

Appendix 8

Hydrology Report

Hydrology Report

Cherry Outpost

Northwest corner of Cherry St and Bundy Canyon Rd

Wildomar, CA

April 30, 2024

This Hydraulic Study has been prepared by, and under the direction of, the undersigned, a duly Registered Civil Engineer in the State of California. Except as noted, the undersigned attests to the technical information contained herein, and has judged to be acceptable the qualifications of any technical specialists providing engineering data for this report, upon which findings, conclusions, and recommendations are based.

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Registered Civil Engineer No. C86581

Exp.: 03/31/25

Prepared for:

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Section 1 Introduction and Background

The client has retained Tait & Associates (Tait) to prepare the drainage design for the Cherry Outpost Improvement Plans. The project site is approximately 6.07 acres and it is located in the City of Wildomar, California. The project located on the northwest corner of Cherry St and Bundy Canyon Rd, adjacent to the I-15 northbound onramp in Wildomar. The proposed project Vicinity Map is provided in Figure 1 below. The Hydrology & Hydraulics Report studies the proposed condition drainage system and patterns. This study follows the requirements of the Riverside County Flood /Control and Water Conservation District (RCFCWD), the Riverside County Hydrology Manual (RCHM), dated 1978 and it was prepared for a 100-year storm event for the proposed condition. The following sections include the general project characteristics, the drainage design, criteria and methodology.

1.1 Project Description

The Cherry Outpost development is proposed for commercial uses. It includes 107-key, four-story hotel, single building pad, a split building pad, which includes a quick serve restaurant, a car wash pad, large fueling canopy, RV fueling canopy, parking areas and driveways. The proposed site includes landscaping, concrete pavement, asphalt pavement, and underground utilities that will service the proposed building. Project grading will occur on approximately 5.95± acres which comprises approximately 99% of the total site area.

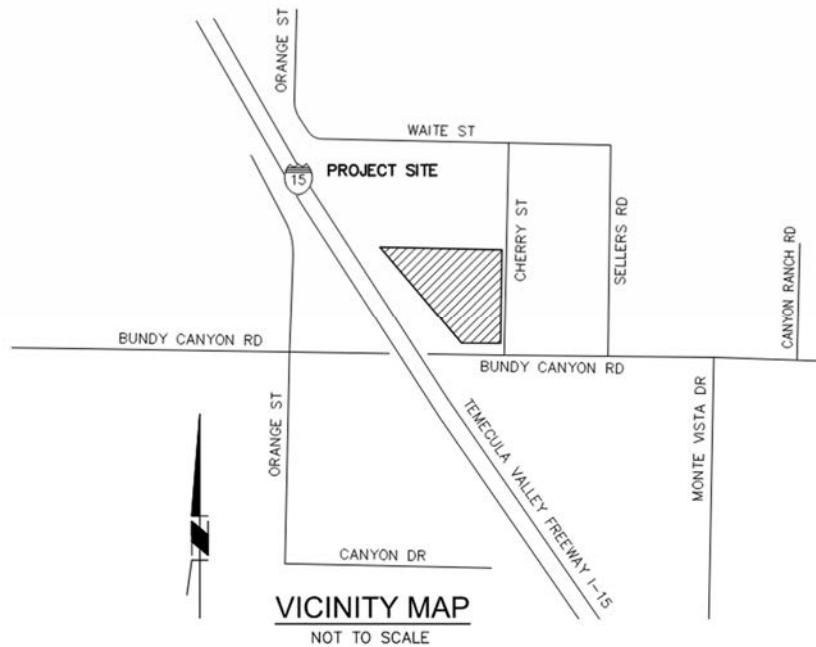


Figure 1 – Vicinity Map (Not To Scale)

Section 2 Hydrology Design Criteria, Methodology, and Analysis

2.1 Hydrology Design Criteria and Methodology

The RCHM uses the Rational Method to determine the runoff flow for watershed areas that are less than 300 to 500 acres in size. The Synthetic Unit Hydrograph is used for watershed areas larger than 300 to 500 acres. The rational method is based on the equation $Q = C \times I \times A$

where:

Q = peak discharge (cfs)

C = runoff coefficient representing the ratio of runoff to rainfall

I = the time-averaged rainfall intensity in inches per hour corresponding to the time of concentration (in/hr)

A = drainage area (acres).

The runoff coefficient is determined from the soil characteristics and the land use types. The time of concentration is the time it takes for the entire watershed to contribute runoff to the concentration point, and it is determined based on the longest flow path. The total drainage area tributary to the project outfall is 6.07 acres which is less than 300 thus only the Rational Method analysis was required. The precipitation was obtained from the NOAA Atlas 14 and Precipitation intensity-duration curves are included in Appendix A. The rational method was prepared using the Advance Engineering Software (AES) RATSCX software which is approved by Riverside County for the Rational Method.

2.2 Hydrology Analysis

The following section describes the existing and proposed drainage patterns and any required mitigation measures proposed for the proposed project.

2.2.1 Soil Conditions

Per the USDA Natural Resources Conservation Service Soil Survey (USDA NRCS), published in 2006, the project site is located within the hydrology soil group of A and C. Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. Group C. Soils having a slow infiltration rate (high runoff potential) when thoroughly wet. The project site location is shown on the USDA Soil Resource map, included in Appendix B.

2.2.2 Existing Condition Hydrology Analysis

The project site is located within Zone 3 of the RCFCD drainage system. The subject of this report, Cherry Outpost, is located on the northwest corner of Cherry St and Bundy Canyon Rd,

adjacent to the I-15 northbound onramp in Wildomar. The site is an approximately 6.07 acre parcel.

The site is an abandoned, now undeveloped parcel. A single-family residential structure (with outbuildings) and an orchard existed on the site until at least 2009. The existing site flows by sheet flow from north to south, and is bounded by the improved I-15 northbound onramp to the west, low-density residences to the north, and Cherry St to the east, and Bundy Canyon Rd to the south. There is a large existing culvert to the south of the site (but north of Bundy Canyon Rd, which drains to Lake Elsinore.

Existing Condition Hydrology calculations from this report are also Provided in Appendix C herein.

2.2.3 Proposed Condition Hydrology Analysis

The proposed project will maintain the existing drainage patterns, draining to the southeast corner of the site. Project grading will occur on approximately $5.95 \pm$ acres which comprises approximately 99% of the total site area. The project will significantly increase the impervious area of the site. The post-development surface conditions are as follows:

Proposed Site (Post development)

Surface type	Runoff Index ³	Area [sf]	Area [ac]
Impervious		189,050	4.34
Soil-A	32	34,412	0.79
Soil-C	69	35,719	0.82
Total		259,182	5.95
	Coefficient of Runoff ²	0.76	
	Imperviousness	73%	

Stormwater runoff from the project site is directed towards bioretention areas for water quality treatment requirements. Stormwater is directed by both sheet flow, and by drainage inlets. The proposed condition flows from these management areas were determined for the 100-year 24-Hr storm event using the Rational Method. Point precipitation depths and intensities were determined using the NOAA Atlas 14.

2.2.4 Basin Design Analysis

The project proposes a surface detention basin to detain runoff increase requirements set forth by Riverside County Flood Control & Water Conservation District, the proposed detention basin has been designed with flow controls to mimic existing 100-year 24-Hr storm flow.

The detention basin will serve a dual purpose of detention and treatment. Stormwater will be allowed to infiltrate out of the basin over time. Proposed Detention basin routing calculations have been provided in Appendix F.

Section 3 Summary of Results and Conclusions

The hydrology calculations demonstrate that the proposed site is designed to meet hydraulic requirements. The existing development will be improved upon with the addition of pad buildings, and associated improvements. The site improvements include the construction of a storm drain system designed to convey the 100-year storm event. The proposed project includes stormwater quality treatment in the form of bioretention areas and surface detention basin.

Table 1: Hydrograph Summary

Condition	100-year peak flow (cfs)
Existing	8.01
Proposed	13.15
Proposed (Mitigated)	5.20

Based on the results of this study, the project mitigation measures proposed will prevent an increase in runoff. Therefore, the proposed project improvements will not have an adverse effect on the downstream storm drain system.

APPENDIX

Appendix A – NOAA Precipitation

**NOAA Atlas 14, Volume 6, Version 2****Location name:** Wildomar, California, USA***Latitude:** 33.6281°, **Longitude:** -117.2719°**Elevation:** m/ft**

* source: ESRI Maps

** source: USGS

**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

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PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour)¹										
Duration	Average recurrence interval (years)									
	1	2	5		25	50		200	500	1000
5-min	0.996 (0.840-1.20)	1.34 (1.13-1.63)	1.84 (1.54-2.22)		2.81 (2.24-3.55)	3.26 (2.56-4.22)		4.25 (3.13-5.80)	4.94 (3.50-7.06)	5.51 (3.76-8.15)
15-min	0.576 (0.484-0.692)	0.780 (0.652-0.940)	1.06 (0.884-1.28)		1.62 (1.30-2.05)	1.89 (1.48-2.44)		2.45 (1.81-3.35)	2.86 (2.02-4.08)	3.18 (2.17-4.71)
30-min	0.450 (0.378-0.542)	0.610 (0.512-0.736)	0.830 (0.692-1.00)		1.27 (1.02-1.61)	1.48 (1.15-1.91)		1.92 (1.42-2.62)	2.24 (1.58-3.20)	2.49 (1.70-3.69)
2-hr	0.262 (0.220-0.316)	0.344 (0.288-0.414)	0.455 (0.380-0.550)		0.678 (0.542-0.858)	0.782 (0.612-1.01)		1.00 (0.742-1.37)	1.16 (0.822-1.66)	1.29 (0.878-1.91)
3-hr	0.215 (0.180-0.259)	0.280 (0.234-0.337)	0.367 (0.306-0.444)		0.542 (0.434-0.686)	0.624 (0.488-0.806)		0.796 (0.589-1.09)	0.918 (0.650-1.31)	1.01 (0.692-1.50)
6-hr	0.153 (0.129-0.185)	0.199 (0.167-0.240)	0.261 (0.218-0.315)		0.382 (0.305-0.483)	0.438 (0.342-0.565)		0.554 (0.410-0.757)	0.636 (0.450-0.908)	0.700 (0.478-1.04)
12-hr	0.099 (0.083-0.119)	0.132 (0.111-0.160)	0.176 (0.147-0.213)		0.261 (0.208-0.329)	0.298 (0.233-0.385)		0.375 (0.277-0.512)	0.427 (0.302-0.610)	0.468 (0.319-0.692)
2-day	0.040 (0.035-0.046)	0.057 (0.050-0.066)	0.079 (0.070-0.092)		0.122 (0.104-0.147)	0.141 (0.117-0.174)		0.180 (0.142-0.233)	0.206 (0.156-0.278)	0.226 (0.166-0.315)
3-day	0.029 (0.025-0.033)	0.042 (0.037-0.049)	0.059 (0.052-0.069)		0.093 (0.079-0.112)	0.108 (0.090-0.133)		0.139 (0.110-0.180)	0.161 (0.122-0.216)	0.177 (0.130-0.247)
4-day	0.023 (0.021-0.027)	0.034 (0.030-0.040)	0.049 (0.043-0.057)		0.077 (0.065-0.093)	0.090 (0.075-0.111)		0.117 (0.092-0.151)	0.136 (0.103-0.183)	0.150 (0.110-0.209)
7-day	0.015 (0.013-0.017)	0.022 (0.020-0.026)	0.032 (0.028-0.037)		0.051 (0.043-0.062)	0.060 (0.050-0.074)		0.079 (0.063-0.103)	0.093 (0.070-0.125)	0.104 (0.076-0.144)
10-day	0.011 (0.010-0.013)	0.016 (0.014-0.019)	0.024 (0.021-0.027)		0.038 (0.033-0.046)	0.045 (0.038-0.056)		0.060 (0.048-0.078)	0.071 (0.054-0.096)	0.080 (0.059-0.111)
20-day	0.006 (0.006-0.007)	0.010 (0.008-0.011)	0.014 (0.012-0.016)		0.023 (0.020-0.028)	0.028 (0.023-0.034)		0.038 (0.030-0.049)	0.045 (0.034-0.061)	0.051 (0.038-0.071)
30-day	0.005 (0.004-0.006)	0.008 (0.007-0.009)	0.011 (0.010-0.013)		0.019 (0.016-0.022)	0.022 (0.018-0.027)		0.031 (0.024-0.040)	0.037 (0.028-0.050)	0.042 (0.031-0.058)
45-day	0.004 (0.003-0.004)	0.006 (0.005-0.007)	0.008 (0.007-0.010)		0.014 (0.012-0.017)	0.017 (0.014-0.021)		0.024 (0.019-0.031)	0.029 (0.022-0.039)	0.033 (0.024-0.046)
60-day	0.003 (0.003-0.004)	0.005 (0.004-0.006)	0.007 (0.006-0.008)		0.012 (0.010-0.015)	0.015 (0.012-0.018)		0.020 (0.016-0.026)	0.025 (0.019-0.033)	0.028 (0.021-0.039)

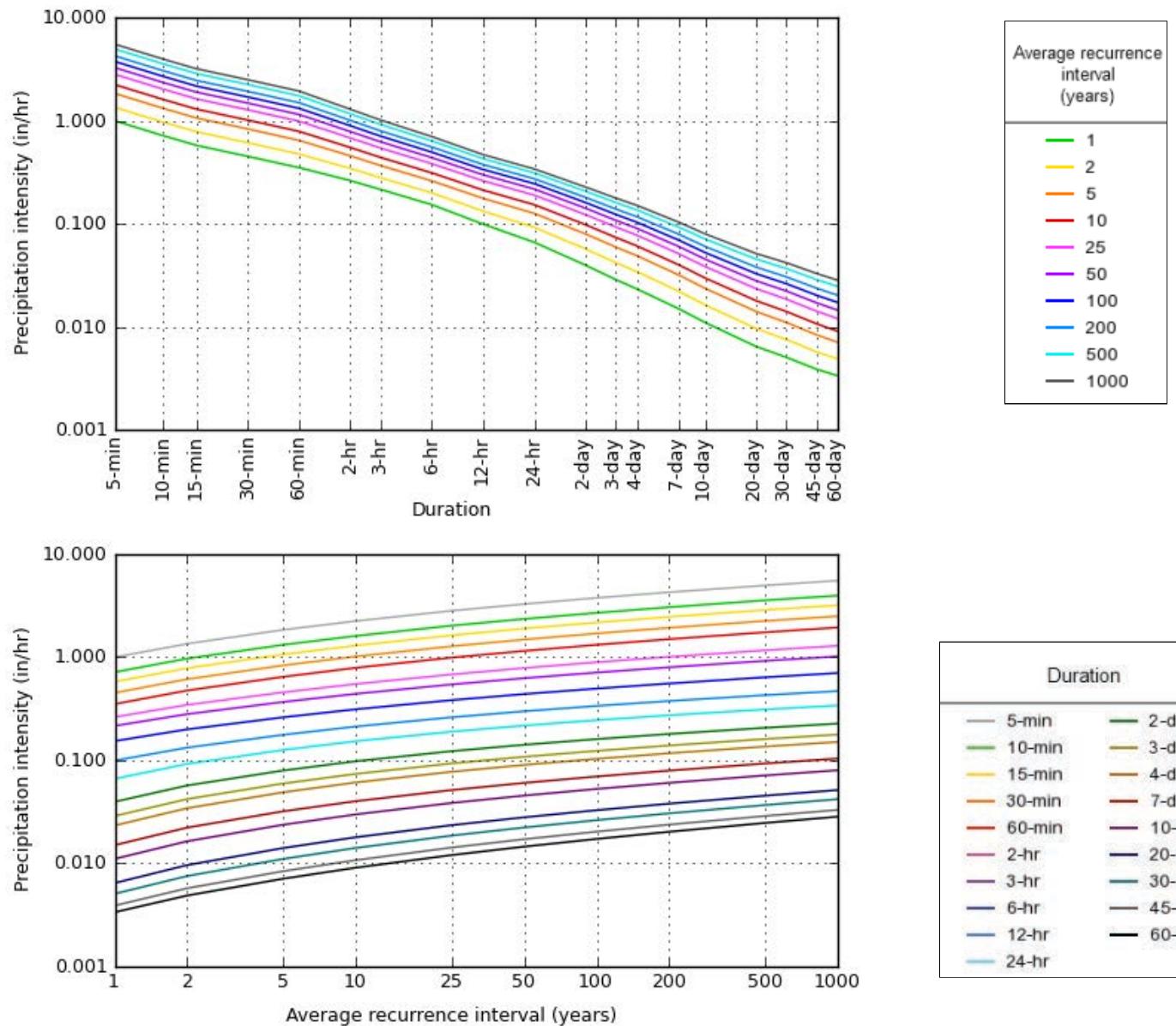
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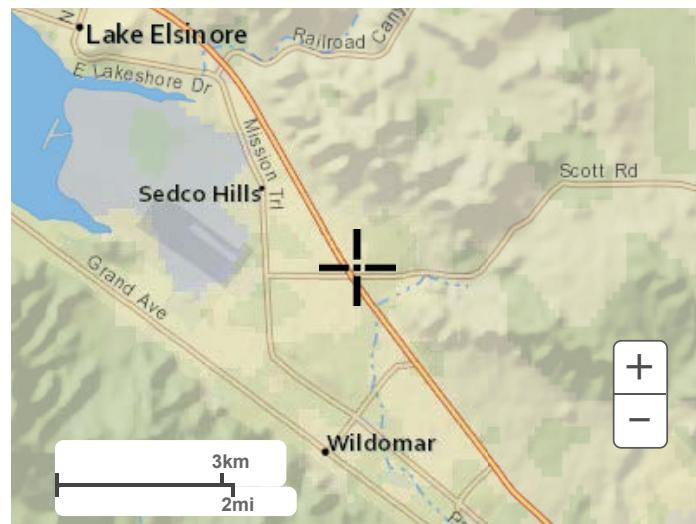
PDS-based intensity-duration-frequency (IDF) curves
Latitude: 33.6281°, Longitude: -117.2719°



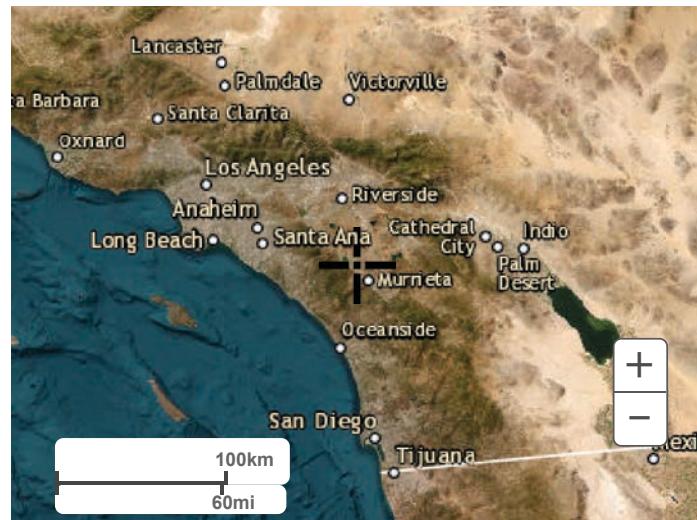
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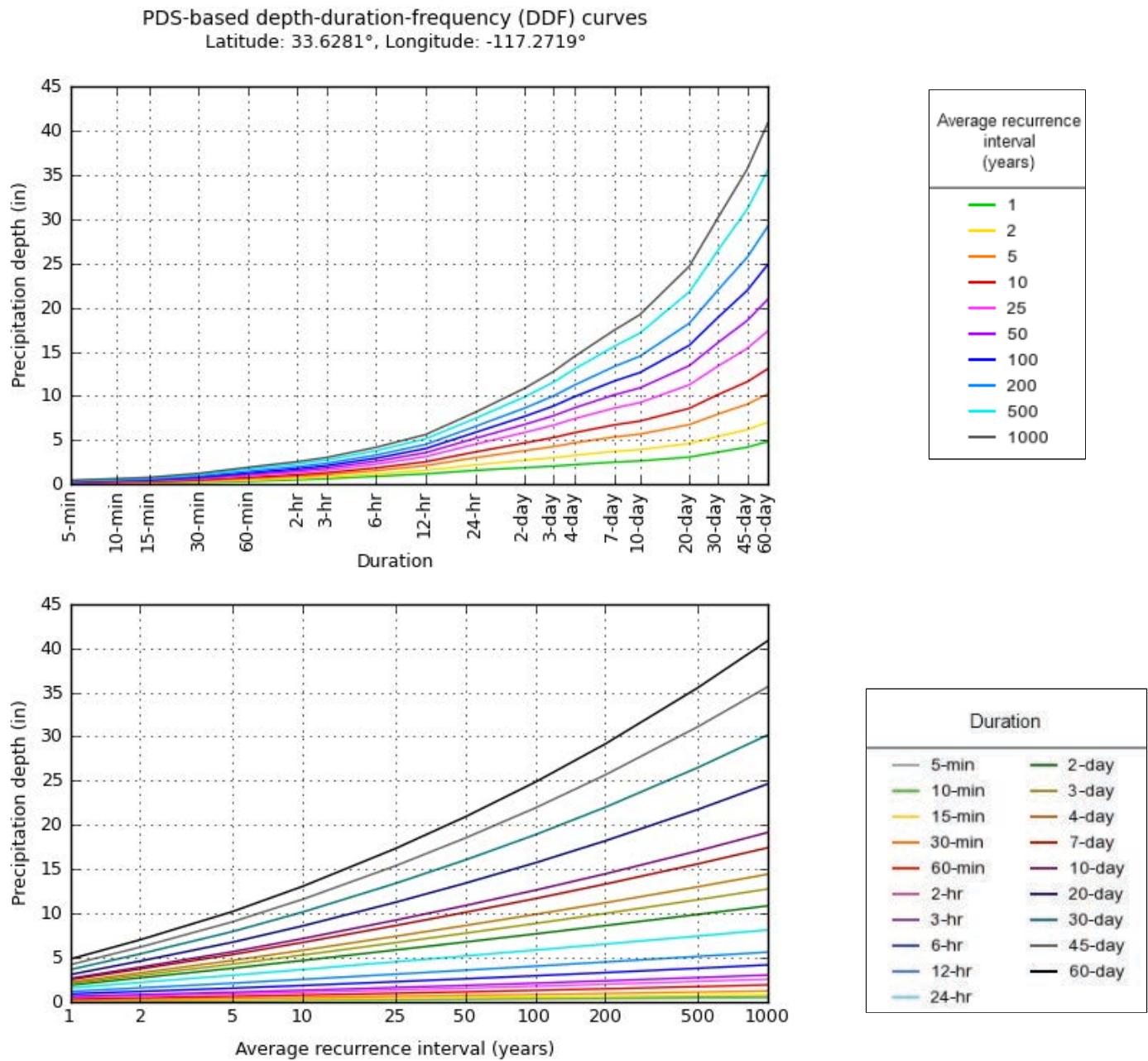
NOAA, National Weather Service, Silver Spring, Maryland

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PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)¹									
Duration	Average recurrence interval (years)						200	500	1000
	1	2	5	10	25	50			
5-min	0.083 (0.070-0.100)	0.112 (0.094-0.136)	0.153 (0.128-0.185)	0.186 (0.154-0.227)	0.234 (0.187-0.296)	0.272 (0.213-0.352)			
10-min	0.119 (0.100-0.143)	0.161 (0.135-0.194)	0.219 (0.183-0.265)	0.267 (0.221-0.326)	0.336 (0.268-0.424)	0.390 (0.305-0.504)	0.354 (0.261-0.483)	0.412 (0.292-0.588)	0.459 (0.313-0.679)
15-min	0.144 (0.121-0.173)	0.195 (0.163-0.235)	0.265 (0.221-0.320)	0.323 (0.268-0.394)	0.406 (0.324-0.513)	0.472 (0.369-0.609)	0.507 (0.375-0.693)	0.591 (0.418-0.843)	0.657 (0.448-0.973)
30-min	0.225 (0.189-0.271)	0.305 (0.256-0.368)	0.415 (0.346-0.501)	0.506 (0.419-0.618)	0.636 (0.508-0.804)	0.739 (0.577-0.955)	0.613 (0.453-0.838)	0.714 (0.505-1.02)	0.795 (0.542-1.18)
60-min	0.350 (0.293-0.421)	0.474 (0.397-0.572)	0.643 (0.537-0.778)	0.786 (0.650-0.958)	0.987 (0.788-1.25)	1.15 (0.896-1.48)	1.49 (1.10-2.04)	1.74 (1.23-2.48)	1.93 (1.32-2.86)
2-hr	0.524 (0.440-0.631)	0.688 (0.576-0.829)	0.910 (0.760-1.10)	1.10 (0.907-1.34)	1.36 (1.09-1.72)	1.57 (1.22-2.02)	2.01 (1.49-2.75)	2.32 (1.65-3.32)	2.57 (1.76-3.81)
3-hr	0.646 (0.542-0.778)	0.840 (0.703-1.01)	1.10 (0.920-1.33)	1.32 (1.09-1.61)	1.63 (1.30-2.06)	1.87 (1.46-2.42)	2.39 (1.77-3.27)	2.76 (1.95-3.94)	3.05 (2.08-4.51)
6-hr	0.918 (0.770-1.11)	1.19 (0.999-1.44)	1.56 (1.30-1.89)	1.87 (1.54-2.28)	2.29 (1.83-2.89)	2.62 (2.05-3.39)	3.32 (2.45-4.54)	3.81 (2.70-5.44)	4.19 (2.86-6.21)
12-hr	1.19 (1.00-1.44)	1.60 (1.34-1.92)	2.12 (1.77-2.57)	2.55 (2.11-3.12)	3.14 (2.51-3.97)	3.59 (2.81-4.64)	4.52 (3.34-6.17)	5.15 (3.64-7.35)	5.64 (3.85-8.34)
2-day	1.90 (1.68-2.19)	2.73 (2.41-3.16)	3.81 (3.36-4.42)	4.69 (4.10-5.48)	5.87 (4.97-7.08)	6.78 (5.62-8.34)	8.63 (6.81-11.2)	9.90 (7.50-13.3)	10.9 (7.97-15.1)
3-day	2.07 (1.83-2.39)	3.02 (2.67-3.50)	4.28 (3.77-4.96)	5.30 (4.63-6.19)	6.70 (5.67-8.07)	7.77 (6.45-9.56)	10.0 (7.89-12.9)	11.6 (8.76-15.6)	12.8 (9.36-17.8)
4-day	2.23 (1.97-2.58)	3.29 (2.90-3.80)	4.69 (4.13-5.44)	5.84 (5.10-6.82)	7.42 (6.28-8.94)	8.64 (7.17-10.6)	11.2 (8.84-14.5)	13.0 (9.86-17.5)	14.4 (10.6-20.1)
7-day	2.52 (2.23-2.91)	3.73 (3.30-4.31)	5.37 (4.73-6.22)	6.73 (5.88-7.86)	8.63 (7.30-10.4)	10.1 (8.40-12.5)	13.3 (10.5-17.2)	15.6 (11.8-21.0)	17.4 (12.8-24.3)
10-day	2.65 (2.34-3.06)	3.93 (3.47-4.55)	5.68 (5.00-6.59)	7.16 (6.25-8.36)	9.24 (7.82-11.1)	10.9 (9.04-13.4)	14.5 (11.4-18.7)	17.1 (12.9-23.0)	19.2 (14.1-26.7)
20-day	3.09 (2.73-3.57)	4.62 (4.08-5.34)	6.76 (5.95-7.83)	8.60 (7.51-10.0)	11.3 (9.53-13.6)	13.4 (11.1-16.5)	18.2 (14.4-23.6)	21.8 (16.5-29.3)	24.7 (18.1-34.3)
30-day	3.65 (3.23-4.22)	5.43 (4.79-6.28)	7.96 (7.01-9.22)	10.2 (8.88-11.9)	13.4 (11.3-16.1)	16.0 (13.3-19.7)	22.0 (17.4-28.5)	26.5 (20.1-35.7)	30.2 (22.1-42.0)
45-day	4.21 (3.72-4.86)	6.20 (5.47-7.16)	9.07 (7.98-10.5)	11.6 (10.1-13.6)	15.4 (13.0-18.5)	18.5 (15.4-22.8)	25.7 (20.2-33.2)	31.1 (23.6-41.9)	35.6 (26.1-49.6)
60-day	4.84 (4.28-5.59)	7.03 (6.20-8.12)	10.2 (9.00-11.8)	13.1 (11.4-15.3)	17.3 (14.7-20.9)	20.9 (17.4-25.7)	29.2 (23.0-37.7)	35.5 (26.9-47.8)	40.8 (29.9-56.8)

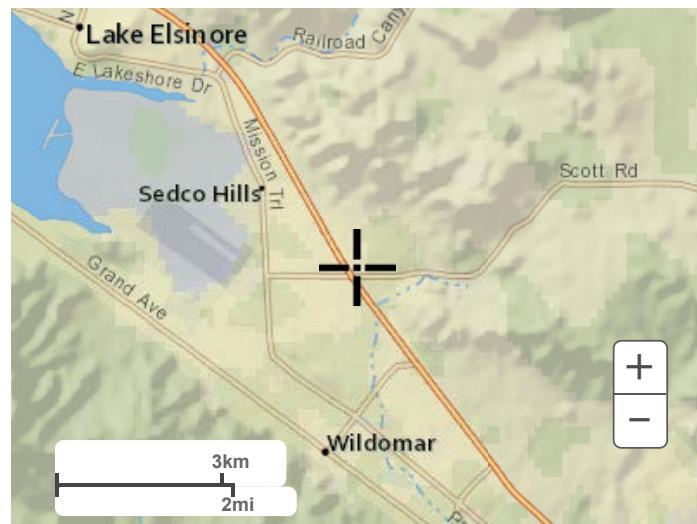
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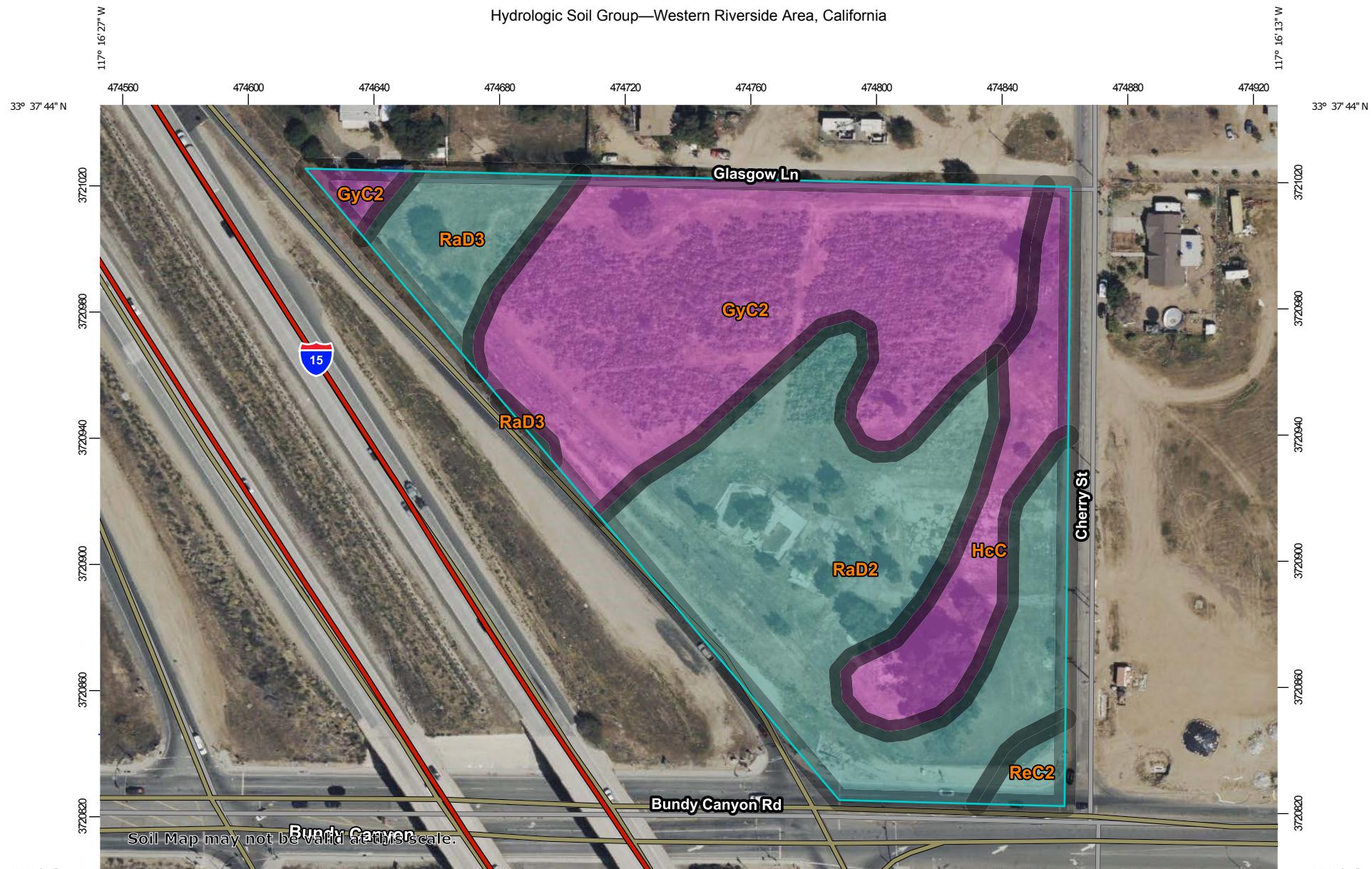
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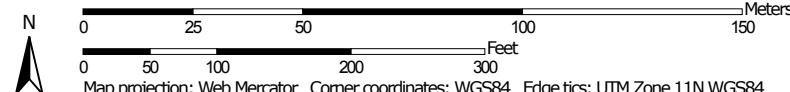
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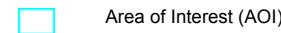
Appendix B – Soils Maps

Hydrologic Soil Group—Western Riverside Area, California



Map Scale: 1:1,720 if printed on A landscape (11" x 8.5") sheet.



MAP LEGEND**Area of Interest (AOI)****Soils****Soil Rating Polygons**

	A
	A/D
	B
	B/D
	C
	C/D
	D
	Not rated or not available

Soil Rating Lines

	A
	A/D
	B
	B/D
	C
	C/D
	D
	Not rated or not available

Soil Rating Points

	A
	A/D
	B
	B/D

C**C/D****D****Not rated or not available****Water Features**

Streams and Canals

Transportation

Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:15,800.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Western Riverside Area, California

Survey Area Data: Version 16, Aug 30, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Mar 14, 2022—Mar 17, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.



Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
GyC2	Greenfield sandy loam, 2 to 8 percent slopes, eroded	A	3.2	41.3%
HcC	Hanford coarse sandy loam, 2 to 8 percent slopes	A	0.9	11.7%
RaD2	Ramona sandy loam, 8 to 15 percent slopes, eroded	C	3.0	38.6%
RaD3	Ramona sandy loam, 8 to 15 percent slopes, severely eroded	C	0.5	6.9%
ReC2	Ramona very fine sandy loam, 0 to 8 percent slopes, eroded	C	0.1	1.6%
Totals for Area of Interest			7.7	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

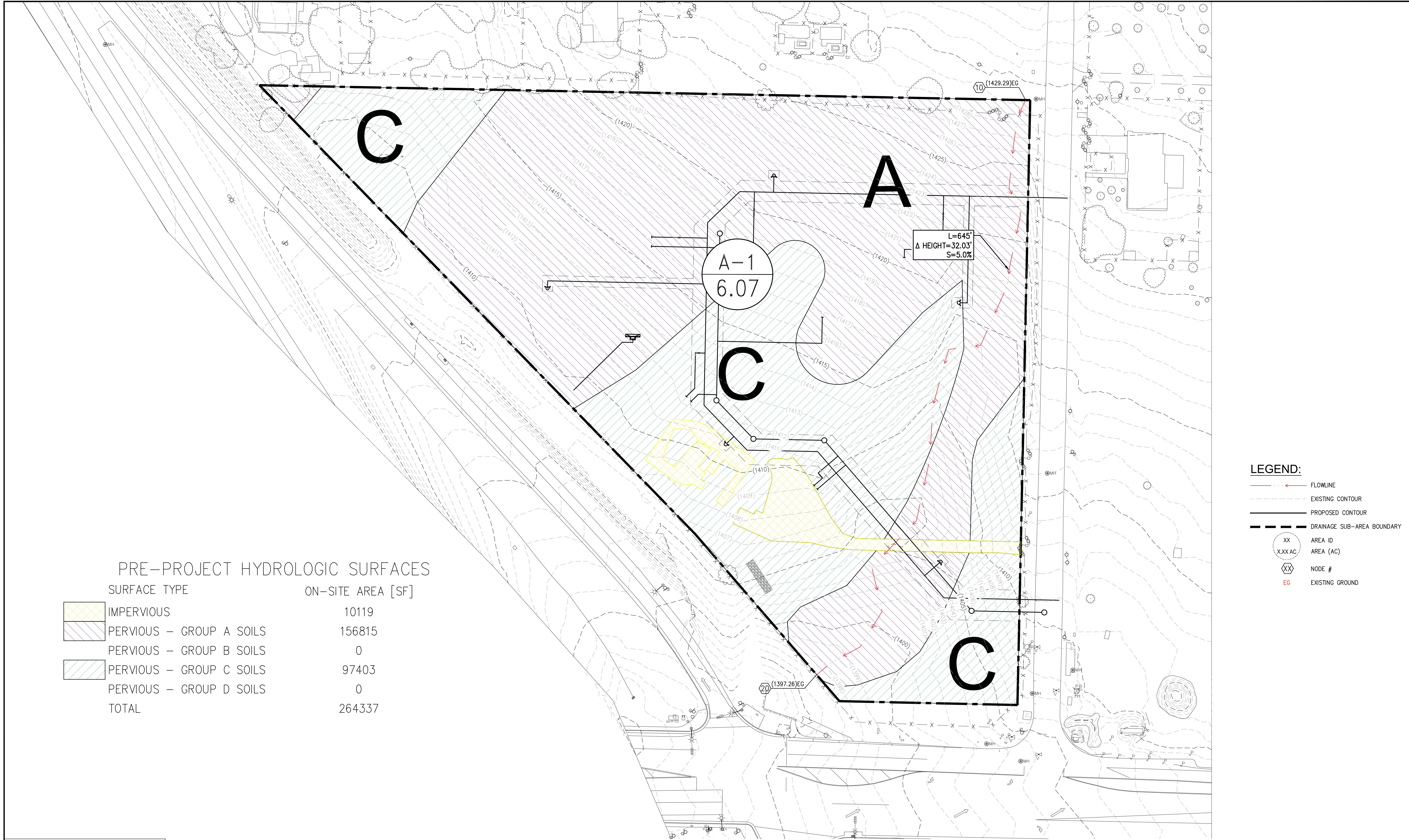
Rating Options

Aggregation Method: Dominant Condition

Component Percent Cutoff: None Specified

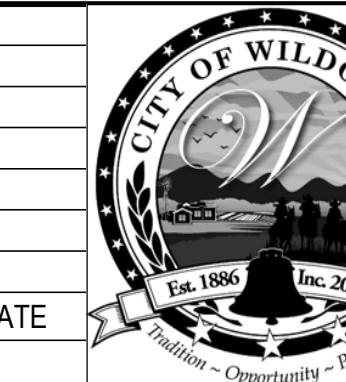
Tie-break Rule: Higher

Appendix C – Existing Hydrology Calculations



NOTE:
WORK CONTAINED WITHIN THESE PLANS SHALL NOT COMMENCE UNTIL AN ENCROACHMENT PERMIT AND/OR A GRADING PERMIT HAS BEEN ISSUED.
The private engineer signing these plans is responsible for assuring the accuracy and acceptability of the design hereon. In the event of discrepancies arising after city acceptance or during construction, the private engineer shall be responsible for determining an acceptable solution and revising the plans for acceptance by the city.

MARK	BY	DATE	APPR.	DATE
REVISIONS			CITY	
ENGINEER				



CITY OF WILDOMAR
ACCEPTED BY:
Date:
Daniel A. York, Director of Public Works/
City Engineer, PE 43212
ACCEPTANCE AS TO CONFORMANCE
WITH APPLICABLE CITY STANDARDS AND
PRACTICES



701 North Parkcenter Drive
Santa Ana, CA 92705
p: 714.540.8200
www.tait.com
Engineering Environmental Building Land
Orange County Sacramento Riverside Denver Boise Dallas Atlanta
San Luis Obispo

BENCHMARK:
Elevation = _____
Datum = _____
BENCHMARK # _____
THIS SURVEY WAS PERFORMED ON (date) BY (surveyor)
L.S. (number), EXP. (date)

(PP, CUP, PM, TM, etc.) (city project number)
CITY OF WILDOMAR
EXISTING CONDITIONS HYDROLOGY MAP
CHERRY OUTPOST IN THE
CITY OF WILDOMAR, RIVERSIDE COUNTY

SHEET No. 1
OF 1 SHTS

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM BASED ON
RIVERSIDE COUNTY FLOOD CONTROL & WATER CONSERVATION DISTRICT
(RCFC&WCD) 1978 HYDROLOGY MANUAL
(c) Copyright 1982-2016 Advanced Engineering Software (aes)
(Rational Tabling Version 23.0)
Release Date: 07/01/2016 License ID 1334

Analysis prepared by:

TAIT & ASSOCIATES INC.
701 N. PARKCENTER DRIVE
SANTA ANA, CALIFORNIA 92705

DESCRIPTION OF STUDY *****
* SP8997 - WILDOMAR CHERRY OUTPOST *
* EXISTING CONDITION RATIONAL METHOD *
* 100-YEAR STORM EVENT *

FILE NAME: WIL100EX.DAT
TIME/DATE OF STUDY: 10:25 03/21/2023

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
10-YEAR STORM 10-MINUTE INTENSITY(INCH/HOUR) = 1.600
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.786
100-YEAR STORM 10-MINUTE INTENSITY(INCH/HOUR) = 2.680
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.310
SLOPE OF 10-YEAR INTENSITY-DURATION CURVE = 0.3967061
SLOPE OF 100-YEAR INTENSITY-DURATION CURVE = 0.3994898
COMPUTED RAINFALL INTENSITY DATA:

STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.310
SLOPE OF INTENSITY DURATION CURVE = 0.3995

RCFC&WCD HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: COMPUTE CONFLUENCE VALUES ACCORDING TO RCFC&WCD HYDROLOGY MANUAL
AND IGNORE OTHER CONFLUENCE COMBINATIONS FOR DOWNSTREAM ANALYSES

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL
HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING
WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (n)
==== ====== ====== ====== ====== ====== ====== ======

1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

FLOW PROCESS FROM NODE 10.00 TO NODE 20.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS: UNDEVELOPED WITH POOR COVER
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 645.00
UPSTREAM ELEVATION(FEET) = 1429.29
DOWNSTREAM ELEVATION(FEET) = 1397.26
ELEVATION DIFFERENCE(FEET) = 32.03
TC = 0.533*[(645.00**3)/(- 32.03)]**.2 = 12.913
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.420
UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .4146
SOIL CLASSIFICATION IS "A"
SUBAREA RUNOFF(CFS) = 3.61
TOTAL AREA(ACRES) = 3.60 TOTAL RUNOFF(CFS) = 3.61

FLOW PROCESS FROM NODE 20.00 TO NODE 20.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.420
UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .7214
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 2.24 SUBAREA RUNOFF(CFS) = 3.91
TOTAL AREA(ACRES) = 5.8 TOTAL RUNOFF(CFS) = 7.52
TC(MIN.) = 12.91

FLOW PROCESS FROM NODE 20.00 TO NODE 20.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.420
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8515
SOIL CLASSIFICATION IS "A"
SUBAREA AREA(ACRES) = 0.02 SUBAREA RUNOFF(CFS) = 0.04
TOTAL AREA(ACRES) = 5.9 TOTAL RUNOFF(CFS) = 7.56
TC(MIN.) = 12.91

FLOW PROCESS FROM NODE 20.00 TO NODE 20.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

===== 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.420

COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8821

SOIL CLASSIFICATION IS "C"

SUBAREA AREA(ACRES) = 0.21 SUBAREA RUNOFF(CFS) = 0.45

TOTAL AREA(ACRES) = 6.1 TOTAL RUNOFF(CFS) = 8.01

TC(MIN.) = 12.91

===== END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 6.1 TC(MIN.) = 12.91

PEAK FLOW RATE(CFS) = 8.01

===== END OF RATIONAL METHOD ANALYSIS

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F L O O D R O U T I N G A N A L Y S I S
U S I N G C O U N T Y H Y D R O L O G Y M A N U A L O F O R A N G E (1 9 8 6)

(c) Copyright 1989-2016 Advanced Engineering Software (aes)
Ver. 23.0 Release Date: 07/01/2016 License ID 1334

Analysis prepared by:

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***** DESCRIPTION OF STUDY *****
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* CHERRY OUTPOST *
* 100 YR - EXISTING CONDITION *
* SMALL AREA UNIT HYDROGRAPH *

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*****
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FILE NAME: 100YREXH.DAT
TIME/DATE OF STUDY: 11:46 03/24/2023

The Small Area Unit Hydrograph Procedures in Section J of the Hydrology Manual provides estimates of runoff hydrograph and runoff volume for watersheds whose time of concentration is less than 25 minutes. The PROGRAM User should check the applicability of using the small area unit hydrograph procedures, and follow the guidelines in Sections J and K.5 in complex watershed modeling.

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FLOW PROCESS FROM NODE 10.00 TO NODE 20.00 IS CODE = 1.2

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>>>SUBAREA RUNOFF (SMALL AREA UNIT-HYDROGRAPH ANALYSIS) <<<

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(SMALL AREA UNIT-HYDROGRAPH ADDED TO STREAM #1)

RATIONAL METHOD CALIBRATION COEFFICIENT = 0.90
TOTAL CATCHMENT AREA(ACRES) = 6.07
SOIL-LOSS RATE, Fm,(INCH/HR) = 0.385
LOW LOSS FRACTION = 0.445
TIME OF CONCENTRATION(MIN.) = 12.91
SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA
USER SPECIFIED RAINFALL VALUES ARE USED:
RETURN FREQUENCY(YEARS) = 100
5-MINUTE POINT RAINFALL VALUE(INCHES) = 0.31

30-MINUTE POINT RAINFALL VALUE(INCHES) = 0.85
1-HOUR POINT RAINFALL VALUE(INCHES) = 1.31
3-HOUR POINT RAINFALL VALUE(INCHES) = 2.13
6-HOUR POINT RAINFALL VALUE(INCHES) = 2.96
24-HOUR POINT RAINFALL VALUE(INCHES) = 5.87

TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 1.56
TOTAL CATCHMENT SOIL-LOSS VOLUME(ACRE-FEET) = 1.41

▲

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2 4 - H O U R S T O R M
R U N O F F H Y D R O G R A P H

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HYDROGRAPH IN ONE-MINUTE UNIT INTERVALS(CFS)

(Notes: Time indicated is at END of Each Unit Intervals.
Peak 5-minute rainfall intensity is modeled as
a constant value for entire 5-minute period.)

TIME(HRS)	VOLUME(AF)	Q(CFS)	0.	2.8	5.7	8.5	11.3
0.017	0.0000	0.00	Q
0.033	0.0000	0.00	Q
0.050	0.0000	0.00	Q
0.067	0.0000	0.00	Q
0.083	0.0000	0.00	Q
0.100	0.0000	0.02	Q
0.117	0.0001	0.05	Q
0.133	0.0002	0.08	Q
0.150	0.0004	0.11	Q
0.167	0.0006	0.14	Q
0.183	0.0008	0.17	Q
0.200	0.0011	0.19	Q
0.217	0.0014	0.22	Q
0.233	0.0017	0.25	Q
0.250	0.0021	0.28	Q
0.267	0.0025	0.31	VQ
0.283	0.0030	0.34	VQ
0.300	0.0035	0.36	VQ
0.317	0.0040	0.37	VQ
0.333	0.0045	0.37	VQ
0.350	0.0050	0.37	VQ
0.367	0.0055	0.37	VQ
0.383	0.0060	0.37	VQ
0.400	0.0065	0.37	VQ
0.417	0.0070	0.37	VQ

0.433	0.0076	0.37	VQ	1.267	0.0333	0.38	VQ
0.450	0.0081	0.37	VQ	1.283	0.0339	0.38	VQ
0.467	0.0086	0.37	VQ	1.300	0.0344	0.38	VQ
0.483	0.0091	0.37	VQ	1.317	0.0349	0.38	VQ
0.500	0.0096	0.37	VQ	1.333	0.0354	0.38	VQ
0.517	0.0101	0.37	VQ	1.350	0.0359	0.38	VQ
0.533	0.0106	0.37	VQ	1.367	0.0365	0.38	VQ
0.550	0.0111	0.37	VQ	1.383	0.0370	0.38	VQ
0.567	0.0116	0.37	VQ	1.400	0.0375	0.38	VQ
0.583	0.0121	0.37	VQ	1.417	0.0380	0.38	VQ
0.600	0.0126	0.37	VQ	1.433	0.0386	0.38	VQ
0.617	0.0132	0.37	VQ	1.450	0.0391	0.38	VQ
0.633	0.0137	0.37	VQ	1.467	0.0396	0.38	.Q
0.650	0.0142	0.37	VQ	1.483	0.0401	0.38	.Q
0.667	0.0147	0.37	VQ	1.500	0.0407	0.38	.Q
0.683	0.0152	0.37	VQ	1.517	0.0412	0.38	.Q
0.700	0.0157	0.37	VQ	1.533	0.0417	0.38	.Q
0.717	0.0162	0.37	VQ	1.550	0.0423	0.38	.Q
0.733	0.0167	0.37	VQ	1.567	0.0428	0.38	.Q
0.750	0.0173	0.37	VQ	1.583	0.0433	0.38	.Q
0.767	0.0178	0.37	VQ	1.600	0.0438	0.38	.Q
0.783	0.0183	0.37	VQ	1.617	0.0444	0.38	.Q
0.800	0.0188	0.37	VQ	1.633	0.0449	0.38	.Q
0.817	0.0193	0.37	VQ	1.650	0.0454	0.38	.Q
0.833	0.0198	0.37	VQ	1.667	0.0460	0.38	.Q
0.850	0.0204	0.37	VQ	1.683	0.0465	0.38	.Q
0.867	0.0209	0.37	VQ	1.700	0.0470	0.39	.Q
0.883	0.0214	0.37	VQ	1.717	0.0476	0.39	.Q
0.900	0.0219	0.37	VQ	1.733	0.0481	0.39	.Q
0.917	0.0224	0.37	VQ	1.750	0.0486	0.39	.Q
0.933	0.0229	0.37	VQ	1.767	0.0491	0.39	.Q
0.950	0.0234	0.37	VQ	1.783	0.0497	0.39	.Q
0.967	0.0240	0.38	VQ	1.800	0.0502	0.39	.Q
0.983	0.0245	0.38	VQ	1.817	0.0507	0.39	.Q
1.000	0.0250	0.38	VQ	1.833	0.0513	0.39	.Q
1.017	0.0255	0.38	VQ	1.850	0.0518	0.39	.Q
1.033	0.0260	0.38	VQ	1.867	0.0523	0.39	.Q
1.050	0.0266	0.38	VQ	1.883	0.0529	0.39	.Q
1.067	0.0271	0.38	VQ	1.900	0.0534	0.39	.Q
1.083	0.0276	0.38	VQ	1.917	0.0539	0.39	.Q
1.100	0.0281	0.38	VQ	1.933	0.0545	0.39	.Q
1.117	0.0286	0.38	VQ	1.950	0.0550	0.39	.Q
1.133	0.0292	0.38	VQ	1.967	0.0556	0.39	.Q
1.150	0.0297	0.38	VQ	1.983	0.0561	0.39	.Q
1.167	0.0302	0.38	VQ	2.000	0.0566	0.39	.Q
1.183	0.0307	0.38	VQ	2.017	0.0572	0.39	.Q
1.200	0.0312	0.38	VQ	2.033	0.0577	0.39	.Q
1.217	0.0318	0.38	VQ	2.050	0.0582	0.39	.Q
1.233	0.0323	0.38	VQ	2.067	0.0588	0.39	.Q
1.250	0.0328	0.38	VQ	2.083	0.0593	0.39	.Q

2.100	0.0599	0.39	.Q	2.933	0.0872	0.40	.QV
2.117	0.0604	0.39	.Q	2.950	0.0877	0.40	.QV
2.133	0.0609	0.39	.Q	2.967	0.0883	0.40	.QV
2.150	0.0615	0.39	.Q	2.983	0.0888	0.40	.QV
2.167	0.0620	0.39	.Q	3.000	0.0894	0.40	.QV
2.183	0.0625	0.39	.Q	3.017	0.0900	0.40	.QV
2.200	0.0631	0.39	.Q	3.033	0.0905	0.40	.QV
2.217	0.0636	0.39	.Q	3.050	0.0911	0.40	.QV
2.233	0.0642	0.39	.Q	3.067	0.0916	0.40	.QV
2.250	0.0647	0.39	.Q	3.083	0.0922	0.40	.QV
2.267	0.0652	0.39	.Q	3.100	0.0927	0.40	.QV
2.283	0.0658	0.39	.Q	3.117	0.0933	0.41	.QV
2.300	0.0663	0.39	.Q	3.133	0.0939	0.41	.QV
2.317	0.0669	0.39	.Q	3.150	0.0944	0.41	.QV
2.333	0.0674	0.39	.Q	3.167	0.0950	0.41	.QV
2.350	0.0680	0.39	.Q	3.183	0.0955	0.41	.QV
2.367	0.0685	0.39	.Q	3.200	0.0961	0.41	.QV
2.383	0.0690	0.39	.Q	3.217	0.0967	0.41	.QV
2.400	0.0696	0.40	.Q	3.233	0.0972	0.41	.QV
2.417	0.0701	0.40	.Q	3.250	0.0978	0.41	.QV
2.433	0.0707	0.40	.Q	3.267	0.0983	0.41	.QV
2.450	0.0712	0.40	.Q	3.283	0.0989	0.41	.QV
2.467	0.0718	0.40	.Q	3.300	0.0995	0.41	.QV
2.483	0.0723	0.40	.Q	3.317	0.1000	0.41	.QV
2.500	0.0729	0.40	.Q	3.333	0.1006	0.41	.QV
2.517	0.0734	0.40	.Q	3.350	0.1012	0.41	.QV
2.533	0.0740	0.40	.Q	3.367	0.1017	0.41	.QV
2.550	0.0745	0.40	.Q	3.383	0.1023	0.41	.QV
2.567	0.0750	0.40	.Q	3.400	0.1029	0.41	.QV
2.583	0.0756	0.40	.Q	3.417	0.1034	0.41	.QV
2.600	0.0761	0.40	.Q	3.433	0.1040	0.41	.QV
2.617	0.0767	0.40	.Q	3.450	0.1046	0.41	.QV
2.633	0.0772	0.40	.Q	3.467	0.1051	0.41	.QV
2.650	0.0778	0.40	.Q	3.483	0.1057	0.41	.QV
2.667	0.0783	0.40	.QV	3.500	0.1063	0.41	.QV
2.683	0.0789	0.40	.QV	3.517	0.1068	0.41	.QV
2.700	0.0794	0.40	.QV	3.533	0.1074	0.41	.QV
2.717	0.0800	0.40	.QV	3.550	0.1080	0.41	.QV
2.733	0.0805	0.40	.QV	3.567	0.1085	0.41	.QV
2.750	0.0811	0.40	.QV	3.583	0.1091	0.41	.QV
2.767	0.0816	0.40	.QV	3.600	0.1097	0.41	.QV
2.783	0.0822	0.40	.QV	3.617	0.1102	0.41	.QV
2.800	0.0827	0.40	.QV	3.633	0.1108	0.41	.QV
2.817	0.0833	0.40	.QV	3.650	0.1114	0.41	.QV
2.833	0.0838	0.40	.QV	3.667	0.1119	0.41	.QV
2.850	0.0844	0.40	.QV	3.683	0.1125	0.42	.QV
2.867	0.0850	0.40	.QV	3.700	0.1131	0.42	.QV
2.883	0.0855	0.40	.QV	3.717	0.1137	0.42	.QV
2.900	0.0861	0.40	.QV	3.733	0.1142	0.42	.QV
2.917	0.0866	0.40	.QV	3.750	0.1148	0.42	.QV

3.767	0.1154	0.42	.QV	4.600	0.1446	0.43	.Q V
3.783	0.1160	0.42	.QV	4.617	0.1452	0.43	.Q V
3.800	0.1165	0.42	.QV	4.633	0.1458	0.43	.Q V
3.817	0.1171	0.42	.QV	4.650	0.1464	0.43	.Q V
3.833	0.1177	0.42	.Q V	4.667	0.1470	0.43	.Q V
3.850	0.1183	0.42	.Q V	4.683	0.1476	0.43	.Q V
3.867	0.1188	0.42	.Q V	4.700	0.1481	0.43	.Q V
3.883	0.1194	0.42	.Q V	4.717	0.1487	0.43	.Q V
3.900	0.1200	0.42	.Q V	4.733	0.1493	0.43	.Q V
3.917	0.1206	0.42	.Q V	4.750	0.1499	0.43	.Q V
3.933	0.1211	0.42	.Q V	4.767	0.1505	0.43	.Q V
3.950	0.1217	0.42	.Q V	4.783	0.1511	0.43	.Q V
3.967	0.1223	0.42	.Q V	4.800	0.1517	0.43	.Q V
3.983	0.1229	0.42	.Q V	4.817	0.1523	0.43	.Q V
4.000	0.1235	0.42	.Q V	4.833	0.1529	0.44	.Q V
4.017	0.1240	0.42	.Q V	4.850	0.1535	0.44	.Q V
4.033	0.1246	0.42	.Q V	4.867	0.1541	0.44	.Q V
4.050	0.1252	0.42	.Q V	4.883	0.1547	0.44	.Q V
4.067	0.1258	0.42	.Q V	4.900	0.1553	0.44	.Q V
4.083	0.1264	0.42	.Q V	4.917	0.1559	0.44	.Q V
4.100	0.1269	0.42	.Q V	4.933	0.1565	0.44	.Q V
4.117	0.1275	0.42	.Q V	4.950	0.1571	0.44	.Q V
4.133	0.1281	0.42	.Q V	4.967	0.1577	0.44	.Q V
4.150	0.1287	0.42	.Q V	4.983	0.1584	0.44	.Q V
4.167	0.1293	0.42	.Q V	5.000	0.1590	0.44	.Q V
4.183	0.1299	0.42	.Q V	5.017	0.1596	0.44	.Q V
4.200	0.1304	0.42	.Q V	5.033	0.1602	0.44	.Q V
4.217	0.1310	0.42	.Q V	5.050	0.1608	0.44	.Q V
4.233	0.1316	0.42	.Q V	5.067	0.1614	0.44	.Q V
4.250	0.1322	0.42	.Q V	5.083	0.1620	0.44	.Q V
4.267	0.1328	0.43	.Q V	5.100	0.1626	0.44	.Q V
4.283	0.1334	0.43	.Q V	5.117	0.1632	0.44	.Q V
4.300	0.1340	0.43	.Q V	5.133	0.1638	0.44	.Q V
4.317	0.1345	0.43	.Q V	5.150	0.1644	0.44	.Q V
4.333	0.1351	0.43	.Q V	5.167	0.1650	0.44	.Q V
4.350	0.1357	0.43	.Q V	5.183	0.1656	0.44	.Q V
4.367	0.1363	0.43	.Q V	5.200	0.1663	0.44	.Q V
4.383	0.1369	0.43	.Q V	5.217	0.1669	0.44	.Q V
4.400	0.1375	0.43	.Q V	5.233	0.1675	0.44	.Q V
4.417	0.1381	0.43	.Q V	5.250	0.1681	0.44	.Q V
4.433	0.1387	0.43	.Q V	5.267	0.1687	0.44	.Q V
4.450	0.1392	0.43	.Q V	5.283	0.1693	0.44	.Q V
4.467	0.1398	0.43	.Q V	5.300	0.1699	0.44	.Q V
4.483	0.1404	0.43	.Q V	5.317	0.1705	0.45	.Q V
4.500	0.1410	0.43	.Q V	5.333	0.1711	0.45	.Q V
4.517	0.1416	0.43	.Q V	5.350	0.1718	0.45	.Q V
4.533	0.1422	0.43	.Q V	5.367	0.1724	0.45	.Q V
4.550	0.1428	0.43	.Q V	5.383	0.1730	0.45	.Q V
4.567	0.1434	0.43	.Q V	5.400	0.1736	0.45	.Q V
4.583	0.1440	0.43	.Q V	5.417	0.1742	0.45	.Q V

8.767	0.3098	0.54	.Q	V	9.600	0.3482	0.57	. Q	V
8.783	0.3106	0.54	.Q	V	9.617	0.3490	0.57	. Q	V
8.800	0.3113	0.54	.Q	V	9.633	0.3498	0.58	. Q	V
8.817	0.3121	0.54	.Q	V	9.650	0.3506	0.58	. Q	V
8.833	0.3128	0.54	.Q	V	9.667	0.3514	0.58	. Q	V
8.850	0.3136	0.54	.Q	V	9.683	0.3522	0.58	. Q	V
8.867	0.3143	0.54	.Q	V	9.700	0.3530	0.58	. Q	V
8.883	0.3151	0.55	.Q	V	9.717	0.3538	0.58	. Q	V
8.900	0.3158	0.55	.Q	V	9.733	0.3546	0.58	. Q	V
8.917	0.3166	0.55	.Q	V	9.750	0.3554	0.58	. Q	V
8.933	0.3173	0.55	.Q	V	9.767	0.3562	0.58	. Q	V
8.950	0.3181	0.55	.Q	V	9.783	0.3570	0.58	. Q	V
8.967	0.3188	0.55	.Q	V	9.800	0.3578	0.58	. Q	V
8.983	0.3196	0.55	.Q	V	9.817	0.3586	0.58	. Q	V
9.000	0.3204	0.55	.Q	V	9.833	0.3594	0.59	. Q	V
9.017	0.3211	0.55	.Q	V	9.850	0.3602	0.59	. Q	V
9.033	0.3219	0.55	.Q	V	9.867	0.3610	0.59	. Q	V
9.050	0.3226	0.55	.Q	V	9.883	0.3618	0.59	. Q	V
9.067	0.3234	0.55	.Q	V	9.900	0.3626	0.59	. Q	V
9.083	0.3241	0.55	.Q	V	9.917	0.3634	0.59	. Q	V
9.100	0.3249	0.55	.Q	V	9.933	0.3642	0.59	. Q	V
9.117	0.3257	0.55	.Q	V	9.950	0.3650	0.59	. Q	V
9.133	0.3264	0.55	.Q	V	9.967	0.3659	0.59	. Q	V
9.150	0.3272	0.55	.Q	V	9.983	0.3667	0.59	. Q	V
9.167	0.3280	0.55	.Q	V	10.000	0.3675	0.59	. Q	V
9.183	0.3287	0.56	.Q	V	10.017	0.3683	0.59	. Q	V
9.200	0.3295	0.56	.Q	V	10.033	0.3691	0.59	. Q	V
9.217	0.3303	0.56	.Q	V	10.050	0.3699	0.59	. Q	V
9.233	0.3310	0.56	.Q	V	10.067	0.3708	0.60	. Q	V
9.250	0.3318	0.56	.Q	V	10.083	0.3716	0.60	. Q	V
9.267	0.3326	0.56	.Q	V	10.100	0.3724	0.60	. Q	V
9.283	0.3333	0.56	.Q	V	10.117	0.3732	0.60	. Q	V
9.300	0.3341	0.56	.Q	V	10.133	0.3740	0.60	. Q	V
9.317	0.3349	0.56	.Q	V	10.150	0.3749	0.60	. Q	V
9.333	0.3357	0.56	.Q	V	10.167	0.3757	0.60	. Q	V
9.350	0.3364	0.56	.Q	V	10.183	0.3765	0.60	. Q	V
9.367	0.3372	0.56	.Q	V	10.200	0.3774	0.60	. Q	V
9.383	0.3380	0.57	.Q	V	10.217	0.3782	0.60	. Q	V
9.400	0.3388	0.57	.Q	V	10.233	0.3790	0.61	. Q	V
9.417	0.3396	0.57	.Q	V	10.250	0.3799	0.61	. Q	V
9.433	0.3403	0.57	.Q	V	10.267	0.3807	0.61	. Q	V
9.450	0.3411	0.57	.Q	V	10.283	0.3815	0.61	. Q	V
9.467	0.3419	0.57	.Q	V	10.300	0.3824	0.61	. Q	V
9.483	0.3427	0.57	.Q	V	10.317	0.3832	0.61	. Q	V
9.500	0.3435	0.57	.Q	V	10.333	0.3841	0.61	. Q	V
9.517	0.3443	0.57	.Q	V	10.350	0.3849	0.61	. Q	V
9.533	0.3450	0.57	.Q	V	10.367	0.3857	0.61	. Q	V
9.550	0.3458	0.57	.Q	V	10.383	0.3866	0.61	. Q	V
9.567	0.3466	0.57	.Q	V	10.400	0.3874	0.61	. Q	V
9.583	0.3474	0.57	.Q	V	10.417	0.3883	0.61	. Q	V

10.433	0.3891	0.61	. Q	V.	11.267	0.4331	0.66	. Q	.V	.	.	.
10.450	0.3899	0.61	. Q	V.	11.283	0.4341	0.66	. Q	.V	.	.	.
10.467	0.3908	0.62	. Q	V.	11.300	0.4350	0.67	. Q	.V	.	.	.
10.483	0.3916	0.62	. Q	V	11.317	0.4359	0.67	. Q	.V	.	.	.
10.500	0.3925	0.62	. Q	V	11.333	0.4368	0.67	. Q	.V	.	.	.
10.517	0.3933	0.62	. Q	V	11.350	0.4377	0.67	. Q	.V	.	.	.
10.533	0.3942	0.62	. Q	V	11.367	0.4387	0.67	. Q	.V	.	.	.
10.550	0.3951	0.62	. Q	V	11.383	0.4396	0.67	. Q	.V	.	.	.
10.567	0.3959	0.62	. Q	V	11.400	0.4405	0.68	. Q	.V	.	.	.
10.583	0.3968	0.62	. Q	V	11.417	0.4415	0.68	. Q	.V	.	.	.
10.600	0.3976	0.63	. Q	V	11.433	0.4424	0.68	. Q	.V	.	.	.
10.617	0.3985	0.63	. Q	V	11.450	0.4433	0.68	. Q	.V	.	.	.
10.633	0.3994	0.63	. Q	V	11.467	0.4443	0.68	. Q	.V	.	.	.
10.650	0.4002	0.63	. Q	V	11.483	0.4452	0.68	. Q	.V	.	.	.
10.667	0.4011	0.63	. Q	V	11.500	0.4461	0.68	. Q	.V	.	.	.
10.683	0.4020	0.63	. Q	V	11.517	0.4471	0.69	. Q	.V	.	.	.
10.700	0.4028	0.63	. Q	V	11.533	0.4480	0.69	. Q	.V	.	.	.
10.717	0.4037	0.63	. Q	V	11.550	0.4490	0.69	. Q	.V	.	.	.
10.733	0.4046	0.63	. Q	V	11.567	0.4499	0.69	. Q	.V	.	.	.
10.750	0.4054	0.63	. Q	V	11.583	0.4509	0.69	. Q	.V	.	.	.
10.767	0.4063	0.63	. Q	V	11.600	0.4518	0.69	. Q	.V	.	.	.
10.783	0.4072	0.63	. Q	V	11.617	0.4528	0.69	. Q	.V	.	.	.
10.800	0.4081	0.63	. Q	V	11.633	0.4537	0.69	. Q	.V	.	.	.
10.817	0.4089	0.63	. Q	V	11.650	0.4547	0.69	. Q	.V	.	.	.
10.833	0.4098	0.64	. Q	V	11.667	0.4556	0.69	. Q	.V	.	.	.
10.850	0.4107	0.64	. Q	V	11.683	0.4566	0.69	. Q	.V	.	.	.
10.867	0.4116	0.64	. Q	V	11.700	0.4575	0.69	. Q	.V	.	.	.
10.883	0.4124	0.64	. Q	V	11.717	0.4585	0.70	. Q	.V	.	.	.
10.900	0.4133	0.64	. Q	V	11.733	0.4595	0.70	. Q	.V	.	.	.
10.917	0.4142	0.64	. Q	V	11.750	0.4604	0.70	. Q	.V	.	.	.
10.933	0.4151	0.64	. Q	V	11.767	0.4614	0.70	. Q	.V	.	.	.
10.950	0.4160	0.64	. Q	V	11.783	0.4624	0.70	. Q	.V	.	.	.
10.967	0.4169	0.65	. Q	V	11.800	0.4633	0.70	. Q	.V	.	.	.
10.983	0.4178	0.65	. Q	V	11.817	0.4643	0.71	. Q	.V	.	.	.
11.000	0.4187	0.65	. Q	V	11.833	0.4653	0.71	. Q	.V	.	.	.
11.017	0.4196	0.65	. Q	V	11.850	0.4663	0.71	. Q	.V	.	.	.
11.033	0.4205	0.65	. Q	V	11.867	0.4672	0.71	. Q	.V	.	.	.
11.050	0.4214	0.65	. Q	V	11.883	0.4682	0.71	. Q	.V	.	.	.
11.067	0.4223	0.65	. Q	V	11.900	0.4692	0.72	. Q	.V	.	.	.
11.083	0.4232	0.65	. Q	V	11.917	0.4702	0.72	. Q	.V	.	.	.
11.100	0.4241	0.66	. Q	V	11.933	0.4712	0.72	. Q	.V	.	.	.
11.117	0.4250	0.66	. Q	V	11.950	0.4722	0.72	. Q	.V	.	.	.
11.133	0.4259	0.66	. Q	V	11.967	0.4732	0.72	. Q	.V	.	.	.
11.150	0.4268	0.66	. Q	V	11.983	0.4742	0.72	. Q	.V	.	.	.
11.167	0.4277	0.66	. Q	V	12.000	0.4752	0.72	. Q	.V	.	.	.
11.183	0.4286	0.66	. Q	V	12.017	0.4762	0.72	. Q	.V	.	.	.
11.200	0.4295	0.66	. Q	V	12.033	0.4772	0.72	. Q	.V	.	.	.
11.217	0.4304	0.66	. Q	.V	12.050	0.4782	0.73	. Q	.V	.	.	.
11.233	0.4313	0.66	. Q	.V	12.067	0.4792	0.73	. Q	.V	.	.	.
11.250	0.4322	0.66	. Q	.V	12.083	0.4802	0.73	. Q	.V	.	.	.

