# APPENDIX H

# PRELIMINARY DRAINAGE STUDY

# PRELIMINARY DRAINAGE STUDY
# FOR
# TENTATIVE PARCEL MAP 20854
## 913 CALIFORNIA ST.
## REDLANDS, CALIFORNIA

**PREPARED FOR**

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**PREPARED BY**

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**APRIL 4, 2025**

This report has been prepared by or under the direction of the following registered civil engineer who attests to the technical information contained herein. The registered civil engineer has also judged the qualifications of any technical specialists providing engineering data upon which recommendations, conclusions, and decisions are based.


4/4/2025

Jimmy C. Chen, RCE 51394 Date
Registered Civil Engineer

## TABLE OF CONTENTS



## APPENDICES



## EXCERPTS

# I. PROJECT BACKGROUND AND DESCRIPTION

## PURPOSE:

The purpose of this study is to determine the potential drainage impacts for the proposed commercial development of Tentative Parcel Map 20854. The scope of this study is to analyze the proposed developed drainage patterns for the 10- and 100-year storm event compared to the existing 10- and 25-year event using the rational method and synthetic unit hydrograph per the San Bernardino County Hydrology Manual.

## DESCRIPTION:

Tentative Parcel Map 20854 (the "Project") proposes the development of approximately 5.08 acres of vacant land located northwest of Redlands Boulevard and California Street in the City of Redlands, San Bernardino County, into three (3) commercial parcels. The Project proposes a four-story hotel, a drive-thru carwash, a drive-thru coffee shop and dedicated parking for each. The project fronts a railroad right of way to the north, a drainage channel and single-family residential to the south, and commercial/retail to the east. The existing topography for the property gently slopes from the northeast to the southwest towards the drainage channel at approximately 0.5 to 2% over natural cover. See *Section V* for the vicinity map.

## PROPOSED DRAINAGE DESIGN CONCEPT:

The Project proposes an infiltration basin (Basin "A") that will provide stormwater treatment and detention capacity for peak developed runoff mitigation. The increased runoff from the Project will be detained on site and released via a calibrated outlet structure with a riser and orifice connected to the adjacent drainage channel with the required DCV being retained and infiltrated onsite.

The Project proposes one major drainage tributary of which collects and coneys the runoff to infiltration basin "A" for detention and stormwater treatment. The Project's basin will retain the required design capture volume (DCV) onsite while detaining and mitigating the developed peak runoff so that they are less than the 25-year existing event. The mitigated runoff discharges from the basin via a calibrated outlet structure into the adjacent drainage channel.

# II. HYDROLOGY AND HYDRAULIC METHODOLOGY

The modified rational method for this study was based on the "County of San Bernardino Hydrology Manual" dated April 1978. Software designed by "CivilDESIGN" of San Bernardino was used to solve the modified rational method drainage models of the site to determine the time of concentration, average runoff index number, the average pervious fraction, and the design flow rates for the proposed drainage conveyance system. For the final version of this study, the results from the rational method will be used to determine the proposed inlet sizes and determine required diameter of the storm water pipelines. The outputs are printed in the Standard San Bernardino County format and can be found in *Appendix B*.

A. Rainfall:
The program utilizes user input for the required runoff intensity rates from NOAA Atlas 14 for Redlands for all the required time vs. intensity date for San Bernardino. See *Appendix A.1.*

| Storm Event & Duration | Rainfall (inches) |
|---|---|
| 10-Year, 1-Hour | 0.734 |
| 100-Year, 1-Hour | 1.16 |

B. Infiltration:
Soil type was based on the San Bernardino County Hydrology Manual Hydrologic Soils Group Map for Southwest-D Area Figure C-16 (HSG=B). See *Appendix A.2.*

C. Runoff and Routing:
After the "C" value is determined, the computer determines the runoff and routes the flood downstream based on the input model and Figures C-2, C-3, and C-4 as necessary.

*Table 1: Rational Method Summary*

| | Existing 10-Year (AMC II) | Existing 25-Year (AMC II) | Proposed 10-Year (AMC II) | Proposed 100-Year (AMC III) |
|---|---|---|---|---|
| **Acreage, A** | 5.55 ac. | | 4.40 ac. | |
| **Runoff, Q** | 5.3 cfs | 7.0 cfs | 8.4 cfs | 14.3 cfs |
| **Time of Concentration, Tc** | 18.768 min. | | 8.20 min. | 7.90 min. |
| **Area Pervious, Ap** | 1.000 | | 0.299 | |
| **Runoff Index, SCS** | 78.0 | | 59.6 | |

**SYNTHETIC UNIT HYDROGRAPH METHOD:**

The Synthetic Unit Hydrograph, a computational procedure for developing peak runoff and discharge for storms of a specified recurrence interval, was used to evaluate our detention needs onsite. This procedure calculates effective rainfall, which is the portion of the total rainfall that

appears as surface runoff, at a specific concentration point. Precipitation data for the project location was taken NOAA Atlas 14 respectfully and are provided in *Appendix A.1* of this report. The 10-, 25- and 100-year storm frequencies for each of the 24-hour durations were analyzed for increased runoff mitigation. The hydrographs and basin routing for the 100-year storm events are included to show that the basins can pass the 100-year storm with sufficient capacity.

The following assumptions/guidelines were applied in the use to the Synthetic Unit Hydrograph Method:

- The 2-, 10-, and 100-Year point rainfall depths at 1-, 6-, and 24-hour durations were estimated from the NOAA Atlas 14 for Redlands.
- Lag times used for the development of the synthetic unit hydrograph were generated based on the size and shape of the sub basin. The watershed sub area lag times were calculated according to the lag time equation as indicated in the San Bernardino County Hydrology Manual.
- The Undeveloped and Developed Valley S-Curve graph was used for this project site. The 24-hour, 5-minute interval data was used.
- An area averaged infiltration rate was calculated based on hydrologic soil type, vegetative cover land use and impervious percentage. The "low loss rate" function was then incorporated. The San Bernardino County Hydrology Manual's synthetic unit hydrograph method includes a "low loss rate" function when calculating effective rainfall (i.e., total rain minus infiltration).

*Table 2: Developed Unit Hydrograph Summary*

| | **Existing 10-Year** | **Existing 25-Year** | **Proposed 10-Year** | **Proposed 100-Year** |
|---|---|---|---|---|
| **Runoff, Q** | 4.9 cfs | 6.4 cfs | 8.3 cfs | 14.4 cfs |
| **Runoff Volume** | 0.656 ac-ft | 0.8967 ac-ft | 0.8321 ac-ft | 1.4981 ac-ft |

The synthetic Unit Hydrograph Method outlined in the San Bernadino County Hydrology Manual was used to develop runoff hydrographs using "CIVILDESIGN" Engineering Software. This software was also used to route the unit hydrographs through the proposed detention basin onsite.

The following assumptions/guidelines were made in the use of Reservoir Routing:

- The Modified Pul's (Storage Indication) Method is used for the detention basin routing studies. The basin routing relationships are based upon the following formula:

  $I - O = \Delta S/\Delta t$
  I = Basin inflow rate (cfs)
  O = Basin outflow rate (cfs)
  $\Delta S$ = Change in basin storage during the time step (cubic feet)
  $\Delta t$ = time step (sec)

- The basin inflow rates are based on the unit hydrograph files (See Appendix C)

- Depth-Storage-Discharge curve is based on Basin Volume worksheet and Stage Discharge Rating Table (See Appendix D)
- The procedure is repeated for each time step until the basin inflow hydrograph has been completely analyzed and the basin outflow becomes negligible.

*Table 3: Basin Routing Analysis Summary*

| **Proposed Basin "A"** | | |
|---|---|---|
| | **10-Year** | **100-Year** |
| **Basin Design Capacity** | 1.52 ac-ft. | |
| **Design Capture Volume, DCV** | 0.24 ac-ft. | |
| **Max. Basin Depth** | 5 ft. | |
| **Peak Runoff Inflow, $Q_{in}$** | 8.3 cfs | 14.4 cfs |
| **Peak Runoff Outflow, $Q_{out}$** | 0.6 cfs | 4.2 cfs |
| **Runoff Reduction** | 92.7% | 70.7% |
| **Max. Ponded Depth** | 2.38 ft. | 3.23 ft. |
| **Max. W.S.E.** | 1147.38 | 1148.23 |
| **Max. Freeboard** | 2.62 ft. | 1.77 ft. |

# III. CONCLUSIONS

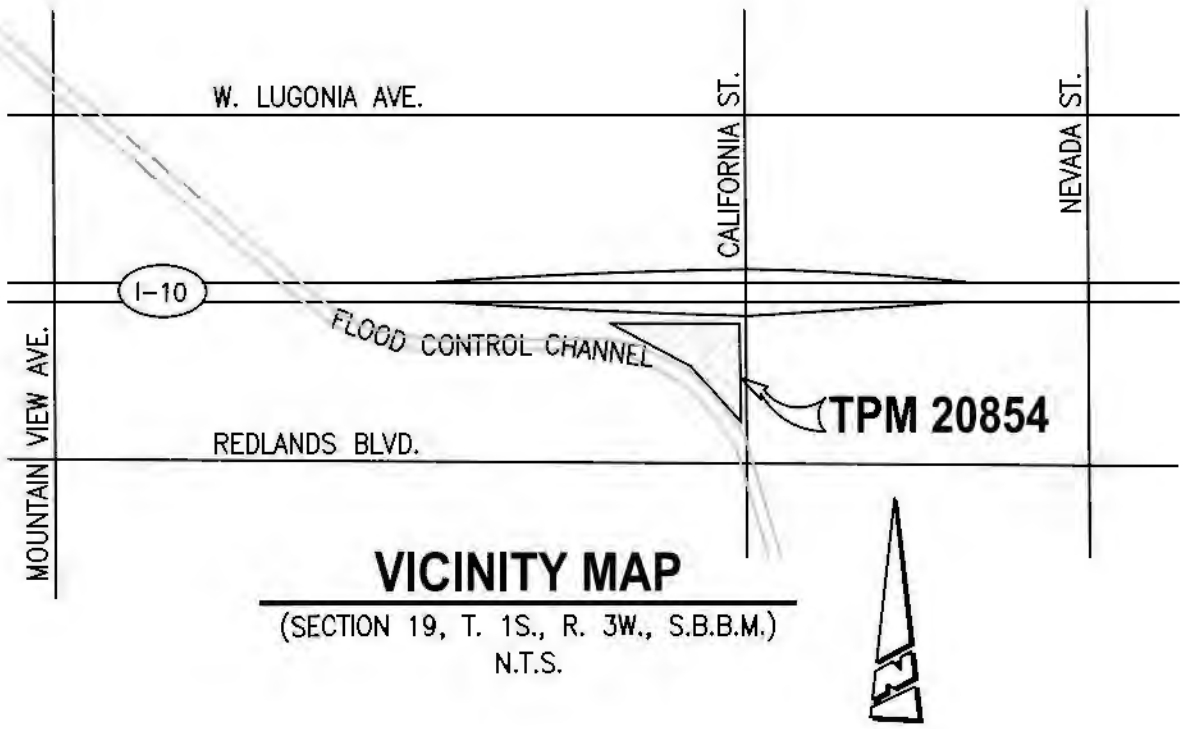
This study evaluated the proposed commercial development to assess the hydrology and hydraulics of the project site. The following has been concluded:

1. Two infiltration basins will be required to stormwater treatment.
2. Mitigation for increased runoff is required as the proposed developed 100-year runoff far exceeds the existing 25-year runoff. However, the proposed infiltration basin "A" has sufficient capacity to retain the DCV and detain the increased runoff volume.
3. The storm drain systems are sized such that they convey flows to the basins and provide flood protection. Catch basins are located such that they provide flood protection.

# IV. REFERENCES

1. County of San Bernardino Hydrology Manual, 1986.

# V. VICINITY MAP



**NOAA Atlas 14, Volume 6, Version 2**
**Location name: Redlands, California, USA***
**Latitude: 34.0652°, Longitude: -117.2274°**
**Elevation: 1158 ft****
* source: ESRI Maps
** source: USGS

**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

## PF tabular

**PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)[1]**

| Duration | Average recurrence interval (years) | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| | 1 | 2 | 5 | 10 | 25 | 50 | 100 | 200 | 500 | 1000 |
| 5-min | 0.097 (0.081-0.118) | 0.126 (0.104-0.153) | 0.164 (0.136-0.200) | 0.195 (0.161-0.240) | 0.239 (0.190-0.304) | 0.273 (0.212-0.355) | 0.308 (0.233-0.410) | 0.344 (0.254-0.472) | 0.395 (0.279-0.565) | 0.434 (0.296-0.644) |
| 10-min | 0.139 (0.116-0.169) | 0.180 (0.150-0.219) | 0.235 (0.195-0.286) | 0.280 (0.230-0.344) | 0.342 (0.272-0.435) | 0.391 (0.304-0.508) | 0.441 (0.335-0.588) | 0.494 (0.364-0.677) | 0.566 (0.399-0.810) | 0.623 (0.424-0.923) |
| 15-min | 0.168 (0.140-0.204) | 0.218 (0.181-0.265) | 0.284 (0.235-0.346) | 0.339 (0.278-0.416) | 0.414 (0.329-0.527) | 0.473 (0.368-0.615) | 0.534 (0.405-0.711) | 0.597 (0.440-0.819) | 0.684 (0.483-0.979) | 0.753 (0.513-1.12) |
| 30-min | 0.249 (0.207-0.302) | 0.322 (0.268-0.392) | 0.420 (0.348-0.512) | 0.501 (0.412-0.616) | 0.613 (0.487-0.779) | 0.700 (0.544-0.909) | 0.790 (0.599-1.05) | 0.883 (0.651-1.21) | 1.01 (0.715-1.45) | 1.11 (0.759-1.65) |
| 60-min | 0.364 (0.303-0.442) | 0.472 (0.393-0.574) | 0.616 (0.511-0.750) | 0.734 (0.604-0.902) | 0.898 (0.713-1.14) | 1.03 (0.797-1.33) | 1.16 (0.877-1.54) | 1.30 (0.954-1.78) | 1.48 (1.05-2.12) | 1.63 (1.11-2.42) |
| 2-hr | 0.523 (0.435-0.634) | 0.669 (0.556-0.813) | 0.863 (0.716-1.05) | 1.02 (0.841-1.26) | 1.24 (0.986-1.58) | 1.41 (1.10-1.83) | 1.59 (1.20-2.11) | 1.77 (1.30-2.42) | 2.01 (1.42-2.88) | 2.21 (1.50-3.27) |
| 3-hr | 0.644 (0.536-0.781) | 0.821 (0.683-0.997) | 1.06 (0.874-1.28) | 1.25 (1.02-1.53) | 1.51 (1.20-1.92) | 1.71 (1.33-2.22) | 1.92 (1.46-2.56) | 2.14 (1.57-2.93) | 2.43 (1.72-3.48) | 2.66 (1.81-3.94) |
| 6-hr | 0.902 (0.751-1.09) | 1.15 (0.953-1.39) | 1.47 (1.22-1.79) | 1.73 (1.42-2.13) | 2.09 (1.66-2.66) | 2.37 (1.84-3.08) | 2.65 (2.01-3.53) | 2.94 (2.17-4.03) | 3.34 (2.36-4.78) | 3.65 (2.48-5.40) |
| 12-hr | 1.19 (0.994-1.45) | 1.52 (1.27-1.85) | 1.96 (1.62-2.38) | 2.31 (1.90-2.84) | 2.79 (2.22-3.54) | 3.16 (2.45-4.10) | 3.53 (2.68-4.70) | 3.91 (2.88-5.36) | 4.43 (3.13-6.34) | 4.83 (3.29-7.16) |
| 24-hr | 1.59 (1.41-1.83) | 2.05 (1.82-2.37) | 2.65 (2.34-3.07) | 3.14 (2.75-3.66) | 3.80 (3.22-4.58) | 4.31 (3.57-5.30) | 4.82 (3.90-6.07) | 5.34 (4.21-6.92) | 6.05 (4.58-8.16) | 6.60 (4.83-9.20) |
| 2-day | 1.95 (1.73-2.25) | 2.55 (2.26-2.95) | 3.35 (2.95-3.87) | 4.00 (3.50-4.66) | 4.88 (4.13-5.88) | 5.56 (4.61-6.83) | 6.25 (5.06-7.87) | 6.96 (5.49-9.01) | 7.93 (6.00-10.7) | 8.68 (6.35-12.1) |
| 3-day | 2.10 (1.86-2.42) | 2.79 (2.47-3.22) | 3.70 (3.26-4.28) | 4.45 (3.90-5.19) | 5.49 (4.65-6.61) | 6.29 (5.22-7.74) | 7.11 (5.76-8.96) | 7.97 (6.28-10.3) | 9.14 (6.92-12.3) | 10.1 (7.36-14.0) |
| 4-day | 2.24 (1.98-2.58) | 3.01 (2.66-3.47) | 4.02 (3.55-4.66) | 4.87 (4.26-5.68) | 6.03 (5.11-7.27) | 6.94 (5.76-8.54) | 7.88 (6.38-9.92) | 8.86 (6.98-11.5) | 10.2 (7.72-13.8) | 11.3 (8.25-15.7) |
| 7-day | 2.59 (2.29-2.99) | 3.52 (3.11-4.06) | 4.76 (4.20-5.51) | 5.79 (5.07-6.76) | 7.22 (6.12-8.70) | 8.34 (6.92-10.3) | 9.50 (7.70-12.0) | 10.7 (8.44-13.9) | 12.4 (9.37-16.7) | 13.7 (10.0-19.1) |
| 10-day | 2.81 (2.49-3.24) | 3.85 (3.41-4.45) | 5.25 (4.63-6.07) | 6.41 (5.60-7.47) | 8.02 (6.79-9.66) | 9.28 (7.70-11.4) | 10.6 (8.58-13.3) | 12.0 (9.43-15.5) | 13.9 (10.5-18.7) | 15.4 (11.3-21.4) |
| 20-day | 3.46 (3.06-3.99) | 4.79 (4.24-5.53) | 6.59 (5.81-7.62) | 8.09 (7.08-9.44) | 10.2 (8.63-12.3) | 11.8 (9.83-14.6) | 13.6 (11.0-17.1) | 15.4 (12.1-19.9) | 17.9 (13.6-24.2) | 19.9 (14.6-27.8) |
| 30-day | 4.08 (3.62-4.71) | 5.66 (5.01-6.53) | 7.79 (6.87-9.02) | 9.58 (8.39-11.2) | 12.1 (10.2-14.6) | 14.1 (11.7-17.3) | 16.2 (13.1-20.4) | 18.4 (14.5-23.8) | 21.5 (16.2-28.9) | 23.9 (17.5-33.4) |
| 45-day | 4.91 (4.35-5.66) | 6.76 (5.98-7.80) | 9.28 (8.19-10.7) | 11.4 (9.98-13.3) | 14.4 (12.2-17.3) | 16.8 (13.9-20.6) | 19.3 (15.6-24.3) | 21.9 (17.3-28.4) | 25.7 (19.4-34.6) | 28.7 (21.0-40.0) |
| 60-day | 5.77 (5.11-6.65) | 7.87 (6.96-9.08) | 10.7 (9.46-12.4) | 13.1 (11.5-15.3) | 16.6 (14.0-20.0) | 19.3 (16.0-23.7) | 22.2 (18.0-27.9) | 25.2 (19.9-32.7) | 29.5 (22.3-39.8) | 33.0 (24.1-46.0) |

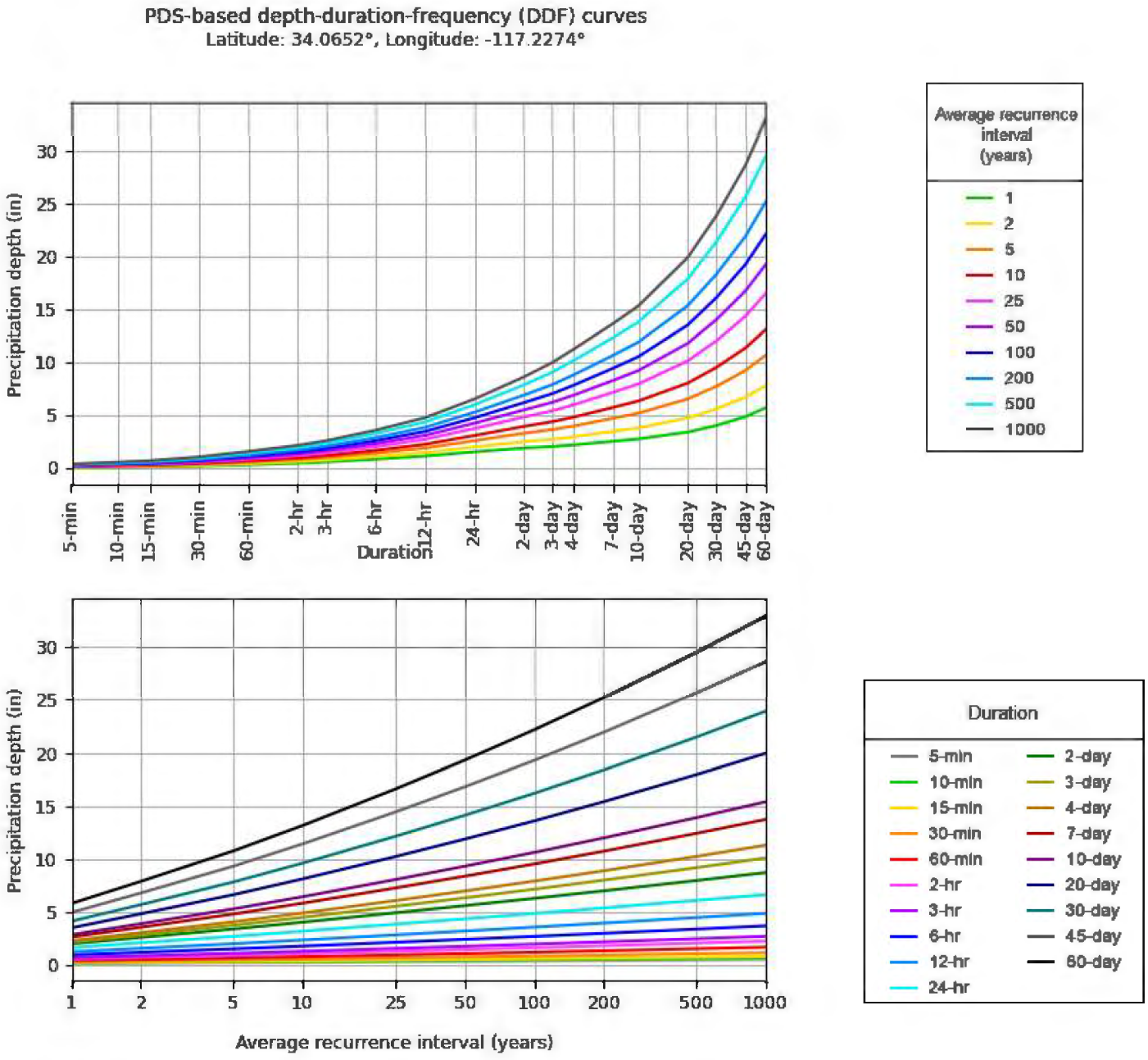
[1] Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

Back to Top

## PF graphical

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Back to Top

## Maps & aerials

**Small scale terrain**


**Large scale terrain**


**Large scale map**


**Large scale aerial**


Back to Top

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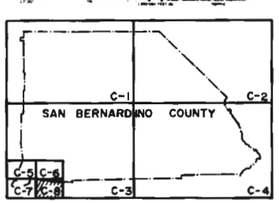
Disclaimer

TPM 20854
HSG=B

SOURCE: GEOLOGY MAP
SOURCE: 1971 SCS SURVEY

SOURCE: 1971 SCS SURVEY



INDEX MAP

LEGEND

SOIL GROUP BOUNDARY

A SOIL GROUP DESIGNATION

BOUNDARY OF INDICATED SOURCE

SCALE 1:48,000

**SCALE REDUCED BY 1/2**

**SAN BERNARDINO COUNTY**
HYDROLOGY MANUAL

HYDROLOGIC SOILS GROUP MAP
FOR
SOUTHWEST-D AREA



FIGURE C-16

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| PUTNAM | D | RANDMAN | D | REELFOOT | C | RIFFE | B | ROLETTE | C | | |
| PUUKALA | D | RANDOLPH | D | REESER | C | RIFLE | A/D | ROLFE | C | | |
| PUUONE | C | RANDS | C | REESVILLE | C | RIGA | D | ROLISS | D | | |
| PUU OO | A | RANGER | D | REEVES | C | RIGGINS | A | ROLLA | C | | |
| PUU OPAE | B | RANIER | C | REFUGE | C | RIGLEY | B | ROLLIN | D | | |
| PUU PA | B | RANKIN | C | REGAN | B | RILEY | C | ROLOFF | C | | |
| PUYALLUP | B | RANTOUL | D | REGENT | C | RILLA | B | ROMBERG | B | | |
| PYLE | A | RANYHAN | B | REHM | C | RILLITO | B | ROMBO | C | | |
| PYLON | D | RAPELJE | C | REICHEL | B | RIMER | C | ROMEO | C | | |
| PYOTE | A | RAPHO | B | REIFF | B | RIMINI | A | ROMNEY | C | | |
| PYRAMID | D | RAPIDAN | B | REILLY | A | RIMROCK | D | ROMULUS | D | | |
| PYRMONT | D | RAPLEE | C | REINACH | B | RIN | B | RONO | C | | |
| | | RARDEN | C | REKOP | D | RINCON | C | RONNEBY | B | | |
| QUACKENBUSH | C | RARICK | B | RELAN | A | RINCONADA | C | RONSON | B | | |
| QUAKER | C | RARITAN | C | RELAY | B | RINDGE | D | ROOSE | B | | |
| QUAKERTOWN | B | RASBAND | B | RELIANCE | C | RINGLING | C | ROOTEL | D | | |
| QUAMBA | D | RASSET | B | RELIZ | D | RINGO | D | ROSACHI | C | | |
| QUAMON | A | RATAKE | C | RELSE | B | RINGOLD | B | ROSAMOND | B | | |
| QUANAH | B | RATHBUN | C | REMBERT | D | RINGWOOD | B | ROSANE | C | | |
| QUANDAHL | B | RATLIFF | B | REMMIT | A | RIO | D | ROSANKY | C | | |
| QUARLES | D | RATON | D | REMSEN | D | RIO ARRIBA | D | ROSARIO | C | | |
| QUARTZBURG | C | RATTLER | B | REMUDAR | B | RIOCONCHO | C | ROSCOE | D | | |
| QUATAMA | C | RATTO | D | REMUNDA | C | RIO GRANDE | B | ROSCOMMON | D | | |
| QUAY | B | RAUB | B | RENBAC | D | RIO KING | C | ROSEBERRY | B/D | | |
| QUAZO | D | RAUVILLE | D | RENCALSON | C | RIO LAJAS | A | ROSEBLOOM | D | | |
| QUEALY | D | RAUZI | B | RENCOT | A | RIO PIEDRAS | B | ROSEBUD | B | | |
| QUEBRADA | C | RAVALLI | C | RENFROW | D | RIPLEY | B | ROSEBURG | B | | |
| QUEENY | D | RAVENDALE | D | RENICK | D | RIPON | B | ROSE CREEK | C | | |
| QUEETS | B | RAVENNA | C | RENNIE | C/D | RIRIE | B | ROSEGLEN | B | | |
| QUEMADO | C | RAVOLA | B | RENO | D | RISBECK | B | ROSEHILL | D | | |
| QUENZER | D | RAWAH | B | RENOHILL | C | RISLEY | D | ROSELAND | D | | |
| QUICKSELL | D | RAWHIDE | D | RENOVA | D | RISTA | C | ROSELLA | D | | |
| QUIETUS | C | RAWSON | B | RENOX | B | RISUE | D | ROSELMS | D | | |
| QUIGLEY | B | RAY | B | RENSHAW | B | RITCHEY | B | ROSEMOUNT | B | | |
| QUILCENE | C | RAYADO | C | RENSLOW | B | RITNER | C | ROSENDALE | B | | |
| QUILLAYUTE | B | RAYENOUF | B | RENSSELAER | C | RITO | B | ROSE VALLEY | C | | |
| QUIMBY | B | RAYMONDVILLE | D | RENTIDE | C | RITTER | B | ROSEVILLE | B | | |
| QUINCY | A | RAYNE | B | RENTON | B/C | RITTMAN | C | ROSEWORTH | C | | |
| QUINLAN | C | RAYNESFORD | B | RENTSAC | C | RITZ | B/D | ROSHE SPRINGS | D | | |
| QUINN | D | RAYNHAM | C | REPARADA | D | RITZCAL | B | ROSITAS | A | | |
| QUINNEY | C | RAYNOR | D | REPP | A | RITZVILLE | B | ROSLYN | B | | |
| QUINTON | | RAZOR | C | REPPART | B | RIVERHEAD | B | ROSMAN | B | | |
| QUITMAN | C | RAZORT | B | REPUBLIC | B | RIVERSIDE | A | ROSNEY | C | | |
| QUONSET | A | READING | C | RESCUE | C | RIVERTON | C | ROSS | B | | |
| | | READINGTON | C | RESERVE | B | RIVERVIEW | B | ROSS FORK | C | | |
| RABER | C | READLYN | B | RESNER | B | RIVRA | A | ROSSI | C | | |
| RABEY | A | REAGAN | B | RET | B/C | RIXIE | C | ROSSMOYNE | C | | |
| RABIDEUX | B | REAKOR | B | RETRIEVER | D | RIXON | C | ROSS VALLEY | C | | |
| RABUN | B | REAL | C | RETSOF | C | RIZ | D | ROTAN | C | | |
| RACE | D | REAP | D | RETSOK | B | ROANOKE | D | ROTHIEMAY | B | | |
| RACHERT | D | REARDAN | C | REXBURG | B | ROBANA | B | ROTHSAY | B | | |
| RACINE | B | REAVILLE | C | REXFORD | C | ROBBINS | B | ROTTULEE | B | | |
| RACOON | D | REBA | C | REXOR | A | ROBBS | D | ROUBIDEAU | C | | |
| RAD | C | REBEL | B | REYES | C/D | ROBERTS | D | ROUEN | C | | |
| RADERSBURG | B | REBUCK | | REYNOLDS | | ROBERTSDALE | C | ROUND BUTTE | D | | |
| RADFORD | B | RECAL | D | REYNOSA | B | ROBERTSVILLE | D | ROUNDLEY | C | | |
| RADLEY | C | RECLUSE | C | REYWAT | D | ROBIN | B | ROUNDTOP | C | | |
| RADNOR | D | REDBANK | B | RHAME | B | ROBINSON | D | ROUNDUP | C | | |
| RAFAEL | D | RED BAY | B | RHEA | B | ROBINSONVILLE | B | ROUNDY | C | | |
| RAGER | B | RED BLUFF | C | RHINEBECK | D | ROBLEDO | D | ROUSSEAU | A | | |
| RAGLAN | C | RED BUTTE | B | RHOADES | D | ROB ROY | C | ROUTON | D | | |
| RAGNAR | B | REDBY | C | RHOAME | C | ROBY | C | ROUTT | C | | |
| RAGO | C | REDCHIEF | C | RIB | C | ROCA | D | ROVAL | D | | |
| RAGSDALE | B/D | REDCLOUD | B | RICCO | D | ROCHE | C | ROWE | D | | |
| RAGTOWN | D | REDDICK | C | RICETON | B | ROCHELLE | C | ROWENA | C | | |
| RAHAL | C | REDDING | D | RICEVILLE | C | ROCHEPORT | C | ROWLAND | C | | |
| RAHM | C | REDFIELD | B | RICHARDSON | B | ROCKAWAY | C | ROWLEY | B | | |
| RAIL | C/D | RED HILL | C | RICHEAU | C | ROCKCASTLE | D | ROXAL | D | | |
| RAINBOW | C | RED HOOK | C | RICHEY | C | ROCK CREEK | D | ROXBURY | B | | |
| RAINEY | B | REDLAKE | D | RICHFIELD | C | ROCKFORD | B | ROY | B | | |
| RAINS | B/D | REDLANDS | B | RICHFORD | A | ROCKHOUSE | A | ROYAL | B | | |
| RAINSBORO | C | REDLODGE | D | RICHLIE | A | ROCKINGHAM | C/D | ROYALTON | C | | |
| RAKE | D | REDMANSON | B | RICHMOND | D | ROCKLIN | C/D | ROYCE | B | | |
| RALSEN | B/C | REDMOND | C | RICHTER | B | ROCKLY | D | ROYSTONE | B | | |
| RAMADA | C | REDNUN | C | RICHVALE | B | ROCKPORT | C | ROZA | D | | |
| RAMADERO | B | REDOLA | B | RICHVIEW | C | ROCK RIVER | B | ROZELLVILLE | B | | |
| RAMBLER | B | REDONA | B | RICHWOOD | B | ROCKTON | B | ROZETTA | B | | |
| RAMELLI | C | REDRIDGE | B | RICKMORE | C | ROCKWELL | B | ROZLEE | C | | |
| RAMIRES | D | REDROB | D | RICKS | A | ROCKWOOD | B | RUARK | C | | |
| RAMMEL | C | RED ROCK | B | RICO | C | ROCKY FORD | B | RUBICON | A | | |
| RAMO | C | RED SPUR | B | RICREST | B | RODDY | | RUBIO | C | | |
| RAMONA | B | REDSTOE | B | RIDD | C | ROCMAN | A | RUBY | B | | |
| RAMPART | B | REDTHAYNE | B | RIDGEBURY | C | ROE | B | RUBYHILL | C | | |
| RAMPARTAR | A | REDTOM | C | RIDGECREST | C | ROEBUCK | D | RUCH | B | | |
| RAMPARTER | A | REDVALE | C | RIDGEDALE | B | ROELLEN | D | RUCKLES | D | | |
| RAMSEY | D | REDVIEW | C | RIDGELAND | D | ROEMER | C | RUCLICK | C | | |
| RAMSHORN | B | REE | B | RIDGELAWN | A | ROESIGER | B | RUDD | D | | |
| RANCE | C | REEBEX | C | RIDGELY | B | ROGERT | D | RUDEEN | B | | |
| RANCHERIA | B | REED | D | RIDGEVILLE | B | ROHNERVILLE | B | RUDOLPH | C | | |
| RAND | B | REEDER | B | RIDGEWAY | D | ROHRERSVILLE | C | RUDYARD | D | | |
| RANDADO | C | REEDPOINT | C | RIDIT | C | ROIC | D | RUELLA | B | | |
| RANDALL | D | REEDY | D | RIETBROCK | C | ROKEBY | D | RUGGLES | B | | |

NOTES A BLANK HYDROLOGIC SOIL GROUP INDICATES THE SOIL GROUP HAS NOT BEEN DETERMINED
TWO SOIL GROUPS SUCH AS B/C INDICATES THE DRAINED/UNDRAINED SITUATION

# SAN BERNARDINO COUNTY
## HYDROLOGY MANUAL

## S.C.S. SOIL NAMES FOR HYDROLOGIC CLASSIFICATIONS

| Rational Method Analysis | | | | | |
|---|---|---|---|---|---|
| | Acreage (ac.) | Runoff, Q (cfs) | Time of Concentration, $T_C$ (min.) | Ap | SCS |
| Exosting 10-Year | 5.55 | 5.348 | 18.768 | 1.000 | 78.0 |
| Existing 25-Year | | 7.0 | 18.768 | | |
| Proposed 10-Year | 4.4 | 8.4 | 8.200 | 0.299 | 59.6 |
| Proposed 100-Year | | 14.3 | 7.900 | | |

# B.1 – Existing 10-Year Analysis

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2019 Version 9.1
Rational Hydrology Study Date: 08/26/24

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TPM 20854
EXISTING CONDITION
10-YEAR

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Program License Serial Number 6568

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********* Hydrology Study Control Information **********

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Rational hydrology study storm event year is 10.0
Computed rainfall intensity:
Storm year = 10.00 1 hour rainfall = 0.734 (In.)
Slope used for rainfall intensity curve b = 0.6000
Soil antecedent moisture condition (AMC) = 2

++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

---

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Initial subarea data:
Initial area flow distance = 935.000(Ft.)
Top (of initial area) elevation = 1162.000(Ft.)
Bottom (of initial area) elevation = 1148.000(Ft.)
Difference in elevation = 14.000(Ft.)
Slope = 0.01497 s(%)= 1.50
TC = k(0.525)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 18.768 min.
Rainfall intensity = 1.474(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.654
Subarea runoff = 5.348(CFS)
Total initial stream area = 5.550(Ac.)

Pervious area fraction = 1.000
Initial area Fm value =  0.404(In/Hr)
End of computations, Total Study Area =  5.55 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.
Note: These figures do not consider reduced effective area
effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged SCS curve number =  78.0

# B.2 – EXISTING 25-YEAR ANALYSIS

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2019 Version 9.1
Rational Hydrology Study Date: 04/18/24

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TPM 20854
EXISTING CONDITION
25-YEAR

---

Program License Serial Number 6568

---

********* Hydrology Study Control Information **********

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Rational hydrology study storm event year is 25.0
10 Year storm 1 hour rainfall = 0.734(In.)
100 Year storm 1 hour rainfall = 1.160(In.)
Computed rainfall intensity:
Storm year = 25.00 1 hour rainfall = 0.904 (In.)
Slope used for rainfall intensity curve b = 0.6000
Soil antecedent moisture condition (AMC) = 2

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Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

---

UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 78.00
Pervious ratio(Ap) = 1.0000 Max loss rate(Fm)= 0.404(In/Hr)
Initial subarea data:
Initial area flow distance = 935.000(Ft.)
Top (of initial area) elevation = 1162.000(Ft.)
Bottom (of initial area) elevation = 1148.000(Ft.)
Difference in elevation = 14.000(Ft.)
Slope = 0.01497 s(%)= 1.50
TC = k(0.525)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 18.768 min.
Rainfall intensity = 1.815(In/Hr) for a 25.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.700

Subarea runoff =  7.048(CFS)
Total initial stream area =  5.550(Ac.)
Pervious area fraction = 1.000
Initial area Fm value =  0.404(In/Hr)
End of computations, Total Study Area =  5.55 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.
Note: These figures do not consider reduced effective area
effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged SCS curve number =  78.0

## B.3 – Proposed 10-Year Analysis

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2019 Version 9.1
Rational Hydrology Study Date: 08/26/24

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TPM 20854
DEVELOPED CONDITION
10-YEAR

---

Program License Serial Number 6568

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********* Hydrology Study Control Information **********

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Rational hydrology study storm event year is 10.0
Computed rainfall intensity:
Storm year = 10.00 1 hour rainfall = 0.734 (In.)
Slope used for rainfall intensity curve b = 0.6000
Soil antecedent moisture condition (AMC) = 2

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Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

---

CONDOMINIUM subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00
Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.257(In/Hr)
Initial subarea data:
Initial area flow distance = 92.000(Ft.)
Top (of initial area) elevation = 1161.000(Ft.)
Bottom (of initial area) elevation = 1160.000(Ft.)
Difference in elevation = 1.000(Ft.)
Slope = 0.01087 s(%)= 1.09
TC = k(0.360)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 5.427 min.
Rainfall intensity = 3.103(In/Hr) for a 10.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.826
Subarea runoff = 0.205(CFS)
Total initial stream area = 0.080(Ac.)

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Pervious area fraction = 0.350
Initial area Fm value =    0.257(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        2.000 to Point/Station        3.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1156.500(Ft.)
Downstream point/station elevation =  1155.800(Ft.)
Pipe length  =   134.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.205(CFS)
Nearest computed pipe diameter  =      6.00(In.)
Calculated individual pipe flow  =     0.205(CFS)
Normal flow depth in pipe =    3.02(In.)
Flow top width inside pipe =    6.00(In.)
Critical Depth =    2.72(In.)
Pipe flow velocity =      2.07(Ft/s)
Travel time through pipe =    1.08 min.
Time of concentration (TC) =     6.50 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        3.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
CONDOMINIUM subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.3500     Max loss rate(Fm)=     0.257(In/Hr)
Time of concentration =     6.50 min.
Rainfall intensity =      2.784(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.817
Subarea runoff =      0.318(CFS) for    0.150(Ac.)
Total runoff =      0.523(CFS)
Effective area this stream =        0.23(Ac.)
Total Study Area (Main Stream No. 1) =        0.23(Ac.)
Area averaged Fm value =    0.257(In/Hr)


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Process from Point/Station        3.000 to Point/Station        4.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1155.800(Ft.)
Downstream point/station elevation =   155.500(Ft.)
Pipe length  =    60.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.523(CFS)
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Nearest computed pipe diameter  =      3.00(In.)
Calculated individual pipe flow  =     0.523(CFS)
Normal flow depth in pipe =    0.77(In.)
Flow top width inside pipe =    2.62(In.)
Critical depth could not be calculated.
Pipe flow velocity =     52.37(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =     6.52 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        4.000 to Point/Station        4.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
UNDEVELOPED (average cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 69.00
Pervious ratio(Ap) = 1.0000     Max loss rate(Fm)=     0.548(In/Hr)
Time of concentration =     6.52 min.
Rainfall intensity =      2.779(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.786
Subarea runoff =      0.220(CFS) for    0.110(Ac.)
Total runoff =      0.743(CFS)
Effective area this stream =        0.34(Ac.)
Total Study Area (Main Stream No. 1) =        0.34(Ac.)
Area averaged Fm value =    0.351(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        4.000 to Point/Station        5.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1155.500(Ft.)
Downstream point/station elevation =  1155.300(Ft.)
Pipe length  =    27.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.743(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     0.743(CFS)
Normal flow depth in pipe =    4.62(In.)
Flow top width inside pipe =    9.00(In.)
Critical Depth =    4.72(In.)
Pipe flow velocity =      3.26(Ft/s)
Travel time through pipe =    0.14 min.
Time of concentration (TC) =     6.66 min.


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Process from Point/Station        5.000 to Point/Station        5.000
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**** SUBAREA FLOW ADDITION ****
_____________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.073(In/Hr)
Time of concentration =     6.66 min.
Rainfall intensity =      2.744(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.816
Subarea runoff =      0.422(CFS) for    0.180(Ac.)
Total runoff =      1.165(CFS)
Effective area this stream =        0.52(Ac.)
Total Study Area (Main Stream No. 1) =        0.52(Ac.)
Area averaged Fm value =    0.255(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        5.000 to Point/Station        6.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
_____________________________________________________________________
Upstream point/station elevation =  1155.300(Ft.)
Downstream point/station elevation =  1155.000(Ft.)
Pipe length  =    54.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.165(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     1.165(CFS)
Normal flow depth in pipe =    6.96(In.)
Flow top width inside pipe =    7.53(In.)
Critical Depth =    5.96(In.)
Pipe flow velocity =      3.17(Ft/s)
Travel time through pipe =    0.28 min.
Time of concentration (TC) =     6.95 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        6.000 to Point/Station        6.000
**** SUBAREA FLOW ADDITION ****
_____________________________________________________________________
CONDOMINIUM subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.3500     Max loss rate(Fm)=     0.257(In/Hr)
Time of concentration =     6.95 min.
Rainfall intensity =      2.676(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
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rational method)(Q=KCIA) is C = 0.814
Subarea runoff =      0.447(CFS) for    0.220(Ac.)
Total runoff =      1.612(CFS)
Effective area this stream =        0.74(Ac.)
Total Study Area (Main Stream No. 1) =        0.74(Ac.)
Area averaged Fm value =    0.256(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        6.000 to Point/Station        7.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1155.000(Ft.)
Downstream point/station elevation =  1154.700(Ft.)
Pipe length  =    46.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.612(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     1.612(CFS)
Normal flow depth in pipe =    6.42(In.)
Flow top width inside pipe =   11.97(In.)
Critical Depth =    6.47(In.)
Pipe flow velocity =      3.77(Ft/s)
Travel time through pipe =    0.20 min.
Time of concentration (TC) =     7.15 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        7.000 to Point/Station        7.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.073(In/Hr)
Time of concentration =     7.15 min.
Rainfall intensity =      2.630(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.815
Subarea runoff =      0.038(CFS) for    0.030(Ac.)
Total runoff =      1.651(CFS)
Effective area this stream =        0.77(Ac.)
Total Study Area (Main Stream No. 1) =        0.77(Ac.)
Area averaged Fm value =    0.248(In/Hr)


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Process from Point/Station        7.000 to Point/Station        8.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
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Upstream point/station elevation =  1154.700(Ft.)
Downstream point/station elevation =  1153.600(Ft.)
Pipe length  =   109.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.651(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     1.651(CFS)
Normal flow depth in pipe =    7.32(In.)
Flow top width inside pipe =    7.01(In.)
Critical Depth =    7.09(In.)
Pipe flow velocity =      4.29(Ft/s)
Travel time through pipe =    0.42 min.
Time of concentration (TC) =     7.57 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        7.000 to Point/Station        8.000
**** CONFLUENCE OF MAIN STREAMS ****
________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =      0.770(Ac.)
Runoff from this stream =      1.651(CFS)
Time of concentration =    7.57 min.
Rainfall intensity =     2.541(In/Hr)
Area averaged loss rate (Fm) =    0.2484(In/Hr)
Area averaged Pervious ratio (Ap) = 0.3747
Program is now starting with Main Stream No. 2


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        9.000 to Point/Station       10.000
**** INITIAL AREA EVALUATION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.073(In/Hr)
Initial subarea data:
Initial area flow distance =   259.000(Ft.)
Top (of initial area) elevation =  1160.200(Ft.)
Bottom (of initial area) elevation =  1158.000(Ft.)
Difference in elevation =     2.200(Ft.)
Slope =    0.00849  s(%)=       0.85
TC = k(0.304)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.284 min.
Rainfall intensity =      2.601(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.875
Subarea runoff =      0.773(CFS)
Total initial stream area =        0.340(Ac.)
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Pervious area fraction = 0.100
Initial area Fm value =    0.073(In/Hr)


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Process from Point/Station       10.000 to Point/Station       11.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1154.500(Ft.)
Downstream point/station elevation =  1154.000(Ft.)
Pipe length  =    81.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.773(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     0.773(CFS)
Normal flow depth in pipe =    5.00(In.)
Flow top width inside pipe =    8.94(In.)
Critical Depth =    4.82(In.)
Pipe flow velocity =      3.07(Ft/s)
Travel time through pipe =    0.44 min.
Time of concentration (TC) =     7.72 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       11.000 to Point/Station       11.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.073(In/Hr)
Time of concentration =     7.72 min.
Rainfall intensity =      2.511(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.874
Subarea runoff =      0.214(CFS) for    0.110(Ac.)
Total runoff =      0.987(CFS)
Effective area this stream =        0.45(Ac.)
Total Study Area (Main Stream No. 2) =        1.22(Ac.)
Area averaged Fm value =    0.073(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       11.000 to Point/Station       12.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1154.000(Ft.)
Downstream point/station elevation =  1153.900(Ft.)
Pipe length  =     8.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.987(CFS)
```

```
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     0.987(CFS)
Normal flow depth in pipe =    4.68(In.)
Flow top width inside pipe =    8.99(In.)
Critical Depth =    5.46(In.)
Pipe flow velocity =      4.25(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =     7.76 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       12.000 to Point/Station       12.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.073(In/Hr)
Time of concentration =     7.76 min.
Rainfall intensity =      2.505(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.874
Subarea runoff =      0.260(CFS) for    0.120(Ac.)
Total runoff =      1.247(CFS)
Effective area this stream =        0.57(Ac.)
Total Study Area (Main Stream No. 2) =        1.34(Ac.)
Area averaged Fm value =    0.073(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       12.000 to Point/Station       13.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1153.900(Ft.)
Downstream point/station elevation =  1153.700(Ft.)
Pipe length  =    34.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.247(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     1.247(CFS)
Normal flow depth in pipe =    7.24(In.)
Flow top width inside pipe =    7.14(In.)
Critical Depth =    6.17(In.)
Pipe flow velocity =      3.27(Ft/s)
Travel time through pipe =    0.17 min.
Time of concentration (TC) =     7.93 min.


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Process from Point/Station       13.000 to Point/Station       13.000
```

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**** SUBAREA FLOW ADDITION ****
_____________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.073(In/Hr)
Time of concentration =     7.93 min.
Rainfall intensity =      2.472(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.873
Subarea runoff =      0.285(CFS) for    0.140(Ac.)
Total runoff =      1.533(CFS)
Effective area this stream =        0.71(Ac.)
Total Study Area (Main Stream No. 2) =        1.48(Ac.)
Area averaged Fm value =    0.073(In/Hr)


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Process from Point/Station       13.000 to Point/Station        8.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
_____________________________________________________________________
Upstream point/station elevation =  1153.700(Ft.)
Downstream point/station elevation =  1153.600(Ft.)
Pipe length  =    13.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.533(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     1.533(CFS)
Normal flow depth in pipe =    5.93(In.)
Flow top width inside pipe =   12.00(In.)
Critical Depth =    6.30(In.)
Pipe flow velocity =      3.96(Ft/s)
Travel time through pipe =    0.05 min.
Time of concentration (TC) =     7.98 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       13.000 to Point/Station        8.000
**** CONFLUENCE OF MAIN STREAMS ****
_____________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      0.710(Ac.)
Runoff from this stream =      1.533(CFS)
Time of concentration =    7.98 min.
Rainfall intensity =     2.462(In/Hr)
Area averaged loss rate (Fm) =    0.0734(In/Hr)
Area averaged Pervious ratio (Ap) = 0.1000
Summary of stream data:
```

```
Stream Flow rate    Area    TC     Fm       Rainfall Intensity
 No.    (CFS)   (Ac.)       (min) (In/Hr)     (In/Hr)


1      1.65     0.770      7.57    0.248      2.541
2      1.53     0.710      7.98    0.073      2.462
Qmax(1) =
           1.000 *    1.000 *     1.651) +
           1.033 *    0.949 *     1.533) + =       3.153
Qmax(2) =
           0.965 *    1.000 *     1.651) +
           1.000 *    1.000 *     1.533) + =       3.127

Total of 2 main streams to confluence:
Flow rates before confluence point:
       2.651       2.533
Maximum flow rates at confluence using above data:
        3.153        3.127
Area of streams before confluence:
        0.770        0.710
Effective area values after confluence:
        1.444        1.480


Results of confluence:
Total flow rate =      3.153(CFS)
Time of concentration =     7.573 min.
Effective stream area after confluence  =      1.444(Ac.)
Study area average Pervious fraction(Ap) =  0.243
Study area average soil loss rate(Fm) =    0.164(In/Hr)
Study area total =       1.48(Ac.)


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Process from Point/Station        8.000 to Point/Station        8.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
APARTMENT subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.2000     Max loss rate(Fm)=     0.147(In/Hr)
Time of concentration =     7.57 min.
Rainfall intensity =      2.541(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.843
Subarea runoff =      0.667(CFS) for    0.340(Ac.)
Total runoff =      3.820(CFS)
Effective area this stream =        1.78(Ac.)
Total Study Area (Main Stream No. 1) =        1.82(Ac.)
```

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Area averaged Fm value =    0.161(In/Hr)


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Process from Point/Station        8.000 to Point/Station       14.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1153.600(Ft.)
Downstream point/station elevation =  1151.900(Ft.)
Pipe length  =   332.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.820(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     3.820(CFS)
Normal flow depth in pipe =   10.39(In.)
Flow top width inside pipe =   13.84(In.)
Critical Depth =    9.48(In.)
Pipe flow velocity =      4.21(Ft/s)
Travel time through pipe =    1.31 min.
Time of concentration (TC) =     8.89 min.


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Process from Point/Station       14.000 to Point/Station       14.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.073(In/Hr)
Time of concentration =     8.89 min.
Rainfall intensity =      2.308(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.842
Subarea runoff =      0.270(CFS) for    0.320(Ac.)
Total runoff =      4.091(CFS)
Effective area this stream =        2.10(Ac.)
Total Study Area (Main Stream No. 1) =        2.14(Ac.)
Area averaged Fm value =    0.148(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.000 to Point/Station       15.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1151.900(Ft.)
Downstream point/station elevation =  1145.300(Ft.)
Pipe length  =   149.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     4.091(CFS)
Nearest computed pipe diameter  =     12.00(In.)
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Calculated individual pipe flow  =     4.091(CFS)
Normal flow depth in pipe =    6.32(In.)
Flow top width inside pipe =   11.98(In.)
Critical Depth =   10.27(In.)
Pipe flow velocity =      9.75(Ft/s)
Travel time through pipe =    0.25 min.
Time of concentration (TC) =     9.14 min.


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Process from Point/Station       14.000 to Point/Station       15.000
**** CONFLUENCE OF MAIN STREAMS ****
________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =      2.104(Ac.)
Runoff from this stream =      4.091(CFS)
Time of concentration =    9.14 min.
Rainfall intensity =     2.270(In/Hr)
Area averaged loss rate (Fm) =    0.1477(In/Hr)
Area averaged Pervious ratio (Ap) = 0.2142
Program is now starting with Main Stream No. 2


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       16.000 to Point/Station       17.000
**** INITIAL AREA EVALUATION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.073(In/Hr)
Initial subarea data:
Initial area flow distance =   136.000(Ft.)
Top (of initial area) elevation =  1160.300(Ft.)
Bottom (of initial area) elevation =  1159.200(Ft.)
Difference in elevation =     1.100(Ft.)
Slope =    0.00809  s(%)=       0.81
TC = k(0.304)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    5.685 min.
Rainfall intensity =      3.018(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.878
Subarea runoff =      0.345(CFS)
Total initial stream area =        0.130(Ac.)
Pervious area fraction = 0.100
Initial area Fm value =    0.073(In/Hr)


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Process from Point/Station       17.000 to Point/Station       18.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =  1156.000(Ft.)
Downstream point/station elevation =  1154.500(Ft.)
Pipe length  =    29.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.345(CFS)
Nearest computed pipe diameter  =      6.00(In.)
Calculated individual pipe flow  =     0.345(CFS)
Normal flow depth in pipe =    2.13(In.)
Flow top width inside pipe =    5.74(In.)
Critical Depth =    3.57(In.)
Pipe flow velocity =      5.52(Ft/s)
Travel time through pipe =    0.09 min.
Time of concentration (TC) =     5.77 min.


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Process from Point/Station       18.000 to Point/Station       18.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.073(In/Hr)
Time of concentration =     5.77 min.
Rainfall intensity =      2.991(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.878
Subarea runoff =      0.522(CFS) for    0.200(Ac.)
Total runoff =      0.866(CFS)
Effective area this stream =        0.33(Ac.)
Total Study Area (Main Stream No. 2) =        2.47(Ac.)
Area averaged Fm value =    0.073(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       18.000 to Point/Station       19.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =  1154.500(Ft.)
Downstream point/station elevation =  1153.900(Ft.)
Pipe length  =   119.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.866(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     0.866(CFS)
Normal flow depth in pipe =    5.75(In.)
Flow top width inside pipe =    8.65(In.)
Critical Depth =    5.11(In.)
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Pipe flow velocity =      2.91(Ft/s)
Travel time through pipe =    0.68 min.
Time of concentration (TC) =     6.45 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       19.000 to Point/Station       19.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
APARTMENT subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.2000     Max loss rate(Fm)=     0.147(In/Hr)
Time of concentration =     6.45 min.
Rainfall intensity =      2.797(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.864
Subarea runoff =      0.777(CFS) for    0.350(Ac.)
Total runoff =      1.644(CFS)
Effective area this stream =        0.68(Ac.)
Total Study Area (Main Stream No. 2) =        2.82(Ac.)
Area averaged Fm value =    0.111(In/Hr)


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Process from Point/Station       19.000 to Point/Station       20.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1153.900(Ft.)
Downstream point/station elevation =  1152.900(Ft.)
Pipe length  =   187.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.644(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     1.644(CFS)
Normal flow depth in pipe =    6.91(In.)
Flow top width inside pipe =   11.86(In.)
Critical Depth =    6.53(In.)
Pipe flow velocity =      3.51(Ft/s)
Travel time through pipe =    0.89 min.
Time of concentration (TC) =     7.34 min.


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Process from Point/Station       20.000 to Point/Station       20.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
```

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Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.073(In/Hr)
Time of concentration =     7.34 min.
Rainfall intensity =      2.589(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.866
Subarea runoff =      0.642(CFS) for    0.340(Ac.)
Total runoff =      2.286(CFS)
Effective area this stream =        1.02(Ac.)
Total Study Area (Main Stream No. 2) =        3.16(Ac.)
Area averaged Fm value =    0.099(In/Hr)


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Process from Point/Station       20.000 to Point/Station       21.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1152.900(Ft.)
Downstream point/station elevation =  1151.900(Ft.)
Pipe length  =   182.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.286(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     2.286(CFS)
Normal flow depth in pipe =    8.63(In.)
Flow top width inside pipe =   10.79(In.)
Critical Depth =    7.76(In.)
Pipe flow velocity =      3.79(Ft/s)
Travel time through pipe =    0.80 min.
Time of concentration (TC) =     8.14 min.


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Process from Point/Station       21.000 to Point/Station       21.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.073(In/Hr)
Time of concentration =     8.14 min.
Rainfall intensity =      2.433(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.867
Subarea runoff =      1.088(CFS) for    0.580(Ac.)
Total runoff =      3.374(CFS)
Effective area this stream =        1.60(Ac.)
Total Study Area (Main Stream No. 2) =        3.74(Ac.)
```

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Area averaged Fm value =    0.089(In/Hr)


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Process from Point/Station       21.000 to Point/Station       15.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1151.900(Ft.)
Downstream point/station elevation =  1145.300(Ft.)
Pipe length  =    47.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.374(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     3.374(CFS)
Normal flow depth in pipe =    4.73(In.)
Flow top width inside pipe =    8.99(In.)
Critical depth could not be calculated.
Pipe flow velocity =     14.33(Ft/s)
Travel time through pipe =    0.05 min.
Time of concentration (TC) =     8.20 min.


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Process from Point/Station       21.000 to Point/Station       15.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      1.600(Ac.)
Runoff from this stream =      3.374(CFS)
Time of concentration =    8.20 min.
Rainfall intensity =     2.423(In/Hr)
Area averaged loss rate (Fm) =    0.0894(In/Hr)
Area averaged Pervious ratio (Ap) = 0.1219
Summary of stream data:

Stream Flow rate    Area    TC     Fm       Rainfall Intensity
 No.    (CFS)   (Ac.)       (min) (In/Hr)     (In/Hr)


1      4.09     2.104      9.14    0.148      2.270
2      3.37     1.600      8.20    0.089      2.423
Qmax(1) =
           1.000 *    1.000 *     4.091) +
           0.934 *    1.000 *     3.374) + =       7.243
Qmax(2) =
           1.072 *    0.897 *     4.091) +
           1.000 *    1.000 *     3.374) + =       7.308

Total of 2 main streams to confluence:
Flow rates before confluence point:
       5.091       4.374
Maximum flow rates at confluence using above data:
```

```
        7.243        7.308
Area of streams before confluence:
        2.104        1.600
Effective area values after confluence:
        3.704        3.486


Results of confluence:
Total flow rate =      7.308(CFS)
Time of concentration =     8.199 min.
Effective stream area after confluence  =      3.486(Ac.)
Study area average Pervious fraction(Ap) =  0.174
Study area average soil loss rate(Fm) =    0.123(In/Hr)
Study area total =       3.70(Ac.)


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Process from Point/Station       15.000 to Point/Station       15.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 78.00
Pervious ratio(Ap) = 1.0000     Max loss rate(Fm)=     0.404(In/Hr)
Time of concentration =     8.20 min.
Rainfall intensity =      2.423(In/Hr) for a    10.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.838
Subarea runoff =      1.110(CFS) for    0.660(Ac.)
Total runoff =      8.418(CFS)
Effective area this stream =        4.15(Ac.)
Total Study Area (Main Stream No. 1) =        4.40(Ac.)
Area averaged Fm value =    0.167(In/Hr)
End of computations, Total Study Area =            4.40 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.
Note: These figures do not consider reduced effective area
effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.299
Area averaged SCS curve number =  59.6
```

# B.4 – PROPOSED 100-YEAR ANALYSIS

San Bernardino County Rational Hydrology Program

(Hydrology Manual Date - August 1986)

CIVILCADD/CIVILDESIGN Engineering Software, (c) 1989-2019 Version 9.1
Rational Hydrology Study Date: 08/26/24

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TPM 20854
DEVELOPED CONDITION
100-YEAR

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Program License Serial Number 6568

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********* Hydrology Study Control Information **********

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Rational hydrology study storm event year is 100.0
10 Year storm 1 hour rainfall = 0.734(In.)
100 Year storm 1 hour rainfall = 1.160(In.)
Computed rainfall intensity:
Storm year = 100.00 1 hour rainfall = 1.160 (In.)
Slope used for rainfall intensity curve b = 0.6000
Soil antecedent moisture condition (AMC) = 3

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Process from Point/Station 1.000 to Point/Station 2.000
**** INITIAL AREA EVALUATION ****

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CONDOMINIUM subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2) = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.3500 Max loss rate(Fm)= 0.154(In/Hr)
Initial subarea data:
Initial area flow distance = 92.000(Ft.)
Top (of initial area) elevation = 1161.000(Ft.)
Bottom (of initial area) elevation = 1160.000(Ft.)
Difference in elevation = 1.000(Ft.)
Slope = 0.01087 s(%)= 1.09
TC = k(0.360)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration = 5.427 min.
Rainfall intensity = 4.905(In/Hr) for a 100.0 year storm

```
Effective runoff coefficient used for area (Q=KCIA) is C = 0.872
Subarea runoff =      0.342(CFS)
Total initial stream area =        0.080(Ac.)
Pervious area fraction = 0.350
Initial area Fm value =    0.154(In/Hr)


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Process from Point/Station        2.000 to Point/Station        3.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1156.500(Ft.)
Downstream point/station elevation =  1155.800(Ft.)
Pipe length  =   134.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.342(CFS)
Nearest computed pipe diameter  =      6.00(In.)
Calculated individual pipe flow  =     0.342(CFS)
Normal flow depth in pipe =    4.22(In.)
Flow top width inside pipe =    5.48(In.)
Critical Depth =    3.56(In.)
Pipe flow velocity =      2.32(Ft/s)
Travel time through pipe =    0.96 min.
Time of concentration (TC) =     6.39 min.


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Process from Point/Station        3.000 to Point/Station        3.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
CONDOMINIUM subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.3500     Max loss rate(Fm)=     0.154(In/Hr)
Time of concentration =     6.39 min.
Rainfall intensity =      4.446(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.869
Subarea runoff =      0.546(CFS) for    0.150(Ac.)
Total runoff =      0.888(CFS)
Effective area this stream =        0.23(Ac.)
Total Study Area (Main Stream No. 1) =        0.23(Ac.)
Area averaged Fm value =    0.154(In/Hr)


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Process from Point/Station        3.000 to Point/Station        4.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
```

```
Upstream point/station elevation =  1155.800(Ft.)
Downstream point/station elevation =   155.500(Ft.)
Pipe length  =    60.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.888(CFS)
Nearest computed pipe diameter  =      3.00(In.)
Calculated individual pipe flow  =     0.888(CFS)
Normal flow depth in pipe =    1.01(In.)
Flow top width inside pipe =    2.84(In.)
Critical depth could not be calculated.
Pipe flow velocity =     60.84(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =     6.41 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        4.000 to Point/Station        4.000
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
UNDEVELOPED (average cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 69.00
Adjusted SCS curve number for AMC 3 = 86.20
Pervious ratio(Ap) = 1.0000     Max loss rate(Fm)=     0.262(In/Hr)
Time of concentration =     6.41 min.
Rainfall intensity =      4.439(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.862
Subarea runoff =      0.412(CFS) for    0.110(Ac.)
Total runoff =      1.301(CFS)
Effective area this stream =        0.34(Ac.)
Total Study Area (Main Stream No. 1) =        0.34(Ac.)
Area averaged Fm value =    0.189(In/Hr)


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Process from Point/Station        4.000 to Point/Station        5.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =  1155.500(Ft.)
Downstream point/station elevation =  1155.300(Ft.)
Pipe length  =    27.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.301(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     1.301(CFS)
Normal flow depth in pipe =    6.76(In.)
Flow top width inside pipe =    7.78(In.)
Critical Depth =    6.31(In.)
Pipe flow velocity =      3.65(Ft/s)
Travel time through pipe =    0.12 min.
```

```
Time of concentration (TC) =     6.53 min.


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Process from Point/Station        5.000 to Point/Station        5.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.044(In/Hr)
Time of concentration =     6.53 min.
Rainfall intensity =      4.389(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.872
Subarea runoff =      0.688(CFS) for    0.180(Ac.)
Total runoff =      1.989(CFS)
Effective area this stream =        0.52(Ac.)
Total Study Area (Main Stream No. 1) =        0.52(Ac.)
Area averaged Fm value =    0.139(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        5.000 to Point/Station        6.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1155.300(Ft.)
Downstream point/station elevation =  1155.000(Ft.)
Pipe length  =    54.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.989(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     1.989(CFS)
Normal flow depth in pipe =    7.75(In.)
Flow top width inside pipe =   11.48(In.)
Critical Depth =    7.22(In.)
Pipe flow velocity =      3.71(Ft/s)
Travel time through pipe =    0.24 min.
Time of concentration (TC) =     6.77 min.


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Process from Point/Station        6.000 to Point/Station        6.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
CONDOMINIUM subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
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Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.3500     Max loss rate(Fm)=     0.154(In/Hr)
Time of concentration =     6.77 min.
Rainfall intensity =      4.294(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.870
Subarea runoff =      0.775(CFS) for    0.220(Ac.)
Total runoff =      2.764(CFS)
Effective area this stream =        0.74(Ac.)
Total Study Area (Main Stream No. 1) =        0.74(Ac.)
Area averaged Fm value =    0.143(In/Hr)


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Process from Point/Station        6.000 to Point/Station        7.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1155.000(Ft.)
Downstream point/station elevation =  1154.700(Ft.)
Pipe length  =    46.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.764(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     2.764(CFS)
Normal flow depth in pipe =    9.45(In.)
Flow top width inside pipe =    9.82(In.)
Critical Depth =    8.56(In.)
Pipe flow velocity =      4.17(Ft/s)
Travel time through pipe =    0.18 min.
Time of concentration (TC) =     6.96 min.


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Process from Point/Station        7.000 to Point/Station        7.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.044(In/Hr)
Time of concentration =     6.96 min.
Rainfall intensity =      4.225(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.870
Subarea runoff =      0.067(CFS) for    0.030(Ac.)
Total runoff =      2.832(CFS)
Effective area this stream =        0.77(Ac.)
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Total Study Area (Main Stream No. 1) =        0.77(Ac.)
Area averaged Fm value =    0.139(In/Hr)


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Process from Point/Station        7.000 to Point/Station        8.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1154.700(Ft.)
Downstream point/station elevation =  1153.600(Ft.)
Pipe length  =   109.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.832(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     2.832(CFS)
Normal flow depth in pipe =    8.05(In.)
Flow top width inside pipe =   11.28(In.)
Critical Depth =    8.65(In.)
Pipe flow velocity =      5.05(Ft/s)
Travel time through pipe =    0.36 min.
Time of concentration (TC) =     7.32 min.


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Process from Point/Station        7.000 to Point/Station        8.000
**** CONFLUENCE OF MAIN STREAMS ****
________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =      0.770(Ac.)
Runoff from this stream =      2.832(CFS)
Time of concentration =    7.32 min.
Rainfall intensity =     4.100(In/Hr)
Area averaged loss rate (Fm) =    0.1393(In/Hr)
Area averaged Pervious ratio (Ap) = 0.3747
Program is now starting with Main Stream No. 2


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Process from Point/Station        9.000 to Point/Station       10.000
**** INITIAL AREA EVALUATION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.044(In/Hr)
Initial subarea data:
Initial area flow distance =   259.000(Ft.)
Top (of initial area) elevation =  1160.200(Ft.)
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```
Bottom (of initial area) elevation =  1158.000(Ft.)
Difference in elevation =     2.200(Ft.)
Slope =    0.00849  s(%)=       0.85
TC = k(0.304)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.284 min.
Rainfall intensity =      4.111(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.890
Subarea runoff =      1.244(CFS)
Total initial stream area =        0.340(Ac.)
Pervious area fraction = 0.100
Initial area Fm value =    0.044(In/Hr)


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Process from Point/Station       10.000 to Point/Station       11.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1154.500(Ft.)
Downstream point/station elevation =  1154.000(Ft.)
Pipe length  =    81.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.244(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     1.244(CFS)
Normal flow depth in pipe =    7.05(In.)
Flow top width inside pipe =    7.41(In.)
Critical Depth =    6.17(In.)
Pipe flow velocity =      3.35(Ft/s)
Travel time through pipe =    0.40 min.
Time of concentration (TC) =     7.69 min.


