Technical Memorandum

Date: **March 19, 2024 (Revised 3/14/2025; 7/21/2025)**

To: **Dilesh Sheth, PE/TE**

From: **Joseph L. Castaneda, P.E.**

Re: **Avenue 50 Street Hydrology in support of proposed Street Improvements**

Overview

JLC Engineering has evaluated the hydrologic conditions of Avenue 50 between Jefferson street and Madison Street in Indio, Ca, see Figure 1. The hydrologic assessment was restricted to the area within the Right of Way (R/W) boundaries on either side of Avenue 50. A boundary was drawn along the Avenue 50 centerline to distinguish the flow on the east bound and west bound sides of Avenue 50. The hydrologic assessment has been executed to determine the influence of proposed improvements along Avenue 50 which will alter the amount of impervious area and thus influence runoff within the street R/W.

By necessity, inflows from adjacent properties or intersections were ignored to determine only the change in magnitude of the runoff generated within Avenue 50 due to the proposed Avenue 50 street improvements. The nature of the existing flow patterns would otherwise yield a major regional study if all tributary inflows were included, which would not be feasible for this project.

Hydrology Analysis

The 100-year rational method was completed for the eastbound and westbound portions of Avenue 50 between Jefferson Street and Madison Street, see Exhibit A. Soil data was obtained from the NRCS Websoil Survey; the soil data illustrates that all subareas are classified by hydrologic soil types A and B, see Figure 2. Subareas were delineated based on identified low points within Avenue 50 or the boundary of the proposed improvements.

Impervious fraction was determined by measuring the paved areas of the streets in the existing and proposed conditions. Impervious fractions were determined for each sub

area. Modeling was completed using the CivilD program in compliance with the Riverside County Flood Control & Water Conservation District (RCFC & WCD) Hydrology Manual. The impervious fractions were calculated for each subarea; however, this input is not enabled in the CivilD program. As a result, the land classifications, with predefined impervious fractions, were picked based on the nearest representative impervious fraction value. For example, if a subarea was found to have an impervious fraction of 0.88 then the "Commercial" land use was selected since it has a predetermined impervious fraction of 0.90 and is most representative of the computed impervious fraction.

The unit hydrograph method was also used to study the same areas for a 100-year return period for a 24-hour duration. Since the unit hydrograph program in CivilD allows direct entry of impervious fraction, the computed impervious fraction for each area was used. Due to the elongated half street areas that were drawn, the centroidal length was assumed to be half of the flow path length. All runoff index values used were defined by the corresponding rational method output. Please note that this is simply the "Urban" cover Runoff Index value defined in the RCFC &WCD Hydrology Manual and only varies by soil type for each area.

Rainfall data was obtained from NOAA Atlas 14, see Attachment 1.

RAINFALL DATA			
		Year	
		2	*100*
Duration	*1*	0.352"	1.45"
	3	0.554"	2.14"
	6	0.726"	2.75"
	24	1.16"	4.44"

Increased Runoff Mitigation

Increased runoff mitigation criteria was selected to be the storage/infiltration of the post-project 100-year, 24-hour hydrograph resulting from the unit hydrograph method. Therefore, assuming 100% capture of the 100-year, 24-hour hydrograph, a subsurface basin was sized for each area based on the following requirements:

1. Infiltration rate within the basin was utilized to compute a basin outflow based on an assumed length (given a constant, transverse cross section). An assumed basin size enabled the determination of a flowrate given the infiltration rate since $Q_{infiltration}$ = Infiltration Rate * Basin Bottom Area over a 24-hour period.
2. The 100-year, 24-hour hydrograph was modified to account for the losses due to infiltration outflow from the subsurface basin at every time step.
3. The remaining hydrograph volume was assumed to be stored.

4. Assumed length of the subsurface basin was iterated until it yielded a basin with sufficient storage for the hydrograph volume remainder after infiltration.

Note that the representative infiltration rate in Avenue 50 was determined to be 4.8 in/hr based on infiltration testing and guidance from the City. The sizing was based on the average infiltration rate per the table below which documents the infiltration rates from the report prepared by Geocon. The City deemed using the in-situ infiltration rate with a safety factor of 3 was acceptable for sizing the subsurface systems. Based on the safety factor of 3, an effective infiltration rate of approximately 1.6 in/hr for subsurface basin sizing was utilized. The resulting subsurface basin lengths can be found in Attachment 3.

Test Number	Infiltration Rate (in/hr)	Depth of Test (inches)
P1	2.4	120
P2	6.3	120
P3	2.4	120
P4	4.3	120
P5	5.9	120
P6	7.1	120
P7	5.2	120
P8(1)	20.4	120
Average Infiltration Rate (in/hr)	**4.8**	
Infiltration Rate with Safety Factor=3 (in/hr)	**1.6**	

(1) Test P8 was omitted from average since it was significantly greater than other tests. This was discussed with the City.

A conceptual subsurface basin cross section is shown in Figure 3. The subsurface basin was assumed to have a pipe with an internal diameter of 5 ft and outer diameter of 5.525 ft. The gravel fill around the proposed pipe was assumed to have a porosity of 0.4. The width was assumed to be 7.58 ft. The internal and external pipe diameters were used to exclude the loss of storage volume due to the pipe thickness. Additionally, stage storage tables were provided for each subsurface system. Basin routing analyses were done for each subsurface basin using the Modified Puls Method to validate the size of the facility. The design goal is to ensure that the ponded depth does not exceed 7.58 feet which is the maximum allowable depth based on Figure 3

The basin routing analysis demonstrates that the 100-year, 24-hour storm event volume that is captured by the proposed subsurface basins will drawdown within 72 hours. Drawdown time is measured from the end of a storm event since this is when the potential for vector issues arises. The routing analysis shows that subsurface basins will be empty at approximately 60 hours from the start of the 24-hour storm event for each of the proposed basins. This indicates that the drawdown time is less than or equal to 36 hours for each proposed basin; therefore, the proposed basins comply with acceptable drawdown time requirements.

Ten catch basins have been located within Avenue 50 to capture the surface runoff and convey flows to the proposed subsurface basins for storage and infiltration. Each watershed subarea within Avenue 50: Areas A1, AA1, B1, BB1, C1, CC1, D1, DD1, E1, and EE1 contain a single catch basin in a sump condition and subsurface basin to capture and mitigate increased stormwater runoff. The ten catch basins have been sized to intercept their tributary 100-year flow rate which was defined using the rational method. Areas A1, AA1, B1, BB1, C1, CC1, D1, DD1, E1, and EE1 contain sump catch basins Catch basins were sized to intercept 100% of the 100-year tributary flow rate. The proposed curb and gutter include 6 inch curbs (0.5ft); catch basins were sized so that the flow depth was less than the curb height. FlowMaster calculations have been included in the attachments. The table below summarizes the proposed catch basins.

Subarea	CB Type	Q_{100} (cfs)	Width (ft)	Q_{INT} (cfs)	Q_{BYP} (cfs)	Depth (ft)
A1	Sump	3.9	4	3.9	-	0.4
AA1	Sump	3.7	4	3.7	-	0.39
B1	Sump	4	4	4	-	0.41
BB1	Sump	3.8	4	3.8	-	0.4
C1	Sump	2.4	4	2.4	-	0.32
CC1	Sump	2.4	4	2.4	-	0.32
D1	Sump	4.5	4	4.5	-	0.43
DD1	Sump	4.2	4	4.2	-	0.42
E1	Sump	1.9	4	1.9	-	0.29
EE1	Sump	1.8	4	1.8	-	0.29

Areas F and FF1 characterize area along Avenue 50 that is tributary to the intersection of Avenue 50 and Madison Street. Improvements are only proposed in a very small portion of these areas just passed the streets highpoint. The 100 year flow rate tributary to the intersection has been computed in the hydrology analysis using the rational method for reference. Note that there is an insignificant increase in the impervious area for these areas and no catch basins or subsurface systems have been proposed here as a result.

Conclusion

In conclusion, the areas containing the proposed street improvements were evaluated hydrologically using the rational method and unit hydrograph methods based on the RCFC&WCD Hydrology Manual. The unit hydrograph was assessed for the 100-year, 24-hour event based on the selected increased runoff mitigation criteria. The rational method was completed for the 100-year. The flow for each subarea has been demonstrated to be 100% captured by proposed catch basins in each area. The catch basins have been confirmed to have adequate size to ensure 100% capture. The catch basins are designed to convey surface runoff to subsurface basins which outflow via

infiltration. The subsurface basins have been shown to have adequate storage capacity to fully contain the 100-year, 24-hour storm event for each subarea. Drawdown time for each basin has been shown to be less than or equal to 36 hours which is compliant with drawdown time requirements (less than 72 hours). The basin routing calculations demonstrate containment by showing that the maximum ponded depth does not exceed the top of basin. Each basin has a maximum allowable ponded depth of 7.58 ft. Basin routing shows that the 100-year, 24-hour event ponds less than 7.58 ft for all proposed basins. The results of the routing analyses have been included in the table below:

Basin Routing Results for Subsurface Systems

Subarea	A1	AA1	B1	BB1	C1	CC1
Drainage Area (acres)	1.28	1.23	1.47	1.47	0.74	0.77
100 Yr, 24 hr Volume (ft^3)	16,583	15,561	19,088	18,372	9,722	8,759
Volume Infiltrated (ft^3)	6,351	5,957	7,309	7,034	3,718	3,349
Recommended Length of System (ft)	315	295	360	350	185	170
Storage Volume (ft^3)	10,403	9,743	11,889	11,559	6,110	5,614
Maximum Ponded Depth Allowed (ft)	7.58	7.58	7.58	7.58	7.58	7.58
Basin Routing Ponded Depth w/in Subsurface Storage System (ft)	7.27	7.26	7.45	7.30	6.58	6.56
Basin Routing Volume Drawdown Time (hours)	34	34	35	35	32	31

Subarea	D1	DD1	E1	EE1
Drainage Area (acres)	1.68	1.70	0.55	0.55
100 Yr, 24 hr Volume (ft^3)	21,931	20,294	7,181	6,827
Volume Infiltrated (ft^3)	8,409	7,780	2,750	2,614
Recommended Length of System (ft)	415	385	140	135
Storage Volume (ft^3)	13,706	12,715	4,623	4,458
Maximum Ponded Depth Allowed (ft)	7.58	7.58	7.58	7.58
Basin Routing Ponded Depth w/in Subsurface Storage System (ft)	7.44	7.37	6.34	6.12
Basin Routing Volume Drawdown Time (hours)	36	35	30	29

Figures

1. Vicinity Map
2. Soils Map
3. Typical Subsurface Basin Cross Section

Attachments

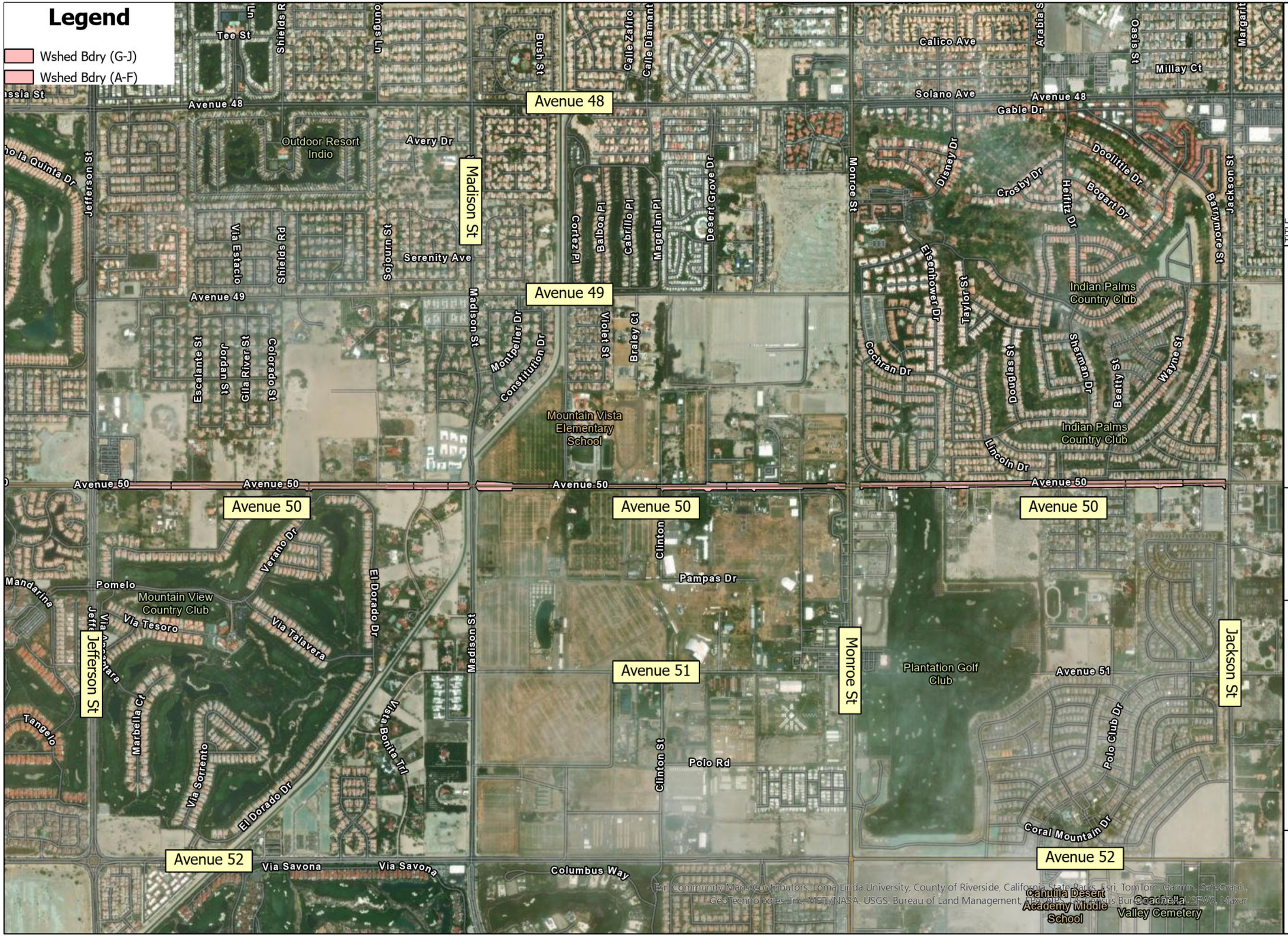
1. NOAA Atlas 14 Rainfall Output
2. Impervious Fraction Table / Hydrology Table
3. Rational Method Output Files
4. Catch Basin FlowMaster Calculations
5. Unit Hydrograph Output Files
6. Subsurface Stage Storage Calculations
7. Infiltration Rate Calculation
8. Infiltration Rate by Basin
9. Stage-Storage-Outflow Tables
10. Infiltration Routing for Drainage Areas

Exhibits

1. Street Hydrology Map

FIGURES

FIGURE 1 – VICINITY MAP



VICINITY MAP

TITLE

PROJECT
AVENUE 50
STREET HYDROLOGY
INDIO, CA

SCALE 1:15,000

DATE 3/20/24

FILE NAME:

JLC Engineering & Consulting, Inc.
MURRIETA, CA 92562
Office 951.304.9552 Fax 951.304.3568

FIGURE
1

FIGURE 2 – SOILS MAP

Figure 2

Hydrologic Soil Group—Riverside County, Coachella Valley Area, California

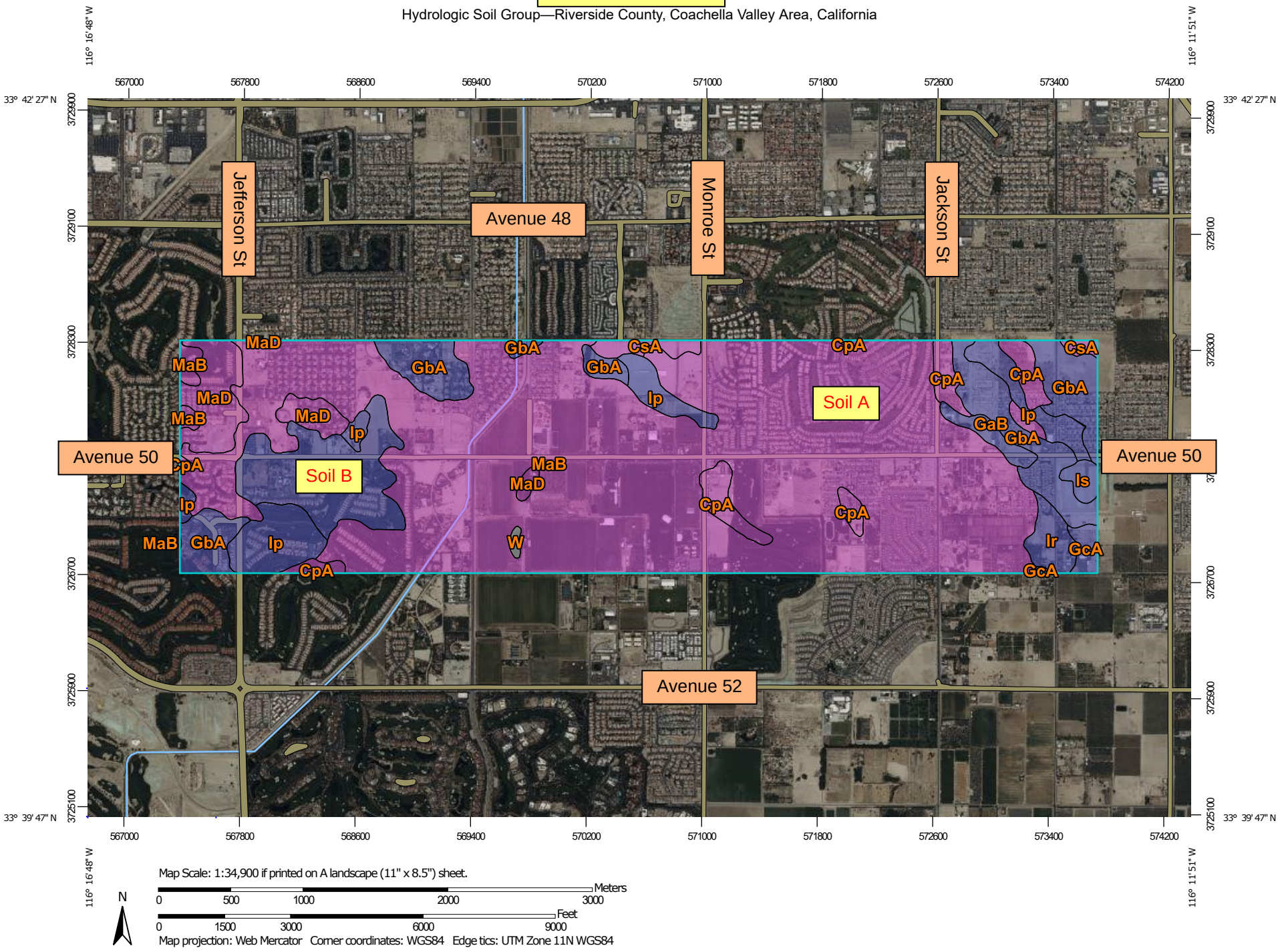
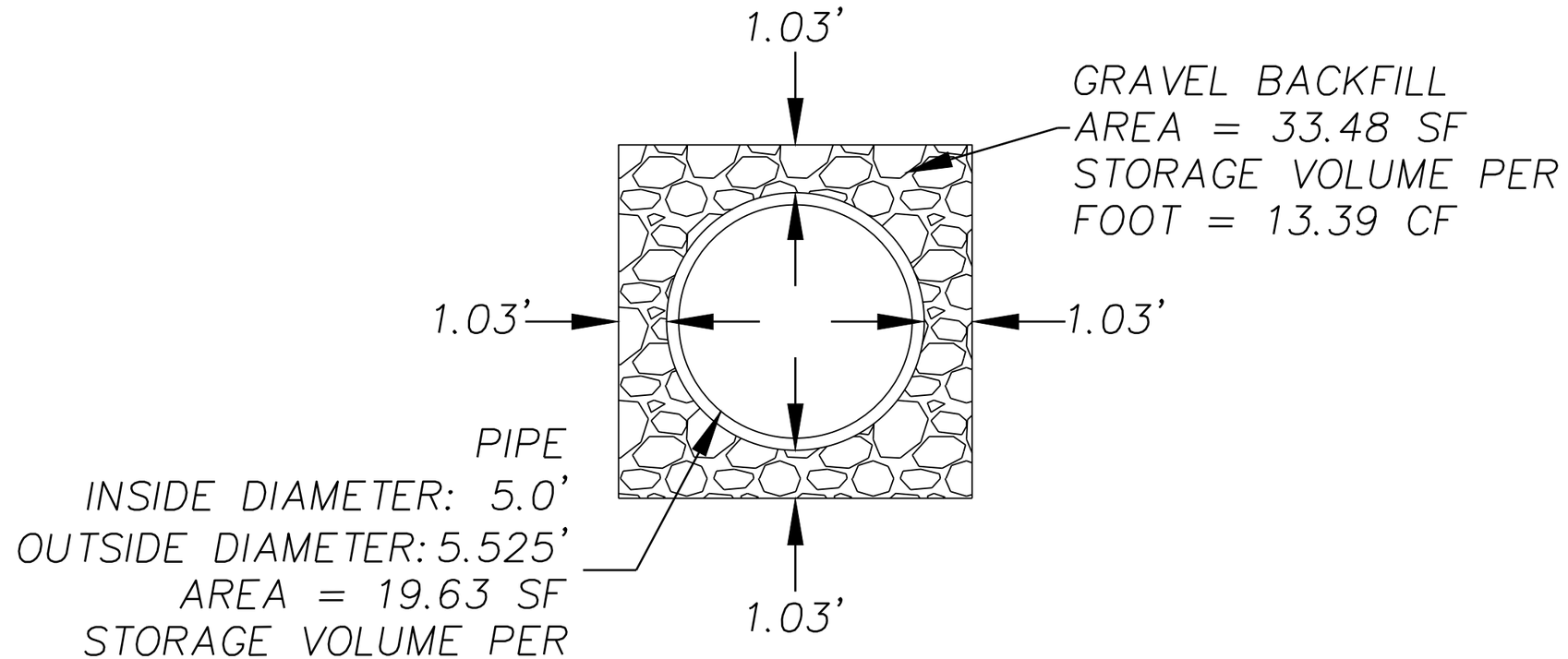


FIGURE 3 – TYPICAL SUBSURFACE BASIN CROSS SECTION

SUBSURFACE BASIN - CROSS SECTION



5' DIAMETER UNDERGROUND CHAMBER

SCALE: 1"=3'

DESIGN NOTES:

1. GRAVEL BACKFILL, n=0.4

JLC Engineering & Consulting, Inc.
41660 IVY STREET, SUITE A
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

FIGURE 3

Drawing Name: O:\173.WEBB\AVENUE 50\Hydrology Ave 52\STORAGE VOLUME.dwg
Last Opened: Apr 02, 2025 - 11:48am by eperez

ATTACHMENTS

NOAA ATLAS 14 RAINFALL OUTPUT

ATTACHMENT 1

NOAA Atlas 14, Volume 6, Version 2
Location name: La Quinta, California, USA*
Latitude: 33.685°, Longitude: -116.2593°
Elevation: 32 ft**
* source: ESRI Maps
** source: USGS

POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)[1]

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.065 (0.054-0.078)	0.100 (0.083-0.121)	0.152 (0.126-0.185)	0.200 (0.164-0.245)	0.273 (0.218-0.347)	0.338 (0.264-0.438)	0.412 (0.313-0.547)	0.497 (0.367-0.679)	0.631 (0.447-0.900)	0.753 (0.514-1.11)
10-min	0.093 (0.077-0.112)	0.143 (0.119-0.173)	0.218 (0.181-0.265)	0.286 (0.236-0.350)	0.392 (0.312-0.497)	0.484 (0.378-0.628)	0.590 (0.449-0.784)	0.712 (0.526-0.974)	0.904 (0.640-1.29)	1.08 (0.737-1.59)
15-min	0.112 (0.093-0.135)	0.173 (0.144-0.209)	0.263 (0.219-0.320)	0.346 (0.285-0.424)	0.474 (0.377-0.601)	0.586 (0.457-0.759)	0.714 (0.543-0.948)	0.861 (0.637-1.18)	1.09 (0.774-1.56)	1.30 (0.892-1.93)
30-min	0.163 (0.136-0.197)	0.251 (0.209-0.304)	0.383 (0.318-0.465)	0.502 (0.414-0.616)	0.688 (0.548-0.873)	0.851 (0.664-1.10)	1.04 (0.788-1.38)	1.25 (0.925-1.71)	1.59 (1.12-2.27)	1.90 (1.30-2.80)
60-min	0.228 (0.190-0.276)	0.352 (0.294-0.427)	0.537 (0.446-0.652)	0.705 (0.581-0.864)	0.965 (0.769-1.22)	1.19 (0.931-1.55)	1.45 (1.11-1.93)	1.76 (1.30-2.40)	2.23 (1.58-3.18)	2.66 (1.82-3.93)
2-hr	0.317 (0.265-0.384)	0.468 (0.390-0.567)	0.694 (0.577-0.843)	0.902 (0.743-1.10)	1.23 (0.976-1.55)	1.51 (1.18-1.96)	1.84 (1.40-2.44)	2.21 (1.63-3.02)	2.79 (1.97-3.98)	3.30 (2.26-4.88)
3-hr	0.382 (0.319-0.462)	0.554 (0.462-0.672)	0.814 (0.677-0.989)	1.06 (0.869-1.29)	1.43 (1.14-1.81)	1.76 (1.37-2.28)	2.14 (1.63-2.84)	2.57 (1.90-3.52)	3.25 (2.30-4.64)	3.85 (2.63-5.69)
6-hr	0.504 (0.421-0.610)	0.726 (0.605-0.879)	1.06 (0.881-1.29)	1.37 (1.13-1.68)	1.85 (1.47-2.34)	2.27 (1.77-2.94)	2.75 (2.09-3.66)	3.31 (2.44-4.52)	4.17 (2.96-5.95)	4.94 (3.38-7.30)
12-hr	0.610 (0.509-0.738)	0.899 (0.749-1.09)	1.33 (1.10-1.61)	1.72 (1.42-2.11)	2.32 (1.85-2.94)	2.84 (2.22-3.68)	3.43 (2.61-4.56)	4.10 (3.03-5.61)	5.13 (3.64-7.32)	6.04 (4.13-8.92)
24-hr	0.760 (0.673-0.877)	1.16 (1.02-1.33)	1.73 (1.53-2.00)	2.25 (1.97-2.62)	3.03 (2.57-3.65)	3.70 (3.07-4.54)	4.44 (3.60-5.58)	5.28 (4.17-6.82)	6.54 (4.96-8.80)	7.63 (5.60-10.6)
2-day	0.877 (0.776-1.01)	1.35 (1.20-1.56)	2.04 (1.80-2.36)	2.65 (2.32-3.09)	3.56 (3.02-4.29)	4.33 (3.60-5.32)	5.18 (4.20-6.52)	6.13 (4.84-7.92)	7.54 (5.72-10.1)	8.75 (6.42-12.2)
3-day	0.938 (0.830-1.08)	1.45 (1.28-1.68)	2.20 (1.94-2.55)	2.86 (2.50-3.34)	3.84 (3.25-4.62)	4.67 (3.88-5.73)	5.58 (4.52-7.01)	6.59 (5.20-8.51)	8.09 (6.14-10.9)	9.38 (6.88-13.0)
4-day	0.991 (0.877-1.14)	1.54 (1.36-1.78)	2.33 (2.05-2.69)	3.02 (2.64-3.53)	4.06 (3.44-4.89)	4.93 (4.09-6.06)	5.88 (4.77-7.40)	6.95 (5.49-8.98)	8.53 (6.47-11.5)	9.86 (7.24-13.7)
7-day	1.05 (0.928-1.21)	1.62 (1.44-1.88)	2.46 (2.16-2.84)	3.19 (2.79-3.72)	4.27 (3.62-5.15)	5.18 (4.30-6.37)	6.17 (5.01-7.77)	7.28 (5.74-9.40)	8.90 (6.75-12.0)	10.3 (7.54-14.3)
10-day	1.08 (0.954-1.24)	1.67 (1.48-1.93)	2.53 (2.23-2.93)	3.28 (2.87-3.83)	4.40 (3.73-5.30)	5.34 (4.43-6.56)	6.36 (5.16-8.00)	7.48 (5.91-9.67)	9.14 (6.94-12.3)	10.5 (7.73-14.6)
20-day	1.14 (1.01-1.32)	1.80 (1.59-2.08)	2.75 (2.42-3.18)	3.58 (3.14-4.18)	4.82 (4.08-5.81)	5.85 (4.86-7.19)	6.97 (5.65-8.76)	8.19 (6.47-10.6)	9.97 (7.56-13.4)	11.4 (8.40-15.9)
30-day	1.19 (1.06-1.37)	1.91 (1.69-2.20)	2.96 (2.61-3.42)	3.88 (3.39-4.53)	5.25 (4.45-6.32)	6.39 (5.30-7.85)	7.61 (6.17-9.57)	8.94 (7.06-11.6)	10.9 (8.24-14.6)	12.4 (9.12-17.3)
45-day	1.28 (1.14-1.48)	2.10 (1.86-2.42)	3.28 (2.90-3.80)	4.33 (3.79-5.06)	5.90 (5.00-7.10)	7.20 (5.98-8.84)	8.59 (6.96-10.8)	10.1 (7.97-13.0)	12.2 (9.29-16.5)	14.0 (10.3-19.5)
60-day	1.35 (1.20-1.56)	2.24 (1.98-2.59)	3.55 (3.13-4.11)	4.71 (4.12-5.49)	6.43 (5.45-7.74)	7.86 (6.53-9.66)	9.40 (7.62-11.8)	11.0 (8.72-14.3)	13.4 (10.2-18.0)	15.3 (11.2-21.3)

[1] Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

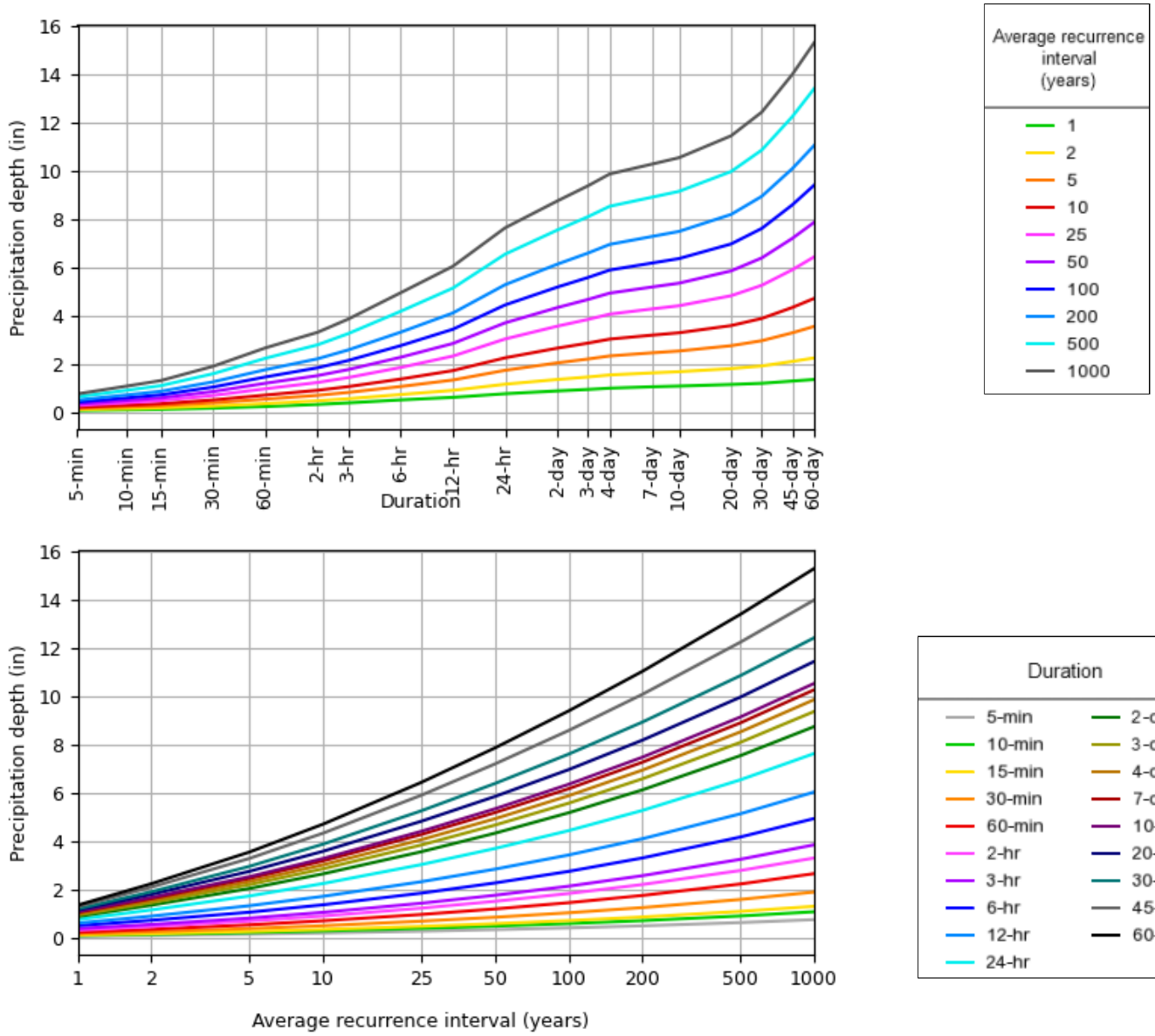
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

Back to Top

PF graphical

PDS-based depth-duration-frequency (DDF) curves
Latitude: 33.6850°, Longitude: -116.2593°



NOAA Atlas 14, Volume 6, Version 2

Created (GMT): Mon Feb 5 17:30:48 2024

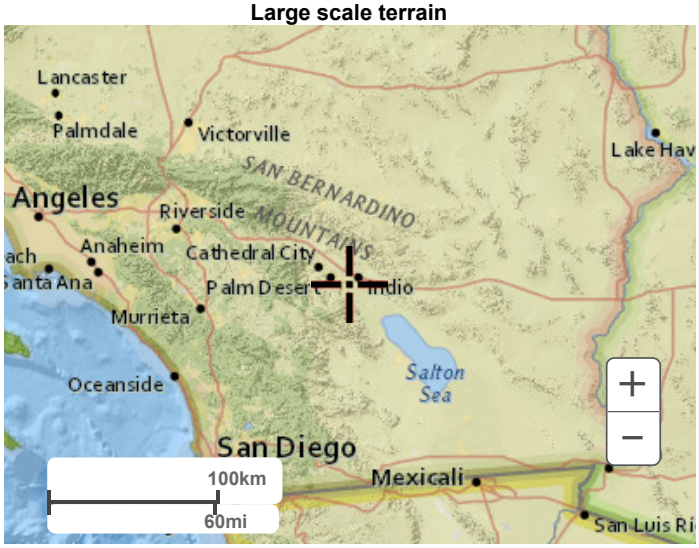
Back to Top

Maps & aerials

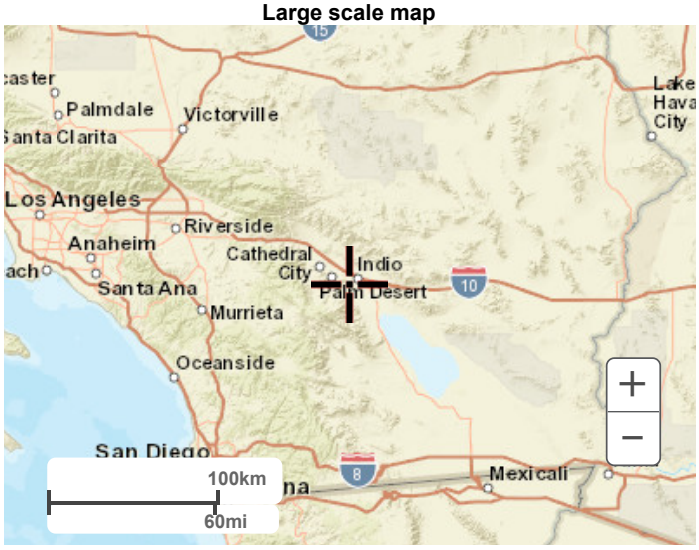
Small scale terrain



Large scale terrain



Large scale map



Large scale aerial



Back to Top

US Department of Commerce
National Oceanic and Atmospheric Administration
National Weather Service
National Water Center
1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

Disclaimer

IMPERVIOUS FRACTION TABLE/HYDROLOGY TABLE

ATTACHMENT 2A

Name	Total Area (ac)	Existing Impervious Area	Existing Imperious Fraction (A_I)	Existing Low Loss Rate	Existing: Nearest Land Use	Proposed Impervious Area	Proposed Imperious Fraction (A_I)	Proposed Low Loss Rate	Proposed: Nearest Land Use
A1	1.28	0.85	0.66	0.37	condo	1.11	0.87	0.20	commercial
AA1	1.23	0.77	0.63	0.40	condo	1.04	0.85	0.22	commercial
B1	1.47	0.44	0.30	0.66	1/2 ac lot	1.29	0.88	0.20	commercial
BB1	1.47	0.97	0.66	0.37	condo	1.23	0.84	0.23	apartments
C1	0.74	0.22	0.30	0.66	1/2 ac lot	0.66	0.89	0.19	commercial
CC1	0.77	0.57	0.75	0.30	mobile hom	0.57	0.75	0.30	mobile home
D1	1.68	0.49	0.29	0.67	1/2 ac lot	1.48	0.88	0.19	commercial
DD1	1.70	1.09	0.64	0.39	condo	1.37	0.81	0.26	apartments
E1	0.55	0.33	0.59	0.42	condo	0.49	0.89	0.19	commercial
EE1	0.55	0.37	0.66	0.37	condo	0.46	0.84	0.23	apartments
F1	0.33	0.26	0.77	0.28	apartments	0.27	0.80	0.26	apartments
FF1	0.36	0.28	0.78	0.28	apartments	0.30	0.85	0.22	commercial

RATIONAL METHOD OUTPUT FILES

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/04/24 File:ARA1.out

PROPOSED CONDITION: 100YR RM HYDROLOGY

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.352(In.)
100 year, 1 hour precipitation = 1.450(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 101.000 to Point/Station 102.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 648.000(Ft.)
Top (of initial area) elevation = 36.000(Ft.)
Bottom (of initial area) elevation = 31.500(Ft.)
Difference in elevation = 4.500(Ft.)
Slope = 0.00694 s(percent)= 0.69
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.800 min.
Rainfall intensity = 3.418(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.879

```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  56.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      3.845(CFS)
Total initial stream area =        1.280(Ac.)
Pervious area fraction = 0.100
End of computations, total study area =            1.28 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.100
Area averaged RI index number =  56.0
```

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/04/24 File:ARAA1.out

PROPOSED CONDITION: 100YR RM HYDROLOGY

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.352(In.)
100 year, 1 hour precipitation = 1.450(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 201.000 to Point/Station 202.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 644.000(Ft.)
Top (of initial area) elevation = 36.000(Ft.)
Bottom (of initial area) elevation = 31.500(Ft.)
Difference in elevation = 4.500(Ft.)
Slope = 0.00699 s(percent)= 0.70
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 10.760 min.
Rainfall intensity = 3.424(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.879

```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  56.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      3.702(CFS)
Total initial stream area =        1.230(Ac.)
Pervious area fraction = 0.100
End of computations, total study area =            1.23 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.100
Area averaged RI index number =  56.0
```

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/04/24 File:ARB1.out

PROPOSED CONDITION: 100YR RM HYDROLOGY

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.352(In.)
100 year, 1 hour precipitation = 1.450(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 103.000 to Point/Station 104.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 972.000(Ft.)
Top (of initial area) elevation = 34.000(Ft.)
Bottom (of initial area) elevation = 28.000(Ft.)
Difference in elevation = 6.000(Ft.)
Slope = 0.00617 s(percent)= 0.62
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 13.004 min.
Rainfall intensity = 3.115(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.877

```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  56.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      4.017(CFS)
Total initial stream area =        1.470(Ac.)
Pervious area fraction = 0.100
End of computations, total study area =            1.47 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.100
Area averaged RI index number =  56.0
```

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/04/24 File:ARBB1.out

PROPOSED CONDITION: 100YR RM HYDROLOGY

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.352(In.)
100 year, 1 hour precipitation = 1.450(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 203.000 to Point/Station 204.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 970.000(Ft.)
Top (of initial area) elevation = 34.000(Ft.)
Bottom (of initial area) elevation = 27.000(Ft.)
Difference in elevation = 7.000(Ft.)
Slope = 0.00722 s(percent)= 0.72
TC = k(0.323)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 13.560 min.
Rainfall intensity = 3.050(In/Hr) for a 100.0 year storm
APARTMENT subarea type
Runoff Coefficient = 0.854

```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  56.00
Pervious area fraction =  0.200; Impervious fraction =  0.800
Initial subarea runoff =      3.829(CFS)
Total initial stream area =        1.470(Ac.)
Pervious area fraction = 0.200
End of computations, total study area =            1.47 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.200
Area averaged RI index number =  56.0
```

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/04/24 File:ARC1.out

PROPOSED CONDITION: 100YR RM HYDROLOGY

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.352(In.)
100 year, 1 hour precipitation = 1.450(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 105.000 to Point/Station 106.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 379.000(Ft.)
Top (of initial area) elevation = 28.500(Ft.)
Bottom (of initial area) elevation = 26.500(Ft.)
Difference in elevation = 2.000(Ft.)
Slope = 0.00528 s(percent)= 0.53
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 9.207 min.
Rainfall intensity = 3.702(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.880

```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  56.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      2.411(CFS)
Total initial stream area =        0.740(Ac.)
Pervious area fraction = 0.100
End of computations, total study area =            0.74 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.100
Area averaged RI index number =  56.0
```

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/04/24 File:ARCC1.out

PROPOSED CONDITION: 100YR RM HYDROLOGY

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.352(In.)
100 year, 1 hour precipitation = 1.450(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 205.000 to Point/Station 206.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 374.000(Ft.)
Top (of initial area) elevation = 28.000(Ft.)
Bottom (of initial area) elevation = 25.500(Ft.)
Difference in elevation = 2.500(Ft.)
Slope = 0.00668 s(percent)= 0.67
TC = k(0.336)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 9.783 min.
Rainfall intensity = 3.591(In/Hr) for a 100.0 year storm
MOBILE HOME PARK subarea type
Runoff Coefficient = 0.849

```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  56.00
Pervious area fraction =  0.250; Impervious fraction =  0.750
Initial subarea runoff =      2.348(CFS)
Total initial stream area =        0.770(Ac.)
Pervious area fraction = 0.250
End of computations, total study area =            0.77 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.250
Area averaged RI index number =  56.0
```

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/05/24 File:ARD1.out

PROPOSED CONDITION: 100YR RM HYDROLOGY

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.352(In.)
100 year, 1 hour precipitation = 1.450(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 107.000 to Point/Station 108.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 941.000(Ft.)
Top (of initial area) elevation = 27.000(Ft.)
Bottom (of initial area) elevation = 22.500(Ft.)
Difference in elevation = 4.500(Ft.)
Slope = 0.00478 s(percent)= 0.48
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 13.509 min.
Rainfall intensity = 3.056(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.867

```
Decimal fraction soil group A = 0.540
Decimal fraction soil group B = 0.460
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  43.04
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      4.451(CFS)
Total initial stream area =        1.680(Ac.)
Pervious area fraction = 0.100
End of computations, total study area =            1.68 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.100
Area averaged RI index number =  43.0
```

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/05/24 File:ARDD1.out

PROPOSED CONDITION: 100YR RM HYDROLOGY

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.352(In.)
100 year, 1 hour precipitation = 1.450(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 207.000 to Point/Station 208.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 935.000(Ft.)
Top (of initial area) elevation = 27.000(Ft.)
Bottom (of initial area) elevation = 22.000(Ft.)
Difference in elevation = 5.000(Ft.)
Slope = 0.00535 s(percent)= 0.53
TC = k(0.323)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 14.187 min.
Rainfall intensity = 2.982(In/Hr) for a 100.0 year storm
APARTMENT subarea type
Runoff Coefficient = 0.833

```
Decimal fraction soil group A = 0.540
Decimal fraction soil group B = 0.460
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  43.04
Pervious area fraction =  0.200; Impervious fraction =  0.800
Initial subarea runoff =      4.223(CFS)
Total initial stream area =        1.700(Ac.)
Pervious area fraction = 0.200
End of computations, total study area =            1.70 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.200
Area averaged RI index number =  43.0
```

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/05/24 File:ARE1.out

PROPOSED CONDITION: 100YR RM HYDROLOGY

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.352(In.)
100 year, 1 hour precipitation = 1.450(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 109.000 to Point/Station 110.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 303.000(Ft.)
Top (of initial area) elevation = 31.000(Ft.)
Bottom (of initial area) elevation = 28.500(Ft.)
Difference in elevation = 2.500(Ft.)
Slope = 0.00825 s(percent)= 0.83
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 7.698 min.
Rainfall intensity = 4.048(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.863

```
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  32.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      1.921(CFS)
Total initial stream area =        0.550(Ac.)
Pervious area fraction = 0.100
End of computations, total study area =            0.55 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.100
Area averaged RI index number =  32.0
```

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/05/24 File:AREE1.out

PROPOSED CONDITION: 100YR RM HYDROLOGY

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.352(In.)
100 year, 1 hour precipitation = 1.450(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 209.000 to Point/Station 210.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 308.000(Ft.)
Top (of initial area) elevation = 31.000(Ft.)
Bottom (of initial area) elevation = 28.500(Ft.)
Difference in elevation = 2.500(Ft.)
Slope = 0.00812 s(percent)= 0.81
TC = k(0.323)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 8.370 min.
Rainfall intensity = 3.882(In/Hr) for a 100.0 year storm
APARTMENT subarea type
Runoff Coefficient = 0.824

```
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  32.00
Pervious area fraction =  0.200; Impervious fraction =  0.800
Initial subarea runoff =      1.760(CFS)
Total initial stream area =        0.550(Ac.)
Pervious area fraction = 0.200
End of computations, total study area =            0.55 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.200
Area averaged RI index number =  32.0
```

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/05/24 File:ARF1.out

PROPOSED CONDITION: 100YR RM HYDROLOGY

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.352(In.)
100 year, 1 hour precipitation = 1.450(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 111.000 to Point/Station 112.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 274.000(Ft.)
Top (of initial area) elevation = 31.000(Ft.)
Bottom (of initial area) elevation = 29.500(Ft.)
Difference in elevation = 1.500(Ft.)
Slope = 0.00547 s(percent)= 0.55
TC = k(0.323)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 8.642 min.
Rainfall intensity = 3.821(In/Hr) for a 100.0 year storm
APARTMENT subarea type
Runoff Coefficient = 0.823

```
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  32.00
Pervious area fraction =  0.200; Impervious fraction =  0.800
Initial subarea runoff =      1.038(CFS)
Total initial stream area =        0.330(Ac.)
Pervious area fraction = 0.200
End of computations, total study area =            0.33 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.200
Area averaged RI index number =  32.0
```

Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2014 Version 9.0
Rational Hydrology Study Date: 02/05/24 File:ARFF1.out

PROPOSED CONDITION: 100YR RM HYDROLOGY

********* Hydrology Study Control Information **********

English (in-lb) Units used in input data file

Program License Serial Number 6279

Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) = 100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation = 0.352(In.)
100 year, 1 hour precipitation = 1.450(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity = 1.450(In/Hr)
Slope of intensity duration curve = 0.5000

++
Process from Point/Station 211.000 to Point/Station 212.000
**** INITIAL AREA EVALUATION ****

Initial area flow distance = 281.000(Ft.)
Top (of initial area) elevation = 31.000(Ft.)
Bottom (of initial area) elevation = 29.500(Ft.)
Difference in elevation = 1.500(Ft.)
Slope = 0.00534 s(percent)= 0.53
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 8.149 min.
Rainfall intensity = 3.934(In/Hr) for a 100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.862

```
Decimal fraction soil group A = 1.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  32.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      1.221(CFS)
Total initial stream area =        0.360(Ac.)
Pervious area fraction = 0.100
End of computations, total study area =            0.36 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.100
Area averaged RI index number =  32.0
```

FLOWMASTER CATCH BASIN CALCULATION FILES

Worksheet for CB-A1-Sump

Project Description	
Solve For	Spread

Input Data	
Discharge	3.90 cfs
Gutter Width	2.00 ft
Gutter Cross Slope	0.083 ft/ft
Road Cross Slope	0.025 ft/ft
Curb Opening Length	4.0 ft
Opening Height	0.5 ft
Curb Throat Type	Inclined
Local Depression	4.0 in
Local Depression Width	48.0 in
Throat Incline Angle	45.00 degrees

Results	
Spread	11.4 ft
Depth	0.40 ft
Gutter Depression	1.4 in
Total Depression	5.4 in

Worksheet for CB-AA1-Sump

Project Description	
Solve For	Spread

Input Data		
Discharge	3.70	cfs
Gutter Width	2.00	ft
Gutter Cross Slope	0.083	ft/ft
Road Cross Slope	0.025	ft/ft
Curb Opening Length	4.0	ft
Opening Height	0.5	ft
Curb Throat Type	Inclined	
Local Depression	4.0	in
Local Depression Width	48.0	in
Throat Incline Angle	45.00	degrees

Results		
Spread	11.0	ft
Depth	0.39	ft
Gutter Depression	1.4	in
Total Depression	5.4	in

Worksheet for CB-B1-Sump

Project Description	
Solve For	Spread

Input Data	
Discharge	4.00 cfs
Gutter Width	2.00 ft
Gutter Cross Slope	0.083 ft/ft
Road Cross Slope	0.025 ft/ft
Curb Opening Length	4.0 ft
Opening Height	0.5 ft
Curb Throat Type	Inclined
Local Depression	4.0 in
Local Depression Width	48.0 in
Throat Incline Angle	45.00 degrees

Results	
Spread	11.6 ft
Depth	0.41 ft
Gutter Depression	1.4 in
Total Depression	5.4 in

Worksheet for CB-BB1-Sump

Project Description	
Solve For	Spread

Input Data	
Discharge	3.80 cfs
Gutter Width	2.00 ft
Gutter Cross Slope	0.083 ft/ft
Road Cross Slope	0.025 ft/ft
Curb Opening Length	4.0 ft
Opening Height	0.5 ft
Curb Throat Type	Inclined
Local Depression	4.0 in
Local Depression Width	48.0 in
Throat Incline Angle	45.00 degrees

Results	
Spread	11.2 ft
Depth	0.40 ft
Gutter Depression	1.4 in
Total Depression	5.4 in

Worksheet for CB-C1-Sump

Project Description	
Solve For	Spread

Input Data	
Discharge	2.40 cfs
Gutter Width	2.00 ft
Gutter Cross Slope	0.083 ft/ft
Road Cross Slope	0.025 ft/ft
Curb Opening Length	4.0 ft
Opening Height	0.5 ft
Curb Throat Type	Inclined
Local Depression	4.0 in
Local Depression Width	48.0 in
Throat Incline Angle	45.00 degrees

Results	
Spread	3.9 ft
Depth	0.32 ft
Gutter Depression	1.4 in
Total Depression	5.4 in

Worksheet for CB-CC1-Sump

Project Description	
Solve For	Spread

Input Data	
Discharge	2.40 cfs
Gutter Width	2.00 ft
Gutter Cross Slope	0.083 ft/ft
Road Cross Slope	0.025 ft/ft
Curb Opening Length	4.0 ft
Opening Height	0.5 ft
Curb Throat Type	Inclined
Local Depression	4.0 in
Local Depression Width	48.0 in
Throat Incline Angle	45.00 degrees

Results	
Spread	3.9 ft
Depth	0.32 ft
Gutter Depression	1.4 in
Total Depression	5.4 in

Worksheet for CB-D1-Sump

Project Description	
Solve For	Spread

Input Data	
Discharge	4.50 cfs
Gutter Width	2.00 ft
Gutter Cross Slope	0.083 ft/ft
Road Cross Slope	0.025 ft/ft
Curb Opening Length	4.0 ft
Opening Height	0.5 ft
Curb Throat Type	Inclined
Local Depression	4.0 in
Local Depression Width	48.0 in
Throat Incline Angle	45.00 degrees

Results	
Spread	12.5 ft
Depth	0.43 ft
Gutter Depression	1.4 in
Total Depression	5.4 in

Worksheet for CB-DD1-Sump

Project Description	
Solve For	Spread

Input Data	
Discharge	4.20 cfs
Gutter Width	2.00 ft
Gutter Cross Slope	0.083 ft/ft
Road Cross Slope	0.025 ft/ft
Curb Opening Length	4.0 ft
Opening Height	0.5 ft
Curb Throat Type	Inclined
Local Depression	4.0 in
Local Depression Width	48.0 in
Throat Incline Angle	45.00 degrees

Results	
Spread	11.9 ft
Depth	0.42 ft
Gutter Depression	1.4 in
Total Depression	5.4 in

Worksheet for CB-E1-Sump

Project Description	
Solve For	Spread

Input Data		
Discharge	1.90	cfs
Gutter Width	2.00	ft
Gutter Cross Slope	0.083	ft/ft
Road Cross Slope	0.025	ft/ft
Curb Opening Length	4.0	ft
Opening Height	0.5	ft
Curb Throat Type	Inclined	
Local Depression	4.0	in
Local Depression Width	48.0	in
Throat Incline Angle	45.00	degrees

Results		
Spread	3.8	ft
Depth	0.29	ft
Gutter Depression	1.4	in
Total Depression	5.4	in

Worksheet for CB-EE1-Sump

Project Description	
Solve For	Spread

Input Data	
Discharge	1.80 cfs
Gutter Width	2.00 ft
Gutter Cross Slope	0.083 ft/ft
Road Cross Slope	0.025 ft/ft
Curb Opening Length	4.0 ft
Opening Height	0.5 ft
Curb Throat Type	Inclined
Local Depression	4.0 in
Local Depression Width	48.0 in
Throat Incline Angle	45.00 degrees

Results	
Spread	3.7 ft
Depth	0.29 ft
Gutter Depression	1.4 in
Total Depression	5.4 in

UNIT HYDROGRAPH OUTPUT FILES

AREA A1

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014, Version 9.0
Study date 02/05/24 File: ARA124100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6279

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

PROPOSED CONDITION: 100YR HYDROLOGY
ARA1

Drainage Area = 1.28(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.28(Ac.) = 0.002 Sq. Mi.
Length along longest watercourse = 648.00(Ft.)
Length along longest watercourse measured to centroid = 324.00(Ft.)
Length along longest watercourse = 0.123 Mi.
Length along longest watercourse measured to centroid = 0.061 Mi.
Difference in elevation = 4.50(Ft.)
Slope along watercourse = 36.6667 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.028 Hr.
Lag time = 1.70 Min.
25% of lag time = 0.42 Min.
40% of lag time = 0.68 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.28	1.16	1.48

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.28	4.44	5.68

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.160(In)
Area Averaged 100-Year Rainfall = 4.440(In)

Point rain (area averaged) = 4.440(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 4.440(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.280	56.00	0.870

Total Area Entered = 1.28(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.870	0.111	1.000	0.111
					Sum (F) =	0.111

Area averaged mean soil loss (F) (In/Hr) = 0.111
Minimum soil loss rate ((In/Hr)) = 0.055
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.200

U n i t H y d r o g r a p h
DESERT S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	294.120	55.498	0.716
2	0.167	588.239	39.132	0.505
3	0.250	882.359	5.371	0.069
		Sum = 100.000	Sum=	1.290

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max		Low	Effective (In/Hr)
1	0.08	0.07	0.036	(0.196)	0.007	0.028
2	0.17	0.07	0.036	(0.196)	0.007	0.028

3	0.25	0.07	0.036	(0.195)	0.007	0.028
4	0.33	0.10	0.053	(0.194)	0.011	0.043
5	0.42	0.10	0.053	(0.193)	0.011	0.043
6	0.50	0.10	0.053	(0.193)	0.011	0.043
7	0.58	0.10	0.053	(0.192)	0.011	0.043
8	0.67	0.10	0.053	(0.191)	0.011	0.043
9	0.75	0.10	0.053	(0.190)	0.011	0.043
10	0.83	0.13	0.071	(0.190)	0.014	0.057
11	0.92	0.13	0.071	(0.189)	0.014	0.057
12	1.00	0.13	0.071	(0.188)	0.014	0.057
13	1.08	0.10	0.053	(0.187)	0.011	0.043
14	1.17	0.10	0.053	(0.187)	0.011	0.043
15	1.25	0.10	0.053	(0.186)	0.011	0.043
16	1.33	0.10	0.053	(0.185)	0.011	0.043
17	1.42	0.10	0.053	(0.185)	0.011	0.043
18	1.50	0.10	0.053	(0.184)	0.011	0.043
19	1.58	0.10	0.053	(0.183)	0.011	0.043
20	1.67	0.10	0.053	(0.182)	0.011	0.043
21	1.75	0.10	0.053	(0.182)	0.011	0.043
22	1.83	0.13	0.071	(0.181)	0.014	0.057
23	1.92	0.13	0.071	(0.180)	0.014	0.057
24	2.00	0.13	0.071	(0.179)	0.014	0.057
25	2.08	0.13	0.071	(0.179)	0.014	0.057
26	2.17	0.13	0.071	(0.178)	0.014	0.057
27	2.25	0.13	0.071	(0.177)	0.014	0.057
28	2.33	0.13	0.071	(0.176)	0.014	0.057
29	2.42	0.13	0.071	(0.176)	0.014	0.057
30	2.50	0.13	0.071	(0.175)	0.014	0.057
31	2.58	0.17	0.089	(0.174)	0.018	0.071
32	2.67	0.17	0.089	(0.174)	0.018	0.071
33	2.75	0.17	0.089	(0.173)	0.018	0.071
34	2.83	0.17	0.089	(0.172)	0.018	0.071
35	2.92	0.17	0.089	(0.171)	0.018	0.071
36	3.00	0.17	0.089	(0.171)	0.018	0.071
37	3.08	0.17	0.089	(0.170)	0.018	0.071
38	3.17	0.17	0.089	(0.169)	0.018	0.071
39	3.25	0.17	0.089	(0.169)	0.018	0.071
40	3.33	0.17	0.089	(0.168)	0.018	0.071
41	3.42	0.17	0.089	(0.167)	0.018	0.071
42	3.50	0.17	0.089	(0.167)	0.018	0.071
43	3.58	0.17	0.089	(0.166)	0.018	0.071
44	3.67	0.17	0.089	(0.165)	0.018	0.071
45	3.75	0.17	0.089	(0.164)	0.018	0.071
46	3.83	0.20	0.107	(0.164)	0.021	0.085
47	3.92	0.20	0.107	(0.163)	0.021	0.085
48	4.00	0.20	0.107	(0.162)	0.021	0.085
49	4.08	0.20	0.107	(0.162)	0.021	0.085
50	4.17	0.20	0.107	(0.161)	0.021	0.085
51	4.25	0.20	0.107	(0.160)	0.021	0.085
52	4.33	0.23	0.124	(0.160)	0.025	0.099
53	4.42	0.23	0.124	(0.159)	0.025	0.099
54	4.50	0.23	0.124	(0.158)	0.025	0.099
55	4.58	0.23	0.124	(0.158)	0.025	0.099

56	4.67	0.23	0.124	(0.157)	0.025	0.099
57	4.75	0.23	0.124	(0.156)	0.025	0.099
58	4.83	0.27	0.142	(0.156)	0.028	0.114
59	4.92	0.27	0.142	(0.155)	0.028	0.114
60	5.00	0.27	0.142	(0.154)	0.028	0.114
61	5.08	0.20	0.107	(0.154)	0.021	0.085
62	5.17	0.20	0.107	(0.153)	0.021	0.085
63	5.25	0.20	0.107	(0.152)	0.021	0.085
64	5.33	0.23	0.124	(0.152)	0.025	0.099
65	5.42	0.23	0.124	(0.151)	0.025	0.099
66	5.50	0.23	0.124	(0.150)	0.025	0.099
67	5.58	0.27	0.142	(0.150)	0.028	0.114
68	5.67	0.27	0.142	(0.149)	0.028	0.114
69	5.75	0.27	0.142	(0.148)	0.028	0.114
70	5.83	0.27	0.142	(0.148)	0.028	0.114
71	5.92	0.27	0.142	(0.147)	0.028	0.114
72	6.00	0.27	0.142	(0.146)	0.028	0.114
73	6.08	0.30	0.160	(0.146)	0.032	0.128
74	6.17	0.30	0.160	(0.145)	0.032	0.128
75	6.25	0.30	0.160	(0.144)	0.032	0.128
76	6.33	0.30	0.160	(0.144)	0.032	0.128
77	6.42	0.30	0.160	(0.143)	0.032	0.128
78	6.50	0.30	0.160	(0.142)	0.032	0.128
79	6.58	0.33	0.178	(0.142)	0.036	0.142
80	6.67	0.33	0.178	(0.141)	0.036	0.142
81	6.75	0.33	0.178	(0.141)	0.036	0.142
82	6.83	0.33	0.178	(0.140)	0.036	0.142
83	6.92	0.33	0.178	(0.139)	0.036	0.142
84	7.00	0.33	0.178	(0.139)	0.036	0.142
85	7.08	0.33	0.178	(0.138)	0.036	0.142
86	7.17	0.33	0.178	(0.137)	0.036	0.142
87	7.25	0.33	0.178	(0.137)	0.036	0.142
88	7.33	0.37	0.195	(0.136)	0.039	0.156
89	7.42	0.37	0.195	(0.135)	0.039	0.156
90	7.50	0.37	0.195	(0.135)	0.039	0.156
91	7.58	0.40	0.213	(0.134)	0.043	0.170
92	7.67	0.40	0.213	(0.134)	0.043	0.170
93	7.75	0.40	0.213	(0.133)	0.043	0.170
94	7.83	0.43	0.231	(0.132)	0.046	0.185
95	7.92	0.43	0.231	(0.132)	0.046	0.185
96	8.00	0.43	0.231	(0.131)	0.046	0.185
97	8.08	0.50	0.266	(0.131)	0.053	0.213
98	8.17	0.50	0.266	(0.130)	0.053	0.213
99	8.25	0.50	0.266	(0.129)	0.053	0.213
100	8.33	0.50	0.266	(0.129)	0.053	0.213
101	8.42	0.50	0.266	(0.128)	0.053	0.213
102	8.50	0.50	0.266	(0.128)	0.053	0.213
103	8.58	0.53	0.284	(0.127)	0.057	0.227
104	8.67	0.53	0.284	(0.126)	0.057	0.227
105	8.75	0.53	0.284	(0.126)	0.057	0.227
106	8.83	0.57	0.302	(0.125)	0.060	0.242
107	8.92	0.57	0.302	(0.125)	0.060	0.242
108	9.00	0.57	0.302	(0.124)	0.060	0.242

109	9.08	0.63	0.337	(0.123)	0.067	0.270
110	9.17	0.63	0.337	(0.123)	0.067	0.270
111	9.25	0.63	0.337	(0.122)	0.067	0.270
112	9.33	0.67	0.355	(0.122)	0.071	0.284
113	9.42	0.67	0.355	(0.121)	0.071	0.284
114	9.50	0.67	0.355	(0.120)	0.071	0.284
115	9.58	0.70	0.373	(0.120)	0.075	0.298
116	9.67	0.70	0.373	(0.119)	0.075	0.298
117	9.75	0.70	0.373	(0.119)	0.075	0.298
118	9.83	0.73	0.391	(0.118)	0.078	0.313
119	9.92	0.73	0.391	(0.118)	0.078	0.313
120	10.00	0.73	0.391	(0.117)	0.078	0.313
121	10.08	0.50	0.266	(0.116)	0.053	0.213
122	10.17	0.50	0.266	(0.116)	0.053	0.213
123	10.25	0.50	0.266	(0.115)	0.053	0.213
124	10.33	0.50	0.266	(0.115)	0.053	0.213
125	10.42	0.50	0.266	(0.114)	0.053	0.213
126	10.50	0.50	0.266	(0.114)	0.053	0.213
127	10.58	0.67	0.355	(0.113)	0.071	0.284
128	10.67	0.67	0.355	(0.113)	0.071	0.284
129	10.75	0.67	0.355	(0.112)	0.071	0.284
130	10.83	0.67	0.355	(0.111)	0.071	0.284
131	10.92	0.67	0.355	(0.111)	0.071	0.284
132	11.00	0.67	0.355	(0.110)	0.071	0.284
133	11.08	0.63	0.337	(0.110)	0.067	0.270
134	11.17	0.63	0.337	(0.109)	0.067	0.270
135	11.25	0.63	0.337	(0.109)	0.067	0.270
136	11.33	0.63	0.337	(0.108)	0.067	0.270
137	11.42	0.63	0.337	(0.108)	0.067	0.270
138	11.50	0.63	0.337	(0.107)	0.067	0.270
139	11.58	0.57	0.302	(0.107)	0.060	0.242
140	11.67	0.57	0.302	(0.106)	0.060	0.242
141	11.75	0.57	0.302	(0.106)	0.060	0.242
142	11.83	0.60	0.320	(0.105)	0.064	0.256
143	11.92	0.60	0.320	(0.105)	0.064	0.256
144	12.00	0.60	0.320	(0.104)	0.064	0.256
145	12.08	0.83	0.444	(0.103)	0.089	0.355
146	12.17	0.83	0.444	(0.103)	0.089	0.355
147	12.25	0.83	0.444	(0.102)	0.089	0.355
148	12.33	0.87	0.462	(0.102)	0.092	0.369
149	12.42	0.87	0.462	(0.101)	0.092	0.369
150	12.50	0.87	0.462	(0.101)	0.092	0.369
151	12.58	0.93	0.497	(0.100)	0.099	0.398
152	12.67	0.93	0.497	(0.100)	0.099	0.398
153	12.75	0.93	0.497	0.099	(0.099)	0.398
154	12.83	0.97	0.515	0.099	(0.103)	0.416
155	12.92	0.97	0.515	0.098	(0.103)	0.417
156	13.00	0.97	0.515	0.098	(0.103)	0.417
157	13.08	1.13	0.604	0.097	(0.121)	0.506
158	13.17	1.13	0.604	0.097	(0.121)	0.507
159	13.25	1.13	0.604	0.096	(0.121)	0.507
160	13.33	1.13	0.604	0.096	(0.121)	0.508
161	13.42	1.13	0.604	0.095	(0.121)	0.508

162	13.50	1.13	0.604		0.095	(	0.121)	0.509
163	13.58	0.77	0.408	(	0.094)		0.082	0.327
164	13.67	0.77	0.408	(	0.094)		0.082	0.327
165	13.75	0.77	0.408	(	0.093)		0.082	0.327
166	13.83	0.77	0.408	(	0.093)		0.082	0.327
167	13.92	0.77	0.408	(	0.093)		0.082	0.327
168	14.00	0.77	0.408	(	0.092)		0.082	0.327
169	14.08	0.90	0.480		0.092	(	0.096)	0.388
170	14.17	0.90	0.480		0.091	(	0.096)	0.388
171	14.25	0.90	0.480		0.091	(	0.096)	0.389
172	14.33	0.87	0.462		0.090	(	0.092)	0.372
173	14.42	0.87	0.462		0.090	(	0.092)	0.372
174	14.50	0.87	0.462		0.089	(	0.092)	0.372
175	14.58	0.87	0.462		0.089	(	0.092)	0.373
176	14.67	0.87	0.462		0.088	(	0.092)	0.373
177	14.75	0.87	0.462		0.088	(	0.092)	0.374
178	14.83	0.83	0.444		0.087	(	0.089)	0.357
179	14.92	0.83	0.444		0.087	(	0.089)	0.357
180	15.00	0.83	0.444		0.087	(	0.089)	0.357
181	15.08	0.80	0.426	(	0.086)		0.085	0.341
182	15.17	0.80	0.426	(	0.086)		0.085	0.341
183	15.25	0.80	0.426	(	0.085)		0.085	0.341
184	15.33	0.77	0.408	(	0.085)		0.082	0.327
185	15.42	0.77	0.408	(	0.084)		0.082	0.327
186	15.50	0.77	0.408	(	0.084)		0.082	0.327
187	15.58	0.63	0.337	(	0.084)		0.067	0.270
188	15.67	0.63	0.337	(	0.083)		0.067	0.270
189	15.75	0.63	0.337	(	0.083)		0.067	0.270
190	15.83	0.63	0.337	(	0.082)		0.067	0.270
191	15.92	0.63	0.337	(	0.082)		0.067	0.270
192	16.00	0.63	0.337	(	0.081)		0.067	0.270
193	16.08	0.13	0.071	(	0.081)		0.014	0.057
194	16.17	0.13	0.071	(	0.081)		0.014	0.057
195	16.25	0.13	0.071	(	0.080)		0.014	0.057
196	16.33	0.13	0.071	(	0.080)		0.014	0.057
197	16.42	0.13	0.071	(	0.079)		0.014	0.057
198	16.50	0.13	0.071	(	0.079)		0.014	0.057
199	16.58	0.10	0.053	(	0.079)		0.011	0.043
200	16.67	0.10	0.053	(	0.078)		0.011	0.043
201	16.75	0.10	0.053	(	0.078)		0.011	0.043
202	16.83	0.10	0.053	(	0.077)		0.011	0.043
203	16.92	0.10	0.053	(	0.077)		0.011	0.043
204	17.00	0.10	0.053	(	0.077)		0.011	0.043
205	17.08	0.17	0.089	(	0.076)		0.018	0.071
206	17.17	0.17	0.089	(	0.076)		0.018	0.071
207	17.25	0.17	0.089	(	0.075)		0.018	0.071
208	17.33	0.17	0.089	(	0.075)		0.018	0.071
209	17.42	0.17	0.089	(	0.075)		0.018	0.071
210	17.50	0.17	0.089	(	0.074)		0.018	0.071
211	17.58	0.17	0.089	(	0.074)		0.018	0.071
212	17.67	0.17	0.089	(	0.074)		0.018	0.071
213	17.75	0.17	0.089	(	0.073)		0.018	0.071
214	17.83	0.13	0.071	(	0.073)		0.014	0.057

215	17.92	0.13	0.071	(0.072)	0.014	0.057
216	18.00	0.13	0.071	(0.072)	0.014	0.057
217	18.08	0.13	0.071	(0.072)	0.014	0.057
218	18.17	0.13	0.071	(0.071)	0.014	0.057
219	18.25	0.13	0.071	(0.071)	0.014	0.057
220	18.33	0.13	0.071	(0.071)	0.014	0.057
221	18.42	0.13	0.071	(0.070)	0.014	0.057
222	18.50	0.13	0.071	(0.070)	0.014	0.057
223	18.58	0.10	0.053	(0.070)	0.011	0.043
224	18.67	0.10	0.053	(0.069)	0.011	0.043
225	18.75	0.10	0.053	(0.069)	0.011	0.043
226	18.83	0.07	0.036	(0.069)	0.007	0.028
227	18.92	0.07	0.036	(0.068)	0.007	0.028
228	19.00	0.07	0.036	(0.068)	0.007	0.028
229	19.08	0.10	0.053	(0.068)	0.011	0.043
230	19.17	0.10	0.053	(0.067)	0.011	0.043
231	19.25	0.10	0.053	(0.067)	0.011	0.043
232	19.33	0.13	0.071	(0.067)	0.014	0.057
233	19.42	0.13	0.071	(0.066)	0.014	0.057
234	19.50	0.13	0.071	(0.066)	0.014	0.057
235	19.58	0.10	0.053	(0.066)	0.011	0.043
236	19.67	0.10	0.053	(0.066)	0.011	0.043
237	19.75	0.10	0.053	(0.065)	0.011	0.043
238	19.83	0.07	0.036	(0.065)	0.007	0.028
239	19.92	0.07	0.036	(0.065)	0.007	0.028
240	20.00	0.07	0.036	(0.064)	0.007	0.028
241	20.08	0.10	0.053	(0.064)	0.011	0.043
242	20.17	0.10	0.053	(0.064)	0.011	0.043
243	20.25	0.10	0.053	(0.064)	0.011	0.043
244	20.33	0.10	0.053	(0.063)	0.011	0.043
245	20.42	0.10	0.053	(0.063)	0.011	0.043
246	20.50	0.10	0.053	(0.063)	0.011	0.043
247	20.58	0.10	0.053	(0.062)	0.011	0.043
248	20.67	0.10	0.053	(0.062)	0.011	0.043
249	20.75	0.10	0.053	(0.062)	0.011	0.043
250	20.83	0.07	0.036	(0.062)	0.007	0.028
251	20.92	0.07	0.036	(0.061)	0.007	0.028
252	21.00	0.07	0.036	(0.061)	0.007	0.028
253	21.08	0.10	0.053	(0.061)	0.011	0.043
254	21.17	0.10	0.053	(0.061)	0.011	0.043
255	21.25	0.10	0.053	(0.060)	0.011	0.043
256	21.33	0.07	0.036	(0.060)	0.007	0.028
257	21.42	0.07	0.036	(0.060)	0.007	0.028
258	21.50	0.07	0.036	(0.060)	0.007	0.028
259	21.58	0.10	0.053	(0.060)	0.011	0.043
260	21.67	0.10	0.053	(0.059)	0.011	0.043
261	21.75	0.10	0.053	(0.059)	0.011	0.043
262	21.83	0.07	0.036	(0.059)	0.007	0.028
263	21.92	0.07	0.036	(0.059)	0.007	0.028
264	22.00	0.07	0.036	(0.059)	0.007	0.028
265	22.08	0.10	0.053	(0.058)	0.011	0.043
266	22.17	0.10	0.053	(0.058)	0.011	0.043
267	22.25	0.10	0.053	(0.058)	0.011	0.043

268	22.33	0.07	0.036	(0.058)	0.007	0.028
269	22.42	0.07	0.036	(0.058)	0.007	0.028
270	22.50	0.07	0.036	(0.057)	0.007	0.028
271	22.58	0.07	0.036	(0.057)	0.007	0.028
272	22.67	0.07	0.036	(0.057)	0.007	0.028
273	22.75	0.07	0.036	(0.057)	0.007	0.028
274	22.83	0.07	0.036	(0.057)	0.007	0.028
275	22.92	0.07	0.036	(0.057)	0.007	0.028
276	23.00	0.07	0.036	(0.057)	0.007	0.028
277	23.08	0.07	0.036	(0.056)	0.007	0.028
278	23.17	0.07	0.036	(0.056)	0.007	0.028
279	23.25	0.07	0.036	(0.056)	0.007	0.028
280	23.33	0.07	0.036	(0.056)	0.007	0.028
281	23.42	0.07	0.036	(0.056)	0.007	0.028
282	23.50	0.07	0.036	(0.056)	0.007	0.028
283	23.58	0.07	0.036	(0.056)	0.007	0.028
284	23.67	0.07	0.036	(0.056)	0.007	0.028
285	23.75	0.07	0.036	(0.056)	0.007	0.028
286	23.83	0.07	0.036	(0.056)	0.007	0.028
287	23.92	0.07	0.036	(0.055)	0.007	0.028
288	24.00	0.07	0.036	(0.055)	0.007	0.028

(Loss Rate Not Used)

Sum = 100.0 Sum = 42.8

Flood volume = Effective rainfall 3.57(In)
times area 1.3(Ac.)/[(In)/(Ft.)] = 0.4(Ac.Ft)
Total soil loss = 0.87(In)
Total soil loss = 0.093(Ac.Ft)
Total rainfall = 4.44(In)
Flood volume = 16581.8 Cubic Feet
Total soil loss = 4048.2 Cubic Feet

Peak flow rate of this hydrograph = 0.657(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.02	Q	|	|	|	|
0+10	0.0004	0.03	Q	|	|	|	|
0+15	0.0006	0.04	Q	|	|	|	|
0+20	0.0010	0.05	Q	|	|	|	|
0+25	0.0013	0.05	Q	|	|	|	|
0+30	0.0017	0.06	Q	|	|	|	|
0+35	0.0021	0.06	Q	|	|	|	|
0+40	0.0025	0.06	Q	|	|	|	|
0+45	0.0028	0.06	Q	|	|	|	|
0+50	0.0033	0.07	Q	|	|	|	|
0+55	0.0038	0.07	Q	|	|	|	|

1+ 0	0.0043	0.07	Q	|	|	|	|
1+ 5	0.0047	0.06	Q	|	|	|	|
1+10	0.0051	0.06	Q	|	|	|	|
1+15	0.0055	0.06	Q	|	|	|	|
1+20	0.0059	0.06	Q	|	|	|	|
1+25	0.0063	0.06	Q	|	|	|	|
1+30	0.0066	0.06	Q	|	|	|	|
1+35	0.0070	0.06	Q	|	|	|	|
1+40	0.0074	0.06	Q	|	|	|	|
1+45	0.0078	0.06	Q	|	|	|	|
1+50	0.0082	0.07	Q	|	|	|	|
1+55	0.0087	0.07	Q	|	|	|	|
2+ 0	0.0092	0.07	Q	|	|	|	|
2+ 5	0.0097	0.07	QV	|	|	|	|
2+10	0.0102	0.07	QV	|	|	|	|
2+15	0.0107	0.07	QV	|	|	|	|
2+20	0.0112	0.07	QV	|	|	|	|
2+25	0.0117	0.07	QV	|	|	|	|
2+30	0.0123	0.07	QV	|	|	|	|
2+35	0.0128	0.08	QV	|	|	|	|
2+40	0.0135	0.09	QV	|	|	|	|
2+45	0.0141	0.09	QV	|	|	|	|
2+50	0.0147	0.09	QV	|	|	|	|
2+55	0.0153	0.09	QV	|	|	|	|
3+ 0	0.0160	0.09	QV	|	|	|	|
3+ 5	0.0166	0.09	QV	|	|	|	|
3+10	0.0172	0.09	QV	|	|	|	|
3+15	0.0179	0.09	QV	|	|	|	|
3+20	0.0185	0.09	QV	|	|	|	|
3+25	0.0191	0.09	Q V	|	|	|	|
3+30	0.0198	0.09	Q V	|	|	|	|
3+35	0.0204	0.09	Q V	|	|	|	|
3+40	0.0210	0.09	Q V	|	|	|	|
3+45	0.0217	0.09	Q V	|	|	|	|
3+50	0.0224	0.10	Q V	|	|	|	|
3+55	0.0231	0.11	Q V	|	|	|	|
4+ 0	0.0239	0.11	Q V	|	|	|	|
4+ 5	0.0246	0.11	Q V	|	|	|	|
4+10	0.0254	0.11	Q V	|	|	|	|
4+15	0.0261	0.11	Q V	|	|	|	|
4+20	0.0270	0.12	Q V	|	|	|	|
4+25	0.0278	0.13	Q V	|	|	|	|
4+30	0.0287	0.13	Q V	|	|	|	|
4+35	0.0296	0.13	Q V	|	|	|	|
4+40	0.0305	0.13	Q V	|	|	|	|
4+45	0.0314	0.13	Q V	|	|	|	|
4+50	0.0323	0.14	Q V	|	|	|	|
4+55	0.0333	0.15	Q V	|	|	|	|
5+ 0	0.0344	0.15	Q V	|	|	|	|
5+ 5	0.0352	0.13	Q V	|	|	|	|
5+10	0.0360	0.11	Q V	|	|	|	|
5+15	0.0368	0.11	Q V	|	|	|	|
5+20	0.0376	0.12	Q V	|	|	|	|

5+25	0.0385	0.13	Q	V	|	|	|	|
5+30	0.0393	0.13	Q	V	|	|	|	|
5+35	0.0403	0.14	Q	V	|	|	|	|
5+40	0.0413	0.15	Q	V	|	|	|	|
5+45	0.0423	0.15	Q	V	|	|	|	|
5+50	0.0433	0.15	Q	V	|	|	|	|
5+55	0.0443	0.15	Q	V	|	|	|	|
6+ 0	0.0453	0.15	Q	V	|	|	|	|
6+ 5	0.0464	0.16	Q	V	|	|	|	|
6+10	0.0476	0.16	Q	V	|	|	|	|
6+15	0.0487	0.17	Q	V	|	|	|	|
6+20	0.0498	0.17	Q	V	|	|	|	|
6+25	0.0510	0.17	Q	V	|	|	|	|
6+30	0.0521	0.17	Q	V	|	|	|	|
6+35	0.0533	0.18	Q	V	|	|	|	|
6+40	0.0546	0.18	Q	V	|	|	|	|
6+45	0.0558	0.18	Q	V	|	|	|	|
6+50	0.0571	0.18	Q	V	|	|	|	|
6+55	0.0583	0.18	Q	V	|	|	|	|
7+ 0	0.0596	0.18	Q	V	|	|	|	|
7+ 5	0.0609	0.18	Q	V	|	|	|	|
7+10	0.0621	0.18	Q	V	|	|	|	|
7+15	0.0634	0.18	Q	V	|	|	|	|
7+20	0.0647	0.19	Q	V	|	|	|	|
7+25	0.0661	0.20	Q	V	|	|	|	|
7+30	0.0675	0.20	Q	V	|	|	|	|
7+35	0.0690	0.21	Q	V	|	|	|	|
7+40	0.0705	0.22	Q	V	|	|	|	|
7+45	0.0720	0.22	Q	V	|	|	|	|
7+50	0.0736	0.23	Q	V	|	|	|	|
7+55	0.0752	0.24	Q	V	|	|	|	|
8+ 0	0.0769	0.24	Q	V	|	|	|	|
8+ 5	0.0786	0.26	|Q	V	|	|	|	|
8+10	0.0805	0.27	|Q	V	|	|	|	|
8+15	0.0824	0.28	|Q	V	|	|	|	|
8+20	0.0843	0.28	|Q	V	|	|	|	|
8+25	0.0862	0.28	|Q	V	|	|	|	|
8+30	0.0881	0.28	|Q	V	|	|	|	|
8+35	0.0901	0.29	|Q	V	|	|	|	|
8+40	0.0921	0.29	|Q	V	|	|	|	|
8+45	0.0941	0.29	|Q	V	|	|	|	|
8+50	0.0962	0.30	|Q	V	|	|	|	|
8+55	0.0983	0.31	|Q	V	|	|	|	|
9+ 0	0.1005	0.31	|Q	V	|	|	|	|
9+ 5	0.1028	0.33	|Q	V	|	|	|	|
9+10	0.1051	0.35	|Q	|V	|	|	|	|
9+15	0.1075	0.35	|Q	|V	|	|	|	|
9+20	0.1100	0.36	|Q	|V	|	|	|	|
9+25	0.1125	0.37	|Q	|V	|	|	|	|
9+30	0.1151	0.37	|Q	| V	|	|	|	|
9+35	0.1177	0.38	|Q	| V	|	|	|	|
9+40	0.1203	0.38	|Q	| V	|	|	|	|
9+45	0.1229	0.39	|Q	| V	|	|	|	|

9+50	0.1257	0.40	Q	V			
9+55	0.1284	0.40	Q	V			
10+ 0	0.1312	0.40	Q	V			
10+ 5	0.1335	0.33	Q	V			
10+10	0.1355	0.28	Q	V			
10+15	0.1373	0.28	Q	V			
10+20	0.1392	0.28	Q	V			
10+25	0.1411	0.28	Q	V			
10+30	0.1430	0.28	Q	V			
10+35	0.1453	0.33	Q	V			
10+40	0.1478	0.36	Q	V			
10+45	0.1503	0.37	Q	V			
10+50	0.1528	0.37	Q	V			
10+55	0.1553	0.37	Q	V			
11+ 0	0.1579	0.37	Q	V			
11+ 5	0.1603	0.36	Q	V			
11+10	0.1627	0.35	Q	V			
11+15	0.1651	0.35	Q	V			
11+20	0.1675	0.35	Q	V			
11+25	0.1699	0.35	Q	V			
11+30	0.1723	0.35	Q	V			
11+35	0.1746	0.33	Q	V			
11+40	0.1767	0.31	Q	V			
11+45	0.1789	0.31	Q	V			
11+50	0.1811	0.32	Q	V			
11+55	0.1834	0.33	Q	V			
12+ 0	0.1857	0.33	Q	V			
12+ 5	0.1884	0.40	Q	V			
12+10	0.1915	0.45	Q	V			
12+15	0.1947	0.46	Q	V			
12+20	0.1979	0.47	Q	V			
12+25	0.2012	0.48	Q	V			
12+30	0.2045	0.48	Q	V			
12+35	0.2079	0.50	Q	V			
12+40	0.2114	0.51	Q	V			
12+45	0.2150	0.51	Q	V			
12+50	0.2186	0.53	Q	V			
12+55	0.2223	0.54	Q	V			
13+ 0	0.2260	0.54	Q	V			
13+ 5	0.2301	0.60	Q	V			
13+10	0.2346	0.65	Q	V			
13+15	0.2391	0.65	Q	V			
13+20	0.2436	0.66	Q	V			
13+25	0.2481	0.66	Q	V			
13+30	0.2527	0.66	Q	V			
13+35	0.2563	0.53	Q	V			
13+40	0.2593	0.43	Q	V			
13+45	0.2622	0.42	Q	V			
13+50	0.2651	0.42	Q	V			
13+55	0.2680	0.42	Q	V			
14+ 0	0.2709	0.42	Q	V			
14+ 5	0.2741	0.47	Q	V			
14+10	0.2775	0.50	Q	V			

14+15	0.2810	0.50	| Q	|	|	V|	|
14+20	0.2843	0.49	|Q	|	|	V|	|
14+25	0.2877	0.48	|Q	|	|	V	|
14+30	0.2910	0.48	|Q	|	|	V	|
14+35	0.2943	0.48	|Q	|	|	V	|
14+40	0.2976	0.48	|Q	|	|	|V	|
14+45	0.3009	0.48	|Q	|	|	|V	|
14+50	0.3041	0.47	|Q	|	|	|V	|
14+55	0.3073	0.46	|Q	|	|	| V	|
15+ 0	0.3105	0.46	|Q	|	|	| V	|
15+ 5	0.3136	0.45	|Q	|	|	| V	|
15+10	0.3166	0.44	|Q	|	|	| V	|
15+15	0.3197	0.44	|Q	|	|	| V	|
15+20	0.3226	0.43	|Q	|	|	| V	|
15+25	0.3255	0.42	|Q	|	|	| V	|
15+30	0.3284	0.42	|Q	|	|	| V	|
15+35	0.3311	0.38	|Q	|	|	| V	|
15+40	0.3335	0.35	|Q	|	|	| V	|
15+45	0.3359	0.35	|Q	|	|	| V	|
15+50	0.3383	0.35	|Q	|	|	| V	|
15+55	0.3407	0.35	|Q	|	|	| V	|
16+ 0	0.3431	0.35	|Q	|	|	| V	|
16+ 5	0.3444	0.20	Q	|	|	| V	|
16+10	0.3451	0.09	Q	|	|	| V	|
16+15	0.3456	0.07	Q	|	|	| V	|
16+20	0.3461	0.07	Q	|	|	| V	|
16+25	0.3466	0.07	Q	|	|	| V	|
16+30	0.3471	0.07	Q	|	|	| V	|
16+35	0.3475	0.06	Q	|	|	| V	|
16+40	0.3479	0.06	Q	|	|	| V	|
16+45	0.3483	0.06	Q	|	|	| V	|
16+50	0.3487	0.06	Q	|	|	| V	|
16+55	0.3490	0.06	Q	|	|	| V	|
17+ 0	0.3494	0.06	Q	|	|	| V	|
17+ 5	0.3499	0.08	Q	|	|	| V	|
17+10	0.3505	0.09	Q	|	|	| V	|
17+15	0.3512	0.09	Q	|	|	| V	|
17+20	0.3518	0.09	Q	|	|	| V	|
17+25	0.3524	0.09	Q	|	|	| V	|
17+30	0.3531	0.09	Q	|	|	| V	|
17+35	0.3537	0.09	Q	|	|	| V	|
17+40	0.3543	0.09	Q	|	|	| V	|
17+45	0.3550	0.09	Q	|	|	| V	|
17+50	0.3555	0.08	Q	|	|	| V	|
17+55	0.3560	0.07	Q	|	|	| V	|
18+ 0	0.3565	0.07	Q	|	|	| V	|
18+ 5	0.3570	0.07	Q	|	|	| V	|
18+10	0.3576	0.07	Q	|	|	| V	|
18+15	0.3581	0.07	Q	|	|	| V	|
18+20	0.3586	0.07	Q	|	|	| V	|
18+25	0.3591	0.07	Q	|	|	| V	|
18+30	0.3596	0.07	Q	|	|	| V	|
18+35	0.3600	0.06	Q	|	|	| V	|

18+40	0.3604	0.06	Q	|	|	|	V |
18+45	0.3608	0.06	Q	|	|	|	V |
18+50	0.3611	0.04	Q	|	|	|	V |
18+55	0.3613	0.04	Q	|	|	|	V |
19+ 0	0.3616	0.04	Q	|	|	|	V |
19+ 5	0.3619	0.05	Q	|	|	|	V |
19+10	0.3623	0.05	Q	|	|	|	V |
19+15	0.3627	0.06	Q	|	|	|	V |
19+20	0.3631	0.07	Q	|	|	|	V |
19+25	0.3636	0.07	Q	|	|	|	V |
19+30	0.3641	0.07	Q	|	|	|	V |
19+35	0.3646	0.06	Q	|	|	|	V |
19+40	0.3649	0.06	Q	|	|	|	V |
19+45	0.3653	0.06	Q	|	|	|	V |
19+50	0.3656	0.04	Q	|	|	|	V |
19+55	0.3659	0.04	Q	|	|	|	V |
20+ 0	0.3661	0.04	Q	|	|	|	V |
20+ 5	0.3665	0.05	Q	|	|	|	V |
20+10	0.3668	0.05	Q	|	|	|	V |
20+15	0.3672	0.06	Q	|	|	|	V |
20+20	0.3676	0.06	Q	|	|	|	V |
20+25	0.3680	0.06	Q	|	|	|	V |
20+30	0.3684	0.06	Q	|	|	|	V |
20+35	0.3687	0.06	Q	|	|	|	V |
20+40	0.3691	0.06	Q	|	|	|	V |
20+45	0.3695	0.06	Q	|	|	|	V |
20+50	0.3698	0.04	Q	|	|	|	V |
20+55	0.3701	0.04	Q	|	|	|	V |
21+ 0	0.3703	0.04	Q	|	|	|	V |
21+ 5	0.3706	0.05	Q	|	|	|	V |
21+10	0.3710	0.05	Q	|	|	|	V |
21+15	0.3714	0.06	Q	|	|	|	V|
21+20	0.3717	0.04	Q	|	|	|	V|
21+25	0.3720	0.04	Q	|	|	|	V|
21+30	0.3722	0.04	Q	|	|	|	V|
21+35	0.3725	0.05	Q	|	|	|	V|
21+40	0.3729	0.05	Q	|	|	|	V|
21+45	0.3733	0.06	Q	|	|	|	V|
21+50	0.3736	0.04	Q	|	|	|	V|
21+55	0.3738	0.04	Q	|	|	|	V|
22+ 0	0.3741	0.04	Q	|	|	|	V|
22+ 5	0.3744	0.05	Q	|	|	|	V|
22+10	0.3748	0.05	Q	|	|	|	V|
22+15	0.3752	0.06	Q	|	|	|	V|
22+20	0.3755	0.04	Q	|	|	|	V|
22+25	0.3757	0.04	Q	|	|	|	V|
22+30	0.3760	0.04	Q	|	|	|	V|
22+35	0.3762	0.04	Q	|	|	|	V|
22+40	0.3765	0.04	Q	|	|	|	V|
22+45	0.3768	0.04	Q	|	|	|	V|
22+50	0.3770	0.04	Q	|	|	|	V|
22+55	0.3773	0.04	Q	|	|	|	V|
23+ 0	0.3775	0.04	Q	|	|	|	V|

```
   23+ 5       0.3778      0.04  Q          |          |          |         V|
   23+10       0.3780      0.04  Q          |          |          |         V|
   23+15       0.3783      0.04  Q          |          |          |         V|
   23+20       0.3785      0.04  Q          |          |          |         V|
   23+25       0.3788      0.04  Q          |          |          |         V|
   23+30       0.3790      0.04  Q          |          |          |         V|
   23+35       0.3793      0.04  Q          |          |          |         V|
   23+40       0.3795      0.04  Q          |          |          |         V|
   23+45       0.3798      0.04  Q          |          |          |         V|
   23+50       0.3800      0.04  Q          |          |          |         V|
   23+55       0.3803      0.04  Q          |          |          |         V|
   24+ 0       0.3805      0.04  Q          |          |          |         V|
   24+ 5       0.3807      0.02  Q          |          |          |         V|
   24+10       0.3807      0.00  Q          |          |          |          V
-------------------------------------------------------------------------------
```

AREA AA1

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014, Version 9.0
Study date 02/05/24 File: ARAA124100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6279

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

PROPOSED CONDITION: 100YR HYDROLOGY
ARAA1

Drainage Area = 1.23(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.23(Ac.) = 0.002 Sq. Mi.
Length along longest watercourse = 644.00(Ft.)
Length along longest watercourse measured to centroid = 322.00(Ft.)
Length along longest watercourse = 0.122 Mi.
Length along longest watercourse measured to centroid = 0.061 Mi.
Difference in elevation = 4.50(Ft.)
Slope along watercourse = 36.8944 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.028 Hr.
Lag time = 1.69 Min.
25% of lag time = 0.42 Min.
40% of lag time = 0.68 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.23	1.16	1.43

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.23	4.44	5.46

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.160(In)
Area Averaged 100-Year Rainfall = 4.440(In)

Point rain (area averaged) = 4.440(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 4.440(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.230	56.00	0.850

Total Area Entered = 1.23(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.850	0.120	1.000	0.120
					Sum (F) =	0.120

Area averaged mean soil loss (F) (In/Hr) = 0.120
Minimum soil loss rate ((In/Hr)) = 0.060
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.220

U n i t H y d r o g r a p h
DESERT S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	295.855	55.690	0.690
2	0.167	591.710	39.018	0.484
3	0.250	887.565	5.292	0.066
		Sum = 100.000	Sum=	1.240

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.036	(0.213)	0.008	0.028
2	0.17	0.07	0.036	(0.212)	0.008	0.028

3	0.25	0.07	0.036	(0.211)	0.008	0.028
4	0.33	0.10	0.053	(0.210)	0.012	0.042
5	0.42	0.10	0.053	(0.210)	0.012	0.042
6	0.50	0.10	0.053	(0.209)	0.012	0.042
7	0.58	0.10	0.053	(0.208)	0.012	0.042
8	0.67	0.10	0.053	(0.207)	0.012	0.042
9	0.75	0.10	0.053	(0.206)	0.012	0.042
10	0.83	0.13	0.071	(0.205)	0.016	0.055
11	0.92	0.13	0.071	(0.205)	0.016	0.055
12	1.00	0.13	0.071	(0.204)	0.016	0.055
13	1.08	0.10	0.053	(0.203)	0.012	0.042
14	1.17	0.10	0.053	(0.202)	0.012	0.042
15	1.25	0.10	0.053	(0.201)	0.012	0.042
16	1.33	0.10	0.053	(0.201)	0.012	0.042
17	1.42	0.10	0.053	(0.200)	0.012	0.042
18	1.50	0.10	0.053	(0.199)	0.012	0.042
19	1.58	0.10	0.053	(0.198)	0.012	0.042
20	1.67	0.10	0.053	(0.197)	0.012	0.042
21	1.75	0.10	0.053	(0.197)	0.012	0.042
22	1.83	0.13	0.071	(0.196)	0.016	0.055
23	1.92	0.13	0.071	(0.195)	0.016	0.055
24	2.00	0.13	0.071	(0.194)	0.016	0.055
25	2.08	0.13	0.071	(0.193)	0.016	0.055
26	2.17	0.13	0.071	(0.193)	0.016	0.055
27	2.25	0.13	0.071	(0.192)	0.016	0.055
28	2.33	0.13	0.071	(0.191)	0.016	0.055
29	2.42	0.13	0.071	(0.190)	0.016	0.055
30	2.50	0.13	0.071	(0.190)	0.016	0.055
31	2.58	0.17	0.089	(0.189)	0.020	0.069
32	2.67	0.17	0.089	(0.188)	0.020	0.069
33	2.75	0.17	0.089	(0.187)	0.020	0.069
34	2.83	0.17	0.089	(0.186)	0.020	0.069
35	2.92	0.17	0.089	(0.186)	0.020	0.069
36	3.00	0.17	0.089	(0.185)	0.020	0.069
37	3.08	0.17	0.089	(0.184)	0.020	0.069
38	3.17	0.17	0.089	(0.183)	0.020	0.069
39	3.25	0.17	0.089	(0.183)	0.020	0.069
40	3.33	0.17	0.089	(0.182)	0.020	0.069
41	3.42	0.17	0.089	(0.181)	0.020	0.069
42	3.50	0.17	0.089	(0.180)	0.020	0.069
43	3.58	0.17	0.089	(0.180)	0.020	0.069
44	3.67	0.17	0.089	(0.179)	0.020	0.069
45	3.75	0.17	0.089	(0.178)	0.020	0.069
46	3.83	0.20	0.107	(0.177)	0.023	0.083
47	3.92	0.20	0.107	(0.177)	0.023	0.083
48	4.00	0.20	0.107	(0.176)	0.023	0.083
49	4.08	0.20	0.107	(0.175)	0.023	0.083
50	4.17	0.20	0.107	(0.174)	0.023	0.083
51	4.25	0.20	0.107	(0.174)	0.023	0.083
52	4.33	0.23	0.124	(0.173)	0.027	0.097
53	4.42	0.23	0.124	(0.172)	0.027	0.097
54	4.50	0.23	0.124	(0.171)	0.027	0.097
55	4.58	0.23	0.124	(0.171)	0.027	0.097

56	4.67	0.23	0.124	(0.170)	0.027	0.097
57	4.75	0.23	0.124	(0.169)	0.027	0.097
58	4.83	0.27	0.142	(0.168)	0.031	0.111
59	4.92	0.27	0.142	(0.168)	0.031	0.111
60	5.00	0.27	0.142	(0.167)	0.031	0.111
61	5.08	0.20	0.107	(0.166)	0.023	0.083
62	5.17	0.20	0.107	(0.166)	0.023	0.083
63	5.25	0.20	0.107	(0.165)	0.023	0.083
64	5.33	0.23	0.124	(0.164)	0.027	0.097
65	5.42	0.23	0.124	(0.163)	0.027	0.097
66	5.50	0.23	0.124	(0.163)	0.027	0.097
67	5.58	0.27	0.142	(0.162)	0.031	0.111
68	5.67	0.27	0.142	(0.161)	0.031	0.111
69	5.75	0.27	0.142	(0.161)	0.031	0.111
70	5.83	0.27	0.142	(0.160)	0.031	0.111
71	5.92	0.27	0.142	(0.159)	0.031	0.111
72	6.00	0.27	0.142	(0.158)	0.031	0.111
73	6.08	0.30	0.160	(0.158)	0.035	0.125
74	6.17	0.30	0.160	(0.157)	0.035	0.125
75	6.25	0.30	0.160	(0.156)	0.035	0.125
76	6.33	0.30	0.160	(0.156)	0.035	0.125
77	6.42	0.30	0.160	(0.155)	0.035	0.125
78	6.50	0.30	0.160	(0.154)	0.035	0.125
79	6.58	0.33	0.178	(0.154)	0.039	0.139
80	6.67	0.33	0.178	(0.153)	0.039	0.139
81	6.75	0.33	0.178	(0.152)	0.039	0.139
82	6.83	0.33	0.178	(0.151)	0.039	0.139
83	6.92	0.33	0.178	(0.151)	0.039	0.139
84	7.00	0.33	0.178	(0.150)	0.039	0.139
85	7.08	0.33	0.178	(0.149)	0.039	0.139
86	7.17	0.33	0.178	(0.149)	0.039	0.139
87	7.25	0.33	0.178	(0.148)	0.039	0.139
88	7.33	0.37	0.195	(0.147)	0.043	0.152
89	7.42	0.37	0.195	(0.147)	0.043	0.152
90	7.50	0.37	0.195	(0.146)	0.043	0.152
91	7.58	0.40	0.213	(0.145)	0.047	0.166
92	7.67	0.40	0.213	(0.145)	0.047	0.166
93	7.75	0.40	0.213	(0.144)	0.047	0.166
94	7.83	0.43	0.231	(0.143)	0.051	0.180
95	7.92	0.43	0.231	(0.143)	0.051	0.180
96	8.00	0.43	0.231	(0.142)	0.051	0.180
97	8.08	0.50	0.266	(0.141)	0.059	0.208
98	8.17	0.50	0.266	(0.141)	0.059	0.208
99	8.25	0.50	0.266	(0.140)	0.059	0.208
100	8.33	0.50	0.266	(0.139)	0.059	0.208
101	8.42	0.50	0.266	(0.139)	0.059	0.208
102	8.50	0.50	0.266	(0.138)	0.059	0.208
103	8.58	0.53	0.284	(0.137)	0.063	0.222
104	8.67	0.53	0.284	(0.137)	0.063	0.222
105	8.75	0.53	0.284	(0.136)	0.063	0.222
106	8.83	0.57	0.302	(0.136)	0.066	0.235
107	8.92	0.57	0.302	(0.135)	0.066	0.235
108	9.00	0.57	0.302	(0.134)	0.066	0.235

109	9.08	0.63	0.337	(0.134)	0.074	0.263
110	9.17	0.63	0.337	(0.133)	0.074	0.263
111	9.25	0.63	0.337	(0.132)	0.074	0.263
112	9.33	0.67	0.355	(0.132)	0.078	0.277
113	9.42	0.67	0.355	(0.131)	0.078	0.277
114	9.50	0.67	0.355	(0.130)	0.078	0.277
115	9.58	0.70	0.373	(0.130)	0.082	0.291
116	9.67	0.70	0.373	(0.129)	0.082	0.291
117	9.75	0.70	0.373	(0.129)	0.082	0.291
118	9.83	0.73	0.391	(0.128)	0.086	0.305
119	9.92	0.73	0.391	(0.127)	0.086	0.305
120	10.00	0.73	0.391	(0.127)	0.086	0.305
121	10.08	0.50	0.266	(0.126)	0.059	0.208
122	10.17	0.50	0.266	(0.126)	0.059	0.208
123	10.25	0.50	0.266	(0.125)	0.059	0.208
124	10.33	0.50	0.266	(0.124)	0.059	0.208
125	10.42	0.50	0.266	(0.124)	0.059	0.208
126	10.50	0.50	0.266	(0.123)	0.059	0.208
127	10.58	0.67	0.355	(0.123)	0.078	0.277
128	10.67	0.67	0.355	(0.122)	0.078	0.277
129	10.75	0.67	0.355	(0.121)	0.078	0.277
130	10.83	0.67	0.355	(0.121)	0.078	0.277
131	10.92	0.67	0.355	(0.120)	0.078	0.277
132	11.00	0.67	0.355	(0.120)	0.078	0.277
133	11.08	0.63	0.337	(0.119)	0.074	0.263
134	11.17	0.63	0.337	(0.118)	0.074	0.263
135	11.25	0.63	0.337	(0.118)	0.074	0.263
136	11.33	0.63	0.337	(0.117)	0.074	0.263
137	11.42	0.63	0.337	(0.117)	0.074	0.263
138	11.50	0.63	0.337	(0.116)	0.074	0.263
139	11.58	0.57	0.302	(0.115)	0.066	0.235
140	11.67	0.57	0.302	(0.115)	0.066	0.235
141	11.75	0.57	0.302	(0.114)	0.066	0.235
142	11.83	0.60	0.320	(0.114)	0.070	0.249
143	11.92	0.60	0.320	(0.113)	0.070	0.249
144	12.00	0.60	0.320	(0.113)	0.070	0.249
145	12.08	0.83	0.444	(0.112)	0.098	0.346
146	12.17	0.83	0.444	(0.111)	0.098	0.346
147	12.25	0.83	0.444	(0.111)	0.098	0.346
148	12.33	0.87	0.462	(0.110)	0.102	0.360
149	12.42	0.87	0.462	(0.110)	0.102	0.360
150	12.50	0.87	0.462	(0.109)	0.102	0.360
151	12.58	0.93	0.497	0.109	(0.109)	0.389
152	12.67	0.93	0.497	0.108	(0.109)	0.389
153	12.75	0.93	0.497	0.108	(0.109)	0.390
154	12.83	0.97	0.515	0.107	(0.113)	0.408
155	12.92	0.97	0.515	0.107	(0.113)	0.408
156	13.00	0.97	0.515	0.106	(0.113)	0.409
157	13.08	1.13	0.604	0.105	(0.133)	0.498
158	13.17	1.13	0.604	0.105	(0.133)	0.499
159	13.25	1.13	0.604	0.104	(0.133)	0.499
160	13.33	1.13	0.604	0.104	(0.133)	0.500
161	13.42	1.13	0.604	0.103	(0.133)	0.500

162	13.50	1.13	0.604		0.103	(0.133)	0.501
163	13.58	0.77	0.408	(	0.102)	0.090	0.319
164	13.67	0.77	0.408	(	0.102)	0.090	0.319
165	13.75	0.77	0.408	(	0.101)	0.090	0.319
166	13.83	0.77	0.408	(	0.101)	0.090	0.319
167	13.92	0.77	0.408	(	0.100)	0.090	0.319
168	14.00	0.77	0.408	(	0.100)	0.090	0.319
169	14.08	0.90	0.480		0.099	(0.105)	0.380
170	14.17	0.90	0.480		0.099	(0.105)	0.381
171	14.25	0.90	0.480		0.098	(0.105)	0.381
172	14.33	0.87	0.462		0.098	(0.102)	0.364
173	14.42	0.87	0.462		0.097	(0.102)	0.365
174	14.50	0.87	0.462		0.097	(0.102)	0.365
175	14.58	0.87	0.462		0.096	(0.102)	0.366
176	14.67	0.87	0.462		0.096	(0.102)	0.366
177	14.75	0.87	0.462		0.095	(0.102)	0.367
178	14.83	0.83	0.444		0.095	(0.098)	0.349
179	14.92	0.83	0.444		0.094	(0.098)	0.350
180	15.00	0.83	0.444		0.094	(0.098)	0.350
181	15.08	0.80	0.426		0.093	(0.094)	0.333
182	15.17	0.80	0.426		0.093	(0.094)	0.333
183	15.25	0.80	0.426		0.092	(0.094)	0.334
184	15.33	0.77	0.408	(	0.092)	0.090	0.319
185	15.42	0.77	0.408	(	0.091)	0.090	0.319
186	15.50	0.77	0.408	(	0.091)	0.090	0.319
187	15.58	0.63	0.337	(	0.090)	0.074	0.263
188	15.67	0.63	0.337	(	0.090)	0.074	0.263
189	15.75	0.63	0.337	(	0.090)	0.074	0.263
190	15.83	0.63	0.337	(	0.089)	0.074	0.263
191	15.92	0.63	0.337	(	0.089)	0.074	0.263
192	16.00	0.63	0.337	(	0.088)	0.074	0.263
193	16.08	0.13	0.071	(	0.088)	0.016	0.055
194	16.17	0.13	0.071	(	0.087)	0.016	0.055
195	16.25	0.13	0.071	(	0.087)	0.016	0.055
196	16.33	0.13	0.071	(	0.086)	0.016	0.055
197	16.42	0.13	0.071	(	0.086)	0.016	0.055
198	16.50	0.13	0.071	(	0.085)	0.016	0.055
199	16.58	0.10	0.053	(	0.085)	0.012	0.042
200	16.67	0.10	0.053	(	0.085)	0.012	0.042
201	16.75	0.10	0.053	(	0.084)	0.012	0.042
202	16.83	0.10	0.053	(	0.084)	0.012	0.042
203	16.92	0.10	0.053	(	0.083)	0.012	0.042
204	17.00	0.10	0.053	(	0.083)	0.012	0.042
205	17.08	0.17	0.089	(	0.082)	0.020	0.069
206	17.17	0.17	0.089	(	0.082)	0.020	0.069
207	17.25	0.17	0.089	(	0.082)	0.020	0.069
208	17.33	0.17	0.089	(	0.081)	0.020	0.069
209	17.42	0.17	0.089	(	0.081)	0.020	0.069
210	17.50	0.17	0.089	(	0.080)	0.020	0.069
211	17.58	0.17	0.089	(	0.080)	0.020	0.069
212	17.67	0.17	0.089	(	0.080)	0.020	0.069
213	17.75	0.17	0.089	(	0.079)	0.020	0.069
214	17.83	0.13	0.071	(	0.079)	0.016	0.055

215	17.92	0.13	0.071	(0.078)	0.016	0.055
216	18.00	0.13	0.071	(0.078)	0.016	0.055
217	18.08	0.13	0.071	(0.078)	0.016	0.055
218	18.17	0.13	0.071	(0.077)	0.016	0.055
219	18.25	0.13	0.071	(0.077)	0.016	0.055
220	18.33	0.13	0.071	(0.077)	0.016	0.055
221	18.42	0.13	0.071	(0.076)	0.016	0.055
222	18.50	0.13	0.071	(0.076)	0.016	0.055
223	18.58	0.10	0.053	(0.075)	0.012	0.042
224	18.67	0.10	0.053	(0.075)	0.012	0.042
225	18.75	0.10	0.053	(0.075)	0.012	0.042
226	18.83	0.07	0.036	(0.074)	0.008	0.028
227	18.92	0.07	0.036	(0.074)	0.008	0.028
228	19.00	0.07	0.036	(0.074)	0.008	0.028
229	19.08	0.10	0.053	(0.073)	0.012	0.042
230	19.17	0.10	0.053	(0.073)	0.012	0.042
231	19.25	0.10	0.053	(0.073)	0.012	0.042
232	19.33	0.13	0.071	(0.072)	0.016	0.055
233	19.42	0.13	0.071	(0.072)	0.016	0.055
234	19.50	0.13	0.071	(0.072)	0.016	0.055
235	19.58	0.10	0.053	(0.071)	0.012	0.042
236	19.67	0.10	0.053	(0.071)	0.012	0.042
237	19.75	0.10	0.053	(0.071)	0.012	0.042
238	19.83	0.07	0.036	(0.070)	0.008	0.028
239	19.92	0.07	0.036	(0.070)	0.008	0.028
240	20.00	0.07	0.036	(0.070)	0.008	0.028
241	20.08	0.10	0.053	(0.069)	0.012	0.042
242	20.17	0.10	0.053	(0.069)	0.012	0.042
243	20.25	0.10	0.053	(0.069)	0.012	0.042
244	20.33	0.10	0.053	(0.068)	0.012	0.042
245	20.42	0.10	0.053	(0.068)	0.012	0.042
246	20.50	0.10	0.053	(0.068)	0.012	0.042
247	20.58	0.10	0.053	(0.068)	0.012	0.042
248	20.67	0.10	0.053	(0.067)	0.012	0.042
249	20.75	0.10	0.053	(0.067)	0.012	0.042
250	20.83	0.07	0.036	(0.067)	0.008	0.028
251	20.92	0.07	0.036	(0.067)	0.008	0.028
252	21.00	0.07	0.036	(0.066)	0.008	0.028
253	21.08	0.10	0.053	(0.066)	0.012	0.042
254	21.17	0.10	0.053	(0.066)	0.012	0.042
255	21.25	0.10	0.053	(0.065)	0.012	0.042
256	21.33	0.07	0.036	(0.065)	0.008	0.028
257	21.42	0.07	0.036	(0.065)	0.008	0.028
258	21.50	0.07	0.036	(0.065)	0.008	0.028
259	21.58	0.10	0.053	(0.065)	0.012	0.042
260	21.67	0.10	0.053	(0.064)	0.012	0.042
261	21.75	0.10	0.053	(0.064)	0.012	0.042
262	21.83	0.07	0.036	(0.064)	0.008	0.028
263	21.92	0.07	0.036	(0.064)	0.008	0.028
264	22.00	0.07	0.036	(0.063)	0.008	0.028
265	22.08	0.10	0.053	(0.063)	0.012	0.042
266	22.17	0.10	0.053	(0.063)	0.012	0.042
267	22.25	0.10	0.053	(0.063)	0.012	0.042

268	22.33	0.07	0.036	(0.063)	0.008	0.028
269	22.42	0.07	0.036	(0.062)	0.008	0.028
270	22.50	0.07	0.036	(0.062)	0.008	0.028
271	22.58	0.07	0.036	(0.062)	0.008	0.028
272	22.67	0.07	0.036	(0.062)	0.008	0.028
273	22.75	0.07	0.036	(0.062)	0.008	0.028
274	22.83	0.07	0.036	(0.062)	0.008	0.028
275	22.92	0.07	0.036	(0.061)	0.008	0.028
276	23.00	0.07	0.036	(0.061)	0.008	0.028
277	23.08	0.07	0.036	(0.061)	0.008	0.028
278	23.17	0.07	0.036	(0.061)	0.008	0.028
279	23.25	0.07	0.036	(0.061)	0.008	0.028
280	23.33	0.07	0.036	(0.061)	0.008	0.028
281	23.42	0.07	0.036	(0.061)	0.008	0.028
282	23.50	0.07	0.036	(0.060)	0.008	0.028
283	23.58	0.07	0.036	(0.060)	0.008	0.028
284	23.67	0.07	0.036	(0.060)	0.008	0.028
285	23.75	0.07	0.036	(0.060)	0.008	0.028
286	23.83	0.07	0.036	(0.060)	0.008	0.028
287	23.92	0.07	0.036	(0.060)	0.008	0.028
288	24.00	0.07	0.036	(0.060)	0.008	0.028

(Loss Rate Not Used)

Sum = 100.0 Sum = 41.8

Flood volume = Effective rainfall 3.48(In)
times area 1.2(Ac.)/[(In)/(Ft.)] = 0.4(Ac.Ft)
Total soil loss = 0.96(In)
Total soil loss = 0.098(Ac.Ft)
Total rainfall = 4.44(In)
Flood volume = 15559.8 Cubic Feet
Total soil loss = 4264.3 Cubic Feet

Peak flow rate of this hydrograph = 0.621(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.02	Q	|	|	|	|
0+10	0.0004	0.03	Q	|	|	|	|
0+15	0.0006	0.03	Q	|	|	|	|
0+20	0.0009	0.04	Q	|	|	|	|
0+25	0.0012	0.05	Q	|	|	|	|
0+30	0.0016	0.05	Q	|	|	|	|
0+35	0.0020	0.05	Q	|	|	|	|
0+40	0.0023	0.05	Q	|	|	|	|
0+45	0.0027	0.05	Q	|	|	|	|
0+50	0.0031	0.06	Q	|	|	|	|
0+55	0.0036	0.07	Q	|	|	|	|

1+ 0	0.0040	0.07	Q	|	|	|	|
1+ 5	0.0044	0.06	Q	|	|	|	|
1+10	0.0048	0.05	Q	|	|	|	|
1+15	0.0051	0.05	Q	|	|	|	|
1+20	0.0055	0.05	Q	|	|	|	|
1+25	0.0059	0.05	Q	|	|	|	|
1+30	0.0062	0.05	Q	|	|	|	|
1+35	0.0066	0.05	Q	|	|	|	|
1+40	0.0069	0.05	Q	|	|	|	|
1+45	0.0073	0.05	Q	|	|	|	|
1+50	0.0077	0.06	Q	|	|	|	|
1+55	0.0082	0.07	Q	|	|	|	|
2+ 0	0.0086	0.07	Q	|	|	|	|
2+ 5	0.0091	0.07	QV	|	|	|	|
2+10	0.0096	0.07	QV	|	|	|	|
2+15	0.0101	0.07	QV	|	|	|	|
2+20	0.0105	0.07	QV	|	|	|	|
2+25	0.0110	0.07	QV	|	|	|	|
2+30	0.0115	0.07	QV	|	|	|	|
2+35	0.0120	0.08	QV	|	|	|	|
2+40	0.0126	0.08	QV	|	|	|	|
2+45	0.0132	0.09	QV	|	|	|	|
2+50	0.0138	0.09	QV	|	|	|	|
2+55	0.0144	0.09	QV	|	|	|	|
3+ 0	0.0150	0.09	QV	|	|	|	|
3+ 5	0.0156	0.09	QV	|	|	|	|
3+10	0.0162	0.09	QV	|	|	|	|
3+15	0.0167	0.09	QV	|	|	|	|
3+20	0.0173	0.09	QV	|	|	|	|
3+25	0.0179	0.09	Q V	|	|	|	|
3+30	0.0185	0.09	Q V	|	|	|	|
3+35	0.0191	0.09	Q V	|	|	|	|
3+40	0.0197	0.09	Q V	|	|	|	|
3+45	0.0203	0.09	Q V	|	|	|	|
3+50	0.0210	0.10	Q V	|	|	|	|
3+55	0.0217	0.10	Q V	|	|	|	|
4+ 0	0.0224	0.10	Q V	|	|	|	|
4+ 5	0.0231	0.10	Q V	|	|	|	|
4+10	0.0238	0.10	Q V	|	|	|	|
4+15	0.0245	0.10	Q V	|	|	|	|
4+20	0.0253	0.11	Q V	|	|	|	|
4+25	0.0261	0.12	Q V	|	|	|	|
4+30	0.0269	0.12	Q V	|	|	|	|
4+35	0.0278	0.12	Q V	|	|	|	|
4+40	0.0286	0.12	Q V	|	|	|	|
4+45	0.0294	0.12	Q V	|	|	|	|
4+50	0.0303	0.13	Q V	|	|	|	|
4+55	0.0312	0.14	Q V	|	|	|	|
5+ 0	0.0322	0.14	Q V	|	|	|	|
5+ 5	0.0330	0.12	Q V	|	|	|	|
5+10	0.0337	0.10	Q V	|	|	|	|
5+15	0.0344	0.10	Q V	|	|	|	|
5+20	0.0352	0.11	Q V	|	|	|	|

5+25	0.0360	0.12	Q	V	|	|	|	|
5+30	0.0369	0.12	Q	V	|	|	|	|
5+35	0.0378	0.13	Q	V	|	|	|	|
5+40	0.0387	0.14	Q	V	|	|	|	|
5+45	0.0396	0.14	Q	V	|	|	|	|
5+50	0.0406	0.14	Q	V	|	|	|	|
5+55	0.0415	0.14	Q	V	|	|	|	|
6+ 0	0.0425	0.14	Q	V	|	|	|	|
6+ 5	0.0435	0.15	Q	V	|	|	|	|
6+10	0.0446	0.15	Q	V	|	|	|	|
6+15	0.0456	0.15	Q	V	|	|	|	|
6+20	0.0467	0.15	Q	V	|	|	|	|
6+25	0.0477	0.15	Q	V	|	|	|	|
6+30	0.0488	0.15	Q	V	|	|	|	|
6+35	0.0499	0.16	Q	V	|	|	|	|
6+40	0.0511	0.17	Q	V	|	|	|	|
6+45	0.0523	0.17	Q	V	|	|	|	|
6+50	0.0535	0.17	Q	V	|	|	|	|
6+55	0.0547	0.17	Q	V	|	|	|	|
7+ 0	0.0559	0.17	Q	V	|	|	|	|
7+ 5	0.0570	0.17	Q	V	|	|	|	|
7+10	0.0582	0.17	Q	V	|	|	|	|
7+15	0.0594	0.17	Q	V	|	|	|	|
7+20	0.0607	0.18	Q	V	|	|	|	|
7+25	0.0619	0.19	Q	V	|	|	|	|
7+30	0.0633	0.19	Q	V	|	|	|	|
7+35	0.0646	0.20	Q	V	|	|	|	|
7+40	0.0660	0.21	Q	V	|	|	|	|
7+45	0.0675	0.21	Q	V	|	|	|	|
7+50	0.0689	0.22	Q	V	|	|	|	|
7+55	0.0705	0.22	Q	V	|	|	|	|
8+ 0	0.0720	0.22	Q	V	|	|	|	|
8+ 5	0.0737	0.24	Q	V	|	|	|	|
8+10	0.0754	0.26	|Q	V	|	|	|	|
8+15	0.0772	0.26	|Q	V	|	|	|	|
8+20	0.0790	0.26	|Q	V	|	|	|	|
8+25	0.0808	0.26	|Q	V	|	|	|	|
8+30	0.0825	0.26	|Q	V	|	|	|	|
8+35	0.0844	0.27	|Q	V	|	|	|	|
8+40	0.0863	0.27	|Q	V	|	|	|	|
8+45	0.0882	0.27	|Q	V	|	|	|	|
8+50	0.0901	0.28	|Q	V	|	|	|	|
8+55	0.0921	0.29	|Q	V	|	|	|	|
9+ 0	0.0941	0.29	|Q	V	|	|	|	|
9+ 5	0.0963	0.31	|Q	V	|	|	|	|
9+10	0.0985	0.32	|Q	|V	|	|	|	|
9+15	0.1008	0.33	|Q	|V	|	|	|	|
9+20	0.1031	0.34	|Q	|V	|	|	|	|
9+25	0.1054	0.34	|Q	|V	|	|	|	|
9+30	0.1078	0.34	|Q	| V	|	|	|	|
9+35	0.1102	0.35	|Q	| V	|	|	|	|
9+40	0.1127	0.36	|Q	| V	|	|	|	|
9+45	0.1152	0.36	|Q	| V	|	|	|	|

```
 9+50       0.1178      0.37  |Q        |  V      |         |         |
 9+55       0.1203      0.38  |Q        |  V      |         |         |
10+ 0       0.1230      0.38  |Q        |  V      |         |         |
10+ 5       0.1251      0.31  |Q        |   V     |         |         |
10+10       0.1269      0.26  |Q        |   V     |         |         |
10+15       0.1287      0.26  |Q        |   V     |         |         |
10+20       0.1305      0.26  |Q        |   V     |         |         |
10+25       0.1322      0.26  |Q        |   V     |         |         |
10+30       0.1340      0.26  |Q        |    V    |         |         |
10+35       0.1361      0.31  |Q        |    V    |         |         |
10+40       0.1385      0.34  |Q        |    V    |         |         |
10+45       0.1408      0.34  |Q        |    V    |         |         |
10+50       0.1432      0.34  |Q        |     V   |         |         |
10+55       0.1456      0.34  |Q        |     V   |         |         |
11+ 0       0.1479      0.34  |Q        |     V   |         |         |
11+ 5       0.1502      0.33  |Q        |     V   |         |         |
11+10       0.1525      0.33  |Q        |      V  |         |         |
11+15       0.1547      0.33  |Q        |      V  |         |         |
11+20       0.1570      0.33  |Q        |      V  |         |         |
11+25       0.1592      0.33  |Q        |      V  |         |         |
11+30       0.1615      0.33  |Q        |       V |         |         |
11+35       0.1636      0.31  |Q        |       V |         |         |
11+40       0.1656      0.29  |Q        |       V |         |         |
11+45       0.1676      0.29  |Q        |       V |         |         |
11+50       0.1697      0.30  |Q        |        V|         |         |
11+55       0.1718      0.31  |Q        |        V|         |         |
12+ 0       0.1739      0.31  |Q        |        V|         |         |
12+ 5       0.1765      0.38  |Q        |        V|         |         |
12+10       0.1795      0.42  |Q        |         V         |         |
12+15       0.1824      0.43  |Q        |         V         |         |
12+20       0.1854      0.44  |Q        |         V         |         |
12+25       0.1885      0.45  |Q        |          |V       |         |
12+30       0.1916      0.45  |Q        |          |V       |         |
12+35       0.1948      0.47  |Q        |          |V       |         |
12+40       0.1981      0.48  |Q        |          | V      |         |
12+45       0.2014      0.48  |Q        |          | V      |         |
12+50       0.2048      0.50  |Q        |          | V      |         |
12+55       0.2083      0.51  | Q       |          |  V     |         |
13+ 0       0.2118      0.51  | Q       |          |  V     |         |
13+ 5       0.2157      0.57  | Q       |          |   V    |         |
13+10       0.2200      0.61  | Q       |          |   V    |         |
13+15       0.2242      0.62  | Q       |          |    V   |         |
13+20       0.2285      0.62  | Q       |          |    V   |         |
13+25       0.2328      0.62  | Q       |          |     V  |         |
13+30       0.2370      0.62  | Q       |          |     V  |         |
13+35       0.2404      0.50  |Q        |          |     V  |         |
13+40       0.2432      0.41  |Q        |          |      V |         |
13+45       0.2460      0.40  |Q        |          |      V |         |
13+50       0.2487      0.40  |Q        |          |      V |         |
13+55       0.2514      0.40  |Q        |          |       V|         |
14+ 0       0.2541      0.40  |Q        |          |       V|         |
14+ 5       0.2571      0.44  |Q        |          |       V|         |
14+10       0.2604      0.47  |Q        |          |        V|        |
```