13.767	0.5917	0.92	.	Q	.	V	14.600	0.6603	1.09	.	Q	.	V	.
13.783	0.5930	0.93	.	Q	.	V	14.617	0.6618	1.09	.	Q	.	V	.
13.800	0.5943	0.93	.	Q	.	V	14.633	0.6633	1.09	.	Q	.	V	.
13.817	0.5955	0.93	.	Q	.	V	14.650	0.6648	1.10	.	Q	.	V	.
13.833	0.5968	0.93	.	Q	.	V	14.667	0.6663	1.10	.	Q	.	V	.
13.850	0.5981	0.93	.	Q	.	V	14.683	0.6678	1.11	.	Q	.	V	.
13.867	0.5994	0.94	.	Q	.	V	14.700	0.6694	1.11	.	Q	.	V	.
13.883	0.6007	0.94	.	Q	.	V	14.717	0.6709	1.12	.	Q	.	V	.
13.900	0.6020	0.95	.	Q	.	V	14.733	0.6725	1.13	.	Q	.	V	.
13.917	0.6033	0.95	.	Q	.	V	14.750	0.6740	1.14	.	Q	.	V	.
13.933	0.6046	0.96	.	Q	.	V	14.767	0.6756	1.15	.	Q	.	V	.
13.950	0.6060	0.96	.	Q	.	V	14.783	0.6772	1.16	.	Q	.	V	.
13.967	0.6073	0.97	.	Q	.	V	14.800	0.6788	1.17	.	Q	.	V	.
13.983	0.6086	0.97	.	Q	.	V	14.817	0.6805	1.18	.	Q	.	V	.
14.000	0.6100	0.98	.	Q	.	V	14.833	0.6821	1.19	.	Q	.	V	.
14.017	0.6114	0.98	.	Q	.	V	14.850	0.6837	1.20	.	Q	.	V	.
14.033	0.6127	0.99	.	Q	.	V	14.867	0.6854	1.21	.	Q	.	V	.
14.050	0.6141	0.99	.	Q	.	V	14.883	0.6871	1.22	.	Q	.	V	.
14.067	0.6155	1.00	.	Q	.	V	14.900	0.6888	1.23	.	Q	.	V	.
14.083	0.6168	1.00	.	Q	.	V	14.917	0.6905	1.25	.	Q	.	V	.
14.100	0.6182	1.00	.	Q	.	V	14.933	0.6923	1.26	.	Q	.	V	.
14.117	0.6196	1.00	.	Q	.	V	14.950	0.6940	1.26	.	Q	.	V	.
14.133	0.6210	0.99	.	Q	.	V	14.967	0.6957	1.27	.	Q	.	V	.
14.150	0.6223	0.99	.	Q	.	V	14.983	0.6975	1.28	.	Q	.	V	.
14.167	0.6237	0.99	.	Q	.	V	15.000	0.6993	1.28	.	Q	.	V	.
14.183	0.6250	0.99	.	Q	.	V	15.017	0.7010	1.29	.	Q	.	V	.
14.200	0.6264	0.99	.	Q	.	V	15.033	0.7028	1.30	.	Q	.	V	.
14.217	0.6278	0.98	.	Q	.	V	15.050	0.7046	1.31	.	Q	.	V	.
14.233	0.6291	0.98	.	Q	.	V	15.067	0.7064	1.31	.	Q	.	V	.
14.250	0.6305	0.98	.	Q	.	V	15.083	0.7083	1.32	.	Q	.	V	.
14.267	0.6318	0.98	.	Q	.	V	15.100	0.7101	1.33	.	Q	.	V	.
14.283	0.6331	0.97	.	Q	.	V	15.117	0.7119	1.33	.	Q	.	V	.
14.300	0.6345	0.98	.	Q	.	V	15.133	0.7138	1.34	.	Q	.	V	.
14.317	0.6358	0.99	.	Q	.	V	15.150	0.7156	1.35	.	Q	.	V	.
14.333	0.6372	0.99	.	Q	.	V	15.167	0.7175	1.37	.	Q	.	V	.
14.350	0.6386	1.00	.	Q	.	V	15.183	0.7194	1.39	.	Q	.	V	.
14.367	0.6400	1.01	.	Q	.	V	15.200	0.7214	1.41	.	Q	.	V	.
14.383	0.6414	1.01	.	Q	.	V	15.217	0.7233	1.43	.	Q	.	V	.
14.400	0.6428	1.02	.	Q	.	V	15.233	0.7253	1.45	.	Q	.	V	.
14.417	0.6442	1.03	.	Q	.	V	15.250	0.7274	1.47	.	Q	.	V	.
14.433	0.6456	1.03	.	Q	.	V	15.267	0.7294	1.49	.	Q	.	V	.
14.450	0.6470	1.04	.	Q	.	V	15.283	0.7315	1.51	.	Q	.	V	.
14.467	0.6485	1.05	.	Q	.	V	15.300	0.7336	1.53	.	Q	.	V	.
14.483	0.6499	1.05	.	Q	.	V	15.317	0.7357	1.55	.	Q	.	V	.
14.500	0.6514	1.06	.	Q	.	V	15.333	0.7379	1.57	.	Q	.	V	.
14.517	0.6529	1.06	.	Q	.	V	15.350	0.7401	1.59	.	Q	.	V	.
14.533	0.6543	1.07	.	Q	.	V	15.367	0.7423	1.61	.	Q	.	V	.
14.550	0.6558	1.07	.	Q	.	V	15.383	0.7446	1.67	.	Q	.	V	.
14.567	0.6573	1.08	.	Q	.	V	15.400	0.7469	1.72	.	Q	.	V	.
14.583	0.6588	1.08	.	Q	.	V	15.417	0.7494	1.77	.	Q	.	V	.

15.433	0.7519	1.82	.	Q	.	V.	.	.	.	16.267	1.0756	9.65	.	.	.	V	.	Q	.
15.450	0.7545	1.87	.	Q	.	V.	.	.	.	16.283	1.0880	8.99	.	.	.	V	.	Q	.
15.467	0.7571	1.92	.	Q	.	V.	.	.	.	16.300	1.0995	8.34	.	.	.	VQ	.	.	.
15.483	0.7598	1.98	.	Q	.	V.	.	.	.	16.317	1.1101	7.69	.	.	.	QV	.	.	.
15.500	0.7626	2.03	.	Q	.	V.	.	.	.	16.333	1.1198	7.03	.	.	.	Q	V	.	.
15.517	0.7655	2.08	.	Q	.	V.	.	.	.	16.350	1.1285	6.38	.	.	.	Q	V	.	.
15.533	0.7684	2.13	.	Q	.	V.	.	.	.	16.367	1.1364	5.73	.	.	.	Q	V	.	.
15.550	0.7714	2.18	.	Q	.	V.	.	.	.	16.383	1.1434	5.08	.	.	.	Q	V	.	.
15.567	0.7745	2.23	.	Q	.	V.	.	.	.	16.400	1.1495	4.42	.	.	.	Q	V	.	.
15.583	0.7777	2.30	.	Q	.	V.	.	.	.	16.417	1.1547	3.77	.	.	.	Q	V	.	.
15.600	0.7810	2.38	.	Q	.	V.	.	.	.	16.433	1.1590	3.12	.	.	.	Q	V	.	.
15.617	0.7844	2.47	.	Q	.	V	.	.	.	16.450	1.1629	2.83	.	.	.	Q	V	.	.
15.633	0.7879	2.55	.	Q	.	V	.	.	.	16.467	1.1667	2.72	.	.	.	Q	V	.	.
15.650	0.7915	2.64	.	Q	.	V	.	.	.	16.483	1.1702	2.61	.	.	.	Q	V	.	.
15.667	0.7953	2.72	.	Q	.	V	.	.	.	16.500	1.1737	2.49	.	.	.	Q	V	.	.
15.683	0.7991	2.81	.	Q	.	V	.	.	.	16.517	1.1770	2.38	.	.	.	Q	V	.	.
15.700	0.8031	2.89	.	Q	.	V	.	.	.	16.533	1.1801	2.27	.	.	.	Q	V	.	.
15.717	0.8072	2.98	.	Q	.	V	.	.	.	16.550	1.1831	2.16	.	.	.	Q	V	.	.
15.733	0.8114	3.06	.	Q	.	V	.	.	.	16.567	1.1859	2.05	.	.	.	Q	V	.	.
15.750	0.8158	3.15	.	Q	.	V	.	.	.	16.583	1.1885	1.93	.	.	.	Q	V	.	.
15.767	0.8202	3.24	.	Q	.	V	.	.	.	16.600	1.1910	1.82	.	.	.	Q	V	.	.
15.783	0.8248	3.32	.	Q	.	V	.	.	.	16.617	1.1934	1.71	.	.	.	Q	V	.	.
15.800	0.8295	3.40	.	Q	.	V	.	.	.	16.633	1.1956	1.60	.	.	.	Q	V	.	.
15.817	0.8343	3.47	.	Q	.	V	.	.	.	16.650	1.1977	1.49	.	.	.	Q	V	.	.
15.833	0.8391	3.53	.	Q	.	V	.	.	.	16.667	1.1996	1.44	.	.	.	Q	V	.	.
15.850	0.8441	3.60	.	Q	.	V	.	.	.	16.683	1.2016	1.42	.	.	.	Q	V	.	.
15.867	0.8491	3.67	.	Q	.	V	.	.	.	16.700	1.2035	1.40	.	.	.	Q	V	.	.
15.883	0.8543	3.73	.	Q	.	V	.	.	.	16.717	1.2054	1.38	.	.	.	Q	V	.	.
15.900	0.8595	3.80	.	Q	.	V	.	.	.	16.733	1.2073	1.36	.	.	.	Q	V	.	.
15.917	0.8648	3.87	.	Q	.	V	.	.	.	16.750	1.2091	1.33	.	.	.	Q	V	.	.
15.933	0.8703	3.93	.	Q	.	V	.	.	.	16.767	1.2109	1.31	.	.	.	Q	V	.	.
15.950	0.8758	4.00	.	Q	.	V	.	.	.	16.783	1.2127	1.29	.	.	.	Q	V	.	.
15.967	0.8814	4.07	.	Q	.	V	.	.	.	16.800	1.2145	1.27	.	.	.	Q	V	.	.
15.983	0.8871	4.14	.	Q	.	V	.	.	.	16.817	1.2162	1.25	.	.	.	Q	V	.	.
16.000	0.8929	4.20	.	Q	.	V	.	.	.	16.833	1.2179	1.23	.	.	.	Q	V	.	.
16.017	0.8991	4.51	.	Q	.	V	.	.	.	16.850	1.2195	1.20	.	.	.	Q	V	.	.
16.033	0.9060	5.06	.	Q	.	V	.	.	.	16.867	1.2212	1.18	.	.	.	Q	V	.	.
16.050	0.9138	5.61	.	Q	.	V	.	.	.	16.883	1.2228	1.17	.	.	.	Q	V	.	.
16.067	0.9223	6.16	.	Q	V	16.900	1.2244	1.16	.	.	.	Q	V	.	.
16.083	0.9315	6.71	.	Q	.	V	.	.	.	16.917	1.2259	1.14	.	.	.	Q	V	.	.
16.100	0.9415	7.26	.	Q	.	VQ	.	.	.	16.933	1.2275	1.13	.	.	.	Q	V	.	.
16.117	0.9523	7.81	.	Q	.	V	Q	.	.	16.950	1.2290	1.12	.	.	.	Q	V	.	.
16.133	0.9638	8.36	.	Q	.	V	Q	.	.	16.967	1.2306	1.10	.	.	.	Q	V	.	.
16.150	0.9761	8.91	.	Q	.	V	Q	.	.	16.983	1.2321	1.09	.	.	.	Q	V	.	.
16.167	0.9891	9.46	.	Q	.	V	Q	.	.	17.000	1.2335	1.08	.	.	.	Q	V	.	.
16.183	1.0029	10.01	.	Q	.	V	Q	.	.	17.017	1.2350	1.07	.	.	.	Q	V	.	.
16.200	1.0174	10.56	.	Q	.	V	Q	.	.	17.033	1.2365	1.05	.	.	.	Q	V	.	.
16.217	1.0330	11.34	.	Q	.	V	Q	.	.	17.050	1.2379	1.04	.	.	.	Q	V	.	.
16.233	1.0481	10.95	.	Q	.	V	Q	.	.	17.067	1.2393	1.03	.	.	.	Q	V	.	.
16.250	1.0623	10.30	.	Q	.	V	Q	.	.	17.083	1.2407	1.01	.	.	.	Q	V	.	.

18.767	1.3513	0.65	. Q	.	.	.	V	.		19.600	1.3929	0.56	.Q	.	.	.	V	.
18.783	1.3522	0.65	. Q	.	.	.	V	.		19.617	1.3936	0.56	.Q	.	.	.	V	.
18.800	1.3531	0.65	. Q	.	.	.	V	.		19.633	1.3944	0.56	.Q	.	.	.	V	.
18.817	1.3540	0.64	. Q	.	.	.	V	.		19.650	1.3952	0.56	.Q	.	.	.	V	.
18.833	1.3549	0.64	. Q	.	.	.	V	.		19.667	1.3959	0.56	.Q	.	.	.	V	.
18.850	1.3558	0.64	. Q	.	.	.	V	.		19.683	1.3967	0.56	.Q	.	.	.	V	.
18.867	1.3566	0.64	. Q	.	.	.	V	.		19.700	1.3975	0.56	.Q	.	.	.	V	.
18.883	1.3575	0.64	. Q	.	.	.	V	.		19.717	1.3982	0.55	.Q	.	.	.	V	.
18.900	1.3584	0.63	. Q	.	.	.	V	.		19.733	1.3990	0.55	.Q	.	.	.	V	.
18.917	1.3593	0.63	. Q	.	.	.	V	.		19.750	1.3998	0.55	.Q	.	.	.	V	.
18.933	1.3601	0.63	. Q	.	.	.	V	.		19.767	1.4005	0.55	.Q	.	.	.	V	.
18.950	1.3610	0.63	. Q	.	.	.	V	.		19.783	1.4013	0.55	.Q	.	.	.	V	.
18.967	1.3619	0.63	. Q	.	.	.	V	.		19.800	1.4020	0.55	.Q	.	.	.	V	.
18.983	1.3627	0.62	. Q	.	.	.	V	.		19.817	1.4028	0.55	.Q	.	.	.	V	.
19.000	1.3636	0.62	. Q	.	.	.	V	.		19.833	1.4035	0.55	.Q	.	.	.	V	.
19.017	1.3644	0.62	. Q	.	.	.	V	.		19.850	1.4043	0.54	.Q	.	.	.	V	.
19.033	1.3653	0.62	. Q	.	.	.	V	.		19.867	1.4050	0.54	.Q	.	.	.	V	.
19.050	1.3661	0.62	. Q	.	.	.	V	.		19.883	1.4058	0.54	.Q	.	.	.	V	.
19.067	1.3670	0.61	. Q	.	.	.	V	.		19.900	1.4065	0.54	.Q	.	.	.	V	.
19.083	1.3678	0.61	. Q	.	.	.	V	.		19.917	1.4073	0.54	.Q	.	.	.	V	.
19.100	1.3687	0.61	. Q	.	.	.	V	.		19.933	1.4080	0.54	.Q	.	.	.	V	.
19.117	1.3695	0.61	. Q	.	.	.	V	.		19.950	1.4087	0.54	.Q	.	.	.	V	.
19.133	1.3703	0.61	. Q	.	.	.	V	.		19.967	1.4095	0.54	.Q	.	.	.	V	.
19.150	1.3712	0.61	. Q	.	.	.	V	.		19.983	1.4102	0.53	.Q	.	.	.	V	.
19.167	1.3720	0.60	. Q	.	.	.	V	.		20.000	1.4110	0.53	.Q	.	.	.	V	.
19.183	1.3728	0.60	. Q	.	.	.	V	.		20.017	1.4117	0.53	.Q	.	.	.	V	.
19.200	1.3737	0.60	. Q	.	.	.	V	.		20.033	1.4124	0.53	.Q	.	.	.	V	.
19.217	1.3745	0.60	. Q	.	.	.	V	.		20.050	1.4131	0.53	.Q	.	.	.	V	.
19.233	1.3753	0.60	. Q	.	.	.	V	.		20.067	1.4139	0.53	.Q	.	.	.	V	.
19.250	1.3761	0.60	. Q	.	.	.	V	.		20.083	1.4146	0.53	.Q	.	.	.	V	.
19.267	1.3769	0.59	. Q	.	.	.	V	.		20.100	1.4153	0.53	.Q	.	.	.	V	.
19.283	1.3778	0.59	. Q	.	.	.	V	.		20.117	1.4160	0.52	.Q	.	.	.	V	.
19.300	1.3786	0.59	. Q	.	.	.	V	.		20.133	1.4168	0.52	.Q	.	.	.	V	.
19.317	1.3794	0.59	. Q	.	.	.	V	.		20.150	1.4175	0.52	.Q	.	.	.	V	.
19.333	1.3802	0.59	. Q	.	.	.	V	.		20.167	1.4182	0.52	.Q	.	.	.	V	.
19.350	1.3810	0.59	. Q	.	.	.	V	.		20.183	1.4189	0.52	.Q	.	.	.	V	.
19.367	1.3818	0.58	. Q	.	.	.	V	.		20.200	1.4196	0.52	.Q	.	.	.	V	.
19.383	1.3826	0.58	. Q	.	.	.	V	.		20.217	1.4204	0.52	.Q	.	.	.	V	.
19.400	1.3834	0.58	. Q	.	.	.	V	.		20.233	1.4211	0.52	.Q	.	.	.	V	.
19.417	1.3842	0.58	. Q	.	.	.	V	.		20.250	1.4218	0.52	.Q	.	.	.	V	.
19.433	1.3850	0.58	. Q	.	.	.	V	.		20.267	1.4225	0.52	.Q	.	.	.	V	.
19.450	1.3858	0.58	. Q	.	.	.	V	.		20.283	1.4232	0.51	.Q	.	.	.	V	.
19.467	1.3866	0.58	. Q	.	.	.	V	.		20.300	1.4239	0.51	.Q	.	.	.	V	.
19.483	1.3874	0.57	. Q	.	.	.	V	.		20.317	1.4246	0.51	.Q	.	.	.	V	.
19.500	1.3882	0.57	. Q	.	.	.	V	.		20.333	1.4253	0.51	.Q	.	.	.	V	.
19.517	1.3890	0.57	. Q	.	.	.	V	.		20.350	1.4260	0.51	.Q	.	.	.	V	.
19.533	1.3897	0.57	. Q	.	.	.	V	.		20.367	1.4267	0.51	.Q	.	.	.	V	.
19.550	1.3905	0.57	. Q	.	.	.	V	.		20.383	1.4274	0.51	.Q	.	.	.	V	.
19.567	1.3913	0.57	. Q	.	.	.	V	.		20.400	1.4281	0.51	.Q	.	.	.	V	.
19.583	1.3921	0.57	. Q	.	.	.	V	.		20.417	1.4288	0.51	.Q	.	.	.	V	.

20.433	1.4295	0.50	.Q	.	.	.	V	.		21.267	1.4627	0.46	.Q	V	.
20.450	1.4302	0.50	.Q	.	.	.	V	.		21.283	1.4633	0.46	.Q	V	.
20.467	1.4309	0.50	.Q	.	.	.	V	.		21.300	1.4639	0.46	.Q	V	.
20.483	1.4316	0.50	.Q	.	.	.	V	.		21.317	1.4646	0.46	.Q	V	.
20.500	1.4323	0.50	.Q	.	.	.	V	.		21.333	1.4652	0.46	.Q	V	.
20.517	1.4330	0.50	.Q	.	.	.	V	.		21.350	1.4658	0.46	.Q	V	.
20.533	1.4336	0.50	.Q	.	.	.	V	.		21.367	1.4664	0.46	.Q	V	.
20.550	1.4343	0.50	.Q	.	.	.	V	.		21.383	1.4671	0.46	.Q	V	.
20.567	1.4350	0.50	.Q	.	.	.	V	.		21.400	1.4677	0.45	.Q	V	.
20.583	1.4357	0.50	.Q	.	.	.	V	.		21.417	1.4683	0.45	.Q	V	.
20.600	1.4364	0.50	.Q	.	.	.	V	.		21.433	1.4690	0.45	.Q	V	.
20.617	1.4371	0.49	.Q	.	.	.	V	.		21.450	1.4696	0.45	.Q	V	.
20.633	1.4377	0.49	.Q	.	.	.	V	.		21.467	1.4702	0.45	.Q	V	.
20.650	1.4384	0.49	.Q	.	.	.	V	.		21.483	1.4708	0.45	.Q	V	.
20.667	1.4391	0.49	.Q	.	.	.	V	.		21.500	1.4714	0.45	.Q	V	.
20.683	1.4398	0.49	.Q	.	.	.	V	.		21.517	1.4721	0.45	.Q	V	.
20.700	1.4404	0.49	.Q	.	.	.	V	.		21.533	1.4727	0.45	.Q	V	.
20.717	1.4411	0.49	.Q	.	.	.	V	.		21.550	1.4733	0.45	.Q	V	.
20.733	1.4418	0.49	.Q	.	.	.	V	.		21.567	1.4739	0.45	.Q	V	.
20.750	1.4425	0.49	.Q	.	.	.	V	.		21.583	1.4745	0.45	.Q	V	.
20.767	1.4431	0.49	.Q	.	.	.	V	.		21.600	1.4751	0.45	.Q	V	.
20.783	1.4438	0.48	.Q	.	.	.	V	.		21.617	1.4758	0.45	.Q	V	.
20.800	1.4445	0.48	.Q	.	.	.	V	.		21.633	1.4764	0.44	.Q	V	.
20.817	1.4451	0.48	.Q	.	.	.	V	.		21.650	1.4770	0.44	.Q	V	.
20.833	1.4458	0.48	.Q	.	.	.	V	.		21.667	1.4776	0.44	.Q	V	.
20.850	1.4465	0.48	.Q	.	.	.	V	.		21.683	1.4782	0.44	.Q	V	.
20.867	1.4471	0.48	.Q	.	.	.	V	.		21.700	1.4788	0.44	.Q	V	.
20.883	1.4478	0.48	.Q	.	.	.	V	.		21.717	1.4794	0.44	.Q	V	.
20.900	1.4484	0.48	.Q	.	.	.	V	.		21.733	1.4800	0.44	.Q	V	.
20.917	1.4491	0.48	.Q	.	.	.	V	.		21.750	1.4806	0.44	.Q	V	.
20.933	1.4498	0.48	.Q	.	.	.	V	.		21.767	1.4812	0.44	.Q	V	.
20.950	1.4504	0.48	.Q	.	.	.	V	.		21.783	1.4818	0.44	.Q	V	.
20.967	1.4511	0.48	.Q	.	.	.	V	.		21.800	1.4825	0.44	.Q	V	.
20.983	1.4517	0.47	.Q	.	.	.	V	.		21.817	1.4831	0.44	.Q	V	.
21.000	1.4524	0.47	.Q	.	.	.	V	.		21.833	1.4837	0.44	.Q	V	.
21.017	1.4530	0.47	.Q	.	.	.	V	.		21.850	1.4843	0.44	.Q	V	.
21.033	1.4537	0.47	.Q	.	.	.	V	.		21.867	1.4849	0.44	.Q	V	.
21.050	1.4543	0.47	.Q	.	.	.	V	.		21.883	1.4855	0.44	.Q	V	.
21.067	1.4550	0.47	.Q	.	.	.	V	.		21.900	1.4861	0.43	.Q	V	.
21.083	1.4556	0.47	.Q	.	.	.	V	.		21.917	1.4867	0.43	.Q	V	.
21.100	1.4563	0.47	.Q	.	.	.	V	.		21.933	1.4872	0.43	.Q	V	.
21.117	1.4569	0.47	.Q	.	.	.	V	.		21.950	1.4878	0.43	.Q	V	.
21.133	1.4576	0.47	.Q	.	.	.	V	.		21.967	1.4884	0.43	.Q	V	.
21.150	1.4582	0.47	.Q	.	.	.	V	.		21.983	1.4890	0.43	.Q	V	.
21.167	1.4588	0.47	.Q	.	.	.	V	.		22.000	1.4896	0.43	.Q	V	.
21.183	1.4595	0.46	.Q	.	.	.	V	.		22.017	1.4902	0.43	.Q	V	.
21.200	1.4601	0.46	.Q	.	.	.	V	.		22.033	1.4908	0.43	.Q	V	.
21.217	1.4608	0.46	.Q	.	.	.	V	.		22.050	1.4914	0.43	.Q	V	.
21.233	1.4614	0.46	.Q	.	.	.	V	.		22.067	1.4920	0.43	.Q	V	.
21.250	1.4620	0.46	.Q	.	.	.	V	.		22.083	1.4926	0.43	.Q	V	.

22.100	1.4932	0.43	.Q	.	.	.	V .		22.933	1.5216	0.40	.Q	V .
22.117	1.4938	0.43	.Q	.	.	.	V .		22.950	1.5221	0.40	.Q	V .
22.133	1.4943	0.43	.Q	.	.	.	V .		22.967	1.5227	0.40	.Q	V .
22.150	1.4949	0.43	.Q	.	.	.	V .		22.983	1.5232	0.40	.Q	V .
22.167	1.4955	0.42	.Q	.	.	.	V .		23.000	1.5238	0.40	.Q	V .
22.183	1.4961	0.42	.Q	.	.	.	V .		23.017	1.5243	0.40	.Q	V .
22.200	1.4967	0.42	.Q	.	.	.	V .		23.033	1.5249	0.40	.Q	V .
22.217	1.4973	0.42	.Q	.	.	.	V .		23.050	1.5254	0.40	.Q	V .
22.233	1.4978	0.42	.Q	.	.	.	V .		23.067	1.5259	0.40	.Q	V .
22.250	1.4984	0.42	.Q	.	.	.	V .		23.083	1.5265	0.39	.Q	V .
22.267	1.4990	0.42	.Q	.	.	.	V .		23.100	1.5270	0.39	.Q	V .
22.283	1.4996	0.42	.Q	.	.	.	V .		23.117	1.5276	0.39	.Q	V .
22.300	1.5002	0.42	.Q	.	.	.	V .		23.133	1.5281	0.39	.Q	V .
22.317	1.5007	0.42	.Q	.	.	.	V .		23.150	1.5287	0.39	.Q	V .
22.333	1.5013	0.42	.Q	.	.	.	V .		23.167	1.5292	0.39	.Q	V .
22.350	1.5019	0.42	.Q	.	.	.	V .		23.183	1.5297	0.39	.Q	V .
22.367	1.5025	0.42	.Q	.	.	.	V .		23.200	1.5303	0.39	.Q	V .
22.383	1.5030	0.42	.Q	.	.	.	V .		23.217	1.5308	0.39	.Q	V .
22.400	1.5036	0.42	.Q	.	.	.	V .		23.233	1.5313	0.39	.Q	V .
22.417	1.5042	0.42	.Q	.	.	.	V .		23.250	1.5319	0.39	.Q	V .
22.433	1.5048	0.42	.Q	.	.	.	V .		23.267	1.5324	0.39	.Q	V .
22.450	1.5053	0.41	.Q	.	.	.	V .		23.283	1.5330	0.39	.Q	V .
22.467	1.5059	0.41	.Q	.	.	.	V .		23.300	1.5335	0.39	.Q	V .
22.483	1.5065	0.41	.Q	.	.	.	V .		23.317	1.5340	0.39	.Q	V .
22.500	1.5070	0.41	.Q	.	.	.	V .		23.333	1.5346	0.39	.Q	V .
22.517	1.5076	0.41	.Q	.	.	.	V .		23.350	1.5351	0.39	.Q	V .
22.533	1.5082	0.41	.Q	.	.	.	V .		23.367	1.5356	0.39	.Q	V .
22.550	1.5087	0.41	.Q	.	.	.	V .		23.383	1.5362	0.39	.Q	V .
22.567	1.5093	0.41	.Q	.	.	.	V .		23.400	1.5367	0.39	.Q	V .
22.583	1.5099	0.41	.Q	.	.	.	V .		23.417	1.5372	0.39	.Q	V .
22.600	1.5104	0.41	.Q	.	.	.	V .		23.433	1.5378	0.39	.Q	V .
22.617	1.5110	0.41	.Q	.	.	.	V .		23.450	1.5383	0.38	.Q	V .
22.633	1.5116	0.41	.Q	.	.	.	V .		23.467	1.5388	0.38	.Q	V .
22.650	1.5121	0.41	.Q	.	.	.	V .		23.483	1.5393	0.38	.Q	V .
22.667	1.5127	0.41	.Q	.	.	.	V .		23.500	1.5399	0.38	.Q	V .
22.683	1.5132	0.41	.Q	.	.	.	V .		23.517	1.5404	0.38	.Q	V .
22.700	1.5138	0.41	.Q	.	.	.	V .		23.533	1.5409	0.38	.Q	V .
22.717	1.5144	0.41	.Q	.	.	.	V .		23.550	1.5415	0.38	.Q	V .
22.733	1.5149	0.41	.Q	.	.	.	V .		23.567	1.5420	0.38	.Q	V .
22.750	1.5155	0.40	.Q	.	.	.	V .		23.583	1.5425	0.38	.Q	V .
22.767	1.5160	0.40	.Q	.	.	.	V .		23.600	1.5430	0.38	.Q	V .
22.783	1.5166	0.40	.Q	.	.	.	V .		23.617	1.5436	0.38	.Q	V .
22.800	1.5171	0.40	.Q	.	.	.	V .		23.633	1.5441	0.38	.Q	V .
22.817	1.5177	0.40	.Q	.	.	.	V .		23.650	1.5446	0.38	.Q	V .
22.833	1.5183	0.40	.Q	.	.	.	V .		23.667	1.5451	0.38	.Q	V .
22.850	1.5188	0.40	.Q	.	.	.	V .		23.683	1.5456	0.38	.Q	V .
22.867	1.5194	0.40	.Q	.	.	.	V .		23.700	1.5462	0.38	.Q	V .
22.883	1.5199	0.40	.Q	.	.	.	V .		23.717	1.5467	0.38	.Q	V .
22.900	1.5205	0.40	.Q	.	.	.	V .		23.733	1.5472	0.38	.Q	V .
22.917	1.5210	0.40	.Q	.	.	.	V .		23.750	1.5477	0.38	.Q	V .

23.767	1.5482	0.38	.Q	.	.	.	V.
23.783	1.5488	0.38	.Q	.	.	.	V.
23.800	1.5493	0.38	.Q	.	.	.	V.
23.817	1.5498	0.38	.Q	.	.	.	V.
23.833	1.5503	0.37	.Q	.	.	.	V.
23.850	1.5508	0.37	.Q	.	.	.	V.
23.867	1.5513	0.37	.Q	.	.	.	V.
23.883	1.5519	0.37	.Q	.	.	.	V.
23.900	1.5524	0.37	.Q	.	.	.	V.
23.917	1.5529	0.37	.Q	.	.	.	V.
23.933	1.5534	0.37	.Q	.	.	.	V.
23.950	1.5539	0.37	.Q	.	.	.	V.
23.967	1.5544	0.37	.Q	.	.	.	V.
23.983	1.5549	0.37	.Q	.	.	.	V.
24.000	1.5554	0.37	.Q	.	.	.	V.

TIME DURATION(minutes) OF PERCENTILES OF ESTIMATED PEAK FLOW RATE:

(Note: 100% of Peak Flow Rate estimate assumed to have
an instantaneous time duration)

Percentile of Estimated Peak Flow Rate	Duration (minutes)
0%	1441.0
10%	655.0
20%	290.0
30%	185.0
40%	110.0
50%	95.0
60%	75.0
70%	55.0
80%	35.0
90%	20.0

0.050	0.0000	0.00	Q
0.067	0.0000	0.00	Q
0.083	0.0000	0.00	Q
0.100	0.0000	0.02	Q
0.117	0.0001	0.05	Q
0.133	0.0002	0.08	Q
0.150	0.0004	0.11	Q
0.167	0.0006	0.14	Q
0.183	0.0008	0.17	Q
0.200	0.0011	0.19	Q
0.217	0.0014	0.22	Q
0.233	0.0017	0.25	Q
0.250	0.0021	0.28	Q
0.267	0.0025	0.31	Q
0.283	0.0030	0.34	Q
0.300	0.0035	0.36	Q
0.317	0.0040	0.37	Q
0.333	0.0045	0.37	Q
0.350	0.0050	0.37	Q
0.367	0.0055	0.37	Q
0.383	0.0060	0.37	Q
0.400	0.0065	0.37	Q
0.417	0.0070	0.37	Q
0.433	0.0076	0.37	Q
0.450	0.0081	0.37	Q
0.467	0.0086	0.37	Q
0.483	0.0091	0.37	Q
0.500	0.0096	0.37	Q
0.517	0.0101	0.37	Q
0.533	0.0106	0.37	Q
0.550	0.0111	0.37	Q
0.567	0.0116	0.37	Q
0.583	0.0121	0.37	Q
0.600	0.0126	0.37	Q
0.617	0.0132	0.37	Q
0.633	0.0137	0.37	Q
0.650	0.0142	0.37	Q
0.667	0.0147	0.37	Q
0.683	0.0152	0.37	Q
0.700	0.0157	0.37	Q
0.717	0.0162	0.37	Q
0.733	0.0167	0.37	Q
0.750	0.0173	0.37	Q
0.767	0.0178	0.37	Q
0.783	0.0183	0.37	Q
0.800	0.0188	0.37	Q
0.817	0.0193	0.37	Q
0.833	0.0198	0.37	Q
0.850	0.0204	0.37	Q
0.867	0.0209	0.37	Q

FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 11

>>>VIEW STREAM NUMBER 1 HYDROGRAPH<<<

STREAM HYDROGRAPH IN ONE-MINUTE UNIT INTERVALS(CFS)
(Notes: Time indicated is at END of Each Unit Intervals.
Peak 5-minute rainfall intensity is modeled as
a constant value for entire 5-minute period.)

TIME(HRS)	VOLUME(AF)	Q(CFS)	0.	5.0	10.0	15.0	20.0
0.017	0.0000	0.00	Q
0.033	0.0000	0.00	Q

0.883	0.0214	0.37 Q	1.717	0.0476	0.39 QV
0.900	0.0219	0.37 Q	1.733	0.0481	0.39 QV
0.917	0.0224	0.37 Q	1.750	0.0486	0.39 QV
0.933	0.0229	0.37 Q	1.767	0.0491	0.39 QV
0.950	0.0234	0.37 Q	1.783	0.0497	0.39 QV
0.967	0.0240	0.38 Q	1.800	0.0502	0.39 QV
0.983	0.0245	0.38 Q	1.817	0.0507	0.39 QV
1.000	0.0250	0.38 Q	1.833	0.0513	0.39 QV
1.017	0.0255	0.38 Q	1.850	0.0518	0.39 QV
1.033	0.0260	0.38 Q	1.867	0.0523	0.39 QV
1.050	0.0266	0.38 Q	1.883	0.0529	0.39 QV
1.067	0.0271	0.38 Q	1.900	0.0534	0.39 QV
1.083	0.0276	0.38 Q	1.917	0.0539	0.39 QV
1.100	0.0281	0.38 Q	1.933	0.0545	0.39 QV
1.117	0.0286	0.38 Q	1.950	0.0550	0.39 QV
1.133	0.0292	0.38 Q	1.967	0.0556	0.39 QV
1.150	0.0297	0.38 Q	1.983	0.0561	0.39 QV
1.167	0.0302	0.38 Q	2.000	0.0566	0.39 QV
1.183	0.0307	0.38 Q	2.017	0.0572	0.39 QV
1.200	0.0312	0.38 Q	2.033	0.0577	0.39 QV
1.217	0.0318	0.38 Q	2.050	0.0582	0.39 QV
1.233	0.0323	0.38 Q	2.067	0.0588	0.39 QV
1.250	0.0328	0.38 Q	2.083	0.0593	0.39 QV
1.267	0.0333	0.38 Q	2.100	0.0599	0.39 QV
1.283	0.0339	0.38 Q	2.117	0.0604	0.39 QV
1.300	0.0344	0.38 Q	2.133	0.0609	0.39 QV
1.317	0.0349	0.38 Q	2.150	0.0615	0.39 QV
1.333	0.0354	0.38 Q	2.167	0.0620	0.39 QV
1.350	0.0359	0.38 Q	2.183	0.0625	0.39 QV
1.367	0.0365	0.38 Q	2.200	0.0631	0.39 QV
1.383	0.0370	0.38 Q	2.217	0.0636	0.39 QV
1.400	0.0375	0.38 Q	2.233	0.0642	0.39 QV
1.417	0.0380	0.38 Q	2.250	0.0647	0.39 QV
1.433	0.0386	0.38 Q	2.267	0.0652	0.39 QV
1.450	0.0391	0.38 Q	2.283	0.0658	0.39 QV
1.467	0.0396	0.38 QV	2.300	0.0663	0.39 QV
1.483	0.0401	0.38 QV	2.317	0.0669	0.39 QV
1.500	0.0407	0.38 QV	2.333	0.0674	0.39 QV
1.517	0.0412	0.38 QV	2.350	0.0680	0.39 QV
1.533	0.0417	0.38 QV	2.367	0.0685	0.39 QV
1.550	0.0423	0.38 QV	2.383	0.0690	0.39 QV
1.567	0.0428	0.38 QV	2.400	0.0696	0.40 QV
1.583	0.0433	0.38 QV	2.417	0.0701	0.40 QV
1.600	0.0438	0.38 QV	2.433	0.0707	0.40 QV
1.617	0.0444	0.38 QV	2.450	0.0712	0.40 QV
1.633	0.0449	0.38 QV	2.467	0.0718	0.40 QV
1.650	0.0454	0.38 QV	2.483	0.0723	0.40 QV
1.667	0.0460	0.38 QV	2.500	0.0729	0.40 QV
1.683	0.0465	0.38 QV	2.517	0.0734	0.40 QV
1.700	0.0470	0.39 QV	2.533	0.0740	0.40 QV

2.550	0.0745	0.40	QV	3.383	0.1023	0.41	Q	V
2.567	0.0750	0.40	QV	3.400	0.1029	0.41	Q	V
2.583	0.0756	0.40	QV	3.417	0.1034	0.41	Q	V
2.600	0.0761	0.40	QV	3.433	0.1040	0.41	Q	V
2.617	0.0767	0.40	QV	3.450	0.1046	0.41	Q	V
2.633	0.0772	0.40	QV	3.467	0.1051	0.41	Q	V
2.650	0.0778	0.40	QV	3.483	0.1057	0.41	Q	V
2.667	0.0783	0.40	Q V	3.500	0.1063	0.41	Q	V
2.683	0.0789	0.40	Q V	3.517	0.1068	0.41	Q	V
2.700	0.0794	0.40	Q V	3.533	0.1074	0.41	Q	V
2.717	0.0800	0.40	Q V	3.550	0.1080	0.41	Q	V
2.733	0.0805	0.40	Q V	3.567	0.1085	0.41	Q	V
2.750	0.0811	0.40	Q V	3.583	0.1091	0.41	Q	V
2.767	0.0816	0.40	Q V	3.600	0.1097	0.41	Q	V
2.783	0.0822	0.40	Q V	3.617	0.1102	0.41	Q	V
2.800	0.0827	0.40	Q V	3.633	0.1108	0.41	Q	V
2.817	0.0833	0.40	Q V	3.650	0.1114	0.41	Q	V
2.833	0.0838	0.40	Q V	3.667	0.1119	0.41	Q	V
2.850	0.0844	0.40	Q V	3.683	0.1125	0.42	Q	V
2.867	0.0850	0.40	Q V	3.700	0.1131	0.42	Q	V
2.883	0.0855	0.40	Q V	3.717	0.1137	0.42	Q	V
2.900	0.0861	0.40	Q V	3.733	0.1142	0.42	Q	V
2.917	0.0866	0.40	Q V	3.750	0.1148	0.42	Q	V
2.933	0.0872	0.40	Q V	3.767	0.1154	0.42	Q	V
2.950	0.0877	0.40	Q V	3.783	0.1160	0.42	Q	V
2.967	0.0883	0.40	Q V	3.800	0.1165	0.42	Q	V
2.983	0.0888	0.40	Q V	3.817	0.1171	0.42	Q	V
3.000	0.0894	0.40	Q V	3.833	0.1177	0.42	Q	V
3.017	0.0900	0.40	Q V	3.850	0.1183	0.42	Q	V
3.033	0.0905	0.40	Q V	3.867	0.1188	0.42	Q	V
3.050	0.0911	0.40	Q V	3.883	0.1194	0.42	Q	V
3.067	0.0916	0.40	Q V	3.900	0.1200	0.42	Q	V
3.083	0.0922	0.40	Q V	3.917	0.1206	0.42	Q	V
3.100	0.0927	0.40	Q V	3.933	0.1211	0.42	Q	V
3.117	0.0933	0.41	Q V	3.950	0.1217	0.42	Q	V
3.133	0.0939	0.41	Q V	3.967	0.1223	0.42	Q	V
3.150	0.0944	0.41	Q V	3.983	0.1229	0.42	Q	V
3.167	0.0950	0.41	Q V	4.000	0.1235	0.42	Q	V
3.183	0.0955	0.41	Q V	4.017	0.1240	0.42	Q	V
3.200	0.0961	0.41	Q V	4.033	0.1246	0.42	Q	V
3.217	0.0967	0.41	Q V	4.050	0.1252	0.42	Q	V
3.233	0.0972	0.41	Q V	4.067	0.1258	0.42	Q	V
3.250	0.0978	0.41	Q V	4.083	0.1264	0.42	Q	V
3.267	0.0983	0.41	Q V	4.100	0.1269	0.42	Q	V
3.283	0.0989	0.41	Q V	4.117	0.1275	0.42	Q	V
3.300	0.0995	0.41	Q V	4.133	0.1281	0.42	Q	V
3.317	0.1000	0.41	Q V	4.150	0.1287	0.42	Q	V
3.333	0.1006	0.41	Q V	4.167	0.1293	0.42	Q	V
3.350	0.1012	0.41	Q V	4.183	0.1299	0.42	Q	V
3.367	0.1017	0.41	Q V	4.200	0.1304	0.42	Q	V

9.217	0.3303	0.56	.Q	V.	10.050	0.3699	0.59	.Q	V.	.	.	.
9.233	0.3310	0.56	.Q	V.	10.067	0.3708	0.60	.Q	V.	.	.	.
9.250	0.3318	0.56	.Q	V.	10.083	0.3716	0.60	.Q	V.	.	.	.
9.267	0.3326	0.56	.Q	V.	10.100	0.3724	0.60	.Q	V.	.	.	.
9.283	0.3333	0.56	.Q	V.	10.117	0.3732	0.60	.Q	V.	.	.	.
9.300	0.3341	0.56	.Q	V.	10.133	0.3740	0.60	.Q	V.	.	.	.
9.317	0.3349	0.56	.Q	V.	10.150	0.3749	0.60	.Q	V.	.	.	.
9.333	0.3357	0.56	.Q	V.	10.167	0.3757	0.60	.Q	V.	.	.	.
9.350	0.3364	0.56	.Q	V.	10.183	0.3765	0.60	.Q	V.	.	.	.
9.367	0.3372	0.56	.Q	V.	10.200	0.3774	0.60	.Q	V.	.	.	.
9.383	0.3380	0.57	.Q	V.	10.217	0.3782	0.60	.Q	V.	.	.	.
9.400	0.3388	0.57	.Q	V.	10.233	0.3790	0.61	.Q	V.	.	.	.
9.417	0.3396	0.57	.Q	V.	10.250	0.3799	0.61	.Q	V.	.	.	.
9.433	0.3403	0.57	.Q	V.	10.267	0.3807	0.61	.Q	V.	.	.	.
9.450	0.3411	0.57	.Q	V.	10.283	0.3815	0.61	.Q	V.	.	.	.
9.467	0.3419	0.57	.Q	V.	10.300	0.3824	0.61	.Q	V.	.	.	.
9.483	0.3427	0.57	.Q	V.	10.317	0.3832	0.61	.Q	V.	.	.	.
9.500	0.3435	0.57	.Q	V.	10.333	0.3841	0.61	.Q	V.	.	.	.
9.517	0.3443	0.57	.Q	V.	10.350	0.3849	0.61	.Q	V.	.	.	.
9.533	0.3450	0.57	.Q	V.	10.367	0.3857	0.61	.Q	V.	.	.	.
9.550	0.3458	0.57	.Q	V.	10.383	0.3866	0.61	.Q	V.	.	.	.
9.567	0.3466	0.57	.Q	V.	10.400	0.3874	0.61	.Q	V.	.	.	.
9.583	0.3474	0.57	.Q	V.	10.417	0.3883	0.61	.Q	V.	.	.	.
9.600	0.3482	0.57	.Q	V.	10.433	0.3891	0.61	.Q	V.	.	.	.
9.617	0.3490	0.57	.Q	V.	10.450	0.3899	0.61	.Q	V.	.	.	.
9.633	0.3498	0.58	.Q	V.	10.467	0.3908	0.62	.Q	V.	.	.	.
9.650	0.3506	0.58	.Q	V.	10.483	0.3916	0.62	.Q	V.	.	.	.
9.667	0.3514	0.58	.Q	V.	10.500	0.3925	0.62	.Q	V.	.	.	.
9.683	0.3522	0.58	.Q	V.	10.517	0.3933	0.62	.Q	V.	.	.	.
9.700	0.3530	0.58	.Q	V.	10.533	0.3942	0.62	.Q	V.	.	.	.
9.717	0.3538	0.58	.Q	V.	10.550	0.3951	0.62	.Q	V.	.	.	.
9.733	0.3546	0.58	.Q	V.	10.567	0.3959	0.62	.Q	V.	.	.	.
9.750	0.3554	0.58	.Q	V.	10.583	0.3968	0.62	.Q	V.	.	.	.
9.767	0.3562	0.58	.Q	V.	10.600	0.3976	0.63	.Q	V.	.	.	.
9.783	0.3570	0.58	.Q	V.	10.617	0.3985	0.63	.Q	V.	.	.	.
9.800	0.3578	0.58	.Q	V.	10.633	0.3994	0.63	.Q	V.	.	.	.
9.817	0.3586	0.58	.Q	V.	10.650	0.4002	0.63	.Q	V.	.	.	.
9.833	0.3594	0.59	.Q	V.	10.667	0.4011	0.63	.Q	V.	.	.	.
9.850	0.3602	0.59	.Q	V.	10.683	0.4020	0.63	.Q	V.	.	.	.
9.867	0.3610	0.59	.Q	V.	10.700	0.4028	0.63	.Q	V.	.	.	.
9.883	0.3618	0.59	.Q	V.	10.717	0.4037	0.63	.Q	V.	.	.	.
9.900	0.3626	0.59	.Q	V.	10.733	0.4046	0.63	.Q	V.	.	.	.
9.917	0.3634	0.59	.Q	V.	10.750	0.4054	0.63	.Q	V.	.	.	.
9.933	0.3642	0.59	.Q	V.	10.767	0.4063	0.63	.Q	V.	.	.	.
9.950	0.3650	0.59	.Q	V.	10.783	0.4072	0.63	.Q	V.	.	.	.
9.967	0.3659	0.59	.Q	V.	10.800	0.4081	0.63	.Q	V.	.	.	.
9.983	0.3667	0.59	.Q	V.	10.817	0.4089	0.63	.Q	V.	.	.	.
10.000	0.3675	0.59	.Q	V.	10.833	0.4098	0.64	.Q	V.	.	.	.
10.017	0.3683	0.59	.Q	V.	10.850	0.4107	0.64	.Q	V.	.	.	.
10.033	0.3691	0.59	.Q	V.	10.867	0.4116	0.64	.Q	V.	.	.	.

10.883	0.4124	0.64	.Q	V	11.717	0.4585	0.70	.Q	.V	.	.	.
10.900	0.4133	0.64	.Q	V	11.733	0.4595	0.70	.Q	.V	.	.	.
10.917	0.4142	0.64	.Q	V	11.750	0.4604	0.70	.Q	.V	.	.	.
10.933	0.4151	0.64	.Q	V	11.767	0.4614	0.70	.Q	.V	.	.	.
10.950	0.4160	0.64	.Q	V	11.783	0.4624	0.70	.Q	.V	.	.	.
10.967	0.4169	0.65	.Q	V	11.800	0.4633	0.70	.Q	.V	.	.	.
10.983	0.4178	0.65	.Q	V	11.817	0.4643	0.71	.Q	.V	.	.	.
11.000	0.4187	0.65	.Q	V	11.833	0.4653	0.71	.Q	.V	.	.	.
11.017	0.4196	0.65	.Q	V	11.850	0.4663	0.71	.Q	.V	.	.	.
11.033	0.4205	0.65	.Q	V	11.867	0.4672	0.71	.Q	.V	.	.	.
11.050	0.4214	0.65	.Q	V	11.883	0.4682	0.71	.Q	.V	.	.	.
11.067	0.4223	0.65	.Q	V	11.900	0.4692	0.72	.Q	.V	.	.	.
11.083	0.4232	0.65	.Q	V	11.917	0.4702	0.72	.Q	.V	.	.	.
11.100	0.4241	0.66	.Q	V	11.933	0.4712	0.72	.Q	.V	.	.	.
11.117	0.4250	0.66	.Q	V	11.950	0.4722	0.72	.Q	.V	.	.	.
11.133	0.4259	0.66	.Q	V	11.967	0.4732	0.72	.Q	.V	.	.	.
11.150	0.4268	0.66	.Q	V	11.983	0.4742	0.72	.Q	.V	.	.	.
11.167	0.4277	0.66	.Q	V	12.000	0.4752	0.72	.Q	.V	.	.	.
11.183	0.4286	0.66	.Q	V	12.017	0.4762	0.72	.Q	.V	.	.	.
11.200	0.4295	0.66	.Q	V	12.033	0.4772	0.72	.Q	.V	.	.	.
11.217	0.4304	0.66	.Q	.V	12.050	0.4782	0.73	.Q	.V	.	.	.
11.233	0.4313	0.66	.Q	.V	12.067	0.4792	0.73	.Q	.V	.	.	.
11.250	0.4322	0.66	.Q	.V	12.083	0.4802	0.73	.Q	.V	.	.	.
11.267	0.4331	0.66	.Q	.V	12.100	0.4812	0.73	.Q	.V	.	.	.
11.283	0.4341	0.66	.Q	.V	12.117	0.4822	0.73	.Q	.V	.	.	.
11.300	0.4350	0.67	.Q	.V	12.133	0.4832	0.73	.Q	.V	.	.	.
11.317	0.4359	0.67	.Q	.V	12.150	0.4842	0.73	.Q	.V	.	.	.
11.333	0.4368	0.67	.Q	.V	12.167	0.4852	0.73	.Q	.V	.	.	.
11.350	0.4377	0.67	.Q	.V	12.183	0.4862	0.73	.Q	.V	.	.	.
11.367	0.4387	0.67	.Q	.V	12.200	0.4872	0.73	.Q	.V	.	.	.
11.383	0.4396	0.67	.Q	.V	12.217	0.4882	0.73	.Q	.V	.	.	.
11.400	0.4405	0.68	.Q	.V	12.233	0.4892	0.73	.Q	.V	.	.	.
11.417	0.4415	0.68	.Q	.V	12.250	0.4902	0.73	.Q	.V	.	.	.
11.433	0.4424	0.68	.Q	.V	12.267	0.4912	0.73	.Q	.V	.	.	.
11.450	0.4433	0.68	.Q	.V	12.283	0.4922	0.73	.Q	.V	.	.	.
11.467	0.4443	0.68	.Q	.V	12.300	0.4932	0.73	.Q	.V	.	.	.
11.483	0.4452	0.68	.Q	.V	12.317	0.4942	0.73	.Q	.V	.	.	.
11.500	0.4461	0.68	.Q	.V	12.333	0.4952	0.73	.Q	.V	.	.	.
11.517	0.4471	0.69	.Q	.V	12.350	0.4963	0.73	.Q	.V	.	.	.
11.533	0.4480	0.69	.Q	.V	12.367	0.4973	0.73	.Q	.V	.	.	.
11.550	0.4490	0.69	.Q	.V	12.383	0.4983	0.73	.Q	.V	.	.	.
11.567	0.4499	0.69	.Q	.V	12.400	0.4993	0.73	.Q	.V	.	.	.
11.583	0.4509	0.69	.Q	.V	12.417	0.5003	0.73	.Q	.V	.	.	.
11.600	0.4518	0.69	.Q	.V	12.433	0.5013	0.74	.Q	.V	.	.	.
11.617	0.4528	0.69	.Q	.V	12.450	0.5023	0.74	.Q	.V	.	.	.
11.633	0.4537	0.69	.Q	.V	12.467	0.5033	0.74	.Q	.V	.	.	.
11.650	0.4547	0.69	.Q	.V	12.483	0.5043	0.74	.Q	.V	.	.	.
11.667	0.4556	0.69	.Q	.V	12.500	0.5054	0.74	.Q	.V	.	.	.
11.683	0.4566	0.69	.Q	.V	12.517	0.5064	0.74	.Q	.V	.	.	.
11.700	0.4575	0.69	.Q	.V	12.533	0.5074	0.74	.Q	.V	.	.	.

14.217	0.6278	0.98	.Q	.	V	15.050	0.7046	1.31	. Q	.	V .
14.233	0.6291	0.98	.Q	.	V	15.067	0.7064	1.31	. Q	.	V .	
14.250	0.6305	0.98	.Q	.	V	15.083	0.7083	1.32	. Q	.	V .	
14.267	0.6318	0.98	.Q	.	V	15.100	0.7101	1.33	. Q	.	V .	
14.283	0.6331	0.97	.Q	.	V	15.117	0.7119	1.33	. Q	.	V .	
14.300	0.6345	0.98	.Q	.	V	15.133	0.7138	1.34	. Q	.	V .	
14.317	0.6358	0.99	.Q	.	V	15.150	0.7156	1.35	. Q	.	V .	
14.333	0.6372	0.99	.Q	.	V	15.167	0.7175	1.37	. Q	.	V .	
14.350	0.6386	1.00	.Q	.	V	15.183	0.7194	1.39	. Q	.	V .	
14.367	0.6400	1.01	.Q	.	V	15.200	0.7214	1.41	. Q	.	V .	
14.383	0.6414	1.01	.Q	.	V	15.217	0.7233	1.43	. Q	.	V .	
14.400	0.6428	1.02	.Q	.	V	15.233	0.7253	1.45	. Q	.	V .	
14.417	0.6442	1.03	.Q	.	V	15.250	0.7274	1.47	. Q	.	V .	
14.433	0.6456	1.03	.Q	.	V	15.267	0.7294	1.49	. Q	.	V .	
14.450	0.6470	1.04	.Q	.	V	15.283	0.7315	1.51	. Q	.	V .	
14.467	0.6485	1.05	.Q	.	V	15.300	0.7336	1.53	. Q	.	V .	
14.483	0.6499	1.05	.Q	.	V	15.317	0.7357	1.55	. Q	.	V .	
14.500	0.6514	1.06	.Q	.	V	15.333	0.7379	1.57	. Q	.	V .	
14.517	0.6529	1.06	.Q	.	V	15.350	0.7401	1.59	. Q	.	V .	
14.533	0.6543	1.07	.Q	.	V	15.367	0.7423	1.61	. Q	.	V .	
14.550	0.6558	1.07	.Q	.	V	15.383	0.7446	1.67	. Q	.	V .	
14.567	0.6573	1.08	.Q	.	V	15.400	0.7469	1.72	. Q	.	V .	
14.583	0.6588	1.08	.Q	.	V	15.417	0.7494	1.77	. Q	.	V .	
14.600	0.6603	1.09	.Q	.	V	15.433	0.7519	1.82	. Q	.	V .	
14.617	0.6618	1.09	.Q	.	V	15.450	0.7545	1.87	. Q	.	V .	
14.633	0.6633	1.09	.Q	.	V	15.467	0.7571	1.92	. Q	.	V .	
14.650	0.6648	1.10	.Q	.	V	15.483	0.7598	1.98	. Q	.	V .	
14.667	0.6663	1.10	.Q	.	V	15.500	0.7626	2.03	. Q	.	V .	
14.683	0.6678	1.11	.Q	.	V	15.517	0.7655	2.08	. Q	.	V .	
14.700	0.6694	1.11	.Q	.	V	15.533	0.7684	2.13	. Q	.	V .	
14.717	0.6709	1.12	.Q	.	V	15.550	0.7714	2.18	. Q	.	V .	
14.733	0.6725	1.13	.Q	.	V	15.567	0.7745	2.23	. Q	.	V .	
14.750	0.6740	1.14	.Q	.	V	15.583	0.7777	2.30	. Q	.	V .	
14.767	0.6756	1.15	.Q	.	V	15.600	0.7810	2.38	. Q	.	V .	
14.783	0.6772	1.16	.Q	.	V	15.617	0.7844	2.47	. Q	.	V .	
14.800	0.6788	1.17	.Q	.	V	15.633	0.7879	2.55	. Q	.	V .	
14.817	0.6805	1.18	.Q	.	V	15.650	0.7915	2.64	. Q	.	V .	
14.833	0.6821	1.19	.Q	.	V	15.667	0.7953	2.72	. Q	.	V .	
14.850	0.6837	1.20	.Q	.	V	15.683	0.7991	2.81	. Q	.	V .	
14.867	0.6854	1.21	.Q	.	V	15.700	0.8031	2.89	. Q	.	V .	
14.883	0.6871	1.22	.Q	.	V	15.717	0.8072	2.98	. Q	.	V .	
14.900	0.6888	1.23	.Q	.	V	15.733	0.8114	3.06	. Q	.	V .	
14.917	0.6905	1.25	.Q	.	V	15.750	0.8158	3.15	. Q	.	V .	
14.933	0.6923	1.26	.Q	.	V	15.767	0.8202	3.24	. Q	.	V .	
14.950	0.6940	1.26	.Q	.	V	15.783	0.8248	3.32	. Q	.	.V .	
14.967	0.6957	1.27	.Q	.	V	15.800	0.8295	3.40	. Q	.	.V .	
14.983	0.6975	1.28	.Q	.	V	15.817	0.8343	3.47	. Q	.	.V .	
15.000	0.6993	1.28	.Q	.	V	15.833	0.8391	3.53	. Q	.	.V .	
15.017	0.7010	1.29	.Q	.	V	15.850	0.8441	3.60	. Q	.	.V .	
15.033	0.7028	1.30	.Q	.	V	15.867	0.8491	3.67	. Q	.	.V .	

