	|	|	|	0.97
50.250	0.00	0.13	0.268	o	|	|	|	0.97
50.333	0.00	0.13	0.267	o	|	|	|	0.97
50.417	0.00	0.13	0.266	o	|	|	|	0.96
50.500	0.00	0.13	0.265	o	|	|	|	0.96
50.583	0.00	0.13	0.264	o	|	|	|	0.96
50.667	0.00	0.13	0.263	o	|	|	|	0.95
50.750	0.00	0.13	0.262	o	|	|	|	0.95
50.833	0.00	0.13	0.261	o	|	|	|	0.95
50.917	0.00	0.13	0.261	o	|	|	|	0.94
51.000	0.00	0.13	0.260	o	|	|	|	0.94
51.083	0.00	0.12	0.259	o	|	|	|	0.94
51.167	0.00	0.12	0.258	o	|	|	|	0.93
51.250	0.00	0.12	0.257	o	|	|	|	0.93
51.333	0.00	0.12	0.256	o	|	|	|	0.93
51.417	0.00	0.12	0.255	o	|	|	|	0.93
51.500	0.00	0.12	0.255	o	|	|	|	0.92
51.583	0.00	0.12	0.254	o	|	|	|	0.92

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51.667    0.00    0.12      0.253  o       |       |       |       |      0.92
51.750    0.00    0.12      0.252  o       |       |       |       |      0.91
51.833    0.00    0.12      0.251  o       |       |       |       |      0.91
51.917    0.00    0.12      0.250  o       |       |       |       |      0.91
52.000    0.00    0.12      0.250  o       |       |       |       |      0.90
52.083    0.00    0.12      0.249  o       |       |       |       |      0.90
52.167    0.00    0.12      0.248  o       |       |       |       |      0.90
52.250    0.00    0.12      0.247  o       |       |       |       |      0.90
52.333    0.00    0.12      0.246  o       |       |       |       |      0.89
52.417    0.00    0.12      0.245  o       |       |       |       |      0.89
52.500    0.00    0.12      0.245  o       |       |       |       |      0.89
52.583    0.00    0.12      0.244  o       |       |       |       |      0.88
52.667    0.00    0.12      0.243  o       |       |       |       |      0.88
52.750    0.00    0.12      0.242  o       |       |       |       |      0.88
52.833    0.00    0.12      0.241  o       |       |       |       |      0.87
52.917    0.00    0.12      0.241  o       |       |       |       |      0.87
53.000    0.00    0.12      0.240  o       |       |       |       |      0.87
53.083    0.00    0.12      0.239  o       |       |       |       |      0.87
53.167    0.00    0.11      0.238  o       |       |       |       |      0.86
53.250    0.00    0.11      0.237  o       |       |       |       |      0.86
53.333    0.00    0.11      0.237  o       |       |       |       |      0.86
53.417    0.00    0.11      0.236  o       |       |       |       |      0.85
53.500    0.00    0.11      0.235  o       |       |       |       |      0.85
53.583    0.00    0.11      0.234  o       |       |       |       |      0.85
53.667    0.00    0.11      0.233  o       |       |       |       |      0.85
53.750    0.00    0.11      0.233  o       |       |       |       |      0.84
53.833    0.00    0.11      0.232  o       |       |       |       |      0.84
53.917    0.00    0.11      0.231  o       |       |       |       |      0.84
54.000    0.00    0.11      0.230  o       |       |       |       |      0.83
54.083    0.00    0.11      0.230  o       |       |       |       |      0.83
54.167    0.00    0.11      0.229  o       |       |       |       |      0.83
54.250    0.00    0.11      0.228  o       |       |       |       |      0.83
54.333    0.00    0.11      0.227  o       |       |       |       |      0.82
54.417    0.00    0.11      0.227  o       |       |       |       |      0.82
54.500    0.00    0.11      0.226  o       |       |       |       |      0.82
54.583    0.00    0.11      0.225  o       |       |       |       |      0.82
54.667    0.00    0.11      0.224  o       |       |       |       |      0.81
54.750    0.00    0.11      0.224  o       |       |       |       |      0.81
54.833    0.00    0.11      0.223  o       |       |       |       |      0.81
54.917    0.00    0.11      0.222  o       |       |       |       |      0.80
55.000    0.00    0.11      0.221  o       |       |       |       |      0.80
55.083    0.00    0.11      0.221  o       |       |       |       |      0.80
55.167    0.00    0.11      0.220  o       |       |       |       |      0.80
55.250    0.00    0.11      0.219  o       |       |       |       |      0.79
55.333    0.00    0.11      0.218  o       |       |       |       |      0.79
55.417    0.00    0.10      0.218  o       |       |       |       |      0.79
55.500    0.00    0.10      0.217  o       |       |       |       |      0.79
55.583    0.00    0.10      0.216  o       |       |       |       |      0.78
55.667    0.00    0.10      0.216  o       |       |       |       |      0.78
55.750    0.00    0.10      0.215  o       |       |       |       |      0.78
55.833    0.00    0.10      0.214  o       |       |       |       |      0.78
55.917    0.00    0.10      0.213  o       |       |       |       |      0.77
56.000    0.00    0.10      0.213  o       |       |       |       |      0.77
56.083    0.00    0.10      0.212  o       |       |       |       |      0.77
56.167    0.00    0.10      0.211  o       |       |       |       |      0.77
56.250    0.00    0.10      0.211  o       |       |       |       |      0.76
56.333    0.00    0.10      0.210  o       |       |       |       |      0.76
56.417    0.00    0.10      0.209  o       |       |       |       |      0.76
56.500    0.00    0.10      0.209  o       |       |       |       |      0.76
56.583    0.00    0.10      0.208  o       |       |       |       |      0.75
56.667    0.00    0.10      0.207  o       |       |       |       |      0.75
      Remaining water in basin =    0.21 (Ac.Ft)
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =   680
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =        7.086 (CFS)
                  Total volume =       1.714 (Ac.Ft)
            Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
      ******************************************************************************

      ------------------------------------------------------------------
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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 05/07/25

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: PRO5245.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =   292
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       4.970 (CFS)
               Total volume =       3.020 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
________________________________________________________________________

User entry of depth-outflow-storage data
------------------------------------------------------------------------
Total number of inflow hydrograph intervals = 292
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
------------------------------------------------------------------------
------------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
------------------------------------------------------------------------
------------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
------------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.276      0.133      0.276        0.276
   2.000      0.584      0.193      0.583        0.585
   3.000      0.930      0.700      0.928        0.932
   3.500      1.118      0.824      1.115        1.121
   4.000      1.316      0.930      1.313        1.319
   4.500      1.528      1.024      1.524        1.532
   4.750      1.637      1.068      1.633        1.641
   5.000      1.749     18.283      1.686        1.812
   6.000      2.231    253.655      1.358        3.104
------------------------------------------------------------------------
               Hydrograph Detention Basin Routing
------------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
------------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                  Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0       1.2    2.48    3.73    4.97 (Ft.)
 0.083    0.12    0.00      0.000  O       |       |       |       |     0.00
 0.167    0.25    0.00      0.002  OI      |       |       |       |     0.01
 0.250    0.28    0.00      0.003  OI      |       |       |       |     0.01
 0.333    0.35    0.00      0.006  O I     |       |       |       |     0.02
 0.417    0.42    0.00      0.008  O I     |       |       |       |     0.03
 0.500    0.43    0.01      0.011  O I     |       |       |       |     0.04
 0.583    0.44    0.01      0.014  O I     |       |       |       |     0.05
 0.667    0.44    0.01      0.017  O I     |       |       |       |     0.06
 0.750    0.44    0.01      0.020  O I     |       |       |       |     0.07
 0.833    0.50    0.01      0.023  O  I    |       |       |       |     0.08
 0.917    0.56    0.01      0.027  O  I    |       |       |       |     0.10
 1.000    0.58    0.01      0.031  O  I    |       |       |       |     0.11
 1.083    0.52    0.02      0.034  O  I    |       |       |       |     0.12
 1.167    0.46    0.02      0.037  O I     |       |       |       |     0.14
 1.250    0.45    0.02      0.040  O I     |       |       |       |     0.15
 1.333    0.44    0.02      0.043  O I     |       |       |       |     0.16
 1.417    0.44    0.02      0.046  O I     |       |       |       |     0.17
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1.500    0.44    0.02      0.049  o I     |       |       |       |     0.18
1.583    0.44    0.03      0.052  o I     |       |       |       |     0.19
1.667    0.44    0.03      0.055  o I     |       |       |       |     0.20
1.750    0.44    0.03      0.058  o I     |       |       |       |     0.21
1.833    0.50    0.03      0.061  o  I    |       |       |       |     0.22
1.917    0.56    0.03      0.064  o  I    |       |       |       |     0.23
2.000    0.58    0.03      0.068  o  I    |       |       |       |     0.25
2.083    0.58    0.03      0.072  o  I    |       |       |       |     0.26
2.167    0.58    0.04      0.075  o  I    |       |       |       |     0.27
2.250    0.58    0.04      0.079  o  I    |       |       |       |     0.29
2.333    0.58    0.04      0.083  o  I    |       |       |       |     0.30
2.417    0.58    0.04      0.087  o  I    |       |       |       |     0.31
2.500    0.58    0.04      0.090  o  I    |       |       |       |     0.33
2.583    0.64    0.05      0.094  o   I   |       |       |       |     0.34
2.667    0.71    0.05      0.099  o   I   |       |       |       |     0.36
2.750    0.72    0.05      0.103  o   I   |       |       |       |     0.37
2.833    0.73    0.05      0.108  o   I   |       |       |       |     0.39
2.917    0.73    0.05      0.113  o   I   |       |       |       |     0.41
3.000    0.73    0.06      0.117  o   I   |       |       |       |     0.42
3.083    0.73    0.06      0.122  o   I   |       |       |       |     0.44
3.167    0.73    0.06      0.126  o   I   |       |       |       |     0.46
3.250    0.73    0.06      0.131  o   I   |       |       |       |     0.47
3.333    0.73    0.07      0.136  o   I   |       |       |       |     0.49
3.417    0.73    0.07      0.140  o   I   |       |       |       |     0.51
3.500    0.73    0.07      0.145  o   I   |       |       |       |     0.52
3.583    0.73    0.07      0.149  o   I   |       |       |       |     0.54
3.667    0.73    0.07      0.154  o   I   |       |       |       |     0.56
3.750    0.73    0.08      0.158  o   I   |       |       |       |     0.57
3.833    0.79    0.08      0.163  o    I  |       |       |       |     0.59
3.917    0.86    0.08      0.168  o    I  |       |       |       |     0.61
4.000    0.87    0.08      0.174  o    I  |       |       |       |     0.63
4.083    0.87    0.09      0.179  o    I  |       |       |       |     0.65
4.167    0.88    0.09      0.184  o    I  |       |       |       |     0.67
4.250    0.88    0.09      0.190  o    I  |       |       |       |     0.69
4.333    0.94    0.09      0.195  o     I |       |       |       |     0.71
4.417    1.00    0.10      0.201  o     I |       |       |       |     0.73
4.500    1.02    0.10      0.208  o     I |       |       |       |     0.75
4.583    1.02    0.10      0.214  o     I |       |       |       |     0.78
4.667    1.02    0.11      0.220  o     I |       |       |       |     0.80
4.750    1.02    0.11      0.227  o     I |       |       |       |     0.82
4.833    1.08    0.11      0.233  o     I |       |       |       |     0.84
4.917    1.15    0.12      0.240  o      I|       |       |       |     0.87
5.000    1.16    0.12      0.247  o      I|       |       |       |     0.90
5.083    1.05    0.12      0.254  o     I |       |       |       |     0.92
5.167    0.92    0.13      0.260  o    I  |       |       |       |     0.94
5.250    0.89    0.13      0.265  o    I  |       |       |       |     0.96
5.333    0.94    0.13      0.271  o     I |       |       |       |     0.98
5.417    1.00    0.13      0.276  o     I |       |       |       |     1.00
5.500    1.02    0.13      0.282  o     I |       |       |       |     1.02
5.583    1.08    0.14      0.289  o     I |       |       |       |     1.04
5.667    1.15    0.14      0.295  o      I|       |       |       |     1.06
5.750    1.16    0.14      0.302  o      I|       |       |       |     1.09
5.833    1.17    0.14      0.310  o      I|       |       |       |     1.11
5.917    1.17    0.14      0.317  o      I|       |       |       |     1.13
6.000    1.17    0.14      0.324  o      I|       |       |       |     1.15
6.083    1.23    0.14      0.331  o      I|       |       |       |     1.18
6.167    1.29    0.15      0.339  o       I       |       |       |     1.20
6.250    1.31    0.15      0.347  o       I       |       |       |     1.23
6.333    1.31    0.15      0.355  o       I       |       |       |     1.26
6.417    1.32    0.15      0.363  o       I       |       |       |     1.28
6.500    1.32    0.15      0.371  o       I       |       |       |     1.31
6.583    1.38    0.15      0.379  o       I       |       |       |     1.33
6.667    1.44    0.15      0.388  o       |I      |       |       |     1.36
6.750    1.45    0.16      0.396  |o      |I      |       |       |     1.39
6.833    1.46    0.16      0.405  |o      |I      |       |       |     1.42
6.917    1.46    0.16      0.414  |o      |I      |       |       |     1.45
7.000    1.46    0.16      0.423  |o      |I      |       |       |     1.48
7.083    1.46    0.16      0.432  |o      |I      |       |       |     1.51
7.167    1.46    0.17      0.441  |o      |I      |       |       |     1.54
7.250    1.46    0.17      0.450  |o      |I      |       |       |     1.57
7.333    1.52    0.17      0.459  |o      |I      |       |       |     1.59
7.417    1.59    0.17      0.469  |o      | I     |       |       |     1.63
7.500    1.60    0.17      0.479  |o      | I     |       |       |     1.66
7.583    1.66    0.17      0.489  |o      | I     |       |       |     1.69
7.667    1.73    0.18      0.499  |o      |  I    |       |       |     1.72
7.750    1.75    0.18      0.510  |o      |  I    |       |       |     1.76
7.833    1.81    0.18      0.521  |o      |  I    |       |       |     1.79
7.917    1.88    0.18      0.532  |o      |   I   |       |       |     1.83
8.000    1.89    0.19      0.544  |o      |   I   |       |       |     1.87
8.083    2.02    0.19      0.556  |o      |   I   |       |       |     1.91
8.167    2.15    0.19      0.569  |o      |    I  |       |       |     1.95
8.250    2.18    0.19      0.583  |o      |     I |       |       |     2.00
8.333    2.19    0.21      0.596  |o      |     I |       |       |     2.04
8.417    2.19    0.23      0.610  |o      |     I |       |       |     2.08
8.500    2.19    0.25      0.623  |o      |     I |       |       |     2.11
8.583    2.25    0.27      0.637  |o      |     I |       |       |     2.15
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 8.667    2.32    0.29      0.651  |O      |      I |       |       |      2.19
 8.750    2.33    0.31      0.665  | O     |       I|       |       |      2.23
 8.833    2.40    0.33      0.679  | O     |       I|       |       |      2.27
 8.917    2.46    0.35      0.693  | O     |       I|       |       |      2.32
 9.000    2.48    0.37      0.708  | O     |       I|       |       |      2.36
 9.083    2.60    0.40      0.722  | O     |        I       |       |      2.40
 9.167    2.73    0.42      0.738  | O     |        |I      |       |      2.45
 9.250    2.76    0.44      0.754  | O     |        |I      |       |      2.49
 9.333    2.83    0.47      0.770  | O     |        | I     |       |      2.54
 9.417    2.90    0.49      0.787  |  O    |        | I     |       |      2.59
 9.500    2.92    0.51      0.803  |  O    |        | I     |       |      2.63
 9.583    2.98    0.54      0.820  |  O    |        |  I    |       |      2.68
 9.667    3.05    0.56      0.837  |  O    |        |  I    |       |      2.73
 9.750    3.06    0.59      0.854  |  O    |        |  I    |       |      2.78
 9.833    3.13    0.61      0.871  |  O    |        |   I   |       |      2.83
 9.917    3.19    0.64      0.888  |   O   |        |   I   |       |      2.88
10.000    3.21    0.66      0.906  |   O   |        |   I   |       |      2.93
10.083    2.80    0.69      0.922  |   O   |        | I     |       |      2.98
10.167    2.34    0.70      0.935  |   O   |        I|      |       |      3.01
10.250    2.25    0.71      0.946  |   O   |       I |      |       |      3.04
10.333    2.21    0.72      0.956  |   O   |       I |      |       |      3.07
10.417    2.19    0.72      0.967  |   O   |       I |      |       |      3.10
10.500    2.19    0.73      0.977  |   O   |       I |      |       |      3.12
10.583    2.49    0.74      0.988  |   O   |         I      |       |      3.15
10.667    2.81    0.75      1.001  |   O   |        | I     |       |      3.19
10.750    2.88    0.76      1.015  |   O   |        | I     |       |      3.23
10.833    2.91    0.77      1.030  |   O   |        | I     |       |      3.27
10.917    2.92    0.78      1.045  |   O   |        | I     |       |      3.31
11.000    2.92    0.79      1.060  |    O  |        | I     |       |      3.34
11.083    2.86    0.80      1.074  |    O  |        | I     |       |      3.38
11.167    2.80    0.80      1.088  |    O  |        | I     |       |      3.42
11.250    2.79    0.81      1.102  |    O  |        |I      |       |      3.46
11.333    2.78    0.82      1.115  |    O  |        |I      |       |      3.49
11.417    2.78    0.83      1.129  |    O  |        |I      |       |      3.53
11.500    2.78    0.84      1.142  |    O  |        |I      |       |      3.56
11.583    2.66    0.84      1.155  |    O  |        |I      |       |      3.59
11.667    2.53    0.85      1.167  |    O  |        I       |       |      3.62
11.750    2.50    0.86      1.178  |    O  |        I       |       |      3.65
11.833    2.55    0.86      1.190  |    O  |        I       |       |      3.68
11.917    2.61    0.87      1.202  |    O  |        I       |       |      3.71
12.000    2.62    0.88      1.214  |    O  |        I       |       |      3.74
12.083    3.05    0.88      1.227  |    O  |        |  I    |       |      3.78
12.167    3.50    0.89      1.244  |    O  |        |    I  |       |      3.82
12.250    3.60    0.90      1.262  |    O  |        |     I |       |      3.86
12.333    3.70    0.91      1.281  |    O  |        |     I |       |      3.91
12.417    3.78    0.92      1.300  |    O  |        |      I|       |      3.96
12.500    3.79    0.93      1.320  |    O  |        |      I|       |      4.01
12.583    3.92    0.94      1.340  |     O |        |       |I      |      4.06
12.667    4.05    0.95      1.361  |     O |        |       | I     |      4.11
12.750    4.08    0.96      1.382  |     O |        |       | I     |      4.16
12.833    4.15    0.97      1.404  |     O |        |       | I     |      4.21
12.917    4.22    0.98      1.426  |     O |        |       |  I    |      4.26
13.000    4.23    0.99      1.448  |     O |        |       |  I    |      4.31
13.083    4.53    1.00      1.472  |     O |        |       |   I   |      4.37
13.167    4.86    1.01      1.497  |     O |        |       |    I  |      4.43
13.250    4.93    1.02      1.524  |     O |        |       |    I  |      4.49
13.333    4.96    1.03      1.551  |     O |        |       |    I  |      4.55
13.417    4.97    1.04      1.578  |     O |        |       |     I |      4.61
13.500    4.97    1.06      1.605  |     O |        |       |     I |      4.68
13.583    4.31    1.07      1.630  |     O |        |       |  I    |      4.73
13.667    3.60    2.32      1.645  |       |      O |       I|      |      4.77
13.750    3.45    3.16      1.651  |       |        |   O I |      |      4.78
13.833    3.39    3.34      1.652  |       |        |    O  |      |      4.78
13.917    3.36    3.36      1.652  |       |        |    O  |      |      4.78
14.000    3.36    3.36      1.652  |       |        |    O  |      |      4.78
14.083    3.60    3.44      1.652  |       |        |     OI|      |      4.78
14.167    3.86    3.64      1.654  |       |        |      OI      |      4.79
14.250    3.91    3.81      1.655  |       |        |       OI     |      4.79
14.333    3.88    3.87      1.655  |       |        |       O      |      4.79
14.417    3.82    3.86      1.655  |       |        |       O      |      4.79
14.500    3.81    3.83      1.655  |       |        |       O      |      4.79
14.583    3.80    3.81      1.655  |       |        |       O      |      4.79
14.667    3.80    3.80      1.655  |       |        |       O      |      4.79
14.750    3.80    3.80      1.655  |       |        |       O      |      4.79
14.833    3.74    3.78      1.655  |       |        |       O      |      4.79
14.917    3.68    3.73      1.654  |       |        |      IO      |      4.79
15.000    3.66    3.69      1.654  |       |        |      O|      |      4.79
15.083    3.60    3.65      1.654  |       |        |      O|      |      4.79
15.167    3.53    3.59      1.653  |       |        |     IO|      |      4.79
15.250    3.52    3.54      1.653  |       |        |     O |      |      4.79
15.333    3.45    3.50      1.653  |       |        |     O |      |      4.79
15.417    3.38    3.44      1.652  |       |        |    IO |      |      4.78
15.500    3.37    3.40      1.652  |       |        |    O  |      |      4.78
15.583    3.13    3.29      1.651  |       |        |   IO  |      |      4.78
15.667    2.86    3.09      1.650  |       |        | IO    |      |      4.78
15.750    2.81    2.91      1.649  |       |        | O     |      |      4.78
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15.833	2.79	2.83	1.648	|	|	|IO	|	|	4.78
15.917	2.78	2.80	1.648	|	|	|IO	|	|	4.78
16.000	2.78	2.78	1.648	|	|	|O	|	|	4.77
16.083	1.88	2.47	1.646	|	| I O|		|	|	4.77
16.167	0.91	1.73	1.641	| I	| O		|	|	4.76
16.250	0.70	1.09	1.637	| I O|			|	|	4.75
16.333	0.62	1.07	1.634	| I O |			|	|	4.74
16.417	0.58	1.07	1.631	| I O |			|	|	4.74
16.500	0.58	1.06	1.628	| I O |			|	|	4.73
16.583	0.53	1.06	1.624	| I O |			|	|	4.72
16.667	0.46	1.06	1.620	| I O |			|	|	4.71
16.750	0.45	1.06	1.616	| I O |			|	|	4.70
16.833	0.44	1.06	1.612	| I O |			|	|	4.69
16.917	0.44	1.06	1.608	| I O |			|	|	4.68
17.000	0.44	1.05	1.603	| I O |			|	|	4.67
17.083	0.56	1.05	1.600	| I O |			|	|	4.66
17.167	0.69	1.05	1.597	| I O |			|	|	4.66
17.250	0.71	1.05	1.594	| I O |			|	|	4.65
17.333	0.73	1.05	1.592	| I O |			|	|	4.65
17.417	0.73	1.05	1.590	| I O |			|	|	4.64
17.500	0.73	1.05	1.588	| I O |			|	|	4.64
17.583	0.73	1.05	1.585	| I O |			|	|	4.63
17.667	0.73	1.05	1.583	| I O |			|	|	4.63
17.750	0.73	1.05	1.581	| I O |			|	|	4.62
17.833	0.67	1.04	1.579	| I O |			|	|	4.62
17.917	0.61	1.04	1.576	| I O |			|	|	4.61
18.000	0.59	1.04	1.573	| I O |			|	|	4.60
18.083	0.59	1.04	1.570	| I O |			|	|	4.60
18.167	0.58	1.04	1.567	| I O |			|	|	4.59
18.250	0.58	1.04	1.563	| I O |			|	|	4.58
18.333	0.58	1.04	1.560	| I O |			|	|	4.57
18.417	0.58	1.04	1.557	| I O |			|	|	4.57
18.500	0.58	1.03	1.554	| I O |			|	|	4.56
18.583	0.53	1.03	1.551	| I O |			|	|	4.55
18.667	0.46	1.03	1.547	| I O |			|	|	4.54
18.750	0.45	1.03	1.543	| I O |			|	|	4.53
18.833	0.38	1.03	1.539	| I O |			|	|	4.52
18.917	0.31	1.03	1.534	| I O |			|	|	4.51
19.000	0.30	1.02	1.529	|I O |			|	|	4.50
19.083	0.35	1.02	1.524	| I O |			|	|	4.49
19.167	0.42	1.02	1.520	| I O |			|	|	4.48
19.250	0.43	1.02	1.516	| I O |			|	|	4.47
19.333	0.50	1.02	1.512	| I O |			|	|	4.46
19.417	0.56	1.02	1.509	| I O |			|	|	4.45
19.500	0.58	1.01	1.506	| I O |			|	|	4.45
19.583	0.52	1.01	1.503	| I O |			|	|	4.44
19.667	0.46	1.01	1.499	| I O |			|	|	4.43
19.750	0.45	1.01	1.495	| I O |			|	|	4.42
19.833	0.38	1.01	1.491	| I O |			|	|	4.41
19.917	0.31	1.01	1.487	| I O |			|	|	4.40
20.000	0.30	1.00	1.482	|I O |			|	|	4.39
20.083	0.35	1.00	1.477	| I O |			|	|	4.38
20.167	0.42	1.00	1.473	| I O |			|	|	4.37
20.250	0.43	1.00	1.469	| I O |			|	|	4.36
20.333	0.44	1.00	1.465	| I O |			|	|	4.35
20.417	0.44	0.99	1.461	| I O |			|	|	4.34
20.500	0.44	0.99	1.457	| I O |			|	|	4.33
20.583	0.44	0.99	1.453	| I O |			|	|	4.32
20.667	0.44	0.99	1.450	| I O |			|	|	4.32
20.750	0.44	0.99	1.446	| I O |			|	|	4.31
20.833	0.38	0.99	1.442	| I O |			|	|	4.30
20.917	0.31	0.98	1.438	| I O |			|	|	4.29
21.000	0.30	0.98	1.433	|I O |			|	|	4.28
21.083	0.35	0.98	1.428	| I O |			|	|	4.27
21.167	0.42	0.98	1.424	| I O |			|	|	4.26
21.250	0.43	0.98	1.420	| I O |			|	|	4.25
21.333	0.38	0.97	1.417	| I O |			|	|	4.24
21.417	0.31	0.97	1.412	| I O |			|	|	4.23
21.500	0.30	0.97	1.408	|I O |			|	|	4.22
21.583	0.35	0.97	1.403	| I O |			|	|	4.21
21.667	0.42	0.97	1.399	| I O |			|	|	4.20
21.750	0.43	0.97	1.395	| I O |			|	|	4.19
21.833	0.38	0.96	1.392	| I O |			|	|	4.18
21.917	0.31	0.96	1.387	| I O |			|	|	4.17
22.000	0.30	0.96	1.383	|I O |			|	|	4.16
22.083	0.35	0.96	1.379	| I O |			|	|	4.15
22.167	0.42	0.96	1.375	| I O |			|	|	4.14
22.250	0.43	0.95	1.371	| I O |			|	|	4.13
22.333	0.38	0.95	1.367	| I O |			|	|	4.12
22.417	0.31	0.95	1.363	| I O |			|	|	4.11
22.500	0.30	0.95	1.359	|I O |			|	|	4.10
22.583	0.29	0.95	1.354	|I O |			|	|	4.09
22.667	0.29	0.94	1.350	|I O |			|	|	4.08
22.750	0.29	0.94	1.345	|I O |			|	|	4.07
22.833	0.29	0.94	1.341	|I O |			|	|	4.06
22.917	0.29	0.94	1.336	|I O |			|	|	4.05

23.000	0.29	0.94	1.332	I o				4.04
23.083	0.29	0.93	1.327	I o				4.03
23.167	0.29	0.93	1.323	I o				4.02
23.250	0.29	0.93	1.318	I o				4.01
23.333	0.29	0.93	1.314	I o				4.00
23.417	0.29	0.93	1.310	I o				3.98
23.500	0.29	0.92	1.305	I o				3.97
23.583	0.29	0.92	1.301	I o				3.96
23.667	0.29	0.92	1.297	I o				3.95
23.750	0.29	0.92	1.292	I o				3.94
23.833	0.29	0.92	1.288	I o				3.93
23.917	0.29	0.91	1.284	I o				3.92
24.000	0.29	0.91	1.279	I o				3.91
24.083	0.17	0.91	1.275	I o				3.90
24.167	0.04	0.91	1.269	I o				3.88
24.250	0.02	0.90	1.263	I o				3.87
24.333	0.00	0.90	1.257	I o				3.85
24.417	0.00	0.90	1.251	I o				3.84
24.500	0.00	0.89	1.245	I o				3.82
24.583	0.00	0.89	1.239	I o				3.80
24.667	0.00	0.89	1.233	I o				3.79
24.750	0.00	0.88	1.227	I o				3.77
24.833	0.00	0.88	1.220	I o				3.76
24.917	0.00	0.88	1.214	I o				3.74
25.000	0.00	0.87	1.208	I o				3.73
25.083	0.00	0.87	1.202	I o				3.71
25.167	0.00	0.87	1.196	I o				3.70
25.250	0.00	0.86	1.190	I o				3.68
25.333	0.00	0.86	1.185	I o				3.67
25.417	0.00	0.86	1.179	I o				3.65
25.500	0.00	0.85	1.173	I o				3.64
25.583	0.00	0.85	1.167	I o				3.62
25.667	0.00	0.85	1.161	I o				3.61
25.750	0.00	0.84	1.155	I o				3.59
25.833	0.00	0.84	1.149	I o				3.58
25.917	0.00	0.84	1.144	I o				3.56
26.000	0.00	0.83	1.138	I o				3.55
26.083	0.00	0.83	1.132	I o				3.54
26.167	0.00	0.83	1.126	I o				3.52
26.250	0.00	0.83	1.121	I o				3.51
26.333	0.00	0.82	1.115	I o				3.49
26.417	0.00	0.82	1.109	I o				3.48
26.500	0.00	0.81	1.104	I o				3.46
26.583	0.00	0.81	1.098	I o				3.45
26.667	0.00	0.81	1.093	I o				3.43
26.750	0.00	0.80	1.087	I o				3.42
26.833	0.00	0.80	1.082	I o				3.40
26.917	0.00	0.80	1.076	I o				3.39
27.000	0.00	0.79	1.071	I o				3.37
27.083	0.00	0.79	1.065	I o				3.36
27.167	0.00	0.79	1.060	I o				3.34
27.250	0.00	0.78	1.054	I o				3.33
27.333	0.00	0.78	1.049	I o				3.32
27.417	0.00	0.77	1.044	I o				3.30
27.500	0.00	0.77	1.038	I o				3.29
27.583	0.00	0.77	1.033	I o				3.27
27.667	0.00	0.76	1.028	I o				3.26
27.750	0.00	0.76	1.022	I o				3.25
27.833	0.00	0.76	1.017	I o				3.23
27.917	0.00	0.75	1.012	I o				3.22
28.000	0.00	0.75	1.007	I o				3.20
28.083	0.00	0.75	1.002	I o				3.19
28.167	0.00	0.74	0.997	I o				3.18
28.250	0.00	0.74	0.991	I o				3.16
28.333	0.00	0.74	0.986	I o				3.15
28.417	0.00	0.73	0.981	I o				3.14
28.500	0.00	0.73	0.976	I o				3.12
28.583	0.00	0.73	0.971	I o				3.11
28.667	0.00	0.72	0.966	I o				3.10
28.750	0.00	0.72	0.961	I o				3.08
28.833	0.00	0.72	0.956	I o				3.07
28.917	0.00	0.71	0.951	I o				3.06
29.000	0.00	0.71	0.946	I o				3.04
29.083	0.00	0.71	0.942	I o				3.03
29.167	0.00	0.70	0.937	I o				3.02
29.250	0.00	0.70	0.932	I o				3.00
29.333	0.00	0.70	0.927	I o				2.99
29.417	0.00	0.69	0.922	I o				2.98
29.500	0.00	0.68	0.918	I o				2.96
29.583	0.00	0.67	0.913	I o				2.95
29.667	0.00	0.67	0.908	I o				2.94
29.750	0.00	0.66	0.904	I o				2.92
29.833	0.00	0.65	0.899	I o				2.91
29.917	0.00	0.65	0.895	I o				2.90
30.000	0.00	0.64	0.890	I o				2.89
30.083	0.00	0.64	0.886	I o				2.87

30.167	0.00	0.63	0.881	I o				2.86
30.250	0.00	0.62	0.877	I o				2.85
30.333	0.00	0.62	0.873	I o				2.83
30.417	0.00	0.61	0.869	I o				2.82
30.500	0.00	0.60	0.864	I o				2.81
30.583	0.00	0.60	0.860	I o				2.80
30.667	0.00	0.59	0.856	I o				2.79
30.750	0.00	0.59	0.852	I o				2.78
30.833	0.00	0.58	0.848	I o				2.76
30.917	0.00	0.57	0.844	I o				2.75
31.000	0.00	0.57	0.840	I o				2.74
31.083	0.00	0.56	0.836	I o				2.73
31.167	0.00	0.56	0.833	I o				2.72
31.250	0.00	0.55	0.829	I o				2.71
31.333	0.00	0.55	0.825	I o				2.70
31.417	0.00	0.54	0.821	I o				2.69
31.500	0.00	0.54	0.817	I o				2.67
31.583	0.00	0.53	0.814	I o				2.66
31.667	0.00	0.52	0.810	I o				2.65
31.750	0.00	0.52	0.807	I o				2.64
31.833	0.00	0.51	0.803	I o				2.63
31.917	0.00	0.51	0.800	I o				2.62
32.000	0.00	0.50	0.796	I o				2.61
32.083	0.00	0.50	0.793	I o				2.60
32.167	0.00	0.49	0.789	I o				2.59
32.250	0.00	0.49	0.786	I o				2.58
32.333	0.00	0.48	0.782	I o				2.57
32.417	0.00	0.48	0.779	I o				2.56
32.500	0.00	0.47	0.776	I o				2.55
32.583	0.00	0.47	0.773	I o				2.55
32.667	0.00	0.46	0.769	I o				2.54
32.750	0.00	0.46	0.766	I o				2.53
32.833	0.00	0.46	0.763	I o				2.52
32.917	0.00	0.45	0.760	I o				2.51
33.000	0.00	0.45	0.757	I o				2.50
33.083	0.00	0.44	0.754	I o				2.49
33.167	0.00	0.44	0.751	I o				2.48
33.250	0.00	0.43	0.748	I o				2.47
33.333	0.00	0.43	0.745	I o				2.46
33.417	0.00	0.42	0.742	I o				2.46
33.500	0.00	0.42	0.739	I o				2.45
33.583	0.00	0.42	0.736	I o				2.44
33.667	0.00	0.41	0.733	I o				2.43
33.750	0.00	0.41	0.730	I o				2.42
33.833	0.00	0.40	0.728	I o				2.41
33.917	0.00	0.40	0.725	I o				2.41
34.000	0.00	0.40	0.722	I o				2.40
34.083	0.00	0.39	0.719	I o				2.39
34.167	0.00	0.39	0.717	I o				2.38
34.250	0.00	0.38	0.714	I o				2.38
34.333	0.00	0.38	0.711	I o				2.37
34.417	0.00	0.38	0.709	I o				2.36
34.500	0.00	0.37	0.706	I o				2.35
34.583	0.00	0.37	0.704	I o				2.35
34.667	0.00	0.36	0.701	I o				2.34
34.750	0.00	0.36	0.699	I o				2.33
34.833	0.00	0.36	0.696	I o				2.32
34.917	0.00	0.35	0.694	I o				2.32
35.000	0.00	0.35	0.691	I o				2.31
35.083	0.00	0.35	0.689	I o				2.30
35.167	0.00	0.34	0.687	I o				2.30
35.250	0.00	0.34	0.684	I o				2.29
35.333	0.00	0.34	0.682	I o				2.28
35.417	0.00	0.33	0.680	I o				2.28
35.500	0.00	0.33	0.677	I o				2.27
35.583	0.00	0.33	0.675	I o				2.26
35.667	0.00	0.32	0.673	I o				2.26
35.750	0.00	0.32	0.671	I o				2.25
35.833	0.00	0.32	0.668	I o				2.24
35.917	0.00	0.31	0.666	I o				2.24
36.000	0.00	0.31	0.664	IO				2.23
36.083	0.00	0.31	0.662	IO				2.23
36.167	0.00	0.30	0.660	IO				2.22
36.250	0.00	0.30	0.658	IO				2.21
36.333	0.00	0.30	0.656	IO				2.21
36.417	0.00	0.30	0.654	IO				2.20
36.500	0.00	0.29	0.652	IO				2.20
36.583	0.00	0.29	0.650	IO				2.19
36.667	0.00	0.29	0.648	IO				2.18
36.750	0.00	0.28	0.646	IO				2.18
36.833	0.00	0.28	0.644	IO				2.17
36.917	0.00	0.28	0.642	IO				2.17
37.000	0.00	0.27	0.640	IO				2.16
37.083	0.00	0.27	0.638	IO				2.16
37.167	0.00	0.27	0.636	IO				2.15
37.250	0.00	0.27	0.634	IO				2.15

37.333	0.00	0.26	0.632	IO					2.14
37.417	0.00	0.26	0.631	IO					2.13
37.500	0.00	0.26	0.629	IO					2.13
37.583	0.00	0.26	0.627	IO					2.12
37.667	0.00	0.25	0.625	IO					2.12
37.750	0.00	0.25	0.624	IO					2.11
37.833	0.00	0.25	0.622	IO					2.11
37.917	0.00	0.25	0.620	IO					2.10
38.000	0.00	0.24	0.618	IO					2.10
38.083	0.00	0.24	0.617	IO					2.09
38.167	0.00	0.24	0.615	IO					2.09
38.250	0.00	0.24	0.614	IO					2.09
38.333	0.00	0.23	0.612	IO					2.08
38.417	0.00	0.23	0.610	IO					2.08
38.500	0.00	0.23	0.609	IO					2.07
38.583	0.00	0.23	0.607	IO					2.07
38.667	0.00	0.22	0.606	IO					2.06
38.750	0.00	0.22	0.604	IO					2.06
38.833	0.00	0.22	0.603	IO					2.05
38.917	0.00	0.22	0.601	IO					2.05
39.000	0.00	0.22	0.600	IO					2.04
39.083	0.00	0.21	0.598	IO					2.04
39.167	0.00	0.21	0.597	IO					2.04
39.250	0.00	0.21	0.595	IO					2.03
39.333	0.00	0.21	0.594	IO					2.03
39.417	0.00	0.21	0.592	IO					2.02
39.500	0.00	0.20	0.591	IO					2.02
39.583	0.00	0.20	0.589	IO					2.02
39.667	0.00	0.20	0.588	IO					2.01
39.750	0.00	0.20	0.587	IO					2.01
39.833	0.00	0.20	0.585	IO					2.00
39.917	0.00	0.19	0.584	IO					2.00
40.000	0.00	0.19	0.583	IO					2.00
40.083	0.00	0.19	0.581	IO					1.99
40.167	0.00	0.19	0.580	IO					1.99
40.250	0.00	0.19	0.579	IO					1.98
40.333	0.00	0.19	0.577	IO					1.98
40.417	0.00	0.19	0.576	IO					1.97
40.500	0.00	0.19	0.575	IO					1.97
40.583	0.00	0.19	0.573	IO					1.97
40.667	0.00	0.19	0.572	IO					1.96
40.750	0.00	0.19	0.571	IO					1.96
40.833	0.00	0.19	0.570	IO					1.95
40.917	0.00	0.19	0.568	IO					1.95
41.000	0.00	0.19	0.567	IO					1.94
41.083	0.00	0.19	0.566	IO					1.94
41.167	0.00	0.19	0.564	IO					1.94
41.250	0.00	0.19	0.563	IO					1.93
41.333	0.00	0.19	0.562	IO					1.93
41.417	0.00	0.19	0.560	IO					1.92
41.500	0.00	0.19	0.559	IO					1.92
41.583	0.00	0.19	0.558	IO					1.92
41.667	0.00	0.19	0.557	IO					1.91
41.750	0.00	0.19	0.555	IO					1.91
41.833	0.00	0.19	0.554	IO					1.90
41.917	0.00	0.19	0.553	IO					1.90
42.000	0.00	0.19	0.551	IO					1.89
42.083	0.00	0.19	0.550	IO					1.89
42.167	0.00	0.19	0.549	IO					1.89
42.250	0.00	0.19	0.548	IO					1.88
42.333	0.00	0.19	0.546	IO					1.88
42.417	0.00	0.19	0.545	IO					1.87
42.500	0.00	0.19	0.544	IO					1.87
42.583	0.00	0.18	0.542	IO					1.87
42.667	0.00	0.18	0.541	IO					1.86
42.750	0.00	0.18	0.540	IO					1.86
42.833	0.00	0.18	0.539	IO					1.85
42.917	0.00	0.18	0.537	IO					1.85
43.000	0.00	0.18	0.536	IO					1.84
43.083	0.00	0.18	0.535	IO					1.84
43.167	0.00	0.18	0.534	IO					1.84
43.250	0.00	0.18	0.532	IO					1.83
43.333	0.00	0.18	0.531	IO					1.83
43.417	0.00	0.18	0.530	IO					1.82
43.500	0.00	0.18	0.529	IO					1.82
43.583	0.00	0.18	0.527	IO					1.82
43.667	0.00	0.18	0.526	IO					1.81
43.750	0.00	0.18	0.525	IO					1.81
43.833	0.00	0.18	0.524	IO					1.80
43.917	0.00	0.18	0.522	IO					1.80
44.000	0.00	0.18	0.521	IO					1.80
44.083	0.00	0.18	0.520	IO					1.79
44.167	0.00	0.18	0.519	IO					1.79
44.250	0.00	0.18	0.517	IO					1.78
44.333	0.00	0.18	0.516	IO					1.78
44.417	0.00	0.18	0.515	IO					1.78

44.500	0.00	0.18	0.514	IO					1.77
44.583	0.00	0.18	0.512	IO					1.77
44.667	0.00	0.18	0.511	IO					1.76
44.750	0.00	0.18	0.510	IO					1.76
44.833	0.00	0.18	0.509	IO					1.76
44.917	0.00	0.18	0.507	IO					1.75
45.000	0.00	0.18	0.506	IO					1.75
45.083	0.00	0.18	0.505	IO					1.74
45.167	0.00	0.18	0.504	IO					1.74
45.250	0.00	0.18	0.503	IO					1.74
45.333	0.00	0.18	0.501	IO					1.73
45.417	0.00	0.18	0.500	IO					1.73
45.500	0.00	0.18	0.499	IO					1.72
45.583	0.00	0.18	0.498	IO					1.72
45.667	0.00	0.18	0.496	IO					1.72
45.750	0.00	0.18	0.495	IO					1.71
45.833	0.00	0.18	0.494	IO					1.71
45.917	0.00	0.18	0.493	IO					1.70
46.000	0.00	0.18	0.492	IO					1.70
46.083	0.00	0.17	0.490	IO					1.70
46.167	0.00	0.17	0.489	IO					1.69
46.250	0.00	0.17	0.488	IO					1.69
46.333	0.00	0.17	0.487	IO					1.68
46.417	0.00	0.17	0.486	IO					1.68
46.500	0.00	0.17	0.484	IO					1.68
46.583	0.00	0.17	0.483	IO					1.67
46.667	0.00	0.17	0.482	IO					1.67
46.750	0.00	0.17	0.481	IO					1.67
46.833	0.00	0.17	0.480	IO					1.66
46.917	0.00	0.17	0.478	IO					1.66
47.000	0.00	0.17	0.477	IO					1.65
47.083	0.00	0.17	0.476	IO					1.65
47.167	0.00	0.17	0.475	IO					1.65
47.250	0.00	0.17	0.474	IO					1.64
47.333	0.00	0.17	0.473	IO					1.64
47.417	0.00	0.17	0.471	IO					1.63
47.500	0.00	0.17	0.470	IO					1.63
47.583	0.00	0.17	0.469	IO					1.63
47.667	0.00	0.17	0.468	IO					1.62
47.750	0.00	0.17	0.467	IO					1.62
47.833	0.00	0.17	0.466	IO					1.62
47.917	0.00	0.17	0.464	IO					1.61
48.000	0.00	0.17	0.463	IO					1.61
48.083	0.00	0.17	0.462	IO					1.60
48.167	0.00	0.17	0.461	IO					1.60
48.250	0.00	0.17	0.460	IO					1.60
48.333	0.00	0.17	0.459	IO					1.59
48.417	0.00	0.17	0.457	IO					1.59
48.500	0.00	0.17	0.456	IO					1.59
48.583	0.00	0.17	0.455	IO					1.58
48.667	0.00	0.17	0.454	IO					1.58
48.750	0.00	0.17	0.453	IO					1.57
48.833	0.00	0.17	0.452	IO					1.57
48.917	0.00	0.17	0.450	IO					1.57
49.000	0.00	0.17	0.449	IO					1.56
49.083	0.00	0.17	0.448	IO					1.56
49.167	0.00	0.17	0.447	IO					1.56
49.250	0.00	0.17	0.446	IO					1.55
49.333	0.00	0.17	0.445	IO					1.55
49.417	0.00	0.17	0.444	IO					1.54
49.500	0.00	0.17	0.442	IO					1.54
49.583	0.00	0.17	0.441	IO					1.54
49.667	0.00	0.16	0.440	IO					1.53
49.750	0.00	0.16	0.439	IO					1.53
49.833	0.00	0.16	0.438	IO					1.53
49.917	0.00	0.16	0.437	IO					1.52
50.000	0.00	0.16	0.436	IO					1.52
50.083	0.00	0.16	0.434	IO					1.51
50.167	0.00	0.16	0.433	IO					1.51
50.250	0.00	0.16	0.432	IO					1.51
50.333	0.00	0.16	0.431	IO					1.50
50.417	0.00	0.16	0.430	IO					1.50
50.500	0.00	0.16	0.429	IO					1.50
50.583	0.00	0.16	0.428	IO					1.49
50.667	0.00	0.16	0.427	IO					1.49
50.750	0.00	0.16	0.425	IO					1.49
50.833	0.00	0.16	0.424	IO					1.48
50.917	0.00	0.16	0.423	IO					1.48
51.000	0.00	0.16	0.422	IO					1.47
51.083	0.00	0.16	0.421	IO					1.47
51.167	0.00	0.16	0.420	IO					1.47
51.250	0.00	0.16	0.419	IO					1.46
51.333	0.00	0.16	0.418	IO					1.46
51.417	0.00	0.16	0.417	IO					1.46
51.500	0.00	0.16	0.416	IO					1.45
51.583	0.00	0.16	0.414	IO					1.45

51.667	0.00	0.16	0.413	IO					1.45
51.750	0.00	0.16	0.412	IO					1.44
51.833	0.00	0.16	0.411	IO					1.44
51.917	0.00	0.16	0.410	IO					1.44
52.000	0.00	0.16	0.409	IO					1.43
52.083	0.00	0.16	0.408	IO					1.43
52.167	0.00	0.16	0.407	IO					1.42
52.250	0.00	0.16	0.406	IO					1.42
52.333	0.00	0.16	0.405	IO					1.42
52.417	0.00	0.16	0.403	IO					1.41
52.500	0.00	0.16	0.402	IO					1.41
52.583	0.00	0.16	0.401	IO					1.41
52.667	0.00	0.16	0.400	IO					1.40
52.750	0.00	0.16	0.399	IO					1.40
52.833	0.00	0.16	0.398	IO					1.40
52.917	0.00	0.16	0.397	IO					1.39
53.000	0.00	0.16	0.396	IO					1.39
53.083	0.00	0.16	0.395	IO					1.39
53.167	0.00	0.16	0.394	IO					1.38
53.250	0.00	0.16	0.393	IO					1.38
53.333	0.00	0.16	0.392	IO					1.38
53.417	0.00	0.16	0.391	IO					1.37
53.500	0.00	0.16	0.389	O					1.37
53.583	0.00	0.15	0.388	O					1.36
53.667	0.00	0.15	0.387	O					1.36
53.750	0.00	0.15	0.386	O					1.36
53.833	0.00	0.15	0.385	O					1.35
53.917	0.00	0.15	0.384	O					1.35
54.000	0.00	0.15	0.383	O					1.35
54.083	0.00	0.15	0.382	O					1.34
54.167	0.00	0.15	0.381	O					1.34
54.250	0.00	0.15	0.380	O					1.34
54.333	0.00	0.15	0.379	O					1.33
54.417	0.00	0.15	0.378	O					1.33
54.500	0.00	0.15	0.377	O					1.33
54.583	0.00	0.15	0.376	O					1.32
54.667	0.00	0.15	0.375	O					1.32
54.750	0.00	0.15	0.374	O					1.32
54.833	0.00	0.15	0.373	O					1.31
54.917	0.00	0.15	0.371	O					1.31
55.000	0.00	0.15	0.370	O					1.31
55.083	0.00	0.15	0.369	O					1.30
55.167	0.00	0.15	0.368	O					1.30
55.250	0.00	0.15	0.367	O					1.30
55.333	0.00	0.15	0.366	O					1.29
55.417	0.00	0.15	0.365	O					1.29
55.500	0.00	0.15	0.364	O					1.29
55.583	0.00	0.15	0.363	O					1.28
55.667	0.00	0.15	0.362	O					1.28
55.750	0.00	0.15	0.361	O					1.28
55.833	0.00	0.15	0.360	O					1.27
55.917	0.00	0.15	0.359	O					1.27
56.000	0.00	0.15	0.358	O					1.27
56.083	0.00	0.15	0.357	O					1.26
56.167	0.00	0.15	0.356	O					1.26
56.250	0.00	0.15	0.355	O					1.26
56.333	0.00	0.15	0.354	O					1.25
56.417	0.00	0.15	0.353	O					1.25
56.500	0.00	0.15	0.352	O					1.25
56.583	0.00	0.15	0.351	O					1.24
56.667	0.00	0.15	0.350	O					1.24
56.750	0.00	0.15	0.349	O					1.24
56.833	0.00	0.15	0.348	O					1.23
56.917	0.00	0.15	0.347	O					1.23
57.000	0.00	0.15	0.346	O					1.23
57.083	0.00	0.15	0.345	O					1.22
57.167	0.00	0.15	0.344	O					1.22
57.250	0.00	0.15	0.343	O					1.22
57.333	0.00	0.15	0.342	O					1.21
57.417	0.00	0.15	0.341	O					1.21
57.500	0.00	0.15	0.340	O					1.21
57.583	0.00	0.15	0.339	O					1.20
57.667	0.00	0.15	0.338	O					1.20
57.750	0.00	0.14	0.337	O					1.20
57.833	0.00	0.14	0.336	O					1.19
57.917	0.00	0.14	0.335	O					1.19
58.000	0.00	0.14	0.334	O					1.19
58.083	0.00	0.14	0.333	O					1.18
58.167	0.00	0.14	0.332	O					1.18
58.250	0.00	0.14	0.331	O					1.18
58.333	0.00	0.14	0.330	O					1.17
58.417	0.00	0.14	0.329	O					1.17
58.500	0.00	0.14	0.328	O					1.17
58.583	0.00	0.14	0.327	O					1.17
58.667	0.00	0.14	0.326	O					1.16
58.750	0.00	0.14	0.325	O					1.16

58.833	0.00	0.14	0.324	o	|	|	|	1.16
58.917	0.00	0.14	0.323	o	|	|	|	1.15
59.000	0.00	0.14	0.322	o	|	|	|	1.15
59.083	0.00	0.14	0.321	o	|	|	|	1.15
59.167	0.00	0.14	0.320	o	|	|	|	1.14
59.250	0.00	0.14	0.319	o	|	|	|	1.14
59.333	0.00	0.14	0.318	o	|	|	|	1.14
59.417	0.00	0.14	0.317	o	|	|	|	1.13
59.500	0.00	0.14	0.316	o	|	|	|	1.13
59.583	0.00	0.14	0.315	o	|	|	|	1.13
59.667	0.00	0.14	0.314	o	|	|	|	1.12
59.750	0.00	0.14	0.313	o	|	|	|	1.12
59.833	0.00	0.14	0.312	o	|	|	|	1.12
59.917	0.00	0.14	0.311	o	|	|	|	1.11
60.000	0.00	0.14	0.310	o	|	|	|	1.11
60.083	0.00	0.14	0.309	o	|	|	|	1.11
60.167	0.00	0.14	0.308	o	|	|	|	1.11
60.250	0.00	0.14	0.307	o	|	|	|	1.10
60.333	0.00	0.14	0.307	o	|	|	|	1.10
60.417	0.00	0.14	0.306	o	|	|	|	1.10
60.500	0.00	0.14	0.305	o	|	|	|	1.09
60.583	0.00	0.14	0.304	o	|	|	|	1.09
60.667	0.00	0.14	0.303	o	|	|	|	1.09
60.750	0.00	0.14	0.302	o	|	|	|	1.08
60.833	0.00	0.14	0.301	o	|	|	|	1.08
60.917	0.00	0.14	0.300	o	|	|	|	1.08
61.000	0.00	0.14	0.299	o	|	|	|	1.07
61.083	0.00	0.14	0.298	o	|	|	|	1.07
61.167	0.00	0.14	0.297	o	|	|	|	1.07
61.250	0.00	0.14	0.296	o	|	|	|	1.07
61.333	0.00	0.14	0.295	o	|	|	|	1.06
61.417	0.00	0.14	0.294	o	|	|	|	1.06
61.500	0.00	0.14	0.293	o	|	|	|	1.06
61.583	0.00	0.14	0.292	o	|	|	|	1.05
61.667	0.00	0.14	0.291	o	|	|	|	1.05
61.750	0.00	0.14	0.290	o	|	|	|	1.05
61.833	0.00	0.14	0.289	o	|	|	|	1.04
61.917	0.00	0.14	0.289	o	|	|	|	1.04
62.000	0.00	0.14	0.288	o	|	|	|	1.04
62.083	0.00	0.14	0.287	o	|	|	|	1.03
62.167	0.00	0.13	0.286	o	|	|	|	1.03
62.250	0.00	0.13	0.285	o	|	|	|	1.03
62.333	0.00	0.13	0.284	o	|	|	|	1.03
62.417	0.00	0.13	0.283	o	|	|	|	1.02
62.500	0.00	0.13	0.282	o	|	|	|	1.02
62.583	0.00	0.13	0.281	o	|	|	|	1.02
62.667	0.00	0.13	0.280	o	|	|	|	1.01
62.750	0.00	0.13	0.279	o	|	|	|	1.01
62.833	0.00	0.13	0.278	o	|	|	|	1.01
62.917	0.00	0.13	0.277	o	|	|	|	1.00
63.000	0.00	0.13	0.277	o	|	|	|	1.00
63.083	0.00	0.13	0.276	o	|	|	|	1.00
63.167	0.00	0.13	0.275	o	|	|	|	1.00
63.250	0.00	0.13	0.274	o	|	|	|	0.99
63.333	0.00	0.13	0.273	o	|	|	|	0.99
63.417	0.00	0.13	0.272	o	|	|	|	0.99
63.500	0.00	0.13	0.271	o	|	|	|	0.98
63.583	0.00	0.13	0.270	o	|	|	|	0.98
63.667	0.00	0.13	0.269	o	|	|	|	0.98
63.750	0.00	0.13	0.268	o	|	|	|	0.97
63.833	0.00	0.13	0.268	o	|	|	|	0.97
63.917	0.00	0.13	0.267	o	|	|	|	0.97
64.000	0.00	0.13	0.266	o	|	|	|	0.96
64.083	0.00	0.13	0.265	o	|	|	|	0.96
64.167	0.00	0.13	0.264	o	|	|	|	0.96
64.250	0.00	0.13	0.263	o	|	|	|	0.95
64.333	0.00	0.13	0.262	o	|	|	|	0.95
64.417	0.00	0.13	0.261	o	|	|	|	0.95
64.500	0.00	0.13	0.260	o	|	|	|	0.94
64.583	0.00	0.13	0.260	o	|	|	|	0.94
64.667	0.00	0.12	0.259	o	|	|	|	0.94
64.750	0.00	0.12	0.258	o	|	|	|	0.93
64.833	0.00	0.12	0.257	o	|	|	|	0.93
64.917	0.00	0.12	0.256	o	|	|	|	0.93
65.000	0.00	0.12	0.255	o	|	|	|	0.93
65.083	0.00	0.12	0.255	o	|	|	|	0.92
65.167	0.00	0.12	0.254	o	|	|	|	0.92
65.250	0.00	0.12	0.253	o	|	|	|	0.92
65.333	0.00	0.12	0.252	o	|	|	|	0.91
65.417	0.00	0.12	0.251	o	|	|	|	0.91
65.500	0.00	0.12	0.250	o	|	|	|	0.91
65.583	0.00	0.12	0.249	o	|	|	|	0.90
65.667	0.00	0.12	0.249	o	|	|	|	0.90
65.750	0.00	0.12	0.248	o	|	|	|	0.90
65.833	0.00	0.12	0.247	o	|	|	|	0.90
65.917	0.00	0.12	0.246	o	|	|	|	0.89

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66.000    0.00    0.12      0.245  o       |       |       |       |      0.89
66.083    0.00    0.12      0.245  o       |       |       |       |      0.89
66.167    0.00    0.12      0.244  o       |       |       |       |      0.88
66.250    0.00    0.12      0.243  o       |       |       |       |      0.88
66.333    0.00    0.12      0.242  o       |       |       |       |      0.88
66.417    0.00    0.12      0.241  o       |       |       |       |      0.87
66.500    0.00    0.12      0.241  o       |       |       |       |      0.87
66.583    0.00    0.12      0.240  o       |       |       |       |      0.87
66.667    0.00    0.12      0.239  o       |       |       |       |      0.87
66.750    0.00    0.11      0.238  o       |       |       |       |      0.86
66.833    0.00    0.11      0.237  o       |       |       |       |      0.86
66.917    0.00    0.11      0.237  o       |       |       |       |      0.86
67.000    0.00    0.11      0.236  o       |       |       |       |      0.85
67.083    0.00    0.11      0.235  o       |       |       |       |      0.85
67.167    0.00    0.11      0.234  o       |       |       |       |      0.85
67.250    0.00    0.11      0.233  o       |       |       |       |      0.85
67.333    0.00    0.11      0.233  o       |       |       |       |      0.84
67.417    0.00    0.11      0.232  o       |       |       |       |      0.84
67.500    0.00    0.11      0.231  o       |       |       |       |      0.84
67.583    0.00    0.11      0.230  o       |       |       |       |      0.83
67.667    0.00    0.11      0.230  o       |       |       |       |      0.83
67.750    0.00    0.11      0.229  o       |       |       |       |      0.83
67.833    0.00    0.11      0.228  o       |       |       |       |      0.83
67.917    0.00    0.11      0.227  o       |       |       |       |      0.82
68.000    0.00    0.11      0.227  o       |       |       |       |      0.82
68.083    0.00    0.11      0.226  o       |       |       |       |      0.82
68.167    0.00    0.11      0.225  o       |       |       |       |      0.82
68.250    0.00    0.11      0.224  o       |       |       |       |      0.81
68.333    0.00    0.11      0.224  o       |       |       |       |      0.81
68.417    0.00    0.11      0.223  o       |       |       |       |      0.81
68.500    0.00    0.11      0.222  o       |       |       |       |      0.80
68.583    0.00    0.11      0.221  o       |       |       |       |      0.80
68.667    0.00    0.11      0.221  o       |       |       |       |      0.80
68.750    0.00    0.11      0.220  o       |       |       |       |      0.80
68.833    0.00    0.11      0.219  o       |       |       |       |      0.79
68.917    0.00    0.11      0.218  o       |       |       |       |      0.79
69.000    0.00    0.10      0.218  o       |       |       |       |      0.79
69.083    0.00    0.10      0.217  o       |       |       |       |      0.79
69.167    0.00    0.10      0.216  o       |       |       |       |      0.78
69.250    0.00    0.10      0.216  o       |       |       |       |      0.78
69.333    0.00    0.10      0.215  o       |       |       |       |      0.78
69.417    0.00    0.10      0.214  o       |       |       |       |      0.78
69.500    0.00    0.10      0.213  o       |       |       |       |      0.77
69.583    0.00    0.10      0.213  o       |       |       |       |      0.77
69.667    0.00    0.10      0.212  o       |       |       |       |      0.77
69.750    0.00    0.10      0.211  o       |       |       |       |      0.77
69.833    0.00    0.10      0.211  o       |       |       |       |      0.76
69.917    0.00    0.10      0.210  o       |       |       |       |      0.76
70.000    0.00    0.10      0.209  o       |       |       |       |      0.76
70.083    0.00    0.10      0.209  o       |       |       |       |      0.76
70.167    0.00    0.10      0.208  o       |       |       |       |      0.75
70.250    0.00    0.10      0.207  o       |       |       |       |      0.75
      Remaining water in basin =    0.21 (Ac.Ft)
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =   843
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =        3.870 (CFS)
                  Total volume =       2.813 (Ac.Ft)
            Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
      ************************************************************************
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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 05/07/25

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: PRO10110.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    16
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       51.576 (CFS)
               Total volume =       1.489 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
*************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
____________________________________________________________________________

User entry of depth-outflow-storage data
---------------------------------------------------------------------
Total number of inflow hydrograph intervals = 16
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
---------------------------------------------------------------------
---------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
---------------------------------------------------------------------
---------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
---------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.276      0.133      0.276        0.276
   2.000      0.584      0.193      0.583        0.585
   3.000      0.930      0.700      0.928        0.932
   3.500      1.118      0.824      1.115        1.121
   4.000      1.316      0.930      1.313        1.319
   4.500      1.528      1.024      1.524        1.532
   4.750      1.637      1.068      1.633        1.641
   5.000      1.749     18.283      1.686        1.812
   6.000      2.231    253.655      1.358        3.104
---------------------------------------------------------------------
               Hydrograph Detention Basin Routing
---------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
---------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                    Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0      12.9   25.79   38.68   51.58 (Ft.)
 0.083    1.92    0.00      0.007  OI      |       |       |       |     0.02
 0.167    4.57    0.01      0.029  O I     |       |       |       |     0.10
 0.250    5.87    0.03      0.065  O  I    |       |       |       |     0.23
 0.333    6.90    0.05      0.108  O   I   |       |       |       |     0.39
 0.417    8.05    0.08      0.159  O   I   |       |       |       |     0.58
 0.500    9.87    0.11      0.220  O     I |       |       |       |     0.80
 0.583   11.99    0.14      0.295  O      I|       |       |       |     1.06
 0.667   15.41    0.15      0.388  O       |I      |       |       |     1.36
 0.750   24.15    0.18      0.523  O       |     I |       |       |     1.80
 0.833   51.58    0.48      0.782  O       |       |       |      I|     2.57
 0.917   47.26    0.82      1.118  O       |       |       |    I  |     3.50
 1.000   18.20    0.94      1.337  O       |  I    |       |       |     4.05
 1.083    7.52    0.98      1.419  O   I   |       |       |       |     4.24
 1.167    2.44    0.99      1.446  OI      |       |       |       |     4.31
 1.250    0.45    0.99      1.450  O       |       |       |       |     4.31
 1.333    0.09    0.99      1.445  O       |       |       |       |     4.30
 1.417    0.00    0.98      1.438  O       |       |       |       |     4.29
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1.500	0.00	0.98	1.431	o	|	|	|	4.27
1.583	0.00	0.98	1.425	o	|	|	|	4.26
1.667	0.00	0.98	1.418	o	|	|	|	4.24
1.750	0.00	0.97	1.411	o	|	|	|	4.22
1.833	0.00	0.97	1.404	o	|	|	|	4.21
1.917	0.00	0.97	1.398	o	|	|	|	4.19
2.000	0.00	0.96	1.391	o	|	|	|	4.18
2.083	0.00	0.96	1.385	o	|	|	|	4.16
2.167	0.00	0.96	1.378	o	|	|	|	4.15
2.250	0.00	0.95	1.371	o	|	|	|	4.13
2.333	0.00	0.95	1.365	o	|	|	|	4.12
2.417	0.00	0.95	1.358	o	|	|	|	4.10
2.500	0.00	0.95	1.352	o	|	|	|	4.08
2.583	0.00	0.94	1.345	o	|	|	|	4.07
2.667	0.00	0.94	1.339	o	|	|	|	4.05
2.750	0.00	0.94	1.332	o	|	|	|	4.04
2.833	0.00	0.93	1.326	o	|	|	|	4.02
2.917	0.00	0.93	1.319	o	|	|	|	4.01
3.000	0.00	0.93	1.313	o	|	|	|	3.99
3.083	0.00	0.92	1.307	o	|	|	|	3.98
3.167	0.00	0.92	1.300	o	|	|	|	3.96
3.250	0.00	0.92	1.294	o	|	|	|	3.94
3.333	0.00	0.91	1.288	o	|	|	|	3.93
3.417	0.00	0.91	1.281	o	|	|	|	3.91
3.500	0.00	0.91	1.275	o	|	|	|	3.90
3.583	0.00	0.90	1.269	o	|	|	|	3.88
3.667	0.00	0.90	1.263	o	|	|	|	3.87
3.750	0.00	0.90	1.256	o	|	|	|	3.85
3.833	0.00	0.89	1.250	o	|	|	|	3.83
3.917	0.00	0.89	1.244	o	|	|	|	3.82
4.000	0.00	0.89	1.238	o	|	|	|	3.80
4.083	0.00	0.88	1.232	o	|	|	|	3.79
4.167	0.00	0.88	1.226	o	|	|	|	3.77
4.250	0.00	0.88	1.220	o	|	|	|	3.76
4.333	0.00	0.88	1.214	o	|	|	|	3.74
4.417	0.00	0.87	1.208	o	|	|	|	3.73
4.500	0.00	0.87	1.202	o	|	|	|	3.71
4.583	0.00	0.87	1.196	o	|	|	|	3.70
4.667	0.00	0.86	1.190	o	|	|	|	3.68
4.750	0.00	0.86	1.184	o	|	|	|	3.67
4.833	0.00	0.86	1.178	o	|	|	|	3.65
4.917	0.00	0.85	1.172	o	|	|	|	3.64
5.000	0.00	0.85	1.166	o	|	|	|	3.62
5.083	0.00	0.85	1.160	o	|	|	|	3.61
5.167	0.00	0.84	1.154	o	|	|	|	3.59
5.250	0.00	0.84	1.149	o	|	|	|	3.58
5.333	0.00	0.84	1.143	o	|	|	|	3.56
5.417	0.00	0.83	1.137	o	|	|	|	3.55
5.500	0.00	0.83	1.131	o	|	|	|	3.53
5.583	0.00	0.83	1.126	o	|	|	|	3.52
5.667	0.00	0.83	1.120	o	|	|	|	3.51
5.750	0.00	0.82	1.114	o	|	|	|	3.49
5.833	0.00	0.82	1.109	o	|	|	|	3.48
5.917	0.00	0.81	1.103	o	|	|	|	3.46
6.000	0.00	0.81	1.097	o	|	|	|	3.45
6.083	0.00	0.81	1.092	o	|	|	|	3.43
6.167	0.00	0.80	1.086	o	|	|	|	3.42
6.250	0.00	0.80	1.081	o	|	|	|	3.40
6.333	0.00	0.80	1.075	o	|	|	|	3.39
6.417	0.00	0.79	1.070	o	|	|	|	3.37
6.500	0.00	0.79	1.064	o	|	|	|	3.36
6.583	0.00	0.79	1.059	o	|	|	|	3.34
6.667	0.00	0.78	1.054	o	|	|	|	3.33
6.750	0.00	0.78	1.048	o	|	|	|	3.31
6.833	0.00	0.77	1.043	o	|	|	|	3.30
6.917	0.00	0.77	1.038	o	|	|	|	3.29
7.000	0.00	0.77	1.032	o	|	|	|	3.27
7.083	0.00	0.76	1.027	o	|	|	|	3.26
7.167	0.00	0.76	1.022	o	|	|	|	3.24
7.250	0.00	0.76	1.017	o	|	|	|	3.23
7.333	0.00	0.75	1.011	o	|	|	|	3.22
7.417	0.00	0.75	1.006	o	|	|	|	3.20
7.500	0.00	0.75	1.001	o	|	|	|	3.19
7.583	0.00	0.74	0.996	o	|	|	|	3.18
7.667	0.00	0.74	0.991	o	|	|	|	3.16
7.750	0.00	0.74	0.986	o	|	|	|	3.15
7.833	0.00	0.73	0.981	o	|	|	|	3.13
7.917	0.00	0.73	0.976	o	|	|	|	3.12
8.000	0.00	0.73	0.971	o	|	|	|	3.11
8.083	0.00	0.72	0.966	o	|	|	|	3.09
8.167	0.00	0.72	0.961	o	|	|	|	3.08
8.250	0.00	0.72	0.956	o	|	|	|	3.07
8.333	0.00	0.71	0.951	o	|	|	|	3.06
8.417	0.00	0.71	0.946	o	|	|	|	3.04
8.500	0.00	0.71	0.941	o	|	|	|	3.03
8.583	0.00	0.70	0.936	o	|	|	|	3.02