14+15	0.2636	0.47	|Q	|	|	V|	|
14+20	0.2668	0.46	|Q	|	|	V|	|
14+25	0.2699	0.45	|Q	|	|	V	|
14+30	0.2730	0.45	|Q	|	|	V	|
14+35	0.2762	0.45	|Q	|	|	V	|
14+40	0.2793	0.45	|Q	|	|	|V	|
14+45	0.2824	0.45	|Q	|	|	|V	|
14+50	0.2855	0.44	|Q	|	|	|V	|
14+55	0.2885	0.43	|Q	|	|	| V	|
15+ 0	0.2914	0.43	|Q	|	|	| V	|
15+ 5	0.2944	0.42	|Q	|	|	| V	|
15+10	0.2972	0.41	|Q	|	|	| V	|
15+15	0.3001	0.41	|Q	|	|	| V	|
15+20	0.3028	0.40	|Q	|	|	| V	|
15+25	0.3056	0.40	|Q	|	|	| V	|
15+30	0.3083	0.40	|Q	|	|	| V	|
15+35	0.3107	0.36	|Q	|	|	| V	|
15+40	0.3130	0.33	|Q	|	|	| V	|
15+45	0.3153	0.33	|Q	|	|	| V	|
15+50	0.3175	0.33	|Q	|	|	| V	|
15+55	0.3198	0.33	|Q	|	|	| V	|
16+ 0	0.3220	0.33	|Q	|	|	| V	|
16+ 5	0.3233	0.18	Q	|	|	| V	|
16+10	0.3238	0.08	Q	|	|	| V	|
16+15	0.3243	0.07	Q	|	|	| V	|
16+20	0.3248	0.07	Q	|	|	| V	|
16+25	0.3253	0.07	Q	|	|	| V	|
16+30	0.3257	0.07	Q	|	|	| V	|
16+35	0.3261	0.06	Q	|	|	| V	|
16+40	0.3265	0.05	Q	|	|	| V	|
16+45	0.3269	0.05	Q	|	|	| V	|
16+50	0.3272	0.05	Q	|	|	| V	|
16+55	0.3276	0.05	Q	|	|	| V	|
17+ 0	0.3279	0.05	Q	|	|	| V	|
17+ 5	0.3284	0.07	Q	|	|	| V	|
17+10	0.3290	0.08	Q	|	|	| V	|
17+15	0.3296	0.09	Q	|	|	| V	|
17+20	0.3302	0.09	Q	|	|	| V	|
17+25	0.3308	0.09	Q	|	|	| V	|
17+30	0.3314	0.09	Q	|	|	| V	|
17+35	0.3319	0.09	Q	|	|	| V	|
17+40	0.3325	0.09	Q	|	|	| V	|
17+45	0.3331	0.09	Q	|	|	| V	|
17+50	0.3337	0.08	Q	|	|	| V	|
17+55	0.3341	0.07	Q	|	|	| V	|
18+ 0	0.3346	0.07	Q	|	|	| V	|
18+ 5	0.3351	0.07	Q	|	|	| V	|
18+10	0.3356	0.07	Q	|	|	| V	|
18+15	0.3360	0.07	Q	|	|	| V	|
18+20	0.3365	0.07	Q	|	|	| V	|
18+25	0.3370	0.07	Q	|	|	| V	|
18+30	0.3374	0.07	Q	|	|	| V	|
18+35	0.3379	0.06	Q	|	|	| V	|

18+40	0.3382	0.05	Q	|	|	|	V |
18+45	0.3386	0.05	Q	|	|	|	V |
18+50	0.3389	0.04	Q	|	|	|	V |
18+55	0.3391	0.04	Q	|	|	|	V |
19+ 0	0.3393	0.03	Q	|	|	|	V |
19+ 5	0.3396	0.04	Q	|	|	|	V |
19+10	0.3400	0.05	Q	|	|	|	V |
19+15	0.3403	0.05	Q	|	|	|	V |
19+20	0.3408	0.06	Q	|	|	|	V |
19+25	0.3412	0.07	Q	|	|	|	V |
19+30	0.3417	0.07	Q	|	|	|	V |
19+35	0.3421	0.06	Q	|	|	|	V |
19+40	0.3425	0.05	Q	|	|	|	V |
19+45	0.3428	0.05	Q	|	|	|	V |
19+50	0.3431	0.04	Q	|	|	|	V |
19+55	0.3434	0.04	Q	|	|	|	V |
20+ 0	0.3436	0.03	Q	|	|	|	V |
20+ 5	0.3439	0.04	Q	|	|	|	V |
20+10	0.3442	0.05	Q	|	|	|	V |
20+15	0.3446	0.05	Q	|	|	|	V |
20+20	0.3450	0.05	Q	|	|	|	V |
20+25	0.3453	0.05	Q	|	|	|	V |
20+30	0.3457	0.05	Q	|	|	|	V |
20+35	0.3460	0.05	Q	|	|	|	V |
20+40	0.3464	0.05	Q	|	|	|	V |
20+45	0.3467	0.05	Q	|	|	|	V |
20+50	0.3470	0.04	Q	|	|	|	V |
20+55	0.3473	0.04	Q	|	|	|	V |
21+ 0	0.3475	0.03	Q	|	|	|	V |
21+ 5	0.3478	0.04	Q	|	|	|	V |
21+10	0.3482	0.05	Q	|	|	|	V |
21+15	0.3485	0.05	Q	|	|	|	V|
21+20	0.3488	0.04	Q	|	|	|	V|
21+25	0.3490	0.04	Q	|	|	|	V|
21+30	0.3493	0.03	Q	|	|	|	V|
21+35	0.3496	0.04	Q	|	|	|	V|
21+40	0.3499	0.05	Q	|	|	|	V|
21+45	0.3503	0.05	Q	|	|	|	V|
21+50	0.3506	0.04	Q	|	|	|	V|
21+55	0.3508	0.04	Q	|	|	|	V|
22+ 0	0.3511	0.03	Q	|	|	|	V|
22+ 5	0.3514	0.04	Q	|	|	|	V|
22+10	0.3517	0.05	Q	|	|	|	V|
22+15	0.3521	0.05	Q	|	|	|	V|
22+20	0.3523	0.04	Q	|	|	|	V|
22+25	0.3526	0.04	Q	|	|	|	V|
22+30	0.3528	0.03	Q	|	|	|	V|
22+35	0.3531	0.03	Q	|	|	|	V|
22+40	0.3533	0.03	Q	|	|	|	V|
22+45	0.3535	0.03	Q	|	|	|	V|
22+50	0.3538	0.03	Q	|	|	|	V|
22+55	0.3540	0.03	Q	|	|	|	V|
23+ 0	0.3542	0.03	Q	|	|	|	V|

```
   23+ 5       0.3545      0.03  Q          |          |          |         V|
   23+10       0.3547      0.03  Q          |          |          |         V|
   23+15       0.3550      0.03  Q          |          |          |         V|
   23+20       0.3552      0.03  Q          |          |          |         V|
   23+25       0.3554      0.03  Q          |          |          |         V|
   23+30       0.3557      0.03  Q          |          |          |         V|
   23+35       0.3559      0.03  Q          |          |          |         V|
   23+40       0.3561      0.03  Q          |          |          |         V|
   23+45       0.3564      0.03  Q          |          |          |         V|
   23+50       0.3566      0.03  Q          |          |          |         V|
   23+55       0.3569      0.03  Q          |          |          |         V|
   24+ 0       0.3571      0.03  Q          |          |          |         V|
   24+ 5       0.3572      0.02  Q          |          |          |         V|
   24+10       0.3572      0.00  Q          |          |          |          V
-------------------------------------------------------------------------------
```

AREA B1

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014, Version 9.0
Study date 02/05/24 File: ARB124100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6279

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

PROPOSED CONDITION: 100YR HYDROLOGY
ARB1

Drainage Area = 1.47(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.47(Ac.) = 0.002 Sq. Mi.
Length along longest watercourse = 972.00(Ft.)
Length along longest watercourse measured to centroid = 486.00(Ft.)
Length along longest watercourse = 0.184 Mi.
Length along longest watercourse measured to centroid = 0.092 Mi.
Difference in elevation = 6.00(Ft.)
Slope along watercourse = 32.5926 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.039 Hr.
Lag time = 2.37 Min.
25% of lag time = 0.59 Min.
40% of lag time = 0.95 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.47	1.16	1.71

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.47	4.44	6.53

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.160(In)
Area Averaged 100-Year Rainfall = 4.440(In)

Point rain (area averaged) = 4.440(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 4.440(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.470	56.00	0.880

Total Area Entered = 1.47(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.880	0.106	1.000	0.106
					Sum (F) =	0.106

Area averaged mean soil loss (F) (In/Hr) = 0.106
Minimum soil loss rate ((In/Hr)) = 0.053
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.200

U n i t H y d r o g r a p h
DESERT S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	211.337	44.180	0.655
2	0.167	422.674	44.738	0.663
3	0.250	634.011	8.237	0.122
4	0.333	845.348	2.845	0.042
		Sum = 100.000	Sum=	1.481

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.036	(0.188)	0.007	0.028

2	0.17	0.07	0.036	(0.188)	0.007	0.028
3	0.25	0.07	0.036	(0.187)	0.007	0.028
4	0.33	0.10	0.053	(0.186)	0.011	0.043
5	0.42	0.10	0.053	(0.185)	0.011	0.043
6	0.50	0.10	0.053	(0.185)	0.011	0.043
7	0.58	0.10	0.053	(0.184)	0.011	0.043
8	0.67	0.10	0.053	(0.183)	0.011	0.043
9	0.75	0.10	0.053	(0.183)	0.011	0.043
10	0.83	0.13	0.071	(0.182)	0.014	0.057
11	0.92	0.13	0.071	(0.181)	0.014	0.057
12	1.00	0.13	0.071	(0.180)	0.014	0.057
13	1.08	0.10	0.053	(0.180)	0.011	0.043
14	1.17	0.10	0.053	(0.179)	0.011	0.043
15	1.25	0.10	0.053	(0.178)	0.011	0.043
16	1.33	0.10	0.053	(0.178)	0.011	0.043
17	1.42	0.10	0.053	(0.177)	0.011	0.043
18	1.50	0.10	0.053	(0.176)	0.011	0.043
19	1.58	0.10	0.053	(0.175)	0.011	0.043
20	1.67	0.10	0.053	(0.175)	0.011	0.043
21	1.75	0.10	0.053	(0.174)	0.011	0.043
22	1.83	0.13	0.071	(0.173)	0.014	0.057
23	1.92	0.13	0.071	(0.173)	0.014	0.057
24	2.00	0.13	0.071	(0.172)	0.014	0.057
25	2.08	0.13	0.071	(0.171)	0.014	0.057
26	2.17	0.13	0.071	(0.171)	0.014	0.057
27	2.25	0.13	0.071	(0.170)	0.014	0.057
28	2.33	0.13	0.071	(0.169)	0.014	0.057
29	2.42	0.13	0.071	(0.168)	0.014	0.057
30	2.50	0.13	0.071	(0.168)	0.014	0.057
31	2.58	0.17	0.089	(0.167)	0.018	0.071
32	2.67	0.17	0.089	(0.166)	0.018	0.071
33	2.75	0.17	0.089	(0.166)	0.018	0.071
34	2.83	0.17	0.089	(0.165)	0.018	0.071
35	2.92	0.17	0.089	(0.164)	0.018	0.071
36	3.00	0.17	0.089	(0.164)	0.018	0.071
37	3.08	0.17	0.089	(0.163)	0.018	0.071
38	3.17	0.17	0.089	(0.162)	0.018	0.071
39	3.25	0.17	0.089	(0.162)	0.018	0.071
40	3.33	0.17	0.089	(0.161)	0.018	0.071
41	3.42	0.17	0.089	(0.160)	0.018	0.071
42	3.50	0.17	0.089	(0.160)	0.018	0.071
43	3.58	0.17	0.089	(0.159)	0.018	0.071
44	3.67	0.17	0.089	(0.158)	0.018	0.071
45	3.75	0.17	0.089	(0.158)	0.018	0.071
46	3.83	0.20	0.107	(0.157)	0.021	0.085
47	3.92	0.20	0.107	(0.156)	0.021	0.085
48	4.00	0.20	0.107	(0.156)	0.021	0.085
49	4.08	0.20	0.107	(0.155)	0.021	0.085
50	4.17	0.20	0.107	(0.154)	0.021	0.085
51	4.25	0.20	0.107	(0.154)	0.021	0.085
52	4.33	0.23	0.124	(0.153)	0.025	0.099
53	4.42	0.23	0.124	(0.152)	0.025	0.099
54	4.50	0.23	0.124	(0.152)	0.025	0.099

55	4.58	0.23	0.124	(0.151)	0.025	0.099
56	4.67	0.23	0.124	(0.150)	0.025	0.099
57	4.75	0.23	0.124	(0.150)	0.025	0.099
58	4.83	0.27	0.142	(0.149)	0.028	0.114
59	4.92	0.27	0.142	(0.148)	0.028	0.114
60	5.00	0.27	0.142	(0.148)	0.028	0.114
61	5.08	0.20	0.107	(0.147)	0.021	0.085
62	5.17	0.20	0.107	(0.147)	0.021	0.085
63	5.25	0.20	0.107	(0.146)	0.021	0.085
64	5.33	0.23	0.124	(0.145)	0.025	0.099
65	5.42	0.23	0.124	(0.145)	0.025	0.099
66	5.50	0.23	0.124	(0.144)	0.025	0.099
67	5.58	0.27	0.142	(0.143)	0.028	0.114
68	5.67	0.27	0.142	(0.143)	0.028	0.114
69	5.75	0.27	0.142	(0.142)	0.028	0.114
70	5.83	0.27	0.142	(0.141)	0.028	0.114
71	5.92	0.27	0.142	(0.141)	0.028	0.114
72	6.00	0.27	0.142	(0.140)	0.028	0.114
73	6.08	0.30	0.160	(0.140)	0.032	0.128
74	6.17	0.30	0.160	(0.139)	0.032	0.128
75	6.25	0.30	0.160	(0.138)	0.032	0.128
76	6.33	0.30	0.160	(0.138)	0.032	0.128
77	6.42	0.30	0.160	(0.137)	0.032	0.128
78	6.50	0.30	0.160	(0.137)	0.032	0.128
79	6.58	0.33	0.178	(0.136)	0.036	0.142
80	6.67	0.33	0.178	(0.135)	0.036	0.142
81	6.75	0.33	0.178	(0.135)	0.036	0.142
82	6.83	0.33	0.178	(0.134)	0.036	0.142
83	6.92	0.33	0.178	(0.133)	0.036	0.142
84	7.00	0.33	0.178	(0.133)	0.036	0.142
85	7.08	0.33	0.178	(0.132)	0.036	0.142
86	7.17	0.33	0.178	(0.132)	0.036	0.142
87	7.25	0.33	0.178	(0.131)	0.036	0.142
88	7.33	0.37	0.195	(0.130)	0.039	0.156
89	7.42	0.37	0.195	(0.130)	0.039	0.156
90	7.50	0.37	0.195	(0.129)	0.039	0.156
91	7.58	0.40	0.213	(0.129)	0.043	0.170
92	7.67	0.40	0.213	(0.128)	0.043	0.170
93	7.75	0.40	0.213	(0.127)	0.043	0.170
94	7.83	0.43	0.231	(0.127)	0.046	0.185
95	7.92	0.43	0.231	(0.126)	0.046	0.185
96	8.00	0.43	0.231	(0.126)	0.046	0.185
97	8.08	0.50	0.266	(0.125)	0.053	0.213
98	8.17	0.50	0.266	(0.125)	0.053	0.213
99	8.25	0.50	0.266	(0.124)	0.053	0.213
100	8.33	0.50	0.266	(0.123)	0.053	0.213
101	8.42	0.50	0.266	(0.123)	0.053	0.213
102	8.50	0.50	0.266	(0.122)	0.053	0.213
103	8.58	0.53	0.284	(0.122)	0.057	0.227
104	8.67	0.53	0.284	(0.121)	0.057	0.227
105	8.75	0.53	0.284	(0.121)	0.057	0.227
106	8.83	0.57	0.302	(0.120)	0.060	0.242
107	8.92	0.57	0.302	(0.119)	0.060	0.242

108	9.00	0.57	0.302	(0.119)	0.060	0.242
109	9.08	0.63	0.337	(0.118)	0.067	0.270
110	9.17	0.63	0.337	(0.118)	0.067	0.270
111	9.25	0.63	0.337	(0.117)	0.067	0.270
112	9.33	0.67	0.355	(0.117)	0.071	0.284
113	9.42	0.67	0.355	(0.116)	0.071	0.284
114	9.50	0.67	0.355	(0.115)	0.071	0.284
115	9.58	0.70	0.373	(0.115)	0.075	0.298
116	9.67	0.70	0.373	(0.114)	0.075	0.298
117	9.75	0.70	0.373	(0.114)	0.075	0.298
118	9.83	0.73	0.391	(0.113)	0.078	0.313
119	9.92	0.73	0.391	(0.113)	0.078	0.313
120	10.00	0.73	0.391	(0.112)	0.078	0.313
121	10.08	0.50	0.266	(0.112)	0.053	0.213
122	10.17	0.50	0.266	(0.111)	0.053	0.213
123	10.25	0.50	0.266	(0.111)	0.053	0.213
124	10.33	0.50	0.266	(0.110)	0.053	0.213
125	10.42	0.50	0.266	(0.110)	0.053	0.213
126	10.50	0.50	0.266	(0.109)	0.053	0.213
127	10.58	0.67	0.355	(0.108)	0.071	0.284
128	10.67	0.67	0.355	(0.108)	0.071	0.284
129	10.75	0.67	0.355	(0.107)	0.071	0.284
130	10.83	0.67	0.355	(0.107)	0.071	0.284
131	10.92	0.67	0.355	(0.106)	0.071	0.284
132	11.00	0.67	0.355	(0.106)	0.071	0.284
133	11.08	0.63	0.337	(0.105)	0.067	0.270
134	11.17	0.63	0.337	(0.105)	0.067	0.270
135	11.25	0.63	0.337	(0.104)	0.067	0.270
136	11.33	0.63	0.337	(0.104)	0.067	0.270
137	11.42	0.63	0.337	(0.103)	0.067	0.270
138	11.50	0.63	0.337	(0.103)	0.067	0.270
139	11.58	0.57	0.302	(0.102)	0.060	0.242
140	11.67	0.57	0.302	(0.102)	0.060	0.242
141	11.75	0.57	0.302	(0.101)	0.060	0.242
142	11.83	0.60	0.320	(0.101)	0.064	0.256
143	11.92	0.60	0.320	(0.100)	0.064	0.256
144	12.00	0.60	0.320	(0.100)	0.064	0.256
145	12.08	0.83	0.444	(0.099)	0.089	0.355
146	12.17	0.83	0.444	(0.099)	0.089	0.355
147	12.25	0.83	0.444	(0.098)	0.089	0.355
148	12.33	0.87	0.462	(0.098)	0.092	0.369
149	12.42	0.87	0.462	(0.097)	0.092	0.369
150	12.50	0.87	0.462	(0.097)	0.092	0.369
151	12.58	0.93	0.497	0.096	(0.099)	0.401
152	12.67	0.93	0.497	0.096	(0.099)	0.402
153	12.75	0.93	0.497	0.095	(0.099)	0.402
154	12.83	0.97	0.515	0.095	(0.103)	0.420
155	12.92	0.97	0.515	0.094	(0.103)	0.421
156	13.00	0.97	0.515	0.094	(0.103)	0.421
157	13.08	1.13	0.604	0.093	(0.121)	0.510
158	13.17	1.13	0.604	0.093	(0.121)	0.511
159	13.25	1.13	0.604	0.092	(0.121)	0.511
160	13.33	1.13	0.604	0.092	(0.121)	0.512

161	13.42	1.13	0.604		0.091	(	0.121)	0.512
162	13.50	1.13	0.604		0.091	(	0.121)	0.513
163	13.58	0.77	0.408	(	0.091)		0.082	0.327
164	13.67	0.77	0.408	(	0.090)		0.082	0.327
165	13.75	0.77	0.408	(	0.090)		0.082	0.327
166	13.83	0.77	0.408	(	0.089)		0.082	0.327
167	13.92	0.77	0.408	(	0.089)		0.082	0.327
168	14.00	0.77	0.408	(	0.088)		0.082	0.327
169	14.08	0.90	0.480		0.088	(	0.096)	0.392
170	14.17	0.90	0.480		0.087	(	0.096)	0.392
171	14.25	0.90	0.480		0.087	(	0.096)	0.393
172	14.33	0.87	0.462		0.086	(	0.092)	0.375
173	14.42	0.87	0.462		0.086	(	0.092)	0.376
174	14.50	0.87	0.462		0.086	(	0.092)	0.376
175	14.58	0.87	0.462		0.085	(	0.092)	0.377
176	14.67	0.87	0.462		0.085	(	0.092)	0.377
177	14.75	0.87	0.462		0.084	(	0.092)	0.377
178	14.83	0.83	0.444		0.084	(	0.089)	0.360
179	14.92	0.83	0.444		0.083	(	0.089)	0.361
180	15.00	0.83	0.444		0.083	(	0.089)	0.361
181	15.08	0.80	0.426		0.083	(	0.085)	0.344
182	15.17	0.80	0.426		0.082	(	0.085)	0.344
183	15.25	0.80	0.426		0.082	(	0.085)	0.345
184	15.33	0.77	0.408		0.081	(	0.082)	0.327
185	15.42	0.77	0.408		0.081	(	0.082)	0.328
186	15.50	0.77	0.408		0.080	(	0.082)	0.328
187	15.58	0.63	0.337	(	0.080)		0.067	0.270
188	15.67	0.63	0.337	(	0.080)		0.067	0.270
189	15.75	0.63	0.337	(	0.079)		0.067	0.270
190	15.83	0.63	0.337	(	0.079)		0.067	0.270
191	15.92	0.63	0.337	(	0.078)		0.067	0.270
192	16.00	0.63	0.337	(	0.078)		0.067	0.270
193	16.08	0.13	0.071	(	0.078)		0.014	0.057
194	16.17	0.13	0.071	(	0.077)		0.014	0.057
195	16.25	0.13	0.071	(	0.077)		0.014	0.057
196	16.33	0.13	0.071	(	0.076)		0.014	0.057
197	16.42	0.13	0.071	(	0.076)		0.014	0.057
198	16.50	0.13	0.071	(	0.076)		0.014	0.057
199	16.58	0.10	0.053	(	0.075)		0.011	0.043
200	16.67	0.10	0.053	(	0.075)		0.011	0.043
201	16.75	0.10	0.053	(	0.075)		0.011	0.043
202	16.83	0.10	0.053	(	0.074)		0.011	0.043
203	16.92	0.10	0.053	(	0.074)		0.011	0.043
204	17.00	0.10	0.053	(	0.073)		0.011	0.043
205	17.08	0.17	0.089	(	0.073)		0.018	0.071
206	17.17	0.17	0.089	(	0.073)		0.018	0.071
207	17.25	0.17	0.089	(	0.072)		0.018	0.071
208	17.33	0.17	0.089	(	0.072)		0.018	0.071
209	17.42	0.17	0.089	(	0.072)		0.018	0.071
210	17.50	0.17	0.089	(	0.071)		0.018	0.071
211	17.58	0.17	0.089	(	0.071)		0.018	0.071
212	17.67	0.17	0.089	(	0.070)		0.018	0.071
213	17.75	0.17	0.089	(	0.070)		0.018	0.071

214	17.83	0.13	0.071	(0.070)	0.014	0.057
215	17.92	0.13	0.071	(0.069)	0.014	0.057
216	18.00	0.13	0.071	(0.069)	0.014	0.057
217	18.08	0.13	0.071	(0.069)	0.014	0.057
218	18.17	0.13	0.071	(0.068)	0.014	0.057
219	18.25	0.13	0.071	(0.068)	0.014	0.057
220	18.33	0.13	0.071	(0.068)	0.014	0.057
221	18.42	0.13	0.071	(0.067)	0.014	0.057
222	18.50	0.13	0.071	(0.067)	0.014	0.057
223	18.58	0.10	0.053	(0.067)	0.011	0.043
224	18.67	0.10	0.053	(0.066)	0.011	0.043
225	18.75	0.10	0.053	(0.066)	0.011	0.043
226	18.83	0.07	0.036	(0.066)	0.007	0.028
227	18.92	0.07	0.036	(0.066)	0.007	0.028
228	19.00	0.07	0.036	(0.065)	0.007	0.028
229	19.08	0.10	0.053	(0.065)	0.011	0.043
230	19.17	0.10	0.053	(0.065)	0.011	0.043
231	19.25	0.10	0.053	(0.064)	0.011	0.043
232	19.33	0.13	0.071	(0.064)	0.014	0.057
233	19.42	0.13	0.071	(0.064)	0.014	0.057
234	19.50	0.13	0.071	(0.063)	0.014	0.057
235	19.58	0.10	0.053	(0.063)	0.011	0.043
236	19.67	0.10	0.053	(0.063)	0.011	0.043
237	19.75	0.10	0.053	(0.063)	0.011	0.043
238	19.83	0.07	0.036	(0.062)	0.007	0.028
239	19.92	0.07	0.036	(0.062)	0.007	0.028
240	20.00	0.07	0.036	(0.062)	0.007	0.028
241	20.08	0.10	0.053	(0.061)	0.011	0.043
242	20.17	0.10	0.053	(0.061)	0.011	0.043
243	20.25	0.10	0.053	(0.061)	0.011	0.043
244	20.33	0.10	0.053	(0.061)	0.011	0.043
245	20.42	0.10	0.053	(0.060)	0.011	0.043
246	20.50	0.10	0.053	(0.060)	0.011	0.043
247	20.58	0.10	0.053	(0.060)	0.011	0.043
248	20.67	0.10	0.053	(0.060)	0.011	0.043
249	20.75	0.10	0.053	(0.059)	0.011	0.043
250	20.83	0.07	0.036	(0.059)	0.007	0.028
251	20.92	0.07	0.036	(0.059)	0.007	0.028
252	21.00	0.07	0.036	(0.059)	0.007	0.028
253	21.08	0.10	0.053	(0.058)	0.011	0.043
254	21.17	0.10	0.053	(0.058)	0.011	0.043
255	21.25	0.10	0.053	(0.058)	0.011	0.043
256	21.33	0.07	0.036	(0.058)	0.007	0.028
257	21.42	0.07	0.036	(0.058)	0.007	0.028
258	21.50	0.07	0.036	(0.057)	0.007	0.028
259	21.58	0.10	0.053	(0.057)	0.011	0.043
260	21.67	0.10	0.053	(0.057)	0.011	0.043
261	21.75	0.10	0.053	(0.057)	0.011	0.043
262	21.83	0.07	0.036	(0.056)	0.007	0.028
263	21.92	0.07	0.036	(0.056)	0.007	0.028
264	22.00	0.07	0.036	(0.056)	0.007	0.028
265	22.08	0.10	0.053	(0.056)	0.011	0.043
266	22.17	0.10	0.053	(0.056)	0.011	0.043

267	22.25	0.10	0.053	(0.056)	0.011	0.043
268	22.33	0.07	0.036	(0.055)	0.007	0.028
269	22.42	0.07	0.036	(0.055)	0.007	0.028
270	22.50	0.07	0.036	(0.055)	0.007	0.028
271	22.58	0.07	0.036	(0.055)	0.007	0.028
272	22.67	0.07	0.036	(0.055)	0.007	0.028
273	22.75	0.07	0.036	(0.055)	0.007	0.028
274	22.83	0.07	0.036	(0.054)	0.007	0.028
275	22.92	0.07	0.036	(0.054)	0.007	0.028
276	23.00	0.07	0.036	(0.054)	0.007	0.028
277	23.08	0.07	0.036	(0.054)	0.007	0.028
278	23.17	0.07	0.036	(0.054)	0.007	0.028
279	23.25	0.07	0.036	(0.054)	0.007	0.028
280	23.33	0.07	0.036	(0.054)	0.007	0.028
281	23.42	0.07	0.036	(0.054)	0.007	0.028
282	23.50	0.07	0.036	(0.054)	0.007	0.028
283	23.58	0.07	0.036	(0.053)	0.007	0.028
284	23.67	0.07	0.036	(0.053)	0.007	0.028
285	23.75	0.07	0.036	(0.053)	0.007	0.028
286	23.83	0.07	0.036	(0.053)	0.007	0.028
287	23.92	0.07	0.036	(0.053)	0.007	0.028
288	24.00	0.07	0.036	(0.053)	0.007	0.028

(Loss Rate Not Used)

Sum = 100.0 Sum = 42.9

Flood volume = Effective rainfall 3.58(In)
times area 1.5(Ac.)/[(In)/(Ft.)] = 0.4(Ac.Ft)
Total soil loss = 0.86(In)
Total soil loss = 0.106(Ac.Ft)
Total rainfall = 4.44(In)
Flood volume = 19089.1 Cubic Feet
Total soil loss = 4603.1 Cubic Feet

Peak flow rate of this hydrograph = 0.760(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.02	Q	|	|	|	|
0+10	0.0004	0.04	Q	|	|	|	|
0+15	0.0007	0.04	Q	|	|	|	|
0+20	0.0010	0.05	Q	|	|	|	|
0+25	0.0014	0.06	Q	|	|	|	|
0+30	0.0019	0.06	Q	|	|	|	|
0+35	0.0023	0.06	Q	|	|	|	|
0+40	0.0027	0.06	Q	|	|	|	|
0+45	0.0032	0.06	Q	|	|	|	|
0+50	0.0037	0.07	Q	|	|	|	|

0+55	0.0042	0.08	Q	|	|	|	|
1+ 0	0.0048	0.08	Q	|	|	|	|
1+ 5	0.0053	0.07	Q	|	|	|	|
1+10	0.0058	0.07	Q	|	|	|	|
1+15	0.0062	0.06	Q	|	|	|	|
1+20	0.0067	0.06	Q	|	|	|	|
1+25	0.0071	0.06	Q	|	|	|	|
1+30	0.0075	0.06	Q	|	|	|	|
1+35	0.0080	0.06	Q	|	|	|	|
1+40	0.0084	0.06	Q	|	|	|	|
1+45	0.0088	0.06	Q	|	|	|	|
1+50	0.0093	0.07	Q	|	|	|	|
1+55	0.0099	0.08	Q	|	|	|	|
2+ 0	0.0105	0.08	Q	|	|	|	|
2+ 5	0.0111	0.08	QV	|	|	|	|
2+10	0.0116	0.08	QV	|	|	|	|
2+15	0.0122	0.08	QV	|	|	|	|
2+20	0.0128	0.08	QV	|	|	|	|
2+25	0.0134	0.08	QV	|	|	|	|
2+30	0.0140	0.08	QV	|	|	|	|
2+35	0.0146	0.09	QV	|	|	|	|
2+40	0.0153	0.10	QV	|	|	|	|
2+45	0.0160	0.10	QV	|	|	|	|
2+50	0.0168	0.11	QV	|	|	|	|
2+55	0.0175	0.11	QV	|	|	|	|
3+ 0	0.0182	0.11	QV	|	|	|	|
3+ 5	0.0189	0.11	QV	|	|	|	|
3+10	0.0197	0.11	QV	|	|	|	|
3+15	0.0204	0.11	QV	|	|	|	|
3+20	0.0211	0.11	QV	|	|	|	|
3+25	0.0218	0.11	QV	|	|	|	|
3+30	0.0226	0.11	Q V	|	|	|	|
3+35	0.0233	0.11	Q V	|	|	|	|
3+40	0.0240	0.11	Q V	|	|	|	|
3+45	0.0247	0.11	Q V	|	|	|	|
3+50	0.0255	0.11	Q V	|	|	|	|
3+55	0.0264	0.12	Q V	|	|	|	|
4+ 0	0.0272	0.13	Q V	|	|	|	|
4+ 5	0.0281	0.13	Q V	|	|	|	|
4+10	0.0290	0.13	Q V	|	|	|	|
4+15	0.0299	0.13	Q V	|	|	|	|
4+20	0.0308	0.14	Q V	|	|	|	|
4+25	0.0318	0.15	Q V	|	|	|	|
4+30	0.0328	0.15	Q V	|	|	|	|
4+35	0.0338	0.15	Q V	|	|	|	|
4+40	0.0348	0.15	Q V	|	|	|	|
4+45	0.0358	0.15	Q V	|	|	|	|
4+50	0.0369	0.16	Q V	|	|	|	|
4+55	0.0381	0.17	Q V	|	|	|	|
5+ 0	0.0392	0.17	Q V	|	|	|	|
5+ 5	0.0403	0.15	Q V	|	|	|	|
5+10	0.0412	0.13	Q V	|	|	|	|
5+15	0.0420	0.13	Q V	|	|	|	|

5+20	0.0430	0.14	Q V	|	|	|	|
5+25	0.0440	0.15	Q V	|	|	|	|
5+30	0.0450	0.15	Q V	|	|	|	|
5+35	0.0461	0.16	Q V	|	|	|	|
5+40	0.0472	0.17	Q V	|	|	|	|
5+45	0.0484	0.17	Q V	|	|	|	|
5+50	0.0495	0.17	Q V	|	|	|	|
5+55	0.0507	0.17	Q V	|	|	|	|
6+ 0	0.0518	0.17	Q V	|	|	|	|
6+ 5	0.0531	0.18	Q V	|	|	|	|
6+10	0.0544	0.19	Q V	|	|	|	|
6+15	0.0557	0.19	Q V	|	|	|	|
6+20	0.0570	0.19	Q V	|	|	|	|
6+25	0.0583	0.19	Q V	|	|	|	|
6+30	0.0596	0.19	Q V	|	|	|	|
6+35	0.0609	0.20	Q V	|	|	|	|
6+40	0.0624	0.21	Q V	|	|	|	|
6+45	0.0638	0.21	Q V	|	|	|	|
6+50	0.0653	0.21	Q V	|	|	|	|
6+55	0.0667	0.21	Q V	|	|	|	|
7+ 0	0.0682	0.21	Q V	|	|	|	|
7+ 5	0.0696	0.21	Q V	|	|	|	|
7+10	0.0711	0.21	Q V	|	|	|	|
7+15	0.0725	0.21	Q V	|	|	|	|
7+20	0.0740	0.22	Q V	|	|	|	|
7+25	0.0756	0.23	Q V	|	|	|	|
7+30	0.0772	0.23	Q V	|	|	|	|
7+35	0.0789	0.24	Q V	|	|	|	|
7+40	0.0806	0.25	|Q V	|	|	|	|
7+45	0.0823	0.25	|Q V	|	|	|	|
7+50	0.0841	0.26	|Q V	|	|	|	|
7+55	0.0860	0.27	|Q V	|	|	|	|
8+ 0	0.0879	0.27	|Q V	|	|	|	|
8+ 5	0.0899	0.29	|Q V	|	|	|	|
8+10	0.0920	0.31	|Q V	|	|	|	|
8+15	0.0942	0.31	|Q V	|	|	|	|
8+20	0.0964	0.32	|Q V	|	|	|	|
8+25	0.0986	0.32	|Q V	|	|	|	|
8+30	0.1007	0.32	|Q V|	|	|	|	|
8+35	0.1030	0.33	|Q V|	|	|	|	|
8+40	0.1053	0.33	|Q V|	|	|	|	|
8+45	0.1076	0.34	|Q V|	|	|	|	|
8+50	0.1100	0.35	|Q V	|	|	|	|
8+55	0.1124	0.36	|Q V	|	|	|	|
9+ 0	0.1149	0.36	|Q V	|	|	|	|
9+ 5	0.1175	0.38	|Q V	|	|	|	|
9+10	0.1202	0.40	|Q V	|	|	|	|
9+15	0.1230	0.40	|Q |V	|	|	|	|
9+20	0.1258	0.41	|Q |V	|	|	|	|
9+25	0.1287	0.42	|Q |V	|	|	|	|
9+30	0.1316	0.42	|Q | V	|	|	|	|
9+35	0.1345	0.43	|Q | V	|	|	|	|
9+40	0.1376	0.44	|Q | V	|	|	|	|

9+45	0.1406	0.44	Q	V			
9+50	0.1437	0.45	Q	V			
9+55	0.1469	0.46	Q	V			
10+ 0	0.1501	0.46	Q	V			
10+ 5	0.1528	0.40	Q	V			
10+10	0.1551	0.33	Q	V			
10+15	0.1573	0.32	Q	V			
10+20	0.1595	0.32	Q	V			
10+25	0.1617	0.32	Q	V			
10+30	0.1638	0.32	Q	V			
10+35	0.1663	0.36	Q	V			
10+40	0.1691	0.41	Q	V			
10+45	0.1720	0.42	Q	V			
10+50	0.1749	0.42	Q	V			
10+55	0.1778	0.42	Q	V			
11+ 0	0.1807	0.42	Q	V			
11+ 5	0.1836	0.41	Q	V			
11+10	0.1863	0.40	Q	V			
11+15	0.1891	0.40	Q	V			
11+20	0.1919	0.40	Q	V			
11+25	0.1946	0.40	Q	V			
11+30	0.1974	0.40	Q	V			
11+35	0.2000	0.38	Q	V			
11+40	0.2025	0.36	Q	V			
11+45	0.2050	0.36	Q	V			
11+50	0.2075	0.37	Q	V			
11+55	0.2101	0.38	Q	V			
12+ 0	0.2127	0.38	Q	V			
12+ 5	0.2158	0.44	Q	V			
12+10	0.2193	0.51	Q	V			
12+15	0.2229	0.52	Q	V			
12+20	0.2266	0.54	Q	V			
12+25	0.2303	0.55	Q	V			
12+30	0.2341	0.55	Q	V			
12+35	0.2380	0.57	Q	V			
12+40	0.2420	0.59	Q	V			
12+45	0.2461	0.59	Q	V			
12+50	0.2503	0.61	Q	V			
12+55	0.2546	0.62	Q	V			
13+ 0	0.2589	0.62	Q	V			
13+ 5	0.2636	0.68	Q	V			
13+10	0.2687	0.74	Q	V			
13+15	0.2739	0.75	Q	V			
13+20	0.2791	0.76	Q	V			
13+25	0.2843	0.76	Q	V			
13+30	0.2896	0.76	Q	V			
13+35	0.2940	0.64	Q	V			
13+40	0.2975	0.51	Q	V			
13+45	0.3009	0.49	Q	V			
13+50	0.3042	0.48	Q	V			
13+55	0.3076	0.48	Q	V			
14+ 0	0.3109	0.48	Q	V			
14+ 5	0.3145	0.53	Q	V			

14+10	0.3185	0.57	| Q	|	|	V|	|
14+15	0.3225	0.58	| Q	|	|	V|	|
14+20	0.3264	0.57	| Q	|	|	V|	|
14+25	0.3302	0.56	| Q	|	|	V	|
14+30	0.3341	0.56	| Q	|	|	V	|
14+35	0.3379	0.56	| Q	|	|	V	|
14+40	0.3418	0.56	| Q	|	|	|V	|
14+45	0.3456	0.56	| Q	|	|	|V	|
14+50	0.3494	0.55	| Q	|	|	|V	|
14+55	0.3531	0.54	| Q	|	|	| V	|
15+ 0	0.3568	0.54	| Q	|	|	| V	|
15+ 5	0.3604	0.52	| Q	|	|	| V	|
15+10	0.3639	0.51	| Q	|	|	| V	|
15+15	0.3674	0.51	| Q	|	|	| V	|
15+20	0.3709	0.50	|Q	|	|	| V	|
15+25	0.3742	0.49	|Q	|	|	| V	|
15+30	0.3776	0.49	|Q	|	|	| V	|
15+35	0.3807	0.45	|Q	|	|	| V	|
15+40	0.3835	0.41	|Q	|	|	| V	|
15+45	0.3863	0.40	|Q	|	|	| V	|
15+50	0.3890	0.40	|Q	|	|	| V	|
15+55	0.3918	0.40	|Q	|	|	| V	|
16+ 0	0.3945	0.40	|Q	|	|	| V	|
16+ 5	0.3963	0.26	|Q	|	|	| V	|
16+10	0.3971	0.12	Q	|	|	| V	|
16+15	0.3978	0.09	Q	|	|	| V	|
16+20	0.3984	0.08	Q	|	|	| V	|
16+25	0.3990	0.08	Q	|	|	| V	|
16+30	0.3995	0.08	Q	|	|	| V	|
16+35	0.4000	0.07	Q	|	|	| V	|
16+40	0.4005	0.07	Q	|	|	| V	|
16+45	0.4009	0.06	Q	|	|	| V	|
16+50	0.4014	0.06	Q	|	|	| V	|
16+55	0.4018	0.06	Q	|	|	| V	|
17+ 0	0.4022	0.06	Q	|	|	| V	|
17+ 5	0.4028	0.08	Q	|	|	| V	|
17+10	0.4035	0.10	Q	|	|	| V	|
17+15	0.4042	0.10	Q	|	|	| V	|
17+20	0.4049	0.11	Q	|	|	| V	|
17+25	0.4057	0.11	Q	|	|	| V	|
17+30	0.4064	0.11	Q	|	|	| V	|
17+35	0.4071	0.11	Q	|	|	| V	|
17+40	0.4078	0.11	Q	|	|	| V	|
17+45	0.4086	0.11	Q	|	|	| V	|
17+50	0.4092	0.10	Q	|	|	| V	|
17+55	0.4098	0.09	Q	|	|	| V	|
18+ 0	0.4104	0.08	Q	|	|	| V	|
18+ 5	0.4110	0.08	Q	|	|	| V	|
18+10	0.4116	0.08	Q	|	|	| V	|
18+15	0.4121	0.08	Q	|	|	| V	|
18+20	0.4127	0.08	Q	|	|	| V	|
18+25	0.4133	0.08	Q	|	|	| V	|
18+30	0.4139	0.08	Q	|	|	| V	|

18+35	0.4144	0.07	Q	|	|	|	V |
18+40	0.4149	0.07	Q	|	|	|	V |
18+45	0.4153	0.06	Q	|	|	|	V |
18+50	0.4157	0.05	Q	|	|	|	V |
18+55	0.4160	0.04	Q	|	|	|	V |
19+ 0	0.4163	0.04	Q	|	|	|	V |
19+ 5	0.4166	0.05	Q	|	|	|	V |
19+10	0.4170	0.06	Q	|	|	|	V |
19+15	0.4175	0.06	Q	|	|	|	V |
19+20	0.4180	0.07	Q	|	|	|	V |
19+25	0.4185	0.08	Q	|	|	|	V |
19+30	0.4191	0.08	Q	|	|	|	V |
19+35	0.4196	0.07	Q	|	|	|	V |
19+40	0.4201	0.07	Q	|	|	|	V |
19+45	0.4205	0.06	Q	|	|	|	V |
19+50	0.4209	0.05	Q	|	|	|	V |
19+55	0.4212	0.04	Q	|	|	|	V |
20+ 0	0.4215	0.04	Q	|	|	|	V |
20+ 5	0.4218	0.05	Q	|	|	|	V |
20+10	0.4223	0.06	Q	|	|	|	V |
20+15	0.4227	0.06	Q	|	|	|	V |
20+20	0.4231	0.06	Q	|	|	|	V |
20+25	0.4236	0.06	Q	|	|	|	V |
20+30	0.4240	0.06	Q	|	|	|	V |
20+35	0.4244	0.06	Q	|	|	|	V |
20+40	0.4249	0.06	Q	|	|	|	V |
20+45	0.4253	0.06	Q	|	|	|	V |
20+50	0.4257	0.05	Q	|	|	|	V |
20+55	0.4260	0.04	Q	|	|	|	V |
21+ 0	0.4263	0.04	Q	|	|	|	V |
21+ 5	0.4266	0.05	Q	|	|	|	V |
21+10	0.4270	0.06	Q	|	|	|	V |
21+15	0.4275	0.06	Q	|	|	|	V|
21+20	0.4279	0.05	Q	|	|	|	V|
21+25	0.4282	0.04	Q	|	|	|	V|
21+30	0.4285	0.04	Q	|	|	|	V|
21+35	0.4288	0.05	Q	|	|	|	V|
21+40	0.4292	0.06	Q	|	|	|	V|
21+45	0.4297	0.06	Q	|	|	|	V|
21+50	0.4300	0.05	Q	|	|	|	V|
21+55	0.4303	0.04	Q	|	|	|	V|
22+ 0	0.4306	0.04	Q	|	|	|	V|
22+ 5	0.4310	0.05	Q	|	|	|	V|
22+10	0.4314	0.06	Q	|	|	|	V|
22+15	0.4318	0.06	Q	|	|	|	V|
22+20	0.4322	0.05	Q	|	|	|	V|
22+25	0.4325	0.04	Q	|	|	|	V|
22+30	0.4328	0.04	Q	|	|	|	V|
22+35	0.4331	0.04	Q	|	|	|	V|
22+40	0.4334	0.04	Q	|	|	|	V|
22+45	0.4337	0.04	Q	|	|	|	V|
22+50	0.4340	0.04	Q	|	|	|	V|
22+55	0.4343	0.04	Q	|	|	|	V|

23+ 0	0.4345	0.04	Q	|	|	|	V|
23+ 5	0.4348	0.04	Q	|	|	|	V|
23+10	0.4351	0.04	Q	|	|	|	V|
23+15	0.4354	0.04	Q	|	|	|	V|
23+20	0.4357	0.04	Q	|	|	|	V|
23+25	0.4360	0.04	Q	|	|	|	V|
23+30	0.4363	0.04	Q	|	|	|	V|
23+35	0.4366	0.04	Q	|	|	|	V|
23+40	0.4369	0.04	Q	|	|	|	V|
23+45	0.4372	0.04	Q	|	|	|	V|
23+50	0.4374	0.04	Q	|	|	|	V|
23+55	0.4377	0.04	Q	|	|	|	V|
24+ 0	0.4380	0.04	Q	|	|	|	V|
24+ 5	0.4382	0.02	Q	|	|	|	V|
24+10	0.4382	0.00	Q	|	|	|	V|
24+15	0.4382	0.00	Q	|	|	|	V|

AREA BB1

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014, Version 9.0
Study date 02/05/24 File: ARBB124100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6279

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

PROPOSED CONDITION: 100YR HYDROLOGY
ARBB1

Drainage Area = 1.47(Ac.) = 0.002 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.47(Ac.) = 0.002 Sq. Mi.
Length along longest watercourse = 970.00(Ft.)
Length along longest watercourse measured to centroid = 485.00(Ft.)
Length along longest watercourse = 0.184 Mi.
Length along longest watercourse measured to centroid = 0.092 Mi.
Difference in elevation = 7.00(Ft.)
Slope along watercourse = 38.1031 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.038 Hr.
Lag time = 2.29 Min.
25% of lag time = 0.57 Min.
40% of lag time = 0.92 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.47	1.16	1.71

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.47	4.44	6.53

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.160(In)
Area Averaged 100-Year Rainfall = 4.440(In)

Point rain (area averaged) = 4.440(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 4.440(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.470	56.00	0.840

Total Area Entered = 1.47(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.840	0.125	1.000	0.125
					Sum (F) =	0.125

Area averaged mean soil loss (F) (In/Hr) = 0.125
Minimum soil loss rate ((In/Hr)) = 0.062
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.230

U n i t H y d r o g r a p h
DESERT S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	218.045	45.289	0.671
2	0.167	436.089	44.264	0.656
3	0.250	654.134	7.895	0.117
4	0.333	872.178	2.552	0.038
		Sum = 100.000	Sum=	1.481

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.036	(0.221)	0.008	0.027

2	0.17	0.07	0.036	(0.220)	0.008	0.027
3	0.25	0.07	0.036	(0.219)	0.008	0.027
4	0.33	0.10	0.053	(0.218)	0.012	0.041
5	0.42	0.10	0.053	(0.218)	0.012	0.041
6	0.50	0.10	0.053	(0.217)	0.012	0.041
7	0.58	0.10	0.053	(0.216)	0.012	0.041
8	0.67	0.10	0.053	(0.215)	0.012	0.041
9	0.75	0.10	0.053	(0.214)	0.012	0.041
10	0.83	0.13	0.071	(0.213)	0.016	0.055
11	0.92	0.13	0.071	(0.212)	0.016	0.055
12	1.00	0.13	0.071	(0.212)	0.016	0.055
13	1.08	0.10	0.053	(0.211)	0.012	0.041
14	1.17	0.10	0.053	(0.210)	0.012	0.041
15	1.25	0.10	0.053	(0.209)	0.012	0.041
16	1.33	0.10	0.053	(0.208)	0.012	0.041
17	1.42	0.10	0.053	(0.207)	0.012	0.041
18	1.50	0.10	0.053	(0.207)	0.012	0.041
19	1.58	0.10	0.053	(0.206)	0.012	0.041
20	1.67	0.10	0.053	(0.205)	0.012	0.041
21	1.75	0.10	0.053	(0.204)	0.012	0.041
22	1.83	0.13	0.071	(0.203)	0.016	0.055
23	1.92	0.13	0.071	(0.203)	0.016	0.055
24	2.00	0.13	0.071	(0.202)	0.016	0.055
25	2.08	0.13	0.071	(0.201)	0.016	0.055
26	2.17	0.13	0.071	(0.200)	0.016	0.055
27	2.25	0.13	0.071	(0.199)	0.016	0.055
28	2.33	0.13	0.071	(0.198)	0.016	0.055
29	2.42	0.13	0.071	(0.198)	0.016	0.055
30	2.50	0.13	0.071	(0.197)	0.016	0.055
31	2.58	0.17	0.089	(0.196)	0.020	0.068
32	2.67	0.17	0.089	(0.195)	0.020	0.068
33	2.75	0.17	0.089	(0.194)	0.020	0.068
34	2.83	0.17	0.089	(0.194)	0.020	0.068
35	2.92	0.17	0.089	(0.193)	0.020	0.068
36	3.00	0.17	0.089	(0.192)	0.020	0.068
37	3.08	0.17	0.089	(0.191)	0.020	0.068
38	3.17	0.17	0.089	(0.190)	0.020	0.068
39	3.25	0.17	0.089	(0.190)	0.020	0.068
40	3.33	0.17	0.089	(0.189)	0.020	0.068
41	3.42	0.17	0.089	(0.188)	0.020	0.068
42	3.50	0.17	0.089	(0.187)	0.020	0.068
43	3.58	0.17	0.089	(0.187)	0.020	0.068
44	3.67	0.17	0.089	(0.186)	0.020	0.068
45	3.75	0.17	0.089	(0.185)	0.020	0.068
46	3.83	0.20	0.107	(0.184)	0.025	0.082
47	3.92	0.20	0.107	(0.183)	0.025	0.082
48	4.00	0.20	0.107	(0.183)	0.025	0.082
49	4.08	0.20	0.107	(0.182)	0.025	0.082
50	4.17	0.20	0.107	(0.181)	0.025	0.082
51	4.25	0.20	0.107	(0.180)	0.025	0.082
52	4.33	0.23	0.124	(0.180)	0.029	0.096
53	4.42	0.23	0.124	(0.179)	0.029	0.096
54	4.50	0.23	0.124	(0.178)	0.029	0.096

55	4.58	0.23	0.124	(0.177)	0.029	0.096
56	4.67	0.23	0.124	(0.176)	0.029	0.096
57	4.75	0.23	0.124	(0.176)	0.029	0.096
58	4.83	0.27	0.142	(0.175)	0.033	0.109
59	4.92	0.27	0.142	(0.174)	0.033	0.109
60	5.00	0.27	0.142	(0.173)	0.033	0.109
61	5.08	0.20	0.107	(0.173)	0.025	0.082
62	5.17	0.20	0.107	(0.172)	0.025	0.082
63	5.25	0.20	0.107	(0.171)	0.025	0.082
64	5.33	0.23	0.124	(0.170)	0.029	0.096
65	5.42	0.23	0.124	(0.170)	0.029	0.096
66	5.50	0.23	0.124	(0.169)	0.029	0.096
67	5.58	0.27	0.142	(0.168)	0.033	0.109
68	5.67	0.27	0.142	(0.167)	0.033	0.109
69	5.75	0.27	0.142	(0.167)	0.033	0.109
70	5.83	0.27	0.142	(0.166)	0.033	0.109
71	5.92	0.27	0.142	(0.165)	0.033	0.109
72	6.00	0.27	0.142	(0.165)	0.033	0.109
73	6.08	0.30	0.160	(0.164)	0.037	0.123
74	6.17	0.30	0.160	(0.163)	0.037	0.123
75	6.25	0.30	0.160	(0.162)	0.037	0.123
76	6.33	0.30	0.160	(0.162)	0.037	0.123
77	6.42	0.30	0.160	(0.161)	0.037	0.123
78	6.50	0.30	0.160	(0.160)	0.037	0.123
79	6.58	0.33	0.178	(0.159)	0.041	0.137
80	6.67	0.33	0.178	(0.159)	0.041	0.137
81	6.75	0.33	0.178	(0.158)	0.041	0.137
82	6.83	0.33	0.178	(0.157)	0.041	0.137
83	6.92	0.33	0.178	(0.157)	0.041	0.137
84	7.00	0.33	0.178	(0.156)	0.041	0.137
85	7.08	0.33	0.178	(0.155)	0.041	0.137
86	7.17	0.33	0.178	(0.154)	0.041	0.137
87	7.25	0.33	0.178	(0.154)	0.041	0.137
88	7.33	0.37	0.195	(0.153)	0.045	0.150
89	7.42	0.37	0.195	(0.152)	0.045	0.150
90	7.50	0.37	0.195	(0.152)	0.045	0.150
91	7.58	0.40	0.213	(0.151)	0.049	0.164
92	7.67	0.40	0.213	(0.150)	0.049	0.164
93	7.75	0.40	0.213	(0.150)	0.049	0.164
94	7.83	0.43	0.231	(0.149)	0.053	0.178
95	7.92	0.43	0.231	(0.148)	0.053	0.178
96	8.00	0.43	0.231	(0.148)	0.053	0.178
97	8.08	0.50	0.266	(0.147)	0.061	0.205
98	8.17	0.50	0.266	(0.146)	0.061	0.205
99	8.25	0.50	0.266	(0.145)	0.061	0.205
100	8.33	0.50	0.266	(0.145)	0.061	0.205
101	8.42	0.50	0.266	(0.144)	0.061	0.205
102	8.50	0.50	0.266	(0.143)	0.061	0.205
103	8.58	0.53	0.284	(0.143)	0.065	0.219
104	8.67	0.53	0.284	(0.142)	0.065	0.219
105	8.75	0.53	0.284	(0.141)	0.065	0.219
106	8.83	0.57	0.302	(0.141)	0.069	0.232
107	8.92	0.57	0.302	(0.140)	0.069	0.232

108	9.00	0.57	0.302	(0.139)	0.069	0.232
109	9.08	0.63	0.337	(0.139)	0.078	0.260
110	9.17	0.63	0.337	(0.138)	0.078	0.260
111	9.25	0.63	0.337	(0.137)	0.078	0.260
112	9.33	0.67	0.355	(0.137)	0.082	0.274
113	9.42	0.67	0.355	(0.136)	0.082	0.274
114	9.50	0.67	0.355	(0.135)	0.082	0.274
115	9.58	0.70	0.373	(0.135)	0.086	0.287
116	9.67	0.70	0.373	(0.134)	0.086	0.287
117	9.75	0.70	0.373	(0.134)	0.086	0.287
118	9.83	0.73	0.391	(0.133)	0.090	0.301
119	9.92	0.73	0.391	(0.132)	0.090	0.301
120	10.00	0.73	0.391	(0.132)	0.090	0.301
121	10.08	0.50	0.266	(0.131)	0.061	0.205
122	10.17	0.50	0.266	(0.130)	0.061	0.205
123	10.25	0.50	0.266	(0.130)	0.061	0.205
124	10.33	0.50	0.266	(0.129)	0.061	0.205
125	10.42	0.50	0.266	(0.128)	0.061	0.205
126	10.50	0.50	0.266	(0.128)	0.061	0.205
127	10.58	0.67	0.355	(0.127)	0.082	0.274
128	10.67	0.67	0.355	(0.127)	0.082	0.274
129	10.75	0.67	0.355	(0.126)	0.082	0.274
130	10.83	0.67	0.355	(0.125)	0.082	0.274
131	10.92	0.67	0.355	(0.125)	0.082	0.274
132	11.00	0.67	0.355	(0.124)	0.082	0.274
133	11.08	0.63	0.337	(0.124)	0.078	0.260
134	11.17	0.63	0.337	(0.123)	0.078	0.260
135	11.25	0.63	0.337	(0.122)	0.078	0.260
136	11.33	0.63	0.337	(0.122)	0.078	0.260
137	11.42	0.63	0.337	(0.121)	0.078	0.260
138	11.50	0.63	0.337	(0.120)	0.078	0.260
139	11.58	0.57	0.302	(0.120)	0.069	0.232
140	11.67	0.57	0.302	(0.119)	0.069	0.232
141	11.75	0.57	0.302	(0.119)	0.069	0.232
142	11.83	0.60	0.320	(0.118)	0.074	0.246
143	11.92	0.60	0.320	(0.118)	0.074	0.246
144	12.00	0.60	0.320	(0.117)	0.074	0.246
145	12.08	0.83	0.444	(0.116)	0.102	0.342
146	12.17	0.83	0.444	(0.116)	0.102	0.342
147	12.25	0.83	0.444	(0.115)	0.102	0.342
148	12.33	0.87	0.462	(0.115)	0.106	0.356
149	12.42	0.87	0.462	(0.114)	0.106	0.356
150	12.50	0.87	0.462	(0.113)	0.106	0.356
151	12.58	0.93	0.497	0.113	(0.114)	0.384
152	12.67	0.93	0.497	0.112	(0.114)	0.385
153	12.75	0.93	0.497	0.112	(0.114)	0.386
154	12.83	0.97	0.515	0.111	(0.118)	0.404
155	12.92	0.97	0.515	0.111	(0.118)	0.404
156	13.00	0.97	0.515	0.110	(0.118)	0.405
157	13.08	1.13	0.604	0.110	(0.139)	0.494
158	13.17	1.13	0.604	0.109	(0.139)	0.495
159	13.25	1.13	0.604	0.108	(0.139)	0.495
160	13.33	1.13	0.604	0.108	(0.139)	0.496

161	13.42	1.13	0.604		0.107	(	0.139)	0.497
162	13.50	1.13	0.604		0.107	(	0.139)	0.497
163	13.58	0.77	0.408	(	0.106)		0.094	0.315
164	13.67	0.77	0.408	(	0.106)		0.094	0.315
165	13.75	0.77	0.408	(	0.105)		0.094	0.315
166	13.83	0.77	0.408	(	0.105)		0.094	0.315
167	13.92	0.77	0.408	(	0.104)		0.094	0.315
168	14.00	0.77	0.408	(	0.104)		0.094	0.315
169	14.08	0.90	0.480		0.103	(	0.110)	0.377
170	14.17	0.90	0.480		0.102	(	0.110)	0.377
171	14.25	0.90	0.480		0.102	(	0.110)	0.378
172	14.33	0.87	0.462		0.101	(	0.106)	0.360
173	14.42	0.87	0.462		0.101	(	0.106)	0.361
174	14.50	0.87	0.462		0.100	(	0.106)	0.361
175	14.58	0.87	0.462		0.100	(	0.106)	0.362
176	14.67	0.87	0.462		0.099	(	0.106)	0.362
177	14.75	0.87	0.462		0.099	(	0.106)	0.363
178	14.83	0.83	0.444		0.098	(	0.102)	0.346
179	14.92	0.83	0.444		0.098	(	0.102)	0.346
180	15.00	0.83	0.444		0.097	(	0.102)	0.347
181	15.08	0.80	0.426		0.097	(	0.098)	0.329
182	15.17	0.80	0.426		0.096	(	0.098)	0.330
183	15.25	0.80	0.426		0.096	(	0.098)	0.330
184	15.33	0.77	0.408	(	0.095)		0.094	0.315
185	15.42	0.77	0.408	(	0.095)		0.094	0.315
186	15.50	0.77	0.408	(	0.094)		0.094	0.315
187	15.58	0.63	0.337	(	0.094)		0.078	0.260
188	15.67	0.63	0.337	(	0.093)		0.078	0.260
189	15.75	0.63	0.337	(	0.093)		0.078	0.260
190	15.83	0.63	0.337	(	0.092)		0.078	0.260
191	15.92	0.63	0.337	(	0.092)		0.078	0.260
192	16.00	0.63	0.337	(	0.092)		0.078	0.260
193	16.08	0.13	0.071	(	0.091)		0.016	0.055
194	16.17	0.13	0.071	(	0.091)		0.016	0.055
195	16.25	0.13	0.071	(	0.090)		0.016	0.055
196	16.33	0.13	0.071	(	0.090)		0.016	0.055
197	16.42	0.13	0.071	(	0.089)		0.016	0.055
198	16.50	0.13	0.071	(	0.089)		0.016	0.055
199	16.58	0.10	0.053	(	0.088)		0.012	0.041
200	16.67	0.10	0.053	(	0.088)		0.012	0.041
201	16.75	0.10	0.053	(	0.087)		0.012	0.041
202	16.83	0.10	0.053	(	0.087)		0.012	0.041
203	16.92	0.10	0.053	(	0.087)		0.012	0.041
204	17.00	0.10	0.053	(	0.086)		0.012	0.041
205	17.08	0.17	0.089	(	0.086)		0.020	0.068
206	17.17	0.17	0.089	(	0.085)		0.020	0.068
207	17.25	0.17	0.089	(	0.085)		0.020	0.068
208	17.33	0.17	0.089	(	0.084)		0.020	0.068
209	17.42	0.17	0.089	(	0.084)		0.020	0.068
210	17.50	0.17	0.089	(	0.084)		0.020	0.068
211	17.58	0.17	0.089	(	0.083)		0.020	0.068
212	17.67	0.17	0.089	(	0.083)		0.020	0.068
213	17.75	0.17	0.089	(	0.082)		0.020	0.068

214	17.83	0.13	0.071	(0.082)	0.016	0.055
215	17.92	0.13	0.071	(0.081)	0.016	0.055
216	18.00	0.13	0.071	(0.081)	0.016	0.055
217	18.08	0.13	0.071	(0.081)	0.016	0.055
218	18.17	0.13	0.071	(0.080)	0.016	0.055
219	18.25	0.13	0.071	(0.080)	0.016	0.055
220	18.33	0.13	0.071	(0.079)	0.016	0.055
221	18.42	0.13	0.071	(0.079)	0.016	0.055
222	18.50	0.13	0.071	(0.079)	0.016	0.055
223	18.58	0.10	0.053	(0.078)	0.012	0.041
224	18.67	0.10	0.053	(0.078)	0.012	0.041
225	18.75	0.10	0.053	(0.078)	0.012	0.041
226	18.83	0.07	0.036	(0.077)	0.008	0.027
227	18.92	0.07	0.036	(0.077)	0.008	0.027
228	19.00	0.07	0.036	(0.076)	0.008	0.027
229	19.08	0.10	0.053	(0.076)	0.012	0.041
230	19.17	0.10	0.053	(0.076)	0.012	0.041
231	19.25	0.10	0.053	(0.075)	0.012	0.041
232	19.33	0.13	0.071	(0.075)	0.016	0.055
233	19.42	0.13	0.071	(0.075)	0.016	0.055
234	19.50	0.13	0.071	(0.074)	0.016	0.055
235	19.58	0.10	0.053	(0.074)	0.012	0.041
236	19.67	0.10	0.053	(0.074)	0.012	0.041
237	19.75	0.10	0.053	(0.073)	0.012	0.041
238	19.83	0.07	0.036	(0.073)	0.008	0.027
239	19.92	0.07	0.036	(0.073)	0.008	0.027
240	20.00	0.07	0.036	(0.072)	0.008	0.027
241	20.08	0.10	0.053	(0.072)	0.012	0.041
242	20.17	0.10	0.053	(0.072)	0.012	0.041
243	20.25	0.10	0.053	(0.071)	0.012	0.041
244	20.33	0.10	0.053	(0.071)	0.012	0.041
245	20.42	0.10	0.053	(0.071)	0.012	0.041
246	20.50	0.10	0.053	(0.071)	0.012	0.041
247	20.58	0.10	0.053	(0.070)	0.012	0.041
248	20.67	0.10	0.053	(0.070)	0.012	0.041
249	20.75	0.10	0.053	(0.070)	0.012	0.041
250	20.83	0.07	0.036	(0.069)	0.008	0.027
251	20.92	0.07	0.036	(0.069)	0.008	0.027
252	21.00	0.07	0.036	(0.069)	0.008	0.027
253	21.08	0.10	0.053	(0.069)	0.012	0.041
254	21.17	0.10	0.053	(0.068)	0.012	0.041
255	21.25	0.10	0.053	(0.068)	0.012	0.041
256	21.33	0.07	0.036	(0.068)	0.008	0.027
257	21.42	0.07	0.036	(0.067)	0.008	0.027
258	21.50	0.07	0.036	(0.067)	0.008	0.027
259	21.58	0.10	0.053	(0.067)	0.012	0.041
260	21.67	0.10	0.053	(0.067)	0.012	0.041
261	21.75	0.10	0.053	(0.066)	0.012	0.041
262	21.83	0.07	0.036	(0.066)	0.008	0.027
263	21.92	0.07	0.036	(0.066)	0.008	0.027
264	22.00	0.07	0.036	(0.066)	0.008	0.027
265	22.08	0.10	0.053	(0.066)	0.012	0.041
266	22.17	0.10	0.053	(0.065)	0.012	0.041

267	22.25	0.10	0.053	(0.065)	0.012	0.041
268	22.33	0.07	0.036	(0.065)	0.008	0.027
269	22.42	0.07	0.036	(0.065)	0.008	0.027
270	22.50	0.07	0.036	(0.065)	0.008	0.027
271	22.58	0.07	0.036	(0.064)	0.008	0.027
272	22.67	0.07	0.036	(0.064)	0.008	0.027
273	22.75	0.07	0.036	(0.064)	0.008	0.027
274	22.83	0.07	0.036	(0.064)	0.008	0.027
275	22.92	0.07	0.036	(0.064)	0.008	0.027
276	23.00	0.07	0.036	(0.064)	0.008	0.027
277	23.08	0.07	0.036	(0.063)	0.008	0.027
278	23.17	0.07	0.036	(0.063)	0.008	0.027
279	23.25	0.07	0.036	(0.063)	0.008	0.027
280	23.33	0.07	0.036	(0.063)	0.008	0.027
281	23.42	0.07	0.036	(0.063)	0.008	0.027
282	23.50	0.07	0.036	(0.063)	0.008	0.027
283	23.58	0.07	0.036	(0.063)	0.008	0.027
284	23.67	0.07	0.036	(0.063)	0.008	0.027
285	23.75	0.07	0.036	(0.062)	0.008	0.027
286	23.83	0.07	0.036	(0.062)	0.008	0.027
287	23.92	0.07	0.036	(0.062)	0.008	0.027
288	24.00	0.07	0.036	(0.062)	0.008	0.027

(Loss Rate Not Used)

Sum = 100.0 Sum = 41.3

Flood volume = Effective rainfall 3.44(In)
times area 1.5(Ac.)/[(In)/(Ft.)] = 0.4(Ac.Ft)
Total soil loss = 1.00(In)
Total soil loss = 0.122(Ac.Ft)
Total rainfall = 4.44(In)
Flood volume = 18372.8 Cubic Feet
Total soil loss = 5319.4 Cubic Feet

Peak flow rate of this hydrograph = 0.736(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.02	Q	|	|	|	|
0+10	0.0004	0.04	Q	|	|	|	|
0+15	0.0006	0.04	Q	|	|	|	|
0+20	0.0010	0.05	Q	|	|	|	|
0+25	0.0014	0.06	Q	|	|	|	|
0+30	0.0018	0.06	Q	|	|	|	|
0+35	0.0022	0.06	Q	|	|	|	|
0+40	0.0026	0.06	Q	|	|	|	|
0+45	0.0031	0.06	Q	|	|	|	|
0+50	0.0035	0.07	Q	|	|	|	|

0+55	0.0041	0.08	Q	|	|	|	|
1+ 0	0.0046	0.08	Q	|	|	|	|
1+ 5	0.0051	0.07	Q	|	|	|	|
1+10	0.0056	0.06	Q	|	|	|	|
1+15	0.0060	0.06	Q	|	|	|	|
1+20	0.0064	0.06	Q	|	|	|	|
1+25	0.0068	0.06	Q	|	|	|	|
1+30	0.0073	0.06	Q	|	|	|	|
1+35	0.0077	0.06	Q	|	|	|	|
1+40	0.0081	0.06	Q	|	|	|	|
1+45	0.0085	0.06	Q	|	|	|	|
1+50	0.0090	0.07	Q	|	|	|	|
1+55	0.0095	0.08	Q	|	|	|	|
2+ 0	0.0101	0.08	Q	|	|	|	|
2+ 5	0.0107	0.08	QV	|	|	|	|
2+10	0.0112	0.08	QV	|	|	|	|
2+15	0.0118	0.08	QV	|	|	|	|
2+20	0.0123	0.08	QV	|	|	|	|
2+25	0.0129	0.08	QV	|	|	|	|
2+30	0.0134	0.08	QV	|	|	|	|
2+35	0.0141	0.09	QV	|	|	|	|
2+40	0.0147	0.10	QV	|	|	|	|
2+45	0.0154	0.10	QV	|	|	|	|
2+50	0.0161	0.10	QV	|	|	|	|
2+55	0.0168	0.10	QV	|	|	|	|
3+ 0	0.0175	0.10	QV	|	|	|	|
3+ 5	0.0182	0.10	QV	|	|	|	|
3+10	0.0189	0.10	QV	|	|	|	|
3+15	0.0196	0.10	QV	|	|	|	|
3+20	0.0203	0.10	QV	|	|	|	|
3+25	0.0210	0.10	QV	|	|	|	|
3+30	0.0217	0.10	Q V	|	|	|	|
3+35	0.0224	0.10	Q V	|	|	|	|
3+40	0.0231	0.10	Q V	|	|	|	|
3+45	0.0238	0.10	Q V	|	|	|	|
3+50	0.0246	0.11	Q V	|	|	|	|
3+55	0.0254	0.12	Q V	|	|	|	|
4+ 0	0.0262	0.12	Q V	|	|	|	|
4+ 5	0.0271	0.12	Q V	|	|	|	|
4+10	0.0279	0.12	Q V	|	|	|	|
4+15	0.0287	0.12	Q V	|	|	|	|
4+20	0.0296	0.13	Q V	|	|	|	|
4+25	0.0306	0.14	Q V	|	|	|	|
4+30	0.0316	0.14	Q V	|	|	|	|
4+35	0.0326	0.14	Q V	|	|	|	|
4+40	0.0335	0.14	Q V	|	|	|	|
4+45	0.0345	0.14	Q V	|	|	|	|
4+50	0.0356	0.15	Q V	|	|	|	|
4+55	0.0367	0.16	Q V	|	|	|	|
5+ 0	0.0378	0.16	Q V	|	|	|	|
5+ 5	0.0388	0.14	Q V	|	|	|	|
5+10	0.0396	0.13	Q V	|	|	|	|
5+15	0.0405	0.12	Q V	|	|	|	|

5+20	0.0414	0.13	Q V	|	|	|	|
5+25	0.0423	0.14	Q V	|	|	|	|
5+30	0.0433	0.14	Q V	|	|	|	|
5+35	0.0444	0.15	Q V	|	|	|	|
5+40	0.0455	0.16	Q V	|	|	|	|
5+45	0.0466	0.16	Q V	|	|	|	|
5+50	0.0477	0.16	Q V	|	|	|	|
5+55	0.0488	0.16	Q V	|	|	|	|
6+ 0	0.0499	0.16	Q V	|	|	|	|
6+ 5	0.0511	0.17	Q V	|	|	|	|
6+10	0.0523	0.18	Q V	|	|	|	|
6+15	0.0536	0.18	Q V	|	|	|	|
6+20	0.0548	0.18	Q V	|	|	|	|
6+25	0.0561	0.18	Q V	|	|	|	|
6+30	0.0574	0.18	Q V	|	|	|	|
6+35	0.0587	0.19	Q V	|	|	|	|
6+40	0.0601	0.20	Q V	|	|	|	|
6+45	0.0615	0.20	Q V	|	|	|	|
6+50	0.0629	0.20	Q V	|	|	|	|
6+55	0.0642	0.20	Q V	|	|	|	|
7+ 0	0.0656	0.20	Q V	|	|	|	|
7+ 5	0.0670	0.20	Q V	|	|	|	|
7+10	0.0684	0.20	Q V	|	|	|	|
7+15	0.0698	0.20	Q V	|	|	|	|
7+20	0.0713	0.21	Q V	|	|	|	|
7+25	0.0728	0.22	Q V	|	|	|	|
7+30	0.0743	0.22	Q V	|	|	|	|
7+35	0.0759	0.23	Q V	|	|	|	|
7+40	0.0776	0.24	Q V	|	|	|	|
7+45	0.0793	0.24	Q V	|	|	|	|
7+50	0.0810	0.25	|Q V	|	|	|	|
7+55	0.0828	0.26	|Q V	|	|	|	|
8+ 0	0.0846	0.26	|Q V	|	|	|	|
8+ 5	0.0866	0.28	|Q V	|	|	|	|
8+10	0.0886	0.30	|Q V	|	|	|	|
8+15	0.0907	0.30	|Q V	|	|	|	|
8+20	0.0928	0.30	|Q V	|	|	|	|
8+25	0.0949	0.30	|Q V|	|	|	|	|
8+30	0.0970	0.30	|Q V|	|	|	|	|
8+35	0.0992	0.31	|Q V|	|	|	|	|
8+40	0.1014	0.32	|Q V|	|	|	|	|
8+45	0.1036	0.32	|Q V|	|	|	|	|
8+50	0.1059	0.33	|Q V	|	|	|	|
8+55	0.1083	0.34	|Q V	|	|	|	|
9+ 0	0.1106	0.34	|Q V	|	|	|	|
9+ 5	0.1131	0.36	|Q V	|	|	|	|
9+10	0.1158	0.38	|Q V	|	|	|	|
9+15	0.1184	0.38	|Q |V	|	|	|	|
9+20	0.1211	0.39	|Q |V	|	|	|	|
9+25	0.1239	0.40	|Q |V	|	|	|	|
9+30	0.1267	0.40	|Q | V	|	|	|	|
9+35	0.1295	0.41	|Q | V	|	|	|	|
9+40	0.1325	0.42	|Q | V	|	|	|	|

9+45	0.1354	0.43	Q	V			
9+50	0.1384	0.43	Q	V			
9+55	0.1414	0.44	Q	V			
10+ 0	0.1445	0.45	Q	V			
10+ 5	0.1471	0.38	Q	V			
10+10	0.1493	0.32	Q	V			
10+15	0.1514	0.31	Q	V			
10+20	0.1535	0.30	Q	V			
10+25	0.1556	0.30	Q	V			
10+30	0.1577	0.30	Q	V			
10+35	0.1601	0.35	Q	V			
10+40	0.1629	0.39	Q	V			
10+45	0.1656	0.40	Q	V			
10+50	0.1684	0.41	Q	V			
10+55	0.1712	0.41	Q	V			
11+ 0	0.1740	0.41	Q	V			
11+ 5	0.1767	0.40	Q	V			
11+10	0.1794	0.39	Q	V			
11+15	0.1821	0.39	Q	V			
11+20	0.1847	0.39	Q	V			
11+25	0.1874	0.39	Q	V			
11+30	0.1900	0.39	Q	V			
11+35	0.1925	0.37	Q	V			
11+40	0.1949	0.35	Q	V			
11+45	0.1973	0.35	Q	V			
11+50	0.1998	0.35	Q	V			
11+55	0.2023	0.36	Q	V			
12+ 0	0.2048	0.36	Q	V			
12+ 5	0.2077	0.43	Q	V			
12+10	0.2111	0.49	Q	V			
12+15	0.2146	0.50	Q	V			
12+20	0.2181	0.52	Q	V			
12+25	0.2217	0.52	Q	V			
12+30	0.2254	0.53	Q	V			
12+35	0.2291	0.55	Q	V			
12+40	0.2330	0.57	Q	V			
12+45	0.2370	0.57	Q	V			
12+50	0.2410	0.58	Q	V			
12+55	0.2451	0.60	Q	V			
13+ 0	0.2492	0.60	Q	V			
13+ 5	0.2538	0.66	Q	V			
13+10	0.2587	0.72	Q	V			
13+15	0.2637	0.73	Q	V			
13+20	0.2688	0.73	Q	V			
13+25	0.2739	0.74	Q	V			
13+30	0.2789	0.74	Q	V			
13+35	0.2832	0.61	Q	V			
13+40	0.2866	0.49	Q	V			
13+45	0.2898	0.47	Q	V			
13+50	0.2930	0.47	Q	V			
13+55	0.2962	0.47	Q	V			
14+ 0	0.2995	0.47	Q	V			
14+ 5	0.3030	0.51	Q	V			

```
14+10       0.3067      0.55  | Q       |         |        V|         |
14+15       0.3106      0.56  | Q       |         |        V|         |
14+20       0.3143      0.55  | Q       |         |        V|         |
14+25       0.3180      0.54  | Q       |         |         V         |
14+30       0.3217      0.54  | Q       |         |         V         |
14+35       0.3254      0.54  | Q       |         |         V         |
14+40       0.3291      0.54  | Q       |         |          |V       |
14+45       0.3328      0.54  | Q       |         |          |V       |
14+50       0.3364      0.53  | Q       |         |          |V       |
14+55       0.3400      0.52  | Q       |         |          | V      |
15+ 0       0.3435      0.51  | Q       |         |          | V      |
15+ 5       0.3470      0.50  | Q       |         |          | V      |
15+10       0.3504      0.49  |Q        |         |          |  V     |
15+15       0.3537      0.49  |Q        |         |          |  V     |
15+20       0.3570      0.48  |Q        |         |          |  V     |
15+25       0.3603      0.47  |Q        |         |          |   V    |
15+30       0.3635      0.47  |Q        |         |          |   V    |
15+35       0.3664      0.43  |Q        |         |          |   V    |
15+40       0.3692      0.39  |Q        |         |          |    V   |
15+45       0.3718      0.39  |Q        |         |          |    V   |
15+50       0.3745      0.39  |Q        |         |          |    V   |
15+55       0.3771      0.39  |Q        |         |          |    V   |
16+ 0       0.3798      0.39  |Q        |         |          |     V  |
16+ 5       0.3815      0.25  Q         |         |          |     V  |
16+10       0.3823      0.11  Q         |         |          |     V  |
16+15       0.3829      0.09  Q         |         |          |     V  |
16+20       0.3834      0.08  Q         |         |          |     V  |
16+25       0.3840      0.08  Q         |         |          |     V  |
16+30       0.3845      0.08  Q         |         |          |     V  |
16+35       0.3850      0.07  Q         |         |          |     V  |
16+40       0.3855      0.06  Q         |         |          |     V  |
16+45       0.3859      0.06  Q         |         |          |     V  |
16+50       0.3863      0.06  Q         |         |          |     V  |
16+55       0.3867      0.06  Q         |         |          |     V  |
17+ 0       0.3872      0.06  Q         |         |          |     V  |
17+ 5       0.3877      0.08  Q         |         |          |     V  |
17+10       0.3884      0.10  Q         |         |          |     V  |
17+15       0.3891      0.10  Q         |         |          |     V  |
17+20       0.3898      0.10  Q         |         |          |     V  |
17+25       0.3905      0.10  Q         |         |          |      V |
17+30       0.3912      0.10  Q         |         |          |      V |
17+35       0.3919      0.10  Q         |         |          |      V |
17+40       0.3926      0.10  Q         |         |          |      V |
17+45       0.3932      0.10  Q         |         |          |      V |
17+50       0.3939      0.09  Q         |         |          |      V |
17+55       0.3945      0.08  Q         |         |          |      V |
18+ 0       0.3950      0.08  Q         |         |          |      V |
18+ 5       0.3956      0.08  Q         |         |          |      V |
18+10       0.3961      0.08  Q         |         |          |      V |
18+15       0.3967      0.08  Q         |         |          |      V |
18+20       0.3973      0.08  Q         |         |          |      V |
18+25       0.3978      0.08  Q         |         |          |      V |
18+30       0.3984      0.08  Q         |         |          |      V |
```

18+35	0.3989	0.07	Q	|	|	|	V |
18+40	0.3993	0.06	Q	|	|	|	V |
18+45	0.3997	0.06	Q	|	|	|	V |
18+50	0.4001	0.05	Q	|	|	|	V |
18+55	0.4004	0.04	Q	|	|	|	V |
19+ 0	0.4007	0.04	Q	|	|	|	V |
19+ 5	0.4010	0.05	Q	|	|	|	V |
19+10	0.4014	0.06	Q	|	|	|	V |
19+15	0.4018	0.06	Q	|	|	|	V |
19+20	0.4023	0.07	Q	|	|	|	V |
19+25	0.4028	0.08	Q	|	|	|	V |
19+30	0.4034	0.08	Q	|	|	|	V |
19+35	0.4039	0.07	Q	|	|	|	V |
19+40	0.4043	0.06	Q	|	|	|	V |
19+45	0.4047	0.06	Q	|	|	|	V |
19+50	0.4051	0.05	Q	|	|	|	V |
19+55	0.4054	0.04	Q	|	|	|	V |
20+ 0	0.4057	0.04	Q	|	|	|	V |
20+ 5	0.4060	0.05	Q	|	|	|	V |
20+10	0.4064	0.06	Q	|	|	|	V |
20+15	0.4068	0.06	Q	|	|	|	V |
20+20	0.4073	0.06	Q	|	|	|	V |
20+25	0.4077	0.06	Q	|	|	|	V |
20+30	0.4081	0.06	Q	|	|	|	V |
20+35	0.4085	0.06	Q	|	|	|	V |
20+40	0.4089	0.06	Q	|	|	|	V |
20+45	0.4094	0.06	Q	|	|	|	V |
20+50	0.4097	0.05	Q	|	|	|	V |
20+55	0.4100	0.04	Q	|	|	|	V |
21+ 0	0.4103	0.04	Q	|	|	|	V |
21+ 5	0.4106	0.05	Q	|	|	|	V |
21+10	0.4110	0.06	Q	|	|	|	V |
21+15	0.4114	0.06	Q	|	|	|	V|
21+20	0.4118	0.05	Q	|	|	|	V|
21+25	0.4121	0.04	Q	|	|	|	V|
21+30	0.4124	0.04	Q	|	|	|	V|
21+35	0.4127	0.05	Q	|	|	|	V|
21+40	0.4131	0.06	Q	|	|	|	V|
21+45	0.4135	0.06	Q	|	|	|	V|
21+50	0.4139	0.05	Q	|	|	|	V|
21+55	0.4142	0.04	Q	|	|	|	V|
22+ 0	0.4145	0.04	Q	|	|	|	V|
22+ 5	0.4148	0.05	Q	|	|	|	V|
22+10	0.4152	0.06	Q	|	|	|	V|
22+15	0.4156	0.06	Q	|	|	|	V|
22+20	0.4160	0.05	Q	|	|	|	V|
22+25	0.4163	0.04	Q	|	|	|	V|
22+30	0.4166	0.04	Q	|	|	|	V|
22+35	0.4168	0.04	Q	|	|	|	V|
22+40	0.4171	0.04	Q	|	|	|	V|
22+45	0.4174	0.04	Q	|	|	|	V|
22+50	0.4177	0.04	Q	|	|	|	V|
22+55	0.4180	0.04	Q	|	|	|	V|

23+ 0	0.4182	0.04	Q	|	|	|	V|
23+ 5	0.4185	0.04	Q	|	|	|	V|
23+10	0.4188	0.04	Q	|	|	|	V|
23+15	0.4191	0.04	Q	|	|	|	V|
23+20	0.4194	0.04	Q	|	|	|	V|
23+25	0.4196	0.04	Q	|	|	|	V|
23+30	0.4199	0.04	Q	|	|	|	V|
23+35	0.4202	0.04	Q	|	|	|	V|
23+40	0.4205	0.04	Q	|	|	|	V|
23+45	0.4208	0.04	Q	|	|	|	V|
23+50	0.4210	0.04	Q	|	|	|	V|
23+55	0.4213	0.04	Q	|	|	|	V|
24+ 0	0.4216	0.04	Q	|	|	|	V|
24+ 5	0.4217	0.02	Q	|	|	|	V|
24+10	0.4218	0.00	Q	|	|	|	V|
24+15	0.4218	0.00	Q	|	|	|	V|

AREA C1

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014, Version 9.0
Study date 02/05/24 File: ARC124100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6279

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

PROPOSED CONDITION: 100YR HYDROLOGY
ARC1

Drainage Area = 0.74(Ac.) = 0.001 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.74(Ac.) = 0.001 Sq. Mi.
Length along longest watercourse = 379.00(Ft.)
Length along longest watercourse measured to centroid = 189.50(Ft.)
Length along longest watercourse = 0.072 Mi.
Length along longest watercourse measured to centroid = 0.036 Mi.
Difference in elevation = 2.00(Ft.)
Slope along watercourse = 27.8628 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.020 Hr.
Lag time = 1.19 Min.
25% of lag time = 0.30 Min.
40% of lag time = 0.48 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.74	1.16	0.86

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.74	4.44	3.29

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.160(In)
Area Averaged 100-Year Rainfall = 4.440(In)

Point rain (area averaged) = 4.440(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 4.440(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.740	56.00	0.890

Total Area Entered = 0.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.890	0.102	1.000	0.102
					Sum (F) =	0.102

Area averaged mean soil loss (F) (In/Hr) = 0.102
Minimum soil loss rate ((In/Hr)) = 0.051
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.190

U n i t H y d r o g r a p h
DESERT S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	419.661	66.347	0.495
2	0.167	839.321	33.653	0.251
			Sum = 100.000 Sum=	0.746

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max		Low	Effective (In/Hr)
1	0.08	0.07	0.036	(0.180)		0.007	0.029
2	0.17	0.07	0.036	(0.179)		0.007	0.029
3	0.25	0.07	0.036	(0.179)		0.007	0.029

4	0.33	0.10	0.053	(0.178)	0.010	0.043
5	0.42	0.10	0.053	(0.177)	0.010	0.043
6	0.50	0.10	0.053	(0.177)	0.010	0.043
7	0.58	0.10	0.053	(0.176)	0.010	0.043
8	0.67	0.10	0.053	(0.175)	0.010	0.043
9	0.75	0.10	0.053	(0.175)	0.010	0.043
10	0.83	0.13	0.071	(0.174)	0.013	0.058
11	0.92	0.13	0.071	(0.173)	0.013	0.058
12	1.00	0.13	0.071	(0.173)	0.013	0.058
13	1.08	0.10	0.053	(0.172)	0.010	0.043
14	1.17	0.10	0.053	(0.171)	0.010	0.043
15	1.25	0.10	0.053	(0.171)	0.010	0.043
16	1.33	0.10	0.053	(0.170)	0.010	0.043
17	1.42	0.10	0.053	(0.169)	0.010	0.043
18	1.50	0.10	0.053	(0.169)	0.010	0.043
19	1.58	0.10	0.053	(0.168)	0.010	0.043
20	1.67	0.10	0.053	(0.167)	0.010	0.043
21	1.75	0.10	0.053	(0.167)	0.010	0.043
22	1.83	0.13	0.071	(0.166)	0.013	0.058
23	1.92	0.13	0.071	(0.165)	0.013	0.058
24	2.00	0.13	0.071	(0.165)	0.013	0.058
25	2.08	0.13	0.071	(0.164)	0.013	0.058
26	2.17	0.13	0.071	(0.163)	0.013	0.058
27	2.25	0.13	0.071	(0.163)	0.013	0.058
28	2.33	0.13	0.071	(0.162)	0.013	0.058
29	2.42	0.13	0.071	(0.161)	0.013	0.058
30	2.50	0.13	0.071	(0.161)	0.013	0.058
31	2.58	0.17	0.089	(0.160)	0.017	0.072
32	2.67	0.17	0.089	(0.159)	0.017	0.072
33	2.75	0.17	0.089	(0.159)	0.017	0.072
34	2.83	0.17	0.089	(0.158)	0.017	0.072
35	2.92	0.17	0.089	(0.157)	0.017	0.072
36	3.00	0.17	0.089	(0.157)	0.017	0.072
37	3.08	0.17	0.089	(0.156)	0.017	0.072
38	3.17	0.17	0.089	(0.155)	0.017	0.072
39	3.25	0.17	0.089	(0.155)	0.017	0.072
40	3.33	0.17	0.089	(0.154)	0.017	0.072
41	3.42	0.17	0.089	(0.153)	0.017	0.072
42	3.50	0.17	0.089	(0.153)	0.017	0.072
43	3.58	0.17	0.089	(0.152)	0.017	0.072
44	3.67	0.17	0.089	(0.151)	0.017	0.072
45	3.75	0.17	0.089	(0.151)	0.017	0.072
46	3.83	0.20	0.107	(0.150)	0.020	0.086
47	3.92	0.20	0.107	(0.150)	0.020	0.086
48	4.00	0.20	0.107	(0.149)	0.020	0.086
49	4.08	0.20	0.107	(0.148)	0.020	0.086
50	4.17	0.20	0.107	(0.148)	0.020	0.086
51	4.25	0.20	0.107	(0.147)	0.020	0.086
52	4.33	0.23	0.124	(0.146)	0.024	0.101
53	4.42	0.23	0.124	(0.146)	0.024	0.101
54	4.50	0.23	0.124	(0.145)	0.024	0.101
55	4.58	0.23	0.124	(0.145)	0.024	0.101
56	4.67	0.23	0.124	(0.144)	0.024	0.101

57	4.75	0.23	0.124	(0.143)	0.024	0.101
58	4.83	0.27	0.142	(0.143)	0.027	0.115
59	4.92	0.27	0.142	(0.142)	0.027	0.115
60	5.00	0.27	0.142	(0.141)	0.027	0.115
61	5.08	0.20	0.107	(0.141)	0.020	0.086
62	5.17	0.20	0.107	(0.140)	0.020	0.086
63	5.25	0.20	0.107	(0.140)	0.020	0.086
64	5.33	0.23	0.124	(0.139)	0.024	0.101
65	5.42	0.23	0.124	(0.138)	0.024	0.101
66	5.50	0.23	0.124	(0.138)	0.024	0.101
67	5.58	0.27	0.142	(0.137)	0.027	0.115
68	5.67	0.27	0.142	(0.137)	0.027	0.115
69	5.75	0.27	0.142	(0.136)	0.027	0.115
70	5.83	0.27	0.142	(0.135)	0.027	0.115
71	5.92	0.27	0.142	(0.135)	0.027	0.115
72	6.00	0.27	0.142	(0.134)	0.027	0.115
73	6.08	0.30	0.160	(0.134)	0.030	0.129
74	6.17	0.30	0.160	(0.133)	0.030	0.129
75	6.25	0.30	0.160	(0.132)	0.030	0.129
76	6.33	0.30	0.160	(0.132)	0.030	0.129
77	6.42	0.30	0.160	(0.131)	0.030	0.129
78	6.50	0.30	0.160	(0.131)	0.030	0.129
79	6.58	0.33	0.178	(0.130)	0.034	0.144
80	6.67	0.33	0.178	(0.129)	0.034	0.144
81	6.75	0.33	0.178	(0.129)	0.034	0.144
82	6.83	0.33	0.178	(0.128)	0.034	0.144
83	6.92	0.33	0.178	(0.128)	0.034	0.144
84	7.00	0.33	0.178	(0.127)	0.034	0.144
85	7.08	0.33	0.178	(0.127)	0.034	0.144
86	7.17	0.33	0.178	(0.126)	0.034	0.144
87	7.25	0.33	0.178	(0.125)	0.034	0.144
88	7.33	0.37	0.195	(0.125)	0.037	0.158
89	7.42	0.37	0.195	(0.124)	0.037	0.158
90	7.50	0.37	0.195	(0.124)	0.037	0.158
91	7.58	0.40	0.213	(0.123)	0.040	0.173
92	7.67	0.40	0.213	(0.123)	0.040	0.173
93	7.75	0.40	0.213	(0.122)	0.040	0.173
94	7.83	0.43	0.231	(0.121)	0.044	0.187
95	7.92	0.43	0.231	(0.121)	0.044	0.187
96	8.00	0.43	0.231	(0.120)	0.044	0.187
97	8.08	0.50	0.266	(0.120)	0.051	0.216
98	8.17	0.50	0.266	(0.119)	0.051	0.216
99	8.25	0.50	0.266	(0.119)	0.051	0.216
100	8.33	0.50	0.266	(0.118)	0.051	0.216
101	8.42	0.50	0.266	(0.118)	0.051	0.216
102	8.50	0.50	0.266	(0.117)	0.051	0.216
103	8.58	0.53	0.284	(0.116)	0.054	0.230
104	8.67	0.53	0.284	(0.116)	0.054	0.230
105	8.75	0.53	0.284	(0.115)	0.054	0.230
106	8.83	0.57	0.302	(0.115)	0.057	0.245
107	8.92	0.57	0.302	(0.114)	0.057	0.245
108	9.00	0.57	0.302	(0.114)	0.057	0.245
109	9.08	0.63	0.337	(0.113)	0.064	0.273

110	9.17	0.63	0.337	(0.113)	0.064	0.273
111	9.25	0.63	0.337	(0.112)	0.064	0.273
112	9.33	0.67	0.355	(0.112)	0.067	0.288
113	9.42	0.67	0.355	(0.111)	0.067	0.288
114	9.50	0.67	0.355	(0.110)	0.067	0.288
115	9.58	0.70	0.373	(0.110)	0.071	0.302
116	9.67	0.70	0.373	(0.109)	0.071	0.302
117	9.75	0.70	0.373	(0.109)	0.071	0.302
118	9.83	0.73	0.391	(0.108)	0.074	0.316
119	9.92	0.73	0.391	(0.108)	0.074	0.316
120	10.00	0.73	0.391	(0.107)	0.074	0.316
121	10.08	0.50	0.266	(0.107)	0.051	0.216
122	10.17	0.50	0.266	(0.106)	0.051	0.216
123	10.25	0.50	0.266	(0.106)	0.051	0.216
124	10.33	0.50	0.266	(0.105)	0.051	0.216
125	10.42	0.50	0.266	(0.105)	0.051	0.216
126	10.50	0.50	0.266	(0.104)	0.051	0.216
127	10.58	0.67	0.355	(0.104)	0.067	0.288
128	10.67	0.67	0.355	(0.103)	0.067	0.288
129	10.75	0.67	0.355	(0.103)	0.067	0.288
130	10.83	0.67	0.355	(0.102)	0.067	0.288
131	10.92	0.67	0.355	(0.102)	0.067	0.288
132	11.00	0.67	0.355	(0.101)	0.067	0.288
133	11.08	0.63	0.337	(0.101)	0.064	0.273
134	11.17	0.63	0.337	(0.100)	0.064	0.273
135	11.25	0.63	0.337	(0.100)	0.064	0.273
136	11.33	0.63	0.337	(0.099)	0.064	0.273
137	11.42	0.63	0.337	(0.099)	0.064	0.273
138	11.50	0.63	0.337	(0.098)	0.064	0.273
139	11.58	0.57	0.302	(0.098)	0.057	0.245
140	11.67	0.57	0.302	(0.097)	0.057	0.245
141	11.75	0.57	0.302	(0.097)	0.057	0.245
142	11.83	0.60	0.320	(0.096)	0.061	0.259
143	11.92	0.60	0.320	(0.096)	0.061	0.259
144	12.00	0.60	0.320	(0.095)	0.061	0.259
145	12.08	0.83	0.444	(0.095)	0.084	0.360
146	12.17	0.83	0.444	(0.094)	0.084	0.360
147	12.25	0.83	0.444	(0.094)	0.084	0.360
148	12.33	0.87	0.462	(0.093)	0.088	0.374
149	12.42	0.87	0.462	(0.093)	0.088	0.374
150	12.50	0.87	0.462	(0.093)	0.088	0.374
151	12.58	0.93	0.497	0.092	(0.094)	0.405
152	12.67	0.93	0.497	0.092	(0.094)	0.406
153	12.75	0.93	0.497	0.091	(0.094)	0.406
154	12.83	0.97	0.515	0.091	(0.098)	0.424
155	12.92	0.97	0.515	0.090	(0.098)	0.425
156	13.00	0.97	0.515	0.090	(0.098)	0.425
157	13.08	1.13	0.604	0.089	(0.115)	0.515
158	13.17	1.13	0.604	0.089	(0.115)	0.515
159	13.25	1.13	0.604	0.088	(0.115)	0.515
160	13.33	1.13	0.604	0.088	(0.115)	0.516
161	13.42	1.13	0.604	0.088	(0.115)	0.516
162	13.50	1.13	0.604	0.087	(0.115)	0.517

163	13.58	0.77	0.408	(	0.087)	0.078		0.331
164	13.67	0.77	0.408	(	0.086)	0.078		0.331
165	13.75	0.77	0.408	(	0.086)	0.078		0.331
166	13.83	0.77	0.408	(	0.085)	0.078		0.331
167	13.92	0.77	0.408	(	0.085)	0.078		0.331
168	14.00	0.77	0.408	(	0.084)	0.078		0.331
169	14.08	0.90	0.480		0.084	(	0.091)	0.396
170	14.17	0.90	0.480		0.084	(	0.091)	0.396
171	14.25	0.90	0.480		0.083	(	0.091)	0.396
172	14.33	0.87	0.462		0.083	(	0.088)	0.379
173	14.42	0.87	0.462		0.082	(	0.088)	0.379
174	14.50	0.87	0.462		0.082	(	0.088)	0.380
175	14.58	0.87	0.462		0.081	(	0.088)	0.380
176	14.67	0.87	0.462		0.081	(	0.088)	0.381
177	14.75	0.87	0.462		0.081	(	0.088)	0.381
178	14.83	0.83	0.444		0.080	(	0.084)	0.364
179	14.92	0.83	0.444		0.080	(	0.084)	0.364
180	15.00	0.83	0.444		0.079	(	0.084)	0.365
181	15.08	0.80	0.426		0.079	(	0.081)	0.347
182	15.17	0.80	0.426		0.079	(	0.081)	0.348
183	15.25	0.80	0.426		0.078	(	0.081)	0.348
184	15.33	0.77	0.408	(	0.078)	0.078		0.331
185	15.42	0.77	0.408		0.077	(	0.078)	0.331
186	15.50	0.77	0.408		0.077	(	0.078)	0.331
187	15.58	0.63	0.337	(	0.077)	0.064		0.273
188	15.67	0.63	0.337	(	0.076)	0.064		0.273
189	15.75	0.63	0.337	(	0.076)	0.064		0.273
190	15.83	0.63	0.337	(	0.075)	0.064		0.273
191	15.92	0.63	0.337	(	0.075)	0.064		0.273
192	16.00	0.63	0.337	(	0.075)	0.064		0.273
193	16.08	0.13	0.071	(	0.074)	0.013		0.058
194	16.17	0.13	0.071	(	0.074)	0.013		0.058
195	16.25	0.13	0.071	(	0.074)	0.013		0.058
196	16.33	0.13	0.071	(	0.073)	0.013		0.058
197	16.42	0.13	0.071	(	0.073)	0.013		0.058
198	16.50	0.13	0.071	(	0.072)	0.013		0.058
199	16.58	0.10	0.053	(	0.072)	0.010		0.043
200	16.67	0.10	0.053	(	0.072)	0.010		0.043
201	16.75	0.10	0.053	(	0.071)	0.010		0.043
202	16.83	0.10	0.053	(	0.071)	0.010		0.043
203	16.92	0.10	0.053	(	0.071)	0.010		0.043
204	17.00	0.10	0.053	(	0.070)	0.010		0.043
205	17.08	0.17	0.089	(	0.070)	0.017		0.072
206	17.17	0.17	0.089	(	0.070)	0.017		0.072
207	17.25	0.17	0.089	(	0.069)	0.017		0.072
208	17.33	0.17	0.089	(	0.069)	0.017		0.072
209	17.42	0.17	0.089	(	0.068)	0.017		0.072
210	17.50	0.17	0.089	(	0.068)	0.017		0.072
211	17.58	0.17	0.089	(	0.068)	0.017		0.072
212	17.67	0.17	0.089	(	0.067)	0.017		0.072
213	17.75	0.17	0.089	(	0.067)	0.017		0.072
214	17.83	0.13	0.071	(	0.067)	0.013		0.058
215	17.92	0.13	0.071	(	0.066)	0.013		0.058

216	18.00	0.13	0.071	(0.066)	0.013	0.058
217	18.08	0.13	0.071	(0.066)	0.013	0.058
218	18.17	0.13	0.071	(0.065)	0.013	0.058
219	18.25	0.13	0.071	(0.065)	0.013	0.058
220	18.33	0.13	0.071	(0.065)	0.013	0.058
221	18.42	0.13	0.071	(0.065)	0.013	0.058
222	18.50	0.13	0.071	(0.064)	0.013	0.058
223	18.58	0.10	0.053	(0.064)	0.010	0.043
224	18.67	0.10	0.053	(0.064)	0.010	0.043
225	18.75	0.10	0.053	(0.063)	0.010	0.043
226	18.83	0.07	0.036	(0.063)	0.007	0.029
227	18.92	0.07	0.036	(0.063)	0.007	0.029
228	19.00	0.07	0.036	(0.062)	0.007	0.029
229	19.08	0.10	0.053	(0.062)	0.010	0.043
230	19.17	0.10	0.053	(0.062)	0.010	0.043
231	19.25	0.10	0.053	(0.062)	0.010	0.043
232	19.33	0.13	0.071	(0.061)	0.013	0.058
233	19.42	0.13	0.071	(0.061)	0.013	0.058
234	19.50	0.13	0.071	(0.061)	0.013	0.058
235	19.58	0.10	0.053	(0.060)	0.010	0.043
236	19.67	0.10	0.053	(0.060)	0.010	0.043
237	19.75	0.10	0.053	(0.060)	0.010	0.043
238	19.83	0.07	0.036	(0.060)	0.007	0.029
239	19.92	0.07	0.036	(0.059)	0.007	0.029
240	20.00	0.07	0.036	(0.059)	0.007	0.029
241	20.08	0.10	0.053	(0.059)	0.010	0.043
242	20.17	0.10	0.053	(0.059)	0.010	0.043
243	20.25	0.10	0.053	(0.058)	0.010	0.043
244	20.33	0.10	0.053	(0.058)	0.010	0.043
245	20.42	0.10	0.053	(0.058)	0.010	0.043
246	20.50	0.10	0.053	(0.058)	0.010	0.043
247	20.58	0.10	0.053	(0.057)	0.010	0.043
248	20.67	0.10	0.053	(0.057)	0.010	0.043
249	20.75	0.10	0.053	(0.057)	0.010	0.043
250	20.83	0.07	0.036	(0.057)	0.007	0.029
251	20.92	0.07	0.036	(0.056)	0.007	0.029
252	21.00	0.07	0.036	(0.056)	0.007	0.029
253	21.08	0.10	0.053	(0.056)	0.010	0.043
254	21.17	0.10	0.053	(0.056)	0.010	0.043
255	21.25	0.10	0.053	(0.055)	0.010	0.043
256	21.33	0.07	0.036	(0.055)	0.007	0.029
257	21.42	0.07	0.036	(0.055)	0.007	0.029
258	21.50	0.07	0.036	(0.055)	0.007	0.029
259	21.58	0.10	0.053	(0.055)	0.010	0.043
260	21.67	0.10	0.053	(0.054)	0.010	0.043
261	21.75	0.10	0.053	(0.054)	0.010	0.043
262	21.83	0.07	0.036	(0.054)	0.007	0.029
263	21.92	0.07	0.036	(0.054)	0.007	0.029
264	22.00	0.07	0.036	(0.054)	0.007	0.029
265	22.08	0.10	0.053	(0.053)	0.010	0.043
266	22.17	0.10	0.053	(0.053)	0.010	0.043
267	22.25	0.10	0.053	(0.053)	0.010	0.043
268	22.33	0.07	0.036	(0.053)	0.007	0.029

269	22.42	0.07	0.036	(0.053)	0.007	0.029
270	22.50	0.07	0.036	(0.053)	0.007	0.029
271	22.58	0.07	0.036	(0.053)	0.007	0.029
272	22.67	0.07	0.036	(0.052)	0.007	0.029
273	22.75	0.07	0.036	(0.052)	0.007	0.029
274	22.83	0.07	0.036	(0.052)	0.007	0.029
275	22.92	0.07	0.036	(0.052)	0.007	0.029
276	23.00	0.07	0.036	(0.052)	0.007	0.029
277	23.08	0.07	0.036	(0.052)	0.007	0.029
278	23.17	0.07	0.036	(0.052)	0.007	0.029
279	23.25	0.07	0.036	(0.051)	0.007	0.029
280	23.33	0.07	0.036	(0.051)	0.007	0.029
281	23.42	0.07	0.036	(0.051)	0.007	0.029
282	23.50	0.07	0.036	(0.051)	0.007	0.029
283	23.58	0.07	0.036	(0.051)	0.007	0.029
284	23.67	0.07	0.036	(0.051)	0.007	0.029
285	23.75	0.07	0.036	(0.051)	0.007	0.029
286	23.83	0.07	0.036	(0.051)	0.007	0.029
287	23.92	0.07	0.036	(0.051)	0.007	0.029
288	24.00	0.07	0.036	(0.051)	0.007	0.029

(Loss Rate Not Used)

Sum = 100.0 Sum = 43.4

Flood volume = Effective rainfall 3.62(In)
times area 0.7(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 0.82(In)
Total soil loss = 0.051(Ac.Ft)
Total rainfall = 4.44(In)
Flood volume = 9721.4 Cubic Feet
Total soil loss = 2205.3 Cubic Feet

Peak flow rate of this hydrograph = 0.385(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.01	Q	|	|	|	|
0+10	0.0002	0.02	Q	|	|	|	|
0+15	0.0004	0.02	Q	|	|	|	|
0+20	0.0006	0.03	Q	|	|	|	|
0+25	0.0008	0.03	Q	|	|	|	|
0+30	0.0010	0.03	Q	|	|	|	|
0+35	0.0013	0.03	Q	|	|	|	|
0+40	0.0015	0.03	Q	|	|	|	|
0+45	0.0017	0.03	Q	|	|	|	|
0+50	0.0020	0.04	Q	|	|	|	|
0+55	0.0023	0.04	Q	|	|	|	|
1+ 0	0.0026	0.04	Q	|	|	|	|

1+ 5	0.0028	0.04	Q	|	|	|	|
1+10	0.0030	0.03	Q	|	|	|	|
1+15	0.0033	0.03	Q	|	|	|	|
1+20	0.0035	0.03	Q	|	|	|	|
1+25	0.0037	0.03	Q	|	|	|	|
1+30	0.0039	0.03	Q	|	|	|	|
1+35	0.0041	0.03	Q	|	|	|	|
1+40	0.0044	0.03	Q	|	|	|	|
1+45	0.0046	0.03	Q	|	|	|	|
1+50	0.0049	0.04	Q	|	|	|	|
1+55	0.0051	0.04	Q	|	|	|	|
2+ 0	0.0054	0.04	Q	|	|	|	|
2+ 5	0.0057	0.04	QV	|	|	|	|
2+10	0.0060	0.04	QV	|	|	|	|
2+15	0.0063	0.04	QV	|	|	|	|
2+20	0.0066	0.04	QV	|	|	|	|
2+25	0.0069	0.04	QV	|	|	|	|
2+30	0.0072	0.04	QV	|	|	|	|
2+35	0.0076	0.05	QV	|	|	|	|
2+40	0.0079	0.05	QV	|	|	|	|
2+45	0.0083	0.05	QV	|	|	|	|
2+50	0.0087	0.05	QV	|	|	|	|
2+55	0.0090	0.05	QV	|	|	|	|
3+ 0	0.0094	0.05	QV	|	|	|	|
3+ 5	0.0098	0.05	QV	|	|	|	|
3+10	0.0102	0.05	QV	|	|	|	|
3+15	0.0105	0.05	QV	|	|	|	|
3+20	0.0109	0.05	QV	|	|	|	|
3+25	0.0113	0.05	Q V	|	|	|	|
3+30	0.0116	0.05	Q V	|	|	|	|
3+35	0.0120	0.05	Q V	|	|	|	|
3+40	0.0124	0.05	Q V	|	|	|	|
3+45	0.0127	0.05	Q V	|	|	|	|
3+50	0.0132	0.06	Q V	|	|	|	|
3+55	0.0136	0.06	Q V	|	|	|	|
4+ 0	0.0140	0.06	Q V	|	|	|	|
4+ 5	0.0145	0.06	Q V	|	|	|	|
4+10	0.0149	0.06	Q V	|	|	|	|
4+15	0.0154	0.06	Q V	|	|	|	|
4+20	0.0159	0.07	Q V	|	|	|	|
4+25	0.0164	0.08	Q V	|	|	|	|
4+30	0.0169	0.08	Q V	|	|	|	|
4+35	0.0174	0.08	Q V	|	|	|	|
4+40	0.0179	0.08	Q V	|	|	|	|
4+45	0.0185	0.08	Q V	|	|	|	|
4+50	0.0190	0.08	Q V	|	|	|	|
4+55	0.0196	0.09	Q V	|	|	|	|
5+ 0	0.0202	0.09	Q V	|	|	|	|
5+ 5	0.0207	0.07	Q V	|	|	|	|
5+10	0.0211	0.06	Q V	|	|	|	|
5+15	0.0216	0.06	Q V	|	|	|	|
5+20	0.0221	0.07	Q V	|	|	|	|
5+25	0.0226	0.08	Q V	|	|	|	|

5+30	0.0231	0.08	Q	V	|	|	|	|
5+35	0.0237	0.08	Q	V	|	|	|	|
5+40	0.0243	0.09	Q	V	|	|	|	|
5+45	0.0249	0.09	Q	V	|	|	|	|
5+50	0.0255	0.09	Q	V	|	|	|	|
5+55	0.0260	0.09	Q	V	|	|	|	|
6+ 0	0.0266	0.09	Q	V	|	|	|	|
6+ 5	0.0273	0.09	Q	V	|	|	|	|
6+10	0.0279	0.10	Q	V	|	|	|	|
6+15	0.0286	0.10	Q	V	|	|	|	|
6+20	0.0293	0.10	Q	V	|	|	|	|
6+25	0.0299	0.10	Q	V	|	|	|	|
6+30	0.0306	0.10	Q	V	|	|	|	|
6+35	0.0313	0.10	Q	V	|	|	|	|
6+40	0.0321	0.11	Q	V	|	|	|	|
6+45	0.0328	0.11	Q	V	|	|	|	|
6+50	0.0335	0.11	Q	V	|	|	|	|
6+55	0.0343	0.11	Q	V	|	|	|	|
7+ 0	0.0350	0.11	Q	V	|	|	|	|
7+ 5	0.0358	0.11	Q	V	|	|	|	|
7+10	0.0365	0.11	Q	V	|	|	|	|
7+15	0.0372	0.11	Q	V	|	|	|	|
7+20	0.0380	0.11	Q	V	|	|	|	|
7+25	0.0388	0.12	Q	V	|	|	|	|
7+30	0.0396	0.12	Q	V	|	|	|	|
7+35	0.0405	0.13	Q	V	|	|	|	|
7+40	0.0414	0.13	Q	V	|	|	|	|
7+45	0.0423	0.13	Q	V	|	|	|	|
7+50	0.0432	0.14	Q	V	|	|	|	|
7+55	0.0442	0.14	Q	V	|	|	|	|
8+ 0	0.0451	0.14	Q	V	|	|	|	|
8+ 5	0.0462	0.15	Q	V	|	|	|	|
8+10	0.0473	0.16	Q	V	|	|	|	|
8+15	0.0484	0.16	Q	V	|	|	|	|
8+20	0.0495	0.16	Q	V	|	|	|	|
8+25	0.0506	0.16	Q	V	|	|	|	|
8+30	0.0517	0.16	Q	V	|	|	|	|
8+35	0.0529	0.17	Q	V	|	|	|	|
8+40	0.0541	0.17	Q	V	|	|	|	|
8+45	0.0553	0.17	Q	V	|	|	|	|
8+50	0.0565	0.18	Q	V	|	|	|	|
8+55	0.0578	0.18	Q	V	|	|	|	|
9+ 0	0.0590	0.18	Q	V	|	|	|	|
9+ 5	0.0604	0.20	Q	V	|	|	|	|
9+10	0.0618	0.20	Q	V	|	|	|	|
9+15	0.0632	0.20	Q	V	|	|	|	|
9+20	0.0646	0.21	Q	V	|	|	|	|
9+25	0.0661	0.21	Q	V	|	|	|	|
9+30	0.0676	0.21	Q	V	|	|	|	|
9+35	0.0691	0.22	Q	V	|	|	|	|
9+40	0.0707	0.23	Q	V	|	|	|	|
9+45	0.0722	0.23	Q	V	|	|	|	|
9+50	0.0738	0.23	Q	V	|	|	|	|

9+55	0.0754	0.24	Q	| V	|	|	|
10+ 0	0.0771	0.24	Q	| V	|	|	|
10+ 5	0.0784	0.19	Q	| V	|	|	|
10+10	0.0795	0.16	Q	| V	|	|	|
10+15	0.0806	0.16	Q	| V	|	|	|
10+20	0.0817	0.16	Q	| V	|	|	|
10+25	0.0828	0.16	Q	| V	|	|	|
10+30	0.0839	0.16	Q	| V	|	|	|
10+35	0.0853	0.20	Q	| V	|	|	|
10+40	0.0867	0.21	Q	| V	|	|	|
10+45	0.0882	0.21	Q	| V	|	|	|
10+50	0.0897	0.21	Q	| V	|	|	|
10+55	0.0912	0.21	Q	| V	|	|	|
11+ 0	0.0926	0.21	Q	| V	|	|	|
11+ 5	0.0941	0.21	Q	| V	|	|	|
11+10	0.0955	0.20	Q	| V	|	|	|
11+15	0.0969	0.20	Q	| V	|	|	|
11+20	0.0983	0.20	Q	| V	|	|	|
11+25	0.0997	0.20	Q	| V	|	|	|
11+30	0.1011	0.20	Q	| V	|	|	|
11+35	0.1024	0.19	Q	| V	|	|	|
11+40	0.1037	0.18	Q	| V	|	|	|
11+45	0.1049	0.18	Q	| V	|	|	|
11+50	0.1062	0.19	Q	| V	|	|	|
11+55	0.1076	0.19	Q	| V	|	|	|
12+ 0	0.1089	0.19	Q	| V	|	|	|
12+ 5	0.1106	0.24	Q	| V	|	|	|
12+10	0.1124	0.27	|Q	| V	|	|	|
12+15	0.1143	0.27	|Q	| V	|	|	|
12+20	0.1162	0.28	|Q	| V	|	|	|
12+25	0.1181	0.28	|Q	| |V	|	|	|
12+30	0.1200	0.28	|Q	| |V	|	|	|
12+35	0.1220	0.29	|Q	| |V	|	|	|
12+40	0.1241	0.30	|Q	| | V	|	|	|
12+45	0.1262	0.30	|Q	| | V	|	|	|
12+50	0.1283	0.31	|Q	| | V	|	|	|
12+55	0.1305	0.32	|Q	| | V	|	|	|
13+ 0	0.1327	0.32	|Q	| | V	|	|	|
13+ 5	0.1352	0.36	|Q	| | V	|	|	|
13+10	0.1379	0.38	|Q	| | V	|	|	|
13+15	0.1405	0.38	|Q	| | V	|	|	|
13+20	0.1431	0.38	|Q	| | V	|	|	|
13+25	0.1458	0.39	|Q	| | V	|	|	|
13+30	0.1485	0.39	|Q	| | V	|	|	|
13+35	0.1505	0.29	|Q	| | V	|	|	|
13+40	0.1522	0.25	Q	| | V	|	|	|
13+45	0.1539	0.25	Q	| | V	|	|	|
13+50	0.1556	0.25	Q	| | V	|	|	|
13+55	0.1573	0.25	Q	| | V	|	|	|
14+ 0	0.1590	0.25	Q	| | V	|	|	|
14+ 5	0.1609	0.28	|Q	| | V	|	|	|
14+10	0.1629	0.30	|Q	| | V	|	|	|
14+15	0.1650	0.30	|Q	| | V	|	|	|

```
14+20       0.1669      0.29  |Q        |         |        V|         |
14+25       0.1689      0.28  |Q        |         |         V         |
14+30       0.1708      0.28  |Q        |         |         V         |
14+35       0.1728      0.28  |Q        |         |         V         |
14+40       0.1748      0.28  |Q        |         |         |V        |
14+45       0.1767      0.28  |Q        |         |         |V        |
14+50       0.1786      0.28  |Q        |         |         | V       |
14+55       0.1805      0.27  |Q        |         |         | V       |
15+ 0       0.1824      0.27  |Q        |         |         | V       |
15+ 5       0.1842      0.26  |Q        |         |         |  V      |
15+10       0.1860      0.26  |Q        |         |         |  V      |
15+15       0.1877      0.26  |Q        |         |         |  V      |
15+20       0.1895      0.25  |Q        |         |         |  V      |
15+25       0.1912      0.25  Q         |         |         |   V     |
15+30       0.1929      0.25  Q         |         |         |   V     |
15+35       0.1944      0.22  Q         |         |         |   V     |
15+40       0.1958      0.20  Q         |         |         |    V    |
15+45       0.1972      0.20  Q         |         |         |    V    |
15+50       0.1986      0.20  Q         |         |         |    V    |
15+55       0.2000      0.20  Q         |         |         |    V    |
16+ 0       0.2014      0.20  Q         |         |         |     V   |
16+ 5       0.2021      0.10  Q         |         |         |     V   |
16+10       0.2024      0.04  Q         |         |         |     V   |
16+15       0.2027      0.04  Q         |         |         |     V   |
16+20       0.2030      0.04  Q         |         |         |     V   |
16+25       0.2033      0.04  Q         |         |         |     V   |
16+30       0.2036      0.04  Q         |         |         |     V   |
16+35       0.2038      0.04  Q         |         |         |     V   |
16+40       0.2040      0.03  Q         |         |         |     V   |
16+45       0.2042      0.03  Q         |         |         |     V   |
16+50       0.2045      0.03  Q         |         |         |     V   |
16+55       0.2047      0.03  Q         |         |         |     V   |
17+ 0       0.2049      0.03  Q         |         |         |     V   |
17+ 5       0.2052      0.05  Q         |         |         |     V   |
17+10       0.2056      0.05  Q         |         |         |     V   |
17+15       0.2060      0.05  Q         |         |         |     V   |
17+20       0.2063      0.05  Q         |         |         |     V   |
17+25       0.2067      0.05  Q         |         |         |      V  |
17+30       0.2071      0.05  Q         |         |         |      V  |
17+35       0.2075      0.05  Q         |         |         |      V  |
17+40       0.2078      0.05  Q         |         |         |      V  |
17+45       0.2082      0.05  Q         |         |         |      V  |
17+50       0.2085      0.05  Q         |         |         |      V  |
17+55       0.2088      0.04  Q         |         |         |      V  |
18+ 0       0.2091      0.04  Q         |         |         |      V  |
18+ 5       0.2094      0.04  Q         |         |         |      V  |
18+10       0.2097      0.04  Q         |         |         |      V  |
18+15       0.2100      0.04  Q         |         |         |      V  |
18+20       0.2103      0.04  Q         |         |         |      V  |
18+25       0.2106      0.04  Q         |         |         |      V  |
18+30       0.2109      0.04  Q         |         |         |      V  |
18+35       0.2111      0.04  Q         |         |         |      V  |
18+40       0.2113      0.03  Q         |         |         |      V  |
```

18+45	0.2116	0.03	Q	|	|	|	V |
18+50	0.2117	0.03	Q	|	|	|	V |
18+55	0.2119	0.02	Q	|	|	|	V |
19+ 0	0.2120	0.02	Q	|	|	|	V |
19+ 5	0.2122	0.03	Q	|	|	|	V |
19+10	0.2125	0.03	Q	|	|	|	V |
19+15	0.2127	0.03	Q	|	|	|	V |
19+20	0.2129	0.04	Q	|	|	|	V |
19+25	0.2132	0.04	Q	|	|	|	V |
19+30	0.2135	0.04	Q	|	|	|	V |
19+35	0.2138	0.04	Q	|	|	|	V |
19+40	0.2140	0.03	Q	|	|	|	V |
19+45	0.2142	0.03	Q	|	|	|	V |
19+50	0.2144	0.03	Q	|	|	|	V |
19+55	0.2145	0.02	Q	|	|	|	V |
20+ 0	0.2147	0.02	Q	|	|	|	V |
20+ 5	0.2149	0.03	Q	|	|	|	V |
20+10	0.2151	0.03	Q	|	|	|	V |
20+15	0.2153	0.03	Q	|	|	|	V |
20+20	0.2156	0.03	Q	|	|	|	V |
20+25	0.2158	0.03	Q	|	|	|	V |
20+30	0.2160	0.03	Q	|	|	|	V |
20+35	0.2162	0.03	Q	|	|	|	V |
20+40	0.2164	0.03	Q	|	|	|	V |
20+45	0.2167	0.03	Q	|	|	|	V |
20+50	0.2168	0.03	Q	|	|	|	V |
20+55	0.2170	0.02	Q	|	|	|	V |
21+ 0	0.2171	0.02	Q	|	|	|	V |
21+ 5	0.2173	0.03	Q	|	|	|	V |
21+10	0.2176	0.03	Q	|	|	|	V |
21+15	0.2178	0.03	Q	|	|	|	V|
21+20	0.2179	0.03	Q	|	|	|	V|
21+25	0.2181	0.02	Q	|	|	|	V|
21+30	0.2182	0.02	Q	|	|	|	V|
21+35	0.2184	0.03	Q	|	|	|	V|
21+40	0.2187	0.03	Q	|	|	|	V|
21+45	0.2189	0.03	Q	|	|	|	V|
21+50	0.2191	0.03	Q	|	|	|	V|
21+55	0.2192	0.02	Q	|	|	|	V|
22+ 0	0.2194	0.02	Q	|	|	|	V|
22+ 5	0.2196	0.03	Q	|	|	|	V|
22+10	0.2198	0.03	Q	|	|	|	V|
22+15	0.2200	0.03	Q	|	|	|	V|
22+20	0.2202	0.03	Q	|	|	|	V|
22+25	0.2203	0.02	Q	|	|	|	V|
22+30	0.2205	0.02	Q	|	|	|	V|
22+35	0.2206	0.02	Q	|	|	|	V|
22+40	0.2208	0.02	Q	|	|	|	V|
22+45	0.2209	0.02	Q	|	|	|	V|
22+50	0.2211	0.02	Q	|	|	|	V|
22+55	0.2212	0.02	Q	|	|	|	V|
23+ 0	0.2213	0.02	Q	|	|	|	V|
23+ 5	0.2215	0.02	Q	|	|	|	V|

23+10	0.2216	0.02	Q	|	|	|	V|
23+15	0.2218	0.02	Q	|	|	|	V|
23+20	0.2219	0.02	Q	|	|	|	V|
23+25	0.2221	0.02	Q	|	|	|	V|
23+30	0.2222	0.02	Q	|	|	|	V|
23+35	0.2224	0.02	Q	|	|	|	V|
23+40	0.2225	0.02	Q	|	|	|	V|
23+45	0.2227	0.02	Q	|	|	|	V|
23+50	0.2228	0.02	Q	|	|	|	V|
23+55	0.2230	0.02	Q	|	|	|	V|
24+ 0	0.2231	0.02	Q	|	|	|	V|
24+ 5	0.2232	0.01	Q	|	|	|	V

AREA CC1

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014, Version 9.0
Study date 02/05/24 File: ARCC124100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6279

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

PROPOSED CONDITION: 100YR HYDROLOGY
ARCC1

Drainage Area = 0.77(Ac.) = 0.001 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.77(Ac.) = 0.001 Sq. Mi.
Length along longest watercourse = 374.00(Ft.)
Length along longest watercourse measured to centroid = 187.00(Ft.)
Length along longest watercourse = 0.071 Mi.
Length along longest watercourse measured to centroid = 0.035 Mi.
Difference in elevation = 2.50(Ft.)
Slope along watercourse = 35.2941 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.019 Hr.
Lag time = 1.13 Min.
25% of lag time = 0.28 Min.
40% of lag time = 0.45 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.77	1.16	0.89

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.77	4.44	3.42

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.160(In)
Area Averaged 100-Year Rainfall = 4.440(In)

Point rain (area averaged) = 4.440(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 4.440(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.770	56.00	0.750

Total Area Entered = 0.77(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
56.0	56.0	0.511	0.750	0.166	1.000	0.166
					Sum (F) =	0.166

Area averaged mean soil loss (F) (In/Hr) = 0.166
Minimum soil loss rate ((In/Hr)) = 0.083
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.300

U n i t H y d r o g r a p h
DESERT S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	443.395	67.879	0.527
2	0.167	886.789	32.121	0.249
		Sum = 100.000	Sum=	0.776

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max		Low	Effective (In/Hr)
1	0.08	0.07	0.036	(0.294)	0.011	0.025
2	0.17	0.07	0.036	(0.293)	0.011	0.025
3	0.25	0.07	0.036	(0.292)	0.011	0.025