15.883	0.8543	3.73	.	Q	.	.V	.	.	.	16.717	1.2054	1.38	.	Q	.	.	.	V	.
15.900	0.8595	3.80	.	Q	.	.V	.	.	.	16.733	1.2073	1.36	.	Q	.	.	.	V	.
15.917	0.8648	3.87	.	Q	.	.V	.	.	.	16.750	1.2091	1.33	.	Q	.	.	.	V	.
15.933	0.8703	3.93	.	Q	.	.V	.	.	.	16.767	1.2109	1.31	.	Q	.	.	.	V	.
15.950	0.8758	4.00	.	Q	.	.V	.	.	.	16.783	1.2127	1.29	.	QV	.
15.967	0.8814	4.07	.	Q	.	.V	.	.	.	16.800	1.2145	1.27	.	Q	.	.	.	V	.
15.983	0.8871	4.14	.	Q	.	.V	.	.	.	16.817	1.2162	1.25	.	QV	.
16.000	0.8929	4.20	.	Q	.	.V	.	.	.	16.833	1.2179	1.23	.	Q	.	.	.	V	.
16.017	0.8991	4.51	.	Q.	.	.V	.	.	.	16.850	1.2195	1.20	.	QV	.
16.033	0.9060	5.06	.	Q	.	.V	.	.	.	16.867	1.2212	1.18	.	Q	.	.	.	V	.
16.050	0.9138	5.61	.	.Q	.	.V	.	.	.	16.883	1.2228	1.17	.	Q	.	.	.	V	.
16.067	0.9223	6.16	.	.Q	.	.V	.	.	.	16.900	1.2244	1.16	.	Q	.	.	.	V	.
16.083	0.9315	6.71	.	.Q	.	.V	.	.	.	16.917	1.2259	1.14	.	Q	.	.	.	V	.
16.100	0.9415	7.26	.	.Q	.	.V	.	.	.	16.933	1.2275	1.13	.	Q	.	.	.	V	.
16.117	0.9523	7.81	.	.Q	.	.V	.	.	.	16.950	1.2290	1.12	.	Q	.	.	.	V	.
16.133	0.9638	8.36	.	.Q	.	.V	.	.	.	16.967	1.2306	1.10	.	Q	.	.	.	V	.
16.150	0.9761	8.91	.	.Q	.	.V	.	.	.	16.983	1.2321	1.09	.	Q	.	.	.	V	.
16.167	0.9891	9.46	.	.Q	.	.V	.	.	.	17.000	1.2335	1.08	.	Q	.	.	.	V	.
16.183	1.0029	10.01	.	Q	.	.V	.	.	.	17.017	1.2350	1.07	.	Q	.	.	.	V	.
16.200	1.0174	10.56	.	.Q	.	.V	.	.	.	17.033	1.2365	1.05	.	QV	.
16.217	1.0330	11.34	.	.Q	.	.V	.	.	.	17.050	1.2379	1.04	.	Q	.	.	.	V	.
16.233	1.0481	10.95	.	.Q	.	.V	.	.	.	17.067	1.2393	1.03	.	QV	.
16.250	1.0623	10.30	.	Q	.	.V	.	.	.	17.083	1.2407	1.01	.	Q	.	.	.	V	.
16.267	1.0756	9.65	.	Q	.	.V	.	.	.	17.100	1.2421	1.01	.	Q	.	.	.	V	.
16.283	1.0880	8.99	.	Q	.	.V	.	.	.	17.117	1.2435	1.01	.	Q	.	.	.	V	.
16.300	1.0995	8.34	.	Q	.	.V	.	.	.	17.133	1.2449	1.00	.	Q	.	.	.	V	.
16.317	1.1101	7.69	.	Q	.	.V	.	.	.	17.150	1.2462	1.00	.	Q	.	.	.	V	.
16.333	1.1198	7.03	.	Q	.	.V	.	.	.	17.167	1.2476	1.00	.	Q	.	.	.	V	.
16.350	1.1285	6.38	.	Q	.	.V	.	.	.	17.183	1.2490	0.99	.	Q	.	.	.	V	.
16.367	1.1364	5.73	.	.Q	.	.V	.	.	.	17.200	1.2503	0.99	.	Q	.	.	.	V	.
16.383	1.1434	5.08	.	Q	.	.V	.	.	.	17.217	1.2517	0.98	.	Q	.	.	.	V	.
16.400	1.1495	4.42	.	Q	.	.V	.	.	.	17.233	1.2530	0.98	.	Q	.	.	.	V	.
16.417	1.1547	3.77	.	Q	.	.V	.	.	.	17.250	1.2544	0.98	.	Q	.	.	.	V	.
16.433	1.1590	3.12	.	Q	.	.V	.	.	.	17.267	1.2557	0.97	.	Q	.	.	.	V	.
16.450	1.1629	2.83	.	Q	.	.V	.	.	.	17.283	1.2571	0.97	.	Q	.	.	.	V	.
16.467	1.1667	2.72	.	Q	.	.V	.	.	.	17.300	1.2584	0.97	.	Q	.	.	.	V	.
16.483	1.1702	2.61	.	Q	.	.V	.	.	.	17.317	1.2597	0.96	.	Q	.	.	.	V	.
16.500	1.1737	2.49	.	Q	.	.V	.	.	.	17.333	1.2610	0.95	.	Q	.	.	.	V	.
16.517	1.1770	2.38	.	Q	.	.V	.	.	.	17.350	1.2623	0.95	.	Q	.	.	.	V	.
16.533	1.1801	2.27	.	Q	.	.V	.	.	.	17.367	1.2636	0.94	.	Q	.	.	.	V	.
16.550	1.1831	2.16	.	Q	.	.V	.	.	.	17.383	1.2649	0.93	.	Q	.	.	.	V	.
16.567	1.1859	2.05	.	Q	.	.V	.	.	.	17.400	1.2662	0.93	.	Q	.	.	.	V	.
16.583	1.1885	1.93	.	Q	.	.V	.	.	.	17.417	1.2674	0.92	.	Q	.	.	.	V	.
16.600	1.1910	1.82	.	Q	.	.V	.	.	.	17.433	1.2687	0.91	.	Q	.	.	.	V	.
16.617	1.1934	1.71	.	Q	.	.V	.	.	.	17.450	1.2700	0.91	.	Q	.	.	.	V	.
16.633	1.1956	1.60	.	Q	.	.V	.	.	.	17.467	1.2712	0.90	.	Q	.	.	.	V	.
16.650	1.1977	1.49	.	Q	.	.V	.	.	.	17.483	1.2724	0.89	.	Q	.	.	.	V	.
16.667	1.1996	1.44	.	Q	.	.V	.	.	.	17.500	1.2736	0.89	.	Q	.	.	.	V	.
16.683	1.2016	1.42	.	Q	.	.V	.	.	.	17.517	1.2749	0.88	.	Q	.	.	.	V	.
16.700	1.2035	1.40	.	Q	.	.V	.	.	.	17.533	1.2761	0.88	.	Q	.	.	.	V	.

17.550	1.2773	0.87	.Q	.	.	.	V	.		18.383	1.3299	0.70	.Q	.	.	.	V	.
17.567	1.2785	0.86	.Q	.	.	.	V	.		18.400	1.3309	0.70	.Q	.	.	.	V	.
17.583	1.2796	0.86	.Q	.	.	.	V	.		18.417	1.3319	0.70	.Q	.	.	.	V	.
17.600	1.2808	0.85	.Q	.	.	.	V	.		18.433	1.3328	0.70	.Q	.	.	.	V	.
17.617	1.2820	0.85	.Q	.	.	.	V	.		18.450	1.3338	0.69	.Q	.	.	.	V	.
17.633	1.2831	0.84	.Q	.	.	.	V	.		18.467	1.3347	0.69	.Q	.	.	.	V	.
17.650	1.2843	0.84	.Q	.	.	.	V	.		18.483	1.3357	0.69	.Q	.	.	.	V	.
17.667	1.2855	0.83	.Q	.	.	.	V	.		18.500	1.3366	0.69	.Q	.	.	.	V	.
17.683	1.2866	0.83	.Q	.	.	.	V	.		18.517	1.3376	0.68	.Q	.	.	.	V	.
17.700	1.2877	0.82	.Q	.	.	.	V	.		18.533	1.3385	0.68	.Q	.	.	.	V	.
17.717	1.2889	0.82	.Q	.	.	.	V	.		18.550	1.3395	0.68	.Q	.	.	.	V	.
17.733	1.2900	0.81	.Q	.	.	.	V	.		18.567	1.3404	0.68	.Q	.	.	.	V	.
17.750	1.2911	0.81	.Q	.	.	.	V	.		18.583	1.3413	0.67	.Q	.	.	.	V	.
17.767	1.2922	0.80	.Q	.	.	.	V	.		18.600	1.3422	0.67	.Q	.	.	.	V	.
17.783	1.2933	0.80	.Q	.	.	.	V	.		18.617	1.3432	0.67	.Q	.	.	.	V	.
17.800	1.2944	0.80	.Q	.	.	.	V	.		18.633	1.3441	0.67	.Q	.	.	.	V	.
17.817	1.2955	0.79	.Q	.	.	.	V	.		18.650	1.3450	0.67	.Q	.	.	.	V	.
17.833	1.2966	0.79	.Q	.	.	.	V	.		18.667	1.3459	0.66	.Q	.	.	.	V	.
17.850	1.2977	0.78	.Q	.	.	.	V	.		18.683	1.3468	0.66	.Q	.	.	.	V	.
17.867	1.2987	0.78	.Q	.	.	.	V	.		18.700	1.3477	0.66	.Q	.	.	.	V	.
17.883	1.2998	0.78	.Q	.	.	.	V	.		18.717	1.3486	0.66	.Q	.	.	.	V	.
17.900	1.3009	0.77	.Q	.	.	.	V	.		18.733	1.3495	0.65	.Q	.	.	.	V	.
17.917	1.3019	0.77	.Q	.	.	.	V	.		18.750	1.3504	0.65	.Q	.	.	.	V	.
17.933	1.3030	0.76	.Q	.	.	.	V	.		18.767	1.3513	0.65	.Q	.	.	.	V	.
17.950	1.3040	0.76	.Q	.	.	.	V	.		18.783	1.3522	0.65	.Q	.	.	.	V	.
17.967	1.3051	0.76	.Q	.	.	.	V	.		18.800	1.3531	0.65	.Q	.	.	.	V	.
17.983	1.3061	0.75	.Q	.	.	.	V	.		18.817	1.3540	0.64	.Q	.	.	.	V	.
18.000	1.3071	0.75	.Q	.	.	.	V	.		18.833	1.3549	0.64	.Q	.	.	.	V	.
18.017	1.3082	0.75	.Q	.	.	.	V	.		18.850	1.3558	0.64	.Q	.	.	.	V	.
18.033	1.3092	0.74	.Q	.	.	.	V	.		18.867	1.3566	0.64	.Q	.	.	.	V	.
18.050	1.3102	0.74	.Q	.	.	.	V	.		18.883	1.3575	0.64	.Q	.	.	.	V	.
18.067	1.3112	0.74	.Q	.	.	.	V	.		18.900	1.3584	0.63	.Q	.	.	.	V	.
18.083	1.3122	0.73	.Q	.	.	.	V	.		18.917	1.3593	0.63	.Q	.	.	.	V	.
18.100	1.3132	0.73	.Q	.	.	.	V	.		18.933	1.3601	0.63	.Q	.	.	.	V	.
18.117	1.3142	0.73	.Q	.	.	.	V	.		18.950	1.3610	0.63	.Q	.	.	.	V	.
18.133	1.3152	0.72	.Q	.	.	.	V	.		18.967	1.3619	0.63	.Q	.	.	.	V	.
18.150	1.3162	0.72	.Q	.	.	.	V	.		18.983	1.3627	0.62	.Q	.	.	.	V	.
18.167	1.3172	0.72	.Q	.	.	.	V	.		19.000	1.3636	0.62	.Q	.	.	.	V	.
18.183	1.3182	0.72	.Q	.	.	.	V	.		19.017	1.3644	0.62	.Q	.	.	.	V	.
18.200	1.3192	0.72	.Q	.	.	.	V	.		19.033	1.3653	0.62	.Q	.	.	.	V	.
18.217	1.3202	0.72	.Q	.	.	.	V	.		19.050	1.3661	0.62	.Q	.	.	.	V	.
18.233	1.3211	0.71	.Q	.	.	.	V	.		19.067	1.3670	0.61	.Q	.	.	.	V	.
18.250	1.3221	0.71	.Q	.	.	.	V	.		19.083	1.3678	0.61	.Q	.	.	.	V	.
18.267	1.3231	0.71	.Q	.	.	.	V	.		19.100	1.3687	0.61	.Q	.	.	.	V	.
18.283	1.3241	0.71	.Q	.	.	.	V	.		19.117	1.3695	0.61	.Q	.	.	.	V	.
18.300	1.3251	0.71	.Q	.	.	.	V	.		19.133	1.3703	0.61	.Q	.	.	.	V	.
18.317	1.3260	0.71	.Q	.	.	.	V	.		19.150	1.3712	0.61	.Q	.	.	.	V	.
18.333	1.3270	0.71	.Q	.	.	.	V	.		19.167	1.3720	0.60	.Q	.	.	.	V	.
18.350	1.3280	0.71	.Q	.	.	.	V	.		19.183	1.3728	0.60	.Q	.	.	.	V	.
18.367	1.3290	0.71	.Q	.	.	.	V	.		19.200	1.3737	0.60	.Q	.	.	.	V	.

19.217	1.3745	0.60	.Q	.	.	.	V	.		20.050	1.4131	0.53	.Q	.	.	.	V	.
19.233	1.3753	0.60	.Q	.	.	.	V	.		20.067	1.4139	0.53	.Q	.	.	.	V	.
19.250	1.3761	0.60	.Q	.	.	.	V	.		20.083	1.4146	0.53	.Q	.	.	.	V	.
19.267	1.3769	0.59	.Q	.	.	.	V	.		20.100	1.4153	0.53	.Q	.	.	.	V	.
19.283	1.3778	0.59	.Q	.	.	.	V	.		20.117	1.4160	0.52	.Q	.	.	.	V	.
19.300	1.3786	0.59	.Q	.	.	.	V	.		20.133	1.4168	0.52	.Q	.	.	.	V	.
19.317	1.3794	0.59	.Q	.	.	.	V	.		20.150	1.4175	0.52	.Q	.	.	.	V	.
19.333	1.3802	0.59	.Q	.	.	.	V	.		20.167	1.4182	0.52	.Q	.	.	.	V	.
19.350	1.3810	0.59	.Q	.	.	.	V	.		20.183	1.4189	0.52	.Q	.	.	.	V	.
19.367	1.3818	0.58	.Q	.	.	.	V	.		20.200	1.4196	0.52	.Q	.	.	.	V	.
19.383	1.3826	0.58	.Q	.	.	.	V	.		20.217	1.4204	0.52	.Q	.	.	.	V	.
19.400	1.3834	0.58	.Q	.	.	.	V	.		20.233	1.4211	0.52	.Q	.	.	.	V	.
19.417	1.3842	0.58	.Q	.	.	.	V	.		20.250	1.4218	0.52	.Q	.	.	.	V	.
19.433	1.3850	0.58	.Q	.	.	.	V	.		20.267	1.4225	0.52	.Q	.	.	.	V	.
19.450	1.3858	0.58	.Q	.	.	.	V	.		20.283	1.4232	0.51	.Q	.	.	.	V	.
19.467	1.3866	0.58	.Q	.	.	.	V	.		20.300	1.4239	0.51	.Q	.	.	.	V	.
19.483	1.3874	0.57	.Q	.	.	.	V	.		20.317	1.4246	0.51	.Q	.	.	.	V	.
19.500	1.3882	0.57	.Q	.	.	.	V	.		20.333	1.4253	0.51	.Q	.	.	.	V	.
19.517	1.3890	0.57	.Q	.	.	.	V	.		20.350	1.4260	0.51	.Q	.	.	.	V	.
19.533	1.3897	0.57	.Q	.	.	.	V	.		20.367	1.4267	0.51	.Q	.	.	.	V	.
19.550	1.3905	0.57	.Q	.	.	.	V	.		20.383	1.4274	0.51	.Q	.	.	.	V	.
19.567	1.3913	0.57	.Q	.	.	.	V	.		20.400	1.4281	0.51	.Q	.	.	.	V	.
19.583	1.3921	0.57	.Q	.	.	.	V	.		20.417	1.4288	0.51	.Q	.	.	.	V	.
19.600	1.3929	0.56	.Q	.	.	.	V	.		20.433	1.4295	0.50	.Q	.	.	.	V	.
19.617	1.3936	0.56	.Q	.	.	.	V	.		20.450	1.4302	0.50	.Q	.	.	.	V	.
19.633	1.3944	0.56	.Q	.	.	.	V	.		20.467	1.4309	0.50	.Q	.	.	.	V	.
19.650	1.3952	0.56	.Q	.	.	.	V	.		20.483	1.4316	0.50	.Q	.	.	.	V	.
19.667	1.3959	0.56	.Q	.	.	.	V	.		20.500	1.4323	0.50	.Q	.	.	.	V	.
19.683	1.3967	0.56	.Q	.	.	.	V	.		20.517	1.4330	0.50	.Q	.	.	.	V	.
19.700	1.3975	0.56	.Q	.	.	.	V	.		20.533	1.4336	0.50	.Q	.	.	.	V	.
19.717	1.3982	0.55	.Q	.	.	.	V	.		20.550	1.4343	0.50	.Q	.	.	.	V	.
19.733	1.3990	0.55	.Q	.	.	.	V	.		20.567	1.4350	0.50	.Q	.	.	.	V	.
19.750	1.3998	0.55	.Q	.	.	.	V	.		20.583	1.4357	0.50	.Q	.	.	.	V	.
19.767	1.4005	0.55	.Q	.	.	.	V	.		20.600	1.4364	0.50	.Q	.	.	.	V	.
19.783	1.4013	0.55	.Q	.	.	.	V	.		20.617	1.4371	0.49	.Q	.	.	.	V	.
19.800	1.4020	0.55	.Q	.	.	.	V	.		20.633	1.4377	0.49	.Q	.	.	.	V	.
19.817	1.4028	0.55	.Q	.	.	.	V	.		20.650	1.4384	0.49	.Q	.	.	.	V	.
19.833	1.4035	0.55	.Q	.	.	.	V	.		20.667	1.4391	0.49	.Q	.	.	.	V	.
19.850	1.4043	0.54	.Q	.	.	.	V	.		20.683	1.4398	0.49	.Q	.	.	.	V	.
19.867	1.4050	0.54	.Q	.	.	.	V	.		20.700	1.4404	0.49	.Q	.	.	.	V	.
19.883	1.4058	0.54	.Q	.	.	.	V	.		20.717	1.4411	0.49	.Q	.	.	.	V	.
19.900	1.4065	0.54	.Q	.	.	.	V	.		20.733	1.4418	0.49	.Q	.	.	.	V	.
19.917	1.4073	0.54	.Q	.	.	.	V	.		20.750	1.4425	0.49	.Q	.	.	.	V	.
19.933	1.4080	0.54	.Q	.	.	.	V	.		20.767	1.4431	0.49	.Q	.	.	.	V	.
19.950	1.4087	0.54	.Q	.	.	.	V	.		20.783	1.4438	0.48	.Q	.	.	.	V	.
19.967	1.4095	0.54	.Q	.	.	.	V	.		20.800	1.4445	0.48	.Q	.	.	.	V	.
19.983	1.4102	0.53	.Q	.	.	.	V	.		20.817	1.4451	0.48	.Q	.	.	.	V	.
20.000	1.4110	0.53	.Q	.	.	.	V	.		20.833	1.4458	0.48	.Q	.	.	.	V	.
20.017	1.4117	0.53	.Q	.	.	.	V	.		20.850	1.4465	0.48	.Q	.	.	.	V	.
20.033	1.4124	0.53	.Q	.	.	.	V	.		20.867	1.4471	0.48	.Q	.	.	.	V	.

20.883	1.4478	0.48	Q	.	.	.	V	.		21.717	1.4794	0.44	Q	V	.
20.900	1.4484	0.48	Q	.	.	.	V	.		21.733	1.4800	0.44	Q	V	.
20.917	1.4491	0.48	Q	.	.	.	V	.		21.750	1.4806	0.44	Q	V	.
20.933	1.4498	0.48	Q	.	.	.	V	.		21.767	1.4812	0.44	Q	V	.
20.950	1.4504	0.48	Q	.	.	.	V	.		21.783	1.4818	0.44	Q	V	.
20.967	1.4511	0.48	Q	.	.	.	V	.		21.800	1.4825	0.44	Q	V	.
20.983	1.4517	0.47	Q	.	.	.	V	.		21.817	1.4831	0.44	Q	V	.
21.000	1.4524	0.47	Q	.	.	.	V	.		21.833	1.4837	0.44	Q	V	.
21.017	1.4530	0.47	Q	.	.	.	V	.		21.850	1.4843	0.44	Q	V	.
21.033	1.4537	0.47	Q	.	.	.	V	.		21.867	1.4849	0.44	Q	V	.
21.050	1.4543	0.47	Q	.	.	.	V	.		21.883	1.4855	0.44	Q	V	.
21.067	1.4550	0.47	Q	.	.	.	V	.		21.900	1.4861	0.43	Q	V	.
21.083	1.4556	0.47	Q	.	.	.	V	.		21.917	1.4867	0.43	Q	V	.
21.100	1.4563	0.47	Q	.	.	.	V	.		21.933	1.4872	0.43	Q	V	.
21.117	1.4569	0.47	Q	.	.	.	V	.		21.950	1.4878	0.43	Q	V	.
21.133	1.4576	0.47	Q	.	.	.	V	.		21.967	1.4884	0.43	Q	V	.
21.150	1.4582	0.47	Q	.	.	.	V	.		21.983	1.4890	0.43	Q	V	.
21.167	1.4588	0.47	Q	.	.	.	V	.		22.000	1.4896	0.43	Q	V	.
21.183	1.4595	0.46	Q	.	.	.	V	.		22.017	1.4902	0.43	Q	V	.
21.200	1.4601	0.46	Q	.	.	.	V	.		22.033	1.4908	0.43	Q	V	.
21.217	1.4608	0.46	Q	.	.	.	V	.		22.050	1.4914	0.43	Q	V	.
21.233	1.4614	0.46	Q	.	.	.	V	.		22.067	1.4920	0.43	Q	V	.
21.250	1.4620	0.46	Q	.	.	.	V	.		22.083	1.4926	0.43	Q	V	.
21.267	1.4627	0.46	Q	.	.	.	V	.		22.100	1.4932	0.43	Q	V	.
21.283	1.4633	0.46	Q	.	.	.	V	.		22.117	1.4938	0.43	Q	V	.
21.300	1.4639	0.46	Q	.	.	.	V	.		22.133	1.4943	0.43	Q	V	.
21.317	1.4646	0.46	Q	.	.	.	V	.		22.150	1.4949	0.43	Q	V	.
21.333	1.4652	0.46	Q	.	.	.	V	.		22.167	1.4955	0.42	Q	V	.
21.350	1.4658	0.46	Q	.	.	.	V	.		22.183	1.4961	0.42	Q	V	.
21.367	1.4664	0.46	Q	.	.	.	V	.		22.200	1.4967	0.42	Q	V	.
21.383	1.4671	0.46	Q	.	.	.	V	.		22.217	1.4973	0.42	Q	V	.
21.400	1.4677	0.45	Q	.	.	.	V	.		22.233	1.4978	0.42	Q	V	.
21.417	1.4683	0.45	Q	.	.	.	V	.		22.250	1.4984	0.42	Q	V	.
21.433	1.4690	0.45	Q	.	.	.	V	.		22.267	1.4990	0.42	Q	V	.
21.450	1.4696	0.45	Q	.	.	.	V	.		22.283	1.4996	0.42	Q	V	.
21.467	1.4702	0.45	Q	.	.	.	V	.		22.300	1.5002	0.42	Q	V	.
21.483	1.4708	0.45	Q	.	.	.	V	.		22.317	1.5007	0.42	Q	V	.
21.500	1.4714	0.45	Q	.	.	.	V	.		22.333	1.5013	0.42	Q	V	.
21.517	1.4721	0.45	Q	.	.	.	V	.		22.350	1.5019	0.42	Q	V	.
21.533	1.4727	0.45	Q	.	.	.	V	.		22.367	1.5025	0.42	Q	V	.
21.550	1.4733	0.45	Q	.	.	.	V	.		22.383	1.5030	0.42	Q	V	.
21.567	1.4739	0.45	Q	.	.	.	V	.		22.400	1.5036	0.42	Q	V	.
21.583	1.4745	0.45	Q	.	.	.	V	.		22.417	1.5042	0.42	Q	V	.
21.600	1.4751	0.45	Q	.	.	.	V	.		22.433	1.5048	0.42	Q	V	.
21.617	1.4758	0.45	Q	.	.	.	V	.		22.450	1.5053	0.41	Q	V	.
21.633	1.4764	0.44	Q	.	.	.	V	.		22.467	1.5059	0.41	Q	V	.
21.650	1.4770	0.44	Q	.	.	.	V	.		22.483	1.5065	0.41	Q	V	.
21.667	1.4776	0.44	Q	.	.	.	V	.		22.500	1.5070	0.41	Q	V	.
21.683	1.4782	0.44	Q	.	.	.	V	.		22.517	1.5076	0.41	Q	V	.
21.700	1.4788	0.44	Q	.	.	.	V	.		22.533	1.5082	0.41	Q	V	.

22.550	1.5087	0.41	Q	.	.	.	V.		23.383	1.5362	0.39	Q	.	.	.	V.
22.567	1.5093	0.41	Q	.	.	.	V.		23.400	1.5367	0.39	Q	.	.	.	V.
22.583	1.5099	0.41	Q	.	.	.	V.		23.417	1.5372	0.39	Q	.	.	.	V.
22.600	1.5104	0.41	Q	.	.	.	V.		23.433	1.5378	0.39	Q	.	.	.	V.
22.617	1.5110	0.41	Q	.	.	.	V.		23.450	1.5383	0.38	Q	.	.	.	V.
22.633	1.5116	0.41	Q	.	.	.	V.		23.467	1.5388	0.38	Q	.	.	.	V.
22.650	1.5121	0.41	Q	.	.	.	V.		23.483	1.5393	0.38	Q	.	.	.	V.
22.667	1.5127	0.41	Q	.	.	.	V.		23.500	1.5399	0.38	Q	.	.	.	V.
22.683	1.5132	0.41	Q	.	.	.	V.		23.517	1.5404	0.38	Q	.	.	.	V.
22.700	1.5138	0.41	Q	.	.	.	V.		23.533	1.5409	0.38	Q	.	.	.	V.
22.717	1.5144	0.41	Q	.	.	.	V.		23.550	1.5415	0.38	Q	.	.	.	V.
22.733	1.5149	0.41	Q	.	.	.	V.		23.567	1.5420	0.38	Q	.	.	.	V.
22.750	1.5155	0.40	Q	.	.	.	V.		23.583	1.5425	0.38	Q	.	.	.	V.
22.767	1.5160	0.40	Q	.	.	.	V.		23.600	1.5430	0.38	Q	.	.	.	V.
22.783	1.5166	0.40	Q	.	.	.	V.		23.617	1.5436	0.38	Q	.	.	.	V.
22.800	1.5171	0.40	Q	.	.	.	V.		23.633	1.5441	0.38	Q	.	.	.	V.
22.817	1.5177	0.40	Q	.	.	.	V.		23.650	1.5446	0.38	Q	.	.	.	V.
22.833	1.5183	0.40	Q	.	.	.	V.		23.667	1.5451	0.38	Q	.	.	.	V.
22.850	1.5188	0.40	Q	.	.	.	V.		23.683	1.5456	0.38	Q	.	.	.	V.
22.867	1.5194	0.40	Q	.	.	.	V.		23.700	1.5462	0.38	Q	.	.	.	V.
22.883	1.5199	0.40	Q	.	.	.	V.		23.717	1.5467	0.38	Q	.	.	.	V.
22.900	1.5205	0.40	Q	.	.	.	V.		23.733	1.5472	0.38	Q	.	.	.	V.
22.917	1.5210	0.40	Q	.	.	.	V.		23.750	1.5477	0.38	Q	.	.	.	V.
22.933	1.5216	0.40	Q	.	.	.	V.		23.767	1.5482	0.38	Q	.	.	.	V.
22.950	1.5221	0.40	Q	.	.	.	V.		23.783	1.5488	0.38	Q	.	.	.	V.
22.967	1.5227	0.40	Q	.	.	.	V.		23.800	1.5493	0.38	Q	.	.	.	V.
22.983	1.5232	0.40	Q	.	.	.	V.		23.817	1.5498	0.38	Q	.	.	.	V.
23.000	1.5238	0.40	Q	.	.	.	V.		23.833	1.5503	0.37	Q	.	.	.	V.
23.017	1.5243	0.40	Q	.	.	.	V.		23.850	1.5508	0.37	Q	.	.	.	V.
23.033	1.5249	0.40	Q	.	.	.	V.		23.867	1.5513	0.37	Q	.	.	.	V.
23.050	1.5254	0.40	Q	.	.	.	V.		23.883	1.5519	0.37	Q	.	.	.	V.
23.067	1.5259	0.40	Q	.	.	.	V.		23.900	1.5524	0.37	Q	.	.	.	V.
23.083	1.5265	0.39	Q	.	.	.	V.		23.917	1.5529	0.37	Q	.	.	.	V.
23.100	1.5270	0.39	Q	.	.	.	V.		23.933	1.5534	0.37	Q	.	.	.	V.
23.117	1.5276	0.39	Q	.	.	.	V.		23.950	1.5539	0.37	Q	.	.	.	V.
23.133	1.5281	0.39	Q	.	.	.	V.		23.967	1.5544	0.37	Q	.	.	.	V.
23.150	1.5287	0.39	Q	.	.	.	V.		23.983	1.5549	0.37	Q	.	.	.	V.
23.167	1.5292	0.39	Q	.	.	.	V.		24.000	1.5554	0.37	Q	.	.	.	V.
23.183	1.5297	0.39	Q	.	.	.	V.									
23.200	1.5303	0.39	Q	.	.	.	V.									
23.217	1.5308	0.39	Q	.	.	.	V.									
23.233	1.5313	0.39	Q	.	.	.	V.									
23.250	1.5319	0.39	Q	.	.	.	V.									
23.267	1.5324	0.39	Q	.	.	.	V.									
23.283	1.5330	0.39	Q	.	.	.	V.									
23.300	1.5335	0.39	Q	.	.	.	V.									
23.317	1.5340	0.39	Q	.	.	.	V.									
23.333	1.5346	0.39	Q	.	.	.	V.									
23.350	1.5351	0.39	Q	.	.	.	V.									
23.367	1.5356	0.39	Q	.	.	.	V.									

TIME DURATION(minutes) OF PERCENTILES OF ESTIMATED PEAK FLOW RATE:

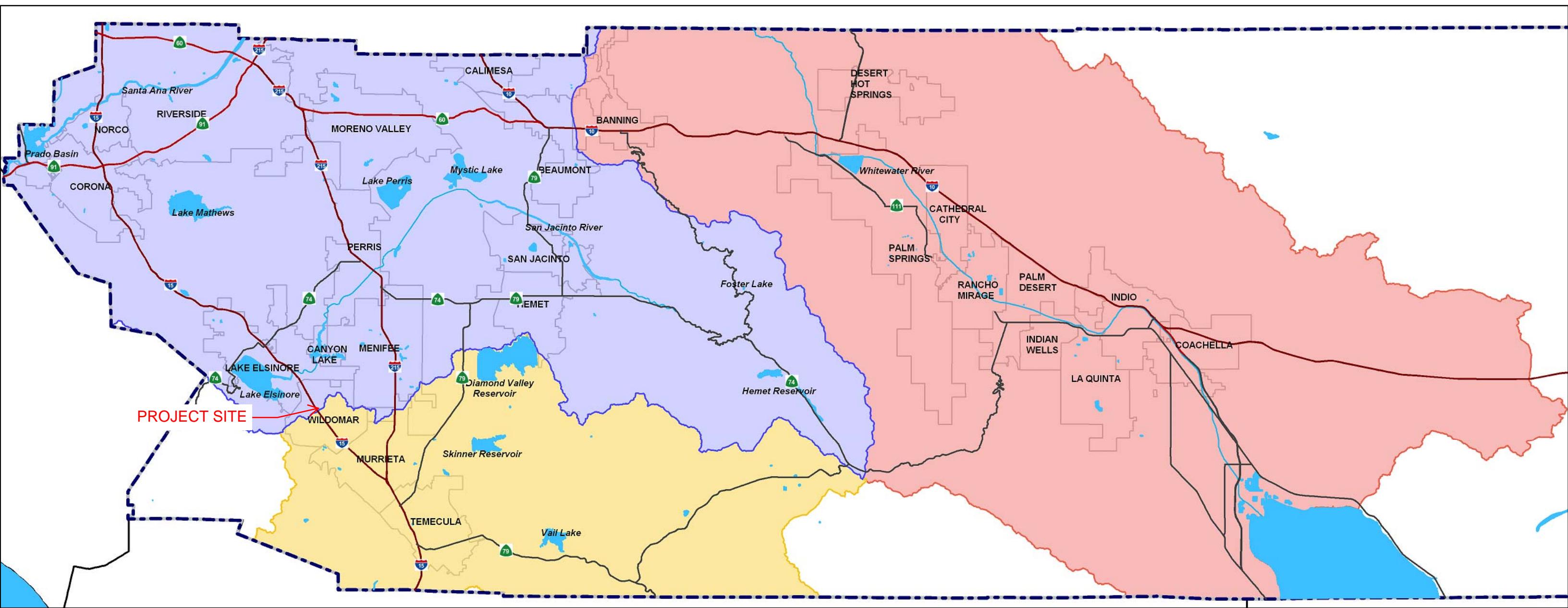
(Note: 100% of Peak Flow Rate estimate assumed to have
an instantaneous time duration)

Percentile of Estimated Peak Flow Rate	Duration (minutes)
0%	1441.0
10%	655.0
20%	290.0
30%	185.0

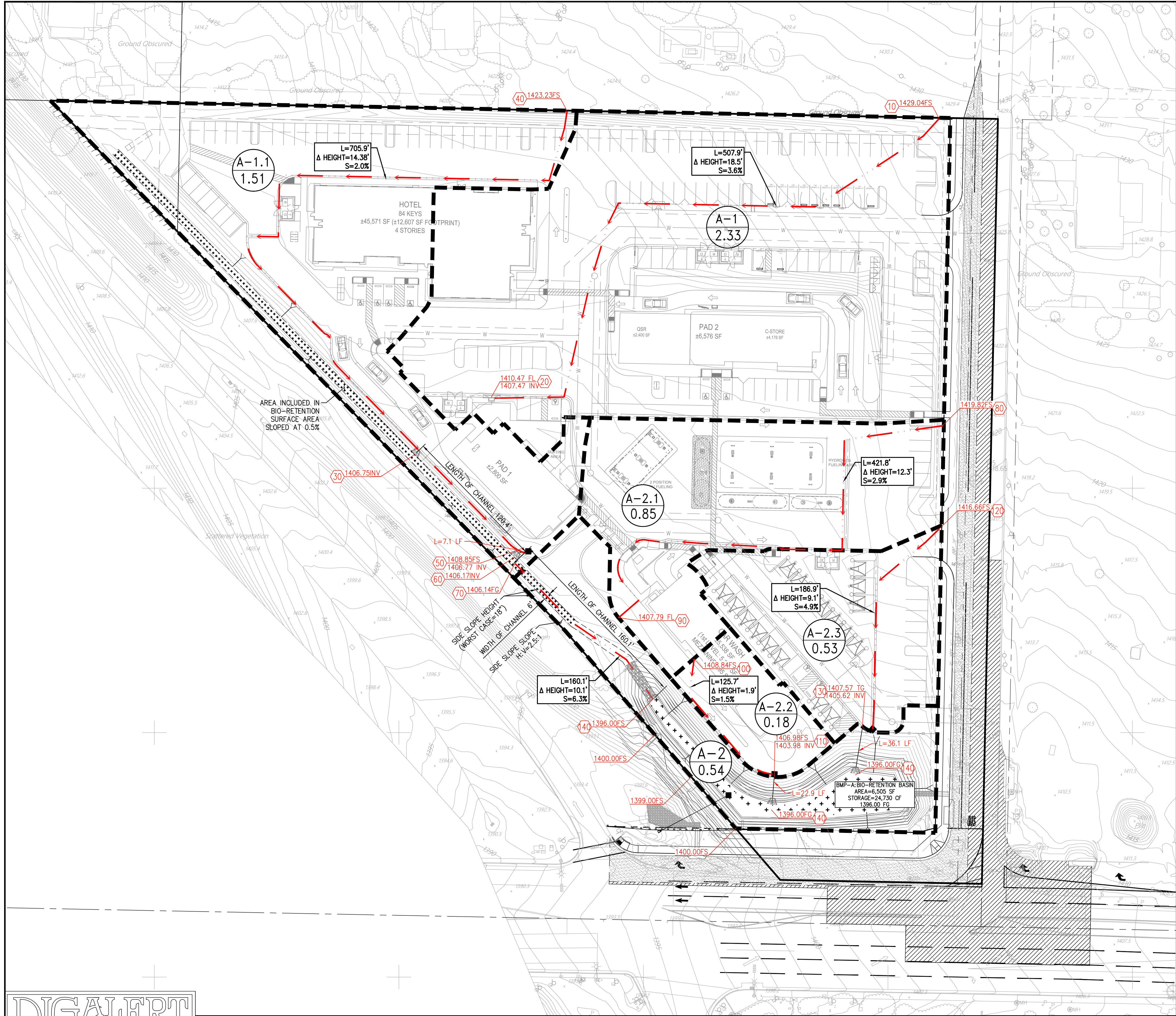
40%	110.0
50%	95.0
60%	75.0
70%	55.0
80%	35.0
90%	20.0

END OF FLOODSCx ROUTING ANALYSIS

Appendix D – Watershed Map



Appendix E – Proposed Hydrology Calculations



LEGEND:

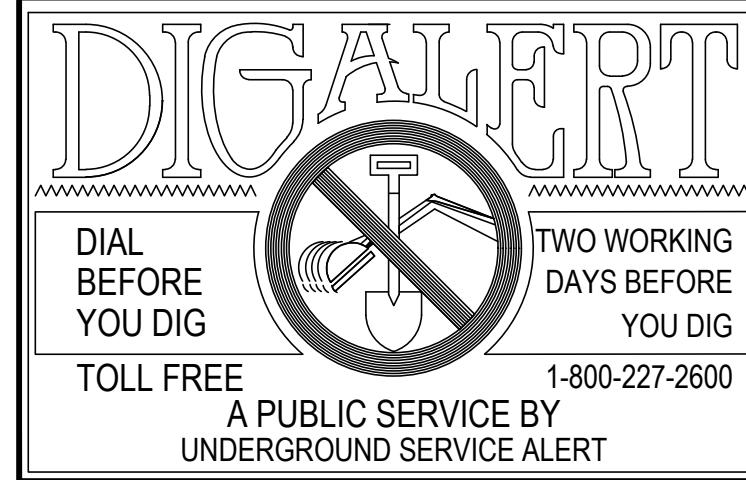
	FLOWLINE
	EXISTING CONTOUR
	PROPOSED CONTOUR
	DRAINAGE SUB-AREA BOUNDARY
	AREA ID
	AREA (AC)
	NODE #
	FINISHED SURFACE
	INVERT

DETENTION BASIN SUMMARY

BMP #	EXISTING PEAK FLOW 100-YR STORM (CFS)	PROPOSED PEAK FLOW 100-YR STORM (CFS)	MITIGATED PEAK FLOW 100-YR STORM (CFS)	DESIGN STORAGE VOLUME (CF)
BMP-A	8.01	13.15	5.20	24,730

N

0 40' 80'
SCALE: 1" = 40'



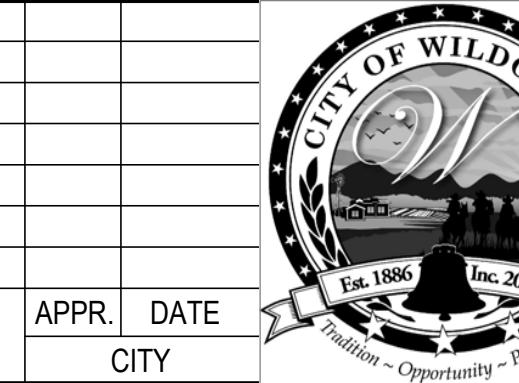
NOTE:
WORK CONTAINED WITHIN THESE PLANS SHALL NOT
COMMENCE UNTIL AN ENCROACHMENT PERMIT
AND/OR A GRADING PERMIT HAS BEEN ISSUED.

The private engineer signing these plans is responsible for assuring
the accuracy and acceptability of the design hereon. In the event of
discrepancies arising after city acceptance or during construction,
the private engineer shall be responsible for determining an
acceptable solution and revising the plans for acceptance by the city.

MARK BY DATE
ENGINEER

REVISIONS

APPR. DATE
CITY



Since 1964

TAIT

& ASSOCIATES

Engineering Environmental Building Land

Orange County Sacramento Riverside Denver

San Luis Obispo Riverside Boise Dallas Atlanta

1407.5

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(PP, CUP, PM, TM, etc.) (city project number)
CITY OF WILDOMAR
PROPOSED HYDROLOGY MAP
CHERRY OUTPOST IN THE
CITY OF WILDOMAR, RIVERSIDE COUNTY

SHEET No.
1
OF 1 SHTS

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM BASED ON
RIVERSIDE COUNTY FLOOD CONTROL & WATER CONSERVATION DISTRICT
(RCFC&WCD) 1978 HYDROLOGY MANUAL
(c) Copyright 1982-2016 Advanced Engineering Software (aes)
(Rational Tabling Version 23.0)
Release Date: 07/01/2016 License ID 1334

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* SP8997 - WILDOMAR CHERRY OUTPOST *
* PROPOSED CONDITION RATIONAL METHOD *
* 100-YEAR STORM EVENT *

FILE NAME: 100YRPR.DAT
TIME/DATE OF STUDY: 15:04 04/30/2024

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 6.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.01
10-YEAR STORM 10-MINUTE INTENSITY(INCH/HOUR) = 1.600
10-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 0.786
100-YEAR STORM 10-MINUTE INTENSITY(INCH/HOUR) = 2.680
100-YEAR STORM 60-MINUTE INTENSITY(INCH/HOUR) = 1.310
SLOPE OF 10-YEAR INTENSITY-DURATION CURVE = 0.3967061
SLOPE OF 100-YEAR INTENSITY-DURATION CURVE = 0.3994898

COMPUTED RAINFALL INTENSITY DATA:
STORM EVENT = 100.00 1-HOUR INTENSITY(INCH/HOUR) = 1.310
SLOPE OF INTENSITY DURATION CURVE = 0.3995

RCFC&WCD HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: COMPUTE CONFLUENCE VALUES ACCORDING TO RCFC&WCD HYDROLOGY MANUAL
AND IGNORE OTHER CONFLUENCE COMBINATIONS FOR DOWNSTREAM ANALYSES

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL
HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING
WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (n)
1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

FLOW PROCESS FROM NODE 10.00 TO NODE 20.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 507.90
UPSTREAM ELEVATION(FEET) = 1429.00
DOWNSTREAM ELEVATION(FEET) = 1410.47
ELEVATION DIFFERENCE(FEET) = 18.53
TC = 0.303*[(507.90**3)/(18.53)]**.2 = 7.104
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.072
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8568
SOIL CLASSIFICATION IS "A"
SUBAREA RUNOFF(CFS) = 4.05
TOTAL AREA(ACRES) = 1.54 TOTAL RUNOFF(CFS) = 4.05

FLOW PROCESS FROM NODE 20.00 TO NODE 20.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.072
UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .4682
SOIL CLASSIFICATION IS "A"
SUBAREA AREA(ACRES) = 0.34 SUBAREA RUNOFF(CFS) = 0.49
TOTAL AREA(ACRES) = 1.9 TOTAL RUNOFF(CFS) = 4.54
TC(MIN.) = 7.10

FLOW PROCESS FROM NODE 20.00 TO NODE 20.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.072
UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .7532
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.02
TOTAL AREA(ACRES) = 1.9 TOTAL RUNOFF(CFS) = 4.57
TC(MIN.) = 7.10

FLOW PROCESS FROM NODE 20.00 TO NODE 20.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.072
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8853
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.29 SUBAREA RUNOFF(CFS) = 0.79
TOTAL AREA(ACRES) = 2.2 TOTAL RUNOFF(CFS) = 5.35
TC(MIN.) = 7.10

FLOW PROCESS FROM NODE 20.00 TO NODE 30.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 1407.47 DOWNSTREAM(FEET) = 1406.75

FLOW LENGTH(FEET) = 129.70 MANNING'S N = 0.013
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 27.9 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 0.91
 ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 5.35
 PIPE TRAVEL TIME(MIN.) = 2.37 Tc(MIN.) = 9.47
 LONGEST FLOWPATH FROM NODE 10.00 TO NODE 30.00 = 637.60 FEET.

FLOW PROCESS FROM NODE 30.00 TO NODE 60.00 IS CODE = 51

>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<
>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 1406.75 DOWNSTREAM(FEET) = 1406.17
CHANNEL LENGTH THRU SUBAREA(FEET) = 120.40 CHANNEL SLOPE = 0.0048
CHANNEL BASE(FEET) = 6.00 "Z" FACTOR = 2.500
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00
CHANNEL FLOW THRU SUBAREA(CFS) = 5.35
FLOW VELOCITY(FEET/SEC.) = 1.76 FLOW DEPTH(FEET) = 0.43
TRAVEL TIME(MIN.) = 1.14 Tc(MIN.) = 10.61
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 60.00 = 758.00 FEET.

FLOW PROCESS FROM NODE 60.00 TO NODE 60.00 IS CODE = 1

>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.61
RAINFALL INTENSITY(INCH/HR) = 2.62
TOTAL STREAM AREA(ACRES) = 2.18
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.35

FLOW PROCESS FROM NODE 40.00 TO NODE 50.00 IS CODE = 21

>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<

=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 705.90
UPSTREAM ELEVATION(FEET) = 1423.23
DOWNSTREAM ELEVATION(FEET) = 1408.85
ELEVATION DIFFERENCE(FEET) = 14.38
TC = 0.303*[(705.90**3)/(- 14.38)]**.2 = 9.105
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.782
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8546
SOIL CLASSIFICATION IS "A"
SUBAREA RUNOFF(CFS) = 1.60
TOTAL AREA(ACRES) = 0.67 TOTAL RUNOFF(CFS) = 1.60

FLOW PROCESS FROM NODE 50.00 TO NODE 50.00 IS CODE = 81

>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.782
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8841
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.33 SUBAREA RUNOFF(CFS) = 0.80
TOTAL AREA(ACRES) = 1.0 TOTAL RUNOFF(CFS) = 2.40
Tc(MIN.) = 9.11

FLOW PROCESS FROM NODE 50.00 TO NODE 50.00 IS CODE = 81

>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.782
UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .4459
SOIL CLASSIFICATION IS "A"
SUBAREA AREA(ACRES) = 0.33 SUBAREA RUNOFF(CFS) = 0.41
TOTAL AREA(ACRES) = 1.3 TOTAL RUNOFF(CFS) = 2.81
Tc(MIN.) = 9.11

FLOW PROCESS FROM NODE 50.00 TO NODE 50.00 IS CODE = 81

>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<

=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.782
UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .7406
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.25 SUBAREA RUNOFF(CFS) = 0.52
TOTAL AREA(ACRES) = 1.6 TOTAL RUNOFF(CFS) = 3.33
Tc(MIN.) = 9.11

FLOW PROCESS FROM NODE 50.00 TO NODE 60.00 IS CODE = 31

>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<

>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 1406.77 DOWNSTREAM(FEET) = 1406.17
FLOW LENGTH(FEET) = 7.10 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.24
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 3.33
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 9.16
LONGEST FLOWPATH FROM NODE 40.00 TO NODE 60.00 = 713.00 FEET.

FLOW PROCESS FROM NODE 60.00 TO NODE 60.00 IS CODE = 1

>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<

>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 9.16
RAINFALL INTENSITY(INCH/HR) = 2.78
TOTAL STREAM AREA(ACRES) = 1.58
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.33

** CONFLUENCE DATA **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	5.35	10.61	2.617	2.18
2	3.33	9.16	2.776	1.58

*****WARNING*****
 IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED
 ON THE RCFC&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA
 WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	7.95	9.16	2.776
2	8.50	10.61	2.617

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE(CFS) = 8.50 Tc(MIN.) = 10.61
 TOTAL AREA(ACRES) = 3.8
 LONGEST FLOWPATH FROM NODE 10.00 TO NODE 60.00 = 758.00 FEET.

 FLOW PROCESS FROM NODE 60.00 TO NODE 140.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 1406.14 DOWNSTREAM(FEET) = 1396.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 160.10 CHANNEL SLOPE = 0.0633
 CHANNEL BASE(FEET) = 6.00 "Z" FACTOR = 3.000
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.50
 CHANNEL FLOW THRU SUBAREA(CFS) = 8.50
 FLOW VELOCITY(FEET/SEC.) = 4.74 FLOW DEPTH(FEET) = 0.26
 TRAVEL TIME(MIN.) = 0.56 Tc(MIN.) = 11.18
 LONGEST FLOWPATH FROM NODE 10.00 TO NODE 140.00 = 918.10 FEET.

 FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 5
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION(MIN.) = 11.18
 RAINFALL INTENSITY(INCH/HR) = 2.56
 TOTAL STREAM AREA(ACRES) = 3.76
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.50

 FLOW PROCESS FROM NODE 70.00 TO NODE 140.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

ASSUMED INITIAL SUBAREA UNIFORM

DEVELOPMENT IS: UNDEVELOPED WITH FAIR COVER
 $TC = K^*[(LENGTH^{**3})/(ELEVATION CHANGE)]^{**.2}$
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 160.10
 UPSTREAM ELEVATION(FEET) = 1406.14
 DOWNSTREAM ELEVATION(FEET) = 1396.00
 ELEVATION DIFFERENCE(FEET) = 10.14
 $TC = 0.709[(160.10^{**3})/(10.14)]^{**.2} = 9.382$
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.749
 UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .7390
 SOIL CLASSIFICATION IS "C"
 SUBAREA RUNOFF(CFS) = 0.88
 TOTAL AREA(ACRES) = 0.43 TOTAL RUNOFF(CFS) = 0.88

 FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.749
 UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .4432
 SOIL CLASSIFICATION IS "A"
 SUBAREA AREA(ACRES) = 0.11 SUBAREA RUNOFF(CFS) = 0.13
 TOTAL AREA(ACRES) = 0.5 TOTAL RUNOFF(CFS) = 1.01
 TC(MIN.) = 9.38

 FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 5
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 9.38
 RAINFALL INTENSITY(INCH/HR) = 2.75
 TOTAL STREAM AREA(ACRES) = 0.54
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.01

 FLOW PROCESS FROM NODE 80.00 TO NODE 90.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

ASSUMED INITIAL SUBAREA UNIFORM
 DEVELOPMENT IS COMMERCIAL
 $TC = K^*[(LENGTH^{**3})/(ELEVATION CHANGE)]^{**.2}$
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 423.50
 UPSTREAM ELEVATION(FEET) = 1420.08
 DOWNSTREAM ELEVATION(FEET) = 1407.79
 ELEVATION DIFFERENCE(FEET) = 12.29
 $TC = 0.303[(423.50^{**3})/(12.29)]^{**.2} = 6.915$
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.106
 COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8854
 SOIL CLASSIFICATION IS "C"
 SUBAREA RUNOFF(CFS) = 1.96
 TOTAL AREA(ACRES) = 0.71 TOTAL RUNOFF(CFS) = 1.96

 FLOW PROCESS FROM NODE 90.00 TO NODE 90.00 IS CODE = 81

```

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.106
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8571
SOIL CLASSIFICATION IS "A"
SUBAREA AREA(ACRES) = 0.16 SUBAREA RUNOFF(CFS) = 0.42
TOTAL AREA(ACRES) = 0.9 TOTAL RUNOFF(CFS) = 2.38
TC(MIN.) = 6.91

*****FLOW PROCESS FROM NODE 90.00 TO NODE 90.00 IS CODE = 81
----->>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.106
UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .4706
SOIL CLASSIFICATION IS "A"
SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.01
TOTAL AREA(ACRES) = 0.9 TOTAL RUNOFF(CFS) = 2.39
TC(MIN.) = 6.91

*****FLOW PROCESS FROM NODE 90.00 TO NODE 90.00 IS CODE = 81
----->>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.106
UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .7545
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.04
TOTAL AREA(ACRES) = 0.9 TOTAL RUNOFF(CFS) = 2.42
TC(MIN.) = 6.91

*****FLOW PROCESS FROM NODE 90.00 TO NODE 140.00 IS CODE = 51
----->>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1406.14 DOWNSTREAM(FEET) = 1396.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 150.08 CHANNEL SLOPE = 0.0676
CHANNEL BASE(FEET) = 6.00 "Z" FACTOR = 3.000
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.50
CHANNEL FLOW THRU SUBAREA(CFS) = 2.42
FLOW VELOCITY(FEET/SEC.) = 3.04 FLOW DEPTH(FEET) = 0.12
TRAVEL TIME(MIN.) = 0.82 Tc(MIN.) = 7.74
LONGEST FLOWPATH FROM NODE 80.00 TO NODE 140.00 = 573.58 FEET.

*****FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 1
----->>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 5
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 7.74
RAINFALL INTENSITY(INCH/HR) = 2.97
TOTAL STREAM AREA(ACRES) = 0.89
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.42

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*****FLOW PROCESS FROM NODE 100.00 TO NODE 110.00 IS CODE = 21
----->>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 125.70
UPSTREAM ELEVATION(FEET) = 1408.84
DOWNSTREAM ELEVATION(FEET) = 1406.98
ELEVATION DIFFERENCE(FEET) = 1.86
TC = 0.303*[( 125.70**3)/(- 1.86)]**.2 = 4.867
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.535
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8600
SOIL CLASSIFICATION IS "A"
SUBAREA RUNOFF(CFS) = 0.29
TOTAL AREA(ACRES) = 0.10 TOTAL RUNOFF(CFS) = 0.29

*****FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 81
----->>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.535
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8870
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.20
TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.49
TC(MIN.) = 5.00

*****FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 81
----->>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.535
UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .4996
SOIL CLASSIFICATION IS "A"
SUBAREA AREA(ACRES) = 0.03 SUBAREA RUNOFF(CFS) = 0.04
TOTAL AREA(ACRES) = 0.2 TOTAL RUNOFF(CFS) = 0.54
TC(MIN.) = 5.00

*****FLOW PROCESS FROM NODE 110.00 TO NODE 140.00 IS CODE = 31
----->>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 1403.98 DOWNSTREAM(FEET) = 1396.00
FLOW LENGTH(FEET) = 22.90 MANNING'S N = 0.013
DEPTH OF FLOW IN 9.0 INCH PIPE IS 4.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.50
ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.54
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 5.15
LONGEST FLOWPATH FROM NODE 100.00 TO NODE 140.00 = 148.60 FEET.

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***** FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 1
----->>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====TOTAL NUMBER OF STREAMS = 5
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 4 ARE:
TIME OF CONCENTRATION(MIN.) = 5.15
RAINFALL INTENSITY(INCH/HOUR) = 3.49
TOTAL STREAM AREA(ACRES) = 0.19
PEAK FLOW RATE(CFS) AT CONFLUENCE = 0.54
***** FLOW PROCESS FROM NODE 120.00 TO NODE 130.00 IS CODE = 21
----->>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====ASSUMED INITIAL SUBAREA UNIFORM
DEVELOPMENT IS COMMERCIAL
TC = K*[(LENGTH**3)/(ELEVATION CHANGE)]**.2
INITIAL SUBAREA FLOW-LENGTH(FEET) = 186.90
UPSTREAM ELEVATION(FEET) = 1416.64
DOWNSTREAM ELEVATION(FEET) = 1407.59
ELEVATION DIFFERENCE(FEET) = 9.05
TC = 0.303*[( 186.90**3)/(- 9.05)]**.2 = 4.500
COMPUTED TIME OF CONCENTRATION INCREASED TO 5 MIN.
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.535
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8870
SOIL CLASSIFICATION IS "C"
SUBAREA RUNOFF(CFS) = 0.90
TOTAL AREA(ACRES) = 0.29 TOTAL RUNOFF(CFS) = 0.90
***** FLOW PROCESS FROM NODE 130.00 TO NODE 130.00 IS CODE = 81
----->>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.535
COMMERCIAL DEVELOPMENT RUNOFF COEFFICIENT = .8600
SOIL CLASSIFICATION IS "A"
SUBAREA AREA(ACRES) = 0.17 SUBAREA RUNOFF(CFS) = 0.50
TOTAL AREA(ACRES) = 0.5 TOTAL RUNOFF(CFS) = 1.40
TC(MIN.) = 5.00
***** FLOW PROCESS FROM NODE 130.00 TO NODE 130.00 IS CODE = 81
----->>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.535
UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .4996
SOIL CLASSIFICATION IS "A"
SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.11
TOTAL AREA(ACRES) = 0.5 TOTAL RUNOFF(CFS) = 1.52
TC(MIN.) = 5.00
***** FLOW PROCESS FROM NODE 130.00 TO NODE 130.00 IS CODE = 81

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----->>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 3.535
UNDEVELOPED WATERSHED RUNOFF COEFFICIENT = .7696
SOIL CLASSIFICATION IS "C"
SUBAREA AREA(ACRES) = 0.06 SUBAREA RUNOFF(CFS) = 0.16
TOTAL AREA(ACRES) = 0.6 TOTAL RUNOFF(CFS) = 1.68
TC(MIN.) = 5.00
***** FLOW PROCESS FROM NODE 130.00 TO NODE 140.00 IS CODE = 31
----->>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====ELEVATION DATA: UPSTREAM(FEET) = 1405.62 DOWNSTREAM(FEET) = 1396.00
FLOW LENGTH(FEET) = 30.20 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 3.19
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.68
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 5.16
LONGEST FLOWPATH FROM NODE 120.00 TO NODE 140.00 = 217.10 FEET.
***** FLOW PROCESS FROM NODE 140.00 TO NODE 140.00 IS CODE = 1
----->>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====TOTAL NUMBER OF STREAMS = 5
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 5 ARE:
TIME OF CONCENTRATION(MIN.) = 5.16
RAINFALL INTENSITY(INCH/HOUR) = 3.49
TOTAL STREAM AREA(ACRES) = 0.58
PEAK FLOW RATE(CFS) AT CONFLUENCE = 1.68
** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 8.50 11.18 2.563 3.76
2 1.01 9.38 2.749 0.54
3 2.42 7.74 2.969 0.89
4 0.54 5.15 3.493 0.19
5 1.68 5.16 3.491 0.58
*****WARNING***** IN THIS COMPUTER PROGRAM, THE CONFLUENCE VALUE USED IS BASED
ON THE RCF&WCD FORMULA OF PLATE D-1 AS DEFAULT VALUE. THIS FORMULA
WILL NOT NECESSARILY RESULT IN THE MAXIMUM VALUE OF PEAK FLOW.
***** RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 5 STREAMS.
** PEAK FLOW RATE TABLE **
STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)

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1	8.30	5.15	3.493
2	8.30	5.16	3.491
3	11.02	7.74	2.969
4	12.13	9.38	2.749
5	13.15	11.18	2.563

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 13.15 Tc(MIN.) = 11.18

TOTAL AREA(ACRES) = 6.0

LONGEST FLOWPATH FROM NODE 10.00 TO NODE 140.00 = 918.10 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 6.0 TC(MIN.) = 11.18

PEAK FLOW RATE(CFS) = 13.15

=====

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END OF RATIONAL METHOD ANALYSIS

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Appendix F – Basin Calculations

Cherry Outpost																
(Existing Condition) Small Area Hydrograph Loss Rates																
Subarea	Area (acres)	Soil Type	Land Use	A_p	A_i	F_p (in/hr) Adj. Infiltration Rate	F_m	Runoff Index (RI)			\bar{y}					
								Storm Event - Year								
								100								
								AMC								
								P_{24} (Inches)		5.87						
A-1		3.60		A		Open Brush (P)		II		I						
A-1		2.24		C		Open Brush (P)		62		42						
A-1		0.02		A		Commercial		84		68						
A-1		0.21		C		Commercial		32		16						
Total =		6.07						69		50						
								84		79						
										1.23						
										1.93						
										0.02						
										0.20						
										0.445						

Cherry Outpost	
(Existing Condition) Loss Rates Summary	
	STORM EVENT
	100-YR
Tc =	12.91
Area =	6.07
\bar{y} =	0.445
F_m =	0.467

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*****
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F L O O D R O U T I N G A N A L Y S I S
USING COUNTY HYDROLOGY MANUAL OF ORANGE(1986)
(c) Copyright 1989-2016 Advanced Engineering Software (aes)
Ver. 23.0 Release Date: 07/01/2016 License ID 1334

Analysis prepared by:

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***** DESCRIPTION OF STUDY *****
```

* CHERRY OUTPOST *
* 100 YR - EXISTING CONDITION *
* SMALL AREA UNIT HYDROGRAPH *

FILE NAME: 100YREXH.DAT

TIME/DATE OF STUDY: 07:41 01/16/2024

The Small Area Unit Hydrograph Procedures in Section J of the Hydrology Manual provides estimates of runoff hydrograph and runoff volume for watersheds whose time of concentration is less than 25 minutes. The PROGRAM User should check the applicability of using the small area unit hydrograph procedures, and follow the guidelines in Sections J and K.5 in complex watershed modeling.

