County of Orange
Stormwater Requirements Template

INTERNAL PROJECTS ONLY

TRANSMITTAL PAGE

Include this document at the charter of every project.
Submit a new transmittal page at each 35%, 65%, 90%, and 100% Design stages, as applicable.

Project Name:	**Orange County Youth Transition Center**			
Project File No:	INSERT PROJECT FILE NO. HERE			
Project Location:	331 The City Drive S		Check One:	
	Orange	92868	☒ North OC	☐ South OC
Project Description:	The County of Orange plans to demolish and replace ten buildings at the Orange County Juvenile Hall Campus in Orange, California, through the YTC Juvenile Hall Replacement Project. This project, located at 331 The City Drive South on a 17-acre property redevelopment is bounded by Interstate 5 (I-5) and the Santa Ana River to the east, Service Way to the north, Justice Center Way to the south, and Hospital Frontage Road to the west. The site is designated for Public Facilities and Institutions (PF/I) land use according to the City of Orange General Plan Land Use Element. The project will occur in three phases, Phase 1 will replace 95,589 sq. ft. of existing structures with new facilities, including YTC living units, vocational/educational, culinary, transitional housing, and administrative/medical buildings, totaling 117,905 sq. ft. Phase 2 will add long-term housing, a classroom/library, and independent living buildings. Phase 3, still in design, will focus on tenant improvements and potentially a couple more building demolitions. Phase 3 does not involve any new construction and therefore, Phase 3 improvements are not subject to WQMP requirements. Overall, the project aims to modernize the campus facilities, enhance services, and support institutional uses.			
Is project part of a Master Plan or larger development?			☒ No	☐ Yes
Name of Project/Development: Orange County Youth Transition Center				
Project Area (total area associated with the Project or total area of the right-of-way):			43.71	acres
Area to be disturbed by the Project (Project Footprint):			8.30	acres
Project Proposed Impervious Area (subset of Project Footprint)			3.20	acres
Project Proposed Pervious Area (subset of Project Footprint)			5.10	acres
The proposed **decrease** in impervious area (subset of project footprint) in the proposed condition as compared to the pre-project condition: **Note**: The proposed 40% decrease in impervious area applies to redevelopment changes within the project footprint (8.30 acres) and not the total project area (43.71 acres).			40	%

Identify the Project type below (refer to the WQMP Applicability Checklist):	Place "X" in only one box below	
Type 1: Priority Project – WQMP required	☒	
Type 2: Green Street Project – WQMP required	☐	
Type 3: Non-Priority Project – WQP required (North OC) or NPP required (South OC)	☐	
Type 4: Maintenance/Other Project – No WQMP required, no WQP/NPP required	☐	
Additional Permits	Yes	No
Does the Project require coverage under a Construction General Permit?	☒	☐
Does the Project require coverage under the Clean Water Act, i.e., Section 401/404?	☐	☒
Does the Project require a California Department of Fish and Wildlife Permit?	☐	☒
Does the Project require a Dewatering Permit?	☐	☒

Date Prepared: 11/18/2024

THIS PAGE INTENTIONALLY LEFT BLANK

North Orange County
WQMP Applicability Checklist

1. Is the Project located in North Orange County (NOC)?

☒ Yes; proceed to Question 2 ☐ No; please refer to the South Orange County WQMP Applicability Checklist

2. Is the Project proposing streets, roads, highways, freeways, sidewalks, and/or bikeways of 5,000 square feet or more of new paved impervious surface?

☐ Yes; proceed to Question 12 ☒ No; proceed to Question 3

3. Is the Project a below-ground linear drainage or utility construction project, such as storm drains, sewers, and water lines, that will result in the replacement of more than 5,000 square feet of impervious surface within a developed public street, road, or highway?

☐ Yes; proceed to Question 4 ☒ No; proceed to Question 6

4. Will the Project maintain original line and grade, and hydraulic capacity/original purpose of the facility?

☐ Yes; proceed to Question 13 ☐ No; proceed to Question 5

5. Is the Project occurring in response to an emergency to protect public health and safety?

☐ Yes; **Type 3: Non-Priority Project**, WQP required; proceed to Section 1 ☐ No; proceed to Question 14

6. Is the Project a new development project that creates 10,000 square feet or more of impervious surfaces (collectively over the entire project site)?

☐ Yes; **Type 1: Priority Project**, WQMP required; proceed to Section 1 ☒ No; proceed to Question 7

7. Is the Project a redevelopment project that creates and/or replaces 5,000 square feet or more of impervious surface (collectively over the entire project site on an existing site of 10,000 square feet or more of impervious surfaces)?

☒ Yes; proceed to Question 14 ☐ No; proceed to Question 8

8. Is the Project a new or redevelopment project that creates and/or replaces 5,000 square feet or more of impervious surface (collectively over the entire project site), and consist primarily of one or more of the following uses:
   i. Restaurants. This category is defined as a facility that sells prepared foods and drinks for consumption, including stationary lunch counters and refreshment stands selling prepared foods and drinks for immediate consumption (Standard Industrial Classification (SIC) code 5812). Information and an SIC search function are available at https://www.osha.gov/pls/imis/sicsearch.html.
   ii. Hillside development projects. This category includes development on any natural slope that is twenty-five percent or greater.
   iii. Parking lots. This category is defined as a land area or facility for the temporary parking or storage of motor vehicles used personally, for business, or for commerce.
   iv. Automotive repair shops. This category is defined as a facility that is categorized in any one of the following SIC codes: 5013, 5014, 5541, 7532-7534, or 7536-7539. Information and an SIC search function are available at https://www.osha.gov/pls/imis/sicsearch.html.
   v. Retail gasoline outlets. This category includes Retail gasoline outlets that meet the following criteria: (a) 5,000 square feet or more or (b) a projected Average Daily Traffic of 100 or more vehicles per day.

☐ Yes; proceed to Question 14 ☐ No; proceed to Question 9

9. Is the Project a new or redevelopment project that creates and/or replaces 2,500 square feet or more of impervious surface (collectively over the entire project site), and discharges directly to an Environmentally Sensitive Area (ESA)?

   Note: "Discharging directly to" includes flow that is conveyed overland a distance of 200 feet or less from the Project to the ESA, or conveyed in a pipe or open channel any distance as an isolated flow from the Project to the ESA (i.e. not comingled with flows from adjacent lands). For projects adjacent to an ESA, but not discharging to an ESA, the 2,500 sq-ft threshold does not apply as long as the Project does not physically disturb the ESA and the ESA is upstream of the Project.

   ☐ Yes; proceed to Question 14 ☐ No; proceed to Question 10

10. Will the Project require discretionary action (grading permit, building permit, etc.) that will include a precise plan of development, except for those projects exempted by the Permittee Water Quality Ordinance (as applicable)?

    ☐ Yes; **Type 3: Non-Priority Project**, WQP required; proceed to Section 1 ☐ No; proceed to Question 11

11. Will the Project require issuance of a non-residential plumbing permit for pipelines conveying hazardous materials (e.g. gasoline) as defined in the Permittee Water Quality/Stormwater Ordinance?

    ☐ Yes; **Type 3: Non-Priority Project**, WQP required; proceed to Section 1 ☐ No; **Type 4: Maintenance/Other Project**, no WQP or WQMP required; proceed to Section 1

12. Is the Project a Maintenance Project (a routine activity that is conducted to maintain the original line and grade, hydraulic capacity, or original purpose of the facility)?

    ☐ Yes; **Type 4: Maintenance/Other Project**, no WQP or WQMP required; proceed to Section 1 ☐ No; **Type 2: Green Street Project**; modified WQMP required; proceed to Section 1

13. Is the Project a Maintenance Project (a routine activity that is conducted to maintain the original line and grade, hydraulic capacity, or original purpose of the facility)?

    ☐ Yes; **Type 4: Maintenance/Other Project**, no WQP or WQMP required; proceed to Section 1 ☐ No; **Type 3: Non-Priority Project**; WQP required; proceed to Section 1

14. Is the Project a Maintenance Project (a routine activity that is conducted to maintain the original line and grade, hydraulic capacity, or original purpose of the facility)?

    ☐ Yes; **Type 4: Maintenance/Other Project**, no WQP or WQMP required; proceed to Section 1 ☒ No; **Type 1: Priority Project**; WQMP required; proceed to Section 1

South Orange County
WQMP Applicability Checklist

1. Is the Project located in South Orange County (SOC)?

   ☐ Yes; proceed to Question 2 ☐ No; please refer to the North Orange County WQMP Applicability Checklist

2. Is the Project proposing new or retrofitting 5,000 square feet of existing paved sidewalks, bicycle lanes, or trails that meet the following criteria:
   a. Designed and constructed to direct storm water runoff to adjacent vegetated areas, or other non-erodible permeable areas; OR
   b. Designed and constructed to be hydraulically disconnected from paved streets or roads; OR
   c. Designed and constructed with permeable pavements or surfaces

   ☐ Yes; proceed to Question 11 ☐ No; proceed to Question 3

3. Is the Project proposing retrofitting or redevelopment of 5,000 square feet of existing paved alleys, streets, or roads?

   ☐ Yes; proceed to Question 11 ☐ No; proceed to Question 4

4. Is the Project a new development project that creates 10,000 square feet or more of impervious surfaces (collectively over the entire project site)?

   ☐ Yes; proceed to Question 12 ☐ No; proceed to Question 5

5. Is the Project a redevelopment project that creates and/or replaces 5,000 square feet or more of impervious surface (collectively over the entire project site on an existing site of 10,000 square feet or more of impervious surfaces)?

   ☐ Yes; proceed to Question 12 ☐ No; proceed to Question 6

6. Is the Project a new or redevelopment project that creates and/or replaces 5,000 square feet or more of impervious surface (collectively over the entire project site), and consist primarily of one or more of the following uses:
   i. Restaurants. This category is defined as a facility that sells prepared foods and drinks for consumption, including stationary lunch counters and refreshment stands selling prepared foods and drinks for immediate consumption (Standard Industrial Classification (SIC) code 5812). Information and an SIC search function are available at https://www.osha.gov/pls/imis/sicsearch.html.
   ii. Hillside development projects. This category includes development on any natural slope that is twenty-five percent or greater.
   iii. Parking lots. This category is defined as a land area or facility for the temporary parking or storage of motor vehicles used personally, for business, or for commerce.
   iv. Automotive repair shops. This category is defined as a facility that is categorized in any one of the following SIC codes: 5013, 5014, 5541, 7532-7534, or 7536-7539. Information and an SIC search function are available at https://www.osha.gov/pls/imis/sicsearch.html.
   v. Retail gasoline outlets. This category includes Retail gasoline outlets that meet the following criteria: (a) 5,000 square feet or more or (b) a projected Average Daily Traffic of 100 or more vehicles per day.

   ☐ Yes; proceed to Question 12 ☐ No; proceed to Question 7

7. Is the Project a new or redevelopment project that creates and/or replaces 2,500 square feet or more of impervious surface (collectively over the entire project site), and discharges directly to an Environmentally Sensitive Area (ESA)?

   Note: "Discharging directly to" includes flow that is conveyed overland a distance of 200 feet or less from the Project to the ESA, or conveyed in a pipe or open channel any distance as an isolated flow from the Project to the ESA (i.e. not comingled with flows from adjacent lands). For projects adjacent to an ESA, but not discharging to an ESA, the 2,500 sq. ft threshold does not apply as long as the Project does not physically disturb the ESA and the ESA is upstream of the Project.

   ☐ Yes; proceed to Question 12 ☐ No; proceed to Question 8

8. Is the Project proposing permeable pavement surfaces?

   ☐ Yes; proceed to Question 9 ☐ No; proceed to Question 10

9. If the proposed permeable pavement surfaces were tabulated as impervious surface, would the Project qualify as a Priority Project per Questions 4-7 above?

   ☐ Yes; proceed to Question 13 ☐ No; proceed to Question 10

10. Is the Project resulting in the disturbance of one or more acres of total land (impervious or pervious) **and** expected to generate pollutants (as identified in Section 2.3.4.1 and 2.3.4.2 of the 2017 SOC WQMP Technical Guidance Document (TGD)) post-construction?

    ☐ Yes; **Type 1: Priority Project**, WQMP required; proceed to Section 1

    ☐ No; **Type 4: Maintenance/Other Project**, no NPP or WQMP required; proceed to Section 1

11. Will the Project propose ONLY routine maintenance activities, such as trenching and resurfacing associated with utility work; pavement grinding; resurfacing existing roadways, sidewalks, pedestrian ramps, or bike lanes on existing roads; and routine replacement of damaged pavement, such as pothole repair?

    ☐ Yes; **Type 4: Maintenance/Other Project**, no NPP or WQMP required; proceed to Section 1

    ☐ No; **Type 2: Green Street Project**; modified WQMP required; proceed to Section 1

12. Will the Project propose ONLY routine maintenance activities, such as trenching and resurfacing associated with utility work; pavement grinding; resurfacing existing roadways, sidewalks, pedestrian ramps, or bike lanes on existing roads; and routine replacement of damaged pavement, such as pothole repair?

    ☐ Yes; **Type 4: Maintenance/Other Project**, no NPP or WQMP required; proceed to Section 1

    ☐ No; **Type 1: Priority Project**; WQMP required; proceed to Section 1

13. Will the Project propose ONLY routine maintenance activities, such as trenching and resurfacing associated with utility work; pavement grinding; resurfacing existing roadways, sidewalks, pedestrian ramps, or bike lanes on existing roads; and routine replacement of damaged pavement, such as pothole repair?

    ☐ Yes; **Type 4: Maintenance/Other Project**, no NPP or WQMP required; proceed to Section 1

    ☐ No; **Type 3: Non-Priority Project**; NPP required; proceed to Section 1

Acronyms

A_{df}	Cross sectional area at design flow depth
A_I	Infiltrating surface area
A_{IMP}	Impervious area
A_P	Pervious area
A_R	Retention area
A_T	Trench footprint area
A_{TT}	Total tributary area
ac	Acres
ac-ft	Acre-feet
b	Swale bottom width
BMP	Best Management Practice
C	Simple runoff coefficient
CCR	California Code of Regulations
CEQA	California Environmental Quality Act
cf	Cubic-feet
D_{24}	Daily harvest water demand
d_{48}	48-hour drawdown time
d_{85}	85th percentile storm event rainfall depth
$d_{effective}$	Effective ponding depth
d_b	Basin depth
d_f	Flow depth
$d_{filtered}$	Depth of water filtered during the design capture storm
d_g	Gravel layer depth
d_{HSC}	Effective storm retention depth
d_m	Bioretention media depth
d_O	Depth of water at overflow
d_P	Ponding depth
d_{PM}	Maximum ponding depth
d_r	Depth of water routed through media
d_R	Aggregate reservoir depth
D_R	Retention depth
d_{RM}	Maximum aggregate reservoir depth
d_T	Trench fill depth
DCV	Design Capture Volume
DCV_i	Initial Design Capture Volume
DCV_{UR}	Upstream Design Capture Volume Reduction
DD	Drawdown time
DD_g	Drawdown time for gravel layer
DD_P	Drawdown time for ponded water
DMA	Drainage Management Area
DQ	Design Flow Rate
E	Capture Efficiency

E_R	Green/Brown Roof Extensiveness
E_{Red}	Reduction Efficiency
ESA	Environmentally Sensitive Area
ET	Evapotranspiration
f_{ED}	Fraction of effective ponding depth to design capture storm depth
f_{EV}	Effective volume factor
f_{PD}	Fraction of design ponding depth to design capture storm depth
FS	Factor of Safety
ft	feet
GIS	Geographic Information System
HCOC	Hydrologic Condition of Concern
hr	Hour
HSC	Hydrologic Source Control
I	Design storm intensity
I_{85}	85^{th} percentile storm event rainfall intensity
I_{full}	Gradient across filter bed assuming storage is full
IA_{HSC}	Impervious area covered by hydrologic source controls
ID	Identification
in	Inch
K_d	Design infiltration rate
K_L	Landscape coefficient
K_{media}	Media design infiltration rate
K_{obs}	Observed saturated infiltration rate
K_{sat}	Design saturated hydraulic conductivity
K_{screen}	Feasibility screening infiltration rate
L	Length
L_{min}	Minimum length
LID	Low Impact Development
min	Minute
MRD_{min}	Minimum required moisture retention depth
MS4	Municipal Separate Storm Sewer System
n	Manning's roughness coefficient
n_g	Porosity of gravel layer
n_m	Porosity of bioretention media
n_R	Porosity of aggregate reservoir fill
n_T	Porosity of trench fill
NA	Not applicable
NOC	North Orange County
NPDES	National Pollutant Discharge Elimination System
NPP	Non-Priority Project Water Quality Plan
NRCS	Natural Resources Conservation Service
OC	Orange County
O&M	Operations and Maintenance
PE	Professional Engineer
Q	Flow rate

R	Ratio of pervious to impervious area
R_{SD}	Percent volume reduction based on soil depth
S	Longitudinal slope
SACF	Surface area Correction Factor
SARWQCB	Santa Ana Regional Water Quality Control Board
SD	Soil depth
SD_{min}	Minimum soil depth
SDRWQCB	San Diego Regional Water Quality Control Board
sf	Square-feet
SIC	Standard Industrial Classification
SOC	South Orange County
T_{HR}	Minimum hydraulic residence time
T_R	Assumed storm duration
Tc	Time of concentration
$Tc_{2\text{-yr, POST}}$	Time of concentration for the 2-year, 24-hour storm under post-development conditions
$Tc_{2\text{-yr, PRE}}$	Time of concentration for the 2-year, 24-hour storm under pre-development conditions
TGD	Technical Guidance Document
TMDL	Total Maximum Daily Load
USEPA	United States Environmental Protection Agency
v	Velocity
$V_{2\text{-yr, POST}}$	Runoff volume for the 2-year, 24-hour storm under post-development conditions
$V_{2\text{-yr, PRE}}$	Runoff volume for the 2-year, 24-hour storm under pre-development conditions
$V_{cistern}$	Cistern volume
V_{max}	Maximum volume
$V_{storage}$	Dead storage volume
w	Filter strip width
WIHMP	Watershed Infiltration and Hydromodification Management Plan
WQMP	Water Quality Management Plan
WQP	Water Quality Plan
yr	Year

1. Required Documents Checklist

A Draft WQMP is required at each phase of the Project (Initiation, 35% Design, 65% Design, and 90% Design, as applicable) with the Final WQMP submitted at Project Completion. Based on the Project type identified by the WQMP Applicability Checklist, select the relevant **Required Documents Checklist** from pages below. Along with the checklist, drafts shall include only the required sections as indicated in the "Project Phase" column, as well as updated documents from every preceding project phase. All sections will be required for the final WQMP at the 100% Design phase. In addition, some attachments may be required. An updated Attachments Checklist should be included at every applicable stage of the Project.

Note that a submittal is required for Type 4: Maintenance/Other Projects. See the **Required Documents Checklist for Type 4 Projects** below.

This Conceptual WQMP is being developed under the Project "Initiation" phase and is for CEQA clearances and approvals only. Phase 1 is currently under design and details will be provided at a level of detail consistent with the construction documents. Phase 2 has not started any design and is only a colored site plan concept. From a CEQA perspective, Phase 2 will be evaluated at a Program-Level EIR. All information provided in the tables of the Conceptual WQMP will include acreages and pervious/impervious conditions for both phases and the detailed explanation below the table will break up the details into Phase 1 and Phase 2.

1.1 Required Documents Checklist for Type 1 Projects

Type 1: Priority Project Water Quality Management Plan (WQMP)

Sections Required			Page	Project Phase	For Internal Use Only
☒	-	Transmittal Page	i	Initiation	
☒	-	WQMP Applicability Checklist	iii-iv or vi-vii	Initiation	
☒	1	Required Documents Checklist 1.1 Required Documents Checklist for Type 1 Projects 1.5 Attachment Checklist	1-1	Initiation	
☒	2	Project Description	2-1	Initiation	
☒	3	Site and Watershed Characterization 3.1 Site Characterization 3.2 Watershed Characterization 3.3 Preliminary Infiltration Investigation Preliminary Infiltration Investigation	3-1	Initiation	
☒	5	Site Design and Drainage Plan 5.1 Project Performance Criteria – NOC Only 5.2 DMA Delineation and BMP Site Selection 5.3 Additional Investigations for Priority Projects	5-1	35% Design	
☒	6	Site Design BMPs for Priority Projects 6.1 Selection of Site Design BMPs 6.2 Site Design BMP Calculations 6.3 Inventory of BMPs	6-1	35% Design	
☒	8	Hydromodification BMPs	8-1	35% Design	
☒	9	BMP Exhibit	9-1	35% Design	
☒	10	Source Control BMPs	10-1	65% Design	
☒	11	Educational Material	11-1	100% Design	
☒	12	Routine Inspections, Operations, and Maintenance 12.1 Inspection / Maintenance Responsibilities 12.2 Operations and Maintenance Plan	12-1	100% Design	
☒	13	Discretionary Permits and Water Quality Conditions 13.1 Discretionary Permits 13.2 Water Quality Conditions	13-1	100% Design	

1.2 Required Documents Checklist for Type 2 Projects

Type 2: Green Streets Project

Sections Required			Page	Project Phase	For Internal Use Only
☐	-	Transmittal Page	i	Initiation	
☐	-	WQMP Applicability Checklist	ii-iii or iv-v	Initiation	
☐	1	Required Documents Checklist 1.2 Required Documents Checklist for Type 2 Projects 1.5 Attachment Checklist	1-1	Initiation	
☐	2	Project Description	2-1	Initiation	
☐	3	Site and Watershed Characterization 3.1 Site Characterization 3.2 Watershed Characterization	3-1	Initiation	
☐	5	Site Design and Drainage Plan 5.1 Project Performance Criteria – NOC Only 5.2 DMA Delineation	5-1	35% Design	
☐	7	Site Design BMPs for Green Street Projects	7-1	35% Design	
☐	8	Hydromodification BMPs	8-1	35% Design	
☐	9	BMP Exhibit	9-1	35% Design	
☐	12	Routine Inspections, Operations, and Maintenance 12.1 Inspection / Maintenance Responsibilities 12.2 Operations and Maintenance Plan	12-1	100% Design	
☐	13	Discretionary Permits and Water Quality Conditions 13.1 Discretionary Permits 13.2 Water Quality Conditions	13-1	100% Design	

1.3 Required Documents Checklist for Type 3 Projects

Type 3: Non-Priority Project Water Quality Plan (WQP/NPP)

Sections Required			Page	Project Phase	For Internal Use Only
☐	-	Transmittal Page	i	Initiation	
☐	-	WQMP Applicability Checklist	ii-iii or iv-v	Initiation	
☐	1	Required Documents Checklist 1.3 Required Documents Checklist for Type 3 Projects 1.5 Attachment Checklist	1-1	Initiation	
☐	2	Project Description	2-1	Initiation	
☐	3	Site and Watershed Characterization 3.1 Site Characterization 3.2 Watershed Characterization	3-1	Initiation	
☐	4	Site Design BMPs for Non-Priority Projects 4.1 Site Design BMPs 4.2 Other BMPs	4-1	35% Design	
☐	9	BMP Exhibit	9-1	35% Design	
☐	10	Source Control BMPs	10-1	65% Design	
☐	12	Routine Inspections, Operations, and Maintenance 12.1 Inspection / Maintenance Responsibilities	12-1	100% Design	

1.4 Required Documents Checklist for Type 4 Projects

Type 4: Maintenance/Other Projects

Sections Required			Page	Project Phase	For Internal Use Only
☐	-	Transmittal Page	i	Initiation	
☐	-	WQMP Applicability Checklist	ii-iii or iv-v	Initiation	
		Required Documents Checklist	1-1		
☐	1	1.4 Required Documents Checklist for Type 4 Projects		Initiation	

1.5 Attachment Checklist

Identify the attachments included in this submittal. Refer to the appropriate sections to determine if attachments are necessary.

Attachment		Section	Included
Attachment 1	Preliminary Infiltration Investigation Report	3.3	☒
Attachment 2	WIHMP Criteria and Opportunities (NOC Only)	5.1	☒
Attachment 3	Additional DMA Delineation Tables	5.2	☒
Attachment 4	DCV Calculations	5.2	☒
Attachment 5	Supplementary Infiltration Investigation Report	5.3.1	☒
Attachment 6	Additional Infiltration and Harvest and Use Feasibility Tables	5.3.3	☒
Attachment 7	Priority Project BMP Conformance Analysis Tables	6.2	☒
Attachment 8	DCV Reduction Calculations	6.2	☒
Attachment 9	Green Street Project BMP Conformance Analysis Tables	7	☐
Attachment 10	Hydromodification Exhibits and Calculations	8	☒
Attachment 11	Hydromodification Management Plan	8	☐
Attachment 12	BMP Exhibit	9	☒
Attachment 13	Additional Educational Material	11	☐
Attachment 14	Additional BMP Inspection and Maintenance Responsibility Tables	12.1	☐
Attachment 15	Operations and Maintenance Plan	12.2	☐
Attachment 16	BMP Inspection Record	14	NA[1]
Attachment 17	Conceptual Hydrology Reports (Phase 1 and Phase 2 Separate)	15	

[1] A BMP Inspection Record is not to be completed by the Plan Developer or submitted with the WQMP/WQP/NPP. A BMP Inspection Record form is provided to allow the Plan Developer to review items that will be inspected and ensure BMPs are designed in a manner that aligns with the requirements identified in the form.

2. Project Description

Section 2 is required for ***Type 1: Priority Projects***, ***Type 2: Green Street Projects,*** and ***Type 3: Non-Priority Projects***.

Describe the Project in a manner that matches the legal description of the Project used as part of project approval. The description shall also identify Project features and attributes relevant for water quality and hydromodification management planning. The purpose of this information is to:

1. Legally define what is meant by the "Project" for the purpose of discretionary and subsequent approval; and
2. Provide a general introduction to proposed development patterns, land uses, site activities as they relate to determining applicable stormwater management provisions.

This section shall not provide a detailed description of the existing or proposed site. That information will be catalogued in more detail as part of Section 3: Site and Watershed Characterization. The Project Description Section of the WQMP/WQP/NPP shall include:

- Project location, parcel numbers, and legal address, as applicable;
- Legal boundaries of the proposed Project;
- Project acreage;
- Proposed land uses and site activities, including associated quantification (e.g., acreages, units);
- Off-site improvements as part of the overall Project action; and
- General description of site grading and drainage modifications as part of proposed development.

Project Description		
Project Area (total area associated with the Project or total area of the right-of-way):	43.71	acres
	1,904,152.77	sq. ft.
Area to be disturbed by the Project (Project Footprint):	8.30	acres
	361,571.91	sq. ft.
Project Proposed Impervious Area (subset of Project Footprint)	3.20	acres
	222,563.86	sq. ft.
Project Proposed Pervious Area (subset of Project Footprint)	5.10	acres
	222,078.21	sq. ft.
The proposed **decrease** in impervious area in the proposed condition as compared to the pre-project condition: **Note**: The proposed 40% decrease in impervious area applies to redevelopment changes within the project footprint (8.30 acres) and not the total project area (43.71 acres).	40	%

Project Description

The County of Orange plans to demolish and replace ten buildings at the Orange County Juvenile Hall Campus in Orange, California, through the YTC Juvenile Hall Replacement Project. This project, located at 331 The City Drive South on a 17-acre property redevelopment is bounded by Interstate 5 (I-5) and the Santa Ana River to the east, Service Way to the north, Justice Center Way to the south, and Hospital Frontage Road to the west. The site is designated for Public Facilities and Institutions (PF/I) land use according to the City of Orange General Plan Land Use Element. The project will occur in three phases, Phase 1 will replace 95,589 sq. ft. of existing structures with new facilities, including YTC living units, vocational/educational, culinary, transitional housing, and administrative/medical buildings, totaling 117,905 sq. ft. Phase 2 will add long-term housing, a classroom/library, and independent living buildings. Phase 3, still in design, will focus on tenant improvements and potentially a couple more building demolitions. Phase 3 does not involve any new construction and therefore, Phase 3 improvements are not subject to WQMP requirements. Overall, the project aims to modernize the campus facilities, enhance services, and support institutional uses.

Grading and Earthwork - The existing grade on the project site is relatively flat, with gentle slopes ranging from 0.5 percent to 2 percent. The proposed pad grades and finish floor elevations for all new buildings would be elevated over the existing highest-grade point at the perimeter of each building, allowing surface drainage to be directed away from the proposed structures and toward appropriate drainage facilities. Existing earth materials in the building footprint areas would be excavated and properly compacted to an anticipated maximum depth of 6 feet below the existing ground surface. Deeper excavations could be conducted, as necessary, at the direction of the Geotechnical Engineer.

Grading would commence with the removal of all existing vegetation and improvements, and debris such as wood and root structures would be exported from the site. Fill and backfill soils would be placed in horizontal loose layers ranging from approximately 6 to 36 inches thick. It is not anticipated that the importation of soil would be necessary under the proposed project, as grading quantities are expected to be balanced on site. The proposed project does not propose any retaining walls but may include vertical mounding landscaping improvements including planter drains and plaza drains in between buildings. An overall Campus Path of Travel Exhibit would be developed in accordance with ADA standards to confirm key walkway locations.

Storm Drainage and Stormwater -

The proposed project (Phase 1 and 2 improvements only) would include new storm drainage laterals to be extended as needed from the existing 42-inch mainline storm drain provided on the Campus. In addition to the existing series of 24-inch by 24-inch inlets in the courtyard areas around the existing Campus buildings, the proposed project would add a new low point with a relocated inlet to direct storm flows to a water quality treatment basin. All hydrology and hydrologic calculations would be performed and verified for protection in a 100-year storm event according to the Orange County Hydrology Manual (1986) and its Addendum (1996) during final design.

The proposed project (Phase 1 and 2 only) would capture on-site water via roof drains, atrium area rains, and catch basins located within the Phase 1 and 2 project limits. The project site would be designed to help route water into a series of designated BIO-1 Bioretention with Underdrains and INF-3 Bioretention with no Underdrain prior to discharge. One storm drain would be connected to the existing mainline, which runs south along The City Drive and discharges into the Santa Ana River Channel, which ultimately leads to the Pacific Ocean.

3. Site and Watershed Characterization

Section 3 is required for ***Type 1: Priority Projects,*** ***Type 2: Green Street Projects,*** and ***Type 3: Non-Priority Projects***.

The purpose of this Section is to describe the Project site conditions that will inform the selection and design of BMPs through an analysis of the physical conditions and limitations of the site and its receiving waters. The Plan Developer shall conduct appropriate investigations to characterize the site and watershed in a manner that supports informed and appropriate decisions about site design, source control, Low Impact Development (LID), and hydromodification BMPs as part of subsequent steps. The Project WQMP/WQP/NPP shall clearly and comprehensively document the investigations completed and describe the site and watershed conditions in a manner that provides appropriate support for subsequent selection of site design, source control, LID and hydromodification BMPs.

3.1 Site Characterization

The Project Site Characterization Section of the WQMP/WQP/NPP shall include:

- Physical setting
  - Address
  - Planning Area/Land Use Designation/Zoning
- Site characteristics
- Topography
- Soil type and geology
- Groundwater considerations
- Geotechnical considerations
- Off-site drainage
- Existing utilities
- Proposed site development activities (including pollutants to be generated)
- Project land uses

Site Characterization

Identify the pollutant(s) expected to be generated by the Project.

- ☐ Metals
- ☒ Nutrients
- ☒ Oil and grease
- ☒ Pathogens (bacteria and viruses)
- ☒ Suspended solids / sediment
- ☒ Toxic organic compounds (pesticides, solvents, and hydrocarbons)
- ☒ Trash and debris

The County of Orange plans to demolish and replace ten buildings at the Orange County Juvenile Hall Campus in Orange, California, located at 331 The City Drive South on a 17-acre property. The site is designated for Public Facilities and Institutions (PF/I) land use according to the City of Orange General Plan. The project will occur in three phases: Phase 1 will replace 95,589 sq. ft. of existing structures with new facilities totaling 117,905 sq. ft. Phase 2 will add long-term housing, a classroom/library, and independent living buildings. Phase 3 will focus on tenant improvements and possibly more demolitions. The project aims to modernize the campus facilities and enhance services.

The site has a relatively flat topography with gentle slopes ranging from 0.5 to 2 percent and is categorized within Hydrologic Group B soils. The most recent geotechnical report is titled Geotechnical Consultation Multipurpose Building site for Juvenile Hall, City of Orange, Orange County, California, dated August 2016, the soils in the area consist of Quaternary Old Alluvial Fan deposits which includes sand, silt, and clay that represents deposits mainly from the Santa Ana River, currently less than 500 ft from the eastern boundary of campus Groundwater was not encountered within the depth of the earth borings investigated with a maximum depth of 38 feet. The approximate elevation of the site is between 137.1 to 126.6 feet above sea level.

Existing utilities will be expanded to include new sewer, water, and storm drainage laterals, as well as electrical improvements for the proposed buildings. Anticipated site development activities may generate pollutants such as nutrients, oil and grease, pathogens, suspended solids, and toxic organic compounds.

Grading will involve removing vegetation and debris, excavating up to 6 feet, and balancing soil on-site. No retaining walls are planned, but landscaping improvements will be included. New storm drainage laterals will be extended from the existing 42-inch mainline storm drain. The project will under Phase 1 will capture and treat stormwater runoff through bioretention basins before discharge into the Santa Ana River Channel. Under Phase 2 project area the project will capture and infiltrate stormwater runoff through bioretention basins.

3.2 Watershed Characterization

The Project Watershed Characterization Section of the WQMP/WQP/NPP shall include:

- Watershed
- Receiving waters
- Water quality impairments and TMDLs
- Pollutants of concern
- Methods for determining stream susceptibility
- Environmentally sensitive areas (ESAs) and areas of special biological concern
- Potential hydrologic conditions of concern (HCOC)

Additional information regarding these topics can be found in Section 2.3 of the NOC WQMP TGD and Section 2.3 of the SOC WQMP TGD.

Watershed Characterization

Identify the watershed(s) applicable to the Project.

- ☐ Aliso Creek
- ☐ Anaheim Bay – Huntington Harbor
- ☐ Dana Point Coastal Streams
- ☐ Laguna Coastal Streams
- ☐ Newport Bay
- ☐ Newport Coastal Streams
- ☐ San Clemente Coastal Streams
- ☐ San Gabriel – Coyote Creek
- ☐ San Juan Creek
- ☐ San Mateo Creek
- ☒ Santa Ana River

The Santa Ana River watershed includes receiving waters such as Santa Ana River, Reach 2; Santa Ana River, Reach 1; and the Pacific Ocean. There are no noted water quality impairments, Total Maximum Daily Loads (TMDLs), pollutants of concern, environmentally sensitive areas (ESAs), or potential hydrologic conditions of concern (HCOC) within the watershed and receiving water bodies.

3.3 Preliminary Infiltration Investigation

Section 3.3 is required only for ***Type 1: Priority Projects***.

A preliminary infiltration investigation is required for all Type 1: Priority Projects. Infiltration BMPs are prioritized on the hierarchy of BMPs; therefore, infiltration testing is necessary to determine feasibility for full or partial infiltration.

Testing shall seek to characterize the infiltration rates at the likely elevation of the infiltration BMPs, but it is recognized that design-level BMP elevations may not be known at this time. Spacing of tests shall be determined based on the variability of conditions. This can be informed by other information about the soils and geology within the Project, such as previous geotechnical investigations. In sites with uniform conditions, a minimum of three tests per site is recommended, coupled with review of other information to interpolate or extrapolate from test results. For larger or more varied sites, additional tests may be needed. Testing locations shall be focused where other soils and geologic data suggests that infiltration is most likely to be feasible.

As described in Section 2.3.1.3 of the SOC WQMP TGD, the goal of this investigation shall be to identify potentially suitable areas for infiltration. **Table 3-1** below, correlates feasibility potential to ranges for the feasibility screening infiltration rate (K_{screen}) and is intended to guide decision making. Note that K_{screen} is equivalent to the observed saturated infiltration rate (K_{obs}) divided by a factor of 2.

Table 3-1 Preliminary Infiltration Feasibility as Indicated by K_{screen}

Infiltration Rate	Indication	Infiltration BMP Category
K_{screen} > 2 in/hr	Highest potential for full infiltration	Full Infiltration
0.3 in/hr < K_{screen} < 2 in/hr	Full infiltration BMPs may be possible, but conditions may be marginal and require more thorough analysis or contingency planning as part of BMP selection	Full Infiltration or Partial Infiltration
0.05 in/hr < K_{screen} < 0.3 in/hr	Incidental infiltration may be possible	Partial Infiltration
K_{screen} < 0.05 in/hr	Negligible infiltration potential	No Infiltration

As part of the planning/screening phase, review of Natural Resources Conservation Service (NRCS) soils maps (provided in Appendix N.1 of the SOC WQMP TGD) and available information may be conducted by the Project design professional. Simple open pit testing may also be conducted by the Project design professional. These forms of testing do not require a report separate from the WQMP. Other types of tests must be conducted by a licensed professional geotechnical engineer or registered geologist. These types of testing require reporting.

A Preliminary Infiltration Investigation Report shall be included as **Attachment 1,** and it shall include a description of methods, identification of other data source uses, geologic setting, testing locations, testing results, interpretation of findings, and a graphical identification of ranges of infiltration rate (if applicable). The Report shall also discuss findings related to seasonal high groundwater, infiltrating into plumes or hazardous areas, and groundwater wells and associated buffer areas. Section 4.2.2.1 of the SOC WQMP TGD provides additional factors related to infiltration feasibility, if applicable, shall be included in the Report.

The results from the Preliminary Infiltration Investigation will be necessary for determining Infiltration Feasibility within the drainage management areas (DMAs) identified in **Section 5.2**.

> **Note**: Infiltration BMPs are proposed for Phase 2 of the site, but additional testing may be necessary. Initial percolation tests show that the average infiltration rates range from 1.40 to 2.73 in/hr, indicating that infiltration is possible. However, when applying the safety factor of 2 as indicated above the infiltration rates ($K_{screen)}$ range from 0.7 to 1.37 in/hr, suggesting that further analysis or planning may be needed.

4. Site Design BMPs for Non-Priority Projects

Section 4 is required for ***Type 3: Non-Priority Projects***.

The purpose of this Section is to document the selected and implemented site design BMPs and source control BMPs.

4.1 Site Design BMPs

Site Design BMPs reduce the volume of stormwater runoff generated on a project site as well as improve the quality of runoff that leaves the site, and are required for all proposed Non-Priority Projects. Descriptions of the most common Site Design BMPs are provided in the NOC and SOC WQMP TGDs. Complete **Table 4-1** below. All incorporated site design BMPs must be included in the BMP Exhibit, further discussed in **Section 9**, and on the construction plan set.

Table 4-1 Site Design BMPs for Non-Priority Projects

Site Design BMP	Included	Brief Description
Hydrologic Source Controls (HSCs)		
Localized On-Lot Infiltration[1]	☐	Phase 1 detail only, Phase 2 to be determined during initial design phase (35%)
Impervious Area Dispersion[2]	☐	Phase 1 detail only, Phase 2 to be determined during initial design phase (35%)
Street Trees[3]	☐	Phase 1 detail only, Phase 2 to be determined during initial design phase (35%)
Amended Soils Over Tight Underlying Soils	☐	
Residential Rain Barrels (Not Actively Managed)	☐	
Infiltration		
Bioretention without Underdrains	☐	
Rain Gardens	☐	
Porous Landscaping	☐	
Infiltration Planters	☐	
Retention Swales	☐	

[1] Also known as Downspout Infiltration, Retention Grading, French Drains, or On-Lot Rain Gardens
[2] Also known as Downspout Dispersion, Downspout Disconnection, Impervious Area Disconnection, or Sheet Flow Dispersion
[3] Also known as Canopy Interception

Site Design BMP	Included	Brief Description
Infiltration Trenches	☐	
Infiltration Basins	☐	
Subsurface Infiltration Galleries	☐	
French Drains	☐	
Permeable Asphalt	☐	
Permeable Concrete	☐	
Permeable Concrete Pavers	☐	
Evapotranspiration		
Green Roofs, Brown Roofs, Blue Roofs	☐	
Rainwater Harvesting		
Above-ground Rain Barrels	☐	
Above-ground Cisterns	☐	
Underground Tanks	☐	
Biotreatment		
Bioretention with Underdrains	☐	Phase 1 detail only, Phase 2 to be determined during initial design phase (35%)
Stormwater Planter Boxes with Underdrains	☐	
Rain Gardens with Underdrains	☐	
Constructed Wetlands	☐	
Vegetated Swales	☐	
Vegetated Filter Strips	☐	
Compost-Amended Road Shoulders	☐	
Proprietary (Ready-To-Install) Vegetated Biotreatment Systems	☐	

4.2 Other BMPs

Other BMPs, such as Treatment Control BMPs (sand filters, cartridge media filters) or Pretreatment BMPs (hydrodynamic separation devices, catch basin inserts), may be appropriate under certain conditions. Please provide details on any other BMPs selected for this Project. All incorporated BMPs must be included in the BMP Exhibit, further discussed in Section 9, and on the construction plan set.

Other BMPs
INSERT DETAILS HERE OR INSERT N/A

5. Site Design and Drainage Plan

Section 5 is required for ***Type 1: Priority Projects*** and ***Type 2: Green Street Projects***.

The purpose of this Section is to develop the site design and drainage plan incorporating all applicable site design BMPs and source control BMPs, and to determine the locations for structural BMPs by dividing the site into separate drainage management areas (DMAs). For Priority Projects in NOC, this section will also establish Project performance criteria and document conformance with performance criteria.

5.1 Project Performance Criteria – NOC Only

Section 5.1 is required for ***NOC Type 1: Priority Projects*** ***and Type 2: Green Street Projects***.

Project Performance Criteria	
1. Is there an approved Watershed Infiltration and Hydromodification Management Plan (WIHMP)[1] or equivalent for the Project area that includes more stringent LID feasibility criteria or opportunities identified for implementing LID on regional or sub-regional basis? If so, describe the WIHMP feasibility criteria or regional/sub-regional LID opportunities:	
☐	A WIHMP applies. A description will be included as **Attachment 2**.
☒	A WIHMP is not applicable.
2. If HCOCs exist, identify applicable hydromodification control performance criteria. Check all that apply.	
☐	Post-development runoff volume for the 2-year, 24-hr storm event ($V_{2\text{-yr, POST}}$) exceeds that of the pre-development condition ($V_{2\text{-yr, PRE}}$) by more than 5%, thereby requiring hydromodification controls.
☐	Post-development time of concentration for the 2-year, 24-hr storm event ($Tc_{2\text{-yr, POST}}$) is less than that of the pre-development condition ($Tc_{2\text{-yr, PRE}}$) by more than 5%, thereby requiring hydromodification controls.
☒	HCOC do not exist within the Project area. Exhibits and/or calculations will be provided as **Attachment 10** demonstrating as such.
3. List applicable LID performance criteria. Check all that apply.	
☒	Selected BMPs will infiltrate, harvest and use, or evapotranspire the runoff from the 85th percentile, 24-hour storm event (Design Capture Volume, or DCV).
☒	Infiltration, harvest and use, and evapotranspiration (ET) cannot be feasibly implemented for the full DCV; and therefore, a properly designed biotreatment system will be considered to treat the runoff from the 85th percentile, 24-hour storm event.
4. List applicable structural treatment control BMP performance criteria.	
☐	Implemented LID BMPs (including biotreatment) are insufficient in treating the full DCV; therefore, structural treatment control BMPs are necessary and will treat the 85th percentile, 24-hour storm event.
☒	The full DCV is treated by LID BMPS; therefore, structural treatment control BMPs are not necessary.

[1]As of December 2019, no WIHMP exists in Orange County.

5.2 DMA Delineation and BMP Site Selection

Section 5.2 is required for all ***Type 1: Priority Projects*** *and Type 2: Green Street Projects*.

The Project site shall be delineated into DMAs per guidance provided in Section 2.4.2.2. of the NOC WQMP TGD or per Section 2.4.3.3 of the SOC WQMP TGD and shall be shown on the BMP Exhibit, further discussed in **Section 9**. Upon delineation, locations for proposed structural BMPs within each DMA shall be identified. These locations, along with areas of potential pollutant generation, impervious and pervious areas, any sensitive environmental features, and infiltration rates (if applicable) shall all be included in the BMP Exhibit. DMAs shall be summarized in **Table 5-1** below, referencing the IDs shown in the exhibit and providing the total area, percent impervious, and Design Capture Volume (DCV). BMPs shall be summarized in **Table 5-2** below, providing the BMP ID as shown in the exhibit, infiltration feasibility, the DMA(s) for which it is providing treatment, and total DCV. Refer to the Preliminary Infiltration Investigation conducted per **Section 3.3** of this template to determine infiltration feasibility for each BMP. Infiltration Feasibility is not required for Type 2: Green Street Projects. Additional tables are provided in and are to be appended to the WQMP as **Attachment 3.** Instructions on how to calculate DCV are provided in Appendix III of the NOC WQMP TGD (Equation III.1) and Appendix E of the SOC WQMP TGD (Equation E.2). Calculations are to be included as **Attachment 4.**

Table 5-1 DMA Summary

DMA ID	Total Area	Imperviousness	DCV
	ac	%	ac-ft
Phase 1 – DMA 1, Behavioral Health	0.289	100%	0.02
Phase 1 – DMA 2, Kitchen	0.096	100%	0.01
Phase 1 – DMA 3, Vocation	0.253	100%	0.01
Phase 1 – DMA 4, Duplex	0.278	100%	0.02
Phase 1 – DMA 5, Triplex	0.273	100%	0.02
Phase 1 – DMA 6, Site	5.382	20%	0.10
Phase 2A – DMA 1, Long-Term Housing	1.409	65%	0.06
Phase 2B – DMA 1, Independent Living	1.083	75%	0.05

Table 5-2 BMP Summary

BMP ID	Infiltration BMP Category			Associated DMA(s)	Total DCV
	Full	Partial	No Infiltration	-	ac-ft
BH	☐	☐	☒	Phase 1 – DMA 1, Behavioral Health	0.02
K	☐	☐	☒	Phase 1 – DMA 2, Kitchen	0.01
V	☐	☐	☒	Phase 1 – DMA 3, Vocation	0.01
D	☐	☐	☒	Phase 1 – DMA 4, Duplex	0.02
T	☐	☐	☒	Phase 1 – DMA 5, Triplex	0.02
LTH	☒	☐	☐	Phase 2A – DMA 1, Long-Term Housing	0.234
IL	☒	☐	☐	Phase 2B – DMA 1, Independent Living	0.201

A narrative is to be provided describing the rationale behind the selected drainage and site plan. At a minimum, the narrative shall include the following:

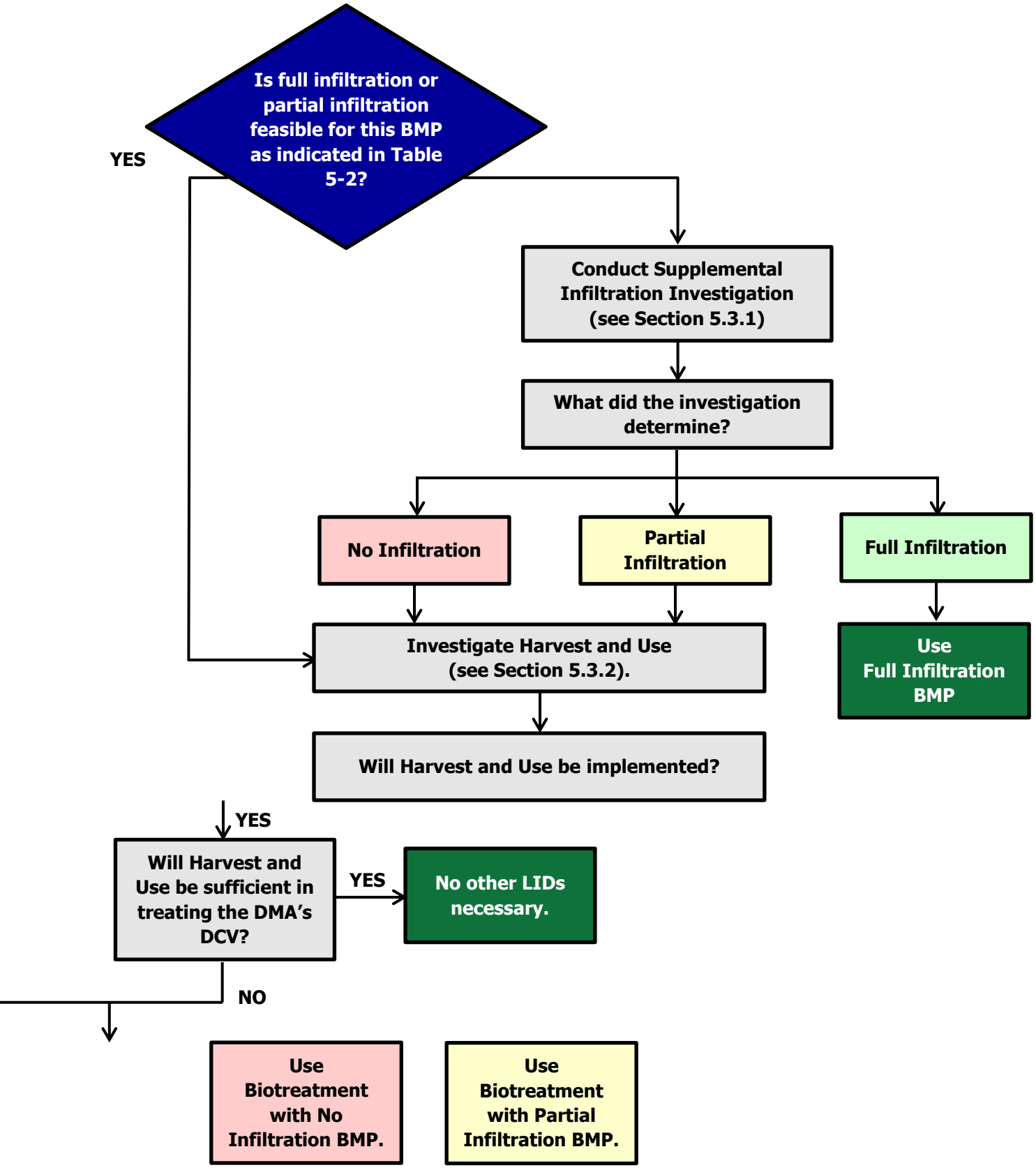
- Provide rationale and methodology for how the site was divided into DMAs and how BMP placement was selected;
- Describe how DMAs and BMP sites were located to maximize retention and site BMPs where infiltration is most feasible, to the extent practicable; and
- Describe any overriding factors affecting drainage and BMP location at the site.

DMA Delineation and BMP Justification
Phase 1 Drainage Management Areas (DMAs) are designated for managing runoff from the building footprint. BMPs are strategically placed based on roof drainage locations and coordinated to integrate with the new landscaping. The selected BMPs are flow-through filtration planters designed to capture roof runoff. Infiltration is not feasible due to the proximity of the planters to the foundations of the new buildings. **Phase 2** Phase 2 is divided into two DMAs, designated as Phase 2A – DMA 1 and Phase 2B – DMA 1. Although specific BMPs have not yet been designed for these areas, the approach will mirror Phase 1. This includes the implementation of retention planters (INF-3 Bioretention with no Underdrain) to effectively capture and manage runoff within each DMA.

5.3 Additional Investigations for Priority Projects

Section 5.3 is required for all ***Type 1: Priority Projects***.

The SOC WQMP TGD defines a hierarchy for BMP prioritization with full infiltration BMPs ranking first. Additionally, the TGD requires consideration of harvest and use for any BMPs for which full infiltration is not feasible. Therefore, to determine the feasibility of each, additional investigations are necessary. The flow chart in **Figure 5-1** below will guide the Plan Developer in determining which investigations are necessary. The sections below provide guidance related to these investigations.



re 5-1 BMP Prioritization Flow Chart

5.3.1 Supplemental Infiltration Investigation

Infiltration BMPs are to be prioritized over any and all other LID BMPs. Therefore, for any BMPs for which "Full Infiltration" or "Partial Infiltration" is feasible, additional infiltration testing is required. This will provide more accurate infiltration rates compared to those provided by the Preliminary Infiltration Investigation. For BMPs for which "No Infiltration" was identified, additional testing is not necessary; however, documentation must be provided demonstrating the unlikelihood of infiltration feasibility. Refer to the NOC and SOC WQMP TGDs for appropriate criteria related to infeasibility and attach all relevant documentation as **Attachment 5**.

Infiltration testing must be conducted or overseen by a qualified professional; either a Professional Engineer (PE) or Registered Geologist licensed in the State of California and shall be conducted at the location of the proposed BMP. The elevation of the tests shall correspond to the facility elevation, plus 1 to 2 feet to account for soil amendments or decompacted zones under the infiltration system. If a confining layer, or soil with a greater percentage of fines, is observed during the subsurface investigation to be within 6 feet of the bottom of the planned infiltration system, the testing shall be conducted within that confining layer. The boring logs shall continue to at least 15 feet below the invert of the proposed BMP. Borings shall be conducted at each test location.

The recommended number of infiltration tests depends up on the footprint size and the soil variability. The following guidance is provided to estimate the number of tests per BMP:

- Three infiltration tests shall be conducted for every Full Infiltration BMP, conducted within the proposed BMP footprint or within 20 feet of the perimeter in representative soil formations.
- For Full Infiltration BMPs with footprints larger than 10,000 square feet, conduct one additional test for every 10,000 square feet of BMP footprint area after the first 10,000 square feet. For example, if a large BMP had an infiltration area of 30,000 square feet, 5 tests shall be conducted (3 for the first 10,000 square feet, 1 for the next 10,000, and 1 for the next 10,000).
- One test for every 100 lineal feet of infiltration facility.
- In general, no more than five valid tests are required per BMP of any footprint, unless more tests would be valuable or necessary (at the discretion of the qualified professional assessing the site, as well as the reviewing jurisdiction).

These recommendations may need to be reduced or increased at the discretion of the Plan Developer and reviewing jurisdiction depending on the complexity and variability of the site.

Reporting shall include:

- Name and qualifications of preparer;
- Scope of investigation, including description of methods, identification of other data source uses;
- Geologic setting;
- Testing locations and depths;
- Testing results;
- Testing records and description of specific measurements;

- Interpretation of findings, including consideration of limiting horizons or groundwater conditions that could limit full scale infiltration;
- Confirmation or adjustment of preliminary infiltration screening (i.e. Is it acceptable to utilize full infiltration BMPs?); and
- Recommended component of the overall factor of safety that is appropriate to account for variability or uncertainty in testing.

For each BMP-site-specific K_{obs} provided by the Supplementary Infiltration Investigation, calculate the updated K_{screen}. Then, using **Table 5-3** below, identify the updated infiltration feasibility the K_{screen} correlates to. Record results in **Table 5-4.**

Table 5-3 Updated Infiltration Feasibility

Infiltration Rate	Infiltration BMP Category
K_{screen} > 2 in/hr	Full Infiltration
0.3 in/hr < K_{screen} < 2 in/hr	Full Infiltration or Partial Infiltration
0.05 in/hr < K_{screen} < 0.3 in/hr	Partial Infiltration
K_{screen} < 0.05 in/hr	No Infiltration

5.3.2 Harvest and Use Investigation

As discussed, full infiltration BMPs shall be implemented wherever feasible; however, in the case that full infiltration is not feasible, harvest and use must first be considered before any biotreatment BMP can be considered. For BMPs for which "Partial Infiltration" or "No Infiltration" was identified, either in **Table 5-2** or by the Supplemental Infiltration Investigation, harvest and use feasibility must be determined. Harvest and use feasibility criteria is provided in Section 4.2.3 of the SOC WQMP TGD. Record results in **Table 5-4** below. Note that harvest and use is not required if found feasible.

5.3.3 Results from Additional Investigations

In **Table 5-4** below, summarize the results from the investigations conducted per **Section 5.3.1** and **Section 5.3.2**. Additional tables are provided in and shall be attached as **Attachment 6**.

Table 5-4 Infiltration and Harvest and Use Feasibility

BMP ID	Infiltration Feasibility			Harvest and Use Feasibility		
	Full	Partial	No Infiltration	Feasible	Not Feasible	NA
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐

6. Site Design BMPs for Priority Projects

Section 6 is required for ***Type 1: Priority Projects***.

Site Design BMPs reduce the volume of stormwater runoff generated on a project site as well as improve the quality of runoff that leaves the site. Site Design BMPs are required for all proposed Priority Projects and shall be included in the BMP Exhibit, discussed further in **Section 9**, and the construction plan set.

6.1 Selection of Site Design BMPs

Refer to Section 2.5 of the SOC WQMP TGD for BMP selection Guidance.

6.2 Site Design BMP Calculations

Attachment 7 contains Priority Project BMP Conformance Analysis Tables for NOC and SOC. One set of tables must be completed for each DMA listed in **Section 5.2** above. Note that a single set of tables may be completed for multiple DMAs if BMPs are shared (i.e. one BMP is designed to treat runoff from multiple DMAs). Be sure to include the DMA ID (or list of DMA IDs) and the corresponding DCV (or sum of DCVs) in each table.

This WQMP Template includes just one set of BMP Conformance Analysis Tables for NOC and SOC. The Plan Developer must include as many sets of tables as necessary to evaluate all DMAs. Each additional set of tables is to be appended within **Attachment 7**.

All calculations are to be included in **Attachment 8**. Calculation procedures shall be in accordance with Appendix E of the SOC WQMP TGD for South Orange County projects, and with Appendix III of the NOC WQMP TGD for North Orange County projects.

6.3 Inventory of BMPs

Using **Table 6-1** below, provide a summary of all HSCs, LID BMPs, Treatment Controls, and/or Regional/Sub-Regional BMPs implemented by the Project. Include the BMP type, treatment capacity, associated DMA(s), and corresponding DCV/Total DCV.

Table 6-1 Priority Project BMP Inventory

BMP ID	BMP Type	Treatment Capacity / DCV Reduction	Associated DMA(s)	DCV / Total DCV	
			-		
BH1	Flowthrough Planter	708.75 cu-ft	BEHAVIORAL HEALTH	345	1,050 cu-ft
BH2	Flowthrough Planter		BEHAVIORAL HEALTH	345	
BH3	Flowthrough Planter		BEHAVIORAL HEALTH	360	
K1	Flowthrough Planter	236.25 cu-ft	KITCHEN		240 cu-ft
V1	Flowthrough Planter	618.75 cu-ft	VOCATIONAL	288	864 cu-ft
V2	Flowthrough Planter		VOCATIONAL	432	
V3	Flowthrough Planter		VOCATIONAL	144	
D1	Flowthrough Planter	680.63 cu-ft	DUPLEX	150	882 cu-ft
D2	Flowthrough Planter		DUPLEX	147	
D3	Flowthrough Planter		DUPLEX	147	
D4	Flowthrough Planter		DUPLEX	150	
D5	Flowthrough Planter		DUPLEX	144	
D6	Flowthrough Planter		DUPLEX	144	
T1	Flowthrough Planter	1,068.75 cu-ft	TRIPLEX	84	1,482 cu-ft
T2	Flowthrough Planter		TRIPLEX	72	
T3	Flowthrough Planter		TRIPLEX	119	
T4	Flowthrough Planter		TRIPLEX	125	
T5	Flowthrough Planter		TRIPLEX	72	
T6	Flowthrough Planter		TRIPLEX	147	
T7	Flowthrough Planter		TRIPLEX	210	
T8	Flowthrough Planter		TRIPLEX	201	
T9	Flowthrough Planter		TRIPLEX	198	
T10	Flowthrough Planter		TRIPLEX	201	
T11	Flowthrough Planter		TRIPLEX	214	
BMP 2A	Bioretention Planter with no Underdrain	1,305 cu-ft	Phase 2A DMA 1	1,309 cu-ft	
BMP 2B	Bioretention Planter with no Underdrain	1,121 cu-ft	Phase 2B DMA 1	1,122 cu-ft	

Total DCV Reduction =		cu-ft	Is compliance achieved? ☒ Yes ☐ No
Total DCV =	0	cu-ft	

7. Site Design BMPs for Green Street Projects

Section 7 is required for ***Type 2: Green Street Projects***.

Generally, Green Street Projects must follow the same criteria as Type 1: Priority Projects regarding site design and drainage management area assessments (see **Section 3** of this template). Green Street Projects must also delineate drainage management areas and determine the DCV for each DMA (see **Section 5** of this template).

The Municipal Separate Storm Sewer System (MS4) Permit cites the requirement that Plan Developers utilize the USEPA municipal handbook "Managing Wet Weather with Green Infrastructure – Green Streets" as guidance for selecting appropriate BMPs. Because street projects typically feature more constraints in terms of utilities, structures, and traffic flow, certain BMPs are a better choice than others for Green Street Projects. The MS4 Permit requires that Plan Developers of applicable Green Streets Projects shall select BMPs consistent with the USEPA Green Streets guidance to the "Maximum Extent Practicable". The "Maximum Extent Practicable" standard is intended to be a relatively stringent standard. Developers of Green Streets Projects must follow a BMP prioritization and selection process for each DMA and must exhaust every physical possibility before declaring that capturing and treating the DCV is not possible.

The following steps are used to size LID BMPs for applicable Green Street Projects.

1. Complete site and watershed characterization (**Section 3**).
2. Delineate DMAs and compute the DCV per each DMA (**Section 5**)
3. For each DMA identified in Step 2, select one or more BMPs consistent with USEPA Green Streets guidance. Refer to Section 2.9.4 of the SOC WQMP TGD for more information. Selected BMPs shall be included in the BMP Exhibit (discussed further in **Section 9)**, and the construction plan set.
4. Complete the tables in **Attachment 9** for each DMA identified in Step 2. Note that a single set of tables may be completed for multiple DMAs if BMPs are shared (i.e. one BMP is designed to treat runoff from multiple DMAs). Be sure to include the DMA ID (or list of DMA IDs) and the corresponding DCV (or sum of DCVs) in each table. This WQMP Template includes just one set of BMP Conformance Analysis Tables. The Plan Developer must include as many sets of tables as necessary to evaluate all DMAs. Each additional set of tables is to be appended within **Attachment 9**. All calculations are to be included in **Attachment 8**. Calculation procedures shall be in accordance with Appendix E of the SOC WQMP TGD for South Orange County projects, and with Appendix III of the NOC WQMP TGD for North Orange County projects.
5. If LID or hydromodification sizing criteria cannot be achieved, document the constraints that override the application of BMPs, and provide the largest portion of the sizing criteria that can be reasonably provided given constraints.

7.1 Inventory of BMPs

Using **Table 7-1** below, provide a summary of all HSCs, LID BMPs, and/or Treatment Controls BMPs implemented by the Project. Include the BMP type, treatment capacity, associated DMA(s), and corresponding DCV/Total DCV.

Table 7-1 Green Street Project BMP Inventory

BMP ID	BMP Type	Treatment Capacity / DCV Reduction	Associated DMA(s)	DCV / Total DCV
		ac-ft	-	ac-ft

8. Hydromodification BMPs

Section 8 is required for ***Type 1: Priority Projects*** and ***Type 2: Green Street Projects***.

Priority Projects and Green Street Projects are required to determine whether HCOCs exist as a result of the Project. Use the appropriate table below to identify whether or not HCOCs exist and whether a Hydromodification Management Plan is necessary. Note that criteria for NOC and SOC are different.

Determination of HCOCs within NOC			
Do HCOCs exist?		**Reasoning**	
☒	No	☐	The volumes and the time of concentration of storm water runoff for the post-development condition do not significantly exceed those of the pre-development condition for a two-year frequency storm event (a difference of 5% or less is considered insignificant). This may be achieved through site design and source control BMPs.
		☒	All downstream conveyance channels that will receive runoff from the Project are engineered, hardened, and regularly maintained to ensure design flow capacity, and no sensitive stream habitat areas will be affected.
☐	Yes	☐	None of the conditions above are met.

Determination of HCOCs within SOC			
Do HCOCs exist?		**Reasoning**	
☐	No	☐	Project discharges directly to a protected conveyance (bed and bank are concrete lined the entire way from the point(s) of discharge to a receiving lake, reservoir, embayment, or the Ocean.
		☐	Project discharges directly to storm drains which discharge directly to a reservoir, lake, embayment, ocean, or protected conveyance.
		☐	The Project discharges to an area identified in the Water Management Area Analysis as exempt from hydromodification concerns.
☐	Yes	☐	None of the conditions above are met.

If HCOCs do not exist for the Priority Project or Green Streets Project, exhibits and/or calculations must be provided as **Attachment 10** demonstrating such.

If HCOCs do exist, additional documentation demonstrating mitigation of possible hydromodification is necessary. Include said documentation as **Attachment 11**. Structural BMPs, if incorporated, shall be included in the BMP Exhibit, discussed further in **Section 9**, and the construction plan set. Note that SOC, specifically, requires a Hydromodification Management Plan. Refer to the SOC WQMP TGD for additional information.

9. BMP Exhibit

Section 9 is required for ***Type 1: Priority Projects***, ***Type 2: Green Street Projects,*** and ***Type 3: Non-Priority Projects***.

An exhibit is to be included with the WQMP/WQP/NPP beginning with the Draft submission due at the 65% Design phase and is to be updated for all submissions up to the Final WQMP/WQP/NPP due at Project completion. Exhibit elements vary depending on the required document type (WQMP, WQP, or NPP) and Project location. Refer to the checklist below for exhibit requirements. Note that items in bold should also be including in the Project's construction plan set.

BMP Exhibit Requirements	
☒	Minimum 24" x 36" sheet
☒	Title block including the Project name, Project file number (as assigned by County), and grading/building or planning application permit numbers, as applicable
☒	Project location (including address, drainage plot plan, tract/lot number(s), etc.)
☒	Legend, north arrow, and scale
☒	Plan Developer name and stamp
☒	Site boundary
☒	Downstream receiving water(s) of the Project, any 303(d) listed or TMDL water bodies, and any hydromodification susceptible water bodies
☐	Land uses and land covers, as applicable
☒	**Each facility and its intended function**
☐	Areas of outdoor activities, as applicable
☒	**Drainage delineations and flow information**
☐	**Key topographic features, environmentally sensitive features, natural drainage courses, and other relevant information**
☒	Relationship between onsite drainage and offsite drainage including all drainage connections
☒	**Stormwater management infrastructure including storm drain facilities**
☐	Conditions relevant to infiltration feasibility findings (as applicable), such as, but not limited to, surficial soil properties, depth to groundwater, and geotechnical hazards, locations of infiltration testing, factors influencing demonstrated space constraints or vertical constraints
☒	**Locations and types of all structural BMPs including, as applicable**
☐	**GIS coordinates for all structural BMPs, as applicable**
☒	**BMP details with detailed design parameters relevant to sizing calculations, as applicable**

10. Source Control BMPs

Section 10 is required for ***Type 1: Priority Projects***, ***Type 2: Green Street Projects,*** and ***Type 3: Non-Priority Projects***.

Source Control BMPs, both non-structural and structural, are required for Priority Projects, Green Street Projects, and Non-Priority Projects where applicable to Project features. Please identify the applicable Source Control BMPs within **Table 10-1** and **Table 10-2** below. For any BMP marked "Not Included", an explanation is required and shall be provided at the bottom of the table. All structural BMPs marked "included" shall be included in the BMP Exhibit discussed in **Section 9**, and in the construction plan set.

Table 10-1 Structural Source Control BMPs

Identifier	Name	Included	Not Included	Not Applicable
S1	Provide storm drain system stenciling and signage	☒	☐	☐
S2	Design and construct outdoor material storage areas to reduce pollution introduction	☒	☐	☐
S3	Design and construct trash and waste storage areas to reduce pollution introduction	☒	☐	☐
S4	Use efficient irrigation systems & landscape design, water conservation, smart controllers, and source control	☒	☐	☐
S5	Protect slopes and channels and provide energy dissipation	☐	☐	☒
	Incorporate requirements applicable to individual priority project categories (from SDRWQCB NPDES Permit)	☒	☐	☐
S6	Dock areas	☐	☐	☒
S7	Maintenance bays	☐	☐	☒
S8	Vehicle wash areas	☐	☐	☒
S9	Outdoor processing areas	☐	☐	☒
S10	Equipment wash areas	☐	☐	☒
S11	Fueling areas	☐	☐	☒
S12	Hillside landscaping	☐	☐	☒
S13	Wash water control for food preparation areas	☐	☐	☒
S14	Community car wash racks	☐	☐	☒

For any Source Control BMPs marked "Not Included" briefly state reasoning:

All BMPs will be provided within the Phase 1 Site Specific WQMP; All BMP's will be provided within the Phase 2 Site Specific BMP when the design phase is initiated.

Describe implementation frequency for each Source Control BMP.

Phase 1 details on frequency to be provided in the Phase 1 Site Specific BMP; Phase 2 details on frequency to be provided when the design phase is initiated.

Table 10-2 Non-Structural Source Control BMPs

Identifier	Name	Included	Not Applicable	Not Included
N1	Education for Property Owners, Tenants and Occupants	☒	☐	☐
N2	Activity Restrictions	☒	☐	☐
N3	Common Area Landscape Management	☒	☐	☐
N4	BMP Maintenance	☒	☐	☐
N5	Title 22 CCR Compliance (How development will comply)	☐	☒	☐
N6	Local Industrial Permit Compliance	☐	☒	☐
N7	Spill Contingency Plan	☐	☒	☐
N8	Underground Storage Tank Compliance	☐	☒	☐
N9	Hazardous Materials Disclosure Compliance	☐	☒	☐
N10	Uniform Fire Code Implementation	☒	☐	☐
N11	Common Area Litter Control	☒	☐	☐
N12	Employee Training	☒	☐	☐
N13	Housekeeping of Loading Docks	☐	☒	☐
N14	Common Area Catch Basin Inspection	☒	☐	☐
N15	Street Sweeping Private Streets and Parking Lots	☒	☐	☐
N16	Retail Gasoline Outlets	☐	☒	☐

For any Source Control BMPs marked "Not Included" briefly state reasoning:

All BMPs will be provided within the Phase 1 Site Specific WQMP; All BMP's will be provided within the Phase 2 Site Specific BMP when the design phase is initiated.

Describe implementation frequency for each Source Control BMP.

Phase 1 details on frequency to be provided in the Phase 1 Site Specific BMP; Phase 2 details on frequency to be provided when the design phase is initiated.

11. Educational Material

Section 11 is required for ***Type 1: Priority Projects***.

Educational materials specifically applicable to the Project must be identified. Identify the applicable educational materials below. Listed materials are available in the provided web links and are not to be included in the WQMP submission; however, additional materials specific to the Project may be included and must be attached as **Attachment 13**.

Educational Material	
Title	**Check If Applicable**
Residential Material (https://h2oc.org/resources/view-order-brochures/resident-brochures/)	
The Ocean Begins at Your Front Door	☒
Tips for Protecting Your Watershed	☒
Proper Disposal of Household Hazardous Waste	☒
Homeowners Guide for Sustainable Water Use	☒
Household Tips	☒
Tips for the Home Mechanic	☒
Recycle at Your Local Used Oil Collection Center (North County)	☒
Recycle at Your Local Used Oil Collection Center (Central County)	☐
Recycle at Your Local Used Oil Collection Center (South County)	☐
Tips for the Home Improvement Projects	☐
Tips for Using Concrete and Mortar	☐
Tips for Projects Using Paint	☒
Sewage Spill Reference Guide for Private Property Owners	☐
Tips for Maintaining a Septic Tank System	☐
Tips for Landscaping and Gardening	☒
Tips to Prevent Overwatering	☒
Responsible Pest Control	☒
Tips for Pet Care	☐
Tips for Horse Care	☐
Tips for Pool Maintenance	☐
Tips for Residential Pool, Landscape and Hardscape Drains	☐
Children's Watershed Workbook	☐
Coloring and Activity Booklet Brochure	☐
Tips for Car Wash Fundraisers	☐
Business Material (https://h2oc.org/resources/view-order-brochures/business-brochures/)	
Tips for the Automotive Industry	☐
Tips for the Food Service Industry	☒
Proper Maintenance Practices for Your Business	☒
Compliance BMPs for Mobile Businesses	☐
Water Quality Requirements for Land Development	☐

Other Material	Check if Attached
	☐
	☐
	☐
	☐
	☐

12. Routine Inspections, Operations, and Maintenance

Section 12 must be completed for ***Type 1: Priority Projects***, ***Type 2: Green Street Projects,*** and ***Type 3: Non-Priority Projects***.

12.1 Inspection / Maintenance Responsibilities

Structural BMPs implemented by Priority Projects, Green Street Projects, and Non-Priority Projects must be regularly inspected and maintained post-construction for proper effectiveness into perpetuity. For each BMP implemented by the Project, document inspection and maintenance information within **Table 12-1**. Additional tables are provided in and are to be appended as **Attachment 14**.

Inspection and maintenance records must be kept for a minimum of five years for inspection by the regulatory agency.

12.2 Operations and Maintenance Plan

Section 12.2 must be completed for ***Type 1: Priority Projects*** ***and Type 2: Green Street Projects***.

Plan Developers of Type 1: Priority Projects and Type 2: Priority Green Street Projects are required to prepare a comprehensive O&M Plan for structural BMPs implemented as part of the Final WQMP submittal. Refer to Section 7 of the NOC WQMP TGD, and Section 2.8 of the SOC WQMP TGD for guidance related to the O&M Plan.

The O&M Plan submitted at the 100% Design phase of the final WQMP must describe the designated party responsible for maintenance, inspection/maintenance activities required, and maintenance frequency. The O&M Plan included in the WQMP is intended to be a starting point for maintenance activities that will take place in the future. Site specific conditions will determine the final maintenance requirements of the site over time, and that ultimately maintenance frequency is set by OC Public Works' asset management system.

The O&M Plan is to be included as **Attachment 15.**

> All BMPs will be provided within the Phase 1 Site Specific WQMP; All BMP's will be provided within the Phase 2 Site Specific BMP when the design phase is initiated.

Table 12-1 BMP Inspection and Maintenance Responsibilities

BMP	DMA	Reponsible Party(s)	Inspection/ Maintenance Activities Required	Minimum Frequency of Activities

13. Discretionary Permits and Water Quality Conditions

Section 13 is required for ***Type 1: Priority Projects*** and ***Type 2: Green Street Projects***.

13.1 Discretionary Permits

List the discretionary permit(s) applicable to the Project and provide the site address or lot and tract/parcel map number describing the property for which the permit was issued.

Permit	Site Address/Lot and Tract/Parcel Map Number
INSERT PERMIT NAME HERE	INSERT ADDRESS HERE
INSERT PERMIT NAME HERE	INSERT ADDRESS HERE
INSERT PERMIT NAME HERE	INSERT ADDRESS HERE
INSERT PERMIT NAME HERE	INSERT ADDRESS HERE
INSERT PERMIT NAME HERE	INSERT ADDRESS HERE

13.2 Water Quality Conditions

List the conditions verbatim, any Water Quality Conditions, including the condition requiring preparation of WQMP, if applicable. Water Quality Conditions may be included as mitigation measures in California Environmental Quality Act (CEQA) documents for the Project. For example, a Mitigation Monitoring and Report Program adopted in a certified CEQA document may include Project Design Features, Standard Conditions, and Mitigation Measures related to water quality protection.

Water Quality Condition
DESCRIBE CONDITION HERE
DESCRIBE CONDITION HERE
DESCRIBE CONDITION HERE
DESCRIBE CONDITION HERE
DESCRIBE CONDITION HERE

14. Submittal Process

A Draft WQMP/WQP/NPP is required at each phase of the Project (Initiation, 35% Design, 65% Design, 90% Design, as applicable) with the Final WQMP submitted at 100% Design. Drafts shall include all required sections as detailed in **Section 1** and shall be submitted at the specified Project Phase as well as the phases that follow. All sections shall be updated prior to each Draft and the Final submission to reflect the latest Project design.

The OC Environmental Resources Division and Operations and Maintenance Division will review the WQMP/WQP/NPP at all stages of design. Upon completion and submission of the Final WQMP/WQP/NPP, both Divisions will review the plan and if approved, no further action is required of the Plan Developer. If the plan is not approved, comments will be provided to the Plan Developer which shall be addressed prior to resubmission. It is expected that the ultimate owner of these public facilities will be involved throughout the design phase.

During construction, the OC Construction Division will conduct inspections on all construction processes related to the structural BMPs identified in the Final WQMP/WQP/NPP. Inspections will monitor construction processes to ensure that the BMPs are designed according to the approved plan. Inspection forms must be completed and submitted to the OC Construction Division by the Inspector for every required inspection. A BMP Inspection Record, available in **Attachment 16**, shall be kept on site by the Contractor and updated following each inspection. Provided that BMPs are constructed according to the approved design plan and modifications are not necessary post construction, responsibility for maintenance of the BMPs will be transferred to the parties identified in **Section 12**.

Following the transfer of responsibility, the following forms will be sent to and filed by the following departments. The Transmittal Page shall be included with every submittal.

Table 14-1 Document Transfer Guide

Recipient	Document(s)
During Project Design	
OC Environmental Resources OC Operations and Maintenance Division OC Facilities Maintenance	➢ All Sections
After Plan Approval, Before Construction Completion	
OC Construction Division	➢ Section 9 – BMP Exhibit ➢ Attachment 12 – BMP Exhibit ➢ Attachment 16 – BMP Inspection Record
After Construction Completion and Project Acceptance by County	
OC Operations and Maintenance Division (for Type 1: Priority Projects not involving buildings or parking lots; all Type 2: Green Street Projects)	➢ Table 6-1 / Table 7-1 - BMP Inventory ➢ Section 9 – BMP Exhibit ➢ Section 10 – Source Control BMPs ➢ Section 12 – Routine Inspections, Operations, and Maintenance ➢ Attachment 12 – BMP Exhibit ➢ Attachment 14 – Additional BMP Inspection and Maintenance Responsibility Tables ➢ Attachment 15 – Operations and Maintenance Plan
OC Facilities Maintenance (for Type 1: Priority Projects involving buildings or parking lots)	➢ Table 6-1 – BMP Inventory ➢ Section 9 - BMP Exhibit ➢ Section 10 – Source Control BMPs ➢ Section 12 – Routine Inspections, Operations, and Maintenance ➢ Attachment 12 – BMP Exhibit ➢ Attachment 14 – Additional BMP Inspection and Maintenance Responsibility Tables ➢ Attachment 15 – Operations and Maintenance Plan
OC Parks Maintenance (for Type 1: Priority Projects and Type 2: Green Street Projects involving bikeways)	➢ Table 6-1 / Table 7-1 - BMP Inventory ➢ Section 9 – BMP Exhibit ➢ Section 10 – Source Control BMPs ➢ Section 12 – Routine Inspections, Operations, and Maintenance ➢ Attachment 12 – BMP Exhibit ➢ Attachment 14 – Additional BMP Inspection and Maintenance Responsibility Tables ➢ Attachment 15 – Operations and Maintenance Plan

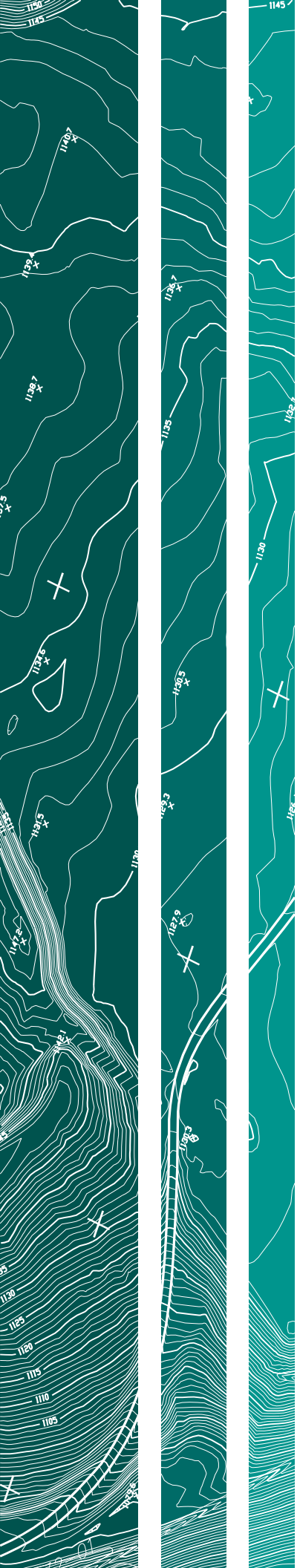
15. Attachments

The following attachments may be required as part of the Project WQMP/WQP/NPP submittal. Refer to sections outlined below for more information.

Attachment		Section
Attachment 1	Preliminary Infiltration Investigation Report	3.3
Attachment 2	WIHMP Criteria and Opportunities (NOC Only)	5.1
Attachment 3	Additional DMA Delineation Tables	5.2
Attachment 4	DCV Calculations	5.2
Attachment 5	Supplementary Infiltration Investigation Report	5.3.1
Attachment 6	Additional Infiltration and Harvest and Use Feasibility Tables	5.3.3
Attachment 7	Additional Priority Project BMP Conformance Analysis Tables	6.2
Attachment 8	DCV Reduction Calculations	6.2
Attachment 9	Additional Green Street Project BMP Conformance Analysis Tables	7
Attachment 10	Hydromodification Exhibits and Calculations	8
Attachment 11	Hydromodification Management Plan	8
Attachment 12	BMP Exhibit	9
Attachment 13	Additional Educational Material	11
Attachment 14	Additional BMP Inspection and Maintenance Responsibility Tables	12.1
Attachment 15	Operations and Maintenance Plan	12.2
Attachment 16	BMP Inspection Record	14
Attachment 17	Conceptual Hydrology Report	

Attachment 1

Preliminary Infiltration Investigation Report



GEOCON

GEOTECHNICAL INVESTIGATION

ORANGE COUNTY YOUTH TRANSITION CENTER
PROJECT (OC YTC)
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

May 21, 2024
PROJECT NO. W1857-88-01

PREPARED FOR:
Balfour Beatty Construction
San Diego, California

Project No. W1857-88-01
May 21, 2024

Balfour Beatty Construction, LLC
13530 Evening Creek Drive North, Suite 270
San Diego, CA 92128

Subject: GEOTECHNICAL INVESTIGATION
ORANGE COUNTY YOUTH TRANSITION CENTER PROJECT (OC YTC)
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

Ladies and Gentlemen:

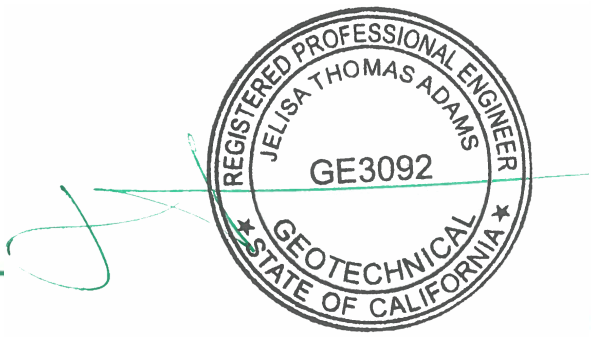
In accordance with your authorization of our proposal dated November 17, 2023, we have performed a geotechnical investigation for the proposed Orange County Youth Transition Center project (OC YTC) located at 331 The City Drive South in the City of Orange, California. The accompanying report presents the findings of our study and our conclusions and recommendations pertaining to the geotechnical aspects of proposed design and construction. Based on the results of our investigation, it is our opinion that the project can be developed as proposed, provided the recommendations of this report are followed and implemented during design and construction.

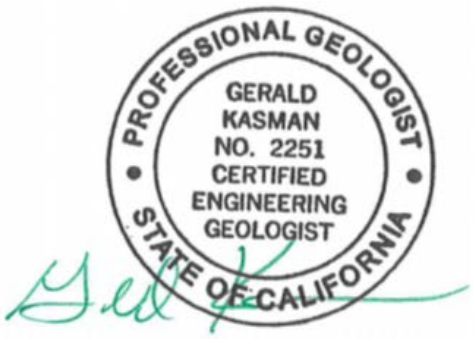
If you have any questions regarding this report, or if we may be of further service, please contact the undersigned.

Very truly yours,

GEOCON WEST, INC.







Andrew Sover
PE 92879

Jelisa Thoms Adams
GE 3092

Gerald A. Kasman
CEG 2251

(email) Addressee

TABLE OF CONTENTS

1. PURPOSE AND SCOPE 1
2. SITE AND PROJECT DESCRIPTION 2
3. GEOLOGIC SETTING 3
4. SOIL AND GEOLOGIC CONDITIONS 3
   4.1 Artificial Fill 3
   4.2 Young Alluvium 3
5. GROUNDWATER 4
6. GEOLOGIC HAZARDS 4
   6.1 Surface Fault Rupture 4
   6.2 Seismicity 5
   6.3 Seismic Design Criteria 6
   6.4 Liquefaction Potential 8
   6.5 Seismically-Induced Settlement 10
   6.6 Slope Stability 10
   6.7 Earthquake-Induced Flooding 10
   6.8 Tsunamis, Seiches, and Flooding 11
   6.9 Oil Fields & Methane Potential 11
   6.10 Subsidence 11
7. CONCLUSIONS AND RECOMMENDATIONS 12
   7.1 General 12
   7.2 Soil and Excavation Characteristics 15
   7.3 Minimum Resistivity, pH, and Water-Soluble Sulfate 16
   7.4 Grading 17
   7.5 Shrinkage 21
   7.6 Foundation Design – General 21
   7.7 Mat Foundation Design 22
   7.8 Conventional Foundation Design 23
   7.9 Miscellaneous Foundations 25
   7.10 Temporary Modular Classrooms Foundation Design 26
   7.11 Lateral Design 26
   7.12 Concrete Slabs-on-Grade 27
   7.13 Preliminary Pavement Recommendations 28
   7.14 Temporary Excavations 30
   7.15 Slot Cutting 31
   7.16 Stormwater Infiltration 32
   7.17 Surface Drainage 33
   7.18 Plan Review 34

LIMITATIONS AND UNIFORMITY OF CONDITIONS

LIST OF REFERENCES

TABLE OF CONTENTS (CONTINUED)

MAPS AND ILLUSTRATIONS
- Figure 1, Vicinity Map
- Figure 2, Site Plan
- Figure 3, Regional Fault Map
- Figure 4, Regional Seismicity Map
- Figures 5 through 7, Correlation of Boring & CPT N60 Blow Counts
- Figure 8, Overall Vertical Settlements – Design Earthquake, Liquefaction
- Figure 9, Overall Vertical Settlements – Maximum Considered Earthquake, Liquefaction
- Figure 10, Overall Vertical Settlements – Design Earthquake, Dry Sands
- Figure 11, Overall Vertical Settlements – Maximum Considered Earthquake, Dry Sands
- Figure 12, Slot-Cut Calculation
- Figures 13 and 14, Percolation Test Results

APPENDIX A
- FIELD INVESTIGATION
- Figures A1 through A15, Boring Logs
- Figures A16 through A17, CPT Logs

APPENDIX B
- LABORATORY TESTING

MARCH 2024 SITE EXPLORATION
- Figures B1 through B4, Direct Shear Test Results
- Figures B5 through B18, Consolidation Test Results
- Figures B19 through B21, Grain Size Analysis Test Results
- Figures B22 through B23, Atterberg Limits Test Results
- Figures B24 through B26, Compaction Test Results
- Figures B27 through B29, Expansion Index Test Results
- Figure B30, Corrosivity Test Results

MAY 2024 SITE EXPLORATION
- Figure B31, Direct Shear Test Results
- Figures B32 through B35, Consolidation Test Results
- Figure B36, Compaction Test Results
- Figure B37, Expansion Index Test Results
- Figure B38, Corrosivity Test Results

APPENDIX C
- CPT ANALYSIS OF LIQUEFACTION POTENTIAL

GEOTECHNICAL INVESTIGATION

1. PURPOSE AND SCOPE

This report presents the results of a geotechnical investigation for the proposed Orange County Youth Transition Center (YTC) project located at 331 The City Drive South, in the City of Orange, California (see Vicinity Map, Figure 1). The purpose of the investigation was to evaluate subsurface soil and geologic conditions underlying the site and, based on conditions encountered, to provide conclusions and recommendations pertaining to the geotechnical aspects of proposed design and construction.

The scope of this investigation included a site reconnaissance, field exploration, laboratory testing, engineering analysis, and the preparation of this report. The site was explored between February 7 and 13, 2024, by excavating eight 8-inch-diameter borings using a truck-mounted hollow-stem auger drilling machine and a limited access drilling machine to depths between 5 and 63.5 feet beneath the ground surface. Additionally, five borings were excavated using 3-inch hand augers to depths between 15 and 16½ feet beneath the ground surface. Percolation testing was performed in two borings to determine the infiltration rate of site soils. Three Cone Penetrometer Tests (CPTs) were advanced on February 12, 2024, to approximate depths of 63 to 100 feet below the ground surface using a truck-mounted 30-ton CPT rig. Additional site exploration was performed on May 2, 2024, by excavating two 8-inch diameter borings using a limited access drilling machine to depths of approximately 20.5 feet below the ground surface. The approximate locations of the exploratory borings and CPT soundings are depicted on the Site Plan (see Figure 2). A detailed discussion of the field investigation, including boring logs and CPT soundings, are presented in Appendix A.

Laboratory tests were performed on selected soil samples obtained during the investigation to determine pertinent physical and chemical soil properties. Appendix B presents a summary of the laboratory test results.

The recommendations presented herein are based on analysis of the data obtained during the investigation and our experience with similar soil and geologic conditions. References reviewed to prepare this report are provided in the *List of References* section.

If project details vary significantly from those described herein, Geocon should be contacted to determine the necessity for review and possible revision of this report.

2. SITE AND PROJECT DESCRIPTION

The subject site is located at 331 The City Drive South in the City of Orange, California. The site is occupied by a youth detention center comprised of one- to two-story dormitories and classrooms, a multipurpose rehabilitation center, and grass fields. The approximate boundary of the area of proposed construction is shown on the Site Plan (see Figure 2). The site is bounded by Service Way South to the north, by Sidwell Way to the east, Justice Center Way to the south, and by the Lamoreaux Justice Center to the west. The site is relatively level and surface water drainage at the site appears to flow to the site drains.

Based on the information provided by the Client, it is our understanding that the proposed project consists of approximately 94,300 gross square feet of new building area and includes site access, new parking areas, outdoor recreation and landscape development and connections to existing Juvenile Hall systems and infrastructure. To create a clear area for construction of new facilities, the project includes demolition of several occupied and unoccupied buildings, perimeter security fencing, site amenities and landscaping. The proposed structures are anticipated to be one- to two-story and constructed at or near present grade. It is anticipated that both masonry and wood framed construction will be used. Temporary modular classrooms will also be constructed to facilitate the project. The existing site conditions are depicted on the Site Plan (see Figure 2). Plans for the proposed project are still being developed and were not available for inclusion in this report.

Based on the preliminary nature of the design at this time, wall and column loads were not available. It is anticipated that column loads for the proposed structures will be up to 20 kips, and wall loads will be up to 2 kips per linear foot.

Once the design phase and foundation loading configuration proceeds to a more finalized plan, the recommendations within this report should be reviewed and revised, if necessary. Any changes in the design, location or elevation of any structure, as outlined in this report, should be reviewed by this office. Geocon should be contacted to determine the necessity for review and possible revision of this report.

3. GEOLOGIC SETTING

The subject site is located on the south-central portion of the Orange County Coastal Plain, a relatively flat-lying alluviated surface with an average slope of less than 20 feet per mile. The lowland surface is bounded by hills and mountains on the north and east, and by the Pacific Ocean to the south and southwest. Prominent structural features within the Orange County Coastal Plain include the central lowland plain, the northwest trending line of low hills and mesas underlain by the Newport-Inglewood Fault Zone along the coast (Newport Mesa, Huntington Beach Mesa, Bolsa Chica Mesa, and Landing Hill), and the San Joaquin Hills to the southeast.

4. SOIL AND GEOLOGIC CONDITIONS

Based on published geologic maps of the area, the site is underlain by artificial fill and Holocene age young alluvial fan deposits that consist of sand and silt, with lesser amounts of clay (California Geological Survey, 2012). Detailed stratigraphic profiles of the materials encountered at the site are provided on the boring logs and CPT soundings in Appendix A.

4.1 Artificial Fill

Artificial fill was encountered in our explorations to a maximum depth of 3½ feet below existing ground surface. The artificial fill generally consists of dark brown silty sand and sandy silt that can be characterized as moist and loose to medium dense or firm. The fill is likely the result of past grading or construction activities at the site. Deeper fill may exist between excavations and in other portions of the site that were not directly explored.

4.2 Young Alluvium

Holocene age alluvial fan deposits were encountered beneath the fill. The alluvium generally consists of brown to yellowish brown, or grayish brown silty sand and poorly graded sand with minor interbeds of sandy silt and sandy clay and various amounts of fine- to coarse-gravel. The alluvial soils are characterized as poorly- to well-graded sand, slightly moist to wet and soft to firm or loose to dense.

5. GROUNDWATER

Review of the Seismic Hazard Zone Report for the Anaheim Quadrangle (California Division of Mines and Geology [CDMG], 1998, revised 2001) indicates that the historically highest groundwater level in the area is between 30 and 40 feet beneath the existing ground surface. Groundwater information presented in this document is generated from data collected in the early 1900's to the late 1990s.

Groundwater was encountered in our borings at a depth of approximately 54 feet below the existing ground surface. The groundwater measurements were performed in a manner that is typical of geotechnical exploration and should not be interpreted as representing a fully equalized water level.

Based the reported historic high groundwater levels in the immediate area (CDMG, 2001), and the depth of proposed construction, static groundwater is neither expected to be encountered during construction, nor have a detrimental effect on the project. However, it is not uncommon for groundwater levels to vary seasonally or for groundwater seepage conditions to develop where none previously existed (especially in impermeable fine-grained soils which are heavily irrigated or after seasonal rainfall), groundwater seepage levels encountered during construction may be actually higher than those encountered during our investigation. In addition, recent requirements for storm water infiltration could result in shallower seepage conditions in the region. Proper surface drainage of irrigation and precipitation will be critical for future performance of the project. Recommendations for drainage are provided in the Surface Drainage section of this report (see Section 7.16).

6. GEOLOGIC HAZARDS

6.1 Surface Fault Rupture

The numerous faults in Southern California include Holocene-active, pre-Holocene, and inactive faults. The criteria for these major groups are based on criteria developed by the California Geological Survey (CGS, formerly known as CDMG) for the Alquist-Priolo Earthquake Fault Zone Program (CGS, 2018). By definition, a Holocene-active fault is one that has had surface displacement within Holocene time (about the last 11,700 years). A pre-Holocene fault has demonstrated surface displacement during Quaternary time (approximately the last 1.6 million years) but has had no known Holocene movement. Faults that have not moved in the last 1.6 million years are considered inactive.

The site is not within a state-designated Alquist-Priolo Earthquake Fault Zone (CGS, 2024a; 2024b) for surface fault rupture hazards. No Holocene-active or pre-Holocene faults with the potential for surface fault rupture are known to pass directly beneath the site. Therefore, the potential for surface rupture due to faulting occurring beneath the site during the design life of the proposed development is considered low. However, the site is located in the seismically active Southern California region, and could be subjected to moderate to strong ground shaking in the event of an earthquake on one of the many active Southern California faults. The faults in the vicinity of the site are shown in Figure 3, Regional Fault Map.

The closest surface trace of a Holocene-active fault to the site is the Newport-Inglewood Fault Zone located approximately 9.7 miles to the southwest. Other nearby active faults are the Whittier Fault, the Chino Fault, the Elsinore Fault, and the Palos Verdes Fault Zone (offshore segment) located approximately 10 miles to the north-northeast, 15 miles to the northeast, 16 miles to the northeast, and 19 miles to the southwest, respectively (USGS, 2006; Ziony and Jones, 1989). The active San Andreas Fault Zone is located approximately 41 miles northeast of the site (USGS, 2006; Ziony and Jones, 1989).

Several buried thrust faults, commonly referred to as blind thrusts, underlie the Southern California area at depth. These faults are not exposed at the ground surface and are typically identified at depths greater than 3.0 kilometers. The October 1, 1987 M_w 5.9 Whittier Narrows earthquake and the January 17, 1994 M_w 6.7 Northridge earthquake were a result of movement on the Puente Hills Blind Thrust and the Northridge Thrust, respectively. The Puente Hills Blind Thrust underlies the site at depth. These thrust faults and others in the Los Angeles area are not exposed at the surface and do not present a potential surface fault rupture hazard at the site; however, these deep thrust faults are considered active features capable of generating future earthquakes that could result in moderate to significant ground shaking at the site.

6.2 Seismicity

As with all of Southern California, the site has experienced historic earthquakes from various regional faults. The seismicity of the region surrounding the site was formulated based on research of an electronic database of earthquake data. The epicenters of recorded earthquakes with magnitudes equal to or greater than 5.0 in the site vicinity are depicted on Figure 4, Regional Seismicity Map. A partial list of moderate to major magnitude earthquakes that have occurred in the Southern California area within the last 100 years is included in the table on the following page.

LIST OF HISTORIC EARTHQUAKES

Earthquake (Oldest to Youngest)	Date of Earthquake	Magnitude	Distance to Epicenter (Miles)	Direction to Epicenter
Long Beach	March 10, 1933	6.4	12	SSW
Tehachapi	July 21, 1952	7.5	106	NW
San Fernando	February 9, 1971	6.6	52	NW
Whittier Narrows	October 1, 1987	5.9	22	NW
Sierra Madre	June 28, 1991	5.8	34	NNW
Landers	June 28, 1992	7.3	88	ENE
Big Bear	June 28, 1992	6.4	67	ENE
Northridge	January 17, 1994	6.7	47	NW
Hector Mine	October 16, 1999	7.1	108	ENE

The site could be subjected to strong ground shaking in the event of an earthquake. However, this hazard is common in Southern California and the effects of ground shaking can be minimized if the proposed structures are designed and constructed in conformance with current building codes and engineering practices.

6.3 Seismic Design Criteria

The following table summarizes the site-specific design criteria obtained from the 2022 California Building Code (CBC; Based on the 2018 International Building Code [IBC] and ASCE 7-16), Chapter 16 Structural Design, Section 1613 Earthquake Loads. The data was calculated using the online application U.S. Seismic Design Maps, provided by the Structural Engineers Association of California (SEAOC). The short spectral response uses a period of 0.2 second. We evaluated the Site Class based on the discussion in Section 1613.2.2 of the 2022 CBC and Table 20.3-1 of ASCE 7-16. The values presented on the following page are for the risk-targeted maximum considered earthquake (MCE_R).

Although there are liquefiable soils underlying the site, we expect the proposed structures will possesses fundamental periods of less than 0.5 seconds; therefore, use of Site Class F is not considered necessary and a site response analysis is not anticipated to be required in accordance with ASCE 7-16, Section 20.3.1.

2022 CBC SEISMIC DESIGN PARAMETERS

Parameter	Value	2022 CBC Reference
Site Class	D	Section 1613.2.2
MCE_R Ground Motion Spectral Response Acceleration – Class B (short), S_S	1.363g	Figure 1613.2.1(1)
MCE_R Ground Motion Spectral Response Acceleration – Class B (1 sec), S_1	0.484g	Figure 1613.2.1(2)
Site Coefficient, F_A	1	Table 1613.2.3(1)
Site Coefficient, F_V	1.816	Table 1613.2.3(2)
Site Class Modified MCE_R Spectral Response Acceleration (short), S_{MS}	1.363g	Section 1613.2.3 (Eqn 16-20)
Site Class Modified MCE_R Spectral Response Acceleration – (1 sec), S_{M1}	0.879g*	Section 1613.2.3 (Eqn 16-21)
5% Damped Design Spectral Response Acceleration (short), S_{DS}	0.909g	Section 1613.2.4 (Eqn 16-22)
5% Damped Design Spectral Response Acceleration (1 sec), S_{D1}	0.586g*	Section 1613.2.4 (Eqn 16-23)

*Per Supplement 3 of ASCE 7-16, a ground motion hazard analysis (GMHA) shall be performed for projects on Site Class "D" sites with 1-second spectral acceleration (S1) greater than or equal to 0.2g, which is true for this site. However, Supplement 3 of ASCE 7-16 provides an exception stating that that the GMHA may be waived provided that the parameter SM1 is increased by 50% for all applications of SM1. The values for parameters SM1 and SD1 presented above have not been increased in accordance with Supplement 3 of ASCE 7-16.

The table below presents the mapped maximum considered geometric mean (MCE_G) seismic design parameters for projects located in Seismic Design Categories of D through F in accordance with ASCE 7-16.

ASCE 7-16 PEAK GROUND ACCELERATION

Parameter	Value	ASCE 7-16 Reference
Mapped MCEG Peak Ground Acceleration, PGA	0.575g	Figure 22-9
Site Coefficient, FPGA	1.1	Table 11.8-1
Site Class Modified MCEG Peak Ground Acceleration, PGAM	0.633g	Section 11.8.3 (Eqn 11.8-1)

Deaggregation of the MCE peak ground acceleration was performed using the USGS online Unified Hazard Tool, 2014 Conterminous U.S. Dynamic edition (v4.2.0). The result of the deaggregation analysis indicates that the mean earthquake contributing to the MCE peak ground acceleration is characterized as a 6.65 magnitude event occurring at a hypocentral distance of 13.63 kilometers from the site.

Deaggregation was also performed for the Design Earthquake (DE) peak ground acceleration, and the result of the analysis indicates that the modal earthquake contributing to the DE peak ground acceleration is characterized as a 6.12 magnitude occurring at a hypocentral distance of 10.68 kilometers from the site.

Conformance to the criteria in the above tables for seismic design does not constitute any kind of guarantee or assurance that significant structural damage or ground failure will not occur if a large earthquake occurs. The primary goal of seismic design is to protect life, not to avoid all damage, since such design may be economically prohibitive.

6.4 Liquefaction Potential

Liquefaction is a phenomenon in which loose, saturated, relatively cohesionless soil deposits lose shear strength during strong ground motions. Primary factors controlling liquefaction include intensity and duration of ground motion, gradation characteristics of the subsurface soils, in-situ stress conditions, and the depth to groundwater. Liquefaction is typified by a loss of shear strength in the liquefied layers due to rapid increases in pore water pressure generated by earthquake accelerations.

The current standard of practice, as outlined in the "Recommended Procedures for Implementation of DMG Special Publication 117, Guidelines for Analyzing and Mitigating Liquefaction in California" and "Special Publication 117A, Guidelines for Evaluating and Mitigating Seismic Hazards in California" requires liquefaction analysis to a depth of 50 feet below the lowest portion of the proposed structure. Liquefaction typically occurs in areas where the soils below the water table are composed of poorly consolidated, fine- to medium-grained, primarily sandy soil. In addition to the requisite soil conditions, the ground acceleration and duration of the earthquake must also be of a sufficient level to induce liquefaction.

The State of California Seismic Hazard Zone Map for the Anaheim Quadrangle (CDMG, 1998) indicates that the site is located within an area identified as a zone of required investigation for liquefaction. The historic high groundwater level in the vicinity of the site is reported to be approximately 30 to 40 feet beneath the ground surface (CDMG, 1997, revised 2001). Groundwater was encountered in the current field explorations at a depth of approximately 54 feet below the existing ground surface.

Liquefaction analyses of the CPT soundings were performed using the program CLiq (Version 3.5.2.17). This program utilizes the 2001 NCEER method of analysis. This semi-empirical method is based on correlations with the data collected from the CPT soundings.

Prior to analysis, the Standard Penetration Test (SPT) blow counts from borings E, F, and I were compared with the blow counts estimated from CPTs 1, 2, and 3 based on the proximity of these explorations. SPTs were performed in the borings at intervals of approximately 5 feet. In order to supplement the SPT blow count data, the California Modified Sampler blow count data were converted to equivalent SPT blow counts based on a correlation factor of 0.55 (Rogers, 2006). The field collected blow counts were corrected for hammer efficiency to N60 blow count values. The boring N60 values were compared with the N60 values generated by the program CPet-IT (Version 3.9.1.3). The comparisons are shown as Figures 5 through 7. It is our opinion that the boring and CPT N60 values show a reasonable correlation and that analysis of the liquefaction potential may be based on the CPT data.

The liquefaction analysis was performed for a Design Earthquake level by using a historic high groundwater table of 30 feet below the ground surface, a magnitude 6.12 earthquake, and a peak horizontal acceleration of 0.422g (⅔PGAM). The enclosed liquefaction analyses, included herein for CPTs 1 through 3, indicate that the alluvial soils below the historic high groundwater could be prone to up to 1.1 inches of liquefaction induced settlement during Design Earthquake ground motion. A summary of the anticipated liquefaction induced settlements is provided as Figure 8; calculations and output from CLiq are provided as Appendix C.

It is our understanding that the intent of the Building Code is to maintain “Life Safety” during Maximum Considered Earthquake level events. Therefore, additional analysis was performed to evaluate the potential for liquefaction during a MCE event. The structural engineer should evaluate the proposed structure for the anticipated MCE liquefaction induced settlements and verify that anticipated deformations would not cause the foundation system to lose the ability to support the gravity loads and/or cause collapse of the structure.

The liquefaction analysis was also performed for the Maximum Considered Earthquake level by using a historic high groundwater table of 30 feet below the ground surface, a magnitude 6.65 earthquake, and a peak horizontal acceleration of 0.633g (PGAM). The enclosed liquefaction analyses, included herein for CPTs 1 through 3, indicate that the alluvial soils below the historic high groundwater could be prone to up to 2.5 inches of liquefaction induced settlement during Maximum Considered Earthquake ground motion. A summary of the anticipated liquefaction induced settlements is provided as Figure 9; calculations and output from CLiq are provided as Appendix C.

6.5 Seismically-Induced Settlement

Dynamic compaction of dry and loose sands may occur during a major earthquake. Typically, settlements occur in thick beds of such soils. Analysis of dry seismic induced settlements were performed using the program CLiq (Version 3.0.3.2). This program utilizes the Robertson and Shao, 2010, method of analysis.

The results of the seismically induced dry settlement calculations for CPTs 1 through 3 indicate that the soil above the historic high groundwater level of 30 feet could be prone to less than ½ inch of settlement as a result of the Design Earthquake peak ground acceleration (⅔PGAM). A summary of the estimated dry seismic settlements during a Design Level Earthquake is provided as Figure 10.

The results of the seismically induced dry settlement calculations for CPTs 1 through 3 indicate that the soil above the historic high groundwater level of 30 feet could be prone up to ⅔ inch of settlement as a result of the Design Earthquake peak ground acceleration (⅔PGAM). A summary of the estimated dry seismic settlements during a Design Level Earthquake is provided as Figure 11.

Calculations and output from CLiq are provided as Appendix C.

6.6 Slope Stability

The site and adjacent sites are relatively flat to sloping gently to the southwest. Based on a review of the City of Orange General Plan (2010) and the Orange County Safety Element (2004), the site is not located within an area identified as having a potential for slope stability hazards. Also, the site is not within an area identified as having a potential for seismic slope instability (CDMG, 1998). There are no known landslides near the site, nor is the site in the path of any known or potential landslides (USGS, 20223a). Therefore, the potential for slope stability hazards to adversely affect the proposed development is considered low.

6.7 Earthquake-Induced Flooding

Earthquake-induced flooding is inundation caused by failure of dams or other water-retaining structures due to earthquakes. The Orange County Safety Element (2004) indicates that the site is located within the Prado Dam and Santiago Reservoir inundation area. However, these reservoirs, as well as others in California, are continually monitored by various governmental agencies (such as the State of California Division of Safety of Dams and the U.S. Army Corps of Engineers) to guard against the threat of dam failure. Current design, construction practices, and ongoing programs of review, modification, or total reconstruction of existing dams are intended to ensure that all dams are capable of withstanding the maximum considered earthquake (MCE) for the site. Therefore, the potential for inundation at the site as a result of an earthquake-induced dam failure is considered low.

6.8 Tsunamis, Seiches, and Flooding

The site is not located within a coastal area. Therefore, tsunamis are not considered a significant hazard at the site.

Seiches are large waves generated in enclosed bodies of water in response to ground shaking. No major water-retaining structures are located immediately up gradient from the project site. Therefore, flooding resulting from a seismically induced seiche is considered unlikely.

According to the City of Orange General Plan (2010) and the Orange County Safety Element (2004), the site is not within a 100-year or 500-year flood zone. No base flood elevation was indicted by FEMA (2021).

6.9 Oil Fields & Methane Potential

Based on a review of the California Geologic Energy Management Division (CalGEM) Well Finder Website, the site is not located within an oil field and oil or gas wells are not documented within ½-mile of the site (CalGEM, 2024). However, due to the voluntary nature of record reporting by the oil well drilling companies, wells may be improperly located or not shown on the location map and undocumented wells could be encountered during construction. Any wells encountered during construction will need to be properly abandoned in accordance with the current requirements of the CalGEM.

Since the site is not located within the boundaries of a known oil field, the potential for the presence of methane or other volatile gases at the site is considered low. However, should it be determined that a methane study is required for the proposed development it is recommended that a qualified methane consultant be retained to perform the study and provide mitigation measures as necessary.

6.10 Subsidence

Subsidence occurs when a large portion of land is displaced vertically, usually due to the withdrawal of groundwater, oil, or natural gas. Soils that are particularly subject to subsidence include those with high silt or clay content. The site is located within an area of known ground subsidence (USGS, 2024). Subsidence related to groundwater pumping commonly occurs in such small magnitudes and over such large areas that it is generally imperceptible at an individual locality. Accordingly, it affects only regionally extensive structures sensitive to slight elevation changes, such as canals and pipelines. The rate of elevation change is usually uniform over a large enough area that it does not result in differential settlements that would cause damage to individual buildings. Therefore, the potential for subsidence to adversely impact the proposed project is considered low.

7. CONCLUSIONS AND RECOMMENDATIONS

7.1 General

7.1.1 It is our opinion that neither soil nor geologic conditions were encountered during the investigation that would preclude the construction of the proposed project provided the recommendations presented herein are followed and implemented during design and construction.

7.1.2 Up to 3½ feet of existing artificial fill was encountered during the site investigation. The existing fill encountered is believed to be the result of past grading and construction activities at the site. Deeper fill may exist in other areas of the site that were not directly explored. Future demolition of the existing structures which occupy the site will likely disturb the upper few feet of soil below those existing improvements. It is our opinion that the existing fill, in its present condition, is not suitable for direct support of proposed foundations or slabs. If needed, the existing fill and site soils are suitable for re-use as engineered fill provided the recommendations in the *Grading* section of this report are followed (see Section 7.4).

7.1.3 The enclosed liquefaction analysis indicates that the site soils could be susceptible to approximately 1¼ inches of total settlement as a result of the Design Earthquake peak ground acceleration (⅔PGA_M), and up to 3 inches of total settlement as a result of the MCE peak ground acceleration (PGA_M). These values exceed the allowable limits of differential settlement for conventional shallow foundations set forth in Chapter 12 of ASCE 7-16. The grading and foundation design recommendations presented herein are intended to reduce the effects of settlement on proposed improvements.

7.1.4 Based on these considerations, the foundation system for the proposed structures must be able to provide sufficient support and minimize the effects of differential settlement resulting from a liquefaction event. One design option is to support proposed buildings on a reinforced mat foundation system. A mat foundation system is more capable of minimizing the effects of differential settlement and has sufficient rigidity to allow the structure to behave more uniformly. Recommendations for the design of a mat foundation system are provided in Section 7.7.

7.1.5 Alternatively, proposed structures may be supported on a conventional foundation system with interconnecting foundation ties. The foundation system should be underlain by a blanket of newly placed engineered fill. Recommendations for the design of a conventional foundation system are provided in Section 7.8.

7.1.6 As a minimum, it is recommended that existing earth materials in the building footprint areas be excavated and properly compacted to a depth of at least 5 feet below the existing ground surface. This depth is based on the existing grades at the time of our site exploration. Deeper excavations should be conducted as necessary to remove existing artificial fill or soft alluvial soil at the direction of the Geotechnical Engineer (a representative of Geocon). Proposed building foundations should be underlain by a minimum of 3 feet of newly placed engineered fill. It is recommended that the grading contractor verify the depth of all building foundations prior to commencement of site grading activities in order to correctly determine the required grading overexcavations for foundations. Where feasible, the excavation should extend laterally a minimum distance of 3 feet beyond the building footprint area, including building appurtenances, or for a distance equal to the depth of fill below the foundation, whichever is greater. The limits of existing fill and/or soft alluvial soil removal will be verified by the Geocon representative during site grading activities. Recommendations for earthwork are provided in the *Grading* section of this report (see Section 7.4).

7.1.7 It should be noted that implementation of the recommendations presented herein is not intended to completely prevent damage to the structure during the occurrence of strong ground shaking as a result of nearby earthquakes. It is intended that the structure be designed in such a way that the amount of damage incurred as a result of strong ground shaking be reduced. Re-leveling of the foundation system and repair of utilities could be necessary following a strong seismic event that triggers liquefaction.

7.1.8 Improvements which are not supported on soil modification, such as walkways, paving, and utilities, may still be subject to seismic and/or static settlement. The client should consider the flexibility of the products and pavements being installed. It is recommended that all utilities traversing through existing site soils utilize flexible connections in order to reduce the damage to underground installations caused by potential soil movements.

7.1.9 Based on our observations during site exploration, areas of loose or soft and overly moist soils may be encountered during grading operations. These conditions may change seasonally. If the soils are more than 3 percent above the optimum moisture content at the time of construction the soils will likely require some spreading and drying activities in order to achieve proper compaction.

7.1.10 If loose or soft and overly moist soils are exposed in excavation bottoms, these soils could be subject to excessive pumping. Operation of rubber tire equipment on the subgrade soils may cause excessive disturbance of the soils. Excavation activities to establish the finished subgrade elevation must be conducted carefully and methodically to avoid excessive disturbance to the subgrade. Stabilization of areas of the excavation bottom may be required in order to provide a firm working surface upon which heavy equipment can operate. Recommendations for bottom stabilization and earthwork are provided in the *Grading* section of this report (see Section 7.4).

7.1.11 It is anticipated that stable excavations for the recommended grading associated with the proposed structure can be achieved with sloping measures. However, if excavations in close proximity to an adjacent property line and/or structure are required, special excavation measures may be necessary in order to maintain lateral support of offsite improvements. Excavation recommendations are provided in the *Temporary Excavations* section of this report (Section 7.13).

7.1.12 Where new paving is to be placed, it is recommended that all existing fill and soft alluvium be excavated and properly compacted for paving support. The client should be aware that excavation and compaction of all existing fill and soft alluvium in the area of new paving is not required, however, paving constructed over existing uncertified fill or unsuitable soils may experience increased settlement and/or cracking, and may therefore have a shorter design life and increased maintenance costs. As a minimum, the upper twelve inches of soil should be scarified and properly compacted for paving support. Paving recommendations are provided in the *Preliminary Pavement Recommendations* section of this report (see Section 7.12).

7.1.13 Foundations for small outlying structures, such as block walls up to 6 feet high, planter walls or trash enclosures, which will not be tied-in to the proposed structure, may be supported on conventional foundations bearing on a minimum of 12 inches of newly placed engineered fill which extends laterally at least 12 inches beyond the foundation area. Where excavation and proper compaction cannot be performed, foundations may derive support directly in the undisturbed alluvial soils and should be deepened as necessary to maintain a minimum of 12-inch embedment into recommended bearing materials. The depth to competent alluvium should be field verified at each location. If the soils exposed in the excavation bottom are soft or loose, compaction of the soft soils will be required prior to placing steel or concrete. Compaction of the foundation excavation bottom is typically accomplished with a compaction wheel or mechanical whacker and must be observed and approved in writing by a Geocon representative.

7.1.14 Based on the results of percolation testing performed at the site, a stormwater infiltration system is considered feasible for this project. Recommendations for infiltration are provided in the Stormwater Infiltration section of this report (see Section 7.15).

7.1.15 Once the design and foundation loading configuration for the proposed structures proceeds to a more finalized plan, the recommendations within this report should be reviewed and revised, if necessary. Based on the final foundation loading configurations, the potential for settlement should be re-evaluated by this office.

7.1.16 Any changes in the design, location or elevation, as outlined in this report, should be reviewed by this office. Geocon should be contacted to determine the necessity for review and possible revision of this report.

7.1.17 The most recent ASTM standards apply to this project and must be utilized, even if older ASTM standards are indicated in this report.

7.2 Soil and Excavation Characteristics

7.2.1 The in-situ soils can be excavated with moderate effort using conventional excavation equipment. Caving should be anticipated in unshored excavations, especially where granular soils are present.

7.2.2 It is the responsibility of the contractor to ensure that all excavations and trenches are properly shored and maintained in accordance with applicable OSHA rules and regulations to maintain safety and maintain the stability of existing adjacent improvements.

7.2.3 All onsite excavations must be conducted in such a manner that potential surcharges from existing structures, construction equipment, and vehicle loads are resisted. The surcharge area may be defined by a 1:1 projection down and away from the bottom of an existing foundation or vehicle load. Penetrations below this 1:1 projection will require special excavation measures such as sloping or shoring. Excavation recommendations are provided in the *Temporary Excavations* section of this report (see Section 7.13).

7.2.4 The upper five feet of existing site soils encountered during the investigation are considered to have a "very low" expansive potential (EI = 0 to 2) and are classified as "non-expansive" in accordance with the 2022 California Building Code (CBC) Section 1803.5.3. The recommendations presented herein assume that foundations and slabs will derive support in these materials.

7.3 Minimum Resistivity, pH, and Water-Soluble Sulfate

7.3.1 Potential of Hydrogen (pH) and resistivity testing as well as chloride content testing were performed on representative samples of soil to generally evaluate the corrosion potential to surface utilities. The tests were performed in accordance with California Test Method Nos. 643 and 422 and indicate that the soils are considered "moderately corrosive" with respect to corrosion of buried ferrous metals on site. The results are presented in Appendix B (Figures B30 and B38) and should be considered for design of underground structures.

7.3.2 Laboratory tests were performed on representative samples of the on-site soil to measure the percentage of water-soluble sulfate content. Results from the laboratory water-soluble sulfate tests are presented in Appendix B (Figures B30 and B38) and indicate that the on-site soil possess a sulfate exposure class of "S0" to concrete structures as defined by 2022 CBC Section 1904 and ACI 318 Chapter 19.

7.3.3 Geocon West, Inc. does not practice in the field of corrosion engineering and mitigation. If corrosion sensitive improvements are planned, it is recommended that a corrosion engineer be retained to evaluate corrosion test results and incorporate the necessary precautions to avoid premature corrosion of buried metal pipes and concrete structures in direct contact with the soils.

7.4 Grading

7.4.1 A preconstruction conference should be held at the site prior to the beginning of excavation operations with the owner, contractor, civil engineer, geotechnical engineer, and building official in attendance. Special soil handling requirements can be discussed at that time.

7.4.2 Earthwork should be observed, and compacted fill tested by representatives of Geocon West, Inc. The existing fill and alluvial soil encountered during exploration are suitable for re-use as an engineered fill, provided any encountered oversize material (greater than 6 inches) and any encountered deleterious debris are removed.