4	0.33	0.10	0.053	(0.291)	0.016	0.037
5	0.42	0.10	0.053	(0.290)	0.016	0.037
6	0.50	0.10	0.053	(0.289)	0.016	0.037
7	0.58	0.10	0.053	(0.287)	0.016	0.037
8	0.67	0.10	0.053	(0.286)	0.016	0.037
9	0.75	0.10	0.053	(0.285)	0.016	0.037
10	0.83	0.13	0.071	(0.284)	0.021	0.050
11	0.92	0.13	0.071	(0.283)	0.021	0.050
12	1.00	0.13	0.071	(0.282)	0.021	0.050
13	1.08	0.10	0.053	(0.281)	0.016	0.037
14	1.17	0.10	0.053	(0.280)	0.016	0.037
15	1.25	0.10	0.053	(0.279)	0.016	0.037
16	1.33	0.10	0.053	(0.277)	0.016	0.037
17	1.42	0.10	0.053	(0.276)	0.016	0.037
18	1.50	0.10	0.053	(0.275)	0.016	0.037
19	1.58	0.10	0.053	(0.274)	0.016	0.037
20	1.67	0.10	0.053	(0.273)	0.016	0.037
21	1.75	0.10	0.053	(0.272)	0.016	0.037
22	1.83	0.13	0.071	(0.271)	0.021	0.050
23	1.92	0.13	0.071	(0.270)	0.021	0.050
24	2.00	0.13	0.071	(0.269)	0.021	0.050
25	2.08	0.13	0.071	(0.268)	0.021	0.050
26	2.17	0.13	0.071	(0.267)	0.021	0.050
27	2.25	0.13	0.071	(0.265)	0.021	0.050
28	2.33	0.13	0.071	(0.264)	0.021	0.050
29	2.42	0.13	0.071	(0.263)	0.021	0.050
30	2.50	0.13	0.071	(0.262)	0.021	0.050
31	2.58	0.17	0.089	(0.261)	0.027	0.062
32	2.67	0.17	0.089	(0.260)	0.027	0.062
33	2.75	0.17	0.089	(0.259)	0.027	0.062
34	2.83	0.17	0.089	(0.258)	0.027	0.062
35	2.92	0.17	0.089	(0.257)	0.027	0.062
36	3.00	0.17	0.089	(0.256)	0.027	0.062
37	3.08	0.17	0.089	(0.255)	0.027	0.062
38	3.17	0.17	0.089	(0.254)	0.027	0.062
39	3.25	0.17	0.089	(0.253)	0.027	0.062
40	3.33	0.17	0.089	(0.252)	0.027	0.062
41	3.42	0.17	0.089	(0.251)	0.027	0.062
42	3.50	0.17	0.089	(0.249)	0.027	0.062
43	3.58	0.17	0.089	(0.248)	0.027	0.062
44	3.67	0.17	0.089	(0.247)	0.027	0.062
45	3.75	0.17	0.089	(0.246)	0.027	0.062
46	3.83	0.20	0.107	(0.245)	0.032	0.075
47	3.92	0.20	0.107	(0.244)	0.032	0.075
48	4.00	0.20	0.107	(0.243)	0.032	0.075
49	4.08	0.20	0.107	(0.242)	0.032	0.075
50	4.17	0.20	0.107	(0.241)	0.032	0.075
51	4.25	0.20	0.107	(0.240)	0.032	0.075
52	4.33	0.23	0.124	(0.239)	0.037	0.087
53	4.42	0.23	0.124	(0.238)	0.037	0.087
54	4.50	0.23	0.124	(0.237)	0.037	0.087
55	4.58	0.23	0.124	(0.236)	0.037	0.087
56	4.67	0.23	0.124	(0.235)	0.037	0.087

57	4.75	0.23	0.124	(0.234)	0.037	0.087
58	4.83	0.27	0.142	(0.233)	0.043	0.099
59	4.92	0.27	0.142	(0.232)	0.043	0.099
60	5.00	0.27	0.142	(0.231)	0.043	0.099
61	5.08	0.20	0.107	(0.230)	0.032	0.075
62	5.17	0.20	0.107	(0.229)	0.032	0.075
63	5.25	0.20	0.107	(0.228)	0.032	0.075
64	5.33	0.23	0.124	(0.227)	0.037	0.087
65	5.42	0.23	0.124	(0.226)	0.037	0.087
66	5.50	0.23	0.124	(0.225)	0.037	0.087
67	5.58	0.27	0.142	(0.224)	0.043	0.099
68	5.67	0.27	0.142	(0.223)	0.043	0.099
69	5.75	0.27	0.142	(0.222)	0.043	0.099
70	5.83	0.27	0.142	(0.221)	0.043	0.099
71	5.92	0.27	0.142	(0.220)	0.043	0.099
72	6.00	0.27	0.142	(0.219)	0.043	0.099
73	6.08	0.30	0.160	(0.218)	0.048	0.112
74	6.17	0.30	0.160	(0.217)	0.048	0.112
75	6.25	0.30	0.160	(0.216)	0.048	0.112
76	6.33	0.30	0.160	(0.215)	0.048	0.112
77	6.42	0.30	0.160	(0.214)	0.048	0.112
78	6.50	0.30	0.160	(0.213)	0.048	0.112
79	6.58	0.33	0.178	(0.212)	0.053	0.124
80	6.67	0.33	0.178	(0.211)	0.053	0.124
81	6.75	0.33	0.178	(0.210)	0.053	0.124
82	6.83	0.33	0.178	(0.210)	0.053	0.124
83	6.92	0.33	0.178	(0.209)	0.053	0.124
84	7.00	0.33	0.178	(0.208)	0.053	0.124
85	7.08	0.33	0.178	(0.207)	0.053	0.124
86	7.17	0.33	0.178	(0.206)	0.053	0.124
87	7.25	0.33	0.178	(0.205)	0.053	0.124
88	7.33	0.37	0.195	(0.204)	0.059	0.137
89	7.42	0.37	0.195	(0.203)	0.059	0.137
90	7.50	0.37	0.195	(0.202)	0.059	0.137
91	7.58	0.40	0.213	(0.201)	0.064	0.149
92	7.67	0.40	0.213	(0.200)	0.064	0.149
93	7.75	0.40	0.213	(0.199)	0.064	0.149
94	7.83	0.43	0.231	(0.198)	0.069	0.162
95	7.92	0.43	0.231	(0.197)	0.069	0.162
96	8.00	0.43	0.231	(0.196)	0.069	0.162
97	8.08	0.50	0.266	(0.196)	0.080	0.186
98	8.17	0.50	0.266	(0.195)	0.080	0.186
99	8.25	0.50	0.266	(0.194)	0.080	0.186
100	8.33	0.50	0.266	(0.193)	0.080	0.186
101	8.42	0.50	0.266	(0.192)	0.080	0.186
102	8.50	0.50	0.266	(0.191)	0.080	0.186
103	8.58	0.53	0.284	(0.190)	0.085	0.199
104	8.67	0.53	0.284	(0.189)	0.085	0.199
105	8.75	0.53	0.284	(0.188)	0.085	0.199
106	8.83	0.57	0.302	(0.187)	0.091	0.211
107	8.92	0.57	0.302	(0.187)	0.091	0.211
108	9.00	0.57	0.302	(0.186)	0.091	0.211
109	9.08	0.63	0.337	(0.185)	0.101	0.236

110	9.17	0.63	0.337	(0.184)	0.101	0.236
111	9.25	0.63	0.337	(0.183)	0.101	0.236
112	9.33	0.67	0.355	(0.182)	0.107	0.249
113	9.42	0.67	0.355	(0.181)	0.107	0.249
114	9.50	0.67	0.355	(0.180)	0.107	0.249
115	9.58	0.70	0.373	(0.180)	0.112	0.261
116	9.67	0.70	0.373	(0.179)	0.112	0.261
117	9.75	0.70	0.373	(0.178)	0.112	0.261
118	9.83	0.73	0.391	(0.177)	0.117	0.274
119	9.92	0.73	0.391	(0.176)	0.117	0.274
120	10.00	0.73	0.391	(0.175)	0.117	0.274
121	10.08	0.50	0.266	(0.174)	0.080	0.186
122	10.17	0.50	0.266	(0.174)	0.080	0.186
123	10.25	0.50	0.266	(0.173)	0.080	0.186
124	10.33	0.50	0.266	(0.172)	0.080	0.186
125	10.42	0.50	0.266	(0.171)	0.080	0.186
126	10.50	0.50	0.266	(0.170)	0.080	0.186
127	10.58	0.67	0.355	(0.169)	0.107	0.249
128	10.67	0.67	0.355	(0.169)	0.107	0.249
129	10.75	0.67	0.355	(0.168)	0.107	0.249
130	10.83	0.67	0.355	(0.167)	0.107	0.249
131	10.92	0.67	0.355	(0.166)	0.107	0.249
132	11.00	0.67	0.355	(0.165)	0.107	0.249
133	11.08	0.63	0.337	(0.165)	0.101	0.236
134	11.17	0.63	0.337	(0.164)	0.101	0.236
135	11.25	0.63	0.337	(0.163)	0.101	0.236
136	11.33	0.63	0.337	(0.162)	0.101	0.236
137	11.42	0.63	0.337	(0.161)	0.101	0.236
138	11.50	0.63	0.337	(0.160)	0.101	0.236
139	11.58	0.57	0.302	(0.160)	0.091	0.211
140	11.67	0.57	0.302	(0.159)	0.091	0.211
141	11.75	0.57	0.302	(0.158)	0.091	0.211
142	11.83	0.60	0.320	(0.157)	0.096	0.224
143	11.92	0.60	0.320	(0.157)	0.096	0.224
144	12.00	0.60	0.320	(0.156)	0.096	0.224
145	12.08	0.83	0.444	(0.155)	0.133	0.311
146	12.17	0.83	0.444	(0.154)	0.133	0.311
147	12.25	0.83	0.444	(0.153)	0.133	0.311
148	12.33	0.87	0.462	(0.153)	0.139	0.323
149	12.42	0.87	0.462	(0.152)	0.139	0.323
150	12.50	0.87	0.462	(0.151)	0.139	0.323
151	12.58	0.93	0.497	(0.150)	0.149	0.348
152	12.67	0.93	0.497	(0.150)	0.149	0.348
153	12.75	0.93	0.497	0.149	(0.149)	0.348
154	12.83	0.97	0.515	0.148	(0.155)	0.367
155	12.92	0.97	0.515	0.147	(0.155)	0.368
156	13.00	0.97	0.515	0.147	(0.155)	0.368
157	13.08	1.13	0.604	0.146	(0.181)	0.458
158	13.17	1.13	0.604	0.145	(0.181)	0.459
159	13.25	1.13	0.604	0.144	(0.181)	0.459
160	13.33	1.13	0.604	0.144	(0.181)	0.460
161	13.42	1.13	0.604	0.143	(0.181)	0.461
162	13.50	1.13	0.604	0.142	(0.181)	0.462

163	13.58	0.77	0.408	(	0.141)	0.123		0.286
164	13.67	0.77	0.408	(	0.141)	0.123		0.286
165	13.75	0.77	0.408	(	0.140)	0.123		0.286
166	13.83	0.77	0.408	(	0.139)	0.123		0.286
167	13.92	0.77	0.408	(	0.139)	0.123		0.286
168	14.00	0.77	0.408	(	0.138)	0.123		0.286
169	14.08	0.90	0.480		0.137	(0.144)		0.342
170	14.17	0.90	0.480		0.136	(0.144)		0.343
171	14.25	0.90	0.480		0.136	(0.144)		0.344
172	14.33	0.87	0.462		0.135	(0.139)		0.327
173	14.42	0.87	0.462		0.134	(0.139)		0.327
174	14.50	0.87	0.462		0.134	(0.139)		0.328
175	14.58	0.87	0.462		0.133	(0.139)		0.329
176	14.67	0.87	0.462		0.132	(0.139)		0.329
177	14.75	0.87	0.462		0.132	(0.139)		0.330
178	14.83	0.83	0.444		0.131	(0.133)		0.313
179	14.92	0.83	0.444		0.130	(0.133)		0.314
180	15.00	0.83	0.444		0.130	(0.133)		0.314
181	15.08	0.80	0.426	(	0.129)	0.128		0.298
182	15.17	0.80	0.426	(	0.128)	0.128		0.298
183	15.25	0.80	0.426		0.128	(0.128)		0.299
184	15.33	0.77	0.408	(	0.127)	0.123		0.286
185	15.42	0.77	0.408	(	0.126)	0.123		0.286
186	15.50	0.77	0.408	(	0.126)	0.123		0.286
187	15.58	0.63	0.337	(	0.125)	0.101		0.236
188	15.67	0.63	0.337	(	0.124)	0.101		0.236
189	15.75	0.63	0.337	(	0.124)	0.101		0.236
190	15.83	0.63	0.337	(	0.123)	0.101		0.236
191	15.92	0.63	0.337	(	0.123)	0.101		0.236
192	16.00	0.63	0.337	(	0.122)	0.101		0.236
193	16.08	0.13	0.071	(	0.121)	0.021		0.050
194	16.17	0.13	0.071	(	0.121)	0.021		0.050
195	16.25	0.13	0.071	(	0.120)	0.021		0.050
196	16.33	0.13	0.071	(	0.119)	0.021		0.050
197	16.42	0.13	0.071	(	0.119)	0.021		0.050
198	16.50	0.13	0.071	(	0.118)	0.021		0.050
199	16.58	0.10	0.053	(	0.118)	0.016		0.037
200	16.67	0.10	0.053	(	0.117)	0.016		0.037
201	16.75	0.10	0.053	(	0.116)	0.016		0.037
202	16.83	0.10	0.053	(	0.116)	0.016		0.037
203	16.92	0.10	0.053	(	0.115)	0.016		0.037
204	17.00	0.10	0.053	(	0.115)	0.016		0.037
205	17.08	0.17	0.089	(	0.114)	0.027		0.062
206	17.17	0.17	0.089	(	0.114)	0.027		0.062
207	17.25	0.17	0.089	(	0.113)	0.027		0.062
208	17.33	0.17	0.089	(	0.112)	0.027		0.062
209	17.42	0.17	0.089	(	0.112)	0.027		0.062
210	17.50	0.17	0.089	(	0.111)	0.027		0.062
211	17.58	0.17	0.089	(	0.111)	0.027		0.062
212	17.67	0.17	0.089	(	0.110)	0.027		0.062
213	17.75	0.17	0.089	(	0.110)	0.027		0.062
214	17.83	0.13	0.071	(	0.109)	0.021		0.050
215	17.92	0.13	0.071	(	0.109)	0.021		0.050

216	18.00	0.13	0.071	(0.108)	0.021	0.050
217	18.08	0.13	0.071	(0.107)	0.021	0.050
218	18.17	0.13	0.071	(0.107)	0.021	0.050
219	18.25	0.13	0.071	(0.106)	0.021	0.050
220	18.33	0.13	0.071	(0.106)	0.021	0.050
221	18.42	0.13	0.071	(0.105)	0.021	0.050
222	18.50	0.13	0.071	(0.105)	0.021	0.050
223	18.58	0.10	0.053	(0.104)	0.016	0.037
224	18.67	0.10	0.053	(0.104)	0.016	0.037
225	18.75	0.10	0.053	(0.103)	0.016	0.037
226	18.83	0.07	0.036	(0.103)	0.011	0.025
227	18.92	0.07	0.036	(0.102)	0.011	0.025
228	19.00	0.07	0.036	(0.102)	0.011	0.025
229	19.08	0.10	0.053	(0.101)	0.016	0.037
230	19.17	0.10	0.053	(0.101)	0.016	0.037
231	19.25	0.10	0.053	(0.100)	0.016	0.037
232	19.33	0.13	0.071	(0.100)	0.021	0.050
233	19.42	0.13	0.071	(0.100)	0.021	0.050
234	19.50	0.13	0.071	(0.099)	0.021	0.050
235	19.58	0.10	0.053	(0.099)	0.016	0.037
236	19.67	0.10	0.053	(0.098)	0.016	0.037
237	19.75	0.10	0.053	(0.098)	0.016	0.037
238	19.83	0.07	0.036	(0.097)	0.011	0.025
239	19.92	0.07	0.036	(0.097)	0.011	0.025
240	20.00	0.07	0.036	(0.096)	0.011	0.025
241	20.08	0.10	0.053	(0.096)	0.016	0.037
242	20.17	0.10	0.053	(0.096)	0.016	0.037
243	20.25	0.10	0.053	(0.095)	0.016	0.037
244	20.33	0.10	0.053	(0.095)	0.016	0.037
245	20.42	0.10	0.053	(0.094)	0.016	0.037
246	20.50	0.10	0.053	(0.094)	0.016	0.037
247	20.58	0.10	0.053	(0.094)	0.016	0.037
248	20.67	0.10	0.053	(0.093)	0.016	0.037
249	20.75	0.10	0.053	(0.093)	0.016	0.037
250	20.83	0.07	0.036	(0.092)	0.011	0.025
251	20.92	0.07	0.036	(0.092)	0.011	0.025
252	21.00	0.07	0.036	(0.092)	0.011	0.025
253	21.08	0.10	0.053	(0.091)	0.016	0.037
254	21.17	0.10	0.053	(0.091)	0.016	0.037
255	21.25	0.10	0.053	(0.091)	0.016	0.037
256	21.33	0.07	0.036	(0.090)	0.011	0.025
257	21.42	0.07	0.036	(0.090)	0.011	0.025
258	21.50	0.07	0.036	(0.090)	0.011	0.025
259	21.58	0.10	0.053	(0.089)	0.016	0.037
260	21.67	0.10	0.053	(0.089)	0.016	0.037
261	21.75	0.10	0.053	(0.089)	0.016	0.037
262	21.83	0.07	0.036	(0.088)	0.011	0.025
263	21.92	0.07	0.036	(0.088)	0.011	0.025
264	22.00	0.07	0.036	(0.088)	0.011	0.025
265	22.08	0.10	0.053	(0.087)	0.016	0.037
266	22.17	0.10	0.053	(0.087)	0.016	0.037
267	22.25	0.10	0.053	(0.087)	0.016	0.037
268	22.33	0.07	0.036	(0.087)	0.011	0.025

269	22.42	0.07	0.036	(0.086)	0.011	0.025
270	22.50	0.07	0.036	(0.086)	0.011	0.025
271	22.58	0.07	0.036	(0.086)	0.011	0.025
272	22.67	0.07	0.036	(0.086)	0.011	0.025
273	22.75	0.07	0.036	(0.085)	0.011	0.025
274	22.83	0.07	0.036	(0.085)	0.011	0.025
275	22.92	0.07	0.036	(0.085)	0.011	0.025
276	23.00	0.07	0.036	(0.085)	0.011	0.025
277	23.08	0.07	0.036	(0.084)	0.011	0.025
278	23.17	0.07	0.036	(0.084)	0.011	0.025
279	23.25	0.07	0.036	(0.084)	0.011	0.025
280	23.33	0.07	0.036	(0.084)	0.011	0.025
281	23.42	0.07	0.036	(0.084)	0.011	0.025
282	23.50	0.07	0.036	(0.084)	0.011	0.025
283	23.58	0.07	0.036	(0.083)	0.011	0.025
284	23.67	0.07	0.036	(0.083)	0.011	0.025
285	23.75	0.07	0.036	(0.083)	0.011	0.025
286	23.83	0.07	0.036	(0.083)	0.011	0.025
287	23.92	0.07	0.036	(0.083)	0.011	0.025
288	24.00	0.07	0.036	(0.083)	0.011	0.025

(Loss Rate Not Used)

Sum = 100.0 Sum = 37.6

Flood volume = Effective rainfall 3.13(In)
times area 0.8(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 1.31(In)
Total soil loss = 0.084(Ac.Ft)
Total rainfall = 4.44(In)
Flood volume = 8758.5 Cubic Feet
Total soil loss = 3651.7 Cubic Feet

Peak flow rate of this hydrograph = 0.358(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.01	Q	|	|	|	|
0+10	0.0002	0.02	Q	|	|	|	|
0+15	0.0004	0.02	Q	|	|	|	|
0+20	0.0005	0.03	Q	|	|	|	|
0+25	0.0007	0.03	Q	|	|	|	|
0+30	0.0009	0.03	Q	|	|	|	|
0+35	0.0011	0.03	Q	|	|	|	|
0+40	0.0013	0.03	Q	|	|	|	|
0+45	0.0015	0.03	Q	|	|	|	|
0+50	0.0018	0.04	Q	|	|	|	|
0+55	0.0020	0.04	Q	|	|	|	|
1+ 0	0.0023	0.04	Q	|	|	|	|

1+ 5	0.0025	0.03	Q	|	|	|	|
1+10	0.0027	0.03	Q	|	|	|	|
1+15	0.0029	0.03	Q	|	|	|	|
1+20	0.0031	0.03	Q	|	|	|	|
1+25	0.0033	0.03	Q	|	|	|	|
1+30	0.0035	0.03	Q	|	|	|	|
1+35	0.0037	0.03	Q	|	|	|	|
1+40	0.0039	0.03	Q	|	|	|	|
1+45	0.0041	0.03	Q	|	|	|	|
1+50	0.0044	0.04	Q	|	|	|	|
1+55	0.0046	0.04	Q	|	|	|	|
2+ 0	0.0049	0.04	Q	|	|	|	|
2+ 5	0.0052	0.04	QV	|	|	|	|
2+10	0.0054	0.04	QV	|	|	|	|
2+15	0.0057	0.04	QV	|	|	|	|
2+20	0.0060	0.04	QV	|	|	|	|
2+25	0.0062	0.04	QV	|	|	|	|
2+30	0.0065	0.04	QV	|	|	|	|
2+35	0.0068	0.05	QV	|	|	|	|
2+40	0.0071	0.05	QV	|	|	|	|
2+45	0.0075	0.05	QV	|	|	|	|
2+50	0.0078	0.05	QV	|	|	|	|
2+55	0.0081	0.05	QV	|	|	|	|
3+ 0	0.0085	0.05	QV	|	|	|	|
3+ 5	0.0088	0.05	QV	|	|	|	|
3+10	0.0091	0.05	QV	|	|	|	|
3+15	0.0095	0.05	QV	|	|	|	|
3+20	0.0098	0.05	QV	|	|	|	|
3+25	0.0101	0.05	Q V	|	|	|	|
3+30	0.0105	0.05	Q V	|	|	|	|
3+35	0.0108	0.05	Q V	|	|	|	|
3+40	0.0111	0.05	Q V	|	|	|	|
3+45	0.0115	0.05	Q V	|	|	|	|
3+50	0.0118	0.05	Q V	|	|	|	|
3+55	0.0122	0.06	Q V	|	|	|	|
4+ 0	0.0126	0.06	Q V	|	|	|	|
4+ 5	0.0130	0.06	Q V	|	|	|	|
4+10	0.0134	0.06	Q V	|	|	|	|
4+15	0.0138	0.06	Q V	|	|	|	|
4+20	0.0143	0.06	Q V	|	|	|	|
4+25	0.0147	0.07	Q V	|	|	|	|
4+30	0.0152	0.07	Q V	|	|	|	|
4+35	0.0157	0.07	Q V	|	|	|	|
4+40	0.0161	0.07	Q V	|	|	|	|
4+45	0.0166	0.07	Q V	|	|	|	|
4+50	0.0171	0.07	Q V	|	|	|	|
4+55	0.0176	0.08	Q V	|	|	|	|
5+ 0	0.0182	0.08	Q V	|	|	|	|
5+ 5	0.0186	0.06	Q V	|	|	|	|
5+10	0.0190	0.06	Q V	|	|	|	|
5+15	0.0194	0.06	Q V	|	|	|	|
5+20	0.0199	0.06	Q V	|	|	|	|
5+25	0.0203	0.07	Q V	|	|	|	|

5+30	0.0208	0.07	Q	V	|	|	|	|
5+35	0.0213	0.07	Q	V	|	|	|	|
5+40	0.0218	0.08	Q	V	|	|	|	|
5+45	0.0224	0.08	Q	V	|	|	|	|
5+50	0.0229	0.08	Q	V	|	|	|	|
5+55	0.0234	0.08	Q	V	|	|	|	|
6+ 0	0.0240	0.08	Q	V	|	|	|	|
6+ 5	0.0245	0.08	Q	V	|	|	|	|
6+10	0.0251	0.09	Q	V	|	|	|	|
6+15	0.0257	0.09	Q	V	|	|	|	|
6+20	0.0263	0.09	Q	V	|	|	|	|
6+25	0.0269	0.09	Q	V	|	|	|	|
6+30	0.0275	0.09	Q	V	|	|	|	|
6+35	0.0282	0.09	Q	V	|	|	|	|
6+40	0.0288	0.10	Q	V	|	|	|	|
6+45	0.0295	0.10	Q	V	|	|	|	|
6+50	0.0302	0.10	Q	V	|	|	|	|
6+55	0.0308	0.10	Q	V	|	|	|	|
7+ 0	0.0315	0.10	Q	V	|	|	|	|
7+ 5	0.0322	0.10	Q	V	|	|	|	|
7+10	0.0328	0.10	Q	V	|	|	|	|
7+15	0.0335	0.10	Q	V	|	|	|	|
7+20	0.0342	0.10	Q	V	|	|	|	|
7+25	0.0349	0.11	Q	V	|	|	|	|
7+30	0.0357	0.11	Q	V	|	|	|	|
7+35	0.0364	0.11	Q	V	|	|	|	|
7+40	0.0372	0.12	Q	V	|	|	|	|
7+45	0.0380	0.12	Q	V	|	|	|	|
7+50	0.0389	0.12	Q	V	|	|	|	|
7+55	0.0397	0.13	Q	V	|	|	|	|
8+ 0	0.0406	0.13	Q	V	|	|	|	|
8+ 5	0.0416	0.14	Q	V	|	|	|	|
8+10	0.0426	0.14	Q	V	|	|	|	|
8+15	0.0436	0.14	Q	V	|	|	|	|
8+20	0.0446	0.14	Q	V	|	|	|	|
8+25	0.0455	0.14	Q	V	|	|	|	|
8+30	0.0465	0.14	Q	V	|	|	|	|
8+35	0.0476	0.15	Q	V	|	|	|	|
8+40	0.0487	0.15	Q	V	|	|	|	|
8+45	0.0497	0.15	Q	V	|	|	|	|
8+50	0.0508	0.16	Q	V	|	|	|	|
8+55	0.0520	0.16	Q	V	|	|	|	|
9+ 0	0.0531	0.16	Q	V	|	|	|	|
9+ 5	0.0543	0.18	Q	V	|	|	|	|
9+10	0.0556	0.18	Q	|	V	|	|	|
9+15	0.0568	0.18	Q	|	V	|	|	|
9+20	0.0581	0.19	Q	|	V	|	|	|
9+25	0.0595	0.19	Q	|	V	|	|	|
9+30	0.0608	0.19	Q	|	V	|	|	|
9+35	0.0622	0.20	Q	|	V	|	|	|
9+40	0.0636	0.20	Q	|	V	|	|	|
9+45	0.0650	0.20	Q	|	V	|	|	|
9+50	0.0664	0.21	Q	|	V	|	|	|

```
 9+55       0.0679      0.21  Q         |  V      |         |         |
10+ 0       0.0693      0.21  Q         |  V      |         |         |
10+ 5       0.0705      0.17  Q         |   V     |         |         |
10+10       0.0715      0.14  Q         |   V     |         |         |
10+15       0.0725      0.14  Q         |   V     |         |         |
10+20       0.0735      0.14  Q         |   V     |         |         |
10+25       0.0745      0.14  Q         |   V     |         |         |
10+30       0.0755      0.14  Q         |    V    |         |         |
10+35       0.0767      0.18  Q         |    V    |         |         |
10+40       0.0780      0.19  Q         |    V    |         |         |
10+45       0.0793      0.19  Q         |    V    |         |         |
10+50       0.0807      0.19  Q         |     V   |         |         |
10+55       0.0820      0.19  Q         |     V   |         |         |
11+ 0       0.0833      0.19  Q         |     V   |         |         |
11+ 5       0.0846      0.19  Q         |     V   |         |         |
11+10       0.0859      0.18  Q         |      V  |         |         |
11+15       0.0871      0.18  Q         |      V  |         |         |
11+20       0.0884      0.18  Q         |      V  |         |         |
11+25       0.0897      0.18  Q         |      V  |         |         |
11+30       0.0909      0.18  Q         |       V |         |         |
11+35       0.0921      0.17  Q         |       V |         |         |
11+40       0.0932      0.16  Q         |       V |         |         |
11+45       0.0944      0.16  Q         |       V |         |         |
11+50       0.0955      0.17  Q         |        V|         |         |
11+55       0.0967      0.17  Q         |        V|         |         |
12+ 0       0.0979      0.17  Q         |        V|         |         |
12+ 5       0.0994      0.22  Q         |        V|         |         |
12+10       0.1011      0.24  Q         |         V         |         |
12+15       0.1028      0.24  Q         |         V         |         |
12+20       0.1045      0.25  Q         |         V         |         |
12+25       0.1062      0.25  |Q        |         |V        |         |
12+30       0.1079      0.25  |Q        |         |V        |         |
12+35       0.1098      0.26  |Q        |         |V        |         |
12+40       0.1116      0.27  |Q        |         | V       |         |
12+45       0.1135      0.27  |Q        |         | V       |         |
12+50       0.1154      0.28  |Q        |         | V       |         |
12+55       0.1174      0.29  |Q        |         |  V      |         |
13+ 0       0.1193      0.29  |Q        |         |  V      |         |
13+ 5       0.1216      0.33  |Q        |         |   V     |         |
13+10       0.1241      0.36  |Q        |         |   V     |         |
13+15       0.1265      0.36  |Q        |         |    V    |         |
13+20       0.1290      0.36  |Q        |         |    V    |         |
13+25       0.1315      0.36  |Q        |         |     V   |         |
13+30       0.1339      0.36  |Q        |         |     V   |         |
13+35       0.1358      0.27  |Q        |         |      V  |         |
13+40       0.1373      0.22  Q         |         |      V  |         |
13+45       0.1388      0.22  Q         |         |      V  |         |
13+50       0.1404      0.22  Q         |         |      V  |         |
13+55       0.1419      0.22  Q         |         |       V |         |
14+ 0       0.1434      0.22  Q         |         |       V |         |
14+ 5       0.1451      0.25  |Q        |         |       V |         |
14+10       0.1470      0.27  |Q        |         |        V|         |
14+15       0.1488      0.27  |Q        |         |        V|         |
```

14+20	0.1506	0.26	|Q	|	|	V|	|
14+25	0.1523	0.25	|Q	|	|	V	|
14+30	0.1541	0.25	|Q	|	|	V	|
14+35	0.1558	0.26	|Q	|	|	|V	|
14+40	0.1576	0.26	|Q	|	|	|V	|
14+45	0.1594	0.26	|Q	|	|	|V	|
14+50	0.1611	0.25	Q	|	|	| V	|
14+55	0.1628	0.24	Q	|	|	| V	|
15+ 0	0.1644	0.24	Q	|	|	| V	|
15+ 5	0.1661	0.24	Q	|	|	| V	|
15+10	0.1676	0.23	Q	|	|	| V	|
15+15	0.1692	0.23	Q	|	|	| V	|
15+20	0.1708	0.23	Q	|	|	| V	|
15+25	0.1723	0.22	Q	|	|	| V	|
15+30	0.1739	0.22	Q	|	|	| V	|
15+35	0.1752	0.20	Q	|	|	| V	|
15+40	0.1765	0.18	Q	|	|	| V	|
15+45	0.1777	0.18	Q	|	|	| V	|
15+50	0.1790	0.18	Q	|	|	| V	|
15+55	0.1803	0.18	Q	|	|	| V	|
16+ 0	0.1815	0.18	Q	|	|	| V	|
16+ 5	0.1821	0.09	Q	|	|	| V	|
16+10	0.1824	0.04	Q	|	|	| V	|
16+15	0.1826	0.04	Q	|	|	| V	|
16+20	0.1829	0.04	Q	|	|	| V	|
16+25	0.1832	0.04	Q	|	|	| V	|
16+30	0.1834	0.04	Q	|	|	| V	|
16+35	0.1837	0.03	Q	|	|	| V	|
16+40	0.1839	0.03	Q	|	|	| V	|
16+45	0.1841	0.03	Q	|	|	| V	|
16+50	0.1843	0.03	Q	|	|	| V	|
16+55	0.1845	0.03	Q	|	|	| V	|
17+ 0	0.1847	0.03	Q	|	|	| V	|
17+ 5	0.1849	0.04	Q	|	|	| V	|
17+10	0.1853	0.05	Q	|	|	| V	|
17+15	0.1856	0.05	Q	|	|	| V	|
17+20	0.1859	0.05	Q	|	|	| V	|
17+25	0.1863	0.05	Q	|	|	| V	|
17+30	0.1866	0.05	Q	|	|	| V	|
17+35	0.1869	0.05	Q	|	|	| V	|
17+40	0.1873	0.05	Q	|	|	| V	|
17+45	0.1876	0.05	Q	|	|	| V	|
17+50	0.1879	0.04	Q	|	|	| V	|
17+55	0.1882	0.04	Q	|	|	| V	|
18+ 0	0.1884	0.04	Q	|	|	| V	|
18+ 5	0.1887	0.04	Q	|	|	| V	|
18+10	0.1890	0.04	Q	|	|	| V	|
18+15	0.1892	0.04	Q	|	|	| V	|
18+20	0.1895	0.04	Q	|	|	| V	|
18+25	0.1897	0.04	Q	|	|	| V	|
18+30	0.1900	0.04	Q	|	|	| V	|
18+35	0.1902	0.03	Q	|	|	| V	|
18+40	0.1904	0.03	Q	|	|	| V	|

18+45	0.1906	0.03	Q	|	|	|	V |
18+50	0.1908	0.02	Q	|	|	|	V |
18+55	0.1909	0.02	Q	|	|	|	V |
19+ 0	0.1911	0.02	Q	|	|	|	V |
19+ 5	0.1912	0.03	Q	|	|	|	V |
19+10	0.1914	0.03	Q	|	|	|	V |
19+15	0.1916	0.03	Q	|	|	|	V |
19+20	0.1919	0.04	Q	|	|	|	V |
19+25	0.1921	0.04	Q	|	|	|	V |
19+30	0.1924	0.04	Q	|	|	|	V |
19+35	0.1926	0.03	Q	|	|	|	V |
19+40	0.1928	0.03	Q	|	|	|	V |
19+45	0.1930	0.03	Q	|	|	|	V |
19+50	0.1932	0.02	Q	|	|	|	V |
19+55	0.1933	0.02	Q	|	|	|	V |
20+ 0	0.1934	0.02	Q	|	|	|	V |
20+ 5	0.1936	0.03	Q	|	|	|	V |
20+10	0.1938	0.03	Q	|	|	|	V |
20+15	0.1940	0.03	Q	|	|	|	V |
20+20	0.1942	0.03	Q	|	|	|	V |
20+25	0.1944	0.03	Q	|	|	|	V |
20+30	0.1946	0.03	Q	|	|	|	V |
20+35	0.1948	0.03	Q	|	|	|	V |
20+40	0.1950	0.03	Q	|	|	|	V |
20+45	0.1952	0.03	Q	|	|	|	V |
20+50	0.1954	0.02	Q	|	|	|	V |
20+55	0.1955	0.02	Q	|	|	|	V |
21+ 0	0.1956	0.02	Q	|	|	|	V |
21+ 5	0.1958	0.03	Q	|	|	|	V |
21+10	0.1960	0.03	Q	|	|	|	V |
21+15	0.1962	0.03	Q	|	|	|	V|
21+20	0.1964	0.02	Q	|	|	|	V|
21+25	0.1965	0.02	Q	|	|	|	V|
21+30	0.1966	0.02	Q	|	|	|	V|
21+35	0.1968	0.03	Q	|	|	|	V|
21+40	0.1970	0.03	Q	|	|	|	V|
21+45	0.1972	0.03	Q	|	|	|	V|
21+50	0.1974	0.02	Q	|	|	|	V|
21+55	0.1975	0.02	Q	|	|	|	V|
22+ 0	0.1976	0.02	Q	|	|	|	V|
22+ 5	0.1978	0.03	Q	|	|	|	V|
22+10	0.1980	0.03	Q	|	|	|	V|
22+15	0.1982	0.03	Q	|	|	|	V|
22+20	0.1984	0.02	Q	|	|	|	V|
22+25	0.1985	0.02	Q	|	|	|	V|
22+30	0.1986	0.02	Q	|	|	|	V|
22+35	0.1988	0.02	Q	|	|	|	V|
22+40	0.1989	0.02	Q	|	|	|	V|
22+45	0.1990	0.02	Q	|	|	|	V|
22+50	0.1992	0.02	Q	|	|	|	V|
22+55	0.1993	0.02	Q	|	|	|	V|
23+ 0	0.1994	0.02	Q	|	|	|	V|
23+ 5	0.1996	0.02	Q	|	|	|	V|

23+10	0.1997	0.02	Q	|	|	|	V|
23+15	0.1998	0.02	Q	|	|	|	V|
23+20	0.2000	0.02	Q	|	|	|	V|
23+25	0.2001	0.02	Q	|	|	|	V|
23+30	0.2002	0.02	Q	|	|	|	V|
23+35	0.2004	0.02	Q	|	|	|	V|
23+40	0.2005	0.02	Q	|	|	|	V|
23+45	0.2006	0.02	Q	|	|	|	V|
23+50	0.2008	0.02	Q	|	|	|	V|
23+55	0.2009	0.02	Q	|	|	|	V|
24+ 0	0.2010	0.02	Q	|	|	|	V|
24+ 5	0.2011	0.01	Q	|	|	|	V

AREA D1

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014, Version 9.0
Study date 02/05/24 File: ARD124100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6279

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

PROPOSED CONDITION: 100YR HYDROLOGY
ARD1

Drainage Area = 1.68(Ac.) = 0.003 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.68(Ac.) = 0.003 Sq. Mi.
Length along longest watercourse = 941.00(Ft.)
Length along longest watercourse measured to centroid = 470.50(Ft.)
Length along longest watercourse = 0.178 Mi.
Length along longest watercourse measured to centroid = 0.089 Mi.
Difference in elevation = 4.50(Ft.)
Slope along watercourse = 25.2497 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.040 Hr.
Lag time = 2.42 Min.
25% of lag time = 0.61 Min.
40% of lag time = 0.97 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.68	1.16	1.95

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.68	4.44	7.46

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.160(In)
Area Averaged 100-Year Rainfall = 4.440(In)

Point rain (area averaged) = 4.440(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 4.440(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.680	43.00	0.880

Total Area Entered = 1.68(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
43.0	43.0	0.641	0.880	0.133	1.000	0.133
					Sum (F) =	0.133

Area averaged mean soil loss (F) (In/Hr) = 0.133
Minimum soil loss rate ((In/Hr)) = 0.067
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.190

U n i t H y d r o g r a p h
DESERT S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	206.353	43.327	0.734
2	0.167	412.705	45.093	0.763
3	0.250	619.058	8.501	0.144
4	0.333	825.411	3.079	0.052
		Sum = 100.000	Sum=	1.693

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.036	(0.236)	0.007	0.029

2	0.17	0.07	0.036	(0.235)	0.007	0.029
3	0.25	0.07	0.036	(0.234)	0.007	0.029
4	0.33	0.10	0.053	(0.233)	0.010	0.043
5	0.42	0.10	0.053	(0.233)	0.010	0.043
6	0.50	0.10	0.053	(0.232)	0.010	0.043
7	0.58	0.10	0.053	(0.231)	0.010	0.043
8	0.67	0.10	0.053	(0.230)	0.010	0.043
9	0.75	0.10	0.053	(0.229)	0.010	0.043
10	0.83	0.13	0.071	(0.228)	0.013	0.058
11	0.92	0.13	0.071	(0.227)	0.013	0.058
12	1.00	0.13	0.071	(0.226)	0.013	0.058
13	1.08	0.10	0.053	(0.225)	0.010	0.043
14	1.17	0.10	0.053	(0.224)	0.010	0.043
15	1.25	0.10	0.053	(0.224)	0.010	0.043
16	1.33	0.10	0.053	(0.223)	0.010	0.043
17	1.42	0.10	0.053	(0.222)	0.010	0.043
18	1.50	0.10	0.053	(0.221)	0.010	0.043
19	1.58	0.10	0.053	(0.220)	0.010	0.043
20	1.67	0.10	0.053	(0.219)	0.010	0.043
21	1.75	0.10	0.053	(0.218)	0.010	0.043
22	1.83	0.13	0.071	(0.217)	0.013	0.058
23	1.92	0.13	0.071	(0.217)	0.013	0.058
24	2.00	0.13	0.071	(0.216)	0.013	0.058
25	2.08	0.13	0.071	(0.215)	0.013	0.058
26	2.17	0.13	0.071	(0.214)	0.013	0.058
27	2.25	0.13	0.071	(0.213)	0.013	0.058
28	2.33	0.13	0.071	(0.212)	0.013	0.058
29	2.42	0.13	0.071	(0.211)	0.013	0.058
30	2.50	0.13	0.071	(0.210)	0.013	0.058
31	2.58	0.17	0.089	(0.210)	0.017	0.072
32	2.67	0.17	0.089	(0.209)	0.017	0.072
33	2.75	0.17	0.089	(0.208)	0.017	0.072
34	2.83	0.17	0.089	(0.207)	0.017	0.072
35	2.92	0.17	0.089	(0.206)	0.017	0.072
36	3.00	0.17	0.089	(0.205)	0.017	0.072
37	3.08	0.17	0.089	(0.204)	0.017	0.072
38	3.17	0.17	0.089	(0.204)	0.017	0.072
39	3.25	0.17	0.089	(0.203)	0.017	0.072
40	3.33	0.17	0.089	(0.202)	0.017	0.072
41	3.42	0.17	0.089	(0.201)	0.017	0.072
42	3.50	0.17	0.089	(0.200)	0.017	0.072
43	3.58	0.17	0.089	(0.199)	0.017	0.072
44	3.67	0.17	0.089	(0.199)	0.017	0.072
45	3.75	0.17	0.089	(0.198)	0.017	0.072
46	3.83	0.20	0.107	(0.197)	0.020	0.086
47	3.92	0.20	0.107	(0.196)	0.020	0.086
48	4.00	0.20	0.107	(0.195)	0.020	0.086
49	4.08	0.20	0.107	(0.194)	0.020	0.086
50	4.17	0.20	0.107	(0.194)	0.020	0.086
51	4.25	0.20	0.107	(0.193)	0.020	0.086
52	4.33	0.23	0.124	(0.192)	0.024	0.101
53	4.42	0.23	0.124	(0.191)	0.024	0.101
54	4.50	0.23	0.124	(0.190)	0.024	0.101

55	4.58	0.23	0.124	(0.189)	0.024	0.101
56	4.67	0.23	0.124	(0.189)	0.024	0.101
57	4.75	0.23	0.124	(0.188)	0.024	0.101
58	4.83	0.27	0.142	(0.187)	0.027	0.115
59	4.92	0.27	0.142	(0.186)	0.027	0.115
60	5.00	0.27	0.142	(0.185)	0.027	0.115
61	5.08	0.20	0.107	(0.185)	0.020	0.086
62	5.17	0.20	0.107	(0.184)	0.020	0.086
63	5.25	0.20	0.107	(0.183)	0.020	0.086
64	5.33	0.23	0.124	(0.182)	0.024	0.101
65	5.42	0.23	0.124	(0.181)	0.024	0.101
66	5.50	0.23	0.124	(0.181)	0.024	0.101
67	5.58	0.27	0.142	(0.180)	0.027	0.115
68	5.67	0.27	0.142	(0.179)	0.027	0.115
69	5.75	0.27	0.142	(0.178)	0.027	0.115
70	5.83	0.27	0.142	(0.177)	0.027	0.115
71	5.92	0.27	0.142	(0.177)	0.027	0.115
72	6.00	0.27	0.142	(0.176)	0.027	0.115
73	6.08	0.30	0.160	(0.175)	0.030	0.129
74	6.17	0.30	0.160	(0.174)	0.030	0.129
75	6.25	0.30	0.160	(0.174)	0.030	0.129
76	6.33	0.30	0.160	(0.173)	0.030	0.129
77	6.42	0.30	0.160	(0.172)	0.030	0.129
78	6.50	0.30	0.160	(0.171)	0.030	0.129
79	6.58	0.33	0.178	(0.170)	0.034	0.144
80	6.67	0.33	0.178	(0.170)	0.034	0.144
81	6.75	0.33	0.178	(0.169)	0.034	0.144
82	6.83	0.33	0.178	(0.168)	0.034	0.144
83	6.92	0.33	0.178	(0.167)	0.034	0.144
84	7.00	0.33	0.178	(0.167)	0.034	0.144
85	7.08	0.33	0.178	(0.166)	0.034	0.144
86	7.17	0.33	0.178	(0.165)	0.034	0.144
87	7.25	0.33	0.178	(0.164)	0.034	0.144
88	7.33	0.37	0.195	(0.164)	0.037	0.158
89	7.42	0.37	0.195	(0.163)	0.037	0.158
90	7.50	0.37	0.195	(0.162)	0.037	0.158
91	7.58	0.40	0.213	(0.161)	0.040	0.173
92	7.67	0.40	0.213	(0.161)	0.040	0.173
93	7.75	0.40	0.213	(0.160)	0.040	0.173
94	7.83	0.43	0.231	(0.159)	0.044	0.187
95	7.92	0.43	0.231	(0.158)	0.044	0.187
96	8.00	0.43	0.231	(0.158)	0.044	0.187
97	8.08	0.50	0.266	(0.157)	0.051	0.216
98	8.17	0.50	0.266	(0.156)	0.051	0.216
99	8.25	0.50	0.266	(0.155)	0.051	0.216
100	8.33	0.50	0.266	(0.155)	0.051	0.216
101	8.42	0.50	0.266	(0.154)	0.051	0.216
102	8.50	0.50	0.266	(0.153)	0.051	0.216
103	8.58	0.53	0.284	(0.153)	0.054	0.230
104	8.67	0.53	0.284	(0.152)	0.054	0.230
105	8.75	0.53	0.284	(0.151)	0.054	0.230
106	8.83	0.57	0.302	(0.150)	0.057	0.245
107	8.92	0.57	0.302	(0.150)	0.057	0.245

108	9.00	0.57	0.302	(0.149)	0.057	0.245
109	9.08	0.63	0.337	(0.148)	0.064	0.273
110	9.17	0.63	0.337	(0.148)	0.064	0.273
111	9.25	0.63	0.337	(0.147)	0.064	0.273
112	9.33	0.67	0.355	(0.146)	0.067	0.288
113	9.42	0.67	0.355	(0.146)	0.067	0.288
114	9.50	0.67	0.355	(0.145)	0.067	0.288
115	9.58	0.70	0.373	(0.144)	0.071	0.302
116	9.67	0.70	0.373	(0.143)	0.071	0.302
117	9.75	0.70	0.373	(0.143)	0.071	0.302
118	9.83	0.73	0.391	(0.142)	0.074	0.316
119	9.92	0.73	0.391	(0.141)	0.074	0.316
120	10.00	0.73	0.391	(0.141)	0.074	0.316
121	10.08	0.50	0.266	(0.140)	0.051	0.216
122	10.17	0.50	0.266	(0.139)	0.051	0.216
123	10.25	0.50	0.266	(0.139)	0.051	0.216
124	10.33	0.50	0.266	(0.138)	0.051	0.216
125	10.42	0.50	0.266	(0.137)	0.051	0.216
126	10.50	0.50	0.266	(0.137)	0.051	0.216
127	10.58	0.67	0.355	(0.136)	0.067	0.288
128	10.67	0.67	0.355	(0.135)	0.067	0.288
129	10.75	0.67	0.355	(0.135)	0.067	0.288
130	10.83	0.67	0.355	(0.134)	0.067	0.288
131	10.92	0.67	0.355	(0.133)	0.067	0.288
132	11.00	0.67	0.355	(0.133)	0.067	0.288
133	11.08	0.63	0.337	(0.132)	0.064	0.273
134	11.17	0.63	0.337	(0.131)	0.064	0.273
135	11.25	0.63	0.337	(0.131)	0.064	0.273
136	11.33	0.63	0.337	(0.130)	0.064	0.273
137	11.42	0.63	0.337	(0.129)	0.064	0.273
138	11.50	0.63	0.337	(0.129)	0.064	0.273
139	11.58	0.57	0.302	(0.128)	0.057	0.245
140	11.67	0.57	0.302	(0.128)	0.057	0.245
141	11.75	0.57	0.302	(0.127)	0.057	0.245
142	11.83	0.60	0.320	(0.126)	0.061	0.259
143	11.92	0.60	0.320	(0.126)	0.061	0.259
144	12.00	0.60	0.320	(0.125)	0.061	0.259
145	12.08	0.83	0.444	(0.124)	0.084	0.360
146	12.17	0.83	0.444	(0.124)	0.084	0.360
147	12.25	0.83	0.444	(0.123)	0.084	0.360
148	12.33	0.87	0.462	(0.123)	0.088	0.374
149	12.42	0.87	0.462	(0.122)	0.088	0.374
150	12.50	0.87	0.462	(0.121)	0.088	0.374
151	12.58	0.93	0.497	(0.121)	0.094	0.403
152	12.67	0.93	0.497	(0.120)	0.094	0.403
153	12.75	0.93	0.497	(0.119)	0.094	0.403
154	12.83	0.97	0.515	(0.119)	0.098	0.417
155	12.92	0.97	0.515	(0.118)	0.098	0.417
156	13.00	0.97	0.515	(0.118)	0.098	0.417
157	13.08	1.13	0.604	(0.117)	0.115	0.489
158	13.17	1.13	0.604	(0.116)	0.115	0.489
159	13.25	1.13	0.604	(0.116)	0.115	0.489
160	13.33	1.13	0.604	(0.115)	0.115	0.489

161	13.42	1.13	0.604		0.115	(	0.115)	0.489
162	13.50	1.13	0.604		0.114	(	0.115)	0.490
163	13.58	0.77	0.408	(	0.114)		0.078	0.331
164	13.67	0.77	0.408	(	0.113)		0.078	0.331
165	13.75	0.77	0.408	(	0.112)		0.078	0.331
166	13.83	0.77	0.408	(	0.112)		0.078	0.331
167	13.92	0.77	0.408	(	0.111)		0.078	0.331
168	14.00	0.77	0.408	(	0.111)		0.078	0.331
169	14.08	0.90	0.480	(	0.110)		0.091	0.388
170	14.17	0.90	0.480	(	0.110)		0.091	0.388
171	14.25	0.90	0.480	(	0.109)		0.091	0.388
172	14.33	0.87	0.462	(	0.108)		0.088	0.374
173	14.42	0.87	0.462	(	0.108)		0.088	0.374
174	14.50	0.87	0.462	(	0.107)		0.088	0.374
175	14.58	0.87	0.462	(	0.107)		0.088	0.374
176	14.67	0.87	0.462	(	0.106)		0.088	0.374
177	14.75	0.87	0.462	(	0.106)		0.088	0.374
178	14.83	0.83	0.444	(	0.105)		0.084	0.360
179	14.92	0.83	0.444	(	0.105)		0.084	0.360
180	15.00	0.83	0.444	(	0.104)		0.084	0.360
181	15.08	0.80	0.426	(	0.104)		0.081	0.345
182	15.17	0.80	0.426	(	0.103)		0.081	0.345
183	15.25	0.80	0.426	(	0.102)		0.081	0.345
184	15.33	0.77	0.408	(	0.102)		0.078	0.331
185	15.42	0.77	0.408	(	0.101)		0.078	0.331
186	15.50	0.77	0.408	(	0.101)		0.078	0.331
187	15.58	0.63	0.337	(	0.100)		0.064	0.273
188	15.67	0.63	0.337	(	0.100)		0.064	0.273
189	15.75	0.63	0.337	(	0.099)		0.064	0.273
190	15.83	0.63	0.337	(	0.099)		0.064	0.273
191	15.92	0.63	0.337	(	0.098)		0.064	0.273
192	16.00	0.63	0.337	(	0.098)		0.064	0.273
193	16.08	0.13	0.071	(	0.097)		0.013	0.058
194	16.17	0.13	0.071	(	0.097)		0.013	0.058
195	16.25	0.13	0.071	(	0.096)		0.013	0.058
196	16.33	0.13	0.071	(	0.096)		0.013	0.058
197	16.42	0.13	0.071	(	0.095)		0.013	0.058
198	16.50	0.13	0.071	(	0.095)		0.013	0.058
199	16.58	0.10	0.053	(	0.094)		0.010	0.043
200	16.67	0.10	0.053	(	0.094)		0.010	0.043
201	16.75	0.10	0.053	(	0.093)		0.010	0.043
202	16.83	0.10	0.053	(	0.093)		0.010	0.043
203	16.92	0.10	0.053	(	0.093)		0.010	0.043
204	17.00	0.10	0.053	(	0.092)		0.010	0.043
205	17.08	0.17	0.089	(	0.092)		0.017	0.072
206	17.17	0.17	0.089	(	0.091)		0.017	0.072
207	17.25	0.17	0.089	(	0.091)		0.017	0.072
208	17.33	0.17	0.089	(	0.090)		0.017	0.072
209	17.42	0.17	0.089	(	0.090)		0.017	0.072
210	17.50	0.17	0.089	(	0.089)		0.017	0.072
211	17.58	0.17	0.089	(	0.089)		0.017	0.072
212	17.67	0.17	0.089	(	0.088)		0.017	0.072
213	17.75	0.17	0.089	(	0.088)		0.017	0.072

214	17.83	0.13	0.071	(0.088)	0.013	0.058
215	17.92	0.13	0.071	(0.087)	0.013	0.058
216	18.00	0.13	0.071	(0.087)	0.013	0.058
217	18.08	0.13	0.071	(0.086)	0.013	0.058
218	18.17	0.13	0.071	(0.086)	0.013	0.058
219	18.25	0.13	0.071	(0.085)	0.013	0.058
220	18.33	0.13	0.071	(0.085)	0.013	0.058
221	18.42	0.13	0.071	(0.085)	0.013	0.058
222	18.50	0.13	0.071	(0.084)	0.013	0.058
223	18.58	0.10	0.053	(0.084)	0.010	0.043
224	18.67	0.10	0.053	(0.083)	0.010	0.043
225	18.75	0.10	0.053	(0.083)	0.010	0.043
226	18.83	0.07	0.036	(0.083)	0.007	0.029
227	18.92	0.07	0.036	(0.082)	0.007	0.029
228	19.00	0.07	0.036	(0.082)	0.007	0.029
229	19.08	0.10	0.053	(0.081)	0.010	0.043
230	19.17	0.10	0.053	(0.081)	0.010	0.043
231	19.25	0.10	0.053	(0.081)	0.010	0.043
232	19.33	0.13	0.071	(0.080)	0.013	0.058
233	19.42	0.13	0.071	(0.080)	0.013	0.058
234	19.50	0.13	0.071	(0.080)	0.013	0.058
235	19.58	0.10	0.053	(0.079)	0.010	0.043
236	19.67	0.10	0.053	(0.079)	0.010	0.043
237	19.75	0.10	0.053	(0.078)	0.010	0.043
238	19.83	0.07	0.036	(0.078)	0.007	0.029
239	19.92	0.07	0.036	(0.078)	0.007	0.029
240	20.00	0.07	0.036	(0.077)	0.007	0.029
241	20.08	0.10	0.053	(0.077)	0.010	0.043
242	20.17	0.10	0.053	(0.077)	0.010	0.043
243	20.25	0.10	0.053	(0.076)	0.010	0.043
244	20.33	0.10	0.053	(0.076)	0.010	0.043
245	20.42	0.10	0.053	(0.076)	0.010	0.043
246	20.50	0.10	0.053	(0.075)	0.010	0.043
247	20.58	0.10	0.053	(0.075)	0.010	0.043
248	20.67	0.10	0.053	(0.075)	0.010	0.043
249	20.75	0.10	0.053	(0.074)	0.010	0.043
250	20.83	0.07	0.036	(0.074)	0.007	0.029
251	20.92	0.07	0.036	(0.074)	0.007	0.029
252	21.00	0.07	0.036	(0.074)	0.007	0.029
253	21.08	0.10	0.053	(0.073)	0.010	0.043
254	21.17	0.10	0.053	(0.073)	0.010	0.043
255	21.25	0.10	0.053	(0.073)	0.010	0.043
256	21.33	0.07	0.036	(0.072)	0.007	0.029
257	21.42	0.07	0.036	(0.072)	0.007	0.029
258	21.50	0.07	0.036	(0.072)	0.007	0.029
259	21.58	0.10	0.053	(0.072)	0.010	0.043
260	21.67	0.10	0.053	(0.071)	0.010	0.043
261	21.75	0.10	0.053	(0.071)	0.010	0.043
262	21.83	0.07	0.036	(0.071)	0.007	0.029
263	21.92	0.07	0.036	(0.071)	0.007	0.029
264	22.00	0.07	0.036	(0.070)	0.007	0.029
265	22.08	0.10	0.053	(0.070)	0.010	0.043
266	22.17	0.10	0.053	(0.070)	0.010	0.043

267	22.25	0.10	0.053	(0.070)	0.010	0.043
268	22.33	0.07	0.036	(0.069)	0.007	0.029
269	22.42	0.07	0.036	(0.069)	0.007	0.029
270	22.50	0.07	0.036	(0.069)	0.007	0.029
271	22.58	0.07	0.036	(0.069)	0.007	0.029
272	22.67	0.07	0.036	(0.069)	0.007	0.029
273	22.75	0.07	0.036	(0.068)	0.007	0.029
274	22.83	0.07	0.036	(0.068)	0.007	0.029
275	22.92	0.07	0.036	(0.068)	0.007	0.029
276	23.00	0.07	0.036	(0.068)	0.007	0.029
277	23.08	0.07	0.036	(0.068)	0.007	0.029
278	23.17	0.07	0.036	(0.068)	0.007	0.029
279	23.25	0.07	0.036	(0.067)	0.007	0.029
280	23.33	0.07	0.036	(0.067)	0.007	0.029
281	23.42	0.07	0.036	(0.067)	0.007	0.029
282	23.50	0.07	0.036	(0.067)	0.007	0.029
283	23.58	0.07	0.036	(0.067)	0.007	0.029
284	23.67	0.07	0.036	(0.067)	0.007	0.029
285	23.75	0.07	0.036	(0.067)	0.007	0.029
286	23.83	0.07	0.036	(0.067)	0.007	0.029
287	23.92	0.07	0.036	(0.067)	0.007	0.029
288	24.00	0.07	0.036	(0.067)	0.007	0.029

(Loss Rate Not Used)

Sum = 100.0 Sum = 43.2

Flood volume = Effective rainfall 3.60(In)
times area 1.7(Ac.)/[(In)/(Ft.)] = 0.5(Ac.Ft)
Total soil loss = 0.84(In)
Total soil loss = 0.118(Ac.Ft)
Total rainfall = 4.44(In)
Flood volume = 21932.5 Cubic Feet
Total soil loss = 5144.3 Cubic Feet

Peak flow rate of this hydrograph = 0.829(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.02	Q	|	|	|	|
0+10	0.0004	0.04	Q	|	|	|	|
0+15	0.0008	0.05	Q	|	|	|	|
0+20	0.0012	0.06	Q	|	|	|	|
0+25	0.0017	0.07	Q	|	|	|	|
0+30	0.0022	0.07	Q	|	|	|	|
0+35	0.0027	0.07	Q	|	|	|	|
0+40	0.0032	0.07	Q	|	|	|	|
0+45	0.0037	0.07	Q	|	|	|	|
0+50	0.0042	0.08	Q	|	|	|	|

0+55	0.0049	0.09	Q	|	|	|	|
1+ 0	0.0056	0.10	Q	|	|	|	|
1+ 5	0.0062	0.09	Q	|	|	|	|
1+10	0.0067	0.08	Q	|	|	|	|
1+15	0.0072	0.07	Q	|	|	|	|
1+20	0.0077	0.07	Q	|	|	|	|
1+25	0.0082	0.07	Q	|	|	|	|
1+30	0.0087	0.07	Q	|	|	|	|
1+35	0.0092	0.07	Q	|	|	|	|
1+40	0.0097	0.07	Q	|	|	|	|
1+45	0.0102	0.07	Q	|	|	|	|
1+50	0.0108	0.08	Q	|	|	|	|
1+55	0.0114	0.09	Q	|	|	|	|
2+ 0	0.0121	0.10	Q	|	|	|	|
2+ 5	0.0128	0.10	QV	|	|	|	|
2+10	0.0135	0.10	QV	|	|	|	|
2+15	0.0141	0.10	QV	|	|	|	|
2+20	0.0148	0.10	QV	|	|	|	|
2+25	0.0155	0.10	QV	|	|	|	|
2+30	0.0161	0.10	QV	|	|	|	|
2+35	0.0169	0.11	QV	|	|	|	|
2+40	0.0177	0.12	QV	|	|	|	|
2+45	0.0185	0.12	QV	|	|	|	|
2+50	0.0194	0.12	QV	|	|	|	|
2+55	0.0202	0.12	QV	|	|	|	|
3+ 0	0.0211	0.12	QV	|	|	|	|
3+ 5	0.0219	0.12	QV	|	|	|	|
3+10	0.0227	0.12	QV	|	|	|	|
3+15	0.0236	0.12	QV	|	|	|	|
3+20	0.0244	0.12	QV	|	|	|	|
3+25	0.0252	0.12	Q V	|	|	|	|
3+30	0.0261	0.12	Q V	|	|	|	|
3+35	0.0269	0.12	Q V	|	|	|	|
3+40	0.0278	0.12	Q V	|	|	|	|
3+45	0.0286	0.12	Q V	|	|	|	|
3+50	0.0295	0.13	Q V	|	|	|	|
3+55	0.0305	0.14	Q V	|	|	|	|
4+ 0	0.0315	0.15	Q V	|	|	|	|
4+ 5	0.0325	0.15	Q V	|	|	|	|
4+10	0.0335	0.15	Q V	|	|	|	|
4+15	0.0345	0.15	Q V	|	|	|	|
4+20	0.0356	0.16	Q V	|	|	|	|
4+25	0.0368	0.17	Q V	|	|	|	|
4+30	0.0379	0.17	Q V	|	|	|	|
4+35	0.0391	0.17	Q V	|	|	|	|
4+40	0.0403	0.17	Q V	|	|	|	|
4+45	0.0415	0.17	Q V	|	|	|	|
4+50	0.0427	0.18	Q V	|	|	|	|
4+55	0.0440	0.19	Q V	|	|	|	|
5+ 0	0.0454	0.19	Q V	|	|	|	|
5+ 5	0.0466	0.17	Q V	|	|	|	|
5+10	0.0476	0.15	Q V	|	|	|	|
5+15	0.0486	0.15	Q V	|	|	|	|

```
5+20       0.0497      0.16  Q  V      |         |         |         |
5+25       0.0509      0.17  Q   V     |         |         |         |
5+30       0.0520      0.17  Q   V     |         |         |         |
5+35       0.0533      0.18  Q   V     |         |         |         |
5+40       0.0546      0.19  Q   V     |         |         |         |
5+45       0.0559      0.19  Q   V     |         |         |         |
5+50       0.0573      0.19  Q   V     |         |         |         |
5+55       0.0586      0.19  Q   V     |         |         |         |
6+ 0       0.0600      0.19  Q   V     |         |         |         |
6+ 5       0.0614      0.21  Q   V     |         |         |         |
6+10       0.0629      0.22  Q   V     |         |         |         |
6+15       0.0644      0.22  Q    V    |         |         |         |
6+20       0.0659      0.22  Q    V    |         |         |         |
6+25       0.0674      0.22  Q    V    |         |         |         |
6+30       0.0689      0.22  Q    V    |         |         |         |
6+35       0.0705      0.23  Q    V    |         |         |         |
6+40       0.0722      0.24  Q    V    |         |         |         |
6+45       0.0738      0.24  Q    V    |         |         |         |
6+50       0.0755      0.24  Q    V    |         |         |         |
6+55       0.0772      0.24  Q     V   |         |         |         |
7+ 0       0.0789      0.24  Q     V   |         |         |         |
7+ 5       0.0805      0.24  Q     V   |         |         |         |
7+10       0.0822      0.24  Q     V   |         |         |         |
7+15       0.0839      0.24  Q     V   |         |         |         |
7+20       0.0856      0.25  |Q    V   |         |         |         |
7+25       0.0875      0.27  |Q    V   |         |         |         |
7+30       0.0893      0.27  |Q     V  |         |         |         |
7+35       0.0912      0.28  |Q     V  |         |         |         |
7+40       0.0932      0.29  |Q     V  |         |         |         |
7+45       0.0952      0.29  |Q     V  |         |         |         |
7+50       0.0973      0.30  |Q     V  |         |         |         |
7+55       0.0995      0.31  |Q     V  |         |         |         |
8+ 0       0.1017      0.32  |Q      V |         |         |         |
8+ 5       0.1040      0.34  |Q      V |         |         |         |
8+10       0.1065      0.36  |Q      V |         |         |         |
8+15       0.1090      0.36  |Q      V |         |         |         |
8+20       0.1115      0.37  |Q      V |         |         |         |
8+25       0.1140      0.37  |Q       V|         |         |         |
8+30       0.1165      0.37  |Q       V|         |         |         |
8+35       0.1191      0.38  |Q       V|         |         |         |
8+40       0.1218      0.39  |Q       V|         |         |         |
8+45       0.1245      0.39  |Q       V|         |         |         |
8+50       0.1272      0.40  |Q        V         |         |         |
8+55       0.1301      0.41  |Q        V         |         |         |
9+ 0       0.1329      0.41  |Q        V         |         |         |
9+ 5       0.1359      0.44  |Q        V         |         |         |
9+10       0.1390      0.46  |Q        |V        |         |         |
9+15       0.1422      0.46  |Q        |V        |         |         |
9+20       0.1455      0.47  |Q        |V        |         |         |
9+25       0.1488      0.48  |Q        |V        |         |         |
9+30       0.1522      0.49  |Q        | V       |         |         |
9+35       0.1556      0.50  |Q        | V       |         |         |
9+40       0.1591      0.51  | Q       | V       |         |         |
```

9+45	0.1626	0.51	Q	V			
9+50	0.1662	0.52	Q	V			
9+55	0.1699	0.53	Q	V			
10+ 0	0.1736	0.54	Q	V			
10+ 5	0.1768	0.46	Q	V			
10+10	0.1794	0.39	Q	V			
10+15	0.1820	0.37	Q	V			
10+20	0.1845	0.37	Q	V			
10+25	0.1870	0.37	Q	V			
10+30	0.1895	0.37	Q	V			
10+35	0.1924	0.42	Q	V			
10+40	0.1957	0.47	Q	V			
10+45	0.1990	0.48	Q	V			
10+50	0.2024	0.49	Q	V			
10+55	0.2057	0.49	Q	V			
11+ 0	0.2091	0.49	Q	V			
11+ 5	0.2124	0.48	Q	V			
11+10	0.2156	0.47	Q	V			
11+15	0.2188	0.46	Q	V			
11+20	0.2219	0.46	Q	V			
11+25	0.2251	0.46	Q	V			
11+30	0.2283	0.46	Q	V			
11+35	0.2314	0.44	Q	V			
11+40	0.2343	0.42	Q	V			
11+45	0.2371	0.42	Q	V			
11+50	0.2401	0.42	Q	V			
11+55	0.2431	0.44	Q	V			
12+ 0	0.2461	0.44	Q	V			
12+ 5	0.2496	0.51	Q	V			
12+10	0.2537	0.59	Q	V			
12+15	0.2578	0.60	Q	V			
12+20	0.2621	0.62	Q	V			
12+25	0.2664	0.63	Q	V			
12+30	0.2708	0.63	Q	V			
12+35	0.2753	0.65	Q	V			
12+40	0.2800	0.68	Q	V			
12+45	0.2846	0.68	Q	V			
12+50	0.2894	0.69	Q	V			
12+55	0.2943	0.70	Q	V			
13+ 0	0.2991	0.71	Q	V			
13+ 5	0.3044	0.76	Q	V			
13+10	0.3100	0.81	Q	V			
13+15	0.3156	0.82	Q	V			
13+20	0.3214	0.83	Q	V			
13+25	0.3271	0.83	Q	V			
13+30	0.3328	0.83	Q	V			
13+35	0.3377	0.71	Q	V			
13+40	0.3418	0.59	Q	V			
13+45	0.3457	0.57	Q	V			
13+50	0.3495	0.56	Q	V			
13+55	0.3534	0.56	Q	V			
14+ 0	0.3573	0.56	Q	V			
14+ 5	0.3614	0.60	Q	V			

14+10	0.3659	0.65	Q			V	
14+15	0.3704	0.65	Q			V	
14+20	0.3748	0.65	Q			V	
14+25	0.3792	0.64	Q			V	
14+30	0.3836	0.63	Q			V	
14+35	0.3879	0.63	Q			V	
14+40	0.3923	0.63	Q			V	
14+45	0.3967	0.63	Q			V	
14+50	0.4010	0.62	Q			V	
14+55	0.4052	0.61	Q			V	
15+ 0	0.4094	0.61	Q			V	
15+ 5	0.4135	0.60	Q			V	
15+10	0.4175	0.59	Q			V	
15+15	0.4216	0.59	Q			V	
15+20	0.4255	0.57	Q			V	
15+25	0.4294	0.56	Q			V	
15+30	0.4333	0.56	Q			V	
15+35	0.4368	0.52	Q			V	
15+40	0.4401	0.47	Q			V	
15+45	0.4433	0.47	Q			V	
15+50	0.4465	0.46	Q			V	
15+55	0.4497	0.46	Q			V	
16+ 0	0.4529	0.46	Q			V	
16+ 5	0.4550	0.30	Q			V	
16+10	0.4560	0.14	Q			V	
16+15	0.4567	0.11	Q			V	
16+20	0.4574	0.10	Q			V	
16+25	0.4580	0.10	Q			V	
16+30	0.4587	0.10	Q			V	
16+35	0.4593	0.09	Q			V	
16+40	0.4598	0.08	Q			V	
16+45	0.4603	0.07	Q			V	
16+50	0.4608	0.07	Q			V	
16+55	0.4614	0.07	Q			V	
17+ 0	0.4619	0.07	Q			V	
17+ 5	0.4625	0.09	Q			V	
17+10	0.4633	0.12	Q			V	
17+15	0.4641	0.12	Q			V	
17+20	0.4650	0.12	Q			V	
17+25	0.4658	0.12	Q			V	
17+30	0.4667	0.12	Q			V	
17+35	0.4675	0.12	Q			V	
17+40	0.4683	0.12	Q			V	
17+45	0.4692	0.12	Q			V	
17+50	0.4699	0.11	Q			V	
17+55	0.4706	0.10	Q			V	
18+ 0	0.4713	0.10	Q			V	
18+ 5	0.4720	0.10	Q			V	
18+10	0.4726	0.10	Q			V	
18+15	0.4733	0.10	Q			V	
18+20	0.4740	0.10	Q			V	
18+25	0.4747	0.10	Q			V	
18+30	0.4753	0.10	Q			V	

18+35	0.4759	0.09	Q	|	|	|	V |
18+40	0.4765	0.08	Q	|	|	|	V |
18+45	0.4770	0.07	Q	|	|	|	V |
18+50	0.4774	0.06	Q	|	|	|	V |
18+55	0.4777	0.05	Q	|	|	|	V |
19+ 0	0.4781	0.05	Q	|	|	|	V |
19+ 5	0.4785	0.06	Q	|	|	|	V |
19+10	0.4790	0.07	Q	|	|	|	V |
19+15	0.4795	0.07	Q	|	|	|	V |
19+20	0.4801	0.08	Q	|	|	|	V |
19+25	0.4807	0.09	Q	|	|	|	V |
19+30	0.4814	0.10	Q	|	|	|	V |
19+35	0.4820	0.09	Q	|	|	|	V |
19+40	0.4825	0.08	Q	|	|	|	V |
19+45	0.4830	0.07	Q	|	|	|	V |
19+50	0.4834	0.06	Q	|	|	|	V |
19+55	0.4838	0.05	Q	|	|	|	V |
20+ 0	0.4841	0.05	Q	|	|	|	V |
20+ 5	0.4845	0.06	Q	|	|	|	V |
20+10	0.4850	0.07	Q	|	|	|	V |
20+15	0.4855	0.07	Q	|	|	|	V |
20+20	0.4860	0.07	Q	|	|	|	V |
20+25	0.4865	0.07	Q	|	|	|	V |
20+30	0.4870	0.07	Q	|	|	|	V |
20+35	0.4875	0.07	Q	|	|	|	V |
20+40	0.4880	0.07	Q	|	|	|	V |
20+45	0.4885	0.07	Q	|	|	|	V |
20+50	0.4890	0.06	Q	|	|	|	V |
20+55	0.4893	0.05	Q	|	|	|	V |
21+ 0	0.4897	0.05	Q	|	|	|	V |
21+ 5	0.4901	0.06	Q	|	|	|	V |
21+10	0.4906	0.07	Q	|	|	|	V |
21+15	0.4911	0.07	Q	|	|	|	V|
21+20	0.4915	0.06	Q	|	|	|	V|
21+25	0.4918	0.05	Q	|	|	|	V|
21+30	0.4922	0.05	Q	|	|	|	V|
21+35	0.4926	0.06	Q	|	|	|	V|
21+40	0.4931	0.07	Q	|	|	|	V|
21+45	0.4936	0.07	Q	|	|	|	V|
21+50	0.4940	0.06	Q	|	|	|	V|
21+55	0.4944	0.05	Q	|	|	|	V|
22+ 0	0.4947	0.05	Q	|	|	|	V|
22+ 5	0.4951	0.06	Q	|	|	|	V|
22+10	0.4956	0.07	Q	|	|	|	V|
22+15	0.4961	0.07	Q	|	|	|	V|
22+20	0.4965	0.06	Q	|	|	|	V|
22+25	0.4969	0.05	Q	|	|	|	V|
22+30	0.4972	0.05	Q	|	|	|	V|
22+35	0.4976	0.05	Q	|	|	|	V|
22+40	0.4979	0.05	Q	|	|	|	V|
22+45	0.4982	0.05	Q	|	|	|	V|
22+50	0.4986	0.05	Q	|	|	|	V|
22+55	0.4989	0.05	Q	|	|	|	V|

23+ 0	0.4992	0.05	Q	|	|	|	V|
23+ 5	0.4996	0.05	Q	|	|	|	V|
23+10	0.4999	0.05	Q	|	|	|	V|
23+15	0.5002	0.05	Q	|	|	|	V|
23+20	0.5006	0.05	Q	|	|	|	V|
23+25	0.5009	0.05	Q	|	|	|	V|
23+30	0.5012	0.05	Q	|	|	|	V|
23+35	0.5016	0.05	Q	|	|	|	V|
23+40	0.5019	0.05	Q	|	|	|	V|
23+45	0.5023	0.05	Q	|	|	|	V|
23+50	0.5026	0.05	Q	|	|	|	V|
23+55	0.5029	0.05	Q	|	|	|	V|
24+ 0	0.5033	0.05	Q	|	|	|	V|
24+ 5	0.5035	0.03	Q	|	|	|	V|
24+10	0.5035	0.01	Q	|	|	|	V|
24+15	0.5035	0.00	Q	|	|	|	V|

AREA DD1

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014, Version 9.0
Study date 02/05/24 File: ARDD124100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6279

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

PROPOSED CONDITION: 100YR HYDROLOGY
ARDD1

Drainage Area = 1.70(Ac.) = 0.003 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 1.70(Ac.) = 0.003 Sq. Mi.
Length along longest watercourse = 935.00(Ft.)
Length along longest watercourse measured to centroid = 467.50(Ft.)
Length along longest watercourse = 0.177 Mi.
Length along longest watercourse measured to centroid = 0.089 Mi.
Difference in elevation = 5.00(Ft.)
Slope along watercourse = 28.2353 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.039 Hr.
Lag time = 2.36 Min.
25% of lag time = 0.59 Min.
40% of lag time = 0.94 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.70	1.16	1.97

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
1.70	4.44	7.55

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.160(In)
Area Averaged 100-Year Rainfall = 4.440(In)

Point rain (area averaged) = 4.440(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 4.440(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
1.700	43.00	0.810

Total Area Entered = 1.70(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
43.0	43.0	0.641	0.810	0.174	1.000	0.174
					Sum (F) =	0.174

Area averaged mean soil loss (F) (In/Hr) = 0.174
Minimum soil loss rate ((In/Hr)) = 0.087
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.260

U n i t H y d r o g r a p h
DESERT S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	211.808	44.259	0.758
2	0.167	423.617	44.705	0.766
3	0.250	635.425	8.212	0.141
4	0.333	847.234	2.824	0.048
		Sum = 100.000	Sum=	1.713

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.036	(0.308)	0.009	0.026

2	0.17	0.07	0.036	(0.307)	0.009	0.026
3	0.25	0.07	0.036	(0.305)	0.009	0.026
4	0.33	0.10	0.053	(0.304)	0.014	0.039
5	0.42	0.10	0.053	(0.303)	0.014	0.039
6	0.50	0.10	0.053	(0.302)	0.014	0.039
7	0.58	0.10	0.053	(0.301)	0.014	0.039
8	0.67	0.10	0.053	(0.299)	0.014	0.039
9	0.75	0.10	0.053	(0.298)	0.014	0.039
10	0.83	0.13	0.071	(0.297)	0.018	0.053
11	0.92	0.13	0.071	(0.296)	0.018	0.053
12	1.00	0.13	0.071	(0.295)	0.018	0.053
13	1.08	0.10	0.053	(0.294)	0.014	0.039
14	1.17	0.10	0.053	(0.292)	0.014	0.039
15	1.25	0.10	0.053	(0.291)	0.014	0.039
16	1.33	0.10	0.053	(0.290)	0.014	0.039
17	1.42	0.10	0.053	(0.289)	0.014	0.039
18	1.50	0.10	0.053	(0.288)	0.014	0.039
19	1.58	0.10	0.053	(0.287)	0.014	0.039
20	1.67	0.10	0.053	(0.286)	0.014	0.039
21	1.75	0.10	0.053	(0.284)	0.014	0.039
22	1.83	0.13	0.071	(0.283)	0.018	0.053
23	1.92	0.13	0.071	(0.282)	0.018	0.053
24	2.00	0.13	0.071	(0.281)	0.018	0.053
25	2.08	0.13	0.071	(0.280)	0.018	0.053
26	2.17	0.13	0.071	(0.279)	0.018	0.053
27	2.25	0.13	0.071	(0.278)	0.018	0.053
28	2.33	0.13	0.071	(0.276)	0.018	0.053
29	2.42	0.13	0.071	(0.275)	0.018	0.053
30	2.50	0.13	0.071	(0.274)	0.018	0.053
31	2.58	0.17	0.089	(0.273)	0.023	0.066
32	2.67	0.17	0.089	(0.272)	0.023	0.066
33	2.75	0.17	0.089	(0.271)	0.023	0.066
34	2.83	0.17	0.089	(0.270)	0.023	0.066
35	2.92	0.17	0.089	(0.269)	0.023	0.066
36	3.00	0.17	0.089	(0.267)	0.023	0.066
37	3.08	0.17	0.089	(0.266)	0.023	0.066
38	3.17	0.17	0.089	(0.265)	0.023	0.066
39	3.25	0.17	0.089	(0.264)	0.023	0.066
40	3.33	0.17	0.089	(0.263)	0.023	0.066
41	3.42	0.17	0.089	(0.262)	0.023	0.066
42	3.50	0.17	0.089	(0.261)	0.023	0.066
43	3.58	0.17	0.089	(0.260)	0.023	0.066
44	3.67	0.17	0.089	(0.259)	0.023	0.066
45	3.75	0.17	0.089	(0.258)	0.023	0.066
46	3.83	0.20	0.107	(0.257)	0.028	0.079
47	3.92	0.20	0.107	(0.255)	0.028	0.079
48	4.00	0.20	0.107	(0.254)	0.028	0.079
49	4.08	0.20	0.107	(0.253)	0.028	0.079
50	4.17	0.20	0.107	(0.252)	0.028	0.079
51	4.25	0.20	0.107	(0.251)	0.028	0.079
52	4.33	0.23	0.124	(0.250)	0.032	0.092
53	4.42	0.23	0.124	(0.249)	0.032	0.092
54	4.50	0.23	0.124	(0.248)	0.032	0.092

55	4.58	0.23	0.124	(0.247)	0.032	0.092
56	4.67	0.23	0.124	(0.246)	0.032	0.092
57	4.75	0.23	0.124	(0.245)	0.032	0.092
58	4.83	0.27	0.142	(0.244)	0.037	0.105
59	4.92	0.27	0.142	(0.243)	0.037	0.105
60	5.00	0.27	0.142	(0.242)	0.037	0.105
61	5.08	0.20	0.107	(0.241)	0.028	0.079
62	5.17	0.20	0.107	(0.239)	0.028	0.079
63	5.25	0.20	0.107	(0.238)	0.028	0.079
64	5.33	0.23	0.124	(0.237)	0.032	0.092
65	5.42	0.23	0.124	(0.236)	0.032	0.092
66	5.50	0.23	0.124	(0.235)	0.032	0.092
67	5.58	0.27	0.142	(0.234)	0.037	0.105
68	5.67	0.27	0.142	(0.233)	0.037	0.105
69	5.75	0.27	0.142	(0.232)	0.037	0.105
70	5.83	0.27	0.142	(0.231)	0.037	0.105
71	5.92	0.27	0.142	(0.230)	0.037	0.105
72	6.00	0.27	0.142	(0.229)	0.037	0.105
73	6.08	0.30	0.160	(0.228)	0.042	0.118
74	6.17	0.30	0.160	(0.227)	0.042	0.118
75	6.25	0.30	0.160	(0.226)	0.042	0.118
76	6.33	0.30	0.160	(0.225)	0.042	0.118
77	6.42	0.30	0.160	(0.224)	0.042	0.118
78	6.50	0.30	0.160	(0.223)	0.042	0.118
79	6.58	0.33	0.178	(0.222)	0.046	0.131
80	6.67	0.33	0.178	(0.221)	0.046	0.131
81	6.75	0.33	0.178	(0.220)	0.046	0.131
82	6.83	0.33	0.178	(0.219)	0.046	0.131
83	6.92	0.33	0.178	(0.218)	0.046	0.131
84	7.00	0.33	0.178	(0.217)	0.046	0.131
85	7.08	0.33	0.178	(0.216)	0.046	0.131
86	7.17	0.33	0.178	(0.215)	0.046	0.131
87	7.25	0.33	0.178	(0.214)	0.046	0.131
88	7.33	0.37	0.195	(0.213)	0.051	0.145
89	7.42	0.37	0.195	(0.212)	0.051	0.145
90	7.50	0.37	0.195	(0.211)	0.051	0.145
91	7.58	0.40	0.213	(0.210)	0.055	0.158
92	7.67	0.40	0.213	(0.209)	0.055	0.158
93	7.75	0.40	0.213	(0.208)	0.055	0.158
94	7.83	0.43	0.231	(0.207)	0.060	0.171
95	7.92	0.43	0.231	(0.206)	0.060	0.171
96	8.00	0.43	0.231	(0.205)	0.060	0.171
97	8.08	0.50	0.266	(0.204)	0.069	0.197
98	8.17	0.50	0.266	(0.204)	0.069	0.197
99	8.25	0.50	0.266	(0.203)	0.069	0.197
100	8.33	0.50	0.266	(0.202)	0.069	0.197
101	8.42	0.50	0.266	(0.201)	0.069	0.197
102	8.50	0.50	0.266	(0.200)	0.069	0.197
103	8.58	0.53	0.284	(0.199)	0.074	0.210
104	8.67	0.53	0.284	(0.198)	0.074	0.210
105	8.75	0.53	0.284	(0.197)	0.074	0.210
106	8.83	0.57	0.302	(0.196)	0.078	0.223
107	8.92	0.57	0.302	(0.195)	0.078	0.223

108	9.00	0.57	0.302	(0.194)	0.078	0.223
109	9.08	0.63	0.337	(0.193)	0.088	0.250
110	9.17	0.63	0.337	(0.192)	0.088	0.250
111	9.25	0.63	0.337	(0.191)	0.088	0.250
112	9.33	0.67	0.355	(0.191)	0.092	0.263
113	9.42	0.67	0.355	(0.190)	0.092	0.263
114	9.50	0.67	0.355	(0.189)	0.092	0.263
115	9.58	0.70	0.373	(0.188)	0.097	0.276
116	9.67	0.70	0.373	(0.187)	0.097	0.276
117	9.75	0.70	0.373	(0.186)	0.097	0.276
118	9.83	0.73	0.391	(0.185)	0.102	0.289
119	9.92	0.73	0.391	(0.184)	0.102	0.289
120	10.00	0.73	0.391	(0.183)	0.102	0.289
121	10.08	0.50	0.266	(0.182)	0.069	0.197
122	10.17	0.50	0.266	(0.182)	0.069	0.197
123	10.25	0.50	0.266	(0.181)	0.069	0.197
124	10.33	0.50	0.266	(0.180)	0.069	0.197
125	10.42	0.50	0.266	(0.179)	0.069	0.197
126	10.50	0.50	0.266	(0.178)	0.069	0.197
127	10.58	0.67	0.355	(0.177)	0.092	0.263
128	10.67	0.67	0.355	(0.176)	0.092	0.263
129	10.75	0.67	0.355	(0.175)	0.092	0.263
130	10.83	0.67	0.355	(0.175)	0.092	0.263
131	10.92	0.67	0.355	(0.174)	0.092	0.263
132	11.00	0.67	0.355	(0.173)	0.092	0.263
133	11.08	0.63	0.337	(0.172)	0.088	0.250
134	11.17	0.63	0.337	(0.171)	0.088	0.250
135	11.25	0.63	0.337	(0.170)	0.088	0.250
136	11.33	0.63	0.337	(0.169)	0.088	0.250
137	11.42	0.63	0.337	(0.169)	0.088	0.250
138	11.50	0.63	0.337	(0.168)	0.088	0.250
139	11.58	0.57	0.302	(0.167)	0.078	0.223
140	11.67	0.57	0.302	(0.166)	0.078	0.223
141	11.75	0.57	0.302	(0.165)	0.078	0.223
142	11.83	0.60	0.320	(0.165)	0.083	0.237
143	11.92	0.60	0.320	(0.164)	0.083	0.237
144	12.00	0.60	0.320	(0.163)	0.083	0.237
145	12.08	0.83	0.444	(0.162)	0.115	0.329
146	12.17	0.83	0.444	(0.161)	0.115	0.329
147	12.25	0.83	0.444	(0.160)	0.115	0.329
148	12.33	0.87	0.462	(0.160)	0.120	0.342
149	12.42	0.87	0.462	(0.159)	0.120	0.342
150	12.50	0.87	0.462	(0.158)	0.120	0.342
151	12.58	0.93	0.497	(0.157)	0.129	0.368
152	12.67	0.93	0.497	(0.156)	0.129	0.368
153	12.75	0.93	0.497	(0.156)	0.129	0.368
154	12.83	0.97	0.515	(0.155)	0.134	0.381
155	12.92	0.97	0.515	(0.154)	0.134	0.381
156	13.00	0.97	0.515	(0.153)	0.134	0.381
157	13.08	1.13	0.604	0.153	(0.157)	0.451
158	13.17	1.13	0.604	0.152	(0.157)	0.452
159	13.25	1.13	0.604	0.151	(0.157)	0.453
160	13.33	1.13	0.604	0.150	(0.157)	0.454

161	13.42	1.13	0.604	0.149	(0.157)	0.454
162	13.50	1.13	0.604	0.149	(0.157)	0.455
163	13.58	0.77	0.408	(0.148)	0.106	0.302
164	13.67	0.77	0.408	(0.147)	0.106	0.302
165	13.75	0.77	0.408	(0.146)	0.106	0.302
166	13.83	0.77	0.408	(0.146)	0.106	0.302
167	13.92	0.77	0.408	(0.145)	0.106	0.302
168	14.00	0.77	0.408	(0.144)	0.106	0.302
169	14.08	0.90	0.480	(0.143)	0.125	0.355
170	14.17	0.90	0.480	(0.143)	0.125	0.355
171	14.25	0.90	0.480	(0.142)	0.125	0.355
172	14.33	0.87	0.462	(0.141)	0.120	0.342
173	14.42	0.87	0.462	(0.141)	0.120	0.342
174	14.50	0.87	0.462	(0.140)	0.120	0.342
175	14.58	0.87	0.462	(0.139)	0.120	0.342
176	14.67	0.87	0.462	(0.138)	0.120	0.342
177	14.75	0.87	0.462	(0.138)	0.120	0.342
178	14.83	0.83	0.444	(0.137)	0.115	0.329
179	14.92	0.83	0.444	(0.136)	0.115	0.329
180	15.00	0.83	0.444	(0.136)	0.115	0.329
181	15.08	0.80	0.426	(0.135)	0.111	0.315
182	15.17	0.80	0.426	(0.134)	0.111	0.315
183	15.25	0.80	0.426	(0.134)	0.111	0.315
184	15.33	0.77	0.408	(0.133)	0.106	0.302
185	15.42	0.77	0.408	(0.132)	0.106	0.302
186	15.50	0.77	0.408	(0.131)	0.106	0.302
187	15.58	0.63	0.337	(0.131)	0.088	0.250
188	15.67	0.63	0.337	(0.130)	0.088	0.250
189	15.75	0.63	0.337	(0.129)	0.088	0.250
190	15.83	0.63	0.337	(0.129)	0.088	0.250
191	15.92	0.63	0.337	(0.128)	0.088	0.250
192	16.00	0.63	0.337	(0.127)	0.088	0.250
193	16.08	0.13	0.071	(0.127)	0.018	0.053
194	16.17	0.13	0.071	(0.126)	0.018	0.053
195	16.25	0.13	0.071	(0.126)	0.018	0.053
196	16.33	0.13	0.071	(0.125)	0.018	0.053
197	16.42	0.13	0.071	(0.124)	0.018	0.053
198	16.50	0.13	0.071	(0.124)	0.018	0.053
199	16.58	0.10	0.053	(0.123)	0.014	0.039
200	16.67	0.10	0.053	(0.122)	0.014	0.039
201	16.75	0.10	0.053	(0.122)	0.014	0.039
202	16.83	0.10	0.053	(0.121)	0.014	0.039
203	16.92	0.10	0.053	(0.121)	0.014	0.039
204	17.00	0.10	0.053	(0.120)	0.014	0.039
205	17.08	0.17	0.089	(0.119)	0.023	0.066
206	17.17	0.17	0.089	(0.119)	0.023	0.066
207	17.25	0.17	0.089	(0.118)	0.023	0.066
208	17.33	0.17	0.089	(0.118)	0.023	0.066
209	17.42	0.17	0.089	(0.117)	0.023	0.066
210	17.50	0.17	0.089	(0.116)	0.023	0.066
211	17.58	0.17	0.089	(0.116)	0.023	0.066
212	17.67	0.17	0.089	(0.115)	0.023	0.066
213	17.75	0.17	0.089	(0.115)	0.023	0.066

214	17.83	0.13	0.071	(0.114)	0.018	0.053
215	17.92	0.13	0.071	(0.113)	0.018	0.053
216	18.00	0.13	0.071	(0.113)	0.018	0.053
217	18.08	0.13	0.071	(0.112)	0.018	0.053
218	18.17	0.13	0.071	(0.112)	0.018	0.053
219	18.25	0.13	0.071	(0.111)	0.018	0.053
220	18.33	0.13	0.071	(0.111)	0.018	0.053
221	18.42	0.13	0.071	(0.110)	0.018	0.053
222	18.50	0.13	0.071	(0.110)	0.018	0.053
223	18.58	0.10	0.053	(0.109)	0.014	0.039
224	18.67	0.10	0.053	(0.109)	0.014	0.039
225	18.75	0.10	0.053	(0.108)	0.014	0.039
226	18.83	0.07	0.036	(0.108)	0.009	0.026
227	18.92	0.07	0.036	(0.107)	0.009	0.026
228	19.00	0.07	0.036	(0.107)	0.009	0.026
229	19.08	0.10	0.053	(0.106)	0.014	0.039
230	19.17	0.10	0.053	(0.106)	0.014	0.039
231	19.25	0.10	0.053	(0.105)	0.014	0.039
232	19.33	0.13	0.071	(0.105)	0.018	0.053
233	19.42	0.13	0.071	(0.104)	0.018	0.053
234	19.50	0.13	0.071	(0.104)	0.018	0.053
235	19.58	0.10	0.053	(0.103)	0.014	0.039
236	19.67	0.10	0.053	(0.103)	0.014	0.039
237	19.75	0.10	0.053	(0.102)	0.014	0.039
238	19.83	0.07	0.036	(0.102)	0.009	0.026
239	19.92	0.07	0.036	(0.101)	0.009	0.026
240	20.00	0.07	0.036	(0.101)	0.009	0.026
241	20.08	0.10	0.053	(0.100)	0.014	0.039
242	20.17	0.10	0.053	(0.100)	0.014	0.039
243	20.25	0.10	0.053	(0.099)	0.014	0.039
244	20.33	0.10	0.053	(0.099)	0.014	0.039
245	20.42	0.10	0.053	(0.099)	0.014	0.039
246	20.50	0.10	0.053	(0.098)	0.014	0.039
247	20.58	0.10	0.053	(0.098)	0.014	0.039
248	20.67	0.10	0.053	(0.097)	0.014	0.039
249	20.75	0.10	0.053	(0.097)	0.014	0.039
250	20.83	0.07	0.036	(0.097)	0.009	0.026
251	20.92	0.07	0.036	(0.096)	0.009	0.026
252	21.00	0.07	0.036	(0.096)	0.009	0.026
253	21.08	0.10	0.053	(0.095)	0.014	0.039
254	21.17	0.10	0.053	(0.095)	0.014	0.039
255	21.25	0.10	0.053	(0.095)	0.014	0.039
256	21.33	0.07	0.036	(0.094)	0.009	0.026
257	21.42	0.07	0.036	(0.094)	0.009	0.026
258	21.50	0.07	0.036	(0.094)	0.009	0.026
259	21.58	0.10	0.053	(0.093)	0.014	0.039
260	21.67	0.10	0.053	(0.093)	0.014	0.039
261	21.75	0.10	0.053	(0.093)	0.014	0.039
262	21.83	0.07	0.036	(0.092)	0.009	0.026
263	21.92	0.07	0.036	(0.092)	0.009	0.026
264	22.00	0.07	0.036	(0.092)	0.009	0.026
265	22.08	0.10	0.053	(0.091)	0.014	0.039
266	22.17	0.10	0.053	(0.091)	0.014	0.039

267	22.25	0.10	0.053	(0.091)	0.014	0.039
268	22.33	0.07	0.036	(0.090)	0.009	0.026
269	22.42	0.07	0.036	(0.090)	0.009	0.026
270	22.50	0.07	0.036	(0.090)	0.009	0.026
271	22.58	0.07	0.036	(0.090)	0.009	0.026
272	22.67	0.07	0.036	(0.089)	0.009	0.026
273	22.75	0.07	0.036	(0.089)	0.009	0.026
274	22.83	0.07	0.036	(0.089)	0.009	0.026
275	22.92	0.07	0.036	(0.089)	0.009	0.026
276	23.00	0.07	0.036	(0.089)	0.009	0.026
277	23.08	0.07	0.036	(0.088)	0.009	0.026
278	23.17	0.07	0.036	(0.088)	0.009	0.026
279	23.25	0.07	0.036	(0.088)	0.009	0.026
280	23.33	0.07	0.036	(0.088)	0.009	0.026
281	23.42	0.07	0.036	(0.088)	0.009	0.026
282	23.50	0.07	0.036	(0.087)	0.009	0.026
283	23.58	0.07	0.036	(0.087)	0.009	0.026
284	23.67	0.07	0.036	(0.087)	0.009	0.026
285	23.75	0.07	0.036	(0.087)	0.009	0.026
286	23.83	0.07	0.036	(0.087)	0.009	0.026
287	23.92	0.07	0.036	(0.087)	0.009	0.026
288	24.00	0.07	0.036	(0.087)	0.009	0.026

(Loss Rate Not Used)

Sum = 100.0 Sum = 39.5

Flood volume = Effective rainfall 3.29(In)
times area 1.7(Ac.)/[(In)/(Ft.)] = 0.5(Ac.Ft)
Total soil loss = 1.15(In)
Total soil loss = 0.163(Ac.Ft)
Total rainfall = 4.44(In)
Flood volume = 20295.1 Cubic Feet
Total soil loss = 7104.1 Cubic Feet

Peak flow rate of this hydrograph = 0.779(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.02	Q	|	|	|	|
0+10	0.0004	0.04	Q	|	|	|	|
0+15	0.0007	0.04	Q	|	|	|	|
0+20	0.0011	0.06	Q	|	|	|	|
0+25	0.0015	0.07	Q	|	|	|	|
0+30	0.0020	0.07	Q	|	|	|	|
0+35	0.0025	0.07	Q	|	|	|	|
0+40	0.0029	0.07	Q	|	|	|	|
0+45	0.0034	0.07	Q	|	|	|	|
0+50	0.0039	0.08	Q	|	|	|	|

0+55	0.0045	0.09	Q	|	|	|	|
1+ 0	0.0052	0.09	Q	|	|	|	|
1+ 5	0.0057	0.08	Q	|	|	|	|
1+10	0.0062	0.07	Q	|	|	|	|
1+15	0.0067	0.07	Q	|	|	|	|
1+20	0.0071	0.07	Q	|	|	|	|
1+25	0.0076	0.07	Q	|	|	|	|
1+30	0.0081	0.07	Q	|	|	|	|
1+35	0.0085	0.07	Q	|	|	|	|
1+40	0.0090	0.07	Q	|	|	|	|
1+45	0.0095	0.07	Q	|	|	|	|
1+50	0.0100	0.08	Q	|	|	|	|
1+55	0.0106	0.09	Q	|	|	|	|
2+ 0	0.0112	0.09	Q	|	|	|	|
2+ 5	0.0118	0.09	QV	|	|	|	|
2+10	0.0124	0.09	QV	|	|	|	|
2+15	0.0131	0.09	QV	|	|	|	|
2+20	0.0137	0.09	QV	|	|	|	|
2+25	0.0143	0.09	QV	|	|	|	|
2+30	0.0149	0.09	QV	|	|	|	|
2+35	0.0156	0.10	QV	|	|	|	|
2+40	0.0164	0.11	QV	|	|	|	|
2+45	0.0171	0.11	QV	|	|	|	|
2+50	0.0179	0.11	QV	|	|	|	|
2+55	0.0187	0.11	QV	|	|	|	|
3+ 0	0.0195	0.11	QV	|	|	|	|
3+ 5	0.0203	0.11	QV	|	|	|	|
3+10	0.0210	0.11	QV	|	|	|	|
3+15	0.0218	0.11	QV	|	|	|	|
3+20	0.0226	0.11	QV	|	|	|	|
3+25	0.0234	0.11	Q V	|	|	|	|
3+30	0.0241	0.11	Q V	|	|	|	|
3+35	0.0249	0.11	Q V	|	|	|	|
3+40	0.0257	0.11	Q V	|	|	|	|
3+45	0.0265	0.11	Q V	|	|	|	|
3+50	0.0273	0.12	Q V	|	|	|	|
3+55	0.0282	0.13	Q V	|	|	|	|
4+ 0	0.0291	0.13	Q V	|	|	|	|
4+ 5	0.0301	0.14	Q V	|	|	|	|
4+10	0.0310	0.14	Q V	|	|	|	|
4+15	0.0319	0.14	Q V	|	|	|	|
4+20	0.0329	0.15	Q V	|	|	|	|
4+25	0.0340	0.16	Q V	|	|	|	|
4+30	0.0351	0.16	Q V	|	|	|	|
4+35	0.0362	0.16	Q V	|	|	|	|
4+40	0.0373	0.16	Q V	|	|	|	|
4+45	0.0383	0.16	Q V	|	|	|	|
4+50	0.0395	0.17	Q V	|	|	|	|
4+55	0.0407	0.18	Q V	|	|	|	|
5+ 0	0.0420	0.18	Q V	|	|	|	|
5+ 5	0.0431	0.16	Q V	|	|	|	|
5+10	0.0440	0.14	Q V	|	|	|	|
5+15	0.0450	0.14	Q V	|	|	|	|

5+20	0.0460	0.15	Q V	|	|	|	|
5+25	0.0470	0.16	Q V	|	|	|	|
5+30	0.0481	0.16	Q V	|	|	|	|
5+35	0.0493	0.17	Q V	|	|	|	|
5+40	0.0505	0.18	Q V	|	|	|	|
5+45	0.0517	0.18	Q V	|	|	|	|
5+50	0.0530	0.18	Q V	|	|	|	|
5+55	0.0542	0.18	Q V	|	|	|	|
6+ 0	0.0555	0.18	Q V	|	|	|	|
6+ 5	0.0568	0.19	Q V	|	|	|	|
6+10	0.0581	0.20	Q V	|	|	|	|
6+15	0.0595	0.20	Q V	|	|	|	|
6+20	0.0609	0.20	Q V	|	|	|	|
6+25	0.0623	0.20	Q V	|	|	|	|
6+30	0.0637	0.20	Q V	|	|	|	|
6+35	0.0652	0.21	Q V	|	|	|	|
6+40	0.0667	0.22	Q V	|	|	|	|
6+45	0.0683	0.22	Q V	|	|	|	|
6+50	0.0698	0.23	Q V	|	|	|	|
6+55	0.0714	0.23	Q V	|	|	|	|
7+ 0	0.0729	0.23	Q V	|	|	|	|
7+ 5	0.0745	0.23	Q V	|	|	|	|
7+10	0.0760	0.23	Q V	|	|	|	|
7+15	0.0776	0.23	Q V	|	|	|	|
7+20	0.0792	0.24	Q V	|	|	|	|
7+25	0.0809	0.25	Q V	|	|	|	|
7+30	0.0826	0.25	Q V	|	|	|	|
7+35	0.0844	0.26	|Q V	|	|	|	|
7+40	0.0862	0.27	|Q V	|	|	|	|
7+45	0.0881	0.27	|Q V	|	|	|	|
7+50	0.0900	0.28	|Q V	|	|	|	|
7+55	0.0920	0.29	|Q V	|	|	|	|
8+ 0	0.0940	0.29	|Q V	|	|	|	|
8+ 5	0.0962	0.31	|Q V	|	|	|	|
8+10	0.0985	0.33	|Q V	|	|	|	|
8+15	0.1008	0.34	|Q V	|	|	|	|
8+20	0.1031	0.34	|Q V	|	|	|	|
8+25	0.1054	0.34	|Q V|	|	|	|	|
8+30	0.1078	0.34	|Q V|	|	|	|	|
8+35	0.1102	0.35	|Q V|	|	|	|	|
8+40	0.1126	0.36	|Q V|	|	|	|	|
8+45	0.1151	0.36	|Q V|	|	|	|	|
8+50	0.1177	0.37	|Q V	|	|	|	|
8+55	0.1203	0.38	|Q V	|	|	|	|
9+ 0	0.1229	0.38	|Q V	|	|	|	|
9+ 5	0.1257	0.40	|Q V	|	|	|	|
9+10	0.1286	0.42	|Q |V	|	|	|	|
9+15	0.1315	0.43	|Q |V	|	|	|	|
9+20	0.1346	0.44	|Q |V	|	|	|	|
9+25	0.1376	0.45	|Q |V	|	|	|	|
9+30	0.1407	0.45	|Q | V	|	|	|	|
9+35	0.1439	0.46	|Q | V	|	|	|	|
9+40	0.1471	0.47	|Q | V	|	|	|	|

9+45	0.1504	0.47	Q	V			
9+50	0.1537	0.48	Q	V			
9+55	0.1571	0.49	Q	V			
10+ 0	0.1605	0.49	Q	V			
10+ 5	0.1635	0.43	Q	V			
10+10	0.1659	0.36	Q	V			
10+15	0.1683	0.34	Q	V			
10+20	0.1706	0.34	Q	V			
10+25	0.1729	0.34	Q	V			
10+30	0.1753	0.34	Q	V			
10+35	0.1779	0.39	Q	V			
10+40	0.1809	0.44	Q	V			
10+45	0.1840	0.45	Q	V			
10+50	0.1871	0.45	Q	V			
10+55	0.1902	0.45	Q	V			
11+ 0	0.1933	0.45	Q	V			
11+ 5	0.1964	0.44	Q	V			
11+10	0.1993	0.43	Q	V			
11+15	0.2023	0.43	Q	V			
11+20	0.2052	0.43	Q	V			
11+25	0.2082	0.43	Q	V			
11+30	0.2111	0.43	Q	V			
11+35	0.2139	0.41	Q	V			
11+40	0.2166	0.39	Q	V			
11+45	0.2193	0.38	Q	V			
11+50	0.2220	0.39	Q	V			
11+55	0.2247	0.40	Q	V			
12+ 0	0.2275	0.40	Q	V			
12+ 5	0.2308	0.48	Q	V			
12+10	0.2346	0.55	Q	V			
12+15	0.2384	0.56	Q	V			
12+20	0.2424	0.57	Q	V			
12+25	0.2464	0.58	Q	V			
12+30	0.2504	0.59	Q	V			
12+35	0.2546	0.61	Q	V			
12+40	0.2589	0.63	Q	V			
12+45	0.2632	0.63	Q	V			
12+50	0.2676	0.64	Q	V			
12+55	0.2721	0.65	Q	V			
13+ 0	0.2766	0.65	Q	V			
13+ 5	0.2815	0.71	Q	V			
13+10	0.2867	0.76	Q	V			
13+15	0.2920	0.77	Q	V			
13+20	0.2974	0.78	Q	V			
13+25	0.3027	0.78	Q	V			
13+30	0.3081	0.78	Q	V			
13+35	0.3127	0.66	Q	V			
13+40	0.3164	0.55	Q	V			
13+45	0.3201	0.53	Q	V			
13+50	0.3236	0.52	Q	V			
13+55	0.3272	0.52	Q	V			
14+ 0	0.3308	0.52	Q	V			
14+ 5	0.3346	0.56	Q	V			

14+10	0.3387	0.60	| Q	|	|	V|	|
14+15	0.3429	0.61	| Q	|	|	V|	|
14+20	0.3470	0.60	| Q	|	|	V|	|
14+25	0.3511	0.59	| Q	|	|	V	|
14+30	0.3551	0.59	| Q	|	|	V	|
14+35	0.3592	0.59	| Q	|	|	V	|
14+40	0.3632	0.59	| Q	|	|	|V	|
14+45	0.3672	0.59	| Q	|	|	|V	|
14+50	0.3712	0.58	| Q	|	|	|V	|
14+55	0.3751	0.57	| Q	|	|	| V	|
15+ 0	0.3790	0.56	| Q	|	|	| V	|
15+ 5	0.3828	0.55	| Q	|	|	| V	|
15+10	0.3865	0.54	| Q	|	|	| V	|
15+15	0.3902	0.54	| Q	|	|	| V	|
15+20	0.3939	0.53	| Q	|	|	| V	|
15+25	0.3975	0.52	| Q	|	|	| V	|
15+30	0.4011	0.52	| Q	|	|	| V	|
15+35	0.4043	0.48	|Q	|	|	| V	|
15+40	0.4074	0.44	|Q	|	|	| V	|
15+45	0.4103	0.43	|Q	|	|	| V	|
15+50	0.4133	0.43	|Q	|	|	| V	|
15+55	0.4162	0.43	|Q	|	|	| V	|
16+ 0	0.4192	0.43	|Q	|	|	| V	|
16+ 5	0.4211	0.28	|Q	|	|	| V	|
16+10	0.4220	0.13	Q	|	|	| V	|
16+15	0.4227	0.10	Q	|	|	| V	|
16+20	0.4233	0.09	Q	|	|	| V	|
16+25	0.4239	0.09	Q	|	|	| V	|
16+30	0.4245	0.09	Q	|	|	| V	|
16+35	0.4251	0.08	Q	|	|	| V	|
16+40	0.4256	0.07	Q	|	|	| V	|
16+45	0.4260	0.07	Q	|	|	| V	|
16+50	0.4265	0.07	Q	|	|	| V	|
16+55	0.4270	0.07	Q	|	|	| V	|
17+ 0	0.4274	0.07	Q	|	|	| V	|
17+ 5	0.4280	0.09	Q	|	|	| V	|
17+10	0.4288	0.11	Q	|	|	| V	|
17+15	0.4295	0.11	Q	|	|	| V	|
17+20	0.4303	0.11	Q	|	|	| V	|
17+25	0.4311	0.11	Q	|	|	| V	|
17+30	0.4319	0.11	Q	|	|	| V	|
17+35	0.4326	0.11	Q	|	|	| V	|
17+40	0.4334	0.11	Q	|	|	| V	|
17+45	0.4342	0.11	Q	|	|	| V	|
17+50	0.4349	0.10	Q	|	|	| V	|
17+55	0.4355	0.09	Q	|	|	| V	|
18+ 0	0.4362	0.09	Q	|	|	| V	|
18+ 5	0.4368	0.09	Q	|	|	| V	|
18+10	0.4374	0.09	Q	|	|	| V	|
18+15	0.4380	0.09	Q	|	|	| V	|
18+20	0.4386	0.09	Q	|	|	| V	|
18+25	0.4393	0.09	Q	|	|	| V	|
18+30	0.4399	0.09	Q	|	|	| V	|

18+35	0.4404	0.08	Q	|	|	|	V |
18+40	0.4409	0.07	Q	|	|	|	V |
18+45	0.4414	0.07	Q	|	|	|	V |
18+50	0.4418	0.06	Q	|	|	|	V |
18+55	0.4421	0.05	Q	|	|	|	V |
19+ 0	0.4424	0.05	Q	|	|	|	V |
19+ 5	0.4428	0.06	Q	|	|	|	V |
19+10	0.4432	0.07	Q	|	|	|	V |
19+15	0.4437	0.07	Q	|	|	|	V |
19+20	0.4442	0.08	Q	|	|	|	V |
19+25	0.4448	0.09	Q	|	|	|	V |
19+30	0.4455	0.09	Q	|	|	|	V |
19+35	0.4460	0.08	Q	|	|	|	V |
19+40	0.4465	0.07	Q	|	|	|	V |
19+45	0.4470	0.07	Q	|	|	|	V |
19+50	0.4474	0.06	Q	|	|	|	V |
19+55	0.4477	0.05	Q	|	|	|	V |
20+ 0	0.4480	0.05	Q	|	|	|	V |
20+ 5	0.4484	0.06	Q	|	|	|	V |
20+10	0.4488	0.07	Q	|	|	|	V |
20+15	0.4493	0.07	Q	|	|	|	V |
20+20	0.4498	0.07	Q	|	|	|	V |
20+25	0.4502	0.07	Q	|	|	|	V |
20+30	0.4507	0.07	Q	|	|	|	V |
20+35	0.4512	0.07	Q	|	|	|	V |
20+40	0.4516	0.07	Q	|	|	|	V |
20+45	0.4521	0.07	Q	|	|	|	V |
20+50	0.4525	0.06	Q	|	|	|	V |
20+55	0.4528	0.05	Q	|	|	|	V |
21+ 0	0.4531	0.05	Q	|	|	|	V |
21+ 5	0.4535	0.06	Q	|	|	|	V |
21+10	0.4540	0.07	Q	|	|	|	V |
21+15	0.4544	0.07	Q	|	|	|	V|
21+20	0.4548	0.06	Q	|	|	|	V|
21+25	0.4551	0.05	Q	|	|	|	V|
21+30	0.4555	0.05	Q	|	|	|	V|
21+35	0.4558	0.06	Q	|	|	|	V|
21+40	0.4563	0.07	Q	|	|	|	V|
21+45	0.4567	0.07	Q	|	|	|	V|
21+50	0.4571	0.06	Q	|	|	|	V|
21+55	0.4575	0.05	Q	|	|	|	V|
22+ 0	0.4578	0.05	Q	|	|	|	V|
22+ 5	0.4582	0.06	Q	|	|	|	V|
22+10	0.4586	0.07	Q	|	|	|	V|
22+15	0.4591	0.07	Q	|	|	|	V|
22+20	0.4595	0.06	Q	|	|	|	V|
22+25	0.4598	0.05	Q	|	|	|	V|
22+30	0.4601	0.05	Q	|	|	|	V|
22+35	0.4604	0.05	Q	|	|	|	V|
22+40	0.4607	0.05	Q	|	|	|	V|
22+45	0.4610	0.05	Q	|	|	|	V|
22+50	0.4614	0.05	Q	|	|	|	V|
22+55	0.4617	0.05	Q	|	|	|	V|

```
   23+ 0       0.4620      0.05  Q          |          |          |         V|
   23+ 5       0.4623      0.05  Q          |          |          |         V|
   23+10       0.4626      0.05  Q          |          |          |         V|
   23+15       0.4629      0.05  Q          |          |          |         V|
   23+20       0.4632      0.05  Q          |          |          |         V|
   23+25       0.4635      0.05  Q          |          |          |         V|
   23+30       0.4638      0.05  Q          |          |          |         V|
   23+35       0.4641      0.05  Q          |          |          |         V|
   23+40       0.4645      0.05  Q          |          |          |         V|
   23+45       0.4648      0.05  Q          |          |          |         V|
   23+50       0.4651      0.05  Q          |          |          |         V|
   23+55       0.4654      0.05  Q          |          |          |         V|
   24+ 0       0.4657      0.05  Q          |          |          |         V|
   24+ 5       0.4659      0.03  Q          |          |          |         V|
   24+10       0.4659      0.00  Q          |          |          |         V|
   24+15       0.4659      0.00  Q          |          |          |          V
-------------------------------------------------------------------------------
```

AREA E1

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014, Version 9.0
Study date 02/05/24 File: ARE124100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6279

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

PROPOSED CONDITION: 100YR HYDROLOGY
ARE1

Drainage Area = 0.55(Ac.) = 0.001 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.55(Ac.) = 0.001 Sq. Mi.
Length along longest watercourse = 303.00(Ft.)
Length along longest watercourse measured to centroid = 151.50(Ft.)
Length along longest watercourse = 0.057 Mi.
Length along longest watercourse measured to centroid = 0.029 Mi.
Difference in elevation = 2.50(Ft.)
Slope along watercourse = 43.5644 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.015 Hr.
Lag time = 0.92 Min.
25% of lag time = 0.23 Min.
40% of lag time = 0.37 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.55	1.16	0.64

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.55	4.44	2.44

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.160(In)
Area Averaged 100-Year Rainfall = 4.440(In)

Point rain (area averaged) = 4.440(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 4.440(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.550	32.00	0.890

Total Area Entered = 0.55(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
32.0	32.0	0.742	0.890	0.148	1.000	0.148
					Sum (F) =	0.148

Area averaged mean soil loss (F) (In/Hr) = 0.148
Minimum soil loss rate ((In/Hr)) = 0.074
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.190

U n i t H y d r o g r a p h
DESERT S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	541.562	73.091	0.405
2	0.167	1083.123	26.909	0.149
		Sum = 100.000	Sum=	0.554

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max		Low	Effective (In/Hr)
1	0.08	0.07	0.036	(0.262)	0.007	0.029
2	0.17	0.07	0.036	(0.261)	0.007	0.029
3	0.25	0.07	0.036	(0.260)	0.007	0.029

4	0.33	0.10	0.053	(0.259)	0.010	0.043
5	0.42	0.10	0.053	(0.258)	0.010	0.043
6	0.50	0.10	0.053	(0.257)	0.010	0.043
7	0.58	0.10	0.053	(0.256)	0.010	0.043
8	0.67	0.10	0.053	(0.255)	0.010	0.043
9	0.75	0.10	0.053	(0.254)	0.010	0.043
10	0.83	0.13	0.071	(0.253)	0.013	0.058
11	0.92	0.13	0.071	(0.252)	0.013	0.058
12	1.00	0.13	0.071	(0.251)	0.013	0.058
13	1.08	0.10	0.053	(0.250)	0.010	0.043
14	1.17	0.10	0.053	(0.249)	0.010	0.043
15	1.25	0.10	0.053	(0.248)	0.010	0.043
16	1.33	0.10	0.053	(0.247)	0.010	0.043
17	1.42	0.10	0.053	(0.246)	0.010	0.043
18	1.50	0.10	0.053	(0.245)	0.010	0.043
19	1.58	0.10	0.053	(0.244)	0.010	0.043
20	1.67	0.10	0.053	(0.243)	0.010	0.043
21	1.75	0.10	0.053	(0.242)	0.010	0.043
22	1.83	0.13	0.071	(0.241)	0.013	0.058
23	1.92	0.13	0.071	(0.240)	0.013	0.058
24	2.00	0.13	0.071	(0.239)	0.013	0.058
25	2.08	0.13	0.071	(0.238)	0.013	0.058
26	2.17	0.13	0.071	(0.237)	0.013	0.058
27	2.25	0.13	0.071	(0.236)	0.013	0.058
28	2.33	0.13	0.071	(0.235)	0.013	0.058
29	2.42	0.13	0.071	(0.234)	0.013	0.058
30	2.50	0.13	0.071	(0.233)	0.013	0.058
31	2.58	0.17	0.089	(0.232)	0.017	0.072
32	2.67	0.17	0.089	(0.231)	0.017	0.072
33	2.75	0.17	0.089	(0.230)	0.017	0.072
34	2.83	0.17	0.089	(0.229)	0.017	0.072
35	2.92	0.17	0.089	(0.228)	0.017	0.072
36	3.00	0.17	0.089	(0.228)	0.017	0.072
37	3.08	0.17	0.089	(0.227)	0.017	0.072
38	3.17	0.17	0.089	(0.226)	0.017	0.072
39	3.25	0.17	0.089	(0.225)	0.017	0.072
40	3.33	0.17	0.089	(0.224)	0.017	0.072
41	3.42	0.17	0.089	(0.223)	0.017	0.072
42	3.50	0.17	0.089	(0.222)	0.017	0.072
43	3.58	0.17	0.089	(0.221)	0.017	0.072
44	3.67	0.17	0.089	(0.220)	0.017	0.072
45	3.75	0.17	0.089	(0.219)	0.017	0.072
46	3.83	0.20	0.107	(0.218)	0.020	0.086
47	3.92	0.20	0.107	(0.217)	0.020	0.086
48	4.00	0.20	0.107	(0.216)	0.020	0.086
49	4.08	0.20	0.107	(0.215)	0.020	0.086
50	4.17	0.20	0.107	(0.215)	0.020	0.086
51	4.25	0.20	0.107	(0.214)	0.020	0.086
52	4.33	0.23	0.124	(0.213)	0.024	0.101
53	4.42	0.23	0.124	(0.212)	0.024	0.101
54	4.50	0.23	0.124	(0.211)	0.024	0.101
55	4.58	0.23	0.124	(0.210)	0.024	0.101
56	4.67	0.23	0.124	(0.209)	0.024	0.101

57	4.75	0.23	0.124	(0.208)	0.024	0.101
58	4.83	0.27	0.142	(0.207)	0.027	0.115
59	4.92	0.27	0.142	(0.206)	0.027	0.115
60	5.00	0.27	0.142	(0.205)	0.027	0.115
61	5.08	0.20	0.107	(0.205)	0.020	0.086
62	5.17	0.20	0.107	(0.204)	0.020	0.086
63	5.25	0.20	0.107	(0.203)	0.020	0.086
64	5.33	0.23	0.124	(0.202)	0.024	0.101
65	5.42	0.23	0.124	(0.201)	0.024	0.101
66	5.50	0.23	0.124	(0.200)	0.024	0.101
67	5.58	0.27	0.142	(0.199)	0.027	0.115
68	5.67	0.27	0.142	(0.198)	0.027	0.115
69	5.75	0.27	0.142	(0.198)	0.027	0.115
70	5.83	0.27	0.142	(0.197)	0.027	0.115
71	5.92	0.27	0.142	(0.196)	0.027	0.115
72	6.00	0.27	0.142	(0.195)	0.027	0.115
73	6.08	0.30	0.160	(0.194)	0.030	0.129
74	6.17	0.30	0.160	(0.193)	0.030	0.129
75	6.25	0.30	0.160	(0.192)	0.030	0.129
76	6.33	0.30	0.160	(0.191)	0.030	0.129
77	6.42	0.30	0.160	(0.191)	0.030	0.129
78	6.50	0.30	0.160	(0.190)	0.030	0.129
79	6.58	0.33	0.178	(0.189)	0.034	0.144
80	6.67	0.33	0.178	(0.188)	0.034	0.144
81	6.75	0.33	0.178	(0.187)	0.034	0.144
82	6.83	0.33	0.178	(0.186)	0.034	0.144
83	6.92	0.33	0.178	(0.186)	0.034	0.144
84	7.00	0.33	0.178	(0.185)	0.034	0.144
85	7.08	0.33	0.178	(0.184)	0.034	0.144
86	7.17	0.33	0.178	(0.183)	0.034	0.144
87	7.25	0.33	0.178	(0.182)	0.034	0.144
88	7.33	0.37	0.195	(0.181)	0.037	0.158
89	7.42	0.37	0.195	(0.180)	0.037	0.158
90	7.50	0.37	0.195	(0.180)	0.037	0.158
91	7.58	0.40	0.213	(0.179)	0.040	0.173
92	7.67	0.40	0.213	(0.178)	0.040	0.173
93	7.75	0.40	0.213	(0.177)	0.040	0.173
94	7.83	0.43	0.231	(0.176)	0.044	0.187
95	7.92	0.43	0.231	(0.176)	0.044	0.187
96	8.00	0.43	0.231	(0.175)	0.044	0.187
97	8.08	0.50	0.266	(0.174)	0.051	0.216
98	8.17	0.50	0.266	(0.173)	0.051	0.216
99	8.25	0.50	0.266	(0.172)	0.051	0.216
100	8.33	0.50	0.266	(0.172)	0.051	0.216
101	8.42	0.50	0.266	(0.171)	0.051	0.216
102	8.50	0.50	0.266	(0.170)	0.051	0.216
103	8.58	0.53	0.284	(0.169)	0.054	0.230
104	8.67	0.53	0.284	(0.168)	0.054	0.230
105	8.75	0.53	0.284	(0.168)	0.054	0.230
106	8.83	0.57	0.302	(0.167)	0.057	0.245
107	8.92	0.57	0.302	(0.166)	0.057	0.245
108	9.00	0.57	0.302	(0.165)	0.057	0.245
109	9.08	0.63	0.337	(0.164)	0.064	0.273

110	9.17	0.63	0.337	(0.164)	0.064	0.273
111	9.25	0.63	0.337	(0.163)	0.064	0.273
112	9.33	0.67	0.355	(0.162)	0.067	0.288
113	9.42	0.67	0.355	(0.161)	0.067	0.288
114	9.50	0.67	0.355	(0.161)	0.067	0.288
115	9.58	0.70	0.373	(0.160)	0.071	0.302
116	9.67	0.70	0.373	(0.159)	0.071	0.302
117	9.75	0.70	0.373	(0.158)	0.071	0.302
118	9.83	0.73	0.391	(0.157)	0.074	0.316
119	9.92	0.73	0.391	(0.157)	0.074	0.316
120	10.00	0.73	0.391	(0.156)	0.074	0.316
121	10.08	0.50	0.266	(0.155)	0.051	0.216
122	10.17	0.50	0.266	(0.154)	0.051	0.216
123	10.25	0.50	0.266	(0.154)	0.051	0.216
124	10.33	0.50	0.266	(0.153)	0.051	0.216
125	10.42	0.50	0.266	(0.152)	0.051	0.216
126	10.50	0.50	0.266	(0.151)	0.051	0.216
127	10.58	0.67	0.355	(0.151)	0.067	0.288
128	10.67	0.67	0.355	(0.150)	0.067	0.288
129	10.75	0.67	0.355	(0.149)	0.067	0.288
130	10.83	0.67	0.355	(0.148)	0.067	0.288
131	10.92	0.67	0.355	(0.148)	0.067	0.288
132	11.00	0.67	0.355	(0.147)	0.067	0.288
133	11.08	0.63	0.337	(0.146)	0.064	0.273
134	11.17	0.63	0.337	(0.146)	0.064	0.273
135	11.25	0.63	0.337	(0.145)	0.064	0.273
136	11.33	0.63	0.337	(0.144)	0.064	0.273
137	11.42	0.63	0.337	(0.143)	0.064	0.273
138	11.50	0.63	0.337	(0.143)	0.064	0.273
139	11.58	0.57	0.302	(0.142)	0.057	0.245
140	11.67	0.57	0.302	(0.141)	0.057	0.245
141	11.75	0.57	0.302	(0.141)	0.057	0.245
142	11.83	0.60	0.320	(0.140)	0.061	0.259
143	11.92	0.60	0.320	(0.139)	0.061	0.259
144	12.00	0.60	0.320	(0.139)	0.061	0.259
145	12.08	0.83	0.444	(0.138)	0.084	0.360
146	12.17	0.83	0.444	(0.137)	0.084	0.360
147	12.25	0.83	0.444	(0.136)	0.084	0.360
148	12.33	0.87	0.462	(0.136)	0.088	0.374
149	12.42	0.87	0.462	(0.135)	0.088	0.374
150	12.50	0.87	0.462	(0.134)	0.088	0.374
151	12.58	0.93	0.497	(0.134)	0.094	0.403
152	12.67	0.93	0.497	(0.133)	0.094	0.403
153	12.75	0.93	0.497	(0.132)	0.094	0.403
154	12.83	0.97	0.515	(0.132)	0.098	0.417
155	12.92	0.97	0.515	(0.131)	0.098	0.417
156	13.00	0.97	0.515	(0.130)	0.098	0.417
157	13.08	1.13	0.604	(0.130)	0.115	0.489
158	13.17	1.13	0.604	(0.129)	0.115	0.489
159	13.25	1.13	0.604	(0.128)	0.115	0.489
160	13.33	1.13	0.604	(0.128)	0.115	0.489
161	13.42	1.13	0.604	(0.127)	0.115	0.489
162	13.50	1.13	0.604	(0.126)	0.115	0.489