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FLOW PROCESS FROM NODE 10.00 TO NODE 20.00 IS CODE = 1.2

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>>>>SUBAREA RUNOFF (SMALL AREA UNIT-HYDROGRAPH ANALYSIS) <<<<

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(SMALL AREA UNIT-HYDROGRAPH ADDED TO STREAM #1)

RATIONAL METHOD CALIBRATION COEFFICIENT = 0.90
TOTAL CATCHMENT AREA(ACRES) = 6.07
SOIL-LOSS RATE, Fm,(INCH/HR) = 0.467
LOW LOSS FRACTION = 0.445
TIME OF CONCENTRATION(MIN.) = 12.91
SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA
USER SPECIFIED RAINFALL VALUES ARE USED:
RETURN FREQUENCY(YEARS) = 100
5-MINUTE POINT RAINFALL VALUE(INCHES) = 0.31

30-MINUTE POINT RAINFALL VALUE(INCHES) = 0.85
 1-HOUR POINT RAINFALL VALUE(INCHES) = 1.31
 3-HOUR POINT RAINFALL VALUE(INCHES) = 2.13
 6-HOUR POINT RAINFALL VALUE(INCHES) = 2.96
 24-HOUR POINT RAINFALL VALUE(INCHES) = 5.87

TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 1.54
 TOTAL CATCHMENT SOIL-LOSS VOLUME(ACRE-FEET) = 1.43

↑

2 4 - H O U R S T O R M
 R U N O F F H Y D R O G R A P H

HYDROGRAPH IN ONE-MINUTE UNIT INTERVALS(CFS)

(Notes: Time indicated is at END of Each Unit Intervals.
 Peak 5-minute rainfall intensity is modeled as
 a constant value for entire 5-minute period.)

TIME(HRS)	VOLUME(AF)	Q(CFS)	0.	2.7	5.4	8.2	10.9
0.017	0.0000	0.00	Q
0.033	0.0000	0.00	Q
0.050	0.0000	0.00	Q
0.067	0.0000	0.00	Q
0.083	0.0000	0.00	Q
0.100	0.0000	0.02	Q
0.117	0.0001	0.05	Q
0.133	0.0002	0.08	Q
0.150	0.0004	0.11	Q
0.167	0.0006	0.14	Q
0.183	0.0008	0.17	Q
0.200	0.0011	0.19	Q
0.217	0.0014	0.22	Q
0.233	0.0017	0.25	Q
0.250	0.0021	0.28	VQ
0.267	0.0025	0.31	VQ
0.283	0.0030	0.34	VQ
0.300	0.0035	0.36	VQ
0.317	0.0040	0.37	VQ
0.333	0.0045	0.37	VQ
0.350	0.0050	0.37	VQ
0.367	0.0055	0.37	VQ
0.383	0.0060	0.37	VQ
0.400	0.0065	0.37	VQ
0.417	0.0070	0.37	VQ

0.433	0.0076	0.37	VQ
0.450	0.0081	0.37	VQ
0.467	0.0086	0.37	VQ
0.483	0.0091	0.37	VQ
0.500	0.0096	0.37	VQ
0.517	0.0101	0.37	VQ
0.533	0.0106	0.37	VQ
0.550	0.0111	0.37	VQ
0.567	0.0116	0.37	VQ
0.583	0.0121	0.37	VQ
0.600	0.0126	0.37	VQ
0.617	0.0132	0.37	VQ
0.633	0.0137	0.37	VQ
0.650	0.0142	0.37	VQ
0.667	0.0147	0.37	VQ
0.683	0.0152	0.37	VQ
0.700	0.0157	0.37	VQ
0.717	0.0162	0.37	VQ
0.733	0.0167	0.37	VQ
0.750	0.0173	0.37	VQ
0.767	0.0178	0.37	VQ
0.783	0.0183	0.37	VQ
0.800	0.0188	0.37	VQ
0.817	0.0193	0.37	VQ
0.833	0.0198	0.37	VQ
0.850	0.0204	0.37	VQ
0.867	0.0209	0.37	VQ
0.883	0.0214	0.37	VQ
0.900	0.0219	0.37	VQ
0.917	0.0224	0.37	VQ
0.933	0.0229	0.37	VQ
0.950	0.0234	0.37	VQ
0.967	0.0240	0.38	VQ
0.983	0.0245	0.38	VQ
1.000	0.0250	0.38	VQ
1.017	0.0255	0.38	VQ
1.033	0.0260	0.38	VQ
1.050	0.0266	0.38	VQ
1.067	0.0271	0.38	VQ
1.083	0.0276	0.38	VQ
1.100	0.0281	0.38	VQ
1.117	0.0286	0.38	VQ
1.133	0.0292	0.38	VQ
1.150	0.0297	0.38	VQ
1.167	0.0302	0.38	VQ
1.183	0.0307	0.38	VQ
1.200	0.0312	0.38	VQ
1.217	0.0318	0.38	VQ
1.233	0.0323	0.38	VQ
1.250	0.0328	0.38	VQ

1.267	0.0333	0.38	VQ
1.283	0.0339	0.38	VQ
1.300	0.0344	0.38	VQ
1.317	0.0349	0.38	VQ
1.333	0.0354	0.38	VQ
1.350	0.0359	0.38	VQ
1.367	0.0365	0.38	VQ
1.383	0.0370	0.38	VQ
1.400	0.0375	0.38	VQ
1.417	0.0380	0.38	VQ
1.433	0.0386	0.38	.Q
1.450	0.0391	0.38	.Q
1.467	0.0396	0.38	.Q
1.483	0.0401	0.38	.Q
1.500	0.0407	0.38	.Q
1.517	0.0412	0.38	.Q
1.533	0.0417	0.38	.Q
1.550	0.0423	0.38	.Q
1.567	0.0428	0.38	.Q
1.583	0.0433	0.38	.Q
1.600	0.0438	0.38	.Q
1.617	0.0444	0.38	.Q
1.633	0.0449	0.38	.Q
1.650	0.0454	0.38	.Q
1.667	0.0460	0.38	.Q
1.683	0.0465	0.38	.Q
1.700	0.0470	0.39	.Q
1.717	0.0476	0.39	.Q
1.733	0.0481	0.39	.Q
1.750	0.0486	0.39	.Q
1.767	0.0491	0.39	.Q
1.783	0.0497	0.39	.Q
1.800	0.0502	0.39	.Q
1.817	0.0507	0.39	.Q
1.833	0.0513	0.39	.Q
1.850	0.0518	0.39	.Q
1.867	0.0523	0.39	.Q
1.883	0.0529	0.39	.Q
1.900	0.0534	0.39	.Q
1.917	0.0539	0.39	.Q
1.933	0.0545	0.39	.Q
1.950	0.0550	0.39	.Q
1.967	0.0556	0.39	.Q
1.983	0.0561	0.39	.Q
2.000	0.0566	0.39	.Q
2.017	0.0572	0.39	.Q
2.033	0.0577	0.39	.Q
2.050	0.0582	0.39	.Q
2.067	0.0588	0.39	.Q
2.083	0.0593	0.39	.Q

2.100	0.0599	0.39	.Q
2.117	0.0604	0.39	.Q
2.133	0.0609	0.39	.Q
2.150	0.0615	0.39	.Q
2.167	0.0620	0.39	.Q
2.183	0.0625	0.39	.Q
2.200	0.0631	0.39	.Q
2.217	0.0636	0.39	.Q
2.233	0.0642	0.39	.Q
2.250	0.0647	0.39	.Q
2.267	0.0652	0.39	.Q
2.283	0.0658	0.39	.Q
2.300	0.0663	0.39	.Q
2.317	0.0669	0.39	.Q
2.333	0.0674	0.39	.Q
2.350	0.0680	0.39	.Q
2.367	0.0685	0.39	.Q
2.383	0.0690	0.39	.Q
2.400	0.0696	0.40	.Q
2.417	0.0701	0.40	.Q
2.433	0.0707	0.40	.Q
2.450	0.0712	0.40	.Q
2.467	0.0718	0.40	.Q
2.483	0.0723	0.40	.Q
2.500	0.0729	0.40	.Q
2.517	0.0734	0.40	.Q
2.533	0.0740	0.40	.Q
2.550	0.0745	0.40	.Q
2.567	0.0750	0.40	.Q
2.583	0.0756	0.40	.Q
2.600	0.0761	0.40	.Q
2.617	0.0767	0.40	.Q
2.633	0.0772	0.40	.QV
2.650	0.0778	0.40	.QV
2.667	0.0783	0.40	.QV
2.683	0.0789	0.40	.QV
2.700	0.0794	0.40	.QV
2.717	0.0800	0.40	.QV
2.733	0.0805	0.40	.QV
2.750	0.0811	0.40	.QV
2.767	0.0816	0.40	.QV
2.783	0.0822	0.40	.QV
2.800	0.0827	0.40	.QV
2.817	0.0833	0.40	.QV
2.833	0.0838	0.40	.QV
2.850	0.0844	0.40	.QV
2.867	0.0850	0.40	.QV
2.883	0.0855	0.40	.QV
2.900	0.0861	0.40	.QV
2.917	0.0866	0.40	.QV

2.933	0.0872	0.40	.QV
2.950	0.0877	0.40	.QV
2.967	0.0883	0.40	.QV
2.983	0.0888	0.40	.QV
3.000	0.0894	0.40	.QV
3.017	0.0900	0.40	.QV
3.033	0.0905	0.40	.QV
3.050	0.0911	0.40	.QV
3.067	0.0916	0.40	.QV
3.083	0.0922	0.40	.QV
3.100	0.0927	0.40	.QV
3.117	0.0933	0.41	.QV
3.133	0.0939	0.41	.QV
3.150	0.0944	0.41	.QV
3.167	0.0950	0.41	.QV
3.183	0.0955	0.41	.QV
3.200	0.0961	0.41	.QV
3.217	0.0967	0.41	.QV
3.233	0.0972	0.41	.QV
3.250	0.0978	0.41	.QV
3.267	0.0983	0.41	.QV
3.283	0.0989	0.41	.QV
3.300	0.0995	0.41	.QV
3.317	0.1000	0.41	.QV
3.333	0.1006	0.41	.QV
3.350	0.1012	0.41	.QV
3.367	0.1017	0.41	.QV
3.383	0.1023	0.41	.QV
3.400	0.1029	0.41	.QV
3.417	0.1034	0.41	.QV
3.433	0.1040	0.41	.QV
3.450	0.1046	0.41	.QV
3.467	0.1051	0.41	.QV
3.483	0.1057	0.41	.QV
3.500	0.1063	0.41	.QV
3.517	0.1068	0.41	.QV
3.533	0.1074	0.41	.QV
3.550	0.1080	0.41	.QV
3.567	0.1085	0.41	.QV
3.583	0.1091	0.41	.QV
3.600	0.1097	0.41	.QV
3.617	0.1102	0.41	.QV
3.633	0.1108	0.41	.QV
3.650	0.1114	0.41	.QV
3.667	0.1119	0.41	.QV
3.683	0.1125	0.42	.QV
3.700	0.1131	0.42	.QV
3.717	0.1137	0.42	.QV
3.733	0.1142	0.42	.QV
3.750	0.1148	0.42	.QV

3.767	0.1154	0.42	.QV
3.783	0.1160	0.42	.Q V
3.800	0.1165	0.42	.Q V
3.817	0.1171	0.42	.Q V
3.833	0.1177	0.42	.Q V
3.850	0.1183	0.42	.Q V
3.867	0.1188	0.42	.Q V
3.883	0.1194	0.42	.Q V
3.900	0.1200	0.42	.Q V
3.917	0.1206	0.42	.Q V
3.933	0.1211	0.42	.Q V
3.950	0.1217	0.42	.Q V
3.967	0.1223	0.42	.Q V
3.983	0.1229	0.42	.Q V
4.000	0.1235	0.42	.Q V
4.017	0.1240	0.42	.Q V
4.033	0.1246	0.42	.Q V
4.050	0.1252	0.42	.Q V
4.067	0.1258	0.42	.Q V
4.083	0.1264	0.42	.Q V
4.100	0.1269	0.42	.Q V
4.117	0.1275	0.42	.Q V
4.133	0.1281	0.42	.Q V
4.150	0.1287	0.42	.Q V
4.167	0.1293	0.42	.Q V
4.183	0.1299	0.42	.Q V
4.200	0.1304	0.42	.Q V
4.217	0.1310	0.42	.Q V
4.233	0.1316	0.42	.Q V
4.250	0.1322	0.42	.Q V
4.267	0.1328	0.43	.Q V
4.283	0.1334	0.43	.Q V
4.300	0.1340	0.43	.Q V
4.317	0.1345	0.43	.Q V
4.333	0.1351	0.43	.Q V
4.350	0.1357	0.43	.Q V
4.367	0.1363	0.43	.Q V
4.383	0.1369	0.43	.Q V
4.400	0.1375	0.43	.Q V
4.417	0.1381	0.43	.Q V
4.433	0.1387	0.43	.Q V
4.450	0.1392	0.43	.Q V
4.467	0.1398	0.43	.Q V
4.483	0.1404	0.43	.Q V
4.500	0.1410	0.43	.Q V
4.517	0.1416	0.43	.Q V
4.533	0.1422	0.43	.Q V
4.550	0.1428	0.43	.Q V
4.567	0.1434	0.43	.Q V
4.583	0.1440	0.43	.Q V

4.600	0.1446	0.43	.Q V
4.617	0.1452	0.43	.Q V
4.633	0.1458	0.43	.Q V
4.650	0.1464	0.43	.Q V
4.667	0.1470	0.43	.Q V
4.683	0.1476	0.43	.Q V
4.700	0.1481	0.43	.Q V
4.717	0.1487	0.43	.Q V
4.733	0.1493	0.43	.Q V
4.750	0.1499	0.43	.Q V
4.767	0.1505	0.43	.Q V
4.783	0.1511	0.43	.Q V
4.800	0.1517	0.43	.Q V
4.817	0.1523	0.43	.Q V
4.833	0.1529	0.44	.Q V
4.850	0.1535	0.44	.Q V
4.867	0.1541	0.44	.Q V
4.883	0.1547	0.44	.Q V
4.900	0.1553	0.44	.Q V
4.917	0.1559	0.44	.Q V
4.933	0.1565	0.44	.Q V
4.950	0.1571	0.44	.Q V
4.967	0.1577	0.44	.Q V
4.983	0.1584	0.44	.Q V
5.000	0.1590	0.44	.Q V
5.017	0.1596	0.44	.Q V
5.033	0.1602	0.44	.Q V
5.050	0.1608	0.44	.Q V
5.067	0.1614	0.44	.Q V
5.083	0.1620	0.44	.Q V
5.100	0.1626	0.44	.Q V
5.117	0.1632	0.44	.Q V
5.133	0.1638	0.44	.Q V
5.150	0.1644	0.44	.Q V
5.167	0.1650	0.44	.Q V
5.183	0.1656	0.44	.Q V
5.200	0.1663	0.44	.Q V
5.217	0.1669	0.44	.Q V
5.233	0.1675	0.44	.Q V
5.250	0.1681	0.44	.Q V
5.267	0.1687	0.44	.Q V
5.283	0.1693	0.44	.Q V
5.300	0.1699	0.44	.Q V
5.317	0.1705	0.45	.Q V
5.333	0.1711	0.45	.Q V
5.350	0.1718	0.45	.Q V
5.367	0.1724	0.45	.Q V
5.383	0.1730	0.45	.Q V
5.400	0.1736	0.45	.Q V
5.417	0.1742	0.45	.Q V

5.433	0.1748	0.45	.Q	V
5.450	0.1755	0.45	.Q	V
5.467	0.1761	0.45	.Q	V
5.483	0.1767	0.45	.Q	V
5.500	0.1773	0.45	.Q	V
5.517	0.1779	0.45	.Q	V
5.533	0.1786	0.45	.Q	V
5.550	0.1792	0.45	.Q	V
5.567	0.1798	0.45	.Q	V
5.583	0.1804	0.45	.Q	V
5.600	0.1810	0.45	.Q	V
5.617	0.1817	0.45	.Q	V
5.633	0.1823	0.45	.Q	V
5.650	0.1829	0.45	.Q	V
5.667	0.1835	0.45	.Q	V
5.683	0.1842	0.45	.Q	V
5.700	0.1848	0.45	.Q	V
5.717	0.1854	0.45	.Q	V
5.733	0.1860	0.45	.Q	V
5.750	0.1867	0.45	.Q	V
5.767	0.1873	0.45	.Q	V
5.783	0.1879	0.46	.Q	V
5.800	0.1885	0.46	.Q	V
5.817	0.1892	0.46	.Q	V
5.833	0.1898	0.46	.Q	V
5.850	0.1904	0.46	.Q	V
5.867	0.1911	0.46	.Q	V
5.883	0.1917	0.46	.Q	V
5.900	0.1923	0.46	.Q	V
5.917	0.1930	0.46	.Q	V
5.933	0.1936	0.46	.Q	V
5.950	0.1942	0.46	.Q	V
5.967	0.1948	0.46	.Q	V
5.983	0.1955	0.46	.Q	V
6.000	0.1961	0.46	.Q	V
6.017	0.1968	0.46	.Q	V
6.033	0.1974	0.46	.Q	V
6.050	0.1980	0.46	.Q	V
6.067	0.1987	0.46	.Q	V
6.083	0.1993	0.46	.Q	V
6.100	0.1999	0.46	.Q	V
6.117	0.2006	0.46	.Q	V
6.133	0.2012	0.46	.Q	V
6.150	0.2018	0.46	.Q	V
6.167	0.2025	0.46	.Q	V
6.183	0.2031	0.46	.Q	V
6.200	0.2038	0.46	.Q	V
6.217	0.2044	0.47	.Q	V
6.233	0.2050	0.47	.Q	V
6.250	0.2057	0.47	.Q	V

6.267	0.2063	0.47	.Q	V
6.283	0.2070	0.47	.Q	V
6.300	0.2076	0.47	.Q	V
6.317	0.2083	0.47	.Q	V
6.333	0.2089	0.47	.Q	V
6.350	0.2096	0.47	.Q	V
6.367	0.2102	0.47	.Q	V
6.383	0.2108	0.47	.Q	V
6.400	0.2115	0.47	.Q	V
6.417	0.2121	0.47	.Q	V
6.433	0.2128	0.47	.Q	V
6.450	0.2134	0.47	.Q	V
6.467	0.2141	0.47	.Q	V
6.483	0.2147	0.47	.Q	V
6.500	0.2154	0.47	.Q	V
6.517	0.2160	0.47	.Q	V
6.533	0.2167	0.47	.Q	V
6.550	0.2173	0.47	.Q	V
6.567	0.2180	0.47	.Q	V
6.583	0.2186	0.47	.Q	V
6.600	0.2193	0.47	.Q	V
6.617	0.2199	0.47	.Q	V
6.633	0.2206	0.48	.Q	V
6.650	0.2213	0.48	.Q	V
6.667	0.2219	0.48	.Q	V
6.683	0.2226	0.48	.Q	V
6.700	0.2232	0.48	.Q	V
6.717	0.2239	0.48	.Q	V
6.733	0.2245	0.48	.Q	V
6.750	0.2252	0.48	.Q	V
6.767	0.2259	0.48	.Q	V
6.783	0.2265	0.48	.Q	V
6.800	0.2272	0.48	.Q	V
6.817	0.2279	0.48	.Q	V
6.833	0.2285	0.48	.Q	V
6.850	0.2292	0.48	.Q	V
6.867	0.2298	0.48	.Q	V
6.883	0.2305	0.48	.Q	V
6.900	0.2312	0.48	.Q	V
6.917	0.2318	0.48	.Q	V
6.933	0.2325	0.48	.Q	V
6.950	0.2332	0.48	.Q	V
6.967	0.2338	0.48	.Q	V
6.983	0.2345	0.48	.Q	V
7.000	0.2352	0.48	.Q	V
7.017	0.2358	0.48	.Q	V
7.033	0.2365	0.49	.Q	V
7.050	0.2372	0.49	.Q	V
7.067	0.2378	0.49	.Q	V
7.083	0.2385	0.49	.Q	V

7.100	0.2392	0.49	.Q	V
7.117	0.2399	0.49	.Q	V
7.133	0.2405	0.49	.Q	V
7.150	0.2412	0.49	.Q	V
7.167	0.2419	0.49	.Q	V
7.183	0.2426	0.49	.Q	V
7.200	0.2432	0.49	.Q	V
7.217	0.2439	0.49	.Q	V
7.233	0.2446	0.49	.Q	V
7.250	0.2453	0.49	.Q	V
7.267	0.2459	0.49	.Q	V
7.283	0.2466	0.49	.Q	V
7.300	0.2473	0.49	.Q	V
7.317	0.2480	0.49	.Q	V
7.333	0.2487	0.49	.Q	V
7.350	0.2493	0.49	.Q	V
7.367	0.2500	0.49	.Q	V
7.383	0.2507	0.49	.Q	V
7.400	0.2514	0.50	.Q	V
7.417	0.2521	0.50	.Q	V
7.433	0.2528	0.50	.Q	V
7.450	0.2534	0.50	.Q	V
7.467	0.2541	0.50	.Q	V
7.483	0.2548	0.50	.Q	V
7.500	0.2555	0.50	.Q	V
7.517	0.2562	0.50	.Q	V
7.533	0.2569	0.50	.Q	V
7.550	0.2576	0.50	.Q	V
7.567	0.2583	0.50	.Q	V
7.583	0.2589	0.50	.Q	V
7.600	0.2596	0.50	.Q	V
7.617	0.2603	0.50	.Q	V
7.633	0.2610	0.50	.Q	V
7.650	0.2617	0.50	.Q	V
7.667	0.2624	0.50	.Q	V
7.683	0.2631	0.50	.Q	V
7.700	0.2638	0.51	.Q	V
7.717	0.2645	0.51	.Q	V
7.733	0.2652	0.51	.Q	V
7.750	0.2659	0.51	.Q	V
7.767	0.2666	0.51	.Q	V
7.783	0.2673	0.51	.Q	V
7.800	0.2680	0.51	.Q	V
7.817	0.2687	0.51	.Q	V
7.833	0.2694	0.51	.Q	V
7.850	0.2701	0.51	.Q	V
7.867	0.2708	0.51	.Q	V
7.883	0.2715	0.51	.Q	V
7.900	0.2722	0.51	.Q	V
7.917	0.2729	0.51	.Q	V

7.933	0.2736	0.51	.Q	V
7.950	0.2743	0.51	.Q	V
7.967	0.2750	0.51	.Q	V
7.983	0.2757	0.51	.Q	V
8.000	0.2764	0.51	.Q	V
8.017	0.2771	0.52	.Q	V
8.033	0.2779	0.52	.Q	V
8.050	0.2786	0.52	.Q	V
8.067	0.2793	0.52	.Q	V
8.083	0.2800	0.52	.Q	V
8.100	0.2807	0.52	.Q	V
8.117	0.2814	0.52	.Q	V
8.133	0.2821	0.52	.Q	V
8.150	0.2828	0.52	.Q	V
8.167	0.2836	0.52	.Q	V
8.183	0.2843	0.52	.Q	V
8.200	0.2850	0.52	.Q	V
8.217	0.2857	0.52	.Q	V
8.233	0.2864	0.52	.Q	V
8.250	0.2871	0.52	.Q	V
8.267	0.2879	0.52	.Q	V
8.283	0.2886	0.52	.Q	V
8.300	0.2893	0.52	.Q	V
8.317	0.2900	0.52	.Q	V
8.333	0.2907	0.52	.Q	V
8.350	0.2915	0.53	.Q	V
8.367	0.2922	0.53	.Q	V
8.383	0.2929	0.53	.Q	V
8.400	0.2936	0.53	.Q	V
8.417	0.2944	0.53	.Q	V
8.433	0.2951	0.53	.Q	V
8.450	0.2958	0.53	.Q	V
8.467	0.2966	0.53	.Q	V
8.483	0.2973	0.53	.Q	V
8.500	0.2980	0.53	.Q	V
8.517	0.2988	0.53	.Q	V
8.533	0.2995	0.53	.Q	V
8.550	0.3002	0.53	.Q	V
8.567	0.3010	0.53	.Q	V
8.583	0.3017	0.53	.Q	V
8.600	0.3024	0.53	.Q	V
8.617	0.3032	0.53	.Q	V
8.633	0.3039	0.53	.Q	V
8.650	0.3046	0.54	.Q	V
8.667	0.3054	0.54	.Q	V
8.683	0.3061	0.54	.Q	V
8.700	0.3069	0.54	.Q	V
8.717	0.3076	0.54	.Q	V
8.733	0.3083	0.54	.Q	V
8.750	0.3091	0.54	.Q	V

8.767	0.3098	0.54	.Q	V
8.783	0.3106	0.54	.Q	V
8.800	0.3113	0.54	.Q	V
8.817	0.3121	0.54	.Q	V
8.833	0.3128	0.54	.Q	V
8.850	0.3136	0.54	.Q	V
8.867	0.3143	0.54	.Q	V
8.883	0.3151	0.55	.Q	V
8.900	0.3158	0.55	.Q	V
8.917	0.3166	0.55	.Q	V
8.933	0.3173	0.55	.Q	V
8.950	0.3181	0.55	.Q	V
8.967	0.3188	0.55	.Q	V
8.983	0.3196	0.55	.Q	V
9.000	0.3204	0.55	.Q	V
9.017	0.3211	0.55	.Q	V
9.033	0.3219	0.55	.Q	V
9.050	0.3226	0.55	.Q	V
9.067	0.3234	0.55	.Q	V
9.083	0.3241	0.55	.Q	V
9.100	0.3249	0.55	.Q	V
9.117	0.3257	0.55	.Q	V
9.133	0.3264	0.55	.Q	V
9.150	0.3272	0.55	.Q	V
9.167	0.3280	0.55	.Q	V
9.183	0.3287	0.56	.Q	V
9.200	0.3295	0.56	.Q	V
9.217	0.3303	0.56	.Q	V
9.233	0.3310	0.56	.Q	V
9.250	0.3318	0.56	.Q	V
9.267	0.3326	0.56	.Q	V
9.283	0.3333	0.56	.Q	V
9.300	0.3341	0.56	.Q	V
9.317	0.3349	0.56	.Q	V
9.333	0.3357	0.56	.Q	V
9.350	0.3364	0.56	.Q	V
9.367	0.3372	0.56	.Q	V
9.383	0.3380	0.57	.Q	V
9.400	0.3388	0.57	.Q	V
9.417	0.3396	0.57	.Q	V
9.433	0.3403	0.57	.Q	V
9.450	0.3411	0.57	.Q	V
9.467	0.3419	0.57	.Q	V
9.483	0.3427	0.57	.Q	V
9.500	0.3435	0.57	.Q	V
9.517	0.3443	0.57	.Q	V
9.533	0.3450	0.57	.Q	V
9.550	0.3458	0.57	.Q	V
9.567	0.3466	0.57	.Q	V
9.583	0.3474	0.57	.Q	V

9.600	0.3482	0.57	.	Q	V.
9.617	0.3490	0.57	.	Q	V.
9.633	0.3498	0.58	.	Q	V.
9.650	0.3506	0.58	.	Q	V.
9.667	0.3514	0.58	.	Q	V.
9.683	0.3522	0.58	.	Q	V.
9.700	0.3530	0.58	.	Q	V.
9.717	0.3538	0.58	.	Q	V.
9.733	0.3546	0.58	.	Q	V.
9.750	0.3554	0.58	.	Q	V.
9.767	0.3562	0.58	.	Q	V.
9.783	0.3570	0.58	.	Q	V.
9.800	0.3578	0.58	.	Q	V.
9.817	0.3586	0.58	.	Q	V.
9.833	0.3594	0.59	.	Q	V.
9.850	0.3602	0.59	.	Q	V.
9.867	0.3610	0.59	.	Q	V.
9.883	0.3618	0.59	.	Q	V.
9.900	0.3626	0.59	.	Q	V.
9.917	0.3634	0.59	.	Q	V.
9.933	0.3642	0.59	.	Q	V.
9.950	0.3650	0.59	.	Q	V.
9.967	0.3659	0.59	.	Q	V.
9.983	0.3667	0.59	.	Q	V.
10.000	0.3675	0.59	.	Q	V.
10.017	0.3683	0.59	.	Q	V.
10.033	0.3691	0.59	.	Q	V.
10.050	0.3699	0.59	.	Q	V.
10.067	0.3708	0.60	.	Q	V.
10.083	0.3716	0.60	.	Q	V.
10.100	0.3724	0.60	.	Q	V.
10.117	0.3732	0.60	.	Q	V.
10.133	0.3740	0.60	.	Q	V.
10.150	0.3749	0.60	.	Q	V.
10.167	0.3757	0.60	.	Q	V.
10.183	0.3765	0.60	.	Q	V.
10.200	0.3774	0.60	.	Q	V.
10.217	0.3782	0.60	.	Q	V.
10.233	0.3790	0.61	.	Q	V.
10.250	0.3799	0.61	.	Q	V.
10.267	0.3807	0.61	.	Q	V.
10.283	0.3815	0.61	.	Q	V.
10.300	0.3824	0.61	.	Q	V.
10.317	0.3832	0.61	.	Q	V.
10.333	0.3841	0.61	.	Q	V.
10.350	0.3849	0.61	.	Q	V.
10.367	0.3857	0.61	.	Q	V
10.383	0.3866	0.61	.	Q	V
10.400	0.3874	0.61	.	Q	V
10.417	0.3883	0.61	.	Q	V

10.433	0.3891	0.61	. Q	V
10.450	0.3899	0.61	. Q	V
10.467	0.3908	0.62	. Q	V
10.483	0.3916	0.62	. Q	V
10.500	0.3925	0.62	. Q	V
10.517	0.3933	0.62	. Q	V
10.533	0.3942	0.62	. Q	V
10.550	0.3951	0.62	. Q	V
10.567	0.3959	0.62	. Q	V
10.583	0.3968	0.62	. Q	V
10.600	0.3976	0.63	. Q	V
10.617	0.3985	0.63	. Q	V
10.633	0.3994	0.63	. Q	V
10.650	0.4002	0.63	. Q	V
10.667	0.4011	0.63	. Q	V
10.683	0.4020	0.63	. Q	V
10.700	0.4028	0.63	. Q	V
10.717	0.4037	0.63	. Q	V
10.733	0.4046	0.63	. Q	V
10.750	0.4054	0.63	. Q	V
10.767	0.4063	0.63	. Q	V
10.783	0.4072	0.63	. Q	V
10.800	0.4081	0.63	. Q	V
10.817	0.4089	0.63	. Q	V
10.833	0.4098	0.64	. Q	V
10.850	0.4107	0.64	. Q	V
10.867	0.4116	0.64	. Q	V
10.883	0.4124	0.64	. Q	V
10.900	0.4133	0.64	. Q	V
10.917	0.4142	0.64	. Q	V
10.933	0.4151	0.64	. Q	V
10.950	0.4160	0.64	. Q	V
10.967	0.4169	0.65	. Q	V
10.983	0.4178	0.65	. Q	V
11.000	0.4187	0.65	. Q	V
11.017	0.4196	0.65	. Q	V
11.033	0.4205	0.65	. Q	V
11.050	0.4214	0.65	. Q	V
11.067	0.4223	0.65	. Q	V
11.083	0.4232	0.65	. Q	V
11.100	0.4241	0.66	. Q	.V
11.117	0.4250	0.66	. Q	.V
11.133	0.4259	0.66	. Q	.V
11.150	0.4268	0.66	. Q	.V
11.167	0.4277	0.66	. Q	.V
11.183	0.4286	0.66	. Q	.V
11.200	0.4295	0.66	. Q	.V
11.217	0.4304	0.66	. Q	.V
11.233	0.4313	0.66	. Q	.V
11.250	0.4322	0.66	. Q	.V

11.267	0.4331	0.66	. Q	.V	.	.	.
11.283	0.4341	0.66	. Q	.V	.	.	.
11.300	0.4350	0.67	. Q	.V	.	.	.
11.317	0.4359	0.67	. Q	.V	.	.	.
11.333	0.4368	0.67	. Q	.V	.	.	.
11.350	0.4377	0.67	. Q	.V	.	.	.
11.367	0.4387	0.67	. Q	.V	.	.	.
11.383	0.4396	0.67	. Q	.V	.	.	.
11.400	0.4405	0.68	. Q	.V	.	.	.
11.417	0.4415	0.68	. Q	.V	.	.	.
11.433	0.4424	0.68	. Q	.V	.	.	.
11.450	0.4433	0.68	. Q	.V	.	.	.
11.467	0.4443	0.68	. Q	.V	.	.	.
11.483	0.4452	0.68	. Q	.V	.	.	.
11.500	0.4461	0.68	. Q	.V	.	.	.
11.517	0.4471	0.69	. Q	.V	.	.	.
11.533	0.4480	0.69	. Q	.V	.	.	.
11.550	0.4490	0.69	. Q	.V	.	.	.
11.567	0.4499	0.69	. Q	.V	.	.	.
11.583	0.4509	0.69	. Q	.V	.	.	.
11.600	0.4518	0.69	. Q	.V	.	.	.
11.617	0.4528	0.69	. Q	.V	.	.	.
11.633	0.4537	0.69	. Q	.V	.	.	.
11.650	0.4547	0.69	. Q	.V	.	.	.
11.667	0.4556	0.69	. Q	.V	.	.	.
11.683	0.4566	0.69	. Q	.V	.	.	.
11.700	0.4575	0.69	. Q	.V	.	.	.
11.717	0.4585	0.70	. Q	.V	.	.	.
11.733	0.4595	0.70	. Q	.V	.	.	.
11.750	0.4604	0.70	. Q	.V	.	.	.
11.767	0.4614	0.70	. Q	.V	.	.	.
11.783	0.4624	0.70	. Q	. V	.	.	.
11.800	0.4633	0.70	. Q	. V	.	.	.
11.817	0.4643	0.71	. Q	. V	.	.	.
11.833	0.4653	0.71	. Q	. V	.	.	.
11.850	0.4663	0.71	. Q	. V	.	.	.
11.867	0.4672	0.71	. Q	. V	.	.	.
11.883	0.4682	0.71	. Q	. V	.	.	.
11.900	0.4692	0.72	. Q	. V	.	.	.
11.917	0.4702	0.72	. Q	. V	.	.	.
11.933	0.4712	0.72	. Q	. V	.	.	.
11.950	0.4722	0.72	. Q	. V	.	.	.
11.967	0.4732	0.72	. Q	. V	.	.	.
11.983	0.4742	0.72	. Q	. V	.	.	.
12.000	0.4752	0.72	. Q	. V	.	.	.
12.017	0.4762	0.72	. Q	. V	.	.	.
12.033	0.4772	0.72	. Q	. V	.	.	.
12.050	0.4782	0.73	. Q	. V	.	.	.
12.067	0.4792	0.73	. Q	. V	.	.	.
12.083	0.4802	0.73	. Q	. V	.	.	.

12.100	0.4812	0.73	.	Q	.	V
12.117	0.4822	0.73	.	Q	.	V
12.133	0.4832	0.73	.	Q	.	V
12.150	0.4842	0.73	.	Q	.	V
12.167	0.4852	0.73	.	Q	.	V
12.183	0.4862	0.73	.	Q	.	V
12.200	0.4872	0.73	.	Q	.	V
12.217	0.4882	0.73	.	Q	.	V
12.233	0.4892	0.73	.	Q	.	V
12.250	0.4902	0.73	.	Q	.	V
12.267	0.4912	0.73	.	Q	.	V
12.283	0.4922	0.73	.	Q	.	V
12.300	0.4932	0.73	.	Q	.	V
12.317	0.4942	0.73	.	Q	.	V
12.333	0.4952	0.73	.	Q	.	V
12.350	0.4963	0.73	.	Q	.	V
12.367	0.4973	0.73	.	Q	.	V
12.383	0.4983	0.73	.	Q	.	V
12.400	0.4993	0.73	.	Q	.	V
12.417	0.5003	0.73	.	Q	.	V
12.433	0.5013	0.74	.	Q	.	V
12.450	0.5023	0.74	.	Q	.	V
12.467	0.5033	0.74	.	Q	.	V
12.483	0.5043	0.74	.	Q	.	V
12.500	0.5054	0.74	.	Q	.	V
12.517	0.5064	0.74	.	Q	.	V
12.533	0.5074	0.74	.	Q	.	V
12.550	0.5084	0.74	.	Q	.	V
12.567	0.5095	0.74	.	Q	.	V
12.583	0.5105	0.75	.	Q	.	V
12.600	0.5115	0.75	.	Q	.	V
12.617	0.5126	0.75	.	Q	.	V
12.633	0.5136	0.75	.	Q	.	V
12.650	0.5146	0.76	.	Q	.	V
12.667	0.5157	0.76	.	Q	.	V
12.683	0.5167	0.76	.	Q	.	V
12.700	0.5178	0.76	.	Q	.	V
12.717	0.5188	0.77	.	Q	.	V
12.733	0.5199	0.77	.	Q	.	V
12.750	0.5210	0.77	.	Q	.	V
12.767	0.5220	0.77	.	Q	.	V
12.783	0.5231	0.78	.	Q	.	V
12.800	0.5242	0.78	.	Q	.	V
12.817	0.5253	0.78	.	Q	.	V
12.833	0.5263	0.78	.	Q	.	V
12.850	0.5274	0.78	.	Q	.	V
12.867	0.5285	0.78	.	Q	.	V
12.883	0.5296	0.79	.	Q	.	V
12.900	0.5307	0.79	.	Q	.	V
12.917	0.5317	0.79	.	Q	.	V

12.933	0.5328	0.79	.	Q	.	V
12.950	0.5339	0.79	.	Q	.	V
12.967	0.5350	0.79	.	Q	.	V
12.983	0.5361	0.79	.	Q	.	V
13.000	0.5372	0.80	.	Q	.	V
13.017	0.5383	0.80	.	Q	.	V
13.033	0.5394	0.80	.	Q	.	V
13.050	0.5405	0.80	.	Q	.	V
13.067	0.5416	0.81	.	Q	.	V
13.083	0.5427	0.81	.	Q	.	V
13.100	0.5439	0.81	.	Q	.	V
13.117	0.5450	0.82	.	Q	.	V
13.133	0.5461	0.82	.	Q	.	V
13.150	0.5472	0.82	.	Q	.	V
13.167	0.5484	0.83	.	Q	.	V
13.183	0.5495	0.83	.	Q	.	V
13.200	0.5507	0.83	.	Q	.	V
13.217	0.5518	0.84	.	Q	.	V
13.233	0.5530	0.84	.	Q	.	V
13.250	0.5541	0.84	.	Q	.	V
13.267	0.5553	0.84	.	Q	.	V
13.283	0.5565	0.84	.	Q	.	V
13.300	0.5576	0.84	.	Q	.	V
13.317	0.5588	0.85	.	Q	.	V
13.333	0.5599	0.85	.	Q	.	V
13.350	0.5611	0.85	.	Q	.	V
13.367	0.5623	0.85	.	Q	.	V
13.383	0.5635	0.85	.	Q	.	V
13.400	0.5646	0.85	.	Q	.	V
13.417	0.5658	0.86	.	Q	.	V
13.433	0.5670	0.86	.	Q	.	V
13.450	0.5682	0.86	.	Q	.	V
13.467	0.5694	0.87	.	Q	.	V
13.483	0.5706	0.87	.	Q	.	V
13.500	0.5718	0.87	.	Q	.	V
13.517	0.5730	0.88	.	Q	.	V
13.533	0.5742	0.88	.	Q	.	V
13.550	0.5754	0.89	.	Q	.	V
13.567	0.5767	0.89	.	Q	.	V
13.583	0.5779	0.89	.	Q	.	V
13.600	0.5791	0.90	.	Q	.	V
13.617	0.5804	0.90	.	Q	.	V
13.633	0.5816	0.91	.	Q	.	V
13.650	0.5829	0.91	.	Q	.	V
13.667	0.5841	0.91	.	Q	.	V
13.683	0.5854	0.91	.	Q	.	V
13.700	0.5866	0.91	.	Q	.	V
13.717	0.5879	0.92	.	Q	.	V
13.733	0.5892	0.92	.	Q	.	V
13.750	0.5904	0.92	.	Q	.	V

13.767	0.5917	0.92	.	Q	.	V	.	.	.
13.783	0.5930	0.93	.	Q	.	V	.	.	.
13.800	0.5943	0.93	.	Q	.	V	.	.	.
13.817	0.5955	0.93	.	Q	.	V	.	.	.
13.833	0.5968	0.93	.	Q	.	V	.	.	.
13.850	0.5981	0.93	.	Q	.	V	.	.	.
13.867	0.5994	0.94	.	Q	.	V	.	.	.
13.883	0.6007	0.94	.	Q	.	V	.	.	.
13.900	0.6020	0.95	.	Q	.	V	.	.	.
13.917	0.6033	0.95	.	Q	.	V	.	.	.
13.933	0.6046	0.96	.	Q	.	V	.	.	.
13.950	0.6060	0.96	.	Q	.	V	.	.	.
13.967	0.6073	0.97	.	Q	.	V	.	.	.
13.983	0.6086	0.97	.	Q	.	V	.	.	.
14.000	0.6100	0.98	.	Q	.	V	.	.	.
14.017	0.6114	0.98	.	Q	.	V	.	.	.
14.033	0.6127	0.99	.	Q	.	V	.	.	.
14.050	0.6141	0.99	.	Q	.	V	.	.	.
14.067	0.6155	1.00	.	Q	.	V	.	.	.
14.083	0.6168	1.00	.	Q	.	V	.	.	.
14.100	0.6182	1.00	.	Q	.	V	.	.	.
14.117	0.6196	1.00	.	Q	.	V	.	.	.
14.133	0.6210	0.99	.	Q	.	V	.	.	.
14.150	0.6223	0.99	.	Q	.	V	.	.	.
14.167	0.6237	0.99	.	Q	.	V	.	.	.
14.183	0.6250	0.99	.	Q	.	V	.	.	.
14.200	0.6264	0.99	.	Q	.	V	.	.	.
14.217	0.6278	0.98	.	Q	.	V	.	.	.
14.233	0.6291	0.98	.	Q	.	V	.	.	.
14.250	0.6305	0.98	.	Q	.	V	.	.	.
14.267	0.6318	0.98	.	Q	.	V	.	.	.
14.283	0.6331	0.97	.	Q	.	V	.	.	.
14.300	0.6345	0.98	.	Q	.	V	.	.	.
14.317	0.6358	0.99	.	Q	.	V	.	.	.
14.333	0.6372	0.99	.	Q	.	V	.	.	.
14.350	0.6386	1.00	.	Q	.	V	.	.	.
14.367	0.6400	1.01	.	Q	.	V	.	.	.
14.383	0.6414	1.01	.	Q	.	V	.	.	.
14.400	0.6428	1.02	.	Q	.	V	.	.	.
14.417	0.6442	1.03	.	Q	.	V	.	.	.
14.433	0.6456	1.03	.	Q	.	V	.	.	.
14.450	0.6470	1.04	.	Q	.	V	.	.	.
14.467	0.6485	1.05	.	Q	.	V	.	.	.
14.483	0.6499	1.05	.	Q	.	V	.	.	.
14.500	0.6514	1.06	.	Q	.	V	.	.	.
14.517	0.6529	1.06	.	Q	.	V	.	.	.
14.533	0.6543	1.07	.	Q	.	V	.	.	.
14.550	0.6558	1.07	.	Q	.	V	.	.	.
14.567	0.6573	1.08	.	Q	.	V	.	.	.
14.583	0.6588	1.08	.	Q	.	V	.	.	.

14.600	0.6603	1.09	.	Q	.	V	.	.	.
14.617	0.6618	1.09	.	Q	.	V	.	.	.
14.633	0.6633	1.09	.	Q	.	V	.	.	.
14.650	0.6648	1.10	.	Q	.	V	.	.	.
14.667	0.6663	1.10	.	Q	.	V	.	.	.
14.683	0.6678	1.11	.	Q	.	V	.	.	.
14.700	0.6694	1.11	.	Q	.	V	.	.	.
14.717	0.6709	1.12	.	Q	.	V	.	.	.
14.733	0.6725	1.13	.	Q	.	V	.	.	.
14.750	0.6740	1.14	.	Q	.	V	.	.	.
14.767	0.6756	1.15	.	Q	.	V	.	.	.
14.783	0.6772	1.16	.	Q	.	V	.	.	.
14.800	0.6788	1.17	.	Q	.	V	.	.	.
14.817	0.6805	1.18	.	Q	.	V	.	.	.
14.833	0.6821	1.19	.	Q	.	V	.	.	.
14.850	0.6837	1.20	.	Q	.	V	.	.	.
14.867	0.6854	1.21	.	Q	.	V	.	.	.
14.883	0.6871	1.22	.	Q	.	V	.	.	.
14.900	0.6888	1.23	.	Q	.	V	.	.	.
14.917	0.6905	1.25	.	Q	.	V	.	.	.
14.933	0.6923	1.26	.	Q	.	V	.	.	.
14.950	0.6940	1.26	.	Q	.	V	.	.	.
14.967	0.6957	1.27	.	Q	.	V	.	.	.
14.983	0.6975	1.28	.	Q	.	V	.	.	.
15.000	0.6993	1.28	.	Q	.	V	.	.	.
15.017	0.7010	1.29	.	Q	.	V	.	.	.
15.033	0.7028	1.30	.	Q	.	V	.	.	.
15.050	0.7046	1.31	.	Q	.	V	.	.	.
15.067	0.7064	1.31	.	Q	.	V	.	.	.
15.083	0.7083	1.32	.	Q	.	V	.	.	.
15.100	0.7101	1.33	.	Q	.	V	.	.	.
15.117	0.7119	1.33	.	Q	.	V	.	.	.
15.133	0.7138	1.34	.	Q	.	V	.	.	.
15.150	0.7156	1.35	.	Q	.	V	.	.	.
15.167	0.7175	1.37	.	Q	.	V	.	.	.
15.183	0.7194	1.39	.	Q	.	V	.	.	.
15.200	0.7214	1.41	.	Q	.	V	.	.	.
15.217	0.7233	1.43	.	Q	.	V	.	.	.
15.233	0.7253	1.45	.	Q	.	V	.	.	.
15.250	0.7274	1.47	.	Q	.	V	.	.	.
15.267	0.7294	1.49	.	Q	.	V	.	.	.
15.283	0.7315	1.51	.	Q	.	V	.	.	.
15.300	0.7336	1.53	.	Q	.	V.	.	.	.
15.317	0.7357	1.55	.	Q	.	V.	.	.	.
15.333	0.7379	1.57	.	Q	.	V.	.	.	.
15.350	0.7401	1.59	.	Q	.	V.	.	.	.
15.367	0.7423	1.61	.	Q	.	V.	.	.	.
15.383	0.7446	1.67	.	Q	.	V.	.	.	.
15.400	0.7469	1.72	.	Q	.	V.	.	.	.
15.417	0.7494	1.77	.	Q	.	V.	.	.	.

15.433	0.7519	1.82	.	Q	.	V.	.	.
15.450	0.7545	1.87	.	Q	.	V.	.	.
15.467	0.7571	1.92	.	Q	.	V.	.	.
15.483	0.7598	1.98	.	Q	.	V.	.	.
15.500	0.7626	2.03	.	Q	.	V.	.	.
15.517	0.7655	2.08	.	Q	.	V.	.	.
15.533	0.7684	2.13	.	Q	.	V.	.	.
15.550	0.7714	2.18	.	Q	.	V	.	.
15.567	0.7745	2.23	.	Q	.	V	.	.
15.583	0.7777	2.29	.	Q	.	V	.	.
15.600	0.7809	2.35	.	Q	.	V	.	.
15.617	0.7842	2.41	.	Q	.	V	.	.
15.633	0.7876	2.47	.	Q.	.	V	.	.
15.650	0.7911	2.53	.	Q.	.	V	.	.
15.667	0.7947	2.59	.	Q.	.	V	.	.
15.683	0.7983	2.65	.	Q.	.	V	.	.
15.700	0.8020	2.71	.	Q.	.	V	.	.
15.717	0.8058	2.76	.	Q	.	V	.	.
15.733	0.8097	2.82	.	Q	.	.V	.	.
15.750	0.8137	2.88	.	Q	.	.V	.	.
15.767	0.8178	2.94	.	Q	.	.V	.	.
15.783	0.8219	3.00	.	.Q	.	.V	.	.
15.800	0.8261	3.06	.	.Q	.	.V	.	.
15.817	0.8304	3.12	.	.Q	.	.V	.	.
15.833	0.8348	3.18	.	.Q	.	.V	.	.
15.850	0.8392	3.24	.	.Q	.	.V	.	.
15.867	0.8438	3.29	.	. Q	.	.V	.	.
15.883	0.8484	3.35	.	. Q	.	.V	.	.
15.900	0.8531	3.41	.	. Q	.	.V	.	.
15.917	0.8579	3.47	.	. Q	.	.V	.	.
15.933	0.8627	3.53	.	. Q	.	.V	.	.
15.950	0.8677	3.58	.	. Q	.	.V	.	.
15.967	0.8727	3.64	.	. Q	.	.V	.	.
15.983	0.8778	3.70	.	. Q	.	.V	.	.
16.000	0.8830	3.76	.	. Q	.	.V	.	.
16.017	0.8886	4.06	.	. Q	.	.V	.	.
16.033	0.8949	4.61	.	. Q	.	.V	.	.
16.050	0.9020	5.16	.	. Q	.	.V	.	.
16.067	0.9099	5.71	.	. Q	.	.V	.	.
16.083	0.9185	6.26	.	. Q	.	.V	.	.
16.100	0.9279	6.81	.	. VQ
16.117	0.9380	7.36	.	. V	.	Q.	.	.
16.133	0.9489	7.91	.	. V	.	Q.	.	.
16.150	0.9606	8.46	.	. V	.	.Q	.	.
16.167	0.9730	9.01	.	. V	.	.Q	.	.
16.183	0.9862	9.56	.	. V	.	.Q	.	.
16.200	1.0001	10.11	.	. V	.	.Q	.	.
16.217	1.0151	10.89	.	. V	.	.Q	.	.
16.233	1.0296	10.52	.	. V	.	.Q	.	.
16.250	1.0432	9.89	.	. V	.	.Q	.	.

16.267	1.0560	9.26	.	.	.	V	.	Q	.
16.283	1.0679	8.63	.	.	.	V	.	Q	.
16.300	1.0789	8.01	.	.	.	VQ.	.	.	.
16.317	1.0891	7.38	.	.	.	QV	.	.	.
16.333	1.0984	6.75	.	.	.	Q	V	.	.
16.350	1.1068	6.12	.	.	.	Q	V	.	.
16.367	1.1144	5.49	.	.	Q	V	.	.	.
16.383	1.1211	4.87	.	.	Q	V	.	.	.
16.400	1.1269	4.24	.	.	Q	V	.	.	.
16.417	1.1319	3.61	.	.	Q	V	.	.	.
16.433	1.1360	2.99	.	Q	.	V	.	.	.
16.450	1.1397	2.71	.	Q.	.	V	.	.	.
16.467	1.1433	2.61	.	Q.	.	V	.	.	.
16.483	1.1468	2.51	.	Q.	.	V	.	.	.
16.500	1.1501	2.40	.	Q.	.	V	.	.	.
16.517	1.1533	2.30	.	Q.	.	V	.	.	.
16.533	1.1563	2.20	.	Q.	.	V	.	.	.
16.550	1.1592	2.10	.	Q	.	V	.	.	.
16.567	1.1619	1.99	.	Q	.	V	.	.	.
16.583	1.1645	1.89	.	Q	.	V	.	.	.
16.600	1.1670	1.79	.	Q	.	V	.	.	.
16.617	1.1693	1.69	.	Q	.	V	.	.	.
16.633	1.1715	1.58	.	Q	.	V	.	.	.
16.650	1.1736	1.49	.	Q	.	V	.	.	.
16.667	1.1755	1.44	.	Q	.	V	.	.	.
16.683	1.1775	1.42	.	Q	.	V	.	.	.
16.700	1.1794	1.40	.	Q	.	V	.	.	.
16.717	1.1813	1.38	.	Q	.	V	.	.	.
16.733	1.1832	1.36	.	Q	.	V	.	.	.
16.750	1.1850	1.33	.	Q	.	V	.	.	.
16.767	1.1868	1.31	.	Q	.	V	.	.	.
16.783	1.1886	1.29	.	Q	.	V	.	.	.
16.800	1.1904	1.27	.	Q	.	V	.	.	.
16.817	1.1921	1.25	.	Q	.	V	.	.	.
16.833	1.1938	1.23	.	Q	.	.V	.	.	.
16.850	1.1954	1.20	.	Q	.	.V	.	.	.
16.867	1.1971	1.18	.	Q	.	.V	.	.	.
16.883	1.1987	1.17	.	Q	.	.V	.	.	.
16.900	1.2003	1.16	.	Q	.	.V	.	.	.
16.917	1.2018	1.14	.	Q	.	.V	.	.	.
16.933	1.2034	1.13	.	Q	.	.V	.	.	.
16.950	1.2049	1.12	.	Q	.	.V	.	.	.
16.967	1.2065	1.10	.	Q	.	.V	.	.	.
16.983	1.2080	1.09	.	Q	.	.V	.	.	.
17.000	1.2094	1.08	.	Q	.	.V	.	.	.
17.017	1.2109	1.07	.	Q	.	.V	.	.	.
17.033	1.2124	1.05	.	Q	.	.V	.	.	.
17.050	1.2138	1.04	.	Q	.	.V	.	.	.
17.067	1.2152	1.03	.	Q	.	.V	.	.	.
17.083	1.2166	1.01	.	Q	.	.V	.	.	.

17.100	1.2180	1.01	.	QV	.
17.117	1.2194	1.01	.	QV	.
17.133	1.2208	1.00	.	QV	.
17.150	1.2221	1.00	.	QV	.
17.167	1.2235	1.00	.	QV	.
17.183	1.2249	0.99	.	QV	.
17.200	1.2262	0.99	.	QV	.
17.217	1.2276	0.98	.	QV	.
17.233	1.2289	0.98	.	QV	.
17.250	1.2303	0.98	.	QV	.
17.267	1.2316	0.97	.	QV	.
17.283	1.2330	0.97	.	QV	.
17.300	1.2343	0.97	.	QV	.
17.317	1.2356	0.96	.	QV	.
17.333	1.2369	0.95	.	QV	.
17.350	1.2382	0.95	.	QV	.
17.367	1.2395	0.94	.	QV	.
17.383	1.2408	0.93	.	QV	.
17.400	1.2421	0.93	.	QV	.
17.417	1.2434	0.92	.	QV	.
17.433	1.2446	0.91	.	QV	.
17.450	1.2459	0.91	.	QV	.
17.467	1.2471	0.90	.	QV	.
17.483	1.2483	0.89	.	QV	.
17.500	1.2496	0.89	.	QV	.
17.517	1.2508	0.88	.	QV	.
17.533	1.2520	0.88	.	QV	.
17.550	1.2532	0.87	.	QV	.
17.567	1.2544	0.86	.	QV	.
17.583	1.2555	0.86	.	QV	.
17.600	1.2567	0.85	.	QV	.
17.617	1.2579	0.85	.	QV	.
17.633	1.2591	0.84	.	QV	.
17.650	1.2602	0.84	.	QV	.
17.667	1.2614	0.83	.	QV	.
17.683	1.2625	0.83	.	QV	.
17.700	1.2636	0.82	.	QV	.
17.717	1.2648	0.82	.	QV	.
17.733	1.2659	0.81	.	QV	.
17.750	1.2670	0.81	.	QV	.
17.767	1.2681	0.80	.	QV	.
17.783	1.2692	0.80	.	QV	.
17.800	1.2703	0.80	.	QV	.
17.817	1.2714	0.79	.	QV	.
17.833	1.2725	0.79	.	QV	.
17.850	1.2736	0.78	.	QV	.
17.867	1.2746	0.78	.	QV	.
17.883	1.2757	0.78	.	QV	.
17.900	1.2768	0.77	.	QV	.
17.917	1.2778	0.77	.	QV	.

17.933	1.2789	0.76	.	Q	.	.	.	V	.
17.950	1.2799	0.76	.	Q	.	.	.	V	.
17.967	1.2810	0.76	.	Q	.	.	.	V	.
17.983	1.2820	0.75	.	Q	.	.	.	V	.
18.000	1.2830	0.75	.	Q	.	.	.	V	.
18.017	1.2841	0.75	.	Q	.	.	.	V	.
18.033	1.2851	0.74	.	Q	.	.	.	V	.
18.050	1.2861	0.74	.	Q	.	.	.	V	.
18.067	1.2871	0.74	.	Q	.	.	.	V	.
18.083	1.2881	0.73	.	Q	.	.	.	V	.
18.100	1.2891	0.73	.	Q	.	.	.	V	.
18.117	1.2901	0.73	.	Q	.	.	.	V	.
18.133	1.2911	0.72	.	Q	.	.	.	V	.
18.150	1.2921	0.72	.	Q	.	.	.	V	.
18.167	1.2931	0.72	.	Q	.	.	.	V	.
18.183	1.2941	0.72	.	Q	.	.	.	V	.
18.200	1.2951	0.72	.	Q	.	.	.	V	.
18.217	1.2961	0.72	.	Q	.	.	.	V	.
18.233	1.2971	0.71	.	Q	.	.	.	V	.
18.250	1.2980	0.71	.	Q	.	.	.	V	.
18.267	1.2990	0.71	.	Q	.	.	.	V	.
18.283	1.3000	0.71	.	Q	.	.	.	V	.
18.300	1.3010	0.71	.	Q	.	.	.	V	.
18.317	1.3019	0.71	.	Q	.	.	.	V	.
18.333	1.3029	0.71	.	Q	.	.	.	V	.
18.350	1.3039	0.71	.	Q	.	.	.	V	.
18.367	1.3049	0.71	.	Q	.	.	.	V	.
18.383	1.3058	0.70	.	Q	.	.	.	V	.
18.400	1.3068	0.70	.	Q	.	.	.	V	.
18.417	1.3078	0.70	.	Q	.	.	.	V	.
18.433	1.3087	0.70	.	Q	.	.	.	V	.
18.450	1.3097	0.69	.	Q	.	.	.	V	.
18.467	1.3106	0.69	.	Q	.	.	.	V	.
18.483	1.3116	0.69	.	Q	.	.	.	V	.
18.500	1.3125	0.69	.	Q	.	.	.	V	.
18.517	1.3135	0.68	.	Q	.	.	.	V	.
18.533	1.3144	0.68	.	Q	.	.	.	V	.
18.550	1.3154	0.68	.	Q	.	.	.	V	.
18.567	1.3163	0.68	.	Q	.	.	.	V	.
18.583	1.3172	0.67	.	Q	.	.	.	V	.
18.600	1.3181	0.67	.	Q	.	.	.	V	.
18.617	1.3191	0.67	.	Q	.	.	.	V	.
18.633	1.3200	0.67	.	Q	.	.	.	V	.
18.650	1.3209	0.67	.	Q	.	.	.	V	.
18.667	1.3218	0.66	.	Q	.	.	.	V	.
18.683	1.3227	0.66	.	Q	.	.	.	V	.
18.700	1.3236	0.66	.	Q	.	.	.	V	.
18.717	1.3245	0.66	.	Q	.	.	.	V	.
18.733	1.3254	0.65	.	Q	.	.	.	V	.
18.750	1.3263	0.65	.	Q	.	.	.	V	.

18.767	1.3272	0.65	.	Q	.	.	.	V	.
18.783	1.3281	0.65	.	Q	.	.	.	V	.
18.800	1.3290	0.65	.	Q	.	.	.	V	.
18.817	1.3299	0.64	.	Q	.	.	.	V	.
18.833	1.3308	0.64	.	Q	.	.	.	V	.
18.850	1.3317	0.64	.	Q	.	.	.	V	.
18.867	1.3325	0.64	.	Q	.	.	.	V	.
18.883	1.3334	0.64	.	Q	.	.	.	V	.
18.900	1.3343	0.63	.	Q	.	.	.	V	.
18.917	1.3352	0.63	.	Q	.	.	.	V	.
18.933	1.3360	0.63	.	Q	.	.	.	V	.
18.950	1.3369	0.63	.	Q	.	.	.	V	.
18.967	1.3378	0.63	.	Q	.	.	.	V	.
18.983	1.3386	0.62	.	Q	.	.	.	V	.
19.000	1.3395	0.62	.	Q	.	.	.	V	.
19.017	1.3403	0.62	.	Q	.	.	.	V	.
19.033	1.3412	0.62	.	Q	.	.	.	V	.
19.050	1.3420	0.62	.	Q	.	.	.	V	.
19.067	1.3429	0.61	.	Q	.	.	.	V	.
19.083	1.3437	0.61	.	Q	.	.	.	V	.
19.100	1.3446	0.61	.	Q	.	.	.	V	.
19.117	1.3454	0.61	.	Q	.	.	.	V	.
19.133	1.3462	0.61	.	Q	.	.	.	V	.
19.150	1.3471	0.61	.	Q	.	.	.	V	.
19.167	1.3479	0.60	.	Q	.	.	.	V	.
19.183	1.3487	0.60	.	Q	.	.	.	V	.
19.200	1.3496	0.60	.	Q	.	.	.	V	.
19.217	1.3504	0.60	.	Q	.	.	.	V	.
19.233	1.3512	0.60	.	Q	.	.	.	V	.
19.250	1.3520	0.60	.	Q	.	.	.	V	.
19.267	1.3528	0.59	.	Q	.	.	.	V	.
19.283	1.3537	0.59	.	Q	.	.	.	V	.
19.300	1.3545	0.59	.	Q	.	.	.	V	.
19.317	1.3553	0.59	.	Q	.	.	.	V	.
19.333	1.3561	0.59	.	Q	.	.	.	V	.
19.350	1.3569	0.59	.	Q	.	.	.	V	.
19.367	1.3577	0.58	.	Q	.	.	.	V	.
19.383	1.3585	0.58	.	Q	.	.	.	V	.
19.400	1.3593	0.58	.	Q	.	.	.	V	.
19.417	1.3601	0.58	.	Q	.	.	.	V	.
19.433	1.3609	0.58	.	Q	.	.	.	V	.
19.450	1.3617	0.58	.	Q	.	.	.	V	.
19.467	1.3625	0.58	.	Q	.	.	.	V	.
19.483	1.3633	0.57	.	Q	.	.	.	V	.
19.500	1.3641	0.57	.	Q	.	.	.	V	.
19.517	1.3649	0.57	.	Q	.	.	.	V	.
19.533	1.3656	0.57	.	Q	.	.	.	V	.
19.550	1.3664	0.57	.	Q	.	.	.	V	.
19.567	1.3672	0.57	.	Q	.	.	.	V	.
19.583	1.3680	0.57	.	Q	.	.	.	V	.