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Process from Point/Station       11.000 to Point/Station       11.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.044(In/Hr)
Time of concentration =     7.69 min.
Rainfall intensity =      3.980(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.890
Subarea runoff =      0.350(CFS) for    0.110(Ac.)
Total runoff =      1.594(CFS)
Effective area this stream =        0.45(Ac.)
Total Study Area (Main Stream No. 2) =        1.22(Ac.)
Area averaged Fm value =    0.044(In/Hr)
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Process from Point/Station       11.000 to Point/Station       12.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1154.000(Ft.)
Downstream point/station elevation =  1153.900(Ft.)
Pipe length  =     8.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.594(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     1.594(CFS)
Normal flow depth in pipe =    6.45(In.)
Flow top width inside pipe =    8.12(In.)
Critical Depth =    6.97(In.)
Pipe flow velocity =      4.71(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =     7.72 min.


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Process from Point/Station       12.000 to Point/Station       12.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.044(In/Hr)
Time of concentration =     7.72 min.
Rainfall intensity =      3.971(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.890
Subarea runoff =      0.421(CFS) for    0.120(Ac.)
Total runoff =      2.015(CFS)
Effective area this stream =        0.57(Ac.)
Total Study Area (Main Stream No. 2) =        1.34(Ac.)
Area averaged Fm value =    0.044(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       12.000 to Point/Station       13.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1153.900(Ft.)
Downstream point/station elevation =  1153.700(Ft.)
Pipe length  =    34.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.015(CFS)
Nearest computed pipe diameter  =     12.00(In.)
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Calculated individual pipe flow  =     2.015(CFS)
Normal flow depth in pipe =    7.66(In.)
Flow top width inside pipe =   11.53(In.)
Critical Depth =    7.27(In.)
Pipe flow velocity =      3.81(Ft/s)
Travel time through pipe =    0.15 min.
Time of concentration (TC) =     7.86 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       13.000 to Point/Station       13.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.044(In/Hr)
Time of concentration =     7.86 min.
Rainfall intensity =      3.926(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.890
Subarea runoff =      0.466(CFS) for    0.140(Ac.)
Total runoff =      2.481(CFS)
Effective area this stream =        0.71(Ac.)
Total Study Area (Main Stream No. 2) =        1.48(Ac.)
Area averaged Fm value =    0.044(In/Hr)


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Process from Point/Station       13.000 to Point/Station        8.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1153.700(Ft.)
Downstream point/station elevation =  1153.600(Ft.)
Pipe length  =    13.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.481(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     2.481(CFS)
Normal flow depth in pipe =    8.07(In.)
Flow top width inside pipe =   11.26(In.)
Critical Depth =    8.09(In.)
Pipe flow velocity =      4.41(Ft/s)
Travel time through pipe =    0.05 min.
Time of concentration (TC) =     7.91 min.


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Process from Point/Station       13.000 to Point/Station        8.000
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**** CONFLUENCE OF MAIN STREAMS ****
_____________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      0.710(Ac.)
Runoff from this stream =      2.481(CFS)
Time of concentration =    7.91 min.
Rainfall intensity =     3.911(In/Hr)
Area averaged loss rate (Fm) =    0.0440(In/Hr)
Area averaged Pervious ratio (Ap) = 0.1000
Summary of stream data:

Stream Flow rate    Area    TC     Fm       Rainfall Intensity
 No.    (CFS)   (Ac.)       (min) (In/Hr)     (In/Hr)


1      2.83     0.770      7.32    0.139      4.100
2      2.48     0.710      7.91    0.044      3.911
Qmax(1) =
           1.000 *    1.000 *     2.832) +
           1.049 *    0.925 *     2.481) + =       5.237
Qmax(2) =
           0.953 *    1.000 *     2.832) +
           1.000 *    1.000 *     2.481) + =       5.178

Total of 2 main streams to confluence:
Flow rates before confluence point:
       3.832       3.481
Maximum flow rates at confluence using above data:
        5.237        5.178
Area of streams before confluence:
        0.770        0.710
Effective area values after confluence:
        1.427        1.480


Results of confluence:
Total flow rate =      5.237(CFS)
Time of concentration =     7.317 min.
Effective stream area after confluence  =      1.427(Ac.)
Study area average Pervious fraction(Ap) =  0.243
Study area average soil loss rate(Fm) =    0.094(In/Hr)
Study area total =       1.48(Ac.)


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Process from Point/Station        8.000 to Point/Station        8.000
**** SUBAREA FLOW ADDITION ****
_____________________________________________________________________________
APARTMENT subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
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Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.2000     Max loss rate(Fm)=     0.088(In/Hr)
Time of concentration =     7.32 min.
Rainfall intensity =      4.100(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.880
Subarea runoff =      1.134(CFS) for    0.340(Ac.)
Total runoff =      6.371(CFS)
Effective area this stream =        1.77(Ac.)
Total Study Area (Main Stream No. 1) =        1.82(Ac.)
Area averaged Fm value =    0.093(In/Hr)


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Process from Point/Station        8.000 to Point/Station       14.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1153.600(Ft.)
Downstream point/station elevation =  1151.900(Ft.)
Pipe length  =   332.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     6.371(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     6.371(CFS)
Normal flow depth in pipe =   12.73(In.)
Flow top width inside pipe =   16.38(In.)
Critical Depth =   11.71(In.)
Pipe flow velocity =      4.77(Ft/s)
Travel time through pipe =    1.16 min.
Time of concentration (TC) =     8.48 min.


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Process from Point/Station       14.000 to Point/Station       14.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.044(In/Hr)
Time of concentration =     8.48 min.
Rainfall intensity =      3.753(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.880
Subarea runoff =      0.518(CFS) for    0.320(Ac.)
Total runoff =      6.888(CFS)
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Effective area this stream =        2.09(Ac.)
Total Study Area (Main Stream No. 1) =        2.14(Ac.)
Area averaged Fm value =    0.085(In/Hr)


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Process from Point/Station       14.000 to Point/Station       15.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1151.900(Ft.)
Downstream point/station elevation =  1145.300(Ft.)
Pipe length  =   149.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     6.888(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     6.888(CFS)
Normal flow depth in pipe =    9.06(In.)
Flow top width inside pipe =   10.32(In.)
Critical depth could not be calculated.
Pipe flow velocity =     10.83(Ft/s)
Travel time through pipe =    0.23 min.
Time of concentration (TC) =     8.71 min.


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Process from Point/Station       14.000 to Point/Station       15.000
**** CONFLUENCE OF MAIN STREAMS ****
________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =      2.087(Ac.)
Runoff from this stream =      6.888(CFS)
Time of concentration =    8.71 min.
Rainfall intensity =     3.694(In/Hr)
Area averaged loss rate (Fm) =    0.0851(In/Hr)
Area averaged Pervious ratio (Ap) = 0.2140
Program is now starting with Main Stream No. 2


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Process from Point/Station       16.000 to Point/Station       17.000
**** INITIAL AREA EVALUATION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.044(In/Hr)
Initial subarea data:
Initial area flow distance =   136.000(Ft.)
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Top (of initial area) elevation =  1160.300(Ft.)
Bottom (of initial area) elevation =  1159.200(Ft.)
Difference in elevation =     1.100(Ft.)
Slope =    0.00809  s(%)=       0.81
TC = k(0.304)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    5.685 min.
Rainfall intensity =      4.770(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area (Q=KCIA) is C = 0.892
Subarea runoff =      0.553(CFS)
Total initial stream area =        0.130(Ac.)
Pervious area fraction = 0.100
Initial area Fm value =    0.044(In/Hr)


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Process from Point/Station       17.000 to Point/Station       18.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1156.000(Ft.)
Downstream point/station elevation =  1154.500(Ft.)
Pipe length  =    29.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     0.553(CFS)
Nearest computed pipe diameter  =      6.00(In.)
Calculated individual pipe flow  =     0.553(CFS)
Normal flow depth in pipe =    2.76(In.)
Flow top width inside pipe =    5.98(In.)
Critical Depth =    4.55(In.)
Pipe flow velocity =      6.26(Ft/s)
Travel time through pipe =    0.08 min.
Time of concentration (TC) =     5.76 min.


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Process from Point/Station       18.000 to Point/Station       18.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.044(In/Hr)
Time of concentration =     5.76 min.
Rainfall intensity =      4.732(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.892
Subarea runoff =      0.839(CFS) for    0.200(Ac.)
Total runoff =      1.392(CFS)
Effective area this stream =        0.33(Ac.)
Total Study Area (Main Stream No. 2) =        2.47(Ac.)
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Area averaged Fm value =    0.044(In/Hr)


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Process from Point/Station       18.000 to Point/Station       19.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1154.500(Ft.)
Downstream point/station elevation =  1153.900(Ft.)
Pipe length  =   119.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.392(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     1.392(CFS)
Normal flow depth in pipe =    6.35(In.)
Flow top width inside pipe =   11.98(In.)
Critical Depth =    5.99(In.)
Pipe flow velocity =      3.30(Ft/s)
Travel time through pipe =    0.60 min.
Time of concentration (TC) =     6.36 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       19.000 to Point/Station       19.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
APARTMENT subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.2000     Max loss rate(Fm)=     0.088(In/Hr)
Time of concentration =     6.36 min.
Rainfall intensity =      4.458(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.887
Subarea runoff =      1.295(CFS) for    0.350(Ac.)
Total runoff =      2.687(CFS)
Effective area this stream =        0.68(Ac.)
Total Study Area (Main Stream No. 2) =        2.82(Ac.)
Area averaged Fm value =    0.067(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       19.000 to Point/Station       20.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1153.900(Ft.)
Downstream point/station elevation =  1152.900(Ft.)
Pipe length  =   187.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.687(CFS)
```

```
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     2.687(CFS)
Normal flow depth in pipe =    8.10(In.)
Flow top width inside pipe =   14.95(In.)
Critical Depth =    7.89(In.)
Pipe flow velocity =      3.97(Ft/s)
Travel time through pipe =    0.78 min.
Time of concentration (TC) =     7.15 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       20.000 to Point/Station       20.000
**** SUBAREA FLOW ADDITION ****
_____________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.044(In/Hr)
Time of concentration =     7.15 min.
Rainfall intensity =      4.158(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.887
Subarea runoff =      1.075(CFS) for    0.340(Ac.)
Total runoff =      3.762(CFS)
Effective area this stream =        1.02(Ac.)
Total Study Area (Main Stream No. 2) =        3.16(Ac.)
Area averaged Fm value =    0.059(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       20.000 to Point/Station       21.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
_____________________________________________________________________________
Upstream point/station elevation =  1152.900(Ft.)
Downstream point/station elevation =  1151.900(Ft.)
Pipe length  =   182.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.762(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     3.762(CFS)
Normal flow depth in pipe =   10.02(In.)
Flow top width inside pipe =   14.13(In.)
Critical Depth =    9.41(In.)
Pipe flow velocity =      4.32(Ft/s)
Travel time through pipe =    0.70 min.
Time of concentration (TC) =     7.85 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
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```
Process from Point/Station       21.000 to Point/Station       21.000
**** SUBAREA FLOW ADDITION ****
____________________________________________________________________________
COMMERCIAL subarea type
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 56.00
Adjusted SCS curve number for AMC 3 = 75.80
Pervious ratio(Ap) = 0.1000     Max loss rate(Fm)=     0.044(In/Hr)
Time of concentration =     7.85 min.
Rainfall intensity =      3.930(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.888
Subarea runoff =      1.820(CFS) for    0.580(Ac.)
Total runoff =      5.582(CFS)
Effective area this stream =        1.60(Ac.)
Total Study Area (Main Stream No. 2) =        3.74(Ac.)
Area averaged Fm value =    0.054(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       21.000 to Point/Station       15.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
____________________________________________________________________________
Upstream point/station elevation =  1151.900(Ft.)
Downstream point/station elevation =  1145.300(Ft.)
Pipe length  =    47.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     5.582(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     5.582(CFS)
Normal flow depth in pipe =    6.68(In.)
Flow top width inside pipe =    7.87(In.)
Critical depth could not be calculated.
Pipe flow velocity =     15.88(Ft/s)
Travel time through pipe =    0.05 min.
Time of concentration (TC) =     7.90 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       21.000 to Point/Station       15.000
**** CONFLUENCE OF MAIN STREAMS ****
____________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      1.600(Ac.)
Runoff from this stream =      5.582(CFS)
Time of concentration =    7.90 min.
Rainfall intensity =     3.916(In/Hr)
Area averaged loss rate (Fm) =    0.0536(In/Hr)
Area averaged Pervious ratio (Ap) = 0.1219
```

```
Summary of stream data:

Stream Flow rate    Area    TC     Fm       Rainfall Intensity
 No.    (CFS)   (Ac.)       (min) (In/Hr)     (In/Hr)


1      6.89     2.087      8.71    0.085      3.694
2      5.58     1.600      7.90    0.054      3.916
Qmax(1) =
           1.000 *    1.000 *     6.888) +
           0.943 *    1.000 *     5.582) + =      12.150
Qmax(2) =
           1.062 *    0.907 *     6.888) +
           1.000 *    1.000 *     5.582) + =      12.217

Total of 2 main streams to confluence:
Flow rates before confluence point:
       7.888       6.582
Maximum flow rates at confluence using above data:
       12.150       12.217
Area of streams before confluence:
        2.087        1.600
Effective area values after confluence:
        3.687        3.493


Results of confluence:
Total flow rate =     12.217(CFS)
Time of concentration =     7.899 min.
Effective stream area after confluence  =      3.493(Ac.)
Study area average Pervious fraction(Ap) =  0.174
Study area average soil loss rate(Fm) =    0.071(In/Hr)
Study area total =       3.69(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       15.000 to Point/Station       15.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
UNDEVELOPED (poor cover) subarea
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
SCS curve number for soil(AMC 2)  = 78.00
Adjusted SCS curve number for AMC 3 = 92.80
Pervious ratio(Ap) = 1.0000     Max loss rate(Fm)=     0.140(In/Hr)
Time of concentration =     7.90 min.
Rainfall intensity =      3.916(In/Hr) for a   100.0 year storm
Effective runoff coefficient used for area,(total area with modified
rational method)(Q=KCIA) is C = 0.881
Subarea runoff =      2.111(CFS) for    0.660(Ac.)
```

Total runoff = 14.328(CFS)
Effective area this stream = 4.15(Ac.)
Total Study Area (Main Stream No. 1) = 4.40(Ac.)
Area averaged Fm value = 0.082(In/Hr)
End of computations, Total Study Area = 4.40 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.
Note: These figures do not consider reduced effective area
effects caused by confluences in the rational equation.

Area averaged pervious area fraction(Ap) = 0.299
Area averaged SCS curve number = 59.6

| Unit Hydrograph Analysis | | | | |
|---|---|---|---|---|
| | Acreage (ac.) | Runoff, Q (cfs) | Runoff Volume (ac-ft.) | Runoff Volume (cu-ft.) |
| Existing 10-yr, 24-hr | 5.55 | 4.9 | 0.656 | 28,575 |
| Existing 25-yr, 24-hr | | 6.4 | 0.8967 | 39,060 |
| Proposed 10-yr, 24-hr | 4.4 | 8.3 | 0.8321 | 36,246 |
| Proposed 100-yr, 24-hr | | 14.4 | 1.4981 | 65,257 |

# C.1 – Existing 10-Year Analysis

U n i t  H y d r o g r a p h  A n a l y s i s



Study date 08/26/24

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San Bernardino County Synthetic Unit Hydrology Method
Manual date - August 1986

Program License Serial Number 6568

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TPM 20854
EXISTING UNIT HYDROGRAPH
10-YEAR
24-HOUR

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Storm Event Year = 10

Antecedent Moisture Condition = 2

English (in-lb) Input Units Used

English Rainfall Data (Inches) Input Values Used

English Units used in output format

Area averaged rainfall intensity isohyetal data:

| Sub-Area (Ac.) | Duration (hours) | Isohyetal (In) |
|---|---|---|
| Rainfall data for year 10 | | |
| 5.55 | 1 | 0.73 |
| Rainfall data for year 2 | | |
| 5.55 | 6 | 1.15 |
| Rainfall data for year 2 | | |
| 5.55 | 24 | 2.05 |
| Rainfall data for year 100 | | |
| 5.55 | 1 | 1.16 |

---

```
Rainfall data for year 100
             5.55            6            2.65
------------------------------------------------------------------------
Rainfall data for year 100
             5.55           24            4.82
------------------------------------------------------------------------
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++

******** Area-averaged max loss rate, Fm ********


SCS curve  SCS curve     Area      Area     Fp(Fig C6)    Ap      Fm
No.(AMCII) NO.(AMC 2)    (Ac.)    Fraction     (In/Hr)  (dec.)   (In/Hr)
 78.0      78.0          5.55      1.000     0.404    1.000    0.404

Area-averaged adjusted loss rate Fm (In/Hr) =  0.404

********* Area-Averaged low loss rate fraction, Yb **********

Area       Area          SCS CN    SCS CN      S     Pervious
 (Ac.)      Fract         (AMC2)    (AMC2)           Yield Fr
     5.55   1.000         78.0      78.0       2.82     0.397

Area-averaged catchment yield fraction, Y =  0.397
Area-averaged low loss fraction, Yb =  0.603
User entry of time of concentration  =   0.313 (hours)
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Watershed area =       5.55(Ac.)
Catchment Lag time =   0.250 hours
Unit interval =   5.000 minutes
Unit interval percentage of lag time = 33.3014
Hydrograph baseflow =     0.00(CFS)
Average maximum watershed loss rate(Fm) =  0.404(In/Hr)
Average low loss rate fraction (Yb) = 0.603 (decimal)
VALLEY UNDEVELOPED S-Graph Selected
Computed peak 5-minute rainfall =  0.272(In)
Computed peak 30-minute rainfall =  0.556(In)
Specified peak 1-hour rainfall =  0.734(In)
Computed peak 3-hour rainfall =  1.258(In)
Specified peak 6-hour rainfall =  1.767(In)
Specified peak 24-hour rainfall =  3.190(In)


Rainfall depth area reduction factors:
Using a total area of       5.55(Ac.) (Ref: fig. E-4)

5-minute factor = 1.000     Adjusted rainfall =  0.272(In)
30-minute factor = 1.000    Adjusted rainfall =  0.556(In)
1-hour factor = 1.000       Adjusted rainfall =  0.734(In)
3-hour factor = 1.000       Adjusted rainfall =  1.258(In)
6-hour factor = 1.000       Adjusted rainfall =  1.767(In)
24-hour factor = 1.000      Adjusted rainfall =  3.190(In)
```

---

U n i t  H y d r o g r a p h

| Interval Number | 'S' Graph Mean values | Unit Hydrograph ((CFS)) |
|---|---|---|
| | (K = 67.12 (CFS)) | |
| 1 | 3.346 | 2.246 |
| 2 | 16.202 | 8.629 |
| 3 | 37.964 | 14.606 |
| 4 | 58.047 | 13.480 |
| 5 | 69.166 | 7.463 |
| 6 | 75.483 | 4.240 |
| 7 | 79.955 | 3.001 |
| 8 | 83.427 | 2.331 |
| 9 | 86.263 | 1.903 |
| 10 | 88.482 | 1.489 |
| 11 | 90.416 | 1.298 |
| 12 | 91.950 | 1.030 |
| 13 | 93.221 | 0.852 |
| 14 | 94.278 | 0.710 |
| 15 | 95.286 | 0.676 |
| 16 | 96.156 | 0.584 |
| 17 | 96.873 | 0.481 |
| 18 | 97.490 | 0.414 |
| 19 | 98.025 | 0.359 |
| 20 | 98.476 | 0.303 |
| 21 | 98.827 | 0.236 |
| 22 | 99.160 | 0.224 |
| 23 | 99.493 | 0.224 |
| 24 | 99.826 | 0.224 |
| 25 | 100.000 | 0.117 |

| Peak Unit Number | Adjusted mass rainfall (In) | Unit rainfall (In) |
|---|---|---|
| 1 | 0.2716 | 0.2716 |
| 2 | 0.3584 | 0.0868 |
| 3 | 0.4215 | 0.0631 |
| 4 | 0.4729 | 0.0514 |
| 5 | 0.5170 | 0.0441 |
| 6 | 0.5561 | 0.0391 |
| 7 | 0.5915 | 0.0354 |
| 8 | 0.6239 | 0.0325 |
| 9 | 0.6540 | 0.0301 |
| 10 | 0.6822 | 0.0282 |
| 11 | 0.7087 | 0.0265 |
| 12 | 0.7338 | 0.0251 |
| 13 | 0.7632 | 0.0294 |
| 14 | 0.7915 | 0.0283 |
| 15 | 0.8187 | 0.0272 |

| | | |
|---|---|---|
| 16 | 0.8450 | 0.0263 |
| 17 | 0.8705 | 0.0255 |
| 18 | 0.8953 | 0.0248 |
| 19 | 0.9194 | 0.0241 |
| 20 | 0.9428 | 0.0234 |
| 21 | 0.9656 | 0.0228 |
| 22 | 0.9879 | 0.0223 |
| 23 | 1.0097 | 0.0218 |
| 24 | 1.0310 | 0.0213 |
| 25 | 1.0518 | 0.0209 |
| 26 | 1.0723 | 0.0204 |
| 27 | 1.0923 | 0.0200 |
| 28 | 1.1120 | 0.0197 |
| 29 | 1.1313 | 0.0193 |
| 30 | 1.1503 | 0.0190 |
| 31 | 1.1689 | 0.0187 |
| 32 | 1.1873 | 0.0183 |
| 33 | 1.2053 | 0.0181 |
| 34 | 1.2231 | 0.0178 |
| 35 | 1.2406 | 0.0175 |
| 36 | 1.2579 | 0.0173 |
| 37 | 1.2749 | 0.0170 |
| 38 | 1.2917 | 0.0168 |
| 39 | 1.3082 | 0.0166 |
| 40 | 1.3246 | 0.0163 |
| 41 | 1.3407 | 0.0161 |
| 42 | 1.3567 | 0.0159 |
| 43 | 1.3724 | 0.0157 |
| 44 | 1.3880 | 0.0156 |
| 45 | 1.4033 | 0.0154 |
| 46 | 1.4185 | 0.0152 |
| 47 | 1.4336 | 0.0150 |
| 48 | 1.4485 | 0.0149 |
| 49 | 1.4632 | 0.0147 |
| 50 | 1.4777 | 0.0146 |
| 51 | 1.4922 | 0.0144 |
| 52 | 1.5064 | 0.0143 |
| 53 | 1.5206 | 0.0141 |
| 54 | 1.5346 | 0.0140 |
| 55 | 1.5485 | 0.0139 |
| 56 | 1.5622 | 0.0137 |
| 57 | 1.5758 | 0.0136 |
| 58 | 1.5893 | 0.0135 |
| 59 | 1.6027 | 0.0134 |
| 60 | 1.6160 | 0.0133 |
| 61 | 1.6291 | 0.0132 |
| 62 | 1.6421 | 0.0130 |
| 63 | 1.6551 | 0.0129 |
| 64 | 1.6679 | 0.0128 |
| 65 | 1.6806 | 0.0127 |
| 66 | 1.6933 | 0.0126 |
| 67 | 1.7058 | 0.0125 |

| | | |
|---|---|---|
| 68 | 1.7182 | 0.0124 |
| 69 | 1.7306 | 0.0123 |
| 70 | 1.7428 | 0.0123 |
| 71 | 1.7550 | 0.0122 |
| 72 | 1.7671 | 0.0121 |
| 73 | 1.7775 | 0.0104 |
| 74 | 1.7878 | 0.0103 |
| 75 | 1.7981 | 0.0103 |
| 76 | 1.8083 | 0.0102 |
| 77 | 1.8184 | 0.0101 |
| 78 | 1.8284 | 0.0100 |
| 79 | 1.8383 | 0.0099 |
| 80 | 1.8482 | 0.0099 |
| 81 | 1.8580 | 0.0098 |
| 82 | 1.8677 | 0.0097 |
| 83 | 1.8774 | 0.0097 |
| 84 | 1.8870 | 0.0096 |
| 85 | 1.8966 | 0.0095 |
| 86 | 1.9060 | 0.0095 |
| 87 | 1.9154 | 0.0094 |
| 88 | 1.9248 | 0.0093 |
| 89 | 1.9341 | 0.0093 |
| 90 | 1.9433 | 0.0092 |
| 91 | 1.9525 | 0.0092 |
| 92 | 1.9616 | 0.0091 |
| 93 | 1.9706 | 0.0091 |
| 94 | 1.9796 | 0.0090 |
| 95 | 1.9886 | 0.0089 |
| 96 | 1.9975 | 0.0089 |
| 97 | 2.0063 | 0.0088 |
| 98 | 2.0151 | 0.0088 |
| 99 | 2.0238 | 0.0087 |
| 100 | 2.0325 | 0.0087 |
| 101 | 2.0411 | 0.0086 |
| 102 | 2.0497 | 0.0086 |
| 103 | 2.0583 | 0.0085 |
| 104 | 2.0668 | 0.0085 |
| 105 | 2.0752 | 0.0084 |
| 106 | 2.0836 | 0.0084 |
| 107 | 2.0919 | 0.0084 |
| 108 | 2.1003 | 0.0083 |
| 109 | 2.1085 | 0.0083 |
| 110 | 2.1167 | 0.0082 |
| 111 | 2.1249 | 0.0082 |
| 112 | 2.1330 | 0.0081 |
| 113 | 2.1411 | 0.0081 |
| 114 | 2.1492 | 0.0081 |
| 115 | 2.1572 | 0.0080 |
| 116 | 2.1652 | 0.0080 |
| 117 | 2.1731 | 0.0079 |
| 118 | 2.1810 | 0.0079 |
| 119 | 2.1888 | 0.0079 |

| | | |
|---|---|---|
| 120 | 2.1967 | 0.0078 |
| 121 | 2.2044 | 0.0078 |
| 122 | 2.2122 | 0.0077 |
| 123 | 2.2199 | 0.0077 |
| 124 | 2.2276 | 0.0077 |
| 125 | 2.2352 | 0.0076 |
| 126 | 2.2428 | 0.0076 |
| 127 | 2.2504 | 0.0076 |
| 128 | 2.2579 | 0.0075 |
| 129 | 2.2654 | 0.0075 |
| 130 | 2.2729 | 0.0075 |
| 131 | 2.2803 | 0.0074 |
| 132 | 2.2877 | 0.0074 |
| 133 | 2.2951 | 0.0074 |
| 134 | 2.3024 | 0.0073 |
| 135 | 2.3097 | 0.0073 |
| 136 | 2.3170 | 0.0073 |
| 137 | 2.3242 | 0.0072 |
| 138 | 2.3314 | 0.0072 |
| 139 | 2.3386 | 0.0072 |
| 140 | 2.3458 | 0.0072 |
| 141 | 2.3529 | 0.0071 |
| 142 | 2.3600 | 0.0071 |
| 143 | 2.3670 | 0.0071 |
| 144 | 2.3741 | 0.0070 |
| 145 | 2.3811 | 0.0070 |
| 146 | 2.3881 | 0.0070 |
| 147 | 2.3950 | 0.0070 |
| 148 | 2.4020 | 0.0069 |
| 149 | 2.4089 | 0.0069 |
| 150 | 2.4157 | 0.0069 |
| 151 | 2.4226 | 0.0068 |
| 152 | 2.4294 | 0.0068 |
| 153 | 2.4362 | 0.0068 |
| 154 | 2.4430 | 0.0068 |
| 155 | 2.4497 | 0.0067 |
| 156 | 2.4564 | 0.0067 |
| 157 | 2.4631 | 0.0067 |
| 158 | 2.4698 | 0.0067 |
| 159 | 2.4764 | 0.0066 |
| 160 | 2.4831 | 0.0066 |
| 161 | 2.4897 | 0.0066 |
| 162 | 2.4962 | 0.0066 |
| 163 | 2.5028 | 0.0066 |
| 164 | 2.5093 | 0.0065 |
| 165 | 2.5158 | 0.0065 |
| 166 | 2.5223 | 0.0065 |
| 167 | 2.5288 | 0.0065 |
| 168 | 2.5352 | 0.0064 |
| 169 | 2.5416 | 0.0064 |
| 170 | 2.5480 | 0.0064 |
| 171 | 2.5544 | 0.0064 |

| | | |
|---|---|---|
| 172 | 2.5608 | 0.0064 |
| 173 | 2.5671 | 0.0063 |
| 174 | 2.5734 | 0.0063 |
| 175 | 2.5797 | 0.0063 |
| 176 | 2.5860 | 0.0063 |
| 177 | 2.5922 | 0.0062 |
| 178 | 2.5984 | 0.0062 |
| 179 | 2.6046 | 0.0062 |
| 180 | 2.6108 | 0.0062 |
| 181 | 2.6170 | 0.0062 |
| 182 | 2.6231 | 0.0061 |
| 183 | 2.6293 | 0.0061 |
| 184 | 2.6354 | 0.0061 |
| 185 | 2.6415 | 0.0061 |
| 186 | 2.6476 | 0.0061 |
| 187 | 2.6536 | 0.0061 |
| 188 | 2.6596 | 0.0060 |
| 189 | 2.6657 | 0.0060 |
| 190 | 2.6717 | 0.0060 |
| 191 | 2.6776 | 0.0060 |
| 192 | 2.6836 | 0.0060 |
| 193 | 2.6896 | 0.0059 |
| 194 | 2.6955 | 0.0059 |
| 195 | 2.7014 | 0.0059 |
| 196 | 2.7073 | 0.0059 |
| 197 | 2.7132 | 0.0059 |
| 198 | 2.7190 | 0.0059 |
| 199 | 2.7249 | 0.0058 |
| 200 | 2.7307 | 0.0058 |
| 201 | 2.7365 | 0.0058 |
| 202 | 2.7423 | 0.0058 |
| 203 | 2.7481 | 0.0058 |
| 204 | 2.7538 | 0.0058 |
| 205 | 2.7596 | 0.0057 |
| 206 | 2.7653 | 0.0057 |
| 207 | 2.7710 | 0.0057 |
| 208 | 2.7767 | 0.0057 |
| 209 | 2.7824 | 0.0057 |
| 210 | 2.7880 | 0.0057 |
| 211 | 2.7937 | 0.0056 |
| 212 | 2.7993 | 0.0056 |
| 213 | 2.8049 | 0.0056 |
| 214 | 2.8105 | 0.0056 |
| 215 | 2.8161 | 0.0056 |
| 216 | 2.8217 | 0.0056 |
| 217 | 2.8272 | 0.0056 |
| 218 | 2.8328 | 0.0055 |
| 219 | 2.8383 | 0.0055 |
| 220 | 2.8438 | 0.0055 |
| 221 | 2.8493 | 0.0055 |
| 222 | 2.8548 | 0.0055 |
| 223 | 2.8603 | 0.0055 |

| | | |
|---|---|---|
| 224 | 2.8657 | 0.0055 |
| 225 | 2.8712 | 0.0054 |
| 226 | 2.8766 | 0.0054 |
| 227 | 2.8820 | 0.0054 |
| 228 | 2.8874 | 0.0054 |
| 229 | 2.8928 | 0.0054 |
| 230 | 2.8982 | 0.0054 |
| 231 | 2.9036 | 0.0054 |
| 232 | 2.9089 | 0.0053 |
| 233 | 2.9142 | 0.0053 |
| 234 | 2.9196 | 0.0053 |
| 235 | 2.9249 | 0.0053 |
| 236 | 2.9302 | 0.0053 |
| 237 | 2.9355 | 0.0053 |
| 238 | 2.9407 | 0.0053 |
| 239 | 2.9460 | 0.0053 |
| 240 | 2.9512 | 0.0052 |
| 241 | 2.9565 | 0.0052 |
| 242 | 2.9617 | 0.0052 |
| 243 | 2.9669 | 0.0052 |
| 244 | 2.9721 | 0.0052 |
| 245 | 2.9773 | 0.0052 |
| 246 | 2.9824 | 0.0052 |
| 247 | 2.9876 | 0.0052 |
| 248 | 2.9927 | 0.0051 |
| 249 | 2.9979 | 0.0051 |
| 250 | 3.0030 | 0.0051 |
| 251 | 3.0081 | 0.0051 |
| 252 | 3.0132 | 0.0051 |
| 253 | 3.0183 | 0.0051 |
| 254 | 3.0234 | 0.0051 |
| 255 | 3.0284 | 0.0051 |
| 256 | 3.0335 | 0.0051 |
| 257 | 3.0385 | 0.0050 |
| 258 | 3.0436 | 0.0050 |
| 259 | 3.0486 | 0.0050 |
| 260 | 3.0536 | 0.0050 |
| 261 | 3.0586 | 0.0050 |
| 262 | 3.0636 | 0.0050 |
| 263 | 3.0686 | 0.0050 |
| 264 | 3.0735 | 0.0050 |
| 265 | 3.0785 | 0.0050 |
| 266 | 3.0834 | 0.0049 |
| 267 | 3.0883 | 0.0049 |
| 268 | 3.0933 | 0.0049 |
| 269 | 3.0982 | 0.0049 |
| 270 | 3.1031 | 0.0049 |
| 271 | 3.1080 | 0.0049 |
| 272 | 3.1129 | 0.0049 |
| 273 | 3.1177 | 0.0049 |
| 274 | 3.1226 | 0.0049 |
| 275 | 3.1274 | 0.0048 |

| | | |
|---|---|---|
| 276 | 3.1323 | 0.0048 |
| 277 | 3.1371 | 0.0048 |
| 278 | 3.1419 | 0.0048 |
| 279 | 3.1467 | 0.0048 |
| 280 | 3.1515 | 0.0048 |
| 281 | 3.1563 | 0.0048 |
| 282 | 3.1611 | 0.0048 |
| 283 | 3.1659 | 0.0048 |
| 284 | 3.1706 | 0.0048 |
| 285 | 3.1754 | 0.0048 |
| 286 | 3.1801 | 0.0047 |
| 287 | 3.1849 | 0.0047 |
| 288 | 3.1896 | 0.0047 |

| Unit Period (number) | Unit Rainfall (In) | Unit Soil-Loss (In) | Effective Rainfall (In) |
|---|---|---|---|
| 1 | 0.0047 | 0.0028 | 0.0019 |
| 2 | 0.0047 | 0.0029 | 0.0019 |
| 3 | 0.0048 | 0.0029 | 0.0019 |
| 4 | 0.0048 | 0.0029 | 0.0019 |
| 5 | 0.0048 | 0.0029 | 0.0019 |
| 6 | 0.0048 | 0.0029 | 0.0019 |
| 7 | 0.0048 | 0.0029 | 0.0019 |
| 8 | 0.0048 | 0.0029 | 0.0019 |
| 9 | 0.0048 | 0.0029 | 0.0019 |
| 10 | 0.0048 | 0.0029 | 0.0019 |
| 11 | 0.0049 | 0.0029 | 0.0019 |
| 12 | 0.0049 | 0.0029 | 0.0019 |
| 13 | 0.0049 | 0.0030 | 0.0019 |
| 14 | 0.0049 | 0.0030 | 0.0019 |
| 15 | 0.0049 | 0.0030 | 0.0020 |
| 16 | 0.0049 | 0.0030 | 0.0020 |
| 17 | 0.0050 | 0.0030 | 0.0020 |
| 18 | 0.0050 | 0.0030 | 0.0020 |
| 19 | 0.0050 | 0.0030 | 0.0020 |
| 20 | 0.0050 | 0.0030 | 0.0020 |
| 21 | 0.0050 | 0.0030 | 0.0020 |
| 22 | 0.0050 | 0.0030 | 0.0020 |
| 23 | 0.0051 | 0.0031 | 0.0020 |
| 24 | 0.0051 | 0.0031 | 0.0020 |
| 25 | 0.0051 | 0.0031 | 0.0020 |
| 26 | 0.0051 | 0.0031 | 0.0020 |
| 27 | 0.0051 | 0.0031 | 0.0020 |
| 28 | 0.0051 | 0.0031 | 0.0020 |
| 29 | 0.0052 | 0.0031 | 0.0021 |
| 30 | 0.0052 | 0.0031 | 0.0021 |
| 31 | 0.0052 | 0.0031 | 0.0021 |
| 32 | 0.0052 | 0.0031 | 0.0021 |
| 33 | 0.0052 | 0.0032 | 0.0021 |
| 34 | 0.0053 | 0.0032 | 0.0021 |

| | | | |
|---|---|---|---|
| 35 | 0.0053 | 0.0032 | 0.0021 |
| 36 | 0.0053 | 0.0032 | 0.0021 |
| 37 | 0.0053 | 0.0032 | 0.0021 |
| 38 | 0.0053 | 0.0032 | 0.0021 |
| 39 | 0.0054 | 0.0032 | 0.0021 |
| 40 | 0.0054 | 0.0032 | 0.0021 |
| 41 | 0.0054 | 0.0033 | 0.0021 |
| 42 | 0.0054 | 0.0033 | 0.0021 |
| 43 | 0.0054 | 0.0033 | 0.0022 |
| 44 | 0.0055 | 0.0033 | 0.0022 |
| 45 | 0.0055 | 0.0033 | 0.0022 |
| 46 | 0.0055 | 0.0033 | 0.0022 |
| 47 | 0.0055 | 0.0033 | 0.0022 |
| 48 | 0.0055 | 0.0033 | 0.0022 |
| 49 | 0.0056 | 0.0034 | 0.0022 |
| 50 | 0.0056 | 0.0034 | 0.0022 |
| 51 | 0.0056 | 0.0034 | 0.0022 |
| 52 | 0.0056 | 0.0034 | 0.0022 |
| 53 | 0.0057 | 0.0034 | 0.0022 |
| 54 | 0.0057 | 0.0034 | 0.0023 |
| 55 | 0.0057 | 0.0034 | 0.0023 |
| 56 | 0.0057 | 0.0035 | 0.0023 |
| 57 | 0.0058 | 0.0035 | 0.0023 |
| 58 | 0.0058 | 0.0035 | 0.0023 |
| 59 | 0.0058 | 0.0035 | 0.0023 |
| 60 | 0.0058 | 0.0035 | 0.0023 |
| 61 | 0.0059 | 0.0035 | 0.0023 |
| 62 | 0.0059 | 0.0035 | 0.0023 |
| 63 | 0.0059 | 0.0036 | 0.0023 |
| 64 | 0.0059 | 0.0036 | 0.0024 |
| 65 | 0.0060 | 0.0036 | 0.0024 |
| 66 | 0.0060 | 0.0036 | 0.0024 |
| 67 | 0.0060 | 0.0036 | 0.0024 |
| 68 | 0.0060 | 0.0036 | 0.0024 |
| 69 | 0.0061 | 0.0037 | 0.0024 |
| 70 | 0.0061 | 0.0037 | 0.0024 |
| 71 | 0.0061 | 0.0037 | 0.0024 |
| 72 | 0.0061 | 0.0037 | 0.0024 |
| 73 | 0.0062 | 0.0037 | 0.0025 |
| 74 | 0.0062 | 0.0037 | 0.0025 |
| 75 | 0.0062 | 0.0038 | 0.0025 |
| 76 | 0.0063 | 0.0038 | 0.0025 |
| 77 | 0.0063 | 0.0038 | 0.0025 |
| 78 | 0.0063 | 0.0038 | 0.0025 |
| 79 | 0.0064 | 0.0038 | 0.0025 |
| 80 | 0.0064 | 0.0039 | 0.0025 |
| 81 | 0.0064 | 0.0039 | 0.0026 |
| 82 | 0.0065 | 0.0039 | 0.0026 |
| 83 | 0.0065 | 0.0039 | 0.0026 |
| 84 | 0.0065 | 0.0039 | 0.0026 |
| 85 | 0.0066 | 0.0040 | 0.0026 |
| 86 | 0.0066 | 0.0040 | 0.0026 |

| | | | |
|---|---|---|---|
| 87 | 0.0066 | 0.0040 | 0.0026 |
| 88 | 0.0067 | 0.0040 | 0.0026 |
| 89 | 0.0067 | 0.0041 | 0.0027 |
| 90 | 0.0067 | 0.0041 | 0.0027 |
| 91 | 0.0068 | 0.0041 | 0.0027 |
| 92 | 0.0068 | 0.0041 | 0.0027 |
| 93 | 0.0069 | 0.0041 | 0.0027 |
| 94 | 0.0069 | 0.0042 | 0.0027 |
| 95 | 0.0070 | 0.0042 | 0.0028 |
| 96 | 0.0070 | 0.0042 | 0.0028 |
| 97 | 0.0070 | 0.0042 | 0.0028 |
| 98 | 0.0071 | 0.0043 | 0.0028 |
| 99 | 0.0071 | 0.0043 | 0.0028 |
| 100 | 0.0072 | 0.0043 | 0.0028 |
| 101 | 0.0072 | 0.0044 | 0.0029 |
| 102 | 0.0072 | 0.0044 | 0.0029 |
| 103 | 0.0073 | 0.0044 | 0.0029 |
| 104 | 0.0073 | 0.0044 | 0.0029 |
| 105 | 0.0074 | 0.0045 | 0.0029 |
| 106 | 0.0074 | 0.0045 | 0.0029 |
| 107 | 0.0075 | 0.0045 | 0.0030 |
| 108 | 0.0075 | 0.0045 | 0.0030 |
| 109 | 0.0076 | 0.0046 | 0.0030 |
| 110 | 0.0076 | 0.0046 | 0.0030 |
| 111 | 0.0077 | 0.0046 | 0.0031 |
| 112 | 0.0077 | 0.0047 | 0.0031 |
| 113 | 0.0078 | 0.0047 | 0.0031 |
| 114 | 0.0079 | 0.0047 | 0.0031 |
| 115 | 0.0079 | 0.0048 | 0.0031 |
| 116 | 0.0080 | 0.0048 | 0.0032 |
| 117 | 0.0081 | 0.0049 | 0.0032 |
| 118 | 0.0081 | 0.0049 | 0.0032 |
| 119 | 0.0082 | 0.0049 | 0.0032 |
| 120 | 0.0082 | 0.0050 | 0.0033 |
| 121 | 0.0083 | 0.0050 | 0.0033 |
| 122 | 0.0084 | 0.0050 | 0.0033 |
| 123 | 0.0084 | 0.0051 | 0.0034 |
| 124 | 0.0085 | 0.0051 | 0.0034 |
| 125 | 0.0086 | 0.0052 | 0.0034 |
| 126 | 0.0086 | 0.0052 | 0.0034 |
| 127 | 0.0087 | 0.0053 | 0.0035 |
| 128 | 0.0088 | 0.0053 | 0.0035 |
| 129 | 0.0089 | 0.0054 | 0.0035 |
| 130 | 0.0089 | 0.0054 | 0.0035 |
| 131 | 0.0091 | 0.0055 | 0.0036 |
| 132 | 0.0091 | 0.0055 | 0.0036 |
| 133 | 0.0092 | 0.0056 | 0.0037 |
| 134 | 0.0093 | 0.0056 | 0.0037 |
| 135 | 0.0094 | 0.0057 | 0.0037 |
| 136 | 0.0095 | 0.0057 | 0.0038 |
| 137 | 0.0096 | 0.0058 | 0.0038 |
| 138 | 0.0097 | 0.0058 | 0.0038 |

| | | | |
|---|---|---|---|
| 139 | 0.0098 | 0.0059 | 0.0039 |
| 140 | 0.0099 | 0.0060 | 0.0039 |
| 141 | 0.0100 | 0.0060 | 0.0040 |
| 142 | 0.0101 | 0.0061 | 0.0040 |
| 143 | 0.0103 | 0.0062 | 0.0041 |
| 144 | 0.0103 | 0.0062 | 0.0041 |
| 145 | 0.0121 | 0.0073 | 0.0048 |
| 146 | 0.0122 | 0.0073 | 0.0048 |
| 147 | 0.0123 | 0.0074 | 0.0049 |
| 148 | 0.0124 | 0.0075 | 0.0049 |
| 149 | 0.0126 | 0.0076 | 0.0050 |
| 150 | 0.0127 | 0.0077 | 0.0051 |
| 151 | 0.0129 | 0.0078 | 0.0051 |
| 152 | 0.0130 | 0.0079 | 0.0052 |
| 153 | 0.0133 | 0.0080 | 0.0053 |
| 154 | 0.0134 | 0.0081 | 0.0053 |
| 155 | 0.0136 | 0.0082 | 0.0054 |
| 156 | 0.0137 | 0.0083 | 0.0055 |
| 157 | 0.0140 | 0.0084 | 0.0056 |
| 158 | 0.0141 | 0.0085 | 0.0056 |
| 159 | 0.0144 | 0.0087 | 0.0057 |
| 160 | 0.0146 | 0.0088 | 0.0058 |
| 161 | 0.0149 | 0.0090 | 0.0059 |
| 162 | 0.0150 | 0.0091 | 0.0060 |
| 163 | 0.0154 | 0.0093 | 0.0061 |
| 164 | 0.0156 | 0.0094 | 0.0062 |
| 165 | 0.0159 | 0.0096 | 0.0063 |
| 166 | 0.0161 | 0.0097 | 0.0064 |
| 167 | 0.0166 | 0.0100 | 0.0066 |
| 168 | 0.0168 | 0.0101 | 0.0067 |
| 169 | 0.0173 | 0.0104 | 0.0069 |
| 170 | 0.0175 | 0.0106 | 0.0070 |
| 171 | 0.0181 | 0.0109 | 0.0072 |
| 172 | 0.0183 | 0.0111 | 0.0073 |
| 173 | 0.0190 | 0.0114 | 0.0075 |
| 174 | 0.0193 | 0.0116 | 0.0077 |
| 175 | 0.0200 | 0.0121 | 0.0080 |
| 176 | 0.0204 | 0.0123 | 0.0081 |
| 177 | 0.0213 | 0.0128 | 0.0085 |
| 178 | 0.0218 | 0.0131 | 0.0086 |
| 179 | 0.0228 | 0.0138 | 0.0091 |
| 180 | 0.0234 | 0.0141 | 0.0093 |
| 181 | 0.0248 | 0.0149 | 0.0098 |
| 182 | 0.0255 | 0.0154 | 0.0101 |
| 183 | 0.0272 | 0.0164 | 0.0108 |
| 184 | 0.0283 | 0.0170 | 0.0112 |
| 185 | 0.0251 | 0.0151 | 0.0100 |
| 186 | 0.0265 | 0.0160 | 0.0105 |
| 187 | 0.0301 | 0.0182 | 0.0119 |
| 188 | 0.0325 | 0.0196 | 0.0129 |
| 189 | 0.0391 | 0.0236 | 0.0155 |
| 190 | 0.0441 | 0.0266 | 0.0175 |

| | | | |
|---|---|---|---|
| 191 | 0.0631 | 0.0336 | 0.0295 |
| 192 | 0.0868 | 0.0336 | 0.0531 |
| 193 | 0.2716 | 0.0336 | 0.2380 |
| 194 | 0.0514 | 0.0310 | 0.0204 |
| 195 | 0.0354 | 0.0213 | 0.0140 |
| 196 | 0.0282 | 0.0170 | 0.0112 |
| 197 | 0.0294 | 0.0177 | 0.0117 |
| 198 | 0.0263 | 0.0159 | 0.0105 |
| 199 | 0.0241 | 0.0145 | 0.0095 |
| 200 | 0.0223 | 0.0134 | 0.0088 |
| 201 | 0.0209 | 0.0126 | 0.0083 |
| 202 | 0.0197 | 0.0119 | 0.0078 |
| 203 | 0.0187 | 0.0113 | 0.0074 |
| 204 | 0.0178 | 0.0107 | 0.0071 |
| 205 | 0.0170 | 0.0103 | 0.0068 |
| 206 | 0.0163 | 0.0099 | 0.0065 |
| 207 | 0.0157 | 0.0095 | 0.0062 |
| 208 | 0.0152 | 0.0092 | 0.0060 |
| 209 | 0.0147 | 0.0089 | 0.0058 |
| 210 | 0.0143 | 0.0086 | 0.0057 |
| 211 | 0.0139 | 0.0084 | 0.0055 |
| 212 | 0.0135 | 0.0081 | 0.0054 |
| 213 | 0.0132 | 0.0079 | 0.0052 |
| 214 | 0.0128 | 0.0077 | 0.0051 |
| 215 | 0.0125 | 0.0076 | 0.0050 |
| 216 | 0.0123 | 0.0074 | 0.0049 |
| 217 | 0.0104 | 0.0063 | 0.0041 |
| 218 | 0.0102 | 0.0061 | 0.0040 |
| 219 | 0.0099 | 0.0060 | 0.0039 |
| 220 | 0.0097 | 0.0059 | 0.0039 |
| 221 | 0.0095 | 0.0058 | 0.0038 |
| 222 | 0.0093 | 0.0056 | 0.0037 |
| 223 | 0.0092 | 0.0055 | 0.0036 |
| 224 | 0.0090 | 0.0054 | 0.0036 |
| 225 | 0.0088 | 0.0053 | 0.0035 |
| 226 | 0.0087 | 0.0052 | 0.0034 |
| 227 | 0.0085 | 0.0051 | 0.0034 |
| 228 | 0.0084 | 0.0051 | 0.0033 |
| 229 | 0.0083 | 0.0050 | 0.0033 |
| 230 | 0.0081 | 0.0049 | 0.0032 |
| 231 | 0.0080 | 0.0048 | 0.0032 |
| 232 | 0.0079 | 0.0048 | 0.0031 |
| 233 | 0.0078 | 0.0047 | 0.0031 |
| 234 | 0.0077 | 0.0046 | 0.0030 |
| 235 | 0.0076 | 0.0046 | 0.0030 |
| 236 | 0.0075 | 0.0045 | 0.0030 |
| 237 | 0.0074 | 0.0044 | 0.0029 |
| 238 | 0.0073 | 0.0044 | 0.0029 |
| 239 | 0.0072 | 0.0043 | 0.0029 |
| 240 | 0.0071 | 0.0043 | 0.0028 |
| 241 | 0.0070 | 0.0042 | 0.0028 |
| 242 | 0.0069 | 0.0042 | 0.0027 |

| | | | |
|---|---|---|---|
| 243 | 0.0068 | 0.0041 | 0.0027 |
| 244 | 0.0068 | 0.0041 | 0.0027 |
| 245 | 0.0067 | 0.0040 | 0.0027 |
| 246 | 0.0066 | 0.0040 | 0.0026 |
| 247 | 0.0066 | 0.0040 | 0.0026 |
| 248 | 0.0065 | 0.0039 | 0.0026 |
| 249 | 0.0064 | 0.0039 | 0.0025 |
| 250 | 0.0064 | 0.0038 | 0.0025 |
| 251 | 0.0063 | 0.0038 | 0.0025 |
| 252 | 0.0062 | 0.0038 | 0.0025 |
| 253 | 0.0062 | 0.0037 | 0.0024 |
| 254 | 0.0061 | 0.0037 | 0.0024 |
| 255 | 0.0061 | 0.0037 | 0.0024 |
| 256 | 0.0060 | 0.0036 | 0.0024 |
| 257 | 0.0059 | 0.0036 | 0.0024 |
| 258 | 0.0059 | 0.0036 | 0.0023 |
| 259 | 0.0058 | 0.0035 | 0.0023 |
| 260 | 0.0058 | 0.0035 | 0.0023 |
| 261 | 0.0057 | 0.0035 | 0.0023 |
| 262 | 0.0057 | 0.0034 | 0.0023 |
| 263 | 0.0056 | 0.0034 | 0.0022 |
| 264 | 0.0056 | 0.0034 | 0.0022 |
| 265 | 0.0056 | 0.0034 | 0.0022 |
| 266 | 0.0055 | 0.0033 | 0.0022 |
| 267 | 0.0055 | 0.0033 | 0.0022 |
| 268 | 0.0054 | 0.0033 | 0.0022 |
| 269 | 0.0054 | 0.0032 | 0.0021 |
| 270 | 0.0053 | 0.0032 | 0.0021 |
| 271 | 0.0053 | 0.0032 | 0.0021 |
| 272 | 0.0053 | 0.0032 | 0.0021 |
| 273 | 0.0052 | 0.0032 | 0.0021 |
| 274 | 0.0052 | 0.0031 | 0.0021 |
| 275 | 0.0052 | 0.0031 | 0.0020 |
| 276 | 0.0051 | 0.0031 | 0.0020 |
| 277 | 0.0051 | 0.0031 | 0.0020 |
| 278 | 0.0051 | 0.0030 | 0.0020 |
| 279 | 0.0050 | 0.0030 | 0.0020 |
| 280 | 0.0050 | 0.0030 | 0.0020 |
| 281 | 0.0050 | 0.0030 | 0.0020 |
| 282 | 0.0049 | 0.0030 | 0.0020 |
| 283 | 0.0049 | 0.0029 | 0.0019 |
| 284 | 0.0049 | 0.0029 | 0.0019 |
| 285 | 0.0048 | 0.0029 | 0.0019 |
| 286 | 0.0048 | 0.0029 | 0.0019 |
| 287 | 0.0048 | 0.0029 | 0.0019 |
| 288 | 0.0047 | 0.0029 | 0.0019 |

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Total soil rain loss = 1.77(In)
Total effective rainfall = 1.42(In)
Peak flow rate in flood hydrograph = 4.88(CFS)

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24 - H O U R  S T O R M

R u n o f f  H y d r o g r a p h

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Hydrograph in 5 Minute intervals ((CFS))

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| Time(h+m) | Volume Ac.Ft | Q(CFS) | 0 | 2.5 | 5.0 | 7.5 | 10.0 |
|---|---|---|---|---|---|---|---|
| 0+ 5 | 0.0000 | 0.00 | Q | | | | |
| 0+10 | 0.0002 | 0.02 | Q | | | | |
| 0+15 | 0.0005 | 0.05 | Q | | | | |
| 0+20 | 0.0010 | 0.07 | Q | | | | |
| 0+25 | 0.0016 | 0.09 | Q | | | | |
| 0+30 | 0.0023 | 0.10 | Q | | | | |
| 0+35 | 0.0030 | 0.10 | Q | | | | |
| 0+40 | 0.0037 | 0.11 | Q | | | | |
| 0+45 | 0.0045 | 0.11 | Q | | | | |
| 0+50 | 0.0052 | 0.11 | Q | | | | |
| 0+55 | 0.0060 | 0.12 | Q | | | | |
| 1+ 0 | 0.0068 | 0.12 | Q | | | | |
| 1+ 5 | 0.0077 | 0.12 | Q | | | | |
| 1+10 | 0.0085 | 0.12 | Q | | | | |
| 1+15 | 0.0094 | 0.12 | Q | | | | |
| 1+20 | 0.0102 | 0.13 | Q | | | | |
| 1+25 | 0.0111 | 0.13 | Q | | | | |
| 1+30 | 0.0120 | 0.13 | Q | | | | |
| 1+35 | 0.0129 | 0.13 | Q | | | | |
| 1+40 | 0.0138 | 0.13 | Q | | | | |
| 1+45 | 0.0147 | 0.13 | Q | | | | |
| 1+50 | 0.0156 | 0.13 | Q | | | | |
| 1+55 | 0.0165 | 0.13 | QV | | | | |
| 2+ 0 | 0.0174 | 0.13 | QV | | | | |
| 2+ 5 | 0.0183 | 0.13 | QV | | | | |
| 2+10 | 0.0192 | 0.13 | QV | | | | |
| 2+15 | 0.0202 | 0.13 | QV | | | | |
| 2+20 | 0.0211 | 0.14 | QV | | | | |
| 2+25 | 0.0220 | 0.14 | QV | | | | |
| 2+30 | 0.0230 | 0.14 | QV | | | | |
| 2+35 | 0.0239 | 0.14 | QV | | | | |
| 2+40 | 0.0248 | 0.14 | QV | | | | |
| 2+45 | 0.0258 | 0.14 | QV | | | | |
| 2+50 | 0.0267 | 0.14 | QV | | | | |
| 2+55 | 0.0277 | 0.14 | QV | | | | |
| 3+ 0 | 0.0286 | 0.14 | QV | | | | |
| 3+ 5 | 0.0296 | 0.14 | QV | | | | |
| 3+10 | 0.0306 | 0.14 | QV | | | | |
| 3+15 | 0.0315 | 0.14 | QV | | | | |
| 3+20 | 0.0325 | 0.14 | QV | | | | |
| 3+25 | 0.0335 | 0.14 | Q V | | | | |
| 3+30 | 0.0345 | 0.14 | Q V | | | | |
| 3+35 | 0.0354 | 0.14 | Q V | | | | |

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 3+40 | 0.0364 | 0.14 | Q V | \| | \| | \| | \| |
| 3+45 | 0.0374 | 0.14 | Q V | \| | \| | \| | \| |
| 3+50 | 0.0384 | 0.14 | Q V | \| | \| | \| | \| |
| 3+55 | 0.0394 | 0.14 | Q V | \| | \| | \| | \| |
| 4+ 0 | 0.0404 | 0.15 | Q V | \| | \| | \| | \| |
| 4+ 5 | 0.0414 | 0.15 | Q V | \| | \| | \| | \| |
| 4+10 | 0.0424 | 0.15 | Q V | \| | \| | \| | \| |
| 4+15 | 0.0434 | 0.15 | Q V | \| | \| | \| | \| |
| 4+20 | 0.0444 | 0.15 | Q V | \| | \| | \| | \| |
| 4+25 | 0.0455 | 0.15 | Q V | \| | \| | \| | \| |
| 4+30 | 0.0465 | 0.15 | Q V | \| | \| | \| | \| |
| 4+35 | 0.0475 | 0.15 | Q V | \| | \| | \| | \| |
| 4+40 | 0.0485 | 0.15 | Q V | \| | \| | \| | \| |
| 4+45 | 0.0496 | 0.15 | Q V | \| | \| | \| | \| |
| 4+50 | 0.0506 | 0.15 | Q V | \| | \| | \| | \| |
| 4+55 | 0.0517 | 0.15 | Q V | \| | \| | \| | \| |
| 5+ 0 | 0.0527 | 0.15 | Q V | \| | \| | \| | \| |
| 5+ 5 | 0.0538 | 0.15 | Q V | \| | \| | \| | \| |
| 5+10 | 0.0548 | 0.15 | Q V | \| | \| | \| | \| |
| 5+15 | 0.0559 | 0.15 | Q V | \| | \| | \| | \| |
| 5+20 | 0.0570 | 0.15 | Q V | \| | \| | \| | \| |
| 5+25 | 0.0580 | 0.16 | Q V | \| | \| | \| | \| |
| 5+30 | 0.0591 | 0.16 | Q V | \| | \| | \| | \| |
| 5+35 | 0.0602 | 0.16 | Q V | \| | \| | \| | \| |
| 5+40 | 0.0613 | 0.16 | Q V | \| | \| | \| | \| |
| 5+45 | 0.0624 | 0.16 | Q V | \| | \| | \| | \| |
| 5+50 | 0.0635 | 0.16 | Q V | \| | \| | \| | \| |
| 5+55 | 0.0646 | 0.16 | Q V | \| | \| | \| | \| |
| 6+ 0 | 0.0657 | 0.16 | Q V | \| | \| | \| | \| |
| 6+ 5 | 0.0668 | 0.16 | Q V | \| | \| | \| | \| |
| 6+10 | 0.0679 | 0.16 | Q V | \| | \| | \| | \| |
| 6+15 | 0.0690 | 0.16 | Q V | \| | \| | \| | \| |
| 6+20 | 0.0701 | 0.16 | Q V | \| | \| | \| | \| |
| 6+25 | 0.0713 | 0.16 | Q V | \| | \| | \| | \| |
| 6+30 | 0.0724 | 0.17 | Q V | \| | \| | \| | \| |
| 6+35 | 0.0736 | 0.17 | Q V | \| | \| | \| | \| |
| 6+40 | 0.0747 | 0.17 | Q V | \| | \| | \| | \| |
| 6+45 | 0.0759 | 0.17 | Q V | \| | \| | \| | \| |
| 6+50 | 0.0770 | 0.17 | Q V | \| | \| | \| | \| |
| 6+55 | 0.0782 | 0.17 | Q V | \| | \| | \| | \| |
| 7+ 0 | 0.0794 | 0.17 | Q V | \| | \| | \| | \| |
| 7+ 5 | 0.0805 | 0.17 | Q V | \| | \| | \| | \| |
| 7+10 | 0.0817 | 0.17 | Q V | \| | \| | \| | \| |
| 7+15 | 0.0829 | 0.17 | Q V | \| | \| | \| | \| |
| 7+20 | 0.0841 | 0.17 | Q V | \| | \| | \| | \| |
| 7+25 | 0.0853 | 0.17 | Q V | \| | \| | \| | \| |
| 7+30 | 0.0865 | 0.18 | Q V | \| | \| | \| | \| |
| 7+35 | 0.0877 | 0.18 | Q V | \| | \| | \| | \| |
| 7+40 | 0.0890 | 0.18 | Q V | \| | \| | \| | \| |
| 7+45 | 0.0902 | 0.18 | Q V | \| | \| | \| | \| |
| 7+50 | 0.0914 | 0.18 | Q V | \| | \| | \| | \| |
| 7+55 | 0.0927 | 0.18 | Q V | \| | \| | \| | \| |

```
 8+ 0       0.0939      0.18  Q    V    |          |          |          |
 8+ 5       0.0952      0.18  Q    V    |          |          |          |
 8+10       0.0964      0.18  Q    V    |          |          |          |
 8+15       0.0977      0.18  Q    V    |          |          |          |
 8+20       0.0990      0.19  Q     V   |          |          |          |
 8+25       0.1003      0.19  Q     V   |          |          |          |
 8+30       0.1016      0.19  Q     V   |          |          |          |
 8+35       0.1029      0.19  Q     V   |          |          |          |
 8+40       0.1042      0.19  Q     V   |          |          |          |
 8+45       0.1055      0.19  Q     V   |          |          |          |
 8+50       0.1068      0.19  Q     V   |          |          |          |
 8+55       0.1082      0.19  Q     V   |          |          |          |
 9+ 0       0.1095      0.20  Q     V   |          |          |          |
 9+ 5       0.1109      0.20  Q     V   |          |          |          |
 9+10       0.1122      0.20  Q     V   |          |          |          |
 9+15       0.1136      0.20  Q     V   |          |          |          |
 9+20       0.1150      0.20  Q      V  |          |          |          |
 9+25       0.1164      0.20  Q      V  |          |          |          |
 9+30       0.1178      0.20  Q      V  |          |          |          |
 9+35       0.1192      0.20  Q      V  |          |          |          |
 9+40       0.1206      0.21  Q      V  |          |          |          |
 9+45       0.1220      0.21  Q      V  |          |          |          |
 9+50       0.1235      0.21  Q      V  |          |          |          |
 9+55       0.1249      0.21  Q      V  |          |          |          |
10+ 0       0.1264      0.21  Q      V  |          |          |          |
10+ 5       0.1278      0.21  Q      V  |          |          |          |
10+10       0.1293      0.22  Q      V  |          |          |          |
10+15       0.1308      0.22  Q      V  |          |          |          |
10+20       0.1323      0.22  Q       V |          |          |          |
10+25       0.1338      0.22  Q       V |          |          |          |
10+30       0.1354      0.22  Q       V |          |          |          |
10+35       0.1369      0.22  Q       V |          |          |          |
10+40       0.1385      0.23  Q       V |          |          |          |
10+45       0.1400      0.23  Q       V |          |          |          |
10+50       0.1416      0.23  Q       V |          |          |          |
10+55       0.1432      0.23  Q       V |          |          |          |
11+ 0       0.1448      0.23  Q       V |          |          |          |
11+ 5       0.1464      0.24  Q       V |          |          |          |
11+10       0.1481      0.24  Q        V|          |          |          |
11+15       0.1497      0.24  Q        V|          |          |          |
11+20       0.1514      0.24  Q        V|          |          |          |
11+25       0.1531      0.24  Q        V|          |          |          |
11+30       0.1548      0.25  Q        V|          |          |          |
11+35       0.1565      0.25  Q        V|          |          |          |
11+40       0.1582      0.25  |Q       V|          |          |          |
11+45       0.1600      0.25  |Q       V|          |          |          |
11+50       0.1618      0.26  |Q       V|          |          |          |
11+55       0.1636      0.26  |Q       V|          |          |          |
12+ 0       0.1654      0.26  |Q        V          |          |          |
12+ 5       0.1672      0.27  |Q        V          |          |          |
12+10       0.1691      0.28  |Q        V          |          |          |
12+15       0.1711      0.29  |Q        V          |          |          |
```

```
12+20       0.1731      0.30  |Q        V         |         |         |
12+25       0.1753      0.31  |Q        V         |         |         |
12+30       0.1774      0.31  |Q        V         |         |         |
12+35       0.1796      0.32  |Q        V         |         |         |
12+40       0.1818      0.32  |Q        |V        |         |         |
12+45       0.1841      0.33  |Q        |V        |         |         |
12+50       0.1864      0.33  |Q        |V        |         |         |
12+55       0.1887      0.34  |Q        |V        |         |         |
13+ 0       0.1911      0.34  |Q        |V        |         |         |
13+ 5       0.1935      0.35  |Q        |V        |         |         |
13+10       0.1959      0.35  |Q        |V        |         |         |
13+15       0.1984      0.36  |Q        | V       |         |         |
13+20       0.2009      0.36  |Q        | V       |         |         |
13+25       0.2035      0.37  |Q        | V       |         |         |
13+30       0.2061      0.38  |Q        | V       |         |         |
13+35       0.2087      0.38  |Q        | V       |         |         |
13+40       0.2114      0.39  |Q        | V       |         |         |
13+45       0.2141      0.39  |Q        |  V      |         |         |
13+50       0.2168      0.40  |Q        |  V      |         |         |
13+55       0.2196      0.41  |Q        |  V      |         |         |
14+ 0       0.2225      0.41  |Q        |  V      |         |         |
14+ 5       0.2254      0.42  |Q        |  V      |         |         |
14+10       0.2284      0.43  |Q        |  V      |         |         |
14+15       0.2314      0.44  |Q        |   V     |         |         |
14+20       0.2345      0.45  |Q        |   V     |         |         |
14+25       0.2376      0.46  |Q        |   V     |         |         |
14+30       0.2408      0.47  |Q        |   V     |         |         |
14+35       0.2441      0.48  |Q        |   V     |         |         |
14+40       0.2475      0.49  |Q        |    V    |         |         |
14+45       0.2510      0.50  | Q       |    V    |         |         |
14+50       0.2545      0.52  | Q       |    V    |         |         |
14+55       0.2582      0.53  | Q       |    V    |         |         |
15+ 0       0.2620      0.55  | Q       |    V    |         |         |
15+ 5       0.2659      0.57  | Q       |     V   |         |         |
15+10       0.2699      0.59  | Q       |     V   |         |         |
15+15       0.2741      0.61  | Q       |     V   |         |         |
15+20       0.2785      0.63  | Q       |     V   |         |         |
15+25       0.2830      0.66  | Q       |      V  |         |         |
15+30       0.2876      0.67  | Q       |      V  |         |         |
15+35       0.2923      0.68  | Q       |      V  |         |         |
15+40       0.2970      0.69  | Q       |       V |         |         |
15+45       0.3021      0.73  | Q       |       V |         |         |
15+50       0.3076      0.80  |  Q      |       V |         |         |
15+55       0.3139      0.91  |  Q      |        V|         |         |
16+ 0       0.3218      1.15  |   Q     |        V|         |         |
16+ 5       0.3355      2.00  |      Q  |         V         |         |
16+10       0.3606      3.64  |         |   Q     |V        |         |
16+15       0.3942      4.88  |         |        Q|   V     |         |
16+20       0.4244      4.38  |         |      Q  |    V    |         |
16+25       0.4441      2.86  |         |Q        |      V  |         |
16+30       0.4579      2.00  |       Q |         |      V  |         |
16+35       0.4692      1.63  |     Q   |         |       V |         |
```