163	13.58	0.77	0.408	(0.126)	0.078	0.331
164	13.67	0.77	0.408	(0.125)	0.078	0.331
165	13.75	0.77	0.408	(0.125)	0.078	0.331
166	13.83	0.77	0.408	(0.124)	0.078	0.331
167	13.92	0.77	0.408	(0.123)	0.078	0.331
168	14.00	0.77	0.408	(0.123)	0.078	0.331
169	14.08	0.90	0.480	(0.122)	0.091	0.388
170	14.17	0.90	0.480	(0.121)	0.091	0.388
171	14.25	0.90	0.480	(0.121)	0.091	0.388
172	14.33	0.87	0.462	(0.120)	0.088	0.374
173	14.42	0.87	0.462	(0.120)	0.088	0.374
174	14.50	0.87	0.462	(0.119)	0.088	0.374
175	14.58	0.87	0.462	(0.118)	0.088	0.374
176	14.67	0.87	0.462	(0.118)	0.088	0.374
177	14.75	0.87	0.462	(0.117)	0.088	0.374
178	14.83	0.83	0.444	(0.117)	0.084	0.360
179	14.92	0.83	0.444	(0.116)	0.084	0.360
180	15.00	0.83	0.444	(0.115)	0.084	0.360
181	15.08	0.80	0.426	(0.115)	0.081	0.345
182	15.17	0.80	0.426	(0.114)	0.081	0.345
183	15.25	0.80	0.426	(0.114)	0.081	0.345
184	15.33	0.77	0.408	(0.113)	0.078	0.331
185	15.42	0.77	0.408	(0.112)	0.078	0.331
186	15.50	0.77	0.408	(0.112)	0.078	0.331
187	15.58	0.63	0.337	(0.111)	0.064	0.273
188	15.67	0.63	0.337	(0.111)	0.064	0.273
189	15.75	0.63	0.337	(0.110)	0.064	0.273
190	15.83	0.63	0.337	(0.110)	0.064	0.273
191	15.92	0.63	0.337	(0.109)	0.064	0.273
192	16.00	0.63	0.337	(0.108)	0.064	0.273
193	16.08	0.13	0.071	(0.108)	0.013	0.058
194	16.17	0.13	0.071	(0.107)	0.013	0.058
195	16.25	0.13	0.071	(0.107)	0.013	0.058
196	16.33	0.13	0.071	(0.106)	0.013	0.058
197	16.42	0.13	0.071	(0.106)	0.013	0.058
198	16.50	0.13	0.071	(0.105)	0.013	0.058
199	16.58	0.10	0.053	(0.105)	0.010	0.043
200	16.67	0.10	0.053	(0.104)	0.010	0.043
201	16.75	0.10	0.053	(0.104)	0.010	0.043
202	16.83	0.10	0.053	(0.103)	0.010	0.043
203	16.92	0.10	0.053	(0.103)	0.010	0.043
204	17.00	0.10	0.053	(0.102)	0.010	0.043
205	17.08	0.17	0.089	(0.101)	0.017	0.072
206	17.17	0.17	0.089	(0.101)	0.017	0.072
207	17.25	0.17	0.089	(0.100)	0.017	0.072
208	17.33	0.17	0.089	(0.100)	0.017	0.072
209	17.42	0.17	0.089	(0.099)	0.017	0.072
210	17.50	0.17	0.089	(0.099)	0.017	0.072
211	17.58	0.17	0.089	(0.098)	0.017	0.072
212	17.67	0.17	0.089	(0.098)	0.017	0.072
213	17.75	0.17	0.089	(0.097)	0.017	0.072
214	17.83	0.13	0.071	(0.097)	0.013	0.058
215	17.92	0.13	0.071	(0.097)	0.013	0.058

216	18.00	0.13	0.071	(0.096)	0.013	0.058
217	18.08	0.13	0.071	(0.096)	0.013	0.058
218	18.17	0.13	0.071	(0.095)	0.013	0.058
219	18.25	0.13	0.071	(0.095)	0.013	0.058
220	18.33	0.13	0.071	(0.094)	0.013	0.058
221	18.42	0.13	0.071	(0.094)	0.013	0.058
222	18.50	0.13	0.071	(0.093)	0.013	0.058
223	18.58	0.10	0.053	(0.093)	0.010	0.043
224	18.67	0.10	0.053	(0.092)	0.010	0.043
225	18.75	0.10	0.053	(0.092)	0.010	0.043
226	18.83	0.07	0.036	(0.091)	0.007	0.029
227	18.92	0.07	0.036	(0.091)	0.007	0.029
228	19.00	0.07	0.036	(0.091)	0.007	0.029
229	19.08	0.10	0.053	(0.090)	0.010	0.043
230	19.17	0.10	0.053	(0.090)	0.010	0.043
231	19.25	0.10	0.053	(0.089)	0.010	0.043
232	19.33	0.13	0.071	(0.089)	0.013	0.058
233	19.42	0.13	0.071	(0.089)	0.013	0.058
234	19.50	0.13	0.071	(0.088)	0.013	0.058
235	19.58	0.10	0.053	(0.088)	0.010	0.043
236	19.67	0.10	0.053	(0.087)	0.010	0.043
237	19.75	0.10	0.053	(0.087)	0.010	0.043
238	19.83	0.07	0.036	(0.087)	0.007	0.029
239	19.92	0.07	0.036	(0.086)	0.007	0.029
240	20.00	0.07	0.036	(0.086)	0.007	0.029
241	20.08	0.10	0.053	(0.085)	0.010	0.043
242	20.17	0.10	0.053	(0.085)	0.010	0.043
243	20.25	0.10	0.053	(0.085)	0.010	0.043
244	20.33	0.10	0.053	(0.084)	0.010	0.043
245	20.42	0.10	0.053	(0.084)	0.010	0.043
246	20.50	0.10	0.053	(0.084)	0.010	0.043
247	20.58	0.10	0.053	(0.083)	0.010	0.043
248	20.67	0.10	0.053	(0.083)	0.010	0.043
249	20.75	0.10	0.053	(0.082)	0.010	0.043
250	20.83	0.07	0.036	(0.082)	0.007	0.029
251	20.92	0.07	0.036	(0.082)	0.007	0.029
252	21.00	0.07	0.036	(0.081)	0.007	0.029
253	21.08	0.10	0.053	(0.081)	0.010	0.043
254	21.17	0.10	0.053	(0.081)	0.010	0.043
255	21.25	0.10	0.053	(0.081)	0.010	0.043
256	21.33	0.07	0.036	(0.080)	0.007	0.029
257	21.42	0.07	0.036	(0.080)	0.007	0.029
258	21.50	0.07	0.036	(0.080)	0.007	0.029
259	21.58	0.10	0.053	(0.079)	0.010	0.043
260	21.67	0.10	0.053	(0.079)	0.010	0.043
261	21.75	0.10	0.053	(0.079)	0.010	0.043
262	21.83	0.07	0.036	(0.078)	0.007	0.029
263	21.92	0.07	0.036	(0.078)	0.007	0.029
264	22.00	0.07	0.036	(0.078)	0.007	0.029
265	22.08	0.10	0.053	(0.078)	0.010	0.043
266	22.17	0.10	0.053	(0.077)	0.010	0.043
267	22.25	0.10	0.053	(0.077)	0.010	0.043
268	22.33	0.07	0.036	(0.077)	0.007	0.029

269	22.42	0.07	0.036	(	0.077)	0.007	0.029
270	22.50	0.07	0.036	(	0.077)	0.007	0.029
271	22.58	0.07	0.036	(	0.076)	0.007	0.029
272	22.67	0.07	0.036	(	0.076)	0.007	0.029
273	22.75	0.07	0.036	(	0.076)	0.007	0.029
274	22.83	0.07	0.036	(	0.076)	0.007	0.029
275	22.92	0.07	0.036	(	0.075)	0.007	0.029
276	23.00	0.07	0.036	(	0.075)	0.007	0.029
277	23.08	0.07	0.036	(	0.075)	0.007	0.029
278	23.17	0.07	0.036	(	0.075)	0.007	0.029
279	23.25	0.07	0.036	(	0.075)	0.007	0.029
280	23.33	0.07	0.036	(	0.075)	0.007	0.029
281	23.42	0.07	0.036	(	0.074)	0.007	0.029
282	23.50	0.07	0.036	(	0.074)	0.007	0.029
283	23.58	0.07	0.036	(	0.074)	0.007	0.029
284	23.67	0.07	0.036	(	0.074)	0.007	0.029
285	23.75	0.07	0.036	(	0.074)	0.007	0.029
286	23.83	0.07	0.036	(	0.074)	0.007	0.029
287	23.92	0.07	0.036	(	0.074)	0.007	0.029
288	24.00	0.07	0.036	(	0.074)	0.007	0.029

(Loss Rate Not Used)

Sum = 100.0 Sum = 43.2

Flood volume = Effective rainfall 3.60(In)
times area 0.6(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 0.84(In)
Total soil loss = 0.039(Ac.Ft)
Total rainfall = 4.44(In)
Flood volume = 7180.2 Cubic Feet
Total soil loss = 1684.2 Cubic Feet

Peak flow rate of this hydrograph = 0.271(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.01	Q	|	|	|	|
0+10	0.0002	0.02	Q	|	|	|	|
0+15	0.0003	0.02	Q	|	|	|	|
0+20	0.0005	0.02	Q	|	|	|	|
0+25	0.0006	0.02	Q	|	|	|	|
0+30	0.0008	0.02	Q	|	|	|	|
0+35	0.0009	0.02	Q	|	|	|	|
0+40	0.0011	0.02	Q	|	|	|	|
0+45	0.0013	0.02	Q	|	|	|	|
0+50	0.0015	0.03	Q	|	|	|	|
0+55	0.0017	0.03	Q	|	|	|	|
1+ 0	0.0019	0.03	Q	|	|	|	|

1+ 5	0.0021	0.03	Q	|	|	|	|
1+10	0.0023	0.02	Q	|	|	|	|
1+15	0.0024	0.02	Q	|	|	|	|
1+20	0.0026	0.02	Q	|	|	|	|
1+25	0.0028	0.02	Q	|	|	|	|
1+30	0.0029	0.02	Q	|	|	|	|
1+35	0.0031	0.02	Q	|	|	|	|
1+40	0.0033	0.02	Q	|	|	|	|
1+45	0.0034	0.02	Q	|	|	|	|
1+50	0.0036	0.03	Q	|	|	|	|
1+55	0.0038	0.03	Q	|	|	|	|
2+ 0	0.0041	0.03	Q	|	|	|	|
2+ 5	0.0043	0.03	QV	|	|	|	|
2+10	0.0045	0.03	QV	|	|	|	|
2+15	0.0047	0.03	QV	|	|	|	|
2+20	0.0049	0.03	QV	|	|	|	|
2+25	0.0052	0.03	QV	|	|	|	|
2+30	0.0054	0.03	QV	|	|	|	|
2+35	0.0056	0.04	QV	|	|	|	|
2+40	0.0059	0.04	QV	|	|	|	|
2+45	0.0062	0.04	QV	|	|	|	|
2+50	0.0065	0.04	QV	|	|	|	|
2+55	0.0067	0.04	QV	|	|	|	|
3+ 0	0.0070	0.04	QV	|	|	|	|
3+ 5	0.0073	0.04	QV	|	|	|	|
3+10	0.0076	0.04	QV	|	|	|	|
3+15	0.0078	0.04	QV	|	|	|	|
3+20	0.0081	0.04	QV	|	|	|	|
3+25	0.0084	0.04	Q V	|	|	|	|
3+30	0.0087	0.04	Q V	|	|	|	|
3+35	0.0089	0.04	Q V	|	|	|	|
3+40	0.0092	0.04	Q V	|	|	|	|
3+45	0.0095	0.04	Q V	|	|	|	|
3+50	0.0098	0.05	Q V	|	|	|	|
3+55	0.0101	0.05	Q V	|	|	|	|
4+ 0	0.0105	0.05	Q V	|	|	|	|
4+ 5	0.0108	0.05	Q V	|	|	|	|
4+10	0.0111	0.05	Q V	|	|	|	|
4+15	0.0114	0.05	Q V	|	|	|	|
4+20	0.0118	0.05	Q V	|	|	|	|
4+25	0.0122	0.06	Q V	|	|	|	|
4+30	0.0126	0.06	Q V	|	|	|	|
4+35	0.0130	0.06	Q V	|	|	|	|
4+40	0.0134	0.06	Q V	|	|	|	|
4+45	0.0137	0.06	Q V	|	|	|	|
4+50	0.0142	0.06	Q V	|	|	|	|
4+55	0.0146	0.06	Q V	|	|	|	|
5+ 0	0.0150	0.06	Q V	|	|	|	|
5+ 5	0.0154	0.05	Q V	|	|	|	|
5+10	0.0157	0.05	Q V	|	|	|	|
5+15	0.0161	0.05	Q V	|	|	|	|
5+20	0.0164	0.05	Q V	|	|	|	|
5+25	0.0168	0.06	Q V	|	|	|	|

5+30	0.0172	0.06	Q	V	|	|	|	|
5+35	0.0176	0.06	Q	V	|	|	|	|
5+40	0.0181	0.06	Q	V	|	|	|	|
5+45	0.0185	0.06	Q	V	|	|	|	|
5+50	0.0189	0.06	Q	V	|	|	|	|
5+55	0.0194	0.06	Q	V	|	|	|	|
6+ 0	0.0198	0.06	Q	V	|	|	|	|
6+ 5	0.0203	0.07	Q	V	|	|	|	|
6+10	0.0208	0.07	Q	V	|	|	|	|
6+15	0.0213	0.07	Q	V	|	|	|	|
6+20	0.0218	0.07	Q	V	|	|	|	|
6+25	0.0223	0.07	Q	V	|	|	|	|
6+30	0.0228	0.07	Q	V	|	|	|	|
6+35	0.0233	0.08	Q	V	|	|	|	|
6+40	0.0239	0.08	Q	V	|	|	|	|
6+45	0.0244	0.08	Q	V	|	|	|	|
6+50	0.0250	0.08	Q	V	|	|	|	|
6+55	0.0255	0.08	Q	V	|	|	|	|
7+ 0	0.0261	0.08	Q	V	|	|	|	|
7+ 5	0.0266	0.08	Q	V	|	|	|	|
7+10	0.0272	0.08	Q	V	|	|	|	|
7+15	0.0277	0.08	Q	V	|	|	|	|
7+20	0.0283	0.09	Q	V	|	|	|	|
7+25	0.0289	0.09	Q	V	|	|	|	|
7+30	0.0295	0.09	Q	V	|	|	|	|
7+35	0.0302	0.09	Q	V	|	|	|	|
7+40	0.0308	0.10	Q	V	|	|	|	|
7+45	0.0315	0.10	Q	V	|	|	|	|
7+50	0.0322	0.10	Q	V	|	|	|	|
7+55	0.0329	0.10	Q	V	|	|	|	|
8+ 0	0.0336	0.10	Q	V	|	|	|	|
8+ 5	0.0344	0.12	Q	V	|	|	|	|
8+10	0.0352	0.12	Q	V	|	|	|	|
8+15	0.0360	0.12	Q	V	|	|	|	|
8+20	0.0369	0.12	Q	V	|	|	|	|
8+25	0.0377	0.12	Q	V	|	|	|	|
8+30	0.0385	0.12	Q	V	|	|	|	|
8+35	0.0394	0.13	Q	V	|	|	|	|
8+40	0.0403	0.13	Q	V	|	|	|	|
8+45	0.0411	0.13	Q	V	|	|	|	|
8+50	0.0421	0.13	Q	V	|	|	|	|
8+55	0.0430	0.14	Q	V	|	|	|	|
9+ 0	0.0439	0.14	Q	V	|	|	|	|
9+ 5	0.0449	0.15	Q	V	|	|	|	|
9+10	0.0460	0.15	Q	|	V	|	|	|
9+15	0.0470	0.15	Q	|	V	|	|	|
9+20	0.0481	0.16	Q	|	V	|	|	|
9+25	0.0492	0.16	Q	|	V	|	|	|
9+30	0.0503	0.16	Q	|	V	|	|	|
9+35	0.0514	0.17	Q	|	V	|	|	|
9+40	0.0526	0.17	Q	|	V	|	|	|
9+45	0.0538	0.17	Q	|	V	|	|	|
9+50	0.0549	0.17	Q	|	V	|	|	|

9+55	0.0562	0.18	Q	| V	|	|	|
10+ 0	0.0574	0.18	Q	| V	|	|	|
10+ 5	0.0583	0.13	Q	| V	|	|	|
10+10	0.0591	0.12	Q	| V	|	|	|
10+15	0.0599	0.12	Q	| V	|	|	|
10+20	0.0608	0.12	Q	| V	|	|	|
10+25	0.0616	0.12	Q	| V	|	|	|
10+30	0.0624	0.12	Q	| V	|	|	|
10+35	0.0634	0.15	Q	| V	|	|	|
10+40	0.0645	0.16	Q	| V	|	|	|
10+45	0.0656	0.16	Q	| V	|	|	|
10+50	0.0667	0.16	Q	| V	|	|	|
10+55	0.0678	0.16	Q	| V	|	|	|
11+ 0	0.0689	0.16	Q	| V	|	|	|
11+ 5	0.0700	0.15	Q	| V	|	|	|
11+10	0.0710	0.15	Q	| V	|	|	|
11+15	0.0721	0.15	Q	| V	|	|	|
11+20	0.0731	0.15	Q	| V	|	|	|
11+25	0.0742	0.15	Q	| V	|	|	|
11+30	0.0752	0.15	Q	| V	|	|	|
11+35	0.0762	0.14	Q	| V	|	|	|
11+40	0.0771	0.14	Q	| V	|	|	|
11+45	0.0780	0.14	Q	| V	|	|	|
11+50	0.0790	0.14	Q	| V	|	|	|
11+55	0.0800	0.14	Q	| V	|	|	|
12+ 0	0.0810	0.14	Q	| V	|	|	|
12+ 5	0.0823	0.18	Q	| V	|	|	|
12+10	0.0836	0.20	Q	| V	|	|	|
12+15	0.0850	0.20	Q	| V	|	|	|
12+20	0.0864	0.21	Q	| V	|	|	|
12+25	0.0879	0.21	Q	| V	|	|	|
12+30	0.0893	0.21	Q	| V	|	|	|
12+35	0.0908	0.22	Q	| V	|	|	|
12+40	0.0923	0.22	Q	| V	|	|	|
12+45	0.0939	0.22	Q	| V	|	|	|
12+50	0.0955	0.23	Q	| V	|	|	|
12+55	0.0970	0.23	Q	| V	|	|	|
13+ 0	0.0986	0.23	Q	| V	|	|	|
13+ 5	0.1004	0.26	|Q	| V	|	|	|
13+10	0.1023	0.27	|Q	| V	|	|	|
13+15	0.1042	0.27	|Q	| V	|	|	|
13+20	0.1060	0.27	|Q	| V	|	|	|
13+25	0.1079	0.27	|Q	| V	|	|	|
13+30	0.1098	0.27	|Q	| V	|	|	|
13+35	0.1112	0.21	Q	| V	|	|	|
13+40	0.1125	0.18	Q	| V	|	|	|
13+45	0.1137	0.18	Q	| V	|	|	|
13+50	0.1150	0.18	Q	| V	|	|	|
13+55	0.1163	0.18	Q	| V	|	|	|
14+ 0	0.1175	0.18	Q	| V	|	|	|
14+ 5	0.1189	0.21	Q	| V	|	|	|
14+10	0.1204	0.22	Q	| V	|	|	|
14+15	0.1219	0.22	Q	| V	|	|	|

14+20	0.1234	0.21	Q	|	|	V|	|
14+25	0.1248	0.21	Q	|	|	V	|
14+30	0.1262	0.21	Q	|	|	V	|
14+35	0.1276	0.21	Q	|	|	V	|
14+40	0.1291	0.21	Q	|	|	|V	|
14+45	0.1305	0.21	Q	|	|	|V	|
14+50	0.1319	0.20	Q	|	|	| V	|
14+55	0.1333	0.20	Q	|	|	| V	|
15+ 0	0.1346	0.20	Q	|	|	| V	|
15+ 5	0.1360	0.19	Q	|	|	| V	|
15+10	0.1373	0.19	Q	|	|	| V	|
15+15	0.1386	0.19	Q	|	|	| V	|
15+20	0.1399	0.19	Q	|	|	| V	|
15+25	0.1411	0.18	Q	|	|	| V	|
15+30	0.1424	0.18	Q	|	|	| V	|
15+35	0.1435	0.16	Q	|	|	| V	|
15+40	0.1446	0.15	Q	|	|	| V	|
15+45	0.1456	0.15	Q	|	|	| V	|
15+50	0.1466	0.15	Q	|	|	| V	|
15+55	0.1477	0.15	Q	|	|	| V	|
16+ 0	0.1487	0.15	Q	|	|	| V	|
16+ 5	0.1492	0.06	Q	|	|	| V	|
16+10	0.1494	0.03	Q	|	|	| V	|
16+15	0.1496	0.03	Q	|	|	| V	|
16+20	0.1498	0.03	Q	|	|	| V	|
16+25	0.1501	0.03	Q	|	|	| V	|
16+30	0.1503	0.03	Q	|	|	| V	|
16+35	0.1504	0.03	Q	|	|	| V	|
16+40	0.1506	0.02	Q	|	|	| V	|
16+45	0.1508	0.02	Q	|	|	| V	|
16+50	0.1509	0.02	Q	|	|	| V	|
16+55	0.1511	0.02	Q	|	|	| V	|
17+ 0	0.1513	0.02	Q	|	|	| V	|
17+ 5	0.1515	0.04	Q	|	|	| V	|
17+10	0.1518	0.04	Q	|	|	| V	|
17+15	0.1521	0.04	Q	|	|	| V	|
17+20	0.1523	0.04	Q	|	|	| V	|
17+25	0.1526	0.04	Q	|	|	| V	|
17+30	0.1529	0.04	Q	|	|	| V	|
17+35	0.1532	0.04	Q	|	|	| V	|
17+40	0.1534	0.04	Q	|	|	| V	|
17+45	0.1537	0.04	Q	|	|	| V	|
17+50	0.1540	0.03	Q	|	|	| V	|
17+55	0.1542	0.03	Q	|	|	| V	|
18+ 0	0.1544	0.03	Q	|	|	| V	|
18+ 5	0.1546	0.03	Q	|	|	| V	|
18+10	0.1548	0.03	Q	|	|	| V	|
18+15	0.1551	0.03	Q	|	|	| V	|
18+20	0.1553	0.03	Q	|	|	| V	|
18+25	0.1555	0.03	Q	|	|	| V	|
18+30	0.1557	0.03	Q	|	|	| V	|
18+35	0.1559	0.03	Q	|	|	| V	|
18+40	0.1561	0.02	Q	|	|	| V	|

18+45	0.1562	0.02	Q	|	|	|	V |
18+50	0.1563	0.02	Q	|	|	|	V |
18+55	0.1565	0.02	Q	|	|	|	V |
19+ 0	0.1566	0.02	Q	|	|	|	V |
19+ 5	0.1567	0.02	Q	|	|	|	V |
19+10	0.1569	0.02	Q	|	|	|	V |
19+15	0.1570	0.02	Q	|	|	|	V |
19+20	0.1572	0.03	Q	|	|	|	V |
19+25	0.1575	0.03	Q	|	|	|	V |
19+30	0.1577	0.03	Q	|	|	|	V |
19+35	0.1579	0.03	Q	|	|	|	V |
19+40	0.1580	0.02	Q	|	|	|	V |
19+45	0.1582	0.02	Q	|	|	|	V |
19+50	0.1583	0.02	Q	|	|	|	V |
19+55	0.1584	0.02	Q	|	|	|	V |
20+ 0	0.1585	0.02	Q	|	|	|	V |
20+ 5	0.1587	0.02	Q	|	|	|	V |
20+10	0.1589	0.02	Q	|	|	|	V |
20+15	0.1590	0.02	Q	|	|	|	V |
20+20	0.1592	0.02	Q	|	|	|	V |
20+25	0.1594	0.02	Q	|	|	|	V |
20+30	0.1595	0.02	Q	|	|	|	V |
20+35	0.1597	0.02	Q	|	|	|	V |
20+40	0.1598	0.02	Q	|	|	|	V |
20+45	0.1600	0.02	Q	|	|	|	V |
20+50	0.1601	0.02	Q	|	|	|	V |
20+55	0.1602	0.02	Q	|	|	|	V |
21+ 0	0.1604	0.02	Q	|	|	|	V |
21+ 5	0.1605	0.02	Q	|	|	|	V |
21+10	0.1607	0.02	Q	|	|	|	V |
21+15	0.1608	0.02	Q	|	|	|	V|
21+20	0.1610	0.02	Q	|	|	|	V|
21+25	0.1611	0.02	Q	|	|	|	V|
21+30	0.1612	0.02	Q	|	|	|	V|
21+35	0.1613	0.02	Q	|	|	|	V|
21+40	0.1615	0.02	Q	|	|	|	V|
21+45	0.1617	0.02	Q	|	|	|	V|
21+50	0.1618	0.02	Q	|	|	|	V|
21+55	0.1619	0.02	Q	|	|	|	V|
22+ 0	0.1620	0.02	Q	|	|	|	V|
22+ 5	0.1622	0.02	Q	|	|	|	V|
22+10	0.1623	0.02	Q	|	|	|	V|
22+15	0.1625	0.02	Q	|	|	|	V|
22+20	0.1626	0.02	Q	|	|	|	V|
22+25	0.1627	0.02	Q	|	|	|	V|
22+30	0.1628	0.02	Q	|	|	|	V|
22+35	0.1629	0.02	Q	|	|	|	V|
22+40	0.1630	0.02	Q	|	|	|	V|
22+45	0.1632	0.02	Q	|	|	|	V|
22+50	0.1633	0.02	Q	|	|	|	V|
22+55	0.1634	0.02	Q	|	|	|	V|
23+ 0	0.1635	0.02	Q	|	|	|	V|
23+ 5	0.1636	0.02	Q	|	|	|	V|

23+10	0.1637	0.02	Q	|	|	|	V|
23+15	0.1638	0.02	Q	|	|	|	V|
23+20	0.1639	0.02	Q	|	|	|	V|
23+25	0.1640	0.02	Q	|	|	|	V|
23+30	0.1641	0.02	Q	|	|	|	V|
23+35	0.1643	0.02	Q	|	|	|	V|
23+40	0.1644	0.02	Q	|	|	|	V|
23+45	0.1645	0.02	Q	|	|	|	V|
23+50	0.1646	0.02	Q	|	|	|	V|
23+55	0.1647	0.02	Q	|	|	|	V|
24+ 0	0.1648	0.02	Q	|	|	|	V|
24+ 5	0.1648	0.00	Q	|	|	|	V|

AREA EE1

U n i t H y d r o g r a p h A n a l y s i s

Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014, Version 9.0
Study date 02/05/24 File: AREE124100.out

++

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 6279

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

PROPOSED CONDITION: 100YR HYDROLOGY
AREE1

Drainage Area = 0.55(Ac.) = 0.001 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 0.55(Ac.) = 0.001 Sq. Mi.
Length along longest watercourse = 308.00(Ft.)
Length along longest watercourse measured to centroid = 154.00(Ft.)
Length along longest watercourse = 0.058 Mi.
Length along longest watercourse measured to centroid = 0.029 Mi.
Difference in elevation = 2.50(Ft.)
Slope along watercourse = 42.8571 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.016 Hr.
Lag time = 0.94 Min.
25% of lag time = 0.23 Min.
40% of lag time = 0.38 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.55	1.16	0.64

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
0.55	4.44	2.44

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.160(In)
Area Averaged 100-Year Rainfall = 4.440(In)

Point rain (area averaged) = 4.440(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 4.440(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
0.550	32.00	0.840

Total Area Entered = 0.55(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
32.0	32.0	0.742	0.840	0.181	1.000	0.181
					Sum (F) =	0.181

Area averaged mean soil loss (F) (In/Hr) = 0.181
Minimum soil loss rate ((In/Hr)) = 0.091
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.230

U n i t H y d r o g r a p h
DESERT S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	533.206	72.708	0.403
2	0.167	1066.413	27.292	0.151
		Sum = 100.000	Sum=	0.554

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max		Low	Effective (In/Hr)
1	0.08	0.07	0.036	(0.321)	0.008	0.027
2	0.17	0.07	0.036	(0.320)	0.008	0.027
3	0.25	0.07	0.036	(0.318)	0.008	0.027

4	0.33	0.10	0.053	(0.317)	0.012	0.041
5	0.42	0.10	0.053	(0.316)	0.012	0.041
6	0.50	0.10	0.053	(0.315)	0.012	0.041
7	0.58	0.10	0.053	(0.314)	0.012	0.041
8	0.67	0.10	0.053	(0.312)	0.012	0.041
9	0.75	0.10	0.053	(0.311)	0.012	0.041
10	0.83	0.13	0.071	(0.310)	0.016	0.055
11	0.92	0.13	0.071	(0.309)	0.016	0.055
12	1.00	0.13	0.071	(0.307)	0.016	0.055
13	1.08	0.10	0.053	(0.306)	0.012	0.041
14	1.17	0.10	0.053	(0.305)	0.012	0.041
15	1.25	0.10	0.053	(0.304)	0.012	0.041
16	1.33	0.10	0.053	(0.303)	0.012	0.041
17	1.42	0.10	0.053	(0.301)	0.012	0.041
18	1.50	0.10	0.053	(0.300)	0.012	0.041
19	1.58	0.10	0.053	(0.299)	0.012	0.041
20	1.67	0.10	0.053	(0.298)	0.012	0.041
21	1.75	0.10	0.053	(0.297)	0.012	0.041
22	1.83	0.13	0.071	(0.295)	0.016	0.055
23	1.92	0.13	0.071	(0.294)	0.016	0.055
24	2.00	0.13	0.071	(0.293)	0.016	0.055
25	2.08	0.13	0.071	(0.292)	0.016	0.055
26	2.17	0.13	0.071	(0.291)	0.016	0.055
27	2.25	0.13	0.071	(0.289)	0.016	0.055
28	2.33	0.13	0.071	(0.288)	0.016	0.055
29	2.42	0.13	0.071	(0.287)	0.016	0.055
30	2.50	0.13	0.071	(0.286)	0.016	0.055
31	2.58	0.17	0.089	(0.285)	0.020	0.068
32	2.67	0.17	0.089	(0.284)	0.020	0.068
33	2.75	0.17	0.089	(0.282)	0.020	0.068
34	2.83	0.17	0.089	(0.281)	0.020	0.068
35	2.92	0.17	0.089	(0.280)	0.020	0.068
36	3.00	0.17	0.089	(0.279)	0.020	0.068
37	3.08	0.17	0.089	(0.278)	0.020	0.068
38	3.17	0.17	0.089	(0.277)	0.020	0.068
39	3.25	0.17	0.089	(0.275)	0.020	0.068
40	3.33	0.17	0.089	(0.274)	0.020	0.068
41	3.42	0.17	0.089	(0.273)	0.020	0.068
42	3.50	0.17	0.089	(0.272)	0.020	0.068
43	3.58	0.17	0.089	(0.271)	0.020	0.068
44	3.67	0.17	0.089	(0.270)	0.020	0.068
45	3.75	0.17	0.089	(0.269)	0.020	0.068
46	3.83	0.20	0.107	(0.268)	0.025	0.082
47	3.92	0.20	0.107	(0.266)	0.025	0.082
48	4.00	0.20	0.107	(0.265)	0.025	0.082
49	4.08	0.20	0.107	(0.264)	0.025	0.082
50	4.17	0.20	0.107	(0.263)	0.025	0.082
51	4.25	0.20	0.107	(0.262)	0.025	0.082
52	4.33	0.23	0.124	(0.261)	0.029	0.096
53	4.42	0.23	0.124	(0.260)	0.029	0.096
54	4.50	0.23	0.124	(0.259)	0.029	0.096
55	4.58	0.23	0.124	(0.257)	0.029	0.096
56	4.67	0.23	0.124	(0.256)	0.029	0.096

57	4.75	0.23	0.124	(0.255)	0.029	0.096
58	4.83	0.27	0.142	(0.254)	0.033	0.109
59	4.92	0.27	0.142	(0.253)	0.033	0.109
60	5.00	0.27	0.142	(0.252)	0.033	0.109
61	5.08	0.20	0.107	(0.251)	0.025	0.082
62	5.17	0.20	0.107	(0.250)	0.025	0.082
63	5.25	0.20	0.107	(0.249)	0.025	0.082
64	5.33	0.23	0.124	(0.248)	0.029	0.096
65	5.42	0.23	0.124	(0.246)	0.029	0.096
66	5.50	0.23	0.124	(0.245)	0.029	0.096
67	5.58	0.27	0.142	(0.244)	0.033	0.109
68	5.67	0.27	0.142	(0.243)	0.033	0.109
69	5.75	0.27	0.142	(0.242)	0.033	0.109
70	5.83	0.27	0.142	(0.241)	0.033	0.109
71	5.92	0.27	0.142	(0.240)	0.033	0.109
72	6.00	0.27	0.142	(0.239)	0.033	0.109
73	6.08	0.30	0.160	(0.238)	0.037	0.123
74	6.17	0.30	0.160	(0.237)	0.037	0.123
75	6.25	0.30	0.160	(0.236)	0.037	0.123
76	6.33	0.30	0.160	(0.235)	0.037	0.123
77	6.42	0.30	0.160	(0.234)	0.037	0.123
78	6.50	0.30	0.160	(0.233)	0.037	0.123
79	6.58	0.33	0.178	(0.232)	0.041	0.137
80	6.67	0.33	0.178	(0.231)	0.041	0.137
81	6.75	0.33	0.178	(0.230)	0.041	0.137
82	6.83	0.33	0.178	(0.228)	0.041	0.137
83	6.92	0.33	0.178	(0.227)	0.041	0.137
84	7.00	0.33	0.178	(0.226)	0.041	0.137
85	7.08	0.33	0.178	(0.225)	0.041	0.137
86	7.17	0.33	0.178	(0.224)	0.041	0.137
87	7.25	0.33	0.178	(0.223)	0.041	0.137
88	7.33	0.37	0.195	(0.222)	0.045	0.150
89	7.42	0.37	0.195	(0.221)	0.045	0.150
90	7.50	0.37	0.195	(0.220)	0.045	0.150
91	7.58	0.40	0.213	(0.219)	0.049	0.164
92	7.67	0.40	0.213	(0.218)	0.049	0.164
93	7.75	0.40	0.213	(0.217)	0.049	0.164
94	7.83	0.43	0.231	(0.216)	0.053	0.178
95	7.92	0.43	0.231	(0.215)	0.053	0.178
96	8.00	0.43	0.231	(0.214)	0.053	0.178
97	8.08	0.50	0.266	(0.213)	0.061	0.205
98	8.17	0.50	0.266	(0.212)	0.061	0.205
99	8.25	0.50	0.266	(0.211)	0.061	0.205
100	8.33	0.50	0.266	(0.210)	0.061	0.205
101	8.42	0.50	0.266	(0.209)	0.061	0.205
102	8.50	0.50	0.266	(0.208)	0.061	0.205
103	8.58	0.53	0.284	(0.207)	0.065	0.219
104	8.67	0.53	0.284	(0.206)	0.065	0.219
105	8.75	0.53	0.284	(0.205)	0.065	0.219
106	8.83	0.57	0.302	(0.204)	0.069	0.232
107	8.92	0.57	0.302	(0.203)	0.069	0.232
108	9.00	0.57	0.302	(0.203)	0.069	0.232
109	9.08	0.63	0.337	(0.202)	0.078	0.260

110	9.17	0.63	0.337	(0.201)	0.078	0.260
111	9.25	0.63	0.337	(0.200)	0.078	0.260
112	9.33	0.67	0.355	(0.199)	0.082	0.274
113	9.42	0.67	0.355	(0.198)	0.082	0.274
114	9.50	0.67	0.355	(0.197)	0.082	0.274
115	9.58	0.70	0.373	(0.196)	0.086	0.287
116	9.67	0.70	0.373	(0.195)	0.086	0.287
117	9.75	0.70	0.373	(0.194)	0.086	0.287
118	9.83	0.73	0.391	(0.193)	0.090	0.301
119	9.92	0.73	0.391	(0.192)	0.090	0.301
120	10.00	0.73	0.391	(0.191)	0.090	0.301
121	10.08	0.50	0.266	(0.190)	0.061	0.205
122	10.17	0.50	0.266	(0.189)	0.061	0.205
123	10.25	0.50	0.266	(0.188)	0.061	0.205
124	10.33	0.50	0.266	(0.188)	0.061	0.205
125	10.42	0.50	0.266	(0.187)	0.061	0.205
126	10.50	0.50	0.266	(0.186)	0.061	0.205
127	10.58	0.67	0.355	(0.185)	0.082	0.274
128	10.67	0.67	0.355	(0.184)	0.082	0.274
129	10.75	0.67	0.355	(0.183)	0.082	0.274
130	10.83	0.67	0.355	(0.182)	0.082	0.274
131	10.92	0.67	0.355	(0.181)	0.082	0.274
132	11.00	0.67	0.355	(0.180)	0.082	0.274
133	11.08	0.63	0.337	(0.179)	0.078	0.260
134	11.17	0.63	0.337	(0.179)	0.078	0.260
135	11.25	0.63	0.337	(0.178)	0.078	0.260
136	11.33	0.63	0.337	(0.177)	0.078	0.260
137	11.42	0.63	0.337	(0.176)	0.078	0.260
138	11.50	0.63	0.337	(0.175)	0.078	0.260
139	11.58	0.57	0.302	(0.174)	0.069	0.232
140	11.67	0.57	0.302	(0.173)	0.069	0.232
141	11.75	0.57	0.302	(0.172)	0.069	0.232
142	11.83	0.60	0.320	(0.172)	0.074	0.246
143	11.92	0.60	0.320	(0.171)	0.074	0.246
144	12.00	0.60	0.320	(0.170)	0.074	0.246
145	12.08	0.83	0.444	(0.169)	0.102	0.342
146	12.17	0.83	0.444	(0.168)	0.102	0.342
147	12.25	0.83	0.444	(0.167)	0.102	0.342
148	12.33	0.87	0.462	(0.166)	0.106	0.356
149	12.42	0.87	0.462	(0.166)	0.106	0.356
150	12.50	0.87	0.462	(0.165)	0.106	0.356
151	12.58	0.93	0.497	(0.164)	0.114	0.383
152	12.67	0.93	0.497	(0.163)	0.114	0.383
153	12.75	0.93	0.497	(0.162)	0.114	0.383
154	12.83	0.97	0.515	(0.162)	0.118	0.397
155	12.92	0.97	0.515	(0.161)	0.118	0.397
156	13.00	0.97	0.515	(0.160)	0.118	0.397
157	13.08	1.13	0.604	(0.159)	0.139	0.465
158	13.17	1.13	0.604	(0.158)	0.139	0.465
159	13.25	1.13	0.604	(0.157)	0.139	0.465
160	13.33	1.13	0.604	(0.157)	0.139	0.465
161	13.42	1.13	0.604	(0.156)	0.139	0.465
162	13.50	1.13	0.604	(0.155)	0.139	0.465

163	13.58	0.77	0.408	(0.154)	0.094	0.315
164	13.67	0.77	0.408	(0.153)	0.094	0.315
165	13.75	0.77	0.408	(0.153)	0.094	0.315
166	13.83	0.77	0.408	(0.152)	0.094	0.315
167	13.92	0.77	0.408	(0.151)	0.094	0.315
168	14.00	0.77	0.408	(0.150)	0.094	0.315
169	14.08	0.90	0.480	(0.150)	0.110	0.369
170	14.17	0.90	0.480	(0.149)	0.110	0.369
171	14.25	0.90	0.480	(0.148)	0.110	0.369
172	14.33	0.87	0.462	(0.147)	0.106	0.356
173	14.42	0.87	0.462	(0.147)	0.106	0.356
174	14.50	0.87	0.462	(0.146)	0.106	0.356
175	14.58	0.87	0.462	(0.145)	0.106	0.356
176	14.67	0.87	0.462	(0.144)	0.106	0.356
177	14.75	0.87	0.462	(0.144)	0.106	0.356
178	14.83	0.83	0.444	(0.143)	0.102	0.342
179	14.92	0.83	0.444	(0.142)	0.102	0.342
180	15.00	0.83	0.444	(0.141)	0.102	0.342
181	15.08	0.80	0.426	(0.141)	0.098	0.328
182	15.17	0.80	0.426	(0.140)	0.098	0.328
183	15.25	0.80	0.426	(0.139)	0.098	0.328
184	15.33	0.77	0.408	(0.139)	0.094	0.315
185	15.42	0.77	0.408	(0.138)	0.094	0.315
186	15.50	0.77	0.408	(0.137)	0.094	0.315
187	15.58	0.63	0.337	(0.136)	0.078	0.260
188	15.67	0.63	0.337	(0.136)	0.078	0.260
189	15.75	0.63	0.337	(0.135)	0.078	0.260
190	15.83	0.63	0.337	(0.134)	0.078	0.260
191	15.92	0.63	0.337	(0.134)	0.078	0.260
192	16.00	0.63	0.337	(0.133)	0.078	0.260
193	16.08	0.13	0.071	(0.132)	0.016	0.055
194	16.17	0.13	0.071	(0.132)	0.016	0.055
195	16.25	0.13	0.071	(0.131)	0.016	0.055
196	16.33	0.13	0.071	(0.130)	0.016	0.055
197	16.42	0.13	0.071	(0.130)	0.016	0.055
198	16.50	0.13	0.071	(0.129)	0.016	0.055
199	16.58	0.10	0.053	(0.128)	0.012	0.041
200	16.67	0.10	0.053	(0.128)	0.012	0.041
201	16.75	0.10	0.053	(0.127)	0.012	0.041
202	16.83	0.10	0.053	(0.126)	0.012	0.041
203	16.92	0.10	0.053	(0.126)	0.012	0.041
204	17.00	0.10	0.053	(0.125)	0.012	0.041
205	17.08	0.17	0.089	(0.124)	0.020	0.068
206	17.17	0.17	0.089	(0.124)	0.020	0.068
207	17.25	0.17	0.089	(0.123)	0.020	0.068
208	17.33	0.17	0.089	(0.123)	0.020	0.068
209	17.42	0.17	0.089	(0.122)	0.020	0.068
210	17.50	0.17	0.089	(0.121)	0.020	0.068
211	17.58	0.17	0.089	(0.121)	0.020	0.068
212	17.67	0.17	0.089	(0.120)	0.020	0.068
213	17.75	0.17	0.089	(0.120)	0.020	0.068
214	17.83	0.13	0.071	(0.119)	0.016	0.055
215	17.92	0.13	0.071	(0.118)	0.016	0.055

216	18.00	0.13	0.071	(0.118)	0.016	0.055
217	18.08	0.13	0.071	(0.117)	0.016	0.055
218	18.17	0.13	0.071	(0.117)	0.016	0.055
219	18.25	0.13	0.071	(0.116)	0.016	0.055
220	18.33	0.13	0.071	(0.115)	0.016	0.055
221	18.42	0.13	0.071	(0.115)	0.016	0.055
222	18.50	0.13	0.071	(0.114)	0.016	0.055
223	18.58	0.10	0.053	(0.114)	0.012	0.041
224	18.67	0.10	0.053	(0.113)	0.012	0.041
225	18.75	0.10	0.053	(0.113)	0.012	0.041
226	18.83	0.07	0.036	(0.112)	0.008	0.027
227	18.92	0.07	0.036	(0.112)	0.008	0.027
228	19.00	0.07	0.036	(0.111)	0.008	0.027
229	19.08	0.10	0.053	(0.111)	0.012	0.041
230	19.17	0.10	0.053	(0.110)	0.012	0.041
231	19.25	0.10	0.053	(0.110)	0.012	0.041
232	19.33	0.13	0.071	(0.109)	0.016	0.055
233	19.42	0.13	0.071	(0.109)	0.016	0.055
234	19.50	0.13	0.071	(0.108)	0.016	0.055
235	19.58	0.10	0.053	(0.108)	0.012	0.041
236	19.67	0.10	0.053	(0.107)	0.012	0.041
237	19.75	0.10	0.053	(0.107)	0.012	0.041
238	19.83	0.07	0.036	(0.106)	0.008	0.027
239	19.92	0.07	0.036	(0.106)	0.008	0.027
240	20.00	0.07	0.036	(0.105)	0.008	0.027
241	20.08	0.10	0.053	(0.105)	0.012	0.041
242	20.17	0.10	0.053	(0.104)	0.012	0.041
243	20.25	0.10	0.053	(0.104)	0.012	0.041
244	20.33	0.10	0.053	(0.103)	0.012	0.041
245	20.42	0.10	0.053	(0.103)	0.012	0.041
246	20.50	0.10	0.053	(0.102)	0.012	0.041
247	20.58	0.10	0.053	(0.102)	0.012	0.041
248	20.67	0.10	0.053	(0.102)	0.012	0.041
249	20.75	0.10	0.053	(0.101)	0.012	0.041
250	20.83	0.07	0.036	(0.101)	0.008	0.027
251	20.92	0.07	0.036	(0.100)	0.008	0.027
252	21.00	0.07	0.036	(0.100)	0.008	0.027
253	21.08	0.10	0.053	(0.100)	0.012	0.041
254	21.17	0.10	0.053	(0.099)	0.012	0.041
255	21.25	0.10	0.053	(0.099)	0.012	0.041
256	21.33	0.07	0.036	(0.098)	0.008	0.027
257	21.42	0.07	0.036	(0.098)	0.008	0.027
258	21.50	0.07	0.036	(0.098)	0.008	0.027
259	21.58	0.10	0.053	(0.097)	0.012	0.041
260	21.67	0.10	0.053	(0.097)	0.012	0.041
261	21.75	0.10	0.053	(0.097)	0.012	0.041
262	21.83	0.07	0.036	(0.096)	0.008	0.027
263	21.92	0.07	0.036	(0.096)	0.008	0.027
264	22.00	0.07	0.036	(0.096)	0.008	0.027
265	22.08	0.10	0.053	(0.095)	0.012	0.041
266	22.17	0.10	0.053	(0.095)	0.012	0.041
267	22.25	0.10	0.053	(0.095)	0.012	0.041
268	22.33	0.07	0.036	(0.094)	0.008	0.027

269	22.42	0.07	0.036	(0.094)	0.008	0.027
270	22.50	0.07	0.036	(0.094)	0.008	0.027
271	22.58	0.07	0.036	(0.094)	0.008	0.027
272	22.67	0.07	0.036	(0.093)	0.008	0.027
273	22.75	0.07	0.036	(0.093)	0.008	0.027
274	22.83	0.07	0.036	(0.093)	0.008	0.027
275	22.92	0.07	0.036	(0.093)	0.008	0.027
276	23.00	0.07	0.036	(0.092)	0.008	0.027
277	23.08	0.07	0.036	(0.092)	0.008	0.027
278	23.17	0.07	0.036	(0.092)	0.008	0.027
279	23.25	0.07	0.036	(0.092)	0.008	0.027
280	23.33	0.07	0.036	(0.092)	0.008	0.027
281	23.42	0.07	0.036	(0.091)	0.008	0.027
282	23.50	0.07	0.036	(0.091)	0.008	0.027
283	23.58	0.07	0.036	(0.091)	0.008	0.027
284	23.67	0.07	0.036	(0.091)	0.008	0.027
285	23.75	0.07	0.036	(0.091)	0.008	0.027
286	23.83	0.07	0.036	(0.091)	0.008	0.027
287	23.92	0.07	0.036	(0.091)	0.008	0.027
288	24.00	0.07	0.036	(0.091)	0.008	0.027

(Loss Rate Not Used)

Sum = 100.0 Sum = 41.0

Flood volume = Effective rainfall 3.42(In)
times area 0.6(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 1.02(In)
Total soil loss = 0.047(Ac.Ft)
Total rainfall = 4.44(In)
Flood volume = 6825.6 Cubic Feet
Total soil loss = 2038.8 Cubic Feet

Peak flow rate of this hydrograph = 0.258(CFS)

++

24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.01	Q	|	|	|	|
0+10	0.0002	0.02	Q	|	|	|	|
0+15	0.0003	0.02	Q	|	|	|	|
0+20	0.0004	0.02	Q	|	|	|	|
0+25	0.0006	0.02	Q	|	|	|	|
0+30	0.0007	0.02	Q	|	|	|	|
0+35	0.0009	0.02	Q	|	|	|	|
0+40	0.0011	0.02	Q	|	|	|	|
0+45	0.0012	0.02	Q	|	|	|	|
0+50	0.0014	0.03	Q	|	|	|	|
0+55	0.0016	0.03	Q	|	|	|	|
1+ 0	0.0018	0.03	Q	|	|	|	|

1+ 5	0.0020	0.02	Q	|	|	|	|
1+10	0.0022	0.02	Q	|	|	|	|
1+15	0.0023	0.02	Q	|	|	|	|
1+20	0.0025	0.02	Q	|	|	|	|
1+25	0.0026	0.02	Q	|	|	|	|
1+30	0.0028	0.02	Q	|	|	|	|
1+35	0.0029	0.02	Q	|	|	|	|
1+40	0.0031	0.02	Q	|	|	|	|
1+45	0.0032	0.02	Q	|	|	|	|
1+50	0.0034	0.03	Q	|	|	|	|
1+55	0.0037	0.03	Q	|	|	|	|
2+ 0	0.0039	0.03	Q	|	|	|	|
2+ 5	0.0041	0.03	QV	|	|	|	|
2+10	0.0043	0.03	QV	|	|	|	|
2+15	0.0045	0.03	QV	|	|	|	|
2+20	0.0047	0.03	QV	|	|	|	|
2+25	0.0049	0.03	QV	|	|	|	|
2+30	0.0051	0.03	QV	|	|	|	|
2+35	0.0054	0.04	QV	|	|	|	|
2+40	0.0056	0.04	QV	|	|	|	|
2+45	0.0059	0.04	QV	|	|	|	|
2+50	0.0061	0.04	QV	|	|	|	|
2+55	0.0064	0.04	QV	|	|	|	|
3+ 0	0.0067	0.04	QV	|	|	|	|
3+ 5	0.0069	0.04	QV	|	|	|	|
3+10	0.0072	0.04	QV	|	|	|	|
3+15	0.0075	0.04	QV	|	|	|	|
3+20	0.0077	0.04	QV	|	|	|	|
3+25	0.0080	0.04	Q V	|	|	|	|
3+30	0.0082	0.04	Q V	|	|	|	|
3+35	0.0085	0.04	Q V	|	|	|	|
3+40	0.0088	0.04	Q V	|	|	|	|
3+45	0.0090	0.04	Q V	|	|	|	|
3+50	0.0093	0.04	Q V	|	|	|	|
3+55	0.0096	0.05	Q V	|	|	|	|
4+ 0	0.0099	0.05	Q V	|	|	|	|
4+ 5	0.0103	0.05	Q V	|	|	|	|
4+10	0.0106	0.05	Q V	|	|	|	|
4+15	0.0109	0.05	Q V	|	|	|	|
4+20	0.0112	0.05	Q V	|	|	|	|
4+25	0.0116	0.05	Q V	|	|	|	|
4+30	0.0120	0.05	Q V	|	|	|	|
4+35	0.0123	0.05	Q V	|	|	|	|
4+40	0.0127	0.05	Q V	|	|	|	|
4+45	0.0131	0.05	Q V	|	|	|	|
4+50	0.0135	0.06	Q V	|	|	|	|
4+55	0.0139	0.06	Q V	|	|	|	|
5+ 0	0.0143	0.06	Q V	|	|	|	|
5+ 5	0.0146	0.05	Q V	|	|	|	|
5+10	0.0150	0.05	Q V	|	|	|	|
5+15	0.0153	0.05	Q V	|	|	|	|
5+20	0.0156	0.05	Q V	|	|	|	|
5+25	0.0160	0.05	Q V	|	|	|	|

5+30	0.0164	0.05	Q	V	|	|	|	|
5+35	0.0168	0.06	Q	V	|	|	|	|
5+40	0.0172	0.06	Q	V	|	|	|	|
5+45	0.0176	0.06	Q	V	|	|	|	|
5+50	0.0180	0.06	Q	V	|	|	|	|
5+55	0.0184	0.06	Q	V	|	|	|	|
6+ 0	0.0188	0.06	Q	V	|	|	|	|
6+ 5	0.0193	0.07	Q	V	|	|	|	|
6+10	0.0198	0.07	Q	V	|	|	|	|
6+15	0.0202	0.07	Q	V	|	|	|	|
6+20	0.0207	0.07	Q	V	|	|	|	|
6+25	0.0212	0.07	Q	V	|	|	|	|
6+30	0.0217	0.07	Q	V	|	|	|	|
6+35	0.0222	0.07	Q	V	|	|	|	|
6+40	0.0227	0.08	Q	V	|	|	|	|
6+45	0.0232	0.08	Q	V	|	|	|	|
6+50	0.0237	0.08	Q	V	|	|	|	|
6+55	0.0242	0.08	Q	V	|	|	|	|
7+ 0	0.0248	0.08	Q	V	|	|	|	|
7+ 5	0.0253	0.08	Q	V	|	|	|	|
7+10	0.0258	0.08	Q	V	|	|	|	|
7+15	0.0263	0.08	Q	V	|	|	|	|
7+20	0.0269	0.08	Q	V	|	|	|	|
7+25	0.0275	0.08	Q	V	|	|	|	|
7+30	0.0280	0.08	Q	V	|	|	|	|
7+35	0.0287	0.09	Q	V	|	|	|	|
7+40	0.0293	0.09	Q	V	|	|	|	|
7+45	0.0299	0.09	Q	V	|	|	|	|
7+50	0.0306	0.10	Q	V	|	|	|	|
7+55	0.0313	0.10	Q	V	|	|	|	|
8+ 0	0.0319	0.10	Q	V	|	|	|	|
8+ 5	0.0327	0.11	Q	V	|	|	|	|
8+10	0.0335	0.11	Q	V	|	|	|	|
8+15	0.0343	0.11	Q	V	|	|	|	|
8+20	0.0350	0.11	Q	V	|	|	|	|
8+25	0.0358	0.11	Q	V	|	|	|	|
8+30	0.0366	0.11	Q	V	|	|	|	|
8+35	0.0374	0.12	Q	V	|	|	|	|
8+40	0.0383	0.12	Q	V	|	|	|	|
8+45	0.0391	0.12	Q	V	|	|	|	|
8+50	0.0400	0.13	Q	V	|	|	|	|
8+55	0.0409	0.13	Q	V	|	|	|	|
9+ 0	0.0418	0.13	Q	V	|	|	|	|
9+ 5	0.0427	0.14	Q	V	|	|	|	|
9+10	0.0437	0.14	Q	|	V	|	|	|
9+15	0.0447	0.14	Q	|	V	|	|	|
9+20	0.0457	0.15	Q	|	V	|	|	|
9+25	0.0468	0.15	Q	|	V	|	|	|
9+30	0.0478	0.15	Q	|	V	|	|	|
9+35	0.0489	0.16	Q	|	V	|	|	|
9+40	0.0500	0.16	Q	|	V	|	|	|
9+45	0.0511	0.16	Q	|	V	|	|	|
9+50	0.0522	0.16	Q	|	V	|	|	|

```
 9+55       0.0534      0.17  Q         |  V      |         |         |
10+ 0       0.0545      0.17  Q         |  V      |         |         |
10+ 5       0.0554      0.13  Q         |   V     |         |         |
10+10       0.0562      0.11  Q         |   V     |         |         |
10+15       0.0570      0.11  Q         |   V     |         |         |
10+20       0.0578      0.11  Q         |   V     |         |         |
10+25       0.0585      0.11  Q         |   V     |         |         |
10+30       0.0593      0.11  Q         |    V    |         |         |
10+35       0.0603      0.14  Q         |    V    |         |         |
10+40       0.0613      0.15  Q         |    V    |         |         |
10+45       0.0624      0.15  Q         |    V    |         |         |
10+50       0.0634      0.15  Q         |     V   |         |         |
10+55       0.0645      0.15  Q         |     V   |         |         |
11+ 0       0.0655      0.15  Q         |     V   |         |         |
11+ 5       0.0665      0.15  Q         |     V   |         |         |
11+10       0.0675      0.14  Q         |      V  |         |         |
11+15       0.0685      0.14  Q         |      V  |         |         |
11+20       0.0695      0.14  Q         |      V  |         |         |
11+25       0.0705      0.14  Q         |      V  |         |         |
11+30       0.0715      0.14  Q         |       V |         |         |
11+35       0.0724      0.13  Q         |       V |         |         |
11+40       0.0733      0.13  Q         |       V |         |         |
11+45       0.0742      0.13  Q         |       V |         |         |
11+50       0.0751      0.13  Q         |        V|         |         |
11+55       0.0761      0.14  Q         |        V|         |         |
12+ 0       0.0770      0.14  Q         |        V|         |         |
12+ 5       0.0782      0.18  Q         |        V|         |         |
12+10       0.0795      0.19  Q         |         V         |         |
12+15       0.0808      0.19  Q         |         V         |         |
12+20       0.0822      0.20  Q         |         V         |         |
12+25       0.0835      0.20  Q         |         |V        |         |
12+30       0.0849      0.20  Q         |         |V        |         |
12+35       0.0863      0.21  Q         |         | V       |         |
12+40       0.0878      0.21  Q         |         | V       |         |
12+45       0.0892      0.21  Q         |         | V       |         |
12+50       0.0907      0.22  Q         |         |  V      |         |
12+55       0.0922      0.22  Q         |         |  V      |         |
13+ 0       0.0938      0.22  Q         |         |  V      |         |
13+ 5       0.0955      0.25  Q         |         |   V     |         |
13+10       0.0972      0.26  |Q        |         |   V     |         |
13+15       0.0990      0.26  |Q        |         |    V    |         |
13+20       0.1008      0.26  |Q        |         |    V    |         |
13+25       0.1026      0.26  |Q        |         |     V   |         |
13+30       0.1043      0.26  |Q        |         |     V   |         |
13+35       0.1057      0.20  Q         |         |     V   |         |
13+40       0.1069      0.17  Q         |         |      V  |         |
13+45       0.1081      0.17  Q         |         |      V  |         |
13+50       0.1093      0.17  Q         |         |      V  |         |
13+55       0.1105      0.17  Q         |         |       V |         |
14+ 0       0.1117      0.17  Q         |         |       V |         |
14+ 5       0.1131      0.20  Q         |         |       V |         |
14+10       0.1145      0.20  Q         |         |        V|         |
14+15       0.1159      0.20  Q         |         |        V|         |
```

14+20	0.1173	0.20	Q	|	|	V|	|
14+25	0.1186	0.20	Q	|	|	V	|
14+30	0.1200	0.20	Q	|	|	V	|
14+35	0.1213	0.20	Q	|	|	V	|
14+40	0.1227	0.20	Q	|	|	|V	|
14+45	0.1240	0.20	Q	|	|	|V	|
14+50	0.1254	0.19	Q	|	|	| V	|
14+55	0.1267	0.19	Q	|	|	| V	|
15+ 0	0.1280	0.19	Q	|	|	| V	|
15+ 5	0.1292	0.18	Q	|	|	| V	|
15+10	0.1305	0.18	Q	|	|	| V	|
15+15	0.1318	0.18	Q	|	|	| V	|
15+20	0.1330	0.18	Q	|	|	| V	|
15+25	0.1342	0.17	Q	|	|	| V	|
15+30	0.1354	0.17	Q	|	|	| V	|
15+35	0.1364	0.15	Q	|	|	| V	|
15+40	0.1374	0.14	Q	|	|	| V	|
15+45	0.1384	0.14	Q	|	|	| V	|
15+50	0.1394	0.14	Q	|	|	| V	|
15+55	0.1404	0.14	Q	|	|	| V	|
16+ 0	0.1414	0.14	Q	|	|	| V	|
16+ 5	0.1418	0.06	Q	|	|	| V	|
16+10	0.1420	0.03	Q	|	|	| V	|
16+15	0.1422	0.03	Q	|	|	| V	|
16+20	0.1424	0.03	Q	|	|	| V	|
16+25	0.1426	0.03	Q	|	|	| V	|
16+30	0.1428	0.03	Q	|	|	| V	|
16+35	0.1430	0.02	Q	|	|	| V	|
16+40	0.1432	0.02	Q	|	|	| V	|
16+45	0.1433	0.02	Q	|	|	| V	|
16+50	0.1435	0.02	Q	|	|	| V	|
16+55	0.1436	0.02	Q	|	|	| V	|
17+ 0	0.1438	0.02	Q	|	|	| V	|
17+ 5	0.1440	0.03	Q	|	|	| V	|
17+10	0.1443	0.04	Q	|	|	| V	|
17+15	0.1446	0.04	Q	|	|	| V	|
17+20	0.1448	0.04	Q	|	|	| V	|
17+25	0.1451	0.04	Q	|	|	| V	|
17+30	0.1453	0.04	Q	|	|	| V	|
17+35	0.1456	0.04	Q	|	|	| V	|
17+40	0.1459	0.04	Q	|	|	| V	|
17+45	0.1461	0.04	Q	|	|	| V	|
17+50	0.1463	0.03	Q	|	|	| V	|
17+55	0.1466	0.03	Q	|	|	| V	|
18+ 0	0.1468	0.03	Q	|	|	| V	|
18+ 5	0.1470	0.03	Q	|	|	| V	|
18+10	0.1472	0.03	Q	|	|	| V	|
18+15	0.1474	0.03	Q	|	|	| V	|
18+20	0.1476	0.03	Q	|	|	| V	|
18+25	0.1478	0.03	Q	|	|	| V	|
18+30	0.1480	0.03	Q	|	|	| V	|
18+35	0.1482	0.02	Q	|	|	| V	|
18+40	0.1483	0.02	Q	|	|	| V	|

18+45	0.1485	0.02	Q	|	|	|	V |
18+50	0.1486	0.02	Q	|	|	|	V |
18+55	0.1487	0.02	Q	|	|	|	V |
19+ 0	0.1488	0.02	Q	|	|	|	V |
19+ 5	0.1490	0.02	Q	|	|	|	V |
19+10	0.1491	0.02	Q	|	|	|	V |
19+15	0.1493	0.02	Q	|	|	|	V |
19+20	0.1495	0.03	Q	|	|	|	V |
19+25	0.1497	0.03	Q	|	|	|	V |
19+30	0.1499	0.03	Q	|	|	|	V |
19+35	0.1501	0.02	Q	|	|	|	V |
19+40	0.1502	0.02	Q	|	|	|	V |
19+45	0.1504	0.02	Q	|	|	|	V |
19+50	0.1505	0.02	Q	|	|	|	V |
19+55	0.1506	0.02	Q	|	|	|	V |
20+ 0	0.1507	0.02	Q	|	|	|	V |
20+ 5	0.1509	0.02	Q	|	|	|	V |
20+10	0.1510	0.02	Q	|	|	|	V |
20+15	0.1512	0.02	Q	|	|	|	V |
20+20	0.1513	0.02	Q	|	|	|	V |
20+25	0.1515	0.02	Q	|	|	|	V |
20+30	0.1516	0.02	Q	|	|	|	V |
20+35	0.1518	0.02	Q	|	|	|	V |
20+40	0.1520	0.02	Q	|	|	|	V |
20+45	0.1521	0.02	Q	|	|	|	V |
20+50	0.1522	0.02	Q	|	|	|	V |
20+55	0.1523	0.02	Q	|	|	|	V |
21+ 0	0.1524	0.02	Q	|	|	|	V |
21+ 5	0.1526	0.02	Q	|	|	|	V |
21+10	0.1527	0.02	Q	|	|	|	V |
21+15	0.1529	0.02	Q	|	|	|	V|
21+20	0.1530	0.02	Q	|	|	|	V|
21+25	0.1531	0.02	Q	|	|	|	V|
21+30	0.1532	0.02	Q	|	|	|	V|
21+35	0.1534	0.02	Q	|	|	|	V|
21+40	0.1535	0.02	Q	|	|	|	V|
21+45	0.1537	0.02	Q	|	|	|	V|
21+50	0.1538	0.02	Q	|	|	|	V|
21+55	0.1539	0.02	Q	|	|	|	V|
22+ 0	0.1540	0.02	Q	|	|	|	V|
22+ 5	0.1541	0.02	Q	|	|	|	V|
22+10	0.1543	0.02	Q	|	|	|	V|
22+15	0.1545	0.02	Q	|	|	|	V|
22+20	0.1546	0.02	Q	|	|	|	V|
22+25	0.1547	0.02	Q	|	|	|	V|
22+30	0.1548	0.02	Q	|	|	|	V|
22+35	0.1549	0.02	Q	|	|	|	V|
22+40	0.1550	0.02	Q	|	|	|	V|
22+45	0.1551	0.02	Q	|	|	|	V|
22+50	0.1552	0.02	Q	|	|	|	V|
22+55	0.1553	0.02	Q	|	|	|	V|
23+ 0	0.1554	0.02	Q	|	|	|	V|
23+ 5	0.1555	0.02	Q	|	|	|	V|

23+10	0.1556	0.02	Q	|	|	|	V|
23+15	0.1557	0.02	Q	|	|	|	V|
23+20	0.1558	0.02	Q	|	|	|	V|
23+25	0.1559	0.02	Q	|	|	|	V|
23+30	0.1560	0.02	Q	|	|	|	V|
23+35	0.1561	0.02	Q	|	|	|	V|
23+40	0.1562	0.02	Q	|	|	|	V|
23+45	0.1564	0.02	Q	|	|	|	V|
23+50	0.1565	0.02	Q	|	|	|	V|
23+55	0.1566	0.02	Q	|	|	|	V|
24+ 0	0.1567	0.02	Q	|	|	|	V|
24+ 5	0.1567	0.00	Q	|	|	|	V

SUBSURFACE STAGE STORAGE CALCULATIONS

BASIN A1 SUBSURFACE SYSTEM

1 Barrel 60-Inch Subsurface Infiltration Basin Volume Calculations

LENGTH OF SUBSURFACE SYSTEM (FT) = 325 **NUMBER OF CELLS 1**

Elevation	Depth	Inner Pipe Depth	Outer Pipe Depth	Outer Pipe Area Each (ft^2)	Inner Pipe Area Each (ft^2)	Pipe Thickness Area Each (ft^2)	Inner Pipe Area Total (ft^2)	Inner Pipe Total Gross Volume at Elev. (ft^3)	Gross Cross Sectional Area of System (ft^2)	Net Gravel Area (ft^2)	Gravel Volume (ft^3)	Cumulative Subsurface System Volume (ft^3)	Cumulative Subsurface System Volume (ac-ft)
0	0	0	0	0.00	0.00	0.00	0.00	0.00	0	0.00	0.00	0.00	0.000
0.5	0.5	0	0	0.00	0.00	0.00	0.00	0.00	3.79	3.79	492.70	492.70	0.011
1	1	0	0	0.00	0.00	0.00	0.00	0.00	7.58	7.58	985.40	985.40	0.023
1.5	1.5	0.21	0.4725	0.99	0.28	0.71	0.28	92.06	11.37	10.38	1349.22	1441.28	0.033
2	2	0.71	0.9725	2.84	1.71	1.14	1.71	554.33	15.16	12.32	1601.40	2155.73	0.049
2.5	2.5	1.21	1.4725	5.13	3.67	1.46	3.67	1191.58	18.95	13.82	1796.81	2988.39	0.069
3	3	1.71	1.9725	7.68	5.93	1.75	5.93	1928.63	22.74	15.06	1957.43	3886.05	0.089
3.5	3.5	2.21	2.4725	10.39	8.37	2.02	8.37	2720.49	26.53	16.14	2098.45	4818.94	0.111
4	4	2.71	2.9725	13.15	10.87	2.28	10.87	3531.53	30.32	17.17	2232.55	5764.08	0.132
4.5	4.5	3.21	3.4725	15.87	13.32	2.55	13.32	4328.73	34.11	18.24	2371.65	6700.38	0.154
5	5	3.71	3.9725	18.45	15.62	2.83	15.62	5077.21	37.9	19.45	2528.21	7605.42	0.175
5.5	5.5	4.21	4.4725	20.79	17.64	3.15	17.64	5734.21	41.69	20.90	2716.84	8451.05	0.194
6	6	4.71	4.9725	22.73	19.18	3.55	19.18	6232.70	45.48	22.75	2957.89	9190.58	0.211
6.5	6.5	5	5.4725	23.94	19.63	4.30	19.63	6381.36	49.27	25.33	3293.27	9674.63	0.222
7	7	5	5.525	23.97	19.63	4.34	19.63	6381.36	53.06	29.09	3781.08	10162.44	0.233
7.5	7.5	5	5.525	23.97	19.63	4.34	19.63	6381.36	56.85	32.88	4273.78	10655.14	0.245
7.58	7.58	5	5.525	23.97	19.63	4.34	19.63	6381.36	57.4564	33.48	4352.61	**10733.97**	0.246

INPUT DATA

SUBSURFACE SYSTEM NAME	A1	-
INNER DIAMETER OF SUBSURFACE SYSTEM	5	FT
OUTER DIAMETER OF SUBSURFACE SYSTEM	5.525	FT
NUMBER OF BARRELS	1	EA
LENGTH OF SUBSURFACE SYSTEM	325	FT
BOTTOM INVERT OF GRAVEL BED	0	FT
EFFECTIVE STORAGE ELEVATION	0	FT
PIPE SPACING	0	FT
EDGE THICKNESS	1.29	FT
TOP CLEARANCE, THICKNESS	1.29	FT
BOTTOM CLEARANCE, THICKNESS	1.29	FT
GRAVEL POROSITY, N	0.4	-
FT2 -> AC	43560	FT^2/AC

BASIN AA1 SUBSURFACE SYSTEM

1 Barrel 60-Inch Subsurface Infiltration Basin Volume Calculations

LENGTH OF SUBSURFACE SYSTEM (FT) = 305 **NUMBER OF CELLS 1**

Elevation	Depth	Inner Pipe Depth	Outer Pipe Depth	Outer Pipe Area Each (ft^2)	Inner Pipe Area Each (ft^2)	Pipe Thickness Area Each (ft^2)	Inner Pipe Area Total (ft^2)	Inner Pipe Total Gross Volume at Elev. (ft^3)	Gross Cross Sectional Area of System (ft^2)	Net Gravel Area (ft^2)	Gravel Volume (ft^3)	Cumulative Subsurface System Volume (ft^3)	Cumulative Subsurface System Volume (ac-ft)
0	0	0	0	0.00	0.00	0.00	0.00	0.00	0	0.00	0.00	0.00	0.000
0.5	0.5	0	0	0.00	0.00	0.00	0.00	0.00	3.79	3.79	462.38	462.38	0.011
1	1	0	0	0.00	0.00	0.00	0.00	0.00	7.58	7.58	924.76	924.76	0.021
1.5	1.5	0.21	0.4725	0.99	0.28	0.71	0.28	86.40	11.37	10.38	1266.19	1352.59	0.031
2	2	0.71	0.9725	2.84	1.71	1.14	1.71	520.22	15.16	12.32	1502.85	2023.07	0.046
2.5	2.5	1.21	1.4725	5.13	3.67	1.46	3.67	1118.25	18.95	13.82	1686.24	2804.49	0.064
3	3	1.71	1.9725	7.68	5.93	1.75	5.93	1809.94	22.74	15.06	1836.97	3646.91	0.084
3.5	3.5	2.21	2.4725	10.39	8.37	2.02	8.37	2553.07	26.53	16.14	1969.31	4522.39	0.104
4	4	2.71	2.9725	13.15	10.87	2.28	10.87	3314.20	30.32	17.17	2095.16	5409.37	0.124
4.5	4.5	3.21	3.4725	15.87	13.32	2.55	13.32	4062.34	34.11	18.24	2225.71	6288.05	0.144
5	5	3.71	3.9725	18.45	15.62	2.83	15.62	4764.77	37.9	19.45	2372.62	7137.39	0.164
5.5	5.5	4.21	4.4725	20.79	17.64	3.15	17.64	5381.33	41.69	20.90	2549.65	7930.98	0.182
6	6	4.71	4.9725	22.73	19.18	3.55	19.18	5849.15	45.48	22.75	2775.86	8625.01	0.198
6.5	6.5	5	5.4725	23.94	19.63	4.30	19.63	5988.66	49.27	25.33	3090.60	9079.27	0.208
7	7	5	5.525	23.97	19.63	4.34	19.63	5988.66	53.06	29.09	3548.40	9537.06	0.219
7.5	7.5	5	5.525	23.97	19.63	4.34	19.63	5988.66	56.85	32.88	4010.78	9999.44	0.230
7.58	7.58	5	5.525	23.97	19.63	4.34	19.63	5988.66	57.4564	33.48	4084.76	**10073.42**	0.231

INPUT DATA

SUBSURFACE SYSTEM NAME	AA1	-
INNER DIAMETER OF SUBSURFACE SYSTEM	5	FT
OUTER DIAMETER OF SUBSURFACE SYSTEM	5.525	FT
NUMBER OF BARRELS	1	EA
LENGTH OF SUBSURFACE SYSTEM	305	FT
BOTTOM INVERT OF GRAVEL BED	0	FT
EFFECTIVE STORAGE ELEVATION	0	FT
PIPE SPACING	0	FT
EDGE THICKNESS	1.29	FT
TOP CLEARANCE, THICKNESS	1.29	FT
BOTTOM CLEARANCE, THICKNESS	1.29	FT
GRAVEL POROSITY, N	0.4	-
FT2 -> AC	43560	FT^2/AC

BASIN B1 SUBSURFACE SYSTEM

1 Barrel 60-Inch Subsurface Infiltration Basin Volume Calculations

LENGTH OF SUBSURFACE SYSTEM (FT) = 370 **NUMBER OF CELLS 1**

Elevation	Depth	Inner Pipe Depth	Outer Pipe Depth	Outer Pipe Area Each (ft^2)	Inner Pipe Area Each (ft^2)	Pipe Thickness Area Each (ft^2)	Inner Pipe Area Total (ft^2)	Inner Pipe Total Gross Volume at Elev. (ft^3)	Gross Cross Sectional Area of System (ft^2)	Net Gravel Area (ft^2)	Gravel Volume (ft^3)	Cumulative Subsurface System Volume (ft^3)	Cumulative Subsurface System Volume (ac-ft)
0	0	0	0	0.00	0.00	0.00	0.00	0.00	0	0.00	0.00	0.00	0.000
0.5	0.5	0	0	0.00	0.00	0.00	0.00	0.00	3.79	3.79	560.92	560.92	0.013
1	1	0	0	0.00	0.00	0.00	0.00	0.00	7.58	7.58	1121.84	1121.84	0.026
1.5	1.5	0.21	0.4725	0.99	0.28	0.71	0.28	104.81	11.37	10.38	1536.04	1640.85	0.038
2	2	0.71	0.9725	2.84	1.71	1.14	1.71	631.08	15.16	12.32	1823.13	2454.21	0.056
2.5	2.5	1.21	1.4725	5.13	3.67	1.46	3.67	1356.56	18.95	13.82	2045.60	3402.16	0.078
3	3	1.71	1.9725	7.68	5.93	1.75	5.93	2195.67	22.74	15.06	2228.45	4424.12	0.102
3.5	3.5	2.21	2.4725	10.39	8.37	2.02	8.37	3097.17	26.53	16.14	2389.00	5486.18	0.126
4	4	2.71	2.9725	13.15	10.87	2.28	10.87	4020.51	30.32	17.17	2541.68	6562.18	0.151
4.5	4.5	3.21	3.4725	15.87	13.32	2.55	13.32	4928.09	34.11	18.24	2700.04	7628.13	0.175
5	5	3.71	3.9725	18.45	15.62	2.83	15.62	5780.21	37.9	19.45	2878.27	8658.47	0.199
5.5	5.5	4.21	4.4725	20.79	17.64	3.15	17.64	6528.17	41.69	20.90	3093.02	9621.19	0.221
6	6	4.71	4.9725	22.73	19.18	3.55	19.18	7095.69	45.48	22.75	3367.44	10463.13	0.240
6.5	6.5	5	5.4725	23.94	19.63	4.30	19.63	7264.93	49.27	25.33	3749.26	11014.19	0.253
7	7	5	5.525	23.97	19.63	4.34	19.63	7264.93	53.06	29.09	4304.61	11569.55	0.266
7.5	7.5	5	5.525	23.97	19.63	4.34	19.63	7264.93	56.85	32.88	4865.53	12130.47	0.278
7.58	7.58	5	5.525	23.97	19.63	4.34	19.63	7264.93	57.4564	33.48	4955.28	**12220.21**	0.281

INPUT DATA

SUBSURFACE SYSTEM NAME	B1	-
INNER DIAMETER OF SUBSURFACE SYSTEM	5	FT
OUTER DIAMETER OF SUBSURFACE SYSTEM	5.525	FT
NUMBER OF BARRELS	1	EA
LENGTH OF SUBSURFACE SYSTEM	370	FT
BOTTOM INVERT OF GRAVEL BED	0	FT
EFFECTIVE STORAGE ELEVATION	0	FT
PIPE SPACING	0	FT
EDGE THICKNESS	1.29	FT
TOP CLEARANCE, THICKNESS	1.29	FT
BOTTOM CLEARANCE, THICKNESS	1.29	FT
GRAVEL POROSITY, N	0.4	-
FT2 -> AC	43560	FT^2/AC

BASIN BB1 SUBSURFACE SYSTEM

1 Barrel 60-Inch Subsurface Infiltration Basin Volume Calculations

LENGTH OF SUBSURFACE SYSTEM (FT) = 360 **NUMBER OF CELLS 1**

Elevation	Depth	Inner Pipe Depth	Outer Pipe Depth	Outer Pipe Area Each (ft^2)	Inner Pipe Area Each (ft^2)	Pipe Thickness Area Each (ft^2)	Inner Pipe Area Total (ft^2)	Inner Pipe Total Gross Volume at Elev. (ft^3)	Gross Cross Sectional Area of System (ft^2)	Net Gravel Area (ft^2)	Gravel Volume (ft^3)	Cumulative Subsurface System Volume (ft^3)	Cumulative Subsurface System Volume (ac-ft)
0	0	0	0	0.00	0.00	0.00	0.00	0.00	0	0.00	0.00	0.00	0.000
0.5	0.5	0	0	0.00	0.00	0.00	0.00	0.00	3.79	3.79	545.76	545.76	0.013
1	1	0	0	0.00	0.00	0.00	0.00	0.00	7.58	7.58	1091.52	1091.52	0.025
1.5	1.5	0.21	0.4725	0.99	0.28	0.71	0.28	101.98	11.37	10.38	1494.52	1596.50	0.037
2	2	0.71	0.9725	2.84	1.71	1.14	1.71	614.03	15.16	12.32	1773.85	2387.88	0.055
2.5	2.5	1.21	1.4725	5.13	3.67	1.46	3.67	1319.90	18.95	13.82	1990.31	3310.21	0.076
3	3	1.71	1.9725	7.68	5.93	1.75	5.93	2136.33	22.74	15.06	2168.23	4304.55	0.099
3.5	3.5	2.21	2.4725	10.39	8.37	2.02	8.37	3013.46	26.53	16.14	2324.44	5337.90	0.123
4	4	2.71	2.9725	13.15	10.87	2.28	10.87	3911.85	30.32	17.17	2472.98	6384.83	0.147
4.5	4.5	3.21	3.4725	15.87	13.32	2.55	13.32	4794.90	34.11	18.24	2627.06	7421.96	0.170
5	5	3.71	3.9725	18.45	15.62	2.83	15.62	5623.99	37.9	19.45	2800.48	8424.46	0.193
5.5	5.5	4.21	4.4725	20.79	17.64	3.15	17.64	6351.74	41.69	20.90	3009.42	9361.16	0.215
6	6	4.71	4.9725	22.73	19.18	3.55	19.18	6903.91	45.48	22.75	3276.43	10180.34	0.234
6.5	6.5	5	5.4725	23.94	19.63	4.30	19.63	7068.58	49.27	25.33	3647.93	10716.51	0.246
7	7	5	5.525	23.97	19.63	4.34	19.63	7068.58	53.06	29.09	4188.27	11256.86	0.258
7.5	7.5	5	5.525	23.97	19.63	4.34	19.63	7068.58	56.85	32.88	4734.03	11802.62	0.271
7.58	7.58	5	5.525	23.97	19.63	4.34	19.63	7068.58	57.4564	33.48	4821.35	**11889.94**	0.273

INPUT DATA

SUBSURFACE SYSTEM NAME	BB1	-
INNER DIAMETER OF SUBSURFACE SYSTEM	5	FT
OUTER DIAMETER OF SUBSURFACE SYSTEM	5.525	FT
NUMBER OF BARRELS	1	EA
LENGTH OF SUBSURFACE SYSTEM	360	FT
BOTTOM INVERT OF GRAVEL BED	0	FT
EFFECTIVE STORAGE ELEVATION	0	FT
PIPE SPACING	0	FT
EDGE THICKNESS	1.29	FT
TOP CLEARANCE, THICKNESS	1.29	FT
BOTTOM CLEARANCE, THICKNESS	1.29	FT
GRAVEL POROSITY, N	0.4	-
FT2 -> AC	43560	FT^2/AC

BASIN C1 SUBSURFACE SYSTEM

1 Barrel 60-Inch Subsurface Infiltration Basin Volume Calculations

LENGTH OF SUBSURFACE SYSTEM (FT) = 200 **NUMBER OF CELLS 1**

Elevation	Depth	Inner Pipe Depth	Outer Pipe Depth	Outer Pipe Area Each (ft^2)	Inner Pipe Area Each (ft^2)	Pipe Thickness Area Each (ft^2)	Inner Pipe Area Total (ft^2)	Inner Pipe Total Gross Volume at Elev. (ft^3)	Gross Cross Sectional Area of System (ft^2)	Net Gravel Area (ft^2)	Gravel Volume (ft^3)	Cumulative Subsurface System Volume (ft^3)	Cumulative Subsurface System Volume (ac-ft)
0	0	0	0	0.00	0.00	0.00	0.00	0.00	0	0.00	0.00	0.00	0.000
0.5	0.5	0	0	0.00	0.00	0.00	0.00	0.00	3.79	3.79	303.20	303.20	0.007
1	1	0	0	0.00	0.00	0.00	0.00	0.00	7.58	7.58	606.40	606.40	0.014
1.5	1.5	0.21	0.4725	0.99	0.28	0.71	0.28	56.65	11.37	10.38	830.29	886.94	0.020
2	2	0.71	0.9725	2.84	1.71	1.14	1.71	341.13	15.16	12.32	985.47	1326.60	0.030
2.5	2.5	1.21	1.4725	5.13	3.67	1.46	3.67	733.28	18.95	13.82	1105.73	1839.01	0.042
3	3	1.71	1.9725	7.68	5.93	1.75	5.93	1186.85	22.74	15.06	1204.57	2391.42	0.055
3.5	3.5	2.21	2.4725	10.39	8.37	2.02	8.37	1674.15	26.53	16.14	1291.35	2965.50	0.068
4	4	2.71	2.9725	13.15	10.87	2.28	10.87	2173.25	30.32	17.17	1373.88	3547.13	0.081
4.5	4.5	3.21	3.4725	15.87	13.32	2.55	13.32	2663.83	34.11	18.24	1459.48	4123.31	0.095
5	5	3.71	3.9725	18.45	15.62	2.83	15.62	3124.44	37.9	19.45	1555.82	4680.26	0.107
5.5	5.5	4.21	4.4725	20.79	17.64	3.15	17.64	3528.74	41.69	20.90	1671.90	5200.64	0.119
6	6	4.71	4.9725	22.73	19.18	3.55	19.18	3835.51	45.48	22.75	1820.24	5655.74	0.130
6.5	6.5	5	5.4725	23.94	19.63	4.30	19.63	3926.99	49.27	25.33	2026.63	5953.62	0.137
7	7	5	5.525	23.97	19.63	4.34	19.63	3926.99	53.06	29.09	2326.82	6253.81	0.144
7.5	7.5	5	5.525	23.97	19.63	4.34	19.63	3926.99	56.85	32.88	2630.02	6557.01	0.151
7.58	7.58	5	5.525	23.97	19.63	4.34	19.63	3926.99	57.4564	33.48	2678.53	**6605.52**	0.152

INPUT DATA

SUBSURFACE SYSTEM NAME	C1	-
INNER DIAMETER OF SUBSURFACE SYSTEM	5	FT
OUTER DIAMETER OF SUBSURFACE SYSTEM	5.525	FT
NUMBER OF BARRELS	1	EA
LENGTH OF SUBSURFACE SYSTEM	200	FT
BOTTOM INVERT OF GRAVEL BED	0	FT
EFFECTIVE STORAGE ELEVATION	0	FT
PIPE SPACING	0	FT
EDGE THICKNESS	1.29	FT
TOP CLEARANCE, THICKNESS	1.29	FT
BOTTOM CLEARANCE, THICKNESS	1.29	FT
GRAVEL POROSITY, N	0.4	-
FT2 -> AC	43560	FT^2/AC

BASIN CC1 SUBSURFACE SYSTEM

1 Barrel 60-Inch Subsurface Infiltration Basin Volume Calculations

LENGTH OF SUBSURFACE SYSTEM (FT) = 180 **NUMBER OF CELLS 1**

Elevation	Depth	Inner Pipe Depth	Outer Pipe Depth	Outer Pipe Area Each (ft^2)	Inner Pipe Area Each (ft^2)	Pipe Thickness Area Each (ft^2)	Inner Pipe Area Total (ft^2)	Inner Pipe Total Gross Volume at Elev. (ft^3)	Gross Cross Sectional Area of System (ft^2)	Net Gravel Area (ft^2)	Gravel Volume (ft^3)	Cumulative Subsurface System Volume (ft^3)	Cumulative Subsurface System Volume (ac-ft)
0	0	0	0	0.00	0.00	0.00	0.00	0.00	0	0.00	0.00	0.00	0.000
0.5	0.5	0	0	0.00	0.00	0.00	0.00	0.00	3.79	3.79	272.88	272.88	0.006
1	1	0	0	0.00	0.00	0.00	0.00	0.00	7.58	7.58	545.76	545.76	0.013
1.5	1.5	0.21	0.4725	0.99	0.28	0.71	0.28	50.99	11.37	10.38	747.26	798.25	0.018
2	2	0.71	0.9725	2.84	1.71	1.14	1.71	307.01	15.16	12.32	886.93	1193.94	0.027
2.5	2.5	1.21	1.4725	5.13	3.67	1.46	3.67	659.95	18.95	13.82	995.16	1655.11	0.038
3	3	1.71	1.9725	7.68	5.93	1.75	5.93	1068.16	22.74	15.06	1084.11	2152.28	0.049
3.5	3.5	2.21	2.4725	10.39	8.37	2.02	8.37	1506.73	26.53	16.14	1162.22	2668.95	0.061
4	4	2.71	2.9725	13.15	10.87	2.28	10.87	1955.92	30.32	17.17	1236.49	3192.41	0.073
4.5	4.5	3.21	3.4725	15.87	13.32	2.55	13.32	2397.45	34.11	18.24	1313.53	3710.98	0.085
5	5	3.71	3.9725	18.45	15.62	2.83	15.62	2811.99	37.9	19.45	1400.24	4212.23	0.097
5.5	5.5	4.21	4.4725	20.79	17.64	3.15	17.64	3175.87	41.69	20.90	1504.71	4680.58	0.107
6	6	4.71	4.9725	22.73	19.18	3.55	19.18	3451.96	45.48	22.75	1638.21	5090.17	0.117
6.5	6.5	5	5.4725	23.94	19.63	4.30	19.63	3534.29	49.27	25.33	1823.96	5358.25	0.123
7	7	5	5.525	23.97	19.63	4.34	19.63	3534.29	53.06	29.09	2094.14	5628.43	0.129
7.5	7.5	5	5.525	23.97	19.63	4.34	19.63	3534.29	56.85	32.88	2367.02	5901.31	0.135
7.58	7.58	5	5.525	23.97	19.63	4.34	19.63	3534.29	57.4564	33.48	2410.68	**5944.97**	0.136

INPUT DATA

SUBSURFACE SYSTEM NAME	CC1	-
INNER DIAMETER OF SUBSURFACE SYSTEM	5	FT
OUTER DIAMETER OF SUBSURFACE SYSTEM	5.525	FT
NUMBER OF BARRELS	1	EA
LENGTH OF SUBSURFACE SYSTEM	180	FT
BOTTOM INVERT OF GRAVEL BED	0	FT
EFFECTIVE STORAGE ELEVATION	0	FT
PIPE SPACING	0	FT
EDGE THICKNESS	1.29	FT
TOP CLEARANCE, THICKNESS	1.29	FT
BOTTOM CLEARANCE, THICKNESS	1.29	FT
GRAVEL POROSITY, N	0.4	-
FT2 -> AC	43560	FT^2/AC

BASIN D1 SUBSURFACE SYSTEM

1 Barrel 60-Inch Subsurface Infiltration Basin Volume Calculations

LENGTH OF SUBSURFACE SYSTEM (FT) = 425 **NUMBER OF CELLS 1**

Elevation	Depth	Inner Pipe Depth	Outer Pipe Depth	Outer Pipe Area Each (ft^2)	Inner Pipe Area Each (ft^2)	Pipe Thickness Area Each (ft^2)	Inner Pipe Area Total (ft^2)	Inner Pipe Total Gross Volume at Elev. (ft^3)	Gross Cross Sectional Area of System (ft^2)	Net Gravel Area (ft^2)	Gravel Volume (ft^3)	Cumulative Subsurface System Volume (ft^3)	Cumulative Subsurface System Volume (ac-ft)
0	0	0	0	0.00	0.00	0.00	0.00	0.00	0	0.00	0.00	0.00	0.000
0.5	0.5	0	0	0.00	0.00	0.00	0.00	0.00	3.79	3.79	644.30	644.30	0.015
1	1	0	0	0.00	0.00	0.00	0.00	0.00	7.58	7.58	1288.60	1288.60	0.030
1.5	1.5	0.21	0.4725	0.99	0.28	0.71	0.28	120.39	11.37	10.38	1764.37	1884.76	0.043
2	2	0.71	0.9725	2.84	1.71	1.14	1.71	724.89	15.16	12.32	2094.13	2819.03	0.065
2.5	2.5	1.21	1.4725	5.13	3.67	1.46	3.67	1558.21	18.95	13.82	2349.68	3907.89	0.090
3	3	1.71	1.9725	7.68	5.93	1.75	5.93	2522.05	22.74	15.06	2559.71	5081.76	0.117
3.5	3.5	2.21	2.4725	10.39	8.37	2.02	8.37	3557.56	26.53	16.14	2744.13	6301.69	0.145
4	4	2.71	2.9725	13.15	10.87	2.28	10.87	4618.15	30.32	17.17	2919.49	7537.64	0.173
4.5	4.5	3.21	3.4725	15.87	13.32	2.55	13.32	5660.64	34.11	18.24	3101.39	8762.04	0.201
5	5	3.71	3.9725	18.45	15.62	2.83	15.62	6639.43	37.9	19.45	3306.12	9945.54	0.228
5.5	5.5	4.21	4.4725	20.79	17.64	3.15	17.64	7498.58	41.69	20.90	3552.79	11051.37	0.254
6	6	4.71	4.9725	22.73	19.18	3.55	19.18	8150.45	45.48	22.75	3868.01	12018.46	0.276
6.5	6.5	5	5.4725	23.94	19.63	4.30	19.63	8344.86	49.27	25.33	4306.58	12651.44	0.290
7	7	5	5.525	23.97	19.63	4.34	19.63	8344.86	53.06	29.09	4944.49	13289.34	0.305
7.5	7.5	5	5.525	23.97	19.63	4.34	19.63	8344.86	56.85	32.88	5588.79	13933.64	0.320
7.58	7.58	5	5.525	23.97	19.63	4.34	19.63	8344.86	57.4564	33.48	5691.88	**14036.73**	0.322

INPUT DATA

SUBSURFACE SYSTEM NAME	D1	-
INNER DIAMETER OF SUBSURFACE SYSTEM	5	FT
OUTER DIAMETER OF SUBSURFACE SYSTEM	5.525	FT
NUMBER OF BARRELS	1	EA
LENGTH OF SUBSURFACE SYSTEM	425	FT
BOTTOM INVERT OF GRAVEL BED	0	FT
EFFECTIVE STORAGE ELEVATION	0	FT
PIPE SPACING	0	FT
EDGE THICKNESS	1.29	FT
TOP CLEARANCE, THICKNESS	1.29	FT
BOTTOM CLEARANCE, THICKNESS	1.29	FT
GRAVEL POROSITY, N	0.4	-
FT2 -> AC	43560	FT^2/AC

BASIN DD1 SUBSURFACE SYSTEM

1 Barrel 60-Inch Subsurface Infiltration Basin Volume Calculations

LENGTH OF SUBSURFACE SYSTEM (FT) = 395 **NUMBER OF CELLS 1**

Elevation	Depth	Inner Pipe Depth	Outer Pipe Depth	Outer Pipe Area Each (ft^2)	Inner Pipe Area Each (ft^2)	Pipe Thickness Area Each (ft^2)	Inner Pipe Area Total (ft^2)	Inner Pipe Total Gross Volume at Elev. (ft^3)	Gross Cross Sectional Area of System (ft^2)	Net Gravel Area (ft^2)	Gravel Volume (ft^3)	Cumulative Subsurface System Volume (ft^3)	Cumulative Subsurface System Volume (ac-ft)
0	0	0	0	0.00	0.00	0.00	0.00	0.00	0	0.00	0.00	0.00	0.000
0.5	0.5	0	0	0.00	0.00	0.00	0.00	0.00	3.79	3.79	598.82	598.82	0.014
1	1	0	0	0.00	0.00	0.00	0.00	0.00	7.58	7.58	1197.64	1197.64	0.027
1.5	1.5	0.21	0.4725	0.99	0.28	0.71	0.28	111.89	11.37	10.38	1639.82	1751.71	0.040
2	2	0.71	0.9725	2.84	1.71	1.14	1.71	673.72	15.16	12.32	1946.31	2620.04	0.060
2.5	2.5	1.21	1.4725	5.13	3.67	1.46	3.67	1448.22	18.95	13.82	2183.82	3632.04	0.083
3	3	1.71	1.9725	7.68	5.93	1.75	5.93	2344.02	22.74	15.06	2379.03	4723.05	0.108
3.5	3.5	2.21	2.4725	10.39	8.37	2.02	8.37	3306.44	26.53	16.14	2550.42	5856.86	0.134
4	4	2.71	2.9725	13.15	10.87	2.28	10.87	4292.17	30.32	17.17	2713.41	7005.58	0.161
4.5	4.5	3.21	3.4725	15.87	13.32	2.55	13.32	5261.07	34.11	18.24	2882.47	8143.54	0.187
5	5	3.71	3.9725	18.45	15.62	2.83	15.62	6170.76	37.9	19.45	3072.74	9243.51	0.212
5.5	5.5	4.21	4.4725	20.79	17.64	3.15	17.64	6969.27	41.69	20.90	3302.01	10271.27	0.236
6	6	4.71	4.9725	22.73	19.18	3.55	19.18	7575.13	45.48	22.75	3594.97	11170.10	0.256
6.5	6.5	5	5.4725	23.94	19.63	4.30	19.63	7755.81	49.27	25.33	4002.59	11758.39	0.270
7	7	5	5.525	23.97	19.63	4.34	19.63	7755.81	53.06	29.09	4595.47	12351.27	0.284
7.5	7.5	5	5.525	23.97	19.63	4.34	19.63	7755.81	56.85	32.88	5194.29	12950.09	0.297
7.58	7.58	5	5.525	23.97	19.63	4.34	19.63	7755.81	57.4564	33.48	5290.10	**13045.90**	0.299

INPUT DATA

SUBSURFACE SYSTEM NAME	DD1	-
INNER DIAMETER OF SUBSURFACE SYSTEM	5	FT
OUTER DIAMETER OF SUBSURFACE SYSTEM	5.525	FT
NUMBER OF BARRELS	1	EA
LENGTH OF SUBSURFACE SYSTEM	395	FT
BOTTOM INVERT OF GRAVEL BED	0	FT
EFFECTIVE STORAGE ELEVATION	0	FT
PIPE SPACING	0	FT
EDGE THICKNESS	1.29	FT
TOP CLEARANCE, THICKNESS	1.29	FT
BOTTOM CLEARANCE, THICKNESS	1.29	FT
GRAVEL POROSITY, N	0.4	-
FT2 -> AC	43560	FT^2/AC

BASIN E1 SUBSURFACE SYSTEM

1 Barrel 60-Inch Subsurface Infiltration Basin Volume Calculations

LENGTH OF SUBSURFACE SYSTEM (FT) = 150 **NUMBER OF CELLS 1**

Elevation	Depth	Inner Pipe Depth	Outer Pipe Depth	Outer Pipe Area Each (ft^2)	Inner Pipe Area Each (ft^2)	Pipe Thickness Area Each (ft^2)	Inner Pipe Area Total (ft^2)	Inner Pipe Total Gross Volume at Elev. (ft^3)	Gross Cross Sectional Area of System (ft^2)	Net Gravel Area (ft^2)	Gravel Volume (ft^3)	Cumulative Subsurface System Volume (ft^3)	Cumulative Subsurface System Volume (ac-ft)
0	0	0	0	0.00	0.00	0.00	0.00	0.00	0	0.00	0.00	0.00	0.000
0.5	0.5	0	0	0.00	0.00	0.00	0.00	0.00	3.79	3.79	227.40	227.40	0.005
1	1	0	0	0.00	0.00	0.00	0.00	0.00	7.58	7.58	454.80	454.80	0.010
1.5	1.5	0.21	0.4725	0.99	0.28	0.71	0.28	42.49	11.37	10.38	622.72	665.21	0.015
2	2	0.71	0.9725	2.84	1.71	1.14	1.71	255.84	15.16	12.32	739.11	994.95	0.023
2.5	2.5	1.21	1.4725	5.13	3.67	1.46	3.67	549.96	18.95	13.82	829.30	1379.26	0.032
3	3	1.71	1.9725	7.68	5.93	1.75	5.93	890.14	22.74	15.06	903.43	1793.56	0.041
3.5	3.5	2.21	2.4725	10.39	8.37	2.02	8.37	1255.61	26.53	16.14	968.52	2224.13	0.051
4	4	2.71	2.9725	13.15	10.87	2.28	10.87	1629.94	30.32	17.17	1030.41	2660.35	0.061
4.5	4.5	3.21	3.4725	15.87	13.32	2.55	13.32	1997.87	34.11	18.24	1094.61	3092.48	0.071
5	5	3.71	3.9725	18.45	15.62	2.83	15.62	2343.33	37.9	19.45	1166.86	3510.19	0.081
5.5	5.5	4.21	4.4725	20.79	17.64	3.15	17.64	2646.56	41.69	20.90	1253.93	3900.48	0.090
6	6	4.71	4.9725	22.73	19.18	3.55	19.18	2876.63	45.48	22.75	1365.18	4241.81	0.097
6.5	6.5	5	5.4725	23.94	19.63	4.30	19.63	2945.24	49.27	25.33	1519.97	4465.21	0.103
7	7	5	5.525	23.97	19.63	4.34	19.63	2945.24	53.06	29.09	1745.11	4690.36	0.108
7.5	7.5	5	5.525	23.97	19.63	4.34	19.63	2945.24	56.85	32.88	1972.51	4917.76	0.113
7.58	7.58	5	5.525	23.97	19.63	4.34	19.63	2945.24	57.4564	33.48	2008.90	**4954.14**	0.114

INPUT DATA

SUBSURFACE SYSTEM NAME	E1	-
INNER DIAMETER OF SUBSURFACE SYSTEM	5	FT
OUTER DIAMETER OF SUBSURFACE SYSTEM	5.525	FT
NUMBER OF BARRELS	1	EA
LENGTH OF SUBSURFACE SYSTEM	150	FT
BOTTOM INVERT OF GRAVEL BED	0	FT
EFFECTIVE STORAGE ELEVATION	0	FT
PIPE SPACING	0	FT
EDGE THICKNESS	1.29	FT
TOP CLEARANCE, THICKNESS	1.29	FT
BOTTOM CLEARANCE, THICKNESS	1.29	FT
GRAVEL POROSITY, N	0.4	-
FT2 -> AC	43560	FT^2/AC

BASIN EE1 SUBSURFACE SYSTEM

1 Barrel 60-Inch Subsurface Infiltration Basin Volume Calculations

LENGTH OF SUBSURFACE SYSTEM (FT) = 145 **NUMBER OF CELLS 1**

Elevation	Depth	Inner Pipe Depth	Outer Pipe Depth	Outer Pipe Area Each (ft^2)	Inner Pipe Area Each (ft^2)	Pipe Thickness Area Each (ft^2)	Inner Pipe Area Total (ft^2)	Inner Pipe Total Gross Volume at Elev. (ft^3)	Gross Cross Sectional Area of System (ft^2)	Net Gravel Area (ft^2)	Gravel Volume (ft^3)	Cumulative Subsurface System Volume (ft^3)	Cumulative Subsurface System Volume (ac-ft)
0	0	0	0	0.00	0.00	0.00	0.00	0.00	0	0.00	0.00	0.00	0.000
0.5	0.5	0	0	0.00	0.00	0.00	0.00	0.00	3.79	3.79	219.82	219.82	0.005
1	1	0	0	0.00	0.00	0.00	0.00	0.00	7.58	7.58	439.64	439.64	0.010
1.5	1.5	0.21	0.4725	0.99	0.28	0.71	0.28	41.07	11.37	10.38	601.96	643.03	0.015
2	2	0.71	0.9725	2.84	1.71	1.14	1.71	247.32	15.16	12.32	714.47	961.79	0.022
2.5	2.5	1.21	1.4725	5.13	3.67	1.46	3.67	531.63	18.95	13.82	801.65	1333.28	0.031
3	3	1.71	1.9725	7.68	5.93	1.75	5.93	860.46	22.74	15.06	873.31	1733.78	0.040
3.5	3.5	2.21	2.4725	10.39	8.37	2.02	8.37	1213.76	26.53	16.14	936.23	2149.99	0.049
4	4	2.71	2.9725	13.15	10.87	2.28	10.87	1575.60	30.32	17.17	996.06	2571.67	0.059
4.5	4.5	3.21	3.4725	15.87	13.32	2.55	13.32	1931.28	34.11	18.24	1058.12	2989.40	0.069
5	5	3.71	3.9725	18.45	15.62	2.83	15.62	2265.22	37.9	19.45	1127.97	3393.19	0.078
5.5	5.5	4.21	4.4725	20.79	17.64	3.15	17.64	2558.34	41.69	20.90	1212.13	3770.47	0.087
6	6	4.71	4.9725	22.73	19.18	3.55	19.18	2780.74	45.48	22.75	1319.67	4100.41	0.094
6.5	6.5	5	5.4725	23.94	19.63	4.30	19.63	2847.07	49.27	25.33	1469.30	4316.37	0.099
7	7	5	5.525	23.97	19.63	4.34	19.63	2847.07	53.06	29.09	1686.94	4534.01	0.104
7.5	7.5	5	5.525	23.97	19.63	4.34	19.63	2847.07	56.85	32.88	1906.76	4753.83	0.109
7.58	7.58	5	5.525	23.97	19.63	4.34	19.63	2847.07	57.4564	33.48	1941.93	**4789.00**	0.110

INPUT DATA

SUBSURFACE SYSTEM NAME	EE1	-
INNER DIAMETER OF SUBSURFACE SYSTEM	5	FT
OUTER DIAMETER OF SUBSURFACE SYSTEM	5.525	FT
NUMBER OF BARRELS	1	EA
LENGTH OF SUBSURFACE SYSTEM	145	FT
BOTTOM INVERT OF GRAVEL BED	0	FT
EFFECTIVE STORAGE ELEVATION	0	FT
PIPE SPACING	0	FT
EDGE THICKNESS	1.29	FT
TOP CLEARANCE, THICKNESS	1.29	FT
BOTTOM CLEARANCE, THICKNESS	1.29	FT
GRAVEL POROSITY, N	0.4	-
FT2 -> AC	43560	FT^2/AC

INFILTRATION RATE CALCULATION

Infiltration Rate Calculation	
infiltration rate (in/hr)	4.8
safety factor	3
adjusted infiltration rate (in/hr)	1.60
adjusted infiltration rate (ft/s)	0.0000370
*unit infiltration outflow (cfs)	0.0000370
*outflow per unit area (=1 ft^2)	

Infiltration Outflow by Basin				
Basin Name	Basin Length (ft)	*Basin Bottom Area (ft^2)	**unit infiltration outflow (cfs)	infiltration outflow (cfs)
A1	325	2463.5	0.0000370	0.091
AA1	305	2311.9	0.0000370	0.086
B1	370	2804.6	0.0000370	0.104
BB1	360	2728.8	0.0000370	0.101
C1	200	1516	0.0000370	0.056
CC1	180	1364.4	0.0000370	0.051
D1	425	3221.5	0.0000370	0.119
DD1	395	2994.1	0.0000370	0.111
E1	150	1137	0.0000370	0.042
EE1	145	1099.1	0.0000370	0.041
*Width=7.58 ft				
**outflow per unit area (=1 ft^2)				

STAGE-STORAGE-OUTFLOW TABLES

Stage-Storage-Outflow: Basin A1			
Stage	Storage (ft^3)	Storage (ac-ft)	Outflow (cfs)
0	0.0	0.000	0
0.5	492.7	0.011	0.091
1	985.4	0.023	0.091
1.5	1441.3	0.033	0.091
2	2155.7	0.049	0.091
2.5	2988.4	0.069	0.091
3	3886.1	0.089	0.091
3.5	4818.9	0.111	0.091
4	5764.1	0.132	0.091
4.5	6700.4	0.154	0.091
5	7605.4	0.175	0.091
5.5	8451.0	0.194	0.091
6	9190.6	0.211	0.091
6.5	9674.6	0.222	0.091
7	10162.4	0.233	0.091
7.5	10655.1	0.245	0.091
7.58	10734.0	0.246	0.091

Stage-Storage-Outflow: Basin AA1			
Stage	Storage (ft^3)	Storage (ac-ft)	Outflow (cfs)
0	0.0	0.000	0
0.5	462.4	0.011	0.086
1	924.8	0.021	0.086
1.5	1352.6	0.031	0.086
2	2023.1	0.046	0.086
2.5	2804.5	0.064	0.086
3	3646.9	0.084	0.086
3.5	4522.4	0.104	0.086
4	5409.4	0.124	0.086
4.5	6288.0	0.144	0.086
5	7137.4	0.164	0.086
5.5	7931.0	0.182	0.086
6	8625.0	0.198	0.086
6.5	9079.3	0.208	0.086
7	9537.1	0.219	0.086
7.5	9999.4	0.230	0.086
7.58	10073.4	0.231	0.086

Stage-Storage-Outflow: Basin B1			
Stage	Storage (ft^3)	Storage (ac-ft)	Outflow (cfs)
0	0.0	0.000	0
0.5	560.9	0.013	0.104
1	1121.8	0.026	0.104
1.5	1640.8	0.038	0.104
2	2454.2	0.056	0.104
2.5	3402.2	0.078	0.104
3	4424.1	0.102	0.104
3.5	5486.2	0.126	0.104
4	6562.2	0.151	0.104
4.5	7628.1	0.175	0.104
5	8658.5	0.199	0.104
5.5	9621.2	0.221	0.104
6	10463.1	0.240	0.104
6.5	11014.2	0.253	0.104
7	11569.5	0.266	0.104
7.5	12130.5	0.278	0.104
7.58	12220.2	0.281	0.104

Stage-Storage-Outflow: Basin BB1			
Stage	Storage (ft^3)	Storage (ac-ft)	Outflow (cfs)
0	0.0	0.000	0
0.5	545.8	0.013	0.101
1	1091.5	0.025	0.101
1.5	1596.5	0.037	0.101
2	2387.9	0.055	0.101
2.5	3310.2	0.076	0.101
3	4304.6	0.099	0.101
3.5	5337.9	0.123	0.101
4	6384.8	0.147	0.101
4.5	7422.0	0.170	0.101
5	8424.5	0.193	0.101
5.5	9361.2	0.215	0.101
6	10180.3	0.234	0.101
6.5	10716.5	0.246	0.101
7	11256.9	0.258	0.101
7.5	11802.6	0.271	0.101
7.58	11889.9	0.273	0.101

Stage-Storage-Outflow: Basin C1			
Stage	Storage (ft^3)	Storage (ac-ft)	Outflow (cfs)
0	0.0	0.000	0
0.5	303.2	0.007	0.056
1	606.4	0.014	0.056
1.5	886.9	0.020	0.056
2	1326.6	0.030	0.056
2.5	1839.0	0.042	0.056
3	2391.4	0.055	0.056
3.5	2965.5	0.068	0.056
4	3547.1	0.081	0.056
4.5	4123.3	0.095	0.056
5	4680.3	0.107	0.056
5.5	5200.6	0.119	0.056
6	5655.7	0.130	0.056
6.5	5953.6	0.137	0.056
7	6253.8	0.144	0.056
7.5	6557.0	0.151	0.056
7.58	6605.5	0.152	0.056

Stage-Storage-Outflow: Basin CC1			
Stage	Storage (ft^3)	Storage (ac-ft)	Outflow (cfs)
0	0.0	0.000	0
0.5	272.9	0.006	0.051
1	545.8	0.013	0.051
1.5	798.2	0.018	0.051
2	1193.9	0.027	0.051
2.5	1655.1	0.038	0.051
3	2152.3	0.049	0.051
3.5	2669.0	0.061	0.051
4	3192.4	0.073	0.051
4.5	3711.0	0.085	0.051
5	4212.2	0.097	0.051
5.5	4680.6	0.107	0.051
6	5090.2	0.117	0.051
6.5	5358.3	0.123	0.051
7	5628.4	0.129	0.051
7.5	5901.3	0.135	0.051
7.58	5945.0	0.136	0.051

Stage-Storage-Outflow: Basin D1			
Stage	Storage (ft^3)	Storage (ac-ft)	Outflow (cfs)
0	0.0	0.000	0
0.5	644.3	0.015	0.119
1	1288.6	0.030	0.119
1.5	1884.8	0.043	0.119
2	2819.0	0.065	0.119
2.5	3907.9	0.090	0.119
3	5081.8	0.117	0.119
3.5	6301.7	0.145	0.119
4	7537.6	0.173	0.119
4.5	8762.0	0.201	0.119
5	9945.5	0.228	0.119
5.5	11051.4	0.254	0.119
6	12018.5	0.276	0.119
6.5	12651.4	0.290	0.119
7	13289.3	0.305	0.119
7.5	13933.6	0.320	0.119
7.58	14036.7	0.322	0.119

Stage-Storage-Outflow: Basin DD1			
Stage	Storage (ft^3)	Storage (ac-ft)	Outflow (cfs)
0	0.0	0.000	0
0.5	598.8	0.014	0.111
1	1197.6	0.027	0.111
1.5	1751.7	0.040	0.111
2	2620.0	0.060	0.111
2.5	3632.0	0.083	0.111
3	4723.0	0.108	0.111
3.5	5856.9	0.134	0.111
4	7005.6	0.161	0.111
4.5	8143.5	0.187	0.111
5	9243.5	0.212	0.111
5.5	10271.3	0.236	0.111
6	11170.1	0.256	0.111
6.5	11758.4	0.270	0.111
7	12351.3	0.284	0.111
7.5	12950.1	0.297	0.111
7.58	13045.9	0.299	0.111

Stage-Storage-Outflow: Basin E1			
Stage	Storage (ft^3)	Storage (ac-ft)	Outflow (cfs)
0	0.0	0.000	0
0.5	227.4	0.005	0.042
1	454.8	0.010	0.042
1.5	665.2	0.015	0.042
2	995.0	0.023	0.042
2.5	1379.3	0.032	0.042
3	1793.6	0.041	0.042
3.5	2224.1	0.051	0.042
4	2660.3	0.061	0.042
4.5	3092.5	0.071	0.042
5	3510.2	0.081	0.042
5.5	3900.5	0.090	0.042
6	4241.8	0.097	0.042
6.5	4465.2	0.103	0.042
7	4690.4	0.108	0.042
7.5	4917.8	0.113	0.042
7.58	4954.1	0.114	0.042

Stage-Storage-Outflow: Basin EE1			
Stage	Storage (ft^3)	Storage (ac-ft)	Outflow (cfs)
0	0.0	0.000	0
0.5	219.8	0.005	0.041
1	439.6	0.010	0.041
1.5	643.0	0.015	0.041
2	961.8	0.022	0.041
2.5	1333.3	0.031	0.041
3	1733.8	0.040	0.041
3.5	2150.0	0.049	0.041
4	2571.7	0.059	0.041
4.5	2989.4	0.069	0.041
5	3393.2	0.078	0.041
5.5	3770.5	0.087	0.041
6	4100.4	0.094	0.041
6.5	4316.4	0.099	0.041
7	4534.0	0.104	0.041
7.5	4753.8	0.109	0.041
7.58	4789.0	0.110	0.041

INFILTRATION ROUTING FOR DRAINAGE AREAS

AREA A1

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 07/21/25

ROUTING: BASIN A1; UNIT HYDROGRAPH A1

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARA124100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 290
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.657 (CFS)
Total volume = 0.381 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 101.000 to Point/Station 102.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 290
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.011	0.091	0.011	0.011
1.000	0.023	0.091	0.023	0.023
1.500	0.033	0.091	0.033	0.033
2.000	0.049	0.091	0.049	0.049
2.500	0.069	0.091	0.069	0.069
3.000	0.089	0.091	0.089	0.089
3.500	0.111	0.091	0.111	0.111
4.000	0.132	0.091	0.132	0.132
4.500	0.154	0.091	0.154	0.154
5.000	0.175	0.091	0.175	0.175
5.500	0.194	0.091	0.194	0.194
6.000	0.211	0.091	0.211	0.211
6.500	0.222	0.091	0.222	0.222
7.000	0.233	0.091	0.233	0.233
7.500	0.245	0.091	0.245	0.245
7.580	0.246	0.091	0.246	0.246

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.2	0.33	0.49	0.66	Depth (Ft.)
0.083	0.02	0.00	0.000	O	|	|	|	|	0.00
0.167	0.03	0.00	0.000	OI	|	|	|	|	0.01
0.250	0.04	0.00	0.000	OI	|	|	|	|	0.02
0.333	0.05	0.01	0.001	O I	|	|	|	|	0.03
0.417	0.05	0.01	0.001	O I	|	|	|	|	0.05
0.500	0.06	0.01	0.001	O I	|	|	|	|	0.06
0.583	0.06	0.01	0.002	O I	|	|	|	|	0.07
0.667	0.06	0.02	0.002	O I	|	|	|	|	0.09
0.750	0.06	0.02	0.002	O I	|	|	|	|	0.10
0.833	0.07	0.02	0.002	O I	|	|	|	|	0.11
0.917	0.07	0.02	0.003	|O I	|	|	|	|	0.13
1.000	0.07	0.03	0.003	|O I	|	|	|	|	0.14
1.083	0.06	0.03	0.003	|O I	|	|	|	|	0.15
1.167	0.06	0.03	0.004	|OI	|	|	|	|	0.16
1.250	0.06	0.03	0.004	|OI	|	|	|	|	0.17
1.333	0.06	0.03	0.004	|OI	|	|	|	|	0.18
1.417	0.06	0.03	0.004	|OI	|	|	|	|	0.19
1.500	0.06	0.03	0.004	|OI	|	|	|	|	0.19
1.583	0.06	0.04	0.004	|OI	|	|	|	|	0.20
1.667	0.06	0.04	0.004	|OI	|	|	|	|	0.20
1.750	0.06	0.04	0.005	|OI	|	|	|	|	0.21
1.833	0.07	0.04	0.005	|O I	|	|	|	|	0.22
1.917	0.07	0.04	0.005	|O I	|	|	|	|	0.23
2.000	0.07	0.04	0.005	| OI	|	|	|	|	0.23
2.083	0.07	0.04	0.005	| OI	|	|	|	|	0.24

2.167	0.07	0.05	0.006	OI				0.25
2.250	0.07	0.05	0.006	OI				0.26
2.333	0.07	0.05	0.006	OI				0.27
2.417	0.07	0.05	0.006	OI				0.28
2.500	0.07	0.05	0.006	OI				0.28
2.583	0.08	0.05	0.006	O I				0.29
2.667	0.09	0.05	0.007	O I				0.30
2.750	0.09	0.06	0.007	O I				0.31
2.833	0.09	0.06	0.007	O I				0.32
2.917	0.09	0.06	0.007	O I				0.33
3.000	0.09	0.06	0.008	OI				0.34
3.083	0.09	0.06	0.008	OI				0.35
3.167	0.09	0.07	0.008	OI				0.36
3.250	0.09	0.07	0.008	OI				0.37
3.333	0.09	0.07	0.008	OI				0.38
3.417	0.09	0.07	0.008	OI				0.38
3.500	0.09	0.07	0.009	OI				0.39
3.583	0.09	0.07	0.009	OI				0.40
3.667	0.09	0.07	0.009	OI				0.40
3.750	0.09	0.07	0.009	OI				0.41
3.833	0.10	0.08	0.009	OI				0.41
3.917	0.11	0.08	0.009	O I				0.42
4.000	0.11	0.08	0.010	O I				0.43
4.083	0.11	0.08	0.010	O I				0.44
4.167	0.11	0.08	0.010	OI				0.45
4.250	0.11	0.08	0.010	OI				0.46
4.333	0.12	0.09	0.010	OI				0.47
4.417	0.13	0.09	0.011	O I				0.48
4.500	0.13	0.09	0.011	O I				0.49
4.583	0.13	0.09	0.011	O I				0.51
4.667	0.13	0.09	0.011	O I				0.52
4.750	0.13	0.09	0.012	O I				0.53
4.833	0.14	0.09	0.012	O I				0.54
4.917	0.15	0.09	0.012	O I				0.55
5.000	0.15	0.09	0.013	O I				0.57
5.083	0.13	0.09	0.013	O I				0.58
5.167	0.11	0.09	0.013	OI				0.59
5.250	0.11	0.09	0.013	OI				0.60
5.333	0.12	0.09	0.013	OI				0.60
5.417	0.13	0.09	0.014	O I				0.61
5.500	0.13	0.09	0.014	O I				0.62
5.583	0.14	0.09	0.014	O I				0.64
5.667	0.15	0.09	0.015	O I				0.65
5.750	0.15	0.09	0.015	O I				0.67
5.833	0.15	0.09	0.015	O I				0.68
5.917	0.15	0.09	0.016	O I				0.70
6.000	0.15	0.09	0.016	O I				0.71
6.083	0.16	0.09	0.017	O I				0.73
6.167	0.16	0.09	0.017	O I				0.75
6.250	0.17	0.09	0.018	O I				0.77
6.333	0.17	0.09	0.018	O I				0.79
6.417	0.17	0.09	0.019	O I				0.81
6.500	0.17	0.09	0.019	O I				0.84

6.583	0.18	0.09	0.020	|	O	I	|	|	0.86
6.667	0.18	0.09	0.020	|	O	I	|	|	0.88
6.750	0.18	0.09	0.021	|	O	I	|	|	0.91
6.833	0.18	0.09	0.021	|	O	I	|	|	0.94
6.917	0.18	0.09	0.022	|	O	I	|	|	0.96
7.000	0.18	0.09	0.023	|	O	I	|	|	0.99
7.083	0.18	0.09	0.023	|	O	I	|	|	1.02
7.167	0.18	0.09	0.024	|	O	I	|	|	1.05
7.250	0.18	0.09	0.025	|	O	I	|	|	1.08
7.333	0.19	0.09	0.025	|	O	|I	|	|	1.12
7.417	0.20	0.09	0.026	|	O	|I	|	|	1.15
7.500	0.20	0.09	0.027	|	O	|I	|	|	1.19
7.583	0.21	0.09	0.028	|	O	| I	|	|	1.23
7.667	0.22	0.09	0.028	|	O	| I	|	|	1.27
7.750	0.22	0.09	0.029	|	O	| I	|	|	1.32
7.833	0.23	0.09	0.030	|	O	| I	|	|	1.36
7.917	0.24	0.09	0.031	|	O	| I	|	|	1.41
8.000	0.24	0.09	0.032	|	O	| I	|	|	1.46
8.083	0.26	0.09	0.033	|	O	| I	|	|	1.51
8.167	0.27	0.09	0.035	|	O	| I	|	|	1.55
8.250	0.28	0.09	0.036	|	O	| I	|	|	1.59
8.333	0.28	0.09	0.037	|	O	| I	|	|	1.63
8.417	0.28	0.09	0.038	|	O	| I	|	|	1.67
8.500	0.28	0.09	0.040	|	O	| I	|	|	1.71
8.583	0.29	0.09	0.041	|	O	| I	|	|	1.75
8.667	0.29	0.09	0.042	|	O	| I	|	|	1.79
8.750	0.29	0.09	0.044	|	O	| I	|	|	1.83
8.833	0.30	0.09	0.045	|	O	| I	|	|	1.88
8.917	0.31	0.09	0.047	|	O	| I|	|	|	1.93
9.000	0.31	0.09	0.048	|	O	| I|	|	|	1.97
9.083	0.33	0.09	0.050	|	O	| I	|	|	2.02
9.167	0.35	0.09	0.051	|	O	| I	|	|	2.06
9.250	0.35	0.09	0.053	|	O	| I	|	|	2.10
9.333	0.36	0.09	0.055	|	O	| |I	|	|	2.15
9.417	0.37	0.09	0.057	|	O	| |I	|	|	2.20
9.500	0.37	0.09	0.059	|	O	| |I	|	|	2.24
9.583	0.38	0.09	0.061	|	O	| | I	|	|	2.29
9.667	0.38	0.09	0.063	|	O	| | I	|	|	2.34
9.750	0.39	0.09	0.065	|	O	| | I	|	|	2.39
9.833	0.40	0.09	0.067	|	O	| | I	|	|	2.44
9.917	0.40	0.09	0.069	|	O	| | I	|	|	2.50
10.000	0.40	0.09	0.071	|	O	| | I	|	|	2.55
10.083	0.33	0.09	0.073	|	O	| I	|	|	2.60
10.167	0.28	0.09	0.074	|	O	| I	|	|	2.64
10.250	0.28	0.09	0.076	|	O	| I	|	|	2.67
10.333	0.28	0.09	0.077	|	O	| I	|	|	2.70
10.417	0.28	0.09	0.078	|	O	| I	|	|	2.73
10.500	0.28	0.09	0.080	|	O	| I	|	|	2.76
10.583	0.33	0.09	0.081	|	O	| I|	|	|	2.80
10.667	0.36	0.09	0.083	|	O	| |I	|	|	2.84
10.750	0.37	0.09	0.085	|	O	| |I	|	|	2.89
10.833	0.37	0.09	0.087	|	O	| |I	|	|	2.94
10.917	0.37	0.09	0.088	|	O	| |I	|	|	2.98