19.600	1.3688	0.56	. Q	V	.
19.617	1.3695	0.56	. Q	V	.
19.633	1.3703	0.56	. Q	V	.
19.650	1.3711	0.56	. Q	V	.
19.667	1.3718	0.56	. Q	V	.
19.683	1.3726	0.56	. Q	V	.
19.700	1.3734	0.56	. Q	V	.
19.717	1.3741	0.55	. Q	V	.
19.733	1.3749	0.55	. Q	V	.
19.750	1.3757	0.55	. Q	V	.
19.767	1.3764	0.55	. Q	V	.
19.783	1.3772	0.55	. Q	V	.
19.800	1.3779	0.55	. Q	V	.
19.817	1.3787	0.55	. Q	V	.
19.833	1.3794	0.55	. Q	V	.
19.850	1.3802	0.54	. Q	V	.
19.867	1.3809	0.54	. Q	V	.
19.883	1.3817	0.54	. Q	V	.
19.900	1.3824	0.54	. Q	V	.
19.917	1.3832	0.54	. Q	V	.
19.933	1.3839	0.54	. Q	V	.
19.950	1.3846	0.54	. Q	V	.
19.967	1.3854	0.54	. Q	V	.
19.983	1.3861	0.53	. Q	V	.
20.000	1.3869	0.53	. Q	V	.
20.017	1.3876	0.53	. Q	V	.
20.033	1.3883	0.53	. Q	V	.
20.050	1.3890	0.53	. Q	V	.
20.067	1.3898	0.53	. Q	V	.
20.083	1.3905	0.53	. Q	V	.
20.100	1.3912	0.53	. Q	V	.
20.117	1.3919	0.52	. Q	V	.
20.133	1.3927	0.52	. Q	V	.
20.150	1.3934	0.52	. Q	V	.
20.167	1.3941	0.52	. Q	V	.
20.183	1.3948	0.52	. Q	V	.
20.200	1.3955	0.52	. Q	V	.
20.217	1.3963	0.52	. Q	V	.
20.233	1.3970	0.52	. Q	V	.
20.250	1.3977	0.52	. Q	V	.
20.267	1.3984	0.52	. Q	V	.
20.283	1.3991	0.51	. Q	V	.
20.300	1.3998	0.51	. Q	V	.
20.317	1.4005	0.51	. Q	V	.
20.333	1.4012	0.51	. Q	V	.
20.350	1.4019	0.51	. Q	V	.
20.367	1.4026	0.51	. Q	V	.
20.383	1.4033	0.51	. Q	V	.
20.400	1.4040	0.51	. Q	V	.
20.417	1.4047	0.51	. Q	V	.

20.433	1.4054	0.50	.Q	.	.	.	V	.
20.450	1.4061	0.50	.Q	.	.	.	V	.
20.467	1.4068	0.50	.Q	.	.	.	V	.
20.483	1.4075	0.50	.Q	.	.	.	V	.
20.500	1.4082	0.50	.Q	.	.	.	V	.
20.517	1.4089	0.50	.Q	.	.	.	V	.
20.533	1.4095	0.50	.Q	.	.	.	V	.
20.550	1.4102	0.50	.Q	.	.	.	V	.
20.567	1.4109	0.50	.Q	.	.	.	V	.
20.583	1.4116	0.50	.Q	.	.	.	V	.
20.600	1.4123	0.50	.Q	.	.	.	V	.
20.617	1.4130	0.49	.Q	.	.	.	V	.
20.633	1.4136	0.49	.Q	.	.	.	V	.
20.650	1.4143	0.49	.Q	.	.	.	V	.
20.667	1.4150	0.49	.Q	.	.	.	V	.
20.683	1.4157	0.49	.Q	.	.	.	V	.
20.700	1.4163	0.49	.Q	.	.	.	V	.
20.717	1.4170	0.49	.Q	.	.	.	V	.
20.733	1.4177	0.49	.Q	.	.	.	V	.
20.750	1.4184	0.49	.Q	.	.	.	V	.
20.767	1.4190	0.49	.Q	.	.	.	V	.
20.783	1.4197	0.48	.Q	.	.	.	V	.
20.800	1.4204	0.48	.Q	.	.	.	V	.
20.817	1.4210	0.48	.Q	.	.	.	V	.
20.833	1.4217	0.48	.Q	.	.	.	V	.
20.850	1.4224	0.48	.Q	.	.	.	V	.
20.867	1.4230	0.48	.Q	.	.	.	V	.
20.883	1.4237	0.48	.Q	.	.	.	V	.
20.900	1.4243	0.48	.Q	.	.	.	V	.
20.917	1.4250	0.48	.Q	.	.	.	V	.
20.933	1.4257	0.48	.Q	.	.	.	V	.
20.950	1.4263	0.48	.Q	.	.	.	V	.
20.967	1.4270	0.48	.Q	.	.	.	V	.
20.983	1.4276	0.47	.Q	.	.	.	V	.
21.000	1.4283	0.47	.Q	.	.	.	V	.
21.017	1.4289	0.47	.Q	.	.	.	V	.
21.033	1.4296	0.47	.Q	.	.	.	V	.
21.050	1.4302	0.47	.Q	.	.	.	V	.
21.067	1.4309	0.47	.Q	.	.	.	V	.
21.083	1.4315	0.47	.Q	.	.	.	V	.
21.100	1.4322	0.47	.Q	.	.	.	V	.
21.117	1.4328	0.47	.Q	.	.	.	V	.
21.133	1.4335	0.47	.Q	.	.	.	V	.
21.150	1.4341	0.47	.Q	.	.	.	V	.
21.167	1.4347	0.47	.Q	.	.	.	V	.
21.183	1.4354	0.46	.Q	.	.	.	V	.
21.200	1.4360	0.46	.Q	.	.	.	V	.
21.217	1.4367	0.46	.Q	.	.	.	V	.
21.233	1.4373	0.46	.Q	.	.	.	V	.
21.250	1.4379	0.46	.Q	.	.	.	V	.

21.267	1.4386	0.46	.Q	V .
21.283	1.4392	0.46	.Q	V .
21.300	1.4398	0.46	.Q	V .
21.317	1.4405	0.46	.Q	V .
21.333	1.4411	0.46	.Q	V .
21.350	1.4417	0.46	.Q	V .
21.367	1.4424	0.46	.Q	V .
21.383	1.4430	0.46	.Q	V .
21.400	1.4436	0.45	.Q	V .
21.417	1.4442	0.45	.Q	V .
21.433	1.4449	0.45	.Q	V .
21.450	1.4455	0.45	.Q	V .
21.467	1.4461	0.45	.Q	V .
21.483	1.4467	0.45	.Q	V .
21.500	1.4473	0.45	.Q	V .
21.517	1.4480	0.45	.Q	V .
21.533	1.4486	0.45	.Q	V .
21.550	1.4492	0.45	.Q	V .
21.567	1.4498	0.45	.Q	V .
21.583	1.4504	0.45	.Q	V .
21.600	1.4510	0.45	.Q	V .
21.617	1.4517	0.45	.Q	V .
21.633	1.4523	0.44	.Q	V .
21.650	1.4529	0.44	.Q	V .
21.667	1.4535	0.44	.Q	V .
21.683	1.4541	0.44	.Q	V .
21.700	1.4547	0.44	.Q	V .
21.717	1.4553	0.44	.Q	V .
21.733	1.4559	0.44	.Q	V .
21.750	1.4565	0.44	.Q	V .
21.767	1.4571	0.44	.Q	V .
21.783	1.4578	0.44	.Q	V .
21.800	1.4584	0.44	.Q	V .
21.817	1.4590	0.44	.Q	V .
21.833	1.4596	0.44	.Q	V .
21.850	1.4602	0.44	.Q	V .
21.867	1.4608	0.44	.Q	V .
21.883	1.4614	0.44	.Q	V .
21.900	1.4620	0.43	.Q	V .
21.917	1.4626	0.43	.Q	V .
21.933	1.4632	0.43	.Q	V .
21.950	1.4637	0.43	.Q	V .
21.967	1.4643	0.43	.Q	V .
21.983	1.4649	0.43	.Q	V .
22.000	1.4655	0.43	.Q	V .
22.017	1.4661	0.43	.Q	V .
22.033	1.4667	0.43	.Q	V .
22.050	1.4673	0.43	.Q	V .
22.067	1.4679	0.43	.Q	V .
22.083	1.4685	0.43	.Q	V .

22.100	1.4691	0.43	.Q	V .
22.117	1.4697	0.43	.Q	V .
22.133	1.4702	0.43	.Q	V .
22.150	1.4708	0.43	.Q	V .
22.167	1.4714	0.42	.Q	V .
22.183	1.4720	0.42	.Q	V .
22.200	1.4726	0.42	.Q	V .
22.217	1.4732	0.42	.Q	V .
22.233	1.4737	0.42	.Q	V .
22.250	1.4743	0.42	.Q	V .
22.267	1.4749	0.42	.Q	V .
22.283	1.4755	0.42	.Q	V .
22.300	1.4761	0.42	.Q	V .
22.317	1.4766	0.42	.Q	V .
22.333	1.4772	0.42	.Q	V .
22.350	1.4778	0.42	.Q	V .
22.367	1.4784	0.42	.Q	V .
22.383	1.4789	0.42	.Q	V .
22.400	1.4795	0.42	.Q	V .
22.417	1.4801	0.42	.Q	V .
22.433	1.4807	0.42	.Q	V .
22.450	1.4812	0.41	.Q	V .
22.467	1.4818	0.41	.Q	V .
22.483	1.4824	0.41	.Q	V .
22.500	1.4829	0.41	.Q	V .
22.517	1.4835	0.41	.Q	V .
22.533	1.4841	0.41	.Q	V .
22.550	1.4846	0.41	.Q	V .
22.567	1.4852	0.41	.Q	V .
22.583	1.4858	0.41	.Q	V .
22.600	1.4863	0.41	.Q	V .
22.617	1.4869	0.41	.Q	V .
22.633	1.4875	0.41	.Q	V .
22.650	1.4880	0.41	.Q	V .
22.667	1.4886	0.41	.Q	V .
22.683	1.4891	0.41	.Q	V .
22.700	1.4897	0.41	.Q	V .
22.717	1.4903	0.41	.Q	V .
22.733	1.4908	0.41	.Q	V .
22.750	1.4914	0.40	.Q	V .
22.767	1.4919	0.40	.Q	V .
22.783	1.4925	0.40	.Q	V .
22.800	1.4930	0.40	.Q	V .
22.817	1.4936	0.40	.Q	V .
22.833	1.4942	0.40	.Q	V .
22.850	1.4947	0.40	.Q	V .
22.867	1.4953	0.40	.Q	V .
22.883	1.4958	0.40	.Q	V .
22.900	1.4964	0.40	.Q	V .
22.917	1.4969	0.40	.Q	V .

22.933	1.4975	0.40	.Q	V .
22.950	1.4980	0.40	.Q	V .
22.967	1.4986	0.40	.Q	V .
22.983	1.4991	0.40	.Q	V .
23.000	1.4997	0.40	.Q	V .
23.017	1.5002	0.40	.Q	V .
23.033	1.5008	0.40	.Q	V .
23.050	1.5013	0.40	.Q	V .
23.067	1.5018	0.40	.Q	V.
23.083	1.5024	0.39	.Q	V.
23.100	1.5029	0.39	.Q	V.
23.117	1.5035	0.39	.Q	V.
23.133	1.5040	0.39	.Q	V.
23.150	1.5046	0.39	.Q	V.
23.167	1.5051	0.39	.Q	V.
23.183	1.5056	0.39	.Q	V.
23.200	1.5062	0.39	.Q	V.
23.217	1.5067	0.39	.Q	V.
23.233	1.5073	0.39	.Q	V.
23.250	1.5078	0.39	.Q	V.
23.267	1.5083	0.39	.Q	V.
23.283	1.5089	0.39	.Q	V.
23.300	1.5094	0.39	.Q	V.
23.317	1.5099	0.39	.Q	V.
23.333	1.5105	0.39	.Q	V.
23.350	1.5110	0.39	.Q	V.
23.367	1.5115	0.39	.Q	V.
23.383	1.5121	0.39	.Q	V.
23.400	1.5126	0.39	.Q	V.
23.417	1.5131	0.39	.Q	V.
23.433	1.5137	0.39	.Q	V.
23.450	1.5142	0.38	.Q	V.
23.467	1.5147	0.38	.Q	V.
23.483	1.5152	0.38	.Q	V.
23.500	1.5158	0.38	.Q	V.
23.517	1.5163	0.38	.Q	V.
23.533	1.5168	0.38	.Q	V.
23.550	1.5174	0.38	.Q	V.
23.567	1.5179	0.38	.Q	V.
23.583	1.5184	0.38	.Q	V.
23.600	1.5189	0.38	.Q	V.
23.617	1.5195	0.38	.Q	V.
23.633	1.5200	0.38	.Q	V.
23.650	1.5205	0.38	.Q	V.
23.667	1.5210	0.38	.Q	V.
23.683	1.5215	0.38	.Q	V.
23.700	1.5221	0.38	.Q	V.
23.717	1.5226	0.38	.Q	V.
23.733	1.5231	0.38	.Q	V.
23.750	1.5236	0.38	.Q	V.

23.767	1.5241	0.38	.Q	.	.	.	V.
23.783	1.5247	0.38	.Q	.	.	.	V.
23.800	1.5252	0.38	.Q	.	.	.	V.
23.817	1.5257	0.38	.Q	.	.	.	V.
23.833	1.5262	0.37	.Q	.	.	.	V.
23.850	1.5267	0.37	.Q	.	.	.	V.
23.867	1.5272	0.37	.Q	.	.	.	V.
23.883	1.5278	0.37	.Q	.	.	.	V.
23.900	1.5283	0.37	.Q	.	.	.	V.
23.917	1.5288	0.37	.Q	.	.	.	V.
23.933	1.5293	0.37	.Q	.	.	.	V.
23.950	1.5298	0.37	.Q	.	.	.	V.
23.967	1.5303	0.37	.Q	.	.	.	V.
23.983	1.5308	0.37	.Q	.	.	.	V.
24.000	1.5313	0.37	.Q	.	.	.	V.

TIME DURATION(minutes) OF PERCENTILES OF ESTIMATED PEAK FLOW RATE:

(Note: 100% of Peak Flow Rate estimate assumed to have
an instantaneous time duration)

Percentile of Estimated Peak Flow Rate	Duration (minutes)
=====	
0%	1441.0
10%	715.0
20%	300.0
30%	170.0
40%	110.0
50%	95.0
60%	75.0
70%	55.0
80%	35.0
90%	20.0

FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 11

>>>>VIEW STREAM NUMBER 1 HYDROGRAPH<<<<

STREAM HYDROGRAPH IN ONE-MINUTE UNIT INTERVALS(CFS)
(Notes: Time indicated is at END of Each Unit Intervals.
Peak 5-minute rainfall intensity is modeled as
a constant value for entire 5-minute period.)

TIME(HRS)	VOLUME(AF)	Q(CFS)	0.	5.0	10.0	15.0	20.0
0.017	0.0000	0.00	Q
0.033	0.0000	0.00	Q

0.050	0.0000	0.00	Q
0.067	0.0000	0.00	Q
0.083	0.0000	0.00	Q
0.100	0.0000	0.02	Q
0.117	0.0001	0.05	Q
0.133	0.0002	0.08	Q
0.150	0.0004	0.11	Q
0.167	0.0006	0.14	Q
0.183	0.0008	0.17	Q
0.200	0.0011	0.19	Q
0.217	0.0014	0.22	Q
0.233	0.0017	0.25	Q
0.250	0.0021	0.28	Q
0.267	0.0025	0.31	Q
0.283	0.0030	0.34	Q
0.300	0.0035	0.36	Q
0.317	0.0040	0.37	Q
0.333	0.0045	0.37	Q
0.350	0.0050	0.37	Q
0.367	0.0055	0.37	Q
0.383	0.0060	0.37	Q
0.400	0.0065	0.37	Q
0.417	0.0070	0.37	Q
0.433	0.0076	0.37	Q
0.450	0.0081	0.37	Q
0.467	0.0086	0.37	Q
0.483	0.0091	0.37	Q
0.500	0.0096	0.37	Q
0.517	0.0101	0.37	Q
0.533	0.0106	0.37	Q
0.550	0.0111	0.37	Q
0.567	0.0116	0.37	Q
0.583	0.0121	0.37	Q
0.600	0.0126	0.37	Q
0.617	0.0132	0.37	Q
0.633	0.0137	0.37	Q
0.650	0.0142	0.37	Q
0.667	0.0147	0.37	Q
0.683	0.0152	0.37	Q
0.700	0.0157	0.37	Q
0.717	0.0162	0.37	Q
0.733	0.0167	0.37	Q
0.750	0.0173	0.37	Q
0.767	0.0178	0.37	Q
0.783	0.0183	0.37	Q
0.800	0.0188	0.37	Q
0.817	0.0193	0.37	Q
0.833	0.0198	0.37	Q
0.850	0.0204	0.37	Q
0.867	0.0209	0.37	Q

0.883	0.0214	0.37	Q
0.900	0.0219	0.37	Q
0.917	0.0224	0.37	Q
0.933	0.0229	0.37	Q
0.950	0.0234	0.37	Q
0.967	0.0240	0.38	Q
0.983	0.0245	0.38	Q
1.000	0.0250	0.38	Q
1.017	0.0255	0.38	Q
1.033	0.0260	0.38	Q
1.050	0.0266	0.38	Q
1.067	0.0271	0.38	Q
1.083	0.0276	0.38	Q
1.100	0.0281	0.38	Q
1.117	0.0286	0.38	Q
1.133	0.0292	0.38	Q
1.150	0.0297	0.38	Q
1.167	0.0302	0.38	Q
1.183	0.0307	0.38	Q
1.200	0.0312	0.38	Q
1.217	0.0318	0.38	Q
1.233	0.0323	0.38	Q
1.250	0.0328	0.38	Q
1.267	0.0333	0.38	Q
1.283	0.0339	0.38	Q
1.300	0.0344	0.38	Q
1.317	0.0349	0.38	Q
1.333	0.0354	0.38	Q
1.350	0.0359	0.38	Q
1.367	0.0365	0.38	Q
1.383	0.0370	0.38	Q
1.400	0.0375	0.38	Q
1.417	0.0380	0.38	Q
1.433	0.0386	0.38	QV
1.450	0.0391	0.38	QV
1.467	0.0396	0.38	QV
1.483	0.0401	0.38	QV
1.500	0.0407	0.38	QV
1.517	0.0412	0.38	QV
1.533	0.0417	0.38	QV
1.550	0.0423	0.38	QV
1.567	0.0428	0.38	QV
1.583	0.0433	0.38	QV
1.600	0.0438	0.38	QV
1.617	0.0444	0.38	QV
1.633	0.0449	0.38	QV
1.650	0.0454	0.38	QV
1.667	0.0460	0.38	QV
1.683	0.0465	0.38	QV
1.700	0.0470	0.39	QV

1.717	0.0476	0.39	QV
1.733	0.0481	0.39	QV
1.750	0.0486	0.39	QV
1.767	0.0491	0.39	QV
1.783	0.0497	0.39	QV
1.800	0.0502	0.39	QV
1.817	0.0507	0.39	QV
1.833	0.0513	0.39	QV
1.850	0.0518	0.39	QV
1.867	0.0523	0.39	QV
1.883	0.0529	0.39	QV
1.900	0.0534	0.39	QV
1.917	0.0539	0.39	QV
1.933	0.0545	0.39	QV
1.950	0.0550	0.39	QV
1.967	0.0556	0.39	QV
1.983	0.0561	0.39	QV
2.000	0.0566	0.39	QV
2.017	0.0572	0.39	QV
2.033	0.0577	0.39	QV
2.050	0.0582	0.39	QV
2.067	0.0588	0.39	QV
2.083	0.0593	0.39	QV
2.100	0.0599	0.39	QV
2.117	0.0604	0.39	QV
2.133	0.0609	0.39	QV
2.150	0.0615	0.39	QV
2.167	0.0620	0.39	QV
2.183	0.0625	0.39	QV
2.200	0.0631	0.39	QV
2.217	0.0636	0.39	QV
2.233	0.0642	0.39	QV
2.250	0.0647	0.39	QV
2.267	0.0652	0.39	QV
2.283	0.0658	0.39	QV
2.300	0.0663	0.39	QV
2.317	0.0669	0.39	QV
2.333	0.0674	0.39	QV
2.350	0.0680	0.39	QV
2.367	0.0685	0.39	QV
2.383	0.0690	0.39	QV
2.400	0.0696	0.40	QV
2.417	0.0701	0.40	QV
2.433	0.0707	0.40	QV
2.450	0.0712	0.40	QV
2.467	0.0718	0.40	QV
2.483	0.0723	0.40	QV
2.500	0.0729	0.40	QV
2.517	0.0734	0.40	QV
2.533	0.0740	0.40	QV

2.550	0.0745	0.40	QV
2.567	0.0750	0.40	QV
2.583	0.0756	0.40	QV
2.600	0.0761	0.40	QV
2.617	0.0767	0.40	QV
2.633	0.0772	0.40	Q V
2.650	0.0778	0.40	Q V
2.667	0.0783	0.40	Q V
2.683	0.0789	0.40	Q V
2.700	0.0794	0.40	Q V
2.717	0.0800	0.40	Q V
2.733	0.0805	0.40	Q V
2.750	0.0811	0.40	Q V
2.767	0.0816	0.40	Q V
2.783	0.0822	0.40	Q V
2.800	0.0827	0.40	Q V
2.817	0.0833	0.40	Q V
2.833	0.0838	0.40	Q V
2.850	0.0844	0.40	Q V
2.867	0.0850	0.40	Q V
2.883	0.0855	0.40	Q V
2.900	0.0861	0.40	Q V
2.917	0.0866	0.40	Q V
2.933	0.0872	0.40	Q V
2.950	0.0877	0.40	Q V
2.967	0.0883	0.40	Q V
2.983	0.0888	0.40	Q V
3.000	0.0894	0.40	Q V
3.017	0.0900	0.40	Q V
3.033	0.0905	0.40	Q V
3.050	0.0911	0.40	Q V
3.067	0.0916	0.40	Q V
3.083	0.0922	0.40	Q V
3.100	0.0927	0.40	Q V
3.117	0.0933	0.41	Q V
3.133	0.0939	0.41	Q V
3.150	0.0944	0.41	Q V
3.167	0.0950	0.41	Q V
3.183	0.0955	0.41	Q V
3.200	0.0961	0.41	Q V
3.217	0.0967	0.41	Q V
3.233	0.0972	0.41	Q V
3.250	0.0978	0.41	Q V
3.267	0.0983	0.41	Q V
3.283	0.0989	0.41	Q V
3.300	0.0995	0.41	Q V
3.317	0.1000	0.41	Q V
3.333	0.1006	0.41	Q V
3.350	0.1012	0.41	Q V
3.367	0.1017	0.41	Q V

3.383	0.1023	0.41	Q	V
3.400	0.1029	0.41	Q	V
3.417	0.1034	0.41	Q	V
3.433	0.1040	0.41	Q	V
3.450	0.1046	0.41	Q	V
3.467	0.1051	0.41	Q	V
3.483	0.1057	0.41	Q	V
3.500	0.1063	0.41	Q	V
3.517	0.1068	0.41	Q	V
3.533	0.1074	0.41	Q	V
3.550	0.1080	0.41	Q	V
3.567	0.1085	0.41	Q	V
3.583	0.1091	0.41	Q	V
3.600	0.1097	0.41	Q	V
3.617	0.1102	0.41	Q	V
3.633	0.1108	0.41	Q	V
3.650	0.1114	0.41	Q	V
3.667	0.1119	0.41	Q	V
3.683	0.1125	0.42	Q	V
3.700	0.1131	0.42	Q	V
3.717	0.1137	0.42	Q	V
3.733	0.1142	0.42	Q	V
3.750	0.1148	0.42	Q	V
3.767	0.1154	0.42	Q	V
3.783	0.1160	0.42	Q	V
3.800	0.1165	0.42	Q	V
3.817	0.1171	0.42	Q	V
3.833	0.1177	0.42	Q	V
3.850	0.1183	0.42	Q	V
3.867	0.1188	0.42	Q	V
3.883	0.1194	0.42	Q	V
3.900	0.1200	0.42	Q	V
3.917	0.1206	0.42	Q	V
3.933	0.1211	0.42	Q	V
3.950	0.1217	0.42	Q	V
3.967	0.1223	0.42	Q	V
3.983	0.1229	0.42	Q	V
4.000	0.1235	0.42	Q	V
4.017	0.1240	0.42	Q	V
4.033	0.1246	0.42	Q	V
4.050	0.1252	0.42	Q	V
4.067	0.1258	0.42	Q	V
4.083	0.1264	0.42	Q	V
4.100	0.1269	0.42	Q	V
4.117	0.1275	0.42	Q	V
4.133	0.1281	0.42	Q	V
4.150	0.1287	0.42	Q	V
4.167	0.1293	0.42	Q	V
4.183	0.1299	0.42	Q	V
4.200	0.1304	0.42	Q	V

4.217	0.1310	0.42	Q	V
4.233	0.1316	0.42	Q	V
4.250	0.1322	0.42	Q	V
4.267	0.1328	0.43	Q	V
4.283	0.1334	0.43	Q	V
4.300	0.1340	0.43	Q	V
4.317	0.1345	0.43	Q	V
4.333	0.1351	0.43	Q	V
4.350	0.1357	0.43	Q	V
4.367	0.1363	0.43	Q	V
4.383	0.1369	0.43	Q	V
4.400	0.1375	0.43	Q	V
4.417	0.1381	0.43	Q	V
4.433	0.1387	0.43	Q	V
4.450	0.1392	0.43	Q	V
4.467	0.1398	0.43	Q	V
4.483	0.1404	0.43	Q	V
4.500	0.1410	0.43	Q	V
4.517	0.1416	0.43	Q	V
4.533	0.1422	0.43	Q	V
4.550	0.1428	0.43	Q	V
4.567	0.1434	0.43	Q	V
4.583	0.1440	0.43	Q	V
4.600	0.1446	0.43	Q	V
4.617	0.1452	0.43	Q	V
4.633	0.1458	0.43	Q	V
4.650	0.1464	0.43	Q	V
4.667	0.1470	0.43	Q	V
4.683	0.1476	0.43	Q	V
4.700	0.1481	0.43	Q	V
4.717	0.1487	0.43	Q	V
4.733	0.1493	0.43	Q	V
4.750	0.1499	0.43	Q	V
4.767	0.1505	0.43	Q	V
4.783	0.1511	0.43	Q	V
4.800	0.1517	0.43	Q	V
4.817	0.1523	0.43	Q	V
4.833	0.1529	0.44	Q	V
4.850	0.1535	0.44	Q	V
4.867	0.1541	0.44	Q	V
4.883	0.1547	0.44	Q	V
4.900	0.1553	0.44	Q	V
4.917	0.1559	0.44	Q	V
4.933	0.1565	0.44	Q	V
4.950	0.1571	0.44	Q	V
4.967	0.1577	0.44	Q	V
4.983	0.1584	0.44	Q	V
5.000	0.1590	0.44	Q	V
5.017	0.1596	0.44	Q	V
5.033	0.1602	0.44	Q	V

5.050	0.1608	0.44	Q	V
5.067	0.1614	0.44	Q	V
5.083	0.1620	0.44	Q	V
5.100	0.1626	0.44	Q	V
5.117	0.1632	0.44	Q	V
5.133	0.1638	0.44	Q	V
5.150	0.1644	0.44	Q	V
5.167	0.1650	0.44	Q	V
5.183	0.1656	0.44	Q	V
5.200	0.1663	0.44	Q	V
5.217	0.1669	0.44	Q	V
5.233	0.1675	0.44	Q	V
5.250	0.1681	0.44	Q	V
5.267	0.1687	0.44	Q	V
5.283	0.1693	0.44	Q	V
5.300	0.1699	0.44	Q	V
5.317	0.1705	0.45	Q	V
5.333	0.1711	0.45	Q	V
5.350	0.1718	0.45	Q	V
5.367	0.1724	0.45	Q	V
5.383	0.1730	0.45	Q	V
5.400	0.1736	0.45	Q	V
5.417	0.1742	0.45	Q	V
5.433	0.1748	0.45	Q	V
5.450	0.1755	0.45	Q	V
5.467	0.1761	0.45	Q	V
5.483	0.1767	0.45	Q	V
5.500	0.1773	0.45	Q	V
5.517	0.1779	0.45	Q	V
5.533	0.1786	0.45	Q	V
5.550	0.1792	0.45	Q	V
5.567	0.1798	0.45	Q	V
5.583	0.1804	0.45	Q	V
5.600	0.1810	0.45	Q	V
5.617	0.1817	0.45	Q	V
5.633	0.1823	0.45	Q	V
5.650	0.1829	0.45	Q	V
5.667	0.1835	0.45	Q	V
5.683	0.1842	0.45	Q	V
5.700	0.1848	0.45	Q	V
5.717	0.1854	0.45	Q	V
5.733	0.1860	0.45	Q	V
5.750	0.1867	0.45	Q	V
5.767	0.1873	0.45	Q	V
5.783	0.1879	0.46	Q	V
5.800	0.1885	0.46	Q	V
5.817	0.1892	0.46	Q	V
5.833	0.1898	0.46	Q	V
5.850	0.1904	0.46	Q	V
5.867	0.1911	0.46	Q	V

5.883	0.1917	0.46	Q	V
5.900	0.1923	0.46	Q	V
5.917	0.1930	0.46	Q	V
5.933	0.1936	0.46	Q	V
5.950	0.1942	0.46	Q	V
5.967	0.1948	0.46	Q	V
5.983	0.1955	0.46	Q	V
6.000	0.1961	0.46	Q	V
6.017	0.1968	0.46	Q	V
6.033	0.1974	0.46	Q	V
6.050	0.1980	0.46	Q	V
6.067	0.1987	0.46	Q	V
6.083	0.1993	0.46	Q	V
6.100	0.1999	0.46	Q	V
6.117	0.2006	0.46	Q	V
6.133	0.2012	0.46	Q	V
6.150	0.2018	0.46	Q	V
6.167	0.2025	0.46	Q	V
6.183	0.2031	0.46	Q	V
6.200	0.2038	0.46	Q	V
6.217	0.2044	0.47	Q	V
6.233	0.2050	0.47	Q	V
6.250	0.2057	0.47	Q	V
6.267	0.2063	0.47	Q	V
6.283	0.2070	0.47	Q	V
6.300	0.2076	0.47	Q	V
6.317	0.2083	0.47	Q	V
6.333	0.2089	0.47	Q	V
6.350	0.2096	0.47	Q	V
6.367	0.2102	0.47	Q	V
6.383	0.2108	0.47	Q	V
6.400	0.2115	0.47	Q	V
6.417	0.2121	0.47	Q	V
6.433	0.2128	0.47	Q	V
6.450	0.2134	0.47	Q	V
6.467	0.2141	0.47	Q	V
6.483	0.2147	0.47	Q	V
6.500	0.2154	0.47	Q	V
6.517	0.2160	0.47	Q	V
6.533	0.2167	0.47	Q	V
6.550	0.2173	0.47	Q	V
6.567	0.2180	0.47	Q	V
6.583	0.2186	0.47	Q	V
6.600	0.2193	0.47	Q	V
6.617	0.2199	0.47	Q	V
6.633	0.2206	0.48	Q	V
6.650	0.2213	0.48	Q	V
6.667	0.2219	0.48	Q	V
6.683	0.2226	0.48	Q	V
6.700	0.2232	0.48	Q	V

6.717	0.2239	0.48	Q	V
6.733	0.2245	0.48	Q	V
6.750	0.2252	0.48	Q	V
6.767	0.2259	0.48	Q	V
6.783	0.2265	0.48	Q	V
6.800	0.2272	0.48	Q	V
6.817	0.2279	0.48	Q	V
6.833	0.2285	0.48	Q	V
6.850	0.2292	0.48	Q	V
6.867	0.2298	0.48	Q	V
6.883	0.2305	0.48	Q	V
6.900	0.2312	0.48	Q	V
6.917	0.2318	0.48	Q	V
6.933	0.2325	0.48	Q	V
6.950	0.2332	0.48	Q	V
6.967	0.2338	0.48	Q	V
6.983	0.2345	0.48	Q	V
7.000	0.2352	0.48	Q	V
7.017	0.2358	0.48	Q	V
7.033	0.2365	0.49	Q	V
7.050	0.2372	0.49	Q	V
7.067	0.2378	0.49	Q	V
7.083	0.2385	0.49	Q	V
7.100	0.2392	0.49	Q	V
7.117	0.2399	0.49	Q	V
7.133	0.2405	0.49	Q	V
7.150	0.2412	0.49	Q	V
7.167	0.2419	0.49	Q	V
7.183	0.2426	0.49	Q	V
7.200	0.2432	0.49	Q	V
7.217	0.2439	0.49	Q	V
7.233	0.2446	0.49	Q	V
7.250	0.2453	0.49	Q	V
7.267	0.2459	0.49	Q	V
7.283	0.2466	0.49	Q	V
7.300	0.2473	0.49	Q	V
7.317	0.2480	0.49	Q	V
7.333	0.2487	0.49	Q	V
7.350	0.2493	0.49	Q	V
7.367	0.2500	0.49	Q	V
7.383	0.2507	0.49	Q	V
7.400	0.2514	0.50	Q	V
7.417	0.2521	0.50	Q	V
7.433	0.2528	0.50	Q	V
7.450	0.2534	0.50	Q	V
7.467	0.2541	0.50	Q	V
7.483	0.2548	0.50	Q	V
7.500	0.2555	0.50	Q	V
7.517	0.2562	0.50	Q	V
7.533	0.2569	0.50	.Q	V

7.550	0.2576	0.50	.Q	V
7.567	0.2583	0.50	.Q	V
7.583	0.2589	0.50	.Q	V
7.600	0.2596	0.50	.Q	V
7.617	0.2603	0.50	.Q	V
7.633	0.2610	0.50	.Q	V
7.650	0.2617	0.50	.Q	V
7.667	0.2624	0.50	.Q	V
7.683	0.2631	0.50	.Q	V
7.700	0.2638	0.51	.Q	V
7.717	0.2645	0.51	.Q	V
7.733	0.2652	0.51	.Q	V
7.750	0.2659	0.51	.Q	V
7.767	0.2666	0.51	.Q	V
7.783	0.2673	0.51	.Q	V
7.800	0.2680	0.51	.Q	V
7.817	0.2687	0.51	.Q	V
7.833	0.2694	0.51	.Q	V
7.850	0.2701	0.51	.Q	V
7.867	0.2708	0.51	.Q	V
7.883	0.2715	0.51	.Q	V
7.900	0.2722	0.51	.Q	V
7.917	0.2729	0.51	.Q	V
7.933	0.2736	0.51	.Q	V
7.950	0.2743	0.51	.Q	V
7.967	0.2750	0.51	.Q	V
7.983	0.2757	0.51	.Q	V
8.000	0.2764	0.51	.Q	V
8.017	0.2771	0.52	.Q	V
8.033	0.2779	0.52	.Q	V
8.050	0.2786	0.52	.Q	V
8.067	0.2793	0.52	.Q	V
8.083	0.2800	0.52	.Q	V
8.100	0.2807	0.52	.Q	V
8.117	0.2814	0.52	.Q	V
8.133	0.2821	0.52	.Q	V
8.150	0.2828	0.52	.Q	V
8.167	0.2836	0.52	.Q	V
8.183	0.2843	0.52	.Q	V
8.200	0.2850	0.52	.Q	V
8.217	0.2857	0.52	.Q	V
8.233	0.2864	0.52	.Q	V
8.250	0.2871	0.52	.Q	V
8.267	0.2879	0.52	.Q	V
8.283	0.2886	0.52	.Q	V
8.300	0.2893	0.52	.Q	V
8.317	0.2900	0.52	.Q	V
8.333	0.2907	0.52	.Q	V
8.350	0.2915	0.53	.Q	V
8.367	0.2922	0.53	.Q	V

8.383	0.2929	0.53	.Q	V
8.400	0.2936	0.53	.Q	V
8.417	0.2944	0.53	.Q	V
8.433	0.2951	0.53	.Q	V
8.450	0.2958	0.53	.Q	V
8.467	0.2966	0.53	.Q	V
8.483	0.2973	0.53	.Q	V
8.500	0.2980	0.53	.Q	V
8.517	0.2988	0.53	.Q	V
8.533	0.2995	0.53	.Q	V
8.550	0.3002	0.53	.Q	V
8.567	0.3010	0.53	.Q	V
8.583	0.3017	0.53	.Q	V
8.600	0.3024	0.53	.Q	V
8.617	0.3032	0.53	.Q	V
8.633	0.3039	0.53	.Q	V
8.650	0.3046	0.54	.Q	V
8.667	0.3054	0.54	.Q	V
8.683	0.3061	0.54	.Q	V
8.700	0.3069	0.54	.Q	V
8.717	0.3076	0.54	.Q	V
8.733	0.3083	0.54	.Q	V
8.750	0.3091	0.54	.Q	V
8.767	0.3098	0.54	.Q	V
8.783	0.3106	0.54	.Q	V
8.800	0.3113	0.54	.Q	V
8.817	0.3121	0.54	.Q	V
8.833	0.3128	0.54	.Q	V
8.850	0.3136	0.54	.Q	V
8.867	0.3143	0.54	.Q	V
8.883	0.3151	0.55	.Q	V
8.900	0.3158	0.55	.Q	V
8.917	0.3166	0.55	.Q	V
8.933	0.3173	0.55	.Q	V
8.950	0.3181	0.55	.Q	V
8.967	0.3188	0.55	.Q	V
8.983	0.3196	0.55	.Q	V
9.000	0.3204	0.55	.Q	V
9.017	0.3211	0.55	.Q	V
9.033	0.3219	0.55	.Q	V
9.050	0.3226	0.55	.Q	V
9.067	0.3234	0.55	.Q	V
9.083	0.3241	0.55	.Q	V
9.100	0.3249	0.55	.Q	V
9.117	0.3257	0.55	.Q	V
9.133	0.3264	0.55	.Q	V
9.150	0.3272	0.55	.Q	V
9.167	0.3280	0.55	.Q	V
9.183	0.3287	0.56	.Q	V
9.200	0.3295	0.56	.Q	V

9.217	0.3303	0.56	.Q	V
9.233	0.3310	0.56	.Q	V
9.250	0.3318	0.56	.Q	V
9.267	0.3326	0.56	.Q	V
9.283	0.3333	0.56	.Q	V
9.300	0.3341	0.56	.Q	V
9.317	0.3349	0.56	.Q	V
9.333	0.3357	0.56	.Q	V
9.350	0.3364	0.56	.Q	V
9.367	0.3372	0.56	.Q	V
9.383	0.3380	0.57	.Q	V
9.400	0.3388	0.57	.Q	V
9.417	0.3396	0.57	.Q	V
9.433	0.3403	0.57	.Q	V
9.450	0.3411	0.57	.Q	V
9.467	0.3419	0.57	.Q	V
9.483	0.3427	0.57	.Q	V
9.500	0.3435	0.57	.Q	V
9.517	0.3443	0.57	.Q	V
9.533	0.3450	0.57	.Q	V
9.550	0.3458	0.57	.Q	V
9.567	0.3466	0.57	.Q	V.
9.583	0.3474	0.57	.Q	V.
9.600	0.3482	0.57	.Q	V.
9.617	0.3490	0.57	.Q	V.
9.633	0.3498	0.58	.Q	V.
9.650	0.3506	0.58	.Q	V.
9.667	0.3514	0.58	.Q	V.
9.683	0.3522	0.58	.Q	V.
9.700	0.3530	0.58	.Q	V.
9.717	0.3538	0.58	.Q	V.
9.733	0.3546	0.58	.Q	V.
9.750	0.3554	0.58	.Q	V.
9.767	0.3562	0.58	.Q	V.
9.783	0.3570	0.58	.Q	V.
9.800	0.3578	0.58	.Q	V.
9.817	0.3586	0.58	.Q	V.
9.833	0.3594	0.59	.Q	V.
9.850	0.3602	0.59	.Q	V.
9.867	0.3610	0.59	.Q	V.
9.883	0.3618	0.59	.Q	V.
9.900	0.3626	0.59	.Q	V.
9.917	0.3634	0.59	.Q	V.
9.933	0.3642	0.59	.Q	V.
9.950	0.3650	0.59	.Q	V.
9.967	0.3659	0.59	.Q	V.
9.983	0.3667	0.59	.Q	V.
10.000	0.3675	0.59	.Q	V.
10.017	0.3683	0.59	.Q	V.
10.033	0.3691	0.59	.Q	V.

10.050	0.3699	0.59	.Q	V.	.	.	.
10.067	0.3708	0.60	.Q	V.	.	.	.
10.083	0.3716	0.60	.Q	V.	.	.	.
10.100	0.3724	0.60	.Q	V.	.	.	.
10.117	0.3732	0.60	.Q	V.	.	.	.
10.133	0.3740	0.60	.Q	V.	.	.	.
10.150	0.3749	0.60	.Q	V.	.	.	.
10.167	0.3757	0.60	.Q	V.	.	.	.
10.183	0.3765	0.60	.Q	V.	.	.	.
10.200	0.3774	0.60	.Q	V.	.	.	.
10.217	0.3782	0.60	.Q	V.	.	.	.
10.233	0.3790	0.61	.Q	V.	.	.	.
10.250	0.3799	0.61	.Q	V.	.	.	.
10.267	0.3807	0.61	.Q	V.	.	.	.
10.283	0.3815	0.61	.Q	V.	.	.	.
10.300	0.3824	0.61	.Q	V.	.	.	.
10.317	0.3832	0.61	.Q	V.	.	.	.
10.333	0.3841	0.61	.Q	V.	.	.	.
10.350	0.3849	0.61	.Q	V.	.	.	.
10.367	0.3857	0.61	.Q	V	.	.	.
10.383	0.3866	0.61	.Q	V	.	.	.
10.400	0.3874	0.61	.Q	V	.	.	.
10.417	0.3883	0.61	.Q	V	.	.	.
10.433	0.3891	0.61	.Q	V	.	.	.
10.450	0.3899	0.61	.Q	V	.	.	.
10.467	0.3908	0.62	.Q	V	.	.	.
10.483	0.3916	0.62	.Q	V	.	.	.
10.500	0.3925	0.62	.Q	V	.	.	.
10.517	0.3933	0.62	.Q	V	.	.	.
10.533	0.3942	0.62	.Q	V	.	.	.
10.550	0.3951	0.62	.Q	V	.	.	.
10.567	0.3959	0.62	.Q	V	.	.	.
10.583	0.3968	0.62	.Q	V	.	.	.
10.600	0.3976	0.63	.Q	V	.	.	.
10.617	0.3985	0.63	.Q	V	.	.	.
10.633	0.3994	0.63	.Q	V	.	.	.
10.650	0.4002	0.63	.Q	V	.	.	.
10.667	0.4011	0.63	.Q	V	.	.	.
10.683	0.4020	0.63	.Q	V	.	.	.
10.700	0.4028	0.63	.Q	V	.	.	.
10.717	0.4037	0.63	.Q	V	.	.	.
10.733	0.4046	0.63	.Q	V	.	.	.
10.750	0.4054	0.63	.Q	V	.	.	.
10.767	0.4063	0.63	.Q	V	.	.	.
10.783	0.4072	0.63	.Q	V	.	.	.
10.800	0.4081	0.63	.Q	V	.	.	.
10.817	0.4089	0.63	.Q	V	.	.	.
10.833	0.4098	0.64	.Q	V	.	.	.
10.850	0.4107	0.64	.Q	V	.	.	.
10.867	0.4116	0.64	.Q	V	.	.	.

10.883	0.4124	0.64	.Q	V
10.900	0.4133	0.64	.Q	V
10.917	0.4142	0.64	.Q	V
10.933	0.4151	0.64	.Q	V
10.950	0.4160	0.64	.Q	V
10.967	0.4169	0.65	.Q	V
10.983	0.4178	0.65	.Q	V
11.000	0.4187	0.65	.Q	V
11.017	0.4196	0.65	.Q	V
11.033	0.4205	0.65	.Q	V
11.050	0.4214	0.65	.Q	V
11.067	0.4223	0.65	.Q	V
11.083	0.4232	0.65	.Q	V
11.100	0.4241	0.66	.Q	.V
11.117	0.4250	0.66	.Q	.V
11.133	0.4259	0.66	.Q	.V
11.150	0.4268	0.66	.Q	.V
11.167	0.4277	0.66	.Q	.V
11.183	0.4286	0.66	.Q	.V
11.200	0.4295	0.66	.Q	.V
11.217	0.4304	0.66	.Q	.V
11.233	0.4313	0.66	.Q	.V
11.250	0.4322	0.66	.Q	.V
11.267	0.4331	0.66	.Q	.V
11.283	0.4341	0.66	.Q	.V
11.300	0.4350	0.67	.Q	.V
11.317	0.4359	0.67	.Q	.V
11.333	0.4368	0.67	.Q	.V
11.350	0.4377	0.67	.Q	.V
11.367	0.4387	0.67	.Q	.V
11.383	0.4396	0.67	.Q	.V
11.400	0.4405	0.68	.Q	.V
11.417	0.4415	0.68	.Q	.V
11.433	0.4424	0.68	.Q	.V
11.450	0.4433	0.68	.Q	.V
11.467	0.4443	0.68	.Q	.V
11.483	0.4452	0.68	.Q	.V
11.500	0.4461	0.68	.Q	.V
11.517	0.4471	0.69	.Q	.V
11.533	0.4480	0.69	.Q	.V
11.550	0.4490	0.69	.Q	.V
11.567	0.4499	0.69	.Q	.V
11.583	0.4509	0.69	.Q	.V
11.600	0.4518	0.69	.Q	.V
11.617	0.4528	0.69	.Q	.V
11.633	0.4537	0.69	.Q	.V
11.650	0.4547	0.69	.Q	.V
11.667	0.4556	0.69	.Q	.V
11.683	0.4566	0.69	.Q	.V
11.700	0.4575	0.69	.Q	.V

11.717	0.4585	0.70	.Q	.V	.	.	.
11.733	0.4595	0.70	.Q	.V	.	.	.
11.750	0.4604	0.70	.Q	.V	.	.	.
11.767	0.4614	0.70	.Q	.V	.	.	.
11.783	0.4624	0.70	.Q	. V	.	.	.
11.800	0.4633	0.70	.Q	. V	.	.	.
11.817	0.4643	0.71	.Q	. V	.	.	.
11.833	0.4653	0.71	.Q	. V	.	.	.
11.850	0.4663	0.71	.Q	. V	.	.	.
11.867	0.4672	0.71	.Q	. V	.	.	.
11.883	0.4682	0.71	.Q	. V	.	.	.
11.900	0.4692	0.72	.Q	. V	.	.	.
11.917	0.4702	0.72	.Q	. V	.	.	.
11.933	0.4712	0.72	.Q	. V	.	.	.
11.950	0.4722	0.72	.Q	. V	.	.	.
11.967	0.4732	0.72	.Q	. V	.	.	.
11.983	0.4742	0.72	.Q	. V	.	.	.
12.000	0.4752	0.72	.Q	. V	.	.	.
12.017	0.4762	0.72	.Q	. V	.	.	.
12.033	0.4772	0.72	.Q	. V	.	.	.
12.050	0.4782	0.73	.Q	. V	.	.	.
12.067	0.4792	0.73	.Q	. V	.	.	.
12.083	0.4802	0.73	.Q	. V	.	.	.
12.100	0.4812	0.73	.Q	. V	.	.	.
12.117	0.4822	0.73	.Q	. V	.	.	.
12.133	0.4832	0.73	.Q	. V	.	.	.
12.150	0.4842	0.73	.Q	. V	.	.	.
12.167	0.4852	0.73	.Q	. V	.	.	.
12.183	0.4862	0.73	.Q	. V	.	.	.
12.200	0.4872	0.73	.Q	. V	.	.	.
12.217	0.4882	0.73	.Q	. V	.	.	.
12.233	0.4892	0.73	.Q	. V	.	.	.
12.250	0.4902	0.73	.Q	. V	.	.	.
12.267	0.4912	0.73	.Q	. V	.	.	.
12.283	0.4922	0.73	.Q	. V	.	.	.
12.300	0.4932	0.73	.Q	. V	.	.	.
12.317	0.4942	0.73	.Q	. V	.	.	.
12.333	0.4952	0.73	.Q	. V	.	.	.
12.350	0.4963	0.73	.Q	. V	.	.	.
12.367	0.4973	0.73	.Q	. V	.	.	.
12.383	0.4983	0.73	.Q	. V	.	.	.
12.400	0.4993	0.73	.Q	. V	.	.	.
12.417	0.5003	0.73	.Q	. V	.	.	.
12.433	0.5013	0.74	.Q	. V	.	.	.
12.450	0.5023	0.74	.Q	. V	.	.	.
12.467	0.5033	0.74	.Q	. V	.	.	.
12.483	0.5043	0.74	.Q	. V	.	.	.
12.500	0.5054	0.74	.Q	. V	.	.	.
12.517	0.5064	0.74	.Q	. V	.	.	.
12.533	0.5074	0.74	.Q	. V	.	.	.

12.550	0.5084	0.74	.Q	.	V	.	.	.
12.567	0.5095	0.74	.Q	.	V	.	.	.
12.583	0.5105	0.75	.Q	.	V	.	.	.
12.600	0.5115	0.75	.Q	.	V	.	.	.
12.617	0.5126	0.75	.Q	.	V	.	.	.
12.633	0.5136	0.75	.Q	.	V	.	.	.
12.650	0.5146	0.76	.Q	.	V	.	.	.
12.667	0.5157	0.76	.Q	.	V	.	.	.
12.683	0.5167	0.76	.Q	.	V	.	.	.
12.700	0.5178	0.76	.Q	.	V	.	.	.
12.717	0.5188	0.77	.Q	.	V	.	.	.
12.733	0.5199	0.77	.Q	.	V	.	.	.
12.750	0.5210	0.77	.Q	.	V	.	.	.
12.767	0.5220	0.77	.Q	.	V	.	.	.
12.783	0.5231	0.78	.Q	.	V	.	.	.
12.800	0.5242	0.78	.Q	.	V	.	.	.
12.817	0.5253	0.78	.Q	.	V	.	.	.
12.833	0.5263	0.78	.Q	.	V	.	.	.
12.850	0.5274	0.78	.Q	.	V	.	.	.
12.867	0.5285	0.78	.Q	.	V	.	.	.
12.883	0.5296	0.79	.Q	.	V	.	.	.
12.900	0.5307	0.79	.Q	.	V	.	.	.
12.917	0.5317	0.79	.Q	.	V	.	.	.
12.933	0.5328	0.79	.Q	.	V	.	.	.
12.950	0.5339	0.79	.Q	.	V	.	.	.
12.967	0.5350	0.79	.Q	.	V	.	.	.
12.983	0.5361	0.79	.Q	.	V	.	.	.
13.000	0.5372	0.80	.Q	.	V	.	.	.
13.017	0.5383	0.80	.Q	.	V	.	.	.
13.033	0.5394	0.80	.Q	.	V	.	.	.
13.050	0.5405	0.80	.Q	.	V	.	.	.
13.067	0.5416	0.81	.Q	.	V	.	.	.
13.083	0.5427	0.81	.Q	.	V	.	.	.
13.100	0.5439	0.81	.Q	.	V	.	.	.
13.117	0.5450	0.82	.Q	.	V	.	.	.
13.133	0.5461	0.82	.Q	.	V	.	.	.
13.150	0.5472	0.82	.Q	.	V	.	.	.
13.167	0.5484	0.83	.Q	.	V	.	.	.
13.183	0.5495	0.83	.Q	.	V	.	.	.
13.200	0.5507	0.83	.Q	.	V	.	.	.
13.217	0.5518	0.84	.Q	.	V	.	.	.
13.233	0.5530	0.84	.Q	.	V	.	.	.
13.250	0.5541	0.84	.Q	.	V	.	.	.
13.267	0.5553	0.84	.Q	.	V	.	.	.
13.283	0.5565	0.84	.Q	.	V	.	.	.
13.300	0.5576	0.84	.Q	.	V	.	.	.
13.317	0.5588	0.85	.Q	.	V	.	.	.
13.333	0.5599	0.85	.Q	.	V	.	.	.
13.350	0.5611	0.85	.Q	.	V	.	.	.
13.367	0.5623	0.85	.Q	.	V	.	.	.

13.383	0.5635	0.85	.Q	.	V	.	.	.
13.400	0.5646	0.85	.Q	.	V	.	.	.
13.417	0.5658	0.86	.Q	.	V	.	.	.
13.433	0.5670	0.86	.Q	.	V	.	.	.
13.450	0.5682	0.86	.Q	.	V	.	.	.
13.467	0.5694	0.87	.Q	.	V	.	.	.
13.483	0.5706	0.87	.Q	.	V	.	.	.
13.500	0.5718	0.87	.Q	.	V	.	.	.
13.517	0.5730	0.88	.Q	.	V	.	.	.
13.533	0.5742	0.88	.Q	.	V	.	.	.
13.550	0.5754	0.89	.Q	.	V	.	.	.
13.567	0.5767	0.89	.Q	.	V	.	.	.
13.583	0.5779	0.89	.Q	.	V	.	.	.
13.600	0.5791	0.90	.Q	.	V	.	.	.
13.617	0.5804	0.90	.Q	.	V	.	.	.
13.633	0.5816	0.91	.Q	.	V	.	.	.
13.650	0.5829	0.91	.Q	.	V	.	.	.
13.667	0.5841	0.91	.Q	.	V	.	.	.
13.683	0.5854	0.91	.Q	.	V	.	.	.
13.700	0.5866	0.91	.Q	.	V	.	.	.
13.717	0.5879	0.92	.Q	.	V	.	.	.
13.733	0.5892	0.92	.Q	.	V	.	.	.
13.750	0.5904	0.92	.Q	.	V	.	.	.
13.767	0.5917	0.92	.Q	.	V	.	.	.
13.783	0.5930	0.93	.Q	.	V	.	.	.
13.800	0.5943	0.93	.Q	.	V	.	.	.
13.817	0.5955	0.93	.Q	.	V	.	.	.
13.833	0.5968	0.93	.Q	.	V	.	.	.
13.850	0.5981	0.93	.Q	.	V	.	.	.
13.867	0.5994	0.94	.Q	.	V	.	.	.
13.883	0.6007	0.94	.Q	.	V	.	.	.
13.900	0.6020	0.95	.Q	.	V	.	.	.
13.917	0.6033	0.95	.Q	.	V	.	.	.
13.933	0.6046	0.96	.Q	.	V	.	.	.
13.950	0.6060	0.96	.Q	.	V	.	.	.
13.967	0.6073	0.97	.Q	.	V	.	.	.
13.983	0.6086	0.97	.Q	.	V	.	.	.
14.000	0.6100	0.98	.Q	.	V	.	.	.
14.017	0.6114	0.98	.Q	.	V	.	.	.
14.033	0.6127	0.99	.Q	.	V	.	.	.
14.050	0.6141	0.99	.Q	.	V	.	.	.
14.067	0.6155	1.00	.Q	.	V	.	.	.
14.083	0.6168	1.00	.Q	.	V	.	.	.
14.100	0.6182	1.00	.Q	.	V	.	.	.
14.117	0.6196	1.00	.Q	.	V	.	.	.
14.133	0.6210	0.99	.Q	.	V	.	.	.
14.150	0.6223	0.99	.Q	.	V	.	.	.
14.167	0.6237	0.99	.Q	.	V	.	.	.
14.183	0.6250	0.99	.Q	.	V	.	.	.
14.200	0.6264	0.99	.Q	.	V	.	.	.

14.217	0.6278	0.98	.Q	.	V	.	.	.
14.233	0.6291	0.98	.Q	.	V	.	.	.
14.250	0.6305	0.98	.Q	.	V	.	.	.
14.267	0.6318	0.98	.Q	.	V	.	.	.
14.283	0.6331	0.97	.Q	.	V	.	.	.
14.300	0.6345	0.98	.Q	.	V	.	.	.
14.317	0.6358	0.99	.Q	.	V	.	.	.
14.333	0.6372	0.99	.Q	.	V	.	.	.
14.350	0.6386	1.00	.Q	.	V	.	.	.
14.367	0.6400	1.01	.Q	.	V	.	.	.
14.383	0.6414	1.01	.Q	.	V	.	.	.
14.400	0.6428	1.02	.Q	.	V	.	.	.
14.417	0.6442	1.03	.Q	.	V	.	.	.
14.433	0.6456	1.03	.Q	.	V	.	.	.
14.450	0.6470	1.04	.Q	.	V	.	.	.
14.467	0.6485	1.05	.Q	.	V	.	.	.
14.483	0.6499	1.05	.Q	.	V	.	.	.
14.500	0.6514	1.06	.Q	.	V	.	.	.
14.517	0.6529	1.06	.Q	.	V	.	.	.
14.533	0.6543	1.07	.Q	.	V	.	.	.
14.550	0.6558	1.07	.Q	.	V	.	.	.
14.567	0.6573	1.08	.Q	.	V	.	.	.
14.583	0.6588	1.08	.Q	.	V	.	.	.
14.600	0.6603	1.09	.Q	.	V	.	.	.
14.617	0.6618	1.09	.Q	.	V	.	.	.
14.633	0.6633	1.09	.Q	.	V	.	.	.
14.650	0.6648	1.10	.Q	.	V	.	.	.
14.667	0.6663	1.10	.Q	.	V	.	.	.
14.683	0.6678	1.11	.Q	.	V	.	.	.
14.700	0.6694	1.11	.Q	.	V	.	.	.
14.717	0.6709	1.12	.Q	.	V	.	.	.
14.733	0.6725	1.13	.Q	.	V	.	.	.
14.750	0.6740	1.14	.Q	.	V	.	.	.
14.767	0.6756	1.15	.Q	.	V	.	.	.
14.783	0.6772	1.16	.Q	.	V	.	.	.
14.800	0.6788	1.17	.Q	.	V	.	.	.
14.817	0.6805	1.18	.Q	.	V	.	.	.
14.833	0.6821	1.19	.Q	.	V	.	.	.
14.850	0.6837	1.20	.Q	.	V	.	.	.
14.867	0.6854	1.21	.Q	.	V	.	.	.
14.883	0.6871	1.22	.Q	.	V	.	.	.
14.900	0.6888	1.23	.Q	.	V	.	.	.
14.917	0.6905	1.25	.Q	.	V	.	.	.
14.933	0.6923	1.26	.Q	.	V	.	.	.
14.950	0.6940	1.26	.Q	.	V	.	.	.
14.967	0.6957	1.27	.Q	.	V	.	.	.
14.983	0.6975	1.28	.Q	.	V	.	.	.
15.000	0.6993	1.28	.Q	.	V	.	.	.
15.017	0.7010	1.29	.Q	.	V	.	.	.
15.033	0.7028	1.30	.Q	.	V	.	.	.

15.050	0.7046	1.31	.	Q	.	V	.	.	.
15.067	0.7064	1.31	.	Q	.	V	.	.	.
15.083	0.7083	1.32	.	Q	.	V	.	.	.
15.100	0.7101	1.33	.	Q	.	V	.	.	.
15.117	0.7119	1.33	.	Q	.	V	.	.	.
15.133	0.7138	1.34	.	Q	.	V	.	.	.
15.150	0.7156	1.35	.	Q	.	V	.	.	.
15.167	0.7175	1.37	.	Q	.	V	.	.	.
15.183	0.7194	1.39	.	Q	.	V	.	.	.
15.200	0.7214	1.41	.	Q	.	V	.	.	.
15.217	0.7233	1.43	.	Q	.	V	.	.	.
15.233	0.7253	1.45	.	Q	.	V	.	.	.
15.250	0.7274	1.47	.	Q	.	V	.	.	.
15.267	0.7294	1.49	.	Q	.	V	.	.	.
15.283	0.7315	1.51	.	Q	.	V	.	.	.
15.300	0.7336	1.53	.	Q	.	V.	.	.	.
15.317	0.7357	1.55	.	Q	.	V.	.	.	.
15.333	0.7379	1.57	.	Q	.	V.	.	.	.
15.350	0.7401	1.59	.	Q	.	V.	.	.	.
15.367	0.7423	1.61	.	Q	.	V.	.	.	.
15.383	0.7446	1.67	.	Q	.	V.	.	.	.
15.400	0.7469	1.72	.	Q	.	V.	.	.	.
15.417	0.7494	1.77	.	Q	.	V.	.	.	.
15.433	0.7519	1.82	.	Q	.	V.	.	.	.
15.450	0.7545	1.87	.	Q	.	V.	.	.	.
15.467	0.7571	1.92	.	Q	.	V.	.	.	.
15.483	0.7598	1.98	.	Q	.	V.	.	.	.
15.500	0.7626	2.03	.	Q	.	V.	.	.	.
15.517	0.7655	2.08	.	Q	.	V.	.	.	.
15.533	0.7684	2.13	.	Q	.	V.	.	.	.
15.550	0.7714	2.18	.	Q	.	V	.	.	.
15.567	0.7745	2.23	.	Q	.	V	.	.	.
15.583	0.7777	2.29	.	Q	.	V	.	.	.
15.600	0.7809	2.35	.	Q	.	V	.	.	.
15.617	0.7842	2.41	.	Q	.	V	.	.	.
15.633	0.7876	2.47	.	Q	.	V	.	.	.
15.650	0.7911	2.53	.	Q	.	V	.	.	.
15.667	0.7947	2.59	.	Q	.	V	.	.	.
15.683	0.7983	2.65	.	Q	.	V	.	.	.
15.700	0.8020	2.71	.	Q	.	V	.	.	.
15.717	0.8058	2.76	.	Q	.	V	.	.	.
15.733	0.8097	2.82	.	Q	.	.V	.	.	.
15.750	0.8137	2.88	.	Q	.	.V	.	.	.
15.767	0.8178	2.94	.	Q	.	.V	.	.	.
15.783	0.8219	3.00	.	Q	.	.V	.	.	.
15.800	0.8261	3.06	.	Q	.	.V	.	.	.
15.817	0.8304	3.12	.	Q	.	.V	.	.	.
15.833	0.8348	3.18	.	Q	.	.V	.	.	.
15.850	0.8392	3.24	.	Q	.	.V	.	.	.
15.867	0.8438	3.29	.	Q	.	.V	.	.	.

15.883	0.8484	3.35	.	Q	.	.	V	.	.
15.900	0.8531	3.41	.	Q	.	.	V	.	.
15.917	0.8579	3.47	.	Q	.	.	V	.	.
15.933	0.8627	3.53	.	Q	.	.	V	.	.
15.950	0.8677	3.58	.	Q	.	.	V	.	.
15.967	0.8727	3.64	.	Q	.	.	V	.	.
15.983	0.8778	3.70	.	Q	.	.	V	.	.
16.000	0.8830	3.76	.	Q	.	.	V	.	.
16.017	0.8886	4.06	.	Q	.	.	V	.	.
16.033	0.8949	4.61	.	Q.	.	.	V	.	.
16.050	0.9020	5.16	.	Q	.	.	V	.	.
16.067	0.9099	5.71	.	.Q	.	.	V	.	.
16.083	0.9185	6.26	.	.Q	.	.	V	.	.
16.100	0.9279	6.81	.	.Q	.	.	V	.	.
16.117	0.9380	7.36	.	.Q	.	.	V	.	.
16.133	0.9489	7.91	.	.Q	.	.	V	.	.
16.150	0.9606	8.46	.	.Q	.	.	V	.	.
16.167	0.9730	9.01	.	.Q	.	.	V	.	.
16.183	0.9862	9.56	.	.Q	.	.	V	.	.
16.200	1.0001	10.11	.	.Q	.	.	V	.	.
16.217	1.0151	10.89	.	.Q	.	.	V	.	.
16.233	1.0296	10.52	.	.Q	.	.	V	.	.
16.250	1.0432	9.89	.	.Q	.	.	V	.	.
16.267	1.0560	9.26	.	.Q	.	.	V	.	.
16.283	1.0679	8.63	.	.Q	.	.	V	.	.
16.300	1.0789	8.01	.	.Q	.	.	V	.	.
16.317	1.0891	7.38	.	.Q	.	.	V	.	.
16.333	1.0984	6.75	.	.Q	.	.	V	.	.
16.350	1.1068	6.12	.	.Q	.	.	V	.	.
16.367	1.1144	5.49	.	.Q	.	.	V	.	.
16.383	1.1211	4.87	.	.Q	.	.	V	.	.
16.400	1.1269	4.24	.	.Q	.	.	V	.	.
16.417	1.1319	3.61	.	.Q	.	.	V	.	.
16.433	1.1360	2.99	.	.Q	.	.	V	.	.
16.450	1.1397	2.71	.	.Q	.	.	V	.	.
16.467	1.1433	2.61	.	.Q	.	.	V	.	.
16.483	1.1468	2.51	.	.Q	.	.	V	.	.
16.500	1.1501	2.40	.	.Q	.	.	V	.	.
16.517	1.1533	2.30	.	.Q	.	.	V	.	.
16.533	1.1563	2.20	.	.Q	.	.	V	.	.
16.550	1.1592	2.10	.	.Q	.	.	V	.	.
16.567	1.1619	1.99	.	.Q	.	.	V	.	.
16.583	1.1645	1.89	.	.Q	.	.	V	.	.
16.600	1.1670	1.79	.	.Q	.	.	V	.	.
16.617	1.1693	1.69	.	.Q	.	.	V	.	.
16.633	1.1715	1.58	.	.Q	.	.	V	.	.
16.650	1.1736	1.49	.	.Q	.	.	V	.	.
16.667	1.1755	1.44	.	.Q	.	.	V	.	.
16.683	1.1775	1.42	.	.Q	.	.	V	.	.
16.700	1.1794	1.40	.	.Q	.	.	V	.	.