```
16+40       0.4789      1.41  |    Q    |         |        V|         |
16+45       0.4875      1.25  |   Q     |         |        V|         |
16+50       0.4951      1.10  |   Q     |         |         V         |
16+55       0.5020      1.00  |   Q     |         |         V         |
17+ 0       0.5082      0.90  |  Q      |         |         V         |
17+ 5       0.5138      0.82  |  Q      |         |         |V        |
17+10       0.5191      0.76  |  Q      |         |         |V        |
17+15       0.5240      0.72  | Q       |         |         |V        |
17+20       0.5286      0.67  | Q       |         |         | V       |
17+25       0.5329      0.62  | Q       |         |         | V       |
17+30       0.5369      0.58  | Q       |         |         | V       |
17+35       0.5407      0.55  | Q       |         |         | V       |
17+40       0.5443      0.52  | Q       |         |         |  V      |
17+45       0.5476      0.49  |Q        |         |         |  V      |
17+50       0.5508      0.47  |Q        |         |         |  V      |
17+55       0.5540      0.45  |Q        |         |         |  V      |
18+ 0       0.5570      0.44  |Q        |         |         |  V      |
18+ 5       0.5597      0.39  |Q        |         |         |   V     |
18+10       0.5621      0.35  |Q        |         |         |   V     |
18+15       0.5644      0.33  |Q        |         |         |   V     |
18+20       0.5665      0.31  |Q        |         |         |   V     |
18+25       0.5686      0.30  |Q        |         |         |   V     |
18+30       0.5706      0.29  |Q        |         |         |   V     |
18+35       0.5726      0.28  |Q        |         |         |   V     |
18+40       0.5744      0.27  |Q        |         |         |    V    |
18+45       0.5763      0.27  |Q        |         |         |    V    |
18+50       0.5781      0.26  |Q        |         |         |    V    |
18+55       0.5798      0.25  |Q        |         |         |    V    |
19+ 0       0.5815      0.25  Q         |         |         |    V    |
19+ 5       0.5832      0.24  Q         |         |         |    V    |
19+10       0.5849      0.24  Q         |         |         |    V    |
19+15       0.5865      0.23  Q         |         |         |    V    |
19+20       0.5880      0.23  Q         |         |         |    V    |
19+25       0.5896      0.23  Q         |         |         |    V    |
19+30       0.5911      0.22  Q         |         |         |     V   |
19+35       0.5926      0.22  Q         |         |         |     V   |
19+40       0.5941      0.21  Q         |         |         |     V   |
19+45       0.5955      0.21  Q         |         |         |     V   |
19+50       0.5970      0.21  Q         |         |         |     V   |
19+55       0.5984      0.20  Q         |         |         |     V   |
20+ 0       0.5998      0.20  Q         |         |         |     V   |
20+ 5       0.6011      0.20  Q         |         |         |     V   |
20+10       0.6025      0.20  Q         |         |         |     V   |
20+15       0.6038      0.19  Q         |         |         |     V   |
20+20       0.6051      0.19  Q         |         |         |     V   |
20+25       0.6064      0.19  Q         |         |         |     V   |
20+30       0.6077      0.19  Q         |         |         |      V  |
20+35       0.6090      0.18  Q         |         |         |      V  |
20+40       0.6102      0.18  Q         |         |         |      V  |
20+45       0.6115      0.18  Q         |         |         |      V  |
20+50       0.6127      0.18  Q         |         |         |      V  |
20+55       0.6139      0.18  Q         |         |         |      V  |
```

```
21+ 0       0.6151      0.17  Q         |          |          |      V  |
21+ 5       0.6163      0.17  Q         |          |          |      V  |
21+10       0.6175      0.17  Q         |          |          |      V  |
21+15       0.6186      0.17  Q         |          |          |      V  |
21+20       0.6198      0.17  Q         |          |          |      V  |
21+25       0.6209      0.17  Q         |          |          |      V  |
21+30       0.6221      0.16  Q         |          |          |      V  |
21+35       0.6232      0.16  Q         |          |          |       V |
21+40       0.6243      0.16  Q         |          |          |       V |
21+45       0.6254      0.16  Q         |          |          |       V |
21+50       0.6265      0.16  Q         |          |          |       V |
21+55       0.6276      0.16  Q         |          |          |       V |
22+ 0       0.6286      0.16  Q         |          |          |       V |
22+ 5       0.6297      0.15  Q         |          |          |       V |
22+10       0.6307      0.15  Q         |          |          |       V |
22+15       0.6318      0.15  Q         |          |          |       V |
22+20       0.6328      0.15  Q         |          |          |       V |
22+25       0.6338      0.15  Q         |          |          |       V |
22+30       0.6349      0.15  Q         |          |          |       V |
22+35       0.6359      0.15  Q         |          |          |       V |
22+40       0.6369      0.15  Q         |          |          |       V |
22+45       0.6379      0.14  Q         |          |          |       V |
22+50       0.6388      0.14  Q         |          |          |       V |
22+55       0.6398      0.14  Q         |          |          |        V|
23+ 0       0.6408      0.14  Q         |          |          |        V|
23+ 5       0.6418      0.14  Q         |          |          |        V|
23+10       0.6427      0.14  Q         |          |          |        V|
23+15       0.6437      0.14  Q         |          |          |        V|
23+20       0.6446      0.14  Q         |          |          |        V|
23+25       0.6456      0.14  Q         |          |          |        V|
23+30       0.6465      0.14  Q         |          |          |        V|
23+35       0.6474      0.13  Q         |          |          |        V|
23+40       0.6483      0.13  Q         |          |          |        V|
23+45       0.6492      0.13  Q         |          |          |        V|
23+50       0.6502      0.13  Q         |          |          |        V|
23+55       0.6511      0.13  Q         |          |          |        V|
24+ 0       0.6519      0.13  Q         |          |          |        V|
24+ 5       0.6528      0.12  Q         |          |          |        V|
24+10       0.6536      0.11  Q         |          |          |        V|
24+15       0.6541      0.08  Q         |          |          |        V|
24+20       0.6545      0.05  Q         |          |          |        V|
24+25       0.6548      0.04  Q         |          |          |        V|
24+30       0.6550      0.03  Q         |          |          |        V|
24+35       0.6552      0.03  Q         |          |          |        V|
24+40       0.6553      0.02  Q         |          |          |        V|
24+45       0.6554      0.02  Q         |          |          |        V|
24+50       0.6555      0.01  Q         |          |          |        V|
24+55       0.6556      0.01  Q         |          |          |        V|
25+ 0       0.6557      0.01  Q         |          |          |        V|
25+ 5       0.6557      0.01  Q         |          |          |        V|
25+10       0.6558      0.01  Q         |          |          |        V|
25+15       0.6558      0.01  Q         |          |          |        V|
```

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 25+20 | 0.6559 | 0.00 | Q | \| | \| | \| | V\| |
| 25+25 | 0.6559 | 0.00 | Q | \| | \| | \| | V\| |
| 25+30 | 0.6559 | 0.00 | Q | \| | \| | \| | V\| |
| 25+35 | 0.6559 | 0.00 | Q | \| | \| | \| | V\| |
| 25+40 | 0.6560 | 0.00 | Q | \| | \| | \| | V\| |
| 25+45 | 0.6560 | 0.00 | Q | \| | \| | \| | V\| |
| 25+50 | 0.6560 | 0.00 | Q | \| | \| | \| | V\| |
| 25+55 | 0.6560 | 0.00 | Q | \| | \| | \| | V\| |
| 26+ 0 | 0.6560 | 0.00 | Q | \| | \| | \| | V\| |

# C.2 – EXISTING 25-YEAR ANALYSIS

U n i t  H y d r o g r a p h  A n a l y s i s



Study date 04/19/24

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San Bernardino County Synthetic Unit Hydrology Method
Manual date - August 1986

Program License Serial Number 6568

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TPM 20854
EXISTING UNIT HYDROGRAPH
25-YEAR
24-HOUR

---

Storm Event Year = 25

Antecedent Moisture Condition = 2

English (in-lb) Input Units Used

English Rainfall Data (Inches) Input Values Used

English Units used in output format

Area averaged rainfall intensity isohyetal data:

| Sub-Area (Ac.) | Duration (hours) | Isohyetal (In) |
|---|---|---|
| Rainfall data for year 10 | | |
| 5.55 | 1 | 0.73 |
| Rainfall data for year 2 | | |
| 5.55 | 6 | 1.15 |
| Rainfall data for year 2 | | |
| 5.55 | 24 | 2.05 |
| Rainfall data for year 100 | | |
| 5.55 | 1 | 1.16 |

---

```
Rainfall data for year 100
             5.55            6            2.65
------------------------------------------------------------------------
Rainfall data for year 100
             5.55           24            4.82
------------------------------------------------------------------------
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++

******** Area-averaged max loss rate, Fm ********


SCS curve  SCS curve     Area      Area     Fp(Fig C6)    Ap      Fm
No.(AMCII) NO.(AMC 2)    (Ac.)    Fraction     (In/Hr)  (dec.)   (In/Hr)
 78.0      78.0          5.55      1.000     0.404    1.000    0.404

Area-averaged adjusted loss rate Fm (In/Hr) =  0.404

********* Area-Averaged low loss rate fraction, Yb **********

Area       Area          SCS CN    SCS CN      S     Pervious
 (Ac.)      Fract         (AMC2)    (AMC2)           Yield Fr
     5.55   1.000         78.0      78.0       2.82     0.458

Area-averaged catchment yield fraction, Y =  0.458
Area-averaged low loss fraction, Yb =  0.542
User entry of time of concentration  =   0.313 (hours)
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Watershed area =       5.55(Ac.)
Catchment Lag time =   0.250 hours
Unit interval =   5.000 minutes
Unit interval percentage of lag time = 33.3014
Hydrograph baseflow =     0.00(CFS)
Average maximum watershed loss rate(Fm) =  0.404(In/Hr)
Average low loss rate fraction (Yb) = 0.542 (decimal)
VALLEY UNDEVELOPED S-Graph Selected
Computed peak 5-minute rainfall =  0.334(In)
Computed peak 30-minute rainfall =  0.685(In)
Specified peak 1-hour rainfall =  0.904(In)
Computed peak 3-hour rainfall =  1.524(In)
Specified peak 6-hour rainfall =  2.118(In)
Specified peak 24-hour rainfall =  3.838(In)


Rainfall depth area reduction factors:
Using a total area of       5.55(Ac.) (Ref: fig. E-4)

5-minute factor = 1.000     Adjusted rainfall =  0.334(In)
30-minute factor = 1.000    Adjusted rainfall =  0.685(In)
1-hour factor = 1.000       Adjusted rainfall =  0.903(In)
3-hour factor = 1.000       Adjusted rainfall =  1.523(In)
6-hour factor = 1.000       Adjusted rainfall =  2.118(In)
24-hour factor = 1.000      Adjusted rainfall =  3.838(In)
```

---

U n i t  H y d r o g r a p h

| Interval Number | 'S' Graph Mean values | Unit Hydrograph ((CFS)) |
|---|---|---|
| | (K = 67.12 (CFS)) | |
| 1 | 3.346 | 2.246 |
| 2 | 16.202 | 8.629 |
| 3 | 37.964 | 14.606 |
| 4 | 58.047 | 13.480 |
| 5 | 69.166 | 7.463 |
| 6 | 75.483 | 4.240 |
| 7 | 79.955 | 3.001 |
| 8 | 83.427 | 2.331 |
| 9 | 86.263 | 1.903 |
| 10 | 88.482 | 1.489 |
| 11 | 90.416 | 1.298 |
| 12 | 91.950 | 1.030 |
| 13 | 93.221 | 0.852 |
| 14 | 94.278 | 0.710 |
| 15 | 95.286 | 0.676 |
| 16 | 96.156 | 0.584 |
| 17 | 96.873 | 0.481 |
| 18 | 97.490 | 0.414 |
| 19 | 98.025 | 0.359 |
| 20 | 98.476 | 0.303 |
| 21 | 98.827 | 0.236 |
| 22 | 99.160 | 0.224 |
| 23 | 99.493 | 0.224 |
| 24 | 99.826 | 0.224 |
| 25 | 100.000 | 0.117 |

| Peak Unit Number | Adjusted mass rainfall (In) | Unit rainfall (In) |
|---|---|---|
| 1 | 0.3343 | 0.3343 |
| 2 | 0.4411 | 0.1068 |
| 3 | 0.5188 | 0.0777 |
| 4 | 0.5821 | 0.0633 |
| 5 | 0.6364 | 0.0543 |
| 6 | 0.6846 | 0.0481 |
| 7 | 0.7281 | 0.0435 |
| 8 | 0.7680 | 0.0399 |
| 9 | 0.8051 | 0.0371 |
| 10 | 0.8398 | 0.0347 |
| 11 | 0.8724 | 0.0326 |
| 12 | 0.9033 | 0.0309 |
| 13 | 0.9384 | 0.0351 |
| 14 | 0.9720 | 0.0337 |
| 15 | 1.0045 | 0.0324 |

| | | |
|---|---|---|
| 16 | 1.0358 | 0.0313 |
| 17 | 1.0661 | 0.0303 |
| 18 | 1.0955 | 0.0294 |
| 19 | 1.1240 | 0.0285 |
| 20 | 1.1518 | 0.0278 |
| 21 | 1.1789 | 0.0271 |
| 22 | 1.2052 | 0.0264 |
| 23 | 1.2310 | 0.0258 |
| 24 | 1.2562 | 0.0252 |
| 25 | 1.2808 | 0.0246 |
| 26 | 1.3050 | 0.0241 |
| 27 | 1.3286 | 0.0236 |
| 28 | 1.3518 | 0.0232 |
| 29 | 1.3745 | 0.0228 |
| 30 | 1.3969 | 0.0224 |
| 31 | 1.4189 | 0.0220 |
| 32 | 1.4405 | 0.0216 |
| 33 | 1.4617 | 0.0212 |
| 34 | 1.4826 | 0.0209 |
| 35 | 1.5032 | 0.0206 |
| 36 | 1.5235 | 0.0203 |
| 37 | 1.5435 | 0.0200 |
| 38 | 1.5632 | 0.0197 |
| 39 | 1.5826 | 0.0194 |
| 40 | 1.6018 | 0.0192 |
| 41 | 1.6207 | 0.0189 |
| 42 | 1.6394 | 0.0187 |
| 43 | 1.6578 | 0.0184 |
| 44 | 1.6761 | 0.0182 |
| 45 | 1.6941 | 0.0180 |
| 46 | 1.7119 | 0.0178 |
| 47 | 1.7295 | 0.0176 |
| 48 | 1.7469 | 0.0174 |
| 49 | 1.7641 | 0.0172 |
| 50 | 1.7811 | 0.0170 |
| 51 | 1.7980 | 0.0169 |
| 52 | 1.8146 | 0.0167 |
| 53 | 1.8312 | 0.0165 |
| 54 | 1.8475 | 0.0164 |
| 55 | 1.8637 | 0.0162 |
| 56 | 1.8798 | 0.0160 |
| 57 | 1.8956 | 0.0159 |
| 58 | 1.9114 | 0.0157 |
| 59 | 1.9270 | 0.0156 |
| 60 | 1.9425 | 0.0155 |
| 61 | 1.9578 | 0.0153 |
| 62 | 1.9730 | 0.0152 |
| 63 | 1.9881 | 0.0151 |
| 64 | 2.0030 | 0.0149 |
| 65 | 2.0178 | 0.0148 |
| 66 | 2.0325 | 0.0147 |
| 67 | 2.0471 | 0.0146 |

| | | |
|---|---|---|
| 68 | 2.0616 | 0.0145 |
| 69 | 2.0760 | 0.0144 |
| 70 | 2.0902 | 0.0143 |
| 71 | 2.1044 | 0.0141 |
| 72 | 2.1184 | 0.0140 |
| 73 | 2.1310 | 0.0126 |
| 74 | 2.1434 | 0.0125 |
| 75 | 2.1558 | 0.0124 |
| 76 | 2.1681 | 0.0123 |
| 77 | 2.1803 | 0.0122 |
| 78 | 2.1924 | 0.0121 |
| 79 | 2.2044 | 0.0120 |
| 80 | 2.2163 | 0.0119 |
| 81 | 2.2281 | 0.0118 |
| 82 | 2.2399 | 0.0118 |
| 83 | 2.2516 | 0.0117 |
| 84 | 2.2632 | 0.0116 |
| 85 | 2.2747 | 0.0115 |
| 86 | 2.2861 | 0.0114 |
| 87 | 2.2975 | 0.0114 |
| 88 | 2.3087 | 0.0113 |
| 89 | 2.3200 | 0.0112 |
| 90 | 2.3311 | 0.0111 |
| 91 | 2.3422 | 0.0111 |
| 92 | 2.3532 | 0.0110 |
| 93 | 2.3641 | 0.0109 |
| 94 | 2.3750 | 0.0109 |
| 95 | 2.3858 | 0.0108 |
| 96 | 2.3965 | 0.0107 |
| 97 | 2.4072 | 0.0107 |
| 98 | 2.4178 | 0.0106 |
| 99 | 2.4283 | 0.0105 |
| 100 | 2.4388 | 0.0105 |
| 101 | 2.4492 | 0.0104 |
| 102 | 2.4596 | 0.0104 |
| 103 | 2.4699 | 0.0103 |
| 104 | 2.4802 | 0.0103 |
| 105 | 2.4904 | 0.0102 |
| 106 | 2.5005 | 0.0101 |
| 107 | 2.5106 | 0.0101 |
| 108 | 2.5206 | 0.0100 |
| 109 | 2.5306 | 0.0100 |
| 110 | 2.5405 | 0.0099 |
| 111 | 2.5504 | 0.0099 |
| 112 | 2.5603 | 0.0098 |
| 113 | 2.5700 | 0.0098 |
| 114 | 2.5798 | 0.0097 |
| 115 | 2.5894 | 0.0097 |
| 116 | 2.5991 | 0.0096 |
| 117 | 2.6086 | 0.0096 |
| 118 | 2.6182 | 0.0095 |
| 119 | 2.6277 | 0.0095 |

| | | |
|---|---|---|
| 120 | 2.6371 | 0.0094 |
| 121 | 2.6465 | 0.0094 |
| 122 | 2.6559 | 0.0094 |
| 123 | 2.6652 | 0.0093 |
| 124 | 2.6745 | 0.0093 |
| 125 | 2.6837 | 0.0092 |
| 126 | 2.6929 | 0.0092 |
| 127 | 2.7020 | 0.0091 |
| 128 | 2.7111 | 0.0091 |
| 129 | 2.7202 | 0.0091 |
| 130 | 2.7292 | 0.0090 |
| 131 | 2.7382 | 0.0090 |
| 132 | 2.7471 | 0.0089 |
| 133 | 2.7560 | 0.0089 |
| 134 | 2.7649 | 0.0089 |
| 135 | 2.7737 | 0.0088 |
| 136 | 2.7825 | 0.0088 |
| 137 | 2.7913 | 0.0088 |
| 138 | 2.8000 | 0.0087 |
| 139 | 2.8087 | 0.0087 |
| 140 | 2.8173 | 0.0086 |
| 141 | 2.8259 | 0.0086 |
| 142 | 2.8345 | 0.0086 |
| 143 | 2.8430 | 0.0085 |
| 144 | 2.8515 | 0.0085 |
| 145 | 2.8600 | 0.0085 |
| 146 | 2.8685 | 0.0084 |
| 147 | 2.8769 | 0.0084 |
| 148 | 2.8852 | 0.0084 |
| 149 | 2.8936 | 0.0083 |
| 150 | 2.9019 | 0.0083 |
| 151 | 2.9102 | 0.0083 |
| 152 | 2.9184 | 0.0082 |
| 153 | 2.9266 | 0.0082 |
| 154 | 2.9348 | 0.0082 |
| 155 | 2.9430 | 0.0082 |
| 156 | 2.9511 | 0.0081 |
| 157 | 2.9592 | 0.0081 |
| 158 | 2.9673 | 0.0081 |
| 159 | 2.9753 | 0.0080 |
| 160 | 2.9833 | 0.0080 |
| 161 | 2.9913 | 0.0080 |
| 162 | 2.9992 | 0.0080 |
| 163 | 3.0072 | 0.0079 |
| 164 | 3.0151 | 0.0079 |
| 165 | 3.0229 | 0.0079 |
| 166 | 3.0308 | 0.0078 |
| 167 | 3.0386 | 0.0078 |
| 168 | 3.0464 | 0.0078 |
| 169 | 3.0541 | 0.0078 |
| 170 | 3.0619 | 0.0077 |
| 171 | 3.0696 | 0.0077 |

| | | |
|---|---|---|
| 172 | 3.0773 | 0.0077 |
| 173 | 3.0849 | 0.0077 |
| 174 | 3.0926 | 0.0076 |
| 175 | 3.1002 | 0.0076 |
| 176 | 3.1077 | 0.0076 |
| 177 | 3.1153 | 0.0076 |
| 178 | 3.1228 | 0.0075 |
| 179 | 3.1303 | 0.0075 |
| 180 | 3.1378 | 0.0075 |
| 181 | 3.1453 | 0.0075 |
| 182 | 3.1527 | 0.0074 |
| 183 | 3.1601 | 0.0074 |
| 184 | 3.1675 | 0.0074 |
| 185 | 3.1749 | 0.0074 |
| 186 | 3.1823 | 0.0073 |
| 187 | 3.1896 | 0.0073 |
| 188 | 3.1969 | 0.0073 |
| 189 | 3.2042 | 0.0073 |
| 190 | 3.2114 | 0.0073 |
| 191 | 3.2187 | 0.0072 |
| 192 | 3.2259 | 0.0072 |
| 193 | 3.2331 | 0.0072 |
| 194 | 3.2402 | 0.0072 |
| 195 | 3.2474 | 0.0072 |
| 196 | 3.2545 | 0.0071 |
| 197 | 3.2616 | 0.0071 |
| 198 | 3.2687 | 0.0071 |
| 199 | 3.2758 | 0.0071 |
| 200 | 3.2828 | 0.0070 |
| 201 | 3.2899 | 0.0070 |
| 202 | 3.2969 | 0.0070 |
| 203 | 3.3039 | 0.0070 |
| 204 | 3.3108 | 0.0070 |
| 205 | 3.3178 | 0.0069 |
| 206 | 3.3247 | 0.0069 |
| 207 | 3.3316 | 0.0069 |
| 208 | 3.3385 | 0.0069 |
| 209 | 3.3454 | 0.0069 |
| 210 | 3.3522 | 0.0069 |
| 211 | 3.3591 | 0.0068 |
| 212 | 3.3659 | 0.0068 |
| 213 | 3.3727 | 0.0068 |
| 214 | 3.3795 | 0.0068 |
| 215 | 3.3862 | 0.0068 |
| 216 | 3.3930 | 0.0067 |
| 217 | 3.3997 | 0.0067 |
| 218 | 3.4064 | 0.0067 |
| 219 | 3.4131 | 0.0067 |
| 220 | 3.4198 | 0.0067 |
| 221 | 3.4264 | 0.0067 |
| 222 | 3.4331 | 0.0066 |
| 223 | 3.4397 | 0.0066 |

| | | |
|---|---|---|
| 224 | 3.4463 | 0.0066 |
| 225 | 3.4529 | 0.0066 |
| 226 | 3.4594 | 0.0066 |
| 227 | 3.4660 | 0.0066 |
| 228 | 3.4725 | 0.0065 |
| 229 | 3.4791 | 0.0065 |
| 230 | 3.4856 | 0.0065 |
| 231 | 3.4921 | 0.0065 |
| 232 | 3.4985 | 0.0065 |
| 233 | 3.5050 | 0.0065 |
| 234 | 3.5114 | 0.0064 |
| 235 | 3.5179 | 0.0064 |
| 236 | 3.5243 | 0.0064 |
| 237 | 3.5307 | 0.0064 |
| 238 | 3.5370 | 0.0064 |
| 239 | 3.5434 | 0.0064 |
| 240 | 3.5498 | 0.0063 |
| 241 | 3.5561 | 0.0063 |
| 242 | 3.5624 | 0.0063 |
| 243 | 3.5687 | 0.0063 |
| 244 | 3.5750 | 0.0063 |
| 245 | 3.5813 | 0.0063 |
| 246 | 3.5875 | 0.0063 |
| 247 | 3.5938 | 0.0062 |
| 248 | 3.6000 | 0.0062 |
| 249 | 3.6062 | 0.0062 |
| 250 | 3.6124 | 0.0062 |
| 251 | 3.6186 | 0.0062 |
| 252 | 3.6248 | 0.0062 |
| 253 | 3.6310 | 0.0062 |
| 254 | 3.6371 | 0.0061 |
| 255 | 3.6432 | 0.0061 |
| 256 | 3.6493 | 0.0061 |
| 257 | 3.6555 | 0.0061 |
| 258 | 3.6615 | 0.0061 |
| 259 | 3.6676 | 0.0061 |
| 260 | 3.6737 | 0.0061 |
| 261 | 3.6797 | 0.0061 |
| 262 | 3.6858 | 0.0060 |
| 263 | 3.6918 | 0.0060 |
| 264 | 3.6978 | 0.0060 |
| 265 | 3.7038 | 0.0060 |
| 266 | 3.7098 | 0.0060 |
| 267 | 3.7158 | 0.0060 |
| 268 | 3.7217 | 0.0060 |
| 269 | 3.7277 | 0.0059 |
| 270 | 3.7336 | 0.0059 |
| 271 | 3.7395 | 0.0059 |
| 272 | 3.7455 | 0.0059 |
| 273 | 3.7513 | 0.0059 |
| 274 | 3.7572 | 0.0059 |
| 275 | 3.7631 | 0.0059 |

| | | |
|---|---|---|
| 276 | 3.7690 | 0.0059 |
| 277 | 3.7748 | 0.0058 |
| 278 | 3.7807 | 0.0058 |
| 279 | 3.7865 | 0.0058 |
| 280 | 3.7923 | 0.0058 |
| 281 | 3.7981 | 0.0058 |
| 282 | 3.8039 | 0.0058 |
| 283 | 3.8097 | 0.0058 |
| 284 | 3.8154 | 0.0058 |
| 285 | 3.8212 | 0.0058 |
| 286 | 3.8269 | 0.0057 |
| 287 | 3.8327 | 0.0057 |
| 288 | 3.8384 | 0.0057 |

| Unit Period (number) | Unit Rainfall (In) | Unit Soil-Loss (In) | Effective Rainfall (In) |
|---|---|---|---|
| 1 | 0.0057 | 0.0031 | 0.0026 |
| 2 | 0.0057 | 0.0031 | 0.0026 |
| 3 | 0.0058 | 0.0031 | 0.0026 |
| 4 | 0.0058 | 0.0031 | 0.0026 |
| 5 | 0.0058 | 0.0031 | 0.0027 |
| 6 | 0.0058 | 0.0031 | 0.0027 |
| 7 | 0.0058 | 0.0032 | 0.0027 |
| 8 | 0.0058 | 0.0032 | 0.0027 |
| 9 | 0.0059 | 0.0032 | 0.0027 |
| 10 | 0.0059 | 0.0032 | 0.0027 |
| 11 | 0.0059 | 0.0032 | 0.0027 |
| 12 | 0.0059 | 0.0032 | 0.0027 |
| 13 | 0.0059 | 0.0032 | 0.0027 |
| 14 | 0.0059 | 0.0032 | 0.0027 |
| 15 | 0.0060 | 0.0032 | 0.0027 |
| 16 | 0.0060 | 0.0032 | 0.0027 |
| 17 | 0.0060 | 0.0033 | 0.0028 |
| 18 | 0.0060 | 0.0033 | 0.0028 |
| 19 | 0.0061 | 0.0033 | 0.0028 |
| 20 | 0.0061 | 0.0033 | 0.0028 |
| 21 | 0.0061 | 0.0033 | 0.0028 |
| 22 | 0.0061 | 0.0033 | 0.0028 |
| 23 | 0.0061 | 0.0033 | 0.0028 |
| 24 | 0.0061 | 0.0033 | 0.0028 |
| 25 | 0.0062 | 0.0033 | 0.0028 |
| 26 | 0.0062 | 0.0034 | 0.0028 |
| 27 | 0.0062 | 0.0034 | 0.0028 |
| 28 | 0.0062 | 0.0034 | 0.0029 |
| 29 | 0.0063 | 0.0034 | 0.0029 |
| 30 | 0.0063 | 0.0034 | 0.0029 |
| 31 | 0.0063 | 0.0034 | 0.0029 |
| 32 | 0.0063 | 0.0034 | 0.0029 |
| 33 | 0.0063 | 0.0034 | 0.0029 |
| 34 | 0.0064 | 0.0034 | 0.0029 |

| | | | |
|---|---|---|---|
| 35 | 0.0064 | 0.0035 | 0.0029 |
| 36 | 0.0064 | 0.0035 | 0.0029 |
| 37 | 0.0064 | 0.0035 | 0.0030 |
| 38 | 0.0065 | 0.0035 | 0.0030 |
| 39 | 0.0065 | 0.0035 | 0.0030 |
| 40 | 0.0065 | 0.0035 | 0.0030 |
| 41 | 0.0065 | 0.0035 | 0.0030 |
| 42 | 0.0066 | 0.0036 | 0.0030 |
| 43 | 0.0066 | 0.0036 | 0.0030 |
| 44 | 0.0066 | 0.0036 | 0.0030 |
| 45 | 0.0066 | 0.0036 | 0.0030 |
| 46 | 0.0067 | 0.0036 | 0.0031 |
| 47 | 0.0067 | 0.0036 | 0.0031 |
| 48 | 0.0067 | 0.0036 | 0.0031 |
| 49 | 0.0067 | 0.0037 | 0.0031 |
| 50 | 0.0068 | 0.0037 | 0.0031 |
| 51 | 0.0068 | 0.0037 | 0.0031 |
| 52 | 0.0068 | 0.0037 | 0.0031 |
| 53 | 0.0069 | 0.0037 | 0.0031 |
| 54 | 0.0069 | 0.0037 | 0.0031 |
| 55 | 0.0069 | 0.0037 | 0.0032 |
| 56 | 0.0069 | 0.0038 | 0.0032 |
| 57 | 0.0070 | 0.0038 | 0.0032 |
| 58 | 0.0070 | 0.0038 | 0.0032 |
| 59 | 0.0070 | 0.0038 | 0.0032 |
| 60 | 0.0070 | 0.0038 | 0.0032 |
| 61 | 0.0071 | 0.0038 | 0.0032 |
| 62 | 0.0071 | 0.0039 | 0.0033 |
| 63 | 0.0072 | 0.0039 | 0.0033 |
| 64 | 0.0072 | 0.0039 | 0.0033 |
| 65 | 0.0072 | 0.0039 | 0.0033 |
| 66 | 0.0072 | 0.0039 | 0.0033 |
| 67 | 0.0073 | 0.0039 | 0.0033 |
| 68 | 0.0073 | 0.0040 | 0.0033 |
| 69 | 0.0073 | 0.0040 | 0.0034 |
| 70 | 0.0074 | 0.0040 | 0.0034 |
| 71 | 0.0074 | 0.0040 | 0.0034 |
| 72 | 0.0074 | 0.0040 | 0.0034 |
| 73 | 0.0075 | 0.0041 | 0.0034 |
| 74 | 0.0075 | 0.0041 | 0.0034 |
| 75 | 0.0076 | 0.0041 | 0.0035 |
| 76 | 0.0076 | 0.0041 | 0.0035 |
| 77 | 0.0076 | 0.0041 | 0.0035 |
| 78 | 0.0077 | 0.0041 | 0.0035 |
| 79 | 0.0077 | 0.0042 | 0.0035 |
| 80 | 0.0077 | 0.0042 | 0.0035 |
| 81 | 0.0078 | 0.0042 | 0.0036 |
| 82 | 0.0078 | 0.0042 | 0.0036 |
| 83 | 0.0079 | 0.0043 | 0.0036 |
| 84 | 0.0079 | 0.0043 | 0.0036 |
| 85 | 0.0080 | 0.0043 | 0.0036 |
| 86 | 0.0080 | 0.0043 | 0.0037 |

| | | | |
|---|---|---|---|
| 87 | 0.0080 | 0.0044 | 0.0037 |
| 88 | 0.0081 | 0.0044 | 0.0037 |
| 89 | 0.0081 | 0.0044 | 0.0037 |
| 90 | 0.0082 | 0.0044 | 0.0037 |
| 91 | 0.0082 | 0.0045 | 0.0038 |
| 92 | 0.0082 | 0.0045 | 0.0038 |
| 93 | 0.0083 | 0.0045 | 0.0038 |
| 94 | 0.0083 | 0.0045 | 0.0038 |
| 95 | 0.0084 | 0.0046 | 0.0039 |
| 96 | 0.0084 | 0.0046 | 0.0039 |
| 97 | 0.0085 | 0.0046 | 0.0039 |
| 98 | 0.0085 | 0.0046 | 0.0039 |
| 99 | 0.0086 | 0.0047 | 0.0039 |
| 100 | 0.0086 | 0.0047 | 0.0040 |
| 101 | 0.0087 | 0.0047 | 0.0040 |
| 102 | 0.0088 | 0.0047 | 0.0040 |
| 103 | 0.0088 | 0.0048 | 0.0040 |
| 104 | 0.0089 | 0.0048 | 0.0041 |
| 105 | 0.0089 | 0.0048 | 0.0041 |
| 106 | 0.0090 | 0.0049 | 0.0041 |
| 107 | 0.0091 | 0.0049 | 0.0042 |
| 108 | 0.0091 | 0.0049 | 0.0042 |
| 109 | 0.0092 | 0.0050 | 0.0042 |
| 110 | 0.0092 | 0.0050 | 0.0042 |
| 111 | 0.0093 | 0.0050 | 0.0043 |
| 112 | 0.0094 | 0.0051 | 0.0043 |
| 113 | 0.0094 | 0.0051 | 0.0043 |
| 114 | 0.0095 | 0.0051 | 0.0043 |
| 115 | 0.0096 | 0.0052 | 0.0044 |
| 116 | 0.0096 | 0.0052 | 0.0044 |
| 117 | 0.0097 | 0.0053 | 0.0045 |
| 118 | 0.0098 | 0.0053 | 0.0045 |
| 119 | 0.0099 | 0.0054 | 0.0045 |
| 120 | 0.0099 | 0.0054 | 0.0045 |
| 121 | 0.0100 | 0.0054 | 0.0046 |
| 122 | 0.0101 | 0.0055 | 0.0046 |
| 123 | 0.0102 | 0.0055 | 0.0047 |
| 124 | 0.0103 | 0.0056 | 0.0047 |
| 125 | 0.0104 | 0.0056 | 0.0048 |
| 126 | 0.0104 | 0.0056 | 0.0048 |
| 127 | 0.0105 | 0.0057 | 0.0048 |
| 128 | 0.0106 | 0.0057 | 0.0049 |
| 129 | 0.0107 | 0.0058 | 0.0049 |
| 130 | 0.0108 | 0.0059 | 0.0049 |
| 131 | 0.0109 | 0.0059 | 0.0050 |
| 132 | 0.0110 | 0.0060 | 0.0050 |
| 133 | 0.0111 | 0.0060 | 0.0051 |
| 134 | 0.0112 | 0.0061 | 0.0051 |
| 135 | 0.0114 | 0.0062 | 0.0052 |
| 136 | 0.0114 | 0.0062 | 0.0052 |
| 137 | 0.0116 | 0.0063 | 0.0053 |
| 138 | 0.0117 | 0.0063 | 0.0053 |

| | | | |
|---|---|---|---|
| 139 | 0.0118 | 0.0064 | 0.0054 |
| 140 | 0.0119 | 0.0065 | 0.0055 |
| 141 | 0.0121 | 0.0066 | 0.0055 |
| 142 | 0.0122 | 0.0066 | 0.0056 |
| 143 | 0.0124 | 0.0067 | 0.0057 |
| 144 | 0.0125 | 0.0068 | 0.0057 |
| 145 | 0.0140 | 0.0076 | 0.0064 |
| 146 | 0.0141 | 0.0077 | 0.0065 |
| 147 | 0.0144 | 0.0078 | 0.0066 |
| 148 | 0.0145 | 0.0078 | 0.0066 |
| 149 | 0.0147 | 0.0080 | 0.0067 |
| 150 | 0.0148 | 0.0080 | 0.0068 |
| 151 | 0.0151 | 0.0082 | 0.0069 |
| 152 | 0.0152 | 0.0082 | 0.0070 |
| 153 | 0.0155 | 0.0084 | 0.0071 |
| 154 | 0.0156 | 0.0085 | 0.0072 |
| 155 | 0.0159 | 0.0086 | 0.0073 |
| 156 | 0.0160 | 0.0087 | 0.0074 |
| 157 | 0.0164 | 0.0089 | 0.0075 |
| 158 | 0.0165 | 0.0089 | 0.0076 |
| 159 | 0.0169 | 0.0091 | 0.0077 |
| 160 | 0.0170 | 0.0092 | 0.0078 |
| 161 | 0.0174 | 0.0094 | 0.0080 |
| 162 | 0.0176 | 0.0095 | 0.0081 |
| 163 | 0.0180 | 0.0098 | 0.0083 |
| 164 | 0.0182 | 0.0099 | 0.0084 |
| 165 | 0.0187 | 0.0101 | 0.0086 |
| 166 | 0.0189 | 0.0103 | 0.0087 |
| 167 | 0.0194 | 0.0105 | 0.0089 |
| 168 | 0.0197 | 0.0107 | 0.0090 |
| 169 | 0.0203 | 0.0110 | 0.0093 |
| 170 | 0.0206 | 0.0112 | 0.0094 |
| 171 | 0.0212 | 0.0115 | 0.0097 |
| 172 | 0.0216 | 0.0117 | 0.0099 |
| 173 | 0.0224 | 0.0121 | 0.0102 |
| 174 | 0.0228 | 0.0123 | 0.0104 |
| 175 | 0.0236 | 0.0128 | 0.0108 |
| 176 | 0.0241 | 0.0131 | 0.0111 |
| 177 | 0.0252 | 0.0136 | 0.0115 |
| 178 | 0.0258 | 0.0140 | 0.0118 |
| 179 | 0.0271 | 0.0147 | 0.0124 |
| 180 | 0.0278 | 0.0150 | 0.0127 |
| 181 | 0.0294 | 0.0159 | 0.0135 |
| 182 | 0.0303 | 0.0164 | 0.0139 |
| 183 | 0.0324 | 0.0176 | 0.0149 |
| 184 | 0.0337 | 0.0182 | 0.0154 |
| 185 | 0.0309 | 0.0167 | 0.0142 |
| 186 | 0.0326 | 0.0177 | 0.0150 |
| 187 | 0.0371 | 0.0201 | 0.0170 |
| 188 | 0.0399 | 0.0216 | 0.0183 |
| 189 | 0.0481 | 0.0261 | 0.0221 |
| 190 | 0.0543 | 0.0294 | 0.0249 |

| | | | |
|---|---|---|---|
| 191 | 0.0777 | 0.0336 | 0.0440 |
| 192 | 0.1068 | 0.0336 | 0.0732 |
| 193 | 0.3343 | 0.0336 | 0.3007 |
| 194 | 0.0633 | 0.0336 | 0.0296 |
| 195 | 0.0435 | 0.0236 | 0.0200 |
| 196 | 0.0347 | 0.0188 | 0.0159 |
| 197 | 0.0351 | 0.0190 | 0.0161 |
| 198 | 0.0313 | 0.0170 | 0.0144 |
| 199 | 0.0285 | 0.0155 | 0.0131 |
| 200 | 0.0264 | 0.0143 | 0.0121 |
| 201 | 0.0246 | 0.0133 | 0.0113 |
| 202 | 0.0232 | 0.0126 | 0.0106 |
| 203 | 0.0220 | 0.0119 | 0.0101 |
| 204 | 0.0209 | 0.0113 | 0.0096 |
| 205 | 0.0200 | 0.0108 | 0.0092 |
| 206 | 0.0192 | 0.0104 | 0.0088 |
| 207 | 0.0184 | 0.0100 | 0.0085 |
| 208 | 0.0178 | 0.0096 | 0.0082 |
| 209 | 0.0172 | 0.0093 | 0.0079 |
| 210 | 0.0167 | 0.0090 | 0.0076 |
| 211 | 0.0162 | 0.0088 | 0.0074 |
| 212 | 0.0157 | 0.0085 | 0.0072 |
| 213 | 0.0153 | 0.0083 | 0.0070 |
| 214 | 0.0149 | 0.0081 | 0.0068 |
| 215 | 0.0146 | 0.0079 | 0.0067 |
| 216 | 0.0143 | 0.0077 | 0.0065 |
| 217 | 0.0126 | 0.0068 | 0.0058 |
| 218 | 0.0123 | 0.0067 | 0.0056 |
| 219 | 0.0120 | 0.0065 | 0.0055 |
| 220 | 0.0118 | 0.0064 | 0.0054 |
| 221 | 0.0115 | 0.0062 | 0.0053 |
| 222 | 0.0113 | 0.0061 | 0.0052 |
| 223 | 0.0111 | 0.0060 | 0.0051 |
| 224 | 0.0109 | 0.0059 | 0.0050 |
| 225 | 0.0107 | 0.0058 | 0.0049 |
| 226 | 0.0105 | 0.0057 | 0.0048 |
| 227 | 0.0103 | 0.0056 | 0.0047 |
| 228 | 0.0101 | 0.0055 | 0.0046 |
| 229 | 0.0100 | 0.0054 | 0.0046 |
| 230 | 0.0098 | 0.0053 | 0.0045 |
| 231 | 0.0097 | 0.0052 | 0.0044 |
| 232 | 0.0095 | 0.0052 | 0.0044 |
| 233 | 0.0094 | 0.0051 | 0.0043 |
| 234 | 0.0093 | 0.0050 | 0.0042 |
| 235 | 0.0091 | 0.0050 | 0.0042 |
| 236 | 0.0090 | 0.0049 | 0.0041 |
| 237 | 0.0089 | 0.0048 | 0.0041 |
| 238 | 0.0088 | 0.0048 | 0.0040 |
| 239 | 0.0087 | 0.0047 | 0.0040 |
| 240 | 0.0086 | 0.0046 | 0.0039 |
| 241 | 0.0085 | 0.0046 | 0.0039 |
| 242 | 0.0084 | 0.0045 | 0.0038 |

| | | | |
|---|---|---|---|
| 243 | 0.0083 | 0.0045 | 0.0038 |
| 244 | 0.0082 | 0.0044 | 0.0038 |
| 245 | 0.0081 | 0.0044 | 0.0037 |
| 246 | 0.0080 | 0.0043 | 0.0037 |
| 247 | 0.0079 | 0.0043 | 0.0036 |
| 248 | 0.0078 | 0.0042 | 0.0036 |
| 249 | 0.0078 | 0.0042 | 0.0036 |
| 250 | 0.0077 | 0.0042 | 0.0035 |
| 251 | 0.0076 | 0.0041 | 0.0035 |
| 252 | 0.0075 | 0.0041 | 0.0035 |
| 253 | 0.0075 | 0.0040 | 0.0034 |
| 254 | 0.0074 | 0.0040 | 0.0034 |
| 255 | 0.0073 | 0.0040 | 0.0034 |
| 256 | 0.0073 | 0.0039 | 0.0033 |
| 257 | 0.0072 | 0.0039 | 0.0033 |
| 258 | 0.0071 | 0.0039 | 0.0033 |
| 259 | 0.0071 | 0.0038 | 0.0032 |
| 260 | 0.0070 | 0.0038 | 0.0032 |
| 261 | 0.0069 | 0.0038 | 0.0032 |
| 262 | 0.0069 | 0.0037 | 0.0032 |
| 263 | 0.0068 | 0.0037 | 0.0031 |
| 264 | 0.0068 | 0.0037 | 0.0031 |
| 265 | 0.0067 | 0.0036 | 0.0031 |
| 266 | 0.0067 | 0.0036 | 0.0031 |
| 267 | 0.0066 | 0.0036 | 0.0030 |
| 268 | 0.0066 | 0.0036 | 0.0030 |
| 269 | 0.0065 | 0.0035 | 0.0030 |
| 270 | 0.0065 | 0.0035 | 0.0030 |
| 271 | 0.0064 | 0.0035 | 0.0029 |
| 272 | 0.0064 | 0.0035 | 0.0029 |
| 273 | 0.0063 | 0.0034 | 0.0029 |
| 274 | 0.0063 | 0.0034 | 0.0029 |
| 275 | 0.0062 | 0.0034 | 0.0029 |
| 276 | 0.0062 | 0.0034 | 0.0028 |
| 277 | 0.0062 | 0.0033 | 0.0028 |
| 278 | 0.0061 | 0.0033 | 0.0028 |
| 279 | 0.0061 | 0.0033 | 0.0028 |
| 280 | 0.0060 | 0.0033 | 0.0028 |
| 281 | 0.0060 | 0.0032 | 0.0027 |
| 282 | 0.0060 | 0.0032 | 0.0027 |
| 283 | 0.0059 | 0.0032 | 0.0027 |
| 284 | 0.0059 | 0.0032 | 0.0027 |
| 285 | 0.0058 | 0.0032 | 0.0027 |
| 286 | 0.0058 | 0.0031 | 0.0027 |
| 287 | 0.0058 | 0.0031 | 0.0026 |
| 288 | 0.0057 | 0.0031 | 0.0026 |

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Total soil rain loss = 1.90(In)
Total effective rainfall = 1.94(In)
Peak flow rate in flood hydrograph = 6.38(CFS)

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24 - H O U R  S T O R M

R u n o f f  H y d r o g r a p h

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Hydrograph in 5 Minute intervals ((CFS))

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| Time(h+m) | Volume Ac.Ft | Q(CFS) | 0 | 2.5 | 5.0 | 7.5 | 10.0 |
|---|---|---|---|---|---|---|---|
| 0+ 5 | 0.0000 | 0.01 | Q | | | | |
| 0+10 | 0.0002 | 0.03 | Q | | | | |
| 0+15 | 0.0007 | 0.07 | Q | | | | |
| 0+20 | 0.0014 | 0.10 | Q | | | | |
| 0+25 | 0.0022 | 0.12 | Q | | | | |
| 0+30 | 0.0032 | 0.13 | Q | | | | |
| 0+35 | 0.0041 | 0.14 | Q | | | | |
| 0+40 | 0.0052 | 0.15 | Q | | | | |
| 0+45 | 0.0062 | 0.15 | Q | | | | |
| 0+50 | 0.0073 | 0.16 | Q | | | | |
| 0+55 | 0.0084 | 0.16 | Q | | | | |
| 1+ 0 | 0.0096 | 0.17 | Q | | | | |
| 1+ 5 | 0.0107 | 0.17 | Q | | | | |
| 1+10 | 0.0119 | 0.17 | Q | | | | |
| 1+15 | 0.0131 | 0.17 | Q | | | | |
| 1+20 | 0.0143 | 0.17 | Q | | | | |
| 1+25 | 0.0155 | 0.18 | Q | | | | |
| 1+30 | 0.0167 | 0.18 | Q | | | | |
| 1+35 | 0.0180 | 0.18 | Q | | | | |
| 1+40 | 0.0192 | 0.18 | Q | | | | |
| 1+45 | 0.0205 | 0.18 | Q | | | | |
| 1+50 | 0.0218 | 0.18 | Q | | | | |
| 1+55 | 0.0230 | 0.18 | QV | | | | |
| 2+ 0 | 0.0243 | 0.19 | QV | | | | |
| 2+ 5 | 0.0256 | 0.19 | QV | | | | |
| 2+10 | 0.0269 | 0.19 | QV | | | | |
| 2+15 | 0.0282 | 0.19 | QV | | | | |
| 2+20 | 0.0295 | 0.19 | QV | | | | |
| 2+25 | 0.0308 | 0.19 | QV | | | | |
| 2+30 | 0.0321 | 0.19 | QV | | | | |
| 2+35 | 0.0334 | 0.19 | QV | | | | |
| 2+40 | 0.0347 | 0.19 | QV | | | | |
| 2+45 | 0.0361 | 0.19 | QV | | | | |
| 2+50 | 0.0374 | 0.19 | QV | | | | |
| 2+55 | 0.0387 | 0.19 | QV | | | | |
| 3+ 0 | 0.0401 | 0.19 | QV | | | | |
| 3+ 5 | 0.0414 | 0.19 | QV | | | | |
| 3+10 | 0.0427 | 0.20 | QV | | | | |
| 3+15 | 0.0441 | 0.20 | QV | | | | |
| 3+20 | 0.0455 | 0.20 | Q V | | | | |
| 3+25 | 0.0468 | 0.20 | Q V | | | | |
| 3+30 | 0.0482 | 0.20 | Q V | | | | |
| 3+35 | 0.0496 | 0.20 | Q V | | | | |

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 3+40 | 0.0509 | 0.20 | Q V | \| | \| | \| | \| |
| 3+45 | 0.0523 | 0.20 | Q V | \| | \| | \| | \| |
| 3+50 | 0.0537 | 0.20 | Q V | \| | \| | \| | \| |
| 3+55 | 0.0551 | 0.20 | Q V | \| | \| | \| | \| |
| 4+ 0 | 0.0565 | 0.20 | Q V | \| | \| | \| | \| |
| 4+ 5 | 0.0579 | 0.20 | Q V | \| | \| | \| | \| |
| 4+10 | 0.0593 | 0.20 | Q V | \| | \| | \| | \| |
| 4+15 | 0.0607 | 0.21 | Q V | \| | \| | \| | \| |
| 4+20 | 0.0621 | 0.21 | Q V | \| | \| | \| | \| |
| 4+25 | 0.0636 | 0.21 | Q V | \| | \| | \| | \| |
| 4+30 | 0.0650 | 0.21 | Q V | \| | \| | \| | \| |
| 4+35 | 0.0664 | 0.21 | Q V | \| | \| | \| | \| |
| 4+40 | 0.0679 | 0.21 | Q V | \| | \| | \| | \| |
| 4+45 | 0.0693 | 0.21 | Q V | \| | \| | \| | \| |
| 4+50 | 0.0708 | 0.21 | Q V | \| | \| | \| | \| |
| 4+55 | 0.0722 | 0.21 | Q V | \| | \| | \| | \| |
| 5+ 0 | 0.0737 | 0.21 | Q V | \| | \| | \| | \| |
| 5+ 5 | 0.0752 | 0.21 | Q V | \| | \| | \| | \| |
| 5+10 | 0.0767 | 0.21 | Q V | \| | \| | \| | \| |
| 5+15 | 0.0781 | 0.22 | Q V | \| | \| | \| | \| |
| 5+20 | 0.0796 | 0.22 | Q V | \| | \| | \| | \| |
| 5+25 | 0.0811 | 0.22 | Q V | \| | \| | \| | \| |
| 5+30 | 0.0826 | 0.22 | Q V | \| | \| | \| | \| |
| 5+35 | 0.0841 | 0.22 | Q V | \| | \| | \| | \| |
| 5+40 | 0.0857 | 0.22 | Q V | \| | \| | \| | \| |
| 5+45 | 0.0872 | 0.22 | Q V | \| | \| | \| | \| |
| 5+50 | 0.0887 | 0.22 | Q V | \| | \| | \| | \| |
| 5+55 | 0.0903 | 0.22 | Q V | \| | \| | \| | \| |
| 6+ 0 | 0.0918 | 0.22 | Q V | \| | \| | \| | \| |
| 6+ 5 | 0.0934 | 0.23 | Q V | \| | \| | \| | \| |
| 6+10 | 0.0949 | 0.23 | Q V | \| | \| | \| | \| |
| 6+15 | 0.0965 | 0.23 | Q V | \| | \| | \| | \| |
| 6+20 | 0.0981 | 0.23 | Q V | \| | \| | \| | \| |
| 6+25 | 0.0996 | 0.23 | Q V | \| | \| | \| | \| |
| 6+30 | 0.1012 | 0.23 | Q V | \| | \| | \| | \| |
| 6+35 | 0.1028 | 0.23 | Q V | \| | \| | \| | \| |
| 6+40 | 0.1044 | 0.23 | Q V | \| | \| | \| | \| |
| 6+45 | 0.1060 | 0.23 | Q V | \| | \| | \| | \| |
| 6+50 | 0.1077 | 0.24 | Q V | \| | \| | \| | \| |
| 6+55 | 0.1093 | 0.24 | Q V | \| | \| | \| | \| |
| 7+ 0 | 0.1109 | 0.24 | Q V | \| | \| | \| | \| |
| 7+ 5 | 0.1126 | 0.24 | Q V | \| | \| | \| | \| |
| 7+10 | 0.1142 | 0.24 | Q V | \| | \| | \| | \| |
| 7+15 | 0.1159 | 0.24 | Q V | \| | \| | \| | \| |
| 7+20 | 0.1176 | 0.24 | Q V | \| | \| | \| | \| |
| 7+25 | 0.1192 | 0.24 | Q V | \| | \| | \| | \| |
| 7+30 | 0.1209 | 0.25 | Q V | \| | \| | \| | \| |
| 7+35 | 0.1226 | 0.25 | Q V | \| | \| | \| | \| |
| 7+40 | 0.1243 | 0.25 | Q V | \| | \| | \| | \| |
| 7+45 | 0.1260 | 0.25 | Q V | \| | \| | \| | \| |
| 7+50 | 0.1278 | 0.25 | \|Q V | \| | \| | \| | \| |
| 7+55 | 0.1295 | 0.25 | \|Q V | \| | \| | \| | \| |

```
 8+ 0       0.1312      0.25  |Q   V    |          |          |          |
 8+ 5       0.1330      0.25  |Q   V    |          |          |          |
 8+10       0.1348      0.26  |Q    V   |          |          |          |
 8+15       0.1365      0.26  |Q    V   |          |          |          |
 8+20       0.1383      0.26  |Q    V   |          |          |          |
 8+25       0.1401      0.26  |Q    V   |          |          |          |
 8+30       0.1419      0.26  |Q    V   |          |          |          |
 8+35       0.1438      0.26  |Q    V   |          |          |          |
 8+40       0.1456      0.27  |Q    V   |          |          |          |
 8+45       0.1474      0.27  |Q    V   |          |          |          |
 8+50       0.1493      0.27  |Q    V   |          |          |          |
 8+55       0.1511      0.27  |Q    V   |          |          |          |
 9+ 0       0.1530      0.27  |Q    V   |          |          |          |
 9+ 5       0.1549      0.27  |Q    V   |          |          |          |
 9+10       0.1568      0.28  |Q    V   |          |          |          |
 9+15       0.1587      0.28  |Q     V  |          |          |          |
 9+20       0.1606      0.28  |Q     V  |          |          |          |
 9+25       0.1626      0.28  |Q     V  |          |          |          |
 9+30       0.1645      0.28  |Q     V  |          |          |          |
 9+35       0.1665      0.29  |Q     V  |          |          |          |
 9+40       0.1685      0.29  |Q     V  |          |          |          |
 9+45       0.1705      0.29  |Q     V  |          |          |          |
 9+50       0.1725      0.29  |Q     V  |          |          |          |
 9+55       0.1745      0.29  |Q     V  |          |          |          |
10+ 0       0.1765      0.30  |Q     V  |          |          |          |
10+ 5       0.1786      0.30  |Q     V  |          |          |          |
10+10       0.1807      0.30  |Q      V |          |          |          |
10+15       0.1827      0.30  |Q      V |          |          |          |
10+20       0.1848      0.30  |Q      V |          |          |          |
10+25       0.1870      0.31  |Q      V |          |          |          |
10+30       0.1891      0.31  |Q      V |          |          |          |
10+35       0.1912      0.31  |Q      V |          |          |          |
10+40       0.1934      0.31  |Q      V |          |          |          |
10+45       0.1956      0.32  |Q      V |          |          |          |
10+50       0.1978      0.32  |Q      V |          |          |          |
10+55       0.2000      0.32  |Q      V |          |          |          |
11+ 0       0.2023      0.33  |Q       V|          |          |          |
11+ 5       0.2045      0.33  |Q       V|          |          |          |
11+10       0.2068      0.33  |Q       V|          |          |          |
11+15       0.2091      0.33  |Q       V|          |          |          |
11+20       0.2115      0.34  |Q       V|          |          |          |
11+25       0.2138      0.34  |Q       V|          |          |          |
11+30       0.2162      0.34  |Q       V|          |          |          |
11+35       0.2186      0.35  |Q       V|          |          |          |
11+40       0.2210      0.35  |Q       V|          |          |          |
11+45       0.2234      0.35  |Q       V|          |          |          |
11+50       0.2259      0.36  |Q        V          |          |          |
11+55       0.2284      0.36  |Q        V          |          |          |
12+ 0       0.2309      0.37  |Q        V          |          |          |
12+ 5       0.2335      0.37  |Q        V          |          |          |
12+10       0.2361      0.38  |Q        V          |          |          |
12+15       0.2388      0.39  |Q        V          |          |          |
```

```
12+20       0.2416      0.41  |Q        V         |         |         |
12+25       0.2445      0.42  |Q        V         |         |         |
12+30       0.2474      0.42  |Q        |V        |         |         |
12+35       0.2504      0.43  |Q        |V        |         |         |
12+40       0.2534      0.44  |Q        |V        |         |         |
12+45       0.2565      0.44  |Q        |V        |         |         |
12+50       0.2596      0.45  |Q        |V        |         |         |
12+55       0.2627      0.46  |Q        |V        |         |         |
13+ 0       0.2659      0.46  |Q        |V        |         |         |
13+ 5       0.2692      0.47  |Q        | V       |         |         |
13+10       0.2724      0.48  |Q        | V       |         |         |
13+15       0.2758      0.48  |Q        | V       |         |         |
13+20       0.2792      0.49  |Q        | V       |         |         |
13+25       0.2826      0.50  |Q        | V       |         |         |
13+30       0.2861      0.51  | Q       | V       |         |         |
13+35       0.2896      0.51  | Q       | V       |         |         |
13+40       0.2932      0.52  | Q       |  V      |         |         |
13+45       0.2969      0.53  | Q       |  V      |         |         |
13+50       0.3006      0.54  | Q       |  V      |         |         |
13+55       0.3044      0.55  | Q       |  V      |         |         |
14+ 0       0.3083      0.56  | Q       |  V      |         |         |
14+ 5       0.3122      0.57  | Q       |  V      |         |         |
14+10       0.3162      0.58  | Q       |   V     |         |         |
14+15       0.3203      0.59  | Q       |   V     |         |         |
14+20       0.3245      0.61  | Q       |   V     |         |         |
14+25       0.3288      0.62  | Q       |   V     |         |         |
14+30       0.3332      0.63  | Q       |   V     |         |         |
14+35       0.3376      0.65  | Q       |    V    |         |         |
14+40       0.3422      0.67  | Q       |    V    |         |         |
14+45       0.3470      0.68  | Q       |    V    |         |         |
14+50       0.3518      0.70  | Q       |    V    |         |         |
14+55       0.3568      0.72  | Q       |    V    |         |         |
15+ 0       0.3619      0.75  | Q       |     V   |         |         |
15+ 5       0.3673      0.77  |  Q      |     V   |         |         |
15+10       0.3728      0.80  |  Q      |     V   |         |         |
15+15       0.3785      0.83  |  Q      |     V   |         |         |
15+20       0.3845      0.87  |  Q      |      V  |         |         |
15+25       0.3907      0.90  |  Q      |      V  |         |         |
15+30       0.3971      0.93  |  Q      |      V  |         |         |
15+35       0.4036      0.94  |  Q      |       V |         |         |
15+40       0.4103      0.97  |  Q      |       V |         |         |
15+45       0.4174      1.03  |   Q     |       V |         |         |
15+50       0.4252      1.13  |   Q     |       V |         |         |
15+55       0.4340      1.29  |    Q    |        V|         |         |
16+ 0       0.4453      1.64  |     Q   |        V|         |         |
16+ 5       0.4643      2.76  |         |Q        V         |         |
16+10       0.4977      4.85  |         |        Q| V       |         |
16+15       0.5416      6.38  |         |         |  VQ     |         |
16+20       0.5810      5.72  |         |         | Q  V    |         |
16+25       0.6071      3.79  |         |    Q    |      V  |         |
16+30       0.6256      2.69  |         Q         |      V  |         |
16+35       0.6407      2.20  |       Q |         |       V |         |
```

```
16+40       0.6538      1.90  |      Q  |         |        V|         |
16+45       0.6654      1.68  |     Q   |         |        V|         |
16+50       0.6756      1.48  |    Q    |         |         V         |
16+55       0.6849      1.35  |    Q    |         |         V         |
17+ 0       0.6933      1.21  |   Q     |         |         V         |
17+ 5       0.7009      1.11  |   Q     |         |         |V        |
17+10       0.7080      1.02  |   Q     |         |         |V        |
17+15       0.7146      0.97  |  Q      |         |         |V        |
17+20       0.7209      0.90  |  Q      |         |         | V       |
17+25       0.7266      0.84  |  Q      |         |         | V       |
17+30       0.7320      0.79  |  Q      |         |         | V       |
17+35       0.7371      0.74  | Q       |         |         | V       |
17+40       0.7419      0.70  | Q       |         |         |  V      |
17+45       0.7465      0.66  | Q       |         |         |  V      |
17+50       0.7508      0.63  | Q       |         |         |  V      |
17+55       0.7550      0.61  | Q       |         |         |  V      |
18+ 0       0.7590      0.58  | Q       |         |         |  V      |
18+ 5       0.7627      0.53  | Q       |         |         |   V     |
18+10       0.7659      0.48  |Q        |         |         |   V     |
18+15       0.7691      0.45  |Q        |         |         |   V     |
18+20       0.7720      0.43  |Q        |         |         |   V     |
18+25       0.7749      0.41  |Q        |         |         |   V     |
18+30       0.7776      0.40  |Q        |         |         |   V     |
18+35       0.7803      0.39  |Q        |         |         |   V     |
18+40       0.7829      0.38  |Q        |         |         |   V     |
18+45       0.7855      0.37  |Q        |         |         |    V    |
18+50       0.7880      0.36  |Q        |         |         |    V    |
18+55       0.7904      0.35  |Q        |         |         |    V    |
19+ 0       0.7928      0.35  |Q        |         |         |    V    |
19+ 5       0.7951      0.34  |Q        |         |         |    V    |
19+10       0.7974      0.33  |Q        |         |         |    V    |
19+15       0.7996      0.33  |Q        |         |         |    V    |
19+20       0.8018      0.32  |Q        |         |         |    V    |
19+25       0.8040      0.31  |Q        |         |         |    V    |
19+30       0.8061      0.31  |Q        |         |         |    V    |
19+35       0.8082      0.30  |Q        |         |         |     V   |
19+40       0.8103      0.30  |Q        |         |         |     V   |
19+45       0.8123      0.29  |Q        |         |         |     V   |
19+50       0.8143      0.29  |Q        |         |         |     V   |
19+55       0.8162      0.29  |Q        |         |         |     V   |
20+ 0       0.8182      0.28  |Q        |         |         |     V   |
20+ 5       0.8201      0.28  |Q        |         |         |     V   |
20+10       0.8220      0.27  |Q        |         |         |     V   |
20+15       0.8238      0.27  |Q        |         |         |     V   |
20+20       0.8257      0.27  |Q        |         |         |     V   |
20+25       0.8275      0.26  |Q        |         |         |     V   |
20+30       0.8293      0.26  |Q        |         |         |     V   |
20+35       0.8310      0.26  |Q        |         |         |      V  |
20+40       0.8328      0.25  |Q        |         |         |      V  |
20+45       0.8345      0.25  |Q        |         |         |      V  |
20+50       0.8362      0.25  Q         |         |         |      V  |
20+55       0.8379      0.25  Q         |         |         |      V  |
```

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 21+ 0 | 0.8396 | 0.24 | Q | \| | \| | \| | V \| |
| 21+ 5 | 0.8413 | 0.24 | Q | \| | \| | \| | V \| |
| 21+10 | 0.8429 | 0.24 | Q | \| | \| | \| | V \| |
| 21+15 | 0.8445 | 0.24 | Q | \| | \| | \| | V \| |
| 21+20 | 0.8461 | 0.23 | Q | \| | \| | \| | V \| |
| 21+25 | 0.8477 | 0.23 | Q | \| | \| | \| | V \| |
| 21+30 | 0.8493 | 0.23 | Q | \| | \| | \| | V \| |
| 21+35 | 0.8509 | 0.23 | Q | \| | \| | \| | V \| |
| 21+40 | 0.8524 | 0.22 | Q | \| | \| | \| | V \| |
| 21+45 | 0.8540 | 0.22 | Q | \| | \| | \| | V \| |
| 21+50 | 0.8555 | 0.22 | Q | \| | \| | \| | V \| |
| 21+55 | 0.8570 | 0.22 | Q | \| | \| | \| | V \| |
| 22+ 0 | 0.8585 | 0.22 | Q | \| | \| | \| | V \| |
| 22+ 5 | 0.8600 | 0.22 | Q | \| | \| | \| | V \| |
| 22+10 | 0.8614 | 0.21 | Q | \| | \| | \| | V \| |
| 22+15 | 0.8629 | 0.21 | Q | \| | \| | \| | V \| |
| 22+20 | 0.8643 | 0.21 | Q | \| | \| | \| | V \| |
| 22+25 | 0.8658 | 0.21 | Q | \| | \| | \| | V \| |
| 22+30 | 0.8672 | 0.21 | Q | \| | \| | \| | V \| |
| 22+35 | 0.8686 | 0.20 | Q | \| | \| | \| | V \| |
| 22+40 | 0.8700 | 0.20 | Q | \| | \| | \| | V \| |
| 22+45 | 0.8714 | 0.20 | Q | \| | \| | \| | V \| |
| 22+50 | 0.8728 | 0.20 | Q | \| | \| | \| | V \| |
| 22+55 | 0.8741 | 0.20 | Q | \| | \| | \| | V \| |
| 23+ 0 | 0.8755 | 0.20 | Q | \| | \| | \| | V\| |
| 23+ 5 | 0.8768 | 0.20 | Q | \| | \| | \| | V\| |
| 23+10 | 0.8782 | 0.19 | Q | \| | \| | \| | V\| |
| 23+15 | 0.8795 | 0.19 | Q | \| | \| | \| | V\| |
| 23+20 | 0.8808 | 0.19 | Q | \| | \| | \| | V\| |
| 23+25 | 0.8821 | 0.19 | Q | \| | \| | \| | V\| |
| 23+30 | 0.8834 | 0.19 | Q | \| | \| | \| | V\| |
| 23+35 | 0.8847 | 0.19 | Q | \| | \| | \| | V\| |
| 23+40 | 0.8860 | 0.19 | Q | \| | \| | \| | V\| |
| 23+45 | 0.8873 | 0.19 | Q | \| | \| | \| | V\| |
| 23+50 | 0.8886 | 0.18 | Q | \| | \| | \| | V\| |
| 23+55 | 0.8898 | 0.18 | Q | \| | \| | \| | V\| |
| 24+ 0 | 0.8911 | 0.18 | Q | \| | \| | \| | V\| |
| 24+ 5 | 0.8923 | 0.17 | Q | \| | \| | \| | V\| |
| 24+10 | 0.8933 | 0.15 | Q | \| | \| | \| | V\| |
| 24+15 | 0.8941 | 0.11 | Q | \| | \| | \| | V\| |
| 24+20 | 0.8946 | 0.08 | Q | \| | \| | \| | V\| |
| 24+25 | 0.8950 | 0.06 | Q | \| | \| | \| | V\| |
| 24+30 | 0.8953 | 0.04 | Q | \| | \| | \| | V\| |
| 24+35 | 0.8956 | 0.04 | Q | \| | \| | \| | V\| |
| 24+40 | 0.8958 | 0.03 | Q | \| | \| | \| | V\| |
| 24+45 | 0.8959 | 0.02 | Q | \| | \| | \| | V\| |
| 24+50 | 0.8961 | 0.02 | Q | \| | \| | \| | V\| |
| 24+55 | 0.8962 | 0.02 | Q | \| | \| | \| | V\| |
| 25+ 0 | 0.8963 | 0.01 | Q | \| | \| | \| | V\| |
| 25+ 5 | 0.8964 | 0.01 | Q | \| | \| | \| | V\| |
| 25+10 | 0.8965 | 0.01 | Q | \| | \| | \| | V\| |
| 25+15 | 0.8965 | 0.01 | Q | \| | \| | \| | V\| |