11.000	0.37	0.09	0.090	|	O	|	|I	|	3.03
11.083	0.36	0.09	0.092	|	O	|	|I	|	3.07
11.167	0.35	0.09	0.094	|	O	|	|I	|	3.11
11.250	0.35	0.09	0.096	|	O	|	I	|	3.15
11.333	0.35	0.09	0.098	|	O	|	I	|	3.19
11.417	0.35	0.09	0.099	|	O	|	I	|	3.23
11.500	0.35	0.09	0.101	|	O	|	I	|	3.27
11.583	0.33	0.09	0.103	|	O	|	I|	|	3.31
11.667	0.31	0.09	0.104	|	O	|	I|	|	3.35
11.750	0.31	0.09	0.106	|	O	|	I|	|	3.38
11.833	0.32	0.09	0.107	|	O	|	I|	|	3.42
11.917	0.33	0.09	0.109	|	O	|	I	|	3.46
12.000	0.33	0.09	0.111	|	O	|	I	|	3.49
12.083	0.40	0.09	0.113	|	O	|	| I	|	3.54
12.167	0.45	0.09	0.115	|	O	|	| I	|	3.59
12.250	0.46	0.09	0.117	|	O	|	| I	|	3.65
12.333	0.47	0.09	0.120	|	O	|	| I	|	3.71
12.417	0.48	0.09	0.123	|	O	|	| I|	|	3.78
12.500	0.48	0.09	0.125	|	O	|	| I|	|	3.84
12.583	0.50	0.09	0.128	|	O	|	| I	|	3.90
12.667	0.51	0.09	0.131	|	O	|	| I	|	3.97
12.750	0.51	0.09	0.134	|	O	|	|I	|	4.04
12.833	0.53	0.09	0.137	|	O	|	|I	|	4.11
12.917	0.54	0.09	0.140	|	O	|	| I	|	4.18
13.000	0.54	0.09	0.143	|	O	|	| I	|	4.24
13.083	0.60	0.09	0.146	|	O	|	| I	|	4.32
13.167	0.65	0.09	0.150	|	O	|	| I|	|	4.40
13.250	0.65	0.09	0.154	|	O	|	| I|	|	4.49
13.333	0.66	0.09	0.157	|	O	|	| I|	|	4.58
13.417	0.66	0.09	0.161	|	O	|	| I|	|	4.68
13.500	0.66	0.09	0.165	|	O	|	| I	|	4.77
13.583	0.53	0.09	0.169	|	O	|	|I	|	4.85
13.667	0.43	0.09	0.171	|	O	|	| I	|	4.91
13.750	0.42	0.09	0.174	|	O	|	| I	|	4.97
13.833	0.42	0.09	0.176	|	O	|	| I	|	5.03
13.917	0.42	0.09	0.178	|	O	|	| I	|	5.09
14.000	0.42	0.09	0.181	|	O	|	| I	|	5.15
14.083	0.47	0.09	0.183	|	O	|	| I	|	5.21
14.167	0.50	0.09	0.186	|	O	|	| I	|	5.28
14.250	0.50	0.09	0.188	|	O	|	| I	|	5.36
14.333	0.49	0.09	0.191	|	O	|	| I|	|	5.43
14.417	0.48	0.09	0.194	|	O	|	| I|	|	5.50
14.500	0.48	0.09	0.197	|	O	|	| I|	|	5.58
14.583	0.48	0.09	0.199	|	O	|	| I|	|	5.66
14.667	0.48	0.09	0.202	|	O	|	| I|	|	5.74
14.750	0.48	0.09	0.205	|	O	|	| I|	|	5.82
14.833	0.47	0.09	0.207	|	O	|	| I	|	5.89
14.917	0.46	0.09	0.210	|	O	|	| I	|	5.97
15.000	0.46	0.09	0.213	|	O	|	| I	|	6.07
15.083	0.45	0.09	0.215	|	O	|	| I	|	6.18
15.167	0.44	0.09	0.217	|	O	|	| I	|	6.29
15.250	0.44	0.09	0.220	|	O	|	| I	|	6.40
15.333	0.43	0.09	0.222	|	O	|	| I	|	6.51

15.417	0.42	0.09	0.225	| O |		| I |			6.62
15.500	0.42	0.09	0.227	| O |		| I |			6.72
15.583	0.38	0.09	0.229	| O |		| I |			6.82
15.667	0.35	0.09	0.231	| O |		|I |			6.90
15.750	0.35	0.09	0.233	| O |		I |			6.98
15.833	0.35	0.09	0.234	| O |		I |			7.06
15.917	0.35	0.09	0.236	| O |		I |			7.13
16.000	0.35	0.09	0.238	| O |		I |			7.21
16.083	0.20	0.09	0.239	| O |	I |				7.26
16.167	0.09	0.09	0.240	| O |		|			7.27
16.250	0.07	0.09	0.240	| IO |		|			7.27
16.333	0.07	0.09	0.239	| IO |		|			7.27
16.417	0.07	0.09	0.239	| IO |		|			7.26
16.500	0.07	0.09	0.239	| IO |		|			7.26
16.583	0.06	0.09	0.239	| IO |		|			7.25
16.667	0.06	0.09	0.239	| I O |		|			7.24
16.750	0.06	0.09	0.239	| I O |		|			7.23
16.833	0.06	0.09	0.238	| I O |		|			7.22
16.917	0.06	0.09	0.238	| I O |		|			7.21
17.000	0.06	0.09	0.238	| I O |		|			7.20
17.083	0.08	0.09	0.238	| IO |		|			7.19
17.167	0.09	0.09	0.238	| O |		|			7.19
17.250	0.09	0.09	0.238	| O |		|			7.19
17.333	0.09	0.09	0.238	| O |		|			7.19
17.417	0.09	0.09	0.238	| O |		|			7.19
17.500	0.09	0.09	0.238	| O |		|			7.19
17.583	0.09	0.09	0.238	| O |		|			7.19
17.667	0.09	0.09	0.238	| O |		|			7.19
17.750	0.09	0.09	0.238	| O |		|			7.19
17.833	0.08	0.09	0.238	| IO |		|			7.19
17.917	0.07	0.09	0.237	| IO |		|			7.19
18.000	0.07	0.09	0.237	| IO |		|			7.18
18.083	0.07	0.09	0.237	| IO |		|			7.18
18.167	0.07	0.09	0.237	| IO |		|			7.17
18.250	0.07	0.09	0.237	| IO |		|			7.17
18.333	0.07	0.09	0.237	| IO |		|			7.16
18.417	0.07	0.09	0.237	| IO |		|			7.16
18.500	0.07	0.09	0.237	| IO |		|			7.15
18.583	0.06	0.09	0.236	| IO |		|			7.14
18.667	0.06	0.09	0.236	| I O |		|			7.13
18.750	0.06	0.09	0.236	| I O |		|			7.12
18.833	0.04	0.09	0.236	| I O |		|			7.11
18.917	0.04	0.09	0.235	|I O |		|			7.10
19.000	0.04	0.09	0.235	|I O |		|			7.08
19.083	0.05	0.09	0.235	| I O |		|			7.07
19.167	0.05	0.09	0.234	| I O |		|			7.06
19.250	0.06	0.09	0.234	| I O |		|			7.05
19.333	0.07	0.09	0.234	| IO |		|			7.04
19.417	0.07	0.09	0.234	| IO |		|			7.03
19.500	0.07	0.09	0.234	| IO |		|			7.03
19.583	0.06	0.09	0.233	| IO |		|			7.02
19.667	0.06	0.09	0.233	| I O |		|			7.01
19.750	0.06	0.09	0.233	| I O |		|			7.00

19.833	0.04	0.09	0.233	| I O	|	|	|	6.99
19.917	0.04	0.09	0.232	|I O	|	|	|	6.97
20.000	0.04	0.09	0.232	|I O	|	|	|	6.96
20.083	0.05	0.09	0.232	| I O	|	|	|	6.94
20.167	0.05	0.09	0.231	| I O	|	|	|	6.93
20.250	0.06	0.09	0.231	| I O	|	|	|	6.92
20.333	0.06	0.09	0.231	| I O	|	|	|	6.90
20.417	0.06	0.09	0.231	| I O	|	|	|	6.89
20.500	0.06	0.09	0.230	| I O	|	|	|	6.88
20.583	0.06	0.09	0.230	| I O	|	|	|	6.87
20.667	0.06	0.09	0.230	| I O	|	|	|	6.86
20.750	0.06	0.09	0.230	| I O	|	|	|	6.85
20.833	0.04	0.09	0.229	| I O	|	|	|	6.84
20.917	0.04	0.09	0.229	|I O	|	|	|	6.82
21.000	0.04	0.09	0.229	|I O	|	|	|	6.80
21.083	0.05	0.09	0.228	| I O	|	|	|	6.79
21.167	0.05	0.09	0.228	| I O	|	|	|	6.78
21.250	0.06	0.09	0.228	| I O	|	|	|	6.76
21.333	0.04	0.09	0.228	| I O	|	|	|	6.75
21.417	0.04	0.09	0.227	|I O	|	|	|	6.74
21.500	0.04	0.09	0.227	|I O	|	|	|	6.72
21.583	0.05	0.09	0.226	| I O	|	|	|	6.70
21.667	0.05	0.09	0.226	| I O	|	|	|	6.69
21.750	0.06	0.09	0.226	| I O	|	|	|	6.68
21.833	0.04	0.09	0.226	| I O	|	|	|	6.67
21.917	0.04	0.09	0.225	|I O	|	|	|	6.65
22.000	0.04	0.09	0.225	|I O	|	|	|	6.63
22.083	0.05	0.09	0.225	| I O	|	|	|	6.62
22.167	0.05	0.09	0.224	| I O	|	|	|	6.61
22.250	0.06	0.09	0.224	| I O	|	|	|	6.59
22.333	0.04	0.09	0.224	| I O	|	|	|	6.58
22.417	0.04	0.09	0.223	|I O	|	|	|	6.57
22.500	0.04	0.09	0.223	|I O	|	|	|	6.55
22.583	0.04	0.09	0.223	|I O	|	|	|	6.53
22.667	0.04	0.09	0.222	|I O	|	|	|	6.51
22.750	0.04	0.09	0.222	|I O	|	|	|	6.50
22.833	0.04	0.09	0.222	|I O	|	|	|	6.48
22.917	0.04	0.09	0.221	|I O	|	|	|	6.46
23.000	0.04	0.09	0.221	|I O	|	|	|	6.45
23.083	0.04	0.09	0.220	|I O	|	|	|	6.43
23.167	0.04	0.09	0.220	|I O	|	|	|	6.41
23.250	0.04	0.09	0.220	|I O	|	|	|	6.40
23.333	0.04	0.09	0.219	|I O	|	|	|	6.38
23.417	0.04	0.09	0.219	|I O	|	|	|	6.36
23.500	0.04	0.09	0.219	|I O	|	|	|	6.34
23.583	0.04	0.09	0.218	|I O	|	|	|	6.33
23.667	0.04	0.09	0.218	|I O	|	|	|	6.31
23.750	0.04	0.09	0.217	|I O	|	|	|	6.29
23.833	0.04	0.09	0.217	|I O	|	|	|	6.28
23.917	0.04	0.09	0.217	|I O	|	|	|	6.26
24.000	0.04	0.09	0.216	|I O	|	|	|	6.24
24.083	0.02	0.09	0.216	I O	|	|	|	6.22
24.167	0.00	0.09	0.215	I O	|	|	|	6.20

24.250	0.00	0.09	0.215	I	O	|	|	|	|	6.17
24.333	0.00	0.09	0.214	I	O	|	|	|	|	6.14
24.417	0.00	0.09	0.213	I	O	|	|	|	|	6.11
24.500	0.00	0.09	0.213	I	O	|	|	|	|	6.08
24.583	0.00	0.09	0.212	I	O	|	|	|	|	6.05
24.667	0.00	0.09	0.212	I	O	|	|	|	|	6.03
24.750	0.00	0.09	0.211	I	O	|	|	|	|	6.00
24.833	0.00	0.09	0.210	I	O	|	|	|	|	5.98
24.917	0.00	0.09	0.210	I	O	|	|	|	|	5.96
25.000	0.00	0.09	0.209	I	O	|	|	|	|	5.94
25.083	0.00	0.09	0.208	I	O	|	|	|	|	5.92
25.167	0.00	0.09	0.208	I	O	|	|	|	|	5.91
25.250	0.00	0.09	0.207	I	O	|	|	|	|	5.89
25.333	0.00	0.09	0.207	I	O	|	|	|	|	5.87
25.417	0.00	0.09	0.206	I	O	|	|	|	|	5.85
25.500	0.00	0.09	0.205	I	O	|	|	|	|	5.83
25.583	0.00	0.09	0.205	I	O	|	|	|	|	5.81
25.667	0.00	0.09	0.204	I	O	|	|	|	|	5.80
25.750	0.00	0.09	0.203	I	O	|	|	|	|	5.78
25.833	0.00	0.09	0.203	I	O	|	|	|	|	5.76
25.917	0.00	0.09	0.202	I	O	|	|	|	|	5.74
26.000	0.00	0.09	0.202	I	O	|	|	|	|	5.72
26.083	0.00	0.09	0.201	I	O	|	|	|	|	5.70
26.167	0.00	0.09	0.200	I	O	|	|	|	|	5.69
26.250	0.00	0.09	0.200	I	O	|	|	|	|	5.67
26.333	0.00	0.09	0.199	I	O	|	|	|	|	5.65
26.417	0.00	0.09	0.198	I	O	|	|	|	|	5.63
26.500	0.00	0.09	0.198	I	O	|	|	|	|	5.61
26.583	0.00	0.09	0.197	I	O	|	|	|	|	5.59
26.667	0.00	0.09	0.197	I	O	|	|	|	|	5.57
26.750	0.00	0.09	0.196	I	O	|	|	|	|	5.56
26.833	0.00	0.09	0.195	I	O	|	|	|	|	5.54
26.917	0.00	0.09	0.195	I	O	|	|	|	|	5.52
27.000	0.00	0.09	0.194	I	O	|	|	|	|	5.50
27.083	0.00	0.09	0.193	I	O	|	|	|	|	5.48
27.167	0.00	0.09	0.193	I	O	|	|	|	|	5.47
27.250	0.00	0.09	0.192	I	O	|	|	|	|	5.45
27.333	0.00	0.09	0.192	I	O	|	|	|	|	5.43
27.417	0.00	0.09	0.191	I	O	|	|	|	|	5.42
27.500	0.00	0.09	0.190	I	O	|	|	|	|	5.40
27.583	0.00	0.09	0.190	I	O	|	|	|	|	5.39
27.667	0.00	0.09	0.189	I	O	|	|	|	|	5.37
27.750	0.00	0.09	0.188	I	O	|	|	|	|	5.35
27.833	0.00	0.09	0.188	I	O	|	|	|	|	5.34
27.917	0.00	0.09	0.187	I	O	|	|	|	|	5.32
28.000	0.00	0.09	0.187	I	O	|	|	|	|	5.30
28.083	0.00	0.09	0.186	I	O	|	|	|	|	5.29
28.167	0.00	0.09	0.185	I	O	|	|	|	|	5.27
28.250	0.00	0.09	0.185	I	O	|	|	|	|	5.25
28.333	0.00	0.09	0.184	I	O	|	|	|	|	5.24
28.417	0.00	0.09	0.183	I	O	|	|	|	|	5.22
28.500	0.00	0.09	0.183	I	O	|	|	|	|	5.20
28.583	0.00	0.09	0.182	I	O	|	|	|	|	5.19

28.667	0.00	0.09	0.181	I	O	|	|	|	|	5.17
28.750	0.00	0.09	0.181	I	O	|	|	|	|	5.15
28.833	0.00	0.09	0.180	I	O	|	|	|	|	5.14
28.917	0.00	0.09	0.180	I	O	|	|	|	|	5.12
29.000	0.00	0.09	0.179	I	O	|	|	|	|	5.10
29.083	0.00	0.09	0.178	I	O	|	|	|	|	5.09
29.167	0.00	0.09	0.178	I	O	|	|	|	|	5.07
29.250	0.00	0.09	0.177	I	O	|	|	|	|	5.06
29.333	0.00	0.09	0.176	I	O	|	|	|	|	5.04
29.417	0.00	0.09	0.176	I	O	|	|	|	|	5.02
29.500	0.00	0.09	0.175	I	O	|	|	|	|	5.01
29.583	0.00	0.09	0.175	I	O	|	|	|	|	4.99
29.667	0.00	0.09	0.174	I	O	|	|	|	|	4.98
29.750	0.00	0.09	0.173	I	O	|	|	|	|	4.96
29.833	0.00	0.09	0.173	I	O	|	|	|	|	4.95
29.917	0.00	0.09	0.172	I	O	|	|	|	|	4.93
30.000	0.00	0.09	0.171	I	O	|	|	|	|	4.92
30.083	0.00	0.09	0.171	I	O	|	|	|	|	4.90
30.167	0.00	0.09	0.170	I	O	|	|	|	|	4.89
30.250	0.00	0.09	0.170	I	O	|	|	|	|	4.87
30.333	0.00	0.09	0.169	I	O	|	|	|	|	4.86
30.417	0.00	0.09	0.168	I	O	|	|	|	|	4.84
30.500	0.00	0.09	0.168	I	O	|	|	|	|	4.83
30.583	0.00	0.09	0.167	I	O	|	|	|	|	4.81
30.667	0.00	0.09	0.166	I	O	|	|	|	|	4.80
30.750	0.00	0.09	0.166	I	O	|	|	|	|	4.78
30.833	0.00	0.09	0.165	I	O	|	|	|	|	4.77
30.917	0.00	0.09	0.165	I	O	|	|	|	|	4.75
31.000	0.00	0.09	0.164	I	O	|	|	|	|	4.74
31.083	0.00	0.09	0.163	I	O	|	|	|	|	4.72
31.167	0.00	0.09	0.163	I	O	|	|	|	|	4.71
31.250	0.00	0.09	0.162	I	O	|	|	|	|	4.69
31.333	0.00	0.09	0.161	I	O	|	|	|	|	4.68
31.417	0.00	0.09	0.161	I	O	|	|	|	|	4.66
31.500	0.00	0.09	0.160	I	O	|	|	|	|	4.65
31.583	0.00	0.09	0.160	I	O	|	|	|	|	4.63
31.667	0.00	0.09	0.159	I	O	|	|	|	|	4.62
31.750	0.00	0.09	0.158	I	O	|	|	|	|	4.60
31.833	0.00	0.09	0.158	I	O	|	|	|	|	4.59
31.917	0.00	0.09	0.157	I	O	|	|	|	|	4.57
32.000	0.00	0.09	0.156	I	O	|	|	|	|	4.56
32.083	0.00	0.09	0.156	I	O	|	|	|	|	4.54
32.167	0.00	0.09	0.155	I	O	|	|	|	|	4.53
32.250	0.00	0.09	0.155	I	O	|	|	|	|	4.51
32.333	0.00	0.09	0.154	I	O	|	|	|	|	4.50
32.417	0.00	0.09	0.153	I	O	|	|	|	|	4.48
32.500	0.00	0.09	0.153	I	O	|	|	|	|	4.47
32.583	0.00	0.09	0.152	I	O	|	|	|	|	4.46
32.667	0.00	0.09	0.151	I	O	|	|	|	|	4.44
32.750	0.00	0.09	0.151	I	O	|	|	|	|	4.43
32.833	0.00	0.09	0.150	I	O	|	|	|	|	4.41
32.917	0.00	0.09	0.150	I	O	|	|	|	|	4.40
33.000	0.00	0.09	0.149	I	O	|	|	|	|	4.38

33.083	0.00	0.09	0.148	I	O	|	|	|	|	4.37
33.167	0.00	0.09	0.148	I	O	|	|	|	|	4.36
33.250	0.00	0.09	0.147	I	O	|	|	|	|	4.34
33.333	0.00	0.09	0.146	I	O	|	|	|	|	4.33
33.417	0.00	0.09	0.146	I	O	|	|	|	|	4.31
33.500	0.00	0.09	0.145	I	O	|	|	|	|	4.30
33.583	0.00	0.09	0.145	I	O	|	|	|	|	4.28
33.667	0.00	0.09	0.144	I	O	|	|	|	|	4.27
33.750	0.00	0.09	0.143	I	O	|	|	|	|	4.26
33.833	0.00	0.09	0.143	I	O	|	|	|	|	4.24
33.917	0.00	0.09	0.142	I	O	|	|	|	|	4.23
34.000	0.00	0.09	0.141	I	O	|	|	|	|	4.21
34.083	0.00	0.09	0.141	I	O	|	|	|	|	4.20
34.167	0.00	0.09	0.140	I	O	|	|	|	|	4.18
34.250	0.00	0.09	0.140	I	O	|	|	|	|	4.17
34.333	0.00	0.09	0.139	I	O	|	|	|	|	4.16
34.417	0.00	0.09	0.138	I	O	|	|	|	|	4.14
34.500	0.00	0.09	0.138	I	O	|	|	|	|	4.13
34.583	0.00	0.09	0.137	I	O	|	|	|	|	4.11
34.667	0.00	0.09	0.136	I	O	|	|	|	|	4.10
34.750	0.00	0.09	0.136	I	O	|	|	|	|	4.09
34.833	0.00	0.09	0.135	I	O	|	|	|	|	4.07
34.917	0.00	0.09	0.134	I	O	|	|	|	|	4.06
35.000	0.00	0.09	0.134	I	O	|	|	|	|	4.04
35.083	0.00	0.09	0.133	I	O	|	|	|	|	4.03
35.167	0.00	0.09	0.133	I	O	|	|	|	|	4.01
35.250	0.00	0.09	0.132	I	O	|	|	|	|	4.00
35.333	0.00	0.09	0.131	I	O	|	|	|	|	3.98
35.417	0.00	0.09	0.131	I	O	|	|	|	|	3.97
35.500	0.00	0.09	0.130	I	O	|	|	|	|	3.95
35.583	0.00	0.09	0.129	I	O	|	|	|	|	3.94
35.667	0.00	0.09	0.129	I	O	|	|	|	|	3.92
35.750	0.00	0.09	0.128	I	O	|	|	|	|	3.91
35.833	0.00	0.09	0.128	I	O	|	|	|	|	3.90
35.917	0.00	0.09	0.127	I	O	|	|	|	|	3.88
36.000	0.00	0.09	0.126	I	O	|	|	|	|	3.87
36.083	0.00	0.09	0.126	I	O	|	|	|	|	3.85
36.167	0.00	0.09	0.125	I	O	|	|	|	|	3.84
36.250	0.00	0.09	0.124	I	O	|	|	|	|	3.82
36.333	0.00	0.09	0.124	I	O	|	|	|	|	3.81
36.417	0.00	0.09	0.123	I	O	|	|	|	|	3.79
36.500	0.00	0.09	0.123	I	O	|	|	|	|	3.78
36.583	0.00	0.09	0.122	I	O	|	|	|	|	3.76
36.667	0.00	0.09	0.121	I	O	|	|	|	|	3.75
36.750	0.00	0.09	0.121	I	O	|	|	|	|	3.73
36.833	0.00	0.09	0.120	I	O	|	|	|	|	3.72
36.917	0.00	0.09	0.119	I	O	|	|	|	|	3.70
37.000	0.00	0.09	0.119	I	O	|	|	|	|	3.69
37.083	0.00	0.09	0.118	I	O	|	|	|	|	3.67
37.167	0.00	0.09	0.118	I	O	|	|	|	|	3.66
37.250	0.00	0.09	0.117	I	O	|	|	|	|	3.64
37.333	0.00	0.09	0.116	I	O	|	|	|	|	3.63
37.417	0.00	0.09	0.116	I	O	|	|	|	|	3.61

37.500	0.00	0.09	0.115	I	O	|	|	|	|	3.60
37.583	0.00	0.09	0.114	I	O	|	|	|	|	3.58
37.667	0.00	0.09	0.114	I	O	|	|	|	|	3.57
37.750	0.00	0.09	0.113	I	O	|	|	|	|	3.55
37.833	0.00	0.09	0.113	I	O	|	|	|	|	3.54
37.917	0.00	0.09	0.112	I	O	|	|	|	|	3.52
38.000	0.00	0.09	0.111	I	O	|	|	|	|	3.51
38.083	0.00	0.09	0.111	I	O	|	|	|	|	3.49
38.167	0.00	0.09	0.110	I	O	|	|	|	|	3.48
38.250	0.00	0.09	0.109	I	O	|	|	|	|	3.46
38.333	0.00	0.09	0.109	I	O	|	|	|	|	3.45
38.417	0.00	0.09	0.108	I	O	|	|	|	|	3.44
38.500	0.00	0.09	0.108	I	O	|	|	|	|	3.42
38.583	0.00	0.09	0.107	I	O	|	|	|	|	3.41
38.667	0.00	0.09	0.106	I	O	|	|	|	|	3.39
38.750	0.00	0.09	0.106	I	O	|	|	|	|	3.38
38.833	0.00	0.09	0.105	I	O	|	|	|	|	3.36
38.917	0.00	0.09	0.104	I	O	|	|	|	|	3.35
39.000	0.00	0.09	0.104	I	O	|	|	|	|	3.34
39.083	0.00	0.09	0.103	I	O	|	|	|	|	3.32
39.167	0.00	0.09	0.103	I	O	|	|	|	|	3.31
39.250	0.00	0.09	0.102	I	O	|	|	|	|	3.29
39.333	0.00	0.09	0.101	I	O	|	|	|	|	3.28
39.417	0.00	0.09	0.101	I	O	|	|	|	|	3.26
39.500	0.00	0.09	0.100	I	O	|	|	|	|	3.25
39.583	0.00	0.09	0.099	I	O	|	|	|	|	3.24
39.667	0.00	0.09	0.099	I	O	|	|	|	|	3.22
39.750	0.00	0.09	0.098	I	O	|	|	|	|	3.21
39.833	0.00	0.09	0.098	I	O	|	|	|	|	3.19
39.917	0.00	0.09	0.097	I	O	|	|	|	|	3.18
40.000	0.00	0.09	0.096	I	O	|	|	|	|	3.16
40.083	0.00	0.09	0.096	I	O	|	|	|	|	3.15
40.167	0.00	0.09	0.095	I	O	|	|	|	|	3.14
40.250	0.00	0.09	0.094	I	O	|	|	|	|	3.12
40.333	0.00	0.09	0.094	I	O	|	|	|	|	3.11
40.417	0.00	0.09	0.093	I	O	|	|	|	|	3.09
40.500	0.00	0.09	0.092	I	O	|	|	|	|	3.08
40.583	0.00	0.09	0.092	I	O	|	|	|	|	3.07
40.667	0.00	0.09	0.091	I	O	|	|	|	|	3.05
40.750	0.00	0.09	0.091	I	O	|	|	|	|	3.04
40.833	0.00	0.09	0.090	I	O	|	|	|	|	3.02
40.917	0.00	0.09	0.089	I	O	|	|	|	|	3.01
41.000	0.00	0.09	0.089	I	O	|	|	|	|	2.99
41.083	0.00	0.09	0.088	I	O	|	|	|	|	2.98
41.167	0.00	0.09	0.087	I	O	|	|	|	|	2.96
41.250	0.00	0.09	0.087	I	O	|	|	|	|	2.95
41.333	0.00	0.09	0.086	I	O	|	|	|	|	2.93
41.417	0.00	0.09	0.086	I	O	|	|	|	|	2.92
41.500	0.00	0.09	0.085	I	O	|	|	|	|	2.90
41.583	0.00	0.09	0.084	I	O	|	|	|	|	2.88
41.667	0.00	0.09	0.084	I	O	|	|	|	|	2.87
41.750	0.00	0.09	0.083	I	O	|	|	|	|	2.85
41.833	0.00	0.09	0.082	I	O	|	|	|	|	2.84

41.917	0.00	0.09	0.082	I	O	|	|	|	|	2.82
42.000	0.00	0.09	0.081	I	O	|	|	|	|	2.81
42.083	0.00	0.09	0.081	I	O	|	|	|	|	2.79
42.167	0.00	0.09	0.080	I	O	|	|	|	|	2.77
42.250	0.00	0.09	0.079	I	O	|	|	|	|	2.76
42.333	0.00	0.09	0.079	I	O	|	|	|	|	2.74
42.417	0.00	0.09	0.078	I	O	|	|	|	|	2.73
42.500	0.00	0.09	0.077	I	O	|	|	|	|	2.71
42.583	0.00	0.09	0.077	I	O	|	|	|	|	2.70
42.667	0.00	0.09	0.076	I	O	|	|	|	|	2.68
42.750	0.00	0.09	0.076	I	O	|	|	|	|	2.66
42.833	0.00	0.09	0.075	I	O	|	|	|	|	2.65
42.917	0.00	0.09	0.074	I	O	|	|	|	|	2.63
43.000	0.00	0.09	0.074	I	O	|	|	|	|	2.62
43.083	0.00	0.09	0.073	I	O	|	|	|	|	2.60
43.167	0.00	0.09	0.072	I	O	|	|	|	|	2.59
43.250	0.00	0.09	0.072	I	O	|	|	|	|	2.57
43.333	0.00	0.09	0.071	I	O	|	|	|	|	2.55
43.417	0.00	0.09	0.071	I	O	|	|	|	|	2.54
43.500	0.00	0.09	0.070	I	O	|	|	|	|	2.52
43.583	0.00	0.09	0.069	I	O	|	|	|	|	2.51
43.667	0.00	0.09	0.069	I	O	|	|	|	|	2.49
43.750	0.00	0.09	0.068	I	O	|	|	|	|	2.48
43.833	0.00	0.09	0.067	I	O	|	|	|	|	2.46
43.917	0.00	0.09	0.067	I	O	|	|	|	|	2.45
44.000	0.00	0.09	0.066	I	O	|	|	|	|	2.43
44.083	0.00	0.09	0.066	I	O	|	|	|	|	2.41
44.167	0.00	0.09	0.065	I	O	|	|	|	|	2.40
44.250	0.00	0.09	0.064	I	O	|	|	|	|	2.38
44.333	0.00	0.09	0.064	I	O	|	|	|	|	2.37
44.417	0.00	0.09	0.063	I	O	|	|	|	|	2.35
44.500	0.00	0.09	0.062	I	O	|	|	|	|	2.34
44.583	0.00	0.09	0.062	I	O	|	|	|	|	2.32
44.667	0.00	0.09	0.061	I	O	|	|	|	|	2.30
44.750	0.00	0.09	0.061	I	O	|	|	|	|	2.29
44.833	0.00	0.09	0.060	I	O	|	|	|	|	2.27
44.917	0.00	0.09	0.059	I	O	|	|	|	|	2.26
45.000	0.00	0.09	0.059	I	O	|	|	|	|	2.24
45.083	0.00	0.09	0.058	I	O	|	|	|	|	2.23
45.167	0.00	0.09	0.057	I	O	|	|	|	|	2.21
45.250	0.00	0.09	0.057	I	O	|	|	|	|	2.19
45.333	0.00	0.09	0.056	I	O	|	|	|	|	2.18
45.417	0.00	0.09	0.056	I	O	|	|	|	|	2.16
45.500	0.00	0.09	0.055	I	O	|	|	|	|	2.15
45.583	0.00	0.09	0.054	I	O	|	|	|	|	2.13
45.667	0.00	0.09	0.054	I	O	|	|	|	|	2.12
45.750	0.00	0.09	0.053	I	O	|	|	|	|	2.10
45.833	0.00	0.09	0.052	I	O	|	|	|	|	2.08
45.917	0.00	0.09	0.052	I	O	|	|	|	|	2.07
46.000	0.00	0.09	0.051	I	O	|	|	|	|	2.05
46.083	0.00	0.09	0.051	I	O	|	|	|	|	2.04
46.167	0.00	0.09	0.050	I	O	|	|	|	|	2.02
46.250	0.00	0.09	0.049	I	O	|	|	|	|	2.01

46.333	0.00	0.09	0.049	I	O	|	|	|	|	1.99
46.417	0.00	0.09	0.048	I	O	|	|	|	|	1.97
46.500	0.00	0.09	0.047	I	O	|	|	|	|	1.95
46.583	0.00	0.09	0.047	I	O	|	|	|	|	1.93
46.667	0.00	0.09	0.046	I	O	|	|	|	|	1.91
46.750	0.00	0.09	0.045	I	O	|	|	|	|	1.89
46.833	0.00	0.09	0.045	I	O	|	|	|	|	1.87
46.917	0.00	0.09	0.044	I	O	|	|	|	|	1.85
47.000	0.00	0.09	0.044	I	O	|	|	|	|	1.83
47.083	0.00	0.09	0.043	I	O	|	|	|	|	1.81
47.167	0.00	0.09	0.042	I	O	|	|	|	|	1.79
47.250	0.00	0.09	0.042	I	O	|	|	|	|	1.77
47.333	0.00	0.09	0.041	I	O	|	|	|	|	1.75
47.417	0.00	0.09	0.040	I	O	|	|	|	|	1.73
47.500	0.00	0.09	0.040	I	O	|	|	|	|	1.71
47.583	0.00	0.09	0.039	I	O	|	|	|	|	1.69
47.667	0.00	0.09	0.039	I	O	|	|	|	|	1.68
47.750	0.00	0.09	0.038	I	O	|	|	|	|	1.66
47.833	0.00	0.09	0.037	I	O	|	|	|	|	1.64
47.917	0.00	0.09	0.037	I	O	|	|	|	|	1.62
48.000	0.00	0.09	0.036	I	O	|	|	|	|	1.60
48.083	0.00	0.09	0.035	I	O	|	|	|	|	1.58
48.167	0.00	0.09	0.035	I	O	|	|	|	|	1.56
48.250	0.00	0.09	0.034	I	O	|	|	|	|	1.54
48.333	0.00	0.09	0.034	I	O	|	|	|	|	1.52
48.417	0.00	0.09	0.033	I	O	|	|	|	|	1.50
48.500	0.00	0.09	0.032	I	O	|	|	|	|	1.47
48.583	0.00	0.09	0.032	I	O	|	|	|	|	1.44
48.667	0.00	0.09	0.031	I	O	|	|	|	|	1.40
48.750	0.00	0.09	0.030	I	O	|	|	|	|	1.37
48.833	0.00	0.09	0.030	I	O	|	|	|	|	1.34
48.917	0.00	0.09	0.029	I	O	|	|	|	|	1.31
49.000	0.00	0.09	0.029	I	O	|	|	|	|	1.28
49.083	0.00	0.09	0.028	I	O	|	|	|	|	1.25
49.167	0.00	0.09	0.027	I	O	|	|	|	|	1.22
49.250	0.00	0.09	0.027	I	O	|	|	|	|	1.18
49.333	0.00	0.09	0.026	I	O	|	|	|	|	1.15
49.417	0.00	0.09	0.025	I	O	|	|	|	|	1.12
49.500	0.00	0.09	0.025	I	O	|	|	|	|	1.09
49.583	0.00	0.09	0.024	I	O	|	|	|	|	1.06
49.667	0.00	0.09	0.024	I	O	|	|	|	|	1.03
49.750	0.00	0.09	0.023	I	O	|	|	|	|	1.00
49.833	0.00	0.09	0.022	I	O	|	|	|	|	0.97
49.917	0.00	0.09	0.022	I	O	|	|	|	|	0.94
50.000	0.00	0.09	0.021	I	O	|	|	|	|	0.92
50.083	0.00	0.09	0.020	I	O	|	|	|	|	0.89
50.167	0.00	0.09	0.020	I	O	|	|	|	|	0.87
50.250	0.00	0.09	0.019	I	O	|	|	|	|	0.84
50.333	0.00	0.09	0.019	I	O	|	|	|	|	0.81
50.417	0.00	0.09	0.018	I	O	|	|	|	|	0.79
50.500	0.00	0.09	0.017	I	O	|	|	|	|	0.76
50.583	0.00	0.09	0.017	I	O	|	|	|	|	0.74
50.667	0.00	0.09	0.016	I	O	|	|	|	|	0.71

50.750	0.00	0.09	0.015	I O	|	|	|	0.68
50.833	0.00	0.09	0.015	I O	|	|	|	0.66
50.917	0.00	0.09	0.014	I O	|	|	|	0.63
51.000	0.00	0.09	0.014	I O	|	|	|	0.61
51.083	0.00	0.09	0.013	I O	|	|	|	0.58
51.167	0.00	0.09	0.012	I O	|	|	|	0.55
51.250	0.00	0.09	0.012	I O	|	|	|	0.53
51.333	0.00	0.09	0.011	I O	|	|	|	0.50
51.417	0.00	0.09	0.010	I O	|	|	|	0.47
51.500	0.00	0.08	0.010	I O	|	|	|	0.45
51.583	0.00	0.08	0.009	I O	|	|	|	0.42
51.667	0.00	0.07	0.009	I O	|	|	|	0.40
51.750	0.00	0.07	0.008	I O	|	|	|	0.38
51.833	0.00	0.06	0.008	I O	|	|	|	0.36
51.917	0.00	0.06	0.007	I O	|	|	|	0.34
52.000	0.00	0.06	0.007	I O	|	|	|	0.32
52.083	0.00	0.05	0.007	I O	|	|	|	0.30
52.167	0.00	0.05	0.006	I O	|	|	|	0.28
52.250	0.00	0.05	0.006	I O	|	|	|	0.27
52.333	0.00	0.05	0.006	I O	|	|	|	0.25
52.417	0.00	0.04	0.005	I O	|	|	|	0.24
52.500	0.00	0.04	0.005	I O	|	|	|	0.23
52.583	0.00	0.04	0.005	IO	|	|	|	0.21
52.667	0.00	0.04	0.004	IO	|	|	|	0.20
52.750	0.00	0.03	0.004	IO	|	|	|	0.19
52.833	0.00	0.03	0.004	IO	|	|	|	0.18
52.917	0.00	0.03	0.004	IO	|	|	|	0.17
53.000	0.00	0.03	0.004	IO	|	|	|	0.16
53.083	0.00	0.03	0.003	IO	|	|	|	0.15
53.167	0.00	0.03	0.003	IO	|	|	|	0.14
53.250	0.00	0.02	0.003	IO	|	|	|	0.14
53.333	0.00	0.02	0.003	IO	|	|	|	0.13
53.417	0.00	0.02	0.003	IO	|	|	|	0.12
53.500	0.00	0.02	0.003	IO	|	|	|	0.11
53.583	0.00	0.02	0.002	O	|	|	|	0.11
53.667	0.00	0.02	0.002	O	|	|	|	0.10
53.750	0.00	0.02	0.002	O	|	|	|	0.10
53.833	0.00	0.02	0.002	O	|	|	|	0.09
53.917	0.00	0.02	0.002	O	|	|	|	0.09
54.000	0.00	0.01	0.002	O	|	|	|	0.08
54.083	0.00	0.01	0.002	O	|	|	|	0.08
54.167	0.00	0.01	0.002	O	|	|	|	0.07
54.250	0.00	0.01	0.002	O	|	|	|	0.07
54.333	0.00	0.01	0.001	O	|	|	|	0.06
54.417	0.00	0.01	0.001	O	|	|	|	0.06
54.500	0.00	0.01	0.001	O	|	|	|	0.06
54.583	0.00	0.01	0.001	O	|	|	|	0.05
54.667	0.00	0.01	0.001	O	|	|	|	0.05
54.750	0.00	0.01	0.001	O	|	|	|	0.05
54.833	0.00	0.01	0.001	O	|	|	|	0.05
54.917	0.00	0.01	0.001	O	|	|	|	0.04
55.000	0.00	0.01	0.001	O	|	|	|	0.04
55.083	0.00	0.01	0.001	O	|	|	|	0.04

55.167	0.00	0.01	0.001	O	|	|	|	|	0.04
55.250	0.00	0.01	0.001	O	|	|	|	|	0.03
55.333	0.00	0.01	0.001	O	|	|	|	|	0.03
55.417	0.00	0.01	0.001	O	|	|	|	|	0.03
55.500	0.00	0.01	0.001	O	|	|	|	|	0.03
55.583	0.00	0.00	0.001	O	|	|	|	|	0.03
55.667	0.00	0.00	0.001	O	|	|	|	|	0.03
55.750	0.00	0.00	0.001	O	|	|	|	|	0.02
55.833	0.00	0.00	0.001	O	|	|	|	|	0.02
55.917	0.00	0.00	0.000	O	|	|	|	|	0.02
56.000	0.00	0.00	0.000	O	|	|	|	|	0.02
56.083	0.00	0.00	0.000	O	|	|	|	|	0.02
56.167	0.00	0.00	0.000	O	|	|	|	|	0.02
56.250	0.00	0.00	0.000	O	|	|	|	|	0.02
56.333	0.00	0.00	0.000	O	|	|	|	|	0.02
56.417	0.00	0.00	0.000	O	|	|	|	|	0.02
56.500	0.00	0.00	0.000	O	|	|	|	|	0.01
56.583	0.00	0.00	0.000	O	|	|	|	|	0.01
56.667	0.00	0.00	0.000	O	|	|	|	|	0.01
56.750	0.00	0.00	0.000	O	|	|	|	|	0.01
56.833	0.00	0.00	0.000	O	|	|	|	|	0.01
56.917	0.00	0.00	0.000	O	|	|	|	|	0.01
57.000	0.00	0.00	0.000	O	|	|	|	|	0.01
57.083	0.00	0.00	0.000	O	|	|	|	|	0.01
57.167	0.00	0.00	0.000	O	|	|	|	|	0.01
57.250	0.00	0.00	0.000	O	|	|	|	|	0.01
57.333	0.00	0.00	0.000	O	|	|	|	|	0.01
57.417	0.00	0.00	0.000	O	|	|	|	|	0.01
57.500	0.00	0.00	0.000	O	|	|	|	|	0.01
57.583	0.00	0.00	0.000	O	|	|	|	|	0.01
57.667	0.00	0.00	0.000	O	|	|	|	|	0.01
57.750	0.00	0.00	0.000	O	|	|	|	|	0.01
57.833	0.00	0.00	0.000	O	|	|	|	|	0.01
57.917	0.00	0.00	0.000	O	|	|	|	|	0.01
58.000	0.00	0.00	0.000	O	|	|	|	|	0.01

**********HYDROGRAPH DATA**********

Number of intervals = 696
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.091 (CFS)
Total volume = 0.381 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

AREA AA1

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 07/21/25

ROUTING: BASIN AA1; UNIT HYDROGRAPH AA1

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARAA124100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 290
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.621 (CFS)
Total volume = 0.357 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 101.000 to Point/Station 102.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 290
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.011	0.086	0.011	0.011
1.000	0.021	0.086	0.021	0.021
1.500	0.031	0.086	0.031	0.031
2.000	0.046	0.086	0.046	0.046
2.500	0.064	0.086	0.064	0.064
3.000	0.084	0.086	0.084	0.084
3.500	0.104	0.086	0.104	0.104
4.000	0.124	0.086	0.124	0.124
4.500	0.144	0.086	0.144	0.144
5.000	0.164	0.086	0.164	0.164
5.500	0.182	0.086	0.182	0.182
6.000	0.198	0.086	0.198	0.198
6.500	0.208	0.086	0.208	0.208
7.000	0.219	0.086	0.219	0.219
7.500	0.230	0.086	0.230	0.230
7.580	0.231	0.086	0.231	0.231

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.2 0.31 0.47 0.62	Depth (Ft.)
0.083	0.02	0.00	0.000	O | | | |	0.00
0.167	0.03	0.00	0.000	OI | | | |	0.01
0.250	0.03	0.00	0.000	OI | | | |	0.02
0.333	0.04	0.01	0.001	O I | | | |	0.03
0.417	0.05	0.01	0.001	O I | | | |	0.04
0.500	0.05	0.01	0.001	O I | | | |	0.06
0.583	0.05	0.01	0.002	O I | | | |	0.07
0.667	0.05	0.01	0.002	O I | | | |	0.08
0.750	0.05	0.02	0.002	O I | | | |	0.09
0.833	0.06	0.02	0.002	O I | | | |	0.11
0.917	0.07	0.02	0.003	|O I | | | |	0.12
1.000	0.07	0.02	0.003	|O I | | | |	0.13
1.083	0.06	0.03	0.003	|O I | | | |	0.15
1.167	0.05	0.03	0.003	|OI | | | |	0.16
1.250	0.05	0.03	0.004	|OI | | | |	0.16
1.333	0.05	0.03	0.004	|OI | | | |	0.17
1.417	0.05	0.03	0.004	|OI | | | |	0.18
1.500	0.05	0.03	0.004	|OI | | | |	0.18
1.583	0.05	0.03	0.004	|OI | | | |	0.19
1.667	0.05	0.03	0.004	|OI | | | |	0.20
1.750	0.05	0.03	0.004	|OI | | | |	0.20
1.833	0.06	0.04	0.005	|O I | | | |	0.21
1.917	0.07	0.04	0.005	|O I | | | |	0.22
2.000	0.07	0.04	0.005	| OI | | | |	0.23
2.083	0.07	0.04	0.005	| OI | | | |	0.24

2.167	0.07	0.04	0.005	OI				0.24
2.250	0.07	0.04	0.006	OI				0.25
2.333	0.07	0.04	0.006	OI				0.26
2.417	0.07	0.05	0.006	OI				0.27
2.500	0.07	0.05	0.006	OI				0.27
2.583	0.08	0.05	0.006	O I				0.28
2.667	0.08	0.05	0.006	O I				0.29
2.750	0.09	0.05	0.007	O I				0.30
2.833	0.09	0.05	0.007	O I				0.31
2.917	0.09	0.06	0.007	O I				0.32
3.000	0.09	0.06	0.007	O I				0.33
3.083	0.09	0.06	0.008	OI				0.34
3.167	0.09	0.06	0.008	OI				0.35
3.250	0.09	0.06	0.008	OI				0.36
3.333	0.09	0.06	0.008	OI				0.36
3.417	0.09	0.06	0.008	OI				0.37
3.500	0.09	0.07	0.008	OI				0.38
3.583	0.09	0.07	0.008	OI				0.38
3.667	0.09	0.07	0.009	OI				0.39
3.750	0.09	0.07	0.009	OI				0.40
3.833	0.10	0.07	0.009	OI				0.40
3.917	0.10	0.07	0.009	O I				0.41
4.000	0.10	0.07	0.009	O I				0.42
4.083	0.10	0.07	0.009	O I				0.43
4.167	0.10	0.08	0.010	O I				0.44
4.250	0.10	0.08	0.010	O I				0.45
4.333	0.11	0.08	0.010	OI				0.46
4.417	0.12	0.08	0.010	O I				0.47
4.500	0.12	0.08	0.011	O I				0.48
4.583	0.12	0.08	0.011	O I				0.49
4.667	0.12	0.09	0.011	O I				0.50
4.750	0.12	0.09	0.011	O I				0.52
4.833	0.13	0.09	0.012	O I				0.53
4.917	0.14	0.09	0.012	O I				0.55
5.000	0.14	0.09	0.012	O I				0.56
5.083	0.12	0.09	0.013	O I				0.58
5.167	0.10	0.09	0.013	OI				0.59
5.250	0.10	0.09	0.013	OI				0.59
5.333	0.11	0.09	0.013	OI				0.60
5.417	0.12	0.09	0.013	O I				0.61
5.500	0.12	0.09	0.013	O I				0.62
5.583	0.13	0.09	0.014	O I				0.64
5.667	0.14	0.09	0.014	O I				0.65
5.750	0.14	0.09	0.014	O I				0.67
5.833	0.14	0.09	0.015	O I				0.69
5.917	0.14	0.09	0.015	O I				0.70
6.000	0.14	0.09	0.015	O I				0.72
6.083	0.15	0.09	0.016	O I				0.74
6.167	0.15	0.09	0.016	O I				0.76
6.250	0.15	0.09	0.017	O I				0.79
6.333	0.15	0.09	0.017	O I				0.81
6.417	0.15	0.09	0.018	O I				0.83
6.500	0.15	0.09	0.018	O I				0.86

6.583	0.16	0.09	0.019	|	O	I	|	|	0.88
6.667	0.17	0.09	0.019	|	O	I	|	|	0.91
6.750	0.17	0.09	0.020	|	O	I	|	|	0.94
6.833	0.17	0.09	0.020	|	O	I	|	|	0.97
6.917	0.17	0.09	0.021	|	O	I	|	|	1.00
7.000	0.17	0.09	0.022	|	O	I	|	|	1.03
7.083	0.17	0.09	0.022	|	O	I	|	|	1.06
7.167	0.17	0.09	0.023	|	O	I	|	|	1.09
7.250	0.17	0.09	0.023	|	O	I	|	|	1.12
7.333	0.18	0.09	0.024	|	O	|I	|	|	1.15
7.417	0.19	0.09	0.025	|	O	|I	|	|	1.18
7.500	0.19	0.09	0.025	|	O	|I	|	|	1.22
7.583	0.20	0.09	0.026	|	O	| I	|	|	1.26
7.667	0.21	0.09	0.027	|	O	| I	|	|	1.30
7.750	0.21	0.09	0.028	|	O	| I	|	|	1.34
7.833	0.22	0.09	0.029	|	O	| I	|	|	1.38
7.917	0.22	0.09	0.030	|	O	| I	|	|	1.43
8.000	0.22	0.09	0.030	|	O	| I	|	|	1.47
8.083	0.24	0.09	0.031	|	O	| I	|	|	1.52
8.167	0.26	0.09	0.033	|	O	| I	|	|	1.55
8.250	0.26	0.09	0.034	|	O	| I	|	|	1.59
8.333	0.26	0.09	0.035	|	O	| I	|	|	1.63
8.417	0.26	0.09	0.036	|	O	| I	|	|	1.67
8.500	0.26	0.09	0.037	|	O	| I	|	|	1.71
8.583	0.27	0.09	0.039	|	O	| I	|	|	1.75
8.667	0.27	0.09	0.040	|	O	| I |	|	|	1.79
8.750	0.27	0.09	0.041	|	O	| I |	|	|	1.84
8.833	0.28	0.09	0.042	|	O	| I |	|	|	1.88
8.917	0.29	0.09	0.044	|	O	| I|	|	|	1.93
9.000	0.29	0.09	0.045	|	O	| I|	|	|	1.97
9.083	0.31	0.09	0.047	|	O	| I	|	|	2.02
9.167	0.32	0.09	0.048	|	O	| I	|	|	2.06
9.250	0.33	0.09	0.050	|	O	| I	|	|	2.11
9.333	0.34	0.09	0.052	|	O	| |I	|	|	2.16
9.417	0.34	0.09	0.053	|	O	| |I	|	|	2.21
9.500	0.34	0.09	0.055	|	O	| |I	|	|	2.25
9.583	0.35	0.09	0.057	|	O	| | I	|	|	2.31
9.667	0.36	0.09	0.059	|	O	| | I	|	|	2.36
9.750	0.36	0.09	0.061	|	O	| | I	|	|	2.41
9.833	0.37	0.09	0.063	|	O	| | I	|	|	2.46
9.917	0.38	0.09	0.065	|	O	| | I	|	|	2.52
10.000	0.38	0.09	0.067	|	O	| | I	|	|	2.57
10.083	0.31	0.09	0.068	|	O	| I	|	|	2.61
10.167	0.26	0.09	0.070	|	O	| I	|	|	2.65
10.250	0.26	0.09	0.071	|	O	| I	|	|	2.68
10.333	0.26	0.09	0.072	|	O	| I	|	|	2.71
10.417	0.26	0.09	0.073	|	O	| I	|	|	2.73
10.500	0.26	0.09	0.075	|	O	| I	|	|	2.76
10.583	0.31	0.09	0.076	|	O	| I|	|	|	2.80
10.667	0.34	0.09	0.078	|	O	| |I	|	|	2.84
10.750	0.34	0.09	0.079	|	O	| |I	|	|	2.88
10.833	0.34	0.09	0.081	|	O	| |I	|	|	2.93
10.917	0.34	0.09	0.083	|	O	| |I	|	|	2.97

11.000	0.34	0.09	0.085	|	O	|	|I	|	3.02
11.083	0.33	0.09	0.086	|	O	|	|I	|	3.06
11.167	0.33	0.09	0.088	|	O	|	I	|	3.10
11.250	0.33	0.09	0.090	|	O	|	I	|	3.14
11.333	0.33	0.09	0.091	|	O	|	I	|	3.18
11.417	0.33	0.09	0.093	|	O	|	I	|	3.23
11.500	0.33	0.09	0.095	|	O	|	I	|	3.27
11.583	0.31	0.09	0.096	|	O	|	I|	|	3.31
11.667	0.29	0.09	0.098	|	O	|	I|	|	3.34
11.750	0.29	0.09	0.099	|	O	|	I|	|	3.38
11.833	0.30	0.09	0.101	|	O	|	I|	|	3.42
11.917	0.31	0.09	0.102	|	O	|	I|	|	3.45
12.000	0.31	0.09	0.104	|	O	|	I|	|	3.49
12.083	0.38	0.09	0.105	|	O	|	| I	|	3.54
12.167	0.42	0.09	0.108	|	O	|	| I	|	3.59
12.250	0.43	0.09	0.110	|	O	|	| I	|	3.65
12.333	0.44	0.09	0.112	|	O	|	| I	|	3.71
12.417	0.45	0.09	0.115	|	O	|	| I	|	3.77
12.500	0.45	0.09	0.117	|	O	|	| I|	|	3.83
12.583	0.47	0.09	0.120	|	O	|	| I	|	3.90
12.667	0.48	0.09	0.122	|	O	|	| I	|	3.96
12.750	0.48	0.09	0.125	|	O	|	| I	|	4.03
12.833	0.50	0.09	0.128	|	O	|	|I	|	4.10
12.917	0.51	0.09	0.131	|	O	|	| I	|	4.17
13.000	0.51	0.09	0.134	|	O	|	| I	|	4.24
13.083	0.57	0.09	0.137	|	O	|	| I	|	4.32
13.167	0.61	0.09	0.140	|	O	|	| I|	|	4.41
13.250	0.62	0.09	0.144	|	O	|	| I|	|	4.50
13.333	0.62	0.09	0.148	|	O	|	| I|	|	4.59
13.417	0.62	0.09	0.151	|	O	|	| I|	|	4.68
13.500	0.62	0.09	0.155	|	O	|	| I	|	4.78
13.583	0.50	0.09	0.158	|	O	|	|I	|	4.86
13.667	0.41	0.09	0.161	|	O	|	| I	|	4.92
13.750	0.40	0.09	0.163	|	O	|	| I	|	4.97
13.833	0.40	0.09	0.165	|	O	|	| I	|	5.03
13.917	0.40	0.09	0.167	|	O	|	| I	|	5.09
14.000	0.40	0.09	0.169	|	O	|	| I	|	5.15
14.083	0.44	0.09	0.172	|	O	|	| I	|	5.21
14.167	0.47	0.09	0.174	|	O	|	| I	|	5.28
14.250	0.47	0.09	0.177	|	O	|	| I	|	5.36
14.333	0.46	0.09	0.179	|	O	|	| I|	|	5.43
14.417	0.45	0.09	0.182	|	O	|	| I|	|	5.50
14.500	0.45	0.09	0.185	|	O	|	| I|	|	5.58
14.583	0.45	0.09	0.187	|	O	|	| I|	|	5.66
14.667	0.45	0.09	0.190	|	O	|	| I|	|	5.74
14.750	0.45	0.09	0.192	|	O	|	| I|	|	5.82
14.833	0.44	0.09	0.195	|	O	|	| I	|	5.89
14.917	0.43	0.09	0.197	|	O	|	| I	|	5.97
15.000	0.43	0.09	0.199	|	O	|	| I	|	6.07
15.083	0.42	0.09	0.202	|	O	|	| I	|	6.19
15.167	0.41	0.09	0.204	|	O	|	| I	|	6.30
15.250	0.41	0.09	0.206	|	O	|	| I	|	6.42
15.333	0.40	0.09	0.209	|	O	|	| I	|	6.52

15.417	0.40	0.09	0.211	| O |		| I |			6.62
15.500	0.40	0.09	0.213	| O |		| I |			6.72
15.583	0.36	0.09	0.215	| O |		| I				6.81
15.667	0.33	0.09	0.217	| O |		|I				6.89
15.750	0.33	0.09	0.218	| O |		I				6.97
15.833	0.33	0.09	0.220	| O |		I				7.04
15.917	0.33	0.09	0.222	| O |		I				7.12
16.000	0.33	0.09	0.223	| O |		I				7.19
16.083	0.18	0.09	0.224	| O |	I					7.25
16.167	0.08	0.09	0.225	| O |						7.26
16.250	0.07	0.09	0.225	| IO |						7.26
16.333	0.07	0.09	0.225	| IO |						7.25
16.417	0.07	0.09	0.224	| IO |						7.25
16.500	0.07	0.09	0.224	| IO |						7.24
16.583	0.06	0.09	0.224	| IO |						7.23
16.667	0.05	0.09	0.224	| I O |						7.22
16.750	0.05	0.09	0.224	| I O |						7.21
16.833	0.05	0.09	0.223	| I O |						7.20
16.917	0.05	0.09	0.223	| I O |						7.19
17.000	0.05	0.09	0.223	| I O |						7.18
17.083	0.07	0.09	0.223	| IO |						7.17
17.167	0.08	0.09	0.223	| O |						7.17
17.250	0.09	0.09	0.223	| O |						7.17
17.333	0.09	0.09	0.223	| O |						7.17
17.417	0.09	0.09	0.223	| O |						7.17
17.500	0.09	0.09	0.223	| O |						7.17
17.583	0.09	0.09	0.223	| O |						7.17
17.667	0.09	0.09	0.223	| O |						7.17
17.750	0.09	0.09	0.223	| O |						7.17
17.833	0.08	0.09	0.223	| IO |						7.17
17.917	0.07	0.09	0.223	| IO |						7.17
18.000	0.07	0.09	0.223	| IO |						7.16
18.083	0.07	0.09	0.222	| IO |						7.15
18.167	0.07	0.09	0.222	| IO |						7.15
18.250	0.07	0.09	0.222	| IO |						7.14
18.333	0.07	0.09	0.222	| IO |						7.14
18.417	0.07	0.09	0.222	| IO |						7.13
18.500	0.07	0.09	0.222	| IO |						7.13
18.583	0.06	0.09	0.222	| IO |						7.12
18.667	0.05	0.09	0.221	| I O |						7.11
18.750	0.05	0.09	0.221	| I O |						7.10
18.833	0.04	0.09	0.221	| I O |						7.09
18.917	0.04	0.09	0.221	|I O |						7.07
19.000	0.03	0.09	0.220	|I O |						7.06
19.083	0.04	0.09	0.220	| I O |						7.04
19.167	0.05	0.09	0.220	| I O |						7.03
19.250	0.05	0.09	0.219	| I O |						7.02
19.333	0.06	0.09	0.219	| IO |						7.01
19.417	0.07	0.09	0.219	| IO |						7.00
19.500	0.07	0.09	0.219	| IO |						7.00
19.583	0.06	0.09	0.219	| IO |						6.99
19.667	0.05	0.09	0.219	| I O |						6.98
19.750	0.05	0.09	0.218	| I O |						6.97

19.833	0.04	0.09	0.218	| I O	|	|	|	6.96
19.917	0.04	0.09	0.218	|I O	|	|	|	6.94
20.000	0.03	0.09	0.217	|I O	|	|	|	6.93
20.083	0.04	0.09	0.217	| I O	|	|	|	6.91
20.167	0.05	0.09	0.217	| I O	|	|	|	6.90
20.250	0.05	0.09	0.217	| I O	|	|	|	6.89
20.333	0.05	0.09	0.216	| I O	|	|	|	6.88
20.417	0.05	0.09	0.216	| I O	|	|	|	6.87
20.500	0.05	0.09	0.216	| I O	|	|	|	6.86
20.583	0.05	0.09	0.216	| I O	|	|	|	6.85
20.667	0.05	0.09	0.215	| I O	|	|	|	6.84
20.750	0.05	0.09	0.215	| I O	|	|	|	6.83
20.833	0.04	0.09	0.215	| I O	|	|	|	6.81
20.917	0.04	0.09	0.215	|I O	|	|	|	6.80
21.000	0.03	0.09	0.214	|I O	|	|	|	6.78
21.083	0.04	0.09	0.214	| I O	|	|	|	6.77
21.167	0.05	0.09	0.214	| I O	|	|	|	6.76
21.250	0.05	0.09	0.213	| I O	|	|	|	6.74
21.333	0.04	0.09	0.213	| I O	|	|	|	6.73
21.417	0.04	0.09	0.213	|I O	|	|	|	6.72
21.500	0.03	0.09	0.212	|I O	|	|	|	6.70
21.583	0.04	0.09	0.212	| I O	|	|	|	6.69
21.667	0.05	0.09	0.212	| I O	|	|	|	6.67
21.750	0.05	0.09	0.212	| I O	|	|	|	6.66
21.833	0.04	0.09	0.211	| I O	|	|	|	6.65
21.917	0.04	0.09	0.211	|I O	|	|	|	6.64
22.000	0.03	0.09	0.211	|I O	|	|	|	6.62
22.083	0.04	0.09	0.210	| I O	|	|	|	6.61
22.167	0.05	0.09	0.210	| I O	|	|	|	6.59
22.250	0.05	0.09	0.210	| I O	|	|	|	6.58
22.333	0.04	0.09	0.210	| I O	|	|	|	6.57
22.417	0.04	0.09	0.209	|I O	|	|	|	6.56
22.500	0.03	0.09	0.209	|I O	|	|	|	6.54
22.583	0.03	0.09	0.209	|I O	|	|	|	6.52
22.667	0.03	0.09	0.208	|I O	|	|	|	6.51
22.750	0.03	0.09	0.208	|I O	|	|	|	6.49
22.833	0.03	0.09	0.207	|I O	|	|	|	6.47
22.917	0.03	0.09	0.207	|I O	|	|	|	6.45
23.000	0.03	0.09	0.207	|I O	|	|	|	6.44
23.083	0.03	0.09	0.206	|I O	|	|	|	6.42
23.167	0.03	0.09	0.206	|I O	|	|	|	6.40
23.250	0.03	0.09	0.206	|I O	|	|	|	6.38
23.333	0.03	0.09	0.205	|I O	|	|	|	6.37
23.417	0.03	0.09	0.205	|I O	|	|	|	6.35
23.500	0.03	0.09	0.205	|I O	|	|	|	6.33
23.583	0.03	0.09	0.204	|I O	|	|	|	6.31
23.667	0.03	0.09	0.204	|I O	|	|	|	6.29
23.750	0.03	0.09	0.204	|I O	|	|	|	6.28
23.833	0.03	0.09	0.203	|I O	|	|	|	6.26
23.917	0.03	0.09	0.203	|I O	|	|	|	6.24
24.000	0.03	0.09	0.202	|I O	|	|	|	6.22
24.083	0.02	0.09	0.202	I O	|	|	|	6.20
24.167	0.00	0.09	0.202	I O	|	|	|	6.18

24.250	0.00	0.09	0.201	I	O	|	|	|	|	6.15
24.333	0.00	0.09	0.200	I	O	|	|	|	|	6.12
24.417	0.00	0.09	0.200	I	O	|	|	|	|	6.09
24.500	0.00	0.09	0.199	I	O	|	|	|	|	6.06
24.583	0.00	0.09	0.199	I	O	|	|	|	|	6.03
24.667	0.00	0.09	0.198	I	O	|	|	|	|	6.00
24.750	0.00	0.09	0.197	I	O	|	|	|	|	5.98
24.833	0.00	0.09	0.197	I	O	|	|	|	|	5.96
24.917	0.00	0.09	0.196	I	O	|	|	|	|	5.94
25.000	0.00	0.09	0.196	I	O	|	|	|	|	5.92
25.083	0.00	0.09	0.195	I	O	|	|	|	|	5.91
25.167	0.00	0.09	0.194	I	O	|	|	|	|	5.89
25.250	0.00	0.09	0.194	I	O	|	|	|	|	5.87
25.333	0.00	0.09	0.193	I	O	|	|	|	|	5.85
25.417	0.00	0.09	0.193	I	O	|	|	|	|	5.83
25.500	0.00	0.09	0.192	I	O	|	|	|	|	5.81
25.583	0.00	0.09	0.191	I	O	|	|	|	|	5.80
25.667	0.00	0.09	0.191	I	O	|	|	|	|	5.78
25.750	0.00	0.09	0.190	I	O	|	|	|	|	5.76
25.833	0.00	0.09	0.190	I	O	|	|	|	|	5.74
25.917	0.00	0.09	0.189	I	O	|	|	|	|	5.72
26.000	0.00	0.09	0.188	I	O	|	|	|	|	5.70
26.083	0.00	0.09	0.188	I	O	|	|	|	|	5.68
26.167	0.00	0.09	0.187	I	O	|	|	|	|	5.67
26.250	0.00	0.09	0.187	I	O	|	|	|	|	5.65
26.333	0.00	0.09	0.186	I	O	|	|	|	|	5.63
26.417	0.00	0.09	0.186	I	O	|	|	|	|	5.61
26.500	0.00	0.09	0.185	I	O	|	|	|	|	5.59
26.583	0.00	0.09	0.184	I	O	|	|	|	|	5.57
26.667	0.00	0.09	0.184	I	O	|	|	|	|	5.55
26.750	0.00	0.09	0.183	I	O	|	|	|	|	5.54
26.833	0.00	0.09	0.183	I	O	|	|	|	|	5.52
26.917	0.00	0.09	0.182	I	O	|	|	|	|	5.50
27.000	0.00	0.09	0.181	I	O	|	|	|	|	5.48
27.083	0.00	0.09	0.181	I	O	|	|	|	|	5.47
27.167	0.00	0.09	0.180	I	O	|	|	|	|	5.45
27.250	0.00	0.09	0.180	I	O	|	|	|	|	5.43
27.333	0.00	0.09	0.179	I	O	|	|	|	|	5.42
27.417	0.00	0.09	0.178	I	O	|	|	|	|	5.40
27.500	0.00	0.09	0.178	I	O	|	|	|	|	5.38
27.583	0.00	0.09	0.177	I	O	|	|	|	|	5.37
27.667	0.00	0.09	0.177	I	O	|	|	|	|	5.35
27.750	0.00	0.09	0.176	I	O	|	|	|	|	5.33
27.833	0.00	0.09	0.175	I	O	|	|	|	|	5.32
27.917	0.00	0.09	0.175	I	O	|	|	|	|	5.30
28.000	0.00	0.09	0.174	I	O	|	|	|	|	5.29
28.083	0.00	0.09	0.174	I	O	|	|	|	|	5.27
28.167	0.00	0.09	0.173	I	O	|	|	|	|	5.25
28.250	0.00	0.09	0.172	I	O	|	|	|	|	5.24
28.333	0.00	0.09	0.172	I	O	|	|	|	|	5.22
28.417	0.00	0.09	0.171	I	O	|	|	|	|	5.20
28.500	0.00	0.09	0.171	I	O	|	|	|	|	5.19
28.583	0.00	0.09	0.170	I	O	|	|	|	|	5.17

28.667	0.00	0.09	0.170	I	O	|	|	|	|	5.15
28.750	0.00	0.09	0.169	I	O	|	|	|	|	5.14
28.833	0.00	0.09	0.168	I	O	|	|	|	|	5.12
28.917	0.00	0.09	0.168	I	O	|	|	|	|	5.10
29.000	0.00	0.09	0.167	I	O	|	|	|	|	5.09
29.083	0.00	0.09	0.167	I	O	|	|	|	|	5.07
29.167	0.00	0.09	0.166	I	O	|	|	|	|	5.06
29.250	0.00	0.09	0.165	I	O	|	|	|	|	5.04
29.333	0.00	0.09	0.165	I	O	|	|	|	|	5.02
29.417	0.00	0.09	0.164	I	O	|	|	|	|	5.01
29.500	0.00	0.09	0.164	I	O	|	|	|	|	4.99
29.583	0.00	0.09	0.163	I	O	|	|	|	|	4.98
29.667	0.00	0.09	0.162	I	O	|	|	|	|	4.96
29.750	0.00	0.09	0.162	I	O	|	|	|	|	4.95
29.833	0.00	0.09	0.161	I	O	|	|	|	|	4.93
29.917	0.00	0.09	0.161	I	O	|	|	|	|	4.92
30.000	0.00	0.09	0.160	I	O	|	|	|	|	4.90
30.083	0.00	0.09	0.159	I	O	|	|	|	|	4.89
30.167	0.00	0.09	0.159	I	O	|	|	|	|	4.87
30.250	0.00	0.09	0.158	I	O	|	|	|	|	4.86
30.333	0.00	0.09	0.158	I	O	|	|	|	|	4.84
30.417	0.00	0.09	0.157	I	O	|	|	|	|	4.83
30.500	0.00	0.09	0.157	I	O	|	|	|	|	4.81
30.583	0.00	0.09	0.156	I	O	|	|	|	|	4.80
30.667	0.00	0.09	0.155	I	O	|	|	|	|	4.78
30.750	0.00	0.09	0.155	I	O	|	|	|	|	4.77
30.833	0.00	0.09	0.154	I	O	|	|	|	|	4.75
30.917	0.00	0.09	0.154	I	O	|	|	|	|	4.74
31.000	0.00	0.09	0.153	I	O	|	|	|	|	4.72
31.083	0.00	0.09	0.152	I	O	|	|	|	|	4.71
31.167	0.00	0.09	0.152	I	O	|	|	|	|	4.69
31.250	0.00	0.09	0.151	I	O	|	|	|	|	4.68
31.333	0.00	0.09	0.151	I	O	|	|	|	|	4.66
31.417	0.00	0.09	0.150	I	O	|	|	|	|	4.65
31.500	0.00	0.09	0.149	I	O	|	|	|	|	4.63
31.583	0.00	0.09	0.149	I	O	|	|	|	|	4.62
31.667	0.00	0.09	0.148	I	O	|	|	|	|	4.61
31.750	0.00	0.09	0.148	I	O	|	|	|	|	4.59
31.833	0.00	0.09	0.147	I	O	|	|	|	|	4.58
31.917	0.00	0.09	0.146	I	O	|	|	|	|	4.56
32.000	0.00	0.09	0.146	I	O	|	|	|	|	4.55
32.083	0.00	0.09	0.145	I	O	|	|	|	|	4.53
32.167	0.00	0.09	0.145	I	O	|	|	|	|	4.52
32.250	0.00	0.09	0.144	I	O	|	|	|	|	4.50
32.333	0.00	0.09	0.143	I	O	|	|	|	|	4.49
32.417	0.00	0.09	0.143	I	O	|	|	|	|	4.47
32.500	0.00	0.09	0.142	I	O	|	|	|	|	4.46
32.583	0.00	0.09	0.142	I	O	|	|	|	|	4.44
32.667	0.00	0.09	0.141	I	O	|	|	|	|	4.43
32.750	0.00	0.09	0.141	I	O	|	|	|	|	4.41
32.833	0.00	0.09	0.140	I	O	|	|	|	|	4.40
32.917	0.00	0.09	0.139	I	O	|	|	|	|	4.38
33.000	0.00	0.09	0.139	I	O	|	|	|	|	4.37

33.083	0.00	0.09	0.138	I	O	|	|	|	|	4.35
33.167	0.00	0.09	0.138	I	O	|	|	|	|	4.34
33.250	0.00	0.09	0.137	I	O	|	|	|	|	4.32
33.333	0.00	0.09	0.136	I	O	|	|	|	|	4.31
33.417	0.00	0.09	0.136	I	O	|	|	|	|	4.29
33.500	0.00	0.09	0.135	I	O	|	|	|	|	4.28
33.583	0.00	0.09	0.135	I	O	|	|	|	|	4.26
33.667	0.00	0.09	0.134	I	O	|	|	|	|	4.25
33.750	0.00	0.09	0.133	I	O	|	|	|	|	4.24
33.833	0.00	0.09	0.133	I	O	|	|	|	|	4.22
33.917	0.00	0.09	0.132	I	O	|	|	|	|	4.21
34.000	0.00	0.09	0.132	I	O	|	|	|	|	4.19
34.083	0.00	0.09	0.131	I	O	|	|	|	|	4.18
34.167	0.00	0.09	0.130	I	O	|	|	|	|	4.16
34.250	0.00	0.09	0.130	I	O	|	|	|	|	4.15
34.333	0.00	0.09	0.129	I	O	|	|	|	|	4.13
34.417	0.00	0.09	0.129	I	O	|	|	|	|	4.12
34.500	0.00	0.09	0.128	I	O	|	|	|	|	4.10
34.583	0.00	0.09	0.127	I	O	|	|	|	|	4.09
34.667	0.00	0.09	0.127	I	O	|	|	|	|	4.07
34.750	0.00	0.09	0.126	I	O	|	|	|	|	4.06
34.833	0.00	0.09	0.126	I	O	|	|	|	|	4.04
34.917	0.00	0.09	0.125	I	O	|	|	|	|	4.03
35.000	0.00	0.09	0.125	I	O	|	|	|	|	4.01
35.083	0.00	0.09	0.124	I	O	|	|	|	|	4.00
35.167	0.00	0.09	0.123	I	O	|	|	|	|	3.98
35.250	0.00	0.09	0.123	I	O	|	|	|	|	3.97
35.333	0.00	0.09	0.122	I	O	|	|	|	|	3.95
35.417	0.00	0.09	0.122	I	O	|	|	|	|	3.94
35.500	0.00	0.09	0.121	I	O	|	|	|	|	3.92
35.583	0.00	0.09	0.120	I	O	|	|	|	|	3.91
35.667	0.00	0.09	0.120	I	O	|	|	|	|	3.89
35.750	0.00	0.09	0.119	I	O	|	|	|	|	3.88
35.833	0.00	0.09	0.119	I	O	|	|	|	|	3.86
35.917	0.00	0.09	0.118	I	O	|	|	|	|	3.85
36.000	0.00	0.09	0.117	I	O	|	|	|	|	3.84
36.083	0.00	0.09	0.117	I	O	|	|	|	|	3.82
36.167	0.00	0.09	0.116	I	O	|	|	|	|	3.81
36.250	0.00	0.09	0.116	I	O	|	|	|	|	3.79
36.333	0.00	0.09	0.115	I	O	|	|	|	|	3.78
36.417	0.00	0.09	0.114	I	O	|	|	|	|	3.76
36.500	0.00	0.09	0.114	I	O	|	|	|	|	3.75
36.583	0.00	0.09	0.113	I	O	|	|	|	|	3.73
36.667	0.00	0.09	0.113	I	O	|	|	|	|	3.72
36.750	0.00	0.09	0.112	I	O	|	|	|	|	3.70
36.833	0.00	0.09	0.111	I	O	|	|	|	|	3.69
36.917	0.00	0.09	0.111	I	O	|	|	|	|	3.67
37.000	0.00	0.09	0.110	I	O	|	|	|	|	3.66
37.083	0.00	0.09	0.110	I	O	|	|	|	|	3.64
37.167	0.00	0.09	0.109	I	O	|	|	|	|	3.63
37.250	0.00	0.09	0.109	I	O	|	|	|	|	3.61
37.333	0.00	0.09	0.108	I	O	|	|	|	|	3.60
37.417	0.00	0.09	0.107	I	O	|	|	|	|	3.58

37.500	0.00	0.09	0.107	I	O	|	|	|	|	3.57
37.583	0.00	0.09	0.106	I	O	|	|	|	|	3.55
37.667	0.00	0.09	0.106	I	O	|	|	|	|	3.54
37.750	0.00	0.09	0.105	I	O	|	|	|	|	3.52
37.833	0.00	0.09	0.104	I	O	|	|	|	|	3.51
37.917	0.00	0.09	0.104	I	O	|	|	|	|	3.49
38.000	0.00	0.09	0.103	I	O	|	|	|	|	3.48
38.083	0.00	0.09	0.103	I	O	|	|	|	|	3.47
38.167	0.00	0.09	0.102	I	O	|	|	|	|	3.45
38.250	0.00	0.09	0.101	I	O	|	|	|	|	3.44
38.333	0.00	0.09	0.101	I	O	|	|	|	|	3.42
38.417	0.00	0.09	0.100	I	O	|	|	|	|	3.41
38.500	0.00	0.09	0.100	I	O	|	|	|	|	3.39
38.583	0.00	0.09	0.099	I	O	|	|	|	|	3.38
38.667	0.00	0.09	0.098	I	O	|	|	|	|	3.36
38.750	0.00	0.09	0.098	I	O	|	|	|	|	3.35
38.833	0.00	0.09	0.097	I	O	|	|	|	|	3.33
38.917	0.00	0.09	0.097	I	O	|	|	|	|	3.32
39.000	0.00	0.09	0.096	I	O	|	|	|	|	3.30
39.083	0.00	0.09	0.096	I	O	|	|	|	|	3.29
39.167	0.00	0.09	0.095	I	O	|	|	|	|	3.27
39.250	0.00	0.09	0.094	I	O	|	|	|	|	3.26
39.333	0.00	0.09	0.094	I	O	|	|	|	|	3.24
39.417	0.00	0.09	0.093	I	O	|	|	|	|	3.23
39.500	0.00	0.09	0.093	I	O	|	|	|	|	3.21
39.583	0.00	0.09	0.092	I	O	|	|	|	|	3.20
39.667	0.00	0.09	0.091	I	O	|	|	|	|	3.18
39.750	0.00	0.09	0.091	I	O	|	|	|	|	3.17
39.833	0.00	0.09	0.090	I	O	|	|	|	|	3.15
39.917	0.00	0.09	0.090	I	O	|	|	|	|	3.14
40.000	0.00	0.09	0.089	I	O	|	|	|	|	3.12
40.083	0.00	0.09	0.088	I	O	|	|	|	|	3.11
40.167	0.00	0.09	0.088	I	O	|	|	|	|	3.10
40.250	0.00	0.09	0.087	I	O	|	|	|	|	3.08
40.333	0.00	0.09	0.087	I	O	|	|	|	|	3.07
40.417	0.00	0.09	0.086	I	O	|	|	|	|	3.05
40.500	0.00	0.09	0.085	I	O	|	|	|	|	3.04
40.583	0.00	0.09	0.085	I	O	|	|	|	|	3.02
40.667	0.00	0.09	0.084	I	O	|	|	|	|	3.01
40.750	0.00	0.09	0.084	I	O	|	|	|	|	2.99
40.833	0.00	0.09	0.083	I	O	|	|	|	|	2.98
40.917	0.00	0.09	0.082	I	O	|	|	|	|	2.96
41.000	0.00	0.09	0.082	I	O	|	|	|	|	2.95
41.083	0.00	0.09	0.081	I	O	|	|	|	|	2.93
41.167	0.00	0.09	0.081	I	O	|	|	|	|	2.92
41.250	0.00	0.09	0.080	I	O	|	|	|	|	2.90
41.333	0.00	0.09	0.080	I	O	|	|	|	|	2.89
41.417	0.00	0.09	0.079	I	O	|	|	|	|	2.87
41.500	0.00	0.09	0.078	I	O	|	|	|	|	2.86
41.583	0.00	0.09	0.078	I	O	|	|	|	|	2.84
41.667	0.00	0.09	0.077	I	O	|	|	|	|	2.83
41.750	0.00	0.09	0.077	I	O	|	|	|	|	2.81
41.833	0.00	0.09	0.076	I	O	|	|	|	|	2.80

41.917	0.00	0.09	0.075	I	O	|	|	|	|	2.78
42.000	0.00	0.09	0.075	I	O	|	|	|	|	2.77
42.083	0.00	0.09	0.074	I	O	|	|	|	|	2.75
42.167	0.00	0.09	0.074	I	O	|	|	|	|	2.74
42.250	0.00	0.09	0.073	I	O	|	|	|	|	2.72
42.333	0.00	0.09	0.072	I	O	|	|	|	|	2.71
42.417	0.00	0.09	0.072	I	O	|	|	|	|	2.70
42.500	0.00	0.09	0.071	I	O	|	|	|	|	2.68
42.583	0.00	0.09	0.071	I	O	|	|	|	|	2.67
42.667	0.00	0.09	0.070	I	O	|	|	|	|	2.65
42.750	0.00	0.09	0.069	I	O	|	|	|	|	2.64
42.833	0.00	0.09	0.069	I	O	|	|	|	|	2.62
42.917	0.00	0.09	0.068	I	O	|	|	|	|	2.61
43.000	0.00	0.09	0.068	I	O	|	|	|	|	2.59
43.083	0.00	0.09	0.067	I	O	|	|	|	|	2.58
43.167	0.00	0.09	0.066	I	O	|	|	|	|	2.56
43.250	0.00	0.09	0.066	I	O	|	|	|	|	2.55
43.333	0.00	0.09	0.065	I	O	|	|	|	|	2.53
43.417	0.00	0.09	0.065	I	O	|	|	|	|	2.52
43.500	0.00	0.09	0.064	I	O	|	|	|	|	2.50
43.583	0.00	0.09	0.064	I	O	|	|	|	|	2.49
43.667	0.00	0.09	0.063	I	O	|	|	|	|	2.47
43.750	0.00	0.09	0.062	I	O	|	|	|	|	2.45
43.833	0.00	0.09	0.062	I	O	|	|	|	|	2.44
43.917	0.00	0.09	0.061	I	O	|	|	|	|	2.42
44.000	0.00	0.09	0.061	I	O	|	|	|	|	2.40
44.083	0.00	0.09	0.060	I	O	|	|	|	|	2.39
44.167	0.00	0.09	0.059	I	O	|	|	|	|	2.37
44.250	0.00	0.09	0.059	I	O	|	|	|	|	2.35
44.333	0.00	0.09	0.058	I	O	|	|	|	|	2.34
44.417	0.00	0.09	0.058	I	O	|	|	|	|	2.32
44.500	0.00	0.09	0.057	I	O	|	|	|	|	2.31
44.583	0.00	0.09	0.056	I	O	|	|	|	|	2.29
44.667	0.00	0.09	0.056	I	O	|	|	|	|	2.27
44.750	0.00	0.09	0.055	I	O	|	|	|	|	2.26
44.833	0.00	0.09	0.055	I	O	|	|	|	|	2.24
44.917	0.00	0.09	0.054	I	O	|	|	|	|	2.22
45.000	0.00	0.09	0.053	I	O	|	|	|	|	2.21
45.083	0.00	0.09	0.053	I	O	|	|	|	|	2.19
45.167	0.00	0.09	0.052	I	O	|	|	|	|	2.17
45.250	0.00	0.09	0.052	I	O	|	|	|	|	2.16
45.333	0.00	0.09	0.051	I	O	|	|	|	|	2.14
45.417	0.00	0.09	0.050	I	O	|	|	|	|	2.12
45.500	0.00	0.09	0.050	I	O	|	|	|	|	2.11
45.583	0.00	0.09	0.049	I	O	|	|	|	|	2.09
45.667	0.00	0.09	0.049	I	O	|	|	|	|	2.08
45.750	0.00	0.09	0.048	I	O	|	|	|	|	2.06
45.833	0.00	0.09	0.048	I	O	|	|	|	|	2.04
45.917	0.00	0.09	0.047	I	O	|	|	|	|	2.03
46.000	0.00	0.09	0.046	I	O	|	|	|	|	2.01
46.083	0.00	0.09	0.046	I	O	|	|	|	|	1.99
46.167	0.00	0.09	0.045	I	O	|	|	|	|	1.97
46.250	0.00	0.09	0.045	I	O	|	|	|	|	1.95

46.333	0.00	0.09	0.044	I	O	|	|	|	|	1.93
46.417	0.00	0.09	0.043	I	O	|	|	|	|	1.91
46.500	0.00	0.09	0.043	I	O	|	|	|	|	1.89
46.583	0.00	0.09	0.042	I	O	|	|	|	|	1.87
46.667	0.00	0.09	0.042	I	O	|	|	|	|	1.85
46.750	0.00	0.09	0.041	I	O	|	|	|	|	1.83
46.833	0.00	0.09	0.040	I	O	|	|	|	|	1.81
46.917	0.00	0.09	0.040	I	O	|	|	|	|	1.79
47.000	0.00	0.09	0.039	I	O	|	|	|	|	1.77
47.083	0.00	0.09	0.039	I	O	|	|	|	|	1.75
47.167	0.00	0.09	0.038	I	O	|	|	|	|	1.73
47.250	0.00	0.09	0.037	I	O	|	|	|	|	1.72
47.333	0.00	0.09	0.037	I	O	|	|	|	|	1.70
47.417	0.00	0.09	0.036	I	O	|	|	|	|	1.68
47.500	0.00	0.09	0.036	I	O	|	|	|	|	1.66
47.583	0.00	0.09	0.035	I	O	|	|	|	|	1.64
47.667	0.00	0.09	0.034	I	O	|	|	|	|	1.62
47.750	0.00	0.09	0.034	I	O	|	|	|	|	1.60
47.833	0.00	0.09	0.033	I	O	|	|	|	|	1.58
47.917	0.00	0.09	0.033	I	O	|	|	|	|	1.56
48.000	0.00	0.09	0.032	I	O	|	|	|	|	1.54
48.083	0.00	0.09	0.032	I	O	|	|	|	|	1.52
48.167	0.00	0.09	0.031	I	O	|	|	|	|	1.50
48.250	0.00	0.09	0.030	I	O	|	|	|	|	1.47
48.333	0.00	0.09	0.030	I	O	|	|	|	|	1.44
48.417	0.00	0.09	0.029	I	O	|	|	|	|	1.41
48.500	0.00	0.09	0.029	I	O	|	|	|	|	1.38
48.583	0.00	0.09	0.028	I	O	|	|	|	|	1.35
48.667	0.00	0.09	0.027	I	O	|	|	|	|	1.32
48.750	0.00	0.09	0.027	I	O	|	|	|	|	1.29
48.833	0.00	0.09	0.026	I	O	|	|	|	|	1.26
48.917	0.00	0.09	0.026	I	O	|	|	|	|	1.23
49.000	0.00	0.09	0.025	I	O	|	|	|	|	1.20
49.083	0.00	0.09	0.024	I	O	|	|	|	|	1.17
49.167	0.00	0.09	0.024	I	O	|	|	|	|	1.14
49.250	0.00	0.09	0.023	I	O	|	|	|	|	1.11
49.333	0.00	0.09	0.023	I	O	|	|	|	|	1.08
49.417	0.00	0.09	0.022	I	O	|	|	|	|	1.05
49.500	0.00	0.09	0.021	I	O	|	|	|	|	1.02
49.583	0.00	0.09	0.021	I	O	|	|	|	|	0.99
49.667	0.00	0.09	0.020	I	O	|	|	|	|	0.96
49.750	0.00	0.09	0.020	I	O	|	|	|	|	0.93
49.833	0.00	0.09	0.019	I	O	|	|	|	|	0.90
49.917	0.00	0.09	0.019	I	O	|	|	|	|	0.88
50.000	0.00	0.09	0.018	I	O	|	|	|	|	0.85
50.083	0.00	0.09	0.017	I	O	|	|	|	|	0.82
50.167	0.00	0.09	0.017	I	O	|	|	|	|	0.79
50.250	0.00	0.09	0.016	I	O	|	|	|	|	0.76
50.333	0.00	0.09	0.016	I	O	|	|	|	|	0.73
50.417	0.00	0.09	0.015	I	O	|	|	|	|	0.70
50.500	0.00	0.09	0.014	I	O	|	|	|	|	0.67
50.583	0.00	0.09	0.014	I	O	|	|	|	|	0.64
50.667	0.00	0.09	0.013	I	O	|	|	|	|	0.61

50.750	0.00	0.09	0.013	I O	|	|	|	0.58
50.833	0.00	0.09	0.012	I O	|	|	|	0.55
50.917	0.00	0.09	0.011	I O	|	|	|	0.52
51.000	0.00	0.08	0.011	I O	|	|	|	0.49
51.083	0.00	0.08	0.010	I O	|	|	|	0.47
51.167	0.00	0.08	0.010	I O	|	|	|	0.44
51.250	0.00	0.07	0.009	I O	|	|	|	0.42
51.333	0.00	0.07	0.009	I O	|	|	|	0.40
51.417	0.00	0.06	0.008	I O	|	|	|	0.38
51.500	0.00	0.06	0.008	I O	|	|	|	0.36
51.583	0.00	0.06	0.007	I O	|	|	|	0.34
51.667	0.00	0.05	0.007	I O	|	|	|	0.32
51.750	0.00	0.05	0.007	I O	|	|	|	0.30
51.833	0.00	0.05	0.006	I O	|	|	|	0.29
51.917	0.00	0.05	0.006	I O	|	|	|	0.27
52.000	0.00	0.04	0.006	I O	|	|	|	0.26
52.083	0.00	0.04	0.005	I O	|	|	|	0.24
52.167	0.00	0.04	0.005	I O	|	|	|	0.23
52.250	0.00	0.04	0.005	IO	|	|	|	0.22
52.333	0.00	0.04	0.005	IO	|	|	|	0.21
52.417	0.00	0.03	0.004	IO	|	|	|	0.20
52.500	0.00	0.03	0.004	IO	|	|	|	0.19
52.583	0.00	0.03	0.004	IO	|	|	|	0.18
52.667	0.00	0.03	0.004	IO	|	|	|	0.17
52.750	0.00	0.03	0.003	IO	|	|	|	0.16
52.833	0.00	0.03	0.003	IO	|	|	|	0.15
52.917	0.00	0.02	0.003	IO	|	|	|	0.14
53.000	0.00	0.02	0.003	IO	|	|	|	0.13
53.083	0.00	0.02	0.003	IO	|	|	|	0.13
53.167	0.00	0.02	0.003	IO	|	|	|	0.12
53.250	0.00	0.02	0.003	IO	|	|	|	0.11
53.333	0.00	0.02	0.002	O	|	|	|	0.11
53.417	0.00	0.02	0.002	O	|	|	|	0.10
53.500	0.00	0.02	0.002	O	|	|	|	0.10
53.583	0.00	0.02	0.002	O	|	|	|	0.09
53.667	0.00	0.02	0.002	O	|	|	|	0.09
53.750	0.00	0.01	0.002	O	|	|	|	0.08
53.833	0.00	0.01	0.002	O	|	|	|	0.08
53.917	0.00	0.01	0.002	O	|	|	|	0.07
54.000	0.00	0.01	0.002	O	|	|	|	0.07
54.083	0.00	0.01	0.001	O	|	|	|	0.07
54.167	0.00	0.01	0.001	O	|	|	|	0.06
54.250	0.00	0.01	0.001	O	|	|	|	0.06
54.333	0.00	0.01	0.001	O	|	|	|	0.06
54.417	0.00	0.01	0.001	O	|	|	|	0.05
54.500	0.00	0.01	0.001	O	|	|	|	0.05
54.583	0.00	0.01	0.001	O	|	|	|	0.05
54.667	0.00	0.01	0.001	O	|	|	|	0.05
54.750	0.00	0.01	0.001	O	|	|	|	0.04
54.833	0.00	0.01	0.001	O	|	|	|	0.04
54.917	0.00	0.01	0.001	O	|	|	|	0.04
55.000	0.00	0.01	0.001	O	|	|	|	0.04
55.083	0.00	0.01	0.001	O	|	|	|	0.04

55.167	0.00	0.01	0.001	O	|	|	|	|	0.03
55.250	0.00	0.01	0.001	O	|	|	|	|	0.03
55.333	0.00	0.01	0.001	O	|	|	|	|	0.03
55.417	0.00	0.00	0.001	O	|	|	|	|	0.03
55.500	0.00	0.00	0.001	O	|	|	|	|	0.03
55.583	0.00	0.00	0.001	O	|	|	|	|	0.03
55.667	0.00	0.00	0.001	O	|	|	|	|	0.02
55.750	0.00	0.00	0.001	O	|	|	|	|	0.02
55.833	0.00	0.00	0.000	O	|	|	|	|	0.02
55.917	0.00	0.00	0.000	O	|	|	|	|	0.02
56.000	0.00	0.00	0.000	O	|	|	|	|	0.02
56.083	0.00	0.00	0.000	O	|	|	|	|	0.02
56.167	0.00	0.00	0.000	O	|	|	|	|	0.02
56.250	0.00	0.00	0.000	O	|	|	|	|	0.02
56.333	0.00	0.00	0.000	O	|	|	|	|	0.02
56.417	0.00	0.00	0.000	O	|	|	|	|	0.01
56.500	0.00	0.00	0.000	O	|	|	|	|	0.01
56.583	0.00	0.00	0.000	O	|	|	|	|	0.01
56.667	0.00	0.00	0.000	O	|	|	|	|	0.01
56.750	0.00	0.00	0.000	O	|	|	|	|	0.01
56.833	0.00	0.00	0.000	O	|	|	|	|	0.01
56.917	0.00	0.00	0.000	O	|	|	|	|	0.01
57.000	0.00	0.00	0.000	O	|	|	|	|	0.01
57.083	0.00	0.00	0.000	O	|	|	|	|	0.01
57.167	0.00	0.00	0.000	O	|	|	|	|	0.01
57.250	0.00	0.00	0.000	O	|	|	|	|	0.01
57.333	0.00	0.00	0.000	O	|	|	|	|	0.01
57.417	0.00	0.00	0.000	O	|	|	|	|	0.01
57.500	0.00	0.00	0.000	O	|	|	|	|	0.01
57.583	0.00	0.00	0.000	O	|	|	|	|	0.01
57.667	0.00	0.00	0.000	O	|	|	|	|	0.01
57.750	0.00	0.00	0.000	O	|	|	|	|	0.01
57.833	0.00	0.00	0.000	O	|	|	|	|	0.01
57.917	0.00	0.00	0.000	O	|	|	|	|	0.01

**********HYDROGRAPH DATA**********

Number of intervals = 695
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.086 (CFS)
Total volume = 0.357 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

AREA B1

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 07/21/25

ROUTING: BASIN B1; UNIT HYDROGRAPH B1

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARB124100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 291
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.760 (CFS)
Total volume = 0.438 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 101.000 to Point/Station 102.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 291
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.013	0.104	0.013	0.013
1.000	0.026	0.104	0.026	0.026
1.500	0.038	0.104	0.038	0.038
2.000	0.056	0.104	0.056	0.056
2.500	0.078	0.104	0.078	0.078
3.000	0.102	0.104	0.102	0.102
3.500	0.126	0.104	0.126	0.126
4.000	0.151	0.104	0.151	0.151
4.500	0.175	0.104	0.175	0.175
5.000	0.199	0.104	0.199	0.199
5.500	0.221	0.104	0.221	0.221
6.000	0.240	0.104	0.240	0.240
6.500	0.253	0.104	0.253	0.253
7.000	0.266	0.104	0.266	0.266
7.500	0.278	0.104	0.278	0.278
7.580	0.281	0.104	0.281	0.281

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.2	0.38	0.57	0.76	Depth (Ft.)
0.083	0.02	0.00	0.000	O	|	|	|	|	0.00
0.167	0.04	0.00	0.000	OI	|	|	|	|	0.01
0.250	0.04	0.00	0.000	OI	|	|	|	|	0.02
0.333	0.05	0.01	0.001	O I	|	|	|	|	0.03
0.417	0.06	0.01	0.001	O I	|	|	|	|	0.04
0.500	0.06	0.01	0.001	O I	|	|	|	|	0.06
0.583	0.06	0.01	0.002	O I	|	|	|	|	0.07
0.667	0.06	0.02	0.002	O I	|	|	|	|	0.08
0.750	0.06	0.02	0.002	O I	|	|	|	|	0.09
0.833	0.07	0.02	0.003	O I	|	|	|	|	0.11
0.917	0.08	0.03	0.003	|O I	|	|	|	|	0.12
1.000	0.08	0.03	0.004	|O I	|	|	|	|	0.14
1.083	0.07	0.03	0.004	|O I	|	|	|	|	0.15
1.167	0.07	0.03	0.004	|OI	|	|	|	|	0.16
1.250	0.06	0.03	0.004	|OI	|	|	|	|	0.17
1.333	0.06	0.04	0.005	|OI	|	|	|	|	0.17
1.417	0.06	0.04	0.005	|OI	|	|	|	|	0.18
1.500	0.06	0.04	0.005	|OI	|	|	|	|	0.19
1.583	0.06	0.04	0.005	|OI	|	|	|	|	0.19
1.667	0.06	0.04	0.005	|OI	|	|	|	|	0.20
1.750	0.06	0.04	0.005	|OI	|	|	|	|	0.21
1.833	0.07	0.04	0.006	|O I	|	|	|	|	0.21
1.917	0.08	0.05	0.006	|O I	|	|	|	|	0.22
2.000	0.08	0.05	0.006	| OI	|	|	|	|	0.23
2.083	0.08	0.05	0.006	| OI	|	|	|	|	0.24

2.167	0.08	0.05	0.006	OI				0.25
2.250	0.08	0.05	0.007	OI				0.26
2.333	0.08	0.06	0.007	OI				0.26
2.417	0.08	0.06	0.007	OI				0.27
2.500	0.08	0.06	0.007	OI				0.28
2.583	0.09	0.06	0.007	OI				0.29
2.667	0.10	0.06	0.008	O I				0.30
2.750	0.10	0.06	0.008	O I				0.31
2.833	0.11	0.07	0.008	O I				0.32
2.917	0.11	0.07	0.009	O I				0.33
3.000	0.11	0.07	0.009	O I				0.34
3.083	0.11	0.07	0.009	OI				0.35
3.167	0.11	0.07	0.009	OI				0.36
3.250	0.11	0.08	0.009	OI				0.36
3.333	0.11	0.08	0.010	OI				0.37
3.417	0.11	0.08	0.010	OI				0.38
3.500	0.11	0.08	0.010	OI				0.39
3.583	0.11	0.08	0.010	OI				0.39
3.667	0.11	0.08	0.010	OI				0.40
3.750	0.11	0.08	0.011	OI				0.40
3.833	0.11	0.09	0.011	OI				0.41
3.917	0.12	0.09	0.011	O I				0.42
4.000	0.13	0.09	0.011	O I				0.43
4.083	0.13	0.09	0.011	O I				0.44
4.167	0.13	0.09	0.012	O I				0.45
4.250	0.13	0.09	0.012	O I				0.46
4.333	0.14	0.10	0.012	OI				0.47
4.417	0.15	0.10	0.012	O I				0.48
4.500	0.15	0.10	0.013	O I				0.49
4.583	0.15	0.10	0.013	O I				0.50
4.667	0.15	0.10	0.013	O I				0.51
4.750	0.15	0.10	0.014	O I				0.52
4.833	0.16	0.10	0.014	O I				0.54
4.917	0.17	0.10	0.014	O I				0.55
5.000	0.17	0.10	0.015	O I				0.57
5.083	0.15	0.10	0.015	O I				0.58
5.167	0.13	0.10	0.015	OI				0.59
5.250	0.13	0.10	0.016	OI				0.60
5.333	0.14	0.10	0.016	OI				0.61
5.417	0.15	0.10	0.016	O I				0.62
5.500	0.15	0.10	0.016	O I				0.63
5.583	0.16	0.10	0.017	O I				0.64
5.667	0.17	0.10	0.017	O I				0.65
5.750	0.17	0.10	0.017	O I				0.67
5.833	0.17	0.10	0.018	O I				0.69
5.917	0.17	0.10	0.018	O I				0.71
6.000	0.17	0.10	0.019	O I				0.72
6.083	0.18	0.10	0.019	O I				0.74
6.167	0.19	0.10	0.020	O I				0.76
6.250	0.19	0.10	0.020	O I				0.78
6.333	0.19	0.10	0.021	O I				0.81
6.417	0.19	0.10	0.022	O I				0.83
6.500	0.19	0.10	0.022	O I				0.85

6.583	0.20	0.10	0.023	|	O	I	|	|	0.88
6.667	0.21	0.10	0.023	|	O	I	|	|	0.90
6.750	0.21	0.10	0.024	|	O	I	|	|	0.93
6.833	0.21	0.10	0.025	|	O	I	|	|	0.96
6.917	0.21	0.10	0.026	|	O	I	|	|	0.99
7.000	0.21	0.10	0.026	|	O	I	|	|	1.02
7.083	0.21	0.10	0.027	|	O	I	|	|	1.05
7.167	0.21	0.10	0.028	|	O	I	|	|	1.08
7.250	0.21	0.10	0.029	|	O	I	|	|	1.11
7.333	0.22	0.10	0.029	|	O	|I	|	|	1.14
7.417	0.23	0.10	0.030	|	O	|I	|	|	1.17
7.500	0.23	0.10	0.031	|	O	|I	|	|	1.21
7.583	0.24	0.10	0.032	|	O	| I	|	|	1.25
7.667	0.25	0.10	0.033	|	O	| I	|	|	1.29
7.750	0.25	0.10	0.034	|	O	| I	|	|	1.33
7.833	0.26	0.10	0.035	|	O	| I	|	|	1.38
7.917	0.27	0.10	0.036	|	O	| I	|	|	1.42
8.000	0.27	0.10	0.037	|	O	| I	|	|	1.47
8.083	0.29	0.10	0.039	|	O	| I	|	|	1.51
8.167	0.31	0.10	0.040	|	O	| I	|	|	1.55
8.250	0.31	0.10	0.041	|	O	| I	|	|	1.59
8.333	0.32	0.10	0.043	|	O	| I	|	|	1.63
8.417	0.32	0.10	0.044	|	O	| I	|	|	1.67
8.500	0.32	0.10	0.046	|	O	| I	|	|	1.71
8.583	0.33	0.10	0.047	|	O	| I	|	|	1.76
8.667	0.33	0.10	0.049	|	O	| I	|	|	1.80
8.750	0.34	0.10	0.050	|	O	| I	|	|	1.84
8.833	0.35	0.10	0.052	|	O	| I	|	|	1.89
8.917	0.36	0.10	0.054	|	O	| I	|	|	1.94
9.000	0.36	0.10	0.055	|	O	| I	|	|	1.98
9.083	0.38	0.10	0.057	|	O	| I	|	|	2.03
9.167	0.40	0.10	0.059	|	O	| I	|	|	2.07
9.250	0.40	0.10	0.061	|	O	| I	|	|	2.12
9.333	0.41	0.10	0.063	|	O	| |I	|	|	2.16
9.417	0.42	0.10	0.065	|	O	| |I	|	|	2.21
9.500	0.42	0.10	0.068	|	O	| |I	|	|	2.26
9.583	0.43	0.10	0.070	|	O	| | I	|	|	2.31
9.667	0.44	0.10	0.072	|	O	| | I	|	|	2.36
9.750	0.44	0.10	0.074	|	O	| | I	|	|	2.42
9.833	0.45	0.10	0.077	|	O	| | I	|	|	2.47
9.917	0.46	0.10	0.079	|	O	| | I	|	|	2.52
10.000	0.46	0.10	0.082	|	O	| | I	|	|	2.58
10.083	0.40	0.10	0.084	|	O	| I	|	|	2.62
10.167	0.33	0.10	0.086	|	O	| I	|	|	2.66
10.250	0.32	0.10	0.087	|	O	| I	|	|	2.69
10.333	0.32	0.10	0.089	|	O	| I	|	|	2.72
10.417	0.32	0.10	0.090	|	O	| I	|	|	2.75
10.500	0.32	0.10	0.092	|	O	| I	|	|	2.78
10.583	0.36	0.10	0.093	|	O	| I	|	|	2.82
10.667	0.41	0.10	0.095	|	O	| |I	|	|	2.86
10.750	0.42	0.10	0.097	|	O	| |I	|	|	2.90
10.833	0.42	0.10	0.099	|	O	| |I	|	|	2.95
10.917	0.42	0.10	0.102	|	O	| |I	|	|	2.99

11.000	0.42	0.10	0.104	|	O	|	|I	|	3.04
11.083	0.41	0.10	0.106	|	O	|	|I	|	3.08
11.167	0.40	0.10	0.108	|	O	|	I	|	3.13
11.250	0.40	0.10	0.110	|	O	|	I	|	3.17
11.333	0.40	0.10	0.112	|	O	|	I	|	3.21
11.417	0.40	0.10	0.114	|	O	|	I	|	3.25
11.500	0.40	0.10	0.116	|	O	|	I	|	3.30
11.583	0.38	0.10	0.118	|	O	|	I	|	3.34
11.667	0.36	0.10	0.120	|	O	|	I|	|	3.38
11.750	0.36	0.10	0.122	|	O	|	I|	|	3.41
11.833	0.37	0.10	0.124	|	O	|	I|	|	3.45
11.917	0.38	0.10	0.125	|	O	|	I|	|	3.49
12.000	0.38	0.10	0.127	|	O	|	I|	|	3.53
12.083	0.44	0.10	0.129	|	O	|	| I	|	3.57
12.167	0.51	0.10	0.132	|	O	|	| I	|	3.62
12.250	0.52	0.10	0.135	|	O	|	| I	|	3.68
12.333	0.54	0.10	0.138	|	O	|	| I	|	3.74
12.417	0.55	0.10	0.141	|	O	|	| I	|	3.80
12.500	0.55	0.10	0.144	|	O	|	| I|	|	3.86
12.583	0.57	0.10	0.147	|	O	|	| I|	|	3.92
12.667	0.59	0.10	0.150	|	O	|	| I	|	3.99
12.750	0.59	0.10	0.154	|	O	|	| |I	|	4.05
12.833	0.61	0.10	0.157	|	O	|	| |I	|	4.13
12.917	0.62	0.10	0.161	|	O	|	| | I	|	4.20
13.000	0.62	0.10	0.164	|	O	|	| | I	|	4.27
13.083	0.68	0.10	0.168	|	O	|	| | I	|	4.35
13.167	0.74	0.10	0.172	|	O	|	| | I|	|	4.44
13.250	0.75	0.10	0.177	|	O	|	| | I|	|	4.53
13.333	0.76	0.10	0.181	|	O	|	| | I|	|	4.63
13.417	0.76	0.10	0.186	|	O	|	| | I|	|	4.72
13.500	0.76	0.10	0.190	|	O	|	| | I	|	4.81
13.583	0.64	0.10	0.194	|	O	|	| | I	|	4.90
13.667	0.51	0.10	0.197	|	O	|	| I	|	4.97
13.750	0.49	0.10	0.200	|	O	|	| I	|	5.03
13.833	0.48	0.10	0.203	|	O	|	| I	|	5.09
13.917	0.48	0.10	0.205	|	O	|	| I	|	5.15
14.000	0.48	0.10	0.208	|	O	|	| I	|	5.20
14.083	0.53	0.10	0.211	|	O	|	| I	|	5.27
14.167	0.57	0.10	0.214	|	O	|	| I	|	5.34
14.250	0.58	0.10	0.217	|	O	|	| I	|	5.41
14.333	0.57	0.10	0.220	|	O	|	| I	|	5.48
14.417	0.56	0.10	0.224	|	O	|	| I|	|	5.57
14.500	0.56	0.10	0.227	|	O	|	| I|	|	5.65
14.583	0.56	0.10	0.230	|	O	|	| I|	|	5.73
14.667	0.56	0.10	0.233	|	O	|	| I|	|	5.81
14.750	0.56	0.10	0.236	|	O	|	| I|	|	5.90
14.833	0.55	0.10	0.239	|	O	|	| I|	|	5.98
14.917	0.54	0.10	0.242	|	O	|	| I	|	6.08
15.000	0.54	0.10	0.245	|	O	|	| I	|	6.20
15.083	0.52	0.10	0.248	|	O	|	| I	|	6.31
15.167	0.51	0.10	0.251	|	O	|	| I	|	6.42
15.250	0.51	0.10	0.254	|	O	|	| I	|	6.53
15.333	0.50	0.10	0.256	|	O	|	| I	|	6.63

15.417	0.49	0.10	0.259	| O |		| I |		|	6.74
15.500	0.49	0.10	0.262	| O |		| I |		|	6.84
15.583	0.45	0.10	0.264	| O |		| I |		|	6.93
15.667	0.41	0.10	0.267	| O |		|I |		|	7.02
15.750	0.40	0.10	0.269	| O |		I |		|	7.11
15.833	0.40	0.10	0.271	| O |		I |		|	7.19
15.917	0.40	0.10	0.273	| O |		I |		|	7.28
16.000	0.40	0.10	0.275	| O |		I |		|	7.36
16.083	0.26	0.10	0.276	| O |	I |			|	7.43
16.167	0.12	0.10	0.277	| OI |				|	7.45
16.250	0.09	0.10	0.277	| IO |				|	7.45
16.333	0.08	0.10	0.277	| IO |				|	7.45
16.417	0.08	0.10	0.277	| IO |				|	7.44
16.500	0.08	0.10	0.277	| IO |				|	7.44
16.583	0.07	0.10	0.276	| IO |				|	7.43
16.667	0.07	0.10	0.276	| I O |				|	7.42
16.750	0.06	0.10	0.276	| I O |				|	7.41
16.833	0.06	0.10	0.276	| I O |				|	7.40
16.917	0.06	0.10	0.275	| I O |				|	7.39
17.000	0.06	0.10	0.275	| I O |				|	7.38
17.083	0.08	0.10	0.275	| IO |				|	7.37
17.167	0.10	0.10	0.275	| O |				|	7.36
17.250	0.10	0.10	0.275	| O |				|	7.36
17.333	0.11	0.10	0.275	| O |				|	7.36
17.417	0.11	0.10	0.275	| O |				|	7.36
17.500	0.11	0.10	0.275	| O |				|	7.36
17.583	0.11	0.10	0.275	| O |				|	7.36
17.667	0.11	0.10	0.275	| O |				|	7.36
17.750	0.11	0.10	0.275	| O |				|	7.36
17.833	0.10	0.10	0.275	| O |				|	7.36
17.917	0.09	0.10	0.275	| IO |				|	7.36
18.000	0.08	0.10	0.275	| IO |				|	7.35
18.083	0.08	0.10	0.274	| IO |				|	7.35
18.167	0.08	0.10	0.274	| IO |				|	7.34
18.250	0.08	0.10	0.274	| IO |				|	7.34
18.333	0.08	0.10	0.274	| IO |				|	7.33
18.417	0.08	0.10	0.274	| IO |				|	7.33
18.500	0.08	0.10	0.274	| IO |				|	7.32
18.583	0.07	0.10	0.274	| IO |				|	7.31
18.667	0.07	0.10	0.273	| I O |				|	7.30
18.750	0.06	0.10	0.273	| I O |				|	7.29
18.833	0.05	0.10	0.273	| I O |				|	7.28
18.917	0.04	0.10	0.272	|I O |				|	7.26
19.000	0.04	0.10	0.272	|I O |				|	7.25
19.083	0.05	0.10	0.272	| I O |				|	7.23
19.167	0.06	0.10	0.271	| I O |				|	7.22
19.250	0.06	0.10	0.271	| I O |				|	7.20
19.333	0.07	0.10	0.271	| IO |				|	7.19
19.417	0.08	0.10	0.270	| IO |				|	7.19
19.500	0.08	0.10	0.270	| IO |				|	7.18
19.583	0.07	0.10	0.270	| IO |				|	7.17
19.667	0.07	0.10	0.270	| I O |				|	7.16
19.750	0.06	0.10	0.270	| I O |				|	7.15

19.833	0.05	0.10	0.269	| I O	|	|	|	7.14
19.917	0.04	0.10	0.269	|I O	|	|	|	7.12
20.000	0.04	0.10	0.269	|I O	|	|	|	7.11
20.083	0.05	0.10	0.268	| I O	|	|	|	7.09
20.167	0.06	0.10	0.268	| I O	|	|	|	7.08
20.250	0.06	0.10	0.268	| I O	|	|	|	7.06
20.333	0.06	0.10	0.267	| I O	|	|	|	7.05
20.417	0.06	0.10	0.267	| I O	|	|	|	7.04
20.500	0.06	0.10	0.267	| I O	|	|	|	7.03
20.583	0.06	0.10	0.266	| I O	|	|	|	7.02
20.667	0.06	0.10	0.266	| I O	|	|	|	7.01
20.750	0.06	0.10	0.266	| I O	|	|	|	6.99
20.833	0.05	0.10	0.266	| I O	|	|	|	6.98
20.917	0.04	0.10	0.265	|I O	|	|	|	6.97
21.000	0.04	0.10	0.265	|I O	|	|	|	6.95
21.083	0.05	0.10	0.264	| I O	|	|	|	6.94
21.167	0.06	0.10	0.264	| I O	|	|	|	6.92
21.250	0.06	0.10	0.264	| I O	|	|	|	6.91
21.333	0.05	0.10	0.263	| I O	|	|	|	6.90
21.417	0.04	0.10	0.263	|I O	|	|	|	6.89
21.500	0.04	0.10	0.263	|I O	|	|	|	6.87
21.583	0.05	0.10	0.262	| I O	|	|	|	6.85
21.667	0.06	0.10	0.262	| I O	|	|	|	6.84
21.750	0.06	0.10	0.262	| I O	|	|	|	6.83
21.833	0.05	0.10	0.261	| I O	|	|	|	6.82
21.917	0.04	0.10	0.261	|I O	|	|	|	6.80
22.000	0.04	0.10	0.260	|I O	|	|	|	6.79
22.083	0.05	0.10	0.260	| I O	|	|	|	6.77
22.167	0.06	0.10	0.260	| I O	|	|	|	6.76
22.250	0.06	0.10	0.259	| I O	|	|	|	6.75
22.333	0.05	0.10	0.259	| I O	|	|	|	6.74
22.417	0.04	0.10	0.259	|I O	|	|	|	6.72
22.500	0.04	0.10	0.258	|I O	|	|	|	6.71
22.583	0.04	0.10	0.258	|I O	|	|	|	6.69
22.667	0.04	0.10	0.258	|I O	|	|	|	6.67
22.750	0.04	0.10	0.257	|I O	|	|	|	6.66
22.833	0.04	0.10	0.257	|I O	|	|	|	6.64
22.917	0.04	0.10	0.256	|I O	|	|	|	6.62
23.000	0.04	0.10	0.256	|I O	|	|	|	6.61
23.083	0.04	0.10	0.255	|I O	|	|	|	6.59
23.167	0.04	0.10	0.255	|I O	|	|	|	6.58
23.250	0.04	0.10	0.255	|I O	|	|	|	6.56
23.333	0.04	0.10	0.254	|I O	|	|	|	6.54
23.417	0.04	0.10	0.254	|I O	|	|	|	6.53
23.500	0.04	0.10	0.253	|I O	|	|	|	6.51
23.583	0.04	0.10	0.253	|I O	|	|	|	6.49
23.667	0.04	0.10	0.252	|I O	|	|	|	6.48
23.750	0.04	0.10	0.252	|I O	|	|	|	6.46
23.833	0.04	0.10	0.252	|I O	|	|	|	6.44
23.917	0.04	0.10	0.251	|I O	|	|	|	6.43
24.000	0.04	0.10	0.251	|I O	|	|	|	6.41
24.083	0.02	0.10	0.250	I O	|	|	|	6.39
24.167	0.00	0.10	0.250	I O	|	|	|	6.37

24.250	0.00	0.10	0.249	I	O	|	|	|	|	6.34
24.333	0.00	0.10	0.248	I	O	|	|	|	|	6.31
24.417	0.00	0.10	0.247	I	O	|	|	|	|	6.29
24.500	0.00	0.10	0.247	I	O	|	|	|	|	6.26
24.583	0.00	0.10	0.246	I	O	|	|	|	|	6.23
24.667	0.00	0.10	0.245	I	O	|	|	|	|	6.20
24.750	0.00	0.10	0.245	I	O	|	|	|	|	6.18
24.833	0.00	0.10	0.244	I	O	|	|	|	|	6.15
24.917	0.00	0.10	0.243	I	O	|	|	|	|	6.12
25.000	0.00	0.10	0.242	I	O	|	|	|	|	6.09
25.083	0.00	0.10	0.242	I	O	|	|	|	|	6.07
25.167	0.00	0.10	0.241	I	O	|	|	|	|	6.04
25.250	0.00	0.10	0.240	I	O	|	|	|	|	6.01
25.333	0.00	0.10	0.240	I	O	|	|	|	|	5.99
25.417	0.00	0.10	0.239	I	O	|	|	|	|	5.97
25.500	0.00	0.10	0.238	I	O	|	|	|	|	5.95
25.583	0.00	0.10	0.237	I	O	|	|	|	|	5.93
25.667	0.00	0.10	0.237	I	O	|	|	|	|	5.91
25.750	0.00	0.10	0.236	I	O	|	|	|	|	5.89
25.833	0.00	0.10	0.235	I	O	|	|	|	|	5.88
25.917	0.00	0.10	0.235	I	O	|	|	|	|	5.86
26.000	0.00	0.10	0.234	I	O	|	|	|	|	5.84
26.083	0.00	0.10	0.233	I	O	|	|	|	|	5.82
26.167	0.00	0.10	0.232	I	O	|	|	|	|	5.80
26.250	0.00	0.10	0.232	I	O	|	|	|	|	5.78
26.333	0.00	0.10	0.231	I	O	|	|	|	|	5.76
26.417	0.00	0.10	0.230	I	O	|	|	|	|	5.74
26.500	0.00	0.10	0.230	I	O	|	|	|	|	5.73
26.583	0.00	0.10	0.229	I	O	|	|	|	|	5.71
26.667	0.00	0.10	0.228	I	O	|	|	|	|	5.69
26.750	0.00	0.10	0.227	I	O	|	|	|	|	5.67
26.833	0.00	0.10	0.227	I	O	|	|	|	|	5.65
26.917	0.00	0.10	0.226	I	O	|	|	|	|	5.63
27.000	0.00	0.10	0.225	I	O	|	|	|	|	5.61
27.083	0.00	0.10	0.225	I	O	|	|	|	|	5.59
27.167	0.00	0.10	0.224	I	O	|	|	|	|	5.57
27.250	0.00	0.10	0.223	I	O	|	|	|	|	5.56
27.333	0.00	0.10	0.222	I	O	|	|	|	|	5.54
27.417	0.00	0.10	0.222	I	O	|	|	|	|	5.52
27.500	0.00	0.10	0.221	I	O	|	|	|	|	5.50
27.583	0.00	0.10	0.220	I	O	|	|	|	|	5.48
27.667	0.00	0.10	0.220	I	O	|	|	|	|	5.47
27.750	0.00	0.10	0.219	I	O	|	|	|	|	5.45
27.833	0.00	0.10	0.218	I	O	|	|	|	|	5.43
27.917	0.00	0.10	0.217	I	O	|	|	|	|	5.42
28.000	0.00	0.10	0.217	I	O	|	|	|	|	5.40
28.083	0.00	0.10	0.216	I	O	|	|	|	|	5.39
28.167	0.00	0.10	0.215	I	O	|	|	|	|	5.37
28.250	0.00	0.10	0.215	I	O	|	|	|	|	5.35
28.333	0.00	0.10	0.214	I	O	|	|	|	|	5.34
28.417	0.00	0.10	0.213	I	O	|	|	|	|	5.32
28.500	0.00	0.10	0.212	I	O	|	|	|	|	5.30
28.583	0.00	0.10	0.212	I	O	|	|	|	|	5.29

28.667	0.00	0.10	0.211	I	O	|	|	|	|	5.27
28.750	0.00	0.10	0.210	I	O	|	|	|	|	5.26
28.833	0.00	0.10	0.210	I	O	|	|	|	|	5.24
28.917	0.00	0.10	0.209	I	O	|	|	|	|	5.22
29.000	0.00	0.10	0.208	I	O	|	|	|	|	5.21
29.083	0.00	0.10	0.207	I	O	|	|	|	|	5.19
29.167	0.00	0.10	0.207	I	O	|	|	|	|	5.17
29.250	0.00	0.10	0.206	I	O	|	|	|	|	5.16
29.333	0.00	0.10	0.205	I	O	|	|	|	|	5.14
29.417	0.00	0.10	0.204	I	O	|	|	|	|	5.12
29.500	0.00	0.10	0.204	I	O	|	|	|	|	5.11
29.583	0.00	0.10	0.203	I	O	|	|	|	|	5.09
29.667	0.00	0.10	0.202	I	O	|	|	|	|	5.08
29.750	0.00	0.10	0.202	I	O	|	|	|	|	5.06
29.833	0.00	0.10	0.201	I	O	|	|	|	|	5.04
29.917	0.00	0.10	0.200	I	O	|	|	|	|	5.03
30.000	0.00	0.10	0.199	I	O	|	|	|	|	5.01
30.083	0.00	0.10	0.199	I	O	|	|	|	|	5.00
30.167	0.00	0.10	0.198	I	O	|	|	|	|	4.98
30.250	0.00	0.10	0.197	I	O	|	|	|	|	4.97
30.333	0.00	0.10	0.197	I	O	|	|	|	|	4.95
30.417	0.00	0.10	0.196	I	O	|	|	|	|	4.94
30.500	0.00	0.10	0.195	I	O	|	|	|	|	4.92
30.583	0.00	0.10	0.194	I	O	|	|	|	|	4.91
30.667	0.00	0.10	0.194	I	O	|	|	|	|	4.89
30.750	0.00	0.10	0.193	I	O	|	|	|	|	4.88
30.833	0.00	0.10	0.192	I	O	|	|	|	|	4.86
30.917	0.00	0.10	0.192	I	O	|	|	|	|	4.85
31.000	0.00	0.10	0.191	I	O	|	|	|	|	4.83
31.083	0.00	0.10	0.190	I	O	|	|	|	|	4.82
31.167	0.00	0.10	0.189	I	O	|	|	|	|	4.80
31.250	0.00	0.10	0.189	I	O	|	|	|	|	4.79
31.333	0.00	0.10	0.188	I	O	|	|	|	|	4.77
31.417	0.00	0.10	0.187	I	O	|	|	|	|	4.76
31.500	0.00	0.10	0.187	I	O	|	|	|	|	4.74
31.583	0.00	0.10	0.186	I	O	|	|	|	|	4.73
31.667	0.00	0.10	0.185	I	O	|	|	|	|	4.71
31.750	0.00	0.10	0.184	I	O	|	|	|	|	4.70
31.833	0.00	0.10	0.184	I	O	|	|	|	|	4.68
31.917	0.00	0.10	0.183	I	O	|	|	|	|	4.67
32.000	0.00	0.10	0.182	I	O	|	|	|	|	4.65
32.083	0.00	0.10	0.182	I	O	|	|	|	|	4.64
32.167	0.00	0.10	0.181	I	O	|	|	|	|	4.62
32.250	0.00	0.10	0.180	I	O	|	|	|	|	4.61
32.333	0.00	0.10	0.179	I	O	|	|	|	|	4.59
32.417	0.00	0.10	0.179	I	O	|	|	|	|	4.58
32.500	0.00	0.10	0.178	I	O	|	|	|	|	4.56
32.583	0.00	0.10	0.177	I	O	|	|	|	|	4.55
32.667	0.00	0.10	0.177	I	O	|	|	|	|	4.53
32.750	0.00	0.10	0.176	I	O	|	|	|	|	4.52
32.833	0.00	0.10	0.175	I	O	|	|	|	|	4.50
32.917	0.00	0.10	0.174	I	O	|	|	|	|	4.49
33.000	0.00	0.10	0.174	I	O	|	|	|	|	4.47

33.083	0.00	0.10	0.173	I	O	|	|	|	|	4.46
33.167	0.00	0.10	0.172	I	O	|	|	|	|	4.44
33.250	0.00	0.10	0.172	I	O	|	|	|	|	4.43
33.333	0.00	0.10	0.171	I	O	|	|	|	|	4.41
33.417	0.00	0.10	0.170	I	O	|	|	|	|	4.40
33.500	0.00	0.10	0.169	I	O	|	|	|	|	4.38
33.583	0.00	0.10	0.169	I	O	|	|	|	|	4.37
33.667	0.00	0.10	0.168	I	O	|	|	|	|	4.35
33.750	0.00	0.10	0.167	I	O	|	|	|	|	4.34
33.833	0.00	0.10	0.167	I	O	|	|	|	|	4.32
33.917	0.00	0.10	0.166	I	O	|	|	|	|	4.31
34.000	0.00	0.10	0.165	I	O	|	|	|	|	4.29
34.083	0.00	0.10	0.164	I	O	|	|	|	|	4.28
34.167	0.00	0.10	0.164	I	O	|	|	|	|	4.26
34.250	0.00	0.10	0.163	I	O	|	|	|	|	4.25
34.333	0.00	0.10	0.162	I	O	|	|	|	|	4.23
34.417	0.00	0.10	0.162	I	O	|	|	|	|	4.22
34.500	0.00	0.10	0.161	I	O	|	|	|	|	4.20
34.583	0.00	0.10	0.160	I	O	|	|	|	|	4.19
34.667	0.00	0.10	0.159	I	O	|	|	|	|	4.17
34.750	0.00	0.10	0.159	I	O	|	|	|	|	4.16
34.833	0.00	0.10	0.158	I	O	|	|	|	|	4.14
34.917	0.00	0.10	0.157	I	O	|	|	|	|	4.13
35.000	0.00	0.10	0.157	I	O	|	|	|	|	4.11
35.083	0.00	0.10	0.156	I	O	|	|	|	|	4.10
35.167	0.00	0.10	0.155	I	O	|	|	|	|	4.08
35.250	0.00	0.10	0.154	I	O	|	|	|	|	4.07
35.333	0.00	0.10	0.154	I	O	|	|	|	|	4.05
35.417	0.00	0.10	0.153	I	O	|	|	|	|	4.04
35.500	0.00	0.10	0.152	I	O	|	|	|	|	4.03
35.583	0.00	0.10	0.151	I	O	|	|	|	|	4.01
35.667	0.00	0.10	0.151	I	O	|	|	|	|	4.00
35.750	0.00	0.10	0.150	I	O	|	|	|	|	3.98
35.833	0.00	0.10	0.149	I	O	|	|	|	|	3.97
35.917	0.00	0.10	0.149	I	O	|	|	|	|	3.95
36.000	0.00	0.10	0.148	I	O	|	|	|	|	3.94
36.083	0.00	0.10	0.147	I	O	|	|	|	|	3.92
36.167	0.00	0.10	0.146	I	O	|	|	|	|	3.91
36.250	0.00	0.10	0.146	I	O	|	|	|	|	3.90
36.333	0.00	0.10	0.145	I	O	|	|	|	|	3.88
36.417	0.00	0.10	0.144	I	O	|	|	|	|	3.87
36.500	0.00	0.10	0.144	I	O	|	|	|	|	3.85
36.583	0.00	0.10	0.143	I	O	|	|	|	|	3.84
36.667	0.00	0.10	0.142	I	O	|	|	|	|	3.82
36.750	0.00	0.10	0.141	I	O	|	|	|	|	3.81
36.833	0.00	0.10	0.141	I	O	|	|	|	|	3.79
36.917	0.00	0.10	0.140	I	O	|	|	|	|	3.78
37.000	0.00	0.10	0.139	I	O	|	|	|	|	3.77
37.083	0.00	0.10	0.139	I	O	|	|	|	|	3.75
37.167	0.00	0.10	0.138	I	O	|	|	|	|	3.74
37.250	0.00	0.10	0.137	I	O	|	|	|	|	3.72
37.333	0.00	0.10	0.136	I	O	|	|	|	|	3.71
37.417	0.00	0.10	0.136	I	O	|	|	|	|	3.69