16.717	1.1813	1.38	. Q	.	.	V	.
16.733	1.1832	1.36	. Q	.	.	V	.
16.750	1.1850	1.33	. Q	.	.	V	.
16.767	1.1868	1.31	. Q	.	.	V	.
16.783	1.1886	1.29	. Q	.	.	V	.
16.800	1.1904	1.27	. Q	.	.	V	.
16.817	1.1921	1.25	. Q	.	.	V	.
16.833	1.1938	1.23	. Q	.	.	.V	.
16.850	1.1954	1.20	. Q	.	.	.V	.
16.867	1.1971	1.18	. Q	.	.	.V	.
16.883	1.1987	1.17	. Q	.	.	.V	.
16.900	1.2003	1.16	. Q	.	.	.V	.
16.917	1.2018	1.14	. Q	.	.	.V	.
16.933	1.2034	1.13	. Q	.	.	.V	.
16.950	1.2049	1.12	. Q	.	.	.V	.
16.967	1.2065	1.10	. Q	.	.	.V	.
16.983	1.2080	1.09	. Q	.	.	.V	.
17.000	1.2094	1.08	. Q	.	.	.V	.
17.017	1.2109	1.07	. Q	.	.	.V	.
17.033	1.2124	1.05	. Q	.	.	.V	.
17.050	1.2138	1.04	. Q	.	.	.V	.
17.067	1.2152	1.03	. Q	.	.	.V	.
17.083	1.2166	1.01	. Q	.	.	.V	.
17.100	1.2180	1.01	. Q	.	.	.V	.
17.117	1.2194	1.01	. Q	.	.	.V	.
17.133	1.2208	1.00	. Q	.	.	.V	.
17.150	1.2221	1.00	. Q	.	.	.V	.
17.167	1.2235	1.00	. Q	.	.	.V	.
17.183	1.2249	0.99	. Q	.	.	.V	.
17.200	1.2262	0.99	. Q	.	.	.V	.
17.217	1.2276	0.98	. Q	.	.	.V	.
17.233	1.2289	0.98	. Q	.	.	.V	.
17.250	1.2303	0.98	. Q	.	.	.V	.
17.267	1.2316	0.97	. Q	.	.	.V	.
17.283	1.2330	0.97	. Q	.	.	. V	.
17.300	1.2343	0.97	. Q	.	.	. V	.
17.317	1.2356	0.96	. Q	.	.	. V	.
17.333	1.2369	0.95	. Q	.	.	. V	.
17.350	1.2382	0.95	. Q	.	.	. V	.
17.367	1.2395	0.94	. Q	.	.	. V	.
17.383	1.2408	0.93	. Q	.	.	. V	.
17.400	1.2421	0.93	. Q	.	.	. V	.
17.417	1.2434	0.92	. Q	.	.	. V	.
17.433	1.2446	0.91	. Q	.	.	. V	.
17.450	1.2459	0.91	. Q	.	.	. V	.
17.467	1.2471	0.90	. Q	.	.	. V	.
17.483	1.2483	0.89	. Q	.	.	. V	.
17.500	1.2496	0.89	. Q	.	.	. V	.
17.517	1.2508	0.88	. Q	.	.	. V	.
17.533	1.2520	0.88	. Q	.	.	. V	.

17.550	1.2532	0.87	.Q	.	.	.	V	.
17.567	1.2544	0.86	.Q	.	.	.	V	.
17.583	1.2555	0.86	.Q	.	.	.	V	.
17.600	1.2567	0.85	.Q	.	.	.	V	.
17.617	1.2579	0.85	.Q	.	.	.	V	.
17.633	1.2591	0.84	.Q	.	.	.	V	.
17.650	1.2602	0.84	.Q	.	.	.	V	.
17.667	1.2614	0.83	.Q	.	.	.	V	.
17.683	1.2625	0.83	.Q	.	.	.	V	.
17.700	1.2636	0.82	.Q	.	.	.	V	.
17.717	1.2648	0.82	.Q	.	.	.	V	.
17.733	1.2659	0.81	.Q	.	.	.	V	.
17.750	1.2670	0.81	.Q	.	.	.	V	.
17.767	1.2681	0.80	.Q	.	.	.	V	.
17.783	1.2692	0.80	.Q	.	.	.	V	.
17.800	1.2703	0.80	.Q	.	.	.	V	.
17.817	1.2714	0.79	.Q	.	.	.	V	.
17.833	1.2725	0.79	.Q	.	.	.	V	.
17.850	1.2736	0.78	.Q	.	.	.	V	.
17.867	1.2746	0.78	.Q	.	.	.	V	.
17.883	1.2757	0.78	.Q	.	.	.	V	.
17.900	1.2768	0.77	.Q	.	.	.	V	.
17.917	1.2778	0.77	.Q	.	.	.	V	.
17.933	1.2789	0.76	.Q	.	.	.	V	.
17.950	1.2799	0.76	.Q	.	.	.	V	.
17.967	1.2810	0.76	.Q	.	.	.	V	.
17.983	1.2820	0.75	.Q	.	.	.	V	.
18.000	1.2830	0.75	.Q	.	.	.	V	.
18.017	1.2841	0.75	.Q	.	.	.	V	.
18.033	1.2851	0.74	.Q	.	.	.	V	.
18.050	1.2861	0.74	.Q	.	.	.	V	.
18.067	1.2871	0.74	.Q	.	.	.	V	.
18.083	1.2881	0.73	.Q	.	.	.	V	.
18.100	1.2891	0.73	.Q	.	.	.	V	.
18.117	1.2901	0.73	.Q	.	.	.	V	.
18.133	1.2911	0.72	.Q	.	.	.	V	.
18.150	1.2921	0.72	.Q	.	.	.	V	.
18.167	1.2931	0.72	.Q	.	.	.	V	.
18.183	1.2941	0.72	.Q	.	.	.	V	.
18.200	1.2951	0.72	.Q	.	.	.	V	.
18.217	1.2961	0.72	.Q	.	.	.	V	.
18.233	1.2971	0.71	.Q	.	.	.	V	.
18.250	1.2980	0.71	.Q	.	.	.	V	.
18.267	1.2990	0.71	.Q	.	.	.	V	.
18.283	1.3000	0.71	.Q	.	.	.	V	.
18.300	1.3010	0.71	.Q	.	.	.	V	.
18.317	1.3019	0.71	.Q	.	.	.	V	.
18.333	1.3029	0.71	.Q	.	.	.	V	.
18.350	1.3039	0.71	.Q	.	.	.	V	.
18.367	1.3049	0.71	.Q	.	.	.	V	.

18.383	1.3058	0.70	.Q	.	.	.	V	.
18.400	1.3068	0.70	.Q	.	.	.	V	.
18.417	1.3078	0.70	.Q	.	.	.	V	.
18.433	1.3087	0.70	.Q	.	.	.	V	.
18.450	1.3097	0.69	.Q	.	.	.	V	.
18.467	1.3106	0.69	.Q	.	.	.	V	.
18.483	1.3116	0.69	.Q	.	.	.	V	.
18.500	1.3125	0.69	.Q	.	.	.	V	.
18.517	1.3135	0.68	.Q	.	.	.	V	.
18.533	1.3144	0.68	.Q	.	.	.	V	.
18.550	1.3154	0.68	.Q	.	.	.	V	.
18.567	1.3163	0.68	.Q	.	.	.	V	.
18.583	1.3172	0.67	.Q	.	.	.	V	.
18.600	1.3181	0.67	.Q	.	.	.	V	.
18.617	1.3191	0.67	.Q	.	.	.	V	.
18.633	1.3200	0.67	.Q	.	.	.	V	.
18.650	1.3209	0.67	.Q	.	.	.	V	.
18.667	1.3218	0.66	.Q	.	.	.	V	.
18.683	1.3227	0.66	.Q	.	.	.	V	.
18.700	1.3236	0.66	.Q	.	.	.	V	.
18.717	1.3245	0.66	.Q	.	.	.	V	.
18.733	1.3254	0.65	.Q	.	.	.	V	.
18.750	1.3263	0.65	.Q	.	.	.	V	.
18.767	1.3272	0.65	.Q	.	.	.	V	.
18.783	1.3281	0.65	.Q	.	.	.	V	.
18.800	1.3290	0.65	.Q	.	.	.	V	.
18.817	1.3299	0.64	.Q	.	.	.	V	.
18.833	1.3308	0.64	.Q	.	.	.	V	.
18.850	1.3317	0.64	.Q	.	.	.	V	.
18.867	1.3325	0.64	.Q	.	.	.	V	.
18.883	1.3334	0.64	.Q	.	.	.	V	.
18.900	1.3343	0.63	.Q	.	.	.	V	.
18.917	1.3352	0.63	.Q	.	.	.	V	.
18.933	1.3360	0.63	.Q	.	.	.	V	.
18.950	1.3369	0.63	.Q	.	.	.	V	.
18.967	1.3378	0.63	.Q	.	.	.	V	.
18.983	1.3386	0.62	.Q	.	.	.	V	.
19.000	1.3395	0.62	.Q	.	.	.	V	.
19.017	1.3403	0.62	.Q	.	.	.	V	.
19.033	1.3412	0.62	.Q	.	.	.	V	.
19.050	1.3420	0.62	.Q	.	.	.	V	.
19.067	1.3429	0.61	.Q	.	.	.	V	.
19.083	1.3437	0.61	.Q	.	.	.	V	.
19.100	1.3446	0.61	.Q	.	.	.	V	.
19.117	1.3454	0.61	.Q	.	.	.	V	.
19.133	1.3462	0.61	.Q	.	.	.	V	.
19.150	1.3471	0.61	.Q	.	.	.	V	.
19.167	1.3479	0.60	.Q	.	.	.	V	.
19.183	1.3487	0.60	.Q	.	.	.	V	.
19.200	1.3496	0.60	.Q	.	.	.	V	.

19.217	1.3504	0.60	.Q	.	.	.	V	.
19.233	1.3512	0.60	.Q	.	.	.	V	.
19.250	1.3520	0.60	.Q	.	.	.	V	.
19.267	1.3528	0.59	.Q	.	.	.	V	.
19.283	1.3537	0.59	.Q	.	.	.	V	.
19.300	1.3545	0.59	.Q	.	.	.	V	.
19.317	1.3553	0.59	.Q	.	.	.	V	.
19.333	1.3561	0.59	.Q	.	.	.	V	.
19.350	1.3569	0.59	.Q	.	.	.	V	.
19.367	1.3577	0.58	.Q	.	.	.	V	.
19.383	1.3585	0.58	.Q	.	.	.	V	.
19.400	1.3593	0.58	.Q	.	.	.	V	.
19.417	1.3601	0.58	.Q	.	.	.	V	.
19.433	1.3609	0.58	.Q	.	.	.	V	.
19.450	1.3617	0.58	.Q	.	.	.	V	.
19.467	1.3625	0.58	.Q	.	.	.	V	.
19.483	1.3633	0.57	.Q	.	.	.	V	.
19.500	1.3641	0.57	.Q	.	.	.	V	.
19.517	1.3649	0.57	.Q	.	.	.	V	.
19.533	1.3656	0.57	.Q	.	.	.	V	.
19.550	1.3664	0.57	.Q	.	.	.	V	.
19.567	1.3672	0.57	.Q	.	.	.	V	.
19.583	1.3680	0.57	.Q	.	.	.	V	.
19.600	1.3688	0.56	.Q	.	.	.	V	.
19.617	1.3695	0.56	.Q	.	.	.	V	.
19.633	1.3703	0.56	.Q	.	.	.	V	.
19.650	1.3711	0.56	.Q	.	.	.	V	.
19.667	1.3718	0.56	.Q	.	.	.	V	.
19.683	1.3726	0.56	.Q	.	.	.	V	.
19.700	1.3734	0.56	.Q	.	.	.	V	.
19.717	1.3741	0.55	.Q	.	.	.	V	.
19.733	1.3749	0.55	.Q	.	.	.	V	.
19.750	1.3757	0.55	.Q	.	.	.	V	.
19.767	1.3764	0.55	.Q	.	.	.	V	.
19.783	1.3772	0.55	.Q	.	.	.	V	.
19.800	1.3779	0.55	.Q	.	.	.	V	.
19.817	1.3787	0.55	.Q	.	.	.	V	.
19.833	1.3794	0.55	.Q	.	.	.	V	.
19.850	1.3802	0.54	.Q	.	.	.	V	.
19.867	1.3809	0.54	.Q	.	.	.	V	.
19.883	1.3817	0.54	.Q	.	.	.	V	.
19.900	1.3824	0.54	.Q	.	.	.	V	.
19.917	1.3832	0.54	.Q	.	.	.	V	.
19.933	1.3839	0.54	.Q	.	.	.	V	.
19.950	1.3846	0.54	.Q	.	.	.	V	.
19.967	1.3854	0.54	.Q	.	.	.	V	.
19.983	1.3861	0.53	.Q	.	.	.	V	.
20.000	1.3869	0.53	.Q	.	.	.	V	.
20.017	1.3876	0.53	.Q	.	.	.	V	.
20.033	1.3883	0.53	.Q	.	.	.	V	.

20.050	1.3890	0.53	.Q	.	.	.	V	.
20.067	1.3898	0.53	.Q	.	.	.	V	.
20.083	1.3905	0.53	.Q	.	.	.	V	.
20.100	1.3912	0.53	.Q	.	.	.	V	.
20.117	1.3919	0.52	.Q	.	.	.	V	.
20.133	1.3927	0.52	.Q	.	.	.	V	.
20.150	1.3934	0.52	.Q	.	.	.	V	.
20.167	1.3941	0.52	.Q	.	.	.	V	.
20.183	1.3948	0.52	.Q	.	.	.	V	.
20.200	1.3955	0.52	.Q	.	.	.	V	.
20.217	1.3963	0.52	.Q	.	.	.	V	.
20.233	1.3970	0.52	.Q	.	.	.	V	.
20.250	1.3977	0.52	.Q	.	.	.	V	.
20.267	1.3984	0.52	.Q	.	.	.	V	.
20.283	1.3991	0.51	.Q	.	.	.	V	.
20.300	1.3998	0.51	.Q	.	.	.	V	.
20.317	1.4005	0.51	.Q	.	.	.	V	.
20.333	1.4012	0.51	.Q	.	.	.	V	.
20.350	1.4019	0.51	.Q	.	.	.	V	.
20.367	1.4026	0.51	.Q	.	.	.	V	.
20.383	1.4033	0.51	.Q	.	.	.	V	.
20.400	1.4040	0.51	.Q	.	.	.	V	.
20.417	1.4047	0.51	.Q	.	.	.	V	.
20.433	1.4054	0.50	.Q	.	.	.	V	.
20.450	1.4061	0.50	.Q	.	.	.	V	.
20.467	1.4068	0.50	.Q	.	.	.	V	.
20.483	1.4075	0.50	.Q	.	.	.	V	.
20.500	1.4082	0.50	.Q	.	.	.	V	.
20.517	1.4089	0.50	Q	.	.	.	V	.
20.533	1.4095	0.50	Q	.	.	.	V	.
20.550	1.4102	0.50	Q	.	.	.	V	.
20.567	1.4109	0.50	Q	.	.	.	V	.
20.583	1.4116	0.50	Q	.	.	.	V	.
20.600	1.4123	0.50	Q	.	.	.	V	.
20.617	1.4130	0.49	Q	.	.	.	V	.
20.633	1.4136	0.49	Q	.	.	.	V	.
20.650	1.4143	0.49	Q	.	.	.	V	.
20.667	1.4150	0.49	Q	.	.	.	V	.
20.683	1.4157	0.49	Q	.	.	.	V	.
20.700	1.4163	0.49	Q	.	.	.	V	.
20.717	1.4170	0.49	Q	.	.	.	V	.
20.733	1.4177	0.49	Q	.	.	.	V	.
20.750	1.4184	0.49	Q	.	.	.	V	.
20.767	1.4190	0.49	Q	.	.	.	V	.
20.783	1.4197	0.48	Q	.	.	.	V	.
20.800	1.4204	0.48	Q	.	.	.	V	.
20.817	1.4210	0.48	Q	.	.	.	V	.
20.833	1.4217	0.48	Q	.	.	.	V	.
20.850	1.4224	0.48	Q	.	.	.	V	.
20.867	1.4230	0.48	Q	.	.	.	V	.

20.883	1.4237	0.48	Q	V	.
20.900	1.4243	0.48	Q	V	.
20.917	1.4250	0.48	Q	V	.
20.933	1.4257	0.48	Q	V	.
20.950	1.4263	0.48	Q	V	.
20.967	1.4270	0.48	Q	V	.
20.983	1.4276	0.47	Q	V	.
21.000	1.4283	0.47	Q	V	.
21.017	1.4289	0.47	Q	V	.
21.033	1.4296	0.47	Q	V	.
21.050	1.4302	0.47	Q	V	.
21.067	1.4309	0.47	Q	V	.
21.083	1.4315	0.47	Q	V	.
21.100	1.4322	0.47	Q	V	.
21.117	1.4328	0.47	Q	V	.
21.133	1.4335	0.47	Q	V	.
21.150	1.4341	0.47	Q	V	.
21.167	1.4347	0.47	Q	V	.
21.183	1.4354	0.46	Q	V	.
21.200	1.4360	0.46	Q	V	.
21.217	1.4367	0.46	Q	V	.
21.233	1.4373	0.46	Q	V	.
21.250	1.4379	0.46	Q	V	.
21.267	1.4386	0.46	Q	V	.
21.283	1.4392	0.46	Q	V	.
21.300	1.4398	0.46	Q	V	.
21.317	1.4405	0.46	Q	V	.
21.333	1.4411	0.46	Q	V	.
21.350	1.4417	0.46	Q	V	.
21.367	1.4424	0.46	Q	V	.
21.383	1.4430	0.46	Q	V	.
21.400	1.4436	0.45	Q	V	.
21.417	1.4442	0.45	Q	V	.
21.433	1.4449	0.45	Q	V	.
21.450	1.4455	0.45	Q	V	.
21.467	1.4461	0.45	Q	V	.
21.483	1.4467	0.45	Q	V	.
21.500	1.4473	0.45	Q	V	.
21.517	1.4480	0.45	Q	V	.
21.533	1.4486	0.45	Q	V	.
21.550	1.4492	0.45	Q	V	.
21.567	1.4498	0.45	Q	V	.
21.583	1.4504	0.45	Q	V	.
21.600	1.4510	0.45	Q	V	.
21.617	1.4517	0.45	Q	V	.
21.633	1.4523	0.44	Q	V	.
21.650	1.4529	0.44	Q	V	.
21.667	1.4535	0.44	Q	V	.
21.683	1.4541	0.44	Q	V	.
21.700	1.4547	0.44	Q	V	.

21.717	1.4553	0.44	Q	V .
21.733	1.4559	0.44	Q	V .
21.750	1.4565	0.44	Q	V .
21.767	1.4571	0.44	Q	V .
21.783	1.4578	0.44	Q	V .
21.800	1.4584	0.44	Q	V .
21.817	1.4590	0.44	Q	V .
21.833	1.4596	0.44	Q	V .
21.850	1.4602	0.44	Q	V .
21.867	1.4608	0.44	Q	V .
21.883	1.4614	0.44	Q	V .
21.900	1.4620	0.43	Q	V .
21.917	1.4626	0.43	Q	V .
21.933	1.4632	0.43	Q	V .
21.950	1.4637	0.43	Q	V .
21.967	1.4643	0.43	Q	V .
21.983	1.4649	0.43	Q	V .
22.000	1.4655	0.43	Q	V .
22.017	1.4661	0.43	Q	V .
22.033	1.4667	0.43	Q	V .
22.050	1.4673	0.43	Q	V .
22.067	1.4679	0.43	Q	V .
22.083	1.4685	0.43	Q	V .
22.100	1.4691	0.43	Q	V .
22.117	1.4697	0.43	Q	V .
22.133	1.4702	0.43	Q	V .
22.150	1.4708	0.43	Q	V .
22.167	1.4714	0.42	Q	V .
22.183	1.4720	0.42	Q	V .
22.200	1.4726	0.42	Q	V .
22.217	1.4732	0.42	Q	V .
22.233	1.4737	0.42	Q	V .
22.250	1.4743	0.42	Q	V .
22.267	1.4749	0.42	Q	V .
22.283	1.4755	0.42	Q	V .
22.300	1.4761	0.42	Q	V .
22.317	1.4766	0.42	Q	V .
22.333	1.4772	0.42	Q	V .
22.350	1.4778	0.42	Q	V .
22.367	1.4784	0.42	Q	V .
22.383	1.4789	0.42	Q	V .
22.400	1.4795	0.42	Q	V .
22.417	1.4801	0.42	Q	V .
22.433	1.4807	0.42	Q	V .
22.450	1.4812	0.41	Q	V .
22.467	1.4818	0.41	Q	V .
22.483	1.4824	0.41	Q	V .
22.500	1.4829	0.41	Q	V .
22.517	1.4835	0.41	Q	V .
22.533	1.4841	0.41	Q	V .

22.550	1.4846	0.41	Q	V .
22.567	1.4852	0.41	Q	V .
22.583	1.4858	0.41	Q	V .
22.600	1.4863	0.41	Q	V .
22.617	1.4869	0.41	Q	V .
22.633	1.4875	0.41	Q	V .
22.650	1.4880	0.41	Q	V .
22.667	1.4886	0.41	Q	V .
22.683	1.4891	0.41	Q	V .
22.700	1.4897	0.41	Q	V .
22.717	1.4903	0.41	Q	V .
22.733	1.4908	0.41	Q	V .
22.750	1.4914	0.40	Q	V .
22.767	1.4919	0.40	Q	V .
22.783	1.4925	0.40	Q	V .
22.800	1.4930	0.40	Q	V .
22.817	1.4936	0.40	Q	V .
22.833	1.4942	0.40	Q	V .
22.850	1.4947	0.40	Q	V .
22.867	1.4953	0.40	Q	V .
22.883	1.4958	0.40	Q	V .
22.900	1.4964	0.40	Q	V .
22.917	1.4969	0.40	Q	V .
22.933	1.4975	0.40	Q	V .
22.950	1.4980	0.40	Q	V .
22.967	1.4986	0.40	Q	V .
22.983	1.4991	0.40	Q	V .
23.000	1.4997	0.40	Q	V .
23.017	1.5002	0.40	Q	V .
23.033	1.5008	0.40	Q	V .
23.050	1.5013	0.40	Q	V .
23.067	1.5018	0.40	Q	V.
23.083	1.5024	0.39	Q	V.
23.100	1.5029	0.39	Q	V.
23.117	1.5035	0.39	Q	V.
23.133	1.5040	0.39	Q	V.
23.150	1.5046	0.39	Q	V.
23.167	1.5051	0.39	Q	V.
23.183	1.5056	0.39	Q	V.
23.200	1.5062	0.39	Q	V.
23.217	1.5067	0.39	Q	V.
23.233	1.5073	0.39	Q	V.
23.250	1.5078	0.39	Q	V.
23.267	1.5083	0.39	Q	V.
23.283	1.5089	0.39	Q	V.
23.300	1.5094	0.39	Q	V.
23.317	1.5099	0.39	Q	V.
23.333	1.5105	0.39	Q	V.
23.350	1.5110	0.39	Q	V.
23.367	1.5115	0.39	Q	V.

23.383	1.5121	0.39	Q	.	.	.	V.
23.400	1.5126	0.39	Q	.	.	.	V.
23.417	1.5131	0.39	Q	.	.	.	V.
23.433	1.5137	0.39	Q	.	.	.	V.
23.450	1.5142	0.38	Q	.	.	.	V.
23.467	1.5147	0.38	Q	.	.	.	V.
23.483	1.5152	0.38	Q	.	.	.	V.
23.500	1.5158	0.38	Q	.	.	.	V.
23.517	1.5163	0.38	Q	.	.	.	V.
23.533	1.5168	0.38	Q	.	.	.	V.
23.550	1.5174	0.38	Q	.	.	.	V.
23.567	1.5179	0.38	Q	.	.	.	V.
23.583	1.5184	0.38	Q	.	.	.	V.
23.600	1.5189	0.38	Q	.	.	.	V.
23.617	1.5195	0.38	Q	.	.	.	V.
23.633	1.5200	0.38	Q	.	.	.	V.
23.650	1.5205	0.38	Q	.	.	.	V.
23.667	1.5210	0.38	Q	.	.	.	V.
23.683	1.5215	0.38	Q	.	.	.	V.
23.700	1.5221	0.38	Q	.	.	.	V.
23.717	1.5226	0.38	Q	.	.	.	V.
23.733	1.5231	0.38	Q	.	.	.	V.
23.750	1.5236	0.38	Q	.	.	.	V.
23.767	1.5241	0.38	Q	.	.	.	V.
23.783	1.5247	0.38	Q	.	.	.	V.
23.800	1.5252	0.38	Q	.	.	.	V.
23.817	1.5257	0.38	Q	.	.	.	V.
23.833	1.5262	0.37	Q	.	.	.	V.
23.850	1.5267	0.37	Q	.	.	.	V.
23.867	1.5272	0.37	Q	.	.	.	V.
23.883	1.5278	0.37	Q	.	.	.	V.
23.900	1.5283	0.37	Q	.	.	.	V.
23.917	1.5288	0.37	Q	.	.	.	V.
23.933	1.5293	0.37	Q	.	.	.	V.
23.950	1.5298	0.37	Q	.	.	.	V.
23.967	1.5303	0.37	Q	.	.	.	V.
23.983	1.5308	0.37	Q	.	.	.	V.
24.000	1.5313	0.37	Q	.	.	.	V.

TIME DURATION(minutes) OF PERCENTILES OF ESTIMATED PEAK FLOW RATE:

(Note: 100% of Peak Flow Rate estimate assumed to have
an instantaneous time duration)

Percentile of Estimated Peak Flow Rate	Duration (minutes)
=====	=====
0%	1441.0
10%	715.0
20%	300.0
30%	170.0

40%	110.0
50%	95.0
60%	75.0
70%	55.0
80%	35.0
90%	20.0

END OF FLOODSCx ROUTING ANALYSIS

Cherry Outpost								
(Proposed Condition) Small Area Hydrograph Loss Rates								
Subarea	Area (acres)	Soil Type	Land Use	A _p	A _i	F _p (in/hr) Adj. Infiltration Rate	F _m	Runoff Index (RI)
								100
								AMC P ₂₄ (Inches)
								II 5.87
A-1	0.218	A	Natural or Agriculture	1.00	0.00	0.742	0.74	32 0.004
A-1	0.010	C	Natural or Agriculture	1.00	0.00	0.373	0.37	69 0.004
A-1	1.664	A	Commercial	0.10	0.90	0.141	0.14	32 1.440
A-1	0.285	C	Commercial	0.10	0.90	0.071	0.07	69 0.259
A-1.1	0.327	A	Natural or Agriculture	1.00	0.00	0.742	0.74	32 0.006
A-1.1	0.254	C	Natural or Agriculture	1.00	0.00	0.373	0.37	69 0.113
A-1.1	0.673	A	Commercial	0.10	0.90	0.141	0.14	32 0.582
A-1.1	0.327	C	Commercial	0.10	0.90	0.071	0.07	69 0.297
A-2	0.108	A	Natural or Agriculture	1.00	0.00	0.742	0.74	32 0.002
A-2	0.432	C	Natural or Agriculture	1.00	0.00	0.373	0.37	69 0.192
A-2.1	0.006	A	Natural or Agriculture	1.00	0.00	0.742	0.74	32 0.000
A-2.1	0.015	C	Natural or Agriculture	1.00	0.00	0.373	0.37	69 0.007
A-2.1	0.158	A	Commercial	0.10	0.90	0.141	0.14	32 0.137
A-2.1	0.712	C	Commercial	0.10	0.90	0.071	0.07	69 0.646
A-2.2	0.025	A	Natural or Agriculture	1.00	0.00	0.742	0.74	32 0.000
A-2.2	0.096	A	Commercial	0.10	0.90	0.141	0.14	32 0.083
A-2.2	0.064	C	Commercial	0.10	0.90	0.071	0.07	69 0.058
A-2.3	0.063	A	Natural or Agriculture	1.00	0.00	0.742	0.74	32 0.001
A-2.3	0.059	C	Natural or Agriculture	1.00	0.00	0.373	0.37	69 0.026
A-2.3	0.166	A	Commercial	0.10	0.90	0.141	0.14	32 0.144
A-2.3	0.287	C	Commercial	0.10	0.90	0.071	0.07	69 0.261
Total =	5.95						0.227	0.283

Cherry Outpost	
(Proposed Condition) Loss Rates Summary	
	STORM EVENT
	100-YR
Tc =	11.180
Area =	5.949
ȳ =	0.283
F _m =	0.227

PROPOSED BASIN A

Rating Table

	Stage (feet)	Depth (feet)	Headwater Elevation* (ft)	Surface Area (ft ²)	Surface Area (acres)	Storage Volume (ac-ft)		Storage Volume (ft ³)	Outlet Discharge (cfs)
						i	S		
1	1396.00	0.00	0.00	3697	0.08		0.00	0	0.0
2	1396.50	0.50	0.00	4149	0.10	0.045	0.045	1961	0.0
3	1397.00	1.00	0.50	4821	0.11	0.051	0.097	4204	2.7
4	1398.00	2.00	1.50	6155	0.14	0.126	0.222	9692	4.8
5	1399.00	3.00	2.50	7535	0.17	0.157	0.380	16537	6.1
6	1400.00	4.00	3.50	8852	0.20	0.188	0.568	24730	7.3



Nyloplast Inlet Capacity Table

DISCLAIMER: SAFETY FACTORS ARE NOT INCLUDED IN THESE CALCULATIONS. ACTUAL CALCULATIONS SHOULD BE CARRIED OUT AND VERIFIED BY THE DESIGN ENGINEER TAKING INTO ACCOUNT ALL LOCAL CONDITIONS. NYLOPLAST RECOMMENDS USING A MINIMUM SAFETY FACTOR OF 1.25 FOR PAVED AREAS AND 2.0 FOR TURF AREAS. ADS/NYLOPLAST IS NOT RESPONSIBLE FOR MISUSE OF THIS TOOL.

Input	
Type of Grate	18" Standard
Head (ft)	0.5
Properties	
Orifice Flow Area (in)	116.72
Orifice Flow Area (ft)	0.81
Weir Flow Perimeter (in)	52.04
Weir Flow Perimeter (ft)	4.34
Solution	
Capacity (cfs)	2.74
Capacity (gpm)	1230.13

$$Q_{weir} = CLH^{3/2}$$

C = 3.33 Weir Discharge Coefficient

L = Perimeter of Grate Opening (ft)

H = Flow Height of Water Surface Above Weir (ft)

$$Q_{orifice} = CA\sqrt{2gh}$$

C = 0.60 Orifice Discharge Coefficient

A = Area of the Orifice (ft²)

g = Gravitational Constant (32.2 ft/s²)

H = Depth of Water Above Center of Orifice (ft)



Nyloplast Inlet Capacity Table

DISCLAIMER: SAFETY FACTORS ARE NOT INCLUDED IN THESE CALCULATIONS. ACTUAL CALCULATIONS SHOULD BE CARRIED OUT AND VERIFIED BY THE DESIGN ENGINEER TAKING INTO ACCOUNT ALL LOCAL CONDITIONS. NYLOPLAST RECOMMENDS USING A MINIMUM SAFETY FACTOR OF 1.25 FOR PAVED AREAS AND 2.0 FOR TURF AREAS. ADS/NYLOPLAST IS NOT RESPONSIBLE FOR MISUSE OF THIS TOOL.

Input	
Type of Grate	18" Standard
Head (ft)	1.5
Properties	
Orifice Flow Area (in)	116.72
Orifice Flow Area (ft)	0.81
Weir Flow Perimeter (in)	52.04
Weir Flow Perimeter (ft)	4.34
Solution	
Capacity (cfs)	4.75
Capacity (gpm)	2130.65

$$Q_{weir} = CLH^{3/2}$$

C = 3.33 Weir Discharge Coefficient

L = Perimeter of Grate Opening (ft)

H = Flow Height of Water Surface Above Weir (ft)

$$Q_{orifice} = CA\sqrt{2gh}$$

C = 0.60 Orifice Discharge Coefficient

A = Area of the Orifice (ft²)

g = Gravitational Constant (32.2 ft/s²)

H = Depth of Water Above Center of Orifice (ft)



Nyloplast Inlet Capacity Table

DISCLAIMER: SAFETY FACTORS ARE NOT INCLUDED IN THESE CALCULATIONS. ACTUAL CALCULATIONS SHOULD BE CARRIED OUT AND VERIFIED BY THE DESIGN ENGINEER TAKING INTO ACCOUNT ALL LOCAL CONDITIONS. NYLOPLAST RECOMMENDS USING A MINIMUM SAFETY FACTOR OF 1.25 FOR PAVED AREAS AND 2.0 FOR TURF AREAS. ADS/NYLOPLAST IS NOT RESPONSIBLE FOR MISUSE OF THIS TOOL.

Input	
Type of Grate	18" Standard
Head (ft)	2.5
Properties	
Orifice Flow Area (in)	116.72
Orifice Flow Area (ft)	0.81
Weir Flow Perimeter (in)	52.04
Weir Flow Perimeter (ft)	4.34
Solution	
Capacity (cfs)	6.13
Capacity (gpm)	2750.65

$$Q_{weir} = CLH^{3/2}$$

C = 3.33 Weir Discharge Coefficient

L = Perimeter of Grate Opening (ft)

H = Flow Height of Water Surface Above Weir (ft)

$$Q_{orifice} = CA\sqrt{2gh}$$

C = 0.60 Orifice Discharge Coefficient

A = Area of the Orifice (ft²)

g = Gravitational Constant (32.2 ft/s²)

H = Depth of Water Above Center of Orifice (ft)



Nyloplast Inlet Capacity Table

DISCLAIMER: SAFETY FACTORS ARE NOT INCLUDED IN THESE CALCULATIONS. ACTUAL CALCULATIONS SHOULD BE CARRIED OUT AND VERIFIED BY THE DESIGN ENGINEER TAKING INTO ACCOUNT ALL LOCAL CONDITIONS. NYLOPLAST RECOMMENDS USING A MINIMUM SAFETY FACTOR OF 1.25 FOR PAVED AREAS AND 2.0 FOR TURF AREAS. ADS/NYLOPLAST IS NOT RESPONSIBLE FOR MISUSE OF THIS TOOL.

Input	
Type of Grate	18" Standard
Head (ft)	3.5
Properties	
Orifice Flow Area (in)	116.72
Orifice Flow Area (ft)	0.81
Weir Flow Perimeter (in)	52.04
Weir Flow Perimeter (ft)	4.34
Solution	
Capacity (cfs)	7.25
Capacity (gpm)	3254.62

$$Q_{weir} = CLH^{3/2}$$

C = 3.33 Weir Discharge Coefficient

L = Perimeter of Grate Opening (ft)

H = Flow Height of Water Surface Above Weir (ft)

$$Q_{orifice} = CA\sqrt{2gh}$$

C = 0.60 Orifice Discharge Coefficient

A = Area of the Orifice (ft²)

g = Gravitational Constant (32.2 ft/s²)

H = Depth of Water Above Center of Orifice (ft)

FLOOD ROUTING ANALYSIS
USING COUNTY HYDROLOGY MANUAL OF ORANGE(1986)
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Ver. 23.0 Release Date: 07/01/2016 License ID 1334

Analysis prepared by:

***** DESCRIPTION OF STUDY *****
* SP8997 - WILDOMAR CHERRY OUTPOST *
* PROPOSED CONDITION SMALL AREA UNIT HYDROGRAPH *
* 100-YEAR STORM EVENT FLOW THROUGH BASIN *

FILE NAME: 100YRPRH.DAT
TIME/DATE OF STUDY: 15:39 04/30/2024

The Small Area Unit Hydrograph Procedures in Section J of the Hydrology Manual provides estimates of runoff hydrograph and runoff volume for watersheds whose time of concentration is less than 25 minutes. The PROGRAM User should check the applicability of using the small area unit hydrograph procedures, and follow the guidelines in Sections J and K.5 in complex watershed modeling.

FLOW PROCESS FROM NODE 10.00 TO NODE 110.00 IS CODE = 1.2

>>>SUBAREA RUNOFF (SMALL AREA UNIT-HYDROGRAPH ANALYSIS) <<<<

(SMALL AREA UNIT-HYDROGRAPH ADDED TO STREAM #1)

RATIONAL METHOD CALIBRATION COEFFICIENT = 0.90
TOTAL CATCHMENT AREA(ACRES) = 5.95
SOIL-LOSS RATE, Fm,(INCH/HR) = 0.227
LOW LOSS FRACTION = 0.283
TIME OF CONCENTRATION(MIN.) = 11.18
SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA
USER SPECIFIED RAINFALL VALUES ARE USED:
RETURN FREQUENCY(YEARS) = 100
5-MINUTE POINT RAINFALL VALUE(INCHES) = 0.31
30-MINUTE POINT RAINFALL VALUE(INCHES) = 0.85
1-HOUR POINT RAINFALL VALUE(INCHES) = 1.31
3-HOUR POINT RAINFALL VALUE(INCHES) = 2.13
6-HOUR POINT RAINFALL VALUE(INCHES) = 2.96
24-HOUR POINT RAINFALL VALUE(INCHES) = 5.87

TOTAL CATCHMENT RUNOFF VOLUME(ACRE-FEET) = 1.93
TOTAL CATCHMENT SOIL-LOSS VOLUME(ACRE-FEET) = 0.98

24 - H O U R S T O R M
R U N O F F H Y D R O G R A P H

HYDROGRAPH IN ONE-MINUTE UNIT INTERVALS(CFS)
(Notes: Time indicated is at END of Each Unit Intervals.
Peak 5-minute rainfall intensity is modeled as
a constant value for entire 5-minute period.)

TIME(HRS)	VOLUME(AF)	Q(CFS)	0.	3.2	6.4	9.6	12.8
0.017	0.0000	0.02	Q
0.033	0.0001	0.07	Q
0.050	0.0003	0.12	Q
0.067	0.0005	0.17	Q
0.083	0.0008	0.22	Q
0.100	0.0012	0.26	Q
0.117	0.0016	0.31	Q
0.133	0.0021	0.36	VQ
0.150	0.0027	0.41	VQ
0.167	0.0033	0.45	VQ
0.183	0.0039	0.46	VQ
0.200	0.0046	0.46	VQ
0.217	0.0052	0.46	VQ
0.233	0.0059	0.47	VQ
0.250	0.0065	0.47	VQ
0.267	0.0071	0.47	VQ
0.283	0.0078	0.47	VQ
0.300	0.0084	0.47	VQ
0.317	0.0091	0.47	VQ
0.333	0.0097	0.47	VQ
0.350	0.0103	0.47	VQ
0.367	0.0110	0.47	VQ
0.383	0.0116	0.47	VQ
0.400	0.0123	0.47	VQ
0.417	0.0129	0.47	VQ
0.433	0.0136	0.47	VQ
0.450	0.0142	0.47	VQ
0.467	0.0149	0.47	VQ
0.483	0.0155	0.47	VQ
0.500	0.0161	0.47	VQ
0.517	0.0168	0.47	VQ
0.533	0.0174	0.47	VQ
0.550	0.0181	0.47	VQ
0.567	0.0187	0.47	VQ
0.583	0.0194	0.47	VQ
0.600	0.0200	0.47	VQ
0.617	0.0207	0.47	VQ
0.633	0.0213	0.47	VQ
0.650	0.0220	0.47	VQ
0.667	0.0226	0.47	VQ
0.683	0.0233	0.47	VQ
0.700	0.0239	0.47	VQ
0.717	0.0246	0.47	VQ

0.733	0.0252	0.47	VQ	1.717	0.0643	0.49	.Q
0.750	0.0259	0.47	VQ	1.733	0.0649	0.49	.Q
0.767	0.0265	0.47	VQ	1.750	0.0656	0.49	.Q
0.783	0.0272	0.47	VQ	1.767	0.0663	0.49	.Q
0.800	0.0278	0.47	VQ	1.783	0.0670	0.49	.Q
0.817	0.0285	0.47	VQ	1.800	0.0676	0.49	.Q
0.833	0.0291	0.47	VQ	1.817	0.0683	0.49	.Q
0.850	0.0298	0.47	VQ	1.833	0.0690	0.49	.Q
0.867	0.0304	0.47	VQ	1.850	0.0697	0.49	.Q
0.883	0.0311	0.48	VQ	1.867	0.0703	0.49	.Q
0.900	0.0317	0.48	VQ	1.883	0.0710	0.49	.Q
0.917	0.0324	0.48	VQ	1.900	0.0717	0.49	.Q
0.933	0.0331	0.48	VQ	1.917	0.0724	0.49	.Q
0.950	0.0337	0.48	VQ	1.933	0.0730	0.49	.Q
0.967	0.0344	0.48	VQ	1.950	0.0737	0.49	.Q
0.983	0.0350	0.48	VQ	1.967	0.0744	0.49	.Q
1.000	0.0357	0.48	VQ	1.983	0.0751	0.49	.Q
1.017	0.0363	0.48	VQ	2.000	0.0758	0.49	.Q
1.033	0.0370	0.48	VQ	2.017	0.0764	0.49	.Q
1.050	0.0377	0.48	VQ	2.033	0.0771	0.49	.Q
1.067	0.0383	0.48	VQ	2.050	0.0778	0.49	.Q
1.083	0.0390	0.48	VQ	2.067	0.0785	0.49	.Q
1.100	0.0396	0.48	VQ	2.083	0.0792	0.50	.Q
1.117	0.0403	0.48	VQ	2.100	0.0798	0.50	.Q
1.133	0.0409	0.48	VQ	2.117	0.0805	0.50	.Q
1.150	0.0416	0.48	VQ	2.133	0.0812	0.50	.Q
1.167	0.0423	0.48	VQ	2.150	0.0819	0.50	.Q
1.183	0.0429	0.48	VQ	2.167	0.0826	0.50	.Q
1.200	0.0436	0.48	VQ	2.183	0.0833	0.50	.Q
1.217	0.0442	0.48	VQ	2.200	0.0839	0.50	.Q
1.233	0.0449	0.48	VQ	2.217	0.0846	0.50	.Q
1.250	0.0456	0.48	VQ	2.233	0.0853	0.50	.Q
1.267	0.0462	0.48	VQ	2.250	0.0860	0.50	.Q
1.283	0.0469	0.48	VQ	2.267	0.0867	0.50	.Q
1.300	0.0476	0.48	VQ	2.283	0.0874	0.50	.Q
1.317	0.0482	0.48	.Q	2.300	0.0881	0.50	.Q
1.333	0.0489	0.48	.Q	2.317	0.0887	0.50	.Q
1.350	0.0496	0.48	.Q	2.333	0.0894	0.50	.Q
1.367	0.0502	0.48	.Q	2.350	0.0901	0.50	.Q
1.383	0.0509	0.48	.Q	2.367	0.0908	0.50	.Q
1.400	0.0516	0.48	.Q	2.383	0.0915	0.50	.Q
1.417	0.0522	0.48	.Q	2.400	0.0922	0.50	.Q
1.433	0.0529	0.48	.Q	2.417	0.0929	0.50	.Q
1.450	0.0535	0.48	.Q	2.433	0.0936	0.50	.Q
1.467	0.0542	0.48	.Q	2.450	0.0943	0.50	.Q
1.483	0.0549	0.48	.Q	2.467	0.0950	0.50	.Q
1.500	0.0555	0.48	.Q	2.483	0.0956	0.50	.Q
1.517	0.0562	0.48	.Q	2.500	0.0963	0.50	.Q
1.533	0.0569	0.49	.Q	2.517	0.0970	0.50	.QV
1.550	0.0576	0.49	.Q	2.533	0.0977	0.50	.QV
1.567	0.0582	0.49	.Q	2.550	0.0984	0.50	.QV
1.583	0.0589	0.49	.Q	2.567	0.0991	0.50	.QV
1.600	0.0596	0.49	.Q	2.583	0.0998	0.50	.QV
1.617	0.0602	0.49	.Q	2.600	0.1005	0.50	.QV
1.633	0.0609	0.49	.Q	2.617	0.1012	0.50	.QV
1.650	0.0616	0.49	.Q	2.633	0.1019	0.50	.QV
1.667	0.0622	0.49	.Q	2.650	0.1026	0.50	.QV
1.683	0.0629	0.49	.Q	2.667	0.1033	0.51	.QV
1.700	0.0636	0.49	.Q	2.683	0.1040	0.51	.QV

2.700	0.1047	0.51	.QV	3.683	0.1466	0.53	.Q V
2.717	0.1054	0.51	.QV	3.700	0.1473	0.53	.Q V
2.733	0.1061	0.51	.QV	3.717	0.1481	0.53	.Q V
2.750	0.1068	0.51	.QV	3.733	0.1488	0.53	.Q V
2.767	0.1075	0.51	.QV	3.750	0.1495	0.53	.Q V
2.783	0.1082	0.51	.QV	3.767	0.1502	0.53	.Q V
2.800	0.1089	0.51	.QV	3.783	0.1510	0.53	.Q V
2.817	0.1096	0.51	.QV	3.800	0.1517	0.53	.Q V
2.833	0.1103	0.51	.QV	3.817	0.1524	0.53	.Q V
2.850	0.1110	0.51	.QV	3.833	0.1532	0.53	.Q V
2.867	0.1117	0.51	.QV	3.850	0.1539	0.53	.Q V
2.883	0.1124	0.51	.QV	3.867	0.1546	0.53	.Q V
2.900	0.1131	0.51	.QV	3.883	0.1553	0.53	.Q V
2.917	0.1138	0.51	.QV	3.900	0.1561	0.53	.Q V
2.933	0.1145	0.51	.QV	3.917	0.1568	0.53	.Q V
2.950	0.1152	0.51	.QV	3.933	0.1575	0.53	.Q V
2.967	0.1159	0.51	.QV	3.950	0.1583	0.53	.Q V
2.983	0.1166	0.51	.QV	3.967	0.1590	0.53	.Q V
3.000	0.1173	0.51	.QV	3.983	0.1597	0.53	.Q V
3.017	0.1180	0.51	.QV	4.000	0.1605	0.53	.Q V
3.033	0.1187	0.51	.QV	4.017	0.1612	0.53	.Q V
3.050	0.1194	0.51	.QV	4.033	0.1619	0.53	.Q V
3.067	0.1201	0.51	.QV	4.050	0.1627	0.53	.Q V
3.083	0.1208	0.51	.QV	4.067	0.1634	0.53	.Q V
3.100	0.1215	0.51	.QV	4.083	0.1641	0.53	.Q V
3.117	0.1222	0.51	.QV	4.100	0.1649	0.53	.Q V
3.133	0.1230	0.52	.QV	4.117	0.1656	0.53	.Q V
3.150	0.1237	0.52	.QV	4.133	0.1664	0.54	.Q V
3.167	0.1244	0.52	.QV	4.150	0.1671	0.54	.Q V
3.183	0.1251	0.52	.QV	4.167	0.1678	0.54	.Q V
3.200	0.1258	0.52	.QV	4.183	0.1686	0.54	.Q V
3.217	0.1265	0.52	.QV	4.200	0.1693	0.54	.Q V
3.233	0.1272	0.52	.QV	4.217	0.1701	0.54	.Q V
3.250	0.1279	0.52	.QV	4.233	0.1708	0.54	.Q V
3.267	0.1286	0.52	.QV	4.250	0.1715	0.54	.Q V
3.283	0.1294	0.52	.QV	4.267	0.1723	0.54	.Q V
3.300	0.1301	0.52	.QV	4.283	0.1730	0.54	.Q V
3.317	0.1308	0.52	.QV	4.300	0.1738	0.54	.Q V
3.333	0.1315	0.52	.QV	4.317	0.1745	0.54	.Q V
3.350	0.1322	0.52	.QV	4.333	0.1753	0.54	.Q V
3.367	0.1329	0.52	.QV	4.350	0.1760	0.54	.Q V
3.383	0.1336	0.52	.QV	4.367	0.1768	0.54	.Q V
3.400	0.1344	0.52	.QV	4.383	0.1775	0.54	.Q V
3.417	0.1351	0.52	.QV	4.400	0.1782	0.54	.Q V
3.433	0.1358	0.52	.QV	4.417	0.1790	0.54	.Q V
3.450	0.1365	0.52	.QV	4.433	0.1797	0.54	.Q V
3.467	0.1372	0.52	.QV	4.450	0.1805	0.54	.Q V
3.483	0.1380	0.52	.QV	4.467	0.1812	0.54	.Q V
3.500	0.1387	0.52	.QV	4.483	0.1820	0.54	.Q V
3.517	0.1394	0.52	.QV	4.500	0.1827	0.54	.Q V
3.533	0.1401	0.52	.QV	4.517	0.1835	0.54	.Q V
3.550	0.1408	0.52	.QV	4.533	0.1842	0.54	.Q V
3.567	0.1416	0.52	.QV	4.550	0.1850	0.55	.Q V
3.583	0.1423	0.52	.QV	4.567	0.1857	0.55	.Q V
3.600	0.1430	0.52	.QV	4.583	0.1865	0.55	.Q V
3.617	0.1437	0.52	.QV	4.600	0.1872	0.55	.Q V
3.633	0.1444	0.52	.QV	4.617	0.1880	0.55	.Q V
3.650	0.1452	0.53	.Q V	4.633	0.1887	0.55	.Q V
3.667	0.1459	0.53	.Q V	4.650	0.1895	0.55	.Q V

4.667	0.1903	0.55	.Q	V	5.650	0.2358	0.57	.Q	V	.	.	.
4.683	0.1910	0.55	.Q	V	5.667	0.2366	0.57	.Q	V	.	.	.
4.700	0.1918	0.55	.Q	V	5.683	0.2374	0.57	.Q	V	.	.	.
4.717	0.1925	0.55	.Q	V	5.700	0.2382	0.58	.Q	V	.	.	.
4.733	0.1933	0.55	.Q	V	5.717	0.2390	0.58	.Q	V	.	.	.
4.750	0.1940	0.55	.Q	V	5.733	0.2398	0.58	.Q	V	.	.	.
4.767	0.1948	0.55	.Q	V	5.750	0.2406	0.58	.Q	V	.	.	.
4.783	0.1956	0.55	.Q	V	5.767	0.2414	0.58	.Q	V	.	.	.
4.800	0.1963	0.55	.Q	V	5.783	0.2422	0.58	.Q	V	.	.	.
4.817	0.1971	0.55	.Q	V	5.800	0.2430	0.58	.Q	V	.	.	.
4.833	0.1978	0.55	.Q	V	5.817	0.2438	0.58	.Q	V	.	.	.
4.850	0.1986	0.55	.Q	V	5.833	0.2446	0.58	.Q	V	.	.	.
4.867	0.1994	0.55	.Q	V	5.850	0.2454	0.58	.Q	V	.	.	.
4.883	0.2001	0.55	.Q	V	5.867	0.2462	0.58	.Q	V	.	.	.
4.900	0.2009	0.55	.Q	V	5.883	0.2470	0.58	.Q	V	.	.	.
4.917	0.2017	0.55	.Q	V	5.900	0.2478	0.58	.Q	V	.	.	.
4.933	0.2024	0.55	.Q	V	5.917	0.2486	0.58	.Q	V	.	.	.
4.950	0.2032	0.56	.Q	V	5.933	0.2494	0.58	.Q	V	.	.	.
4.967	0.2039	0.56	.Q	V	5.950	0.2502	0.58	.Q	V	.	.	.
4.983	0.2047	0.56	.Q	V	5.967	0.2510	0.58	.Q	V	.	.	.
5.000	0.2055	0.56	.Q	V	5.983	0.2518	0.58	.Q	V	.	.	.
5.017	0.2062	0.56	.Q	V	6.000	0.2526	0.58	.Q	V	.	.	.
5.033	0.2070	0.56	.Q	V	6.017	0.2534	0.58	.Q	V	.	.	.
5.050	0.2078	0.56	.Q	V	6.033	0.2542	0.58	.Q	V	.	.	.
5.067	0.2086	0.56	.Q	V	6.050	0.2550	0.59	.Q	V	.	.	.
5.083	0.2093	0.56	.Q	V	6.067	0.2558	0.59	.Q	V	.	.	.
5.100	0.2101	0.56	.Q	V	6.083	0.2566	0.59	.Q	V	.	.	.
5.117	0.2109	0.56	.Q	V	6.100	0.2574	0.59	.Q	V	.	.	.
5.133	0.2116	0.56	.Q	V	6.117	0.2582	0.59	.Q	V	.	.	.
5.150	0.2124	0.56	.Q	V	6.133	0.2590	0.59	.Q	V	.	.	.
5.167	0.2132	0.56	.Q	V	6.150	0.2598	0.59	.Q	V	.	.	.
5.183	0.2140	0.56	.Q	V	6.167	0.2607	0.59	.Q	V	.	.	.
5.200	0.2147	0.56	.Q	V	6.183	0.2615	0.59	.Q	V	.	.	.
5.217	0.2155	0.56	.Q	V	6.200	0.2623	0.59	.Q	V	.	.	.
5.233	0.2163	0.56	.Q	V	6.217	0.2631	0.59	.Q	V	.	.	.
5.250	0.2170	0.56	.Q	V	6.233	0.2639	0.59	.Q	V	.	.	.
5.267	0.2178	0.56	.Q	V	6.250	0.2647	0.59	.Q	V	.	.	.
5.283	0.2186	0.56	.Q	V	6.267	0.2655	0.59	.Q	V	.	.	.
5.300	0.2194	0.56	.Q	V	6.283	0.2664	0.59	.Q	V	.	.	.
5.317	0.2202	0.56	.Q	V	6.300	0.2672	0.59	.Q	V	.	.	.
5.333	0.2209	0.57	.Q	V	6.317	0.2680	0.59	.Q	V	.	.	.
5.350	0.2217	0.57	.Q	V	6.333	0.2688	0.59	.Q	V	.	.	.
5.367	0.2225	0.57	.Q	V	6.350	0.2696	0.59	.Q	V	.	.	.
5.383	0.2233	0.57	.Q	V	6.367	0.2704	0.59	.Q	V	.	.	.
5.400	0.2241	0.57	.Q	V	6.383	0.2713	0.59	.Q	V	.	.	.
5.417	0.2248	0.57	.Q	V	6.400	0.2721	0.60	.Q	V	.	.	.
5.433	0.2256	0.57	.Q	V	6.417	0.2729	0.60	.Q	V	.	.	.
5.450	0.2264	0.57	.Q	V	6.433	0.2737	0.60	.Q	V	.	.	.
5.467	0.2272	0.57	.Q	V	6.450	0.2745	0.60	.Q	V	.	.	.
5.483	0.2280	0.57	.Q	V	6.467	0.2754	0.60	.Q	V	.	.	.
5.500	0.2288	0.57	.Q	V	6.483	0.2762	0.60	.Q	V	.	.	.
5.517	0.2295	0.57	.Q	V	6.500	0.2770	0.60	.Q	V	.	.	.
5.533	0.2303	0.57	.Q	V	6.517	0.2778	0.60	.Q	V	.	.	.
5.550	0.2311	0.57	.Q	V	6.533	0.2787	0.60	.Q	V	.	.	.
5.567	0.2319	0.57	.Q	V	6.550	0.2795	0.60	.Q	V	.	.	.
5.583	0.2327	0.57	.Q	V	6.567	0.2803	0.60	.Q	V	.	.	.
5.600	0.2335	0.57	.Q	V	6.583	0.2812	0.60	.Q	V	.	.	.
5.617	0.2343	0.57	.Q	V	6.600	0.2820	0.60	.Q	V	.	.	.
5.633	0.2350	0.57	.Q	V	6.617	0.2828	0.60	.Q	V	.	.	.

10.567	0.5060	0.79	. Q	V		11.550	0.5733	0.87	. Q	.V	
10.583	0.5071	0.79	. Q	V		11.567	0.5745	0.87	. Q	.V	
10.600	0.5082	0.79	. Q	V		11.583	0.5757	0.87	. Q	.V	
10.617	0.5093	0.79	. Q	V		11.600	0.5770	0.87	. Q	.V	
10.633	0.5104	0.80	. Q	V		11.617	0.5782	0.88	. Q	.V	
10.650	0.5115	0.80	. Q	V		11.633	0.5794	0.88	. Q	.V	
10.667	0.5126	0.80	. Q	V		11.650	0.5806	0.88	. Q	.V	
10.683	0.5137	0.80	. Q	V		11.667	0.5818	0.88	. Q	.V	
10.700	0.5148	0.80	. Q	V		11.683	0.5830	0.89	. Q	.V	
10.717	0.5159	0.80	. Q	V		11.700	0.5842	0.89	. Q	.V	
10.733	0.5170	0.80	. Q	V		11.717	0.5855	0.89	. Q	.V	
10.750	0.5181	0.80	. Q	V		11.733	0.5867	0.89	. Q	.V	
10.767	0.5192	0.80	. Q	V		11.750	0.5879	0.89	. Q	.V	
10.783	0.5203	0.80	. Q	V		11.767	0.5892	0.89	. Q	.V	
10.800	0.5214	0.80	. Q	V		11.783	0.5904	0.89	. Q	.V	
10.817	0.5225	0.81	. Q	V		11.800	0.5916	0.90	. Q	.V	
10.833	0.5236	0.81	. Q	V		11.817	0.5929	0.90	. Q	.V	
10.850	0.5247	0.81	. Q	V		11.833	0.5941	0.90	. Q	.V	
10.867	0.5259	0.81	. Q	V		11.850	0.5953	0.90	. Q	.V	
10.883	0.5270	0.81	. Q	V		11.867	0.5966	0.90	. Q	.V	
10.900	0.5281	0.81	. Q	V		11.883	0.5978	0.90	. Q	.V	
10.917	0.5292	0.82	. Q	V		11.900	0.5991	0.90	. Q	.V	
10.933	0.5304	0.82	. Q	.V		11.917	0.6003	0.90	. Q	.V	
10.950	0.5315	0.82	. Q	.V		11.933	0.6016	0.91	. Q	.V	
10.967	0.5326	0.82	. Q	.V		11.950	0.6028	0.91	. Q	.V	
10.983	0.5338	0.82	. Q	.V		11.967	0.6041	0.91	. Q	.V	
11.000	0.5349	0.82	. Q	.V		11.983	0.6053	0.91	. Q	.V	
11.017	0.5360	0.82	. Q	.V		12.000	0.6066	0.91	. Q	.V	
11.033	0.5372	0.83	. Q	.V		12.017	0.6078	0.92	. Q	.V	
11.050	0.5383	0.83	. Q	.V		12.033	0.6091	0.92	. Q	.V	
11.067	0.5394	0.83	. Q	.V		12.050	0.6104	0.92	. Q	.V	
11.083	0.5406	0.83	. Q	.V		12.067	0.6116	0.92	. Q	.V	
11.100	0.5417	0.83	. Q	.V		12.083	0.6129	0.92	. Q	.V	
11.117	0.5429	0.83	. Q	.V		12.100	0.6142	0.92	. Q	.V	
11.133	0.5440	0.83	. Q	.V		12.117	0.6154	0.92	. Q	.V	
11.150	0.5452	0.83	. Q	.V		12.133	0.6167	0.92	. Q	.V	
11.167	0.5463	0.83	. Q	.V		12.150	0.6180	0.92	. Q	.V	
11.183	0.5475	0.84	. Q	.V		12.167	0.6192	0.92	. Q	.V	
11.200	0.5486	0.84	. Q	.V		12.183	0.6205	0.92	. Q	.V	
11.217	0.5498	0.84	. Q	.V		12.200	0.6218	0.92	. Q	.V	
11.233	0.5509	0.84	. Q	.V		12.217	0.6230	0.91	. Q	.V	
11.250	0.5521	0.84	. Q	.V		12.233	0.6243	0.91	. Q	.V	
11.267	0.5533	0.84	. Q	.V		12.250	0.6255	0.91	. Q	.V	
11.283	0.5544	0.85	. Q	.V		12.267	0.6268	0.91	. Q	.V	
11.300	0.5556	0.85	. Q	.V		12.283	0.6280	0.91	. Q	.V	
11.317	0.5568	0.85	. Q	.V		12.300	0.6293	0.91	. Q	.V	
11.333	0.5579	0.85	. Q	.V		12.317	0.6306	0.92	. Q	.V	
11.350	0.5591	0.85	. Q	.V		12.333	0.6318	0.92	. Q	.V	
11.367	0.5603	0.86	. Q	.V		12.350	0.6331	0.92	. Q	.V	
11.383	0.5615	0.86	. Q	.V		12.367	0.6344	0.92	. Q	.V	
11.400	0.5627	0.86	. Q	.V		12.383	0.6357	0.93	. Q	.V	
11.417	0.5638	0.86	. Q	.V		12.400	0.6369	0.93	. Q	.V	
11.433	0.5650	0.86	. Q	.V		12.417	0.6382	0.93	. Q	.V	
11.450	0.5662	0.86	. Q	.V		12.433	0.6395	0.94	. Q	.V	
11.467	0.5674	0.86	. Q	.V		12.450	0.6408	0.94	. Q	.V	
11.483	0.5686	0.86	. Q	.V		12.467	0.6421	0.94	. Q	.V	
11.500	0.5698	0.86	. Q	.V		12.483	0.6434	0.94	. Q	.V	
11.517	0.5710	0.86	. Q	.V		12.500	0.6447	0.94	. Q	.V	
11.533	0.5722	0.87	. Q	.V		12.517	0.6460	0.95	. Q	.V	

12.533	0.6473	0.95	.	Q	.	V	13.517	0.7307	1.12	.	Q	.	V	.	.
12.550	0.6486	0.95	.	Q	.	V	13.533	0.7322	1.12	.	Q	.	V	.	.
12.567	0.6499	0.95	.	Q	.	V	13.550	0.7338	1.13	.	Q	.	V	.	.
12.583	0.6512	0.95	.	Q	.	V	13.567	0.7354	1.13	.	Q	.	V	.	.
12.600	0.6525	0.95	.	Q	.	V	13.583	0.7369	1.14	.	Q	.	V	.	.
12.617	0.6539	0.96	.	Q	.	V	13.600	0.7385	1.14	.	Q	.	V	.	.
12.633	0.6552	0.96	.	Q	.	V	13.617	0.7401	1.15	.	Q	.	V	.	.
12.650	0.6565	0.96	.	Q	.	V	13.633	0.7417	1.15	.	Q	.	V	.	.
12.667	0.6578	0.96	.	Q	.	V	13.650	0.7432	1.15	.	Q	.	V	.	.
12.683	0.6592	0.96	.	Q	.	V	13.667	0.7448	1.15	.	Q	.	V	.	.
12.700	0.6605	0.97	.	Q	.	V	13.683	0.7464	1.16	.	Q	.	V	.	.
12.717	0.6618	0.97	.	Q	.	V	13.700	0.7480	1.16	.	Q	.	V	.	.
12.733	0.6632	0.97	.	Q	.	V	13.717	0.7496	1.16	.	Q	.	V	.	.
12.750	0.6645	0.98	.	Q	.	V	13.733	0.7512	1.16	.	Q	.	V	.	.
12.767	0.6659	0.98	.	Q	.	V	13.750	0.7528	1.17	.	Q	.	V	.	.
12.783	0.6672	0.98	.	Q	.	V	13.767	0.7544	1.17	.	Q	.	V	.	.
12.800	0.6686	0.99	.	Q	.	V	13.783	0.7561	1.17	.	Q	.	V	.	.
12.817	0.6700	0.99	.	Q	.	V	13.800	0.7577	1.18	.	Q	.	V	.	.
12.833	0.6713	0.99	.	Q	.	V	13.817	0.7593	1.19	.	Q	.	V	.	.
12.850	0.6727	1.00	.	Q	.	V	13.833	0.7610	1.19	.	Q	.	V	.	.
12.867	0.6741	1.00	.	Q	.	V	13.850	0.7626	1.20	.	Q	.	V	.	.
12.883	0.6754	1.00	.	Q	.	V	13.867	0.7643	1.21	.	Q	.	V	.	.
12.900	0.6768	1.00	.	Q	.	V	13.883	0.7659	1.21	.	Q	.	V	.	.
12.917	0.6782	1.00	.	Q	.	V	13.900	0.7676	1.22	.	Q	.	V	.	.
12.933	0.6796	1.01	.	Q	.	V	13.917	0.7693	1.22	.	Q	.	V	.	.
12.950	0.6810	1.01	.	Q	.	V	13.933	0.7710	1.23	.	Q	.	V	.	.
12.967	0.6824	1.01	.	Q	.	V	13.950	0.7727	1.24	.	Q	.	V	.	.
12.983	0.6838	1.01	.	Q	.	V	13.967	0.7744	1.24	.	Q	.	V	.	.
13.000	0.6852	1.01	.	Q	.	V	13.983	0.7761	1.24	.	Q	.	V	.	.
13.017	0.6866	1.02	.	Q	.	V	14.000	0.7778	1.25	.	Q	.	V	.	.
13.033	0.6880	1.02	.	Q	.	V	14.017	0.7796	1.25	.	Q	.	V	.	.
13.050	0.6894	1.02	.	Q	.	V	14.033	0.7813	1.25	.	Q	.	V	.	.
13.067	0.6908	1.03	.	Q	.	V	14.050	0.7830	1.25	.	Q	.	V	.	.
13.083	0.6922	1.03	.	Q	.	V	14.067	0.7847	1.26	.	Q	.	V	.	.
13.100	0.6936	1.03	.	Q	.	V	14.083	0.7865	1.26	.	Q	.	V	.	.
13.117	0.6951	1.04	.	Q	.	V	14.100	0.7882	1.26	.	Q	.	V	.	.
13.133	0.6965	1.04	.	Q	.	V	14.117	0.7900	1.26	.	Q	.	V	.	.
13.150	0.6979	1.05	.	Q	.	V	14.133	0.7917	1.27	.	Q	.	V	.	.
13.167	0.6994	1.05	.	Q	.	V	14.150	0.7934	1.27	.	Q	.	V	.	.
13.183	0.7008	1.05	.	Q	.	V	14.167	0.7952	1.27	.	Q	.	V	.	.
13.200	0.7023	1.06	.	Q	.	V	14.183	0.7969	1.27	.	Q	.	V	.	.
13.217	0.7038	1.06	.	Q	.	V	14.200	0.7987	1.27	.	Q	.	V	.	.
13.233	0.7052	1.06	.	Q	.	V	14.217	0.8005	1.27	.	Q	.	V	.	.
13.250	0.7067	1.07	.	Q	.	V	14.233	0.8022	1.27	.	Q	.	V	.	.
13.267	0.7082	1.07	.	Q	.	V	14.250	0.8040	1.27	.	Q	.	V	.	.
13.283	0.7096	1.07	.	Q	.	V	14.267	0.8057	1.28	.	Q	.	V	.	.
13.300	0.7111	1.07	.	Q	.	V	14.283	0.8075	1.28	.	Q	.	V	.	.
13.317	0.7126	1.07	.	Q	.	V	14.300	0.8092	1.28	.	Q	.	V	.	.
13.333	0.7141	1.08	.	Q	.	V	14.317	0.8110	1.28	.	Q	.	V	.	.
13.350	0.7156	1.08	.	Q	.	V	14.333	0.8128	1.28	.	Q	.	V	.	.
13.367	0.7171	1.08	.	Q	.	V	14.350	0.8145	1.28	.	Q	.	V	.	.
13.383	0.7185	1.08	.	Q	.	V	14.367	0.8163	1.29	.	Q	.	V	.	.
13.400	0.7200	1.09	.	Q	.	V	14.383	0.8181	1.29	.	Q	.	V	.	.
13.417	0.7215	1.09	.	Q	.	V	14.400	0.8199	1.30	.	Q	.	V	.	.
13.433	0.7231	1.10	.	Q	.	V	14.417	0.8217	1.30	.	Q	.	V	.	.
13.450	0.7246	1.10	.	Q	.	V	14.433	0.8235	1.31	.	Q	.	V	.	.
13.467	0.7261	1.11	.	Q	.	V	14.450	0.8253	1.31	.	Q	.	V	.	.
13.483	0.7276	1.11	.	Q	.	V	14.467	0.8271	1.32	.	Q	.	V	.	.
13.500	0.7292	1.11	.	Q	.	V	14.483	0.8289	1.32	.	Q	.	V	.	.