```
   25+20       0.8966      0.01  Q         |         |         |         V|
   25+25       0.8966      0.01  Q         |         |         |         V|
   25+30       0.8966      0.00  Q         |         |         |         V|
   25+35       0.8967      0.00  Q         |         |         |         V|
   25+40       0.8967      0.00  Q         |         |         |         V|
   25+45       0.8967      0.00  Q         |         |         |         V|
   25+50       0.8967      0.00  Q         |         |         |         V|
   25+55       0.8967      0.00  Q         |         |         |         V|
   26+ 0       0.8967      0.00  Q         |         |         |         V|
-------------------------------------------------------------------------
```

# C.3 – Proposed 10-Year Analysis

U n i t  H y d r o g r a p h  A n a l y s i s



Study date 08/26/24

++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
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San Bernardino County Synthetic Unit Hydrology Method
Manual date - August 1986

Program License Serial Number 6568

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TPM 20854
DEVELOPED CONDITION
10-YEAR
24-HOUR

---

Storm Event Year = 10

Antecedent Moisture Condition = 2

English (in-lb) Input Units Used

English Rainfall Data (Inches) Input Values Used

English Units used in output format

Area averaged rainfall intensity isohyetal data:

| Sub-Area (Ac.) | Duration (hours) | Isohyetal (In) |
|---|---|---|
| Rainfall data for year 10 | | |
| 4.40 | 1 | 0.73 |
| Rainfall data for year 2 | | |
| 4.40 | 6 | 1.15 |
| Rainfall data for year 2 | | |
| 4.40 | 24 | 2.05 |
| Rainfall data for year 100 | | |
| 4.40 | 1 | 1.16 |

---

```
Rainfall data for year 100
             4.40            6            2.65
------------------------------------------------------------------------
Rainfall data for year 100
             4.40           24            4.82
------------------------------------------------------------------------
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++

******** Area-averaged max loss rate, Fm ********


SCS curve  SCS curve     Area     Area     Fp(Fig C6)    Ap      Fm
No.(AMCII) NO.(AMC 2)    (Ac.)    Fraction     (In/Hr)  (dec.)   (In/Hr)
 59.6      59.6          4.40      1.000     0.685    0.299    0.205

Area-averaged adjusted loss rate Fm (In/Hr) =  0.205

********* Area-Averaged low loss rate fraction, Yb **********

Area       Area          SCS CN    SCS CN      S     Pervious
 (Ac.)      Fract         (AMC2)    (AMC2)           Yield Fr
     1.32   0.299         59.6      59.6       6.78     0.122
     3.08   0.701         98.0      98.0       0.20     0.927

Area-averaged catchment yield fraction, Y =  0.687
Area-averaged low loss fraction, Yb =  0.313
User entry of time of concentration  =   0.137 (hours)
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Watershed area =       4.40(Ac.)
Catchment Lag time =   0.109 hours
Unit interval =   5.000 minutes
Unit interval percentage of lag time = 76.2009
Hydrograph baseflow =     0.00(CFS)
Average maximum watershed loss rate(Fm) =  0.205(In/Hr)
Average low loss rate fraction (Yb) = 0.313 (decimal)
VALLEY DEVELOPED S-Graph Selected
Computed peak 5-minute rainfall =  0.272(In)
Computed peak 30-minute rainfall =  0.556(In)
Specified peak 1-hour rainfall =  0.734(In)
Computed peak 3-hour rainfall =  1.258(In)
Specified peak 6-hour rainfall =  1.767(In)
Specified peak 24-hour rainfall =  3.190(In)


Rainfall depth area reduction factors:
Using a total area of       4.40(Ac.) (Ref: fig. E-4)

5-minute factor = 1.000     Adjusted rainfall =  0.272(In)
30-minute factor = 1.000    Adjusted rainfall =  0.556(In)
1-hour factor = 1.000       Adjusted rainfall =  0.734(In)
3-hour factor = 1.000       Adjusted rainfall =  1.258(In)
6-hour factor = 1.000       Adjusted rainfall =  1.767(In)
```

24-hour factor = 1.000  Adjusted rainfall =  3.190(In)

U n i t  H y d r o g r a p h

| Interval Number | 'S' Graph Mean values | Unit Hydrograph ((CFS)) |
|---|---|---|
| | (K = 53.21 (CFS)) | |
| 1 | 10.314 | 5.488 |
| 2 | 60.003 | 26.441 |
| 3 | 92.533 | 17.310 |
| 4 | 98.569 | 3.212 |
| 5 | 100.000 | 0.761 |

| Peak Unit Number | Adjusted mass rainfall (In) | Unit rainfall (In) |
|---|---|---|
| 1 | 0.2716 | 0.2716 |
| 2 | 0.3584 | 0.0868 |
| 3 | 0.4215 | 0.0631 |
| 4 | 0.4729 | 0.0514 |
| 5 | 0.5170 | 0.0441 |
| 6 | 0.5562 | 0.0391 |
| 7 | 0.5915 | 0.0354 |
| 8 | 0.6240 | 0.0325 |
| 9 | 0.6541 | 0.0301 |
| 10 | 0.6822 | 0.0282 |
| 11 | 0.7087 | 0.0265 |
| 12 | 0.7338 | 0.0251 |
| 13 | 0.7632 | 0.0294 |
| 14 | 0.7915 | 0.0283 |
| 15 | 0.8187 | 0.0272 |
| 16 | 0.8451 | 0.0263 |
| 17 | 0.8706 | 0.0255 |
| 18 | 0.8953 | 0.0248 |
| 19 | 0.9194 | 0.0241 |
| 20 | 0.9428 | 0.0234 |
| 21 | 0.9657 | 0.0228 |
| 22 | 0.9879 | 0.0223 |
| 23 | 1.0097 | 0.0218 |
| 24 | 1.0310 | 0.0213 |
| 25 | 1.0519 | 0.0209 |
| 26 | 1.0723 | 0.0204 |
| 27 | 1.0923 | 0.0200 |
| 28 | 1.1120 | 0.0197 |
| 29 | 1.1313 | 0.0193 |
| 30 | 1.1503 | 0.0190 |
| 31 | 1.1689 | 0.0187 |
| 32 | 1.1873 | 0.0183 |
| 33 | 1.2053 | 0.0181 |
| 34 | 1.2231 | 0.0178 |

| | | |
|---|---|---|
| 35 | 1.2406 | 0.0175 |
| 36 | 1.2579 | 0.0173 |
| 37 | 1.2749 | 0.0170 |
| 38 | 1.2917 | 0.0168 |
| 39 | 1.3082 | 0.0166 |
| 40 | 1.3246 | 0.0163 |
| 41 | 1.3407 | 0.0161 |
| 42 | 1.3567 | 0.0159 |
| 43 | 1.3724 | 0.0157 |
| 44 | 1.3880 | 0.0156 |
| 45 | 1.4033 | 0.0154 |
| 46 | 1.4185 | 0.0152 |
| 47 | 1.4336 | 0.0150 |
| 48 | 1.4485 | 0.0149 |
| 49 | 1.4632 | 0.0147 |
| 50 | 1.4778 | 0.0146 |
| 51 | 1.4922 | 0.0144 |
| 52 | 1.5064 | 0.0143 |
| 53 | 1.5206 | 0.0141 |
| 54 | 1.5346 | 0.0140 |
| 55 | 1.5485 | 0.0139 |
| 56 | 1.5622 | 0.0137 |
| 57 | 1.5758 | 0.0136 |
| 58 | 1.5893 | 0.0135 |
| 59 | 1.6027 | 0.0134 |
| 60 | 1.6160 | 0.0133 |
| 61 | 1.6291 | 0.0132 |
| 62 | 1.6422 | 0.0130 |
| 63 | 1.6551 | 0.0129 |
| 64 | 1.6679 | 0.0128 |
| 65 | 1.6806 | 0.0127 |
| 66 | 1.6933 | 0.0126 |
| 67 | 1.7058 | 0.0125 |
| 68 | 1.7182 | 0.0124 |
| 69 | 1.7306 | 0.0123 |
| 70 | 1.7428 | 0.0123 |
| 71 | 1.7550 | 0.0122 |
| 72 | 1.7671 | 0.0121 |
| 73 | 1.7775 | 0.0104 |
| 74 | 1.7878 | 0.0103 |
| 75 | 1.7981 | 0.0103 |
| 76 | 1.8083 | 0.0102 |
| 77 | 1.8184 | 0.0101 |
| 78 | 1.8284 | 0.0100 |
| 79 | 1.8383 | 0.0099 |
| 80 | 1.8482 | 0.0099 |
| 81 | 1.8580 | 0.0098 |
| 82 | 1.8678 | 0.0097 |
| 83 | 1.8774 | 0.0097 |
| 84 | 1.8870 | 0.0096 |
| 85 | 1.8966 | 0.0095 |
| 86 | 1.9060 | 0.0095 |

| | | |
|---|---|---|
| 87 | 1.9154 | 0.0094 |
| 88 | 1.9248 | 0.0093 |
| 89 | 1.9341 | 0.0093 |
| 90 | 1.9433 | 0.0092 |
| 91 | 1.9525 | 0.0092 |
| 92 | 1.9616 | 0.0091 |
| 93 | 1.9706 | 0.0091 |
| 94 | 1.9796 | 0.0090 |
| 95 | 1.9886 | 0.0089 |
| 96 | 1.9975 | 0.0089 |
| 97 | 2.0063 | 0.0088 |
| 98 | 2.0151 | 0.0088 |
| 99 | 2.0238 | 0.0087 |
| 100 | 2.0325 | 0.0087 |
| 101 | 2.0412 | 0.0086 |
| 102 | 2.0497 | 0.0086 |
| 103 | 2.0583 | 0.0085 |
| 104 | 2.0668 | 0.0085 |
| 105 | 2.0752 | 0.0084 |
| 106 | 2.0836 | 0.0084 |
| 107 | 2.0920 | 0.0084 |
| 108 | 2.1003 | 0.0083 |
| 109 | 2.1085 | 0.0083 |
| 110 | 2.1167 | 0.0082 |
| 111 | 2.1249 | 0.0082 |
| 112 | 2.1330 | 0.0081 |
| 113 | 2.1411 | 0.0081 |
| 114 | 2.1492 | 0.0081 |
| 115 | 2.1572 | 0.0080 |
| 116 | 2.1652 | 0.0080 |
| 117 | 2.1731 | 0.0079 |
| 118 | 2.1810 | 0.0079 |
| 119 | 2.1889 | 0.0079 |
| 120 | 2.1967 | 0.0078 |
| 121 | 2.2045 | 0.0078 |
| 122 | 2.2122 | 0.0077 |
| 123 | 2.2199 | 0.0077 |
| 124 | 2.2276 | 0.0077 |
| 125 | 2.2352 | 0.0076 |
| 126 | 2.2428 | 0.0076 |
| 127 | 2.2504 | 0.0076 |
| 128 | 2.2579 | 0.0075 |
| 129 | 2.2654 | 0.0075 |
| 130 | 2.2729 | 0.0075 |
| 131 | 2.2803 | 0.0074 |
| 132 | 2.2877 | 0.0074 |
| 133 | 2.2951 | 0.0074 |
| 134 | 2.3024 | 0.0073 |
| 135 | 2.3097 | 0.0073 |
| 136 | 2.3170 | 0.0073 |
| 137 | 2.3242 | 0.0072 |
| 138 | 2.3314 | 0.0072 |

| | | |
|---|---|---|
| 139 | 2.3386 | 0.0072 |
| 140 | 2.3458 | 0.0072 |
| 141 | 2.3529 | 0.0071 |
| 142 | 2.3600 | 0.0071 |
| 143 | 2.3670 | 0.0071 |
| 144 | 2.3741 | 0.0070 |
| 145 | 2.3811 | 0.0070 |
| 146 | 2.3881 | 0.0070 |
| 147 | 2.3950 | 0.0070 |
| 148 | 2.4020 | 0.0069 |
| 149 | 2.4089 | 0.0069 |
| 150 | 2.4157 | 0.0069 |
| 151 | 2.4226 | 0.0068 |
| 152 | 2.4294 | 0.0068 |
| 153 | 2.4362 | 0.0068 |
| 154 | 2.4430 | 0.0068 |
| 155 | 2.4497 | 0.0067 |
| 156 | 2.4564 | 0.0067 |
| 157 | 2.4631 | 0.0067 |
| 158 | 2.4698 | 0.0067 |
| 159 | 2.4764 | 0.0066 |
| 160 | 2.4831 | 0.0066 |
| 161 | 2.4897 | 0.0066 |
| 162 | 2.4962 | 0.0066 |
| 163 | 2.5028 | 0.0066 |
| 164 | 2.5093 | 0.0065 |
| 165 | 2.5158 | 0.0065 |
| 166 | 2.5223 | 0.0065 |
| 167 | 2.5288 | 0.0065 |
| 168 | 2.5352 | 0.0064 |
| 169 | 2.5416 | 0.0064 |
| 170 | 2.5480 | 0.0064 |
| 171 | 2.5544 | 0.0064 |
| 172 | 2.5608 | 0.0064 |
| 173 | 2.5671 | 0.0063 |
| 174 | 2.5734 | 0.0063 |
| 175 | 2.5797 | 0.0063 |
| 176 | 2.5860 | 0.0063 |
| 177 | 2.5922 | 0.0062 |
| 178 | 2.5984 | 0.0062 |
| 179 | 2.6046 | 0.0062 |
| 180 | 2.6108 | 0.0062 |
| 181 | 2.6170 | 0.0062 |
| 182 | 2.6232 | 0.0061 |
| 183 | 2.6293 | 0.0061 |
| 184 | 2.6354 | 0.0061 |
| 185 | 2.6415 | 0.0061 |
| 186 | 2.6476 | 0.0061 |
| 187 | 2.6536 | 0.0061 |
| 188 | 2.6596 | 0.0060 |
| 189 | 2.6657 | 0.0060 |
| 190 | 2.6717 | 0.0060 |

| | | |
|---|---|---|
| 191 | 2.6776 | 0.0060 |
| 192 | 2.6836 | 0.0060 |
| 193 | 2.6896 | 0.0059 |
| 194 | 2.6955 | 0.0059 |
| 195 | 2.7014 | 0.0059 |
| 196 | 2.7073 | 0.0059 |
| 197 | 2.7132 | 0.0059 |
| 198 | 2.7190 | 0.0059 |
| 199 | 2.7249 | 0.0058 |
| 200 | 2.7307 | 0.0058 |
| 201 | 2.7365 | 0.0058 |
| 202 | 2.7423 | 0.0058 |
| 203 | 2.7481 | 0.0058 |
| 204 | 2.7538 | 0.0058 |
| 205 | 2.7596 | 0.0057 |
| 206 | 2.7653 | 0.0057 |
| 207 | 2.7710 | 0.0057 |
| 208 | 2.7767 | 0.0057 |
| 209 | 2.7824 | 0.0057 |
| 210 | 2.7880 | 0.0057 |
| 211 | 2.7937 | 0.0056 |
| 212 | 2.7993 | 0.0056 |
| 213 | 2.8049 | 0.0056 |
| 214 | 2.8105 | 0.0056 |
| 215 | 2.8161 | 0.0056 |
| 216 | 2.8217 | 0.0056 |
| 217 | 2.8273 | 0.0056 |
| 218 | 2.8328 | 0.0055 |
| 219 | 2.8383 | 0.0055 |
| 220 | 2.8438 | 0.0055 |
| 221 | 2.8493 | 0.0055 |
| 222 | 2.8548 | 0.0055 |
| 223 | 2.8603 | 0.0055 |
| 224 | 2.8658 | 0.0055 |
| 225 | 2.8712 | 0.0054 |
| 226 | 2.8766 | 0.0054 |
| 227 | 2.8820 | 0.0054 |
| 228 | 2.8874 | 0.0054 |
| 229 | 2.8928 | 0.0054 |
| 230 | 2.8982 | 0.0054 |
| 231 | 2.9036 | 0.0054 |
| 232 | 2.9089 | 0.0053 |
| 233 | 2.9142 | 0.0053 |
| 234 | 2.9196 | 0.0053 |
| 235 | 2.9249 | 0.0053 |
| 236 | 2.9302 | 0.0053 |
| 237 | 2.9355 | 0.0053 |
| 238 | 2.9407 | 0.0053 |
| 239 | 2.9460 | 0.0053 |
| 240 | 2.9512 | 0.0052 |
| 241 | 2.9565 | 0.0052 |
| 242 | 2.9617 | 0.0052 |

| | | |
|---|---|---|
| 243 | 2.9669 | 0.0052 |
| 244 | 2.9721 | 0.0052 |
| 245 | 2.9773 | 0.0052 |
| 246 | 2.9824 | 0.0052 |
| 247 | 2.9876 | 0.0052 |
| 248 | 2.9927 | 0.0051 |
| 249 | 2.9979 | 0.0051 |
| 250 | 3.0030 | 0.0051 |
| 251 | 3.0081 | 0.0051 |
| 252 | 3.0132 | 0.0051 |
| 253 | 3.0183 | 0.0051 |
| 254 | 3.0234 | 0.0051 |
| 255 | 3.0284 | 0.0051 |
| 256 | 3.0335 | 0.0051 |
| 257 | 3.0385 | 0.0050 |
| 258 | 3.0436 | 0.0050 |
| 259 | 3.0486 | 0.0050 |
| 260 | 3.0536 | 0.0050 |
| 261 | 3.0586 | 0.0050 |
| 262 | 3.0636 | 0.0050 |
| 263 | 3.0686 | 0.0050 |
| 264 | 3.0735 | 0.0050 |
| 265 | 3.0785 | 0.0050 |
| 266 | 3.0834 | 0.0049 |
| 267 | 3.0884 | 0.0049 |
| 268 | 3.0933 | 0.0049 |
| 269 | 3.0982 | 0.0049 |
| 270 | 3.1031 | 0.0049 |
| 271 | 3.1080 | 0.0049 |
| 272 | 3.1129 | 0.0049 |
| 273 | 3.1177 | 0.0049 |
| 274 | 3.1226 | 0.0049 |
| 275 | 3.1274 | 0.0048 |
| 276 | 3.1323 | 0.0048 |
| 277 | 3.1371 | 0.0048 |
| 278 | 3.1419 | 0.0048 |
| 279 | 3.1467 | 0.0048 |
| 280 | 3.1515 | 0.0048 |
| 281 | 3.1563 | 0.0048 |
| 282 | 3.1611 | 0.0048 |
| 283 | 3.1659 | 0.0048 |
| 284 | 3.1706 | 0.0048 |
| 285 | 3.1754 | 0.0048 |
| 286 | 3.1801 | 0.0047 |
| 287 | 3.1849 | 0.0047 |
| 288 | 3.1896 | 0.0047 |

| Unit Period (number) | Unit Rainfall (In) | Unit Soil-Loss (In) | Effective Rainfall (In) |
|---|---|---|---|
| 1 | 0.0047 | 0.0015 | 0.0032 |

| | | | |
|---|---|---|---|
| 2 | 0.0047 | 0.0015 | 0.0032 |
| 3 | 0.0048 | 0.0015 | 0.0033 |
| 4 | 0.0048 | 0.0015 | 0.0033 |
| 5 | 0.0048 | 0.0015 | 0.0033 |
| 6 | 0.0048 | 0.0015 | 0.0033 |
| 7 | 0.0048 | 0.0015 | 0.0033 |
| 8 | 0.0048 | 0.0015 | 0.0033 |
| 9 | 0.0048 | 0.0015 | 0.0033 |
| 10 | 0.0048 | 0.0015 | 0.0033 |
| 11 | 0.0049 | 0.0015 | 0.0033 |
| 12 | 0.0049 | 0.0015 | 0.0034 |
| 13 | 0.0049 | 0.0015 | 0.0034 |
| 14 | 0.0049 | 0.0015 | 0.0034 |
| 15 | 0.0049 | 0.0015 | 0.0034 |
| 16 | 0.0049 | 0.0015 | 0.0034 |
| 17 | 0.0050 | 0.0016 | 0.0034 |
| 18 | 0.0050 | 0.0016 | 0.0034 |
| 19 | 0.0050 | 0.0016 | 0.0034 |
| 20 | 0.0050 | 0.0016 | 0.0034 |
| 21 | 0.0050 | 0.0016 | 0.0035 |
| 22 | 0.0050 | 0.0016 | 0.0035 |
| 23 | 0.0051 | 0.0016 | 0.0035 |
| 24 | 0.0051 | 0.0016 | 0.0035 |
| 25 | 0.0051 | 0.0016 | 0.0035 |
| 26 | 0.0051 | 0.0016 | 0.0035 |
| 27 | 0.0051 | 0.0016 | 0.0035 |
| 28 | 0.0051 | 0.0016 | 0.0035 |
| 29 | 0.0052 | 0.0016 | 0.0035 |
| 30 | 0.0052 | 0.0016 | 0.0036 |
| 31 | 0.0052 | 0.0016 | 0.0036 |
| 32 | 0.0052 | 0.0016 | 0.0036 |
| 33 | 0.0052 | 0.0016 | 0.0036 |
| 34 | 0.0053 | 0.0016 | 0.0036 |
| 35 | 0.0053 | 0.0017 | 0.0036 |
| 36 | 0.0053 | 0.0017 | 0.0036 |
| 37 | 0.0053 | 0.0017 | 0.0037 |
| 38 | 0.0053 | 0.0017 | 0.0037 |
| 39 | 0.0054 | 0.0017 | 0.0037 |
| 40 | 0.0054 | 0.0017 | 0.0037 |
| 41 | 0.0054 | 0.0017 | 0.0037 |
| 42 | 0.0054 | 0.0017 | 0.0037 |
| 43 | 0.0054 | 0.0017 | 0.0037 |
| 44 | 0.0055 | 0.0017 | 0.0037 |
| 45 | 0.0055 | 0.0017 | 0.0038 |
| 46 | 0.0055 | 0.0017 | 0.0038 |
| 47 | 0.0055 | 0.0017 | 0.0038 |
| 48 | 0.0055 | 0.0017 | 0.0038 |
| 49 | 0.0056 | 0.0017 | 0.0038 |
| 50 | 0.0056 | 0.0018 | 0.0038 |
| 51 | 0.0056 | 0.0018 | 0.0039 |
| 52 | 0.0056 | 0.0018 | 0.0039 |
| 53 | 0.0057 | 0.0018 | 0.0039 |

| | | | |
|---|---|---|---|
| 54 | 0.0057 | 0.0018 | 0.0039 |
| 55 | 0.0057 | 0.0018 | 0.0039 |
| 56 | 0.0057 | 0.0018 | 0.0039 |
| 57 | 0.0058 | 0.0018 | 0.0040 |
| 58 | 0.0058 | 0.0018 | 0.0040 |
| 59 | 0.0058 | 0.0018 | 0.0040 |
| 60 | 0.0058 | 0.0018 | 0.0040 |
| 61 | 0.0059 | 0.0018 | 0.0040 |
| 62 | 0.0059 | 0.0018 | 0.0040 |
| 63 | 0.0059 | 0.0019 | 0.0041 |
| 64 | 0.0059 | 0.0019 | 0.0041 |
| 65 | 0.0060 | 0.0019 | 0.0041 |
| 66 | 0.0060 | 0.0019 | 0.0041 |
| 67 | 0.0060 | 0.0019 | 0.0041 |
| 68 | 0.0060 | 0.0019 | 0.0041 |
| 69 | 0.0061 | 0.0019 | 0.0042 |
| 70 | 0.0061 | 0.0019 | 0.0042 |
| 71 | 0.0061 | 0.0019 | 0.0042 |
| 72 | 0.0061 | 0.0019 | 0.0042 |
| 73 | 0.0062 | 0.0019 | 0.0042 |
| 74 | 0.0062 | 0.0019 | 0.0043 |
| 75 | 0.0062 | 0.0020 | 0.0043 |
| 76 | 0.0063 | 0.0020 | 0.0043 |
| 77 | 0.0063 | 0.0020 | 0.0043 |
| 78 | 0.0063 | 0.0020 | 0.0043 |
| 79 | 0.0064 | 0.0020 | 0.0044 |
| 80 | 0.0064 | 0.0020 | 0.0044 |
| 81 | 0.0064 | 0.0020 | 0.0044 |
| 82 | 0.0065 | 0.0020 | 0.0044 |
| 83 | 0.0065 | 0.0020 | 0.0045 |
| 84 | 0.0065 | 0.0020 | 0.0045 |
| 85 | 0.0066 | 0.0021 | 0.0045 |
| 86 | 0.0066 | 0.0021 | 0.0045 |
| 87 | 0.0066 | 0.0021 | 0.0046 |
| 88 | 0.0067 | 0.0021 | 0.0046 |
| 89 | 0.0067 | 0.0021 | 0.0046 |
| 90 | 0.0067 | 0.0021 | 0.0046 |
| 91 | 0.0068 | 0.0021 | 0.0047 |
| 92 | 0.0068 | 0.0021 | 0.0047 |
| 93 | 0.0069 | 0.0022 | 0.0047 |
| 94 | 0.0069 | 0.0022 | 0.0047 |
| 95 | 0.0070 | 0.0022 | 0.0048 |
| 96 | 0.0070 | 0.0022 | 0.0048 |
| 97 | 0.0070 | 0.0022 | 0.0048 |
| 98 | 0.0071 | 0.0022 | 0.0049 |
| 99 | 0.0071 | 0.0022 | 0.0049 |
| 100 | 0.0072 | 0.0022 | 0.0049 |
| 101 | 0.0072 | 0.0023 | 0.0050 |
| 102 | 0.0072 | 0.0023 | 0.0050 |
| 103 | 0.0073 | 0.0023 | 0.0050 |
| 104 | 0.0073 | 0.0023 | 0.0050 |
| 105 | 0.0074 | 0.0023 | 0.0051 |

| | | | |
|---|---|---|---|
| 106 | 0.0074 | 0.0023 | 0.0051 |
| 107 | 0.0075 | 0.0024 | 0.0051 |
| 108 | 0.0075 | 0.0024 | 0.0052 |
| 109 | 0.0076 | 0.0024 | 0.0052 |
| 110 | 0.0076 | 0.0024 | 0.0052 |
| 111 | 0.0077 | 0.0024 | 0.0053 |
| 112 | 0.0077 | 0.0024 | 0.0053 |
| 113 | 0.0078 | 0.0025 | 0.0054 |
| 114 | 0.0079 | 0.0025 | 0.0054 |
| 115 | 0.0079 | 0.0025 | 0.0054 |
| 116 | 0.0080 | 0.0025 | 0.0055 |
| 117 | 0.0081 | 0.0025 | 0.0055 |
| 118 | 0.0081 | 0.0025 | 0.0056 |
| 119 | 0.0082 | 0.0026 | 0.0056 |
| 120 | 0.0082 | 0.0026 | 0.0056 |
| 121 | 0.0083 | 0.0026 | 0.0057 |
| 122 | 0.0084 | 0.0026 | 0.0057 |
| 123 | 0.0084 | 0.0026 | 0.0058 |
| 124 | 0.0085 | 0.0027 | 0.0058 |
| 125 | 0.0086 | 0.0027 | 0.0059 |
| 126 | 0.0086 | 0.0027 | 0.0059 |
| 127 | 0.0087 | 0.0027 | 0.0060 |
| 128 | 0.0088 | 0.0028 | 0.0060 |
| 129 | 0.0089 | 0.0028 | 0.0061 |
| 130 | 0.0089 | 0.0028 | 0.0061 |
| 131 | 0.0091 | 0.0028 | 0.0062 |
| 132 | 0.0091 | 0.0029 | 0.0063 |
| 133 | 0.0092 | 0.0029 | 0.0063 |
| 134 | 0.0093 | 0.0029 | 0.0064 |
| 135 | 0.0094 | 0.0029 | 0.0065 |
| 136 | 0.0095 | 0.0030 | 0.0065 |
| 137 | 0.0096 | 0.0030 | 0.0066 |
| 138 | 0.0097 | 0.0030 | 0.0066 |
| 139 | 0.0098 | 0.0031 | 0.0067 |
| 140 | 0.0099 | 0.0031 | 0.0068 |
| 141 | 0.0100 | 0.0031 | 0.0069 |
| 142 | 0.0101 | 0.0032 | 0.0069 |
| 143 | 0.0103 | 0.0032 | 0.0070 |
| 144 | 0.0103 | 0.0032 | 0.0071 |
| 145 | 0.0121 | 0.0038 | 0.0083 |
| 146 | 0.0122 | 0.0038 | 0.0084 |
| 147 | 0.0123 | 0.0039 | 0.0085 |
| 148 | 0.0124 | 0.0039 | 0.0085 |
| 149 | 0.0126 | 0.0040 | 0.0087 |
| 150 | 0.0127 | 0.0040 | 0.0087 |
| 151 | 0.0129 | 0.0041 | 0.0089 |
| 152 | 0.0130 | 0.0041 | 0.0090 |
| 153 | 0.0133 | 0.0042 | 0.0091 |
| 154 | 0.0134 | 0.0042 | 0.0092 |
| 155 | 0.0136 | 0.0043 | 0.0093 |
| 156 | 0.0137 | 0.0043 | 0.0094 |
| 157 | 0.0140 | 0.0044 | 0.0096 |

| | | | |
|---|---|---|---|
| 158 | 0.0141 | 0.0044 | 0.0097 |
| 159 | 0.0144 | 0.0045 | 0.0099 |
| 160 | 0.0146 | 0.0046 | 0.0100 |
| 161 | 0.0149 | 0.0047 | 0.0102 |
| 162 | 0.0150 | 0.0047 | 0.0103 |
| 163 | 0.0154 | 0.0048 | 0.0106 |
| 164 | 0.0156 | 0.0049 | 0.0107 |
| 165 | 0.0159 | 0.0050 | 0.0109 |
| 166 | 0.0161 | 0.0051 | 0.0111 |
| 167 | 0.0166 | 0.0052 | 0.0114 |
| 168 | 0.0168 | 0.0053 | 0.0115 |
| 169 | 0.0173 | 0.0054 | 0.0119 |
| 170 | 0.0175 | 0.0055 | 0.0120 |
| 171 | 0.0181 | 0.0057 | 0.0124 |
| 172 | 0.0183 | 0.0058 | 0.0126 |
| 173 | 0.0190 | 0.0059 | 0.0130 |
| 174 | 0.0193 | 0.0061 | 0.0133 |
| 175 | 0.0200 | 0.0063 | 0.0138 |
| 176 | 0.0204 | 0.0064 | 0.0140 |
| 177 | 0.0213 | 0.0067 | 0.0146 |
| 178 | 0.0218 | 0.0068 | 0.0150 |
| 179 | 0.0228 | 0.0072 | 0.0157 |
| 180 | 0.0234 | 0.0073 | 0.0161 |
| 181 | 0.0248 | 0.0078 | 0.0170 |
| 182 | 0.0255 | 0.0080 | 0.0175 |
| 183 | 0.0272 | 0.0085 | 0.0187 |
| 184 | 0.0283 | 0.0089 | 0.0194 |
| 185 | 0.0251 | 0.0079 | 0.0172 |
| 186 | 0.0265 | 0.0083 | 0.0182 |
| 187 | 0.0301 | 0.0094 | 0.0207 |
| 188 | 0.0325 | 0.0102 | 0.0223 |
| 189 | 0.0391 | 0.0123 | 0.0269 |
| 190 | 0.0441 | 0.0138 | 0.0303 |
| 191 | 0.0631 | 0.0171 | 0.0460 |
| 192 | 0.0868 | 0.0171 | 0.0697 |
| 193 | 0.2716 | 0.0171 | 0.2545 |
| 194 | 0.0514 | 0.0161 | 0.0353 |
| 195 | 0.0354 | 0.0111 | 0.0243 |
| 196 | 0.0282 | 0.0088 | 0.0193 |
| 197 | 0.0294 | 0.0092 | 0.0202 |
| 198 | 0.0263 | 0.0083 | 0.0181 |
| 199 | 0.0241 | 0.0075 | 0.0165 |
| 200 | 0.0223 | 0.0070 | 0.0153 |
| 201 | 0.0209 | 0.0065 | 0.0143 |
| 202 | 0.0197 | 0.0062 | 0.0135 |
| 203 | 0.0187 | 0.0058 | 0.0128 |
| 204 | 0.0178 | 0.0056 | 0.0122 |
| 205 | 0.0170 | 0.0053 | 0.0117 |
| 206 | 0.0163 | 0.0051 | 0.0112 |
| 207 | 0.0157 | 0.0049 | 0.0108 |
| 208 | 0.0152 | 0.0048 | 0.0104 |
| 209 | 0.0147 | 0.0046 | 0.0101 |

| | | | |
|---|---|---|---|
| 210 | 0.0143 | 0.0045 | 0.0098 |
| 211 | 0.0139 | 0.0043 | 0.0095 |
| 212 | 0.0135 | 0.0042 | 0.0093 |
| 213 | 0.0132 | 0.0041 | 0.0090 |
| 214 | 0.0128 | 0.0040 | 0.0088 |
| 215 | 0.0125 | 0.0039 | 0.0086 |
| 216 | 0.0123 | 0.0038 | 0.0084 |
| 217 | 0.0104 | 0.0033 | 0.0071 |
| 218 | 0.0102 | 0.0032 | 0.0070 |
| 219 | 0.0099 | 0.0031 | 0.0068 |
| 220 | 0.0097 | 0.0031 | 0.0067 |
| 221 | 0.0095 | 0.0030 | 0.0065 |
| 222 | 0.0093 | 0.0029 | 0.0064 |
| 223 | 0.0092 | 0.0029 | 0.0063 |
| 224 | 0.0090 | 0.0028 | 0.0062 |
| 225 | 0.0088 | 0.0028 | 0.0061 |
| 226 | 0.0087 | 0.0027 | 0.0060 |
| 227 | 0.0085 | 0.0027 | 0.0059 |
| 228 | 0.0084 | 0.0026 | 0.0058 |
| 229 | 0.0083 | 0.0026 | 0.0057 |
| 230 | 0.0081 | 0.0025 | 0.0056 |
| 231 | 0.0080 | 0.0025 | 0.0055 |
| 232 | 0.0079 | 0.0025 | 0.0054 |
| 233 | 0.0078 | 0.0024 | 0.0053 |
| 234 | 0.0077 | 0.0024 | 0.0053 |
| 235 | 0.0076 | 0.0024 | 0.0052 |
| 236 | 0.0075 | 0.0023 | 0.0051 |
| 237 | 0.0074 | 0.0023 | 0.0051 |
| 238 | 0.0073 | 0.0023 | 0.0050 |
| 239 | 0.0072 | 0.0023 | 0.0049 |
| 240 | 0.0071 | 0.0022 | 0.0049 |
| 241 | 0.0070 | 0.0022 | 0.0048 |
| 242 | 0.0069 | 0.0022 | 0.0048 |
| 243 | 0.0068 | 0.0021 | 0.0047 |
| 244 | 0.0068 | 0.0021 | 0.0046 |
| 245 | 0.0067 | 0.0021 | 0.0046 |
| 246 | 0.0066 | 0.0021 | 0.0045 |
| 247 | 0.0066 | 0.0021 | 0.0045 |
| 248 | 0.0065 | 0.0020 | 0.0045 |
| 249 | 0.0064 | 0.0020 | 0.0044 |
| 250 | 0.0064 | 0.0020 | 0.0044 |
| 251 | 0.0063 | 0.0020 | 0.0043 |
| 252 | 0.0062 | 0.0020 | 0.0043 |
| 253 | 0.0062 | 0.0019 | 0.0042 |
| 254 | 0.0061 | 0.0019 | 0.0042 |
| 255 | 0.0061 | 0.0019 | 0.0042 |
| 256 | 0.0060 | 0.0019 | 0.0041 |
| 257 | 0.0059 | 0.0019 | 0.0041 |
| 258 | 0.0059 | 0.0018 | 0.0040 |
| 259 | 0.0058 | 0.0018 | 0.0040 |
| 260 | 0.0058 | 0.0018 | 0.0040 |
| 261 | 0.0057 | 0.0018 | 0.0039 |

| | | | |
|---|---|---|---|
| 262 | 0.0057 | 0.0018 | 0.0039 |
| 263 | 0.0056 | 0.0018 | 0.0039 |
| 264 | 0.0056 | 0.0018 | 0.0038 |
| 265 | 0.0056 | 0.0017 | 0.0038 |
| 266 | 0.0055 | 0.0017 | 0.0038 |
| 267 | 0.0055 | 0.0017 | 0.0038 |
| 268 | 0.0054 | 0.0017 | 0.0037 |
| 269 | 0.0054 | 0.0017 | 0.0037 |
| 270 | 0.0053 | 0.0017 | 0.0037 |
| 271 | 0.0053 | 0.0017 | 0.0036 |
| 272 | 0.0053 | 0.0017 | 0.0036 |
| 273 | 0.0052 | 0.0016 | 0.0036 |
| 274 | 0.0052 | 0.0016 | 0.0036 |
| 275 | 0.0052 | 0.0016 | 0.0035 |
| 276 | 0.0051 | 0.0016 | 0.0035 |
| 277 | 0.0051 | 0.0016 | 0.0035 |
| 278 | 0.0051 | 0.0016 | 0.0035 |
| 279 | 0.0050 | 0.0016 | 0.0034 |
| 280 | 0.0050 | 0.0016 | 0.0034 |
| 281 | 0.0050 | 0.0016 | 0.0034 |
| 282 | 0.0049 | 0.0015 | 0.0034 |
| 283 | 0.0049 | 0.0015 | 0.0034 |
| 284 | 0.0049 | 0.0015 | 0.0033 |
| 285 | 0.0048 | 0.0015 | 0.0033 |
| 286 | 0.0048 | 0.0015 | 0.0033 |
| 287 | 0.0048 | 0.0015 | 0.0033 |
| 288 | 0.0047 | 0.0015 | 0.0033 |

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Total soil rain loss = 0.92(In)
Total effective rainfall = 2.27(In)
Peak flow rate in flood hydrograph = 8.30(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

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Hydrograph in 5 Minute intervals ((CFS))

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| Time(h+m) | Volume Ac.Ft | Q(CFS) | 0 | 2.5 | 5.0 | 7.5 | 10.0 |
|---|---|---|---|---|---|---|---|
| 0+ 5 | 0.0001 | 0.02 | Q | \| | \| | \| | \| |
| 0+10 | 0.0008 | 0.10 | Q | \| | \| | \| | \| |
| 0+15 | 0.0019 | 0.16 | Q | \| | \| | \| | \| |
| 0+20 | 0.0031 | 0.17 | Q | \| | \| | \| | \| |
| 0+25 | 0.0043 | 0.17 | Q | \| | \| | \| | \| |
| 0+30 | 0.0055 | 0.17 | Q | \| | \| | \| | \| |
| 0+35 | 0.0067 | 0.17 | Q | \| | \| | \| | \| |
| 0+40 | 0.0079 | 0.18 | Q | \| | \| | \| | \| |
| 0+45 | 0.0091 | 0.18 | Q | \| | \| | \| | \| |
| 0+50 | 0.0104 | 0.18 | Q | \| | \| | \| | \| |

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 0+55 | 0.0116 | 0.18 | Q | \| | \| | \| | \| |
| 1+ 0 | 0.0128 | 0.18 | Q | \| | \| | \| | \| |
| 1+ 5 | 0.0140 | 0.18 | Q | \| | \| | \| | \| |
| 1+10 | 0.0153 | 0.18 | Q | \| | \| | \| | \| |
| 1+15 | 0.0165 | 0.18 | Q | \| | \| | \| | \| |
| 1+20 | 0.0177 | 0.18 | Q | \| | \| | \| | \| |
| 1+25 | 0.0190 | 0.18 | Q | \| | \| | \| | \| |
| 1+30 | 0.0202 | 0.18 | Q | \| | \| | \| | \| |
| 1+35 | 0.0215 | 0.18 | QV | \| | \| | \| | \| |
| 1+40 | 0.0227 | 0.18 | QV | \| | \| | \| | \| |
| 1+45 | 0.0240 | 0.18 | QV | \| | \| | \| | \| |
| 1+50 | 0.0252 | 0.18 | QV | \| | \| | \| | \| |
| 1+55 | 0.0265 | 0.18 | QV | \| | \| | \| | \| |
| 2+ 0 | 0.0278 | 0.18 | QV | \| | \| | \| | \| |
| 2+ 5 | 0.0291 | 0.19 | QV | \| | \| | \| | \| |
| 2+10 | 0.0303 | 0.19 | QV | \| | \| | \| | \| |
| 2+15 | 0.0316 | 0.19 | QV | \| | \| | \| | \| |
| 2+20 | 0.0329 | 0.19 | QV | \| | \| | \| | \| |
| 2+25 | 0.0342 | 0.19 | QV | \| | \| | \| | \| |
| 2+30 | 0.0355 | 0.19 | QV | \| | \| | \| | \| |
| 2+35 | 0.0368 | 0.19 | QV | \| | \| | \| | \| |
| 2+40 | 0.0381 | 0.19 | QV | \| | \| | \| | \| |
| 2+45 | 0.0394 | 0.19 | QV | \| | \| | \| | \| |
| 2+50 | 0.0407 | 0.19 | QV | \| | \| | \| | \| |
| 2+55 | 0.0421 | 0.19 | Q V | \| | \| | \| | \| |
| 3+ 0 | 0.0434 | 0.19 | Q V | \| | \| | \| | \| |
| 3+ 5 | 0.0447 | 0.19 | Q V | \| | \| | \| | \| |
| 3+10 | 0.0461 | 0.19 | Q V | \| | \| | \| | \| |
| 3+15 | 0.0474 | 0.19 | Q V | \| | \| | \| | \| |
| 3+20 | 0.0487 | 0.20 | Q V | \| | \| | \| | \| |
| 3+25 | 0.0501 | 0.20 | Q V | \| | \| | \| | \| |
| 3+30 | 0.0515 | 0.20 | Q V | \| | \| | \| | \| |
| 3+35 | 0.0528 | 0.20 | Q V | \| | \| | \| | \| |
| 3+40 | 0.0542 | 0.20 | Q V | \| | \| | \| | \| |
| 3+45 | 0.0556 | 0.20 | Q V | \| | \| | \| | \| |
| 3+50 | 0.0569 | 0.20 | Q V | \| | \| | \| | \| |
| 3+55 | 0.0583 | 0.20 | Q V | \| | \| | \| | \| |
| 4+ 0 | 0.0597 | 0.20 | Q V | \| | \| | \| | \| |
| 4+ 5 | 0.0611 | 0.20 | Q V | \| | \| | \| | \| |
| 4+10 | 0.0625 | 0.20 | Q  V | \| | \| | \| | \| |
| 4+15 | 0.0639 | 0.20 | Q  V | \| | \| | \| | \| |
| 4+20 | 0.0653 | 0.20 | Q  V | \| | \| | \| | \| |
| 4+25 | 0.0667 | 0.21 | Q  V | \| | \| | \| | \| |
| 4+30 | 0.0681 | 0.21 | Q  V | \| | \| | \| | \| |
| 4+35 | 0.0696 | 0.21 | Q  V | \| | \| | \| | \| |
| 4+40 | 0.0710 | 0.21 | Q  V | \| | \| | \| | \| |
| 4+45 | 0.0724 | 0.21 | Q  V | \| | \| | \| | \| |
| 4+50 | 0.0739 | 0.21 | Q  V | \| | \| | \| | \| |
| 4+55 | 0.0753 | 0.21 | Q  V | \| | \| | \| | \| |
| 5+ 0 | 0.0768 | 0.21 | Q  V | \| | \| | \| | \| |
| 5+ 5 | 0.0783 | 0.21 | Q  V | \| | \| | \| | \| |
| 5+10 | 0.0797 | 0.21 | Q  V | \| | \| | \| | \| |

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5+15       0.0812      0.21  Q  V      |          |          |          |
5+20       0.0827      0.22  Q  V      |          |          |          |
5+25       0.0842      0.22  Q   V     |          |          |          |
5+30       0.0857      0.22  Q   V     |          |          |          |
5+35       0.0872      0.22  Q   V     |          |          |          |
5+40       0.0887      0.22  Q   V     |          |          |          |
5+45       0.0902      0.22  Q   V     |          |          |          |
5+50       0.0917      0.22  Q   V     |          |          |          |
5+55       0.0933      0.22  Q   V     |          |          |          |
6+ 0       0.0948      0.22  Q   V     |          |          |          |
6+ 5       0.0964      0.22  Q   V     |          |          |          |
6+10       0.0979      0.23  Q   V     |          |          |          |
6+15       0.0995      0.23  Q   V     |          |          |          |
6+20       0.1010      0.23  Q   V     |          |          |          |
6+25       0.1026      0.23  Q   V     |          |          |          |
6+30       0.1042      0.23  Q    V    |          |          |          |
6+35       0.1058      0.23  Q    V    |          |          |          |
6+40       0.1074      0.23  Q    V    |          |          |          |
6+45       0.1090      0.23  Q    V    |          |          |          |
6+50       0.1106      0.23  Q    V    |          |          |          |
6+55       0.1122      0.24  Q    V    |          |          |          |
7+ 0       0.1139      0.24  Q    V    |          |          |          |
7+ 5       0.1155      0.24  Q    V    |          |          |          |
7+10       0.1172      0.24  Q    V    |          |          |          |
7+15       0.1188      0.24  Q    V    |          |          |          |
7+20       0.1205      0.24  Q    V    |          |          |          |
7+25       0.1222      0.24  Q    V    |          |          |          |
7+30       0.1238      0.24  Q    V    |          |          |          |
7+35       0.1255      0.25  Q     V   |          |          |          |
7+40       0.1272      0.25  Q     V   |          |          |          |
7+45       0.1290      0.25  Q     V   |          |          |          |
7+50       0.1307      0.25  |Q    V   |          |          |          |
7+55       0.1324      0.25  |Q    V   |          |          |          |
8+ 0       0.1342      0.25  |Q    V   |          |          |          |
8+ 5       0.1359      0.25  |Q    V   |          |          |          |
8+10       0.1377      0.26  |Q    V   |          |          |          |
8+15       0.1395      0.26  |Q    V   |          |          |          |
8+20       0.1412      0.26  |Q    V   |          |          |          |
8+25       0.1430      0.26  |Q    V   |          |          |          |
8+30       0.1448      0.26  |Q    V   |          |          |          |
8+35       0.1467      0.26  |Q     V  |          |          |          |
8+40       0.1485      0.27  |Q     V  |          |          |          |
8+45       0.1503      0.27  |Q     V  |          |          |          |
8+50       0.1522      0.27  |Q     V  |          |          |          |
8+55       0.1541      0.27  |Q     V  |          |          |          |
9+ 0       0.1559      0.27  |Q     V  |          |          |          |
9+ 5       0.1578      0.27  |Q     V  |          |          |          |
9+10       0.1597      0.28  |Q     V  |          |          |          |
9+15       0.1617      0.28  |Q     V  |          |          |          |
9+20       0.1636      0.28  |Q     V  |          |          |          |
9+25       0.1655      0.28  |Q     V  |          |          |          |
9+30       0.1675      0.28  |Q      V |          |          |          |
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 9+35       0.1695      0.29  |Q      V |          |          |          |
 9+40       0.1715      0.29  |Q      V |          |          |          |
 9+45       0.1735      0.29  |Q      V |          |          |          |
 9+50       0.1755      0.29  |Q      V |          |          |          |
 9+55       0.1775      0.30  |Q      V |          |          |          |
10+ 0       0.1796      0.30  |Q      V |          |          |          |
10+ 5       0.1816      0.30  |Q      V |          |          |          |
10+10       0.1837      0.30  |Q      V |          |          |          |
10+15       0.1858      0.30  |Q      V |          |          |          |
10+20       0.1879      0.31  |Q       V|          |          |          |
10+25       0.1900      0.31  |Q       V|          |          |          |
10+30       0.1922      0.31  |Q       V|          |          |          |
10+35       0.1944      0.31  |Q       V|          |          |          |
10+40       0.1965      0.32  |Q       V|          |          |          |
10+45       0.1988      0.32  |Q       V|          |          |          |
10+50       0.2010      0.32  |Q       V|          |          |          |
10+55       0.2032      0.33  |Q       V|          |          |          |
11+ 0       0.2055      0.33  |Q       V|          |          |          |
11+ 5       0.2078      0.33  |Q       V|          |          |          |
11+10       0.2101      0.34  |Q        V          |          |          |
11+15       0.2124      0.34  |Q        V          |          |          |
11+20       0.2148      0.34  |Q        V          |          |          |
11+25       0.2172      0.35  |Q        V          |          |          |
11+30       0.2196      0.35  |Q        V          |          |          |
11+35       0.2220      0.35  |Q        V          |          |          |
11+40       0.2244      0.36  |Q        V          |          |          |
11+45       0.2269      0.36  |Q        V          |          |          |
11+50       0.2294      0.36  |Q        |V          |          |          |
11+55       0.2320      0.37  |Q        |V          |          |          |
12+ 0       0.2345      0.37  |Q        |V          |          |          |
12+ 5       0.2372      0.38  |Q        |V          |          |          |
12+10       0.2400      0.42  |Q        |V          |          |          |
12+15       0.2430      0.44  |Q        |V          |          |          |
12+20       0.2461      0.45  |Q        |V          |          |          |
12+25       0.2492      0.45  |Q        |V          |          |          |
12+30       0.2524      0.46  |Q        | V         |          |          |
12+35       0.2556      0.46  |Q        | V         |          |          |
12+40       0.2588      0.47  |Q        | V         |          |          |
12+45       0.2621      0.48  |Q        | V         |          |          |
12+50       0.2654      0.48  |Q        | V         |          |          |
12+55       0.2688      0.49  |Q        | V         |          |          |
13+ 0       0.2722      0.49  |Q        |  V        |          |          |
13+ 5       0.2756      0.50  | Q       |  V        |          |          |
13+10       0.2791      0.51  | Q       |  V        |          |          |
13+15       0.2827      0.51  | Q       |  V        |          |          |
13+20       0.2863      0.52  | Q       |  V        |          |          |
13+25       0.2899      0.53  | Q       |  V        |          |          |
13+30       0.2936      0.54  | Q       |   V       |          |          |
13+35       0.2974      0.55  | Q       |   V       |          |          |
13+40       0.3012      0.56  | Q       |   V       |          |          |
13+45       0.3051      0.57  | Q       |   V       |          |          |
13+50       0.3091      0.58  | Q       |   V       |          |          |
```

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 13+55 | 0.3131 | 0.59 | Q | V | | | |
| 14+ 0 | 0.3173 | 0.60 | Q | V | | | |
| 14+ 5 | 0.3215 | 0.61 | Q | V | | | |
| 14+10 | 0.3258 | 0.62 | Q | V | | | |
| 14+15 | 0.3302 | 0.64 | Q | V | | | |
| 14+20 | 0.3346 | 0.65 | Q | V | | | |
| 14+25 | 0.3392 | 0.67 | Q | V | | | |
| 14+30 | 0.3440 | 0.68 | Q | V | | | |
| 14+35 | 0.3488 | 0.70 | Q | V | | | |
| 14+40 | 0.3537 | 0.72 | Q | V | | | |
| 14+45 | 0.3589 | 0.74 | Q | V | | | |
| 14+50 | 0.3641 | 0.77 | Q | V | | | |
| 14+55 | 0.3696 | 0.79 | Q | V | | | |
| 15+ 0 | 0.3752 | 0.82 | Q | V | | | |
| 15+ 5 | 0.3811 | 0.85 | Q | V | | | |
| 15+10 | 0.3872 | 0.89 | Q | V | | | |
| 15+15 | 0.3935 | 0.92 | Q | V | | | |
| 15+20 | 0.4002 | 0.97 | Q | V | | | |
| 15+25 | 0.4071 | 1.00 | Q | V | | | |
| 15+30 | 0.4137 | 0.96 | Q | V | | | |
| 15+35 | 0.4204 | 0.97 | Q | V | | | |
| 15+40 | 0.4277 | 1.05 | Q | V | | | |
| 15+45 | 0.4357 | 1.17 | Q | V | | | |
| 15+50 | 0.4449 | 1.34 | Q | V | | | |
| 15+55 | 0.4560 | 1.61 | Q | V | | | |
| 16+ 0 | 0.4714 | 2.23 | Q | V | | | |
| 16+ 5 | 0.5000 | 4.15 | Q | V | | | |
| 16+10 | 0.5571 | 8.30 | V | Q | | | |
| 16+15 | 0.5966 | 5.73 | Q | V | | | |
| 16+20 | 0.6120 | 2.23 | Q | V | | | |
| 16+25 | 0.6213 | 1.35 | Q | V | | | |
| 16+30 | 0.6286 | 1.07 | Q | V | | | |
| 16+35 | 0.6355 | 1.00 | Q | V | | | |
| 16+40 | 0.6418 | 0.91 | Q | V | | | |
| 16+45 | 0.6476 | 0.84 | Q | V | | | |
| 16+50 | 0.6530 | 0.78 | Q | V | | | |
| 16+55 | 0.6581 | 0.74 | Q | V | | | |
| 17+ 0 | 0.6629 | 0.70 | Q | V | | | |
| 17+ 5 | 0.6674 | 0.66 | Q | V | | | |
| 17+10 | 0.6718 | 0.63 | Q | V | | | |
| 17+15 | 0.6760 | 0.61 | Q | V | | | |
| 17+20 | 0.6800 | 0.58 | Q | V | | | |
| 17+25 | 0.6839 | 0.56 | Q | V | | | |
| 17+30 | 0.6876 | 0.54 | Q | V | | | |
| 17+35 | 0.6913 | 0.53 | Q | V | | | |
| 17+40 | 0.6948 | 0.51 | Q | V | | | |
| 17+45 | 0.6982 | 0.50 | Q | V | | | |
| 17+50 | 0.7016 | 0.49 | Q | V | | | |
| 17+55 | 0.7048 | 0.47 | Q | V | | | |
| 18+ 0 | 0.7080 | 0.46 | Q | V | | | |
| 18+ 5 | 0.7111 | 0.45 | Q | V | | | |
| 18+10 | 0.7139 | 0.41 | Q | V | | | |

```
18+15       0.7165      0.38  |Q        |         |         |   V     |
18+20       0.7190      0.37  |Q        |         |         |   V     |
18+25       0.7215      0.36  |Q        |         |         |   V     |
18+30       0.7239      0.35  |Q        |         |         |   V     |
18+35       0.7263      0.34  |Q        |         |         |   V     |
18+40       0.7286      0.34  |Q        |         |         |    V    |
18+45       0.7309      0.33  |Q        |         |         |    V    |
18+50       0.7332      0.33  |Q        |         |         |    V    |
18+55       0.7354      0.32  |Q        |         |         |    V    |
19+ 0       0.7375      0.31  |Q        |         |         |    V    |
19+ 5       0.7396      0.31  |Q        |         |         |    V    |
19+10       0.7417      0.30  |Q        |         |         |    V    |
19+15       0.7438      0.30  |Q        |         |         |    V    |
19+20       0.7458      0.29  |Q        |         |         |    V    |
19+25       0.7478      0.29  |Q        |         |         |    V    |
19+30       0.7498      0.29  |Q        |         |         |     V   |
19+35       0.7517      0.28  |Q        |         |         |     V   |
19+40       0.7536      0.28  |Q        |         |         |     V   |
19+45       0.7555      0.27  |Q        |         |         |     V   |
19+50       0.7574      0.27  |Q        |         |         |     V   |
19+55       0.7592      0.27  |Q        |         |         |     V   |
20+ 0       0.7611      0.26  |Q        |         |         |     V   |
20+ 5       0.7628      0.26  |Q        |         |         |     V   |
20+10       0.7646      0.26  |Q        |         |         |     V   |
20+15       0.7664      0.25  |Q        |         |         |     V   |
20+20       0.7681      0.25  |Q        |         |         |     V   |
20+25       0.7698      0.25  Q         |         |         |      V  |
20+30       0.7715      0.25  Q         |         |         |      V  |
20+35       0.7732      0.24  Q         |         |         |      V  |
20+40       0.7748      0.24  Q         |         |         |      V  |
20+45       0.7765      0.24  Q         |         |         |      V  |
20+50       0.7781      0.24  Q         |         |         |      V  |
20+55       0.7797      0.23  Q         |         |         |      V  |
21+ 0       0.7813      0.23  Q         |         |         |      V  |
21+ 5       0.7829      0.23  Q         |         |         |      V  |
21+10       0.7844      0.23  Q         |         |         |      V  |
21+15       0.7860      0.22  Q         |         |         |      V  |
21+20       0.7875      0.22  Q         |         |         |      V  |
21+25       0.7890      0.22  Q         |         |         |      V  |
21+30       0.7905      0.22  Q         |         |         |      V  |
21+35       0.7920      0.22  Q         |         |         |       V |
21+40       0.7935      0.21  Q         |         |         |       V |
21+45       0.7949      0.21  Q         |         |         |       V |
21+50       0.7964      0.21  Q         |         |         |       V |
21+55       0.7978      0.21  Q         |         |         |       V |
22+ 0       0.7992      0.21  Q         |         |         |       V |
22+ 5       0.8007      0.21  Q         |         |         |       V |
22+10       0.8021      0.20  Q         |         |         |       V |
22+15       0.8034      0.20  Q         |         |         |       V |
22+20       0.8048      0.20  Q         |         |         |       V |
22+25       0.8062      0.20  Q         |         |         |       V |
22+30       0.8076      0.20  Q         |         |         |       V |
```

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   22+35       0.8089      0.20  Q          |          |          |        V |
   22+40       0.8102      0.19  Q          |          |          |        V |
   22+45       0.8116      0.19  Q          |          |          |         V|
   22+50       0.8129      0.19  Q          |          |          |         V|
   22+55       0.8142      0.19  Q          |          |          |         V|
   23+ 0       0.8155      0.19  Q          |          |          |         V|
   23+ 5       0.8168      0.19  Q          |          |          |         V|
   23+10       0.8181      0.19  Q          |          |          |         V|
   23+15       0.8194      0.19  Q          |          |          |         V|
   23+20       0.8206      0.18  Q          |          |          |         V|
   23+25       0.8219      0.18  Q          |          |          |         V|
   23+30       0.8231      0.18  Q          |          |          |         V|
   23+35       0.8244      0.18  Q          |          |          |         V|
   23+40       0.8256      0.18  Q          |          |          |         V|
   23+45       0.8268      0.18  Q          |          |          |         V|
   23+50       0.8281      0.18  Q          |          |          |         V|
   23+55       0.8293      0.18  Q          |          |          |         V|
   24+ 0       0.8305      0.17  Q          |          |          |         V|
   24+ 5       0.8315      0.16  Q          |          |          |         V|
   24+10       0.8320      0.07  Q          |          |          |         V|
   24+15       0.8321      0.01  Q          |          |          |         V|
   24+20       0.8321      0.00  Q          |          |          |          V
-------------------------------------------------------------------------------
```

# C.4 – Proposed 100-Year Analysis

U n i t  H y d r o g r a p h  A n a l y s i s



Study date 08/26/24

++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
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San Bernardino County Synthetic Unit Hydrology Method
Manual date - August 1986

Program License Serial Number 6568

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TPM 20854
DEVELOPED CONDITION
100-YEAR
24-HOUR

---

Storm Event Year = 100

Antecedent Moisture Condition = 3

English (in-lb) Input Units Used

English Rainfall Data (Inches) Input Values Used

English Units used in output format

Area averaged rainfall intensity isohyetal data:

| Sub-Area (Ac.) | Duration (hours) | Isohyetal (In) |
|---|---|---|
| Rainfall data for year 10 | | |
| 4.40 | 1 | 0.73 |
| Rainfall data for year 2 | | |
| 4.40 | 6 | 1.15 |
| Rainfall data for year 2 | | |
| 4.40 | 24 | 2.05 |
| Rainfall data for year 100 | | |
| 4.40 | 1 | 1.16 |

---

```
Rainfall data for year 100
             4.40            6            2.65
------------------------------------------------------------------------
Rainfall data for year 100
             4.40           24            4.82
------------------------------------------------------------------------
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++

******** Area-averaged max loss rate, Fm ********


SCS curve  SCS curve     Area      Area     Fp(Fig C6)    Ap      Fm
No.(AMCII) NO.(AMC 3)    (Ac.)    Fraction     (In/Hr)  (dec.)   (In/Hr)
 59.6      78.7          4.40      1.000     0.392    0.299    0.117

Area-averaged adjusted loss rate Fm (In/Hr) =  0.117

********* Area-Averaged low loss rate fraction, Yb **********

Area        Area          SCS CN    SCS CN      S     Pervious
 (Ac.)       Fract         (AMC2)    (AMC3)           Yield Fr
     1.32   0.299         59.6      78.7       2.71     0.543
     3.08   0.701         98.0      98.0       0.20     0.951

Area-averaged catchment yield fraction, Y =  0.829
Area-averaged low loss fraction, Yb =  0.171
User entry of time of concentration  =   0.132 (hours)
++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Watershed area =       4.40(Ac.)
Catchment Lag time =   0.105 hours
Unit interval =   5.000 minutes
Unit interval percentage of lag time = 79.0939
Hydrograph baseflow =     0.00(CFS)
Average maximum watershed loss rate(Fm) =  0.117(In/Hr)
Average low loss rate fraction (Yb) = 0.171 (decimal)
VALLEY DEVELOPED S-Graph Selected
Computed peak 5-minute rainfall =  0.429(In)
Computed peak 30-minute rainfall =  0.879(In)
Specified peak 1-hour rainfall =  1.160(In)
Computed peak 3-hour rainfall =  1.925(In)
Specified peak 6-hour rainfall =  2.650(In)
Specified peak 24-hour rainfall =  4.820(In)


Rainfall depth area reduction factors:
Using a total area of       4.40(Ac.) (Ref: fig. E-4)