37.500	0.00	0.10	0.135	I	O	|	|	|	|	3.68
37.583	0.00	0.10	0.134	I	O	|	|	|	|	3.67
37.667	0.00	0.10	0.134	I	O	|	|	|	|	3.65
37.750	0.00	0.10	0.133	I	O	|	|	|	|	3.64
37.833	0.00	0.10	0.132	I	O	|	|	|	|	3.62
37.917	0.00	0.10	0.131	I	O	|	|	|	|	3.61
38.000	0.00	0.10	0.131	I	O	|	|	|	|	3.59
38.083	0.00	0.10	0.130	I	O	|	|	|	|	3.58
38.167	0.00	0.10	0.129	I	O	|	|	|	|	3.57
38.250	0.00	0.10	0.129	I	O	|	|	|	|	3.55
38.333	0.00	0.10	0.128	I	O	|	|	|	|	3.54
38.417	0.00	0.10	0.127	I	O	|	|	|	|	3.52
38.500	0.00	0.10	0.126	I	O	|	|	|	|	3.51
38.583	0.00	0.10	0.126	I	O	|	|	|	|	3.49
38.667	0.00	0.10	0.125	I	O	|	|	|	|	3.48
38.750	0.00	0.10	0.124	I	O	|	|	|	|	3.46
38.833	0.00	0.10	0.124	I	O	|	|	|	|	3.45
38.917	0.00	0.10	0.123	I	O	|	|	|	|	3.43
39.000	0.00	0.10	0.122	I	O	|	|	|	|	3.42
39.083	0.00	0.10	0.121	I	O	|	|	|	|	3.40
39.167	0.00	0.10	0.121	I	O	|	|	|	|	3.39
39.250	0.00	0.10	0.120	I	O	|	|	|	|	3.37
39.333	0.00	0.10	0.119	I	O	|	|	|	|	3.36
39.417	0.00	0.10	0.119	I	O	|	|	|	|	3.34
39.500	0.00	0.10	0.118	I	O	|	|	|	|	3.33
39.583	0.00	0.10	0.117	I	O	|	|	|	|	3.31
39.667	0.00	0.10	0.116	I	O	|	|	|	|	3.30
39.750	0.00	0.10	0.116	I	O	|	|	|	|	3.28
39.833	0.00	0.10	0.115	I	O	|	|	|	|	3.27
39.917	0.00	0.10	0.114	I	O	|	|	|	|	3.26
40.000	0.00	0.10	0.114	I	O	|	|	|	|	3.24
40.083	0.00	0.10	0.113	I	O	|	|	|	|	3.23
40.167	0.00	0.10	0.112	I	O	|	|	|	|	3.21
40.250	0.00	0.10	0.111	I	O	|	|	|	|	3.20
40.333	0.00	0.10	0.111	I	O	|	|	|	|	3.18
40.417	0.00	0.10	0.110	I	O	|	|	|	|	3.17
40.500	0.00	0.10	0.109	I	O	|	|	|	|	3.15
40.583	0.00	0.10	0.109	I	O	|	|	|	|	3.14
40.667	0.00	0.10	0.108	I	O	|	|	|	|	3.12
40.750	0.00	0.10	0.107	I	O	|	|	|	|	3.11
40.833	0.00	0.10	0.106	I	O	|	|	|	|	3.09
40.917	0.00	0.10	0.106	I	O	|	|	|	|	3.08
41.000	0.00	0.10	0.105	I	O	|	|	|	|	3.06
41.083	0.00	0.10	0.104	I	O	|	|	|	|	3.05
41.167	0.00	0.10	0.103	I	O	|	|	|	|	3.03
41.250	0.00	0.10	0.103	I	O	|	|	|	|	3.02
41.333	0.00	0.10	0.102	I	O	|	|	|	|	3.00
41.417	0.00	0.10	0.101	I	O	|	|	|	|	2.99
41.500	0.00	0.10	0.101	I	O	|	|	|	|	2.97
41.583	0.00	0.10	0.100	I	O	|	|	|	|	2.96
41.667	0.00	0.10	0.099	I	O	|	|	|	|	2.94
41.750	0.00	0.10	0.098	I	O	|	|	|	|	2.93
41.833	0.00	0.10	0.098	I	O	|	|	|	|	2.91

41.917	0.00	0.10	0.097	I	O	|	|	|	|	2.90
42.000	0.00	0.10	0.096	I	O	|	|	|	|	2.88
42.083	0.00	0.10	0.096	I	O	|	|	|	|	2.87
42.167	0.00	0.10	0.095	I	O	|	|	|	|	2.85
42.250	0.00	0.10	0.094	I	O	|	|	|	|	2.84
42.333	0.00	0.10	0.093	I	O	|	|	|	|	2.82
42.417	0.00	0.10	0.093	I	O	|	|	|	|	2.81
42.500	0.00	0.10	0.092	I	O	|	|	|	|	2.79
42.583	0.00	0.10	0.091	I	O	|	|	|	|	2.78
42.667	0.00	0.10	0.091	I	O	|	|	|	|	2.76
42.750	0.00	0.10	0.090	I	O	|	|	|	|	2.75
42.833	0.00	0.10	0.089	I	O	|	|	|	|	2.73
42.917	0.00	0.10	0.088	I	O	|	|	|	|	2.72
43.000	0.00	0.10	0.088	I	O	|	|	|	|	2.70
43.083	0.00	0.10	0.087	I	O	|	|	|	|	2.69
43.167	0.00	0.10	0.086	I	O	|	|	|	|	2.67
43.250	0.00	0.10	0.086	I	O	|	|	|	|	2.66
43.333	0.00	0.10	0.085	I	O	|	|	|	|	2.64
43.417	0.00	0.10	0.084	I	O	|	|	|	|	2.63
43.500	0.00	0.10	0.083	I	O	|	|	|	|	2.61
43.583	0.00	0.10	0.083	I	O	|	|	|	|	2.60
43.667	0.00	0.10	0.082	I	O	|	|	|	|	2.58
43.750	0.00	0.10	0.081	I	O	|	|	|	|	2.57
43.833	0.00	0.10	0.081	I	O	|	|	|	|	2.55
43.917	0.00	0.10	0.080	I	O	|	|	|	|	2.54
44.000	0.00	0.10	0.079	I	O	|	|	|	|	2.52
44.083	0.00	0.10	0.078	I	O	|	|	|	|	2.51
44.167	0.00	0.10	0.078	I	O	|	|	|	|	2.49
44.250	0.00	0.10	0.077	I	O	|	|	|	|	2.48
44.333	0.00	0.10	0.076	I	O	|	|	|	|	2.46
44.417	0.00	0.10	0.076	I	O	|	|	|	|	2.44
44.500	0.00	0.10	0.075	I	O	|	|	|	|	2.43
44.583	0.00	0.10	0.074	I	O	|	|	|	|	2.41
44.667	0.00	0.10	0.073	I	O	|	|	|	|	2.40
44.750	0.00	0.10	0.073	I	O	|	|	|	|	2.38
44.833	0.00	0.10	0.072	I	O	|	|	|	|	2.36
44.917	0.00	0.10	0.071	I	O	|	|	|	|	2.35
45.000	0.00	0.10	0.071	I	O	|	|	|	|	2.33
45.083	0.00	0.10	0.070	I	O	|	|	|	|	2.31
45.167	0.00	0.10	0.069	I	O	|	|	|	|	2.30
45.250	0.00	0.10	0.068	I	O	|	|	|	|	2.28
45.333	0.00	0.10	0.068	I	O	|	|	|	|	2.27
45.417	0.00	0.10	0.067	I	O	|	|	|	|	2.25
45.500	0.00	0.10	0.066	I	O	|	|	|	|	2.23
45.583	0.00	0.10	0.066	I	O	|	|	|	|	2.22
45.667	0.00	0.10	0.065	I	O	|	|	|	|	2.20
45.750	0.00	0.10	0.064	I	O	|	|	|	|	2.18
45.833	0.00	0.10	0.063	I	O	|	|	|	|	2.17
45.917	0.00	0.10	0.063	I	O	|	|	|	|	2.15
46.000	0.00	0.10	0.062	I	O	|	|	|	|	2.14
46.083	0.00	0.10	0.061	I	O	|	|	|	|	2.12
46.167	0.00	0.10	0.061	I	O	|	|	|	|	2.10
46.250	0.00	0.10	0.060	I	O	|	|	|	|	2.09

46.333	0.00	0.10	0.059	I	O	|	|	|	|	2.07
46.417	0.00	0.10	0.058	I	O	|	|	|	|	2.05
46.500	0.00	0.10	0.058	I	O	|	|	|	|	2.04
46.583	0.00	0.10	0.057	I	O	|	|	|	|	2.02
46.667	0.00	0.10	0.056	I	O	|	|	|	|	2.01
46.750	0.00	0.10	0.056	I	O	|	|	|	|	1.99
46.833	0.00	0.10	0.055	I	O	|	|	|	|	1.97
46.917	0.00	0.10	0.054	I	O	|	|	|	|	1.95
47.000	0.00	0.10	0.053	I	O	|	|	|	|	1.93
47.083	0.00	0.10	0.053	I	O	|	|	|	|	1.91
47.167	0.00	0.10	0.052	I	O	|	|	|	|	1.89
47.250	0.00	0.10	0.051	I	O	|	|	|	|	1.87
47.333	0.00	0.10	0.050	I	O	|	|	|	|	1.85
47.417	0.00	0.10	0.050	I	O	|	|	|	|	1.83
47.500	0.00	0.10	0.049	I	O	|	|	|	|	1.81
47.583	0.00	0.10	0.048	I	O	|	|	|	|	1.79
47.667	0.00	0.10	0.048	I	O	|	|	|	|	1.77
47.750	0.00	0.10	0.047	I	O	|	|	|	|	1.75
47.833	0.00	0.10	0.046	I	O	|	|	|	|	1.73
47.917	0.00	0.10	0.045	I	O	|	|	|	|	1.71
48.000	0.00	0.10	0.045	I	O	|	|	|	|	1.69
48.083	0.00	0.10	0.044	I	O	|	|	|	|	1.67
48.167	0.00	0.10	0.043	I	O	|	|	|	|	1.65
48.250	0.00	0.10	0.043	I	O	|	|	|	|	1.63
48.333	0.00	0.10	0.042	I	O	|	|	|	|	1.61
48.417	0.00	0.10	0.041	I	O	|	|	|	|	1.59
48.500	0.00	0.10	0.040	I	O	|	|	|	|	1.57
48.583	0.00	0.10	0.040	I	O	|	|	|	|	1.55
48.667	0.00	0.10	0.039	I	O	|	|	|	|	1.53
48.750	0.00	0.10	0.038	I	O	|	|	|	|	1.51
48.833	0.00	0.10	0.038	I	O	|	|	|	|	1.48
48.917	0.00	0.10	0.037	I	O	|	|	|	|	1.45
49.000	0.00	0.10	0.036	I	O	|	|	|	|	1.42
49.083	0.00	0.10	0.035	I	O	|	|	|	|	1.39
49.167	0.00	0.10	0.035	I	O	|	|	|	|	1.36
49.250	0.00	0.10	0.034	I	O	|	|	|	|	1.33
49.333	0.00	0.10	0.033	I	O	|	|	|	|	1.30
49.417	0.00	0.10	0.033	I	O	|	|	|	|	1.27
49.500	0.00	0.10	0.032	I	O	|	|	|	|	1.24
49.583	0.00	0.10	0.031	I	O	|	|	|	|	1.21
49.667	0.00	0.10	0.030	I	O	|	|	|	|	1.19
49.750	0.00	0.10	0.030	I	O	|	|	|	|	1.16
49.833	0.00	0.10	0.029	I	O	|	|	|	|	1.13
49.917	0.00	0.10	0.028	I	O	|	|	|	|	1.10
50.000	0.00	0.10	0.028	I	O	|	|	|	|	1.07
50.083	0.00	0.10	0.027	I	O	|	|	|	|	1.04
50.167	0.00	0.10	0.026	I	O	|	|	|	|	1.01
50.250	0.00	0.10	0.025	I	O	|	|	|	|	0.98
50.333	0.00	0.10	0.025	I	O	|	|	|	|	0.95
50.417	0.00	0.10	0.024	I	O	|	|	|	|	0.92
50.500	0.00	0.10	0.023	I	O	|	|	|	|	0.90
50.583	0.00	0.10	0.023	I	O	|	|	|	|	0.87
50.667	0.00	0.10	0.022	I	O	|	|	|	|	0.84

50.750	0.00	0.10	0.021	I O	|	|	|	0.81
50.833	0.00	0.10	0.020	I O	|	|	|	0.79
50.917	0.00	0.10	0.020	I O	|	|	|	0.76
51.000	0.00	0.10	0.019	I O	|	|	|	0.73
51.083	0.00	0.10	0.018	I O	|	|	|	0.70
51.167	0.00	0.10	0.018	I O	|	|	|	0.67
51.250	0.00	0.10	0.017	I O	|	|	|	0.65
51.333	0.00	0.10	0.016	I O	|	|	|	0.62
51.417	0.00	0.10	0.015	I O	|	|	|	0.59
51.500	0.00	0.10	0.015	I O	|	|	|	0.56
51.583	0.00	0.10	0.014	I O	|	|	|	0.54
51.667	0.00	0.10	0.013	I O	|	|	|	0.51
51.750	0.00	0.10	0.013	I O	|	|	|	0.48
51.833	0.00	0.09	0.012	I O	|	|	|	0.46
51.917	0.00	0.09	0.011	I O	|	|	|	0.43
52.000	0.00	0.09	0.011	I O	|	|	|	0.41
52.083	0.00	0.08	0.010	I O	|	|	|	0.39
52.167	0.00	0.08	0.010	I O	|	|	|	0.37
52.250	0.00	0.07	0.009	I O	|	|	|	0.35
52.333	0.00	0.07	0.009	I O	|	|	|	0.33
52.417	0.00	0.06	0.008	I O	|	|	|	0.31
52.500	0.00	0.06	0.008	I O	|	|	|	0.29
52.583	0.00	0.06	0.007	I O	|	|	|	0.28
52.667	0.00	0.05	0.007	I O	|	|	|	0.26
52.750	0.00	0.05	0.006	I O	|	|	|	0.25
52.833	0.00	0.05	0.006	I O	|	|	|	0.24
52.917	0.00	0.05	0.006	IO	|	|	|	0.22
53.000	0.00	0.04	0.005	IO	|	|	|	0.21
53.083	0.00	0.04	0.005	IO	|	|	|	0.20
53.167	0.00	0.04	0.005	IO	|	|	|	0.19
53.250	0.00	0.04	0.005	IO	|	|	|	0.18
53.333	0.00	0.04	0.004	IO	|	|	|	0.17
53.417	0.00	0.03	0.004	IO	|	|	|	0.16
53.500	0.00	0.03	0.004	IO	|	|	|	0.15
53.583	0.00	0.03	0.004	IO	|	|	|	0.14
53.667	0.00	0.03	0.004	IO	|	|	|	0.14
53.750	0.00	0.03	0.003	IO	|	|	|	0.13
53.833	0.00	0.03	0.003	IO	|	|	|	0.12
53.917	0.00	0.02	0.003	IO	|	|	|	0.12
54.000	0.00	0.02	0.003	O	|	|	|	0.11
54.083	0.00	0.02	0.003	O	|	|	|	0.10
54.167	0.00	0.02	0.003	O	|	|	|	0.10
54.250	0.00	0.02	0.002	O	|	|	|	0.09
54.333	0.00	0.02	0.002	O	|	|	|	0.09
54.417	0.00	0.02	0.002	O	|	|	|	0.08
54.500	0.00	0.02	0.002	O	|	|	|	0.08
54.583	0.00	0.02	0.002	O	|	|	|	0.07
54.667	0.00	0.01	0.002	O	|	|	|	0.07
54.750	0.00	0.01	0.002	O	|	|	|	0.07
54.833	0.00	0.01	0.002	O	|	|	|	0.06
54.917	0.00	0.01	0.002	O	|	|	|	0.06
55.000	0.00	0.01	0.001	O	|	|	|	0.06
55.083	0.00	0.01	0.001	O	|	|	|	0.05

55.167	0.00	0.01	0.001	O	|	|	|	|	0.05
55.250	0.00	0.01	0.001	O	|	|	|	|	0.05
55.333	0.00	0.01	0.001	O	|	|	|	|	0.05
55.417	0.00	0.01	0.001	O	|	|	|	|	0.04
55.500	0.00	0.01	0.001	O	|	|	|	|	0.04
55.583	0.00	0.01	0.001	O	|	|	|	|	0.04
55.667	0.00	0.01	0.001	O	|	|	|	|	0.04
55.750	0.00	0.01	0.001	O	|	|	|	|	0.03
55.833	0.00	0.01	0.001	O	|	|	|	|	0.03
55.917	0.00	0.01	0.001	O	|	|	|	|	0.03
56.000	0.00	0.01	0.001	O	|	|	|	|	0.03
56.083	0.00	0.01	0.001	O	|	|	|	|	0.03
56.167	0.00	0.01	0.001	O	|	|	|	|	0.03
56.250	0.00	0.01	0.001	O	|	|	|	|	0.02
56.333	0.00	0.00	0.001	O	|	|	|	|	0.02
56.417	0.00	0.00	0.001	O	|	|	|	|	0.02
56.500	0.00	0.00	0.001	O	|	|	|	|	0.02
56.583	0.00	0.00	0.001	O	|	|	|	|	0.02
56.667	0.00	0.00	0.000	O	|	|	|	|	0.02
56.750	0.00	0.00	0.000	O	|	|	|	|	0.02
56.833	0.00	0.00	0.000	O	|	|	|	|	0.02
56.917	0.00	0.00	0.000	O	|	|	|	|	0.02
57.000	0.00	0.00	0.000	O	|	|	|	|	0.01
57.083	0.00	0.00	0.000	O	|	|	|	|	0.01
57.167	0.00	0.00	0.000	O	|	|	|	|	0.01
57.250	0.00	0.00	0.000	O	|	|	|	|	0.01
57.333	0.00	0.00	0.000	O	|	|	|	|	0.01
57.417	0.00	0.00	0.000	O	|	|	|	|	0.01
57.500	0.00	0.00	0.000	O	|	|	|	|	0.01
57.583	0.00	0.00	0.000	O	|	|	|	|	0.01
57.667	0.00	0.00	0.000	O	|	|	|	|	0.01
57.750	0.00	0.00	0.000	O	|	|	|	|	0.01
57.833	0.00	0.00	0.000	O	|	|	|	|	0.01
57.917	0.00	0.00	0.000	O	|	|	|	|	0.01
58.000	0.00	0.00	0.000	O	|	|	|	|	0.01
58.083	0.00	0.00	0.000	O	|	|	|	|	0.01
58.167	0.00	0.00	0.000	O	|	|	|	|	0.01
58.250	0.00	0.00	0.000	O	|	|	|	|	0.01
58.333	0.00	0.00	0.000	O	|	|	|	|	0.01
58.417	0.00	0.00	0.000	O	|	|	|	|	0.01
58.500	0.00	0.00	0.000	O	|	|	|	|	0.01
58.583	0.00	0.00	0.000	O	|	|	|	|	0.01
58.667	0.00	0.00	0.000	O	|	|	|	|	0.00
58.750	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 705
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.104 (CFS)
Total volume = 0.438 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000

Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

AREA BB1

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 07/21/25

ROUTING: BASIN BB1; UNIT HYDROGRAPH BB1

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARBB124100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 291
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.736 (CFS)
Total volume = 0.422 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 101.000 to Point/Station 102.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 291
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.013	0.101	0.013	0.013
1.000	0.025	0.101	0.025	0.025
1.500	0.037	0.101	0.037	0.037
2.000	0.055	0.101	0.055	0.055
2.500	0.076	0.101	0.076	0.076
3.000	0.099	0.101	0.099	0.099
3.500	0.123	0.101	0.123	0.123
4.000	0.147	0.101	0.147	0.147
4.500	0.170	0.101	0.170	0.170
5.000	0.193	0.101	0.193	0.193
5.500	0.215	0.101	0.215	0.215
6.000	0.234	0.101	0.234	0.234
6.500	0.246	0.101	0.246	0.246
7.000	0.258	0.101	0.258	0.258
7.500	0.271	0.101	0.271	0.271
7.580	0.273	0.101	0.273	0.273

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.2 0.37 0.55 0.74	Depth (Ft.)
0.083	0.02	0.00	0.000	O | | | |	0.00
0.167	0.04	0.00	0.000	OI | | | |	0.01
0.250	0.04	0.00	0.000	OI | | | |	0.02
0.333	0.05	0.01	0.001	O I | | | |	0.03
0.417	0.06	0.01	0.001	O I | | | |	0.04
0.500	0.06	0.01	0.001	O I | | | |	0.05
0.583	0.06	0.01	0.002	O I | | | |	0.07
0.667	0.06	0.02	0.002	O I | | | |	0.08
0.750	0.06	0.02	0.002	O I | | | |	0.09
0.833	0.07	0.02	0.003	O I | | | |	0.10
0.917	0.08	0.02	0.003	|O I | | | |	0.12
1.000	0.08	0.03	0.003	|O I | | | |	0.13
1.083	0.07	0.03	0.004	|O I | | | |	0.14
1.167	0.06	0.03	0.004	|OI | | | |	0.15
1.250	0.06	0.03	0.004	|OI | | | |	0.16
1.333	0.06	0.03	0.004	|OI | | | |	0.17
1.417	0.06	0.04	0.005	|OI | | | |	0.18
1.500	0.06	0.04	0.005	|OI | | | |	0.18
1.583	0.06	0.04	0.005	|OI | | | |	0.19
1.667	0.06	0.04	0.005	|OI | | | |	0.19
1.750	0.06	0.04	0.005	|OI | | | |	0.20
1.833	0.07	0.04	0.005	|O I | | | |	0.21
1.917	0.08	0.04	0.006	|O I | | | |	0.22
2.000	0.08	0.05	0.006	|O I | | | |	0.22
2.083	0.08	0.05	0.006	| OI | | | |	0.23

2.167	0.08	0.05	0.006	OI				0.24
2.250	0.08	0.05	0.007	OI				0.25
2.333	0.08	0.05	0.007	OI				0.26
2.417	0.08	0.05	0.007	OI				0.27
2.500	0.08	0.06	0.007	OI				0.27
2.583	0.09	0.06	0.007	OI				0.28
2.667	0.10	0.06	0.008	O I				0.29
2.750	0.10	0.06	0.008	O I				0.30
2.833	0.10	0.06	0.008	O I				0.31
2.917	0.10	0.06	0.008	O I				0.32
3.000	0.10	0.07	0.009	O I				0.33
3.083	0.10	0.07	0.009	O I				0.34
3.167	0.10	0.07	0.009	OI				0.35
3.250	0.10	0.07	0.009	OI				0.36
3.333	0.10	0.07	0.009	OI				0.36
3.417	0.10	0.07	0.010	OI				0.37
3.500	0.10	0.08	0.010	OI				0.38
3.583	0.10	0.08	0.010	OI				0.38
3.667	0.10	0.08	0.010	OI				0.39
3.750	0.10	0.08	0.010	OI				0.40
3.833	0.11	0.08	0.010	OI				0.40
3.917	0.12	0.08	0.011	O I				0.41
4.000	0.12	0.09	0.011	O I				0.42
4.083	0.12	0.09	0.011	O I				0.43
4.167	0.12	0.09	0.011	O I				0.44
4.250	0.12	0.09	0.012	O I				0.45
4.333	0.13	0.09	0.012	OI				0.46
4.417	0.14	0.09	0.012	O I				0.47
4.500	0.14	0.10	0.012	O I				0.48
4.583	0.14	0.10	0.013	O I				0.49
4.667	0.14	0.10	0.013	O I				0.50
4.750	0.14	0.10	0.013	O I				0.51
4.833	0.15	0.10	0.014	O I				0.53
4.917	0.16	0.10	0.014	O I				0.54
5.000	0.16	0.10	0.014	O I				0.56
5.083	0.14	0.10	0.015	O I				0.58
5.167	0.13	0.10	0.015	OI				0.59
5.250	0.12	0.10	0.015	OI				0.59
5.333	0.13	0.10	0.015	OI				0.60
5.417	0.14	0.10	0.016	O I				0.61
5.500	0.14	0.10	0.016	O I				0.62
5.583	0.15	0.10	0.016	O I				0.63
5.667	0.16	0.10	0.017	O I				0.65
5.750	0.16	0.10	0.017	O I				0.67
5.833	0.16	0.10	0.017	O I				0.68
5.917	0.16	0.10	0.018	O I				0.70
6.000	0.16	0.10	0.018	O I				0.72
6.083	0.17	0.10	0.019	O I				0.74
6.167	0.18	0.10	0.019	O I				0.76
6.250	0.18	0.10	0.020	O I				0.78
6.333	0.18	0.10	0.020	O I				0.81
6.417	0.18	0.10	0.021	O I				0.83
6.500	0.18	0.10	0.021	O I				0.85

6.583	0.19	0.10	0.022	|	O	I	|	|	0.88
6.667	0.20	0.10	0.023	|	O	I	|	|	0.90
6.750	0.20	0.10	0.023	|	O	I	|	|	0.93
6.833	0.20	0.10	0.024	|	O	I	|	|	0.96
6.917	0.20	0.10	0.025	|	O	I	|	|	0.99
7.000	0.20	0.10	0.025	|	O	I	|	|	1.02
7.083	0.20	0.10	0.026	|	O	I	|	|	1.05
7.167	0.20	0.10	0.027	|	O	I	|	|	1.08
7.250	0.20	0.10	0.028	|	O	I	|	|	1.11
7.333	0.21	0.10	0.028	|	O	|I	|	|	1.14
7.417	0.22	0.10	0.029	|	O	|I	|	|	1.17
7.500	0.22	0.10	0.030	|	O	|I	|	|	1.21
7.583	0.23	0.10	0.031	|	O	| I	|	|	1.24
7.667	0.24	0.10	0.032	|	O	| I	|	|	1.28
7.750	0.24	0.10	0.033	|	O	| I	|	|	1.32
7.833	0.25	0.10	0.034	|	O	| I	|	|	1.36
7.917	0.26	0.10	0.035	|	O	| I	|	|	1.41
8.000	0.26	0.10	0.036	|	O	| I	|	|	1.45
8.083	0.28	0.10	0.037	|	O	| I	|	|	1.50
8.167	0.30	0.10	0.038	|	O	| I	|	|	1.54
8.250	0.30	0.10	0.040	|	O	| I	|	|	1.58
8.333	0.30	0.10	0.041	|	O	| I	|	|	1.62
8.417	0.30	0.10	0.043	|	O	| I	|	|	1.65
8.500	0.30	0.10	0.044	|	O	| I	|	|	1.69
8.583	0.31	0.10	0.045	|	O	| I	|	|	1.73
8.667	0.32	0.10	0.047	|	O	| I	|	|	1.77
8.750	0.32	0.10	0.048	|	O	| I	|	|	1.82
8.833	0.33	0.10	0.050	|	O	| I	|	|	1.86
8.917	0.34	0.10	0.052	|	O	| I	|	|	1.91
9.000	0.34	0.10	0.053	|	O	| I	|	|	1.95
9.083	0.36	0.10	0.055	|	O	| I|	|	|	2.00
9.167	0.38	0.10	0.057	|	O	| I	|	|	2.05
9.250	0.38	0.10	0.059	|	O	| I	|	|	2.09
9.333	0.39	0.10	0.061	|	O	| |I	|	|	2.14
9.417	0.40	0.10	0.063	|	O	| |I	|	|	2.19
9.500	0.40	0.10	0.065	|	O	| |I	|	|	2.24
9.583	0.41	0.10	0.067	|	O	| | I	|	|	2.29
9.667	0.42	0.10	0.069	|	O	| | I	|	|	2.34
9.750	0.43	0.10	0.072	|	O	| | I	|	|	2.39
9.833	0.43	0.10	0.074	|	O	| | I	|	|	2.45
9.917	0.44	0.10	0.076	|	O	| | I	|	|	2.50
10.000	0.45	0.10	0.078	|	O	| | I	|	|	2.55
10.083	0.38	0.10	0.081	|	O	| I	|	|	2.60
10.167	0.32	0.10	0.082	|	O	| I	|	|	2.64
10.250	0.31	0.10	0.084	|	O	| I	|	|	2.67
10.333	0.30	0.10	0.085	|	O	| I	|	|	2.70
10.417	0.30	0.10	0.087	|	O	| I	|	|	2.73
10.500	0.30	0.10	0.088	|	O	| I	|	|	2.76
10.583	0.35	0.10	0.090	|	O	| I|	|	|	2.79
10.667	0.39	0.10	0.091	|	O	| |I	|	|	2.84
10.750	0.40	0.10	0.093	|	O	| |I	|	|	2.88
10.833	0.41	0.10	0.096	|	O	| |I	|	|	2.93
10.917	0.41	0.10	0.098	|	O	| |I	|	|	2.97

11.000	0.41	0.10	0.100	|	O	|	|I	|	3.02
11.083	0.40	0.10	0.102	|	O	|	|I	|	3.06
11.167	0.39	0.10	0.104	|	O	|	I	|	3.10
11.250	0.39	0.10	0.106	|	O	|	I	|	3.14
11.333	0.39	0.10	0.108	|	O	|	I	|	3.18
11.417	0.39	0.10	0.110	|	O	|	I	|	3.22
11.500	0.39	0.10	0.112	|	O	|	I	|	3.26
11.583	0.37	0.10	0.114	|	O	|	I|	|	3.30
11.667	0.35	0.10	0.115	|	O	|	I|	|	3.34
11.750	0.35	0.10	0.117	|	O	|	I|	|	3.38
11.833	0.35	0.10	0.119	|	O	|	I|	|	3.41
11.917	0.36	0.10	0.121	|	O	|	I|	|	3.45
12.000	0.36	0.10	0.122	|	O	|	I|	|	3.49
12.083	0.43	0.10	0.124	|	O	|	| I	|	3.53
12.167	0.49	0.10	0.127	|	O	|	| I	|	3.58
12.250	0.50	0.10	0.130	|	O	|	| I	|	3.64
12.333	0.52	0.10	0.132	|	O	|	| I	|	3.70
12.417	0.52	0.10	0.135	|	O	|	| I	|	3.76
12.500	0.53	0.10	0.138	|	O	|	| I	|	3.82
12.583	0.55	0.10	0.141	|	O	|	| I|	|	3.88
12.667	0.57	0.10	0.144	|	O	|	| I	|	3.94
12.750	0.57	0.10	0.148	|	O	|	| I	|	4.01
12.833	0.58	0.10	0.151	|	O	|	|I	|	4.08
12.917	0.60	0.10	0.154	|	O	|	|I	|	4.16
13.000	0.60	0.10	0.158	|	O	|	| I	|	4.23
13.083	0.66	0.10	0.161	|	O	|	| I	|	4.31
13.167	0.72	0.10	0.165	|	O	|	| I|	|	4.40
13.250	0.73	0.10	0.170	|	O	|	| I|	|	4.49
13.333	0.73	0.10	0.174	|	O	|	| I|	|	4.59
13.417	0.74	0.10	0.178	|	O	|	| I|	|	4.68
13.500	0.74	0.10	0.183	|	O	|	| I	|	4.78
13.583	0.61	0.10	0.187	|	O	|	| I	|	4.86
13.667	0.49	0.10	0.190	|	O	|	| I	|	4.93
13.750	0.47	0.10	0.192	|	O	|	| I	|	4.99
13.833	0.47	0.10	0.195	|	O	|	| I	|	5.04
13.917	0.47	0.10	0.197	|	O	|	| I	|	5.10
14.000	0.47	0.10	0.200	|	O	|	| I	|	5.16
14.083	0.51	0.10	0.203	|	O	|	| I	|	5.22
14.167	0.55	0.10	0.206	|	O	|	| I|	|	5.29
14.250	0.56	0.10	0.209	|	O	|	| I	|	5.36
14.333	0.55	0.10	0.212	|	O	|	| I|	|	5.43
14.417	0.54	0.10	0.215	|	O	|	| I|	|	5.50
14.500	0.54	0.10	0.218	|	O	|	| I|	|	5.57
14.583	0.54	0.10	0.221	|	O	|	| I|	|	5.65
14.667	0.54	0.10	0.224	|	O	|	| I|	|	5.73
14.750	0.54	0.10	0.227	|	O	|	| I|	|	5.81
14.833	0.53	0.10	0.230	|	O	|	| I	|	5.89
14.917	0.52	0.10	0.233	|	O	|	| I	|	5.97
15.000	0.51	0.10	0.236	|	O	|	| I	|	6.06
15.083	0.50	0.10	0.238	|	O	|	| I	|	6.18
15.167	0.49	0.10	0.241	|	O	|	| I	|	6.29
15.250	0.49	0.10	0.244	|	O	|	| I	|	6.41
15.333	0.48	0.10	0.246	|	O	|	| I	|	6.52

15.417	0.47	0.10	0.249	| O |		| I |		|	6.62
15.500	0.47	0.10	0.251	| O |		| I |		|	6.73
15.583	0.43	0.10	0.254	| O |		| I |		|	6.83
15.667	0.39	0.10	0.256	| O |		|I |		|	6.92
15.750	0.39	0.10	0.258	| O |		I |		|	7.00
15.833	0.39	0.10	0.260	| O |		I |		|	7.08
15.917	0.39	0.10	0.262	| O |		I |		|	7.15
16.000	0.39	0.10	0.264	| O |		I |		|	7.23
16.083	0.25	0.10	0.265	| O |	I	|		|	7.28
16.167	0.11	0.10	0.266	| O |		|		|	7.30
16.250	0.09	0.10	0.266	| IO |		|		|	7.30
16.333	0.08	0.10	0.266	| IO |		|		|	7.30
16.417	0.08	0.10	0.266	| IO |		|		|	7.29
16.500	0.08	0.10	0.266	| IO |		|		|	7.29
16.583	0.07	0.10	0.265	| IO |		|		|	7.28
16.667	0.06	0.10	0.265	| I O |		|		|	7.27
16.750	0.06	0.10	0.265	| I O |		|		|	7.26
16.833	0.06	0.10	0.265	| I O |		|		|	7.25
16.917	0.06	0.10	0.264	| I O |		|		|	7.24
17.000	0.06	0.10	0.264	| I O |		|		|	7.23
17.083	0.08	0.10	0.264	| IO |		|		|	7.22
17.167	0.10	0.10	0.264	| O |		|		|	7.22
17.250	0.10	0.10	0.264	| O |		|		|	7.22
17.333	0.10	0.10	0.264	| O |		|		|	7.22
17.417	0.10	0.10	0.264	| O |		|		|	7.22
17.500	0.10	0.10	0.264	| O |		|		|	7.22
17.583	0.10	0.10	0.264	| O |		|		|	7.22
17.667	0.10	0.10	0.264	| O |		|		|	7.22
17.750	0.10	0.10	0.264	| O |		|		|	7.22
17.833	0.09	0.10	0.264	| O |		|		|	7.22
17.917	0.08	0.10	0.264	| IO |		|		|	7.22
18.000	0.08	0.10	0.263	| IO |		|		|	7.21
18.083	0.08	0.10	0.263	| IO |		|		|	7.20
18.167	0.08	0.10	0.263	| IO |		|		|	7.20
18.250	0.08	0.10	0.263	| IO |		|		|	7.19
18.333	0.08	0.10	0.263	| IO |		|		|	7.19
18.417	0.08	0.10	0.263	| IO |		|		|	7.18
18.500	0.08	0.10	0.263	| IO |		|		|	7.18
18.583	0.07	0.10	0.262	| IO |		|		|	7.17
18.667	0.06	0.10	0.262	| I O |		|		|	7.16
18.750	0.06	0.10	0.262	| I O |		|		|	7.15
18.833	0.05	0.10	0.262	| I O |		|		|	7.14
18.917	0.04	0.10	0.261	|I O |		|		|	7.13
19.000	0.04	0.10	0.261	|I O |		|		|	7.11
19.083	0.05	0.10	0.261	| I O |		|		|	7.10
19.167	0.06	0.10	0.260	| I O |		|		|	7.08
19.250	0.06	0.10	0.260	| I O |		|		|	7.07
19.333	0.07	0.10	0.260	| IO |		|		|	7.06
19.417	0.08	0.10	0.259	| IO |		|		|	7.06
19.500	0.08	0.10	0.259	| IO |		|		|	7.05
19.583	0.07	0.10	0.259	| IO |		|		|	7.04
19.667	0.06	0.10	0.259	| I O |		|		|	7.04
19.750	0.06	0.10	0.259	| I O |		|		|	7.03

19.833	0.05	0.10	0.258	| I O	|	|	|	7.01
19.917	0.04	0.10	0.258	|I O	|	|	|	7.00
20.000	0.04	0.10	0.258	|I O	|	|	|	6.98
20.083	0.05	0.10	0.257	| I O	|	|	|	6.97
20.167	0.06	0.10	0.257	| I O	|	|	|	6.95
20.250	0.06	0.10	0.257	| I O	|	|	|	6.94
20.333	0.06	0.10	0.256	| I O	|	|	|	6.93
20.417	0.06	0.10	0.256	| I O	|	|	|	6.92
20.500	0.06	0.10	0.256	| I O	|	|	|	6.91
20.583	0.06	0.10	0.255	| I O	|	|	|	6.89
20.667	0.06	0.10	0.255	| I O	|	|	|	6.88
20.750	0.06	0.10	0.255	| I O	|	|	|	6.87
20.833	0.05	0.10	0.255	| I O	|	|	|	6.86
20.917	0.04	0.10	0.254	|I O	|	|	|	6.84
21.000	0.04	0.10	0.254	|I O	|	|	|	6.83
21.083	0.05	0.10	0.253	| I O	|	|	|	6.81
21.167	0.06	0.10	0.253	| I O	|	|	|	6.80
21.250	0.06	0.10	0.253	| I O	|	|	|	6.78
21.333	0.05	0.10	0.253	| I O	|	|	|	6.77
21.417	0.04	0.10	0.252	|I O	|	|	|	6.76
21.500	0.04	0.10	0.252	|I O	|	|	|	6.74
21.583	0.05	0.10	0.251	| I O	|	|	|	6.72
21.667	0.06	0.10	0.251	| I O	|	|	|	6.71
21.750	0.06	0.10	0.251	| I O	|	|	|	6.70
21.833	0.05	0.10	0.250	| I O	|	|	|	6.69
21.917	0.04	0.10	0.250	|I O	|	|	|	6.67
22.000	0.04	0.10	0.250	|I O	|	|	|	6.65
22.083	0.05	0.10	0.249	| I O	|	|	|	6.64
22.167	0.06	0.10	0.249	| I O	|	|	|	6.62
22.250	0.06	0.10	0.249	| I O	|	|	|	6.61
22.333	0.05	0.10	0.248	| I O	|	|	|	6.60
22.417	0.04	0.10	0.248	|I O	|	|	|	6.58
22.500	0.04	0.10	0.248	|I O	|	|	|	6.57
22.583	0.04	0.10	0.247	|I O	|	|	|	6.55
22.667	0.04	0.10	0.247	|I O	|	|	|	6.53
22.750	0.04	0.10	0.246	|I O	|	|	|	6.51
22.833	0.04	0.10	0.246	|I O	|	|	|	6.50
22.917	0.04	0.10	0.246	|I O	|	|	|	6.48
23.000	0.04	0.10	0.245	|I O	|	|	|	6.46
23.083	0.04	0.10	0.245	|I O	|	|	|	6.44
23.167	0.04	0.10	0.244	|I O	|	|	|	6.43
23.250	0.04	0.10	0.244	|I O	|	|	|	6.41
23.333	0.04	0.10	0.243	|I O	|	|	|	6.39
23.417	0.04	0.10	0.243	|I O	|	|	|	6.38
23.500	0.04	0.10	0.243	|I O	|	|	|	6.36
23.583	0.04	0.10	0.242	|I O	|	|	|	6.34
23.667	0.04	0.10	0.242	|I O	|	|	|	6.32
23.750	0.04	0.10	0.241	|I O	|	|	|	6.31
23.833	0.04	0.10	0.241	|I O	|	|	|	6.29
23.917	0.04	0.10	0.241	|I O	|	|	|	6.27
24.000	0.04	0.10	0.240	|I O	|	|	|	6.25
24.083	0.02	0.10	0.240	I O	|	|	|	6.23
24.167	0.00	0.10	0.239	I O	|	|	|	6.21

24.250	0.00	0.10	0.238	I	O	|	|	|	|	6.18
24.333	0.00	0.10	0.238	I	O	|	|	|	|	6.15
24.417	0.00	0.10	0.237	I	O	|	|	|	|	6.12
24.500	0.00	0.10	0.236	I	O	|	|	|	|	6.09
24.583	0.00	0.10	0.236	I	O	|	|	|	|	6.06
24.667	0.00	0.10	0.235	I	O	|	|	|	|	6.04
24.750	0.00	0.10	0.234	I	O	|	|	|	|	6.01
24.833	0.00	0.10	0.233	I	O	|	|	|	|	5.99
24.917	0.00	0.10	0.233	I	O	|	|	|	|	5.97
25.000	0.00	0.10	0.232	I	O	|	|	|	|	5.95
25.083	0.00	0.10	0.231	I	O	|	|	|	|	5.93
25.167	0.00	0.10	0.231	I	O	|	|	|	|	5.91
25.250	0.00	0.10	0.230	I	O	|	|	|	|	5.89
25.333	0.00	0.10	0.229	I	O	|	|	|	|	5.88
25.417	0.00	0.10	0.229	I	O	|	|	|	|	5.86
25.500	0.00	0.10	0.228	I	O	|	|	|	|	5.84
25.583	0.00	0.10	0.227	I	O	|	|	|	|	5.82
25.667	0.00	0.10	0.227	I	O	|	|	|	|	5.80
25.750	0.00	0.10	0.226	I	O	|	|	|	|	5.78
25.833	0.00	0.10	0.225	I	O	|	|	|	|	5.77
25.917	0.00	0.10	0.224	I	O	|	|	|	|	5.75
26.000	0.00	0.10	0.224	I	O	|	|	|	|	5.73
26.083	0.00	0.10	0.223	I	O	|	|	|	|	5.71
26.167	0.00	0.10	0.222	I	O	|	|	|	|	5.69
26.250	0.00	0.10	0.222	I	O	|	|	|	|	5.67
26.333	0.00	0.10	0.221	I	O	|	|	|	|	5.66
26.417	0.00	0.10	0.220	I	O	|	|	|	|	5.64
26.500	0.00	0.10	0.220	I	O	|	|	|	|	5.62
26.583	0.00	0.10	0.219	I	O	|	|	|	|	5.60
26.667	0.00	0.10	0.218	I	O	|	|	|	|	5.58
26.750	0.00	0.10	0.217	I	O	|	|	|	|	5.56
26.833	0.00	0.10	0.217	I	O	|	|	|	|	5.55
26.917	0.00	0.10	0.216	I	O	|	|	|	|	5.53
27.000	0.00	0.10	0.215	I	O	|	|	|	|	5.51
27.083	0.00	0.10	0.215	I	O	|	|	|	|	5.49
27.167	0.00	0.10	0.214	I	O	|	|	|	|	5.48
27.250	0.00	0.10	0.213	I	O	|	|	|	|	5.46
27.333	0.00	0.10	0.213	I	O	|	|	|	|	5.45
27.417	0.00	0.10	0.212	I	O	|	|	|	|	5.43
27.500	0.00	0.10	0.211	I	O	|	|	|	|	5.41
27.583	0.00	0.10	0.211	I	O	|	|	|	|	5.40
27.667	0.00	0.10	0.210	I	O	|	|	|	|	5.38
27.750	0.00	0.10	0.209	I	O	|	|	|	|	5.37
27.833	0.00	0.10	0.208	I	O	|	|	|	|	5.35
27.917	0.00	0.10	0.208	I	O	|	|	|	|	5.33
28.000	0.00	0.10	0.207	I	O	|	|	|	|	5.32
28.083	0.00	0.10	0.206	I	O	|	|	|	|	5.30
28.167	0.00	0.10	0.206	I	O	|	|	|	|	5.29
28.250	0.00	0.10	0.205	I	O	|	|	|	|	5.27
28.333	0.00	0.10	0.204	I	O	|	|	|	|	5.26
28.417	0.00	0.10	0.204	I	O	|	|	|	|	5.24
28.500	0.00	0.10	0.203	I	O	|	|	|	|	5.22
28.583	0.00	0.10	0.202	I	O	|	|	|	|	5.21

28.667	0.00	0.10	0.201	I	O	|	|	|	|	5.19
28.750	0.00	0.10	0.201	I	O	|	|	|	|	5.18
28.833	0.00	0.10	0.200	I	O	|	|	|	|	5.16
28.917	0.00	0.10	0.199	I	O	|	|	|	|	5.15
29.000	0.00	0.10	0.199	I	O	|	|	|	|	5.13
29.083	0.00	0.10	0.198	I	O	|	|	|	|	5.11
29.167	0.00	0.10	0.197	I	O	|	|	|	|	5.10
29.250	0.00	0.10	0.197	I	O	|	|	|	|	5.08
29.333	0.00	0.10	0.196	I	O	|	|	|	|	5.07
29.417	0.00	0.10	0.195	I	O	|	|	|	|	5.05
29.500	0.00	0.10	0.195	I	O	|	|	|	|	5.03
29.583	0.00	0.10	0.194	I	O	|	|	|	|	5.02
29.667	0.00	0.10	0.193	I	O	|	|	|	|	5.00
29.750	0.00	0.10	0.192	I	O	|	|	|	|	4.99
29.833	0.00	0.10	0.192	I	O	|	|	|	|	4.97
29.917	0.00	0.10	0.191	I	O	|	|	|	|	4.96
30.000	0.00	0.10	0.190	I	O	|	|	|	|	4.94
30.083	0.00	0.10	0.190	I	O	|	|	|	|	4.93
30.167	0.00	0.10	0.189	I	O	|	|	|	|	4.91
30.250	0.00	0.10	0.188	I	O	|	|	|	|	4.90
30.333	0.00	0.10	0.188	I	O	|	|	|	|	4.88
30.417	0.00	0.10	0.187	I	O	|	|	|	|	4.87
30.500	0.00	0.10	0.186	I	O	|	|	|	|	4.85
30.583	0.00	0.10	0.185	I	O	|	|	|	|	4.84
30.667	0.00	0.10	0.185	I	O	|	|	|	|	4.82
30.750	0.00	0.10	0.184	I	O	|	|	|	|	4.81
30.833	0.00	0.10	0.183	I	O	|	|	|	|	4.79
30.917	0.00	0.10	0.183	I	O	|	|	|	|	4.78
31.000	0.00	0.10	0.182	I	O	|	|	|	|	4.76
31.083	0.00	0.10	0.181	I	O	|	|	|	|	4.75
31.167	0.00	0.10	0.181	I	O	|	|	|	|	4.73
31.250	0.00	0.10	0.180	I	O	|	|	|	|	4.72
31.333	0.00	0.10	0.179	I	O	|	|	|	|	4.70
31.417	0.00	0.10	0.179	I	O	|	|	|	|	4.69
31.500	0.00	0.10	0.178	I	O	|	|	|	|	4.67
31.583	0.00	0.10	0.177	I	O	|	|	|	|	4.65
31.667	0.00	0.10	0.176	I	O	|	|	|	|	4.64
31.750	0.00	0.10	0.176	I	O	|	|	|	|	4.62
31.833	0.00	0.10	0.175	I	O	|	|	|	|	4.61
31.917	0.00	0.10	0.174	I	O	|	|	|	|	4.59
32.000	0.00	0.10	0.174	I	O	|	|	|	|	4.58
32.083	0.00	0.10	0.173	I	O	|	|	|	|	4.56
32.167	0.00	0.10	0.172	I	O	|	|	|	|	4.55
32.250	0.00	0.10	0.172	I	O	|	|	|	|	4.53
32.333	0.00	0.10	0.171	I	O	|	|	|	|	4.52
32.417	0.00	0.10	0.170	I	O	|	|	|	|	4.50
32.500	0.00	0.10	0.169	I	O	|	|	|	|	4.49
32.583	0.00	0.10	0.169	I	O	|	|	|	|	4.47
32.667	0.00	0.10	0.168	I	O	|	|	|	|	4.46
32.750	0.00	0.10	0.167	I	O	|	|	|	|	4.44
32.833	0.00	0.10	0.167	I	O	|	|	|	|	4.43
32.917	0.00	0.10	0.166	I	O	|	|	|	|	4.41
33.000	0.00	0.10	0.165	I	O	|	|	|	|	4.40

33.083	0.00	0.10	0.165	I	O	|	|	|	|	4.38
33.167	0.00	0.10	0.164	I	O	|	|	|	|	4.37
33.250	0.00	0.10	0.163	I	O	|	|	|	|	4.35
33.333	0.00	0.10	0.163	I	O	|	|	|	|	4.34
33.417	0.00	0.10	0.162	I	O	|	|	|	|	4.32
33.500	0.00	0.10	0.161	I	O	|	|	|	|	4.31
33.583	0.00	0.10	0.160	I	O	|	|	|	|	4.29
33.667	0.00	0.10	0.160	I	O	|	|	|	|	4.28
33.750	0.00	0.10	0.159	I	O	|	|	|	|	4.26
33.833	0.00	0.10	0.158	I	O	|	|	|	|	4.25
33.917	0.00	0.10	0.158	I	O	|	|	|	|	4.23
34.000	0.00	0.10	0.157	I	O	|	|	|	|	4.22
34.083	0.00	0.10	0.156	I	O	|	|	|	|	4.20
34.167	0.00	0.10	0.156	I	O	|	|	|	|	4.19
34.250	0.00	0.10	0.155	I	O	|	|	|	|	4.17
34.333	0.00	0.10	0.154	I	O	|	|	|	|	4.16
34.417	0.00	0.10	0.153	I	O	|	|	|	|	4.14
34.500	0.00	0.10	0.153	I	O	|	|	|	|	4.13
34.583	0.00	0.10	0.152	I	O	|	|	|	|	4.11
34.667	0.00	0.10	0.151	I	O	|	|	|	|	4.10
34.750	0.00	0.10	0.151	I	O	|	|	|	|	4.08
34.833	0.00	0.10	0.150	I	O	|	|	|	|	4.07
34.917	0.00	0.10	0.149	I	O	|	|	|	|	4.05
35.000	0.00	0.10	0.149	I	O	|	|	|	|	4.03
35.083	0.00	0.10	0.148	I	O	|	|	|	|	4.02
35.167	0.00	0.10	0.147	I	O	|	|	|	|	4.00
35.250	0.00	0.10	0.147	I	O	|	|	|	|	3.99
35.333	0.00	0.10	0.146	I	O	|	|	|	|	3.98
35.417	0.00	0.10	0.145	I	O	|	|	|	|	3.96
35.500	0.00	0.10	0.144	I	O	|	|	|	|	3.95
35.583	0.00	0.10	0.144	I	O	|	|	|	|	3.93
35.667	0.00	0.10	0.143	I	O	|	|	|	|	3.92
35.750	0.00	0.10	0.142	I	O	|	|	|	|	3.90
35.833	0.00	0.10	0.142	I	O	|	|	|	|	3.89
35.917	0.00	0.10	0.141	I	O	|	|	|	|	3.87
36.000	0.00	0.10	0.140	I	O	|	|	|	|	3.86
36.083	0.00	0.10	0.140	I	O	|	|	|	|	3.85
36.167	0.00	0.10	0.139	I	O	|	|	|	|	3.83
36.250	0.00	0.10	0.138	I	O	|	|	|	|	3.82
36.333	0.00	0.10	0.137	I	O	|	|	|	|	3.80
36.417	0.00	0.10	0.137	I	O	|	|	|	|	3.79
36.500	0.00	0.10	0.136	I	O	|	|	|	|	3.77
36.583	0.00	0.10	0.135	I	O	|	|	|	|	3.76
36.667	0.00	0.10	0.135	I	O	|	|	|	|	3.74
36.750	0.00	0.10	0.134	I	O	|	|	|	|	3.73
36.833	0.00	0.10	0.133	I	O	|	|	|	|	3.71
36.917	0.00	0.10	0.133	I	O	|	|	|	|	3.70
37.000	0.00	0.10	0.132	I	O	|	|	|	|	3.69
37.083	0.00	0.10	0.131	I	O	|	|	|	|	3.67
37.167	0.00	0.10	0.131	I	O	|	|	|	|	3.66
37.250	0.00	0.10	0.130	I	O	|	|	|	|	3.64
37.333	0.00	0.10	0.129	I	O	|	|	|	|	3.63
37.417	0.00	0.10	0.128	I	O	|	|	|	|	3.61

37.500	0.00	0.10	0.128	I	O	|	|	|	|	3.60
37.583	0.00	0.10	0.127	I	O	|	|	|	|	3.58
37.667	0.00	0.10	0.126	I	O	|	|	|	|	3.57
37.750	0.00	0.10	0.126	I	O	|	|	|	|	3.56
37.833	0.00	0.10	0.125	I	O	|	|	|	|	3.54
37.917	0.00	0.10	0.124	I	O	|	|	|	|	3.53
38.000	0.00	0.10	0.124	I	O	|	|	|	|	3.51
38.083	0.00	0.10	0.123	I	O	|	|	|	|	3.50
38.167	0.00	0.10	0.122	I	O	|	|	|	|	3.48
38.250	0.00	0.10	0.121	I	O	|	|	|	|	3.47
38.333	0.00	0.10	0.121	I	O	|	|	|	|	3.45
38.417	0.00	0.10	0.120	I	O	|	|	|	|	3.44
38.500	0.00	0.10	0.119	I	O	|	|	|	|	3.42
38.583	0.00	0.10	0.119	I	O	|	|	|	|	3.41
38.667	0.00	0.10	0.118	I	O	|	|	|	|	3.40
38.750	0.00	0.10	0.117	I	O	|	|	|	|	3.38
38.833	0.00	0.10	0.117	I	O	|	|	|	|	3.37
38.917	0.00	0.10	0.116	I	O	|	|	|	|	3.35
39.000	0.00	0.10	0.115	I	O	|	|	|	|	3.34
39.083	0.00	0.10	0.115	I	O	|	|	|	|	3.32
39.167	0.00	0.10	0.114	I	O	|	|	|	|	3.31
39.250	0.00	0.10	0.113	I	O	|	|	|	|	3.29
39.333	0.00	0.10	0.112	I	O	|	|	|	|	3.28
39.417	0.00	0.10	0.112	I	O	|	|	|	|	3.27
39.500	0.00	0.10	0.111	I	O	|	|	|	|	3.25
39.583	0.00	0.10	0.110	I	O	|	|	|	|	3.24
39.667	0.00	0.10	0.110	I	O	|	|	|	|	3.22
39.750	0.00	0.10	0.109	I	O	|	|	|	|	3.21
39.833	0.00	0.10	0.108	I	O	|	|	|	|	3.19
39.917	0.00	0.10	0.108	I	O	|	|	|	|	3.18
40.000	0.00	0.10	0.107	I	O	|	|	|	|	3.16
40.083	0.00	0.10	0.106	I	O	|	|	|	|	3.15
40.167	0.00	0.10	0.105	I	O	|	|	|	|	3.13
40.250	0.00	0.10	0.105	I	O	|	|	|	|	3.12
40.333	0.00	0.10	0.104	I	O	|	|	|	|	3.11
40.417	0.00	0.10	0.103	I	O	|	|	|	|	3.09
40.500	0.00	0.10	0.103	I	O	|	|	|	|	3.08
40.583	0.00	0.10	0.102	I	O	|	|	|	|	3.06
40.667	0.00	0.10	0.101	I	O	|	|	|	|	3.05
40.750	0.00	0.10	0.101	I	O	|	|	|	|	3.03
40.833	0.00	0.10	0.100	I	O	|	|	|	|	3.02
40.917	0.00	0.10	0.099	I	O	|	|	|	|	3.00
41.000	0.00	0.10	0.099	I	O	|	|	|	|	2.99
41.083	0.00	0.10	0.098	I	O	|	|	|	|	2.97
41.167	0.00	0.10	0.097	I	O	|	|	|	|	2.96
41.250	0.00	0.10	0.096	I	O	|	|	|	|	2.94
41.333	0.00	0.10	0.096	I	O	|	|	|	|	2.93
41.417	0.00	0.10	0.095	I	O	|	|	|	|	2.91
41.500	0.00	0.10	0.094	I	O	|	|	|	|	2.90
41.583	0.00	0.10	0.094	I	O	|	|	|	|	2.88
41.667	0.00	0.10	0.093	I	O	|	|	|	|	2.87
41.750	0.00	0.10	0.092	I	O	|	|	|	|	2.85
41.833	0.00	0.10	0.092	I	O	|	|	|	|	2.84

41.917	0.00	0.10	0.091	I	O	|	|	|	|	2.82
42.000	0.00	0.10	0.090	I	O	|	|	|	|	2.81
42.083	0.00	0.10	0.089	I	O	|	|	|	|	2.79
42.167	0.00	0.10	0.089	I	O	|	|	|	|	2.78
42.250	0.00	0.10	0.088	I	O	|	|	|	|	2.76
42.333	0.00	0.10	0.087	I	O	|	|	|	|	2.75
42.417	0.00	0.10	0.087	I	O	|	|	|	|	2.73
42.500	0.00	0.10	0.086	I	O	|	|	|	|	2.72
42.583	0.00	0.10	0.085	I	O	|	|	|	|	2.70
42.667	0.00	0.10	0.085	I	O	|	|	|	|	2.69
42.750	0.00	0.10	0.084	I	O	|	|	|	|	2.67
42.833	0.00	0.10	0.083	I	O	|	|	|	|	2.66
42.917	0.00	0.10	0.083	I	O	|	|	|	|	2.64
43.000	0.00	0.10	0.082	I	O	|	|	|	|	2.63
43.083	0.00	0.10	0.081	I	O	|	|	|	|	2.61
43.167	0.00	0.10	0.080	I	O	|	|	|	|	2.60
43.250	0.00	0.10	0.080	I	O	|	|	|	|	2.58
43.333	0.00	0.10	0.079	I	O	|	|	|	|	2.57
43.417	0.00	0.10	0.078	I	O	|	|	|	|	2.55
43.500	0.00	0.10	0.078	I	O	|	|	|	|	2.54
43.583	0.00	0.10	0.077	I	O	|	|	|	|	2.52
43.667	0.00	0.10	0.076	I	O	|	|	|	|	2.51
43.750	0.00	0.10	0.076	I	O	|	|	|	|	2.49
43.833	0.00	0.10	0.075	I	O	|	|	|	|	2.47
43.917	0.00	0.10	0.074	I	O	|	|	|	|	2.46
44.000	0.00	0.10	0.073	I	O	|	|	|	|	2.44
44.083	0.00	0.10	0.073	I	O	|	|	|	|	2.42
44.167	0.00	0.10	0.072	I	O	|	|	|	|	2.41
44.250	0.00	0.10	0.071	I	O	|	|	|	|	2.39
44.333	0.00	0.10	0.071	I	O	|	|	|	|	2.37
44.417	0.00	0.10	0.070	I	O	|	|	|	|	2.36
44.500	0.00	0.10	0.069	I	O	|	|	|	|	2.34
44.583	0.00	0.10	0.069	I	O	|	|	|	|	2.32
44.667	0.00	0.10	0.068	I	O	|	|	|	|	2.31
44.750	0.00	0.10	0.067	I	O	|	|	|	|	2.29
44.833	0.00	0.10	0.067	I	O	|	|	|	|	2.27
44.917	0.00	0.10	0.066	I	O	|	|	|	|	2.26
45.000	0.00	0.10	0.065	I	O	|	|	|	|	2.24
45.083	0.00	0.10	0.064	I	O	|	|	|	|	2.22
45.167	0.00	0.10	0.064	I	O	|	|	|	|	2.21
45.250	0.00	0.10	0.063	I	O	|	|	|	|	2.19
45.333	0.00	0.10	0.062	I	O	|	|	|	|	2.18
45.417	0.00	0.10	0.062	I	O	|	|	|	|	2.16
45.500	0.00	0.10	0.061	I	O	|	|	|	|	2.14
45.583	0.00	0.10	0.060	I	O	|	|	|	|	2.13
45.667	0.00	0.10	0.060	I	O	|	|	|	|	2.11
45.750	0.00	0.10	0.059	I	O	|	|	|	|	2.09
45.833	0.00	0.10	0.058	I	O	|	|	|	|	2.08
45.917	0.00	0.10	0.057	I	O	|	|	|	|	2.06
46.000	0.00	0.10	0.057	I	O	|	|	|	|	2.04
46.083	0.00	0.10	0.056	I	O	|	|	|	|	2.03
46.167	0.00	0.10	0.055	I	O	|	|	|	|	2.01
46.250	0.00	0.10	0.055	I	O	|	|	|	|	1.99

46.333	0.00	0.10	0.054	I	O	|	|	|	|	1.97
46.417	0.00	0.10	0.053	I	O	|	|	|	|	1.95
46.500	0.00	0.10	0.053	I	O	|	|	|	|	1.93
46.583	0.00	0.10	0.052	I	O	|	|	|	|	1.91
46.667	0.00	0.10	0.051	I	O	|	|	|	|	1.90
46.750	0.00	0.10	0.051	I	O	|	|	|	|	1.88
46.833	0.00	0.10	0.050	I	O	|	|	|	|	1.86
46.917	0.00	0.10	0.049	I	O	|	|	|	|	1.84
47.000	0.00	0.10	0.048	I	O	|	|	|	|	1.82
47.083	0.00	0.10	0.048	I	O	|	|	|	|	1.80
47.167	0.00	0.10	0.047	I	O	|	|	|	|	1.78
47.250	0.00	0.10	0.046	I	O	|	|	|	|	1.76
47.333	0.00	0.10	0.046	I	O	|	|	|	|	1.74
47.417	0.00	0.10	0.045	I	O	|	|	|	|	1.72
47.500	0.00	0.10	0.044	I	O	|	|	|	|	1.70
47.583	0.00	0.10	0.044	I	O	|	|	|	|	1.68
47.667	0.00	0.10	0.043	I	O	|	|	|	|	1.66
47.750	0.00	0.10	0.042	I	O	|	|	|	|	1.64
47.833	0.00	0.10	0.041	I	O	|	|	|	|	1.62
47.917	0.00	0.10	0.041	I	O	|	|	|	|	1.61
48.000	0.00	0.10	0.040	I	O	|	|	|	|	1.59
48.083	0.00	0.10	0.039	I	O	|	|	|	|	1.57
48.167	0.00	0.10	0.039	I	O	|	|	|	|	1.55
48.250	0.00	0.10	0.038	I	O	|	|	|	|	1.53
48.333	0.00	0.10	0.037	I	O	|	|	|	|	1.51
48.417	0.00	0.10	0.037	I	O	|	|	|	|	1.48
48.500	0.00	0.10	0.036	I	O	|	|	|	|	1.46
48.583	0.00	0.10	0.035	I	O	|	|	|	|	1.43
48.667	0.00	0.10	0.035	I	O	|	|	|	|	1.40
48.750	0.00	0.10	0.034	I	O	|	|	|	|	1.37
48.833	0.00	0.10	0.033	I	O	|	|	|	|	1.34
48.917	0.00	0.10	0.032	I	O	|	|	|	|	1.31
49.000	0.00	0.10	0.032	I	O	|	|	|	|	1.28
49.083	0.00	0.10	0.031	I	O	|	|	|	|	1.25
49.167	0.00	0.10	0.030	I	O	|	|	|	|	1.22
49.250	0.00	0.10	0.030	I	O	|	|	|	|	1.19
49.333	0.00	0.10	0.029	I	O	|	|	|	|	1.17
49.417	0.00	0.10	0.028	I	O	|	|	|	|	1.14
49.500	0.00	0.10	0.028	I	O	|	|	|	|	1.11
49.583	0.00	0.10	0.027	I	O	|	|	|	|	1.08
49.667	0.00	0.10	0.026	I	O	|	|	|	|	1.05
49.750	0.00	0.10	0.025	I	O	|	|	|	|	1.02
49.833	0.00	0.10	0.025	I	O	|	|	|	|	0.99
49.917	0.00	0.10	0.024	I	O	|	|	|	|	0.96
50.000	0.00	0.10	0.023	I	O	|	|	|	|	0.93
50.083	0.00	0.10	0.023	I	O	|	|	|	|	0.90
50.167	0.00	0.10	0.022	I	O	|	|	|	|	0.88
50.250	0.00	0.10	0.021	I	O	|	|	|	|	0.85
50.333	0.00	0.10	0.021	I	O	|	|	|	|	0.82
50.417	0.00	0.10	0.020	I	O	|	|	|	|	0.79
50.500	0.00	0.10	0.019	I	O	|	|	|	|	0.76
50.583	0.00	0.10	0.019	I	O	|	|	|	|	0.73
50.667	0.00	0.10	0.018	I	O	|	|	|	|	0.70

50.750	0.00	0.10	0.017	I O	|	|	|	0.67
50.833	0.00	0.10	0.016	I O	|	|	|	0.64
50.917	0.00	0.10	0.016	I O	|	|	|	0.61
51.000	0.00	0.10	0.015	I O	|	|	|	0.59
51.083	0.00	0.10	0.014	I O	|	|	|	0.56
51.167	0.00	0.10	0.014	I O	|	|	|	0.53
51.250	0.00	0.10	0.013	I O	|	|	|	0.50
51.333	0.00	0.10	0.012	I O	|	|	|	0.47
51.417	0.00	0.09	0.012	I O	|	|	|	0.45
51.500	0.00	0.09	0.011	I O	|	|	|	0.42
51.583	0.00	0.08	0.010	I O	|	|	|	0.40
51.667	0.00	0.08	0.010	I O	|	|	|	0.38
51.750	0.00	0.07	0.009	I O	|	|	|	0.36
51.833	0.00	0.07	0.009	I O	|	|	|	0.34
51.917	0.00	0.07	0.008	I O	|	|	|	0.33
52.000	0.00	0.06	0.008	I O	|	|	|	0.31
52.083	0.00	0.06	0.008	I O	|	|	|	0.29
52.167	0.00	0.06	0.007	I O	|	|	|	0.28
52.250	0.00	0.05	0.007	I O	|	|	|	0.26
52.333	0.00	0.05	0.006	I O	|	|	|	0.25
52.417	0.00	0.05	0.006	I O	|	|	|	0.24
52.500	0.00	0.05	0.006	IO	|	|	|	0.22
52.583	0.00	0.04	0.006	IO	|	|	|	0.21
52.667	0.00	0.04	0.005	IO	|	|	|	0.20
52.750	0.00	0.04	0.005	IO	|	|	|	0.19
52.833	0.00	0.04	0.005	IO	|	|	|	0.18
52.917	0.00	0.03	0.004	IO	|	|	|	0.17
53.000	0.00	0.03	0.004	IO	|	|	|	0.16
53.083	0.00	0.03	0.004	IO	|	|	|	0.15
53.167	0.00	0.03	0.004	IO	|	|	|	0.15
53.250	0.00	0.03	0.004	IO	|	|	|	0.14
53.333	0.00	0.03	0.003	IO	|	|	|	0.13
53.417	0.00	0.03	0.003	IO	|	|	|	0.12
53.500	0.00	0.02	0.003	IO	|	|	|	0.12
53.583	0.00	0.02	0.003	O	|	|	|	0.11
53.667	0.00	0.02	0.003	O	|	|	|	0.11
53.750	0.00	0.02	0.003	O	|	|	|	0.10
53.833	0.00	0.02	0.002	O	|	|	|	0.09
53.917	0.00	0.02	0.002	O	|	|	|	0.09
54.000	0.00	0.02	0.002	O	|	|	|	0.09
54.083	0.00	0.02	0.002	O	|	|	|	0.08
54.167	0.00	0.02	0.002	O	|	|	|	0.08
54.250	0.00	0.01	0.002	O	|	|	|	0.07
54.333	0.00	0.01	0.002	O	|	|	|	0.07
54.417	0.00	0.01	0.002	O	|	|	|	0.07
54.500	0.00	0.01	0.002	O	|	|	|	0.06
54.583	0.00	0.01	0.002	O	|	|	|	0.06
54.667	0.00	0.01	0.001	O	|	|	|	0.06
54.750	0.00	0.01	0.001	O	|	|	|	0.05
54.833	0.00	0.01	0.001	O	|	|	|	0.05
54.917	0.00	0.01	0.001	O	|	|	|	0.05
55.000	0.00	0.01	0.001	O	|	|	|	0.04
55.083	0.00	0.01	0.001	O	|	|	|	0.04

55.167	0.00	0.01	0.001	O	|	|	|	|	0.04
55.250	0.00	0.01	0.001	O	|	|	|	|	0.04
55.333	0.00	0.01	0.001	O	|	|	|	|	0.04
55.417	0.00	0.01	0.001	O	|	|	|	|	0.03
55.500	0.00	0.01	0.001	O	|	|	|	|	0.03
55.583	0.00	0.01	0.001	O	|	|	|	|	0.03
55.667	0.00	0.01	0.001	O	|	|	|	|	0.03
55.750	0.00	0.01	0.001	O	|	|	|	|	0.03
55.833	0.00	0.01	0.001	O	|	|	|	|	0.03
55.917	0.00	0.01	0.001	O	|	|	|	|	0.02
56.000	0.00	0.00	0.001	O	|	|	|	|	0.02
56.083	0.00	0.00	0.001	O	|	|	|	|	0.02
56.167	0.00	0.00	0.001	O	|	|	|	|	0.02
56.250	0.00	0.00	0.001	O	|	|	|	|	0.02
56.333	0.00	0.00	0.000	O	|	|	|	|	0.02
56.417	0.00	0.00	0.000	O	|	|	|	|	0.02
56.500	0.00	0.00	0.000	O	|	|	|	|	0.02
56.583	0.00	0.00	0.000	O	|	|	|	|	0.02
56.667	0.00	0.00	0.000	O	|	|	|	|	0.02
56.750	0.00	0.00	0.000	O	|	|	|	|	0.01
56.833	0.00	0.00	0.000	O	|	|	|	|	0.01
56.917	0.00	0.00	0.000	O	|	|	|	|	0.01
57.000	0.00	0.00	0.000	O	|	|	|	|	0.01
57.083	0.00	0.00	0.000	O	|	|	|	|	0.01
57.167	0.00	0.00	0.000	O	|	|	|	|	0.01
57.250	0.00	0.00	0.000	O	|	|	|	|	0.01
57.333	0.00	0.00	0.000	O	|	|	|	|	0.01
57.417	0.00	0.00	0.000	O	|	|	|	|	0.01
57.500	0.00	0.00	0.000	O	|	|	|	|	0.01
57.583	0.00	0.00	0.000	O	|	|	|	|	0.01
57.667	0.00	0.00	0.000	O	|	|	|	|	0.01
57.750	0.00	0.00	0.000	O	|	|	|	|	0.01
57.833	0.00	0.00	0.000	O	|	|	|	|	0.01
57.917	0.00	0.00	0.000	O	|	|	|	|	0.01
58.000	0.00	0.00	0.000	O	|	|	|	|	0.01
58.083	0.00	0.00	0.000	O	|	|	|	|	0.01
58.167	0.00	0.00	0.000	O	|	|	|	|	0.01
58.250	0.00	0.00	0.000	O	|	|	|	|	0.01
58.333	0.00	0.00	0.000	O	|	|	|	|	0.01
58.417	0.00	0.00	0.000	O	|	|	|	|	0.00
58.500	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 702
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.101 (CFS)
Total volume = 0.422 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

AREA C1

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 07/21/25

ROUTING: BASIN C1; UNIT HYDROGRAPH C1

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARC124100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 289
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.385 (CFS)
Total volume = 0.223 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 101.000 to Point/Station 102.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 289
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.007	0.056	0.007	0.007
1.000	0.014	0.056	0.014	0.014
1.500	0.020	0.056	0.020	0.020
2.000	0.030	0.056	0.030	0.030
2.500	0.042	0.056	0.042	0.042
3.000	0.055	0.056	0.055	0.055
3.500	0.068	0.056	0.068	0.068
4.000	0.081	0.056	0.081	0.081
4.500	0.095	0.056	0.095	0.095
5.000	0.107	0.056	0.107	0.107
5.500	0.119	0.056	0.119	0.119
6.000	0.130	0.056	0.130	0.130
6.500	0.137	0.056	0.137	0.137
7.000	0.144	0.056	0.144	0.144
7.500	0.151	0.056	0.151	0.151
7.580	0.152	0.056	0.152	0.152

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.1	0.19	0.29	0.39	Depth (Ft.)
0.083	0.01	0.00	0.000	OI	|	|	|	|	0.00
0.167	0.02	0.00	0.000	OI	|	|	|	|	0.01
0.250	0.02	0.00	0.000	OI	|	|	|	|	0.02
0.333	0.03	0.00	0.000	O I	|	|	|	|	0.03
0.417	0.03	0.01	0.001	O I	|	|	|	|	0.05
0.500	0.03	0.01	0.001	O I	|	|	|	|	0.06
0.583	0.03	0.01	0.001	O I	|	|	|	|	0.07
0.667	0.03	0.01	0.001	O I	|	|	|	|	0.08
0.750	0.03	0.01	0.001	O I	|	|	|	|	0.09
0.833	0.04	0.01	0.001	O I	|	|	|	|	0.11
0.917	0.04	0.01	0.002	|O I	|	|	|	|	0.12
1.000	0.04	0.01	0.002	|O I	|	|	|	|	0.13
1.083	0.04	0.02	0.002	|OI	|	|	|	|	0.15
1.167	0.03	0.02	0.002	|OI	|	|	|	|	0.15
1.250	0.03	0.02	0.002	|OI	|	|	|	|	0.16
1.333	0.03	0.02	0.002	|OI	|	|	|	|	0.17
1.417	0.03	0.02	0.002	|OI	|	|	|	|	0.17
1.500	0.03	0.02	0.003	|OI	|	|	|	|	0.18
1.583	0.03	0.02	0.003	|OI	|	|	|	|	0.19
1.667	0.03	0.02	0.003	|OI	|	|	|	|	0.19
1.750	0.03	0.02	0.003	|OI	|	|	|	|	0.20
1.833	0.04	0.02	0.003	|O I	|	|	|	|	0.20
1.917	0.04	0.02	0.003	|O I	|	|	|	|	0.21
2.000	0.04	0.02	0.003	| OI	|	|	|	|	0.22
2.083	0.04	0.03	0.003	| OI	|	|	|	|	0.23

2.167	0.04	0.03	0.003	OI				0.24
2.250	0.04	0.03	0.003	OI				0.25
2.333	0.04	0.03	0.004	OI				0.25
2.417	0.04	0.03	0.004	OI				0.26
2.500	0.04	0.03	0.004	OI				0.27
2.583	0.05	0.03	0.004	O I				0.27
2.667	0.05	0.03	0.004	O I				0.28
2.750	0.05	0.03	0.004	O I				0.30
2.833	0.05	0.03	0.004	O I				0.31
2.917	0.05	0.04	0.004	O I				0.31
3.000	0.05	0.04	0.005	OI				0.32
3.083	0.05	0.04	0.005	OI				0.33
3.167	0.05	0.04	0.005	OI				0.34
3.250	0.05	0.04	0.005	OI				0.35
3.333	0.05	0.04	0.005	OI				0.35
3.417	0.05	0.04	0.005	OI				0.36
3.500	0.05	0.04	0.005	OI				0.37
3.583	0.05	0.04	0.005	OI				0.37
3.667	0.05	0.04	0.005	OI				0.38
3.750	0.05	0.04	0.005	OI				0.38
3.833	0.06	0.04	0.005	O I				0.39
3.917	0.06	0.04	0.006	O I				0.40
4.000	0.06	0.05	0.006	O I				0.41
4.083	0.06	0.05	0.006	O I				0.42
4.167	0.06	0.05	0.006	O I				0.43
4.250	0.06	0.05	0.006	OI				0.43
4.333	0.07	0.05	0.006	OI				0.44
4.417	0.08	0.05	0.006	O I				0.46
4.500	0.08	0.05	0.007	O I				0.47
4.583	0.08	0.05	0.007	O I				0.48
4.667	0.08	0.05	0.007	O I				0.49
4.750	0.08	0.06	0.007	O I				0.50
4.833	0.08	0.06	0.007	O I				0.51
4.917	0.09	0.06	0.007	O I				0.52
5.000	0.09	0.06	0.008	O I				0.54
5.083	0.07	0.06	0.008	OI				0.55
5.167	0.06	0.06	0.008	OI				0.55
5.250	0.06	0.06	0.008	OI				0.56
5.333	0.07	0.06	0.008	OI				0.56
5.417	0.08	0.06	0.008	O I				0.57
5.500	0.08	0.06	0.008	O I				0.58
5.583	0.08	0.06	0.008	O I				0.59
5.667	0.09	0.06	0.009	O I				0.61
5.750	0.09	0.06	0.009	O I				0.62
5.833	0.09	0.06	0.009	O I				0.64
5.917	0.09	0.06	0.009	O I				0.65
6.000	0.09	0.06	0.009	O I				0.67
6.083	0.09	0.06	0.010	O I				0.68
6.167	0.10	0.06	0.010	O I				0.70
6.250	0.10	0.06	0.010	O I				0.72
6.333	0.10	0.06	0.010	O I				0.74
6.417	0.10	0.06	0.011	O I				0.76
6.500	0.10	0.06	0.011	O I				0.78

6.583	0.10	0.06	0.011	|	O	I	|	|	0.80
6.667	0.11	0.06	0.012	|	O	I	|	|	0.83
6.750	0.11	0.06	0.012	|	O	I	|	|	0.85
6.833	0.11	0.06	0.012	|	O	I	|	|	0.88
6.917	0.11	0.06	0.013	|	O	I	|	|	0.90
7.000	0.11	0.06	0.013	|	O	I	|	|	0.93
7.083	0.11	0.06	0.013	|	O	I	|	|	0.95
7.167	0.11	0.06	0.014	|	O	I	|	|	0.98
7.250	0.11	0.06	0.014	|	O	I	|	|	1.01
7.333	0.11	0.06	0.014	|	O	|I	|	|	1.04
7.417	0.12	0.06	0.015	|	O	|I	|	|	1.07
7.500	0.12	0.06	0.015	|	O	|I	|	|	1.11
7.583	0.13	0.06	0.016	|	O	| I	|	|	1.14
7.667	0.13	0.06	0.016	|	O	| I	|	|	1.19
7.750	0.13	0.06	0.017	|	O	| I	|	|	1.23
7.833	0.14	0.06	0.017	|	O	| I	|	|	1.27
7.917	0.14	0.06	0.018	|	O	| I	|	|	1.32
8.000	0.14	0.06	0.018	|	O	| I	|	|	1.37
8.083	0.15	0.06	0.019	|	O	| I	|	|	1.42
8.167	0.16	0.06	0.020	|	O	| I	|	|	1.48
8.250	0.16	0.06	0.020	|	O	| I	|	|	1.52
8.333	0.16	0.06	0.021	|	O	| I	|	|	1.56
8.417	0.16	0.06	0.022	|	O	| I	|	|	1.59
8.500	0.16	0.06	0.023	|	O	| I	|	|	1.63
8.583	0.17	0.06	0.023	|	O	| I	|	|	1.67
8.667	0.17	0.06	0.024	|	O	| I |	|	|	1.71
8.750	0.17	0.06	0.025	|	O	| I |	|	|	1.75
8.833	0.18	0.06	0.026	|	O	| I |	|	|	1.79
8.917	0.18	0.06	0.027	|	O	| I|	|	|	1.83
9.000	0.18	0.06	0.027	|	O	| I|	|	|	1.87
9.083	0.20	0.06	0.028	|	O	| I	|	|	1.92
9.167	0.20	0.06	0.029	|	O	| I	|	|	1.97
9.250	0.20	0.06	0.030	|	O	| I	|	|	2.02
9.333	0.21	0.06	0.031	|	O	| |I	|	|	2.06
9.417	0.21	0.06	0.033	|	O	| |I	|	|	2.11
9.500	0.21	0.06	0.034	|	O	| |I	|	|	2.15
9.583	0.22	0.06	0.035	|	O	| | I	|	|	2.20
9.667	0.23	0.06	0.036	|	O	| | I	|	|	2.25
9.750	0.23	0.06	0.037	|	O	| | I	|	|	2.29
9.833	0.23	0.06	0.038	|	O	| | I	|	|	2.34
9.917	0.24	0.06	0.039	|	O	| | I	|	|	2.40
10.000	0.24	0.06	0.041	|	O	| | I	|	|	2.45
10.083	0.19	0.06	0.042	|	O	| I|	|	|	2.49
10.167	0.16	0.06	0.043	|	O	| I	|	|	2.52
10.250	0.16	0.06	0.043	|	O	| I	|	|	2.55
10.333	0.16	0.06	0.044	|	O	| I	|	|	2.58
10.417	0.16	0.06	0.045	|	O	| I	|	|	2.61
10.500	0.16	0.06	0.046	|	O	| I	|	|	2.64
10.583	0.20	0.06	0.046	|	O	| I	|	|	2.67
10.667	0.21	0.06	0.047	|	O	| |I	|	|	2.71
10.750	0.21	0.06	0.048	|	O	| |I	|	|	2.75
10.833	0.21	0.06	0.050	|	O	| |I	|	|	2.79
10.917	0.21	0.06	0.051	|	O	| |I	|	|	2.83

11.000	0.21	0.06	0.052	|	O	|	|I	|	|	2.88
11.083	0.21	0.06	0.053	|	O	|	|I	|	|	2.92
11.167	0.20	0.06	0.054	|	O	|	I	|	|	2.96
11.250	0.20	0.06	0.055	|	O	|	I	|	|	3.00
11.333	0.20	0.06	0.056	|	O	|	I	|	|	3.03
11.417	0.20	0.06	0.057	|	O	|	I	|	|	3.07
11.500	0.20	0.06	0.058	|	O	|	I	|	|	3.11
11.583	0.19	0.06	0.059	|	O	|	I|	|	|	3.15
11.667	0.18	0.06	0.060	|	O	|	I|	|	|	3.18
11.750	0.18	0.06	0.061	|	O	|	I|	|	|	3.22
11.833	0.19	0.06	0.062	|	O	|	I|	|	|	3.25
11.917	0.19	0.06	0.062	|	O	|	I	|	|	3.29
12.000	0.19	0.06	0.063	|	O	|	I	|	|	3.32
12.083	0.24	0.06	0.065	|	O	|	| I	|	|	3.37
12.167	0.27	0.06	0.066	|	O	|	| I	|	|	3.42
12.250	0.27	0.06	0.067	|	O	|	| I	|	|	3.48
12.333	0.28	0.06	0.069	|	O	|	| I	|	|	3.53
12.417	0.28	0.06	0.070	|	O	|	| I|	|	|	3.59
12.500	0.28	0.06	0.072	|	O	|	| I|	|	|	3.65
12.583	0.29	0.06	0.074	|	O	|	| I	|	|	3.71
12.667	0.30	0.06	0.075	|	O	|	| |I	|	|	3.78
12.750	0.30	0.06	0.077	|	O	|	| |I	|	|	3.84
12.833	0.31	0.06	0.079	|	O	|	| |I	|	|	3.91
12.917	0.32	0.06	0.080	|	O	|	| | I	|	|	3.98
13.000	0.32	0.06	0.082	|	O	|	| | I	|	|	4.04
13.083	0.36	0.06	0.084	|	O	|	| | I	|	|	4.11
13.167	0.38	0.06	0.086	|	O	|	| | I|	|	|	4.19
13.250	0.38	0.06	0.089	|	O	|	| | I|	|	|	4.27
13.333	0.38	0.06	0.091	|	O	|	| | I|	|	|	4.35
13.417	0.39	0.06	0.093	|	O	|	| | I|	|	|	4.43
13.500	0.39	0.06	0.095	|	O	|	| | I	|	|	4.52
13.583	0.29	0.06	0.097	|	O	|	| I	|	|	4.60
13.667	0.25	0.06	0.099	|	O	|	| I	|	|	4.66
13.750	0.25	0.06	0.100	|	O	|	| I	|	|	4.71
13.833	0.25	0.06	0.101	|	O	|	| I	|	|	4.77
13.917	0.25	0.06	0.103	|	O	|	| I	|	|	4.82
14.000	0.25	0.06	0.104	|	O	|	| I	|	|	4.88
14.083	0.28	0.06	0.106	|	O	|	| I|	|	|	4.94
14.167	0.30	0.06	0.107	|	O	|	| I	|	|	5.00
14.250	0.30	0.06	0.109	|	O	|	| I	|	|	5.07
14.333	0.29	0.06	0.110	|	O	|	| I|	|	|	5.14
14.417	0.28	0.06	0.112	|	O	|	| I|	|	|	5.21
14.500	0.28	0.06	0.114	|	O	|	| I|	|	|	5.27
14.583	0.28	0.06	0.115	|	O	|	| I|	|	|	5.34
14.667	0.28	0.06	0.117	|	O	|	| I|	|	|	5.40
14.750	0.28	0.06	0.118	|	O	|	| I|	|	|	5.47
14.833	0.28	0.06	0.120	|	O	|	| I	|	|	5.54
14.917	0.27	0.06	0.121	|	O	|	| I	|	|	5.60
15.000	0.27	0.06	0.123	|	O	|	| I	|	|	5.67
15.083	0.26	0.06	0.124	|	O	|	| I	|	|	5.74
15.167	0.26	0.06	0.126	|	O	|	| I	|	|	5.80
15.250	0.26	0.06	0.127	|	O	|	| I	|	|	5.87
15.333	0.25	0.06	0.128	|	O	|	| I	|	|	5.93

15.417	0.25	0.06	0.130	| O |		| I |			5.99
15.500	0.25	0.06	0.131	| O |		| I |			6.08
15.583	0.22	0.06	0.132	| O |		| I			6.16
15.667	0.20	0.06	0.133	| O |		I			6.24
15.750	0.20	0.06	0.134	| O |		I			6.31
15.833	0.20	0.06	0.135	| O |		I			6.38
15.917	0.20	0.06	0.136	| O |		I			6.46
16.000	0.20	0.06	0.137	| O |		I			6.53
16.083	0.10	0.06	0.138	| O	I				6.58
16.167	0.04	0.06	0.138	| IO |					6.58
16.250	0.04	0.06	0.138	| IO |					6.58
16.333	0.04	0.06	0.138	| IO |					6.57
16.417	0.04	0.06	0.138	| IO |					6.56
16.500	0.04	0.06	0.138	| IO |					6.56
16.583	0.04	0.06	0.138	| I O |					6.55
16.667	0.03	0.06	0.138	| I O |					6.54
16.750	0.03	0.06	0.137	| I O |					6.53
16.833	0.03	0.06	0.137	| I O |					6.52
16.917	0.03	0.06	0.137	| I O |					6.50
17.000	0.03	0.06	0.137	| I O |					6.49
17.083	0.05	0.06	0.137	| IO |					6.48
17.167	0.05	0.06	0.137	| O |					6.48
17.250	0.05	0.06	0.137	| O |					6.48
17.333	0.05	0.06	0.137	| O |					6.48
17.417	0.05	0.06	0.137	| O |					6.48
17.500	0.05	0.06	0.137	| O |					6.48
17.583	0.05	0.06	0.137	| O |					6.47
17.667	0.05	0.06	0.137	| O |					6.47
17.750	0.05	0.06	0.137	| O |					6.47
17.833	0.05	0.06	0.137	| IO |					6.47
17.917	0.04	0.06	0.136	| IO |					6.46
18.000	0.04	0.06	0.136	| IO |					6.46
18.083	0.04	0.06	0.136	| IO |					6.45
18.167	0.04	0.06	0.136	| IO |					6.44
18.250	0.04	0.06	0.136	| IO |					6.44
18.333	0.04	0.06	0.136	| IO |					6.43
18.417	0.04	0.06	0.136	| IO |					6.43
18.500	0.04	0.06	0.136	| IO |					6.42
18.583	0.04	0.06	0.136	| I O |					6.41
18.667	0.03	0.06	0.136	| I O |					6.40
18.750	0.03	0.06	0.135	| I O |					6.39
18.833	0.03	0.06	0.135	| I O |					6.37
18.917	0.02	0.06	0.135	|I O |					6.36
19.000	0.02	0.06	0.135	|I O |					6.34
19.083	0.03	0.06	0.135	| I O |					6.33
19.167	0.03	0.06	0.134	| I O |					6.31
19.250	0.03	0.06	0.134	| I O |					6.30
19.333	0.04	0.06	0.134	| IO |					6.29
19.417	0.04	0.06	0.134	| IO |					6.28
19.500	0.04	0.06	0.134	| IO |					6.28
19.583	0.04	0.06	0.134	| I O |					6.27
19.667	0.03	0.06	0.134	| I O |					6.26
19.750	0.03	0.06	0.133	| I O |					6.25

19.833	0.03	0.06	0.133	| I O	|	|	|	6.23
19.917	0.02	0.06	0.133	|I O	|	|	|	6.22
20.000	0.02	0.06	0.133	|I O	|	|	|	6.20
20.083	0.03	0.06	0.133	| I O	|	|	|	6.19
20.167	0.03	0.06	0.132	| I O	|	|	|	6.17
20.250	0.03	0.06	0.132	| I O	|	|	|	6.16
20.333	0.03	0.06	0.132	| I O	|	|	|	6.15
20.417	0.03	0.06	0.132	| I O	|	|	|	6.14
20.500	0.03	0.06	0.132	| I O	|	|	|	6.13
20.583	0.03	0.06	0.132	| I O	|	|	|	6.11
20.667	0.03	0.06	0.131	| I O	|	|	|	6.10
20.750	0.03	0.06	0.131	| I O	|	|	|	6.09
20.833	0.03	0.06	0.131	| I O	|	|	|	6.08
20.917	0.02	0.06	0.131	|I O	|	|	|	6.06
21.000	0.02	0.06	0.131	|I O	|	|	|	6.04
21.083	0.03	0.06	0.130	| I O	|	|	|	6.03
21.167	0.03	0.06	0.130	| I O	|	|	|	6.02
21.250	0.03	0.06	0.130	| I O	|	|	|	6.01
21.333	0.03	0.06	0.130	| I O	|	|	|	5.99
21.417	0.02	0.06	0.130	|I O	|	|	|	5.98
21.500	0.02	0.06	0.129	|I O	|	|	|	5.97
21.583	0.03	0.06	0.129	| I O	|	|	|	5.96
21.667	0.03	0.06	0.129	| I O	|	|	|	5.96
21.750	0.03	0.06	0.129	| I O	|	|	|	5.95
21.833	0.03	0.06	0.129	| I O	|	|	|	5.94
21.917	0.02	0.06	0.128	|I O	|	|	|	5.93
22.000	0.02	0.06	0.128	|I O	|	|	|	5.92
22.083	0.03	0.06	0.128	| I O	|	|	|	5.91
22.167	0.03	0.06	0.128	| I O	|	|	|	5.90
22.250	0.03	0.06	0.128	| I O	|	|	|	5.89
22.333	0.03	0.06	0.127	| I O	|	|	|	5.89
22.417	0.02	0.06	0.127	|I O	|	|	|	5.88
22.500	0.02	0.06	0.127	|I O	|	|	|	5.86
22.583	0.02	0.06	0.127	|I O	|	|	|	5.85
22.667	0.02	0.06	0.127	|I O	|	|	|	5.84
22.750	0.02	0.06	0.126	|I O	|	|	|	5.83
22.833	0.02	0.06	0.126	|I O	|	|	|	5.82
22.917	0.02	0.06	0.126	|I O	|	|	|	5.81
23.000	0.02	0.06	0.126	|I O	|	|	|	5.80
23.083	0.02	0.06	0.125	|I O	|	|	|	5.79
23.167	0.02	0.06	0.125	|I O	|	|	|	5.78
23.250	0.02	0.06	0.125	|I O	|	|	|	5.77
23.333	0.02	0.06	0.125	|I O	|	|	|	5.76
23.417	0.02	0.06	0.124	|I O	|	|	|	5.75
23.500	0.02	0.06	0.124	|I O	|	|	|	5.73
23.583	0.02	0.06	0.124	|I O	|	|	|	5.72
23.667	0.02	0.06	0.124	|I O	|	|	|	5.71
23.750	0.02	0.06	0.123	|I O	|	|	|	5.70
23.833	0.02	0.06	0.123	|I O	|	|	|	5.69
23.917	0.02	0.06	0.123	|I O	|	|	|	5.68
24.000	0.02	0.06	0.123	|I O	|	|	|	5.67
24.083	0.01	0.06	0.122	I O	|	|	|	5.66
24.167	0.00	0.06	0.122	I O	|	|	|	5.64

24.250	0.00	0.06	0.122	I	O	|	|	|	|	5.62
24.333	0.00	0.06	0.121	I	O	|	|	|	|	5.61
24.417	0.00	0.06	0.121	I	O	|	|	|	|	5.59
24.500	0.00	0.06	0.121	I	O	|	|	|	|	5.57
24.583	0.00	0.06	0.120	I	O	|	|	|	|	5.55
24.667	0.00	0.06	0.120	I	O	|	|	|	|	5.54
24.750	0.00	0.06	0.119	I	O	|	|	|	|	5.52
24.833	0.00	0.06	0.119	I	O	|	|	|	|	5.50
24.917	0.00	0.06	0.119	I	O	|	|	|	|	5.48
25.000	0.00	0.06	0.118	I	O	|	|	|	|	5.47
25.083	0.00	0.06	0.118	I	O	|	|	|	|	5.45
25.167	0.00	0.06	0.117	I	O	|	|	|	|	5.44
25.250	0.00	0.06	0.117	I	O	|	|	|	|	5.42
25.333	0.00	0.06	0.117	I	O	|	|	|	|	5.40
25.417	0.00	0.06	0.116	I	O	|	|	|	|	5.39
25.500	0.00	0.06	0.116	I	O	|	|	|	|	5.37
25.583	0.00	0.06	0.116	I	O	|	|	|	|	5.36
25.667	0.00	0.06	0.115	I	O	|	|	|	|	5.34
25.750	0.00	0.06	0.115	I	O	|	|	|	|	5.32
25.833	0.00	0.06	0.114	I	O	|	|	|	|	5.31
25.917	0.00	0.06	0.114	I	O	|	|	|	|	5.29
26.000	0.00	0.06	0.114	I	O	|	|	|	|	5.28
26.083	0.00	0.06	0.113	I	O	|	|	|	|	5.26
26.167	0.00	0.06	0.113	I	O	|	|	|	|	5.24
26.250	0.00	0.06	0.112	I	O	|	|	|	|	5.23
26.333	0.00	0.06	0.112	I	O	|	|	|	|	5.21
26.417	0.00	0.06	0.112	I	O	|	|	|	|	5.19
26.500	0.00	0.06	0.111	I	O	|	|	|	|	5.18
26.583	0.00	0.06	0.111	I	O	|	|	|	|	5.16
26.667	0.00	0.06	0.111	I	O	|	|	|	|	5.15
26.750	0.00	0.06	0.110	I	O	|	|	|	|	5.13
26.833	0.00	0.06	0.110	I	O	|	|	|	|	5.11
26.917	0.00	0.06	0.109	I	O	|	|	|	|	5.10
27.000	0.00	0.06	0.109	I	O	|	|	|	|	5.08
27.083	0.00	0.06	0.109	I	O	|	|	|	|	5.07
27.167	0.00	0.06	0.108	I	O	|	|	|	|	5.05
27.250	0.00	0.06	0.108	I	O	|	|	|	|	5.03
27.333	0.00	0.06	0.107	I	O	|	|	|	|	5.02
27.417	0.00	0.06	0.107	I	O	|	|	|	|	5.00
27.500	0.00	0.06	0.107	I	O	|	|	|	|	4.99
27.583	0.00	0.06	0.106	I	O	|	|	|	|	4.97
27.667	0.00	0.06	0.106	I	O	|	|	|	|	4.95
27.750	0.00	0.06	0.106	I	O	|	|	|	|	4.94
27.833	0.00	0.06	0.105	I	O	|	|	|	|	4.92
27.917	0.00	0.06	0.105	I	O	|	|	|	|	4.91
28.000	0.00	0.06	0.104	I	O	|	|	|	|	4.89
28.083	0.00	0.06	0.104	I	O	|	|	|	|	4.87
28.167	0.00	0.06	0.104	I	O	|	|	|	|	4.86
28.250	0.00	0.06	0.103	I	O	|	|	|	|	4.84
28.333	0.00	0.06	0.103	I	O	|	|	|	|	4.83
28.417	0.00	0.06	0.102	I	O	|	|	|	|	4.81
28.500	0.00	0.06	0.102	I	O	|	|	|	|	4.79
28.583	0.00	0.06	0.102	I	O	|	|	|	|	4.78

28.667	0.00	0.06	0.101	I	O	|	|	|	|	4.76
28.750	0.00	0.06	0.101	I	O	|	|	|	|	4.74
28.833	0.00	0.06	0.100	I	O	|	|	|	|	4.73
28.917	0.00	0.06	0.100	I	O	|	|	|	|	4.71
29.000	0.00	0.06	0.100	I	O	|	|	|	|	4.70
29.083	0.00	0.06	0.099	I	O	|	|	|	|	4.68
29.167	0.00	0.06	0.099	I	O	|	|	|	|	4.66
29.250	0.00	0.06	0.099	I	O	|	|	|	|	4.65
29.333	0.00	0.06	0.098	I	O	|	|	|	|	4.63
29.417	0.00	0.06	0.098	I	O	|	|	|	|	4.62
29.500	0.00	0.06	0.097	I	O	|	|	|	|	4.60
29.583	0.00	0.06	0.097	I	O	|	|	|	|	4.58
29.667	0.00	0.06	0.097	I	O	|	|	|	|	4.57
29.750	0.00	0.06	0.096	I	O	|	|	|	|	4.55
29.833	0.00	0.06	0.096	I	O	|	|	|	|	4.54
29.917	0.00	0.06	0.095	I	O	|	|	|	|	4.52
30.000	0.00	0.06	0.095	I	O	|	|	|	|	4.50
30.083	0.00	0.06	0.095	I	O	|	|	|	|	4.49
30.167	0.00	0.06	0.094	I	O	|	|	|	|	4.48
30.250	0.00	0.06	0.094	I	O	|	|	|	|	4.46
30.333	0.00	0.06	0.094	I	O	|	|	|	|	4.45
30.417	0.00	0.06	0.093	I	O	|	|	|	|	4.43
30.500	0.00	0.06	0.093	I	O	|	|	|	|	4.42
30.583	0.00	0.06	0.092	I	O	|	|	|	|	4.41
30.667	0.00	0.06	0.092	I	O	|	|	|	|	4.39
30.750	0.00	0.06	0.092	I	O	|	|	|	|	4.38
30.833	0.00	0.06	0.091	I	O	|	|	|	|	4.37
30.917	0.00	0.06	0.091	I	O	|	|	|	|	4.35
31.000	0.00	0.06	0.090	I	O	|	|	|	|	4.34
31.083	0.00	0.06	0.090	I	O	|	|	|	|	4.32
31.167	0.00	0.06	0.090	I	O	|	|	|	|	4.31
31.250	0.00	0.06	0.089	I	O	|	|	|	|	4.30
31.333	0.00	0.06	0.089	I	O	|	|	|	|	4.28
31.417	0.00	0.06	0.089	I	O	|	|	|	|	4.27
31.500	0.00	0.06	0.088	I	O	|	|	|	|	4.26
31.583	0.00	0.06	0.088	I	O	|	|	|	|	4.24
31.667	0.00	0.06	0.087	I	O	|	|	|	|	4.23
31.750	0.00	0.06	0.087	I	O	|	|	|	|	4.21
31.833	0.00	0.06	0.087	I	O	|	|	|	|	4.20
31.917	0.00	0.06	0.086	I	O	|	|	|	|	4.19
32.000	0.00	0.06	0.086	I	O	|	|	|	|	4.17
32.083	0.00	0.06	0.085	I	O	|	|	|	|	4.16
32.167	0.00	0.06	0.085	I	O	|	|	|	|	4.15
32.250	0.00	0.06	0.085	I	O	|	|	|	|	4.13
32.333	0.00	0.06	0.084	I	O	|	|	|	|	4.12
32.417	0.00	0.06	0.084	I	O	|	|	|	|	4.10
32.500	0.00	0.06	0.084	I	O	|	|	|	|	4.09
32.583	0.00	0.06	0.083	I	O	|	|	|	|	4.08
32.667	0.00	0.06	0.083	I	O	|	|	|	|	4.06
32.750	0.00	0.06	0.082	I	O	|	|	|	|	4.05
32.833	0.00	0.06	0.082	I	O	|	|	|	|	4.03
32.917	0.00	0.06	0.082	I	O	|	|	|	|	4.02
33.000	0.00	0.06	0.081	I	O	|	|	|	|	4.01

33.083	0.00	0.06	0.081	I	O	|	|	|	|	3.99
33.167	0.00	0.06	0.080	I	O	|	|	|	|	3.98
33.250	0.00	0.06	0.080	I	O	|	|	|	|	3.96
33.333	0.00	0.06	0.080	I	O	|	|	|	|	3.95
33.417	0.00	0.06	0.079	I	O	|	|	|	|	3.93
33.500	0.00	0.06	0.079	I	O	|	|	|	|	3.92
33.583	0.00	0.06	0.079	I	O	|	|	|	|	3.90
33.667	0.00	0.06	0.078	I	O	|	|	|	|	3.89
33.750	0.00	0.06	0.078	I	O	|	|	|	|	3.87
33.833	0.00	0.06	0.077	I	O	|	|	|	|	3.86
33.917	0.00	0.06	0.077	I	O	|	|	|	|	3.84
34.000	0.00	0.06	0.077	I	O	|	|	|	|	3.83
34.083	0.00	0.06	0.076	I	O	|	|	|	|	3.82
34.167	0.00	0.06	0.076	I	O	|	|	|	|	3.80
34.250	0.00	0.06	0.075	I	O	|	|	|	|	3.79
34.333	0.00	0.06	0.075	I	O	|	|	|	|	3.77
34.417	0.00	0.06	0.075	I	O	|	|	|	|	3.76
34.500	0.00	0.06	0.074	I	O	|	|	|	|	3.74
34.583	0.00	0.06	0.074	I	O	|	|	|	|	3.73
34.667	0.00	0.06	0.073	I	O	|	|	|	|	3.71
34.750	0.00	0.06	0.073	I	O	|	|	|	|	3.70
34.833	0.00	0.06	0.073	I	O	|	|	|	|	3.68
34.917	0.00	0.06	0.072	I	O	|	|	|	|	3.67
35.000	0.00	0.06	0.072	I	O	|	|	|	|	3.65
35.083	0.00	0.06	0.072	I	O	|	|	|	|	3.64
35.167	0.00	0.06	0.071	I	O	|	|	|	|	3.62
35.250	0.00	0.06	0.071	I	O	|	|	|	|	3.61
35.333	0.00	0.06	0.070	I	O	|	|	|	|	3.59
35.417	0.00	0.06	0.070	I	O	|	|	|	|	3.58
35.500	0.00	0.06	0.070	I	O	|	|	|	|	3.56
35.583	0.00	0.06	0.069	I	O	|	|	|	|	3.55
35.667	0.00	0.06	0.069	I	O	|	|	|	|	3.53
35.750	0.00	0.06	0.068	I	O	|	|	|	|	3.52
35.833	0.00	0.06	0.068	I	O	|	|	|	|	3.50
35.917	0.00	0.06	0.068	I	O	|	|	|	|	3.49
36.000	0.00	0.06	0.067	I	O	|	|	|	|	3.47
36.083	0.00	0.06	0.067	I	O	|	|	|	|	3.46
36.167	0.00	0.06	0.067	I	O	|	|	|	|	3.44
36.250	0.00	0.06	0.066	I	O	|	|	|	|	3.43
36.333	0.00	0.06	0.066	I	O	|	|	|	|	3.41
36.417	0.00	0.06	0.065	I	O	|	|	|	|	3.40
36.500	0.00	0.06	0.065	I	O	|	|	|	|	3.38
36.583	0.00	0.06	0.065	I	O	|	|	|	|	3.37
36.667	0.00	0.06	0.064	I	O	|	|	|	|	3.36
36.750	0.00	0.06	0.064	I	O	|	|	|	|	3.34
36.833	0.00	0.06	0.063	I	O	|	|	|	|	3.33
36.917	0.00	0.06	0.063	I	O	|	|	|	|	3.31
37.000	0.00	0.06	0.063	I	O	|	|	|	|	3.30
37.083	0.00	0.06	0.062	I	O	|	|	|	|	3.28
37.167	0.00	0.06	0.062	I	O	|	|	|	|	3.27
37.250	0.00	0.06	0.062	I	O	|	|	|	|	3.25
37.333	0.00	0.06	0.061	I	O	|	|	|	|	3.24
37.417	0.00	0.06	0.061	I	O	|	|	|	|	3.22

37.500	0.00	0.06	0.060	I	O	|	|	|	|	3.21
37.583	0.00	0.06	0.060	I	O	|	|	|	|	3.19
37.667	0.00	0.06	0.060	I	O	|	|	|	|	3.18
37.750	0.00	0.06	0.059	I	O	|	|	|	|	3.16
37.833	0.00	0.06	0.059	I	O	|	|	|	|	3.15
37.917	0.00	0.06	0.058	I	O	|	|	|	|	3.13
38.000	0.00	0.06	0.058	I	O	|	|	|	|	3.12
38.083	0.00	0.06	0.058	I	O	|	|	|	|	3.10
38.167	0.00	0.06	0.057	I	O	|	|	|	|	3.09
38.250	0.00	0.06	0.057	I	O	|	|	|	|	3.07
38.333	0.00	0.06	0.057	I	O	|	|	|	|	3.06
38.417	0.00	0.06	0.056	I	O	|	|	|	|	3.04
38.500	0.00	0.06	0.056	I	O	|	|	|	|	3.03
38.583	0.00	0.06	0.055	I	O	|	|	|	|	3.01
38.667	0.00	0.06	0.055	I	O	|	|	|	|	3.00
38.750	0.00	0.06	0.055	I	O	|	|	|	|	2.98
38.833	0.00	0.06	0.054	I	O	|	|	|	|	2.97
38.917	0.00	0.06	0.054	I	O	|	|	|	|	2.95
39.000	0.00	0.06	0.053	I	O	|	|	|	|	2.94
39.083	0.00	0.06	0.053	I	O	|	|	|	|	2.92
39.167	0.00	0.06	0.053	I	O	|	|	|	|	2.91
39.250	0.00	0.06	0.052	I	O	|	|	|	|	2.90
39.333	0.00	0.06	0.052	I	O	|	|	|	|	2.88
39.417	0.00	0.06	0.052	I	O	|	|	|	|	2.87
39.500	0.00	0.06	0.051	I	O	|	|	|	|	2.85
39.583	0.00	0.06	0.051	I	O	|	|	|	|	2.84
39.667	0.00	0.06	0.050	I	O	|	|	|	|	2.82
39.750	0.00	0.06	0.050	I	O	|	|	|	|	2.81
39.833	0.00	0.06	0.050	I	O	|	|	|	|	2.79
39.917	0.00	0.06	0.049	I	O	|	|	|	|	2.78
40.000	0.00	0.06	0.049	I	O	|	|	|	|	2.76
40.083	0.00	0.06	0.048	I	O	|	|	|	|	2.75
40.167	0.00	0.06	0.048	I	O	|	|	|	|	2.73
40.250	0.00	0.06	0.048	I	O	|	|	|	|	2.72
40.333	0.00	0.06	0.047	I	O	|	|	|	|	2.70
40.417	0.00	0.06	0.047	I	O	|	|	|	|	2.69
40.500	0.00	0.06	0.046	I	O	|	|	|	|	2.67
40.583	0.00	0.06	0.046	I	O	|	|	|	|	2.66
40.667	0.00	0.06	0.046	I	O	|	|	|	|	2.64
40.750	0.00	0.06	0.045	I	O	|	|	|	|	2.63
40.833	0.00	0.06	0.045	I	O	|	|	|	|	2.61
40.917	0.00	0.06	0.045	I	O	|	|	|	|	2.60
41.000	0.00	0.06	0.044	I	O	|	|	|	|	2.58
41.083	0.00	0.06	0.044	I	O	|	|	|	|	2.57
41.167	0.00	0.06	0.043	I	O	|	|	|	|	2.55
41.250	0.00	0.06	0.043	I	O	|	|	|	|	2.54
41.333	0.00	0.06	0.043	I	O	|	|	|	|	2.52
41.417	0.00	0.06	0.042	I	O	|	|	|	|	2.51
41.500	0.00	0.06	0.042	I	O	|	|	|	|	2.49
41.583	0.00	0.06	0.041	I	O	|	|	|	|	2.48
41.667	0.00	0.06	0.041	I	O	|	|	|	|	2.46
41.750	0.00	0.06	0.041	I	O	|	|	|	|	2.45
41.833	0.00	0.06	0.040	I	O	|	|	|	|	2.43

41.917	0.00	0.06	0.040	I	O	|	|	|	|	2.41
42.000	0.00	0.06	0.040	I	O	|	|	|	|	2.40
42.083	0.00	0.06	0.039	I	O	|	|	|	|	2.38
42.167	0.00	0.06	0.039	I	O	|	|	|	|	2.37
42.250	0.00	0.06	0.038	I	O	|	|	|	|	2.35
42.333	0.00	0.06	0.038	I	O	|	|	|	|	2.33
42.417	0.00	0.06	0.038	I	O	|	|	|	|	2.32
42.500	0.00	0.06	0.037	I	O	|	|	|	|	2.30
42.583	0.00	0.06	0.037	I	O	|	|	|	|	2.29
42.667	0.00	0.06	0.036	I	O	|	|	|	|	2.27
42.750	0.00	0.06	0.036	I	O	|	|	|	|	2.25
42.833	0.00	0.06	0.036	I	O	|	|	|	|	2.24
42.917	0.00	0.06	0.035	I	O	|	|	|	|	2.22
43.000	0.00	0.06	0.035	I	O	|	|	|	|	2.21
43.083	0.00	0.06	0.035	I	O	|	|	|	|	2.19
43.167	0.00	0.06	0.034	I	O	|	|	|	|	2.17
43.250	0.00	0.06	0.034	I	O	|	|	|	|	2.16
43.333	0.00	0.06	0.033	I	O	|	|	|	|	2.14
43.417	0.00	0.06	0.033	I	O	|	|	|	|	2.12
43.500	0.00	0.06	0.033	I	O	|	|	|	|	2.11
43.583	0.00	0.06	0.032	I	O	|	|	|	|	2.09
43.667	0.00	0.06	0.032	I	O	|	|	|	|	2.08
43.750	0.00	0.06	0.031	I	O	|	|	|	|	2.06
43.833	0.00	0.06	0.031	I	O	|	|	|	|	2.04
43.917	0.00	0.06	0.031	I	O	|	|	|	|	2.03
44.000	0.00	0.06	0.030	I	O	|	|	|	|	2.01
44.083	0.00	0.06	0.030	I	O	|	|	|	|	2.00
44.167	0.00	0.06	0.030	I	O	|	|	|	|	1.98
44.250	0.00	0.06	0.029	I	O	|	|	|	|	1.96
44.333	0.00	0.06	0.029	I	O	|	|	|	|	1.94
44.417	0.00	0.06	0.028	I	O	|	|	|	|	1.92
44.500	0.00	0.06	0.028	I	O	|	|	|	|	1.90
44.583	0.00	0.06	0.028	I	O	|	|	|	|	1.88
44.667	0.00	0.06	0.027	I	O	|	|	|	|	1.86
44.750	0.00	0.06	0.027	I	O	|	|	|	|	1.84
44.833	0.00	0.06	0.026	I	O	|	|	|	|	1.82
44.917	0.00	0.06	0.026	I	O	|	|	|	|	1.80
45.000	0.00	0.06	0.026	I	O	|	|	|	|	1.78
45.083	0.00	0.06	0.025	I	O	|	|	|	|	1.76
45.167	0.00	0.06	0.025	I	O	|	|	|	|	1.74
45.250	0.00	0.06	0.025	I	O	|	|	|	|	1.73
45.333	0.00	0.06	0.024	I	O	|	|	|	|	1.71
45.417	0.00	0.06	0.024	I	O	|	|	|	|	1.69
45.500	0.00	0.06	0.023	I	O	|	|	|	|	1.67
45.583	0.00	0.06	0.023	I	O	|	|	|	|	1.65
45.667	0.00	0.06	0.023	I	O	|	|	|	|	1.63
45.750	0.00	0.06	0.022	I	O	|	|	|	|	1.61
45.833	0.00	0.06	0.022	I	O	|	|	|	|	1.59
45.917	0.00	0.06	0.021	I	O	|	|	|	|	1.57
46.000	0.00	0.06	0.021	I	O	|	|	|	|	1.55
46.083	0.00	0.06	0.021	I	O	|	|	|	|	1.53
46.167	0.00	0.06	0.020	I	O	|	|	|	|	1.51
46.250	0.00	0.06	0.020	I	O	|	|	|	|	1.49

46.333	0.00	0.06	0.019	I	O	|	|	|	1.46
46.417	0.00	0.06	0.019	I	O	|	|	|	1.43
46.500	0.00	0.06	0.019	I	O	|	|	|	1.39
46.583	0.00	0.06	0.018	I	O	|	|	|	1.36
46.667	0.00	0.06	0.018	I	O	|	|	|	1.33
46.750	0.00	0.06	0.018	I	O	|	|	|	1.30
46.833	0.00	0.06	0.017	I	O	|	|	|	1.27
46.917	0.00	0.06	0.017	I	O	|	|	|	1.23
47.000	0.00	0.06	0.016	I	O	|	|	|	1.20
47.083	0.00	0.06	0.016	I	O	|	|	|	1.17
47.167	0.00	0.06	0.016	I	O	|	|	|	1.14
47.250	0.00	0.06	0.015	I	O	|	|	|	1.10
47.333	0.00	0.06	0.015	I	O	|	|	|	1.07
47.417	0.00	0.06	0.014	I	O	|	|	|	1.04
47.500	0.00	0.06	0.014	I	O	|	|	|	1.01
47.583	0.00	0.06	0.014	I	O	|	|	|	0.98
47.667	0.00	0.06	0.013	I	O	|	|	|	0.95
47.750	0.00	0.06	0.013	I	O	|	|	|	0.92
47.833	0.00	0.06	0.013	I	O	|	|	|	0.90
47.917	0.00	0.06	0.012	I	O	|	|	|	0.87
48.000	0.00	0.06	0.012	I	O	|	|	|	0.84
48.083	0.00	0.06	0.011	I	O	|	|	|	0.81
48.167	0.00	0.06	0.011	I	O	|	|	|	0.79
48.250	0.00	0.06	0.011	I	O	|	|	|	0.76
48.333	0.00	0.06	0.010	I	O	|	|	|	0.73
48.417	0.00	0.06	0.010	I	O	|	|	|	0.70
48.500	0.00	0.06	0.009	I	O	|	|	|	0.68
48.583	0.00	0.06	0.009	I	O	|	|	|	0.65
48.667	0.00	0.06	0.009	I	O	|	|	|	0.62
48.750	0.00	0.06	0.008	I	O	|	|	|	0.59
48.833	0.00	0.06	0.008	I	O	|	|	|	0.57
48.917	0.00	0.06	0.008	I	O	|	|	|	0.54
49.000	0.00	0.06	0.007	I	O	|	|	|	0.51
49.083	0.00	0.05	0.007	I	O	|	|	|	0.48
49.167	0.00	0.05	0.006	I	O	|	|	|	0.46
49.250	0.00	0.05	0.006	I	O	|	|	|	0.43
49.333	0.00	0.05	0.006	I	O	|	|	|	0.41
49.417	0.00	0.04	0.005	I	O	|	|	|	0.39
49.500	0.00	0.04	0.005	I	O	|	|	|	0.37
49.583	0.00	0.04	0.005	I	O	|	|	|	0.35
49.667	0.00	0.04	0.005	I	O	|	|	|	0.33
49.750	0.00	0.03	0.004	I	O	|	|	|	0.31
49.833	0.00	0.03	0.004	I	O	|	|	|	0.29
49.917	0.00	0.03	0.004	I	O	|	|	|	0.28
50.000	0.00	0.03	0.004	I	O	|	|	|	0.26
50.083	0.00	0.03	0.003	I	O	|	|	|	0.25
50.167	0.00	0.03	0.003	I	O	|	|	|	0.24
50.250	0.00	0.03	0.003	I	O	|	|	|	0.22
50.333	0.00	0.02	0.003	I	O	|	|	|	0.21
50.417	0.00	0.02	0.003	I	O	|	|	|	0.20
50.500	0.00	0.02	0.003	I	O	|	|	|	0.19
50.583	0.00	0.02	0.003	I	O	|	|	|	0.18
50.667	0.00	0.02	0.002	I	O	|	|	|	0.17

50.750	0.00	0.02	0.002	IO					0.16
50.833	0.00	0.02	0.002	IO					0.15
50.917	0.00	0.02	0.002	IO					0.14
51.000	0.00	0.02	0.002	IO					0.14
51.083	0.00	0.01	0.002	IO					0.13
51.167	0.00	0.01	0.002	IO					0.12
51.250	0.00	0.01	0.002	IO					0.12
51.333	0.00	0.01	0.002	IO					0.11
51.417	0.00	0.01	0.001	O					0.10
51.500	0.00	0.01	0.001	O					0.10
51.583	0.00	0.01	0.001	O					0.09
51.667	0.00	0.01	0.001	O					0.09
51.750	0.00	0.01	0.001	O					0.08
51.833	0.00	0.01	0.001	O					0.08
51.917	0.00	0.01	0.001	O					0.07
52.000	0.00	0.01	0.001	O					0.07
52.083	0.00	0.01	0.001	O					0.07
52.167	0.00	0.01	0.001	O					0.06
52.250	0.00	0.01	0.001	O					0.06
52.333	0.00	0.01	0.001	O					0.06
52.417	0.00	0.01	0.001	O					0.05
52.500	0.00	0.01	0.001	O					0.05
52.583	0.00	0.01	0.001	O					0.05
52.667	0.00	0.01	0.001	O					0.05
52.750	0.00	0.00	0.001	O					0.04
52.833	0.00	0.00	0.001	O					0.04
52.917	0.00	0.00	0.001	O					0.04
53.000	0.00	0.00	0.001	O					0.04
53.083	0.00	0.00	0.000	O					0.03
53.167	0.00	0.00	0.000	O					0.03
53.250	0.00	0.00	0.000	O					0.03
53.333	0.00	0.00	0.000	O					0.03
53.417	0.00	0.00	0.000	O					0.03
53.500	0.00	0.00	0.000	O					0.03
53.583	0.00	0.00	0.000	O					0.02
53.667	0.00	0.00	0.000	O					0.02
53.750	0.00	0.00	0.000	O					0.02
53.833	0.00	0.00	0.000	O					0.02
53.917	0.00	0.00	0.000	O					0.02
54.000	0.00	0.00	0.000	O					0.02
54.083	0.00	0.00	0.000	O					0.02
54.167	0.00	0.00	0.000	O					0.02
54.250	0.00	0.00	0.000	O					0.02
54.333	0.00	0.00	0.000	O					0.02
54.417	0.00	0.00	0.000	O					0.01
54.500	0.00	0.00	0.000	O					0.01
54.583	0.00	0.00	0.000	O					0.01
54.667	0.00	0.00	0.000	O					0.01
54.750	0.00	0.00	0.000	O					0.01
54.833	0.00	0.00	0.000	O					0.01
54.917	0.00	0.00	0.000	O					0.01
55.000	0.00	0.00	0.000	O					0.01
55.083	0.00	0.00	0.000	O					0.01

```
55.167    0.00    0.00      0.000  O       |       |       |       |     0.01

     ****************************HYDROGRAPH DATA****************************
                 Number of intervals =   662
                 Time interval =    5.0 (Min.)
                 Maximum/Peak flow rate =        0.056 (CFS)
                 Total volume =       0.223 (Ac.Ft)
           Status of hydrographs being held in storage
                      Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
           Peak (CFS)      0.000     0.000     0.000     0.000     0.000
           Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
     ***********************************************************************

     -----------------------------------------------------------------------
```

AREA CC1

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 07/21/25

ROUTING: BASIN CC1; UNIT HYDROGRAPH CC1

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARCC124100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 289
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.358 (CFS)
Total volume = 0.201 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 101.000 to Point/Station 102.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 289
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.006	0.051	0.006	0.006
1.000	0.013	0.051	0.013	0.013
1.500	0.018	0.051	0.018	0.018
2.000	0.027	0.051	0.027	0.027
2.500	0.038	0.051	0.038	0.038
3.000	0.049	0.051	0.049	0.049
3.500	0.061	0.051	0.061	0.061
4.000	0.073	0.051	0.073	0.073
4.500	0.085	0.051	0.085	0.085
5.000	0.097	0.051	0.097	0.097
5.500	0.107	0.051	0.107	0.107
6.000	0.117	0.051	0.117	0.117
6.500	0.123	0.051	0.123	0.123
7.000	0.129	0.051	0.129	0.129
7.500	0.135	0.051	0.135	0.135
7.580	0.136	0.051	0.136	0.136

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.1 0.18 0.27 0.36	Depth (Ft.)
0.083	0.01	0.00	0.000	OI | | | |	0.00
0.167	0.02	0.00	0.000	OI | | | |	0.01
0.250	0.02	0.00	0.000	OI | | | |	0.02
0.333	0.03	0.00	0.000	O I | | | |	0.03
0.417	0.03	0.00	0.001	O I | | | |	0.05
0.500	0.03	0.01	0.001	O I | | | |	0.06
0.583	0.03	0.01	0.001	O I | | | |	0.07
0.667	0.03	0.01	0.001	O I | | | |	0.09
0.750	0.03	0.01	0.001	O I | | | |	0.10
0.833	0.04	0.01	0.001	O I | | | |	0.11
0.917	0.04	0.01	0.001	|O I | | | |	0.12
1.000	0.04	0.01	0.002	|O I | | | |	0.14
1.083	0.03	0.02	0.002	|OI | | | |	0.15
1.167	0.03	0.02	0.002	|OI | | | |	0.16
1.250	0.03	0.02	0.002	|OI | | | |	0.17
1.333	0.03	0.02	0.002	|OI | | | |	0.17
1.417	0.03	0.02	0.002	|OI | | | |	0.18
1.500	0.03	0.02	0.002	|OI | | | |	0.18
1.583	0.03	0.02	0.002	|OI | | | |	0.19
1.667	0.03	0.02	0.002	|OI | | | |	0.20
1.750	0.03	0.02	0.002	|OI | | | |	0.20
1.833	0.04	0.02	0.002	|O I | | | |	0.21
1.917	0.04	0.02	0.003	|O I | | | |	0.22
2.000	0.04	0.02	0.003	| OI | | | |	0.23
2.083	0.04	0.02	0.003	| OI | | | |	0.23

2.167	0.04	0.02	0.003	OI				0.24
2.250	0.04	0.03	0.003	OI				0.25
2.333	0.04	0.03	0.003	OI				0.26
2.417	0.04	0.03	0.003	OI				0.26
2.500	0.04	0.03	0.003	OI				0.27
2.583	0.05	0.03	0.003	O I				0.28
2.667	0.05	0.03	0.003	O I				0.29
2.750	0.05	0.03	0.004	O I				0.30
2.833	0.05	0.03	0.004	O I				0.31
2.917	0.05	0.03	0.004	O I				0.32
3.000	0.05	0.03	0.004	O I				0.33
3.083	0.05	0.03	0.004	OI				0.34
3.167	0.05	0.04	0.004	OI				0.34
3.250	0.05	0.04	0.004	OI				0.35
3.333	0.05	0.04	0.004	OI				0.36
3.417	0.05	0.04	0.004	OI				0.36
3.500	0.05	0.04	0.004	OI				0.37
3.583	0.05	0.04	0.005	OI				0.38
3.667	0.05	0.04	0.005	OI				0.38
3.750	0.05	0.04	0.005	OI				0.39
3.833	0.05	0.04	0.005	OI				0.39
3.917	0.06	0.04	0.005	O I				0.40
4.000	0.06	0.04	0.005	O I				0.41
4.083	0.06	0.04	0.005	O I				0.42
4.167	0.06	0.04	0.005	O I				0.43
4.250	0.06	0.04	0.005	O I				0.44
4.333	0.06	0.05	0.005	OI				0.45
4.417	0.07	0.05	0.005	O I				0.46
4.500	0.07	0.05	0.006	O I				0.47
4.583	0.07	0.05	0.006	O I				0.48
4.667	0.07	0.05	0.006	O I				0.49
4.750	0.07	0.05	0.006	O I				0.50
4.833	0.07	0.05	0.006	O I				0.51
4.917	0.08	0.05	0.006	O I				0.52
5.000	0.08	0.05	0.006	O I				0.54
5.083	0.06	0.05	0.007	OI				0.55
5.167	0.06	0.05	0.007	OI				0.55
5.250	0.06	0.05	0.007	OI				0.55
5.333	0.06	0.05	0.007	OI				0.56
5.417	0.07	0.05	0.007	O I				0.57
5.500	0.07	0.05	0.007	O I				0.57
5.583	0.07	0.05	0.007	O I				0.58
5.667	0.08	0.05	0.007	O I				0.60
5.750	0.08	0.05	0.008	O I				0.61
5.833	0.08	0.05	0.008	O I				0.62
5.917	0.08	0.05	0.008	O I				0.63
6.000	0.08	0.05	0.008	O I				0.65
6.083	0.08	0.05	0.008	O I				0.66
6.167	0.09	0.05	0.009	O I				0.68
6.250	0.09	0.05	0.009	O I				0.70
6.333	0.09	0.05	0.009	O I				0.71
6.417	0.09	0.05	0.009	O I				0.73
6.500	0.09	0.05	0.009	O I				0.75