14.500	0.8307	1.33	.	Q	.	V	.	.	.
14.517	0.8326	1.33	.	Q	.	V	.	.	.
14.533	0.8344	1.34	.	Q	.	V	.	.	.
14.550	0.8363	1.35	.	Q	.	V	.	.	.
14.567	0.8382	1.36	.	Q	.	V	.	.	.
14.583	0.8401	1.37	.	Q	.	V	.	.	.
14.600	0.8420	1.39	.	Q	.	V	.	.	.
14.617	0.8439	1.40	.	Q	.	V	.	.	.
14.633	0.8458	1.41	.	Q	.	V	.	.	.
14.650	0.8478	1.42	.	Q	.	V	.	.	.
14.667	0.8498	1.43	.	Q	.	V	.	.	.
14.683	0.8517	1.44	.	Q	.	V	.	.	.
14.700	0.8537	1.45	.	Q	.	V	.	.	.
14.717	0.8557	1.46	.	Q	.	V	.	.	.
14.733	0.8578	1.47	.	Q	.	V	.	.	.
14.750	0.8598	1.47	.	Q	.	V	.	.	.
14.767	0.8618	1.48	.	Q	.	V	.	.	.
14.783	0.8639	1.49	.	Q	.	V	.	.	.
14.800	0.8659	1.49	.	Q	.	V	.	.	.
14.817	0.8680	1.50	.	Q	.	V	.	.	.
14.833	0.8701	1.51	.	Q	.	V	.	.	.
14.850	0.8722	1.51	.	Q	.	V	.	.	.
14.867	0.8743	1.52	.	Q	.	V	.	.	.
14.883	0.8764	1.53	.	Q	.	V	.	.	.
14.900	0.8785	1.54	.	Q	.	V	.	.	.
14.917	0.8807	1.56	.	Q	.	V	.	.	.
14.933	0.8828	1.58	.	Q	.	V	.	.	.
14.950	0.8850	1.59	.	Q	.	V	.	.	.
14.967	0.8872	1.61	.	Q	.	V	.	.	.
14.983	0.8895	1.63	.	Q	.	V	.	.	.
15.000	0.8917	1.64	.	Q	.	V	.	.	.
15.017	0.8940	1.66	.	Q	.	V	.	.	.
15.033	0.8963	1.68	.	Q	.	V	.	.	.
15.050	0.8987	1.70	.	Q	.	V	.	.	.
15.067	0.9010	1.71	.	Q	.	V	.	.	.
15.083	0.9034	1.73	.	Q	.	V	.	.	.
15.100	0.9058	1.74	.	Q	.	V	.	.	.
15.117	0.9082	1.75	.	Q	.	V	.	.	.
15.133	0.9106	1.76	.	Q	.	V	.	.	.
15.150	0.9131	1.77	.	Q	.	V	.	.	.
15.167	0.9155	1.78	.	Q	.	V	.	.	.
15.183	0.9180	1.79	.	Q	.	V	.	.	.
15.200	0.9205	1.81	.	Q	.	V	.	.	.
15.217	0.9230	1.82	.	Q	.	V	.	.	.
15.233	0.9255	1.83	.	Q	.	V	.	.	.
15.250	0.9281	1.84	.	Q	.	V	.	.	.
15.267	0.9306	1.86	.	Q	.	V	.	.	.
15.283	0.9333	1.92	.	Q	.	V	.	.	.
15.300	0.9360	1.98	.	Q	.	V	.	.	.
15.317	0.9388	2.04	.	Q	.	V	.	.	.
15.333	0.9417	2.11	.	Q	.	V	.	.	.
15.350	0.9447	2.17	.	Q	.	V	.	.	.
15.367	0.9478	2.23	.	Q	.	V	.	.	.
15.383	0.9509	2.29	.	Q	.	V	.	.	.
15.400	0.9542	2.35	.	Q	.	V	.	.	.
15.417	0.9575	2.41	.	Q	.	V	.	.	.
15.433	0.9609	2.47	.	Q	.	V	.	.	.
15.450	0.9644	2.54	.	Q	.	V	.	.	.
15.467	0.9680	2.62	.	Q	.	V	.	.	.

15.483	0.9717	2.70	.	Q.	V	.
15.500	0.9756	2.79	.	Q.	V	.
15.517	0.9795	2.87	.	Q.	V	.
15.533	0.9836	2.95	.	Q.	V	.
15.550	0.9878	3.04	.	Q.	V	.
15.567	0.9921	3.12	.	Q.	V	.
15.583	0.9965	3.20	.	Q.	V	.
15.600	1.0010	3.29	.	Q.	V	.
15.617	1.0056	3.37	.	Q.	V	.
15.633	1.0104	3.45	.	Q	V	.
15.650	1.0153	3.53	.	.Q	.V	.
15.667	1.0202	3.60	.	.Q	.V	.
15.683	1.0253	3.67	.	.Q	.V	.
15.700	1.0304	3.74	.	.Q	.V	.
15.717	1.0357	3.82	.	.Q	.V	.
15.733	1.0410	3.89	.	.Q	.V	.
15.750	1.0465	3.96	.	.Q	.V	.
15.767	1.0521	4.03	.	.Q	.V	.
15.783	1.0577	4.10	.	.Q	.V	.
15.800	1.0635	4.18	.	.Q	.V	.
15.817	1.0693	4.25	.	.Q	.V	.
15.833	1.0753	4.34	.	.Q	.V	.
15.850	1.0814	4.45	.	.Q	.V	.
15.867	1.0877	4.56	.	.Q	.V	.
15.883	1.0941	4.67	.	.Q	.V	.
15.900	1.1007	4.77	.	.Q	.V	.
15.917	1.1074	4.88	.	.Q	.V	.
15.933	1.1143	4.99	.	.Q	.V	.
15.950	1.1213	5.10	.	.Q	.V	.
15.967	1.1285	5.20	.	.Q	.V	.
15.983	1.1358	5.31	.	.Q	.V	.
16.000	1.1433	5.42	.	.Q	.V	.
16.017	1.1513	5.80	.	Q	.V	.
16.033	1.1602	6.46	.	Q	V	.
16.050	1.1700	7.11	.	Q	V	.
16.067	1.1807	7.77	.	Q	.	.
16.083	1.1923	8.42	.	V	Q	.
16.100	1.2048	9.08	.	V	Q	.
16.117	1.2182	9.73	.	V	Q	.
16.133	1.2325	10.39	.	V	Q	.
16.150	1.2477	11.04	.	V	.	Q
16.167	1.2638	11.70	.	V	.	Q
16.183	1.2808	12.35	.	V	.	Q
16.200	1.2984	12.80	.	V	.	Q
16.217	1.3146	11.75	.	V	.	Q
16.233	1.3297	10.96	.	V	.	Q
16.250	1.3437	10.17	.	V	Q	.
16.267	1.3566	9.37	.	VQ	.	.
16.283	1.3684	8.58	.	V	Q	.
16.300	1.3792	7.79	.	Q	V	.
16.317	1.3888	6.99	.	Q	V	.
16.333	1.3974	6.20	.	Q.	V	.
16.350	1.4048	5.41	.	Q	V	.
16.367	1.4112	4.62	.	Q	V	.
16.383	1.4166	3.95	.	Q	V	.
16.400	1.4217	3.74	.	Q	V	.
16.417	1.4267	3.56	.	Q	V	.
16.433	1.4313	3.39	.	Q	V	.
16.450	1.4358	3.22	.	Q	V	.

16.467	1.4400	3.05	.	Q.	.	V.	.		17.450	1.5629	1.14	.	Q V	.
16.483	1.4439	2.87	.	Q	.	V.	.		17.467	1.5645	1.13	.	Q V	.
16.500	1.4476	2.70	.	Q	.	V	.		17.483	1.5660	1.12	.	Q V	.
16.517	1.4511	2.53	.	Q	.	V	.		17.500	1.5676	1.11	.	Q V	.
16.533	1.4544	2.35	.	Q	.	V	.		17.517	1.5691	1.10	.	Q V	.
16.550	1.4574	2.18	.	Q	.	V	.		17.533	1.5706	1.10	.	Q V	.
16.567	1.4602	2.02	.	Q	.	V	.		17.550	1.5721	1.09	.	Q V	.
16.583	1.4629	1.97	.	Q	.	V	.		17.567	1.5736	1.09	.	Q V	.
16.600	1.4655	1.93	.	Q	.	V	.		17.583	1.5751	1.08	.	Q V	.
16.617	1.4681	1.90	.	Q	.	V	.		17.600	1.5765	1.07	.	Q V	.
16.633	1.4707	1.87	.	Q	.	V	.		17.617	1.5780	1.07	.	Q V	.
16.650	1.4732	1.83	.	Q	.	V	.		17.633	1.5795	1.06	.	Q V	.
16.667	1.4757	1.80	.	Q	.	V	.		17.650	1.5809	1.05	.	Q V	.
16.683	1.4781	1.76	.	Q	.	V	.		17.667	1.5824	1.05	.	Q V	.
16.700	1.4805	1.73	.	Q	.	V	.		17.683	1.5838	1.04	.	Q V	.
16.717	1.4829	1.70	.	Q	.	V	.		17.700	1.5852	1.03	.	Q V	.
16.733	1.4852	1.66	.	Q	.	V	.		17.717	1.5866	1.03	.	Q V	.
16.750	1.4874	1.63	.	Q	.	V	.		17.733	1.5880	1.02	.	Q V	.
16.767	1.4896	1.60	.	Q	.	V	.		17.750	1.5894	1.02	.	Q V	.
16.783	1.4918	1.58	.	Q	.	V	.		17.767	1.5908	1.01	.	Q V	.
16.800	1.4939	1.56	.	Q	.	.V	.		17.783	1.5922	1.01	.	Q V	.
16.817	1.4961	1.54	.	Q	.	.V	.		17.800	1.5936	1.00	.	Q V	.
16.833	1.4982	1.52	.	Q	.	.V	.		17.817	1.5950	1.00	.	Q V	.
16.850	1.5002	1.50	.	Q	.	.V	.		17.833	1.5963	0.99	.	Q V	.
16.867	1.5023	1.48	.	Q	.	.V	.		17.850	1.5977	0.98	.	Q V	.
16.883	1.5043	1.46	.	Q	.	.V	.		17.867	1.5990	0.98	.	Q V	.
16.900	1.5062	1.44	.	Q	.	.V	.		17.883	1.6004	0.97	.	Q V	.
16.917	1.5082	1.42	.	Q	.	.V	.		17.900	1.6017	0.97	.	Q V	.
16.933	1.5101	1.40	.	Q	.	.V	.		17.917	1.6030	0.96	.	Q V	.
16.950	1.5120	1.38	.	Q	.	.V	.		17.933	1.6044	0.96	.	Q V	.
16.967	1.5139	1.37	.	Q	.	.V	.		17.950	1.6057	0.96	.	Q V	.
16.983	1.5158	1.35	.	Q	.	.V	.		17.967	1.6070	0.95	.	Q V	.
17.000	1.5176	1.34	.	Q	.	.V	.		17.983	1.6083	0.95	.	Q V	.
17.017	1.5194	1.32	.	Q	.	.V	.		18.000	1.6096	0.94	.	Q V	.
17.033	1.5212	1.31	.	Q	.	.V	.		18.017	1.6109	0.94	.	Q V	.
17.050	1.5230	1.30	.	Q	.	.V	.		18.033	1.6122	0.93	.	Q V	.
17.067	1.5248	1.28	.	Q	.	.V	.		18.050	1.6134	0.93	.	Q V	.
17.083	1.5265	1.27	.	Q	.	.V	.		18.067	1.6147	0.92	.	Q V	.
17.100	1.5283	1.25	.	Q	.	.V	.		18.083	1.6160	0.92	.	Q V	.
17.117	1.5300	1.24	.	Q	.	.V	.		18.100	1.6173	0.92	.	Q V	.
17.133	1.5317	1.23	.	Q	.	.V	.		18.117	1.6185	0.92	.	Q V	.
17.150	1.5334	1.23	.	Q	.	.V	.		18.133	1.6198	0.92	.	Q V	.
17.167	1.5351	1.23	.	Q	.	.V	.		18.150	1.6211	0.92	.	Q V	.
17.183	1.5367	1.22	.	Q	.	.V	.		18.167	1.6223	0.92	.	Q V	.
17.200	1.5384	1.22	.	Q	.	.V	.		18.183	1.6236	0.92	.	Q V	.
17.217	1.5401	1.22	.	Q	.	.V	.		18.200	1.6249	0.92	.	Q V	.
17.233	1.5418	1.22	.	Q	.	.V	.		18.217	1.6261	0.92	.	Q V	.
17.250	1.5434	1.21	.	Q	.	.V	.		18.233	1.6274	0.92	.	Q V	.
17.267	1.5451	1.21	.	Q	.	.V	.		18.250	1.6287	0.92	.	Q V	.
17.283	1.5468	1.21	.	Q	.	.V	.		18.267	1.6299	0.91	.	Q V	.
17.300	1.5484	1.21	.	Q	.	.V	.		18.283	1.6312	0.91	.	Q V	.
17.317	1.5501	1.20	.	Q	.	.V	.		18.300	1.6324	0.91	.	Q V	.
17.333	1.5517	1.19	.	Q	.	.V	.		18.317	1.6337	0.90	.	Q V	.
17.350	1.5534	1.18	.	Q	.	.V	.		18.333	1.6349	0.90	.	Q V	.
17.367	1.5550	1.18	.	Q	.	.V	.		18.350	1.6361	0.89	.	Q V	.
17.383	1.5566	1.17	.	Q	.	.V	.		18.367	1.6374	0.89	.	Q V	.
17.400	1.5582	1.16	.	Q	.	.V	.		18.383	1.6386	0.89	.	Q V	.
17.417	1.5598	1.15	.	Q	.	.V	.		18.400	1.6398	0.88	.	Q V	.
17.433	1.5614	1.14	.	Q	.	.V	.		18.417	1.6410	0.88	.	Q V	.

18.433	1.6422	0.88	. Q	.	.	.	V	.		19.417	1.7070	0.73	. Q	.	.	.	V	.
18.450	1.6434	0.87	. Q	.	.	.	V	.		19.433	1.7080	0.73	. Q	.	.	.	V	.
18.467	1.6446	0.87	. Q	.	.	.	V	.		19.450	1.7090	0.73	. Q	.	.	.	V	.
18.483	1.6458	0.87	. Q	.	.	.	V	.		19.467	1.7100	0.73	. Q	.	.	.	V	.
18.500	1.6470	0.87	. Q	.	.	.	V	.		19.483	1.7110	0.72	. Q	.	.	.	V	.
18.517	1.6482	0.86	. Q	.	.	.	V	.		19.500	1.7120	0.72	. Q	.	.	.	V	.
18.533	1.6494	0.86	. Q	.	.	.	V	.		19.517	1.7130	0.72	. Q	.	.	.	V	.
18.550	1.6506	0.86	. Q	.	.	.	V	.		19.533	1.7140	0.72	. Q	.	.	.	V	.
18.567	1.6517	0.85	. Q	.	.	.	V	.		19.550	1.7149	0.72	. Q	.	.	.	V	.
18.583	1.6529	0.85	. Q	.	.	.	V	.		19.567	1.7159	0.71	. Q	.	.	.	V	.
18.600	1.6541	0.85	. Q	.	.	.	V	.		19.583	1.7169	0.71	. Q	.	.	.	V	.
18.617	1.6552	0.84	. Q	.	.	.	V	.		19.600	1.7179	0.71	. Q	.	.	.	V	.
18.633	1.6564	0.84	. Q	.	.	.	V	.		19.617	1.7189	0.71	. Q	.	.	.	V	.
18.650	1.6575	0.84	. Q	.	.	.	V	.		19.633	1.7198	0.71	. Q	.	.	.	V	.
18.667	1.6587	0.84	. Q	.	.	.	V	.		19.650	1.7208	0.71	. Q	.	.	.	V	.
18.683	1.6598	0.83	. Q	.	.	.	V	.		19.667	1.7218	0.70	. Q	.	.	.	V	.
18.700	1.6610	0.83	. Q	.	.	.	V	.		19.683	1.7228	0.70	. Q	.	.	.	V	.
18.717	1.6621	0.83	. Q	.	.	.	V	.		19.700	1.7237	0.70	. Q	.	.	.	V	.
18.733	1.6633	0.82	. Q	.	.	.	V	.		19.717	1.7247	0.70	. Q	.	.	.	V	.
18.750	1.6644	0.82	. Q	.	.	.	V	.		19.733	1.7256	0.70	. Q	.	.	.	V	.
18.767	1.6655	0.82	. Q	.	.	.	V	.		19.750	1.7266	0.70	. Q	.	.	.	V	.
18.783	1.6666	0.82	. Q	.	.	.	V	.		19.767	1.7276	0.69	. Q	.	.	.	V	.
18.800	1.6678	0.81	. Q	.	.	.	V	.		19.783	1.7285	0.69	. Q	.	.	.	V	.
18.817	1.6689	0.81	. Q	.	.	.	V	.		19.800	1.7295	0.69	. Q	.	.	.	V	.
18.833	1.6700	0.81	. Q	.	.	.	V	.		19.817	1.7304	0.69	. Q	.	.	.	V	.
18.850	1.6711	0.81	. Q	.	.	.	V	.		19.833	1.7314	0.69	. Q	.	.	.	V	.
18.867	1.6722	0.80	. Q	.	.	.	V	.		19.850	1.7323	0.69	. Q	.	.	.	V	.
18.883	1.6733	0.80	. Q	.	.	.	V	.		19.867	1.7333	0.69	. Q	.	.	.	V	.
18.900	1.6744	0.80	. Q	.	.	.	V	.		19.883	1.7342	0.68	. Q	.	.	.	V	.
18.917	1.6755	0.80	. Q	.	.	.	V	.		19.900	1.7351	0.68	. Q	.	.	.	V	.
18.933	1.6766	0.79	. Q	.	.	.	V	.		19.917	1.7361	0.68	. Q	.	.	.	V	.
18.950	1.6777	0.79	. Q	.	.	.	V	.		19.933	1.7370	0.68	. Q	.	.	.	V	.
18.967	1.6788	0.79	. Q	.	.	.	V	.		19.950	1.7379	0.68	. Q	.	.	.	V	.
18.983	1.6799	0.79	. Q	.	.	.	V	.		19.967	1.7389	0.68	. Q	.	.	.	V	.
19.000	1.6809	0.78	. Q	.	.	.	V	.		19.983	1.7398	0.67	. Q	.	.	.	V	.
19.017	1.6820	0.78	. Q	.	.	.	V	.		20.000	1.7407	0.67	. Q	.	.	.	V	.
19.033	1.6831	0.78	. Q	.	.	.	V	.		20.017	1.7417	0.67	. Q	.	.	.	V	.
19.050	1.6842	0.78	. Q	.	.	.	V	.		20.033	1.7426	0.67	. Q	.	.	.	V	.
19.067	1.6852	0.78	. Q	.	.	.	V	.		20.050	1.7435	0.67	. Q	.	.	.	V	.
19.083	1.6863	0.77	. Q	.	.	.	V	.		20.067	1.7444	0.67	. Q	.	.	.	V	.
19.100	1.6874	0.77	. Q	.	.	.	V	.		20.083	1.7453	0.67	. Q	.	.	.	V	.
19.117	1.6884	0.77	. Q	.	.	.	V	.		20.100	1.7462	0.66	. Q	.	.	.	V	.
19.133	1.6895	0.77	. Q	.	.	.	V	.		20.117	1.7472	0.66	. Q	.	.	.	V	.
19.150	1.6905	0.76	. Q	.	.	.	V	.		20.133	1.7481	0.66	. Q	.	.	.	V	.
19.167	1.6916	0.76	. Q	.	.	.	V	.		20.150	1.7490	0.66	. Q	.	.	.	V	.
19.183	1.6926	0.76	. Q	.	.	.	V	.		20.167	1.7499	0.66	. Q	.	.	.	V	.
19.200	1.6937	0.76	. Q	.	.	.	V	.		20.183	1.7508	0.66	. Q	.	.	.	V	.
19.217	1.6947	0.76	. Q	.	.	.	V	.		20.200	1.7517	0.66	. Q	.	.	.	V	.
19.233	1.6957	0.75	. Q	.	.	.	V	.		20.217	1.7526	0.65	. Q	.	.	.	V	.
19.250	1.6968	0.75	. Q	.	.	.	V	.		20.233	1.7535	0.65	. Q	.	.	.	V	.
19.267	1.6978	0.75	. Q	.	.	.	V	.		20.250	1.7544	0.65	. Q	.	.	.	V	.
19.283	1.6988	0.75	. Q	.	.	.	V	.		20.267	1.7553	0.65	. Q	.	.	.	V	.
19.300	1.6999	0.75	. Q	.	.	.	V	.		20.283	1.7562	0.65	. Q	.	.	.	V	.
19.317	1.7009	0.74	. Q	.	.	.	V	.		20.300	1.7571	0.65	. Q	.	.	.	V	.
19.333	1.7019	0.74	. Q	.	.	.	V	.		20.317	1.7580	0.65	. Q	.	.	.	V	.
19.350	1.7029	0.74	. Q	.	.	.	V	.		20.333	1.7589	0.65	. Q	.	.	.	V	.
19.367	1.7039	0.74	. Q	.	.	.	V	.		20.350	1.7597	0.64	. Q	.	.	.	V	.
19.383	1.7050	0.74	. Q	.	.	.	V	.		20.367	1.7606	0.64	. Q	.	.	.	V	.
19.400	1.7060	0.73	. Q	.	.	.	V	.		20.383	1.7615	0.64	. Q	.	.	.	V	.

20.400	1.7624	0.64	. Q	.	.	.	V	.		21.383	1.8116	0.58	. Q	V .
20.417	1.7633	0.64	. Q	.	.	.	V	.		21.400	1.8124	0.57	. Q	V .
20.433	1.7641	0.64	. Q	.	.	.	V	.		21.417	1.8132	0.57	. Q	V .
20.450	1.7650	0.64	. Q	.	.	.	V	.		21.433	1.8140	0.57	. Q	V .
20.467	1.7659	0.63	. Q	.	.	.	V	.		21.450	1.8148	0.57	. Q	V .
20.483	1.7668	0.63	. Q	.	.	.	V	.		21.467	1.8156	0.57	. Q	V .
20.500	1.7676	0.63	. Q	.	.	.	V	.		21.483	1.8163	0.57	. Q	V .
20.517	1.7685	0.63	. Q	.	.	.	V	.		21.500	1.8171	0.57	. Q	V .
20.533	1.7694	0.63	. Q	.	.	.	V	.		21.517	1.8179	0.57	. Q	V .
20.550	1.7702	0.63	. Q	.	.	.	V	.		21.533	1.8187	0.57	. Q	V .
20.567	1.7711	0.63	. Q	.	.	.	V	.		21.550	1.8195	0.57	. Q	V .
20.583	1.7720	0.63	. Q	.	.	.	V	.		21.567	1.8202	0.57	. Q	V .
20.600	1.7728	0.63	. Q	.	.	.	V	.		21.583	1.8210	0.56	. Q	V .
20.617	1.7737	0.62	. Q	.	.	.	V	.		21.600	1.8218	0.56	. Q	V .
20.633	1.7746	0.62	. Q	.	.	.	V	.		21.617	1.8226	0.56	. Q	V .
20.650	1.7754	0.62	. Q	.	.	.	V	.		21.633	1.8234	0.56	. Q	V .
20.667	1.7763	0.62	. Q	.	.	.	V	.		21.650	1.8241	0.56	. Q	V .
20.683	1.7771	0.62	. Q	.	.	.	V	.		21.667	1.8249	0.56	. Q	V .
20.700	1.7780	0.62	. Q	.	.	.	V	.		21.683	1.8257	0.56	. Q	V .
20.717	1.7788	0.62	. Q	.	.	.	V	.		21.700	1.8264	0.56	. Q	V .
20.733	1.7797	0.62	. Q	.	.	.	V	.		21.717	1.8272	0.56	. Q	V .
20.750	1.7805	0.61	. Q	.	.	.	V	.		21.733	1.8280	0.56	. Q	V .
20.767	1.7814	0.61	. Q	.	.	.	V	.		21.750	1.8287	0.56	. Q	V .
20.783	1.7822	0.61	. Q	.	.	.	V	.		21.767	1.8295	0.56	. Q	V .
20.800	1.7830	0.61	. Q	.	.	.	V	.		21.783	1.8303	0.55	. Q	V .
20.817	1.7839	0.61	. Q	.	.	.	V	.		21.800	1.8310	0.55	. Q	V .
20.833	1.7847	0.61	. Q	.	.	.	V	.		21.817	1.8318	0.55	. Q	V .
20.850	1.7856	0.61	. Q	.	.	.	V	.		21.833	1.8326	0.55	. Q	V .
20.867	1.7864	0.61	. Q	.	.	.	V	.		21.850	1.8333	0.55	. Q	V .
20.883	1.7872	0.61	. Q	.	.	.	V	.		21.867	1.8341	0.55	. Q	V .
20.900	1.7881	0.60	. Q	.	.	.	V	.		21.883	1.8348	0.55	. Q	V .
20.917	1.7889	0.60	. Q	.	.	.	V	.		21.900	1.8356	0.55	. Q	V .
20.933	1.7897	0.60	. Q	.	.	.	V	.		21.917	1.8363	0.55	. Q	V .
20.950	1.7906	0.60	. Q	.	.	.	V	.		21.933	1.8371	0.55	. Q	V .
20.967	1.7914	0.60	. Q	.	.	.	V	.		21.950	1.8378	0.55	. Q	V .
20.983	1.7922	0.60	. Q	.	.	.	V	.		21.967	1.8386	0.55	. Q	V .
21.000	1.7930	0.60	. Q	.	.	.	V	.		21.983	1.8393	0.54	. Q	V .
21.017	1.7939	0.60	. Q	.	.	.	V	.		22.000	1.8401	0.54	. Q	V .
21.033	1.7947	0.60	. Q	.	.	.	V	.		22.017	1.8408	0.54	. Q	V .
21.050	1.7955	0.60	. Q	.	.	.	V	.		22.033	1.8416	0.54	. Q	V .
21.067	1.7963	0.59	. Q	.	.	.	V	.		22.050	1.8423	0.54	. Q	V .
21.083	1.7971	0.59	. Q	.	.	.	V	.		22.067	1.8431	0.54	. Q	V .
21.100	1.7979	0.59	. Q	.	.	.	V	.		22.083	1.8438	0.54	. Q	V .
21.117	1.7988	0.59	. Q	.	.	.	V	.		22.100	1.8446	0.54	. Q	V .
21.133	1.7996	0.59	. Q	.	.	.	V	.		22.117	1.8453	0.54	. Q	V .
21.150	1.8004	0.59	. Q	.	.	.	V	.		22.133	1.8461	0.54	. Q	V .
21.167	1.8012	0.59	. Q	.	.	.	V	.		22.150	1.8468	0.54	. Q	V .
21.183	1.8020	0.59	. Q	.	.	.	V	.		22.167	1.8475	0.54	. Q	V .
21.200	1.8028	0.59	. Q	.	.	.	V	.		22.183	1.8483	0.54	. Q	V .
21.217	1.8036	0.59	. Q	.	.	.	V	.		22.200	1.8490	0.53	. Q	V .
21.233	1.8044	0.58	. Q	.	.	.	V	.		22.217	1.8497	0.53	. Q	V .
21.250	1.8052	0.58	. Q	.	.	.	V	.		22.233	1.8505	0.53	. Q	V .
21.267	1.8060	0.58	. Q	.	.	.	V	.		22.250	1.8512	0.53	. Q	V .
21.283	1.8068	0.58	. Q	.	.	.	V	.		22.267	1.8519	0.53	. Q	V .
21.300	1.8076	0.58	. Q	.	.	.	V	.		22.283	1.8527	0.53	. Q	V .
21.317	1.8084	0.58	. Q	.	.	.	V	.		22.300	1.8534	0.53	. Q	V .
21.333	1.8092	0.58	. Q	.	.	.	V	.		22.317	1.8541	0.53	. Q	V .
21.350	1.8100	0.58	. Q	.	.	.	V	.		22.333	1.8549	0.53	. Q	V .
21.367	1.8108	0.58	. Q	.	.	.	V	.		22.350	1.8556	0.53	. Q	V .

22.367	1.8563	0.53	.Q	.	.	.	V .
22.383	1.8570	0.53	.Q	.	.	.	V .
22.400	1.8578	0.53	.Q	.	.	.	V .
22.417	1.8585	0.53	.Q	.	.	.	V .
22.433	1.8592	0.52	.Q	.	.	.	V .
22.450	1.8599	0.52	.Q	.	.	.	V .
22.467	1.8607	0.52	.Q	.	.	.	V .
22.483	1.8614	0.52	.Q	.	.	.	V .
22.500	1.8621	0.52	.Q	.	.	.	V .
22.517	1.8628	0.52	.Q	.	.	.	V .
22.533	1.8635	0.52	.Q	.	.	.	V .
22.550	1.8642	0.52	.Q	.	.	.	V .
22.567	1.8650	0.52	.Q	.	.	.	V .
22.583	1.8657	0.52	.Q	.	.	.	V .
22.600	1.8664	0.52	.Q	.	.	.	V .
22.617	1.8671	0.52	.Q	.	.	.	V .
22.633	1.8678	0.52	.Q	.	.	.	V .
22.650	1.8685	0.52	.Q	.	.	.	V .
22.667	1.8692	0.52	.Q	.	.	.	V .
22.683	1.8699	0.51	.Q	.	.	.	V .
22.700	1.8706	0.51	.Q	.	.	.	V .
22.717	1.8714	0.51	.Q	.	.	.	V .
22.733	1.8721	0.51	.Q	.	.	.	V .
22.750	1.8728	0.51	.Q	.	.	.	V .
22.767	1.8735	0.51	.Q	.	.	.	V .
22.783	1.8742	0.51	.Q	.	.	.	V .
22.800	1.8749	0.51	.Q	.	.	.	V .
22.817	1.8756	0.51	.Q	.	.	.	V .
22.833	1.8763	0.51	.Q	.	.	.	V .
22.850	1.8770	0.51	.Q	.	.	.	V .
22.867	1.8777	0.51	.Q	.	.	.	V .
22.883	1.8784	0.51	.Q	.	.	.	V .
22.900	1.8791	0.51	.Q	.	.	.	V .
22.917	1.8798	0.51	.Q	.	.	V.	
22.933	1.8805	0.50	.Q	.	.	V.	
22.950	1.8812	0.50	.Q	.	.	V.	
22.967	1.8818	0.50	.Q	.	.	V.	
22.983	1.8825	0.50	.Q	.	.	V.	
23.000	1.8832	0.50	.Q	.	.	V.	
23.017	1.8839	0.50	.Q	.	.	V.	
23.033	1.8846	0.50	.Q	.	.	V.	
23.050	1.8853	0.50	.Q	.	.	V.	
23.067	1.8860	0.50	.Q	.	.	V.	
23.083	1.8867	0.50	.Q	.	.	V.	
23.100	1.8874	0.50	.Q	.	.	V.	
23.117	1.8881	0.50	.Q	.	.	V.	
23.133	1.8887	0.50	.Q	.	.	V.	
23.150	1.8894	0.50	.Q	.	.	V.	
23.167	1.8901	0.50	.Q	.	.	V.	
23.183	1.8908	0.50	.Q	.	.	V.	
23.200	1.8915	0.49	.Q	.	.	V.	
23.217	1.8922	0.49	.Q	.	.	V.	
23.233	1.8928	0.49	.Q	.	.	V.	
23.250	1.8935	0.49	.Q	.	.	V.	
23.267	1.8942	0.49	.Q	.	.	V.	
23.283	1.8949	0.49	.Q	.	.	V.	
23.300	1.8955	0.49	.Q	.	.	V.	
23.317	1.8962	0.49	.Q	.	.	V.	
23.333	1.8969	0.49	.Q	.	.	V.	

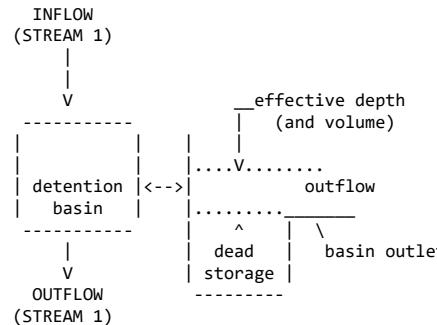
23.350	1.8976	0.49	.Q	.	.	.	V.
23.367	1.8982	0.49	.Q	.	.	.	V.
23.383	1.8989	0.49	.Q	.	.	.	V.
23.400	1.8996	0.49	.Q	.	.	.	V.
23.417	1.9003	0.49	.Q	.	.	.	V.
23.433	1.9009	0.49	.Q	.	.	.	V.
23.450	1.9016	0.49	.Q	.	.	.	V.
23.467	1.9023	0.49	.Q	.	.	.	V.
23.483	1.9029	0.49	.Q	.	.	.	V.
23.500	1.9036	0.48	.Q	.	.	.	V.
23.517	1.9043	0.48	.Q	.	.	.	V.
23.533	1.9049	0.48	.Q	.	.	.	V.
23.550	1.9056	0.48	.Q	.	.	.	V.
23.567	1.9063	0.48	.Q	.	.	.	V.
23.583	1.9069	0.48	.Q	.	.	.	V.
23.600	1.9076	0.48	.Q	.	.	.	V.
23.617	1.9083	0.48	.Q	.	.	.	V.
23.633	1.9089	0.48	.Q	.	.	.	V.
23.650	1.9096	0.48	.Q	.	.	.	V.
23.667	1.9102	0.48	.Q	.	.	.	V.
23.683	1.9109	0.48	.Q	.	.	.	V.
23.700	1.9116	0.48	.Q	.	.	.	V.
23.717	1.9122	0.48	.Q	.	.	.	V.
23.733	1.9129	0.48	.Q	.	.	.	V.
23.750	1.9135	0.48	.Q	.	.	.	V.
23.767	1.9142	0.48	.Q	.	.	.	V.
23.783	1.9148	0.48	.Q	.	.	.	V.
23.800	1.9155	0.47	.Q	.	.	.	V.
23.817	1.9161	0.47	.Q	.	.	.	V.
23.833	1.9168	0.47	.Q	.	.	.	V.
23.850	1.9174	0.47	.Q	.	.	.	V.
23.867	1.9181	0.47	.Q	.	.	.	V.
23.883	1.9187	0.47	.Q	.	.	.	V.
23.900	1.9194	0.47	.Q	.	.	.	V.
23.917	1.9200	0.47	.Q	.	.	.	V.
23.933	1.9207	0.47	.Q	.	.	.	V.
23.950	1.9213	0.47	.Q	.	.	.	V.
23.967	1.9220	0.47	.Q	.	.	.	V.
23.983	1.9226	0.47	.Q	.	.	.	V.
24.000	1.9233	0.47	.Q	.	.	.	V.

TIME DURATION(minutes) OF PERCENTILES OF ESTIMATED PEAK FLOW RATE:
 (Note: 100% of Peak Flow Rate estimate assumed to have
 an instantaneous time duration)

Percentile of Estimated Peak Flow Rate	Duration (minutes)
0%	1441.0
10%	820.0
20%	315.0
30%	200.0
40%	120.0
50%	90.0
60%	75.0
70%	55.0
80%	35.0
90%	20.0

FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 3.2

>>>> FLOW-THROUGH DETENTION BASIN ROUTING MODEL APPLIED TO STREAM #1<<<<



ROUTE RUNOFF HYDROGRAPH FROM STREAM NUMBER 1

THROUGH A FLOW-THROUGH DETENTION BASIN

SPECIFIED BASIN CONDITIONS ARE AS FOLLOWS:

DEAD STORAGE(AF) = 0.000

SPECIFIED DEAD STORAGE(AF) FILLED = 0.000

SPECIFIED EFFECTIVE VOLUME(AF) FILLED ABOVE OUTLET = 0.000

DETENTION BASIN CONSTANT LOSS RATE(CFS) = 0.00

BASIN DEPTH VERSUS OUTFLOW AND STORAGE INFORMATION:

INTERVAL NUMBER	DEPTH (FT)	OUTFLOW (CFS)	STORAGE (AF)
1	0.00	0.00	0.000
2	0.50	0.01	0.045
3	1.00	2.70	0.097
4	2.00	4.80	0.222
5	3.00	6.10	0.380
6	4.00	7.30	0.568

0.083	0.000	0.22	0.00	0.01	0.0	0.001
0.100	0.000	0.26	0.00	0.01	0.0	0.001
0.117	0.000	0.31	0.00	0.02	0.0	0.002
0.133	0.000	0.36	0.00	0.02	0.0	0.002
0.150	0.000	0.41	0.00	0.03	0.0	0.003
0.167	0.000	0.45	0.00	0.04	0.0	0.003
0.183	0.000	0.46	0.00	0.04	0.0	0.004
0.200	0.000	0.46	0.00	0.05	0.0	0.005
0.217	0.000	0.46	0.00	0.06	0.0	0.005
0.233	0.000	0.47	0.00	0.06	0.0	0.006
0.250	0.000	0.47	0.00	0.07	0.0	0.006
0.267	0.000	0.47	0.00	0.08	0.0	0.007
0.283	0.000	0.47	0.00	0.09	0.0	0.008
0.300	0.000	0.47	0.00	0.09	0.0	0.008
0.317	0.000	0.47	0.00	0.10	0.0	0.009
0.333	0.000	0.47	0.00	0.11	0.0	0.010
0.350	0.000	0.47	0.00	0.11	0.0	0.010
0.367	0.000	0.47	0.00	0.12	0.0	0.011
0.383	0.000	0.47	0.00	0.13	0.0	0.012
0.400	0.000	0.47	0.00	0.14	0.0	0.012
0.417	0.000	0.47	0.00	0.14	0.0	0.013
0.433	0.000	0.47	0.00	0.15	0.0	0.014
0.450	0.000	0.47	0.00	0.16	0.0	0.014
0.467	0.000	0.47	0.00	0.16	0.0	0.015
0.483	0.000	0.47	0.00	0.17	0.0	0.015
0.500	0.000	0.47	0.00	0.18	0.0	0.016
0.517	0.000	0.47	0.00	0.19	0.0	0.017
0.533	0.000	0.47	0.00	0.19	0.0	0.017
0.550	0.000	0.47	0.00	0.20	0.0	0.018
0.567	0.000	0.47	0.00	0.21	0.0	0.019
0.583	0.000	0.47	0.00	0.21	0.0	0.019
0.600	0.000	0.47	0.00	0.22	0.0	0.020
0.617	0.000	0.47	0.00	0.23	0.0	0.021
0.633	0.000	0.47	0.00	0.24	0.0	0.021
0.650	0.000	0.47	0.00	0.24	0.0	0.022
0.667	0.000	0.47	0.00	0.25	0.0	0.022
0.683	0.000	0.47	0.00	0.26	0.0	0.023
0.700	0.000	0.47	0.00	0.26	0.0	0.024
0.717	0.000	0.47	0.00	0.27	0.0	0.024
0.733	0.000	0.47	0.00	0.28	0.0	0.025
0.750	0.000	0.47	0.00	0.29	0.0	0.026
0.767	0.000	0.47	0.00	0.29	0.0	0.026
0.783	0.000	0.47	0.00	0.30	0.0	0.027
0.800	0.000	0.47	0.00	0.31	0.0	0.028
0.817	0.000	0.47	0.00	0.31	0.0	0.028
0.833	0.000	0.47	0.00	0.32	0.0	0.029
0.850	0.000	0.47	0.00	0.33	0.0	0.030
0.867	0.000	0.47	0.00	0.34	0.0	0.030
0.883	0.000	0.48	0.00	0.34	0.0	0.031
0.900	0.000	0.48	0.00	0.35	0.0	0.031
0.917	0.000	0.48	0.00	0.36	0.0	0.032
0.933	0.000	0.48	0.00	0.36	0.0	0.033
0.950	0.000	0.48	0.00	0.37	0.0	0.033
0.967	0.000	0.48	0.00	0.38	0.0	0.034
0.983	0.000	0.48	0.00	0.39	0.0	0.035
1.000	0.000	0.48	0.00	0.39	0.0	0.035
1.017	0.000	0.48	0.00	0.40	0.0	0.036
1.033	0.000	0.48	0.00	0.41	0.0	0.037
1.050	0.000	0.48	0.00	0.41	0.0	0.037

MODIFIED-PULS BASIN ROUTING MODEL RESULTS(1-MINUTE COMPUTATION INTERVALS):

(Note: Computed EFFECTIVE DEPTH and VOLUME are estimated at the clock time;
MEAN OUTFLOW is the average value during the unit interval.)

CLOCK TIME (HRS)	DEAD-STORAGE (FILLED(AF))	INFLOW (CFS)	LOSS (CFS)	EFFECTIVE DEPTH(FT)	OUTFLOW (CFS)	MEAN EFFECTIVE VOLUME(AF)
0.017	0.000	0.02	0.00	0.0	0.000	
0.033	0.000	0.07	0.00	0.0	0.000	
0.050	0.000	0.12	0.00	0.0	0.000	
0.067	0.000	0.17	0.00	0.01	0.001	

14.833	0.000	1.51	0.00	0.76	1.4	0.072		15.817	0.000	4.25	0.00	1.12	2.9	0.112
14.850	0.000	1.51	0.00	0.76	1.4	0.072		15.833	0.000	4.34	0.00	1.13	3.0	0.114
14.867	0.000	1.52	0.00	0.76	1.4	0.072		15.850	0.000	4.45	0.00	1.15	3.0	0.116
14.883	0.000	1.53	0.00	0.76	1.4	0.072		15.867	0.000	4.56	0.00	1.17	3.0	0.118
14.900	0.000	1.54	0.00	0.77	1.4	0.073		15.883	0.000	4.67	0.00	1.18	3.1	0.120
14.917	0.000	1.56	0.00	0.77	1.4	0.073		15.900	0.000	4.77	0.00	1.20	3.1	0.122
14.933	0.000	1.58	0.00	0.77	1.5	0.073		15.917	0.000	4.88	0.00	1.22	3.1	0.125
14.950	0.000	1.59	0.00	0.77	1.5	0.073		15.933	0.000	4.99	0.00	1.24	3.2	0.127
14.967	0.000	1.61	0.00	0.77	1.5	0.073		15.950	0.000	5.10	0.00	1.26	3.2	0.130
14.983	0.000	1.63	0.00	0.77	1.5	0.074		15.967	0.000	5.20	0.00	1.28	3.3	0.132
15.000	0.000	1.64	0.00	0.78	1.5	0.074		15.983	0.000	5.31	0.00	1.30	3.3	0.135
15.017	0.000	1.66	0.00	0.78	1.5	0.074		16.000	0.000	5.42	0.00	1.33	3.4	0.138
15.033	0.000	1.68	0.00	0.78	1.5	0.074		16.017	0.000	5.80	0.00	1.35	3.4	0.141
15.050	0.000	1.70	0.00	0.78	1.5	0.074		16.033	0.000	6.46	0.00	1.39	3.5	0.145
15.067	0.000	1.71	0.00	0.79	1.5	0.075		16.050	0.000	7.11	0.00	1.43	3.6	0.150
15.083	0.000	1.73	0.00	0.79	1.6	0.075		16.067	0.000	7.77	0.00	1.47	3.6	0.156
15.100	0.000	1.74	0.00	0.79	1.6	0.075		16.083	0.000	8.42	0.00	1.52	3.7	0.162
15.117	0.000	1.75	0.00	0.79	1.6	0.075		16.100	0.000	9.08	0.00	1.58	3.9	0.169
15.133	0.000	1.76	0.00	0.79	1.6	0.076		16.117	0.000	9.73	0.00	1.64	4.0	0.177
15.150	0.000	1.77	0.00	0.80	1.6	0.076		16.133	0.000	10.39	0.00	1.71	4.1	0.186
15.167	0.000	1.78	0.00	0.80	1.6	0.076		16.150	0.000	11.04	0.00	1.79	4.3	0.195
15.183	0.000	1.79	0.00	0.80	1.6	0.076		16.167	0.000	11.70	0.00	1.87	4.4	0.205
15.200	0.000	1.81	0.00	0.80	1.6	0.077		16.183	0.000	12.35	0.00	1.95	4.6	0.216
15.217	0.000	1.82	0.00	0.81	1.6	0.077		16.200	0.000	12.80	0.00	2.03	4.8	0.227
15.233	0.000	1.83	0.00	0.81	1.7	0.077		16.217	0.000	11.75	0.00	2.09	4.9	0.237
15.250	0.000	1.84	0.00	0.81	1.7	0.077		16.233	0.000	10.96	0.00	2.14	5.0	0.245
15.267	0.000	1.86	0.00	0.81	1.7	0.077		16.250	0.000	10.17	0.00	2.19	5.0	0.252
15.283	0.000	1.92	0.00	0.82	1.7	0.078		16.267	0.000	9.37	0.00	2.23	5.1	0.258
15.300	0.000	1.98	0.00	0.82	1.7	0.078		16.283	0.000	8.58	0.00	2.26	5.1	0.263
15.317	0.000	2.04	0.00	0.82	1.7	0.079		16.300	0.000	7.79	0.00	2.28	5.1	0.266
15.333	0.000	2.11	0.00	0.83	1.8	0.079		16.317	0.000	6.99	0.00	2.30	5.2	0.269
15.350	0.000	2.17	0.00	0.83	1.8	0.080		16.333	0.000	6.20	0.00	2.30	5.2	0.270
15.367	0.000	2.23	0.00	0.84	1.8	0.080		16.350	0.000	5.41	0.00	2.31	5.2	0.270
15.383	0.000	2.29	0.00	0.84	1.8	0.081		16.367	0.000	4.62	0.00	2.30	5.2	0.270
15.400	0.000	2.35	0.00	0.85	1.9	0.081		16.383	0.000	3.95	0.00	2.29	5.2	0.268
15.417	0.000	2.41	0.00	0.86	1.9	0.082		16.400	0.000	3.74	0.00	2.28	5.2	0.266
15.433	0.000	2.47	0.00	0.86	1.9	0.083		16.417	0.000	3.56	0.00	2.26	5.2	0.264
15.450	0.000	2.54	0.00	0.87	2.0	0.084		16.433	0.000	3.39	0.00	2.25	5.1	0.261
15.467	0.000	2.62	0.00	0.88	2.0	0.084		16.450	0.000	3.22	0.00	2.23	5.1	0.259
15.483	0.000	2.70	0.00	0.89	2.1	0.085		16.467	0.000	3.05	0.00	2.21	5.1	0.256
15.500	0.000	2.79	0.00	0.90	2.1	0.086		16.483	0.000	2.87	0.00	2.20	5.1	0.253
15.517	0.000	2.87	0.00	0.91	2.2	0.087		16.500	0.000	2.70	0.00	2.18	5.0	0.250
15.533	0.000	2.95	0.00	0.92	2.2	0.088		16.517	0.000	2.53	0.00	2.15	5.0	0.246
15.550	0.000	3.04	0.00	0.93	2.3	0.089		16.533	0.000	2.35	0.00	2.13	5.0	0.243
15.567	0.000	3.12	0.00	0.94	2.3	0.090		16.550	0.000	2.18	0.00	2.11	5.0	0.239
15.583	0.000	3.20	0.00	0.95	2.4	0.091		16.567	0.000	2.02	0.00	2.08	4.9	0.235
15.600	0.000	3.29	0.00	0.96	2.4	0.093		16.583	0.000	1.97	0.00	2.06	4.9	0.231
15.617	0.000	3.37	0.00	0.97	2.5	0.094		16.600	0.000	1.93	0.00	2.03	4.9	0.227
15.633	0.000	3.45	0.00	0.98	2.6	0.095		16.617	0.000	1.90	0.00	2.00	4.8	0.223
15.650	0.000	3.53	0.00	0.99	2.6	0.096		16.633	0.000	1.87	0.00	1.97	4.8	0.219
15.667	0.000	3.60	0.00	1.00	2.7	0.098		16.650	0.000	1.83	0.00	1.94	4.7	0.215
15.683	0.000	3.67	0.00	1.01	2.7	0.099		16.667	0.000	1.80	0.00	1.91	4.6	0.211
15.700	0.000	3.74	0.00	1.03	2.7	0.100		16.683	0.000	1.76	0.00	1.88	4.6	0.207
15.717	0.000	3.82	0.00	1.04	2.8	0.102		16.700	0.000	1.73	0.00	1.85	4.5	0.203
15.733	0.000	3.89	0.00	1.05	2.8	0.103		16.717	0.000	1.70	0.00	1.82	4.5	0.199
15.750	0.000	3.96	0.00	1.06	2.8	0.105		16.733	0.000	1.66	0.00	1.79	4.4	0.196
15.767	0.000	4.03	0.00	1.08	2.8	0.106		16.750	0.000	1.63	0.00	1.76	4.3	0.192
15.783	0.000	4.10	0.00	1.09	2.9	0.108		16.767	0.000	1.60	0.00	1.73	4.3	0.188
15.800	0.000	4.18	0.00	1.10	2.9	0.110		16.783	0.000	1.58	0.00	1.70	4.2	0.185

16.800	0.000	1.56	0.00	1.67	4.1	0.181		17.783	0.000	1.01	0.00	0.73	1.3	0.069
16.817	0.000	1.54	0.00	1.64	4.1	0.178		17.800	0.000	1.00	0.00	0.73	1.3	0.069
16.833	0.000	1.52	0.00	1.62	4.0	0.174		17.817	0.000	1.00	0.00	0.73	1.2	0.069
16.850	0.000	1.50	0.00	1.59	4.0	0.171		17.833	0.000	0.99	0.00	0.72	1.2	0.068
16.867	0.000	1.48	0.00	1.56	3.9	0.167		17.850	0.000	0.98	0.00	0.72	1.2	0.068
16.883	0.000	1.46	0.00	1.54	3.9	0.164		17.867	0.000	0.98	0.00	0.72	1.2	0.068
16.900	0.000	1.44	0.00	1.51	3.8	0.161		17.883	0.000	0.97	0.00	0.72	1.2	0.067
16.917	0.000	1.42	0.00	1.48	3.7	0.158		17.900	0.000	0.97	0.00	0.71	1.2	0.067
16.933	0.000	1.40	0.00	1.46	3.7	0.154		17.917	0.000	0.96	0.00	0.71	1.2	0.067
16.950	0.000	1.38	0.00	1.43	3.6	0.151		17.933	0.000	0.96	0.00	0.71	1.1	0.067
16.967	0.000	1.37	0.00	1.41	3.6	0.148		17.950	0.000	0.96	0.00	0.71	1.1	0.066
16.983	0.000	1.35	0.00	1.39	3.5	0.145		17.967	0.000	0.95	0.00	0.70	1.1	0.066
17.000	0.000	1.34	0.00	1.36	3.5	0.142		17.983	0.000	0.95	0.00	0.70	1.1	0.066
17.017	0.000	1.32	0.00	1.34	3.4	0.139		18.000	0.000	0.94	0.00	0.70	1.1	0.066
17.033	0.000	1.31	0.00	1.32	3.4	0.137		18.017	0.000	0.94	0.00	0.70	1.1	0.066
17.050	0.000	1.30	0.00	1.29	3.3	0.134		18.033	0.000	0.93	0.00	0.70	1.1	0.065
17.067	0.000	1.28	0.00	1.27	3.3	0.131		18.050	0.000	0.93	0.00	0.69	1.1	0.065
17.083	0.000	1.27	0.00	1.25	3.2	0.128		18.067	0.000	0.92	0.00	0.69	1.1	0.065
17.100	0.000	1.25	0.00	1.23	3.2	0.126		18.083	0.000	0.92	0.00	0.69	1.0	0.065
17.117	0.000	1.24	0.00	1.21	3.2	0.123		18.100	0.000	0.92	0.00	0.69	1.0	0.065
17.133	0.000	1.23	0.00	1.19	3.1	0.120		18.117	0.000	0.92	0.00	0.69	1.0	0.065
17.150	0.000	1.23	0.00	1.17	3.1	0.118		18.133	0.000	0.92	0.00	0.69	1.0	0.064
17.167	0.000	1.23	0.00	1.15	3.0	0.115		18.150	0.000	0.92	0.00	0.69	1.0	0.064
17.183	0.000	1.22	0.00	1.13	3.0	0.113		18.167	0.000	0.92	0.00	0.68	1.0	0.064
17.200	0.000	1.22	0.00	1.11	2.9	0.110		18.183	0.000	0.92	0.00	0.68	1.0	0.064
17.217	0.000	1.22	0.00	1.09	2.9	0.108		18.200	0.000	0.92	0.00	0.68	1.0	0.064
17.233	0.000	1.22	0.00	1.07	2.9	0.106		18.217	0.000	0.92	0.00	0.68	1.0	0.064
17.250	0.000	1.21	0.00	1.05	2.8	0.104		18.233	0.000	0.92	0.00	0.68	1.0	0.064
17.267	0.000	1.21	0.00	1.04	2.8	0.101		18.250	0.000	0.92	0.00	0.68	1.0	0.064
17.283	0.000	1.21	0.00	1.02	2.8	0.099		18.267	0.000	0.91	0.00	0.68	1.0	0.064
17.300	0.000	1.21	0.00	1.00	2.7	0.097		18.283	0.000	0.91	0.00	0.68	1.0	0.064
17.317	0.000	1.20	0.00	0.98	2.7	0.095		18.300	0.000	0.91	0.00	0.68	1.0	0.063
17.333	0.000	1.19	0.00	0.97	2.6	0.093		18.317	0.000	0.90	0.00	0.68	1.0	0.063
17.350	0.000	1.18	0.00	0.95	2.5	0.092		18.333	0.000	0.90	0.00	0.68	1.0	0.063
17.367	0.000	1.18	0.00	0.93	2.4	0.090		18.350	0.000	0.89	0.00	0.67	1.0	0.063
17.383	0.000	1.17	0.00	0.92	2.3	0.088		18.367	0.000	0.89	0.00	0.67	0.9	0.063
17.400	0.000	1.16	0.00	0.90	2.2	0.087		18.383	0.000	0.89	0.00	0.67	0.9	0.063
17.417	0.000	1.15	0.00	0.89	2.1	0.086		18.400	0.000	0.88	0.00	0.67	0.9	0.063
17.433	0.000	1.14	0.00	0.88	2.1	0.084		18.417	0.000	0.88	0.00	0.67	0.9	0.063
17.450	0.000	1.14	0.00	0.87	2.0	0.083		18.433	0.000	0.88	0.00	0.67	0.9	0.063
17.467	0.000	1.13	0.00	0.86	2.0	0.082		18.450	0.000	0.87	0.00	0.67	0.9	0.063
17.483	0.000	1.12	0.00	0.85	1.9	0.081		18.467	0.000	0.87	0.00	0.67	0.9	0.063
17.500	0.000	1.11	0.00	0.84	1.8	0.080		18.483	0.000	0.87	0.00	0.67	0.9	0.063
17.517	0.000	1.10	0.00	0.83	1.8	0.079		18.500	0.000	0.87	0.00	0.67	0.9	0.063
17.533	0.000	1.10	0.00	0.82	1.7	0.078		18.517	0.000	0.86	0.00	0.67	0.9	0.062
17.550	0.000	1.09	0.00	0.81	1.7	0.077		18.533	0.000	0.86	0.00	0.67	0.9	0.062
17.567	0.000	1.09	0.00	0.80	1.7	0.076		18.550	0.000	0.86	0.00	0.67	0.9	0.062
17.583	0.000	1.08	0.00	0.80	1.6	0.076		18.567	0.000	0.85	0.00	0.67	0.9	0.062
17.600	0.000	1.07	0.00	0.79	1.6	0.075		18.583	0.000	0.85	0.00	0.66	0.9	0.062
17.617	0.000	1.07	0.00	0.78	1.5	0.074		18.600	0.000	0.85	0.00	0.66	0.9	0.062
17.633	0.000	1.06	0.00	0.78	1.5	0.074		18.617	0.000	0.84	0.00	0.66	0.9	0.062
17.650	0.000	1.05	0.00	0.77	1.5	0.073		18.633	0.000	0.84	0.00	0.66	0.9	0.062
17.667	0.000	1.05	0.00	0.76	1.5	0.073		18.650	0.000	0.84	0.00	0.66	0.9	0.062
17.683	0.000	1.04	0.00	0.76	1.4	0.072		18.667	0.000	0.84	0.00	0.66	0.9	0.062
17.700	0.000	1.03	0.00	0.76	1.4	0.072		18.683	0.000	0.83	0.00	0.66	0.9	0.062
17.717	0.000	1.03	0.00	0.75	1.4	0.071		18.700	0.000	0.83	0.00	0.66	0.9	0.062
17.733	0.000	1.02	0.00	0.75	1.3	0.071		18.717	0.000	0.83	0.00	0.66	0.9	0.062
17.750	0.000	1.02	0.00	0.74	1.3	0.070		18.733	0.000	0.82	0.00	0.66	0.9	0.062
17.767	0.000	1.01	0.00	0.74	1.3	0.070		18.750	0.000	0.82	0.00	0.66	0.9	0.062

22.700	0.000	0.51	0.00	0.60	0.5	0.055
22.716	0.000	0.51	0.00	0.60	0.5	0.055
22.733	0.000	0.51	0.00	0.59	0.5	0.055
22.750	0.000	0.51	0.00	0.59	0.5	0.055
22.766	0.000	0.51	0.00	0.59	0.5	0.055
22.783	0.000	0.51	0.00	0.59	0.5	0.055
22.800	0.000	0.51	0.00	0.59	0.5	0.055
22.816	0.000	0.51	0.00	0.59	0.5	0.055
22.833	0.000	0.51	0.00	0.59	0.5	0.055
22.850	0.000	0.51	0.00	0.59	0.5	0.055
22.866	0.000	0.51	0.00	0.59	0.5	0.055
22.883	0.000	0.51	0.00	0.59	0.5	0.055
22.900	0.000	0.51	0.00	0.59	0.5	0.055
22.916	0.000	0.51	0.00	0.59	0.5	0.055
22.933	0.000	0.50	0.00	0.59	0.5	0.055
22.950	0.000	0.50	0.00	0.59	0.5	0.055
22.966	0.000	0.50	0.00	0.59	0.5	0.055
22.983	0.000	0.50	0.00	0.59	0.5	0.055
23.000	0.000	0.50	0.00	0.59	0.5	0.055
23.016	0.000	0.50	0.00	0.59	0.5	0.055
23.033	0.000	0.50	0.00	0.59	0.5	0.055
23.050	0.000	0.50	0.00	0.59	0.5	0.055
23.066	0.000	0.50	0.00	0.59	0.5	0.055
23.083	0.000	0.50	0.00	0.59	0.5	0.055
23.100	0.000	0.50	0.00	0.59	0.5	0.055
23.116	0.000	0.50	0.00	0.59	0.5	0.055
23.133	0.000	0.50	0.00	0.59	0.5	0.055
23.150	0.000	0.50	0.00	0.59	0.5	0.055
23.166	0.000	0.50	0.00	0.59	0.5	0.055
23.183	0.000	0.50	0.00	0.59	0.5	0.055
23.200	0.000	0.49	0.00	0.59	0.5	0.055
23.216	0.000	0.49	0.00	0.59	0.5	0.055
23.233	0.000	0.49	0.00	0.59	0.5	0.054
23.250	0.000	0.49	0.00	0.59	0.5	0.054
23.266	0.000	0.49	0.00	0.59	0.5	0.054
23.283	0.000	0.49	0.00	0.59	0.5	0.054
23.300	0.000	0.49	0.00	0.59	0.5	0.054
23.316	0.000	0.49	0.00	0.59	0.5	0.054
23.333	0.000	0.49	0.00	0.59	0.5	0.054
23.350	0.000	0.49	0.00	0.59	0.5	0.054
23.366	0.000	0.49	0.00	0.59	0.5	0.054
23.383	0.000	0.49	0.00	0.59	0.5	0.054
23.400	0.000	0.49	0.00	0.59	0.5	0.054
23.416	0.000	0.49	0.00	0.59	0.5	0.054
23.433	0.000	0.49	0.00	0.59	0.5	0.054
23.450	0.000	0.49	0.00	0.59	0.5	0.054
23.466	0.000	0.49	0.00	0.59	0.5	0.054
23.483	0.000	0.49	0.00	0.59	0.5	0.054
23.500	0.000	0.48	0.00	0.59	0.5	0.054
23.516	0.000	0.48	0.00	0.59	0.5	0.054
23.533	0.000	0.48	0.00	0.59	0.5	0.054
23.550	0.000	0.48	0.00	0.59	0.5	0.054
23.566	0.000	0.48	0.00	0.59	0.5	0.054
23.583	0.000	0.48	0.00	0.59	0.5	0.054
23.600	0.000	0.48	0.00	0.59	0.5	0.054
23.616	0.000	0.48	0.00	0.59	0.5	0.054
23.633	0.000	0.48	0.00	0.59	0.5	0.054
23.650	0.000	0.48	0.00	0.59	0.5	0.054
23.666	0.000	0.48	0.00	0.59	0.5	0.054

23.683	0.000	0.48	0.00	0.59	0.5	0.054
23.700	0.000	0.48	0.00	0.59	0.5	0.054
23.716	0.000	0.48	0.00	0.59	0.5	0.054
23.733	0.000	0.48	0.00	0.59	0.5	0.054
23.750	0.000	0.48	0.00	0.59	0.5	0.054
23.766	0.000	0.48	0.00	0.59	0.5	0.054
23.783	0.000	0.48	0.00	0.59	0.5	0.054
23.800	0.000	0.47	0.00	0.59	0.5	0.054
23.816	0.000	0.47	0.00	0.59	0.5	0.054
23.833	0.000	0.47	0.00	0.59	0.5	0.054
23.850	0.000	0.47	0.00	0.59	0.5	0.054
23.866	0.000	0.47	0.00	0.59	0.5	0.054
23.883	0.000	0.47	0.00	0.59	0.5	0.054
23.900	0.000	0.47	0.00	0.59	0.5	0.054
23.916	0.000	0.47	0.00	0.59	0.5	0.054
23.933	0.000	0.47	0.00	0.59	0.5	0.054
23.950	0.000	0.47	0.00	0.59	0.5	0.054
23.966	0.000	0.47	0.00	0.59	0.5	0.054
23.983	0.000	0.47	0.00	0.59	0.5	0.054
24.000	0.000	0.47	0.00	0.59	0.5	0.054

PROCESS SUMMARY OF STORAGE:

INFLOW VOLUME = 1.927 AF
 BASIN STORAGE = 0.003 AF (WITH 0.000 AF INITIALLY FILLED)
 OUTFLOW VOLUME = 1.925 AF
 LOSS VOLUME = 0.000 AF

 FLOW PROCESS FROM NODE 110.00 TO NODE 110.00 IS CODE = 11
 =====

>>>VIEW STREAM NUMBER 1 HYDROGRAPH<<<

STREAM HYDROGRAPH IN ONE-MINUTE UNIT INTERVALS(CFS)
 (Notes: Time indicated is at END of Each Unit Intervals.
 Peak 5-minute rainfall intensity is modeled as
 a constant value for entire 5-minute period.)