8.667	0.00	0.70	0.931	o	|	|	|	3.00
8.750	0.00	0.69	0.926	o	|	|	|	2.99
8.833	0.00	0.69	0.922	o	|	|	|	2.98
8.917	0.00	0.68	0.917	o	|	|	|	2.96
9.000	0.00	0.67	0.912	o	|	|	|	2.95
9.083	0.00	0.67	0.908	o	|	|	|	2.94
9.167	0.00	0.66	0.903	o	|	|	|	2.92
9.250	0.00	0.65	0.899	o	|	|	|	2.91
9.333	0.00	0.65	0.894	o	|	|	|	2.90
9.417	0.00	0.64	0.890	o	|	|	|	2.88
9.500	0.00	0.63	0.885	o	|	|	|	2.87
9.583	0.00	0.63	0.881	o	|	|	|	2.86
9.667	0.00	0.62	0.877	o	|	|	|	2.85
9.750	0.00	0.62	0.872	o	|	|	|	2.83
9.833	0.00	0.61	0.868	o	|	|	|	2.82
9.917	0.00	0.60	0.864	o	|	|	|	2.81
10.000	0.00	0.60	0.860	o	|	|	|	2.80
10.083	0.00	0.59	0.856	o	|	|	|	2.79
10.167	0.00	0.59	0.852	o	|	|	|	2.77
10.250	0.00	0.58	0.848	o	|	|	|	2.76
10.333	0.00	0.57	0.844	o	|	|	|	2.75
10.417	0.00	0.57	0.840	o	|	|	|	2.74
10.500	0.00	0.56	0.836	o	|	|	|	2.73
10.583	0.00	0.56	0.832	o	|	|	|	2.72
10.667	0.00	0.55	0.828	o	|	|	|	2.71
10.750	0.00	0.55	0.824	o	|	|	|	2.69
10.833	0.00	0.54	0.821	o	|	|	|	2.68
10.917	0.00	0.53	0.817	o	|	|	|	2.67
11.000	0.00	0.53	0.813	o	|	|	|	2.66
11.083	0.00	0.52	0.810	o	|	|	|	2.65
11.167	0.00	0.52	0.806	o	|	|	|	2.64
11.250	0.00	0.51	0.803	o	|	|	|	2.63
11.333	0.00	0.51	0.799	o	|	|	|	2.62
11.417	0.00	0.50	0.796	o	|	|	|	2.61
11.500	0.00	0.50	0.792	o	|	|	|	2.60
11.583	0.00	0.49	0.789	o	|	|	|	2.59
11.667	0.00	0.49	0.785	o	|	|	|	2.58
11.750	0.00	0.48	0.782	o	|	|	|	2.57
11.833	0.00	0.48	0.779	o	|	|	|	2.56
11.917	0.00	0.47	0.775	o	|	|	|	2.55
12.000	0.00	0.47	0.772	o	|	|	|	2.54
12.083	0.00	0.46	0.769	o	|	|	|	2.53
12.167	0.00	0.46	0.766	o	|	|	|	2.53
12.250	0.00	0.45	0.763	o	|	|	|	2.52
12.333	0.00	0.45	0.760	o	|	|	|	2.51
12.417	0.00	0.45	0.756	o	|	|	|	2.50
12.500	0.00	0.44	0.753	o	|	|	|	2.49
12.583	0.00	0.44	0.750	o	|	|	|	2.48
12.667	0.00	0.43	0.747	o	|	|	|	2.47
12.750	0.00	0.43	0.744	o	|	|	|	2.46
12.833	0.00	0.42	0.741	o	|	|	|	2.46
12.917	0.00	0.42	0.739	o	|	|	|	2.45
13.000	0.00	0.42	0.736	o	|	|	|	2.44
13.083	0.00	0.41	0.733	o	|	|	|	2.43
13.167	0.00	0.41	0.730	o	|	|	|	2.42
13.250	0.00	0.40	0.727	o	|	|	|	2.41
13.333	0.00	0.40	0.724	o	|	|	|	2.41
13.417	0.00	0.39	0.722	o	|	|	|	2.40
13.500	0.00	0.39	0.719	o	|	|	|	2.39
13.583	0.00	0.39	0.716	o	|	|	|	2.38
13.667	0.00	0.38	0.714	o	|	|	|	2.37
13.750	0.00	0.38	0.711	o	|	|	|	2.37
13.833	0.00	0.38	0.708	o	|	|	|	2.36
13.917	0.00	0.37	0.706	o	|	|	|	2.35
14.000	0.00	0.37	0.703	o	|	|	|	2.34
14.083	0.00	0.36	0.701	o	|	|	|	2.34
14.167	0.00	0.36	0.698	o	|	|	|	2.33
14.250	0.00	0.36	0.696	o	|	|	|	2.32
14.333	0.00	0.35	0.693	o	|	|	|	2.32
14.417	0.00	0.35	0.691	o	|	|	|	2.31
14.500	0.00	0.35	0.689	o	|	|	|	2.30
14.583	0.00	0.34	0.686	o	|	|	|	2.30
14.667	0.00	0.34	0.684	o	|	|	|	2.29
14.750	0.00	0.34	0.682	o	|	|	|	2.28
14.833	0.00	0.33	0.679	o	|	|	|	2.28
14.917	0.00	0.33	0.677	o	|	|	|	2.27
15.000	0.00	0.33	0.675	o	|	|	|	2.26
15.083	0.00	0.32	0.672	o	|	|	|	2.26
15.167	0.00	0.32	0.670	o	|	|	|	2.25
15.250	0.00	0.32	0.668	o	|	|	|	2.24
15.333	0.00	0.31	0.666	o	|	|	|	2.24
15.417	0.00	0.31	0.664	o	|	|	|	2.23
15.500	0.00	0.31	0.662	o	|	|	|	2.22
15.583	0.00	0.30	0.660	o	|	|	|	2.22
15.667	0.00	0.30	0.657	o	|	|	|	2.21
15.750	0.00	0.30	0.655	o	|	|	|	2.21

15.833	0.00	0.29	0.653	o	|	|	|	|	2.20
15.917	0.00	0.29	0.651	o	|	|	|	|	2.19
16.000	0.00	0.29	0.649	o	|	|	|	|	2.19
16.083	0.00	0.29	0.647	o	|	|	|	|	2.18
16.167	0.00	0.28	0.645	o	|	|	|	|	2.18
16.250	0.00	0.28	0.643	o	|	|	|	|	2.17
16.333	0.00	0.28	0.642	o	|	|	|	|	2.17
16.417	0.00	0.27	0.640	o	|	|	|	|	2.16
16.500	0.00	0.27	0.638	o	|	|	|	|	2.16
16.583	0.00	0.27	0.636	o	|	|	|	|	2.15
16.667	0.00	0.27	0.634	o	|	|	|	|	2.14
16.750	0.00	0.26	0.632	o	|	|	|	|	2.14
16.833	0.00	0.26	0.630	o	|	|	|	|	2.13
16.917	0.00	0.26	0.629	o	|	|	|	|	2.13
17.000	0.00	0.26	0.627	o	|	|	|	|	2.12
17.083	0.00	0.25	0.625	o	|	|	|	|	2.12
17.167	0.00	0.25	0.623	o	|	|	|	|	2.11
17.250	0.00	0.25	0.622	o	|	|	|	|	2.11
17.333	0.00	0.25	0.620	o	|	|	|	|	2.10
17.417	0.00	0.24	0.618	o	|	|	|	|	2.10
17.500	0.00	0.24	0.617	o	|	|	|	|	2.09
17.583	0.00	0.24	0.615	o	|	|	|	|	2.09
17.667	0.00	0.24	0.613	o	|	|	|	|	2.08
17.750	0.00	0.23	0.612	o	|	|	|	|	2.08
17.833	0.00	0.23	0.610	o	|	|	|	|	2.08
17.917	0.00	0.23	0.609	o	|	|	|	|	2.07
18.000	0.00	0.23	0.607	o	|	|	|	|	2.07
18.083	0.00	0.22	0.605	o	|	|	|	|	2.06
18.167	0.00	0.22	0.604	o	|	|	|	|	2.06
18.250	0.00	0.22	0.602	o	|	|	|	|	2.05
18.333	0.00	0.22	0.601	o	|	|	|	|	2.05
18.417	0.00	0.22	0.599	o	|	|	|	|	2.04
18.500	0.00	0.21	0.598	o	|	|	|	|	2.04
18.583	0.00	0.21	0.596	o	|	|	|	|	2.04
18.667	0.00	0.21	0.595	o	|	|	|	|	2.03
18.750	0.00	0.21	0.594	o	|	|	|	|	2.03
18.833	0.00	0.20	0.592	o	|	|	|	|	2.02
18.917	0.00	0.20	0.591	o	|	|	|	|	2.02
19.000	0.00	0.20	0.589	o	|	|	|	|	2.02
19.083	0.00	0.20	0.588	o	|	|	|	|	2.01
19.167	0.00	0.20	0.587	o	|	|	|	|	2.01
19.250	0.00	0.19	0.585	o	|	|	|	|	2.00
19.333	0.00	0.19	0.584	o	|	|	|	|	2.00
19.417	0.00	0.19	0.583	o	|	|	|	|	2.00
19.500	0.00	0.19	0.581	o	|	|	|	|	1.99
19.583	0.00	0.19	0.580	o	|	|	|	|	1.99
19.667	0.00	0.19	0.579	o	|	|	|	|	1.98
19.750	0.00	0.19	0.577	o	|	|	|	|	1.98
19.833	0.00	0.19	0.576	o	|	|	|	|	1.97
19.917	0.00	0.19	0.575	o	|	|	|	|	1.97
20.000	0.00	0.19	0.573	o	|	|	|	|	1.97
20.083	0.00	0.19	0.572	o	|	|	|	|	1.96
20.167	0.00	0.19	0.571	o	|	|	|	|	1.96
20.250	0.00	0.19	0.569	o	|	|	|	|	1.95
20.333	0.00	0.19	0.568	o	|	|	|	|	1.95
20.417	0.00	0.19	0.567	o	|	|	|	|	1.94
20.500	0.00	0.19	0.565	o	|	|	|	|	1.94
20.583	0.00	0.19	0.564	o	|	|	|	|	1.94
20.667	0.00	0.19	0.563	o	|	|	|	|	1.93
20.750	0.00	0.19	0.562	o	|	|	|	|	1.93
20.833	0.00	0.19	0.560	o	|	|	|	|	1.92
20.917	0.00	0.19	0.559	o	|	|	|	|	1.92
21.000	0.00	0.19	0.558	o	|	|	|	|	1.91
21.083	0.00	0.19	0.556	o	|	|	|	|	1.91
21.167	0.00	0.19	0.555	o	|	|	|	|	1.91
21.250	0.00	0.19	0.554	o	|	|	|	|	1.90
21.333	0.00	0.19	0.553	o	|	|	|	|	1.90
21.417	0.00	0.19	0.551	o	|	|	|	|	1.89
21.500	0.00	0.19	0.550	o	|	|	|	|	1.89
21.583	0.00	0.19	0.549	o	|	|	|	|	1.89
21.667	0.00	0.19	0.547	o	|	|	|	|	1.88
21.750	0.00	0.19	0.546	o	|	|	|	|	1.88
21.833	0.00	0.19	0.545	o	|	|	|	|	1.87
21.917	0.00	0.19	0.544	o	|	|	|	|	1.87
22.000	0.00	0.18	0.542	o	|	|	|	|	1.86
22.083	0.00	0.18	0.541	o	|	|	|	|	1.86
22.167	0.00	0.18	0.540	o	|	|	|	|	1.86
22.250	0.00	0.18	0.538	o	|	|	|	|	1.85
22.333	0.00	0.18	0.537	o	|	|	|	|	1.85
22.417	0.00	0.18	0.536	o	|	|	|	|	1.84
22.500	0.00	0.18	0.535	o	|	|	|	|	1.84
22.583	0.00	0.18	0.533	o	|	|	|	|	1.84
22.667	0.00	0.18	0.532	o	|	|	|	|	1.83
22.750	0.00	0.18	0.531	o	|	|	|	|	1.83
22.833	0.00	0.18	0.530	o	|	|	|	|	1.82
22.917	0.00	0.18	0.528	o	|	|	|	|	1.82

23.000	0.00	0.18	0.527	o	|	|	|	|	1.82
23.083	0.00	0.18	0.526	o	|	|	|	|	1.81
23.167	0.00	0.18	0.525	o	|	|	|	|	1.81
23.250	0.00	0.18	0.523	o	|	|	|	|	1.80
23.333	0.00	0.18	0.522	o	|	|	|	|	1.80
23.417	0.00	0.18	0.521	o	|	|	|	|	1.80
23.500	0.00	0.18	0.520	o	|	|	|	|	1.79
23.583	0.00	0.18	0.518	o	|	|	|	|	1.79
23.667	0.00	0.18	0.517	o	|	|	|	|	1.78
23.750	0.00	0.18	0.516	o	|	|	|	|	1.78
23.833	0.00	0.18	0.515	o	|	|	|	|	1.77
23.917	0.00	0.18	0.513	o	|	|	|	|	1.77
24.000	0.00	0.18	0.512	o	|	|	|	|	1.77
24.083	0.00	0.18	0.511	o	|	|	|	|	1.76
24.167	0.00	0.18	0.510	o	|	|	|	|	1.76
24.250	0.00	0.18	0.509	o	|	|	|	|	1.75
24.333	0.00	0.18	0.507	o	|	|	|	|	1.75
24.417	0.00	0.18	0.506	o	|	|	|	|	1.75
24.500	0.00	0.18	0.505	o	|	|	|	|	1.74
24.583	0.00	0.18	0.504	o	|	|	|	|	1.74
24.667	0.00	0.18	0.502	o	|	|	|	|	1.74
24.750	0.00	0.18	0.501	o	|	|	|	|	1.73
24.833	0.00	0.18	0.500	o	|	|	|	|	1.73
24.917	0.00	0.18	0.499	o	|	|	|	|	1.72
25.000	0.00	0.18	0.498	o	|	|	|	|	1.72
25.083	0.00	0.18	0.496	o	|	|	|	|	1.72
25.167	0.00	0.18	0.495	o	|	|	|	|	1.71
25.250	0.00	0.18	0.494	o	|	|	|	|	1.71
25.333	0.00	0.18	0.493	o	|	|	|	|	1.70
25.417	0.00	0.17	0.491	o	|	|	|	|	1.70
25.500	0.00	0.17	0.490	o	|	|	|	|	1.70
25.583	0.00	0.17	0.489	o	|	|	|	|	1.69
25.667	0.00	0.17	0.488	o	|	|	|	|	1.69
25.750	0.00	0.17	0.487	o	|	|	|	|	1.68
25.833	0.00	0.17	0.485	o	|	|	|	|	1.68
25.917	0.00	0.17	0.484	o	|	|	|	|	1.68
26.000	0.00	0.17	0.483	o	|	|	|	|	1.67
26.083	0.00	0.17	0.482	o	|	|	|	|	1.67
26.167	0.00	0.17	0.481	o	|	|	|	|	1.66
26.250	0.00	0.17	0.480	o	|	|	|	|	1.66
26.333	0.00	0.17	0.478	o	|	|	|	|	1.66
26.417	0.00	0.17	0.477	o	|	|	|	|	1.65
26.500	0.00	0.17	0.476	o	|	|	|	|	1.65
26.583	0.00	0.17	0.475	o	|	|	|	|	1.65
26.667	0.00	0.17	0.474	o	|	|	|	|	1.64
26.750	0.00	0.17	0.472	o	|	|	|	|	1.64
26.833	0.00	0.17	0.471	o	|	|	|	|	1.63
26.917	0.00	0.17	0.470	o	|	|	|	|	1.63
27.000	0.00	0.17	0.469	o	|	|	|	|	1.63
27.083	0.00	0.17	0.468	o	|	|	|	|	1.62
27.167	0.00	0.17	0.467	o	|	|	|	|	1.62
27.250	0.00	0.17	0.465	o	|	|	|	|	1.61
27.333	0.00	0.17	0.464	o	|	|	|	|	1.61
27.417	0.00	0.17	0.463	o	|	|	|	|	1.61
27.500	0.00	0.17	0.462	o	|	|	|	|	1.60
27.583	0.00	0.17	0.461	o	|	|	|	|	1.60
27.667	0.00	0.17	0.460	o	|	|	|	|	1.60
27.750	0.00	0.17	0.458	o	|	|	|	|	1.59
27.833	0.00	0.17	0.457	o	|	|	|	|	1.59
27.917	0.00	0.17	0.456	o	|	|	|	|	1.58
28.000	0.00	0.17	0.455	o	|	|	|	|	1.58
28.083	0.00	0.17	0.454	o	|	|	|	|	1.58
28.167	0.00	0.17	0.453	o	|	|	|	|	1.57
28.250	0.00	0.17	0.451	o	|	|	|	|	1.57
28.333	0.00	0.17	0.450	o	|	|	|	|	1.57
28.417	0.00	0.17	0.449	o	|	|	|	|	1.56
28.500	0.00	0.17	0.448	o	|	|	|	|	1.56
28.583	0.00	0.17	0.447	o	|	|	|	|	1.55
28.667	0.00	0.17	0.446	o	|	|	|	|	1.55
28.750	0.00	0.17	0.445	o	|	|	|	|	1.55
28.833	0.00	0.17	0.443	o	|	|	|	|	1.54
28.917	0.00	0.17	0.442	o	|	|	|	|	1.54
29.000	0.00	0.17	0.441	o	|	|	|	|	1.54
29.083	0.00	0.16	0.440	o	|	|	|	|	1.53
29.167	0.00	0.16	0.439	o	|	|	|	|	1.53
29.250	0.00	0.16	0.438	o	|	|	|	|	1.53
29.333	0.00	0.16	0.437	o	|	|	|	|	1.52
29.417	0.00	0.16	0.435	o	|	|	|	|	1.52
29.500	0.00	0.16	0.434	o	|	|	|	|	1.51
29.583	0.00	0.16	0.433	o	|	|	|	|	1.51
29.667	0.00	0.16	0.432	o	|	|	|	|	1.51
29.750	0.00	0.16	0.431	o	|	|	|	|	1.50
29.833	0.00	0.16	0.430	o	|	|	|	|	1.50
29.917	0.00	0.16	0.429	o	|	|	|	|	1.50
30.000	0.00	0.16	0.428	o	|	|	|	|	1.49
30.083	0.00	0.16	0.426	o	|	|	|	|	1.49

30.167	0.00	0.16	0.425	o	|	|	|	1.48
30.250	0.00	0.16	0.424	o	|	|	|	1.48
30.333	0.00	0.16	0.423	o	|	|	|	1.48
30.417	0.00	0.16	0.422	o	|	|	|	1.47
30.500	0.00	0.16	0.421	o	|	|	|	1.47
30.583	0.00	0.16	0.420	o	|	|	|	1.47
30.667	0.00	0.16	0.419	o	|	|	|	1.46
30.750	0.00	0.16	0.418	o	|	|	|	1.46
30.833	0.00	0.16	0.416	o	|	|	|	1.46
30.917	0.00	0.16	0.415	o	|	|	|	1.45
31.000	0.00	0.16	0.414	o	|	|	|	1.45
31.083	0.00	0.16	0.413	o	|	|	|	1.45
31.167	0.00	0.16	0.412	o	|	|	|	1.44
31.250	0.00	0.16	0.411	o	|	|	|	1.44
31.333	0.00	0.16	0.410	o	|	|	|	1.43
31.417	0.00	0.16	0.409	o	|	|	|	1.43
31.500	0.00	0.16	0.408	o	|	|	|	1.43
31.583	0.00	0.16	0.407	o	|	|	|	1.42
31.667	0.00	0.16	0.405	o	|	|	|	1.42
31.750	0.00	0.16	0.404	o	|	|	|	1.42
31.833	0.00	0.16	0.403	o	|	|	|	1.41
31.917	0.00	0.16	0.402	o	|	|	|	1.41
32.000	0.00	0.16	0.401	o	|	|	|	1.41
32.083	0.00	0.16	0.400	o	|	|	|	1.40
32.167	0.00	0.16	0.399	o	|	|	|	1.40
32.250	0.00	0.16	0.398	o	|	|	|	1.40
32.333	0.00	0.16	0.397	o	|	|	|	1.39
32.417	0.00	0.16	0.396	o	|	|	|	1.39
32.500	0.00	0.16	0.395	o	|	|	|	1.39
32.583	0.00	0.16	0.394	o	|	|	|	1.38
32.667	0.00	0.16	0.393	o	|	|	|	1.38
32.750	0.00	0.16	0.391	o	|	|	|	1.37
32.833	0.00	0.16	0.390	o	|	|	|	1.37
32.917	0.00	0.16	0.389	o	|	|	|	1.37
33.000	0.00	0.15	0.388	o	|	|	|	1.36
33.083	0.00	0.15	0.387	o	|	|	|	1.36
33.167	0.00	0.15	0.386	o	|	|	|	1.36
33.250	0.00	0.15	0.385	o	|	|	|	1.35
33.333	0.00	0.15	0.384	o	|	|	|	1.35
33.417	0.00	0.15	0.383	o	|	|	|	1.35
33.500	0.00	0.15	0.382	o	|	|	|	1.34
33.583	0.00	0.15	0.381	o	|	|	|	1.34
33.667	0.00	0.15	0.380	o	|	|	|	1.34
33.750	0.00	0.15	0.379	o	|	|	|	1.33
33.833	0.00	0.15	0.378	o	|	|	|	1.33
33.917	0.00	0.15	0.377	o	|	|	|	1.33
34.000	0.00	0.15	0.376	o	|	|	|	1.32
34.083	0.00	0.15	0.374	o	|	|	|	1.32
34.167	0.00	0.15	0.373	o	|	|	|	1.32
34.250	0.00	0.15	0.372	o	|	|	|	1.31
34.333	0.00	0.15	0.371	o	|	|	|	1.31
34.417	0.00	0.15	0.370	o	|	|	|	1.31
34.500	0.00	0.15	0.369	o	|	|	|	1.30
34.583	0.00	0.15	0.368	o	|	|	|	1.30
34.667	0.00	0.15	0.367	o	|	|	|	1.30
34.750	0.00	0.15	0.366	o	|	|	|	1.29
34.833	0.00	0.15	0.365	o	|	|	|	1.29
34.917	0.00	0.15	0.364	o	|	|	|	1.29
35.000	0.00	0.15	0.363	o	|	|	|	1.28
35.083	0.00	0.15	0.362	o	|	|	|	1.28
35.167	0.00	0.15	0.361	o	|	|	|	1.28
35.250	0.00	0.15	0.360	o	|	|	|	1.27
35.333	0.00	0.15	0.359	o	|	|	|	1.27
35.417	0.00	0.15	0.358	o	|	|	|	1.27
35.500	0.00	0.15	0.357	o	|	|	|	1.26
35.583	0.00	0.15	0.356	o	|	|	|	1.26
35.667	0.00	0.15	0.355	o	|	|	|	1.26
35.750	0.00	0.15	0.354	o	|	|	|	1.25
35.833	0.00	0.15	0.353	o	|	|	|	1.25
35.917	0.00	0.15	0.352	o	|	|	|	1.25
36.000	0.00	0.15	0.351	o	|	|	|	1.24
36.083	0.00	0.15	0.350	o	|	|	|	1.24
36.167	0.00	0.15	0.349	o	|	|	|	1.24
36.250	0.00	0.15	0.348	o	|	|	|	1.23
36.333	0.00	0.15	0.347	o	|	|	|	1.23
36.417	0.00	0.15	0.346	o	|	|	|	1.23
36.500	0.00	0.15	0.345	o	|	|	|	1.22
36.583	0.00	0.15	0.344	o	|	|	|	1.22
36.667	0.00	0.15	0.343	o	|	|	|	1.22
36.750	0.00	0.15	0.342	o	|	|	|	1.21
36.833	0.00	0.15	0.341	o	|	|	|	1.21
36.917	0.00	0.15	0.340	o	|	|	|	1.21
37.000	0.00	0.15	0.339	o	|	|	|	1.20
37.083	0.00	0.15	0.338	o	|	|	|	1.20
37.167	0.00	0.14	0.337	o	|	|	|	1.20
37.250	0.00	0.14	0.336	o	|	|	|	1.19

37.333	0.00	0.14	0.335	o	|	|	|	|	1.19
37.417	0.00	0.14	0.334	o	|	|	|	|	1.19
37.500	0.00	0.14	0.333	o	|	|	|	|	1.18
37.583	0.00	0.14	0.332	o	|	|	|	|	1.18
37.667	0.00	0.14	0.331	o	|	|	|	|	1.18
37.750	0.00	0.14	0.330	o	|	|	|	|	1.17
37.833	0.00	0.14	0.329	o	|	|	|	|	1.17
37.917	0.00	0.14	0.328	o	|	|	|	|	1.17
38.000	0.00	0.14	0.327	o	|	|	|	|	1.16
38.083	0.00	0.14	0.326	o	|	|	|	|	1.16
38.167	0.00	0.14	0.325	o	|	|	|	|	1.16
38.250	0.00	0.14	0.324	o	|	|	|	|	1.16
38.333	0.00	0.14	0.323	o	|	|	|	|	1.15
38.417	0.00	0.14	0.322	o	|	|	|	|	1.15
38.500	0.00	0.14	0.321	o	|	|	|	|	1.15
38.583	0.00	0.14	0.320	o	|	|	|	|	1.14
38.667	0.00	0.14	0.319	o	|	|	|	|	1.14
38.750	0.00	0.14	0.318	o	|	|	|	|	1.14
38.833	0.00	0.14	0.317	o	|	|	|	|	1.13
38.917	0.00	0.14	0.316	o	|	|	|	|	1.13
39.000	0.00	0.14	0.315	o	|	|	|	|	1.13
39.083	0.00	0.14	0.314	o	|	|	|	|	1.12
39.167	0.00	0.14	0.313	o	|	|	|	|	1.12
39.250	0.00	0.14	0.312	o	|	|	|	|	1.12
39.333	0.00	0.14	0.311	o	|	|	|	|	1.11
39.417	0.00	0.14	0.310	o	|	|	|	|	1.11
39.500	0.00	0.14	0.309	o	|	|	|	|	1.11
39.583	0.00	0.14	0.308	o	|	|	|	|	1.10
39.667	0.00	0.14	0.307	o	|	|	|	|	1.10
39.750	0.00	0.14	0.306	o	|	|	|	|	1.10
39.833	0.00	0.14	0.305	o	|	|	|	|	1.10
39.917	0.00	0.14	0.304	o	|	|	|	|	1.09
40.000	0.00	0.14	0.304	o	|	|	|	|	1.09
40.083	0.00	0.14	0.303	o	|	|	|	|	1.09
40.167	0.00	0.14	0.302	o	|	|	|	|	1.08
40.250	0.00	0.14	0.301	o	|	|	|	|	1.08
40.333	0.00	0.14	0.300	o	|	|	|	|	1.08
40.417	0.00	0.14	0.299	o	|	|	|	|	1.07
40.500	0.00	0.14	0.298	o	|	|	|	|	1.07
40.583	0.00	0.14	0.297	o	|	|	|	|	1.07
40.667	0.00	0.14	0.296	o	|	|	|	|	1.06
40.750	0.00	0.14	0.295	o	|	|	|	|	1.06
40.833	0.00	0.14	0.294	o	|	|	|	|	1.06
40.917	0.00	0.14	0.293	o	|	|	|	|	1.06
41.000	0.00	0.14	0.292	o	|	|	|	|	1.05
41.083	0.00	0.14	0.291	o	|	|	|	|	1.05
41.167	0.00	0.14	0.290	o	|	|	|	|	1.05
41.250	0.00	0.14	0.289	o	|	|	|	|	1.04
41.333	0.00	0.14	0.288	o	|	|	|	|	1.04
41.417	0.00	0.14	0.288	o	|	|	|	|	1.04
41.500	0.00	0.14	0.287	o	|	|	|	|	1.03
41.583	0.00	0.13	0.286	o	|	|	|	|	1.03
41.667	0.00	0.13	0.285	o	|	|	|	|	1.03
41.750	0.00	0.13	0.284	o	|	|	|	|	1.03
41.833	0.00	0.13	0.283	o	|	|	|	|	1.02
41.917	0.00	0.13	0.282	o	|	|	|	|	1.02
42.000	0.00	0.13	0.281	o	|	|	|	|	1.02
42.083	0.00	0.13	0.280	o	|	|	|	|	1.01
42.167	0.00	0.13	0.279	o	|	|	|	|	1.01
42.250	0.00	0.13	0.278	o	|	|	|	|	1.01
42.333	0.00	0.13	0.277	o	|	|	|	|	1.00
42.417	0.00	0.13	0.276	o	|	|	|	|	1.00
42.500	0.00	0.13	0.275	o	|	|	|	|	1.00
42.583	0.00	0.13	0.275	o	|	|	|	|	0.99
42.667	0.00	0.13	0.274	o	|	|	|	|	0.99
42.750	0.00	0.13	0.273	o	|	|	|	|	0.99
42.833	0.00	0.13	0.272	o	|	|	|	|	0.99
42.917	0.00	0.13	0.271	o	|	|	|	|	0.98
43.000	0.00	0.13	0.270	o	|	|	|	|	0.98
43.083	0.00	0.13	0.269	o	|	|	|	|	0.98
43.167	0.00	0.13	0.268	o	|	|	|	|	0.97
43.250	0.00	0.13	0.267	o	|	|	|	|	0.97
43.333	0.00	0.13	0.267	o	|	|	|	|	0.97
43.417	0.00	0.13	0.266	o	|	|	|	|	0.96
43.500	0.00	0.13	0.265	o	|	|	|	|	0.96
43.583	0.00	0.13	0.264	o	|	|	|	|	0.96
43.667	0.00	0.13	0.263	o	|	|	|	|	0.95
43.750	0.00	0.13	0.262	o	|	|	|	|	0.95
43.833	0.00	0.13	0.261	o	|	|	|	|	0.95
43.917	0.00	0.13	0.260	o	|	|	|	|	0.94
44.000	0.00	0.13	0.260	o	|	|	|	|	0.94
44.083	0.00	0.12	0.259	o	|	|	|	|	0.94
44.167	0.00	0.12	0.258	o	|	|	|	|	0.93
44.250	0.00	0.12	0.257	o	|	|	|	|	0.93
44.333	0.00	0.12	0.256	o	|	|	|	|	0.93
44.417	0.00	0.12	0.255	o	|	|	|	|	0.92

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44.500    0.00    0.12      0.254  o       |       |       |       |     0.92
44.583    0.00    0.12      0.254  o       |       |       |       |     0.92
44.667    0.00    0.12      0.253  o       |       |       |       |     0.92
44.750    0.00    0.12      0.252  o       |       |       |       |     0.91
44.833    0.00    0.12      0.251  o       |       |       |       |     0.91
44.917    0.00    0.12      0.250  o       |       |       |       |     0.91
45.000    0.00    0.12      0.249  o       |       |       |       |     0.90
45.083    0.00    0.12      0.249  o       |       |       |       |     0.90
45.167    0.00    0.12      0.248  o       |       |       |       |     0.90
45.250    0.00    0.12      0.247  o       |       |       |       |     0.89
45.333    0.00    0.12      0.246  o       |       |       |       |     0.89
45.417    0.00    0.12      0.245  o       |       |       |       |     0.89
45.500    0.00    0.12      0.244  o       |       |       |       |     0.89
45.583    0.00    0.12      0.244  o       |       |       |       |     0.88
45.667    0.00    0.12      0.243  o       |       |       |       |     0.88
45.750    0.00    0.12      0.242  o       |       |       |       |     0.88
45.833    0.00    0.12      0.241  o       |       |       |       |     0.87
45.917    0.00    0.12      0.240  o       |       |       |       |     0.87
46.000    0.00    0.12      0.240  o       |       |       |       |     0.87
46.083    0.00    0.12      0.239  o       |       |       |       |     0.87
46.167    0.00    0.11      0.238  o       |       |       |       |     0.86
46.250    0.00    0.11      0.237  o       |       |       |       |     0.86
46.333    0.00    0.11      0.236  o       |       |       |       |     0.86
46.417    0.00    0.11      0.236  o       |       |       |       |     0.85
46.500    0.00    0.11      0.235  o       |       |       |       |     0.85
46.583    0.00    0.11      0.234  o       |       |       |       |     0.85
46.667    0.00    0.11      0.233  o       |       |       |       |     0.85
46.750    0.00    0.11      0.233  o       |       |       |       |     0.84
46.833    0.00    0.11      0.232  o       |       |       |       |     0.84
46.917    0.00    0.11      0.231  o       |       |       |       |     0.84
47.000    0.00    0.11      0.230  o       |       |       |       |     0.83
47.083    0.00    0.11      0.230  o       |       |       |       |     0.83
47.167    0.00    0.11      0.229  o       |       |       |       |     0.83
47.250    0.00    0.11      0.228  o       |       |       |       |     0.83
47.333    0.00    0.11      0.227  o       |       |       |       |     0.82
47.417    0.00    0.11      0.227  o       |       |       |       |     0.82
47.500    0.00    0.11      0.226  o       |       |       |       |     0.82
47.583    0.00    0.11      0.225  o       |       |       |       |     0.82
47.667    0.00    0.11      0.224  o       |       |       |       |     0.81
47.750    0.00    0.11      0.224  o       |       |       |       |     0.81
47.833    0.00    0.11      0.223  o       |       |       |       |     0.81
47.917    0.00    0.11      0.222  o       |       |       |       |     0.80
48.000    0.00    0.11      0.221  o       |       |       |       |     0.80
48.083    0.00    0.11      0.221  o       |       |       |       |     0.80
48.167    0.00    0.11      0.220  o       |       |       |       |     0.80
48.250    0.00    0.11      0.219  o       |       |       |       |     0.79
48.333    0.00    0.11      0.218  o       |       |       |       |     0.79
48.417    0.00    0.10      0.218  o       |       |       |       |     0.79
48.500    0.00    0.10      0.217  o       |       |       |       |     0.79
48.583    0.00    0.10      0.216  o       |       |       |       |     0.78
48.667    0.00    0.10      0.216  o       |       |       |       |     0.78
48.750    0.00    0.10      0.215  o       |       |       |       |     0.78
48.833    0.00    0.10      0.214  o       |       |       |       |     0.78
48.917    0.00    0.10      0.213  o       |       |       |       |     0.77
49.000    0.00    0.10      0.213  o       |       |       |       |     0.77
49.083    0.00    0.10      0.212  o       |       |       |       |     0.77
49.167    0.00    0.10      0.211  o       |       |       |       |     0.77
49.250    0.00    0.10      0.211  o       |       |       |       |     0.76
49.333    0.00    0.10      0.210  o       |       |       |       |     0.76
49.417    0.00    0.10      0.209  o       |       |       |       |     0.76
49.500    0.00    0.10      0.208  o       |       |       |       |     0.76
49.583    0.00    0.10      0.208  o       |       |       |       |     0.75
49.667    0.00    0.10      0.207  o       |       |       |       |     0.75
      Remaining water in basin =    0.21 (Ac.Ft)
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =   596
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =        0.989 (CFS)
                  Total volume =       1.283 (Ac.Ft)
            Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
      ******************************************************************************

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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 05/07/25

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: PRO10310.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    40
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       27.216 (CFS)
               Total volume =       1.911 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
____________________________________________________________________________

User entry of depth-outflow-storage data
------------------------------------------------------------------------
Total number of inflow hydrograph intervals = 40
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
------------------------------------------------------------------------
------------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
------------------------------------------------------------------------
------------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
------------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.276      0.133      0.276        0.276
   2.000      0.584      0.193      0.583        0.585
   3.000      0.930      0.700      0.928        0.932
   3.500      1.118      0.824      1.115        1.121
   4.000      1.316      0.930      1.313        1.319
   4.500      1.528      1.024      1.524        1.532
   4.750      1.637      1.068      1.633        1.641
   5.000      1.749     18.283      1.686        1.812
   6.000      2.231    253.655      1.358        3.104
------------------------------------------------------------------------
               Hydrograph Detention Basin Routing
------------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
------------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                    Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0       6.8   13.61   20.41   27.22 (Ft.)
 0.083    1.18    0.00      0.004  OI      |       |       |       |     0.01
 0.167    2.46    0.01      0.017  O I     |       |       |       |     0.06
 0.250    2.55    0.02      0.034  O  I    |       |       |       |     0.12
 0.333    2.83    0.03      0.052  O  I    |       |       |       |     0.19
 0.417    3.23    0.04      0.073  O  I    |       |       |       |     0.26
 0.500    3.57    0.05      0.096  O   I   |       |       |       |     0.35
 0.583    3.62    0.06      0.120  O   I   |       |       |       |     0.44
 0.667    3.67    0.07      0.145  O   I   |       |       |       |     0.53
 0.750    3.93    0.08      0.171  O   I   |       |       |       |     0.62
 0.833    3.71    0.09      0.196  O   I   |       |       |       |     0.71
 0.917    3.52    0.11      0.221  O   I   |       |       |       |     0.80
 1.000    3.74    0.12      0.245  O   I   |       |       |       |     0.89
 1.083    4.30    0.13      0.272  O    I  |       |       |       |     0.98
 1.167    4.73    0.14      0.302  O    I  |       |       |       |     1.08
 1.250    4.84    0.14      0.334  O    I  |       |       |       |     1.19
 1.333    4.70    0.15      0.366  O    I  |       |       |       |     1.29
 1.417    5.06    0.16      0.398  O    I  |       |       |       |     1.40
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1.500	5.75	0.16	0.434	O	I	|	|	|	1.51
1.583	5.69	0.17	0.473	O	I	|	|	|	1.64
1.667	5.74	0.18	0.511	O	I	|	|	|	1.76
1.750	7.14	0.19	0.554	O	I	|	|	|	1.90
1.833	8.02	0.22	0.605	O	|I	|	|	|	2.06
1.917	7.53	0.30	0.656	O	I	|	|	|	2.21
2.000	7.34	0.37	0.705	O	I	|	|	|	2.35
2.083	7.65	0.44	0.754	O	I	|	|	|	2.49
2.167	9.83	0.53	0.811	O	| I	|	|	|	2.66
2.250	13.50	0.64	0.887	O	| I	|	|	|	2.88
2.333	12.85	0.73	0.973	O	| I	|	|	|	3.12
2.417	16.39	0.79	1.069	O	| I	|	|	|	3.37
2.500	23.41	0.87	1.200	|O	|	| I	|	3.71
2.583	27.22	0.95	1.368	|O	|	|	| I	4.12
2.667	25.49	1.03	1.543	|O	|	| I	|	4.53
2.750	15.16	4.95	1.662	| O	|	|I	|	4.81
2.833	7.13	9.24	1.690	| I O	|	|	|	4.87
2.917	5.11	7.08	1.676	| I O	|	|	|	4.84
3.000	3.20	5.05	1.663	| I O	|	|	|	4.81
3.083	1.20	3.08	1.650	|I O	|	|	|	4.78
3.167	0.34	1.48	1.640	IO	|	|	|	|	4.76
3.250	0.12	1.07	1.632	IO	|	|	|	|	4.74
3.333	0.02	1.06	1.626	IO	|	|	|	|	4.72
3.417	0.00	1.06	1.618	IO	|	|	|	|	4.71
3.500	0.00	1.06	1.611	IO	|	|	|	|	4.69
3.583	0.00	1.05	1.604	IO	|	|	|	|	4.67
3.667	0.00	1.05	1.597	IO	|	|	|	|	4.66
3.750	0.00	1.05	1.589	IO	|	|	|	|	4.64
3.833	0.00	1.05	1.582	IO	|	|	|	|	4.62
3.917	0.00	1.04	1.575	IO	|	|	|	|	4.61
4.000	0.00	1.04	1.568	IO	|	|	|	|	4.59
4.083	0.00	1.04	1.561	IO	|	|	|	|	4.57
4.167	0.00	1.03	1.553	IO	|	|	|	|	4.56
4.250	0.00	1.03	1.546	IO	|	|	|	|	4.54
4.333	0.00	1.03	1.539	IO	|	|	|	|	4.53
4.417	0.00	1.03	1.532	IO	|	|	|	|	4.51
4.500	0.00	1.02	1.525	IO	|	|	|	|	4.49
4.583	0.00	1.02	1.518	IO	|	|	|	|	4.48
4.667	0.00	1.02	1.511	IO	|	|	|	|	4.46
4.750	0.00	1.01	1.504	IO	|	|	|	|	4.44
4.833	0.00	1.01	1.497	IO	|	|	|	|	4.43
4.917	0.00	1.01	1.490	IO	|	|	|	|	4.41
5.000	0.00	1.00	1.483	IO	|	|	|	|	4.39
5.083	0.00	1.00	1.476	IO	|	|	|	|	4.38
5.167	0.00	1.00	1.469	IO	|	|	|	|	4.36
5.250	0.00	1.00	1.463	IO	|	|	|	|	4.35
5.333	0.00	0.99	1.456	IO	|	|	|	|	4.33
5.417	0.00	0.99	1.449	IO	|	|	|	|	4.31
5.500	0.00	0.99	1.442	IO	|	|	|	|	4.30
5.583	0.00	0.98	1.435	IO	|	|	|	|	4.28
5.667	0.00	0.98	1.429	IO	|	|	|	|	4.27
5.750	0.00	0.98	1.422	IO	|	|	|	|	4.25
5.833	0.00	0.97	1.415	IO	|	|	|	|	4.23
5.917	0.00	0.97	1.408	IO	|	|	|	|	4.22
6.000	0.00	0.97	1.402	IO	|	|	|	|	4.20
6.083	0.00	0.97	1.395	IO	|	|	|	|	4.19
6.167	0.00	0.96	1.388	IO	|	|	|	|	4.17
6.250	0.00	0.96	1.382	IO	|	|	|	|	4.16
6.333	0.00	0.96	1.375	IO	|	|	|	|	4.14
6.417	0.00	0.95	1.369	IO	|	|	|	|	4.12
6.500	0.00	0.95	1.362	IO	|	|	|	|	4.11
6.583	0.00	0.95	1.356	IO	|	|	|	|	4.09
6.667	0.00	0.94	1.349	IO	|	|	|	|	4.08
6.750	0.00	0.94	1.343	IO	|	|	|	|	4.06
6.833	0.00	0.94	1.336	IO	|	|	|	|	4.05
6.917	0.00	0.94	1.330	IO	|	|	|	|	4.03
7.000	0.00	0.93	1.323	IO	|	|	|	|	4.02
7.083	0.00	0.93	1.317	IO	|	|	|	|	4.00
7.167	0.00	0.93	1.310	IO	|	|	|	|	3.99
7.250	0.00	0.92	1.304	IO	|	|	|	|	3.97
7.333	0.00	0.92	1.298	IO	|	|	|	|	3.95
7.417	0.00	0.92	1.291	IO	|	|	|	|	3.94
7.500	0.00	0.91	1.285	IO	|	|	|	|	3.92
7.583	0.00	0.91	1.279	IO	|	|	|	|	3.91
7.667	0.00	0.91	1.273	IO	|	|	|	|	3.89
7.750	0.00	0.90	1.266	IO	|	|	|	|	3.87
7.833	0.00	0.90	1.260	IO	|	|	|	|	3.86
7.917	0.00	0.90	1.254	IO	|	|	|	|	3.84
8.000	0.00	0.89	1.248	IO	|	|	|	|	3.83
8.083	0.00	0.89	1.242	IO	|	|	|	|	3.81
8.167	0.00	0.89	1.235	IO	|	|	|	|	3.80
8.250	0.00	0.88	1.229	IO	|	|	|	|	3.78
8.333	0.00	0.88	1.223	IO	|	|	|	|	3.77
8.417	0.00	0.88	1.217	IO	|	|	|	|	3.75
8.500	0.00	0.87	1.211	IO	|	|	|	|	3.74
8.583	0.00	0.87	1.205	IO	|	|	|	|	3.72

8.667	0.00	0.87	1.199	IO	|	|	|	3.71
8.750	0.00	0.86	1.193	IO	|	|	|	3.69
8.833	0.00	0.86	1.187	IO	|	|	|	3.68
8.917	0.00	0.86	1.181	IO	|	|	|	3.66
9.000	0.00	0.85	1.176	IO	|	|	|	3.65
9.083	0.00	0.85	1.170	IO	|	|	|	3.63
9.167	0.00	0.85	1.164	O	|	|	|	3.62
9.250	0.00	0.85	1.158	O	|	|	|	3.60
9.333	0.00	0.84	1.152	O	|	|	|	3.59
9.417	0.00	0.84	1.146	O	|	|	|	3.57
9.500	0.00	0.84	1.141	O	|	|	|	3.56
9.583	0.00	0.83	1.135	O	|	|	|	3.54
9.667	0.00	0.83	1.129	O	|	|	|	3.53
9.750	0.00	0.83	1.123	O	|	|	|	3.51
9.833	0.00	0.82	1.118	O	|	|	|	3.50
9.917	0.00	0.82	1.112	O	|	|	|	3.48
10.000	0.00	0.82	1.106	O	|	|	|	3.47
10.083	0.00	0.81	1.101	O	|	|	|	3.45
10.167	0.00	0.81	1.095	O	|	|	|	3.44
10.250	0.00	0.81	1.090	O	|	|	|	3.42
10.333	0.00	0.80	1.084	O	|	|	|	3.41
10.417	0.00	0.80	1.079	O	|	|	|	3.40
10.500	0.00	0.79	1.073	O	|	|	|	3.38
10.583	0.00	0.79	1.068	O	|	|	|	3.37
10.667	0.00	0.79	1.062	O	|	|	|	3.35
10.750	0.00	0.78	1.057	O	|	|	|	3.34
10.833	0.00	0.78	1.051	O	|	|	|	3.32
10.917	0.00	0.78	1.046	O	|	|	|	3.31
11.000	0.00	0.77	1.041	O	|	|	|	3.29
11.083	0.00	0.77	1.035	O	|	|	|	3.28
11.167	0.00	0.77	1.030	O	|	|	|	3.27
11.250	0.00	0.76	1.025	O	|	|	|	3.25
11.333	0.00	0.76	1.020	O	|	|	|	3.24
11.417	0.00	0.76	1.014	O	|	|	|	3.22
11.500	0.00	0.75	1.009	O	|	|	|	3.21
11.583	0.00	0.75	1.004	O	|	|	|	3.20
11.667	0.00	0.75	0.999	O	|	|	|	3.18
11.750	0.00	0.74	0.994	O	|	|	|	3.17
11.833	0.00	0.74	0.989	O	|	|	|	3.16
11.917	0.00	0.74	0.984	O	|	|	|	3.14
12.000	0.00	0.73	0.979	O	|	|	|	3.13
12.083	0.00	0.73	0.974	O	|	|	|	3.12
12.167	0.00	0.73	0.969	O	|	|	|	3.10
12.250	0.00	0.72	0.964	O	|	|	|	3.09
12.333	0.00	0.72	0.959	O	|	|	|	3.08
12.417	0.00	0.72	0.954	O	|	|	|	3.06
12.500	0.00	0.71	0.949	O	|	|	|	3.05
12.583	0.00	0.71	0.944	O	|	|	|	3.04
12.667	0.00	0.71	0.939	O	|	|	|	3.02
12.750	0.00	0.70	0.934	O	|	|	|	3.01
12.833	0.00	0.70	0.929	O	|	|	|	3.00
12.917	0.00	0.69	0.924	O	|	|	|	2.98
13.000	0.00	0.68	0.920	O	|	|	|	2.97
13.083	0.00	0.68	0.915	O	|	|	|	2.96
13.167	0.00	0.67	0.910	O	|	|	|	2.94
13.250	0.00	0.66	0.906	O	|	|	|	2.93
13.333	0.00	0.66	0.901	O	|	|	|	2.92
13.417	0.00	0.65	0.897	O	|	|	|	2.90
13.500	0.00	0.64	0.892	O	|	|	|	2.89
13.583	0.00	0.64	0.888	O	|	|	|	2.88
13.667	0.00	0.63	0.883	O	|	|	|	2.87
13.750	0.00	0.63	0.879	O	|	|	|	2.85
13.833	0.00	0.62	0.875	O	|	|	|	2.84
13.917	0.00	0.61	0.871	O	|	|	|	2.83
14.000	0.00	0.61	0.866	O	|	|	|	2.82
14.083	0.00	0.60	0.862	O	|	|	|	2.80
14.167	0.00	0.59	0.858	O	|	|	|	2.79
14.250	0.00	0.59	0.854	O	|	|	|	2.78
14.333	0.00	0.58	0.850	O	|	|	|	2.77
14.417	0.00	0.58	0.846	O	|	|	|	2.76
14.500	0.00	0.57	0.842	O	|	|	|	2.75
14.583	0.00	0.57	0.838	O	|	|	|	2.73
14.667	0.00	0.56	0.834	O	|	|	|	2.72
14.750	0.00	0.55	0.830	O	|	|	|	2.71
14.833	0.00	0.55	0.827	O	|	|	|	2.70
14.917	0.00	0.54	0.823	O	|	|	|	2.69
15.000	0.00	0.54	0.819	O	|	|	|	2.68
15.083	0.00	0.53	0.816	O	|	|	|	2.67
15.167	0.00	0.53	0.812	O	|	|	|	2.66
15.250	0.00	0.52	0.808	O	|	|	|	2.65
15.333	0.00	0.52	0.805	O	|	|	|	2.64
15.417	0.00	0.51	0.801	O	|	|	|	2.63
15.500	0.00	0.51	0.798	O	|	|	|	2.62
15.583	0.00	0.50	0.794	O	|	|	|	2.61
15.667	0.00	0.50	0.791	O	|	|	|	2.60
15.750	0.00	0.49	0.787	O	|	|	|	2.59

15.833	0.00	0.49	0.784	o	|	|	|	2.58
15.917	0.00	0.48	0.781	o	|	|	|	2.57
16.000	0.00	0.48	0.777	o	|	|	|	2.56
16.083	0.00	0.47	0.774	o	|	|	|	2.55
16.167	0.00	0.47	0.771	o	|	|	|	2.54
16.250	0.00	0.46	0.768	o	|	|	|	2.53
16.333	0.00	0.46	0.764	o	|	|	|	2.52
16.417	0.00	0.45	0.761	o	|	|	|	2.51
16.500	0.00	0.45	0.758	o	|	|	|	2.50
16.583	0.00	0.44	0.755	o	|	|	|	2.49
16.667	0.00	0.44	0.752	o	|	|	|	2.49
16.750	0.00	0.43	0.749	o	|	|	|	2.48
16.833	0.00	0.43	0.746	o	|	|	|	2.47
16.917	0.00	0.43	0.743	o	|	|	|	2.46
17.000	0.00	0.42	0.740	o	|	|	|	2.45
17.083	0.00	0.42	0.737	o	|	|	|	2.44
17.167	0.00	0.41	0.735	o	|	|	|	2.44
17.250	0.00	0.41	0.732	o	|	|	|	2.43
17.333	0.00	0.41	0.729	o	|	|	|	2.42
17.417	0.00	0.40	0.726	o	|	|	|	2.41
17.500	0.00	0.40	0.723	o	|	|	|	2.40
17.583	0.00	0.39	0.721	o	|	|	|	2.39
17.667	0.00	0.39	0.718	o	|	|	|	2.39
17.750	0.00	0.39	0.715	o	|	|	|	2.38
17.833	0.00	0.38	0.713	o	|	|	|	2.37
17.917	0.00	0.38	0.710	o	|	|	|	2.36
18.000	0.00	0.37	0.707	o	|	|	|	2.36
18.083	0.00	0.37	0.705	o	|	|	|	2.35
18.167	0.00	0.37	0.702	o	|	|	|	2.34
18.250	0.00	0.36	0.700	o	|	|	|	2.33
18.333	0.00	0.36	0.697	o	|	|	|	2.33
18.417	0.00	0.36	0.695	o	|	|	|	2.32
18.500	0.00	0.35	0.692	o	|	|	|	2.31
18.583	0.00	0.35	0.690	o	|	|	|	2.31
18.667	0.00	0.34	0.688	o	|	|	|	2.30
18.750	0.00	0.34	0.685	o	|	|	|	2.29
18.833	0.00	0.34	0.683	o	|	|	|	2.29
18.917	0.00	0.33	0.681	o	|	|	|	2.28
19.000	0.00	0.33	0.678	o	|	|	|	2.27
19.083	0.00	0.33	0.676	o	|	|	|	2.27
19.167	0.00	0.32	0.674	o	|	|	|	2.26
19.250	0.00	0.32	0.672	o	|	|	|	2.25
19.333	0.00	0.32	0.669	o	|	|	|	2.25
19.417	0.00	0.31	0.667	o	|	|	|	2.24
19.500	0.00	0.31	0.665	o	|	|	|	2.23
19.583	0.00	0.31	0.663	o	|	|	|	2.23
19.667	0.00	0.31	0.661	o	|	|	|	2.22
19.750	0.00	0.30	0.659	o	|	|	|	2.22
19.833	0.00	0.30	0.657	o	|	|	|	2.21
19.917	0.00	0.30	0.655	o	|	|	|	2.20
20.000	0.00	0.29	0.653	o	|	|	|	2.20
20.083	0.00	0.29	0.651	o	|	|	|	2.19
20.167	0.00	0.29	0.649	o	|	|	|	2.19
20.250	0.00	0.28	0.647	o	|	|	|	2.18
20.333	0.00	0.28	0.645	o	|	|	|	2.18
20.417	0.00	0.28	0.643	o	|	|	|	2.17
20.500	0.00	0.28	0.641	o	|	|	|	2.16
20.583	0.00	0.27	0.639	o	|	|	|	2.16
20.667	0.00	0.27	0.637	o	|	|	|	2.15
20.750	0.00	0.27	0.635	o	|	|	|	2.15
20.833	0.00	0.27	0.633	o	|	|	|	2.14
20.917	0.00	0.26	0.632	o	|	|	|	2.14
21.000	0.00	0.26	0.630	o	|	|	|	2.13
21.083	0.00	0.26	0.628	o	|	|	|	2.13
21.167	0.00	0.25	0.626	o	|	|	|	2.12
21.250	0.00	0.25	0.624	o	|	|	|	2.12
21.333	0.00	0.25	0.623	o	|	|	|	2.11
21.417	0.00	0.25	0.621	o	|	|	|	2.11
21.500	0.00	0.24	0.619	o	|	|	|	2.10
21.583	0.00	0.24	0.618	o	|	|	|	2.10
21.667	0.00	0.24	0.616	o	|	|	|	2.09
21.750	0.00	0.24	0.614	o	|	|	|	2.09
21.833	0.00	0.24	0.613	o	|	|	|	2.08
21.917	0.00	0.23	0.611	o	|	|	|	2.08
22.000	0.00	0.23	0.609	o	|	|	|	2.07
22.083	0.00	0.23	0.608	o	|	|	|	2.07
22.167	0.00	0.23	0.606	o	|	|	|	2.06
22.250	0.00	0.22	0.605	o	|	|	|	2.06
22.333	0.00	0.22	0.603	o	|	|	|	2.06
22.417	0.00	0.22	0.602	o	|	|	|	2.05
22.500	0.00	0.22	0.600	o	|	|	|	2.05
22.583	0.00	0.21	0.599	o	|	|	|	2.04
22.667	0.00	0.21	0.597	o	|	|	|	2.04
22.750	0.00	0.21	0.596	o	|	|	|	2.03
22.833	0.00	0.21	0.594	o	|	|	|	2.03
22.917	0.00	0.21	0.593	o	|	|	|	2.03

23.000	0.00	0.20	0.592	o	|	|	|	|	2.02
23.083	0.00	0.20	0.590	o	|	|	|	|	2.02
23.167	0.00	0.20	0.589	o	|	|	|	|	2.01
23.250	0.00	0.20	0.587	o	|	|	|	|	2.01
23.333	0.00	0.20	0.586	o	|	|	|	|	2.01
23.417	0.00	0.19	0.585	o	|	|	|	|	2.00
23.500	0.00	0.19	0.583	o	|	|	|	|	2.00
23.583	0.00	0.19	0.582	o	|	|	|	|	1.99
23.667	0.00	0.19	0.581	o	|	|	|	|	1.99
23.750	0.00	0.19	0.579	o	|	|	|	|	1.99
23.833	0.00	0.19	0.578	o	|	|	|	|	1.98
23.917	0.00	0.19	0.577	o	|	|	|	|	1.98
24.000	0.00	0.19	0.575	o	|	|	|	|	1.97
24.083	0.00	0.19	0.574	o	|	|	|	|	1.97
24.167	0.00	0.19	0.573	o	|	|	|	|	1.96
24.250	0.00	0.19	0.571	o	|	|	|	|	1.96
24.333	0.00	0.19	0.570	o	|	|	|	|	1.96
24.417	0.00	0.19	0.569	o	|	|	|	|	1.95
24.500	0.00	0.19	0.568	o	|	|	|	|	1.95
24.583	0.00	0.19	0.566	o	|	|	|	|	1.94
24.667	0.00	0.19	0.565	o	|	|	|	|	1.94
24.750	0.00	0.19	0.564	o	|	|	|	|	1.93
24.833	0.00	0.19	0.562	o	|	|	|	|	1.93
24.917	0.00	0.19	0.561	o	|	|	|	|	1.93
25.000	0.00	0.19	0.560	o	|	|	|	|	1.92
25.083	0.00	0.19	0.558	o	|	|	|	|	1.92
25.167	0.00	0.19	0.557	o	|	|	|	|	1.91
25.250	0.00	0.19	0.556	o	|	|	|	|	1.91
25.333	0.00	0.19	0.555	o	|	|	|	|	1.90
25.417	0.00	0.19	0.553	o	|	|	|	|	1.90
25.500	0.00	0.19	0.552	o	|	|	|	|	1.90
25.583	0.00	0.19	0.551	o	|	|	|	|	1.89
25.667	0.00	0.19	0.549	o	|	|	|	|	1.89
25.750	0.00	0.19	0.548	o	|	|	|	|	1.88
25.833	0.00	0.19	0.547	o	|	|	|	|	1.88
25.917	0.00	0.19	0.546	o	|	|	|	|	1.88
26.000	0.00	0.19	0.544	o	|	|	|	|	1.87
26.083	0.00	0.19	0.543	o	|	|	|	|	1.87
26.167	0.00	0.18	0.542	o	|	|	|	|	1.86
26.250	0.00	0.18	0.540	o	|	|	|	|	1.86
26.333	0.00	0.18	0.539	o	|	|	|	|	1.85
26.417	0.00	0.18	0.538	o	|	|	|	|	1.85
26.500	0.00	0.18	0.537	o	|	|	|	|	1.85
26.583	0.00	0.18	0.535	o	|	|	|	|	1.84
26.667	0.00	0.18	0.534	o	|	|	|	|	1.84
26.750	0.00	0.18	0.533	o	|	|	|	|	1.83
26.833	0.00	0.18	0.532	o	|	|	|	|	1.83
26.917	0.00	0.18	0.530	o	|	|	|	|	1.83
27.000	0.00	0.18	0.529	o	|	|	|	|	1.82
27.083	0.00	0.18	0.528	o	|	|	|	|	1.82
27.167	0.00	0.18	0.527	o	|	|	|	|	1.81
27.250	0.00	0.18	0.525	o	|	|	|	|	1.81
27.333	0.00	0.18	0.524	o	|	|	|	|	1.81
27.417	0.00	0.18	0.523	o	|	|	|	|	1.80
27.500	0.00	0.18	0.522	o	|	|	|	|	1.80
27.583	0.00	0.18	0.520	o	|	|	|	|	1.79
27.667	0.00	0.18	0.519	o	|	|	|	|	1.79
27.750	0.00	0.18	0.518	o	|	|	|	|	1.79
27.833	0.00	0.18	0.517	o	|	|	|	|	1.78
27.917	0.00	0.18	0.515	o	|	|	|	|	1.78
28.000	0.00	0.18	0.514	o	|	|	|	|	1.77
28.083	0.00	0.18	0.513	o	|	|	|	|	1.77
28.167	0.00	0.18	0.512	o	|	|	|	|	1.77
28.250	0.00	0.18	0.510	o	|	|	|	|	1.76
28.333	0.00	0.18	0.509	o	|	|	|	|	1.76
28.417	0.00	0.18	0.508	o	|	|	|	|	1.75
28.500	0.00	0.18	0.507	o	|	|	|	|	1.75
28.583	0.00	0.18	0.506	o	|	|	|	|	1.75
28.667	0.00	0.18	0.504	o	|	|	|	|	1.74
28.750	0.00	0.18	0.503	o	|	|	|	|	1.74
28.833	0.00	0.18	0.502	o	|	|	|	|	1.73
28.917	0.00	0.18	0.501	o	|	|	|	|	1.73
29.000	0.00	0.18	0.499	o	|	|	|	|	1.73
29.083	0.00	0.18	0.498	o	|	|	|	|	1.72
29.167	0.00	0.18	0.497	o	|	|	|	|	1.72
29.250	0.00	0.18	0.496	o	|	|	|	|	1.71
29.333	0.00	0.18	0.495	o	|	|	|	|	1.71
29.417	0.00	0.18	0.493	o	|	|	|	|	1.71
29.500	0.00	0.18	0.492	o	|	|	|	|	1.70
29.583	0.00	0.17	0.491	o	|	|	|	|	1.70
29.667	0.00	0.17	0.490	o	|	|	|	|	1.69
29.750	0.00	0.17	0.489	o	|	|	|	|	1.69
29.833	0.00	0.17	0.487	o	|	|	|	|	1.69
29.917	0.00	0.17	0.486	o	|	|	|	|	1.68
30.000	0.00	0.17	0.485	o	|	|	|	|	1.68
30.083	0.00	0.17	0.484	o	|	|	|	|	1.67