7.4.3 Grading should commence with the removal of all existing vegetation and existing improvements from the area to be graded. Deleterious debris such as wood and root structures should be exported from the site and should not be mixed with the fill soils. Asphalt and concrete should not be mixed with the fill soils unless approved by the Geotechnical Engineer. All existing underground improvements planned for removal should be completely excavated and the resulting depressions properly backfilled in accordance with the procedures described herein. Once a clean excavation bottom has been established it must be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon West, Inc.).

7.4.4 As a minimum, it is recommended that the upper 5 feet of existing earth materials within proposed permanent structure footprint areas be excavated and properly compacted for foundation and slab support. This depth is based on the existing grades at the time of our site exploration. Deeper excavations should be conducted as necessary to remove any encountered fill or soft soil as necessary at the direction of the Geotechnical Engineer (a representative of Geocon). Proposed foundations should be underlain by a minimum of 3 feet of newly placed engineered fill. It is recommended that the grading contractor verify the depth of all building foundations prior to commencement of site grading activities in order to correctly determine the required grading overexcavations for foundations. The limits of existing fill and/or soft soil removal will be verified by the Geocon representative during site grading activities.

7.4.5 The excavation should extend laterally a minimum distance of 3 feet beyond the building footprint area, including building appurtenances, or a distance equal to the depth of fill below the foundation, whichever is greater. Where the recommended lateral over-excavation cannot be performed, such as adjacent to property lines and/or an existing structure, the lateral component of the foundation design can rely solely on friction between the bottom of the foundation and the underlying subgrade soils. The foundation should not utilize passive pressure unless foundations are bounded by and in direct contact with newly placed engineered fill.

7.4.6 Within the area of the temporary modular classrooms, it is recommended that the upper 2 feet of existing earth materials within proposed structures footprint areas be excavated and properly compacted for foundation and slab support. This depth is based on the existing grades at the time of our site exploration. Deeper excavations should be conducted as necessary to remove any encountered fill or soft soil as necessary at the direction of the Geotechnical Engineer (a representative of Geocon). The excavation should extend laterally a minimum distance of 2 feet beyond the building footprint areas, including building appurtenances, or a distance equal to the depth of fill below the foundation, whichever is greater. The limits of existing fill and/or soft soil removal will be verified by the Geocon representative during site grading activities.

7.4.7 All fill and backfill soils should be placed in horizontal loose layers approximately 6 to 8 inches thick, moisture conditioned to near optimum moisture content, and properly compacted to a minimum 90 percent of the maximum dry density in accordance with ASTM D 1557 (latest edition).

7.4.8 All excavations must be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon).

7.4.9 Based on our observations during site exploration, areas of loose or soft and overly moist soils may be encountered during grading operations. These conditions may change seasonally. If the soils are more than 3 percent above the optimum moisture content at the time of construction the soils will likely require some spreading and drying activities in order to achieve proper compaction.

7.4.10 Prior to placing fill, a stable excavation bottom must be established. In areas where the subgrade is saturated or soft, proper compaction will likely not be possible or achieved in a timely manner without introducing stabilization measures. If subgrade stabilization is required at the excavation bottom, rubber tire equipment should not be allowed in the excavation bottom until it is stabilized or extensive soil disturbance could result. It is suggested that excavation and grading be performed during the summer season to promote moisture control of the soils. In addition, the use of track equipment should be used to minimize disturbance to the soils at the excavation bottom.

7.4.11 Bottom stabilization, if necessary, may be achieved placing a thin lift of 3- to 6-inch-diameter crushed angular rock into the soft excavation bottom. The use of crushed concrete will also be acceptable. The crushed rock should be spread thinly across the excavation bottom and pressed into the soils by track rolling or wheel rolling with heavy equipment. It is very important that voids between the rock fragments are not created so the rock must be thoroughly pressed or blended into the soils. All subgrade soils must be properly compacted and proof-rolled in the presence of the Geotechnical Engineer (a representative of Geocon West, Inc.).

7.4.12 An additional method of subgrade stabilization would be to place a minimum 12 inches thick layer of aggregate base over Tensar InterAx NX850 geogrid or equivalent extruded (nonwoven) geotextile. The Tensar geogrids should be installed taught and should overlap in accordance with the manufacturer's recommendations. Prior to placing the geogrid, excessively soft or wet materials should be removed and the resulting excavation bottom should be free of loose material. Non-vibratory compaction methods should be used for compaction of the base material. The aggregate base should be compacted to a dry density of at least 95 percent of the laboratory maximum density near the optimum moisture. If pumping of the subgrade continues, a thicker layer of aggregate base may be placed. It is very important that subgrade stabilization be performed uniformly across the entire excavation bottom.

7.4.13 It is anticipated that stable excavations for the recommended grading can be achieved with sloping measures. However, if excavations in close proximity to an adjacent property line and/or structure are required, special excavation measures may be necessary in order to maintain lateral support of the existing offsite improvements. Excavation recommendations are provided in the *Temporary Excavations* section of this report (Section 7.13).

7.4.14. Where new paving is to be placed, it is recommended that all existing fill and soft alluvium be excavated and properly compacted for paving support. As a minimum, the upper 12 inches of soil should be scarified, moisture conditioned to near optimum moisture content, and compacted to at least 95 percent relative compaction, as determined by ASTM Test Method D 1557 (latest edition). Paving recommendations are provided in the *Preliminary Pavement Recommendations* section of this report (see Section 7.12).

7.4.15 Although not anticipated for this project, all imported fill shall be observed, tested, and approved by Geocon West, Inc. prior to bringing soil to the site. Import fill should consist of the characteristics presented in the table below.

SUMMARY OF IMPORT FILL RECOMMENDATIONS

Soil Characteristic	Values
Expansion Potential	"Very Low" (Expansion Index of 20 or less)
Particle Size	Maximum Dimension Less Than 6 Inches
	Free of Debris
Corrosivity	Less Detrimental Than Existing Onsite Soils

7.4.16 Foundations for small outlying structures, such as block walls up to 6 feet high, planter walls or trash enclosures, which will not be tied to the proposed building, may be supported on conventional foundations deriving support on a minimum of 12 inches of newly placed engineered fill which extends laterally at least 12 inches beyond the foundation area. Where excavation and proper compaction cannot be performed, foundations may derive support directly in the undisturbed alluvial soils and should be deepened as necessary to maintain a minimum 12-inch embedment into the recommended bearing materials. The depth to competent alluvium should be field verified at each location. If the soils exposed in the excavation bottom are soft or loose, compaction of the soils will be required prior to placing steel or concrete. Compaction of the foundation excavation bottom is typically accomplished with a compaction wheel or mechanical whacker and must be observed and approved by a Geocon representative.

7.4.17 It is recommended that flexible utility connections be utilized for all rigid utilities to reduce or prevent damage to utilities from minor differential movements. Utility trenches should be properly backfilled in accordance with the following requirements. The pipe should be bedded with clean sands (Sand Equivalent greater than 30) to a depth of at least 1 foot over the pipe, and the bedding material must be inspected and approved in writing by the Geotechnical Engineer (a representative of Geocon). The use of gravel is not acceptable unless used in conjunction with filter fabric to prevent the gravel from having direct contact with soil. The remainder of the trench backfill may be derived from onsite soil or approved import soil, compacted as necessary, until the required compaction is obtained. The use of minimum 2-sack slurry as backfill is also acceptable. Prior to placing any bedding materials or pipes, the excavation bottom must be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon).

7.4.18 All trench and foundation excavation bottoms must be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon), prior to placing bedding materials, fill, steel, gravel, or concrete.

7.5 Shrinkage

7.5.1 Shrinkage results when a volume of material removed at one density is compacted to a higher density. A shrinkage factor of between 5 and 15 percent should be anticipated when excavating and compacting the upper site soils to an average relative compaction of 90 percent.

7.5.2 If import soils will be utilized in the building pad, the soils must be placed uniformly and at equal thickness at the direction of the Geotechnical Engineer (a representative of Geocon West, Inc.).

7.6 Foundation Design – General

7.6.1 Proposed foundations that are situated immediately adjacent to the existing foundations should be deepened as necessary to match the depth of the existing foundation to prevent a surcharge on the existing foundation.

7.6.2 Where proposed foundations will be deeper than the existing foundation, the proposed foundation must be designed to resist the surcharge imposed by the existing foundation. The surcharge area may be defined by a 1:1 projection up and away from the bottom of an existing foundation.

7.6.3 Foundation excavations should be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon West, Inc.), prior to the placement of reinforcing steel and concrete to verify that the exposed soil conditions are consistent with those anticipated. If unanticipated soil conditions are encountered, foundation modifications may be required.

7.6.4 This office should be provided a copy of the final construction plans so that the recommendations presented herein could be properly reviewed and revised if necessary.

7.7 Mat Foundation Design

7.7.1 A reinforced concrete mat foundation deriving support in newly placed engineered fill may also be utilized for support the proposed structures. Proposed foundations should be underlain by a minimum of 3 feet of newly placed engineered fill. Foundation excavations should be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon West, Inc.), prior to the placement of reinforcing steel and concrete.

7.7.2 The recommended maximum allowable bearing value for the design of a reinforced concrete mat foundation is 4,000 pounds per square foot (psf). The allowable bearing pressure may be increased by up to one-third for transient loads due to wind or seismic forces.

7.7.3 It is recommended that a modulus of subgrade reaction of 150 pounds per cubic inch (pci) be utilized for the design of the mat foundation bearing in newly placed engineered fill. This value is a unit value for use with a 1-foot square footing. The modulus should be reduced in accordance with the following equation when used with larger foundations:

$$K_R = K\left[\frac{B+1}{2B}\right]^2$$

where: K_R = reduced subgrade modulus
K = unit subgrade modulus
B = foundation width (in feet)

7.7.4 The thickness of and reinforcement for the mat foundation should be designed by the project structural engineer.

7.7.5 The maximum expected static settlement for a structure supported on a mat foundation system deriving support in the recommended bearing materials and designed with a maximum bearing pressure of 4,000 psf is estimated to be less than 1 inch and occur below the heaviest loaded structural element. Settlement of the foundation system is expected to occur on initial application of loading. Differential settlement is not expected to exceed ½ inch between the center and corner of the mat foundation.

7.7.6 Based on seismic considerations, proposed structures supported on a mat foundation system should be designed for a combined static and seismically-induced differential settlement of than 1¼ inches.

7.7.7 Settlement resulting from mat foundation loading depends on the pressure distribution across the mat. Typically, some areas of the mat foundation induce larger stresses in the soil than other areas based on the applied loading. Once the design and foundation loading configurations for the proposed structure proceeds to a more finalized plan, the estimated settlements presented in this report should be reviewed and revised, if necessary. If the final foundation loading configurations are greater than the assumed loading conditions, the potential for settlement should be reevaluated by this office.

7.7.8 For seismic design purposes, a coefficient of friction of 0.35 may be utilized between concrete slab and subgrade soils without a moisture barrier, and 0.15 for slabs underlain by a moisture barrier.

7.8 Conventional Foundation Design

7.8.1 Subsequent to the recommended grading, proposed structures may be supported on a conventional spread foundation system deriving support in newly placed engineered fill. Proposed building foundations should be underlain by a minimum of 3 feet of newly placed engineered fill. The use of a conventional foundation system requires the use of interconnecting foundation ties.

7.8.2 Conventional shallow spread foundations should consist of continuous strip footings and/or isolated spread footings with interconnecting foundation ties and should be designed using the parameters in the table on the following page.

SUMMARY OF FOUNDATION RECOMMENDATIONS

Parameter	Value
Minimum Continuous Foundation Width	12 Inches
Minimum Isolated Foundation Width	24 Inches
Minimum Foundation Depth	18 Inches Below Lowest Adjacent Grade & 12 inches into recommended bearing material
Minimum Steel Reinforcement	4 No. 4 Bars, 2 Top and 2 Bottom
Allowable Bearing Capacity – Continuous Foundation	2,500 psf
Allowable Bearing Capacity – Isolated Foundation	3,000 psf
Bearing Capacity Increase	300 psf per Foot of Width
	600 psf per Foot of Depth
Maximum Allowable Bearing Capacity	4,000 psf
Estimated Total Settlement	¾ Inch
Estimated Differential Settlement	½ Inch over 20 Feet

7.8.3 The above foundation dimensions and minimum reinforcement recommendations are based on soil conditions and building code requirements only, and are not intended to be used in lieu of those required for structural purposes.

7.8.4 The allowable bearing pressures may be increased by one-third for transient loads due to wind or seismic forces.

7.8.5 The analyses presented herein indicate the site could be susceptible to seismically-induced settlement. These settlements are in addition to the static settlements indicated above and must be considered in the structural design. Based on seismic considerations, the proposed structure should be designed for a combined static and seismically-induced differential settlement indicated in the table below.

SUMMARY OF ANTICIPATED DIFFERENTIAL SETTLEMENT

Parameter	Value
Estimated Differential Static Settlement	½ Inch over 20 Feet
Estimated Differential Seismic Settlement	⅔ Inch over 20 Feet
Recommended Combined Differential Static + Seismic Settlement	1¼ over 20 feet

7.8.6 Once the design and foundation loading configurations for the proposed structures proceeds to a more finalized plan, the estimated settlements presented in this report should be reviewed and revised, if necessary. If the final foundation loading configurations are greater than the assumed loading conditions, the potential for settlement should be reevaluated by this office.

7.8.7 No special subgrade presaturation is required prior to placement of concrete. However, the moisture in the foundation subgrade should be sprinkled as necessary to maintain a moist condition at the time of concrete placement.

7.8.8 If depth increases are utilized for the exterior wall footings, this office should be provided a copy of the final construction plans so that the excavation recommendations presented herein could be properly reviewed and revised if necessary. Additional grading should be conducted as needed in order to maintain the required 3-foot-thick blanket of engineered fill below foundations.

7.9 Miscellaneous Foundations

7.9.1 Foundations for small outlying structures, such as block walls up to 6 feet in height, planter walls or trash enclosures, which will not be tied to the proposed structure, may be supported on conventional foundations deriving support on a minimum of 12 inches of newly placed engineered fill which extends laterally at least 12 inches beyond the foundation area. Where excavation and compaction cannot be performed, foundations may derive support directly in the competent undisturbed alluvial soils and should be deepened as necessary to maintain a minimum 12-inch embedment into the recommended bearing materials. The depth to competent alluvium should be field verified at each location.

7.9.2 If the soils exposed in the excavation bottom are soft, compaction of the soft soils will be required prior to placing steel or concrete. Compaction of the foundation excavation bottom is typically accomplished with a compaction wheel or mechanical whacker and must be observed and approved by a Geocon representative. Miscellaneous foundations may be designed for a bearing value of 1,500 psf, and should be a minimum of 12 inches in width, 18 inches in depth below the lowest adjacent grade and 12 inches into the recommended bearing material. The allowable bearing pressure may be increased by up to one-third for transient loads due to wind or seismic forces.

7.9.3 Foundation excavations should be observed and approved in writing by the Geotechnical Engineer (a representative of Geocon West, Inc.), prior to the placement of reinforcing steel and concrete to verify that the excavations and exposed soil conditions are consistent with those anticipated.

7.10 Temporary Modular Classrooms Foundation Design

7.10.1 It is our understanding that the temporary modular classrooms will be supported on pier foundations deriving support on cribbing underlain by newly placed engineered fill. Provided the area of the modular classroom is prepared in accordance with the Grading recommendations provided herein (Section 7.4), the modular classroom structure foundations may be designed with an allowable bearing pressure of 1,000 pounds per square foot.

7.11 Lateral Design

7.11.1 Resistance to lateral loading may be provided by friction acting at the base of foundations, slabs and by passive earth pressure. An allowable coefficient of friction of 0.35 may be used with the dead load forces in the newly placed engineered fill or undisturbed older alluvial soils.

7.11.2 Passive earth pressure for the sides of foundations and slabs poured against newly placed engineered fill or undisturbed older alluvial soils may be computed as an equivalent fluid having a density of 250 pounds per cubic foot (pcf) with a maximum earth pressure of 2,500 psf. When combining passive and friction for lateral resistance, the passive component should be reduced by one-third. A one-third increase in the passive value may be used for wind or seismic loads.

7.10.3 Where the recommended lateral over-excavation cannot be performed, such as adjacent to property lines and/or an existing structure, the lateral component of the foundation design can rely solely on friction between the bottom of the foundation and the underlying subgrade soils. The foundation should not utilize passive pressure unless foundations are bounded by and in direct contact with newly placed engineered fill.

7.12 Concrete Slabs-on-Grade

7.12.1 Subsequent to the recommended grading, concrete slabs-on-grade for structures, not subject to vehicle loading, should be a minimum of 4 inches thick and minimum slab reinforcement should consist of No. 3 steel reinforcing bars placed 18 inches on center in both horizontal directions. Steel reinforcing should be positioned vertically near the slab midpoint.

7.12.2 Slabs-on-grade at the ground surface that may receive moisture-sensitive floor coverings or may be used to store moisture-sensitive materials should be underlain by a vapor retarder placed directly beneath the slab. The vapor retarder and acceptable permeance should be specified by the project architect or developer based on the type of floor covering that will be installed. The vapor retarder selection and design should be consistent with the guidelines presented in Section 9.3 of the American Concrete Institute's (ACI) Guide for Concrete Slabs that Receive Moisture-Sensitive Flooring Materials (ACI 302.2R-06) as well as ASTM E1745 and should be installed in general conformance with ASTM E 1643 (latest edition) and the manufacturer's recommendations. A minimum thickness of 15 mils extruded polyolefin plastic is recommended; vapor retarders which contain recycled content or woven materials are not recommended. The vapor retarder should have a permeance of less than 0.01 perms demonstrated by testing before and after mandatory conditioning is recommended. The vapor retarder should be installed in direct contact with the concrete slab with proper perimeter seal. If the California Green Building Code requirements apply to this project, the vapor retarder should be underlain by 4 inches of clean aggregate. It is important that the vapor retarder be puncture resistant since it will be in direct contact with angular gravel. As an alternative to the clean aggregate suggested in the Green Building Code, it is our opinion that the concrete slab-on-grade may be underlain by a vapor retarder over 4-inches of clean sand (sand equivalent greater than 30), since the sand will serve a capillary break and will minimize the potential for punctures and damage to the vapor barrier.

7.12.3 For seismic design purposes, a coefficient of friction of 0.35 may be utilized between concrete slabs and subgrade soils without a moisture barrier, and 0.15 for slabs underlain by a moisture barrier.

7.12.4 Exterior slabs for walkways and flatwork, not subject to traffic loads, should be at least 4 inches thick and reinforced with No. 3 steel reinforcing bars placed 18 inches on center in both horizontal directions, positioned near the slab midpoint. Prior to construction of slabs, the upper 12 inches of subgrade should be moistened to near optimum moisture content and properly compacted to at least 95 percent relative compaction, as determined by ASTM Test Method D 1557 (latest edition). Crack control joints should be spaced at intervals not greater than 10 feet and should be constructed using saw-cuts or other methods as soon as practical following concrete placement. Crack control joints should extend a minimum depth of one-fourth the slab thickness. Construction joints should be designed by the project structural engineer.

7.12.5 The moisture content of the slab subgrade should be maintained and sprinkled as necessary to maintain a moist condition as would be expected in any concrete placement.

7.12.6 The recommendations of this report are intended to reduce the potential for cracking of slabs due to settlement. However, even with the incorporation of the recommendations presented herein, foundations, stucco walls, and slabs-on-grade may exhibit some cracking due to minor soil movement and/or concrete shrinkage. The occurrence of concrete shrinkage cracks is independent of the supporting soil characteristics. Their occurrence may be reduced and/or controlled by limiting the slump of the concrete, proper concrete placement and curing, and by the placement of crack control joints at periodic intervals, in particular, where re-entrant slab corners occur.

7.13 Preliminary Pavement Recommendations

7.13.1 Where new paving is to be placed, it is recommended that all existing fill and soft alluvium be excavated and properly compacted for paving support. The client should be aware that excavation and compaction of all existing artificial fill and soft alluvium in the area of new paving is not required; however, paving constructed over existing uncertified fill or unsuitable alluvium may experience increased settlement and/or cracking, and may therefore have a shorter design life and increased maintenance costs. As a minimum, the upper 12 inches of paving subgrade should be scarified, moisture conditioned to near optimum moisture content, and properly compacted to at least 95 percent relative compaction, as determined by ASTM Test Method D 1557 (latest edition).

7.13.2 The following pavement sections are based on an assumed R-Value of 20. Once site grading activities are complete an R-Value should be obtained by laboratory testing to confirm the properties of the soils serving as paving subgrade, prior to placing pavement.

7.13.3 The Traffic Indices listed below are estimates. Geocon does not practice in the field of traffic engineering. The actual Traffic Index for each area should be determined by the project civil engineer. If pavement sections for Traffic Indices other than those listed below are required, Geocon should be contacted to provide additional recommendations. Pavement thicknesses were determined following procedures outlined in the *California Highway Design Manual* (Caltrans). It is anticipated that the majority of traffic will consist of automobile and large truck traffic.

PRELIMINARY PAVEMENT DESIGN SECTIONS

Location	Estimated Traffic Index (TI)	Asphalt Concrete (inches)	Class 2 Aggregate Base (inches)
Automobile Parking and Driveways	4.0	3.0	6.0
Trash Truck & Fire Lanes	7.0	4.0	12.0

7.13.4 We understand that decomposed granite (DG) paving will be constructed for pedestrian and vehicular loading. It is recommended that the DG material be underlain by aggregate base. For the purpose of providing pavement design recommendations, we have assumed that the DG does not contribute to the paving structural section.

PRELIMINARY PAVEMENT DESIGN SECTIONS – BASE ONLY

Location	Estimated Traffic Index (TI)	Class 2 Aggregate Base (inches)
Pedestrian Walkways	n/a	4.0
Trash Truck & Fire Lanes	7.0	20.0

7.13.5 Asphalt concrete should conform to Section 203-6 of the "*Standard Specifications for Public Works Construction*" (Green Book). Class 2 aggregate base materials should conform to Section 26-1.02A of the "*Standard Specifications of the State of California, Department of Transportation*" (Caltrans). The use of Crushed Miscellaneous Base (CMB) in lieu of Class 2 aggregate base is acceptable. Crushed Miscellaneous Base should conform to Section 200-2.4 of the "*Standard Specifications for Public Works Construction*" (Green Book).

7.13.6 Unless specifically designed and evaluated by the project structural engineer, where exterior concrete paving will be utilized for support of vehicles, it is recommended that the concrete be a minimum of 6 inches of concrete reinforced with No. 3 steel reinforcing bars placed 18 inches on center in both horizontal directions. Concrete paving supporting vehicular traffic should be underlain by a minimum of 4 inches of aggregate base and a properly compacted subgrade. The subgrade and base material should be compacted to 95 percent relative compaction as determined by ASTM Test Method D 1557 (latest edition).

7.13.7 The performance of pavements is highly dependent upon providing positive surface drainage away from the edge of pavements. Ponding of water on or adjacent to the pavement will likely result in saturation of the subgrade materials and subsequent cracking, subsidence and pavement distress. If planters are planned adjacent to paving, it is recommended that the perimeter curb be extended at least 12 inches below the bottom of the aggregate base to minimize the introduction of water beneath the paving.

7.14 Temporary Excavations

7.14.1 Excavations on the order of 5 feet in height may be required during grading operations. The excavations are expected to expose artificial fill and alluvial soils, which may be subject to caving where granular soils are exposed. Temporary vertical excavations up to 5 feet in height may be attempted where loose soils or caving sands are not present, and where excavations are not surcharged by adjacent traffic or structures.

7.14.2 Vertical excavations greater than 5 feet or where surcharged by existing structures will require sloping or shoring measures in order to provide a stable excavation. Where sufficient space is available, temporary unsurcharged embankments could be sloped back at a uniform 1:1 slope gradient or flatter up to a maximum of 10 feet in height. A uniform slope does not have a vertical portion. Where space is limited, shoring measures will be required.

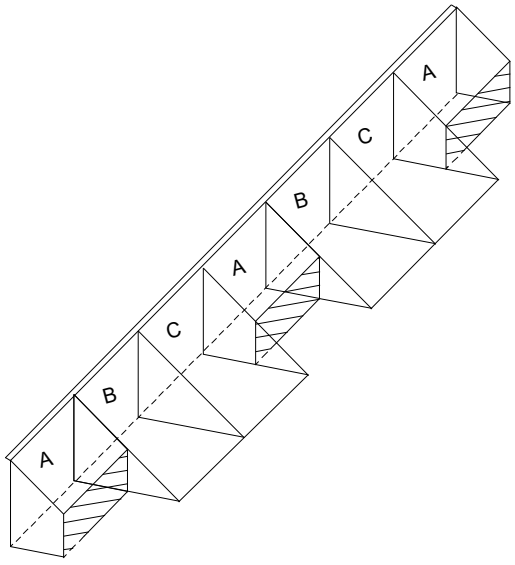
7.14.3 If excavations in close proximity to an adjacent property line and/or structure are required, special excavation measures such as slot-cutting or shoring may be necessary in order to maintain lateral support of offsite improvements. Recommendations for slot-cutting are provided in the following section.

7.14.4 Where temporary construction slopes are utilized, the top of the slope should be barricaded to prevent vehicles and storage loads at the top of the slope within a horizontal distance equal to the height of the slope. If the temporary construction slopes are to be maintained during the rainy season, berms are suggested along the tops of the slopes where necessary to prevent runoff water from entering the excavation and eroding the slope faces. The soils exposed in the cut slopes should be inspected during excavation by our personnel and the contractor's competent person so that modifications of the slopes can be made if variations in the soil conditions occur. All excavations should be stabilized within 30 days of initial excavation.

7.15 Slot Cutting

7.15.1 The slot-cutting method employs the earth as a buttress and allows the earth excavation to proceed in phases. Where slot-cutting is used for foundation construction, the proposed construction techniques should be discussed with the structural engineer so that appropriate modifications can be made to the foundation design; such as additional reinforcing or details for doweling.

7.15.2 It is recommended that the initial temporary excavation along the property line be sloped back at a uniform 1:1 (H:V) slope gradient or flatter for excavation of the existing soils to the necessary depth. The temporary excavation should not extend below the surcharge area of any adjacent foundations. The surcharge area may be defined by a 1:1 projection down and away from the bottom of an existing foundation. The temporary slope may then be excavated using the slot-cutting (see illustration below).



7.15.3 Alternate "A" slots of 8 feet in width may be worked. The remaining earth buttresses ("B" and "C" slots) should also be 8 feet in width. The wall, foundation, or backfill should be completed in the "A" slots to a point where support of the offsite property and/or any existing structures is restored before the "B" slots are excavated. After completing the wall, foundation, or backfill in the "B" slots, finally the "C" slots may be excavated. Slot-cutting is not recommended for vertical excavations greater than 5 feet in height. A slot-cut calculation is provided as Figure 12 and assumes no surcharge loads will be acting on the excavation. If surcharge loads will be present, the slot-cut calculation should be revised as necessary.

7.16 Stormwater Infiltration

7.16.1 During the site exploration, borings L and M were used to perform percolation testing. The borings were advanced to the depth listed in the table below. Slotted casing was placed in the borings, and the annular space between the casing and excavation was filled with filter pack. The borings were then filled with water to pre-saturate the soils. The casings were refilled with water and percolation test readings were performed after repeated flooding of the cased excavation. Based on the test results, the average infiltration rate (adjusted percolation rate), for the earth materials encountered, is provided in the following table. The field-measured percolation rate has been adjusted to infiltration rates in accordance with the County of Orange Technical Guidance Document for the Preparation of Conceptual/Preliminary and/or Project Water Quality Management Plans (December 2013). Additional correction factors may be required and should be applied by the engineer in responsible charge of the design of the stormwater infiltration system and based on applicable guidelines. Percolation test results are provided on Figures 13 and 14.

Boring	Soil Type	Infiltration Depth (ft)	Average Infiltration Rate (in / hour)
L	Silty Sand (SM)	5-10	1.40
M	Silty Sand (SM)	3.5-5	2.73

7.16.2 The results of the percolation testing indicate that the soils are conductive to infiltration. It is our opinion that the soil zones encountered at the depths and locations as listed in the table above are suitable for infiltration of stormwater.

7.16.3 It is our opinion that the introduction of stormwater at the depth and location indicated above will not induce excessive hydro-consolidation, will not create a perched groundwater condition, will not affect soil structure interaction of existing or proposed foundations due to expansive soils, will not saturate soils supported by existing or proposed retaining walls, and will not increase the potential for liquefaction. Resulting settlements are anticipated to be less than ¼ inch, if any.

7.16.4 If infiltration is planned for any location or depth other than where the above testing was performed, additional testing may be required.

7.16.5 The infiltration system should be located such that the closest distance between an adjacent foundation is at least 15 feet in all directions from the zone of saturation. The zone of saturation may be assumed to project downward from the discharge of the infiltration facility at a gradient of 1:1. Additional property line or foundation setbacks may be required by the governing jurisdiction and should be incorporated into the stormwater infiltration system design as necessary.

7.16.6 Subsequent to the placement of the infiltration system, it is acceptable to backfill the resulting void space between the excavation sidewalls and the infiltration system with minimum two-sack slurry provided the slurry is not placed in the infiltration zone. It is recommended that pea gravel be utilized adjacent to the infiltration zone so communication of water to the soil is not hindered.

7.16.7 Due to the preliminary nature of the project at this time, the type of stormwater infiltration system and location of the stormwater infiltration systems has not yet been determined. The design drawings should be reviewed and approved by the Geotechnical Engineer. The installation of the stormwater infiltration system should be observed and approved by the Geotechnical Engineer (a representative of Geocon).

7.17 Surface Drainage

7.17.1 Proper surface drainage is critical to the future performance of the project. Uncontrolled infiltration of irrigation excess and storm runoff into the soils can adversely affect the performance of the planned improvements. Saturation of a soil can cause it to lose internal shear strength and increase its compressibility, resulting in a change in the original designed engineering properties. Proper drainage should be maintained at all times.

7.17.2 All site drainage should be collected and controlled in non-erosive drainage devices. Drainage should not be allowed to pond anywhere on the site, and especially not against any foundation or retaining wall. The site should be graded and maintained such that surface drainage is directed away from structures in accordance with 2022 CBC 1804.4 or other applicable standards. In addition, drainage should not be allowed to flow uncontrolled over any descending slope. Discharge from downspouts, roof drains and scuppers are not recommended onto unprotected soils within 5 feet of the building perimeter. Planters which are located adjacent to foundations should be sealed to prevent moisture intrusion into the soils providing foundation support. Landscape irrigation is not recommended within 5 feet of the building perimeter footings except when enclosed in protected planters.

7.17.3 Positive site drainage should be provided away from structures, pavement, and the tops of slopes to swales or other controlled drainage structures.

7.17.4 Landscaping planters immediately adjacent to paved areas are not recommended due to the potential for surface or irrigation water to infiltrate the pavement's subgrade and base course. Either a subdrain, which collects excess irrigation water and transmits it to drainage structures, or impervious above-grade planter boxes should be used. In addition, where landscaping is planned adjacent to the pavement, it is recommended that consideration be given to providing a cutoff wall along the edge of the pavement that extends at least 12 inches below the base material.

7.18 Plan Review

7.18.1 Grading, foundation, and shoring plans should be reviewed by the Geotechnical Engineer (a representative of Geocon West, Inc.), prior to finalization to verify that the plans have been prepared in substantial conformance with the recommendations of this report and to provide additional analyses or recommendations.

LIMITATIONS AND UNIFORMITY OF CONDITIONS

1. The firm that performed the geotechnical investigation for the project should be retained to provide testing and observation services during construction to provide continuity of geotechnical interpretation and to check that the recommendations presented for geotechnical aspects of site development are incorporated during site grading, construction of improvements, and excavation of foundations. If another geotechnical firm is selected to perform the testing and observation services during construction operations, that firm should prepare a letter indicating their intent to assume the responsibilities of project geotechnical engineer of record. A copy of the letter should be provided to the regulatory agency for their records. In addition, that firm should provide revised recommendations concerning the geotechnical aspects of the proposed development, or a written acknowledgement of their concurrence with the recommendations presented in our report. They should also perform additional analyses deemed necessary to assume the role of Geotechnical Engineer of Record.

2. The recommendations of this report pertain only to the site investigated and are based upon the assumption that the soil conditions do not deviate from those disclosed in the investigation. If any variations or undesirable conditions are encountered during construction, or if the proposed construction will differ from that anticipated herein, Geocon Incorporated should be notified so that supplemental recommendations can be given. The evaluation or identification of the potential presence of hazardous or corrosive materials was not part of the scope of services provided by Geocon Incorporated.

3. This report is issued with the understanding that it is the responsibility of the owner or his representative to ensure that the information and recommendations contained herein are brought to the attention of the architect and engineer for the project and incorporated into the plans, and the necessary steps are taken to see that the contractor and subcontractors carry out such recommendations in the field.

4. The findings of this report are valid as of the present date. However, changes in the conditions of a property can occur with the passage of time, whether they be due to natural processes or the works of man on this or adjacent properties. In addition, changes in applicable or appropriate standards may occur, whether they result from legislation or the broadening of knowledge. Accordingly, the findings of this report may be invalidated wholly or partially by changes outside our control. Therefore, this report is subject to review and should not be relied upon after a period of three years.

LIST OF REFERENCES

1. *California Department of Water Resources, 1961, Planned Utilization of Groundwater Basins of the Coastal Plain of Los Angeles County, Bulletin 104, Appendix A.*

2. *California Division of Mines and Geology, 1998, State of California, Seismic Hazard Zones, Anaheim Quadrangle, Revised Official Map Released: April 15, 1998.*

3. *California Division of Mines and Geology, 1997 (revised 2001), Seismic Hazard Evaluation Report for the Anaheim and Newport Beach 7.5-Minute Quadrangles, Orange County, California, Seismic Hazard Zone Report 003.*

4. *California Geologic Energy Management Division, 2024, CalGEM Resources Well Finder, http://maps.conservation.ca.gov.doggr/index.html#close.*

5. *California Geological Survey, 2024a, CGS Information Warehouse, Regulatory Map Portal, http://maps.conservation.ca.gov/cgs/informationwarehouse/index.html?map=regulatorymaps.*

6. *California Geological Survey, 2024b, Earthquake Zones of Required Investigation, https://maps.conservation.ca.gov/cgs/EQZApp/app/.*

7. *California Geological Survey, 2018, Earthquake Fault Zones, A Guide for Government Agencies, Property Owners/Developers, and Geoscience Practitioners for Assessing Fault Rupture Hazards in California, Special Publication 42, Revised 2018.*

8. *California Geological Survey, 2017, Earthquake Zones of Required Investigation,*

9. *California Geological Survey, 2012, Geologic Compilation of Quaternary Surficial Deposits in Southern California, Santa Ana 30' X 60' Quadrangle, A Project for the Department of Water Resources by the California Geological Survey, Compiled from existing sources by Trinda L. Bedrossian, CEG and Peter D. Roffers, CGS Special Report 217, Plate 16, Scale 1:100,000.*

10. *City of Anaheim, General Plan, (2010) Public Safety Element.*

11. *FEMA, 2024, Online Flood Hazard Maps, http://www.esri.com/hazards/index.html.*

12. *Orange County General Plan, 2004, Safety Element, Advance Planning Program, Environmental Management Agency.*

13. *Jennings, C. W. and Bryant, W. A., 2010, Fault Activity Map of California, California Geological Survey Geologic Data Map No. 6.*

14. *Toppozada, T., Branum, D., Petersen, M, Hallstrom, C., and Reichle, M., 2000, Epicenters and Areas Damaged by M> 5 California Earthquakes, 1800 – 1999, California Geological Survey, Map Sheet 49.*

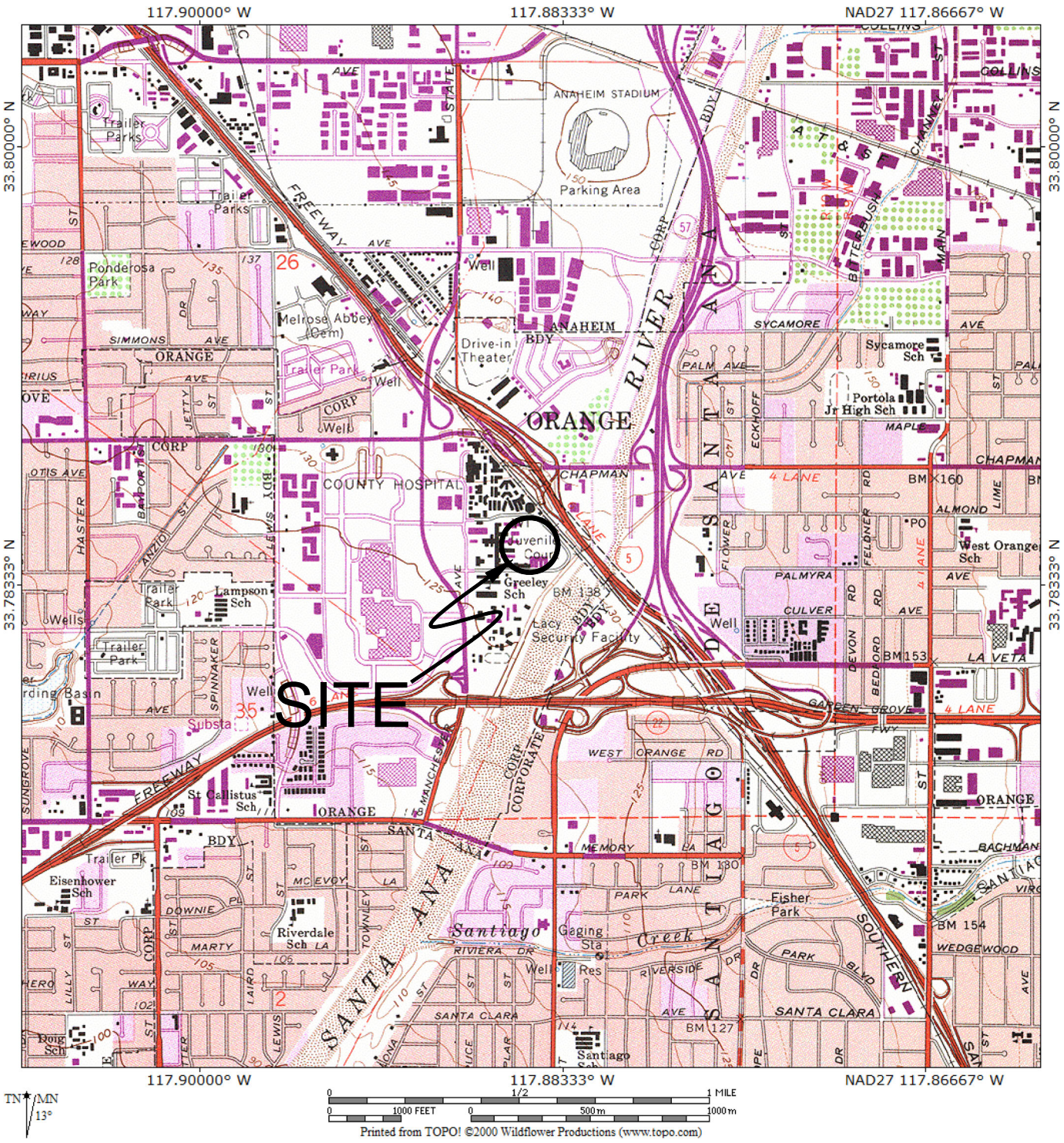
LIST OF REFERENCES (CONTINUED)

15. U.S. Geological Survey Landslide Hazard Program, 2023a, U.S. Landslide Inventory, https://usgs.maps.arcgis.com/apps/webappviewer/index.html?id=ae120962f459434b8c904b456c82669d.Risk Engineering, *EZ-FRISK*, 2016.

16. U.S. Geological Survey, 2024, Areas of Land Subsidence in California Website, https://ca.water.usgs.gov/land_subsidence/california-subsidence-areas.html

17. U.S. Geological Survey and California Geological Survey, 2006, Quaternary Fault and Fold Database for the United States, accessed September 28, 2022, from USGS web site: http//earthquake.usgs.gov/hazards/qfaults/.

18. Ziony, J. I., and Jones, L. M., 1989, Map Showing Late Quaternary Faults and 1978–1984 Seismicity of the Los Angeles Region, California, U.S. Geological Survey Miscellaneous Field Studies Map MF-1964.



REFERENCE: U.S.G.S. TOPOGRAPHIC MAPS, 7.5 MINUTE SERIES, ANAHEIM, CA QUADRANGLE

GEOCON
W E S T, I N C.

ENVIRONMENTAL GEOTECHNICAL MATERIALS
2807 MCGAW BOULEVARD - IRVINE, CA 92618
PHONE (949) 491-6570 - FAX (949) 299-4550

DRAFTED BY: ACS	CHECKED BY: JTA

VICINITY MAP

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024	PROJECT NO. W1857-88-01	FIG. 1



LEGEND

- Approximate Boring Locations
- Approximate CPT Location
- Approximate Limits of Project
- Area of Temp. Modular Classrooms

NORTH

0 100' 200'

GEOCON WEST, INC.
ENVIRONMENTAL GEOTECHNICAL MATERIALS
2807 MCGAW BOULEVARD - IRVINE, CA 92618
PHONE (949) 491-6570 - FAX (949) 299-4550

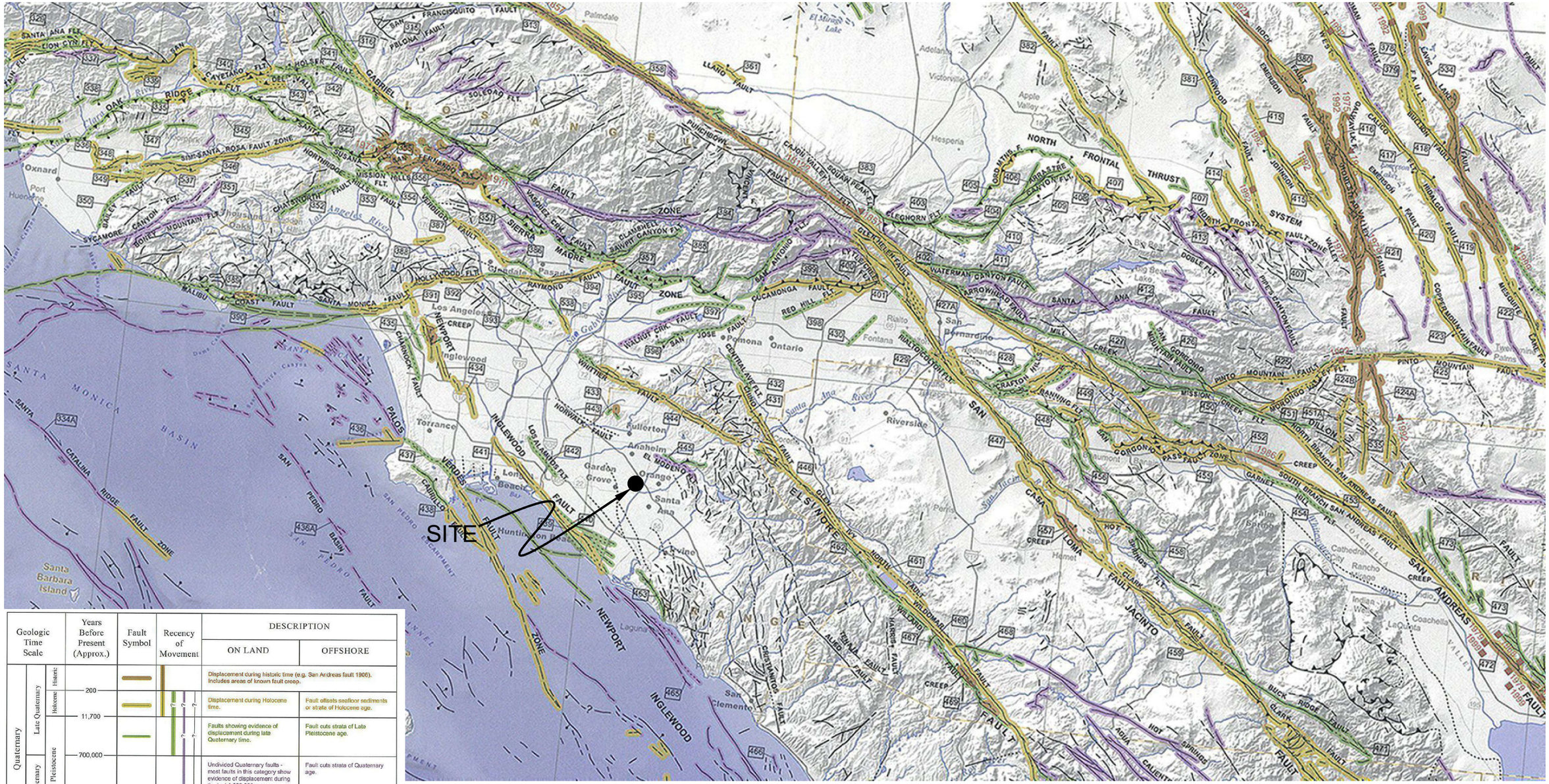
DRAFTED BY: ACS | CHECKED BY: JTA

SITE PLAN

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 | PROJECT NO. W1857-88-01 | FIG. 2

Reference: Jennings, C.W. and Bryant, W. A., 2010, Fault Activity Map of California, California Geological Survey Geologic Data Map No. 6.



Geologic Time Scale			Years Before Present (Approx.)	Fault Symbol	Recency of Movement	DESCRIPTION	
						ON LAND	OFFSHORE
Quaternary	Late Quaternary	Historic				Displacement during historic time (e.g. San Andreas fault 1906). Includes areas of known fault creep.	
		Holocene	200			Displacement during Holocene time.	Fault offsets seafloor sediments or strata of Holocene age.
			11,700			Faults showing evidence of displacement during late Quaternary time.	Fault cuts strata of Late Pleistocene age.
	Early Quaternary	Pleistocene	700,000			Undivided Quaternary faults - most faults in this category show evidence of displacement during the last 1,600,000 years; possible exceptions are faults which displace rocks of undifferentiated Plio-Pleistocene age.	Fault cuts strata of Quaternary age.
			1,600,000*				
Pre-Quaternary			4.5 billion (Age of Earth)			Faults without recognized Quaternary displacement or showing evidence of no displacement during Quaternary time. Not necessarily inactive.	Fault cuts strata of Pliocene or older age.

* Quaternary now recognized as extending to 2.6 Ma (Walker and Geissman, 2009). Quaternary faults in this map were established using the previous 1.6 Ma criterion.

N

0 12 24 Miles

GEOCON WEST, INC.

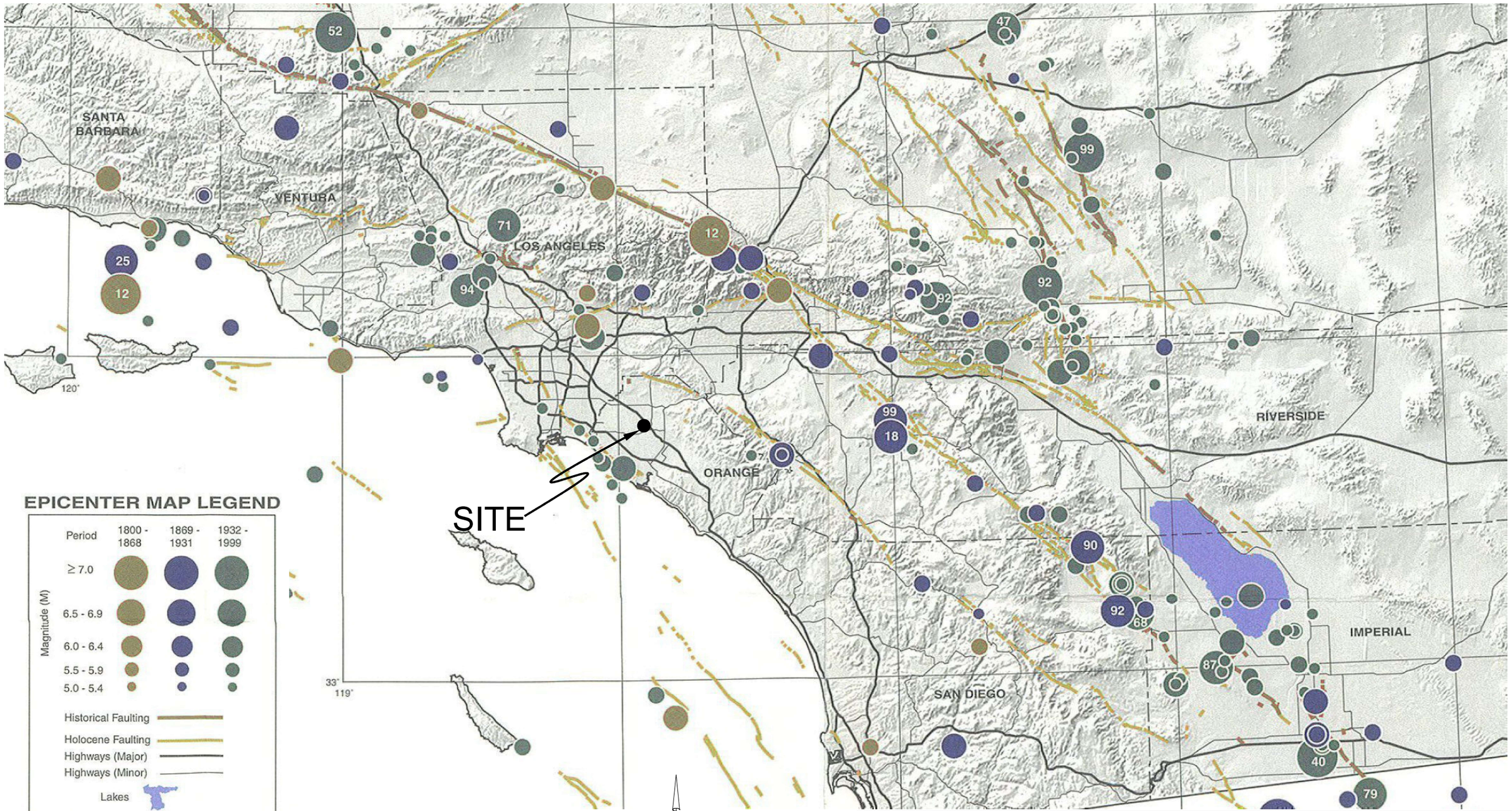
ENVIRONMENTAL GEOTECHNICAL MATERIALS
2807 MCGAW BOULEVARD - IRVINE, CA 92618
PHONE (949) 491-6570 - FAX (949) 299-4550

DRAFTED BY: RA | CHECKED BY: GK

REGIONAL FAULT MAP

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 | PROJECT NO. W1857-88-01 | FIG. 3



Reference: Toppozada, T., Branum, D., Petersen, M., Hallstrom, C., Cramer, C., and Reichle, M., 2000, Epicenters and Areas Damaged by M>5 California Earthquakes, 1800 - 1999, California Geological Survey, Map Sheet 49.

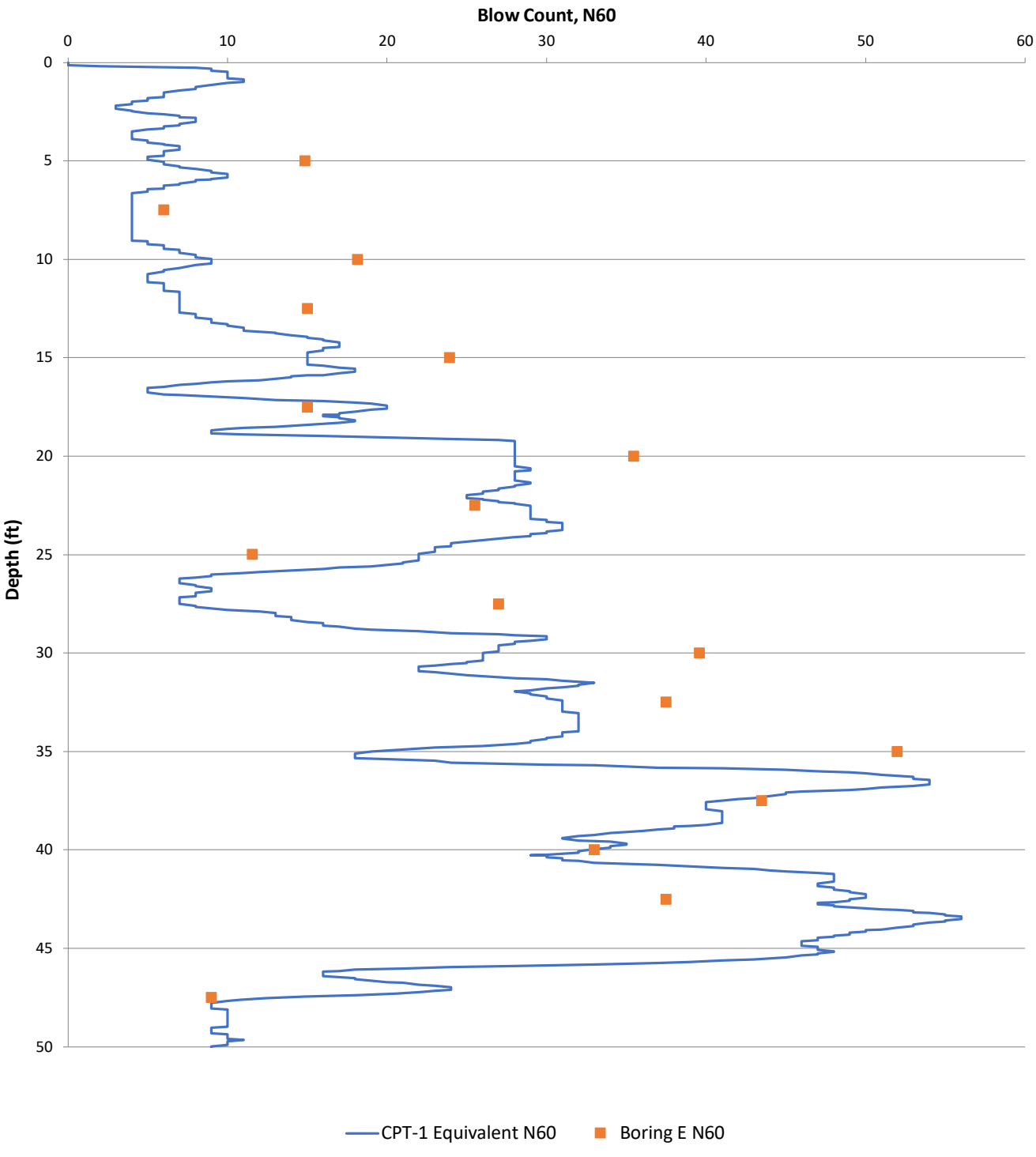
GEOCON
W E S T, I N C.
ENVIRONMENTAL GEOTECHNICAL MATERIALS
2807 MCGAW AVENUE, IRVINE, CA 92614
PHONE (949) 491-6570

DRAFTED BY: RA	CHECKED BY: GK

REGIONAL SEISMICITY MAP

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024	PROJECT NO. W1857-88-01	FIG. 4



GEOCON
WEST, INC.

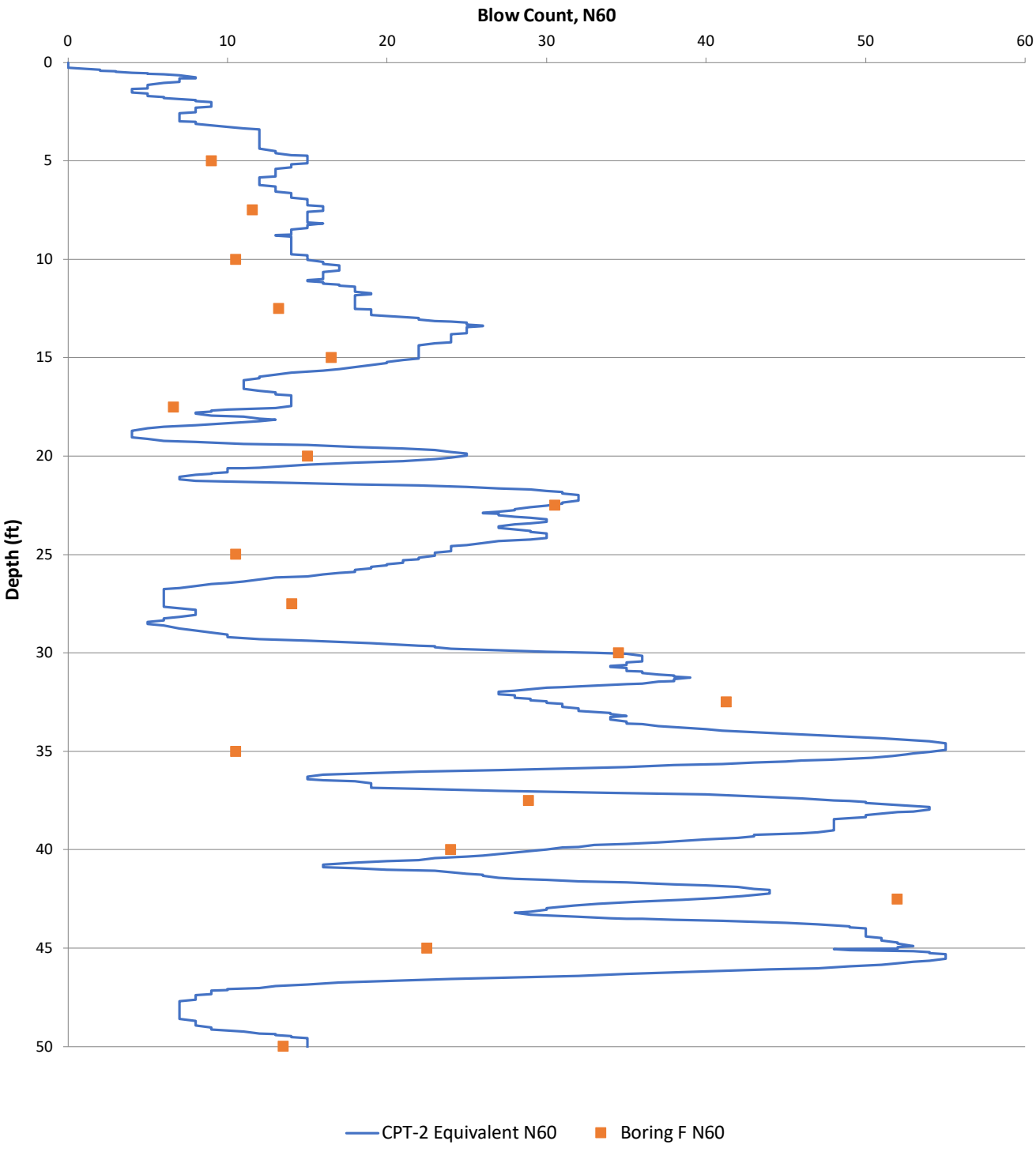
ENVIRONMENTAL GEOTECHNICAL MATERIALS
2807 MCGAW AVENUE - IRVINE, CALIFORNIA, 92614
PHONE: 949-491-6570

DRAFTED BY: ACS	CHECKED BY: JTA

CORRELATION OF BORING AND CPT N60

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024	PROJECT NO. W1857-88-01	FIG. 5



GEOCON WEST, INC.

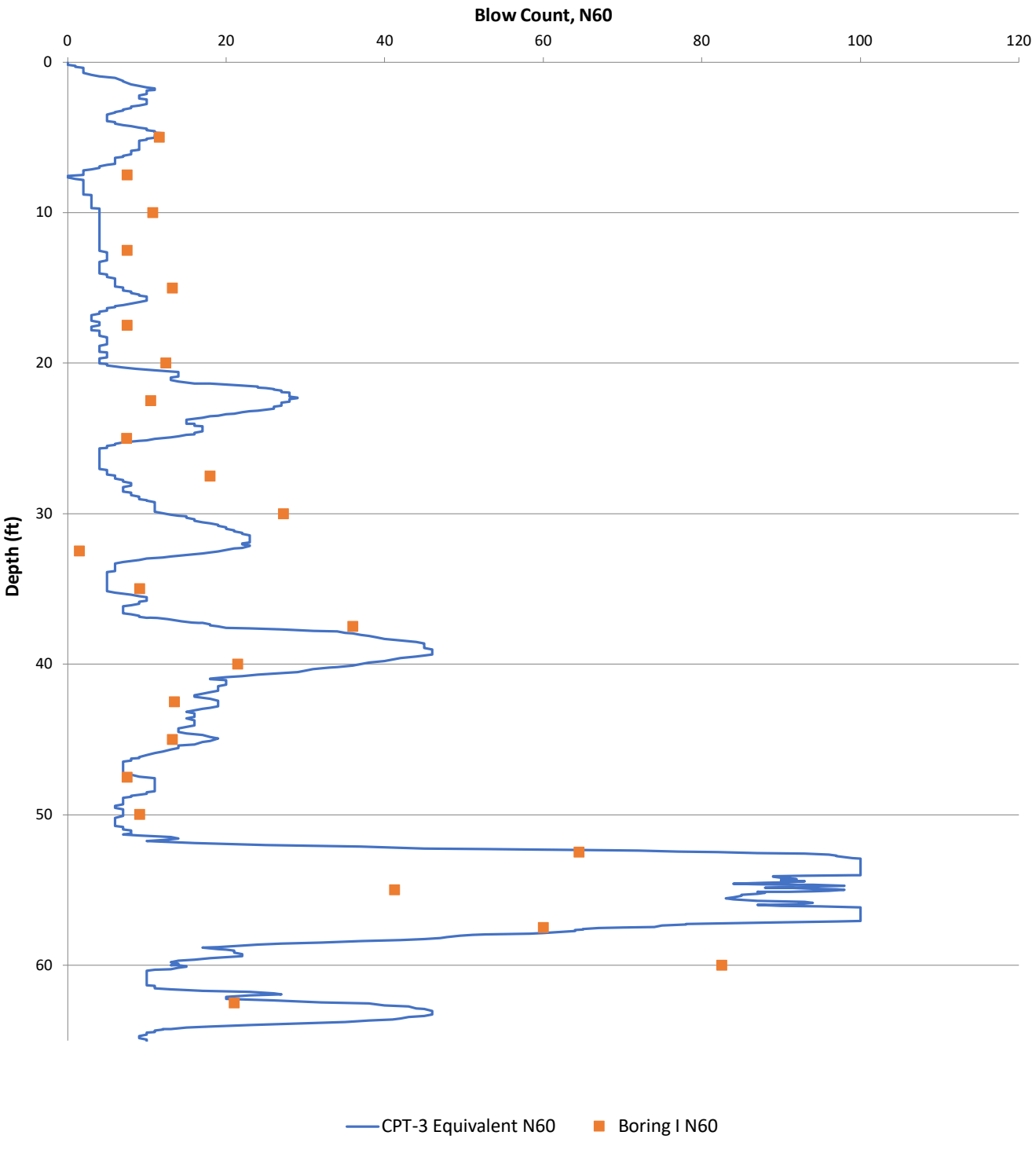
ENVIRONMENTAL GEOTECHNICAL MATERIALS
2807 MCGAW AVENUE - IRVINE, CALIFORNIA, 92614
PHONE: 949-491-6570

DRAFTED BY: ACS	CHECKED BY: JTA

CORRELATION OF BORING AND CPT N60

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024	PROJECT NO. W1857-88-01	FIG. 6



GEOCON WEST, INC.

ENVIRONMENTAL GEOTECHNICAL MATERIALS
2807 MCGAW AVENUE - IRVINE, CALIFORNIA, 92614
PHONE: 949-491-6570

DRAFTED BY: ACS	CHECKED BY: JTA

CORRELATION OF BORING AND CPT N60

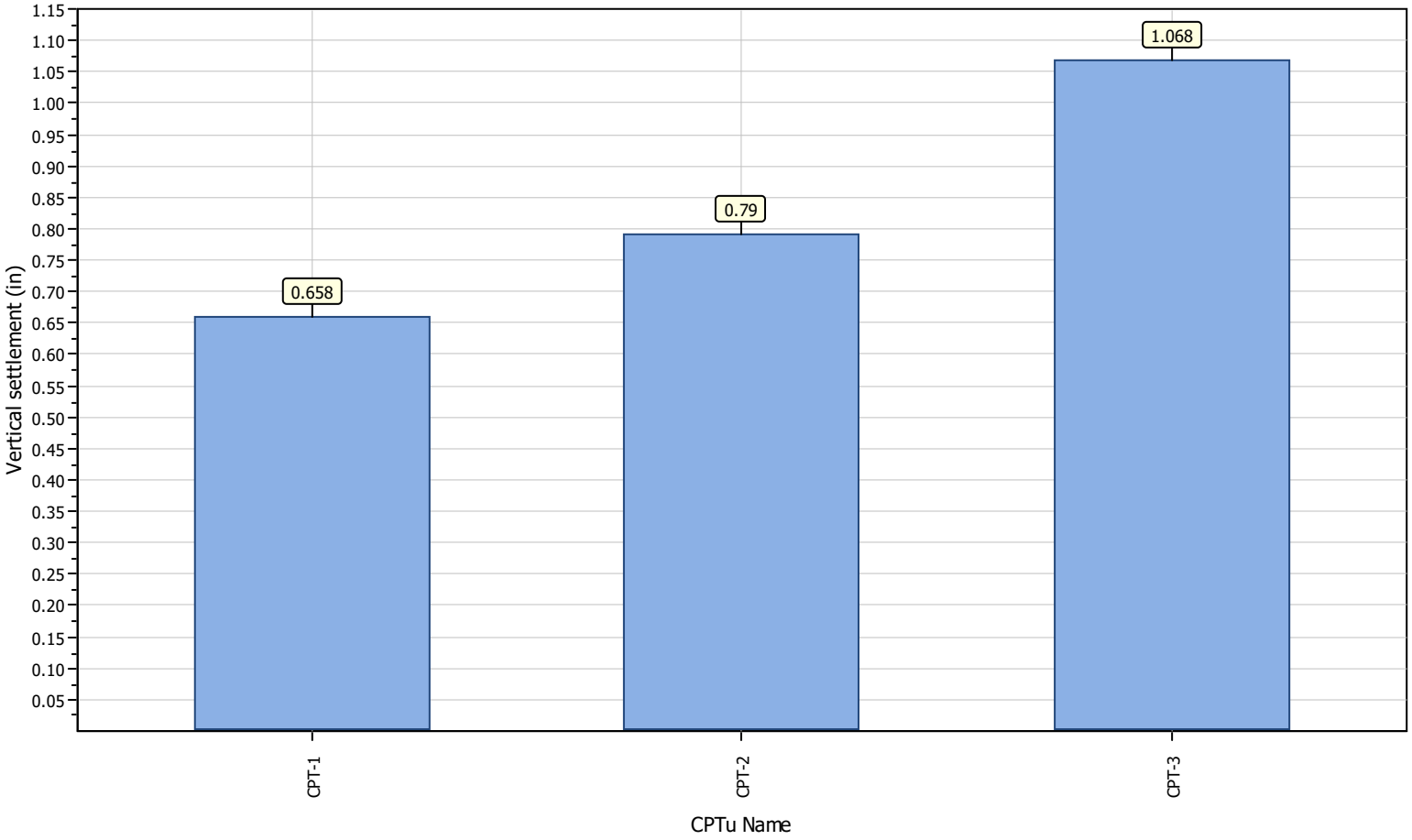
OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024	PROJECT NO. W1857-88-01	FIG. 7

Project title : W1857-88-01

Location : 331 The City Drive S

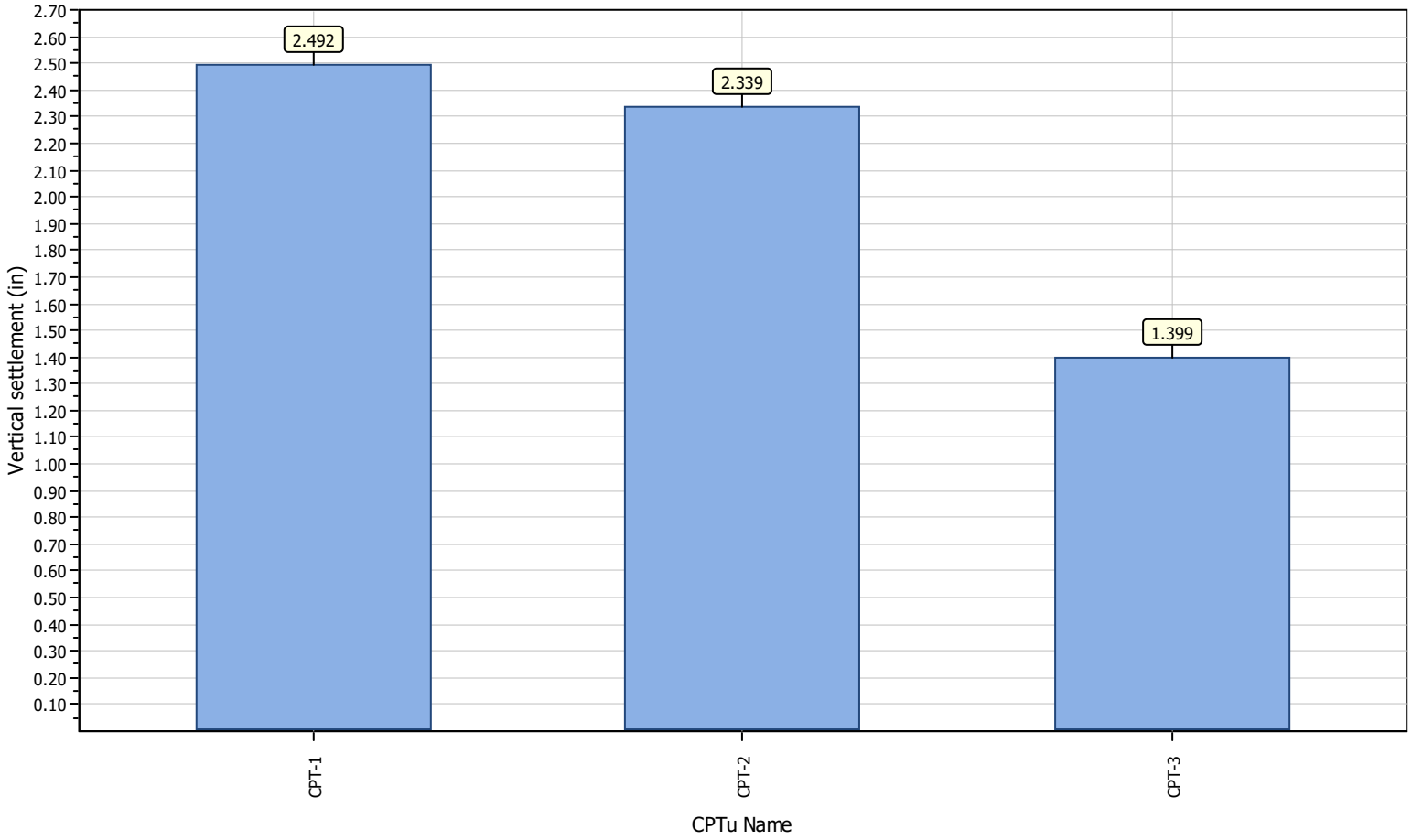
DE Overall vertical settlements report



Project title : W1857-88-01

Location : 331 The City Drive S

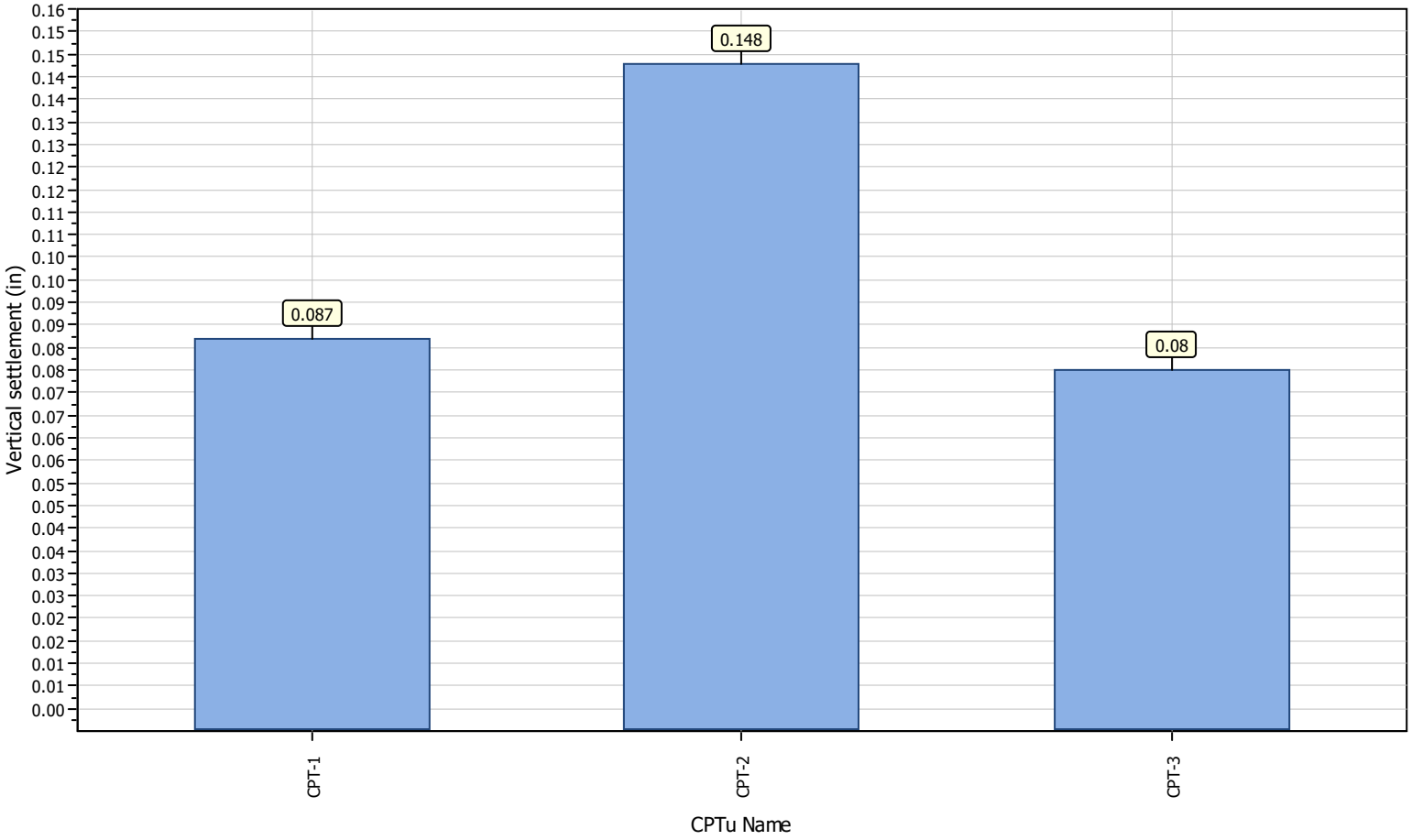
MCE Overall vertical settlements report



Project title : W1857-88-01

Location : 331 The City Drive S

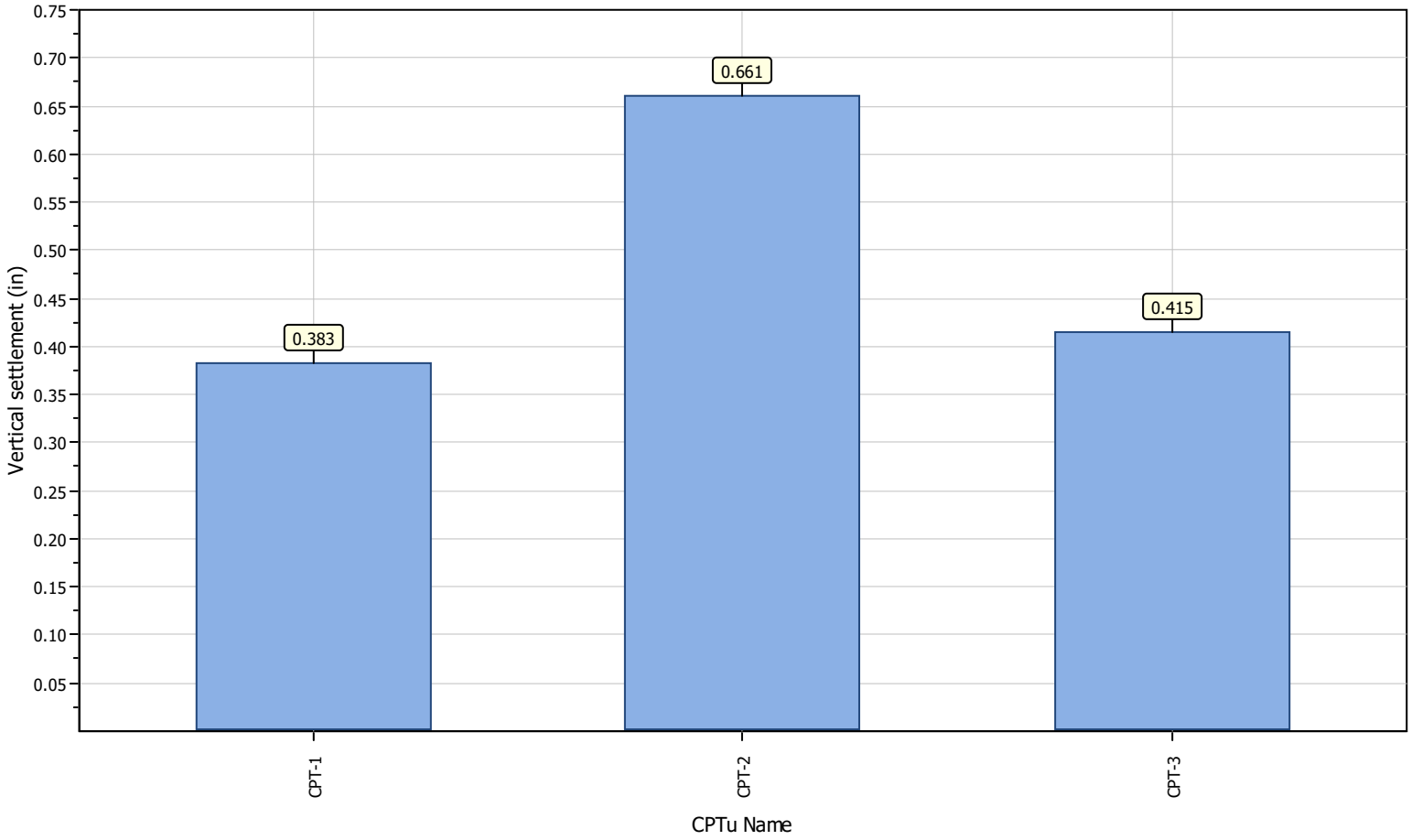
DE Overall vertical settlements report Dry Sands



Project title : W1857-88-01

Location : 331 The City Drive S

MCE Overall vertical settlements report Dry Sands



Slot Cut Calculation

Input:

Height of Slots	(H)	5.00	feet
Unit Weight of Soils	(γ)	115.0	pcf
Friction Angle of Soils	(ϕ)	31.0	degrees
Cohesion of Soils	(c)	150.0	psf
Factor of Safety	(FS)	1.25	

Factor of Safety = Resistance Force/Driving Force

Design Equations

$b = H/(\tan \alpha)$

$A = 0.5*H*b$

$W = 0.5*H*b*\gamma$ *(per lineal foot of slot width)*

$F_1 = d*W*(\sin \alpha)$

$R_1 = d*[W*(\cos\alpha)*(\tan \phi)+(c*b)]$

$R_2 = 2*[(0.5*H*b)*c]$

FS = Resistance Force/Driving Force

FS = $(R_1+R_2)/(F_1)$

Surcharge Pressure:

Line Load Surcharge	(q_L)	0.0	plf
Distance Away from Excavation	(X)	0.0	feet

Failure Angle (α)	Width of Failure Wedge (b)	Area of Wedge (A)	Weight of Wedge (W)	**Driving Force (F_1)** Wedge + Surcharge per lineal foot of Slot Wdith	**Resisting Force (R_1)** Failure Wedge per lineal foot of Slot Width	**Resisting Force (R_2)** Side Resistance Force lbs	**Allowable Width of Slots* (d)**
degrees	feet	$feet^2$	lbs/lineal foot				feet
45	5.0	13	1437.5	1016.5	1671.4	3750.0	8.0
46	4.8	12	1388.2	998.6	1622.0	3621.3	8.0
47	4.7	12	1340.5	980.4	1574.8	3496.9	8.0
48	4.5	11	1294.3	961.9	1529.6	3376.5	8.0
49	4.3	11	1249.6	943.1	1486.4	3259.8	8.0
50	4.2	10	1206.2	924.0	1444.9	3146.6	8.0
51	4.0	10	1164.1	904.6	1405.2	3036.7	8.0
52	3.9	10	1123.1	885.0	1367.2	2929.8	8.0
53	3.8	9	1083.2	865.1	1330.8	2825.8	8.0
54	3.6	9	1044.4	844.9	1295.9	2724.5	8.0
55	3.5	9	1006.5	824.5	1262.5	2625.8	8.0
56	3.4	8	969.6	803.8	1230.4	2529.4	8.0
57	3.2	8	933.5	782.9	1199.8	2435.3	8.0
58	3.1	8	898.2	761.8	1170.4	2343.3	8.0
59	3.0	8	863.7	740.4	1142.3	2253.2	8.0
60	2.9	7	829.9	718.8	1115.4	2165.1	8.0
61	2.8	7	796.8	696.9	1089.6	2078.7	8.0
62	2.7	7	764.3	674.9	1065.0	1993.9	8.0
63	2.5	6	732.4	652.6	1041.5	1910.7	8.0
64	2.4	6	701.1	630.2	1019.1	1829.0	8.0
65	2.3	6	670.3	607.5	997.8	1748.7	8.0
66	2.2	6	640.0	584.7	977.4	1669.6	8.0
67	2.1	5	610.2	561.7	958.0	1591.8	8.0
68	2.0	5	580.8	538.5	939.6	1515.1	8.0
69	1.9	5	551.8	515.2	922.2	1439.5	8.0
70	1.8	5	523.2	491.7	905.7	1364.9	8.0

* Width of Slots to achieve a minimum of 1.25 Factor of Safety, with a Maximum Allowable Slot Width of 8-feet.

Critical Slot Width with Factor of Safety equal or exceeding 1.25:

d_{allow} = 8.0 feet

GEOCON WEST, INC.

ENVIRONMENTAL GEOTECHNICAL MATERIALS

SLOT CUT CALCULATION

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

DRAFTED BY: JTA	CHECKED BY: JTA	MAY 2024	PROJECT NO. W1857-88-01	FIG. 12

PERCOLATION TEST DATA SHEET

Project:	OC YTC	**Project No.:**	W1857-88-01	**Date:**	Tuesday, February 13, 2024
Test Hole No.:	L	**Tested By:**	JC		
Depth of Test Hole, DT:	10	**USCS Soil Classification:**	SM		
Test Hole Dimensions (inches)			**Length**	**Width**	
Diameter (if round) =	8	**Sides (if rectangular) =**	-	-	

Sandy Soil Criteria Test*

Trial No.	Start Time	End Time	Δt Time Interval (min)	D_0 Initial Depth to Water (in)	D_f Final Depth to Water (in)	ΔD Change in Water Level (in)	Greater than or Equal to 6"? (y/n)
1	8:02 AM	8:27 AM	25	**60.0**	**83.4**	**23.4**	**yes**
2	8:30 AM	8:55 AM	25	**60.0**	**81**	**21**	**yes**

*If two consecutive measurements show that six inches of water seeps away in less than 25 minutes, the test shall be run for an additional hour with measurements, taken every 10 minutes. Otherwise, pre-soak (fill) overnight. Obtain at least twelve measurements per hole over at least six hours (approximately 30 minute intervals) with a precision of at least 0.25".

Trial No.	Start Time	End Time	Δt Time Interval (min)	D_0 Initial Depth to Water (in)	D_f Final Depth to Water (in)	ΔD Change in Water Level (in)	Percolation Rate (min/in)
1	9:14 AM	9:24 AM	10.00	60.0	68.0	8.0	1.24
2	9:26 AM	9:36 AM	10.00	60.0	68.0	8.0	1.24
3	9:38 AM	9:48 AM	10.00	60.0	67.2	7.2	1.39
4	9:50 AM	10:00 AM	10.00	60.0	66.8	6.8	1.46
5	10:01 AM	10:11 AM	10.00	60.0	66.8	6.8	1.46
6	10:13 AM	10:23 AM	10.00	60.0	66.8	6.8	1.46
7							
8							

Infiltration Rate Calculation:

Time Interval, Δt =	10.00	minutes	H_o =	60.0	inches
Final Depth to Water, D_f =	66.8	inches	H_f =	53.2	inches
Test Hole Radius, r =	4	inches	ΔH =	6.8	inches
Initial Depth to Water, D_0 =	60.0	inches	H_{avg} =	56.6	inches
Total Depth of Test Hole, D_t =	120	inches	$I_t = \frac{\Delta H(60r)}{\Delta t(r+2H_{avg})}$		
			Infiltration Rate, I_t =	**1.40**	**inches/hour**

GEOCON WEST, INC.

ENVIRONMENTAL GEOTECHNICAL MATERIALS
2807 MCGAW AVENUE - IRVINE, CALIFORNIA, 92614
PHONE: 949-491-6570

PERCOLATION TEST RESULTS AND CALCULATIONS

331 THE CITY DRIVE S
ORANGE, CALIFORNIA
OC YTC

DRAFTED BY: ACS	CHECKED BY: JTA	
MAY 2024	PROJECT NO. W1857-88-01	FIG. 13

PERCOLATION TEST DATA SHEET

Project:	OC YTC	**Project No.:**	W1857-88-01	**Date:**	Tuesday, February 13, 2024
Test Hole No.:	M	**Tested By:**	JC		
Depth of Test Hole, DT:	5	**USCS Soil Classification:**	SM		
Test Hole Dimensions (inches)			**Length**	**Width**	
Diameter (if round) =	8	**Sides (if rectangular) =**	-	-	

Sandy Soil Criteria Test*

Trial No.	Start Time	End Time	Δt Time Interval (min)	D_0 Initial Depth to Water (in)	D_f Final Depth to Water (in)	ΔD Change in Water Level (in)	Greater than or Equal to 6"? (y/n)
1	8:16 AM	8:41 AM	25	**39.0**	**49.8**	**10.8**	**yes**
2	8:44 AM	9:09 AM	25	**31.8**	**42.6**	**10.8**	**yes**

*If two consecutive measurements show that six inches of water seeps away in less than 25 minutes, the test shall be run for an additional hour with measurements, taken every 10 minutes. Otherwise, pre-soak (fill) overnight. Obtain at least twelve measurements per hole over at least six hours (approximately 30 minute intervals) with a precision of at least 0.25".

Trial No.	Start Time	End Time	Δt Time Interval (min)	D_0 Initial Depth to Water (in)	D_f Final Depth to Water (in)	ΔD Change in Water Level (in)	Percolation Rate (min/in)
1	10:32 AM	10:42 AM	10.00	42.6	45.4	2.8	3.62
2	10:45 AM	10:55 AM	10.00	42.6	46.2	3.6	2.78
3	11:03 AM	11:13 AM	10.00	42.6	46.3	3.7	2.69
4	11:16 AM	11:26 AM	10.00	42.6	46.3	3.7	2.69
5	11:28 AM	11:38 AM	10.00	42.6	46.3	3.7	2.69
6	11:41 AM	11:51 AM	10.00	42.6	46.6	4.0	2.53
7							
8							

Infiltration Rate Calculation:

Time Interval, Δt =	10.00	minutes	H_o =	17.4	inches
Final Depth to Water, D_f =	46.6	inches	H_f =	13.4	inches
Test Hole Radius, r =	4	inches	ΔH =	4.0	inches
Initial Depth to Water, D_0 =	42.6	inches	H_{avg} =	15.4	inches
Total Depth of Test Hole, D_t =	60	inches	$I_t = \frac{\Delta H(60r)}{\Delta t(r+2H_{avg})}$		
			Infiltration Rate, I_t =	**2.73**	**inches/hour**

GEOCON WEST, INC.

ENVIRONMENTAL GEOTECHNICAL MATERIALS
2807 MCGAW AVENUE - IRVINE, CALIFORNIA, 92614
PHONE: 949-491-6570

PERCOLATION TEST RESULTS AND CALCULATIONS

331 THE CITY DRIVE S
ORANGE, CALIFORNIA
OC YTC

DRAFTED BY: ACS	CHECKED BY: JTA	MAY 2024	PROJECT NO. W1857-88-01	FIG. 14

APPENDIX A

APPENDIX A

FIELD INVESTIGATION

The site was explored between February 7 and 13, 2024, by excavating eight 8-inch-diameter borings using a truck-mounted hollow-stem auger drilling machine and a limited access drilling machine to depths of 5 to 63.5 feet beneath the ground surface. Additionally, five borings were excavated using 3-inch hand augers to depths between 15 and 16½ feet beneath the ground surface. Additional site exploration was performed on May 2, 2024, by excavating two 8-inch diameter borings using a limited access drilling machine to depths of approximately 20.5 feet below the ground surface.

Representative and relatively undisturbed samples were obtained from them borings by driving a 3-inch, O. D., California Modified Sampler into the "undisturbed" soil mass with blows from a 140-pound auto-hammer falling 30 inches (hollow stem borings) or from a slide hammer (hand auger borings). The California Modified Sampler was equipped with 1-inch by 2⅜-inch diameter brass sampler rings to facilitate soil removal and testing. Standard Penetration Tests were performed and bulk samples were also obtained.

The soil conditions encountered in the borings were visually examined, classified and logged in general accordance with the Unified Soil Classification System (USCS). The logs of the borings are presented on Figures A1 through A15. The logs depict the soil and geologic conditions encountered and the depth at which samples were obtained. The logs also include our interpretation of the conditions between sampling intervals. Therefore, the logs contain both observed and interpreted data. We determined the lines designating the interface between soil materials on the logs using visual observations, penetration rates, excavation characteristics and other factors. The transition between materials may be abrupt or gradual. Where applicable, the logs were revised based on subsequent laboratory testing. Three Cone Penetrometer Tests (CPTs) were also advanced on February 12, 2024, to approximate depths of 63 to 100 feet below the ground surface using a truck-mounted 30-ton CPT rig. Logs of the CPTS are provided as Figures A16 and A17.

The approximate locations of the borings and CPTs are shown on Figure 2.

PROJECT NO. W1857-88-01

BORING A

ELEV. (MSL.) -- DATE COMPLETED **02/12/2024**

EQUIPMENT **HAND AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	BULK 0-5'				**ARTIFICIAL FILL** Silty Sand, loose, moist, brown, fine-grained.			
2					**ALLUVIUM**			
4	A@3'			SP	Sand, poorly graded, loose, moist, gray, fine-grained.		99.6	7.5
6	A@5'						102.2	10.2
8	A@7'			CL	Sandy Clay, firm, moist, brown, fine-grained.		96.8	24.5
10	A@10'			SM	Silty Sand, medium dense, moist, brown, fine- to medium-grained.		106.2	16.6
12								
14								
16	A@15'						97.2	8.1
					Total depth of boring: 16.5 feet Fill to 2 feet. No groundwater encountered. Backfilled with soil cuttings and tamped. *Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer. NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.			

W1857-88-01 BORING LOGS.GPJ

Figure A1,
Log of Boring A, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING B

ELEV. (MSL.) -- DATE COMPLETED **02/12/2024**

EQUIPMENT **HAND AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	BULK 0-5'				**ARTIFICIAL FILL** Silty Sand, loose, moist, brown, fine- to medium-grained.			
2					**ALLUVIUM** Silty Sand, loose, moist, gray, fine-grained.			
4	B@3'			SM				
6	B@5'				- loose, fine- to medium-grained		100.5	14.2
8	B@7'				Sand, poorly graded, loose, moist, brown, fine-grained.		104.0	19.1
10	B@10'			SP	- fine- to medium-grained		87.3	19.4
12								
14				SC	Clayey Sand, medium dense, moist, brown, fine- to medium-grained.			
					Silty Sand, loose, moist, brown, fine-grained.			
16	B@15'			SM			34.1	16.8
					Total depth of boring: 16 feet Fill to 2 feet. No groundwater encountered. Backfilled with soil cuttings and tamped. *Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer. NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.			

W1857-88-01 BORING LOGS.GPJ

Figure A2,
Log of Boring B, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING C

ELEV. (MSL.) -- DATE COMPLETED **02/09/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0					**ARTIFICIAL FILL** Silty Sand, loose, moist, dark brown, fine-grained.			
2					**ALLUVIUM** Silty Sand, loose, moist, gray, fine-grained.			
4								
6	C@5'			SM		12	100.2	13.7
8	C@7'					12	98.2	25.0
10	C@10'					10	88.6	22.4
12	C@12'				- medium dense	23	106.1	16.1
14	C@15'					25	94.6	9.9
					Total depth of boring: 15.5 feet Fill to 2 feet. No groundwater encountered. Backfilled with soil cuttings and tamped. *Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer. NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.			

W1857-88-01 BORING LOGS.GPJ

Figure A3,
Log of Boring C, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING D

ELEV. (MSL.) -- DATE COMPLETED **02/07/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	BULK 0-5'		**ARTIFICIAL FILL** Silty Sand, medium dense, moist, dark brown, fine- to medium-grained.			
			ALLUVIUM Sand, poorly graded, medium dense, moist, light brown, medium- to coarse-grained.			
6	D@5'	SP	- loose	17	91.3	3.7
8	D@7'			12	85.7	4.1
10	D@10'		- medium dense	20	104.1	5.5
12	D@12'			9	100.0	2.3
			Silty Sand, loose, moist, dark brown, fine- to medium-grained.			
16	D@15'	SM		13	92.1	10.2
20	D@20'	ML	Sandy Silt, firm, moist, brown, fine-grained.	20	95.3	24.8
			Total depth of boring: 20.5 feet Fill to 1 foot. No groundwater encountered. Backfilled with soil cuttings and tamped.			

*Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer.

NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.

W1857-88-01 BORING LOGS.GPJ

Figure A4,
Log of Boring D, Page 1 of 1

SAMPLE SYMBOLS

- ... SAMPLING UNSUCCESSFUL
- ... STANDARD PENETRATION TEST
- ... DRIVE SAMPLE (UNDISTURBED)
- ... DISTURBED OR BAG SAMPLE
- ... CHUNK SAMPLE
- ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING E

ELEV. (MSL.) -- DATE COMPLETED **02/08/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	BULK 0-5'				**ARTIFICIAL FILL** Silty Sand, loose, moist, dark brown.			
2					**ALLUVIUM** Sandy Silt, stiff, moist, gray, fine- to medium-grained.			
4								
6	E@5'					18	92.1	23.9
8	E@7.5'			ML	- brown, fine-grained	4		
10	E@10'				- stiff, slightly moist, fine- to medium-grained	22	109.4	17.4
12	E@12.5'				- firm, fine-grained	10		
14								
16	E@15'				Silty Sand, medium dense, slightly moist, brown, fine- to medium-grained.	29	96.2	8.5
18	E@17'			SM	- loose	10		
20	E@20'				- medium dense	43	99.1	1.1
22	E@22.5'				Sand, poorly graded, medium dense, slightly moist, gray, fine-grained.	17		
24				SP				
26	E@25'				- loose	14	73.8	12.4
28	E@27.5'			SM	Silty Sand, medium dense, slightly moist, gray, fine-grained.	18		

W1857-88-01 BORING LOGS.GPJ

Figure A5,
Log of Boring E, Page 1 of 2

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◹ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING E

ELEV. (MSL.) -- DATE COMPLETED **02/08/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
30	E@30'			SM	- fine- to medium-grained.	48	106.6	10.2
32	E@32.5'			SP	Sand, poorly graded, medium dense, slightly moist, gray, fine- to medium-grained.	25		
34	E@35'				- dense	63	104.0	4.7
36								
38	E@37.5'				- medium dense, fine-grained	29		
40	E@40'					40	91.0	29.5
42	E@42.5'			SM	Silty Sand, medium dense, slightly moist, gray, fine- to medium-grained.	25		
44								
46								
48	E@47.5'			ML	Sandy Silt, soft, moist, brown, fine-grained.	6		

Total depth of boring: 48.5 feet
Fill to 2 feet.
No groundwater encountered.
Backfilled with soil cuttings and tamped.

*Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer.
NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.

W1857-88-01 BORING LOGS.GPJ

Figure A5,
Log of Boring E, Page 2 of 2

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING F

ELEV. (MSL.) -- DATE COMPLETED **02/08/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	BULK 0-5'				**ARTIFICIAL FILL** Silty Sand, loose to medium dense, moist, dark brown.			
2					**ALLUVIUM** Sand, poorly graded, loose, moist, light brown, medium- to coarse-grained.			
4								
6	F@5'					6		
8	F@7.5'			SP	- gray	14	97.2	3.7
10	F@10'				- yellowish brown	7		
12	F@12.5'				- fine- to medium-grained	16	94.1	4.1
14								
16	F@15'				- medium dense, grayish brown	11		
18	F@17.5'				Sandy Silt, soft, moist, brown, fine-grained.	8	86.7	30.5
20	F@20'			ML	- firm	10		
22	F@22.5'				Silty Sand, medium dense, slightly moist, grayish brown, fine- to medium-grained.	37	105.3	5.3
24				SM				
26	F@25'				Sandy Silt, soft, moist, brown, fine-grained.	7		
28	F@27.5'			ML	- firm	17	109.5	19.3

W1857-88-01 BORING LOGS.GPJ

Figure A6,
Log of Boring F, Page 1 of 3

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◥ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING F

ELEV. (MSL.) -- DATE COMPLETED **02/08/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
30	F@30'			SP	Sand, poorly graded, medium dense, slightly moist, light brown, fine-grained.	23		
32	F@32.5'			SP		50	111.1	11.1
34								
36	F@35'			SM	Silty Sand, loose, slightly moist, light brown, fine-grained.	7		
38	F@37.5'			SP	Sand, poorly graded, medium dense, slightly moist, yellowish brown, medium- to coarse-grained.	35	103.4	2.2
40	F@40'			ML	Sandy Silt, firm, moist, brown, fine-grained.	16		
42	F@42.5'			SM	Silty Sand, dense, slightly moist, gray, mottled reddish brown.	63	103.1	8.5
44	F@45'			SM		15		
46								
48								
50	F@50'		▼	ML	Sandy Silt, firm, slightly moist, brown.	9		
52								
54								
56	F@55'			SM	Silty Sand, dense, wet, brown, some fine gravel.	35		
58								

W1857-88-01 BORING LOGS.GPJ

Figure A6,
Log of Boring F, Page 2 of 3

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◥ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	**BORING F** ELEV. (MSL.) -- DATE COMPLETED **02/08/2024** EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
					MATERIAL DESCRIPTION			
60	F@60'			GW	Gravel, dense, wet, brown to black, fine to coarse gravel, some medium- to coarse-grained sand.	29		11.5
					Total depth of boring: 61 feet Fill to 2 feet. Groundwater encountered at 54 feet. Backfilled with soil cuttings and tamped. *Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer. NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.			

W1857-88-01 BORING LOGS.GPJ

Figure A6,
Log of Boring F, Page 3 of 3

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

PROJECT NO. W1857-88-01

BORING G

ELEV. (MSL.) -- DATE COMPLETED **02/09/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0					**ARTIFICIAL FILL** Silty Sand, loose, moist, brown to dark brown, fine-grained.			
2								
4				SM	**ALLUVIUM** Silty Sand, loose, moist, gray, fine-grained.			
6	G@5'				Sandy Silt, soft, moist, brown, fine-grained.	8		
8	G@7'			ML		9	98.1	23.4
10	G@10'					6	96.8	21.6
					Total depth of boring: 10.5 feet Fill to 2 feet. No groundwater encountered. Backfilled with soil cuttings and tamped. *Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer. NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.			

W1857-88-01 BORING LOGS.GPJ

Figure A7,
Log of Boring G, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING H

ELEV. (MSL.) -- DATE COMPLETED **02/09/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0					**ARTIFICIAL FILL** Silty Sand, loose, moist, dark brown, fine-grained.			
2					**ALLUVIUM** Sand, poorly graded, loose, moist, brown, medium- to coarse-grained.			
4								
6	H@5'					16	101.4	2.8
8	H@7'				- slightly moist	18	95.3	5.4
10	H@10'			SP		13	99.8	5.5
12	H@12'				- medium dense	19	100.4	5.2
14								
16	H@15'					32	98.9	8.8
18								
20	H@20'			SM	Silty Sand, medium dense, slightly moist, brown, fine-grained.	20	100.0	9.2

Total depth of boring: 20.5 feet
Fill to 2 feet.
No groundwater encountered.
Backfilled with soil cuttings and tamped.

*Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer.
NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.

W1857-88-01 BORING LOGS.GPJ

Figure A8,
Log of Boring H, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◥ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING I

ELEV. (MSL.) -- DATE COMPLETED **02/08/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0					**ARTIFICIAL FILL** Sandy Silt, firm, moist, dark brown, fine-grained.			
2					**ALLUVIUM** Sand, well-graded, loose, moist, brown.			
4				SW				
6	I@5'					14		
8	I@7.5'				Sandy Clay, soft, moist, dark brown, fine-grained.	5		
10	I@10'			CL	- firm	13	105.6	20.2
12	I@12.5'				- soft	5		
14								
16	I@15'			SM	Silty Sand, loose, moist, brown, fine-grained.	16		
18	I@17.5'			CL	Silty Clay, soft, moist, dark brown.	5		
20	I@20'			SM	Silty Sand, medium dense, slightly moist, grayish brown, fine-grained.	15	89.4	32.6
22	I@22.5'				- loose	7		
24								
26	I@25'			ML	Silt, soft, moist, brown.	9		
28	I@27.5'			SM	Silty Sand, medium dense, slightly moist, grayish brown, fine-grained.	12		

W1857-88-01 BORING LOGS.GPJ

Figure A9,
Log of Boring I, Page 1 of 3

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◥ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

PROJECT NO. W1857-88-01

BORING I

ELEV. (MSL.) -- DATE COMPLETED **02/08/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
30	I@30'			SM		33	107.7	9.5
32	I@32.5'			CL	Sandy Clay, very soft, moist, brown, fine-grained.	PUSH		
34	I@35'					11		
36								
38	I@37.5'			SM	Silty Sand, medium dense, slightly moist, gray, fine-grained.	24		
40	I@40'					26	102.2	7.4
42	I@42.5'			ML	Sandy Silt, firm, slightly moist, gray, fine-grained.	9		
44	I@45'					16	77.6	37.9
46								
48	I@47.5'			CL	Sandy Clay, soft, moist, fine-grained, trace fine gravel.	5		
50	I@50'				- no recovery	11		
52	I@52.5'		▼	SM	- groundwater encountered at 53'11" Silty Sand, dense, moist, brown, medium-grained, some fine gravel. - groundwater encountered	43		6.4
54	I@55'				- medium dense, wet	50	118.0	15.8
56								
58	I@57.5'			GP	Gravel, dense, wet, brown.	40		7.7

W1857-88-01 BORING LOGS.GPJ

Figure A9,
Log of Boring I, Page 2 of 3

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◥ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	**BORING I** ELEV. (MSL.) -- DATE COMPLETED **02/08/2024** EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
					MATERIAL DESCRIPTION			
60	I@60'			SC	Clayey Sand, wet, brown, medium-grained, some fine gravel, trace silt.	50 (5")	128.9	11.1
62	I@62.5'			CL	Clay, firm, wet, brown, trace medium-grained sand.	14		
					Total depth of boring: 63.5 feet Fill to 2 feet. Groundwater encountered at 53 feet 11 inches. Backfilled with soil cuttings and tamped. *Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer. NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.			

W1857-88-01 BORING LOGS.GPJ

Figure A9,
Log of Boring I, Page 3 of 3

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING J

ELEV. (MSL.) -- DATE COMPLETED **02/13/2024**

EQUIPMENT **HAND AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0					**ARTIFICIAL FILL** Silty Sand, loose, moist, brown, fine- to medium-grained.			
2	J@3'						119.4	8.6
4				SM	**ALLUVIUM** Silty Sand, medium dense, moist, some fine-grained.			
6	J@5'			SP	Sand, poorly graded, loose, slightly moist, dark brown, medium-grained.		99.7	4.3
8	J@7'						100.6	6.9
10	J@10'			CL	Sandy Clay, firm, slightly moist, brown, fine-grained.		99.2	22.2
12								
14								
16	J@15'						98.5	20.0
					Total depth of boring: 16 feet 4 inches Fill to 3.5 feet. No groundwater encountered. Backfilled with soil cuttings and tamped. Asphalt patched. *Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer. NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.			

W1857-88-01 BORING LOGS.GPJ

Figure A10,
Log of Boring J, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING K

ELEV. (MSL.) -- DATE COMPLETED **02/12/2024**

EQUIPMENT **HAND AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0					**ARTIFICIAL FILL** Silty Sand, loose, moist, brown, some coarse gravel.			
2	K@3'							
4				SM	**ALLUVIUM** Silty Sand, loose, moist, brown, fine- to medium-grained.			
6	K@5'			SP	Sand, poorly graded, loose, slightly moist, light brown, medium- to coarse-grained.		103.6	4.2
8	K@7'				- coarse-grained		105.6	7.7
10	K@10'			CL	Sandy Clay, firm, slightly moist, brown, fine-grained.		96.2	26.2
12								
14								
16	K@15'						102.2	24.0
					Total depth of boring: 16.5 feet Fill to 3.5 feet. No groundwater encountered. Backfilled with soil cuttings and tamped. Asphalt patched. *Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer. NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.			

W1857-88-01 BORING LOGS.GPJ

Figure A11,
Log of Boring K, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING L

ELEV. (MSL.) -- DATE COMPLETED **02/09/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0					**ARTIFICIAL FILL** Silty Sand, loose, moist, dark brown, fine-grained.			
2				SP	**ALLUVIUM** Sand, poorly graded, loose, moist, gray, fine-grained.			
4								
6	L@5'			ML	Sandy Silt, soft, moist, brown, fine-grained.	12		
8	L@7'			SM	Silty Sand, very loose, moist, grayish brown, fine-grained.	5	78.0	30.7
10	L@10'					22	95.6	3.6

Total depth of boring: 10.5 feet
Fill to 2 feet.
No groundwater encountered.
Percolation testing performed.
Backfilled with soil cuttings and tamped.

*Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer.
NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.

W1857-88-01 BORING LOGS.GPJ

Figure A12,
Log of Boring L, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	**BORING M** ELEV. (MSL.) -- DATE COMPLETED **02/09/2024** EQUIPMENT **HAND AUGER** BY: **ACS**	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
					MATERIAL DESCRIPTION			
0	BULK 0-5'				**ARTIFICIAL FILL** Silty Sand, loose, moist, dark brown.			
2				SM	**ALLUVIUM** Silty Sand, loose, moist, grayish brown.			
4								
					Total depth of boring: 5 feet Fill to 2 feet. No groundwater encountered. Percolation testing performed. Backfilled with soil cuttings and tamped. *Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer. NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.			

W1857-88-01 BORING LOGS.GPJ

Figure A13,
Log of Boring M, Page 1 of 1

SAMPLE SYMBOLS

☐ ... SAMPLING UNSUCCESSFUL ◧ ... STANDARD PENETRATION TEST ■ ... DRIVE SAMPLE (UNDISTURBED)

⊠ ... DISTURBED OR BAG SAMPLE ◥ ... CHUNK SAMPLE ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING N

ELEV. (MSL.) -- DATE COMPLETED **05/02/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	BULK 0-5'				**ARTIFICIAL FILL** Silty Sand, loose, dry, brown, fine-grained, roots, trace fine-grained.			
2				SP	**ALLUVIUM** Sand, poorly graded, loose, dry, brown, fine- to medium-grained, trace fine gravel.			
4				SM	Silty Sand, loose, dry, brown, fine-grained.			
6	BN@5'			SP	Sand, poorly graded, loose, dry, brown, fine- to medium-grained.	18	98.5	5.6
8	BN@7'			ML	Sandy Silt, soft, moist, brown, fine-grained.	4	84.6	26.4
10	BN@10'			ML	- trace clay	9	98.9	23.9
12	BN@12'			ML	Clayey Silt, soft, moist, brown.	11	103.7	21.3
16	BN@15'			SM	Silty Sand, loose, slightly moist, brown, fine-grained.	18	102.4	20.5
20	BN@20'			SM	- medium dense	28	97.3	8.1

Total depth of boring: 20.5 feet
Fill to 2 feet.
No groundwater encountered.
Backfilled with soil cuttings and tamped.

*Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer.
NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.

W1857-88-01 BORING LOGS.GPJ

Figure A14,
Log of Boring N, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

PROJECT NO. W1857-88-01

BORING O

ELEV. (MSL.) -- DATE COMPLETED **05/02/2024**

EQUIPMENT **HOLLOW STEM AUGER** BY: **ACS**

DEPTH IN FEET	SAMPLE NO.	LITHOLOGY	GROUNDWATER	SOIL CLASS (USCS)	MATERIAL DESCRIPTION	PENETRATION RESISTANCE (BLOWS/FT*)	DRY DENSITY (P.C.F.)	MOISTURE CONTENT (%)
0	BULK 0-5'				**ARTIFICIAL FILL** Silty Sand, loose, slightly moist, brown, fine-grained, trace fine gravel and roots.			
2					**ALLUVIUM** Sand, poorly graded, loose, slightly moist, brown, fine- to medium-grained.			
4								
6	BO@5'				- fine-grained	13	93.4	9.1
8	BO@7'					12	94.3	3.9
10	BO@10'			SP	- gray, medium-grained	19	100.3	4.0
12	BO@12'				- no recovery	33		
14								
16	BO@15'				- medium dense	29	106.7	3.5
18								
20	BO@20'			ML SM	Sandy Silt, firm, moist, brown, fine-grained. Silty Sand, loose, moist, brown, fine-grained.	15	91.1	32.6

Total depth of boring: 20.5 feet
Fill to 2 feet.
No groundwater encountered.
Backfilled with soil cuttings and tamped.

*Penetration resistance for 140-pound hammer falling 30 inches by auto-hammer.
NOTE: The stratification lines presented herein represent the approximate boundary between earth types; the transitions may be gradual.

W1857-88-01 BORING LOGS.GPJ

Figure A15,
Log of Boring O, Page 1 of 1

SAMPLE SYMBOLS

- ☐ ... SAMPLING UNSUCCESSFUL
- ◧ ... STANDARD PENETRATION TEST
- ■ ... DRIVE SAMPLE (UNDISTURBED)
- ⊠ ... DISTURBED OR BAG SAMPLE
- ◪ ... CHUNK SAMPLE
- ▼ ... WATER TABLE OR SEEPAGE

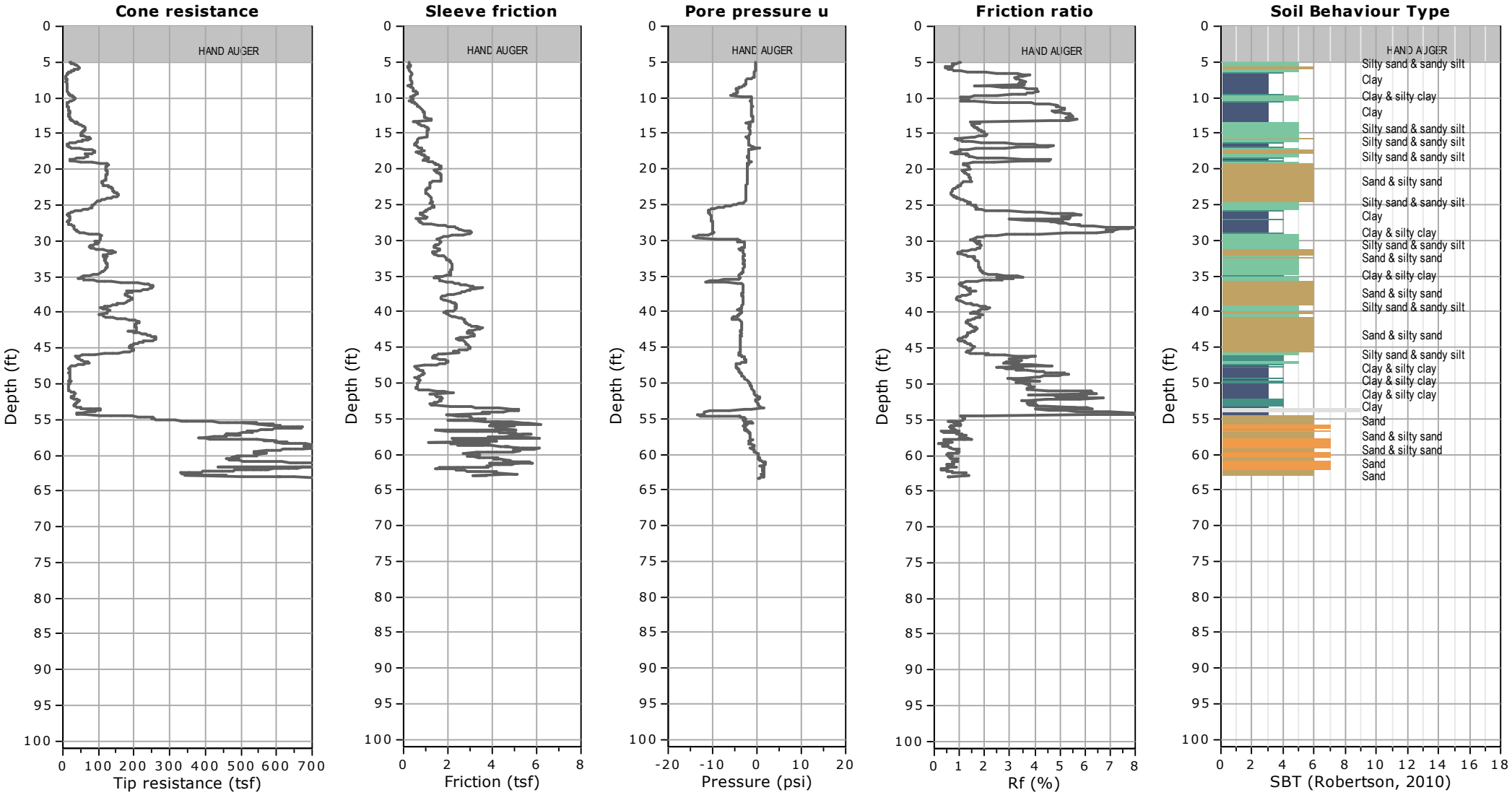
NOTE: THE LOG OF SUBSURFACE CONDITIONS SHOWN HEREON APPLIES ONLY AT THE SPECIFIC BORING OR TRENCH LOCATION AND AT THE DATE INDICATED. IT IS NOT WARRANTED TO BE REPRESENTATIVE OF SUBSURFACE CONDITIONS AT OTHER LOCATIONS AND TIMES.