5-minute factor = 1.000     Adjusted rainfall =  0.429(In)
30-minute factor = 1.000    Adjusted rainfall =  0.879(In)
1-hour factor = 1.000       Adjusted rainfall =  1.160(In)
3-hour factor = 1.000       Adjusted rainfall =  1.925(In)
6-hour factor = 1.000       Adjusted rainfall =  2.650(In)
```

24-hour factor = 1.000  Adjusted rainfall =  4.820(In)

U n i t  H y d r o g r a p h

| Interval Number | 'S' Graph Mean values | Unit Hydrograph ((CFS)) |
|---|---|---|
| | (K = 53.21 (CFS)) | |
| 1 | 11.067 | 5.889 |
| 2 | 62.890 | 27.576 |
| 3 | 93.659 | 16.373 |
| 4 | 98.782 | 2.726 |
| 5 | 100.000 | 0.648 |

| Peak Unit Number | Adjusted mass rainfall (In) | Unit rainfall (In) |
|---|---|---|
| 1 | 0.4292 | 0.4292 |
| 2 | 0.5664 | 0.1371 |
| 3 | 0.6661 | 0.0997 |
| 4 | 0.7473 | 0.0812 |
| 5 | 0.8171 | 0.0698 |
| 6 | 0.8789 | 0.0618 |
| 7 | 0.9348 | 0.0559 |
| 8 | 0.9861 | 0.0513 |
| 9 | 1.0337 | 0.0476 |
| 10 | 1.0782 | 0.0445 |
| 11 | 1.1201 | 0.0419 |
| 12 | 1.1598 | 0.0397 |
| 13 | 1.2034 | 0.0436 |
| 14 | 1.2452 | 0.0418 |
| 15 | 1.2855 | 0.0403 |
| 16 | 1.3243 | 0.0388 |
| 17 | 1.3619 | 0.0376 |
| 18 | 1.3983 | 0.0364 |
| 19 | 1.4336 | 0.0353 |
| 20 | 1.4679 | 0.0343 |
| 21 | 1.5013 | 0.0334 |
| 22 | 1.5339 | 0.0326 |
| 23 | 1.5656 | 0.0318 |
| 24 | 1.5967 | 0.0310 |
| 25 | 1.6270 | 0.0303 |
| 26 | 1.6567 | 0.0297 |
| 27 | 1.6858 | 0.0291 |
| 28 | 1.7143 | 0.0285 |
| 29 | 1.7423 | 0.0280 |
| 30 | 1.7698 | 0.0275 |
| 31 | 1.7967 | 0.0270 |
| 32 | 1.8232 | 0.0265 |
| 33 | 1.8493 | 0.0261 |
| 34 | 1.8749 | 0.0256 |

| | | |
|---|---|---|
| 35 | 1.9002 | 0.0252 |
| 36 | 1.9250 | 0.0249 |
| 37 | 1.9495 | 0.0245 |
| 38 | 1.9736 | 0.0241 |
| 39 | 1.9974 | 0.0238 |
| 40 | 2.0209 | 0.0235 |
| 41 | 2.0440 | 0.0231 |
| 42 | 2.0668 | 0.0228 |
| 43 | 2.0894 | 0.0225 |
| 44 | 2.1116 | 0.0223 |
| 45 | 2.1336 | 0.0220 |
| 46 | 2.1554 | 0.0217 |
| 47 | 2.1769 | 0.0215 |
| 48 | 2.1981 | 0.0212 |
| 49 | 2.2191 | 0.0210 |
| 50 | 2.2399 | 0.0208 |
| 51 | 2.2604 | 0.0205 |
| 52 | 2.2807 | 0.0203 |
| 53 | 2.3008 | 0.0201 |
| 54 | 2.3208 | 0.0199 |
| 55 | 2.3405 | 0.0197 |
| 56 | 2.3600 | 0.0195 |
| 57 | 2.3793 | 0.0193 |
| 58 | 2.3985 | 0.0192 |
| 59 | 2.4175 | 0.0190 |
| 60 | 2.4363 | 0.0188 |
| 61 | 2.4549 | 0.0186 |
| 62 | 2.4734 | 0.0185 |
| 63 | 2.4917 | 0.0183 |
| 64 | 2.5099 | 0.0182 |
| 65 | 2.5279 | 0.0180 |
| 66 | 2.5458 | 0.0179 |
| 67 | 2.5635 | 0.0177 |
| 68 | 2.5810 | 0.0176 |
| 69 | 2.5985 | 0.0174 |
| 70 | 2.6158 | 0.0173 |
| 71 | 2.6329 | 0.0172 |
| 72 | 2.6500 | 0.0170 |
| 73 | 2.6658 | 0.0158 |
| 74 | 2.6815 | 0.0157 |
| 75 | 2.6971 | 0.0156 |
| 76 | 2.7125 | 0.0155 |
| 77 | 2.7279 | 0.0153 |
| 78 | 2.7431 | 0.0152 |
| 79 | 2.7582 | 0.0151 |
| 80 | 2.7732 | 0.0150 |
| 81 | 2.7881 | 0.0149 |
| 82 | 2.8029 | 0.0148 |
| 83 | 2.8176 | 0.0147 |
| 84 | 2.8322 | 0.0146 |
| 85 | 2.8467 | 0.0145 |
| 86 | 2.8611 | 0.0144 |

| | | |
|---|---|---|
| 87 | 2.8754 | 0.0143 |
| 88 | 2.8897 | 0.0142 |
| 89 | 2.9038 | 0.0141 |
| 90 | 2.9178 | 0.0140 |
| 91 | 2.9318 | 0.0139 |
| 92 | 2.9456 | 0.0139 |
| 93 | 2.9594 | 0.0138 |
| 94 | 2.9731 | 0.0137 |
| 95 | 2.9867 | 0.0136 |
| 96 | 3.0002 | 0.0135 |
| 97 | 3.0137 | 0.0134 |
| 98 | 3.0270 | 0.0134 |
| 99 | 3.0403 | 0.0133 |
| 100 | 3.0535 | 0.0132 |
| 101 | 3.0667 | 0.0131 |
| 102 | 3.0798 | 0.0131 |
| 103 | 3.0927 | 0.0130 |
| 104 | 3.1057 | 0.0129 |
| 105 | 3.1185 | 0.0129 |
| 106 | 3.1313 | 0.0128 |
| 107 | 3.1440 | 0.0127 |
| 108 | 3.1567 | 0.0126 |
| 109 | 3.1692 | 0.0126 |
| 110 | 3.1818 | 0.0125 |
| 111 | 3.1942 | 0.0124 |
| 112 | 3.2066 | 0.0124 |
| 113 | 3.2189 | 0.0123 |
| 114 | 3.2312 | 0.0123 |
| 115 | 3.2434 | 0.0122 |
| 116 | 3.2555 | 0.0121 |
| 117 | 3.2676 | 0.0121 |
| 118 | 3.2796 | 0.0120 |
| 119 | 3.2916 | 0.0120 |
| 120 | 3.3035 | 0.0119 |
| 121 | 3.3153 | 0.0119 |
| 122 | 3.3271 | 0.0118 |
| 123 | 3.3389 | 0.0117 |
| 124 | 3.3506 | 0.0117 |
| 125 | 3.3622 | 0.0116 |
| 126 | 3.3738 | 0.0116 |
| 127 | 3.3853 | 0.0115 |
| 128 | 3.3968 | 0.0115 |
| 129 | 3.4082 | 0.0114 |
| 130 | 3.4196 | 0.0114 |
| 131 | 3.4309 | 0.0113 |
| 132 | 3.4422 | 0.0113 |
| 133 | 3.4534 | 0.0112 |
| 134 | 3.4646 | 0.0112 |
| 135 | 3.4757 | 0.0111 |
| 136 | 3.4868 | 0.0111 |
| 137 | 3.4979 | 0.0110 |
| 138 | 3.5089 | 0.0110 |

| | | |
|---|---|---|
| 139 | 3.5198 | 0.0109 |
| 140 | 3.5307 | 0.0109 |
| 141 | 3.5416 | 0.0109 |
| 142 | 3.5524 | 0.0108 |
| 143 | 3.5632 | 0.0108 |
| 144 | 3.5739 | 0.0107 |
| 145 | 3.5846 | 0.0107 |
| 146 | 3.5952 | 0.0106 |
| 147 | 3.6058 | 0.0106 |
| 148 | 3.6164 | 0.0106 |
| 149 | 3.6269 | 0.0105 |
| 150 | 3.6374 | 0.0105 |
| 151 | 3.6479 | 0.0104 |
| 152 | 3.6583 | 0.0104 |
| 153 | 3.6686 | 0.0104 |
| 154 | 3.6790 | 0.0103 |
| 155 | 3.6892 | 0.0103 |
| 156 | 3.6995 | 0.0103 |
| 157 | 3.7097 | 0.0102 |
| 158 | 3.7199 | 0.0102 |
| 159 | 3.7300 | 0.0101 |
| 160 | 3.7401 | 0.0101 |
| 161 | 3.7502 | 0.0101 |
| 162 | 3.7602 | 0.0100 |
| 163 | 3.7702 | 0.0100 |
| 164 | 3.7802 | 0.0100 |
| 165 | 3.7901 | 0.0099 |
| 166 | 3.8000 | 0.0099 |
| 167 | 3.8099 | 0.0099 |
| 168 | 3.8197 | 0.0098 |
| 169 | 3.8295 | 0.0098 |
| 170 | 3.8393 | 0.0098 |
| 171 | 3.8490 | 0.0097 |
| 172 | 3.8587 | 0.0097 |
| 173 | 3.8684 | 0.0097 |
| 174 | 3.8780 | 0.0096 |
| 175 | 3.8876 | 0.0096 |
| 176 | 3.8972 | 0.0096 |
| 177 | 3.9067 | 0.0095 |
| 178 | 3.9162 | 0.0095 |
| 179 | 3.9257 | 0.0095 |
| 180 | 3.9352 | 0.0094 |
| 181 | 3.9446 | 0.0094 |
| 182 | 3.9540 | 0.0094 |
| 183 | 3.9633 | 0.0094 |
| 184 | 3.9727 | 0.0093 |
| 185 | 3.9820 | 0.0093 |
| 186 | 3.9912 | 0.0093 |
| 187 | 4.0005 | 0.0092 |
| 188 | 4.0097 | 0.0092 |
| 189 | 4.0189 | 0.0092 |
| 190 | 4.0280 | 0.0092 |

| | | |
|---|---|---|
| 191 | 4.0372 | 0.0091 |
| 192 | 4.0463 | 0.0091 |
| 193 | 4.0554 | 0.0091 |
| 194 | 4.0644 | 0.0091 |
| 195 | 4.0734 | 0.0090 |
| 196 | 4.0825 | 0.0090 |
| 197 | 4.0914 | 0.0090 |
| 198 | 4.1004 | 0.0089 |
| 199 | 4.1093 | 0.0089 |
| 200 | 4.1182 | 0.0089 |
| 201 | 4.1271 | 0.0089 |
| 202 | 4.1359 | 0.0088 |
| 203 | 4.1447 | 0.0088 |
| 204 | 4.1535 | 0.0088 |
| 205 | 4.1623 | 0.0088 |
| 206 | 4.1711 | 0.0087 |
| 207 | 4.1798 | 0.0087 |
| 208 | 4.1885 | 0.0087 |
| 209 | 4.1972 | 0.0087 |
| 210 | 4.2058 | 0.0087 |
| 211 | 4.2145 | 0.0086 |
| 212 | 4.2231 | 0.0086 |
| 213 | 4.2316 | 0.0086 |
| 214 | 4.2402 | 0.0086 |
| 215 | 4.2487 | 0.0085 |
| 216 | 4.2573 | 0.0085 |
| 217 | 4.2658 | 0.0085 |
| 218 | 4.2742 | 0.0085 |
| 219 | 4.2827 | 0.0084 |
| 220 | 4.2911 | 0.0084 |
| 221 | 4.2995 | 0.0084 |
| 222 | 4.3079 | 0.0084 |
| 223 | 4.3163 | 0.0084 |
| 224 | 4.3246 | 0.0083 |
| 225 | 4.3329 | 0.0083 |
| 226 | 4.3412 | 0.0083 |
| 227 | 4.3495 | 0.0083 |
| 228 | 4.3578 | 0.0083 |
| 229 | 4.3660 | 0.0082 |
| 230 | 4.3742 | 0.0082 |
| 231 | 4.3824 | 0.0082 |
| 232 | 4.3906 | 0.0082 |
| 233 | 4.3987 | 0.0082 |
| 234 | 4.4069 | 0.0081 |
| 235 | 4.4150 | 0.0081 |
| 236 | 4.4231 | 0.0081 |
| 237 | 4.4312 | 0.0081 |
| 238 | 4.4392 | 0.0081 |
| 239 | 4.4473 | 0.0080 |
| 240 | 4.4553 | 0.0080 |
| 241 | 4.4633 | 0.0080 |
| 242 | 4.4713 | 0.0080 |

| | | |
|---|---|---|
| 243 | 4.4792 | 0.0080 |
| 244 | 4.4872 | 0.0079 |
| 245 | 4.4951 | 0.0079 |
| 246 | 4.5030 | 0.0079 |
| 247 | 4.5109 | 0.0079 |
| 248 | 4.5188 | 0.0079 |
| 249 | 4.5266 | 0.0079 |
| 250 | 4.5345 | 0.0078 |
| 251 | 4.5423 | 0.0078 |
| 252 | 4.5501 | 0.0078 |
| 253 | 4.5579 | 0.0078 |
| 254 | 4.5656 | 0.0078 |
| 255 | 4.5734 | 0.0077 |
| 256 | 4.5811 | 0.0077 |
| 257 | 4.5888 | 0.0077 |
| 258 | 4.5965 | 0.0077 |
| 259 | 4.6042 | 0.0077 |
| 260 | 4.6119 | 0.0077 |
| 261 | 4.6195 | 0.0076 |
| 262 | 4.6271 | 0.0076 |
| 263 | 4.6348 | 0.0076 |
| 264 | 4.6424 | 0.0076 |
| 265 | 4.6499 | 0.0076 |
| 266 | 4.6575 | 0.0076 |
| 267 | 4.6650 | 0.0075 |
| 268 | 4.6726 | 0.0075 |
| 269 | 4.6801 | 0.0075 |
| 270 | 4.6876 | 0.0075 |
| 271 | 4.6951 | 0.0075 |
| 272 | 4.7025 | 0.0075 |
| 273 | 4.7100 | 0.0075 |
| 274 | 4.7174 | 0.0074 |
| 275 | 4.7249 | 0.0074 |
| 276 | 4.7323 | 0.0074 |
| 277 | 4.7397 | 0.0074 |
| 278 | 4.7470 | 0.0074 |
| 279 | 4.7544 | 0.0074 |
| 280 | 4.7617 | 0.0073 |
| 281 | 4.7691 | 0.0073 |
| 282 | 4.7764 | 0.0073 |
| 283 | 4.7837 | 0.0073 |
| 284 | 4.7910 | 0.0073 |
| 285 | 4.7982 | 0.0073 |
| 286 | 4.8055 | 0.0073 |
| 287 | 4.8127 | 0.0072 |
| 288 | 4.8200 | 0.0072 |

| Unit Period (number) | Unit Rainfall (In) | Unit Soil-Loss (In) | Effective Rainfall (In) |
|---|---|---|---|
| 1 | 0.0072 | 0.0012 | 0.0060 |

| | | | |
|---|---|---|---|
| 2 | 0.0072 | 0.0012 | 0.0060 |
| 3 | 0.0073 | 0.0012 | 0.0060 |
| 4 | 0.0073 | 0.0012 | 0.0060 |
| 5 | 0.0073 | 0.0013 | 0.0061 |
| 6 | 0.0073 | 0.0013 | 0.0061 |
| 7 | 0.0074 | 0.0013 | 0.0061 |
| 8 | 0.0074 | 0.0013 | 0.0061 |
| 9 | 0.0074 | 0.0013 | 0.0061 |
| 10 | 0.0074 | 0.0013 | 0.0062 |
| 11 | 0.0075 | 0.0013 | 0.0062 |
| 12 | 0.0075 | 0.0013 | 0.0062 |
| 13 | 0.0075 | 0.0013 | 0.0062 |
| 14 | 0.0075 | 0.0013 | 0.0062 |
| 15 | 0.0075 | 0.0013 | 0.0063 |
| 16 | 0.0076 | 0.0013 | 0.0063 |
| 17 | 0.0076 | 0.0013 | 0.0063 |
| 18 | 0.0076 | 0.0013 | 0.0063 |
| 19 | 0.0076 | 0.0013 | 0.0063 |
| 20 | 0.0077 | 0.0013 | 0.0064 |
| 21 | 0.0077 | 0.0013 | 0.0064 |
| 22 | 0.0077 | 0.0013 | 0.0064 |
| 23 | 0.0077 | 0.0013 | 0.0064 |
| 24 | 0.0078 | 0.0013 | 0.0064 |
| 25 | 0.0078 | 0.0013 | 0.0065 |
| 26 | 0.0078 | 0.0013 | 0.0065 |
| 27 | 0.0079 | 0.0013 | 0.0065 |
| 28 | 0.0079 | 0.0013 | 0.0065 |
| 29 | 0.0079 | 0.0014 | 0.0066 |
| 30 | 0.0079 | 0.0014 | 0.0066 |
| 31 | 0.0080 | 0.0014 | 0.0066 |
| 32 | 0.0080 | 0.0014 | 0.0066 |
| 33 | 0.0080 | 0.0014 | 0.0066 |
| 34 | 0.0080 | 0.0014 | 0.0067 |
| 35 | 0.0081 | 0.0014 | 0.0067 |
| 36 | 0.0081 | 0.0014 | 0.0067 |
| 37 | 0.0081 | 0.0014 | 0.0067 |
| 38 | 0.0082 | 0.0014 | 0.0068 |
| 39 | 0.0082 | 0.0014 | 0.0068 |
| 40 | 0.0082 | 0.0014 | 0.0068 |
| 41 | 0.0083 | 0.0014 | 0.0068 |
| 42 | 0.0083 | 0.0014 | 0.0069 |
| 43 | 0.0083 | 0.0014 | 0.0069 |
| 44 | 0.0083 | 0.0014 | 0.0069 |
| 45 | 0.0084 | 0.0014 | 0.0070 |
| 46 | 0.0084 | 0.0014 | 0.0070 |
| 47 | 0.0084 | 0.0014 | 0.0070 |
| 48 | 0.0085 | 0.0014 | 0.0070 |
| 49 | 0.0085 | 0.0015 | 0.0071 |
| 50 | 0.0085 | 0.0015 | 0.0071 |
| 51 | 0.0086 | 0.0015 | 0.0071 |
| 52 | 0.0086 | 0.0015 | 0.0071 |
| 53 | 0.0087 | 0.0015 | 0.0072 |

| | | | |
|---|---|---|---|
| 54 | 0.0087 | 0.0015 | 0.0072 |
| 55 | 0.0087 | 0.0015 | 0.0072 |
| 56 | 0.0087 | 0.0015 | 0.0073 |
| 57 | 0.0088 | 0.0015 | 0.0073 |
| 58 | 0.0088 | 0.0015 | 0.0073 |
| 59 | 0.0089 | 0.0015 | 0.0074 |
| 60 | 0.0089 | 0.0015 | 0.0074 |
| 61 | 0.0089 | 0.0015 | 0.0074 |
| 62 | 0.0090 | 0.0015 | 0.0074 |
| 63 | 0.0090 | 0.0015 | 0.0075 |
| 64 | 0.0091 | 0.0015 | 0.0075 |
| 65 | 0.0091 | 0.0016 | 0.0076 |
| 66 | 0.0091 | 0.0016 | 0.0076 |
| 67 | 0.0092 | 0.0016 | 0.0076 |
| 68 | 0.0092 | 0.0016 | 0.0076 |
| 69 | 0.0093 | 0.0016 | 0.0077 |
| 70 | 0.0093 | 0.0016 | 0.0077 |
| 71 | 0.0094 | 0.0016 | 0.0078 |
| 72 | 0.0094 | 0.0016 | 0.0078 |
| 73 | 0.0094 | 0.0016 | 0.0078 |
| 74 | 0.0095 | 0.0016 | 0.0079 |
| 75 | 0.0095 | 0.0016 | 0.0079 |
| 76 | 0.0096 | 0.0016 | 0.0079 |
| 77 | 0.0096 | 0.0016 | 0.0080 |
| 78 | 0.0097 | 0.0017 | 0.0080 |
| 79 | 0.0097 | 0.0017 | 0.0081 |
| 80 | 0.0098 | 0.0017 | 0.0081 |
| 81 | 0.0098 | 0.0017 | 0.0081 |
| 82 | 0.0099 | 0.0017 | 0.0082 |
| 83 | 0.0099 | 0.0017 | 0.0082 |
| 84 | 0.0100 | 0.0017 | 0.0083 |
| 85 | 0.0100 | 0.0017 | 0.0083 |
| 86 | 0.0101 | 0.0017 | 0.0083 |
| 87 | 0.0101 | 0.0017 | 0.0084 |
| 88 | 0.0102 | 0.0017 | 0.0084 |
| 89 | 0.0103 | 0.0018 | 0.0085 |
| 90 | 0.0103 | 0.0018 | 0.0085 |
| 91 | 0.0104 | 0.0018 | 0.0086 |
| 92 | 0.0104 | 0.0018 | 0.0086 |
| 93 | 0.0105 | 0.0018 | 0.0087 |
| 94 | 0.0105 | 0.0018 | 0.0087 |
| 95 | 0.0106 | 0.0018 | 0.0088 |
| 96 | 0.0106 | 0.0018 | 0.0088 |
| 97 | 0.0107 | 0.0018 | 0.0089 |
| 98 | 0.0108 | 0.0018 | 0.0089 |
| 99 | 0.0109 | 0.0019 | 0.0090 |
| 100 | 0.0109 | 0.0019 | 0.0090 |
| 101 | 0.0110 | 0.0019 | 0.0091 |
| 102 | 0.0110 | 0.0019 | 0.0092 |
| 103 | 0.0111 | 0.0019 | 0.0092 |
| 104 | 0.0112 | 0.0019 | 0.0093 |
| 105 | 0.0113 | 0.0019 | 0.0093 |

| | | | |
|---|---|---|---|
| 106 | 0.0113 | 0.0019 | 0.0094 |
| 107 | 0.0114 | 0.0020 | 0.0095 |
| 108 | 0.0115 | 0.0020 | 0.0095 |
| 109 | 0.0116 | 0.0020 | 0.0096 |
| 110 | 0.0116 | 0.0020 | 0.0096 |
| 111 | 0.0117 | 0.0020 | 0.0097 |
| 112 | 0.0118 | 0.0020 | 0.0098 |
| 113 | 0.0119 | 0.0020 | 0.0099 |
| 114 | 0.0120 | 0.0020 | 0.0099 |
| 115 | 0.0121 | 0.0021 | 0.0100 |
| 116 | 0.0121 | 0.0021 | 0.0101 |
| 117 | 0.0123 | 0.0021 | 0.0102 |
| 118 | 0.0123 | 0.0021 | 0.0102 |
| 119 | 0.0124 | 0.0021 | 0.0103 |
| 120 | 0.0125 | 0.0021 | 0.0104 |
| 121 | 0.0126 | 0.0022 | 0.0105 |
| 122 | 0.0127 | 0.0022 | 0.0105 |
| 123 | 0.0129 | 0.0022 | 0.0107 |
| 124 | 0.0129 | 0.0022 | 0.0107 |
| 125 | 0.0131 | 0.0022 | 0.0108 |
| 126 | 0.0131 | 0.0022 | 0.0109 |
| 127 | 0.0133 | 0.0023 | 0.0110 |
| 128 | 0.0134 | 0.0023 | 0.0111 |
| 129 | 0.0135 | 0.0023 | 0.0112 |
| 130 | 0.0136 | 0.0023 | 0.0113 |
| 131 | 0.0138 | 0.0024 | 0.0114 |
| 132 | 0.0139 | 0.0024 | 0.0115 |
| 133 | 0.0140 | 0.0024 | 0.0116 |
| 134 | 0.0141 | 0.0024 | 0.0117 |
| 135 | 0.0143 | 0.0024 | 0.0119 |
| 136 | 0.0144 | 0.0025 | 0.0119 |
| 137 | 0.0146 | 0.0025 | 0.0121 |
| 138 | 0.0147 | 0.0025 | 0.0122 |
| 139 | 0.0149 | 0.0025 | 0.0124 |
| 140 | 0.0150 | 0.0026 | 0.0124 |
| 141 | 0.0152 | 0.0026 | 0.0126 |
| 142 | 0.0153 | 0.0026 | 0.0127 |
| 143 | 0.0156 | 0.0027 | 0.0129 |
| 144 | 0.0157 | 0.0027 | 0.0130 |
| 145 | 0.0170 | 0.0029 | 0.0141 |
| 146 | 0.0172 | 0.0029 | 0.0142 |
| 147 | 0.0174 | 0.0030 | 0.0145 |
| 148 | 0.0176 | 0.0030 | 0.0146 |
| 149 | 0.0179 | 0.0031 | 0.0148 |
| 150 | 0.0180 | 0.0031 | 0.0149 |
| 151 | 0.0183 | 0.0031 | 0.0152 |
| 152 | 0.0185 | 0.0032 | 0.0153 |
| 153 | 0.0188 | 0.0032 | 0.0156 |
| 154 | 0.0190 | 0.0032 | 0.0157 |
| 155 | 0.0193 | 0.0033 | 0.0160 |
| 156 | 0.0195 | 0.0033 | 0.0162 |
| 157 | 0.0199 | 0.0034 | 0.0165 |

| | | | |
|---|---|---|---|
| 158 | 0.0201 | 0.0034 | 0.0167 |
| 159 | 0.0205 | 0.0035 | 0.0170 |
| 160 | 0.0208 | 0.0035 | 0.0172 |
| 161 | 0.0212 | 0.0036 | 0.0176 |
| 162 | 0.0215 | 0.0037 | 0.0178 |
| 163 | 0.0220 | 0.0038 | 0.0182 |
| 164 | 0.0223 | 0.0038 | 0.0185 |
| 165 | 0.0228 | 0.0039 | 0.0189 |
| 166 | 0.0231 | 0.0040 | 0.0192 |
| 167 | 0.0238 | 0.0041 | 0.0197 |
| 168 | 0.0241 | 0.0041 | 0.0200 |
| 169 | 0.0249 | 0.0042 | 0.0206 |
| 170 | 0.0252 | 0.0043 | 0.0209 |
| 171 | 0.0261 | 0.0045 | 0.0216 |
| 172 | 0.0265 | 0.0045 | 0.0220 |
| 173 | 0.0275 | 0.0047 | 0.0228 |
| 174 | 0.0280 | 0.0048 | 0.0232 |
| 175 | 0.0291 | 0.0050 | 0.0241 |
| 176 | 0.0297 | 0.0051 | 0.0246 |
| 177 | 0.0310 | 0.0053 | 0.0257 |
| 178 | 0.0318 | 0.0054 | 0.0263 |
| 179 | 0.0334 | 0.0057 | 0.0277 |
| 180 | 0.0343 | 0.0059 | 0.0285 |
| 181 | 0.0364 | 0.0062 | 0.0302 |
| 182 | 0.0376 | 0.0064 | 0.0311 |
| 183 | 0.0403 | 0.0069 | 0.0334 |
| 184 | 0.0418 | 0.0072 | 0.0347 |
| 185 | 0.0397 | 0.0068 | 0.0329 |
| 186 | 0.0419 | 0.0072 | 0.0347 |
| 187 | 0.0476 | 0.0081 | 0.0394 |
| 188 | 0.0513 | 0.0088 | 0.0425 |
| 189 | 0.0618 | 0.0098 | 0.0520 |
| 190 | 0.0698 | 0.0098 | 0.0600 |
| 191 | 0.0997 | 0.0098 | 0.0900 |
| 192 | 0.1371 | 0.0098 | 0.1274 |
| 193 | 0.4292 | 0.0098 | 0.4195 |
| 194 | 0.0812 | 0.0098 | 0.0715 |
| 195 | 0.0559 | 0.0096 | 0.0463 |
| 196 | 0.0445 | 0.0076 | 0.0369 |
| 197 | 0.0436 | 0.0075 | 0.0362 |
| 198 | 0.0388 | 0.0066 | 0.0322 |
| 199 | 0.0353 | 0.0060 | 0.0293 |
| 200 | 0.0326 | 0.0056 | 0.0270 |
| 201 | 0.0303 | 0.0052 | 0.0252 |
| 202 | 0.0285 | 0.0049 | 0.0236 |
| 203 | 0.0270 | 0.0046 | 0.0224 |
| 204 | 0.0256 | 0.0044 | 0.0213 |
| 205 | 0.0245 | 0.0042 | 0.0203 |
| 206 | 0.0235 | 0.0040 | 0.0194 |
| 207 | 0.0225 | 0.0039 | 0.0187 |
| 208 | 0.0217 | 0.0037 | 0.0180 |
| 209 | 0.0210 | 0.0036 | 0.0174 |

| | | | |
|---|---|---|---|
| 210 | 0.0203 | 0.0035 | 0.0169 |
| 211 | 0.0197 | 0.0034 | 0.0163 |
| 212 | 0.0192 | 0.0033 | 0.0159 |
| 213 | 0.0186 | 0.0032 | 0.0155 |
| 214 | 0.0182 | 0.0031 | 0.0151 |
| 215 | 0.0177 | 0.0030 | 0.0147 |
| 216 | 0.0173 | 0.0030 | 0.0143 |
| 217 | 0.0158 | 0.0027 | 0.0131 |
| 218 | 0.0155 | 0.0026 | 0.0128 |
| 219 | 0.0151 | 0.0026 | 0.0125 |
| 220 | 0.0148 | 0.0025 | 0.0123 |
| 221 | 0.0145 | 0.0025 | 0.0120 |
| 222 | 0.0142 | 0.0024 | 0.0118 |
| 223 | 0.0139 | 0.0024 | 0.0116 |
| 224 | 0.0137 | 0.0023 | 0.0114 |
| 225 | 0.0134 | 0.0023 | 0.0111 |
| 226 | 0.0132 | 0.0023 | 0.0110 |
| 227 | 0.0130 | 0.0022 | 0.0108 |
| 228 | 0.0128 | 0.0022 | 0.0106 |
| 229 | 0.0126 | 0.0022 | 0.0104 |
| 230 | 0.0124 | 0.0021 | 0.0103 |
| 231 | 0.0122 | 0.0021 | 0.0101 |
| 232 | 0.0120 | 0.0021 | 0.0100 |
| 233 | 0.0119 | 0.0020 | 0.0098 |
| 234 | 0.0117 | 0.0020 | 0.0097 |
| 235 | 0.0115 | 0.0020 | 0.0096 |
| 236 | 0.0114 | 0.0019 | 0.0094 |
| 237 | 0.0112 | 0.0019 | 0.0093 |
| 238 | 0.0111 | 0.0019 | 0.0092 |
| 239 | 0.0109 | 0.0019 | 0.0091 |
| 240 | 0.0108 | 0.0018 | 0.0090 |
| 241 | 0.0107 | 0.0018 | 0.0089 |
| 242 | 0.0106 | 0.0018 | 0.0088 |
| 243 | 0.0104 | 0.0018 | 0.0087 |
| 244 | 0.0103 | 0.0018 | 0.0086 |
| 245 | 0.0102 | 0.0017 | 0.0085 |
| 246 | 0.0101 | 0.0017 | 0.0084 |
| 247 | 0.0100 | 0.0017 | 0.0083 |
| 248 | 0.0099 | 0.0017 | 0.0082 |
| 249 | 0.0098 | 0.0017 | 0.0081 |
| 250 | 0.0097 | 0.0017 | 0.0080 |
| 251 | 0.0096 | 0.0016 | 0.0080 |
| 252 | 0.0095 | 0.0016 | 0.0079 |
| 253 | 0.0094 | 0.0016 | 0.0078 |
| 254 | 0.0093 | 0.0016 | 0.0077 |
| 255 | 0.0092 | 0.0016 | 0.0077 |
| 256 | 0.0092 | 0.0016 | 0.0076 |
| 257 | 0.0091 | 0.0016 | 0.0075 |
| 258 | 0.0090 | 0.0015 | 0.0075 |
| 259 | 0.0089 | 0.0015 | 0.0074 |
| 260 | 0.0088 | 0.0015 | 0.0073 |
| 261 | 0.0088 | 0.0015 | 0.0073 |

| | | | |
|---|---|---|---|
| 262 | 0.0087 | 0.0015 | 0.0072 |
| 263 | 0.0086 | 0.0015 | 0.0072 |
| 264 | 0.0086 | 0.0015 | 0.0071 |
| 265 | 0.0085 | 0.0015 | 0.0070 |
| 266 | 0.0084 | 0.0014 | 0.0070 |
| 267 | 0.0084 | 0.0014 | 0.0069 |
| 268 | 0.0083 | 0.0014 | 0.0069 |
| 269 | 0.0082 | 0.0014 | 0.0068 |
| 270 | 0.0082 | 0.0014 | 0.0068 |
| 271 | 0.0081 | 0.0014 | 0.0067 |
| 272 | 0.0081 | 0.0014 | 0.0067 |
| 273 | 0.0080 | 0.0014 | 0.0066 |
| 274 | 0.0079 | 0.0014 | 0.0066 |
| 275 | 0.0079 | 0.0013 | 0.0065 |
| 276 | 0.0078 | 0.0013 | 0.0065 |
| 277 | 0.0078 | 0.0013 | 0.0065 |
| 278 | 0.0077 | 0.0013 | 0.0064 |
| 279 | 0.0077 | 0.0013 | 0.0064 |
| 280 | 0.0076 | 0.0013 | 0.0063 |
| 281 | 0.0076 | 0.0013 | 0.0063 |
| 282 | 0.0075 | 0.0013 | 0.0062 |
| 283 | 0.0075 | 0.0013 | 0.0062 |
| 284 | 0.0074 | 0.0013 | 0.0062 |
| 285 | 0.0074 | 0.0013 | 0.0061 |
| 286 | 0.0073 | 0.0013 | 0.0061 |
| 287 | 0.0073 | 0.0012 | 0.0061 |
| 288 | 0.0073 | 0.0012 | 0.0060 |

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Total soil rain loss = 0.73(In)
Total effective rainfall = 4.09(In)
Peak flow rate in flood hydrograph = 14.36(CFS)

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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

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Hydrograph in 5 Minute intervals ((CFS))

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| Time(h+m) | Volume Ac.Ft | Q(CFS) | 0 | 5.0 | 10.0 | 15.0 | 20.0 |
|---|---|---|---|---|---|---|---|
| 0+ 5 | 0.0002 | 0.04 | Q | \| | \| | \| | \| |
| 0+10 | 0.0016 | 0.20 | Q | \| | \| | \| | \| |
| 0+15 | 0.0037 | 0.30 | Q | \| | \| | \| | \| |
| 0+20 | 0.0059 | 0.32 | Q | \| | \| | \| | \| |
| 0+25 | 0.0081 | 0.32 | Q | \| | \| | \| | \| |
| 0+30 | 0.0103 | 0.32 | Q | \| | \| | \| | \| |
| 0+35 | 0.0125 | 0.32 | Q | \| | \| | \| | \| |
| 0+40 | 0.0148 | 0.32 | Q | \| | \| | \| | \| |
| 0+45 | 0.0170 | 0.33 | Q | \| | \| | \| | \| |
| 0+50 | 0.0192 | 0.33 | Q | \| | \| | \| | \| |

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| 0+55 | 0.0215 | 0.33 | Q | \| | \| | \| | \| |
| 1+ 0 | 0.0238 | 0.33 | Q | \| | \| | \| | \| |
| 1+ 5 | 0.0260 | 0.33 | Q | \| | \| | \| | \| |
| 1+10 | 0.0283 | 0.33 | Q | \| | \| | \| | \| |
| 1+15 | 0.0306 | 0.33 | Q | \| | \| | \| | \| |
| 1+20 | 0.0329 | 0.33 | Q | \| | \| | \| | \| |
| 1+25 | 0.0352 | 0.33 | Q | \| | \| | \| | \| |
| 1+30 | 0.0375 | 0.33 | QV | \| | \| | \| | \| |
| 1+35 | 0.0398 | 0.34 | QV | \| | \| | \| | \| |
| 1+40 | 0.0421 | 0.34 | QV | \| | \| | \| | \| |
| 1+45 | 0.0444 | 0.34 | QV | \| | \| | \| | \| |
| 1+50 | 0.0468 | 0.34 | QV | \| | \| | \| | \| |
| 1+55 | 0.0491 | 0.34 | QV | \| | \| | \| | \| |
| 2+ 0 | 0.0515 | 0.34 | QV | \| | \| | \| | \| |
| 2+ 5 | 0.0538 | 0.34 | QV | \| | \| | \| | \| |
| 2+10 | 0.0562 | 0.34 | QV | \| | \| | \| | \| |
| 2+15 | 0.0586 | 0.34 | QV | \| | \| | \| | \| |
| 2+20 | 0.0609 | 0.35 | QV | \| | \| | \| | \| |
| 2+25 | 0.0633 | 0.35 | QV | \| | \| | \| | \| |
| 2+30 | 0.0657 | 0.35 | QV | \| | \| | \| | \| |
| 2+35 | 0.0681 | 0.35 | QV | \| | \| | \| | \| |
| 2+40 | 0.0706 | 0.35 | QV | \| | \| | \| | \| |
| 2+45 | 0.0730 | 0.35 | QV | \| | \| | \| | \| |
| 2+50 | 0.0754 | 0.35 | Q V | \| | \| | \| | \| |
| 2+55 | 0.0779 | 0.35 | Q V | \| | \| | \| | \| |
| 3+ 0 | 0.0803 | 0.36 | Q V | \| | \| | \| | \| |
| 3+ 5 | 0.0828 | 0.36 | Q V | \| | \| | \| | \| |
| 3+10 | 0.0852 | 0.36 | Q V | \| | \| | \| | \| |
| 3+15 | 0.0877 | 0.36 | Q V | \| | \| | \| | \| |
| 3+20 | 0.0902 | 0.36 | Q V | \| | \| | \| | \| |
| 3+25 | 0.0927 | 0.36 | Q V | \| | \| | \| | \| |
| 3+30 | 0.0952 | 0.36 | Q V | \| | \| | \| | \| |
| 3+35 | 0.0977 | 0.36 | Q V | \| | \| | \| | \| |
| 3+40 | 0.1002 | 0.37 | Q V | \| | \| | \| | \| |
| 3+45 | 0.1028 | 0.37 | Q V | \| | \| | \| | \| |
| 3+50 | 0.1053 | 0.37 | Q V | \| | \| | \| | \| |
| 3+55 | 0.1079 | 0.37 | Q V | \| | \| | \| | \| |
| 4+ 0 | 0.1104 | 0.37 | Q V | \| | \| | \| | \| |
| 4+ 5 | 0.1130 | 0.37 | Q  V | \| | \| | \| | \| |
| 4+10 | 0.1156 | 0.38 | Q  V | \| | \| | \| | \| |
| 4+15 | 0.1182 | 0.38 | Q  V | \| | \| | \| | \| |
| 4+20 | 0.1208 | 0.38 | Q  V | \| | \| | \| | \| |
| 4+25 | 0.1234 | 0.38 | Q  V | \| | \| | \| | \| |
| 4+30 | 0.1260 | 0.38 | Q  V | \| | \| | \| | \| |
| 4+35 | 0.1286 | 0.38 | Q  V | \| | \| | \| | \| |
| 4+40 | 0.1313 | 0.38 | Q  V | \| | \| | \| | \| |
| 4+45 | 0.1339 | 0.39 | Q  V | \| | \| | \| | \| |
| 4+50 | 0.1366 | 0.39 | Q  V | \| | \| | \| | \| |
| 4+55 | 0.1393 | 0.39 | Q  V | \| | \| | \| | \| |
| 5+ 0 | 0.1420 | 0.39 | Q  V | \| | \| | \| | \| |
| 5+ 5 | 0.1447 | 0.39 | Q  V | \| | \| | \| | \| |
| 5+10 | 0.1474 | 0.39 | Q  V | \| | \| | \| | \| |

```
5+15       0.1501      0.40  Q   V     |           |           |           |
5+20       0.1529      0.40  Q   V     |           |           |           |
5+25       0.1556      0.40  Q   V     |           |           |           |
5+30       0.1584      0.40  Q   V     |           |           |           |
5+35       0.1611      0.40  Q   V     |           |           |           |
5+40       0.1639      0.40  Q   V     |           |           |           |
5+45       0.1667      0.41  Q   V     |           |           |           |
5+50       0.1695      0.41  Q   V     |           |           |           |
5+55       0.1724      0.41  Q   V     |           |           |           |
6+ 0       0.1752      0.41  Q   V     |           |           |           |
6+ 5       0.1780      0.41  Q   V     |           |           |           |
6+10       0.1809      0.42  Q   V     |           |           |           |
6+15       0.1838      0.42  Q   V     |           |           |           |
6+20       0.1867      0.42  Q   V     |           |           |           |
6+25       0.1896      0.42  Q    V    |           |           |           |
6+30       0.1925      0.42  Q    V    |           |           |           |
6+35       0.1954      0.43  Q    V    |           |           |           |
6+40       0.1984      0.43  Q    V    |           |           |           |
6+45       0.2014      0.43  Q    V    |           |           |           |
6+50       0.2043      0.43  Q    V    |           |           |           |
6+55       0.2073      0.43  Q    V    |           |           |           |
7+ 0       0.2103      0.44  Q    V    |           |           |           |
7+ 5       0.2134      0.44  Q    V    |           |           |           |
7+10       0.2164      0.44  Q    V    |           |           |           |
7+15       0.2195      0.44  Q    V    |           |           |           |
7+20       0.2225      0.45  Q    V    |           |           |           |
7+25       0.2256      0.45  Q     V   |           |           |           |
7+30       0.2287      0.45  Q     V   |           |           |           |
7+35       0.2318      0.45  Q     V   |           |           |           |
7+40       0.2350      0.46  Q     V   |           |           |           |
7+45       0.2381      0.46  Q     V   |           |           |           |
7+50       0.2413      0.46  Q     V   |           |           |           |
7+55       0.2445      0.46  Q     V   |           |           |           |
8+ 0       0.2477      0.47  Q     V   |           |           |           |
8+ 5       0.2510      0.47  Q     V   |           |           |           |
8+10       0.2542      0.47  Q     V   |           |           |           |
8+15       0.2575      0.47  Q     V   |           |           |           |
8+20       0.2608      0.48  Q     V   |           |           |           |
8+25       0.2641      0.48  Q      V  |           |           |           |
8+30       0.2674      0.48  Q      V  |           |           |           |
8+35       0.2708      0.49  Q      V  |           |           |           |
8+40       0.2741      0.49  Q      V  |           |           |           |
8+45       0.2775      0.49  Q      V  |           |           |           |
8+50       0.2809      0.50  Q      V  |           |           |           |
8+55       0.2844      0.50  Q      V  |           |           |           |
9+ 0       0.2878      0.50  |Q     V  |           |           |           |
9+ 5       0.2913      0.51  |Q     V  |           |           |           |
9+10       0.2948      0.51  |Q     V  |           |           |           |
9+15       0.2984      0.51  |Q     V  |           |           |           |
9+20       0.3019      0.52  |Q      V |           |           |           |
9+25       0.3055      0.52  |Q      V |           |           |           |
9+30       0.3091      0.52  |Q      V |           |           |           |
```

```
 9+35       0.3127      0.53  |Q      V |          |          |          |
 9+40       0.3164      0.53  |Q      V |          |          |          |
 9+45       0.3201      0.53  |Q      V |          |          |          |
 9+50       0.3238      0.54  |Q      V |          |          |          |
 9+55       0.3275      0.54  |Q      V |          |          |          |
10+ 0       0.3313      0.55  |Q      V |          |          |          |
10+ 5       0.3351      0.55  |Q      V |          |          |          |
10+10       0.3389      0.56  |Q       V|          |          |          |
10+15       0.3428      0.56  |Q       V|          |          |          |
10+20       0.3467      0.56  |Q       V|          |          |          |
10+25       0.3506      0.57  |Q       V|          |          |          |
10+30       0.3545      0.57  |Q       V|          |          |          |
10+35       0.3585      0.58  |Q       V|          |          |          |
10+40       0.3626      0.58  |Q       V|          |          |          |
10+45       0.3666      0.59  |Q       V|          |          |          |
10+50       0.3707      0.59  |Q       V|          |          |          |
10+55       0.3748      0.60  |Q        V          |          |          |
11+ 0       0.3790      0.61  |Q        V          |          |          |
11+ 5       0.3832      0.61  |Q        V          |          |          |
11+10       0.3874      0.62  |Q        V          |          |          |
11+15       0.3917      0.62  |Q        V          |          |          |
11+20       0.3961      0.63  |Q        V          |          |          |
11+25       0.4004      0.63  |Q        V          |          |          |
11+30       0.4048      0.64  |Q        V          |          |          |
11+35       0.4093      0.65  |Q        V          |          |          |
11+40       0.4138      0.65  |Q        |V          |          |          |
11+45       0.4184      0.66  |Q        |V          |          |          |
11+50       0.4230      0.67  |Q        |V          |          |          |
11+55       0.4276      0.68  |Q        |V          |          |          |
12+ 0       0.4323      0.68  |Q        |V          |          |          |
12+ 5       0.4371      0.70  |Q        |V          |          |          |
12+10       0.4421      0.73  |Q        |V          |          |          |
12+15       0.4473      0.75  |Q        |V          |          |          |
12+20       0.4526      0.76  |Q        | V         |          |          |
12+25       0.4579      0.77  |Q        | V         |          |          |
12+30       0.4633      0.78  |Q        | V         |          |          |
12+35       0.4688      0.79  |Q        | V         |          |          |
12+40       0.4743      0.80  |Q        | V         |          |          |
12+45       0.4799      0.81  |Q        | V         |          |          |
12+50       0.4856      0.82  |Q        | V         |          |          |
12+55       0.4913      0.84  |Q        |  V        |          |          |
13+ 0       0.4972      0.85  |Q        |  V        |          |          |
13+ 5       0.5031      0.86  |Q        |  V        |          |          |
13+10       0.5091      0.87  |Q        |  V        |          |          |
13+15       0.5152      0.89  |Q        |  V        |          |          |
13+20       0.5214      0.90  |Q        |  V        |          |          |
13+25       0.5277      0.91  |Q        |   V       |          |          |
13+30       0.5341      0.93  |Q        |   V       |          |          |
13+35       0.5406      0.94  |Q        |   V       |          |          |
13+40       0.5472      0.96  |Q        |   V       |          |          |
13+45       0.5540      0.98  |Q        |   V       |          |          |
13+50       0.5608      1.00  |Q        |   V       |          |          |
```

```
13+55       0.5678      1.02  | Q       |    V    |         |          |
14+ 0       0.5750      1.04  | Q       |    V    |         |          |
14+ 5       0.5823      1.06  | Q       |    V    |         |          |
14+10       0.5898      1.08  | Q       |    V    |         |          |
14+15       0.5974      1.11  | Q       |    V    |         |          |
14+20       0.6052      1.14  | Q       |     V   |         |          |
14+25       0.6133      1.16  | Q       |     V   |         |          |
14+30       0.6215      1.20  | Q       |     V   |         |          |
14+35       0.6300      1.23  | Q       |     V   |         |          |
14+40       0.6387      1.27  | Q       |      V  |         |          |
14+45       0.6477      1.30  | Q       |      V  |         |          |
14+50       0.6569      1.35  | Q       |      V  |         |          |
14+55       0.6665      1.39  | Q       |      V  |         |          |
15+ 0       0.6765      1.45  | Q       |       V |         |          |
15+ 5       0.6869      1.50  |  Q      |       V |         |          |
15+10       0.6977      1.57  |  Q      |       V |         |          |
15+15       0.7090      1.64  |  Q      |       V |         |          |
15+20       0.7210      1.74  |  Q      |        V|         |          |
15+25       0.7334      1.80  |  Q      |        V|         |          |
15+30       0.7457      1.79  |  Q      |        V|         |          |
15+35       0.7584      1.84  |  Q      |         V         |          |
15+40       0.7723      2.02  |   Q     |         V         |          |
15+45       0.7878      2.24  |   Q     |          |V       |          |
15+50       0.8058      2.61  |    Q    |          |V       |          |
15+55       0.8277      3.18  |     Q   |          | V      |          |
16+ 0       0.8579      4.38  |       Q |          | V      |          |
16+ 5       0.9106      7.65  |         |    Q     |   V    |          |
16+10       1.0094     14.36  |         |          |     V Q|          |
16+15       1.0750      9.52  |         |        Q|       V |          |
16+20       1.1018      3.89  |      Q  |          |        V|          |
16+25       1.1187      2.46  |   Q     |          |        V|          |
16+30       1.1322      1.96  |  Q      |          |         V          |
16+35       1.1445      1.78  |  Q      |          |         V          |
16+40       1.1556      1.62  |  Q      |          |         V          |
16+45       1.1659      1.48  | Q       |          |         |V         |
16+50       1.1753      1.38  | Q       |          |         |V         |
16+55       1.1842      1.29  | Q       |          |         |V         |
17+ 0       1.1926      1.21  | Q       |          |         |V         |
17+ 5       1.2005      1.15  | Q       |          |         | V        |
17+10       1.2081      1.10  | Q       |          |         | V        |
17+15       1.2153      1.05  | Q       |          |         | V        |
17+20       1.2223      1.01  | Q       |          |         | V        |
17+25       1.2289      0.97  |Q        |          |         | V        |
17+30       1.2354      0.94  |Q        |          |         | V        |
17+35       1.2417      0.91  |Q        |          |         |  V       |
17+40       1.2477      0.88  |Q        |          |         |  V       |
17+45       1.2536      0.85  |Q        |          |         |  V       |
17+50       1.2593      0.83  |Q        |          |         |  V       |
17+55       1.2649      0.81  |Q        |          |         |  V       |
18+ 0       1.2703      0.79  |Q        |          |         |  V       |
18+ 5       1.2756      0.76  |Q        |          |         |   V      |
18+10       1.2805      0.72  |Q        |          |         |   V      |
```

```
18+15       1.2853      0.69  |Q        |          |          |   V      |
18+20       1.2899      0.67  |Q        |          |          |   V      |
18+25       1.2945      0.66  |Q        |          |          |   V      |
18+30       1.2989      0.64  |Q        |          |          |   V      |
18+35       1.3033      0.63  |Q        |          |          |   V      |
18+40       1.3075      0.62  |Q        |          |          |   V      |
18+45       1.3117      0.61  |Q        |          |          |    V     |
18+50       1.3158      0.60  |Q        |          |          |    V     |
18+55       1.3199      0.59  |Q        |          |          |    V     |
19+ 0       1.3238      0.58  |Q        |          |          |    V     |
19+ 5       1.3277      0.57  |Q        |          |          |    V     |
19+10       1.3316      0.56  |Q        |          |          |    V     |
19+15       1.3354      0.55  |Q        |          |          |    V     |
19+20       1.3391      0.54  |Q        |          |          |    V     |
19+25       1.3428      0.53  |Q        |          |          |    V     |
19+30       1.3464      0.53  |Q        |          |          |    V     |
19+35       1.3499      0.52  |Q        |          |          |     V    |
19+40       1.3535      0.51  |Q        |          |          |     V    |
19+45       1.3569      0.50  |Q        |          |          |     V    |
19+50       1.3604      0.50  Q         |          |          |     V    |
19+55       1.3637      0.49  Q         |          |          |     V    |
20+ 0       1.3671      0.49  Q         |          |          |     V    |
20+ 5       1.3704      0.48  Q         |          |          |     V    |
20+10       1.3736      0.47  Q         |          |          |     V    |
20+15       1.3769      0.47  Q         |          |          |     V    |
20+20       1.3801      0.46  Q         |          |          |     V    |
20+25       1.3832      0.46  Q         |          |          |     V    |
20+30       1.3863      0.45  Q         |          |          |      V   |
20+35       1.3894      0.45  Q         |          |          |      V   |
20+40       1.3925      0.44  Q         |          |          |      V   |
20+45       1.3955      0.44  Q         |          |          |      V   |
20+50       1.3985      0.43  Q         |          |          |      V   |
20+55       1.4014      0.43  Q         |          |          |      V   |
21+ 0       1.4043      0.43  Q         |          |          |      V   |
21+ 5       1.4072      0.42  Q         |          |          |      V   |
21+10       1.4101      0.42  Q         |          |          |      V   |
21+15       1.4130      0.41  Q         |          |          |      V   |
21+20       1.4158      0.41  Q         |          |          |      V   |
21+25       1.4186      0.41  Q         |          |          |      V   |
21+30       1.4213      0.40  Q         |          |          |      V   |
21+35       1.4241      0.40  Q         |          |          |       V  |
21+40       1.4268      0.39  Q         |          |          |       V  |
21+45       1.4295      0.39  Q         |          |          |       V  |
21+50       1.4322      0.39  Q         |          |          |       V  |
21+55       1.4348      0.38  Q         |          |          |       V  |
22+ 0       1.4374      0.38  Q         |          |          |       V  |
22+ 5       1.4401      0.38  Q         |          |          |       V  |
22+10       1.4426      0.38  Q         |          |          |       V  |
22+15       1.4452      0.37  Q         |          |          |       V  |
22+20       1.4478      0.37  Q         |          |          |       V  |
22+25       1.4503      0.37  Q         |          |          |       V  |
22+30       1.4528      0.36  Q         |          |          |       V  |
```