30.167	0.00	0.17	0.483	o	|	|	|	|	1.67
30.250	0.00	0.17	0.481	o	|	|	|	|	1.67
30.333	0.00	0.17	0.480	o	|	|	|	|	1.66
30.417	0.00	0.17	0.479	o	|	|	|	|	1.66
30.500	0.00	0.17	0.478	o	|	|	|	|	1.66
30.583	0.00	0.17	0.477	o	|	|	|	|	1.65
30.667	0.00	0.17	0.475	o	|	|	|	|	1.65
30.750	0.00	0.17	0.474	o	|	|	|	|	1.64
30.833	0.00	0.17	0.473	o	|	|	|	|	1.64
30.917	0.00	0.17	0.472	o	|	|	|	|	1.64
31.000	0.00	0.17	0.471	o	|	|	|	|	1.63
31.083	0.00	0.17	0.470	o	|	|	|	|	1.63
31.167	0.00	0.17	0.468	o	|	|	|	|	1.62
31.250	0.00	0.17	0.467	o	|	|	|	|	1.62
31.333	0.00	0.17	0.466	o	|	|	|	|	1.62
31.417	0.00	0.17	0.465	o	|	|	|	|	1.61
31.500	0.00	0.17	0.464	o	|	|	|	|	1.61
31.583	0.00	0.17	0.463	o	|	|	|	|	1.61
31.667	0.00	0.17	0.461	o	|	|	|	|	1.60
31.750	0.00	0.17	0.460	o	|	|	|	|	1.60
31.833	0.00	0.17	0.459	o	|	|	|	|	1.59
31.917	0.00	0.17	0.458	o	|	|	|	|	1.59
32.000	0.00	0.17	0.457	o	|	|	|	|	1.59
32.083	0.00	0.17	0.456	o	|	|	|	|	1.58
32.167	0.00	0.17	0.454	o	|	|	|	|	1.58
32.250	0.00	0.17	0.453	o	|	|	|	|	1.58
32.333	0.00	0.17	0.452	o	|	|	|	|	1.57
32.417	0.00	0.17	0.451	o	|	|	|	|	1.57
32.500	0.00	0.17	0.450	o	|	|	|	|	1.56
32.583	0.00	0.17	0.449	o	|	|	|	|	1.56
32.667	0.00	0.17	0.448	o	|	|	|	|	1.56
32.750	0.00	0.17	0.446	o	|	|	|	|	1.55
32.833	0.00	0.17	0.445	o	|	|	|	|	1.55
32.917	0.00	0.17	0.444	o	|	|	|	|	1.55
33.000	0.00	0.17	0.443	o	|	|	|	|	1.54
33.083	0.00	0.17	0.442	o	|	|	|	|	1.54
33.167	0.00	0.17	0.441	o	|	|	|	|	1.53
33.250	0.00	0.16	0.440	o	|	|	|	|	1.53
33.333	0.00	0.16	0.438	o	|	|	|	|	1.53
33.417	0.00	0.16	0.437	o	|	|	|	|	1.52
33.500	0.00	0.16	0.436	o	|	|	|	|	1.52
33.583	0.00	0.16	0.435	o	|	|	|	|	1.52
33.667	0.00	0.16	0.434	o	|	|	|	|	1.51
33.750	0.00	0.16	0.433	o	|	|	|	|	1.51
33.833	0.00	0.16	0.432	o	|	|	|	|	1.51
33.917	0.00	0.16	0.430	o	|	|	|	|	1.50
34.000	0.00	0.16	0.429	o	|	|	|	|	1.50
34.083	0.00	0.16	0.428	o	|	|	|	|	1.49
34.167	0.00	0.16	0.427	o	|	|	|	|	1.49
34.250	0.00	0.16	0.426	o	|	|	|	|	1.49
34.333	0.00	0.16	0.425	o	|	|	|	|	1.48
34.417	0.00	0.16	0.424	o	|	|	|	|	1.48
34.500	0.00	0.16	0.423	o	|	|	|	|	1.48
34.583	0.00	0.16	0.422	o	|	|	|	|	1.47
34.667	0.00	0.16	0.420	o	|	|	|	|	1.47
34.750	0.00	0.16	0.419	o	|	|	|	|	1.47
34.833	0.00	0.16	0.418	o	|	|	|	|	1.46
34.917	0.00	0.16	0.417	o	|	|	|	|	1.46
35.000	0.00	0.16	0.416	o	|	|	|	|	1.45
35.083	0.00	0.16	0.415	o	|	|	|	|	1.45
35.167	0.00	0.16	0.414	o	|	|	|	|	1.45
35.250	0.00	0.16	0.413	o	|	|	|	|	1.44
35.333	0.00	0.16	0.412	o	|	|	|	|	1.44
35.417	0.00	0.16	0.411	o	|	|	|	|	1.44
35.500	0.00	0.16	0.409	o	|	|	|	|	1.43
35.583	0.00	0.16	0.408	o	|	|	|	|	1.43
35.667	0.00	0.16	0.407	o	|	|	|	|	1.43
35.750	0.00	0.16	0.406	o	|	|	|	|	1.42
35.833	0.00	0.16	0.405	o	|	|	|	|	1.42
35.917	0.00	0.16	0.404	o	|	|	|	|	1.42
36.000	0.00	0.16	0.403	o	|	|	|	|	1.41
36.083	0.00	0.16	0.402	o	|	|	|	|	1.41
36.167	0.00	0.16	0.401	o	|	|	|	|	1.40
36.250	0.00	0.16	0.400	o	|	|	|	|	1.40
36.333	0.00	0.16	0.399	o	|	|	|	|	1.40
36.417	0.00	0.16	0.397	o	|	|	|	|	1.39
36.500	0.00	0.16	0.396	o	|	|	|	|	1.39
36.583	0.00	0.16	0.395	o	|	|	|	|	1.39
36.667	0.00	0.16	0.394	o	|	|	|	|	1.38
36.750	0.00	0.16	0.393	o	|	|	|	|	1.38
36.833	0.00	0.16	0.392	o	|	|	|	|	1.38
36.917	0.00	0.16	0.391	o	|	|	|	|	1.37
37.000	0.00	0.16	0.390	o	|	|	|	|	1.37
37.083	0.00	0.15	0.389	o	|	|	|	|	1.37
37.167	0.00	0.15	0.388	o	|	|	|	|	1.36
37.250	0.00	0.15	0.387	o	|	|	|	|	1.36

37.333	0.00	0.15	0.386	o	|	|	|	1.36
37.417	0.00	0.15	0.385	o	|	|	|	1.35
37.500	0.00	0.15	0.384	o	|	|	|	1.35
37.583	0.00	0.15	0.383	o	|	|	|	1.35
37.667	0.00	0.15	0.381	o	|	|	|	1.34
37.750	0.00	0.15	0.380	o	|	|	|	1.34
37.833	0.00	0.15	0.379	o	|	|	|	1.34
37.917	0.00	0.15	0.378	o	|	|	|	1.33
38.000	0.00	0.15	0.377	o	|	|	|	1.33
38.083	0.00	0.15	0.376	o	|	|	|	1.33
38.167	0.00	0.15	0.375	o	|	|	|	1.32
38.250	0.00	0.15	0.374	o	|	|	|	1.32
38.333	0.00	0.15	0.373	o	|	|	|	1.32
38.417	0.00	0.15	0.372	o	|	|	|	1.31
38.500	0.00	0.15	0.371	o	|	|	|	1.31
38.583	0.00	0.15	0.370	o	|	|	|	1.30
38.667	0.00	0.15	0.369	o	|	|	|	1.30
38.750	0.00	0.15	0.368	o	|	|	|	1.30
38.833	0.00	0.15	0.367	o	|	|	|	1.29
38.917	0.00	0.15	0.366	o	|	|	|	1.29
39.000	0.00	0.15	0.365	o	|	|	|	1.29
39.083	0.00	0.15	0.364	o	|	|	|	1.28
39.167	0.00	0.15	0.363	o	|	|	|	1.28
39.250	0.00	0.15	0.362	o	|	|	|	1.28
39.333	0.00	0.15	0.361	o	|	|	|	1.27
39.417	0.00	0.15	0.360	o	|	|	|	1.27
39.500	0.00	0.15	0.359	o	|	|	|	1.27
39.583	0.00	0.15	0.357	o	|	|	|	1.26
39.667	0.00	0.15	0.356	o	|	|	|	1.26
39.750	0.00	0.15	0.355	o	|	|	|	1.26
39.833	0.00	0.15	0.354	o	|	|	|	1.25
39.917	0.00	0.15	0.353	o	|	|	|	1.25
40.000	0.00	0.15	0.352	o	|	|	|	1.25
40.083	0.00	0.15	0.351	o	|	|	|	1.24
40.167	0.00	0.15	0.350	o	|	|	|	1.24
40.250	0.00	0.15	0.349	o	|	|	|	1.24
40.333	0.00	0.15	0.348	o	|	|	|	1.23
40.417	0.00	0.15	0.347	o	|	|	|	1.23
40.500	0.00	0.15	0.346	o	|	|	|	1.23
40.583	0.00	0.15	0.345	o	|	|	|	1.22
40.667	0.00	0.15	0.344	o	|	|	|	1.22
40.750	0.00	0.15	0.343	o	|	|	|	1.22
40.833	0.00	0.15	0.342	o	|	|	|	1.22
40.917	0.00	0.15	0.341	o	|	|	|	1.21
41.000	0.00	0.15	0.340	o	|	|	|	1.21
41.083	0.00	0.15	0.339	o	|	|	|	1.21
41.167	0.00	0.15	0.338	o	|	|	|	1.20
41.250	0.00	0.14	0.337	o	|	|	|	1.20
41.333	0.00	0.14	0.336	o	|	|	|	1.20
41.417	0.00	0.14	0.335	o	|	|	|	1.19
41.500	0.00	0.14	0.334	o	|	|	|	1.19
41.583	0.00	0.14	0.333	o	|	|	|	1.19
41.667	0.00	0.14	0.332	o	|	|	|	1.18
41.750	0.00	0.14	0.331	o	|	|	|	1.18
41.833	0.00	0.14	0.330	o	|	|	|	1.18
41.917	0.00	0.14	0.329	o	|	|	|	1.17
42.000	0.00	0.14	0.328	o	|	|	|	1.17
42.083	0.00	0.14	0.327	o	|	|	|	1.17
42.167	0.00	0.14	0.326	o	|	|	|	1.16
42.250	0.00	0.14	0.325	o	|	|	|	1.16
42.333	0.00	0.14	0.324	o	|	|	|	1.16
42.417	0.00	0.14	0.323	o	|	|	|	1.15
42.500	0.00	0.14	0.322	o	|	|	|	1.15
42.583	0.00	0.14	0.321	o	|	|	|	1.15
42.667	0.00	0.14	0.320	o	|	|	|	1.14
42.750	0.00	0.14	0.320	o	|	|	|	1.14
42.833	0.00	0.14	0.319	o	|	|	|	1.14
42.917	0.00	0.14	0.318	o	|	|	|	1.13
43.000	0.00	0.14	0.317	o	|	|	|	1.13
43.083	0.00	0.14	0.316	o	|	|	|	1.13
43.167	0.00	0.14	0.315	o	|	|	|	1.13
43.250	0.00	0.14	0.314	o	|	|	|	1.12
43.333	0.00	0.14	0.313	o	|	|	|	1.12
43.417	0.00	0.14	0.312	o	|	|	|	1.12
43.500	0.00	0.14	0.311	o	|	|	|	1.11
43.583	0.00	0.14	0.310	o	|	|	|	1.11
43.667	0.00	0.14	0.309	o	|	|	|	1.11
43.750	0.00	0.14	0.308	o	|	|	|	1.10
43.833	0.00	0.14	0.307	o	|	|	|	1.10
43.917	0.00	0.14	0.306	o	|	|	|	1.10
44.000	0.00	0.14	0.305	o	|	|	|	1.09
44.083	0.00	0.14	0.304	o	|	|	|	1.09
44.167	0.00	0.14	0.303	o	|	|	|	1.09
44.250	0.00	0.14	0.302	o	|	|	|	1.08
44.333	0.00	0.14	0.301	o	|	|	|	1.08
44.417	0.00	0.14	0.300	o	|	|	|	1.08

44.500	0.00	0.14	0.299	o	|	|	|	1.08
44.583	0.00	0.14	0.298	o	|	|	|	1.07
44.667	0.00	0.14	0.297	o	|	|	|	1.07
44.750	0.00	0.14	0.296	o	|	|	|	1.07
44.833	0.00	0.14	0.296	o	|	|	|	1.06
44.917	0.00	0.14	0.295	o	|	|	|	1.06
45.000	0.00	0.14	0.294	o	|	|	|	1.06
45.083	0.00	0.14	0.293	o	|	|	|	1.05
45.167	0.00	0.14	0.292	o	|	|	|	1.05
45.250	0.00	0.14	0.291	o	|	|	|	1.05
45.333	0.00	0.14	0.290	o	|	|	|	1.05
45.417	0.00	0.14	0.289	o	|	|	|	1.04
45.500	0.00	0.14	0.288	o	|	|	|	1.04
45.583	0.00	0.14	0.287	o	|	|	|	1.04
45.667	0.00	0.13	0.286	o	|	|	|	1.03
45.750	0.00	0.13	0.285	o	|	|	|	1.03
45.833	0.00	0.13	0.284	o	|	|	|	1.03
45.917	0.00	0.13	0.283	o	|	|	|	1.02
46.000	0.00	0.13	0.282	o	|	|	|	1.02
46.083	0.00	0.13	0.282	o	|	|	|	1.02
46.167	0.00	0.13	0.281	o	|	|	|	1.02
46.250	0.00	0.13	0.280	o	|	|	|	1.01
46.333	0.00	0.13	0.279	o	|	|	|	1.01
46.417	0.00	0.13	0.278	o	|	|	|	1.01
46.500	0.00	0.13	0.277	o	|	|	|	1.00
46.583	0.00	0.13	0.276	o	|	|	|	1.00
46.667	0.00	0.13	0.275	o	|	|	|	1.00
46.750	0.00	0.13	0.274	o	|	|	|	0.99
46.833	0.00	0.13	0.273	o	|	|	|	0.99
46.917	0.00	0.13	0.272	o	|	|	|	0.99
47.000	0.00	0.13	0.271	o	|	|	|	0.98
47.083	0.00	0.13	0.271	o	|	|	|	0.98
47.167	0.00	0.13	0.270	o	|	|	|	0.98
47.250	0.00	0.13	0.269	o	|	|	|	0.97
47.333	0.00	0.13	0.268	o	|	|	|	0.97
47.417	0.00	0.13	0.267	o	|	|	|	0.97
47.500	0.00	0.13	0.266	o	|	|	|	0.96
47.583	0.00	0.13	0.265	o	|	|	|	0.96
47.667	0.00	0.13	0.264	o	|	|	|	0.96
47.750	0.00	0.13	0.264	o	|	|	|	0.95
47.833	0.00	0.13	0.263	o	|	|	|	0.95
47.917	0.00	0.13	0.262	o	|	|	|	0.95
48.000	0.00	0.13	0.261	o	|	|	|	0.95
48.083	0.00	0.13	0.260	o	|	|	|	0.94
48.167	0.00	0.12	0.259	o	|	|	|	0.94
48.250	0.00	0.12	0.258	o	|	|	|	0.94
48.333	0.00	0.12	0.257	o	|	|	|	0.93
48.417	0.00	0.12	0.257	o	|	|	|	0.93
48.500	0.00	0.12	0.256	o	|	|	|	0.93
48.583	0.00	0.12	0.255	o	|	|	|	0.92
48.667	0.00	0.12	0.254	o	|	|	|	0.92
48.750	0.00	0.12	0.253	o	|	|	|	0.92
48.833	0.00	0.12	0.252	o	|	|	|	0.91
48.917	0.00	0.12	0.252	o	|	|	|	0.91
49.000	0.00	0.12	0.251	o	|	|	|	0.91
49.083	0.00	0.12	0.250	o	|	|	|	0.91
49.167	0.00	0.12	0.249	o	|	|	|	0.90
49.250	0.00	0.12	0.248	o	|	|	|	0.90
49.333	0.00	0.12	0.247	o	|	|	|	0.90
49.417	0.00	0.12	0.247	o	|	|	|	0.89
49.500	0.00	0.12	0.246	o	|	|	|	0.89
49.583	0.00	0.12	0.245	o	|	|	|	0.89
49.667	0.00	0.12	0.244	o	|	|	|	0.88
49.750	0.00	0.12	0.243	o	|	|	|	0.88
49.833	0.00	0.12	0.243	o	|	|	|	0.88
49.917	0.00	0.12	0.242	o	|	|	|	0.88
50.000	0.00	0.12	0.241	o	|	|	|	0.87
50.083	0.00	0.12	0.240	o	|	|	|	0.87
50.167	0.00	0.12	0.239	o	|	|	|	0.87
50.250	0.00	0.11	0.239	o	|	|	|	0.86
50.333	0.00	0.11	0.238	o	|	|	|	0.86
50.417	0.00	0.11	0.237	o	|	|	|	0.86
50.500	0.00	0.11	0.236	o	|	|	|	0.86
50.583	0.00	0.11	0.235	o	|	|	|	0.85
50.667	0.00	0.11	0.235	o	|	|	|	0.85
50.750	0.00	0.11	0.234	o	|	|	|	0.85
50.833	0.00	0.11	0.233	o	|	|	|	0.84
50.917	0.00	0.11	0.232	o	|	|	|	0.84
51.000	0.00	0.11	0.232	o	|	|	|	0.84
51.083	0.00	0.11	0.231	o	|	|	|	0.84
51.167	0.00	0.11	0.230	o	|	|	|	0.83
51.250	0.00	0.11	0.229	o	|	|	|	0.83
51.333	0.00	0.11	0.228	o	|	|	|	0.83
51.417	0.00	0.11	0.228	o	|	|	|	0.83
51.500	0.00	0.11	0.227	o	|	|	|	0.82
51.583	0.00	0.11	0.226	o	|	|	|	0.82

51.667	0.00	0.11	0.225	o	|	|	|	|	0.82
51.750	0.00	0.11	0.225	o	|	|	|	|	0.81
51.833	0.00	0.11	0.224	o	|	|	|	|	0.81
51.917	0.00	0.11	0.223	o	|	|	|	|	0.81
52.000	0.00	0.11	0.222	o	|	|	|	|	0.81
52.083	0.00	0.11	0.222	o	|	|	|	|	0.80
52.167	0.00	0.11	0.221	o	|	|	|	|	0.80
52.250	0.00	0.11	0.220	o	|	|	|	|	0.80
52.333	0.00	0.11	0.220	o	|	|	|	|	0.80
52.417	0.00	0.11	0.219	o	|	|	|	|	0.79
52.500	0.00	0.11	0.218	o	|	|	|	|	0.79
52.583	0.00	0.10	0.217	o	|	|	|	|	0.79
52.667	0.00	0.10	0.217	o	|	|	|	|	0.78
52.750	0.00	0.10	0.216	o	|	|	|	|	0.78
52.833	0.00	0.10	0.215	o	|	|	|	|	0.78
52.917	0.00	0.10	0.215	o	|	|	|	|	0.78
53.000	0.00	0.10	0.214	o	|	|	|	|	0.77
53.083	0.00	0.10	0.213	o	|	|	|	|	0.77
53.167	0.00	0.10	0.212	o	|	|	|	|	0.77
53.250	0.00	0.10	0.212	o	|	|	|	|	0.77
53.333	0.00	0.10	0.211	o	|	|	|	|	0.76
53.417	0.00	0.10	0.210	o	|	|	|	|	0.76
53.500	0.00	0.10	0.210	o	|	|	|	|	0.76
53.583	0.00	0.10	0.209	o	|	|	|	|	0.76
53.667	0.00	0.10	0.208	o	|	|	|	|	0.75
53.750	0.00	0.10	0.208	o	|	|	|	|	0.75

Remaining water in basin = 0.21 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 645
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 9.236 (CFS)
Total volume = 1.704 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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                    FLOOD HYDROGRAPH ROUTING PROGRAM
                Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                            Study date: 05/07/25

      ---------------------------------------------------------------------



      Program License Serial Number 5006

      ---------------------------------------------------------------------
      ********************* HYDROGRAPH INFORMATION **********************

                  From study/file name: PRO10610.rte
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =    76
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =       26.296 (CFS)
                  Total volume =       2.644 (Ac.Ft)
            Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      *********************************************************************



      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
      Process from Point/Station        1.000 to Point/Station        2.000
      **** RETARDING BASIN ROUTING ****
      _____________________________________________________________________

      User entry of depth-outflow-storage data
      ---------------------------------------------------------------------
      Total number of inflow hydrograph intervals = 76
      Hydrograph time unit =  5.000 (Min.)
      Initial depth in storage basin =   0.00(Ft.)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Initial basin depth =   0.00 (Ft.)
      Initial basin storage =      0.00 (Ac.Ft)
      Initial basin outflow =   0.00 (CFS)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Depth vs. Storage and Depth vs. Discharge data:
       Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
            (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
      ---------------------------------------------------------------------
         0.000      0.000      0.000      0.000        0.000
         1.000      0.276      0.133      0.276        0.276
         2.000      0.584      0.193      0.583        0.585
         3.000      0.930      0.700      0.928        0.932
         3.500      1.118      0.824      1.115        1.121
         4.000      1.316      0.930      1.313        1.319
         4.500      1.528      1.024      1.524        1.532
         4.750      1.637      1.068      1.633        1.641
         5.000      1.749     18.283      1.686        1.812
         6.000      2.231    253.655      1.358        3.104
      ---------------------------------------------------------------------
                     Hydrograph Detention Basin Routing
      ---------------------------------------------------------------------

      Graph values: 'I'= unit inflow; 'O'=outflow at time shown
      ---------------------------------------------------------------------
       Time   Inflow  Outflow    Storage                                    Depth
      (Hours)  (CFS)   (CFS)     (Ac.Ft) .0       6.6   13.15   19.72   26.30 (Ft.)
       0.083    0.66    0.00      0.002  O       |       |       |       |     0.01
       0.167    1.51    0.00      0.010  OI      |       |       |       |     0.04
       0.250    1.81    0.01      0.021  O I     |       |       |       |     0.08
       0.333    1.90    0.02      0.034  O I     |       |       |       |     0.12
       0.417    1.94    0.02      0.047  O I     |       |       |       |     0.17
       0.500    2.07    0.03      0.060  O I     |       |       |       |     0.22
       0.583    2.22    0.04      0.075  O I     |       |       |       |     0.27
       0.667    2.25    0.04      0.090  O I     |       |       |       |     0.33
       0.750    2.26    0.05      0.105  O I     |       |       |       |     0.38
       0.833    2.27    0.06      0.120  O I     |       |       |       |     0.44
       0.917    2.27    0.07      0.136  O I     |       |       |       |     0.49
       1.000    2.40    0.07      0.151  O I     |       |       |       |     0.55
       1.083    2.54    0.08      0.168  O  I    |       |       |       |     0.61
       1.167    2.57    0.09      0.185  O  I    |       |       |       |     0.67
       1.250    2.58    0.10      0.202  O  I    |       |       |       |     0.73
       1.333    2.59    0.11      0.219  O  I    |       |       |       |     0.79
       1.417    2.59    0.11      0.236  O  I    |       |       |       |     0.86
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1.500    2.59    0.12      0.253  O  I    |        |        |        |     0.92
1.583    2.59    0.13      0.270  O  I    |        |        |        |     0.98
1.667    2.59    0.14      0.287  O  I    |        |        |        |     1.04
1.750    2.59    0.14      0.304  O  I    |        |        |        |     1.09
1.833    2.59    0.14      0.321  O  I    |        |        |        |     1.15
1.917    2.59    0.14      0.338  O  I    |        |        |        |     1.20
2.000    2.72    0.15      0.355  O  I    |        |        |        |     1.26
2.083    2.73    0.15      0.373  O  I    |        |        |        |     1.31
2.167    2.75    0.16      0.390  O  I    |        |        |        |     1.37
2.250    2.88    0.16      0.409  O  I    |        |        |        |     1.43
2.333    2.90    0.16      0.427  O  I    |        |        |        |     1.49
2.417    2.91    0.17      0.446  O  I    |        |        |        |     1.55
2.500    2.91    0.17      0.465  O  I    |        |        |        |     1.61
2.583    2.91    0.17      0.484  O  I    |        |        |        |     1.68
2.667    2.91    0.18      0.503  O  I    |        |        |        |     1.74
2.750    3.04    0.18      0.522  O  I    |        |        |        |     1.80
2.833    3.19    0.18      0.542  O  I    |        |        |        |     1.87
2.917    3.22    0.19      0.563  O  I    |        |        |        |     1.93
3.000    3.23    0.19      0.584  O  I    |        |        |        |     2.00
3.083    3.24    0.22      0.605  O  I    |        |        |        |     2.06
3.167    3.37    0.25      0.626  O   I   |        |        |        |     2.12
3.250    3.51    0.29      0.648  O   I   |        |        |        |     2.18
3.333    3.54    0.32      0.670  O   I   |        |        |        |     2.25
3.417    3.69    0.35      0.693  O   I   |        |        |        |     2.31
3.500    3.97    0.39      0.716  O   I   |        |        |        |     2.38
3.583    4.27    0.42      0.742  O    I  |        |        |        |     2.46
3.667    4.46    0.46      0.769  O    I  |        |        |        |     2.53
3.750    4.64    0.51      0.797  O    I  |        |        |        |     2.62
3.833    4.80    0.55      0.826  O    I  |        |        |        |     2.70
3.917    4.97    0.59      0.856  O     I |        |        |        |     2.79
4.000    5.12    0.64      0.886  O     I |        |        |        |     2.87
4.083    5.29    0.68      0.917  O     I |        |        |        |     2.96
4.167    5.58    0.71      0.950  O     I |        |        |        |     3.05
4.250    6.00    0.74      0.985  O      I|        |        |        |     3.15
4.333    6.57    0.76      1.023  O      I|        |        |        |     3.25
4.417    7.20    0.79      1.065  O       I        |        |        |     3.36
4.500    7.57    0.82      1.111  O       |I       |        |        |     3.48
4.583    7.93    0.85      1.158  |O      |I       |        |        |     3.60
4.667    8.52    0.87      1.209  |O      | I      |        |        |     3.73
4.750    9.14    0.90      1.264  |O      |  I     |        |        |     3.87
4.833    9.51    0.93      1.322  |O      |  I     |        |        |     4.01
4.917    9.87    0.96      1.382  |O      |   I    |        |        |     4.16
5.000   10.46    0.99      1.445  |O      |   I    |        |        |     4.30
5.083   12.14    1.02      1.516  |O      |     I  |        |        |     4.47
5.167   14.98    1.05      1.602  |O      |      I |        |        |     4.67
5.250   17.55    8.10      1.683  |       |O       |    I   |        |     4.85
5.333   19.64   15.36      1.730  |       |        |  O   I |        |     4.96
5.417   22.18   19.94      1.752  |       |        |       O I      |     5.01
5.500   26.30   25.33      1.763  |       |        |         |    O I     5.03
5.583   19.54   22.31      1.757  |       |        |       I |  O     |     5.02
5.667    8.18   14.66      1.725  |       |I       |O        |        |     4.95
5.750    4.25    8.81      1.687  |    I  | O      |         |        |     4.86
5.833    2.54    5.06      1.663  |  I  O |        |         |        |     4.81
5.917    1.51    2.96      1.649  |I O    |        |         |        |     4.78
6.000    0.97    1.77      1.642  |IO     |        |         |        |     4.76
6.083    0.47    1.07      1.637  IO      |        |         |        |     4.75
6.167    0.12    1.07      1.631  IO      |        |         |        |     4.74
6.250    0.04    1.06      1.625  IO      |        |         |        |     4.72
6.333    0.01    1.06      1.618  IO      |        |         |        |     4.71
6.417    0.00    1.06      1.610  IO      |        |         |        |     4.69
6.500    0.00    1.05      1.603  IO      |        |         |        |     4.67
6.583    0.00    1.05      1.596  IO      |        |         |        |     4.66
6.667    0.00    1.05      1.589  IO      |        |         |        |     4.64
6.750    0.00    1.05      1.581  IO      |        |         |        |     4.62
6.833    0.00    1.04      1.574  IO      |        |         |        |     4.61
6.917    0.00    1.04      1.567  IO      |        |         |        |     4.59
7.000    0.00    1.04      1.560  IO      |        |         |        |     4.57
7.083    0.00    1.03      1.553  IO      |        |         |        |     4.56
7.167    0.00    1.03      1.546  IO      |        |         |        |     4.54
7.250    0.00    1.03      1.539  IO      |        |         |        |     4.52
7.333    0.00    1.03      1.531  IO      |        |         |        |     4.51
7.417    0.00    1.02      1.524  IO      |        |         |        |     4.49
7.500    0.00    1.02      1.517  IO      |        |         |        |     4.47
7.583    0.00    1.02      1.510  IO      |        |         |        |     4.46
7.667    0.00    1.01      1.503  IO      |        |         |        |     4.44
7.750    0.00    1.01      1.496  IO      |        |         |        |     4.43
7.833    0.00    1.01      1.489  IO      |        |         |        |     4.41
7.917    0.00    1.00      1.483  IO      |        |         |        |     4.39
8.000    0.00    1.00      1.476  IO      |        |         |        |     4.38
8.083    0.00    1.00      1.469  IO      |        |         |        |     4.36
8.167    0.00    0.99      1.462  IO      |        |         |        |     4.34
8.250    0.00    0.99      1.455  IO      |        |         |        |     4.33
8.333    0.00    0.99      1.448  IO      |        |         |        |     4.31
8.417    0.00    0.99      1.441  IO      |        |         |        |     4.30
8.500    0.00    0.98      1.435  IO      |        |         |        |     4.28
8.583    0.00    0.98      1.428  IO      |        |         |        |     4.26
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8.667	0.00	0.98	1.421	IO					4.25
8.750	0.00	0.97	1.414	IO					4.23
8.833	0.00	0.97	1.408	IO					4.22
8.917	0.00	0.97	1.401	IO					4.20
9.000	0.00	0.96	1.394	IO					4.18
9.083	0.00	0.96	1.388	IO					4.17
9.167	0.00	0.96	1.381	IO					4.15
9.250	0.00	0.96	1.375	IO					4.14
9.333	0.00	0.95	1.368	IO					4.12
9.417	0.00	0.95	1.361	IO					4.11
9.500	0.00	0.95	1.355	IO					4.09
9.583	0.00	0.94	1.348	IO					4.08
9.667	0.00	0.94	1.342	IO					4.06
9.750	0.00	0.94	1.335	IO					4.05
9.833	0.00	0.94	1.329	IO					4.03
9.917	0.00	0.93	1.323	IO					4.02
10.000	0.00	0.93	1.316	IO					4.00
10.083	0.00	0.93	1.310	IO					3.98
10.167	0.00	0.92	1.303	IO					3.97
10.250	0.00	0.92	1.297	IO					3.95
10.333	0.00	0.92	1.291	IO					3.94
10.417	0.00	0.91	1.284	IO					3.92
10.500	0.00	0.91	1.278	IO					3.90
10.583	0.00	0.91	1.272	IO					3.89
10.667	0.00	0.90	1.266	IO					3.87
10.750	0.00	0.90	1.259	IO					3.86
10.833	0.00	0.90	1.253	IO					3.84
10.917	0.00	0.89	1.247	IO					3.83
11.000	0.00	0.89	1.241	IO					3.81
11.083	0.00	0.89	1.235	IO					3.79
11.167	0.00	0.88	1.229	IO					3.78
11.250	0.00	0.88	1.223	IO					3.76
11.333	0.00	0.88	1.217	IO					3.75
11.417	0.00	0.87	1.211	IO					3.73
11.500	0.00	0.87	1.205	IO					3.72
11.583	0.00	0.87	1.199	IO					3.70
11.667	0.00	0.86	1.193	IO					3.69
11.750	0.00	0.86	1.187	IO					3.67
11.833	0.00	0.86	1.181	IO					3.66
11.917	0.00	0.85	1.175	IO					3.64
12.000	0.00	0.85	1.169	IO					3.63
12.083	0.00	0.85	1.163	IO					3.61
12.167	0.00	0.85	1.157	IO					3.60
12.250	0.00	0.84	1.151	IO					3.58
12.333	0.00	0.84	1.146	IO					3.57
12.417	0.00	0.84	1.140	IO					3.56
12.500	0.00	0.83	1.134	IO					3.54
12.583	0.00	0.83	1.128	IO					3.53
12.667	0.00	0.83	1.123	IO					3.51
12.750	0.00	0.82	1.117	IO					3.50
12.833	0.00	0.82	1.111	O					3.48
12.917	0.00	0.82	1.106	O					3.47
13.000	0.00	0.81	1.100	O					3.45
13.083	0.00	0.81	1.095	O					3.44
13.167	0.00	0.80	1.089	O					3.42
13.250	0.00	0.80	1.084	O					3.41
13.333	0.00	0.80	1.078	O					3.39
13.417	0.00	0.79	1.073	O					3.38
13.500	0.00	0.79	1.067	O					3.36
13.583	0.00	0.79	1.062	O					3.35
13.667	0.00	0.78	1.056	O					3.34
13.750	0.00	0.78	1.051	O					3.32
13.833	0.00	0.78	1.046	O					3.31
13.917	0.00	0.77	1.040	O					3.29
14.000	0.00	0.77	1.035	O					3.28
14.083	0.00	0.77	1.030	O					3.26
14.167	0.00	0.76	1.024	O					3.25
14.250	0.00	0.76	1.019	O					3.24
14.333	0.00	0.76	1.014	O					3.22
14.417	0.00	0.75	1.009	O					3.21
14.500	0.00	0.75	1.004	O					3.20
14.583	0.00	0.75	0.998	O					3.18
14.667	0.00	0.74	0.993	O					3.17
14.750	0.00	0.74	0.988	O					3.15
14.833	0.00	0.74	0.983	O					3.14
14.917	0.00	0.73	0.978	O					3.13
15.000	0.00	0.73	0.973	O					3.11
15.083	0.00	0.73	0.968	O					3.10
15.167	0.00	0.72	0.963	O					3.09
15.250	0.00	0.72	0.958	O					3.07
15.333	0.00	0.72	0.953	O					3.06
15.417	0.00	0.71	0.948	O					3.05
15.500	0.00	0.71	0.943	O					3.04
15.583	0.00	0.71	0.938	O					3.02
15.667	0.00	0.70	0.934	O					3.01
15.750	0.00	0.70	0.929	O					3.00

15.833	0.00	0.69	0.924	o	|	|	|	2.98
15.917	0.00	0.68	0.919	o	|	|	|	2.97
16.000	0.00	0.68	0.915	o	|	|	|	2.96
16.083	0.00	0.67	0.910	o	|	|	|	2.94
16.167	0.00	0.66	0.905	o	|	|	|	2.93
16.250	0.00	0.66	0.901	o	|	|	|	2.92
16.333	0.00	0.65	0.896	o	|	|	|	2.90
16.417	0.00	0.64	0.892	o	|	|	|	2.89
16.500	0.00	0.64	0.887	o	|	|	|	2.88
16.583	0.00	0.63	0.883	o	|	|	|	2.86
16.667	0.00	0.62	0.879	o	|	|	|	2.85
16.750	0.00	0.62	0.874	o	|	|	|	2.84
16.833	0.00	0.61	0.870	o	|	|	|	2.83
16.917	0.00	0.61	0.866	o	|	|	|	2.81
17.000	0.00	0.60	0.862	o	|	|	|	2.80
17.083	0.00	0.59	0.858	o	|	|	|	2.79
17.167	0.00	0.59	0.854	o	|	|	|	2.78
17.250	0.00	0.58	0.850	o	|	|	|	2.77
17.333	0.00	0.58	0.846	o	|	|	|	2.76
17.417	0.00	0.57	0.842	o	|	|	|	2.74
17.500	0.00	0.56	0.838	o	|	|	|	2.73
17.583	0.00	0.56	0.834	o	|	|	|	2.72
17.667	0.00	0.55	0.830	o	|	|	|	2.71
17.750	0.00	0.55	0.826	o	|	|	|	2.70
17.833	0.00	0.54	0.823	o	|	|	|	2.69
17.917	0.00	0.54	0.819	o	|	|	|	2.68
18.000	0.00	0.53	0.815	o	|	|	|	2.67
18.083	0.00	0.53	0.811	o	|	|	|	2.66
18.167	0.00	0.52	0.808	o	|	|	|	2.65
18.250	0.00	0.52	0.804	o	|	|	|	2.64
18.333	0.00	0.51	0.801	o	|	|	|	2.63
18.417	0.00	0.51	0.797	o	|	|	|	2.62
18.500	0.00	0.50	0.794	o	|	|	|	2.61
18.583	0.00	0.50	0.790	o	|	|	|	2.60
18.667	0.00	0.49	0.787	o	|	|	|	2.59
18.750	0.00	0.49	0.784	o	|	|	|	2.58
18.833	0.00	0.48	0.780	o	|	|	|	2.57
18.917	0.00	0.48	0.777	o	|	|	|	2.56
19.000	0.00	0.47	0.774	o	|	|	|	2.55
19.083	0.00	0.47	0.771	o	|	|	|	2.54
19.167	0.00	0.46	0.767	o	|	|	|	2.53
19.250	0.00	0.46	0.764	o	|	|	|	2.52
19.333	0.00	0.45	0.761	o	|	|	|	2.51
19.417	0.00	0.45	0.758	o	|	|	|	2.50
19.500	0.00	0.44	0.755	o	|	|	|	2.49
19.583	0.00	0.44	0.752	o	|	|	|	2.49
19.667	0.00	0.43	0.749	o	|	|	|	2.48
19.750	0.00	0.43	0.746	o	|	|	|	2.47
19.833	0.00	0.43	0.743	o	|	|	|	2.46
19.917	0.00	0.42	0.740	o	|	|	|	2.45
20.000	0.00	0.42	0.737	o	|	|	|	2.44
20.083	0.00	0.41	0.734	o	|	|	|	2.43
20.167	0.00	0.41	0.731	o	|	|	|	2.43
20.250	0.00	0.40	0.729	o	|	|	|	2.42
20.333	0.00	0.40	0.726	o	|	|	|	2.41
20.417	0.00	0.40	0.723	o	|	|	|	2.40
20.500	0.00	0.39	0.720	o	|	|	|	2.39
20.583	0.00	0.39	0.718	o	|	|	|	2.39
20.667	0.00	0.38	0.715	o	|	|	|	2.38
20.750	0.00	0.38	0.712	o	|	|	|	2.37
20.833	0.00	0.38	0.710	o	|	|	|	2.36
20.917	0.00	0.37	0.707	o	|	|	|	2.36
21.000	0.00	0.37	0.705	o	|	|	|	2.35
21.083	0.00	0.37	0.702	o	|	|	|	2.34
21.167	0.00	0.36	0.700	o	|	|	|	2.33
21.250	0.00	0.36	0.697	o	|	|	|	2.33
21.333	0.00	0.36	0.695	o	|	|	|	2.32
21.417	0.00	0.35	0.692	o	|	|	|	2.31
21.500	0.00	0.35	0.690	o	|	|	|	2.31
21.583	0.00	0.34	0.687	o	|	|	|	2.30
21.667	0.00	0.34	0.685	o	|	|	|	2.29
21.750	0.00	0.34	0.683	o	|	|	|	2.29
21.833	0.00	0.33	0.680	o	|	|	|	2.28
21.917	0.00	0.33	0.678	o	|	|	|	2.27
22.000	0.00	0.33	0.676	o	|	|	|	2.27
22.083	0.00	0.32	0.674	o	|	|	|	2.26
22.167	0.00	0.32	0.671	o	|	|	|	2.25
22.250	0.00	0.32	0.669	o	|	|	|	2.25
22.333	0.00	0.31	0.667	o	|	|	|	2.24
22.417	0.00	0.31	0.665	o	|	|	|	2.23
22.500	0.00	0.31	0.663	o	|	|	|	2.23
22.583	0.00	0.31	0.661	o	|	|	|	2.22
22.667	0.00	0.30	0.658	o	|	|	|	2.22
22.750	0.00	0.30	0.656	o	|	|	|	2.21
22.833	0.00	0.30	0.654	o	|	|	|	2.20
22.917	0.00	0.29	0.652	o	|	|	|	2.20

23.000	0.00	0.29	0.650	o	|	|	|	|	2.19
23.083	0.00	0.29	0.648	o	|	|	|	|	2.19
23.167	0.00	0.28	0.646	o	|	|	|	|	2.18
23.250	0.00	0.28	0.644	o	|	|	|	|	2.17
23.333	0.00	0.28	0.642	o	|	|	|	|	2.17
23.417	0.00	0.28	0.641	o	|	|	|	|	2.16
23.500	0.00	0.27	0.639	o	|	|	|	|	2.16
23.583	0.00	0.27	0.637	o	|	|	|	|	2.15
23.667	0.00	0.27	0.635	o	|	|	|	|	2.15
23.750	0.00	0.26	0.633	o	|	|	|	|	2.14
23.833	0.00	0.26	0.631	o	|	|	|	|	2.14
23.917	0.00	0.26	0.630	o	|	|	|	|	2.13
24.000	0.00	0.26	0.628	o	|	|	|	|	2.13
24.083	0.00	0.25	0.626	o	|	|	|	|	2.12
24.167	0.00	0.25	0.624	o	|	|	|	|	2.12
24.250	0.00	0.25	0.623	o	|	|	|	|	2.11
24.333	0.00	0.25	0.621	o	|	|	|	|	2.11
24.417	0.00	0.24	0.619	o	|	|	|	|	2.10
24.500	0.00	0.24	0.617	o	|	|	|	|	2.10
24.583	0.00	0.24	0.616	o	|	|	|	|	2.09
24.667	0.00	0.24	0.614	o	|	|	|	|	2.09
24.750	0.00	0.23	0.612	o	|	|	|	|	2.08
24.833	0.00	0.23	0.611	o	|	|	|	|	2.08
24.917	0.00	0.23	0.609	o	|	|	|	|	2.07
25.000	0.00	0.23	0.608	o	|	|	|	|	2.07
25.083	0.00	0.23	0.606	o	|	|	|	|	2.06
25.167	0.00	0.22	0.605	o	|	|	|	|	2.06
25.250	0.00	0.22	0.603	o	|	|	|	|	2.06
25.333	0.00	0.22	0.602	o	|	|	|	|	2.05
25.417	0.00	0.22	0.600	o	|	|	|	|	2.05
25.500	0.00	0.21	0.599	o	|	|	|	|	2.04
25.583	0.00	0.21	0.597	o	|	|	|	|	2.04
25.667	0.00	0.21	0.596	o	|	|	|	|	2.03
25.750	0.00	0.21	0.594	o	|	|	|	|	2.03
25.833	0.00	0.21	0.593	o	|	|	|	|	2.03
25.917	0.00	0.20	0.591	o	|	|	|	|	2.02
26.000	0.00	0.20	0.590	o	|	|	|	|	2.02
26.083	0.00	0.20	0.589	o	|	|	|	|	2.01
26.167	0.00	0.20	0.587	o	|	|	|	|	2.01
26.250	0.00	0.20	0.586	o	|	|	|	|	2.01
26.333	0.00	0.19	0.585	o	|	|	|	|	2.00
26.417	0.00	0.19	0.583	o	|	|	|	|	2.00
26.500	0.00	0.19	0.582	o	|	|	|	|	1.99
26.583	0.00	0.19	0.581	o	|	|	|	|	1.99
26.667	0.00	0.19	0.579	o	|	|	|	|	1.98
26.750	0.00	0.19	0.578	o	|	|	|	|	1.98
26.833	0.00	0.19	0.577	o	|	|	|	|	1.98
26.917	0.00	0.19	0.575	o	|	|	|	|	1.97
27.000	0.00	0.19	0.574	o	|	|	|	|	1.97
27.083	0.00	0.19	0.573	o	|	|	|	|	1.96
27.167	0.00	0.19	0.571	o	|	|	|	|	1.96
27.250	0.00	0.19	0.570	o	|	|	|	|	1.95
27.333	0.00	0.19	0.569	o	|	|	|	|	1.95
27.417	0.00	0.19	0.567	o	|	|	|	|	1.95
27.500	0.00	0.19	0.566	o	|	|	|	|	1.94
27.583	0.00	0.19	0.565	o	|	|	|	|	1.94
27.667	0.00	0.19	0.563	o	|	|	|	|	1.93
27.750	0.00	0.19	0.562	o	|	|	|	|	1.93
27.833	0.00	0.19	0.561	o	|	|	|	|	1.92
27.917	0.00	0.19	0.560	o	|	|	|	|	1.92
28.000	0.00	0.19	0.558	o	|	|	|	|	1.92
28.083	0.00	0.19	0.557	o	|	|	|	|	1.91
28.167	0.00	0.19	0.556	o	|	|	|	|	1.91
28.250	0.00	0.19	0.554	o	|	|	|	|	1.90
28.333	0.00	0.19	0.553	o	|	|	|	|	1.90
28.417	0.00	0.19	0.552	o	|	|	|	|	1.90
28.500	0.00	0.19	0.551	o	|	|	|	|	1.89
28.583	0.00	0.19	0.549	o	|	|	|	|	1.89
28.667	0.00	0.19	0.548	o	|	|	|	|	1.88
28.750	0.00	0.19	0.547	o	|	|	|	|	1.88
28.833	0.00	0.19	0.545	o	|	|	|	|	1.87
28.917	0.00	0.19	0.544	o	|	|	|	|	1.87
29.000	0.00	0.18	0.543	o	|	|	|	|	1.87
29.083	0.00	0.18	0.542	o	|	|	|	|	1.86
29.167	0.00	0.18	0.540	o	|	|	|	|	1.86
29.250	0.00	0.18	0.539	o	|	|	|	|	1.85
29.333	0.00	0.18	0.538	o	|	|	|	|	1.85
29.417	0.00	0.18	0.537	o	|	|	|	|	1.85
29.500	0.00	0.18	0.535	o	|	|	|	|	1.84
29.583	0.00	0.18	0.534	o	|	|	|	|	1.84
29.667	0.00	0.18	0.533	o	|	|	|	|	1.83
29.750	0.00	0.18	0.531	o	|	|	|	|	1.83
29.833	0.00	0.18	0.530	o	|	|	|	|	1.83
29.917	0.00	0.18	0.529	o	|	|	|	|	1.82
30.000	0.00	0.18	0.528	o	|	|	|	|	1.82
30.083	0.00	0.18	0.526	o	|	|	|	|	1.81

30.167	0.00	0.18	0.525	o	|	|	|	|	1.81
30.250	0.00	0.18	0.524	o	|	|	|	|	1.81
30.333	0.00	0.18	0.523	o	|	|	|	|	1.80
30.417	0.00	0.18	0.521	o	|	|	|	|	1.80
30.500	0.00	0.18	0.520	o	|	|	|	|	1.79
30.583	0.00	0.18	0.519	o	|	|	|	|	1.79
30.667	0.00	0.18	0.518	o	|	|	|	|	1.78
30.750	0.00	0.18	0.517	o	|	|	|	|	1.78
30.833	0.00	0.18	0.515	o	|	|	|	|	1.78
30.917	0.00	0.18	0.514	o	|	|	|	|	1.77
31.000	0.00	0.18	0.513	o	|	|	|	|	1.77
31.083	0.00	0.18	0.512	o	|	|	|	|	1.76
31.167	0.00	0.18	0.510	o	|	|	|	|	1.76
31.250	0.00	0.18	0.509	o	|	|	|	|	1.76
31.333	0.00	0.18	0.508	o	|	|	|	|	1.75
31.417	0.00	0.18	0.507	o	|	|	|	|	1.75
31.500	0.00	0.18	0.505	o	|	|	|	|	1.74
31.583	0.00	0.18	0.504	o	|	|	|	|	1.74
31.667	0.00	0.18	0.503	o	|	|	|	|	1.74
31.750	0.00	0.18	0.502	o	|	|	|	|	1.73
31.833	0.00	0.18	0.501	o	|	|	|	|	1.73
31.917	0.00	0.18	0.499	o	|	|	|	|	1.73
32.000	0.00	0.18	0.498	o	|	|	|	|	1.72
32.083	0.00	0.18	0.497	o	|	|	|	|	1.72
32.167	0.00	0.18	0.496	o	|	|	|	|	1.71
32.250	0.00	0.18	0.494	o	|	|	|	|	1.71
32.333	0.00	0.18	0.493	o	|	|	|	|	1.71
32.417	0.00	0.18	0.492	o	|	|	|	|	1.70
32.500	0.00	0.17	0.491	o	|	|	|	|	1.70
32.583	0.00	0.17	0.490	o	|	|	|	|	1.69
32.667	0.00	0.17	0.488	o	|	|	|	|	1.69
32.750	0.00	0.17	0.487	o	|	|	|	|	1.69
32.833	0.00	0.17	0.486	o	|	|	|	|	1.68
32.917	0.00	0.17	0.485	o	|	|	|	|	1.68
33.000	0.00	0.17	0.484	o	|	|	|	|	1.67
33.083	0.00	0.17	0.482	o	|	|	|	|	1.67
33.167	0.00	0.17	0.481	o	|	|	|	|	1.67
33.250	0.00	0.17	0.480	o	|	|	|	|	1.66
33.333	0.00	0.17	0.479	o	|	|	|	|	1.66
33.417	0.00	0.17	0.478	o	|	|	|	|	1.65
33.500	0.00	0.17	0.477	o	|	|	|	|	1.65
33.583	0.00	0.17	0.475	o	|	|	|	|	1.65
33.667	0.00	0.17	0.474	o	|	|	|	|	1.64
33.750	0.00	0.17	0.473	o	|	|	|	|	1.64
33.833	0.00	0.17	0.472	o	|	|	|	|	1.64
33.917	0.00	0.17	0.471	o	|	|	|	|	1.63
34.000	0.00	0.17	0.469	o	|	|	|	|	1.63
34.083	0.00	0.17	0.468	o	|	|	|	|	1.62
34.167	0.00	0.17	0.467	o	|	|	|	|	1.62
34.250	0.00	0.17	0.466	o	|	|	|	|	1.62
34.333	0.00	0.17	0.465	o	|	|	|	|	1.61
34.417	0.00	0.17	0.464	o	|	|	|	|	1.61
34.500	0.00	0.17	0.462	o	|	|	|	|	1.61
34.583	0.00	0.17	0.461	o	|	|	|	|	1.60
34.667	0.00	0.17	0.460	o	|	|	|	|	1.60
34.750	0.00	0.17	0.459	o	|	|	|	|	1.59
34.833	0.00	0.17	0.458	o	|	|	|	|	1.59
34.917	0.00	0.17	0.457	o	|	|	|	|	1.59
35.000	0.00	0.17	0.455	o	|	|	|	|	1.58
35.083	0.00	0.17	0.454	o	|	|	|	|	1.58
35.167	0.00	0.17	0.453	o	|	|	|	|	1.58
35.250	0.00	0.17	0.452	o	|	|	|	|	1.57
35.333	0.00	0.17	0.451	o	|	|	|	|	1.57
35.417	0.00	0.17	0.450	o	|	|	|	|	1.56
35.500	0.00	0.17	0.449	o	|	|	|	|	1.56
35.583	0.00	0.17	0.447	o	|	|	|	|	1.56
35.667	0.00	0.17	0.446	o	|	|	|	|	1.55
35.750	0.00	0.17	0.445	o	|	|	|	|	1.55
35.833	0.00	0.17	0.444	o	|	|	|	|	1.55
35.917	0.00	0.17	0.443	o	|	|	|	|	1.54
36.000	0.00	0.17	0.442	o	|	|	|	|	1.54
36.083	0.00	0.17	0.441	o	|	|	|	|	1.53
36.167	0.00	0.16	0.439	o	|	|	|	|	1.53
36.250	0.00	0.16	0.438	o	|	|	|	|	1.53
36.333	0.00	0.16	0.437	o	|	|	|	|	1.52
36.417	0.00	0.16	0.436	o	|	|	|	|	1.52
36.500	0.00	0.16	0.435	o	|	|	|	|	1.52
36.583	0.00	0.16	0.434	o	|	|	|	|	1.51
36.667	0.00	0.16	0.433	o	|	|	|	|	1.51
36.750	0.00	0.16	0.431	o	|	|	|	|	1.50
36.833	0.00	0.16	0.430	o	|	|	|	|	1.50
36.917	0.00	0.16	0.429	o	|	|	|	|	1.50
37.000	0.00	0.16	0.428	o	|	|	|	|	1.49
37.083	0.00	0.16	0.427	o	|	|	|	|	1.49
37.167	0.00	0.16	0.426	o	|	|	|	|	1.49
37.250	0.00	0.16	0.425	o	|	|	|	|	1.48

37.333	0.00	0.16	0.424	o	|	|	|	1.48
37.417	0.00	0.16	0.423	o	|	|	|	1.48
37.500	0.00	0.16	0.421	o	|	|	|	1.47
37.583	0.00	0.16	0.420	o	|	|	|	1.47
37.667	0.00	0.16	0.419	o	|	|	|	1.46
37.750	0.00	0.16	0.418	o	|	|	|	1.46
37.833	0.00	0.16	0.417	o	|	|	|	1.46
37.917	0.00	0.16	0.416	o	|	|	|	1.45
38.000	0.00	0.16	0.415	o	|	|	|	1.45
38.083	0.00	0.16	0.414	o	|	|	|	1.45
38.167	0.00	0.16	0.413	o	|	|	|	1.44
38.250	0.00	0.16	0.411	o	|	|	|	1.44
38.333	0.00	0.16	0.410	o	|	|	|	1.44
38.417	0.00	0.16	0.409	o	|	|	|	1.43
38.500	0.00	0.16	0.408	o	|	|	|	1.43
38.583	0.00	0.16	0.407	o	|	|	|	1.43
38.667	0.00	0.16	0.406	o	|	|	|	1.42
38.750	0.00	0.16	0.405	o	|	|	|	1.42
38.833	0.00	0.16	0.404	o	|	|	|	1.42
38.917	0.00	0.16	0.403	o	|	|	|	1.41
39.000	0.00	0.16	0.402	o	|	|	|	1.41
39.083	0.00	0.16	0.401	o	|	|	|	1.40
39.167	0.00	0.16	0.400	o	|	|	|	1.40
39.250	0.00	0.16	0.398	o	|	|	|	1.40
39.333	0.00	0.16	0.397	o	|	|	|	1.39
39.417	0.00	0.16	0.396	o	|	|	|	1.39
39.500	0.00	0.16	0.395	o	|	|	|	1.39
39.583	0.00	0.16	0.394	o	|	|	|	1.38
39.667	0.00	0.16	0.393	o	|	|	|	1.38
39.750	0.00	0.16	0.392	o	|	|	|	1.38
39.833	0.00	0.16	0.391	o	|	|	|	1.37
39.917	0.00	0.16	0.390	o	|	|	|	1.37
40.000	0.00	0.15	0.389	o	|	|	|	1.37
40.083	0.00	0.15	0.388	o	|	|	|	1.36
40.167	0.00	0.15	0.387	o	|	|	|	1.36
40.250	0.00	0.15	0.386	o	|	|	|	1.36
40.333	0.00	0.15	0.385	o	|	|	|	1.35
40.417	0.00	0.15	0.383	o	|	|	|	1.35
40.500	0.00	0.15	0.382	o	|	|	|	1.35
40.583	0.00	0.15	0.381	o	|	|	|	1.34
40.667	0.00	0.15	0.380	o	|	|	|	1.34
40.750	0.00	0.15	0.379	o	|	|	|	1.34
40.833	0.00	0.15	0.378	o	|	|	|	1.33
40.917	0.00	0.15	0.377	o	|	|	|	1.33
41.000	0.00	0.15	0.376	o	|	|	|	1.32
41.083	0.00	0.15	0.375	o	|	|	|	1.32
41.167	0.00	0.15	0.374	o	|	|	|	1.32
41.250	0.00	0.15	0.373	o	|	|	|	1.31
41.333	0.00	0.15	0.372	o	|	|	|	1.31
41.417	0.00	0.15	0.371	o	|	|	|	1.31
41.500	0.00	0.15	0.370	o	|	|	|	1.30
41.583	0.00	0.15	0.369	o	|	|	|	1.30
41.667	0.00	0.15	0.368	o	|	|	|	1.30
41.750	0.00	0.15	0.367	o	|	|	|	1.29
41.833	0.00	0.15	0.366	o	|	|	|	1.29
41.917	0.00	0.15	0.365	o	|	|	|	1.29
42.000	0.00	0.15	0.364	o	|	|	|	1.28
42.083	0.00	0.15	0.363	o	|	|	|	1.28
42.167	0.00	0.15	0.361	o	|	|	|	1.28
42.250	0.00	0.15	0.360	o	|	|	|	1.27
42.333	0.00	0.15	0.359	o	|	|	|	1.27
42.417	0.00	0.15	0.358	o	|	|	|	1.27
42.500	0.00	0.15	0.357	o	|	|	|	1.26
42.583	0.00	0.15	0.356	o	|	|	|	1.26
42.667	0.00	0.15	0.355	o	|	|	|	1.26
42.750	0.00	0.15	0.354	o	|	|	|	1.25
42.833	0.00	0.15	0.353	o	|	|	|	1.25
42.917	0.00	0.15	0.352	o	|	|	|	1.25
43.000	0.00	0.15	0.351	o	|	|	|	1.24
43.083	0.00	0.15	0.350	o	|	|	|	1.24
43.167	0.00	0.15	0.349	o	|	|	|	1.24
43.250	0.00	0.15	0.348	o	|	|	|	1.23
43.333	0.00	0.15	0.347	o	|	|	|	1.23
43.417	0.00	0.15	0.346	o	|	|	|	1.23
43.500	0.00	0.15	0.345	o	|	|	|	1.22
43.583	0.00	0.15	0.344	o	|	|	|	1.22
43.667	0.00	0.15	0.343	o	|	|	|	1.22
43.750	0.00	0.15	0.342	o	|	|	|	1.21
43.833	0.00	0.15	0.341	o	|	|	|	1.21
43.917	0.00	0.15	0.340	o	|	|	|	1.21
44.000	0.00	0.15	0.339	o	|	|	|	1.21
44.083	0.00	0.15	0.338	o	|	|	|	1.20
44.167	0.00	0.14	0.337	o	|	|	|	1.20
44.250	0.00	0.14	0.336	o	|	|	|	1.20
44.333	0.00	0.14	0.335	o	|	|	|	1.19
44.417	0.00	0.14	0.334	o	|	|	|	1.19

44.500	0.00	0.14	0.333	o	|	|	|	|	1.19
44.583	0.00	0.14	0.332	o	|	|	|	|	1.18
44.667	0.00	0.14	0.331	o	|	|	|	|	1.18
44.750	0.00	0.14	0.330	o	|	|	|	|	1.18
44.833	0.00	0.14	0.329	o	|	|	|	|	1.17
44.917	0.00	0.14	0.328	o	|	|	|	|	1.17
45.000	0.00	0.14	0.327	o	|	|	|	|	1.17
45.083	0.00	0.14	0.326	o	|	|	|	|	1.16
45.167	0.00	0.14	0.325	o	|	|	|	|	1.16
45.250	0.00	0.14	0.324	o	|	|	|	|	1.16
45.333	0.00	0.14	0.323	o	|	|	|	|	1.15
45.417	0.00	0.14	0.322	o	|	|	|	|	1.15
45.500	0.00	0.14	0.321	o	|	|	|	|	1.15
45.583	0.00	0.14	0.320	o	|	|	|	|	1.14
45.667	0.00	0.14	0.319	o	|	|	|	|	1.14
45.750	0.00	0.14	0.318	o	|	|	|	|	1.14
45.833	0.00	0.14	0.317	o	|	|	|	|	1.13
45.917	0.00	0.14	0.316	o	|	|	|	|	1.13
46.000	0.00	0.14	0.316	o	|	|	|	|	1.13
46.083	0.00	0.14	0.315	o	|	|	|	|	1.13
46.167	0.00	0.14	0.314	o	|	|	|	|	1.12
46.250	0.00	0.14	0.313	o	|	|	|	|	1.12
46.333	0.00	0.14	0.312	o	|	|	|	|	1.12
46.417	0.00	0.14	0.311	o	|	|	|	|	1.11
46.500	0.00	0.14	0.310	o	|	|	|	|	1.11
46.583	0.00	0.14	0.309	o	|	|	|	|	1.11
46.667	0.00	0.14	0.308	o	|	|	|	|	1.10
46.750	0.00	0.14	0.307	o	|	|	|	|	1.10
46.833	0.00	0.14	0.306	o	|	|	|	|	1.10
46.917	0.00	0.14	0.305	o	|	|	|	|	1.09
47.000	0.00	0.14	0.304	o	|	|	|	|	1.09
47.083	0.00	0.14	0.303	o	|	|	|	|	1.09
47.167	0.00	0.14	0.302	o	|	|	|	|	1.08
47.250	0.00	0.14	0.301	o	|	|	|	|	1.08
47.333	0.00	0.14	0.300	o	|	|	|	|	1.08
47.417	0.00	0.14	0.299	o	|	|	|	|	1.08
47.500	0.00	0.14	0.298	o	|	|	|	|	1.07
47.583	0.00	0.14	0.297	o	|	|	|	|	1.07
47.667	0.00	0.14	0.296	o	|	|	|	|	1.07
47.750	0.00	0.14	0.295	o	|	|	|	|	1.06
47.833	0.00	0.14	0.295	o	|	|	|	|	1.06
47.917	0.00	0.14	0.294	o	|	|	|	|	1.06
48.000	0.00	0.14	0.293	o	|	|	|	|	1.05
48.083	0.00	0.14	0.292	o	|	|	|	|	1.05
48.167	0.00	0.14	0.291	o	|	|	|	|	1.05
48.250	0.00	0.14	0.290	o	|	|	|	|	1.04
48.333	0.00	0.14	0.289	o	|	|	|	|	1.04
48.417	0.00	0.14	0.288	o	|	|	|	|	1.04
48.500	0.00	0.14	0.287	o	|	|	|	|	1.04
48.583	0.00	0.13	0.286	o	|	|	|	|	1.03
48.667	0.00	0.13	0.285	o	|	|	|	|	1.03
48.750	0.00	0.13	0.284	o	|	|	|	|	1.03
48.833	0.00	0.13	0.283	o	|	|	|	|	1.02
48.917	0.00	0.13	0.282	o	|	|	|	|	1.02
49.000	0.00	0.13	0.281	o	|	|	|	|	1.02
49.083	0.00	0.13	0.281	o	|	|	|	|	1.01
49.167	0.00	0.13	0.280	o	|	|	|	|	1.01
49.250	0.00	0.13	0.279	o	|	|	|	|	1.01
49.333	0.00	0.13	0.278	o	|	|	|	|	1.01
49.417	0.00	0.13	0.277	o	|	|	|	|	1.00
49.500	0.00	0.13	0.276	o	|	|	|	|	1.00
49.583	0.00	0.13	0.275	o	|	|	|	|	1.00
49.667	0.00	0.13	0.274	o	|	|	|	|	0.99
49.750	0.00	0.13	0.273	o	|	|	|	|	0.99
49.833	0.00	0.13	0.272	o	|	|	|	|	0.99
49.917	0.00	0.13	0.271	o	|	|	|	|	0.98
50.000	0.00	0.13	0.271	o	|	|	|	|	0.98
50.083	0.00	0.13	0.270	o	|	|	|	|	0.98
50.167	0.00	0.13	0.269	o	|	|	|	|	0.97
50.250	0.00	0.13	0.268	o	|	|	|	|	0.97
50.333	0.00	0.13	0.267	o	|	|	|	|	0.97
50.417	0.00	0.13	0.266	o	|	|	|	|	0.96
50.500	0.00	0.13	0.265	o	|	|	|	|	0.96
50.583	0.00	0.13	0.264	o	|	|	|	|	0.96
50.667	0.00	0.13	0.263	o	|	|	|	|	0.95
50.750	0.00	0.13	0.263	o	|	|	|	|	0.95
50.833	0.00	0.13	0.262	o	|	|	|	|	0.95
50.917	0.00	0.13	0.261	o	|	|	|	|	0.94
51.000	0.00	0.13	0.260	o	|	|	|	|	0.94
51.083	0.00	0.12	0.259	o	|	|	|	|	0.94
51.167	0.00	0.12	0.258	o	|	|	|	|	0.94
51.250	0.00	0.12	0.257	o	|	|	|	|	0.93
51.333	0.00	0.12	0.257	o	|	|	|	|	0.93
51.417	0.00	0.12	0.256	o	|	|	|	|	0.93
51.500	0.00	0.12	0.255	o	|	|	|	|	0.92
51.583	0.00	0.12	0.254	o	|	|	|	|	0.92