GEOCON

Kehoe Testing and Engineering
714-901-7270
steve@kehoetesting.com
www.kehoetesting.com

Project: **Geocon West / Juvenille Hall - Youth Transition Center**
Location: **331 The City Drive S, Orange, CA**

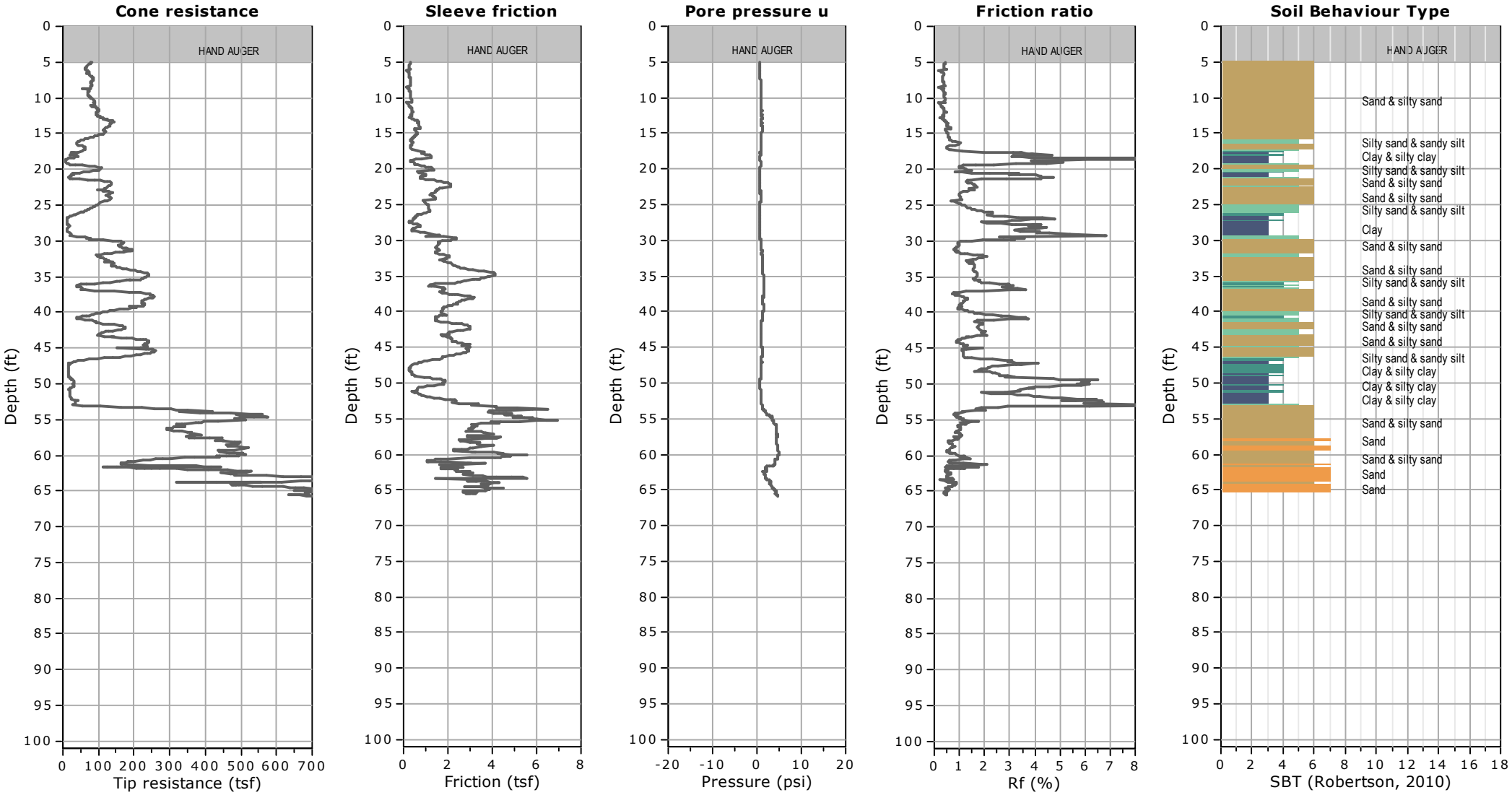
CPT-1
Total depth: 63.40 ft, Date: 2/12/2024



Kehoe Testing and Engineering
714-901-7270
steve@kehoetesting.com
www.kehoetesting.com

Project: **Geocon West / Juvenille Hall - Youth Transition Center**
Location: **331 The City Drive S, Orange, CA**

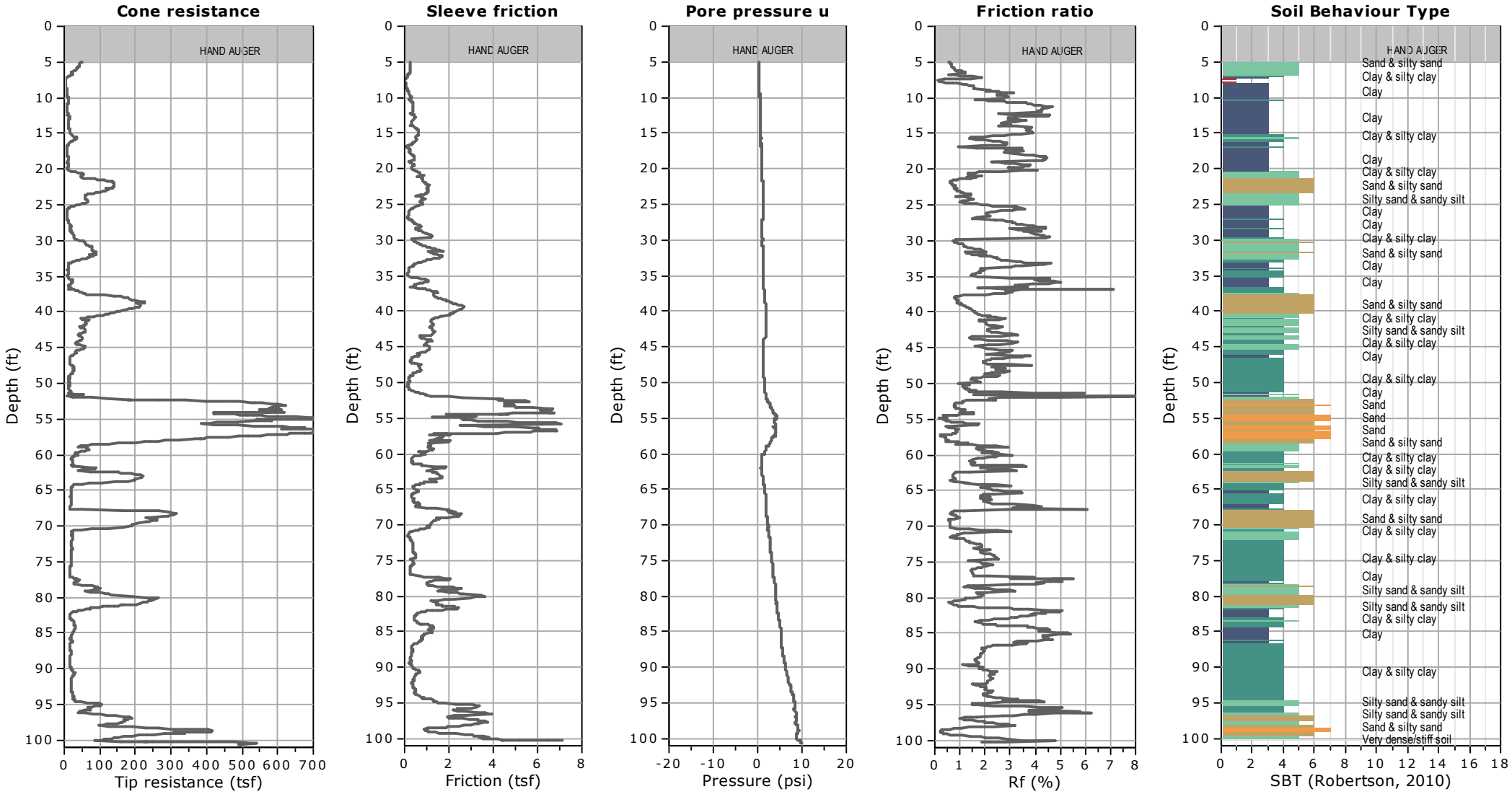
CPT-2
Total depth: 65.96 ft, Date: 2/12/2024



Kehoe Testing and Engineering
714-901-7270
steve@kehoetesting.com
www.kehoetesting.com

Project: **Geocon West / Juvenille Hall - Youth Transition Center**
Location: **331 The City Drive S, Orange, CA**

CPT-3
Total depth: 100.60 ft, Date: 2/12/2024



APPENDIX B

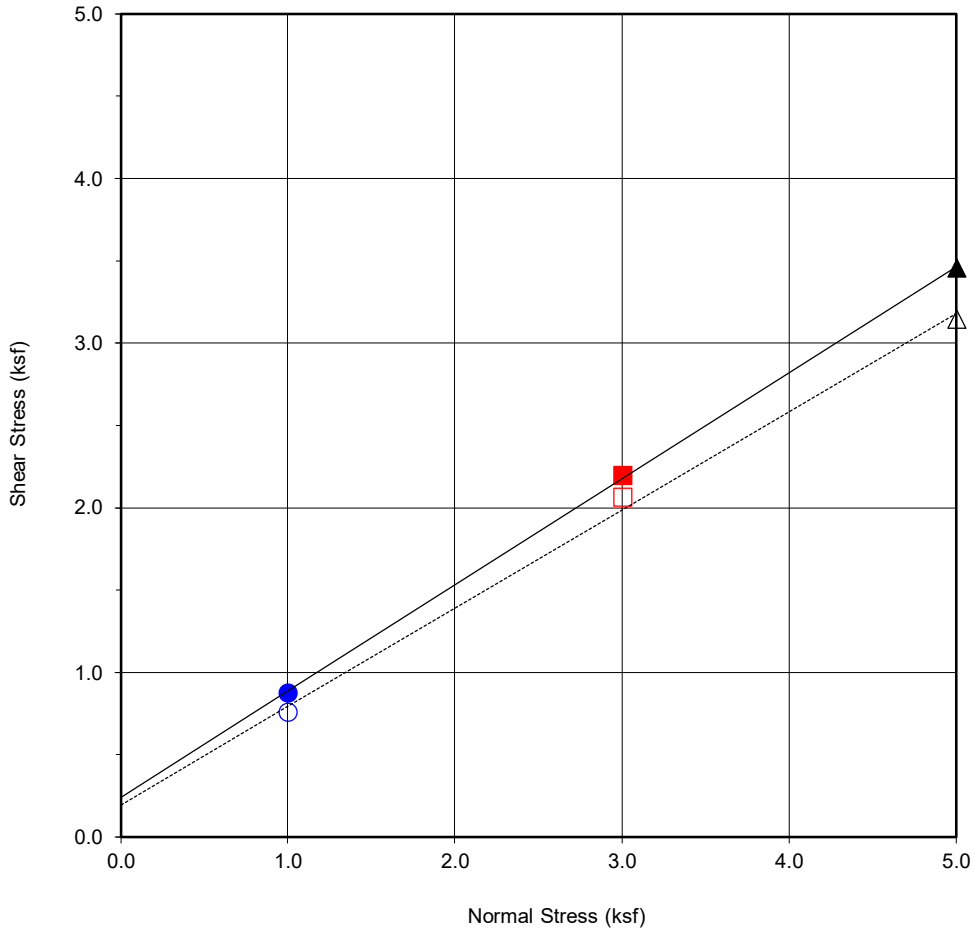
APPENDIX B

LABORATORY TESTING

We performed laboratory tests in accordance with generally accepted test methods of the American Society for Testing and Materials (ASTM) or other suggested procedures. We tested selected soil samples for direct shear strength, consolidation and expansion characteristics, corrosivity, and maximum dry density and optimum moisture content relationship. The in-place dry density and moisture content of the samples tested are presented on the boring logs, Appendix A.

The results of the laboratory tests from the March 2024 site exploration are summarized in Figures B1 through B30.

The results of the laboratory tests from the May 2024 site exploration are summarized in Figures B31 through B38.



Boring No.	**B**
Sample No.	**B@3'**
Depth (ft)	**3'**
Sample Type:	Ring

Soil Identification:		
Silty Sand (SM)		
Strength Parameters		
	C (psf)	ϕ (^{o})
Peak	241	33
Ultimate	197	31

Normal Stress (kip/ft²)	1	3	5
Peak Shear Stress (kip/ft²)	● 0.88	■ 2.20	▲ 3.46
Shear Stress @ End of Test (ksf)	○ 0.76	□ 2.06	△ 3.14
Deformation Rate (in./min.)	0.05	0.05	0.05
Initial Sample Height (in.)	1.0	1.0	1.0
Ring Inside Diameter (in.)	2.375	2.375	2.375
Initial Moisture Content (%)	13.7	14.6	13.2
Initial Dry Density (pcf)	97.5	97.1	101.4
Initial Degree of Saturation (%)	50.7	53.3	53.8
Soil Height Before Shearing (in.)	1.2	1.2	1.2
Final Moisture Content (%)	21.5	21.2	19.7

GEOCON

DIRECT SHEAR TEST RESULTS

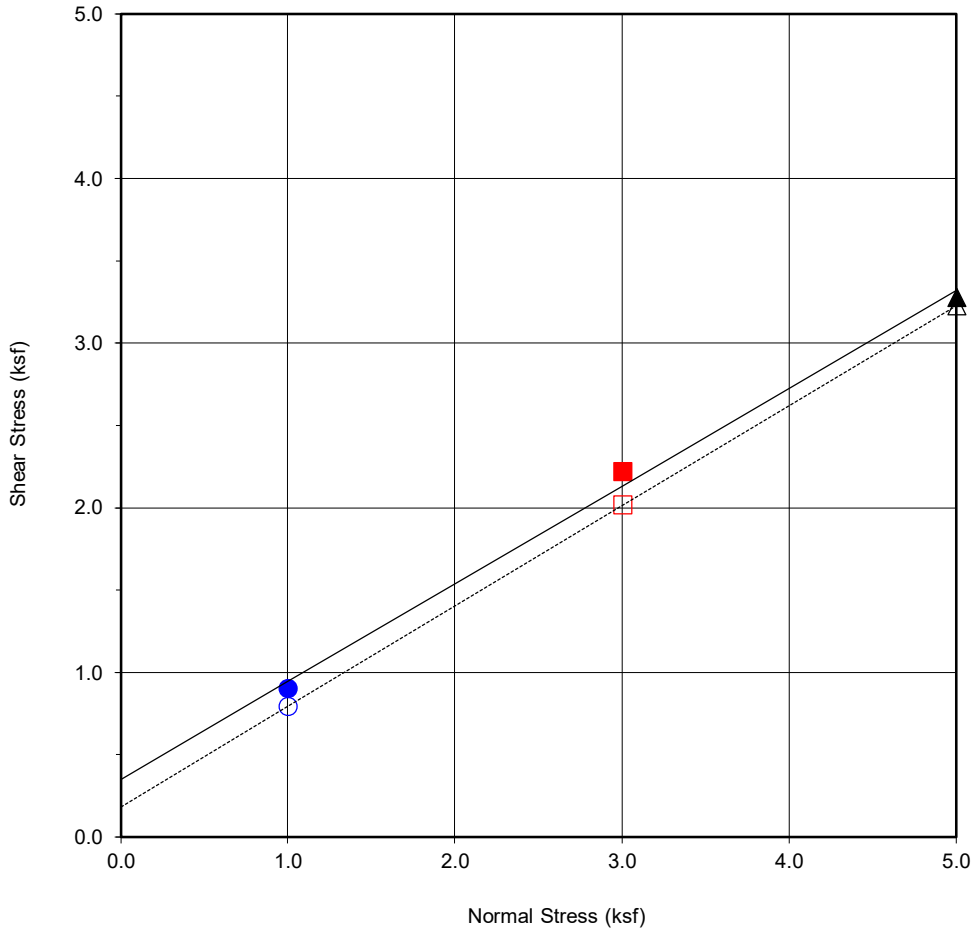
Consolidated Drained ASTM D-3080

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B1



Boring No.	**G**
Sample No.	**G@5'**
Depth (ft)	**5'**
Sample Type:	Ring

Soil Identification:		
Sandy Silt (ML)		
Strength Parameters		
	C (psf)	ϕ (^{o})
Peak	350	31
Ultimate	185	31

Normal Stress (kip/ft²)	1	3	5
Peak Shear Stress (kip/ft²)	● 0.90	■ 2.22	▲ 3.28
Shear Stress @ End of Test (ksf)	○ 0.79	□ 2.02	△ 3.23
Deformation Rate (in./min.)	0.05	0.05	0.05
Initial Sample Height (in.)	1.0	1.0	1.0
Ring Inside Diameter (in.)	2.375	2.375	2.375
Initial Moisture Content (%)	36.2	46.1	42.5
Initial Dry Density (pcf)	88.6	84.3	86.7
Initial Degree of Saturation (%)	108.2	124.5	121.6
Soil Height Before Shearing (in.)	1.2	1.2	1.2
Final Moisture Content (%)	32.6	33.0	32.7

GEOCON

DIRECT SHEAR TEST RESULTS

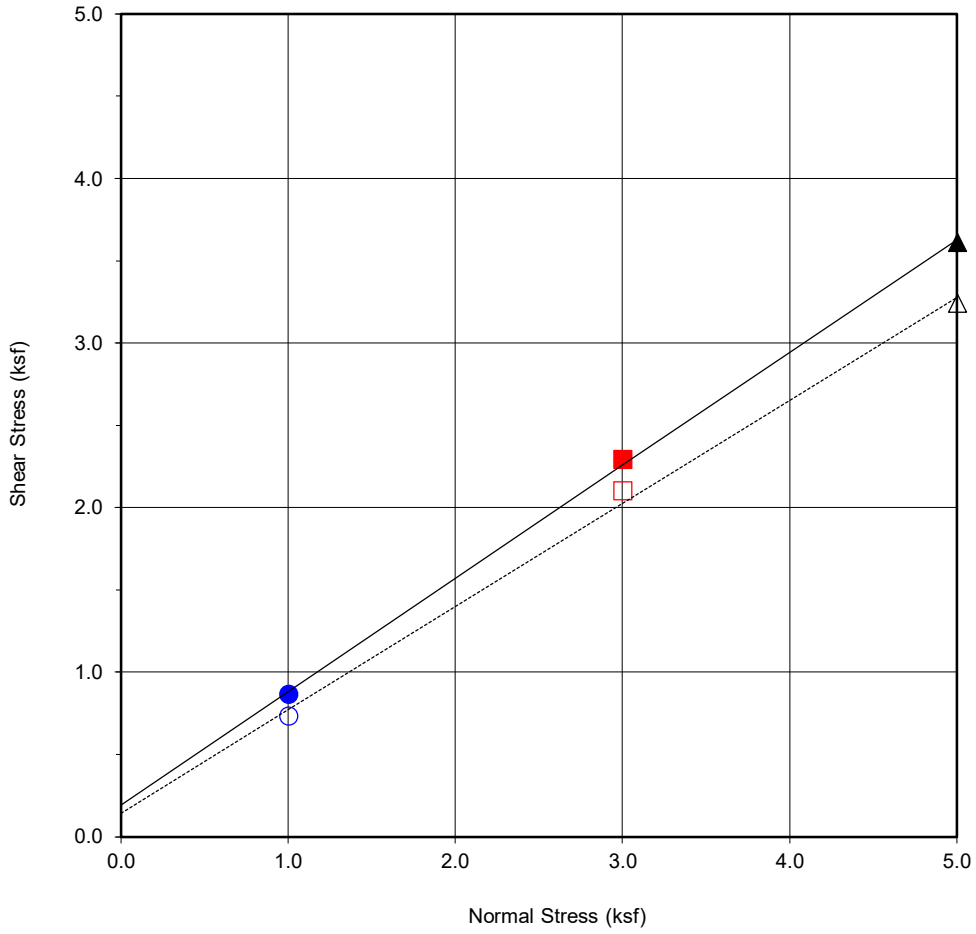
Consolidated Drained ASTM D-3080

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B2



Boring No.	**K**
Sample No.	**K@3'**
Depth (ft)	**3'**
Sample Type:	Ring

Soil Identification:		
Silty Sand (SM)		
Strength Parameters		
	C (psf)	ϕ (^{o})
Peak	195	34
Ultimate	143	32

Normal Stress (kip/ft²)	1	3	5
Peak Shear Stress (kip/ft²)	● 0.86	■ 2.29	▲ 3.61
Shear Stress @ End of Test (ksf)	○ 0.73	□ 2.10	△ 3.24
Deformation Rate (in./min.)	0.05	0.05	0.05
Initial Sample Height (in.)	1.0	1.0	1.0
Ring Inside Diameter (in.)	2.375	2.375	2.375
Initial Moisture Content (%)	20.6	13.7	17.8
Initial Dry Density (pcf)	85.5	91.7	87.4
Initial Degree of Saturation (%)	57.4	44.1	51.7
Soil Height Before Shearing (in.)	1.2	1.2	1.2
Final Moisture Content (%)	28.2	25.1	26.5

GEOCON

DIRECT SHEAR TEST RESULTS

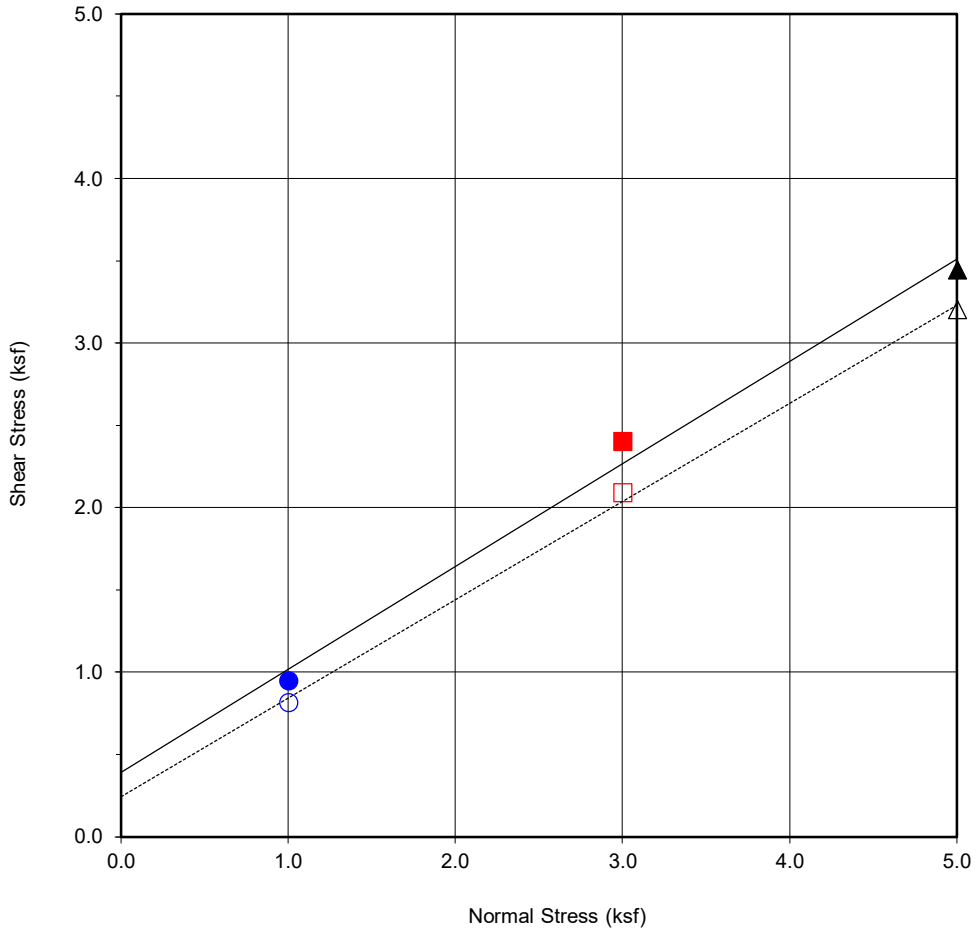
Consolidated Drained ASTM D-3080

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B3



Boring No.	**L**
Sample No.	**L@5'**
Depth (ft)	**5'**
Sample Type:	Ring

Soil Identification:		
Sandy Silt (ML)		
Strength Parameters		
	C (psf)	ϕ (^{o})
Peak	392	32
Ultimate	245	31

Normal Stress (kip/ft²)	1	3	5
Peak Shear Stress (kip/ft²)	● 0.95	■ 2.40	▲ 3.44
Shear Stress @ End of Test (ksf)	○ 0.82	□ 2.09	△ 3.20
Deformation Rate (in./min.)	0.05	0.05	0.05
Initial Sample Height (in.)	1.0	1.0	1.0
Ring Inside Diameter (in.)	2.375	2.375	2.375
Initial Moisture Content (%)	15.4	14.9	15.6
Initial Dry Density (pcf)	85.6	86.9	88.2
Initial Degree of Saturation (%)	43.0	42.9	46.2
Soil Height Before Shearing (in.)	1.2	1.2	1.2
Final Moisture Content (%)	29.9	29.4	29.0

GEOCON

DIRECT SHEAR TEST RESULTS

Consolidated Drained ASTM D-3080

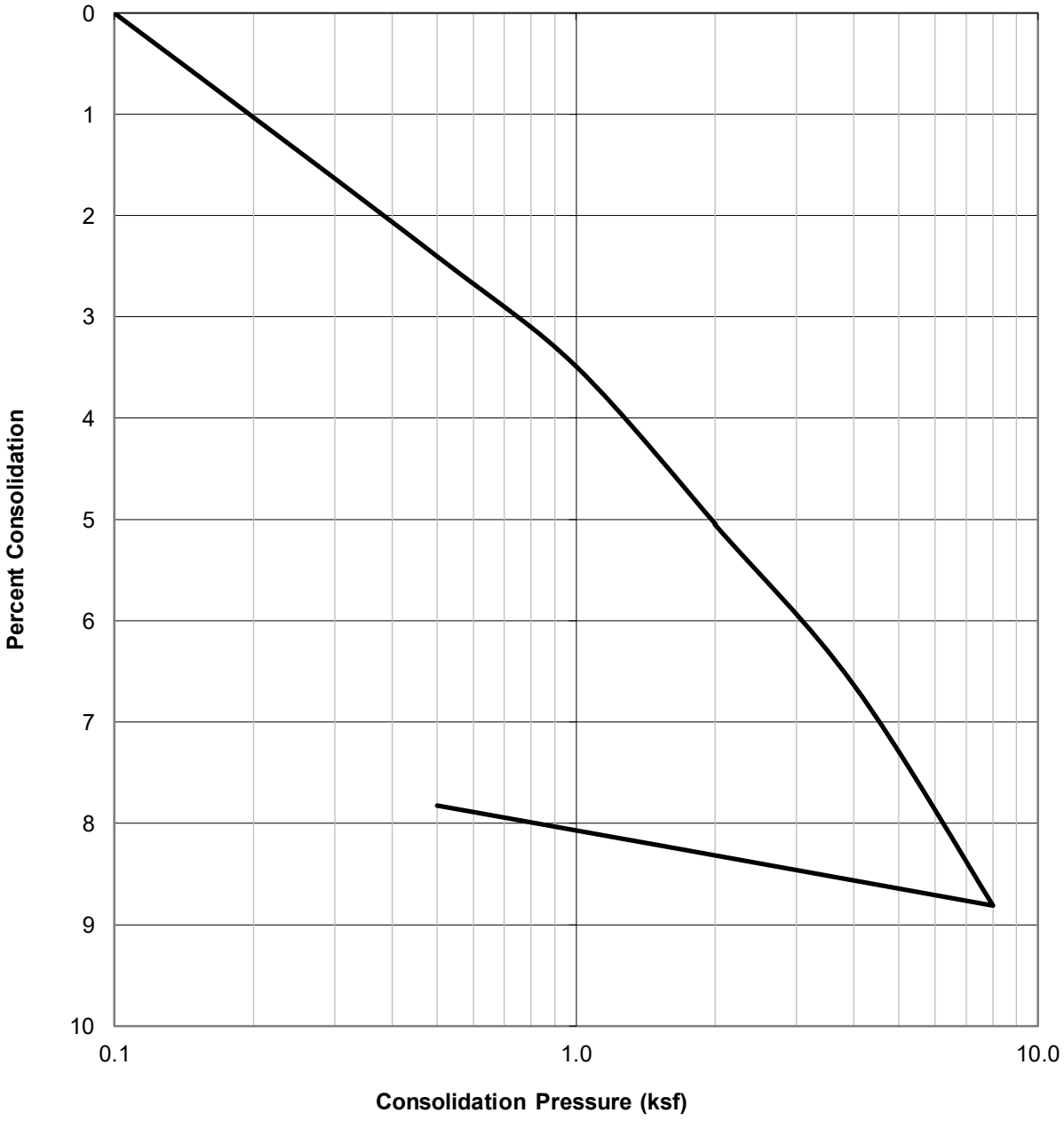
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B4

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
A@7	Sandy Clay (CL)	101.4	24.8	21.4

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

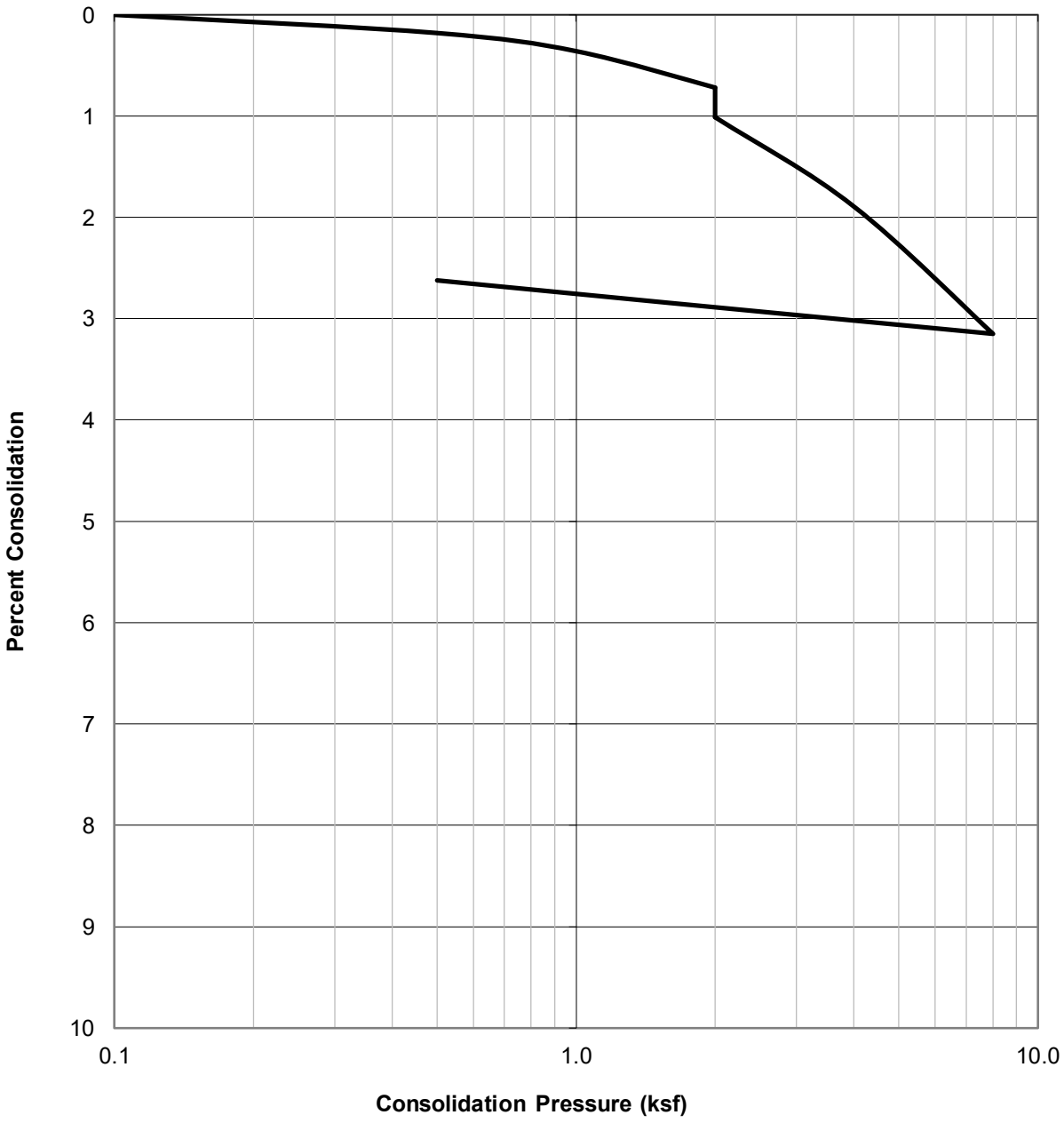
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B5

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
B@3	Silty Sand (SM)	97.8	10.4	21.7

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

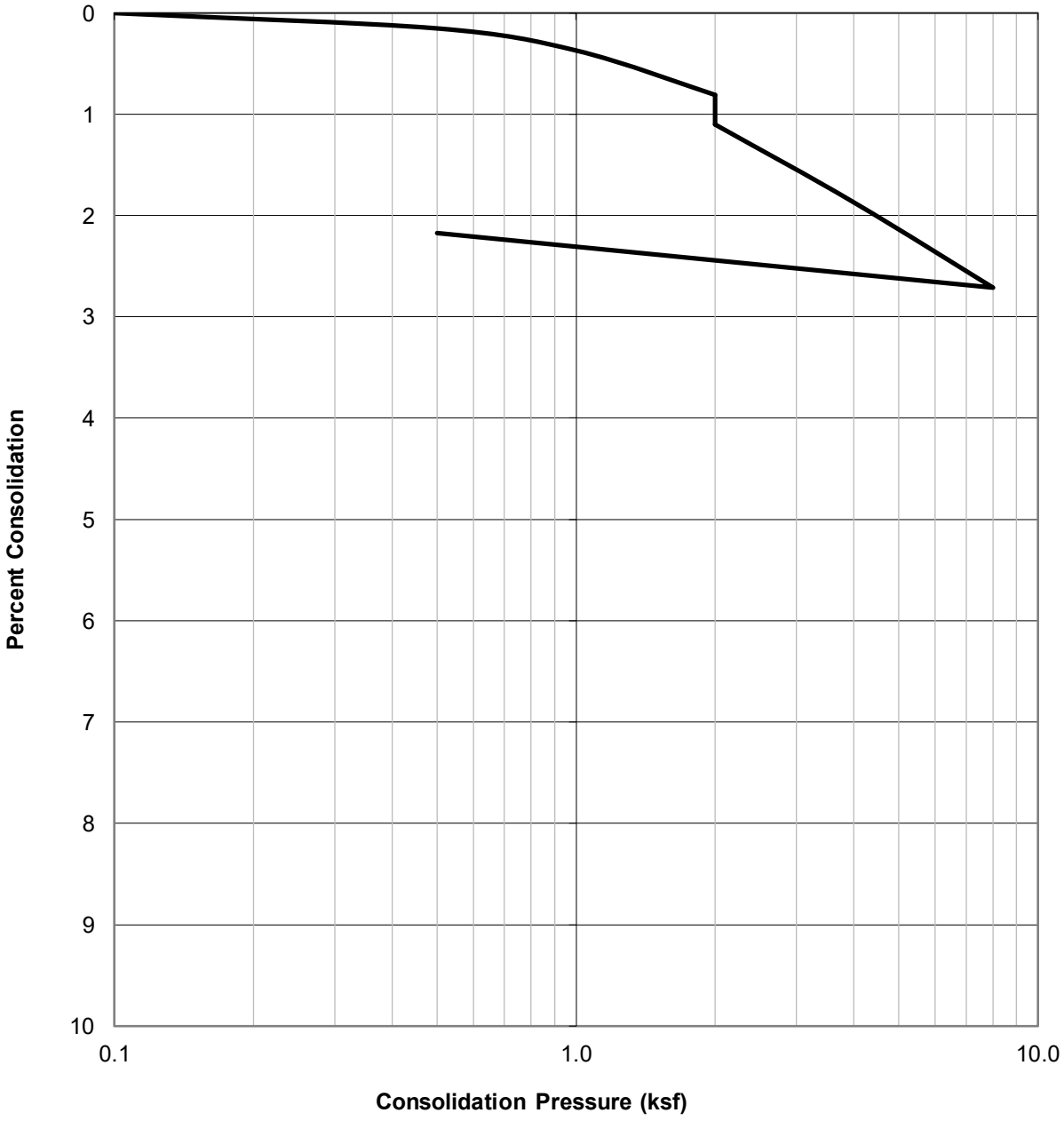
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B6

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
F@7.5	Sand (SP)	92.6	5.5	28.1

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

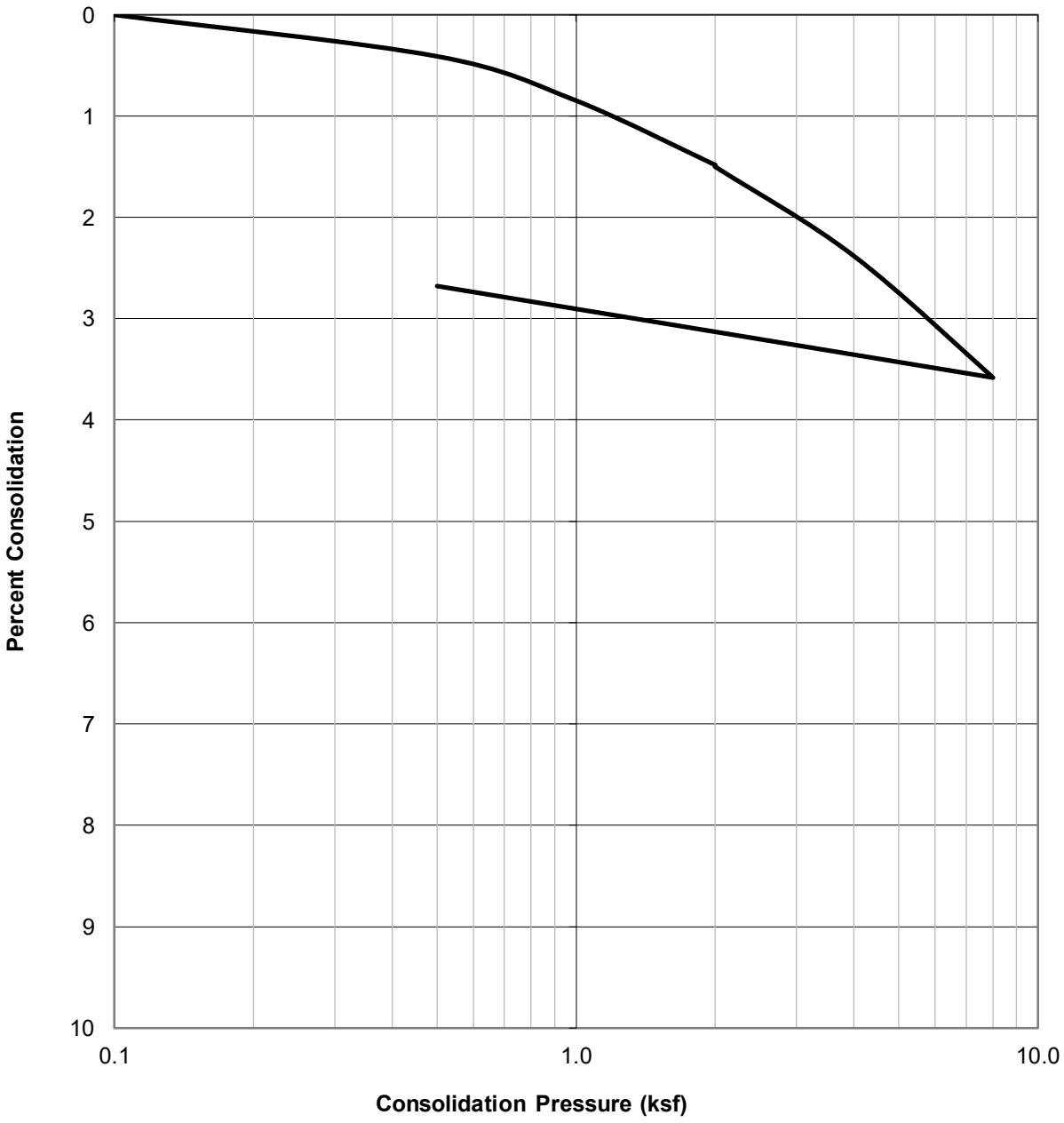
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B7

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
G@5	Sandy Silt (ML)	95.1	29.9	29.9

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

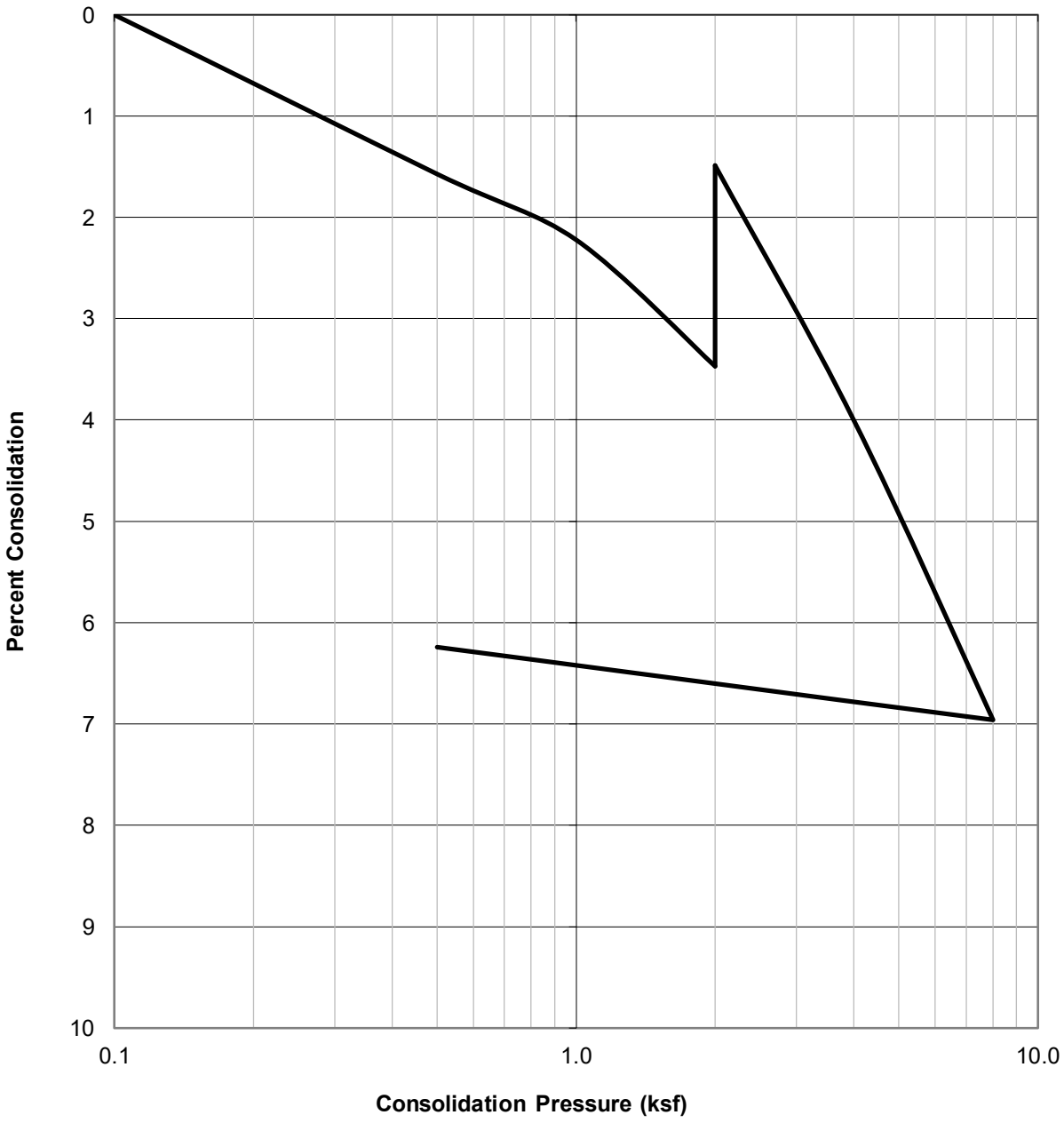
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B8

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
G@7	Sandy Silt (ML)	102.7	23.6	19.8

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

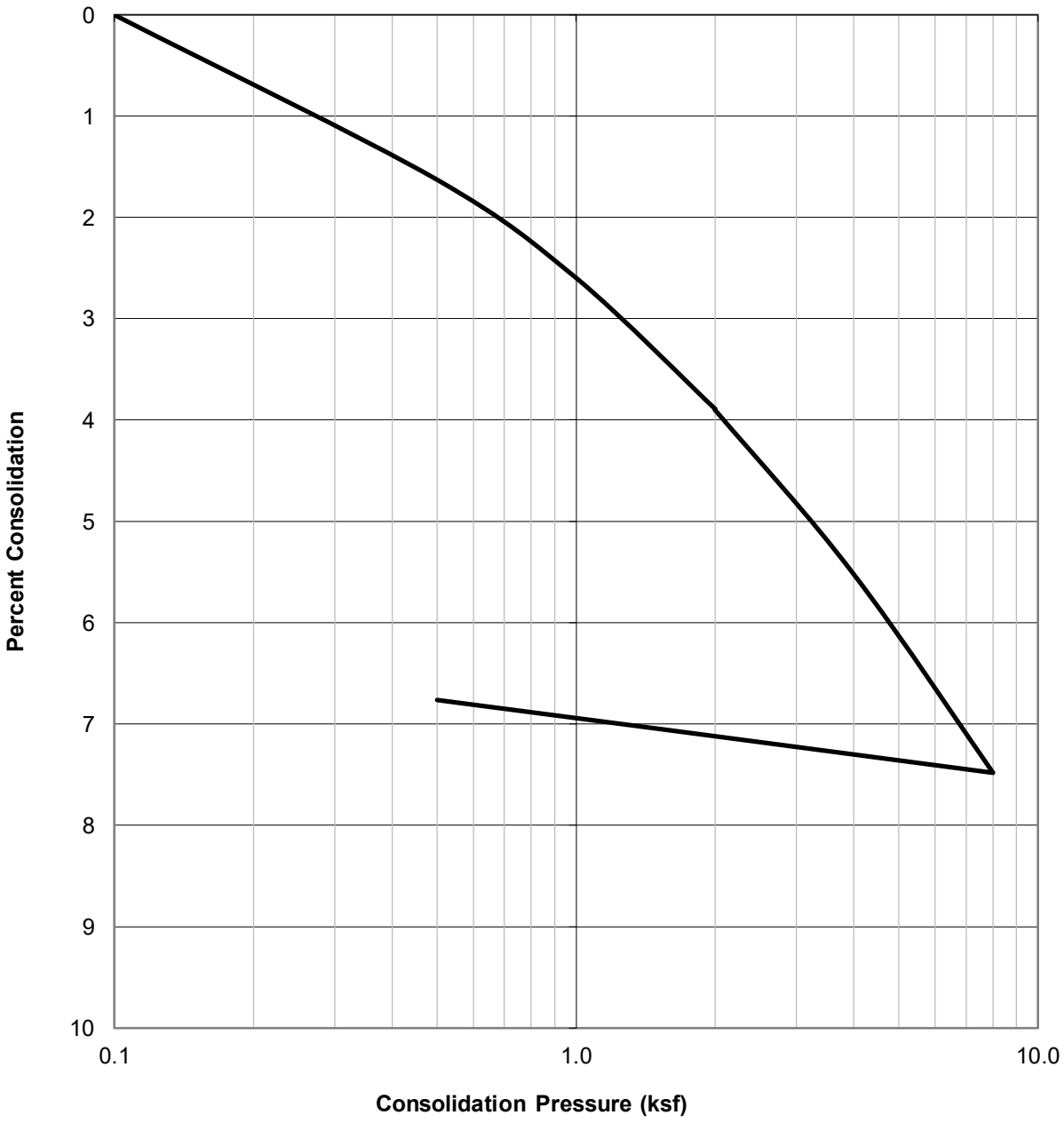
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B9

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
G@10	Sandy Silt (ML)	105.5	22.4	19.6

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

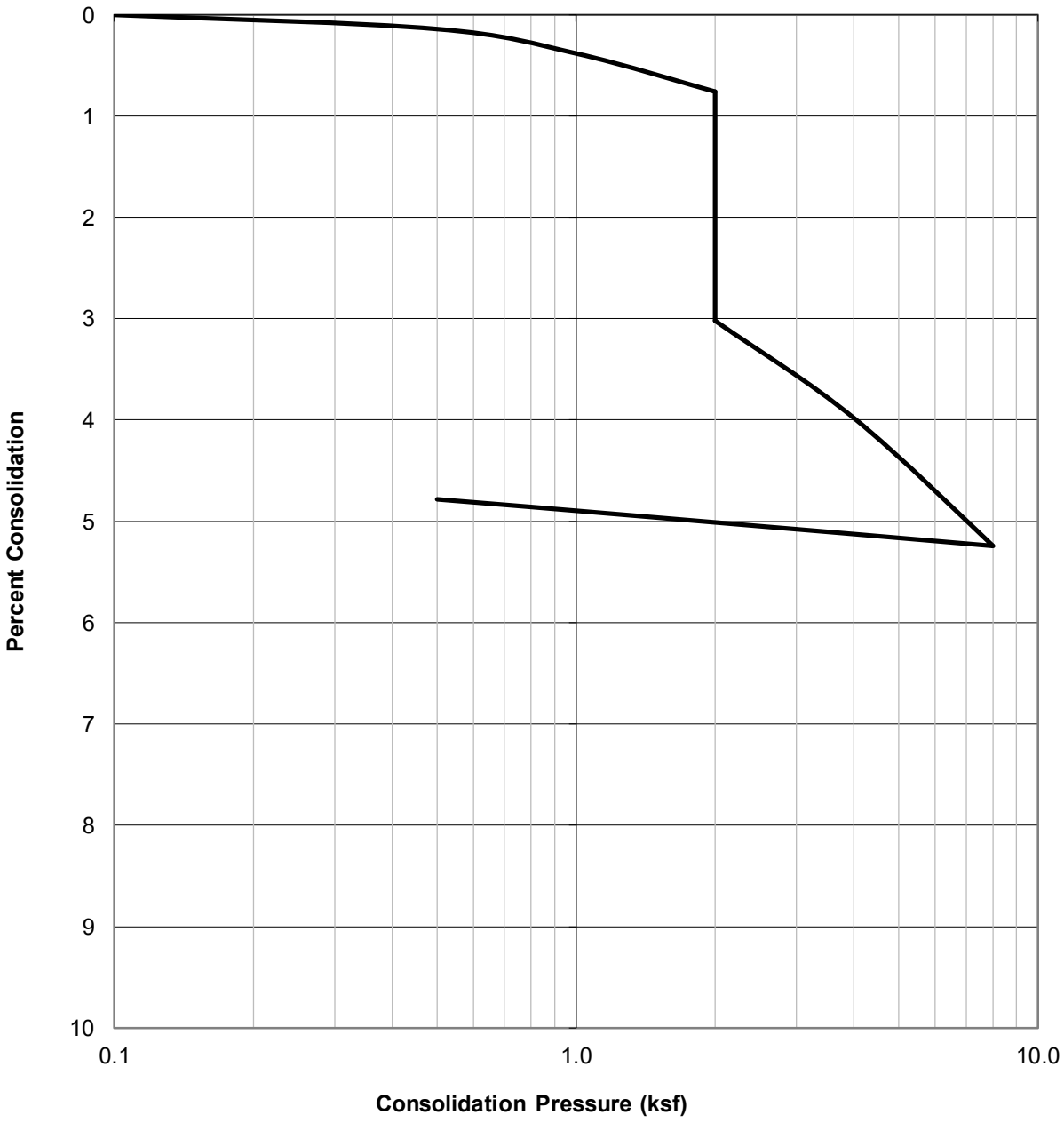
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B10

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
H@7	Sand (SP)	86.9	10.4	29.9

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

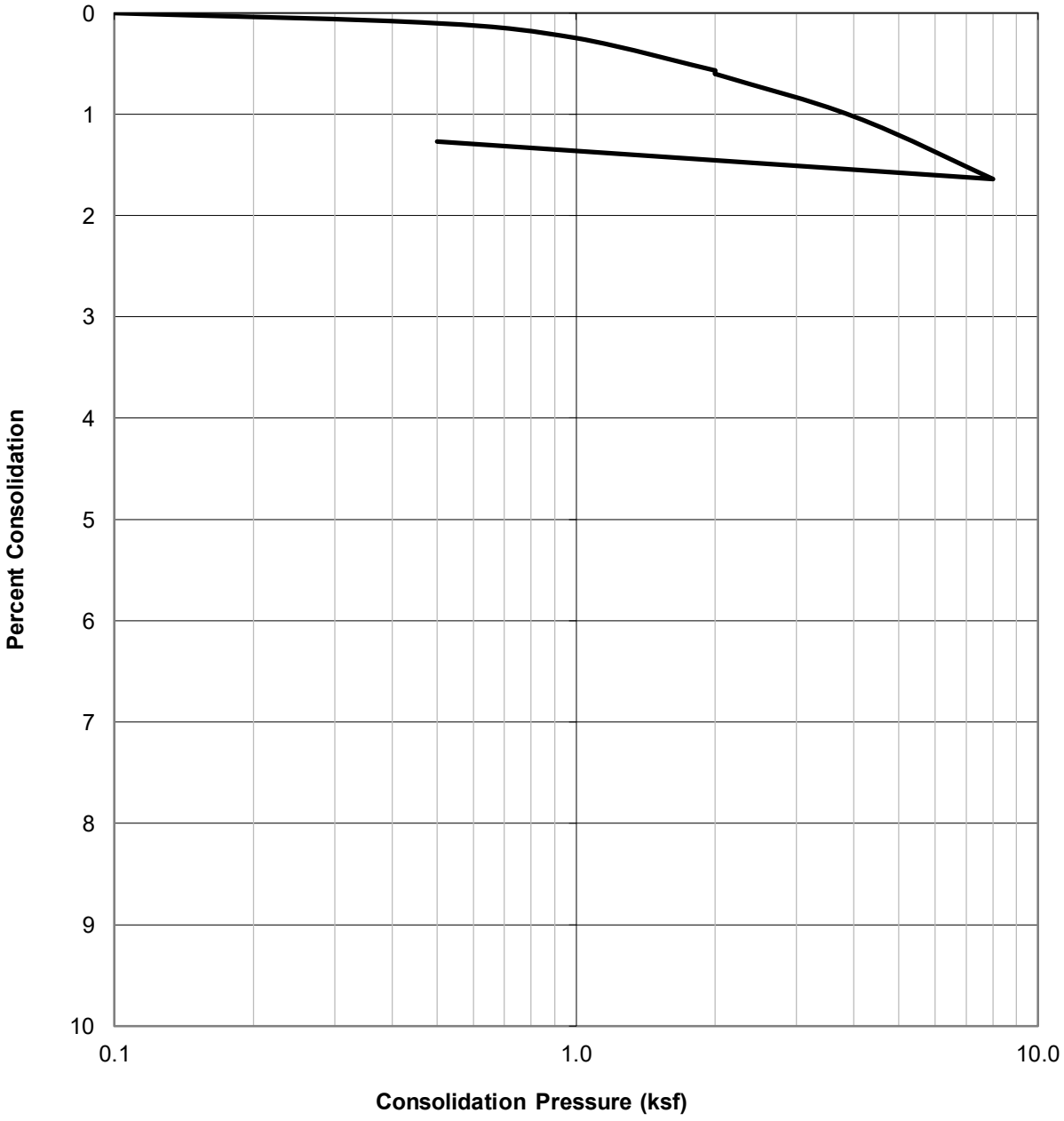
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B11

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
H@12	Sand (SP)	95.2	5.1	24.4

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

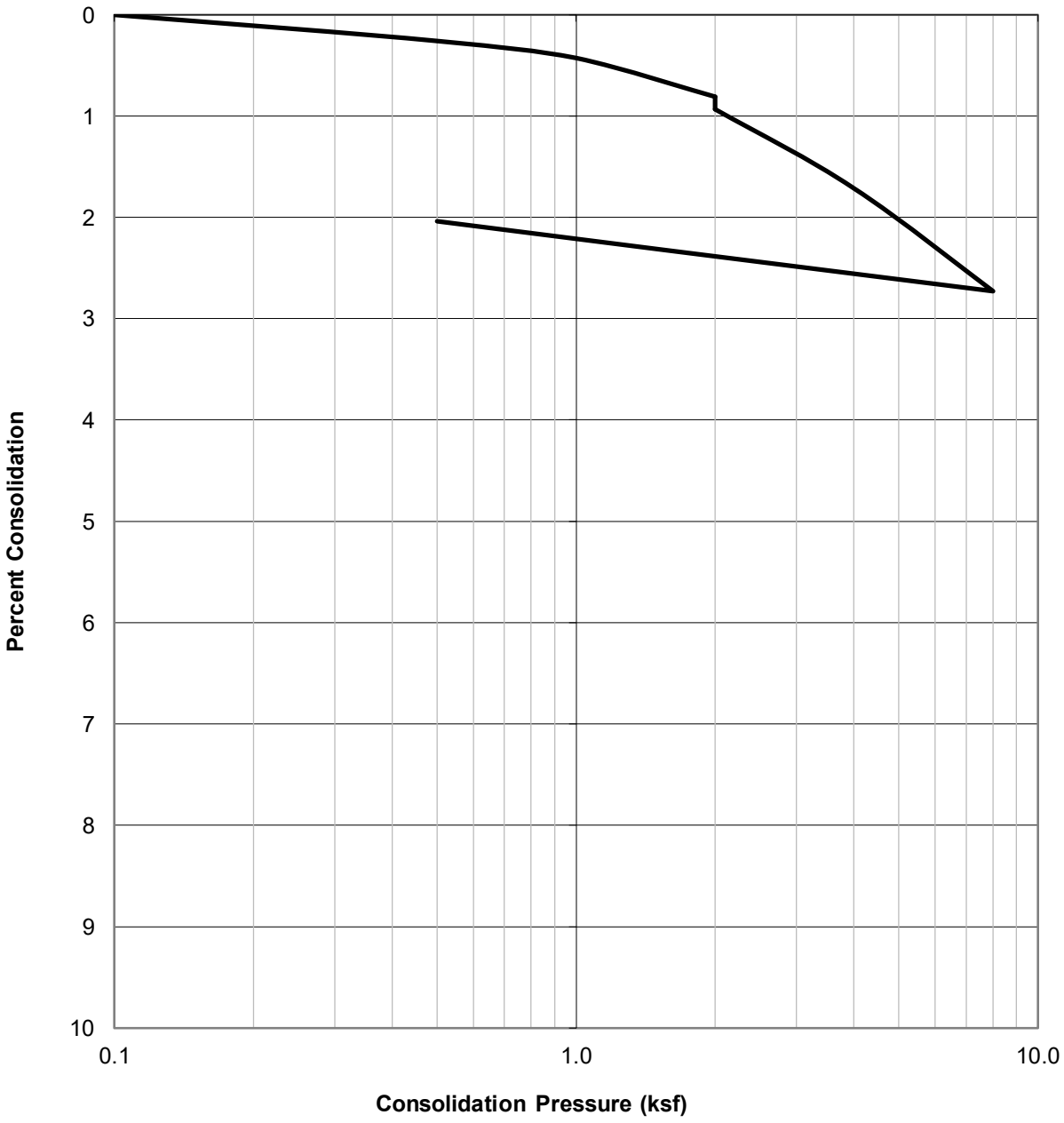
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B12

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
H@20	Silty Sand (SM)	102.2	14.7	20.8

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

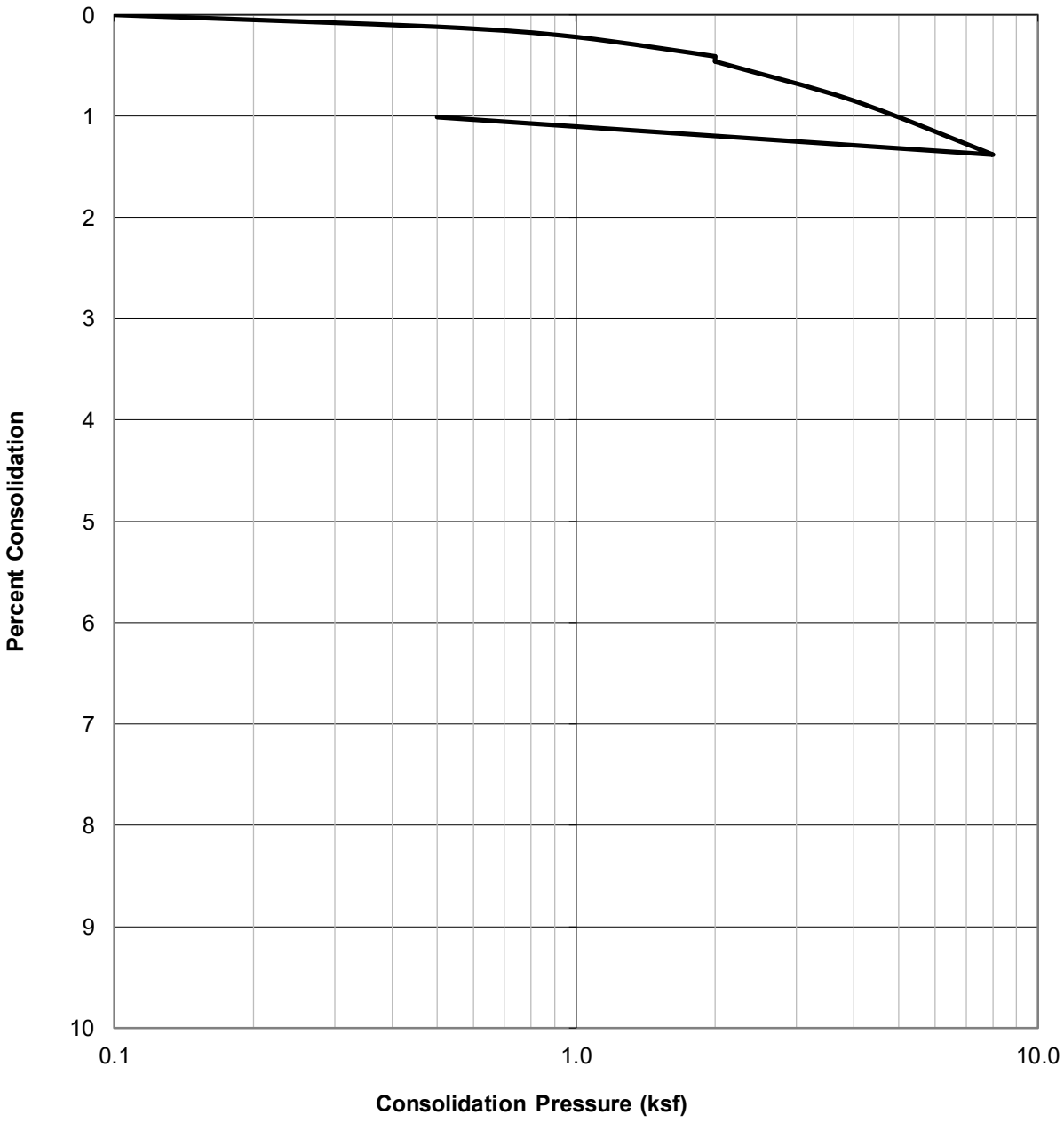
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B13

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
J@5	Sand (SP)	96.1	4.1	23.7

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

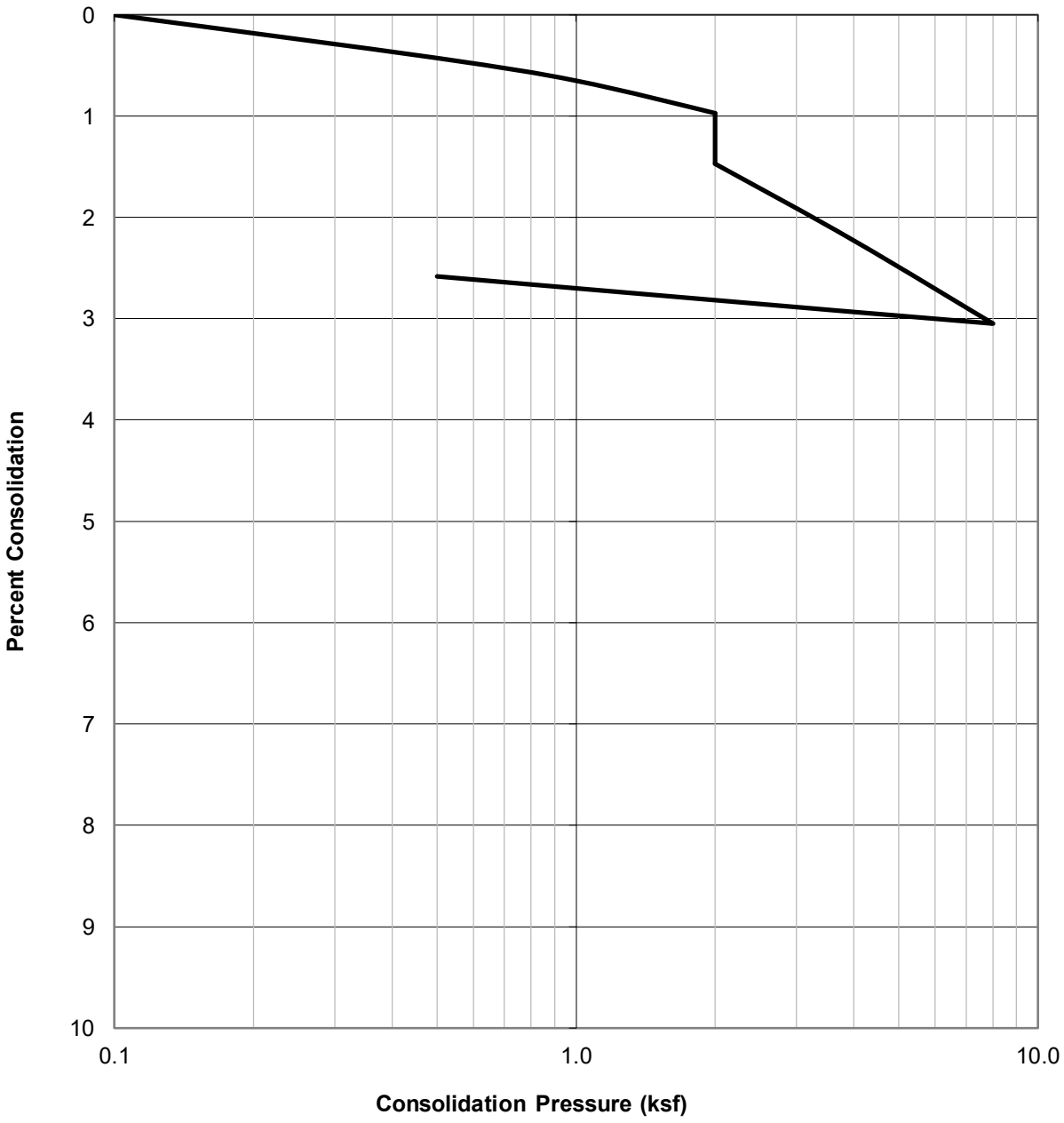
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B14

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
J@7	Sand (SP)	91.0	12.9	26.3

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

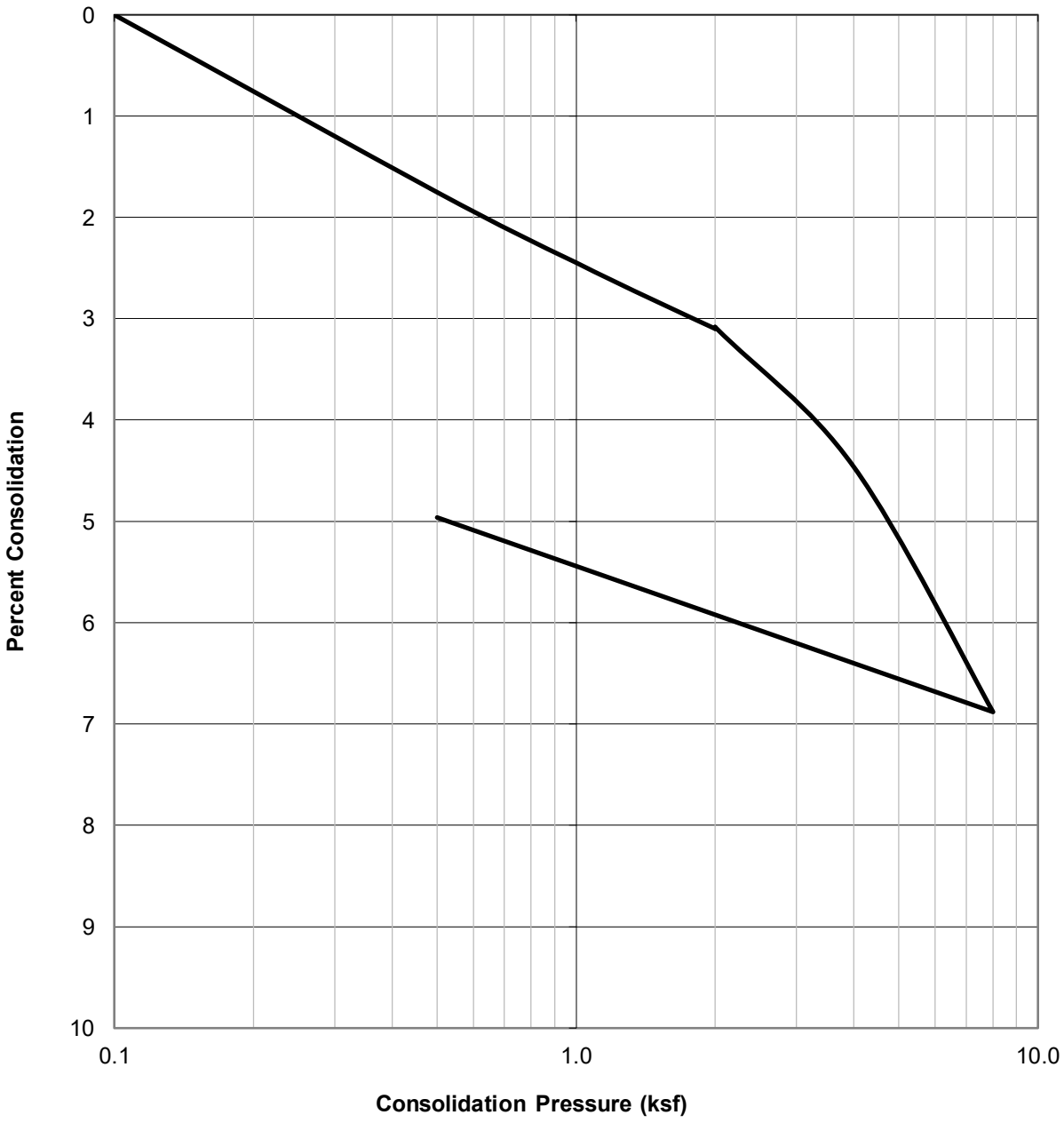
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B15

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
J@10	Sandy Clay (CL)	101.9	25.1	26.2

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

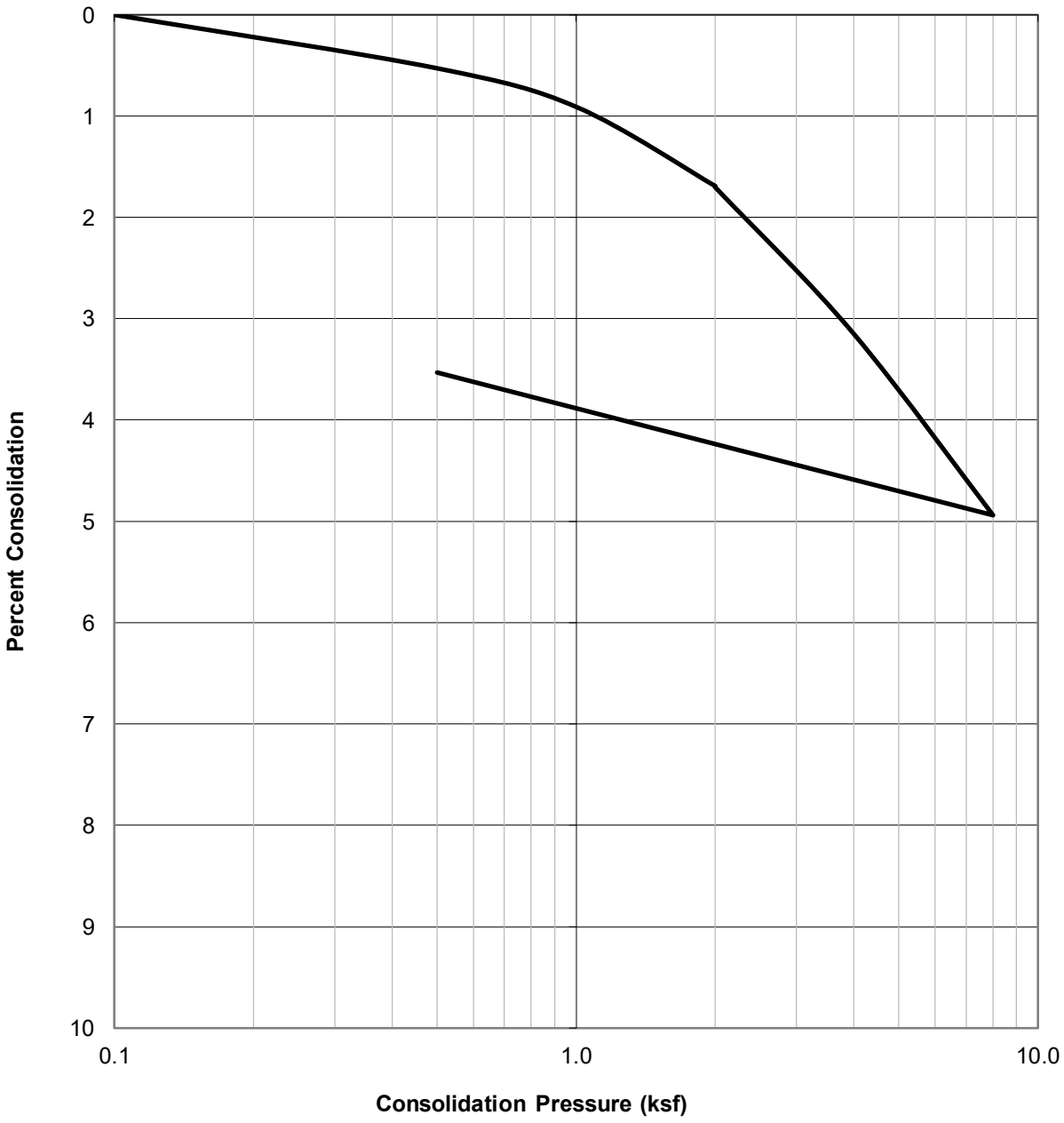
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B16

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
J@15	Sandy Clay (CL)	106.8	21.3	21.1

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

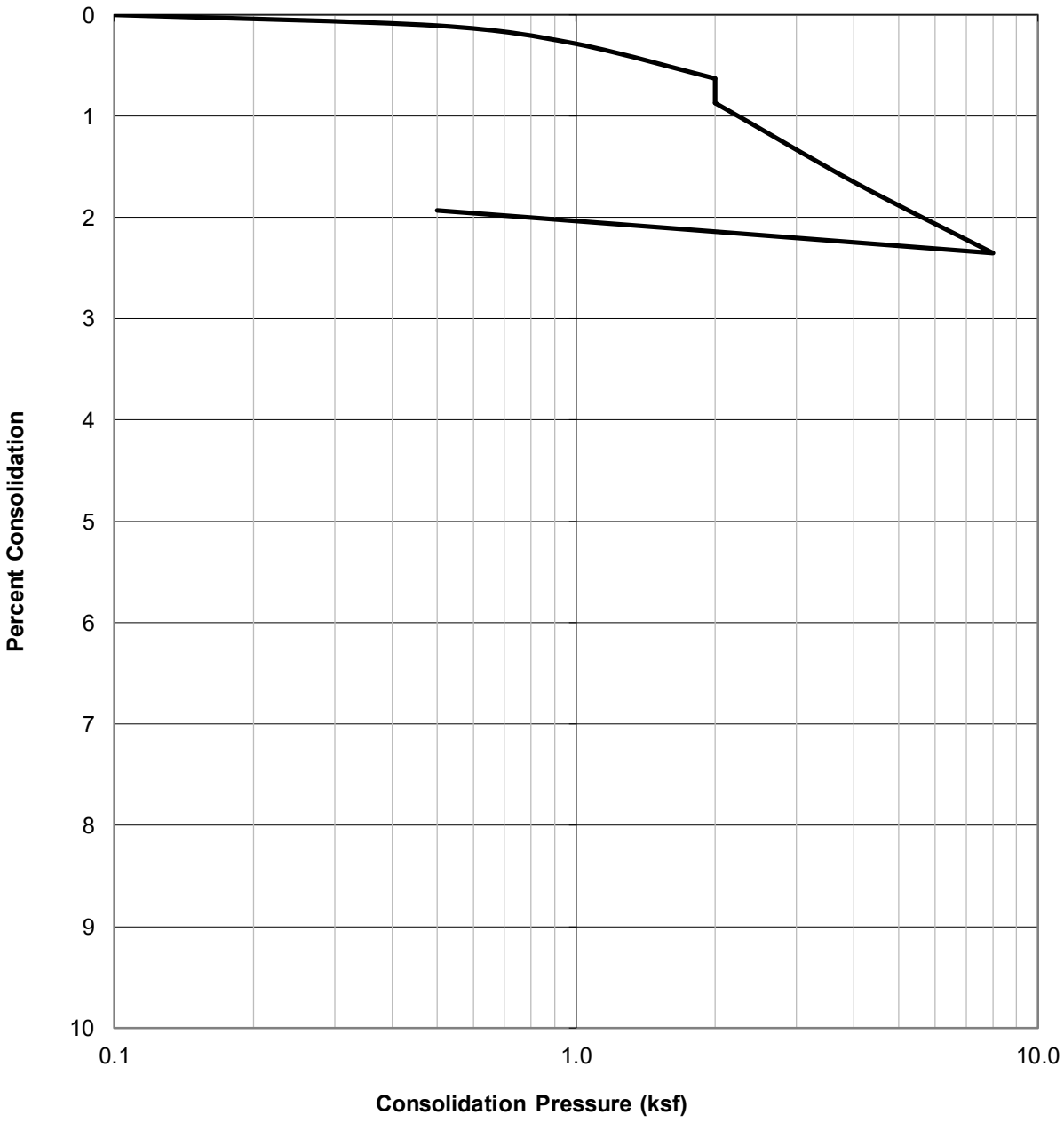
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B17

WATER ADDED AT 2.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
L@10	Silty Sand (SM)	93.5	5.3	29.3

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B18

SUMMARY OF LABORATORY NO. 200 TEST RESULTS

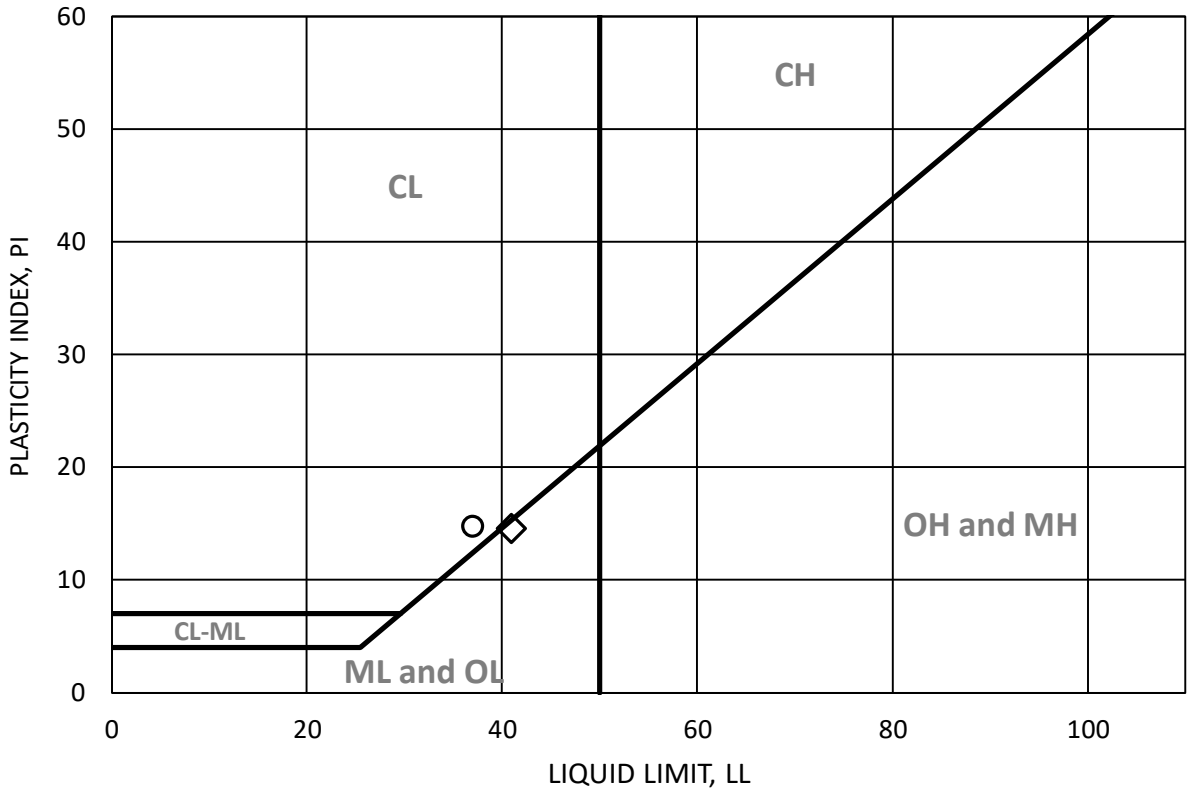
Sample No.	Percent Passing No. 200 Sieve
E @ 5'	**79.9**
E @ 7.5'	**67.6**
E @ 12.5'	**59.3**
E @ 17.5'	**34.7**
E @ 22.5'	**8.7**
E @ 27.5'	**29.1**
E @ 32.5'	**11.9**
E @ 37.5'	**3.8**
E @ 42.5'	**14.9**
E @ 47.5'	**70.5**

SUMMARY OF LABORATORY NO. 200 TEST RESULTS

Sample No.	Percent Passing No. 200 Sieve
F @ 5'	1.4
F @ 10'	1.0
F @ 15'	3.9
F @ 20'	83.3
F @ 25'	50.7
F @ 30'	8.8
F @ 35'	30.8
F @ 40'	65.9
F @ 45'	14.6
F @ 50'	66.3
F @ 55	16.4

SUMMARY OF LABORATORY NO. 200 TEST RESULTS

Sample No.	Percent Passing No. 200 Sieve
I @ 5'	5.2
I @ 7.5'	83.3
I @ 12.5'	84.7
I @ 15'	42.2
I @ 17.5'	98.8
I @ 22.5'	36.3
I @ 25'	97.5
I @ 27.5'	45.1
I @ 32.5'	80.8
I @ 35'	64.3
I @ 37.5'	11.4
I @ 42.5'	81.8
I @ 47.5'	64.6
I @ 62.5	88.8



SYMBOL	BORING	DEPTH (ft)	LL	PL	PI	MOISTURE CONTENT AT SATURATION	SOIL BEHAVIOR
■	E	47.5	N/P	N/P	N/P		N/P
◆	F	25	N/P	N/P	N/P		N/P
▲	F	35	N/P	N/P	N/P		N/P
●	F	40	N/P	N/P	N/P		N/P
□	F	50	N/P	N/P	N/P		N/P
◇	I	25	41	26	15		ML
△	I	27.5	N/P	N/P	N/P		N/P
○	I	32.5	37	22	15		CL

N/P = Non-Plastic

GEOCON

ATTERBERG LIMITS

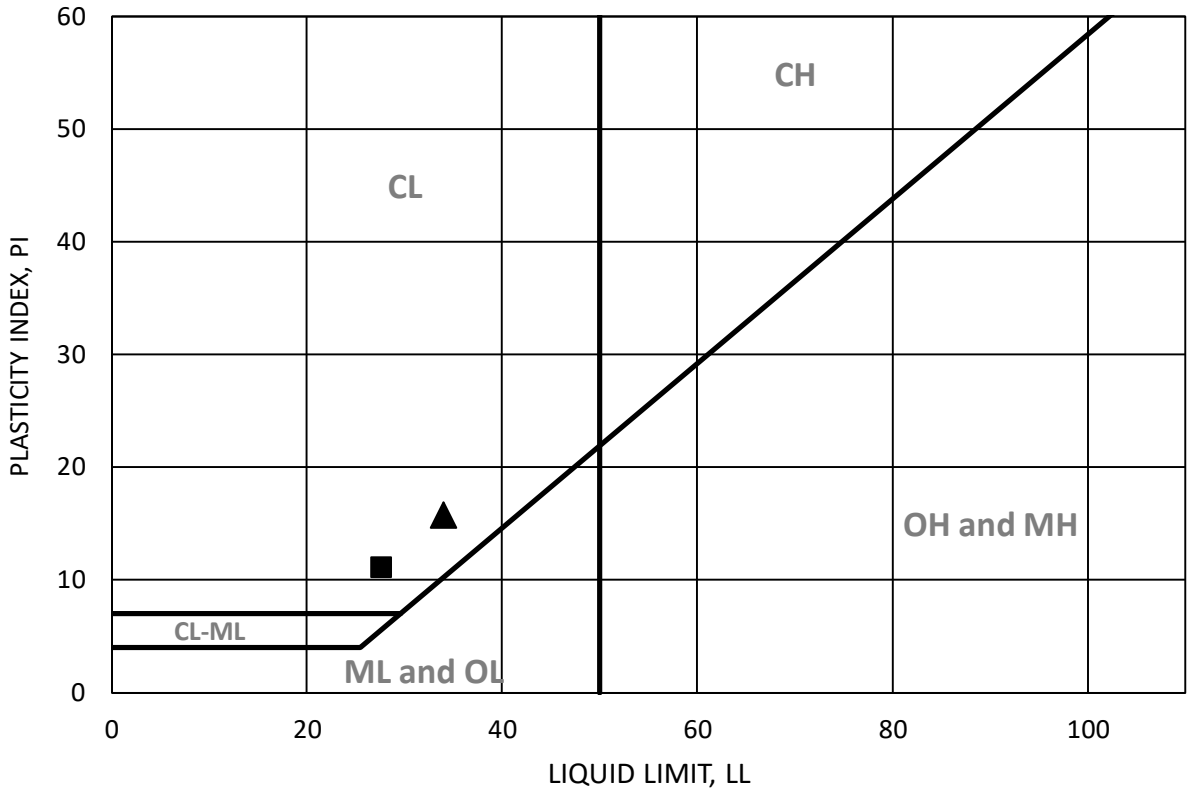
ASTM D-4318

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B22



SYMBOL	BORING	DEPTH (ft)	LL	PL	PI	MOISTURE CONTENT AT SATURATION	SOIL BEHAVIOR
■	I	42.5	N/P	N/P	N/P		N/P
◆	I	47.5	28	17	11		CL
▲	I	62.5	34	18	16		CL
●							
□							
◇							
△							
○							

N/P = Non-Plastic

GEOCON

ATTERBERG LIMITS

ASTM D-4318

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B23

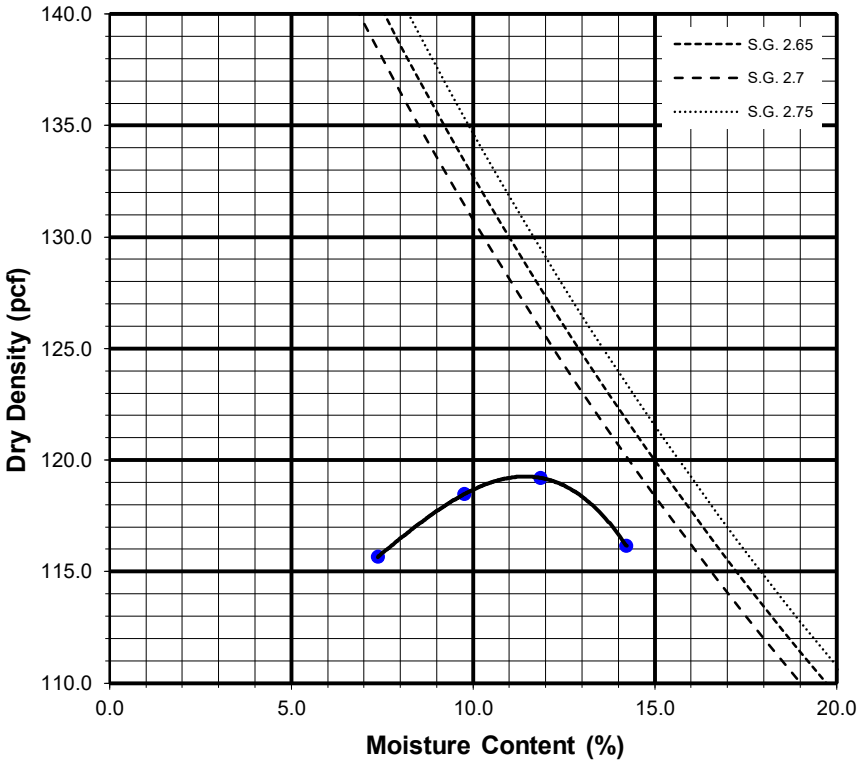
Sample No:

A+B@0-5	Silty Sand (SM)

TEST NO.		1	2	3	4	5	6
Wt. Compacted Soil + Mold	(g)	6158	6246	6296	6286		
Weight of Mold	(g)	4282	4282	4282	4282		
Net Weight of Soil	(g)	1876	1964	2014	2004		
Wet Weight of Soil + Cont.	(g)	2261.4	2323.1	2400.7	2392.5		
Dry Weight of Soil + Cont.	(g)	2131.9	2150.2	2186.3	2141.6		
Weight of Container	(g)	377.8	377.9	378.1	377.8		
Moisture Content	(%)	7.4	9.8	11.9	14.2		
Wet Density	(pcf)	124.2	130.0	133.3	132.7		
Dry Density	(pcf)	115.7	118.5	119.2	116.2		

Maximum Dry Density (pcf)	**119.5**

Optimum Moisture Content (%)	**11.0**



Preparation Method: A

GEOCON

COMPACTION CHARACTERISTICS USING MODIFIED EFFORT TEST RESULTS

ASTM D-1557

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B24

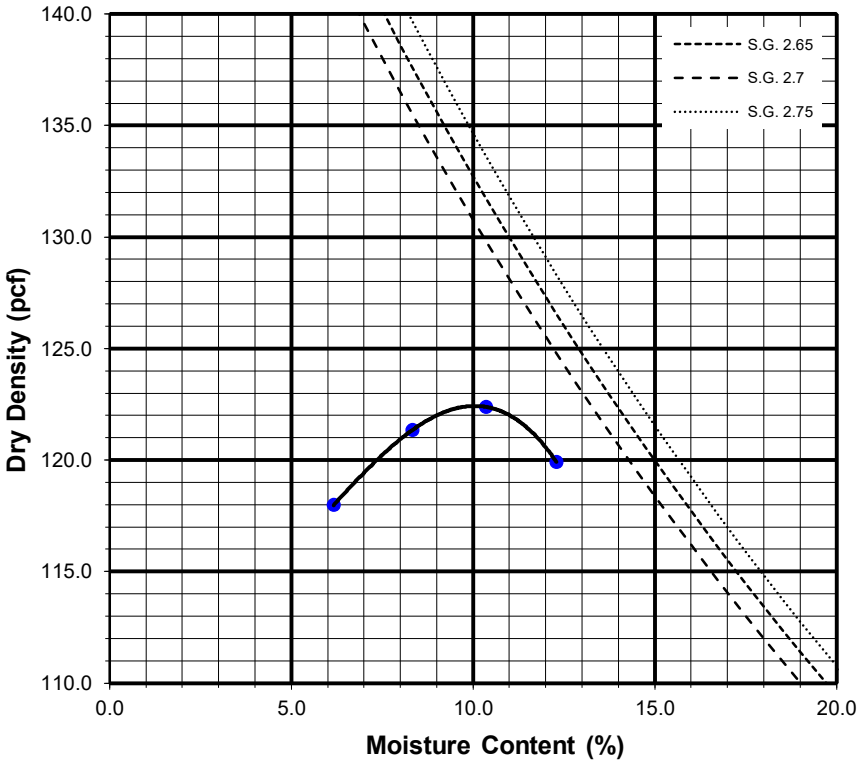
Sample No:

E+F@0-5	Silty Sand (SM)

TEST NO.		1	2	3	4	5	6
Wt. Compacted Soil + Mold	(g)	6174	6268	6322	6316		
Weight of Mold	(g)	4282	4282	4282	4282		
Net Weight of Soil	(g)	1892	1986	2040	2034		
Wet Weight of Soil + Cont.	(g)	2278.4	2367.7	2429.0	2422.6		
Dry Weight of Soil + Cont.	(g)	2167.9	2214.5	2236.6	2198.7		
Weight of Container	(g)	376.3	377.9	378.2	377.8		
Moisture Content	(%)	6.2	8.3	10.4	12.3		
Wet Density	(pcf)	125.3	131.5	135.1	134.7		
Dry Density	(pcf)	118.0	121.4	122.4	119.9		

Maximum Dry Density (pcf)	**123.0**

Optimum Moisture Content (%)	**9.5**



Preparation Method: A

GEOCON

COMPACTION CHARACTERISTICS USING MODIFIED EFFORT TEST RESULTS

ASTM D-1557

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

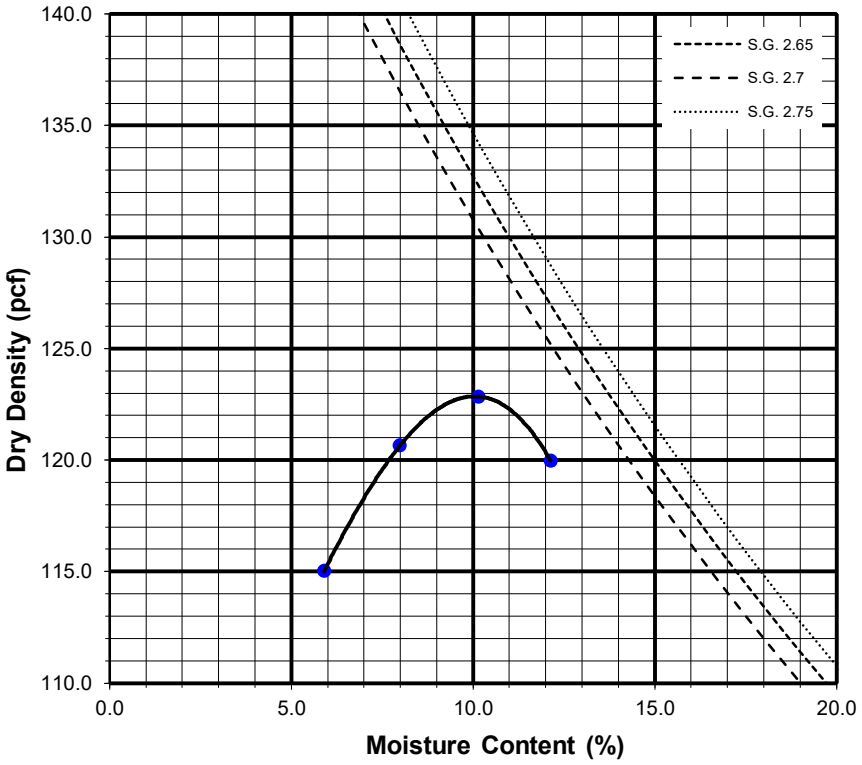
MAY 2024 Figure B25

Sample No:

M@0-5	Silty Sand (SM)

TEST NO.		1	2	3	4	5	6
Wt. Compacted Soil + Mold	(g)	6326	6314	6250	6122		
Weight of Mold	(g)	4282	4282	4282	4282		
Net Weight of Soil	(g)	2044	2032	1968	1840		
Wet Weight of Soil + Cont.	(g)	2429.4	2418.9	2322.1	2224.9		
Dry Weight of Soil + Cont.	(g)	2240.4	2197.9	2178.2	2122.0		
Weight of Container	(g)	378.5	377.2	377.3	379.0		
Moisture Content	(%)	10.2	12.1	8.0	5.9		
Wet Density	(pcf)	135.3	134.5	130.3	121.8		
Dry Density	(pcf)	122.9	120.0	120.6	115.0		

Maximum Dry Density (pcf)	**123.0**	**Optimum Moisture Content (%)**	**9.5**



Preparation Method: A

GEOCON

COMPACTION CHARACTERISTICS USING MODIFIED EFFORT TEST RESULTS

ASTM D-1557

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B26

A+B@0-5

MOLDED SPECIMEN		BEFORE TEST	AFTER TEST
Specimen Diameter	(in.)	4.0	4.0
Specimen Height	(in.)	1.0	1.0
Wt. Comp. Soil + Mold	(gm)	584.4	623.1
Wt. of Mold	(gm)	201.8	201.8
Specific Gravity	(Assumed)	2.7	2.7
Wet Wt. of Soil + Cont.	(gm)	300.0	623.1
Dry Wt. of Soil + Cont.	(gm)	267.9	341.6
Wt. of Container	(gm)	0.0	201.8
Moisture Content	(%)	12.0	23.3
Wet Density	(pcf)	115.4	126.9
Dry Density	(pcf)	103.0	102.9
Void Ratio		0.6	0.6
Total Porosity		0.4	0.4
Pore Volume	(cc)	80.5	80.5
Degree of Saturation	(%) [S_{meas}]	51.3	99.1

Date	Time	Pressure (psi)	Elapsed Time (min)	Dial Readings (in.)
2/29/2024	10:00	1.0	0	0.4451
2/29/2024	10:10	1.0	10	0.4449
Add Distilled Water to the Specimen				
3/1/2024	10:00	1.0	1430	0.4448
3/1/2024	11:00	1.0	1490	0.4448

Expansion Index (EI meas) =	-0.1
Expansion Index (Report) =	**0**

Expansion Index, EI_{50}	CBC CLASSIFICATION *	UBC CLASSIFICATION **
0-20	Non-Expansive	Very Low
21-50	Expansive	Low
51-90	Expansive	Medium
91-130	Expansive	High
>130	Expansive	Very High

* Reference: 2022 California Building Code, Section 1803.5.3

** Reference: 1997 Uniform Building Code, Table 18-I-B.

GEOCON

EXPANSION INDEX TEST RESULTS

ASTM D-4829

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B27

E+F@0-5

MOLDED SPECIMEN		BEFORE TEST	AFTER TEST
Specimen Diameter	(in.)	4.0	4.0
Specimen Height	(in.)	1.0	1.0
Wt. Comp. Soil + Mold	(gm)	572.2	597.5
Wt. of Mold	(gm)	171.3	171.3
Specific Gravity	(Assumed)	2.7	2.7
Wet Wt. of Soil + Cont.	(gm)	300.0	597.5
Dry Wt. of Soil + Cont.	(gm)	272.7	364.5
Wt. of Container	(gm)	0.0	171.3
Moisture Content	(%)	10.0	16.9
Wet Density	(pcf)	120.9	128.4
Dry Density	(pcf)	109.9	109.8
Void Ratio		0.5	0.5
Total Porosity		0.3	0.3
Pore Volume	(cc)	72.0	72.0
Degree of Saturation	(%) [S_{meas}]	51.0	85.8

Date	Time	Pressure (psi)	Elapsed Time (min)	Dial Readings (in.)
2/29/2024	10:00	1.0	0	0.4441
2/29/2024	10:10	1.0	10	0.444
Add Distilled Water to the Specimen				
3/1/2024	10:00	1.0	1430	0.4439
3/1/2024	11:00	1.0	1490	0.4439

Expansion Index (EI meas) =	-0.1
Expansion Index (Report) =	**0**

Expansion Index, EI_{50}	CBC CLASSIFICATION *	UBC CLASSIFICATION **
0-20	Non-Expansive	Very Low
21-50	Expansive	Low
51-90	Expansive	Medium
91-130	Expansive	High
>130	Expansive	Very High

* Reference: 2022 California Building Code, Section 1803.5.3

** Reference: 1997 Uniform Building Code, Table 18-I-B.

GEOCON

EXPANSION INDEX TEST RESULTS

ASTM D-4829

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B28

M@0-5

MOLDED SPECIMEN		BEFORE TEST	AFTER TEST
Specimen Diameter	(in.)	4.0	4.0
Specimen Height	(in.)	1.0	1.0
Wt. Comp. Soil + Mold	(gm)	576.2	584.3
Wt. of Mold	(gm)	176.4	176.4
Specific Gravity	(Assumed)	2.7	2.7
Wet Wt. of Soil + Cont.	(gm)	300.0	584.3
Dry Wt. of Soil + Cont.	(gm)	272.2	362.8
Wt. of Container	(gm)	0.0	176.4
Moisture Content	(%)	10.2	12.4
Wet Density	(pcf)	120.6	122.9
Dry Density	(pcf)	109.4	109.3
Void Ratio		0.5	0.5
Total Porosity		0.4	0.4
Pore Volume	(cc)	72.6	73.0
Degree of Saturation	(%) [S_{meas}]	51.4	61.8

Date	Time	Pressure (psi)	Elapsed Time (min)	Dial Readings (in.)
2/29/2024	10:00	1.0	0	0.4416
2/29/2024	10:10	1.0	10	0.4416
Add Distilled Water to the Specimen				
3/1/2024	10:00	1.0	1430	0.4434
3/1/2024	11:00	1.0	1490	0.4434

Expansion Index (EI meas) =	1.8
Expansion Index (Report) =	**2**

Expansion Index, EI_{50}	CBC CLASSIFICATION *	UBC CLASSIFICATION **
0-20	Non-Expansive	Very Low
21-50	Expansive	Low
51-90	Expansive	Medium
91-130	Expansive	High
>130	Expansive	Very High

* Reference: 2022 California Building Code, Section 1803.5.3
** Reference: 1997 Uniform Building Code, Table 18-I-B.

GEOCON

EXPANSION INDEX TEST RESULTS
ASTM D-4829

Checked by: ACS

Project No.: W1857-88-01
OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B29

SUMMARY OF LABORATORY
POTENTIAL OF HYDROGEN (pH) AND RESISTIVITY TEST RESULTS
AASHTO T289 ASTM D4972 and AASHTO T288 ASTM G187

Sample No.	pH	Resistivity (ohm centimeters)
E+F@0-5	8.4	5900 (Moderately Corrosive)
M@0-5	8.7	2800 (Moderately Corrosive)

SUMMARY OF LABORATORY CHLORIDE CONTENT TEST RESULTS
AASHTO T291 ASTM C1218

Sample No.	Chloride Ion Content (%)
E+F@0-5	0.002
M@0-5	0.075

SUMMARY OF LABORATORY WATER SOLUBLE SULFATE TEST RESULTS
AASHTO T290 ASTM C1580

Sample No.	Water Soluble Sulfate (% SO_4)	Sulfate Exposure
E+F@0-5	0.001	S0
M@0-5	0.000	S0

GEOCON

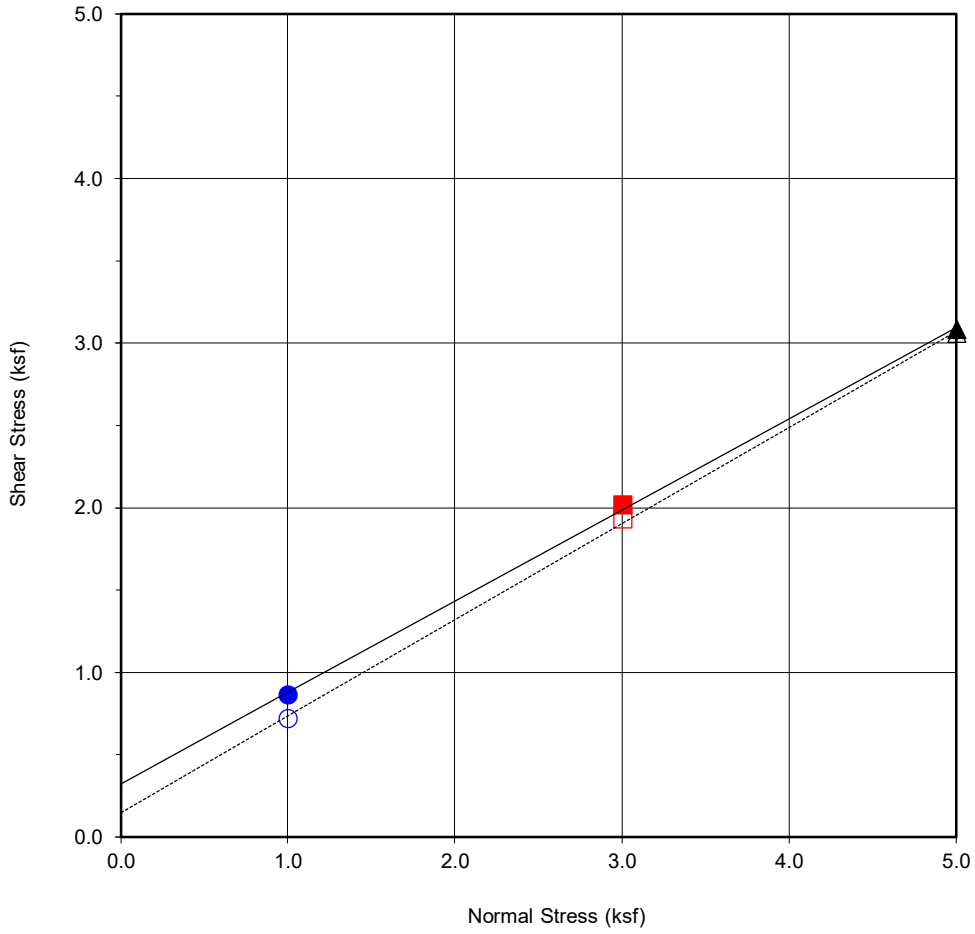
CORROSIVITY TEST RESULTS

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

MAY 2024 Figure B30



Boring No.	**N+O**
Sample No.	**N+O@0-5'**
Depth (ft)	**0-5'**
Sample Type:	REMOLD

Soil Identification:		
Silty Sand (SM)		
Strength Parameters		
	C (psf)	ϕ (^{o})
Peak	323	29
Ultimate	149	30

Normal Stress (kip/ft²)	1	3	5
Peak Shear Stress (kip/ft²)	● 0.86	■ 2.02	▲ 3.08
Shear Stress @ End of Test (ksf)	○ 0.72	□ 1.93	△ 3.06
Deformation Rate (in./min.)	0.05	0.05	0.05
Initial Sample Height (in.)	1.0	1.0	1.0
Ring Inside Diameter (in.)	2.375	2.375	2.375
Initial Moisture Content (%)	12.6	12.6	12.1
Initial Dry Density (pcf)	110.0	109.9	110.5
Initial Degree of Saturation (%)	63.9	63.9	62.4
Soil Height Before Shearing (in.)	1.2	1.2	1.2
Final Moisture Content (%)	18.0	18.4	17.2

GEOCON

DIRECT SHEAR TEST RESULTS

Consolidated Drained ASTM D-3080

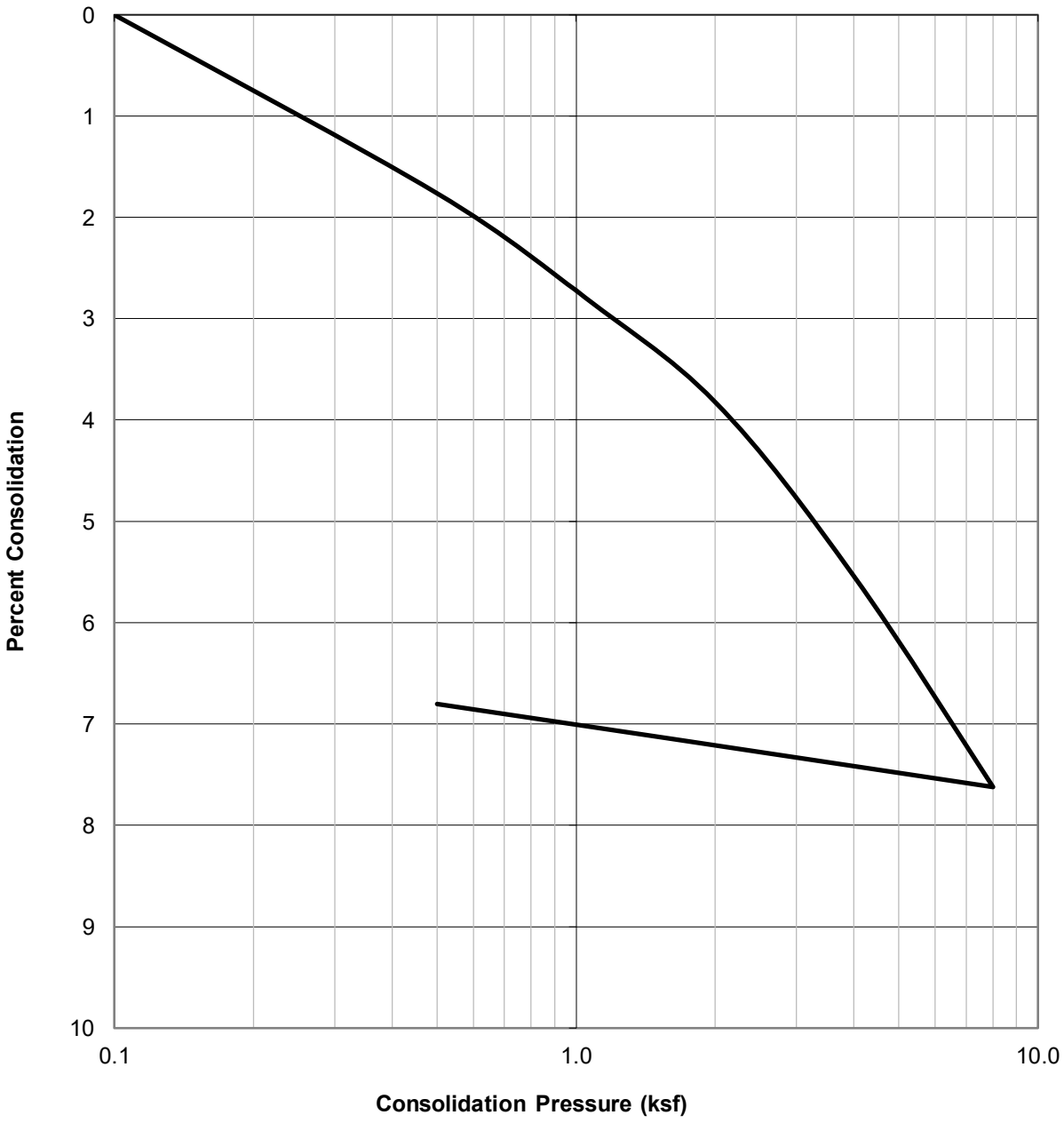
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

May 2024 Figure B31

WATER ADDED AT 1.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
N@7'	Sandy Silt (ML)	98.2	26.6	22.5

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

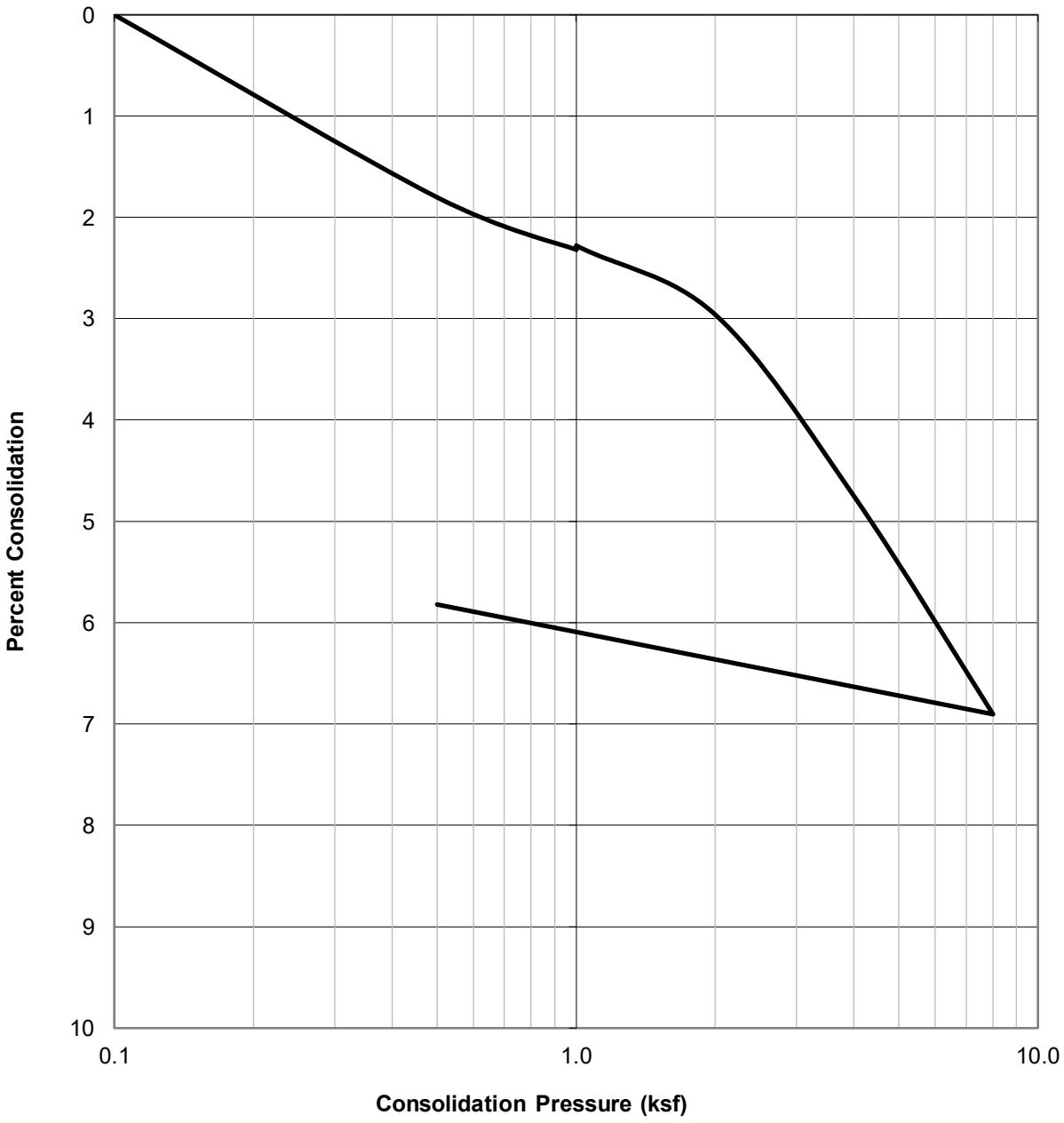
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

May 2024 Figure B32

WATER ADDED AT 1.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
N@12'	Clayey Silt (ML)	106.3	21.9	19.6

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

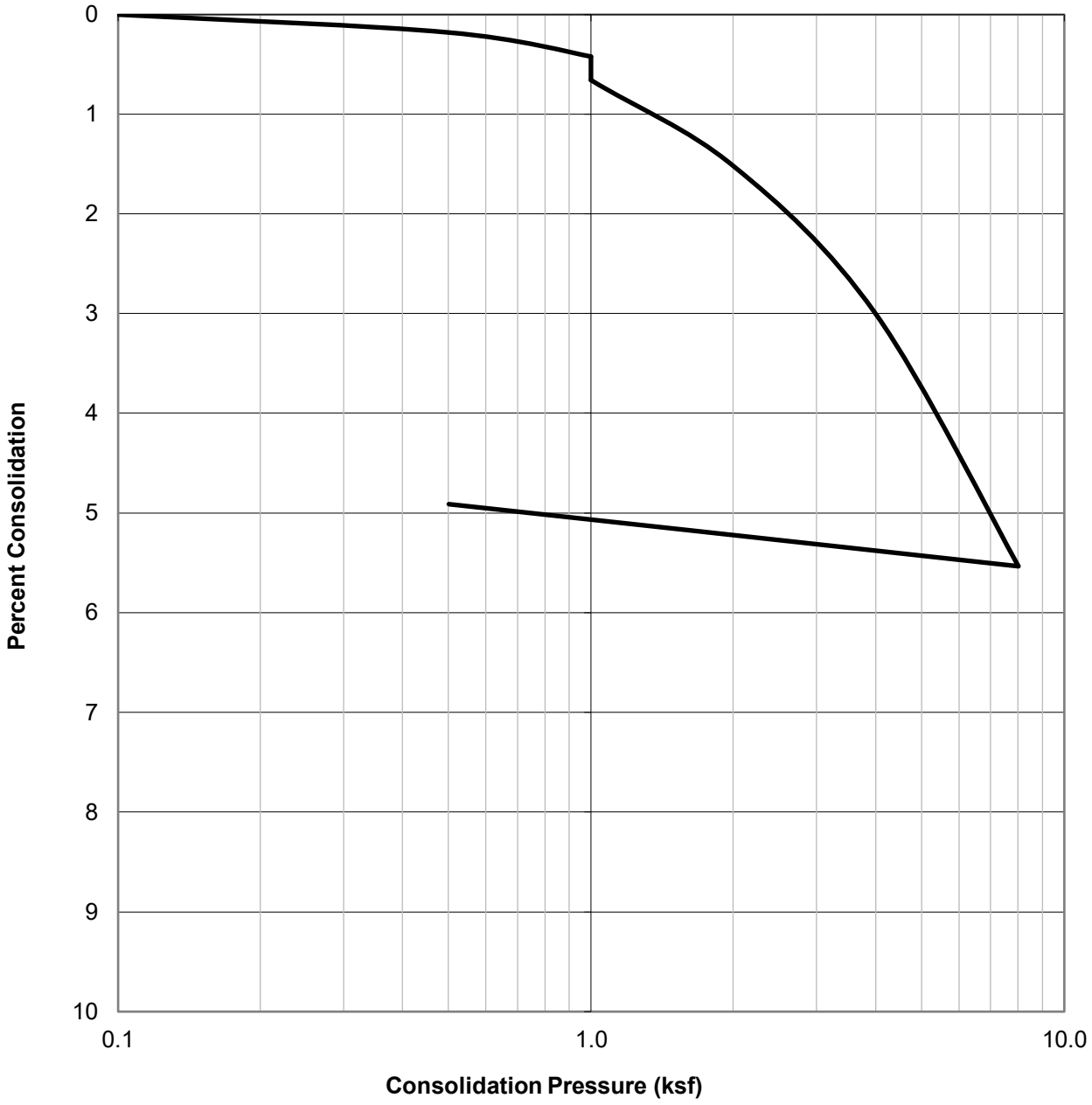
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

May 2024 Figure B33

WATER ADDED AT 1.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
O@5'	Sand (SP)	91.3	13.7	26.6

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

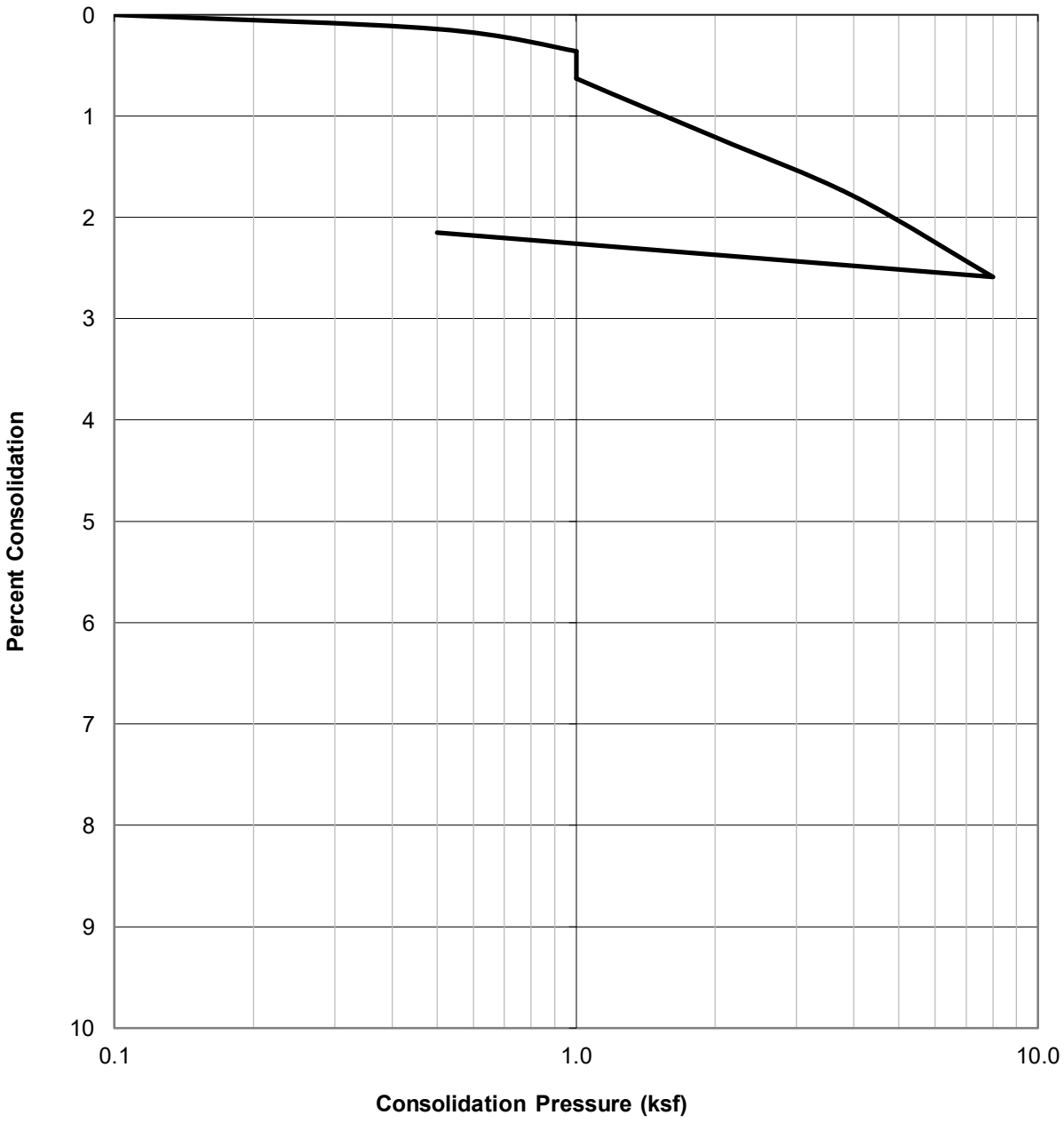
Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