TIME(HRS)	VOLUME(AF)	Q(CFS)	0.	2.5	5.0	7.5	10.0
0.017	0.0000	0.00 Q
0.033	0.0000	0.00 Q
0.050	0.0000	0.00 Q
0.067	0.0000	0.00 Q
0.083	0.0000	0.00 Q
0.100	0.0000	0.00 Q
0.117	0.0000	0.00 Q
0.133	0.0000	0.00 Q
0.150	0.0000	0.00 Q
0.167	0.0000	0.00 Q
0.183	0.0000	0.00 Q
0.200	0.0000	0.00 Q
0.217	0.0000	0.00 Q
0.233	0.0000	0.00 Q
0.250	0.0000	0.00 Q
0.267	0.0000	0.00 Q
0.283	0.0000	0.00 Q
0.300	0.0000	0.00 Q

0.317	0.0000	0.00	Q	1.300	0.0008	0.09	Q
0.333	0.0000	0.00	Q	1.317	0.0009	0.12	Q
0.350	0.0000	0.00	Q	1.333	0.0011	0.14	Q
0.367	0.0000	0.00	Q	1.350	0.0014	0.16	Q
0.383	0.0000	0.00	Q	1.367	0.0016	0.19	Q
0.400	0.0000	0.00	Q	1.383	0.0019	0.21	Q
0.417	0.0000	0.00	Q	1.400	0.0022	0.23	Q
0.433	0.0000	0.00	Q	1.417	0.0026	0.24	Q
0.450	0.0001	0.00	Q	1.433	0.0029	0.26	VQ
0.467	0.0001	0.00	Q	1.450	0.0033	0.28	VQ
0.483	0.0001	0.00	Q	1.467	0.0037	0.29	VQ
0.500	0.0001	0.00	Q	1.483	0.0041	0.30	VQ
0.517	0.0001	0.00	Q	1.500	0.0045	0.32	VQ
0.533	0.0001	0.00	Q	1.517	0.0050	0.33	VQ
0.550	0.0001	0.00	Q	1.533	0.0055	0.34	VQ
0.567	0.0001	0.00	Q	1.550	0.0059	0.35	VQ
0.583	0.0001	0.00	Q	1.567	0.0064	0.36	VQ
0.600	0.0001	0.00	Q	1.583	0.0069	0.37	VQ
0.617	0.0001	0.00	Q	1.600	0.0075	0.37	VQ
0.633	0.0001	0.01	Q	1.617	0.0080	0.38	VQ
0.650	0.0001	0.01	Q	1.633	0.0085	0.39	VQ
0.667	0.0001	0.01	Q	1.650	0.0091	0.40	VQ
0.683	0.0001	0.01	Q	1.667	0.0096	0.40	VQ
0.700	0.0001	0.01	Q	1.683	0.0102	0.41	VQ
0.717	0.0002	0.01	Q	1.700	0.0107	0.41	VQ
0.733	0.0002	0.01	Q	1.717	0.0113	0.42	VQ
0.750	0.0002	0.01	Q	1.733	0.0119	0.42	VQ
0.767	0.0002	0.01	Q	1.750	0.0125	0.43	VQ
0.783	0.0002	0.01	Q	1.767	0.0131	0.43	VQ
0.800	0.0002	0.01	Q	1.783	0.0137	0.44	VQ
0.817	0.0002	0.01	Q	1.800	0.0143	0.44	VQ
0.833	0.0002	0.01	Q	1.817	0.0149	0.44	VQ
0.850	0.0002	0.01	Q	1.833	0.0155	0.45	VQ
0.867	0.0002	0.01	Q	1.850	0.0161	0.45	VQ
0.883	0.0003	0.01	Q	1.867	0.0168	0.45	VQ
0.900	0.0003	0.01	Q	1.883	0.0174	0.46	VQ
0.917	0.0003	0.01	Q	1.900	0.0180	0.46	VQ
0.933	0.0003	0.01	Q	1.917	0.0187	0.46	VQ
0.950	0.0003	0.01	Q	1.933	0.0193	0.46	VQ
0.967	0.0003	0.01	Q	1.950	0.0199	0.46	VQ
0.983	0.0003	0.01	Q	1.967	0.0206	0.47	VQ
1.000	0.0003	0.01	Q	1.983	0.0212	0.47	VQ
1.017	0.0003	0.01	Q	2.000	0.0219	0.47	VQ
1.033	0.0004	0.01	Q	2.017	0.0225	0.47	VQ
1.050	0.0004	0.01	Q	2.033	0.0232	0.47	VQ
1.067	0.0004	0.01	Q	2.050	0.0238	0.47	VQ
1.083	0.0004	0.01	Q	2.067	0.0245	0.48	VQ
1.100	0.0004	0.01	Q	2.083	0.0251	0.48	VQ
1.117	0.0004	0.01	Q	2.100	0.0258	0.48	VQ
1.133	0.0004	0.01	Q	2.117	0.0265	0.48	VQ
1.150	0.0004	0.01	Q	2.133	0.0271	0.48	VQ
1.167	0.0005	0.01	Q	2.150	0.0278	0.48	VQ
1.183	0.0005	0.01	Q	2.167	0.0285	0.48	VQ
1.200	0.0005	0.01	Q	2.183	0.0291	0.48	VQ
1.217	0.0005	0.01	Q	2.200	0.0298	0.48	VQ
1.233	0.0005	0.01	Q	2.217	0.0305	0.49	VQ
1.250	0.0005	0.01	Q	2.233	0.0311	0.49	VQ
1.267	0.0006	0.03	Q	2.250	0.0318	0.49	VQ
1.283	0.0007	0.06	Q	2.267	0.0325	0.49	VQ

2.283	0.0331	0.49	VQ	3.267	0.0739	0.51	.VQ
2.300	0.0338	0.49	VQ	3.283	0.0747	0.51	.VQ
2.317	0.0345	0.49	VQ	3.300	0.0754	0.51	.VQ
2.333	0.0352	0.49	VQ	3.317	0.0761	0.51	.VQ
2.350	0.0358	0.49	VQ	3.333	0.0768	0.51	.VQ
2.367	0.0365	0.49	VQ	3.350	0.0775	0.51	.VQ
2.383	0.0372	0.49	VQ	3.367	0.0782	0.51	.VQ
2.400	0.0379	0.49	VQ	3.383	0.0789	0.51	.VQ
2.417	0.0386	0.49	VQ	3.400	0.0796	0.52	.VQ
2.433	0.0392	0.49	VQ	3.417	0.0803	0.52	.VQ
2.450	0.0399	0.49	VQ	3.433	0.0810	0.52	.VQ
2.467	0.0406	0.49	VQ	3.450	0.0817	0.52	.VQ
2.483	0.0413	0.50	VQ	3.467	0.0825	0.52	.VQ
2.500	0.0420	0.50	VQ	3.483	0.0832	0.52	.VQ
2.517	0.0426	0.50	VQ	3.500	0.0839	0.52	.VQ
2.533	0.0433	0.50	VQ	3.517	0.0846	0.52	.VQ
2.550	0.0440	0.50	VQ	3.533	0.0853	0.52	.VQ
2.567	0.0447	0.50	VQ	3.550	0.0860	0.52	.VQ
2.583	0.0454	0.50	VQ	3.567	0.0867	0.52	.VQ
2.600	0.0461	0.50	VQ	3.583	0.0874	0.52	.VQ
2.617	0.0468	0.50	VQ	3.600	0.0882	0.52	.VQ
2.633	0.0474	0.50	VQ	3.617	0.0889	0.52	.VQ
2.650	0.0481	0.50	.Q	3.633	0.0896	0.52	.VQ
2.667	0.0488	0.50	.Q	3.650	0.0903	0.52	.VQ
2.683	0.0495	0.50	.VQ	3.667	0.0910	0.52	.VQ
2.700	0.0502	0.50	.VQ	3.683	0.0917	0.52	.VQ
2.717	0.0509	0.50	.VQ	3.700	0.0925	0.52	.VQ
2.733	0.0516	0.50	.VQ	3.717	0.0932	0.52	.VQ
2.750	0.0523	0.50	.VQ	3.733	0.0939	0.52	.VQ
2.767	0.0530	0.50	.VQ	3.750	0.0946	0.52	.VQ
2.783	0.0537	0.50	.VQ	3.767	0.0953	0.52	.VQ
2.800	0.0544	0.50	.VQ	3.783	0.0961	0.52	.VQ
2.817	0.0550	0.50	.VQ	3.800	0.0968	0.52	. . Q
2.833	0.0557	0.50	.VQ	3.817	0.0975	0.52	. . Q
2.850	0.0564	0.50	.VQ	3.833	0.0982	0.52	. . Q
2.867	0.0571	0.50	.VQ	3.850	0.0989	0.52	. . Q
2.883	0.0578	0.50	.VQ	3.867	0.0997	0.52	. . Q
2.900	0.0585	0.51	.VQ	3.883	0.1004	0.53	. . Q
2.917	0.0592	0.51	.VQ	3.900	0.1011	0.53	. . Q
2.933	0.0599	0.51	.VQ	3.917	0.1018	0.53	. . Q
2.950	0.0606	0.51	.VQ	3.933	0.1026	0.53	. . Q
2.967	0.0613	0.51	.VQ	3.950	0.1033	0.53	. . Q
2.983	0.0620	0.51	.VQ	3.967	0.1040	0.53	. . Q
3.000	0.0627	0.51	.VQ	3.983	0.1047	0.53	. . Q
3.017	0.0634	0.51	.VQ	4.000	0.1055	0.53	. . Q
3.033	0.0641	0.51	.VQ	4.017	0.1062	0.53	. . Q
3.050	0.0648	0.51	.VQ	4.033	0.1069	0.53	. . Q
3.067	0.0655	0.51	.VQ	4.050	0.1077	0.53	. . Q
3.083	0.0662	0.51	.VQ	4.067	0.1084	0.53	. . Q
3.100	0.0669	0.51	.VQ	4.083	0.1091	0.53	. . Q
3.117	0.0676	0.51	.VQ	4.100	0.1098	0.53	. . Q
3.133	0.0683	0.51	.VQ	4.117	0.1106	0.53	. . Q
3.150	0.0690	0.51	.VQ	4.133	0.1113	0.53	. . Q
3.167	0.0697	0.51	.VQ	4.150	0.1120	0.53	. . Q
3.183	0.0704	0.51	.VQ	4.167	0.1128	0.53	. . Q
3.200	0.0711	0.51	.VQ	4.183	0.1135	0.53	. . Q
3.217	0.0718	0.51	.VQ	4.200	0.1142	0.53	. . Q
3.233	0.0725	0.51	.VQ	4.217	0.1150	0.53	. . Q
3.250	0.0732	0.51	.VQ	4.233	0.1157	0.53	. . Q

4.250	0.1164	0.53	. Q	5.233	0.1607	0.56	. QV
4.267	0.1172	0.53	. Q	5.250	0.1615	0.56	. QV
4.283	0.1179	0.53	. Q	5.267	0.1623	0.56	. QV
4.300	0.1186	0.53	. Q	5.283	0.1630	0.56	. QV
4.317	0.1194	0.53	. Q	5.300	0.1638	0.56	. QV
4.333	0.1201	0.54	. Q	5.317	0.1646	0.56	. QV
4.350	0.1209	0.54	. Q	5.333	0.1653	0.56	. QV
4.367	0.1216	0.54	. Q	5.350	0.1661	0.56	. QV
4.383	0.1223	0.54	. Q	5.367	0.1669	0.56	. QV
4.400	0.1231	0.54	. Q	5.383	0.1676	0.56	. QV
4.417	0.1238	0.54	. Q	5.400	0.1684	0.56	. QV
4.433	0.1246	0.54	. Q	5.417	0.1692	0.56	. QV
4.450	0.1253	0.54	. Q	5.433	0.1700	0.56	. QV
4.467	0.1260	0.54	. Q	5.450	0.1707	0.56	. QV
4.483	0.1268	0.54	. Q	5.467	0.1715	0.56	. QV
4.500	0.1275	0.54	. Q	5.483	0.1723	0.56	. QV
4.517	0.1283	0.54	. Q	5.500	0.1731	0.56	. QV
4.533	0.1290	0.54	. Q	5.517	0.1738	0.56	. QV
4.550	0.1297	0.54	. Q	5.533	0.1746	0.56	. QV
4.567	0.1305	0.54	. Q	5.550	0.1754	0.56	. QV
4.583	0.1312	0.54	. Q	5.567	0.1762	0.57	. QV
4.600	0.1320	0.54	. Q	5.583	0.1770	0.57	. QV
4.617	0.1327	0.54	. Q	5.600	0.1777	0.57	. QV
4.633	0.1335	0.54	. Q	5.617	0.1785	0.57	. QV
4.650	0.1342	0.54	. Q	5.633	0.1793	0.57	. QV
4.667	0.1350	0.54	. Q	5.650	0.1801	0.57	. QV
4.683	0.1357	0.54	. Q	5.667	0.1809	0.57	. QV
4.700	0.1365	0.54	. Q	5.683	0.1816	0.57	. QV
4.717	0.1372	0.54	. Q	5.700	0.1824	0.57	. QV
4.733	0.1380	0.54	. Q	5.717	0.1832	0.57	. QV
4.750	0.1387	0.54	. Q	5.733	0.1840	0.57	. QV
4.767	0.1395	0.55	. Q	5.750	0.1848	0.57	. QV
4.783	0.1402	0.55	. Q	5.767	0.1856	0.57	. QV
4.800	0.1410	0.55	. Q	5.783	0.1864	0.57	. QV
4.817	0.1417	0.55	. Q	5.800	0.1871	0.57	. QV
4.833	0.1425	0.55	. Q	5.817	0.1879	0.57	. QV
4.850	0.1432	0.55	. Q	5.833	0.1887	0.57	. QV
4.867	0.1440	0.55	. Q	5.850	0.1895	0.57	. QV
4.883	0.1447	0.55	. QV	5.867	0.1903	0.57	. QV
4.900	0.1455	0.55	. QV	5.883	0.1911	0.57	. QV
4.917	0.1463	0.55	. QV	5.900	0.1919	0.57	. QV
4.933	0.1470	0.55	. QV	5.917	0.1927	0.57	. Q V
4.950	0.1478	0.55	. QV	5.933	0.1935	0.58	. Q V
4.967	0.1485	0.55	. QV	5.950	0.1943	0.58	. Q V
4.983	0.1493	0.55	. QV	5.967	0.1950	0.58	. Q V
5.000	0.1500	0.55	. QV	5.983	0.1958	0.58	. Q V
5.017	0.1508	0.55	. QV	6.000	0.1966	0.58	. Q V
5.033	0.1516	0.55	. QV	6.017	0.1974	0.58	. Q V
5.050	0.1523	0.55	. QV	6.033	0.1982	0.58	. Q V
5.067	0.1531	0.55	. QV	6.050	0.1990	0.58	. Q V
5.083	0.1538	0.55	. QV	6.067	0.1998	0.58	. Q V
5.100	0.1546	0.55	. QV	6.083	0.2006	0.58	. Q V
5.117	0.1554	0.55	. QV	6.100	0.2014	0.58	. Q V
5.133	0.1561	0.55	. QV	6.117	0.2022	0.58	. Q V
5.150	0.1569	0.55	. QV	6.133	0.2030	0.58	. Q V
5.167	0.1577	0.55	. QV	6.150	0.2038	0.58	. Q V
5.183	0.1584	0.56	. QV	6.167	0.2046	0.58	. Q V
5.200	0.1592	0.56	. QV	6.183	0.2054	0.58	. Q V
5.217	0.1600	0.56	. QV	6.200	0.2062	0.58	. Q V

12.117	0.5532	0.90	.	Q	.V	13.100	0.6295	1.00	.	Q	.	V	.
12.133	0.5544	0.90	.	Q	.V	13.117	0.6309	1.00	.	Q	.	V	.
12.150	0.5557	0.91	.	Q	.V	13.133	0.6323	1.00	.	Q	.	V	.
12.167	0.5569	0.91	.	Q	.V	13.150	0.6337	1.01	.	Q	.	V	.
12.183	0.5582	0.91	.	Q	.V	13.167	0.6351	1.01	.	Q	.	V	.
12.200	0.5594	0.91	.	Q	.V	13.183	0.6365	1.01	.	Q	.	V	.
12.217	0.5607	0.91	.	Q	.V	13.200	0.6379	1.01	.	Q	.	V	.
12.233	0.5619	0.91	.	Q	.V	13.217	0.6393	1.02	.	Q	.	V	.
12.250	0.5632	0.91	.	Q	.V	13.233	0.6407	1.02	.	Q	.	V	.
12.267	0.5644	0.91	.	Q	.V	13.250	0.6421	1.02	.	Q	.	V	.
12.283	0.5657	0.91	.	Q	.V	13.267	0.6435	1.03	.	Q	.	V	.
12.300	0.5669	0.91	.	Q	.V	13.283	0.6449	1.03	.	Q	.	V	.
12.317	0.5682	0.91	.	Q	.V	13.300	0.6463	1.03	.	Q	.	V	.
12.333	0.5694	0.91	.	Q	.V	13.317	0.6478	1.04	.	Q	.	V	.
12.350	0.5707	0.91	.	Q	.V	13.333	0.6492	1.04	.	Q	.	V	.
12.367	0.5720	0.91	.	Q	.V	13.350	0.6506	1.04	.	Q	.	V	.
12.383	0.5732	0.91	.	Q	.V	13.367	0.6521	1.04	.	Q	.	V	.
12.400	0.5745	0.91	.	Q	.V	13.383	0.6535	1.05	.	Q	.	V	.
12.417	0.5757	0.91	.	Q	.V	13.400	0.6549	1.05	.	Q	.	V	.
12.433	0.5770	0.92	.	Q	.V	13.417	0.6564	1.05	.	Q	.	V	.
12.450	0.5783	0.92	.	Q	.V	13.433	0.6578	1.05	.	Q	.	V	.
12.467	0.5795	0.92	.	Q	.V	13.450	0.6593	1.06	.	Q	.	V	.
12.483	0.5808	0.92	.	Q	.V	13.467	0.6608	1.06	.	Q	.	V	.
12.500	0.5821	0.92	.	Q	.V	13.483	0.6622	1.06	.	Q	.	V	.
12.517	0.5833	0.92	.	Q	.V	13.500	0.6637	1.07	.	Q	.	V	.
12.533	0.5846	0.93	.	Q	.V	13.517	0.6652	1.07	.	Q	.	V	.
12.550	0.5859	0.93	.	Q	.V	13.533	0.6667	1.07	.	Q	.	V	.
12.567	0.5872	0.93	.	Q	.V	13.550	0.6681	1.08	.	Q	.	V	.
12.583	0.5884	0.93	.	Q	.V	13.567	0.6696	1.08	.	Q	.	V	.
12.600	0.5897	0.93	.	Q	.V	13.583	0.6711	1.09	.	Q	.	V	.
12.617	0.5910	0.93	.	Q	.V	13.600	0.6726	1.09	.	Q	.	V	.
12.633	0.5923	0.93	.	Q	.V	13.617	0.6741	1.09	.	Q	.	V	.
12.650	0.5936	0.94	.	Q	.V	13.633	0.6756	1.10	.	Q	.	V	.
12.667	0.5949	0.94	.	Q	.V	13.650	0.6772	1.10	.	Q	.	V	.
12.683	0.5962	0.94	.	Q	.V	13.667	0.6787	1.10	.	Q	.	V	.
12.700	0.5975	0.94	.	Q	.V	13.683	0.6802	1.11	.	Q	.	V	.
12.717	0.5988	0.94	.	Q	.V	13.700	0.6817	1.11	.	Q	.	V	.
12.733	0.6001	0.95	.	Q	.V	13.717	0.6833	1.11	.	Q	.	V	.
12.750	0.6014	0.95	.	Q	.V	13.733	0.6848	1.12	.	Q	.	V	.
12.767	0.6027	0.95	.	Q	.V	13.750	0.6863	1.12	.	Q	.	V	.
12.783	0.6040	0.95	.	Q	.V	13.767	0.6879	1.12	.	Q	.	V	.
12.800	0.6053	0.95	.	Q	.V	13.783	0.6894	1.13	.	Q	.	V	.
12.817	0.6066	0.96	.	Q	.V	13.800	0.6910	1.13	.	Q	.	V	.
12.833	0.6080	0.96	.	Q	.V	13.817	0.6926	1.13	.	Q	.	V	.
12.850	0.6093	0.96	.	Q	.V	13.833	0.6941	1.14	.	Q	.	V	.
12.867	0.6106	0.96	.	Q	.V	13.850	0.6957	1.14	.	Q	.	V	.
12.883	0.6119	0.97	.	Q	.V	13.867	0.6973	1.15	.	Q	.	V	.
12.900	0.6133	0.97	.	Q	.V	13.883	0.6989	1.15	.	Q	.	V	.
12.917	0.6146	0.97	.	Q	.V	13.900	0.7005	1.15	.	Q	.	V	.
12.933	0.6160	0.97	.	Q	.V	13.917	0.7021	1.16	.	Q	.	V	.
12.950	0.6173	0.98	.	Q	.V	13.933	0.7037	1.16	.	Q	.	V	.
12.967	0.6186	0.98	.	Q	.V	13.950	0.7053	1.17	.	Q	.	V	.
12.983	0.6200	0.98	.	Q	.V	13.967	0.7069	1.17	.	Q	.	V	.
13.000	0.6214	0.98	.	Q	.V	13.983	0.7085	1.18	.	Q	.	V	.
13.017	0.6227	0.99	.	Q	.V	14.000	0.7101	1.18	.	Q	.	V	.
13.033	0.6241	0.99	.	Q	.V	14.017	0.7118	1.19	.	Q	.	V	.
13.050	0.6254	0.99	.	Q	.V	14.033	0.7134	1.19	.	Q	.	V	.
13.067	0.6268	0.99	.	Q	.V	14.050	0.7151	1.20	.	Q	.	V	.
13.083	0.6282	0.99	.	Q	.V	14.067	0.7167	1.20	.	Q	.	V	.

14.083	0.7184	1.20	.	Q	.	V	15.067	0.8264	1.54	.	Q	.	V	.
14.100	0.7200	1.21	.	Q	.	V	15.083	0.8285	1.55	.	Q	.	V	.
14.117	0.7217	1.21	.	Q	.	V	15.100	0.8307	1.56	.	Q	.	V	.
14.133	0.7234	1.22	.	Q	.	V	15.117	0.8328	1.58	.	Q	.	V	.
14.150	0.7251	1.22	.	Q	.	V	15.133	0.8350	1.59	.	Q	.	V	.
14.167	0.7267	1.22	.	Q	.	V	15.150	0.8372	1.60	.	Q	.	V	.
14.183	0.7284	1.23	.	Q	.	V	15.167	0.8395	1.61	.	Q	.	V	.
14.200	0.7301	1.23	.	Q	.	V	15.183	0.8417	1.62	.	Q	.	V	.
14.217	0.7318	1.23	.	Q	.	V	15.200	0.8439	1.64	.	Q	.	V	.
14.233	0.7335	1.23	.	Q	.	V	15.217	0.8462	1.65	.	Q	.	V	.
14.250	0.7352	1.24	.	Q	.	V	15.233	0.8485	1.66	.	Q	.	V	.
14.267	0.7369	1.24	.	Q	.	V	15.250	0.8508	1.67	.	Q	.	V	.
14.283	0.7386	1.24	.	Q	.	V	15.267	0.8531	1.68	.	Q	.	V	.
14.300	0.7404	1.24	.	Q	.	V	15.283	0.8555	1.70	.	Q	.	V	.
14.317	0.7421	1.25	.	Q	.	V	15.300	0.8578	1.72	.	Q	.	V	.
14.333	0.7438	1.25	.	Q	.	V	15.317	0.8602	1.74	.	Q	.	V	.
14.350	0.7455	1.25	.	Q	.	V	15.333	0.8627	1.76	.	Q	.	V	.
14.367	0.7472	1.25	.	Q	.	V	15.350	0.8651	1.79	.	Q	.	V	.
14.383	0.7490	1.26	.	Q	.	V	15.367	0.8676	1.81	.	Q	.	V	.
14.400	0.7507	1.26	.	Q	.	V	15.383	0.8702	1.85	.	Q	.	V	.
14.417	0.7524	1.26	.	Q	.	V	15.400	0.8727	1.88	.	Q	.	V	.
14.433	0.7542	1.26	.	Q	.	V	15.417	0.8754	1.91	.	Q	.	V	.
14.450	0.7559	1.27	.	Q	.	V	15.433	0.8781	1.95	.	Q	.	V	.
14.467	0.7577	1.27	.	Q	.	V	15.450	0.8808	1.99	.	Q	.	V	.
14.483	0.7594	1.27	.	Q	.	V	15.467	0.8836	2.03	.	Q	.	V	.
14.500	0.7612	1.28	.	Q	.	V	15.483	0.8864	2.07	.	Q	.	V	.
14.517	0.7630	1.28	.	Q	.	V	15.500	0.8894	2.12	.	Q	.	V	.
14.533	0.7647	1.29	.	Q	.	V	15.517	0.8923	2.17	.	Q	.	V	.
14.550	0.7665	1.29	.	Q	.	V	15.533	0.8954	2.22	.	Q	.	V	.
14.567	0.7683	1.29	.	Q	.	V	15.550	0.8985	2.27	.	Q	.	V	.
14.583	0.7701	1.30	.	Q	.	V	15.567	0.9017	2.33	.	Q	.	V	.
14.600	0.7719	1.30	.	Q	.	V	15.583	0.9050	2.38	.	Q	.	V	.
14.617	0.7737	1.31	.	Q	.	V	15.600	0.9084	2.44	.	Q	.	V	.
14.633	0.7755	1.32	.	Q	.	V	15.617	0.9118	2.50	.	Q	.	V	.
14.650	0.7773	1.32	.	Q	.	V	15.633	0.9154	2.57	.	Q	.	V	.
14.667	0.7792	1.33	.	Q	.	V	15.650	0.9190	2.63	.	Q	.	V	.
14.683	0.7810	1.34	.	Q	.	V	15.667	0.9227	2.69	.	Q	.	V	.
14.700	0.7829	1.35	.	Q	.	V	15.683	0.9264	2.72	.	Q	.	V	.
14.717	0.7847	1.35	.	Q	.	V	15.700	0.9302	2.74	.	Q	.	V	.
14.733	0.7866	1.36	.	Q	.	V	15.717	0.9340	2.77	.	Q	.	V	.
14.750	0.7885	1.37	.	Q	.	V	15.733	0.9379	2.79	.	Q	.	V	.
14.767	0.7904	1.38	.	Q	.	V	15.750	0.9417	2.82	.	Q	.	V	.
14.783	0.7923	1.38	.	Q	.	V	15.767	0.9457	2.84	.	Q	.	V	.
14.800	0.7942	1.39	.	Q	.	V	15.783	0.9496	2.87	.	Q	.	V	.
14.817	0.7961	1.40	.	Q	.	V	15.800	0.9536	2.90	.	Q	.	V	.
14.833	0.7981	1.41	.	Q	.	V	15.817	0.9577	2.93	.	Q	.	V	.
14.850	0.8000	1.41	.	Q	.	V	15.833	0.9617	2.96	.	Q	.	V	.
14.867	0.8020	1.42	.	Q	.	V	15.850	0.9659	3.00	.	Q	.	V	.
14.883	0.8039	1.43	.	Q	.	V	15.867	0.9700	3.03	.	Q	.	V	.
14.900	0.8059	1.43	.	Q	.	V	15.883	0.9743	3.07	.	Q	.	V	.
14.917	0.8079	1.44	.	Q	.	V	15.900	0.9785	3.10	.	Q	.	V	.
14.933	0.8099	1.45	.	Q	.	V	15.917	0.9829	3.14	.	Q	.	V	.
14.950	0.8119	1.46	.	Q	.	V	15.933	0.9872	3.18	.	Q	.	V	.
14.967	0.8139	1.47	.	Q	.	V	15.950	0.9917	3.23	.	Q	.	V	.
14.983	0.8160	1.48	.	Q	.	V	15.967	0.9962	3.27	.	Q	.	V	.
15.000	0.8180	1.49	.	Q	.	V	15.983	1.0008	3.32	.	Q	.	V	.
15.017	0.8201	1.50	.	Q	.	V	16.000	1.0054	3.36	.	Q	.	V	.
15.033	0.8222	1.51	.	Q	.	V	16.017	1.0101	3.41	.	Q	.	V	.
15.050	0.8243	1.53	.	Q	.	V	16.033	1.0149	3.48	.	Q	.	V	.

16.050	1.0198	3.55	.	.	Q	.V	.	.		17.033	1.3847	3.39	.	.	Q	.	V	.
16.067	1.0248	3.64	.	.	Q	.V	.	.		17.050	1.3893	3.34	.	.	Q	.	V	.
16.083	1.0300	3.74	.	.	Q	.V	.	.		17.067	1.3938	3.29	.	.	Q	.	V	.
16.100	1.0353	3.86	.	.	Q	.V	.	.		17.083	1.3983	3.25	.	.	Q	.	V	.
16.117	1.0408	3.98	.	.	Q	.V	.	.		17.100	1.4027	3.20	.	.	Q	.	V	.
16.133	1.0464	4.12	.	.	Q	.V	.	.		17.117	1.4071	3.16	.	.	Q	.	V	.
16.150	1.0523	4.27	.	.	Q	.V	.	.		17.133	1.4114	3.11	.	.	Q	.	V	.
16.167	1.0584	4.44	.	.	Q	.V	.	.		17.150	1.4156	3.07	.	.	Q	.	V	.
16.183	1.0648	4.61	.	.	Q	.V	.	.		17.167	1.4198	3.03	.	.	Q	.	V	.
16.200	1.0713	4.77	.	.	Q	.V	.	.		17.183	1.4239	2.99	.	.	Q	.	V	.
16.217	1.0781	4.88	.	.	Q	.V	.	.		17.200	1.4279	2.95	.	.	Q	.	V	.
16.233	1.0849	4.95	.	.	Q	.V	.	.		17.217	1.4319	2.91	.	.	Q	.	V	.
16.250	1.0918	5.02	.	.	Q	.V	.	.		17.233	1.4359	2.87	.	.	Q	.	V	.
16.267	1.0988	5.07	.	.	Q	.V	.	.		17.250	1.4398	2.83	.	.	Q	.	V	.
16.283	1.1058	5.11	.	.	Q	.V	.	.		17.267	1.4436	2.79	.	.	Q	.	V	.
16.300	1.1129	5.15	.	.	Q	.V	.	.		17.283	1.4474	2.76	.	.	Q	.	V	.
16.317	1.1201	5.17	.	.	Q	.V	.	.		17.300	1.4512	2.72	.	.	Q	.	V	.
16.333	1.1272	5.19	.	.	Q	.V	.	.		17.317	1.4548	2.66	.	.	Q	.	V	.
16.350	1.1344	5.20	.	.	Q	.V	.	.		17.333	1.4584	2.56	.	.	Q	.	V	.
16.367	1.1415	5.20	.	.	Q	.V	.	.		17.350	1.4618	2.47	.	.	Q	.	V	.
16.383	1.1487	5.18	.	.	Q	.V	.	.		17.367	1.4650	2.38	.	.	Q	.	V	.
16.400	1.1558	5.17	.	.	Q	.V	.	.		17.383	1.4682	2.30	.	.	Q	.	V	.
16.417	1.1629	5.15	.	.	Q	.V	.	.		17.400	1.4713	2.22	.	.	Q	.	V	.
16.433	1.1700	5.13	.	.	Q	.V	.	.		17.417	1.4742	2.14	.	.	Q	.	V	.
16.450	1.1770	5.11	.	.	Q	.V	.	.		17.433	1.4771	2.08	.	.	Q	.	V	.
16.467	1.1840	5.09	.	.	Q	.V	.	.		17.450	1.4798	2.01	.	.	Q	.	V	.
16.483	1.1910	5.07	.	.	Q	.V	.	.		17.467	1.4825	1.95	.	.	Q	.	V	.
16.500	1.1979	5.04	.	.	Q	.V	.	.		17.483	1.4851	1.89	.	.	Q	.	V	.
16.517	1.2048	5.01	.	.	Q	.V	.	.		17.500	1.4877	1.84	.	.	Q	.	V	.
16.533	1.2117	4.98	.	.	Q	.V	.	.		17.517	1.4901	1.79	.	.	Q	.	V	.
16.550	1.2185	4.95	.	.	Q	.V	.	.		17.533	1.4925	1.74	.	.	Q	.	V	.
16.567	1.2253	4.92	.	.	Q	.V	.	.		17.550	1.4949	1.70	.	.	Q	.	V	.
16.583	1.2320	4.89	.	.	Q	.V	.	.		17.567	1.4972	1.66	.	.	Q	.	V	.
16.600	1.2387	4.86	.	.	Q	.V	.	.		17.583	1.4994	1.62	.	.	Q	.	V	.
16.617	1.2454	4.82	.	.	Q	.V	.	.		17.600	1.5016	1.58	.	.	Q	.	V	.
16.633	1.2520	4.78	.	.	Q	.V	.	.		17.617	1.5037	1.54	.	.	Q	.	V	.
16.650	1.2584	4.71	.	.	Q	.V	.	.		17.633	1.5058	1.51	.	.	Q	.	V	.
16.667	1.2648	4.65	.	.	Q	.V	.	.		17.650	1.5078	1.48	.	.	Q	.	V	.
16.683	1.2712	4.58	.	.	Q	.V	.	.		17.667	1.5098	1.45	.	.	Q	.	V	.
16.700	1.2774	4.52	.	.	Q	.V	.	.		17.683	1.5118	1.42	.	.	Q	.	V	.
16.717	1.2835	4.45	.	.	Q	.V	.	.		17.700	1.5137	1.40	.	.	Q	.	V	.
16.733	1.2895	4.39	.	.	Q	.V	.	.		17.717	1.5156	1.37	.	.	Q	.	V	.
16.750	1.2955	4.33	.	.	Q	.V	.	.		17.733	1.5174	1.35	.	.	Q	.	V	.
16.767	1.3014	4.26	.	.	Q	.V	.	.		17.750	1.5193	1.32	.	.	Q	.	V	.
16.783	1.3072	4.20	.	.	Q	.V	.	.		17.767	1.5211	1.30	.	.	Q	.	V	.
16.800	1.3129	4.14	.	.	Q	.V	.	.		17.783	1.5228	1.28	.	.	Q	.	V	.
16.817	1.3185	4.08	.	.	Q	.V	.	.		17.800	1.5246	1.26	.	.	Q	.	V	.
16.833	1.3240	4.02	.	.	Q	.V	.	.		17.817	1.5263	1.25	.	.	Q	.	V	.
16.850	1.3295	3.97	.	.	Q	.V	.	.		17.833	1.5280	1.23	.	.	Q	.	V	.
16.867	1.3349	3.91	.	.	Q	.V	.	.		17.850	1.5296	1.21	.	.	Q	.	V	.
16.883	1.3402	3.85	.	.	Q	.V	.	.		17.867	1.5313	1.20	.	.	Q	.	V	.
16.900	1.3454	3.80	.	.	Q	.V	.	.		17.883	1.5329	1.18	.	.	Q	.	V	.
16.917	1.3506	3.75	.	.	Q	.V	.	.		17.900	1.5345	1.17	.	.	Q	.	V	.
16.933	1.3557	3.69	.	.	Q	.V	.	.		17.917	1.5361	1.15	.	.	Q	.	V	.
16.950	1.3607	3.64	.	.	Q	.V	.	.		17.933	1.5377	1.14	.	.	Q	.	V	.
16.967	1.3656	3.59	.	.	Q	.V	.	.		17.950	1.5392	1.13	.	.	Q	.	V	.
16.983	1.3705	3.54	.	.	Q	.V	.	.		17.967	1.5408	1.11	.	.	Q	.	V	.
17.000	1.3753	3.49	.	.	Q	.V	.	.		17.983	1.5423	1.10	.	.	Q	.	V	.
17.017	1.3800	3.44	.	.	Q	.V	.	.		18.000	1.5438	1.09	.	.	Q	.	V	.

18.017	1.5453	1.08	.	Q	.	.	.	V	.		19.000	1.6203	0.82	.	Q	.	.	.	V
18.033	1.5467	1.07	.	Q	.	.	.	V	.		19.017	1.6214	0.82	.	Q	.	.	.	V
18.050	1.5482	1.06	.	Q	.	.	.	V	.		19.033	1.6225	0.82	.	Q	.	.	.	V
18.067	1.5497	1.05	.	Q	.	.	.	V	.		19.050	1.6237	0.81	.	Q	.	.	.	V
18.083	1.5511	1.04	.	Q	.	.	.	V	.		19.067	1.6248	0.81	.	Q	.	.	.	V
18.100	1.5525	1.04	.	Q	.	.	.	V	.		19.083	1.6259	0.81	.	Q	.	.	.	V
18.117	1.5539	1.03	.	Q	.	.	.	V	.		19.100	1.6270	0.81	.	Q	.	.	.	V
18.133	1.5553	1.02	.	Q	.	.	.	V	.		19.117	1.6281	0.80	.	Q	.	.	.	V
18.150	1.5567	1.01	.	Q	.	.	.	V	.		19.133	1.6292	0.80	.	Q	.	.	.	V
18.167	1.5581	1.01	.	Q	.	.	.	V	.		19.150	1.6303	0.80	.	Q	.	.	.	V
18.183	1.5595	1.00	.	Q	.	.	.	V	.		19.167	1.6314	0.80	.	Q	.	.	.	V
18.200	1.5609	1.00	.	Q	.	.	.	V	.		19.183	1.6325	0.79	.	Q	.	.	.	V
18.217	1.5622	0.99	.	Q	.	.	.	V	.		19.200	1.6336	0.79	.	Q	.	.	.	V
18.233	1.5636	0.99	.	Q	.	.	.	V	.		19.217	1.6347	0.79	.	Q	.	.	.	V
18.250	1.5650	0.98	.	Q	.	.	.	V	.		19.233	1.6358	0.79	.	Q	.	.	.	V
18.267	1.5663	0.98	.	Q	.	.	.	V	.		19.250	1.6368	0.78	.	Q	.	.	.	V
18.283	1.5676	0.97	.	Q	.	.	.	V	.		19.267	1.6379	0.78	.	Q	.	.	.	V
18.300	1.5690	0.97	.	Q	.	.	.	V	.		19.283	1.6390	0.78	.	Q	.	.	.	V
18.317	1.5703	0.96	.	Q	.	.	.	V	.		19.300	1.6401	0.78	.	Q	.	.	.	V
18.333	1.5716	0.96	.	Q	.	.	.	V	.		19.317	1.6411	0.78	.	Q	.	.	.	V
18.350	1.5729	0.95	.	Q	.	.	.	V	.		19.333	1.6422	0.77	.	Q	.	.	.	V
18.367	1.5742	0.95	.	Q	.	.	.	V	.		19.350	1.6433	0.77	.	Q	.	.	.	V
18.383	1.5755	0.95	.	Q	.	.	.	V	.		19.367	1.6443	0.77	.	Q	.	.	.	V
18.400	1.5768	0.94	.	Q	.	.	.	V	.		19.383	1.6454	0.77	.	Q	.	.	.	V
18.417	1.5781	0.94	.	Q	.	.	.	V	.		19.400	1.6464	0.76	.	Q	.	.	.	V
18.433	1.5794	0.93	.	Q	.	.	.	V	.		19.417	1.6475	0.76	.	Q	.	.	.	V
18.450	1.5807	0.93	.	Q	.	.	.	V	.		19.433	1.6485	0.76	.	Q	.	.	.	V
18.467	1.5820	0.93	.	Q	.	.	.	V	.		19.450	1.6496	0.76	.	Q	.	.	.	V
18.483	1.5832	0.92	.	Q	.	.	.	V	.		19.467	1.6506	0.76	.	Q	.	.	.	V
18.500	1.5845	0.92	.	Q	.	.	.	V	.		19.483	1.6516	0.75	.	Q	.	.	.	V
18.517	1.5858	0.91	.	Q	.	.	.	V	.		19.500	1.6527	0.75	.	Q	.	.	.	V
18.533	1.5870	0.91	.	Q	.	.	.	V	.		19.517	1.6537	0.75	.	Q	.	.	.	V
18.550	1.5883	0.91	.	Q	.	.	.	V	.		19.533	1.6547	0.75	.	Q	.	.	.	V
18.567	1.5895	0.90	.	Q	.	.	.	V	.		19.550	1.6558	0.75	.	Q	.	.	.	V
18.583	1.5908	0.90	.	Q	.	.	.	V	.		19.567	1.6568	0.74	.	Q	.	.	.	V
18.600	1.5920	0.90	.	Q	.	.	.	V	.		19.583	1.6578	0.74	.	Q	.	.	.	V
18.617	1.5932	0.89	.	Q	.	.	.	V	.		19.600	1.6588	0.74	.	Q	.	.	.	V
18.633	1.5944	0.89	.	Q	.	.	.	V	.		19.617	1.6598	0.74	.	Q	.	.	.	V
18.650	1.5957	0.89	.	Q	.	.	.	V	.		19.633	1.6609	0.74	.	Q	.	.	.	V
18.667	1.5969	0.88	.	Q	.	.	.	V	.		19.650	1.6619	0.73	.	Q	.	.	.	V
18.683	1.5981	0.88	.	Q	.	.	.	V	.		19.667	1.6629	0.73	.	Q	.	.	.	V
18.700	1.5993	0.88	.	Q	.	.	.	V	.		19.683	1.6639	0.73	.	Q	.	.	.	V
18.717	1.6005	0.87	.	Q	.	.	.	V	.		19.700	1.6649	0.73	.	Q	.	.	.	V
18.733	1.6017	0.87	.	Q	.	.	.	V	.		19.717	1.6659	0.73	.	Q	.	.	.	V
18.750	1.6029	0.87	.	Q	.	.	.	V	.		19.733	1.6669	0.72	.	Q	.	.	.	V
18.767	1.6041	0.86	.	Q	.	.	.	V	.		19.750	1.6679	0.72	.	Q	.	.	.	V
18.783	1.6053	0.86	.	Q	.	.	.	V	.		19.767	1.6689	0.72	.	Q	.	.	.	V
18.800	1.6064	0.86	.	Q	.	.	.	V	.		19.783	1.6699	0.72	.	Q	.	.	.	V
18.817	1.6076	0.85	.	Q	.	.	.	V	.		19.800	1.6708	0.72	.	Q	.	.	.	V
18.833	1.6088	0.85	.	Q	.	.	.	V	.		19.817	1.6718	0.71	.	Q	.	.	.	V
18.850	1.6100	0.85	.	Q	.	.	.	V	.		19.833	1.6728	0.71	.	Q	.	.	.	V
18.867	1.6111	0.84	.	Q	.	.	.	V	.		19.850	1.6738	0.71	.	Q	.	.	.	V
18.883	1.6123	0.84	.	Q	.	.	.	V	.		19.867	1.6748	0.71	.	Q	.	.	.	V
18.900	1.6134	0.84	.	Q	.	.	.	V	.		19.883	1.6757	0.71	.	Q	.	.	.	V
18.917	1.6146	0.84	.	Q	.	.	.	V	.		19.900	1.6767	0.71	.	Q	.	.	.	V
18.933	1.6157	0.83	.	Q	.	.	.	V	.		19.917	1.6777	0.70	.	Q	.	.	.	V
18.950	1.6169	0.83	.	Q	.	.	.	V	.		19.933	1.6786	0.70	.	Q	.	.	.	V
18.967	1.6180	0.83	.	Q	.	.	.	V	.		19.950	1.6796	0.70	.	Q	.	.	.	V
18.983	1.6192	0.82	.	Q	.	.	.	V	.		19.967	1.6806	0.70	.	Q	.	.	.	V

19.983	1.6815	0.70	. Q	.	.	.	V	.		20.967	1.7347	0.62	. Q	V	.
20.000	1.6825	0.70	. Q	.	.	.	V	.		20.983	1.7355	0.62	. Q	V	.
20.017	1.6835	0.69	. Q	.	.	.	V	.		21.000	1.7364	0.61	. Q	V	.
20.033	1.6844	0.69	. Q	.	.	.	V	.		21.017	1.7372	0.61	. Q	V	.
20.050	1.6854	0.69	. Q	.	.	.	V	.		21.033	1.7381	0.61	. Q	V	.
20.067	1.6863	0.69	. Q	.	.	.	V	.		21.050	1.7389	0.61	. Q	V	.
20.083	1.6873	0.69	. Q	.	.	.	V	.		21.067	1.7397	0.61	. Q	V	.
20.100	1.6882	0.69	. Q	.	.	.	V	.		21.083	1.7406	0.61	. Q	V	.
20.117	1.6891	0.68	. Q	.	.	.	V	.		21.100	1.7414	0.61	. Q	V	.
20.133	1.6901	0.68	. Q	.	.	.	V	.		21.117	1.7423	0.61	. Q	V	.
20.150	1.6910	0.68	. Q	.	.	.	V	.		21.133	1.7431	0.61	. Q	V	.
20.167	1.6920	0.68	. Q	.	.	.	V	.		21.150	1.7439	0.60	. Q	V	.
20.183	1.6929	0.68	. Q	.	.	.	V	.		21.167	1.7448	0.60	. Q	V	.
20.200	1.6938	0.68	. Q	.	.	.	V	.		21.183	1.7456	0.60	. Q	V	.
20.217	1.6948	0.68	. Q	.	.	.	V	.		21.200	1.7464	0.60	. Q	V	.
20.233	1.6957	0.67	. Q	.	.	.	V	.		21.217	1.7472	0.60	. Q	V	.
20.250	1.6966	0.67	. Q	.	.	.	V	.		21.233	1.7481	0.60	. Q	V	.
20.267	1.6975	0.67	. Q	.	.	.	V	.		21.250	1.7489	0.60	. Q	V	.
20.283	1.6985	0.67	. Q	.	.	.	V	.		21.267	1.7497	0.60	. Q	V	.
20.300	1.6994	0.67	. Q	.	.	.	V	.		21.283	1.7505	0.60	. Q	V	.
20.317	1.7003	0.67	. Q	.	.	.	V	.		21.300	1.7513	0.59	. Q	V	.
20.333	1.7012	0.67	. Q	.	.	.	V	.		21.317	1.7522	0.59	. Q	V	.
20.350	1.7021	0.66	. Q	.	.	.	V	.		21.333	1.7530	0.59	. Q	V	.
20.367	1.7030	0.66	. Q	.	.	.	V	.		21.350	1.7538	0.59	. Q	V	.
20.383	1.7040	0.66	. Q	.	.	.	V	.		21.367	1.7546	0.59	. Q	V	.
20.400	1.7049	0.66	. Q	.	.	.	V	.		21.383	1.7554	0.59	. Q	V	.
20.417	1.7058	0.66	. Q	.	.	.	V	.		21.400	1.7562	0.59	. Q	V	.
20.433	1.7067	0.66	. Q	.	.	.	V	.		21.417	1.7570	0.59	. Q	V	.
20.450	1.7076	0.66	. Q	.	.	.	V	.		21.433	1.7579	0.59	. Q	V	.
20.467	1.7085	0.65	. Q	.	.	.	V	.		21.450	1.7587	0.59	. Q	V	.
20.483	1.7094	0.65	. Q	.	.	.	V	.		21.467	1.7595	0.58	. Q	V	.
20.500	1.7103	0.65	. Q	.	.	.	V	.		21.483	1.7603	0.58	. Q	V	.
20.517	1.7112	0.65	. Q	.	.	.	V	.		21.500	1.7611	0.58	. Q	V	.
20.533	1.7121	0.65	. Q	.	.	.	V	.		21.517	1.7619	0.58	. Q	V	.
20.550	1.7130	0.65	. Q	.	.	.	V	.		21.533	1.7627	0.58	. Q	V	.
20.567	1.7138	0.65	. Q	.	.	.	V	.		21.550	1.7635	0.58	. Q	V	.
20.583	1.7147	0.64	. Q	.	.	.	V	.		21.567	1.7643	0.58	. Q	V	.
20.600	1.7156	0.64	. Q	.	.	.	V	.		21.583	1.7651	0.58	. Q	V	.
20.617	1.7165	0.64	. Q	.	.	.	V	.		21.600	1.7659	0.58	. Q	V	.
20.633	1.7174	0.64	. Q	.	.	.	V	.		21.617	1.7667	0.58	. Q	V	.
20.650	1.7183	0.64	. Q	.	.	.	V	.		21.633	1.7674	0.58	. Q	V	.
20.667	1.7191	0.64	. Q	.	.	.	V	.		21.650	1.7682	0.57	. Q	V	.
20.683	1.7200	0.64	. Q	.	.	.	V	.		21.667	1.7690	0.57	. Q	V	.
20.700	1.7209	0.64	. Q	.	.	.	V	.		21.683	1.7698	0.57	. Q	V	.
20.717	1.7218	0.63	. Q	.	.	.	V	.		21.700	1.7706	0.57	. Q	V	.
20.733	1.7226	0.63	. Q	.	.	.	V	.		21.717	1.7714	0.57	. Q	V	.
20.750	1.7235	0.63	. Q	.	.	.	V	.		21.733	1.7722	0.57	. Q	V	.
20.767	1.7244	0.63	. Q	.	.	.	V	.		21.750	1.7730	0.57	. Q	V	.
20.783	1.7252	0.63	. Q	.	.	.	V	.		21.767	1.7737	0.57	. Q	V	.
20.800	1.7261	0.63	. Q	.	.	.	V	.		21.783	1.7745	0.57	. Q	V	.
20.817	1.7270	0.63	. Q	.	.	.	V	.		21.800	1.7753	0.57	. Q	V	.
20.833	1.7278	0.63	. Q	.	.	.	V	.		21.817	1.7761	0.57	. Q	V	.
20.850	1.7287	0.62	. Q	.	.	.	V	.		21.833	1.7769	0.56	. Q	V	.
20.867	1.7296	0.62	. Q	.	.	.	V	.		21.850	1.7776	0.56	. Q	V	.
20.883	1.7304	0.62	. Q	.	.	.	V	.		21.867	1.7784	0.56	. Q	V	.
20.900	1.7313	0.62	. Q	.	.	.	V	.		21.883	1.7792	0.56	. Q	V	.
20.917	1.7321	0.62	. Q	.	.	.	V	.		21.900	1.7800	0.56	. Q	V	.
20.933	1.7330	0.62	. Q	.	.	.	V	.		21.917	1.7807	0.56	. Q	V	.
20.950	1.7338	0.62	. Q	.	.	.	V	.		21.933	1.7815	0.56	. Q	V	.

21.950	1.7823	0.56	. Q	.	.	.	V	.		22.933	1.8257	0.51	. Q	V .
21.967	1.7830	0.56	. Q	.	.	.	V	.		22.950	1.8264	0.51	. Q	V .
21.983	1.7838	0.56	. Q	.	.	.	V	.		22.967	1.8272	0.51	. Q	V .
22.000	1.7846	0.56	. Q	.	.	.	V	.		22.983	1.8279	0.51	. Q	V .
22.017	1.7853	0.56	. Q	.	.	.	V	.		23.000	1.8286	0.51	. Q	V .
22.033	1.7861	0.55	. Q	.	.	.	V	.		23.017	1.8293	0.51	. Q	V .
22.050	1.7869	0.55	. Q	.	.	.	V	.		23.033	1.8300	0.51	. Q	V .
22.067	1.7876	0.55	. Q	.	.	.	V	.		23.050	1.8307	0.51	. Q	V .
22.083	1.7884	0.55	. Q	.	.	.	V	.		23.067	1.8314	0.51	. Q	V .
22.100	1.7891	0.55	. Q	.	.	.	V	.		23.083	1.8321	0.51	. Q	V .
22.117	1.7899	0.55	. Q	.	.	.	V	.		23.100	1.8328	0.51	. Q	V .
22.133	1.7907	0.55	. Q	.	.	.	V	.		23.117	1.8335	0.51	. Q	V .
22.150	1.7914	0.55	. Q	.	.	.	V	.		23.133	1.8342	0.51	. Q	V .
22.167	1.7922	0.55	. Q	.	.	.	V	.		23.150	1.8349	0.51	. Q	V .
22.183	1.7929	0.55	. Q	.	.	.	V	.		23.167	1.8356	0.50	. Q	V .
22.200	1.7937	0.55	. Q	.	.	.	V	.		23.183	1.8363	0.50	. Q	V .
22.217	1.7944	0.55	. Q	.	.	.	V	.		23.200	1.8369	0.50	. Q	V .
22.233	1.7952	0.54	. Q	.	.	.	V	.		23.217	1.8376	0.50	. Q	V .
22.250	1.7959	0.54	. Q	.	.	.	V	.		23.233	1.8383	0.50	. Q	V .
22.267	1.7967	0.54	. Q	.	.	.	V	.		23.250	1.8390	0.50	. Q	V .
22.283	1.7974	0.54	. Q	.	.	.	V	.		23.267	1.8397	0.50	. Q	V .
22.300	1.7982	0.54	. Q	.	.	.	V	.		23.283	1.8404	0.50	. Q	V .
22.317	1.7989	0.54	. Q	.	.	.	V	.		23.300	1.8411	0.50	. Q	V .
22.333	1.7996	0.54	. Q	.	.	.	V	.		23.317	1.8418	0.50	. Q	V .
22.350	1.8004	0.54	. Q	.	.	.	V	.		23.333	1.8425	0.50	. Q	V .
22.367	1.8011	0.54	. Q	.	.	.	V	.		23.350	1.8432	0.50	. Q	V .
22.383	1.8019	0.54	. Q	.	.	.	V	.		23.367	1.8438	0.50	. Q	V .
22.400	1.8026	0.54	. Q	.	.	.	V	.		23.383	1.8445	0.50	. Q	V .
22.417	1.8033	0.54	. Q	.	.	.	V	.		23.400	1.8452	0.50	. Q	V .
22.433	1.8041	0.54	. Q	.	.	.	V	.		23.417	1.8459	0.50	. Q	V .
22.450	1.8048	0.53	. Q	.	.	.	V	.		23.433	1.8466	0.50	. Q	V .
22.467	1.8056	0.53	. Q	.	.	.	V	.		23.450	1.8473	0.49	. Q	V .
22.483	1.8063	0.53	. Q	.	.	.	V	.		23.467	1.8479	0.49	. Q	V .
22.500	1.8070	0.53	. Q	.	.	.	V	.		23.483	1.8486	0.49	. Q	V .
22.517	1.8078	0.53	. Q	.	.	.	V	.		23.500	1.8493	0.49	. Q	V .
22.533	1.8085	0.53	. Q	.	.	.	V	.		23.517	1.8500	0.49	. Q	V .
22.550	1.8092	0.53	. Q	.	.	.	V	.		23.533	1.8506	0.49	. Q	V .
22.567	1.8099	0.53	. Q	.	.	.	V	.		23.550	1.8513	0.49	. Q	V .
22.583	1.8107	0.53	. Q	.	.	.	V	.		23.567	1.8520	0.49	. Q	V .
22.600	1.8114	0.53	. Q	.	.	.	V	.		23.583	1.8527	0.49	. Q	V .
22.617	1.8121	0.53	. Q	.	.	.	V	.		23.600	1.8533	0.49	. Q	V .
22.633	1.8129	0.53	. Q	.	.	.	V	.		23.617	1.8540	0.49	. Q	V .
22.650	1.8136	0.53	. Q	.	.	.	V	.		23.633	1.8547	0.49	. Q	V .
22.667	1.8143	0.53	. Q	.	.	.	V	.		23.650	1.8554	0.49	. Q	V .
22.683	1.8150	0.52	. Q	.	.	.	V	.		23.667	1.8560	0.49	. Q	V .
22.700	1.8157	0.52	. Q	.	.	.	V	.		23.683	1.8567	0.49	. Q	V .
22.717	1.8165	0.52	. Q	.	.	.	V	.		23.700	1.8574	0.49	. Q	V .
22.733	1.8172	0.52	. Q	.	.	.	V	.		23.717	1.8580	0.49	. Q	V .
22.750	1.8179	0.52	. Q	.	.	.	V	.		23.733	1.8587	0.48	. Q	V .
22.767	1.8186	0.52	. Q	.	.	.	V	.		23.750	1.8594	0.48	. Q	V .
22.783	1.8193	0.52	. Q	.	.	.	V	.		23.767	1.8600	0.48	. Q	V .
22.800	1.8200	0.52	. Q	.	.	.	V	.		23.783	1.8607	0.48	. Q	V .
22.817	1.8208	0.52	. Q	.	.	.	V	.		23.800	1.8614	0.48	. Q	V .
22.833	1.8215	0.52	. Q	.	.	.	V	.		23.817	1.8620	0.48	. Q	V .
22.850	1.8222	0.52	. Q	.	.	.	V	.		23.833	1.8627	0.48	. Q	V .
22.867	1.8229	0.52	. Q	.	.	.	V	.		23.850	1.8634	0.48	. Q	V .
22.883	1.8236	0.52	. Q	.	.	.	V	.		23.867	1.8640	0.48	. Q	V .
22.900	1.8243	0.52	. Q	.	.	.	V	.		23.883	1.8647	0.48	. Q	V .
22.917	1.8250	0.51	. Q	.	.	.	V	.		23.900	1.8653	0.48	. Q	V .

23.917	1.8660	0.48	.Q	.	.	.	V .
23.933	1.8667	0.48	.Q	.	.	.	V .
23.950	1.8673	0.48	.Q	.	.	.	V .
23.967	1.8680	0.48	.Q	.	.	.	V .
23.983	1.8686	0.48	.Q	.	.	.	V .
24.000	1.8693	0.48	.Q	.	.	.	V .

TIME DURATION(minutes) OF PERCENTILES OF ESTIMATED PEAK FLOW RATE:

(Note: 100% of Peak Flow Rate estimate assumed to have
an instantaneous time duration)

Percentile of Estimated Peak Flow Rate	Duration (minutes)
=====	=====
0%	1441.0
10%	1441.0
20%	1425.0
30%	755.0
40%	580.0
50%	505.0
60%	365.0
70%	270.0
80%	195.0
90%	140.0
=====	=====

END OF FLOODSCx ROUTING ANALYSIS