```
   22+35       1.4553      0.36  Q          |          |          |        V |
   22+40       1.4578      0.36  Q          |          |          |        V |
   22+45       1.4602      0.36  Q          |          |          |        V |
   22+50       1.4627      0.35  Q          |          |          |         V|
   22+55       1.4651      0.35  Q          |          |          |         V|
   23+ 0       1.4675      0.35  Q          |          |          |         V|
   23+ 5       1.4699      0.35  Q          |          |          |         V|
   23+10       1.4722      0.34  Q          |          |          |         V|
   23+15       1.4746      0.34  Q          |          |          |         V|
   23+20       1.4769      0.34  Q          |          |          |         V|
   23+25       1.4792      0.34  Q          |          |          |         V|
   23+30       1.4816      0.34  Q          |          |          |         V|
   23+35       1.4838      0.33  Q          |          |          |         V|
   23+40       1.4861      0.33  Q          |          |          |         V|
   23+45       1.4884      0.33  Q          |          |          |         V|
   23+50       1.4906      0.33  Q          |          |          |         V|
   23+55       1.4929      0.32  Q          |          |          |         V|
   24+ 0       1.4951      0.32  Q          |          |          |         V|
   24+ 5       1.4971      0.29  Q          |          |          |         V|
   24+10       1.4979      0.12  Q          |          |          |         V|
   24+15       1.4980      0.02  Q          |          |          |         V|
   24+20       1.4981      0.00  Q          |          |          |          V
-------------------------------------------------------------------------------
```

D.1 – BASIN "A" STAGE-STORAGE-OUTFLOW SUMMARY & 100-YEAR ROUTING

| Proposed Infiltration Basin "A" | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| Input | Basin Depth (ft) | Total Vol. (af) | Infiltration Outflow (cfs) | Orifice #1 (cfs) | Weir 1 Outflow (cfs) | Weir 2 - Emergancy Overflow (cfs) | Total Q outflow (cfs) | Contour Elevation | Contour Area (sf) | Inc. Volume (cf) | Inc. Volume (af) |
| **1** | **0.00** | **0.00** | 0.07 | | | | **0.07** | 1145.00 | 7,474 | | |
| **2** | **1.00** | **0.19** | 0.10 | | | | **0.10** | 1146.00 | 9,529 | 8,480 | 0.19 |
| **3** | **2.00** | **0.44** | 0.12 | 0.39 | | | **0.51** | 1147.00 | 11,794 | 10,641 | 0.24 |
| **4** | **3.00** | **0.74** | 0.14 | 0.60 | | | **0.75** | 1148.00 | 14,293 | 13,023 | 0.30 |
| **5** | **4.00** | **1.10** | 0.17 | 0.76 | 14.79 | | **15.72** | 1149.00 | 16,915 | 15,585 | 0.36 |
| **6** | **5.00** | **1.52** | 0.20 | 0.89 | 76.88 | 23.55 | **101.51** | 1150.00 | 19,690 | 18,285 | 0.42 |

| Infiltration | | | | |
|---|---|---|---|---|
| In-Situ: | 1.3 | in/hr | | |
| Factor of Safety: | 3 | | | |
| $k_{design}$ = | 0.43 | in/hr | 0.00001 | cfs/sq-ft |

| Orifice Outflow [$Q=CA(2g(h_{el.}-h_{ft}$ | | |
|---|---|---|
| | #1 | #2 |
| d (in)= | 4 | 0 |
| C= | 0.66 | 0.66 |
| A ($ft^2$)= | 0.087 | 0.000 |
| FL Elev. | 1146.30 | |

| Weir Flow [$Q=(C_w)(L)(H)^{3/2}$] | | |
|---|---|---|
| | #1 | #2 |
| L (ft) | 12.57 | 0 |
| $C_w$ | 3.33 | 3.33 |
| A ($ft^2$)= | 12.56637 | 0 |
| FL Elev. | 1148.50 | |
| | | |

| Emergancy Overflow | |
|---|---|
| L (ft) | 20 |
| $C_w$ | 3.33 |
| FL Elev. | 1149.5 |

Target 100-yr outflow: 6.9 cfs

# WATER QUALITY CALCULATIONS
## VOLUME-BASED BMP FOR SAN BERNARDINO COUNTY

| | |
|---|---|
| Project number: | 2023.08008 |
| Project Name: | 913 California St. Redlands |
| Project Region: | VALLEY |

Equations: $R_C = 0.858i^3 - 0.78i^2 + 0.774i + 0.04$

$P_6 = (P_{2yr,1hr})(C_1)$

$P_{2yr, 1hr}$ = 0.47 (FROM FIGURE D-1 NOAA Atlas 14 INSET MAP)

$DCV = 1/12 \times DA * R_C * P_6 * C_2$

| Location | DA ($ft^2$) | *i* | $R_C$ | $P_6$ | $C_2$ | DCV ($ft^3$) |
|---|---|---|---|---|---|---|
| DA1 | 215,657 | 0.64 | 0.44 | 0.70 | 1.963 | 10,795 |
| | | | | | | 0 |
| | | | | | | 0 |
| | | | | | | 0 |
| | | | | | | 0 |
| | | | | | | 0 |
| | | | | | | 0 |
| | | | | | | |
| **Total** | 215,657 | | | | | 10,795 |

Where: DA = Project Drainage Area, in square feet

*i* = watershed imperviousness ratio which is equal to the percent total impervious divided by 100

$R_C$ = runoff coefficient

$P_{2yr, 1hr}$ = 1-hour rainfall depth for a 2-year return period, in inches

$P_6$ = mean annual runoff-producing rainfall depths. In watershed inches, Table #-1 in Appendix D

valley, $C_1$ = 1.4807

mountain, $C_1$ = 1.9090

desert, $C_1$ = 1.2371

$C_2$ = regression constant, 1.582 and 1.963 for 24 and 48 hour draw down, respectively

DCV = Design Capture Volume, in cubic feet

Urban Runoff Quality Management Approach
(WEF Manual of Practice No. 23/ASCE Manual of Practice No. 87

| Routing Anaylsis: Infiltration Basin "A" | | |
|---|---|---|
| | **10-YR** | **100-YR** |
| Basin Capacity | 1.52 ac-ft | |
| Total Depth | 5 ft | |
| Peak Inflow, Q (cfs) | 8.3 | 14.4 |
| Peak Outflow, Q (cfs) | 0.6 | 4.2 |
| Runoff reduction (%) | 92.7% | 70.7% |
| Peak Basin Depth (ft) | 2.38 | 3.23 |
| Peak W.S.E. | 1147.38 | 1148.23 |
| Max. Freeboard (ft) | 2.62 | 1.77 |

FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 08/26/24

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TPM 20854
PROPOSED INFILTRATION BASIN ROUTING ANALYSIS
BASIN "A"
10-YR; 24-HOUR
---

Program License Serial Number 6545

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********** HYDROGRAPH INFORMATION **********

From study/file name: D10.rte
**********HYDROGRAPH DATA**********
Number of intervals = 292
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 8.301 (CFS)
Total volume = 0.832 (Ac.Ft)
Status of hydrographs being held in storage

| | Stream 1 | Stream 2 | Stream 3 | Stream 4 | Stream 5 |
|---|---|---|---|---|---|
| Peak (CFS) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Vol (Ac.Ft) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

**********

++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station 1.000 to Point/Station 15.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data
---
Total number of inflow hydrograph intervals = 292
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 1.22(Ft.)
---
---
Initial basin depth = 1.22 (Ft.)
Initial basin storage = 0.25 (Ac.Ft)
Initial basin outflow = 0.19 (CFS)
---
---

Depth vs. Storage and Depth vs. Discharge data:

| Basin Depth (Ft.) | Storage (Ac.Ft) | Outflow (CFS) | (S-O*dt/2) (Ac.Ft) | (S+O*dt/2) (Ac.Ft) |
|---|---|---|---|---|
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.000 | 0.190 | 0.100 | 0.190 | 0.190 |
| 2.000 | 0.440 | 0.510 | 0.438 | 0.442 |
| 3.000 | 0.740 | 0.750 | 0.737 | 0.743 |
| 4.000 | 1.100 | 15.720 | 1.046 | 1.154 |
| 5.000 | 1.520 | 101.510 | 1.170 | 1.870 |

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

| Time (Hours) | Inflow (CFS) | Outflow (CFS) | Storage (Ac.Ft) | .0 | 2.1 | 4.15 | 6.23 | 8.30 | Depth (Ft.) |
|---|---|---|---|---|---|---|---|---|---|
| 0.083 | 0.02 | 0.19 | 0.243 | O | \| | \| | \| | \| | 1.21 |
| 0.167 | 0.10 | 0.19 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 0.250 | 0.16 | 0.19 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 0.333 | 0.17 | 0.18 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 0.417 | 0.17 | 0.18 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 0.500 | 0.17 | 0.18 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 0.583 | 0.17 | 0.18 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 0.667 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.21 |
| 0.750 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.21 |
| 0.833 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.21 |
| 0.917 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.21 |
| 1.000 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 1.083 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 1.167 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 1.250 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 1.333 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 1.417 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 1.500 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 1.583 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 1.667 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 1.750 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 1.833 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 1.917 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 2.000 | 0.18 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 2.083 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 2.167 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 2.250 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 2.333 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 2.417 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 2.500 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 2.583 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 2.667 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 2.750 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 2.833 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.21 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.917 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.21 |
| 3.000 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.21 |
| 3.083 | 0.19 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.21 |
| 3.167 | 0.19 | 0.18 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 3.250 | 0.19 | 0.18 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 3.333 | 0.20 | 0.18 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 3.417 | 0.20 | 0.18 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 3.500 | 0.20 | 0.18 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 3.583 | 0.20 | 0.19 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 3.667 | 0.20 | 0.19 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 3.750 | 0.20 | 0.19 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 3.833 | 0.20 | 0.19 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 3.917 | 0.20 | 0.19 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 4.000 | 0.20 | 0.19 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 4.083 | 0.20 | 0.19 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 4.167 | 0.20 | 0.19 | 0.243 | O | \| | \| | \| | \| | 1.21 |
| 4.250 | 0.20 | 0.19 | 0.243 | O | \| | \| | \| | \| | 1.21 |
| 4.333 | 0.20 | 0.19 | 0.243 | O | \| | \| | \| | \| | 1.21 |
| 4.417 | 0.21 | 0.19 | 0.243 | O | \| | \| | \| | \| | 1.21 |
| 4.500 | 0.21 | 0.19 | 0.243 | O | \| | \| | \| | \| | 1.21 |
| 4.583 | 0.21 | 0.19 | 0.243 | O | \| | \| | \| | \| | 1.21 |
| 4.667 | 0.21 | 0.19 | 0.243 | O | \| | \| | \| | \| | 1.21 |
| 4.750 | 0.21 | 0.19 | 0.244 | O | \| | \| | \| | \| | 1.21 |
| 4.833 | 0.21 | 0.19 | 0.244 | O | \| | \| | \| | \| | 1.21 |
| 4.917 | 0.21 | 0.19 | 0.244 | O | \| | \| | \| | \| | 1.22 |
| 5.000 | 0.21 | 0.19 | 0.244 | O | \| | \| | \| | \| | 1.22 |
| 5.083 | 0.21 | 0.19 | 0.244 | O | \| | \| | \| | \| | 1.22 |
| 5.167 | 0.21 | 0.19 | 0.244 | O | \| | \| | \| | \| | 1.22 |
| 5.250 | 0.21 | 0.19 | 0.244 | O | \| | \| | \| | \| | 1.22 |
| 5.333 | 0.22 | 0.19 | 0.245 | O | \| | \| | \| | \| | 1.22 |
| 5.417 | 0.22 | 0.19 | 0.245 | O | \| | \| | \| | \| | 1.22 |
| 5.500 | 0.22 | 0.19 | 0.245 | O | \| | \| | \| | \| | 1.22 |
| 5.583 | 0.22 | 0.19 | 0.245 | O | \| | \| | \| | \| | 1.22 |
| 5.667 | 0.22 | 0.19 | 0.245 | O | \| | \| | \| | \| | 1.22 |
| 5.750 | 0.22 | 0.19 | 0.246 | O | \| | \| | \| | \| | 1.22 |
| 5.833 | 0.22 | 0.19 | 0.246 | O | \| | \| | \| | \| | 1.22 |
| 5.917 | 0.22 | 0.19 | 0.246 | O | \| | \| | \| | \| | 1.22 |
| 6.000 | 0.22 | 0.19 | 0.246 | O | \| | \| | \| | \| | 1.22 |
| 6.083 | 0.22 | 0.19 | 0.246 | O | \| | \| | \| | \| | 1.23 |
| 6.167 | 0.23 | 0.19 | 0.247 | O | \| | \| | \| | \| | 1.23 |
| 6.250 | 0.23 | 0.19 | 0.247 | O | \| | \| | \| | \| | 1.23 |
| 6.333 | 0.23 | 0.19 | 0.247 | O | \| | \| | \| | \| | 1.23 |
| 6.417 | 0.23 | 0.19 | 0.247 | O | \| | \| | \| | \| | 1.23 |
| 6.500 | 0.23 | 0.19 | 0.248 | O | \| | \| | \| | \| | 1.23 |
| 6.583 | 0.23 | 0.19 | 0.248 | O | \| | \| | \| | \| | 1.23 |
| 6.667 | 0.23 | 0.20 | 0.248 | O | \| | \| | \| | \| | 1.23 |
| 6.750 | 0.23 | 0.20 | 0.248 | O | \| | \| | \| | \| | 1.23 |
| 6.833 | 0.23 | 0.20 | 0.249 | O | \| | \| | \| | \| | 1.23 |
| 6.917 | 0.24 | 0.20 | 0.249 | O | \| | \| | \| | \| | 1.24 |
| 7.000 | 0.24 | 0.20 | 0.249 | O | \| | \| | \| | \| | 1.24 |
| 7.083 | 0.24 | 0.20 | 0.249 | O | \| | \| | \| | \| | 1.24 |
| 7.167 | 0.24 | 0.20 | 0.250 | O | \| | \| | \| | \| | 1.24 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 7.250 | 0.24 | 0.20 | 0.250 | O | | | | | 1.24 |
| 7.333 | 0.24 | 0.20 | 0.250 | O | | | | | 1.24 |
| 7.417 | 0.24 | 0.20 | 0.251 | O | | | | | 1.24 |
| 7.500 | 0.24 | 0.20 | 0.251 | O | | | | | 1.24 |
| 7.583 | 0.25 | 0.20 | 0.251 | O | | | | | 1.24 |
| 7.667 | 0.25 | 0.20 | 0.252 | O | | | | | 1.25 |
| 7.750 | 0.25 | 0.20 | 0.252 | O | | | | | 1.25 |
| 7.833 | 0.25 | 0.20 | 0.252 | O | | | | | 1.25 |
| 7.917 | 0.25 | 0.20 | 0.253 | O | | | | | 1.25 |
| 8.000 | 0.25 | 0.20 | 0.253 | O | | | | | 1.25 |
| 8.083 | 0.25 | 0.20 | 0.253 | O | | | | | 1.25 |
| 8.167 | 0.26 | 0.20 | 0.254 | O | | | | | 1.25 |
| 8.250 | 0.26 | 0.20 | 0.254 | O | | | | | 1.26 |
| 8.333 | 0.26 | 0.21 | 0.254 | O | | | | | 1.26 |
| 8.417 | 0.26 | 0.21 | 0.255 | OI | | | | | 1.26 |
| 8.500 | 0.26 | 0.21 | 0.255 | OI | | | | | 1.26 |
| 8.583 | 0.26 | 0.21 | 0.255 | OI | | | | | 1.26 |
| 8.667 | 0.27 | 0.21 | 0.256 | OI | | | | | 1.26 |
| 8.750 | 0.27 | 0.21 | 0.256 | OI | | | | | 1.26 |
| 8.833 | 0.27 | 0.21 | 0.257 | OI | | | | | 1.27 |
| 8.917 | 0.27 | 0.21 | 0.257 | OI | | | | | 1.27 |
| 9.000 | 0.27 | 0.21 | 0.257 | OI | | | | | 1.27 |
| 9.083 | 0.27 | 0.21 | 0.258 | OI | | | | | 1.27 |
| 9.167 | 0.28 | 0.21 | 0.258 | OI | | | | | 1.27 |
| 9.250 | 0.28 | 0.21 | 0.259 | OI | | | | | 1.28 |
| 9.333 | 0.28 | 0.21 | 0.259 | OI | | | | | 1.28 |
| 9.417 | 0.28 | 0.21 | 0.260 | OI | | | | | 1.28 |
| 9.500 | 0.28 | 0.22 | 0.260 | OI | | | | | 1.28 |
| 9.583 | 0.29 | 0.22 | 0.261 | OI | | | | | 1.28 |
| 9.667 | 0.29 | 0.22 | 0.261 | OI | | | | | 1.28 |
| 9.750 | 0.29 | 0.22 | 0.262 | OI | | | | | 1.29 |
| 9.833 | 0.29 | 0.22 | 0.262 | OI | | | | | 1.29 |
| 9.917 | 0.30 | 0.22 | 0.263 | OI | | | | | 1.29 |
| 10.000 | 0.30 | 0.22 | 0.263 | OI | | | | | 1.29 |
| 10.083 | 0.30 | 0.22 | 0.264 | OI | | | | | 1.30 |
| 10.167 | 0.30 | 0.22 | 0.264 | OI | | | | | 1.30 |
| 10.250 | 0.30 | 0.22 | 0.265 | OI | | | | | 1.30 |
| 10.333 | 0.31 | 0.22 | 0.265 | OI | | | | | 1.30 |
| 10.417 | 0.31 | 0.22 | 0.266 | OI | | | | | 1.30 |
| 10.500 | 0.31 | 0.23 | 0.267 | OI | | | | | 1.31 |
| 10.583 | 0.31 | 0.23 | 0.267 | OI | | | | | 1.31 |
| 10.667 | 0.32 | 0.23 | 0.268 | OI | | | | | 1.31 |
| 10.750 | 0.32 | 0.23 | 0.268 | OI | | | | | 1.31 |
| 10.833 | 0.32 | 0.23 | 0.269 | OI | | | | | 1.32 |
| 10.917 | 0.33 | 0.23 | 0.270 | OI | | | | | 1.32 |
| 11.000 | 0.33 | 0.23 | 0.270 | OI | | | | | 1.32 |
| 11.083 | 0.33 | 0.23 | 0.271 | OI | | | | | 1.32 |
| 11.167 | 0.34 | 0.23 | 0.272 | OI | | | | | 1.33 |
| 11.250 | 0.34 | 0.24 | 0.272 | OI | | | | | 1.33 |
| 11.333 | 0.34 | 0.24 | 0.273 | OI | | | | | 1.33 |
| 11.417 | 0.35 | 0.24 | 0.274 | OI | | | | | 1.34 |
| 11.500 | 0.35 | 0.24 | 0.275 | OI | | | | | 1.34 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 11.583 | 0.35 | 0.24 | 0.275 | OI | \| | \| | \| | 1.34 |
| 11.667 | 0.36 | 0.24 | 0.276 | OI | \| | \| | \| | 1.34 |
| 11.750 | 0.36 | 0.24 | 0.277 | OI | \| | \| | \| | 1.35 |
| 11.833 | 0.36 | 0.24 | 0.278 | OI | \| | \| | \| | 1.35 |
| 11.917 | 0.37 | 0.25 | 0.279 | OI | \| | \| | \| | 1.35 |
| 12.000 | 0.37 | 0.25 | 0.280 | OI | \| | \| | \| | 1.36 |
| 12.083 | 0.38 | 0.25 | 0.280 | OI | \| | \| | \| | 1.36 |
| 12.167 | 0.42 | 0.25 | 0.281 | OI | \| | \| | \| | 1.37 |
| 12.250 | 0.44 | 0.25 | 0.283 | OI | \| | \| | \| | 1.37 |
| 12.333 | 0.45 | 0.25 | 0.284 | OI | \| | \| | \| | 1.38 |
| 12.417 | 0.45 | 0.26 | 0.285 | OI | \| | \| | \| | 1.38 |
| 12.500 | 0.46 | 0.26 | 0.287 | OI | \| | \| | \| | 1.39 |
| 12.583 | 0.46 | 0.26 | 0.288 | \|O | \| | \| | \| | 1.39 |
| 12.667 | 0.47 | 0.26 | 0.289 | \|O | \| | \| | \| | 1.40 |
| 12.750 | 0.48 | 0.27 | 0.291 | \|O | \| | \| | \| | 1.40 |
| 12.833 | 0.48 | 0.27 | 0.292 | \|O | \| | \| | \| | 1.41 |
| 12.917 | 0.49 | 0.27 | 0.294 | \|O | \| | \| | \| | 1.42 |
| 13.000 | 0.49 | 0.27 | 0.295 | \|O | \| | \| | \| | 1.42 |
| 13.083 | 0.50 | 0.28 | 0.297 | \|O | \| | \| | \| | 1.43 |
| 13.167 | 0.51 | 0.28 | 0.298 | \|O | \| | \| | \| | 1.43 |
| 13.250 | 0.51 | 0.28 | 0.300 | \|O | \| | \| | \| | 1.44 |
| 13.333 | 0.52 | 0.28 | 0.302 | \|OI | \| | \| | \| | 1.45 |
| 13.417 | 0.53 | 0.29 | 0.303 | \|OI | \| | \| | \| | 1.45 |
| 13.500 | 0.54 | 0.29 | 0.305 | \|OI | \| | \| | \| | 1.46 |
| 13.583 | 0.55 | 0.29 | 0.307 | \|OI | \| | \| | \| | 1.47 |
| 13.667 | 0.56 | 0.29 | 0.309 | \|OI | \| | \| | \| | 1.47 |
| 13.750 | 0.57 | 0.30 | 0.310 | \|OI | \| | \| | \| | 1.48 |
| 13.833 | 0.58 | 0.30 | 0.312 | \|OI | \| | \| | \| | 1.49 |
| 13.917 | 0.59 | 0.30 | 0.314 | \|OI | \| | \| | \| | 1.50 |
| 14.000 | 0.60 | 0.31 | 0.316 | \|OI | \| | \| | \| | 1.50 |
| 14.083 | 0.61 | 0.31 | 0.318 | \|OI | \| | \| | \| | 1.51 |
| 14.167 | 0.62 | 0.31 | 0.320 | \|OI | \| | \| | \| | 1.52 |
| 14.250 | 0.64 | 0.32 | 0.323 | \|OI | \| | \| | \| | 1.53 |
| 14.333 | 0.65 | 0.32 | 0.325 | \|OI | \| | \| | \| | 1.54 |
| 14.417 | 0.67 | 0.32 | 0.327 | \|OI | \| | \| | \| | 1.55 |
| 14.500 | 0.68 | 0.33 | 0.329 | \|OI | \| | \| | \| | 1.56 |
| 14.583 | 0.70 | 0.33 | 0.332 | \|OI | \| | \| | \| | 1.57 |
| 14.667 | 0.72 | 0.34 | 0.335 | \|OI | \| | \| | \| | 1.58 |
| 14.750 | 0.74 | 0.34 | 0.337 | \|OI | \| | \| | \| | 1.59 |
| 14.833 | 0.77 | 0.35 | 0.340 | \|OI | \| | \| | \| | 1.60 |
| 14.917 | 0.79 | 0.35 | 0.343 | \|O I | \| | \| | \| | 1.61 |
| 15.000 | 0.82 | 0.36 | 0.346 | \|O I | \| | \| | \| | 1.62 |
| 15.083 | 0.85 | 0.36 | 0.349 | \|O I | \| | \| | \| | 1.64 |
| 15.167 | 0.89 | 0.37 | 0.353 | \|O I | \| | \| | \| | 1.65 |
| 15.250 | 0.92 | 0.37 | 0.357 | \|O I | \| | \| | \| | 1.67 |
| 15.333 | 0.97 | 0.38 | 0.360 | \|O I | \| | \| | \| | 1.68 |
| 15.417 | 1.00 | 0.39 | 0.365 | \|O I | \| | \| | \| | 1.70 |
| 15.500 | 0.96 | 0.39 | 0.369 | \|O I | \| | \| | \| | 1.71 |
| 15.583 | 0.97 | 0.40 | 0.373 | \|O I | \| | \| | \| | 1.73 |
| 15.667 | 1.05 | 0.41 | 0.377 | \|O  I | \| | \| | \| | 1.75 |
| 15.750 | 1.17 | 0.41 | 0.382 | \|O  I | \| | \| | \| | 1.77 |
| 15.833 | 1.34 | 0.42 | 0.387 | \|O   I | \| | \| | \| | 1.79 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 15.917 | 1.61 | 0.44 | 0.395 | O I | | | | 1.82 |
| 16.000 | 2.23 | 0.45 | 0.405 | O I | | | | 1.86 |
| 16.083 | 4.15 | 0.48 | 0.424 | O \| I | | | | 1.93 |
| 16.167 | 8.30 | 0.53 | 0.463 | O \| | | | I | 2.08 |
| 16.250 | 5.73 | 0.56 | 0.507 | O \| | | I | | 2.22 |
| 16.333 | 2.23 | 0.58 | 0.531 | O I | | | | 2.30 |
| 16.417 | 1.35 | 0.59 | 0.539 | O I \| | | | | 2.33 |
| 16.500 | 1.07 | 0.59 | 0.544 | O I \| | | | | 2.35 |
| 16.583 | 1.00 | 0.60 | 0.547 | OI \| | | | | 2.36 |
| 16.667 | 0.91 | 0.60 | 0.549 | OI \| | | | | 2.36 |
| 16.750 | 0.84 | 0.60 | 0.551 | OI \| | | | | 2.37 |
| 16.833 | 0.78 | 0.60 | 0.552 | OI \| | | | | 2.37 |
| 16.917 | 0.74 | 0.60 | 0.554 | O \| | | | | 2.38 |
| 17.000 | 0.70 | 0.60 | 0.554 | O \| | | | | 2.38 |
| 17.083 | 0.66 | 0.60 | 0.555 | O \| | | | | 2.38 |
| 17.167 | 0.63 | 0.60 | 0.555 | O \| | | | | 2.38 |
| 17.250 | 0.61 | 0.60 | 0.555 | O \| | | | | 2.38 |
| 17.333 | 0.58 | 0.60 | 0.555 | O \| | | | | 2.38 |
| 17.417 | 0.56 | 0.60 | 0.555 | O \| | | | | 2.38 |
| 17.500 | 0.54 | 0.60 | 0.555 | O \| | | | | 2.38 |
| 17.583 | 0.53 | 0.60 | 0.554 | O \| | | | | 2.38 |
| 17.667 | 0.51 | 0.60 | 0.554 | IO \| | | | | 2.38 |
| 17.750 | 0.50 | 0.60 | 0.553 | IO \| | | | | 2.38 |
| 17.833 | 0.49 | 0.60 | 0.552 | IO \| | | | | 2.37 |
| 17.917 | 0.47 | 0.60 | 0.551 | IO \| | | | | 2.37 |
| 18.000 | 0.46 | 0.60 | 0.551 | IO \| | | | | 2.37 |
| 18.083 | 0.45 | 0.60 | 0.550 | IO \| | | | | 2.37 |
| 18.167 | 0.41 | 0.60 | 0.548 | IO \| | | | | 2.36 |
| 18.250 | 0.38 | 0.60 | 0.547 | IO \| | | | | 2.36 |
| 18.333 | 0.37 | 0.59 | 0.546 | IO \| | | | | 2.35 |
| 18.417 | 0.36 | 0.59 | 0.544 | IO \| | | | | 2.35 |
| 18.500 | 0.35 | 0.59 | 0.542 | IO \| | | | | 2.34 |
| 18.583 | 0.34 | 0.59 | 0.541 | IO \| | | | | 2.34 |
| 18.667 | 0.34 | 0.59 | 0.539 | IO \| | | | | 2.33 |
| 18.750 | 0.33 | 0.59 | 0.537 | IO \| | | | | 2.32 |
| 18.833 | 0.33 | 0.59 | 0.535 | IO \| | | | | 2.32 |
| 18.917 | 0.32 | 0.58 | 0.534 | IO \| | | | | 2.31 |
| 19.000 | 0.31 | 0.58 | 0.532 | IO \| | | | | 2.31 |
| 19.083 | 0.31 | 0.58 | 0.530 | IO \| | | | | 2.30 |
| 19.167 | 0.30 | 0.58 | 0.528 | IO \| | | | | 2.29 |
| 19.250 | 0.30 | 0.58 | 0.526 | IO \| | | | | 2.29 |
| 19.333 | 0.29 | 0.58 | 0.524 | IO \| | | | | 2.28 |
| 19.417 | 0.29 | 0.58 | 0.522 | IO \| | | | | 2.27 |
| 19.500 | 0.29 | 0.57 | 0.520 | IO \| | | | | 2.27 |
| 19.583 | 0.28 | 0.57 | 0.518 | IO \| | | | | 2.26 |
| 19.667 | 0.28 | 0.57 | 0.516 | IO \| | | | | 2.25 |
| 19.750 | 0.27 | 0.57 | 0.514 | IO \| | | | | 2.25 |
| 19.833 | 0.27 | 0.57 | 0.512 | IO \| | | | | 2.24 |
| 19.917 | 0.27 | 0.57 | 0.510 | IO \| | | | | 2.23 |
| 20.000 | 0.26 | 0.56 | 0.508 | IO \| | | | | 2.23 |
| 20.083 | 0.26 | 0.56 | 0.506 | IO \| | | | | 2.22 |
| 20.167 | 0.26 | 0.56 | 0.504 | I O \| | | | | 2.21 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 20.250 | 0.25 | 0.56 | 0.502 | I O | | | | 2.21 |
| 20.333 | 0.25 | 0.56 | 0.500 | I O | | | | 2.20 |
| 20.417 | 0.25 | 0.56 | 0.497 | I O | | | | 2.19 |
| 20.500 | 0.25 | 0.55 | 0.495 | I O | | | | 2.18 |
| 20.583 | 0.24 | 0.55 | 0.493 | I O | | | | 2.18 |
| 20.667 | 0.24 | 0.55 | 0.491 | I O | | | | 2.17 |
| 20.750 | 0.24 | 0.55 | 0.489 | I O | | | | 2.16 |
| 20.833 | 0.24 | 0.55 | 0.487 | I O | | | | 2.16 |
| 20.917 | 0.23 | 0.55 | 0.485 | I O | | | | 2.15 |
| 21.000 | 0.23 | 0.54 | 0.483 | I O | | | | 2.14 |
| 21.083 | 0.23 | 0.54 | 0.480 | I O | | | | 2.13 |
| 21.167 | 0.23 | 0.54 | 0.478 | I O | | | | 2.13 |
| 21.250 | 0.22 | 0.54 | 0.476 | I O | | | | 2.12 |
| 21.333 | 0.22 | 0.54 | 0.474 | I O | | | | 2.11 |
| 21.417 | 0.22 | 0.54 | 0.472 | I O | | | | 2.11 |
| 21.500 | 0.22 | 0.53 | 0.470 | I O | | | | 2.10 |
| 21.583 | 0.22 | 0.53 | 0.467 | I O | | | | 2.09 |
| 21.667 | 0.21 | 0.53 | 0.465 | I O | | | | 2.08 |
| 21.750 | 0.21 | 0.53 | 0.463 | I O | | | | 2.08 |
| 21.833 | 0.21 | 0.53 | 0.461 | I O | | | | 2.07 |
| 21.917 | 0.21 | 0.52 | 0.459 | I O | | | | 2.06 |
| 22.000 | 0.21 | 0.52 | 0.456 | I O | | | | 2.05 |
| 22.083 | 0.21 | 0.52 | 0.454 | I O | | | | 2.05 |
| 22.167 | 0.20 | 0.52 | 0.452 | I O | | | | 2.04 |
| 22.250 | 0.20 | 0.52 | 0.450 | IO | | | | 2.03 |
| 22.333 | 0.20 | 0.52 | 0.448 | IO | | | | 2.03 |
| 22.417 | 0.20 | 0.51 | 0.446 | IO | | | | 2.02 |
| 22.500 | 0.20 | 0.51 | 0.443 | IO | | | | 2.01 |
| 22.583 | 0.20 | 0.51 | 0.441 | IO | | | | 2.00 |
| 22.667 | 0.19 | 0.51 | 0.439 | IO | | | | 2.00 |
| 22.750 | 0.19 | 0.50 | 0.437 | IO | | | | 1.99 |
| 22.833 | 0.19 | 0.50 | 0.435 | IO | | | | 1.98 |
| 22.917 | 0.19 | 0.50 | 0.433 | IO | | | | 1.97 |
| 23.000 | 0.19 | 0.49 | 0.431 | IO | | | | 1.96 |
| 23.083 | 0.19 | 0.49 | 0.428 | IO | | | | 1.95 |
| 23.167 | 0.19 | 0.49 | 0.426 | IO | | | | 1.95 |
| 23.250 | 0.19 | 0.48 | 0.424 | IO | | | | 1.94 |
| 23.333 | 0.18 | 0.48 | 0.422 | IO | | | | 1.93 |
| 23.417 | 0.18 | 0.48 | 0.420 | IO | | | | 1.92 |
| 23.500 | 0.18 | 0.47 | 0.418 | IO | | | | 1.91 |
| 23.583 | 0.18 | 0.47 | 0.416 | IO | | | | 1.90 |
| 23.667 | 0.18 | 0.47 | 0.414 | IO | | | | 1.90 |
| 23.750 | 0.18 | 0.46 | 0.412 | IO | | | | 1.89 |
| 23.833 | 0.18 | 0.46 | 0.410 | IO | | | | 1.88 |
| 23.917 | 0.18 | 0.46 | 0.408 | IO | | | | 1.87 |
| 24.000 | 0.17 | 0.45 | 0.406 | IO | | | | 1.87 |
| 24.083 | 0.16 | 0.45 | 0.404 | IO | | | | 1.86 |
| 24.167 | 0.07 | 0.45 | 0.402 | IO | | | | 1.85 |
| 24.250 | 0.01 | 0.44 | 0.399 | IO | | | | 1.84 |
| 24.333 | 0.00 | 0.44 | 0.396 | IO | | | | 1.83 |
| 24.417 | 0.00 | 0.43 | 0.393 | IO | | | | 1.81 |
| 24.500 | 0.00 | 0.43 | 0.390 | IO | | | | 1.80 |

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|---|---|---|---|---|---|---|---|---|
| 24.583 | 0.00 | 0.42 | 0.387 | IO | | | | 1.79 |
| 24.667 | 0.00 | 0.42 | 0.384 | IO | | | | 1.78 |
| 24.750 | 0.00 | 0.41 | 0.382 | IO | | | | 1.77 |
| 24.833 | 0.00 | 0.41 | 0.379 | IO | | | | 1.76 |
| 24.917 | 0.00 | 0.40 | 0.376 | IO | | | | 1.74 |
| 25.000 | 0.00 | 0.40 | 0.373 | IO | | | | 1.73 |
| 25.083 | 0.00 | 0.40 | 0.370 | IO | | | | 1.72 |
| 25.167 | 0.00 | 0.39 | 0.368 | IO | | | | 1.71 |
| 25.250 | 0.00 | 0.39 | 0.365 | IO | | | | 1.70 |
| 25.333 | 0.00 | 0.38 | 0.362 | IO | | | | 1.69 |
| 25.417 | 0.00 | 0.38 | 0.360 | IO | | | | 1.68 |
| 25.500 | 0.00 | 0.37 | 0.357 | IO | | | | 1.67 |
| 25.583 | 0.00 | 0.37 | 0.355 | IO | | | | 1.66 |
| 25.667 | 0.00 | 0.37 | 0.352 | IO | | | | 1.65 |
| 25.750 | 0.00 | 0.36 | 0.350 | IO | | | | 1.64 |
| 25.833 | 0.00 | 0.36 | 0.347 | IO | | | | 1.63 |
| 25.917 | 0.00 | 0.35 | 0.345 | IO | | | | 1.62 |
| 26.000 | 0.00 | 0.35 | 0.342 | IO | | | | 1.61 |
| 26.083 | 0.00 | 0.35 | 0.340 | IO | | | | 1.60 |
| 26.167 | 0.00 | 0.34 | 0.337 | IO | | | | 1.59 |
| 26.250 | 0.00 | 0.34 | 0.335 | IO | | | | 1.58 |
| 26.333 | 0.00 | 0.33 | 0.333 | IO | | | | 1.57 |
| 26.417 | 0.00 | 0.33 | 0.331 | IO | | | | 1.56 |
| 26.500 | 0.00 | 0.33 | 0.328 | IO | | | | 1.55 |
| 26.583 | 0.00 | 0.32 | 0.326 | IO | | | | 1.54 |
| 26.667 | 0.00 | 0.32 | 0.324 | IO | | | | 1.54 |
| 26.750 | 0.00 | 0.32 | 0.322 | IO | | | | 1.53 |
| 26.833 | 0.00 | 0.31 | 0.319 | IO | | | | 1.52 |
| 26.917 | 0.00 | 0.31 | 0.317 | IO | | | | 1.51 |
| 27.000 | 0.00 | 0.31 | 0.315 | IO | | | | 1.50 |
| 27.083 | 0.00 | 0.30 | 0.313 | IO | | | | 1.49 |
| 27.167 | 0.00 | 0.30 | 0.311 | IO | | | | 1.48 |
| 27.250 | 0.00 | 0.30 | 0.309 | IO | | | | 1.48 |
| 27.333 | 0.00 | 0.29 | 0.307 | IO | | | | 1.47 |
| 27.417 | 0.00 | 0.29 | 0.305 | IO | | | | 1.46 |
| 27.500 | 0.00 | 0.29 | 0.303 | IO | | | | 1.45 |
| 27.583 | 0.00 | 0.28 | 0.301 | IO | | | | 1.44 |
| 27.667 | 0.00 | 0.28 | 0.299 | IO | | | | 1.44 |
| 27.750 | 0.00 | 0.28 | 0.297 | IO | | | | 1.43 |
| 27.833 | 0.00 | 0.27 | 0.295 | IO | | | | 1.42 |
| 27.917 | 0.00 | 0.27 | 0.293 | IO | | | | 1.41 |
| 28.000 | 0.00 | 0.27 | 0.292 | IO | | | | 1.41 |
| 28.083 | 0.00 | 0.26 | 0.290 | IO | | | | 1.40 |
| 28.167 | 0.00 | 0.26 | 0.288 | IO | | | | 1.39 |
| 28.250 | 0.00 | 0.26 | 0.286 | O | | | | 1.38 |
| 28.333 | 0.00 | 0.25 | 0.284 | O | | | | 1.38 |
| 28.417 | 0.00 | 0.25 | 0.283 | O | | | | 1.37 |
| 28.500 | 0.00 | 0.25 | 0.281 | O | | | | 1.36 |
| 28.583 | 0.00 | 0.25 | 0.279 | O | | | | 1.36 |
| 28.667 | 0.00 | 0.24 | 0.278 | O | | | | 1.35 |
| 28.750 | 0.00 | 0.24 | 0.276 | O | | | | 1.34 |
| 28.833 | 0.00 | 0.24 | 0.274 | O | | | | 1.34 |

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|---|---|---|---|---|---|---|---|---|---|
| 28.917 | 0.00 | 0.24 | 0.273 | O | \| | \| | \| | \| | 1.33 |
| 29.000 | 0.00 | 0.23 | 0.271 | O | \| | \| | \| | \| | 1.32 |
| 29.083 | 0.00 | 0.23 | 0.269 | O | \| | \| | \| | \| | 1.32 |
| 29.167 | 0.00 | 0.23 | 0.268 | O | \| | \| | \| | \| | 1.31 |
| 29.250 | 0.00 | 0.23 | 0.266 | O | \| | \| | \| | \| | 1.31 |
| 29.333 | 0.00 | 0.22 | 0.265 | O | \| | \| | \| | \| | 1.30 |
| 29.417 | 0.00 | 0.22 | 0.263 | O | \| | \| | \| | \| | 1.29 |
| 29.500 | 0.00 | 0.22 | 0.262 | O | \| | \| | \| | \| | 1.29 |
| 29.583 | 0.00 | 0.22 | 0.260 | O | \| | \| | \| | \| | 1.28 |
| 29.667 | 0.00 | 0.21 | 0.259 | O | \| | \| | \| | \| | 1.27 |
| 29.750 | 0.00 | 0.21 | 0.257 | O | \| | \| | \| | \| | 1.27 |
| 29.833 | 0.00 | 0.21 | 0.256 | O | \| | \| | \| | \| | 1.26 |
| 29.917 | 0.00 | 0.21 | 0.254 | O | \| | \| | \| | \| | 1.26 |
| 30.000 | 0.00 | 0.20 | 0.253 | O | \| | \| | \| | \| | 1.25 |
| 30.083 | 0.00 | 0.20 | 0.252 | O | \| | \| | \| | \| | 1.25 |
| 30.167 | 0.00 | 0.20 | 0.250 | O | \| | \| | \| | \| | 1.24 |
| 30.250 | 0.00 | 0.20 | 0.249 | O | \| | \| | \| | \| | 1.24 |
| 30.333 | 0.00 | 0.19 | 0.248 | O | \| | \| | \| | \| | 1.23 |
| 30.417 | 0.00 | 0.19 | 0.246 | O | \| | \| | \| | \| | 1.22 |
| 30.500 | 0.00 | 0.19 | 0.245 | O | \| | \| | \| | \| | 1.22 |
| 30.583 | 0.00 | 0.19 | 0.244 | O | \| | \| | \| | \| | 1.21 |
| 30.667 | 0.00 | 0.19 | 0.242 | O | \| | \| | \| | \| | 1.21 |
| 30.750 | 0.00 | 0.18 | 0.241 | O | \| | \| | \| | \| | 1.20 |
| 30.833 | 0.00 | 0.18 | 0.240 | O | \| | \| | \| | \| | 1.20 |
| 30.917 | 0.00 | 0.18 | 0.239 | O | \| | \| | \| | \| | 1.19 |
| 31.000 | 0.00 | 0.18 | 0.237 | O | \| | \| | \| | \| | 1.19 |
| 31.083 | 0.00 | 0.18 | 0.236 | O | \| | \| | \| | \| | 1.18 |
| 31.167 | 0.00 | 0.17 | 0.235 | O | \| | \| | \| | \| | 1.18 |
| 31.250 | 0.00 | 0.17 | 0.234 | O | \| | \| | \| | \| | 1.17 |
| 31.333 | 0.00 | 0.17 | 0.233 | O | \| | \| | \| | \| | 1.17 |
| 31.417 | 0.00 | 0.17 | 0.231 | O | \| | \| | \| | \| | 1.17 |
| 31.500 | 0.00 | 0.17 | 0.230 | O | \| | \| | \| | \| | 1.16 |
| 31.583 | 0.00 | 0.16 | 0.229 | O | \| | \| | \| | \| | 1.16 |
| 31.667 | 0.00 | 0.16 | 0.228 | O | \| | \| | \| | \| | 1.15 |
| 31.750 | 0.00 | 0.16 | 0.227 | O | \| | \| | \| | \| | 1.15 |
| 31.833 | 0.00 | 0.16 | 0.226 | O | \| | \| | \| | \| | 1.14 |
| 31.917 | 0.00 | 0.16 | 0.225 | O | \| | \| | \| | \| | 1.14 |
| 32.000 | 0.00 | 0.16 | 0.224 | O | \| | \| | \| | \| | 1.13 |
| 32.083 | 0.00 | 0.15 | 0.223 | O | \| | \| | \| | \| | 1.13 |
| 32.167 | 0.00 | 0.15 | 0.221 | O | \| | \| | \| | \| | 1.13 |
| 32.250 | 0.00 | 0.15 | 0.220 | O | \| | \| | \| | \| | 1.12 |
| 32.333 | 0.00 | 0.15 | 0.219 | O | \| | \| | \| | \| | 1.12 |
| 32.417 | 0.00 | 0.15 | 0.218 | O | \| | \| | \| | \| | 1.11 |
| 32.500 | 0.00 | 0.14 | 0.217 | O | \| | \| | \| | \| | 1.11 |
| 32.583 | 0.00 | 0.14 | 0.216 | O | \| | \| | \| | \| | 1.11 |
| 32.667 | 0.00 | 0.14 | 0.215 | O | \| | \| | \| | \| | 1.10 |
| 32.750 | 0.00 | 0.14 | 0.214 | O | \| | \| | \| | \| | 1.10 |
| 32.833 | 0.00 | 0.14 | 0.213 | O | \| | \| | \| | \| | 1.09 |
| 32.917 | 0.00 | 0.14 | 0.213 | O | \| | \| | \| | \| | 1.09 |
| 33.000 | 0.00 | 0.14 | 0.212 | O | \| | \| | \| | \| | 1.09 |
| 33.083 | 0.00 | 0.13 | 0.211 | O | \| | \| | \| | \| | 1.08 |
| 33.167 | 0.00 | 0.13 | 0.210 | O | \| | \| | \| | \| | 1.08 |

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|---|---|---|---|---|---|---|---|---|
| 33.250 | 0.00 | 0.13 | 0.209 | O | \| | \| | \| | 1.08 |
| 33.333 | 0.00 | 0.13 | 0.208 | O | \| | \| | \| | 1.07 |
| 33.417 | 0.00 | 0.13 | 0.207 | O | \| | \| | \| | 1.07 |
| 33.500 | 0.00 | 0.13 | 0.206 | O | \| | \| | \| | 1.06 |
| 33.583 | 0.00 | 0.13 | 0.205 | O | \| | \| | \| | 1.06 |
| 33.667 | 0.00 | 0.12 | 0.204 | O | \| | \| | \| | 1.06 |
| 33.750 | 0.00 | 0.12 | 0.204 | O | \| | \| | \| | 1.05 |
| 33.833 | 0.00 | 0.12 | 0.203 | O | \| | \| | \| | 1.05 |
| 33.917 | 0.00 | 0.12 | 0.202 | O | \| | \| | \| | 1.05 |
| 34.000 | 0.00 | 0.12 | 0.201 | O | \| | \| | \| | 1.04 |
| 34.083 | 0.00 | 0.12 | 0.200 | O | \| | \| | \| | 1.04 |
| 34.167 | 0.00 | 0.12 | 0.200 | O | \| | \| | \| | 1.04 |
| 34.250 | 0.00 | 0.11 | 0.199 | O | \| | \| | \| | 1.03 |
| 34.333 | 0.00 | 0.11 | 0.198 | O | \| | \| | \| | 1.03 |
| 34.417 | 0.00 | 0.11 | 0.197 | O | \| | \| | \| | 1.03 |
| 34.500 | 0.00 | 0.11 | 0.196 | O | \| | \| | \| | 1.03 |
| 34.583 | 0.00 | 0.11 | 0.196 | O | \| | \| | \| | 1.02 |
| 34.667 | 0.00 | 0.11 | 0.195 | O | \| | \| | \| | 1.02 |
| 34.750 | 0.00 | 0.11 | 0.194 | O | \| | \| | \| | 1.02 |
| 34.833 | 0.00 | 0.11 | 0.193 | O | \| | \| | \| | 1.01 |
| 34.917 | 0.00 | 0.10 | 0.193 | O | \| | \| | \| | 1.01 |
| 35.000 | 0.00 | 0.10 | 0.192 | O | \| | \| | \| | 1.01 |
| 35.083 | 0.00 | 0.10 | 0.191 | O | \| | \| | \| | 1.01 |
| 35.167 | 0.00 | 0.10 | 0.191 | O | \| | \| | \| | 1.00 |
| 35.250 | 0.00 | 0.10 | 0.190 | O | \| | \| | \| | 1.00 |
| 35.333 | 0.00 | 0.10 | 0.189 | O | \| | \| | \| | 1.00 |
| 35.417 | 0.00 | 0.10 | 0.189 | O | \| | \| | \| | 0.99 |
| 35.500 | 0.00 | 0.10 | 0.188 | O | \| | \| | \| | 0.99 |
| 35.583 | 0.00 | 0.10 | 0.187 | O | \| | \| | \| | 0.98 |
| 35.667 | 0.00 | 0.10 | 0.186 | O | \| | \| | \| | 0.98 |
| 35.750 | 0.00 | 0.10 | 0.186 | O | \| | \| | \| | 0.98 |
| 35.833 | 0.00 | 0.10 | 0.185 | O | \| | \| | \| | 0.97 |
| 35.917 | 0.00 | 0.10 | 0.184 | O | \| | \| | \| | 0.97 |
| 36.000 | 0.00 | 0.10 | 0.184 | O | \| | \| | \| | 0.97 |
| 36.083 | 0.00 | 0.10 | 0.183 | O | \| | \| | \| | 0.96 |
| 36.167 | 0.00 | 0.10 | 0.182 | O | \| | \| | \| | 0.96 |
| 36.250 | 0.00 | 0.10 | 0.182 | O | \| | \| | \| | 0.96 |
| 36.333 | 0.00 | 0.10 | 0.181 | O | \| | \| | \| | 0.95 |
| 36.417 | 0.00 | 0.09 | 0.180 | O | \| | \| | \| | 0.95 |
| 36.500 | 0.00 | 0.09 | 0.180 | O | \| | \| | \| | 0.95 |
| 36.583 | 0.00 | 0.09 | 0.179 | O | \| | \| | \| | 0.94 |
| 36.667 | 0.00 | 0.09 | 0.179 | O | \| | \| | \| | 0.94 |
| 36.750 | 0.00 | 0.09 | 0.178 | O | \| | \| | \| | 0.94 |
| 36.833 | 0.00 | 0.09 | 0.177 | O | \| | \| | \| | 0.93 |
| 36.917 | 0.00 | 0.09 | 0.177 | O | \| | \| | \| | 0.93 |
| 37.000 | 0.00 | 0.09 | 0.176 | O | \| | \| | \| | 0.93 |
| 37.083 | 0.00 | 0.09 | 0.175 | O | \| | \| | \| | 0.92 |
| 37.167 | 0.00 | 0.09 | 0.175 | O | \| | \| | \| | 0.92 |
| 37.250 | 0.00 | 0.09 | 0.174 | O | \| | \| | \| | 0.92 |
| 37.333 | 0.00 | 0.09 | 0.173 | O | \| | \| | \| | 0.91 |
| 37.417 | 0.00 | 0.09 | 0.173 | O | \| | \| | \| | 0.91 |
| 37.500 | 0.00 | 0.09 | 0.172 | O | \| | \| | \| | 0.91 |

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|---|---|---|---|---|---|---|---|---|
| 37.583 | 0.00 | 0.09 | 0.172 | O | \| | \| | \| | 0.90 |
| 37.667 | 0.00 | 0.09 | 0.171 | O | \| | \| | \| | 0.90 |
| 37.750 | 0.00 | 0.09 | 0.170 | O | \| | \| | \| | 0.90 |
| 37.833 | 0.00 | 0.09 | 0.170 | O | \| | \| | \| | 0.89 |
| 37.917 | 0.00 | 0.09 | 0.169 | O | \| | \| | \| | 0.89 |
| 38.000 | 0.00 | 0.09 | 0.168 | O | \| | \| | \| | 0.89 |
| 38.083 | 0.00 | 0.09 | 0.168 | O | \| | \| | \| | 0.88 |
| 38.167 | 0.00 | 0.09 | 0.167 | O | \| | \| | \| | 0.88 |
| 38.250 | 0.00 | 0.09 | 0.167 | O | \| | \| | \| | 0.88 |
| 38.333 | 0.00 | 0.09 | 0.166 | O | \| | \| | \| | 0.87 |
| 38.417 | 0.00 | 0.09 | 0.165 | O | \| | \| | \| | 0.87 |
| 38.500 | 0.00 | 0.09 | 0.165 | O | \| | \| | \| | 0.87 |
| 38.583 | 0.00 | 0.09 | 0.164 | O | \| | \| | \| | 0.86 |
| 38.667 | 0.00 | 0.09 | 0.164 | O | \| | \| | \| | 0.86 |
| 38.750 | 0.00 | 0.09 | 0.163 | O | \| | \| | \| | 0.86 |
| 38.833 | 0.00 | 0.09 | 0.162 | O | \| | \| | \| | 0.86 |
| 38.917 | 0.00 | 0.09 | 0.162 | O | \| | \| | \| | 0.85 |
| 39.000 | 0.00 | 0.08 | 0.161 | O | \| | \| | \| | 0.85 |
| 39.083 | 0.00 | 0.08 | 0.161 | O | \| | \| | \| | 0.85 |
| 39.167 | 0.00 | 0.08 | 0.160 | O | \| | \| | \| | 0.84 |
| 39.250 | 0.00 | 0.08 | 0.160 | O | \| | \| | \| | 0.84 |
| 39.333 | 0.00 | 0.08 | 0.159 | O | \| | \| | \| | 0.84 |
| 39.417 | 0.00 | 0.08 | 0.158 | O | \| | \| | \| | 0.83 |
| 39.500 | 0.00 | 0.08 | 0.158 | O | \| | \| | \| | 0.83 |
| 39.583 | 0.00 | 0.08 | 0.157 | O | \| | \| | \| | 0.83 |
| 39.667 | 0.00 | 0.08 | 0.157 | O | \| | \| | \| | 0.82 |
| 39.750 | 0.00 | 0.08 | 0.156 | O | \| | \| | \| | 0.82 |
| 39.833 | 0.00 | 0.08 | 0.156 | O | \| | \| | \| | 0.82 |
| 39.917 | 0.00 | 0.08 | 0.155 | O | \| | \| | \| | 0.82 |
| 40.000 | 0.00 | 0.08 | 0.154 | O | \| | \| | \| | 0.81 |
| 40.083 | 0.00 | 0.08 | 0.154 | O | \| | \| | \| | 0.81 |
| 40.167 | 0.00 | 0.08 | 0.153 | O | \| | \| | \| | 0.81 |
| 40.250 | 0.00 | 0.08 | 0.153 | O | \| | \| | \| | 0.80 |
| 40.333 | 0.00 | 0.08 | 0.152 | O | \| | \| | \| | 0.80 |
| 40.417 | 0.00 | 0.08 | 0.152 | O | \| | \| | \| | 0.80 |
| 40.500 | 0.00 | 0.08 | 0.151 | O | \| | \| | \| | 0.80 |
| 40.583 | 0.00 | 0.08 | 0.151 | O | \| | \| | \| | 0.79 |
| 40.667 | 0.00 | 0.08 | 0.150 | O | \| | \| | \| | 0.79 |
| 40.750 | 0.00 | 0.08 | 0.149 | O | \| | \| | \| | 0.79 |
| 40.833 | 0.00 | 0.08 | 0.149 | O | \| | \| | \| | 0.78 |
| 40.917 | 0.00 | 0.08 | 0.148 | O | \| | \| | \| | 0.78 |
| 41.000 | 0.00 | 0.08 | 0.148 | O | \| | \| | \| | 0.78 |
| 41.083 | 0.00 | 0.08 | 0.147 | O | \| | \| | \| | 0.78 |
| 41.167 | 0.00 | 0.08 | 0.147 | O | \| | \| | \| | 0.77 |
| 41.250 | 0.00 | 0.08 | 0.146 | O | \| | \| | \| | 0.77 |
| 41.333 | 0.00 | 0.08 | 0.146 | O | \| | \| | \| | 0.77 |
| 41.417 | 0.00 | 0.08 | 0.145 | O | \| | \| | \| | 0.76 |
| 41.500 | 0.00 | 0.08 | 0.145 | O | \| | \| | \| | 0.76 |
| 41.583 | 0.00 | 0.08 | 0.144 | O | \| | \| | \| | 0.76 |
| 41.667 | 0.00 | 0.08 | 0.144 | O | \| | \| | \| | 0.76 |
| 41.750 | 0.00 | 0.08 | 0.143 | O | \| | \| | \| | 0.75 |
| 41.833 | 0.00 | 0.08 | 0.143 | O | \| | \| | \| | 0.75 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 41.917 | 0.00 | 0.07 | 0.142 | O | \| | \| | \| | 0.75 |
| 42.000 | 0.00 | 0.07 | 0.142 | O | \| | \| | \| | 0.75 |
| 42.083 | 0.00 | 0.07 | 0.141 | O | \| | \| | \| | 0.74 |
| 42.167 | 0.00 | 0.07 | 0.141 | O | \| | \| | \| | 0.74 |
| 42.250 | 0.00 | 0.07 | 0.140 | O | \| | \| | \| | 0.74 |
| 42.333 | 0.00 | 0.07 | 0.140 | O | \| | \| | \| | 0.73 |
| 42.417 | 0.00 | 0.07 | 0.139 | O | \| | \| | \| | 0.73 |
| 42.500 | 0.00 | 0.07 | 0.139 | O | \| | \| | \| | 0.73 |
| 42.583 | 0.00 | 0.07 | 0.138 | O | \| | \| | \| | 0.73 |
| 42.667 | 0.00 | 0.07 | 0.138 | O | \| | \| | \| | 0.72 |
| 42.750 | 0.00 | 0.07 | 0.137 | O | \| | \| | \| | 0.72 |
| 42.833 | 0.00 | 0.07 | 0.137 | O | \| | \| | \| | 0.72 |
| 42.917 | 0.00 | 0.07 | 0.136 | O | \| | \| | \| | 0.72 |
| 43.000 | 0.00 | 0.07 | 0.136 | O | \| | \| | \| | 0.71 |
| 43.083 | 0.00 | 0.07 | 0.135 | O | \| | \| | \| | 0.71 |
| 43.167 | 0.00 | 0.07 | 0.135 | O | \| | \| | \| | 0.71 |
| 43.250 | 0.00 | 0.07 | 0.134 | O | \| | \| | \| | 0.71 |
| 43.333 | 0.00 | 0.07 | 0.134 | O | \| | \| | \| | 0.70 |
| 43.417 | 0.00 | 0.07 | 0.133 | O | \| | \| | \| | 0.70 |
| 43.500 | 0.00 | 0.07 | 0.133 | O | \| | \| | \| | 0.70 |
| 43.583 | 0.00 | 0.07 | 0.132 | O | \| | \| | \| | 0.70 |
| 43.667 | 0.00 | 0.07 | 0.132 | O | \| | \| | \| | 0.69 |
| 43.750 | 0.00 | 0.07 | 0.131 | O | \| | \| | \| | 0.69 |
| 43.833 | 0.00 | 0.07 | 0.131 | O | \| | \| | \| | 0.69 |
| 43.917 | 0.00 | 0.07 | 0.130 | O | \| | \| | \| | 0.69 |
| 44.000 | 0.00 | 0.07 | 0.130 | O | \| | \| | \| | 0.68 |
| 44.083 | 0.00 | 0.07 | 0.129 | O | \| | \| | \| | 0.68 |
| 44.167 | 0.00 | 0.07 | 0.129 | O | \| | \| | \| | 0.68 |
| 44.250 | 0.00 | 0.07 | 0.128 | O | \| | \| | \| | 0.68 |
| 44.333 | 0.00 | 0.07 | 0.128 | O | \| | \| | \| | 0.67 |
| 44.417 | 0.00 | 0.07 | 0.127 | O | \| | \| | \| | 0.67 |
| 44.500 | 0.00 | 0.07 | 0.127 | O | \| | \| | \| | 0.67 |
| 44.583 | 0.00 | 0.07 | 0.127 | O | \| | \| | \| | 0.67 |
| 44.667 | 0.00 | 0.07 | 0.126 | O | \| | \| | \| | 0.66 |
| 44.750 | 0.00 | 0.07 | 0.126 | O | \| | \| | \| | 0.66 |
| 44.833 | 0.00 | 0.07 | 0.125 | O | \| | \| | \| | 0.66 |
| 44.917 | 0.00 | 0.07 | 0.125 | O | \| | \| | \| | 0.66 |
| 45.000 | 0.00 | 0.07 | 0.124 | O | \| | \| | \| | 0.65 |
| 45.083 | 0.00 | 0.07 | 0.124 | O | \| | \| | \| | 0.65 |
| 45.167 | 0.00 | 0.06 | 0.123 | O | \| | \| | \| | 0.65 |
| 45.250 | 0.00 | 0.06 | 0.123 | O | \| | \| | \| | 0.65 |
| 45.333 | 0.00 | 0.06 | 0.122 | O | \| | \| | \| | 0.64 |
| 45.417 | 0.00 | 0.06 | 0.122 | O | \| | \| | \| | 0.64 |
| 45.500 | 0.00 | 0.06 | 0.122 | O | \| | \| | \| | 0.64 |
| 45.583 | 0.00 | 0.06 | 0.121 | O | \| | \| | \| | 0.64 |
| 45.667 | 0.00 | 0.06 | 0.121 | O | \| | \| | \| | 0.64 |
| 45.750 | 0.00 | 0.06 | 0.120 | O | \| | \| | \| | 0.63 |
| 45.833 | 0.00 | 0.06 | 0.120 | O | \| | \| | \| | 0.63 |
| 45.917 | 0.00 | 0.06 | 0.119 | O | \| | \| | \| | 0.63 |
| 46.000 | 0.00 | 0.06 | 0.119 | O | \| | \| | \| | 0.63 |
| 46.083 | 0.00 | 0.06 | 0.119 | O | \| | \| | \| | 0.62 |
| 46.167 | 0.00 | 0.06 | 0.118 | O | \| | \| | \| | 0.62 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 46.250 | 0.00 | 0.06 | 0.118 | O | \| | \| | \| | \| | 0.62 |
| 46.333 | 0.00 | 0.06 | 0.117 | O | \| | \| | \| | \| | 0.62 |
| 46.417 | 0.00 | 0.06 | 0.117 | O | \| | \| | \| | \| | 0.61 |
| 46.500 | 0.00 | 0.06 | 0.116 | O | \| | \| | \| | \| | 0.61 |
| 46.583 | 0.00 | 0.06 | 0.116 | O | \| | \| | \| | \| | 0.61 |
| 46.667 | 0.00 | 0.06 | 0.116 | O | \| | \| | \| | \| | 0.61 |
| 46.750 | 0.00 | 0.06 | 0.115 | O | \| | \| | \| | \| | 0.61 |
| 46.833 | 0.00 | 0.06 | 0.115 | O | \| | \| | \| | \| | 0.60 |
| 46.917 | 0.00 | 0.06 | 0.114 | O | \| | \| | \| | \| | 0.60 |
| 47.000 | 0.00 | 0.06 | 0.114 | O | \| | \| | \| | \| | 0.60 |
| 47.083 | 0.00 | 0.06 | 0.113 | O | \| | \| | \| | \| | 0.60 |
| 47.167 | 0.00 | 0.06 | 0.113 | O | \| | \| | \| | \| | 0.60 |
| 47.250 | 0.00 | 0.06 | 0.113 | O | \| | \| | \| | \| | 0.59 |
| 47.333 | 0.00 | 0.06 | 0.112 | O | \| | \| | \| | \| | 0.59 |
| 47.417 | 0.00 | 0.06 | 0.112 | O | \| | \| | \| | \| | 0.59 |
| 47.500 | 0.00 | 0.06 | 0.111 | O | \| | \| | \| | \| | 0.59 |
| 47.583 | 0.00 | 0.06 | 0.111 | O | \| | \| | \| | \| | 0.58 |
| 47.667 | 0.00 | 0.06 | 0.111 | O | \| | \| | \| | \| | 0.58 |
| 47.750 | 0.00 | 0.06 | 0.110 | O | \| | \| | \| | \| | 0.58 |
| 47.833 | 0.00 | 0.06 | 0.110 | O | \| | \| | \| | \| | 0.58 |
| 47.917 | 0.00 | 0.06 | 0.109 | O | \| | \| | \| | \| | 0.58 |
| 48.000 | 0.00 | 0.06 | 0.109 | O | \| | \| | \| | \| | 0.57 |
| 48.083 | 0.00 | 0.06 | 0.109 | O | \| | \| | \| | \| | 0.57 |
| 48.167 | 0.00 | 0.06 | 0.108 | O | \| | \| | \| | \| | 0.57 |
| 48.250 | 0.00 | 0.06 | 0.108 | O | \| | \| | \| | \| | 0.57 |
| 48.333 | 0.00 | 0.06 | 0.107 | O | \| | \| | \| | \| | 0.57 |
| 48.417 | 0.00 | 0.06 | 0.107 | O | \| | \| | \| | \| | 0.56 |
| 48.500 | 0.00 | 0.06 | 0.107 | O | \| | \| | \| | \| | 0.56 |
| 48.583 | 0.00 | 0.06 | 0.106 | O | \| | \| | \| | \| | 0.56 |
| 48.667 | 0.00 | 0.06 | 0.106 | O | \| | \| | \| | \| | 0.56 |
| 48.750 | 0.00 | 0.06 | 0.106 | O | \| | \| | \| | \| | 0.56 |
| 48.833 | 0.00 | 0.06 | 0.105 | O | \| | \| | \| | \| | 0.55 |
| 48.917 | 0.00 | 0.06 | 0.105 | O | \| | \| | \| | \| | 0.55 |
| 49.000 | 0.00 | 0.05 | 0.104 | O | \| | \| | \| | \| | 0.55 |
| 49.083 | 0.00 | 0.05 | 0.104 | O | \| | \| | \| | \| | 0.55 |
| 49.167 | 0.00 | 0.05 | 0.104 | O | \| | \| | \| | \| | 0.55 |
| 49.250 | 0.00 | 0.05 | 0.103 | O | \| | \| | \| | \| | 0.54 |
| 49.333 | 0.00 | 0.05 | 0.103 | O | \| | \| | \| | \| | 0.54 |
| 49.417 | 0.00 | 0.05 | 0.103 | O | \| | \| | \| | \| | 0.54 |
| 49.500 | 0.00 | 0.05 | 0.102 | O | \| | \| | \| | \| | 0.54 |
| 49.583 | 0.00 | 0.05 | 0.102 | O | \| | \| | \| | \| | 0.54 |
| 49.667 | 0.00 | 0.05 | 0.101 | O | \| | \| | \| | \| | 0.53 |
| 49.750 | 0.00 | 0.05 | 0.101 | O | \| | \| | \| | \| | 0.53 |
| 49.833 | 0.00 | 0.05 | 0.101 | O | \| | \| | \| | \| | 0.53 |
| 49.917 | 0.00 | 0.05 | 0.100 | O | \| | \| | \| | \| | 0.53 |
| 50.000 | 0.00 | 0.05 | 0.100 | O | \| | \| | \| | \| | 0.53 |
| 50.083 | 0.00 | 0.05 | 0.100 | O | \| | \| | \| | \| | 0.52 |
| 50.167 | 0.00 | 0.05 | 0.099 | O | \| | \| | \| | \| | 0.52 |
| 50.250 | 0.00 | 0.05 | 0.099 | O | \| | \| | \| | \| | 0.52 |
| 50.333 | 0.00 | 0.05 | 0.099 | O | \| | \| | \| | \| | 0.52 |
| 50.417 | 0.00 | 0.05 | 0.098 | O | \| | \| | \| | \| | 0.52 |
| 50.500 | 0.00 | 0.05 | 0.098 | O | \| | \| | \| | \| | 0.51 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 50.583 | 0.00 | 0.05 | 0.097 | O | \| | \| | \| | 0.51 |
| 50.667 | 0.00 | 0.05 | 0.097 | O | \| | \| | \| | 0.51 |
| 50.750 | 0.00 | 0.05 | 0.097 | O | \| | \| | \| | 0.51 |
| 50.833 | 0.00 | 0.05 | 0.096 | O | \| | \| | \| | 0.51 |
| 50.917 | 0.00 | 0.05 | 0.096 | O | \| | \| | \| | 0.51 |
| 51.000 | 0.00 | 0.05 | 0.096 | O | \| | \| | \| | 0.50 |
| 51.083 | 0.00 | 0.05 | 0.095 | O | \| | \| | \| | 0.50 |
| 51.167 | 0.00 | 0.05 | 0.095 | O | \| | \| | \| | 0.50 |
| 51.250 | 0.00 | 0.05 | 0.095 | O | \| | \| | \| | 0.50 |
| 51.333 | 0.00 | 0.05 | 0.094 | O | \| | \| | \| | 0.50 |
| 51.417 | 0.00 | 0.05 | 0.094 | O | \| | \| | \| | 0.49 |
| 51.500 | 0.00 | 0.05 | 0.094 | O | \| | \| | \| | 0.49 |
| 51.583 | 0.00 | 0.05 | 0.093 | O | \| | \| | \| | 0.49 |
| 51.667 | 0.00 | 0.05 | 0.093 | O | \| | \| | \| | 0.49 |
| 51.750 | 0.00 | 0.05 | 0.093 | O | \| | \| | \| | 0.49 |
| 51.833 | 0.00 | 0.05 | 0.092 | O | \| | \| | \| | 0.49 |
| 51.917 | 0.00 | 0.05 | 0.092 | O | \| | \| | \| | 0.48 |
| 52.000 | 0.00 | 0.05 | 0.092 | O | \| | \| | \| | 0.48 |
| 52.083 | 0.00 | 0.05 | 0.091 | O | \| | \| | \| | 0.48 |
| 52.167 | 0.00 | 0.05 | 0.091 | O | \| | \| | \| | 0.48 |
| 52.250 | 0.00 | 0.05 | 0.091 | O | \| | \| | \| | 0.48 |
| 52.333 | 0.00 | 0.05 | 0.090 | O | \| | \| | \| | 0.48 |
| 52.417 | 0.00 | 0.05 | 0.090 | O | \| | \| | \| | 0.47 |
| 52.500 | 0.00 | 0.05 | 0.090 | O | \| | \| | \| | 0.47 |
| 52.583 | 0.00 | 0.05 | 0.089 | O | \| | \| | \| | 0.47 |
| 52.667 | 0.00 | 0.05 | 0.089 | O | \| | \| | \| | 0.47 |
| 52.750 | 0.00 | 0.05 | 0.089 | O | \| | \| | \| | 0.47 |
| 52.833 | 0.00 | 0.05 | 0.088 | O | \| | \| | \| | 0.47 |
| 52.917 | 0.00 | 0.05 | 0.088 | O | \| | \| | \| | 0.46 |
| 53.000 | 0.00 | 0.05 | 0.088 | O | \| | \| | \| | 0.46 |
| 53.083 | 0.00 | 0.05 | 0.087 | O | \| | \| | \| | 0.46 |
| 53.167 | 0.00 | 0.05 | 0.087 | O | \| | \| | \| | 0.46 |
| 53.250 | 0.00 | 0.05 | 0.087 | O | \| | \| | \| | 0.46 |
| 53.333 | 0.00 | 0.05 | 0.086 | O | \| | \| | \| | 0.46 |
| 53.417 | 0.00 | 0.05 | 0.086 | O | \| | \| | \| | 0.45 |
| 53.500 | 0.00 | 0.05 | 0.086 | O | \| | \| | \| | 0.45 |
| 53.583 | 0.00 | 0.05 | 0.086 | O | \| | \| | \| | 0.45 |
| 53.667 | 0.00 | 0.04 | 0.085 | O | \| | \| | \| | 0.45 |
| 53.750 | 0.00 | 0.04 | 0.085 | O | \| | \| | \| | 0.45 |
| 53.833 | 0.00 | 0.04 | 0.085 | O | \| | \| | \| | 0.45 |
| 53.917 | 0.00 | 0.04 | 0.084 | O | \| | \| | \| | 0.44 |
| 54.000 | 0.00 | 0.04 | 0.084 | O | \| | \| | \| | 0.44 |
| 54.083 | 0.00 | 0.04 | 0.084 | O | \| | \| | \| | 0.44 |
| 54.167 | 0.00 | 0.04 | 0.083 | O | \| | \| | \| | 0.44 |
| 54.250 | 0.00 | 0.04 | 0.083 | O | \| | \| | \| | 0.44 |
| 54.333 | 0.00 | 0.04 | 0.083 | O | \| | \| | \| | 0.44 |
| 54.417 | 0.00 | 0.04 | 0.082 | O | \| | \| | \| | 0.43 |
| 54.500 | 0.00 | 0.04 | 0.082 | O | \| | \| | \| | 0.43 |
| 54.583 | 0.00 | 0.04 | 0.082 | O | \| | \| | \| | 0.43 |
| 54.667 | 0.00 | 0.04 | 0.082 | O | \| | \| | \| | 0.43 |
| 54.750 | 0.00 | 0.04 | 0.081 | O | \| | \| | \| | 0.43 |
| 54.833 | 0.00 | 0.04 | 0.081 | O | \| | \| | \| | 0.43 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 54.917 | 0.00 | 0.04 | 0.081 | O | \| | \| | \| | 0.42 |
| 55.000 | 0.00 | 0.04 | 0.080 | O | \| | \| | \| | 0.42 |
| 55.083 | 0.00 | 0.04 | 0.080 | O | \| | \| | \| | 0.42 |
| 55.167 | 0.00 | 0.04 | 0.080 | O | \| | \| | \| | 0.42 |
| 55.250 | 0.00 | 0.04 | 0.080 | O | \| | \| | \| | 0.42 |
| 55.333 | 0.00 | 0.04 | 0.079 | O | \| | \| | \| | 0.42 |
| 55.417 | 0.00 | 0.04 | 0.079 | O | \| | \| | \| | 0.42 |
| 55.500 | 0.00 | 0.04 | 0.079 | O | \| | \| | \| | 0.41 |
| 55.583 | 0.00 | 0.04 | 0.078 | O | \| | \| | \| | 0.41 |
| 55.667 | 0.00 | 0.04 | 0.078 | O | \| | \| | \| | 0.41 |
| 55.750 | 0.00 | 0.04 | 0.078 | O | \| | \| | \| | 0.41 |
| 55.833 | 0.00 | 0.04 | 0.078 | O | \| | \| | \| | 0.41 |
| 55.917 | 0.00 | 0.04 | 0.077 | O | \| | \| | \| | 0.41 |
| 56.000 | 0.00 | 0.04 | 0.077 | O | \| | \| | \| | 0.41 |
| 56.083 | 0.00 | 0.04 | 0.077 | O | \| | \| | \| | 0.40 |
| 56.167 | 0.00 | 0.04 | 0.076 | O | \| | \| | \| | 0.40 |
| 56.250 | 0.00 | 0.04 | 0.076 | O | \| | \| | \| | 0.40 |
| 56.333 | 0.00 | 0.04 | 0.076 | O | \| | \| | \| | 0.40 |
| 56.417 | 0.00 | 0.04 | 0.076 | O | \| | \| | \| | 0.40 |
| 56.500 | 0.00 | 0.04 | 0.075 | O | \| | \| | \| | 0.40 |
| 56.583 | 0.00 | 0.04 | 0.075 | O | \| | \| | \| | 0.40 |
| 56.667 | 0.00 | 0.04 | 0.075 | O | \| | \| | \| | 0.39 |
| 56.750 | 0.00 | 0.04 | 0.075 | O | \| | \| | \| | 0.39 |
| 56.833 | 0.00 | 0.04 | 0.074 | O | \| | \| | \| | 0.39 |
| 56.917 | 0.00 | 0.04 | 0.074 | O | \| | \| | \| | 0.39 |
| 57.000 | 0.00 | 0.04 | 0.074 | O | \| | \| | \| | 0.39 |
| 57.083 | 0.00 | 0.04 | 0.073 | O | \| | \| | \| | 0.39 |
| 57.167 | 0.00 | 0.04 | 0.073 | O | \| | \| | \| | 0.39 |
| 57.250 | 0.00 | 0.04 | 0.073 | O | \| | \| | \| | 0.38 |
| 57.333 | 0.00 | 0.04 | 0.073 | O | \| | \| | \| | 0.38 |
| 57.417 | 0.00 | 0.04 | 0.072 | O | \| | \| | \| | 0.38 |
| 57.500 | 0.00 | 0.04 | 0.072 | O | \| | \| | \| | 0.38 |
| 57.583 | 0.00 | 0.04 | 0.072 | O | \| | \| | \| | 0.38 |
| 57.667 | 0.00 | 0.04 | 0.072 | O | \| | \| | \| | 0.38 |
| 57.750 | 0.00 | 0.04 | 0.071 | O | \| | \| | \| | 0.38 |
| 57.833 | 0.00 | 0.04 | 0.071 | O | \| | \| | \| | 0.37 |
| 57.917 | 0.00 | 0.04 | 0.071 | O | \| | \| | \| | 0.37 |
| 58.000 | 0.00 | 0.04 | 0.071 | O | \| | \| | \| | 0.37 |
| 58.083 | 0.00 | 0.04 | 0.070 | O | \| | \| | \| | 0.37 |
| 58.167 | 0.00 | 0.04 | 0.070 | O | \| | \| | \| | 0.37 |
| 58.250 | 0.00 | 0.04 | 0.070 | O | \| | \| | \| | 0.37 |
| 58.333 | 0.00 | 0.04 | 0.070 | O | \| | \| | \| | 0.37 |
| 58.417 | 0.00 | 0.04 | 0.069 | O | \| | \| | \| | 0.36 |
| 58.500 | 0.00 | 0.04 | 0.069 | O | \| | \| | \| | 0.36 |
| 58.583 | 0.00 | 0.04 | 0.069 | O | \| | \| | \| | 0.36 |
| 58.667 | 0.00 | 0.04 | 0.069 | O | \| | \| | \| | 0.36 |
| 58.750 | 0.00 | 0.04 | 0.068 | O | \| | \| | \| | 0.36 |
| 58.833 | 0.00 | 0.04 | 0.068 | O | \| | \| | \| | 0.36 |
| 58.917 | 0.00 | 0.04 | 0.068 | O | \| | \| | \| | 0.36 |
| 59.000 | 0.00 | 0.04 | 0.068 | O | \| | \| | \| | 0.36 |
| 59.083 | 0.00 | 0.04 | 0.067 | O | \| | \| | \| | 0.35 |
| 59.167 | 0.00 | 0.04 | 0.067 | O | \| | \| | \| | 0.35 |

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|---|---|---|---|---|---|---|---|---|---|
| 59.250 | 0.00 | 0.04 | 0.067 | O | \| | \| | \| | \| | 0.35 |
| 59.333 | 0.00 | 0.04 | 0.067 | O | \| | \| | \| | \| | 0.35 |
| 59.417 | 0.00 | 0.03 | 0.066 | O | \| | \| | \| | \| | 0.35 |
| 59.500 | 0.00 | 0.03 | 0.066 | O | \| | \| | \| | \| | 0.35 |
| 59.583 | 0.00 | 0.03 | 0.066 | O | \| | \| | \| | \| | 0.35 |
| 59.667 | 0.00 | 0.03 | 0.066 | O | \| | \| | \| | \| | 0.35 |
| 59.750 | 0.00 | 0.03 | 0.065 | O | \| | \| | \| | \| | 0.34 |
| 59.833 | 0.00 | 0.03 | 0.065 | O | \| | \| | \| | \| | 0.34 |
| 59.917 | 0.00 | 0.03 | 0.065 | O | \| | \| | \| | \| | 0.34 |
| 60.000 | 0.00 | 0.03 | 0.065 | O | \| | \| | \| | \| | 0.34 |
| 60.083 | 0.00 | 0.03 | 0.064 | O | \| | \| | \| | \| | 0.34 |
| 60.167 | 0.00 | 0.03 | 0.064 | O | \| | \| | \| | \| | 0.34 |
| 60.250 | 0.00 | 0.03 | 0.064 | O | \| | \| | \| | \| | 0.34 |
| 60.333 | 0.00 | 0.03 | 0.064 | O | \| | \| | \| | \| | 0.34 |
| 60.417 | 0.00 | 0.03 | 0.064 | O | \| | \| | \| | \| | 0.33 |
| 60.500 | 0.00 | 0.03 | 0.063 | O | \| | \| | \| | \| | 0.33 |
| 60.583 | 0.00 | 0.03 | 0.063 | O | \| | \| | \| | \| | 0.33 |
| 60.667 | 0.00 | 0.03 | 0.063 | O | \| | \| | \| | \| | 0.33 |
| 60.750 | 0.00 | 0.03 | 0.063 | O | \| | \| | \| | \| | 0.33 |
| 60.833 | 0.00 | 0.03 | 0.062 | O | \| | \| | \| | \| | 0.33 |
| 60.917 | 0.00 | 0.03 | 0.062 | O | \| | \| | \| | \| | 0.33 |
| 61.000 | 0.00 | 0.03 | 0.062 | O | \| | \| | \| | \| | 0.33 |
| 61.083 | 0.00 | 0.03 | 0.062 | O | \| | \| | \| | \| | 0.32 |
| 61.167 | 0.00 | 0.03 | 0.062 | O | \| | \| | \| | \| | 0.32 |
| 61.250 | 0.00 | 0.03 | 0.061 | O | \| | \| | \| | \| | 0.32 |
| 61.333 | 0.00 | 0.03 | 0.061 | O | \| | \| | \| | \| | 0.32 |
| 61.417 | 0.00 | 0.03 | 0.061 | O | \| | \| | \| | \| | 0.32 |
| 61.500 | 0.00 | 0.03 | 0.061 | O | \| | \| | \| | \| | 0.32 |
| 61.583 | 0.00 | 0.03 | 0.060 | O | \| | \| | \| | \| | 0.32 |
| 61.667 | 0.00 | 0.03 | 0.060 | O | \| | \| | \| | \| | 0.32 |
| 61.750 | 0.00 | 0.03 | 0.060 | O | \| | \| | \| | \| | 0.32 |
| 61.833 | 0.00 | 0.03 | 0.060 | O | \| | \| | \| | \| | 0.31 |
| 61.917 | 0.00 | 0.03 | 0.060 | O | \| | \| | \| | \| | 0.31 |
| 62.000 | 0.00 | 0.03 | 0.059 | O | \| | \| | \| | \| | 0.31 |
| 62.083 | 0.00 | 0.03 | 0.059 | O | \| | \| | \| | \| | 0.31 |
| 62.167 | 0.00 | 0.03 | 0.059 | O | \| | \| | \| | \| | 0.31 |
| 62.250 | 0.00 | 0.03 | 0.059 | O | \| | \| | \| | \| | 0.31 |
| 62.333 | 0.00 | 0.03 | 0.058 | O | \| | \| | \| | \| | 0.31 |
| 62.417 | 0.00 | 0.03 | 0.058 | O | \| | \| | \| | \| | 0.31 |
| 62.500 | 0.00 | 0.03 | 0.058 | O | \| | \| | \| | \| | 0.31 |
| 62.583 | 0.00 | 0.03 | 0.058 | O | \| | \| | \| | \| | 0.30 |
| 62.667 | 0.00 | 0.03 | 0.058 | O | \| | \| | \| | \| | 0.30 |
| 62.750 | 0.00 | 0.03 | 0.057 | O | \| | \| | \| | \| | 0.30 |
| 62.833 | 0.00 | 0.03 | 0.057 | O | \| | \| | \| | \| | 0.30 |
| 62.917 | 0.00 | 0.03 | 0.057 | O | \| | \| | \| | \| | 0.30 |
| 63.000 | 0.00 | 0.03 | 0.057 | O | \| | \| | \| | \| | 0.30 |
| 63.083 | 0.00 | 0.03 | 0.057 | O | \| | \| | \| | \| | 0.30 |
| 63.167 | 0.00 | 0.03 | 0.056 | O | \| | \| | \| | \| | 0.30 |
| 63.250 | 0.00 | 0.03 | 0.056 | O | \| | \| | \| | \| | 0.30 |
| 63.333 | 0.00 | 0.03 | 0.056 | O | \| | \| | \| | \| | 0.29 |
| 63.417 | 0.00 | 0.03 | 0.056 | O | \| | \| | \| | \| | 0.29 |
| 63.500 | 0.00 | 0.03 | 0.056 | O | \| | \| | \| | \| | 0.29 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 63.583 | 0.00 | 0.03 | 0.055 | O | \| | \| | \| | 0.29 |
| 63.667 | 0.00 | 0.03 | 0.055 | O | \| | \| | \| | 0.29 |
| 63.750 | 0.00 | 0.03 | 0.055 | O | \| | \| | \| | 0.29 |
| 63.833 | 0.00 | 0.03 | 0.055 | O | \| | \| | \| | 0.29 |
| 63.917 | 0.00 | 0.03 | 0.055 | O | \| | \| | \| | 0.29 |
| 64.000 | 0.00 | 0.03 | 0.054 | O | \| | \| | \| | 0.29 |
| 64.083 | 0.00 | 0.03 | 0.054 | O | \| | \| | \| | 0.29 |
| 64.167 | 0.00 | 0.03 | 0.054 | O | \| | \| | \| | 0.28 |
| 64.250 | 0.00 | 0.03 | 0.054 | O | \| | \| | \| | 0.28 |
| 64.333 | 0.00 | 0.03 | 0.054 | O | \| | \| | \| | 0.28 |
| 64.417 | 0.00 | 0.03 | 0.053 | O | \| | \| | \| | 0.28 |
| 64.500 | 0.00 | 0.03 | 0.053 | O | \| | \| | \| | 0.28 |
| 64.583 | 0.00 | 0.03 | 0.053 | O | \| | \| | \| | 0.28 |
| 64.667 | 0.00 | 0.03 | 0.053 | O | \| | \| | \| | 0.28 |
| 64.750 | 0.00 | 0.03 | 0.053 | O | \| | \| | \| | 0.28 |
| 64.833 | 0.00 | 0.03 | 0.052 | O | \| | \| | \| | 0.28 |
| 64.917 | 0.00 | 0.03 | 0.052 | O | \| | \| | \| | 0.27 |
| 65.000 | 0.00 | 0.03 | 0.052 | O | \| | \| | \| | 0.27 |
| 65.083 | 0.00 | 0.03 | 0.052 | O | \| | \| | \| | 0.27 |
| 65.167 | 0.00 | 0.03 | 0.052 | O | \| | \| | \| | 0.27 |
| 65.250 | 0.00 | 0.03 | 0.051 | O | \| | \| | \| | 0.27 |
| 65.333 | 0.00 | 0.03 | 0.051 | O | \| | \| | \| | 0.27 |
| 65.417 | 0.00 | 0.03 | 0.051 | O | \| | \| | \| | 0.27 |
| 65.500 | 0.00 | 0.03 | 0.051 | O | \| | \| | \| | 0.27 |
| 65.583 | 0.00 | 0.03 | 0.051 | O | \| | \| | \| | 0.27 |
| 65.667 | 0.00 | 0.03 | 0.051 | O | \| | \| | \| | 0.27 |
| 65.750 | 0.00 | 0.03 | 0.050 | O | \| | \| | \| | 0.27 |
| 65.833 | 0.00 | 0.03 | 0.050 | O | \| | \| | \| | 0.26 |
| 65.917 | 0.00 | 0.03 | 0.050 | O | \| | \| | \| | 0.26 |
| 66.000 | 0.00 | 0.03 | 0.050 | O | \| | \| | \| | 0.26 |
| 66.083 | 0.00 | 0.03 | 0.050 | O | \| | \| | \| | 0.26 |
| 66.167 | 0.00 | 0.03 | 0.049 | O | \| | \| | \| | 0.26 |
| 66.250 | 0.00 | 0.03 | 0.049 | O | \| | \| | \| | 0.26 |
| 66.333 | 0.00 | 0.03 | 0.049 | O | \| | \| | \| | 0.26 |
| 66.417 | 0.00 | 0.03 | 0.049 | O | \| | \| | \| | 0.26 |
| 66.500 | 0.00 | 0.03 | 0.049 | O | \| | \| | \| | 0.26 |
| 66.583 | 0.00 | 0.03 | 0.049 | O | \| | \| | \| | 0.26 |
| 66.667 | 0.00 | 0.03 | 0.048 | O | \| | \| | \| | 0.25 |
| 66.750 | 0.00 | 0.03 | 0.048 | O | \| | \| | \| | 0.25 |
| 66.833 | 0.00 | 0.03 | 0.048 | O | \| | \| | \| | 0.25 |
| 66.917 | 0.00 | 0.03 | 0.048 | O | \| | \| | \| | 0.25 |
| 67.000 | 0.00 | 0.03 | 0.048 | O | \| | \| | \| | 0.25 |
| 67.083 | 0.00 | 0.03 | 0.048 | O | \| | \| | \| | 0.25 |
| 67.167 | 0.00 | 0.02 | 0.047 | O | \| | \| | \| | 0.25 |
| 67.250 | 0.00 | 0.02 | 0.047 | O | \| | \| | \| | 0.25 |
| 67.333 | 0.00 | 0.02 | 0.047 | O | \| | \| | \| | 0.25 |
| 67.417 | 0.00 | 0.02 | 0.047 | O | \| | \| | \| | 0.25 |
| 67.500 | 0.00 | 0.02 | 0.047 | O | \| | \| | \| | 0.25 |
| 67.583 | 0.00 | 0.02 | 0.047 | O | \| | \| | \| | 0.24 |
| 67.667 | 0.00 | 0.02 | 0.046 | O | \| | \| | \| | 0.24 |
| 67.750 | 0.00 | 0.02 | 0.046 | O | \| | \| | \| | 0.24 |
| 67.833 | 0.00 | 0.02 | 0.046 | O | \| | \| | \| | 0.24 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 67.917 | 0.00 | 0.02 | 0.046 | O | \| | \| | \| | 0.24 |
| 68.000 | 0.00 | 0.02 | 0.046 | O | \| | \| | \| | 0.24 |
| 68.083 | 0.00 | 0.02 | 0.046 | O | \| | \| | \| | 0.24 |
| 68.167 | 0.00 | 0.02 | 0.045 | O | \| | \| | \| | 0.24 |
| 68.250 | 0.00 | 0.02 | 0.045 | O | \| | \| | \| | 0.24 |
| 68.333 | 0.00 | 0.02 | 0.045 | O | \| | \| | \| | 0.24 |
| 68.417 | 0.00 | 0.02 | 0.045 | O | \| | \| | \| | 0.24 |
| 68.500 | 0.00 | 0.02 | 0.045 | O | \| | \| | \| | 0.24 |
| 68.583 | 0.00 | 0.02 | 0.045 | O | \| | \| | \| | 0.23 |
| 68.667 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 68.750 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 68.833 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 68.917 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 69.000 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 69.083 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 69.167 | 0.00 | 0.02 | 0.043 | O | \| | \| | \| | 0.23 |
| 69.250 | 0.00 | 0.02 | 0.043 | O | \| | \| | \| | 0.23 |
| 69.333 | 0.00 | 0.02 | 0.043 | O | \| | \| | \| | 0.23 |
| 69.417 | 0.00 | 0.02 | 0.043 | O | \| | \| | \| | 0.23 |
| 69.500 | 0.00 | 0.02 | 0.043 | O | \| | \| | \| | 0.23 |
| 69.583 | 0.00 | 0.02 | 0.043 | O | \| | \| | \| | 0.22 |
| 69.667 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 69.750 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 69.833 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 69.917 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 70.000 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 70.083 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 70.167 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 70.250 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.22 |
| 70.333 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.22 |
| 70.417 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.22 |
| 70.500 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.22 |
| 70.583 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.21 |
| 70.667 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.21 |
| 70.750 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.21 |
| 70.833 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 70.917 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 71.000 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 71.083 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 71.167 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 71.250 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 71.333 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 71.417 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.21 |
| 71.500 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.21 |
| 71.583 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.21 |
| 71.667 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.21 |
| 71.750 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.20 |
| 71.833 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.20 |
| 71.917 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.20 |
| 72.000 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 72.083 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 72.167 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 72.250 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 72.333 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 72.417 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 72.500 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 72.583 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.20 |
| 72.667 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.20 |
| 72.750 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.20 |
| 72.833 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.19 |
| 72.917 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.19 |
| 73.000 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.19 |
| 73.083 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.19 |
| 73.167 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 73.250 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 73.333 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 73.417 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 73.500 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 73.583 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 73.667 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 73.750 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 73.833 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.19 |
| 73.917 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.19 |
| 74.000 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.19 |
| 74.083 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.18 |
| 74.167 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.18 |
| 74.250 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.18 |
| 74.333 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.18 |
| 74.417 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.18 |
| 74.500 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 74.583 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 74.667 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 74.750 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 74.833 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 74.917 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 75.000 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 75.083 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 75.167 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.18 |
| 75.250 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.18 |
| 75.333 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.17 |
| 75.417 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.17 |
| 75.500 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.17 |
| 75.583 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.17 |
| 75.667 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.17 |
| 75.750 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.17 |
| 75.833 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 75.917 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 76.000 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 76.083 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 76.167 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 76.250 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 76.333 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 76.417 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 76.500 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |

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|---|---|---|---|---|---|---|---|---|
| 76.583 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.17 |
| 76.667 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 76.750 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 76.833 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 76.917 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 77.000 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 77.083 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 77.167 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 77.250 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 77.333 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 77.417 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 77.500 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 77.583 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 77.667 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 77.750 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 77.833 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 77.917 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 78.000 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 78.083 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.16 |
| 78.167 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 78.250 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 78.333 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 78.417 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 78.500 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 78.583 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 78.667 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 78.750 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 78.833 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 78.917 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 79.000 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 79.083 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 79.167 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 79.250 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 79.333 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 79.417 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 79.500 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 79.583 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 79.667 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.14 |
| 79.750 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 79.833 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 79.917 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 80.000 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 80.083 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 80.167 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 80.250 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 80.333 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 80.417 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 80.500 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 80.583 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 80.667 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 80.750 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 80.833 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 80.917 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 81.000 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 81.083 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 81.167 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 81.250 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 81.333 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.13 |
| 81.417 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 81.500 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 81.583 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 81.667 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 81.750 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 81.833 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 81.917 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 82.000 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 82.083 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 82.167 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 82.250 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 82.333 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 82.417 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 82.500 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 82.583 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 82.667 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 82.750 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 82.833 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 82.917 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 83.000 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 83.083 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.12 |
| 83.167 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.12 |
| 83.250 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.12 |
| 83.333 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 83.417 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 83.500 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 83.583 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 83.667 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 83.750 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 83.833 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 83.917 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 84.000 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 84.083 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 84.167 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 84.250 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 84.333 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 84.417 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 84.500 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 84.583 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 84.667 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 84.750 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 84.833 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 84.917 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 85.000 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.11 |
| 85.083 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.11 |
| 85.167 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.11 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 85.250 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.11 |
| 85.333 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 85.417 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 85.500 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 85.583 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 85.667 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 85.750 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 85.833 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 85.917 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 86.000 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 86.083 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 86.167 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 86.250 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 86.333 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 86.417 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | 0.11 |
| 86.500 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.11 |
| 86.583 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.11 |
| 86.667 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.11 |
| 86.750 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.11 |
| 86.833 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.11 |
| 86.917 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.11 |
| 87.000 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.11 |
| 87.083 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.10 |
| 87.167 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.10 |
| 87.250 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.10 |
| 87.333 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.10 |
| 87.417 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.10 |
| 87.500 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | 0.10 |
| 87.583 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 87.667 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 87.750 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 87.833 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 87.917 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 88.000 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 88.083 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 88.167 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 88.250 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 88.333 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 88.417 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 88.500 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 88.583 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 88.667 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 88.750 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | 0.10 |
| 88.833 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.10 |
| 88.917 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.10 |
| 89.000 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.10 |
| 89.083 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.10 |
| 89.167 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.10 |
| 89.250 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.10 |
| 89.333 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.10 |
| 89.417 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 89.500 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 89.583 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 89.667 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 89.750 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 89.833 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 89.917 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 90.000 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 90.083 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 90.167 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 90.250 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 90.333 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 90.417 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 90.500 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 90.583 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 90.667 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 90.750 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 90.833 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 90.917 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 91.000 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 91.083 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 91.167 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 91.250 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 91.333 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 91.417 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.09 |
| 91.500 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.09 |
| 91.583 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.09 |
| 91.667 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.09 |
| 91.750 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.09 |
| 91.833 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.09 |
| 91.917 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 92.000 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 92.083 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 92.167 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 92.250 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 92.333 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 92.417 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 92.500 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 92.583 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 92.667 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 92.750 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 92.833 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 92.917 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 93.000 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 93.083 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 93.167 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 93.250 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 93.333 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 93.417 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 93.500 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 93.583 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 93.667 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 93.750 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 93.833 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 93.917 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 94.000 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 94.083 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 94.167 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 94.250 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 94.333 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 94.417 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.08 |
| 94.500 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.08 |
| 94.583 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.08 |
| 94.667 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.08 |
| 94.750 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.08 |
| 94.833 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 94.917 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 95.000 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 95.083 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 95.167 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 95.250 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 95.333 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 95.417 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 95.500 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 95.583 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 95.667 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 95.750 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 95.833 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 95.917 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 96.000 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 96.083 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 96.167 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 96.250 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 96.333 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 96.417 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 96.500 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 96.583 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 96.667 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 96.750 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 96.833 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 96.917 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 97.000 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 97.083 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 97.167 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 97.250 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 97.333 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 97.417 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 97.500 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 97.583 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 97.667 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 97.750 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 97.833 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.07 |
| 97.917 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.07 |
| 98.000 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.07 |
| 98.083 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 98.167 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 98.250 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 98.333 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 98.417 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 98.500 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 98.583 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 98.667 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 98.750 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 98.833 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 98.917 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 99.000 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 99.083 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 99.167 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 99.250 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 99.333 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 99.417 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 99.500 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 99.583 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 99.667 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 99.750 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 99.833 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 99.917 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 100.000 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 100.083 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 100.167 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 100.250 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 100.333 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 100.417 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 100.500 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 100.583 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 100.667 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 100.750 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 100.833 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 100.917 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 101.000 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 101.083 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 101.167 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 101.250 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 101.333 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 101.417 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 101.500 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 101.583 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 101.667 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 101.750 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 101.833 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.06 |
| 101.917 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 102.000 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 102.083 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 102.167 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 102.250 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 102.333 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 102.417 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 102.500 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 102.583 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 102.667 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 102.750 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 102.833 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 102.917 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 103.000 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 103.083 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 103.167 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 103.250 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 103.333 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 103.417 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 103.500 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 103.583 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 103.667 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 103.750 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 103.833 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 103.917 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 104.000 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 104.083 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | \| | 0.05 |
| 104.167 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 104.250 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 104.333 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 104.417 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 104.500 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 104.583 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 104.667 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 104.750 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 104.833 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 104.917 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 105.000 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 105.083 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 105.167 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 105.250 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 105.333 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 105.417 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 105.500 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 105.583 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 105.667 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 105.750 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 105.833 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 105.917 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 106.000 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 106.083 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 106.167 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 106.250 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 106.333 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 106.417 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 106.500 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.05 |
| 106.583 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | \| | 0.04 |
| 106.667 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 106.750 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 106.833 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 106.917 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 107.000 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 107.083 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 107.167 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 107.250 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 107.333 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 107.417 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 107.500 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 107.583 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 107.667 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 107.750 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 107.833 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 107.917 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 108.000 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 108.083 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 108.167 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 108.250 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 108.333 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 108.417 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 108.500 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 108.583 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 108.667 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 108.750 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 108.833 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 108.917 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 109.000 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 109.083 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 109.167 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 109.250 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 109.333 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 109.417 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 109.500 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 109.583 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 109.667 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 109.750 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 109.833 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 109.917 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 110.000 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 110.083 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 110.167 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 110.250 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 110.333 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 110.417 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 110.500 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 110.583 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 110.667 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 110.750 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 110.833 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 110.917 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 111.000 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 111.083 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 111.167 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 111.250 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 111.333 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 111.417 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 111.500 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 111.583 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 111.667 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 111.750 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 111.833 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 111.917 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 112.000 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 112.083 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 112.167 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 112.250 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 112.333 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.03 |
| 112.417 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.03 |
| 112.500 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.03 |
| 112.583 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.03 |
| 112.667 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.03 |
| 112.750 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.03 |
| 112.833 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 112.917 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 113.000 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 113.083 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 113.167 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 113.250 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 113.333 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 113.417 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 113.500 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 113.583 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 113.667 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 113.750 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 113.833 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 113.917 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 114.000 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 114.083 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 114.167 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 114.250 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 114.333 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 114.417 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 114.500 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 114.583 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 114.667 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 114.750 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 114.833 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 114.917 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 115.000 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 115.083 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 115.167 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 115.250 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 115.333 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 115.417 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 115.500 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 115.583 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 115.667 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 115.750 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 115.833 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 115.917 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 116.000 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 116.083 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 116.167 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 116.250 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 116.333 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 116.417 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 116.500 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 116.583 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 116.667 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 116.750 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 116.833 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 116.917 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 117.000 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 117.083 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 117.167 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 117.250 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 117.333 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 117.417 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 117.500 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 117.583 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 117.667 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 117.750 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 117.833 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 117.917 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 118.000 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 118.083 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 118.167 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 118.250 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 118.333 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 118.417 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 118.500 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 118.583 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 118.667 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 118.750 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 118.833 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 118.917 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 119.000 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 119.083 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 119.167 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 119.250 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 119.333 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 119.417 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 119.500 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 119.583 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 119.667 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 119.750 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 119.833 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 119.917 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.03 |
| 120.000 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.03 |
| 120.083 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 120.167 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 120.250 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 120.333 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 120.417 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 120.500 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 120.583 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 120.667 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 120.750 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 120.833 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 120.917 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 121.000 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 121.083 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 121.167 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 121.250 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | \| 0.02 |
| 121.333 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 121.417 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 121.500 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 121.583 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 121.667 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 121.750 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 121.833 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 121.917 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 122.000 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 122.083 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 122.167 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 122.250 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 122.333 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 122.417 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 122.500 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 122.583 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 122.667 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 122.750 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 122.833 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 122.917 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 123.000 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 123.083 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 123.167 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 123.250 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 123.333 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 123.417 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 123.500 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 123.583 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 123.667 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 123.750 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 123.833 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 123.917 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 124.000 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 124.083 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |
| 124.167 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | \| 0.02 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 124.250 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 124.333 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 124.417 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 124.500 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 124.583 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 124.667 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 124.750 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 124.833 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 124.917 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.000 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.083 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.167 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.250 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.333 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.417 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.500 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.583 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.667 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.750 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.833 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.917 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.000 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.083 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.167 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.250 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.333 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.417 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.500 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.583 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.667 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.750 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.833 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.917 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.000 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 127.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 127.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 127.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 127.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 127.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 127.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 127.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 127.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 127.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 127.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 128.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 128.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 128.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 128.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 128.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 128.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 128.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 128.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 128.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 128.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 128.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 128.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 129.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 129.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 129.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 129.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 129.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 129.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 129.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 129.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 129.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 129.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 129.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 129.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 130.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 130.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 130.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 130.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 130.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 130.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 130.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 130.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 130.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 130.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 130.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 130.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 131.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 132.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 132.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 132.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 132.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 132.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 132.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 132.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 132.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 132.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 132.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 132.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 132.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 133.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 133.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 133.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 133.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 133.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 133.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 133.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 133.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 133.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 133.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 133.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 133.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 134.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 134.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 134.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 134.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 134.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 134.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 134.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 134.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 134.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 134.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| 0.01 |
| 134.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 134.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 135.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 135.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 135.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 135.250 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 135.333 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 135.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 135.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 135.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 135.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 135.750 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 135.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 135.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 136.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 136.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 136.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 136.250 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 136.333 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 136.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 136.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 136.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 136.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 136.750 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 136.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 136.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 137.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 137.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |
| 137.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| 0.01 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 137.250 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 137.333 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 137.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 137.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 137.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 137.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 137.750 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 137.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 137.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 138.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 138.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 138.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 138.250 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 138.333 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 138.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 138.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 138.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 138.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 138.750 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 138.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 138.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.250 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.333 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.750 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.250 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.333 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.750 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |

**********HYDROGRAPH DATA**********

Number of intervals = 1694

Time interval = 5.0 (Min.)