May 2024 Figure B34

WATER ADDED AT 1.0 KSF



SAMPLE ID.	SOIL TYPE	DRY DENSITY (PCF)	INITIAL MOISTURE (%)	FINAL MOISTURE (%)
O@10'	Sand (SP)	92.1	5.0	29.0

GEOCON

CONSOLIDATION TEST RESULTS

ASTM D-2435

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

May 2024 Figure B35

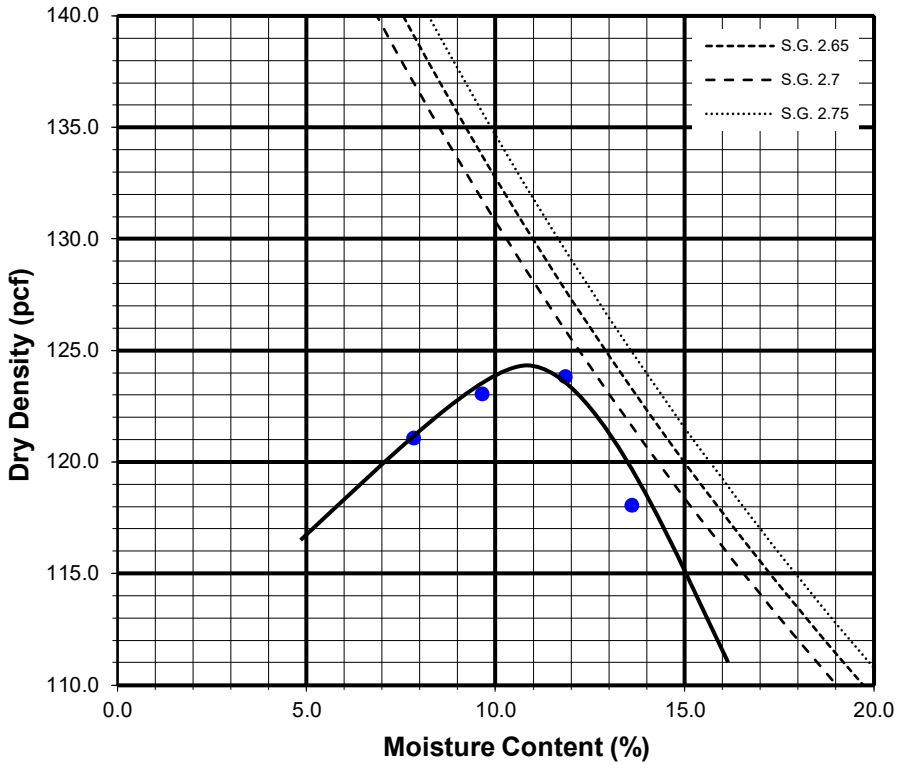
Sample No:

N+O @0-5'	Silty Sand (SM)

TEST NO.		1	2	3	4	5	6
Wt. Compacted Soil + Mold	(g)	6254	6320	6374	6308		
Weight of Mold	(g)	4282	4282	4282	4282		
Net Weight of Soil	(g)	1972	2038	2092	2026		
Wet Weight of Soil + Cont.	(g)	2359.6	2415.4	2467.4	2412.9		
Dry Weight of Soil + Cont.	(g)	2215.7	2236.4	2246.2	2169.4		
Weight of Container	(g)	377.8	377.3	377.2	378.1		
Moisture Content	(%)	7.8	9.6	11.8	13.6		
Wet Density	(pcf)	130.6	134.9	138.5	134.1		
Dry Density	(pcf)	121.1	123.1	123.8	118.1		

Maximum Dry Density (pcf)	**124.1**

Optimum Moisture Content (%)	**10.7**



Preparation Method: A

GEOCON

COMPACTION CHARACTERISTICS USING MODIFIED EFFORT TEST RESULTS

ASTM D-1557

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

May 2024 Figure B36

N+O@0-5'

MOLDED SPECIMEN		BEFORE TEST	AFTER TEST
Specimen Diameter	(in.)	4.0	4.0
Specimen Height	(in.)	1.0	1.0
Wt. Comp. Soil + Mold	(gm)	609.4	622.2
Wt. of Mold	(gm)	200.8	200.8
Specific Gravity	(Assumed)	2.7	2.7
Wet Wt. of Soil + Cont.	(gm)	308.5	622.2
Dry Wt. of Soil + Cont.	(gm)	282.5	373.2
Wt. of Container	(gm)	8.5	200.8
Moisture Content	(%)	9.5	12.9
Wet Density	(pcf)	123.3	126.9
Dry Density	(pcf)	112.6	112.4
Void Ratio		0.5	0.5
Total Porosity		0.3	0.3
Pore Volume	(cc)	68.8	68.5
Degree of Saturation	(%) [S_{meas}]	51.9	70.5

Date	Time	Pressure (psi)	Elapsed Time (min)	Dial Readings (in.)
5/8/2024	10:00	1.0	0	0.4214
5/8/2024	10:10	1.0	10	0.4213
Add Distilled Water to the Specimen				
5/9/2024	10:00	1.0	1430	0.4198
5/9/2024	11:00	1.0	1490	0.4198

Expansion Index (EI meas) =	-1.5
Expansion Index (Report) =	**0**

Expansion Index, EI_{50}	CBC CLASSIFICATION *	UBC CLASSIFICATION **
0-20	Non-Expansive	Very Low
21-50	Expansive	Low
51-90	Expansive	Medium
91-130	Expansive	High
>130	Expansive	Very High

* Reference: 2022 California Building Code, Section 1803.5.3

** Reference: 1997 Uniform Building Code, Table 18-I-B.

GEOCON

EXPANSION INDEX TEST RESULTS

ASTM D-4829

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

May 2024 Figure B37

SUMMARY OF LABORATORY
POTENTIAL OF HYDROGEN (pH) AND RESISTIVITY TEST RESULTS
AASHTO T289 ASTM D4972 and AASHTO T288 ASTM G187

Sample No.	pH	Resistivity (ohm centimeters)
N+O@0-5'	8.6	10000 (Moderately Corrosive)

SUMMARY OF LABORATORY CHLORIDE CONTENT TEST RESULTS
AASHTO T291 ASTM C1218

Sample No.	Chloride Ion Content (%)
N+O@0-5'	0.016

SUMMARY OF LABORATORY WATER SOLUBLE SULFATE TEST RESULTS
AASHTO T290 ASTM C1580

Sample No.	Water Soluble Sulfate (% SO_4)	Sulfate Exposure
N+O@0-5'	0.002	S0

GEOCON

CORROSIVITY TEST RESULTS

Checked by: ACS

Project No.: W1857-88-01

OC YTC
331 THE CITY DRIVE SOUTH
ORANGE, CALIFORNIA

May 2024 Figure B38

APPENDIX C

APPENDIX C

CPT ANALYSIS OF LIQUEFACTION POTENTIAL

TABLE OF CONTENTS

CPT-1 results

Summary data report	1
Transition layer aglorithm summary report	8
Transition layer aglorithm data report	9
Input field data	10
Cyclic stress resistance results	33
Cyclic resistance ratio results	56
Liquefaction potential index data	79
Vertical settlements summary report	91
Vertical settlements data report	92
Strength loss data report	99

CPT-2 results

Summary data report	124
Transition layer aglorithm summary report	131
Transition layer aglorithm data report	132
Input field data	133
Cyclic stress resistance results	155
Cyclic resistance ratio results	177
Liquefaction potential index data	199
Vertical settlements summary report	210
Vertical settlements data report	211
Strength loss data report	218

CPT-3 results

Summary data report	242
Transition layer aglorithm summary report	249
Transition layer aglorithm data report	250
Input field data	252
Cyclic stress resistance results	281
Cyclic resistance ratio results	310
Liquefaction potential index data	339
Vertical settlements summary report	354
Vertical settlements data report	355
Strength loss data report	366

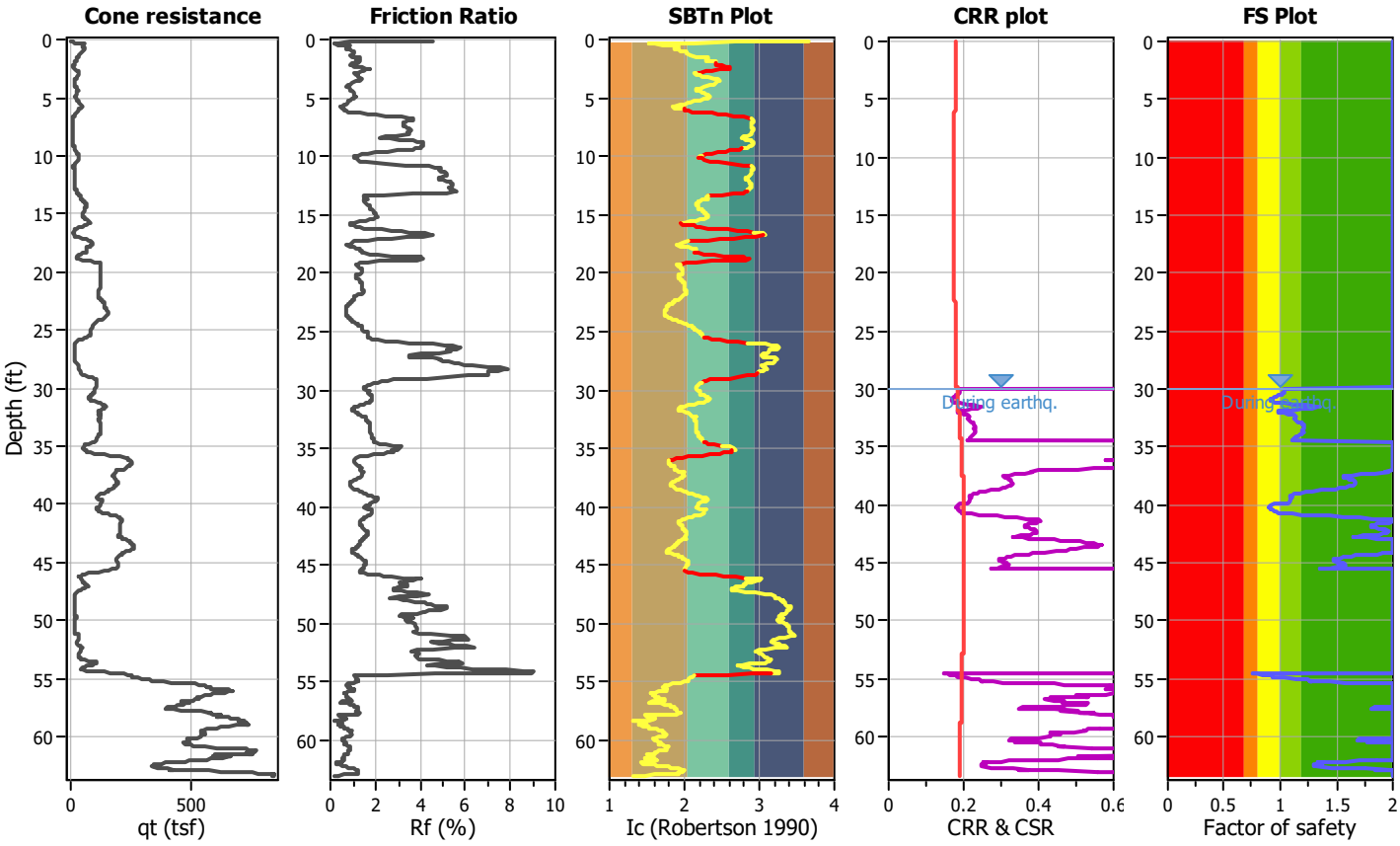
LIQUEFACTION ANALYSIS REPORT

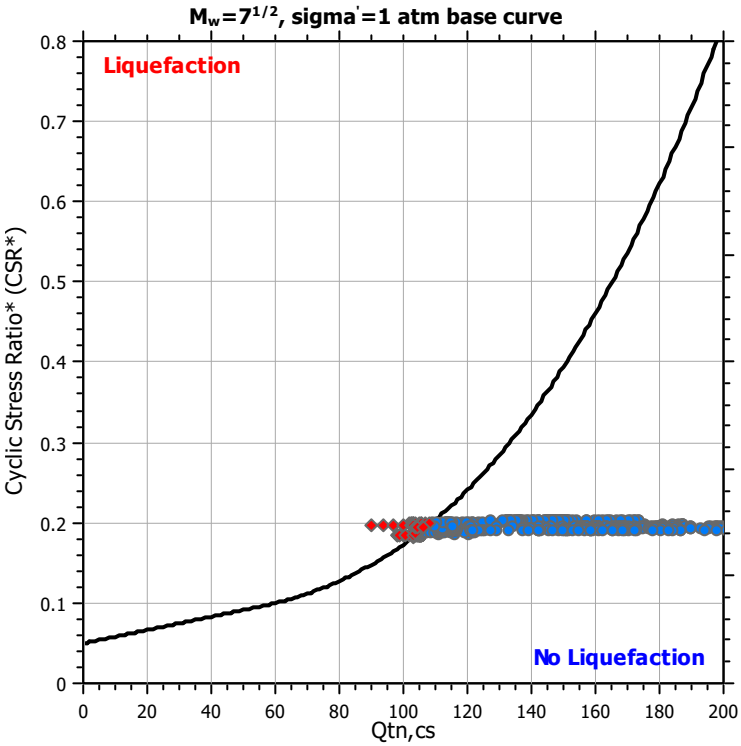
Project title : W1857-88-01 **Location : 331 The City Drive S**

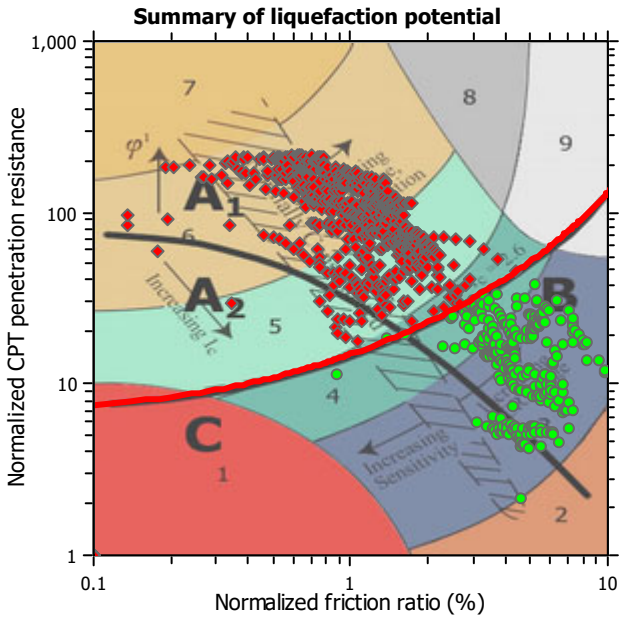
CPT file : CPT-1

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	54.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	30.00 ft	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.12	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.42	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

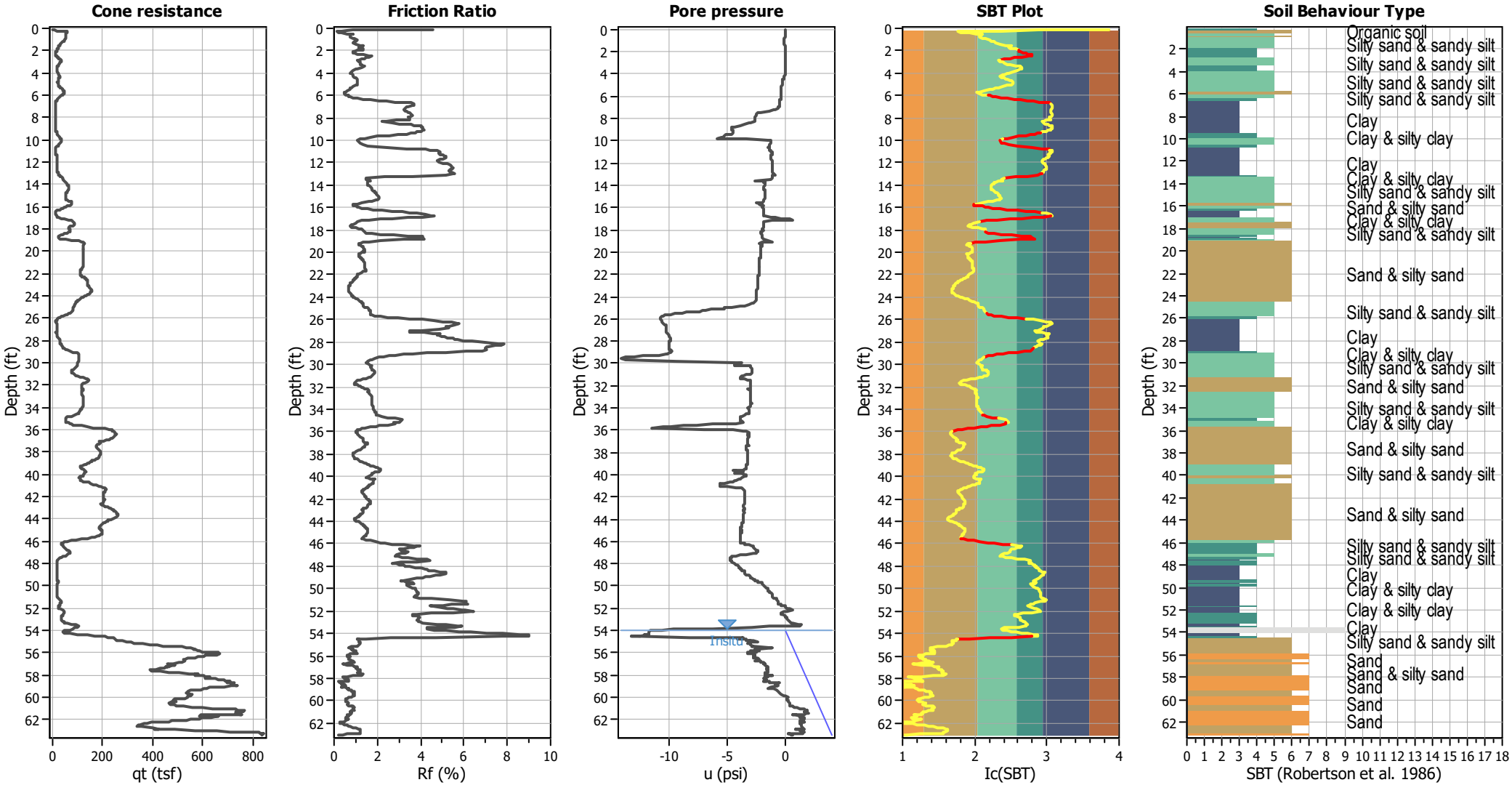






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



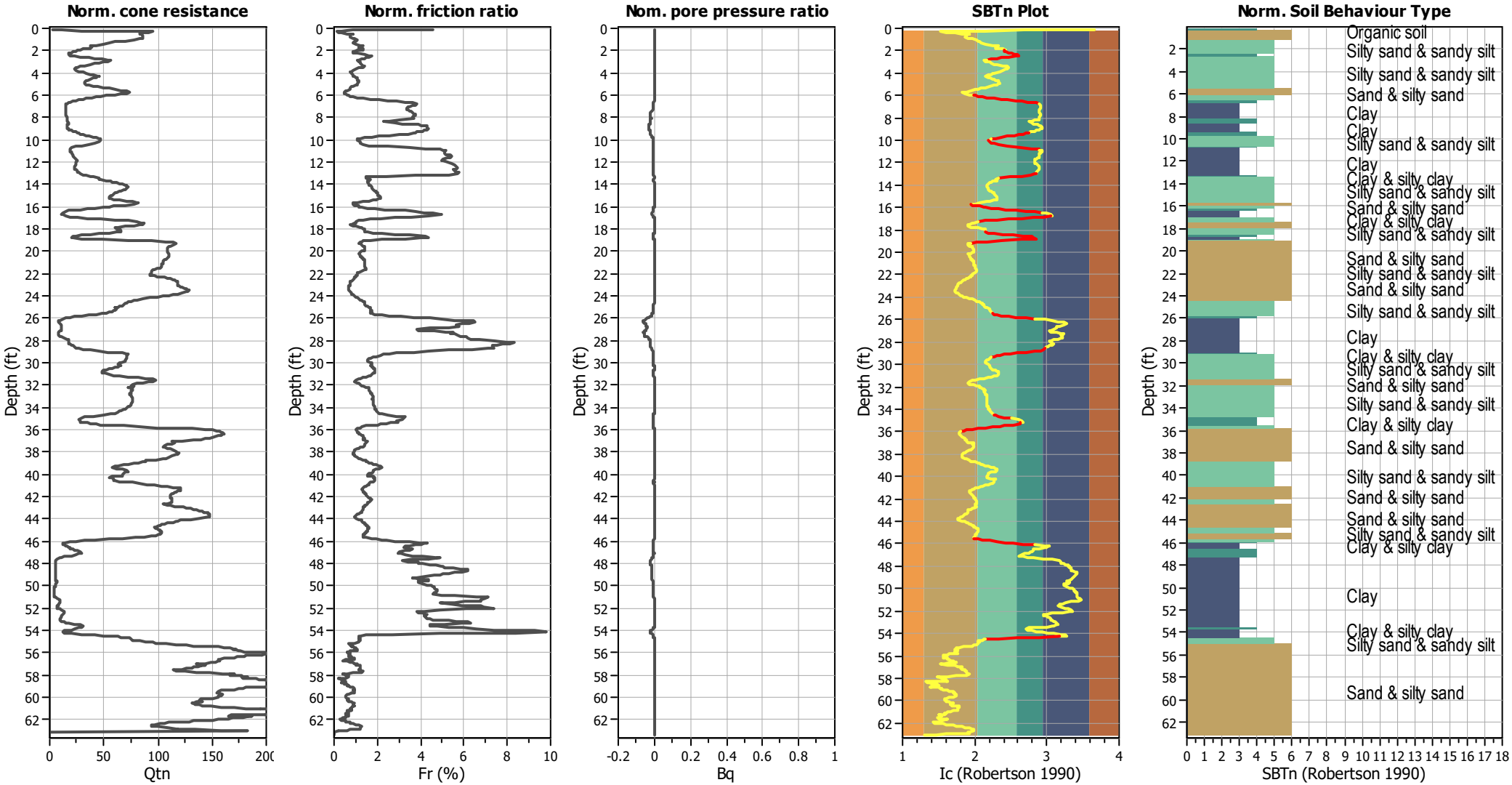
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



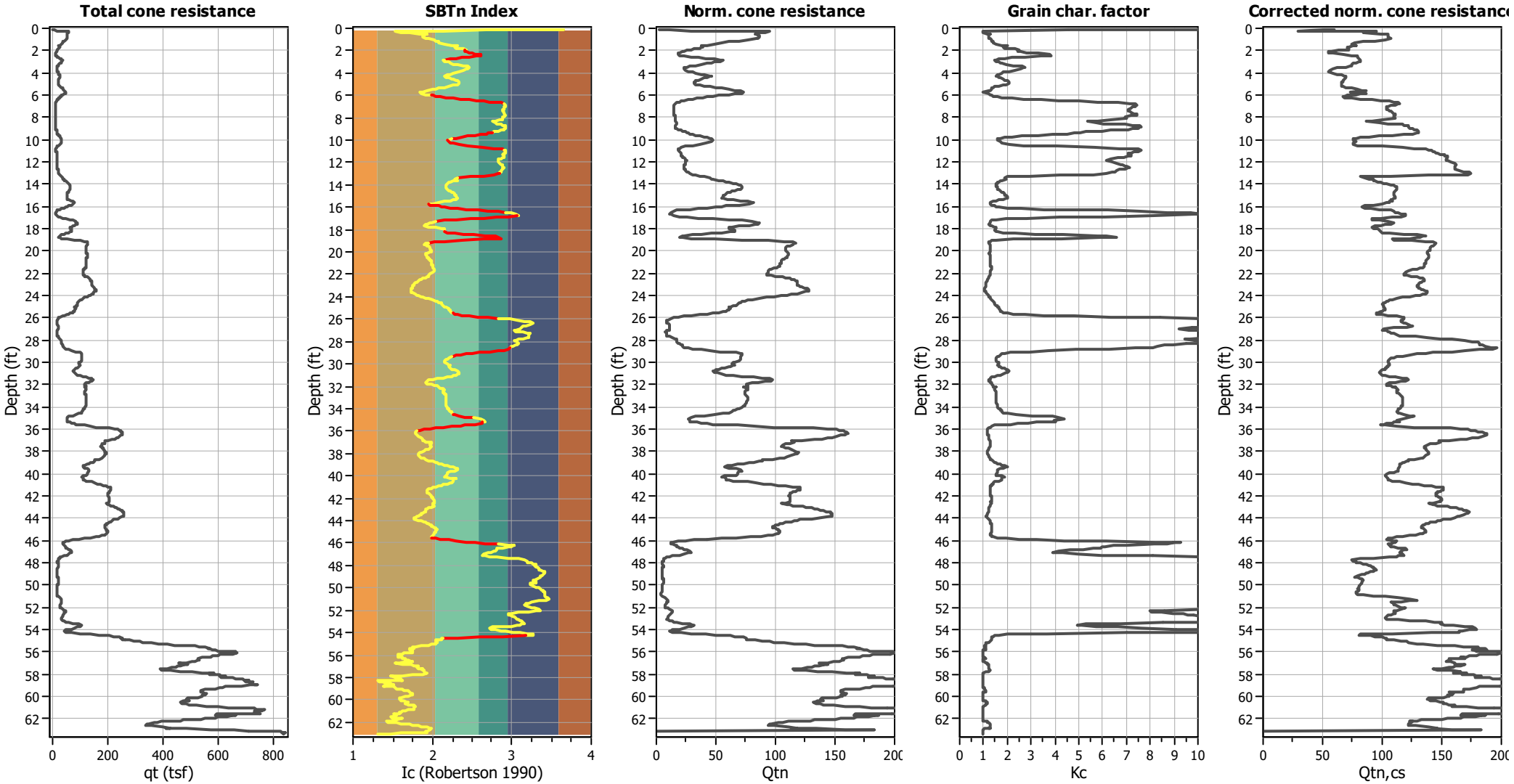
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

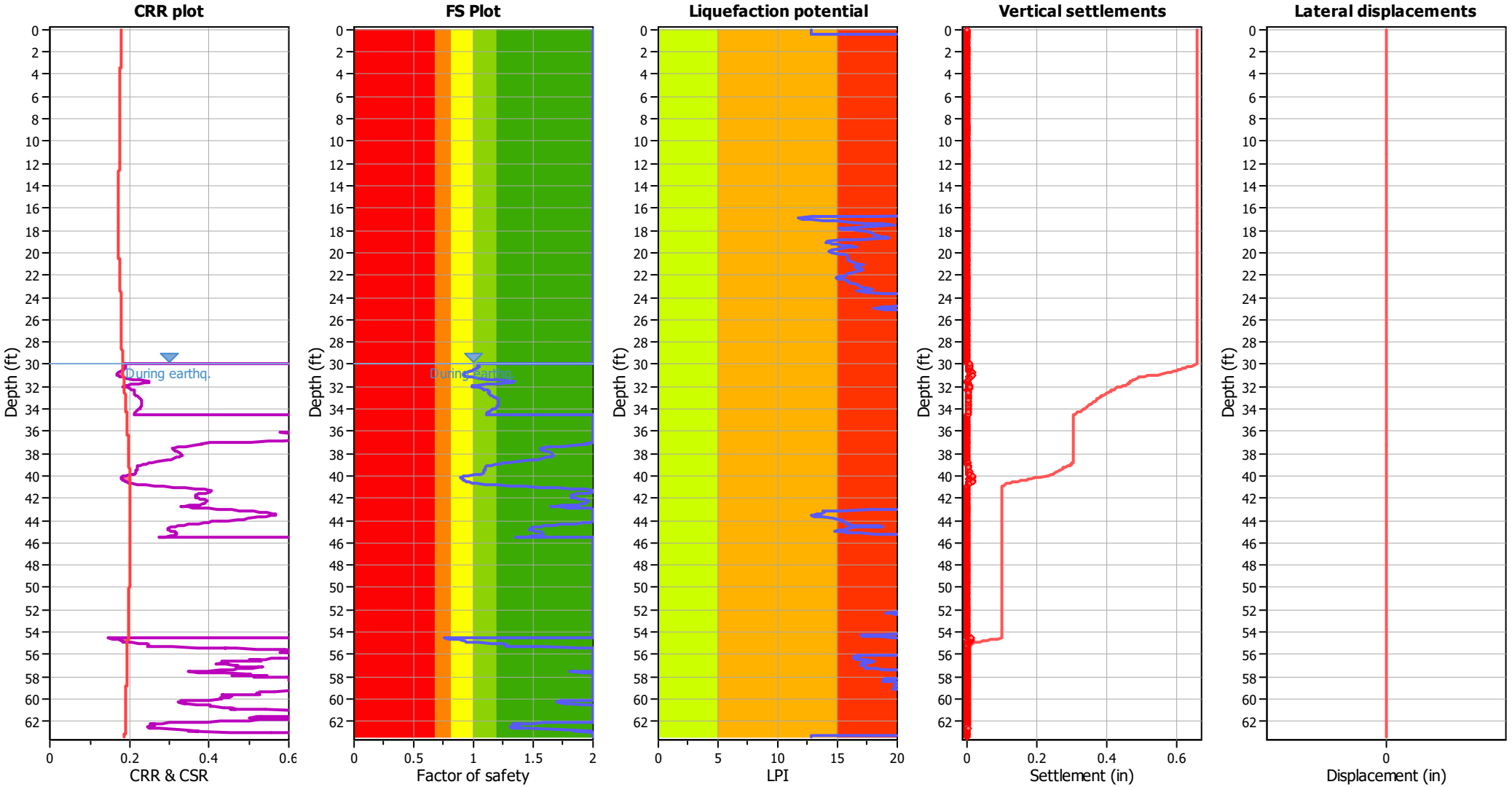
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

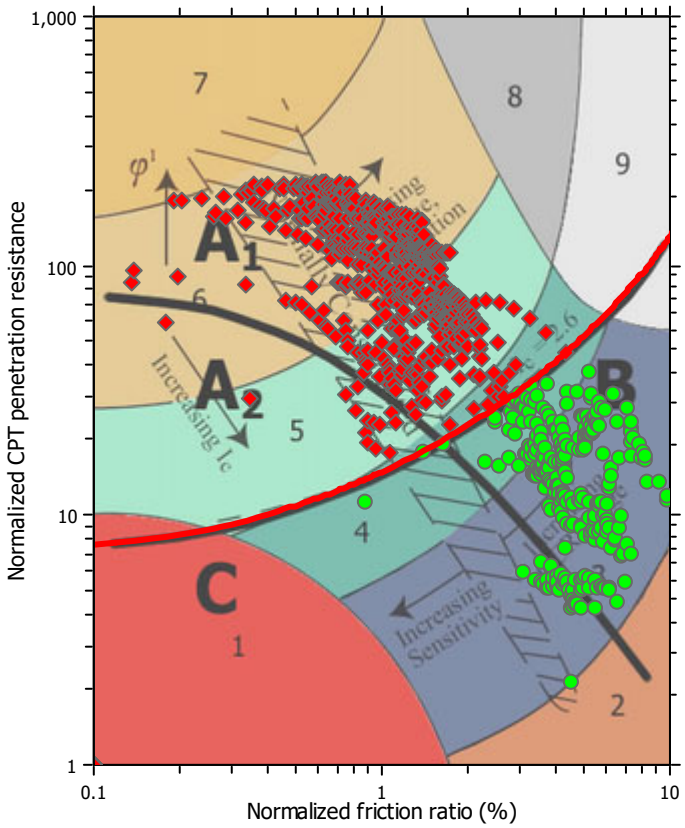
F.S. color scheme

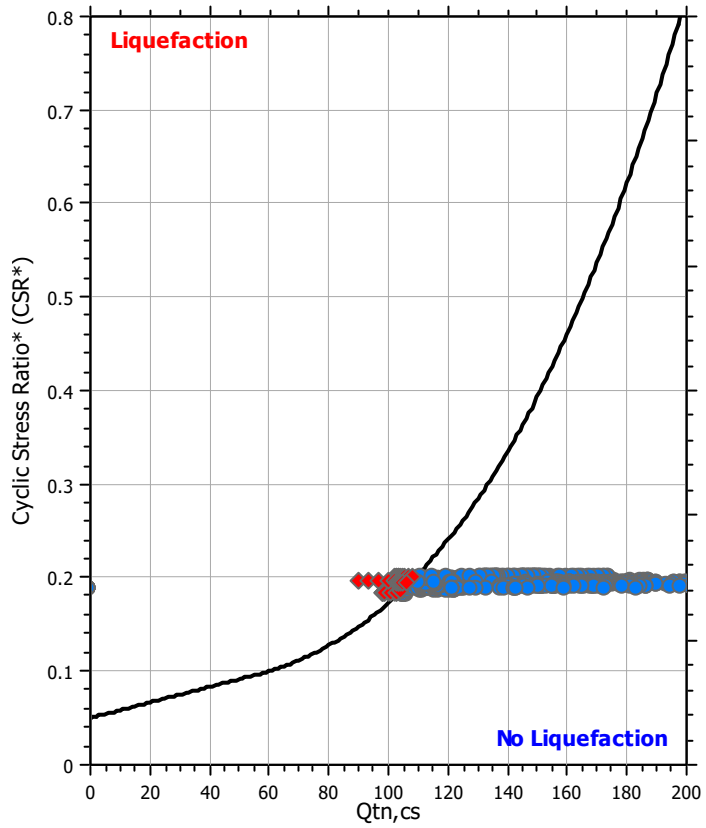
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

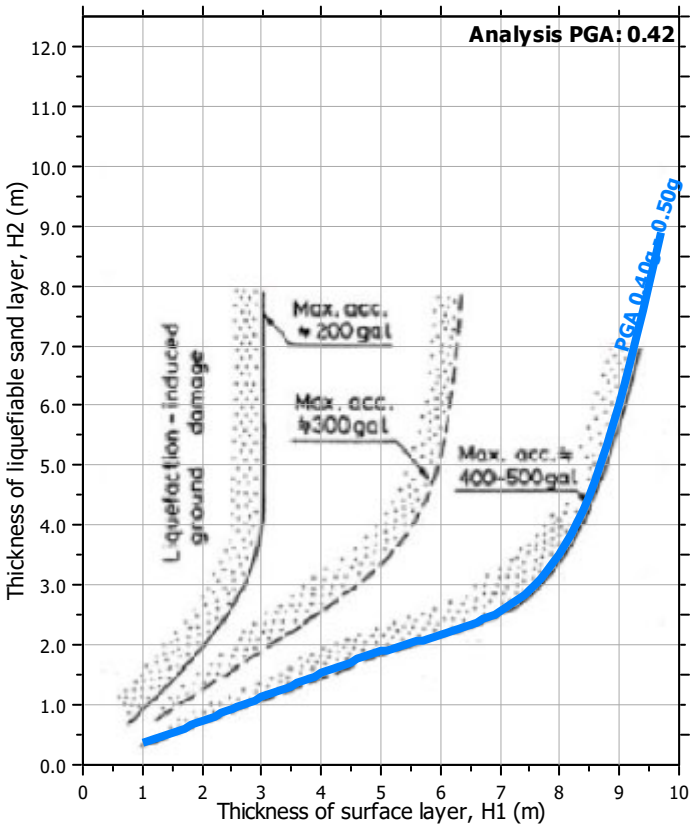
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



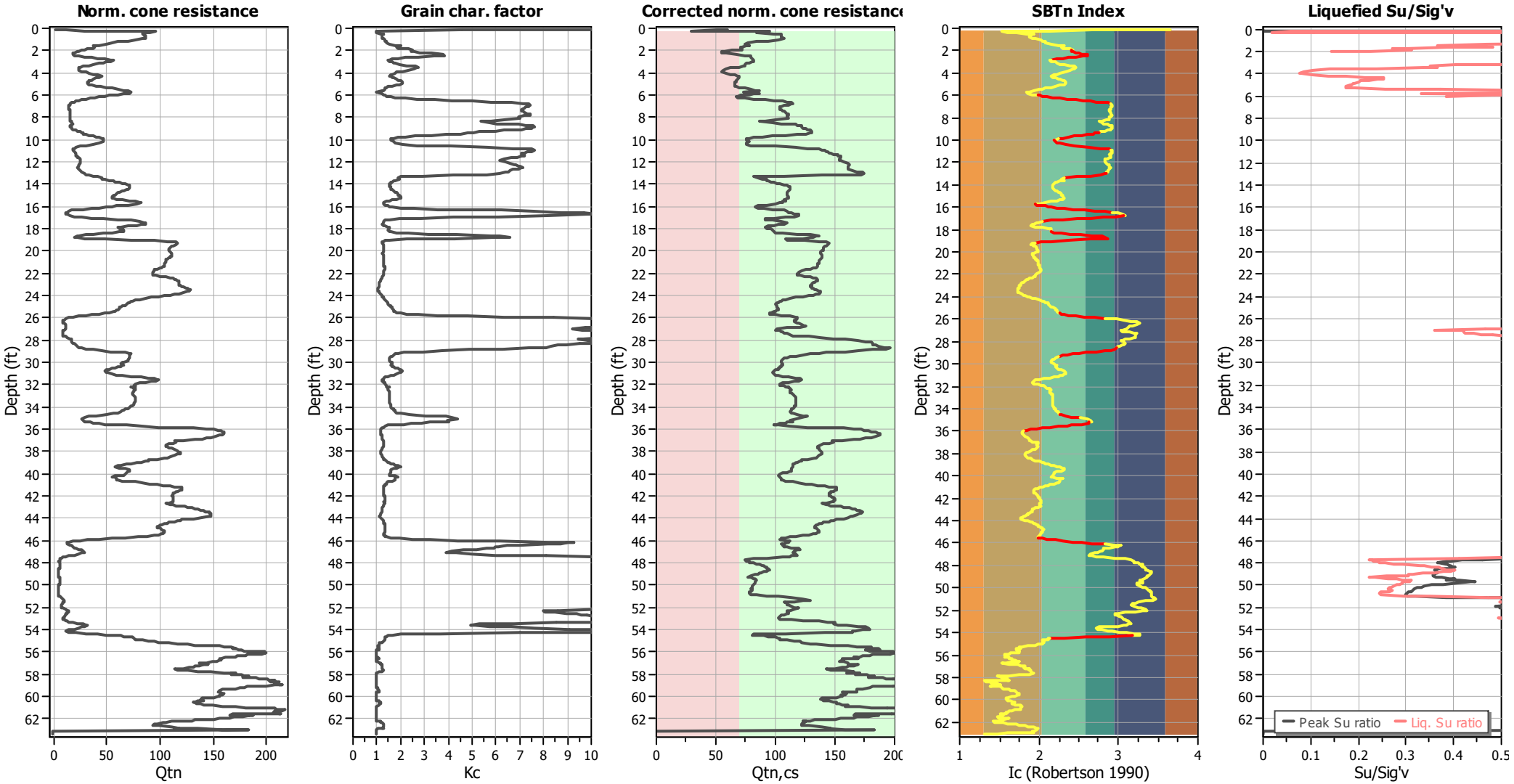




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

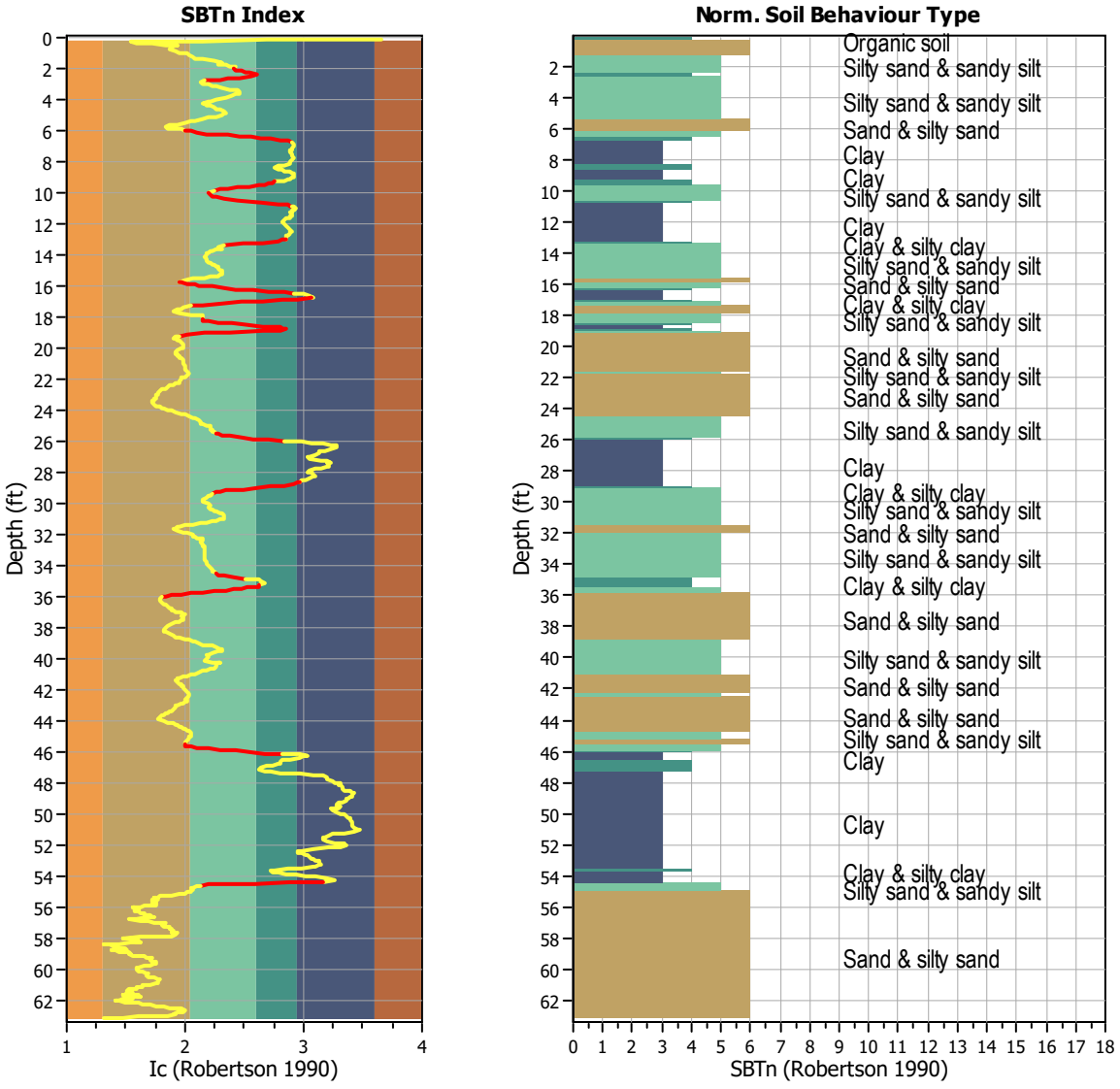
Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	1063
I_c maximum check value:	3.00	Total points excluded:	146
I_c change ratio value:	0.0250	Exclusion percentage:	13.73%
Minimum number of points in layer:	4	Number of layers detected:	16

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	6	Start depth: 2.05 (ft)	5	Silty sand & sandy silt
		End depth: 2.34 (ft)	4	Clay & silty clay
Transition layer 2	8	Start depth: 2.44 (ft)	4	Clay & silty clay
		End depth: 2.89 (ft)	5	Silty sand & sandy silt
Transition layer 3	14	Start depth: 6.02 (ft)	6	Sand & silty sand
		End depth: 6.83 (ft)	3	Clay
Transition layer 4	10	Start depth: 9.38 (ft)	4	Clay & silty clay
		End depth: 9.97 (ft)	5	Silty sand & sandy silt
Transition layer 5	10	Start depth: 10.20 (ft)	5	Silty sand & sandy silt
		End depth: 10.89 (ft)	3	Clay
Transition layer 6	6	Start depth: 13.04 (ft)	3	Clay
		End depth: 13.47 (ft)	5	Silty sand & sandy silt
Transition layer 7	13	Start depth: 15.79 (ft)	6	Sand & silty sand
		End depth: 16.54 (ft)	3	Clay
Transition layer 8	8	Start depth: 16.86 (ft)	3	Clay
		End depth: 17.34 (ft)	6	Sand & silty sand
Transition layer 9	9	Start depth: 18.22 (ft)	5	Silty sand & sandy silt
		End depth: 18.76 (ft)	3	Clay
Transition layer 10	8	Start depth: 18.76 (ft)	3	Clay
		End depth: 19.24 (ft)	6	Sand & silty sand
Transition layer 11	8	Start depth: 25.52 (ft)	5	Silty sand & sandy silt
		End depth: 26.02 (ft)	3	Clay
Transition layer 12	12	Start depth: 28.67 (ft)	3	Clay
		End depth: 29.43 (ft)	5	Silty sand & sandy silt
Transition layer 13	5	Start depth: 34.55 (ft)	5	Silty sand & sandy silt
		End depth: 34.90 (ft)	4	Clay & silty clay
Transition layer 14	13	Start depth: 35.33 (ft)	4	Clay & silty clay
		End depth: 36.06 (ft)	6	Sand & silty sand
Transition layer 15	10	Start depth: 45.56 (ft)	6	Sand & silty sand
		End depth: 46.15 (ft)	3	Clay
Transition layer 16	6	Start depth: 54.34 (ft)	3	Clay
		End depth: 54.53 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.01	0.00	0.01	0.00	N/A	120.90
2	0.04	0.00	0.03	0.00	N/A	120.90
3	0.09	0.00	0.06	0.00	N/A	120.90
4	0.11	0.00	0.06	0.00	N/A	120.90
5	0.14	0.00	0.06	0.00	N/A	120.90
6	0.14	0.00	0.06	0.00	100.00	90.58
7	0.18	4.04	0.06	0.00	39.81	94.62
8	0.23	16.88	0.06	0.00	5.00	97.10
9	0.24	33.66	0.06	0.00	5.00	99.09
10	0.28	59.84	0.07	0.00	4.02	100.70
11	0.33	65.70	0.08	0.00	3.32	101.83
12	0.38	52.26	0.09	0.00	4.29	104.01
13	0.42	51.86	0.16	0.00	5.00	107.23
14	0.47	52.21	0.28	0.00	8.85	111.04
15	0.51	51.45	0.45	0.00	10.39	113.09
16	0.52	52.16	0.45	0.00	11.07	113.95
17	0.57	52.66	0.42	0.00	10.65	113.68
18	0.61	53.17	0.40	0.00	10.18	113.34
19	0.67	53.88	0.39	0.00	9.91	113.08
20	0.73	53.37	0.38	0.00	9.72	112.99
21	0.81	54.28	0.39	-0.10	9.70	112.87
22	0.86	53.22	0.37	-0.10	10.78	114.14
23	0.98	53.07	0.60	-0.10	11.85	114.82
24	1.05	50.14	0.53	-0.10	13.47	114.97
25	1.15	41.44	0.44	-0.10	14.02	113.60
26	1.24	39.42	0.37	-0.10	14.97	111.74
27	1.34	32.75	0.28	-0.10	15.41	110.26
28	1.43	31.24	0.27	0.00	17.53	109.89
29	1.53	27.90	0.36	0.00	20.70	109.99
30	1.58	21.43	0.33	0.00	23.01	110.04
31	1.62	24.36	0.30	0.00	23.24	109.31
32	1.67	24.66	0.28	0.00	21.78	108.90
33	1.75	24.06	0.27	0.00	21.84	108.54
34	1.77	22.95	0.27	0.00	22.45	108.33
35	1.81	22.24	0.27	0.00	23.98	108.08
36	1.86	19.31	0.26	0.00	25.81	107.68
37	1.91	17.59	0.25	0.00	27.51	107.00
38	1.95	16.98	0.22	0.00	27.58	105.88
39	2.00	16.38	0.17	0.00	26.85	104.31
40	2.05	15.26	0.13	0.00	26.79	102.37
41	2.11	13.04	0.11	0.00	27.77	100.94
42	2.20	12.23	0.11	0.00	29.43	100.17
43	2.24	11.73	0.11	0.00	30.90	100.15
44	2.29	11.22	0.11	0.00	32.65	100.53
45	2.34	10.82	0.13	0.00	35.39	102.57
46	2.44	11.93	0.22	0.00	35.96	104.47
47	2.48	13.75	0.24	0.00	33.48	106.65
48	2.58	17.99	0.29	0.00	29.16	108.19

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	2.63	22.34	0.33	0.00	25.09	109.71
50	2.71	26.89	0.36	0.00	22.48	110.79
51	2.78	29.01	0.39	0.00	19.70	111.55
52	2.82	35.08	0.39	0.00	17.69	111.93
53	2.89	37.10	0.38	0.00	16.81	111.84
54	2.96	32.65	0.36	0.00	17.52	111.71
55	3.03	31.13	0.39	0.00	19.08	111.39
56	3.11	28.91	0.36	0.00	20.03	110.91
57	3.19	26.89	0.31	0.00	21.15	109.99
58	3.25	23.55	0.29	0.00	22.96	109.06
59	3.35	20.12	0.28	0.00	25.68	108.30
60	3.41	17.79	0.26	0.00	28.08	107.14
61	3.50	15.47	0.20	0.00	29.06	105.47
62	3.59	14.46	0.15	0.00	28.55	103.57
63	3.69	14.56	0.13	0.00	27.72	102.55
64	3.79	14.76	0.14	0.00	26.19	102.21
65	3.88	16.27	0.13	0.00	24.04	102.29
66	3.97	18.60	0.13	0.00	21.42	103.22
67	4.07	22.54	0.17	0.00	20.94	104.68
68	4.14	21.33	0.21	-0.08	19.71	106.20
69	4.17	26.59	0.22	-0.08	18.89	107.22
70	4.26	28.61	0.25	-0.08	17.51	107.99
71	4.32	29.21	0.26	-0.09	17.59	108.49
72	4.37	28.30	0.27	-0.09	18.27	108.68
73	4.42	26.79	0.27	-0.10	19.47	108.64
74	4.51	24.77	0.27	-0.19	20.53	108.32
75	4.61	23.65	0.25	-0.19	21.42	107.89
76	4.65	22.64	0.24	-0.19	22.24	107.37
77	4.74	20.82	0.23	-0.19	23.28	106.98
78	4.80	19.81	0.22	-0.19	23.69	106.69
79	4.89	20.82	0.22	-0.19	24.07	106.54
80	4.95	19.51	0.22	-0.19	23.69	106.58
81	5.04	20.82	0.22	-0.19	23.00	106.70
82	5.13	22.84	0.22	-0.29	21.27	106.93
83	5.18	24.77	0.22	-0.29	19.16	107.22
84	5.28	28.20	0.23	-0.29	17.18	107.58
85	5.32	31.24	0.23	-0.29	15.37	108.17
86	5.42	34.97	0.25	-0.29	14.24	109.03
87	5.51	37.81	0.29	-0.29	13.16	109.85
88	5.60	41.65	0.30	-0.29	11.39	109.42
89	5.66	44.38	0.19	-0.29	9.82	108.84
90	5.76	46.70	0.21	-0.29	5.00	108.20
91	5.85	46.50	0.23	-0.29	9.42	108.60
92	5.92	41.55	0.23	-0.29	10.81	108.56
93	5.95	35.28	0.23	-0.33	11.91	108.38
94	5.97	37.81	0.23	-0.33	12.79	108.24
95	6.02	35.38	0.23	-0.33	13.11	108.15
96	6.06	32.95	0.23	-0.38	14.35	107.90

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.16	29.92	0.22	-0.38	15.93	107.69
98	6.21	27.09	0.23	-0.38	18.25	107.74
99	6.26	23.96	0.26	-0.38	21.09	108.07
100	6.31	21.83	0.28	-0.48	24.86	108.67
101	6.40	19.10	0.33	-0.48	28.84	109.09
102	6.44	16.78	0.34	-0.48	33.47	109.42
103	6.52	14.86	0.37	-0.48	37.59	109.55
104	6.57	13.75	0.38	-0.48	41.98	109.58
105	6.64	11.83	0.39	-0.48	45.80	109.43
106	6.69	10.92	0.39	-0.48	49.59	109.18
107	6.78	10.21	0.38	-0.48	51.74	108.94
108	6.83	9.91	0.38	-0.48	52.73	108.51
109	6.92	9.60	0.34	-0.48	53.03	108.02
110	6.97	9.30	0.32	-0.57	52.79	107.48
111	7.03	9.30	0.31	-0.57	52.62	107.19
112	7.12	9.30	0.30	-0.57	52.17	107.05
113	7.22	9.40	0.30	-0.86	51.84	107.03
114	7.27	9.50	0.31	-0.95	51.49	107.14
115	7.36	9.70	0.31	-1.34	51.37	107.36
116	7.43	9.81	0.33	-2.10	51.48	107.59
117	7.50	9.81	0.33	-2.39	51.81	107.80
118	7.59	9.81	0.34	-2.48	52.08	107.91
119	7.64	9.81	0.34	-2.48	52.59	107.98
120	7.75	9.60	0.35	-2.48	53.06	108.03
121	7.79	9.60	0.35	-2.48	52.94	108.11
122	7.89	10.01	0.35	-2.58	51.93	108.20
123	7.99	10.41	0.35	-2.58	51.00	108.32
124	8.04	10.41	0.36	-2.58	50.93	108.47
125	8.13	10.31	0.37	-2.58	51.23	108.53
126	8.23	10.31	0.36	-2.67	48.25	107.10
127	8.32	10.31	0.16	-2.96	45.66	105.82
128	8.37	10.31	0.23	-3.15	43.57	105.27
129	8.46	11.12	0.30	-3.44	45.48	107.20
130	8.56	11.83	0.36	-3.53	46.89	108.35
131	8.59	11.12	0.37	-3.93	48.24	108.98
132	8.61	11.12	0.39	-3.93	49.87	109.23
133	8.67	11.02	0.41	-3.93	51.01	109.48
134	8.71	10.71	0.41	-4.39	52.13	109.59
135	8.72	10.51	0.42	-4.49	53.07	109.66
136	8.78	10.51	0.43	-4.58	53.51	109.72
137	8.80	10.51	0.43	-4.58	53.62	109.76
138	8.86	10.51	0.43	-4.58	53.65	109.77
139	8.90	10.51	0.43	-4.58	53.45	109.87
140	8.95	10.82	0.44	-4.58	53.21	110.02
141	8.96	10.92	0.45	-4.58	52.79	110.21
142	9.00	11.12	0.45	-4.58	52.52	110.39
143	9.05	11.32	0.47	-4.49	52.13	110.62
144	9.09	11.62	0.48	-4.49	51.55	110.83

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.10	11.93	0.48	-4.49	50.65	111.10
146	9.14	12.53	0.51	-4.49	49.64	111.46
147	9.20	13.14	0.53	-4.49	48.16	111.91
148	9.24	14.15	0.55	-4.49	46.46	112.37
149	9.29	15.16	0.57	-4.49	44.67	112.78
150	9.31	15.97	0.59	-4.49	43.27	113.20
151	9.38	16.78	0.62	-4.58	42.21	113.51
152	9.41	17.29	0.63	-4.77	40.91	113.67
153	9.47	18.09	0.60	-5.15	39.32	113.64
154	9.53	18.90	0.58	-5.25	36.22	113.38
155	9.62	21.23	0.52	-5.34	32.67	113.07
156	9.67	23.35	0.49	-5.54	28.33	112.63
157	9.77	26.79	0.43	-5.92	25.15	112.27
158	9.81	28.81	0.41	-3.34	22.18	111.77
159	9.90	31.03	0.36	-1.43	20.30	111.35
160	9.97	32.25	0.34	-1.24	18.94	111.09
161	10.06	33.56	0.35	-1.24	18.88	111.19
162	10.20	32.14	0.37	-1.24	19.84	111.65
163	10.30	30.73	0.42	-1.34	21.09	110.81
164	10.44	25.07	0.26	-1.34	23.79	110.16
165	10.54	20.82	0.33	-1.43	28.52	109.42
166	10.63	16.27	0.39	-1.40	37.17	110.42
167	10.74	12.64	0.49	-1.40	45.02	111.01
168	10.78	12.64	0.51	-1.37	49.84	111.50
169	10.83	12.64	0.53	-1.37	50.94	111.75
170	10.88	12.23	0.55	-1.34	52.01	111.93
171	10.89	12.13	0.55	-1.24	53.26	112.19
172	10.97	12.13	0.60	-1.24	53.74	112.49
173	11.02	12.53	0.61	-1.15	53.76	112.83
174	11.07	12.84	0.63	-1.15	53.28	113.04
175	11.11	13.04	0.63	-1.15	52.89	113.23
176	11.16	13.34	0.65	-1.05	52.38	113.46
177	11.21	13.85	0.67	-1.15	51.91	113.73
178	11.26	14.15	0.69	-1.15	51.53	114.03
179	11.30	14.46	0.72	-1.24	51.55	114.31
180	11.36	14.56	0.74	-1.24	51.71	114.56
181	11.40	14.66	0.76	-1.24	51.84	114.75
182	11.45	14.86	0.77	-1.24	51.87	114.90
183	11.50	14.96	0.78	-1.24	51.65	115.06
184	11.55	15.36	0.79	-1.24	51.39	115.24
185	11.60	15.67	0.81	-1.24	50.61	115.51
186	11.66	16.58	0.84	-1.24	49.52	115.80
187	11.74	17.49	0.86	-1.15	48.09	116.04
188	11.84	18.19	0.85	-1.15	47.34	116.23
189	11.93	18.30	0.88	-1.15	47.43	116.42
190	12.04	18.09	0.91	-1.15	48.38	116.63
191	12.13	17.79	0.93	-1.15	49.30	116.79
192	12.22	17.79	0.95	-1.15	50.08	116.85

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.27	17.49	0.95	-1.15	50.46	116.81
194	12.37	17.29	0.93	-1.15	51.02	116.74
195	12.41	17.08	0.93	-1.15	51.24	116.69
196	12.51	17.18	0.94	-1.15	51.67	116.70
197	12.56	16.98	0.94	-1.15	51.47	116.76
198	12.65	17.59	0.95	-1.05	50.92	116.90
199	12.71	18.40	0.97	-1.05	49.81	117.22
200	12.79	19.41	1.02	-1.05	49.34	117.71
201	12.89	19.91	1.11	-0.95	48.93	118.28
202	12.96	21.03	1.17	-0.95	48.62	118.87
203	13.04	22.04	1.25	-0.86	47.37	119.33
204	13.13	23.65	1.26	-1.05	44.91	119.65
205	13.23	26.69	1.23	-1.05	37.79	118.14
206	13.30	30.12	0.44	-1.05	30.22	116.19
207	13.37	34.27	0.48	-1.15	23.39	113.77
208	13.47	38.11	0.56	-1.24	22.02	114.92
209	13.57	42.66	0.63	-2.58	22.72	115.65
210	13.61	35.68	0.65	-1.72	23.01	116.05
211	13.62	39.32	0.66	-1.72	22.69	116.34
212	13.68	45.99	0.69	-1.72	21.00	116.83
213	13.73	47.71	0.72	-1.91	19.82	117.32
214	13.77	49.83	0.75	-1.72	19.40	117.84
215	13.87	52.77	0.82	-1.72	18.89	118.41
216	13.93	56.20	0.87	-1.72	18.50	119.05
217	14.00	58.43	0.92	-1.72	18.11	119.60
218	14.06	61.05	0.98	-1.72	17.96	120.09
219	14.12	62.47	1.02	-1.81	17.96	120.53
220	14.21	63.18	1.08	-1.81	18.11	120.86
221	14.25	63.58	1.10	-1.81	18.27	121.08
222	14.35	63.68	1.12	-1.81	18.46	121.16
223	14.45	62.87	1.11	-1.72	18.76	121.14
224	14.50	61.36	1.11	-1.72	19.22	121.02
225	14.59	59.03	1.09	-1.72	19.83	120.88
226	14.64	57.21	1.08	-1.72	20.46	120.71
227	14.74	55.39	1.07	-1.72	21.03	120.57
228	14.80	54.28	1.06	-1.72	21.53	120.45
229	14.88	53.07	1.06	-1.72	21.95	120.36
230	14.97	52.26	1.05	-1.72	22.36	120.29
231	15.05	51.45	1.05	-1.72	22.79	120.27
232	15.13	50.64	1.07	-1.72	23.16	120.29
233	15.21	50.54	1.07	-1.72	23.18	120.30
234	15.28	51.76	1.05	-1.81	22.62	120.34
235	15.36	54.48	1.06	-1.91	21.45	120.45
236	15.41	59.13	1.06	-1.91	19.60	120.68
237	15.50	67.12	1.06	-2.00	17.73	120.96
238	15.55	72.98	1.07	-2.48	14.99	120.29
239	15.65	78.34	0.69	-2.00	12.97	119.36
240	15.71	79.55	0.68	-2.29	11.49	118.07

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.79	76.72	0.66	-2.00	11.94	117.74
242	15.89	69.04	0.63	-1.81	13.58	117.28
243	15.90	56.20	0.63	-1.93	15.06	116.86
244	15.94	58.12	0.62	-1.93	16.49	116.54
245	16.00	54.38	0.60	-1.93	17.46	116.33
246	16.06	47.31	0.61	-1.81	19.74	116.08
247	16.14	41.44	0.62	-1.81	23.40	115.82
248	16.19	33.56	0.63	-1.81	27.82	115.40
249	16.26	27.39	0.61	-1.81	33.97	114.66
250	16.33	20.42	0.58	-1.81	40.60	113.74
251	16.38	16.88	0.54	-1.81	47.75	112.60
252	16.47	13.95	0.48	-1.81	53.58	111.81
253	16.54	12.53	0.50	-1.81	58.20	111.16
254	16.62	11.52	0.48	-1.81	61.95	111.19
255	16.70	11.42	0.52	-1.81	63.86	111.41
256	16.76	11.73	0.55	-1.72	62.72	112.21
257	16.86	13.75	0.62	-1.24	55.66	113.21
258	16.90	19.21	0.65	-0.86	46.99	114.45
259	16.98	25.07	0.71	-0.29	37.95	115.60
260	17.05	33.26	0.75	0.38	29.58	116.88
261	17.14	47.91	0.80	0.67	22.70	117.88
262	17.20	61.46	0.80	-1.15	17.44	118.65
263	17.29	75.11	0.79	-1.91	14.33	119.10
264	17.34	82.59	0.81	-1.91	12.57	119.56
265	17.44	88.35	0.86	-1.91	12.10	120.15
266	17.50	89.76	0.95	-1.91	11.17	119.56
267	17.58	88.65	0.59	-1.91	10.61	118.74
268	17.64	86.12	0.61	-1.91	10.36	117.68
269	17.75	80.36	0.68	-1.91	11.68	118.09
270	17.82	75.11	0.73	-1.91	14.12	118.45
271	17.89	60.85	0.79	-1.94	16.11	118.58
272	17.89	62.17	0.79	-1.94	17.43	118.74
273	17.96	65.10	0.82	-1.94	17.29	119.02
274	18.02	65.00	0.86	-1.91	17.38	119.46
275	18.07	66.01	0.93	-2.00	17.40	119.89
276	18.17	69.65	0.96	-2.00	17.19	120.21
277	18.22	70.76	0.96	-2.10	17.38	120.34
278	18.30	65.91	0.98	-2.10	18.63	120.33
279	18.36	59.03	1.01	-2.10	21.57	120.25
280	18.42	48.22	1.05	-2.00	25.82	120.15
281	18.50	40.43	1.10	-2.00	31.86	119.89
282	18.56	31.34	1.11	-2.00	38.47	119.44
283	18.62	25.47	1.08	-2.00	45.73	118.51
284	18.69	20.42	0.95	-2.00	47.28	117.84
285	18.76	26.08	0.90	-2.00	49.35	117.26
286	18.84	20.22	0.92	-1.91	46.20	117.56
287	18.89	26.69	0.98	-1.81	38.13	118.84
288	18.98	48.82	1.15	-1.53	25.23	120.89

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	19.05	83.09	1.28	-1.15	17.63	122.71
290	19.12	103.41	1.40	-2.00	13.45	123.88
291	19.18	118.98	1.44	-2.19	11.63	124.47
292	19.24	125.34	1.44	-2.00	10.70	124.75
293	19.32	127.97	1.47	-2.10	10.50	124.90
294	19.38	127.06	1.50	-2.00	10.78	125.14
295	19.46	124.64	1.59	-2.00	11.28	125.37
296	19.54	122.82	1.64	-2.10	11.83	125.56
297	19.62	120.49	1.66	-2.10	12.18	125.64
298	19.70	119.78	1.66	-2.10	12.37	125.65
299	19.80	119.78	1.65	-2.10	12.42	125.63
300	19.85	119.78	1.65	-2.10	12.39	125.59
301	19.94	119.78	1.64	-2.10	12.46	125.66
302	20.03	120.39	1.70	-2.10	11.91	125.24
303	20.13	122.11	1.36	-2.10	11.37	124.85
304	20.19	123.12	1.38	-2.10	10.74	124.42
305	20.29	124.84	1.43	-2.10	10.87	124.64
306	20.39	124.28	1.47	-2.15	11.01	124.81
307	20.43	124.49	1.48	-2.15	11.19	124.93
308	20.47	123.73	1.51	-2.15	11.32	125.04
309	20.52	124.13	1.54	-2.19	11.55	125.23
310	20.61	124.13	1.61	-2.19	11.79	125.44
311	20.66	123.73	1.64	-2.19	12.08	125.60
312	20.71	122.01	1.65	-2.19	12.32	125.65
313	20.77	121.00	1.66	-2.19	12.55	125.68
314	20.85	120.09	1.67	-2.19	12.67	125.69
315	20.91	120.59	1.67	-2.19	12.69	125.72
316	21.00	121.30	1.67	-2.19	12.68	125.74
317	21.05	121.20	1.68	-2.19	12.72	125.75
318	21.11	120.39	1.68	-2.19	12.82	125.76
319	21.19	119.99	1.69	-2.19	12.93	125.79
320	21.24	120.19	1.70	-2.19	12.99	125.84
321	21.34	120.59	1.71	-2.19	13.03	125.87
322	21.39	120.49	1.71	-2.19	13.11	125.88
323	21.48	118.98	1.71	-2.19	13.31	125.83
324	21.53	116.65	1.70	-2.19	13.57	125.71
325	21.64	113.62	1.66	-2.19	13.84	125.53
326	21.72	111.39	1.62	-2.19	13.51	124.89
327	21.81	110.48	1.31	-2.19	12.90	124.15
328	21.89	110.59	1.24	-2.29	12.18	123.40
329	21.97	110.59	1.21	-2.29	11.93	123.16
330	22.05	110.99	1.19	-2.29	11.80	123.03
331	22.12	110.94	1.17	-2.34	11.72	122.95
332	22.13	110.94	1.17	-2.34	11.70	122.93
333	22.18	110.89	1.18	-2.34	11.57	122.96
334	22.22	114.22	1.18	-2.39	11.23	123.02
335	22.28	118.47	1.17	-2.39	10.74	123.13
336	22.33	122.82	1.19	-2.39	10.28	123.26

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.38	126.46	1.20	-2.39	9.90	123.41
338	22.41	129.89	1.21	-2.39	9.50	123.49
339	22.51	133.73	1.20	-2.39	9.14	123.51
340	22.56	135.96	1.18	-2.39	8.79	123.46
341	22.61	137.98	1.16	-2.39	8.51	123.37
342	22.65	139.19	1.14	-2.39	8.23	123.24
343	22.71	140.61	1.11	-2.39	8.00	123.09
344	22.76	141.21	1.08	-2.39	7.75	122.87
345	22.85	141.72	1.03	-2.39	7.57	122.67
346	22.89	141.82	1.02	-2.39	7.41	122.48
347	22.99	141.92	1.00	-2.39	7.34	122.38
348	23.04	141.92	0.99	-2.39	7.26	122.31
349	23.12	142.83	0.99	-2.39	7.17	122.30
350	23.18	145.06	0.99	-2.39	7.02	122.35
351	23.24	147.58	1.00	-2.39	6.88	122.47
352	23.33	150.11	1.02	-2.39	6.74	122.61
353	23.38	153.24	1.03	-2.48	6.65	122.79
354	23.47	155.06	1.05	-2.48	6.58	122.94
355	23.52	156.58	1.07	-2.48	6.66	123.16
356	23.61	156.07	1.12	-2.48	6.86	123.36
357	23.68	153.95	1.15	-2.48	7.23	123.57
358	23.76	150.31	1.19	-2.48	7.68	123.69
359	23.83	145.46	1.20	-2.48	8.20	123.74
360	23.90	140.61	1.21	-2.48	8.71	123.73
361	23.97	136.36	1.22	-2.48	9.28	123.71
362	24.05	131.21	1.23	-2.48	9.97	123.67
363	24.10	123.63	1.24	-2.48	10.81	123.59
364	24.19	116.75	1.24	-2.48	11.87	123.44
365	24.27	108.16	1.24	-2.48	12.89	123.28
366	24.34	103.31	1.24	-2.48	13.89	123.13
367	24.43	98.56	1.23	-2.58	14.65	123.04
368	24.48	96.03	1.24	-2.58	15.39	123.04
369	24.57	93.50	1.28	-2.77	16.07	123.15
370	24.62	91.89	1.32	-2.86	16.33	122.96
371	24.72	90.17	1.17	-3.15	16.56	122.82
372	24.81	89.06	1.23	-3.53	16.74	122.68
373	24.86	88.15	1.26	-3.91	17.34	122.92
374	24.95	86.83	1.31	-4.58	18.26	123.01
375	25.01	80.77	1.32	-5.22	19.01	123.05
376	25.02	81.12	1.32	-5.22	19.54	123.03
377	25.05	81.47	1.33	-5.22	19.39	123.10
378	25.11	83.09	1.34	-6.01	19.35	123.16
379	25.15	82.69	1.35	-6.39	19.38	123.22
380	25.21	82.08	1.36	-6.87	19.61	123.23
381	25.25	81.27	1.36	-7.16	19.86	123.21
382	25.30	80.16	1.35	-7.45	20.12	123.10
383	25.40	78.24	1.31	-8.49	20.43	122.88
384	25.45	76.01	1.27	-8.88	20.89	122.49

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.52	71.57	1.20	-9.54	21.58	121.99
386	25.60	66.92	1.12	-9.93	23.10	121.43
387	25.66	58.73	1.10	-10.40	25.37	120.85
388	25.74	51.45	1.05	-10.50	29.28	120.35
389	25.80	42.15	1.06	-10.69	34.11	119.74
390	25.88	34.67	1.01	-10.79	40.89	119.02
391	25.94	26.89	0.97	-10.79	48.17	118.23
392	26.02	22.64	0.95	-10.79	56.96	117.39
393	26.09	19.00	0.88	-10.79	63.54	116.56
394	26.17	16.38	0.82	-10.69	70.12	115.68
395	26.23	14.15	0.78	-10.69	75.56	115.05
396	26.29	13.44	0.77	-10.69	79.02	114.78
397	26.37	13.55	0.78	-10.50	78.84	114.95
398	26.46	14.66	0.82	-10.50	75.43	115.54
399	26.55	17.08	0.90	-10.40	71.32	116.21
400	26.60	18.40	0.93	-10.31	68.23	116.84
401	26.70	19.10	0.98	-10.31	67.29	117.29
402	26.78	19.31	1.04	-10.31	67.28	117.57
403	26.87	19.31	1.03	-10.31	65.46	116.94
404	26.94	19.31	0.72	-10.31	62.21	115.56
405	27.03	19.00	0.56	-10.31	60.24	114.24
406	27.13	17.99	0.66	-10.31	61.72	113.90
407	27.18	16.98	0.66	-10.31	68.38	114.01
408	27.27	13.14	0.67	-10.20	73.05	113.89
409	27.32	14.15	0.68	-10.20	75.75	113.91
410	27.37	15.16	0.70	-10.20	73.86	114.24
411	27.41	15.16	0.73	-10.12	73.36	114.52
412	27.46	15.16	0.75	-10.12	74.03	114.74
413	27.51	15.16	0.76	-10.02	74.31	115.06
414	27.61	15.67	0.82	-10.02	73.92	115.57
415	27.66	16.68	0.89	-9.93	72.75	116.57
416	27.73	18.50	1.06	-9.93	69.00	118.04
417	27.80	23.15	1.28	-9.93	64.92	119.84
418	27.88	27.09	1.57	-9.93	61.75	121.59
419	27.96	29.72	1.88	-9.93	61.15	122.86
420	28.04	29.82	2.03	-10.02	62.65	123.82
421	28.12	29.21	2.29	-10.02	64.46	124.33
422	28.18	29.31	2.33	-10.02	64.94	124.77
423	28.27	31.24	2.40	-10.02	63.60	125.01
424	28.32	32.85	2.43	-10.02	61.44	125.31
425	28.42	34.87	2.48	-10.02	59.28	125.61
426	28.47	37.40	2.56	-10.02	57.63	126.07
427	28.61	39.22	2.75	-10.02	56.63	126.53
428	28.67	40.43	2.86	-10.02	55.75	127.05
429	28.75	43.16	3.02	-10.02	52.70	127.47
430	28.81	47.71	3.06	-9.93	47.96	127.92
431	28.90	58.12	3.04	-9.83	41.37	128.35
432	29.00	72.07	3.02	-9.93	35.34	128.76

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	29.05	82.28	3.02	-10.02	30.50	129.11
434	29.10	94.11	3.00	-10.21	27.19	129.31
435	29.15	101.79	2.92	-10.31	24.40	129.24
436	29.24	107.76	2.68	-10.98	22.48	128.87
437	29.29	108.56	2.46	-12.31	21.04	128.21
438	29.37	106.54	2.19	-13.08	20.19	127.50
439	29.43	105.43	2.02	-13.84	19.39	126.74
440	29.53	104.93	1.82	-14.22	18.65	126.11
441	29.62	104.93	1.70	-13.79	18.12	125.67
442	29.68	104.93	1.71	-13.74	17.48	125.18
443	29.80	104.93	1.48	-9.45	17.32	124.98
444	29.91	103.81	1.57	-4.29	17.30	124.83
445	30.00	102.90	1.62	-3.72	18.66	124.98
446	30.07	90.77	1.65	-4.39	19.24	125.07
447	30.15	98.76	1.66	-4.39	19.60	125.10
448	30.21	99.47	1.66	-4.39	19.01	125.18
449	30.26	99.06	1.66	-2.96	19.09	125.17
450	30.31	97.75	1.66	-2.96	19.36	125.12
451	30.38	95.83	1.65	-2.96	19.77	125.02
452	30.45	93.10	1.62	-2.86	20.38	124.87
453	30.50	89.06	1.61	-2.86	21.16	124.68
454	30.55	85.31	1.58	-2.86	22.05	124.38
455	30.64	80.56	1.51	-2.86	22.84	124.05
456	30.70	77.83	1.46	-2.86	23.38	123.62
457	30.79	75.51	1.39	-2.86	23.69	123.34
458	30.84	74.90	1.38	-2.86	23.72	123.20
459	30.93	76.12	1.39	-2.96	23.33	123.30
460	30.98	79.96	1.42	-3.05	22.53	123.52
461	31.05	84.51	1.45	-3.34	21.39	123.92
462	31.13	91.68	1.54	-3.63	20.20	124.38
463	31.17	98.66	1.60	-3.72	18.55	124.91
464	31.27	111.19	1.64	-3.91	16.70	125.32
465	31.32	123.12	1.65	-3.82	14.63	125.57
466	31.41	135.55	1.59	-3.44	13.02	125.62
467	31.46	141.82	1.54	-3.25	11.83	125.51
468	31.52	145.46	1.49	-3.05	11.07	125.22
469	31.61	145.97	1.37	-3.05	10.64	124.85
470	31.66	143.74	1.32	-3.05	10.61	124.43
471	31.75	136.87	1.28	-3.05	11.17	124.24
472	31.80	129.59	1.32	-3.05	12.39	124.35
473	31.90	121.10	1.46	-2.96	13.62	124.39
474	31.94	115.44	1.39	-2.96	14.62	124.45
475	32.04	114.12	1.42	-2.96	14.97	124.60
476	32.09	118.67	1.55	-2.96	15.15	125.24
477	32.20	124.84	1.74	-3.02	15.99	125.83
478	32.24	112.71	1.82	-3.02	16.70	126.23
479	32.28	115.74	1.85	-3.07	17.46	126.32
480	32.29	115.74	1.86	-3.07	17.17	126.42

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	32.30	118.77	1.87	-3.25	16.87	126.53
482	32.40	122.41	1.90	-3.05	16.70	126.62
483	32.45	120.49	1.91	-3.05	16.81	126.69
484	32.55	118.67	1.92	-3.05	17.10	126.69
485	32.59	118.37	1.92	-3.05	17.33	126.73
486	32.69	118.07	1.95	-3.05	17.51	126.82
487	32.76	118.07	1.99	-2.96	17.74	126.96
488	32.84	118.27	2.04	-2.96	17.92	127.13
489	32.90	118.98	2.08	-2.96	18.01	127.28
490	32.98	119.89	2.11	-2.96	17.99	127.39
491	33.06	121.10	2.12	-3.05	17.91	127.48
492	33.12	122.21	2.13	-3.05	17.81	127.55
493	33.22	123.12	2.15	-3.05	17.76	127.60
494	33.31	123.32	2.16	-3.05	17.76	127.64
495	33.37	123.32	2.16	-2.96	17.77	127.65
496	33.46	123.32	2.16	-2.96	17.80	127.65
497	33.55	123.32	2.17	-2.86	17.87	127.68
498	33.65	123.02	2.18	-2.96	17.99	127.72
499	33.70	122.72	2.20	-2.96	18.14	127.75
500	33.79	122.11	2.21	-2.96	18.29	127.77
501	33.89	121.40	2.21	-3.05	18.48	127.74
502	33.99	119.89	2.19	-3.25	18.70	127.68
503	34.04	118.17	2.18	-3.25	18.98	127.58
504	34.13	115.44	2.15	-3.15	19.34	127.46
505	34.23	113.01	2.13	-3.15	19.82	127.32
506	34.32	109.78	2.11	-3.15	20.27	127.22
507	34.37	108.16	2.10	-3.15	20.65	127.13
508	34.47	106.85	2.09	-3.15	21.01	127.08
509	34.55	104.93	2.10	-3.34	21.77	127.01
510	34.63	98.76	2.11	-3.53	23.58	126.91
511	34.73	86.43	2.14	-3.72	26.59	126.63
512	34.80	74.09	2.10	-3.91	31.19	126.00
513	34.90	57.92	1.93	-3.91	36.19	125.07
514	35.00	49.53	1.74	-3.91	37.59	123.92
515	35.12	57.47	1.42	-3.91	38.98	122.90
516	35.20	44.27	1.40	-3.72	36.68	122.71
517	35.33	57.01	1.55	-3.63	36.87	123.05
518	35.41	59.84	1.61	-4.20	32.11	123.80
519	35.44	73.57	1.62	-6.27	29.94	124.11
520	35.48	72.58	1.63	-6.27	26.74	124.41
521	35.57	84.61	1.62	-7.64	24.34	124.63
522	35.62	95.42	1.62	-8.78	20.42	125.05
523	35.67	116.45	1.64	-9.93	17.13	125.56
524	35.71	134.74	1.71	-10.60	14.14	126.40
525	35.82	161.84	1.91	-11.55	12.01	127.28
526	35.86	183.57	2.03	-11.17	10.22	128.24
527	35.93	210.36	2.20	-6.97	8.94	129.00
528	36.01	229.56	2.33	-4.49	8.16	129.62

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	36.06	236.44	2.41	-3.63	7.85	130.06
530	36.12	240.88	2.52	-3.34	7.80	130.37
531	36.18	244.83	2.59	-3.15	7.84	130.72
532	36.25	249.58	2.73	-3.15	7.88	131.01
533	36.30	251.80	2.80	-3.15	8.05	131.37
534	36.39	253.32	2.97	-3.25	8.23	131.64
535	36.44	253.52	3.03	-3.15	8.49	131.92
536	36.53	252.51	3.13	-3.25	8.77	132.08
537	36.59	248.57	3.20	-3.15	9.37	132.44
538	36.68	244.22	3.54	-3.25	9.70	132.41
539	36.75	237.75	3.16	-3.25	9.93	132.25
540	36.83	233.20	3.05	-3.25	9.92	131.78
541	36.90	225.32	3.02	-3.25	10.25	131.57
542	36.97	217.43	2.99	-3.25	10.78	131.42
543	37.02	208.94	2.97	-3.25	11.95	131.17
544	37.04	178.92	2.94	-3.25	12.56	130.99
545	37.08	193.37	2.89	-3.25	12.85	130.76
546	37.17	193.68	2.77	-3.25	12.27	130.55
547	37.27	188.42	2.66	-3.25	12.36	130.20
548	37.37	179.93	2.56	-3.15	12.63	129.85
549	37.42	175.89	2.48	-3.34	12.60	129.41
550	37.51	175.94	2.26	-3.34	12.21	128.93
551	37.58	175.99	2.11	-3.34	11.53	128.42
552	37.66	179.12	2.01	-3.34	10.87	128.00
553	37.76	182.05	1.88	-3.34	10.12	127.61
554	37.85	186.70	1.77	-3.25	9.43	127.24
555	37.93	189.63	1.70	-3.25	8.90	127.02
556	38.04	192.67	1.69	-3.25	8.61	126.94
557	38.13	194.59	1.69	-3.25	8.49	126.94
558	38.18	194.49	1.69	-3.25	8.53	126.96
559	38.28	191.76	1.70	-3.25	8.89	127.11
560	38.37	187.61	1.81	-3.25	9.47	127.34
561	38.47	182.96	1.89	-3.25	10.26	127.74
562	38.57	180.23	2.05	-3.25	10.93	128.06
563	38.62	178.11	2.10	-3.25	11.67	128.38
564	38.72	172.15	2.20	-3.25	12.92	128.49
565	38.78	152.33	2.27	-3.26	13.99	128.58
566	38.81	156.28	2.28	-3.25	14.73	128.61
567	38.86	157.49	2.30	-3.25	14.82	128.67
568	38.91	151.93	2.32	-3.25	15.34	128.70
569	38.95	146.77	2.36	-3.25	16.32	128.70
570	39.05	139.19	2.39	-3.25	17.39	128.67
571	39.09	132.82	2.40	-3.34	18.62	128.58
572	39.14	125.24	2.40	-3.34	19.92	128.44
573	39.24	117.26	2.39	-3.34	21.20	128.25
574	39.29	112.20	2.35	-3.34	22.35	128.02
575	39.39	107.15	2.30	-3.34	23.14	127.89
576	39.43	106.24	2.34	-3.34	23.05	127.94

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	39.53	114.22	2.38	-3.53	21.86	128.13
578	39.57	124.74	2.36	-3.63	20.02	128.31
579	39.68	133.73	2.34	-4.49	18.81	128.39
580	39.73	133.63	2.33	-3.67	18.53	128.37
581	39.81	128.68	2.32	-4.39	18.86	128.23
582	39.89	125.85	2.25	-3.72	18.82	127.76
583	39.96	124.74	1.96	-3.44	18.19	127.14
584	40.06	125.34	1.81	-3.34	17.66	126.63
585	40.15	123.63	1.86	-3.34	17.93	126.54
586	40.20	119.28	1.91	-3.44	19.75	126.53
587	40.24	100.48	1.93	-3.71	21.16	126.50
588	40.26	106.09	1.93	-3.71	22.23	126.44
589	40.27	106.09	1.94	-3.71	21.47	126.59
590	40.37	111.70	1.99	-3.91	21.22	126.73
591	40.42	111.70	2.01	-4.01	21.04	126.91
592	40.52	111.70	2.06	-4.20	21.09	127.05
593	40.56	113.92	2.09	-4.39	20.77	127.30
594	40.66	120.39	2.17	-4.49	19.70	127.64
595	40.70	132.62	2.24	-4.77	18.40	128.08
596	40.75	141.82	2.32	-5.25	17.09	128.59
597	40.85	153.55	2.47	-5.63	16.06	129.13
598	40.91	165.07	2.59	-5.63	15.13	129.61
599	40.96	173.76	2.65	-5.63	14.17	129.97
600	41.04	185.49	2.68	-5.63	13.29	130.19
601	41.09	193.78	2.70	-4.96	12.46	130.39
602	41.18	202.77	2.73	-4.20	11.82	130.54
603	41.23	209.35	2.74	-3.72	11.36	130.66
604	41.29	211.97	2.74	-3.63	11.10	130.71
605	41.38	213.59	2.74	-3.63	11.02	130.73
606	41.42	212.88	2.74	-3.53	11.10	130.74
607	41.52	209.95	2.77	-3.53	11.32	130.76
608	41.57	207.42	2.79	-3.53	11.64	130.80
609	41.62	204.59	2.83	-3.44	11.95	130.86
610	41.71	202.88	2.87	-3.44	12.22	130.92
611	41.76	202.07	2.89	-3.44	12.42	131.01
612	41.84	201.66	2.94	-3.44	12.59	131.09
613	41.91	201.36	2.97	-3.44	12.74	131.20
614	41.95	201.76	3.03	-3.53	12.88	131.32
615	42.01	202.27	3.09	-3.53	13.08	131.54
616	42.10	203.68	3.24	-3.53	13.30	131.80
617	42.15	204.90	3.34	-3.53	13.56	132.12
618	42.24	206.51	3.49	-3.53	13.76	132.35
619	42.28	206.82	3.55	-3.53	13.82	132.43
620	42.39	206.21	3.45	-3.53	13.78	132.37
621	42.43	205.91	3.41	-3.53	13.60	132.21
622	42.50	206.26	3.33	-3.53	13.33	131.99
623	42.58	206.31	3.14	-3.53	12.97	131.71
624	42.65	206.41	3.03	-3.53	13.30	131.34

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	42.70	184.28	2.97	-3.61	13.40	131.14
626	42.73	197.11	2.95	-3.61	13.48	131.01
627	42.77	199.94	2.91	-3.61	12.77	131.00
628	42.82	203.68	2.86	-3.62	12.36	130.97
629	42.87	208.03	2.85	-3.62	11.87	131.00
630	42.91	215.81	2.87	-3.63	11.40	131.10
631	42.97	222.69	2.90	-3.53	11.00	131.25
632	43.02	226.93	2.94	-3.44	10.78	131.43
633	43.06	230.98	3.03	-3.53	10.72	131.66
634	43.11	233.71	3.13	-3.53	10.67	131.89
635	43.17	238.46	3.19	-3.63	10.57	132.05
636	43.21	241.79	3.19	-3.63	10.32	132.13
637	43.29	246.54	3.17	-3.63	10.05	132.16
638	43.34	250.39	3.16	-3.63	9.74	132.17
639	43.39	254.83	3.15	-3.53	9.49	132.17
640	43.45	257.26	3.12	-3.53	9.24	132.11
641	43.51	258.67	3.05	-3.63	8.93	131.89
642	43.59	258.98	2.87	-3.63	8.66	131.64
643	43.64	258.27	2.81	-3.63	8.23	131.24
644	43.70	260.49	2.58	-3.63	7.80	130.79
645	43.78	259.28	2.37	-3.63	7.50	130.39
646	43.88	255.44	2.40	-3.63	7.60	130.26
647	43.94	250.99	2.49	-3.63	8.46	130.43
648	44.04	228.05	2.65	-3.66	9.36	130.60
649	44.07	225.92	2.69	-3.63	10.23	130.73
650	44.12	223.80	2.73	-3.66	10.49	130.79
651	44.16	221.17	2.75	-3.63	10.73	130.81
652	44.21	218.64	2.74	-3.63	11.01	130.81
653	44.26	214.50	2.77	-3.63	11.32	130.81
654	44.31	210.96	2.79	-3.63	11.70	130.81
655	44.35	207.12	2.80	-3.72	12.07	130.81
656	44.40	202.98	2.81	-3.72	12.44	130.79
657	44.45	199.84	2.82	-3.72	12.75	130.78
658	44.50	197.82	2.82	-3.72	12.98	130.76
659	44.54	196.00	2.82	-3.72	13.20	130.75
660	44.60	193.78	2.85	-3.72	13.50	130.78
661	44.64	190.75	2.88	-3.72	13.86	130.82
662	44.69	188.52	2.92	-3.72	14.21	130.87
663	44.74	186.60	2.94	-3.82	14.38	130.92
664	44.79	188.37	2.96	-3.82	14.49	130.94
665	44.83	186.70	2.95	-3.82	14.44	130.96
666	44.88	188.22	2.95	-3.82	14.34	130.97
667	44.93	191.76	2.96	-3.82	14.12	131.02
668	44.98	193.78	2.97	-3.72	13.90	131.07
669	45.03	195.70	2.97	-3.82	13.77	131.11
670	45.08	196.61	2.98	-3.72	13.68	131.13
671	45.16	197.32	2.98	-3.82	13.57	131.13
672	45.19	198.83	2.96	-3.72	13.41	131.06

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	45.27	198.73	2.88	-3.82	13.22	130.92
674	45.32	197.92	2.81	-3.82	13.07	130.71
675	45.37	196.20	2.73	-3.82	12.89	130.37
676	45.45	192.77	2.52	-3.82	12.75	129.96
677	45.51	188.52	2.41	-3.82	12.79	129.49
678	45.56	180.54	2.32	-3.82	13.16	129.13
679	45.61	172.65	2.26	-3.82	14.11	128.81
680	45.69	156.48	2.24	-3.82	15.78	128.59
681	45.75	140.00	2.30	-3.82	18.95	128.52
682	45.81	115.94	2.49	-3.91	22.57	127.65
683	45.89	90.17	1.83	-3.91	27.28	126.48
684	45.94	73.89	1.73	-3.91	32.45	124.69
685	46.04	56.20	1.58	-3.91	38.98	123.71
686	46.08	47.71	1.52	-3.91	47.47	122.68
687	46.15	36.09	1.45	-3.82	56.21	122.08
688	46.17	36.19	1.44	-3.53	60.34	121.69
689	46.18	36.19	1.43	-3.53	60.04	121.61
690	46.23	36.29	1.40	-3.53	59.44	121.53
691	46.27	37.10	1.38	-3.44	58.23	121.42
692	46.32	38.31	1.34	-3.15	56.14	121.33
693	46.41	40.64	1.30	-2.86	51.16	121.34
694	46.47	43.06	1.32	-2.77	48.66	121.54
695	46.52	45.89	1.37	-2.77	47.10	121.93
696	46.56	47.51	1.45	-2.77	46.43	122.56
697	46.65	49.43	1.62	-2.67	46.28	123.25
698	46.71	51.45	1.75	-2.58	46.04	123.95
699	46.76	53.78	1.86	-2.48	44.89	124.54
700	46.85	58.12	1.95	-2.39	42.94	124.99
701	46.90	62.77	1.97	-2.39	40.08	125.34
702	46.99	69.04	1.98	-2.48	37.61	125.55
703	47.04	71.97	1.98	-2.48	36.35	125.63
704	47.10	70.15	1.97	-2.77	36.71	125.56
705	47.16	66.51	1.95	-3.34	38.66	125.31
706	47.23	59.84	1.90	-3.82	41.64	124.83
707	47.30	52.66	1.77	-4.20	46.53	124.02
708	47.38	42.05	1.62	-4.58	55.83	123.02
709	47.43	33.76	1.52	-4.58	63.91	121.70
710	47.52	27.09	1.27	-4.77	70.43	120.03
711	47.59	23.86	0.95	-4.77	72.90	117.35
712	47.66	21.03	0.52	-4.77	72.89	114.76
713	47.77	19.51	0.53	-4.68	73.13	112.86
714	47.82	18.80	0.54	-4.58	76.41	112.94
715	47.91	18.19	0.56	-4.58	78.15	113.07
716	47.93	18.35	0.57	-4.36	81.01	113.17
717	47.97	16.68	0.58	-4.36	81.15	113.36
718	48.02	18.50	0.60	-4.36	81.66	113.65
719	48.07	18.60	0.64	-4.23	80.69	114.13
720	48.12	18.60	0.68	-4.10	82.08	114.75

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	48.19	18.80	0.77	-4.01	83.29	115.28
722	48.23	18.90	0.79	-4.01	83.94	115.75
723	48.31	19.21	0.82	-4.01	83.94	116.02
724	48.35	19.51	0.84	-3.91	83.94	116.26
725	48.40	19.51	0.86	-3.91	84.74	116.39
726	48.45	18.90	0.88	-3.91	86.54	116.45
727	48.50	18.19	0.88	-3.82	89.36	116.43
728	48.55	17.29	0.89	-3.72	90.62	116.47
729	48.59	18.09	0.90	-3.72	91.76	116.60
730	48.67	17.69	0.94	-3.53	91.23	116.72
731	48.73	17.99	0.92	-3.53	91.27	116.67
732	48.78	17.99	0.89	-3.53	89.99	116.42
733	48.83	18.09	0.84	-3.53	88.84	116.04
734	48.91	17.99	0.79	-3.44	87.70	115.60
735	48.98	17.89	0.74	-3.34	86.94	115.19
736	49.03	17.79	0.72	-3.15	86.65	114.95
737	49.12	17.69	0.72	-3.05	85.60	114.48
738	49.17	17.69	0.61	-2.96	83.33	113.76
739	49.27	17.99	0.53	-2.96	80.70	113.14
740	49.31	18.50	0.56	-2.86	79.11	113.26
741	49.38	19.31	0.62	-2.77	78.69	113.92
742	49.45	19.91	0.66	-2.67	78.67	114.51
743	49.51	20.01	0.70	-2.67	81.86	114.78
744	49.54	17.18	0.72	-2.34	81.23	115.10
745	49.59	21.23	0.74	-2.34	79.36	115.30
746	49.64	22.24	0.73	-2.34	75.47	115.37
747	49.73	21.23	0.70	-2.00	76.06	115.20
748	49.83	20.22	0.70	-2.00	78.94	114.89
749	49.92	18.70	0.68	-1.91	82.21	114.64
750	49.98	17.79	0.67	-1.81	85.18	114.35
751	50.07	17.18	0.66	-1.72	86.78	114.13
752	50.16	17.08	0.64	-1.62	87.78	113.97
753	50.24	16.78	0.64	-1.53	88.72	113.83
754	50.32	16.27	0.63	-1.43	89.58	113.75
755	50.41	16.38	0.63	-1.43	90.32	113.77
756	50.50	16.38	0.65	-1.34	90.32	113.80
757	50.56	16.38	0.64	-1.34	90.32	113.63
758	50.66	16.07	0.59	-1.24	90.38	113.36
759	50.74	15.87	0.59	-1.15	90.68	113.17
760	50.84	15.87	0.60	-1.15	92.49	113.65
761	50.93	15.87	0.71	-1.05	95.02	114.60
762	50.98	16.17	0.85	-1.05	96.87	116.37
763	51.08	18.30	1.14	-0.95	92.70	118.68
764	51.17	24.36	1.53	-0.76	84.52	120.98
765	51.24	30.73	1.80	-0.76	77.19	122.97
766	51.34	35.28	2.14	-0.57	74.02	124.16
767	51.41	34.97	2.26	-0.57	71.12	123.46
768	51.51	32.25	1.21	-0.57	70.63	122.43

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	51.58	31.24	1.48	-0.57	69.74	121.04
770	51.68	30.12	1.47	-0.38	72.97	121.32
771	51.79	28.51	1.42	-0.38	77.64	121.01
772	51.82	23.55	1.42	0.00	80.70	120.81
773	51.85	25.57	1.43	0.00	84.43	120.74
774	51.91	24.06	1.47	0.10	84.06	121.14
775	52.00	25.37	1.63	0.19	85.77	121.55
776	52.05	25.17	1.70	0.48	82.19	122.20
777	52.10	30.63	1.77	0.67	73.91	122.79
778	52.19	39.52	1.77	0.67	64.23	123.22
779	52.28	45.29	1.67	0.19	57.68	123.38
780	52.34	47.31	1.65	-0.10	55.15	123.36
781	52.42	46.50	1.68	-0.38	55.52	123.38
782	52.48	44.48	1.70	-0.29	57.37	123.35
783	52.57	42.05	1.69	-0.29	59.26	123.14
784	52.62	40.43	1.61	-0.19	60.78	122.72
785	52.69	38.31	1.49	0.00	61.59	122.10
786	52.77	36.79	1.37	0.10	62.55	121.57
787	52.87	35.58	1.36	0.19	63.92	121.31
788	52.91	34.27	1.39	0.19	65.28	120.93
789	53.01	32.35	1.22	0.19	67.19	120.67
790	53.10	31.03	1.28	0.29	68.16	120.77
791	53.16	33.16	1.47	0.38	69.53	122.45
792	53.25	37.91	2.14	0.48	67.34	124.27
793	53.29	44.98	2.40	0.57	65.53	126.29
794	53.38	49.94	3.03	0.67	63.67	127.54
795	53.42	51.76	3.26	1.15	57.59	128.96
796	53.47	76.22	3.60	1.34	50.04	130.26
797	53.52	95.93	4.09	1.43	43.49	131.46
798	53.58	106.44	4.29	1.24	41.58	132.45
799	53.66	106.44	4.88	-1.34	42.62	133.05
800	53.75	98.56	5.19	-2.86	45.49	133.37
801	53.81	91.08	5.18	-6.30	49.54	133.18
802	53.87	77.43	5.01	-9.74	53.77	132.67
803	53.95	68.54	4.74	-10.69	59.61	131.92
804	54.01	56.20	4.47	-11.74	65.69	131.12
805	54.06	47.81	4.22	-11.84	72.92	129.99
806	54.15	39.02	3.56	-11.84	77.78	129.07
807	54.20	39.02	3.50	-11.84	78.61	128.77
808	54.29	44.27	3.87	-11.84	70.76	129.29
809	54.34	59.94	3.77	-11.84	51.11	129.21
810	54.43	104.52	2.08	-12.22	34.79	128.49
811	54.45	137.17	1.94	-11.93	23.26	127.27
812	54.48	170.33	1.92	-12.60	19.04	127.74
813	54.52	191.25	2.08	-13.36	17.01	128.18
814	54.53	195.50	2.08	-13.08	16.36	128.98
815	54.58	210.36	2.46	-12.79	16.17	129.67
816	54.62	218.44	2.63	-8.30	15.74	130.34

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	54.65	230.47	2.63	-4.01	14.88	130.73
818	54.70	251.70	2.72	-3.63	14.37	131.15
819	54.76	252.00	2.98	-4.09	14.25	131.53
820	54.77	249.83	2.99	-3.42	14.61	131.77
821	54.82	247.96	3.02	-3.42	14.54	131.82
822	54.87	256.85	3.02	-3.42	14.47	131.87
823	54.88	254.53	3.03	-2.96	14.29	131.89
824	54.91	255.64	3.02	-3.09	14.24	131.96
825	54.96	261.81	3.08	-2.96	13.92	132.10
826	54.97	272.93	3.13	-2.77	13.35	132.49
827	55.03	295.47	3.37	-2.39	12.75	133.09
828	55.09	316.39	3.69	-2.96	11.80	133.38
829	55.15	333.88	3.31	-3.25	10.23	132.43
830	55.20	333.38	2.00	-3.05	9.28	131.93
831	55.25	347.93	3.01	-3.05	7.69	130.99
832	55.30	393.32	2.16	-3.05	7.43	132.16
833	55.34	419.40	3.03	-2.96	6.93	132.95
834	55.39	439.92	3.71	-2.77	7.32	134.46
835	55.40	460.94	4.01	-2.86	7.35	135.39
836	55.44	486.11	4.30	-2.67	7.07	135.83
837	55.44	501.48	4.26	-2.67	6.42	136.02
838	55.49	546.16	4.10	-2.64	6.52	136.38
839	55.54	505.72	4.89	-1.24	6.65	137.08
840	55.59	548.48	5.43	-1.05	7.22	137.28
841	55.63	550.81	5.64	-2.46	7.14	137.28
842	55.64	554.04	5.65	-2.46	7.12	137.28
843	55.68	555.66	5.52	-2.67	6.77	137.28
844	55.69	591.24	5.48	-2.60	6.62	137.28
845	55.69	564.35	5.44	-2.60	6.75	137.28
846	55.71	543.02	5.64	-2.53	7.10	137.28
847	55.76	577.59	6.17	-2.53	7.22	137.28
848	55.78	581.33	6.12	-2.39	7.02	137.28
849	55.81	581.74	5.86	-2.19	6.58	137.28
850	55.85	580.73	4.95	-2.67	5.96	137.28
851	55.86	590.13	4.53	-2.96	5.19	136.82
852	55.91	594.27	4.00	-2.96	4.62	136.29
853	55.92	611.66	3.93	-2.58	4.30	135.90
854	55.96	600.94	3.86	-2.48	3.98	135.87
855	55.97	644.61	3.85	-2.96	3.85	136.11
856	56.00	656.84	4.22	-3.15	3.75	136.51
857	56.01	661.80	4.40	-3.25	4.03	137.12
858	56.03	661.85	4.90	-3.25	4.27	137.28
859	56.05	661.85	5.01	-3.05	4.38	137.28
860	56.10	661.90	4.73	-2.86	4.31	137.28
861	56.12	671.50	4.82	-2.77	4.05	137.28
862	56.16	670.79	4.37	-2.67	3.91	137.12
863	56.17	660.89	4.28	-2.77	3.94	136.81
864	56.20	632.79	4.35	-2.77	4.25	136.76

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	56.22	611.76	4.41	-2.77	4.54	136.69
866	56.24	608.02	4.27	-2.67	4.60	136.52
867	56.30	605.70	4.12	-2.77	4.63	136.39
868	56.31	594.48	4.22	-2.67	4.86	136.51
869	56.34	587.00	4.54	-2.67	5.22	136.76
870	56.39	577.29	4.62	-2.67	5.42	136.81
871	56.45	572.94	4.38	-2.77	5.52	136.73
872	56.48	566.78	4.44	-2.58	5.63	136.67
873	56.49	556.57	4.57	-2.48	6.11	137.00
874	56.53	543.12	5.08	-2.39	6.65	137.27
875	56.58	526.85	5.09	-2.29	7.00	137.27
876	56.63	517.25	4.68	-2.39	5.57	135.21
877	56.68	530.19	1.47	-2.67	4.07	132.85
878	56.73	530.69	1.99	-2.19	3.28	131.52
879	56.78	533.22	3.31	-2.10	4.70	133.92
880	56.83	515.12	4.11	-2.10	5.98	135.53
881	56.89	505.72	4.38	-1.81	6.76	136.05
882	56.95	489.35	4.29	-1.72	7.57	136.39
883	56.99	460.13	4.89	-1.77	8.27	136.67
884	57.01	461.35	5.04	-1.81	8.73	136.83
885	57.04	461.35	4.71	-1.77	8.64	136.75
886	57.09	462.56	4.73	-1.77	8.37	136.69
887	57.11	480.76	4.85	-1.72	8.26	136.91
888	57.13	489.04	5.06	-1.72	8.28	137.28
889	57.18	496.12	5.48	-1.72	8.57	137.28
890	57.19	481.26	5.56	-1.72	9.17	137.28
891	57.21	456.09	5.75	-1.53	9.62	137.28
892	57.24	456.14	5.61	-1.53	9.80	137.28
893	57.28	456.19	5.36	-1.53	9.62	137.28
894	57.32	457.91	5.35	-1.53	9.68	137.28
895	57.35	438.71	5.32	-1.62	9.84	137.28
896	57.38	439.61	5.31	-1.43	10.12	137.28
897	57.43	428.50	5.24	-1.43	10.11	137.06
898	57.48	423.44	4.91	-1.62	10.27	136.57
899	57.52	392.11	4.48	-1.53	10.16	135.74
900	57.57	380.28	3.84	-1.53	10.70	135.89
901	57.62	396.35	5.29	-1.53	11.26	136.75
902	57.68	413.43	6.11	-1.53	10.99	137.28
903	57.76	472.77	5.74	-1.43	9.99	137.28
904	57.81	500.57	5.68	-1.72	7.13	136.51
905	57.86	543.23	2.17	-1.72	4.79	134.57
906	57.89	587.00	2.33	-1.72	2.67	131.65
907	57.91	587.40	2.22	-1.72	2.56	131.81
908	57.92	576.28	2.27	-1.72	2.86	132.23
909	57.95	567.79	2.76	-1.72	3.35	132.94
910	57.99	563.14	3.00	-1.72	3.71	133.65
911	58.01	581.13	3.08	-1.72	3.92	134.30
912	58.05	591.95	3.53	-1.72	3.96	134.78

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	58.05	600.54	3.58	-1.05	4.23	135.48
914	58.10	604.18	4.04	-1.43	4.36	135.85
915	58.13	609.64	4.08	-1.53	4.44	136.17
916	58.15	619.75	4.05	-1.53	4.30	136.16
917	58.17	626.22	3.98	-1.53	4.19	136.18
918	58.20	629.45	4.07	-1.53	4.24	136.22
919	58.21	614.69	4.13	-1.72	4.37	136.30
920	58.21	614.14	4.14	-1.72	4.48	136.33
921	58.23	614.14	4.16	-1.72	4.50	136.34
922	58.24	613.58	4.15	-1.81	4.62	136.36
923	58.25	596.70	4.21	-1.81	3.41	134.35
924	58.29	617.42	1.15	-1.72	2.07	131.70
925	58.31	627.93	1.23	-1.72	0.59	127.71
926	58.33	636.43	1.41	-1.72	0.81	129.01
927	58.38	652.70	1.86	-1.62	1.14	130.50
928	58.39	665.03	2.22	-1.70	1.43	131.67
929	58.43	667.96	2.33	-1.62	1.54	132.23
930	58.43	678.68	2.34	-1.70	1.38	132.20
931	58.48	701.62	2.15	-1.62	1.49	132.66
932	58.53	683.83	2.76	-1.62	1.70	133.35
933	58.56	697.78	3.03	-1.81	2.25	134.65
934	58.58	707.59	3.68	-1.91	2.48	135.33
935	58.59	707.99	3.65	-1.73	2.66	135.86
936	58.63	717.19	3.78	-1.54	2.76	135.95
937	58.63	696.42	3.83	-1.37	2.82	136.12
938	58.63	714.06	3.90	-1.37	2.92	135.93
939	58.68	675.65	3.56	-1.03	2.66	135.58
940	58.69	710.92	3.27	-1.03	2.12	134.51
941	58.72	719.11	2.44	-1.03	1.55	133.64
942	58.73	723.56	2.46	-0.91	1.34	133.28
943	58.74	726.19	2.85	-0.48	1.62	134.13
944	58.77	736.20	3.38	-0.85	2.06	135.06
945	58.81	718.51	3.65	-0.85	2.44	135.72
946	58.82	713.35	3.81	-0.85	2.73	136.05
947	58.83	710.01	3.91	-0.86	2.96	136.52
948	58.87	724.07	4.41	-0.86	3.17	137.07
949	58.91	732.96	4.71	-0.86	3.32	137.28
950	58.92	738.02	4.73	-0.76	3.35	137.28
951	58.93	742.66	4.76	-0.67	3.28	137.28
952	58.96	740.95	4.59	-0.57	3.26	137.28
953	59.01	733.57	4.60	-0.57	3.68	137.28
954	59.06	674.43	5.18	-1.24	4.25	137.28
955	59.08	653.91	5.10	-1.24	4.86	137.28
956	59.11	637.54	4.96	-1.24	5.19	137.28
957	59.15	625.41	5.36	-1.24	5.74	137.28
958	59.21	618.74	6.10	-1.43	6.20	137.28
959	59.26	610.75	5.85	-0.95	6.43	137.28
960	59.30	588.81	5.33	-0.67	6.35	137.28

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	59.35	577.39	5.07	-0.67	6.33	137.28
962	59.40	573.45	5.09	-0.67	6.60	137.28
963	59.42	537.46	5.10	-0.62	6.81	137.28
964	59.47	542.01	4.94	-0.62	7.03	137.28
965	59.51	538.58	4.99	-0.62	7.10	137.28
966	59.56	537.67	5.28	-0.48	7.14	137.28
967	59.61	537.67	4.95	-0.48	6.86	137.10
968	59.67	536.76	4.21	-0.48	6.15	136.33
969	59.71	551.52	3.80	-0.29	5.22	135.39
970	59.80	572.94	3.30	-0.29	4.51	134.34
971	59.85	543.02	2.68	-0.10	4.17	133.65
972	59.90	541.41	2.94	0.00	4.17	133.27
973	60.00	542.21	2.91	0.29	4.27	133.47
974	60.04	545.35	2.91	0.19	4.40	133.64
975	60.10	537.57	3.16	0.19	4.95	133.98
976	60.15	496.63	3.43	0.19	5.55	134.23
977	60.19	490.76	3.36	0.19	6.05	134.17
978	60.23	474.79	3.20	0.19	5.92	133.82
979	60.28	484.90	2.99	0.29	5.71	133.46
980	60.33	488.14	2.90	0.29	5.51	133.41
981	60.38	493.90	3.10	0.29	5.65	133.73
982	60.42	493.85	3.38	0.29	5.89	134.17
983	60.44	493.80	3.46	0.29	6.33	134.53
984	60.47	473.88	3.65	0.38	6.98	134.97
985	60.52	460.13	4.12	0.48	7.63	135.40
986	60.56	462.56	4.23	0.38	8.01	135.74
987	60.57	465.39	4.25	0.38	7.98	135.80
988	60.61	467.11	4.21	0.38	7.76	135.74
989	60.66	479.34	4.08	0.38	7.57	135.77
990	60.71	485.41	4.24	0.38	7.40	135.90
991	60.76	495.21	4.35	0.48	7.47	136.31
992	60.81	505.12	4.72	0.67	7.48	136.65
993	60.86	513.91	4.79	0.76	7.09	136.81
994	60.91	550.10	4.48	0.95	6.19	136.86
995	60.95	615.30	4.50	1.05	5.45	137.13
996	61.00	639.05	4.99	1.24	5.05	137.28
997	61.02	658.56	5.11	1.72	5.00	137.28
998	61.05	675.54	5.33	1.72	4.74	137.28
999	61.08	721.13	5.51	1.62	4.50	137.28
1000	61.09	733.97	5.54	1.62	4.27	137.28
1001	61.13	740.34	5.59	1.81	4.24	137.28
1002	61.14	739.43	5.66	1.91	4.28	137.28
1003	61.16	738.52	5.76	1.91	4.32	137.28
1004	61.20	746.30	5.81	1.91	4.05	137.28
1005	61.23	767.73	5.15	1.91	3.75	137.28
1006	61.24	772.28	5.21	1.81	3.14	137.28
1007	61.29	760.66	3.90	1.81	2.97	137.28
1008	61.30	743.57	4.26	1.72	3.09	137.25

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1009	61.33	728.41	5.05	1.81	3.50	137.28
1010	61.38	731.65	4.85	2.00	3.57	137.28
1011	61.43	732.56	4.32	1.81	3.24	137.17
1012	61.48	728.92	3.98	1.81	2.87	136.68
1013	61.53	753.18	3.97	1.62	2.61	136.51
1014	61.56	770.56	3.96	1.72	2.53	136.46
1015	61.58	740.54	3.88	1.72	2.82	136.29
1016	61.59	669.61	3.85	1.46	3.07	136.12
1017	61.62	696.97	3.82	0.67	4.53	135.66
1018	61.63	435.47	3.76	0.86	4.59	135.59
1019	61.67	653.41	3.77	1.34	4.68	135.51
1020	61.71	676.15	3.74	1.43	3.52	135.82
1021	61.76	658.36	3.79	1.34	3.57	135.69
1022	61.81	631.98	3.61	1.34	3.48	134.89
1023	61.86	611.66	2.70	1.53	3.19	133.76
1024	61.87	601.35	2.42	1.62	2.51	131.84
1025	61.91	589.42	1.65	1.72	2.08	130.34
1026	61.95	575.78	1.49	1.72	1.72	128.91
1027	61.96	568.80	1.46	1.62	1.77	128.59
1028	62.00	555.56	1.48	1.53	2.11	128.99
1029	62.04	536.66	1.77	1.43	2.73	129.80
1030	62.06	513.20	2.07	1.34	3.63	130.78
1031	62.10	482.98	2.34	1.34	4.36	131.39
1032	62.14	478.73	2.39	1.34	4.98	131.79
1033	62.20	464.78	2.54	1.34	5.42	131.98
1034	62.22	445.68	2.60	1.62	6.21	132.17
1035	62.27	407.07	2.72	1.43	7.02	132.25
1036	62.29	393.62	2.77	1.34	7.80	132.39
1037	62.34	388.36	2.89	1.43	8.52	132.51
1038	62.39	358.75	2.98	1.24	9.48	132.97
1039	62.43	352.68	3.46	1.43	11.11	133.79
1040	62.49	331.86	4.17	1.43	12.15	134.44
1041	62.57	335.80	4.05	1.43	12.81	134.86
1042	62.68	341.56	4.21	1.43	12.34	135.49
1043	62.75	394.13	5.02	1.53	11.19	136.33
1044	62.87	459.02	5.12	1.62	10.57	136.91
1045	62.88	425.46	5.04	1.53	11.01	136.62
1046	62.89	343.08	4.64	0.86	9.46	135.64
1047	62.93	504.41	3.12	1.53	6.80	134.88
1048	62.98	608.73	3.27	1.24	4.56	134.66
1049	63.02	602.56	3.75	1.53	2.42	132.17
1050	63.07	649.36	0.00	1.53	0.48	127.73
1051	63.12	723.66	0.00	1.62	N/A	87.36
1052	63.14	759.24	0.00	1.62	N/A	87.36
1053	63.17	774.10	0.00	1.72	N/A	87.36
1054	63.17	810.49	0.00	1.53	N/A	87.36
1055	63.20	813.42	0.00	1.53	N/A	87.36
1056	63.21	853.96	0.00	1.53	N/A	87.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1057	63.23	825.05	0.00	1.43	N/A	87.36
1058	63.26	849.66	0.00	0.99	N/A	87.36
1059	63.28	829.50	0.00	0.99	N/A	87.36
1060	63.31	845.37	0.00	0.29	N/A	87.36
1061	63.32	839.40	0.00	0.48	N/A	87.36
1062	63.36	833.34	0.00	0.57	N/A	87.36
1063	63.40	838.59	0.00	0.67	N/A	87.36