51.667	0.00	0.12	0.253	o	|	|	|	0.92
51.750	0.00	0.12	0.252	o	|	|	|	0.91
51.833	0.00	0.12	0.251	o	|	|	|	0.91
51.917	0.00	0.12	0.251	o	|	|	|	0.91
52.000	0.00	0.12	0.250	o	|	|	|	0.91
52.083	0.00	0.12	0.249	o	|	|	|	0.90
52.167	0.00	0.12	0.248	o	|	|	|	0.90
52.250	0.00	0.12	0.247	o	|	|	|	0.90
52.333	0.00	0.12	0.246	o	|	|	|	0.89
52.417	0.00	0.12	0.246	o	|	|	|	0.89
52.500	0.00	0.12	0.245	o	|	|	|	0.89
52.583	0.00	0.12	0.244	o	|	|	|	0.88
52.667	0.00	0.12	0.243	o	|	|	|	0.88
52.750	0.00	0.12	0.242	o	|	|	|	0.88
52.833	0.00	0.12	0.242	o	|	|	|	0.88
52.917	0.00	0.12	0.241	o	|	|	|	0.87
53.000	0.00	0.12	0.240	o	|	|	|	0.87
53.083	0.00	0.12	0.239	o	|	|	|	0.87
53.167	0.00	0.11	0.238	o	|	|	|	0.86
53.250	0.00	0.11	0.238	o	|	|	|	0.86
53.333	0.00	0.11	0.237	o	|	|	|	0.86
53.417	0.00	0.11	0.236	o	|	|	|	0.86
53.500	0.00	0.11	0.235	o	|	|	|	0.85
53.583	0.00	0.11	0.235	o	|	|	|	0.85
53.667	0.00	0.11	0.234	o	|	|	|	0.85
53.750	0.00	0.11	0.233	o	|	|	|	0.84
53.833	0.00	0.11	0.232	o	|	|	|	0.84
53.917	0.00	0.11	0.231	o	|	|	|	0.84
54.000	0.00	0.11	0.231	o	|	|	|	0.84
54.083	0.00	0.11	0.230	o	|	|	|	0.83
54.167	0.00	0.11	0.229	o	|	|	|	0.83
54.250	0.00	0.11	0.228	o	|	|	|	0.83
54.333	0.00	0.11	0.228	o	|	|	|	0.82
54.417	0.00	0.11	0.227	o	|	|	|	0.82
54.500	0.00	0.11	0.226	o	|	|	|	0.82
54.583	0.00	0.11	0.225	o	|	|	|	0.82
54.667	0.00	0.11	0.225	o	|	|	|	0.81
54.750	0.00	0.11	0.224	o	|	|	|	0.81
54.833	0.00	0.11	0.223	o	|	|	|	0.81
54.917	0.00	0.11	0.222	o	|	|	|	0.81
55.000	0.00	0.11	0.222	o	|	|	|	0.80
55.083	0.00	0.11	0.221	o	|	|	|	0.80
55.167	0.00	0.11	0.220	o	|	|	|	0.80
55.250	0.00	0.11	0.219	o	|	|	|	0.80
55.333	0.00	0.11	0.219	o	|	|	|	0.79
55.417	0.00	0.11	0.218	o	|	|	|	0.79
55.500	0.00	0.10	0.217	o	|	|	|	0.79
55.583	0.00	0.10	0.217	o	|	|	|	0.78
55.667	0.00	0.10	0.216	o	|	|	|	0.78
55.750	0.00	0.10	0.215	o	|	|	|	0.78
55.833	0.00	0.10	0.214	o	|	|	|	0.78
55.917	0.00	0.10	0.214	o	|	|	|	0.77
56.000	0.00	0.10	0.213	o	|	|	|	0.77
56.083	0.00	0.10	0.212	o	|	|	|	0.77
56.167	0.00	0.10	0.212	o	|	|	|	0.77
56.250	0.00	0.10	0.211	o	|	|	|	0.76
56.333	0.00	0.10	0.210	o	|	|	|	0.76
56.417	0.00	0.10	0.210	o	|	|	|	0.76
56.500	0.00	0.10	0.209	o	|	|	|	0.76
56.583	0.00	0.10	0.208	o	|	|	|	0.75
56.667	0.00	0.10	0.207	o	|	|	|	0.75

Remaining water in basin = 0.21 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 680
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 25.327 (CFS)
Total volume = 2.437 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/07/25

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********
From study/file name: pro102410.rte
**********HYDROGRAPH DATA**********
Number of intervals = 292
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 7.094 (CFS)
Total volume = 3.732 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****
++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 292
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.276	0.133	0.276	0.276
2.000	0.584	0.193	0.583	0.585
3.000	0.930	0.700	0.928	0.932
3.500	1.118	0.824	1.115	1.121
4.000	1.316	0.930	1.313	1.319
4.500	1.528	1.024	1.524	1.532
4.750	1.637	1.068	1.633	1.641
5.000	1.749	18.283	1.686	1.812
6.000	2.231	253.655	1.358	3.104

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	1.8	3.55	5.32	7.09	Depth (Ft.)
0.083	0.15	0.00	0.001	O	|	|	|	|	0.00
0.167	0.30	0.00	0.002	OI	|	|	|	|	0.01
0.250	0.34	0.00	0.004	OI	|	|	|	|	0.02
0.333	0.42	0.00	0.007	OI	|	|	|	|	0.02
0.417	0.51	0.00	0.010	O I	|	|	|	|	0.04
0.500	0.53	0.01	0.014	O I	|	|	|	|	0.05
0.583	0.53	0.01	0.017	O I	|	|	|	|	0.06
0.667	0.54	0.01	0.021	O I	|	|	|	|	0.08
0.750	0.54	0.01	0.024	O I	|	|	|	|	0.09
0.833	0.61	0.01	0.028	O I	|	|	|	|	0.10
0.917	0.69	0.02	0.033	O I	|	|	|	|	0.12
1.000	0.70	0.02	0.037	O I	|	|	|	|	0.14
1.083	0.64	0.02	0.042	O I	|	|	|	|	0.15
1.167	0.56	0.02	0.046	O I	|	|	|	|	0.17
1.250	0.55	0.02	0.049	O I	|	|	|	|	0.18
1.333	0.54	0.03	0.053	O I	|	|	|	|	0.19
1.417	0.54	0.03	0.057	O I	|	|	|	|	0.20
1.500	0.54	0.03	0.060	O I	|	|	|	|	0.22
1.583	0.54	0.03	0.064	O I	|	|	|	|	0.23
1.667	0.54	0.03	0.067	O I	|	|	|	|	0.24
1.750	0.54	0.03	0.070	O I	|	|	|	|	0.26
1.833	0.61	0.04	0.074	O I	|	|	|	|	0.27
1.917	0.69	0.04	0.078	O I	|	|	|	|	0.28
2.000	0.70	0.04	0.083	O I	|	|	|	|	0.30
2.083	0.71	0.04	0.087	O I	|	|	|	|	0.32

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2.167   0.71   0.04    0.092  o  I    |       |       |       |    0.33
2.250   0.71   0.05    0.097  o  I    |       |       |       |    0.35
2.333   0.71   0.05    0.101  o  I    |       |       |       |    0.37
2.417   0.71   0.05    0.106  o  I    |       |       |       |    0.38
2.500   0.71   0.05    0.110  o  I    |       |       |       |    0.40
2.583   0.79   0.06    0.115  o  I    |       |       |       |    0.42
2.667   0.87   0.06    0.121  o  I    |       |       |       |    0.44
2.750   0.88   0.06    0.126  o  I    |       |       |       |    0.46
2.833   0.89   0.06    0.132  o   I   |       |       |       |    0.48
2.917   0.89   0.07    0.138  o   I   |       |       |       |    0.50
3.000   0.89   0.07    0.143  o   I   |       |       |       |    0.52
3.083   0.89   0.07    0.149  o   I   |       |       |       |    0.54
3.167   0.89   0.07    0.155  o   I   |       |       |       |    0.56
3.250   0.89   0.08    0.160  o   I   |       |       |       |    0.58
3.333   0.89   0.08    0.166  o   I   |       |       |       |    0.60
3.417   0.89   0.08    0.171  o   I   |       |       |       |    0.62
3.500   0.89   0.09    0.177  o   I   |       |       |       |    0.64
3.583   0.89   0.09    0.183  o   I   |       |       |       |    0.66
3.667   0.89   0.09    0.188  o   I   |       |       |       |    0.68
3.750   0.89   0.09    0.194  o   I   |       |       |       |    0.70
3.833   0.97   0.10    0.199  o   I   |       |       |       |    0.72
3.917   1.05   0.10    0.206  o   I   |       |       |       |    0.74
4.000   1.06   0.10    0.212  o   I   |       |       |       |    0.77
4.083   1.07   0.11    0.219  o   I   |       |       |       |    0.79
4.167   1.07   0.11    0.225  o   I   |       |       |       |    0.82
4.250   1.07   0.11    0.232  o   I   |       |       |       |    0.84
4.333   1.14   0.12    0.239  o    I  |       |       |       |    0.87
4.417   1.22   0.12    0.246  o    I  |       |       |       |    0.89
4.500   1.24   0.12    0.254  o    I  |       |       |       |    0.92
4.583   1.25   0.13    0.262  o    I  |       |       |       |    0.95
4.667   1.25   0.13    0.269  o    I  |       |       |       |    0.98
4.750   1.25   0.13    0.277  o    I  |       |       |       |    1.00
4.833   1.32   0.13    0.285  o    I  |       |       |       |    1.03
4.917   1.40   0.14    0.293  o     I |       |       |       |    1.06
5.000   1.42   0.14    0.302  o     I |       |       |       |    1.09
5.083   1.28   0.14    0.311  o    I  |       |       |       |    1.11
5.167   1.13   0.14    0.318  o    I  |       |       |       |    1.14
5.250   1.09   0.14    0.325  o   I   |       |       |       |    1.16
5.333   1.15   0.14    0.331  o    I  |       |       |       |    1.18
5.417   1.22   0.15    0.338  o    I  |       |       |       |    1.20
5.500   1.24   0.15    0.346  o    I  |       |       |       |    1.23
5.583   1.32   0.15    0.354  o    I  |       |       |       |    1.25
5.667   1.40   0.15    0.362  o     I |       |       |       |    1.28
5.750   1.42   0.15    0.371  o     I |       |       |       |    1.31
5.833   1.43   0.15    0.380  o     I |       |       |       |    1.34
5.917   1.43   0.15    0.388  o     I |       |       |       |    1.36
6.000   1.43   0.16    0.397  o     I |       |       |       |    1.39
6.083   1.50   0.16    0.406  o     I |       |       |       |    1.42
6.167   1.58   0.16    0.416  o      I|       |       |       |    1.45
6.250   1.60   0.16    0.425  o      I|       |       |       |    1.49
6.333   1.61   0.16    0.435  o      I|       |       |       |    1.52
6.417   1.61   0.17    0.445  o      I|       |       |       |    1.55
6.500   1.61   0.17    0.455  o      I|       |       |       |    1.58
6.583   1.68   0.17    0.465  o      I|       |       |       |    1.61
6.667   1.76   0.17    0.476  o      I|       |       |       |    1.65
6.750   1.78   0.17    0.487  o       I       |       |       |    1.69
6.833   1.78   0.18    0.498  o       I       |       |       |    1.72
6.917   1.79   0.18    0.509  o       I       |       |       |    1.76
7.000   1.79   0.18    0.520  o       I       |       |       |    1.79
7.083   1.79   0.18    0.531  o       I       |       |       |    1.83
7.167   1.79   0.18    0.542  o       I       |       |       |    1.86
7.250   1.79   0.19    0.553  o       I       |       |       |    1.90
7.333   1.86   0.19    0.565  o       I       |       |       |    1.94
7.417   1.94   0.19    0.576  o       I       |       |       |    1.98
7.500   1.96   0.20    0.588  o       I       |       |       |    2.01
7.583   2.04   0.22    0.601  o       |I      |       |       |    2.05
7.667   2.12   0.24    0.613  |o      |I      |       |       |    2.09
7.750   2.13   0.26    0.626  |o      |I      |       |       |    2.12
7.833   2.21   0.27    0.640  |o      |I      |       |       |    2.16
7.917   2.30   0.29    0.653  |o      | I     |       |       |    2.20
8.000   2.31   0.31    0.667  |o      | I     |       |       |    2.24
8.083   2.47   0.34    0.681  |o      |  I    |       |       |    2.28
8.167   2.63   0.36    0.696  |o      |  I    |       |       |    2.32
8.250   2.66   0.38    0.712  |o      |   I   |       |       |    2.37
8.333   2.67   0.40    0.728  |o      |   I   |       |       |    2.42
8.417   2.68   0.43    0.743  |o      |   I   |       |       |    2.46
8.500   2.68   0.45    0.759  | o     |   I   |       |       |    2.50
8.583   2.75   0.47    0.774  | o     |   I   |       |       |    2.55
8.667   2.83   0.49    0.790  | o     |   I   |       |       |    2.60
8.750   2.85   0.52    0.806  | o     |   I   |       |       |    2.64
8.833   2.93   0.54    0.822  | o     |    I  |       |       |    2.69
8.917   3.01   0.57    0.839  | o     |    I  |       |       |    2.74
9.000   3.03   0.59    0.856  | o     |    I  |       |       |    2.79
9.083   3.18   0.62    0.873  | o     |     I |       |       |    2.84
9.167   3.34   0.64    0.891  | o     |      I|       |       |    2.89
9.250   3.38   0.67    0.910  |  o    |      I|       |       |    2.94
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9.333	3.46	0.70	0.929	O	I			3.00
9.417	3.55	0.71	0.948	O	I			3.05
9.500	3.56	0.72	0.967	O	I			3.10
9.583	3.64	0.74	0.987	O	I			3.15
9.667	3.73	0.75	1.007	O	I			3.21
9.750	3.74	0.76	1.028	O	I			3.26
9.833	3.82	0.78	1.049	O	I			3.32
9.917	3.90	0.79	1.070	O	I			3.37
10.000	3.92	0.81	1.091	O	I			3.43
10.083	3.42	0.82	1.111	O	I			3.48
10.167	2.87	0.83	1.127	O	I			3.52
10.250	2.75	0.84	1.141	O	I			3.56
10.333	2.70	0.84	1.154	O	I			3.59
10.417	2.68	0.85	1.166	O	I			3.62
10.500	2.68	0.86	1.179	O	I			3.65
10.583	3.04	0.86	1.193	O	I			3.69
10.667	3.44	0.87	1.209	O	I			3.73
10.750	3.52	0.88	1.227	O	I			3.78
10.833	3.56	0.89	1.245	O	I			3.82
10.917	3.57	0.90	1.264	O	I			3.87
11.000	3.57	0.91	1.282	O	I			3.91
11.083	3.50	0.92	1.300	O	I			3.96
11.167	3.42	0.93	1.317	O	I			4.00
11.250	3.40	0.94	1.335	O	I			4.04
11.333	3.40	0.95	1.351	O	I			4.08
11.417	3.39	0.95	1.368	O	I			4.12
11.500	3.39	0.96	1.385	O	I			4.16
11.583	3.25	0.97	1.401	O	I			4.20
11.667	3.09	0.97	1.416	O	I			4.24
11.750	3.06	0.98	1.431	O	I			4.27
11.833	3.12	0.99	1.445	O	I			4.31
11.917	3.19	0.99	1.460	O	I			4.34
12.000	3.21	1.00	1.475	O	I			4.38
12.083	3.72	1.01	1.492	O	I			4.42
12.167	4.28	1.02	1.513	O	I			4.46
12.250	4.40	1.03	1.536	O	I			4.52
12.333	4.52	1.04	1.559	O	I			4.57
12.417	4.62	1.05	1.584	O	I			4.63
12.500	4.64	1.06	1.608	O	I			4.68
12.583	4.79	1.07	1.633	O	I			4.74
12.667	4.95	3.34	1.652	O	I			4.78
12.750	4.98	4.47	1.659	O	I			4.80
12.833	5.07	4.85	1.662	O	I			4.80
12.917	5.15	5.03	1.663	O	I			4.81
13.000	5.17	5.12	1.663	O	I			4.81
13.083	5.91	5.41	1.665	O	I			4.81
13.167	6.73	6.04	1.669	O	I			4.82
13.250	6.92	6.58	1.673	O	I			4.83
13.333	7.01	6.85	1.675	O	I			4.83
13.417	7.07	6.98	1.675	O	I			4.84
13.500	7.09	7.05	1.676	O	I			4.84
13.583	5.89	6.66	1.673	O	I			4.83
13.667	4.55	5.66	1.667	O	I			4.82
13.750	4.27	4.80	1.661	O	I			4.80
13.833	4.16	4.39	1.659	O	I			4.80
13.917	4.11	4.21	1.657	O	I			4.80
14.000	4.11	4.14	1.657	O	I			4.79
14.083	4.40	4.22	1.658	O	I			4.80
14.167	4.72	4.45	1.659	O	I			4.80
14.250	4.79	4.66	1.660	O	I			4.80
14.333	4.75	4.74	1.661	O	I			4.80
14.417	4.67	4.72	1.661	O	I			4.80
14.500	4.66	4.68	1.661	O	I			4.80
14.583	4.65	4.66	1.660	O	I			4.80
14.667	4.65	4.65	1.660	O	I			4.80
14.750	4.65	4.65	1.660	O	I			4.80
14.833	4.57	4.62	1.660	O	I			4.80
14.917	4.49	4.56	1.660	O	I			4.80
15.000	4.48	4.51	1.659	O	I			4.80
15.083	4.40	4.46	1.659	O	I			4.80
15.167	4.31	4.39	1.659	O	I			4.80
15.250	4.30	4.33	1.658	O	I			4.80
15.333	4.22	4.28	1.658	O	I			4.80
15.417	4.14	4.21	1.657	O	I			4.80
15.500	4.12	4.15	1.657	O	I			4.79
15.583	3.82	4.03	1.656	O	I			4.79
15.667	3.50	3.77	1.655	O	I			4.79
15.750	3.43	3.56	1.653	O	I			4.79
15.833	3.41	3.46	1.653	O	I			4.78
15.917	3.39	3.42	1.652	O	I			4.78
16.000	3.39	3.40	1.652	O	I			4.78
16.083	2.30	3.02	1.650	O	I			4.78
16.167	1.11	2.11	1.644	O	I			4.77
16.250	0.86	1.33	1.639	O	I			4.75
16.333	0.76	1.07	1.636	O	I			4.75
16.417	0.71	1.07	1.634	O	I			4.74

16.500	0.71	1.07	1.631	IO				4.74
16.583	0.64	1.06	1.629	I O				4.73
16.667	0.56	1.06	1.625	I O				4.72
16.750	0.55	1.06	1.622	I O				4.72
16.833	0.54	1.06	1.618	I O				4.71
16.917	0.54	1.06	1.615	I O				4.70
17.000	0.54	1.06	1.611	I O				4.69
17.083	0.68	1.06	1.608	IO				4.68
17.167	0.84	1.06	1.606	IO				4.68
17.250	0.87	1.05	1.605	IO				4.68
17.333	0.89	1.05	1.604	O				4.67
17.417	0.89	1.05	1.602	O				4.67
17.500	0.89	1.05	1.601	O				4.67
17.583	0.89	1.05	1.600	O				4.67
17.667	0.89	1.05	1.599	O				4.66
17.750	0.89	1.05	1.598	O				4.66
17.833	0.82	1.05	1.597	IO				4.66
17.917	0.74	1.05	1.595	IO				4.65
18.000	0.72	1.05	1.593	IO				4.65
18.083	0.72	1.05	1.590	IO				4.64
18.167	0.71	1.05	1.588	IO				4.64
18.250	0.71	1.05	1.586	IO				4.63
18.333	0.71	1.05	1.583	IO				4.63
18.417	0.71	1.05	1.581	IO				4.62
18.500	0.71	1.04	1.579	IO				4.62
18.583	0.64	1.04	1.576	I O				4.61
18.667	0.56	1.04	1.573	I O				4.60
18.750	0.55	1.04	1.570	I O				4.60
18.833	0.47	1.04	1.566	I O				4.59
18.917	0.38	1.04	1.562	I O				4.58
19.000	0.37	1.04	1.558	I O				4.57
19.083	0.43	1.03	1.553	I O				4.56
19.167	0.51	1.03	1.549	I O				4.55
19.250	0.53	1.03	1.546	I O				4.54
19.333	0.61	1.03	1.543	I O				4.53
19.417	0.69	1.03	1.540	IO				4.53
19.500	0.70	1.03	1.538	IO				4.52
19.583	0.64	1.03	1.535	I O				4.52
19.667	0.56	1.03	1.532	I O				4.51
19.750	0.55	1.02	1.529	I O				4.50
19.833	0.47	1.02	1.525	I O				4.49
19.917	0.38	1.02	1.521	I O				4.48
20.000	0.37	1.02	1.517	I O				4.47
20.083	0.43	1.02	1.513	I O				4.46
20.167	0.51	1.02	1.509	I O				4.45
20.250	0.53	1.01	1.505	I O				4.45
20.333	0.53	1.01	1.502	I O				4.44
20.417	0.54	1.01	1.499	I O				4.43
20.500	0.54	1.01	1.496	I O				4.42
20.583	0.54	1.01	1.492	I O				4.42
20.667	0.54	1.01	1.489	I O				4.41
20.750	0.54	1.01	1.486	I O				4.40
20.833	0.46	1.00	1.482	I O				4.39
20.917	0.38	1.00	1.478	I O				4.38
21.000	0.37	1.00	1.474	I O				4.37
21.083	0.43	1.00	1.470	I O				4.36
21.167	0.51	1.00	1.466	I O				4.35
21.250	0.53	1.00	1.463	I O				4.35
21.333	0.46	0.99	1.460	I O				4.34
21.417	0.38	0.99	1.456	I O				4.33
21.500	0.37	0.99	1.451	I O				4.32
21.583	0.43	0.99	1.447	I O				4.31
21.667	0.51	0.99	1.444	I O				4.30
21.750	0.53	0.99	1.441	I O				4.29
21.833	0.46	0.98	1.437	I O				4.29
21.917	0.38	0.98	1.433	I O				4.28
22.000	0.37	0.98	1.429	I O				4.27
22.083	0.43	0.98	1.425	I O				4.26
22.167	0.51	0.98	1.422	I O				4.25
22.250	0.53	0.98	1.419	I O				4.24
22.333	0.46	0.97	1.415	I O				4.23
22.417	0.38	0.97	1.411	I O				4.23
22.500	0.37	0.97	1.407	I O				4.22
22.583	0.36	0.97	1.403	I O				4.21
22.667	0.36	0.97	1.399	I O				4.20
22.750	0.36	0.96	1.395	I O				4.19
22.833	0.36	0.96	1.391	I O				4.18
22.917	0.36	0.96	1.386	I O				4.17
23.000	0.36	0.96	1.382	I O				4.16
23.083	0.36	0.96	1.378	I O				4.15
23.167	0.36	0.96	1.374	I O				4.14
23.250	0.36	0.95	1.370	I O				4.13
23.333	0.36	0.95	1.366	I O				4.12
23.417	0.36	0.95	1.362	I O				4.11
23.500	0.36	0.95	1.358	I O				4.10
23.583	0.36	0.95	1.354	I O				4.09

23.667	0.36	0.94	1.349	|I o	|	|	|	4.08
23.750	0.36	0.94	1.345	|I o	|	|	|	4.07
23.833	0.36	0.94	1.341	|I o	|	|	|	4.06
23.917	0.36	0.94	1.337	|I o	|	|	|	4.05
24.000	0.36	0.94	1.333	|I o	|	|	|	4.04
24.083	0.21	0.94	1.329	I o	|	|	|	4.03
24.167	0.05	0.93	1.323	I o	|	|	|	4.02
24.250	0.02	0.93	1.317	I o	|	|	|	4.00
24.333	0.01	0.93	1.311	I o	|	|	|	3.99
24.417	0.00	0.92	1.305	I o	|	|	|	3.97
24.500	0.00	0.92	1.298	I o	|	|	|	3.96
24.583	0.00	0.92	1.292	I o	|	|	|	3.94
24.667	0.00	0.91	1.286	I o	|	|	|	3.92
24.750	0.00	0.91	1.279	I o	|	|	|	3.91
24.833	0.00	0.91	1.273	I o	|	|	|	3.89
24.917	0.00	0.90	1.267	I o	|	|	|	3.88
25.000	0.00	0.90	1.261	I o	|	|	|	3.86
25.083	0.00	0.90	1.254	I o	|	|	|	3.84
25.167	0.00	0.89	1.248	I o	|	|	|	3.83
25.250	0.00	0.89	1.242	I o	|	|	|	3.81
25.333	0.00	0.89	1.236	I o	|	|	|	3.80
25.417	0.00	0.88	1.230	I o	|	|	|	3.78
25.500	0.00	0.88	1.224	I o	|	|	|	3.77
25.583	0.00	0.88	1.218	I o	|	|	|	3.75
25.667	0.00	0.87	1.212	I o	|	|	|	3.74
25.750	0.00	0.87	1.206	I o	|	|	|	3.72
25.833	0.00	0.87	1.200	I o	|	|	|	3.71
25.917	0.00	0.86	1.194	I o	|	|	|	3.69
26.000	0.00	0.86	1.188	I o	|	|	|	3.68
26.083	0.00	0.86	1.182	I o	|	|	|	3.66
26.167	0.00	0.86	1.176	I o	|	|	|	3.65
26.250	0.00	0.85	1.170	I o	|	|	|	3.63
26.333	0.00	0.85	1.164	I o	|	|	|	3.62
26.417	0.00	0.85	1.158	I o	|	|	|	3.60
26.500	0.00	0.84	1.153	I o	|	|	|	3.59
26.583	0.00	0.84	1.147	I o	|	|	|	3.57
26.667	0.00	0.84	1.141	I o	|	|	|	3.56
26.750	0.00	0.83	1.135	I o	|	|	|	3.54
26.833	0.00	0.83	1.130	I o	|	|	|	3.53
26.917	0.00	0.83	1.124	I o	|	|	|	3.51
27.000	0.00	0.82	1.118	I o	|	|	|	3.50
27.083	0.00	0.82	1.113	I o	|	|	|	3.49
27.167	0.00	0.82	1.107	I o	|	|	|	3.47
27.250	0.00	0.81	1.101	I o	|	|	|	3.46
27.333	0.00	0.81	1.096	I o	|	|	|	3.44
27.417	0.00	0.81	1.090	I o	|	|	|	3.43
27.500	0.00	0.80	1.085	I o	|	|	|	3.41
27.583	0.00	0.80	1.079	I o	|	|	|	3.40
27.667	0.00	0.79	1.074	I o	|	|	|	3.38
27.750	0.00	0.79	1.068	I o	|	|	|	3.37
27.833	0.00	0.79	1.063	I o	|	|	|	3.35
27.917	0.00	0.78	1.057	I o	|	|	|	3.34
28.000	0.00	0.78	1.052	I o	|	|	|	3.32
28.083	0.00	0.78	1.047	I o	|	|	|	3.31
28.167	0.00	0.77	1.041	I o	|	|	|	3.30
28.250	0.00	0.77	1.036	I o	|	|	|	3.28
28.333	0.00	0.77	1.031	I o	|	|	|	3.27
28.417	0.00	0.76	1.025	I o	|	|	|	3.25
28.500	0.00	0.76	1.020	I o	|	|	|	3.24
28.583	0.00	0.76	1.015	I o	|	|	|	3.23
28.667	0.00	0.75	1.010	I o	|	|	|	3.21
28.750	0.00	0.75	1.004	I o	|	|	|	3.20
28.833	0.00	0.75	0.999	I o	|	|	|	3.18
28.917	0.00	0.74	0.994	I o	|	|	|	3.17
29.000	0.00	0.74	0.989	I o	|	|	|	3.16
29.083	0.00	0.74	0.984	I o	|	|	|	3.14
29.167	0.00	0.73	0.979	I o	|	|	|	3.13
29.250	0.00	0.73	0.974	I o	|	|	|	3.12
29.333	0.00	0.73	0.969	I o	|	|	|	3.10
29.417	0.00	0.72	0.964	I o	|	|	|	3.09
29.500	0.00	0.72	0.959	I o	|	|	|	3.08
29.583	0.00	0.72	0.954	I o	|	|	|	3.06
29.667	0.00	0.71	0.949	I o	|	|	|	3.05
29.750	0.00	0.71	0.944	I o	|	|	|	3.04
29.833	0.00	0.71	0.939	I o	|	|	|	3.02
29.917	0.00	0.70	0.935	I o	|	|	|	3.01
30.000	0.00	0.70	0.930	I o	|	|	|	3.00
30.083	0.00	0.69	0.925	I o	|	|	|	2.99
30.167	0.00	0.69	0.920	I o	|	|	|	2.97
30.250	0.00	0.68	0.915	I o	|	|	|	2.96
30.333	0.00	0.67	0.911	I o	|	|	|	2.94
30.417	0.00	0.67	0.906	I o	|	|	|	2.93
30.500	0.00	0.66	0.902	I o	|	|	|	2.92
30.583	0.00	0.65	0.897	I o	|	|	|	2.90
30.667	0.00	0.65	0.893	I o	|	|	|	2.89
30.750	0.00	0.64	0.888	I o	|	|	|	2.88

30.833	0.00	0.63	0.884	I O	|	|	|	2.87
30.917	0.00	0.63	0.880	I O	|	|	|	2.85
31.000	0.00	0.62	0.875	I O	|	|	|	2.84
31.083	0.00	0.61	0.871	I O	|	|	|	2.83
31.167	0.00	0.61	0.867	I O	|	|	|	2.82
31.250	0.00	0.60	0.863	I O	|	|	|	2.81
31.333	0.00	0.60	0.858	I O	|	|	|	2.79
31.417	0.00	0.59	0.854	I O	|	|	|	2.78
31.500	0.00	0.58	0.850	I O	|	|	|	2.77
31.583	0.00	0.58	0.846	I O	|	|	|	2.76
31.667	0.00	0.57	0.842	I O	|	|	|	2.75
31.750	0.00	0.57	0.839	I O	|	|	|	2.74
31.833	0.00	0.56	0.835	I O	|	|	|	2.72
31.917	0.00	0.55	0.831	I O	|	|	|	2.71
32.000	0.00	0.55	0.827	I O	|	|	|	2.70
32.083	0.00	0.54	0.823	I O	|	|	|	2.69
32.167	0.00	0.54	0.820	I O	|	|	|	2.68
32.250	0.00	0.53	0.816	I O	|	|	|	2.67
32.333	0.00	0.53	0.812	I O	|	|	|	2.66
32.417	0.00	0.52	0.809	I O	|	|	|	2.65
32.500	0.00	0.52	0.805	I O	|	|	|	2.64
32.583	0.00	0.51	0.801	I O	|	|	|	2.63
32.667	0.00	0.51	0.798	I O	|	|	|	2.62
32.750	0.00	0.50	0.794	I O	|	|	|	2.61
32.833	0.00	0.50	0.791	I O	|	|	|	2.60
32.917	0.00	0.49	0.788	I O	|	|	|	2.59
33.000	0.00	0.49	0.784	I O	|	|	|	2.58
33.083	0.00	0.48	0.781	I O	|	|	|	2.57
33.167	0.00	0.48	0.778	I O	|	|	|	2.56
33.250	0.00	0.47	0.774	I O	|	|	|	2.55
33.333	0.00	0.47	0.771	I O	|	|	|	2.54
33.417	0.00	0.46	0.768	I O	|	|	|	2.53
33.500	0.00	0.46	0.765	I O	|	|	|	2.52
33.583	0.00	0.45	0.762	I O	|	|	|	2.51
33.667	0.00	0.45	0.759	I O	|	|	|	2.50
33.750	0.00	0.44	0.755	I O	|	|	|	2.50
33.833	0.00	0.44	0.752	IO	|	|	|	2.49
33.917	0.00	0.44	0.749	IO	|	|	|	2.48
34.000	0.00	0.43	0.746	IO	|	|	|	2.47
34.083	0.00	0.43	0.743	IO	|	|	|	2.46
34.167	0.00	0.42	0.741	IO	|	|	|	2.45
34.250	0.00	0.42	0.738	IO	|	|	|	2.44
34.333	0.00	0.41	0.735	IO	|	|	|	2.44
34.417	0.00	0.41	0.732	IO	|	|	|	2.43
34.500	0.00	0.41	0.729	IO	|	|	|	2.42
34.583	0.00	0.40	0.726	IO	|	|	|	2.41
34.667	0.00	0.40	0.724	IO	|	|	|	2.40
34.750	0.00	0.39	0.721	IO	|	|	|	2.40
34.833	0.00	0.39	0.718	IO	|	|	|	2.39
34.917	0.00	0.39	0.715	IO	|	|	|	2.38
35.000	0.00	0.38	0.713	IO	|	|	|	2.37
35.083	0.00	0.38	0.710	IO	|	|	|	2.36
35.167	0.00	0.37	0.708	IO	|	|	|	2.36
35.250	0.00	0.37	0.705	IO	|	|	|	2.35
35.333	0.00	0.37	0.703	IO	|	|	|	2.34
35.417	0.00	0.36	0.700	IO	|	|	|	2.34
35.500	0.00	0.36	0.698	IO	|	|	|	2.33
35.583	0.00	0.36	0.695	IO	|	|	|	2.32
35.667	0.00	0.35	0.693	IO	|	|	|	2.31
35.750	0.00	0.35	0.690	IO	|	|	|	2.31
35.833	0.00	0.35	0.688	IO	|	|	|	2.30
35.917	0.00	0.34	0.685	IO	|	|	|	2.29
36.000	0.00	0.34	0.683	IO	|	|	|	2.29
36.083	0.00	0.33	0.681	IO	|	|	|	2.28
36.167	0.00	0.33	0.679	IO	|	|	|	2.27
36.250	0.00	0.33	0.676	IO	|	|	|	2.27
36.333	0.00	0.32	0.674	IO	|	|	|	2.26
36.417	0.00	0.32	0.672	IO	|	|	|	2.25
36.500	0.00	0.32	0.670	IO	|	|	|	2.25
36.583	0.00	0.32	0.667	IO	|	|	|	2.24
36.667	0.00	0.31	0.665	IO	|	|	|	2.23
36.750	0.00	0.31	0.663	IO	|	|	|	2.23
36.833	0.00	0.31	0.661	IO	|	|	|	2.22
36.917	0.00	0.30	0.659	IO	|	|	|	2.22
37.000	0.00	0.30	0.657	IO	|	|	|	2.21
37.083	0.00	0.30	0.655	IO	|	|	|	2.20
37.167	0.00	0.29	0.653	IO	|	|	|	2.20
37.250	0.00	0.29	0.651	IO	|	|	|	2.19
37.333	0.00	0.29	0.649	IO	|	|	|	2.19
37.417	0.00	0.28	0.647	IO	|	|	|	2.18
37.500	0.00	0.28	0.645	IO	|	|	|	2.18
37.583	0.00	0.28	0.643	IO	|	|	|	2.17
37.667	0.00	0.28	0.641	IO	|	|	|	2.16
37.750	0.00	0.27	0.639	IO	|	|	|	2.16
37.833	0.00	0.27	0.637	IO	|	|	|	2.15
37.917	0.00	0.27	0.635	IO	|	|	|	2.15

38.000	0.00	0.27	0.633	IO					2.14
38.083	0.00	0.26	0.632	IO					2.14
38.167	0.00	0.26	0.630	IO					2.13
38.250	0.00	0.26	0.628	IO					2.13
38.333	0.00	0.25	0.626	IO					2.12
38.417	0.00	0.25	0.625	IO					2.12
38.500	0.00	0.25	0.623	IO					2.11
38.583	0.00	0.25	0.621	IO					2.11
38.667	0.00	0.24	0.619	IO					2.10
38.750	0.00	0.24	0.618	IO					2.10
38.833	0.00	0.24	0.616	IO					2.09
38.917	0.00	0.24	0.614	IO					2.09
39.000	0.00	0.24	0.613	IO					2.08
39.083	0.00	0.23	0.611	IO					2.08
39.167	0.00	0.23	0.610	IO					2.07
39.250	0.00	0.23	0.608	IO					2.07
39.333	0.00	0.23	0.606	IO					2.06
39.417	0.00	0.22	0.605	IO					2.06
39.500	0.00	0.22	0.603	O					2.06
39.583	0.00	0.22	0.602	O					2.05
39.667	0.00	0.22	0.600	O					2.05
39.750	0.00	0.21	0.599	O					2.04
39.833	0.00	0.21	0.597	O					2.04
39.917	0.00	0.21	0.596	O					2.03
40.000	0.00	0.21	0.594	O					2.03
40.083	0.00	0.21	0.593	O					2.03
40.167	0.00	0.20	0.592	O					2.02
40.250	0.00	0.20	0.590	O					2.02
40.333	0.00	0.20	0.589	O					2.01
40.417	0.00	0.20	0.588	O					2.01
40.500	0.00	0.20	0.586	O					2.01
40.583	0.00	0.19	0.585	O					2.00
40.667	0.00	0.19	0.583	O					2.00
40.750	0.00	0.19	0.582	O					1.99
40.833	0.00	0.19	0.581	O					1.99
40.917	0.00	0.19	0.579	O					1.99
41.000	0.00	0.19	0.578	O					1.98
41.083	0.00	0.19	0.577	O					1.98
41.167	0.00	0.19	0.576	O					1.97
41.250	0.00	0.19	0.574	O					1.97
41.333	0.00	0.19	0.573	O					1.96
41.417	0.00	0.19	0.572	O					1.96
41.500	0.00	0.19	0.570	O					1.96
41.583	0.00	0.19	0.569	O					1.95
41.667	0.00	0.19	0.568	O					1.95
41.750	0.00	0.19	0.566	O					1.94
41.833	0.00	0.19	0.565	O					1.94
41.917	0.00	0.19	0.564	O					1.93
42.000	0.00	0.19	0.562	O					1.93
42.083	0.00	0.19	0.561	O					1.93
42.167	0.00	0.19	0.560	O					1.92
42.250	0.00	0.19	0.559	O					1.92
42.333	0.00	0.19	0.557	O					1.91
42.417	0.00	0.19	0.556	O					1.91
42.500	0.00	0.19	0.555	O					1.90
42.583	0.00	0.19	0.553	O					1.90
42.667	0.00	0.19	0.552	O					1.90
42.750	0.00	0.19	0.551	O					1.89
42.833	0.00	0.19	0.550	O					1.89
42.917	0.00	0.19	0.548	O					1.88
43.000	0.00	0.19	0.547	O					1.88
43.083	0.00	0.19	0.546	O					1.88
43.167	0.00	0.19	0.544	O					1.87
43.250	0.00	0.19	0.543	O					1.87
43.333	0.00	0.18	0.542	O					1.86
43.417	0.00	0.18	0.541	O					1.86
43.500	0.00	0.18	0.539	O					1.85
43.583	0.00	0.18	0.538	O					1.85
43.667	0.00	0.18	0.537	O					1.85
43.750	0.00	0.18	0.536	O					1.84
43.833	0.00	0.18	0.534	O					1.84
43.917	0.00	0.18	0.533	O					1.83
44.000	0.00	0.18	0.532	O					1.83
44.083	0.00	0.18	0.530	O					1.83
44.167	0.00	0.18	0.529	O					1.82
44.250	0.00	0.18	0.528	O					1.82
44.333	0.00	0.18	0.527	O					1.81
44.417	0.00	0.18	0.525	O					1.81
44.500	0.00	0.18	0.524	O					1.81
44.583	0.00	0.18	0.523	O					1.80
44.667	0.00	0.18	0.522	O					1.80
44.750	0.00	0.18	0.520	O					1.79
44.833	0.00	0.18	0.519	O					1.79
44.917	0.00	0.18	0.518	O					1.79
45.000	0.00	0.18	0.517	O					1.78
45.083	0.00	0.18	0.516	O					1.78

45.167	0.00	0.18	0.514	o	|	|	|	|	1.77
45.250	0.00	0.18	0.513	o	|	|	|	|	1.77
45.333	0.00	0.18	0.512	o	|	|	|	|	1.77
45.417	0.00	0.18	0.511	o	|	|	|	|	1.76
45.500	0.00	0.18	0.509	o	|	|	|	|	1.76
45.583	0.00	0.18	0.508	o	|	|	|	|	1.75
45.667	0.00	0.18	0.507	o	|	|	|	|	1.75
45.750	0.00	0.18	0.506	o	|	|	|	|	1.75
45.833	0.00	0.18	0.504	o	|	|	|	|	1.74
45.917	0.00	0.18	0.503	o	|	|	|	|	1.74
46.000	0.00	0.18	0.502	o	|	|	|	|	1.73
46.083	0.00	0.18	0.501	o	|	|	|	|	1.73
46.167	0.00	0.18	0.500	o	|	|	|	|	1.73
46.250	0.00	0.18	0.498	o	|	|	|	|	1.72
46.333	0.00	0.18	0.497	o	|	|	|	|	1.72
46.417	0.00	0.18	0.496	o	|	|	|	|	1.71
46.500	0.00	0.18	0.495	o	|	|	|	|	1.71
46.583	0.00	0.18	0.493	o	|	|	|	|	1.71
46.667	0.00	0.18	0.492	o	|	|	|	|	1.70
46.750	0.00	0.17	0.491	o	|	|	|	|	1.70
46.833	0.00	0.17	0.490	o	|	|	|	|	1.69
46.917	0.00	0.17	0.489	o	|	|	|	|	1.69
47.000	0.00	0.17	0.487	o	|	|	|	|	1.69
47.083	0.00	0.17	0.486	o	|	|	|	|	1.68
47.167	0.00	0.17	0.485	o	|	|	|	|	1.68
47.250	0.00	0.17	0.484	o	|	|	|	|	1.67
47.333	0.00	0.17	0.483	o	|	|	|	|	1.67
47.417	0.00	0.17	0.482	o	|	|	|	|	1.67
47.500	0.00	0.17	0.480	o	|	|	|	|	1.66
47.583	0.00	0.17	0.479	o	|	|	|	|	1.66
47.667	0.00	0.17	0.478	o	|	|	|	|	1.66
47.750	0.00	0.17	0.477	o	|	|	|	|	1.65
47.833	0.00	0.17	0.476	o	|	|	|	|	1.65
47.917	0.00	0.17	0.474	o	|	|	|	|	1.64
48.000	0.00	0.17	0.473	o	|	|	|	|	1.64
48.083	0.00	0.17	0.472	o	|	|	|	|	1.64
48.167	0.00	0.17	0.471	o	|	|	|	|	1.63
48.250	0.00	0.17	0.470	o	|	|	|	|	1.63
48.333	0.00	0.17	0.468	o	|	|	|	|	1.62
48.417	0.00	0.17	0.467	o	|	|	|	|	1.62
48.500	0.00	0.17	0.466	o	|	|	|	|	1.62
48.583	0.00	0.17	0.465	o	|	|	|	|	1.61
48.667	0.00	0.17	0.464	o	|	|	|	|	1.61
48.750	0.00	0.17	0.463	o	|	|	|	|	1.61
48.833	0.00	0.17	0.461	o	|	|	|	|	1.60
48.917	0.00	0.17	0.460	o	|	|	|	|	1.60
49.000	0.00	0.17	0.459	o	|	|	|	|	1.59
49.083	0.00	0.17	0.458	o	|	|	|	|	1.59
49.167	0.00	0.17	0.457	o	|	|	|	|	1.59
49.250	0.00	0.17	0.456	o	|	|	|	|	1.58
49.333	0.00	0.17	0.455	o	|	|	|	|	1.58
49.417	0.00	0.17	0.453	o	|	|	|	|	1.58
49.500	0.00	0.17	0.452	o	|	|	|	|	1.57
49.583	0.00	0.17	0.451	o	|	|	|	|	1.57
49.667	0.00	0.17	0.450	o	|	|	|	|	1.56
49.750	0.00	0.17	0.449	o	|	|	|	|	1.56
49.833	0.00	0.17	0.448	o	|	|	|	|	1.56
49.917	0.00	0.17	0.446	o	|	|	|	|	1.55
50.000	0.00	0.17	0.445	o	|	|	|	|	1.55
50.083	0.00	0.17	0.444	o	|	|	|	|	1.55
50.167	0.00	0.17	0.443	o	|	|	|	|	1.54
50.250	0.00	0.17	0.442	o	|	|	|	|	1.54
50.333	0.00	0.17	0.441	o	|	|	|	|	1.53
50.417	0.00	0.16	0.440	o	|	|	|	|	1.53
50.500	0.00	0.16	0.438	o	|	|	|	|	1.53
50.583	0.00	0.16	0.437	o	|	|	|	|	1.52
50.667	0.00	0.16	0.436	o	|	|	|	|	1.52
50.750	0.00	0.16	0.435	o	|	|	|	|	1.52
50.833	0.00	0.16	0.434	o	|	|	|	|	1.51
50.917	0.00	0.16	0.433	o	|	|	|	|	1.51
51.000	0.00	0.16	0.432	o	|	|	|	|	1.51
51.083	0.00	0.16	0.431	o	|	|	|	|	1.50
51.167	0.00	0.16	0.429	o	|	|	|	|	1.50
51.250	0.00	0.16	0.428	o	|	|	|	|	1.49
51.333	0.00	0.16	0.427	o	|	|	|	|	1.49
51.417	0.00	0.16	0.426	o	|	|	|	|	1.49
51.500	0.00	0.16	0.425	o	|	|	|	|	1.48
51.583	0.00	0.16	0.424	o	|	|	|	|	1.48
51.667	0.00	0.16	0.423	o	|	|	|	|	1.48
51.750	0.00	0.16	0.422	o	|	|	|	|	1.47
51.833	0.00	0.16	0.421	o	|	|	|	|	1.47
51.917	0.00	0.16	0.419	o	|	|	|	|	1.47
52.000	0.00	0.16	0.418	o	|	|	|	|	1.46
52.083	0.00	0.16	0.417	o	|	|	|	|	1.46
52.167	0.00	0.16	0.416	o	|	|	|	|	1.45
52.250	0.00	0.16	0.415	o	|	|	|	|	1.45

52.333	0.00	0.16	0.414	o	|	|	|	|	1.45
52.417	0.00	0.16	0.413	o	|	|	|	|	1.44
52.500	0.00	0.16	0.412	o	|	|	|	|	1.44
52.583	0.00	0.16	0.411	o	|	|	|	|	1.44
52.667	0.00	0.16	0.410	o	|	|	|	|	1.43
52.750	0.00	0.16	0.408	o	|	|	|	|	1.43
52.833	0.00	0.16	0.407	o	|	|	|	|	1.43
52.917	0.00	0.16	0.406	o	|	|	|	|	1.42
53.000	0.00	0.16	0.405	o	|	|	|	|	1.42
53.083	0.00	0.16	0.404	o	|	|	|	|	1.42
53.167	0.00	0.16	0.403	o	|	|	|	|	1.41
53.250	0.00	0.16	0.402	o	|	|	|	|	1.41
53.333	0.00	0.16	0.401	o	|	|	|	|	1.41
53.417	0.00	0.16	0.400	o	|	|	|	|	1.40
53.500	0.00	0.16	0.399	o	|	|	|	|	1.40
53.583	0.00	0.16	0.398	o	|	|	|	|	1.39
53.667	0.00	0.16	0.396	o	|	|	|	|	1.39
53.750	0.00	0.16	0.395	o	|	|	|	|	1.39
53.833	0.00	0.16	0.394	o	|	|	|	|	1.38
53.917	0.00	0.16	0.393	o	|	|	|	|	1.38
54.000	0.00	0.16	0.392	o	|	|	|	|	1.38
54.083	0.00	0.16	0.391	o	|	|	|	|	1.37
54.167	0.00	0.16	0.390	o	|	|	|	|	1.37
54.250	0.00	0.16	0.389	o	|	|	|	|	1.37
54.333	0.00	0.15	0.388	o	|	|	|	|	1.36
54.417	0.00	0.15	0.387	o	|	|	|	|	1.36
54.500	0.00	0.15	0.386	o	|	|	|	|	1.36
54.583	0.00	0.15	0.385	o	|	|	|	|	1.35
54.667	0.00	0.15	0.384	o	|	|	|	|	1.35
54.750	0.00	0.15	0.383	o	|	|	|	|	1.35
54.833	0.00	0.15	0.382	o	|	|	|	|	1.34
54.917	0.00	0.15	0.380	o	|	|	|	|	1.34
55.000	0.00	0.15	0.379	o	|	|	|	|	1.34
55.083	0.00	0.15	0.378	o	|	|	|	|	1.33
55.167	0.00	0.15	0.377	o	|	|	|	|	1.33
55.250	0.00	0.15	0.376	o	|	|	|	|	1.33
55.333	0.00	0.15	0.375	o	|	|	|	|	1.32
55.417	0.00	0.15	0.374	o	|	|	|	|	1.32
55.500	0.00	0.15	0.373	o	|	|	|	|	1.32
55.583	0.00	0.15	0.372	o	|	|	|	|	1.31
55.667	0.00	0.15	0.371	o	|	|	|	|	1.31
55.750	0.00	0.15	0.370	o	|	|	|	|	1.31
55.833	0.00	0.15	0.369	o	|	|	|	|	1.30
55.917	0.00	0.15	0.368	o	|	|	|	|	1.30
56.000	0.00	0.15	0.367	o	|	|	|	|	1.30
56.083	0.00	0.15	0.366	o	|	|	|	|	1.29
56.167	0.00	0.15	0.365	o	|	|	|	|	1.29
56.250	0.00	0.15	0.364	o	|	|	|	|	1.28
56.333	0.00	0.15	0.363	o	|	|	|	|	1.28
56.417	0.00	0.15	0.362	o	|	|	|	|	1.28
56.500	0.00	0.15	0.361	o	|	|	|	|	1.27
56.583	0.00	0.15	0.360	o	|	|	|	|	1.27
56.667	0.00	0.15	0.359	o	|	|	|	|	1.27
56.750	0.00	0.15	0.358	o	|	|	|	|	1.26
56.833	0.00	0.15	0.357	o	|	|	|	|	1.26
56.917	0.00	0.15	0.356	o	|	|	|	|	1.26
57.000	0.00	0.15	0.355	o	|	|	|	|	1.25
57.083	0.00	0.15	0.353	o	|	|	|	|	1.25
57.167	0.00	0.15	0.352	o	|	|	|	|	1.25
57.250	0.00	0.15	0.351	o	|	|	|	|	1.24
57.333	0.00	0.15	0.350	o	|	|	|	|	1.24
57.417	0.00	0.15	0.349	o	|	|	|	|	1.24
57.500	0.00	0.15	0.348	o	|	|	|	|	1.24
57.583	0.00	0.15	0.347	o	|	|	|	|	1.23
57.667	0.00	0.15	0.346	o	|	|	|	|	1.23
57.750	0.00	0.15	0.345	o	|	|	|	|	1.23
57.833	0.00	0.15	0.344	o	|	|	|	|	1.22
57.917	0.00	0.15	0.343	o	|	|	|	|	1.22
58.000	0.00	0.15	0.342	o	|	|	|	|	1.22
58.083	0.00	0.15	0.341	o	|	|	|	|	1.21
58.167	0.00	0.15	0.340	o	|	|	|	|	1.21
58.250	0.00	0.15	0.339	o	|	|	|	|	1.21
58.333	0.00	0.15	0.338	o	|	|	|	|	1.20
58.417	0.00	0.14	0.337	o	|	|	|	|	1.20
58.500	0.00	0.14	0.336	o	|	|	|	|	1.20
58.583	0.00	0.14	0.335	o	|	|	|	|	1.19
58.667	0.00	0.14	0.334	o	|	|	|	|	1.19
58.750	0.00	0.14	0.333	o	|	|	|	|	1.19
58.833	0.00	0.14	0.332	o	|	|	|	|	1.18
58.917	0.00	0.14	0.331	o	|	|	|	|	1.18
59.000	0.00	0.14	0.330	o	|	|	|	|	1.18
59.083	0.00	0.14	0.329	o	|	|	|	|	1.17
59.167	0.00	0.14	0.328	o	|	|	|	|	1.17
59.250	0.00	0.14	0.327	o	|	|	|	|	1.17
59.333	0.00	0.14	0.326	o	|	|	|	|	1.16
59.417	0.00	0.14	0.325	o	|	|	|	|	1.16

59.500	0.00	0.14	0.324	o	|	|	|	|	1.16
59.583	0.00	0.14	0.323	o	|	|	|	|	1.15
59.667	0.00	0.14	0.323	o	|	|	|	|	1.15
59.750	0.00	0.14	0.322	o	|	|	|	|	1.15
59.833	0.00	0.14	0.321	o	|	|	|	|	1.14
59.917	0.00	0.14	0.320	o	|	|	|	|	1.14
60.000	0.00	0.14	0.319	o	|	|	|	|	1.14
60.083	0.00	0.14	0.318	o	|	|	|	|	1.14
60.167	0.00	0.14	0.317	o	|	|	|	|	1.13
60.250	0.00	0.14	0.316	o	|	|	|	|	1.13
60.333	0.00	0.14	0.315	o	|	|	|	|	1.13
60.417	0.00	0.14	0.314	o	|	|	|	|	1.12
60.500	0.00	0.14	0.313	o	|	|	|	|	1.12
60.583	0.00	0.14	0.312	o	|	|	|	|	1.12
60.667	0.00	0.14	0.311	o	|	|	|	|	1.11
60.750	0.00	0.14	0.310	o	|	|	|	|	1.11
60.833	0.00	0.14	0.309	o	|	|	|	|	1.11
60.917	0.00	0.14	0.308	o	|	|	|	|	1.10
61.000	0.00	0.14	0.307	o	|	|	|	|	1.10
61.083	0.00	0.14	0.306	o	|	|	|	|	1.10
61.167	0.00	0.14	0.305	o	|	|	|	|	1.09
61.250	0.00	0.14	0.304	o	|	|	|	|	1.09
61.333	0.00	0.14	0.303	o	|	|	|	|	1.09
61.417	0.00	0.14	0.302	o	|	|	|	|	1.09
61.500	0.00	0.14	0.301	o	|	|	|	|	1.08
61.583	0.00	0.14	0.300	o	|	|	|	|	1.08
61.667	0.00	0.14	0.299	o	|	|	|	|	1.08
61.750	0.00	0.14	0.298	o	|	|	|	|	1.07
61.833	0.00	0.14	0.298	o	|	|	|	|	1.07
61.917	0.00	0.14	0.297	o	|	|	|	|	1.07
62.000	0.00	0.14	0.296	o	|	|	|	|	1.06
62.083	0.00	0.14	0.295	o	|	|	|	|	1.06
62.167	0.00	0.14	0.294	o	|	|	|	|	1.06
62.250	0.00	0.14	0.293	o	|	|	|	|	1.05
62.333	0.00	0.14	0.292	o	|	|	|	|	1.05
62.417	0.00	0.14	0.291	o	|	|	|	|	1.05
62.500	0.00	0.14	0.290	o	|	|	|	|	1.05
62.583	0.00	0.14	0.289	o	|	|	|	|	1.04
62.667	0.00	0.14	0.288	o	|	|	|	|	1.04
62.750	0.00	0.14	0.287	o	|	|	|	|	1.04
62.833	0.00	0.14	0.286	o	|	|	|	|	1.03
62.917	0.00	0.13	0.285	o	|	|	|	|	1.03
63.000	0.00	0.13	0.284	o	|	|	|	|	1.03
63.083	0.00	0.13	0.283	o	|	|	|	|	1.02
63.167	0.00	0.13	0.283	o	|	|	|	|	1.02
63.250	0.00	0.13	0.282	o	|	|	|	|	1.02
63.333	0.00	0.13	0.281	o	|	|	|	|	1.02
63.417	0.00	0.13	0.280	o	|	|	|	|	1.01
63.500	0.00	0.13	0.279	o	|	|	|	|	1.01
63.583	0.00	0.13	0.278	o	|	|	|	|	1.01
63.667	0.00	0.13	0.277	o	|	|	|	|	1.00
63.750	0.00	0.13	0.276	o	|	|	|	|	1.00
63.833	0.00	0.13	0.275	o	|	|	|	|	1.00
63.917	0.00	0.13	0.274	o	|	|	|	|	0.99
64.000	0.00	0.13	0.273	o	|	|	|	|	0.99
64.083	0.00	0.13	0.272	o	|	|	|	|	0.99
64.167	0.00	0.13	0.272	o	|	|	|	|	0.98
64.250	0.00	0.13	0.271	o	|	|	|	|	0.98
64.333	0.00	0.13	0.270	o	|	|	|	|	0.98
64.417	0.00	0.13	0.269	o	|	|	|	|	0.97
64.500	0.00	0.13	0.268	o	|	|	|	|	0.97
64.583	0.00	0.13	0.267	o	|	|	|	|	0.97
64.667	0.00	0.13	0.266	o	|	|	|	|	0.96
64.750	0.00	0.13	0.265	o	|	|	|	|	0.96
64.833	0.00	0.13	0.264	o	|	|	|	|	0.96
64.917	0.00	0.13	0.264	o	|	|	|	|	0.96
65.000	0.00	0.13	0.263	o	|	|	|	|	0.95
65.083	0.00	0.13	0.262	o	|	|	|	|	0.95
65.167	0.00	0.13	0.261	o	|	|	|	|	0.95
65.250	0.00	0.13	0.260	o	|	|	|	|	0.94
65.333	0.00	0.12	0.259	o	|	|	|	|	0.94
65.417	0.00	0.12	0.258	o	|	|	|	|	0.94
65.500	0.00	0.12	0.258	o	|	|	|	|	0.93
65.583	0.00	0.12	0.257	o	|	|	|	|	0.93
65.667	0.00	0.12	0.256	o	|	|	|	|	0.93
65.750	0.00	0.12	0.255	o	|	|	|	|	0.92
65.833	0.00	0.12	0.254	o	|	|	|	|	0.92
65.917	0.00	0.12	0.253	o	|	|	|	|	0.92
66.000	0.00	0.12	0.252	o	|	|	|	|	0.91
66.083	0.00	0.12	0.252	o	|	|	|	|	0.91
66.167	0.00	0.12	0.251	o	|	|	|	|	0.91
66.250	0.00	0.12	0.250	o	|	|	|	|	0.91
66.333	0.00	0.12	0.249	o	|	|	|	|	0.90
66.417	0.00	0.12	0.248	o	|	|	|	|	0.90
66.500	0.00	0.12	0.247	o	|	|	|	|	0.90
66.583	0.00	0.12	0.247	o	|	|	|	|	0.89

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66.667    0.00    0.12      0.246  o       |       |       |       |      0.89
66.750    0.00    0.12      0.245  o       |       |       |       |      0.89
66.833    0.00    0.12      0.244  o       |       |       |       |      0.88
66.917    0.00    0.12      0.243  o       |       |       |       |      0.88
67.000    0.00    0.12      0.243  o       |       |       |       |      0.88
67.083    0.00    0.12      0.242  o       |       |       |       |      0.88
67.167    0.00    0.12      0.241  o       |       |       |       |      0.87
67.250    0.00    0.12      0.240  o       |       |       |       |      0.87
67.333    0.00    0.12      0.239  o       |       |       |       |      0.87
67.417    0.00    0.11      0.239  o       |       |       |       |      0.86
67.500    0.00    0.11      0.238  o       |       |       |       |      0.86
67.583    0.00    0.11      0.237  o       |       |       |       |      0.86
67.667    0.00    0.11      0.236  o       |       |       |       |      0.86
67.750    0.00    0.11      0.235  o       |       |       |       |      0.85
67.833    0.00    0.11      0.235  o       |       |       |       |      0.85
67.917    0.00    0.11      0.234  o       |       |       |       |      0.85
68.000    0.00    0.11      0.233  o       |       |       |       |      0.84
68.083    0.00    0.11      0.232  o       |       |       |       |      0.84
68.167    0.00    0.11      0.232  o       |       |       |       |      0.84
68.250    0.00    0.11      0.231  o       |       |       |       |      0.84
68.333    0.00    0.11      0.230  o       |       |       |       |      0.83
68.417    0.00    0.11      0.229  o       |       |       |       |      0.83
68.500    0.00    0.11      0.229  o       |       |       |       |      0.83
68.583    0.00    0.11      0.228  o       |       |       |       |      0.83
68.667    0.00    0.11      0.227  o       |       |       |       |      0.82
68.750    0.00    0.11      0.226  o       |       |       |       |      0.82
68.833    0.00    0.11      0.226  o       |       |       |       |      0.82
68.917    0.00    0.11      0.225  o       |       |       |       |      0.81
69.000    0.00    0.11      0.224  o       |       |       |       |      0.81
69.083    0.00    0.11      0.223  o       |       |       |       |      0.81
69.167    0.00    0.11      0.223  o       |       |       |       |      0.81
69.250    0.00    0.11      0.222  o       |       |       |       |      0.80
69.333    0.00    0.11      0.221  o       |       |       |       |      0.80
69.417    0.00    0.11      0.220  o       |       |       |       |      0.80
69.500    0.00    0.11      0.220  o       |       |       |       |      0.80
69.583    0.00    0.11      0.219  o       |       |       |       |      0.79
69.667    0.00    0.11      0.218  o       |       |       |       |      0.79
69.750    0.00    0.10      0.217  o       |       |       |       |      0.79
69.833    0.00    0.10      0.217  o       |       |       |       |      0.79
69.917    0.00    0.10      0.216  o       |       |       |       |      0.78
70.000    0.00    0.10      0.215  o       |       |       |       |      0.78
70.083    0.00    0.10      0.215  o       |       |       |       |      0.78
70.167    0.00    0.10      0.214  o       |       |       |       |      0.77
70.250    0.00    0.10      0.213  o       |       |       |       |      0.77
70.333    0.00    0.10      0.212  o       |       |       |       |      0.77
70.417    0.00    0.10      0.212  o       |       |       |       |      0.77
70.500    0.00    0.10      0.211  o       |       |       |       |      0.76
70.583    0.00    0.10      0.210  o       |       |       |       |      0.76
70.667    0.00    0.10      0.210  o       |       |       |       |      0.76
70.750    0.00    0.10      0.209  o       |       |       |       |      0.76
70.833    0.00    0.10      0.208  o       |       |       |       |      0.75
70.917    0.00    0.10      0.208  o       |       |       |       |      0.75
71.000    0.00    0.10      0.207  o       |       |       |       |      0.75
      Remaining water in basin =    0.21 (Ac.Ft)
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =   852
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =        7.051 (CFS)
                  Total volume =       3.525 (Ac.Ft)
            Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      ************************************************************************

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                FLOOD HYDROGRAPH ROUTING PROGRAM
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                      Study date: 05/07/25

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: PRO1001100.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    16
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       84.206 (CFS)
               Total volume =       2.593 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
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Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data
---------------------------------------------------------------------
Total number of inflow hydrograph intervals = 16
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
---------------------------------------------------------------------
---------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
---------------------------------------------------------------------
---------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
---------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.276      0.133      0.276        0.276
   2.000      0.584      0.193      0.583        0.585
   3.000      0.930      0.700      0.928        0.932
   3.500      1.118      0.824      1.115        1.121
   4.000      1.316      0.930      1.313        1.319
   4.500      1.528      1.024      1.524        1.532
   4.750      1.637      1.068      1.633        1.641
   5.000      1.749     18.283      1.686        1.812
   6.000      2.231    253.655      1.358        3.104
---------------------------------------------------------------------
               Hydrograph Detention Basin Routing
---------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
---------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                    Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0      21.1   42.10   63.15   84.21 (Ft.)
 0.083    3.61    0.01      0.012  OI      |       |       |       |     0.05
 0.167    9.19    0.03      0.056  O  I    |       |       |       |     0.20
 0.250   12.18    0.06      0.130  O   I   |       |       |       |     0.47
 0.333   14.03    0.11      0.219  O    I  |       |       |       |     0.79
 0.417   15.93    0.14      0.322  O     I |       |       |       |     1.15
 0.500   18.81    0.17      0.440  O      I|       |       |       |     1.53
 0.583   22.14    0.19      0.580  O       I       |       |       |     1.99
 0.667   27.49    0.43      0.749  O       | I     |       |       |     2.48
 0.750   41.20    0.73      0.981  O       |      I|       |       |     3.14
 0.833   84.21    0.97      1.407  O       |       |       |      I|     4.22
 0.917   77.43   45.35      1.804  |       |       |O      |    I  |     5.12
 1.000   31.58   56.83      1.828  |       |  I    |    O  |       |     5.16
 1.083   13.45   15.81      1.733  |    IO |       |       |       |     4.96
 1.167    4.25   10.99      1.702  |I  O   |       |       |       |     4.89
 1.250    0.85    5.15      1.664  IO      |       |       |       |     4.81
 1.333    0.18    1.94      1.643  O       |       |       |       |     4.76
 1.417    0.00    1.07      1.633  O       |       |       |       |     4.74
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1.500	0.00	1.06	1.626	o	|	|	|	4.72
1.583	0.00	1.06	1.618	o	|	|	|	4.71
1.667	0.00	1.06	1.611	o	|	|	|	4.69
1.750	0.00	1.05	1.604	o	|	|	|	4.67
1.833	0.00	1.05	1.596	o	|	|	|	4.66
1.917	0.00	1.05	1.589	o	|	|	|	4.64
2.000	0.00	1.05	1.582	o	|	|	|	4.62
2.083	0.00	1.04	1.575	o	|	|	|	4.61
2.167	0.00	1.04	1.568	o	|	|	|	4.59
2.250	0.00	1.04	1.561	o	|	|	|	4.57
2.333	0.00	1.03	1.553	o	|	|	|	4.56
2.417	0.00	1.03	1.546	o	|	|	|	4.54
2.500	0.00	1.03	1.539	o	|	|	|	4.53
2.583	0.00	1.03	1.532	o	|	|	|	4.51
2.667	0.00	1.02	1.525	o	|	|	|	4.49
2.750	0.00	1.02	1.518	o	|	|	|	4.48
2.833	0.00	1.02	1.511	o	|	|	|	4.46
2.917	0.00	1.01	1.504	o	|	|	|	4.44
3.000	0.00	1.01	1.497	o	|	|	|	4.43
3.083	0.00	1.01	1.490	o	|	|	|	4.41
3.167	0.00	1.00	1.483	o	|	|	|	4.39
3.250	0.00	1.00	1.476	o	|	|	|	4.38
3.333	0.00	1.00	1.469	o	|	|	|	4.36
3.417	0.00	0.99	1.463	o	|	|	|	4.35
3.500	0.00	0.99	1.456	o	|	|	|	4.33
3.583	0.00	0.99	1.449	o	|	|	|	4.31
3.667	0.00	0.99	1.442	o	|	|	|	4.30
3.750	0.00	0.98	1.435	o	|	|	|	4.28
3.833	0.00	0.98	1.429	o	|	|	|	4.27
3.917	0.00	0.98	1.422	o	|	|	|	4.25
4.000	0.00	0.97	1.415	o	|	|	|	4.23
4.083	0.00	0.97	1.408	o	|	|	|	4.22
4.167	0.00	0.97	1.402	o	|	|	|	4.20
4.250	0.00	0.97	1.395	o	|	|	|	4.19
4.333	0.00	0.96	1.388	o	|	|	|	4.17
4.417	0.00	0.96	1.382	o	|	|	|	4.16
4.500	0.00	0.96	1.375	o	|	|	|	4.14
4.583	0.00	0.95	1.369	o	|	|	|	4.12
4.667	0.00	0.95	1.362	o	|	|	|	4.11
4.750	0.00	0.95	1.356	o	|	|	|	4.09
4.833	0.00	0.94	1.349	o	|	|	|	4.08
4.917	0.00	0.94	1.343	o	|	|	|	4.06
5.000	0.00	0.94	1.336	o	|	|	|	4.05
5.083	0.00	0.94	1.330	o	|	|	|	4.03
5.167	0.00	0.93	1.323	o	|	|	|	4.02
5.250	0.00	0.93	1.317	o	|	|	|	4.00
5.333	0.00	0.93	1.310	o	|	|	|	3.99
5.417	0.00	0.92	1.304	o	|	|	|	3.97
5.500	0.00	0.92	1.298	o	|	|	|	3.95
5.583	0.00	0.92	1.291	o	|	|	|	3.94
5.667	0.00	0.91	1.285	o	|	|	|	3.92
5.750	0.00	0.91	1.279	o	|	|	|	3.91
5.833	0.00	0.91	1.272	o	|	|	|	3.89
5.917	0.00	0.90	1.266	o	|	|	|	3.87
6.000	0.00	0.90	1.260	o	|	|	|	3.86
6.083	0.00	0.90	1.254	o	|	|	|	3.84
6.167	0.00	0.89	1.248	o	|	|	|	3.83
6.250	0.00	0.89	1.242	o	|	|	|	3.81
6.333	0.00	0.89	1.235	o	|	|	|	3.80
6.417	0.00	0.88	1.229	o	|	|	|	3.78
6.500	0.00	0.88	1.223	o	|	|	|	3.77
6.583	0.00	0.88	1.217	o	|	|	|	3.75
6.667	0.00	0.87	1.211	o	|	|	|	3.74
6.750	0.00	0.87	1.205	o	|	|	|	3.72
6.833	0.00	0.87	1.199	o	|	|	|	3.70
6.917	0.00	0.86	1.193	o	|	|	|	3.69
7.000	0.00	0.86	1.187	o	|	|	|	3.67
7.083	0.00	0.86	1.181	o	|	|	|	3.66
7.167	0.00	0.85	1.175	o	|	|	|	3.65
7.250	0.00	0.85	1.170	o	|	|	|	3.63
7.333	0.00	0.85	1.164	o	|	|	|	3.62
7.417	0.00	0.85	1.158	o	|	|	|	3.60
7.500	0.00	0.84	1.152	o	|	|	|	3.59
7.583	0.00	0.84	1.146	o	|	|	|	3.57
7.667	0.00	0.84	1.141	o	|	|	|	3.56
7.750	0.00	0.83	1.135	o	|	|	|	3.54
7.833	0.00	0.83	1.129	o	|	|	|	3.53
7.917	0.00	0.83	1.123	o	|	|	|	3.51
8.000	0.00	0.82	1.118	o	|	|	|	3.50
8.083	0.00	0.82	1.112	o	|	|	|	3.48
8.167	0.00	0.82	1.106	o	|	|	|	3.47
8.250	0.00	0.81	1.101	o	|	|	|	3.45
8.333	0.00	0.81	1.095	o	|	|	|	3.44
8.417	0.00	0.81	1.090	o	|	|	|	3.42
8.500	0.00	0.80	1.084	o	|	|	|	3.41
8.583	0.00	0.80	1.079	o	|	|	|	3.40