6.583	0.09	0.05	0.010	|	O	I	|	|	0.77
6.667	0.10	0.05	0.010	|	O	I	|	|	0.79
6.750	0.10	0.05	0.010	|	O	I	|	|	0.81
6.833	0.10	0.05	0.011	|	O	I	|	|	0.84
6.917	0.10	0.05	0.011	|	O	I	|	|	0.86
7.000	0.10	0.05	0.011	|	O	I	|	|	0.88
7.083	0.10	0.05	0.012	|	O	I	|	|	0.90
7.167	0.10	0.05	0.012	|	O	I	|	|	0.92
7.250	0.10	0.05	0.012	|	O	I	|	|	0.95
7.333	0.10	0.05	0.013	|	O	|I	|	|	0.97
7.417	0.11	0.05	0.013	|	O	|I	|	|	1.00
7.500	0.11	0.05	0.013	|	O	|I	|	|	1.03
7.583	0.11	0.05	0.014	|	O	| I	|	|	1.07
7.667	0.12	0.05	0.014	|	O	| I	|	|	1.12
7.750	0.12	0.05	0.015	|	O	| I	|	|	1.16
7.833	0.12	0.05	0.015	|	O	| I	|	|	1.21
7.917	0.13	0.05	0.016	|	O	| I	|	|	1.26
8.000	0.13	0.05	0.016	|	O	| I	|	|	1.31
8.083	0.14	0.05	0.017	|	O	| I	|	|	1.37
8.167	0.14	0.05	0.017	|	O	| I	|	|	1.43
8.250	0.14	0.05	0.018	|	O	| I	|	|	1.49
8.333	0.14	0.05	0.019	|	O	| I	|	|	1.53
8.417	0.14	0.05	0.019	|	O	| I	|	|	1.57
8.500	0.14	0.05	0.020	|	O	| I	|	|	1.60
8.583	0.15	0.05	0.021	|	O	| I	|	|	1.64
8.667	0.15	0.05	0.021	|	O	| I	|	|	1.68
8.750	0.15	0.05	0.022	|	O	| I	|	|	1.72
8.833	0.16	0.05	0.023	|	O	| I	|	|	1.76
8.917	0.16	0.05	0.023	|	O	| I	|	|	1.80
9.000	0.16	0.05	0.024	|	O	| I	|	|	1.85
9.083	0.18	0.05	0.025	|	O	| I|	|	|	1.89
9.167	0.18	0.05	0.026	|	O	| I	|	|	1.94
9.250	0.18	0.05	0.027	|	O	| I	|	|	1.99
9.333	0.19	0.05	0.028	|	O	| I	|	|	2.04
9.417	0.19	0.05	0.029	|	O	| |I	|	|	2.08
9.500	0.19	0.05	0.030	|	O	| |I	|	|	2.13
9.583	0.20	0.05	0.031	|	O	| |I	|	|	2.17
9.667	0.20	0.05	0.032	|	O	| | I	|	|	2.22
9.750	0.20	0.05	0.033	|	O	| | I	|	|	2.27
9.833	0.21	0.05	0.034	|	O	| | I	|	|	2.31
9.917	0.21	0.05	0.035	|	O	| | I	|	|	2.36
10.000	0.21	0.05	0.036	|	O	| | I	|	|	2.41
10.083	0.17	0.05	0.037	|	O	| I	|	|	2.46
10.167	0.14	0.05	0.038	|	O	| I	|	|	2.49
10.250	0.14	0.05	0.038	|	O	| I	|	|	2.52
10.333	0.14	0.05	0.039	|	O	| I	|	|	2.55
10.417	0.14	0.05	0.040	|	O	| I	|	|	2.58
10.500	0.14	0.05	0.040	|	O	| I	|	|	2.61
10.583	0.18	0.05	0.041	|	O	| I|	|	|	2.64
10.667	0.19	0.05	0.042	|	O	| |I	|	|	2.68
10.750	0.19	0.05	0.043	|	O	| |I	|	|	2.73
10.833	0.19	0.05	0.044	|	O	| |I	|	|	2.77
10.917	0.19	0.05	0.045	|	O	| |I	|	|	2.82

11.000	0.19	0.05	0.046	|	O	|	|I	|	2.86
11.083	0.19	0.05	0.047	|	O	|	I	|	2.91
11.167	0.18	0.05	0.048	|	O	|	I	|	2.95
11.250	0.18	0.05	0.049	|	O	|	I	|	2.99
11.333	0.18	0.05	0.050	|	O	|	I	|	3.03
11.417	0.18	0.05	0.051	|	O	|	I	|	3.07
11.500	0.18	0.05	0.051	|	O	|	I	|	3.10
11.583	0.17	0.05	0.052	|	O	|	I|	|	3.14
11.667	0.16	0.05	0.053	|	O	|	I |	|	3.17
11.750	0.16	0.05	0.054	|	O	|	I |	|	3.21
11.833	0.17	0.05	0.055	|	O	|	I|	|	3.24
11.917	0.17	0.05	0.056	|	O	|	I|	|	3.27
12.000	0.17	0.05	0.056	|	O	|	I|	|	3.31
12.083	0.22	0.05	0.057	|	O	|	| I	|	3.35
12.167	0.24	0.05	0.059	|	O	|	| I	|	3.40
12.250	0.24	0.05	0.060	|	O	|	| I	|	3.46
12.333	0.25	0.05	0.061	|	O	|	| I	|	3.51
12.417	0.25	0.05	0.063	|	O	|	| I	|	3.57
12.500	0.25	0.05	0.064	|	O	|	| I	|	3.63
12.583	0.26	0.05	0.065	|	O	|	| I|	|	3.69
12.667	0.27	0.05	0.067	|	O	|	| I	|	3.75
12.750	0.27	0.05	0.068	|	O	|	| I	|	3.81
12.833	0.28	0.05	0.070	|	O	|	|I	|	3.88
12.917	0.29	0.05	0.072	|	O	|	|I	|	3.94
13.000	0.29	0.05	0.073	|	O	|	|I	|	4.01
13.083	0.33	0.05	0.075	|	O	|	|	I |	4.08
13.167	0.36	0.05	0.077	|	O	|	|	I|	4.17
13.250	0.36	0.05	0.079	|	O	|	|	I|	4.26
13.333	0.36	0.05	0.081	|	O	|	|	I|	4.34
13.417	0.36	0.05	0.083	|	O	|	|	I|	4.43
13.500	0.36	0.05	0.085	|	O	|	|	I	4.52
13.583	0.27	0.05	0.087	|	O	|	| I|	|	4.59
13.667	0.22	0.05	0.089	|	O	|	| I	|	4.65
13.750	0.22	0.05	0.090	|	O	|	| I	|	4.70
13.833	0.22	0.05	0.091	|	O	|	| I	|	4.75
13.917	0.22	0.05	0.092	|	O	|	| I	|	4.80
14.000	0.22	0.05	0.093	|	O	|	| I	|	4.85
14.083	0.25	0.05	0.095	|	O	|	| I	|	4.90
14.167	0.27	0.05	0.096	|	O	|	| I|	|	4.96
14.250	0.27	0.05	0.097	|	O	|	| I|	|	5.02
14.333	0.26	0.05	0.099	|	O	|	| I|	|	5.10
14.417	0.25	0.05	0.100	|	O	|	| I	|	5.17
14.500	0.25	0.05	0.102	|	O	|	| I	|	5.24
14.583	0.26	0.05	0.103	|	O	|	| I	|	5.31
14.667	0.26	0.05	0.105	|	O	|	| I	|	5.38
14.750	0.26	0.05	0.106	|	O	|	| I	|	5.45
14.833	0.25	0.05	0.107	|	O	|	| I	|	5.52
14.917	0.24	0.05	0.109	|	O	|	| I	|	5.58
15.000	0.24	0.05	0.110	|	O	|	| I	|	5.65
15.083	0.24	0.05	0.111	|	O	|	| I	|	5.72
15.167	0.23	0.05	0.113	|	O	|	| I	|	5.78
15.250	0.23	0.05	0.114	|	O	|	| I	|	5.84
15.333	0.23	0.05	0.115	|	O	|	| I	|	5.90

15.417	0.22	0.05	0.116	| O |		| I |			5.96
15.500	0.22	0.05	0.117	| O |		| I |			6.03
15.583	0.20	0.05	0.119	| O |		|I			6.13
15.667	0.18	0.05	0.119	| O |		I			6.20
15.750	0.18	0.05	0.120	| O |		I			6.28
15.833	0.18	0.05	0.121	| O |		I			6.36
15.917	0.18	0.05	0.122	| O |		I			6.43
16.000	0.18	0.05	0.123	| O |		I			6.51
16.083	0.09	0.05	0.124	| O I|					6.56
16.167	0.04	0.05	0.124	| IO |					6.56
16.250	0.04	0.05	0.124	| IO |					6.56
16.333	0.04	0.05	0.124	| IO |					6.55
16.417	0.04	0.05	0.123	| IO |					6.54
16.500	0.04	0.05	0.123	| IO |					6.53
16.583	0.03	0.05	0.123	| I O |					6.53
16.667	0.03	0.05	0.123	| I O |					6.51
16.750	0.03	0.05	0.123	| I O |					6.50
16.833	0.03	0.05	0.123	| I O |					6.49
16.917	0.03	0.05	0.123	| I O |					6.48
17.000	0.03	0.05	0.123	| I O |					6.46
17.083	0.04	0.05	0.122	| IO |					6.45
17.167	0.05	0.05	0.122	| O |					6.45
17.250	0.05	0.05	0.122	| O |					6.45
17.333	0.05	0.05	0.122	| O |					6.45
17.417	0.05	0.05	0.122	| O |					6.45
17.500	0.05	0.05	0.122	| O |					6.44
17.583	0.05	0.05	0.122	| O |					6.44
17.667	0.05	0.05	0.122	| O |					6.44
17.750	0.05	0.05	0.122	| O |					6.44
17.833	0.04	0.05	0.122	| IO |					6.44
17.917	0.04	0.05	0.122	| IO |					6.43
18.000	0.04	0.05	0.122	| IO |					6.42
18.083	0.04	0.05	0.122	| IO |					6.42
18.167	0.04	0.05	0.122	| IO |					6.41
18.250	0.04	0.05	0.122	| IO |					6.40
18.333	0.04	0.05	0.122	| IO |					6.39
18.417	0.04	0.05	0.122	| IO |					6.39
18.500	0.04	0.05	0.122	| IO |					6.38
18.583	0.03	0.05	0.121	| I O |					6.37
18.667	0.03	0.05	0.121	| I O |					6.36
18.750	0.03	0.05	0.121	| I O |					6.35
18.833	0.02	0.05	0.121	| I O |					6.33
18.917	0.02	0.05	0.121	|I O |					6.32
19.000	0.02	0.05	0.121	|I O |					6.30
19.083	0.03	0.05	0.120	| I O |					6.28
19.167	0.03	0.05	0.120	| I O |					6.27
19.250	0.03	0.05	0.120	| I O |					6.25
19.333	0.04	0.05	0.120	| IO |					6.24
19.417	0.04	0.05	0.120	| IO |					6.24
19.500	0.04	0.05	0.120	| IO |					6.23
19.583	0.03	0.05	0.120	| I O |					6.22
19.667	0.03	0.05	0.119	| I O |					6.21
19.750	0.03	0.05	0.119	| I O |					6.20

19.833	0.02	0.05	0.119	| I O |	|	|	|	6.18
19.917	0.02	0.05	0.119	|I O |	|	|	|	6.16
20.000	0.02	0.05	0.119	|I O |	|	|	|	6.15
20.083	0.03	0.05	0.119	| I O |	|	|	|	6.13
20.167	0.03	0.05	0.118	| I O |	|	|	|	6.12
20.250	0.03	0.05	0.118	| I O |	|	|	|	6.10
20.333	0.03	0.05	0.118	| I O |	|	|	|	6.09
20.417	0.03	0.05	0.118	| I O |	|	|	|	6.08
20.500	0.03	0.05	0.118	| I O |	|	|	|	6.06
20.583	0.03	0.05	0.118	| I O |	|	|	|	6.05
20.667	0.03	0.05	0.117	| I O |	|	|	|	6.04
20.750	0.03	0.05	0.117	| I O |	|	|	|	6.03
20.833	0.02	0.05	0.117	| I O |	|	|	|	6.01
20.917	0.02	0.05	0.117	|I O |	|	|	|	6.00
21.000	0.02	0.05	0.117	|I O |	|	|	|	5.99
21.083	0.03	0.05	0.117	| I O |	|	|	|	5.98
21.167	0.03	0.05	0.116	| I O |	|	|	|	5.97
21.250	0.03	0.05	0.116	| I O |	|	|	|	5.96
21.333	0.02	0.05	0.116	| I O |	|	|	|	5.95
21.417	0.02	0.05	0.116	|I O |	|	|	|	5.94
21.500	0.02	0.05	0.116	|I O |	|	|	|	5.93
21.583	0.03	0.05	0.115	| I O |	|	|	|	5.92
21.667	0.03	0.05	0.115	| I O |	|	|	|	5.91
21.750	0.03	0.05	0.115	| I O |	|	|	|	5.91
21.833	0.02	0.05	0.115	| I O |	|	|	|	5.90
21.917	0.02	0.05	0.115	|I O |	|	|	|	5.89
22.000	0.02	0.05	0.114	|I O |	|	|	|	5.87
22.083	0.03	0.05	0.114	| I O |	|	|	|	5.87
22.167	0.03	0.05	0.114	| I O |	|	|	|	5.86
22.250	0.03	0.05	0.114	| I O |	|	|	|	5.85
22.333	0.02	0.05	0.114	| I O |	|	|	|	5.84
22.417	0.02	0.05	0.114	|I O |	|	|	|	5.83
22.500	0.02	0.05	0.113	|I O |	|	|	|	5.82
22.583	0.02	0.05	0.113	|I O |	|	|	|	5.81
22.667	0.02	0.05	0.113	|I O |	|	|	|	5.80
22.750	0.02	0.05	0.113	|I O |	|	|	|	5.79
22.833	0.02	0.05	0.113	|I O |	|	|	|	5.78
22.917	0.02	0.05	0.112	|I O |	|	|	|	5.76
23.000	0.02	0.05	0.112	|I O |	|	|	|	5.75
23.083	0.02	0.05	0.112	|I O |	|	|	|	5.74
23.167	0.02	0.05	0.112	|I O |	|	|	|	5.73
23.250	0.02	0.05	0.111	|I O |	|	|	|	5.72
23.333	0.02	0.05	0.111	|I O |	|	|	|	5.71
23.417	0.02	0.05	0.111	|I O |	|	|	|	5.70
23.500	0.02	0.05	0.111	|I O |	|	|	|	5.69
23.583	0.02	0.05	0.111	|I O |	|	|	|	5.68
23.667	0.02	0.05	0.110	|I O |	|	|	|	5.67
23.750	0.02	0.05	0.110	|I O |	|	|	|	5.66
23.833	0.02	0.05	0.110	|I O |	|	|	|	5.64
23.917	0.02	0.05	0.110	|I O |	|	|	|	5.63
24.000	0.02	0.05	0.109	|I O |	|	|	|	5.62
24.083	0.01	0.05	0.109	I O |	|	|	|	5.61
24.167	0.00	0.05	0.109	I O |	|	|	|	5.59

24.250	0.00	0.05	0.109	I	O	|	|	|	|	5.58
24.333	0.00	0.05	0.108	I	O	|	|	|	|	5.56
24.417	0.00	0.05	0.108	I	O	|	|	|	|	5.54
24.500	0.00	0.05	0.107	I	O	|	|	|	|	5.52
24.583	0.00	0.05	0.107	I	O	|	|	|	|	5.51
24.667	0.00	0.05	0.107	I	O	|	|	|	|	5.49
24.750	0.00	0.05	0.106	I	O	|	|	|	|	5.47
24.833	0.00	0.05	0.106	I	O	|	|	|	|	5.45
24.917	0.00	0.05	0.106	I	O	|	|	|	|	5.44
25.000	0.00	0.05	0.105	I	O	|	|	|	|	5.42
25.083	0.00	0.05	0.105	I	O	|	|	|	|	5.40
25.167	0.00	0.05	0.105	I	O	|	|	|	|	5.38
25.250	0.00	0.05	0.104	I	O	|	|	|	|	5.37
25.333	0.00	0.05	0.104	I	O	|	|	|	|	5.35
25.417	0.00	0.05	0.104	I	O	|	|	|	|	5.33
25.500	0.00	0.05	0.103	I	O	|	|	|	|	5.31
25.583	0.00	0.05	0.103	I	O	|	|	|	|	5.29
25.667	0.00	0.05	0.103	I	O	|	|	|	|	5.28
25.750	0.00	0.05	0.102	I	O	|	|	|	|	5.26
25.833	0.00	0.05	0.102	I	O	|	|	|	|	5.24
25.917	0.00	0.05	0.101	I	O	|	|	|	|	5.22
26.000	0.00	0.05	0.101	I	O	|	|	|	|	5.21
26.083	0.00	0.05	0.101	I	O	|	|	|	|	5.19
26.167	0.00	0.05	0.100	I	O	|	|	|	|	5.17
26.250	0.00	0.05	0.100	I	O	|	|	|	|	5.15
26.333	0.00	0.05	0.100	I	O	|	|	|	|	5.14
26.417	0.00	0.05	0.099	I	O	|	|	|	|	5.12
26.500	0.00	0.05	0.099	I	O	|	|	|	|	5.10
26.583	0.00	0.05	0.099	I	O	|	|	|	|	5.08
26.667	0.00	0.05	0.098	I	O	|	|	|	|	5.07
26.750	0.00	0.05	0.098	I	O	|	|	|	|	5.05
26.833	0.00	0.05	0.098	I	O	|	|	|	|	5.03
26.917	0.00	0.05	0.097	I	O	|	|	|	|	5.01
27.000	0.00	0.05	0.097	I	O	|	|	|	|	5.00
27.083	0.00	0.05	0.097	I	O	|	|	|	|	4.98
27.167	0.00	0.05	0.096	I	O	|	|	|	|	4.97
27.250	0.00	0.05	0.096	I	O	|	|	|	|	4.95
27.333	0.00	0.05	0.096	I	O	|	|	|	|	4.94
27.417	0.00	0.05	0.095	I	O	|	|	|	|	4.92
27.500	0.00	0.05	0.095	I	O	|	|	|	|	4.91
27.583	0.00	0.05	0.094	I	O	|	|	|	|	4.89
27.667	0.00	0.05	0.094	I	O	|	|	|	|	4.88
27.750	0.00	0.05	0.094	I	O	|	|	|	|	4.87
27.833	0.00	0.05	0.093	I	O	|	|	|	|	4.85
27.917	0.00	0.05	0.093	I	O	|	|	|	|	4.84
28.000	0.00	0.05	0.093	I	O	|	|	|	|	4.82
28.083	0.00	0.05	0.092	I	O	|	|	|	|	4.81
28.167	0.00	0.05	0.092	I	O	|	|	|	|	4.79
28.250	0.00	0.05	0.092	I	O	|	|	|	|	4.78
28.333	0.00	0.05	0.091	I	O	|	|	|	|	4.76
28.417	0.00	0.05	0.091	I	O	|	|	|	|	4.75
28.500	0.00	0.05	0.091	I	O	|	|	|	|	4.73
28.583	0.00	0.05	0.090	I	O	|	|	|	|	4.72

28.667	0.00	0.05	0.090	I	O	|	|	|	|	4.70
28.750	0.00	0.05	0.090	I	O	|	|	|	|	4.69
28.833	0.00	0.05	0.089	I	O	|	|	|	|	4.67
28.917	0.00	0.05	0.089	I	O	|	|	|	|	4.66
29.000	0.00	0.05	0.088	I	O	|	|	|	|	4.65
29.083	0.00	0.05	0.088	I	O	|	|	|	|	4.63
29.167	0.00	0.05	0.088	I	O	|	|	|	|	4.62
29.250	0.00	0.05	0.087	I	O	|	|	|	|	4.60
29.333	0.00	0.05	0.087	I	O	|	|	|	|	4.59
29.417	0.00	0.05	0.087	I	O	|	|	|	|	4.57
29.500	0.00	0.05	0.086	I	O	|	|	|	|	4.56
29.583	0.00	0.05	0.086	I	O	|	|	|	|	4.54
29.667	0.00	0.05	0.086	I	O	|	|	|	|	4.53
29.750	0.00	0.05	0.085	I	O	|	|	|	|	4.51
29.833	0.00	0.05	0.085	I	O	|	|	|	|	4.50
29.917	0.00	0.05	0.085	I	O	|	|	|	|	4.48
30.000	0.00	0.05	0.084	I	O	|	|	|	|	4.47
30.083	0.00	0.05	0.084	I	O	|	|	|	|	4.46
30.167	0.00	0.05	0.084	I	O	|	|	|	|	4.44
30.250	0.00	0.05	0.083	I	O	|	|	|	|	4.43
30.333	0.00	0.05	0.083	I	O	|	|	|	|	4.41
30.417	0.00	0.05	0.083	I	O	|	|	|	|	4.40
30.500	0.00	0.05	0.082	I	O	|	|	|	|	4.38
30.583	0.00	0.05	0.082	I	O	|	|	|	|	4.37
30.667	0.00	0.05	0.081	I	O	|	|	|	|	4.35
30.750	0.00	0.05	0.081	I	O	|	|	|	|	4.34
30.833	0.00	0.05	0.081	I	O	|	|	|	|	4.32
30.917	0.00	0.05	0.080	I	O	|	|	|	|	4.31
31.000	0.00	0.05	0.080	I	O	|	|	|	|	4.29
31.083	0.00	0.05	0.080	I	O	|	|	|	|	4.28
31.167	0.00	0.05	0.079	I	O	|	|	|	|	4.27
31.250	0.00	0.05	0.079	I	O	|	|	|	|	4.25
31.333	0.00	0.05	0.079	I	O	|	|	|	|	4.24
31.417	0.00	0.05	0.078	I	O	|	|	|	|	4.22
31.500	0.00	0.05	0.078	I	O	|	|	|	|	4.21
31.583	0.00	0.05	0.078	I	O	|	|	|	|	4.19
31.667	0.00	0.05	0.077	I	O	|	|	|	|	4.18
31.750	0.00	0.05	0.077	I	O	|	|	|	|	4.16
31.833	0.00	0.05	0.077	I	O	|	|	|	|	4.15
31.917	0.00	0.05	0.076	I	O	|	|	|	|	4.13
32.000	0.00	0.05	0.076	I	O	|	|	|	|	4.12
32.083	0.00	0.05	0.075	I	O	|	|	|	|	4.10
32.167	0.00	0.05	0.075	I	O	|	|	|	|	4.09
32.250	0.00	0.05	0.075	I	O	|	|	|	|	4.07
32.333	0.00	0.05	0.074	I	O	|	|	|	|	4.06
32.417	0.00	0.05	0.074	I	O	|	|	|	|	4.05
32.500	0.00	0.05	0.074	I	O	|	|	|	|	4.03
32.583	0.00	0.05	0.073	I	O	|	|	|	|	4.02
32.667	0.00	0.05	0.073	I	O	|	|	|	|	4.00
32.750	0.00	0.05	0.073	I	O	|	|	|	|	3.99
32.833	0.00	0.05	0.072	I	O	|	|	|	|	3.97
32.917	0.00	0.05	0.072	I	O	|	|	|	|	3.96
33.000	0.00	0.05	0.072	I	O	|	|	|	|	3.94

33.083	0.00	0.05	0.071	I	O	|	|	|	|	3.93
33.167	0.00	0.05	0.071	I	O	|	|	|	|	3.91
33.250	0.00	0.05	0.071	I	O	|	|	|	|	3.90
33.333	0.00	0.05	0.070	I	O	|	|	|	|	3.88
33.417	0.00	0.05	0.070	I	O	|	|	|	|	3.87
33.500	0.00	0.05	0.070	I	O	|	|	|	|	3.86
33.583	0.00	0.05	0.069	I	O	|	|	|	|	3.84
33.667	0.00	0.05	0.069	I	O	|	|	|	|	3.83
33.750	0.00	0.05	0.068	I	O	|	|	|	|	3.81
33.833	0.00	0.05	0.068	I	O	|	|	|	|	3.80
33.917	0.00	0.05	0.068	I	O	|	|	|	|	3.78
34.000	0.00	0.05	0.067	I	O	|	|	|	|	3.77
34.083	0.00	0.05	0.067	I	O	|	|	|	|	3.75
34.167	0.00	0.05	0.067	I	O	|	|	|	|	3.74
34.250	0.00	0.05	0.066	I	O	|	|	|	|	3.72
34.333	0.00	0.05	0.066	I	O	|	|	|	|	3.71
34.417	0.00	0.05	0.066	I	O	|	|	|	|	3.69
34.500	0.00	0.05	0.065	I	O	|	|	|	|	3.68
34.583	0.00	0.05	0.065	I	O	|	|	|	|	3.67
34.667	0.00	0.05	0.065	I	O	|	|	|	|	3.65
34.750	0.00	0.05	0.064	I	O	|	|	|	|	3.64
34.833	0.00	0.05	0.064	I	O	|	|	|	|	3.62
34.917	0.00	0.05	0.064	I	O	|	|	|	|	3.61
35.000	0.00	0.05	0.063	I	O	|	|	|	|	3.59
35.083	0.00	0.05	0.063	I	O	|	|	|	|	3.58
35.167	0.00	0.05	0.063	I	O	|	|	|	|	3.56
35.250	0.00	0.05	0.062	I	O	|	|	|	|	3.55
35.333	0.00	0.05	0.062	I	O	|	|	|	|	3.53
35.417	0.00	0.05	0.061	I	O	|	|	|	|	3.52
35.500	0.00	0.05	0.061	I	O	|	|	|	|	3.50
35.583	0.00	0.05	0.061	I	O	|	|	|	|	3.49
35.667	0.00	0.05	0.060	I	O	|	|	|	|	3.47
35.750	0.00	0.05	0.060	I	O	|	|	|	|	3.46
35.833	0.00	0.05	0.060	I	O	|	|	|	|	3.45
35.917	0.00	0.05	0.059	I	O	|	|	|	|	3.43
36.000	0.00	0.05	0.059	I	O	|	|	|	|	3.42
36.083	0.00	0.05	0.059	I	O	|	|	|	|	3.40
36.167	0.00	0.05	0.058	I	O	|	|	|	|	3.39
36.250	0.00	0.05	0.058	I	O	|	|	|	|	3.37
36.333	0.00	0.05	0.058	I	O	|	|	|	|	3.36
36.417	0.00	0.05	0.057	I	O	|	|	|	|	3.34
36.500	0.00	0.05	0.057	I	O	|	|	|	|	3.33
36.583	0.00	0.05	0.057	I	O	|	|	|	|	3.31
36.667	0.00	0.05	0.056	I	O	|	|	|	|	3.30
36.750	0.00	0.05	0.056	I	O	|	|	|	|	3.28
36.833	0.00	0.05	0.055	I	O	|	|	|	|	3.27
36.917	0.00	0.05	0.055	I	O	|	|	|	|	3.26
37.000	0.00	0.05	0.055	I	O	|	|	|	|	3.24
37.083	0.00	0.05	0.054	I	O	|	|	|	|	3.23
37.167	0.00	0.05	0.054	I	O	|	|	|	|	3.21
37.250	0.00	0.05	0.054	I	O	|	|	|	|	3.20
37.333	0.00	0.05	0.053	I	O	|	|	|	|	3.18
37.417	0.00	0.05	0.053	I	O	|	|	|	|	3.17

37.500	0.00	0.05	0.053	I	O	|	|	|	|	3.15
37.583	0.00	0.05	0.052	I	O	|	|	|	|	3.14
37.667	0.00	0.05	0.052	I	O	|	|	|	|	3.12
37.750	0.00	0.05	0.052	I	O	|	|	|	|	3.11
37.833	0.00	0.05	0.051	I	O	|	|	|	|	3.09
37.917	0.00	0.05	0.051	I	O	|	|	|	|	3.08
38.000	0.00	0.05	0.051	I	O	|	|	|	|	3.07
38.083	0.00	0.05	0.050	I	O	|	|	|	|	3.05
38.167	0.00	0.05	0.050	I	O	|	|	|	|	3.04
38.250	0.00	0.05	0.050	I	O	|	|	|	|	3.02
38.333	0.00	0.05	0.049	I	O	|	|	|	|	3.01
38.417	0.00	0.05	0.049	I	O	|	|	|	|	2.99
38.500	0.00	0.05	0.048	I	O	|	|	|	|	2.98
38.583	0.00	0.05	0.048	I	O	|	|	|	|	2.96
38.667	0.00	0.05	0.048	I	O	|	|	|	|	2.94
38.750	0.00	0.05	0.047	I	O	|	|	|	|	2.93
38.833	0.00	0.05	0.047	I	O	|	|	|	|	2.91
38.917	0.00	0.05	0.047	I	O	|	|	|	|	2.90
39.000	0.00	0.05	0.046	I	O	|	|	|	|	2.88
39.083	0.00	0.05	0.046	I	O	|	|	|	|	2.86
39.167	0.00	0.05	0.046	I	O	|	|	|	|	2.85
39.250	0.00	0.05	0.045	I	O	|	|	|	|	2.83
39.333	0.00	0.05	0.045	I	O	|	|	|	|	2.82
39.417	0.00	0.05	0.045	I	O	|	|	|	|	2.80
39.500	0.00	0.05	0.044	I	O	|	|	|	|	2.78
39.583	0.00	0.05	0.044	I	O	|	|	|	|	2.77
39.667	0.00	0.05	0.044	I	O	|	|	|	|	2.75
39.750	0.00	0.05	0.043	I	O	|	|	|	|	2.74
39.833	0.00	0.05	0.043	I	O	|	|	|	|	2.72
39.917	0.00	0.05	0.042	I	O	|	|	|	|	2.70
40.000	0.00	0.05	0.042	I	O	|	|	|	|	2.69
40.083	0.00	0.05	0.042	I	O	|	|	|	|	2.67
40.167	0.00	0.05	0.041	I	O	|	|	|	|	2.66
40.250	0.00	0.05	0.041	I	O	|	|	|	|	2.64
40.333	0.00	0.05	0.041	I	O	|	|	|	|	2.62
40.417	0.00	0.05	0.040	I	O	|	|	|	|	2.61
40.500	0.00	0.05	0.040	I	O	|	|	|	|	2.59
40.583	0.00	0.05	0.040	I	O	|	|	|	|	2.58
40.667	0.00	0.05	0.039	I	O	|	|	|	|	2.56
40.750	0.00	0.05	0.039	I	O	|	|	|	|	2.54
40.833	0.00	0.05	0.039	I	O	|	|	|	|	2.53
40.917	0.00	0.05	0.038	I	O	|	|	|	|	2.51
41.000	0.00	0.05	0.038	I	O	|	|	|	|	2.50
41.083	0.00	0.05	0.038	I	O	|	|	|	|	2.48
41.167	0.00	0.05	0.037	I	O	|	|	|	|	2.46
41.250	0.00	0.05	0.037	I	O	|	|	|	|	2.45
41.333	0.00	0.05	0.037	I	O	|	|	|	|	2.43
41.417	0.00	0.05	0.036	I	O	|	|	|	|	2.42
41.500	0.00	0.05	0.036	I	O	|	|	|	|	2.40
41.583	0.00	0.05	0.035	I	O	|	|	|	|	2.38
41.667	0.00	0.05	0.035	I	O	|	|	|	|	2.37
41.750	0.00	0.05	0.035	I	O	|	|	|	|	2.35
41.833	0.00	0.05	0.034	I	O	|	|	|	|	2.34

41.917	0.00	0.05	0.034	I	O	|	|	|	|	2.32
42.000	0.00	0.05	0.034	I	O	|	|	|	|	2.30
42.083	0.00	0.05	0.033	I	O	|	|	|	|	2.29
42.167	0.00	0.05	0.033	I	O	|	|	|	|	2.27
42.250	0.00	0.05	0.033	I	O	|	|	|	|	2.26
42.333	0.00	0.05	0.032	I	O	|	|	|	|	2.24
42.417	0.00	0.05	0.032	I	O	|	|	|	|	2.22
42.500	0.00	0.05	0.032	I	O	|	|	|	|	2.21
42.583	0.00	0.05	0.031	I	O	|	|	|	|	2.19
42.667	0.00	0.05	0.031	I	O	|	|	|	|	2.18
42.750	0.00	0.05	0.031	I	O	|	|	|	|	2.16
42.833	0.00	0.05	0.030	I	O	|	|	|	|	2.14
42.917	0.00	0.05	0.030	I	O	|	|	|	|	2.13
43.000	0.00	0.05	0.029	I	O	|	|	|	|	2.11
43.083	0.00	0.05	0.029	I	O	|	|	|	|	2.10
43.167	0.00	0.05	0.029	I	O	|	|	|	|	2.08
43.250	0.00	0.05	0.028	I	O	|	|	|	|	2.07
43.333	0.00	0.05	0.028	I	O	|	|	|	|	2.05
43.417	0.00	0.05	0.028	I	O	|	|	|	|	2.03
43.500	0.00	0.05	0.027	I	O	|	|	|	|	2.02
43.583	0.00	0.05	0.027	I	O	|	|	|	|	2.00
43.667	0.00	0.05	0.027	I	O	|	|	|	|	1.98
43.750	0.00	0.05	0.026	I	O	|	|	|	|	1.96
43.833	0.00	0.05	0.026	I	O	|	|	|	|	1.94
43.917	0.00	0.05	0.026	I	O	|	|	|	|	1.92
44.000	0.00	0.05	0.025	I	O	|	|	|	|	1.90
44.083	0.00	0.05	0.025	I	O	|	|	|	|	1.88
44.167	0.00	0.05	0.025	I	O	|	|	|	|	1.86
44.250	0.00	0.05	0.024	I	O	|	|	|	|	1.85
44.333	0.00	0.05	0.024	I	O	|	|	|	|	1.83
44.417	0.00	0.05	0.024	I	O	|	|	|	|	1.81
44.500	0.00	0.05	0.023	I	O	|	|	|	|	1.79
44.583	0.00	0.05	0.023	I	O	|	|	|	|	1.77
44.667	0.00	0.05	0.022	I	O	|	|	|	|	1.75
44.750	0.00	0.05	0.022	I	O	|	|	|	|	1.73
44.833	0.00	0.05	0.022	I	O	|	|	|	|	1.71
44.917	0.00	0.05	0.021	I	O	|	|	|	|	1.69
45.000	0.00	0.05	0.021	I	O	|	|	|	|	1.67
45.083	0.00	0.05	0.021	I	O	|	|	|	|	1.65
45.167	0.00	0.05	0.020	I	O	|	|	|	|	1.63
45.250	0.00	0.05	0.020	I	O	|	|	|	|	1.61
45.333	0.00	0.05	0.020	I	O	|	|	|	|	1.59
45.417	0.00	0.05	0.019	I	O	|	|	|	|	1.57
45.500	0.00	0.05	0.019	I	O	|	|	|	|	1.55
45.583	0.00	0.05	0.019	I	O	|	|	|	|	1.53
45.667	0.00	0.05	0.018	I	O	|	|	|	|	1.51
45.750	0.00	0.05	0.018	I	O	|	|	|	|	1.49
45.833	0.00	0.05	0.018	I	O	|	|	|	|	1.45
45.917	0.00	0.05	0.017	I	O	|	|	|	|	1.42
46.000	0.00	0.05	0.017	I	O	|	|	|	|	1.38
46.083	0.00	0.05	0.016	I	O	|	|	|	|	1.35
46.167	0.00	0.05	0.016	I	O	|	|	|	|	1.31
46.250	0.00	0.05	0.016	I	O	|	|	|	|	1.28

46.333	0.00	0.05	0.015	I	O	|	|	|	1.24
46.417	0.00	0.05	0.015	I	O	|	|	|	1.21
46.500	0.00	0.05	0.015	I	O	|	|	|	1.17
46.583	0.00	0.05	0.014	I	O	|	|	|	1.14
46.667	0.00	0.05	0.014	I	O	|	|	|	1.10
46.750	0.00	0.05	0.014	I	O	|	|	|	1.07
46.833	0.00	0.05	0.013	I	O	|	|	|	1.03
46.917	0.00	0.05	0.013	I	O	|	|	|	1.00
47.000	0.00	0.05	0.013	I	O	|	|	|	0.97
47.083	0.00	0.05	0.012	I	O	|	|	|	0.95
47.167	0.00	0.05	0.012	I	O	|	|	|	0.92
47.250	0.00	0.05	0.012	I	O	|	|	|	0.90
47.333	0.00	0.05	0.011	I	O	|	|	|	0.87
47.417	0.00	0.05	0.011	I	O	|	|	|	0.85
47.500	0.00	0.05	0.011	I	O	|	|	|	0.82
47.583	0.00	0.05	0.010	I	O	|	|	|	0.80
47.667	0.00	0.05	0.010	I	O	|	|	|	0.77
47.750	0.00	0.05	0.009	I	O	|	|	|	0.75
47.833	0.00	0.05	0.009	I	O	|	|	|	0.72
47.917	0.00	0.05	0.009	I	O	|	|	|	0.70
48.000	0.00	0.05	0.008	I	O	|	|	|	0.67
48.083	0.00	0.05	0.008	I	O	|	|	|	0.65
48.167	0.00	0.05	0.008	I	O	|	|	|	0.62
48.250	0.00	0.05	0.007	I	O	|	|	|	0.60
48.333	0.00	0.05	0.007	I	O	|	|	|	0.57
48.417	0.00	0.05	0.007	I	O	|	|	|	0.55
48.500	0.00	0.05	0.006	I	O	|	|	|	0.52
48.583	0.00	0.05	0.006	I	O	|	|	|	0.50
48.667	0.00	0.05	0.006	I	O	|	|	|	0.47
48.750	0.00	0.05	0.005	I	O	|	|	|	0.44
48.833	0.00	0.04	0.005	I	O	|	|	|	0.42
48.917	0.00	0.04	0.005	I	O	|	|	|	0.39
49.000	0.00	0.04	0.004	I	O	|	|	|	0.37
49.083	0.00	0.04	0.004	I	O	|	|	|	0.35
49.167	0.00	0.03	0.004	I	O	|	|	|	0.33
49.250	0.00	0.03	0.004	I	O	|	|	|	0.31
49.333	0.00	0.03	0.004	I	O	|	|	|	0.29
49.417	0.00	0.03	0.003	I	O	|	|	|	0.28
49.500	0.00	0.03	0.003	I	O	|	|	|	0.26
49.583	0.00	0.03	0.003	I	O	|	|	|	0.25
49.667	0.00	0.02	0.003	I	O	|	|	|	0.23
49.750	0.00	0.02	0.003	I	O	|	|	|	0.22
49.833	0.00	0.02	0.002	I	O	|	|	|	0.21
49.917	0.00	0.02	0.002	I	O	|	|	|	0.19
50.000	0.00	0.02	0.002	I	O	|	|	|	0.18
50.083	0.00	0.02	0.002	I	O	|	|	|	0.17
50.167	0.00	0.02	0.002	I	O	|	|	|	0.16
50.250	0.00	0.02	0.002	I	O	|	|	|	0.15
50.333	0.00	0.01	0.002	I	O	|	|	|	0.15
50.417	0.00	0.01	0.002	I	O	|	|	|	0.14
50.500	0.00	0.01	0.002	I	O	|	|	|	0.13
50.583	0.00	0.01	0.001	I	O	|	|	|	0.12
50.667	0.00	0.01	0.001	I	O	|	|	|	0.11

50.750	0.00	0.01	0.001	O	|	|	|	|	0.11
50.833	0.00	0.01	0.001	O	|	|	|	|	0.10
50.917	0.00	0.01	0.001	O	|	|	|	|	0.10
51.000	0.00	0.01	0.001	O	|	|	|	|	0.09
51.083	0.00	0.01	0.001	O	|	|	|	|	0.09
51.167	0.00	0.01	0.001	O	|	|	|	|	0.08
51.250	0.00	0.01	0.001	O	|	|	|	|	0.08
51.333	0.00	0.01	0.001	O	|	|	|	|	0.07
51.417	0.00	0.01	0.001	O	|	|	|	|	0.07
51.500	0.00	0.01	0.001	O	|	|	|	|	0.06
51.583	0.00	0.01	0.001	O	|	|	|	|	0.06
51.667	0.00	0.01	0.001	O	|	|	|	|	0.06
51.750	0.00	0.01	0.001	O	|	|	|	|	0.05
51.833	0.00	0.01	0.001	O	|	|	|	|	0.05
51.917	0.00	0.00	0.001	O	|	|	|	|	0.05
52.000	0.00	0.00	0.001	O	|	|	|	|	0.04
52.083	0.00	0.00	0.001	O	|	|	|	|	0.04
52.167	0.00	0.00	0.000	O	|	|	|	|	0.04
52.250	0.00	0.00	0.000	O	|	|	|	|	0.04
52.333	0.00	0.00	0.000	O	|	|	|	|	0.04
52.417	0.00	0.00	0.000	O	|	|	|	|	0.03
52.500	0.00	0.00	0.000	O	|	|	|	|	0.03
52.583	0.00	0.00	0.000	O	|	|	|	|	0.03
52.667	0.00	0.00	0.000	O	|	|	|	|	0.03
52.750	0.00	0.00	0.000	O	|	|	|	|	0.03
52.833	0.00	0.00	0.000	O	|	|	|	|	0.03
52.917	0.00	0.00	0.000	O	|	|	|	|	0.02
53.000	0.00	0.00	0.000	O	|	|	|	|	0.02
53.083	0.00	0.00	0.000	O	|	|	|	|	0.02
53.167	0.00	0.00	0.000	O	|	|	|	|	0.02
53.250	0.00	0.00	0.000	O	|	|	|	|	0.02
53.333	0.00	0.00	0.000	O	|	|	|	|	0.02
53.417	0.00	0.00	0.000	O	|	|	|	|	0.02
53.500	0.00	0.00	0.000	O	|	|	|	|	0.02
53.583	0.00	0.00	0.000	O	|	|	|	|	0.01
53.667	0.00	0.00	0.000	O	|	|	|	|	0.01
53.750	0.00	0.00	0.000	O	|	|	|	|	0.01
53.833	0.00	0.00	0.000	O	|	|	|	|	0.01
53.917	0.00	0.00	0.000	O	|	|	|	|	0.01
54.000	0.00	0.00	0.000	O	|	|	|	|	0.01
54.083	0.00	0.00	0.000	O	|	|	|	|	0.01
54.167	0.00	0.00	0.000	O	|	|	|	|	0.01
54.250	0.00	0.00	0.000	O	|	|	|	|	0.01

**********HYDROGRAPH DATA**********

Number of intervals = 651
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.051 (CFS)
Total volume = 0.201 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

AREA D1

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 07/21/25

ROUTING: BASIN D1; UNIT HYDROGRAPH D1

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARD124100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 291
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.829 (CFS)
Total volume = 0.504 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 101.000 to Point/Station 102.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 291
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.015	0.119	0.015	0.015
1.000	0.030	0.119	0.030	0.030
1.500	0.043	0.119	0.043	0.043
2.000	0.065	0.119	0.065	0.065
2.500	0.090	0.119	0.090	0.090
3.000	0.117	0.119	0.117	0.117
3.500	0.145	0.119	0.145	0.145
4.000	0.173	0.119	0.173	0.173
4.500	0.201	0.119	0.201	0.201
5.000	0.228	0.119	0.228	0.228
5.500	0.254	0.119	0.254	0.254
6.000	0.276	0.119	0.276	0.276
6.500	0.290	0.119	0.290	0.290
7.000	0.305	0.119	0.305	0.305
7.500	0.320	0.119	0.320	0.320
7.580	0.322	0.119	0.322	0.322

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.2 0.41 0.62 0.83	Depth (Ft.)
0.083	0.02	0.00	0.000	O | | | |	0.00
0.167	0.04	0.00	0.000	OI | | | |	0.01
0.250	0.05	0.00	0.001	OI | | | |	0.02
0.333	0.06	0.01	0.001	O I | | | |	0.03
0.417	0.07	0.01	0.001	O I | | | |	0.04
0.500	0.07	0.01	0.002	O I | | | |	0.06
0.583	0.07	0.02	0.002	O I | | | |	0.07
0.667	0.07	0.02	0.002	O I | | | |	0.08
0.750	0.07	0.02	0.003	O I | | | |	0.09
0.833	0.08	0.03	0.003	O I | | | |	0.11
0.917	0.09	0.03	0.004	|O I | | | |	0.12
1.000	0.10	0.03	0.004	|O I | | | |	0.14
1.083	0.09	0.04	0.004	|O I | | | |	0.15
1.167	0.08	0.04	0.005	|OI | | | |	0.16
1.250	0.07	0.04	0.005	|OI | | | |	0.17
1.333	0.07	0.04	0.005	|OI | | | |	0.18
1.417	0.07	0.04	0.005	|OI | | | |	0.18
1.500	0.07	0.04	0.006	|OI | | | |	0.19
1.583	0.07	0.05	0.006	|OI | | | |	0.20
1.667	0.07	0.05	0.006	|OI | | | |	0.20
1.750	0.07	0.05	0.006	|OI | | | |	0.21
1.833	0.08	0.05	0.006	|O I | | | |	0.21
1.917	0.09	0.05	0.007	| OI | | | |	0.22
2.000	0.10	0.06	0.007	| OI | | | |	0.23
2.083	0.10	0.06	0.007	| OI | | | |	0.24

2.167	0.10	0.06	0.007	OI				0.25
2.250	0.10	0.06	0.008	OI				0.26
2.333	0.10	0.06	0.008	OI				0.27
2.417	0.10	0.07	0.008	OI				0.27
2.500	0.10	0.07	0.008	OI				0.28
2.583	0.11	0.07	0.009	O I				0.29
2.667	0.12	0.07	0.009	O I				0.30
2.750	0.12	0.07	0.009	O I				0.31
2.833	0.12	0.08	0.010	O I				0.32
2.917	0.12	0.08	0.010	OI				0.33
3.000	0.12	0.08	0.010	OI				0.34
3.083	0.12	0.08	0.010	OI				0.35
3.167	0.12	0.09	0.011	OI				0.36
3.250	0.12	0.09	0.011	OI				0.37
3.333	0.12	0.09	0.011	OI				0.37
3.417	0.12	0.09	0.011	OI				0.38
3.500	0.12	0.09	0.012	OI				0.39
3.583	0.12	0.09	0.012	OI				0.40
3.667	0.12	0.10	0.012	OI				0.40
3.750	0.12	0.10	0.012	OI				0.41
3.833	0.13	0.10	0.012	O I				0.41
3.917	0.14	0.10	0.013	O I				0.42
4.000	0.15	0.10	0.013	O I				0.43
4.083	0.15	0.11	0.013	OI				0.44
4.167	0.15	0.11	0.014	OI				0.45
4.250	0.15	0.11	0.014	OI				0.46
4.333	0.16	0.11	0.014	O I				0.47
4.417	0.17	0.11	0.014	O I				0.48
4.500	0.17	0.12	0.015	O I				0.49
4.583	0.17	0.12	0.015	O I				0.50
4.667	0.17	0.12	0.015	O I				0.52
4.750	0.17	0.12	0.016	O I				0.53
4.833	0.18	0.12	0.016	O I				0.54
4.917	0.19	0.12	0.017	O I				0.56
5.000	0.19	0.12	0.017	O I				0.57
5.083	0.17	0.12	0.018	O I				0.59
5.167	0.15	0.12	0.018	OI				0.60
5.250	0.15	0.12	0.018	OI				0.61
5.333	0.16	0.12	0.018	O I				0.61
5.417	0.17	0.12	0.019	O I				0.62
5.500	0.17	0.12	0.019	O I				0.64
5.583	0.18	0.12	0.019	O I				0.65
5.667	0.19	0.12	0.020	O I				0.66
5.750	0.19	0.12	0.020	O I				0.68
5.833	0.19	0.12	0.021	O I				0.70
5.917	0.19	0.12	0.021	O I				0.72
6.000	0.19	0.12	0.022	O I				0.73
6.083	0.21	0.12	0.023	O I				0.75
6.167	0.22	0.12	0.023	O I				0.77
6.250	0.22	0.12	0.024	O I				0.80
6.333	0.22	0.12	0.025	O I				0.82
6.417	0.22	0.12	0.025	O I				0.84
6.500	0.22	0.12	0.026	O I				0.86

6.583	0.23	0.12	0.027	|	O	I	|	|	0.89
6.667	0.24	0.12	0.027	|	O	|I	|	|	0.92
6.750	0.24	0.12	0.028	|	O	|I	|	|	0.94
6.833	0.24	0.12	0.029	|	O	|I	|	|	0.97
6.917	0.24	0.12	0.030	|	O	|I	|	|	1.00
7.000	0.24	0.12	0.031	|	O	|I	|	|	1.03
7.083	0.24	0.12	0.032	|	O	|I	|	|	1.07
7.167	0.24	0.12	0.033	|	O	|I	|	|	1.10
7.250	0.24	0.12	0.033	|	O	|I	|	|	1.13
7.333	0.25	0.12	0.034	|	O	|I	|	|	1.17
7.417	0.27	0.12	0.035	|	O	| I	|	|	1.20
7.500	0.27	0.12	0.036	|	O	| I	|	|	1.24
7.583	0.28	0.12	0.037	|	O	| I	|	|	1.28
7.667	0.29	0.12	0.039	|	O	| I	|	|	1.33
7.750	0.29	0.12	0.040	|	O	| I	|	|	1.37
7.833	0.30	0.12	0.041	|	O	| I	|	|	1.42
7.917	0.31	0.12	0.042	|	O	| I	|	|	1.47
8.000	0.32	0.12	0.044	|	O	| I	|	|	1.51
8.083	0.34	0.12	0.045	|	O	| I	|	|	1.55
8.167	0.36	0.12	0.047	|	O	| I	|	|	1.58
8.250	0.36	0.12	0.048	|	O	| I	|	|	1.62
8.333	0.37	0.12	0.050	|	O	| I	|	|	1.66
8.417	0.37	0.12	0.052	|	O	| I	|	|	1.70
8.500	0.37	0.12	0.053	|	O	| I	|	|	1.74
8.583	0.38	0.12	0.055	|	O	| I	|	|	1.78
8.667	0.39	0.12	0.057	|	O	| I	|	|	1.82
8.750	0.39	0.12	0.059	|	O	| I|	|	|	1.86
8.833	0.40	0.12	0.061	|	O	| I|	|	|	1.90
8.917	0.41	0.12	0.063	|	O	| I|	|	|	1.95
9.000	0.41	0.12	0.065	|	O	| I|	|	|	1.99
9.083	0.44	0.12	0.067	|	O	| I	|	|	2.04
9.167	0.46	0.12	0.069	|	O	| |I	|	|	2.08
9.250	0.46	0.12	0.071	|	O	| |I	|	|	2.13
9.333	0.47	0.12	0.074	|	O	| | I	|	|	2.18
9.417	0.48	0.12	0.076	|	O	| | I	|	|	2.22
9.500	0.49	0.12	0.079	|	O	| | I	|	|	2.28
9.583	0.50	0.12	0.081	|	O	| | I	|	|	2.33
9.667	0.51	0.12	0.084	|	O	| | I	|	|	2.38
9.750	0.51	0.12	0.087	|	O	| | I	|	|	2.43
9.833	0.52	0.12	0.089	|	O	| | I	|	|	2.49
9.917	0.53	0.12	0.092	|	O	| | I	|	|	2.54
10.000	0.54	0.12	0.095	|	O	| | I	|	|	2.59
10.083	0.46	0.12	0.098	|	O	| |I	|	|	2.64
10.167	0.39	0.12	0.100	|	O	| I |	|	|	2.68
10.250	0.37	0.12	0.102	|	O	| I |	|	|	2.71
10.333	0.37	0.12	0.103	|	O	| I |	|	|	2.75
10.417	0.37	0.12	0.105	|	O	| I |	|	|	2.78
10.500	0.37	0.12	0.107	|	O	| I |	|	|	2.81
10.583	0.42	0.12	0.109	|	O	| I	|	|	2.84
10.667	0.47	0.12	0.111	|	O	| | I	|	|	2.89
10.750	0.48	0.12	0.113	|	O	| | I	|	|	2.93
10.833	0.49	0.12	0.116	|	O	| | I	|	|	2.98
10.917	0.49	0.12	0.118	|	O	| | I	|	|	3.02

11.000	0.49	0.12	0.121	|	O	|	| I |	|	3.07
11.083	0.48	0.12	0.123	|	O	|	| I |	|	3.11
11.167	0.47	0.12	0.126	|	O	|	|I |	|	3.16
11.250	0.46	0.12	0.128	|	O	|	|I |	|	3.20
11.333	0.46	0.12	0.131	|	O	|	|I |	|	3.24
11.417	0.46	0.12	0.133	|	O	|	|I |	|	3.29
11.500	0.46	0.12	0.135	|	O	|	|I |	|	3.33
11.583	0.44	0.12	0.138	|	O	|	|I |	|	3.37
11.667	0.42	0.12	0.140	|	O	|	I |	|	3.41
11.750	0.42	0.12	0.142	|	O	|	I |	|	3.44
11.833	0.42	0.12	0.144	|	O	|	I |	|	3.48
11.917	0.44	0.12	0.146	|	O	|	I |	|	3.52
12.000	0.44	0.12	0.148	|	O	|	I |	|	3.56
12.083	0.51	0.12	0.151	|	O	|	| I |	|	3.60
12.167	0.59	0.12	0.154	|	O	|	| I |	|	3.65
12.250	0.60	0.12	0.157	|	O	|	| I|	|	3.71
12.333	0.62	0.12	0.160	|	O	|	| I|	|	3.77
12.417	0.63	0.12	0.164	|	O	|	| I |	|	3.84
12.500	0.63	0.12	0.167	|	O	|	| I |	|	3.90
12.583	0.65	0.12	0.171	|	O	|	|I |	|	3.96
12.667	0.68	0.12	0.175	|	O	|	| I |	|	4.03
12.750	0.68	0.12	0.179	|	O	|	| I |	|	4.10
12.833	0.69	0.12	0.183	|	O	|	| I |	|	4.17
12.917	0.70	0.12	0.187	|	O	|	| I |	|	4.24
13.000	0.71	0.12	0.191	|	O	|	| I |	|	4.31
13.083	0.76	0.12	0.195	|	O	|	| I |	|	4.39
13.167	0.81	0.12	0.199	|	O	|	| I|	|	4.47
13.250	0.82	0.12	0.204	|	O	|	| I|	|	4.56
13.333	0.83	0.12	0.209	|	O	|	| I|	|	4.65
13.417	0.83	0.12	0.214	|	O	|	| I|	|	4.74
13.500	0.83	0.12	0.219	|	O	|	| I|	|	4.83
13.583	0.71	0.12	0.223	|	O	|	| I |	|	4.91
13.667	0.59	0.12	0.227	|	O	|	| I |	|	4.98
13.750	0.57	0.12	0.230	|	O	|	| I |	|	5.04
13.833	0.56	0.12	0.233	|	O	|	| I |	|	5.10
13.917	0.56	0.12	0.236	|	O	|	| I |	|	5.16
14.000	0.56	0.12	0.239	|	O	|	| I |	|	5.22
14.083	0.60	0.12	0.243	|	O	|	| I|	|	5.28
14.167	0.65	0.12	0.246	|	O	|	| I |	|	5.35
14.250	0.65	0.12	0.250	|	O	|	|I |	|	5.42
14.333	0.65	0.12	0.253	|	O	|	| I |	|	5.49
14.417	0.64	0.12	0.257	|	O	|	| I |	|	5.57
14.500	0.63	0.12	0.260	|	O	|	| I |	|	5.65
14.583	0.63	0.12	0.264	|	O	|	| I |	|	5.73
14.667	0.63	0.12	0.268	|	O	|	| I |	|	5.81
14.750	0.63	0.12	0.271	|	O	|	| I |	|	5.89
14.833	0.62	0.12	0.275	|	O	|	| I |	|	5.97
14.917	0.61	0.12	0.278	|	O	|	| I|	|	6.07
15.000	0.61	0.12	0.281	|	O	|	| I|	|	6.19
15.083	0.60	0.12	0.285	|	O	|	| I|	|	6.31
15.167	0.59	0.12	0.288	|	O	|	| I |	|	6.43
15.250	0.59	0.12	0.291	|	O	|	| I |	|	6.54
15.333	0.57	0.12	0.294	|	O	|	| I |	|	6.65

15.417	0.56	0.12	0.298	| O |		| I |		|	6.75
15.500	0.56	0.12	0.301	| O |		| I |		|	6.85
15.583	0.52	0.12	0.304	| O |		| I |		|	6.95
15.667	0.47	0.12	0.306	| O |		| I |		|	7.04
15.750	0.47	0.12	0.309	| O |		|I |		|	7.12
15.833	0.46	0.12	0.311	| O |		|I |		|	7.20
15.917	0.46	0.12	0.313	| O |		|I |		|	7.28
16.000	0.46	0.12	0.316	| O |		|I |		|	7.35
16.083	0.30	0.12	0.317	| O |	I	|		|	7.42
16.167	0.14	0.12	0.318	| OI |		|		|	7.44
16.250	0.11	0.12	0.318	| O |		|		|	7.44
16.333	0.10	0.12	0.318	| IO |		|		|	7.44
16.417	0.10	0.12	0.318	| IO |		|		|	7.43
16.500	0.10	0.12	0.318	| IO |		|		|	7.43
16.583	0.09	0.12	0.318	| IO |		|		|	7.42
16.667	0.08	0.12	0.317	| I O |		|		|	7.41
16.750	0.07	0.12	0.317	| I O |		|		|	7.40
16.833	0.07	0.12	0.317	| I O |		|		|	7.39
16.917	0.07	0.12	0.316	| I O |		|		|	7.38
17.000	0.07	0.12	0.316	| I O |		|		|	7.37
17.083	0.09	0.12	0.316	| IO |		|		|	7.36
17.167	0.12	0.12	0.316	| O |		|		|	7.36
17.250	0.12	0.12	0.316	| O |		|		|	7.36
17.333	0.12	0.12	0.316	| O |		|		|	7.36
17.417	0.12	0.12	0.316	| O |		|		|	7.36
17.500	0.12	0.12	0.316	| O |		|		|	7.36
17.583	0.12	0.12	0.316	| O |		|		|	7.36
17.667	0.12	0.12	0.316	| O |		|		|	7.36
17.750	0.12	0.12	0.316	| O |		|		|	7.36
17.833	0.11	0.12	0.316	| O |		|		|	7.36
17.917	0.10	0.12	0.316	| IO |		|		|	7.36
18.000	0.10	0.12	0.316	| IO |		|		|	7.35
18.083	0.10	0.12	0.315	| IO |		|		|	7.35
18.167	0.10	0.12	0.315	| IO |		|		|	7.34
18.250	0.10	0.12	0.315	| IO |		|		|	7.34
18.333	0.10	0.12	0.315	| IO |		|		|	7.33
18.417	0.10	0.12	0.315	| IO |		|		|	7.33
18.500	0.10	0.12	0.315	| IO |		|		|	7.33
18.583	0.09	0.12	0.315	| IO |		|		|	7.32
18.667	0.08	0.12	0.314	| I O |		|		|	7.31
18.750	0.07	0.12	0.314	| I O |		|		|	7.30
18.833	0.06	0.12	0.314	| I O |		|		|	7.29
18.917	0.05	0.12	0.313	|I O |		|		|	7.27
19.000	0.05	0.12	0.313	|I O |		|		|	7.26
19.083	0.06	0.12	0.312	| I O |		|		|	7.24
19.167	0.07	0.12	0.312	| I O |		|		|	7.23
19.250	0.07	0.12	0.312	| I O |		|		|	7.22
19.333	0.08	0.12	0.311	| IO |		|		|	7.21
19.417	0.09	0.12	0.311	| IO |		|		|	7.20
19.500	0.10	0.12	0.311	| IO |		|		|	7.20
19.583	0.09	0.12	0.311	| IO |		|		|	7.19
19.667	0.08	0.12	0.311	| I O |		|		|	7.18
19.750	0.07	0.12	0.310	| I O |		|		|	7.17

19.833	0.06	0.12	0.310	| I O	|	|	|	7.16
19.917	0.05	0.12	0.309	|I O	|	|	|	7.15
20.000	0.05	0.12	0.309	|I O	|	|	|	7.13
20.083	0.06	0.12	0.309	| I O	|	|	|	7.12
20.167	0.07	0.12	0.308	| I O	|	|	|	7.10
20.250	0.07	0.12	0.308	| I O	|	|	|	7.09
20.333	0.07	0.12	0.307	| I O	|	|	|	7.08
20.417	0.07	0.12	0.307	| I O	|	|	|	7.07
20.500	0.07	0.12	0.307	| I O	|	|	|	7.06
20.583	0.07	0.12	0.307	| I O	|	|	|	7.05
20.667	0.07	0.12	0.306	| I O	|	|	|	7.04
20.750	0.07	0.12	0.306	| I O	|	|	|	7.03
20.833	0.06	0.12	0.306	| I O	|	|	|	7.02
20.917	0.05	0.12	0.305	|I O	|	|	|	7.00
21.000	0.05	0.12	0.305	|I O	|	|	|	6.99
21.083	0.06	0.12	0.304	| I O	|	|	|	6.97
21.167	0.07	0.12	0.304	| I O	|	|	|	6.96
21.250	0.07	0.12	0.304	| I O	|	|	|	6.95
21.333	0.06	0.12	0.303	| I O	|	|	|	6.94
21.417	0.05	0.12	0.303	|I O	|	|	|	6.92
21.500	0.05	0.12	0.302	|I O	|	|	|	6.91
21.583	0.06	0.12	0.302	| I O	|	|	|	6.89
21.667	0.07	0.12	0.301	| I O	|	|	|	6.88
21.750	0.07	0.12	0.301	| I O	|	|	|	6.87
21.833	0.06	0.12	0.301	| I O	|	|	|	6.86
21.917	0.05	0.12	0.300	|I O	|	|	|	6.84
22.000	0.05	0.12	0.300	|I O	|	|	|	6.83
22.083	0.06	0.12	0.299	| I O	|	|	|	6.81
22.167	0.07	0.12	0.299	| I O	|	|	|	6.80
22.250	0.07	0.12	0.299	| I O	|	|	|	6.79
22.333	0.06	0.12	0.298	| I O	|	|	|	6.78
22.417	0.05	0.12	0.298	|I O	|	|	|	6.76
22.500	0.05	0.12	0.297	|I O	|	|	|	6.75
22.583	0.05	0.12	0.297	|I O	|	|	|	6.73
22.667	0.05	0.12	0.297	|I O	|	|	|	6.72
22.750	0.05	0.12	0.296	|I O	|	|	|	6.70
22.833	0.05	0.12	0.296	|I O	|	|	|	6.68
22.917	0.05	0.12	0.295	|I O	|	|	|	6.67
23.000	0.05	0.12	0.295	|I O	|	|	|	6.65
23.083	0.05	0.12	0.294	|I O	|	|	|	6.64
23.167	0.05	0.12	0.294	|I O	|	|	|	6.62
23.250	0.05	0.12	0.293	|I O	|	|	|	6.60
23.333	0.05	0.12	0.293	|I O	|	|	|	6.59
23.417	0.05	0.12	0.292	|I O	|	|	|	6.57
23.500	0.05	0.12	0.292	|I O	|	|	|	6.56
23.583	0.05	0.12	0.291	|I O	|	|	|	6.54
23.667	0.05	0.12	0.291	|I O	|	|	|	6.52
23.750	0.05	0.12	0.290	|I O	|	|	|	6.51
23.833	0.05	0.12	0.290	|I O	|	|	|	6.49
23.917	0.05	0.12	0.289	|I O	|	|	|	6.47
24.000	0.05	0.12	0.289	|I O	|	|	|	6.46
24.083	0.03	0.12	0.288	|I O	|	|	|	6.44
24.167	0.01	0.12	0.287	I O	|	|	|	6.41

24.250	0.00	0.12	0.287	I	O	|	|	|	|	6.38
24.333	0.00	0.12	0.286	I	O	|	|	|	|	6.35
24.417	0.00	0.12	0.285	I	O	|	|	|	|	6.32
24.500	0.00	0.12	0.284	I	O	|	|	|	|	6.29
24.583	0.00	0.12	0.283	I	O	|	|	|	|	6.27
24.667	0.00	0.12	0.283	I	O	|	|	|	|	6.24
24.750	0.00	0.12	0.282	I	O	|	|	|	|	6.21
24.833	0.00	0.12	0.281	I	O	|	|	|	|	6.18
24.917	0.00	0.12	0.280	I	O	|	|	|	|	6.15
25.000	0.00	0.12	0.279	I	O	|	|	|	|	6.12
25.083	0.00	0.12	0.279	I	O	|	|	|	|	6.09
25.167	0.00	0.12	0.278	I	O	|	|	|	|	6.06
25.250	0.00	0.12	0.277	I	O	|	|	|	|	6.03
25.333	0.00	0.12	0.276	I	O	|	|	|	|	6.00
25.417	0.00	0.12	0.275	I	O	|	|	|	|	5.98
25.500	0.00	0.12	0.274	I	O	|	|	|	|	5.96
25.583	0.00	0.12	0.274	I	O	|	|	|	|	5.95
25.667	0.00	0.12	0.273	I	O	|	|	|	|	5.93
25.750	0.00	0.12	0.272	I	O	|	|	|	|	5.91
25.833	0.00	0.12	0.271	I	O	|	|	|	|	5.89
25.917	0.00	0.12	0.270	I	O	|	|	|	|	5.87
26.000	0.00	0.12	0.269	I	O	|	|	|	|	5.85
26.083	0.00	0.12	0.269	I	O	|	|	|	|	5.83
26.167	0.00	0.12	0.268	I	O	|	|	|	|	5.81
26.250	0.00	0.12	0.267	I	O	|	|	|	|	5.80
26.333	0.00	0.12	0.266	I	O	|	|	|	|	5.78
26.417	0.00	0.12	0.265	I	O	|	|	|	|	5.76
26.500	0.00	0.12	0.265	I	O	|	|	|	|	5.74
26.583	0.00	0.12	0.264	I	O	|	|	|	|	5.72
26.667	0.00	0.12	0.263	I	O	|	|	|	|	5.70
26.750	0.00	0.12	0.262	I	O	|	|	|	|	5.68
26.833	0.00	0.12	0.261	I	O	|	|	|	|	5.67
26.917	0.00	0.12	0.260	I	O	|	|	|	|	5.65
27.000	0.00	0.12	0.260	I	O	|	|	|	|	5.63
27.083	0.00	0.12	0.259	I	O	|	|	|	|	5.61
27.167	0.00	0.12	0.258	I	O	|	|	|	|	5.59
27.250	0.00	0.12	0.257	I	O	|	|	|	|	5.57
27.333	0.00	0.12	0.256	I	O	|	|	|	|	5.55
27.417	0.00	0.12	0.256	I	O	|	|	|	|	5.54
27.500	0.00	0.12	0.255	I	O	|	|	|	|	5.52
27.583	0.00	0.12	0.254	I	O	|	|	|	|	5.50
27.667	0.00	0.12	0.253	I	O	|	|	|	|	5.48
27.750	0.00	0.12	0.252	I	O	|	|	|	|	5.47
27.833	0.00	0.12	0.251	I	O	|	|	|	|	5.45
27.917	0.00	0.12	0.251	I	O	|	|	|	|	5.44
28.000	0.00	0.12	0.250	I	O	|	|	|	|	5.42
28.083	0.00	0.12	0.249	I	O	|	|	|	|	5.40
28.167	0.00	0.12	0.248	I	O	|	|	|	|	5.39
28.250	0.00	0.12	0.247	I	O	|	|	|	|	5.37
28.333	0.00	0.12	0.247	I	O	|	|	|	|	5.36
28.417	0.00	0.12	0.246	I	O	|	|	|	|	5.34
28.500	0.00	0.12	0.245	I	O	|	|	|	|	5.33
28.583	0.00	0.12	0.244	I	O	|	|	|	|	5.31

28.667	0.00	0.12	0.243	I	O	|	|	|	|	5.29
28.750	0.00	0.12	0.242	I	O	|	|	|	|	5.28
28.833	0.00	0.12	0.242	I	O	|	|	|	|	5.26
28.917	0.00	0.12	0.241	I	O	|	|	|	|	5.25
29.000	0.00	0.12	0.240	I	O	|	|	|	|	5.23
29.083	0.00	0.12	0.239	I	O	|	|	|	|	5.21
29.167	0.00	0.12	0.238	I	O	|	|	|	|	5.20
29.250	0.00	0.12	0.238	I	O	|	|	|	|	5.18
29.333	0.00	0.12	0.237	I	O	|	|	|	|	5.17
29.417	0.00	0.12	0.236	I	O	|	|	|	|	5.15
29.500	0.00	0.12	0.235	I	O	|	|	|	|	5.14
29.583	0.00	0.12	0.234	I	O	|	|	|	|	5.12
29.667	0.00	0.12	0.233	I	O	|	|	|	|	5.10
29.750	0.00	0.12	0.233	I	O	|	|	|	|	5.09
29.833	0.00	0.12	0.232	I	O	|	|	|	|	5.07
29.917	0.00	0.12	0.231	I	O	|	|	|	|	5.06
30.000	0.00	0.12	0.230	I	O	|	|	|	|	5.04
30.083	0.00	0.12	0.229	I	O	|	|	|	|	5.03
30.167	0.00	0.12	0.229	I	O	|	|	|	|	5.01
30.250	0.00	0.12	0.228	I	O	|	|	|	|	4.99
30.333	0.00	0.12	0.227	I	O	|	|	|	|	4.98
30.417	0.00	0.12	0.226	I	O	|	|	|	|	4.96
30.500	0.00	0.12	0.225	I	O	|	|	|	|	4.95
30.583	0.00	0.12	0.224	I	O	|	|	|	|	4.93
30.667	0.00	0.12	0.224	I	O	|	|	|	|	4.92
30.750	0.00	0.12	0.223	I	O	|	|	|	|	4.90
30.833	0.00	0.12	0.222	I	O	|	|	|	|	4.89
30.917	0.00	0.12	0.221	I	O	|	|	|	|	4.87
31.000	0.00	0.12	0.220	I	O	|	|	|	|	4.86
31.083	0.00	0.12	0.220	I	O	|	|	|	|	4.84
31.167	0.00	0.12	0.219	I	O	|	|	|	|	4.83
31.250	0.00	0.12	0.218	I	O	|	|	|	|	4.81
31.333	0.00	0.12	0.217	I	O	|	|	|	|	4.80
31.417	0.00	0.12	0.216	I	O	|	|	|	|	4.78
31.500	0.00	0.12	0.215	I	O	|	|	|	|	4.77
31.583	0.00	0.12	0.215	I	O	|	|	|	|	4.75
31.667	0.00	0.12	0.214	I	O	|	|	|	|	4.74
31.750	0.00	0.12	0.213	I	O	|	|	|	|	4.72
31.833	0.00	0.12	0.212	I	O	|	|	|	|	4.71
31.917	0.00	0.12	0.211	I	O	|	|	|	|	4.69
32.000	0.00	0.12	0.210	I	O	|	|	|	|	4.68
32.083	0.00	0.12	0.210	I	O	|	|	|	|	4.66
32.167	0.00	0.12	0.209	I	O	|	|	|	|	4.65
32.250	0.00	0.12	0.208	I	O	|	|	|	|	4.63
32.333	0.00	0.12	0.207	I	O	|	|	|	|	4.62
32.417	0.00	0.12	0.206	I	O	|	|	|	|	4.60
32.500	0.00	0.12	0.206	I	O	|	|	|	|	4.58
32.583	0.00	0.12	0.205	I	O	|	|	|	|	4.57
32.667	0.00	0.12	0.204	I	O	|	|	|	|	4.55
32.750	0.00	0.12	0.203	I	O	|	|	|	|	4.54
32.833	0.00	0.12	0.202	I	O	|	|	|	|	4.52
32.917	0.00	0.12	0.201	I	O	|	|	|	|	4.51
33.000	0.00	0.12	0.201	I	O	|	|	|	|	4.49

33.083	0.00	0.12	0.200	I	O	|	|	|	|	4.48
33.167	0.00	0.12	0.199	I	O	|	|	|	|	4.46
33.250	0.00	0.12	0.198	I	O	|	|	|	|	4.45
33.333	0.00	0.12	0.197	I	O	|	|	|	|	4.44
33.417	0.00	0.12	0.197	I	O	|	|	|	|	4.42
33.500	0.00	0.12	0.196	I	O	|	|	|	|	4.41
33.583	0.00	0.12	0.195	I	O	|	|	|	|	4.39
33.667	0.00	0.12	0.194	I	O	|	|	|	|	4.38
33.750	0.00	0.12	0.193	I	O	|	|	|	|	4.36
33.833	0.00	0.12	0.192	I	O	|	|	|	|	4.35
33.917	0.00	0.12	0.192	I	O	|	|	|	|	4.33
34.000	0.00	0.12	0.191	I	O	|	|	|	|	4.32
34.083	0.00	0.12	0.190	I	O	|	|	|	|	4.30
34.167	0.00	0.12	0.189	I	O	|	|	|	|	4.29
34.250	0.00	0.12	0.188	I	O	|	|	|	|	4.27
34.333	0.00	0.12	0.188	I	O	|	|	|	|	4.26
34.417	0.00	0.12	0.187	I	O	|	|	|	|	4.25
34.500	0.00	0.12	0.186	I	O	|	|	|	|	4.23
34.583	0.00	0.12	0.185	I	O	|	|	|	|	4.22
34.667	0.00	0.12	0.184	I	O	|	|	|	|	4.20
34.750	0.00	0.12	0.183	I	O	|	|	|	|	4.19
34.833	0.00	0.12	0.183	I	O	|	|	|	|	4.17
34.917	0.00	0.12	0.182	I	O	|	|	|	|	4.16
35.000	0.00	0.12	0.181	I	O	|	|	|	|	4.14
35.083	0.00	0.12	0.180	I	O	|	|	|	|	4.13
35.167	0.00	0.12	0.179	I	O	|	|	|	|	4.11
35.250	0.00	0.12	0.179	I	O	|	|	|	|	4.10
35.333	0.00	0.12	0.178	I	O	|	|	|	|	4.08
35.417	0.00	0.12	0.177	I	O	|	|	|	|	4.07
35.500	0.00	0.12	0.176	I	O	|	|	|	|	4.05
35.583	0.00	0.12	0.175	I	O	|	|	|	|	4.04
35.667	0.00	0.12	0.174	I	O	|	|	|	|	4.03
35.750	0.00	0.12	0.174	I	O	|	|	|	|	4.01
35.833	0.00	0.12	0.173	I	O	|	|	|	|	4.00
35.917	0.00	0.12	0.172	I	O	|	|	|	|	3.98
36.000	0.00	0.12	0.171	I	O	|	|	|	|	3.97
36.083	0.00	0.12	0.170	I	O	|	|	|	|	3.95
36.167	0.00	0.12	0.170	I	O	|	|	|	|	3.94
36.250	0.00	0.12	0.169	I	O	|	|	|	|	3.92
36.333	0.00	0.12	0.168	I	O	|	|	|	|	3.91
36.417	0.00	0.12	0.167	I	O	|	|	|	|	3.89
36.500	0.00	0.12	0.166	I	O	|	|	|	|	3.88
36.583	0.00	0.12	0.165	I	O	|	|	|	|	3.86
36.667	0.00	0.12	0.165	I	O	|	|	|	|	3.85
36.750	0.00	0.12	0.164	I	O	|	|	|	|	3.84
36.833	0.00	0.12	0.163	I	O	|	|	|	|	3.82
36.917	0.00	0.12	0.162	I	O	|	|	|	|	3.81
37.000	0.00	0.12	0.161	I	O	|	|	|	|	3.79
37.083	0.00	0.12	0.160	I	O	|	|	|	|	3.78
37.167	0.00	0.12	0.160	I	O	|	|	|	|	3.76
37.250	0.00	0.12	0.159	I	O	|	|	|	|	3.75
37.333	0.00	0.12	0.158	I	O	|	|	|	|	3.73
37.417	0.00	0.12	0.157	I	O	|	|	|	|	3.72

37.500	0.00	0.12	0.156	I	O	|	|	|	|	3.70
37.583	0.00	0.12	0.156	I	O	|	|	|	|	3.69
37.667	0.00	0.12	0.155	I	O	|	|	|	|	3.67
37.750	0.00	0.12	0.154	I	O	|	|	|	|	3.66
37.833	0.00	0.12	0.153	I	O	|	|	|	|	3.65
37.917	0.00	0.12	0.152	I	O	|	|	|	|	3.63
38.000	0.00	0.12	0.151	I	O	|	|	|	|	3.62
38.083	0.00	0.12	0.151	I	O	|	|	|	|	3.60
38.167	0.00	0.12	0.150	I	O	|	|	|	|	3.59
38.250	0.00	0.12	0.149	I	O	|	|	|	|	3.57
38.333	0.00	0.12	0.148	I	O	|	|	|	|	3.56
38.417	0.00	0.12	0.147	I	O	|	|	|	|	3.54
38.500	0.00	0.12	0.147	I	O	|	|	|	|	3.53
38.583	0.00	0.12	0.146	I	O	|	|	|	|	3.51
38.667	0.00	0.12	0.145	I	O	|	|	|	|	3.50
38.750	0.00	0.12	0.144	I	O	|	|	|	|	3.48
38.833	0.00	0.12	0.143	I	O	|	|	|	|	3.47
38.917	0.00	0.12	0.142	I	O	|	|	|	|	3.45
39.000	0.00	0.12	0.142	I	O	|	|	|	|	3.44
39.083	0.00	0.12	0.141	I	O	|	|	|	|	3.43
39.167	0.00	0.12	0.140	I	O	|	|	|	|	3.41
39.250	0.00	0.12	0.139	I	O	|	|	|	|	3.40
39.333	0.00	0.12	0.138	I	O	|	|	|	|	3.38
39.417	0.00	0.12	0.138	I	O	|	|	|	|	3.37
39.500	0.00	0.12	0.137	I	O	|	|	|	|	3.35
39.583	0.00	0.12	0.136	I	O	|	|	|	|	3.34
39.667	0.00	0.12	0.135	I	O	|	|	|	|	3.32
39.750	0.00	0.12	0.134	I	O	|	|	|	|	3.31
39.833	0.00	0.12	0.133	I	O	|	|	|	|	3.29
39.917	0.00	0.12	0.133	I	O	|	|	|	|	3.28
40.000	0.00	0.12	0.132	I	O	|	|	|	|	3.26
40.083	0.00	0.12	0.131	I	O	|	|	|	|	3.25
40.167	0.00	0.12	0.130	I	O	|	|	|	|	3.24
40.250	0.00	0.12	0.129	I	O	|	|	|	|	3.22
40.333	0.00	0.12	0.129	I	O	|	|	|	|	3.21
40.417	0.00	0.12	0.128	I	O	|	|	|	|	3.19
40.500	0.00	0.12	0.127	I	O	|	|	|	|	3.18
40.583	0.00	0.12	0.126	I	O	|	|	|	|	3.16
40.667	0.00	0.12	0.125	I	O	|	|	|	|	3.15
40.750	0.00	0.12	0.124	I	O	|	|	|	|	3.13
40.833	0.00	0.12	0.124	I	O	|	|	|	|	3.12
40.917	0.00	0.12	0.123	I	O	|	|	|	|	3.10
41.000	0.00	0.12	0.122	I	O	|	|	|	|	3.09
41.083	0.00	0.12	0.121	I	O	|	|	|	|	3.07
41.167	0.00	0.12	0.120	I	O	|	|	|	|	3.06
41.250	0.00	0.12	0.120	I	O	|	|	|	|	3.04
41.333	0.00	0.12	0.119	I	O	|	|	|	|	3.03
41.417	0.00	0.12	0.118	I	O	|	|	|	|	3.02
41.500	0.00	0.12	0.117	I	O	|	|	|	|	3.00
41.583	0.00	0.12	0.116	I	O	|	|	|	|	2.99
41.667	0.00	0.12	0.115	I	O	|	|	|	|	2.97
41.750	0.00	0.12	0.115	I	O	|	|	|	|	2.96
41.833	0.00	0.12	0.114	I	O	|	|	|	|	2.94

41.917	0.00	0.12	0.113	I	O	|	|	|	|	2.93
42.000	0.00	0.12	0.112	I	O	|	|	|	|	2.91
42.083	0.00	0.12	0.111	I	O	|	|	|	|	2.89
42.167	0.00	0.12	0.111	I	O	|	|	|	|	2.88
42.250	0.00	0.12	0.110	I	O	|	|	|	|	2.86
42.333	0.00	0.12	0.109	I	O	|	|	|	|	2.85
42.417	0.00	0.12	0.108	I	O	|	|	|	|	2.83
42.500	0.00	0.12	0.107	I	O	|	|	|	|	2.82
42.583	0.00	0.12	0.106	I	O	|	|	|	|	2.80
42.667	0.00	0.12	0.106	I	O	|	|	|	|	2.79
42.750	0.00	0.12	0.105	I	O	|	|	|	|	2.77
42.833	0.00	0.12	0.104	I	O	|	|	|	|	2.76
42.917	0.00	0.12	0.103	I	O	|	|	|	|	2.74
43.000	0.00	0.12	0.102	I	O	|	|	|	|	2.73
43.083	0.00	0.12	0.101	I	O	|	|	|	|	2.71
43.167	0.00	0.12	0.101	I	O	|	|	|	|	2.70
43.250	0.00	0.12	0.100	I	O	|	|	|	|	2.68
43.333	0.00	0.12	0.099	I	O	|	|	|	|	2.67
43.417	0.00	0.12	0.098	I	O	|	|	|	|	2.65
43.500	0.00	0.12	0.097	I	O	|	|	|	|	2.64
43.583	0.00	0.12	0.097	I	O	|	|	|	|	2.62
43.667	0.00	0.12	0.096	I	O	|	|	|	|	2.61
43.750	0.00	0.12	0.095	I	O	|	|	|	|	2.59
43.833	0.00	0.12	0.094	I	O	|	|	|	|	2.58
43.917	0.00	0.12	0.093	I	O	|	|	|	|	2.56
44.000	0.00	0.12	0.092	I	O	|	|	|	|	2.55
44.083	0.00	0.12	0.092	I	O	|	|	|	|	2.53
44.167	0.00	0.12	0.091	I	O	|	|	|	|	2.52
44.250	0.00	0.12	0.090	I	O	|	|	|	|	2.50
44.333	0.00	0.12	0.089	I	O	|	|	|	|	2.48
44.417	0.00	0.12	0.088	I	O	|	|	|	|	2.47
44.500	0.00	0.12	0.088	I	O	|	|	|	|	2.45
44.583	0.00	0.12	0.087	I	O	|	|	|	|	2.43
44.667	0.00	0.12	0.086	I	O	|	|	|	|	2.42
44.750	0.00	0.12	0.085	I	O	|	|	|	|	2.40
44.833	0.00	0.12	0.084	I	O	|	|	|	|	2.39
44.917	0.00	0.12	0.083	I	O	|	|	|	|	2.37
45.000	0.00	0.12	0.083	I	O	|	|	|	|	2.35
45.083	0.00	0.12	0.082	I	O	|	|	|	|	2.34
45.167	0.00	0.12	0.081	I	O	|	|	|	|	2.32
45.250	0.00	0.12	0.080	I	O	|	|	|	|	2.30
45.333	0.00	0.12	0.079	I	O	|	|	|	|	2.29
45.417	0.00	0.12	0.079	I	O	|	|	|	|	2.27
45.500	0.00	0.12	0.078	I	O	|	|	|	|	2.25
45.583	0.00	0.12	0.077	I	O	|	|	|	|	2.24
45.667	0.00	0.12	0.076	I	O	|	|	|	|	2.22
45.750	0.00	0.12	0.075	I	O	|	|	|	|	2.21
45.833	0.00	0.12	0.074	I	O	|	|	|	|	2.19
45.917	0.00	0.12	0.074	I	O	|	|	|	|	2.17
46.000	0.00	0.12	0.073	I	O	|	|	|	|	2.16
46.083	0.00	0.12	0.072	I	O	|	|	|	|	2.14
46.167	0.00	0.12	0.071	I	O	|	|	|	|	2.12
46.250	0.00	0.12	0.070	I	O	|	|	|	|	2.11

46.333	0.00	0.12	0.070	I	O	|	|	|	|	2.09
46.417	0.00	0.12	0.069	I	O	|	|	|	|	2.07
46.500	0.00	0.12	0.068	I	O	|	|	|	|	2.06
46.583	0.00	0.12	0.067	I	O	|	|	|	|	2.04
46.667	0.00	0.12	0.066	I	O	|	|	|	|	2.02
46.750	0.00	0.12	0.065	I	O	|	|	|	|	2.01
46.833	0.00	0.12	0.065	I	O	|	|	|	|	1.99
46.917	0.00	0.12	0.064	I	O	|	|	|	|	1.97
47.000	0.00	0.12	0.063	I	O	|	|	|	|	1.95
47.083	0.00	0.12	0.062	I	O	|	|	|	|	1.94
47.167	0.00	0.12	0.061	I	O	|	|	|	|	1.92
47.250	0.00	0.12	0.061	I	O	|	|	|	|	1.90
47.333	0.00	0.12	0.060	I	O	|	|	|	|	1.88
47.417	0.00	0.12	0.059	I	O	|	|	|	|	1.86
47.500	0.00	0.12	0.058	I	O	|	|	|	|	1.84
47.583	0.00	0.12	0.057	I	O	|	|	|	|	1.82
47.667	0.00	0.12	0.056	I	O	|	|	|	|	1.80
47.750	0.00	0.12	0.056	I	O	|	|	|	|	1.79
47.833	0.00	0.12	0.055	I	O	|	|	|	|	1.77
47.917	0.00	0.12	0.054	I	O	|	|	|	|	1.75
48.000	0.00	0.12	0.053	I	O	|	|	|	|	1.73
48.083	0.00	0.12	0.052	I	O	|	|	|	|	1.71
48.167	0.00	0.12	0.051	I	O	|	|	|	|	1.69
48.250	0.00	0.12	0.051	I	O	|	|	|	|	1.67
48.333	0.00	0.12	0.050	I	O	|	|	|	|	1.66
48.417	0.00	0.12	0.049	I	O	|	|	|	|	1.64
48.500	0.00	0.12	0.048	I	O	|	|	|	|	1.62
48.583	0.00	0.12	0.047	I	O	|	|	|	|	1.60
48.667	0.00	0.12	0.047	I	O	|	|	|	|	1.58
48.750	0.00	0.12	0.046	I	O	|	|	|	|	1.56
48.833	0.00	0.12	0.045	I	O	|	|	|	|	1.54
48.917	0.00	0.12	0.044	I	O	|	|	|	|	1.53
49.000	0.00	0.12	0.043	I	O	|	|	|	|	1.51
49.083	0.00	0.12	0.042	I	O	|	|	|	|	1.48
49.167	0.00	0.12	0.042	I	O	|	|	|	|	1.45
49.250	0.00	0.12	0.041	I	O	|	|	|	|	1.42
49.333	0.00	0.12	0.040	I	O	|	|	|	|	1.39
49.417	0.00	0.12	0.039	I	O	|	|	|	|	1.35
49.500	0.00	0.12	0.038	I	O	|	|	|	|	1.32
49.583	0.00	0.12	0.038	I	O	|	|	|	|	1.29
49.667	0.00	0.12	0.037	I	O	|	|	|	|	1.26
49.750	0.00	0.12	0.036	I	O	|	|	|	|	1.23
49.833	0.00	0.12	0.035	I	O	|	|	|	|	1.20
49.917	0.00	0.12	0.034	I	O	|	|	|	|	1.16
50.000	0.00	0.12	0.033	I	O	|	|	|	|	1.13
50.083	0.00	0.12	0.033	I	O	|	|	|	|	1.10
50.167	0.00	0.12	0.032	I	O	|	|	|	|	1.07
50.250	0.00	0.12	0.031	I	O	|	|	|	|	1.04
50.333	0.00	0.12	0.030	I	O	|	|	|	|	1.01
50.417	0.00	0.12	0.029	I	O	|	|	|	|	0.98
50.500	0.00	0.12	0.029	I	O	|	|	|	|	0.95
50.583	0.00	0.12	0.028	I	O	|	|	|	|	0.92
50.667	0.00	0.12	0.027	I	O	|	|	|	|	0.90

50.750	0.00	0.12	0.026	I	O	|	|	|	0.87
50.833	0.00	0.12	0.025	I	O	|	|	|	0.84
50.917	0.00	0.12	0.024	I	O	|	|	|	0.82
51.000	0.00	0.12	0.024	I	O	|	|	|	0.79
51.083	0.00	0.12	0.023	I	O	|	|	|	0.76
51.167	0.00	0.12	0.022	I	O	|	|	|	0.73
51.250	0.00	0.12	0.021	I	O	|	|	|	0.71
51.333	0.00	0.12	0.020	I	O	|	|	|	0.68
51.417	0.00	0.12	0.020	I	O	|	|	|	0.65
51.500	0.00	0.12	0.019	I	O	|	|	|	0.62
51.583	0.00	0.12	0.018	I	O	|	|	|	0.60
51.667	0.00	0.12	0.017	I	O	|	|	|	0.57
51.750	0.00	0.12	0.016	I	O	|	|	|	0.54
51.833	0.00	0.12	0.015	I	O	|	|	|	0.51
51.917	0.00	0.12	0.015	I	O	|	|	|	0.49
52.000	0.00	0.11	0.014	I	O	|	|	|	0.46
52.083	0.00	0.10	0.013	I	O	|	|	|	0.44
52.167	0.00	0.10	0.012	I	O	|	|	|	0.41
52.250	0.00	0.09	0.012	I	O	|	|	|	0.39
52.333	0.00	0.09	0.011	I	O	|	|	|	0.37
52.417	0.00	0.08	0.011	I	O	|	|	|	0.35
52.500	0.00	0.08	0.010	I	O	|	|	|	0.33
52.583	0.00	0.07	0.009	I	O	|	|	|	0.31
52.667	0.00	0.07	0.009	I	O	|	|	|	0.30
52.750	0.00	0.07	0.008	I	O	|	|	|	0.28
52.833	0.00	0.06	0.008	I	O	|	|	|	0.27
52.917	0.00	0.06	0.008	I	O	|	|	|	0.25
53.000	0.00	0.06	0.007	I	O	|	|	|	0.24
53.083	0.00	0.05	0.007	I	O	|	|	|	0.23
53.167	0.00	0.05	0.006	I	O	|	|	|	0.21
53.250	0.00	0.05	0.006	I	O	|	|	|	0.20
53.333	0.00	0.05	0.006	I	O	|	|	|	0.19
53.417	0.00	0.04	0.005	I	O	|	|	|	0.18
53.500	0.00	0.04	0.005	I	O	|	|	|	0.17
53.583	0.00	0.04	0.005	I	O	|	|	|	0.16
53.667	0.00	0.04	0.005	I	O	|	|	|	0.15
53.750	0.00	0.03	0.004	I	O	|	|	|	0.15
53.833	0.00	0.03	0.004	I	O	|	|	|	0.14
53.917	0.00	0.03	0.004	I	O	|	|	|	0.13
54.000	0.00	0.03	0.004	I	O	|	|	|	0.12
54.083	0.00	0.03	0.004	I	O	|	|	|	0.12
54.167	0.00	0.03	0.003	I	O	|	|	|	0.11
54.250	0.00	0.03	0.003	O		|	|	|	0.11
54.333	0.00	0.02	0.003	O		|	|	|	0.10
54.417	0.00	0.02	0.003	O		|	|	|	0.09
54.500	0.00	0.02	0.003	O		|	|	|	0.09
54.583	0.00	0.02	0.003	O		|	|	|	0.08
54.667	0.00	0.02	0.002	O		|	|	|	0.08
54.750	0.00	0.02	0.002	O		|	|	|	0.08
54.833	0.00	0.02	0.002	O		|	|	|	0.07
54.917	0.00	0.02	0.002	O		|	|	|	0.07
55.000	0.00	0.02	0.002	O		|	|	|	0.06
55.083	0.00	0.01	0.002	O		|	|	|	0.06

55.167	0.00	0.01	0.002	O	|	|	|	|	0.06
55.250	0.00	0.01	0.002	O	|	|	|	|	0.05
55.333	0.00	0.01	0.002	O	|	|	|	|	0.05
55.417	0.00	0.01	0.001	O	|	|	|	|	0.05
55.500	0.00	0.01	0.001	O	|	|	|	|	0.05
55.583	0.00	0.01	0.001	O	|	|	|	|	0.04
55.667	0.00	0.01	0.001	O	|	|	|	|	0.04
55.750	0.00	0.01	0.001	O	|	|	|	|	0.04
55.833	0.00	0.01	0.001	O	|	|	|	|	0.04
55.917	0.00	0.01	0.001	O	|	|	|	|	0.04
56.000	0.00	0.01	0.001	O	|	|	|	|	0.03
56.083	0.00	0.01	0.001	O	|	|	|	|	0.03
56.167	0.00	0.01	0.001	O	|	|	|	|	0.03
56.250	0.00	0.01	0.001	O	|	|	|	|	0.03
56.333	0.00	0.01	0.001	O	|	|	|	|	0.03
56.417	0.00	0.01	0.001	O	|	|	|	|	0.03
56.500	0.00	0.01	0.001	O	|	|	|	|	0.02
56.583	0.00	0.01	0.001	O	|	|	|	|	0.02
56.667	0.00	0.01	0.001	O	|	|	|	|	0.02
56.750	0.00	0.00	0.001	O	|	|	|	|	0.02
56.833	0.00	0.00	0.001	O	|	|	|	|	0.02
56.917	0.00	0.00	0.001	O	|	|	|	|	0.02
57.000	0.00	0.00	0.001	O	|	|	|	|	0.02
57.083	0.00	0.00	0.000	O	|	|	|	|	0.02
57.167	0.00	0.00	0.000	O	|	|	|	|	0.02
57.250	0.00	0.00	0.000	O	|	|	|	|	0.01
57.333	0.00	0.00	0.000	O	|	|	|	|	0.01
57.417	0.00	0.00	0.000	O	|	|	|	|	0.01
57.500	0.00	0.00	0.000	O	|	|	|	|	0.01
57.583	0.00	0.00	0.000	O	|	|	|	|	0.01
57.667	0.00	0.00	0.000	O	|	|	|	|	0.01
57.750	0.00	0.00	0.000	O	|	|	|	|	0.01
57.833	0.00	0.00	0.000	O	|	|	|	|	0.01
57.917	0.00	0.00	0.000	O	|	|	|	|	0.01
58.000	0.00	0.00	0.000	O	|	|	|	|	0.01
58.083	0.00	0.00	0.000	O	|	|	|	|	0.01
58.167	0.00	0.00	0.000	O	|	|	|	|	0.01
58.250	0.00	0.00	0.000	O	|	|	|	|	0.01
58.333	0.00	0.00	0.000	O	|	|	|	|	0.01
58.417	0.00	0.00	0.000	O	|	|	|	|	0.01
58.500	0.00	0.00	0.000	O	|	|	|	|	0.01
58.583	0.00	0.00	0.000	O	|	|	|	|	0.01
58.667	0.00	0.00	0.000	O	|	|	|	|	0.01
58.750	0.00	0.00	0.000	O	|	|	|	|	0.01
58.833	0.00	0.00	0.000	O	|	|	|	|	0.01
58.917	0.00	0.00	0.000	O	|	|	|	|	0.00
59.000	0.00	0.00	0.000	O	|	|	|	|	0.00
59.083	0.00	0.00	0.000	O	|	|	|	|	0.00
59.167	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 710

Time interval = 5.0 (Min.)

```
      Maximum/Peak flow rate =        0.119 (CFS)
      Total volume =       0.503 (Ac.Ft)
   Status of hydrographs being held in storage
            Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
   Peak (CFS)      0.000     0.000     0.000     0.000     0.000
   Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
************************************************************************

------------------------------------------------------------------------
```

AREA DD1

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 07/22/25

ROUTING: BASIN DD1; UNIT HYDROGRAPH DD1

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARDD124100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 291
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.779 (CFS)
Total volume = 0.466 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 101.000 to Point/Station 102.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 291
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.014	0.111	0.014	0.014
1.000	0.027	0.111	0.027	0.027
1.500	0.040	0.111	0.040	0.040
2.000	0.060	0.111	0.060	0.060
2.500	0.083	0.111	0.083	0.083
3.000	0.108	0.111	0.108	0.108
3.500	0.134	0.111	0.134	0.134
4.000	0.161	0.111	0.161	0.161
4.500	0.187	0.111	0.187	0.187
5.000	0.212	0.111	0.212	0.212
5.500	0.236	0.111	0.236	0.236
6.000	0.256	0.111	0.256	0.256
6.500	0.270	0.111	0.270	0.270
7.000	0.284	0.111	0.284	0.284
7.500	0.297	0.111	0.297	0.297
7.580	0.299	0.111	0.299	0.299

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 0.2 0.39 0.58 0.78	Depth (Ft.)
0.083	0.02	0.00	0.000	O | | | |	0.00
0.167	0.04	0.00	0.000	OI | | | |	0.01
0.250	0.04	0.00	0.001	OI | | | |	0.02
0.333	0.06	0.01	0.001	O I | | | |	0.03
0.417	0.07	0.01	0.001	O I | | | |	0.04
0.500	0.07	0.01	0.002	O I | | | |	0.06
0.583	0.07	0.02	0.002	O I | | | |	0.07
0.667	0.07	0.02	0.002	O I | | | |	0.08
0.750	0.07	0.02	0.003	O I | | | |	0.09
0.833	0.08	0.02	0.003	O I | | | |	0.11
0.917	0.09	0.03	0.003	|O I | | | |	0.12
1.000	0.09	0.03	0.004	|O I | | | |	0.13
1.083	0.08	0.03	0.004	|O I | | | |	0.15
1.167	0.07	0.04	0.004	|OI | | | |	0.16
1.250	0.07	0.04	0.005	|OI | | | |	0.17
1.333	0.07	0.04	0.005	|OI | | | |	0.17
1.417	0.07	0.04	0.005	|OI | | | |	0.18
1.500	0.07	0.04	0.005	|OI | | | |	0.19
1.583	0.07	0.04	0.005	|OI | | | |	0.19
1.667	0.07	0.04	0.006	|OI | | | |	0.20
1.750	0.07	0.05	0.006	|OI | | | |	0.20
1.833	0.08	0.05	0.006	|O I | | | |	0.21
1.917	0.09	0.05	0.006	| OI | | | |	0.22
2.000	0.09	0.05	0.006	| OI | | | |	0.23
2.083	0.09	0.05	0.007	| OI | | | |	0.24

2.167	0.09	0.05	0.007	OI				0.25
2.250	0.09	0.06	0.007	OI				0.26
2.333	0.09	0.06	0.007	OI				0.26
2.417	0.09	0.06	0.008	OI				0.27
2.500	0.09	0.06	0.008	OI				0.28
2.583	0.10	0.06	0.008	O I				0.29
2.667	0.11	0.07	0.008	O I				0.30
2.750	0.11	0.07	0.009	O I				0.31
2.833	0.11	0.07	0.009	O I				0.32
2.917	0.11	0.07	0.009	O I				0.33
3.000	0.11	0.07	0.009	OI				0.34
3.083	0.11	0.08	0.010	OI				0.35
3.167	0.11	0.08	0.010	OI				0.36
3.250	0.11	0.08	0.010	OI				0.36
3.333	0.11	0.08	0.010	OI				0.37
3.417	0.11	0.08	0.011	OI				0.38
3.500	0.11	0.09	0.011	OI				0.39
3.583	0.11	0.09	0.011	OI				0.39
3.667	0.11	0.09	0.011	OI				0.40
3.750	0.11	0.09	0.011	OI				0.40
3.833	0.12	0.09	0.011	O I				0.41
3.917	0.13	0.09	0.012	O I				0.42
4.000	0.13	0.10	0.012	O I				0.43
4.083	0.14	0.10	0.012	O I				0.44
4.167	0.14	0.10	0.013	OI				0.45
4.250	0.14	0.10	0.013	OI				0.46
4.333	0.15	0.10	0.013	OI				0.47
4.417	0.16	0.11	0.013	O I				0.48
4.500	0.16	0.11	0.014	O I				0.49
4.583	0.16	0.11	0.014	O I				0.50
4.667	0.16	0.11	0.014	O I				0.51
4.750	0.16	0.11	0.015	O I				0.52
4.833	0.17	0.11	0.015	O I				0.54
4.917	0.18	0.11	0.015	O I				0.56
5.000	0.18	0.11	0.016	O I				0.57
5.083	0.16	0.11	0.016	O I				0.59
5.167	0.14	0.11	0.017	OI				0.60
5.250	0.14	0.11	0.017	OI				0.61
5.333	0.15	0.11	0.017	OI				0.61
5.417	0.16	0.11	0.017	O I				0.62
5.500	0.16	0.11	0.018	O I				0.64
5.583	0.17	0.11	0.018	O I				0.65
5.667	0.18	0.11	0.018	O I				0.67
5.750	0.18	0.11	0.019	O I				0.68
5.833	0.18	0.11	0.019	O I				0.70
5.917	0.18	0.11	0.020	O I				0.72
6.000	0.18	0.11	0.020	O I				0.74
6.083	0.19	0.11	0.021	O I				0.76
6.167	0.20	0.11	0.021	O I				0.78
6.250	0.20	0.11	0.022	O I				0.81
6.333	0.20	0.11	0.023	O I				0.83
6.417	0.20	0.11	0.023	O I				0.85
6.500	0.20	0.11	0.024	O I				0.88

6.583	0.21	0.11	0.024	|	O	I	|	|	0.90
6.667	0.22	0.11	0.025	|	O	|I	|	|	0.93
6.750	0.22	0.11	0.026	|	O	|I	|	|	0.96
6.833	0.23	0.11	0.027	|	O	|I	|	|	0.99
6.917	0.23	0.11	0.028	|	O	|I	|	|	1.02
7.000	0.23	0.11	0.028	|	O	|I	|	|	1.05
7.083	0.23	0.11	0.029	|	O	|I	|	|	1.08
7.167	0.23	0.11	0.030	|	O	|I	|	|	1.11
7.250	0.23	0.11	0.031	|	O	|I	|	|	1.14
7.333	0.24	0.11	0.032	|	O	|I	|	|	1.17
7.417	0.25	0.11	0.032	|	O	| I	|	|	1.21
7.500	0.25	0.11	0.033	|	O	| I	|	|	1.24
7.583	0.26	0.11	0.034	|	O	| I	|	|	1.28
7.667	0.27	0.11	0.035	|	O	| I	|	|	1.32
7.750	0.27	0.11	0.036	|	O	| I	|	|	1.36
7.833	0.28	0.11	0.038	|	O	| I	|	|	1.41
7.917	0.29	0.11	0.039	|	O	| I	|	|	1.45
8.000	0.29	0.11	0.040	|	O	| I	|	|	1.50
8.083	0.31	0.11	0.041	|	O	| I	|	|	1.53
8.167	0.33	0.11	0.043	|	O	| I	|	|	1.57
8.250	0.34	0.11	0.044	|	O	| I	|	|	1.61
8.333	0.34	0.11	0.046	|	O	| I	|	|	1.65
8.417	0.34	0.11	0.047	|	O	| I	|	|	1.69
8.500	0.34	0.11	0.049	|	O	| I	|	|	1.73
8.583	0.35	0.11	0.051	|	O	| I	|	|	1.77
8.667	0.36	0.11	0.052	|	O	| I	|	|	1.81
8.750	0.36	0.11	0.054	|	O	| I	|	|	1.85
8.833	0.37	0.11	0.056	|	O	| I|	|	|	1.89
8.917	0.38	0.11	0.058	|	O	| I|	|	|	1.94
9.000	0.38	0.11	0.059	|	O	| I|	|	|	1.99
9.083	0.40	0.11	0.061	|	O	| I	|	|	2.03
9.167	0.42	0.11	0.063	|	O	| |I	|	|	2.08
9.250	0.43	0.11	0.066	|	O	| |I	|	|	2.12
9.333	0.44	0.11	0.068	|	O	| |I	|	|	2.17
9.417	0.45	0.11	0.070	|	O	| | I	|	|	2.22
9.500	0.45	0.11	0.072	|	O	| | I	|	|	2.27
9.583	0.46	0.11	0.075	|	O	| | I	|	|	2.32
9.667	0.47	0.11	0.077	|	O	| | I	|	|	2.38
9.750	0.47	0.11	0.080	|	O	| | I	|	|	2.43
9.833	0.48	0.11	0.082	|	O	| | I	|	|	2.48
9.917	0.49	0.11	0.085	|	O	| | I	|	|	2.54
10.000	0.49	0.11	0.088	|	O	| | I	|	|	2.59
10.083	0.43	0.11	0.090	|	O	| |I	|	|	2.64
10.167	0.36	0.11	0.092	|	O	| I	|	|	2.68
10.250	0.34	0.11	0.093	|	O	| I	|	|	2.71
10.333	0.34	0.11	0.095	|	O	| I	|	|	2.74
10.417	0.34	0.11	0.097	|	O	| I	|	|	2.77
10.500	0.34	0.11	0.098	|	O	| I	|	|	2.80
10.583	0.39	0.11	0.100	|	O	| I|	|	|	2.84
10.667	0.44	0.11	0.102	|	O	| |I	|	|	2.88
10.750	0.45	0.11	0.104	|	O	| | I	|	|	2.93
10.833	0.45	0.11	0.107	|	O	| | I	|	|	2.97
10.917	0.45	0.11	0.109	|	O	| | I	|	|	3.02

11.000	0.45	0.11	0.111	|	O	|	| I |	|	3.06
11.083	0.44	0.11	0.114	|	O	|	| I |	|	3.11
11.167	0.43	0.11	0.116	|	O	|	|I |	|	3.15
11.250	0.43	0.11	0.118	|	O	|	|I |	|	3.19
11.333	0.43	0.11	0.120	|	O	|	|I |	|	3.23
11.417	0.43	0.11	0.122	|	O	|	|I |	|	3.28
11.500	0.43	0.11	0.125	|	O	|	|I |	|	3.32
11.583	0.41	0.11	0.127	|	O	|	I |	|	3.36
11.667	0.39	0.11	0.129	|	O	|	I|	|	3.40
11.750	0.38	0.11	0.131	|	O	|	I|	|	3.43
11.833	0.39	0.11	0.132	|	O	|	I |	|	3.47
11.917	0.40	0.11	0.134	|	O	|	I |	|	3.51
12.000	0.40	0.11	0.136	|	O	|	I |	|	3.55
12.083	0.48	0.11	0.139	|	O	|	| I |	|	3.59
12.167	0.55	0.11	0.141	|	O	|	| I |	|	3.64
12.250	0.56	0.11	0.145	|	O	|	| I |	|	3.70
12.333	0.57	0.11	0.148	|	O	|	| I|	|	3.75
12.417	0.58	0.11	0.151	|	O	|	| I|	|	3.81
12.500	0.59	0.11	0.154	|	O	|	| I |	|	3.87
12.583	0.61	0.11	0.157	|	O	|	| I |	|	3.93
12.667	0.63	0.11	0.161	|	O	|	|I |	|	4.00
12.750	0.63	0.11	0.165	|	O	|	|I |	|	4.07
12.833	0.64	0.11	0.168	|	O	|	| I |	|	4.14
12.917	0.65	0.11	0.172	|	O	|	| I |	|	4.21
13.000	0.65	0.11	0.176	|	O	|	| I |	|	4.28
13.083	0.71	0.11	0.179	|	O	|	| I |	|	4.35
13.167	0.76	0.11	0.184	|	O	|	| I|	|	4.44
13.250	0.77	0.11	0.188	|	O	|	| I|	|	4.52
13.333	0.78	0.11	0.193	|	O	|	| I|	|	4.62
13.417	0.78	0.11	0.197	|	O	|	| I|	|	4.71
13.500	0.78	0.11	0.202	|	O	|	| I	|	4.80
13.583	0.66	0.11	0.206	|	O	|	| I |	|	4.88
13.667	0.55	0.11	0.210	|	O	|	| I |	|	4.95
13.750	0.53	0.11	0.213	|	O	|	| I |	|	5.01
13.833	0.52	0.11	0.215	|	O	|	| I |	|	5.07
13.917	0.52	0.11	0.218	|	O	|	| I |	|	5.13
14.000	0.52	0.11	0.221	|	O	|	| I |	|	5.19
14.083	0.56	0.11	0.224	|	O	|	| I |	|	5.25
14.167	0.60	0.11	0.227	|	O	|	| I |	|	5.32
14.250	0.61	0.11	0.231	|	O	|	| I |	|	5.39
14.333	0.60	0.11	0.234	|	O	|	| I |	|	5.46
14.417	0.59	0.11	0.237	|	O	|	| I |	|	5.53
14.500	0.59	0.11	0.241	|	O	|	| I |	|	5.61
14.583	0.59	0.11	0.244	|	O	|	| I |	|	5.69
14.667	0.59	0.11	0.247	|	O	|	| I |	|	5.78
14.750	0.59	0.11	0.250	|	O	|	| I |	|	5.86
14.833	0.58	0.11	0.254	|	O	|	| I|	|	5.94
14.917	0.57	0.11	0.257	|	O	|	| I|	|	6.03
15.000	0.56	0.11	0.260	|	O	|	| I|	|	6.14
15.083	0.55	0.11	0.263	|	O	|	| I |	|	6.25
15.167	0.54	0.11	0.266	|	O	|	| I |	|	6.35
15.250	0.54	0.11	0.269	|	O	|	| I |	|	6.46
15.333	0.53	0.11	0.272	|	O	|	| I |	|	6.57

15.417	0.52	0.11	0.275	O			I		6.67
15.500	0.52	0.11	0.278	O			I		6.77
15.583	0.48	0.11	0.280	O		I			6.86
15.667	0.44	0.11	0.283	O		I			6.95
15.750	0.43	0.11	0.285	O		I			7.03
15.833	0.43	0.11	0.287	O		I			7.11
15.917	0.43	0.11	0.289	O		I			7.20
16.000	0.43	0.11	0.291	O		I			7.28
16.083	0.28	0.11	0.293	O	I				7.35
16.167	0.13	0.11	0.294	OI					7.37
16.250	0.10	0.11	0.294	O					7.37
16.333	0.09	0.11	0.294	IO					7.37
16.417	0.09	0.11	0.293	IO					7.36
16.500	0.09	0.11	0.293	IO					7.36
16.583	0.08	0.11	0.293	IO					7.35
16.667	0.07	0.11	0.293	I O					7.34
16.750	0.07	0.11	0.293	I O					7.33
16.833	0.07	0.11	0.292	I O					7.32
16.917	0.07	0.11	0.292	I O					7.31
17.000	0.07	0.11	0.292	I O					7.29
17.083	0.09	0.11	0.291	IO					7.29
17.167	0.11	0.11	0.291	O					7.28
17.250	0.11	0.11	0.291	O					7.28
17.333	0.11	0.11	0.291	O					7.28
17.417	0.11	0.11	0.291	O					7.28
17.500	0.11	0.11	0.291	O					7.28
17.583	0.11	0.11	0.291	O					7.28
17.667	0.11	0.11	0.291	O					7.28
17.750	0.11	0.11	0.291	O					7.28
17.833	0.10	0.11	0.291	O					7.28
17.917	0.09	0.11	0.291	IO					7.28
18.000	0.09	0.11	0.291	IO					7.27
18.083	0.09	0.11	0.291	IO					7.27
18.167	0.09	0.11	0.291	IO					7.26
18.250	0.09	0.11	0.291	IO					7.26
18.333	0.09	0.11	0.291	IO					7.25
18.417	0.09	0.11	0.290	IO					7.25
18.500	0.09	0.11	0.290	IO					7.24
18.583	0.08	0.11	0.290	IO					7.23
18.667	0.07	0.11	0.290	I O					7.23
18.750	0.07	0.11	0.290	I O					7.21
18.833	0.06	0.11	0.289	I O					7.20
18.917	0.05	0.11	0.289	I O					7.19
19.000	0.05	0.11	0.288	I O					7.17
19.083	0.06	0.11	0.288	I O					7.15
19.167	0.07	0.11	0.288	I O					7.14
19.250	0.07	0.11	0.287	I O					7.13
19.333	0.08	0.11	0.287	IO					7.12
19.417	0.09	0.11	0.287	IO					7.11
19.500	0.09	0.11	0.287	IO					7.10
19.583	0.08	0.11	0.287	IO					7.10
19.667	0.07	0.11	0.286	I O					7.09
19.750	0.07	0.11	0.286	I O					7.08

19.833	0.06	0.11	0.286	| I O |	|	|	|	7.06
19.917	0.05	0.11	0.285	|I O |	|	|	|	7.05
20.000	0.05	0.11	0.285	|I O |	|	|	|	7.03
20.083	0.06	0.11	0.284	| I O |	|	|	|	7.01
20.167	0.07	0.11	0.284	| I O |	|	|	|	7.00
20.250	0.07	0.11	0.284	| I O |	|	|	|	6.99
20.333	0.07	0.11	0.283	| I O |	|	|	|	6.98
20.417	0.07	0.11	0.283	| I O |	|	|	|	6.97
20.500	0.07	0.11	0.283	| I O |	|	|	|	6.96
20.583	0.07	0.11	0.283	| I O |	|	|	|	6.95
20.667	0.07	0.11	0.282	| I O |	|	|	|	6.94
20.750	0.07	0.11	0.282	| I O |	|	|	|	6.93
20.833	0.06	0.11	0.282	| I O |	|	|	|	6.91
20.917	0.05	0.11	0.281	|I O |	|	|	|	6.90
21.000	0.05	0.11	0.281	|I O |	|	|	|	6.88
21.083	0.06	0.11	0.280	| I O |	|	|	|	6.87
21.167	0.07	0.11	0.280	| I O |	|	|	|	6.86
21.250	0.07	0.11	0.280	| I O |	|	|	|	6.85
21.333	0.06	0.11	0.279	| I O |	|	|	|	6.83
21.417	0.05	0.11	0.279	|I O |	|	|	|	6.82
21.500	0.05	0.11	0.278	|I O |	|	|	|	6.80
21.583	0.06	0.11	0.278	| I O |	|	|	|	6.79
21.667	0.07	0.11	0.278	| I O |	|	|	|	6.78
21.750	0.07	0.11	0.277	| I O |	|	|	|	6.76
21.833	0.06	0.11	0.277	| I O |	|	|	|	6.75
21.917	0.05	0.11	0.277	|I O |	|	|	|	6.74
22.000	0.05	0.11	0.276	|I O |	|	|	|	6.72
22.083	0.06	0.11	0.276	| I O |	|	|	|	6.71
22.167	0.07	0.11	0.275	| I O |	|	|	|	6.70
22.250	0.07	0.11	0.275	| I O |	|	|	|	6.68
22.333	0.06	0.11	0.275	| I O |	|	|	|	6.67
22.417	0.05	0.11	0.274	|I O |	|	|	|	6.66
22.500	0.05	0.11	0.274	|I O |	|	|	|	6.64
22.583	0.05	0.11	0.274	|I O |	|	|	|	6.63
22.667	0.05	0.11	0.273	|I O |	|	|	|	6.61
22.750	0.05	0.11	0.273	|I O |	|	|	|	6.59
22.833	0.05	0.11	0.272	|I O |	|	|	|	6.58
22.917	0.05	0.11	0.272	|I O |	|	|	|	6.56
23.000	0.05	0.11	0.271	|I O |	|	|	|	6.54
23.083	0.05	0.11	0.271	|I O |	|	|	|	6.53
23.167	0.05	0.11	0.270	|I O |	|	|	|	6.51
23.250	0.05	0.11	0.270	|I O |	|	|	|	6.50
23.333	0.05	0.11	0.269	|I O |	|	|	|	6.48
23.417	0.05	0.11	0.269	|I O |	|	|	|	6.46
23.500	0.05	0.11	0.269	|I O |	|	|	|	6.45
23.583	0.05	0.11	0.268	|I O |	|	|	|	6.43
23.667	0.05	0.11	0.268	|I O |	|	|	|	6.41
23.750	0.05	0.11	0.267	|I O |	|	|	|	6.40
23.833	0.05	0.11	0.267	|I O |	|	|	|	6.38
23.917	0.05	0.11	0.266	|I O |	|	|	|	6.37
24.000	0.05	0.11	0.266	|I O |	|	|	|	6.35
24.083	0.03	0.11	0.265	|I O |	|	|	|	6.33
24.167	0.00	0.11	0.265	I O |	|	|	|	6.31

24.250	0.00	0.11	0.264	I	O	|	|	|	|	6.28
24.333	0.00	0.11	0.263	I	O	|	|	|	|	6.25
24.417	0.00	0.11	0.262	I	O	|	|	|	|	6.23
24.500	0.00	0.11	0.262	I	O	|	|	|	|	6.20
24.583	0.00	0.11	0.261	I	O	|	|	|	|	6.17
24.667	0.00	0.11	0.260	I	O	|	|	|	|	6.14
24.750	0.00	0.11	0.259	I	O	|	|	|	|	6.12
24.833	0.00	0.11	0.259	I	O	|	|	|	|	6.09
24.917	0.00	0.11	0.258	I	O	|	|	|	|	6.06
25.000	0.00	0.11	0.257	I	O	|	|	|	|	6.04
25.083	0.00	0.11	0.256	I	O	|	|	|	|	6.01
25.167	0.00	0.11	0.255	I	O	|	|	|	|	5.99
25.250	0.00	0.11	0.255	I	O	|	|	|	|	5.97
25.333	0.00	0.11	0.254	I	O	|	|	|	|	5.95
25.417	0.00	0.11	0.253	I	O	|	|	|	|	5.93
25.500	0.00	0.11	0.252	I	O	|	|	|	|	5.91
25.583	0.00	0.11	0.252	I	O	|	|	|	|	5.89
25.667	0.00	0.11	0.251	I	O	|	|	|	|	5.87
25.750	0.00	0.11	0.250	I	O	|	|	|	|	5.85
25.833	0.00	0.11	0.249	I	O	|	|	|	|	5.83
25.917	0.00	0.11	0.249	I	O	|	|	|	|	5.81
26.000	0.00	0.11	0.248	I	O	|	|	|	|	5.80
26.083	0.00	0.11	0.247	I	O	|	|	|	|	5.78
26.167	0.00	0.11	0.246	I	O	|	|	|	|	5.76
26.250	0.00	0.11	0.246	I	O	|	|	|	|	5.74
26.333	0.00	0.11	0.245	I	O	|	|	|	|	5.72
26.417	0.00	0.11	0.244	I	O	|	|	|	|	5.70
26.500	0.00	0.11	0.243	I	O	|	|	|	|	5.68
26.583	0.00	0.11	0.242	I	O	|	|	|	|	5.66
26.667	0.00	0.11	0.242	I	O	|	|	|	|	5.64
26.750	0.00	0.11	0.241	I	O	|	|	|	|	5.62
26.833	0.00	0.11	0.240	I	O	|	|	|	|	5.60
26.917	0.00	0.11	0.239	I	O	|	|	|	|	5.59
27.000	0.00	0.11	0.239	I	O	|	|	|	|	5.57
27.083	0.00	0.11	0.238	I	O	|	|	|	|	5.55
27.167	0.00	0.11	0.237	I	O	|	|	|	|	5.53
27.250	0.00	0.11	0.236	I	O	|	|	|	|	5.51
27.333	0.00	0.11	0.236	I	O	|	|	|	|	5.49
27.417	0.00	0.11	0.235	I	O	|	|	|	|	5.48
27.500	0.00	0.11	0.234	I	O	|	|	|	|	5.46
27.583	0.00	0.11	0.233	I	O	|	|	|	|	5.44
27.667	0.00	0.11	0.233	I	O	|	|	|	|	5.43
27.750	0.00	0.11	0.232	I	O	|	|	|	|	5.41
27.833	0.00	0.11	0.231	I	O	|	|	|	|	5.40
27.917	0.00	0.11	0.230	I	O	|	|	|	|	5.38
28.000	0.00	0.11	0.229	I	O	|	|	|	|	5.36
28.083	0.00	0.11	0.229	I	O	|	|	|	|	5.35
28.167	0.00	0.11	0.228	I	O	|	|	|	|	5.33
28.250	0.00	0.11	0.227	I	O	|	|	|	|	5.32
28.333	0.00	0.11	0.226	I	O	|	|	|	|	5.30
28.417	0.00	0.11	0.226	I	O	|	|	|	|	5.28
28.500	0.00	0.11	0.225	I	O	|	|	|	|	5.27
28.583	0.00	0.11	0.224	I	O	|	|	|	|	5.25

28.667	0.00	0.11	0.223	I	O	|	|	|	|	5.24
28.750	0.00	0.11	0.223	I	O	|	|	|	|	5.22
28.833	0.00	0.11	0.222	I	O	|	|	|	|	5.20
28.917	0.00	0.11	0.221	I	O	|	|	|	|	5.19
29.000	0.00	0.11	0.220	I	O	|	|	|	|	5.17
29.083	0.00	0.11	0.220	I	O	|	|	|	|	5.16
29.167	0.00	0.11	0.219	I	O	|	|	|	|	5.14
29.250	0.00	0.11	0.218	I	O	|	|	|	|	5.13
29.333	0.00	0.11	0.217	I	O	|	|	|	|	5.11
29.417	0.00	0.11	0.216	I	O	|	|	|	|	5.09
29.500	0.00	0.11	0.216	I	O	|	|	|	|	5.08
29.583	0.00	0.11	0.215	I	O	|	|	|	|	5.06
29.667	0.00	0.11	0.214	I	O	|	|	|	|	5.05
29.750	0.00	0.11	0.213	I	O	|	|	|	|	5.03
29.833	0.00	0.11	0.213	I	O	|	|	|	|	5.01
29.917	0.00	0.11	0.212	I	O	|	|	|	|	5.00
30.000	0.00	0.11	0.211	I	O	|	|	|	|	4.98
30.083	0.00	0.11	0.210	I	O	|	|	|	|	4.97
30.167	0.00	0.11	0.210	I	O	|	|	|	|	4.95
30.250	0.00	0.11	0.209	I	O	|	|	|	|	4.94
30.333	0.00	0.11	0.208	I	O	|	|	|	|	4.92
30.417	0.00	0.11	0.207	I	O	|	|	|	|	4.91
30.500	0.00	0.11	0.207	I	O	|	|	|	|	4.89
30.583	0.00	0.11	0.206	I	O	|	|	|	|	4.88
30.667	0.00	0.11	0.205	I	O	|	|	|	|	4.86
30.750	0.00	0.11	0.204	I	O	|	|	|	|	4.84
30.833	0.00	0.11	0.203	I	O	|	|	|	|	4.83
30.917	0.00	0.11	0.203	I	O	|	|	|	|	4.81
31.000	0.00	0.11	0.202	I	O	|	|	|	|	4.80
31.083	0.00	0.11	0.201	I	O	|	|	|	|	4.78
31.167	0.00	0.11	0.200	I	O	|	|	|	|	4.77
31.250	0.00	0.11	0.200	I	O	|	|	|	|	4.75
31.333	0.00	0.11	0.199	I	O	|	|	|	|	4.74
31.417	0.00	0.11	0.198	I	O	|	|	|	|	4.72
31.500	0.00	0.11	0.197	I	O	|	|	|	|	4.71
31.583	0.00	0.11	0.197	I	O	|	|	|	|	4.69
31.667	0.00	0.11	0.196	I	O	|	|	|	|	4.68
31.750	0.00	0.11	0.195	I	O	|	|	|	|	4.66
31.833	0.00	0.11	0.194	I	O	|	|	|	|	4.65
31.917	0.00	0.11	0.194	I	O	|	|	|	|	4.63
32.000	0.00	0.11	0.193	I	O	|	|	|	|	4.62
32.083	0.00	0.11	0.192	I	O	|	|	|	|	4.60
32.167	0.00	0.11	0.191	I	O	|	|	|	|	4.59
32.250	0.00	0.11	0.190	I	O	|	|	|	|	4.57
32.333	0.00	0.11	0.190	I	O	|	|	|	|	4.55
32.417	0.00	0.11	0.189	I	O	|	|	|	|	4.54
32.500	0.00	0.11	0.188	I	O	|	|	|	|	4.52
32.583	0.00	0.11	0.187	I	O	|	|	|	|	4.51
32.667	0.00	0.11	0.187	I	O	|	|	|	|	4.49
32.750	0.00	0.11	0.186	I	O	|	|	|	|	4.48
32.833	0.00	0.11	0.185	I	O	|	|	|	|	4.46
32.917	0.00	0.11	0.184	I	O	|	|	|	|	4.45
33.000	0.00	0.11	0.184	I	O	|	|	|	|	4.43