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c:	Measured cone resistance (tsf)
f_s:	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.01	0.00	0.00	0.00	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
2	0.04	0.00	0.00	0.00	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
3	0.09	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
4	0.11	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
5	0.14	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
6	0.14	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
7	0.18	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
8	0.23	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
9	0.24	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
10	0.28	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
11	0.33	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
12	0.38	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
13	0.42	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
14	0.47	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
15	0.51	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
16	0.52	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
17	0.57	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
18	0.61	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
19	0.67	0.04	0.00	0.04	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
20	0.73	0.04	0.00	0.04	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
21	0.81	0.04	0.00	0.04	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
22	0.86	0.05	0.00	0.05	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
23	0.98	0.05	0.00	0.05	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
24	1.05	0.06	0.00	0.06	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
25	1.15	0.06	0.00	0.06	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
26	1.24	0.07	0.00	0.07	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
27	1.34	0.07	0.00	0.07	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
28	1.43	0.08	0.00	0.08	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
29	1.53	0.09	0.00	0.09	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
30	1.58	0.09	0.00	0.09	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
31	1.62	0.09	0.00	0.09	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
32	1.67	0.09	0.00	0.09	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
33	1.75	0.10	0.00	0.10	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
34	1.77	0.10	0.00	0.10	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
35	1.81	0.10	0.00	0.10	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
36	1.86	0.10	0.00	0.10	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
37	1.91	0.11	0.00	0.11	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
38	1.95	0.11	0.00	0.11	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
39	2.00	0.11	0.00	0.11	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
40	2.05	0.11	0.00	0.11	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
41	2.11	0.12	0.00	0.12	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
42	2.20	0.12	0.00	0.12	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
43	2.24	0.12	0.00	0.12	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
44	2.29	0.13	0.00	0.13	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
45	2.34	0.13	0.00	0.13	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
46	2.44	0.13	0.00	0.13	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
47	2.48	0.13	0.00	0.13	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
48	2.58	0.14	0.00	0.14	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	2.63	0.14	0.00	0.14	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
50	2.71	0.15	0.00	0.15	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
51	2.78	0.15	0.00	0.15	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
52	2.82	0.15	0.00	0.15	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
53	2.89	0.16	0.00	0.16	1.00	0.272	1.68	0.161	1.00	1.10	2.000	Yes
54	2.96	0.16	0.00	0.16	1.00	0.272	1.68	0.161	1.00	1.10	2.000	No
55	3.03	0.17	0.00	0.17	0.99	0.272	1.68	0.161	1.00	1.10	2.000	No
56	3.11	0.17	0.00	0.17	0.99	0.272	1.68	0.161	1.00	1.10	2.000	No
57	3.19	0.17	0.00	0.17	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
58	3.25	0.18	0.00	0.18	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
59	3.35	0.18	0.00	0.18	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
60	3.41	0.19	0.00	0.19	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
61	3.50	0.19	0.00	0.19	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
62	3.59	0.20	0.00	0.20	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
63	3.69	0.20	0.00	0.20	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
64	3.79	0.21	0.00	0.21	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
65	3.88	0.21	0.00	0.21	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
66	3.97	0.22	0.00	0.22	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
67	4.07	0.22	0.00	0.22	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
68	4.14	0.22	0.00	0.22	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
69	4.17	0.23	0.00	0.23	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
70	4.26	0.23	0.00	0.23	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
71	4.32	0.23	0.00	0.23	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
72	4.37	0.24	0.00	0.24	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
73	4.42	0.24	0.00	0.24	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
74	4.51	0.24	0.00	0.24	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
75	4.61	0.25	0.00	0.25	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
76	4.65	0.25	0.00	0.25	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
77	4.74	0.26	0.00	0.26	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
78	4.80	0.26	0.00	0.26	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
79	4.89	0.26	0.00	0.26	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
80	4.95	0.27	0.00	0.27	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
81	5.04	0.27	0.00	0.27	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
82	5.13	0.28	0.00	0.28	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
83	5.18	0.28	0.00	0.28	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
84	5.28	0.29	0.00	0.29	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
85	5.32	0.29	0.00	0.29	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
86	5.42	0.29	0.00	0.29	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
87	5.51	0.30	0.00	0.30	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
88	5.60	0.30	0.00	0.30	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
89	5.66	0.31	0.00	0.31	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
90	5.76	0.31	0.00	0.31	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
91	5.85	0.32	0.00	0.32	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
92	5.92	0.32	0.00	0.32	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
93	5.95	0.32	0.00	0.32	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
94	5.97	0.32	0.00	0.32	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
95	6.02	0.33	0.00	0.33	0.99	0.270	1.68	0.160	1.00	1.10	2.000	Yes
96	6.06	0.33	0.00	0.33	0.99	0.270	1.68	0.160	1.00	1.10	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	6.16	0.33	0.00	0.33	0.99	0.270	1.68	0.160	1.00	1.10	2.000	Yes
98	6.21	0.34	0.00	0.34	0.99	0.270	1.68	0.160	1.00	1.10	2.000	Yes
99	6.26	0.34	0.00	0.34	0.99	0.270	1.68	0.160	1.00	1.10	2.000	Yes
100	6.31	0.34	0.00	0.34	0.99	0.270	1.68	0.160	1.00	1.10	2.000	Yes
101	6.40	0.35	0.00	0.35	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
102	6.44	0.35	0.00	0.35	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
103	6.52	0.35	0.00	0.35	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
104	6.57	0.36	0.00	0.36	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
105	6.64	0.36	0.00	0.36	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
106	6.69	0.36	0.00	0.36	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
107	6.78	0.37	0.00	0.37	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
108	6.83	0.37	0.00	0.37	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
109	6.92	0.37	0.00	0.37	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
110	6.97	0.38	0.00	0.38	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
111	7.03	0.38	0.00	0.38	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
112	7.12	0.38	0.00	0.38	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
113	7.22	0.39	0.00	0.39	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
114	7.27	0.39	0.00	0.39	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
115	7.36	0.40	0.00	0.40	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
116	7.43	0.40	0.00	0.40	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
117	7.50	0.41	0.00	0.41	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
118	7.59	0.41	0.00	0.41	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
119	7.64	0.41	0.00	0.41	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
120	7.75	0.42	0.00	0.42	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
121	7.79	0.42	0.00	0.42	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
122	7.89	0.43	0.00	0.43	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
123	7.99	0.43	0.00	0.43	0.98	0.268	1.68	0.160	1.00	1.10	2.000	No
124	8.04	0.43	0.00	0.43	0.98	0.268	1.68	0.160	1.00	1.10	2.000	No
125	8.13	0.44	0.00	0.44	0.98	0.268	1.68	0.160	1.00	1.10	2.000	No
126	8.23	0.44	0.00	0.44	0.98	0.268	1.68	0.160	1.00	1.10	2.000	No
127	8.32	0.45	0.00	0.45	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
128	8.37	0.45	0.00	0.45	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
129	8.46	0.46	0.00	0.46	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
130	8.56	0.46	0.00	0.46	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
131	8.59	0.46	0.00	0.46	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
132	8.61	0.47	0.00	0.47	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
133	8.67	0.47	0.00	0.47	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
134	8.71	0.47	0.00	0.47	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
135	8.72	0.47	0.00	0.47	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
136	8.78	0.47	0.00	0.47	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
137	8.80	0.48	0.00	0.48	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
138	8.86	0.48	0.00	0.48	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
139	8.90	0.48	0.00	0.48	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
140	8.95	0.48	0.00	0.48	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
141	8.96	0.48	0.00	0.48	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
142	9.00	0.49	0.00	0.49	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
143	9.05	0.49	0.00	0.49	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
144	9.09	0.49	0.00	0.49	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	9.10	0.49	0.00	0.49	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
146	9.14	0.49	0.00	0.49	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
147	9.20	0.50	0.00	0.50	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
148	9.24	0.50	0.00	0.50	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
149	9.29	0.50	0.00	0.50	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
150	9.31	0.50	0.00	0.50	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
151	9.38	0.51	0.00	0.51	0.98	0.268	1.68	0.159	1.00	1.10	2.000	Yes
152	9.41	0.51	0.00	0.51	0.98	0.268	1.68	0.159	1.00	1.10	2.000	Yes
153	9.47	0.51	0.00	0.51	0.98	0.268	1.68	0.159	1.00	1.10	2.000	Yes
154	9.53	0.52	0.00	0.52	0.98	0.268	1.68	0.159	1.00	1.10	2.000	Yes
155	9.62	0.52	0.00	0.52	0.98	0.268	1.68	0.159	1.00	1.10	2.000	Yes
156	9.67	0.52	0.00	0.52	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
157	9.77	0.53	0.00	0.53	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
158	9.81	0.53	0.00	0.53	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
159	9.90	0.54	0.00	0.54	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
160	9.97	0.54	0.00	0.54	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
161	10.06	0.55	0.00	0.55	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
162	10.20	0.55	0.00	0.55	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
163	10.30	0.56	0.00	0.56	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
164	10.44	0.57	0.00	0.57	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
165	10.54	0.57	0.00	0.57	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
166	10.63	0.58	0.00	0.58	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
167	10.74	0.58	0.00	0.58	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
168	10.78	0.59	0.00	0.59	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
169	10.83	0.59	0.00	0.59	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
170	10.88	0.59	0.00	0.59	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
171	10.89	0.59	0.00	0.59	0.98	0.267	1.68	0.159	1.00	1.10	2.000	Yes
172	10.97	0.60	0.00	0.60	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
173	11.02	0.60	0.00	0.60	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
174	11.07	0.60	0.00	0.60	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
175	11.11	0.60	0.00	0.60	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
176	11.16	0.61	0.00	0.61	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
177	11.21	0.61	0.00	0.61	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
178	11.26	0.61	0.00	0.61	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
179	11.30	0.62	0.00	0.62	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
180	11.36	0.62	0.00	0.62	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
181	11.40	0.62	0.00	0.62	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
182	11.45	0.62	0.00	0.62	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
183	11.50	0.63	0.00	0.63	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
184	11.55	0.63	0.00	0.63	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
185	11.60	0.63	0.00	0.63	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
186	11.66	0.64	0.00	0.64	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
187	11.74	0.64	0.00	0.64	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
188	11.84	0.65	0.00	0.65	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
189	11.93	0.65	0.00	0.65	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
190	12.04	0.66	0.00	0.66	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
191	12.13	0.66	0.00	0.66	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
192	12.22	0.67	0.00	0.67	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	12.27	0.67	0.00	0.67	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
194	12.37	0.68	0.00	0.68	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
195	12.41	0.68	0.00	0.68	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
196	12.51	0.69	0.00	0.69	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
197	12.56	0.69	0.00	0.69	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
198	12.65	0.69	0.00	0.69	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
199	12.71	0.70	0.00	0.70	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
200	12.79	0.70	0.00	0.70	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
201	12.89	0.71	0.00	0.71	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
202	12.96	0.71	0.00	0.71	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
203	13.04	0.72	0.00	0.72	0.97	0.266	1.68	0.158	1.00	1.10	2.000	Yes
204	13.13	0.72	0.00	0.72	0.97	0.266	1.68	0.158	1.00	1.10	2.000	Yes
205	13.23	0.73	0.00	0.73	0.97	0.265	1.68	0.158	1.00	1.10	2.000	Yes
206	13.30	0.73	0.00	0.73	0.97	0.265	1.68	0.158	1.00	1.10	2.000	Yes
207	13.37	0.74	0.00	0.74	0.97	0.265	1.68	0.158	1.00	1.10	2.000	Yes
208	13.47	0.74	0.00	0.74	0.97	0.265	1.68	0.158	1.00	1.10	2.000	Yes
209	13.57	0.75	0.00	0.75	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
210	13.61	0.75	0.00	0.75	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
211	13.62	0.75	0.00	0.75	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
212	13.68	0.75	0.00	0.75	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
213	13.73	0.76	0.00	0.76	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
214	13.77	0.76	0.00	0.76	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
215	13.87	0.77	0.00	0.77	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
216	13.93	0.77	0.00	0.77	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
217	14.00	0.77	0.00	0.77	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
218	14.06	0.78	0.00	0.78	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
219	14.12	0.78	0.00	0.78	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
220	14.21	0.79	0.00	0.79	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
221	14.25	0.79	0.00	0.79	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
222	14.35	0.79	0.00	0.79	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
223	14.45	0.80	0.00	0.80	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
224	14.50	0.80	0.00	0.80	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
225	14.59	0.81	0.00	0.81	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
226	14.64	0.81	0.00	0.81	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
227	14.74	0.82	0.00	0.82	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
228	14.80	0.82	0.00	0.82	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
229	14.88	0.83	0.00	0.83	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
230	14.97	0.83	0.00	0.83	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
231	15.05	0.84	0.00	0.84	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
232	15.13	0.84	0.00	0.84	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
233	15.21	0.85	0.00	0.85	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
234	15.28	0.85	0.00	0.85	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
235	15.36	0.86	0.00	0.86	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
236	15.41	0.86	0.00	0.86	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
237	15.50	0.86	0.00	0.86	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
238	15.55	0.87	0.00	0.87	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
239	15.65	0.87	0.00	0.87	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
240	15.71	0.88	0.00	0.88	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	15.79	0.88	0.00	0.88	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
242	15.89	0.89	0.00	0.89	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
243	15.90	0.89	0.00	0.89	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
244	15.94	0.89	0.00	0.89	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
245	16.00	0.89	0.00	0.89	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
246	16.06	0.90	0.00	0.90	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
247	16.14	0.90	0.00	0.90	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
248	16.19	0.90	0.00	0.90	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
249	16.26	0.91	0.00	0.91	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
250	16.33	0.91	0.00	0.91	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
251	16.38	0.91	0.00	0.91	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
252	16.47	0.92	0.00	0.92	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
253	16.54	0.92	0.00	0.92	0.97	0.263	1.68	0.157	1.00	1.10	2.000	Yes
254	16.62	0.93	0.00	0.93	0.97	0.263	1.68	0.157	1.00	1.10	2.000	No
255	16.70	0.93	0.00	0.93	0.96	0.263	1.68	0.157	1.00	1.10	2.000	No
256	16.76	0.94	0.00	0.94	0.96	0.263	1.68	0.157	1.00	1.10	2.000	No
257	16.86	0.94	0.00	0.94	0.96	0.263	1.68	0.157	1.00	1.10	2.000	Yes
258	16.90	0.94	0.00	0.94	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
259	16.98	0.95	0.00	0.95	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
260	17.05	0.95	0.00	0.95	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
261	17.14	0.96	0.00	0.96	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
262	17.20	0.96	0.00	0.96	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
263	17.29	0.97	0.00	0.97	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
264	17.34	0.97	0.00	0.97	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
265	17.44	0.98	0.00	0.98	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
266	17.50	0.98	0.00	0.98	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
267	17.58	0.98	0.00	0.98	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
268	17.64	0.99	0.00	0.99	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
269	17.75	0.99	0.00	0.99	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
270	17.82	1.00	0.00	1.00	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
271	17.89	1.00	0.00	1.00	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
272	17.89	1.00	0.00	1.00	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
273	17.96	1.01	0.00	1.01	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
274	18.02	1.01	0.00	1.01	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
275	18.07	1.01	0.00	1.01	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
276	18.17	1.02	0.00	1.02	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
277	18.22	1.02	0.00	1.02	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
278	18.30	1.03	0.00	1.03	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
279	18.36	1.03	0.00	1.03	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
280	18.42	1.03	0.00	1.03	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
281	18.50	1.04	0.00	1.04	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
282	18.56	1.04	0.00	1.04	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
283	18.62	1.05	0.00	1.05	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
284	18.69	1.05	0.00	1.05	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
285	18.76	1.05	0.00	1.05	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
286	18.84	1.06	0.00	1.06	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
287	18.89	1.06	0.00	1.06	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
288	18.98	1.07	0.00	1.07	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	19.05	1.07	0.00	1.07	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
290	19.12	1.08	0.00	1.08	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
291	19.18	1.08	0.00	1.08	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
292	19.24	1.08	0.00	1.08	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
293	19.32	1.09	0.00	1.09	0.96	0.262	1.68	0.156	0.99	1.10	2.000	No
294	19.38	1.09	0.00	1.09	0.96	0.262	1.68	0.156	0.99	1.10	2.000	No
295	19.46	1.10	0.00	1.10	0.96	0.262	1.68	0.156	0.99	1.10	2.000	No
296	19.54	1.10	0.00	1.10	0.96	0.262	1.68	0.155	0.99	1.10	2.000	No
297	19.62	1.11	0.00	1.11	0.96	0.262	1.68	0.155	0.99	1.10	2.000	No
298	19.70	1.11	0.00	1.11	0.96	0.261	1.68	0.155	0.99	1.10	2.000	No
299	19.80	1.12	0.00	1.12	0.96	0.261	1.68	0.155	0.99	1.10	2.000	No
300	19.85	1.12	0.00	1.12	0.96	0.261	1.68	0.155	0.99	1.10	2.000	No
301	19.94	1.13	0.00	1.13	0.96	0.261	1.68	0.155	0.99	1.10	2.000	No
302	20.03	1.13	0.00	1.13	0.96	0.261	1.68	0.155	0.99	1.10	2.000	No
303	20.13	1.14	0.00	1.14	0.96	0.261	1.68	0.155	0.99	1.10	2.000	No
304	20.19	1.14	0.00	1.14	0.96	0.261	1.68	0.155	0.98	1.10	2.000	No
305	20.29	1.15	0.00	1.15	0.96	0.261	1.68	0.155	0.98	1.10	2.000	No
306	20.39	1.16	0.00	1.16	0.96	0.261	1.68	0.155	0.98	1.10	2.000	No
307	20.43	1.16	0.00	1.16	0.96	0.261	1.68	0.155	0.98	1.10	2.000	No
308	20.47	1.16	0.00	1.16	0.96	0.261	1.68	0.155	0.98	1.10	2.000	No
309	20.52	1.16	0.00	1.16	0.96	0.261	1.68	0.155	0.98	1.10	2.000	No
310	20.61	1.17	0.00	1.17	0.96	0.261	1.68	0.155	0.98	1.10	2.000	No
311	20.66	1.17	0.00	1.17	0.96	0.261	1.68	0.155	0.98	1.10	2.000	No
312	20.71	1.18	0.00	1.18	0.96	0.261	1.68	0.155	0.98	1.10	2.000	No
313	20.77	1.18	0.00	1.18	0.95	0.261	1.68	0.155	0.98	1.10	2.000	No
314	20.85	1.18	0.00	1.18	0.95	0.261	1.68	0.155	0.98	1.10	2.000	No
315	20.91	1.19	0.00	1.19	0.95	0.261	1.68	0.155	0.98	1.10	2.000	No
316	21.00	1.19	0.00	1.19	0.95	0.261	1.68	0.155	0.98	1.10	2.000	No
317	21.05	1.20	0.00	1.20	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
318	21.11	1.20	0.00	1.20	0.95	0.260	1.68	0.155	0.97	1.10	2.000	No
319	21.19	1.21	0.00	1.21	0.95	0.260	1.68	0.155	0.97	1.10	2.000	No
320	21.24	1.21	0.00	1.21	0.95	0.260	1.68	0.155	0.97	1.10	2.000	No
321	21.34	1.22	0.00	1.22	0.95	0.260	1.68	0.155	0.97	1.10	2.000	No
322	21.39	1.22	0.00	1.22	0.95	0.260	1.68	0.155	0.97	1.10	2.000	No
323	21.48	1.22	0.00	1.22	0.95	0.260	1.68	0.155	0.97	1.10	2.000	No
324	21.53	1.23	0.00	1.23	0.95	0.260	1.68	0.155	0.97	1.10	2.000	No
325	21.64	1.23	0.00	1.23	0.95	0.260	1.68	0.155	0.97	1.10	2.000	No
326	21.72	1.24	0.00	1.24	0.95	0.260	1.68	0.155	0.97	1.10	2.000	No
327	21.81	1.24	0.00	1.24	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
328	21.89	1.25	0.00	1.25	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
329	21.97	1.25	0.00	1.25	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
330	22.05	1.26	0.00	1.26	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
331	22.12	1.26	0.00	1.26	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
332	22.13	1.26	0.00	1.26	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
333	22.18	1.27	0.00	1.27	0.95	0.260	1.68	0.154	0.96	1.10	2.000	No
334	22.22	1.27	0.00	1.27	0.95	0.260	1.68	0.154	0.96	1.10	2.000	No
335	22.28	1.27	0.00	1.27	0.95	0.260	1.68	0.154	0.96	1.10	2.000	No
336	22.33	1.28	0.00	1.28	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	22.38	1.28	0.00	1.28	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
338	22.41	1.28	0.00	1.28	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
339	22.51	1.29	0.00	1.29	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
340	22.56	1.29	0.00	1.29	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
341	22.61	1.29	0.00	1.29	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
342	22.65	1.30	0.00	1.30	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
343	22.71	1.30	0.00	1.30	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
344	22.76	1.30	0.00	1.30	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
345	22.85	1.31	0.00	1.31	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
346	22.89	1.31	0.00	1.31	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
347	22.99	1.32	0.00	1.32	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
348	23.04	1.32	0.00	1.32	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
349	23.12	1.33	0.00	1.33	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
350	23.18	1.33	0.00	1.33	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
351	23.24	1.33	0.00	1.33	0.95	0.259	1.68	0.154	0.95	1.10	2.000	No
352	23.33	1.34	0.00	1.34	0.95	0.259	1.68	0.154	0.95	1.10	2.000	No
353	23.38	1.34	0.00	1.34	0.95	0.259	1.68	0.154	0.95	1.10	2.000	No
354	23.47	1.35	0.00	1.35	0.95	0.259	1.68	0.154	0.95	1.10	2.000	No
355	23.52	1.35	0.00	1.35	0.95	0.258	1.68	0.154	0.95	1.10	2.000	No
356	23.61	1.36	0.00	1.36	0.95	0.258	1.68	0.154	0.95	1.10	2.000	No
357	23.68	1.36	0.00	1.36	0.95	0.258	1.68	0.154	0.95	1.10	2.000	No
358	23.76	1.36	0.00	1.36	0.95	0.258	1.68	0.154	0.95	1.10	2.000	No
359	23.83	1.37	0.00	1.37	0.95	0.258	1.68	0.153	0.95	1.10	2.000	No
360	23.90	1.37	0.00	1.37	0.95	0.258	1.68	0.153	0.95	1.10	2.000	No
361	23.97	1.38	0.00	1.38	0.95	0.258	1.68	0.153	0.95	1.10	2.000	No
362	24.05	1.38	0.00	1.38	0.95	0.258	1.68	0.153	0.95	1.10	2.000	No
363	24.10	1.39	0.00	1.39	0.94	0.258	1.68	0.153	0.95	1.10	2.000	No
364	24.19	1.39	0.00	1.39	0.94	0.258	1.68	0.153	0.95	1.10	2.000	No
365	24.27	1.40	0.00	1.40	0.94	0.258	1.68	0.153	0.95	1.10	2.000	No
366	24.34	1.40	0.00	1.40	0.94	0.258	1.68	0.153	0.95	1.10	2.000	No
367	24.43	1.41	0.00	1.41	0.94	0.258	1.68	0.153	0.94	1.10	2.000	No
368	24.48	1.41	0.00	1.41	0.94	0.258	1.68	0.153	0.94	1.10	2.000	No
369	24.57	1.41	0.00	1.41	0.94	0.258	1.68	0.153	0.94	1.10	2.000	No
370	24.62	1.42	0.00	1.42	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
371	24.72	1.42	0.00	1.42	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
372	24.81	1.43	0.00	1.43	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
373	24.86	1.43	0.00	1.43	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
374	24.95	1.44	0.00	1.44	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
375	25.01	1.44	0.00	1.44	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
376	25.02	1.44	0.00	1.44	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
377	25.05	1.44	0.00	1.44	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
378	25.11	1.45	0.00	1.45	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
379	25.15	1.45	0.00	1.45	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
380	25.21	1.45	0.00	1.45	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
381	25.25	1.46	0.00	1.46	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
382	25.30	1.46	0.00	1.46	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
383	25.40	1.47	0.00	1.47	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
384	25.45	1.47	0.00	1.47	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	25.52	1.47	0.00	1.47	0.94	0.257	1.68	0.153	0.94	1.10	2.000	Yes
386	25.60	1.48	0.00	1.48	0.94	0.257	1.68	0.152	0.94	1.10	2.000	Yes
387	25.66	1.48	0.00	1.48	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
388	25.74	1.49	0.00	1.49	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
389	25.80	1.49	0.00	1.49	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
390	25.88	1.49	0.00	1.49	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
391	25.94	1.50	0.00	1.50	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
392	26.02	1.50	0.00	1.50	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
393	26.09	1.51	0.00	1.51	0.94	0.256	1.68	0.152	0.93	1.10	2.000	No
394	26.17	1.51	0.00	1.51	0.94	0.256	1.68	0.152	0.93	1.10	2.000	No
395	26.23	1.52	0.00	1.52	0.94	0.256	1.68	0.152	0.93	1.10	2.000	No
396	26.29	1.52	0.00	1.52	0.94	0.256	1.68	0.152	0.93	1.10	2.000	No
397	26.37	1.52	0.00	1.52	0.94	0.256	1.68	0.152	0.93	1.10	2.000	No
398	26.46	1.53	0.00	1.53	0.94	0.256	1.68	0.152	0.93	1.10	2.000	No
399	26.55	1.53	0.00	1.53	0.94	0.256	1.68	0.152	0.93	1.10	2.000	No
400	26.60	1.54	0.00	1.54	0.94	0.255	1.68	0.152	0.93	1.10	2.000	No
401	26.70	1.54	0.00	1.54	0.94	0.255	1.68	0.152	0.93	1.10	2.000	No
402	26.78	1.55	0.00	1.55	0.94	0.255	1.68	0.152	0.93	1.10	2.000	No
403	26.87	1.55	0.00	1.55	0.93	0.255	1.68	0.152	0.93	1.10	2.000	No
404	26.94	1.56	0.00	1.56	0.93	0.255	1.68	0.152	0.93	1.10	2.000	No
405	27.03	1.56	0.00	1.56	0.93	0.255	1.68	0.152	0.93	1.10	2.000	No
406	27.13	1.57	0.00	1.57	0.93	0.255	1.68	0.152	0.92	1.10	2.000	No
407	27.18	1.57	0.00	1.57	0.93	0.255	1.68	0.151	0.92	1.10	2.000	No
408	27.27	1.58	0.00	1.58	0.93	0.255	1.68	0.151	0.92	1.10	2.000	No
409	27.32	1.58	0.00	1.58	0.93	0.255	1.68	0.151	0.92	1.10	2.000	No
410	27.37	1.58	0.00	1.58	0.93	0.255	1.68	0.151	0.92	1.10	2.000	No
411	27.41	1.58	0.00	1.58	0.93	0.255	1.68	0.151	0.92	1.10	2.000	No
412	27.46	1.59	0.00	1.59	0.93	0.255	1.68	0.151	0.92	1.10	2.000	No
413	27.51	1.59	0.00	1.59	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
414	27.61	1.59	0.00	1.59	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
415	27.66	1.60	0.00	1.60	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
416	27.73	1.60	0.00	1.60	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
417	27.80	1.61	0.00	1.61	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
418	27.88	1.61	0.00	1.61	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
419	27.96	1.62	0.00	1.62	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
420	28.04	1.62	0.00	1.62	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
421	28.12	1.63	0.00	1.63	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
422	28.18	1.63	0.00	1.63	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
423	28.27	1.64	0.00	1.64	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
424	28.32	1.64	0.00	1.64	0.93	0.253	1.68	0.151	0.92	1.10	2.000	No
425	28.42	1.64	0.00	1.64	0.93	0.253	1.68	0.151	0.92	1.10	2.000	No
426	28.47	1.65	0.00	1.65	0.93	0.253	1.68	0.151	0.92	1.10	2.000	No
427	28.61	1.66	0.00	1.66	0.93	0.253	1.68	0.150	0.91	1.10	2.000	No
428	28.67	1.66	0.00	1.66	0.93	0.253	1.68	0.150	0.91	1.10	2.000	Yes
429	28.75	1.67	0.00	1.67	0.93	0.253	1.68	0.150	0.91	1.10	2.000	Yes
430	28.81	1.67	0.00	1.67	0.93	0.253	1.68	0.150	0.91	1.10	2.000	Yes
431	28.90	1.68	0.00	1.68	0.93	0.253	1.68	0.150	0.91	1.10	2.000	Yes
432	29.00	1.68	0.00	1.68	0.93	0.253	1.68	0.150	0.91	1.10	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	29.05	1.68	0.00	1.68	0.93	0.253	1.68	0.150	0.91	1.10	2.000	Yes
434	29.10	1.69	0.00	1.69	0.93	0.253	1.68	0.150	0.91	1.10	2.000	Yes
435	29.15	1.69	0.00	1.69	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
436	29.24	1.70	0.00	1.70	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
437	29.29	1.70	0.00	1.70	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
438	29.37	1.71	0.00	1.71	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
439	29.43	1.71	0.00	1.71	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
440	29.53	1.72	0.00	1.72	0.92	0.252	1.68	0.150	0.91	1.10	2.000	No
441	29.62	1.72	0.00	1.72	0.92	0.252	1.68	0.150	0.91	1.10	2.000	No
442	29.68	1.72	0.00	1.72	0.92	0.252	1.68	0.150	0.91	1.10	2.000	No
443	29.80	1.73	0.00	1.73	0.92	0.252	1.68	0.150	0.91	1.10	2.000	No
444	29.91	1.74	0.00	1.74	0.92	0.251	1.68	0.149	0.91	1.10	2.000	No
445	30.00	1.74	0.00	1.74	0.92	0.251	1.68	0.149	0.90	1.10	0.182	No
446	30.07	1.75	0.00	1.75	0.92	0.252	1.68	0.150	0.90	1.10	0.182	No
447	30.15	1.75	0.00	1.75	0.92	0.252	1.68	0.150	0.90	1.10	0.182	No
448	30.21	1.76	0.01	1.75	0.92	0.252	1.68	0.150	0.90	1.10	0.182	No
449	30.26	1.76	0.01	1.75	0.92	0.252	1.68	0.150	0.90	1.10	0.182	No
450	30.31	1.76	0.01	1.75	0.92	0.252	1.68	0.150	0.90	1.10	0.182	No
451	30.38	1.77	0.01	1.76	0.92	0.252	1.68	0.150	0.90	1.10	0.183	No
452	30.45	1.77	0.01	1.76	0.92	0.253	1.68	0.150	0.90	1.10	0.183	No
453	30.50	1.78	0.02	1.76	0.92	0.253	1.68	0.150	0.90	1.10	0.183	No
454	30.55	1.78	0.02	1.76	0.92	0.253	1.68	0.150	0.90	1.10	0.183	No
455	30.64	1.78	0.02	1.76	0.92	0.253	1.68	0.151	0.90	1.10	0.183	No
456	30.70	1.79	0.02	1.77	0.92	0.253	1.68	0.151	0.90	1.10	0.184	No
457	30.79	1.79	0.02	1.77	0.92	0.254	1.68	0.151	0.90	1.10	0.184	No
458	30.84	1.80	0.03	1.77	0.92	0.254	1.68	0.151	0.90	1.10	0.184	No
459	30.93	1.80	0.03	1.77	0.92	0.254	1.68	0.151	0.90	1.10	0.184	No
460	30.98	1.81	0.03	1.78	0.92	0.254	1.68	0.151	0.90	1.10	0.184	No
461	31.05	1.81	0.03	1.78	0.92	0.254	1.68	0.151	0.90	1.10	0.185	No
462	31.13	1.81	0.04	1.78	0.91	0.255	1.68	0.151	0.90	1.10	0.185	No
463	31.17	1.82	0.04	1.78	0.91	0.255	1.68	0.151	0.90	1.10	0.185	No
464	31.27	1.82	0.04	1.78	0.91	0.255	1.68	0.152	0.90	1.10	0.185	No
465	31.32	1.83	0.04	1.79	0.91	0.255	1.68	0.152	0.90	1.10	0.185	No
466	31.41	1.83	0.04	1.79	0.91	0.255	1.68	0.152	0.90	1.10	0.185	No
467	31.46	1.84	0.05	1.79	0.91	0.256	1.68	0.152	0.90	1.10	0.186	No
468	31.52	1.84	0.05	1.79	0.91	0.256	1.68	0.152	0.90	1.10	0.186	No
469	31.61	1.84	0.05	1.79	0.91	0.256	1.68	0.152	0.90	1.10	0.186	No
470	31.66	1.85	0.05	1.80	0.91	0.256	1.68	0.152	0.90	1.10	0.186	No
471	31.75	1.85	0.05	1.80	0.91	0.256	1.68	0.152	0.90	1.10	0.186	No
472	31.80	1.86	0.06	1.80	0.91	0.256	1.68	0.152	0.90	1.10	0.186	No
473	31.90	1.86	0.06	1.80	0.91	0.257	1.68	0.153	0.90	1.10	0.187	No
474	31.94	1.87	0.06	1.81	0.91	0.257	1.68	0.153	0.90	1.10	0.187	No
475	32.04	1.87	0.06	1.81	0.91	0.257	1.68	0.153	0.90	1.10	0.187	No
476	32.09	1.87	0.07	1.81	0.91	0.257	1.68	0.153	0.90	1.10	0.187	No
477	32.20	1.88	0.07	1.81	0.91	0.257	1.68	0.153	0.90	1.10	0.187	No
478	32.24	1.88	0.07	1.81	0.91	0.258	1.68	0.153	0.90	1.10	0.188	No
479	32.28	1.89	0.07	1.82	0.91	0.258	1.68	0.153	0.90	1.10	0.188	No
480	32.29	1.89	0.07	1.82	0.91	0.258	1.68	0.153	0.90	1.10	0.188	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	32.30	1.89	0.07	1.82	0.91	0.258	1.68	0.153	0.90	1.10	0.188	No
482	32.40	1.89	0.07	1.82	0.91	0.258	1.68	0.153	0.90	1.10	0.188	No
483	32.45	1.90	0.08	1.82	0.91	0.258	1.68	0.153	0.90	1.10	0.188	No
484	32.55	1.90	0.08	1.82	0.91	0.258	1.68	0.154	0.90	1.10	0.188	No
485	32.59	1.91	0.08	1.83	0.91	0.258	1.68	0.154	0.90	1.10	0.188	No
486	32.69	1.91	0.08	1.83	0.91	0.259	1.68	0.154	0.90	1.10	0.189	No
487	32.76	1.92	0.09	1.83	0.91	0.259	1.68	0.154	0.90	1.10	0.189	No
488	32.84	1.92	0.09	1.83	0.90	0.259	1.68	0.154	0.90	1.10	0.189	No
489	32.90	1.93	0.09	1.84	0.90	0.259	1.68	0.154	0.90	1.10	0.189	No
490	32.98	1.93	0.09	1.84	0.90	0.259	1.68	0.154	0.90	1.10	0.189	No
491	33.06	1.94	0.10	1.84	0.90	0.259	1.68	0.154	0.90	1.10	0.189	No
492	33.12	1.94	0.10	1.84	0.90	0.260	1.68	0.154	0.89	1.10	0.190	No
493	33.22	1.95	0.10	1.85	0.90	0.260	1.68	0.154	0.89	1.10	0.190	No
494	33.31	1.95	0.10	1.85	0.90	0.260	1.68	0.155	0.89	1.10	0.190	No
495	33.37	1.96	0.10	1.85	0.90	0.260	1.68	0.155	0.89	1.10	0.190	No
496	33.46	1.96	0.11	1.85	0.90	0.260	1.68	0.155	0.89	1.10	0.190	No
497	33.55	1.97	0.11	1.86	0.90	0.260	1.68	0.155	0.89	1.10	0.191	No
498	33.65	1.97	0.11	1.86	0.90	0.261	1.68	0.155	0.89	1.10	0.191	No
499	33.70	1.98	0.12	1.86	0.90	0.261	1.68	0.155	0.89	1.10	0.191	No
500	33.79	1.98	0.12	1.86	0.90	0.261	1.68	0.155	0.89	1.10	0.191	No
501	33.89	1.99	0.12	1.87	0.90	0.261	1.68	0.155	0.89	1.10	0.191	No
502	33.99	2.00	0.12	1.87	0.90	0.261	1.68	0.155	0.89	1.10	0.191	No
503	34.04	2.00	0.13	1.87	0.90	0.261	1.68	0.155	0.89	1.10	0.192	No
504	34.13	2.00	0.13	1.88	0.90	0.262	1.68	0.155	0.89	1.10	0.192	No
505	34.23	2.01	0.13	1.88	0.90	0.262	1.68	0.156	0.89	1.10	0.192	No
506	34.32	2.02	0.13	1.88	0.90	0.262	1.68	0.156	0.89	1.10	0.192	No
507	34.37	2.02	0.14	1.88	0.89	0.262	1.68	0.156	0.89	1.10	0.192	No
508	34.47	2.03	0.14	1.89	0.89	0.262	1.68	0.156	0.89	1.10	0.192	No
509	34.55	2.03	0.14	1.89	0.89	0.262	1.68	0.156	0.89	1.10	2.000	Yes
510	34.63	2.04	0.14	1.89	0.89	0.262	1.68	0.156	0.89	1.10	2.000	Yes
511	34.73	2.04	0.15	1.90	0.89	0.263	1.68	0.156	0.89	1.10	2.000	Yes
512	34.80	2.05	0.15	1.90	0.89	0.263	1.68	0.156	0.89	1.10	2.000	Yes
513	34.90	2.05	0.15	1.90	0.89	0.263	1.68	0.156	0.89	1.10	2.000	Yes
514	35.00	2.06	0.16	1.90	0.89	0.263	1.68	0.156	0.89	1.10	0.193	No
515	35.12	2.07	0.16	1.91	0.89	0.263	1.68	0.156	0.89	1.10	0.194	No
516	35.20	2.07	0.16	1.91	0.89	0.263	1.68	0.157	0.89	1.10	0.194	No
517	35.33	2.08	0.17	1.91	0.89	0.264	1.68	0.157	0.89	1.10	2.000	Yes
518	35.41	2.08	0.17	1.92	0.89	0.264	1.68	0.157	0.89	1.10	2.000	Yes
519	35.44	2.09	0.17	1.92	0.89	0.264	1.68	0.157	0.89	1.10	2.000	Yes
520	35.48	2.09	0.17	1.92	0.89	0.264	1.68	0.157	0.89	1.10	2.000	Yes
521	35.57	2.10	0.17	1.92	0.89	0.264	1.68	0.157	0.89	1.10	2.000	Yes
522	35.62	2.10	0.18	1.92	0.89	0.264	1.68	0.157	0.89	1.10	2.000	Yes
523	35.67	2.10	0.18	1.92	0.89	0.264	1.68	0.157	0.89	1.10	2.000	Yes
524	35.71	2.10	0.18	1.93	0.89	0.264	1.68	0.157	0.89	1.10	2.000	Yes
525	35.82	2.11	0.18	1.93	0.88	0.264	1.68	0.157	0.89	1.10	2.000	Yes
526	35.86	2.11	0.18	1.93	0.88	0.264	1.68	0.157	0.89	1.10	2.000	Yes
527	35.93	2.12	0.19	1.93	0.88	0.264	1.68	0.157	0.89	1.10	2.000	Yes
528	36.01	2.12	0.19	1.94	0.88	0.265	1.68	0.157	0.89	1.10	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	36.06	2.13	0.19	1.94	0.88	0.265	1.68	0.157	0.89	1.10	2.000	Yes
530	36.12	2.13	0.19	1.94	0.88	0.265	1.68	0.157	0.89	1.10	0.195	No
531	36.18	2.13	0.19	1.94	0.88	0.265	1.68	0.157	0.89	1.10	0.195	No
532	36.25	2.14	0.19	1.94	0.88	0.265	1.68	0.157	0.89	1.10	0.196	No
533	36.30	2.14	0.20	1.95	0.88	0.265	1.68	0.157	0.89	1.10	0.196	No
534	36.39	2.15	0.20	1.95	0.88	0.265	1.68	0.158	0.89	1.10	0.196	No
535	36.44	2.15	0.20	1.95	0.88	0.265	1.68	0.158	0.88	1.10	0.196	No
536	36.53	2.16	0.20	1.95	0.88	0.265	1.68	0.158	0.88	1.10	0.196	No
537	36.59	2.16	0.21	1.96	0.88	0.265	1.68	0.158	0.88	1.10	0.196	No
538	36.68	2.17	0.21	1.96	0.88	0.265	1.68	0.158	0.88	1.10	0.196	No
539	36.75	2.17	0.21	1.96	0.88	0.265	1.68	0.158	0.88	1.10	0.196	No
540	36.83	2.18	0.21	1.96	0.88	0.265	1.68	0.158	0.88	1.10	0.196	No
541	36.90	2.18	0.22	1.97	0.88	0.266	1.68	0.158	0.88	1.10	0.197	No
542	36.97	2.19	0.22	1.97	0.88	0.266	1.68	0.158	0.88	1.10	0.197	No
543	37.02	2.19	0.22	1.97	0.88	0.266	1.68	0.158	0.88	1.10	0.197	No
544	37.04	2.19	0.22	1.97	0.88	0.266	1.68	0.158	0.88	1.10	0.197	No
545	37.08	2.19	0.22	1.97	0.88	0.266	1.68	0.158	0.88	1.10	0.197	No
546	37.17	2.20	0.22	1.98	0.87	0.266	1.68	0.158	0.88	1.10	0.197	No
547	37.27	2.21	0.23	1.98	0.87	0.266	1.68	0.158	0.88	1.10	0.197	No
548	37.37	2.21	0.23	1.98	0.87	0.266	1.68	0.158	0.88	1.10	0.197	No
549	37.42	2.22	0.23	1.98	0.87	0.266	1.68	0.158	0.88	1.10	0.197	No
550	37.51	2.22	0.23	1.99	0.87	0.266	1.68	0.158	0.88	1.10	0.197	No
551	37.58	2.23	0.24	1.99	0.87	0.266	1.68	0.158	0.88	1.10	0.197	No
552	37.66	2.23	0.24	1.99	0.87	0.266	1.68	0.158	0.88	1.10	0.198	No
553	37.76	2.24	0.24	1.99	0.87	0.266	1.68	0.158	0.88	1.10	0.198	No
554	37.85	2.24	0.24	2.00	0.87	0.266	1.68	0.158	0.88	1.10	0.198	No
555	37.93	2.25	0.25	2.00	0.87	0.266	1.68	0.158	0.88	1.10	0.198	No
556	38.04	2.26	0.25	2.00	0.87	0.267	1.68	0.158	0.88	1.10	0.198	No
557	38.13	2.26	0.25	2.01	0.87	0.267	1.68	0.158	0.88	1.10	0.198	No
558	38.18	2.26	0.26	2.01	0.87	0.267	1.68	0.158	0.88	1.10	0.198	No
559	38.28	2.27	0.26	2.01	0.87	0.267	1.68	0.159	0.88	1.10	0.198	No
560	38.37	2.28	0.26	2.01	0.86	0.267	1.68	0.159	0.88	1.10	0.198	No
561	38.47	2.28	0.26	2.02	0.86	0.267	1.68	0.159	0.88	1.10	0.198	No
562	38.57	2.29	0.27	2.02	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
563	38.62	2.29	0.27	2.02	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
564	38.72	2.30	0.27	2.03	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
565	38.78	2.30	0.27	2.03	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
566	38.81	2.30	0.27	2.03	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
567	38.86	2.31	0.28	2.03	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
568	38.91	2.31	0.28	2.03	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
569	38.95	2.31	0.28	2.03	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
570	39.05	2.32	0.28	2.04	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
571	39.09	2.32	0.28	2.04	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
572	39.14	2.33	0.29	2.04	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
573	39.24	2.33	0.29	2.04	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
574	39.29	2.33	0.29	2.05	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
575	39.39	2.34	0.29	2.05	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
576	39.43	2.34	0.29	2.05	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	39.53	2.35	0.30	2.05	0.86	0.267	1.68	0.159	0.88	1.10	0.200	No
578	39.57	2.35	0.30	2.05	0.85	0.267	1.68	0.159	0.88	1.10	0.200	No
579	39.68	2.36	0.30	2.06	0.85	0.267	1.68	0.159	0.88	1.10	0.200	No
580	39.73	2.36	0.30	2.06	0.85	0.267	1.68	0.159	0.88	1.10	0.200	No
581	39.81	2.37	0.31	2.06	0.85	0.267	1.68	0.159	0.88	1.10	0.200	No
582	39.89	2.37	0.31	2.07	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
583	39.96	2.38	0.31	2.07	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
584	40.06	2.38	0.31	2.07	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
585	40.15	2.39	0.32	2.07	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
586	40.20	2.39	0.32	2.07	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
587	40.24	2.40	0.32	2.08	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
588	40.26	2.40	0.32	2.08	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
589	40.27	2.40	0.32	2.08	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
590	40.37	2.40	0.32	2.08	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
591	40.42	2.41	0.32	2.08	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
592	40.52	2.41	0.33	2.09	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
593	40.56	2.42	0.33	2.09	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
594	40.66	2.42	0.33	2.09	0.85	0.267	1.68	0.159	0.87	1.10	0.200	No
595	40.70	2.43	0.33	2.09	0.84	0.267	1.68	0.159	0.87	1.10	0.200	No
596	40.75	2.43	0.34	2.09	0.84	0.267	1.68	0.159	0.87	1.10	0.200	No
597	40.85	2.43	0.34	2.10	0.84	0.267	1.68	0.159	0.87	1.10	0.200	No
598	40.91	2.44	0.34	2.10	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
599	40.96	2.44	0.34	2.10	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
600	41.04	2.45	0.34	2.10	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
601	41.09	2.45	0.35	2.10	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
602	41.18	2.46	0.35	2.11	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
603	41.23	2.46	0.35	2.11	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
604	41.29	2.46	0.35	2.11	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
605	41.38	2.47	0.36	2.11	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
606	41.42	2.47	0.36	2.12	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
607	41.52	2.48	0.36	2.12	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
608	41.57	2.48	0.36	2.12	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
609	41.62	2.49	0.36	2.12	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
610	41.71	2.49	0.37	2.13	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
611	41.76	2.49	0.37	2.13	0.84	0.267	1.68	0.159	0.87	1.10	0.201	No
612	41.84	2.50	0.37	2.13	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
613	41.91	2.50	0.37	2.13	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
614	41.95	2.51	0.37	2.13	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
615	42.01	2.51	0.37	2.14	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
616	42.10	2.52	0.38	2.14	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
617	42.15	2.52	0.38	2.14	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
618	42.24	2.53	0.38	2.14	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
619	42.28	2.53	0.38	2.15	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
620	42.39	2.54	0.39	2.15	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
621	42.43	2.54	0.39	2.15	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
622	42.50	2.54	0.39	2.15	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
623	42.58	2.55	0.39	2.16	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
624	42.65	2.55	0.39	2.16	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	42.70	2.56	0.40	2.16	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
626	42.73	2.56	0.40	2.16	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
627	42.77	2.56	0.40	2.16	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
628	42.82	2.56	0.40	2.16	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
629	42.87	2.57	0.40	2.17	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
630	42.91	2.57	0.40	2.17	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
631	42.97	2.57	0.40	2.17	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
632	43.02	2.58	0.41	2.17	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
633	43.06	2.58	0.41	2.17	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
634	43.11	2.58	0.41	2.17	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
635	43.17	2.59	0.41	2.18	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
636	43.21	2.59	0.41	2.18	0.82	0.267	1.68	0.158	0.87	1.10	0.201	No
637	43.29	2.59	0.41	2.18	0.82	0.267	1.68	0.158	0.87	1.10	0.201	No
638	43.34	2.60	0.42	2.18	0.82	0.267	1.68	0.158	0.87	1.10	0.201	No
639	43.39	2.60	0.42	2.18	0.82	0.267	1.68	0.158	0.87	1.10	0.201	No
640	43.45	2.61	0.42	2.19	0.82	0.266	1.68	0.158	0.86	1.10	0.201	No
641	43.51	2.61	0.42	2.19	0.82	0.266	1.68	0.158	0.86	1.10	0.201	No
642	43.59	2.61	0.42	2.19	0.82	0.266	1.68	0.158	0.86	1.10	0.201	No
643	43.64	2.62	0.43	2.19	0.82	0.266	1.68	0.158	0.86	1.10	0.201	No
644	43.70	2.62	0.43	2.19	0.82	0.266	1.68	0.158	0.86	1.10	0.201	No
645	43.78	2.63	0.43	2.20	0.82	0.266	1.68	0.158	0.86	1.10	0.201	No
646	43.88	2.63	0.43	2.20	0.81	0.266	1.68	0.158	0.86	1.10	0.201	No
647	43.94	2.64	0.43	2.20	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
648	44.04	2.64	0.44	2.21	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
649	44.07	2.65	0.44	2.21	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
650	44.12	2.65	0.44	2.21	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
651	44.16	2.65	0.44	2.21	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
652	44.21	2.65	0.44	2.21	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
653	44.26	2.66	0.44	2.21	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
654	44.31	2.66	0.45	2.22	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
655	44.35	2.66	0.45	2.22	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
656	44.40	2.67	0.45	2.22	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
657	44.45	2.67	0.45	2.22	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
658	44.50	2.67	0.45	2.22	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
659	44.54	2.68	0.45	2.22	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
660	44.60	2.68	0.46	2.22	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
661	44.64	2.68	0.46	2.23	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
662	44.69	2.69	0.46	2.23	0.81	0.266	1.68	0.158	0.86	1.10	0.202	No
663	44.74	2.69	0.46	2.23	0.81	0.265	1.68	0.158	0.86	1.10	0.202	No
664	44.79	2.69	0.46	2.23	0.81	0.265	1.68	0.158	0.86	1.10	0.201	No
665	44.83	2.70	0.46	2.23	0.81	0.265	1.68	0.158	0.86	1.10	0.201	No
666	44.88	2.70	0.46	2.23	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
667	44.93	2.70	0.47	2.24	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
668	44.98	2.71	0.47	2.24	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
669	45.03	2.71	0.47	2.24	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
670	45.08	2.71	0.47	2.24	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
671	45.16	2.72	0.47	2.24	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
672	45.19	2.72	0.47	2.25	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	45.27	2.72	0.48	2.25	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
674	45.32	2.73	0.48	2.25	0.80	0.265	1.68	0.157	0.86	1.10	0.201	No
675	45.37	2.73	0.48	2.25	0.80	0.265	1.68	0.157	0.86	1.10	0.201	No
676	45.45	2.74	0.48	2.25	0.80	0.265	1.68	0.157	0.86	1.10	0.201	No
677	45.51	2.74	0.48	2.26	0.80	0.265	1.68	0.157	0.86	1.10	0.201	No
678	45.56	2.74	0.49	2.26	0.80	0.265	1.68	0.157	0.86	1.10	2.000	Yes
679	45.61	2.75	0.49	2.26	0.80	0.265	1.68	0.157	0.86	1.10	2.000	Yes
680	45.69	2.75	0.49	2.26	0.80	0.265	1.68	0.157	0.86	1.10	2.000	Yes
681	45.75	2.76	0.49	2.26	0.80	0.265	1.68	0.157	0.86	1.10	2.000	Yes
682	45.81	2.76	0.49	2.27	0.80	0.264	1.68	0.157	0.86	1.10	2.000	Yes
683	45.89	2.76	0.50	2.27	0.79	0.264	1.68	0.157	0.86	1.10	2.000	Yes
684	45.94	2.77	0.50	2.27	0.79	0.264	1.68	0.157	0.86	1.10	2.000	Yes
685	46.04	2.77	0.50	2.27	0.79	0.264	1.68	0.157	0.86	1.10	2.000	Yes
686	46.08	2.78	0.50	2.27	0.79	0.264	1.68	0.157	0.86	1.10	2.000	Yes
687	46.15	2.78	0.50	2.28	0.79	0.264	1.68	0.157	0.86	1.10	2.000	Yes
688	46.17	2.78	0.50	2.28	0.79	0.264	1.68	0.157	0.86	1.10	0.201	No
689	46.18	2.78	0.50	2.28	0.79	0.264	1.68	0.157	0.86	1.10	0.201	No
690	46.23	2.79	0.51	2.28	0.79	0.264	1.68	0.157	0.86	1.10	0.201	No
691	46.27	2.79	0.51	2.28	0.79	0.264	1.68	0.157	0.86	1.10	0.201	No
692	46.32	2.79	0.51	2.28	0.79	0.264	1.68	0.157	0.86	1.10	0.201	No
693	46.41	2.80	0.51	2.28	0.79	0.264	1.68	0.157	0.86	1.10	0.201	No
694	46.47	2.80	0.51	2.29	0.79	0.264	1.68	0.157	0.86	1.10	0.201	No
695	46.52	2.80	0.52	2.29	0.79	0.264	1.68	0.157	0.86	1.10	0.201	No
696	46.56	2.81	0.52	2.29	0.79	0.264	1.68	0.157	0.86	1.10	0.201	No
697	46.65	2.81	0.52	2.29	0.79	0.264	1.68	0.157	0.86	1.10	0.201	No
698	46.71	2.81	0.52	2.29	0.79	0.263	1.68	0.157	0.86	1.10	0.201	No
699	46.76	2.82	0.52	2.29	0.79	0.263	1.68	0.157	0.86	1.10	0.201	No
700	46.85	2.82	0.53	2.30	0.78	0.263	1.68	0.157	0.86	1.10	0.201	No
701	46.90	2.83	0.53	2.30	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
702	46.99	2.83	0.53	2.30	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
703	47.04	2.84	0.53	2.30	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
704	47.10	2.84	0.53	2.31	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
705	47.16	2.84	0.54	2.31	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
706	47.23	2.85	0.54	2.31	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
707	47.30	2.85	0.54	2.31	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
708	47.38	2.86	0.54	2.31	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
709	47.43	2.86	0.54	2.32	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
710	47.52	2.86	0.55	2.32	0.78	0.263	1.68	0.156	0.85	1.10	0.201	No
711	47.59	2.87	0.55	2.32	0.78	0.262	1.68	0.156	0.85	1.10	0.201	No
712	47.66	2.87	0.55	2.32	0.78	0.262	1.68	0.156	0.85	1.10	0.201	No
713	47.77	2.88	0.55	2.32	0.78	0.262	1.68	0.156	0.85	1.10	0.201	No
714	47.82	2.88	0.56	2.33	0.77	0.262	1.68	0.156	0.85	1.10	0.201	No
715	47.91	2.89	0.56	2.33	0.77	0.262	1.68	0.156	0.85	1.10	0.201	No
716	47.93	2.89	0.56	2.33	0.77	0.262	1.68	0.156	0.85	1.10	0.201	No
717	47.97	2.89	0.56	2.33	0.77	0.262	1.68	0.156	0.85	1.10	0.201	No
718	48.02	2.89	0.56	2.33	0.77	0.262	1.68	0.156	0.85	1.10	0.201	No
719	48.07	2.90	0.56	2.33	0.77	0.262	1.68	0.156	0.85	1.10	0.201	No
720	48.12	2.90	0.57	2.33	0.77	0.262	1.68	0.156	0.85	1.10	0.201	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	48.19	2.90	0.57	2.34	0.77	0.262	1.68	0.156	0.85	1.10	0.200	No
722	48.23	2.91	0.57	2.34	0.77	0.262	1.68	0.156	0.85	1.10	0.200	No
723	48.31	2.91	0.57	2.34	0.77	0.262	1.68	0.155	0.85	1.10	0.200	No
724	48.35	2.91	0.57	2.34	0.77	0.262	1.68	0.155	0.85	1.10	0.200	No
725	48.40	2.92	0.57	2.34	0.77	0.261	1.68	0.155	0.85	1.10	0.200	No
726	48.45	2.92	0.58	2.34	0.77	0.261	1.68	0.155	0.85	1.10	0.200	No
727	48.50	2.92	0.58	2.34	0.77	0.261	1.68	0.155	0.85	1.10	0.200	No
728	48.55	2.92	0.58	2.35	0.77	0.261	1.68	0.155	0.85	1.10	0.200	No
729	48.59	2.93	0.58	2.35	0.77	0.261	1.68	0.155	0.85	1.10	0.200	No
730	48.67	2.93	0.58	2.35	0.77	0.261	1.68	0.155	0.85	1.10	0.200	No
731	48.73	2.93	0.58	2.35	0.77	0.261	1.68	0.155	0.85	1.10	0.200	No
732	48.78	2.94	0.59	2.35	0.77	0.261	1.68	0.155	0.85	1.10	0.200	No
733	48.83	2.94	0.59	2.35	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
734	48.91	2.94	0.59	2.35	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
735	48.98	2.95	0.59	2.36	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
736	49.03	2.95	0.59	2.36	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
737	49.12	2.96	0.60	2.36	0.76	0.260	1.68	0.155	0.85	1.10	0.200	No
738	49.17	2.96	0.60	2.36	0.76	0.260	1.68	0.155	0.85	1.10	0.200	No
739	49.27	2.97	0.60	2.36	0.76	0.260	1.68	0.155	0.85	1.10	0.200	No
740	49.31	2.97	0.60	2.37	0.76	0.260	1.68	0.155	0.85	1.10	0.200	No
741	49.38	2.97	0.60	2.37	0.76	0.260	1.68	0.155	0.85	1.10	0.200	No
742	49.45	2.98	0.61	2.37	0.76	0.260	1.68	0.155	0.85	1.10	0.200	No
743	49.51	2.98	0.61	2.37	0.76	0.260	1.68	0.155	0.85	1.10	0.200	No
744	49.54	2.98	0.61	2.37	0.76	0.260	1.68	0.155	0.85	1.10	0.200	No
745	49.59	2.98	0.61	2.37	0.76	0.260	1.68	0.154	0.85	1.10	0.200	No
746	49.64	2.99	0.61	2.37	0.76	0.260	1.68	0.154	0.85	1.10	0.200	No
747	49.73	2.99	0.62	2.38	0.76	0.260	1.68	0.154	0.85	1.10	0.200	No
748	49.83	3.00	0.62	2.38	0.75	0.260	1.68	0.154	0.85	1.10	0.200	No
749	49.92	3.00	0.62	2.38	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
750	49.98	3.01	0.62	2.38	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
751	50.07	3.01	0.63	2.39	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
752	50.16	3.02	0.63	2.39	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
753	50.24	3.02	0.63	2.39	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
754	50.32	3.03	0.63	2.39	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
755	50.41	3.03	0.64	2.39	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
756	50.50	3.04	0.64	2.40	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
757	50.56	3.04	0.64	2.40	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
758	50.66	3.04	0.64	2.40	0.75	0.258	1.68	0.154	0.85	1.10	0.199	No
759	50.74	3.05	0.65	2.40	0.75	0.258	1.68	0.153	0.85	1.10	0.199	No
760	50.84	3.05	0.65	2.40	0.74	0.258	1.68	0.153	0.85	1.10	0.199	No
761	50.93	3.06	0.65	2.41	0.74	0.258	1.68	0.153	0.85	1.10	0.199	No
762	50.98	3.06	0.65	2.41	0.74	0.258	1.68	0.153	0.85	1.10	0.199	No
763	51.08	3.07	0.66	2.41	0.74	0.258	1.68	0.153	0.85	1.10	0.199	No
764	51.17	3.07	0.66	2.41	0.74	0.258	1.68	0.153	0.85	1.10	0.199	No
765	51.24	3.08	0.66	2.42	0.74	0.257	1.68	0.153	0.85	1.10	0.199	No
766	51.34	3.09	0.67	2.42	0.74	0.257	1.68	0.153	0.85	1.10	0.199	No
767	51.41	3.09	0.67	2.42	0.74	0.257	1.68	0.153	0.85	1.10	0.198	No
768	51.51	3.10	0.67	2.42	0.74	0.257	1.68	0.153	0.85	1.10	0.198	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	51.58	3.10	0.67	2.43	0.74	0.257	1.68	0.153	0.85	1.10	0.198	No
770	51.68	3.11	0.68	2.43	0.74	0.257	1.68	0.153	0.85	1.10	0.198	No
771	51.79	3.11	0.68	2.43	0.73	0.257	1.68	0.153	0.85	1.10	0.198	No
772	51.82	3.11	0.68	2.43	0.73	0.257	1.68	0.152	0.85	1.10	0.198	No
773	51.85	3.12	0.68	2.43	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
774	51.91	3.12	0.68	2.44	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
775	52.00	3.13	0.69	2.44	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
776	52.05	3.13	0.69	2.44	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
777	52.10	3.13	0.69	2.44	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
778	52.19	3.14	0.69	2.44	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
779	52.28	3.14	0.70	2.45	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
780	52.34	3.15	0.70	2.45	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
781	52.42	3.15	0.70	2.45	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
782	52.48	3.15	0.70	2.45	0.73	0.255	1.68	0.152	0.85	1.10	0.198	No
783	52.57	3.16	0.70	2.46	0.73	0.255	1.68	0.152	0.84	1.10	0.198	No
784	52.62	3.16	0.71	2.46	0.73	0.255	1.68	0.152	0.84	1.10	0.198	No
785	52.69	3.17	0.71	2.46	0.73	0.255	1.68	0.152	0.84	1.10	0.197	No
786	52.77	3.17	0.71	2.46	0.72	0.255	1.68	0.152	0.84	1.10	0.197	No
787	52.87	3.18	0.71	2.46	0.72	0.255	1.68	0.151	0.84	1.10	0.197	No
788	52.91	3.18	0.71	2.47	0.72	0.255	1.68	0.151	0.84	1.10	0.197	No
789	53.01	3.19	0.72	2.47	0.72	0.255	1.68	0.151	0.84	1.10	0.197	No
790	53.10	3.19	0.72	2.47	0.72	0.254	1.68	0.151	0.84	1.10	0.197	No
791	53.16	3.20	0.72	2.47	0.72	0.254	1.68	0.151	0.84	1.10	0.197	No
792	53.25	3.20	0.73	2.48	0.72	0.254	1.68	0.151	0.84	1.10	0.197	No
793	53.29	3.20	0.73	2.48	0.72	0.254	1.68	0.151	0.84	1.10	0.197	No
794	53.38	3.21	0.73	2.48	0.72	0.254	1.68	0.151	0.84	1.10	0.197	No
795	53.42	3.21	0.73	2.48	0.72	0.254	1.68	0.151	0.84	1.10	0.197	No
796	53.47	3.22	0.73	2.48	0.72	0.254	1.68	0.151	0.84	1.10	0.197	No
797	53.52	3.22	0.73	2.49	0.72	0.254	1.68	0.151	0.84	1.10	0.197	No
798	53.58	3.22	0.74	2.49	0.72	0.254	1.68	0.151	0.84	1.10	0.197	No
799	53.66	3.23	0.74	2.49	0.72	0.253	1.68	0.151	0.84	1.10	0.197	No
800	53.75	3.23	0.74	2.49	0.72	0.253	1.68	0.151	0.84	1.10	0.197	No
801	53.81	3.24	0.74	2.50	0.71	0.253	1.68	0.151	0.84	1.10	0.197	No
802	53.87	3.24	0.74	2.50	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
803	53.95	3.25	0.75	2.50	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
804	54.01	3.25	0.75	2.50	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
805	54.06	3.26	0.75	2.50	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
806	54.15	3.26	0.75	2.51	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
807	54.20	3.26	0.76	2.51	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No
808	54.29	3.27	0.76	2.51	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No
809	54.34	3.27	0.76	2.51	0.71	0.252	1.68	0.150	0.84	1.10	2.000	Yes
810	54.43	3.28	0.76	2.52	0.71	0.252	1.68	0.150	0.84	1.10	2.000	Yes
811	54.45	3.28	0.76	2.52	0.71	0.252	1.68	0.150	0.84	1.10	2.000	Yes
812	54.48	3.28	0.76	2.52	0.71	0.252	1.68	0.150	0.84	1.10	2.000	Yes
813	54.52	3.28	0.76	2.52	0.71	0.252	1.68	0.150	0.84	1.10	2.000	Yes
814	54.53	3.29	0.77	2.52	0.71	0.252	1.68	0.150	0.84	1.10	2.000	Yes
815	54.58	3.29	0.77	2.52	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No
816	54.62	3.29	0.77	2.52	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	54.65	3.29	0.77	2.52	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No
818	54.70	3.30	0.77	2.53	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No
819	54.76	3.30	0.77	2.53	0.71	0.252	1.68	0.149	0.84	1.10	0.196	No
820	54.77	3.30	0.77	2.53	0.71	0.251	1.68	0.149	0.84	1.10	0.196	No
821	54.82	3.30	0.77	2.53	0.71	0.251	1.68	0.149	0.84	1.10	0.196	No
822	54.87	3.31	0.78	2.53	0.70	0.251	1.68	0.149	0.84	1.10	0.196	No
823	54.88	3.31	0.78	2.53	0.70	0.251	1.68	0.149	0.84	1.10	0.196	No
824	54.91	3.31	0.78	2.53	0.70	0.251	1.68	0.149	0.84	1.10	0.196	No
825	54.96	3.31	0.78	2.53	0.70	0.251	1.68	0.149	0.84	1.10	0.196	No
826	54.97	3.31	0.78	2.53	0.70	0.251	1.68	0.149	0.84	1.10	0.196	No
827	55.03	3.32	0.78	2.54	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
828	55.09	3.32	0.78	2.54	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
829	55.15	3.33	0.78	2.54	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
830	55.20	3.33	0.79	2.54	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
831	55.25	3.33	0.79	2.54	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
832	55.30	3.34	0.79	2.55	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
833	55.34	3.34	0.79	2.55	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
834	55.39	3.34	0.79	2.55	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
835	55.40	3.34	0.79	2.55	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
836	55.44	3.34	0.79	2.55	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
837	55.44	3.35	0.79	2.55	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
838	55.49	3.35	0.80	2.55	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
839	55.54	3.35	0.80	2.56	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
840	55.59	3.36	0.80	2.56	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
841	55.63	3.36	0.80	2.56	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
842	55.64	3.36	0.80	2.56	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
843	55.68	3.36	0.80	2.56	0.70	0.250	1.68	0.148	0.84	1.10	0.195	No
844	55.69	3.36	0.80	2.56	0.70	0.250	1.68	0.148	0.84	1.10	0.195	No
845	55.69	3.36	0.80	2.56	0.70	0.250	1.68	0.148	0.84	1.10	0.195	No
846	55.71	3.36	0.80	2.56	0.70	0.250	1.68	0.148	0.84	1.10	0.195	No
847	55.76	3.37	0.80	2.56	0.70	0.250	1.68	0.148	0.84	1.10	0.195	No
848	55.78	3.37	0.80	2.56	0.70	0.250	1.68	0.148	0.84	1.10	0.195	No
849	55.81	3.37	0.81	2.57	0.70	0.250	1.68	0.148	0.84	1.10	0.195	No
850	55.85	3.37	0.81	2.57	0.70	0.249	1.68	0.148	0.84	1.10	0.195	No
851	55.86	3.37	0.81	2.57	0.70	0.249	1.68	0.148	0.84	1.10	0.195	No
852	55.91	3.38	0.81	2.57	0.69	0.249	1.68	0.148	0.84	1.10	0.195	No
853	55.92	3.38	0.81	2.57	0.69	0.249	1.68	0.148	0.84	1.10	0.195	No
854	55.96	3.38	0.81	2.57	0.69	0.249	1.68	0.148	0.84	1.10	0.195	No
855	55.97	3.38	0.81	2.57	0.69	0.249	1.68	0.148	0.84	1.10	0.195	No
856	56.00	3.38	0.81	2.57	0.69	0.249	1.68	0.148	0.84	1.10	0.195	No
857	56.01	3.38	0.81	2.57	0.69	0.249	1.68	0.148	0.84	1.10	0.195	No
858	56.03	3.39	0.81	2.57	0.69	0.249	1.68	0.148	0.84	1.10	0.195	No
859	56.05	3.39	0.81	2.57	0.69	0.249	1.68	0.148	0.84	1.10	0.195	No
860	56.10	3.39	0.81	2.58	0.69	0.249	1.68	0.148	0.84	1.10	0.195	No
861	56.12	3.39	0.81	2.58	0.69	0.249	1.68	0.148	0.84	1.10	0.195	No
862	56.16	3.39	0.82	2.58	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
863	56.17	3.40	0.82	2.58	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
864	56.20	3.40	0.82	2.58	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	56.22	3.40	0.82	2.58	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
866	56.24	3.40	0.82	2.58	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
867	56.30	3.40	0.82	2.58	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
868	56.31	3.40	0.82	2.58	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
869	56.34	3.41	0.82	2.59	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
870	56.39	3.41	0.82	2.59	0.69	0.248	1.68	0.148	0.84	1.10	0.194	No
871	56.45	3.41	0.83	2.59	0.69	0.248	1.68	0.148	0.84	1.10	0.194	No
872	56.48	3.42	0.83	2.59	0.69	0.248	1.68	0.148	0.84	1.10	0.194	No
873	56.49	3.42	0.83	2.59	0.69	0.248	1.68	0.148	0.84	1.10	0.194	No
874	56.53	3.42	0.83	2.59	0.69	0.248	1.68	0.148	0.84	1.10	0.194	No
875	56.58	3.42	0.83	2.59	0.69	0.248	1.68	0.147	0.84	1.10	0.194	No
876	56.63	3.43	0.83	2.60	0.69	0.248	1.68	0.147	0.84	1.10	0.194	No
877	56.68	3.43	0.83	2.60	0.69	0.248	1.68	0.147	0.84	1.10	0.194	No
878	56.73	3.43	0.83	2.60	0.69	0.248	1.68	0.147	0.84	1.10	0.194	No
879	56.78	3.44	0.84	2.60	0.69	0.248	1.68	0.147	0.84	1.10	0.194	No
880	56.83	3.44	0.84	2.60	0.69	0.248	1.68	0.147	0.84	1.10	0.194	No
881	56.89	3.44	0.84	2.61	0.69	0.248	1.68	0.147	0.84	1.10	0.194	No
882	56.95	3.45	0.84	2.61	0.69	0.247	1.68	0.147	0.83	1.10	0.194	No
883	56.99	3.45	0.84	2.61	0.68	0.247	1.68	0.147	0.83	1.10	0.194	No
884	57.01	3.45	0.84	2.61	0.68	0.247	1.68	0.147	0.83	1.10	0.194	No
885	57.04	3.45	0.84	2.61	0.68	0.247	1.68	0.147	0.83	1.10	0.194	No
886	57.09	3.46	0.85	2.61	0.68	0.247	1.68	0.147	0.83	1.10	0.194	No
887	57.11	3.46	0.85	2.61	0.68	0.247	1.68	0.147	0.83	1.10	0.194	No
888	57.13	3.46	0.85	2.61	0.68	0.247	1.68	0.147	0.83	1.10	0.194	No
889	57.18	3.46	0.85	2.62	0.68	0.247	1.68	0.147	0.83	1.10	0.194	No
890	57.19	3.46	0.85	2.62	0.68	0.247	1.68	0.147	0.83	1.10	0.194	No
891	57.21	3.47	0.85	2.62	0.68	0.247	1.68	0.147	0.83	1.10	0.194	No
892	57.24	3.47	0.85	2.62	0.68	0.247	1.68	0.147	0.83	1.10	0.194	No
893	57.28	3.47	0.85	2.62	0.68	0.247	1.68	0.147	0.83	1.10	0.193	No
894	57.32	3.47	0.85	2.62	0.68	0.247	1.68	0.147	0.83	1.10	0.193	No
895	57.35	3.48	0.85	2.62	0.68	0.247	1.68	0.147	0.83	1.10	0.193	No
896	57.38	3.48	0.85	2.62	0.68	0.247	1.68	0.147	0.83	1.10	0.193	No
897	57.43	3.48	0.86	2.63	0.68	0.247	1.68	0.147	0.83	1.10	0.193	No
898	57.48	3.48	0.86	2.63	0.68	0.246	1.68	0.147	0.83	1.10	0.193	No
899	57.52	3.49	0.86	2.63	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
900	57.57	3.49	0.86	2.63	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
901	57.62	3.49	0.86	2.63	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
902	57.68	3.50	0.86	2.63	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
903	57.76	3.50	0.87	2.64	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
904	57.81	3.51	0.87	2.64	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
905	57.86	3.51	0.87	2.64	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
906	57.89	3.51	0.87	2.64	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
907	57.91	3.51	0.87	2.64	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
908	57.92	3.51	0.87	2.64	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
909	57.95	3.52	0.87	2.64	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
910	57.99	3.52	0.87	2.65	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
911	58.01	3.52	0.87	2.65	0.68	0.245	1.68	0.146	0.83	1.10	0.193	No
912	58.05	3.52	0.88	2.65	0.68	0.245	1.68	0.146	0.83	1.10	0.193	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	58.05	3.52	0.88	2.65	0.68	0.245	1.68	0.146	0.83	1.10	0.193	No
914	58.10	3.53	0.88	2.65	0.68	0.245	1.68	0.146	0.83	1.10	0.193	No
915	58.13	3.53	0.88	2.65	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
916	58.15	3.53	0.88	2.65	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
917	58.17	3.53	0.88	2.65	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
918	58.20	3.53	0.88	2.65	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
919	58.21	3.53	0.88	2.65	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
920	58.21	3.53	0.88	2.65	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
921	58.23	3.54	0.88	2.65	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
922	58.24	3.54	0.88	2.66	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
923	58.25	3.54	0.88	2.66	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
924	58.29	3.54	0.88	2.66	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
925	58.31	3.54	0.88	2.66	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
926	58.33	3.54	0.88	2.66	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
927	58.38	3.55	0.89	2.66	0.67	0.245	1.68	0.146	0.83	1.10	0.192	No
928	58.39	3.55	0.89	2.66	0.67	0.245	1.68	0.146	0.83	1.10	0.192	No
929	58.43	3.55	0.89	2.66	0.67	0.245	1.68	0.145	0.83	1.10	0.192	No
930	58.43	3.55	0.89	2.66	0.67	0.245	1.68	0.145	0.83	1.10	0.192	No
931	58.48	3.55	0.89	2.66	0.67	0.245	1.68	0.145	0.83	1.10	0.192	No
932	58.53	3.56	0.89	2.67	0.67	0.245	1.68	0.145	0.83	1.10	0.192	No
933	58.56	3.56	0.89	2.67	0.67	0.245	1.68	0.145	0.83	1.10	0.192	No
934	58.58	3.56	0.89	2.67	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
935	58.59	3.56	0.89	2.67	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
936	58.63	3.56	0.89	2.67	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
937	58.63	3.56	0.89	2.67	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
938	58.63	3.56	0.89	2.67	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
939	58.68	3.57	0.89	2.67	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
940	58.69	3.57	0.90	2.67	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
941	58.72	3.57	0.90	2.67	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
942	58.73	3.57	0.90	2.67	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
943	58.74	3.57	0.90	2.67	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
944	58.77	3.57	0.90	2.67	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
945	58.81	3.57	0.90	2.68	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
946	58.82	3.57	0.90	2.68	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
947	58.83	3.58	0.90	2.68	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
948	58.87	3.58	0.90	2.68	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
949	58.91	3.58	0.90	2.68	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
950	58.92	3.58	0.90	2.68	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
951	58.93	3.58	0.90	2.68	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
952	58.96	3.58	0.90	2.68	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
953	59.01	3.59	0.91	2.68	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
954	59.06	3.59	0.91	2.68	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
955	59.08	3.59	0.91	2.69	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
956	59.11	3.59	0.91	2.69	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
957	59.15	3.60	0.91	2.69	0.67	0.243	1.68	0.145	0.83	1.10	0.192	No
958	59.21	3.60	0.91	2.69	0.67	0.243	1.68	0.145	0.83	1.10	0.192	No
959	59.26	3.60	0.91	2.69	0.67	0.243	1.68	0.145	0.83	1.10	0.192	No
960	59.30	3.61	0.91	2.69	0.66	0.243	1.68	0.145	0.83	1.10	0.192	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
961	59.35	3.61	0.92	2.70	0.66	0.243	1.68	0.144	0.83	1.10	0.192	No
962	59.40	3.61	0.92	2.70	0.66	0.243	1.68	0.144	0.83	1.10	0.192	No
963	59.42	3.62	0.92	2.70	0.66	0.243	1.68	0.144	0.83	1.10	0.192	No
964	59.47	3.62	0.92	2.70	0.66	0.243	1.68	0.144	0.83	1.10	0.192	No
965	59.51	3.62	0.92	2.70	0.66	0.243	1.68	0.144	0.83	1.10	0.191	No
966	59.56	3.63	0.92	2.70	0.66	0.243	1.68	0.144	0.83	1.10	0.191	No
967	59.61	3.63	0.92	2.71	0.66	0.243	1.68	0.144	0.83	1.10	0.191	No
968	59.67	3.63	0.93	2.71	0.66	0.243	1.68	0.144	0.83	1.10	0.191	No
969	59.71	3.64	0.93	2.71	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
970	59.80	3.64	0.93	2.71	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
971	59.85	3.65	0.93	2.71	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
972	59.90	3.65	0.93	2.72	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
973	60.00	3.65	0.94	2.72	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
974	60.04	3.66	0.94	2.72	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
975	60.10	3.66	0.94	2.72	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
976	60.15	3.67	0.94	2.72	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
977	60.19	3.67	0.94	2.73	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
978	60.23	3.67	0.94	2.73	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
979	60.28	3.67	0.94	2.73	0.66	0.241	1.68	0.144	0.83	1.10	0.191	No
980	60.33	3.68	0.95	2.73	0.66	0.241	1.68	0.143	0.83	1.10	0.191	No
981	60.38	3.68	0.95	2.73	0.66	0.241	1.68	0.143	0.83	1.10	0.191	No
982	60.42	3.68	0.95	2.73	0.66	0.241	1.68	0.143	0.83	1.10	0.191	No
983	60.44	3.68	0.95	2.73	0.66	0.241	1.68	0.143	0.83	1.10	0.191	No
984	60.47	3.69	0.95	2.74	0.66	0.241	1.68	0.143	0.83	1.10	0.191	No
985	60.52	3.69	0.95	2.74	0.66	0.241	1.68	0.143	0.83	1.10	0.191	No
986	60.56	3.69	0.95	2.74	0.65	0.241	1.68	0.143	0.83	1.10	0.191	No
987	60.57	3.69	0.95	2.74	0.65	0.241	1.68	0.143	0.83	1.10	0.191	No
988	60.61	3.70	0.96	2.74	0.65	0.241	1.68	0.143	0.83	1.10	0.191	No
989	60.66	3.70	0.96	2.74	0.65	0.241	1.68	0.143	0.83	1.10	0.190	No
990	60.71	3.70	0.96	2.74	0.65	0.241	1.68	0.143	0.83	1.10	0.190	No
991	60.76	3.71	0.96	2.75	0.65	0.241	1.68	0.143	0.83	1.10	0.190	No
992	60.81	3.71	0.96	2.75	0.65	0.241	1.68	0.143	0.83	1.10	0.190	No
993	60.86	3.71	0.96	2.75	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
994	60.91	3.72	0.96	2.75	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
995	60.95	3.72	0.97	2.75	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
996	61.00	3.72	0.97	2.76	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
997	61.02	3.72	0.97	2.76	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
998	61.05	3.73	0.97	2.76	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
999	61.08	3.73	0.97	2.76	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
1000	61.09	3.73	0.97	2.76	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
1001	61.13	3.73	0.97	2.76	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
1002	61.14	3.73	0.97	2.76	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
1003	61.16	3.73	0.97	2.76	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
1004	61.20	3.74	0.97	2.76	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
1005	61.23	3.74	0.97	2.76	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
1006	61.24	3.74	0.97	2.76	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
1007	61.29	3.74	0.98	2.77	0.65	0.240	1.68	0.142	0.83	1.10	0.190	No
1008	61.30	3.74	0.98	2.77	0.65	0.240	1.68	0.142	0.83	1.10	0.190	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1009	61.33	3.75	0.98	2.77	0.65	0.240	1.68	0.142	0.83	1.10	0.190	No
1010	61.38	3.75	0.98	2.77	0.65	0.240	1.68	0.142	0.82	1.10	0.190	No
1011	61.43	3.75	0.98	2.77	0.65	0.239	1.68	0.142	0.82	1.10	0.190	No
1012	61.48	3.76	0.98	2.77	0.65	0.239	1.68	0.142	0.82	1.10	0.190	No
1013	61.53	3.76	0.98	2.78	0.65	0.239	1.68	0.142	0.82	1.10	0.190	No
1014	61.56	3.76	0.98	2.78	0.65	0.239	1.68	0.142	0.82	1.10	0.190	No
1015	61.58	3.76	0.99	2.78	0.65	0.239	1.68	0.142	0.82	1.10	0.190	No
1016	61.59	3.76	0.99	2.78	0.65	0.239	1.68	0.142	0.82	1.10	0.190	No
1017	61.62	3.76	0.99	2.78	0.65	0.239	1.68	0.142	0.82	1.10	0.190	No
1018	61.63	3.77	0.99	2.78	0.65	0.239	1.68	0.142	0.82	1.10	0.190	No
1019	61.67	3.77	0.99	2.78	0.65	0.239	1.68	0.142	0.82	1.10	0.190	No
1020	61.71	3.77	0.99	2.78	0.65	0.239	1.68	0.142	0.82	1.10	0.190	No
1021	61.76	3.77	0.99	2.78	0.65	0.239	1.68	0.142	0.82	1.10	0.190	No
1022	61.81	3.78	0.99	2.79	0.64	0.239	1.68	0.142	0.82	1.10	0.189	No
1023	61.86	3.78	0.99	2.79	0.64	0.239	1.68	0.142	0.82	1.10	0.189	No
1024	61.87	3.78	0.99	2.79	0.64	0.239	1.68	0.142	0.82	1.10	0.189	No
1025	61.91	3.78	1.00	2.79	0.64	0.239	1.68	0.142	0.82	1.10	0.189	No
1026	61.95	3.79	1.00	2.79	0.64	0.239	1.68	0.142	0.82	1.10	0.189	No
1027	61.96	3.79	1.00	2.79	0.64	0.239	1.68	0.142	0.82	1.10	0.189	No
1028	62.00	3.79	1.00	2.79	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
1029	62.04	3.79	1.00	2.79	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
1030	62.06	3.79	1.00	2.79	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
1031	62.10	3.80	1.00	2.80	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
1032	62.14	3.80	1.00	2.80	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
1033	62.20	3.80	1.00	2.80	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
1034	62.22	3.80	1.01	2.80	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
1035	62.27	3.81	1.01	2.80	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
1036	62.29	3.81	1.01	2.80	0.64	0.238	1.68	0.141	0.82	1.10	0.189	No
1037	62.34	3.81	1.01	2.80	0.64	0.238	1.68	0.141	0.82	1.10	0.189	No
1038	62.39	3.82	1.01	2.81	0.64	0.238	1.68	0.141	0.82	1.10	0.189	No
1039	62.43	3.82	1.01	2.81	0.64	0.238	1.68	0.141	0.82	1.10	0.189	No
1040	62.49	3.82	1.01	2.81	0.64	0.238	1.68	0.141	0.82	1.10	0.189	No
1041	62.57	3.83	1.02	2.81	0.64	0.238	1.68	0.141	0.82	1.10	0.189	No
1042	62.68	3.84	1.02	2.82	0.64	0.237	1.68	0.141	0.82	1.10	0.189	No
1043	62.75	3.84	1.02	2.82	0.64	0.237	1.68	0.141	0.82	1.10	0.189	No
1044	62.87	3.85	1.03	2.82	0.64	0.237	1.68	0.141	0.82	1.10	0.189	No
1045	62.88	3.85	1.03	2.82	0.64	0.237	1.68	0.141	0.82	1.10	0.189	No
1046	62.89	3.85	1.03	2.82	0.64	0.237	1.68	0.141	0.82	1.10	0.189	No
1047	62.93	3.85	1.03	2.83	0.64	0.237	1.68	0.141	0.82	1.10	0.189	No
1048	62.98	3.86	1.03	2.83	0.64	0.237	1.68	0.141	0.82	1.10	0.189	No
1049	63.02	3.86	1.03	2.83	0.64	0.237	1.68	0.141	0.82	1.10	0.189	No
1050	63.07	3.86	1.03	2.83	0.64	0.237	1.68	0.141	0.82	1.10	0.188	No
1051	63.12	3.86	1.03	2.83	0.64	0.237	1.68	0.141	0.82	1.10	0.188	No
1052	63.14	3.86	1.03	2.83	0.64	0.237	1.68	0.141	0.82	1.10	0.188	No
1053	63.17	3.87	1.03	2.83	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
1054	63.17	3.87	1.04	2.83	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
1055	63.20	3.87	1.04	2.83	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
1056	63.21	3.87	1.04	2.83	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1057	63.23	3.87	1.04	2.83	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
1058	63.26	3.87	1.04	2.83	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
1059	63.28	3.87	1.04	2.83	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
1060	63.31	3.87	1.04	2.83	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
1061	63.32	3.87	1.04	2.83	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
1062	63.36	3.87	1.04	2.83	0.63	0.236	1.68	0.141	0.82	1.10	0.188	No
1063	63.40	3.88	1.04	2.83	0.63	0.236	1.68	0.141	0.82	1.10	0.188	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
σ_v: Total overburden pressure at test point (tsf)
u_0: Water pressure at test point (tsf)
σ_v': Effective overburden pressure based on GWT during earthquake (tsf)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.01	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
2	0.04	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
3	0.09	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
4	0.11	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
5	0.14	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
6	0.14	1.35	3.66	4.59	1.00	2.15	27.82	59.81	4.000	No	Yes	2.00
7	0.18	6.97	2.69	0.89	0.81	11.19	4.58	51.24	4.000	No	Yes	2.00
8	0.23	18.19	2.14	0.35	0.65	29.21	1.00	29.21	4.000	No	No	2.00
9	0.24	36.79	1.76	0.18	0.54	59.09	1.00	59.09	4.000	No	No	2.00
10	0.28	53.07	1.58	0.14	0.50	85.23	1.00	85.23	4.000	No	No	2.00
11	0.33	59.27	1.53	0.14	0.50	95.19	1.00	95.19	4.000	No	No	2.00
12	0.38	56.61	1.60	0.20	0.50	90.91	1.00	90.91	4.000	No	No	2.00
13	0.42	52.11	1.72	0.34	0.52	83.69	1.00	83.69	4.000	No	No	2.00
14	0.47	51.84	1.83	0.58	0.56	83.25	1.19	98.77	4.000	No	No	2.00
15	0.51	51.94	1.90	0.76	0.58	83.40	1.24	103.16	4.000	No	No	2.00
16	0.52	52.09	1.93	0.85	0.59	83.64	1.26	104.99	4.000	No	No	2.00
17	0.57	52.66	1.91	0.81	0.58	84.56	1.24	105.20	4.000	No	No	2.00
18	0.61	53.24	1.89	0.76	0.58	85.48	1.23	105.23	4.000	No	No	2.00
19	0.67	53.47	1.88	0.73	0.57	85.85	1.22	105.00	4.000	No	No	2.00
20	0.73	53.84	1.87	0.71	0.57	86.44	1.22	105.23	4.000	No	No	2.00
21	0.81	53.62	1.87	0.71	0.57	86.08	1.22	104.72	4.000	No	No	2.00
22	0.86	53.52	1.92	0.84	0.58	85.91	1.25	107.16	4.000	No	No	2.00
23	0.98	52.14	1.96	0.96	0.60	83.69	1.28	106.78	4.000	No	No	2.00
24	1.05	48.22	2.02	1.08	0.61	77.37	1.32	102.42	4.000	No	No	2.00
25	1.15	43.67	2.04	1.03	0.62	70.05	1.34	94.07	4.000	No	No	2.00
26	1.24	37.87	2.07	0.96	0.63	60.73	1.38	83.84	4.000	No	No	2.00
27	1.34	34.47	2.09	0.89	0.63	55.26	1.40	77.37	4.000	No	No	2.00
28	1.43	30.63	2.16	0.99	0.65	49.08	1.51	74.33	4.000	No	No	2.00
29	1.53	26.86	2.25	1.20	0.68	43.01	1.75	75.37	4.000	No	No	2.00
30	1.58	24.56	2.31	1.36	0.70	39.32	1.98	77.68	4.000	No	No	2.00
31	1.62	23.48	2.32	1.31	0.70	37.59	2.00	75.15	4.000	No	No	2.00
32	1.67	24.36	2.28	1.18	0.69	38.99	1.85	72.19	4.000	No	No	2.00
33	1.75	23.89	2.28	1.15	0.69	38.23	1.86	70.99	4.000	No	No	2.00
34	1.77	23.08	2.30	1.17	0.70	36.93	1.92	70.79	4.000	No	No	2.00
35	1.81	21.50	2.34	1.25	0.71	34.38	2.08	71.55	4.000	No	No	2.00
36	1.86	19.71	2.39	1.32	0.72	31.51	2.30	72.37	4.000	No	No	2.00
37	1.91	17.96	2.43	1.37	0.74	28.69	2.52	72.24	4.000	No	No	2.00
38	1.95	16.98	2.43	1.26	0.74	27.11	2.53	68.54	4.000	No	No	2.00
39	2.00	16.21	2.41	1.09	0.73	25.86	2.43	62.85	4.000	No	No	2.00
40	2.05	14.89	2.41	0.93	0.73	23.75	2.42	57.52	4.000	Yes	No	2.00
41	2.11	13.51	2.43	0.88	0.74	21.52	2.55	54.95	4.000	Yes	No	2.00
42	2.20	12.33	2.47	0.89	0.75	19.62	2.79	54.76	4.000	Yes	No	2.00
43	2.24	11.73	2.50	0.95	0.76	18.64	3.01	56.15	4.000	Yes	No	2.00
44	2.29	11.26	2.54	1.06	0.77	17.88	3.29	58.85	4.000	Yes	No	2.00
45	2.34	11.32	2.60	1.39	0.79	17.99	3.76	67.59	4.000	Yes	Yes	2.00
46	2.44	12.17	2.61	1.64	0.79	19.33	3.86	74.63	4.000	Yes	Yes	2.00
47	2.48	14.56	2.56	1.73	0.78	23.17	3.43	79.44	4.000	Yes	No	2.00
48	2.58	18.03	2.47	1.60	0.75	28.74	2.75	79.05	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	2.63	22.41	2.37	1.48	0.72	35.77	2.21	79.01	4.000	Yes	No	2.00
50	2.71	26.08	2.30	1.39	0.70	41.66	1.92	80.03	4.000	Yes	No	2.00
51	2.78	30.33	2.22	1.27	0.67	48.48	1.67	80.89	4.000	Yes	No	2.00
52	2.82	33.73	2.16	1.16	0.66	53.95	1.52	82.21	4.000	Yes	No	2.00
53	2.89	34.94	2.13	1.09	0.65	55.89	1.47	82.24	4.000	Yes	No	2.00
54	2.96	33.63	2.16	1.13	0.65	53.77	1.51	81.39	4.000	No	No	2.00
55	3.03	30.90	2.20	1.21	0.67	49.37	1.62	80.00	4.000	No	No	2.00
56	3.11	28.98	2.23	1.23	0.68	46.28	1.70	78.46	4.000	No	No	2.00
57	3.19	26.45	2.26	1.23	0.69	42.22	1.79	75.65	4.000	No	No	2.00
58	3.25	23.52	2.31	1.27	0.70	37.50	1.97	73.87	4.000	No	No	2.00
59	3.35	20.49	2.38	1.38	0.72	32.62	2.28	74.42	4.000	No	No	2.00
60	3.41	17.79	2.44	1.42	0.74	28.29	2.60	73.49	4.000	No	No	2.00
61	3.50	15.91	2.46	1.31	0.75	25.25	2.74	69.10	4.000	No	No	2.00
62	3.59	14.83	2.45	1.11	0.74	23.51	2.66	62.63	4.000	No	No	2.00
63	3.69	14.59	2.43	0.99	0.74	23.12	2.55	58.90	4.000	No	No	2.00
64	3.79	15.20	2.39	0.89	0.73	24.09	2.35	56.48	4.000	No	No	2.00
65	3.88	16.54	2.34	0.81	0.71	26.24	2.09	54.78	4.000	No	No	2.00
66	3.97	19.14	2.27	0.75	0.69	30.40	1.82	55.25	4.000	No	No	2.00
67	4.07	20.82	2.26	0.82	0.68	33.10	1.77	58.69	4.000	No	No	2.00
68	4.14	23.49	2.22	0.86	0.67	37.37	1.67	62.38	4.000	No	No	2.00
69	4.17	25.51	2.20	0.89	0.67	40.62	1.61	65.25	4.000	No	No	2.00
70	4.26	28.14	2.15	0.86	0.65	44.83	1.51	67.83	4.000	No	No	2.00
71	4.32	28.71	2.16	0.90	0.66	45.74	1.52	69.43	4.000	No	No	2.00
72	4.37	28.10	2.18	0.95	0.66	44.77	1.56	69.94	4.000	No	No	2.00
73	4.42	26.62	2.21	1.02	0.67	42.38	1.65	69.93	4.000	No	No	2.00
74	4.51	25.07	2.24	1.05	0.68	39.88	1.74	69.30	4.000	No	No	2.00
75	4.61	23.68	2.27	1.07	0.69	37.65	1.82	68.42	4.000	No	No	2.00
76	4.65	22.37	2.29	1.08	0.70	35.53	1.90	67.38	4.000	No	No	2.00
77	4.74	21.09	2.32	1.11	0.70	33.47	2.00	67.06	4.000	No	No	2.00
78	4.80	20.48	2.33	1.11	0.71	32.49	2.05	66.55	4.000	No	No	2.00
79	4.89	20.04	2.34	1.12	0.71	31.78	2.09	66.46	4.000	No	No	2.00
80	4.95	20.38	2.33	1.10	0.71	32.32	2.05	66.20	4.000	No	No	2.00
81	5.04	21.05	2.31	1.07	0.70	33.39	1.97	65.92	4.000	No	No	2.00
82	5.13	22.81	2.27	0.99	0.69	36.20	1.80	65.26	4.000	No	No	2.00
83	5.18	25.27	2.20	0.90	0.67	40.14	1.63	65.28	4.000	No	No	2.00
84	5.28	28.07	2.14	0.82	0.65	44.63	1.49	66.64	4.000	No	No	2.00
85	5.32	31.47	2.09	0.76	0.63	50.09	1.40	70.04	4.000	No	No	2.00
86	5.42	34.67	2.05	0.75	0.62	55.23	1.35	74.62	4.000	No	No	2.00
87	5.51	38.14	2.01	0.74	0.61	60.80	1.31	79.86	4.000	No	No	2.00
88	5.60	41.28	1.94	0.63	0.59	65.83	1.26	83.18	4.000	No	No	2.00
89	5.66	44.24	1.88	0.53	0.57	70.58	1.22	86.14	4.000	No	No	2.00
90	5.76	45.86	1.83	0.46	0.56	73.17	1.00	73.17	4.000	No	No	2.00
91	5.85	44.91	1.86	0.50	0.57	71.65	1.21	86.53	4.000	No	No	2.00
92	5.92	41.11	1.92	0.56	0.58	65.53	1.25	81.79	4.000	No	No	2.00
93	5.95	38.21	1.96	0.61	0.60	60.87	1.28	77.76	4.000	No	No	2.00
94	5.97	36.15	1.99	0.64	0.61	57.56	1.30	74.97	4.000	No	No	2.00
95	6.02	35.37	2.01	0.65	0.61	56.31	1.31	73.90	4.000	Yes	No	2.00
96	6.06	32.74	2.05	0.70	0.62	52.08	1.36	70.59	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	6.16	29.98	2.10	0.76	0.64	47.63	1.42	67.87	4.000	Yes	No	2.00
98	6.21	26.98	2.18	0.88	0.66	42.82	1.56	66.83	4.000	Yes	No	2.00
99	6.26	24.29	2.26	1.07	0.69	38.48	1.79	68.74	4.000	Yes	No	2.00
100	6.31	21.62	2.36	1.35	0.72	34.19	2.18	74.63	4.000	Yes	No	2.00
101	6.40	19.23	2.46	1.68	0.75	30.34	2.70	82.06	4.000	Yes	No	2.00
102	6.44	16.91	2.56	2.09	0.78	26.60	3.43	91.18	4.000	Yes	No	2.00
103	6.52	15.12	2.64	2.48	0.80	23.73	4.16	98.65	4.000	Yes	Yes	2.00
104	6.57	13.47	2.73	2.91	0.83	21.08	5.01	105.63	4.000	Yes	Yes	2.00
105	6.64	12.16	2.80	3.29	0.85	18.96	5.81	110.19	4.000	Yes	Yes	2.00
106	6.69	10.98	2.86	3.65	0.87	17.06	6.65	113.46	4.000	Yes	Yes	2.00
107	6.78	10.34	2.90	3.84	0.88	16.02	7.15	114.49	4.000	Yes	Yes	2.00
108	6.83	9.90	2.91	3.84	0.88	15.31	7.38	112.96	4.000	Yes	Yes	2.00
109	6.92	9.60	2.92	3.75	0.88	14.82	7.45	110.37	4.000	No	Yes	2.00
110	6.97	9.39	2.91	3.59	0.88	14.48	7.39	107.07	4.000	No	Yes	2.00
111	7.03	9.29	2.91	3.50	0.88	14.32	7.35	105.27	4.000	No	Yes	2.00
112	7.12	9.32	2.90	3.42	0.88	14.36	7.25	104.07	4.000	No	Yes	2.00
113	7.22	9.39	2.90	3.38	0.88	14.46	7.17	103.64	4.000	No	Yes	2.00
114	7.27	9.52	2.89	3.37	0.88	14.66	7.09	103.89	4.000	No	Yes	2.00
115	7.36	9.65	2.89	3.41	0.87	14.86	7.06	104.93	4.000	No	Yes	2.00
116	7.43	9.75	2.89	3.48	0.88	15.01	7.08	106.34	4.000	No	Yes	2.00
117	7.50	9.78	2.90	3.56	0.88	15.06	7.16	107.82	4.000	No	Yes	2.00
118	7.59	9.77	2.90	3.61	0.88	15.04	7.22	108.69	4.000	No	Yes	2.00
119	7.64	9.70	2.91	3.69	0.88	14.93	7.34	109.64	4.000	No	Yes	2.00
120	7.75	9.63	2.92	3.75	0.88	14.81	7.46	110.40	4.000	No	Yes	2.00
121	7.79	9.70	2.92	3.76	0.88	14.91	7.43	110.74	4.000	No	Yes	2.00
122	7.89	9.97	2.90	3.67	0.88	15.33	7.19	110.22	4.000	No	Yes	2.00
123	7.99	10.24	2.88	3.59	0.87	15.76	6.97	109.89	4.000	No	Yes	2.00
124	8.04	10.34	2.88	3.62	0.87	15.91	6.96	110.71	4.000	No	Yes	2.00
125	8.13	10.31	2.89	3.67	0.87	15.85	7.03	111.39	4.000	No	Yes	2.00
126	8.23	10.27	2.84	3.03	0.86	15.79	6.35	100.23	4.000	No	Yes	2.00
127	8.32	10.27	2.79	2.55	0.85	15.77	5.78	91.18	4.000	No	Yes	2.00
128	8.37	10.53	2.76	2.28	0.84	16.20	5.34	86.47	4.000	No	Yes	2.00
129	8.46	11.04	2.79	2.79	0.85	17.00	5.74	97.61	4.000	No	Yes	2.00
130	8.56	11.30	2.82	3.16	0.85	17.42	6.05	105.35	4.000	No	Yes	2.00
131	8.59	11.30	2.84	3.44	0.86	17.41	6.35	110.51	4.000	No	Yes	2.00
132	8.61	11.03	2.87	3.69	0.87	16.97	6.71	113.97	4.000	No	Yes	2.00
133	8.67	10.89	2.88	3.88	0.87	16.75	6.98	116.82	4.000	No	Yes	2.00
134	8.71	10.69	2.90	4.05	0.88	16.41	7.24	118.78	4.000	No	Yes	2.00
135	8.72	10.51	2.92	4.18	0.88	16.13	7.46	120.30	4.000	No	Yes	2.00
136	8.78	10.44	2.92	4.25	0.89	16.02	7.56	121.13	4.000	No	Yes	2.00
137	8.80	10.44	2.93	4.28	0.89	16.02	7.59	121.54	4.000	No	Yes	2.00
138	8.86	10.44	2.93	4.29	0.89	16.01	7.60	121.62	4.000	No	Yes	2.00
139	8.90	10.55	2.92	4.29	0.88	16.17	7.55	122.08	4.000	No	Yes	2.00
140	8.95	10.68	2.92	4.30	0.88	16.39	7.49	122.77	4.000	No	Yes	2.00
141	8.96	10.89	2.91	4.30	0.88	16.71	7.39	123.54	4.000	No	Yes	2.00
142	9.00	11.05	2.91	4.31	0.88	16.98	7.33	124.43	4.000	No	Yes	2.00
143	9.05	11.29	2.90	4.33	0.88	17.35	7.24	125.55	4.000	No	Yes	2.00
144	9.09	11.56	2.89	4.31	0.88	17.78	7.10	126.26	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	9.10	11.96	2.88	4.27	0.87	18.43	6.89	127.03	4.000	No	Yes	2.00
146	9.14	12.47	2.86	4.24	0.87	19.24	6.66	128.15	4.000	No	Yes	2.00
147	9.20	13.21	2.84	4.16	0.86	20.42	6.33	129.23	4.000	No	Yes	2.00
148	9.24	14.09	2.81	4.06	0.85	21.83	5.95	129.98	4.000	No	Yes	2.00
149	9.29	15.03	2.78	3.93	0.84	23.34	5.57	129.97	4.000	No	Yes	2.00
150	9.31	15.90	2.75	3.85	0.83	24.74	5.28	130.54	4.000	No	Yes	2.00
151	9.38	16.61	2.73	3.79	0.83	25.88	5.06	130.87	4.000	Yes	Yes	2.00
152	9.41	17.32	2.71	3.66	0.82	27.00	4.80	129.53	4.000	Yes	Yes	2.00
153	9.47	18.02	2.68	3.45	0.81	28.13	4.48	126.15	4.000	Yes	Yes	2.00
154	9.53	19.33	2.62	3.03	0.79	30.23	3.91	118.10	4.000	Yes	Yes	2.00
155	9.62	21.08	2.54	2.58	0.77	33.03	3.29	108.83	4.000	Yes	No	2.00
156	9.67	23.71	2.45	2.07	0.74	36.88	2.63	97.08	4.000	Yes	No	2.00
157	9.77	26.25	2.37	1.72	0.72	39.96	2.22	88.55	4.000	Yes	No	2.00
158	9.81	28.83	2.29	1.42	0.70	43.12	1.89	81.52	4.000	Yes	No	2.00
159	9.90	30.67	2.24	1.23	0.68	45.16	1.72	77.57	4.000	Yes	No	2.00
160	9.97	32.26	2.20	1.11	0.67	46.92	1.61	75.55	4.000	Yes	No	2.00
161	10.06	32.63	2.20	1.11	0.67	47.13	1.61	75.67	4.000	No	No	2.00
162	10.20	32.13	2.22	1.20	0.68	46.19	1.68	77.59	4.000	Yes	No	2.00
163	10.30	29.29	2.26	1.22	0.69	42.06	1.79	75.15	4.000	Yes	No	2.00
164	10.44	25.52	2.33	1.34	0.71	36.67	2.06	75.52	4.000	Yes	No	2.00
165	10.54	20.70	2.45	1.61	0.74	30.03	2.66	79.87	4.000	Yes	No	2.00
166	10.63	16.56	2.64	2.51	0.80	24.49	4.08	99.92	4.000	Yes	Yes	2.00
167	10.74	13.83	2.78	3.48	0.84	20.66	5.64	116.62	4.000	Yes	Yes	2.00
168	10.78	12.62	2.86	4.22	0.87	18.99	6.71	127.39	4.000	Yes	Yes	2.00
169	10.83	12.48	2.88	4.44	0.87	18.76	6.96	130.59	4.000	Yes	Yes	2.00
170	10.88	12.31	2.90	4.63	0.88	18.47	7.21	133.16	4.000	Yes	Yes	2.00
171	10.89	12.15	2.92	4.89	0.88	18.24	7.50	136.86	4.000	Yes	Yes	2.00
172	10.97	12.25	2.93	5.04	0.89	18.30	7.62	139.36	4.000	No	Yes	2.00
173	11.02	12.48	2.93	5.14	0.89	18.59	7.62	141.70	4.000	No	Yes	2.00
174	11.07	12.79	2.92	5.12	0.88	18.96	7.51	142.37	4.000	No	Yes	2.00
175	11.11	13.06	2.91	5.11	0.88	19.28	7.42	143.00	4.000	No	Yes	2.00
176	11.16	13.39	2.91	5.09	0.88	19.70	7.30	143.71	4.000	No	Yes	2.00
177	11.21	13.76	2.90	5.09	0.88	20.15	7.19	144.81	4.000	No	Yes	2.00
178	11.26	14.14	2.89	5.11	0.88	20.62	7.10	146.37	4.000	No	Yes	2.00
179	11.30	14.37	2.89	5.20	0.88	20.90	7.10	148.42	4.000	No	Yes	2.00
180	11.36	14.54	2.90	5.29	0.88	21.07	7.14	150.43	4.000	No	Yes	2.00
181	11.40	14.68	2.90	5.36	0.88	21.19	7.17	151.92	4.000	No	Yes	2.00
182	11.45	14.81	2.90	5.40	0.88	21.32	7.18	152.97	4.000	No	Yes	2.00
183	11.50	15.04	2.89	5.41	0.88	21.57	7.12	153.64	4.000	No	Yes	2.00
184	11.55	15.31	2.89	5.41	0.88	21.86	7.06	154.44	4.000	No	Yes	2.00
185	11.60	15.85	2.88	5.35	0.87	22.53	6.88	155.07	4.000	No	Yes	2.00
186	11.66	16.56	2.86	5.25	0.87	23.39	6.63	155.14	4.000	No	Yes	2.00
187	11.74	17.40	2.84	5.06	0.86	24.38	6.31	153.92	4.000	No	Yes	2.00
188	11.84	17.98	2.82	4.98	0.86	24.97	6.15	153.46	4.000	No	Yes	2.00
189	11.93	18.18	2.82	5.03	0.86	25.08	6.17	154.65	4.000	No	Yes	2.00
190	12.04	18.04	2.84	5.23	0.86	24.73	6.38	157.76	4.000	No	Yes	2.00
191	12.13	17.87	2.86	5.42	0.87	24.37	6.58	160.42	4.000	No	Yes	2.00
192	12.22	17.67	2.87	5.55	0.87	23.94	6.76	161.87	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	12.27	17.51	2.88	5.59	0.87	23.64	6.85	161.93	4.000	No	Yes	2.00
194	12.37	17.27	2.88	5.64	0.87	23.16	6.98	161.58	4.000	No	Yes	2.00
195	12.41	17.17	2.89	5.65	0.87	22.94	7.03	161.26	4.000	No	Yes	2.00
196	12.51	17.06	2.89	5.71	0.88	22.65	7.13	161.48	4.000	No	Yes	2.00
197	12.56	17.23	2.89	5.68	0.88	22.78	7.08	161.37	4.000	No	Yes	2.00
198	12.65	17.64	2.88	5.61	0.87	23.15	6.96	161.03	4.000	No	Yes	2.00
199	12.71	18.45	2.86	5.51	0.87	24.09	6.70	161.44	4.000	No	Yes	2.00
200	12.79	19.23	2.86	5.57	0.87	24.96	6.59	164.56	4.000	No	Yes	2.00
201	12.89	20.10	2.85	5.67	0.86	25.92	6.50	168.54	4.000	No	Yes	2.00
202	12.96	20.98	2.84	5.80	0.86	26.96	6.43	173.33	4.000	No	Yes	2.00
203	13.04	22.23	2.82	5.70	0.86	28.37	6.15	174.57	4.000	Yes	Yes	2.00
204	13.13	24.11	2.78	5.33	0.84	30.49	5.62	171.40	4.000	Yes	Yes	2.00
205	13.23	26.80	2.65	3.76	0.80	33.27	4.19	139.58	4.000	Yes	Yes	2.00
206	13.30	30.34	2.49	2.43	0.76	36.95	2.91	107.47	4.000	Yes	No	2.00
207	13.37	34.15	2.32	1.49	0.70	40.77	2.02	82.17	4.000	Yes	No	2.00
208	13.47	38.32	2.29	1.49	0.69	45.44	1.87	85.15	4.000	Yes	No	2.00
209	13.57	38.79	2.31	1.62	0.70	45.84	1.94	89.15	4.000	No	No	2.00
210	13.61	39.19	2.31	1.69	0.70	46.27	1.98	91.39	4.000	No	No	2.00
211	13.62	40.31	2.30	1.69	0.70	47.52	1.94	92.31	4.000	No	No	2.00
212	13.68	44.31	2.26	1.59	0.69	51.92	1.78	92.36	4.000	No	No	2.00
213	13.73	47.82	2.22	1.53	0.68	55.76	1.68	93.57	4.000	No	No	2.00
214	13.77	50.08	2.21	1.55	0.67	58.23	1.65	95.79	4.000	No	No	2.00
215	13.87	52.91	2.20	1.55	0.67	61.16	1.61	98.26	4.000	No	No	2.00
216	13.93	55.78	2.19	1.58	0.66	64.26	1.58	101.41	4.000	No	No	2.00
217	14.00	58.54	2.17	1.60	0.66	67.15	1.55	104.21	4.000	No	No	2.00
218	14.06	60.62	2.17	1.63	0.66	69.33	1.54	106.89	4.000	No	No	2.00
219	14.12	62.21	2.17	1.67	0.66	70.95	1.54	109.37	4.000	No	No	2.00
220	14.21	63.05	2.17	1.71	0.66	71.63	1.55	111.13	4.000	No	No	2.00
221	14.25	63.45	2.18	1.75	0.66	71.96	1.56	112.44	4.000	No	No	2.00
222	14.35	63.35	2.18	1.78	0.66	71.51	1.58	112.67	4.000	No	No	2.00
223	14.45	62.61	2.19	1.80	0.67	70.37	1.60	112.38	4.000	No	No	2.00
224	14.50	61.06	2.21	1.83	0.67	68.50	1.63	111.75	4.000	No	No	2.00
225	14.59	59.18	2.22	1.87	0.68	66.15	1.68	111.04	4.000	No	No	2.00
226	14.64	57.19	2.24	1.92	0.68	63.82	1.73	110.49	4.000	No	No	2.00
227	14.74	55.60	2.26	1.95	0.69	61.79	1.78	110.08	4.000	No	No	2.00
228	14.80	54.22	2.27	1.99	0.69	60.12	1.83	109.86	4.000	No	No	2.00
229	14.88	53.18	2.28	2.02	0.69	58.73	1.87	109.70	4.000	No	No	2.00
230	14.97	52.24	2.30	2.05	0.70	57.45	1.91	109.62	4.000	No	No	2.00
231	15.05	51.43	2.31	2.08	0.70	56.38	1.95	110.04	4.000	No	No	2.00
232	15.13	50.85	2.32	2.12	0.70	55.53	1.99	110.56	4.000	No	No	2.00
233	15.21	50.95	2.32	2.12	0.70	55.42	1.99	110.46	4.000	No	No	2.00
234	15.28	52.23	2.30	2.06	0.70	56.58	1.93	109.48	4.000	No	No	2.00
235	15.36	55.10	2.27	1.95	0.69	59.37	1.82	108.07	4.000	No	No	2.00
236	15.41	60.22	2.22	1.78	0.67	64.61	1.66	107.30	4.000	No	No	2.00
237	15.50	66.38	2.16	1.62	0.66	70.74	1.53	108.00	4.000	No	No	2.00
238	15.55	72.78	2.07	1.31	0.63	77.07	1.38	106.45	4.000	No	No	2.00
239	15.65	76.92	2.00	1.07	0.61	80.83	1.31	105.71	4.000	No	No	2.00
240	15.71	78.17	1.94	0.88	0.59	81.68	1.27	103.43	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	15.79	75.07	1.96	0.89	0.60	78.22	1.28	99.99	4.000	Yes	No	2.00
242	15.89	67.29	2.02	0.97	0.61	69.97	1.33	92.88	4.000	Yes	No	2.00
243	15.90	61.09	2.07	1.04	0.63	63.58	1.38	88.03	4.000	Yes	No	2.00
244	15.94	56.21	2.12	1.11	0.64	58.47	1.45	84.99	4.000	Yes	No	2.00
245	16.00	53.24	2.15	1.16	0.65	55.28	1.51	83.45	4.000	Yes	No	2.00
246	16.06	47.68	2.22	1.30	0.67	49.45	1.67	82.65	4.000	Yes	No	2.00
247	16.14	40.74	2.32	1.56	0.71	42.17	2.02	85.02	4.000	Yes	No	2.00
248	16.19	34.10	2.43	1.87	0.74	35.24	2.56	90.26	4.000	Yes	No	2.00
249	16.26	27.10	2.57	2.32	0.78	27.88	3.51	97.89	4.000	Yes	No	2.00
250	16.33	21.54	2.70	2.80	0.82	22.01	4.74	104.24	4.000	Yes	Yes	2.00
251	16.38	17.06	2.83	3.31	0.86	17.28	6.24	107.80	4.000	Yes	Yes	2.00
252	16.47	14.43	2.93	3.75	0.89	14.45	7.58	109.50	4.000	Yes	Yes	2.00
253	16.54	12.64	3.00	4.14	1.00	12.69	8.71	110.54	4.000	Yes	Yes	2.00
254	16.62	11.80	3.05	4.58	1.00	11.71	9.67	113.31	4.000	No	Yes	2.00
255	16.70	11.53	3.08	4.88	1.00	11.36	10.18	115.66	4.000	No	Yes	2.00
256	16.76	12.28	3.06	4.98	1.00	12.12	9.88	119.66	4.000	No	Yes	2.00
257	16.86	14.88	2.96	4.36	1.00	14.80	8.08	119.59	4.000	Yes	Yes	2.00
258	16.90	19.33	2.82	3.59	0.85	19.15	6.07	116.24	4.000	Yes	Yes	2.00
259	16.98	25.84	2.65	2.82	0.80	25.69	4.22	108.51	4.000	Yes	Yes	2.00
260	17.05	35.42	2.48	2.18	0.75	35.23	2.81	99.11	4.000	Yes	No	2.00
261	17.14	47.54	2.30	1.68	0.70	47.19	1.94	91.71	4.000	Yes	No	2.00
262	17.20	61.48	2.15	1.32	0.65	60.90	1.51	91.88	4.000	Yes	No	2.00
263	17.29	73.03	2.05	1.11	0.62	72.03	1.35	97.56	4.000	Yes	No	2.00
264	17.34	81.99	1.99	1.01	0.60	80.70	1.30	104.58	4.000	Yes	No	2.00
265	17.44	86.87	1.97	1.01	0.60	85.21	1.28	109.31	4.000	No	No	2.00
266	17.50	88.89	1.93	0.91	0.59	86.96	1.26	109.36	4.000	No	No	2.00
267	17.58	88.15	1.91	0.82	0.58	85.91	1.24	106.78	4.000	No	No	2.00
268	17.64	85.02	1.90	0.75	0.58	82.63	1.24	102.13	4.000	No	No	2.00
269	17.75	80.50	1.95	0.85	0.59	77.97	1.27	99.12	4.000	No	No	2.00
270	17.82	72.08	2.04	1.03	0.62	69.66	1.35	93.80	4.000	No	No	2.00
271	17.89	66.02	2.11	1.19	0.64	63.60	1.43	91.18	4.000	No	No	2.00
272	17.89	62.68	2.15	1.30	0.65	60.37	1.51	91.04	4.000	No	No	2.00
273	17.96	64.06	2.15	1.31	0.65	61.55	1.50	92.30	4.000	No	No	2.00
274	18.02	65.34	2.15	1.35	0.65	62.67	1.51	94.33	4.000	No	No	2.00
275	18.07	66.86	2.15	1.39	0.65	64.01	1.51	96.43	4.000	No	No	2.00
276	18.17	68.78	2.14	1.40	0.65	65.62	1.49	98.02	4.000	No	No	2.00
277	18.22	68.74	2.15	1.43	0.65	65.47	1.51	98.54	4.000	Yes	No	2.00
278	18.30	65.20	2.19	1.53	0.66	61.85	1.59	98.20	4.000	Yes	No	2.00
279	18.36	57.69	2.27	1.79	0.69	54.52	1.83	99.83	4.000	Yes	No	2.00
280	18.42	49.20	2.39	2.19	0.72	46.28	2.30	106.36	4.000	Yes	No	2.00
281	18.50	39.97	2.53	2.80	0.77	37.31	3.16	118.00	4.000	Yes	No	2.00
282	18.56	32.38	2.66	3.50	0.81	29.97	4.32	129.55	4.000	Yes	Yes	2.00
283	18.62	25.71	2.80	4.24	0.85	23.53	5.80	136.40	4.000	Yes	Yes	2.00
284	18.69	23.96	2.82	4.26	0.85	21.78	6.13	133.60	4.000	Yes	Yes	2.00
285	18.76	22.21	2.86	4.37	0.87	20.05	6.60	132.24	4.000	Yes	Yes	2.00
286	18.84	24.30	2.80	4.02	0.85	21.95	5.90	129.41	4.000	Yes	Yes	2.00
287	18.89	31.88	2.66	3.30	0.80	29.04	4.26	123.66	4.000	Yes	Yes	2.00
288	18.98	52.85	2.37	2.20	0.72	48.61	2.23	108.20	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	19.05	78.42	2.16	1.65	0.66	72.48	1.52	110.23	4.000	Yes	No	2.00
290	19.12	101.80	2.02	1.36	0.61	94.21	1.32	124.65	4.000	Yes	No	2.00
291	19.18	115.88	1.95	1.24	0.59	107.18	1.27	136.09	4.000	Yes	No	2.00
292	19.24	124.07	1.91	1.18	0.58	114.61	1.25	142.72	4.000	Yes	No	2.00
293	19.32	126.76	1.90	1.17	0.58	116.83	1.24	144.84	4.000	No	No	2.00
294	19.38	126.53	1.92	1.21	0.58	116.38	1.25	145.16	4.000	No	No	2.00
295	19.46	124.81	1.94	1.27	0.59	114.42	1.26	144.25	4.000	No	No	2.00
296	19.54	122.62	1.96	1.34	0.60	112.08	1.28	142.92	4.000	No	No	2.00
297	19.62	121.00	1.97	1.38	0.60	110.26	1.28	141.68	4.000	No	No	2.00
298	19.70	119.99	1.98	1.40	0.60	109.01	1.29	140.65	4.000	No	No	2.00
299	19.80	119.75	1.98	1.39	0.60	108.41	1.29	140.01	4.000	No	No	2.00
300	19.85	119.75	1.98	1.39	0.60	108.23	1.29	139.71	4.000	No	No	2.00
301	19.94	119.95	1.98	1.40	0.60	108.07	1.29	139.71	4.000	No	No	2.00
302	20.03	120.73	1.96	1.31	0.60	108.50	1.28	138.61	4.000	No	No	2.00
303	20.13	121.84	1.94	1.23	0.59	109.19	1.26	137.92	4.000	No	No	2.00
304	20.19	123.33	1.91	1.14	0.58	110.40	1.25	137.60	4.000	No	No	2.00
305	20.29	124.05	1.92	1.16	0.58	110.67	1.25	138.32	4.000	No	No	2.00
306	20.39	124.51	1.93	1.18	0.59	110.70	1.25	138.76	4.000	No	No	2.00
307	20.43	124.14	1.93	1.21	0.59	110.23	1.26	138.70	4.000	No	No	2.00
308	20.47	124.09	1.94	1.23	0.59	109.99	1.26	138.78	4.000	No	No	2.00
309	20.52	123.97	1.95	1.26	0.59	109.69	1.27	139.06	4.000	No	No	2.00
310	20.61	123.97	1.96	1.30	0.59	109.33	1.27	139.29	4.000	No	No	2.00
311	20.66	123.26	1.97	1.34	0.60	108.48	1.28	139.08	4.000	No	No	2.00
312	20.71	122.22	1.98	1.36	0.60	107.35	1.29	138.34	4.000	No	No	2.00
313	20.77	121.00	1.99	1.39	0.60	106.04	1.30	137.35	4.000	No	No	2.00
314	20.85	120.53	1.99	1.40	0.60	105.33	1.30	136.79	4.000	No	No	2.00
315	20.91	120.63	1.99	1.40	0.61	105.23	1.30	136.74	4.000	No	No	2.00
316	21.00	121.00	1.99	1.40	0.61	105.23	1.30	136.71	4.000	No	No	2.00
317	21.05	120.93	1.99	1.40	0.61	105.01	1.30	136.53	4.000	No	No	2.00
318	21.11	120.50	2.00	1.41	0.61	104.40	1.30	136.06	4.000	No	No	2.00
319	21.19	120.16	2.00	1.42	0.61	103.82	1.31	135.66	4.000	No	No	2.00
320	21.24	120.23	2.00	1.43	0.61	103.70	1.31	135.67	4.000	No	No	2.00
321	21.34	120.39	2.00	1.43	0.61	103.52	1.31	135.57	4.000	No	No	2.00
322	21.39	119.99	2.01	1.44	0.61	103.00	1.31	135.16	4.000	No	No	2.00
323	21.48	118.68	2.01	1.45	0.61	101.52	1.32	133.84	4.000	No	No	2.00
324	21.53	116.39	2.02	1.47	0.61	99.34	1.33	131.86	4.000	No	No	2.00
325	21.64	113.86	2.03	1.47	0.62	96.79	1.34	129.36	4.000	No	No	2.00
326	21.72	111.80	2.02	1.38	0.61	94.83	1.33	125.65	4.000	No	No	2.00
327	21.81	110.79	2.00	1.27	0.61	93.80	1.31	122.48	4.000	No	No	2.00
328	21.89	110.52	1.97	1.15	0.60	93.48	1.28	120.09	4.000	No	No	2.00
329	21.97	110.69	1.96	1.11	0.60	93.44	1.28	119.40	4.000	No	No	2.00
330	22.05	110.81	1.96	1.09	0.60	93.32	1.27	118.94	4.000	No	No	2.00
331	22.12	110.92	1.95	1.07	0.59	93.25	1.27	118.64	4.000	No	No	2.00
332	22.13	110.89	1.95	1.07	0.59	93.20	1.27	118.54	4.000	No	No	2.00
333	22.18	111.98	1.95	1.06	0.59	94.01	1.27	119.22	4.000	No	No	2.00
334	22.22	114.49	1.93	1.04	0.59	96.10	1.26	121.02	4.000	No	No	2.00
335	22.28	118.47	1.91	1.01	0.58	99.41	1.25	123.90	4.000	No	No	2.00
336	22.33	122.55	1.90	0.98	0.58	102.85	1.23	126.89	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	22.38	126.36	1.88	0.96	0.57	106.02	1.22	129.64	4.000	No	No	2.00
338	22.41	129.99	1.86	0.93	0.57	109.11	1.21	132.05	4.000	No	No	2.00
339	22.51	133.16	1.85	0.91	0.56	111.59	1.20	133.67	4.000	No	No	2.00
340	22.56	135.86	1.83	0.88	0.56	113.83	1.18	134.77	4.000	No	No	2.00
341	22.61	137.68	1.82	0.85	0.55	115.29	1.17	135.13	4.000	No	No	2.00
342	22.65	139.23	1.81	0.82	0.55	116.56	1.16	135.07	4.000	No	No	2.00
343	22.71	140.30	1.79	0.80	0.55	117.38	1.15	134.57	4.000	No	No	2.00
344	22.76	141.15	1.78	0.77	0.54	118.01	1.13	133.54	4.000	No	No	2.00
345	22.85	141.55	1.77	0.74	0.54	118.16	1.12	132.33	4.000	No	No	2.00
346	22.89	141.79	1.77	0.72	0.54	118.28	1.11	131.19	4.000	No	No	2.00
347	22.99	141.85	1.76	0.71	0.54	118.07	1.10	130.38	4.000	No	No	2.00
348	23.04	142.19	1.76	0.71	0.54	118.24	1.10	129.89	4.000	No	No	2.00
349	23.12	143.24	1.75	0.70	0.53	118.92	1.09	129.72	4.000	No	No	2.00
350	23.18	145.12	1.75	0.69	0.53	120.36	1.08	129.86	4.000	No	No	2.00
351	23.24	147.55	1.74	0.69	0.53	122.28	1.07	130.48	4.000	No	No	2.00
352	23.33	150.28	1.73	0.68	0.53	124.35	1.05	131.06	4.000	No	No	2.00
353	23.38	152.77	1.73	0.68	0.53	126.31	1.04	131.98	4.000	No	No	2.00
354	23.47	154.92	1.72	0.68	0.53	127.86	1.04	132.70	4.000	No	No	2.00
355	23.52	155.87	1.73	0.70	0.53	128.46	1.05	134.34	4.000	No	No	2.00
356	23.61	155.50	1.74	0.72	0.53	127.76	1.06	136.02	4.000	No	No	2.00
357	23.68	153.41	1.76	0.76	0.54	125.65	1.10	137.67	4.000	No	No	2.00
358	23.76	149.87	1.78	0.79	0.54	122.29	1.13	137.84	4.000	No	No	2.00
359	23.83	145.42	1.80	0.83	0.55	118.19	1.16	136.72	4.000	No	No	2.00
360	23.90	140.77	1.83	0.87	0.56	113.95	1.18	134.56	4.000	No	No	2.00
361	23.97	136.02	1.85	0.91	0.56	109.66	1.20	131.87	4.000	No	No	2.00
362	24.05	130.36	1.88	0.95	0.57	104.58	1.22	128.11	4.000	No	No	2.00
363	24.10	123.83	1.92	1.01	0.58	98.86	1.25	123.41	4.000	No	No	2.00
364	24.19	116.14	1.96	1.08	0.60	92.13	1.28	117.58	4.000	No	No	2.00
365	24.27	109.37	2.00	1.15	0.61	86.22	1.31	112.54	4.000	No	No	2.00
366	24.34	103.31	2.03	1.21	0.62	80.98	1.34	108.37	4.000	No	No	2.00
367	24.43	99.26	2.06	1.26	0.63	77.39	1.37	105.81	4.000	No	No	2.00
368	24.48	95.99	2.09	1.32	0.63	74.54	1.40	104.29	4.000	No	No	2.00
369	24.57	93.77	2.11	1.39	0.64	72.46	1.43	103.72	4.000	No	No	2.00
370	24.62	91.81	2.12	1.39	0.64	70.77	1.45	102.28	4.000	No	No	2.00
371	24.72	90.33	2.12	1.39	0.65	69.37	1.46	101.12	4.000	No	No	2.00
372	24.81	89.08	2.13	1.39	0.65	68.17	1.47	100.03	4.000	No	No	2.00
373	24.86	87.96	2.15	1.46	0.65	67.09	1.50	100.81	4.000	No	No	2.00
374	24.95	85.18	2.18	1.55	0.66	64.60	1.56	100.88	4.000	No	No	2.00
375	25.01	82.83	2.20	1.62	0.67	62.55	1.62	101.05	4.000	No	No	2.00
376	25.02	81.04	2.22	1.66	0.67	61.07	1.66	101.09	4.000	No	No	2.00
377	25.05	81.81	2.21	1.65	0.67	61.63	1.64	101.34	4.000	No	No	2.00
378	25.11	82.33	2.21	1.65	0.67	61.92	1.64	101.59	4.000	No	No	2.00
379	25.15	82.53	2.21	1.66	0.67	61.99	1.64	101.87	4.000	No	No	2.00
380	25.21	81.92	2.22	1.68	0.67	61.38	1.66	101.94	4.000	No	No	2.00
381	25.25	81.07	2.23	1.70	0.68	60.61	1.68	101.90	4.000	No	No	2.00
382	25.30	79.78	2.23	1.71	0.68	59.50	1.70	101.32	4.000	No	No	2.00
383	25.40	78.02	2.24	1.71	0.68	57.95	1.73	100.17	4.000	No	No	2.00
384	25.45	75.14	2.25	1.71	0.68	55.63	1.77	98.38	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	25.52	71.36	2.27	1.71	0.69	52.56	1.83	96.28	4.000	Yes	No	2.00
386	25.60	65.60	2.32	1.78	0.70	47.92	1.99	95.12	4.000	Yes	No	2.00
387	25.66	58.89	2.37	1.90	0.72	42.57	2.24	95.48	4.000	Yes	No	2.00
388	25.74	50.63	2.47	2.18	0.75	36.01	2.77	99.69	4.000	Yes	No	2.00
389	25.80	42.60	2.57	2.54	0.78	29.74	3.54	105.15	4.000	Yes	No	2.00
390	25.88	34.42	2.71	3.09	0.82	23.44	4.79	112.31	4.000	Yes	Yes	2.00
391	25.94	27.91	2.84	3.70	0.86	18.51	6.33	117.20	4.000	Yes	Yes	2.00
392	26.02	22.69	2.98	4.41	1.00	14.10	8.40	118.43	4.000	Yes	Yes	2.00
393	26.09	19.19	3.07	4.99	1.00	11.73	10.09	118.41	4.000	No	Yes	2.00
394	26.17	16.36	3.16	5.56	1.00	9.82	11.90	116.89	4.000	No	Yes	2.00
395	26.23	14.50	3.23	6.07	1.00	8.57	13.49	115.61	4.000	No	Yes	2.00
396	26.29	13.56	3.28	6.45	1.00	7.93	14.54	115.33	4.000	No	Yes	2.00
397	26.37	13.73	3.27	6.48	1.00	8.01	14.49	116.10	4.000	No	Yes	2.00
398	26.46	14.95	3.23	6.22	1.00	8.78	13.45	118.10	4.000	No	Yes	2.00
399	26.55	16.56	3.18	5.88	1.00	9.80	12.25	120.00	4.000	No	Yes	2.00
400	26.60	18.04	3.14	5.67	1.00	10.74	11.37	122.14	4.000	No	Yes	2.00
401	26.70	18.79	3.12	5.69	1.00	11.18	11.11	124.24	4.000	No	Yes	2.00
402	26.78	19.09	3.12	5.78	1.00	11.34	11.11	125.96	4.000	No	Yes	2.00
403	26.87	19.16	3.10	5.28	1.00	11.34	10.61	120.33	4.000	No	Yes	2.00
404	26.94	19.06	3.05	4.41	1.00	11.25	9.74	109.55	4.000	No	Yes	2.00
405	27.03	18.62	3.03	3.81	1.00	10.92	9.23	100.80	4.000	No	Yes	2.00
406	27.13	17.84	3.05	3.86	1.00	10.38	9.61	99.83	4.000	No	Yes	2.00
407	27.18	15.89	3.14	4.63	1.00	9.12	11.41	104.10	4.000	No	Yes	2.00
408	27.27	14.61	3.20	5.14	1.00	8.27	12.75	105.48	4.000	No	Yes	2.00
409	27.32	14.00	3.23	5.49	1.00	7.87	13.55	106.67	4.000	No	Yes	2.00
410	27.37	14.68	3.21	5.36	1.00	8.28	12.99	107.59	4.000	No	Yes	2.00
411	27.41	15.01	3.20	5.40	1.00	8.48	12.84	108.89	4.000	No	Yes	2.00
412	27.46	15.01	3.21	5.56	1.00	8.47	13.04	110.36	4.000	No	Yes	2.00
413	27.51	15.19	3.22	5.71	1.00	8.56	13.12	112.25	4.000	No	Yes	2.00
414	27.61	15.69	3.21	5.85	1.00	8.84	13.00	114.96	4.000	No	Yes	2.00
415	27.66	16.81	3.20	6.07	1.00	9.52	12.66	120.53	4.000	No	Yes	2.00
416	27.73	19.30	3.15	6.09	1.00	11.05	11.59	128.02	4.000	No	Yes	2.00
417	27.80	22.77	3.09	6.16	1.00	13.18	10.46	137.91	4.000	No	Yes	2.00
418	27.88	26.51	3.05	6.33	1.00	15.46	9.62	148.75	4.000	No	Yes	2.00
419	27.96	28.73	3.04	6.73	1.00	16.78	9.46	158.82	4.000	No	Yes	2.00
420	28.04	29.44	3.06	7.42	1.00	17.16	9.86	169.19	4.000	No	Yes	2.00
421	28.12	29.30	3.09	8.01	1.00	17.02	10.34	175.99	4.000	No	Yes	2.00
422	28.18	29.78	3.09	8.32	1.00	17.27	10.47	180.83	4.000	No	Yes	2.00
423	28.27	30.99	3.07	8.13	1.00	17.95	10.11	181.45	4.000	No	Yes	2.00
424	28.32	32.84	3.04	7.81	1.00	19.04	9.54	181.70	4.000	No	Yes	2.00
425	28.42	34.90	3.01	7.49	1.00	20.22	8.98	181.66	4.000	No	Yes	2.00
426	28.47	37.02	2.99	7.35	1.00	21.47	8.57	183.98	4.000	No	Yes	2.00
427	28.61	38.87	2.97	7.32	1.00	22.47	8.32	186.93	4.000	No	Yes	2.00
428	28.67	40.79	2.96	7.36	1.00	23.57	8.10	190.99	4.000	Yes	Yes	2.00
429	28.75	43.62	2.91	7.10	0.88	26.58	7.37	195.90	4.000	Yes	Yes	2.00
430	28.81	49.52	2.83	6.35	0.86	30.58	6.28	192.19	4.000	Yes	Yes	2.00
431	28.90	59.16	2.72	5.28	0.82	37.21	4.89	181.92	4.000	Yes	Yes	2.00
432	29.00	70.68	2.60	4.38	0.79	45.27	3.75	169.71	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	29.05	82.68	2.50	3.72	0.76	53.82	2.95	158.84	4.000	Yes	No	2.00
434	29.10	92.58	2.42	3.28	0.73	60.99	2.48	151.03	4.000	Yes	No	2.00
435	29.15	101.07	2.35	2.88	0.71	67.24	2.13	143.11	4.000	Yes	No	2.00
436	29.24	105.88	2.30	2.58	0.70	70.82	1.92	136.02	4.000	Yes	No	2.00
437	29.29	107.45	2.26	2.31	0.69	72.19	1.78	128.66	4.000	Yes	No	2.00
438	29.37	106.66	2.23	2.12	0.68	71.76	1.71	122.57	4.000	Yes	No	2.00
439	29.43	105.44	2.21	1.94	0.67	71.05	1.64	116.77	4.000	Yes	No	2.00
440	29.53	104.90	2.19	1.79	0.66	70.72	1.59	112.38	4.000	No	No	2.00
441	29.62	104.73	2.17	1.69	0.66	70.61	1.55	109.62	4.000	No	No	2.00
442	29.68	104.75	2.15	1.58	0.65	70.73	1.51	106.89	4.000	No	No	2.00
443	29.80	104.42	2.15	1.54	0.65	70.36	1.50	105.63	4.000	No	No	2.00
444	29.91	103.80	2.15	1.52	0.65	69.74	1.50	104.61	4.000	No	No	2.00
445	30.00	99.10	2.19	1.66	0.66	65.97	1.59	104.86	0.187	No	No	1.03
446	30.07	97.42	2.21	1.72	0.67	64.55	1.63	105.36	0.189	No	No	1.04
447	30.15	96.27	2.22	1.75	0.67	63.56	1.66	105.54	0.189	No	No	1.04
448	30.21	99.04	2.20	1.70	0.67	65.49	1.62	105.77	0.190	No	No	1.04
449	30.26	98.71	2.20	1.71	0.67	65.16	1.62	105.66	0.190	No	No	1.04
450	30.31	97.50	2.21	1.73	0.67	64.21	1.64	105.39	0.189	No	No	1.03
451	30.38	95.52	2.22	1.75	0.67	62.65	1.67	104.86	0.187	No	No	1.02
452	30.45	92.62	2.24	1.79	0.68	60.44	1.72	104.23	0.185	No	No	1.01
453	30.50	89.12	2.26	1.84	0.69	57.84	1.79	103.72	0.184	No	No	1.00
454	30.55	84.94	2.29	1.88	0.69	54.79	1.88	102.88	0.181	No	No	0.99
455	30.64	81.19	2.31	1.91	0.70	52.03	1.96	101.83	0.178	No	No	0.97
456	30.70	77.93	2.32	1.91	0.70	49.71	2.01	100.16	0.173	No	No	0.94
457	30.79	76.04	2.33	1.90	0.71	48.30	2.05	98.96	0.170	No	No	0.93
458	30.84	75.47	2.33	1.88	0.71	47.86	2.05	98.19	0.168	No	No	0.91
459	30.93	76.95	2.32	1.86	0.70	48.79	2.01	98.05	0.168	No	No	0.91
460	30.98	80.15	2.30	1.81	0.70	50.98	1.93	98.14	0.168	No	No	0.91
461	31.05	85.34	2.27	1.76	0.69	54.54	1.81	98.98	0.170	No	No	0.92
462	31.13	91.57	2.24	1.70	0.68	58.82	1.71	100.51	0.174	No	No	0.94
463	31.17	100.46	2.19	1.61	0.66	65.08	1.58	102.97	0.182	No	No	0.98
464	31.27	110.94	2.13	1.49	0.65	72.52	1.47	106.25	0.192	No	No	1.03
465	31.32	123.23	2.06	1.34	0.63	81.52	1.37	111.37	0.208	No	No	1.13
466	31.41	133.45	2.00	1.21	0.61	89.03	1.31	116.56	0.227	No	No	1.23
467	31.46	140.90	1.96	1.11	0.60	94.67	1.28	120.72	0.244	No	No	1.31
468	31.52	144.37	1.93	1.03	0.59	97.40	1.26	122.24	0.250	No	No	1.35
469	31.61	145.01	1.91	0.97	0.58	97.95	1.24	121.83	0.248	No	No	1.33
470	31.66	142.15	1.91	0.95	0.58	95.90	1.24	119.20	0.238	No	No	1.28
471	31.75	136.69	1.93	0.97	0.59	91.66	1.26	115.29	0.223	No	No	1.19
472	31.80	129.14	1.98	1.06	0.60	85.76	1.29	110.68	0.206	No	No	1.11
473	31.90	122.00	2.02	1.16	0.62	80.16	1.33	106.52	0.192	No	No	1.03
474	31.94	116.84	2.06	1.24	0.63	76.18	1.37	104.07	0.185	No	No	0.99
475	32.04	116.03	2.07	1.27	0.63	75.33	1.38	104.00	0.185	No	No	0.99
476	32.09	119.17	2.08	1.34	0.63	77.25	1.39	107.23	0.195	No	No	1.04
477	32.20	118.70	2.11	1.46	0.64	76.38	1.43	109.06	0.201	No	No	1.07
478	32.24	117.72	2.13	1.56	0.65	75.37	1.47	110.44	0.205	No	No	1.09
479	32.28	114.69	2.15	1.64	0.65	73.02	1.51	110.26	0.205	No	No	1.09
480	32.29	116.70	2.14	1.62	0.65	74.43	1.49	111.09	0.207	No	No	1.11