8.667	0.00	0.79	1.073	o	|	|	|	|	3.38
8.750	0.00	0.79	1.068	o	|	|	|	|	3.37
8.833	0.00	0.79	1.062	o	|	|	|	|	3.35
8.917	0.00	0.78	1.057	o	|	|	|	|	3.34
9.000	0.00	0.78	1.051	o	|	|	|	|	3.32
9.083	0.00	0.78	1.046	o	|	|	|	|	3.31
9.167	0.00	0.77	1.041	o	|	|	|	|	3.29
9.250	0.00	0.77	1.035	o	|	|	|	|	3.28
9.333	0.00	0.77	1.030	o	|	|	|	|	3.27
9.417	0.00	0.76	1.025	o	|	|	|	|	3.25
9.500	0.00	0.76	1.020	o	|	|	|	|	3.24
9.583	0.00	0.76	1.014	o	|	|	|	|	3.22
9.667	0.00	0.75	1.009	o	|	|	|	|	3.21
9.750	0.00	0.75	1.004	o	|	|	|	|	3.20
9.833	0.00	0.75	0.999	o	|	|	|	|	3.18
9.917	0.00	0.74	0.994	o	|	|	|	|	3.17
10.000	0.00	0.74	0.989	o	|	|	|	|	3.16
10.083	0.00	0.74	0.984	o	|	|	|	|	3.14
10.167	0.00	0.73	0.979	o	|	|	|	|	3.13
10.250	0.00	0.73	0.973	o	|	|	|	|	3.12
10.333	0.00	0.73	0.968	o	|	|	|	|	3.10
10.417	0.00	0.72	0.963	o	|	|	|	|	3.09
10.500	0.00	0.72	0.959	o	|	|	|	|	3.08
10.583	0.00	0.72	0.954	o	|	|	|	|	3.06
10.667	0.00	0.71	0.949	o	|	|	|	|	3.05
10.750	0.00	0.71	0.944	o	|	|	|	|	3.04
10.833	0.00	0.71	0.939	o	|	|	|	|	3.02
10.917	0.00	0.70	0.934	o	|	|	|	|	3.01
11.000	0.00	0.70	0.929	o	|	|	|	|	3.00
11.083	0.00	0.69	0.924	o	|	|	|	|	2.98
11.167	0.00	0.68	0.920	o	|	|	|	|	2.97
11.250	0.00	0.68	0.915	o	|	|	|	|	2.96
11.333	0.00	0.67	0.910	o	|	|	|	|	2.94
11.417	0.00	0.66	0.906	o	|	|	|	|	2.93
11.500	0.00	0.66	0.901	o	|	|	|	|	2.92
11.583	0.00	0.65	0.897	o	|	|	|	|	2.90
11.667	0.00	0.64	0.892	o	|	|	|	|	2.89
11.750	0.00	0.64	0.888	o	|	|	|	|	2.88
11.833	0.00	0.63	0.883	o	|	|	|	|	2.87
11.917	0.00	0.63	0.879	o	|	|	|	|	2.85
12.000	0.00	0.62	0.875	o	|	|	|	|	2.84
12.083	0.00	0.61	0.871	o	|	|	|	|	2.83
12.167	0.00	0.61	0.866	o	|	|	|	|	2.82
12.250	0.00	0.60	0.862	o	|	|	|	|	2.80
12.333	0.00	0.59	0.858	o	|	|	|	|	2.79
12.417	0.00	0.59	0.854	o	|	|	|	|	2.78
12.500	0.00	0.58	0.850	o	|	|	|	|	2.77
12.583	0.00	0.58	0.846	o	|	|	|	|	2.76
12.667	0.00	0.57	0.842	o	|	|	|	|	2.75
12.750	0.00	0.57	0.838	o	|	|	|	|	2.73
12.833	0.00	0.56	0.834	o	|	|	|	|	2.72
12.917	0.00	0.55	0.830	o	|	|	|	|	2.71
13.000	0.00	0.55	0.827	o	|	|	|	|	2.70
13.083	0.00	0.54	0.823	o	|	|	|	|	2.69
13.167	0.00	0.54	0.819	o	|	|	|	|	2.68
13.250	0.00	0.53	0.815	o	|	|	|	|	2.67
13.333	0.00	0.53	0.812	o	|	|	|	|	2.66
13.417	0.00	0.52	0.808	o	|	|	|	|	2.65
13.500	0.00	0.52	0.805	o	|	|	|	|	2.64
13.583	0.00	0.51	0.801	o	|	|	|	|	2.63
13.667	0.00	0.51	0.798	o	|	|	|	|	2.62
13.750	0.00	0.50	0.794	o	|	|	|	|	2.61
13.833	0.00	0.50	0.791	o	|	|	|	|	2.60
13.917	0.00	0.49	0.787	o	|	|	|	|	2.59
14.000	0.00	0.49	0.784	o	|	|	|	|	2.58
14.083	0.00	0.48	0.781	o	|	|	|	|	2.57
14.167	0.00	0.48	0.777	o	|	|	|	|	2.56
14.250	0.00	0.47	0.774	o	|	|	|	|	2.55
14.333	0.00	0.47	0.771	o	|	|	|	|	2.54
14.417	0.00	0.46	0.768	o	|	|	|	|	2.53
14.500	0.00	0.46	0.764	o	|	|	|	|	2.52
14.583	0.00	0.45	0.761	o	|	|	|	|	2.51
14.667	0.00	0.45	0.758	o	|	|	|	|	2.50
14.750	0.00	0.44	0.755	o	|	|	|	|	2.49
14.833	0.00	0.44	0.752	o	|	|	|	|	2.49
14.917	0.00	0.43	0.749	o	|	|	|	|	2.48
15.000	0.00	0.43	0.746	o	|	|	|	|	2.47
15.083	0.00	0.43	0.743	o	|	|	|	|	2.46
15.167	0.00	0.42	0.740	o	|	|	|	|	2.45
15.250	0.00	0.42	0.737	o	|	|	|	|	2.44
15.333	0.00	0.41	0.734	o	|	|	|	|	2.43
15.417	0.00	0.41	0.732	o	|	|	|	|	2.43
15.500	0.00	0.41	0.729	o	|	|	|	|	2.42
15.583	0.00	0.40	0.726	o	|	|	|	|	2.41
15.667	0.00	0.40	0.723	o	|	|	|	|	2.40
15.750	0.00	0.39	0.721	o	|	|	|	|	2.39

15.833	0.00	0.39	0.718	o	|	|	|	|	2.39
15.917	0.00	0.39	0.715	o	|	|	|	|	2.38
16.000	0.00	0.38	0.713	o	|	|	|	|	2.37
16.083	0.00	0.38	0.710	o	|	|	|	|	2.36
16.167	0.00	0.37	0.707	o	|	|	|	|	2.36
16.250	0.00	0.37	0.705	o	|	|	|	|	2.35
16.333	0.00	0.37	0.702	o	|	|	|	|	2.34
16.417	0.00	0.36	0.700	o	|	|	|	|	2.33
16.500	0.00	0.36	0.697	o	|	|	|	|	2.33
16.583	0.00	0.36	0.695	o	|	|	|	|	2.32
16.667	0.00	0.35	0.692	o	|	|	|	|	2.31
16.750	0.00	0.35	0.690	o	|	|	|	|	2.31
16.833	0.00	0.34	0.688	o	|	|	|	|	2.30
16.917	0.00	0.34	0.685	o	|	|	|	|	2.29
17.000	0.00	0.34	0.683	o	|	|	|	|	2.29
17.083	0.00	0.33	0.681	o	|	|	|	|	2.28
17.167	0.00	0.33	0.678	o	|	|	|	|	2.27
17.250	0.00	0.33	0.676	o	|	|	|	|	2.27
17.333	0.00	0.32	0.674	o	|	|	|	|	2.26
17.417	0.00	0.32	0.672	o	|	|	|	|	2.25
17.500	0.00	0.32	0.669	o	|	|	|	|	2.25
17.583	0.00	0.31	0.667	o	|	|	|	|	2.24
17.667	0.00	0.31	0.665	o	|	|	|	|	2.23
17.750	0.00	0.31	0.663	o	|	|	|	|	2.23
17.833	0.00	0.31	0.661	o	|	|	|	|	2.22
17.917	0.00	0.30	0.659	o	|	|	|	|	2.22
18.000	0.00	0.30	0.657	o	|	|	|	|	2.21
18.083	0.00	0.30	0.655	o	|	|	|	|	2.20
18.167	0.00	0.29	0.653	o	|	|	|	|	2.20
18.250	0.00	0.29	0.651	o	|	|	|	|	2.19
18.333	0.00	0.29	0.649	o	|	|	|	|	2.19
18.417	0.00	0.28	0.647	o	|	|	|	|	2.18
18.500	0.00	0.28	0.645	o	|	|	|	|	2.18
18.583	0.00	0.28	0.643	o	|	|	|	|	2.17
18.667	0.00	0.28	0.641	o	|	|	|	|	2.16
18.750	0.00	0.27	0.639	o	|	|	|	|	2.16
18.833	0.00	0.27	0.637	o	|	|	|	|	2.15
18.917	0.00	0.27	0.635	o	|	|	|	|	2.15
19.000	0.00	0.27	0.633	o	|	|	|	|	2.14
19.083	0.00	0.26	0.631	o	|	|	|	|	2.14
19.167	0.00	0.26	0.630	o	|	|	|	|	2.13
19.250	0.00	0.26	0.628	o	|	|	|	|	2.13
19.333	0.00	0.25	0.626	o	|	|	|	|	2.12
19.417	0.00	0.25	0.624	o	|	|	|	|	2.12
19.500	0.00	0.25	0.623	o	|	|	|	|	2.11
19.583	0.00	0.25	0.621	o	|	|	|	|	2.11
19.667	0.00	0.24	0.619	o	|	|	|	|	2.10
19.750	0.00	0.24	0.618	o	|	|	|	|	2.10
19.833	0.00	0.24	0.616	o	|	|	|	|	2.09
19.917	0.00	0.24	0.614	o	|	|	|	|	2.09
20.000	0.00	0.23	0.613	o	|	|	|	|	2.08
20.083	0.00	0.23	0.611	o	|	|	|	|	2.08
20.167	0.00	0.23	0.609	o	|	|	|	|	2.07
20.250	0.00	0.23	0.608	o	|	|	|	|	2.07
20.333	0.00	0.23	0.606	o	|	|	|	|	2.06
20.417	0.00	0.22	0.605	o	|	|	|	|	2.06
20.500	0.00	0.22	0.603	o	|	|	|	|	2.06
20.583	0.00	0.22	0.602	o	|	|	|	|	2.05
20.667	0.00	0.22	0.600	o	|	|	|	|	2.05
20.750	0.00	0.21	0.599	o	|	|	|	|	2.04
20.833	0.00	0.21	0.597	o	|	|	|	|	2.04
20.917	0.00	0.21	0.596	o	|	|	|	|	2.03
21.000	0.00	0.21	0.594	o	|	|	|	|	2.03
21.083	0.00	0.21	0.593	o	|	|	|	|	2.03
21.167	0.00	0.20	0.592	o	|	|	|	|	2.02
21.250	0.00	0.20	0.590	o	|	|	|	|	2.02
21.333	0.00	0.20	0.589	o	|	|	|	|	2.01
21.417	0.00	0.20	0.587	o	|	|	|	|	2.01
21.500	0.00	0.20	0.586	o	|	|	|	|	2.01
21.583	0.00	0.19	0.585	o	|	|	|	|	2.00
21.667	0.00	0.19	0.583	o	|	|	|	|	2.00
21.750	0.00	0.19	0.582	o	|	|	|	|	1.99
21.833	0.00	0.19	0.581	o	|	|	|	|	1.99
21.917	0.00	0.19	0.579	o	|	|	|	|	1.98
22.000	0.00	0.19	0.578	o	|	|	|	|	1.98
22.083	0.00	0.19	0.577	o	|	|	|	|	1.98
22.167	0.00	0.19	0.575	o	|	|	|	|	1.97
22.250	0.00	0.19	0.574	o	|	|	|	|	1.97
22.333	0.00	0.19	0.573	o	|	|	|	|	1.96
22.417	0.00	0.19	0.571	o	|	|	|	|	1.96
22.500	0.00	0.19	0.570	o	|	|	|	|	1.96
22.583	0.00	0.19	0.569	o	|	|	|	|	1.95
22.667	0.00	0.19	0.568	o	|	|	|	|	1.95
22.750	0.00	0.19	0.566	o	|	|	|	|	1.94
22.833	0.00	0.19	0.565	o	|	|	|	|	1.94
22.917	0.00	0.19	0.564	o	|	|	|	|	1.93

23.000	0.00	0.19	0.562	o	|	|	|	|	1.93
23.083	0.00	0.19	0.561	o	|	|	|	|	1.93
23.167	0.00	0.19	0.560	o	|	|	|	|	1.92
23.250	0.00	0.19	0.558	o	|	|	|	|	1.92
23.333	0.00	0.19	0.557	o	|	|	|	|	1.91
23.417	0.00	0.19	0.556	o	|	|	|	|	1.91
23.500	0.00	0.19	0.555	o	|	|	|	|	1.90
23.583	0.00	0.19	0.553	o	|	|	|	|	1.90
23.667	0.00	0.19	0.552	o	|	|	|	|	1.90
23.750	0.00	0.19	0.551	o	|	|	|	|	1.89
23.833	0.00	0.19	0.549	o	|	|	|	|	1.89
23.917	0.00	0.19	0.548	o	|	|	|	|	1.88
24.000	0.00	0.19	0.547	o	|	|	|	|	1.88
24.083	0.00	0.19	0.546	o	|	|	|	|	1.88
24.167	0.00	0.19	0.544	o	|	|	|	|	1.87
24.250	0.00	0.19	0.543	o	|	|	|	|	1.87
24.333	0.00	0.18	0.542	o	|	|	|	|	1.86
24.417	0.00	0.18	0.540	o	|	|	|	|	1.86
24.500	0.00	0.18	0.539	o	|	|	|	|	1.85
24.583	0.00	0.18	0.538	o	|	|	|	|	1.85
24.667	0.00	0.18	0.537	o	|	|	|	|	1.85
24.750	0.00	0.18	0.535	o	|	|	|	|	1.84
24.833	0.00	0.18	0.534	o	|	|	|	|	1.84
24.917	0.00	0.18	0.533	o	|	|	|	|	1.83
25.000	0.00	0.18	0.532	o	|	|	|	|	1.83
25.083	0.00	0.18	0.530	o	|	|	|	|	1.83
25.167	0.00	0.18	0.529	o	|	|	|	|	1.82
25.250	0.00	0.18	0.528	o	|	|	|	|	1.82
25.333	0.00	0.18	0.527	o	|	|	|	|	1.81
25.417	0.00	0.18	0.525	o	|	|	|	|	1.81
25.500	0.00	0.18	0.524	o	|	|	|	|	1.81
25.583	0.00	0.18	0.523	o	|	|	|	|	1.80
25.667	0.00	0.18	0.522	o	|	|	|	|	1.80
25.750	0.00	0.18	0.520	o	|	|	|	|	1.79
25.833	0.00	0.18	0.519	o	|	|	|	|	1.79
25.917	0.00	0.18	0.518	o	|	|	|	|	1.79
26.000	0.00	0.18	0.517	o	|	|	|	|	1.78
26.083	0.00	0.18	0.515	o	|	|	|	|	1.78
26.167	0.00	0.18	0.514	o	|	|	|	|	1.77
26.250	0.00	0.18	0.513	o	|	|	|	|	1.77
26.333	0.00	0.18	0.512	o	|	|	|	|	1.77
26.417	0.00	0.18	0.510	o	|	|	|	|	1.76
26.500	0.00	0.18	0.509	o	|	|	|	|	1.76
26.583	0.00	0.18	0.508	o	|	|	|	|	1.75
26.667	0.00	0.18	0.507	o	|	|	|	|	1.75
26.750	0.00	0.18	0.506	o	|	|	|	|	1.75
26.833	0.00	0.18	0.504	o	|	|	|	|	1.74
26.917	0.00	0.18	0.503	o	|	|	|	|	1.74
27.000	0.00	0.18	0.502	o	|	|	|	|	1.73
27.083	0.00	0.18	0.501	o	|	|	|	|	1.73
27.167	0.00	0.18	0.499	o	|	|	|	|	1.73
27.250	0.00	0.18	0.498	o	|	|	|	|	1.72
27.333	0.00	0.18	0.497	o	|	|	|	|	1.72
27.417	0.00	0.18	0.496	o	|	|	|	|	1.71
27.500	0.00	0.18	0.495	o	|	|	|	|	1.71
27.583	0.00	0.18	0.493	o	|	|	|	|	1.71
27.667	0.00	0.18	0.492	o	|	|	|	|	1.70
27.750	0.00	0.17	0.491	o	|	|	|	|	1.70
27.833	0.00	0.17	0.490	o	|	|	|	|	1.69
27.917	0.00	0.17	0.489	o	|	|	|	|	1.69
28.000	0.00	0.17	0.487	o	|	|	|	|	1.69
28.083	0.00	0.17	0.486	o	|	|	|	|	1.68
28.167	0.00	0.17	0.485	o	|	|	|	|	1.68
28.250	0.00	0.17	0.484	o	|	|	|	|	1.67
28.333	0.00	0.17	0.483	o	|	|	|	|	1.67
28.417	0.00	0.17	0.481	o	|	|	|	|	1.67
28.500	0.00	0.17	0.480	o	|	|	|	|	1.66
28.583	0.00	0.17	0.479	o	|	|	|	|	1.66
28.667	0.00	0.17	0.478	o	|	|	|	|	1.66
28.750	0.00	0.17	0.477	o	|	|	|	|	1.65
28.833	0.00	0.17	0.475	o	|	|	|	|	1.65
28.917	0.00	0.17	0.474	o	|	|	|	|	1.64
29.000	0.00	0.17	0.473	o	|	|	|	|	1.64
29.083	0.00	0.17	0.472	o	|	|	|	|	1.64
29.167	0.00	0.17	0.471	o	|	|	|	|	1.63
29.250	0.00	0.17	0.470	o	|	|	|	|	1.63
29.333	0.00	0.17	0.468	o	|	|	|	|	1.62
29.417	0.00	0.17	0.467	o	|	|	|	|	1.62
29.500	0.00	0.17	0.466	o	|	|	|	|	1.62
29.583	0.00	0.17	0.465	o	|	|	|	|	1.61
29.667	0.00	0.17	0.464	o	|	|	|	|	1.61
29.750	0.00	0.17	0.463	o	|	|	|	|	1.61
29.833	0.00	0.17	0.461	o	|	|	|	|	1.60
29.917	0.00	0.17	0.460	o	|	|	|	|	1.60
30.000	0.00	0.17	0.459	o	|	|	|	|	1.59
30.083	0.00	0.17	0.458	o	|	|	|	|	1.59

30.167	0.00	0.17	0.457	o	|	|	|	|	1.59
30.250	0.00	0.17	0.456	o	|	|	|	|	1.58
30.333	0.00	0.17	0.454	o	|	|	|	|	1.58
30.417	0.00	0.17	0.453	o	|	|	|	|	1.58
30.500	0.00	0.17	0.452	o	|	|	|	|	1.57
30.583	0.00	0.17	0.451	o	|	|	|	|	1.57
30.667	0.00	0.17	0.450	o	|	|	|	|	1.56
30.750	0.00	0.17	0.449	o	|	|	|	|	1.56
30.833	0.00	0.17	0.447	o	|	|	|	|	1.56
30.917	0.00	0.17	0.446	o	|	|	|	|	1.55
31.000	0.00	0.17	0.445	o	|	|	|	|	1.55
31.083	0.00	0.17	0.444	o	|	|	|	|	1.55
31.167	0.00	0.17	0.443	o	|	|	|	|	1.54
31.250	0.00	0.17	0.442	o	|	|	|	|	1.54
31.333	0.00	0.17	0.441	o	|	|	|	|	1.53
31.417	0.00	0.16	0.440	o	|	|	|	|	1.53
31.500	0.00	0.16	0.438	o	|	|	|	|	1.53
31.583	0.00	0.16	0.437	o	|	|	|	|	1.52
31.667	0.00	0.16	0.436	o	|	|	|	|	1.52
31.750	0.00	0.16	0.435	o	|	|	|	|	1.52
31.833	0.00	0.16	0.434	o	|	|	|	|	1.51
31.917	0.00	0.16	0.433	o	|	|	|	|	1.51
32.000	0.00	0.16	0.432	o	|	|	|	|	1.51
32.083	0.00	0.16	0.430	o	|	|	|	|	1.50
32.167	0.00	0.16	0.429	o	|	|	|	|	1.50
32.250	0.00	0.16	0.428	o	|	|	|	|	1.49
32.333	0.00	0.16	0.427	o	|	|	|	|	1.49
32.417	0.00	0.16	0.426	o	|	|	|	|	1.49
32.500	0.00	0.16	0.425	o	|	|	|	|	1.48
32.583	0.00	0.16	0.424	o	|	|	|	|	1.48
32.667	0.00	0.16	0.423	o	|	|	|	|	1.48
32.750	0.00	0.16	0.422	o	|	|	|	|	1.47
32.833	0.00	0.16	0.420	o	|	|	|	|	1.47
32.917	0.00	0.16	0.419	o	|	|	|	|	1.47
33.000	0.00	0.16	0.418	o	|	|	|	|	1.46
33.083	0.00	0.16	0.417	o	|	|	|	|	1.46
33.167	0.00	0.16	0.416	o	|	|	|	|	1.45
33.250	0.00	0.16	0.415	o	|	|	|	|	1.45
33.333	0.00	0.16	0.414	o	|	|	|	|	1.45
33.417	0.00	0.16	0.413	o	|	|	|	|	1.44
33.500	0.00	0.16	0.412	o	|	|	|	|	1.44
33.583	0.00	0.16	0.411	o	|	|	|	|	1.44
33.667	0.00	0.16	0.409	o	|	|	|	|	1.43
33.750	0.00	0.16	0.408	o	|	|	|	|	1.43
33.833	0.00	0.16	0.407	o	|	|	|	|	1.43
33.917	0.00	0.16	0.406	o	|	|	|	|	1.42
34.000	0.00	0.16	0.405	o	|	|	|	|	1.42
34.083	0.00	0.16	0.404	o	|	|	|	|	1.42
34.167	0.00	0.16	0.403	o	|	|	|	|	1.41
34.250	0.00	0.16	0.402	o	|	|	|	|	1.41
34.333	0.00	0.16	0.401	o	|	|	|	|	1.40
34.417	0.00	0.16	0.400	o	|	|	|	|	1.40
34.500	0.00	0.16	0.399	o	|	|	|	|	1.40
34.583	0.00	0.16	0.397	o	|	|	|	|	1.39
34.667	0.00	0.16	0.396	o	|	|	|	|	1.39
34.750	0.00	0.16	0.395	o	|	|	|	|	1.39
34.833	0.00	0.16	0.394	o	|	|	|	|	1.38
34.917	0.00	0.16	0.393	o	|	|	|	|	1.38
35.000	0.00	0.16	0.392	o	|	|	|	|	1.38
35.083	0.00	0.16	0.391	o	|	|	|	|	1.37
35.167	0.00	0.16	0.390	o	|	|	|	|	1.37
35.250	0.00	0.15	0.389	o	|	|	|	|	1.37
35.333	0.00	0.15	0.388	o	|	|	|	|	1.36
35.417	0.00	0.15	0.387	o	|	|	|	|	1.36
35.500	0.00	0.15	0.386	o	|	|	|	|	1.36
35.583	0.00	0.15	0.385	o	|	|	|	|	1.35
35.667	0.00	0.15	0.384	o	|	|	|	|	1.35
35.750	0.00	0.15	0.382	o	|	|	|	|	1.35
35.833	0.00	0.15	0.381	o	|	|	|	|	1.34
35.917	0.00	0.15	0.380	o	|	|	|	|	1.34
36.000	0.00	0.15	0.379	o	|	|	|	|	1.34
36.083	0.00	0.15	0.378	o	|	|	|	|	1.33
36.167	0.00	0.15	0.377	o	|	|	|	|	1.33
36.250	0.00	0.15	0.376	o	|	|	|	|	1.33
36.333	0.00	0.15	0.375	o	|	|	|	|	1.32
36.417	0.00	0.15	0.374	o	|	|	|	|	1.32
36.500	0.00	0.15	0.373	o	|	|	|	|	1.31
36.583	0.00	0.15	0.372	o	|	|	|	|	1.31
36.667	0.00	0.15	0.371	o	|	|	|	|	1.31
36.750	0.00	0.15	0.370	o	|	|	|	|	1.30
36.833	0.00	0.15	0.369	o	|	|	|	|	1.30
36.917	0.00	0.15	0.368	o	|	|	|	|	1.30
37.000	0.00	0.15	0.367	o	|	|	|	|	1.29
37.083	0.00	0.15	0.366	o	|	|	|	|	1.29
37.167	0.00	0.15	0.365	o	|	|	|	|	1.29
37.250	0.00	0.15	0.364	o	|	|	|	|	1.28

37.333	0.00	0.15	0.363	o	|	|	|	1.28
37.417	0.00	0.15	0.362	o	|	|	|	1.28
37.500	0.00	0.15	0.361	o	|	|	|	1.27
37.583	0.00	0.15	0.360	o	|	|	|	1.27
37.667	0.00	0.15	0.359	o	|	|	|	1.27
37.750	0.00	0.15	0.357	o	|	|	|	1.26
37.833	0.00	0.15	0.356	o	|	|	|	1.26
37.917	0.00	0.15	0.355	o	|	|	|	1.26
38.000	0.00	0.15	0.354	o	|	|	|	1.25
38.083	0.00	0.15	0.353	o	|	|	|	1.25
38.167	0.00	0.15	0.352	o	|	|	|	1.25
38.250	0.00	0.15	0.351	o	|	|	|	1.24
38.333	0.00	0.15	0.350	o	|	|	|	1.24
38.417	0.00	0.15	0.349	o	|	|	|	1.24
38.500	0.00	0.15	0.348	o	|	|	|	1.23
38.583	0.00	0.15	0.347	o	|	|	|	1.23
38.667	0.00	0.15	0.346	o	|	|	|	1.23
38.750	0.00	0.15	0.345	o	|	|	|	1.22
38.833	0.00	0.15	0.344	o	|	|	|	1.22
38.917	0.00	0.15	0.343	o	|	|	|	1.22
39.000	0.00	0.15	0.342	o	|	|	|	1.22
39.083	0.00	0.15	0.341	o	|	|	|	1.21
39.167	0.00	0.15	0.340	o	|	|	|	1.21
39.250	0.00	0.15	0.339	o	|	|	|	1.21
39.333	0.00	0.15	0.338	o	|	|	|	1.20
39.417	0.00	0.14	0.337	o	|	|	|	1.20
39.500	0.00	0.14	0.336	o	|	|	|	1.20
39.583	0.00	0.14	0.335	o	|	|	|	1.19
39.667	0.00	0.14	0.334	o	|	|	|	1.19
39.750	0.00	0.14	0.333	o	|	|	|	1.19
39.833	0.00	0.14	0.332	o	|	|	|	1.18
39.917	0.00	0.14	0.331	o	|	|	|	1.18
40.000	0.00	0.14	0.330	o	|	|	|	1.18
40.083	0.00	0.14	0.329	o	|	|	|	1.17
40.167	0.00	0.14	0.328	o	|	|	|	1.17
40.250	0.00	0.14	0.327	o	|	|	|	1.17
40.333	0.00	0.14	0.326	o	|	|	|	1.16
40.417	0.00	0.14	0.325	o	|	|	|	1.16
40.500	0.00	0.14	0.324	o	|	|	|	1.16
40.583	0.00	0.14	0.323	o	|	|	|	1.15
40.667	0.00	0.14	0.322	o	|	|	|	1.15
40.750	0.00	0.14	0.321	o	|	|	|	1.15
40.833	0.00	0.14	0.320	o	|	|	|	1.14
40.917	0.00	0.14	0.319	o	|	|	|	1.14
41.000	0.00	0.14	0.319	o	|	|	|	1.14
41.083	0.00	0.14	0.318	o	|	|	|	1.13
41.167	0.00	0.14	0.317	o	|	|	|	1.13
41.250	0.00	0.14	0.316	o	|	|	|	1.13
41.333	0.00	0.14	0.315	o	|	|	|	1.13
41.417	0.00	0.14	0.314	o	|	|	|	1.12
41.500	0.00	0.14	0.313	o	|	|	|	1.12
41.583	0.00	0.14	0.312	o	|	|	|	1.12
41.667	0.00	0.14	0.311	o	|	|	|	1.11
41.750	0.00	0.14	0.310	o	|	|	|	1.11
41.833	0.00	0.14	0.309	o	|	|	|	1.11
41.917	0.00	0.14	0.308	o	|	|	|	1.10
42.000	0.00	0.14	0.307	o	|	|	|	1.10
42.083	0.00	0.14	0.306	o	|	|	|	1.10
42.167	0.00	0.14	0.305	o	|	|	|	1.09
42.250	0.00	0.14	0.304	o	|	|	|	1.09
42.333	0.00	0.14	0.303	o	|	|	|	1.09
42.417	0.00	0.14	0.302	o	|	|	|	1.08
42.500	0.00	0.14	0.301	o	|	|	|	1.08
42.583	0.00	0.14	0.300	o	|	|	|	1.08
42.667	0.00	0.14	0.299	o	|	|	|	1.08
42.750	0.00	0.14	0.298	o	|	|	|	1.07
42.833	0.00	0.14	0.297	o	|	|	|	1.07
42.917	0.00	0.14	0.296	o	|	|	|	1.07
43.000	0.00	0.14	0.296	o	|	|	|	1.06
43.083	0.00	0.14	0.295	o	|	|	|	1.06
43.167	0.00	0.14	0.294	o	|	|	|	1.06
43.250	0.00	0.14	0.293	o	|	|	|	1.05
43.333	0.00	0.14	0.292	o	|	|	|	1.05
43.417	0.00	0.14	0.291	o	|	|	|	1.05
43.500	0.00	0.14	0.290	o	|	|	|	1.05
43.583	0.00	0.14	0.289	o	|	|	|	1.04
43.667	0.00	0.14	0.288	o	|	|	|	1.04
43.750	0.00	0.14	0.287	o	|	|	|	1.04
43.833	0.00	0.13	0.286	o	|	|	|	1.03
43.917	0.00	0.13	0.285	o	|	|	|	1.03
44.000	0.00	0.13	0.284	o	|	|	|	1.03
44.083	0.00	0.13	0.283	o	|	|	|	1.02
44.167	0.00	0.13	0.282	o	|	|	|	1.02
44.250	0.00	0.13	0.282	o	|	|	|	1.02
44.333	0.00	0.13	0.281	o	|	|	|	1.02
44.417	0.00	0.13	0.280	o	|	|	|	1.01

44.500	0.00	0.13	0.279	o	|	|	|	1.01
44.583	0.00	0.13	0.278	o	|	|	|	1.01
44.667	0.00	0.13	0.277	o	|	|	|	1.00
44.750	0.00	0.13	0.276	o	|	|	|	1.00
44.833	0.00	0.13	0.275	o	|	|	|	1.00
44.917	0.00	0.13	0.274	o	|	|	|	0.99
45.000	0.00	0.13	0.273	o	|	|	|	0.99
45.083	0.00	0.13	0.272	o	|	|	|	0.99
45.167	0.00	0.13	0.271	o	|	|	|	0.98
45.250	0.00	0.13	0.271	o	|	|	|	0.98
45.333	0.00	0.13	0.270	o	|	|	|	0.98
45.417	0.00	0.13	0.269	o	|	|	|	0.97
45.500	0.00	0.13	0.268	o	|	|	|	0.97
45.583	0.00	0.13	0.267	o	|	|	|	0.97
45.667	0.00	0.13	0.266	o	|	|	|	0.96
45.750	0.00	0.13	0.265	o	|	|	|	0.96
45.833	0.00	0.13	0.264	o	|	|	|	0.96
45.917	0.00	0.13	0.263	o	|	|	|	0.95
46.000	0.00	0.13	0.263	o	|	|	|	0.95
46.083	0.00	0.13	0.262	o	|	|	|	0.95
46.167	0.00	0.13	0.261	o	|	|	|	0.95
46.250	0.00	0.13	0.260	o	|	|	|	0.94
46.333	0.00	0.12	0.259	o	|	|	|	0.94
46.417	0.00	0.12	0.258	o	|	|	|	0.94
46.500	0.00	0.12	0.257	o	|	|	|	0.93
46.583	0.00	0.12	0.257	o	|	|	|	0.93
46.667	0.00	0.12	0.256	o	|	|	|	0.93
46.750	0.00	0.12	0.255	o	|	|	|	0.92
46.833	0.00	0.12	0.254	o	|	|	|	0.92
46.917	0.00	0.12	0.253	o	|	|	|	0.92
47.000	0.00	0.12	0.252	o	|	|	|	0.91
47.083	0.00	0.12	0.252	o	|	|	|	0.91
47.167	0.00	0.12	0.251	o	|	|	|	0.91
47.250	0.00	0.12	0.250	o	|	|	|	0.91
47.333	0.00	0.12	0.249	o	|	|	|	0.90
47.417	0.00	0.12	0.248	o	|	|	|	0.90
47.500	0.00	0.12	0.247	o	|	|	|	0.90
47.583	0.00	0.12	0.247	o	|	|	|	0.89
47.667	0.00	0.12	0.246	o	|	|	|	0.89
47.750	0.00	0.12	0.245	o	|	|	|	0.89
47.833	0.00	0.12	0.244	o	|	|	|	0.88
47.917	0.00	0.12	0.243	o	|	|	|	0.88
48.000	0.00	0.12	0.243	o	|	|	|	0.88
48.083	0.00	0.12	0.242	o	|	|	|	0.88
48.167	0.00	0.12	0.241	o	|	|	|	0.87
48.250	0.00	0.12	0.240	o	|	|	|	0.87
48.333	0.00	0.12	0.239	o	|	|	|	0.87
48.417	0.00	0.11	0.239	o	|	|	|	0.86
48.500	0.00	0.11	0.238	o	|	|	|	0.86
48.583	0.00	0.11	0.237	o	|	|	|	0.86
48.667	0.00	0.11	0.236	o	|	|	|	0.86
48.750	0.00	0.11	0.235	o	|	|	|	0.85
48.833	0.00	0.11	0.235	o	|	|	|	0.85
48.917	0.00	0.11	0.234	o	|	|	|	0.85
49.000	0.00	0.11	0.233	o	|	|	|	0.84
49.083	0.00	0.11	0.232	o	|	|	|	0.84
49.167	0.00	0.11	0.232	o	|	|	|	0.84
49.250	0.00	0.11	0.231	o	|	|	|	0.84
49.333	0.00	0.11	0.230	o	|	|	|	0.83
49.417	0.00	0.11	0.229	o	|	|	|	0.83
49.500	0.00	0.11	0.228	o	|	|	|	0.83
49.583	0.00	0.11	0.228	o	|	|	|	0.82
49.667	0.00	0.11	0.227	o	|	|	|	0.82
49.750	0.00	0.11	0.226	o	|	|	|	0.82
49.833	0.00	0.11	0.225	o	|	|	|	0.82
49.917	0.00	0.11	0.225	o	|	|	|	0.81
50.000	0.00	0.11	0.224	o	|	|	|	0.81
50.083	0.00	0.11	0.223	o	|	|	|	0.81
50.167	0.00	0.11	0.222	o	|	|	|	0.81
50.250	0.00	0.11	0.222	o	|	|	|	0.80
50.333	0.00	0.11	0.221	o	|	|	|	0.80
50.417	0.00	0.11	0.220	o	|	|	|	0.80
50.500	0.00	0.11	0.220	o	|	|	|	0.80
50.583	0.00	0.11	0.219	o	|	|	|	0.79
50.667	0.00	0.11	0.218	o	|	|	|	0.79
50.750	0.00	0.10	0.217	o	|	|	|	0.79
50.833	0.00	0.10	0.217	o	|	|	|	0.78
50.917	0.00	0.10	0.216	o	|	|	|	0.78
51.000	0.00	0.10	0.215	o	|	|	|	0.78
51.083	0.00	0.10	0.214	o	|	|	|	0.78
51.167	0.00	0.10	0.214	o	|	|	|	0.77
51.250	0.00	0.10	0.213	o	|	|	|	0.77
51.333	0.00	0.10	0.212	o	|	|	|	0.77
51.417	0.00	0.10	0.212	o	|	|	|	0.77
51.500	0.00	0.10	0.211	o	|	|	|	0.76
51.583	0.00	0.10	0.210	o	|	|	|	0.76

```
51.667    0.00    0.10      0.210  o       |       |       |       |     0.76
51.750    0.00    0.10      0.209  o       |       |       |       |     0.76
51.833    0.00    0.10      0.208  o       |       |       |       |     0.75
51.917    0.00    0.10      0.207  o       |       |       |       |     0.75

      Remaining water in basin =    0.21 (Ac.Ft)


      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =   623
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =       56.831 (CFS)
                  Total volume =       2.386 (Ac.Ft)
            Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      ***********************************************************************

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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 05/07/25

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: PRO1003100.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    40
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       45.284 (CFS)
               Total volume =       3.363 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
____________________________________________________________________________

User entry of depth-outflow-storage data
------------------------------------------------------------------------
Total number of inflow hydrograph intervals = 40
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
------------------------------------------------------------------------
------------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
------------------------------------------------------------------------
------------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
------------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.276      0.133      0.276        0.276
   2.000      0.584      0.193      0.583        0.585
   3.000      0.930      0.700      0.928        0.932
   3.500      1.118      0.824      1.115        1.121
   4.000      1.316      0.930      1.313        1.319
   4.500      1.528      1.024      1.524        1.532
   4.750      1.637      1.068      1.633        1.641
   5.000      1.749     18.283      1.686        1.812
   6.000      2.231    253.655      1.358        3.104
------------------------------------------------------------------------
               Hydrograph Detention Basin Routing
------------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
------------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                    Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0      11.3   22.64   33.96   45.28 (Ft.)
 0.083    1.82    0.00      0.006  OI      |       |       |       |     0.02
 0.167    3.81    0.01      0.026  O I     |       |       |       |     0.09
 0.250    3.95    0.03      0.052  O I     |       |       |       |     0.19
 0.333    4.37    0.04      0.081  O  I    |       |       |       |     0.29
 0.417    4.99    0.05      0.113  O  I    |       |       |       |     0.41
 0.500    5.64    0.07      0.149  O  I    |       |       |       |     0.54
 0.583    5.73    0.09      0.187  O   I   |       |       |       |     0.68
 0.667    5.83    0.11      0.226  O   I   |       |       |       |     0.82
 0.750    6.36    0.13      0.268  O   I   |       |       |       |     0.97
 0.833    5.91    0.14      0.309  O   I   |       |       |       |     1.11
 0.917    5.48    0.15      0.347  O  I    |       |       |       |     1.23
 1.000    5.93    0.15      0.385  O   I   |       |       |       |     1.36
 1.083    7.48    0.16      0.431  O    I  |       |       |       |     1.50
 1.167    8.79    0.17      0.485  O     I |       |       |       |     1.68
 1.250    9.09    0.19      0.546  O     I |       |       |       |     1.88
 1.333    8.65    0.22      0.605  O     I |       |       |       |     2.06
 1.417    9.77    0.31      0.667  O     I |       |       |       |     2.24
```

1.500	11.75	0.42	0.738	O	I	|	|	|	2.45
1.583	11.55	0.53	0.815	O	I	|	|	|	2.67
1.667	11.67	0.64	0.891	O	I	|	|	|	2.89
1.750	14.17	0.73	0.976	O	| I	|	|	|	3.12
1.833	15.57	0.79	1.073	O	| I	|	|	|	3.38
1.917	14.83	0.85	1.172	O	| I	|	|	|	3.64
2.000	14.56	0.90	1.267	O	| I	|	|	|	3.88
2.083	15.03	0.95	1.363	O	| I	|	|	|	4.11
2.167	18.41	1.00	1.471	O	| I	|	|	|	4.37
2.250	24.08	1.06	1.610	O	| |I	|	|	|	4.69
2.333	23.08	13.97	1.721	|	|O I	|	|	|	4.94
2.417	28.55	25.32	1.763	|	| |O I	|	|	|	5.03
2.500	39.40	36.18	1.786	|	| |	|O I |	|	5.08
2.583	45.28	43.91	1.801	|	| |	| | OI	5.11
2.667	42.61	43.96	1.802	|	| |	| IO|	5.11
2.750	25.74	31.69	1.776	|	| | I O	| |	5.06
2.833	12.07	16.83	1.740	|	I O |	| |	4.98
2.917	8.43	12.28	1.710	| I O	| |	| |	4.91
3.000	5.21	8.50	1.685	| I O |	| |	| |	4.86
3.083	1.91	5.08	1.663	|I O |	| |	| |	4.81
3.167	0.55	2.41	1.646	IO |	| |	| |	4.77
3.250	0.18	1.07	1.636	O |	| |	| |	4.75
3.333	0.03	1.07	1.630	O |	| |	| |	4.73
3.417	0.00	1.06	1.622	O |	| |	| |	4.72
3.500	0.00	1.06	1.615	O |	| |	| |	4.70
3.583	0.00	1.06	1.608	O |	| |	| |	4.68
3.667	0.00	1.05	1.601	O |	| |	| |	4.67
3.750	0.00	1.05	1.593	O |	| |	| |	4.65
3.833	0.00	1.05	1.586	O |	| |	| |	4.63
3.917	0.00	1.04	1.579	O |	| |	| |	4.62
4.000	0.00	1.04	1.572	O |	| |	| |	4.60
4.083	0.00	1.04	1.565	O |	| |	| |	4.58
4.167	0.00	1.04	1.557	O |	| |	| |	4.57
4.250	0.00	1.03	1.550	O |	| |	| |	4.55
4.333	0.00	1.03	1.543	O |	| |	| |	4.53
4.417	0.00	1.03	1.536	O |	| |	| |	4.52
4.500	0.00	1.02	1.529	O |	| |	| |	4.50
4.583	0.00	1.02	1.522	O |	| |	| |	4.49
4.667	0.00	1.02	1.515	O |	| |	| |	4.47
4.750	0.00	1.02	1.508	O |	| |	| |	4.45
4.833	0.00	1.01	1.501	O |	| |	| |	4.44
4.917	0.00	1.01	1.494	O |	| |	| |	4.42
5.000	0.00	1.01	1.487	O |	| |	| |	4.40
5.083	0.00	1.00	1.480	O |	| |	| |	4.39
5.167	0.00	1.00	1.473	O |	| |	| |	4.37
5.250	0.00	1.00	1.466	O |	| |	| |	4.35
5.333	0.00	0.99	1.460	O |	| |	| |	4.34
5.417	0.00	0.99	1.453	O |	| |	| |	4.32
5.500	0.00	0.99	1.446	O |	| |	| |	4.31
5.583	0.00	0.98	1.439	O |	| |	| |	4.29
5.667	0.00	0.98	1.432	O |	| |	| |	4.27
5.750	0.00	0.98	1.426	O |	| |	| |	4.26
5.833	0.00	0.98	1.419	O |	| |	| |	4.24
5.917	0.00	0.97	1.412	O |	| |	| |	4.23
6.000	0.00	0.97	1.406	O |	| |	| |	4.21
6.083	0.00	0.97	1.399	O |	| |	| |	4.20
6.167	0.00	0.96	1.392	O |	| |	| |	4.18
6.250	0.00	0.96	1.386	O |	| |	| |	4.16
6.333	0.00	0.96	1.379	O |	| |	| |	4.15
6.417	0.00	0.95	1.372	O |	| |	| |	4.13
6.500	0.00	0.95	1.366	O |	| |	| |	4.12
6.583	0.00	0.95	1.359	O |	| |	| |	4.10
6.667	0.00	0.95	1.353	O |	| |	| |	4.09
6.750	0.00	0.94	1.346	O |	| |	| |	4.07
6.833	0.00	0.94	1.340	O |	| |	| |	4.06
6.917	0.00	0.94	1.333	O |	| |	| |	4.04
7.000	0.00	0.93	1.327	O |	| |	| |	4.03
7.083	0.00	0.93	1.320	O |	| |	| |	4.01
7.167	0.00	0.93	1.314	O |	| |	| |	3.99
7.250	0.00	0.93	1.308	O |	| |	| |	3.98
7.333	0.00	0.92	1.301	O |	| |	| |	3.96
7.417	0.00	0.92	1.295	O |	| |	| |	3.95
7.500	0.00	0.92	1.289	O |	| |	| |	3.93
7.583	0.00	0.91	1.282	O |	| |	| |	3.91
7.667	0.00	0.91	1.276	O |	| |	| |	3.90
7.750	0.00	0.91	1.270	O |	| |	| |	3.88
7.833	0.00	0.90	1.264	O |	| |	| |	3.87
7.917	0.00	0.90	1.257	O |	| |	| |	3.85
8.000	0.00	0.90	1.251	O |	| |	| |	3.84
8.083	0.00	0.89	1.245	O |	| |	| |	3.82
8.167	0.00	0.89	1.239	O |	| |	| |	3.81
8.250	0.00	0.89	1.233	O |	| |	| |	3.79
8.333	0.00	0.88	1.227	O |	| |	| |	3.77
8.417	0.00	0.88	1.221	O |	| |	| |	3.76
8.500	0.00	0.88	1.215	O |	| |	| |	3.74
8.583	0.00	0.87	1.209	O |	| |	| |	3.73

8.667	0.00	0.87	1.203	o	|	|	|	|	3.71
8.750	0.00	0.87	1.197	o	|	|	|	|	3.70
8.833	0.00	0.86	1.191	o	|	|	|	|	3.68
8.917	0.00	0.86	1.185	o	|	|	|	|	3.67
9.000	0.00	0.86	1.179	o	|	|	|	|	3.65
9.083	0.00	0.85	1.173	o	|	|	|	|	3.64
9.167	0.00	0.85	1.167	o	|	|	|	|	3.62
9.250	0.00	0.85	1.161	o	|	|	|	|	3.61
9.333	0.00	0.84	1.155	o	|	|	|	|	3.59
9.417	0.00	0.84	1.150	o	|	|	|	|	3.58
9.500	0.00	0.84	1.144	o	|	|	|	|	3.57
9.583	0.00	0.83	1.138	o	|	|	|	|	3.55
9.667	0.00	0.83	1.132	o	|	|	|	|	3.54
9.750	0.00	0.83	1.127	o	|	|	|	|	3.52
9.833	0.00	0.83	1.121	o	|	|	|	|	3.51
9.917	0.00	0.82	1.115	o	|	|	|	|	3.49
10.000	0.00	0.82	1.110	o	|	|	|	|	3.48
10.083	0.00	0.81	1.104	o	|	|	|	|	3.46
10.167	0.00	0.81	1.098	o	|	|	|	|	3.45
10.250	0.00	0.81	1.093	o	|	|	|	|	3.43
10.333	0.00	0.80	1.087	o	|	|	|	|	3.42
10.417	0.00	0.80	1.082	o	|	|	|	|	3.40
10.500	0.00	0.80	1.076	o	|	|	|	|	3.39
10.583	0.00	0.79	1.071	o	|	|	|	|	3.37
10.667	0.00	0.79	1.065	o	|	|	|	|	3.36
10.750	0.00	0.79	1.060	o	|	|	|	|	3.35
10.833	0.00	0.78	1.054	o	|	|	|	|	3.33
10.917	0.00	0.78	1.049	o	|	|	|	|	3.32
11.000	0.00	0.78	1.044	o	|	|	|	|	3.30
11.083	0.00	0.77	1.038	o	|	|	|	|	3.29
11.167	0.00	0.77	1.033	o	|	|	|	|	3.27
11.250	0.00	0.76	1.028	o	|	|	|	|	3.26
11.333	0.00	0.76	1.023	o	|	|	|	|	3.25
11.417	0.00	0.76	1.017	o	|	|	|	|	3.23
11.500	0.00	0.75	1.012	o	|	|	|	|	3.22
11.583	0.00	0.75	1.007	o	|	|	|	|	3.20
11.667	0.00	0.75	1.002	o	|	|	|	|	3.19
11.750	0.00	0.74	0.997	o	|	|	|	|	3.18
11.833	0.00	0.74	0.992	o	|	|	|	|	3.16
11.917	0.00	0.74	0.986	o	|	|	|	|	3.15
12.000	0.00	0.73	0.981	o	|	|	|	|	3.14
12.083	0.00	0.73	0.976	o	|	|	|	|	3.12
12.167	0.00	0.73	0.971	o	|	|	|	|	3.11
12.250	0.00	0.72	0.966	o	|	|	|	|	3.10
12.333	0.00	0.72	0.961	o	|	|	|	|	3.08
12.417	0.00	0.72	0.956	o	|	|	|	|	3.07
12.500	0.00	0.71	0.951	o	|	|	|	|	3.06
12.583	0.00	0.71	0.947	o	|	|	|	|	3.04
12.667	0.00	0.71	0.942	o	|	|	|	|	3.03
12.750	0.00	0.70	0.937	o	|	|	|	|	3.02
12.833	0.00	0.70	0.932	o	|	|	|	|	3.01
12.917	0.00	0.70	0.927	o	|	|	|	|	2.99
13.000	0.00	0.69	0.922	o	|	|	|	|	2.98
13.083	0.00	0.68	0.918	o	|	|	|	|	2.96
13.167	0.00	0.68	0.913	o	|	|	|	|	2.95
13.250	0.00	0.67	0.908	o	|	|	|	|	2.94
13.333	0.00	0.66	0.904	o	|	|	|	|	2.92
13.417	0.00	0.65	0.899	o	|	|	|	|	2.91
13.500	0.00	0.65	0.895	o	|	|	|	|	2.90
13.583	0.00	0.64	0.890	o	|	|	|	|	2.89
13.667	0.00	0.64	0.886	o	|	|	|	|	2.87
13.750	0.00	0.63	0.882	o	|	|	|	|	2.86
13.833	0.00	0.62	0.877	o	|	|	|	|	2.85
13.917	0.00	0.62	0.873	o	|	|	|	|	2.84
14.000	0.00	0.61	0.869	o	|	|	|	|	2.82
14.083	0.00	0.60	0.865	o	|	|	|	|	2.81
14.167	0.00	0.60	0.860	o	|	|	|	|	2.80
14.250	0.00	0.59	0.856	o	|	|	|	|	2.79
14.333	0.00	0.59	0.852	o	|	|	|	|	2.78
14.417	0.00	0.58	0.848	o	|	|	|	|	2.76
14.500	0.00	0.57	0.844	o	|	|	|	|	2.75
14.583	0.00	0.57	0.840	o	|	|	|	|	2.74
14.667	0.00	0.56	0.836	o	|	|	|	|	2.73
14.750	0.00	0.56	0.833	o	|	|	|	|	2.72
14.833	0.00	0.55	0.829	o	|	|	|	|	2.71
14.917	0.00	0.55	0.825	o	|	|	|	|	2.70
15.000	0.00	0.54	0.821	o	|	|	|	|	2.69
15.083	0.00	0.54	0.818	o	|	|	|	|	2.68
15.167	0.00	0.53	0.814	o	|	|	|	|	2.66
15.250	0.00	0.52	0.810	o	|	|	|	|	2.65
15.333	0.00	0.52	0.807	o	|	|	|	|	2.64
15.417	0.00	0.51	0.803	o	|	|	|	|	2.63
15.500	0.00	0.51	0.800	o	|	|	|	|	2.62
15.583	0.00	0.50	0.796	o	|	|	|	|	2.61
15.667	0.00	0.50	0.793	o	|	|	|	|	2.60
15.750	0.00	0.49	0.789	o	|	|	|	|	2.59

15.833	0.00	0.49	0.786	o	|	|	|	|	2.58
15.917	0.00	0.48	0.783	o	|	|	|	|	2.57
16.000	0.00	0.48	0.779	o	|	|	|	|	2.56
16.083	0.00	0.47	0.776	o	|	|	|	|	2.55
16.167	0.00	0.47	0.773	o	|	|	|	|	2.55
16.250	0.00	0.46	0.769	o	|	|	|	|	2.54
16.333	0.00	0.46	0.766	o	|	|	|	|	2.53
16.417	0.00	0.46	0.763	o	|	|	|	|	2.52
16.500	0.00	0.45	0.760	o	|	|	|	|	2.51
16.583	0.00	0.45	0.757	o	|	|	|	|	2.50
16.667	0.00	0.44	0.754	o	|	|	|	|	2.49
16.750	0.00	0.44	0.751	o	|	|	|	|	2.48
16.833	0.00	0.43	0.748	o	|	|	|	|	2.47
16.917	0.00	0.43	0.745	o	|	|	|	|	2.46
17.000	0.00	0.42	0.742	o	|	|	|	|	2.46
17.083	0.00	0.42	0.739	o	|	|	|	|	2.45
17.167	0.00	0.42	0.736	o	|	|	|	|	2.44
17.250	0.00	0.41	0.733	o	|	|	|	|	2.43
17.333	0.00	0.41	0.730	o	|	|	|	|	2.42
17.417	0.00	0.40	0.728	o	|	|	|	|	2.42
17.500	0.00	0.40	0.725	o	|	|	|	|	2.41
17.583	0.00	0.40	0.722	o	|	|	|	|	2.40
17.667	0.00	0.39	0.719	o	|	|	|	|	2.39
17.750	0.00	0.39	0.717	o	|	|	|	|	2.38
17.833	0.00	0.38	0.714	o	|	|	|	|	2.38
17.917	0.00	0.38	0.711	o	|	|	|	|	2.37
18.000	0.00	0.38	0.709	o	|	|	|	|	2.36
18.083	0.00	0.37	0.706	o	|	|	|	|	2.35
18.167	0.00	0.37	0.704	o	|	|	|	|	2.35
18.250	0.00	0.36	0.701	o	|	|	|	|	2.34
18.333	0.00	0.36	0.699	o	|	|	|	|	2.33
18.417	0.00	0.36	0.696	o	|	|	|	|	2.32
18.500	0.00	0.35	0.694	o	|	|	|	|	2.32
18.583	0.00	0.35	0.691	o	|	|	|	|	2.31
18.667	0.00	0.35	0.689	o	|	|	|	|	2.30
18.750	0.00	0.34	0.687	o	|	|	|	|	2.30
18.833	0.00	0.34	0.684	o	|	|	|	|	2.29
18.917	0.00	0.34	0.682	o	|	|	|	|	2.28
19.000	0.00	0.33	0.680	o	|	|	|	|	2.28
19.083	0.00	0.33	0.677	o	|	|	|	|	2.27
19.167	0.00	0.33	0.675	o	|	|	|	|	2.26
19.250	0.00	0.32	0.673	o	|	|	|	|	2.26
19.333	0.00	0.32	0.671	o	|	|	|	|	2.25
19.417	0.00	0.32	0.668	o	|	|	|	|	2.24
19.500	0.00	0.31	0.666	o	|	|	|	|	2.24
19.583	0.00	0.31	0.664	o	|	|	|	|	2.23
19.667	0.00	0.31	0.662	o	|	|	|	|	2.23
19.750	0.00	0.30	0.660	o	|	|	|	|	2.22
19.833	0.00	0.30	0.658	o	|	|	|	|	2.21
19.917	0.00	0.30	0.656	o	|	|	|	|	2.21
20.000	0.00	0.30	0.654	o	|	|	|	|	2.20
20.083	0.00	0.29	0.652	o	|	|	|	|	2.20
20.167	0.00	0.29	0.650	o	|	|	|	|	2.19
20.250	0.00	0.29	0.648	o	|	|	|	|	2.18
20.333	0.00	0.28	0.646	o	|	|	|	|	2.18
20.417	0.00	0.28	0.644	o	|	|	|	|	2.17
20.500	0.00	0.28	0.642	o	|	|	|	|	2.17
20.583	0.00	0.27	0.640	o	|	|	|	|	2.16
20.667	0.00	0.27	0.638	o	|	|	|	|	2.16
20.750	0.00	0.27	0.636	o	|	|	|	|	2.15
20.833	0.00	0.27	0.634	o	|	|	|	|	2.15
20.917	0.00	0.26	0.633	o	|	|	|	|	2.14
21.000	0.00	0.26	0.631	o	|	|	|	|	2.14
21.083	0.00	0.26	0.629	o	|	|	|	|	2.13
21.167	0.00	0.26	0.627	o	|	|	|	|	2.12
21.250	0.00	0.25	0.625	o	|	|	|	|	2.12
21.333	0.00	0.25	0.624	o	|	|	|	|	2.11
21.417	0.00	0.25	0.622	o	|	|	|	|	2.11
21.500	0.00	0.25	0.620	o	|	|	|	|	2.10
21.583	0.00	0.24	0.619	o	|	|	|	|	2.10
21.667	0.00	0.24	0.617	o	|	|	|	|	2.10
21.750	0.00	0.24	0.615	o	|	|	|	|	2.09
21.833	0.00	0.24	0.614	o	|	|	|	|	2.09
21.917	0.00	0.23	0.612	o	|	|	|	|	2.08
22.000	0.00	0.23	0.610	o	|	|	|	|	2.08
22.083	0.00	0.23	0.609	o	|	|	|	|	2.07
22.167	0.00	0.23	0.607	o	|	|	|	|	2.07
22.250	0.00	0.22	0.606	o	|	|	|	|	2.06
22.333	0.00	0.22	0.604	o	|	|	|	|	2.06
22.417	0.00	0.22	0.603	o	|	|	|	|	2.05
22.500	0.00	0.22	0.601	o	|	|	|	|	2.05
22.583	0.00	0.22	0.600	o	|	|	|	|	2.05
22.667	0.00	0.21	0.598	o	|	|	|	|	2.04
22.750	0.00	0.21	0.597	o	|	|	|	|	2.04
22.833	0.00	0.21	0.595	o	|	|	|	|	2.03
22.917	0.00	0.21	0.594	o	|	|	|	|	2.03

23.000	0.00	0.21	0.592	o	|	|	|	|	2.02
23.083	0.00	0.20	0.591	o	|	|	|	|	2.02
23.167	0.00	0.20	0.590	o	|	|	|	|	2.02
23.250	0.00	0.20	0.588	o	|	|	|	|	2.01
23.333	0.00	0.20	0.587	o	|	|	|	|	2.01
23.417	0.00	0.20	0.585	o	|	|	|	|	2.00
23.500	0.00	0.19	0.584	o	|	|	|	|	2.00
23.583	0.00	0.19	0.583	o	|	|	|	|	2.00
23.667	0.00	0.19	0.581	o	|	|	|	|	1.99
23.750	0.00	0.19	0.580	o	|	|	|	|	1.99
23.833	0.00	0.19	0.579	o	|	|	|	|	1.98
23.917	0.00	0.19	0.577	o	|	|	|	|	1.98
24.000	0.00	0.19	0.576	o	|	|	|	|	1.97
24.083	0.00	0.19	0.575	o	|	|	|	|	1.97
24.167	0.00	0.19	0.574	o	|	|	|	|	1.97
24.250	0.00	0.19	0.572	o	|	|	|	|	1.96
24.333	0.00	0.19	0.571	o	|	|	|	|	1.96
24.417	0.00	0.19	0.570	o	|	|	|	|	1.95
24.500	0.00	0.19	0.568	o	|	|	|	|	1.95
24.583	0.00	0.19	0.567	o	|	|	|	|	1.94
24.667	0.00	0.19	0.566	o	|	|	|	|	1.94
24.750	0.00	0.19	0.564	o	|	|	|	|	1.94
24.833	0.00	0.19	0.563	o	|	|	|	|	1.93
24.917	0.00	0.19	0.562	o	|	|	|	|	1.93
25.000	0.00	0.19	0.560	o	|	|	|	|	1.92
25.083	0.00	0.19	0.559	o	|	|	|	|	1.92
25.167	0.00	0.19	0.558	o	|	|	|	|	1.92
25.250	0.00	0.19	0.557	o	|	|	|	|	1.91
25.333	0.00	0.19	0.555	o	|	|	|	|	1.91
25.417	0.00	0.19	0.554	o	|	|	|	|	1.90
25.500	0.00	0.19	0.553	o	|	|	|	|	1.90
25.583	0.00	0.19	0.551	o	|	|	|	|	1.89
25.667	0.00	0.19	0.550	o	|	|	|	|	1.89
25.750	0.00	0.19	0.549	o	|	|	|	|	1.89
25.833	0.00	0.19	0.548	o	|	|	|	|	1.88
25.917	0.00	0.19	0.546	o	|	|	|	|	1.88
26.000	0.00	0.19	0.545	o	|	|	|	|	1.87
26.083	0.00	0.19	0.544	o	|	|	|	|	1.87
26.167	0.00	0.18	0.542	o	|	|	|	|	1.87
26.250	0.00	0.18	0.541	o	|	|	|	|	1.86
26.333	0.00	0.18	0.540	o	|	|	|	|	1.86
26.417	0.00	0.18	0.539	o	|	|	|	|	1.85
26.500	0.00	0.18	0.537	o	|	|	|	|	1.85
26.583	0.00	0.18	0.536	o	|	|	|	|	1.84
26.667	0.00	0.18	0.535	o	|	|	|	|	1.84
26.750	0.00	0.18	0.534	o	|	|	|	|	1.84
26.833	0.00	0.18	0.532	o	|	|	|	|	1.83
26.917	0.00	0.18	0.531	o	|	|	|	|	1.83
27.000	0.00	0.18	0.530	o	|	|	|	|	1.82
27.083	0.00	0.18	0.529	o	|	|	|	|	1.82
27.167	0.00	0.18	0.527	o	|	|	|	|	1.82
27.250	0.00	0.18	0.526	o	|	|	|	|	1.81
27.333	0.00	0.18	0.525	o	|	|	|	|	1.81
27.417	0.00	0.18	0.524	o	|	|	|	|	1.80
27.500	0.00	0.18	0.522	o	|	|	|	|	1.80
27.583	0.00	0.18	0.521	o	|	|	|	|	1.80
27.667	0.00	0.18	0.520	o	|	|	|	|	1.79
27.750	0.00	0.18	0.519	o	|	|	|	|	1.79
27.833	0.00	0.18	0.517	o	|	|	|	|	1.78
27.917	0.00	0.18	0.516	o	|	|	|	|	1.78
28.000	0.00	0.18	0.515	o	|	|	|	|	1.78
28.083	0.00	0.18	0.514	o	|	|	|	|	1.77
28.167	0.00	0.18	0.512	o	|	|	|	|	1.77
28.250	0.00	0.18	0.511	o	|	|	|	|	1.76
28.333	0.00	0.18	0.510	o	|	|	|	|	1.76
28.417	0.00	0.18	0.509	o	|	|	|	|	1.76
28.500	0.00	0.18	0.507	o	|	|	|	|	1.75
28.583	0.00	0.18	0.506	o	|	|	|	|	1.75
28.667	0.00	0.18	0.505	o	|	|	|	|	1.74
28.750	0.00	0.18	0.504	o	|	|	|	|	1.74
28.833	0.00	0.18	0.503	o	|	|	|	|	1.74
28.917	0.00	0.18	0.501	o	|	|	|	|	1.73
29.000	0.00	0.18	0.500	o	|	|	|	|	1.73
29.083	0.00	0.18	0.499	o	|	|	|	|	1.72
29.167	0.00	0.18	0.498	o	|	|	|	|	1.72
29.250	0.00	0.18	0.496	o	|	|	|	|	1.72
29.333	0.00	0.18	0.495	o	|	|	|	|	1.71
29.417	0.00	0.18	0.494	o	|	|	|	|	1.71
29.500	0.00	0.18	0.493	o	|	|	|	|	1.70
29.583	0.00	0.18	0.492	o	|	|	|	|	1.70
29.667	0.00	0.17	0.490	o	|	|	|	|	1.70
29.750	0.00	0.17	0.489	o	|	|	|	|	1.69
29.833	0.00	0.17	0.488	o	|	|	|	|	1.69
29.917	0.00	0.17	0.487	o	|	|	|	|	1.68
30.000	0.00	0.17	0.486	o	|	|	|	|	1.68
30.083	0.00	0.17	0.484	o	|	|	|	|	1.68