33.083	0.00	0.11	0.183	I	O	|	|	|	|	4.42
33.167	0.00	0.11	0.182	I	O	|	|	|	|	4.41
33.250	0.00	0.11	0.181	I	O	|	|	|	|	4.39
33.333	0.00	0.11	0.181	I	O	|	|	|	|	4.38
33.417	0.00	0.11	0.180	I	O	|	|	|	|	4.36
33.500	0.00	0.11	0.179	I	O	|	|	|	|	4.35
33.583	0.00	0.11	0.178	I	O	|	|	|	|	4.33
33.667	0.00	0.11	0.177	I	O	|	|	|	|	4.32
33.750	0.00	0.11	0.177	I	O	|	|	|	|	4.30
33.833	0.00	0.11	0.176	I	O	|	|	|	|	4.29
33.917	0.00	0.11	0.175	I	O	|	|	|	|	4.27
34.000	0.00	0.11	0.174	I	O	|	|	|	|	4.26
34.083	0.00	0.11	0.174	I	O	|	|	|	|	4.24
34.167	0.00	0.11	0.173	I	O	|	|	|	|	4.23
34.250	0.00	0.11	0.172	I	O	|	|	|	|	4.21
34.333	0.00	0.11	0.171	I	O	|	|	|	|	4.20
34.417	0.00	0.11	0.171	I	O	|	|	|	|	4.18
34.500	0.00	0.11	0.170	I	O	|	|	|	|	4.17
34.583	0.00	0.11	0.169	I	O	|	|	|	|	4.16
34.667	0.00	0.11	0.168	I	O	|	|	|	|	4.14
34.750	0.00	0.11	0.168	I	O	|	|	|	|	4.13
34.833	0.00	0.11	0.167	I	O	|	|	|	|	4.11
34.917	0.00	0.11	0.166	I	O	|	|	|	|	4.10
35.000	0.00	0.11	0.165	I	O	|	|	|	|	4.08
35.083	0.00	0.11	0.164	I	O	|	|	|	|	4.07
35.167	0.00	0.11	0.164	I	O	|	|	|	|	4.05
35.250	0.00	0.11	0.163	I	O	|	|	|	|	4.04
35.333	0.00	0.11	0.162	I	O	|	|	|	|	4.02
35.417	0.00	0.11	0.161	I	O	|	|	|	|	4.01
35.500	0.00	0.11	0.161	I	O	|	|	|	|	3.99
35.583	0.00	0.11	0.160	I	O	|	|	|	|	3.98
35.667	0.00	0.11	0.159	I	O	|	|	|	|	3.97
35.750	0.00	0.11	0.158	I	O	|	|	|	|	3.95
35.833	0.00	0.11	0.158	I	O	|	|	|	|	3.94
35.917	0.00	0.11	0.157	I	O	|	|	|	|	3.92
36.000	0.00	0.11	0.156	I	O	|	|	|	|	3.91
36.083	0.00	0.11	0.155	I	O	|	|	|	|	3.89
36.167	0.00	0.11	0.155	I	O	|	|	|	|	3.88
36.250	0.00	0.11	0.154	I	O	|	|	|	|	3.87
36.333	0.00	0.11	0.153	I	O	|	|	|	|	3.85
36.417	0.00	0.11	0.152	I	O	|	|	|	|	3.84
36.500	0.00	0.11	0.152	I	O	|	|	|	|	3.82
36.583	0.00	0.11	0.151	I	O	|	|	|	|	3.81
36.667	0.00	0.11	0.150	I	O	|	|	|	|	3.80
36.750	0.00	0.11	0.149	I	O	|	|	|	|	3.78
36.833	0.00	0.11	0.148	I	O	|	|	|	|	3.77
36.917	0.00	0.11	0.148	I	O	|	|	|	|	3.75
37.000	0.00	0.11	0.147	I	O	|	|	|	|	3.74
37.083	0.00	0.11	0.146	I	O	|	|	|	|	3.72
37.167	0.00	0.11	0.145	I	O	|	|	|	|	3.71
37.250	0.00	0.11	0.145	I	O	|	|	|	|	3.70
37.333	0.00	0.11	0.144	I	O	|	|	|	|	3.68
37.417	0.00	0.11	0.143	I	O	|	|	|	|	3.67

37.500	0.00	0.11	0.142	I	O	|	|	|	|	3.65
37.583	0.00	0.11	0.142	I	O	|	|	|	|	3.64
37.667	0.00	0.11	0.141	I	O	|	|	|	|	3.63
37.750	0.00	0.11	0.140	I	O	|	|	|	|	3.61
37.833	0.00	0.11	0.139	I	O	|	|	|	|	3.60
37.917	0.00	0.11	0.139	I	O	|	|	|	|	3.58
38.000	0.00	0.11	0.138	I	O	|	|	|	|	3.57
38.083	0.00	0.11	0.137	I	O	|	|	|	|	3.56
38.167	0.00	0.11	0.136	I	O	|	|	|	|	3.54
38.250	0.00	0.11	0.135	I	O	|	|	|	|	3.53
38.333	0.00	0.11	0.135	I	O	|	|	|	|	3.51
38.417	0.00	0.11	0.134	I	O	|	|	|	|	3.50
38.500	0.00	0.11	0.133	I	O	|	|	|	|	3.48
38.583	0.00	0.11	0.132	I	O	|	|	|	|	3.47
38.667	0.00	0.11	0.132	I	O	|	|	|	|	3.45
38.750	0.00	0.11	0.131	I	O	|	|	|	|	3.44
38.833	0.00	0.11	0.130	I	O	|	|	|	|	3.42
38.917	0.00	0.11	0.129	I	O	|	|	|	|	3.41
39.000	0.00	0.11	0.129	I	O	|	|	|	|	3.40
39.083	0.00	0.11	0.128	I	O	|	|	|	|	3.38
39.167	0.00	0.11	0.127	I	O	|	|	|	|	3.37
39.250	0.00	0.11	0.126	I	O	|	|	|	|	3.35
39.333	0.00	0.11	0.126	I	O	|	|	|	|	3.34
39.417	0.00	0.11	0.125	I	O	|	|	|	|	3.32
39.500	0.00	0.11	0.124	I	O	|	|	|	|	3.31
39.583	0.00	0.11	0.123	I	O	|	|	|	|	3.29
39.667	0.00	0.11	0.122	I	O	|	|	|	|	3.28
39.750	0.00	0.11	0.122	I	O	|	|	|	|	3.26
39.833	0.00	0.11	0.121	I	O	|	|	|	|	3.25
39.917	0.00	0.11	0.120	I	O	|	|	|	|	3.23
40.000	0.00	0.11	0.119	I	O	|	|	|	|	3.22
40.083	0.00	0.11	0.119	I	O	|	|	|	|	3.20
40.167	0.00	0.11	0.118	I	O	|	|	|	|	3.19
40.250	0.00	0.11	0.117	I	O	|	|	|	|	3.17
40.333	0.00	0.11	0.116	I	O	|	|	|	|	3.16
40.417	0.00	0.11	0.116	I	O	|	|	|	|	3.15
40.500	0.00	0.11	0.115	I	O	|	|	|	|	3.13
40.583	0.00	0.11	0.114	I	O	|	|	|	|	3.12
40.667	0.00	0.11	0.113	I	O	|	|	|	|	3.10
40.750	0.00	0.11	0.113	I	O	|	|	|	|	3.09
40.833	0.00	0.11	0.112	I	O	|	|	|	|	3.07
40.917	0.00	0.11	0.111	I	O	|	|	|	|	3.06
41.000	0.00	0.11	0.110	I	O	|	|	|	|	3.04
41.083	0.00	0.11	0.109	I	O	|	|	|	|	3.03
41.167	0.00	0.11	0.109	I	O	|	|	|	|	3.01
41.250	0.00	0.11	0.108	I	O	|	|	|	|	3.00
41.333	0.00	0.11	0.107	I	O	|	|	|	|	2.98
41.417	0.00	0.11	0.106	I	O	|	|	|	|	2.97
41.500	0.00	0.11	0.106	I	O	|	|	|	|	2.95
41.583	0.00	0.11	0.105	I	O	|	|	|	|	2.94
41.667	0.00	0.11	0.104	I	O	|	|	|	|	2.92
41.750	0.00	0.11	0.103	I	O	|	|	|	|	2.91
41.833	0.00	0.11	0.103	I	O	|	|	|	|	2.89

41.917	0.00	0.11	0.102	I	O	|	|	|	|	2.88
42.000	0.00	0.11	0.101	I	O	|	|	|	|	2.86
42.083	0.00	0.11	0.100	I	O	|	|	|	|	2.85
42.167	0.00	0.11	0.100	I	O	|	|	|	|	2.83
42.250	0.00	0.11	0.099	I	O	|	|	|	|	2.82
42.333	0.00	0.11	0.098	I	O	|	|	|	|	2.80
42.417	0.00	0.11	0.097	I	O	|	|	|	|	2.78
42.500	0.00	0.11	0.096	I	O	|	|	|	|	2.77
42.583	0.00	0.11	0.096	I	O	|	|	|	|	2.75
42.667	0.00	0.11	0.095	I	O	|	|	|	|	2.74
42.750	0.00	0.11	0.094	I	O	|	|	|	|	2.72
42.833	0.00	0.11	0.093	I	O	|	|	|	|	2.71
42.917	0.00	0.11	0.093	I	O	|	|	|	|	2.69
43.000	0.00	0.11	0.092	I	O	|	|	|	|	2.68
43.083	0.00	0.11	0.091	I	O	|	|	|	|	2.66
43.167	0.00	0.11	0.090	I	O	|	|	|	|	2.65
43.250	0.00	0.11	0.090	I	O	|	|	|	|	2.63
43.333	0.00	0.11	0.089	I	O	|	|	|	|	2.62
43.417	0.00	0.11	0.088	I	O	|	|	|	|	2.60
43.500	0.00	0.11	0.087	I	O	|	|	|	|	2.59
43.583	0.00	0.11	0.087	I	O	|	|	|	|	2.57
43.667	0.00	0.11	0.086	I	O	|	|	|	|	2.56
43.750	0.00	0.11	0.085	I	O	|	|	|	|	2.54
43.833	0.00	0.11	0.084	I	O	|	|	|	|	2.52
43.917	0.00	0.11	0.083	I	O	|	|	|	|	2.51
44.000	0.00	0.11	0.083	I	O	|	|	|	|	2.49
44.083	0.00	0.11	0.082	I	O	|	|	|	|	2.48
44.167	0.00	0.11	0.081	I	O	|	|	|	|	2.46
44.250	0.00	0.11	0.080	I	O	|	|	|	|	2.44
44.333	0.00	0.11	0.080	I	O	|	|	|	|	2.43
44.417	0.00	0.11	0.079	I	O	|	|	|	|	2.41
44.500	0.00	0.11	0.078	I	O	|	|	|	|	2.39
44.583	0.00	0.11	0.077	I	O	|	|	|	|	2.38
44.667	0.00	0.11	0.077	I	O	|	|	|	|	2.36
44.750	0.00	0.11	0.076	I	O	|	|	|	|	2.34
44.833	0.00	0.11	0.075	I	O	|	|	|	|	2.33
44.917	0.00	0.11	0.074	I	O	|	|	|	|	2.31
45.000	0.00	0.11	0.074	I	O	|	|	|	|	2.29
45.083	0.00	0.11	0.073	I	O	|	|	|	|	2.28
45.167	0.00	0.11	0.072	I	O	|	|	|	|	2.26
45.250	0.00	0.11	0.071	I	O	|	|	|	|	2.24
45.333	0.00	0.11	0.070	I	O	|	|	|	|	2.23
45.417	0.00	0.11	0.070	I	O	|	|	|	|	2.21
45.500	0.00	0.11	0.069	I	O	|	|	|	|	2.19
45.583	0.00	0.11	0.068	I	O	|	|	|	|	2.18
45.667	0.00	0.11	0.067	I	O	|	|	|	|	2.16
45.750	0.00	0.11	0.067	I	O	|	|	|	|	2.14
45.833	0.00	0.11	0.066	I	O	|	|	|	|	2.13
45.917	0.00	0.11	0.065	I	O	|	|	|	|	2.11
46.000	0.00	0.11	0.064	I	O	|	|	|	|	2.09
46.083	0.00	0.11	0.064	I	O	|	|	|	|	2.08
46.167	0.00	0.11	0.063	I	O	|	|	|	|	2.06
46.250	0.00	0.11	0.062	I	O	|	|	|	|	2.04

46.333	0.00	0.11	0.061	I	O	|	|	|	|	2.03
46.417	0.00	0.11	0.061	I	O	|	|	|	|	2.01
46.500	0.00	0.11	0.060	I	O	|	|	|	|	1.99
46.583	0.00	0.11	0.059	I	O	|	|	|	|	1.98
46.667	0.00	0.11	0.058	I	O	|	|	|	|	1.96
46.750	0.00	0.11	0.057	I	O	|	|	|	|	1.94
46.833	0.00	0.11	0.057	I	O	|	|	|	|	1.92
46.917	0.00	0.11	0.056	I	O	|	|	|	|	1.90
47.000	0.00	0.11	0.055	I	O	|	|	|	|	1.88
47.083	0.00	0.11	0.054	I	O	|	|	|	|	1.86
47.167	0.00	0.11	0.054	I	O	|	|	|	|	1.84
47.250	0.00	0.11	0.053	I	O	|	|	|	|	1.82
47.333	0.00	0.11	0.052	I	O	|	|	|	|	1.80
47.417	0.00	0.11	0.051	I	O	|	|	|	|	1.78
47.500	0.00	0.11	0.051	I	O	|	|	|	|	1.76
47.583	0.00	0.11	0.050	I	O	|	|	|	|	1.75
47.667	0.00	0.11	0.049	I	O	|	|	|	|	1.73
47.750	0.00	0.11	0.048	I	O	|	|	|	|	1.71
47.833	0.00	0.11	0.048	I	O	|	|	|	|	1.69
47.917	0.00	0.11	0.047	I	O	|	|	|	|	1.67
48.000	0.00	0.11	0.046	I	O	|	|	|	|	1.65
48.083	0.00	0.11	0.045	I	O	|	|	|	|	1.63
48.167	0.00	0.11	0.044	I	O	|	|	|	|	1.61
48.250	0.00	0.11	0.044	I	O	|	|	|	|	1.59
48.333	0.00	0.11	0.043	I	O	|	|	|	|	1.57
48.417	0.00	0.11	0.042	I	O	|	|	|	|	1.55
48.500	0.00	0.11	0.041	I	O	|	|	|	|	1.54
48.583	0.00	0.11	0.041	I	O	|	|	|	|	1.52
48.667	0.00	0.11	0.040	I	O	|	|	|	|	1.50
48.750	0.00	0.11	0.039	I	O	|	|	|	|	1.47
48.833	0.00	0.11	0.038	I	O	|	|	|	|	1.44
48.917	0.00	0.11	0.038	I	O	|	|	|	|	1.41
49.000	0.00	0.11	0.037	I	O	|	|	|	|	1.38
49.083	0.00	0.11	0.036	I	O	|	|	|	|	1.35
49.167	0.00	0.11	0.035	I	O	|	|	|	|	1.32
49.250	0.00	0.11	0.035	I	O	|	|	|	|	1.29
49.333	0.00	0.11	0.034	I	O	|	|	|	|	1.26
49.417	0.00	0.11	0.033	I	O	|	|	|	|	1.23
49.500	0.00	0.11	0.032	I	O	|	|	|	|	1.20
49.583	0.00	0.11	0.031	I	O	|	|	|	|	1.17
49.667	0.00	0.11	0.031	I	O	|	|	|	|	1.14
49.750	0.00	0.11	0.030	I	O	|	|	|	|	1.11
49.833	0.00	0.11	0.029	I	O	|	|	|	|	1.08
49.917	0.00	0.11	0.028	I	O	|	|	|	|	1.05
50.000	0.00	0.11	0.028	I	O	|	|	|	|	1.03
50.083	0.00	0.11	0.027	I	O	|	|	|	|	1.00
50.167	0.00	0.11	0.026	I	O	|	|	|	|	0.97
50.250	0.00	0.11	0.025	I	O	|	|	|	|	0.94
50.333	0.00	0.11	0.025	I	O	|	|	|	|	0.91
50.417	0.00	0.11	0.024	I	O	|	|	|	|	0.88
50.500	0.00	0.11	0.023	I	O	|	|	|	|	0.85
50.583	0.00	0.11	0.022	I	O	|	|	|	|	0.82
50.667	0.00	0.11	0.022	I	O	|	|	|	|	0.79

50.750	0.00	0.11	0.021	I O	|	|	|	0.76
50.833	0.00	0.11	0.020	I O	|	|	|	0.73
50.917	0.00	0.11	0.019	I O	|	|	|	0.70
51.000	0.00	0.11	0.018	I O	|	|	|	0.67
51.083	0.00	0.11	0.018	I O	|	|	|	0.64
51.167	0.00	0.11	0.017	I O	|	|	|	0.61
51.250	0.00	0.11	0.016	I O	|	|	|	0.58
51.333	0.00	0.11	0.015	I O	|	|	|	0.55
51.417	0.00	0.11	0.015	I O	|	|	|	0.53
51.500	0.00	0.11	0.014	I O	|	|	|	0.50
51.583	0.00	0.10	0.013	I O	|	|	|	0.47
51.667	0.00	0.10	0.012	I O	|	|	|	0.45
51.750	0.00	0.09	0.012	I O	|	|	|	0.42
51.833	0.00	0.09	0.011	I O	|	|	|	0.40
51.917	0.00	0.08	0.011	I O	|	|	|	0.38
52.000	0.00	0.08	0.010	I O	|	|	|	0.36
52.083	0.00	0.08	0.009	I O	|	|	|	0.34
52.167	0.00	0.07	0.009	I O	|	|	|	0.32
52.250	0.00	0.07	0.009	I O	|	|	|	0.30
52.333	0.00	0.06	0.008	I O	|	|	|	0.29
52.417	0.00	0.06	0.008	I O	|	|	|	0.27
52.500	0.00	0.06	0.007	I O	|	|	|	0.26
52.583	0.00	0.05	0.007	I O	|	|	|	0.24
52.667	0.00	0.05	0.006	I O	|	|	|	0.23
52.750	0.00	0.05	0.006	IO	|	|	|	0.22
52.833	0.00	0.05	0.006	IO	|	|	|	0.21
52.917	0.00	0.04	0.005	IO	|	|	|	0.20
53.000	0.00	0.04	0.005	IO	|	|	|	0.19
53.083	0.00	0.04	0.005	IO	|	|	|	0.18
53.167	0.00	0.04	0.005	IO	|	|	|	0.17
53.250	0.00	0.04	0.004	IO	|	|	|	0.16
53.333	0.00	0.03	0.004	IO	|	|	|	0.15
53.417	0.00	0.03	0.004	IO	|	|	|	0.14
53.500	0.00	0.03	0.004	IO	|	|	|	0.13
53.583	0.00	0.03	0.004	IO	|	|	|	0.13
53.667	0.00	0.03	0.003	IO	|	|	|	0.12
53.750	0.00	0.03	0.003	IO	|	|	|	0.11
53.833	0.00	0.02	0.003	O	|	|	|	0.11
53.917	0.00	0.02	0.003	O	|	|	|	0.10
54.000	0.00	0.02	0.003	O	|	|	|	0.10
54.083	0.00	0.02	0.003	O	|	|	|	0.09
54.167	0.00	0.02	0.002	O	|	|	|	0.09
54.250	0.00	0.02	0.002	O	|	|	|	0.08
54.333	0.00	0.02	0.002	O	|	|	|	0.08
54.417	0.00	0.02	0.002	O	|	|	|	0.07
54.500	0.00	0.02	0.002	O	|	|	|	0.07
54.583	0.00	0.01	0.002	O	|	|	|	0.07
54.667	0.00	0.01	0.002	O	|	|	|	0.06
54.750	0.00	0.01	0.002	O	|	|	|	0.06
54.833	0.00	0.01	0.002	O	|	|	|	0.06
54.917	0.00	0.01	0.001	O	|	|	|	0.05
55.000	0.00	0.01	0.001	O	|	|	|	0.05
55.083	0.00	0.01	0.001	O	|	|	|	0.05

55.167	0.00	0.01	0.001	O	|	|	|	|	0.04
55.250	0.00	0.01	0.001	O	|	|	|	|	0.04
55.333	0.00	0.01	0.001	O	|	|	|	|	0.04
55.417	0.00	0.01	0.001	O	|	|	|	|	0.04
55.500	0.00	0.01	0.001	O	|	|	|	|	0.04
55.583	0.00	0.01	0.001	O	|	|	|	|	0.03
55.667	0.00	0.01	0.001	O	|	|	|	|	0.03
55.750	0.00	0.01	0.001	O	|	|	|	|	0.03
55.833	0.00	0.01	0.001	O	|	|	|	|	0.03
55.917	0.00	0.01	0.001	O	|	|	|	|	0.03
56.000	0.00	0.01	0.001	O	|	|	|	|	0.03
56.083	0.00	0.01	0.001	O	|	|	|	|	0.02
56.167	0.00	0.01	0.001	O	|	|	|	|	0.02
56.250	0.00	0.00	0.001	O	|	|	|	|	0.02
56.333	0.00	0.00	0.001	O	|	|	|	|	0.02
56.417	0.00	0.00	0.001	O	|	|	|	|	0.02
56.500	0.00	0.00	0.001	O	|	|	|	|	0.02
56.583	0.00	0.00	0.000	O	|	|	|	|	0.02
56.667	0.00	0.00	0.000	O	|	|	|	|	0.02
56.750	0.00	0.00	0.000	O	|	|	|	|	0.02
56.833	0.00	0.00	0.000	O	|	|	|	|	0.02
56.917	0.00	0.00	0.000	O	|	|	|	|	0.01
57.000	0.00	0.00	0.000	O	|	|	|	|	0.01
57.083	0.00	0.00	0.000	O	|	|	|	|	0.01
57.167	0.00	0.00	0.000	O	|	|	|	|	0.01
57.250	0.00	0.00	0.000	O	|	|	|	|	0.01
57.333	0.00	0.00	0.000	O	|	|	|	|	0.01
57.417	0.00	0.00	0.000	O	|	|	|	|	0.01
57.500	0.00	0.00	0.000	O	|	|	|	|	0.01
57.583	0.00	0.00	0.000	O	|	|	|	|	0.01
57.667	0.00	0.00	0.000	O	|	|	|	|	0.01
57.750	0.00	0.00	0.000	O	|	|	|	|	0.01
57.833	0.00	0.00	0.000	O	|	|	|	|	0.01
57.917	0.00	0.00	0.000	O	|	|	|	|	0.01
58.000	0.00	0.00	0.000	O	|	|	|	|	0.01
58.083	0.00	0.00	0.000	O	|	|	|	|	0.01
58.167	0.00	0.00	0.000	O	|	|	|	|	0.01
58.250	0.00	0.00	0.000	O	|	|	|	|	0.01
58.333	0.00	0.00	0.000	O	|	|	|	|	0.01
58.417	0.00	0.00	0.000	O	|	|	|	|	0.01
58.500	0.00	0.00	0.000	O	|	|	|	|	0.01
58.583	0.00	0.00	0.000	O	|	|	|	|	0.00
58.667	0.00	0.00	0.000	O	|	|	|	|	0.00
58.750	0.00	0.00	0.000	O	|	|	|	|	0.00

**********HYDROGRAPH DATA**********

Number of intervals = 705
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.111 (CFS)
Total volume = 0.466 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000

Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

AREA E1

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 07/22/25

ROUTING: BASIN E1; UNIT HYDROGRAPH E1

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: ARE124100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 289
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.271 (CFS)
Total volume = 0.165 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 101.000 to Point/Station 102.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 289
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.005	0.042	0.005	0.005
1.000	0.010	0.042	0.010	0.010
1.500	0.015	0.042	0.015	0.015
2.000	0.023	0.042	0.023	0.023
2.500	0.032	0.042	0.032	0.032
3.000	0.041	0.042	0.041	0.041
3.500	0.051	0.042	0.051	0.051
4.000	0.061	0.042	0.061	0.061
4.500	0.071	0.042	0.071	0.071
5.000	0.081	0.042	0.081	0.081
5.500	0.090	0.042	0.090	0.090
6.000	0.097	0.042	0.097	0.097
6.500	0.103	0.042	0.103	0.103
7.000	0.108	0.042	0.108	0.108
7.500	0.113	0.042	0.113	0.113
7.580	0.114	0.042	0.114	0.114

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.1	0.14	0.20	0.27	Depth (Ft.)
0.083	0.01	0.00	0.000	OI	|	|	|	|	0.00
0.167	0.02	0.00	0.000	OI	|	|	|	|	0.01
0.250	0.02	0.00	0.000	OI	|	|	|	|	0.02
0.333	0.02	0.00	0.000	O I	|	|	|	|	0.03
0.417	0.02	0.00	0.000	O I	|	|	|	|	0.05
0.500	0.02	0.01	0.001	O I	|	|	|	|	0.06
0.583	0.02	0.01	0.001	O I	|	|	|	|	0.07
0.667	0.02	0.01	0.001	O I	|	|	|	|	0.09
0.750	0.02	0.01	0.001	O I	|	|	|	|	0.10
0.833	0.03	0.01	0.001	|O I	|	|	|	|	0.11
0.917	0.03	0.01	0.001	|O I	|	|	|	|	0.12
1.000	0.03	0.01	0.001	|O I	|	|	|	|	0.14
1.083	0.03	0.01	0.001	|O I	|	|	|	|	0.15
1.167	0.02	0.01	0.002	|OI	|	|	|	|	0.16
1.250	0.02	0.01	0.002	|OI	|	|	|	|	0.17
1.333	0.02	0.01	0.002	|OI	|	|	|	|	0.17
1.417	0.02	0.01	0.002	|OI	|	|	|	|	0.18
1.500	0.02	0.02	0.002	|OI	|	|	|	|	0.18
1.583	0.02	0.02	0.002	|OI	|	|	|	|	0.19
1.667	0.02	0.02	0.002	|OI	|	|	|	|	0.20
1.750	0.02	0.02	0.002	|OI	|	|	|	|	0.20
1.833	0.03	0.02	0.002	| OI	|	|	|	|	0.21
1.917	0.03	0.02	0.002	| OI	|	|	|	|	0.22
2.000	0.03	0.02	0.002	| OI	|	|	|	|	0.23
2.083	0.03	0.02	0.002	| OI	|	|	|	|	0.23

2.167	0.03	0.02	0.002	OI				0.24
2.250	0.03	0.02	0.002	OI				0.25
2.333	0.03	0.02	0.003	OI				0.26
2.417	0.03	0.02	0.003	OI				0.26
2.500	0.03	0.02	0.003	OI				0.27
2.583	0.04	0.02	0.003	O I				0.28
2.667	0.04	0.02	0.003	O I				0.29
2.750	0.04	0.03	0.003	O I				0.30
2.833	0.04	0.03	0.003	OI				0.31
2.917	0.04	0.03	0.003	OI				0.32
3.000	0.04	0.03	0.003	OI				0.33
3.083	0.04	0.03	0.003	OI				0.34
3.167	0.04	0.03	0.003	OI				0.34
3.250	0.04	0.03	0.004	OI				0.35
3.333	0.04	0.03	0.004	OI				0.36
3.417	0.04	0.03	0.004	OI				0.36
3.500	0.04	0.03	0.004	OI				0.37
3.583	0.04	0.03	0.004	OI				0.38
3.667	0.04	0.03	0.004	OI				0.38
3.750	0.04	0.03	0.004	OI				0.39
3.833	0.05	0.03	0.004	O I				0.39
3.917	0.05	0.03	0.004	O I				0.40
4.000	0.05	0.03	0.004	OI				0.41
4.083	0.05	0.04	0.004	OI				0.42
4.167	0.05	0.04	0.004	OI				0.43
4.250	0.05	0.04	0.004	OI				0.44
4.333	0.05	0.04	0.004	O I				0.45
4.417	0.06	0.04	0.005	O I				0.46
4.500	0.06	0.04	0.005	O I				0.47
4.583	0.06	0.04	0.005	O I				0.48
4.667	0.06	0.04	0.005	O I				0.49
4.750	0.06	0.04	0.005	O I				0.50
4.833	0.06	0.04	0.005	O I				0.51
4.917	0.06	0.04	0.005	O I				0.53
5.000	0.06	0.04	0.005	O I				0.54
5.083	0.05	0.04	0.006	O I				0.55
5.167	0.05	0.04	0.006	OI				0.56
5.250	0.05	0.04	0.006	OI				0.56
5.333	0.05	0.04	0.006	O I				0.57
5.417	0.06	0.04	0.006	O I				0.58
5.500	0.06	0.04	0.006	O I				0.59
5.583	0.06	0.04	0.006	O I				0.60
5.667	0.06	0.04	0.006	O I				0.61
5.750	0.06	0.04	0.006	O I				0.63
5.833	0.06	0.04	0.006	O I				0.64
5.917	0.06	0.04	0.007	O I				0.66
6.000	0.06	0.04	0.007	O I				0.67
6.083	0.07	0.04	0.007	O I				0.69
6.167	0.07	0.04	0.007	O I				0.71
6.250	0.07	0.04	0.007	O I				0.73
6.333	0.07	0.04	0.008	O I				0.75
6.417	0.07	0.04	0.008	O I				0.77
6.500	0.07	0.04	0.008	O I				0.79

6.583	0.08	0.04	0.008	|	O	|I	|	|	0.81
6.667	0.08	0.04	0.008	|	O	|I	|	|	0.84
6.750	0.08	0.04	0.009	|	O	|I	|	|	0.87
6.833	0.08	0.04	0.009	|	O	|I	|	|	0.89
6.917	0.08	0.04	0.009	|	O	|I	|	|	0.92
7.000	0.08	0.04	0.009	|	O	|I	|	|	0.94
7.083	0.08	0.04	0.010	|	O	|I	|	|	0.97
7.167	0.08	0.04	0.010	|	O	|I	|	|	1.00
7.250	0.08	0.04	0.010	|	O	|I	|	|	1.02
7.333	0.09	0.04	0.010	|	O	| I	|	|	1.05
7.417	0.09	0.04	0.011	|	O	| I	|	|	1.08
7.500	0.09	0.04	0.011	|	O	| I	|	|	1.11
7.583	0.09	0.04	0.011	|	O	| I	|	|	1.15
7.667	0.10	0.04	0.012	|	O	| I	|	|	1.18
7.750	0.10	0.04	0.012	|	O	| I	|	|	1.22
7.833	0.10	0.04	0.013	|	O	| I	|	|	1.26
7.917	0.10	0.04	0.013	|	O	| I	|	|	1.30
8.000	0.10	0.04	0.013	|	O	| I	|	|	1.34
8.083	0.12	0.04	0.014	|	O	| I	|	|	1.39
8.167	0.12	0.04	0.014	|	O	| I |	|	|	1.44
8.250	0.12	0.04	0.015	|	O	| I |	|	|	1.49
8.333	0.12	0.04	0.015	|	O	| I |	|	|	1.53
8.417	0.12	0.04	0.016	|	O	| I |	|	|	1.56
8.500	0.12	0.04	0.017	|	O	| I |	|	|	1.60
8.583	0.13	0.04	0.017	|	O	| I |	|	|	1.63
8.667	0.13	0.04	0.018	|	O	| I|	|	|	1.67
8.750	0.13	0.04	0.018	|	O	| I|	|	|	1.70
8.833	0.13	0.04	0.019	|	O	| I|	|	|	1.74
8.917	0.14	0.04	0.020	|	O	| I	|	|	1.78
9.000	0.14	0.04	0.020	|	O	| I	|	|	1.82
9.083	0.15	0.04	0.021	|	O	| |I	|	|	1.87
9.167	0.15	0.04	0.022	|	O	| |I	|	|	1.91
9.250	0.15	0.04	0.022	|	O	| |I	|	|	1.96
9.333	0.16	0.04	0.023	|	O	| | I	|	|	2.01
9.417	0.16	0.04	0.024	|	O	| | I	|	|	2.05
9.500	0.16	0.04	0.025	|	O	| | I	|	|	2.10
9.583	0.17	0.04	0.026	|	O	| | I	|	|	2.14
9.667	0.17	0.04	0.026	|	O	| | I	|	|	2.19
9.750	0.17	0.04	0.027	|	O	| | I	|	|	2.24
9.833	0.17	0.04	0.028	|	O	| | I	|	|	2.29
9.917	0.18	0.04	0.029	|	O	| | I	|	|	2.34
10.000	0.18	0.04	0.030	|	O	| | I	|	|	2.39
10.083	0.13	0.04	0.031	|	O	| I|	|	|	2.43
10.167	0.12	0.04	0.031	|	O	| I |	|	|	2.46
10.250	0.12	0.04	0.032	|	O	| I |	|	|	2.49
10.333	0.12	0.04	0.032	|	O	| I |	|	|	2.52
10.417	0.12	0.04	0.033	|	O	| I |	|	|	2.55
10.500	0.12	0.04	0.034	|	O	| I |	|	|	2.58
10.583	0.15	0.04	0.034	|	O	| |I	|	|	2.62
10.667	0.16	0.04	0.035	|	O	| | I	|	|	2.66
10.750	0.16	0.04	0.036	|	O	| | I	|	|	2.71
10.833	0.16	0.04	0.037	|	O	| | I	|	|	2.75
10.917	0.16	0.04	0.037	|	O	| | I	|	|	2.80

11.000	0.16	0.04	0.038	O		I			2.84
11.083	0.15	0.04	0.039	O		I			2.89
11.167	0.15	0.04	0.040	O	I				2.93
11.250	0.15	0.04	0.040	O	I				2.97
11.333	0.15	0.04	0.041	O	I				3.01
11.417	0.15	0.04	0.042	O	I				3.05
11.500	0.15	0.04	0.043	O	I				3.09
11.583	0.14	0.04	0.043	O	I				3.12
11.667	0.14	0.04	0.044	O	I				3.15
11.750	0.14	0.04	0.045	O	I				3.19
11.833	0.14	0.04	0.045	O	I				3.22
11.917	0.14	0.04	0.046	O	I				3.26
12.000	0.14	0.04	0.047	O	I				3.29
12.083	0.18	0.04	0.048	O		I			3.33
12.167	0.20	0.04	0.049	O		I			3.38
12.250	0.20	0.04	0.050	O		I			3.44
12.333	0.21	0.04	0.051	O		I			3.49
12.417	0.21	0.04	0.052	O		I			3.55
12.500	0.21	0.04	0.053	O		I			3.61
12.583	0.22	0.04	0.054	O		I			3.67
12.667	0.22	0.04	0.056	O		I			3.73
12.750	0.22	0.04	0.057	O		I			3.79
12.833	0.23	0.04	0.058	O		I			3.85
12.917	0.23	0.04	0.059	O		I			3.92
13.000	0.23	0.04	0.061	O		I			3.98
13.083	0.26	0.04	0.062	O				I	4.05
13.167	0.27	0.04	0.064	O				I	4.13
13.250	0.27	0.04	0.065	O				I	4.21
13.333	0.27	0.04	0.067	O				I	4.29
13.417	0.27	0.04	0.068	O				I	4.37
13.500	0.27	0.04	0.070	O				I	4.45
13.583	0.21	0.04	0.071	O		I			4.51
13.667	0.18	0.04	0.072	O		I			4.57
13.750	0.18	0.04	0.073	O		I			4.62
13.833	0.18	0.04	0.074	O		I			4.66
13.917	0.18	0.04	0.075	O		I			4.71
14.000	0.18	0.04	0.076	O		I			4.76
14.083	0.21	0.04	0.077	O		I			4.81
14.167	0.22	0.04	0.078	O		I			4.87
14.250	0.22	0.04	0.080	O		I			4.93
14.333	0.21	0.04	0.081	O		I			4.99
14.417	0.21	0.04	0.082	O		I			5.05
14.500	0.21	0.04	0.083	O		I			5.12
14.583	0.21	0.04	0.084	O		I			5.18
14.667	0.21	0.04	0.085	O		I			5.24
14.750	0.21	0.04	0.087	O		I			5.31
14.833	0.20	0.04	0.088	O		I			5.37
14.917	0.20	0.04	0.089	O		I			5.43
15.000	0.20	0.04	0.090	O		I			5.49
15.083	0.19	0.04	0.091	O		I			5.56
15.167	0.19	0.04	0.092	O		I			5.64
15.250	0.19	0.04	0.093	O		I			5.71
15.333	0.19	0.04	0.094	O		I			5.78

15.417	0.18	0.04	0.095	O		I		5.85
15.500	0.18	0.04	0.096	O		I		5.92
15.583	0.16	0.04	0.097	O	I			5.99
15.667	0.15	0.04	0.098	O	I			6.05
15.750	0.15	0.04	0.098	O	I			6.11
15.833	0.15	0.04	0.099	O	I			6.18
15.917	0.15	0.04	0.100	O	I			6.24
16.000	0.15	0.04	0.101	O	I			6.30
16.083	0.06	0.04	0.101	O I				6.34
16.167	0.03	0.04	0.101	IO				6.34
16.250	0.03	0.04	0.101	IO				6.34
16.333	0.03	0.04	0.101	IO				6.33
16.417	0.03	0.04	0.101	IO				6.33
16.500	0.03	0.04	0.101	IO				6.32
16.583	0.03	0.04	0.101	IO				6.31
16.667	0.02	0.04	0.101	I O				6.30
16.750	0.02	0.04	0.101	I O				6.29
16.833	0.02	0.04	0.100	I O				6.28
16.917	0.02	0.04	0.100	I O				6.27
17.000	0.02	0.04	0.100	I O				6.26
17.083	0.04	0.04	0.100	O				6.25
17.167	0.04	0.04	0.100	O				6.25
17.250	0.04	0.04	0.100	O				6.25
17.333	0.04	0.04	0.100	O				6.25
17.417	0.04	0.04	0.100	O				6.25
17.500	0.04	0.04	0.100	O				6.25
17.583	0.04	0.04	0.100	O				6.25
17.667	0.04	0.04	0.100	O				6.24
17.750	0.04	0.04	0.100	O				6.24
17.833	0.03	0.04	0.100	O				6.24
17.917	0.03	0.04	0.100	IO				6.24
18.000	0.03	0.04	0.100	IO				6.23
18.083	0.03	0.04	0.100	IO				6.22
18.167	0.03	0.04	0.100	IO				6.22
18.250	0.03	0.04	0.100	IO				6.21
18.333	0.03	0.04	0.099	IO				6.21
18.417	0.03	0.04	0.099	IO				6.20
18.500	0.03	0.04	0.099	IO				6.19
18.583	0.03	0.04	0.099	IO				6.19
18.667	0.02	0.04	0.099	I O				6.18
18.750	0.02	0.04	0.099	I O				6.17
18.833	0.02	0.04	0.099	I O				6.15
18.917	0.02	0.04	0.099	I O				6.14
19.000	0.02	0.04	0.099	I O				6.13
19.083	0.02	0.04	0.098	I O				6.11
19.167	0.02	0.04	0.098	I O				6.10
19.250	0.02	0.04	0.098	I O				6.09
19.333	0.03	0.04	0.098	IO				6.08
19.417	0.03	0.04	0.098	IO				6.08
19.500	0.03	0.04	0.098	IO				6.07
19.583	0.03	0.04	0.098	IO				6.06
19.667	0.02	0.04	0.098	I O				6.05
19.750	0.02	0.04	0.098	I O				6.04

19.833	0.02	0.04	0.097	| I O	|	|	|	6.03
19.917	0.02	0.04	0.097	|I O	|	|	|	6.02
20.000	0.02	0.04	0.097	|I O	|	|	|	6.00
20.083	0.02	0.04	0.097	| I O	|	|	|	5.99
20.167	0.02	0.04	0.097	| I O	|	|	|	5.98
20.250	0.02	0.04	0.097	| I O	|	|	|	5.97
20.333	0.02	0.04	0.096	| I O	|	|	|	5.96
20.417	0.02	0.04	0.096	| I O	|	|	|	5.95
20.500	0.02	0.04	0.096	| I O	|	|	|	5.94
20.583	0.02	0.04	0.096	| I O	|	|	|	5.94
20.667	0.02	0.04	0.096	| I O	|	|	|	5.93
20.750	0.02	0.04	0.096	| I O	|	|	|	5.92
20.833	0.02	0.04	0.096	| I O	|	|	|	5.91
20.917	0.02	0.04	0.096	|I O	|	|	|	5.90
21.000	0.02	0.04	0.095	|I O	|	|	|	5.88
21.083	0.02	0.04	0.095	| I O	|	|	|	5.87
21.167	0.02	0.04	0.095	| I O	|	|	|	5.86
21.250	0.02	0.04	0.095	| I O	|	|	|	5.85
21.333	0.02	0.04	0.095	| I O	|	|	|	5.84
21.417	0.02	0.04	0.095	|I O	|	|	|	5.83
21.500	0.02	0.04	0.094	|I O	|	|	|	5.82
21.583	0.02	0.04	0.094	| I O	|	|	|	5.81
21.667	0.02	0.04	0.094	| I O	|	|	|	5.80
21.750	0.02	0.04	0.094	| I O	|	|	|	5.79
21.833	0.02	0.04	0.094	| I O	|	|	|	5.78
21.917	0.02	0.04	0.094	|I O	|	|	|	5.77
22.000	0.02	0.04	0.094	|I O	|	|	|	5.75
22.083	0.02	0.04	0.093	| I O	|	|	|	5.74
22.167	0.02	0.04	0.093	| I O	|	|	|	5.73
22.250	0.02	0.04	0.093	| I O	|	|	|	5.72
22.333	0.02	0.04	0.093	| I O	|	|	|	5.71
22.417	0.02	0.04	0.093	|I O	|	|	|	5.70
22.500	0.02	0.04	0.093	|I O	|	|	|	5.69
22.583	0.02	0.04	0.092	|I O	|	|	|	5.67
22.667	0.02	0.04	0.092	|I O	|	|	|	5.66
22.750	0.02	0.04	0.092	|I O	|	|	|	5.65
22.833	0.02	0.04	0.092	|I O	|	|	|	5.64
22.917	0.02	0.04	0.092	|I O	|	|	|	5.62
23.000	0.02	0.04	0.092	|I O	|	|	|	5.61
23.083	0.02	0.04	0.091	|I O	|	|	|	5.60
23.167	0.02	0.04	0.091	|I O	|	|	|	5.58
23.250	0.02	0.04	0.091	|I O	|	|	|	5.57
23.333	0.02	0.04	0.091	|I O	|	|	|	5.56
23.417	0.02	0.04	0.091	|I O	|	|	|	5.55
23.500	0.02	0.04	0.090	|I O	|	|	|	5.53
23.583	0.02	0.04	0.090	|I O	|	|	|	5.52
23.667	0.02	0.04	0.090	|I O	|	|	|	5.51
23.750	0.02	0.04	0.090	|I O	|	|	|	5.50
23.833	0.02	0.04	0.090	|I O	|	|	|	5.49
23.917	0.02	0.04	0.090	|I O	|	|	|	5.48
24.000	0.02	0.04	0.089	|I O	|	|	|	5.47
24.083	0.00	0.04	0.089	I O	|	|	|	5.45
24.167	0.00	0.04	0.089	I O	|	|	|	5.44

24.250	0.00	0.04	0.089	I	O	|	|	|	|	5.42
24.333	0.00	0.04	0.088	I	O	|	|	|	|	5.41
24.417	0.00	0.04	0.088	I	O	|	|	|	|	5.39
24.500	0.00	0.04	0.088	I	O	|	|	|	|	5.37
24.583	0.00	0.04	0.087	I	O	|	|	|	|	5.36
24.667	0.00	0.04	0.087	I	O	|	|	|	|	5.34
24.750	0.00	0.04	0.087	I	O	|	|	|	|	5.33
24.833	0.00	0.04	0.087	I	O	|	|	|	|	5.31
24.917	0.00	0.04	0.086	I	O	|	|	|	|	5.29
25.000	0.00	0.04	0.086	I	O	|	|	|	|	5.28
25.083	0.00	0.04	0.086	I	O	|	|	|	|	5.26
25.167	0.00	0.04	0.085	I	O	|	|	|	|	5.25
25.250	0.00	0.04	0.085	I	O	|	|	|	|	5.23
25.333	0.00	0.04	0.085	I	O	|	|	|	|	5.21
25.417	0.00	0.04	0.085	I	O	|	|	|	|	5.20
25.500	0.00	0.04	0.084	I	O	|	|	|	|	5.18
25.583	0.00	0.04	0.084	I	O	|	|	|	|	5.17
25.667	0.00	0.04	0.084	I	O	|	|	|	|	5.15
25.750	0.00	0.04	0.083	I	O	|	|	|	|	5.13
25.833	0.00	0.04	0.083	I	O	|	|	|	|	5.12
25.917	0.00	0.04	0.083	I	O	|	|	|	|	5.10
26.000	0.00	0.04	0.083	I	O	|	|	|	|	5.09
26.083	0.00	0.04	0.082	I	O	|	|	|	|	5.07
26.167	0.00	0.04	0.082	I	O	|	|	|	|	5.05
26.250	0.00	0.04	0.082	I	O	|	|	|	|	5.04
26.333	0.00	0.04	0.081	I	O	|	|	|	|	5.02
26.417	0.00	0.04	0.081	I	O	|	|	|	|	5.01
26.500	0.00	0.04	0.081	I	O	|	|	|	|	4.99
26.583	0.00	0.04	0.081	I	O	|	|	|	|	4.98
26.667	0.00	0.04	0.080	I	O	|	|	|	|	4.96
26.750	0.00	0.04	0.080	I	O	|	|	|	|	4.95
26.833	0.00	0.04	0.080	I	O	|	|	|	|	4.93
26.917	0.00	0.04	0.079	I	O	|	|	|	|	4.92
27.000	0.00	0.04	0.079	I	O	|	|	|	|	4.90
27.083	0.00	0.04	0.079	I	O	|	|	|	|	4.89
27.167	0.00	0.04	0.078	I	O	|	|	|	|	4.87
27.250	0.00	0.04	0.078	I	O	|	|	|	|	4.86
27.333	0.00	0.04	0.078	I	O	|	|	|	|	4.85
27.417	0.00	0.04	0.078	I	O	|	|	|	|	4.83
27.500	0.00	0.04	0.077	I	O	|	|	|	|	4.82
27.583	0.00	0.04	0.077	I	O	|	|	|	|	4.80
27.667	0.00	0.04	0.077	I	O	|	|	|	|	4.79
27.750	0.00	0.04	0.076	I	O	|	|	|	|	4.77
27.833	0.00	0.04	0.076	I	O	|	|	|	|	4.76
27.917	0.00	0.04	0.076	I	O	|	|	|	|	4.74
28.000	0.00	0.04	0.076	I	O	|	|	|	|	4.73
28.083	0.00	0.04	0.075	I	O	|	|	|	|	4.72
28.167	0.00	0.04	0.075	I	O	|	|	|	|	4.70
28.250	0.00	0.04	0.075	I	O	|	|	|	|	4.69
28.333	0.00	0.04	0.074	I	O	|	|	|	|	4.67
28.417	0.00	0.04	0.074	I	O	|	|	|	|	4.66
28.500	0.00	0.04	0.074	I	O	|	|	|	|	4.64
28.583	0.00	0.04	0.074	I	O	|	|	|	|	4.63

28.667	0.00	0.04	0.073	I	O	|	|	|	|	4.61
28.750	0.00	0.04	0.073	I	O	|	|	|	|	4.60
28.833	0.00	0.04	0.073	I	O	|	|	|	|	4.59
28.917	0.00	0.04	0.072	I	O	|	|	|	|	4.57
29.000	0.00	0.04	0.072	I	O	|	|	|	|	4.56
29.083	0.00	0.04	0.072	I	O	|	|	|	|	4.54
29.167	0.00	0.04	0.072	I	O	|	|	|	|	4.53
29.250	0.00	0.04	0.071	I	O	|	|	|	|	4.51
29.333	0.00	0.04	0.071	I	O	|	|	|	|	4.50
29.417	0.00	0.04	0.071	I	O	|	|	|	|	4.48
29.500	0.00	0.04	0.070	I	O	|	|	|	|	4.47
29.583	0.00	0.04	0.070	I	O	|	|	|	|	4.45
29.667	0.00	0.04	0.070	I	O	|	|	|	|	4.44
29.750	0.00	0.04	0.070	I	O	|	|	|	|	4.43
29.833	0.00	0.04	0.069	I	O	|	|	|	|	4.41
29.917	0.00	0.04	0.069	I	O	|	|	|	|	4.40
30.000	0.00	0.04	0.069	I	O	|	|	|	|	4.38
30.083	0.00	0.04	0.068	I	O	|	|	|	|	4.37
30.167	0.00	0.04	0.068	I	O	|	|	|	|	4.35
30.250	0.00	0.04	0.068	I	O	|	|	|	|	4.34
30.333	0.00	0.04	0.067	I	O	|	|	|	|	4.32
30.417	0.00	0.04	0.067	I	O	|	|	|	|	4.31
30.500	0.00	0.04	0.067	I	O	|	|	|	|	4.30
30.583	0.00	0.04	0.067	I	O	|	|	|	|	4.28
30.667	0.00	0.04	0.066	I	O	|	|	|	|	4.27
30.750	0.00	0.04	0.066	I	O	|	|	|	|	4.25
30.833	0.00	0.04	0.066	I	O	|	|	|	|	4.24
30.917	0.00	0.04	0.065	I	O	|	|	|	|	4.22
31.000	0.00	0.04	0.065	I	O	|	|	|	|	4.21
31.083	0.00	0.04	0.065	I	O	|	|	|	|	4.19
31.167	0.00	0.04	0.065	I	O	|	|	|	|	4.18
31.250	0.00	0.04	0.064	I	O	|	|	|	|	4.17
31.333	0.00	0.04	0.064	I	O	|	|	|	|	4.15
31.417	0.00	0.04	0.064	I	O	|	|	|	|	4.14
31.500	0.00	0.04	0.063	I	O	|	|	|	|	4.12
31.583	0.00	0.04	0.063	I	O	|	|	|	|	4.11
31.667	0.00	0.04	0.063	I	O	|	|	|	|	4.09
31.750	0.00	0.04	0.063	I	O	|	|	|	|	4.08
31.833	0.00	0.04	0.062	I	O	|	|	|	|	4.06
31.917	0.00	0.04	0.062	I	O	|	|	|	|	4.05
32.000	0.00	0.04	0.062	I	O	|	|	|	|	4.04
32.083	0.00	0.04	0.061	I	O	|	|	|	|	4.02
32.167	0.00	0.04	0.061	I	O	|	|	|	|	4.01
32.250	0.00	0.04	0.061	I	O	|	|	|	|	3.99
32.333	0.00	0.04	0.061	I	O	|	|	|	|	3.98
32.417	0.00	0.04	0.060	I	O	|	|	|	|	3.96
32.500	0.00	0.04	0.060	I	O	|	|	|	|	3.95
32.583	0.00	0.04	0.060	I	O	|	|	|	|	3.93
32.667	0.00	0.04	0.059	I	O	|	|	|	|	3.92
32.750	0.00	0.04	0.059	I	O	|	|	|	|	3.91
32.833	0.00	0.04	0.059	I	O	|	|	|	|	3.89
32.917	0.00	0.04	0.059	I	O	|	|	|	|	3.88
33.000	0.00	0.04	0.058	I	O	|	|	|	|	3.86

33.083	0.00	0.04	0.058	I	O	|	|	|	|	3.85
33.167	0.00	0.04	0.058	I	O	|	|	|	|	3.83
33.250	0.00	0.04	0.057	I	O	|	|	|	|	3.82
33.333	0.00	0.04	0.057	I	O	|	|	|	|	3.80
33.417	0.00	0.04	0.057	I	O	|	|	|	|	3.79
33.500	0.00	0.04	0.057	I	O	|	|	|	|	3.78
33.583	0.00	0.04	0.056	I	O	|	|	|	|	3.76
33.667	0.00	0.04	0.056	I	O	|	|	|	|	3.75
33.750	0.00	0.04	0.056	I	O	|	|	|	|	3.73
33.833	0.00	0.04	0.055	I	O	|	|	|	|	3.72
33.917	0.00	0.04	0.055	I	O	|	|	|	|	3.70
34.000	0.00	0.04	0.055	I	O	|	|	|	|	3.69
34.083	0.00	0.04	0.054	I	O	|	|	|	|	3.67
34.167	0.00	0.04	0.054	I	O	|	|	|	|	3.66
34.250	0.00	0.04	0.054	I	O	|	|	|	|	3.65
34.333	0.00	0.04	0.054	I	O	|	|	|	|	3.63
34.417	0.00	0.04	0.053	I	O	|	|	|	|	3.62
34.500	0.00	0.04	0.053	I	O	|	|	|	|	3.60
34.583	0.00	0.04	0.053	I	O	|	|	|	|	3.59
34.667	0.00	0.04	0.052	I	O	|	|	|	|	3.57
34.750	0.00	0.04	0.052	I	O	|	|	|	|	3.56
34.833	0.00	0.04	0.052	I	O	|	|	|	|	3.54
34.917	0.00	0.04	0.052	I	O	|	|	|	|	3.53
35.000	0.00	0.04	0.051	I	O	|	|	|	|	3.51
35.083	0.00	0.04	0.051	I	O	|	|	|	|	3.50
35.167	0.00	0.04	0.051	I	O	|	|	|	|	3.49
35.250	0.00	0.04	0.050	I	O	|	|	|	|	3.47
35.333	0.00	0.04	0.050	I	O	|	|	|	|	3.46
35.417	0.00	0.04	0.050	I	O	|	|	|	|	3.44
35.500	0.00	0.04	0.050	I	O	|	|	|	|	3.43
35.583	0.00	0.04	0.049	I	O	|	|	|	|	3.41
35.667	0.00	0.04	0.049	I	O	|	|	|	|	3.40
35.750	0.00	0.04	0.049	I	O	|	|	|	|	3.38
35.833	0.00	0.04	0.048	I	O	|	|	|	|	3.37
35.917	0.00	0.04	0.048	I	O	|	|	|	|	3.36
36.000	0.00	0.04	0.048	I	O	|	|	|	|	3.34
36.083	0.00	0.04	0.048	I	O	|	|	|	|	3.33
36.167	0.00	0.04	0.047	I	O	|	|	|	|	3.31
36.250	0.00	0.04	0.047	I	O	|	|	|	|	3.30
36.333	0.00	0.04	0.047	I	O	|	|	|	|	3.28
36.417	0.00	0.04	0.046	I	O	|	|	|	|	3.27
36.500	0.00	0.04	0.046	I	O	|	|	|	|	3.25
36.583	0.00	0.04	0.046	I	O	|	|	|	|	3.24
36.667	0.00	0.04	0.046	I	O	|	|	|	|	3.23
36.750	0.00	0.04	0.045	I	O	|	|	|	|	3.21
36.833	0.00	0.04	0.045	I	O	|	|	|	|	3.20
36.917	0.00	0.04	0.045	I	O	|	|	|	|	3.18
37.000	0.00	0.04	0.044	I	O	|	|	|	|	3.17
37.083	0.00	0.04	0.044	I	O	|	|	|	|	3.15
37.167	0.00	0.04	0.044	I	O	|	|	|	|	3.14
37.250	0.00	0.04	0.043	I	O	|	|	|	|	3.12
37.333	0.00	0.04	0.043	I	O	|	|	|	|	3.11
37.417	0.00	0.04	0.043	I	O	|	|	|	|	3.10

37.500	0.00	0.04	0.043	I	O	|	|	|	|	3.08
37.583	0.00	0.04	0.042	I	O	|	|	|	|	3.07
37.667	0.00	0.04	0.042	I	O	|	|	|	|	3.05
37.750	0.00	0.04	0.042	I	O	|	|	|	|	3.04
37.833	0.00	0.04	0.041	I	O	|	|	|	|	3.02
37.917	0.00	0.04	0.041	I	O	|	|	|	|	3.01
38.000	0.00	0.04	0.041	I	O	|	|	|	|	2.99
38.083	0.00	0.04	0.041	I	O	|	|	|	|	2.98
38.167	0.00	0.04	0.040	I	O	|	|	|	|	2.96
38.250	0.00	0.04	0.040	I	O	|	|	|	|	2.95
38.333	0.00	0.04	0.040	I	O	|	|	|	|	2.93
38.417	0.00	0.04	0.039	I	O	|	|	|	|	2.91
38.500	0.00	0.04	0.039	I	O	|	|	|	|	2.90
38.583	0.00	0.04	0.039	I	O	|	|	|	|	2.88
38.667	0.00	0.04	0.039	I	O	|	|	|	|	2.87
38.750	0.00	0.04	0.038	I	O	|	|	|	|	2.85
38.833	0.00	0.04	0.038	I	O	|	|	|	|	2.83
38.917	0.00	0.04	0.038	I	O	|	|	|	|	2.82
39.000	0.00	0.04	0.037	I	O	|	|	|	|	2.80
39.083	0.00	0.04	0.037	I	O	|	|	|	|	2.78
39.167	0.00	0.04	0.037	I	O	|	|	|	|	2.77
39.250	0.00	0.04	0.037	I	O	|	|	|	|	2.75
39.333	0.00	0.04	0.036	I	O	|	|	|	|	2.74
39.417	0.00	0.04	0.036	I	O	|	|	|	|	2.72
39.500	0.00	0.04	0.036	I	O	|	|	|	|	2.70
39.583	0.00	0.04	0.035	I	O	|	|	|	|	2.69
39.667	0.00	0.04	0.035	I	O	|	|	|	|	2.67
39.750	0.00	0.04	0.035	I	O	|	|	|	|	2.66
39.833	0.00	0.04	0.035	I	O	|	|	|	|	2.64
39.917	0.00	0.04	0.034	I	O	|	|	|	|	2.62
40.000	0.00	0.04	0.034	I	O	|	|	|	|	2.61
40.083	0.00	0.04	0.034	I	O	|	|	|	|	2.59
40.167	0.00	0.04	0.033	I	O	|	|	|	|	2.58
40.250	0.00	0.04	0.033	I	O	|	|	|	|	2.56
40.333	0.00	0.04	0.033	I	O	|	|	|	|	2.54
40.417	0.00	0.04	0.032	I	O	|	|	|	|	2.53
40.500	0.00	0.04	0.032	I	O	|	|	|	|	2.51
40.583	0.00	0.04	0.032	I	O	|	|	|	|	2.50
40.667	0.00	0.04	0.032	I	O	|	|	|	|	2.48
40.750	0.00	0.04	0.031	I	O	|	|	|	|	2.46
40.833	0.00	0.04	0.031	I	O	|	|	|	|	2.45
40.917	0.00	0.04	0.031	I	O	|	|	|	|	2.43
41.000	0.00	0.04	0.030	I	O	|	|	|	|	2.42
41.083	0.00	0.04	0.030	I	O	|	|	|	|	2.40
41.167	0.00	0.04	0.030	I	O	|	|	|	|	2.38
41.250	0.00	0.04	0.030	I	O	|	|	|	|	2.37
41.333	0.00	0.04	0.029	I	O	|	|	|	|	2.35
41.417	0.00	0.04	0.029	I	O	|	|	|	|	2.33
41.500	0.00	0.04	0.029	I	O	|	|	|	|	2.32
41.583	0.00	0.04	0.028	I	O	|	|	|	|	2.30
41.667	0.00	0.04	0.028	I	O	|	|	|	|	2.29
41.750	0.00	0.04	0.028	I	O	|	|	|	|	2.27
41.833	0.00	0.04	0.028	I	O	|	|	|	|	2.25

41.917	0.00	0.04	0.027	I	O	|	|	|	|	2.24
42.000	0.00	0.04	0.027	I	O	|	|	|	|	2.22
42.083	0.00	0.04	0.027	I	O	|	|	|	|	2.21
42.167	0.00	0.04	0.026	I	O	|	|	|	|	2.19
42.250	0.00	0.04	0.026	I	O	|	|	|	|	2.17
42.333	0.00	0.04	0.026	I	O	|	|	|	|	2.16
42.417	0.00	0.04	0.026	I	O	|	|	|	|	2.14
42.500	0.00	0.04	0.025	I	O	|	|	|	|	2.13
42.583	0.00	0.04	0.025	I	O	|	|	|	|	2.11
42.667	0.00	0.04	0.025	I	O	|	|	|	|	2.09
42.750	0.00	0.04	0.024	I	O	|	|	|	|	2.08
42.833	0.00	0.04	0.024	I	O	|	|	|	|	2.06
42.917	0.00	0.04	0.024	I	O	|	|	|	|	2.05
43.000	0.00	0.04	0.024	I	O	|	|	|	|	2.03
43.083	0.00	0.04	0.023	I	O	|	|	|	|	2.01
43.167	0.00	0.04	0.023	I	O	|	|	|	|	2.00
43.250	0.00	0.04	0.023	I	O	|	|	|	|	1.98
43.333	0.00	0.04	0.022	I	O	|	|	|	|	1.96
43.417	0.00	0.04	0.022	I	O	|	|	|	|	1.94
43.500	0.00	0.04	0.022	I	O	|	|	|	|	1.92
43.583	0.00	0.04	0.022	I	O	|	|	|	|	1.91
43.667	0.00	0.04	0.021	I	O	|	|	|	|	1.89
43.750	0.00	0.04	0.021	I	O	|	|	|	|	1.87
43.833	0.00	0.04	0.021	I	O	|	|	|	|	1.85
43.917	0.00	0.04	0.020	I	O	|	|	|	|	1.83
44.000	0.00	0.04	0.020	I	O	|	|	|	|	1.82
44.083	0.00	0.04	0.020	I	O	|	|	|	|	1.80
44.167	0.00	0.04	0.019	I	O	|	|	|	|	1.78
44.250	0.00	0.04	0.019	I	O	|	|	|	|	1.76
44.333	0.00	0.04	0.019	I	O	|	|	|	|	1.74
44.417	0.00	0.04	0.019	I	O	|	|	|	|	1.73
44.500	0.00	0.04	0.018	I	O	|	|	|	|	1.71
44.583	0.00	0.04	0.018	I	O	|	|	|	|	1.69
44.667	0.00	0.04	0.018	I	O	|	|	|	|	1.67
44.750	0.00	0.04	0.017	I	O	|	|	|	|	1.65
44.833	0.00	0.04	0.017	I	O	|	|	|	|	1.64
44.917	0.00	0.04	0.017	I	O	|	|	|	|	1.62
45.000	0.00	0.04	0.017	I	O	|	|	|	|	1.60
45.083	0.00	0.04	0.016	I	O	|	|	|	|	1.58
45.167	0.00	0.04	0.016	I	O	|	|	|	|	1.56
45.250	0.00	0.04	0.016	I	O	|	|	|	|	1.54
45.333	0.00	0.04	0.015	I	O	|	|	|	|	1.53
45.417	0.00	0.04	0.015	I	O	|	|	|	|	1.51
45.500	0.00	0.04	0.015	I	O	|	|	|	|	1.49
45.583	0.00	0.04	0.015	I	O	|	|	|	|	1.46
45.667	0.00	0.04	0.014	I	O	|	|	|	|	1.43
45.750	0.00	0.04	0.014	I	O	|	|	|	|	1.40
45.833	0.00	0.04	0.014	I	O	|	|	|	|	1.37
45.917	0.00	0.04	0.013	I	O	|	|	|	|	1.34
46.000	0.00	0.04	0.013	I	O	|	|	|	|	1.31
46.083	0.00	0.04	0.013	I	O	|	|	|	|	1.28
46.167	0.00	0.04	0.013	I	O	|	|	|	|	1.25
46.250	0.00	0.04	0.012	I	O	|	|	|	|	1.22

46.333	0.00	0.04	0.012	I	O	|	|	|	1.20
46.417	0.00	0.04	0.012	I	O	|	|	|	1.17
46.500	0.00	0.04	0.011	I	O	|	|	|	1.14
46.583	0.00	0.04	0.011	I	O	|	|	|	1.11
46.667	0.00	0.04	0.011	I	O	|	|	|	1.08
46.750	0.00	0.04	0.011	I	O	|	|	|	1.05
46.833	0.00	0.04	0.010	I	O	|	|	|	1.02
46.917	0.00	0.04	0.010	I	O	|	|	|	0.99
47.000	0.00	0.04	0.010	I	O	|	|	|	0.96
47.083	0.00	0.04	0.009	I	O	|	|	|	0.94
47.167	0.00	0.04	0.009	I	O	|	|	|	0.91
47.250	0.00	0.04	0.009	I	O	|	|	|	0.88
47.333	0.00	0.04	0.008	I	O	|	|	|	0.85
47.417	0.00	0.04	0.008	I	O	|	|	|	0.82
47.500	0.00	0.04	0.008	I	O	|	|	|	0.79
47.583	0.00	0.04	0.008	I	O	|	|	|	0.76
47.667	0.00	0.04	0.007	I	O	|	|	|	0.73
47.750	0.00	0.04	0.007	I	O	|	|	|	0.70
47.833	0.00	0.04	0.007	I	O	|	|	|	0.68
47.917	0.00	0.04	0.006	I	O	|	|	|	0.65
48.000	0.00	0.04	0.006	I	O	|	|	|	0.62
48.083	0.00	0.04	0.006	I	O	|	|	|	0.59
48.167	0.00	0.04	0.006	I	O	|	|	|	0.56
48.250	0.00	0.04	0.005	I	O	|	|	|	0.53
48.333	0.00	0.04	0.005	I	O	|	|	|	0.50
48.417	0.00	0.04	0.005	I	O	|	|	|	0.47
48.500	0.00	0.04	0.004	I	O	|	|	|	0.45
48.583	0.00	0.04	0.004	I	O	|	|	|	0.42
48.667	0.00	0.03	0.004	I	O	|	|	|	0.40
48.750	0.00	0.03	0.004	I	O	|	|	|	0.38
48.833	0.00	0.03	0.004	I	O	|	|	|	0.35
48.917	0.00	0.03	0.003	I	O	|	|	|	0.33
49.000	0.00	0.03	0.003	I	O	|	|	|	0.32
49.083	0.00	0.03	0.003	I	O	|	|	|	0.30
49.167	0.00	0.02	0.003	I	O	|	|	|	0.28
49.250	0.00	0.02	0.003	I	O	|	|	|	0.27
49.333	0.00	0.02	0.003	I	O	|	|	|	0.25
49.417	0.00	0.02	0.002	I	O	|	|	|	0.24
49.500	0.00	0.02	0.002	I	O	|	|	|	0.22
49.583	0.00	0.02	0.002	I	O	|	|	|	0.21
49.667	0.00	0.02	0.002	I	O	|	|	|	0.20
49.750	0.00	0.02	0.002	I	O	|	|	|	0.19
49.833	0.00	0.01	0.002	I	O	|	|	|	0.18
49.917	0.00	0.01	0.002	I	O	|	|	|	0.17
50.000	0.00	0.01	0.002	I	O	|	|	|	0.16
50.083	0.00	0.01	0.001	I	O	|	|	|	0.15
50.167	0.00	0.01	0.001	I	O	|	|	|	0.14
50.250	0.00	0.01	0.001	I	O	|	|	|	0.13
50.333	0.00	0.01	0.001	I	O	|	|	|	0.13
50.417	0.00	0.01	0.001	I	O	|	|	|	0.12
50.500	0.00	0.01	0.001	I	O	|	|	|	0.11
50.583	0.00	0.01	0.001	I	O	|	|	|	0.11
50.667	0.00	0.01	0.001	O		|	|	|	0.10

50.750	0.00	0.01	0.001	O	|	|	|	|	0.09
50.833	0.00	0.01	0.001	O	|	|	|	|	0.09
50.917	0.00	0.01	0.001	O	|	|	|	|	0.08
51.000	0.00	0.01	0.001	O	|	|	|	|	0.08
51.083	0.00	0.01	0.001	O	|	|	|	|	0.07
51.167	0.00	0.01	0.001	O	|	|	|	|	0.07
51.250	0.00	0.01	0.001	O	|	|	|	|	0.07
51.333	0.00	0.01	0.001	O	|	|	|	|	0.06
51.417	0.00	0.00	0.001	O	|	|	|	|	0.06
51.500	0.00	0.00	0.001	O	|	|	|	|	0.06
51.583	0.00	0.00	0.001	O	|	|	|	|	0.05
51.667	0.00	0.00	0.000	O	|	|	|	|	0.05
51.750	0.00	0.00	0.000	O	|	|	|	|	0.05
51.833	0.00	0.00	0.000	O	|	|	|	|	0.04
51.917	0.00	0.00	0.000	O	|	|	|	|	0.04
52.000	0.00	0.00	0.000	O	|	|	|	|	0.04
52.083	0.00	0.00	0.000	O	|	|	|	|	0.04
52.167	0.00	0.00	0.000	O	|	|	|	|	0.04
52.250	0.00	0.00	0.000	O	|	|	|	|	0.03
52.333	0.00	0.00	0.000	O	|	|	|	|	0.03
52.417	0.00	0.00	0.000	O	|	|	|	|	0.03
52.500	0.00	0.00	0.000	O	|	|	|	|	0.03
52.583	0.00	0.00	0.000	O	|	|	|	|	0.03
52.667	0.00	0.00	0.000	O	|	|	|	|	0.02
52.750	0.00	0.00	0.000	O	|	|	|	|	0.02
52.833	0.00	0.00	0.000	O	|	|	|	|	0.02
52.917	0.00	0.00	0.000	O	|	|	|	|	0.02
53.000	0.00	0.00	0.000	O	|	|	|	|	0.02
53.083	0.00	0.00	0.000	O	|	|	|	|	0.02
53.167	0.00	0.00	0.000	O	|	|	|	|	0.02
53.250	0.00	0.00	0.000	O	|	|	|	|	0.02
53.333	0.00	0.00	0.000	O	|	|	|	|	0.02
53.417	0.00	0.00	0.000	O	|	|	|	|	0.01
53.500	0.00	0.00	0.000	O	|	|	|	|	0.01
53.583	0.00	0.00	0.000	O	|	|	|	|	0.01
53.667	0.00	0.00	0.000	O	|	|	|	|	0.01
53.750	0.00	0.00	0.000	O	|	|	|	|	0.01

**********HYDROGRAPH DATA**********

Number of intervals = 645
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.042 (CFS)
Total volume = 0.165 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

AREA EE1

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2014
Study date: 07/22/25

ROUTING: BASIN EE1; UNIT HYDROGRAPH EE1

Program License Serial Number 6279

********** HYDROGRAPH INFORMATION **********

From study/file name: AREE124100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 289
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.258 (CFS)
Total volume = 0.157 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

++
Process from Point/Station 101.000 to Point/Station 102.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 289
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
0.500	0.005	0.041	0.005	0.005
1.000	0.010	0.041	0.010	0.010
1.500	0.015	0.041	0.015	0.015
2.000	0.022	0.041	0.022	0.022
2.500	0.031	0.041	0.031	0.031
3.000	0.040	0.041	0.040	0.040
3.500	0.049	0.041	0.049	0.049
4.000	0.059	0.041	0.059	0.059
4.500	0.069	0.041	0.069	0.069
5.000	0.078	0.041	0.078	0.078
5.500	0.087	0.041	0.087	0.087
6.000	0.094	0.041	0.094	0.094
6.500	0.099	0.041	0.099	0.099
7.000	0.104	0.041	0.104	0.104
7.500	0.109	0.041	0.109	0.109
7.580	0.110	0.041	0.110	0.110

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.1	0.13	0.19	0.26	Depth (Ft.)
0.083	0.01	0.00	0.000	OI	|	|	|	|	0.00
0.167	0.02	0.00	0.000	OI	|	|	|	|	0.01
0.250	0.02	0.00	0.000	OI	|	|	|	|	0.02
0.333	0.02	0.00	0.000	O I	|	|	|	|	0.03
0.417	0.02	0.00	0.000	O I	|	|	|	|	0.05
0.500	0.02	0.00	0.001	O I	|	|	|	|	0.06
0.583	0.02	0.01	0.001	O I	|	|	|	|	0.07
0.667	0.02	0.01	0.001	O I	|	|	|	|	0.08
0.750	0.02	0.01	0.001	O I	|	|	|	|	0.09
0.833	0.03	0.01	0.001	|O I	|	|	|	|	0.10
0.917	0.03	0.01	0.001	|O I	|	|	|	|	0.12
1.000	0.03	0.01	0.001	|O I	|	|	|	|	0.13
1.083	0.02	0.01	0.001	|O I	|	|	|	|	0.14
1.167	0.02	0.01	0.002	|OI	|	|	|	|	0.15
1.250	0.02	0.01	0.002	|OI	|	|	|	|	0.16
1.333	0.02	0.01	0.002	|OI	|	|	|	|	0.16
1.417	0.02	0.01	0.002	|OI	|	|	|	|	0.17
1.500	0.02	0.01	0.002	|OI	|	|	|	|	0.18
1.583	0.02	0.01	0.002	|OI	|	|	|	|	0.18
1.667	0.02	0.02	0.002	|OI	|	|	|	|	0.19
1.750	0.02	0.02	0.002	|OI	|	|	|	|	0.19
1.833	0.03	0.02	0.002	| OI	|	|	|	|	0.20
1.917	0.03	0.02	0.002	| OI	|	|	|	|	0.21
2.000	0.03	0.02	0.002	| OI	|	|	|	|	0.22
2.083	0.03	0.02	0.002	| OI	|	|	|	|	0.23

2.167	0.03	0.02	0.002	OI				0.23
2.250	0.03	0.02	0.002	OI				0.24
2.333	0.03	0.02	0.002	OI				0.25
2.417	0.03	0.02	0.003	OI				0.25
2.500	0.03	0.02	0.003	OI				0.26
2.583	0.04	0.02	0.003	O I				0.27
2.667	0.04	0.02	0.003	O I				0.28
2.750	0.04	0.02	0.003	O I				0.29
2.833	0.04	0.02	0.003	OI				0.30
2.917	0.04	0.03	0.003	OI				0.31
3.000	0.04	0.03	0.003	OI				0.32
3.083	0.04	0.03	0.003	OI				0.32
3.167	0.04	0.03	0.003	OI				0.33
3.250	0.04	0.03	0.003	OI				0.34
3.333	0.04	0.03	0.003	OI				0.35
3.417	0.04	0.03	0.004	OI				0.35
3.500	0.04	0.03	0.004	OI				0.36
3.583	0.04	0.03	0.004	OI				0.36
3.667	0.04	0.03	0.004	OI				0.37
3.750	0.04	0.03	0.004	OI				0.37
3.833	0.04	0.03	0.004	O I				0.38
3.917	0.05	0.03	0.004	O I				0.39
4.000	0.05	0.03	0.004	OI				0.40
4.083	0.05	0.03	0.004	OI				0.41
4.167	0.05	0.03	0.004	OI				0.42
4.250	0.05	0.03	0.004	OI				0.42
4.333	0.05	0.04	0.004	O I				0.43
4.417	0.05	0.04	0.004	O I				0.44
4.500	0.05	0.04	0.005	O I				0.45
4.583	0.05	0.04	0.005	O I				0.47
4.667	0.05	0.04	0.005	O I				0.48
4.750	0.05	0.04	0.005	O I				0.48
4.833	0.06	0.04	0.005	O I				0.50
4.917	0.06	0.04	0.005	O I				0.51
5.000	0.06	0.04	0.005	O I				0.52
5.083	0.05	0.04	0.005	OI				0.53
5.167	0.05	0.04	0.005	O				0.54
5.250	0.05	0.04	0.005	O				0.54
5.333	0.05	0.04	0.005	OI				0.54
5.417	0.05	0.04	0.006	OI				0.55
5.500	0.05	0.04	0.006	OI				0.56
5.583	0.06	0.04	0.006	O I				0.57
5.667	0.06	0.04	0.006	O I				0.58
5.750	0.06	0.04	0.006	O I				0.60
5.833	0.06	0.04	0.006	O I				0.61
5.917	0.06	0.04	0.006	O I				0.62
6.000	0.06	0.04	0.006	O I				0.64
6.083	0.07	0.04	0.007	O I				0.65
6.167	0.07	0.04	0.007	O I				0.67
6.250	0.07	0.04	0.007	O I				0.69
6.333	0.07	0.04	0.007	O I				0.71
6.417	0.07	0.04	0.007	O I				0.73
6.500	0.07	0.04	0.007	O I				0.75

6.583	0.07	0.04	0.008	|	O	|I	|	|	0.77
6.667	0.08	0.04	0.008	|	O	|I	|	|	0.79
6.750	0.08	0.04	0.008	|	O	|I	|	|	0.81
6.833	0.08	0.04	0.008	|	O	|I	|	|	0.84
6.917	0.08	0.04	0.009	|	O	|I	|	|	0.86
7.000	0.08	0.04	0.009	|	O	|I	|	|	0.89
7.083	0.08	0.04	0.009	|	O	|I	|	|	0.91
7.167	0.08	0.04	0.009	|	O	|I	|	|	0.93
7.250	0.08	0.04	0.010	|	O	|I	|	|	0.96
7.333	0.08	0.04	0.010	|	O	| I	|	|	0.98
7.417	0.08	0.04	0.010	|	O	| I	|	|	1.01
7.500	0.08	0.04	0.010	|	O	| I	|	|	1.04
7.583	0.09	0.04	0.011	|	O	| I	|	|	1.07
7.667	0.09	0.04	0.011	|	O	| I	|	|	1.11
7.750	0.09	0.04	0.011	|	O	| I	|	|	1.14
7.833	0.10	0.04	0.012	|	O	| I	|	|	1.18
7.917	0.10	0.04	0.012	|	O	| I	|	|	1.22
8.000	0.10	0.04	0.013	|	O	| I	|	|	1.26
8.083	0.11	0.04	0.013	|	O	| I	|	|	1.30
8.167	0.11	0.04	0.013	|	O	| I |	|	|	1.35
8.250	0.11	0.04	0.014	|	O	| I |	|	|	1.40
8.333	0.11	0.04	0.014	|	O	| I |	|	|	1.45
8.417	0.11	0.04	0.015	|	O	| I |	|	|	1.50
8.500	0.11	0.04	0.015	|	O	| I |	|	|	1.53
8.583	0.12	0.04	0.016	|	O	| I |	|	|	1.57
8.667	0.12	0.04	0.017	|	O	| I|	|	|	1.61
8.750	0.12	0.04	0.017	|	O	| I|	|	|	1.65
8.833	0.13	0.04	0.018	|	O	| I|	|	|	1.69
8.917	0.13	0.04	0.018	|	O	| I	|	|	1.73
9.000	0.13	0.04	0.019	|	O	| I	|	|	1.78
9.083	0.14	0.04	0.020	|	O	| |I	|	|	1.82
9.167	0.14	0.04	0.020	|	O	| |I	|	|	1.87
9.250	0.14	0.04	0.021	|	O	| |I	|	|	1.92
9.333	0.15	0.04	0.022	|	O	| | I	|	|	1.98
9.417	0.15	0.04	0.022	|	O	| | I	|	|	2.02
9.500	0.15	0.04	0.023	|	O	| | I	|	|	2.07
9.583	0.16	0.04	0.024	|	O	| | I	|	|	2.11
9.667	0.16	0.04	0.025	|	O	| | I	|	|	2.15
9.750	0.16	0.04	0.026	|	O	| | I	|	|	2.20
9.833	0.16	0.04	0.026	|	O	| | I	|	|	2.25
9.917	0.17	0.04	0.027	|	O	| | I	|	|	2.29
10.000	0.17	0.04	0.028	|	O	| | I	|	|	2.34
10.083	0.13	0.04	0.029	|	O	| I|	|	|	2.38
10.167	0.11	0.04	0.029	|	O	| I |	|	|	2.41
10.250	0.11	0.04	0.030	|	O	| I |	|	|	2.44
10.333	0.11	0.04	0.030	|	O	| I |	|	|	2.47
10.417	0.11	0.04	0.031	|	O	| I |	|	|	2.50
10.500	0.11	0.04	0.031	|	O	| I |	|	|	2.52
10.583	0.14	0.04	0.032	|	O	| |I	|	|	2.56
10.667	0.15	0.04	0.033	|	O	| | I	|	|	2.60
10.750	0.15	0.04	0.034	|	O	| | I	|	|	2.64
10.833	0.15	0.04	0.034	|	O	| | I	|	|	2.68
10.917	0.15	0.04	0.035	|	O	| | I	|	|	2.72

11.000	0.15	0.04	0.036	|	O	|	| I	|	2.77
11.083	0.15	0.04	0.037	|	O	|	| I	|	2.81
11.167	0.14	0.04	0.037	|	O	|	|I	|	2.85
11.250	0.14	0.04	0.038	|	O	|	|I	|	2.89
11.333	0.14	0.04	0.039	|	O	|	|I	|	2.93
11.417	0.14	0.04	0.039	|	O	|	|I	|	2.97
11.500	0.14	0.04	0.040	|	O	|	|I	|	3.01
11.583	0.13	0.04	0.041	|	O	|	I	|	3.04
11.667	0.13	0.04	0.041	|	O	|	I	|	3.08
11.750	0.13	0.04	0.042	|	O	|	I	|	3.11
11.833	0.13	0.04	0.043	|	O	|	I	|	3.15
11.917	0.14	0.04	0.043	|	O	|	I	|	3.18
12.000	0.14	0.04	0.044	|	O	|	I	|	3.22
12.083	0.18	0.04	0.045	|	O	|	| I	|	3.26
12.167	0.19	0.04	0.046	|	O	|	| I|	|	3.32
12.250	0.19	0.04	0.047	|	O	|	| I|	|	3.37
12.333	0.20	0.04	0.048	|	O	|	| I	|	3.43
12.417	0.20	0.04	0.049	|	O	|	| I	|	3.49
12.500	0.20	0.04	0.050	|	O	|	| I	|	3.55
12.583	0.21	0.04	0.051	|	O	|	|I	|	3.60
12.667	0.21	0.04	0.052	|	O	|	| I	|	3.66
12.750	0.21	0.04	0.053	|	O	|	| I	|	3.72
12.833	0.22	0.04	0.055	|	O	|	| I	|	3.78
12.917	0.22	0.04	0.056	|	O	|	| I	|	3.84
13.000	0.22	0.04	0.057	|	O	|	| I	|	3.90
13.083	0.25	0.04	0.058	|	O	|	|	I |	3.97
13.167	0.26	0.04	0.060	|	O	|	|	I	4.04
13.250	0.26	0.04	0.061	|	O	|	|	I	4.12
13.333	0.26	0.04	0.063	|	O	|	|	I	4.19
13.417	0.26	0.04	0.064	|	O	|	|	I	4.26
13.500	0.26	0.04	0.066	|	O	|	|	I	4.34
13.583	0.20	0.04	0.067	|	O	|	| I	|	4.40
13.667	0.17	0.04	0.068	|	O	|	| I	|	4.45
13.750	0.17	0.04	0.069	|	O	|	| I	|	4.50
13.833	0.17	0.04	0.070	|	O	|	| I	|	4.55
13.917	0.17	0.04	0.071	|	O	|	| I	|	4.60
14.000	0.17	0.04	0.072	|	O	|	| I	|	4.65
14.083	0.20	0.04	0.073	|	O	|	| I	|	4.71
14.167	0.20	0.04	0.074	|	O	|	|I	|	4.77
14.250	0.20	0.04	0.075	|	O	|	|I	|	4.83
14.333	0.20	0.04	0.076	|	O	|	| I	|	4.89
14.417	0.20	0.04	0.077	|	O	|	| I	|	4.95
14.500	0.20	0.04	0.078	|	O	|	| I	|	5.01
14.583	0.20	0.04	0.079	|	O	|	| I	|	5.07
14.667	0.20	0.04	0.080	|	O	|	| I	|	5.13
14.750	0.20	0.04	0.081	|	O	|	| I	|	5.19
14.833	0.19	0.04	0.083	|	O	|	| I|	|	5.25
14.917	0.19	0.04	0.084	|	O	|	| I|	|	5.31
15.000	0.19	0.04	0.085	|	O	|	| I|	|	5.36
15.083	0.18	0.04	0.086	|	O	|	| I |	|	5.42
15.167	0.18	0.04	0.087	|	O	|	| I |	|	5.47
15.250	0.18	0.04	0.088	|	O	|	| I |	|	5.54
15.333	0.18	0.04	0.088	|	O	|	| I	|	5.61

15.417	0.17	0.04	0.089	| O |	| I |	|	5.67
15.500	0.17	0.04	0.090	| O |	| I |	|	5.74
15.583	0.15	0.04	0.091	| O |	| I |	|	5.80
15.667	0.14	0.04	0.092	| O |	|I |	|	5.85
15.750	0.14	0.04	0.093	| O |	|I |	|	5.90
15.833	0.14	0.04	0.093	| O |	|I |	|	5.95
15.917	0.14	0.04	0.094	| O |	|I |	|	6.00
16.000	0.14	0.04	0.095	| O |	|I |	|	6.07
16.083	0.06	0.04	0.095	| O I|	|	|	6.12
16.167	0.03	0.04	0.095	| I O |	|	|	6.12
16.250	0.03	0.04	0.095	| I O |	|	|	6.11
16.333	0.03	0.04	0.095	| I O |	|	|	6.11
16.417	0.03	0.04	0.095	| I O |	|	|	6.10
16.500	0.03	0.04	0.095	| I O |	|	|	6.09
16.583	0.02	0.04	0.095	| I O |	|	|	6.08
16.667	0.02	0.04	0.095	| I O |	|	|	6.07
16.750	0.02	0.04	0.095	| I O |	|	|	6.06
16.833	0.02	0.04	0.094	| I O |	|	|	6.04
16.917	0.02	0.04	0.094	| I O |	|	|	6.03
17.000	0.02	0.04	0.094	| I O |	|	|	6.02
17.083	0.03	0.04	0.094	| IO |	|	|	6.01
17.167	0.04	0.04	0.094	| IO |	|	|	6.01
17.250	0.04	0.04	0.094	| IO |	|	|	6.00
17.333	0.04	0.04	0.094	| IO |	|	|	6.00
17.417	0.04	0.04	0.094	| IO |	|	|	6.00
17.500	0.04	0.04	0.094	| IO |	|	|	6.00
17.583	0.04	0.04	0.094	| IO |	|	|	6.00
17.667	0.04	0.04	0.094	| IO |	|	|	6.00
17.750	0.04	0.04	0.094	| IO |	|	|	5.99
17.833	0.03	0.04	0.094	| IO |	|	|	5.99
17.917	0.03	0.04	0.094	| I O |	|	|	5.99
18.000	0.03	0.04	0.094	| I O |	|	|	5.98
18.083	0.03	0.04	0.094	| I O |	|	|	5.98
18.167	0.03	0.04	0.094	| I O |	|	|	5.97
18.250	0.03	0.04	0.094	| I O |	|	|	5.97
18.333	0.03	0.04	0.093	| I O |	|	|	5.96
18.417	0.03	0.04	0.093	| I O |	|	|	5.96
18.500	0.03	0.04	0.093	| I O |	|	|	5.95
18.583	0.02	0.04	0.093	| I O |	|	|	5.94
18.667	0.02	0.04	0.093	| I O |	|	|	5.93
18.750	0.02	0.04	0.093	| I O |	|	|	5.93
18.833	0.02	0.04	0.093	| I O |	|	|	5.92
18.917	0.02	0.04	0.093	|I O |	|	|	5.90
19.000	0.02	0.04	0.092	|I O |	|	|	5.89
19.083	0.02	0.04	0.092	| I O |	|	|	5.88
19.167	0.02	0.04	0.092	| I O |	|	|	5.87
19.250	0.02	0.04	0.092	| I O |	|	|	5.86
19.333	0.03	0.04	0.092	| I O |	|	|	5.85
19.417	0.03	0.04	0.092	| I O |	|	|	5.85
19.500	0.03	0.04	0.092	| I O |	|	|	5.84
19.583	0.02	0.04	0.092	| I O |	|	|	5.84
19.667	0.02	0.04	0.092	| I O |	|	|	5.83
19.750	0.02	0.04	0.091	| I O |	|	|	5.82

19.833	0.02	0.04	0.091	| I	O |	|	|	|	5.81
19.917	0.02	0.04	0.091	|I	O |	|	|	|	5.80
20.000	0.02	0.04	0.091	|I	O |	|	|	|	5.78
20.083	0.02	0.04	0.091	| I	O |	|	|	|	5.77
20.167	0.02	0.04	0.091	| I	O |	|	|	|	5.76
20.250	0.02	0.04	0.091	| I	O |	|	|	|	5.75
20.333	0.02	0.04	0.090	| I	O |	|	|	|	5.74
20.417	0.02	0.04	0.090	| I	O |	|	|	|	5.74
20.500	0.02	0.04	0.090	| I	O |	|	|	|	5.73
20.583	0.02	0.04	0.090	| I	O |	|	|	|	5.72
20.667	0.02	0.04	0.090	| I	O |	|	|	|	5.71
20.750	0.02	0.04	0.090	| I	O |	|	|	|	5.70
20.833	0.02	0.04	0.090	| I	O |	|	|	|	5.69
20.917	0.02	0.04	0.089	|I	O |	|	|	|	5.68
21.000	0.02	0.04	0.089	|I	O |	|	|	|	5.66
21.083	0.02	0.04	0.089	| I	O |	|	|	|	5.65
21.167	0.02	0.04	0.089	| I	O |	|	|	|	5.64
21.250	0.02	0.04	0.089	| I	O |	|	|	|	5.63
21.333	0.02	0.04	0.089	| I	O |	|	|	|	5.62
21.417	0.02	0.04	0.089	|I	O |	|	|	|	5.61
21.500	0.02	0.04	0.088	|I	O |	|	|	|	5.60
21.583	0.02	0.04	0.088	| I	O |	|	|	|	5.59
21.667	0.02	0.04	0.088	| I	O |	|	|	|	5.58
21.750	0.02	0.04	0.088	| I	O |	|	|	|	5.57
21.833	0.02	0.04	0.088	| I	O |	|	|	|	5.56
21.917	0.02	0.04	0.088	|I	O |	|	|	|	5.55
22.000	0.02	0.04	0.087	|I	O |	|	|	|	5.53
22.083	0.02	0.04	0.087	| I	O |	|	|	|	5.52
22.167	0.02	0.04	0.087	| I	O |	|	|	|	5.51
22.250	0.02	0.04	0.087	| I	O |	|	|	|	5.50
22.333	0.02	0.04	0.087	| I	O |	|	|	|	5.50
22.417	0.02	0.04	0.087	|I	O |	|	|	|	5.49
22.500	0.02	0.04	0.087	|I	O |	|	|	|	5.48
22.583	0.02	0.04	0.086	|I	O |	|	|	|	5.47
22.667	0.02	0.04	0.086	|I	O |	|	|	|	5.46
22.750	0.02	0.04	0.086	|I	O |	|	|	|	5.45
22.833	0.02	0.04	0.086	|I	O |	|	|	|	5.44
22.917	0.02	0.04	0.086	|I	O |	|	|	|	5.43
23.000	0.02	0.04	0.085	|I	O |	|	|	|	5.42
23.083	0.02	0.04	0.085	|I	O |	|	|	|	5.41
23.167	0.02	0.04	0.085	|I	O |	|	|	|	5.40
23.250	0.02	0.04	0.085	|I	O |	|	|	|	5.39
23.333	0.02	0.04	0.085	|I	O |	|	|	|	5.38
23.417	0.02	0.04	0.085	|I	O |	|	|	|	5.37
23.500	0.02	0.04	0.084	|I	O |	|	|	|	5.36
23.583	0.02	0.04	0.084	|I	O |	|	|	|	5.35
23.667	0.02	0.04	0.084	|I	O |	|	|	|	5.34
23.750	0.02	0.04	0.084	|I	O |	|	|	|	5.33
23.833	0.02	0.04	0.084	|I	O |	|	|	|	5.32
23.917	0.02	0.04	0.084	|I	O |	|	|	|	5.31
24.000	0.02	0.04	0.083	|I	O |	|	|	|	5.30
24.083	0.00	0.04	0.083	I	O |	|	|	|	5.29
24.167	0.00	0.04	0.083	I	O |	|	|	|	5.27

24.250	0.00	0.04	0.083	I	O	|	|	|	|	5.26
24.333	0.00	0.04	0.082	I	O	|	|	|	|	5.24
24.417	0.00	0.04	0.082	I	O	|	|	|	|	5.22
24.500	0.00	0.04	0.082	I	O	|	|	|	|	5.21
24.583	0.00	0.04	0.081	I	O	|	|	|	|	5.19
24.667	0.00	0.04	0.081	I	O	|	|	|	|	5.18
24.750	0.00	0.04	0.081	I	O	|	|	|	|	5.16
24.833	0.00	0.04	0.081	I	O	|	|	|	|	5.15
24.917	0.00	0.04	0.080	I	O	|	|	|	|	5.13
25.000	0.00	0.04	0.080	I	O	|	|	|	|	5.11
25.083	0.00	0.04	0.080	I	O	|	|	|	|	5.10
25.167	0.00	0.04	0.079	I	O	|	|	|	|	5.08
25.250	0.00	0.04	0.079	I	O	|	|	|	|	5.07
25.333	0.00	0.04	0.079	I	O	|	|	|	|	5.05
25.417	0.00	0.04	0.079	I	O	|	|	|	|	5.04
25.500	0.00	0.04	0.078	I	O	|	|	|	|	5.02
25.583	0.00	0.04	0.078	I	O	|	|	|	|	5.00
25.667	0.00	0.04	0.078	I	O	|	|	|	|	4.99
25.750	0.00	0.04	0.078	I	O	|	|	|	|	4.97
25.833	0.00	0.04	0.077	I	O	|	|	|	|	4.96
25.917	0.00	0.04	0.077	I	O	|	|	|	|	4.94
26.000	0.00	0.04	0.077	I	O	|	|	|	|	4.93
26.083	0.00	0.04	0.076	I	O	|	|	|	|	4.91
26.167	0.00	0.04	0.076	I	O	|	|	|	|	4.89
26.250	0.00	0.04	0.076	I	O	|	|	|	|	4.88
26.333	0.00	0.04	0.076	I	O	|	|	|	|	4.86
26.417	0.00	0.04	0.075	I	O	|	|	|	|	4.85
26.500	0.00	0.04	0.075	I	O	|	|	|	|	4.83
26.583	0.00	0.04	0.075	I	O	|	|	|	|	4.82
26.667	0.00	0.04	0.074	I	O	|	|	|	|	4.80
26.750	0.00	0.04	0.074	I	O	|	|	|	|	4.78
26.833	0.00	0.04	0.074	I	O	|	|	|	|	4.77
26.917	0.00	0.04	0.074	I	O	|	|	|	|	4.75
27.000	0.00	0.04	0.073	I	O	|	|	|	|	4.74
27.083	0.00	0.04	0.073	I	O	|	|	|	|	4.72
27.167	0.00	0.04	0.073	I	O	|	|	|	|	4.71
27.250	0.00	0.04	0.072	I	O	|	|	|	|	4.69
27.333	0.00	0.04	0.072	I	O	|	|	|	|	4.67
27.417	0.00	0.04	0.072	I	O	|	|	|	|	4.66
27.500	0.00	0.04	0.072	I	O	|	|	|	|	4.64
27.583	0.00	0.04	0.071	I	O	|	|	|	|	4.63
27.667	0.00	0.04	0.071	I	O	|	|	|	|	4.61
27.750	0.00	0.04	0.071	I	O	|	|	|	|	4.60
27.833	0.00	0.04	0.070	I	O	|	|	|	|	4.58
27.917	0.00	0.04	0.070	I	O	|	|	|	|	4.56
28.000	0.00	0.04	0.070	I	O	|	|	|	|	4.55
28.083	0.00	0.04	0.070	I	O	|	|	|	|	4.53
28.167	0.00	0.04	0.069	I	O	|	|	|	|	4.52
28.250	0.00	0.04	0.069	I	O	|	|	|	|	4.50
28.333	0.00	0.04	0.069	I	O	|	|	|	|	4.49
28.417	0.00	0.04	0.068	I	O	|	|	|	|	4.47
28.500	0.00	0.04	0.068	I	O	|	|	|	|	4.46
28.583	0.00	0.04	0.068	I	O	|	|	|	|	4.45

28.667	0.00	0.04	0.068	I	O	|	|	|	|	4.43
28.750	0.00	0.04	0.067	I	O	|	|	|	|	4.42
28.833	0.00	0.04	0.067	I	O	|	|	|	|	4.40
28.917	0.00	0.04	0.067	I	O	|	|	|	|	4.39
29.000	0.00	0.04	0.066	I	O	|	|	|	|	4.37
29.083	0.00	0.04	0.066	I	O	|	|	|	|	4.36
29.167	0.00	0.04	0.066	I	O	|	|	|	|	4.35
29.250	0.00	0.04	0.066	I	O	|	|	|	|	4.33
29.333	0.00	0.04	0.065	I	O	|	|	|	|	4.32
29.417	0.00	0.04	0.065	I	O	|	|	|	|	4.30
29.500	0.00	0.04	0.065	I	O	|	|	|	|	4.29
29.583	0.00	0.04	0.065	I	O	|	|	|	|	4.28
29.667	0.00	0.04	0.064	I	O	|	|	|	|	4.26
29.750	0.00	0.04	0.064	I	O	|	|	|	|	4.25
29.833	0.00	0.04	0.064	I	O	|	|	|	|	4.23
29.917	0.00	0.04	0.063	I	O	|	|	|	|	4.22
30.000	0.00	0.04	0.063	I	O	|	|	|	|	4.21
30.083	0.00	0.04	0.063	I	O	|	|	|	|	4.19
30.167	0.00	0.04	0.063	I	O	|	|	|	|	4.18
30.250	0.00	0.04	0.062	I	O	|	|	|	|	4.16
30.333	0.00	0.04	0.062	I	O	|	|	|	|	4.15
30.417	0.00	0.04	0.062	I	O	|	|	|	|	4.13
30.500	0.00	0.04	0.061	I	O	|	|	|	|	4.12
30.583	0.00	0.04	0.061	I	O	|	|	|	|	4.11
30.667	0.00	0.04	0.061	I	O	|	|	|	|	4.09
30.750	0.00	0.04	0.061	I	O	|	|	|	|	4.08
30.833	0.00	0.04	0.060	I	O	|	|	|	|	4.06
30.917	0.00	0.04	0.060	I	O	|	|	|	|	4.05
31.000	0.00	0.04	0.060	I	O	|	|	|	|	4.04
31.083	0.00	0.04	0.059	I	O	|	|	|	|	4.02
31.167	0.00	0.04	0.059	I	O	|	|	|	|	4.01
31.250	0.00	0.04	0.059	I	O	|	|	|	|	3.99
31.333	0.00	0.04	0.059	I	O	|	|	|	|	3.98
31.417	0.00	0.04	0.058	I	O	|	|	|	|	3.97
31.500	0.00	0.04	0.058	I	O	|	|	|	|	3.95
31.583	0.00	0.04	0.058	I	O	|	|	|	|	3.94
31.667	0.00	0.04	0.057	I	O	|	|	|	|	3.92
31.750	0.00	0.04	0.057	I	O	|	|	|	|	3.91
31.833	0.00	0.04	0.057	I	O	|	|	|	|	3.89
31.917	0.00	0.04	0.057	I	O	|	|	|	|	3.88
32.000	0.00	0.04	0.056	I	O	|	|	|	|	3.87
32.083	0.00	0.04	0.056	I	O	|	|	|	|	3.85
32.167	0.00	0.04	0.056	I	O	|	|	|	|	3.84
32.250	0.00	0.04	0.055	I	O	|	|	|	|	3.82
32.333	0.00	0.04	0.055	I	O	|	|	|	|	3.81
32.417	0.00	0.04	0.055	I	O	|	|	|	|	3.80
32.500	0.00	0.04	0.055	I	O	|	|	|	|	3.78
32.583	0.00	0.04	0.054	I	O	|	|	|	|	3.77
32.667	0.00	0.04	0.054	I	O	|	|	|	|	3.75
32.750	0.00	0.04	0.054	I	O	|	|	|	|	3.74
32.833	0.00	0.04	0.054	I	O	|	|	|	|	3.73
32.917	0.00	0.04	0.053	I	O	|	|	|	|	3.71
33.000	0.00	0.04	0.053	I	O	|	|	|	|	3.70

33.083	0.00	0.04	0.053	I	O	|	|	|	|	3.68
33.167	0.00	0.04	0.052	I	O	|	|	|	|	3.67
33.250	0.00	0.04	0.052	I	O	|	|	|	|	3.65
33.333	0.00	0.04	0.052	I	O	|	|	|	|	3.64
33.417	0.00	0.04	0.052	I	O	|	|	|	|	3.63
33.500	0.00	0.04	0.051	I	O	|	|	|	|	3.61
33.583	0.00	0.04	0.051	I	O	|	|	|	|	3.60
33.667	0.00	0.04	0.051	I	O	|	|	|	|	3.58
33.750	0.00	0.04	0.050	I	O	|	|	|	|	3.57
33.833	0.00	0.04	0.050	I	O	|	|	|	|	3.56
33.917	0.00	0.04	0.050	I	O	|	|	|	|	3.54
34.000	0.00	0.04	0.050	I	O	|	|	|	|	3.53
34.083	0.00	0.04	0.049	I	O	|	|	|	|	3.51
34.167	0.00	0.04	0.049	I	O	|	|	|	|	3.50
34.250	0.00	0.04	0.049	I	O	|	|	|	|	3.48
34.333	0.00	0.04	0.048	I	O	|	|	|	|	3.47
34.417	0.00	0.04	0.048	I	O	|	|	|	|	3.45
34.500	0.00	0.04	0.048	I	O	|	|	|	|	3.44
34.583	0.00	0.04	0.048	I	O	|	|	|	|	3.42
34.667	0.00	0.04	0.047	I	O	|	|	|	|	3.41
34.750	0.00	0.04	0.047	I	O	|	|	|	|	3.39
34.833	0.00	0.04	0.047	I	O	|	|	|	|	3.37
34.917	0.00	0.04	0.046	I	O	|	|	|	|	3.36
35.000	0.00	0.04	0.046	I	O	|	|	|	|	3.34
35.083	0.00	0.04	0.046	I	O	|	|	|	|	3.33
35.167	0.00	0.04	0.046	I	O	|	|	|	|	3.31
35.250	0.00	0.04	0.045	I	O	|	|	|	|	3.30
35.333	0.00	0.04	0.045	I	O	|	|	|	|	3.28
35.417	0.00	0.04	0.045	I	O	|	|	|	|	3.26
35.500	0.00	0.04	0.044	I	O	|	|	|	|	3.25
35.583	0.00	0.04	0.044	I	O	|	|	|	|	3.23
35.667	0.00	0.04	0.044	I	O	|	|	|	|	3.22
35.750	0.00	0.04	0.044	I	O	|	|	|	|	3.20
35.833	0.00	0.04	0.043	I	O	|	|	|	|	3.19
35.917	0.00	0.04	0.043	I	O	|	|	|	|	3.17
36.000	0.00	0.04	0.043	I	O	|	|	|	|	3.15
36.083	0.00	0.04	0.042	I	O	|	|	|	|	3.14
36.167	0.00	0.04	0.042	I	O	|	|	|	|	3.12
36.250	0.00	0.04	0.042	I	O	|	|	|	|	3.11
36.333	0.00	0.04	0.042	I	O	|	|	|	|	3.09
36.417	0.00	0.04	0.041	I	O	|	|	|	|	3.08
36.500	0.00	0.04	0.041	I	O	|	|	|	|	3.06
36.583	0.00	0.04	0.041	I	O	|	|	|	|	3.04
36.667	0.00	0.04	0.041	I	O	|	|	|	|	3.03
36.750	0.00	0.04	0.040	I	O	|	|	|	|	3.01
36.833	0.00	0.04	0.040	I	O	|	|	|	|	3.00
36.917	0.00	0.04	0.040	I	O	|	|	|	|	2.98
37.000	0.00	0.04	0.039	I	O	|	|	|	|	2.97
37.083	0.00	0.04	0.039	I	O	|	|	|	|	2.95
37.167	0.00	0.04	0.039	I	O	|	|	|	|	2.93
37.250	0.00	0.04	0.039	I	O	|	|	|	|	2.92
37.333	0.00	0.04	0.038	I	O	|	|	|	|	2.90
37.417	0.00	0.04	0.038	I	O	|	|	|	|	2.89

37.500	0.00	0.04	0.038	I	O	|	|	|	|	2.87
37.583	0.00	0.04	0.037	I	O	|	|	|	|	2.86
37.667	0.00	0.04	0.037	I	O	|	|	|	|	2.84
37.750	0.00	0.04	0.037	I	O	|	|	|	|	2.83
37.833	0.00	0.04	0.037	I	O	|	|	|	|	2.81
37.917	0.00	0.04	0.036	I	O	|	|	|	|	2.79
38.000	0.00	0.04	0.036	I	O	|	|	|	|	2.78
38.083	0.00	0.04	0.036	I	O	|	|	|	|	2.76
38.167	0.00	0.04	0.035	I	O	|	|	|	|	2.75
38.250	0.00	0.04	0.035	I	O	|	|	|	|	2.73
38.333	0.00	0.04	0.035	I	O	|	|	|	|	2.72
38.417	0.00	0.04	0.035	I	O	|	|	|	|	2.70
38.500	0.00	0.04	0.034	I	O	|	|	|	|	2.68
38.583	0.00	0.04	0.034	I	O	|	|	|	|	2.67
38.667	0.00	0.04	0.034	I	O	|	|	|	|	2.65
38.750	0.00	0.04	0.033	I	O	|	|	|	|	2.64
38.833	0.00	0.04	0.033	I	O	|	|	|	|	2.62
38.917	0.00	0.04	0.033	I	O	|	|	|	|	2.61
39.000	0.00	0.04	0.033	I	O	|	|	|	|	2.59
39.083	0.00	0.04	0.032	I	O	|	|	|	|	2.57
39.167	0.00	0.04	0.032	I	O	|	|	|	|	2.56
39.250	0.00	0.04	0.032	I	O	|	|	|	|	2.54
39.333	0.00	0.04	0.031	I	O	|	|	|	|	2.53
39.417	0.00	0.04	0.031	I	O	|	|	|	|	2.51
39.500	0.00	0.04	0.031	I	O	|	|	|	|	2.50
39.583	0.00	0.04	0.031	I	O	|	|	|	|	2.48
39.667	0.00	0.04	0.030	I	O	|	|	|	|	2.46
39.750	0.00	0.04	0.030	I	O	|	|	|	|	2.45
39.833	0.00	0.04	0.030	I	O	|	|	|	|	2.43
39.917	0.00	0.04	0.030	I	O	|	|	|	|	2.42
40.000	0.00	0.04	0.029	I	O	|	|	|	|	2.40
40.083	0.00	0.04	0.029	I	O	|	|	|	|	2.39
40.167	0.00	0.04	0.029	I	O	|	|	|	|	2.37
40.250	0.00	0.04	0.028	I	O	|	|	|	|	2.35
40.333	0.00	0.04	0.028	I	O	|	|	|	|	2.34
40.417	0.00	0.04	0.028	I	O	|	|	|	|	2.32
40.500	0.00	0.04	0.028	I	O	|	|	|	|	2.31
40.583	0.00	0.04	0.027	I	O	|	|	|	|	2.29
40.667	0.00	0.04	0.027	I	O	|	|	|	|	2.28
40.750	0.00	0.04	0.027	I	O	|	|	|	|	2.26
40.833	0.00	0.04	0.026	I	O	|	|	|	|	2.24
40.917	0.00	0.04	0.026	I	O	|	|	|	|	2.23
41.000	0.00	0.04	0.026	I	O	|	|	|	|	2.21
41.083	0.00	0.04	0.026	I	O	|	|	|	|	2.20
41.167	0.00	0.04	0.025	I	O	|	|	|	|	2.18
41.250	0.00	0.04	0.025	I	O	|	|	|	|	2.17
41.333	0.00	0.04	0.025	I	O	|	|	|	|	2.15
41.417	0.00	0.04	0.024	I	O	|	|	|	|	2.13
41.500	0.00	0.04	0.024	I	O	|	|	|	|	2.12
41.583	0.00	0.04	0.024	I	O	|	|	|	|	2.10
41.667	0.00	0.04	0.024	I	O	|	|	|	|	2.09
41.750	0.00	0.04	0.023	I	O	|	|	|	|	2.07
41.833	0.00	0.04	0.023	I	O	|	|	|	|	2.06

41.917	0.00	0.04	0.023	I	O	|	|	|	|	2.04
42.000	0.00	0.04	0.022	I	O	|	|	|	|	2.02
42.083	0.00	0.04	0.022	I	O	|	|	|	|	2.01
42.167	0.00	0.04	0.022	I	O	|	|	|	|	1.99
42.250	0.00	0.04	0.022	I	O	|	|	|	|	1.97
42.333	0.00	0.04	0.021	I	O	|	|	|	|	1.95
42.417	0.00	0.04	0.021	I	O	|	|	|	|	1.93
42.500	0.00	0.04	0.021	I	O	|	|	|	|	1.91
42.583	0.00	0.04	0.020	I	O	|	|	|	|	1.89
42.667	0.00	0.04	0.020	I	O	|	|	|	|	1.87
42.750	0.00	0.04	0.020	I	O	|	|	|	|	1.85
42.833	0.00	0.04	0.020	I	O	|	|	|	|	1.83
42.917	0.00	0.04	0.019	I	O	|	|	|	|	1.81
43.000	0.00	0.04	0.019	I	O	|	|	|	|	1.79
43.083	0.00	0.04	0.019	I	O	|	|	|	|	1.77
43.167	0.00	0.04	0.018	I	O	|	|	|	|	1.75
43.250	0.00	0.04	0.018	I	O	|	|	|	|	1.73
43.333	0.00	0.04	0.018	I	O	|	|	|	|	1.71
43.417	0.00	0.04	0.018	I	O	|	|	|	|	1.69
43.500	0.00	0.04	0.017	I	O	|	|	|	|	1.67
43.583	0.00	0.04	0.017	I	O	|	|	|	|	1.65
43.667	0.00	0.04	0.017	I	O	|	|	|	|	1.63
43.750	0.00	0.04	0.017	I	O	|	|	|	|	1.61
43.833	0.00	0.04	0.016	I	O	|	|	|	|	1.59
43.917	0.00	0.04	0.016	I	O	|	|	|	|	1.57
44.000	0.00	0.04	0.016	I	O	|	|	|	|	1.55
44.083	0.00	0.04	0.015	I	O	|	|	|	|	1.53
44.167	0.00	0.04	0.015	I	O	|	|	|	|	1.51
44.250	0.00	0.04	0.015	I	O	|	|	|	|	1.48
44.333	0.00	0.04	0.015	I	O	|	|	|	|	1.45
44.417	0.00	0.04	0.014	I	O	|	|	|	|	1.43
44.500	0.00	0.04	0.014	I	O	|	|	|	|	1.40
44.583	0.00	0.04	0.014	I	O	|	|	|	|	1.37
44.667	0.00	0.04	0.013	I	O	|	|	|	|	1.34
44.750	0.00	0.04	0.013	I	O	|	|	|	|	1.31
44.833	0.00	0.04	0.013	I	O	|	|	|	|	1.28
44.917	0.00	0.04	0.013	I	O	|	|	|	|	1.26
45.000	0.00	0.04	0.012	I	O	|	|	|	|	1.23
45.083	0.00	0.04	0.012	I	O	|	|	|	|	1.20
45.167	0.00	0.04	0.012	I	O	|	|	|	|	1.17
45.250	0.00	0.04	0.011	I	O	|	|	|	|	1.14
45.333	0.00	0.04	0.011	I	O	|	|	|	|	1.12
45.417	0.00	0.04	0.011	I	O	|	|	|	|	1.09
45.500	0.00	0.04	0.011	I	O	|	|	|	|	1.06
45.583	0.00	0.04	0.010	I	O	|	|	|	|	1.03
45.667	0.00	0.04	0.010	I	O	|	|	|	|	1.00
45.750	0.00	0.04	0.010	I	O	|	|	|	|	0.97
45.833	0.00	0.04	0.009	I	O	|	|	|	|	0.95
45.917	0.00	0.04	0.009	I	O	|	|	|	|	0.92
46.000	0.00	0.04	0.009	I	O	|	|	|	|	0.89
46.083	0.00	0.04	0.009	I	O	|	|	|	|	0.86
46.167	0.00	0.04	0.008	I	O	|	|	|	|	0.83
46.250	0.00	0.04	0.008	I	O	|	|	|	|	0.80

46.333	0.00	0.04	0.008	I O	|	|	|	0.78
46.417	0.00	0.04	0.007	I O	|	|	|	0.75
46.500	0.00	0.04	0.007	I O	|	|	|	0.72
46.583	0.00	0.04	0.007	I O	|	|	|	0.69
46.667	0.00	0.04	0.007	I O	|	|	|	0.66
46.750	0.00	0.04	0.006	I O	|	|	|	0.64
46.833	0.00	0.04	0.006	I O	|	|	|	0.61
46.917	0.00	0.04	0.006	I O	|	|	|	0.58
47.000	0.00	0.04	0.006	I O	|	|	|	0.55
47.083	0.00	0.04	0.005	I O	|	|	|	0.52
47.167	0.00	0.04	0.005	I O	|	|	|	0.49
47.250	0.00	0.04	0.005	I O	|	|	|	0.47
47.333	0.00	0.04	0.004	I O	|	|	|	0.44
47.417	0.00	0.03	0.004	I O	|	|	|	0.42
47.500	0.00	0.03	0.004	I O	|	|	|	0.39
47.583	0.00	0.03	0.004	I O	|	|	|	0.37
47.667	0.00	0.03	0.004	I O	|	|	|	0.35
47.750	0.00	0.03	0.003	I O	|	|	|	0.33
47.833	0.00	0.03	0.003	I O	|	|	|	0.31
47.917	0.00	0.02	0.003	I O	|	|	|	0.30
48.000	0.00	0.02	0.003	I O	|	|	|	0.28
48.083	0.00	0.02	0.003	I O	|	|	|	0.27
48.167	0.00	0.02	0.003	I O	|	|	|	0.25
48.250	0.00	0.02	0.002	I O	|	|	|	0.24
48.333	0.00	0.02	0.002	I O	|	|	|	0.22
48.417	0.00	0.02	0.002	I O	|	|	|	0.21
48.500	0.00	0.02	0.002	I O	|	|	|	0.20
48.583	0.00	0.02	0.002	IO	|	|	|	0.19
48.667	0.00	0.01	0.002	IO	|	|	|	0.18
48.750	0.00	0.01	0.002	IO	|	|	|	0.17
48.833	0.00	0.01	0.002	IO	|	|	|	0.16
48.917	0.00	0.01	0.002	IO	|	|	|	0.15
49.000	0.00	0.01	0.001	IO	|	|	|	0.14
49.083	0.00	0.01	0.001	IO	|	|	|	0.13
49.167	0.00	0.01	0.001	IO	|	|	|	0.13
49.250	0.00	0.01	0.001	IO	|	|	|	0.12
49.333	0.00	0.01	0.001	IO	|	|	|	0.11
49.417	0.00	0.01	0.001	IO	|	|	|	0.11
49.500	0.00	0.01	0.001	IO	|	|	|	0.10
49.583	0.00	0.01	0.001	O	|	|	|	0.10
49.667	0.00	0.01	0.001	O	|	|	|	0.09
49.750	0.00	0.01	0.001	O	|	|	|	0.09
49.833	0.00	0.01	0.001	O	|	|	|	0.08
49.917	0.00	0.01	0.001	O	|	|	|	0.08
50.000	0.00	0.01	0.001	O	|	|	|	0.07
50.083	0.00	0.01	0.001	O	|	|	|	0.07
50.167	0.00	0.01	0.001	O	|	|	|	0.06
50.250	0.00	0.01	0.001	O	|	|	|	0.06
50.333	0.00	0.00	0.001	O	|	|	|	0.06
50.417	0.00	0.00	0.001	O	|	|	|	0.05
50.500	0.00	0.00	0.001	O	|	|	|	0.05
50.583	0.00	0.00	0.000	O	|	|	|	0.05
50.667	0.00	0.00	0.000	O	|	|	|	0.05

50.750	0.00	0.00	0.000	O	|	|	|	0.04
50.833	0.00	0.00	0.000	O	|	|	|	0.04
50.917	0.00	0.00	0.000	O	|	|	|	0.04
51.000	0.00	0.00	0.000	O	|	|	|	0.04
51.083	0.00	0.00	0.000	O	|	|	|	0.03
51.167	0.00	0.00	0.000	O	|	|	|	0.03
51.250	0.00	0.00	0.000	O	|	|	|	0.03
51.333	0.00	0.00	0.000	O	|	|	|	0.03
51.417	0.00	0.00	0.000	O	|	|	|	0.03
51.500	0.00	0.00	0.000	O	|	|	|	0.03
51.583	0.00	0.00	0.000	O	|	|	|	0.02
51.667	0.00	0.00	0.000	O	|	|	|	0.02
51.750	0.00	0.00	0.000	O	|	|	|	0.02
51.833	0.00	0.00	0.000	O	|	|	|	0.02
51.917	0.00	0.00	0.000	O	|	|	|	0.02
52.000	0.00	0.00	0.000	O	|	|	|	0.02
52.083	0.00	0.00	0.000	O	|	|	|	0.02
52.167	0.00	0.00	0.000	O	|	|	|	0.02
52.250	0.00	0.00	0.000	O	|	|	|	0.02
52.333	0.00	0.00	0.000	O	|	|	|	0.01
52.417	0.00	0.00	0.000	O	|	|	|	0.01
52.500	0.00	0.00	0.000	O	|	|	|	0.01
52.583	0.00	0.00	0.000	O	|	|	|	0.01
52.667	0.00	0.00	0.000	O	|	|	|	0.01

**********HYDROGRAPH DATA**********

Number of intervals = 632
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.041 (CFS)
Total volume = 0.157 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

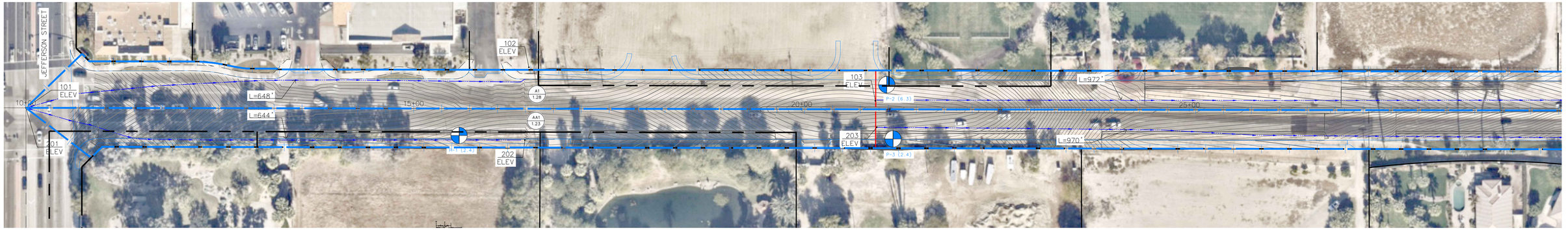
****

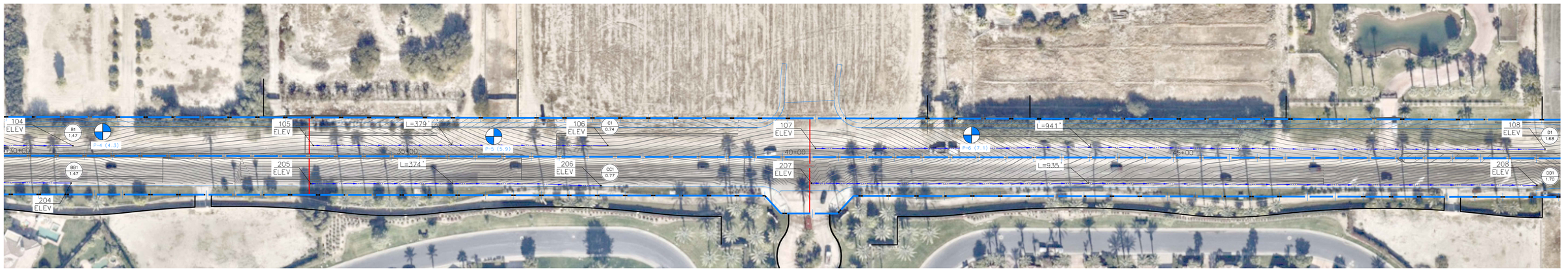
EXHIBITS

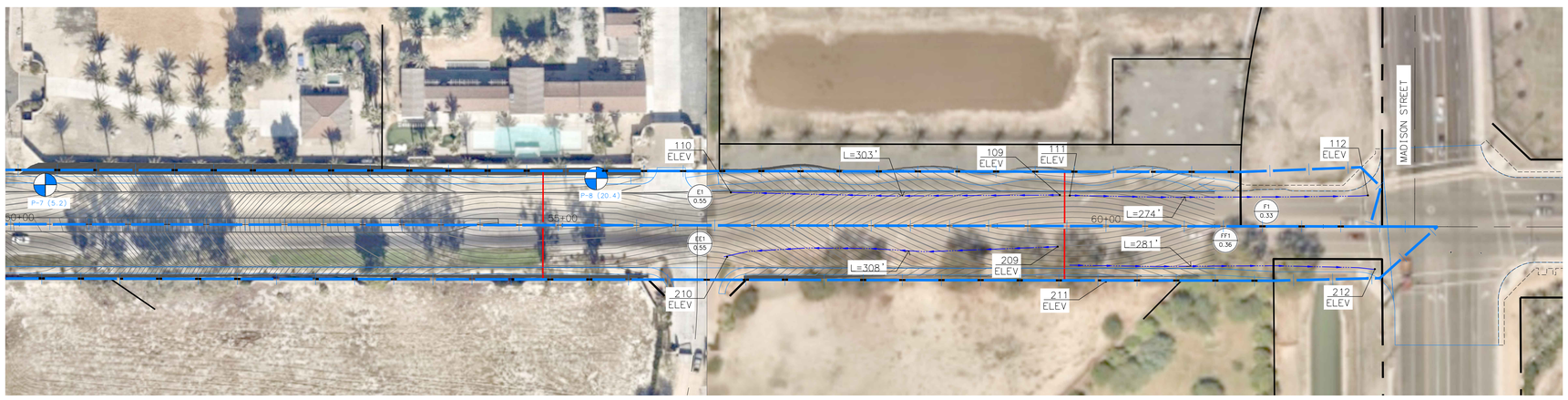
AVENUE 50 STREET IMPROVEMENTS

COUNTY OF RIVERSIDE, STATE OF CALIFORNIA

POST-PROJECT CONDITION SITE HYDROLOGY MAP







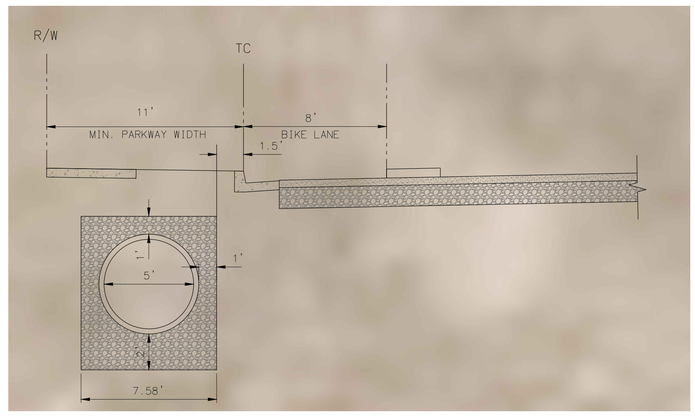


EXHIBIT "A"

AVENUE 50 IMPROVEMENTS

POST-CONDITIION HYDROLOLGY MAP

JLC Engineering & Consulting, Inc.
41660 IVY STREET, SUITE A
MURRIETA, CA 92562
PH. 951.304.9552 FAX 951.304.3568

Drawing Name: O:\173.WEBB\AVENUE 50\Hydrology Ave 50\Exhibits\EXHIBIT B_POST_Hydrology.dwg
Last Opened: Jul 22, 2025 - 1:58pm by jacob