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	32.30	118.93	2.13	1.60	0.65	75.98	1.47	112.06	0.211	No	No	1.12
482	32.40	120.51	2.13	1.59	0.65	76.91	1.47	112.71	0.213	No	No	1.13
483	32.45	120.48	2.13	1.61	0.65	76.77	1.47	112.95	0.214	No	No	1.14
484	32.55	119.13	2.14	1.63	0.65	75.61	1.49	112.51	0.212	No	No	1.13
485	32.59	118.33	2.15	1.66	0.65	74.91	1.50	112.50	0.212	No	No	1.13
486	32.69	118.13	2.15	1.68	0.65	74.54	1.51	112.79	0.213	No	No	1.13
487	32.76	118.09	2.16	1.72	0.66	74.31	1.53	113.51	0.216	No	No	1.14
488	32.84	118.40	2.17	1.75	0.66	74.31	1.54	114.35	0.219	No	No	1.16
489	32.90	119.00	2.17	1.77	0.66	74.55	1.55	115.19	0.222	No	No	1.17
490	32.98	119.95	2.17	1.78	0.66	75.02	1.54	115.83	0.225	No	No	1.19
491	33.06	121.02	2.17	1.78	0.66	75.61	1.54	116.33	0.226	No	No	1.19
492	33.12	122.10	2.16	1.78	0.66	76.23	1.53	116.77	0.228	No	No	1.20
493	33.22	122.84	2.16	1.78	0.66	76.56	1.53	117.03	0.229	No	No	1.21
494	33.31	123.21	2.16	1.78	0.66	76.64	1.53	117.14	0.229	No	No	1.21
495	33.37	123.28	2.16	1.78	0.66	76.59	1.53	117.11	0.229	No	No	1.21
496	33.46	123.28	2.16	1.78	0.66	76.41	1.53	117.00	0.229	No	No	1.20
497	33.55	123.18	2.17	1.79	0.66	76.17	1.54	117.00	0.229	No	No	1.20
498	33.65	122.98	2.17	1.80	0.66	75.83	1.54	117.07	0.229	No	No	1.20
499	33.70	122.57	2.17	1.82	0.66	75.42	1.55	117.18	0.230	No	No	1.20
500	33.79	122.03	2.18	1.84	0.66	74.86	1.56	117.10	0.229	No	No	1.20
501	33.89	121.09	2.18	1.85	0.66	74.04	1.58	116.76	0.228	No	No	1.19
502	33.99	119.77	2.19	1.86	0.67	72.98	1.59	116.20	0.226	No	No	1.18
503	34.04	117.79	2.20	1.88	0.67	71.55	1.61	115.43	0.223	No	No	1.16
504	34.13	115.49	2.21	1.89	0.67	69.85	1.64	114.59	0.220	No	No	1.15
505	34.23	112.70	2.22	1.92	0.68	67.80	1.68	113.76	0.217	No	No	1.13
506	34.32	110.27	2.24	1.95	0.68	66.01	1.71	113.20	0.215	No	No	1.12
507	34.37	108.22	2.25	1.98	0.68	64.55	1.75	112.84	0.214	No	No	1.11
508	34.47	106.60	2.26	2.00	0.69	63.31	1.78	112.69	0.213	No	No	1.11
509	34.55	103.47	2.28	2.07	0.69	61.05	1.85	112.96	4.000	Yes	No	2.00
510	34.63	96.66	2.33	2.24	0.71	56.31	2.04	114.64	4.000	Yes	No	2.00
511	34.73	86.37	2.40	2.51	0.73	49.33	2.40	118.21	4.000	Yes	No	2.00
512	34.80	72.76	2.51	2.91	0.76	40.42	3.06	123.59	4.000	Yes	No	2.00
513	34.90	60.46	2.62	3.30	0.79	32.62	3.90	127.28	4.000	Yes	Yes	2.00
514	35.00	54.92	2.64	3.21	0.80	29.29	4.16	121.79	3.600	No	Yes	2.00
515	35.12	50.37	2.67	3.15	0.81	26.54	4.42	117.31	3.600	No	Yes	2.00
516	35.20	52.86	2.63	2.87	0.80	28.11	3.99	112.19	3.600	No	Yes	2.00
517	35.33	53.65	2.63	2.95	0.80	28.43	4.02	114.42	4.000	Yes	Yes	2.00
518	35.41	63.41	2.53	2.60	0.77	34.44	3.20	110.34	4.000	Yes	No	2.00
519	35.44	68.58	2.48	2.43	0.75	37.68	2.87	108.02	4.000	Yes	No	2.00
520	35.48	76.82	2.41	2.17	0.73	42.96	2.42	103.82	4.000	Yes	No	2.00
521	35.57	84.09	2.35	1.98	0.71	47.63	2.12	101.05	4.000	Yes	No	2.00
522	35.62	98.70	2.24	1.69	0.68	57.30	1.73	98.99	4.000	Yes	No	2.00
523	35.67	115.40	2.14	1.46	0.65	68.51	1.49	102.07	4.000	Yes	No	2.00
524	35.71	137.52	2.04	1.30	0.62	83.52	1.35	112.52	4.000	Yes	No	2.00
525	35.82	159.89	1.96	1.19	0.60	98.71	1.28	126.36	4.000	Yes	No	2.00
526	35.86	185.11	1.89	1.12	0.58	116.11	1.23	143.07	4.000	Yes	No	2.00
527	35.93	207.72	1.84	1.06	0.56	131.80	1.19	156.85	4.000	Yes	No	2.00
528	36.01	225.38	1.80	1.04	0.55	144.00	1.16	166.33	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	36.06	235.57	1.79	1.04	0.54	150.92	1.14	171.69	4.000	Yes	No	2.00
530	36.12	240.67	1.78	1.05	0.54	154.12	1.13	174.89	0.578	No	No	2.00
531	36.18	245.05	1.79	1.08	0.54	156.73	1.14	178.20	0.606	No	No	2.00
532	36.25	248.69	1.79	1.10	0.54	158.84	1.14	180.98	0.631	No	No	2.00
533	36.30	251.52	1.80	1.14	0.55	160.26	1.15	184.12	0.661	No	No	2.00
534	36.39	252.83	1.81	1.17	0.55	160.54	1.16	185.99	0.678	No	No	2.00
535	36.44	253.07	1.82	1.21	0.55	160.15	1.17	187.57	0.694	No	No	2.00
536	36.53	251.49	1.83	1.25	0.56	158.45	1.18	187.51	0.693	No	No	2.00
537	36.59	248.39	1.86	1.34	0.57	155.45	1.21	187.43	0.692	No	No	2.00
538	36.68	243.47	1.87	1.37	0.57	151.62	1.22	184.49	0.664	No	No	2.00
539	36.75	238.34	1.88	1.38	0.57	147.93	1.22	180.99	0.631	No	No	2.00
540	36.83	232.04	1.88	1.34	0.57	143.78	1.22	175.91	0.586	No	No	2.00
541	36.90	225.27	1.89	1.35	0.58	138.95	1.23	171.34	0.548	No	No	2.00
542	36.97	217.18	1.92	1.39	0.58	133.11	1.25	166.05	0.506	No	No	2.00
543	37.02	201.72	1.96	1.49	0.60	122.19	1.28	156.23	0.435	No	No	2.00
544	37.04	193.70	1.99	1.53	0.60	116.64	1.30	151.13	0.401	No	No	2.00
545	37.08	188.61	2.00	1.54	0.61	113.19	1.30	147.61	0.379	No	No	1.93
546	37.17	191.78	1.97	1.46	0.60	115.46	1.29	148.65	0.385	No	No	1.96
547	37.27	187.30	1.98	1.44	0.60	112.45	1.29	145.04	0.364	No	No	1.85
548	37.37	181.37	1.99	1.43	0.60	108.42	1.30	140.68	0.339	No	No	1.72
549	37.42	177.21	1.99	1.39	0.60	105.83	1.30	137.22	0.320	No	No	1.62
550	37.51	175.89	1.97	1.32	0.60	105.19	1.29	135.25	0.310	No	No	1.57
551	37.58	176.97	1.95	1.22	0.59	106.34	1.27	134.76	0.308	No	No	1.56
552	37.66	179.01	1.92	1.13	0.58	108.07	1.25	135.08	0.309	No	No	1.57
553	37.76	182.58	1.89	1.05	0.57	110.83	1.23	136.26	0.315	No	No	1.59
554	37.85	186.08	1.86	0.97	0.57	113.57	1.21	137.18	0.320	No	No	1.62
555	37.93	189.62	1.84	0.92	0.56	116.22	1.19	138.14	0.325	No	No	1.64
556	38.04	192.25	1.82	0.89	0.55	117.99	1.18	138.80	0.329	No	No	1.66
557	38.13	193.87	1.82	0.88	0.55	118.97	1.17	139.30	0.331	No	No	1.67
558	38.18	193.57	1.82	0.88	0.55	118.63	1.17	139.16	0.331	No	No	1.67
559	38.28	191.24	1.84	0.92	0.56	116.58	1.19	138.51	0.327	No	No	1.65
560	38.37	187.40	1.86	0.97	0.57	113.37	1.21	137.08	0.320	No	No	1.61
561	38.47	183.55	1.89	1.06	0.58	109.99	1.23	135.63	0.312	No	No	1.57
562	38.57	180.39	1.92	1.13	0.58	107.19	1.25	134.14	0.304	No	No	1.53
563	38.62	176.78	1.95	1.21	0.59	104.23	1.27	132.48	0.296	No	No	1.49
564	38.72	167.48	2.00	1.33	0.61	97.43	1.31	127.27	0.272	No	No	1.37
565	38.78	160.21	2.04	1.42	0.62	92.19	1.34	123.72	0.256	No	No	1.29
566	38.81	155.32	2.06	1.49	0.63	88.77	1.37	121.63	0.247	No	No	1.24
567	38.86	155.19	2.07	1.50	0.63	88.54	1.37	121.68	0.248	No	No	1.24
568	38.91	152.02	2.08	1.55	0.63	86.27	1.40	120.51	0.243	No	No	1.22
569	38.95	145.92	2.12	1.64	0.64	82.06	1.44	118.55	0.235	No	No	1.18
570	39.05	139.55	2.15	1.74	0.65	77.66	1.51	116.91	0.229	No	No	1.15
571	39.09	132.37	2.19	1.84	0.66	72.88	1.59	115.64	0.224	No	No	1.12
572	39.14	125.06	2.23	1.95	0.68	68.10	1.69	114.83	0.221	No	No	1.11
573	39.24	118.19	2.26	2.05	0.69	63.61	1.80	114.32	0.219	No	No	1.10
574	39.29	112.16	2.30	2.14	0.70	59.80	1.91	114.03	0.218	No	No	1.09
575	39.39	108.48	2.32	2.20	0.70	57.39	1.99	114.16	0.218	No	No	1.10
576	39.43	109.15	2.31	2.19	0.70	57.74	1.98	114.28	0.219	No	No	1.10

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	39.53	115.02	2.28	2.10	0.69	61.25	1.86	113.89	0.217	No	No	1.09
578	39.57	124.17	2.23	1.94	0.68	67.01	1.69	113.55	0.216	No	No	1.08
579	39.68	130.64	2.19	1.83	0.67	71.04	1.60	113.69	0.217	No	No	1.09
580	39.73	131.95	2.19	1.80	0.66	71.83	1.58	113.53	0.216	No	No	1.08
581	39.81	129.33	2.20	1.81	0.67	70.10	1.60	112.48	0.212	No	No	1.06
582	39.89	126.37	2.19	1.75	0.67	68.39	1.60	109.51	0.202	No	No	1.01
583	39.96	125.26	2.18	1.63	0.66	68.01	1.56	105.89	0.190	No	No	0.95
584	40.06	124.52	2.16	1.53	0.66	67.75	1.52	103.14	0.182	No	No	0.91
585	40.15	122.70	2.17	1.55	0.66	66.50	1.54	102.38	0.180	No	No	0.90
586	40.20	114.41	2.22	1.70	0.67	61.03	1.67	102.07	0.179	No	No	0.89
587	40.24	108.56	2.26	1.81	0.69	57.23	1.79	102.62	0.181	No	No	0.90
588	40.26	104.17	2.29	1.90	0.70	54.45	1.90	103.22	0.182	No	No	0.91
589	40.27	107.91	2.27	1.85	0.69	56.72	1.82	103.36	0.183	No	No	0.91
590	40.37	109.77	2.26	1.84	0.69	57.73	1.80	103.81	0.184	No	No	0.92
591	40.42	111.64	2.26	1.85	0.69	58.75	1.78	104.71	0.187	No	No	0.93
592	40.52	112.38	2.26	1.87	0.69	59.02	1.79	105.44	0.189	No	No	0.94
593	40.56	115.27	2.25	1.87	0.68	60.66	1.76	106.63	0.193	No	No	0.96
594	40.66	122.24	2.22	1.81	0.67	64.78	1.67	108.06	0.197	No	No	0.99
595	40.70	131.54	2.18	1.74	0.66	70.42	1.57	110.67	0.206	No	No	1.03
596	40.75	142.59	2.14	1.67	0.65	77.15	1.49	114.79	0.221	No	No	1.10
597	40.85	153.40	2.11	1.63	0.64	83.66	1.43	119.75	0.240	No	No	1.20
598	40.91	164.05	2.08	1.59	0.63	90.16	1.39	125.10	0.262	No	No	1.31
599	40.96	174.69	2.04	1.53	0.62	96.83	1.35	130.56	0.287	No	No	1.43
600	41.04	184.27	2.01	1.47	0.61	102.87	1.32	135.59	0.312	No	No	1.55
601	41.09	193.94	1.98	1.41	0.60	109.10	1.29	141.03	0.341	No	No	1.70
602	41.18	201.90	1.96	1.36	0.60	114.17	1.28	145.57	0.367	No	No	1.83
603	41.23	207.97	1.94	1.33	0.59	118.08	1.26	149.12	0.388	No	No	1.94
604	41.29	211.58	1.93	1.31	0.59	120.37	1.26	151.17	0.401	No	No	2.00
605	41.38	212.76	1.93	1.30	0.59	120.98	1.25	151.67	0.404	No	No	2.00
606	41.42	212.09	1.93	1.31	0.59	120.40	1.26	151.21	0.402	No	No	2.00
607	41.52	210.03	1.94	1.33	0.59	118.76	1.26	149.86	0.393	No	No	1.96
608	41.57	207.27	1.95	1.36	0.59	116.72	1.27	148.26	0.383	No	No	1.91
609	41.62	204.91	1.96	1.40	0.60	114.93	1.28	146.93	0.375	No	No	1.87
610	41.71	203.13	1.97	1.43	0.60	113.45	1.29	145.89	0.369	No	No	1.84
611	41.76	202.15	1.98	1.45	0.60	112.60	1.29	145.43	0.366	No	No	1.82
612	41.84	201.65	1.99	1.47	0.60	111.98	1.30	145.17	0.364	No	No	1.81
613	41.91	201.54	1.99	1.50	0.61	111.64	1.30	145.22	0.365	No	No	1.81
614	41.95	201.75	2.00	1.52	0.61	111.52	1.31	145.53	0.367	No	No	1.82
615	42.01	202.52	2.00	1.56	0.61	111.63	1.31	146.36	0.372	No	No	1.85
616	42.10	203.57	2.01	1.60	0.61	111.82	1.32	147.40	0.378	No	No	1.88
617	42.15	204.98	2.02	1.66	0.61	112.23	1.33	148.90	0.387	No	No	1.92
618	42.24	206.03	2.03	1.70	0.62	112.44	1.33	149.94	0.394	No	No	1.96
619	42.28	206.46	2.03	1.71	0.62	112.53	1.34	150.31	0.396	No	No	1.97
620	42.39	206.26	2.03	1.70	0.62	112.27	1.33	149.81	0.393	No	No	1.95
621	42.43	206.08	2.02	1.67	0.62	112.28	1.33	149.14	0.389	No	No	1.93
622	42.50	206.11	2.01	1.62	0.61	112.45	1.32	148.36	0.384	No	No	1.91
623	42.58	206.28	2.00	1.56	0.61	112.80	1.31	147.54	0.379	No	No	1.88
624	42.65	198.95	2.01	1.55	0.61	108.28	1.32	142.73	0.350	No	No	1.74

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	42.70	195.88	2.02	1.54	0.61	106.39	1.32	140.58	0.338	No	No	1.68
626	42.73	193.72	2.02	1.54	0.61	105.08	1.32	139.14	0.331	No	No	1.64
627	42.77	200.19	1.99	1.47	0.61	109.31	1.30	142.31	0.348	No	No	1.73
628	42.82	203.83	1.98	1.43	0.60	111.68	1.29	144.06	0.358	No	No	1.78
629	42.87	209.12	1.96	1.39	0.60	115.10	1.28	146.92	0.375	No	No	1.86
630	42.91	215.46	1.94	1.35	0.59	119.14	1.26	150.57	0.397	No	No	1.97
631	42.97	221.76	1.92	1.32	0.59	123.09	1.25	154.27	0.421	No	No	2.00
632	43.02	226.82	1.92	1.32	0.58	126.14	1.25	157.35	0.442	No	No	2.00
633	43.06	230.49	1.91	1.33	0.58	128.19	1.25	159.72	0.459	No	No	2.00
634	43.11	234.33	1.91	1.34	0.58	130.34	1.24	162.21	0.477	No	No	2.00
635	43.17	237.93	1.91	1.35	0.58	132.40	1.24	164.40	0.493	No	No	2.00
636	43.21	242.21	1.90	1.33	0.58	135.09	1.23	166.83	0.512	No	No	2.00
637	43.29	246.19	1.89	1.30	0.57	137.59	1.23	168.85	0.528	No	No	2.00
638	43.34	250.53	1.87	1.28	0.57	140.43	1.22	171.05	0.545	No	No	2.00
639	43.39	254.11	1.86	1.25	0.57	142.76	1.21	172.71	0.559	No	No	2.00
640	43.45	256.87	1.85	1.22	0.56	144.64	1.20	173.74	0.568	No	No	2.00
641	43.51	258.25	1.84	1.18	0.56	145.84	1.19	173.50	0.566	No	No	2.00
642	43.59	258.59	1.82	1.14	0.56	146.35	1.18	172.47	0.557	No	No	2.00
643	43.64	259.19	1.80	1.07	0.55	147.38	1.16	170.73	0.543	No	No	2.00
644	43.70	259.29	1.78	1.01	0.54	148.12	1.13	168.10	0.522	No	No	2.00
645	43.78	258.35	1.77	0.96	0.54	147.98	1.12	165.08	0.498	No	No	2.00
646	43.88	255.18	1.77	0.96	0.54	145.77	1.12	163.55	0.487	No	No	2.00
647	43.94	244.77	1.82	1.04	0.55	138.10	1.17	161.52	0.472	No	No	2.00
648	44.04	234.93	1.86	1.12	0.57	130.84	1.21	157.74	0.445	No	No	2.00
649	44.07	225.87	1.89	1.21	0.58	124.41	1.23	153.31	0.415	No	No	2.00
650	44.12	223.58	1.90	1.23	0.58	122.68	1.24	152.08	0.407	No	No	2.00
651	44.16	221.15	1.91	1.25	0.58	120.94	1.25	150.70	0.398	No	No	1.98
652	44.21	218.05	1.93	1.28	0.59	118.76	1.25	148.86	0.387	No	No	1.92
653	44.26	214.65	1.94	1.30	0.59	116.39	1.26	146.86	0.375	No	No	1.86
654	44.31	210.81	1.95	1.34	0.59	113.73	1.27	144.63	0.361	No	No	1.79
655	44.35	206.97	1.97	1.37	0.60	111.11	1.28	142.44	0.349	No	No	1.73
656	44.40	203.26	1.98	1.40	0.60	108.60	1.29	140.32	0.337	No	No	1.67
657	44.45	200.16	1.99	1.43	0.61	106.49	1.30	138.56	0.327	No	No	1.62
658	44.50	197.83	2.00	1.45	0.61	104.91	1.31	137.24	0.320	No	No	1.59
659	44.54	195.81	2.01	1.47	0.61	103.53	1.32	136.15	0.315	No	No	1.56
660	44.60	193.46	2.02	1.49	0.61	101.86	1.32	134.97	0.309	No	No	1.53
661	44.64	190.96	2.03	1.53	0.62	100.11	1.34	133.85	0.303	No	No	1.50
662	44.69	188.57	2.05	1.57	0.62	98.42	1.35	132.85	0.298	No	No	1.48
663	44.74	187.78	2.05	1.59	0.62	97.76	1.36	132.59	0.297	No	No	1.47
664	44.79	187.17	2.06	1.60	0.62	97.27	1.36	132.34	0.296	No	No	1.47
665	44.83	187.71	2.05	1.60	0.62	97.52	1.36	132.53	0.296	No	No	1.47
666	44.88	188.84	2.05	1.59	0.62	98.15	1.35	132.96	0.299	No	No	1.48
667	44.93	191.20	2.04	1.57	0.62	99.52	1.35	134.02	0.304	No	No	1.51
668	44.98	193.69	2.03	1.55	0.62	100.99	1.34	135.20	0.310	No	No	1.54
669	45.03	195.31	2.03	1.54	0.62	101.90	1.33	135.95	0.314	No	No	1.56
670	45.08	196.49	2.03	1.54	0.62	102.54	1.33	136.45	0.316	No	No	1.57
671	45.16	197.53	2.02	1.52	0.62	103.08	1.33	136.81	0.318	No	No	1.58
672	45.19	198.24	2.02	1.50	0.61	103.58	1.32	136.91	0.319	No	No	1.58

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	45.27	198.44	2.01	1.47	0.61	103.76	1.32	136.53	0.317	No	No	1.57
674	45.32	197.56	2.00	1.44	0.61	103.38	1.31	135.53	0.312	No	No	1.55
675	45.37	195.58	2.00	1.39	0.61	102.45	1.31	133.73	0.302	No	No	1.50
676	45.45	192.44	1.99	1.35	0.61	100.80	1.30	131.17	0.290	No	No	1.44
677	45.51	187.22	1.99	1.31	0.61	97.91	1.30	127.52	0.273	No	No	1.35
678	45.56	180.52	2.01	1.31	0.61	93.92	1.31	123.37	4.000	Yes	No	2.00
679	45.61	169.84	2.04	1.36	0.62	87.34	1.35	117.60	4.000	Yes	No	2.00
680	45.69	156.32	2.10	1.48	0.64	78.89	1.42	111.79	4.000	Yes	No	2.00
681	45.75	137.42	2.20	1.74	0.67	67.17	1.61	108.19	4.000	Yes	No	2.00
682	45.81	115.31	2.30	1.96	0.70	54.45	1.93	105.04	4.000	Yes	No	2.00
683	45.89	93.28	2.42	2.23	0.73	42.25	2.49	105.10	4.000	Yes	No	2.00
684	45.94	73.36	2.54	2.43	0.77	31.83	3.26	103.73	4.000	Yes	No	2.00
685	46.04	59.21	2.67	2.85	0.81	24.44	4.42	108.05	4.000	Yes	Yes	2.00
686	46.08	46.61	2.83	3.46	0.86	18.15	6.18	112.07	4.000	Yes	Yes	2.00
687	46.15	39.94	2.97	3.96	1.00	13.37	8.22	109.85	4.000	Yes	Yes	2.00
688	46.17	36.10	3.03	4.33	1.00	11.98	9.26	110.89	3.600	No	Yes	2.00
689	46.18	36.17	3.02	4.27	1.00	12.00	9.18	110.17	3.600	No	Yes	2.00
690	46.23	36.48	3.01	4.17	1.00	12.10	9.03	109.18	3.600	No	Yes	2.00
691	46.27	37.18	3.00	4.00	1.00	12.34	8.72	107.58	3.600	No	Yes	2.00
692	46.32	38.64	2.96	3.74	1.00	12.85	8.20	105.33	3.600	No	Yes	2.00
693	46.41	40.63	2.89	3.49	0.87	15.29	7.01	107.19	3.600	No	Yes	2.00
694	46.47	43.16	2.85	3.30	0.86	16.49	6.44	106.19	3.600	No	Yes	2.00
695	46.52	45.45	2.82	3.23	0.85	17.54	6.09	106.89	3.600	No	Yes	2.00
696	46.56	47.57	2.81	3.31	0.85	18.46	5.95	109.81	3.600	No	Yes	2.00
697	46.65	49.42	2.80	3.44	0.85	19.21	5.91	113.60	3.600	No	Yes	2.00
698	46.71	51.52	2.80	3.58	0.85	20.07	5.86	117.68	3.600	No	Yes	2.00
699	46.76	54.41	2.78	3.59	0.84	21.37	5.62	120.04	3.600	No	Yes	2.00
700	46.85	58.19	2.75	3.48	0.83	23.13	5.21	120.43	3.600	No	Yes	2.00
701	46.90	63.28	2.69	3.26	0.82	25.63	4.63	118.71	3.600	No	Yes	2.00
702	46.99	67.89	2.65	3.04	0.80	27.93	4.16	116.19	3.600	No	Yes	2.00
703	47.04	70.35	2.62	2.93	0.79	29.16	3.93	114.63	3.600	No	Yes	2.00
704	47.10	69.50	2.63	2.95	0.80	28.71	4.00	114.71	3.600	No	Yes	2.00
705	47.16	65.45	2.67	3.09	0.81	26.63	4.36	116.10	3.600	No	Yes	2.00
706	47.23	59.62	2.72	3.30	0.82	23.71	4.94	117.23	3.600	No	Yes	2.00
707	47.30	51.46	2.81	3.62	0.85	19.76	5.97	117.96	3.600	No	Yes	2.00
708	47.38	42.76	2.96	4.09	1.00	13.97	8.12	113.48	3.600	No	Yes	2.00
709	47.43	34.23	3.08	4.68	1.00	10.97	10.19	111.84	3.600	No	Yes	2.00
710	47.52	28.17	3.17	4.93	1.00	8.83	11.99	105.92	3.600	No	Yes	2.00
711	47.59	23.92	3.20	4.34	1.00	7.34	12.70	93.23	3.600	No	Yes	2.00
712	47.66	21.40	3.20	3.59	1.00	6.45	12.70	81.89	3.600	No	Yes	2.00
713	47.77	19.71	3.20	3.13	1.00	5.85	12.77	74.67	3.600	No	Yes	2.00
714	47.82	18.77	3.24	3.41	1.00	5.51	13.75	75.76	3.600	No	Yes	2.00
715	47.91	18.38	3.26	3.59	1.00	5.37	14.28	76.63	3.600	No	Yes	2.00
716	47.93	17.68	3.30	3.86	1.00	5.12	15.17	77.65	3.600	No	Yes	2.00
717	47.97	17.78	3.30	3.92	1.00	5.15	15.21	78.37	3.600	No	Yes	2.00
718	48.02	17.86	3.31	4.05	1.00	5.17	15.38	79.56	3.600	No	Yes	2.00
719	48.07	18.51	3.30	4.11	1.00	5.39	15.07	81.21	3.600	No	Yes	2.00
720	48.12	18.61	3.31	4.43	1.00	5.42	15.51	84.04	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	48.19	18.71	3.33	4.73	1.00	5.44	15.90	86.54	3.600	No	Yes	2.00
722	48.23	18.91	3.33	4.96	1.00	5.51	16.11	88.74	3.600	No	Yes	2.00
723	48.31	19.15	3.33	5.05	1.00	5.58	16.11	89.88	3.600	No	Yes	2.00
724	48.35	19.35	3.33	5.13	1.00	5.64	16.11	90.92	3.600	No	Yes	2.00
725	48.40	19.25	3.34	5.27	1.00	5.60	16.37	91.72	3.600	No	Yes	2.00
726	48.45	18.81	3.36	5.50	1.00	5.45	16.96	92.39	3.600	No	Yes	2.00
727	48.50	18.07	3.40	5.83	1.00	5.19	17.92	92.93	3.600	No	Yes	2.00
728	48.55	17.80	3.41	6.00	1.00	5.09	18.35	93.37	3.600	No	Yes	2.00
729	48.59	17.64	3.42	6.20	1.00	5.03	18.75	94.24	3.600	No	Yes	2.00
730	48.67	17.87	3.42	6.18	1.00	5.10	18.56	94.62	3.600	No	Yes	2.00
731	48.73	17.84	3.42	6.16	1.00	5.08	18.58	94.36	3.600	No	Yes	2.00
732	48.78	17.97	3.40	5.89	1.00	5.12	18.13	92.80	3.600	No	Yes	2.00
733	48.83	17.97	3.39	5.58	1.00	5.11	17.74	90.68	3.600	No	Yes	2.00
734	48.91	17.94	3.38	5.27	1.00	5.09	17.35	88.35	3.600	No	Yes	2.00
735	48.98	17.84	3.37	5.04	1.00	5.05	17.10	86.35	3.600	No	Yes	2.00
736	49.03	17.74	3.37	4.91	1.00	5.01	17.00	85.19	3.600	No	Yes	2.00
737	49.12	17.68	3.35	4.63	1.00	4.98	16.65	82.90	3.600	No	Yes	2.00
738	49.17	17.75	3.33	4.17	1.00	5.00	15.91	79.48	3.600	No	Yes	2.00
739	49.27	18.02	3.30	3.75	1.00	5.08	15.07	76.51	3.600	No	Yes	2.00
740	49.31	18.56	3.28	3.65	1.00	5.25	14.57	76.55	3.600	No	Yes	2.00
741	49.38	19.20	3.27	3.79	1.00	5.46	14.44	78.88	3.600	No	Yes	2.00
742	49.45	19.70	3.27	3.95	1.00	5.62	14.44	81.15	3.600	No	Yes	2.00
743	49.51	19.00	3.31	4.33	1.00	5.38	15.44	83.00	3.600	No	Yes	2.00
744	49.54	19.44	3.30	4.37	1.00	5.52	15.24	84.13	3.600	No	Yes	2.00
745	49.59	20.18	3.28	4.25	1.00	5.76	14.65	84.45	3.600	No	Yes	2.00
746	49.64	21.53	3.23	3.89	1.00	6.21	13.47	83.63	3.600	No	Yes	2.00
747	49.73	21.20	3.24	3.89	1.00	6.09	13.64	83.01	3.600	No	Yes	2.00
748	49.83	20.02	3.27	4.07	1.00	5.68	14.52	82.47	3.600	No	Yes	2.00
749	49.92	18.88	3.31	4.30	1.00	5.29	15.55	82.19	3.600	No	Yes	2.00
750	49.98	17.86	3.35	4.49	1.00	4.94	16.51	81.62	3.600	No	Yes	2.00
751	50.07	17.33	3.37	4.57	1.00	4.75	17.04	81.01	3.600	No	Yes	2.00
752	50.16	16.99	3.38	4.61	1.00	4.63	17.38	80.51	3.600	No	Yes	2.00
753	50.24	16.69	3.39	4.65	1.00	4.52	17.70	80.06	3.600	No	Yes	2.00
754	50.32	16.46	3.40	4.71	1.00	4.44	17.99	79.87	3.600	No	Yes	2.00
755	50.41	16.32	3.41	4.79	1.00	4.39	18.25	80.02	3.600	No	Yes	2.00
756	50.50	16.36	3.41	4.79	1.00	4.39	18.25	80.09	3.600	No	Yes	2.00
757	50.56	16.26	3.41	4.73	1.00	4.35	18.25	79.36	3.600	No	Yes	2.00
758	50.66	16.09	3.41	4.63	1.00	4.28	18.27	78.27	3.600	No	Yes	2.00
759	50.74	15.92	3.41	4.59	1.00	4.22	18.37	77.53	3.600	No	Yes	2.00
760	50.84	15.85	3.43	4.94	1.00	4.19	19.00	79.62	3.600	No	Yes	2.00
761	50.93	15.95	3.46	5.57	1.00	4.21	19.91	83.88	3.600	No	Yes	2.00
762	50.98	16.77	3.48	6.56	1.00	4.47	20.59	92.08	3.600	No	Yes	2.00
763	51.08	19.60	3.43	7.08	1.00	5.39	19.08	102.75	3.600	No	Yes	2.00
764	51.17	24.45	3.34	6.97	1.00	6.95	16.30	113.31	3.600	No	Yes	2.00
765	51.24	30.11	3.25	6.75	1.00	8.78	13.98	122.80	3.600	No	Yes	2.00
766	51.34	33.65	3.21	6.76	1.00	9.91	13.03	129.12	3.600	No	Yes	2.00
767	51.41	34.16	3.18	6.01	1.00	10.06	12.19	122.59	3.600	No	Yes	2.00
768	51.51	32.81	3.17	5.54	1.00	9.60	12.05	115.66	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	51.58	31.20	3.16	4.92	1.00	9.06	11.80	106.93	3.600	No	Yes	2.00
770	51.68	29.95	3.20	5.43	1.00	8.64	12.73	109.98	3.600	No	Yes	2.00
771	51.79	27.39	3.26	5.93	1.00	7.80	14.12	110.16	3.600	No	Yes	2.00
772	51.82	25.87	3.30	6.27	1.00	7.31	15.07	110.15	3.600	No	Yes	2.00
773	51.85	24.39	3.34	6.78	1.00	6.83	16.27	111.07	3.600	No	Yes	2.00
774	51.91	25.00	3.34	6.90	1.00	7.01	16.14	113.23	3.600	No	Yes	2.00
775	52.00	24.87	3.36	7.36	1.00	6.96	16.71	116.25	3.600	No	Yes	2.00
776	52.05	27.06	3.31	7.10	1.00	7.65	15.54	118.92	3.600	No	Yes	2.00
777	52.10	31.78	3.21	6.10	1.00	9.15	13.00	118.95	3.600	No	Yes	2.00
778	52.19	38.49	3.08	4.92	1.00	11.27	10.28	115.81	3.600	No	Yes	2.00
779	52.28	44.04	2.99	4.15	1.00	13.02	8.58	111.69	3.600	No	Yes	2.00
780	52.34	46.37	2.95	3.85	1.00	13.74	7.96	109.32	3.600	No	Yes	2.00
781	52.42	46.09	2.96	3.90	1.00	13.63	8.05	109.66	3.600	No	Yes	2.00
782	52.48	44.34	2.98	4.10	1.00	13.05	8.50	111.03	3.600	No	Yes	2.00
783	52.57	42.32	3.01	4.26	1.00	12.39	8.98	111.27	3.600	No	Yes	2.00
784	52.62	40.26	3.03	4.31	1.00	11.73	9.37	109.88	3.600	No	Yes	2.00
785	52.69	38.51	3.05	4.22	1.00	11.16	9.58	106.89	3.600	No	Yes	2.00
786	52.77	36.89	3.06	4.17	1.00	10.63	9.83	104.50	3.600	No	Yes	2.00
787	52.87	35.55	3.08	4.24	1.00	10.19	10.19	103.83	3.600	No	Yes	2.00
788	52.91	34.07	3.10	4.28	1.00	9.71	10.56	102.56	3.600	No	Yes	2.00
789	53.01	32.55	3.12	4.42	1.00	9.21	11.08	102.13	3.600	No	Yes	2.00
790	53.10	32.18	3.14	4.56	1.00	9.08	11.35	103.11	3.600	No	Yes	2.00
791	53.16	34.04	3.15	5.28	1.00	9.65	11.74	113.26	3.600	No	Yes	2.00
792	53.25	38.69	3.13	5.64	1.00	11.08	11.13	123.32	3.600	No	Yes	2.00
793	53.29	44.28	3.10	6.15	1.00	12.82	10.63	136.25	3.600	No	Yes	2.00
794	53.38	48.90	3.07	6.34	1.00	14.23	10.13	144.18	3.600	No	Yes	2.00
795	53.42	59.32	2.99	5.88	1.00	17.47	8.56	149.47	3.600	No	Yes	2.00
796	53.47	74.66	2.87	5.11	1.00	22.21	6.75	150.02	3.600	No	Yes	2.00
797	53.52	92.88	2.76	4.46	1.00	27.85	5.32	148.22	3.600	No	Yes	2.00
798	53.58	102.94	2.72	4.44	1.00	30.94	4.93	152.55	3.600	No	Yes	2.00
799	53.66	103.80	2.74	4.76	1.00	31.15	5.14	160.18	3.600	No	Yes	2.00
800	53.75	98.64	2.79	5.33	1.00	29.50	5.74	169.41	3.600	No	Yes	2.00
801	53.81	88.93	2.86	5.98	1.00	26.46	6.64	175.67	3.600	No	Yes	2.00
802	53.87	78.89	2.93	6.58	1.00	23.33	7.63	177.89	3.600	No	Yes	2.00
803	53.95	67.24	3.02	7.41	1.00	19.70	9.07	178.71	3.600	No	Yes	2.00
804	54.01	57.35	3.10	8.28	1.00	16.64	10.67	177.57	3.600	No	Yes	2.00
805	54.06	47.51	3.20	9.23	1.00	13.60	12.71	172.90	3.600	No	Yes	2.00
806	54.15	41.78	3.26	9.77	1.00	11.83	14.16	167.57	3.600	No	Yes	2.00
807	54.20	40.60	3.27	9.77	1.00	11.46	14.42	165.24	3.600	No	Yes	2.00
808	54.29	47.57	3.17	8.38	1.00	13.59	12.09	164.23	3.600	No	Yes	2.00
809	54.34	69.40	2.89	4.90	1.00	20.27	7.00	141.87	4.000	Yes	Yes	2.00
810	54.43	100.37	2.59	2.67	1.00	29.73	3.65	108.63	4.000	Yes	No	2.00
811	54.45	137.16	2.32	1.48	1.00	41.00	2.00	82.07	4.000	Yes	No	2.00
812	54.48	166.07	2.20	1.22	1.00	49.83	1.62	80.59	4.000	Yes	No	2.00
813	54.52	185.51	2.14	1.11	1.00	55.76	1.48	82.69	4.000	Yes	No	2.00
814	54.53	198.85	2.12	1.13	1.00	59.83	1.45	86.57	4.000	Yes	No	2.00
815	54.58	207.94	2.11	1.17	1.00	62.58	1.44	89.91	0.148	No	No	0.75
816	54.62	219.64	2.10	1.19	1.00	66.13	1.42	93.59	0.156	No	No	0.80

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	54.65	233.46	2.07	1.16	1.00	70.33	1.38	96.81	0.164	No	No	0.84
818	54.70	244.67	2.05	1.15	1.00	73.72	1.36	99.98	0.173	No	No	0.88
819	54.76	251.12	2.05	1.17	1.00	75.64	1.35	102.23	0.179	No	No	0.92
820	54.77	249.88	2.06	1.22	1.00	75.25	1.37	102.77	0.181	No	No	0.92
821	54.82	251.50	2.06	1.21	1.00	75.71	1.36	103.16	0.182	No	No	0.93
822	54.87	253.07	2.05	1.21	1.00	76.14	1.36	103.55	0.183	No	No	0.94
823	54.88	255.63	2.05	1.20	1.00	76.92	1.35	104.08	0.185	No	No	0.94
824	54.91	257.28	2.05	1.20	1.00	77.39	1.35	104.56	0.186	No	No	0.95
825	54.96	263.42	2.04	1.18	1.00	79.22	1.34	106.09	0.191	No	No	0.98
826	54.97	276.70	2.01	1.17	1.00	83.26	1.32	109.90	0.203	No	No	1.04
827	55.03	294.89	1.99	1.17	1.00	88.74	1.30	115.47	0.223	No	No	1.14
828	55.09	315.21	1.96	1.11	1.00	94.86	1.27	120.89	0.244	No	No	1.25
829	55.15	327.84	1.89	0.92	1.00	98.63	1.23	121.55	0.247	No	No	1.26
830	55.20	338.35	1.85	0.83	1.00	101.77	1.20	122.41	0.251	No	No	1.28
831	55.25	358.17	1.78	0.67	1.00	107.74	1.13	121.49	0.247	No	No	1.26
832	55.30	386.84	1.77	0.71	1.00	116.38	1.11	129.28	0.281	No	No	1.44
833	55.34	417.50	1.74	0.72	1.00	125.63	1.07	134.62	0.307	No	No	1.57
834	55.39	440.05	1.76	0.82	1.00	132.40	1.10	146.03	0.370	No	No	1.89
835	55.40	462.28	1.76	0.87	1.00	139.13	1.10	153.71	0.418	No	No	2.00
836	55.44	482.80	1.75	0.87	1.00	145.29	1.08	157.35	0.442	No	No	2.00
837	55.44	511.21	1.72	0.83	1.00	153.88	1.02	157.04	0.440	No	No	2.00
838	55.49	517.76	1.72	0.86	1.00	155.78	1.03	160.78	0.467	No	No	2.00
839	55.54	533.43	1.73	0.91	1.00	160.44	1.05	167.71	0.519	No	No	2.00
840	55.59	534.98	1.76	1.00	1.00	160.82	1.10	176.17	0.588	No	No	2.00
841	55.63	551.08	1.75	1.02	1.00	165.61	1.09	180.34	0.625	No	No	2.00
842	55.64	553.47	1.75	1.02	1.00	166.31	1.09	180.79	0.630	No	No	2.00
843	55.68	566.94	1.73	0.98	1.00	170.31	1.06	179.92	0.622	No	No	2.00
844	55.69	570.38	1.73	0.97	1.00	171.33	1.04	178.50	0.609	No	No	2.00
845	55.69	566.17	1.73	0.98	1.00	170.04	1.05	179.38	0.617	No	No	2.00
846	55.71	561.62	1.75	1.03	1.00	168.63	1.09	183.08	0.651	No	No	2.00
847	55.76	567.28	1.76	1.06	1.00	170.25	1.10	186.45	0.683	No	No	2.00
848	55.78	580.19	1.75	1.05	1.00	174.11	1.08	187.85	0.696	No	No	2.00
849	55.81	581.23	1.72	0.98	1.00	174.36	1.04	180.96	0.631	No	No	2.00
850	55.85	584.16	1.69	0.88	1.00	175.16	1.00	175.16	0.580	No	No	2.00
851	55.86	588.34	1.65	0.77	1.00	176.41	1.00	176.41	0.591	No	No	2.00
852	55.91	598.65	1.62	0.70	1.00	179.42	1.00	179.42	0.617	No	No	2.00
853	55.92	602.25	1.60	0.66	1.00	180.48	1.00	180.48	0.627	No	No	2.00
854	55.96	619.03	1.58	0.63	1.00	185.46	1.00	185.46	0.673	No	No	2.00
855	55.97	634.09	1.57	0.63	1.00	189.98	1.00	189.98	0.718	No	No	2.00
856	56.00	654.37	1.56	0.64	1.00	196.01	1.00	196.01	0.780	No	No	2.00
857	56.01	660.12	1.58	0.69	1.00	197.72	1.00	197.72	0.799	No	No	2.00
858	56.03	661.79	1.59	0.72	1.00	198.18	1.00	198.18	0.804	No	No	2.00
859	56.05	661.82	1.60	0.74	1.00	198.14	1.00	198.14	0.803	No	No	2.00
860	56.10	665.04	1.60	0.73	1.00	198.99	1.00	198.99	0.813	No	No	2.00
861	56.12	668.02	1.58	0.70	1.00	199.86	1.00	199.86	0.822	No	No	2.00
862	56.16	667.69	1.57	0.68	1.00	199.67	1.00	199.67	0.820	No	No	2.00
863	56.17	654.78	1.57	0.67	1.00	195.76	1.00	195.76	0.778	No	No	2.00
864	56.20	635.11	1.59	0.69	1.00	189.78	1.00	189.78	0.716	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	56.22	617.48	1.61	0.71	1.00	184.46	1.00	184.46	0.664	No	No	2.00
866	56.24	608.45	1.61	0.71	1.00	181.69	1.00	181.69	0.638	No	No	2.00
867	56.30	602.69	1.62	0.70	1.00	179.84	1.00	179.84	0.621	No	No	2.00
868	56.31	595.69	1.63	0.72	1.00	177.72	1.00	177.72	0.602	No	No	2.00
869	56.34	586.22	1.65	0.77	1.00	174.82	1.00	174.82	0.577	No	No	2.00
870	56.39	579.04	1.66	0.78	1.00	172.57	1.00	172.57	0.558	No	No	2.00
871	56.45	572.30	1.67	0.79	1.00	170.44	1.00	170.44	0.540	No	No	2.00
872	56.48	565.39	1.67	0.79	1.00	168.31	1.00	168.31	0.523	No	No	2.00
873	56.49	555.45	1.70	0.85	1.00	165.32	1.00	165.32	0.500	No	No	2.00
874	56.53	542.15	1.73	0.91	1.00	161.25	1.05	168.57	0.525	No	No	2.00
875	56.58	529.04	1.75	0.94	1.00	157.24	1.08	169.38	0.532	No	No	2.00
876	56.63	524.73	1.67	0.72	1.00	155.86	1.00	155.86	0.432	No	No	2.00
877	56.68	526.01	1.58	0.52	1.00	156.17	1.00	156.17	0.434	No	No	2.00
878	56.73	531.33	1.53	0.43	1.00	157.68	1.00	157.68	0.445	No	No	2.00
879	56.78	526.31	1.62	0.60	1.00	156.09	1.00	156.09	0.434	No	No	2.00
880	56.83	517.99	1.69	0.76	1.00	153.53	1.00	153.53	0.417	No	No	2.00
881	56.89	503.37	1.73	0.85	1.00	149.05	1.06	157.35	0.442	No	No	2.00
882	56.95	485.04	1.77	0.94	1.00	143.50	1.12	160.76	0.466	No	No	2.00
883	56.99	470.25	1.81	1.02	1.00	139.02	1.16	161.37	0.471	No	No	2.00
884	57.01	460.92	1.83	1.07	1.00	136.23	1.18	160.98	0.468	No	No	2.00
885	57.04	461.73	1.82	1.05	1.00	136.41	1.18	160.65	0.466	No	No	2.00
886	57.09	468.20	1.81	1.02	1.00	138.26	1.17	161.13	0.469	No	No	2.00
887	57.11	477.43	1.81	1.03	1.00	140.98	1.16	163.57	0.487	No	No	2.00
888	57.13	488.62	1.81	1.06	1.00	144.26	1.16	167.47	0.517	No	No	2.00
889	57.18	488.78	1.82	1.11	1.00	144.24	1.17	169.44	0.532	No	No	2.00
890	57.19	477.80	1.85	1.18	1.00	140.96	1.20	168.95	0.529	No	No	2.00
891	57.21	464.47	1.87	1.22	1.00	136.96	1.21	166.30	0.508	No	No	2.00
892	57.24	456.12	1.88	1.23	1.00	134.45	1.22	164.00	0.490	No	No	2.00
893	57.28	456.72	1.87	1.20	1.00	134.56	1.21	163.35	0.485	No	No	2.00
894	57.32	450.91	1.87	1.19	1.00	132.78	1.22	161.45	0.471	No	No	2.00
895	57.35	445.39	1.88	1.21	1.00	131.08	1.22	160.03	0.461	No	No	2.00
896	57.38	435.59	1.89	1.22	1.00	128.14	1.23	157.50	0.443	No	No	2.00
897	57.43	430.50	1.89	1.21	1.00	126.56	1.23	155.53	0.430	No	No	2.00
898	57.48	414.66	1.90	1.19	1.00	121.80	1.23	150.26	0.396	No	No	2.00
899	57.52	398.59	1.89	1.12	1.00	116.98	1.23	143.92	0.357	No	No	1.85
900	57.57	389.56	1.91	1.18	1.00	114.25	1.25	142.28	0.348	No	No	1.80
901	57.62	396.66	1.94	1.29	1.00	116.29	1.26	146.53	0.373	No	No	1.93
902	57.68	427.50	1.92	1.35	1.00	125.32	1.25	157.03	0.440	No	No	2.00
903	57.76	462.23	1.88	1.27	1.00	135.46	1.23	166.00	0.505	No	No	2.00
904	57.81	505.50	1.75	0.90	1.00	148.16	1.09	161.17	0.469	No	No	2.00
905	57.86	543.58	1.63	0.63	1.00	159.31	1.00	159.31	0.456	No	No	2.00
906	57.89	572.52	1.49	0.39	1.00	167.80	1.00	167.80	0.519	No	No	2.00
907	57.91	583.54	1.48	0.39	1.00	171.02	1.00	171.02	0.545	No	No	2.00
908	57.92	577.13	1.50	0.42	1.00	169.11	1.00	169.11	0.530	No	No	2.00
909	57.95	569.05	1.54	0.47	1.00	166.67	1.00	166.67	0.511	No	No	2.00
910	57.99	570.66	1.56	0.52	1.00	167.08	1.00	167.08	0.514	No	No	2.00
911	58.01	578.72	1.57	0.56	1.00	169.42	1.00	169.42	0.532	No	No	2.00
912	58.05	591.19	1.58	0.58	1.00	173.02	1.00	173.02	0.562	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	58.05	598.87	1.59	0.62	1.00	175.27	1.00	175.27	0.581	No	No	2.00
914	58.10	604.77	1.60	0.65	1.00	176.91	1.00	176.91	0.595	No	No	2.00
915	58.13	611.17	1.60	0.67	1.00	178.73	1.00	178.73	0.611	No	No	2.00
916	58.15	618.51	1.60	0.66	1.00	180.87	1.00	180.87	0.630	No	No	2.00
917	58.17	625.12	1.59	0.65	1.00	182.75	1.00	182.75	0.648	No	No	2.00
918	58.20	623.43	1.59	0.66	1.00	182.21	1.00	182.21	0.643	No	No	2.00
919	58.21	619.40	1.60	0.67	1.00	181.00	1.00	181.00	0.632	No	No	2.00
920	58.21	614.30	1.61	0.68	1.00	179.50	1.00	179.50	0.618	No	No	2.00
921	58.23	613.93	1.61	0.68	1.00	179.34	1.00	179.34	0.616	No	No	2.00
922	58.24	608.11	1.62	0.69	1.00	177.62	1.00	177.62	0.601	No	No	2.00
923	58.25	609.21	1.54	0.52	1.00	177.92	1.00	177.92	0.604	No	No	2.00
924	58.29	613.99	1.44	0.36	1.00	179.26	1.00	179.26	0.616	No	No	2.00
925	58.31	627.24	1.32	0.20	1.00	183.11	1.00	183.11	0.651	No	No	2.00
926	58.33	639.00	1.34	0.24	1.00	186.52	1.00	186.52	0.683	No	No	2.00
927	58.38	651.36	1.37	0.28	1.00	190.06	1.00	190.06	0.718	No	No	2.00
928	58.39	661.87	1.39	0.32	1.00	193.13	1.00	193.13	0.750	No	No	2.00
929	58.43	670.53	1.40	0.34	1.00	195.59	1.00	195.59	0.776	No	No	2.00
930	58.43	682.73	1.39	0.33	1.00	199.15	1.00	199.15	0.815	No	No	2.00
931	58.48	688.02	1.40	0.35	1.00	200.60	1.00	200.60	4.000	No	No	2.00
932	58.53	694.39	1.41	0.38	1.00	202.36	1.00	202.36	4.000	No	No	2.00
933	58.56	696.37	1.46	0.46	1.00	202.90	1.00	202.90	4.000	No	No	2.00
934	58.58	704.43	1.47	0.49	1.00	205.20	1.00	205.20	4.000	No	No	2.00
935	58.59	710.90	1.49	0.52	1.00	207.06	1.00	207.06	4.000	No	No	2.00
936	58.63	707.18	1.49	0.53	1.00	205.90	1.00	205.90	4.000	No	No	2.00
937	58.63	709.20	1.50	0.54	1.00	206.49	1.00	206.49	4.000	No	No	2.00
938	58.63	695.36	1.51	0.54	1.00	202.42	1.00	202.42	4.000	No	No	2.00
939	58.68	700.19	1.49	0.51	1.00	203.74	1.00	203.74	4.000	No	No	2.00
940	58.69	701.88	1.45	0.44	1.00	204.22	1.00	204.22	4.000	No	No	2.00
941	58.72	717.85	1.40	0.38	1.00	208.81	1.00	208.81	4.000	No	No	2.00
942	58.73	722.94	1.38	0.36	1.00	210.28	1.00	210.28	4.000	No	No	2.00
943	58.74	728.64	1.41	0.40	1.00	211.92	1.00	211.92	4.000	No	No	2.00
944	58.77	726.96	1.44	0.45	1.00	211.36	1.00	211.36	4.000	No	No	2.00
945	58.81	722.67	1.47	0.50	1.00	210.02	1.00	210.02	4.000	No	No	2.00
946	58.82	713.94	1.49	0.53	1.00	207.44	1.00	207.44	4.000	No	No	2.00
947	58.83	715.80	1.51	0.57	1.00	207.97	1.00	207.97	4.000	No	No	2.00
948	58.87	722.33	1.52	0.60	1.00	209.78	1.00	209.78	4.000	No	No	2.00
949	58.91	731.67	1.53	0.63	1.00	212.41	1.00	212.41	4.000	No	No	2.00
950	58.92	737.87	1.54	0.64	1.00	214.21	1.00	214.21	4.000	No	No	2.00
951	58.93	740.53	1.53	0.64	1.00	214.95	1.00	214.95	4.000	No	No	2.00
952	58.96	739.05	1.53	0.63	1.00	214.44	1.00	214.44	4.000	No	No	2.00
953	59.01	716.31	1.56	0.67	1.00	207.70	1.00	207.70	4.000	No	No	2.00
954	59.06	687.29	1.59	0.73	1.00	199.13	1.00	199.13	0.814	No	No	2.00
955	59.08	655.28	1.63	0.78	1.00	189.77	1.00	189.77	0.716	No	No	2.00
956	59.11	638.94	1.65	0.81	1.00	184.95	1.00	184.95	0.668	No	No	2.00
957	59.15	627.21	1.68	0.88	1.00	181.46	1.00	181.46	0.636	No	No	2.00
958	59.21	618.28	1.70	0.94	1.00	178.75	1.00	178.75	0.611	No	No	2.00
959	59.26	606.09	1.72	0.96	1.00	175.11	1.02	178.89	0.612	No	No	2.00
960	59.30	592.31	1.71	0.92	1.00	171.02	1.01	173.20	0.563	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
961	59.35	579.87	1.71	0.90	1.00	167.32	1.01	169.07	0.529	No	No	2.00
962	59.40	562.76	1.73	0.91	1.00	162.26	1.04	168.73	0.527	No	No	2.00
963	59.42	550.96	1.74	0.92	1.00	158.81	1.06	168.34	0.524	No	No	2.00
964	59.47	539.34	1.75	0.93	1.00	155.35	1.08	167.78	0.519	No	No	2.00
965	59.51	539.41	1.75	0.95	1.00	155.29	1.09	168.63	0.526	No	No	2.00
966	59.56	537.97	1.75	0.95	1.00	154.79	1.09	168.59	0.526	No	No	2.00
967	59.61	537.36	1.74	0.90	1.00	154.53	1.06	164.50	0.494	No	No	2.00
968	59.67	541.98	1.70	0.80	1.00	155.77	1.00	155.77	0.432	No	No	2.00
969	59.71	553.73	1.65	0.69	1.00	159.11	1.00	159.11	0.455	No	No	2.00
970	59.80	555.82	1.61	0.59	1.00	159.56	1.00	159.56	0.458	No	No	2.00
971	59.85	552.45	1.59	0.54	1.00	158.50	1.00	158.50	0.450	No	No	2.00
972	59.90	542.21	1.59	0.53	1.00	155.47	1.00	155.47	0.429	No	No	2.00
973	60.00	542.99	1.59	0.54	1.00	155.53	1.00	155.53	0.430	No	No	2.00
974	60.04	541.71	1.60	0.56	1.00	155.09	1.00	155.09	0.427	No	No	2.00
975	60.10	526.52	1.63	0.60	1.00	150.62	1.00	150.62	0.398	No	No	2.00
976	60.15	508.32	1.67	0.66	1.00	145.30	1.00	145.30	0.365	No	No	1.91
977	60.19	487.40	1.70	0.69	1.00	139.22	1.00	139.22	0.331	No	No	1.73
978	60.23	483.49	1.69	0.66	1.00	138.03	1.00	138.03	0.325	No	No	1.70
979	60.28	482.61	1.68	0.63	1.00	137.71	1.00	137.71	0.323	No	No	1.69
980	60.33	488.98	1.67	0.62	1.00	139.47	1.00	139.47	0.332	No	No	1.74
981	60.38	491.97	1.67	0.64	1.00	140.26	1.00	140.26	0.337	No	No	1.77
982	60.42	493.85	1.69	0.68	1.00	140.74	1.00	140.74	0.339	No	No	1.78
983	60.44	487.18	1.71	0.72	1.00	138.79	1.01	140.24	0.337	No	No	1.76
984	60.47	475.94	1.74	0.79	1.00	135.53	1.08	145.72	0.368	No	No	1.93
985	60.52	465.53	1.78	0.87	1.00	132.47	1.12	148.94	0.387	No	No	2.00
986	60.56	462.70	1.79	0.92	1.00	131.60	1.15	150.90	0.400	No	No	2.00
987	60.57	465.03	1.79	0.92	1.00	132.25	1.15	151.48	0.403	No	No	2.00
988	60.61	470.62	1.78	0.89	1.00	133.80	1.13	151.48	0.403	No	No	2.00
989	60.66	477.29	1.77	0.88	1.00	135.64	1.12	151.98	0.406	No	No	2.00
990	60.71	486.66	1.77	0.87	1.00	138.25	1.11	153.21	0.414	No	No	2.00
991	60.76	495.25	1.77	0.90	1.00	140.63	1.11	156.59	0.437	No	No	2.00
992	60.81	504.76	1.77	0.92	1.00	143.27	1.11	159.58	0.458	No	No	2.00
993	60.86	523.05	1.75	0.90	1.00	148.43	1.08	161.02	0.468	No	No	2.00
994	60.91	559.78	1.70	0.83	1.00	158.84	1.00	158.84	0.453	No	No	2.00
995	60.95	601.50	1.66	0.78	1.00	170.69	1.00	170.69	0.542	No	No	2.00
996	61.00	637.66	1.64	0.77	1.00	180.91	1.00	180.91	0.631	No	No	2.00
997	61.02	657.74	1.64	0.79	1.00	186.60	1.00	186.60	0.684	No	No	2.00
998	61.05	685.10	1.62	0.78	1.00	194.34	1.00	194.34	0.763	No	No	2.00
999	61.08	710.24	1.61	0.77	1.00	201.44	1.00	201.44	4.000	No	No	2.00
1000	61.09	731.84	1.59	0.76	1.00	207.57	1.00	207.57	4.000	No	No	2.00
1001	61.13	737.94	1.59	0.76	1.00	209.24	1.00	209.24	4.000	No	No	2.00
1002	61.14	739.46	1.60	0.77	1.00	209.63	1.00	209.63	4.000	No	No	2.00
1003	61.16	741.44	1.60	0.78	1.00	210.15	1.00	210.15	4.000	No	No	2.00
1004	61.20	750.88	1.58	0.75	1.00	212.77	1.00	212.77	4.000	No	No	2.00
1005	61.23	762.13	1.56	0.71	1.00	215.88	1.00	215.88	4.000	No	No	2.00
1006	61.24	766.92	1.52	0.62	1.00	217.23	1.00	217.23	4.000	No	No	2.00
1007	61.29	758.86	1.51	0.59	1.00	214.83	1.00	214.83	4.000	No	No	2.00
1008	61.30	744.24	1.52	0.59	1.00	210.65	1.00	210.65	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1009	61.33	734.57	1.55	0.65	1.00	207.82	1.00	207.82	4.000	No	No	2.00
1010	61.38	730.90	1.55	0.65	1.00	206.66	1.00	206.66	4.000	No	No	2.00
1011	61.43	731.07	1.53	0.60	1.00	206.60	1.00	206.60	4.000	No	No	2.00
1012	61.48	738.25	1.50	0.56	1.00	208.54	1.00	208.54	4.000	No	No	2.00
1013	61.53	750.91	1.48	0.53	1.00	212.02	1.00	212.02	4.000	No	No	2.00
1014	61.56	754.78	1.48	0.52	1.00	213.05	1.00	213.05	4.000	No	No	2.00
1015	61.58	726.93	1.50	0.54	1.00	205.10	1.00	205.10	4.000	No	No	2.00
1016	61.59	702.39	1.52	0.55	1.00	198.13	1.00	198.13	0.803	No	No	2.00
1017	61.62	600.70	1.61	0.64	1.00	169.24	1.00	169.24	0.531	No	No	2.00
1018	61.63	595.30	1.61	0.64	1.00	167.67	1.00	167.67	0.518	No	No	2.00
1019	61.67	588.36	1.62	0.64	1.00	165.65	1.00	165.65	0.503	No	No	2.00
1020	61.71	662.66	1.55	0.57	1.00	186.61	1.00	186.61	0.684	No	No	2.00
1021	61.76	655.52	1.55	0.57	1.00	184.50	1.00	184.50	0.664	No	No	2.00
1022	61.81	634.02	1.54	0.53	1.00	178.32	1.00	178.32	0.607	No	No	2.00
1023	61.86	615.02	1.52	0.48	1.00	172.85	1.00	172.85	0.560	No	No	2.00
1024	61.87	600.83	1.48	0.38	1.00	168.83	1.00	168.83	0.528	No	No	2.00
1025	61.91	588.87	1.44	0.32	1.00	165.39	1.00	165.39	0.501	No	No	2.00
1026	61.95	578.02	1.42	0.27	1.00	162.25	1.00	162.25	0.477	No	No	2.00
1027	61.96	566.74	1.42	0.26	1.00	159.04	1.00	159.04	0.454	No	No	2.00
1028	62.00	553.70	1.45	0.29	1.00	155.30	1.00	155.30	0.428	No	No	2.00
1029	62.04	535.16	1.49	0.33	1.00	150.01	1.00	150.01	0.394	No	No	2.00
1030	62.06	510.97	1.55	0.41	1.00	143.15	1.00	143.15	0.353	No	No	1.86
1031	62.10	491.66	1.60	0.47	1.00	137.65	1.00	137.65	0.323	No	No	1.70
1032	62.14	475.52	1.64	0.51	1.00	133.04	1.00	133.04	0.299	No	No	1.58
1033	62.20	463.08	1.66	0.55	1.00	129.46	1.00	129.46	0.282	No	No	1.49
1034	62.22	439.20	1.71	0.60	1.00	122.70	1.00	122.70	0.252	No	No	1.33
1035	62.27	415.48	1.75	0.66	1.00	115.96	1.08	125.13	0.262	No	No	1.39
1036	62.29	396.37	1.78	0.71	1.00	110.55	1.13	125.44	0.264	No	No	1.39
1037	62.34	380.26	1.82	0.77	1.00	105.96	1.17	124.22	0.258	No	No	1.37
1038	62.39	366.62	1.86	0.86	1.00	102.08	1.21	123.46	0.255	No	No	1.35
1039	62.43	347.78	1.93	1.03	1.00	96.73	1.26	121.51	0.247	No	No	1.31
1040	62.49	340.13	1.97	1.16	1.00	94.52	1.28	121.38	0.246	No	No	1.30
1041	62.57	336.43	1.99	1.25	1.00	93.40	1.30	121.70	0.248	No	No	1.31
1042	62.68	357.18	1.98	1.25	1.00	99.12	1.29	127.79	0.274	No	No	1.45
1043	62.75	398.26	1.93	1.21	1.00	110.56	1.26	139.12	0.330	No	No	1.75
1044	62.87	426.23	1.91	1.20	1.00	118.25	1.24	146.86	0.375	No	No	1.99
1045	62.88	409.21	1.93	1.22	1.00	113.48	1.25	142.25	0.348	No	No	1.84
1046	62.89	424.34	1.86	1.01	1.00	117.70	1.21	142.29	0.348	No	No	1.84
1047	62.93	485.42	1.74	0.76	1.00	134.75	1.06	142.80	0.351	No	No	1.86
1048	62.98	571.92	1.61	0.59	1.00	158.87	1.00	158.87	0.453	No	No	2.00
1049	63.02	620.24	1.47	0.38	1.00	172.30	1.00	172.30	0.556	No	No	2.00
1050	63.07	658.55	1.31	0.19	1.00	182.93	1.00	182.93	0.649	No	No	2.00
1051	63.12	710.78	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1052	63.14	752.36	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1053	63.17	781.30	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1054	63.17	799.36	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1055	63.20	825.98	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1056	63.21	830.83	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1057	63.23	842.91	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1058	63.26	834.75	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1059	63.28	841.52	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1060	63.31	838.10	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1061	63.32	839.38	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1062	63.36	837.12	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1063	63.40	836.85	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_t: Total cone resistance
I_c: Soil behavior type index
Fr: Normalized friction ratio (%)
n: Stress exponent
Q_{tn}: Normalized cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
0.01	2.00	0.00	0.00	0.02	0.00	0.04	2.00	0.00	0.00	0.02	0.00
0.09	2.00	0.00	0.00	0.05	0.00	0.11	2.00	0.00	0.00	0.02	0.00
0.14	2.00	0.00	0.00	0.03	0.00	0.14	2.00	0.00	0.00	0.01	0.00
0.18	2.00	0.00	0.00	0.04	0.00	0.23	2.00	0.00	0.00	0.05	0.00
0.24	2.00	0.00	0.00	0.01	0.00	0.28	2.00	0.00	0.00	0.04	0.00
0.33	2.00	0.00	0.00	0.05	0.00	0.38	2.00	0.00	0.00	0.05	0.00
0.42	2.00	0.00	0.00	0.05	0.00	0.47	2.00	0.00	0.00	0.05	0.00
0.51	2.00	0.00	0.00	0.04	0.00	0.52	2.00	0.00	0.00	0.01	0.00
0.57	2.00	0.00	0.00	0.05	0.00	0.61	2.00	0.00	0.00	0.04	0.00
0.67	2.00	0.00	0.00	0.05	0.00	0.73	2.00	0.00	0.00	0.06	0.00
0.81	2.00	0.00	0.00	0.08	0.00	0.86	2.00	0.00	0.00	0.05	0.00
0.98	2.00	0.00	0.00	0.12	0.00	1.05	2.00	0.00	0.00	0.07	0.00
1.15	2.00	0.00	0.00	0.10	0.00	1.24	2.00	0.00	0.00	0.09	0.00
1.34	2.00	0.00	0.00	0.10	0.00	1.43	2.00	0.00	0.00	0.09	0.00
1.53	2.00	0.00	0.00	0.10	0.00	1.58	2.00	0.00	0.00	0.05	0.00
1.62	2.00	0.00	0.00	0.04	0.00	1.67	2.00	0.00	0.00	0.05	0.00
1.75	2.00	0.00	0.00	0.07	0.00	1.77	2.00	0.00	0.00	0.03	0.00
1.81	2.00	0.00	0.00	0.04	0.00	1.86	2.00	0.00	0.00	0.04	0.00
1.91	2.00	0.00	0.00	0.05	0.00	1.95	2.00	0.00	0.00	0.04	0.00
2.00	2.00	0.00	0.00	0.05	0.00	2.05	2.00	0.00	0.00	0.05	0.00
2.11	2.00	0.00	0.00	0.06	0.00	2.20	2.00	0.00	0.00	0.09	0.00
2.24	2.00	0.00	0.00	0.05	0.00	2.29	2.00	0.00	0.00	0.05	0.00
2.34	2.00	0.00	0.00	0.05	0.00	2.44	2.00	0.00	0.00	0.10	0.00
2.48	2.00	0.00	0.00	0.05	0.00	2.58	2.00	0.00	0.00	0.10	0.00
2.63	2.00	0.00	0.00	0.05	0.00	2.71	2.00	0.00	0.00	0.08	0.00
2.78	2.00	0.00	0.00	0.07	0.00	2.82	2.00	0.00	0.00	0.04	0.00
2.89	2.00	0.00	0.00	0.07	0.00	2.96	2.00	0.00	0.00	0.08	0.00
3.03	2.00	0.00	0.00	0.07	0.00	3.11	2.00	0.00	0.00	0.08	0.00
3.19	2.00	0.00	0.00	0.09	0.00	3.25	2.00	0.00	0.00	0.06	0.00
3.35	2.00	0.00	0.00	0.10	0.00	3.41	2.00	0.00	0.00	0.05	0.00
3.50	2.00	0.00	0.00	0.09	0.00	3.59	2.00	0.00	0.00	0.09	0.00
3.69	2.00	0.00	0.00	0.10	0.00	3.79	2.00	0.00	0.00	0.09	0.00
3.88	2.00	0.00	0.00	0.09	0.00	3.97	2.00	0.00	0.00	0.10	0.00
4.07	2.00	0.00	0.00	0.09	0.00	4.14	2.00	0.00	0.00	0.07	0.00
4.17	2.00	0.00	0.00	0.04	0.00	4.26	2.00	0.00	0.00	0.09	0.00
4.32	2.00	0.00	0.00	0.05	0.00	4.37	2.00	0.00	0.00	0.05	0.00
4.42	2.00	0.00	0.00	0.06	0.00	4.51	2.00	0.00	0.00	0.08	0.00
4.61	2.00	0.00	0.00	0.10	0.00	4.65	2.00	0.00	0.00	0.05	0.00
4.74	2.00	0.00	0.00	0.09	0.00	4.80	2.00	0.00	0.00	0.06	0.00
4.89	2.00	0.00	0.00	0.09	0.00	4.95	2.00	0.00	0.00	0.05	0.00
5.04	2.00	0.00	0.00	0.09	0.00	5.13	2.00	0.00	0.00	0.09	0.00
5.18	2.00	0.00	0.00	0.05	0.00	5.28	2.00	0.00	0.00	0.10	0.00
5.32	2.00	0.00	0.00	0.04	0.00	5.42	2.00	0.00	0.00	0.10	0.00
5.51	2.00	0.00	0.00	0.09	0.00	5.60	2.00	0.00	0.00	0.09	0.00
5.66	2.00	0.00	0.00	0.06	0.00	5.76	2.00	0.00	0.00	0.09	0.00
5.85	2.00	0.00	0.00	0.09	0.00	5.92	2.00	0.00	0.00	0.07	0.00
5.95	2.00	0.00	0.00	0.03	0.00	5.97	2.00	0.00	0.00	0.02	0.00
6.02	2.00	0.00	0.00	0.06	0.00	6.06	2.00	0.00	0.00	0.04	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
6.16	2.00	0.00	0.00	0.10	0.00	6.21	2.00	0.00	0.00	0.04	0.00
6.26	2.00	0.00	0.00	0.06	0.00	6.31	2.00	0.00	0.00	0.04	0.00
6.40	2.00	0.00	0.00	0.09	0.00	6.44	2.00	0.00	0.00	0.04	0.00
6.52	2.00	0.00	0.00	0.08	0.00	6.57	2.00	0.00	0.00	0.05	0.00
6.64	2.00	0.00	0.00	0.07	0.00	6.69	2.00	0.00	0.00	0.05	0.00
6.78	2.00	0.00	0.00	0.09	0.00	6.83	2.00	0.00	0.00	0.05	0.00
6.92	2.00	0.00	0.00	0.09	0.00	6.97	2.00	0.00	0.00	0.05	0.00
7.03	2.00	0.00	0.00	0.05	0.00	7.12	2.00	0.00	0.00	0.09	0.00
7.22	2.00	0.00	0.00	0.10	0.00	7.27	2.00	0.00	0.00	0.05	0.00
7.36	2.00	0.00	0.00	0.09	0.00	7.43	2.00	0.00	0.00	0.08	0.00
7.50	2.00	0.00	0.00	0.07	0.00	7.59	2.00	0.00	0.00	0.09	0.00
7.64	2.00	0.00	0.00	0.05	0.00	7.75	2.00	0.00	0.00	0.10	0.00
7.79	2.00	0.00	0.00	0.04	0.00	7.89	2.00	0.00	0.00	0.10	0.00
7.99	2.00	0.00	0.00	0.10	0.00	8.04	2.00	0.00	0.00	0.05	0.00
8.13	2.00	0.00	0.00	0.09	0.00	8.23	2.00	0.00	0.00	0.10	0.00
8.32	2.00	0.00	0.00	0.09	0.00	8.37	2.00	0.00	0.00	0.05	0.00
8.46	2.00	0.00	0.00	0.09	0.00	8.56	2.00	0.00	0.00	0.10	0.00
8.59	2.00	0.00	0.00	0.02	0.00	8.61	2.00	0.00	0.00	0.03	0.00
8.67	2.00	0.00	0.00	0.05	0.00	8.71	2.00	0.00	0.00	0.04	0.00
8.72	2.00	0.00	0.00	0.01	0.00	8.78	2.00	0.00	0.00	0.06	0.00
8.80	2.00	0.00	0.00	0.02	0.00	8.86	2.00	0.00	0.00	0.05	0.00
8.90	2.00	0.00	0.00	0.04	0.00	8.95	2.00	0.00	0.00	0.05	0.00
8.96	2.00	0.00	0.00	0.01	0.00	9.00	2.00	0.00	0.00	0.04	0.00
9.05	2.00	0.00	0.00	0.05	0.00	9.09	2.00	0.00	0.00	0.04	0.00
9.10	2.00	0.00	0.00	0.01	0.00	9.14	2.00	0.00	0.00	0.05	0.00
9.20	2.00	0.00	0.00	0.05	0.00	9.24	2.00	0.00	0.00	0.04	0.00
9.29	2.00	0.00	0.00	0.05	0.00	9.31	2.00	0.00	0.00	0.02	0.00
9.38	2.00	0.00	0.00	0.07	0.00	9.41	2.00	0.00	0.00	0.03	0.00
9.47	2.00	0.00	0.00	0.06	0.00	9.53	2.00	0.00	0.00	0.05	0.00
9.62	2.00	0.00	0.00	0.09	0.00	9.67	2.00	0.00	0.00	0.05	0.00
9.77	2.00	0.00	0.00	0.10	0.00	9.81	2.00	0.00	0.00	0.05	0.00
9.90	2.00	0.00	0.00	0.08	0.00	9.97	2.00	0.00	0.00	0.08	0.00
10.06	2.00	0.00	0.00	0.09	0.00	10.20	2.00	0.00	0.00	0.14	0.00
10.30	2.00	0.00	0.00	0.09	0.00	10.44	2.00	0.00	0.00	0.14	0.00
10.54	2.00	0.00	0.00	0.10	0.00	10.63	2.00	0.00	0.00	0.09	0.00
10.74	2.00	0.00	0.00	0.11	0.00	10.78	2.00	0.00	0.00	0.04	0.00
10.83	2.00	0.00	0.00	0.05	0.00	10.88	2.00	0.00	0.00	0.05	0.00
10.89	2.00	0.00	0.00	0.02	0.00	10.97	2.00	0.00	0.00	0.08	0.00
11.02	2.00	0.00	0.00	0.05	0.00	11.07	2.00	0.00	0.00	0.05	0.00
11.11	2.00	0.00	0.00	0.05	0.00	11.16	2.00	0.00	0.00	0.05	0.00
11.21	2.00	0.00	0.00	0.05	0.00	11.26	2.00	0.00	0.00	0.04	0.00
11.30	2.00	0.00	0.00	0.05	0.00	11.36	2.00	0.00	0.00	0.05	0.00
11.40	2.00	0.00	0.00	0.05	0.00	11.45	2.00	0.00	0.00	0.04	0.00
11.50	2.00	0.00	0.00	0.05	0.00	11.55	2.00	0.00	0.00	0.05	0.00
11.60	2.00	0.00	0.00	0.05	0.00	11.66	2.00	0.00	0.00	0.07	0.00
11.74	2.00	0.00	0.00	0.08	0.00	11.84	2.00	0.00	0.00	0.10	0.00
11.93	2.00	0.00	0.00	0.09	0.00	12.04	2.00	0.00	0.00	0.11	0.00
12.13	2.00	0.00	0.00	0.09	0.00	12.22	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
12.27	2.00	0.00	0.00	0.04	0.00	12.37	2.00	0.00	0.00	0.10	0.00
12.41	2.00	0.00	0.00	0.05	0.00	12.51	2.00	0.00	0.00	0.09	0.00
12.56	2.00	0.00	0.00	0.05	0.00	12.65	2.00	0.00	0.00	0.09	0.00
12.71	2.00	0.00	0.00	0.06	0.00	12.79	2.00	0.00	0.00	0.08	0.00
12.89	2.00	0.00	0.00	0.10	0.00	12.96	2.00	0.00	0.00	0.06	0.00
13.04	2.00	0.00	0.00	0.08	0.00	13.13	2.00	0.00	0.00	0.09	0.00
13.23	2.00	0.00	0.00	0.10	0.00	13.30	2.00	0.00	0.00	0.07	0.00
13.37	2.00	0.00	0.00	0.07	0.00	13.47	2.00	0.00	0.00	0.10	0.00
13.57	2.00	0.00	0.00	0.10	0.00	13.61	2.00	0.00	0.00	0.04	0.00
13.62	2.00	0.00	0.00	0.02	0.00	13.68	2.00	0.00	0.00	0.06	0.00
13.73	2.00	0.00	0.00	0.05	0.00	13.77	2.00	0.00	0.00	0.04	0.00
13.87	2.00	0.00	0.00	0.10	0.00	13.93	2.00	0.00	0.00	0.06	0.00
14.00	2.00	0.00	0.00	0.07	0.00	14.06	2.00	0.00	0.00	0.06	0.00
14.12	2.00	0.00	0.00	0.06	0.00	14.21	2.00	0.00	0.00	0.09	0.00
14.25	2.00	0.00	0.00	0.05	0.00	14.35	2.00	0.00	0.00	0.10	0.00
14.45	2.00	0.00	0.00	0.09	0.00	14.50	2.00	0.00	0.00	0.05	0.00
14.59	2.00	0.00	0.00	0.09	0.00	14.64	2.00	0.00	0.00	0.05	0.00
14.74	2.00	0.00	0.00	0.10	0.00	14.80	2.00	0.00	0.00	0.06	0.00
14.88	2.00	0.00	0.00	0.09	0.00	14.97	2.00	0.00	0.00	0.09	0.00
15.05	2.00	0.00	0.00	0.08	0.00	15.13	2.00	0.00	0.00	0.09	0.00
15.21	2.00	0.00	0.00	0.08	0.00	15.28	2.00	0.00	0.00	0.07	0.00
15.36	2.00	0.00	0.00	0.08	0.00	15.41	2.00	0.00	0.00	0.04	0.00
15.50	2.00	0.00	0.00	0.10	0.00	15.55	2.00	0.00	0.00	0.05	0.00
15.65	2.00	0.00	0.00	0.10	0.00	15.71	2.00	0.00	0.00	0.06	0.00
15.79	2.00	0.00	0.00	0.08	0.00	15.89	2.00	0.00	0.00	0.10	0.00
15.90	2.00	0.00	0.00	0.01	0.00	15.94	2.00	0.00	0.00	0.04	0.00
16.00	2.00	0.00	0.00	0.06	0.00	16.06	2.00	0.00	0.00	0.06	0.00
16.14	2.00	0.00	0.00	0.08	0.00	16.19	2.00	0.00	0.00	0.05	0.00
16.26	2.00	0.00	0.00	0.07	0.00	16.33	2.00	0.00	0.00	0.07	0.00
16.38	2.00	0.00	0.00	0.05	0.00	16.47	2.00	0.00	0.00	0.09	0.00
16.54	2.00	0.00	0.00	0.06	0.00	16.62	2.00	0.00	0.00	0.08	0.00
16.70	2.00	0.00	0.00	0.09	0.00	16.76	2.00	0.00	0.00	0.06	0.00
16.86	2.00	0.00	0.00	0.10	0.00	16.90	2.00	0.00	0.00	0.04	0.00
16.98	2.00	0.00	0.00	0.08	0.00	17.05	2.00	0.00	0.00	0.07	0.00
17.14	2.00	0.00	0.00	0.09	0.00	17.20	2.00	0.00	0.00	0.05	0.00
17.29	2.00	0.00	0.00	0.10	0.00	17.34	2.00	0.00	0.00	0.05	0.00
17.44	2.00	0.00	0.00	0.10	0.00	17.50	2.00	0.00	0.00	0.06	0.00
17.58	2.00	0.00	0.00	0.09	0.00	17.64	2.00	0.00	0.00	0.06	0.00
17.75	2.00	0.00	0.00	0.11	0.00	17.82	2.00	0.00	0.00	0.06	0.00
17.89	2.00	0.00	0.00	0.07	0.00	17.89	2.00	0.00	0.00	0.00	0.00
17.96	2.00	0.00	0.00	0.07	0.00	18.02	2.00	0.00	0.00	0.05	0.00
18.07	2.00	0.00	0.00	0.05	0.00	18.17	2.00	0.00	0.00	0.10	0.00
18.22	2.00	0.00	0.00	0.05	0.00	18.30	2.00	0.00	0.00	0.09	0.00
18.36	2.00	0.00	0.00	0.06	0.00	18.42	2.00	0.00	0.00	0.06	0.00
18.50	2.00	0.00	0.00	0.08	0.00	18.56	2.00	0.00	0.00	0.06	0.00
18.62	2.00	0.00	0.00	0.06	0.00	18.69	2.00	0.00	0.00	0.07	0.00
18.76	2.00	0.00	0.00	0.07	0.00	18.84	2.00	0.00	0.00	0.08	0.00
18.89	2.00	0.00	0.00	0.05	0.00	18.98	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
19.05	2.00	0.00	0.00	0.06	0.00	19.12	2.00	0.00	0.00	0.07	0.00
19.18	2.00	0.00	0.00	0.06	0.00	19.24	2.00	0.00	0.00	0.06	0.00
19.32	2.00	0.00	0.00	0.07	0.00	19.38	2.00	0.00	0.00	0.06	0.00
19.46	2.00	0.00	0.00	0.09	0.00	19.54	2.00	0.00	0.00	0.07	0.00
19.62	2.00	0.00	0.00	0.08	0.00	19.70	2.00	0.00	0.00	0.08	0.00
19.80	2.00	0.00	0.00	0.10	0.00	19.85	2.00	0.00	0.00	0.05	0.00
19.94	2.00	0.00	0.00	0.09	0.00	20.03	2.00	0.00	0.00	0.09	0.00
20.13	2.00	0.00	0.00	0.10	0.00	20.19	2.00	0.00	0.00	0.06	0.00
20.29	2.00	0.00	0.00	0.10	0.00	20.39	2.00	0.00	0.00	0.10	0.00
20.43	2.00	0.00	0.00	0.03	0.00	20.47	2.00	0.00	0.00	0.05	0.00
20.52	2.00	0.00	0.00	0.05	0.00	20.61	2.00	0.00	0.00	0.09	0.00
20.66	2.00	0.00	0.00	0.05	0.00	20.71	2.00	0.00	0.00	0.05	0.00
20.77	2.00	0.00	0.00	0.06	0.00	20.85	2.00	0.00	0.00	0.08	0.00
20.91	2.00	0.00	0.00	0.05	0.00	21.00	2.00	0.00	0.00	0.09	0.00
21.05	2.00	0.00	0.00	0.05	0.00	21.11	2.00	0.00	0.00	0.06	0.00
21.19	2.00	0.00	0.00	0.08	0.00	21.24	2.00	0.00	0.00	0.05	0.00
21.34	2.00	0.00	0.00	0.09	0.00	21.39	2.00	0.00	0.00	0.05	0.00
21.48	2.00	0.00	0.00	0.10	0.00	21.53	2.00	0.00	0.00	0.05	0.00
21.64	2.00	0.00	0.00	0.11	0.00	21.72	2.00	0.00	0.00	0.08	0.00
21.81	2.00	0.00	0.00	0.09	0.00	21.89	2.00	0.00	0.00	0.08	0.00
21.97	2.00	0.00	0.00	0.08	0.00	22.05	2.00	0.00	0.00	0.09	0.00
22.12	2.00	0.00	0.00	0.07	0.00	22.13	2.00	0.00	0.00	0.01	0.00
22.18	2.00	0.00	0.00	0.05	0.00	22.22	2.00	0.00	0.00	0.04	0.00
22.28	2.00	0.00	0.00	0.06	0.00	22.33	2.00	0.00	0.00	0.05	0.00
22.38	2.00	0.00	0.00	0.05	0.00	22.41	2.00	0.00	0.00	0.03	0.00
22.51	2.00	0.00	0.00	0.10	0.00	22.56	2.00	0.00	0.00	0.05	0.00
22.61	2.00	0.00	0.00	0.05	0.00	22.65	2.00	0.00	0.00	0.04	0.00
22.71	2.00	0.00	0.00	0.05	0.00	22.76	2.00	0.00	0.00	0.06	0.00
22.85	2.00	0.00	0.00	0.08	0.00	22.89	2.00	0.00	0.00	0.05	0.00
22.99	2.00	0.00	0.00	0.10	0.00	23.04	2.00	0.00	0.00	0.05	0.00
23.12	2.00	0.00	0.00	0.08	0.00	23.18	2.00	0.00	0.00	0.07	0.00
23.24	2.00	0.00	0.00	0.06	0.00	23.33	2.00	0.00	0.00	0.09	0.00
23.38	2.00	0.00	0.00	0.05	0.00	23.47	2.00	0.00	0.00	0.09	0.00
23.52	2.00	0.00	0.00	0.05	0.00	23.61	2.00	0.00	0.00	0.09	0.00
23.68	2.00	0.00	0.00	0.07	0.00	23.76	2.00	0.00	0.00	0.08	0.00
23.83	2.00	0.00	0.00	0.07	0.00	23.90	2.00	0.00	0.00	0.08	0.00
23.97	2.00	0.00	0.00	0.07	0.00	24.05	2.00	0.00	0.00	0.08	0.00
24.10	2.00	0.00	0.00	0.05	0.00	24.19	2.00	0.00	0.00	0.09	0.00
24.27	2.00	0.00	0.00	0.08	0.00	24.34	2.00	0.00	0.00	0.07	0.00
24.43	2.00	0.00	0.00	0.09	0.00	24.48	2.00	0.00	0.00	0.05	0.00
24.57	2.00	0.00	0.00	0.09	0.00	24.62	2.00	0.00	0.00	0.05	0.00
24.72	2.00	0.00	0.00	0.09	0.00	24.81	2.00	0.00	0.00	0.10	0.00
24.86	2.00	0.00	0.00	0.05	0.00	24.95	2.00	0.00	0.00	0.09	0.00
25.01	2.00	0.00	0.00	0.06	0.00	25.02	2.00	0.00	0.00	0.01	0.00
25.05	2.00	0.00	0.00	0.03	0.00	25.11	2.00	0.00	0.00	0.06	0.00
25.15	2.00	0.00	0.00	0.04	0.00	25.21	2.00	0.00	0.00	0.06	0.00
25.25	2.00	0.00	0.00	0.04	0.00	25.30	2.00	0.00	0.00	0.05	0.00
25.40	2.00	0.00	0.00	0.10	0.00	25.45	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
25.52	2.00	0.00	0.00	0.07	0.00	25.60	2.00	0.00	0.00	0.07	0.00
25.66	2.00	0.00	0.00	0.06	0.00	25.74	2.00	0.00	0.00	0.08	0.00
25.80	2.00	0.00	0.00	0.06	0.00	25.88	2.00	0.00	0.00	0.07	0.00
25.94	2.00	0.00	0.00	0.07	0.00	26.02	2.00	0.00	0.00	0.08	0.00
26.09	2.00	0.00	0.00	0.07	0.00	26.17	2.00	0.00	0.00	0.08	0.00
26.23	2.00	0.00	0.00	0.06	0.00	26.29	2.00	0.00	0.00	0.06	0.00
26.37	2.00	0.00	0.00	0.08	0.00	26.46	2.00	0.00	0.00	0.08	0.00
26.55	2.00	0.00	0.00	0.09	0.00	26.60	2.00	0.00	0.00	0.05	0.00
26.70	2.00	0.00	0.00	0.10	0.00	26.78	2.00	0.00	0.00	0.08	0.00
26.87	2.00	0.00	0.00	0.09	0.00	26.94	2.00	0.00	0.00	0.06	0.00
27.03	2.00	0.00	0.00	0.10	0.00	27.13	2.00	0.00	0.00	0.10	0.00
27.18	2.00	0.00	0.00	0.05	0.00	27.27	2.00	0.00	0.00	0.09	0.00
27.32	2.00	0.00	0.00	0.05	0.00	27.37	2.00	0.00	0.00	0.05	0.00
27.41	2.00	0.00	0.00	0.05	0.00	27.46	2.00	0.00	0.00	0.05	0.00
27.51	2.00	0.00	0.00	0.05	0.00	27.61	2.00	0.00	0.00	0.09	0.00
27.66	2.00	0.00	0.00	0.05	0.00	27.73	2.00	0.00	0.00	0.07	0.00
27.80	2.00	0.00	0.00	0.07	0.00	27.88	2.00	0.00	0.00	0.08	0.00
27.96	2.00	0.00	0.00	0.09	0.00	28.04	2.00	0.00	0.00	0.08	0.00
28.12	2.00	0.00	0.00	0.08	0.00	28.18	2.00	0.00	0.00	0.06	0.00
28.27	2.00	0.00	0.00	0.09	0.00	28.32	2.00	0.00	0.00	0.05	0.00
28.42	2.00	0.00	0.00	0.10	0.00	28.47	2.00	0.00	0.00	0.05	0.00
28.61	2.00	0.00	0.00	0.14	0.00	28.67	2.00	0.00	0.00	0.06	0.00
28.75	2.00	0.00	0.00	0.09	0.00	28.81	2.00	0.00	0.00	0.05	0.00
28.90	2.00	0.00	0.00	0.10	0.00	29.00	2.00	0.00	0.00	0.09	0.00
29.05	2.00	0.00	0.00	0.05	0.00	29.10	2.00	0.00	0.00	0.05	0.00
29.15	2.00	0.00	0.00	0.05	0.00	29.24	2.00	0.00	0.00	0.09	0.00
29.29	2.00	0.00	0.00	0.05	0.00	29.37	2.00	0.00	0.00	0.07	0.00
29.43	2.00	0.00	0.00	0.06	0.00	29.53	2.00	0.00	0.00	0.10	0.00
29.62	2.00	0.00	0.00	0.09	0.00	29.68	2.00	0.00	0.00	0.06	0.00
29.80	2.00	0.00	0.00	0.12	0.00	29.91	2.00	0.00	0.00	0.12	0.00
30.00	1.03	0.00	0.00	0.09	0.00	30.07	1.04	0.00	0.00	0.07	0.00
30.15	1.04	0.00	0.00	0.08	0.00	30.21	1.04	0.00	0.00	0.07	0.00
30.26	1.04	0.00	0.00	0.05	0.00	30.31	1.03	0.00	0.00	0.05	0.00
30.38	1.02	0.00	0.00	0.07	0.00	30.45	1.01	0.00	0.00	0.07	0.00
30.50	1.00	0.00	0.00	0.05	0.00	30.55	0.99	0.01	1521965149 4	0.05	0.00
30.64	0.97	0.03	956.57	0.09	0.00	30.70	0.94	0.06	33.53	0.05	0.00
30.79	0.93	0.07	12.83	0.09	0.01	30.84	0.91	0.09	8.56	0.05	0.01
30.93	0.91	0.09	7.83	0.09	0.01	30.98	0.91	0.09	7.97	0.05	0.01
31.05	0.92	0.08	11.40	0.06	0.01	31.13	0.94	0.06	32.36	0.08	0.01
31.17	0.98	0.02	54585.68	0.05	0.00	31.27	1.03	0.00	0.00	0.10	0.00
31.32	1.13	0.00	0.00	0.05	0.00	31.41	1.23	0.00	0.00	0.10	0.00
31.46	1.31	0.00	0.00	0.05	0.00	31.52	1.35	0.00	0.00	0.06	0.00
31.61	1.33	0.00	0.00	0.08	0.00	31.66	1.28	0.00	0.00	0.06	0.00
31.75	1.19	0.00	0.00	0.09	0.00	31.80	1.11	0.00	0.00	0.05	0.00
31.90	1.03	0.00	0.00	0.10	0.00	31.94	0.99	0.01	83727543. 34	0.05	0.00
32.04	0.99	0.01	2535344.1 6	0.10	0.00	32.09	1.04	0.00	0.00	0.04	0.00
32.20	1.07	0.00	0.00	0.11	0.00	32.24	1.09	0.00	0.00	0.04	0.00
32.28	1.09	0.00	0.00	0.04	0.00	32.29	1.11	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
32.30	1.12	0.00	0.00	0.01	0.00	32.40	1.13	0.00	0.00	0.10	0.00
32.45	1.14	0.00	0.00	0.04	0.00	32.55	1.13	0.00	0.00	0.10	0.00
32.59	1.13	0.00	0.00	0.05	0.00	32.69	1.13	0.00	0.00	0.10	0.00
32.76	1.14	0.00	0.00	0.07	0.00	32.84	1.16	0.00	0.00	0.08	0.00
32.90	1.17	0.00	0.00	0.07	0.00	32.98	1.19	0.00	0.00	0.08	0.00
33.06	1.19	0.00	0.00	0.08	0.00	33.12	1.20	0.00	0.00	0.06	0.00
33.22	1.21	0.00	0.00	0.10	0.00	33.31	1.21	0.00	0.00	0.09	0.00
33.37	1.21	0.00	0.00	0.05	0.00	33.46	1.20	0.00	0.00	0.09	0.00
33.55	1.20	0.00	0.00	0.09	0.00	33.65	1.20	0.00	0.00	0.10	0.00
33.70	1.20	0.00	0.00	0.05	0.00	33.79	1.20	0.00	0.00	0.09	0.00
33.89	1.19	0.00	0.00	0.10	0.00	33.99	1.18	0.00	0.00	0.09	0.00
34.04	1.16	0.00	0.00	0.05	0.00	34.13	1.15	0.00	0.00	0.09	0.00
34.23	1.13	0.00	0.00	0.10	0.00	34.32	1.12	0.00	0.00	0.09	0.00
34.37	1.11	0.00	0.00	0.05	0.00	34.47	1.11	0.00	0.00	0.10	0.00
34.55	2.00	0.00	0.00	0.08	0.00	34.63	2.00	0.00	0.00	0.08	0.00
34.73	2.00	0.00	0.00	0.10	0.00	34.80	2.00	0.00	0.00	0.08	0.00
34.90	2.00	0.00	0.00	0.09	0.00	35.00	2.00	0.00	0.00	0.10	0.00
35.12	2.00	0.00	0.00	0.13	0.00	35.20	2.00	0.00	0.00	0.07	0.00
35.33	2.00	0.00	0.00	0.13	0.00	35.41	2.00	0.00	0.00	0.07	0.00
35.44	2.00	0.00	0.00	0.03	0.00	35.48	2.00	0.00	0.00	0.05	0.00
35.57	2.00	0.00	0.00	0.09	0.00	35.62	2.00	0.00	0.00	0.05	0.00
35.67	2.00	0.00	0.00	0.05	0.00	35.71	2.00	0.00	0.00	0.04	0.00
35.82	2.00	0.00	0.00	0.10	0.00	35.86	2.00	0.00	0.00	0.05	0.00
35.93	2.00	0.00	0.00	0.07	0.00	36.01	2.00	0.00	0.00	0.08	0.00
36.06	2.00	0.00	0.00	0.05	0.00	36.12	2.00	0.00	0.00	0.06	0.00
36.18	2.00	0.00	0.00	0.06	0.00	36.25	2.00	0.00	0.00	0.07	0.00
36.30	2.00	0.00	0.00	0.05	0.00	36.39	2.00	0.00	0.00	0.10	0.00
36.44	2.00	0.00	0.00	0.05	0.00	36.53	2.00	0.00	0.00	0.09	0.00
36.59	2.00	0.00	0.00	0.05	0.00	36.68	2.00	0.00	0.00	0.09	0.00
36.75	2.00	0.00	0.00	0.07	0.00	36.83	2.00	0.00	0.00	0.08	0.00
36.90	2.00	0.00	0.00	0.07	0.00	36.97	2.00	0.00	0.00	0.07	0.00
37.02	2.00	0.00	0.00	0.05	0.00	37.04	2.00	0.00	0.00	0.02	0.00
37.08	1.93	0.00	0.00	0.04	0.00	37.17	1.96	0.00	0.00	0.09	0.00
37.27	1.85	0.00	0.00	0.10	0.00	37.37	1.72	0.00	0.00	0.09	0.00
37.42	1.62	0.00	0.00	0.05	0.00	37.51	1.57	0.00	0.00	0.09	0.00
37.58	1.56	0.00	0.00	0.07	0.00	37.66	1.57	0.00	0.00	0.07	0.00
37.76	1.59	0.00	0.00	0.10	0.00	37.85	1.62	0.00	0.00	0.09	0.00
37.93	1.64	0.00	0.00	0.08	0.00	38.04	1.66	0.00	0.00	0.11	0.00
38.13	1.67	0.00	0.00	0.09	0.00	38.18	1.67	0.00	0.00	0.05	0.00
38.28	1.65	0.00	0.00	0.10	0.00	38.37	1.61	0.00	0.00	0.09	0.00
38.47	1.57	0.00	0.00	0.09	0.00	38.57	1.53	0.00	0.00	0.10	0.00
38.62	1.49	0.00	0.00	0.04	0.00	38.72	1.37	0.00	0.00	0.10	0.00
38.78	1.29	0.00	0.00	0.06	0.00	38.81	1.24	0.00	0.00	0.02	0.00
38.86	1.24	0.00	0.00	0.05	0.00	38.91	1.22	0.00	0.00	0.05	0.00
38.95	1.18	0.00	0.00	0.05	0.00	39.05	1.15	0.00	0.00	0.10	0.00
39.09	1.12	0.00	0.00	0.05	0.00	39.14	1.11	0.00	0.00	0.05	0.00
39.24	1.10	0.00	0.00	0.10	0.00	39.29	1.09	0.00	0.00	0.05	0.00
39.39	1.10	0.00	0.00	0.10	0.00	39.43	1.10	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
39.53	1.09	0.00	0.00	0.10	0.00	39.57	1.08	0.00	0.00	0.04	0.00
39.68	1.09	0.00	0.00	0.10	0.00	39.73	1.08	0.00	0.00	0.05	0.00
39.81	1.06	0.00	0.00	0.08	0.00	39.89	1.01	0.00	0.00	0.08	0.00
39.96	0.95	0.05	61.50	0.07	0.00	40.06	0.91	0.09	7.89	0.10	0.01
40.15	0.90	0.10	5.93	0.09	0.01	40.20	0.89	0.11	5.36	0.06	0.01
40.24	0.90	0.10	6.39	0.04	0.00	40.26	0.91	0.09	8.01	0.01	0.00
40.27	0.91	0.09	8.48	0.02	0.00	40.37	0.92	0.08	10.34	0.09	0.01
40.42	0.93	0.07	17.38	0.05	0.00	40.52	0.94	0.06	31.57	0.10	0.01
40.56	0.96	0.04	178.66	0.04	0.00	40.66	0.99	0.01	470504.39	0.10	0.00
40.70	1.03	0.00	0.00	0.05	0.00	40.75	1.10	0.00	0.00	0.05	0.00
40.85	1.20	0.00	0.00	0.10	0.00	40.91	1.31	0.00	0.00	0.06	0.00
40.96	1.43	0.00	0.00	0.05	0.00	41.04	1.55	0.00	0.00	0.08	0.00
41.09	1.70	0.00	0.00	0.05	0.00	41.18	1.83	0.00	0.00	0.09	0.00
41.23	1.94	0.00	0.00	0.05	0.00	41.29	2.00	0.00	0.00	0.06	0.00
41.38	2.00	0.00	0.00	0.09	0.00	41.42	2.00	0.00	0.00	0.05	0.00
41.52	1.96	0.00	0.00	0.10	0.00	41.57	1.91	0.00	0.00	0.05	0.00
41.62	1.87	0.00	0.00	0.05	0.00	41.71	1.84	0.00	0.00	0.09	0.00
41.76	1.82	0.00	0.00	0.04	0.00	41.84	1.81	0.00	0.00	0.09	0.00
41.91	1.81	0.00	0.00	0.07	0.00	41.95	1.82	0.00	0.00	0.05	0.00
42.01	1.85	0.00	0.00	0.06	0.00	42.10	1.88	0.00	0.00	0.08	0.00
42.15	1.92	0.00	0.00	0.05	0.00	42.24	1.96	0.00	0.00	0.09	0.00
42.28	1.97	0.00	0.00	0.04	0.00	42.39	1.95	0.00	0.00	0.10	0.00
42.43	1.93	0.00	0.00	0.04	0.00	42.50	1.91	0.00	0.00	0.07	0.00
42.58	1.88	0.00	0.00	0.08	0.00	42.65	1.74	0.00	0.00	0.07	0.00
42.70	1.68	0.00	0.00	0.06	0.00	42.73	1.64	0.00	0.00	0.02	0.00
42.77	1.73	0.00	0.00	0.04	0.00	42.82	1.78	0.00	0.00	0.05	0.00
42.87	1.86	0.00	0.00	0.05	0.00	42.91	1.97	0.00	0.00	0.04	0.00
42.97	2.00	0.00	0.00	0.05	0.00	43.02	2.00	0.00	0.00	0.05	0.00
43.06	2.00	0.00	0.00	0.05	0.00	43.11	2.00	0.00	0.00	0.04	0.00
43.17	2.00	0.00	0.00	0.06	0.00	43.21	2.00	0.00	0.00	0.04	0.00
43.29	2.00	0.00	0.00	0.08	0.00	43.34	2.00	0.00	0.00	0.05	0.00
43.39	2.00	0.00	0.00	0.06	0.00	43.45	2.00	0.00	0.00	0.05	0.00
43.51	2.00	0.00	0.00	0.06	0.00	43.59	2.00	0.00	0.00	0.08	0.00
43.64	2.00	0.00	0.00	0.05	0.00	43.70	2.00	0.00	0.00	0.06	0.00
43.78	2.00	0.00	0.00	0.09	0.00	43.88	2.00	0.00	0.00	0.10	0.00
43.94	2.00	0.00	0.00	0.06	0.00	44.04	2.00	0.00	0.00	0.10	0.00
44.07	2.00	0.00	0.00	0.03	0.00	44.12	2.00	0.00	0.00	0.05	0.00
44.16	1.98	0.00	0.00	0.04	0.00	44.21	1.92	0.00	0.00	0.05	0.00
44.26	1.86	0.00	0.00	0.05	0.00	44.31	1.79	0.00	0.00	0.05	0.00
44.35	1.73	0.00	0.00	0.04	0.00	44.40	1.67	0.00	0.00	0.05	0.00
44.45	1.62	0.00	0.00	0.05	0.00	44.50	1.59	0.00	0.00	0.05	0.00
44.54	1.56	0.00	0.00	0.04	0.00	44.60	1.53	0.00	0.00	0.06	0.00
44.64	1.50	0.00	0.00	0.05	0.00	44.69	1.48	0.00	0.00	0.05	0.00
44.74	1.47	0.00	0.00	0.05	0.00	44.79	1.47	0.00	0.00	0.04	0.00
44.83	1.47	0.00	0.00	0.05	0.00	44.88	1.48	0.00	0.00	0.05	0.00
44.93	1.51	0.00	0.00	0.05	0.00	44.98	1.54	0.00	0.00	0.05	0.00
45.03	1.56	0.00	0.00	0.05	0.00	45.08	1.57	0.00	0.00	0.06	0.00
45.16	1.58	0.00	0.00	0.08	0.00	45.19	1.58	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
45.27	1.57	0.00	0.00	0.08	0.00	45.32	1.55	0.00	0.00	0.05	0.00
45.37	1.50	0.00	0.00	0.05	0.00	45.45	1.44	0.00	0.00	0.09	0.00
45.51	1.35	0.00	0.00	0.05	0.00	45.56	2.00	0.00	0.00	0.05	0.00
45.61	2.00	0.00	0.00	0.05	0.00	45.69	2.00	0.00	0.00	0.08	0.00
45.75	2.00	0.00	0.00	0.06	0.00	45.81	2.00	0.00	0.00	0.07	0.00
45.89	2.00	0.00	0.00	0.08	0.00	45.94	2.00	0.00	0.00	0.05	0.00
46.04	2.00	0.00	0.00	0.10	0.00	46.08	2.00	0.00	0.00	0.04	0.00
46.15	2.00	0.00	0.00	0.06	0.00	46.17	2.00	0.00	0.00	0.02	0.00
46.18	2.00	0.00	0.00	0.01	0.00	46.23	2.00	0.00	0.00	0.05	0.00
46.27	2.00	0.00	0.00	0.05	0.00	46.32	2.00	0.00	0.00	0.05	0.00
46.41	2.00	0.00	0.00	0.09	0.00	46.47	2.00	0.00	0.00	0.06	0.00
46.52	2.00	0.00	0.00	0.05	0.00	46.56	2.00	0.00	0.00	0.04	0.00
46.65	2.00	0.00	0.00	0.09	0.00	46.71	2.00	0.00	0.00	0.06	0.00
46.76	2.00	0.00	0.00	0.05	0.00	46.85	2.00	0.00	0.00	0.09	0.00
46.90	2.00	0.00	0.00	0.05	0.00	46.99	2.00	0.00	0.00	0.09	0.00
47.04	2.00	0.00	0.00	0.06	0.00	47.10	2.00	0.00	0.00	0.05	0.00
47.16	2.00	0.00	0.00	0.06	0.00	47.23	2.00	0.00	0.00	0.07	0.00
47.30	2.00	0.00	0.00	0.06	0.00	47.38	2.00	0.00	0.00	0.09	0.00
47.43	2.00	0.00	0.00	0.05	0.00	47.52	2.00	0.00	0.00	0.09	0.00
47.59	2.00	0.00	0.00	0.07	0.00	47.66	2.00	0.00	0.00	0.07	0.00
47.77	2.00	0.00	0.00	0.10	0.00	47.82	2.00	0.00	0.00	0.05	0.00
47.91	2.00	0.00	0.00	0.08	0.00	47.93	2.00	0.00	0.00	0.03	0.00
47.97	2.00	0.00	0.00	0.04	0.00	48.02	2.00	0.00	0.00	0.05	0.00
48.07	2.00	0.00	0.00	0.05	0.00	48.12	2.00	0.00	0.00	0.05	0.00
48.19	2.00	0.00	0.00	0.07	0.00	48.23	2.00	0.00	0.00	0.04	0.00
48.31	2.00	0.00	0.00	0.08	0.00	48.35	2.00	0.00	0.00	0.05	0.00
48.40	2.00	0.00	0.00	0.05	0.00	48.45	2.00	0.00	0.00	0.05	0.00
48.50	2.00	0.00	0.00	0.05	0.00	48.55	2.00	0.00	0.00	0.05	0.00
48.59	2.00	0.00	0.00	0.04	0.00	48.67	2.00	0.00	0.00	0.08	0.00
48.73	2.00	0.00	0.00	0.05	0.00	48.78	2.00	0.00	0.00	0.06	0.00
48.83	2.00	0.00	0.00	0.05	0.00	48.91	2.00	0.00	0.00	0.07	0.00
48.98	2.00	0.00	0.00	0.07	0.00	49.03	2.00	0.00	0.00	0.05	0.00
49.12	2.00	0.00	0.00	0.09	0.00	49.17	2.00	0.00	0.00	0.05	0.00
49.27	2.00	0.00	0.00	0.09	0.00	49.31	2.00	0.00	0.00	0.05	0.00
49.38	2.00	0.00	0.00	0.06	0.00	49.45	2.00	0.00	0.00	0.08	0.00
49.51	2.00	0.00	0.00	0.05	0.00	49.54	2.00	0.00	0.00	0.03	0.00
49.59	2.00	0.00	0.00	0.05	0.00	49.64	2.00	0.00	0.00	0.05	0.00
49.73	2.00	0.00	0.00	0.10	0.00	49.83	2.00	0.00	0.00	0.10	0.00
49.92	2.00	0.00	0.00	0.10	0.00	49.98	2.00	0.00	0.00	0.05	0.00
50.07	2.00	0.00	0.00	0.09	0.00	50.16	2.00	0.00	0.00	0.09	0.00
50.24	2.00	0.00	0.00	0.09	0.00	50.32	2.00	0.00	0.00	0.08	0.00
50.41	2.00	0.00	0.00	0.09	0.00	50.50	2.00	0.00	0.00	0.09	0.00
50.56	2.00	0.00	0.00	0.06	0.00	50.66	2.00	0.00	0.00	0.10	0.00
50.74	2.00	0.00	0.00	0.09	0.00	50.84	2.00	0.00	0.00	0.10	0.00
50.93	2.00	0.00	0.00	0.09	0.00	50.98	2.00	0.00	0.00	0.05	0.00
51.08	2.00	0.00	0.00	0.09	0.00	51.17	2.00	0.00	0.00	0.10	0.00
51.24	2.00	0.00	0.00	0.06	0.00	51.34	2.00	0.00	0.00	0.10	0.00
51.41	2.00	0.00	0.00	0.07	0.00	51.51	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
51.58	2.00	0.00	0.00	0.07	0.00	51.68	2.00	0.00	0.00	0.10	0.00
51.79	2.00	0.00	0.00	0.11	0.00	51.82	2.00	0.00	0.00	0.03	0.00
51.85	2.00	0.00	0.00	0.03	0.00	51.91	2.00	0.00	0.00	0.06	0.00
52.00	2.00	0.00	0.00	0.09	0.00	52.05	2.00	0.00	0.00	0.05	0.00
52.10	2.00	0.00	0.00	0.06	0.00	52.19	2.00	0.00	0.00	0.09	0.00
52.28	2.00	0.00	0.00	0.09	0.00	52.34	2.00	0.00	0.00	0.06	0.00
52.42	2.00	0.00	0.00	0.08	0.00	52.48	2.00	0.00	0.00	0.06	0.00
52.57	2.00	0.00	0.00	0.09	0.00	52.62	2.00	0.00	0.00	0.05	0.00
52.69	2.00	0.00	0.00	0.07	0.00	52.77	2.00	0.00	0.00	0.08	0.00
52.87	2.00	0.00	0.00	0.10	0.00	52.91	2.00	0.00	0.00	0.04	0.00
53.01	2.00	0.00	0.00	0.10	0.00	53.10	2.00	0.00	0.00	0.09	0.00
53.16	2.00	0.00	0.00	0.06	0.00	53.25	2.00	0.00	0.00	0.09	0.00
53.29	2.00	0.00	0.00	0.04	0.00	53.38	2.00	0.00	0.00	0.09	0.00
53.42	2.00	0.00	0.00	0.04	0.00	53.47	2.00	0.00	0.00	0.05	0.00
53.52	2.00	0.00	0.00	0.05	0.00	53.58	2.00	0.00	0.00	0.05	0.00
53.66	2.00	0.00	0.00	0.08	0.00	53.75	2.00	0.00	0.00	0.09	0.00
53.81	2.00	0.00	0.00	0.05	0.00	53.87	2.00	0.00	0.00	0.06	0.00
53.95	2.00	0.00	0.00	0.08	0.00	54.01	2.00	0.00	0.00	0.06	0.00
54.06	2.00	0.00	0.00	0.05	0.00	54.15	2.00	0.00	0.00	0.08	0.00
54.20	2.00	0.00	0.00	0.06	0.00	54.29	2.00	0.00	0.00	0.08	0.00
54.34	2.00	0.00	0.00	0.05	0.00	54.43	2.00	0.00	0.00	0.09	0.00
54.45	2.00	0.00	0.00	0.02	0.00	54.48	2.00	0.00	0.00	0.03	0.00
54.52	2.00	0.00	0.00	0.03	0.00	54.53	2.00	0.00	0.00	0.01	0.00
54.58	0.75	0.25	1.21	0.05	0.01	54.62	0.80	0.20	1.63	0.04	0.00
54.65	0.84	0.16	2.38	0.03	0.00	54.70	0.88	0.12	4.34	0.04	0.00
54.76	0.92	0.08	9.38	0.06	0.00	54.77	0.92	0.08	12.33	0.01	0.00
54.82	0.93	0.07	15.78	0.05	0.00	54.87	0.94	0.06	21.07	0.05	0.00
54.88	0.94	0.06	33.79	0.01	0.00	54.91	0.95	0.05	61.01	0.03	0.00
54.96	0.98	0.02	4897.12	0.05	0.00	54.97	1.04	0.00	0.00	0.01	0.00
55.03	1.14	0.00	0.00	0.06	0.00	55.09	1.25	0.00	0.00	0.06	0.00
55.15	1.26	0.00	0.00	0.06	0.00	55.20	1.28	0.00	0.00	0.05	0.00
55.25	1.26	0.00	0.00	0.05	0.00	55.30	1.44	0.00	0.00	0.05	0.00
55.34	1.57	0.00	0.00	0.05	0.00	55.39	1.89	0.00	0.00	0.04	0.00
55.40	2.00	0.00	0.00	0.01	0.00	55.44	2.00	0.00	0.00	0.04	0.00
55.44	2.00	0.00	0.00	0.01	0.00	55.49	2.00	0.00	0.00	0.05	0.00
55.54	2.00	0.00	0.00	0.05	0.00	55.59	2.00	0.00	0.00	0.05	0.00
55.63	2.00	0.00	0.00	0.04	0.00	55.64	2.00	0.00	0.00	0.01	0.00
55.68	2.00	0.00	0.00	0.04	0.00	55.69	2.00	0.00	0.00	0.01	0.00
55.69	2.00	0.00	0.00	0.01	0.00	55.71	2.00	0.00	0.00	0.02	0.00
55.76	2.00	0.00	0.00	0.05	0.00	55.78	2.00	0.00	0.00	0.02	0.00
55.81	2.00	0.00	0.00	0.04	0.00	55.85	2.00	0.00	0.00	0.04	0.00
55.86	2.00	0.00	0.00	0.01	0.00	55.91	2.00	0.00	0.00	0.05	0.00
55.92	2.00	0.00	0.00	0.01	0.00	55.96	2.00	0.00	0.00	0.04	0.00
55.97	2.00	0.00	0.00	0.01	0.00	56.00	2.00	0.00	0.00	0.03	0.00
56.01	2.00	0.00	0.00	0.01	0.00	56.03	2.00	0.00	0.00	0.02	0.00
56.05	2.00	0.00	0.00	0.02	0.00	56.10	2.00	0.00	0.00	0.05	0.00
56.12	2.00	0.00	0.00	0.02	0.00	56.16	2.00	0.00	0.00	0.04	0.00
56.17	2.00	0.00	0.00	0.02	0.00	56.20	2.00	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
56.22	2.00	0.00	0.00	0.02	0.00	56.24	2.00	0.00	0.00	0.03	0.00
56.30	2.00	0.00	0.00	0.06	0.00	56.31	2.00	0.00	0.00	0.01	0.00
56.34	2.00	0.00	0.00	0.03	0.00	56.39	2.00	0.00	0.00	0.05	0.00
56.45	2.00	0.00	0.00	0.06	0.00	56.48	2.00	0.00	0.00	0.03	0.00
56.49	2.00	0.00	0.00	0.01	0.00	56.53	2.00	0.00	0.00	0.04	0.00
56.58	2.00	0.00	0.00	0.05	0.00	56.63	2.00	0.00	0.00	0.05	0.00
56.68	2.00	0.00	0.00	0.04	0.00	56.73	2.00	0.00	0.00	0.05	0.00
56.78	2.00	0.00	0.00	0.05	0.00	56.83	2.00	0.00	0.00	0.05	0.00
56.89	2.00	0.00	0.00	0.07	0.00	56.95	2.00	0.00	0.00	0.06	0.00
56.99	2.00	0.00	0.00	0.04	0.00	57.01	2.00	0.00	0.00	0.01	0.00
57.04	2.00	0.00	0.00	0.04	0.00	57.09	2.00	0.00	0.00	0.05	0.00
57.11	2.00	0.00	0.00	0.02	0.00	57.13	2.00	0.00	0.00	0.03	0.00
57.18	2.00	0.00	0.00	0.04	0.00	57.19	2.00	0.00	0.00	0.01	0.00
57.21	2.00	0.00	0.00	0.03	0.00	57.24	2.00	0.00	0.00	0.02	0.00
57.28	2.00	0.00	0.00	0.05	0.00	57.32	2.00	0.00	0.00	0.04	0.00
57.35	2.00	0.00	0.00	0.04	0.00	57.38	2.00	0.00	0.00	0.03	0.00
57.43	2.00	0.00	0.00	0.04	0.00	57.48	2.00	0.00	0.00	0.05	0.00
57.52	1.85	0.00	0.00	0.05	0.00	57.57	1.80	0.00	0.00	0.05	0.00
57.62	1.93	0.00	0.00	0.05	0.00	57.68	2.00	0.00	0.00	0.06	0.00
57.76	2.00	0.00	0.00	0.08	0.00	57.81	2.00	0.00	0.00	0.05	0.00
57.86	2.00	0.00	0.00	0.05	0.00	57.89	2.00	0.00	0.00	0.03	0.00
57.91	2.00	0.00	0.00	0.02	0.00	57.92	2.00	0.00	0.00	0.01	0.00
57.95	2.00	0.00	0.00	0.03	0.00	57.99	2.00	0.00	0.00	0.04	0.00
58.01	2.00	0.00	0.00	0.02	0.00	58.05	2.00	0.00	0.00	0.04	0.00
58.05	2.00	0.00	0.00	0.01	0.00	58.10	2.00	0.00	0.00	0.05	0.00
58.13	2.00	0.00	0.00	0.03	0.00	58.15	2.00	0.00	0.00	0.01	0.00
58.17	2.00	0.00	0.00	0.03	0.00	58.20	2.00	0.00	0.00	0.02	0.00
58.21	2.00	0.00	0.00	0.01	0.00	58.21	2.00	0.00	0.00	0.00	0.00
58.23	2.00	0.00	0.00	0.02	0.00	58.24	2.00	0.00	0.00	0.01	0.00
58.25	2.00	0.00	0.00	0.01	0.00	58.29	2.00	0.00	0.00	0.04	0.00
58.31	2.00	0.00	0.00	0.02	0.00	58.33	2.00	0.00	0.00	0.02	0.00
58.38	2.00	0.00	0.00	0.05	0.00	58.39	2.00	0.00	0.00	0.01	0.00
58.43	2.00	0.00	0.00	0.04	0.00	58.43	2.00	0.00	0.00	0.01	0.00
58.48	2.00	0.00	0.00	0.05	0.00	58.53	2.00	0.00	0.00	0.05	0.00
58.56	2.00	0.00	0.00	0.02	0.00	58.58	2.00	0.00	0.00	0.03	0.00
58.59	2.00	0.00	0.00	0.01	0.00	58.63	2.00	0.00	0.00	0.03	0.00
58.63	2.00	0.00	0.00	0.00	0.00	58.63	2.00	0.00	0.00	0.01	0.00
58.68	2.00	0.00	0.00	0.04	0.00	58.69	2.00	0.00	0.00	0.01	0.00
58.72	2.00	0.00	0.00	0.03	0.00	58.73	2.00	0.00	0.00	0.01	0.00
58.74	2.00	0.00	0.00	0.01	0.00	58.77	2.00	0.00	0.00	0.03	0.00
58.81	2.00	0.00	0.00	0.04	0.00	58.82	2.00	0.00	0.00	0.01	0.00
58.83	2.00	0.00	0.00	0.01	0.00	58.87	2.00	0.00	0.00	0.04	0.00
58.91	2.00	0.00	0.00	0.04	0.00	58.92	2.00	0.00	0.00	0.01	0.00
58.93	2.00	0.00	0.00	0.01	0.00	58.96	2.00	0.00	0.00	0.03	0.00
59.01	2.00	0.00	0.00	0.05	0.00	59.06	2.00	0.00	0.00	0.05	0.00
59.08	2.00	0.00	0.00	0.02	0.00	59.11	2.00	0.00	0.00	0.03	0.00
59.15	2.00	0.00	0.00	0.04	0.00	59.21	2.00	0.00	0.00	0.05	0.00
59.26	2.00	0.00	0.00	0.05	0.00	59.30	2.00	0.00	0.00	0.04	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
59.35	2.00	0.00	0.00	0.05	0.00	59.40	2.00	0.00	0.00	0.05	0.00
59.42	2.00	0.00	0.00	0.02	0.00	59.47	2.00	0.00	0.00	0.05	0.00
59.51	2.00	0.00	0.00	0.05	0.00	59.56	2.00	0.00	0.00	0.05	0.00
59.61	2.00	0.00	0.00	0.05	0.00	59.67	2.00	0.00	0.00	0.05	0.00
59.71	2.00	0.00	0.00	0.04	0.00	59.80	2.00	0.00	0.00	0.09	0.00
59.85	2.00	0.00	0.00	0.05	0.00	59.90	2.00	0.00	0.00	0.05	0.00
60.00	2.00	0.00	0.00	0.10	0.00	60.04	2.00	0.00	0.00	0.05	0.00
60.10	2.00	0.00	0.00	0.06	0.00	60.15	1.91	0.00	0.00	0.05	0.00
60.19	1.73	0.00	0.00	0.03	0.00	60.23	1.70	0.00	0.00	0.05	0.00
60.28	1.69	0.00	0.00	0.05	0.00	60.33	1.74	0.00	0.00	0.05	0.00
60.38	1.77	0.00	0.00	0.04	0.00	60.42	1.78	0.00	0.00	0.04	0.00
60.44	1.76	0.00	0.00	0.02	0.00	60.47	1.93	0.00	0.00	0.02	0.00
60.52	2.00	0.00	0.00	0.05	0.00	60.56	2.00	0.00	0.00	0.04	0.00
60.57	2.00	0.00	0.00	0.01	0.00	60.61	2.00	0.00	0.00	0.04	0.00
60.66	2.00	0.00	0.00	0.05	0.00	60.71	2.00	0.00	0.00	0.05	0.00
60.76	2.00	0.00	0.00	0.05	0.00	60.81	2.00	0.00	0.00	0.05	0.00
60.86	2.00	0.00	0.00	0.05	0.00	60.91	2.00	0.00	0.00	0.05	0.00
60.95	2.00	0.00	0.00	0.04	0.00	61.00	2.00	0.00	0.00	0.05	0.00
61.02	2.00	0.00	0.00	0.02	0.00	61.05	2.00	0.00	0.00	0.03	0.00
61.08	2.00	0.00	0.00	0.03	0.00	61.09	2.00	0.00	0.00	0.02	0.00
61.13	2.00	0.00	0.00	0.03	0.00	61.14	2.00	0.00	0.00	0.02	0.00
61.16	2.00	0.00	0.00	0.02	0.00	61.20	2.00	0.00	0.00	0.03	0.00
61.23	2.00	0.00	0.00	0.04	0.00	61.24	2.00	0.00	0.00	0.01	0.00
61.29	2.00	0.00	0.00	0.05	0.00	61.30	2.00	0.00	0.00	0.01	0.00
61.33	2.00	0.00	0.00	0.04	0.00	61.38	2.00	0.00	0.00	0.05	0.00
61.43	2.00	0.00	0.00	0.05	0.00	61.48	2.00	0.00	0.00	0.04	0.00
61.53	2.00	0.00	0.00	0.05	0.00	61.56	2.00	0.00	0.00	0.03	0.00
61.58	2.00	0.00	0.00	0.02	0.00	61.59	2.00	0.00	0.00	0.01	0.00
61.62	2.00	0.00	0.00	0.03	0.00	61.63	2.00	0.00	0.00	0.02	0.00
61.67	2.00	0.00	0.00	0.03	0.00	61.71	2.00	0.00	0.00	0.05	0.00
61.76	2.00	0.00	0.00	0.05	0.00	61.81	2.00	0.00	0.00	0.05	0.00
61.86	2.00	0.00	0.00	0.05	0.00	61.87	2.00	0.00	0.00	0.01	0.00
61.91	2.00	0.00	0.00	0.04	0.00	61.95	2.00	0.00	0.00	0.04	0.00
61.96	2.00	0.00	0.00	0.01	0.00	62.00	2.00	0.00	0.00	0.04	0.00
62.04	2.00	0.00	0.00	0.04	0.00	62.06	1.86	0.00	0.00	0.02	0.00
62.10	1.70	0.00	0.00	0.04	0.00	62.14	1.58	0.00	0.00	0.04	0.00
62.20	1.49	0.00	0.00	0.05	0.00	62.22	1.33	0.00	0.00	0.02	0.00
62.27	1.39	0.00	0.00	0.05	0.00	62.29	1.39	0.00	0.00	0.02	0.00
62.34	1.37	0.00	0.00	0.05	0.00	62.39	1.35	0.00	0.00	0.04	0.00
62.43	1.31	0.00	0.00	0.05	0.00	62.49	1.30	0.00	0.00	0.06	0.00
62.57	1.31	0.00	0.00	0.08	0.00	62.68	1.45	0.00	0.00	0.10	0.00
62.75	1.75	0.00	0.00	0.08	0.00	62.87	1.99	0.00	0.00	0.12	0.00
62.88	1.84	0.00	0.00	0.01	0.00	62.89	1.84	0.00	0.00	0.01	0.00
62.93	1.86	0.00	0.00	0.04	0.00	62.98	2.00	0.00	0.00	0.05	0.00
63.02	2.00	0.00	0.00	0.05	0.00	63.07	2.00	0.00	0.00	0.05	0.00
63.12	2.00	0.00	0.00	0.05	0.00	63.14	2.00	0.00	0.00	0.02	0.00
63.17	2.00	0.00	0.00	0.03	0.00	63.17	2.00	0.00	0.00	0.01	0.00
63.20	2.00	0.00	0.00	0.02	0.00	63.21	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
63.23	2.00	0.00	0.00	0.02	0.00	63.26	2.00	0.00	0.00	0.03	0.00
63.28	2.00	0.00	0.00	0.02	0.00	63.31	2.00	0.00	0.00	0.03	0.00
63.32	2.00	0.00	0.00	0.01	0.00	63.36	2.00	0.00	0.00	0.04	0.00
63.40	2.00	0.00	0.00	0.04	0.00						