30.167	0.00	0.17	0.483	o	|	|	|	1.67
30.250	0.00	0.17	0.482	o	|	|	|	1.67
30.333	0.00	0.17	0.481	o	|	|	|	1.67
30.417	0.00	0.17	0.480	o	|	|	|	1.66
30.500	0.00	0.17	0.479	o	|	|	|	1.66
30.583	0.00	0.17	0.477	o	|	|	|	1.65
30.667	0.00	0.17	0.476	o	|	|	|	1.65
30.750	0.00	0.17	0.475	o	|	|	|	1.65
30.833	0.00	0.17	0.474	o	|	|	|	1.64
30.917	0.00	0.17	0.473	o	|	|	|	1.64
31.000	0.00	0.17	0.471	o	|	|	|	1.63
31.083	0.00	0.17	0.470	o	|	|	|	1.63
31.167	0.00	0.17	0.469	o	|	|	|	1.63
31.250	0.00	0.17	0.468	o	|	|	|	1.62
31.333	0.00	0.17	0.467	o	|	|	|	1.62
31.417	0.00	0.17	0.466	o	|	|	|	1.62
31.500	0.00	0.17	0.464	o	|	|	|	1.61
31.583	0.00	0.17	0.463	o	|	|	|	1.61
31.667	0.00	0.17	0.462	o	|	|	|	1.60
31.750	0.00	0.17	0.461	o	|	|	|	1.60
31.833	0.00	0.17	0.460	o	|	|	|	1.60
31.917	0.00	0.17	0.459	o	|	|	|	1.59
32.000	0.00	0.17	0.457	o	|	|	|	1.59
32.083	0.00	0.17	0.456	o	|	|	|	1.59
32.167	0.00	0.17	0.455	o	|	|	|	1.58
32.250	0.00	0.17	0.454	o	|	|	|	1.58
32.333	0.00	0.17	0.453	o	|	|	|	1.57
32.417	0.00	0.17	0.452	o	|	|	|	1.57
32.500	0.00	0.17	0.450	o	|	|	|	1.57
32.583	0.00	0.17	0.449	o	|	|	|	1.56
32.667	0.00	0.17	0.448	o	|	|	|	1.56
32.750	0.00	0.17	0.447	o	|	|	|	1.56
32.833	0.00	0.17	0.446	o	|	|	|	1.55
32.917	0.00	0.17	0.445	o	|	|	|	1.55
33.000	0.00	0.17	0.444	o	|	|	|	1.54
33.083	0.00	0.17	0.442	o	|	|	|	1.54
33.167	0.00	0.17	0.441	o	|	|	|	1.54
33.250	0.00	0.16	0.440	o	|	|	|	1.53
33.333	0.00	0.16	0.439	o	|	|	|	1.53
33.417	0.00	0.16	0.438	o	|	|	|	1.53
33.500	0.00	0.16	0.437	o	|	|	|	1.52
33.583	0.00	0.16	0.436	o	|	|	|	1.52
33.667	0.00	0.16	0.435	o	|	|	|	1.51
33.750	0.00	0.16	0.433	o	|	|	|	1.51
33.833	0.00	0.16	0.432	o	|	|	|	1.51
33.917	0.00	0.16	0.431	o	|	|	|	1.50
34.000	0.00	0.16	0.430	o	|	|	|	1.50
34.083	0.00	0.16	0.429	o	|	|	|	1.50
34.167	0.00	0.16	0.428	o	|	|	|	1.49
34.250	0.00	0.16	0.427	o	|	|	|	1.49
34.333	0.00	0.16	0.426	o	|	|	|	1.49
34.417	0.00	0.16	0.424	o	|	|	|	1.48
34.500	0.00	0.16	0.423	o	|	|	|	1.48
34.583	0.00	0.16	0.422	o	|	|	|	1.47
34.667	0.00	0.16	0.421	o	|	|	|	1.47
34.750	0.00	0.16	0.420	o	|	|	|	1.47
34.833	0.00	0.16	0.419	o	|	|	|	1.46
34.917	0.00	0.16	0.418	o	|	|	|	1.46
35.000	0.00	0.16	0.417	o	|	|	|	1.46
35.083	0.00	0.16	0.416	o	|	|	|	1.45
35.167	0.00	0.16	0.414	o	|	|	|	1.45
35.250	0.00	0.16	0.413	o	|	|	|	1.45
35.333	0.00	0.16	0.412	o	|	|	|	1.44
35.417	0.00	0.16	0.411	o	|	|	|	1.44
35.500	0.00	0.16	0.410	o	|	|	|	1.44
35.583	0.00	0.16	0.409	o	|	|	|	1.43
35.667	0.00	0.16	0.408	o	|	|	|	1.43
35.750	0.00	0.16	0.407	o	|	|	|	1.42
35.833	0.00	0.16	0.406	o	|	|	|	1.42
35.917	0.00	0.16	0.405	o	|	|	|	1.42
36.000	0.00	0.16	0.403	o	|	|	|	1.41
36.083	0.00	0.16	0.402	o	|	|	|	1.41
36.167	0.00	0.16	0.401	o	|	|	|	1.41
36.250	0.00	0.16	0.400	o	|	|	|	1.40
36.333	0.00	0.16	0.399	o	|	|	|	1.40
36.417	0.00	0.16	0.398	o	|	|	|	1.40
36.500	0.00	0.16	0.397	o	|	|	|	1.39
36.583	0.00	0.16	0.396	o	|	|	|	1.39
36.667	0.00	0.16	0.395	o	|	|	|	1.39
36.750	0.00	0.16	0.394	o	|	|	|	1.38
36.833	0.00	0.16	0.393	o	|	|	|	1.38
36.917	0.00	0.16	0.392	o	|	|	|	1.38
37.000	0.00	0.16	0.391	o	|	|	|	1.37
37.083	0.00	0.16	0.389	o	|	|	|	1.37
37.167	0.00	0.15	0.388	o	|	|	|	1.36
37.250	0.00	0.15	0.387	o	|	|	|	1.36

37.333	0.00	0.15	0.386	o	|	|	|	|	1.36
37.417	0.00	0.15	0.385	o	|	|	|	|	1.35
37.500	0.00	0.15	0.384	o	|	|	|	|	1.35
37.583	0.00	0.15	0.383	o	|	|	|	|	1.35
37.667	0.00	0.15	0.382	o	|	|	|	|	1.34
37.750	0.00	0.15	0.381	o	|	|	|	|	1.34
37.833	0.00	0.15	0.380	o	|	|	|	|	1.34
37.917	0.00	0.15	0.379	o	|	|	|	|	1.33
38.000	0.00	0.15	0.378	o	|	|	|	|	1.33
38.083	0.00	0.15	0.377	o	|	|	|	|	1.33
38.167	0.00	0.15	0.376	o	|	|	|	|	1.32
38.250	0.00	0.15	0.375	o	|	|	|	|	1.32
38.333	0.00	0.15	0.374	o	|	|	|	|	1.32
38.417	0.00	0.15	0.373	o	|	|	|	|	1.31
38.500	0.00	0.15	0.372	o	|	|	|	|	1.31
38.583	0.00	0.15	0.370	o	|	|	|	|	1.31
38.667	0.00	0.15	0.369	o	|	|	|	|	1.30
38.750	0.00	0.15	0.368	o	|	|	|	|	1.30
38.833	0.00	0.15	0.367	o	|	|	|	|	1.30
38.917	0.00	0.15	0.366	o	|	|	|	|	1.29
39.000	0.00	0.15	0.365	o	|	|	|	|	1.29
39.083	0.00	0.15	0.364	o	|	|	|	|	1.29
39.167	0.00	0.15	0.363	o	|	|	|	|	1.28
39.250	0.00	0.15	0.362	o	|	|	|	|	1.28
39.333	0.00	0.15	0.361	o	|	|	|	|	1.28
39.417	0.00	0.15	0.360	o	|	|	|	|	1.27
39.500	0.00	0.15	0.359	o	|	|	|	|	1.27
39.583	0.00	0.15	0.358	o	|	|	|	|	1.27
39.667	0.00	0.15	0.357	o	|	|	|	|	1.26
39.750	0.00	0.15	0.356	o	|	|	|	|	1.26
39.833	0.00	0.15	0.355	o	|	|	|	|	1.26
39.917	0.00	0.15	0.354	o	|	|	|	|	1.25
40.000	0.00	0.15	0.353	o	|	|	|	|	1.25
40.083	0.00	0.15	0.352	o	|	|	|	|	1.25
40.167	0.00	0.15	0.351	o	|	|	|	|	1.24
40.250	0.00	0.15	0.350	o	|	|	|	|	1.24
40.333	0.00	0.15	0.349	o	|	|	|	|	1.24
40.417	0.00	0.15	0.348	o	|	|	|	|	1.23
40.500	0.00	0.15	0.347	o	|	|	|	|	1.23
40.583	0.00	0.15	0.346	o	|	|	|	|	1.23
40.667	0.00	0.15	0.345	o	|	|	|	|	1.22
40.750	0.00	0.15	0.344	o	|	|	|	|	1.22
40.833	0.00	0.15	0.343	o	|	|	|	|	1.22
40.917	0.00	0.15	0.342	o	|	|	|	|	1.21
41.000	0.00	0.15	0.341	o	|	|	|	|	1.21
41.083	0.00	0.15	0.340	o	|	|	|	|	1.21
41.167	0.00	0.15	0.339	o	|	|	|	|	1.20
41.250	0.00	0.15	0.338	o	|	|	|	|	1.20
41.333	0.00	0.14	0.337	o	|	|	|	|	1.20
41.417	0.00	0.14	0.336	o	|	|	|	|	1.19
41.500	0.00	0.14	0.335	o	|	|	|	|	1.19
41.583	0.00	0.14	0.334	o	|	|	|	|	1.19
41.667	0.00	0.14	0.333	o	|	|	|	|	1.18
41.750	0.00	0.14	0.332	o	|	|	|	|	1.18
41.833	0.00	0.14	0.331	o	|	|	|	|	1.18
41.917	0.00	0.14	0.330	o	|	|	|	|	1.17
42.000	0.00	0.14	0.329	o	|	|	|	|	1.17
42.083	0.00	0.14	0.328	o	|	|	|	|	1.17
42.167	0.00	0.14	0.327	o	|	|	|	|	1.17
42.250	0.00	0.14	0.326	o	|	|	|	|	1.16
42.333	0.00	0.14	0.325	o	|	|	|	|	1.16
42.417	0.00	0.14	0.324	o	|	|	|	|	1.16
42.500	0.00	0.14	0.323	o	|	|	|	|	1.15
42.583	0.00	0.14	0.322	o	|	|	|	|	1.15
42.667	0.00	0.14	0.321	o	|	|	|	|	1.15
42.750	0.00	0.14	0.320	o	|	|	|	|	1.14
42.833	0.00	0.14	0.319	o	|	|	|	|	1.14
42.917	0.00	0.14	0.318	o	|	|	|	|	1.14
43.000	0.00	0.14	0.317	o	|	|	|	|	1.13
43.083	0.00	0.14	0.316	o	|	|	|	|	1.13
43.167	0.00	0.14	0.315	o	|	|	|	|	1.13
43.250	0.00	0.14	0.314	o	|	|	|	|	1.12
43.333	0.00	0.14	0.313	o	|	|	|	|	1.12
43.417	0.00	0.14	0.312	o	|	|	|	|	1.12
43.500	0.00	0.14	0.311	o	|	|	|	|	1.11
43.583	0.00	0.14	0.310	o	|	|	|	|	1.11
43.667	0.00	0.14	0.309	o	|	|	|	|	1.11
43.750	0.00	0.14	0.308	o	|	|	|	|	1.11
43.833	0.00	0.14	0.307	o	|	|	|	|	1.10
43.917	0.00	0.14	0.307	o	|	|	|	|	1.10
44.000	0.00	0.14	0.306	o	|	|	|	|	1.10
44.083	0.00	0.14	0.305	o	|	|	|	|	1.09
44.167	0.00	0.14	0.304	o	|	|	|	|	1.09
44.250	0.00	0.14	0.303	o	|	|	|	|	1.09
44.333	0.00	0.14	0.302	o	|	|	|	|	1.08
44.417	0.00	0.14	0.301	o	|	|	|	|	1.08

44.500	0.00	0.14	0.300	o	|	|	|	|	1.08
44.583	0.00	0.14	0.299	o	|	|	|	|	1.07
44.667	0.00	0.14	0.298	o	|	|	|	|	1.07
44.750	0.00	0.14	0.297	o	|	|	|	|	1.07
44.833	0.00	0.14	0.296	o	|	|	|	|	1.07
44.917	0.00	0.14	0.295	o	|	|	|	|	1.06
45.000	0.00	0.14	0.294	o	|	|	|	|	1.06
45.083	0.00	0.14	0.293	o	|	|	|	|	1.06
45.167	0.00	0.14	0.292	o	|	|	|	|	1.05
45.250	0.00	0.14	0.291	o	|	|	|	|	1.05
45.333	0.00	0.14	0.290	o	|	|	|	|	1.05
45.417	0.00	0.14	0.290	o	|	|	|	|	1.04
45.500	0.00	0.14	0.289	o	|	|	|	|	1.04
45.583	0.00	0.14	0.288	o	|	|	|	|	1.04
45.667	0.00	0.14	0.287	o	|	|	|	|	1.03
45.750	0.00	0.13	0.286	o	|	|	|	|	1.03
45.833	0.00	0.13	0.285	o	|	|	|	|	1.03
45.917	0.00	0.13	0.284	o	|	|	|	|	1.03
46.000	0.00	0.13	0.283	o	|	|	|	|	1.02
46.083	0.00	0.13	0.282	o	|	|	|	|	1.02
46.167	0.00	0.13	0.281	o	|	|	|	|	1.02
46.250	0.00	0.13	0.280	o	|	|	|	|	1.01
46.333	0.00	0.13	0.279	o	|	|	|	|	1.01
46.417	0.00	0.13	0.278	o	|	|	|	|	1.01
46.500	0.00	0.13	0.277	o	|	|	|	|	1.00
46.583	0.00	0.13	0.277	o	|	|	|	|	1.00
46.667	0.00	0.13	0.276	o	|	|	|	|	1.00
46.750	0.00	0.13	0.275	o	|	|	|	|	1.00
46.833	0.00	0.13	0.274	o	|	|	|	|	0.99
46.917	0.00	0.13	0.273	o	|	|	|	|	0.99
47.000	0.00	0.13	0.272	o	|	|	|	|	0.99
47.083	0.00	0.13	0.271	o	|	|	|	|	0.98
47.167	0.00	0.13	0.270	o	|	|	|	|	0.98
47.250	0.00	0.13	0.269	o	|	|	|	|	0.98
47.333	0.00	0.13	0.268	o	|	|	|	|	0.97
47.417	0.00	0.13	0.268	o	|	|	|	|	0.97
47.500	0.00	0.13	0.267	o	|	|	|	|	0.97
47.583	0.00	0.13	0.266	o	|	|	|	|	0.96
47.667	0.00	0.13	0.265	o	|	|	|	|	0.96
47.750	0.00	0.13	0.264	o	|	|	|	|	0.96
47.833	0.00	0.13	0.263	o	|	|	|	|	0.95
47.917	0.00	0.13	0.262	o	|	|	|	|	0.95
48.000	0.00	0.13	0.261	o	|	|	|	|	0.95
48.083	0.00	0.13	0.261	o	|	|	|	|	0.94
48.167	0.00	0.13	0.260	o	|	|	|	|	0.94
48.250	0.00	0.12	0.259	o	|	|	|	|	0.94
48.333	0.00	0.12	0.258	o	|	|	|	|	0.93
48.417	0.00	0.12	0.257	o	|	|	|	|	0.93
48.500	0.00	0.12	0.256	o	|	|	|	|	0.93
48.583	0.00	0.12	0.255	o	|	|	|	|	0.93
48.667	0.00	0.12	0.255	o	|	|	|	|	0.92
48.750	0.00	0.12	0.254	o	|	|	|	|	0.92
48.833	0.00	0.12	0.253	o	|	|	|	|	0.92
48.917	0.00	0.12	0.252	o	|	|	|	|	0.91
49.000	0.00	0.12	0.251	o	|	|	|	|	0.91
49.083	0.00	0.12	0.250	o	|	|	|	|	0.91
49.167	0.00	0.12	0.250	o	|	|	|	|	0.90
49.250	0.00	0.12	0.249	o	|	|	|	|	0.90
49.333	0.00	0.12	0.248	o	|	|	|	|	0.90
49.417	0.00	0.12	0.247	o	|	|	|	|	0.90
49.500	0.00	0.12	0.246	o	|	|	|	|	0.89
49.583	0.00	0.12	0.245	o	|	|	|	|	0.89
49.667	0.00	0.12	0.245	o	|	|	|	|	0.89
49.750	0.00	0.12	0.244	o	|	|	|	|	0.88
49.833	0.00	0.12	0.243	o	|	|	|	|	0.88
49.917	0.00	0.12	0.242	o	|	|	|	|	0.88
50.000	0.00	0.12	0.241	o	|	|	|	|	0.87
50.083	0.00	0.12	0.241	o	|	|	|	|	0.87
50.167	0.00	0.12	0.240	o	|	|	|	|	0.87
50.250	0.00	0.12	0.239	o	|	|	|	|	0.87
50.333	0.00	0.11	0.238	o	|	|	|	|	0.86
50.417	0.00	0.11	0.237	o	|	|	|	|	0.86
50.500	0.00	0.11	0.237	o	|	|	|	|	0.86
50.583	0.00	0.11	0.236	o	|	|	|	|	0.85
50.667	0.00	0.11	0.235	o	|	|	|	|	0.85
50.750	0.00	0.11	0.234	o	|	|	|	|	0.85
50.833	0.00	0.11	0.233	o	|	|	|	|	0.85
50.917	0.00	0.11	0.233	o	|	|	|	|	0.84
51.000	0.00	0.11	0.232	o	|	|	|	|	0.84
51.083	0.00	0.11	0.231	o	|	|	|	|	0.84
51.167	0.00	0.11	0.230	o	|	|	|	|	0.83
51.250	0.00	0.11	0.230	o	|	|	|	|	0.83
51.333	0.00	0.11	0.229	o	|	|	|	|	0.83
51.417	0.00	0.11	0.228	o	|	|	|	|	0.83
51.500	0.00	0.11	0.227	o	|	|	|	|	0.82
51.583	0.00	0.11	0.227	o	|	|	|	|	0.82

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51.667    0.00    0.11      0.226  o       |       |       |       |     0.82
51.750    0.00    0.11      0.225  o       |       |       |       |     0.82
51.833    0.00    0.11      0.224  o       |       |       |       |     0.81
51.917    0.00    0.11      0.224  o       |       |       |       |     0.81
52.000    0.00    0.11      0.223  o       |       |       |       |     0.81
52.083    0.00    0.11      0.222  o       |       |       |       |     0.80
52.167    0.00    0.11      0.221  o       |       |       |       |     0.80
52.250    0.00    0.11      0.221  o       |       |       |       |     0.80
52.333    0.00    0.11      0.220  o       |       |       |       |     0.80
52.417    0.00    0.11      0.219  o       |       |       |       |     0.79
52.500    0.00    0.11      0.218  o       |       |       |       |     0.79
52.583    0.00    0.10      0.218  o       |       |       |       |     0.79
52.667    0.00    0.10      0.217  o       |       |       |       |     0.79
52.750    0.00    0.10      0.216  o       |       |       |       |     0.78
52.833    0.00    0.10      0.216  o       |       |       |       |     0.78
52.917    0.00    0.10      0.215  o       |       |       |       |     0.78
53.000    0.00    0.10      0.214  o       |       |       |       |     0.78
53.083    0.00    0.10      0.213  o       |       |       |       |     0.77
53.167    0.00    0.10      0.213  o       |       |       |       |     0.77
53.250    0.00    0.10      0.212  o       |       |       |       |     0.77
53.333    0.00    0.10      0.211  o       |       |       |       |     0.77
53.417    0.00    0.10      0.211  o       |       |       |       |     0.76
53.500    0.00    0.10      0.210  o       |       |       |       |     0.76
53.583    0.00    0.10      0.209  o       |       |       |       |     0.76
53.667    0.00    0.10      0.209  o       |       |       |       |     0.76
53.750    0.00    0.10      0.208  o       |       |       |       |     0.75
53.833    0.00    0.10      0.207  o       |       |       |       |     0.75

 Remaining water in basin =    0.21 (Ac.Ft)

 ****************************HYDROGRAPH DATA****************************
               Number of intervals =   646
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       43.957 (CFS)
               Total volume =       3.156 (Ac.Ft)
        Status of hydrographs being held in storage
                   Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
        Peak (CFS)      0.000     0.000     0.000     0.000     0.000
        Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/07/25

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: PRO1006100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 76
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 45.417 (CFS)
Total volume = 4.752 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 76
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.276	0.133	0.276	0.276
2.000	0.584	0.193	0.583	0.585
3.000	0.930	0.700	0.928	0.932
3.500	1.118	0.824	1.115	1.121
4.000	1.316	0.930	1.313	1.319
4.500	1.528	1.024	1.524	1.532
4.750	1.637	1.068	1.633	1.641
5.000	1.749	18.283	1.686	1.812
6.000	2.231	253.655	1.358	3.104

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 11.4 22.71 34.06 45.42	Depth (Ft.)
0.083	1.05	0.00	0.004	O	0.01
0.167	2.41	0.01	0.015	OI	0.06
0.250	2.88	0.02	0.034	O I	0.12
0.333	3.03	0.03	0.054	O I	0.19
0.417	3.09	0.04	0.075	O I	0.27
0.500	3.31	0.05	0.096	O I	0.35
0.583	3.53	0.06	0.120	O I	0.43
0.667	3.58	0.07	0.144	O I	0.52
0.750	3.60	0.08	0.168	O I	0.61
0.833	3.61	0.09	0.192	O I	0.70
0.917	3.61	0.10	0.216	O I	0.78
1.000	3.82	0.12	0.241	O I	0.87
1.083	4.05	0.13	0.267	O I	0.97
1.167	4.10	0.14	0.295	O I	1.06
1.250	4.12	0.14	0.322	O I	1.15
1.333	4.13	0.15	0.349	O I	1.24
1.417	4.13	0.15	0.377	O I	1.33

1.500	4.13	0.16	0.404	O I	|	|	|	|	1.42
1.583	4.13	0.16	0.431	O I	|	|	|	|	1.50
1.667	4.13	0.17	0.459	O I	|	|	|	|	1.59
1.750	4.13	0.17	0.486	O I	|	|	|	|	1.68
1.833	4.13	0.18	0.513	O I	|	|	|	|	1.77
1.917	4.13	0.18	0.540	O I	|	|	|	|	1.86
2.000	4.34	0.19	0.568	O I	|	|	|	|	1.95
2.083	4.36	0.21	0.597	O I	|	|	|	|	2.04
2.167	4.39	0.25	0.625	O I	|	|	|	|	2.12
2.250	4.59	0.30	0.654	O I	|	|	|	|	2.20
2.333	4.62	0.34	0.684	O I	|	|	|	|	2.29
2.417	4.64	0.38	0.713	O I	|	|	|	|	2.37
2.500	4.64	0.43	0.742	O I	|	|	|	|	2.46
2.583	4.64	0.47	0.771	O I	|	|	|	|	2.54
2.667	4.64	0.51	0.800	O I	|	|	|	|	2.62
2.750	4.85	0.55	0.829	O I	|	|	|	|	2.71
2.833	5.08	0.60	0.859	O I	|	|	|	|	2.80
2.917	5.13	0.64	0.890	O I	|	|	|	|	2.88
3.000	5.15	0.69	0.921	O I	|	|	|	|	2.97
3.083	5.16	0.71	0.952	O I	|	|	|	|	3.06
3.167	5.37	0.73	0.983	O I	|	|	|	|	3.14
3.250	5.60	0.76	1.015	O I	|	|	|	|	3.23
3.333	5.65	0.78	1.049	O I	|	|	|	|	3.32
3.417	6.00	0.80	1.084	O I	|	|	|	|	3.41
3.500	6.80	0.83	1.122	O I	|	|	|	|	3.51
3.583	7.76	0.85	1.166	O I	|	|	|	|	3.62
3.667	8.35	0.88	1.216	O I	|	|	|	|	3.75
3.750	8.92	0.90	1.269	O I	|	|	|	|	3.88
3.833	9.43	0.93	1.326	O I	|	|	|	|	4.02
3.917	9.96	0.96	1.386	O I	|	|	|	|	4.17
4.000	10.46	0.99	1.450	O I	|	|	|	|	4.32
4.083	11.00	1.02	1.517	O I	|	|	|	|	4.47
4.167	11.91	1.05	1.589	O I	|	|	|	|	4.64
4.250	12.91	4.08	1.657	| O I	|	|	|	|	4.79
4.333	13.92	10.54	1.699	| O I	|	|	|	|	4.89
4.417	14.95	13.24	1.716	| OI	|	|	|	|	4.93
4.500	15.57	14.64	1.725	| O	|	|	|	|	4.95
4.583	16.14	15.48	1.731	| OI	|	|	|	|	4.96
4.667	17.07	16.26	1.736	| OI	|	|	|	|	4.97
4.750	18.07	17.17	1.742	| O	|	|	|	|	4.98
4.833	18.66	18.00	1.747	| OI	|	|	|	|	5.00
4.917	19.24	18.96	1.750	| O	|	|	|	|	5.00
5.000	20.17	19.89	1.752	| O	|	|	|	|	5.01
5.083	22.84	21.92	1.756	| OI	|	|	|	|	5.02
5.167	27.37	25.92	1.765	| OI	|	|	|	|	5.03
5.250	31.47	30.31	1.774	| OI	|	|	|	|	5.05
5.333	34.80	33.85	1.781	| OI	|	|	|	|	5.07
5.417	38.85	37.58	1.789	| OI	|	|	|	|	5.08
5.500	45.42	43.29	1.800	| O I	|	|	|	|	5.11
5.583	34.65	39.21	1.792	| I O	|	|	|	|	5.09
5.667	15.12	21.24	1.755	| I O	|	|	|	|	5.01
5.750	7.29	12.97	1.714	| I O	|	|	|	|	4.92
5.833	4.24	7.98	1.682	| I O	|	|	|	|	4.85
5.917	2.47	4.78	1.661	|I O	|	|	|	|	4.80
6.000	1.54	2.86	1.649	|IO	|	|	|	|	4.78
6.083	0.75	1.68	1.641	IO	|	|	|	|	4.76
6.167	0.20	1.07	1.635	O	|	|	|	|	4.74
6.250	0.06	1.06	1.628	O	|	|	|	|	4.73
6.333	0.02	1.06	1.621	O	|	|	|	|	4.71
6.417	0.00	1.06	1.614	O	|	|	|	|	4.70
6.500	0.00	1.06	1.607	O	|	|	|	|	4.68
6.583	0.00	1.05	1.600	O	|	|	|	|	4.66
6.667	0.00	1.05	1.592	O	|	|	|	|	4.65
6.750	0.00	1.05	1.585	O	|	|	|	|	4.63
6.833	0.00	1.04	1.578	O	|	|	|	|	4.61
6.917	0.00	1.04	1.571	O	|	|	|	|	4.60
7.000	0.00	1.04	1.564	O	|	|	|	|	4.58
7.083	0.00	1.04	1.556	O	|	|	|	|	4.57
7.167	0.00	1.03	1.549	O	|	|	|	|	4.55
7.250	0.00	1.03	1.542	O	|	|	|	|	4.53
7.333	0.00	1.03	1.535	O	|	|	|	|	4.52
7.417	0.00	1.02	1.528	O	|	|	|	|	4.50
7.500	0.00	1.02	1.521	O	|	|	|	|	4.48
7.583	0.00	1.02	1.514	O	|	|	|	|	4.47
7.667	0.00	1.01	1.507	O	|	|	|	|	4.45
7.750	0.00	1.01	1.500	O	|	|	|	|	4.43
7.833	0.00	1.01	1.493	O	|	|	|	|	4.42
7.917	0.00	1.01	1.486	O	|	|	|	|	4.40
8.000	0.00	1.00	1.479	O	|	|	|	|	4.38
8.083	0.00	1.00	1.472	O	|	|	|	|	4.37
8.167	0.00	1.00	1.465	O	|	|	|	|	4.35
8.250	0.00	0.99	1.459	O	|	|	|	|	4.34
8.333	0.00	0.99	1.452	O	|	|	|	|	4.32
8.417	0.00	0.99	1.445	O	|	|	|	|	4.30
8.500	0.00	0.98	1.438	O	|	|	|	|	4.29
8.583	0.00	0.98	1.431	O	|	|	|	|	4.27

8.667	0.00	0.98	1.425	o	|	|	|	|	4.26
8.750	0.00	0.98	1.418	o	|	|	|	|	4.24
8.833	0.00	0.97	1.411	o	|	|	|	|	4.22
8.917	0.00	0.97	1.404	o	|	|	|	|	4.21
9.000	0.00	0.97	1.398	o	|	|	|	|	4.19
9.083	0.00	0.96	1.391	o	|	|	|	|	4.18
9.167	0.00	0.96	1.385	o	|	|	|	|	4.16
9.250	0.00	0.96	1.378	o	|	|	|	|	4.15
9.333	0.00	0.95	1.371	o	|	|	|	|	4.13
9.417	0.00	0.95	1.365	o	|	|	|	|	4.12
9.500	0.00	0.95	1.358	o	|	|	|	|	4.10
9.583	0.00	0.95	1.352	o	|	|	|	|	4.08
9.667	0.00	0.94	1.345	o	|	|	|	|	4.07
9.750	0.00	0.94	1.339	o	|	|	|	|	4.05
9.833	0.00	0.94	1.332	o	|	|	|	|	4.04
9.917	0.00	0.93	1.326	o	|	|	|	|	4.02
10.000	0.00	0.93	1.319	o	|	|	|	|	4.01
10.083	0.00	0.93	1.313	o	|	|	|	|	3.99
10.167	0.00	0.92	1.307	o	|	|	|	|	3.98
10.250	0.00	0.92	1.300	o	|	|	|	|	3.96
10.333	0.00	0.92	1.294	o	|	|	|	|	3.94
10.417	0.00	0.91	1.288	o	|	|	|	|	3.93
10.500	0.00	0.91	1.281	o	|	|	|	|	3.91
10.583	0.00	0.91	1.275	o	|	|	|	|	3.90
10.667	0.00	0.90	1.269	o	|	|	|	|	3.88
10.750	0.00	0.90	1.263	o	|	|	|	|	3.87
10.833	0.00	0.90	1.256	o	|	|	|	|	3.85
10.917	0.00	0.89	1.250	o	|	|	|	|	3.83
11.000	0.00	0.89	1.244	o	|	|	|	|	3.82
11.083	0.00	0.89	1.238	o	|	|	|	|	3.80
11.167	0.00	0.88	1.232	o	|	|	|	|	3.79
11.250	0.00	0.88	1.226	o	|	|	|	|	3.77
11.333	0.00	0.88	1.220	o	|	|	|	|	3.76
11.417	0.00	0.88	1.214	o	|	|	|	|	3.74
11.500	0.00	0.87	1.208	o	|	|	|	|	3.73
11.583	0.00	0.87	1.202	o	|	|	|	|	3.71
11.667	0.00	0.87	1.196	o	|	|	|	|	3.70
11.750	0.00	0.86	1.190	o	|	|	|	|	3.68
11.833	0.00	0.86	1.184	o	|	|	|	|	3.67
11.917	0.00	0.86	1.178	o	|	|	|	|	3.65
12.000	0.00	0.85	1.172	o	|	|	|	|	3.64
12.083	0.00	0.85	1.166	o	|	|	|	|	3.62
12.167	0.00	0.85	1.160	o	|	|	|	|	3.61
12.250	0.00	0.84	1.154	o	|	|	|	|	3.59
12.333	0.00	0.84	1.149	o	|	|	|	|	3.58
12.417	0.00	0.84	1.143	o	|	|	|	|	3.56
12.500	0.00	0.83	1.137	o	|	|	|	|	3.55
12.583	0.00	0.83	1.131	o	|	|	|	|	3.53
12.667	0.00	0.83	1.126	o	|	|	|	|	3.52
12.750	0.00	0.83	1.120	o	|	|	|	|	3.51
12.833	0.00	0.82	1.114	o	|	|	|	|	3.49
12.917	0.00	0.82	1.109	o	|	|	|	|	3.48
13.000	0.00	0.81	1.103	o	|	|	|	|	3.46
13.083	0.00	0.81	1.097	o	|	|	|	|	3.45
13.167	0.00	0.81	1.092	o	|	|	|	|	3.43
13.250	0.00	0.80	1.086	o	|	|	|	|	3.42
13.333	0.00	0.80	1.081	o	|	|	|	|	3.40
13.417	0.00	0.80	1.075	o	|	|	|	|	3.39
13.500	0.00	0.79	1.070	o	|	|	|	|	3.37
13.583	0.00	0.79	1.064	o	|	|	|	|	3.36
13.667	0.00	0.79	1.059	o	|	|	|	|	3.34
13.750	0.00	0.78	1.054	o	|	|	|	|	3.33
13.833	0.00	0.78	1.048	o	|	|	|	|	3.31
13.917	0.00	0.77	1.043	o	|	|	|	|	3.30
14.000	0.00	0.77	1.038	o	|	|	|	|	3.29
14.083	0.00	0.77	1.032	o	|	|	|	|	3.27
14.167	0.00	0.76	1.027	o	|	|	|	|	3.26
14.250	0.00	0.76	1.022	o	|	|	|	|	3.24
14.333	0.00	0.76	1.017	o	|	|	|	|	3.23
14.417	0.00	0.75	1.011	o	|	|	|	|	3.22
14.500	0.00	0.75	1.006	o	|	|	|	|	3.20
14.583	0.00	0.75	1.001	o	|	|	|	|	3.19
14.667	0.00	0.74	0.996	o	|	|	|	|	3.18
14.750	0.00	0.74	0.991	o	|	|	|	|	3.16
14.833	0.00	0.74	0.986	o	|	|	|	|	3.15
14.917	0.00	0.73	0.981	o	|	|	|	|	3.13
15.000	0.00	0.73	0.976	o	|	|	|	|	3.12
15.083	0.00	0.73	0.971	o	|	|	|	|	3.11
15.167	0.00	0.72	0.966	o	|	|	|	|	3.09
15.250	0.00	0.72	0.961	o	|	|	|	|	3.08
15.333	0.00	0.72	0.956	o	|	|	|	|	3.07
15.417	0.00	0.71	0.951	o	|	|	|	|	3.06
15.500	0.00	0.71	0.946	o	|	|	|	|	3.04
15.583	0.00	0.71	0.941	o	|	|	|	|	3.03
15.667	0.00	0.70	0.936	o	|	|	|	|	3.02
15.750	0.00	0.70	0.931	o	|	|	|	|	3.00

15.833	0.00	0.69	0.926	o	|	|	|	|	2.99
15.917	0.00	0.69	0.922	o	|	|	|	|	2.98
16.000	0.00	0.68	0.917	o	|	|	|	|	2.96
16.083	0.00	0.67	0.912	o	|	|	|	|	2.95
16.167	0.00	0.67	0.908	o	|	|	|	|	2.94
16.250	0.00	0.66	0.903	o	|	|	|	|	2.92
16.333	0.00	0.65	0.899	o	|	|	|	|	2.91
16.417	0.00	0.65	0.894	o	|	|	|	|	2.90
16.500	0.00	0.64	0.890	o	|	|	|	|	2.88
16.583	0.00	0.63	0.885	o	|	|	|	|	2.87
16.667	0.00	0.63	0.881	o	|	|	|	|	2.86
16.750	0.00	0.62	0.877	o	|	|	|	|	2.85
16.833	0.00	0.62	0.872	o	|	|	|	|	2.83
16.917	0.00	0.61	0.868	o	|	|	|	|	2.82
17.000	0.00	0.60	0.864	o	|	|	|	|	2.81
17.083	0.00	0.60	0.860	o	|	|	|	|	2.80
17.167	0.00	0.59	0.856	o	|	|	|	|	2.79
17.250	0.00	0.59	0.852	o	|	|	|	|	2.77
17.333	0.00	0.58	0.848	o	|	|	|	|	2.76
17.417	0.00	0.57	0.844	o	|	|	|	|	2.75
17.500	0.00	0.57	0.840	o	|	|	|	|	2.74
17.583	0.00	0.56	0.836	o	|	|	|	|	2.73
17.667	0.00	0.56	0.832	o	|	|	|	|	2.72
17.750	0.00	0.55	0.828	o	|	|	|	|	2.71
17.833	0.00	0.55	0.824	o	|	|	|	|	2.69
17.917	0.00	0.54	0.821	o	|	|	|	|	2.68
18.000	0.00	0.53	0.817	o	|	|	|	|	2.67
18.083	0.00	0.53	0.813	o	|	|	|	|	2.66
18.167	0.00	0.52	0.810	o	|	|	|	|	2.65
18.250	0.00	0.52	0.806	o	|	|	|	|	2.64
18.333	0.00	0.51	0.803	o	|	|	|	|	2.63
18.417	0.00	0.51	0.799	o	|	|	|	|	2.62
18.500	0.00	0.50	0.796	o	|	|	|	|	2.61
18.583	0.00	0.50	0.792	o	|	|	|	|	2.60
18.667	0.00	0.49	0.789	o	|	|	|	|	2.59
18.750	0.00	0.49	0.785	o	|	|	|	|	2.58
18.833	0.00	0.48	0.782	o	|	|	|	|	2.57
18.917	0.00	0.48	0.779	o	|	|	|	|	2.56
19.000	0.00	0.47	0.775	o	|	|	|	|	2.55
19.083	0.00	0.47	0.772	o	|	|	|	|	2.54
19.167	0.00	0.46	0.769	o	|	|	|	|	2.53
19.250	0.00	0.46	0.766	o	|	|	|	|	2.53
19.333	0.00	0.45	0.763	o	|	|	|	|	2.52
19.417	0.00	0.45	0.760	o	|	|	|	|	2.51
19.500	0.00	0.45	0.756	o	|	|	|	|	2.50
19.583	0.00	0.44	0.753	o	|	|	|	|	2.49
19.667	0.00	0.44	0.750	o	|	|	|	|	2.48
19.750	0.00	0.43	0.747	o	|	|	|	|	2.47
19.833	0.00	0.43	0.744	o	|	|	|	|	2.46
19.917	0.00	0.42	0.741	o	|	|	|	|	2.46
20.000	0.00	0.42	0.739	o	|	|	|	|	2.45
20.083	0.00	0.42	0.736	o	|	|	|	|	2.44
20.167	0.00	0.41	0.733	o	|	|	|	|	2.43
20.250	0.00	0.41	0.730	o	|	|	|	|	2.42
20.333	0.00	0.40	0.727	o	|	|	|	|	2.41
20.417	0.00	0.40	0.724	o	|	|	|	|	2.41
20.500	0.00	0.39	0.722	o	|	|	|	|	2.40
20.583	0.00	0.39	0.719	o	|	|	|	|	2.39
20.667	0.00	0.39	0.716	o	|	|	|	|	2.38
20.750	0.00	0.38	0.714	o	|	|	|	|	2.37
20.833	0.00	0.38	0.711	o	|	|	|	|	2.37
20.917	0.00	0.38	0.708	o	|	|	|	|	2.36
21.000	0.00	0.37	0.706	o	|	|	|	|	2.35
21.083	0.00	0.37	0.703	o	|	|	|	|	2.34
21.167	0.00	0.36	0.701	o	|	|	|	|	2.34
21.250	0.00	0.36	0.698	o	|	|	|	|	2.33
21.333	0.00	0.36	0.696	o	|	|	|	|	2.32
21.417	0.00	0.35	0.693	o	|	|	|	|	2.32
21.500	0.00	0.35	0.691	o	|	|	|	|	2.31
21.583	0.00	0.35	0.689	o	|	|	|	|	2.30
21.667	0.00	0.34	0.686	o	|	|	|	|	2.30
21.750	0.00	0.34	0.684	o	|	|	|	|	2.29
21.833	0.00	0.34	0.682	o	|	|	|	|	2.28
21.917	0.00	0.33	0.679	o	|	|	|	|	2.28
22.000	0.00	0.33	0.677	o	|	|	|	|	2.27
22.083	0.00	0.33	0.675	o	|	|	|	|	2.26
22.167	0.00	0.32	0.672	o	|	|	|	|	2.26
22.250	0.00	0.32	0.670	o	|	|	|	|	2.25
22.333	0.00	0.32	0.668	o	|	|	|	|	2.24
22.417	0.00	0.31	0.666	o	|	|	|	|	2.24
22.500	0.00	0.31	0.664	o	|	|	|	|	2.23
22.583	0.00	0.31	0.662	o	|	|	|	|	2.22
22.667	0.00	0.30	0.660	o	|	|	|	|	2.22
22.750	0.00	0.30	0.657	o	|	|	|	|	2.21
22.833	0.00	0.30	0.655	o	|	|	|	|	2.21
22.917	0.00	0.29	0.653	o	|	|	|	|	2.20

23.000	0.00	0.29	0.651	o	|	|	|	2.19
23.083	0.00	0.29	0.649	o	|	|	|	2.19
23.167	0.00	0.29	0.647	o	|	|	|	2.18
23.250	0.00	0.28	0.645	o	|	|	|	2.18
23.333	0.00	0.28	0.643	o	|	|	|	2.17
23.417	0.00	0.28	0.642	o	|	|	|	2.17
23.500	0.00	0.27	0.640	o	|	|	|	2.16
23.583	0.00	0.27	0.638	o	|	|	|	2.16
23.667	0.00	0.27	0.636	o	|	|	|	2.15
23.750	0.00	0.27	0.634	o	|	|	|	2.14
23.833	0.00	0.26	0.632	o	|	|	|	2.14
23.917	0.00	0.26	0.630	o	|	|	|	2.13
24.000	0.00	0.26	0.629	o	|	|	|	2.13
24.083	0.00	0.26	0.627	o	|	|	|	2.12
24.167	0.00	0.25	0.625	o	|	|	|	2.12
24.250	0.00	0.25	0.623	o	|	|	|	2.11
24.333	0.00	0.25	0.622	o	|	|	|	2.11
24.417	0.00	0.25	0.620	o	|	|	|	2.10
24.500	0.00	0.24	0.618	o	|	|	|	2.10
24.583	0.00	0.24	0.617	o	|	|	|	2.09
24.667	0.00	0.24	0.615	o	|	|	|	2.09
24.750	0.00	0.24	0.613	o	|	|	|	2.08
24.833	0.00	0.23	0.612	o	|	|	|	2.08
24.917	0.00	0.23	0.610	o	|	|	|	2.08
25.000	0.00	0.23	0.609	o	|	|	|	2.07
25.083	0.00	0.23	0.607	o	|	|	|	2.07
25.167	0.00	0.22	0.605	o	|	|	|	2.06
25.250	0.00	0.22	0.604	o	|	|	|	2.06
25.333	0.00	0.22	0.602	o	|	|	|	2.05
25.417	0.00	0.22	0.601	o	|	|	|	2.05
25.500	0.00	0.22	0.599	o	|	|	|	2.04
25.583	0.00	0.21	0.598	o	|	|	|	2.04
25.667	0.00	0.21	0.596	o	|	|	|	2.04
25.750	0.00	0.21	0.595	o	|	|	|	2.03
25.833	0.00	0.21	0.594	o	|	|	|	2.03
25.917	0.00	0.20	0.592	o	|	|	|	2.02
26.000	0.00	0.20	0.591	o	|	|	|	2.02
26.083	0.00	0.20	0.589	o	|	|	|	2.02
26.167	0.00	0.20	0.588	o	|	|	|	2.01
26.250	0.00	0.20	0.587	o	|	|	|	2.01
26.333	0.00	0.19	0.585	o	|	|	|	2.00
26.417	0.00	0.19	0.584	o	|	|	|	2.00
26.500	0.00	0.19	0.583	o	|	|	|	2.00
26.583	0.00	0.19	0.581	o	|	|	|	1.99
26.667	0.00	0.19	0.580	o	|	|	|	1.99
26.750	0.00	0.19	0.579	o	|	|	|	1.98
26.833	0.00	0.19	0.577	o	|	|	|	1.98
26.917	0.00	0.19	0.576	o	|	|	|	1.97
27.000	0.00	0.19	0.575	o	|	|	|	1.97
27.083	0.00	0.19	0.573	o	|	|	|	1.97
27.167	0.00	0.19	0.572	o	|	|	|	1.96
27.250	0.00	0.19	0.571	o	|	|	|	1.96
27.333	0.00	0.19	0.569	o	|	|	|	1.95
27.417	0.00	0.19	0.568	o	|	|	|	1.95
27.500	0.00	0.19	0.567	o	|	|	|	1.94
27.583	0.00	0.19	0.565	o	|	|	|	1.94
27.667	0.00	0.19	0.564	o	|	|	|	1.94
27.750	0.00	0.19	0.563	o	|	|	|	1.93
27.833	0.00	0.19	0.562	o	|	|	|	1.93
27.917	0.00	0.19	0.560	o	|	|	|	1.92
28.000	0.00	0.19	0.559	o	|	|	|	1.92
28.083	0.00	0.19	0.558	o	|	|	|	1.91
28.167	0.00	0.19	0.556	o	|	|	|	1.91
28.250	0.00	0.19	0.555	o	|	|	|	1.91
28.333	0.00	0.19	0.554	o	|	|	|	1.90
28.417	0.00	0.19	0.553	o	|	|	|	1.90
28.500	0.00	0.19	0.551	o	|	|	|	1.89
28.583	0.00	0.19	0.550	o	|	|	|	1.89
28.667	0.00	0.19	0.549	o	|	|	|	1.89
28.750	0.00	0.19	0.547	o	|	|	|	1.88
28.833	0.00	0.19	0.546	o	|	|	|	1.88
28.917	0.00	0.19	0.545	o	|	|	|	1.87
29.000	0.00	0.19	0.544	o	|	|	|	1.87
29.083	0.00	0.18	0.542	o	|	|	|	1.86
29.167	0.00	0.18	0.541	o	|	|	|	1.86
29.250	0.00	0.18	0.540	o	|	|	|	1.86
29.333	0.00	0.18	0.538	o	|	|	|	1.85
29.417	0.00	0.18	0.537	o	|	|	|	1.85
29.500	0.00	0.18	0.536	o	|	|	|	1.84
29.583	0.00	0.18	0.535	o	|	|	|	1.84
29.667	0.00	0.18	0.533	o	|	|	|	1.84
29.750	0.00	0.18	0.532	o	|	|	|	1.83
29.833	0.00	0.18	0.531	o	|	|	|	1.83
29.917	0.00	0.18	0.530	o	|	|	|	1.82
30.000	0.00	0.18	0.528	o	|	|	|	1.82
30.083	0.00	0.18	0.527	o	|	|	|	1.82

30.167	0.00	0.18	0.526	o	|	|	|	|	1.81
30.250	0.00	0.18	0.525	o	|	|	|	|	1.81
30.333	0.00	0.18	0.523	o	|	|	|	|	1.80
30.417	0.00	0.18	0.522	o	|	|	|	|	1.80
30.500	0.00	0.18	0.521	o	|	|	|	|	1.80
30.583	0.00	0.18	0.520	o	|	|	|	|	1.79
30.667	0.00	0.18	0.518	o	|	|	|	|	1.79
30.750	0.00	0.18	0.517	o	|	|	|	|	1.78
30.833	0.00	0.18	0.516	o	|	|	|	|	1.78
30.917	0.00	0.18	0.515	o	|	|	|	|	1.77
31.000	0.00	0.18	0.513	o	|	|	|	|	1.77
31.083	0.00	0.18	0.512	o	|	|	|	|	1.77
31.167	0.00	0.18	0.511	o	|	|	|	|	1.76
31.250	0.00	0.18	0.510	o	|	|	|	|	1.76
31.333	0.00	0.18	0.509	o	|	|	|	|	1.75
31.417	0.00	0.18	0.507	o	|	|	|	|	1.75
31.500	0.00	0.18	0.506	o	|	|	|	|	1.75
31.583	0.00	0.18	0.505	o	|	|	|	|	1.74
31.667	0.00	0.18	0.504	o	|	|	|	|	1.74
31.750	0.00	0.18	0.502	o	|	|	|	|	1.74
31.833	0.00	0.18	0.501	o	|	|	|	|	1.73
31.917	0.00	0.18	0.500	o	|	|	|	|	1.73
32.000	0.00	0.18	0.499	o	|	|	|	|	1.72
32.083	0.00	0.18	0.498	o	|	|	|	|	1.72
32.167	0.00	0.18	0.496	o	|	|	|	|	1.72
32.250	0.00	0.18	0.495	o	|	|	|	|	1.71
32.333	0.00	0.18	0.494	o	|	|	|	|	1.71
32.417	0.00	0.18	0.493	o	|	|	|	|	1.70
32.500	0.00	0.17	0.491	o	|	|	|	|	1.70
32.583	0.00	0.17	0.490	o	|	|	|	|	1.70
32.667	0.00	0.17	0.489	o	|	|	|	|	1.69
32.750	0.00	0.17	0.488	o	|	|	|	|	1.69
32.833	0.00	0.17	0.487	o	|	|	|	|	1.68
32.917	0.00	0.17	0.485	o	|	|	|	|	1.68
33.000	0.00	0.17	0.484	o	|	|	|	|	1.68
33.083	0.00	0.17	0.483	o	|	|	|	|	1.67
33.167	0.00	0.17	0.482	o	|	|	|	|	1.67
33.250	0.00	0.17	0.481	o	|	|	|	|	1.66
33.333	0.00	0.17	0.480	o	|	|	|	|	1.66
33.417	0.00	0.17	0.478	o	|	|	|	|	1.66
33.500	0.00	0.17	0.477	o	|	|	|	|	1.65
33.583	0.00	0.17	0.476	o	|	|	|	|	1.65
33.667	0.00	0.17	0.475	o	|	|	|	|	1.65
33.750	0.00	0.17	0.474	o	|	|	|	|	1.64
33.833	0.00	0.17	0.472	o	|	|	|	|	1.64
33.917	0.00	0.17	0.471	o	|	|	|	|	1.63
34.000	0.00	0.17	0.470	o	|	|	|	|	1.63
34.083	0.00	0.17	0.469	o	|	|	|	|	1.63
34.167	0.00	0.17	0.468	o	|	|	|	|	1.62
34.250	0.00	0.17	0.467	o	|	|	|	|	1.62
34.333	0.00	0.17	0.465	o	|	|	|	|	1.61
34.417	0.00	0.17	0.464	o	|	|	|	|	1.61
34.500	0.00	0.17	0.463	o	|	|	|	|	1.61
34.583	0.00	0.17	0.462	o	|	|	|	|	1.60
34.667	0.00	0.17	0.461	o	|	|	|	|	1.60
34.750	0.00	0.17	0.460	o	|	|	|	|	1.60
34.833	0.00	0.17	0.458	o	|	|	|	|	1.59
34.917	0.00	0.17	0.457	o	|	|	|	|	1.59
35.000	0.00	0.17	0.456	o	|	|	|	|	1.58
35.083	0.00	0.17	0.455	o	|	|	|	|	1.58
35.167	0.00	0.17	0.454	o	|	|	|	|	1.58
35.250	0.00	0.17	0.453	o	|	|	|	|	1.57
35.333	0.00	0.17	0.451	o	|	|	|	|	1.57
35.417	0.00	0.17	0.450	o	|	|	|	|	1.57
35.500	0.00	0.17	0.449	o	|	|	|	|	1.56
35.583	0.00	0.17	0.448	o	|	|	|	|	1.56
35.667	0.00	0.17	0.447	o	|	|	|	|	1.55
35.750	0.00	0.17	0.446	o	|	|	|	|	1.55
35.833	0.00	0.17	0.445	o	|	|	|	|	1.55
35.917	0.00	0.17	0.443	o	|	|	|	|	1.54
36.000	0.00	0.17	0.442	o	|	|	|	|	1.54
36.083	0.00	0.17	0.441	o	|	|	|	|	1.54
36.167	0.00	0.16	0.440	o	|	|	|	|	1.53
36.250	0.00	0.16	0.439	o	|	|	|	|	1.53
36.333	0.00	0.16	0.438	o	|	|	|	|	1.53
36.417	0.00	0.16	0.437	o	|	|	|	|	1.52
36.500	0.00	0.16	0.435	o	|	|	|	|	1.52
36.583	0.00	0.16	0.434	o	|	|	|	|	1.51
36.667	0.00	0.16	0.433	o	|	|	|	|	1.51
36.750	0.00	0.16	0.432	o	|	|	|	|	1.51
36.833	0.00	0.16	0.431	o	|	|	|	|	1.50
36.917	0.00	0.16	0.430	o	|	|	|	|	1.50
37.000	0.00	0.16	0.429	o	|	|	|	|	1.50
37.083	0.00	0.16	0.428	o	|	|	|	|	1.49
37.167	0.00	0.16	0.426	o	|	|	|	|	1.49
37.250	0.00	0.16	0.425	o	|	|	|	|	1.48

37.333	0.00	0.16	0.424	o	|	|	|	|	1.48
37.417	0.00	0.16	0.423	o	|	|	|	|	1.48
37.500	0.00	0.16	0.422	o	|	|	|	|	1.47
37.583	0.00	0.16	0.421	o	|	|	|	|	1.47
37.667	0.00	0.16	0.420	o	|	|	|	|	1.47
37.750	0.00	0.16	0.419	o	|	|	|	|	1.46
37.833	0.00	0.16	0.418	o	|	|	|	|	1.46
37.917	0.00	0.16	0.416	o	|	|	|	|	1.46
38.000	0.00	0.16	0.415	o	|	|	|	|	1.45
38.083	0.00	0.16	0.414	o	|	|	|	|	1.45
38.167	0.00	0.16	0.413	o	|	|	|	|	1.45
38.250	0.00	0.16	0.412	o	|	|	|	|	1.44
38.333	0.00	0.16	0.411	o	|	|	|	|	1.44
38.417	0.00	0.16	0.410	o	|	|	|	|	1.43
38.500	0.00	0.16	0.409	o	|	|	|	|	1.43
38.583	0.00	0.16	0.408	o	|	|	|	|	1.43
38.667	0.00	0.16	0.407	o	|	|	|	|	1.42
38.750	0.00	0.16	0.405	o	|	|	|	|	1.42
38.833	0.00	0.16	0.404	o	|	|	|	|	1.42
38.917	0.00	0.16	0.403	o	|	|	|	|	1.41
39.000	0.00	0.16	0.402	o	|	|	|	|	1.41
39.083	0.00	0.16	0.401	o	|	|	|	|	1.41
39.167	0.00	0.16	0.400	o	|	|	|	|	1.40
39.250	0.00	0.16	0.399	o	|	|	|	|	1.40
39.333	0.00	0.16	0.398	o	|	|	|	|	1.40
39.417	0.00	0.16	0.397	o	|	|	|	|	1.39
39.500	0.00	0.16	0.396	o	|	|	|	|	1.39
39.583	0.00	0.16	0.395	o	|	|	|	|	1.39
39.667	0.00	0.16	0.394	o	|	|	|	|	1.38
39.750	0.00	0.16	0.393	o	|	|	|	|	1.38
39.833	0.00	0.16	0.391	o	|	|	|	|	1.37
39.917	0.00	0.16	0.390	o	|	|	|	|	1.37
40.000	0.00	0.16	0.389	o	|	|	|	|	1.37
40.083	0.00	0.15	0.388	o	|	|	|	|	1.36
40.167	0.00	0.15	0.387	o	|	|	|	|	1.36
40.250	0.00	0.15	0.386	o	|	|	|	|	1.36
40.333	0.00	0.15	0.385	o	|	|	|	|	1.35
40.417	0.00	0.15	0.384	o	|	|	|	|	1.35
40.500	0.00	0.15	0.383	o	|	|	|	|	1.35
40.583	0.00	0.15	0.382	o	|	|	|	|	1.34
40.667	0.00	0.15	0.381	o	|	|	|	|	1.34
40.750	0.00	0.15	0.380	o	|	|	|	|	1.34
40.833	0.00	0.15	0.379	o	|	|	|	|	1.33
40.917	0.00	0.15	0.378	o	|	|	|	|	1.33
41.000	0.00	0.15	0.377	o	|	|	|	|	1.33
41.083	0.00	0.15	0.376	o	|	|	|	|	1.32
41.167	0.00	0.15	0.375	o	|	|	|	|	1.32
41.250	0.00	0.15	0.373	o	|	|	|	|	1.32
41.333	0.00	0.15	0.372	o	|	|	|	|	1.31
41.417	0.00	0.15	0.371	o	|	|	|	|	1.31
41.500	0.00	0.15	0.370	o	|	|	|	|	1.31
41.583	0.00	0.15	0.369	o	|	|	|	|	1.30
41.667	0.00	0.15	0.368	o	|	|	|	|	1.30
41.750	0.00	0.15	0.367	o	|	|	|	|	1.30
41.833	0.00	0.15	0.366	o	|	|	|	|	1.29
41.917	0.00	0.15	0.365	o	|	|	|	|	1.29
42.000	0.00	0.15	0.364	o	|	|	|	|	1.29
42.083	0.00	0.15	0.363	o	|	|	|	|	1.28
42.167	0.00	0.15	0.362	o	|	|	|	|	1.28
42.250	0.00	0.15	0.361	o	|	|	|	|	1.28
42.333	0.00	0.15	0.360	o	|	|	|	|	1.27
42.417	0.00	0.15	0.359	o	|	|	|	|	1.27
42.500	0.00	0.15	0.358	o	|	|	|	|	1.27
42.583	0.00	0.15	0.357	o	|	|	|	|	1.26
42.667	0.00	0.15	0.356	o	|	|	|	|	1.26
42.750	0.00	0.15	0.355	o	|	|	|	|	1.26
42.833	0.00	0.15	0.354	o	|	|	|	|	1.25
42.917	0.00	0.15	0.353	o	|	|	|	|	1.25
43.000	0.00	0.15	0.352	o	|	|	|	|	1.25
43.083	0.00	0.15	0.351	o	|	|	|	|	1.24
43.167	0.00	0.15	0.350	o	|	|	|	|	1.24
43.250	0.00	0.15	0.349	o	|	|	|	|	1.24
43.333	0.00	0.15	0.348	o	|	|	|	|	1.23
43.417	0.00	0.15	0.347	o	|	|	|	|	1.23
43.500	0.00	0.15	0.346	o	|	|	|	|	1.23
43.583	0.00	0.15	0.345	o	|	|	|	|	1.22
43.667	0.00	0.15	0.344	o	|	|	|	|	1.22
43.750	0.00	0.15	0.343	o	|	|	|	|	1.22
43.833	0.00	0.15	0.342	o	|	|	|	|	1.21
43.917	0.00	0.15	0.341	o	|	|	|	|	1.21
44.000	0.00	0.15	0.340	o	|	|	|	|	1.21
44.083	0.00	0.15	0.339	o	|	|	|	|	1.20
44.167	0.00	0.15	0.338	o	|	|	|	|	1.20
44.250	0.00	0.14	0.337	o	|	|	|	|	1.20
44.333	0.00	0.14	0.336	o	|	|	|	|	1.19
44.417	0.00	0.14	0.335	o	|	|	|	|	1.19

44.500	0.00	0.14	0.334	o	|	|	|	|	1.19
44.583	0.00	0.14	0.333	o	|	|	|	|	1.18
44.667	0.00	0.14	0.332	o	|	|	|	|	1.18
44.750	0.00	0.14	0.331	o	|	|	|	|	1.18
44.833	0.00	0.14	0.330	o	|	|	|	|	1.17
44.917	0.00	0.14	0.329	o	|	|	|	|	1.17
45.000	0.00	0.14	0.328	o	|	|	|	|	1.17
45.083	0.00	0.14	0.327	o	|	|	|	|	1.16
45.167	0.00	0.14	0.326	o	|	|	|	|	1.16
45.250	0.00	0.14	0.325	o	|	|	|	|	1.16
45.333	0.00	0.14	0.324	o	|	|	|	|	1.16
45.417	0.00	0.14	0.323	o	|	|	|	|	1.15
45.500	0.00	0.14	0.322	o	|	|	|	|	1.15
45.583	0.00	0.14	0.321	o	|	|	|	|	1.15
45.667	0.00	0.14	0.320	o	|	|	|	|	1.14
45.750	0.00	0.14	0.319	o	|	|	|	|	1.14
45.833	0.00	0.14	0.318	o	|	|	|	|	1.14
45.917	0.00	0.14	0.317	o	|	|	|	|	1.13
46.000	0.00	0.14	0.316	o	|	|	|	|	1.13
46.083	0.00	0.14	0.315	o	|	|	|	|	1.13
46.167	0.00	0.14	0.314	o	|	|	|	|	1.12
46.250	0.00	0.14	0.313	o	|	|	|	|	1.12
46.333	0.00	0.14	0.312	o	|	|	|	|	1.12
46.417	0.00	0.14	0.311	o	|	|	|	|	1.11
46.500	0.00	0.14	0.310	o	|	|	|	|	1.11
46.583	0.00	0.14	0.309	o	|	|	|	|	1.11
46.667	0.00	0.14	0.308	o	|	|	|	|	1.10
46.750	0.00	0.14	0.307	o	|	|	|	|	1.10
46.833	0.00	0.14	0.306	o	|	|	|	|	1.10
46.917	0.00	0.14	0.305	o	|	|	|	|	1.10
47.000	0.00	0.14	0.304	o	|	|	|	|	1.09
47.083	0.00	0.14	0.304	o	|	|	|	|	1.09
47.167	0.00	0.14	0.303	o	|	|	|	|	1.09
47.250	0.00	0.14	0.302	o	|	|	|	|	1.08
47.333	0.00	0.14	0.301	o	|	|	|	|	1.08
47.417	0.00	0.14	0.300	o	|	|	|	|	1.08
47.500	0.00	0.14	0.299	o	|	|	|	|	1.07
47.583	0.00	0.14	0.298	o	|	|	|	|	1.07
47.667	0.00	0.14	0.297	o	|	|	|	|	1.07
47.750	0.00	0.14	0.296	o	|	|	|	|	1.06
47.833	0.00	0.14	0.295	o	|	|	|	|	1.06
47.917	0.00	0.14	0.294	o	|	|	|	|	1.06
48.000	0.00	0.14	0.293	o	|	|	|	|	1.06
48.083	0.00	0.14	0.292	o	|	|	|	|	1.05
48.167	0.00	0.14	0.291	o	|	|	|	|	1.05
48.250	0.00	0.14	0.290	o	|	|	|	|	1.05
48.333	0.00	0.14	0.289	o	|	|	|	|	1.04
48.417	0.00	0.14	0.288	o	|	|	|	|	1.04
48.500	0.00	0.14	0.288	o	|	|	|	|	1.04
48.583	0.00	0.14	0.287	o	|	|	|	|	1.03
48.667	0.00	0.13	0.286	o	|	|	|	|	1.03
48.750	0.00	0.13	0.285	o	|	|	|	|	1.03
48.833	0.00	0.13	0.284	o	|	|	|	|	1.03
48.917	0.00	0.13	0.283	o	|	|	|	|	1.02
49.000	0.00	0.13	0.282	o	|	|	|	|	1.02
49.083	0.00	0.13	0.281	o	|	|	|	|	1.02
49.167	0.00	0.13	0.280	o	|	|	|	|	1.01
49.250	0.00	0.13	0.279	o	|	|	|	|	1.01
49.333	0.00	0.13	0.278	o	|	|	|	|	1.01
49.417	0.00	0.13	0.277	o	|	|	|	|	1.00
49.500	0.00	0.13	0.276	o	|	|	|	|	1.00
49.583	0.00	0.13	0.275	o	|	|	|	|	1.00
49.667	0.00	0.13	0.275	o	|	|	|	|	0.99
49.750	0.00	0.13	0.274	o	|	|	|	|	0.99
49.833	0.00	0.13	0.273	o	|	|	|	|	0.99
49.917	0.00	0.13	0.272	o	|	|	|	|	0.99
50.000	0.00	0.13	0.271	o	|	|	|	|	0.98
50.083	0.00	0.13	0.270	o	|	|	|	|	0.98
50.167	0.00	0.13	0.269	o	|	|	|	|	0.98
50.250	0.00	0.13	0.268	o	|	|	|	|	0.97
50.333	0.00	0.13	0.267	o	|	|	|	|	0.97
50.417	0.00	0.13	0.267	o	|	|	|	|	0.97
50.500	0.00	0.13	0.266	o	|	|	|	|	0.96
50.583	0.00	0.13	0.265	o	|	|	|	|	0.96
50.667	0.00	0.13	0.264	o	|	|	|	|	0.96
50.750	0.00	0.13	0.263	o	|	|	|	|	0.95
50.833	0.00	0.13	0.262	o	|	|	|	|	0.95
50.917	0.00	0.13	0.261	o	|	|	|	|	0.95
51.000	0.00	0.13	0.260	o	|	|	|	|	0.94
51.083	0.00	0.13	0.260	o	|	|	|	|	0.94
51.167	0.00	0.12	0.259	o	|	|	|	|	0.94
51.250	0.00	0.12	0.258	o	|	|	|	|	0.93
51.333	0.00	0.12	0.257	o	|	|	|	|	0.93
51.417	0.00	0.12	0.256	o	|	|	|	|	0.93
51.500	0.00	0.12	0.255	o	|	|	|	|	0.92
51.583	0.00	0.12	0.254	o	|	|	|	|	0.92