```
                Maximum/Peak flow rate =        0.602 (CFS)
                Total volume =       1.074 (Ac.Ft)
        Status of hydrographs being held in storage
                    Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
        Peak (CFS)      0.000     0.000     0.000     0.000     0.000
        Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
**************************************************************************

--------------------------------------------------------------------------
```

FLOOD HYDROGRAPH ROUTING PROGRAM

Study date: 08/26/24

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TPM 20854
PROPOSED INFILTRATION BASIN ROUTING ANALYSIS
BASIN "A"
100-YR; 24-HOUR
---

Program License Serial Number 6545

---
********** HYDROGRAPH INFORMATION **********

From study/file name: D100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 292
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 14.358 (CFS)
Total volume = 1.498 (Ac.Ft)

Status of hydrographs being held in storage

| | Stream 1 | Stream 2 | Stream 3 | Stream 4 | Stream 5 |
|---|---|---|---|---|---|
| Peak (CFS) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Vol (Ac.Ft) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

**********

++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station 1.000 to Point/Station 15.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data
---
Total number of inflow hydrograph intervals = 292
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 1.22(Ft.)
---
---
Initial basin depth = 1.22 (Ft.)
Initial basin storage = 0.25 (Ac.Ft)
Initial basin outflow = 0.19 (CFS)
---
---

Depth vs. Storage and Depth vs. Discharge data:

| Basin Depth (Ft.) | Storage (Ac.Ft) | Outflow (CFS) | (S-O*dt/2) (Ac.Ft) | (S+O*dt/2) (Ac.Ft) |
|---|---|---|---|---|
| 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| 1.000 | 0.190 | 0.100 | 0.190 | 0.190 |
| 2.000 | 0.440 | 0.510 | 0.438 | 0.442 |
| 3.000 | 0.740 | 0.750 | 0.737 | 0.743 |
| 4.000 | 1.100 | 15.720 | 1.046 | 1.154 |
| 5.000 | 1.520 | 101.510 | 1.170 | 1.870 |

## Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

| Time (Hours) | Inflow (CFS) | Outflow (CFS) | Storage (Ac.Ft) | .0 | 3.6 | 7.18 | 10.77 | 14.36 | Depth (Ft.) |
|---|---|---|---|---|---|---|---|---|---|
| 0.083 | 0.04 | 0.19 | 0.243 | O | \| | \| | \| | \| | 1.21 |
| 0.167 | 0.20 | 0.19 | 0.243 | O | \| | \| | \| | \| | 1.21 |
| 0.250 | 0.30 | 0.19 | 0.243 | O | \| | \| | \| | \| | 1.21 |
| 0.333 | 0.32 | 0.19 | 0.244 | O | \| | \| | \| | \| | 1.22 |
| 0.417 | 0.32 | 0.19 | 0.245 | O | \| | \| | \| | \| | 1.22 |
| 0.500 | 0.32 | 0.19 | 0.246 | O | \| | \| | \| | \| | 1.22 |
| 0.583 | 0.32 | 0.19 | 0.247 | O | \| | \| | \| | \| | 1.23 |
| 0.667 | 0.32 | 0.19 | 0.248 | O | \| | \| | \| | \| | 1.23 |
| 0.750 | 0.33 | 0.20 | 0.248 | O | \| | \| | \| | \| | 1.23 |
| 0.833 | 0.33 | 0.20 | 0.249 | O | \| | \| | \| | \| | 1.24 |
| 0.917 | 0.33 | 0.20 | 0.250 | O | \| | \| | \| | \| | 1.24 |
| 1.000 | 0.33 | 0.20 | 0.251 | O | \| | \| | \| | \| | 1.24 |
| 1.083 | 0.33 | 0.20 | 0.252 | O | \| | \| | \| | \| | 1.25 |
| 1.167 | 0.33 | 0.20 | 0.253 | O | \| | \| | \| | \| | 1.25 |
| 1.250 | 0.33 | 0.20 | 0.254 | O | \| | \| | \| | \| | 1.25 |
| 1.333 | 0.33 | 0.21 | 0.255 | O | \| | \| | \| | \| | 1.26 |
| 1.417 | 0.33 | 0.21 | 0.255 | O | \| | \| | \| | \| | 1.26 |
| 1.500 | 0.33 | 0.21 | 0.256 | O | \| | \| | \| | \| | 1.27 |
| 1.583 | 0.34 | 0.21 | 0.257 | O | \| | \| | \| | \| | 1.27 |
| 1.667 | 0.34 | 0.21 | 0.258 | O | \| | \| | \| | \| | 1.27 |
| 1.750 | 0.34 | 0.21 | 0.259 | O | \| | \| | \| | \| | 1.28 |
| 1.833 | 0.34 | 0.21 | 0.260 | O | \| | \| | \| | \| | 1.28 |
| 1.917 | 0.34 | 0.22 | 0.261 | O | \| | \| | \| | \| | 1.28 |
| 2.000 | 0.34 | 0.22 | 0.262 | O | \| | \| | \| | \| | 1.29 |
| 2.083 | 0.34 | 0.22 | 0.262 | O | \| | \| | \| | \| | 1.29 |
| 2.167 | 0.34 | 0.22 | 0.263 | O | \| | \| | \| | \| | 1.29 |
| 2.250 | 0.34 | 0.22 | 0.264 | O | \| | \| | \| | \| | 1.30 |
| 2.333 | 0.35 | 0.22 | 0.265 | O | \| | \| | \| | \| | 1.30 |
| 2.417 | 0.35 | 0.22 | 0.266 | O | \| | \| | \| | \| | 1.30 |
| 2.500 | 0.35 | 0.23 | 0.267 | O | \| | \| | \| | \| | 1.31 |
| 2.583 | 0.35 | 0.23 | 0.267 | O | \| | \| | \| | \| | 1.31 |
| 2.667 | 0.35 | 0.23 | 0.268 | O | \| | \| | \| | \| | 1.31 |
| 2.750 | 0.35 | 0.23 | 0.269 | O | \| | \| | \| | \| | 1.32 |
| 2.833 | 0.35 | 0.23 | 0.270 | O | \| | \| | \| | \| | 1.32 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 2.917 | 0.35 | 0.23 | 0.271 | O | \| | \| | \| | \| | 1.32 |
| 3.000 | 0.36 | 0.23 | 0.272 | O | \| | \| | \| | \| | 1.33 |
| 3.083 | 0.36 | 0.24 | 0.272 | O | \| | \| | \| | \| | 1.33 |
| 3.167 | 0.36 | 0.24 | 0.273 | O | \| | \| | \| | \| | 1.33 |
| 3.250 | 0.36 | 0.24 | 0.274 | O | \| | \| | \| | \| | 1.34 |
| 3.333 | 0.36 | 0.24 | 0.275 | O | \| | \| | \| | \| | 1.34 |
| 3.417 | 0.36 | 0.24 | 0.276 | O | \| | \| | \| | \| | 1.34 |
| 3.500 | 0.36 | 0.24 | 0.277 | O | \| | \| | \| | \| | 1.35 |
| 3.583 | 0.36 | 0.24 | 0.278 | O | \| | \| | \| | \| | 1.35 |
| 3.667 | 0.37 | 0.24 | 0.278 | O | \| | \| | \| | \| | 1.35 |
| 3.750 | 0.37 | 0.25 | 0.279 | O | \| | \| | \| | \| | 1.36 |
| 3.833 | 0.37 | 0.25 | 0.280 | O | \| | \| | \| | \| | 1.36 |
| 3.917 | 0.37 | 0.25 | 0.281 | O | \| | \| | \| | \| | 1.36 |
| 4.000 | 0.37 | 0.25 | 0.282 | O | \| | \| | \| | \| | 1.37 |
| 4.083 | 0.37 | 0.25 | 0.283 | O | \| | \| | \| | \| | 1.37 |
| 4.167 | 0.38 | 0.25 | 0.283 | O | \| | \| | \| | \| | 1.37 |
| 4.250 | 0.38 | 0.25 | 0.284 | O | \| | \| | \| | \| | 1.38 |
| 4.333 | 0.38 | 0.26 | 0.285 | O | \| | \| | \| | \| | 1.38 |
| 4.417 | 0.38 | 0.26 | 0.286 | O | \| | \| | \| | \| | 1.38 |
| 4.500 | 0.38 | 0.26 | 0.287 | O | \| | \| | \| | \| | 1.39 |
| 4.583 | 0.38 | 0.26 | 0.288 | O | \| | \| | \| | \| | 1.39 |
| 4.667 | 0.38 | 0.26 | 0.288 | O | \| | \| | \| | \| | 1.39 |
| 4.750 | 0.39 | 0.26 | 0.289 | O | \| | \| | \| | \| | 1.40 |
| 4.833 | 0.39 | 0.26 | 0.290 | O | \| | \| | \| | \| | 1.40 |
| 4.917 | 0.39 | 0.27 | 0.291 | O | \| | \| | \| | \| | 1.40 |
| 5.000 | 0.39 | 0.27 | 0.292 | O | \| | \| | \| | \| | 1.41 |
| 5.083 | 0.39 | 0.27 | 0.293 | O | \| | \| | \| | \| | 1.41 |
| 5.167 | 0.39 | 0.27 | 0.294 | O | \| | \| | \| | \| | 1.41 |
| 5.250 | 0.40 | 0.27 | 0.294 | O | \| | \| | \| | \| | 1.42 |
| 5.333 | 0.40 | 0.27 | 0.295 | O | \| | \| | \| | \| | 1.42 |
| 5.417 | 0.40 | 0.27 | 0.296 | O | \| | \| | \| | \| | 1.42 |
| 5.500 | 0.40 | 0.28 | 0.297 | O | \| | \| | \| | \| | 1.43 |
| 5.583 | 0.40 | 0.28 | 0.298 | O | \| | \| | \| | \| | 1.43 |
| 5.667 | 0.40 | 0.28 | 0.299 | O | \| | \| | \| | \| | 1.43 |
| 5.750 | 0.41 | 0.28 | 0.300 | O | \| | \| | \| | \| | 1.44 |
| 5.833 | 0.41 | 0.28 | 0.300 | O | \| | \| | \| | \| | 1.44 |
| 5.917 | 0.41 | 0.28 | 0.301 | O | \| | \| | \| | \| | 1.45 |
| 6.000 | 0.41 | 0.28 | 0.302 | O | \| | \| | \| | \| | 1.45 |
| 6.083 | 0.41 | 0.29 | 0.303 | O | \| | \| | \| | \| | 1.45 |
| 6.167 | 0.42 | 0.29 | 0.304 | O | \| | \| | \| | \| | 1.46 |
| 6.250 | 0.42 | 0.29 | 0.305 | O | \| | \| | \| | \| | 1.46 |
| 6.333 | 0.42 | 0.29 | 0.306 | O | \| | \| | \| | \| | 1.46 |
| 6.417 | 0.42 | 0.29 | 0.307 | O | \| | \| | \| | \| | 1.47 |
| 6.500 | 0.42 | 0.29 | 0.308 | O | \| | \| | \| | \| | 1.47 |
| 6.583 | 0.43 | 0.29 | 0.308 | O | \| | \| | \| | \| | 1.47 |
| 6.667 | 0.43 | 0.30 | 0.309 | O | \| | \| | \| | \| | 1.48 |
| 6.750 | 0.43 | 0.30 | 0.310 | O | \| | \| | \| | \| | 1.48 |
| 6.833 | 0.43 | 0.30 | 0.311 | O | \| | \| | \| | \| | 1.48 |
| 6.917 | 0.43 | 0.30 | 0.312 | O | \| | \| | \| | \| | 1.49 |
| 7.000 | 0.44 | 0.30 | 0.313 | O | \| | \| | \| | \| | 1.49 |
| 7.083 | 0.44 | 0.30 | 0.314 | O | \| | \| | \| | \| | 1.50 |
| 7.167 | 0.44 | 0.30 | 0.315 | O | \| | \| | \| | \| | 1.50 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 7.250 | 0.44 | 0.31 | 0.316 | O | | | | | 1.50 |
| 7.333 | 0.45 | 0.31 | 0.317 | O | | | | | 1.51 |
| 7.417 | 0.45 | 0.31 | 0.318 | O | | | | | 1.51 |
| 7.500 | 0.45 | 0.31 | 0.319 | OI | | | | | 1.51 |
| 7.583 | 0.45 | 0.31 | 0.320 | OI | | | | | 1.52 |
| 7.667 | 0.46 | 0.31 | 0.321 | OI | | | | | 1.52 |
| 7.750 | 0.46 | 0.32 | 0.322 | OI | | | | | 1.53 |
| 7.833 | 0.46 | 0.32 | 0.323 | OI | | | | | 1.53 |
| 7.917 | 0.46 | 0.32 | 0.324 | OI | | | | | 1.53 |
| 8.000 | 0.47 | 0.32 | 0.325 | OI | | | | | 1.54 |
| 8.083 | 0.47 | 0.32 | 0.326 | OI | | | | | 1.54 |
| 8.167 | 0.47 | 0.32 | 0.327 | OI | | | | | 1.55 |
| 8.250 | 0.47 | 0.33 | 0.328 | OI | | | | | 1.55 |
| 8.333 | 0.48 | 0.33 | 0.329 | OI | | | | | 1.55 |
| 8.417 | 0.48 | 0.33 | 0.330 | OI | | | | | 1.56 |
| 8.500 | 0.48 | 0.33 | 0.331 | OI | | | | | 1.56 |
| 8.583 | 0.49 | 0.33 | 0.332 | OI | | | | | 1.57 |
| 8.667 | 0.49 | 0.33 | 0.333 | OI | | | | | 1.57 |
| 8.750 | 0.49 | 0.34 | 0.334 | OI | | | | | 1.58 |
| 8.833 | 0.50 | 0.34 | 0.335 | OI | | | | | 1.58 |
| 8.917 | 0.50 | 0.34 | 0.336 | OI | | | | | 1.58 |
| 9.000 | 0.50 | 0.34 | 0.337 | OI | | | | | 1.59 |
| 9.083 | 0.51 | 0.34 | 0.338 | OI | | | | | 1.59 |
| 9.167 | 0.51 | 0.35 | 0.340 | OI | | | | | 1.60 |
| 9.250 | 0.51 | 0.35 | 0.341 | OI | | | | | 1.60 |
| 9.333 | 0.52 | 0.35 | 0.342 | OI | | | | | 1.61 |
| 9.417 | 0.52 | 0.35 | 0.343 | OI | | | | | 1.61 |
| 9.500 | 0.52 | 0.35 | 0.344 | OI | | | | | 1.62 |
| 9.583 | 0.53 | 0.35 | 0.345 | OI | | | | | 1.62 |
| 9.667 | 0.53 | 0.36 | 0.346 | OI | | | | | 1.63 |
| 9.750 | 0.53 | 0.36 | 0.348 | OI | | | | | 1.63 |
| 9.833 | 0.54 | 0.36 | 0.349 | OI | | | | | 1.64 |
| 9.917 | 0.54 | 0.36 | 0.350 | OI | | | | | 1.64 |
| 10.000 | 0.55 | 0.36 | 0.351 | OI | | | | | 1.65 |
| 10.083 | 0.55 | 0.37 | 0.353 | OI | | | | | 1.65 |
| 10.167 | 0.56 | 0.37 | 0.354 | OI | | | | | 1.66 |
| 10.250 | 0.56 | 0.37 | 0.355 | OI | | | | | 1.66 |
| 10.333 | 0.56 | 0.37 | 0.357 | OI | | | | | 1.67 |
| 10.417 | 0.57 | 0.38 | 0.358 | OI | | | | | 1.67 |
| 10.500 | 0.57 | 0.38 | 0.359 | OI | | | | | 1.68 |
| 10.583 | 0.58 | 0.38 | 0.361 | OI | | | | | 1.68 |
| 10.667 | 0.58 | 0.38 | 0.362 | OI | | | | | 1.69 |
| 10.750 | 0.59 | 0.38 | 0.363 | OI | | | | | 1.69 |
| 10.833 | 0.59 | 0.39 | 0.365 | OI | | | | | 1.70 |
| 10.917 | 0.60 | 0.39 | 0.366 | OI | | | | | 1.70 |
| 11.000 | 0.61 | 0.39 | 0.368 | OI | | | | | 1.71 |
| 11.083 | 0.61 | 0.39 | 0.369 | OI | | | | | 1.72 |
| 11.167 | 0.62 | 0.40 | 0.371 | OI | | | | | 1.72 |
| 11.250 | 0.62 | 0.40 | 0.372 | OI | | | | | 1.73 |
| 11.333 | 0.63 | 0.40 | 0.374 | OI | | | | | 1.73 |
| 11.417 | 0.63 | 0.40 | 0.375 | OI | | | | | 1.74 |
| 11.500 | 0.64 | 0.41 | 0.377 | OI | | | | | 1.75 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 11.583 | 0.65 | 0.41 | 0.379 | OI | \| | \| | \| | 1.75 |
| 11.667 | 0.65 | 0.41 | 0.380 | OI | \| | \| | \| | 1.76 |
| 11.750 | 0.66 | 0.41 | 0.382 | OI | \| | \| | \| | 1.77 |
| 11.833 | 0.67 | 0.42 | 0.384 | OI | \| | \| | \| | 1.77 |
| 11.917 | 0.68 | 0.42 | 0.385 | OI | \| | \| | \| | 1.78 |
| 12.000 | 0.68 | 0.42 | 0.387 | OI | \| | \| | \| | 1.79 |
| 12.083 | 0.70 | 0.43 | 0.389 | OI | \| | \| | \| | 1.80 |
| 12.167 | 0.73 | 0.43 | 0.391 | OI | \| | \| | \| | 1.80 |
| 12.250 | 0.75 | 0.43 | 0.393 | OI | \| | \| | \| | 1.81 |
| 12.333 | 0.76 | 0.44 | 0.395 | OI | \| | \| | \| | 1.82 |
| 12.417 | 0.77 | 0.44 | 0.398 | OI | \| | \| | \| | 1.83 |
| 12.500 | 0.78 | 0.44 | 0.400 | OI | \| | \| | \| | 1.84 |
| 12.583 | 0.79 | 0.45 | 0.402 | OI | \| | \| | \| | 1.85 |
| 12.667 | 0.80 | 0.45 | 0.405 | \|O | \| | \| | \| | 1.86 |
| 12.750 | 0.81 | 0.46 | 0.407 | \|O | \| | \| | \| | 1.87 |
| 12.833 | 0.82 | 0.46 | 0.410 | \|O | \| | \| | \| | 1.88 |
| 12.917 | 0.84 | 0.46 | 0.412 | \|O | \| | \| | \| | 1.89 |
| 13.000 | 0.85 | 0.47 | 0.415 | \|O | \| | \| | \| | 1.90 |
| 13.083 | 0.86 | 0.47 | 0.417 | \|O | \| | \| | \| | 1.91 |
| 13.167 | 0.87 | 0.48 | 0.420 | \|O | \| | \| | \| | 1.92 |
| 13.250 | 0.89 | 0.48 | 0.423 | \|O | \| | \| | \| | 1.93 |
| 13.333 | 0.90 | 0.49 | 0.426 | \|OI | \| | \| | \| | 1.94 |
| 13.417 | 0.91 | 0.49 | 0.428 | \|OI | \| | \| | \| | 1.95 |
| 13.500 | 0.93 | 0.50 | 0.431 | \|OI | \| | \| | \| | 1.97 |
| 13.583 | 0.94 | 0.50 | 0.434 | \|OI | \| | \| | \| | 1.98 |
| 13.667 | 0.96 | 0.51 | 0.437 | \|OI | \| | \| | \| | 1.99 |
| 13.750 | 0.98 | 0.51 | 0.441 | \|OI | \| | \| | \| | 2.00 |
| 13.833 | 1.00 | 0.51 | 0.444 | \|OI | \| | \| | \| | 2.01 |
| 13.917 | 1.02 | 0.52 | 0.447 | \|OI | \| | \| | \| | 2.02 |
| 14.000 | 1.04 | 0.52 | 0.451 | \|OI | \| | \| | \| | 2.04 |
| 14.083 | 1.06 | 0.52 | 0.455 | \|OI | \| | \| | \| | 2.05 |
| 14.167 | 1.08 | 0.52 | 0.458 | \|OI | \| | \| | \| | 2.06 |
| 14.250 | 1.11 | 0.53 | 0.462 | \|OI | \| | \| | \| | 2.07 |
| 14.333 | 1.14 | 0.53 | 0.466 | \|OI | \| | \| | \| | 2.09 |
| 14.417 | 1.16 | 0.53 | 0.471 | \|OI | \| | \| | \| | 2.10 |
| 14.500 | 1.20 | 0.54 | 0.475 | \|OI | \| | \| | \| | 2.12 |
| 14.583 | 1.23 | 0.54 | 0.480 | \|OI | \| | \| | \| | 2.13 |
| 14.667 | 1.27 | 0.55 | 0.484 | \|OI | \| | \| | \| | 2.15 |
| 14.750 | 1.30 | 0.55 | 0.490 | \|OI | \| | \| | \| | 2.17 |
| 14.833 | 1.35 | 0.55 | 0.495 | \|O I | \| | \| | \| | 2.18 |
| 14.917 | 1.39 | 0.56 | 0.501 | \|O I | \| | \| | \| | 2.20 |
| 15.000 | 1.45 | 0.56 | 0.506 | \|O I | \| | \| | \| | 2.22 |
| 15.083 | 1.50 | 0.57 | 0.513 | \|O I | \| | \| | \| | 2.24 |
| 15.167 | 1.57 | 0.57 | 0.519 | \|O I | \| | \| | \| | 2.26 |
| 15.250 | 1.64 | 0.58 | 0.526 | \|O I | \| | \| | \| | 2.29 |
| 15.333 | 1.74 | 0.59 | 0.534 | \|O I | \| | \| | \| | 2.31 |
| 15.417 | 1.80 | 0.59 | 0.542 | \|O  I | \| | \| | \| | 2.34 |
| 15.500 | 1.79 | 0.60 | 0.551 | \|O I | \| | \| | \| | 2.37 |
| 15.583 | 1.84 | 0.61 | 0.559 | \|O  I | \| | \| | \| | 2.40 |
| 15.667 | 2.02 | 0.61 | 0.568 | \|O  I | \| | \| | \| | 2.43 |
| 15.750 | 2.24 | 0.62 | 0.578 | \|O  I | \| | \| | \| | 2.46 |
| 15.833 | 2.61 | 0.63 | 0.591 | \|O   I | \| | \| | \| | 2.50 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 15.917 | 3.18 | 0.64 | 0.606 | O I | | | | 2.55 |
| 16.000 | 4.38 | 0.66 | 0.628 | O I | | | | 2.63 |
| 16.083 | 7.65 | 0.69 | 0.665 | O | I | | | 2.75 |
| 16.167 | 14.36 | 0.75 | 0.736 | O | | | I | 2.99 |
| 16.250 | 9.52 | 3.39 | 0.804 | O | | I | | 3.18 |
| 16.333 | 3.89 | 4.22 | 0.824 | IO | | | | 3.23 |
| 16.417 | 2.46 | 3.96 | 0.817 | I O | | | | 3.21 |
| 16.500 | 1.96 | 3.52 | 0.807 | I O | | | | 3.19 |
| 16.583 | 1.78 | 3.11 | 0.797 | I O | | | | 3.16 |
| 16.667 | 1.62 | 2.76 | 0.788 | I O | | | | 3.13 |
| 16.750 | 1.48 | 2.45 | 0.781 | I O | | | | 3.11 |
| 16.833 | 1.38 | 2.20 | 0.775 | IO | | | | 3.10 |
| 16.917 | 1.29 | 1.98 | 0.770 | I O | | | | 3.08 |
| 17.000 | 1.21 | 1.80 | 0.765 | I O | | | | 3.07 |
| 17.083 | 1.15 | 1.64 | 0.761 | IO | | | | 3.06 |
| 17.167 | 1.10 | 1.51 | 0.758 | IO | | | | 3.05 |
| 17.250 | 1.05 | 1.40 | 0.756 | IO | | | | 3.04 |
| 17.333 | 1.01 | 1.31 | 0.753 | O | | | | 3.04 |
| 17.417 | 0.97 | 1.23 | 0.752 | O | | | | 3.03 |
| 17.500 | 0.94 | 1.16 | 0.750 | O | | | | 3.03 |
| 17.583 | 0.91 | 1.10 | 0.748 | O | | | | 3.02 |
| 17.667 | 0.88 | 1.05 | 0.747 | IO | | | | 3.02 |
| 17.750 | 0.85 | 1.00 | 0.746 | IO | | | | 3.02 |
| 17.833 | 0.83 | 0.96 | 0.745 | IO | | | | 3.01 |
| 17.917 | 0.81 | 0.93 | 0.744 | IO | | | | 3.01 |
| 18.000 | 0.79 | 0.89 | 0.743 | O | | | | 3.01 |
| 18.083 | 0.76 | 0.87 | 0.743 | O | | | | 3.01 |
| 18.167 | 0.72 | 0.83 | 0.742 | O | | | | 3.01 |
| 18.250 | 0.69 | 0.80 | 0.741 | O | | | | 3.00 |
| 18.333 | 0.67 | 0.77 | 0.741 | O | | | | 3.00 |
| 18.417 | 0.66 | 0.75 | 0.740 | O | | | | 3.00 |
| 18.500 | 0.64 | 0.75 | 0.739 | O | | | | 3.00 |
| 18.583 | 0.63 | 0.75 | 0.738 | O | | | | 2.99 |
| 18.667 | 0.62 | 0.75 | 0.738 | O | | | | 2.99 |
| 18.750 | 0.61 | 0.75 | 0.737 | O | | | | 2.99 |
| 18.833 | 0.60 | 0.75 | 0.736 | O | | | | 2.99 |
| 18.917 | 0.59 | 0.75 | 0.735 | O | | | | 2.98 |
| 19.000 | 0.58 | 0.74 | 0.733 | O | | | | 2.98 |
| 19.083 | 0.57 | 0.74 | 0.732 | O | | | | 2.97 |
| 19.167 | 0.56 | 0.74 | 0.731 | O | | | | 2.97 |
| 19.250 | 0.55 | 0.74 | 0.730 | O | | | | 2.97 |
| 19.333 | 0.54 | 0.74 | 0.728 | O | | | | 2.96 |
| 19.417 | 0.53 | 0.74 | 0.727 | O | | | | 2.96 |
| 19.500 | 0.53 | 0.74 | 0.726 | O | | | | 2.95 |
| 19.583 | 0.52 | 0.74 | 0.724 | O | | | | 2.95 |
| 19.667 | 0.51 | 0.74 | 0.723 | O | | | | 2.94 |
| 19.750 | 0.50 | 0.73 | 0.721 | O | | | | 2.94 |
| 19.833 | 0.50 | 0.73 | 0.719 | O | | | | 2.93 |
| 19.917 | 0.49 | 0.73 | 0.718 | O | | | | 2.93 |
| 20.000 | 0.49 | 0.73 | 0.716 | O | | | | 2.92 |
| 20.083 | 0.48 | 0.73 | 0.714 | O | | | | 2.91 |
| 20.167 | 0.47 | 0.73 | 0.713 | O | | | | 2.91 |

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|---|---|---|---|---|---|---|---|---|
| 20.250 | 0.47 | 0.73 | 0.711 | \|O | \| | \| | \| | 2.90 |
| 20.333 | 0.46 | 0.73 | 0.709 | \|O | \| | \| | \| | 2.90 |
| 20.417 | 0.46 | 0.72 | 0.707 | \|O | \| | \| | \| | 2.89 |
| 20.500 | 0.45 | 0.72 | 0.705 | \|O | \| | \| | \| | 2.88 |
| 20.583 | 0.45 | 0.72 | 0.703 | IO | \| | \| | \| | 2.88 |
| 20.667 | 0.44 | 0.72 | 0.702 | IO | \| | \| | \| | 2.87 |
| 20.750 | 0.44 | 0.72 | 0.700 | IO | \| | \| | \| | 2.87 |
| 20.833 | 0.43 | 0.72 | 0.698 | IO | \| | \| | \| | 2.86 |
| 20.917 | 0.43 | 0.71 | 0.696 | IO | \| | \| | \| | 2.85 |
| 21.000 | 0.43 | 0.71 | 0.694 | IO | \| | \| | \| | 2.85 |
| 21.083 | 0.42 | 0.71 | 0.692 | IO | \| | \| | \| | 2.84 |
| 21.167 | 0.42 | 0.71 | 0.690 | IO | \| | \| | \| | 2.83 |
| 21.250 | 0.41 | 0.71 | 0.688 | IO | \| | \| | \| | 2.83 |
| 21.333 | 0.41 | 0.71 | 0.686 | IO | \| | \| | \| | 2.82 |
| 21.417 | 0.41 | 0.70 | 0.684 | IO | \| | \| | \| | 2.81 |
| 21.500 | 0.40 | 0.70 | 0.682 | IO | \| | \| | \| | 2.81 |
| 21.583 | 0.40 | 0.70 | 0.680 | IO | \| | \| | \| | 2.80 |
| 21.667 | 0.39 | 0.70 | 0.677 | IO | \| | \| | \| | 2.79 |
| 21.750 | 0.39 | 0.70 | 0.675 | IO | \| | \| | \| | 2.78 |
| 21.833 | 0.39 | 0.70 | 0.673 | IO | \| | \| | \| | 2.78 |
| 21.917 | 0.38 | 0.69 | 0.671 | IO | \| | \| | \| | 2.77 |
| 22.000 | 0.38 | 0.69 | 0.669 | IO | \| | \| | \| | 2.76 |
| 22.083 | 0.38 | 0.69 | 0.667 | IO | \| | \| | \| | 2.76 |
| 22.167 | 0.38 | 0.69 | 0.665 | IO | \| | \| | \| | 2.75 |
| 22.250 | 0.37 | 0.69 | 0.662 | IO | \| | \| | \| | 2.74 |
| 22.333 | 0.37 | 0.69 | 0.660 | IO | \| | \| | \| | 2.73 |
| 22.417 | 0.37 | 0.68 | 0.658 | IO | \| | \| | \| | 2.73 |
| 22.500 | 0.36 | 0.68 | 0.656 | IO | \| | \| | \| | 2.72 |
| 22.583 | 0.36 | 0.68 | 0.654 | IO | \| | \| | \| | 2.71 |
| 22.667 | 0.36 | 0.68 | 0.652 | IO | \| | \| | \| | 2.71 |
| 22.750 | 0.36 | 0.68 | 0.649 | IO | \| | \| | \| | 2.70 |
| 22.833 | 0.35 | 0.68 | 0.647 | IO | \| | \| | \| | 2.69 |
| 22.917 | 0.35 | 0.67 | 0.645 | IO | \| | \| | \| | 2.68 |
| 23.000 | 0.35 | 0.67 | 0.643 | IO | \| | \| | \| | 2.68 |
| 23.083 | 0.35 | 0.67 | 0.640 | IO | \| | \| | \| | 2.67 |
| 23.167 | 0.34 | 0.67 | 0.638 | IO | \| | \| | \| | 2.66 |
| 23.250 | 0.34 | 0.67 | 0.636 | IO | \| | \| | \| | 2.65 |
| 23.333 | 0.34 | 0.66 | 0.634 | IO | \| | \| | \| | 2.65 |
| 23.417 | 0.34 | 0.66 | 0.631 | IO | \| | \| | \| | 2.64 |
| 23.500 | 0.34 | 0.66 | 0.629 | IO | \| | \| | \| | 2.63 |
| 23.583 | 0.33 | 0.66 | 0.627 | IO | \| | \| | \| | 2.62 |
| 23.667 | 0.33 | 0.66 | 0.625 | IO | \| | \| | \| | 2.62 |
| 23.750 | 0.33 | 0.66 | 0.622 | IO | \| | \| | \| | 2.61 |
| 23.833 | 0.33 | 0.65 | 0.620 | IO | \| | \| | \| | 2.60 |
| 23.917 | 0.32 | 0.65 | 0.618 | IO | \| | \| | \| | 2.59 |
| 24.000 | 0.32 | 0.65 | 0.616 | IO | \| | \| | \| | 2.59 |
| 24.083 | 0.29 | 0.65 | 0.613 | IO | \| | \| | \| | 2.58 |
| 24.167 | 0.12 | 0.65 | 0.610 | IO | \| | \| | \| | 2.57 |
| 24.250 | 0.02 | 0.64 | 0.606 | IO | \| | \| | \| | 2.55 |
| 24.333 | 0.00 | 0.64 | 0.602 | IO | \| | \| | \| | 2.54 |
| 24.417 | 0.00 | 0.64 | 0.598 | IO | \| | \| | \| | 2.53 |
| 24.500 | 0.00 | 0.63 | 0.593 | IO | \| | \| | \| | 2.51 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 24.583 | 0.00 | 0.63 | 0.589 | IO | | | | 2.50 |
| 24.667 | 0.00 | 0.63 | 0.585 | IO | | | | 2.48 |
| 24.750 | 0.00 | 0.62 | 0.580 | IO | | | | 2.47 |
| 24.833 | 0.00 | 0.62 | 0.576 | IO | | | | 2.45 |
| 24.917 | 0.00 | 0.62 | 0.572 | IO | | | | 2.44 |
| 25.000 | 0.00 | 0.61 | 0.568 | IO | | | | 2.43 |
| 25.083 | 0.00 | 0.61 | 0.563 | IO | | | | 2.41 |
| 25.167 | 0.00 | 0.61 | 0.559 | IO | | | | 2.40 |
| 25.250 | 0.00 | 0.60 | 0.555 | IO | | | | 2.38 |
| 25.333 | 0.00 | 0.60 | 0.551 | IO | | | | 2.37 |
| 25.417 | 0.00 | 0.60 | 0.547 | IO | | | | 2.36 |
| 25.500 | 0.00 | 0.59 | 0.543 | IO | | | | 2.34 |
| 25.583 | 0.00 | 0.59 | 0.539 | IO | | | | 2.33 |
| 25.667 | 0.00 | 0.59 | 0.535 | IO | | | | 2.32 |
| 25.750 | 0.00 | 0.58 | 0.531 | IO | | | | 2.30 |
| 25.833 | 0.00 | 0.58 | 0.527 | IO | | | | 2.29 |
| 25.917 | 0.00 | 0.58 | 0.523 | IO | | | | 2.28 |
| 26.000 | 0.00 | 0.57 | 0.519 | IO | | | | 2.26 |
| 26.083 | 0.00 | 0.57 | 0.515 | IO | | | | 2.25 |
| 26.167 | 0.00 | 0.57 | 0.511 | IO | | | | 2.24 |
| 26.250 | 0.00 | 0.56 | 0.507 | IO | | | | 2.22 |
| 26.333 | 0.00 | 0.56 | 0.503 | IO | | | | 2.21 |
| 26.417 | 0.00 | 0.56 | 0.499 | IO | | | | 2.20 |
| 26.500 | 0.00 | 0.55 | 0.495 | IO | | | | 2.18 |
| 26.583 | 0.00 | 0.55 | 0.491 | IO | | | | 2.17 |
| 26.667 | 0.00 | 0.55 | 0.488 | IO | | | | 2.16 |
| 26.750 | 0.00 | 0.55 | 0.484 | IO | | | | 2.15 |
| 26.833 | 0.00 | 0.54 | 0.480 | IO | | | | 2.13 |
| 26.917 | 0.00 | 0.54 | 0.476 | IO | | | | 2.12 |
| 27.000 | 0.00 | 0.54 | 0.473 | IO | | | | 2.11 |
| 27.083 | 0.00 | 0.53 | 0.469 | IO | | | | 2.10 |
| 27.167 | 0.00 | 0.53 | 0.465 | IO | | | | 2.08 |
| 27.250 | 0.00 | 0.53 | 0.462 | IO | | | | 2.07 |
| 27.333 | 0.00 | 0.52 | 0.458 | IO | | | | 2.06 |
| 27.417 | 0.00 | 0.52 | 0.455 | IO | | | | 2.05 |
| 27.500 | 0.00 | 0.52 | 0.451 | IO | | | | 2.04 |
| 27.583 | 0.00 | 0.52 | 0.447 | IO | | | | 2.02 |
| 27.667 | 0.00 | 0.51 | 0.444 | IO | | | | 2.01 |
| 27.750 | 0.00 | 0.51 | 0.440 | IO | | | | 2.00 |
| 27.833 | 0.00 | 0.50 | 0.437 | IO | | | | 1.99 |
| 27.917 | 0.00 | 0.50 | 0.433 | IO | | | | 1.97 |
| 28.000 | 0.00 | 0.49 | 0.430 | IO | | | | 1.96 |
| 28.083 | 0.00 | 0.49 | 0.427 | IO | | | | 1.95 |
| 28.167 | 0.00 | 0.48 | 0.423 | IO | | | | 1.93 |
| 28.250 | 0.00 | 0.48 | 0.420 | IO | | | | 1.92 |
| 28.333 | 0.00 | 0.47 | 0.417 | IO | | | | 1.91 |
| 28.417 | 0.00 | 0.47 | 0.413 | IO | | | | 1.89 |
| 28.500 | 0.00 | 0.46 | 0.410 | IO | | | | 1.88 |
| 28.583 | 0.00 | 0.46 | 0.407 | IO | | | | 1.87 |
| 28.667 | 0.00 | 0.45 | 0.404 | IO | | | | 1.86 |
| 28.750 | 0.00 | 0.45 | 0.401 | O | | | | 1.84 |
| 28.833 | 0.00 | 0.44 | 0.398 | O | | | | 1.83 |

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|---|---|---|---|---|---|---|---|---|---|
| 28.917 | 0.00 | 0.44 | 0.395 | O | \| | \| | \| | \| | 1.82 |
| 29.000 | 0.00 | 0.43 | 0.392 | O | \| | \| | \| | \| | 1.81 |
| 29.083 | 0.00 | 0.43 | 0.389 | O | \| | \| | \| | \| | 1.80 |
| 29.167 | 0.00 | 0.42 | 0.386 | O | \| | \| | \| | \| | 1.78 |
| 29.250 | 0.00 | 0.42 | 0.383 | O | \| | \| | \| | \| | 1.77 |
| 29.333 | 0.00 | 0.41 | 0.380 | O | \| | \| | \| | \| | 1.76 |
| 29.417 | 0.00 | 0.41 | 0.377 | O | \| | \| | \| | \| | 1.75 |
| 29.500 | 0.00 | 0.40 | 0.375 | O | \| | \| | \| | \| | 1.74 |
| 29.583 | 0.00 | 0.40 | 0.372 | O | \| | \| | \| | \| | 1.73 |
| 29.667 | 0.00 | 0.39 | 0.369 | O | \| | \| | \| | \| | 1.72 |
| 29.750 | 0.00 | 0.39 | 0.366 | O | \| | \| | \| | \| | 1.71 |
| 29.833 | 0.00 | 0.38 | 0.364 | O | \| | \| | \| | \| | 1.70 |
| 29.917 | 0.00 | 0.38 | 0.361 | O | \| | \| | \| | \| | 1.68 |
| 30.000 | 0.00 | 0.38 | 0.359 | O | \| | \| | \| | \| | 1.67 |
| 30.083 | 0.00 | 0.37 | 0.356 | O | \| | \| | \| | \| | 1.66 |
| 30.167 | 0.00 | 0.37 | 0.353 | O | \| | \| | \| | \| | 1.65 |
| 30.250 | 0.00 | 0.36 | 0.351 | O | \| | \| | \| | \| | 1.64 |
| 30.333 | 0.00 | 0.36 | 0.348 | O | \| | \| | \| | \| | 1.63 |
| 30.417 | 0.00 | 0.36 | 0.346 | O | \| | \| | \| | \| | 1.62 |
| 30.500 | 0.00 | 0.35 | 0.343 | O | \| | \| | \| | \| | 1.61 |
| 30.583 | 0.00 | 0.35 | 0.341 | O | \| | \| | \| | \| | 1.60 |
| 30.667 | 0.00 | 0.34 | 0.339 | O | \| | \| | \| | \| | 1.59 |
| 30.750 | 0.00 | 0.34 | 0.336 | O | \| | \| | \| | \| | 1.59 |
| 30.833 | 0.00 | 0.34 | 0.334 | O | \| | \| | \| | \| | 1.58 |
| 30.917 | 0.00 | 0.33 | 0.332 | O | \| | \| | \| | \| | 1.57 |
| 31.000 | 0.00 | 0.33 | 0.329 | O | \| | \| | \| | \| | 1.56 |
| 31.083 | 0.00 | 0.32 | 0.327 | O | \| | \| | \| | \| | 1.55 |
| 31.167 | 0.00 | 0.32 | 0.325 | O | \| | \| | \| | \| | 1.54 |
| 31.250 | 0.00 | 0.32 | 0.323 | O | \| | \| | \| | \| | 1.53 |
| 31.333 | 0.00 | 0.31 | 0.321 | O | \| | \| | \| | \| | 1.52 |
| 31.417 | 0.00 | 0.31 | 0.318 | O | \| | \| | \| | \| | 1.51 |
| 31.500 | 0.00 | 0.31 | 0.316 | O | \| | \| | \| | \| | 1.51 |
| 31.583 | 0.00 | 0.30 | 0.314 | O | \| | \| | \| | \| | 1.50 |
| 31.667 | 0.00 | 0.30 | 0.312 | O | \| | \| | \| | \| | 1.49 |
| 31.750 | 0.00 | 0.30 | 0.310 | O | \| | \| | \| | \| | 1.48 |
| 31.833 | 0.00 | 0.29 | 0.308 | O | \| | \| | \| | \| | 1.47 |
| 31.917 | 0.00 | 0.29 | 0.306 | O | \| | \| | \| | \| | 1.46 |
| 32.000 | 0.00 | 0.29 | 0.304 | O | \| | \| | \| | \| | 1.46 |
| 32.083 | 0.00 | 0.28 | 0.302 | O | \| | \| | \| | \| | 1.45 |
| 32.167 | 0.00 | 0.28 | 0.300 | O | \| | \| | \| | \| | 1.44 |
| 32.250 | 0.00 | 0.28 | 0.298 | O | \| | \| | \| | \| | 1.43 |
| 32.333 | 0.00 | 0.27 | 0.296 | O | \| | \| | \| | \| | 1.43 |
| 32.417 | 0.00 | 0.27 | 0.294 | O | \| | \| | \| | \| | 1.42 |
| 32.500 | 0.00 | 0.27 | 0.293 | O | \| | \| | \| | \| | 1.41 |
| 32.583 | 0.00 | 0.27 | 0.291 | O | \| | \| | \| | \| | 1.40 |
| 32.667 | 0.00 | 0.26 | 0.289 | O | \| | \| | \| | \| | 1.40 |
| 32.750 | 0.00 | 0.26 | 0.287 | O | \| | \| | \| | \| | 1.39 |
| 32.833 | 0.00 | 0.26 | 0.285 | O | \| | \| | \| | \| | 1.38 |
| 32.917 | 0.00 | 0.25 | 0.284 | O | \| | \| | \| | \| | 1.37 |
| 33.000 | 0.00 | 0.25 | 0.282 | O | \| | \| | \| | \| | 1.37 |
| 33.083 | 0.00 | 0.25 | 0.280 | O | \| | \| | \| | \| | 1.36 |
| 33.167 | 0.00 | 0.25 | 0.278 | O | \| | \| | \| | \| | 1.35 |

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|---|---|---|---|---|---|---|---|---|
| 33.250 | 0.00 | 0.24 | 0.277 | O | \| | \| | \| | 1.35 |
| 33.333 | 0.00 | 0.24 | 0.275 | O | \| | \| | \| | 1.34 |
| 33.417 | 0.00 | 0.24 | 0.273 | O | \| | \| | \| | 1.33 |
| 33.500 | 0.00 | 0.23 | 0.272 | O | \| | \| | \| | 1.33 |
| 33.583 | 0.00 | 0.23 | 0.270 | O | \| | \| | \| | 1.32 |
| 33.667 | 0.00 | 0.23 | 0.269 | O | \| | \| | \| | 1.31 |
| 33.750 | 0.00 | 0.23 | 0.267 | O | \| | \| | \| | 1.31 |
| 33.833 | 0.00 | 0.22 | 0.266 | O | \| | \| | \| | 1.30 |
| 33.917 | 0.00 | 0.22 | 0.264 | O | \| | \| | \| | 1.30 |
| 34.000 | 0.00 | 0.22 | 0.262 | O | \| | \| | \| | 1.29 |
| 34.083 | 0.00 | 0.22 | 0.261 | O | \| | \| | \| | 1.28 |
| 34.167 | 0.00 | 0.21 | 0.259 | O | \| | \| | \| | 1.28 |
| 34.250 | 0.00 | 0.21 | 0.258 | O | \| | \| | \| | 1.27 |
| 34.333 | 0.00 | 0.21 | 0.257 | O | \| | \| | \| | 1.27 |
| 34.417 | 0.00 | 0.21 | 0.255 | O | \| | \| | \| | 1.26 |
| 34.500 | 0.00 | 0.20 | 0.254 | O | \| | \| | \| | 1.25 |
| 34.583 | 0.00 | 0.20 | 0.252 | O | \| | \| | \| | 1.25 |
| 34.667 | 0.00 | 0.20 | 0.251 | O | \| | \| | \| | 1.24 |
| 34.750 | 0.00 | 0.20 | 0.250 | O | \| | \| | \| | 1.24 |
| 34.833 | 0.00 | 0.20 | 0.248 | O | \| | \| | \| | 1.23 |
| 34.917 | 0.00 | 0.19 | 0.247 | O | \| | \| | \| | 1.23 |
| 35.000 | 0.00 | 0.19 | 0.246 | O | \| | \| | \| | 1.22 |
| 35.083 | 0.00 | 0.19 | 0.244 | O | \| | \| | \| | 1.22 |
| 35.167 | 0.00 | 0.19 | 0.243 | O | \| | \| | \| | 1.21 |
| 35.250 | 0.00 | 0.18 | 0.242 | O | \| | \| | \| | 1.21 |
| 35.333 | 0.00 | 0.18 | 0.240 | O | \| | \| | \| | 1.20 |
| 35.417 | 0.00 | 0.18 | 0.239 | O | \| | \| | \| | 1.20 |
| 35.500 | 0.00 | 0.18 | 0.238 | O | \| | \| | \| | 1.19 |
| 35.583 | 0.00 | 0.18 | 0.237 | O | \| | \| | \| | 1.19 |
| 35.667 | 0.00 | 0.17 | 0.235 | O | \| | \| | \| | 1.18 |
| 35.750 | 0.00 | 0.17 | 0.234 | O | \| | \| | \| | 1.18 |
| 35.833 | 0.00 | 0.17 | 0.233 | O | \| | \| | \| | 1.17 |
| 35.917 | 0.00 | 0.17 | 0.232 | O | \| | \| | \| | 1.17 |
| 36.000 | 0.00 | 0.17 | 0.231 | O | \| | \| | \| | 1.16 |
| 36.083 | 0.00 | 0.17 | 0.230 | O | \| | \| | \| | 1.16 |
| 36.167 | 0.00 | 0.16 | 0.229 | O | \| | \| | \| | 1.15 |
| 36.250 | 0.00 | 0.16 | 0.227 | O | \| | \| | \| | 1.15 |
| 36.333 | 0.00 | 0.16 | 0.226 | O | \| | \| | \| | 1.15 |
| 36.417 | 0.00 | 0.16 | 0.225 | O | \| | \| | \| | 1.14 |
| 36.500 | 0.00 | 0.16 | 0.224 | O | \| | \| | \| | 1.14 |
| 36.583 | 0.00 | 0.15 | 0.223 | O | \| | \| | \| | 1.13 |
| 36.667 | 0.00 | 0.15 | 0.222 | O | \| | \| | \| | 1.13 |
| 36.750 | 0.00 | 0.15 | 0.221 | O | \| | \| | \| | 1.12 |
| 36.833 | 0.00 | 0.15 | 0.220 | O | \| | \| | \| | 1.12 |
| 36.917 | 0.00 | 0.15 | 0.219 | O | \| | \| | \| | 1.12 |
| 37.000 | 0.00 | 0.15 | 0.218 | O | \| | \| | \| | 1.11 |
| 37.083 | 0.00 | 0.14 | 0.217 | O | \| | \| | \| | 1.11 |
| 37.167 | 0.00 | 0.14 | 0.216 | O | \| | \| | \| | 1.10 |
| 37.250 | 0.00 | 0.14 | 0.215 | O | \| | \| | \| | 1.10 |
| 37.333 | 0.00 | 0.14 | 0.214 | O | \| | \| | \| | 1.10 |
| 37.417 | 0.00 | 0.14 | 0.213 | O | \| | \| | \| | 1.09 |
| 37.500 | 0.00 | 0.14 | 0.212 | O | \| | \| | \| | 1.09 |

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|---|---|---|---|---|---|---|---|---|
| 37.583 | 0.00 | 0.13 | 0.211 | O | \| | \| | \| | 1.08 |
| 37.667 | 0.00 | 0.13 | 0.210 | O | \| | \| | \| | 1.08 |
| 37.750 | 0.00 | 0.13 | 0.209 | O | \| | \| | \| | 1.08 |
| 37.833 | 0.00 | 0.13 | 0.208 | O | \| | \| | \| | 1.07 |
| 37.917 | 0.00 | 0.13 | 0.208 | O | \| | \| | \| | 1.07 |
| 38.000 | 0.00 | 0.13 | 0.207 | O | \| | \| | \| | 1.07 |
| 38.083 | 0.00 | 0.13 | 0.206 | O | \| | \| | \| | 1.06 |
| 38.167 | 0.00 | 0.12 | 0.205 | O | \| | \| | \| | 1.06 |
| 38.250 | 0.00 | 0.12 | 0.204 | O | \| | \| | \| | 1.06 |
| 38.333 | 0.00 | 0.12 | 0.203 | O | \| | \| | \| | 1.05 |
| 38.417 | 0.00 | 0.12 | 0.202 | O | \| | \| | \| | 1.05 |
| 38.500 | 0.00 | 0.12 | 0.202 | O | \| | \| | \| | 1.05 |
| 38.583 | 0.00 | 0.12 | 0.201 | O | \| | \| | \| | 1.04 |
| 38.667 | 0.00 | 0.12 | 0.200 | O | \| | \| | \| | 1.04 |
| 38.750 | 0.00 | 0.11 | 0.199 | O | \| | \| | \| | 1.04 |
| 38.833 | 0.00 | 0.11 | 0.198 | O | \| | \| | \| | 1.03 |
| 38.917 | 0.00 | 0.11 | 0.198 | O | \| | \| | \| | 1.03 |
| 39.000 | 0.00 | 0.11 | 0.197 | O | \| | \| | \| | 1.03 |
| 39.083 | 0.00 | 0.11 | 0.196 | O | \| | \| | \| | 1.02 |
| 39.167 | 0.00 | 0.11 | 0.195 | O | \| | \| | \| | 1.02 |
| 39.250 | 0.00 | 0.11 | 0.195 | O | \| | \| | \| | 1.02 |
| 39.333 | 0.00 | 0.11 | 0.194 | O | \| | \| | \| | 1.02 |
| 39.417 | 0.00 | 0.11 | 0.193 | O | \| | \| | \| | 1.01 |
| 39.500 | 0.00 | 0.10 | 0.192 | O | \| | \| | \| | 1.01 |
| 39.583 | 0.00 | 0.10 | 0.192 | O | \| | \| | \| | 1.01 |
| 39.667 | 0.00 | 0.10 | 0.191 | O | \| | \| | \| | 1.00 |
| 39.750 | 0.00 | 0.10 | 0.190 | O | \| | \| | \| | 1.00 |
| 39.833 | 0.00 | 0.10 | 0.190 | O | \| | \| | \| | 1.00 |
| 39.917 | 0.00 | 0.10 | 0.189 | O | \| | \| | \| | 0.99 |
| 40.000 | 0.00 | 0.10 | 0.188 | O | \| | \| | \| | 0.99 |
| 40.083 | 0.00 | 0.10 | 0.187 | O | \| | \| | \| | 0.99 |
| 40.167 | 0.00 | 0.10 | 0.187 | O | \| | \| | \| | 0.98 |
| 40.250 | 0.00 | 0.10 | 0.186 | O | \| | \| | \| | 0.98 |
| 40.333 | 0.00 | 0.10 | 0.185 | O | \| | \| | \| | 0.98 |
| 40.417 | 0.00 | 0.10 | 0.185 | O | \| | \| | \| | 0.97 |
| 40.500 | 0.00 | 0.10 | 0.184 | O | \| | \| | \| | 0.97 |
| 40.583 | 0.00 | 0.10 | 0.183 | O | \| | \| | \| | 0.97 |
| 40.667 | 0.00 | 0.10 | 0.183 | O | \| | \| | \| | 0.96 |
| 40.750 | 0.00 | 0.10 | 0.182 | O | \| | \| | \| | 0.96 |
| 40.833 | 0.00 | 0.10 | 0.181 | O | \| | \| | \| | 0.96 |
| 40.917 | 0.00 | 0.10 | 0.181 | O | \| | \| | \| | 0.95 |
| 41.000 | 0.00 | 0.09 | 0.180 | O | \| | \| | \| | 0.95 |
| 41.083 | 0.00 | 0.09 | 0.180 | O | \| | \| | \| | 0.94 |
| 41.167 | 0.00 | 0.09 | 0.179 | O | \| | \| | \| | 0.94 |
| 41.250 | 0.00 | 0.09 | 0.178 | O | \| | \| | \| | 0.94 |
| 41.333 | 0.00 | 0.09 | 0.178 | O | \| | \| | \| | 0.93 |
| 41.417 | 0.00 | 0.09 | 0.177 | O | \| | \| | \| | 0.93 |
| 41.500 | 0.00 | 0.09 | 0.176 | O | \| | \| | \| | 0.93 |
| 41.583 | 0.00 | 0.09 | 0.176 | O | \| | \| | \| | 0.92 |
| 41.667 | 0.00 | 0.09 | 0.175 | O | \| | \| | \| | 0.92 |
| 41.750 | 0.00 | 0.09 | 0.174 | O | \| | \| | \| | 0.92 |
| 41.833 | 0.00 | 0.09 | 0.174 | O | \| | \| | \| | 0.91 |

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|---|---|---|---|---|---|---|---|---|
| 41.917 | 0.00 | 0.09 | 0.173 | O | \| | \| | \| | 0.91 |
| 42.000 | 0.00 | 0.09 | 0.173 | O | \| | \| | \| | 0.91 |
| 42.083 | 0.00 | 0.09 | 0.172 | O | \| | \| | \| | 0.90 |
| 42.167 | 0.00 | 0.09 | 0.171 | O | \| | \| | \| | 0.90 |
| 42.250 | 0.00 | 0.09 | 0.171 | O | \| | \| | \| | 0.90 |
| 42.333 | 0.00 | 0.09 | 0.170 | O | \| | \| | \| | 0.89 |
| 42.417 | 0.00 | 0.09 | 0.169 | O | \| | \| | \| | 0.89 |
| 42.500 | 0.00 | 0.09 | 0.169 | O | \| | \| | \| | 0.89 |
| 42.583 | 0.00 | 0.09 | 0.168 | O | \| | \| | \| | 0.89 |
| 42.667 | 0.00 | 0.09 | 0.168 | O | \| | \| | \| | 0.88 |
| 42.750 | 0.00 | 0.09 | 0.167 | O | \| | \| | \| | 0.88 |
| 42.833 | 0.00 | 0.09 | 0.166 | O | \| | \| | \| | 0.88 |
| 42.917 | 0.00 | 0.09 | 0.166 | O | \| | \| | \| | 0.87 |
| 43.000 | 0.00 | 0.09 | 0.165 | O | \| | \| | \| | 0.87 |
| 43.083 | 0.00 | 0.09 | 0.165 | O | \| | \| | \| | 0.87 |
| 43.167 | 0.00 | 0.09 | 0.164 | O | \| | \| | \| | 0.86 |
| 43.250 | 0.00 | 0.09 | 0.163 | O | \| | \| | \| | 0.86 |
| 43.333 | 0.00 | 0.09 | 0.163 | O | \| | \| | \| | 0.86 |
| 43.417 | 0.00 | 0.09 | 0.162 | O | \| | \| | \| | 0.85 |
| 43.500 | 0.00 | 0.09 | 0.162 | O | \| | \| | \| | 0.85 |
| 43.583 | 0.00 | 0.08 | 0.161 | O | \| | \| | \| | 0.85 |
| 43.667 | 0.00 | 0.08 | 0.160 | O | \| | \| | \| | 0.84 |
| 43.750 | 0.00 | 0.08 | 0.160 | O | \| | \| | \| | 0.84 |
| 43.833 | 0.00 | 0.08 | 0.159 | O | \| | \| | \| | 0.84 |
| 43.917 | 0.00 | 0.08 | 0.159 | O | \| | \| | \| | 0.84 |
| 44.000 | 0.00 | 0.08 | 0.158 | O | \| | \| | \| | 0.83 |
| 44.083 | 0.00 | 0.08 | 0.158 | O | \| | \| | \| | 0.83 |
| 44.167 | 0.00 | 0.08 | 0.157 | O | \| | \| | \| | 0.83 |
| 44.250 | 0.00 | 0.08 | 0.156 | O | \| | \| | \| | 0.82 |
| 44.333 | 0.00 | 0.08 | 0.156 | O | \| | \| | \| | 0.82 |
| 44.417 | 0.00 | 0.08 | 0.155 | O | \| | \| | \| | 0.82 |
| 44.500 | 0.00 | 0.08 | 0.155 | O | \| | \| | \| | 0.81 |
| 44.583 | 0.00 | 0.08 | 0.154 | O | \| | \| | \| | 0.81 |
| 44.667 | 0.00 | 0.08 | 0.154 | O | \| | \| | \| | 0.81 |
| 44.750 | 0.00 | 0.08 | 0.153 | O | \| | \| | \| | 0.81 |
| 44.833 | 0.00 | 0.08 | 0.152 | O | \| | \| | \| | 0.80 |
| 44.917 | 0.00 | 0.08 | 0.152 | O | \| | \| | \| | 0.80 |
| 45.000 | 0.00 | 0.08 | 0.151 | O | \| | \| | \| | 0.80 |
| 45.083 | 0.00 | 0.08 | 0.151 | O | \| | \| | \| | 0.79 |
| 45.167 | 0.00 | 0.08 | 0.150 | O | \| | \| | \| | 0.79 |
| 45.250 | 0.00 | 0.08 | 0.150 | O | \| | \| | \| | 0.79 |
| 45.333 | 0.00 | 0.08 | 0.149 | O | \| | \| | \| | 0.79 |
| 45.417 | 0.00 | 0.08 | 0.149 | O | \| | \| | \| | 0.78 |
| 45.500 | 0.00 | 0.08 | 0.148 | O | \| | \| | \| | 0.78 |
| 45.583 | 0.00 | 0.08 | 0.148 | O | \| | \| | \| | 0.78 |
| 45.667 | 0.00 | 0.08 | 0.147 | O | \| | \| | \| | 0.77 |
| 45.750 | 0.00 | 0.08 | 0.147 | O | \| | \| | \| | 0.77 |
| 45.833 | 0.00 | 0.08 | 0.146 | O | \| | \| | \| | 0.77 |
| 45.917 | 0.00 | 0.08 | 0.145 | O | \| | \| | \| | 0.77 |
| 46.000 | 0.00 | 0.08 | 0.145 | O | \| | \| | \| | 0.76 |
| 46.083 | 0.00 | 0.08 | 0.144 | O | \| | \| | \| | 0.76 |
| 46.167 | 0.00 | 0.08 | 0.144 | O | \| | \| | \| | 0.76 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 46.250 | 0.00 | 0.08 | 0.143 | O | \| | \| | \| | \| | 0.75 |
| 46.333 | 0.00 | 0.08 | 0.143 | O | \| | \| | \| | \| | 0.75 |
| 46.417 | 0.00 | 0.07 | 0.142 | O | \| | \| | \| | \| | 0.75 |
| 46.500 | 0.00 | 0.07 | 0.142 | O | \| | \| | \| | \| | 0.75 |
| 46.583 | 0.00 | 0.07 | 0.141 | O | \| | \| | \| | \| | 0.74 |
| 46.667 | 0.00 | 0.07 | 0.141 | O | \| | \| | \| | \| | 0.74 |
| 46.750 | 0.00 | 0.07 | 0.140 | O | \| | \| | \| | \| | 0.74 |
| 46.833 | 0.00 | 0.07 | 0.140 | O | \| | \| | \| | \| | 0.74 |
| 46.917 | 0.00 | 0.07 | 0.139 | O | \| | \| | \| | \| | 0.73 |
| 47.000 | 0.00 | 0.07 | 0.139 | O | \| | \| | \| | \| | 0.73 |
| 47.083 | 0.00 | 0.07 | 0.138 | O | \| | \| | \| | \| | 0.73 |
| 47.167 | 0.00 | 0.07 | 0.138 | O | \| | \| | \| | \| | 0.73 |
| 47.250 | 0.00 | 0.07 | 0.137 | O | \| | \| | \| | \| | 0.72 |
| 47.333 | 0.00 | 0.07 | 0.137 | O | \| | \| | \| | \| | 0.72 |
| 47.417 | 0.00 | 0.07 | 0.136 | O | \| | \| | \| | \| | 0.72 |
| 47.500 | 0.00 | 0.07 | 0.136 | O | \| | \| | \| | \| | 0.71 |
| 47.583 | 0.00 | 0.07 | 0.135 | O | \| | \| | \| | \| | 0.71 |
| 47.667 | 0.00 | 0.07 | 0.135 | O | \| | \| | \| | \| | 0.71 |
| 47.750 | 0.00 | 0.07 | 0.134 | O | \| | \| | \| | \| | 0.71 |
| 47.833 | 0.00 | 0.07 | 0.134 | O | \| | \| | \| | \| | 0.70 |
| 47.917 | 0.00 | 0.07 | 0.133 | O | \| | \| | \| | \| | 0.70 |
| 48.000 | 0.00 | 0.07 | 0.133 | O | \| | \| | \| | \| | 0.70 |
| 48.083 | 0.00 | 0.07 | 0.132 | O | \| | \| | \| | \| | 0.70 |
| 48.167 | 0.00 | 0.07 | 0.132 | O | \| | \| | \| | \| | 0.69 |
| 48.250 | 0.00 | 0.07 | 0.131 | O | \| | \| | \| | \| | 0.69 |
| 48.333 | 0.00 | 0.07 | 0.131 | O | \| | \| | \| | \| | 0.69 |
| 48.417 | 0.00 | 0.07 | 0.130 | O | \| | \| | \| | \| | 0.69 |
| 48.500 | 0.00 | 0.07 | 0.130 | O | \| | \| | \| | \| | 0.68 |
| 48.583 | 0.00 | 0.07 | 0.130 | O | \| | \| | \| | \| | 0.68 |
| 48.667 | 0.00 | 0.07 | 0.129 | O | \| | \| | \| | \| | 0.68 |
| 48.750 | 0.00 | 0.07 | 0.129 | O | \| | \| | \| | \| | 0.68 |
| 48.833 | 0.00 | 0.07 | 0.128 | O | \| | \| | \| | \| | 0.67 |
| 48.917 | 0.00 | 0.07 | 0.128 | O | \| | \| | \| | \| | 0.67 |
| 49.000 | 0.00 | 0.07 | 0.127 | O | \| | \| | \| | \| | 0.67 |
| 49.083 | 0.00 | 0.07 | 0.127 | O | \| | \| | \| | \| | 0.67 |
| 49.167 | 0.00 | 0.07 | 0.126 | O | \| | \| | \| | \| | 0.66 |
| 49.250 | 0.00 | 0.07 | 0.126 | O | \| | \| | \| | \| | 0.66 |
| 49.333 | 0.00 | 0.07 | 0.125 | O | \| | \| | \| | \| | 0.66 |
| 49.417 | 0.00 | 0.07 | 0.125 | O | \| | \| | \| | \| | 0.66 |
| 49.500 | 0.00 | 0.07 | 0.124 | O | \| | \| | \| | \| | 0.66 |
| 49.583 | 0.00 | 0.07 | 0.124 | O | \| | \| | \| | \| | 0.65 |
| 49.667 | 0.00 | 0.07 | 0.124 | O | \| | \| | \| | \| | 0.65 |
| 49.750 | 0.00 | 0.06 | 0.123 | O | \| | \| | \| | \| | 0.65 |
| 49.833 | 0.00 | 0.06 | 0.123 | O | \| | \| | \| | \| | 0.65 |
| 49.917 | 0.00 | 0.06 | 0.122 | O | \| | \| | \| | \| | 0.64 |
| 50.000 | 0.00 | 0.06 | 0.122 | O | \| | \| | \| | \| | 0.64 |
| 50.083 | 0.00 | 0.06 | 0.121 | O | \| | \| | \| | \| | 0.64 |
| 50.167 | 0.00 | 0.06 | 0.121 | O | \| | \| | \| | \| | 0.64 |
| 50.250 | 0.00 | 0.06 | 0.120 | O | \| | \| | \| | \| | 0.63 |
| 50.333 | 0.00 | 0.06 | 0.120 | O | \| | \| | \| | \| | 0.63 |
| 50.417 | 0.00 | 0.06 | 0.120 | O | \| | \| | \| | \| | 0.63 |
| 50.500 | 0.00 | 0.06 | 0.119 | O | \| | \| | \| | \| | 0.63 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 50.583 | 0.00 | 0.06 | 0.119 | O | \| | \| | \| | 0.63 |
| 50.667 | 0.00 | 0.06 | 0.118 | O | \| | \| | \| | 0.62 |
| 50.750 | 0.00 | 0.06 | 0.118 | O | \| | \| | \| | 0.62 |
| 50.833 | 0.00 | 0.06 | 0.117 | O | \| | \| | \| | 0.62 |
| 50.917 | 0.00 | 0.06 | 0.117 | O | \| | \| | \| | 0.62 |
| 51.000 | 0.00 | 0.06 | 0.117 | O | \| | \| | \| | 0.61 |
| 51.083 | 0.00 | 0.06 | 0.116 | O | \| | \| | \| | 0.61 |
| 51.167 | 0.00 | 0.06 | 0.116 | O | \| | \| | \| | 0.61 |
| 51.250 | 0.00 | 0.06 | 0.115 | O | \| | \| | \| | 0.61 |
| 51.333 | 0.00 | 0.06 | 0.115 | O | \| | \| | \| | 0.60 |
| 51.417 | 0.00 | 0.06 | 0.115 | O | \| | \| | \| | 0.60 |
| 51.500 | 0.00 | 0.06 | 0.114 | O | \| | \| | \| | 0.60 |
| 51.583 | 0.00 | 0.06 | 0.114 | O | \| | \| | \| | 0.60 |
| 51.667 | 0.00 | 0.06 | 0.113 | O | \| | \| | \| | 0.60 |
| 51.750 | 0.00 | 0.06 | 0.113 | O | \| | \| | \| | 0.59 |
| 51.833 | 0.00 | 0.06 | 0.112 | O | \| | \| | \| | 0.59 |
| 51.917 | 0.00 | 0.06 | 0.112 | O | \| | \| | \| | 0.59 |
| 52.000 | 0.00 | 0.06 | 0.112 | O | \| | \| | \| | 0.59 |
| 52.083 | 0.00 | 0.06 | 0.111 | O | \| | \| | \| | 0.59 |
| 52.167 | 0.00 | 0.06 | 0.111 | O | \| | \| | \| | 0.58 |
| 52.250 | 0.00 | 0.06 | 0.110 | O | \| | \| | \| | 0.58 |
| 52.333 | 0.00 | 0.06 | 0.110 | O | \| | \| | \| | 0.58 |
| 52.417 | 0.00 | 0.06 | 0.110 | O | \| | \| | \| | 0.58 |
| 52.500 | 0.00 | 0.06 | 0.109 | O | \| | \| | \| | 0.58 |
| 52.583 | 0.00 | 0.06 | 0.109 | O | \| | \| | \| | 0.57 |
| 52.667 | 0.00 | 0.06 | 0.108 | O | \| | \| | \| | 0.57 |
| 52.750 | 0.00 | 0.06 | 0.108 | O | \| | \| | \| | 0.57 |
| 52.833 | 0.00 | 0.06 | 0.108 | O | \| | \| | \| | 0.57 |
| 52.917 | 0.00 | 0.06 | 0.107 | O | \| | \| | \| | 0.56 |
| 53.000 | 0.00 | 0.06 | 0.107 | O | \| | \| | \| | 0.56 |
| 53.083 | 0.00 | 0.06 | 0.107 | O | \| | \| | \| | 0.56 |
| 53.167 | 0.00 | 0.06 | 0.106 | O | \| | \| | \| | 0.56 |
| 53.250 | 0.00 | 0.06 | 0.106 | O | \| | \| | \| | 0.56 |
| 53.333 | 0.00 | 0.06 | 0.105 | O | \| | \| | \| | 0.55 |
| 53.417 | 0.00 | 0.06 | 0.105 | O | \| | \| | \| | 0.55 |
| 53.500 | 0.00 | 0.06 | 0.105 | O | \| | \| | \| | 0.55 |
| 53.583 | 0.00 | 0.05 | 0.104 | O | \| | \| | \| | 0.55 |
| 53.667 | 0.00 | 0.05 | 0.104 | O | \| | \| | \| | 0.55 |
| 53.750 | 0.00 | 0.05 | 0.103 | O | \| | \| | \| | 0.54 |
| 53.833 | 0.00 | 0.05 | 0.103 | O | \| | \| | \| | 0.54 |
| 53.917 | 0.00 | 0.05 | 0.103 | O | \| | \| | \| | 0.54 |
| 54.000 | 0.00 | 0.05 | 0.102 | O | \| | \| | \| | 0.54 |
| 54.083 | 0.00 | 0.05 | 0.102 | O | \| | \| | \| | 0.54 |
| 54.167 | 0.00 | 0.05 | 0.102 | O | \| | \| | \| | 0.53 |
| 54.250 | 0.00 | 0.05 | 0.101 | O | \| | \| | \| | 0.53 |
| 54.333 | 0.00 | 0.05 | 0.101 | O | \| | \| | \| | 0.53 |
| 54.417 | 0.00 | 0.05 | 0.101 | O | \| | \| | \| | 0.53 |
| 54.500 | 0.00 | 0.05 | 0.100 | O | \| | \| | \| | 0.53 |
| 54.583 | 0.00 | 0.05 | 0.100 | O | \| | \| | \| | 0.53 |
| 54.667 | 0.00 | 0.05 | 0.099 | O | \| | \| | \| | 0.52 |
| 54.750 | 0.00 | 0.05 | 0.099 | O | \| | \| | \| | 0.52 |
| 54.833 | 0.00 | 0.05 | 0.099 | O | \| | \| | \| | 0.52 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 54.917 | 0.00 | 0.05 | 0.098 | O | \| | \| | \| | 0.52 |
| 55.000 | 0.00 | 0.05 | 0.098 | O | \| | \| | \| | 0.52 |
| 55.083 | 0.00 | 0.05 | 0.098 | O | \| | \| | \| | 0.51 |
| 55.167 | 0.00 | 0.05 | 0.097 | O | \| | \| | \| | 0.51 |
| 55.250 | 0.00 | 0.05 | 0.097 | O | \| | \| | \| | 0.51 |
| 55.333 | 0.00 | 0.05 | 0.097 | O | \| | \| | \| | 0.51 |
| 55.417 | 0.00 | 0.05 | 0.096 | O | \| | \| | \| | 0.51 |
| 55.500 | 0.00 | 0.05 | 0.096 | O | \| | \| | \| | 0.50 |
| 55.583 | 0.00 | 0.05 | 0.096 | O | \| | \| | \| | 0.50 |
| 55.667 | 0.00 | 0.05 | 0.095 | O | \| | \| | \| | 0.50 |
| 55.750 | 0.00 | 0.05 | 0.095 | O | \| | \| | \| | 0.50 |
| 55.833 | 0.00 | 0.05 | 0.095 | O | \| | \| | \| | 0.50 |
| 55.917 | 0.00 | 0.05 | 0.094 | O | \| | \| | \| | 0.50 |
| 56.000 | 0.00 | 0.05 | 0.094 | O | \| | \| | \| | 0.49 |
| 56.083 | 0.00 | 0.05 | 0.093 | O | \| | \| | \| | 0.49 |
| 56.167 | 0.00 | 0.05 | 0.093 | O | \| | \| | \| | 0.49 |
| 56.250 | 0.00 | 0.05 | 0.093 | O | \| | \| | \| | 0.49 |
| 56.333 | 0.00 | 0.05 | 0.092 | O | \| | \| | \| | 0.49 |
| 56.417 | 0.00 | 0.05 | 0.092 | O | \| | \| | \| | 0.48 |
| 56.500 | 0.00 | 0.05 | 0.092 | O | \| | \| | \| | 0.48 |
| 56.583 | 0.00 | 0.05 | 0.091 | O | \| | \| | \| | 0.48 |
| 56.667 | 0.00 | 0.05 | 0.091 | O | \| | \| | \| | 0.48 |
| 56.750 | 0.00 | 0.05 | 0.091 | O | \| | \| | \| | 0.48 |
| 56.833 | 0.00 | 0.05 | 0.090 | O | \| | \| | \| | 0.48 |
| 56.917 | 0.00 | 0.05 | 0.090 | O | \| | \| | \| | 0.47 |
| 57.000 | 0.00 | 0.05 | 0.090 | O | \| | \| | \| | 0.47 |
| 57.083 | 0.00 | 0.05 | 0.090 | O | \| | \| | \| | 0.47 |
| 57.167 | 0.00 | 0.05 | 0.089 | O | \| | \| | \| | 0.47 |
| 57.250 | 0.00 | 0.05 | 0.089 | O | \| | \| | \| | 0.47 |
| 57.333 | 0.00 | 0.05 | 0.089 | O | \| | \| | \| | 0.47 |
| 57.417 | 0.00 | 0.05 | 0.088 | O | \| | \| | \| | 0.46 |
| 57.500 | 0.00 | 0.05 | 0.088 | O | \| | \| | \| | 0.46 |
| 57.583 | 0.00 | 0.05 | 0.088 | O | \| | \| | \| | 0.46 |
| 57.667 | 0.00 | 0.05 | 0.087 | O | \| | \| | \| | 0.46 |
| 57.750 | 0.00 | 0.05 | 0.087 | O | \| | \| | \| | 0.46 |
| 57.833 | 0.00 | 0.05 | 0.087 | O | \| | \| | \| | 0.46 |
| 57.917 | 0.00 | 0.05 | 0.086 | O | \| | \| | \| | 0.45 |
| 58.000 | 0.00 | 0.05 | 0.086 | O | \| | \| | \| | 0.45 |
| 58.083 | 0.00 | 0.05 | 0.086 | O | \| | \| | \| | 0.45 |
| 58.167 | 0.00 | 0.04 | 0.085 | O | \| | \| | \| | 0.45 |
| 58.250 | 0.00 | 0.04 | 0.085 | O | \| | \| | \| | 0.45 |
| 58.333 | 0.00 | 0.04 | 0.085 | O | \| | \| | \| | 0.45 |
| 58.417 | 0.00 | 0.04 | 0.084 | O | \| | \| | \| | 0.44 |
| 58.500 | 0.00 | 0.04 | 0.084 | O | \| | \| | \| | 0.44 |
| 58.583 | 0.00 | 0.04 | 0.084 | O | \| | \| | \| | 0.44 |
| 58.667 | 0.00 | 0.04 | 0.084 | O | \| | \| | \| | 0.44 |
| 58.750 | 0.00 | 0.04 | 0.083 | O | \| | \| | \| | 0.44 |
| 58.833 | 0.00 | 0.04 | 0.083 | O | \| | \| | \| | 0.44 |
| 58.917 | 0.00 | 0.04 | 0.083 | O | \| | \| | \| | 0.43 |
| 59.000 | 0.00 | 0.04 | 0.082 | O | \| | \| | \| | 0.43 |
| 59.083 | 0.00 | 0.04 | 0.082 | O | \| | \| | \| | 0.43 |
| 59.167 | 0.00 | 0.04 | 0.082 | O | \| | \| | \| | 0.43 |

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|---|---|---|---|---|---|---|---|---|
| 59.250 | 0.00 | 0.04 | 0.081 | O | \| | \| | \| | 0.43 |
| 59.333 | 0.00 | 0.04 | 0.081 | O | \| | \| | \| | 0.43 |
| 59.417 | 0.00 | 0.04 | 0.081 | O | \| | \| | \| | 0.43 |
| 59.500 | 0.00 | 0.04 | 0.081 | O | \| | \| | \| | 0.42 |
| 59.583 | 0.00 | 0.04 | 0.080 | O | \| | \| | \| | 0.42 |
| 59.667 | 0.00 | 0.04 | 0.080 | O | \| | \| | \| | 0.42 |
| 59.750 | 0.00 | 0.04 | 0.080 | O | \| | \| | \| | 0.42 |
| 59.833 | 0.00 | 0.04 | 0.079 | O | \| | \| | \| | 0.42 |
| 59.917 | 0.00 | 0.04 | 0.079 | O | \| | \| | \| | 0.42 |
| 60.000 | 0.00 | 0.04 | 0.079 | O | \| | \| | \| | 0.41 |
| 60.083 | 0.00 | 0.04 | 0.079 | O | \| | \| | \| | 0.41 |
| 60.167 | 0.00 | 0.04 | 0.078 | O | \| | \| | \| | 0.41 |
| 60.250 | 0.00 | 0.04 | 0.078 | O | \| | \| | \| | 0.41 |
| 60.333 | 0.00 | 0.04 | 0.078 | O | \| | \| | \| | 0.41 |
| 60.417 | 0.00 | 0.04 | 0.077 | O | \| | \| | \| | 0.41 |
| 60.500 | 0.00 | 0.04 | 0.077 | O | \| | \| | \| | 0.41 |
| 60.583 | 0.00 | 0.04 | 0.077 | O | \| | \| | \| | 0.40 |
| 60.667 | 0.00 | 0.04 | 0.077 | O | \| | \| | \| | 0.40 |
| 60.750 | 0.00 | 0.04 | 0.076 | O | \| | \| | \| | 0.40 |
| 60.833 | 0.00 | 0.04 | 0.076 | O | \| | \| | \| | 0.40 |
| 60.917 | 0.00 | 0.04 | 0.076 | O | \| | \| | \| | 0.40 |
| 61.000 | 0.00 | 0.04 | 0.075 | O | \| | \| | \| | 0.40 |
| 61.083 | 0.00 | 0.04 | 0.075 | O | \| | \| | \| | 0.40 |
| 61.167 | 0.00 | 0.04 | 0.075 | O | \| | \| | \| | 0.39 |
| 61.250 | 0.00 | 0.04 | 0.075 | O | \| | \| | \| | 0.39 |
| 61.333 | 0.00 | 0.04 | 0.074 | O | \| | \| | \| | 0.39 |
| 61.417 | 0.00 | 0.04 | 0.074 | O | \| | \| | \| | 0.39 |
| 61.500 | 0.00 | 0.04 | 0.074 | O | \| | \| | \| | 0.39 |
| 61.583 | 0.00 | 0.04 | 0.074 | O | \| | \| | \| | 0.39 |
| 61.667 | 0.00 | 0.04 | 0.073 | O | \| | \| | \| | 0.39 |
| 61.750 | 0.00 | 0.04 | 0.073 | O | \| | \| | \| | 0.38 |
| 61.833 | 0.00 | 0.04 | 0.073 | O | \| | \| | \| | 0.38 |
| 61.917 | 0.00 | 0.04 | 0.073 | O | \| | \| | \| | 0.38 |
| 62.000 | 0.00 | 0.04 | 0.072 | O | \| | \| | \| | 0.38 |
| 62.083 | 0.00 | 0.04 | 0.072 | O | \| | \| | \| | 0.38 |
| 62.167 | 0.00 | 0.04 | 0.072 | O | \| | \| | \| | 0.38 |
| 62.250 | 0.00 | 0.04 | 0.071 | O | \| | \| | \| | 0.38 |
| 62.333 | 0.00 | 0.04 | 0.071 | O | \| | \| | \| | 0.37 |
| 62.417 | 0.00 | 0.04 | 0.071 | O | \| | \| | \| | 0.37 |
| 62.500 | 0.00 | 0.04 | 0.071 | O | \| | \| | \| | 0.37 |
| 62.583 | 0.00 | 0.04 | 0.070 | O | \| | \| | \| | 0.37 |
| 62.667 | 0.00 | 0.04 | 0.070 | O | \| | \| | \| | 0.37 |
| 62.750 | 0.00 | 0.04 | 0.070 | O | \| | \| | \| | 0.37 |
| 62.833 | 0.00 | 0.04 | 0.070 | O | \| | \| | \| | 0.37 |
| 62.917 | 0.00 | 0.04 | 0.069 | O | \| | \| | \| | 0.37 |
| 63.000 | 0.00 | 0.04 | 0.069 | O | \| | \| | \| | 0.36 |
| 63.083 | 0.00 | 0.04 | 0.069 | O | \| | \| | \| | 0.36 |
| 63.167 | 0.00 | 0.04 | 0.069 | O | \| | \| | \| | 0.36 |
| 63.250 | 0.00 | 0.04 | 0.068 | O | \| | \| | \| | 0.36 |
| 63.333 | 0.00 | 0.04 | 0.068 | O | \| | \| | \| | 0.36 |
| 63.417 | 0.00 | 0.04 | 0.068 | O | \| | \| | \| | 0.36 |
| 63.500 | 0.00 | 0.04 | 0.068 | O | \| | \| | \| | 0.36 |

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|---|---|---|---|---|---|---|---|---|
| 63.583 | 0.00 | 0.04 | 0.067 | O | \| | \| | \| | 0.36 |
| 63.667 | 0.00 | 0.04 | 0.067 | O | \| | \| | \| | 0.35 |
| 63.750 | 0.00 | 0.04 | 0.067 | O | \| | \| | \| | 0.35 |
| 63.833 | 0.00 | 0.04 | 0.067 | O | \| | \| | \| | 0.35 |
| 63.917 | 0.00 | 0.03 | 0.066 | O | \| | \| | \| | 0.35 |
| 64.000 | 0.00 | 0.03 | 0.066 | O | \| | \| | \| | 0.35 |
| 64.083 | 0.00 | 0.03 | 0.066 | O | \| | \| | \| | 0.35 |
| 64.167 | 0.00 | 0.03 | 0.066 | O | \| | \| | \| | 0.35 |
| 64.250 | 0.00 | 0.03 | 0.066 | O | \| | \| | \| | 0.34 |
| 64.333 | 0.00 | 0.03 | 0.065 | O | \| | \| | \| | 0.34 |
| 64.417 | 0.00 | 0.03 | 0.065 | O | \| | \| | \| | 0.34 |
| 64.500 | 0.00 | 0.03 | 0.065 | O | \| | \| | \| | 0.34 |
| 64.583 | 0.00 | 0.03 | 0.065 | O | \| | \| | \| | 0.34 |
| 64.667 | 0.00 | 0.03 | 0.064 | O | \| | \| | \| | 0.34 |
| 64.750 | 0.00 | 0.03 | 0.064 | O | \| | \| | \| | 0.34 |
| 64.833 | 0.00 | 0.03 | 0.064 | O | \| | \| | \| | 0.34 |
| 64.917 | 0.00 | 0.03 | 0.064 | O | \| | \| | \| | 0.34 |
| 65.000 | 0.00 | 0.03 | 0.063 | O | \| | \| | \| | 0.33 |
| 65.083 | 0.00 | 0.03 | 0.063 | O | \| | \| | \| | 0.33 |
| 65.167 | 0.00 | 0.03 | 0.063 | O | \| | \| | \| | 0.33 |
| 65.250 | 0.00 | 0.03 | 0.063 | O | \| | \| | \| | 0.33 |
| 65.333 | 0.00 | 0.03 | 0.063 | O | \| | \| | \| | 0.33 |
| 65.417 | 0.00 | 0.03 | 0.062 | O | \| | \| | \| | 0.33 |
| 65.500 | 0.00 | 0.03 | 0.062 | O | \| | \| | \| | 0.33 |
| 65.583 | 0.00 | 0.03 | 0.062 | O | \| | \| | \| | 0.33 |
| 65.667 | 0.00 | 0.03 | 0.062 | O | \| | \| | \| | 0.32 |
| 65.750 | 0.00 | 0.03 | 0.061 | O | \| | \| | \| | 0.32 |
| 65.833 | 0.00 | 0.03 | 0.061 | O | \| | \| | \| | 0.32 |
| 65.917 | 0.00 | 0.03 | 0.061 | O | \| | \| | \| | 0.32 |
| 66.000 | 0.00 | 0.03 | 0.061 | O | \| | \| | \| | 0.32 |
| 66.083 | 0.00 | 0.03 | 0.061 | O | \| | \| | \| | 0.32 |
| 66.167 | 0.00 | 0.03 | 0.060 | O | \| | \| | \| | 0.32 |
| 66.250 | 0.00 | 0.03 | 0.060 | O | \| | \| | \| | 0.32 |
| 66.333 | 0.00 | 0.03 | 0.060 | O | \| | \| | \| | 0.32 |
| 66.417 | 0.00 | 0.03 | 0.060 | O | \| | \| | \| | 0.31 |
| 66.500 | 0.00 | 0.03 | 0.059 | O | \| | \| | \| | 0.31 |
| 66.583 | 0.00 | 0.03 | 0.059 | O | \| | \| | \| | 0.31 |
| 66.667 | 0.00 | 0.03 | 0.059 | O | \| | \| | \| | 0.31 |
| 66.750 | 0.00 | 0.03 | 0.059 | O | \| | \| | \| | 0.31 |
| 66.833 | 0.00 | 0.03 | 0.059 | O | \| | \| | \| | 0.31 |
| 66.917 | 0.00 | 0.03 | 0.058 | O | \| | \| | \| | 0.31 |
| 67.000 | 0.00 | 0.03 | 0.058 | O | \| | \| | \| | 0.31 |
| 67.083 | 0.00 | 0.03 | 0.058 | O | \| | \| | \| | 0.30 |
| 67.167 | 0.00 | 0.03 | 0.058 | O | \| | \| | \| | 0.30 |
| 67.250 | 0.00 | 0.03 | 0.058 | O | \| | \| | \| | 0.30 |
| 67.333 | 0.00 | 0.03 | 0.057 | O | \| | \| | \| | 0.30 |
| 67.417 | 0.00 | 0.03 | 0.057 | O | \| | \| | \| | 0.30 |
| 67.500 | 0.00 | 0.03 | 0.057 | O | \| | \| | \| | 0.30 |
| 67.583 | 0.00 | 0.03 | 0.057 | O | \| | \| | \| | 0.30 |
| 67.667 | 0.00 | 0.03 | 0.056 | O | \| | \| | \| | 0.30 |
| 67.750 | 0.00 | 0.03 | 0.056 | O | \| | \| | \| | 0.30 |
| 67.833 | 0.00 | 0.03 | 0.056 | O | \| | \| | \| | 0.30 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 67.917 | 0.00 | 0.03 | 0.056 | O | \| | \| | \| | 0.29 |
| 68.000 | 0.00 | 0.03 | 0.056 | O | \| | \| | \| | 0.29 |
| 68.083 | 0.00 | 0.03 | 0.055 | O | \| | \| | \| | 0.29 |
| 68.167 | 0.00 | 0.03 | 0.055 | O | \| | \| | \| | 0.29 |
| 68.250 | 0.00 | 0.03 | 0.055 | O | \| | \| | \| | 0.29 |
| 68.333 | 0.00 | 0.03 | 0.055 | O | \| | \| | \| | 0.29 |
| 68.417 | 0.00 | 0.03 | 0.055 | O | \| | \| | \| | 0.29 |
| 68.500 | 0.00 | 0.03 | 0.054 | O | \| | \| | \| | 0.29 |
| 68.583 | 0.00 | 0.03 | 0.054 | O | \| | \| | \| | 0.29 |
| 68.667 | 0.00 | 0.03 | 0.054 | O | \| | \| | \| | 0.28 |
| 68.750 | 0.00 | 0.03 | 0.054 | O | \| | \| | \| | 0.28 |
| 68.833 | 0.00 | 0.03 | 0.054 | O | \| | \| | \| | 0.28 |
| 68.917 | 0.00 | 0.03 | 0.053 | O | \| | \| | \| | 0.28 |
| 69.000 | 0.00 | 0.03 | 0.053 | O | \| | \| | \| | 0.28 |
| 69.083 | 0.00 | 0.03 | 0.053 | O | \| | \| | \| | 0.28 |
| 69.167 | 0.00 | 0.03 | 0.053 | O | \| | \| | \| | 0.28 |
| 69.250 | 0.00 | 0.03 | 0.053 | O | \| | \| | \| | 0.28 |
| 69.333 | 0.00 | 0.03 | 0.053 | O | \| | \| | \| | 0.28 |
| 69.417 | 0.00 | 0.03 | 0.052 | O | \| | \| | \| | 0.28 |
| 69.500 | 0.00 | 0.03 | 0.052 | O | \| | \| | \| | 0.27 |
| 69.583 | 0.00 | 0.03 | 0.052 | O | \| | \| | \| | 0.27 |
| 69.667 | 0.00 | 0.03 | 0.052 | O | \| | \| | \| | 0.27 |
| 69.750 | 0.00 | 0.03 | 0.052 | O | \| | \| | \| | 0.27 |
| 69.833 | 0.00 | 0.03 | 0.051 | O | \| | \| | \| | 0.27 |
| 69.917 | 0.00 | 0.03 | 0.051 | O | \| | \| | \| | 0.27 |
| 70.000 | 0.00 | 0.03 | 0.051 | O | \| | \| | \| | 0.27 |
| 70.083 | 0.00 | 0.03 | 0.051 | O | \| | \| | \| | 0.27 |
| 70.167 | 0.00 | 0.03 | 0.051 | O | \| | \| | \| | 0.27 |
| 70.250 | 0.00 | 0.03 | 0.050 | O | \| | \| | \| | 0.27 |
| 70.333 | 0.00 | 0.03 | 0.050 | O | \| | \| | \| | 0.26 |
| 70.417 | 0.00 | 0.03 | 0.050 | O | \| | \| | \| | 0.26 |
| 70.500 | 0.00 | 0.03 | 0.050 | O | \| | \| | \| | 0.26 |
| 70.583 | 0.00 | 0.03 | 0.050 | O | \| | \| | \| | 0.26 |
| 70.667 | 0.00 | 0.03 | 0.050 | O | \| | \| | \| | 0.26 |
| 70.750 | 0.00 | 0.03 | 0.049 | O | \| | \| | \| | 0.26 |
| 70.833 | 0.00 | 0.03 | 0.049 | O | \| | \| | \| | 0.26 |
| 70.917 | 0.00 | 0.03 | 0.049 | O | \| | \| | \| | 0.26 |
| 71.000 | 0.00 | 0.03 | 0.049 | O | \| | \| | \| | 0.26 |
| 71.083 | 0.00 | 0.03 | 0.049 | O | \| | \| | \| | 0.26 |
| 71.167 | 0.00 | 0.03 | 0.049 | O | \| | \| | \| | 0.26 |
| 71.250 | 0.00 | 0.03 | 0.048 | O | \| | \| | \| | 0.25 |
| 71.333 | 0.00 | 0.03 | 0.048 | O | \| | \| | \| | 0.25 |
| 71.417 | 0.00 | 0.03 | 0.048 | O | \| | \| | \| | 0.25 |
| 71.500 | 0.00 | 0.03 | 0.048 | O | \| | \| | \| | 0.25 |
| 71.583 | 0.00 | 0.03 | 0.048 | O | \| | \| | \| | 0.25 |
| 71.667 | 0.00 | 0.02 | 0.047 | O | \| | \| | \| | 0.25 |
| 71.750 | 0.00 | 0.02 | 0.047 | O | \| | \| | \| | 0.25 |
| 71.833 | 0.00 | 0.02 | 0.047 | O | \| | \| | \| | 0.25 |
| 71.917 | 0.00 | 0.02 | 0.047 | O | \| | \| | \| | 0.25 |
| 72.000 | 0.00 | 0.02 | 0.047 | O | \| | \| | \| | 0.25 |
| 72.083 | 0.00 | 0.02 | 0.047 | O | \| | \| | \| | 0.25 |
| 72.167 | 0.00 | 0.02 | 0.046 | O | \| | \| | \| | 0.24 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 72.250 | 0.00 | 0.02 | 0.046 | O | \| | \| | \| | 0.24 |
| 72.333 | 0.00 | 0.02 | 0.046 | O | \| | \| | \| | 0.24 |
| 72.417 | 0.00 | 0.02 | 0.046 | O | \| | \| | \| | 0.24 |
| 72.500 | 0.00 | 0.02 | 0.046 | O | \| | \| | \| | 0.24 |
| 72.583 | 0.00 | 0.02 | 0.046 | O | \| | \| | \| | 0.24 |
| 72.667 | 0.00 | 0.02 | 0.045 | O | \| | \| | \| | 0.24 |
| 72.750 | 0.00 | 0.02 | 0.045 | O | \| | \| | \| | 0.24 |
| 72.833 | 0.00 | 0.02 | 0.045 | O | \| | \| | \| | 0.24 |
| 72.917 | 0.00 | 0.02 | 0.045 | O | \| | \| | \| | 0.24 |
| 73.000 | 0.00 | 0.02 | 0.045 | O | \| | \| | \| | 0.24 |
| 73.083 | 0.00 | 0.02 | 0.045 | O | \| | \| | \| | 0.23 |