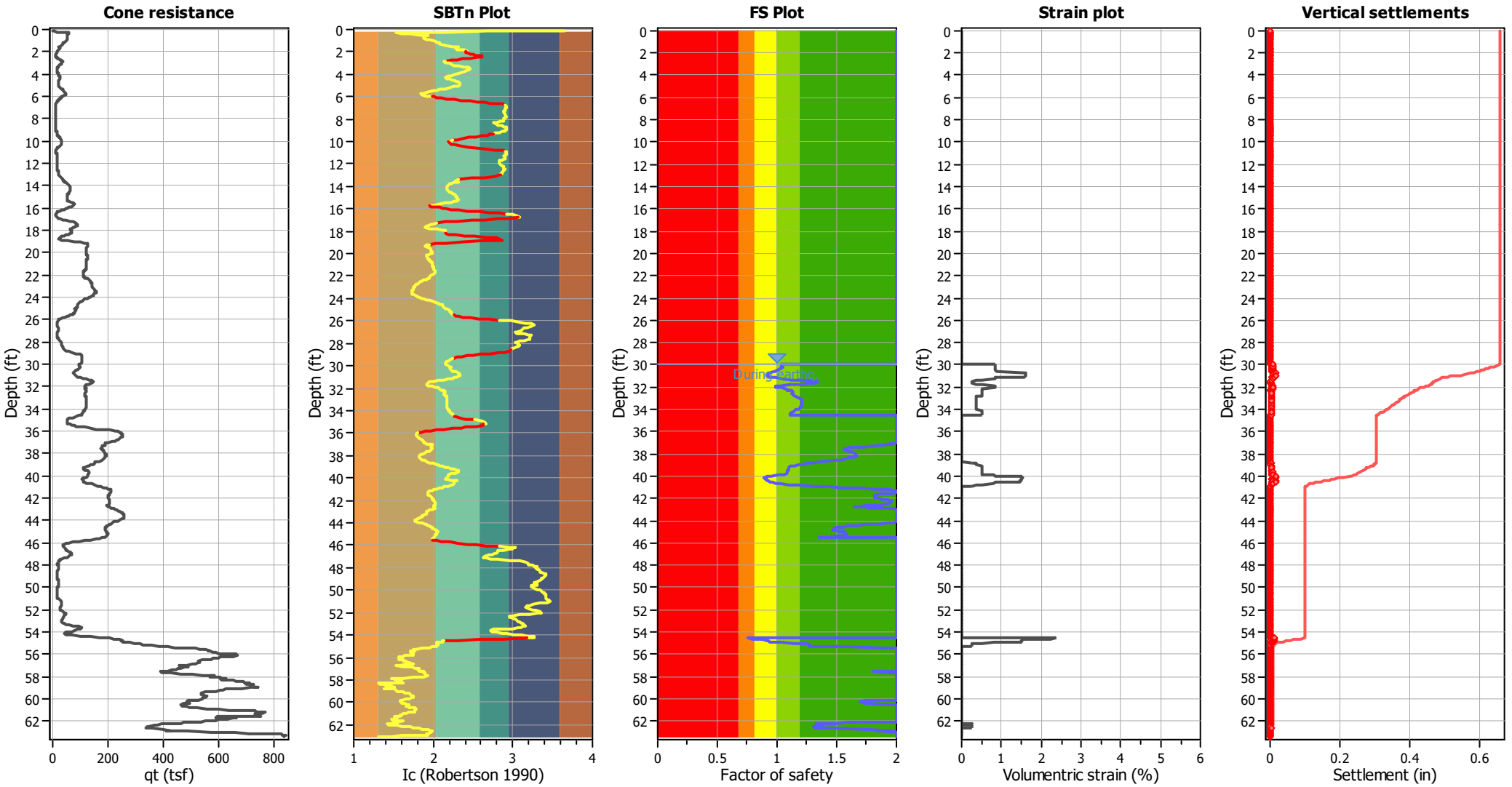
Overall liquefaction potential: 0.15

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
30.00	104.86	1.03	0.85	1.00	0.01	30.07	105.36	1.04	0.84	1.00	0.01
30.15	105.54	1.04	0.84	1.00	0.01	30.21	105.77	1.04	0.84	1.00	0.01
30.26	105.66	1.04	0.84	1.00	0.00	30.31	105.39	1.03	0.84	1.00	0.00
30.38	104.86	1.02	0.85	1.00	0.01	30.45	104.23	1.01	0.85	1.00	0.01
30.50	103.72	1.00	0.85	1.00	0.00	30.55	102.88	0.99	0.86	1.00	0.01
30.64	101.83	0.97	0.87	1.00	0.01	30.70	100.16	0.94	1.56	1.00	0.01
30.79	98.96	0.93	1.59	1.00	0.02	30.84	98.19	0.91	1.61	1.00	0.01
30.93	98.05	0.91	1.61	1.00	0.02	30.98	98.14	0.91	1.61	1.00	0.01
31.05	98.98	0.92	1.59	1.00	0.01	31.13	100.51	0.94	1.56	1.00	0.01
31.17	102.97	0.98	0.86	1.00	0.00	31.27	106.25	1.03	0.84	1.00	0.01
31.32	111.37	1.13	0.51	1.00	0.00	31.41	116.56	1.23	0.36	1.00	0.00
31.46	120.72	1.31	0.25	1.00	0.00	31.52	122.24	1.35	0.25	1.00	0.00
31.61	121.83	1.33	0.25	1.00	0.00	31.66	119.20	1.28	0.26	1.00	0.00
31.75	115.29	1.19	0.37	1.00	0.00	31.80	110.68	1.11	0.52	1.00	0.00
31.90	106.52	1.03	0.83	1.00	0.01	31.94	104.07	0.99	0.85	1.00	0.00
32.04	104.00	0.99	0.85	1.00	0.01	32.09	107.23	1.04	0.83	1.00	0.00
32.20	109.06	1.07	0.52	1.00	0.01	32.24	110.44	1.09	0.52	1.00	0.00
32.28	110.26	1.09	0.52	1.00	0.00	32.29	111.09	1.11	0.51	1.00	0.00
32.30	112.06	1.12	0.51	1.00	0.00	32.40	112.71	1.13	0.51	1.00	0.01
32.45	112.95	1.14	0.51	1.00	0.00	32.55	112.51	1.13	0.51	1.00	0.01
32.59	112.50	1.13	0.51	1.00	0.00	32.69	112.79	1.13	0.51	1.00	0.01
32.76	113.51	1.14	0.51	1.00	0.00	32.84	114.35	1.16	0.37	1.00	0.00
32.90	115.19	1.17	0.37	1.00	0.00	32.98	115.83	1.19	0.37	1.00	0.00
33.06	116.33	1.19	0.36	1.00	0.00	33.12	116.77	1.20	0.36	1.00	0.00
33.22	117.03	1.21	0.36	1.00	0.00	33.31	117.14	1.21	0.36	1.00	0.00
33.37	117.11	1.21	0.36	1.00	0.00	33.46	117.00	1.20	0.36	1.00	0.00
33.55	117.00	1.20	0.36	1.00	0.00	33.65	117.07	1.20	0.36	1.00	0.00
33.70	117.18	1.20	0.36	1.00	0.00	33.79	117.10	1.20	0.36	1.00	0.00
33.89	116.76	1.19	0.36	1.00	0.00	33.99	116.20	1.18	0.36	1.00	0.00
34.04	115.43	1.16	0.37	1.00	0.00	34.13	114.59	1.15	0.50	1.00	0.01
34.23	113.76	1.13	0.51	1.00	0.01	34.32	113.20	1.12	0.51	1.00	0.01
34.37	112.84	1.11	0.51	1.00	0.00	34.47	112.69	1.11	0.51	1.00	0.01
34.55	112.96	2.00	0.00	1.00	0.00	34.63	114.64	2.00	0.00	1.00	0.00
34.73	118.21	2.00	0.00	1.00	0.00	34.80	123.59	2.00	0.00	1.00	0.00
34.90	127.28	2.00	0.00	1.00	0.00	35.00	121.79	2.00	0.00	1.00	0.00
35.12	117.31	2.00	0.00	1.00	0.00	35.20	112.19	2.00	0.00	1.00	0.00
35.33	114.42	2.00	0.00	1.00	0.00	35.41	110.34	2.00	0.00	1.00	0.00
35.44	108.02	2.00	0.00	1.00	0.00	35.48	103.82	2.00	0.00	1.00	0.00
35.57	101.05	2.00	0.00	1.00	0.00	35.62	98.99	2.00	0.00	1.00	0.00
35.67	102.07	2.00	0.00	1.00	0.00	35.71	112.52	2.00	0.00	1.00	0.00
35.82	126.36	2.00	0.00	1.00	0.00	35.86	143.07	2.00	0.00	1.00	0.00
35.93	156.85	2.00	0.00	1.00	0.00	36.01	166.33	2.00	0.00	1.00	0.00
36.06	171.69	2.00	0.00	1.00	0.00	36.12	174.89	2.00	0.00	1.00	0.00
36.18	178.20	2.00	0.00	1.00	0.00	36.25	180.98	2.00	0.00	1.00	0.00
36.30	184.12	2.00	0.00	1.00	0.00	36.39	185.99	2.00	0.00	1.00	0.00
36.44	187.57	2.00	0.00	1.00	0.00	36.53	187.51	2.00	0.00	1.00	0.00
36.59	187.43	2.00	0.00	1.00	0.00	36.68	184.49	2.00	0.00	1.00	0.00
36.75	180.99	2.00	0.00	1.00	0.00	36.83	175.91	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
36.90	171.34	2.00	0.00	1.00	0.00	36.97	166.05	2.00	0.00	1.00	0.00
37.02	156.23	2.00	0.00	1.00	0.00	37.04	151.13	2.00	0.00	1.00	0.00
37.08	147.61	1.93	0.00	1.00	0.00	37.17	148.65	1.96	0.00	1.00	0.00
37.27	145.04	1.85	0.00	1.00	0.00	37.37	140.68	1.72	0.00	1.00	0.00
37.42	137.22	1.62	0.00	1.00	0.00	37.51	135.25	1.57	0.00	1.00	0.00
37.58	134.76	1.56	0.00	1.00	0.00	37.66	135.08	1.57	0.00	1.00	0.00
37.76	136.26	1.59	0.00	1.00	0.00	37.85	137.18	1.62	0.00	1.00	0.00
37.93	138.14	1.64	0.00	1.00	0.00	38.04	138.80	1.66	0.00	1.00	0.00
38.13	139.30	1.67	0.00	1.00	0.00	38.18	139.16	1.67	0.00	1.00	0.00
38.28	138.51	1.65	0.00	1.00	0.00	38.37	137.08	1.61	0.00	1.00	0.00
38.47	135.63	1.57	0.00	1.00	0.00	38.57	134.14	1.53	0.00	1.00	0.00
38.62	132.48	1.49	0.00	1.00	0.00	38.72	127.27	1.37	0.00	1.00	0.00
38.78	123.72	1.29	0.25	1.00	0.00	38.81	121.63	1.24	0.35	1.00	0.00
38.86	121.68	1.24	0.35	1.00	0.00	38.91	120.51	1.22	0.36	1.00	0.00
38.95	118.55	1.18	0.36	1.00	0.00	39.05	116.91	1.15	0.50	1.00	0.01
39.09	115.64	1.12	0.50	1.00	0.00	39.14	114.83	1.11	0.50	1.00	0.00
39.24	114.32	1.10	0.51	1.00	0.01	39.29	114.03	1.09	0.51	1.00	0.00
39.39	114.16	1.10	0.51	1.00	0.01	39.43	114.28	1.10	0.51	1.00	0.00
39.53	113.89	1.09	0.51	1.00	0.01	39.57	113.55	1.08	0.51	1.00	0.00
39.68	113.69	1.09	0.51	1.00	0.01	39.73	113.53	1.08	0.51	1.00	0.00
39.81	112.48	1.06	0.51	1.00	0.01	39.89	109.51	1.01	0.81	1.00	0.01
39.96	105.89	0.95	0.84	1.00	0.01	40.06	103.14	0.91	1.50	1.00	0.02
40.15	102.38	0.90	1.51	1.00	0.02	40.20	102.07	0.89	1.52	1.00	0.01
40.24	102.62	0.90	1.51	1.00	0.01	40.26	103.22	0.91	1.50	1.00	0.00
40.27	103.36	0.91	1.49	1.00	0.00	40.37	103.81	0.92	1.48	1.00	0.02
40.42	104.71	0.93	1.46	1.00	0.01	40.52	105.44	0.94	1.45	1.00	0.02
40.56	106.63	0.96	0.83	1.00	0.00	40.66	108.06	0.99	0.82	1.00	0.01
40.70	110.67	1.03	0.80	1.00	0.00	40.75	114.79	1.10	0.50	1.00	0.00
40.85	119.75	1.20	0.36	1.00	0.00	40.91	125.10	1.31	0.25	1.00	0.00
40.96	130.56	1.43	0.00	1.00	0.00	41.04	135.59	1.55	0.00	1.00	0.00
41.09	141.03	1.70	0.00	1.00	0.00	41.18	145.57	1.83	0.00	1.00	0.00
41.23	149.12	1.94	0.00	1.00	0.00	41.29	151.17	2.00	0.00	1.00	0.00
41.38	151.67	2.00	0.00	1.00	0.00	41.42	151.21	2.00	0.00	1.00	0.00
41.52	149.86	1.96	0.00	1.00	0.00	41.57	148.26	1.91	0.00	1.00	0.00
41.62	146.93	1.87	0.00	1.00	0.00	41.71	145.89	1.84	0.00	1.00	0.00
41.76	145.43	1.82	0.00	1.00	0.00	41.84	145.17	1.81	0.00	1.00	0.00
41.91	145.22	1.81	0.00	1.00	0.00	41.95	145.53	1.82	0.00	1.00	0.00
42.01	146.36	1.85	0.00	1.00	0.00	42.10	147.40	1.88	0.00	1.00	0.00
42.15	148.90	1.92	0.00	1.00	0.00	42.24	149.94	1.96	0.00	1.00	0.00
42.28	150.31	1.97	0.00	1.00	0.00	42.39	149.81	1.95	0.00	1.00	0.00
42.43	149.14	1.93	0.00	1.00	0.00	42.50	148.36	1.91	0.00	1.00	0.00
42.58	147.54	1.88	0.00	1.00	0.00	42.65	142.73	1.74	0.00	1.00	0.00
42.70	140.58	1.68	0.00	1.00	0.00	42.73	139.14	1.64	0.00	1.00	0.00
42.77	142.31	1.73	0.00	1.00	0.00	42.82	144.06	1.78	0.00	1.00	0.00
42.87	146.92	1.86	0.00	1.00	0.00	42.91	150.57	1.97	0.00	1.00	0.00
42.97	154.27	2.00	0.00	1.00	0.00	43.02	157.35	2.00	0.00	1.00	0.00
43.06	159.72	2.00	0.00	1.00	0.00	43.11	162.21	2.00	0.00	1.00	0.00
43.17	164.40	2.00	0.00	1.00	0.00	43.21	166.83	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
43.29	168.85	2.00	0.00	1.00	0.00	43.34	171.05	2.00	0.00	1.00	0.00
43.39	172.71	2.00	0.00	1.00	0.00	43.45	173.74	2.00	0.00	1.00	0.00
43.51	173.50	2.00	0.00	1.00	0.00	43.59	172.47	2.00	0.00	1.00	0.00
43.64	170.73	2.00	0.00	1.00	0.00	43.70	168.10	2.00	0.00	1.00	0.00
43.78	165.08	2.00	0.00	1.00	0.00	43.88	163.55	2.00	0.00	1.00	0.00
43.94	161.52	2.00	0.00	1.00	0.00	44.04	157.74	2.00	0.00	1.00	0.00
44.07	153.31	2.00	0.00	1.00	0.00	44.12	152.08	2.00	0.00	1.00	0.00
44.16	150.70	1.98	0.00	1.00	0.00	44.21	148.86	1.92	0.00	1.00	0.00
44.26	146.86	1.86	0.00	1.00	0.00	44.31	144.63	1.79	0.00	1.00	0.00
44.35	142.44	1.73	0.00	1.00	0.00	44.40	140.32	1.67	0.00	1.00	0.00
44.45	138.56	1.62	0.00	1.00	0.00	44.50	137.24	1.59	0.00	1.00	0.00
44.54	136.15	1.56	0.00	1.00	0.00	44.60	134.97	1.53	0.00	1.00	0.00
44.64	133.85	1.50	0.00	1.00	0.00	44.69	132.85	1.48	0.00	1.00	0.00
44.74	132.59	1.47	0.00	1.00	0.00	44.79	132.34	1.47	0.00	1.00	0.00
44.83	132.53	1.47	0.00	1.00	0.00	44.88	132.96	1.48	0.00	1.00	0.00
44.93	134.02	1.51	0.00	1.00	0.00	44.98	135.20	1.54	0.00	1.00	0.00
45.03	135.95	1.56	0.00	1.00	0.00	45.08	136.45	1.57	0.00	1.00	0.00
45.16	136.81	1.58	0.00	1.00	0.00	45.19	136.91	1.58	0.00	1.00	0.00
45.27	136.53	1.57	0.00	1.00	0.00	45.32	135.53	1.55	0.00	1.00	0.00
45.37	133.73	1.50	0.00	1.00	0.00	45.45	131.17	1.44	0.00	1.00	0.00
45.51	127.52	1.35	0.00	1.00	0.00	45.56	123.37	2.00	0.00	1.00	0.00
45.61	117.60	2.00	0.00	1.00	0.00	45.69	111.79	2.00	0.00	1.00	0.00
45.75	108.19	2.00	0.00	1.00	0.00	45.81	105.04	2.00	0.00	1.00	0.00
45.89	105.10	2.00	0.00	1.00	0.00	45.94	103.73	2.00	0.00	1.00	0.00
46.04	108.05	2.00	0.00	1.00	0.00	46.08	112.07	2.00	0.00	1.00	0.00
46.15	109.85	2.00	0.00	1.00	0.00	46.17	110.89	2.00	0.00	1.00	0.00
46.18	110.17	2.00	0.00	1.00	0.00	46.23	109.18	2.00	0.00	1.00	0.00
46.27	107.58	2.00	0.00	1.00	0.00	46.32	105.33	2.00	0.00	1.00	0.00
46.41	107.19	2.00	0.00	1.00	0.00	46.47	106.19	2.00	0.00	1.00	0.00
46.52	106.89	2.00	0.00	1.00	0.00	46.56	109.81	2.00	0.00	1.00	0.00
46.65	113.60	2.00	0.00	1.00	0.00	46.71	117.68	2.00	0.00	1.00	0.00
46.76	120.04	2.00	0.00	1.00	0.00	46.85	120.43	2.00	0.00	1.00	0.00
46.90	118.71	2.00	0.00	1.00	0.00	46.99	116.19	2.00	0.00	1.00	0.00
47.04	114.63	2.00	0.00	1.00	0.00	47.10	114.71	2.00	0.00	1.00	0.00
47.16	116.10	2.00	0.00	1.00	0.00	47.23	117.23	2.00	0.00	1.00	0.00
47.30	117.96	2.00	0.00	1.00	0.00	47.38	113.48	2.00	0.00	1.00	0.00
47.43	111.84	2.00	0.00	1.00	0.00	47.52	105.92	2.00	0.00	1.00	0.00
47.59	93.23	2.00	0.00	1.00	0.00	47.66	81.89	2.00	0.00	1.00	0.00
47.77	74.67	2.00	0.00	1.00	0.00	47.82	75.76	2.00	0.00	1.00	0.00
47.91	76.63	2.00	0.00	1.00	0.00	47.93	77.65	2.00	0.00	1.00	0.00
47.97	78.37	2.00	0.00	1.00	0.00	48.02	79.56	2.00	0.00	1.00	0.00
48.07	81.21	2.00	0.00	1.00	0.00	48.12	84.04	2.00	0.00	1.00	0.00
48.19	86.54	2.00	0.00	1.00	0.00	48.23	88.74	2.00	0.00	1.00	0.00
48.31	89.88	2.00	0.00	1.00	0.00	48.35	90.92	2.00	0.00	1.00	0.00
48.40	91.72	2.00	0.00	1.00	0.00	48.45	92.39	2.00	0.00	1.00	0.00
48.50	92.93	2.00	0.00	1.00	0.00	48.55	93.37	2.00	0.00	1.00	0.00
48.59	94.24	2.00	0.00	1.00	0.00	48.67	94.62	2.00	0.00	1.00	0.00
48.73	94.36	2.00	0.00	1.00	0.00	48.78	92.80	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
48.83	90.68	2.00	0.00	1.00	0.00	48.91	88.35	2.00	0.00	1.00	0.00
48.98	86.35	2.00	0.00	1.00	0.00	49.03	85.19	2.00	0.00	1.00	0.00
49.12	82.90	2.00	0.00	1.00	0.00	49.17	79.48	2.00	0.00	1.00	0.00
49.27	76.51	2.00	0.00	1.00	0.00	49.31	76.55	2.00	0.00	1.00	0.00
49.38	78.88	2.00	0.00	1.00	0.00	49.45	81.15	2.00	0.00	1.00	0.00
49.51	83.00	2.00	0.00	1.00	0.00	49.54	84.13	2.00	0.00	1.00	0.00
49.59	84.45	2.00	0.00	1.00	0.00	49.64	83.63	2.00	0.00	1.00	0.00
49.73	83.01	2.00	0.00	1.00	0.00	49.83	82.47	2.00	0.00	1.00	0.00
49.92	82.19	2.00	0.00	1.00	0.00	49.98	81.62	2.00	0.00	1.00	0.00
50.07	81.01	2.00	0.00	1.00	0.00	50.16	80.51	2.00	0.00	1.00	0.00
50.24	80.06	2.00	0.00	1.00	0.00	50.32	79.87	2.00	0.00	1.00	0.00
50.41	80.02	2.00	0.00	1.00	0.00	50.50	80.09	2.00	0.00	1.00	0.00
50.56	79.36	2.00	0.00	1.00	0.00	50.66	78.27	2.00	0.00	1.00	0.00
50.74	77.53	2.00	0.00	1.00	0.00	50.84	79.62	2.00	0.00	1.00	0.00
50.93	83.88	2.00	0.00	1.00	0.00	50.98	92.08	2.00	0.00	1.00	0.00
51.08	102.75	2.00	0.00	1.00	0.00	51.17	113.31	2.00	0.00	1.00	0.00
51.24	122.80	2.00	0.00	1.00	0.00	51.34	129.12	2.00	0.00	1.00	0.00
51.41	122.59	2.00	0.00	1.00	0.00	51.51	115.66	2.00	0.00	1.00	0.00
51.58	106.93	2.00	0.00	1.00	0.00	51.68	109.98	2.00	0.00	1.00	0.00
51.79	110.16	2.00	0.00	1.00	0.00	51.82	110.15	2.00	0.00	1.00	0.00
51.85	111.07	2.00	0.00	1.00	0.00	51.91	113.23	2.00	0.00	1.00	0.00
52.00	116.25	2.00	0.00	1.00	0.00	52.05	118.92	2.00	0.00	1.00	0.00
52.10	118.95	2.00	0.00	1.00	0.00	52.19	115.81	2.00	0.00	1.00	0.00
52.28	111.69	2.00	0.00	1.00	0.00	52.34	109.32	2.00	0.00	1.00	0.00
52.42	109.66	2.00	0.00	1.00	0.00	52.48	111.03	2.00	0.00	1.00	0.00
52.57	111.27	2.00	0.00	1.00	0.00	52.62	109.88	2.00	0.00	1.00	0.00
52.69	106.89	2.00	0.00	1.00	0.00	52.77	104.50	2.00	0.00	1.00	0.00
52.87	103.83	2.00	0.00	1.00	0.00	52.91	102.56	2.00	0.00	1.00	0.00
53.01	102.13	2.00	0.00	1.00	0.00	53.10	103.11	2.00	0.00	1.00	0.00
53.16	113.26	2.00	0.00	1.00	0.00	53.25	123.32	2.00	0.00	1.00	0.00
53.29	136.25	2.00	0.00	1.00	0.00	53.38	144.18	2.00	0.00	1.00	0.00
53.42	149.47	2.00	0.00	1.00	0.00	53.47	150.02	2.00	0.00	1.00	0.00
53.52	148.22	2.00	0.00	1.00	0.00	53.58	152.55	2.00	0.00	1.00	0.00
53.66	160.18	2.00	0.00	1.00	0.00	53.75	169.41	2.00	0.00	1.00	0.00
53.81	175.67	2.00	0.00	1.00	0.00	53.87	177.89	2.00	0.00	1.00	0.00
53.95	178.71	2.00	0.00	1.00	0.00	54.01	177.57	2.00	0.00	1.00	0.00
54.06	172.90	2.00	0.00	1.00	0.00	54.15	167.57	2.00	0.00	1.00	0.00
54.20	165.24	2.00	0.00	1.00	0.00	54.29	164.23	2.00	0.00	1.00	0.00
54.34	141.87	2.00	0.00	1.00	0.00	54.43	108.63	2.00	0.00	1.00	0.00
54.45	82.07	2.00	0.00	1.00	0.00	54.48	80.59	2.00	0.00	1.00	0.00
54.52	82.69	2.00	0.00	1.00	0.00	54.53	86.57	2.00	0.00	1.00	0.00
54.58	89.91	0.75	2.37	1.00	0.01	54.62	93.59	0.80	2.24	1.00	0.01
54.65	96.81	0.84	2.13	1.00	0.01	54.70	99.98	0.88	1.57	1.00	0.01
54.76	102.23	0.92	1.52	1.00	0.01	54.77	102.77	0.92	1.51	1.00	0.00
54.82	103.16	0.93	1.50	1.00	0.01	54.87	103.55	0.94	1.49	1.00	0.01
54.88	104.08	0.94	1.48	1.00	0.00	54.91	104.56	0.95	0.85	1.00	0.00
54.96	106.09	0.98	0.84	1.00	0.00	54.97	109.90	1.04	0.81	1.00	0.00
55.03	115.47	1.14	0.50	1.00	0.00	55.09	120.89	1.25	0.25	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
55.15	121.55	1.26	0.25	1.00	0.00	55.20	122.41	1.28	0.25	1.00	0.00
55.25	121.49	1.26	0.25	1.00	0.00	55.30	129.28	1.44	0.00	1.00	0.00
55.34	134.62	1.57	0.00	1.00	0.00	55.39	146.03	1.89	0.00	1.00	0.00
55.40	153.71	2.00	0.00	1.00	0.00	55.44	157.35	2.00	0.00	1.00	0.00
55.44	157.04	2.00	0.00	1.00	0.00	55.49	160.78	2.00	0.00	1.00	0.00
55.54	167.71	2.00	0.00	1.00	0.00	55.59	176.17	2.00	0.00	1.00	0.00
55.63	180.34	2.00	0.00	1.00	0.00	55.64	180.79	2.00	0.00	1.00	0.00
55.68	179.92	2.00	0.00	1.00	0.00	55.69	178.50	2.00	0.00	1.00	0.00
55.69	179.38	2.00	0.00	1.00	0.00	55.71	183.08	2.00	0.00	1.00	0.00
55.76	186.45	2.00	0.00	1.00	0.00	55.78	187.85	2.00	0.00	1.00	0.00
55.81	180.96	2.00	0.00	1.00	0.00	55.85	175.16	2.00	0.00	1.00	0.00
55.86	176.41	2.00	0.00	1.00	0.00	55.91	179.42	2.00	0.00	1.00	0.00
55.92	180.48	2.00	0.00	1.00	0.00	55.96	185.46	2.00	0.00	1.00	0.00
55.97	189.98	2.00	0.00	1.00	0.00	56.00	196.01	2.00	0.00	1.00	0.00
56.01	197.72	2.00	0.00	1.00	0.00	56.03	198.18	2.00	0.00	1.00	0.00
56.05	198.14	2.00	0.00	1.00	0.00	56.10	198.99	2.00	0.00	1.00	0.00
56.12	199.86	2.00	0.00	1.00	0.00	56.16	199.67	2.00	0.00	1.00	0.00
56.17	195.76	2.00	0.00	1.00	0.00	56.20	189.78	2.00	0.00	1.00	0.00
56.22	184.46	2.00	0.00	1.00	0.00	56.24	181.69	2.00	0.00	1.00	0.00
56.30	179.84	2.00	0.00	1.00	0.00	56.31	177.72	2.00	0.00	1.00	0.00
56.34	174.82	2.00	0.00	1.00	0.00	56.39	172.57	2.00	0.00	1.00	0.00
56.45	170.44	2.00	0.00	1.00	0.00	56.48	168.31	2.00	0.00	1.00	0.00
56.49	165.32	2.00	0.00	1.00	0.00	56.53	168.57	2.00	0.00	1.00	0.00
56.58	169.38	2.00	0.00	1.00	0.00	56.63	155.86	2.00	0.00	1.00	0.00
56.68	156.17	2.00	0.00	1.00	0.00	56.73	157.68	2.00	0.00	1.00	0.00
56.78	156.09	2.00	0.00	1.00	0.00	56.83	153.53	2.00	0.00	1.00	0.00
56.89	157.35	2.00	0.00	1.00	0.00	56.95	160.76	2.00	0.00	1.00	0.00
56.99	161.37	2.00	0.00	1.00	0.00	57.01	160.98	2.00	0.00	1.00	0.00
57.04	160.65	2.00	0.00	1.00	0.00	57.09	161.13	2.00	0.00	1.00	0.00
57.11	163.57	2.00	0.00	1.00	0.00	57.13	167.47	2.00	0.00	1.00	0.00
57.18	169.44	2.00	0.00	1.00	0.00	57.19	168.95	2.00	0.00	1.00	0.00
57.21	166.30	2.00	0.00	1.00	0.00	57.24	164.00	2.00	0.00	1.00	0.00
57.28	163.35	2.00	0.00	1.00	0.00	57.32	161.45	2.00	0.00	1.00	0.00
57.35	160.03	2.00	0.00	1.00	0.00	57.38	157.50	2.00	0.00	1.00	0.00
57.43	155.53	2.00	0.00	1.00	0.00	57.48	150.26	2.00	0.00	1.00	0.00
57.52	143.92	1.85	0.00	1.00	0.00	57.57	142.28	1.80	0.00	1.00	0.00
57.62	146.53	1.93	0.00	1.00	0.00	57.68	157.03	2.00	0.00	1.00	0.00
57.76	166.00	2.00	0.00	1.00	0.00	57.81	161.17	2.00	0.00	1.00	0.00
57.86	159.31	2.00	0.00	1.00	0.00	57.89	167.80	2.00	0.00	1.00	0.00
57.91	171.02	2.00	0.00	1.00	0.00	57.92	169.11	2.00	0.00	1.00	0.00
57.95	166.67	2.00	0.00	1.00	0.00	57.99	167.08	2.00	0.00	1.00	0.00
58.01	169.42	2.00	0.00	1.00	0.00	58.05	173.02	2.00	0.00	1.00	0.00
58.05	175.27	2.00	0.00	1.00	0.00	58.10	176.91	2.00	0.00	1.00	0.00
58.13	178.73	2.00	0.00	1.00	0.00	58.15	180.87	2.00	0.00	1.00	0.00
58.17	182.75	2.00	0.00	1.00	0.00	58.20	182.21	2.00	0.00	1.00	0.00
58.21	181.00	2.00	0.00	1.00	0.00	58.21	179.50	2.00	0.00	1.00	0.00
58.23	179.34	2.00	0.00	1.00	0.00	58.24	177.62	2.00	0.00	1.00	0.00
58.25	177.92	2.00	0.00	1.00	0.00	58.29	179.26	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
58.31	183.11	2.00	0.00	1.00	0.00	58.33	186.52	2.00	0.00	1.00	0.00
58.38	190.06	2.00	0.00	1.00	0.00	58.39	193.13	2.00	0.00	1.00	0.00
58.43	195.59	2.00	0.00	1.00	0.00	58.43	199.15	2.00	0.00	1.00	0.00
58.48	200.60	2.00	0.00	1.00	0.00	58.53	202.36	2.00	0.00	1.00	0.00
58.56	202.90	2.00	0.00	1.00	0.00	58.58	205.20	2.00	0.00	1.00	0.00
58.59	207.06	2.00	0.00	1.00	0.00	58.63	205.90	2.00	0.00	1.00	0.00
58.63	206.49	2.00	0.00	1.00	0.00	58.63	202.42	2.00	0.00	1.00	0.00
58.68	203.74	2.00	0.00	1.00	0.00	58.69	204.22	2.00	0.00	1.00	0.00
58.72	208.81	2.00	0.00	1.00	0.00	58.73	210.28	2.00	0.00	1.00	0.00
58.74	211.92	2.00	0.00	1.00	0.00	58.77	211.36	2.00	0.00	1.00	0.00
58.81	210.02	2.00	0.00	1.00	0.00	58.82	207.44	2.00	0.00	1.00	0.00
58.83	207.97	2.00	0.00	1.00	0.00	58.87	209.78	2.00	0.00	1.00	0.00
58.91	212.41	2.00	0.00	1.00	0.00	58.92	214.21	2.00	0.00	1.00	0.00
58.93	214.95	2.00	0.00	1.00	0.00	58.96	214.44	2.00	0.00	1.00	0.00
59.01	207.70	2.00	0.00	1.00	0.00	59.06	199.13	2.00	0.00	1.00	0.00
59.08	189.77	2.00	0.00	1.00	0.00	59.11	184.95	2.00	0.00	1.00	0.00
59.15	181.46	2.00	0.00	1.00	0.00	59.21	178.75	2.00	0.00	1.00	0.00
59.26	178.89	2.00	0.00	1.00	0.00	59.30	173.20	2.00	0.00	1.00	0.00
59.35	169.07	2.00	0.00	1.00	0.00	59.40	168.73	2.00	0.00	1.00	0.00
59.42	168.34	2.00	0.00	1.00	0.00	59.47	167.78	2.00	0.00	1.00	0.00
59.51	168.63	2.00	0.00	1.00	0.00	59.56	168.59	2.00	0.00	1.00	0.00
59.61	164.50	2.00	0.00	1.00	0.00	59.67	155.77	2.00	0.00	1.00	0.00
59.71	159.11	2.00	0.00	1.00	0.00	59.80	159.56	2.00	0.00	1.00	0.00
59.85	158.50	2.00	0.00	1.00	0.00	59.90	155.47	2.00	0.00	1.00	0.00
60.00	155.53	2.00	0.00	1.00	0.00	60.04	155.09	2.00	0.00	1.00	0.00
60.10	150.62	2.00	0.00	1.00	0.00	60.15	145.30	1.91	0.00	1.00	0.00
60.19	139.22	1.73	0.00	1.00	0.00	60.23	138.03	1.70	0.00	1.00	0.00
60.28	137.71	1.69	0.00	1.00	0.00	60.33	139.47	1.74	0.00	1.00	0.00
60.38	140.26	1.77	0.00	1.00	0.00	60.42	140.74	1.78	0.00	1.00	0.00
60.44	140.24	1.76	0.00	1.00	0.00	60.47	145.72	1.93	0.00	1.00	0.00
60.52	148.94	2.00	0.00	1.00	0.00	60.56	150.90	2.00	0.00	1.00	0.00
60.57	151.48	2.00	0.00	1.00	0.00	60.61	151.48	2.00	0.00	1.00	0.00
60.66	151.98	2.00	0.00	1.00	0.00	60.71	153.21	2.00	0.00	1.00	0.00
60.76	156.59	2.00	0.00	1.00	0.00	60.81	159.58	2.00	0.00	1.00	0.00
60.86	161.02	2.00	0.00	1.00	0.00	60.91	158.84	2.00	0.00	1.00	0.00
60.95	170.69	2.00	0.00	1.00	0.00	61.00	180.91	2.00	0.00	1.00	0.00
61.02	186.60	2.00	0.00	1.00	0.00	61.05	194.34	2.00	0.00	1.00	0.00
61.08	201.44	2.00	0.00	1.00	0.00	61.09	207.57	2.00	0.00	1.00	0.00
61.13	209.24	2.00	0.00	1.00	0.00	61.14	209.63	2.00	0.00	1.00	0.00
61.16	210.15	2.00	0.00	1.00	0.00	61.20	212.77	2.00	0.00	1.00	0.00
61.23	215.88	2.00	0.00	1.00	0.00	61.24	217.23	2.00	0.00	1.00	0.00
61.29	214.83	2.00	0.00	1.00	0.00	61.30	210.65	2.00	0.00	1.00	0.00
61.33	207.82	2.00	0.00	1.00	0.00	61.38	206.66	2.00	0.00	1.00	0.00
61.43	206.60	2.00	0.00	1.00	0.00	61.48	208.54	2.00	0.00	1.00	0.00
61.53	212.02	2.00	0.00	1.00	0.00	61.56	213.05	2.00	0.00	1.00	0.00
61.58	205.10	2.00	0.00	1.00	0.00	61.59	198.13	2.00	0.00	1.00	0.00
61.62	169.24	2.00	0.00	1.00	0.00	61.63	167.67	2.00	0.00	1.00	0.00
61.67	165.65	2.00	0.00	1.00	0.00	61.71	186.61	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
61.76	184.50	2.00	0.00	1.00	0.00	61.81	178.32	2.00	0.00	1.00	0.00
61.86	172.85	2.00	0.00	1.00	0.00	61.87	168.83	2.00	0.00	1.00	0.00
61.91	165.39	2.00	0.00	1.00	0.00	61.95	162.25	2.00	0.00	1.00	0.00
61.96	159.04	2.00	0.00	1.00	0.00	62.00	155.30	2.00	0.00	1.00	0.00
62.04	150.01	2.00	0.00	1.00	0.00	62.06	143.15	1.86	0.00	1.00	0.00
62.10	137.65	1.70	0.00	1.00	0.00	62.14	133.04	1.58	0.00	1.00	0.00
62.20	129.46	1.49	0.00	1.00	0.00	62.22	122.70	1.33	0.25	1.00	0.00
62.27	125.13	1.39	0.00	1.00	0.00	62.29	125.44	1.39	0.00	1.00	0.00
62.34	124.22	1.37	0.00	1.00	0.00	62.39	123.46	1.35	0.25	1.00	0.00
62.43	121.51	1.31	0.25	1.00	0.00	62.49	121.38	1.30	0.25	1.00	0.00
62.57	121.70	1.31	0.25	1.00	0.00	62.68	127.79	1.45	0.00	1.00	0.00
62.75	139.12	1.75	0.00	1.00	0.00	62.87	146.86	1.99	0.00	1.00	0.00
62.88	142.25	1.84	0.00	1.00	0.00	62.89	142.29	1.84	0.00	1.00	0.00
62.93	142.80	1.86	0.00	1.00	0.00	62.98	158.87	2.00	0.00	1.00	0.00
63.02	172.30	2.00	0.00	1.00	0.00	63.07	182.93	2.00	0.00	1.00	0.00
63.12	-1.00	2.00	0.00	1.00	0.00	63.14	-1.00	2.00	0.00	1.00	0.00
63.17	-1.00	2.00	0.00	1.00	0.00	63.17	-1.00	2.00	0.00	1.00	0.00
63.20	-1.00	2.00	0.00	1.00	0.00	63.21	-1.00	2.00	0.00	1.00	0.00
63.23	-1.00	2.00	0.00	1.00	0.00	63.26	-1.00	2.00	0.00	1.00	0.00
63.28	-1.00	2.00	0.00	1.00	0.00	63.31	-1.00	2.00	0.00	1.00	0.00
63.32	-1.00	2.00	0.00	1.00	0.00	63.36	-1.00	2.00	0.00	1.00	0.00
63.40	-1.00	2.00	0.00	1.00	0.00						

Total estimated settlement: 0.66

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation (Robertson (2009) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.01	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.04	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.09	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.11	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.14	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.14	1.35	2.15	27.82	59.81	3.66	7.03	11.25
0.18	6.97	11.19	4.58	51.24	2.69	0.06	0.63
0.23	18.19	29.21	1.00	29.21	2.14	0.02	0.62
0.24	36.79	59.09	1.00	59.09	1.76	0.11	0.65
0.28	53.07	85.23	1.00	85.23	1.58	0.72	0.72
0.33	59.27	95.19	1.00	95.19	1.53	0.74	0.74
0.38	56.61	90.91	1.00	90.91	1.60	0.73	0.73
0.42	52.11	83.69	1.00	83.69	1.72	0.72	0.72
0.47	51.84	83.25	1.19	98.77	1.83	0.75	0.75
0.51	51.94	83.40	1.24	103.16	1.90	0.75	0.75
0.52	52.09	83.64	1.26	104.99	1.93	0.76	0.76
0.57	52.66	84.56	1.24	105.20	1.91	0.76	0.76
0.61	53.24	85.48	1.23	105.23	1.89	0.76	0.76
0.67	53.47	85.85	1.22	105.00	1.88	0.76	0.76
0.73	53.84	86.44	1.22	105.23	1.87	0.76	0.76
0.81	53.62	86.08	1.22	104.72	1.87	0.76	0.76
0.86	53.52	85.91	1.25	107.16	1.92	0.76	0.76
0.98	52.14	83.69	1.28	106.78	1.96	0.76	0.76
1.05	48.22	77.37	1.32	102.42	2.02	0.75	0.75
1.15	43.67	70.05	1.34	94.07	2.04	0.74	0.74
1.24	37.87	60.73	1.38	83.84	2.07	0.72	0.72
1.34	34.47	55.26	1.40	77.37	2.09	0.47	0.70
1.43	30.63	49.08	1.51	74.33	2.16	0.36	0.69
1.53	26.86	43.01	1.75	75.37	2.25	0.40	0.70
1.58	24.56	39.32	1.98	77.68	2.31	0.48	0.70
1.62	23.48	37.59	2.00	75.15	2.32	0.39	0.70
1.67	24.36	38.99	1.85	72.19	2.28	0.31	0.69
1.75	23.89	38.23	1.86	70.99	2.28	0.28	0.69
1.77	23.08	36.93	1.92	70.79	2.30	0.27	0.69
1.81	21.50	34.38	2.08	71.55	2.34	0.29	0.69
1.86	19.71	31.51	2.30	72.37	2.39	0.31	0.69
1.91	17.96	28.69	2.52	72.24	2.43	0.31	0.69
1.95	16.98	27.11	2.53	68.54	2.43	0.23	0.68
2.00	16.21	25.86	2.43	62.85	2.41	0.14	0.66
2.05	14.89	23.75	2.42	57.52	2.41	0.09	0.65
2.11	13.51	21.52	2.55	54.95	2.43	0.08	0.64
2.20	12.33	19.62	2.79	54.76	2.47	0.08	0.64
2.24	11.73	18.64	3.01	56.15	2.50	0.08	0.65
2.29	11.26	17.88	3.29	58.85	2.54	0.10	0.65
2.34	11.32	17.99	3.76	67.59	2.60	0.21	0.68
2.44	12.17	19.33	3.86	74.63	2.61	0.37	0.69
2.48	14.56	23.17	3.43	79.44	2.56	0.56	0.71
2.58	18.03	28.74	2.75	79.05	2.47	0.54	0.70

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.63	22.41	35.77	2.21	79.01	2.37	0.54	0.70
2.71	26.08	41.66	1.92	80.03	2.30	0.59	0.71
2.78	30.33	48.48	1.67	80.89	2.22	0.63	0.71
2.82	33.73	53.95	1.52	82.21	2.16	0.70	0.71
2.89	34.94	55.89	1.47	82.24	2.13	0.70	0.71
2.96	33.63	53.77	1.51	81.39	2.16	0.66	0.71
3.03	30.90	49.37	1.62	80.00	2.20	0.58	0.71
3.11	28.98	46.28	1.70	78.46	2.23	0.51	0.70
3.19	26.45	42.22	1.79	75.65	2.26	0.41	0.70
3.25	23.52	37.50	1.97	73.87	2.31	0.35	0.69
3.35	20.49	32.62	2.28	74.42	2.38	0.37	0.69
3.41	17.79	28.29	2.60	73.49	2.44	0.34	0.69
3.50	15.91	25.25	2.74	69.10	2.46	0.24	0.68
3.59	14.83	23.51	2.66	62.63	2.45	0.14	0.66
3.69	14.59	23.12	2.55	58.90	2.43	0.10	0.65
3.79	15.20	24.09	2.35	56.48	2.39	0.09	0.65
3.88	16.54	26.24	2.09	54.78	2.34	0.08	0.64
3.97	19.14	30.40	1.82	55.25	2.27	0.08	0.64
4.07	20.82	33.10	1.77	58.69	2.26	0.10	0.65
4.14	23.49	37.37	1.67	62.38	2.22	0.14	0.66
4.17	25.51	40.62	1.61	65.25	2.20	0.17	0.67
4.26	28.14	44.83	1.51	67.83	2.15	0.21	0.68
4.32	28.71	45.74	1.52	69.43	2.16	0.24	0.68
4.37	28.10	44.77	1.56	69.94	2.18	0.25	0.68
4.42	26.62	42.38	1.65	69.93	2.21	0.25	0.68
4.51	25.07	39.88	1.74	69.30	2.24	0.24	0.68
4.61	23.68	37.65	1.82	68.42	2.27	0.22	0.68
4.65	22.37	35.53	1.90	67.38	2.29	0.21	0.68
4.74	21.09	33.47	2.00	67.06	2.32	0.20	0.68
4.80	20.48	32.49	2.05	66.55	2.33	0.19	0.67
4.89	20.04	31.78	2.09	66.46	2.34	0.19	0.67
4.95	20.38	32.32	2.05	66.20	2.33	0.19	0.67
5.04	21.05	33.39	1.97	65.92	2.31	0.18	0.67
5.13	22.81	36.20	1.80	65.26	2.27	0.17	0.67
5.18	25.27	40.14	1.63	65.28	2.20	0.17	0.67
5.28	28.07	44.63	1.49	66.64	2.14	0.19	0.67
5.32	31.47	50.09	1.40	70.04	2.09	0.26	0.68
5.42	34.67	55.23	1.35	74.62	2.05	0.37	0.69
5.51	38.14	60.80	1.31	79.86	2.01	0.58	0.71
5.60	41.28	65.83	1.26	83.18	1.94	0.71	0.71
5.66	44.24	70.58	1.22	86.14	1.88	0.72	0.72
5.76	45.86	73.17	1.00	73.17	1.83	0.33	0.69
5.85	44.91	71.65	1.21	86.53	1.86	0.72	0.72
5.92	41.11	65.53	1.25	81.79	1.92	0.68	0.71
5.95	38.21	60.87	1.28	77.76	1.96	0.48	0.70
5.97	36.15	57.56	1.30	74.97	1.99	0.38	0.70
6.02	35.37	56.31	1.31	73.90	2.01	0.35	0.69
6.06	32.74	52.08	1.36	70.59	2.05	0.27	0.68

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.16	29.98	47.63	1.42	67.87	2.10	0.21	0.68
6.21	26.98	42.82	1.56	66.83	2.18	0.20	0.68
6.26	24.29	38.48	1.79	68.74	2.26	0.23	0.68
6.31	21.62	34.19	2.18	74.63	2.36	0.37	0.69
6.40	19.23	30.34	2.70	82.06	2.46	0.69	0.71
6.44	16.91	26.60	3.43	91.18	2.56	0.73	0.73
6.52	15.12	23.73	4.16	98.65	2.64	0.75	0.75
6.57	13.47	21.08	5.01	105.63	2.73	0.76	0.76
6.64	12.16	18.96	5.81	110.19	2.80	0.77	0.77
6.69	10.98	17.06	6.65	113.46	2.86	0.77	0.77
6.78	10.34	16.02	7.15	114.49	2.90	0.77	0.77
6.83	9.90	15.31	7.38	112.96	2.91	0.77	0.77
6.92	9.60	14.82	7.45	110.37	2.92	0.77	0.77
6.97	9.39	14.48	7.39	107.07	2.91	0.76	0.76
7.03	9.29	14.32	7.35	105.27	2.91	0.76	0.76
7.12	9.32	14.36	7.25	104.07	2.90	0.76	0.76
7.22	9.39	14.46	7.17	103.64	2.90	0.75	0.75
7.27	9.52	14.66	7.09	103.89	2.89	0.76	0.76
7.36	9.65	14.86	7.06	104.93	2.89	0.76	0.76
7.43	9.75	15.01	7.08	106.34	2.89	0.76	0.76
7.50	9.78	15.06	7.16	107.82	2.90	0.76	0.76
7.59	9.77	15.04	7.22	108.69	2.90	0.76	0.76
7.64	9.70	14.93	7.34	109.64	2.91	0.77	0.77
7.75	9.63	14.81	7.46	110.40	2.92	0.77	0.77
7.79	9.70	14.91	7.43	110.74	2.92	0.77	0.77
7.89	9.97	15.33	7.19	110.22	2.90	0.77	0.77
7.99	10.24	15.76	6.97	109.89	2.88	0.77	0.77
8.04	10.34	15.91	6.96	110.71	2.88	0.77	0.77
8.13	10.31	15.85	7.03	111.39	2.89	0.77	0.77
8.23	10.27	15.79	6.35	100.23	2.84	0.75	0.75
8.32	10.27	15.77	5.78	91.18	2.79	0.73	0.73
8.37	10.53	16.20	5.34	86.47	2.76	0.72	0.72
8.46	11.04	17.00	5.74	97.61	2.79	0.74	0.74
8.56	11.30	17.42	6.05	105.35	2.82	0.76	0.76
8.59	11.30	17.41	6.35	110.51	2.84	0.77	0.77
8.61	11.03	16.97	6.71	113.97	2.87	0.77	0.77
8.67	10.89	16.75	6.98	116.82	2.88	0.78	0.78
8.71	10.69	16.41	7.24	118.78	2.90	0.78	0.78
8.72	10.51	16.13	7.46	120.30	2.92	0.78	0.78
8.78	10.44	16.02	7.56	121.13	2.92	0.78	0.78
8.80	10.44	16.02	7.59	121.54	2.93	0.79	0.79
8.86	10.44	16.01	7.60	121.62	2.93	0.79	0.79
8.90	10.55	16.17	7.55	122.08	2.92	0.79	0.79
8.95	10.68	16.39	7.49	122.77	2.92	0.79	0.79
8.96	10.89	16.71	7.39	123.54	2.91	0.79	0.79
9.00	11.05	16.98	7.33	124.43	2.91	0.79	0.79
9.05	11.29	17.35	7.24	125.55	2.90	0.79	0.79
9.09	11.56	17.78	7.10	126.26	2.89	0.79	0.79

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.10	11.96	18.43	6.89	127.03	2.88	0.79	0.79
9.14	12.47	19.24	6.66	128.15	2.86	0.80	0.80
9.20	13.21	20.42	6.33	129.23	2.84	0.80	0.80
9.24	14.09	21.83	5.95	129.98	2.81	0.80	0.80
9.29	15.03	23.34	5.57	129.97	2.78	0.80	0.80
9.31	15.90	24.74	5.28	130.54	2.75	0.80	0.80
9.38	16.61	25.88	5.06	130.87	2.73	0.80	0.80
9.41	17.32	27.00	4.80	129.53	2.71	0.80	0.80
9.47	18.02	28.13	4.48	126.15	2.68	0.79	0.79
9.53	19.33	30.23	3.91	118.10	2.62	0.78	0.78
9.62	21.08	33.03	3.29	108.83	2.54	0.76	0.76
9.67	23.71	36.88	2.63	97.08	2.45	0.74	0.74
9.77	26.25	39.96	2.22	88.55	2.37	0.73	0.73
9.81	28.83	43.12	1.89	81.52	2.29	0.66	0.71
9.90	30.67	45.16	1.72	77.57	2.24	0.48	0.70
9.97	32.26	46.92	1.61	75.55	2.20	0.40	0.70
10.06	32.63	47.13	1.61	75.67	2.20	0.41	0.70
10.20	32.13	46.19	1.68	77.59	2.22	0.48	0.70
10.30	29.29	42.06	1.79	75.15	2.26	0.39	0.70
10.44	25.52	36.67	2.06	75.52	2.33	0.40	0.70
10.54	20.70	30.03	2.66	79.87	2.45	0.58	0.71
10.63	16.56	24.49	4.08	99.92	2.64	0.75	0.75
10.74	13.83	20.66	5.64	116.62	2.78	0.78	0.78
10.78	12.62	18.99	6.71	127.39	2.86	0.79	0.79
10.83	12.48	18.76	6.96	130.59	2.88	0.80	0.80
10.88	12.31	18.47	7.21	133.16	2.90	0.80	0.80
10.89	12.15	18.24	7.50	136.86	2.92	0.81	0.81
10.97	12.25	18.30	7.62	139.36	2.93	0.81	0.81
11.02	12.48	18.59	7.62	141.70	2.93	0.82	0.82
11.07	12.79	18.96	7.51	142.37	2.92	0.82	0.82
11.11	13.06	19.28	7.42	143.00	2.91	0.82	0.82
11.16	13.39	19.70	7.30	143.71	2.91	0.82	0.82
11.21	13.76	20.15	7.19	144.81	2.90	0.82	0.82
11.26	14.14	20.62	7.10	146.37	2.89	0.82	0.82
11.30	14.37	20.90	7.10	148.42	2.89	0.82	0.82
11.36	14.54	21.07	7.14	150.43	2.90	0.83	0.83
11.40	14.68	21.19	7.17	151.92	2.90	0.83	0.83
11.45	14.81	21.32	7.18	152.97	2.90	0.83	0.83
11.50	15.04	21.57	7.12	153.64	2.89	0.83	0.83
11.55	15.31	21.86	7.06	154.44	2.89	0.83	0.83
11.60	15.85	22.53	6.88	155.07	2.88	0.83	0.83
11.66	16.56	23.39	6.63	155.14	2.86	0.83	0.83
11.74	17.40	24.38	6.31	153.92	2.84	0.83	0.83
11.84	17.98	24.97	6.15	153.46	2.82	0.83	0.83
11.93	18.18	25.08	6.17	154.65	2.82	0.83	0.83
12.04	18.04	24.73	6.38	157.76	2.84	0.84	0.84
12.13	17.87	24.37	6.58	160.42	2.86	0.84	0.84
12.22	17.67	23.94	6.76	161.87	2.87	0.84	0.84

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.27	17.51	23.64	6.85	161.93	2.88	0.84	0.84
12.37	17.27	23.16	6.98	161.58	2.88	0.84	0.84
12.41	17.17	22.94	7.03	161.26	2.89	0.84	0.84
12.51	17.06	22.65	7.13	161.48	2.89	0.84	0.84
12.56	17.23	22.78	7.08	161.37	2.89	0.84	0.84
12.65	17.64	23.15	6.96	161.03	2.88	0.84	0.84
12.71	18.45	24.09	6.70	161.44	2.86	0.84	0.84
12.79	19.23	24.96	6.59	164.56	2.86	0.85	0.85
12.89	20.10	25.92	6.50	168.54	2.85	0.85	0.85
12.96	20.98	26.96	6.43	173.33	2.84	0.86	0.86
13.04	22.23	28.37	6.15	174.57	2.82	0.86	0.86
13.13	24.11	30.49	5.62	171.40	2.78	0.85	0.85
13.23	26.80	33.27	4.19	139.58	2.65	0.81	0.81
13.30	30.34	36.95	2.91	107.47	2.49	0.76	0.76
13.37	34.15	40.77	2.02	82.17	2.32	0.70	0.71
13.47	38.32	45.44	1.87	85.15	2.29	0.72	0.72
13.57	38.79	45.84	1.94	89.15	2.31	0.73	0.73
13.61	39.19	46.27	1.98	91.39	2.31	0.73	0.73
13.62	40.31	47.52	1.94	92.31	2.30	0.73	0.73
13.68	44.31	51.92	1.78	92.36	2.26	0.73	0.73
13.73	47.82	55.76	1.68	93.57	2.22	0.74	0.74
13.77	50.08	58.23	1.65	95.79	2.21	0.74	0.74
13.87	52.91	61.16	1.61	98.26	2.20	0.74	0.74
13.93	55.78	64.26	1.58	101.41	2.19	0.75	0.75
14.00	58.54	67.15	1.55	104.21	2.17	0.76	0.76
14.06	60.62	69.33	1.54	106.89	2.17	0.76	0.76
14.12	62.21	70.95	1.54	109.37	2.17	0.77	0.77
14.21	63.05	71.63	1.55	111.13	2.17	0.77	0.77
14.25	63.45	71.96	1.56	112.44	2.18	0.77	0.77
14.35	63.35	71.51	1.58	112.67	2.18	0.77	0.77
14.45	62.61	70.37	1.60	112.38	2.19	0.77	0.77
14.50	61.06	68.50	1.63	111.75	2.21	0.77	0.77
14.59	59.18	66.15	1.68	111.04	2.22	0.77	0.77
14.64	57.19	63.82	1.73	110.49	2.24	0.77	0.77
14.74	55.60	61.79	1.78	110.08	2.26	0.77	0.77
14.80	54.22	60.12	1.83	109.86	2.27	0.77	0.77
14.88	53.18	58.73	1.87	109.70	2.28	0.77	0.77
14.97	52.24	57.45	1.91	109.62	2.30	0.77	0.77
15.05	51.43	56.38	1.95	110.04	2.31	0.77	0.77
15.13	50.85	55.53	1.99	110.56	2.32	0.77	0.77
15.21	50.95	55.42	1.99	110.46	2.32	0.77	0.77
15.28	52.23	56.58	1.93	109.48	2.30	0.77	0.77
15.36	55.10	59.37	1.82	108.07	2.27	0.76	0.76
15.41	60.22	64.61	1.66	107.30	2.22	0.76	0.76
15.50	66.38	70.74	1.53	108.00	2.16	0.76	0.76
15.55	72.78	77.07	1.38	106.45	2.07	0.76	0.76
15.65	76.92	80.83	1.31	105.71	2.00	0.76	0.76
15.71	78.17	81.68	1.27	103.43	1.94	0.75	0.75

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.79	75.07	78.22	1.28	99.99	1.96	0.75	0.75
15.89	67.29	69.97	1.33	92.88	2.02	0.73	0.73
15.90	61.09	63.58	1.38	88.03	2.07	0.72	0.72
15.94	56.21	58.47	1.45	84.99	2.12	0.72	0.72
16.00	53.24	55.28	1.51	83.45	2.15	0.71	0.71
16.06	47.68	49.45	1.67	82.65	2.22	0.71	0.71
16.14	40.74	42.17	2.02	85.02	2.32	0.72	0.72
16.19	34.10	35.24	2.56	90.26	2.43	0.73	0.73
16.26	27.10	27.88	3.51	97.89	2.57	0.74	0.74
16.33	21.54	22.01	4.74	104.24	2.70	0.76	0.76
16.38	17.06	17.28	6.24	107.80	2.83	0.76	0.76
16.47	14.43	14.45	7.58	109.50	2.93	0.77	0.77
16.54	12.64	12.69	8.71	110.54	3.00	0.77	0.77
16.62	11.80	11.71	9.67	113.31	3.05	0.52	0.84
16.70	11.53	11.36	10.18	115.66	3.08	0.56	0.81
16.76	12.28	12.12	9.88	119.66	3.06	0.59	0.87
16.86	14.88	14.80	8.08	119.59	2.96	0.78	0.78
16.90	19.33	19.15	6.07	116.24	2.82	0.78	0.78
16.98	25.84	25.69	4.22	108.51	2.65	0.76	0.76
17.05	35.42	35.23	2.81	99.11	2.48	0.75	0.75
17.14	47.54	47.19	1.94	91.71	2.30	0.73	0.73
17.20	61.48	60.90	1.51	91.88	2.15	0.73	0.73
17.29	73.03	72.03	1.35	97.56	2.05	0.74	0.74
17.34	81.99	80.70	1.30	104.58	1.99	0.76	0.76
17.44	86.87	85.21	1.28	109.31	1.97	0.76	0.76
17.50	88.89	86.96	1.26	109.36	1.93	0.76	0.76
17.58	88.15	85.91	1.24	106.78	1.91	0.76	0.76
17.64	85.02	82.63	1.24	102.13	1.90	0.75	0.75
17.75	80.50	77.97	1.27	99.12	1.95	0.75	0.75
17.82	72.08	69.66	1.35	93.80	2.04	0.74	0.74
17.89	66.02	63.60	1.43	91.18	2.11	0.73	0.73
17.89	62.68	60.37	1.51	91.04	2.15	0.73	0.73
17.96	64.06	61.55	1.50	92.30	2.15	0.73	0.73
18.02	65.34	62.67	1.51	94.33	2.15	0.74	0.74
18.07	66.86	64.01	1.51	96.43	2.15	0.74	0.74
18.17	68.78	65.62	1.49	98.02	2.14	0.74	0.74
18.22	68.74	65.47	1.51	98.54	2.15	0.75	0.75
18.30	65.20	61.85	1.59	98.20	2.19	0.74	0.74
18.36	57.69	54.52	1.83	99.83	2.27	0.75	0.75
18.42	49.20	46.28	2.30	106.36	2.39	0.76	0.76
18.50	39.97	37.31	3.16	118.00	2.53	0.78	0.78
18.56	32.38	29.97	4.32	129.55	2.66	0.80	0.80
18.62	25.71	23.53	5.80	136.40	2.80	0.81	0.81
18.69	23.96	21.78	6.13	133.60	2.82	0.80	0.80
18.76	22.21	20.05	6.60	132.24	2.86	0.80	0.80
18.84	24.30	21.95	5.90	129.41	2.80	0.80	0.80
18.89	31.88	29.04	4.26	123.66	2.66	0.79	0.79
18.98	52.85	48.61	2.23	108.20	2.37	0.76	0.76

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.05	78.42	72.48	1.52	110.23	2.16	0.77	0.77
19.12	101.80	94.21	1.32	124.65	2.02	0.79	0.79
19.18	115.88	107.18	1.27	136.09	1.95	0.81	0.81
19.24	124.07	114.61	1.25	142.72	1.91	0.82	0.82
19.32	126.76	116.83	1.24	144.84	1.90	0.82	0.82
19.38	126.53	116.38	1.25	145.16	1.92	0.82	0.82
19.46	124.81	114.42	1.26	144.25	1.94	0.82	0.82
19.54	122.62	112.08	1.28	142.92	1.96	0.82	0.82
19.62	121.00	110.26	1.28	141.68	1.97	0.82	0.82
19.70	119.99	109.01	1.29	140.65	1.98	0.81	0.81
19.80	119.75	108.41	1.29	140.01	1.98	0.81	0.81
19.85	119.75	108.23	1.29	139.71	1.98	0.81	0.81
19.94	119.95	108.07	1.29	139.71	1.98	0.81	0.81
20.03	120.73	108.50	1.28	138.61	1.96	0.81	0.81
20.13	121.84	109.19	1.26	137.92	1.94	0.81	0.81
20.19	123.33	110.40	1.25	137.60	1.91	0.81	0.81
20.29	124.05	110.67	1.25	138.32	1.92	0.81	0.81
20.39	124.51	110.70	1.25	138.76	1.93	0.81	0.81
20.43	124.14	110.23	1.26	138.70	1.93	0.81	0.81
20.47	124.09	109.99	1.26	138.78	1.94	0.81	0.81
20.52	123.97	109.69	1.27	139.06	1.95	0.81	0.81
20.61	123.97	109.33	1.27	139.29	1.96	0.81	0.81
20.66	123.26	108.48	1.28	139.08	1.97	0.81	0.81
20.71	122.22	107.35	1.29	138.34	1.98	0.81	0.81
20.77	121.00	106.04	1.30	137.35	1.99	0.81	0.81
20.85	120.53	105.33	1.30	136.79	1.99	0.81	0.81
20.91	120.63	105.23	1.30	136.74	1.99	0.81	0.81
21.00	121.00	105.23	1.30	136.71	1.99	0.81	0.81
21.05	120.93	105.01	1.30	136.53	1.99	0.81	0.81
21.11	120.50	104.40	1.30	136.06	2.00	0.81	0.81
21.19	120.16	103.82	1.31	135.66	2.00	0.81	0.81
21.24	120.23	103.70	1.31	135.67	2.00	0.81	0.81
21.34	120.39	103.52	1.31	135.57	2.00	0.81	0.81
21.39	119.99	103.00	1.31	135.16	2.01	0.81	0.81
21.48	118.68	101.52	1.32	133.84	2.01	0.80	0.80
21.53	116.39	99.34	1.33	131.86	2.02	0.80	0.80
21.64	113.86	96.79	1.34	129.36	2.03	0.80	0.80
21.72	111.80	94.83	1.33	125.65	2.02	0.79	0.79
21.81	110.79	93.80	1.31	122.48	2.00	0.79	0.79
21.89	110.52	93.48	1.28	120.09	1.97	0.78	0.78
21.97	110.69	93.44	1.28	119.40	1.96	0.78	0.78
22.05	110.81	93.32	1.27	118.94	1.96	0.78	0.78
22.12	110.92	93.25	1.27	118.64	1.95	0.78	0.78
22.13	110.89	93.20	1.27	118.54	1.95	0.78	0.78
22.18	111.98	94.01	1.27	119.22	1.95	0.78	0.78
22.22	114.49	96.10	1.26	121.02	1.93	0.78	0.78
22.28	118.47	99.41	1.25	123.90	1.91	0.79	0.79
22.33	122.55	102.85	1.23	126.89	1.90	0.79	0.79

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.38	126.36	106.02	1.22	129.64	1.88	0.80	0.80
22.41	129.99	109.11	1.21	132.05	1.86	0.80	0.80
22.51	133.16	111.59	1.20	133.67	1.85	0.80	0.80
22.56	135.86	113.83	1.18	134.77	1.83	0.81	0.81
22.61	137.68	115.29	1.17	135.13	1.82	0.81	0.81
22.65	139.23	116.56	1.16	135.07	1.81	0.81	0.81
22.71	140.30	117.38	1.15	134.57	1.79	0.81	0.81
22.76	141.15	118.01	1.13	133.54	1.78	0.80	0.80
22.85	141.55	118.16	1.12	132.33	1.77	0.80	0.80
22.89	141.79	118.28	1.11	131.19	1.77	0.80	0.80
22.99	141.85	118.07	1.10	130.38	1.76	0.80	0.80
23.04	142.19	118.24	1.10	129.89	1.76	0.80	0.80
23.12	143.24	118.92	1.09	129.72	1.75	0.80	0.80
23.18	145.12	120.36	1.08	129.86	1.75	0.80	0.80
23.24	147.55	122.28	1.07	130.48	1.74	0.80	0.80
23.33	150.28	124.35	1.05	131.06	1.73	0.80	0.80
23.38	152.77	126.31	1.04	131.98	1.73	0.80	0.80
23.47	154.92	127.86	1.04	132.70	1.72	0.80	0.80
23.52	155.87	128.46	1.05	134.34	1.73	0.80	0.80
23.61	155.50	127.76	1.06	136.02	1.74	0.81	0.81
23.68	153.41	125.65	1.10	137.67	1.76	0.81	0.81
23.76	149.87	122.29	1.13	137.84	1.78	0.81	0.81
23.83	145.42	118.19	1.16	136.72	1.80	0.81	0.81
23.90	140.77	113.95	1.18	134.56	1.83	0.81	0.81
23.97	136.02	109.66	1.20	131.87	1.85	0.80	0.80
24.05	130.36	104.58	1.22	128.11	1.88	0.80	0.80
24.10	123.83	98.86	1.25	123.41	1.92	0.79	0.79
24.19	116.14	92.13	1.28	117.58	1.96	0.78	0.78
24.27	109.37	86.22	1.31	112.54	2.00	0.77	0.77
24.34	103.31	80.98	1.34	108.37	2.03	0.76	0.76
24.43	99.26	77.39	1.37	105.81	2.06	0.76	0.76
24.48	95.99	74.54	1.40	104.29	2.09	0.76	0.76
24.57	93.77	72.46	1.43	103.72	2.11	0.75	0.75
24.62	91.81	70.77	1.45	102.28	2.12	0.75	0.75
24.72	90.33	69.37	1.46	101.12	2.12	0.75	0.75
24.81	89.08	68.17	1.47	100.03	2.13	0.75	0.75
24.86	87.96	67.09	1.50	100.81	2.15	0.75	0.75
24.95	85.18	64.60	1.56	100.88	2.18	0.75	0.75
25.01	82.83	62.55	1.62	101.05	2.20	0.75	0.75
25.02	81.04	61.07	1.66	101.09	2.22	0.75	0.75
25.05	81.81	61.63	1.64	101.34	2.21	0.75	0.75
25.11	82.33	61.92	1.64	101.59	2.21	0.75	0.75
25.15	82.53	61.99	1.64	101.87	2.21	0.75	0.75
25.21	81.92	61.38	1.66	101.94	2.22	0.75	0.75
25.25	81.07	60.61	1.68	101.90	2.23	0.75	0.75
25.30	79.78	59.50	1.70	101.32	2.23	0.75	0.75
25.40	78.02	57.95	1.73	100.17	2.24	0.75	0.75
25.45	75.14	55.63	1.77	98.38	2.25	0.75	0.75

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.52	71.36	52.56	1.83	96.28	2.27	0.74	0.74
25.60	65.60	47.92	1.99	95.12	2.32	0.74	0.74
25.66	58.89	42.57	2.24	95.48	2.37	0.74	0.74
25.74	50.63	36.01	2.77	99.69	2.47	0.75	0.75
25.80	42.60	29.74	3.54	105.15	2.57	0.76	0.76
25.88	34.42	23.44	4.79	112.31	2.71	0.77	0.77
25.94	27.91	18.51	6.33	117.20	2.84	0.78	0.78
26.02	22.69	14.10	8.40	118.43	2.98	0.78	0.78
26.09	19.19	11.73	10.09	118.41	3.07	0.59	0.84
26.17	16.36	9.82	11.90	116.89	3.16	0.54	0.70
26.23	14.50	8.57	13.49	115.61	3.23	0.51	0.61
26.29	13.56	7.93	14.54	115.33	3.28	0.51	0.57
26.37	13.73	8.01	14.49	116.10	3.27	0.51	0.57
26.46	14.95	8.78	13.45	118.10	3.23	0.54	0.63
26.55	16.56	9.80	12.25	120.00	3.18	0.59	0.70
26.60	18.04	10.74	11.37	122.14	3.14	0.60	0.77
26.70	18.79	11.18	11.11	124.24	3.12	0.63	0.80
26.78	19.09	11.34	11.11	125.96	3.12	0.67	0.81
26.87	19.16	11.34	10.61	120.33	3.10	0.66	0.81
26.94	19.06	11.25	9.74	109.55	3.05	0.47	0.80
27.03	18.62	10.92	9.23	100.80	3.03	0.36	0.78
27.13	17.84	10.38	9.61	99.83	3.05	0.42	0.74
27.18	15.89	9.12	11.41	104.10	3.14	0.42	0.65
27.27	14.61	8.27	12.75	105.48	3.20	0.42	0.59
27.32	14.00	7.87	13.55	106.67	3.23	0.43	0.56
27.37	14.68	8.28	12.99	107.59	3.21	0.44	0.59
27.41	15.01	8.48	12.84	108.89	3.20	0.46	0.61
27.46	15.01	8.47	13.04	110.36	3.21	0.47	0.60
27.51	15.19	8.56	13.12	112.25	3.22	0.48	0.61
27.61	15.69	8.84	13.00	114.96	3.21	0.51	0.63
27.66	16.81	9.52	12.66	120.53	3.20	0.56	0.68
27.73	19.30	11.05	11.59	128.02	3.15	0.66	0.79
27.80	22.77	13.18	10.46	137.91	3.09	0.80	0.94
27.88	26.51	15.46	9.62	148.75	3.05	0.98	1.10
27.96	28.73	16.78	9.46	158.82	3.04	1.16	1.20
28.04	29.44	17.16	9.86	169.19	3.06	1.25	1.23
28.12	29.30	17.02	10.34	175.99	3.09	1.41	1.22
28.18	29.78	17.27	10.47	180.83	3.09	1.43	1.23
28.27	30.99	17.95	10.11	181.45	3.07	1.47	1.28
28.32	32.84	19.04	9.54	181.70	3.04	1.48	1.36
28.42	34.90	20.22	8.98	181.66	3.01	1.51	1.44
28.47	37.02	21.47	8.57	183.98	2.99	0.87	0.87
28.61	38.87	22.47	8.32	186.93	2.97	0.87	0.87
28.67	40.79	23.57	8.10	190.99	2.96	0.88	0.88
28.75	43.62	26.58	7.37	195.90	2.91	0.88	0.88
28.81	49.52	30.58	6.28	192.19	2.83	0.88	0.88
28.90	59.16	37.21	4.89	181.92	2.72	0.87	0.87
29.00	70.68	45.27	3.75	169.71	2.60	0.85	0.85

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
29.05	82.68	53.82	2.95	158.84	2.50	0.84	0.84
29.10	92.58	60.99	2.48	151.03	2.42	0.83	0.83
29.15	101.07	67.24	2.13	143.11	2.35	0.82	0.82
29.24	105.88	70.82	1.92	136.02	2.30	0.81	0.81
29.29	107.45	72.19	1.78	128.66	2.26	0.80	0.80
29.37	106.66	71.76	1.71	122.57	2.23	0.79	0.79
29.43	105.44	71.05	1.64	116.77	2.21	0.78	0.78
29.53	104.90	70.72	1.59	112.38	2.19	0.77	0.77
29.62	104.73	70.61	1.55	109.62	2.17	0.77	0.77
29.68	104.75	70.73	1.51	106.89	2.15	0.76	0.76
29.80	104.42	70.36	1.50	105.63	2.15	0.76	0.76
29.91	103.80	69.74	1.50	104.61	2.15	0.76	0.76
30.00	99.10	65.97	1.59	104.86	2.19	0.76	0.76
30.07	97.42	64.55	1.63	105.36	2.21	0.76	0.76
30.15	96.27	63.56	1.66	105.54	2.22	0.76	0.76
30.21	99.04	65.49	1.62	105.77	2.20	0.76	0.76
30.26	98.71	65.16	1.62	105.66	2.20	0.76	0.76
30.31	97.50	64.21	1.64	105.39	2.21	0.76	0.76
30.38	95.52	62.65	1.67	104.86	2.22	0.76	0.76
30.45	92.62	60.44	1.72	104.23	2.24	0.76	0.76
30.50	89.12	57.84	1.79	103.72	2.26	0.75	0.75
30.55	84.94	54.79	1.88	102.88	2.29	0.75	0.75
30.64	81.19	52.03	1.96	101.83	2.31	0.75	0.75
30.70	77.93	49.71	2.01	100.16	2.32	0.75	0.75
30.79	76.04	48.30	2.05	98.96	2.33	0.75	0.75
30.84	75.47	47.86	2.05	98.19	2.33	0.74	0.74
30.93	76.95	48.79	2.01	98.05	2.32	0.74	0.74
30.98	80.15	50.98	1.93	98.14	2.30	0.74	0.74
31.05	85.34	54.54	1.81	98.98	2.27	0.75	0.75
31.13	91.57	58.82	1.71	100.51	2.24	0.75	0.75
31.17	100.46	65.08	1.58	102.97	2.19	0.75	0.75
31.27	110.94	72.52	1.47	106.25	2.13	0.76	0.76
31.32	123.23	81.52	1.37	111.37	2.06	0.77	0.77
31.41	133.45	89.03	1.31	116.56	2.00	0.78	0.78
31.46	140.90	94.67	1.28	120.72	1.96	0.78	0.78
31.52	144.37	97.40	1.26	122.24	1.93	0.79	0.79
31.61	145.01	97.95	1.24	121.83	1.91	0.79	0.79
31.66	142.15	95.90	1.24	119.20	1.91	0.78	0.78
31.75	136.69	91.66	1.26	115.29	1.93	0.78	0.78
31.80	129.14	85.76	1.29	110.68	1.98	0.77	0.77
31.90	122.00	80.16	1.33	106.52	2.02	0.76	0.76
31.94	116.84	76.18	1.37	104.07	2.06	0.76	0.76
32.04	116.03	75.33	1.38	104.00	2.07	0.76	0.76
32.09	119.17	77.25	1.39	107.23	2.08	0.76	0.76
32.20	118.70	76.38	1.43	109.06	2.11	0.76	0.76
32.24	117.72	75.37	1.47	110.44	2.13	0.77	0.77
32.28	114.69	73.02	1.51	110.26	2.15	0.77	0.77
32.29	116.70	74.43	1.49	111.09	2.14	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
32.30	118.93	75.98	1.47	112.06	2.13	0.77	0.77
32.40	120.51	76.91	1.47	112.71	2.13	0.77	0.77
32.45	120.48	76.77	1.47	112.95	2.13	0.77	0.77
32.55	119.13	75.61	1.49	112.51	2.14	0.77	0.77
32.59	118.33	74.91	1.50	112.50	2.15	0.77	0.77
32.69	118.13	74.54	1.51	112.79	2.15	0.77	0.77
32.76	118.09	74.31	1.53	113.51	2.16	0.77	0.77
32.84	118.40	74.31	1.54	114.35	2.17	0.77	0.77
32.90	119.00	74.55	1.55	115.19	2.17	0.77	0.77
32.98	119.95	75.02	1.54	115.83	2.17	0.78	0.78
33.06	121.02	75.61	1.54	116.33	2.17	0.78	0.78
33.12	122.10	76.23	1.53	116.77	2.16	0.78	0.78
33.22	122.84	76.56	1.53	117.03	2.16	0.78	0.78
33.31	123.21	76.64	1.53	117.14	2.16	0.78	0.78
33.37	123.28	76.59	1.53	117.11	2.16	0.78	0.78
33.46	123.28	76.41	1.53	117.00	2.16	0.78	0.78
33.55	123.18	76.17	1.54	117.00	2.17	0.78	0.78
33.65	122.98	75.83	1.54	117.07	2.17	0.78	0.78
33.70	122.57	75.42	1.55	117.18	2.17	0.78	0.78
33.79	122.03	74.86	1.56	117.10	2.18	0.78	0.78
33.89	121.09	74.04	1.58	116.76	2.18	0.78	0.78
33.99	119.77	72.98	1.59	116.20	2.19	0.78	0.78
34.04	117.79	71.55	1.61	115.43	2.20	0.78	0.78
34.13	115.49	69.85	1.64	114.59	2.21	0.77	0.77
34.23	112.70	67.80	1.68	113.76	2.22	0.77	0.77
34.32	110.27	66.01	1.71	113.20	2.24	0.77	0.77
34.37	108.22	64.55	1.75	112.84	2.25	0.77	0.77
34.47	106.60	63.31	1.78	112.69	2.26	0.77	0.77
34.55	103.47	61.05	1.85	112.96	2.28	0.77	0.77
34.63	96.66	56.31	2.04	114.64	2.33	0.77	0.77
34.73	86.37	49.33	2.40	118.21	2.40	0.78	0.78
34.80	72.76	40.42	3.06	123.59	2.51	0.79	0.79
34.90	60.46	32.62	3.90	127.28	2.62	0.79	0.79
35.00	54.92	29.29	4.16	121.79	2.64	0.79	0.79
35.12	50.37	26.54	4.42	117.31	2.67	0.78	0.78
35.20	52.86	28.11	3.99	112.19	2.63	0.77	0.77
35.33	53.65	28.43	4.02	114.42	2.63	0.77	0.77
35.41	63.41	34.44	3.20	110.34	2.53	0.77	0.77
35.44	68.58	37.68	2.87	108.02	2.48	0.76	0.76
35.48	76.82	42.96	2.42	103.82	2.41	0.76	0.76
35.57	84.09	47.63	2.12	101.05	2.35	0.75	0.75
35.62	98.70	57.30	1.73	98.99	2.24	0.75	0.75
35.67	115.40	68.51	1.49	102.07	2.14	0.75	0.75
35.71	137.52	83.52	1.35	112.52	2.04	0.77	0.77
35.82	159.89	98.71	1.28	126.36	1.96	0.79	0.79
35.86	185.11	116.11	1.23	143.07	1.89	0.82	0.82
35.93	207.72	131.80	1.19	156.85	1.84	0.84	0.84
36.01	225.38	144.00	1.16	166.33	1.80	0.85	0.85

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
36.06	235.57	150.92	1.14	171.69	1.79	0.85	0.85
36.12	240.67	154.12	1.13	174.89	1.78	0.86	0.86
36.18	245.05	156.73	1.14	178.20	1.79	0.86	0.86
36.25	248.69	158.84	1.14	180.98	1.79	0.87	0.87
36.30	251.52	160.26	1.15	184.12	1.80	0.87	0.87
36.39	252.83	160.54	1.16	185.99	1.81	0.87	0.87
36.44	253.07	160.15	1.17	187.57	1.82	0.87	0.87
36.53	251.49	158.45	1.18	187.51	1.83	0.87	0.87
36.59	248.39	155.45	1.21	187.43	1.86	0.87	0.87
36.68	243.47	151.62	1.22	184.49	1.87	0.87	0.87
36.75	238.34	147.93	1.22	180.99	1.88	0.87	0.87
36.83	232.04	143.78	1.22	175.91	1.88	0.86	0.86
36.90	225.27	138.95	1.23	171.34	1.89	0.85	0.85
36.97	217.18	133.11	1.25	166.05	1.92	0.85	0.85
37.02	201.72	122.19	1.28	156.23	1.96	0.84	0.84
37.04	193.70	116.64	1.30	151.13	1.99	0.83	0.83
37.08	188.61	113.19	1.30	147.61	2.00	0.82	0.82
37.17	191.78	115.46	1.29	148.65	1.97	0.83	0.83
37.27	187.30	112.45	1.29	145.04	1.98	0.82	0.82
37.37	181.37	108.42	1.30	140.68	1.99	0.81	0.81
37.42	177.21	105.83	1.30	137.22	1.99	0.81	0.81
37.51	175.89	105.19	1.29	135.25	1.97	0.81	0.81
37.58	176.97	106.34	1.27	134.76	1.95	0.81	0.81
37.66	179.01	108.07	1.25	135.08	1.92	0.81	0.81
37.76	182.58	110.83	1.23	136.26	1.89	0.81	0.81
37.85	186.08	113.57	1.21	137.18	1.86	0.81	0.81
37.93	189.62	116.22	1.19	138.14	1.84	0.81	0.81
38.04	192.25	117.99	1.18	138.80	1.82	0.81	0.81
38.13	193.87	118.97	1.17	139.30	1.82	0.81	0.81
38.18	193.57	118.63	1.17	139.16	1.82	0.81	0.81
38.28	191.24	116.58	1.19	138.51	1.84	0.81	0.81
38.37	187.40	113.37	1.21	137.08	1.86	0.81	0.81
38.47	183.55	109.99	1.23	135.63	1.89	0.81	0.81
38.57	180.39	107.19	1.25	134.14	1.92	0.80	0.80
38.62	176.78	104.23	1.27	132.48	1.95	0.80	0.80
38.72	167.48	97.43	1.31	127.27	2.00	0.79	0.79
38.78	160.21	92.19	1.34	123.72	2.04	0.79	0.79
38.81	155.32	88.77	1.37	121.63	2.06	0.79	0.79
38.86	155.19	88.54	1.37	121.68	2.07	0.79	0.79
38.91	152.02	86.27	1.40	120.51	2.08	0.78	0.78
38.95	145.92	82.06	1.44	118.55	2.12	0.78	0.78
39.05	139.55	77.66	1.51	116.91	2.15	0.78	0.78
39.09	132.37	72.88	1.59	115.64	2.19	0.78	0.78
39.14	125.06	68.10	1.69	114.83	2.23	0.77	0.77
39.24	118.19	63.61	1.80	114.32	2.26	0.77	0.77
39.29	112.16	59.80	1.91	114.03	2.30	0.77	0.77
39.39	108.48	57.39	1.99	114.16	2.32	0.77	0.77
39.43	109.15	57.74	1.98	114.28	2.31	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
39.53	115.02	61.25	1.86	113.89	2.28	0.77	0.77
39.57	124.17	67.01	1.69	113.55	2.23	0.77	0.77
39.68	130.64	71.04	1.60	113.69	2.19	0.77	0.77
39.73	131.95	71.83	1.58	113.53	2.19	0.77	0.77
39.81	129.33	70.10	1.60	112.48	2.20	0.77	0.77
39.89	126.37	68.39	1.60	109.51	2.19	0.77	0.77
39.96	125.26	68.01	1.56	105.89	2.18	0.76	0.76
40.06	124.52	67.75	1.52	103.14	2.16	0.75	0.75
40.15	122.70	66.50	1.54	102.38	2.17	0.75	0.75
40.20	114.41	61.03	1.67	102.07	2.22	0.75	0.75
40.24	108.56	57.23	1.79	102.62	2.26	0.75	0.75
40.26	104.17	54.45	1.90	103.22	2.29	0.75	0.75
40.27	107.91	56.72	1.82	103.36	2.27	0.75	0.75
40.37	109.77	57.73	1.80	103.81	2.26	0.76	0.76
40.42	111.64	58.75	1.78	104.71	2.26	0.76	0.76
40.52	112.38	59.02	1.79	105.44	2.26	0.76	0.76
40.56	115.27	60.66	1.76	106.63	2.25	0.76	0.76
40.66	122.24	64.78	1.67	108.06	2.22	0.76	0.76
40.70	131.54	70.42	1.57	110.67	2.18	0.77	0.77
40.75	142.59	77.15	1.49	114.79	2.14	0.77	0.77
40.85	153.40	83.66	1.43	119.75	2.11	0.78	0.78
40.91	164.05	90.16	1.39	125.10	2.08	0.79	0.79
40.96	174.69	96.83	1.35	130.56	2.04	0.80	0.80
41.04	184.27	102.87	1.32	135.59	2.01	0.81	0.81
41.09	193.94	109.10	1.29	141.03	1.98	0.81	0.81
41.18	201.90	114.17	1.28	145.57	1.96	0.82	0.82
41.23	207.97	118.08	1.26	149.12	1.94	0.83	0.83
41.29	211.58	120.37	1.26	151.17	1.93	0.83	0.83
41.38	212.76	120.98	1.25	151.67	1.93	0.83	0.83
41.42	212.09	120.40	1.26	151.21	1.93	0.83	0.83
41.52	210.03	118.76	1.26	149.86	1.94	0.83	0.83
41.57	207.27	116.72	1.27	148.26	1.95	0.82	0.82
41.62	204.91	114.93	1.28	146.93	1.96	0.82	0.82
41.71	203.13	113.45	1.29	145.89	1.97	0.82	0.82
41.76	202.15	112.60	1.29	145.43	1.98	0.82	0.82
41.84	201.65	111.98	1.30	145.17	1.99	0.82	0.82
41.91	201.54	111.64	1.30	145.22	1.99	0.82	0.82
41.95	201.75	111.52	1.31	145.53	2.00	0.82	0.82
42.01	202.52	111.63	1.31	146.36	2.00	0.82	0.82
42.10	203.57	111.82	1.32	147.40	2.01	0.82	0.82
42.15	204.98	112.23	1.33	148.90	2.02	0.83	0.83
42.24	206.03	112.44	1.33	149.94	2.03	0.83	0.83
42.28	206.46	112.53	1.34	150.31	2.03	0.83	0.83
42.39	206.26	112.27	1.33	149.81	2.03	0.83	0.83
42.43	206.08	112.28	1.33	149.14	2.02	0.83	0.83
42.50	206.11	112.45	1.32	148.36	2.01	0.82	0.82
42.58	206.28	112.80	1.31	147.54	2.00	0.82	0.82
42.65	198.95	108.28	1.32	142.73	2.01	0.82	0.82

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
42.70	195.88	106.39	1.32	140.58	2.02	0.81	0.81
42.73	193.72	105.08	1.32	139.14	2.02	0.81	0.81
42.77	200.19	109.31	1.30	142.31	1.99	0.82	0.82
42.82	203.83	111.68	1.29	144.06	1.98	0.82	0.82
42.87	209.12	115.10	1.28	146.92	1.96	0.82	0.82
42.91	215.46	119.14	1.26	150.57	1.94	0.83	0.83
42.97	221.76	123.09	1.25	154.27	1.92	0.83	0.83
43.02	226.82	126.14	1.25	157.35	1.92	0.84	0.84
43.06	230.49	128.19	1.25	159.72	1.91	0.84	0.84
43.11	234.33	130.34	1.24	162.21	1.91	0.84	0.84
43.17	237.93	132.40	1.24	164.40	1.91	0.85	0.85
43.21	242.21	135.09	1.23	166.83	1.90	0.85	0.85
43.29	246.19	137.59	1.23	168.85	1.89	0.85	0.85
43.34	250.53	140.43	1.22	171.05	1.87	0.85	0.85
43.39	254.11	142.76	1.21	172.71	1.86	0.86	0.86
43.45	256.87	144.64	1.20	173.74	1.85	0.86	0.86
43.51	258.25	145.84	1.19	173.50	1.84	0.86	0.86
43.59	258.59	146.35	1.18	172.47	1.82	0.86	0.86
43.64	259.19	147.38	1.16	170.73	1.80	0.85	0.85
43.70	259.29	148.12	1.13	168.10	1.78	0.85	0.85
43.78	258.35	147.98	1.12	165.08	1.77	0.85	0.85
43.88	255.18	145.77	1.12	163.55	1.77	0.84	0.84
43.94	244.77	138.10	1.17	161.52	1.82	0.84	0.84
44.04	234.93	130.84	1.21	157.74	1.86	0.84	0.84
44.07	225.87	124.41	1.23	153.31	1.89	0.83	0.83
44.12	223.58	122.68	1.24	152.08	1.90	0.83	0.83
44.16	221.15	120.94	1.25	150.70	1.91	0.83	0.83
44.21	218.05	118.76	1.25	148.86	1.93	0.83	0.83
44.26	214.65	116.39	1.26	146.86	1.94	0.82	0.82
44.31	210.81	113.73	1.27	144.63	1.95	0.82	0.82
44.35	206.97	111.11	1.28	142.44	1.97	0.82	0.82
44.40	203.26	108.60	1.29	140.32	1.98	0.81	0.81
44.45	200.16	106.49	1.30	138.56	1.99	0.81	0.81
44.50	197.83	104.91	1.31	137.24	2.00	0.81	0.81
44.54	195.81	103.53	1.32	136.15	2.01	0.81	0.81
44.60	193.46	101.86	1.32	134.97	2.02	0.81	0.81
44.64	190.96	100.11	1.34	133.85	2.03	0.80	0.80
44.69	188.57	98.42	1.35	132.85	2.05	0.80	0.80
44.74	187.78	97.76	1.36	132.59	2.05	0.80	0.80
44.79	187.17	97.27	1.36	132.34	2.06	0.80	0.80
44.83	187.71	97.52	1.36	132.53	2.05	0.80	0.80
44.88	188.84	98.15	1.35	132.96	2.05	0.80	0.80
44.93	191.20	99.52	1.35	134.02	2.04	0.80	0.80
44.98	193.69	100.99	1.34	135.20	2.03	0.81	0.81
45.03	195.31	101.90	1.33	135.95	2.03	0.81	0.81
45.08	196.49	102.54	1.33	136.45	2.03	0.81	0.81
45.16	197.53	103.08	1.33	136.81	2.02	0.81	0.81
45.19	198.24	103.58	1.32	136.91	2.02	0.81	0.81

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
45.27	198.44	103.76	1.32	136.53	2.01	0.81	0.81
45.32	197.56	103.38	1.31	135.53	2.00	0.81	0.81
45.37	195.58	102.45	1.31	133.73	2.00	0.80	0.80
45.45	192.44	100.80	1.30	131.17	1.99	0.80	0.80
45.51	187.22	97.91	1.30	127.52	1.99	0.79	0.79
45.56	180.52	93.92	1.31	123.37	2.01	0.79	0.79
45.61	169.84	87.34	1.35	117.60	2.04	0.78	0.78
45.69	156.32	78.89	1.42	111.79	2.10	0.77	0.77
45.75	137.42	67.17	1.61	108.19	2.20	0.76	0.76
45.81	115.31	54.45	1.93	105.04	2.30	0.76	0.76
45.89	93.28	42.25	2.49	105.10	2.42	0.76	0.76
45.94	73.36	31.83	3.26	103.73	2.54	0.75	0.75
46.04	59.21	24.44	4.42	108.05	2.67	0.76	0.76
46.08	46.61	18.15	6.18	112.07	2.83	0.77	0.77
46.15	39.94	13.37	8.22	109.85	2.97	0.77	0.77
46.17	36.10	11.98	9.26	110.89	3.03	0.63	0.86
46.18	36.17	12.00	9.18	110.17	3.02	0.63	0.86
46.23	36.48	12.10	9.03	109.18	3.01	0.62	0.86
46.27	37.18	12.34	8.72	107.58	3.00	0.76	0.76
46.32	38.64	12.85	8.20	105.33	2.96	0.76	0.76
46.41	40.63	15.29	7.01	107.19	2.89	0.76	0.76
46.47	43.16	16.49	6.44	106.19	2.85	0.76	0.76
46.52	45.45	17.54	6.09	106.89	2.82	0.76	0.76
46.56	47.57	18.46	5.95	109.81	2.81	0.77	0.77
46.65	49.42	19.21	5.91	113.60	2.80	0.77	0.77
46.71	51.52	20.07	5.86	117.68	2.80	0.78	0.78
46.76	54.41	21.37	5.62	120.04	2.78	0.78	0.78
46.85	58.19	23.13	5.21	120.43	2.75	0.78	0.78
46.90	63.28	25.63	4.63	118.71	2.69	0.78	0.78
46.99	67.89	27.93	4.16	116.19	2.65	0.78	0.78
47.04	70.35	29.16	3.93	114.63	2.62	0.77	0.77
47.10	69.50	28.71	4.00	114.71	2.63	0.77	0.77
47.16	65.45	26.63	4.36	116.10	2.67	0.78	0.78
47.23	59.62	23.71	4.94	117.23	2.72	0.78	0.78
47.30	51.46	19.76	5.97	117.96	2.81	0.78	0.78
47.38	42.76	13.97	8.12	113.48	2.96	0.77	0.77
47.43	34.23	10.97	10.19	111.84	3.08	0.65	0.78
47.52	28.17	8.83	11.99	105.92	3.17	0.55	0.63
47.59	23.92	7.34	12.70	93.23	3.20	0.41	0.52
47.66	21.40	6.45	12.70	81.89	3.20	0.22	0.46
47.77	19.71	5.85	12.77	74.67	3.20	0.23	0.42
47.82	18.77	5.51	13.75	75.76	3.24	0.23	0.39
47.91	18.38	5.37	14.28	76.63	3.26	0.24	0.38
47.93	17.68	5.12	15.17	77.65	3.30	0.24	0.37
47.97	17.78	5.15	15.21	78.37	3.30	0.25	0.37
48.02	17.86	5.17	15.38	79.56	3.31	0.26	0.37
48.07	18.51	5.39	15.07	81.21	3.30	0.27	0.38
48.12	18.61	5.42	15.51	84.04	3.31	0.29	0.39

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.19	18.71	5.44	15.90	86.54	3.33	0.33	0.39
48.23	18.91	5.51	16.11	88.74	3.33	0.34	0.39
48.31	19.15	5.58	16.11	89.88	3.33	0.35	0.40
48.35	19.35	5.64	16.11	90.92	3.33	0.36	0.40
48.40	19.25	5.60	16.37	91.72	3.34	0.37	0.40
48.45	18.81	5.45	16.96	92.39	3.36	0.37	0.39
48.50	18.07	5.19	17.92	92.93	3.40	0.38	0.37
48.55	17.80	5.09	18.35	93.37	3.41	0.38	0.36
48.59	17.64	5.03	18.75	94.24	3.42	0.39	0.36
48.67	17.87	5.10	18.56	94.62	3.42	0.40	0.36
48.73	17.84	5.08	18.58	94.36	3.42	0.39	0.36
48.78	17.97	5.12	18.13	92.80	3.40	0.38	0.37
48.83	17.97	5.11	17.74	90.68	3.39	0.36	0.37
48.91	17.94	5.09	17.35	88.35	3.38	0.33	0.36
48.98	17.84	5.05	17.10	86.35	3.37	0.32	0.36
49.03	17.74	5.01	17.00	85.19	3.37	0.31	0.36
49.12	17.68	4.98	16.65	82.90	3.35	0.30	0.36
49.17	17.75	5.00	15.91	79.48	3.33	0.26	0.36
49.27	18.02	5.08	15.07	76.51	3.30	0.22	0.36
49.31	18.56	5.25	14.57	76.55	3.28	0.24	0.38
49.38	19.20	5.46	14.44	78.88	3.27	0.26	0.39
49.45	19.70	5.62	14.44	81.15	3.27	0.28	0.40
49.51	19.00	5.38	15.44	83.00	3.31	0.29	0.38
49.54	19.44	5.52	15.24	84.13	3.30	0.30	0.39
49.59	20.18	5.76	14.65	84.45	3.28	0.31	0.41
49.64	21.53	6.21	13.47	83.63	3.23	0.31	0.44
49.73	21.20	6.09	13.64	83.01	3.24	0.29	0.43
49.83	20.02	5.68	14.52	82.47	3.27	0.29	0.41
49.92	18.88	5.29	15.55	82.19	3.31	0.29	0.38
49.98	17.86	4.94	16.51	81.62	3.35	0.28	0.35
50.07	17.33	4.75	17.04	81.01	3.37	0.27	0.34
50.16	16.99	4.63	17.38	80.51	3.38	0.27	0.33
50.24	16.69	4.52	17.70	80.06	3.39	0.27	0.32
50.32	16.46	4.44	17.99	79.87	3.40	0.26	0.32
50.41	16.32	4.39	18.25	80.02	3.41	0.26	0.31
50.50	16.36	4.39	18.25	80.09	3.41	0.27	0.31
50.56	16.26	4.35	18.25	79.36	3.41	0.27	0.31
50.66	16.09	4.28	18.27	78.27	3.41	0.25	0.31
50.74	15.92	4.22	18.37	77.53	3.41	0.24	0.30
50.84	15.85	4.19	19.00	79.62	3.43	0.25	0.30
50.93	15.95	4.21	19.91	83.88	3.46	0.30	0.30
50.98	16.77	4.47	20.59	92.08	3.48	0.35	0.32
51.08	19.60	5.39	19.08	102.75	3.43	0.47	0.38
51.17	24.45	6.95	16.30	113.31	3.34	0.63	0.50
51.24	30.11	8.78	13.98	122.80	3.25	0.75	0.63
51.34	33.65	9.91	13.03	129.12	3.21	0.89	0.71
51.41	34.16	10.06	12.19	122.59	3.18	0.93	0.72
51.51	32.81	9.60	12.05	115.66	3.17	0.50	0.69