51.667	0.00	0.12	0.254	o	|	|	|	| 0.92
51.750	0.00	0.12	0.253	o	|	|	|	| 0.92
51.833	0.00	0.12	0.252	o	|	|	|	| 0.91
51.917	0.00	0.12	0.251	o	|	|	|	| 0.91
52.000	0.00	0.12	0.250	o	|	|	|	| 0.91
52.083	0.00	0.12	0.249	o	|	|	|	| 0.90
52.167	0.00	0.12	0.249	o	|	|	|	| 0.90
52.250	0.00	0.12	0.248	o	|	|	|	| 0.90
52.333	0.00	0.12	0.247	o	|	|	|	| 0.89
52.417	0.00	0.12	0.246	o	|	|	|	| 0.89
52.500	0.00	0.12	0.245	o	|	|	|	| 0.89
52.583	0.00	0.12	0.244	o	|	|	|	| 0.89
52.667	0.00	0.12	0.244	o	|	|	|	| 0.88
52.750	0.00	0.12	0.243	o	|	|	|	| 0.88
52.833	0.00	0.12	0.242	o	|	|	|	| 0.88
52.917	0.00	0.12	0.241	o	|	|	|	| 0.87
53.000	0.00	0.12	0.240	o	|	|	|	| 0.87
53.083	0.00	0.12	0.240	o	|	|	|	| 0.87
53.167	0.00	0.12	0.239	o	|	|	|	| 0.87
53.250	0.00	0.11	0.238	o	|	|	|	| 0.86
53.333	0.00	0.11	0.237	o	|	|	|	| 0.86
53.417	0.00	0.11	0.236	o	|	|	|	| 0.86
53.500	0.00	0.11	0.236	o	|	|	|	| 0.85
53.583	0.00	0.11	0.235	o	|	|	|	| 0.85
53.667	0.00	0.11	0.234	o	|	|	|	| 0.85
53.750	0.00	0.11	0.233	o	|	|	|	| 0.85
53.833	0.00	0.11	0.233	o	|	|	|	| 0.84
53.917	0.00	0.11	0.232	o	|	|	|	| 0.84
54.000	0.00	0.11	0.231	o	|	|	|	| 0.84
54.083	0.00	0.11	0.230	o	|	|	|	| 0.83
54.167	0.00	0.11	0.230	o	|	|	|	| 0.83
54.250	0.00	0.11	0.229	o	|	|	|	| 0.83
54.333	0.00	0.11	0.228	o	|	|	|	| 0.83
54.417	0.00	0.11	0.227	o	|	|	|	| 0.82
54.500	0.00	0.11	0.227	o	|	|	|	| 0.82
54.583	0.00	0.11	0.226	o	|	|	|	| 0.82
54.667	0.00	0.11	0.225	o	|	|	|	| 0.82
54.750	0.00	0.11	0.224	o	|	|	|	| 0.81
54.833	0.00	0.11	0.224	o	|	|	|	| 0.81
54.917	0.00	0.11	0.223	o	|	|	|	| 0.81
55.000	0.00	0.11	0.222	o	|	|	|	| 0.80
55.083	0.00	0.11	0.221	o	|	|	|	| 0.80
55.167	0.00	0.11	0.221	o	|	|	|	| 0.80
55.250	0.00	0.11	0.220	o	|	|	|	| 0.80
55.333	0.00	0.11	0.219	o	|	|	|	| 0.79
55.417	0.00	0.11	0.218	o	|	|	|	| 0.79
55.500	0.00	0.10	0.218	o	|	|	|	| 0.79
55.583	0.00	0.10	0.217	o	|	|	|	| 0.79
55.667	0.00	0.10	0.216	o	|	|	|	| 0.78
55.750	0.00	0.10	0.216	o	|	|	|	| 0.78
55.833	0.00	0.10	0.215	o	|	|	|	| 0.78
55.917	0.00	0.10	0.214	o	|	|	|	| 0.78
56.000	0.00	0.10	0.213	o	|	|	|	| 0.77
56.083	0.00	0.10	0.213	o	|	|	|	| 0.77
56.167	0.00	0.10	0.212	o	|	|	|	| 0.77
56.250	0.00	0.10	0.211	o	|	|	|	| 0.77
56.333	0.00	0.10	0.211	o	|	|	|	| 0.76
56.417	0.00	0.10	0.210	o	|	|	|	| 0.76
56.500	0.00	0.10	0.209	o	|	|	|	| 0.76
56.583	0.00	0.10	0.208	o	|	|	|	| 0.76
56.667	0.00	0.10	0.208	o	|	|	|	| 0.75
56.750	0.00	0.10	0.207	o	|	|	|	| 0.75

Remaining water in basin = 0.21 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 681
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 43.291 (CFS)
Total volume = 4.546 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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                    FLOOD HYDROGRAPH ROUTING PROGRAM
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                            Study date: 05/07/25

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 Program License Serial Number 5006

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 ********************** HYDROGRAPH INFORMATION **********************

                 From study/file name: PRO10024100.rte
 ****************************HYDROGRAPH DATA*****************************
                 Number of intervals =   292
                 Time interval =    5.0 (Min.)
                 Maximum/Peak flow rate =       14.437 (CFS)
                 Total volume =       6.745 (Ac.Ft)
        Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
        Peak (CFS)       0.000     0.000     0.000     0.000     0.000
        Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
 *************************************************************************



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 Process from Point/Station        1.000 to Point/Station        2.000
 **** RETARDING BASIN ROUTING ****
 _________________________________________________________________________

 User entry of depth-outflow-storage data
 ---------------------------------------------------------------------
 Total number of inflow hydrograph intervals = 292
 Hydrograph time unit =  5.000 (Min.)
 Initial depth in storage basin =   0.00(Ft.)
 ---------------------------------------------------------------------
 ---------------------------------------------------------------------
 Initial basin depth =   0.00 (Ft.)
 Initial basin storage =      0.00 (Ac.Ft)
 Initial basin outflow =   0.00 (CFS)
 ---------------------------------------------------------------------
 ---------------------------------------------------------------------
 Depth vs. Storage and Depth vs. Discharge data:
  Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
      (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
 ---------------------------------------------------------------------
    0.000      0.000      0.000      0.000        0.000
    1.000      0.276      0.133      0.276        0.276
    2.000      0.584      0.193      0.583        0.585
    3.000      0.930      0.700      0.928        0.932
    3.500      1.118      0.824      1.115        1.121
    4.000      1.316      0.930      1.313        1.319
    4.500      1.528      1.024      1.524        1.532
    4.750      1.637      1.068      1.633        1.641
    5.000      1.749     18.283      1.686        1.812
    6.000      2.231    253.655      1.358        3.104
 ---------------------------------------------------------------------
                 Hydrograph Detention Basin Routing
 ---------------------------------------------------------------------

 Graph values: 'I'= unit inflow; 'O'=outflow at time shown
 ---------------------------------------------------------------------
  Time   Inflow  Outflow    Storage                                Depth
 (Hours)  (CFS)   (CFS)     (Ac.Ft) .0       3.6    7.22   10.83   14.44 (Ft.)
  0.083    0.23    0.00      0.001  O       |      |      |      |     0.00
  0.167    0.49    0.00      0.003  OI      |      |      |      |     0.01
  0.250    0.54    0.00      0.007  OI      |      |      |      |     0.02
  0.333    0.68    0.01      0.011  OI      |      |      |      |     0.04
  0.417    0.82    0.01      0.016  OI      |      |      |      |     0.06
  0.500    0.84    0.01      0.022  OI      |      |      |      |     0.08
  0.583    0.86    0.01      0.028  OI      |      |      |      |     0.10
  0.667    0.86    0.02      0.033  OI      |      |      |      |     0.12
  0.750    0.86    0.02      0.039  OI      |      |      |      |     0.14
  0.833    0.98    0.02      0.045  O I     |      |      |      |     0.16
  0.917    1.10    0.03      0.052  O I     |      |      |      |     0.19
  1.000    1.13    0.03      0.060  O I     |      |      |      |     0.22
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1.083	1.03	0.03	0.067	o I	|	|	|	0.24
1.167	0.90	0.04	0.073	o I	|	|	|	0.27
1.250	0.88	0.04	0.079	oI	|	|	|	0.29
1.333	0.86	0.04	0.085	oI	|	|	|	0.31
1.417	0.86	0.04	0.091	oI	|	|	|	0.33
1.500	0.86	0.05	0.096	oI	|	|	|	0.35
1.583	0.86	0.05	0.102	oI	|	|	|	0.37
1.667	0.86	0.05	0.107	oI	|	|	|	0.39
1.750	0.86	0.05	0.113	oI	|	|	|	0.41
1.833	0.98	0.06	0.119	o I	|	|	|	0.43
1.917	1.10	0.06	0.126	o I	|	|	|	0.46
2.000	1.13	0.06	0.133	o I	|	|	|	0.48
2.083	1.14	0.07	0.140	o I	|	|	|	0.51
2.167	1.15	0.07	0.148	o I	|	|	|	0.54
2.250	1.15	0.07	0.155	o I	|	|	|	0.56
2.333	1.15	0.08	0.163	o I	|	|	|	0.59
2.417	1.15	0.08	0.170	o I	|	|	|	0.62
2.500	1.15	0.09	0.177	o I	|	|	|	0.64
2.583	1.26	0.09	0.185	o I	|	|	|	0.67
2.667	1.39	0.09	0.193	o I	|	|	|	0.70
2.750	1.42	0.10	0.202	o I	|	|	|	0.73
2.833	1.43	0.10	0.212	o I	|	|	|	0.77
2.917	1.43	0.11	0.221	o I	|	|	|	0.80
3.000	1.43	0.11	0.230	o I	|	|	|	0.83
3.083	1.43	0.12	0.239	o I	|	|	|	0.87
3.167	1.43	0.12	0.248	o I	|	|	|	0.90
3.250	1.43	0.12	0.257	o I	|	|	|	0.93
3.333	1.43	0.13	0.266	o I	|	|	|	0.96
3.417	1.43	0.13	0.275	o I	|	|	|	1.00
3.500	1.43	0.13	0.284	o I	|	|	|	1.03
3.583	1.43	0.14	0.293	o I	|	|	|	1.05
3.667	1.43	0.14	0.302	o I	|	|	|	1.08
3.750	1.43	0.14	0.311	o I	|	|	|	1.11
3.833	1.55	0.14	0.320	o I	|	|	|	1.14
3.917	1.68	0.14	0.330	o I	|	|	|	1.18
4.000	1.70	0.15	0.341	o I	|	|	|	1.21
4.083	1.72	0.15	0.352	o I	|	|	|	1.25
4.167	1.72	0.15	0.362	o I	|	|	|	1.28
4.250	1.72	0.15	0.373	o I	|	|	|	1.32
4.333	1.84	0.15	0.384	o I	|	|	|	1.35
4.417	1.96	0.16	0.396	o I	|	|	|	1.39
4.500	1.99	0.16	0.409	o I	|	|	|	1.43
4.583	2.00	0.16	0.422	o I	|	|	|	1.47
4.667	2.01	0.16	0.434	o I	|	|	|	1.51
4.750	2.01	0.17	0.447	o I	|	|	|	1.55
4.833	2.12	0.17	0.460	o I	|	|	|	1.60
4.917	2.25	0.17	0.474	o I	|	|	|	1.64
5.000	2.28	0.17	0.488	o I	|	|	|	1.69
5.083	2.06	0.18	0.502	o I	|	|	|	1.73
5.167	1.81	0.18	0.514	o I	|	|	|	1.77
5.250	1.75	0.18	0.525	o I	|	|	|	1.81
5.333	1.85	0.18	0.536	o I	|	|	|	1.84
5.417	1.96	0.19	0.548	o I	|	|	|	1.88
5.500	1.99	0.19	0.560	o I	|	|	|	1.92
5.583	2.12	0.19	0.573	o I	|	|	|	1.96
5.667	2.25	0.20	0.587	o I	|	|	|	2.01
5.750	2.28	0.22	0.601	o I	|	|	|	2.05
5.833	2.29	0.24	0.615	o I	|	|	|	2.09
5.917	2.29	0.26	0.629	o I	|	|	|	2.13
6.000	2.29	0.28	0.643	o I	|	|	|	2.17
6.083	2.41	0.30	0.657	o I	|	|	|	2.21
6.167	2.54	0.32	0.672	o I	|	|	|	2.26
6.250	2.56	0.34	0.688	o I	|	|	|	2.30
6.333	2.58	0.37	0.703	o I	|	|	|	2.34
6.417	2.58	0.39	0.718	o I	|	|	|	2.39
6.500	2.58	0.41	0.733	o I	|	|	|	2.43
6.583	2.70	0.43	0.748	o I	|	|	|	2.47
6.667	2.82	0.46	0.764	|o I	|	|	|	2.52
6.750	2.85	0.48	0.781	|o I	|	|	|	2.57
6.833	2.86	0.50	0.797	|o I	|	|	|	2.61
6.917	2.87	0.53	0.813	|o I	|	|	|	2.66
7.000	2.87	0.55	0.829	|o I	|	|	|	2.71
7.083	2.87	0.58	0.845	|o I	|	|	|	2.75
7.167	2.87	0.60	0.861	|o I	|	|	|	2.80
7.250	2.87	0.62	0.876	|o I	|	|	|	2.84
7.333	2.98	0.64	0.892	|o I	|	|	|	2.89
7.417	3.11	0.67	0.908	|o I	|	|	|	2.94
7.500	3.14	0.69	0.925	|o I	|	|	|	2.99
7.583	3.27	0.71	0.942	|o I|	|	|	|	3.03
7.667	3.40	0.72	0.960	|o I|	|	|	|	3.08
7.750	3.42	0.73	0.979	|o I|	|	|	|	3.13

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 7.833    3.55    0.74      0.998  |O     I|       |        |        |      3.18
 7.917    3.68    0.76      1.018  |O      I       |        |        |      3.23
 8.000    3.71    0.77      1.038  |O      I       |        |        |      3.29
 8.083    3.96    0.78      1.059  |O      I       |        |        |      3.34
 8.167    4.21    0.80      1.081  |O      |I      |        |        |      3.40
 8.250    4.27    0.82      1.105  |O      |I      |        |        |      3.47
 8.333    4.29    0.83      1.129  |O      |I      |        |        |      3.53
 8.417    4.30    0.84      1.153  |O      |I      |        |        |      3.59
 8.500    4.30    0.86      1.177  |O      |I      |        |        |      3.65
 8.583    4.42    0.87      1.201  |O      |I      |        |        |      3.71
 8.667    4.54    0.88      1.225  |O      | I     |        |        |      3.77
 8.750    4.57    0.90      1.251  |O      | I     |        |        |      3.84
 8.833    4.70    0.91      1.276  | O     | I     |        |        |      3.90
 8.917    4.83    0.92      1.303  | O     | I     |        |        |      3.97
 9.000    4.86    0.94      1.330  | O     | I     |        |        |      4.03
 9.083    5.10    0.95      1.358  | O     |  I    |        |        |      4.10
 9.167    5.36    0.96      1.387  | O     |  I    |        |        |      4.17
 9.250    5.42    0.98      1.418  | O     |   I   |        |        |      4.24
 9.333    5.55    0.99      1.449  | O     |   I   |        |        |      4.31
 9.417    5.69    1.00      1.480  | O     |   I   |        |        |      4.39
 9.500    5.72    1.02      1.513  | O     |   I   |        |        |      4.46
 9.583    5.85    1.03      1.546  | O     |   I   |        |        |      4.54
 9.667    5.98    1.04      1.579  | O     |    I  |        |        |      4.62
 9.750    6.00    1.06      1.613  | O     |    I  |        |        |      4.70
 9.833    6.15    2.14      1.644  |   O   |    I  |        |        |      4.77
 9.917    6.31    4.97      1.662  |       |  O I  |        |        |      4.81
10.000    6.37    5.92      1.669  |       |   OI  |        |        |      4.82
10.083    5.54    5.94      1.669  |       |   IO  |        |        |      4.82
10.167    4.61    5.34      1.665  |       | IO    |        |        |      4.81
10.250    4.41    4.77      1.661  |       |IO     |        |        |      4.80
10.333    4.33    4.50      1.659  |       |O      |        |        |      4.80
10.417    4.30    4.37      1.658  |       |O      |        |        |      4.80
10.500    4.30    4.32      1.658  |       |O      |        |        |      4.80
10.583    4.88    4.51      1.659  |       |OI     |        |        |      4.80
10.667    5.52    4.99      1.663  |       |  OI   |        |        |      4.81
10.750    5.66    5.40      1.665  |       |  OI   |        |        |      4.81
10.833    5.71    5.60      1.666  |       |   O   |        |        |      4.82
10.917    5.73    5.68      1.667  |       |   O   |        |        |      4.82
11.000    5.73    5.72      1.667  |       |   O   |        |        |      4.82
11.083    5.62    5.69      1.667  |       |   O   |        |        |      4.82
11.167    5.49    5.59      1.666  |       |   O   |        |        |      4.82
11.250    5.46    5.51      1.666  |       |   O   |        |        |      4.81
11.333    5.45    5.47      1.666  |       |   O   |        |        |      4.81
11.417    5.45    5.46      1.666  |       |   O   |        |        |      4.81
11.500    5.45    5.45      1.666  |       |   O   |        |        |      4.81
11.583    5.21    5.37      1.665  |       |  O    |        |        |      4.81
11.667    4.96    5.17      1.664  |       | IO    |        |        |      4.81
11.750    4.90    5.01      1.663  |       | IO    |        |        |      4.81
11.833    5.00    4.97      1.662  |       |  O    |        |        |      4.81
11.917    5.12    5.03      1.663  |       |  O    |        |        |      4.81
12.000    5.14    5.10      1.663  |       |  O    |        |        |      4.81
12.083    6.66    5.65      1.667  |       |   O I |        |        |      4.82
12.167    8.31    6.92      1.675  |       |      O| I      |        |      4.83
12.250    8.68    8.01      1.682  |       |       |O I    |        |      4.85
12.333    9.08    8.61      1.686  |       |       |  OI   |        |      4.86
12.417    9.42    9.05      1.689  |       |       |   O   |        |      4.87
12.500    9.50    9.34      1.691  |       |       |   OI  |        |      4.87
12.583   10.02    9.63      1.693  |       |       |    OI |        |      4.87
12.667   10.56   10.09      1.696  |       |       |     OI|        |      4.88
12.750   10.70   10.46      1.698  |       |       |      O|        |      4.89
12.833   11.00   10.73      1.700  |       |       |      OI        |      4.89
12.917   11.30   11.02      1.702  |       |       |       OI       |      4.89
13.000   11.38   11.24      1.703  |       |       |       OI       |      4.90
13.083   12.60   11.76      1.707  |       |       |        | OI    |      4.91
13.167   13.91   12.79      1.713  |       |       |        |   O I |      4.92
13.250   14.20   13.67      1.719  |       |       |        |     OI|      4.93
13.333   14.34   14.08      1.722  |       |       |        |      O|      4.94
13.417   14.41   14.29      1.723  |       |       |        |      O|      4.94
13.500   14.44   14.38      1.724  |       |       |        |      O|      4.94
13.583   11.89   13.54      1.718  |       |       |        | I   O |      4.93
13.667    9.12   11.44      1.704  |       |       |   I    |O      |      4.90
13.750    8.55    9.64      1.693  |       |       | I  O   |       |      4.87
13.833    8.34    8.81      1.687  |       |       | IO     |       |      4.86
13.917    8.26    8.46      1.685  |       |       | O      |       |      4.86
14.000    8.28    8.33      1.684  |       |       | O      |       |      4.86
14.083    9.24    8.63      1.686  |       |       |  OI    |       |      4.86
14.167   10.29    9.41      1.691  |       |       |   O I  |       |      4.87
14.250   10.53   10.10      1.696  |       |       |     OI|       |      4.88
14.333   10.40   10.35      1.697  |       |       |     OI|       |      4.88
14.417   10.21   10.32      1.697  |       |       |     O |       |      4.88
14.500   10.18   10.24      1.697  |       |       |     O |       |      4.88
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14.583	10.19	10.20	1.696	|	|	| O	|	|	4.88
14.667	10.20	10.19	1.696	|	|	| O	|	|	4.88
14.750	10.22	10.21	1.696	|	|	| O	|	|	4.88
14.833	10.01	10.15	1.696	|	|	| O	|	|	4.88
14.917	9.78	9.98	1.695	|	|	| IO	|	|	4.88
15.000	9.75	9.83	1.694	|	|	| O	|	|	4.88
15.083	9.52	9.70	1.693	|	|	| O	|	|	4.88
15.167	9.28	9.49	1.692	|	|	| IO	|	|	4.87
15.250	9.25	9.34	1.691	|	|	| O	|	|	4.87
15.333	9.02	9.20	1.690	|	|	| IO	|	|	4.87
15.417	8.78	8.99	1.689	|	|	| O	|	|	4.87
15.500	8.75	8.83	1.688	|	|	| O	|	|	4.86
15.583	7.81	8.45	1.685	|	|	IO	|	|	4.86
15.667	6.81	7.66	1.680	|	| IO	|	|	|	4.85
15.750	6.62	7.00	1.676	|	| IO	|	|	|	4.84
15.833	6.55	6.71	1.674	|	| O	|	|	|	4.83
15.917	6.54	6.60	1.673	|	| O	|	|	|	4.83
16.000	6.56	6.56	1.673	|	| O	|	|	|	4.83
16.083	4.36	5.80	1.668	|	I O	|	|	|	4.82
16.167	1.95	3.97	1.656	| I O	|	|	|	|	4.79
16.250	1.44	2.40	1.646	| I O	|	|	|	|	4.77
16.333	1.24	1.66	1.641	| IO	|	|	|	|	4.76
16.417	1.15	1.34	1.639	| O	|	|	|	|	4.75
16.500	1.15	1.21	1.638	| O	|	|	|	|	4.75
16.583	1.03	1.12	1.637	| O	|	|	|	|	4.75
16.667	0.90	1.07	1.636	| O	|	|	|	|	4.75
16.750	0.88	1.07	1.635	|IO	|	|	|	|	4.75
16.833	0.86	1.07	1.634	|IO	|	|	|	|	4.74
16.917	0.86	1.07	1.632	|IO	|	|	|	|	4.74
17.000	0.86	1.07	1.631	|IO	|	|	|	|	4.74
17.083	1.09	1.07	1.630	| O	|	|	|	|	4.73
17.167	1.35	1.07	1.632	| O	|	|	|	|	4.74
17.250	1.40	1.07	1.634	| OI	|	|	|	|	4.74
17.333	1.42	1.07	1.636	| OI	|	|	|	|	4.75
17.417	1.43	1.22	1.638	| OI	|	|	|	|	4.75
17.500	1.43	1.37	1.639	| O	|	|	|	|	4.75
17.583	1.43	1.41	1.639	| O	|	|	|	|	4.76
17.667	1.43	1.43	1.639	| O	|	|	|	|	4.76
17.750	1.43	1.43	1.639	| O	|	|	|	|	4.76
17.833	1.32	1.39	1.639	| IO	|	|	|	|	4.75
17.917	1.19	1.30	1.638	| O	|	|	|	|	4.75
18.000	1.16	1.21	1.638	| O	|	|	|	|	4.75
18.083	1.15	1.17	1.638	| O	|	|	|	|	4.75
18.167	1.15	1.16	1.638	| O	|	|	|	|	4.75
18.250	1.15	1.15	1.638	| O	|	|	|	|	4.75
18.333	1.15	1.15	1.638	| O	|	|	|	|	4.75
18.417	1.15	1.15	1.638	| O	|	|	|	|	4.75
18.500	1.15	1.15	1.638	| O	|	|	|	|	4.75
18.583	1.03	1.11	1.637	| O	|	|	|	|	4.75
18.667	0.90	1.07	1.636	| O	|	|	|	|	4.75
18.750	0.88	1.07	1.635	|IO	|	|	|	|	4.75
18.833	0.75	1.07	1.633	|IO	|	|	|	|	4.74
18.917	0.62	1.07	1.631	|IO	|	|	|	|	4.74
19.000	0.59	1.06	1.628	|IO	|	|	|	|	4.73
19.083	0.69	1.06	1.625	|IO	|	|	|	|	4.72
19.167	0.82	1.06	1.623	|IO	|	|	|	|	4.72
19.250	0.84	1.06	1.621	|IO	|	|	|	|	4.71
19.333	0.97	1.06	1.620	| O	|	|	|	|	4.71
19.417	1.10	1.06	1.620	| O	|	|	|	|	4.71
19.500	1.13	1.06	1.620	| O	|	|	|	|	4.71
19.583	1.03	1.06	1.620	| O	|	|	|	|	4.71
19.667	0.90	1.06	1.620	| O	|	|	|	|	4.71
19.750	0.88	1.06	1.618	|IO	|	|	|	|	4.71
19.833	0.75	1.06	1.617	|IO	|	|	|	|	4.70
19.917	0.62	1.06	1.614	|IO	|	|	|	|	4.70
20.000	0.59	1.06	1.611	|IO	|	|	|	|	4.69
20.083	0.69	1.06	1.608	|IO	|	|	|	|	4.68
20.167	0.82	1.06	1.606	|IO	|	|	|	|	4.68
20.250	0.84	1.05	1.605	|IO	|	|	|	|	4.68
20.333	0.86	1.05	1.603	|IO	|	|	|	|	4.67
20.417	0.86	1.05	1.602	|IO	|	|	|	|	4.67
20.500	0.86	1.05	1.600	|IO	|	|	|	|	4.67
20.583	0.86	1.05	1.599	|IO	|	|	|	|	4.66
20.667	0.86	1.05	1.598	|IO	|	|	|	|	4.66
20.750	0.86	1.05	1.596	|IO	|	|	|	|	4.66
20.833	0.74	1.05	1.595	|IO	|	|	|	|	4.65
20.917	0.62	1.05	1.592	|IO	|	|	|	|	4.65
21.000	0.59	1.05	1.589	|IO	|	|	|	|	4.64
21.083	0.69	1.05	1.586	|IO	|	|	|	|	4.63
21.167	0.82	1.05	1.584	|IO	|	|	|	|	4.63
21.250	0.84	1.05	1.583	|IO	|	|	|	|	4.63

21.333	0.74	1.05	1.581	IO				4.62
21.417	0.62	1.04	1.579	IO				4.62
21.500	0.59	1.04	1.575	IO				4.61
21.583	0.69	1.04	1.573	IO				4.60
21.667	0.82	1.04	1.571	IO				4.60
21.750	0.84	1.04	1.569	IO				4.59
21.833	0.74	1.04	1.568	IO				4.59
21.917	0.62	1.04	1.565	IO				4.59
22.000	0.59	1.04	1.562	IO				4.58
22.083	0.69	1.04	1.559	IO				4.57
22.167	0.82	1.04	1.557	IO				4.57
22.250	0.84	1.04	1.556	IO				4.56
22.333	0.74	1.03	1.554	IO				4.56
22.417	0.62	1.03	1.552	IO				4.55
22.500	0.59	1.03	1.549	IO				4.55
22.583	0.58	1.03	1.546	IO				4.54
22.667	0.57	1.03	1.543	IO				4.53
22.750	0.57	1.03	1.540	IO				4.53
22.833	0.57	1.03	1.536	IO				4.52
22.917	0.57	1.03	1.533	IO				4.51
23.000	0.57	1.02	1.530	IO				4.51
23.083	0.57	1.02	1.527	IO				4.50
23.167	0.57	1.02	1.524	IO				4.49
23.250	0.57	1.02	1.521	IO				4.48
23.333	0.57	1.02	1.518	IO				4.48
23.417	0.57	1.02	1.515	IO				4.47
23.500	0.57	1.02	1.512	IO				4.46
23.583	0.57	1.02	1.509	IO				4.45
23.667	0.57	1.01	1.506	IO				4.45
23.750	0.57	1.01	1.503	IO				4.44
23.833	0.57	1.01	1.500	IO				4.43
23.917	0.57	1.01	1.497	IO				4.43
24.000	0.57	1.01	1.494	IO				4.42
24.083	0.34	1.01	1.490	I O				4.41
24.167	0.09	1.00	1.484	I O				4.40
24.250	0.03	1.00	1.478	I O				4.38
24.333	0.01	1.00	1.471	I O				4.37
24.417	0.00	1.00	1.464	I O				4.35
24.500	0.00	0.99	1.457	I O				4.33
24.583	0.00	0.99	1.451	I O				4.32
24.667	0.00	0.99	1.444	I O				4.30
24.750	0.00	0.98	1.437	I O				4.29
24.833	0.00	0.98	1.430	I O				4.27
24.917	0.00	0.98	1.423	I O				4.25
25.000	0.00	0.97	1.417	I O				4.24
25.083	0.00	0.97	1.410	I O				4.22
25.167	0.00	0.97	1.403	I O				4.21
25.250	0.00	0.97	1.397	I O				4.19
25.333	0.00	0.96	1.390	I O				4.17
25.417	0.00	0.96	1.383	I O				4.16
25.500	0.00	0.96	1.377	I O				4.14
25.583	0.00	0.95	1.370	I O				4.13
25.667	0.00	0.95	1.364	I O				4.11
25.750	0.00	0.95	1.357	I O				4.10
25.833	0.00	0.95	1.351	I O				4.08
25.917	0.00	0.94	1.344	I O				4.07
26.000	0.00	0.94	1.338	I O				4.05
26.083	0.00	0.94	1.331	I O				4.04
26.167	0.00	0.93	1.325	I O				4.02
26.250	0.00	0.93	1.318	I O				4.01
26.333	0.00	0.93	1.312	I O				3.99
26.417	0.00	0.92	1.306	I O				3.97
26.500	0.00	0.92	1.299	I O				3.96
26.583	0.00	0.92	1.293	I O				3.94
26.667	0.00	0.91	1.287	I O				3.93
26.750	0.00	0.91	1.280	I O				3.91
26.833	0.00	0.91	1.274	I O				3.89
26.917	0.00	0.90	1.268	I O				3.88
27.000	0.00	0.90	1.262	IO				3.86
27.083	0.00	0.90	1.255	IO				3.85
27.167	0.00	0.89	1.249	IO				3.83
27.250	0.00	0.89	1.243	IO				3.82
27.333	0.00	0.89	1.237	IO				3.80
27.417	0.00	0.88	1.231	IO				3.78
27.500	0.00	0.88	1.225	IO				3.77
27.583	0.00	0.88	1.219	IO				3.75
27.667	0.00	0.87	1.213	IO				3.74
27.750	0.00	0.87	1.207	IO				3.72
27.833	0.00	0.87	1.201	IO				3.71
27.917	0.00	0.87	1.195	IO				3.69
28.000	0.00	0.86	1.189	IO				3.68

28.083	0.00	0.86	1.183	IO					3.66
28.167	0.00	0.86	1.177	IO					3.65
28.250	0.00	0.85	1.171	IO					3.63
28.333	0.00	0.85	1.165	IO					3.62
28.417	0.00	0.85	1.159	IO					3.60
28.500	0.00	0.84	1.153	IO					3.59
28.583	0.00	0.84	1.148	IO					3.57
28.667	0.00	0.84	1.142	IO					3.56
28.750	0.00	0.83	1.136	IO					3.55
28.833	0.00	0.83	1.130	IO					3.53
28.917	0.00	0.83	1.125	IO					3.52
29.000	0.00	0.82	1.119	IO					3.50
29.083	0.00	0.82	1.113	IO					3.49
29.167	0.00	0.82	1.108	IO					3.47
29.250	0.00	0.81	1.102	IO					3.46
29.333	0.00	0.81	1.096	IO					3.44
29.417	0.00	0.81	1.091	IO					3.43
29.500	0.00	0.80	1.085	IO					3.41
29.583	0.00	0.80	1.080	IO					3.40
29.667	0.00	0.80	1.074	IO					3.38
29.750	0.00	0.79	1.069	IO					3.37
29.833	0.00	0.79	1.063	IO					3.36
29.917	0.00	0.78	1.058	IO					3.34
30.000	0.00	0.78	1.053	IO					3.33
30.083	0.00	0.78	1.047	IO					3.31
30.167	0.00	0.77	1.042	IO					3.30
30.250	0.00	0.77	1.037	IO					3.28
30.333	0.00	0.77	1.031	IO					3.27
30.417	0.00	0.76	1.026	IO					3.26
30.500	0.00	0.76	1.021	IO					3.24
30.583	0.00	0.76	1.016	IO					3.23
30.667	0.00	0.75	1.010	IO					3.21
30.750	0.00	0.75	1.005	IO					3.20
30.833	0.00	0.75	1.000	IO					3.19
30.917	0.00	0.74	0.995	IO					3.17
31.000	0.00	0.74	0.990	IO					3.16
31.083	0.00	0.74	0.985	IO					3.15
31.167	0.00	0.73	0.980	IO					3.13
31.250	0.00	0.73	0.975	IO					3.12
31.333	0.00	0.73	0.970	IO					3.11
31.417	0.00	0.72	0.965	IO					3.09
31.500	0.00	0.72	0.960	IO					3.08
31.583	0.00	0.72	0.955	IO					3.07
31.667	0.00	0.71	0.950	IO					3.05
31.750	0.00	0.71	0.945	IO					3.04
31.833	0.00	0.71	0.940	IO					3.03
31.917	0.00	0.70	0.935	IO					3.01
32.000	0.00	0.70	0.930	IO					3.00
32.083	0.00	0.69	0.926	IO					2.99
32.167	0.00	0.69	0.921	IO					2.97
32.250	0.00	0.68	0.916	IO					2.96
32.333	0.00	0.67	0.911	IO					2.95
32.417	0.00	0.67	0.907	IO					2.93
32.500	0.00	0.66	0.902	IO					2.92
32.583	0.00	0.65	0.898	IO					2.91
32.667	0.00	0.65	0.893	IO					2.89
32.750	0.00	0.64	0.889	IO					2.88
32.833	0.00	0.63	0.884	IO					2.87
32.917	0.00	0.63	0.880	IO					2.86
33.000	0.00	0.62	0.876	IO					2.84
33.083	0.00	0.61	0.872	IO					2.83
33.167	0.00	0.61	0.867	IO					2.82
33.250	0.00	0.60	0.863	IO					2.81
33.333	0.00	0.60	0.859	IO					2.80
33.417	0.00	0.59	0.855	IO					2.78
33.500	0.00	0.58	0.851	IO					2.77
33.583	0.00	0.58	0.847	IO					2.76
33.667	0.00	0.57	0.843	IO					2.75
33.750	0.00	0.57	0.839	IO					2.74
33.833	0.00	0.56	0.835	IO					2.73
33.917	0.00	0.56	0.831	IO					2.71
34.000	0.00	0.55	0.828	IO					2.70
34.083	0.00	0.54	0.824	IO					2.69
34.167	0.00	0.54	0.820	IO					2.68
34.250	0.00	0.53	0.816	IO					2.67
34.333	0.00	0.53	0.813	IO					2.66
34.417	0.00	0.52	0.809	IO					2.65
34.500	0.00	0.52	0.806	IO					2.64
34.583	0.00	0.51	0.802	IO					2.63
34.667	0.00	0.51	0.798	IO					2.62
34.750	0.00	0.50	0.795	IO					2.61

34.833	0.00	0.50	0.792	IO				2.60
34.917	0.00	0.49	0.788	IO				2.59
35.000	0.00	0.49	0.785	IO				2.58
35.083	0.00	0.48	0.781	IO				2.57
35.167	0.00	0.48	0.778	IO				2.56
35.250	0.00	0.47	0.775	IO				2.55
35.333	0.00	0.47	0.772	IO				2.54
35.417	0.00	0.46	0.768	IO				2.53
35.500	0.00	0.46	0.765	IO				2.52
35.583	0.00	0.45	0.762	IO				2.51
35.667	0.00	0.45	0.759	O				2.51
35.750	0.00	0.44	0.756	O				2.50
35.833	0.00	0.44	0.753	O				2.49
35.917	0.00	0.44	0.750	O				2.48
36.000	0.00	0.43	0.747	O				2.47
36.083	0.00	0.43	0.744	O				2.46
36.167	0.00	0.42	0.741	O				2.45
36.250	0.00	0.42	0.738	O				2.45
36.333	0.00	0.41	0.735	O				2.44
36.417	0.00	0.41	0.732	O				2.43
36.500	0.00	0.41	0.730	O				2.42
36.583	0.00	0.40	0.727	O				2.41
36.667	0.00	0.40	0.724	O				2.40
36.750	0.00	0.39	0.721	O				2.40
36.833	0.00	0.39	0.719	O				2.39
36.917	0.00	0.39	0.716	O				2.38
37.000	0.00	0.38	0.713	O				2.37
37.083	0.00	0.38	0.711	O				2.37
37.167	0.00	0.37	0.708	O				2.36
37.250	0.00	0.37	0.705	O				2.35
37.333	0.00	0.37	0.703	O				2.34
37.417	0.00	0.36	0.700	O				2.34
37.500	0.00	0.36	0.698	O				2.33
37.583	0.00	0.36	0.695	O				2.32
37.667	0.00	0.35	0.693	O				2.32
37.750	0.00	0.35	0.691	O				2.31
37.833	0.00	0.35	0.688	O				2.30
37.917	0.00	0.34	0.686	O				2.29
38.000	0.00	0.34	0.683	O				2.29
38.083	0.00	0.34	0.681	O				2.28
38.167	0.00	0.33	0.679	O				2.27
38.250	0.00	0.33	0.677	O				2.27
38.333	0.00	0.33	0.674	O				2.26
38.417	0.00	0.32	0.672	O				2.25
38.500	0.00	0.32	0.670	O				2.25
38.583	0.00	0.32	0.668	O				2.24
38.667	0.00	0.31	0.666	O				2.24
38.750	0.00	0.31	0.663	O				2.23
38.833	0.00	0.31	0.661	O				2.22
38.917	0.00	0.30	0.659	O				2.22
39.000	0.00	0.30	0.657	O				2.21
39.083	0.00	0.30	0.655	O				2.21
39.167	0.00	0.29	0.653	O				2.20
39.250	0.00	0.29	0.651	O				2.19
39.333	0.00	0.29	0.649	O				2.19
39.417	0.00	0.29	0.647	O				2.18
39.500	0.00	0.28	0.645	O				2.18
39.583	0.00	0.28	0.643	O				2.17
39.667	0.00	0.28	0.641	O				2.17
39.750	0.00	0.27	0.639	O				2.16
39.833	0.00	0.27	0.637	O				2.15
39.917	0.00	0.27	0.636	O				2.15
40.000	0.00	0.27	0.634	O				2.14
40.083	0.00	0.26	0.632	O				2.14
40.167	0.00	0.26	0.630	O				2.13
40.250	0.00	0.26	0.628	O				2.13
40.333	0.00	0.26	0.627	O				2.12
40.417	0.00	0.25	0.625	O				2.12
40.500	0.00	0.25	0.623	O				2.11
40.583	0.00	0.25	0.621	O				2.11
40.667	0.00	0.25	0.620	O				2.10
40.750	0.00	0.24	0.618	O				2.10
40.833	0.00	0.24	0.616	O				2.09
40.917	0.00	0.24	0.615	O				2.09
41.000	0.00	0.24	0.613	O				2.08
41.083	0.00	0.23	0.611	O				2.08
41.167	0.00	0.23	0.610	O				2.07
41.250	0.00	0.23	0.608	O				2.07
41.333	0.00	0.23	0.607	O				2.07
41.417	0.00	0.22	0.605	O				2.06
41.500	0.00	0.22	0.604	O				2.06

41.583	0.00	0.22	0.602	o					2.05
41.667	0.00	0.22	0.601	o					2.05
41.750	0.00	0.22	0.599	o					2.04
41.833	0.00	0.21	0.598	o					2.04
41.917	0.00	0.21	0.596	o					2.04
42.000	0.00	0.21	0.595	o					2.03
42.083	0.00	0.21	0.593	o					2.03
42.167	0.00	0.20	0.592	o					2.02
42.250	0.00	0.20	0.590	o					2.02
42.333	0.00	0.20	0.589	o					2.01
42.417	0.00	0.20	0.588	o					2.01
42.500	0.00	0.20	0.586	o					2.01
42.583	0.00	0.19	0.585	o					2.00
42.667	0.00	0.19	0.584	o					2.00
42.750	0.00	0.19	0.582	o					1.99
42.833	0.00	0.19	0.581	o					1.99
42.917	0.00	0.19	0.580	o					1.99
43.000	0.00	0.19	0.578	o					1.98
43.083	0.00	0.19	0.577	o					1.98
43.167	0.00	0.19	0.576	o					1.97
43.250	0.00	0.19	0.574	o					1.97
43.333	0.00	0.19	0.573	o					1.96
43.417	0.00	0.19	0.572	o					1.96
43.500	0.00	0.19	0.570	o					1.96
43.583	0.00	0.19	0.569	o					1.95
43.667	0.00	0.19	0.568	o					1.95
43.750	0.00	0.19	0.567	o					1.94
43.833	0.00	0.19	0.565	o					1.94
43.917	0.00	0.19	0.564	o					1.93
44.000	0.00	0.19	0.563	o					1.93
44.083	0.00	0.19	0.561	o					1.93
44.167	0.00	0.19	0.560	o					1.92
44.250	0.00	0.19	0.559	o					1.92
44.333	0.00	0.19	0.557	o					1.91
44.417	0.00	0.19	0.556	o					1.91
44.500	0.00	0.19	0.555	o					1.91
44.583	0.00	0.19	0.554	o					1.90
44.667	0.00	0.19	0.552	o					1.90
44.750	0.00	0.19	0.551	o					1.89
44.833	0.00	0.19	0.550	o					1.89
44.917	0.00	0.19	0.548	o					1.88
45.000	0.00	0.19	0.547	o					1.88
45.083	0.00	0.19	0.546	o					1.88
45.167	0.00	0.19	0.545	o					1.87
45.250	0.00	0.19	0.543	o					1.87
45.333	0.00	0.18	0.542	o					1.86
45.417	0.00	0.18	0.541	o					1.86
45.500	0.00	0.18	0.540	o					1.86
45.583	0.00	0.18	0.538	o					1.85
45.667	0.00	0.18	0.537	o					1.85
45.750	0.00	0.18	0.536	o					1.84
45.833	0.00	0.18	0.534	o					1.84
45.917	0.00	0.18	0.533	o					1.83
46.000	0.00	0.18	0.532	o					1.83
46.083	0.00	0.18	0.531	o					1.83
46.167	0.00	0.18	0.529	o					1.82
46.250	0.00	0.18	0.528	o					1.82
46.333	0.00	0.18	0.527	o					1.81
46.417	0.00	0.18	0.526	o					1.81
46.500	0.00	0.18	0.524	o					1.81
46.583	0.00	0.18	0.523	o					1.80
46.667	0.00	0.18	0.522	o					1.80
46.750	0.00	0.18	0.521	o					1.79
46.833	0.00	0.18	0.519	o					1.79
46.917	0.00	0.18	0.518	o					1.79
47.000	0.00	0.18	0.517	o					1.78
47.083	0.00	0.18	0.516	o					1.78
47.167	0.00	0.18	0.514	o					1.77
47.250	0.00	0.18	0.513	o					1.77
47.333	0.00	0.18	0.512	o					1.77
47.417	0.00	0.18	0.511	o					1.76
47.500	0.00	0.18	0.510	o					1.76
47.583	0.00	0.18	0.508	o					1.75
47.667	0.00	0.18	0.507	o					1.75
47.750	0.00	0.18	0.506	o					1.75
47.833	0.00	0.18	0.505	o					1.74
47.917	0.00	0.18	0.503	o					1.74
48.000	0.00	0.18	0.502	o					1.73
48.083	0.00	0.18	0.501	o					1.73
48.167	0.00	0.18	0.500	o					1.73
48.250	0.00	0.18	0.499	o					1.72

48.333	0.00	0.18	0.497	o					1.72
48.417	0.00	0.18	0.496	o					1.71
48.500	0.00	0.18	0.495	o					1.71
48.583	0.00	0.18	0.494	o					1.71
48.667	0.00	0.18	0.492	o					1.70
48.750	0.00	0.17	0.491	o					1.70
48.833	0.00	0.17	0.490	o					1.70
48.917	0.00	0.17	0.489	o					1.69
49.000	0.00	0.17	0.488	o					1.69
49.083	0.00	0.17	0.486	o					1.68
49.167	0.00	0.17	0.485	o					1.68
49.250	0.00	0.17	0.484	o					1.68
49.333	0.00	0.17	0.483	o					1.67
49.417	0.00	0.17	0.482	o					1.67
49.500	0.00	0.17	0.480	o					1.66
49.583	0.00	0.17	0.479	o					1.66
49.667	0.00	0.17	0.478	o					1.66
49.750	0.00	0.17	0.477	o					1.65
49.833	0.00	0.17	0.476	o					1.65
49.917	0.00	0.17	0.475	o					1.64
50.000	0.00	0.17	0.473	o					1.64
50.083	0.00	0.17	0.472	o					1.64
50.167	0.00	0.17	0.471	o					1.63
50.250	0.00	0.17	0.470	o					1.63
50.333	0.00	0.17	0.469	o					1.63
50.417	0.00	0.17	0.467	o					1.62
50.500	0.00	0.17	0.466	o					1.62
50.583	0.00	0.17	0.465	o					1.61
50.667	0.00	0.17	0.464	o					1.61
50.750	0.00	0.17	0.463	o					1.61
50.833	0.00	0.17	0.462	o					1.60
50.917	0.00	0.17	0.460	o					1.60
51.000	0.00	0.17	0.459	o					1.60
51.083	0.00	0.17	0.458	o					1.59
51.167	0.00	0.17	0.457	o					1.59
51.250	0.00	0.17	0.456	o					1.58
51.333	0.00	0.17	0.455	o					1.58
51.417	0.00	0.17	0.454	o					1.58
51.500	0.00	0.17	0.452	o					1.57
51.583	0.00	0.17	0.451	o					1.57
51.667	0.00	0.17	0.450	o					1.57
51.750	0.00	0.17	0.449	o					1.56
51.833	0.00	0.17	0.448	o					1.56
51.917	0.00	0.17	0.447	o					1.55
52.000	0.00	0.17	0.445	o					1.55
52.083	0.00	0.17	0.444	o					1.55
52.167	0.00	0.17	0.443	o					1.54
52.250	0.00	0.17	0.442	o					1.54
52.333	0.00	0.17	0.441	o					1.54
52.417	0.00	0.16	0.440	o					1.53
52.500	0.00	0.16	0.439	o					1.53
52.583	0.00	0.16	0.438	o					1.52
52.667	0.00	0.16	0.436	o					1.52
52.750	0.00	0.16	0.435	o					1.52
52.833	0.00	0.16	0.434	o					1.51
52.917	0.00	0.16	0.433	o					1.51
53.000	0.00	0.16	0.432	o					1.51
53.083	0.00	0.16	0.431	o					1.50
53.167	0.00	0.16	0.430	o					1.50
53.250	0.00	0.16	0.429	o					1.50
53.333	0.00	0.16	0.427	o					1.49
53.417	0.00	0.16	0.426	o					1.49
53.500	0.00	0.16	0.425	o					1.48
53.583	0.00	0.16	0.424	o					1.48
53.667	0.00	0.16	0.423	o					1.48
53.750	0.00	0.16	0.422	o					1.47
53.833	0.00	0.16	0.421	o					1.47
53.917	0.00	0.16	0.420	o					1.47
54.000	0.00	0.16	0.418	o					1.46
54.083	0.00	0.16	0.417	o					1.46
54.167	0.00	0.16	0.416	o					1.46
54.250	0.00	0.16	0.415	o					1.45
54.333	0.00	0.16	0.414	o					1.45
54.417	0.00	0.16	0.413	o					1.44
54.500	0.00	0.16	0.412	o					1.44
54.583	0.00	0.16	0.411	o					1.44
54.667	0.00	0.16	0.410	o					1.43
54.750	0.00	0.16	0.409	o					1.43
54.833	0.00	0.16	0.407	o					1.43
54.917	0.00	0.16	0.406	o					1.42
55.000	0.00	0.16	0.405	o					1.42

55.083	0.00	0.16	0.404	o	|	|	|	|	1.42
55.167	0.00	0.16	0.403	o	|	|	|	|	1.41
55.250	0.00	0.16	0.402	o	|	|	|	|	1.41
55.333	0.00	0.16	0.401	o	|	|	|	|	1.41
55.417	0.00	0.16	0.400	o	|	|	|	|	1.40
55.500	0.00	0.16	0.399	o	|	|	|	|	1.40
55.583	0.00	0.16	0.398	o	|	|	|	|	1.40
55.667	0.00	0.16	0.397	o	|	|	|	|	1.39
55.750	0.00	0.16	0.396	o	|	|	|	|	1.39
55.833	0.00	0.16	0.394	o	|	|	|	|	1.38
55.917	0.00	0.16	0.393	o	|	|	|	|	1.38
56.000	0.00	0.16	0.392	o	|	|	|	|	1.38
56.083	0.00	0.16	0.391	o	|	|	|	|	1.37
56.167	0.00	0.16	0.390	o	|	|	|	|	1.37
56.250	0.00	0.16	0.389	o	|	|	|	|	1.37
56.333	0.00	0.15	0.388	o	|	|	|	|	1.36
56.417	0.00	0.15	0.387	o	|	|	|	|	1.36
56.500	0.00	0.15	0.386	o	|	|	|	|	1.36
56.583	0.00	0.15	0.385	o	|	|	|	|	1.35
56.667	0.00	0.15	0.384	o	|	|	|	|	1.35
56.750	0.00	0.15	0.383	o	|	|	|	|	1.35
56.833	0.00	0.15	0.382	o	|	|	|	|	1.34
56.917	0.00	0.15	0.381	o	|	|	|	|	1.34
57.000	0.00	0.15	0.380	o	|	|	|	|	1.34
57.083	0.00	0.15	0.379	o	|	|	|	|	1.33
57.167	0.00	0.15	0.377	o	|	|	|	|	1.33
57.250	0.00	0.15	0.376	o	|	|	|	|	1.33
57.333	0.00	0.15	0.375	o	|	|	|	|	1.32
57.417	0.00	0.15	0.374	o	|	|	|	|	1.32
57.500	0.00	0.15	0.373	o	|	|	|	|	1.32
57.583	0.00	0.15	0.372	o	|	|	|	|	1.31
57.667	0.00	0.15	0.371	o	|	|	|	|	1.31
57.750	0.00	0.15	0.370	o	|	|	|	|	1.31
57.833	0.00	0.15	0.369	o	|	|	|	|	1.30
57.917	0.00	0.15	0.368	o	|	|	|	|	1.30
58.000	0.00	0.15	0.367	o	|	|	|	|	1.30
58.083	0.00	0.15	0.366	o	|	|	|	|	1.29
58.167	0.00	0.15	0.365	o	|	|	|	|	1.29
58.250	0.00	0.15	0.364	o	|	|	|	|	1.29
58.333	0.00	0.15	0.363	o	|	|	|	|	1.28
58.417	0.00	0.15	0.362	o	|	|	|	|	1.28
58.500	0.00	0.15	0.361	o	|	|	|	|	1.28
58.583	0.00	0.15	0.360	o	|	|	|	|	1.27
58.667	0.00	0.15	0.359	o	|	|	|	|	1.27
58.750	0.00	0.15	0.358	o	|	|	|	|	1.27
58.833	0.00	0.15	0.357	o	|	|	|	|	1.26
58.917	0.00	0.15	0.356	o	|	|	|	|	1.26
59.000	0.00	0.15	0.355	o	|	|	|	|	1.26
59.083	0.00	0.15	0.354	o	|	|	|	|	1.25
59.167	0.00	0.15	0.353	o	|	|	|	|	1.25
59.250	0.00	0.15	0.352	o	|	|	|	|	1.25
59.333	0.00	0.15	0.351	o	|	|	|	|	1.24
59.417	0.00	0.15	0.350	o	|	|	|	|	1.24
59.500	0.00	0.15	0.349	o	|	|	|	|	1.24
59.583	0.00	0.15	0.348	o	|	|	|	|	1.23
59.667	0.00	0.15	0.347	o	|	|	|	|	1.23
59.750	0.00	0.15	0.346	o	|	|	|	|	1.23
59.833	0.00	0.15	0.345	o	|	|	|	|	1.22
59.917	0.00	0.15	0.344	o	|	|	|	|	1.22
60.000	0.00	0.15	0.342	o	|	|	|	|	1.22
60.083	0.00	0.15	0.341	o	|	|	|	|	1.21
60.167	0.00	0.15	0.340	o	|	|	|	|	1.21
60.250	0.00	0.15	0.339	o	|	|	|	|	1.21
60.333	0.00	0.15	0.338	o	|	|	|	|	1.20
60.417	0.00	0.14	0.337	o	|	|	|	|	1.20
60.500	0.00	0.14	0.336	o	|	|	|	|	1.20
60.583	0.00	0.14	0.335	o	|	|	|	|	1.19
60.667	0.00	0.14	0.334	o	|	|	|	|	1.19
60.750	0.00	0.14	0.334	o	|	|	|	|	1.19
60.833	0.00	0.14	0.333	o	|	|	|	|	1.18
60.917	0.00	0.14	0.332	o	|	|	|	|	1.18
61.000	0.00	0.14	0.331	o	|	|	|	|	1.18
61.083	0.00	0.14	0.330	o	|	|	|	|	1.17
61.167	0.00	0.14	0.329	o	|	|	|	|	1.17
61.250	0.00	0.14	0.328	o	|	|	|	|	1.17
61.333	0.00	0.14	0.327	o	|	|	|	|	1.16
61.417	0.00	0.14	0.326	o	|	|	|	|	1.16
61.500	0.00	0.14	0.325	o	|	|	|	|	1.16
61.583	0.00	0.14	0.324	o	|	|	|	|	1.15
61.667	0.00	0.14	0.323	o	|	|	|	|	1.15
61.750	0.00	0.14	0.322	o	|	|	|	|	1.15

61.833	0.00	0.14	0.321	o					1.15
61.917	0.00	0.14	0.320	o					1.14
62.000	0.00	0.14	0.319	o					1.14
62.083	0.00	0.14	0.318	o					1.14
62.167	0.00	0.14	0.317	o					1.13
62.250	0.00	0.14	0.316	o					1.13
62.333	0.00	0.14	0.315	o					1.13
62.417	0.00	0.14	0.314	o					1.12
62.500	0.00	0.14	0.313	o					1.12
62.583	0.00	0.14	0.312	o					1.12
62.667	0.00	0.14	0.311	o					1.11
62.750	0.00	0.14	0.310	o					1.11
62.833	0.00	0.14	0.309	o					1.11
62.917	0.00	0.14	0.308	o					1.10
63.000	0.00	0.14	0.307	o					1.10
63.083	0.00	0.14	0.306	o					1.10
63.167	0.00	0.14	0.305	o					1.09
63.250	0.00	0.14	0.304	o					1.09
63.333	0.00	0.14	0.303	o					1.09
63.417	0.00	0.14	0.302	o					1.09
63.500	0.00	0.14	0.301	o					1.08
63.583	0.00	0.14	0.300	o					1.08
63.667	0.00	0.14	0.300	o					1.08
63.750	0.00	0.14	0.299	o					1.07
63.833	0.00	0.14	0.298	o					1.07
63.917	0.00	0.14	0.297	o					1.07
64.000	0.00	0.14	0.296	o					1.06
64.083	0.00	0.14	0.295	o					1.06
64.167	0.00	0.14	0.294	o					1.06
64.250	0.00	0.14	0.293	o					1.06
64.333	0.00	0.14	0.292	o					1.05
64.417	0.00	0.14	0.291	o					1.05
64.500	0.00	0.14	0.290	o					1.05
64.583	0.00	0.14	0.289	o					1.04
64.667	0.00	0.14	0.288	o					1.04
64.750	0.00	0.14	0.287	o					1.04
64.833	0.00	0.14	0.286	o					1.03
64.917	0.00	0.13	0.285	o					1.03
65.000	0.00	0.13	0.285	o					1.03
65.083	0.00	0.13	0.284	o					1.02
65.167	0.00	0.13	0.283	o					1.02
65.250	0.00	0.13	0.282	o					1.02
65.333	0.00	0.13	0.281	o					1.02
65.417	0.00	0.13	0.280	o					1.01
65.500	0.00	0.13	0.279	o					1.01
65.583	0.00	0.13	0.278	o					1.01
65.667	0.00	0.13	0.277	o					1.00
65.750	0.00	0.13	0.276	o					1.00
65.833	0.00	0.13	0.275	o					1.00
65.917	0.00	0.13	0.274	o					0.99
66.000	0.00	0.13	0.274	o					0.99
66.083	0.00	0.13	0.273	o					0.99
66.167	0.00	0.13	0.272	o					0.98
66.250	0.00	0.13	0.271	o					0.98
66.333	0.00	0.13	0.270	o					0.98
66.417	0.00	0.13	0.269	o					0.97
66.500	0.00	0.13	0.268	o					0.97
66.583	0.00	0.13	0.267	o					0.97
66.667	0.00	0.13	0.266	o					0.97
66.750	0.00	0.13	0.265	o					0.96
66.833	0.00	0.13	0.265	o					0.96
66.917	0.00	0.13	0.264	o					0.96
67.000	0.00	0.13	0.263	o					0.95
67.083	0.00	0.13	0.262	o					0.95
67.167	0.00	0.13	0.261	o					0.95
67.250	0.00	0.13	0.260	o					0.94
67.333	0.00	0.12	0.259	o					0.94
67.417	0.00	0.12	0.259	o					0.94
67.500	0.00	0.12	0.258	o					0.93
67.583	0.00	0.12	0.257	o					0.93
67.667	0.00	0.12	0.256	o					0.93
67.750	0.00	0.12	0.255	o					0.92
67.833	0.00	0.12	0.254	o					0.92
67.917	0.00	0.12	0.253	o					0.92
68.000	0.00	0.12	0.253	o					0.92
68.083	0.00	0.12	0.252	o					0.91
68.167	0.00	0.12	0.251	o					0.91
68.250	0.00	0.12	0.250	o					0.91
68.333	0.00	0.12	0.249	o					0.90
68.417	0.00	0.12	0.248	o					0.90
68.500	0.00	0.12	0.248	o					0.90

68.583	0.00	0.12	0.247	o	|	|	|	|	0.89
68.667	0.00	0.12	0.246	o	|	|	|	|	0.89
68.750	0.00	0.12	0.245	o	|	|	|	|	0.89
68.833	0.00	0.12	0.244	o	|	|	|	|	0.89
68.917	0.00	0.12	0.244	o	|	|	|	|	0.88
69.000	0.00	0.12	0.243	o	|	|	|	|	0.88
69.083	0.00	0.12	0.242	o	|	|	|	|	0.88
69.167	0.00	0.12	0.241	o	|	|	|	|	0.87
69.250	0.00	0.12	0.240	o	|	|	|	|	0.87
69.333	0.00	0.12	0.240	o	|	|	|	|	0.87
69.417	0.00	0.12	0.239	o	|	|	|	|	0.86
69.500	0.00	0.11	0.238	o	|	|	|	|	0.86
69.583	0.00	0.11	0.237	o	|	|	|	|	0.86
69.667	0.00	0.11	0.236	o	|	|	|	|	0.86
69.750	0.00	0.11	0.236	o	|	|	|	|	0.85
69.833	0.00	0.11	0.235	o	|	|	|	|	0.85
69.917	0.00	0.11	0.234	o	|	|	|	|	0.85
70.000	0.00	0.11	0.233	o	|	|	|	|	0.85
70.083	0.00	0.11	0.232	o	|	|	|	|	0.84
70.167	0.00	0.11	0.232	o	|	|	|	|	0.84
70.250	0.00	0.11	0.231	o	|	|	|	|	0.84
70.333	0.00	0.11	0.230	o	|	|	|	|	0.83
70.417	0.00	0.11	0.229	o	|	|	|	|	0.83
70.500	0.00	0.11	0.229	o	|	|	|	|	0.83
70.583	0.00	0.11	0.228	o	|	|	|	|	0.83
70.667	0.00	0.11	0.227	o	|	|	|	|	0.82
70.750	0.00	0.11	0.226	o	|	|	|	|	0.82
70.833	0.00	0.11	0.226	o	|	|	|	|	0.82
70.917	0.00	0.11	0.225	o	|	|	|	|	0.81
71.000	0.00	0.11	0.224	o	|	|	|	|	0.81
71.083	0.00	0.11	0.223	o	|	|	|	|	0.81
71.167	0.00	0.11	0.223	o	|	|	|	|	0.81
71.250	0.00	0.11	0.222	o	|	|	|	|	0.80
71.333	0.00	0.11	0.221	o	|	|	|	|	0.80
71.417	0.00	0.11	0.220	o	|	|	|	|	0.80
71.500	0.00	0.11	0.220	o	|	|	|	|	0.80
71.583	0.00	0.11	0.219	o	|	|	|	|	0.79
71.667	0.00	0.11	0.218	o	|	|	|	|	0.79
71.750	0.00	0.10	0.218	o	|	|	|	|	0.79
71.833	0.00	0.10	0.217	o	|	|	|	|	0.79
71.917	0.00	0.10	0.216	o	|	|	|	|	0.78
72.000	0.00	0.10	0.215	o	|	|	|	|	0.78
72.083	0.00	0.10	0.215	o	|	|	|	|	0.78
72.167	0.00	0.10	0.214	o	|	|	|	|	0.78
72.250	0.00	0.10	0.213	o	|	|	|	|	0.77
72.333	0.00	0.10	0.213	o	|	|	|	|	0.77
72.417	0.00	0.10	0.212	o	|	|	|	|	0.77
72.500	0.00	0.10	0.211	o	|	|	|	|	0.76
72.583	0.00	0.10	0.210	o	|	|	|	|	0.76
72.667	0.00	0.10	0.210	o	|	|	|	|	0.76
72.750	0.00	0.10	0.209	o	|	|	|	|	0.76
72.833	0.00	0.10	0.208	o	|	|	|	|	0.75
72.917	0.00	0.10	0.208	o	|	|	|	|	0.75
73.000	0.00	0.10	0.207	o	|	|	|	|	0.75

Remaining water in basin = 0.21 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 876
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 14.381 (CFS)
Total volume = 6.538 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

Appendix F – Catch Basin and Streert Capacity Calculations

Interior Streets
Worksheet for Irregular Channel

Project Description	
Worksheet	Interior Streets
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data		
Slope	0.010000	ft/ft
Water Surface Elevation	0.50	ft

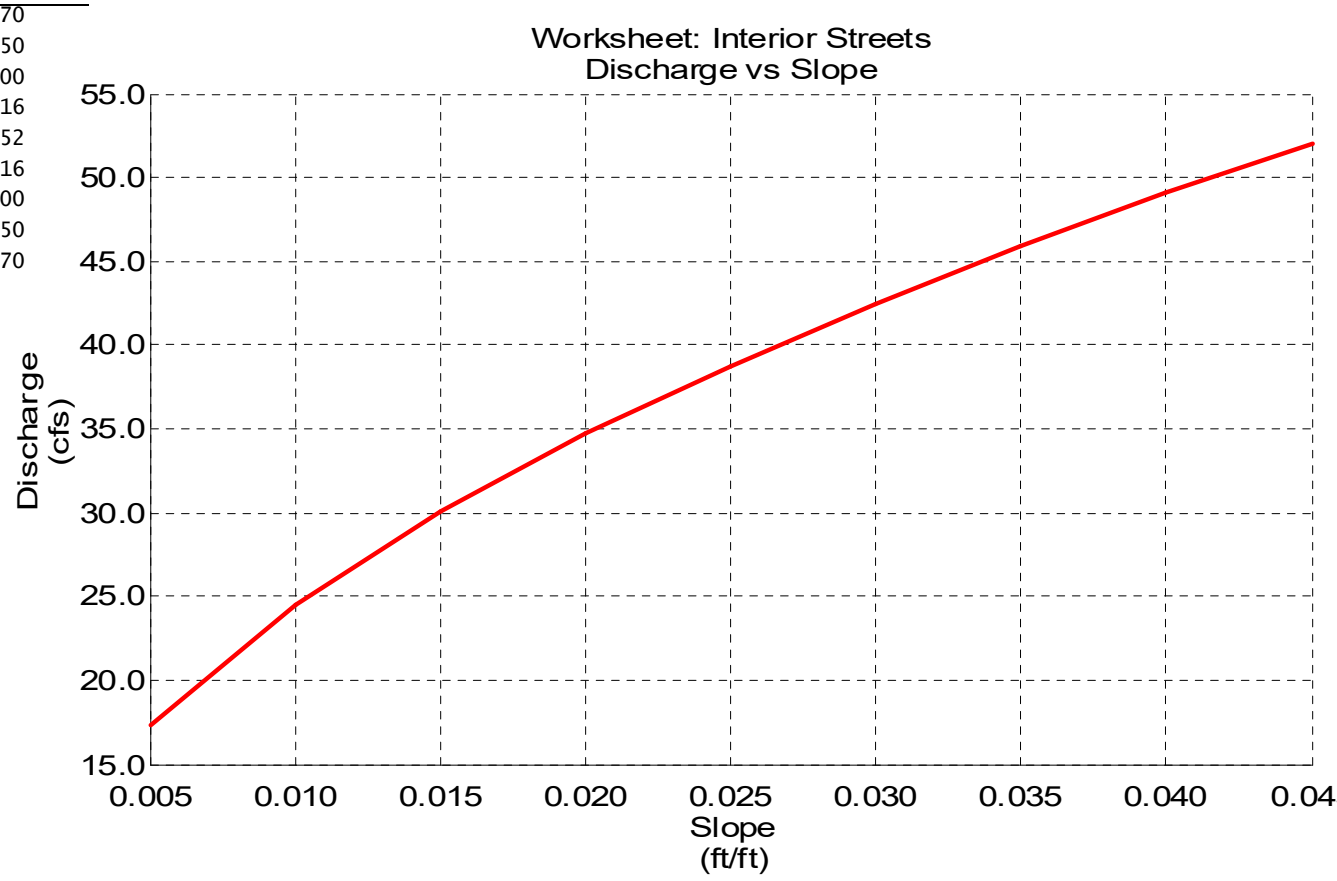
Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

Results		
Mannings Coefficient	0.015	
Elevation Range	0.00 to 0.70	
Discharge	24.53	cfs
Flow Area	7.5	ft²
Wetted Perimeter	39.02	ft
Top Width	38.00	ft
Actual Depth	0.50	ft
Critical Elevation	0.55	ft
Critical Slope	0.005677	ft/ft
Velocity	3.29	ft/s
Velocity Head	0.17	ft
Specific Energy	0.67	ft
Froude Number	1.31	
Flow Type	Supercritical	

Calculation Messages:
Flow is divided.