| 73.167 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 73.250 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 73.333 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 73.417 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 73.500 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 73.583 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 73.667 | 0.00 | 0.02 | 0.044 | O | \| | \| | \| | 0.23 |
| 73.750 | 0.00 | 0.02 | 0.043 | O | \| | \| | \| | 0.23 |
| 73.833 | 0.00 | 0.02 | 0.043 | O | \| | \| | \| | 0.23 |
| 73.917 | 0.00 | 0.02 | 0.043 | O | \| | \| | \| | 0.23 |
| 74.000 | 0.00 | 0.02 | 0.043 | O | \| | \| | \| | 0.23 |
| 74.083 | 0.00 | 0.02 | 0.043 | O | \| | \| | \| | 0.22 |
| 74.167 | 0.00 | 0.02 | 0.043 | O | \| | \| | \| | 0.22 |
| 74.250 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 74.333 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 74.417 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 74.500 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 74.583 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 74.667 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 74.750 | 0.00 | 0.02 | 0.042 | O | \| | \| | \| | 0.22 |
| 74.833 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.22 |
| 74.917 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.22 |
| 75.000 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.22 |
| 75.083 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.22 |
| 75.167 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.21 |
| 75.250 | 0.00 | 0.02 | 0.041 | O | \| | \| | \| | 0.21 |
| 75.333 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 75.417 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 75.500 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 75.583 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 75.667 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 75.750 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 75.833 | 0.00 | 0.02 | 0.040 | O | \| | \| | \| | 0.21 |
| 75.917 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.21 |
| 76.000 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.21 |
| 76.083 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.21 |
| 76.167 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.21 |
| 76.250 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.20 |
| 76.333 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.20 |
| 76.417 | 0.00 | 0.02 | 0.039 | O | \| | \| | \| | 0.20 |
| 76.500 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |

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|---|---|---|---|---|---|---|---|---|
| 76.583 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 76.667 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 76.750 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 76.833 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 76.917 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 77.000 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 77.083 | 0.00 | 0.02 | 0.038 | O | \| | \| | \| | 0.20 |
| 77.167 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.20 |
| 77.250 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.20 |
| 77.333 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.20 |
| 77.417 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.19 |
| 77.500 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.19 |
| 77.583 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.19 |
| 77.667 | 0.00 | 0.02 | 0.037 | O | \| | \| | \| | 0.19 |
| 77.750 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 77.833 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 77.917 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 78.000 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 78.083 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 78.167 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 78.250 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 78.333 | 0.00 | 0.02 | 0.036 | O | \| | \| | \| | 0.19 |
| 78.417 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.19 |
| 78.500 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.19 |
| 78.583 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.18 |
| 78.667 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.18 |
| 78.750 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.18 |
| 78.833 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.18 |
| 78.917 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.18 |
| 79.000 | 0.00 | 0.02 | 0.035 | O | \| | \| | \| | 0.18 |
| 79.083 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 79.167 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 79.250 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 79.333 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 79.417 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 79.500 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 79.583 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 79.667 | 0.00 | 0.02 | 0.034 | O | \| | \| | \| | 0.18 |
| 79.750 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.18 |
| 79.833 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.18 |
| 79.917 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.17 |
| 80.000 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.17 |
| 80.083 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.17 |
| 80.167 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.17 |
| 80.250 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.17 |
| 80.333 | 0.00 | 0.02 | 0.033 | O | \| | \| | \| | 0.17 |
| 80.417 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 80.500 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 80.583 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 80.667 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 80.750 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 80.833 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |

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|---|---|---|---|---|---|---|---|---|
| 80.917 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 81.000 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 81.083 | 0.00 | 0.02 | 0.032 | O | \| | \| | \| | 0.17 |
| 81.167 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.17 |
| 81.250 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 81.333 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 81.417 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 81.500 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 81.583 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 81.667 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 81.750 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 81.833 | 0.00 | 0.02 | 0.031 | O | \| | \| | \| | 0.16 |
| 81.917 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 82.000 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 82.083 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 82.167 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 82.250 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 82.333 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 82.417 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 82.500 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 82.583 | 0.00 | 0.02 | 0.030 | O | \| | \| | \| | 0.16 |
| 82.667 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 82.750 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 82.833 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 82.917 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 83.000 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 83.083 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 83.167 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 83.250 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 83.333 | 0.00 | 0.02 | 0.029 | O | \| | \| | \| | 0.15 |
| 83.417 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 83.500 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 83.583 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 83.667 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 83.750 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 83.833 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 83.917 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 84.000 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 84.083 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 84.167 | 0.00 | 0.01 | 0.028 | O | \| | \| | \| | 0.15 |
| 84.250 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 84.333 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 84.417 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 84.500 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 84.583 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 84.667 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 84.750 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 84.833 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 84.917 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 85.000 | 0.00 | 0.01 | 0.027 | O | \| | \| | \| | 0.14 |
| 85.083 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 85.167 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 85.250 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 85.333 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 85.417 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 85.500 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 85.583 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 85.667 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 85.750 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.14 |
| 85.833 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.13 |
| 85.917 | 0.00 | 0.01 | 0.026 | O | \| | \| | \| | 0.13 |
| 86.000 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 86.083 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 86.167 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 86.250 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 86.333 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 86.417 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 86.500 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 86.583 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 86.667 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 86.750 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 86.833 | 0.00 | 0.01 | 0.025 | O | \| | \| | \| | 0.13 |
| 86.917 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 87.000 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 87.083 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 87.167 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 87.250 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 87.333 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 87.417 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 87.500 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 87.583 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.13 |
| 87.667 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.12 |
| 87.750 | 0.00 | 0.01 | 0.024 | O | \| | \| | \| | 0.12 |
| 87.833 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 87.917 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 88.000 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 88.083 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 88.167 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 88.250 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 88.333 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 88.417 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 88.500 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 88.583 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 88.667 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 88.750 | 0.00 | 0.01 | 0.023 | O | \| | \| | \| | 0.12 |
| 88.833 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 88.917 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 89.000 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 89.083 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 89.167 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 89.250 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 89.333 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 89.417 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |
| 89.500 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | 0.12 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 89.583 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | \| | 0.11 |
| 89.667 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | \| | 0.11 |
| 89.750 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | \| | 0.11 |
| 89.833 | 0.00 | 0.01 | 0.022 | O | \| | \| | \| | \| | 0.11 |
| 89.917 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 90.000 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 90.083 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 90.167 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 90.250 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 90.333 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 90.417 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 90.500 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 90.583 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 90.667 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 90.750 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 90.833 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 90.917 | 0.00 | 0.01 | 0.021 | O | \| | \| | \| | \| | 0.11 |
| 91.000 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.11 |
| 91.083 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.11 |
| 91.167 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.11 |
| 91.250 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.11 |
| 91.333 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.11 |
| 91.417 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.11 |
| 91.500 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.11 |
| 91.583 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.11 |
| 91.667 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.10 |
| 91.750 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.10 |
| 91.833 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.10 |
| 91.917 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.10 |
| 92.000 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.10 |
| 92.083 | 0.00 | 0.01 | 0.020 | O | \| | \| | \| | \| | 0.10 |
| 92.167 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 92.250 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 92.333 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 92.417 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 92.500 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 92.583 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 92.667 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 92.750 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 92.833 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 92.917 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 93.000 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 93.083 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 93.167 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 93.250 | 0.00 | 0.01 | 0.019 | O | \| | \| | \| | \| | 0.10 |
| 93.333 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | \| | 0.10 |
| 93.417 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | \| | 0.10 |
| 93.500 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | \| | 0.10 |
| 93.583 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | \| | 0.10 |
| 93.667 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | \| | 0.10 |
| 93.750 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | \| | 0.10 |
| 93.833 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | \| | 0.10 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 93.917 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 94.000 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 94.083 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 94.167 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 94.250 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 94.333 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 94.417 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 94.500 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 94.583 | 0.00 | 0.01 | 0.018 | O | \| | \| | \| | 0.09 |
| 94.667 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 94.750 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 94.833 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 94.917 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 95.000 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 95.083 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 95.167 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 95.250 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 95.333 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 95.417 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 95.500 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 95.583 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 95.667 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 95.750 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 95.833 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 95.917 | 0.00 | 0.01 | 0.017 | O | \| | \| | \| | 0.09 |
| 96.000 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.09 |
| 96.083 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.09 |
| 96.167 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.09 |
| 96.250 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.09 |
| 96.333 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.09 |
| 96.417 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.09 |
| 96.500 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 96.583 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 96.667 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 96.750 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 96.833 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 96.917 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 97.000 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 97.083 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 97.167 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 97.250 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 97.333 | 0.00 | 0.01 | 0.016 | O | \| | \| | \| | 0.08 |
| 97.417 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 97.500 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 97.583 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 97.667 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 97.750 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 97.833 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 97.917 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 98.000 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 98.083 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 98.167 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 98.250 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 98.333 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 98.417 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 98.500 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 98.583 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 98.667 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 98.750 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 98.833 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 98.917 | 0.00 | 0.01 | 0.015 | O | \| | \| | \| | 0.08 |
| 99.000 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.08 |
| 99.083 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.08 |
| 99.167 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.08 |
| 99.250 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.08 |
| 99.333 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 99.417 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 99.500 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 99.583 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 99.667 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 99.750 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 99.833 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 99.917 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 100.000 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 100.083 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 100.167 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 100.250 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 100.333 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 100.417 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 100.500 | 0.00 | 0.01 | 0.014 | O | \| | \| | \| | 0.07 |
| 100.583 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 100.667 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 100.750 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 100.833 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 100.917 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 101.000 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 101.083 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 101.167 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 101.250 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 101.333 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 101.417 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 101.500 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 101.583 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 101.667 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 101.750 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 101.833 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 101.917 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 102.000 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 102.083 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 102.167 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 102.250 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 102.333 | 0.00 | 0.01 | 0.013 | O | \| | \| | \| | 0.07 |
| 102.417 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.07 |
| 102.500 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.07 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 102.583 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.07 |
| 102.667 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 102.750 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 102.833 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 102.917 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 103.000 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 103.083 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 103.167 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 103.250 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 103.333 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 103.417 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 103.500 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 103.583 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 103.667 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 103.750 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 103.833 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 103.917 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 104.000 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 104.083 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 104.167 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 104.250 | 0.00 | 0.01 | 0.012 | O | \| | \| | \| | 0.06 |
| 104.333 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 104.417 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 104.500 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 104.583 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 104.667 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 104.750 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 104.833 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 104.917 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 105.000 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 105.083 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 105.167 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 105.250 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 105.333 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 105.417 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 105.500 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 105.583 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 105.667 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 105.750 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 105.833 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 105.917 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 106.000 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 106.083 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 106.167 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 106.250 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 106.333 | 0.00 | 0.01 | 0.011 | O | \| | \| | \| | 0.06 |
| 106.417 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.06 |
| 106.500 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 106.583 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 106.667 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 106.750 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 106.833 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 106.917 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 107.000 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 107.083 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 107.167 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 107.250 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 107.333 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 107.417 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 107.500 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 107.583 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 107.667 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 107.750 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 107.833 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 107.917 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 108.000 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 108.083 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 108.167 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 108.250 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 108.333 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 108.417 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 108.500 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 108.583 | 0.00 | 0.01 | 0.010 | O | \| | \| | \| | 0.05 |
| 108.667 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 108.750 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 108.833 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 108.917 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 109.000 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 109.083 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 109.167 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 109.250 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 109.333 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 109.417 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 109.500 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 109.583 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 109.667 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 109.750 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 109.833 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 109.917 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 110.000 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 110.083 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 110.167 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 110.250 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 110.333 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 110.417 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 110.500 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 110.583 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 110.667 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 110.750 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 110.833 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 110.917 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 111.000 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.05 |
| 111.083 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.04 |
| 111.167 | 0.00 | 0.00 | 0.009 | O | \| | \| | \| | 0.04 |

| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 111.250 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 111.333 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 111.417 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 111.500 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 111.583 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 111.667 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 111.750 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 111.833 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 111.917 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 112.000 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 112.083 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 112.167 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 112.250 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 112.333 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 112.417 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 112.500 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 112.583 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 112.667 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 112.750 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 112.833 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 112.917 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 113.000 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 113.083 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 113.167 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 113.250 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 113.333 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 113.417 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 113.500 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 113.583 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 113.667 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 113.750 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 113.833 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 113.917 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 114.000 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 114.083 | 0.00 | 0.00 | 0.008 | O | \| | \| | \| | \| | 0.04 |
| 114.167 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 114.250 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 114.333 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 114.417 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 114.500 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 114.583 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 114.667 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 114.750 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 114.833 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 114.917 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 115.000 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 115.083 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 115.167 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 115.250 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 115.333 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 115.417 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |
| 115.500 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | \| | 0.04 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 115.583 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 115.667 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 115.750 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 115.833 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 115.917 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 116.000 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 116.083 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 116.167 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 116.250 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 116.333 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 116.417 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 116.500 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 116.583 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 116.667 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 116.750 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 116.833 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.04 |
| 116.917 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.03 |
| 117.000 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.03 |
| 117.083 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.03 |
| 117.167 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.03 |
| 117.250 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.03 |
| 117.333 | 0.00 | 0.00 | 0.007 | O | \| | \| | \| | 0.03 |
| 117.417 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 117.500 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 117.583 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 117.667 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 117.750 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 117.833 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 117.917 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 118.000 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 118.083 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 118.167 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 118.250 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 118.333 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 118.417 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 118.500 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 118.583 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 118.667 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 118.750 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 118.833 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 118.917 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 119.000 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 119.083 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 119.167 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 119.250 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 119.333 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 119.417 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 119.500 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 119.583 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 119.667 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 119.750 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 119.833 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 119.917 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 120.000 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 120.083 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 120.167 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 120.250 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 120.333 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 120.417 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 120.500 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 120.583 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 120.667 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 120.750 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 120.833 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 120.917 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 121.000 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 121.083 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 121.167 | 0.00 | 0.00 | 0.006 | O | \| | \| | \| | 0.03 |
| 121.250 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 121.333 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 121.417 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 121.500 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 121.583 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 121.667 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 121.750 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 121.833 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 121.917 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 122.000 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 122.083 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 122.167 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 122.250 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 122.333 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 122.417 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 122.500 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 122.583 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 122.667 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 122.750 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 122.833 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 122.917 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 123.000 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 123.083 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 123.167 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 123.250 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 123.333 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 123.417 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 123.500 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 123.583 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 123.667 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 123.750 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 123.833 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 123.917 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 124.000 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 124.083 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 124.167 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 124.250 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 124.333 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 124.417 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 124.500 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 124.583 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.03 |
| 124.667 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 124.750 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 124.833 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 124.917 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 125.000 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 125.083 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 125.167 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 125.250 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 125.333 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 125.417 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 125.500 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 125.583 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 125.667 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 125.750 | 0.00 | 0.00 | 0.005 | O | \| | \| | \| | 0.02 |
| 125.833 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 125.917 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.000 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.083 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.167 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.250 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.333 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.417 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.500 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.583 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.667 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.750 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.833 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 126.917 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.000 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.083 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.167 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.250 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.333 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.417 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.500 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.583 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.667 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.750 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.833 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 127.917 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 128.000 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 128.083 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 128.167 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 128.250 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 128.333 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 128.417 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 128.500 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 128.583 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 128.667 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 128.750 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 128.833 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 128.917 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 129.000 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 129.083 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 129.167 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 129.250 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 129.333 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 129.417 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 129.500 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 129.583 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 129.667 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 129.750 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 129.833 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 129.917 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 130.000 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 130.083 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 130.167 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 130.250 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 130.333 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 130.417 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 130.500 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 130.583 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 130.667 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 130.750 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 130.833 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 130.917 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 131.000 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 131.083 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 131.167 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 131.250 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 131.333 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 131.417 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 131.500 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 131.583 | 0.00 | 0.00 | 0.004 | O | \| | \| | \| | 0.02 |
| 131.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 131.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 132.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 132.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 132.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 132.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 132.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 132.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 132.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 132.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 132.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 132.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 132.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |

| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 132.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 133.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 133.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 133.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 133.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 133.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 133.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 133.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 133.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 133.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 133.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 133.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 133.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 134.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 134.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 134.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 134.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 134.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 134.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 134.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 134.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 134.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 134.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 134.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 134.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 135.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 135.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 135.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 135.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 135.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 135.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 135.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 135.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 135.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 135.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 135.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 135.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 136.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 136.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 136.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 136.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.02 |
| 136.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 136.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 136.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 136.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 136.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 136.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 136.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 136.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 137.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 137.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |
| 137.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | 0.01 |

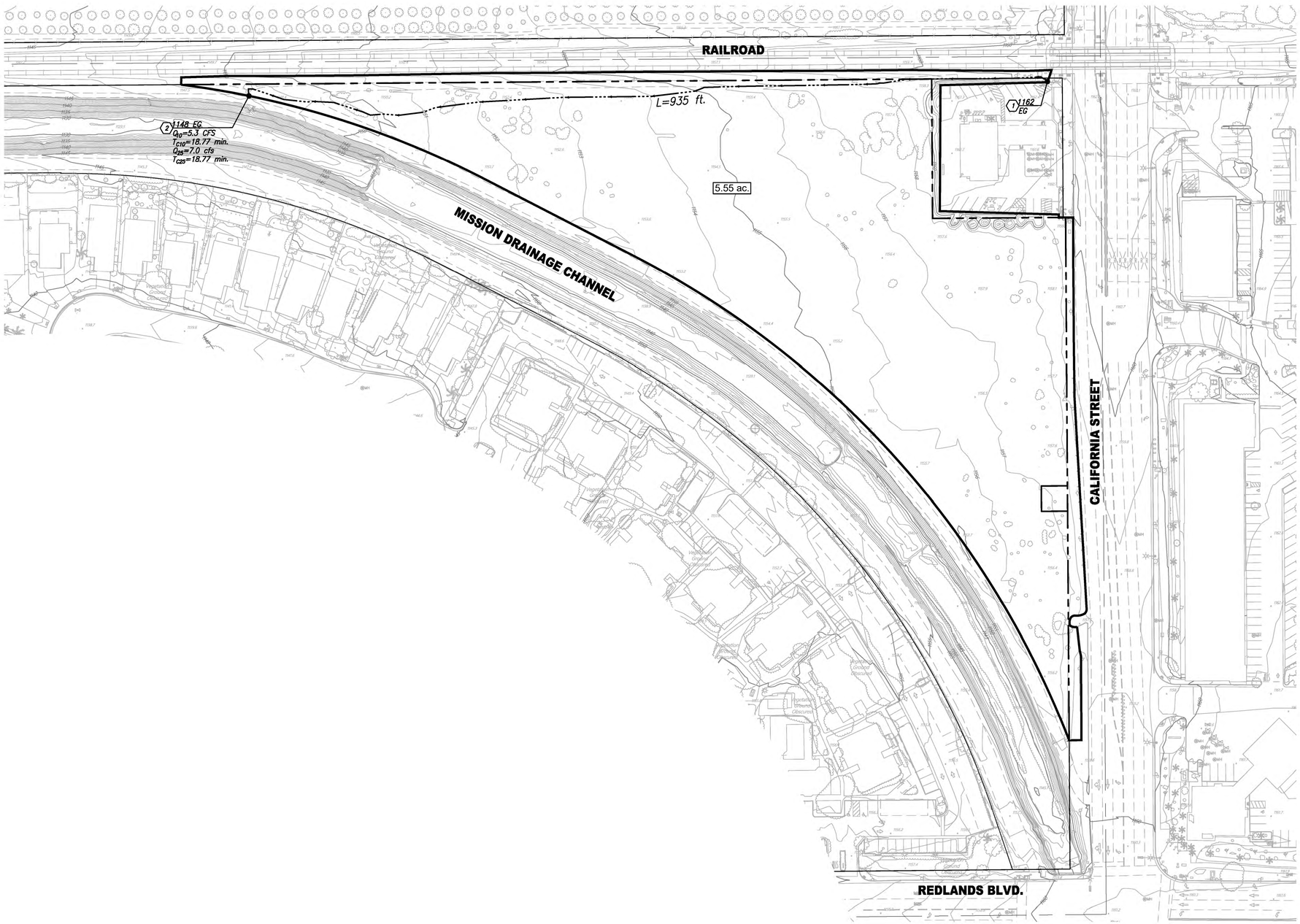
| | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|
| 137.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 137.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 137.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 137.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 137.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 137.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 137.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 137.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 137.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 138.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 138.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 138.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 138.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 138.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 138.417 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 138.500 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 138.583 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 138.667 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 138.750 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 138.833 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 138.917 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 139.000 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 139.083 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 139.167 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 139.250 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 139.333 | 0.00 | 0.00 | 0.003 | O | \| | \| | \| | \| | 0.01 |
| 139.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.750 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 139.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.250 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.333 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.750 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 140.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.250 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.333 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |

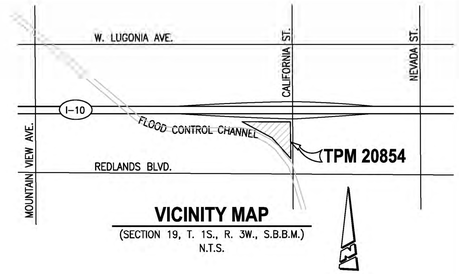
| | | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| 141.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.750 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 141.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 142.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 142.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 142.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 142.250 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 142.333 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 142.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 142.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 142.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 142.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 142.750 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 142.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 142.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 143.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 143.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 143.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 143.250 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 143.333 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 143.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 143.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 143.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 143.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 143.750 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 143.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 143.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 144.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 144.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 144.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 144.250 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 144.333 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 144.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 144.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 144.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 144.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 144.750 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 144.833 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 144.917 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 145.000 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 145.083 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 145.167 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 145.250 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 145.333 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 145.417 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 145.500 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 145.583 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |
| 145.667 | 0.00 | 0.00 | 0.002 | O | \| | \| | \| | \| | 0.01 |

**********HYDROGRAPH DATA**********

```
                Number of intervals =  1748
                Time interval =    5.0 (Min.)
                Maximum/Peak flow rate =        4.223 (CFS)
                Total volume =       1.740 (Ac.Ft)
        Status of hydrographs being held in storage
                    Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
        Peak (CFS)      0.000     0.000     0.000     0.000     0.000
        Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
****************************************************************************

----------------------------------------------------------------------
```




## VICINITY MAP

(SECTION 19, T. 1S., R. 3W., S.B.B.M.)
N.T.S.

## LEGEND

- MAJOR DRAINAGE BOUNDARY
- FLOW PATH
- XX.XX — DRAINAGE TRIBUTARY ACREAGE
- ELEVATION (10) — HYDROLOGY NODE AND ELEVATION

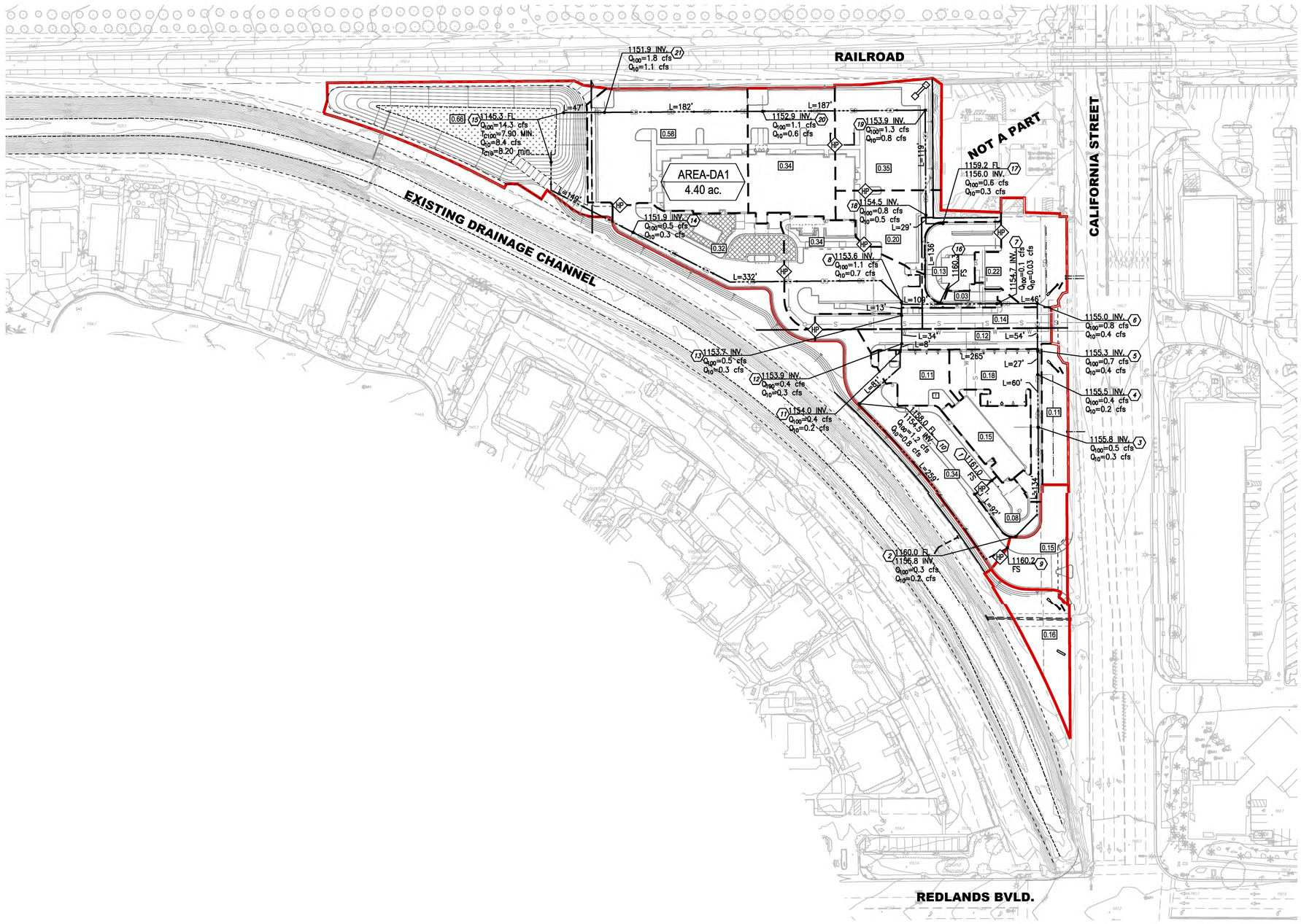
SCALE: 1"=60'

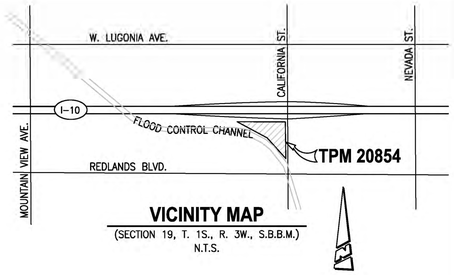
0 60 120 180


SP2 & Co.
A LAND DEVELOPMENT SERVICES COMPANY
451 W LAMBERT RD. STE 216
BREA, CA 92821
PHONE: (714) 490-1500
"SERVING THE DEVELOPMENT COMMUNITY SINCE 1985"


TENTATIVE PARCEL MAP 20854
PRELIMINARY HYDROLOGY KEY MAP
EXISTING CONDITION


Plotted: Aug 27, 2024 - 8:56am By: AlexanderJaramillo DWG: \\sp2-nas2\SP2-Data\SP2 Active\2023.08008 913 California St, Redlands - Chandresh Rawal\hydrology\Stormwater\Preliminary Drainage\Calcs\Prelim-Existing RM.dwg




## VICINITY MAP

(SECTION 19, T. 1S., R. 3W., S.B.B.M.)
N.T.S.

## LEGEND

- MAJOR DRAINAGE BOUNDARY
- MINOR DRAINAGE SUB-BOUNDARY
- FLOW PATH
- AREA-X / XX.XX — DRAINAGE AREA NUMBER AND ACREAGE
- XX.XX — MINOR DRAINAGE ACREAGE
- ELEVATION / ID — HYDROLOGY NODE AND ELEVATION

SCALE: 1"=60'

0 60 120 180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BREA, CA 92821
PHONE: (714) 490-1500
"SERVING THE DEVELOPMENT COMMUNITY SINCE 1985"


TENTATIVE PARCEL MAP 20854
PRELIMINARY HYDROLOGY KEY MAP
EXISTING CONDITION


Plotted: Aug 27, 2024 - 8:09am By: Alexander Jaramillo DWG: \\sp2-nas2\SP2-Data\SP2 Active\2023\23008 813 California St, Redlands - Chandreth Rawlley\Stormwater\Preliminary Drainage\Calcs\Prelim-Proposed RM Key Map.dwg