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00	0+60	0.015

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00	0.70
0+10	0.50
0+10	0.00
0+12	0.16
0+30	0.52
0+48	0.16
0+50	0.00
0+50	0.50
0+60	0.70



Node 2
Worksheet for Curb Inlet On Grade

Project Description	
Worksheet	NODE 2
Type	Curb Inlet On Grade
Solve For	Efficiency

Input Data		
Discharge	15.93	cfs
Slope	0.030000	ft/ft
Gutter Width	2.00	ft
Gutter Cross Slope	0.080000	ft/ft
Road Cross Slope	0.020000	ft/ft
Mannings Coefficient	0.013	
Curb Opening Length	21.00	ft
Local Depression	12.0	in
Local Depression Width	2.00	ft

Results		
Efficiency	1.00	
Intercepted Flow	15.93	cfs
Bypass Flow	0.00	cfs
Spread	14.65	ft
Depth	0.41	ft
Flow Area	2.3	ft²
Gutter Depression	1.4	in
Total Depression	13.4	in
Velocity	7.03	ft/s
Equivalent Cross Slope	0.245382	ft/ft
Length Factor	1.00	
Total Interception Length	21.08	ft

Node 6
Worksheet for Curb Inlet On Grade

Project Description	
Worksheet	NODE 6
Type	Curb Inlet On Grade
Solve For	Efficiency

Input Data		
Discharge	18.27	cfs
Slope	0.010000	ft/ft
Gutter Width	2.00	ft
Gutter Cross Slope	0.080000	ft/ft
Road Cross Slope	0.020000	ft/ft
Mannings Coefficient	0.013	
Curb Opening Length	21.00	ft
Local Depression	10.0	in
Local Depression Width	2.00	ft

Results		
Efficiency	1.00	
Intercepted Flow	18.27	cfs
Bypass Flow	0.00	cfs
Spread	19.32	ft
Depth	0.51	ft
Flow Area	3.9	ft²
Gutter Depression	1.4	in
Total Depression	11.4	in
Velocity	4.74	ft/s
Equivalent Cross Slope	0.165268	ft/ft
Length Factor	1.03	
Total Interception Length	20.36	ft

Node 7
Worksheet for Curb Inlet On Grade

Project Description	
Worksheet	NODE 7
Type	Curb Inlet On Grade
Solve For	Efficiency

Input Data		
Discharge	14.67	cfs
Slope	0.010000	ft/ft
Gutter Width	2.00	ft
Gutter Cross Slope	0.080000	ft/ft
Road Cross Slope	0.020000	ft/ft
Mannings Coefficient	0.013	
Curb Opening Length	21.00	ft
Local Depression	10.0	in
Local Depression Width	2.00	ft

Results		
Efficiency	1.00	
Intercepted Flow	14.67	cfs
Bypass Flow	0.00	cfs
Spread	17.70	ft
Depth	0.47	ft
Flow Area	3.3	ft²
Gutter Depression	1.4	in
Total Depression	11.4	in
Velocity	4.51	ft/s
Equivalent Cross Slope	0.178803	ft/ft
Length Factor	1.19	
Total Interception Length	17.71	ft

Node 10
Worksheet for Curb Inlet On Grade

Project Description	
Worksheet	NODE 10
Type	Curb Inlet On Grade
Solve For	Efficiency

Input Data		
Discharge	6.96	cfs
Slope	0.030000	ft/ft
Gutter Width	2.00	ft
Gutter Cross Slope	0.080000	ft/ft
Road Cross Slope	0.020000	ft/ft
Mannings Coefficient	0.013	
Curb Opening Length	21.00	ft
Local Depression	10.0	in
Local Depression Width	2.00	ft

Results		
Efficiency	1.00	
Intercepted Flow	6.96	cfs
Bypass Flow	0.00	cfs
Spread	10.28	ft
Depth	0.33	ft
Flow Area	1.2	ft²
Gutter Depression	1.4	in
Total Depression	11.4	in
Velocity	5.92	ft/s
Equivalent Cross Slope	0.286422	ft/ft
Length Factor	1.55	
Total Interception Length	13.57	ft

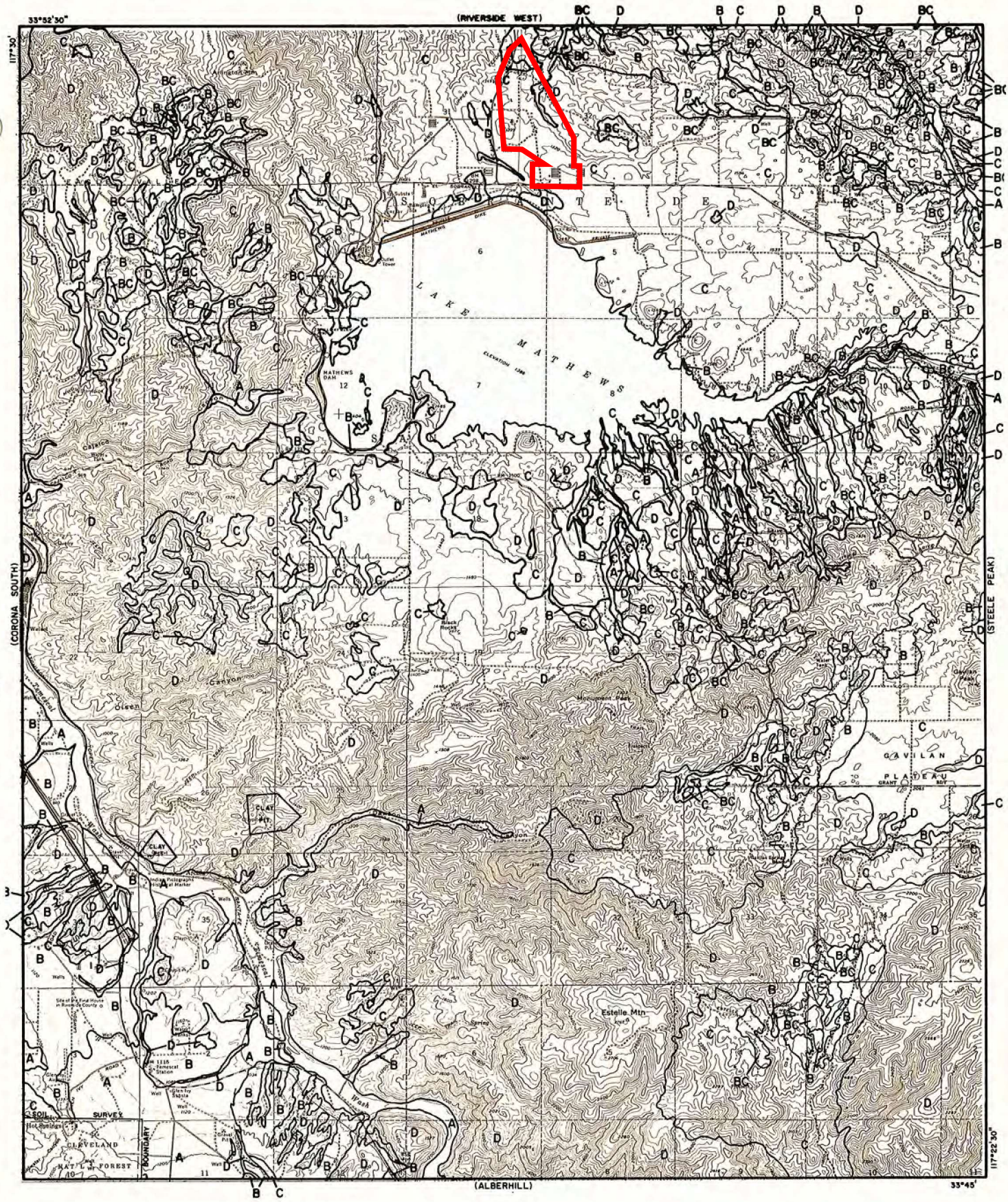
Node 12
Worksheet for Curb Inlet On Grade

Project Description	
Worksheet	NODE 12
Type	Curb Inlet On Grade
Solve For	Efficiency

Input Data		
Discharge	6.47	cfs
Slope	0.030000	ft/ft
Gutter Width	2.00	ft
Gutter Cross Slope	0.080000	ft/ft
Road Cross Slope	0.020000	ft/ft
Mannings Coefficient	0.013	
Curb Opening Length	14.00	ft
Local Depression	10.0	in
Local Depression Width	2.00	ft

Results		
Efficiency	1.00	
Intercepted Flow	6.47	cfs
Bypass Flow	0.00	cfs
Spread	9.94	ft
Depth	0.32	ft
Flow Area	1.1	ft²
Gutter Depression	1.4	in
Total Depression	11.4	in
Velocity	5.83	ft/s
Equivalent Cross Slope	0.294017	ft/ft
Length Factor	1.08	
Total Interception Length	12.96	ft

Appendix G – Riverside County Flood Control Hydology Manual Plates



LEGEND

—— SOILS GROUP BOUNDARY

A SOILS GROUP DESIGNATION

RCFC&WCD

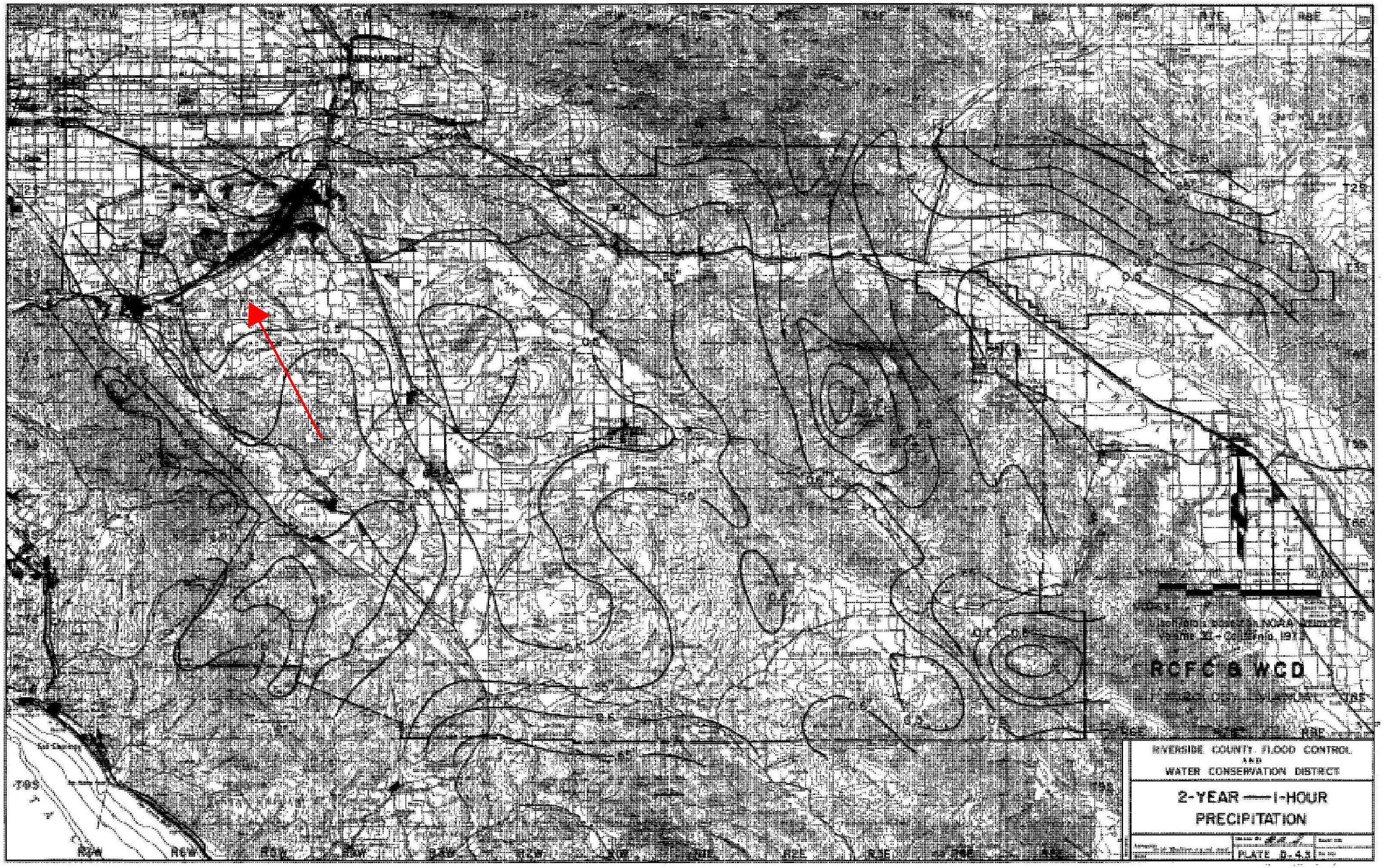
HYDROLOGY MANUAL

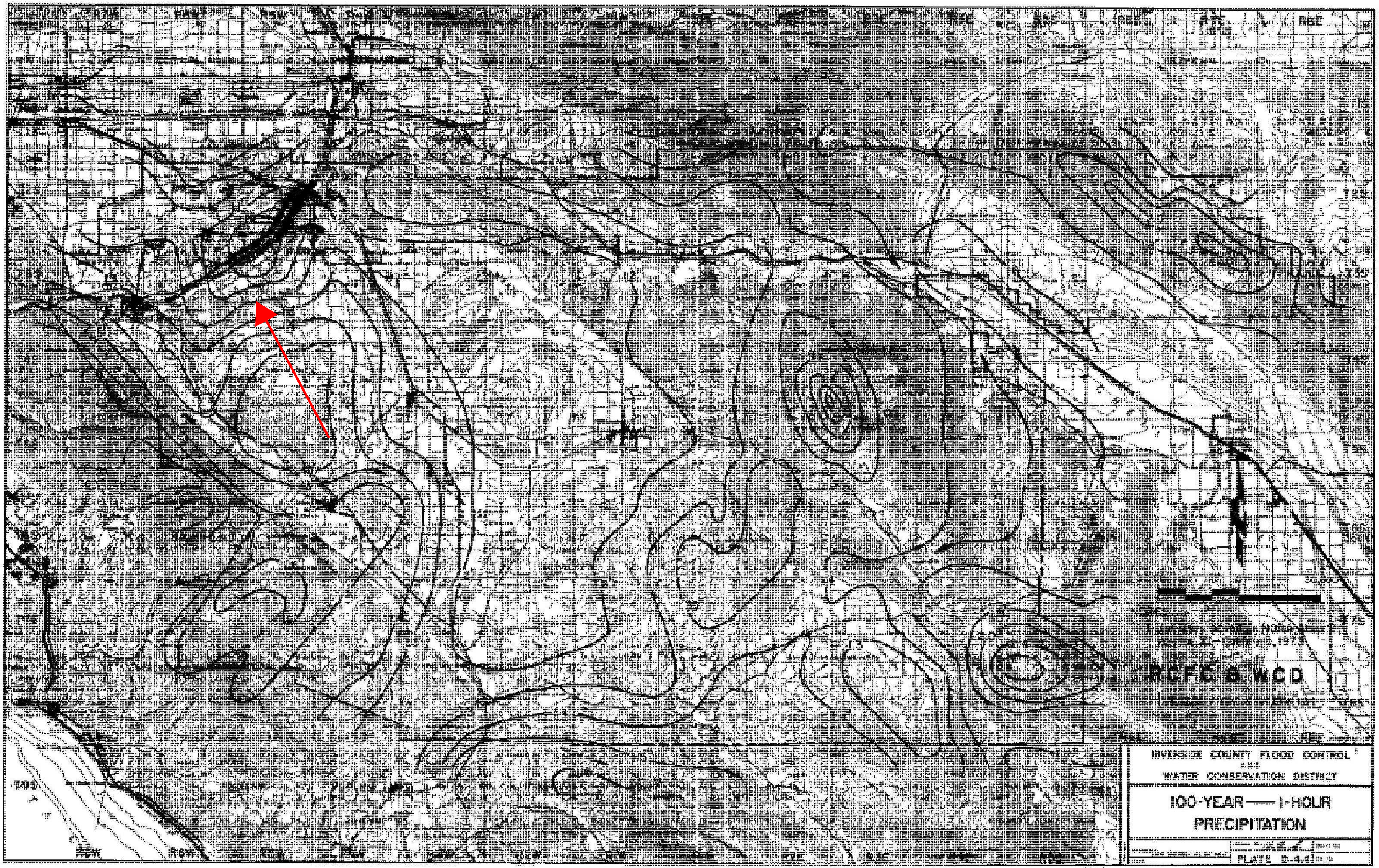
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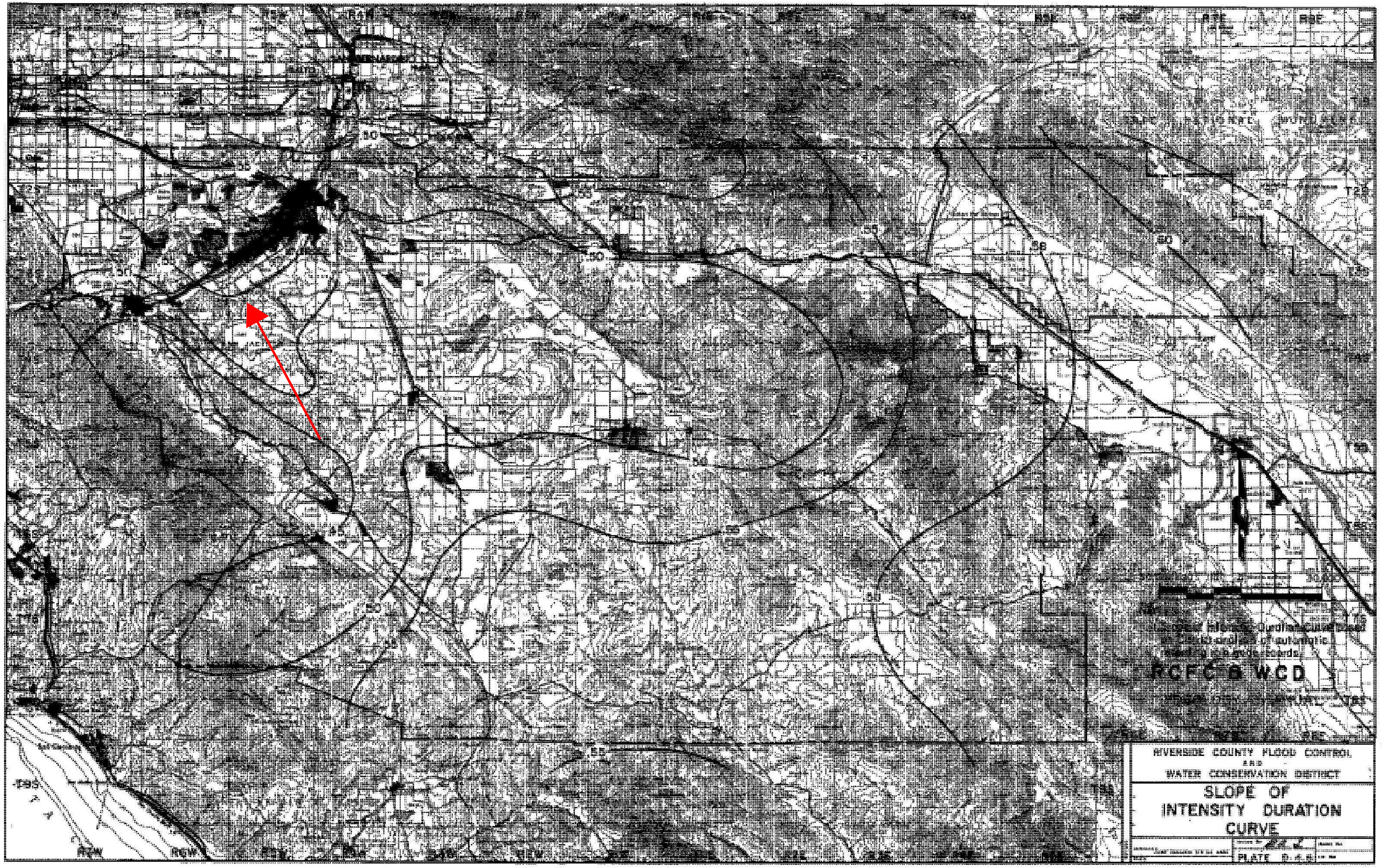
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HYDROLOGIC SOILS GROUP MAP FOR LAKE MATHEWS

PLATE C-1.28


RIVERSIDE COUNTY FLOOD CONTROL
AND
WATER CONSERVATION DISTRICT
2-YEAR — 1-HOUR
PRECIPITATION
PLATE D-4.3
RCFC & WCD


RCFC & WCD
RIVERSIDE COUNTY FLOOD CONTROL AND WATER CONSERVATION DISTRICT
100-YEAR — 1-HOUR PRECIPITATION
PLATE D-4.4


RIVERSIDE COUNTY FLOOD CONTROL
AND
WATER CONSERVATION DISTRICT
SLOPE OF
INTENSITY DURATION
CURVE
PLATE D-4.8
RCFC & WCD

ACTUAL IMPERVIOUS COVER

Land Use (1)	Range-Percent	Recommended Value For Average Conditions-Percent(2)
Natural or Agriculture	0 - 10	0
Single Family Residential: (3)		
40,000 S. F. (1 Acre) Lots	10 - 25	20
20,000 S. F. (½ Acre) Lots	30 - 45	40
7,200 - 10,000 S. F. Lots	45 - 55	50
Multiple Family Residential:		
Condominiums	45 - 70	65
Apartments	65 - 90	80
Mobile Home Park	60 - 85	75
Commercial, Downtown Business or Industrial	80 -100	90

Notes:

1. Land use should be based on ultimate development of the watershed. Long range master plans for the County and incorporated cities should be reviewed to insure reasonable land use assumptions.

2. Recommended values are based on average conditions which may not apply to a particular study area. The percentage impervious may vary greatly even on comparable sized lots due to differences in dwelling size, improvements, etc. Landscape practices should also be considered as it is common in some areas to use ornamental gravels underlain by impervious plastic materials in place of lawns and shrubs. A field investigation of a study area should always be made, and a review of aerial photos, where available may assist in estimating the percentage of impervious cover in developed areas.

3. For typical horse ranch subdivisions increase impervious area 5 percent over the values recommended in the table above.

RCFC & WCD
HYDROLOGY MANUAL

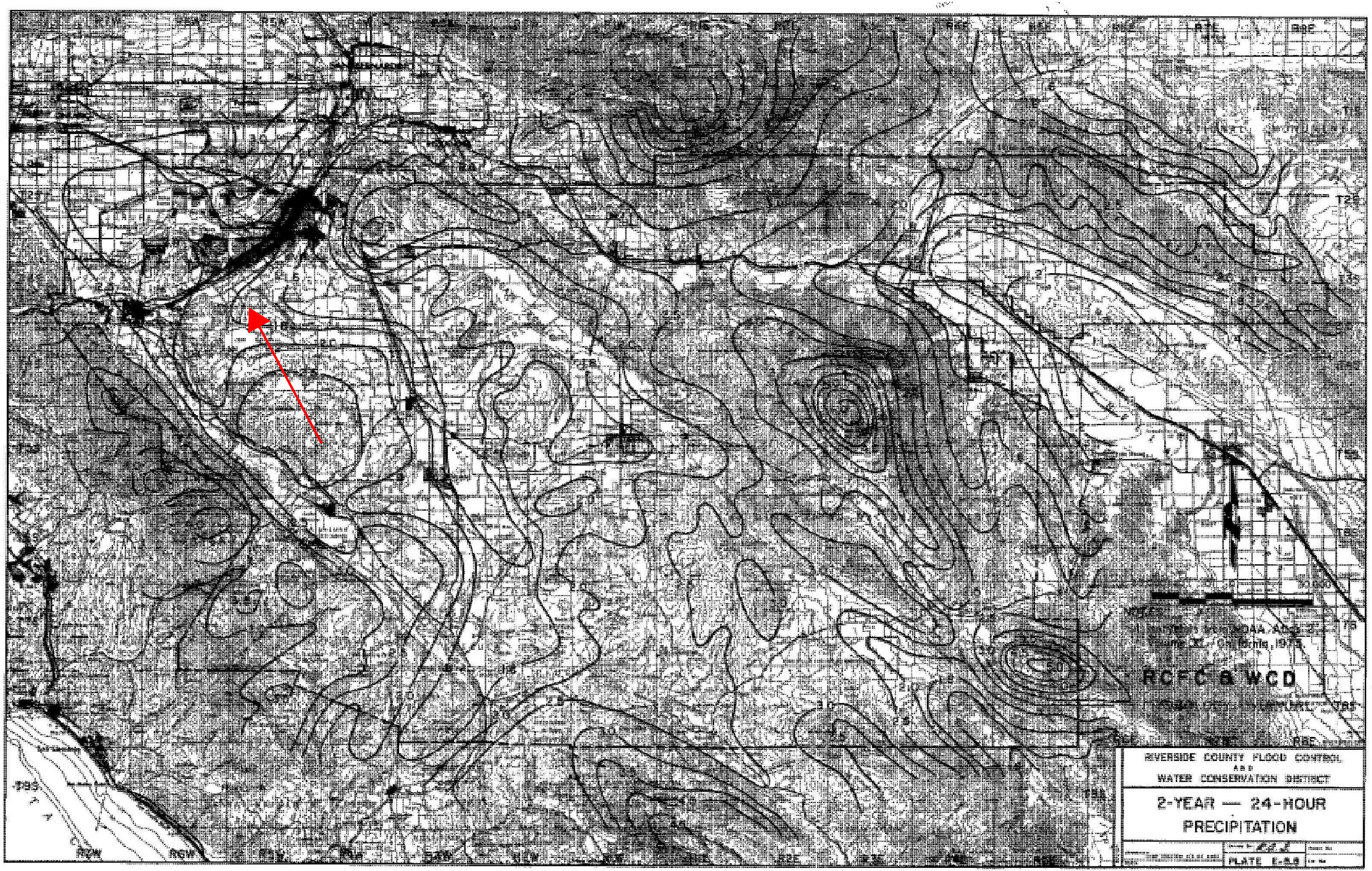
IMPERVIOUS COVER FOR DEVELOPED AREAS

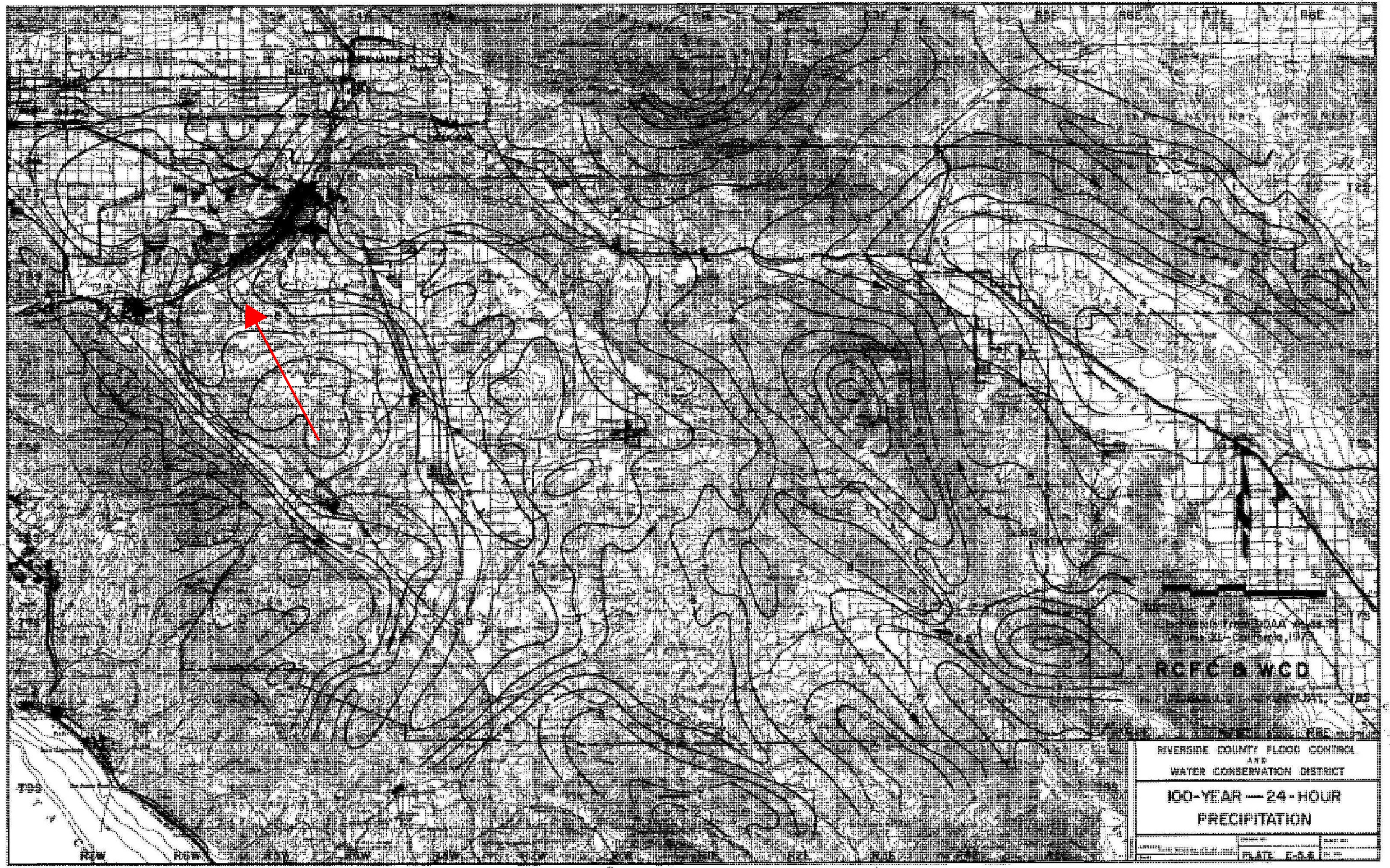
RUNOFF INDEX NUMBERS OF HYDROLOGIC SOIL-COVER COMPLEXES FOR PERVIOUS AREAS-AMC II

Cover Type (3)	Quality of Cover (2)	Soil Group A	B	C	D
NATURAL COVERS -					
Barren (Rockland, eroded and graded land)		78	86	91	93
Chaparrel, Broadleaf (Manzonita, ceanothus and scrub oak)	Poor	53	70	80	85
	Fair	40	63	75	81
	Good	31	57	71	78
Chaparrel, Narrowleaf (Chamise and redshank)	Poor	71	82	88	91
	Fair	55	72	81	86
Grass, Annual or Perennial	Poor	67	78	86	89
	Fair	50	69	79	84
	Good	38	61	74	80
Meadows or Cienegas (Areas with seasonally high water table, principal vegetation is sod forming grass)	Poor	63	77	85	88
	Fair	51	70	80	84
	Good	30	58	72	78
Open Brush (Soft wood shrubs - buckwheat, sage, etc.)	Poor	62	76	84	88
	Fair	46	66	77	83
	Good	41	63	75	81
Woodland (Coniferous or broadleaf trees predominate. Canopy density is at least 50 percent)	Poor	45	66	77	83
	Fair	36	60	73	79
	Good	28	55	70	77
Woodland, Grass (Coniferous or broadleaf trees with canopy density from 20 to 50 percent)	Poor	57	73	82	86
	Fair	44	65	77	82
	Good	33	58	72	79
URBAN COVERS -					
Residential or Commercial Landscaping (Lawn, shrubs, etc.)	Good	32	56	69	75
Turf (Irrigated and mowed grass)	Poor	58	74	83	87
	Fair	44	65	77	82
	Good	33	58	72	79
AGRICULTURAL COVERS -					
Fallow (Land plowed but not tilled or seeded)		76	85	90	92

RCFC & WCD
HYDROLOGY MANUAL

RUNOFF INDEX NUMBERS FOR PERVIOUS AREA


RCFC & WCD
RIVERSIDE COUNTY FLOOD CONTROL
AND
WATER CONSERVATION DISTRICT
2-YEAR — 24-HOUR
PRECIPITATION
PLATE E-5.6


RCFC & WCD
RIVERSIDE COUNTY FLOOD CONTROL
AND
WATER CONSERVATION DISTRICT
100-YEAR — 24-HOUR
PRECIPITATION
PLATE E-4.6

Appendix H – Basin Drawdown Routing

```
                    FLOOD HYDROGRAPH ROUTING PROGRAM
              Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                          Study date: 05/07/25
      ---------------------------------------------------------------------

      Program License Serial Number 5006

      ---------------------------------------------------------------------
      ********************** HYDROGRAPH INFORMATION **********************
                    From study/file name: 72hr.rte
      ********************** Hydrograph Information ***********************
                     From manual input hydrograph
      ****************************HYDROGRAPH DATA*****************************
                    Number of intervals =   432
                    Time interval =   10.0 (Min.)
                    Maximum/Peak flow rate =      127.013 (CFS)
                    Total volume =       1.749 (Ac.Ft)
             Status of hydrographs being held in storage
                       Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
             Peak (CFS)      0.000     0.000     0.000     0.000     0.000
             Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      *************************************************************************
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
      Process from Point/Station        1.000 to Point/Station        1.000
      **** RETARDING BASIN ROUTING ****
      _________________________________________________________________________
      User entry of depth-outflow-storage data
      ---------------------------------------------------------------------
      Total number of inflow hydrograph intervals = 432
      Hydrograph time unit = 10.000 (Min.)
      Initial depth in storage basin =   0.00(Ft.)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Initial basin depth =   0.00 (Ft.)
      Initial basin storage =      0.00 (Ac.Ft)
      Initial basin outflow =   0.00 (CFS)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Depth vs. Storage and Depth vs. Discharge data:
       Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
           (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
      ---------------------------------------------------------------------
         0.000      0.000      0.000      0.000        0.000
         1.000      0.276      0.133      0.275        0.277
         2.000      0.584      0.193      0.583        0.585
         3.000      0.930      0.700      0.925        0.935
         3.500      1.118      0.824      1.112        1.124
         4.000      1.316      0.930      1.310        1.322
         4.500      1.528      1.024      1.521        1.535
         4.750      1.637      1.068      1.630        1.644
         5.000      1.749     18.283      1.623        1.875
         6.000      2.231    253.655      0.484        3.978
      ---------------------------------------------------------------------
                      Hydrograph Detention Basin Routing
      ---------------------------------------------------------------------
      Graph values: 'I'= unit inflow; 'O'=outflow at time shown
      ---------------------------------------------------------------------
       Time   Inflow  Outflow    Storage                                  Depth
      (Hours)  (CFS)   (CFS)     (Ac.Ft) .0      31.8   63.51   95.26  127.01 (Ft.)
       0.167  127.01    0.61      0.871  O       |       |       |       I     2.83
       0.333    0.00    8.29      1.684  I O     |       |       |       |     4.85
       0.500    0.00    1.06      1.620  O       |       |       |       |     4.71
       0.667    0.00    1.06      1.605  O       |       |       |       |     4.68
       0.833    0.00    1.05      1.591  O       |       |       |       |     4.64
       1.000    0.00    1.04      1.576  O       |       |       |       |     4.61
       1.167    0.00    1.04      1.562  O       |       |       |       |     4.58
       1.333    0.00    1.03      1.548  O       |       |       |       |     4.54
       1.500    0.00    1.03      1.533  O       |       |       |       |     4.51
       1.667    0.00    1.02      1.519  O       |       |       |       |     4.48
       1.833    0.00    1.01      1.505  O       |       |       |       |     4.45
       2.000    0.00    1.01      1.491  O       |       |       |       |     4.41
       2.167    0.00    1.00      1.477  O       |       |       |       |     4.38
       2.333    0.00    1.00      1.464  O       |       |       |       |     4.35
       2.500    0.00    0.99      1.450  O       |       |       |       |     4.32
       2.667    0.00    0.98      1.436  O       |       |       |       |     4.28
       2.833    0.00    0.98      1.423  O       |       |       |       |     4.25
       3.000    0.00    0.97      1.410  O       |       |       |       |     4.22
       3.167    0.00    0.97      1.396  O       |       |       |       |     4.19
       3.333    0.00    0.96      1.383  O       |       |       |       |     4.16
       3.500    0.00    0.95      1.370  O       |       |       |       |     4.13
       3.667    0.00    0.95      1.357  O       |       |       |       |     4.10
       3.833    0.00    0.94      1.344  O       |       |       |       |     4.07
       4.000    0.00    0.94      1.331  O       |       |       |       |     4.03
       4.167    0.00    0.93      1.318  O       |       |       |       |     4.00
       4.333    0.00    0.92      1.305  O       |       |       |       |     3.97
       4.500    0.00    0.92      1.292  O       |       |       |       |     3.94
```

4.667	0.00	0.91	1.280	o					3.91
4.833	0.00	0.90	1.267	o					3.88
5.000	0.00	0.90	1.255	o					3.85
5.167	0.00	0.89	1.243	o					3.81
5.333	0.00	0.88	1.230	o					3.78
5.500	0.00	0.88	1.218	o					3.75
5.667	0.00	0.87	1.206	o					3.72
5.833	0.00	0.86	1.194	o					3.69
6.000	0.00	0.86	1.182	o					3.66
6.167	0.00	0.85	1.171	o					3.63
6.333	0.00	0.85	1.159	o					3.60
6.500	0.00	0.84	1.147	o					3.57
6.667	0.00	0.83	1.136	o					3.54
6.833	0.00	0.83	1.124	o					3.52
7.000	0.00	0.82	1.113	o					3.49
7.167	0.00	0.81	1.102	o					3.46
7.333	0.00	0.81	1.091	o					3.43
7.500	0.00	0.80	1.080	o					3.40
7.667	0.00	0.79	1.069	o					3.37
7.833	0.00	0.78	1.058	o					3.34
8.000	0.00	0.78	1.047	o					3.31
8.167	0.00	0.77	1.036	o					3.28
8.333	0.00	0.76	1.026	o					3.25
8.500	0.00	0.76	1.015	o					3.23
8.667	0.00	0.75	1.005	o					3.20
8.833	0.00	0.74	0.995	o					3.17
9.000	0.00	0.74	0.984	o					3.14
9.167	0.00	0.73	0.974	o					3.12
9.333	0.00	0.72	0.964	o					3.09
9.500	0.00	0.72	0.954	o					3.07
9.667	0.00	0.71	0.945	o					3.04
9.833	0.00	0.70	0.935	o					3.01
10.000	0.00	0.69	0.925	o					2.99
10.167	0.00	0.68	0.916	o					2.96
10.333	0.00	0.67	0.907	o					2.93
10.500	0.00	0.65	0.897	o					2.91
10.667	0.00	0.64	0.889	o					2.88
10.833	0.00	0.63	0.880	o					2.86
11.000	0.00	0.61	0.871	o					2.83
11.167	0.00	0.60	0.863	o					2.81
11.333	0.00	0.59	0.855	o					2.78
11.500	0.00	0.58	0.847	o					2.76
11.667	0.00	0.57	0.839	o					2.74
11.833	0.00	0.56	0.831	o					2.71
12.000	0.00	0.54	0.824	o					2.69
12.167	0.00	0.53	0.816	o					2.67
12.333	0.00	0.52	0.809	o					2.65
12.500	0.00	0.51	0.802	o					2.63
12.667	0.00	0.50	0.795	o					2.61
12.833	0.00	0.49	0.788	o					2.59
13.000	0.00	0.48	0.781	o					2.57
13.167	0.00	0.47	0.775	o					2.55
13.333	0.00	0.46	0.768	o					2.53
13.500	0.00	0.45	0.762	o					2.51
13.667	0.00	0.44	0.756	o					2.50
13.833	0.00	0.44	0.750	o					2.48
14.000	0.00	0.43	0.744	o					2.46
14.167	0.00	0.42	0.738	o					2.44
14.333	0.00	0.41	0.732	o					2.43
14.500	0.00	0.40	0.727	o					2.41
14.667	0.00	0.39	0.721	o					2.40
14.833	0.00	0.39	0.716	o					2.38
15.000	0.00	0.38	0.710	o					2.37
15.167	0.00	0.37	0.705	o					2.35
15.333	0.00	0.36	0.700	o					2.34
15.500	0.00	0.36	0.695	o					2.32
15.667	0.00	0.35	0.690	o					2.31
15.833	0.00	0.34	0.686	o					2.29
16.000	0.00	0.34	0.681	o					2.28
16.167	0.00	0.33	0.676	o					2.27
16.333	0.00	0.32	0.672	o					2.25
16.500	0.00	0.32	0.668	o					2.24
16.667	0.00	0.31	0.663	o					2.23
16.833	0.00	0.30	0.659	o					2.22
17.000	0.00	0.30	0.655	o					2.20
17.167	0.00	0.29	0.651	o					2.19
17.333	0.00	0.29	0.647	o					2.18
17.500	0.00	0.28	0.643	o					2.17
17.667	0.00	0.27	0.639	o					2.16
17.833	0.00	0.27	0.635	o					2.15
18.000	0.00	0.26	0.632	o					2.14
18.167	0.00	0.26	0.628	o					2.13
18.333	0.00	0.25	0.625	o					2.12
18.500	0.00	0.25	0.621	o					2.11
18.667	0.00	0.24	0.618	o					2.10
18.833	0.00	0.24	0.615	o					2.09

19.000	0.00	0.23	0.611	o				2.08
19.167	0.00	0.23	0.608	o				2.07
19.333	0.00	0.22	0.605	o				2.06
19.500	0.00	0.22	0.602	o				2.05
19.667	0.00	0.21	0.599	o				2.04
19.833	0.00	0.21	0.596	o				2.03
20.000	0.00	0.21	0.593	o				2.03
20.167	0.00	0.20	0.590	o				2.02
20.333	0.00	0.20	0.588	o				2.01
20.500	0.00	0.19	0.585	o				2.00
20.667	0.00	0.19	0.582	o				1.99
20.833	0.00	0.19	0.580	o				1.99
21.000	0.00	0.19	0.577	o				1.98
21.167	0.00	0.19	0.574	o				1.97
21.333	0.00	0.19	0.572	o				1.96
21.500	0.00	0.19	0.569	o				1.95
21.667	0.00	0.19	0.566	o				1.94
21.833	0.00	0.19	0.564	o				1.93
22.000	0.00	0.19	0.561	o				1.93
22.167	0.00	0.19	0.559	o				1.92
22.333	0.00	0.19	0.556	o				1.91
22.500	0.00	0.19	0.553	o				1.90
22.667	0.00	0.19	0.551	o				1.89
22.833	0.00	0.19	0.548	o				1.88
23.000	0.00	0.19	0.546	o				1.88
23.167	0.00	0.19	0.543	o				1.87
23.333	0.00	0.18	0.541	o				1.86
23.500	0.00	0.18	0.538	o				1.85
23.667	0.00	0.18	0.536	o				1.84
23.833	0.00	0.18	0.533	o				1.83
24.000	0.00	0.18	0.531	o				1.83
24.167	0.00	0.18	0.528	o				1.82
24.333	0.00	0.18	0.526	o				1.81
24.500	0.00	0.18	0.523	o				1.80
24.667	0.00	0.18	0.521	o				1.79
24.833	0.00	0.18	0.518	o				1.79
25.000	0.00	0.18	0.516	o				1.78
25.167	0.00	0.18	0.513	o				1.77
25.333	0.00	0.18	0.511	o				1.76
25.500	0.00	0.18	0.508	o				1.75
25.667	0.00	0.18	0.506	o				1.75
25.833	0.00	0.18	0.503	o				1.74
26.000	0.00	0.18	0.501	o				1.73
26.167	0.00	0.18	0.498	o				1.72
26.333	0.00	0.18	0.496	o				1.71
26.500	0.00	0.18	0.494	o				1.71
26.667	0.00	0.17	0.491	o				1.70
26.833	0.00	0.17	0.489	o				1.69
27.000	0.00	0.17	0.486	o				1.68
27.167	0.00	0.17	0.484	o				1.68
27.333	0.00	0.17	0.482	o				1.67
27.500	0.00	0.17	0.479	o				1.66
27.667	0.00	0.17	0.477	o				1.65
27.833	0.00	0.17	0.474	o				1.64
28.000	0.00	0.17	0.472	o				1.64
28.167	0.00	0.17	0.470	o				1.63
28.333	0.00	0.17	0.467	o				1.62
28.500	0.00	0.17	0.465	o				1.61
28.667	0.00	0.17	0.463	o				1.61
28.833	0.00	0.17	0.460	o				1.60
29.000	0.00	0.17	0.458	o				1.59
29.167	0.00	0.17	0.456	o				1.58
29.333	0.00	0.17	0.453	o				1.58
29.500	0.00	0.17	0.451	o				1.57
29.667	0.00	0.17	0.449	o				1.56
29.833	0.00	0.17	0.447	o				1.55
30.000	0.00	0.17	0.444	o				1.55
30.167	0.00	0.17	0.442	o				1.54
30.333	0.00	0.16	0.440	o				1.53
30.500	0.00	0.16	0.437	o				1.52
30.667	0.00	0.16	0.435	o				1.52
30.833	0.00	0.16	0.433	o				1.51
31.000	0.00	0.16	0.431	o				1.50
31.167	0.00	0.16	0.428	o				1.49
31.333	0.00	0.16	0.426	o				1.49
31.500	0.00	0.16	0.424	o				1.48
31.667	0.00	0.16	0.422	o				1.47
31.833	0.00	0.16	0.420	o				1.47
32.000	0.00	0.16	0.417	o				1.46
32.167	0.00	0.16	0.415	o				1.45
32.333	0.00	0.16	0.413	o				1.44
32.500	0.00	0.16	0.411	o				1.44
32.667	0.00	0.16	0.409	o				1.43
32.833	0.00	0.16	0.406	o				1.42
33.000	0.00	0.16	0.404	o				1.42
33.167	0.00	0.16	0.402	o				1.41

33.333	0.00	0.16	0.400	o	|	|	|	1.40
33.500	0.00	0.16	0.398	o	|	|	|	1.39
33.667	0.00	0.16	0.395	o	|	|	|	1.39
33.833	0.00	0.16	0.393	o	|	|	|	1.38
34.000	0.00	0.16	0.391	o	|	|	|	1.37
34.167	0.00	0.16	0.389	o	|	|	|	1.37
34.333	0.00	0.15	0.387	o	|	|	|	1.36
34.500	0.00	0.15	0.385	o	|	|	|	1.35
34.667	0.00	0.15	0.383	o	|	|	|	1.35
34.833	0.00	0.15	0.381	o	|	|	|	1.34
35.000	0.00	0.15	0.378	o	|	|	|	1.33
35.167	0.00	0.15	0.376	o	|	|	|	1.33
35.333	0.00	0.15	0.374	o	|	|	|	1.32
35.500	0.00	0.15	0.372	o	|	|	|	1.31
35.667	0.00	0.15	0.370	o	|	|	|	1.31
35.833	0.00	0.15	0.368	o	|	|	|	1.30
36.000	0.00	0.15	0.366	o	|	|	|	1.29
36.167	0.00	0.15	0.364	o	|	|	|	1.29
36.333	0.00	0.15	0.362	o	|	|	|	1.28
36.500	0.00	0.15	0.360	o	|	|	|	1.27
36.667	0.00	0.15	0.358	o	|	|	|	1.27
36.833	0.00	0.15	0.356	o	|	|	|	1.26
37.000	0.00	0.15	0.354	o	|	|	|	1.25
37.167	0.00	0.15	0.352	o	|	|	|	1.25
37.333	0.00	0.15	0.349	o	|	|	|	1.24
37.500	0.00	0.15	0.347	o	|	|	|	1.23
37.667	0.00	0.15	0.345	o	|	|	|	1.23
37.833	0.00	0.15	0.343	o	|	|	|	1.22
38.000	0.00	0.15	0.341	o	|	|	|	1.21
38.167	0.00	0.15	0.339	o	|	|	|	1.21
38.333	0.00	0.14	0.337	o	|	|	|	1.20
38.500	0.00	0.14	0.335	o	|	|	|	1.19
38.667	0.00	0.14	0.333	o	|	|	|	1.19
38.833	0.00	0.14	0.331	o	|	|	|	1.18
39.000	0.00	0.14	0.329	o	|	|	|	1.17
39.167	0.00	0.14	0.328	o	|	|	|	1.17
39.333	0.00	0.14	0.326	o	|	|	|	1.16
39.500	0.00	0.14	0.324	o	|	|	|	1.15
39.667	0.00	0.14	0.322	o	|	|	|	1.15
39.833	0.00	0.14	0.320	o	|	|	|	1.14
40.000	0.00	0.14	0.318	o	|	|	|	1.14
40.167	0.00	0.14	0.316	o	|	|	|	1.13
40.333	0.00	0.14	0.314	o	|	|	|	1.12
40.500	0.00	0.14	0.312	o	|	|	|	1.12
40.667	0.00	0.14	0.310	o	|	|	|	1.11
40.833	0.00	0.14	0.308	o	|	|	|	1.10
41.000	0.00	0.14	0.306	o	|	|	|	1.10
41.167	0.00	0.14	0.304	o	|	|	|	1.09
41.333	0.00	0.14	0.302	o	|	|	|	1.09
41.500	0.00	0.14	0.300	o	|	|	|	1.08
41.667	0.00	0.14	0.299	o	|	|	|	1.07
41.833	0.00	0.14	0.297	o	|	|	|	1.07
42.000	0.00	0.14	0.295	o	|	|	|	1.06
42.167	0.00	0.14	0.293	o	|	|	|	1.05
42.333	0.00	0.14	0.291	o	|	|	|	1.05
42.500	0.00	0.14	0.289	o	|	|	|	1.04
42.667	0.00	0.14	0.287	o	|	|	|	1.04
42.833	0.00	0.13	0.285	o	|	|	|	1.03
43.000	0.00	0.13	0.284	o	|	|	|	1.02
43.167	0.00	0.13	0.282	o	|	|	|	1.02
43.333	0.00	0.13	0.280	o	|	|	|	1.01
43.500	0.00	0.13	0.278	o	|	|	|	1.01
43.667	0.00	0.13	0.276	o	|	|	|	1.00
43.833	0.00	0.13	0.274	o	|	|	|	0.99
44.000	0.00	0.13	0.273	o	|	|	|	0.99
44.167	0.00	0.13	0.271	o	|	|	|	0.98
44.333	0.00	0.13	0.269	o	|	|	|	0.97
44.500	0.00	0.13	0.267	o	|	|	|	0.97
44.667	0.00	0.13	0.265	o	|	|	|	0.96
44.833	0.00	0.13	0.264	o	|	|	|	0.96
45.000	0.00	0.13	0.262	o	|	|	|	0.95
45.167	0.00	0.13	0.260	o	|	|	|	0.94
45.333	0.00	0.12	0.258	o	|	|	|	0.94
45.500	0.00	0.12	0.257	o	|	|	|	0.93
45.667	0.00	0.12	0.255	o	|	|	|	0.92
45.833	0.00	0.12	0.253	o	|	|	|	0.92
46.000	0.00	0.12	0.252	o	|	|	|	0.91
46.167	0.00	0.12	0.250	o	|	|	|	0.91
46.333	0.00	0.12	0.248	o	|	|	|	0.90
46.500	0.00	0.12	0.247	o	|	|	|	0.89
46.667	0.00	0.12	0.245	o	|	|	|	0.89
46.833	0.00	0.12	0.243	o	|	|	|	0.88
47.000	0.00	0.12	0.242	o	|	|	|	0.88
47.167	0.00	0.12	0.240	o	|	|	|	0.87
47.333	0.00	0.12	0.239	o	|	|	|	0.86
47.500	0.00	0.11	0.237	o	|	|	|	0.86

47.667	0.00	0.11	0.236	o	|	|	|	0.85
47.833	0.00	0.11	0.234	o	|	|	|	0.85
48.000	0.00	0.11	0.232	o	|	|	|	0.84
48.167	0.00	0.11	0.231	o	|	|	|	0.84
48.333	0.00	0.11	0.229	o	|	|	|	0.83
48.500	0.00	0.11	0.228	o	|	|	|	0.83
48.667	0.00	0.11	0.226	o	|	|	|	0.82
48.833	0.00	0.11	0.225	o	|	|	|	0.81
49.000	0.00	0.11	0.223	o	|	|	|	0.81
49.167	0.00	0.11	0.222	o	|	|	|	0.80
49.333	0.00	0.11	0.220	o	|	|	|	0.80
49.500	0.00	0.11	0.219	o	|	|	|	0.79
49.667	0.00	0.10	0.217	o	|	|	|	0.79
49.833	0.00	0.10	0.216	o	|	|	|	0.78
50.000	0.00	0.10	0.215	o	|	|	|	0.78
50.167	0.00	0.10	0.213	o	|	|	|	0.77
50.333	0.00	0.10	0.212	o	|	|	|	0.77
50.500	0.00	0.10	0.210	o	|	|	|	0.76
50.667	0.00	0.10	0.209	o	|	|	|	0.76
50.833	0.00	0.10	0.208	o	|	|	|	0.75
51.000	0.00	0.10	0.206	o	|	|	|	0.75
51.167	0.00	0.10	0.205	o	|	|	|	0.74
51.333	0.00	0.10	0.204	o	|	|	|	0.74
51.500	0.00	0.10	0.202	o	|	|	|	0.73
51.667	0.00	0.10	0.201	o	|	|	|	0.73
51.833	0.00	0.10	0.200	o	|	|	|	0.72
52.000	0.00	0.10	0.198	o	|	|	|	0.72
52.167	0.00	0.09	0.197	o	|	|	|	0.71
52.333	0.00	0.09	0.196	o	|	|	|	0.71
52.500	0.00	0.09	0.194	o	|	|	|	0.70
52.667	0.00	0.09	0.193	o	|	|	|	0.70
52.833	0.00	0.09	0.192	o	|	|	|	0.69
53.000	0.00	0.09	0.190	o	|	|	|	0.69
53.167	0.00	0.09	0.189	o	|	|	|	0.69
53.333	0.00	0.09	0.188	o	|	|	|	0.68
53.500	0.00	0.09	0.187	o	|	|	|	0.68
53.667	0.00	0.09	0.185	o	|	|	|	0.67
53.833	0.00	0.09	0.184	o	|	|	|	0.67
54.000	0.00	0.09	0.183	o	|	|	|	0.66
54.167	0.00	0.09	0.182	o	|	|	|	0.66
54.333	0.00	0.09	0.181	o	|	|	|	0.65
54.500	0.00	0.09	0.179	o	|	|	|	0.65
54.667	0.00	0.09	0.178	o	|	|	|	0.65
54.833	0.00	0.09	0.177	o	|	|	|	0.64
55.000	0.00	0.08	0.176	o	|	|	|	0.64
55.167	0.00	0.08	0.175	o	|	|	|	0.63
55.333	0.00	0.08	0.174	o	|	|	|	0.63
55.500	0.00	0.08	0.172	o	|	|	|	0.62
55.667	0.00	0.08	0.171	o	|	|	|	0.62
55.833	0.00	0.08	0.170	o	|	|	|	0.62
56.000	0.00	0.08	0.169	o	|	|	|	0.61
56.167	0.00	0.08	0.168	o	|	|	|	0.61
56.333	0.00	0.08	0.167	o	|	|	|	0.60
56.500	0.00	0.08	0.166	o	|	|	|	0.60
56.667	0.00	0.08	0.165	o	|	|	|	0.60
56.833	0.00	0.08	0.163	o	|	|	|	0.59
57.000	0.00	0.08	0.162	o	|	|	|	0.59
57.167	0.00	0.08	0.161	o	|	|	|	0.58
57.333	0.00	0.08	0.160	o	|	|	|	0.58
57.500	0.00	0.08	0.159	o	|	|	|	0.58
57.667	0.00	0.08	0.158	o	|	|	|	0.57
57.833	0.00	0.08	0.157	o	|	|	|	0.57
58.000	0.00	0.08	0.156	o	|	|	|	0.57
58.167	0.00	0.07	0.155	o	|	|	|	0.56
58.333	0.00	0.07	0.154	o	|	|	|	0.56
58.500	0.00	0.07	0.153	o	|	|	|	0.55
58.667	0.00	0.07	0.152	o	|	|	|	0.55
58.833	0.00	0.07	0.151	o	|	|	|	0.55
59.000	0.00	0.07	0.150	o	|	|	|	0.54
59.167	0.00	0.07	0.149	o	|	|	|	0.54
59.333	0.00	0.07	0.148	o	|	|	|	0.54
59.500	0.00	0.07	0.147	o	|	|	|	0.53
59.667	0.00	0.07	0.146	o	|	|	|	0.53
59.833	0.00	0.07	0.145	o	|	|	|	0.53
60.000	0.00	0.07	0.144	o	|	|	|	0.52
60.167	0.00	0.07	0.143	o	|	|	|	0.52
60.333	0.00	0.07	0.142	o	|	|	|	0.52
60.500	0.00	0.07	0.141	o	|	|	|	0.51
60.667	0.00	0.07	0.140	o	|	|	|	0.51
60.833	0.00	0.07	0.139	o	|	|	|	0.51
61.000	0.00	0.07	0.138	o	|	|	|	0.50
61.167	0.00	0.07	0.138	o	|	|	|	0.50
61.333	0.00	0.07	0.137	o	|	|	|	0.50
61.500	0.00	0.07	0.136	o	|	|	|	0.49
61.667	0.00	0.06	0.135	o	|	|	|	0.49
61.833	0.00	0.06	0.134	o	|	|	|	0.49

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62.000    0.00    0.06      0.133  o       |       |       |       |      0.48
62.167    0.00    0.06      0.132  o       |       |       |       |      0.48
62.333    0.00    0.06      0.131  o       |       |       |       |      0.48
62.500    0.00    0.06      0.130  o       |       |       |       |      0.47
62.667    0.00    0.06      0.130  o       |       |       |       |      0.47
62.833    0.00    0.06      0.129  o       |       |       |       |      0.47
63.000    0.00    0.06      0.128  o       |       |       |       |      0.46
63.167    0.00    0.06      0.127  o       |       |       |       |      0.46
63.333    0.00    0.06      0.126  o       |       |       |       |      0.46
63.500    0.00    0.06      0.125  o       |       |       |       |      0.45
63.667    0.00    0.06      0.125  o       |       |       |       |      0.45
63.833    0.00    0.06      0.124  o       |       |       |       |      0.45
64.000    0.00    0.06      0.123  o       |       |       |       |      0.45
64.167    0.00    0.06      0.122  o       |       |       |       |      0.44
64.333    0.00    0.06      0.121  o       |       |       |       |      0.44
64.500    0.00    0.06      0.120  o       |       |       |       |      0.44
64.667    0.00    0.06      0.120  o       |       |       |       |      0.43
64.833    0.00    0.06      0.119  o       |       |       |       |      0.43
65.000    0.00    0.06      0.118  o       |       |       |       |      0.43
65.167    0.00    0.06      0.117  o       |       |       |       |      0.43
65.333    0.00    0.06      0.117  o       |       |       |       |      0.42
65.500    0.00    0.06      0.116  o       |       |       |       |      0.42
65.667    0.00    0.06      0.115  o       |       |       |       |      0.42
65.833    0.00    0.06      0.114  o       |       |       |       |      0.41
66.000    0.00    0.05      0.113  o       |       |       |       |      0.41
66.167    0.00    0.05      0.113  o       |       |       |       |      0.41
66.333    0.00    0.05      0.112  o       |       |       |       |      0.41
66.500    0.00    0.05      0.111  o       |       |       |       |      0.40
66.667    0.00    0.05      0.111  o       |       |       |       |      0.40
66.833    0.00    0.05      0.110  o       |       |       |       |      0.40
67.000    0.00    0.05      0.109  o       |       |       |       |      0.40
67.167    0.00    0.05      0.108  o       |       |       |       |      0.39
67.333    0.00    0.05      0.108  o       |       |       |       |      0.39
67.500    0.00    0.05      0.107  o       |       |       |       |      0.39
67.667    0.00    0.05      0.106  o       |       |       |       |      0.38
67.833    0.00    0.05      0.105  o       |       |       |       |      0.38
68.000    0.00    0.05      0.105  o       |       |       |       |      0.38
68.167    0.00    0.05      0.104  o       |       |       |       |      0.38
68.333    0.00    0.05      0.103  o       |       |       |       |      0.37
68.500    0.00    0.05      0.103  o       |       |       |       |      0.37
68.667    0.00    0.05      0.102  o       |       |       |       |      0.37
68.833    0.00    0.05      0.101  o       |       |       |       |      0.37
69.000    0.00    0.05      0.101  o       |       |       |       |      0.36
69.167    0.00    0.05      0.100  o       |       |       |       |      0.36
69.333    0.00    0.05      0.099  o       |       |       |       |      0.36
69.500    0.00    0.05      0.099  o       |       |       |       |      0.36
69.667    0.00    0.05      0.098  o       |       |       |       |      0.36
69.833    0.00    0.05      0.097  o       |       |       |       |      0.35
70.000    0.00    0.05      0.097  o       |       |       |       |      0.35
70.167    0.00    0.05      0.096  o       |       |       |       |      0.35
70.333    0.00    0.05      0.095  o       |       |       |       |      0.35
70.500    0.00    0.05      0.095  o       |       |       |       |      0.34
70.667    0.00    0.05      0.094  o       |       |       |       |      0.34
70.833    0.00    0.05      0.094  o       |       |       |       |      0.34
71.000    0.00    0.04      0.093  o       |       |       |       |      0.34
71.167    0.00    0.04      0.092  o       |       |       |       |      0.33
71.333    0.00    0.04      0.092  o       |       |       |       |      0.33
71.500    0.00    0.04      0.091  o       |       |       |       |      0.33
71.667    0.00    0.04      0.091  o       |       |       |       |      0.33
71.833    0.00    0.04      0.090  o       |       |       |       |      0.33
72.000    0.00    0.04      0.089  o       |       |       |       |      0.32
72.167    0.00    0.04      0.089  o       |       |       |       |      0.32
      Remaining water in basin =    0.09 (Ac.Ft)

      ****************************HYDROGRAPH DATA****************************
                Number of intervals =   433
                Time interval =   10.0 (Min.)
                Maximum/Peak flow rate =        8.287 (CFS)
                Total volume =       1.661 (Ac.Ft)
          Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
          Peak (CFS)      0.000     0.000     0.000     0.000     0.000
          Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
      ************************************************************************
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