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
51.58	31.20	9.06	11.80	106.93	3.16	0.61	0.65
51.68	29.95	8.64	12.73	109.98	3.20	0.60	0.62
51.79	27.39	7.80	14.12	110.16	3.26	0.59	0.56
51.82	25.87	7.31	15.07	110.15	3.30	0.59	0.52
51.85	24.39	6.83	16.27	111.07	3.34	0.59	0.49
51.91	25.00	7.01	16.14	113.23	3.34	0.60	0.50
52.00	24.87	6.96	16.71	116.25	3.36	0.67	0.50
52.05	27.06	7.65	15.54	118.92	3.31	0.70	0.55
52.10	31.78	9.15	13.00	118.95	3.21	0.72	0.65
52.19	38.49	11.27	10.28	115.81	3.08	0.73	0.80
52.28	44.04	13.02	8.58	111.69	2.99	0.77	0.77
52.34	46.37	13.74	7.96	109.32	2.95	0.76	0.76
52.42	46.09	13.63	8.05	109.66	2.96	0.77	0.77
52.48	44.34	13.05	8.50	111.03	2.98	0.77	0.77
52.57	42.32	12.39	8.98	111.27	3.01	0.69	0.88
52.62	40.26	11.73	9.37	109.88	3.03	0.66	0.84
52.69	38.51	11.16	9.58	106.89	3.05	0.61	0.80
52.77	36.89	10.63	9.83	104.50	3.06	0.56	0.76
52.87	35.55	10.19	10.19	103.83	3.08	0.55	0.73
52.91	34.07	9.71	10.56	102.56	3.10	0.57	0.69
53.01	32.55	9.21	11.08	102.13	3.12	0.49	0.66
53.10	32.18	9.08	11.35	103.11	3.14	0.52	0.65
53.16	34.04	9.65	11.74	113.26	3.15	0.59	0.69
53.25	38.69	11.08	11.13	123.32	3.13	0.87	0.79
53.29	44.28	12.82	10.63	136.25	3.10	0.97	0.92
53.38	48.90	14.23	10.13	144.18	3.07	1.22	1.02
53.42	59.32	17.47	8.56	149.47	2.99	0.83	0.83
53.47	74.66	22.21	6.75	150.02	2.87	0.83	0.83
53.52	92.88	27.85	5.32	148.22	2.76	0.82	0.82
53.58	102.94	30.94	4.93	152.55	2.72	0.83	0.83
53.66	103.80	31.15	5.14	160.18	2.74	0.84	0.84
53.75	98.64	29.50	5.74	169.41	2.79	0.85	0.85
53.81	88.93	26.46	6.64	175.67	2.86	0.86	0.86
53.87	78.89	23.33	7.63	177.89	2.93	0.86	0.86
53.95	67.24	19.70	9.07	178.71	3.02	1.90	1.41
54.01	57.35	16.64	10.67	177.57	3.10	1.79	1.19
54.06	47.51	13.60	12.71	172.90	3.20	1.68	0.97
54.15	41.78	11.83	14.16	167.57	3.26	1.42	0.85
54.20	40.60	11.46	14.42	165.24	3.27	1.40	0.82
54.29	47.57	13.59	12.09	164.23	3.17	1.54	0.97
54.34	69.40	20.27	7.00	141.87	2.89	0.82	0.82
54.43	100.37	29.73	3.65	108.63	2.59	0.76	0.76
54.45	137.16	41.00	2.00	82.07	2.32	0.69	0.71
54.48	166.07	49.83	1.62	80.59	2.20	0.61	0.71
54.52	185.51	55.76	1.48	82.69	2.14	0.71	0.71
54.53	198.85	59.83	1.45	86.57	2.12	0.72	0.72
54.58	207.94	62.58	1.44	89.91	2.11	0.73	0.73
54.62	219.64	66.13	1.42	93.59	2.10	0.74	0.74

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
54.65	233.46	70.33	1.38	96.81	2.07	0.74	0.74
54.70	244.67	73.72	1.36	99.98	2.05	0.75	0.75
54.76	251.12	75.64	1.35	102.23	2.05	0.75	0.75
54.77	249.88	75.25	1.37	102.77	2.06	0.75	0.75
54.82	251.50	75.71	1.36	103.16	2.06	0.75	0.75
54.87	253.07	76.14	1.36	103.55	2.05	0.75	0.75
54.88	255.63	76.92	1.35	104.08	2.05	0.76	0.76
54.91	257.28	77.39	1.35	104.56	2.05	0.76	0.76
54.96	263.42	79.22	1.34	106.09	2.04	0.76	0.76
54.97	276.70	83.26	1.32	109.90	2.01	0.77	0.77
55.03	294.89	88.74	1.30	115.47	1.99	0.78	0.78
55.09	315.21	94.86	1.27	120.89	1.96	0.78	0.78
55.15	327.84	98.63	1.23	121.55	1.89	0.79	0.79
55.20	338.35	101.77	1.20	122.41	1.85	0.79	0.79
55.25	358.17	107.74	1.13	121.49	1.78	0.79	0.79
55.30	386.84	116.38	1.11	129.28	1.77	0.80	0.80
55.34	417.50	125.63	1.07	134.62	1.74	0.81	0.81
55.39	440.05	132.40	1.10	146.03	1.76	0.82	0.82
55.40	462.28	139.13	1.10	153.71	1.76	0.83	0.83
55.44	482.80	145.29	1.08	157.35	1.75	0.84	0.84
55.44	511.21	153.88	1.02	157.04	1.72	0.84	0.84
55.49	517.76	155.78	1.03	160.78	1.72	0.84	0.84
55.54	533.43	160.44	1.05	167.71	1.73	0.85	0.85
55.59	534.98	160.82	1.10	176.17	1.76	0.86	0.86
55.63	551.08	165.61	1.09	180.34	1.75	0.86	0.86
55.64	553.47	166.31	1.09	180.79	1.75	0.87	0.87
55.68	566.94	170.31	1.06	179.92	1.73	0.86	0.86
55.69	570.38	171.33	1.04	178.50	1.73	0.86	0.86
55.69	566.17	170.04	1.05	179.38	1.73	0.86	0.86
55.71	561.62	168.63	1.09	183.08	1.75	0.87	0.87
55.76	567.28	170.25	1.10	186.45	1.76	0.87	0.87
55.78	580.19	174.11	1.08	187.85	1.75	0.87	0.87
55.81	581.23	174.36	1.04	180.96	1.72	0.87	0.87
55.85	584.16	175.16	1.00	175.16	1.69	0.86	0.86
55.86	588.34	176.41	1.00	176.41	1.65	0.86	0.86
55.91	598.65	179.42	1.00	179.42	1.62	0.86	0.86
55.92	602.25	180.48	1.00	180.48	1.60	0.87	0.87
55.96	619.03	185.46	1.00	185.46	1.58	0.87	0.87
55.97	634.09	189.98	1.00	189.98	1.57	0.88	0.88
56.00	654.37	196.01	1.00	196.01	1.56	0.88	0.88
56.01	660.12	197.72	1.00	197.72	1.58	0.88	0.88
56.03	661.79	198.18	1.00	198.18	1.59	0.88	0.88
56.05	661.82	198.14	1.00	198.14	1.60	0.88	0.88
56.10	665.04	198.99	1.00	198.99	1.60	0.89	0.89
56.12	668.02	199.86	1.00	199.86	1.58	0.89	0.89
56.16	667.69	199.67	1.00	199.67	1.57	0.89	0.89
56.17	654.78	195.76	1.00	195.76	1.57	0.88	0.88
56.20	635.11	189.78	1.00	189.78	1.59	0.88	0.88

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
56.22	617.48	184.46	1.00	184.46	1.61	0.87	0.87
56.24	608.45	181.69	1.00	181.69	1.61	0.87	0.87
56.30	602.69	179.84	1.00	179.84	1.62	0.86	0.86
56.31	595.69	177.72	1.00	177.72	1.63	0.86	0.86
56.34	586.22	174.82	1.00	174.82	1.65	0.86	0.86
56.39	579.04	172.57	1.00	172.57	1.66	0.86	0.86
56.45	572.30	170.44	1.00	170.44	1.67	0.85	0.85
56.48	565.39	168.31	1.00	168.31	1.67	0.85	0.85
56.49	555.45	165.32	1.00	165.32	1.70	0.85	0.85
56.53	542.15	161.25	1.05	168.57	1.73	0.85	0.85
56.58	529.04	157.24	1.08	169.38	1.75	0.85	0.85
56.63	524.73	155.86	1.00	155.86	1.67	0.83	0.83
56.68	526.01	156.17	1.00	156.17	1.58	0.84	0.84
56.73	531.33	157.68	1.00	157.68	1.53	0.84	0.84
56.78	526.31	156.09	1.00	156.09	1.62	0.84	0.84
56.83	517.99	153.53	1.00	153.53	1.69	0.83	0.83
56.89	503.37	149.05	1.06	157.35	1.73	0.84	0.84
56.95	485.04	143.50	1.12	160.76	1.77	0.84	0.84
56.99	470.25	139.02	1.16	161.37	1.81	0.84	0.84
57.01	460.92	136.23	1.18	160.98	1.83	0.84	0.84
57.04	461.73	136.41	1.18	160.65	1.82	0.84	0.84
57.09	468.20	138.26	1.17	161.13	1.81	0.84	0.84
57.11	477.43	140.98	1.16	163.57	1.81	0.84	0.84
57.13	488.62	144.26	1.16	167.47	1.81	0.85	0.85
57.18	488.78	144.24	1.17	169.44	1.82	0.85	0.85
57.19	477.80	140.96	1.20	168.95	1.85	0.85	0.85
57.21	464.47	136.96	1.21	166.30	1.87	0.85	0.85
57.24	456.12	134.45	1.22	164.00	1.88	0.85	0.85
57.28	456.72	134.56	1.21	163.35	1.87	0.84	0.84
57.32	450.91	132.78	1.22	161.45	1.87	0.84	0.84
57.35	445.39	131.08	1.22	160.03	1.88	0.84	0.84
57.38	435.59	128.14	1.23	157.50	1.89	0.84	0.84
57.43	430.50	126.56	1.23	155.53	1.89	0.83	0.83
57.48	414.66	121.80	1.23	150.26	1.90	0.83	0.83
57.52	398.59	116.98	1.23	143.92	1.89	0.82	0.82
57.57	389.56	114.25	1.25	142.28	1.91	0.82	0.82
57.62	396.66	116.29	1.26	146.53	1.94	0.82	0.82
57.68	427.50	125.32	1.25	157.03	1.92	0.84	0.84
57.76	462.23	135.46	1.23	166.00	1.88	0.85	0.85
57.81	505.50	148.16	1.09	161.17	1.75	0.84	0.84
57.86	543.58	159.31	1.00	159.31	1.63	0.84	0.84
57.89	572.52	167.80	1.00	167.80	1.49	0.85	0.85
57.91	583.54	171.02	1.00	171.02	1.48	0.85	0.85
57.92	577.13	169.11	1.00	169.11	1.50	0.85	0.85
57.95	569.05	166.67	1.00	166.67	1.54	0.85	0.85
57.99	570.66	167.08	1.00	167.08	1.56	0.85	0.85
58.01	578.72	169.42	1.00	169.42	1.57	0.85	0.85
58.05	591.19	173.02	1.00	173.02	1.58	0.86	0.86

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
58.05	598.87	175.27	1.00	175.27	1.59	0.86	0.86
58.10	604.77	176.91	1.00	176.91	1.60	0.86	0.86
58.13	611.17	178.73	1.00	178.73	1.60	0.86	0.86
58.15	618.51	180.87	1.00	180.87	1.60	0.87	0.87
58.17	625.12	182.75	1.00	182.75	1.59	0.87	0.87
58.20	623.43	182.21	1.00	182.21	1.59	0.87	0.87
58.21	619.40	181.00	1.00	181.00	1.60	0.87	0.87
58.21	614.30	179.50	1.00	179.50	1.61	0.86	0.86
58.23	613.93	179.34	1.00	179.34	1.61	0.86	0.86
58.24	608.11	177.62	1.00	177.62	1.62	0.86	0.86
58.25	609.21	177.92	1.00	177.92	1.54	0.86	0.86
58.29	613.99	179.26	1.00	179.26	1.44	0.86	0.86
58.31	627.24	183.11	1.00	183.11	1.32	0.87	0.87
58.33	639.00	186.52	1.00	186.52	1.34	0.87	0.87
58.38	651.36	190.06	1.00	190.06	1.37	0.88	0.88
58.39	661.87	193.13	1.00	193.13	1.39	0.88	0.88
58.43	670.53	195.59	1.00	195.59	1.40	0.88	0.88
58.43	682.73	199.15	1.00	199.15	1.39	0.89	0.89
58.48	688.02	200.60	1.00	200.60	1.40	0.89	0.89
58.53	694.39	202.36	1.00	202.36	1.41	0.89	0.89
58.56	696.37	202.90	1.00	202.90	1.46	0.89	0.89
58.58	704.43	205.20	1.00	205.20	1.47	0.89	0.89
58.59	710.90	207.06	1.00	207.06	1.49	0.89	0.89
58.63	707.18	205.90	1.00	205.90	1.49	0.89	0.89
58.63	709.20	206.49	1.00	206.49	1.50	0.89	0.89
58.63	695.36	202.42	1.00	202.42	1.51	0.89	0.89
58.68	700.19	203.74	1.00	203.74	1.49	0.89	0.89
58.69	701.88	204.22	1.00	204.22	1.45	0.89	0.89
58.72	717.85	208.81	1.00	208.81	1.40	0.90	0.90
58.73	722.94	210.28	1.00	210.28	1.38	0.90	0.90
58.74	728.64	211.92	1.00	211.92	1.41	0.90	0.90
58.77	726.96	211.36	1.00	211.36	1.44	0.90	0.90
58.81	722.67	210.02	1.00	210.02	1.47	0.90	0.90
58.82	713.94	207.44	1.00	207.44	1.49	0.89	0.89
58.83	715.80	207.97	1.00	207.97	1.51	0.90	0.90
58.87	722.33	209.78	1.00	209.78	1.52	0.90	0.90
58.91	731.67	212.41	1.00	212.41	1.53	0.90	0.90
58.92	737.87	214.21	1.00	214.21	1.54	0.90	0.90
58.93	740.53	214.95	1.00	214.95	1.53	0.90	0.90
58.96	739.05	214.44	1.00	214.44	1.53	0.90	0.90
59.01	716.31	207.70	1.00	207.70	1.56	0.89	0.89
59.06	687.29	199.13	1.00	199.13	1.59	0.89	0.89
59.08	655.28	189.77	1.00	189.77	1.63	0.88	0.88
59.11	638.94	184.95	1.00	184.95	1.65	0.87	0.87
59.15	627.21	181.46	1.00	181.46	1.68	0.87	0.87
59.21	618.28	178.75	1.00	178.75	1.70	0.86	0.86
59.26	606.09	175.11	1.02	178.89	1.72	0.86	0.86
59.30	592.31	171.02	1.01	173.20	1.71	0.86	0.86

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
59.35	579.87	167.32	1.01	169.07	1.71	0.85	0.85
59.40	562.76	162.26	1.04	168.73	1.73	0.85	0.85
59.42	550.96	158.81	1.06	168.34	1.74	0.85	0.85
59.47	539.34	155.35	1.08	167.78	1.75	0.85	0.85
59.51	539.41	155.29	1.09	168.63	1.75	0.85	0.85
59.56	537.97	154.79	1.09	168.59	1.75	0.85	0.85
59.61	537.36	154.53	1.06	164.50	1.74	0.85	0.85
59.67	541.98	155.77	1.00	155.77	1.70	0.83	0.83
59.71	553.73	159.11	1.00	159.11	1.65	0.84	0.84
59.80	555.82	159.56	1.00	159.56	1.61	0.84	0.84
59.85	552.45	158.50	1.00	158.50	1.59	0.84	0.84
59.90	542.21	155.47	1.00	155.47	1.59	0.83	0.83
60.00	542.99	155.53	1.00	155.53	1.59	0.83	0.83
60.04	541.71	155.09	1.00	155.09	1.60	0.83	0.83
60.10	526.52	150.62	1.00	150.62	1.63	0.83	0.83
60.15	508.32	145.30	1.00	145.30	1.67	0.82	0.82
60.19	487.40	139.22	1.00	139.22	1.70	0.81	0.81
60.23	483.49	138.03	1.00	138.03	1.69	0.81	0.81
60.28	482.61	137.71	1.00	137.71	1.68	0.81	0.81
60.33	488.98	139.47	1.00	139.47	1.67	0.81	0.81
60.38	491.97	140.26	1.00	140.26	1.67	0.81	0.81
60.42	493.85	140.74	1.00	140.74	1.69	0.81	0.81
60.44	487.18	138.79	1.01	140.24	1.71	0.81	0.81
60.47	475.94	135.53	1.08	145.72	1.74	0.82	0.82
60.52	465.53	132.47	1.12	148.94	1.78	0.83	0.83
60.56	462.70	131.60	1.15	150.90	1.79	0.83	0.83
60.57	465.03	132.25	1.15	151.48	1.79	0.83	0.83
60.61	470.62	133.80	1.13	151.48	1.78	0.83	0.83
60.66	477.29	135.64	1.12	151.98	1.77	0.83	0.83
60.71	486.66	138.25	1.11	153.21	1.77	0.83	0.83
60.76	495.25	140.63	1.11	156.59	1.77	0.84	0.84
60.81	504.76	143.27	1.11	159.58	1.77	0.84	0.84
60.86	523.05	148.43	1.08	161.02	1.75	0.84	0.84
60.91	559.78	158.84	1.00	158.84	1.70	0.84	0.84
60.95	601.50	170.69	1.00	170.69	1.66	0.85	0.85
61.00	637.66	180.91	1.00	180.91	1.64	0.87	0.87
61.02	657.74	186.60	1.00	186.60	1.64	0.87	0.87
61.05	685.10	194.34	1.00	194.34	1.62	0.88	0.88
61.08	710.24	201.44	1.00	201.44	1.61	0.89	0.89
61.09	731.84	207.57	1.00	207.57	1.59	0.89	0.89
61.13	737.94	209.24	1.00	209.24	1.59	0.90	0.90
61.14	739.46	209.63	1.00	209.63	1.60	0.90	0.90
61.16	741.44	210.15	1.00	210.15	1.60	0.90	0.90
61.20	750.88	212.77	1.00	212.77	1.58	0.90	0.90
61.23	762.13	215.88	1.00	215.88	1.56	0.90	0.90
61.24	766.92	217.23	1.00	217.23	1.52	0.90	0.90
61.29	758.86	214.83	1.00	214.83	1.51	0.90	0.90
61.30	744.24	210.65	1.00	210.65	1.52	0.90	0.90

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
61.33	734.57	207.82	1.00	207.82	1.55	0.90	0.90
61.38	730.90	206.66	1.00	206.66	1.55	0.89	0.89
61.43	731.07	206.60	1.00	206.60	1.53	0.89	0.89
61.48	738.25	208.54	1.00	208.54	1.50	0.90	0.90
61.53	750.91	212.02	1.00	212.02	1.48	0.90	0.90
61.56	754.78	213.05	1.00	213.05	1.48	0.90	0.90
61.58	726.93	205.10	1.00	205.10	1.50	0.89	0.89
61.59	702.39	198.13	1.00	198.13	1.52	0.88	0.88
61.62	600.70	169.24	1.00	169.24	1.61	0.85	0.85
61.63	595.30	167.67	1.00	167.67	1.61	0.85	0.85
61.67	588.36	165.65	1.00	165.65	1.62	0.85	0.85
61.71	662.66	186.61	1.00	186.61	1.55	0.87	0.87
61.76	655.52	184.50	1.00	184.50	1.55	0.87	0.87
61.81	634.02	178.32	1.00	178.32	1.54	0.86	0.86
61.86	615.02	172.85	1.00	172.85	1.52	0.86	0.86
61.87	600.83	168.83	1.00	168.83	1.48	0.85	0.85
61.91	588.87	165.39	1.00	165.39	1.44	0.85	0.85
61.95	578.02	162.25	1.00	162.25	1.42	0.84	0.84
61.96	566.74	159.04	1.00	159.04	1.42	0.84	0.84
62.00	553.70	155.30	1.00	155.30	1.45	0.83	0.83
62.04	535.16	150.01	1.00	150.01	1.49	0.83	0.83
62.06	510.97	143.15	1.00	143.15	1.55	0.82	0.82
62.10	491.66	137.65	1.00	137.65	1.60	0.81	0.81
62.14	475.52	133.04	1.00	133.04	1.64	0.80	0.80
62.20	463.08	129.46	1.00	129.46	1.66	0.80	0.80
62.22	439.20	122.70	1.00	122.70	1.71	0.79	0.79
62.27	415.48	115.96	1.08	125.13	1.75	0.79	0.79
62.29	396.37	110.55	1.13	125.44	1.78	0.79	0.79
62.34	380.26	105.96	1.17	124.22	1.82	0.79	0.79
62.39	366.62	102.08	1.21	123.46	1.86	0.79	0.79
62.43	347.78	96.73	1.26	121.51	1.93	0.79	0.79
62.49	340.13	94.52	1.28	121.38	1.97	0.79	0.79
62.57	336.43	93.40	1.30	121.70	1.99	0.79	0.79
62.68	357.18	99.12	1.29	127.79	1.98	0.80	0.80
62.75	398.26	110.56	1.26	139.12	1.93	0.81	0.81
62.87	426.23	118.25	1.24	146.86	1.91	0.82	0.82
62.88	409.21	113.48	1.25	142.25	1.93	0.82	0.82
62.89	424.34	117.70	1.21	142.29	1.86	0.82	0.82
62.93	485.42	134.75	1.06	142.80	1.74	0.82	0.82
62.98	571.92	158.87	1.00	158.87	1.61	0.84	0.84
63.02	620.24	172.30	1.00	172.30	1.47	0.86	0.86
63.07	658.55	182.93	1.00	182.93	1.31	0.87	0.87
63.12	710.78	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.14	752.36	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.17	781.30	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.17	799.36	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.20	825.98	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.21	830.83	-1.00	1.00	-1.00	-1.00	0.00	0.00

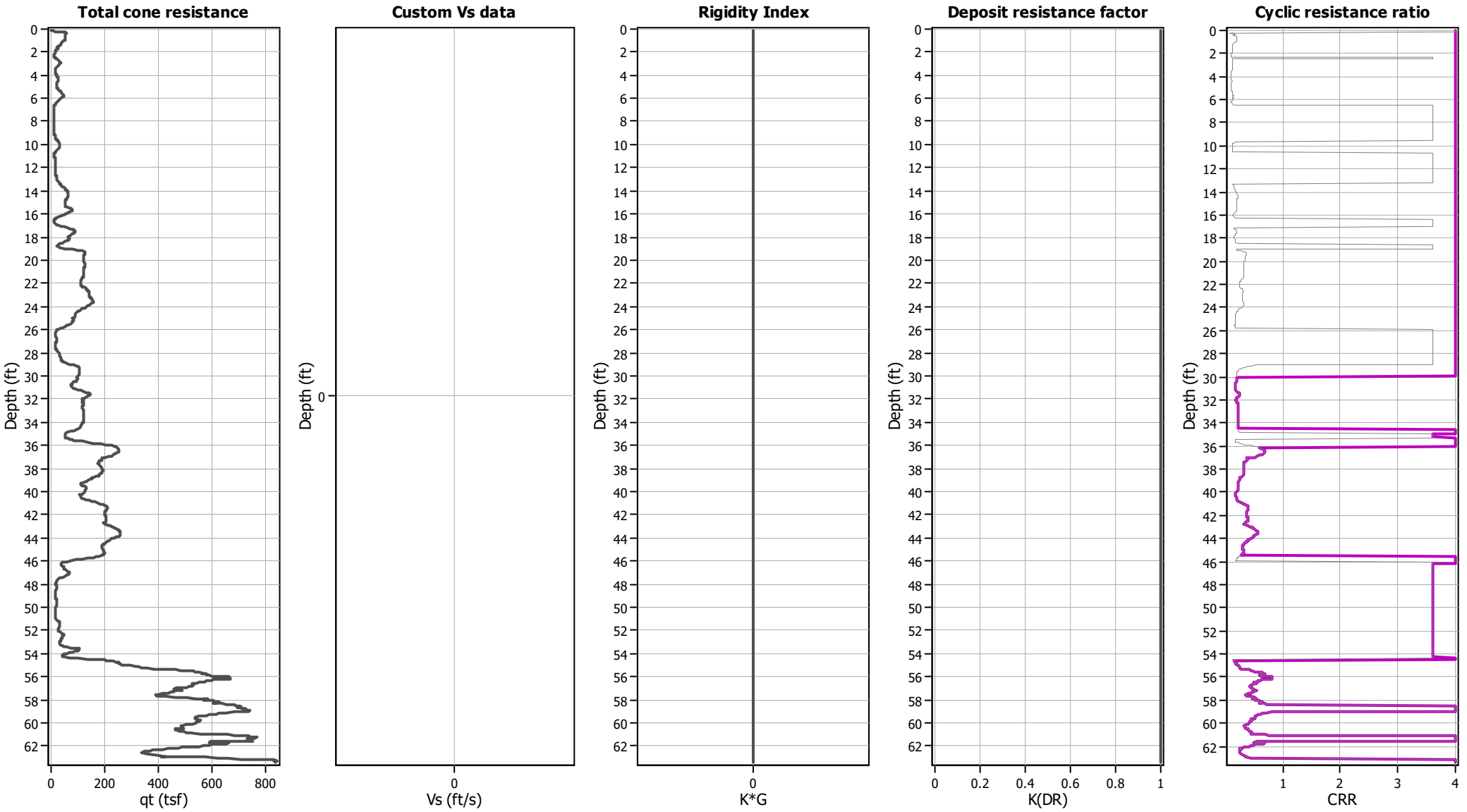
:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
63.23	842.91	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.26	834.75	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.28	841.52	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.31	838.10	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.32	839.38	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.36	837.12	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.40	836.85	-1.00	1.00	-1.00	-1.00	0.00	0.00

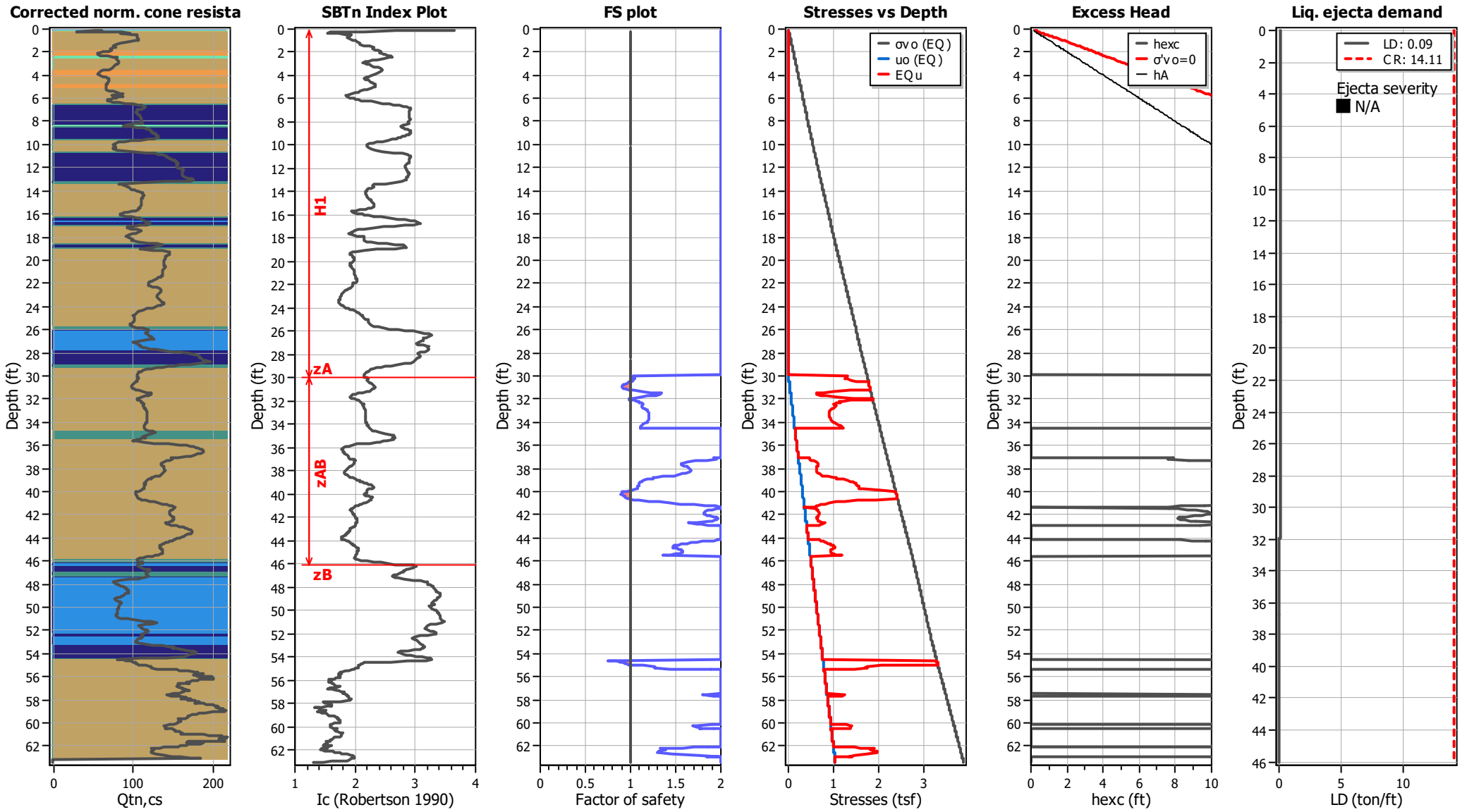
Abbreviations

q_t: Total cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Adjusted and corrected cone resistance due to fines
I_c: Soil behavior type index
$S_{u(liq)}/\sigma'_v$: Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$: Calculated peak undrained strength ratio

Aging Calculation Estimation



Ejecta Severity Estimation



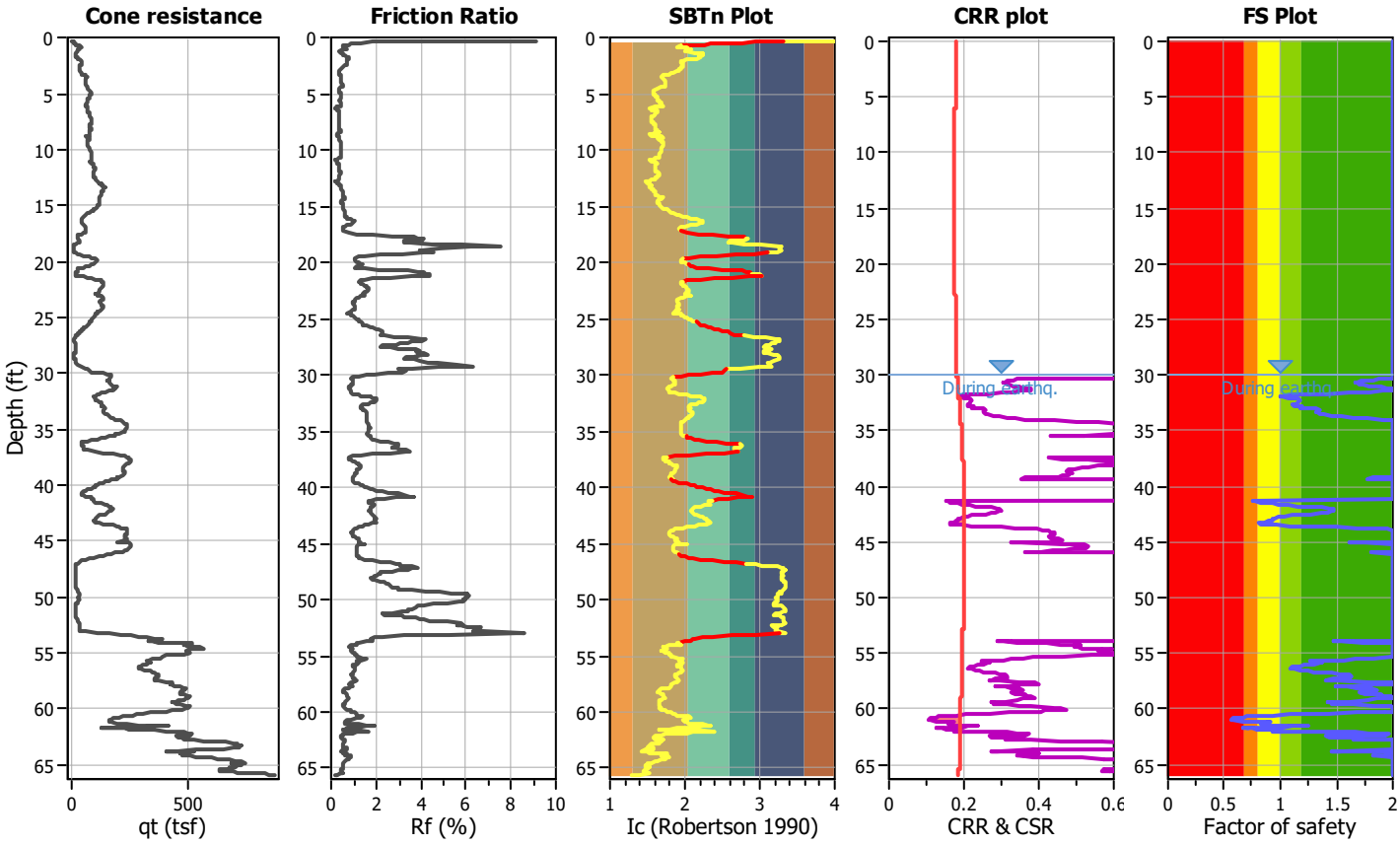
LIQUEFACTION ANALYSIS REPORT

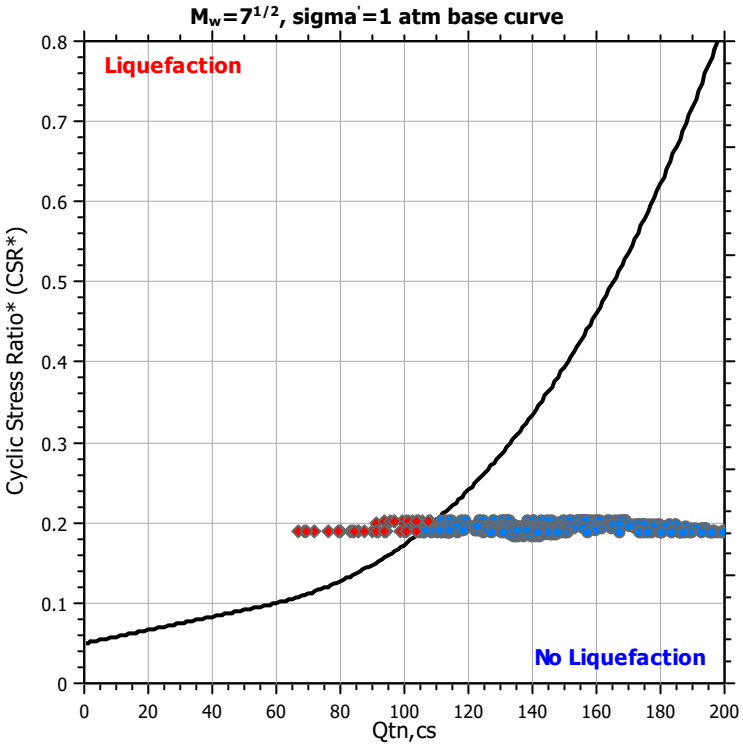
Project title : W1857-88-01 **Location : 331 The City Drive S**

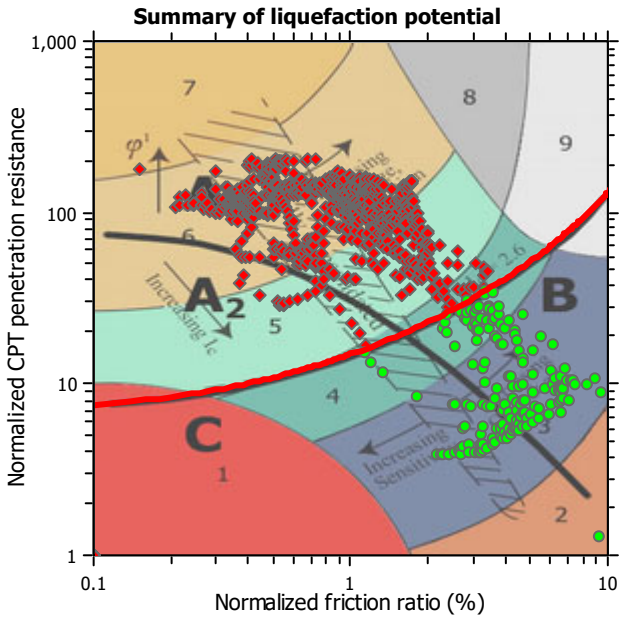
CPT file : CPT-2

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	54.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	30.00 ft	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.12	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.42	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

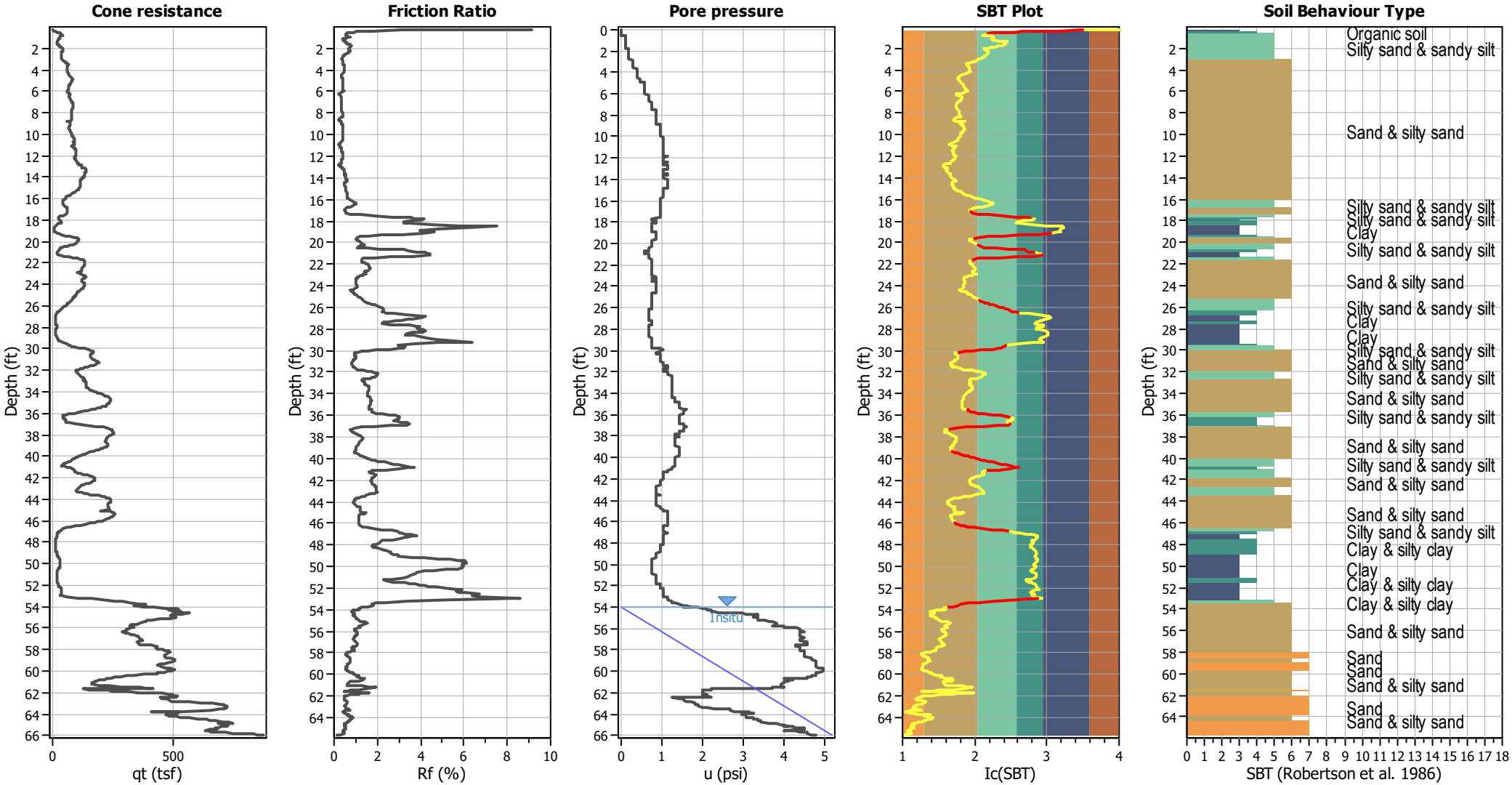






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



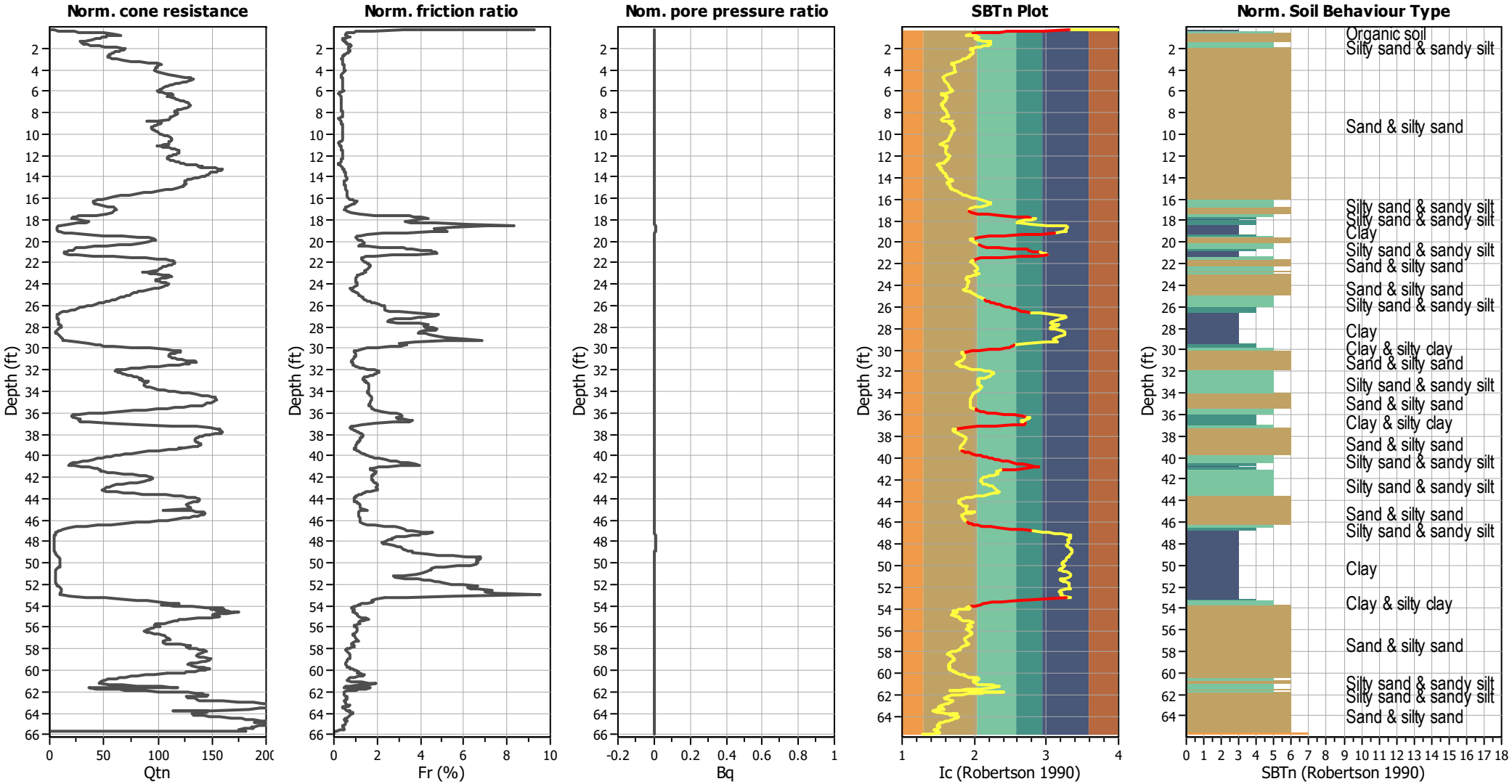
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



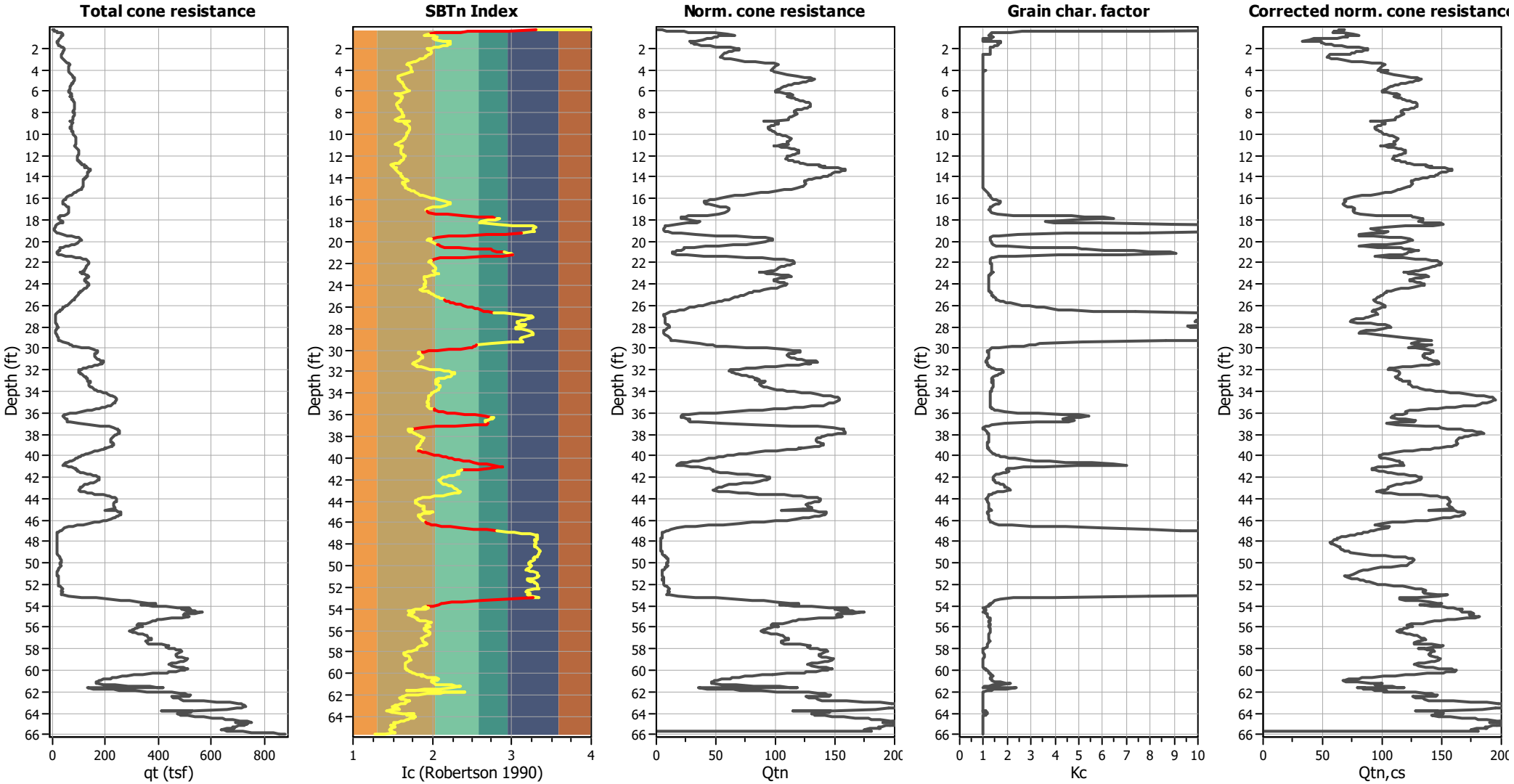
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

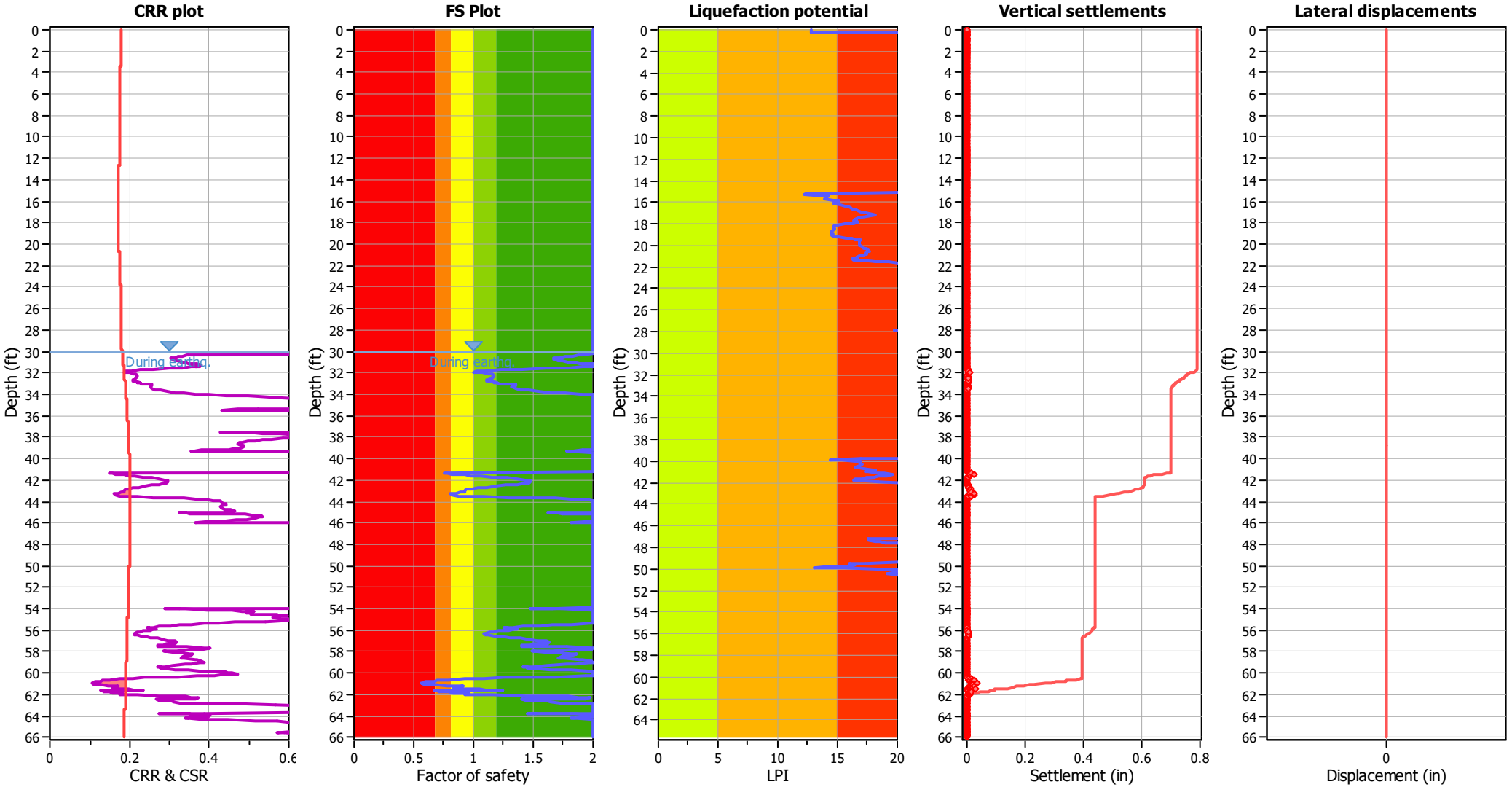
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

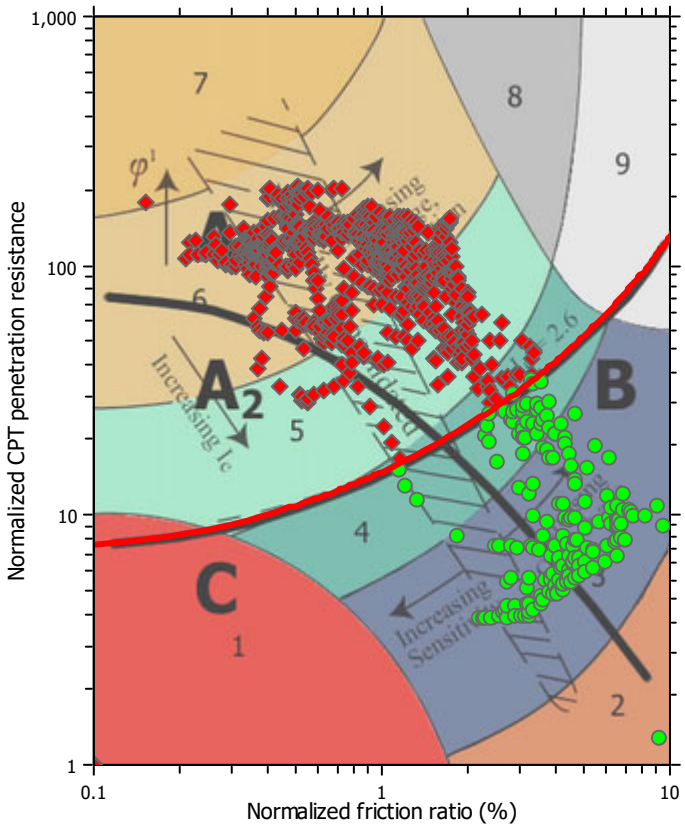
F.S. color scheme

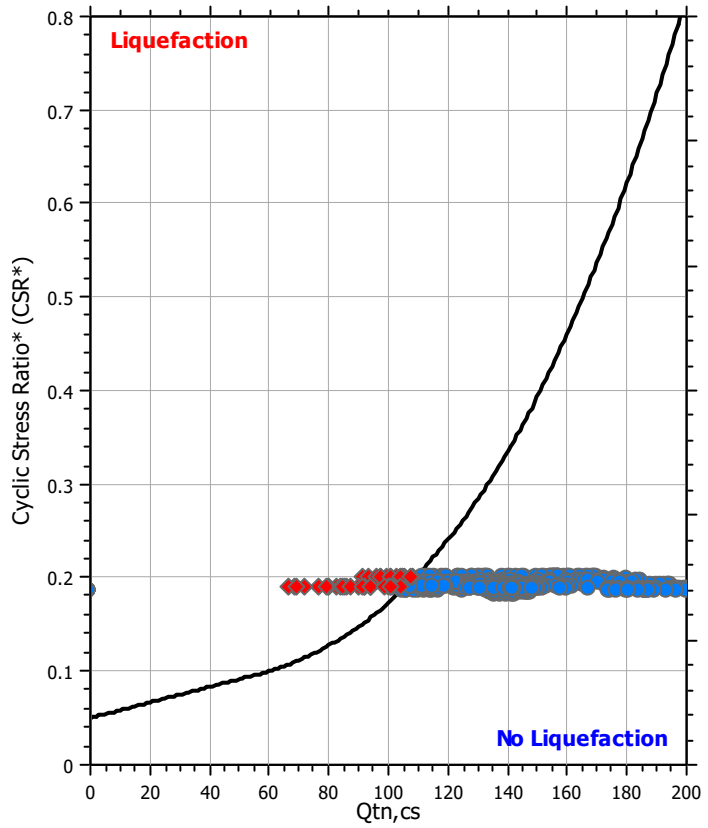
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

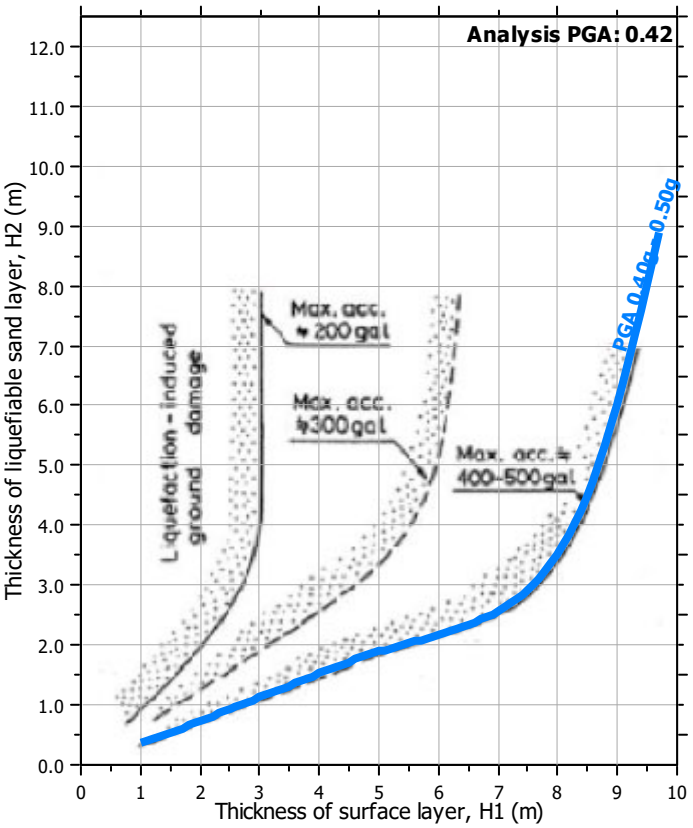
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



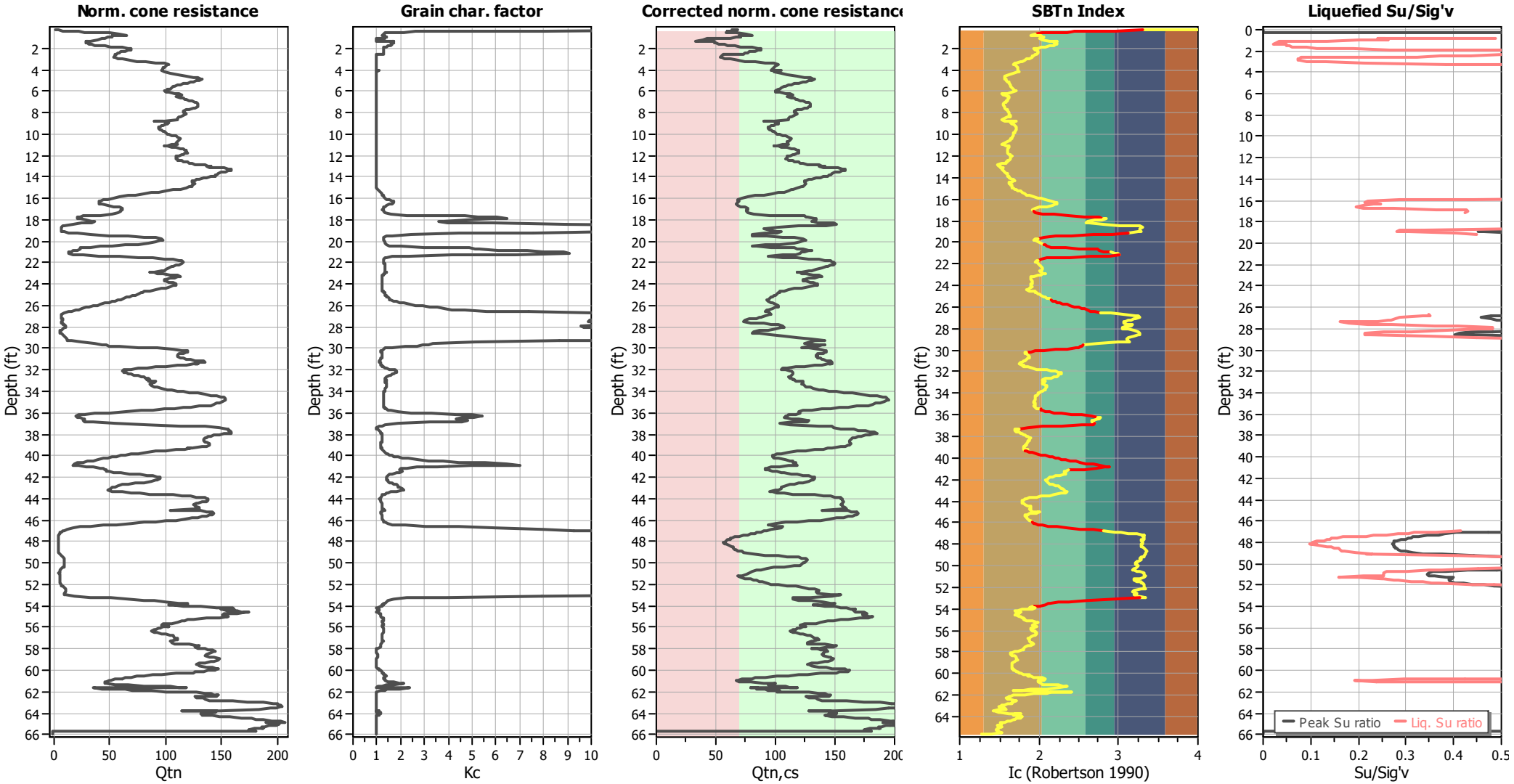




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

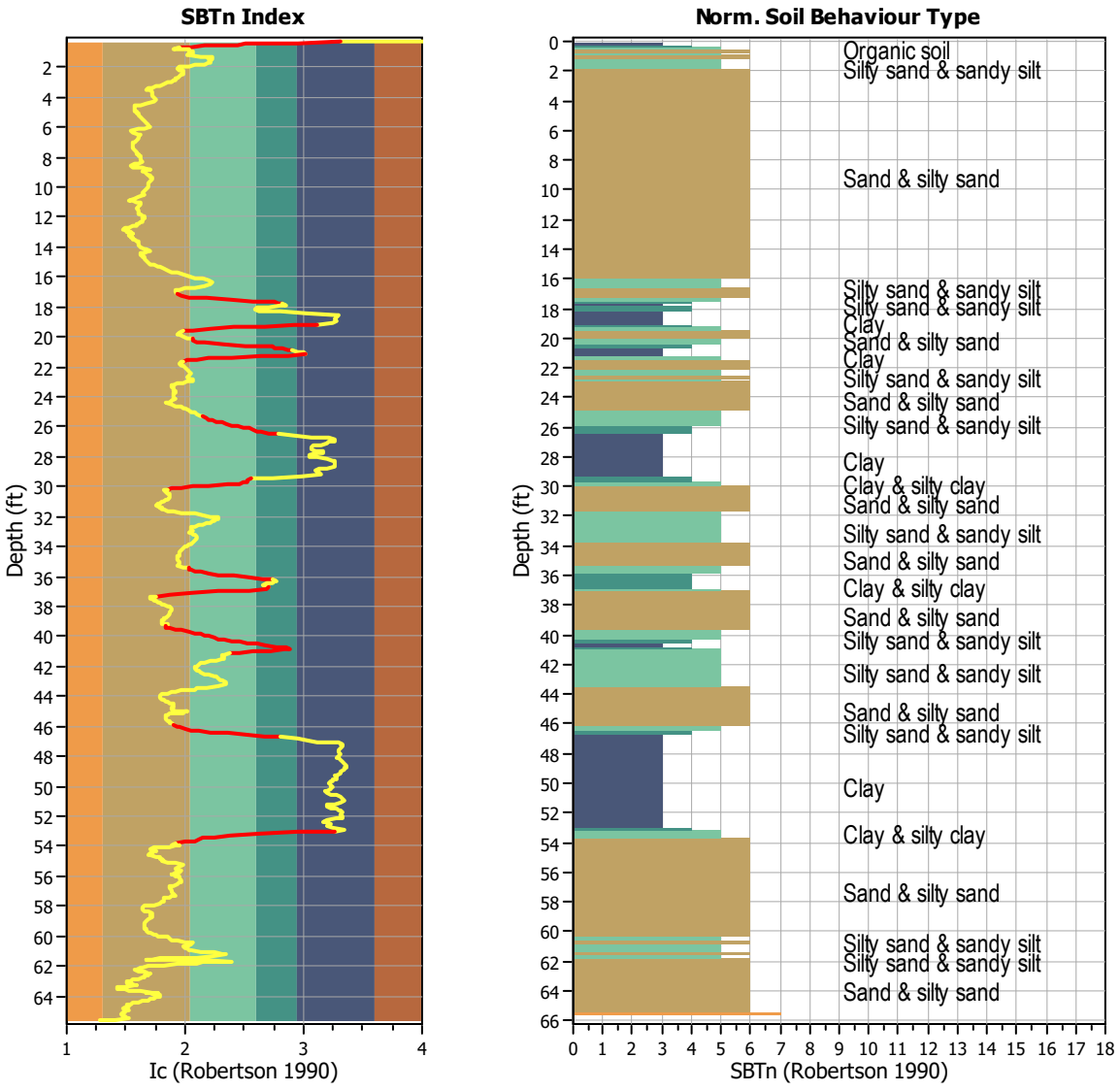
Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	1012
I_c maximum check value:	3.00	Total points excluded:	145
I_c change ratio value:	0.0250	Exclusion percentage:	14.33%
Minimum number of points in layer:	4	Number of layers detected:	13

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	13	Start depth: 0.36 (ft)	3	Clay
		End depth: 0.76 (ft)	6	Sand & silty sand
Transition layer 2	10	Start depth: 17.22 (ft)	6	Sand & silty sand
		End depth: 17.85 (ft)	3	Clay
Transition layer 3	7	Start depth: 19.22 (ft)	3	Clay
		End depth: 19.69 (ft)	6	Sand & silty sand
Transition layer 4	13	Start depth: 20.26 (ft)	5	Silty sand & sandy silt
		End depth: 20.96 (ft)	3	Clay
Transition layer 5	8	Start depth: 21.25 (ft)	3	Clay
		End depth: 21.69 (ft)	6	Sand & silty sand
Transition layer 6	16	Start depth: 25.41 (ft)	5	Silty sand & sandy silt
		End depth: 26.61 (ft)	3	Clay
Transition layer 7	12	Start depth: 29.63 (ft)	4	Clay & silty clay
		End depth: 30.24 (ft)	6	Sand & silty sand
Transition layer 8	11	Start depth: 35.51 (ft)	5	Silty sand & sandy silt
		End depth: 36.28 (ft)	4	Clay & silty clay
Transition layer 9	7	Start depth: 36.86 (ft)	4	Clay & silty clay
		End depth: 37.39 (ft)	6	Sand & silty sand
Transition layer 10	20	Start depth: 39.39 (ft)	6	Sand & silty sand
		End depth: 40.84 (ft)	3	Clay
Transition layer 11	7	Start depth: 40.84 (ft)	3	Clay
		End depth: 41.22 (ft)	5	Silty sand & sandy silt
Transition layer 12	11	Start depth: 46.02 (ft)	6	Sand & silty sand
		End depth: 46.84 (ft)	3	Clay
Transition layer 13	10	Start depth: 53.10 (ft)	3	Clay
		End depth: 53.92 (ft)	6	Sand & silty sand

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.01	0.00	0.00	0.00	N/A	120.90
2	0.04	-0.10	0.01	0.00	N/A	120.90
3	0.08	0.00	0.01	0.00	N/A	120.90
4	0.10	-0.10	0.01	0.00	N/A	120.90
5	0.13	0.00	0.02	0.00	N/A	120.90
6	0.18	0.00	0.03	0.00	N/A	120.90
7	0.22	0.00	0.05	0.00	N/A	120.90
8	0.27	0.00	0.08	0.00	100.00	90.68
9	0.33	2.43	0.09	0.00	81.96	94.98
10	0.36	5.87	0.09	0.00	55.30	96.98
11	0.37	7.19	0.09	0.00	43.87	97.82
12	0.38	8.30	0.10	0.00	39.79	98.46
13	0.42	9.11	0.11	0.00	36.64	99.41
14	0.44	10.73	0.12	0.00	34.37	100.58
15	0.47	11.94	0.14	0.00	31.37	101.55
16	0.47	13.87	0.14	0.00	28.15	102.58
17	0.52	16.90	0.16	0.00	24.51	103.55
18	0.56	20.24	0.17	0.00	21.06	104.60
19	0.58	24.29	0.18	0.00	17.61	105.59
20	0.61	30.26	0.19	0.10	14.26	106.54
21	0.66	37.55	0.20	0.10	11.58	107.34
22	0.76	43.02	0.21	0.10	10.25	107.74
23	0.80	41.80	0.21	0.10	11.05	107.65
24	0.81	31.17	0.21	0.10	12.33	107.41
25	0.85	33.50	0.20	0.10	13.76	107.15
26	0.86	32.59	0.20	0.10	13.66	107.29
27	0.90	32.29	0.22	0.10	14.33	107.68
28	0.95	31.78	0.24	0.10	14.92	108.07
29	1.00	31.38	0.24	0.10	14.72	106.94
30	1.05	28.44	0.12	0.10	14.03	104.83
31	1.14	26.82	0.10	0.10	5.00	101.56
32	1.24	24.39	0.08	0.10	5.00	100.45
33	1.31	21.66	0.09	0.10	5.00	100.02
34	1.36	15.49	0.10	0.10	19.77	100.07
35	1.37	16.65	0.10	0.10	20.16	100.28
36	1.39	21.17	0.10	0.10	19.32	100.40
37	1.43	17.81	0.10	0.10	18.80	100.44
38	1.44	18.12	0.10	0.10	19.86	100.33
39	1.49	18.22	0.10	0.10	19.73	100.60
40	1.53	18.72	0.11	0.10	19.64	101.22
41	1.58	19.74	0.12	0.10	19.61	102.17
42	1.63	20.55	0.14	0.10	19.60	103.26
43	1.68	21.56	0.16	0.10	19.49	104.34
44	1.72	22.98	0.18	0.10	18.93	105.39
45	1.77	25.40	0.20	0.10	17.98	106.40
46	1.82	28.04	0.22	0.19	16.68	107.38
47	1.86	31.48	0.24	0.19	15.32	108.26
48	1.92	35.02	0.26	0.19	13.84	108.95

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	1.97	38.77	0.26	0.19	12.52	109.50
50	2.01	42.21	0.27	0.19	11.75	110.13
51	2.09	43.83	0.31	0.19	11.40	110.51
52	2.16	43.62	0.30	0.19	11.59	110.65
53	2.20	41.70	0.29	0.19	12.00	110.35
54	2.25	39.07	0.28	0.19	12.39	109.98
55	2.31	38.77	0.27	0.19	12.55	109.49
56	2.37	37.96	0.25	0.19	12.51	108.98
57	2.40	36.64	0.24	0.19	12.56	108.51
58	2.46	36.03	0.23	0.19	12.53	107.92
59	2.54	35.22	0.20	0.19	12.28	107.21
60	2.59	34.82	0.18	0.19	5.00	106.07
61	2.69	34.01	0.14	0.19	5.00	105.12
62	2.74	33.91	0.14	0.19	5.00	104.27
63	2.83	33.91	0.13	0.29	5.00	104.04
64	2.88	33.81	0.13	0.29	5.00	103.96
65	2.98	35.32	0.13	0.29	5.00	104.13
66	3.03	37.96	0.13	0.29	5.00	104.69
67	3.12	42.41	0.15	0.29	5.00	105.94
68	3.21	46.56	0.19	0.29	5.00	107.29
69	3.27	51.52	0.21	0.29	5.00	108.51
70	3.34	56.88	0.23	0.29	5.00	109.32
71	3.41	62.75	0.24	0.29	5.00	110.12
72	3.51	66.09	0.27	0.29	5.00	110.66
73	3.55	63.76	0.28	0.29	5.00	111.08
74	3.65	61.03	0.29	0.38	5.00	111.24
75	3.75	62.45	0.30	0.38	5.00	111.31
76	3.83	61.64	0.29	0.38	5.00	111.22
77	3.94	60.22	0.28	0.38	5.00	111.12
78	4.04	61.44	0.28	0.38	5.00	111.07
79	4.13	59.21	0.29	0.38	7.02	111.59
80	4.24	61.23	0.34	0.38	5.00	111.65
81	4.38	64.57	0.29	0.38	5.00	110.97
82	4.50	69.64	0.19	0.38	4.69	110.20
83	4.62	72.57	0.25	0.48	3.95	110.29
84	4.71	80.16	0.28	0.48	3.93	111.40
85	4.75	80.92	0.29	0.48	3.90	112.19
86	4.84	81.68	0.33	0.48	3.97	112.65
87	4.89	83.70	0.33	0.57	4.02	112.99
88	4.94	83.40	0.33	0.57	4.04	113.02
89	4.98	81.68	0.33	0.57	4.17	112.97
90	5.07	80.06	0.33	0.57	4.33	112.85
91	5.13	78.54	0.33	0.57	4.49	112.71
92	5.17	76.82	0.32	0.57	4.57	112.40
93	5.27	75.00	0.30	0.57	4.72	112.10
94	5.32	72.47	0.30	0.57	4.84	111.72
95	5.42	70.75	0.28	0.57	4.99	111.41
96	5.46	69.33	0.27	0.57	5.00	111.08

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	5.56	67.91	0.26	0.57	5.00	110.88
98	5.61	66.80	0.26	0.57	5.00	110.75
99	5.71	65.89	0.26	0.57	5.00	110.68
100	5.78	64.88	0.26	0.57	5.00	110.63
101	5.85	63.97	0.26	0.57	5.00	110.57
102	5.95	62.65	0.26	0.57	5.00	110.53
103	6.00	61.84	0.26	0.57	5.00	110.86
104	6.09	62.45	0.30	0.67	5.00	109.42
105	6.14	64.47	0.11	0.67	4.43	108.06
106	6.24	67.31	0.14	0.67	3.33	106.15
107	6.30	70.75	0.17	0.67	3.46	107.71
108	6.38	73.18	0.20	0.67	3.76	108.87
109	6.46	70.24	0.23	0.67	4.34	109.63
110	6.50	65.28	0.24	0.67	4.73	110.08
111	6.56	69.74	0.25	0.67	4.82	110.41
112	6.63	71.46	0.26	0.67	4.59	110.75
113	6.68	72.67	0.26	0.67	4.51	110.97
114	6.76	73.38	0.27	0.76	4.44	111.12
115	6.82	74.39	0.27	0.76	4.37	111.23
116	6.88	75.81	0.27	0.76	4.21	111.32
117	6.96	78.34	0.27	0.76	3.98	111.40
118	7.03	80.97	0.27	0.76	3.77	111.49
119	7.11	82.29	0.27	0.76	3.64	111.55
120	7.16	82.89	0.27	0.76	3.60	111.70
121	7.26	83.91	0.29	0.76	3.62	111.86
122	7.31	84.62	0.29	0.76	3.65	112.04
123	7.40	84.72	0.29	0.76	3.70	112.13
124	7.45	84.51	0.30	0.76	3.76	112.18
125	7.54	84.31	0.30	0.86	3.86	112.16
126	7.60	83.00	0.30	0.86	3.98	112.07
127	7.68	81.17	0.29	0.86	4.16	111.94
128	7.74	79.45	0.29	0.86	4.33	111.82
129	7.83	78.44	0.29	0.86	4.51	111.77
130	7.90	77.73	0.29	0.86	4.60	111.85
131	7.98	78.85	0.30	0.86	4.65	112.09
132	8.05	80.67	0.31	0.86	4.62	112.42
133	8.12	82.29	0.32	0.86	4.65	112.70
134	8.19	82.08	0.33	0.86	4.77	112.88
135	8.27	80.57	0.34	0.86	5.03	113.00
136	8.36	78.74	0.34	0.86	5.00	112.80
137	8.41	78.04	0.31	0.86	4.51	111.23
138	8.50	78.24	0.15	0.86	3.85	109.61
139	8.60	78.95	0.18	0.86	3.40	108.40
140	8.70	79.15	0.21	0.86	3.76	109.30
141	8.74	78.14	0.22	0.86	4.96	109.52
142	8.78	55.57	0.22	0.86	5.00	109.55
143	8.81	62.96	0.23	0.96	5.00	109.69
144	8.86	72.17	0.24	0.96	5.00	110.13

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	8.91	74.09	0.25	0.96	5.00	110.49
146	8.94	75.00	0.25	0.96	5.00	110.79
147	9.02	73.89	0.27	0.96	5.00	111.08
148	9.10	72.47	0.28	0.96	5.00	111.34
149	9.17	71.15	0.28	0.96	5.00	111.44
150	9.22	69.84	0.28	0.96	5.00	111.44
151	9.31	68.83	0.28	0.96	5.00	111.41
152	9.37	68.32	0.28	0.96	5.00	111.39
153	9.42	68.32	0.28	0.96	5.00	111.39
154	9.52	69.13	0.28	0.96	5.00	111.41
155	9.60	70.04	0.28	0.96	5.00	111.49
156	9.66	71.36	0.29	0.96	5.00	111.61
157	9.74	73.18	0.29	0.96	5.00	111.74
158	9.81	74.80	0.29	0.96	5.00	111.88
159	9.89	75.71	0.30	0.96	5.00	112.10
160	9.98	76.82	0.32	0.96	5.00	112.42
161	10.03	78.54	0.33	1.05	5.00	112.78
162	10.13	80.97	0.34	1.05	5.00	113.14
163	10.23	84.21	0.35	1.05	5.00	113.45
164	10.32	86.94	0.36	1.05	5.00	113.68
165	10.38	88.16	0.36	1.05	5.00	113.80
166	10.47	89.17	0.37	1.05	5.00	113.83
167	10.57	88.66	0.36	1.05	5.00	113.81
168	10.66	87.45	0.36	1.05	4.50	112.22
169	10.76	87.65	0.16	1.05	3.90	110.65
170	10.85	87.85	0.19	1.05	3.30	108.99
171	10.92	88.46	0.22	1.05	3.57	109.92
172	11.00	89.27	0.23	1.05	4.11	110.26
173	11.07	77.73	0.23	1.05	4.54	110.35
174	11.10	79.45	0.23	1.05	4.87	110.48
175	11.15	83.40	0.25	1.05	4.71	110.88
176	11.19	85.53	0.26	1.05	4.61	111.40
177	11.24	87.25	0.28	1.05	4.59	111.90
178	11.29	89.47	0.30	1.05	4.51	112.30
179	11.34	92.21	0.31	1.05	4.40	112.73
180	11.40	95.14	0.33	1.05	4.33	113.17
181	11.47	97.27	0.35	1.05	4.32	113.59
182	11.53	97.98	0.36	1.05	4.38	113.88
183	11.58	97.87	0.36	1.05	4.42	114.06
184	11.65	98.78	0.37	1.05	4.46	114.22
185	11.72	99.39	0.38	1.05	4.50	114.36
186	11.77	99.29	0.38	1.05	4.57	114.43
187	11.82	98.28	0.38	1.05	4.67	114.45
188	11.88	97.47	0.38	1.15	5.03	114.87
189	11.97	95.95	0.45	1.05	5.00	114.84
190	12.02	94.84	0.38	1.05	5.00	114.75
191	12.06	93.42	0.38	1.05	5.00	114.18
192	12.11	92.31	0.37	1.05	5.00	114.03

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.21	93.32	0.36	1.05	5.00	113.85
194	12.25	92.21	0.35	1.05	5.00	113.70
195	12.30	93.22	0.35	1.05	5.01	113.58
196	12.31	93.52	0.35	1.05	4.95	113.56
197	12.32	93.52	0.35	1.05	4.93	113.57
198	12.35	93.83	0.35	1.05	4.77	113.38
199	12.40	95.24	0.32	1.05	4.60	113.25
200	12.45	96.66	0.32	1.15	4.38	113.11
201	12.52	98.38	0.32	1.05	4.29	113.28
202	12.56	100.20	0.33	1.05	4.25	113.61
203	12.62	102.33	0.36	1.05	4.25	113.99
204	12.65	103.54	0.37	1.05	3.77	113.26
205	12.71	105.16	0.23	1.15	3.23	112.19
206	12.76	106.68	0.23	1.15	2.62	110.90
207	12.83	110.12	0.23	1.15	2.60	111.55
208	12.88	114.17	0.28	1.15	2.77	112.94
209	12.93	118.52	0.37	1.15	2.90	114.26
210	12.98	124.09	0.40	1.15	3.08	115.17
211	13.03	121.66	0.41	1.15	3.06	115.51
212	13.04	125.50	0.42	1.15	3.47	115.78
213	13.07	113.26	0.46	1.05	3.50	116.29
214	13.13	129.35	0.50	1.05	3.58	116.95
215	13.17	134.31	0.54	1.05	3.26	117.70
216	13.22	139.37	0.58	1.05	3.29	118.28
217	13.27	139.88	0.62	1.05	3.36	118.74
218	13.32	141.09	0.64	1.05	3.46	119.07
219	13.37	142.31	0.66	1.05	3.56	119.26
220	13.41	140.38	0.67	1.05	3.64	119.30
221	13.46	139.27	0.66	1.05	3.75	119.26
222	13.51	137.45	0.66	1.15	3.85	119.23
223	13.56	136.13	0.66	1.15	4.04	119.31
224	13.60	134.31	0.69	1.05	4.26	119.44
225	13.66	132.39	0.70	1.05	4.38	119.40
226	13.75	131.68	0.66	1.05	4.42	119.28
227	13.80	131.27	0.66	1.05	4.39	119.11
228	13.89	130.57	0.66	1.05	4.46	119.13
229	13.94	130.36	0.67	1.05	4.60	119.22
230	13.99	128.44	0.69	1.15	4.88	119.41
231	14.09	125.71	0.72	1.15	5.27	119.59
232	14.14	121.96	0.73	1.15	5.70	119.79
233	14.23	119.13	0.76	1.15	6.08	119.87
234	14.28	117.00	0.76	1.15	5.80	119.04
235	14.38	115.38	0.51	1.15	5.31	118.06
236	14.42	116.85	0.51	1.15	4.82	116.96
237	14.52	113.76	0.52	1.15	4.88	117.10
238	14.57	116.70	0.53	1.15	4.95	117.39
239	14.67	119.74	0.57	1.15	5.03	117.62
240	14.68	116.09	0.57	1.15	5.00	117.81

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	14.70	117.61	0.58	1.15	5.00	117.84
242	14.75	115.48	0.58	1.15	5.31	117.93
243	14.80	116.60	0.59	1.15	5.43	118.05
244	14.89	116.40	0.61	1.05	5.52	118.17
245	14.94	115.59	0.61	1.05	5.70	118.20
246	15.04	112.25	0.60	1.05	5.96	118.05
247	15.13	107.59	0.59	1.05	6.34	117.77
248	15.21	101.82	0.57	1.05	6.81	117.40
249	15.28	95.75	0.55	1.05	7.34	116.95
250	15.38	89.98	0.52	1.05	7.88	116.40
251	15.47	84.21	0.48	1.05	8.48	115.75
252	15.57	77.33	0.45	1.05	9.19	115.05
253	15.67	71.05	0.42	1.05	10.08	114.27
254	15.77	63.87	0.38	0.96	11.15	113.43
255	15.86	56.78	0.35	0.96	12.43	112.60
256	15.96	51.11	0.33	0.96	13.84	112.03
257	16.05	47.27	0.34	0.96	15.41	111.80
258	16.15	43.52	0.35	0.96	17.50	112.16
259	16.25	39.98	0.42	0.96	19.14	112.43
260	16.31	39.78	0.40	0.96	20.17	112.68
261	16.39	39.78	0.40	0.96	20.08	112.48
262	16.48	39.57	0.38	0.96	19.41	112.23
263	16.59	42.10	0.35	0.96	17.84	112.02
264	16.68	47.47	0.35	0.96	15.50	111.89
265	16.76	54.25	0.33	0.96	13.16	111.73
266	16.86	59.92	0.29	0.96	11.62	111.63
267	16.92	61.94	0.31	0.96	10.95	111.65
268	17.02	61.84	0.32	0.96	10.86	111.63
269	17.11	61.13	0.29	0.96	11.26	111.95
270	17.22	60.42	0.35	0.96	11.88	112.47
271	17.35	59.61	0.39	0.96	14.04	114.30
272	17.45	55.47	0.60	0.96	18.38	116.52
273	17.55	44.33	0.88	0.96	25.48	117.93
274	17.61	30.36	0.95	0.96	33.75	118.25
275	17.64	27.02	0.93	0.76	40.43	117.69
276	17.70	24.80	0.87	0.76	43.23	117.15
277	17.75	22.67	0.84	0.76	45.31	116.73
278	17.80	21.86	0.84	0.76	46.98	116.55
279	17.85	21.56	0.84	0.86	48.89	116.96
280	17.94	21.26	1.00	0.86	45.90	117.91
281	17.99	30.26	1.09	0.86	40.69	119.19
282	18.09	37.65	1.19	0.86	35.41	120.26
283	18.15	41.30	1.27	0.76	34.54	120.72
284	18.23	36.03	1.26	0.76	36.66	120.67
285	18.33	30.87	1.23	0.76	46.11	119.75
286	18.43	14.17	1.16	0.76	59.31	117.89
287	18.52	10.22	0.82	0.76	78.74	114.99
288	18.59	9.41	0.56	0.76	81.21	111.71

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	18.72	8.10	0.35	0.76	78.82	108.87
290	18.81	7.79	0.30	0.76	77.80	106.89
291	18.87	7.69	0.30	0.76	78.37	106.65
292	18.95	7.69	0.32	0.86	79.72	107.66
293	19.05	8.40	0.43	0.86	76.48	109.13
294	19.14	10.73	0.48	0.86	66.73	110.57
295	19.22	14.78	0.48	0.86	53.52	111.65
296	19.29	20.75	0.49	0.86	39.10	113.06
297	19.38	34.31	0.56	0.86	26.85	114.86
298	19.44	55.26	0.63	0.86	19.18	117.03
299	19.53	74.70	0.80	0.86	14.77	118.92
300	19.62	90.89	0.91	0.86	12.57	120.49
301	19.69	102.43	1.00	0.76	11.54	121.67
302	19.79	108.50	1.15	0.76	11.36	122.57
303	19.86	109.41	1.24	0.76	11.84	123.28
304	19.97	106.58	1.33	0.76	12.61	123.60
305	20.07	101.72	1.35	0.76	13.52	123.57
306	20.16	94.94	1.29	0.76	14.68	123.29
307	20.26	85.73	1.27	0.76	14.95	121.49
308	20.34	72.77	0.61	0.67	15.95	119.48
309	20.43	59.51	0.65	0.67	17.67	117.13
310	20.50	47.17	0.70	0.67	23.52	117.36
311	20.60	37.15	0.83	0.67	30.86	117.42
312	20.62	28.74	0.85	0.67	38.22	117.36
313	20.63	25.51	0.86	0.57	41.38	117.35
314	20.68	29.96	0.89	0.57	42.41	117.60
315	20.73	27.73	0.95	0.57	43.48	118.01
316	20.82	25.20	1.01	0.57	47.06	118.03
317	20.87	23.48	0.98	0.57	50.17	117.77
318	20.91	21.66	0.93	0.57	52.49	117.09
319	20.96	19.53	0.83	0.67	55.24	116.20
320	21.05	17.51	0.75	0.67	58.65	115.41
321	21.11	15.69	0.75	0.67	59.61	115.06
322	21.17	17.71	0.75	0.67	59.41	115.10
323	21.25	17.91	0.76	0.67	50.49	115.80
324	21.30	28.04	0.80	0.67	37.44	117.17
325	21.37	47.77	0.89	0.67	25.95	118.97
326	21.45	69.84	1.01	0.76	19.10	120.73
327	21.49	88.87	1.16	0.76	15.54	122.37
328	21.58	104.65	1.36	0.76	13.61	123.67
329	21.64	116.80	1.47	0.76	12.50	124.67
330	21.69	125.61	1.57	0.76	11.91	125.41
331	21.78	131.07	1.71	0.76	11.69	126.01
332	21.83	134.51	1.80	0.76	11.79	126.54
333	21.89	135.73	1.90	0.76	12.04	126.96
334	21.98	136.03	2.02	0.76	12.40	127.34
335	22.03	136.23	2.09	0.76	12.75	127.63
336	22.12	135.42	2.15	0.76	13.09	127.77

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.22	132.99	2.16	0.76	13.41	127.81
338	22.26	131.17	2.15	0.76	13.69	127.73
339	22.36	128.44	2.12	0.76	13.97	127.61
340	22.41	125.51	2.10	0.76	14.35	127.56
341	22.51	123.38	2.14	0.76	14.15	127.06
342	22.60	121.66	1.74	0.76	13.83	126.45
343	22.70	118.93	1.65	0.76	13.30	125.68
344	22.75	117.41	1.61	0.76	13.43	125.41
345	22.84	114.27	1.59	0.76	14.48	125.10
346	22.89	96.25	1.56	0.76	14.75	124.96
347	22.90	110.88	1.55	0.76	15.01	124.78
348	22.94	107.49	1.51	0.76	13.97	124.76
349	23.00	111.94	1.47	0.76	13.47	124.67
350	23.08	117.61	1.47	0.86	12.40	124.71
351	23.13	127.23	1.45	0.86	11.31	124.84
352	23.20	136.23	1.45	0.86	10.47	124.96
353	23.27	138.66	1.46	0.86	10.12	124.97
354	23.33	136.23	1.43	0.76	10.11	124.75
355	23.42	131.78	1.34	0.86	10.24	124.32
356	23.48	126.62	1.25	0.76	10.39	123.80
357	23.57	122.37	1.20	0.86	10.62	123.46
358	23.61	120.44	1.20	0.86	10.81	123.34
359	23.66	120.75	1.21	0.86	10.87	123.44
360	23.73	123.28	1.25	0.86	10.80	123.73
361	23.80	128.04	1.32	0.86	10.61	124.10
362	23.85	132.49	1.37	0.86	10.45	124.49
363	23.94	135.32	1.42	0.86	10.34	124.75
364	24.00	136.54	1.44	0.86	10.35	124.89
365	24.09	135.73	1.44	0.86	10.44	124.90
366	24.16	133.80	1.43	0.86	10.68	124.85
367	24.24	130.46	1.43	0.86	10.08	123.73
368	24.33	125.81	0.86	0.86	9.54	122.48
369	24.43	121.05	0.88	0.86	8.99	121.06
370	24.52	116.40	0.91	0.86	9.98	121.07
371	24.58	105.36	0.92	0.86	10.82	121.05
372	24.59	104.91	0.92	0.86	11.52	121.00
373	24.63	103.24	0.93	0.76	11.65	121.07
374	24.68	104.45	0.95	0.76	11.99	121.27
375	24.77	102.63	1.00	0.76	12.42	121.51
376	24.82	100.30	1.03	0.76	13.12	121.77
377	24.92	97.98	1.08	0.76	13.83	121.94
378	25.01	95.24	1.10	0.76	14.55	122.06
379	25.06	92.41	1.11	0.76	15.23	122.08
380	25.16	89.47	1.12	0.76	15.90	122.02
381	25.25	86.54	1.11	0.76	16.59	121.94
382	25.30	83.50	1.11	0.76	17.28	121.83
383	25.41	80.57	1.11	0.76	18.09	121.73
384	25.49	77.23	1.11	0.76	18.98	121.65

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.55	73.99	1.11	0.76	20.07	121.62
386	25.64	70.65	1.15	0.76	21.32	121.62
387	25.70	67.11	1.16	0.76	22.79	121.64
388	25.79	63.26	1.19	0.76	24.37	121.58
389	25.89	59.31	1.18	0.76	26.26	121.42
390	25.94	54.15	1.17	0.76	28.33	121.11
391	26.02	49.29	1.13	0.76	30.48	120.54
392	26.12	44.64	1.03	0.76	32.30	119.79
393	26.17	41.19	0.94	0.67	34.00	118.80
394	26.28	36.64	0.83	0.67	35.82	117.81
395	26.36	33.20	0.76	0.67	37.65	116.64
396	26.45	30.06	0.64	0.67	40.39	115.51
397	26.50	25.00	0.59	0.67	44.96	114.33
398	26.61	19.74	0.56	0.67	52.70	113.36
399	26.70	15.69	0.53	0.67	63.56	112.54
400	26.77	12.45	0.54	0.67	73.76	111.85
401	26.85	10.73	0.52	0.67	77.64	111.21
402	26.94	12.35	0.44	0.67	78.19	110.57
403	27.04	11.23	0.43	0.67	74.40	110.13
404	27.14	12.25	0.42	0.67	72.81	110.00
405	27.23	13.16	0.41	0.76	69.26	109.81
406	27.28	13.26	0.38	0.76	67.37	109.59
407	27.29	13.21	0.37	0.76	64.60	108.54
408	27.38	13.36	0.25	0.76	63.04	107.81
409	27.48	13.26	0.28	0.76	62.75	107.60
410	27.57	13.16	0.35	0.76	65.67	108.83
411	27.64	13.36	0.41	0.76	68.02	109.83
412	27.65	13.36	0.43	0.67	70.74	111.13
413	27.74	13.56	0.57	0.67	69.81	112.46
414	27.80	16.60	0.65	0.67	65.76	114.19
415	27.90	20.55	0.77	0.67	61.65	115.18
416	27.99	20.34	0.77	0.67	61.92	115.44
417	28.07	17.11	0.72	0.67	66.57	114.64
418	28.16	13.87	0.62	0.67	72.64	113.23
419	28.25	12.35	0.50	0.67	76.77	111.52
420	28.34	11.34	0.41	0.67	77.68	109.88
421	28.44	10.83	0.35	0.67	77.85	108.83
422	28.53	10.83	0.35	0.67	78.14	108.53
423	28.62	10.83	0.37	0.67	77.38	110.10
424	28.76	13.56	0.57	0.67	72.35	112.51
425	28.86	18.22	0.74	0.76	67.30	115.27
426	28.96	21.15	0.97	0.76	65.09	117.31
427	29.08	21.56	1.17	0.76	67.25	119.00
428	29.19	21.15	1.43	0.76	69.03	120.29
429	29.29	23.48	1.60	0.76	57.91	120.47
430	29.39	37.85	0.97	0.76	42.67	122.13
431	29.50	60.73	1.83	0.76	33.13	124.03
432	29.63	74.39	2.28	0.76	32.04	126.13

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	29.65	65.49	2.34	0.76	31.66	126.80
434	29.66	70.75	2.34	0.76	31.48	126.90
435	29.72	76.72	2.35	0.76	30.48	126.99
436	29.80	73.08	2.34	0.76	28.82	127.09
437	29.85	83.60	2.30	0.96	24.74	127.25
438	29.94	111.74	2.18	1.05	19.12	127.53
439	30.00	139.37	2.11	0.96	14.70	127.66
440	30.05	155.36	1.99	0.96	11.90	127.40
441	30.14	164.17	1.72	0.86	10.16	126.80
442	30.19	168.22	1.55	0.86	9.10	126.23
443	30.24	170.24	1.55	0.86	8.70	126.01
444	30.29	170.34	1.56	0.86	8.77	126.09
445	30.38	168.42	1.60	0.96	9.02	126.13
446	30.43	164.37	1.60	0.96	9.33	126.13
447	30.48	161.54	1.59	0.96	9.59	126.05
448	30.54	158.91	1.58	0.96	9.78	125.95
449	30.62	156.98	1.55	0.96	9.79	125.86
450	30.67	159.11	1.54	0.96	9.79	125.78
451	30.72	157.18	1.54	0.96	9.69	125.76
452	30.76	159.31	1.53	0.96	9.55	125.70
453	30.86	161.84	1.49	0.96	9.23	125.64
454	30.91	164.98	1.48	0.96	8.91	125.62
455	30.95	168.42	1.49	0.96	8.55	125.64
456	31.03	173.38	1.47	0.96	8.12	125.67
457	31.10	179.65	1.45	1.05	7.69	125.73
458	31.15	185.02	1.48	1.05	7.34	125.89
459	31.20	190.38	1.52	1.05	7.18	126.13
460	31.26	193.52	1.57	1.05	7.15	126.36
461	31.34	193.62	1.60	1.05	7.71	126.40
462	31.37	171.46	1.60	1.05	7.87	126.43
463	31.38	188.76	1.60	1.15	8.09	126.36
464	31.43	183.91	1.58	1.15	7.77	126.31
465	31.47	181.17	1.53	1.15	8.03	126.07
466	31.55	172.87	1.49	1.15	8.51	125.78
467	31.59	160.83	1.47	1.15	9.39	125.48
468	31.66	147.27	1.45	1.15	10.59	125.21
469	31.73	135.12	1.45	1.05	12.03	125.03
470	31.78	124.80	1.48	1.05	13.62	124.95
471	31.84	115.28	1.53	1.05	15.49	125.08
472	31.93	106.78	1.65	1.05	17.52	125.26
473	31.98	99.59	1.73	1.15	19.53	125.52
474	32.02	94.84	1.82	1.15	20.69	125.90
475	32.09	100.05	1.96	1.15	21.58	126.26
476	32.16	96.05	2.03	1.15	21.57	126.59
477	32.22	100.51	2.04	1.15	21.42	126.73
478	32.27	104.25	2.05	1.15	20.75	126.84
479	32.34	105.67	2.06	1.24	20.20	126.90
480	32.42	108.10	2.04	1.24	19.56	126.93

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	32.46	112.85	2.02	1.24	18.55	126.88
482	32.54	118.12	1.95	1.24	17.41	126.77
483	32.60	122.16	1.87	1.24	16.07	126.34
484	32.67	124.90	1.62	1.24	15.05	125.97
485	32.75	127.33	1.63	1.24	14.32	125.74
486	32.81	130.26	1.68	1.24	14.20	126.03
487	32.89	133.50	1.79	1.24	14.12	126.37
488	32.94	136.34	1.83	1.24	14.96	126.52
489	32.95	118.52	1.84	1.24	14.91	126.69
490	33.00	138.16	1.90	1.24	14.89	126.92
491	33.06	141.90	1.98	1.24	14.05	127.30
492	33.11	143.12	2.03	1.24	14.18	127.55
493	33.20	141.70	2.09	1.24	14.56	127.71
494	33.25	138.76	2.13	1.24	15.10	127.86
495	33.34	136.54	2.19	1.24	15.55	127.94
496	33.38	135.73	2.19	1.24	15.74	128.03
497	33.48	137.75	2.22	1.24	15.68	128.19
498	33.58	141.70	2.30	1.24	15.42	128.42
499	33.63	146.25	2.34	1.24	15.06	128.72
500	33.73	152.23	2.43	1.24	14.62	129.02
501	33.82	158.70	2.51	1.24	14.13	129.36
502	33.87	165.89	2.57	1.24	13.67	129.70
503	33.96	172.57	2.69	1.24	13.23	130.04
504	34.02	179.65	2.77	1.24	12.84	130.48
505	34.11	189.47	2.95	1.24	12.43	131.00
506	34.18	200.91	3.15	1.24	12.08	131.61
507	34.26	211.03	3.36	1.24	11.89	132.25
508	34.35	219.33	3.65	1.24	11.82	132.88
509	34.44	227.93	3.92	1.34	11.72	133.37
510	34.49	235.22	3.98	1.34	11.56	133.69
511	34.59	238.66	4.05	1.34	11.45	133.86
512	34.69	239.88	4.13	1.34	11.44	133.98
513	34.76	241.39	4.15	1.34	11.40	134.01
514	34.83	241.50	4.07	1.43	11.43	134.00
515	34.93	238.86	4.12	1.43	11.44	133.81
516	35.02	233.50	3.89	1.43	11.54	133.60
517	35.12	229.05	3.79	1.43	11.46	133.22
518	35.22	226.72	3.60	1.43	11.42	132.94
519	35.30	223.58	3.51	1.43	11.44	132.63
520	35.38	216.29	3.41	1.43	12.34	132.31
521	35.43	185.73	3.36	1.43	13.07	132.03
522	35.46	192.21	3.30	1.53	13.71	131.78
523	35.51	190.18	3.21	1.62	13.68	131.56
524	35.56	179.15	3.11	1.62	14.30	131.05
525	35.66	160.93	2.83	1.53	15.30	130.47
526	35.70	150.40	2.73	1.53	16.62	129.73
527	35.80	133.20	2.53	1.53	18.63	129.08
528	35.89	111.94	2.45	1.53	21.97	128.26

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	35.96	88.76	2.31	1.53	26.84	127.15
530	36.04	66.50	1.99	1.43	32.56	125.33
531	36.14	49.39	1.45	1.43	38.50	123.16
532	36.19	40.49	1.23	1.43	42.06	121.28
533	36.28	40.49	1.16	1.43	44.05	120.76
534	36.33	40.49	1.27	1.43	43.63	120.56
535	36.42	40.49	1.14	1.43	42.36	120.82
536	36.48	45.85	1.23	1.43	39.85	121.28
537	36.52	51.52	1.40	1.43	38.41	122.62
538	36.62	55.67	1.74	1.43	38.39	123.71
539	36.68	55.06	1.84	1.43	39.88	124.37
540	36.77	51.42	1.88	1.43	40.89	124.37
541	36.86	51.92	1.78	1.43	39.71	124.46
542	36.90	60.53	1.84	1.53	32.23	124.83
543	37.00	90.49	1.76	1.53	21.98	125.79
544	37.10	143.32	1.82	1.62	14.18	126.63
545	37.20	187.14	1.82	1.53	9.48	127.07
546	37.29	217.10	1.62	1.53	7.15	127.31
547	37.39	234.82	1.72	1.53	6.16	127.69
548	37.49	245.04	1.93	1.53	6.15	128.39
549	37.53	245.80	2.08	1.53	6.43	129.01
550	37.58	245.80	2.19	1.43	6.79	129.47
551	37.62	246.56	2.33	1.43	7.05	129.90
552	37.69	251.11	2.46	1.43	7.41	130.49
553	37.77	253.95	2.76	1.43	7.74	131.04
554	37.82	255.46	2.89	1.34	8.12	131.53
555	37.87	255.46	3.00	1.34	8.40	131.80
556	37.91	253.54	3.09	1.34	8.73	131.98
557	37.97	249.09	3.14	1.34	9.14	132.07
558	38.06	242.00	3.17	1.43	9.58	132.05
559	38.10	234.61	3.14	1.34	9.96	131.95
560	38.17	230.06	3.08	1.34	10.09	131.72
561	38.25	227.93	2.95	1.34	9.95	131.37
562	38.35	226.21	2.75	1.34	9.74	130.98
563	38.40	223.18	2.65	1.34	9.59	130.66
564	38.46	220.85	2.61	1.34	9.55	130.46
565	38.54	220.85	2.57	1.34	9.50	130.34
566	38.60	220.85	2.53	1.34	9.36	130.20
567	38.69	220.85	2.46	1.34	9.14	130.07
568	38.74	224.90	2.42	1.34	8.84	129.97
569	38.83	228.95	2.40	1.34	8.66	130.01
570	38.88	229.65	2.47	1.34	8.43	129.87
571	38.97	228.95	2.27	1.43	8.33	129.71
572	39.02	227.63	2.26	1.43	8.17	129.42
573	39.11	225.10	2.21	1.43	8.23	129.25
574	39.16	220.54	2.14	1.43	8.40	128.95
575	39.23	209.82	2.04	1.43	9.12	128.58
576	39.24	186.03	2.02	1.43	9.26	128.31

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	39.28	206.53	1.96	1.43	9.26	128.10
578	39.32	203.24	1.90	1.43	8.75	127.86
579	39.39	195.95	1.80	1.43	9.08	127.52
580	39.47	184.41	1.77	1.43	9.80	127.22
581	39.54	171.46	1.78	1.43	10.93	127.03
582	39.62	158.50	1.78	1.43	12.28	126.82
583	39.71	145.24	1.76	1.43	13.78	126.57
584	39.76	133.40	1.75	1.43	15.25	126.29
585	39.85	124.80	1.72	1.43	16.63	126.05
586	39.90	117.71	1.71	1.43	17.85	125.82
587	40.00	111.03	1.69	1.34	19.15	125.63
588	40.06	104.35	1.69	1.34	20.49	125.46
589	40.15	98.68	1.69	1.34	21.96	125.31
590	40.21	92.91	1.69	1.34	23.70	125.27
591	40.29	86.84	1.76	1.34	25.91	125.29
592	40.35	79.96	1.83	1.34	28.93	125.45
593	40.43	72.17	1.95	1.34	31.85	125.15
594	40.52	64.47	1.72	1.34	35.38	124.58
595	40.58	54.86	1.64	1.34	39.26	123.64
596	40.67	46.25	1.54	1.34	44.53	122.80
597	40.77	39.47	1.43	1.34	48.71	122.20
598	40.84	39.12	1.45	1.34	51.09	121.91
599	40.89	38.77	1.46	1.24	47.89	122.14
600	40.94	48.89	1.45	1.24	41.53	122.58
601	41.03	61.54	1.47	1.24	34.10	123.11
602	41.08	73.89	1.47	1.24	28.70	123.52
603	41.14	83.60	1.45	1.15	25.34	123.76
604	41.22	88.56	1.45	1.15	23.58	123.93
605	41.28	90.89	1.47	1.15	23.00	124.13
606	41.33	91.80	1.53	1.05	23.16	124.56
607	41.42	93.22	1.69	1.05	23.59	125.16
608	41.47	95.85	1.84	1.05	23.66	125.86
609	41.52	101.92	1.97	1.05	22.91	126.69
610	41.62	114.27	2.20	1.05	21.31	127.57
611	41.67	130.16	2.38	1.05	19.54	128.55
612	41.76	145.55	2.62	1.05	17.95	129.34
613	41.82	157.59	2.74	1.05	16.90	130.00
614	41.90	165.99	2.90	1.05	16.15	130.44
615	41.99	172.67	2.96	1.05	15.70	130.73
616	42.05	176.01	2.98	1.05	15.44	130.86
617	42.15	175.71	3.00	0.96	15.47	130.91
618	42.23	173.89	3.02	0.96	15.76	130.92
619	42.30	170.34	3.03	0.96	16.20	130.85
620	42.38	164.37	2.97	0.96	16.79	130.64
621	42.48	156.17	2.87	0.96	17.75	130.21
622	42.57	140.79	2.70	0.96	19.03	129.66
623	42.64	128.95	2.56	0.86	20.48	129.02
624	42.72	120.14	2.42	0.86	21.44	128.37

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	42.82	114.47	2.21	0.86	22.03	127.72
626	42.90	109.51	2.08	0.86	22.42	127.19
627	42.97	106.07	2.04	0.86	23.04	126.89
628	43.06	102.53	2.03	0.86	23.94	126.76
629	43.15	98.28	2.05	0.86	24.28	126.30
630	43.20	95.44	1.73	0.86	23.92	125.87
631	43.30	99.49	1.72	0.86	21.66	125.62
632	43.40	117.61	1.75	0.86	18.56	126.10
633	43.48	142.51	1.83	0.96	16.70	126.59
634	43.51	137.14	1.89	0.96	15.94	126.91
635	43.52	137.65	1.91	0.86	15.16	127.23
636	43.56	163.87	1.98	0.86	13.67	127.68
637	43.61	178.84	2.08	0.86	11.96	128.22
638	43.67	193.82	2.13	0.86	10.83	128.59
639	43.72	206.98	2.13	0.86	9.87	128.82
640	43.80	217.20	2.15	0.86	9.14	128.98
641	43.85	225.30	2.16	0.86	8.63	129.13
642	43.90	231.68	2.18	0.86	8.26	129.25
643	43.94	236.74	2.19	0.86	7.97	129.33
644	43.99	240.69	2.18	0.86	7.76	129.35
645	44.08	242.00	2.18	0.86	7.68	129.38
646	44.14	241.90	2.20	0.86	7.83	129.54
647	44.22	240.59	2.33	0.86	8.11	129.75
648	44.28	238.66	2.39	0.86	8.47	129.97
649	44.33	235.63	2.43	0.86	8.80	130.11
650	44.40	232.69	2.50	0.86	9.29	130.33
651	44.48	228.44	2.64	0.86	9.67	130.62
652	44.52	232.74	2.75	0.86	10.35	131.05
653	44.61	224.49	3.00	0.96	10.26	131.06
654	44.72	232.79	2.65	0.96	10.27	131.18
655	44.77	237.24	2.86	0.96	9.91	131.18
656	44.91	238.36	2.94	1.05	10.09	131.47
657	44.95	237.95	2.96	1.05	10.63	131.50
658	45.02	218.72	2.98	1.05	10.98	131.47
659	45.04	225.50	2.97	1.15	13.35	131.14
660	45.06	152.63	2.96	1.15	12.86	131.13
661	45.11	232.29	2.89	1.15	12.30	131.08
662	45.15	240.38	2.84	1.15	9.78	131.30
663	45.21	247.16	2.81	1.15	9.27	131.31
664	45.25	253.14	2.82	1.15	8.95	131.37
665	45.30	256.98	2.86	1.15	8.80	131.48
666	45.35	258.70	2.90	1.15	8.79	131.59
667	45.41	258.40	2.92	1.15	8.84	131.65
668	45.49	258.10	2.93	1.15	8.94	131.65
669	45.55	254.45	2.91	1.15	9.06	131.57
670	45.63	249.80	2.86	1.15	9.25	131.42
671	45.69	244.23	2.81	1.15	9.48	131.22
672	45.78	236.94	2.74	1.15	9.80	131.01

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	45.84	228.64	2.69	1.15	10.17	130.69
674	45.93	218.52	2.57	1.15	10.59	130.25
675	46.02	205.87	2.39	1.15	11.15	129.68
676	46.08	190.89	2.26	1.15	11.83	128.94
677	46.16	174.39	2.03	1.15	12.80	128.17
678	46.24	157.89	1.90	1.15	14.14	127.35
679	46.31	139.07	1.81	1.15	16.32	126.66
680	46.41	117.21	1.75	1.05	19.70	126.05
681	46.48	95.75	1.74	1.05	24.72	125.44
682	46.56	74.29	1.72	1.05	31.32	124.66
683	46.65	57.08	1.60	1.05	39.23	123.40
684	46.75	42.81	1.33	1.05	46.43	121.67
685	46.84	36.34	1.06	1.05	55.36	119.83
686	46.94	30.67	0.95	1.05	60.33	118.19
687	47.02	25.20	0.82	1.15	66.74	116.92
688	47.08	21.46	0.75	1.15	74.89	115.79
689	47.12	17.41	0.72	1.15	81.21	115.04
690	47.16	17.36	0.69	1.05	83.23	114.56
691	47.21	18.72	0.65	1.05	82.03	114.08
692	47.27	17.31	0.59	1.05	81.52	113.39
693	47.35	16.30	0.53	1.05	83.53	112.58
694	47.40	15.59	0.49	1.05	83.45	111.48
695	47.50	15.28	0.39	1.05	82.43	110.45
696	47.55	15.18	0.36	1.05	80.62	109.38
697	47.61	14.98	0.33	1.05	80.14	108.87
698	47.69	14.78	0.32	1.05	80.47	108.49
699	47.76	14.37	0.31	1.05	81.28	108.16
700	47.83	13.97	0.29	1.05	81.76	107.60
701	47.93	13.66	0.26	1.05	81.12	106.97
702	48.02	13.87	0.24	1.05	80.49	106.61
703	48.09	13.87	0.26	1.05	79.44	106.28
704	48.18	13.87	0.22	0.96	80.27	106.53
705	48.27	13.76	0.27	0.96	81.39	107.03
706	48.37	13.97	0.31	0.96	83.22	107.94
707	48.46	14.17	0.33	0.96	84.23	108.58
708	48.52	14.17	0.35	0.96	85.01	108.99
709	48.60	14.17	0.36	0.96	85.57	109.30
710	48.70	14.37	0.37	0.96	85.68	109.56
711	48.79	14.57	0.38	0.96	85.16	109.83
712	48.85	14.98	0.40	0.96	84.80	110.40
713	48.94	15.59	0.45	0.86	84.36	111.35
714	49.04	16.60	0.53	0.86	82.26	112.03
715	49.13	17.81	0.50	0.86	82.44	114.35
716	49.23	20.45	0.95	0.86	79.90	116.80
717	49.33	25.10	1.19	0.86	78.26	119.08
718	49.38	26.52	1.32	0.86	79.49	120.23
719	49.42	22.98	1.49	0.86	79.52	121.11
720	49.48	28.24	1.64	0.76	79.69	121.78

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	49.53	28.85	1.70	0.76	76.78	122.38
722	49.58	29.25	1.78	0.76	76.54	122.73
723	49.63	30.16	1.86	0.76	76.14	123.06
724	49.72	30.87	1.90	0.76	75.17	123.25
725	49.77	31.68	1.88	0.76	74.33	123.29
726	49.83	31.68	1.86	0.76	74.18	123.23
727	49.92	30.87	1.85	0.76	75.14	123.07
728	49.97	29.55	1.80	0.76	75.30	122.90
729	50.04	30.72	1.75	0.76	76.58	122.68
730	50.11	28.14	1.74	0.76	75.95	122.69
731	50.20	30.57	1.79	0.76	74.75	122.53
732	50.27	31.88	1.62	0.76	72.22	122.03
733	50.34	29.86	1.37	0.76	71.16	120.74
734	50.45	26.72	1.07	0.76	72.38	119.07
735	50.54	23.68	0.89	0.76	75.35	117.45
736	50.59	20.75	0.82	0.76	79.17	116.17
737	50.68	18.93	0.71	0.76	82.34	115.07
738	50.79	18.02	0.62	0.76	83.79	114.12
739	50.88	17.41	0.60	0.76	83.70	113.63
740	50.98	17.97	0.60	0.86	84.20	113.54
741	51.07	17.51	0.60	0.86	82.59	113.17
742	51.17	17.91	0.50	0.86	77.88	112.22
743	51.24	19.84	0.38	0.86	73.04	111.69
744	51.33	20.75	0.47	0.86	72.41	112.26
745	51.46	19.94	0.60	0.86	75.43	113.32
746	51.46	19.53	0.60	0.86	78.27	114.06
747	51.51	19.89	0.66	0.86	79.25	114.37
748	51.56	19.84	0.68	0.86	80.43	114.92
749	51.65	19.84	0.75	0.86	81.58	115.41
750	51.71	20.14	0.80	0.86	82.75	115.96
751	51.79	20.24	0.85	0.86	82.76	116.41
752	51.85	21.05	0.88	0.96	82.60	117.17
753	51.94	22.37	1.05	0.96	82.55	118.05
754	51.99	22.87	1.16	0.96	82.91	119.26
755	52.09	24.39	1.38	0.96	83.97	120.45
756	52.19	25.20	1.63	0.96	79.61	121.96
757	52.28	33.60	1.89	1.05	72.62	123.41
758	52.35	41.19	2.10	1.05	70.52	124.45
759	52.43	34.41	2.30	1.05	71.21	125.03
760	52.52	35.53	2.36	1.05	74.91	125.21
761	52.62	35.53	2.39	1.05	74.30	125.23
762	52.72	35.73	2.30	1.05	73.23	125.06
763	52.81	36.64	2.18	1.05	76.25	125.06
764	52.91	30.36	2.50	1.05	84.74	125.89
765	53.00	26.92	3.37	1.05	78.34	127.32
766	53.10	54.35	3.37	1.15	54.98	129.03
767	53.20	105.77	3.09	1.15	36.28	130.96
768	53.29	164.47	4.18	1.15	25.56	132.47

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	53.38	221.05	4.12	1.24	20.37	133.80
770	53.46	256.07	4.20	1.24	17.07	134.82
771	53.53	303.03	5.14	1.24	16.36	136.29
772	53.63	317.00	6.49	1.34	15.39	137.26
773	53.73	349.49	5.84	1.43	13.15	137.28
774	53.82	418.82	4.63	1.53	10.93	136.47
775	53.92	396.66	4.29	1.62	10.04	135.51
776	53.94	347.57	4.04	1.72	10.76	134.94
777	53.96	336.23	3.96	1.53	11.60	134.54
778	53.97	324.90	3.90	1.82	10.87	134.48
779	54.05	386.03	3.80	1.91	9.65	134.60
780	54.08	421.76	3.84	2.01	7.98	134.88
781	54.13	470.95	3.88	2.01	6.82	135.32
782	54.19	526.82	4.09	2.10	6.18	136.15
783	54.25	558.50	4.85	2.10	6.33	136.53
784	54.28	487.24	4.52	2.20	6.83	136.70
785	54.29	486.79	4.52	2.20	7.28	136.40
786	54.34	486.33	4.52	2.20	7.28	136.41
787	54.35	487.45	4.52	2.20	7.16	136.45
788	54.40	502.73	4.55	2.29	6.91	136.58
789	54.44	524.39	4.66	2.29	6.59	136.78
790	54.49	539.67	4.74	2.39	6.33	136.88
791	54.53	542.71	4.62	2.39	6.16	137.00
792	54.57	556.27	4.81	2.68	6.01	137.19
793	54.58	575.70	5.00	2.96	6.08	137.28
794	54.63	571.25	5.32	3.06	6.35	137.28
795	54.68	535.62	5.13	3.15	7.02	137.28
796	54.73	501.92	5.33	3.35	7.61	137.28
797	54.78	493.82	5.24	3.25	7.81	137.28
798	54.83	503.13	4.96	3.35	8.02	137.28
799	54.88	483.80	5.42	3.25	8.15	137.28
800	54.92	504.35	5.80	3.35	8.44	137.28
801	54.97	513.76	5.91	3.35	8.28	137.28
802	55.02	514.17	5.71	3.35	8.29	137.28
803	55.12	512.24	5.99	3.35	9.19	137.28
804	55.17	437.14	6.44	3.35	10.90	137.28
805	55.25	397.97	6.94	3.54	12.33	137.28
806	55.31	396.35	6.00	3.63	12.48	137.28
807	55.36	388.16	5.24	3.73	11.51	136.87
808	55.45	379.86	4.35	3.82	10.76	135.80
809	55.50	375.10	3.96	3.82	10.78	135.09
810	55.60	342.61	4.16	3.82	11.41	134.98
811	55.65	335.83	4.33	3.82	12.01	134.55
812	55.71	318.11	3.48	3.73	11.81	133.90
813	55.75	318.32	3.23	4.01	11.15	133.00
814	55.79	324.59	3.09	4.01	10.75	132.84
815	55.84	332.28	3.22	4.01	10.43	132.92
816	55.89	340.38	3.26	4.11	10.29	133.07

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	55.90	341.19	3.24	4.30	10.16	133.10
818	55.94	341.70	3.23	4.30	10.40	133.09
819	55.99	325.71	3.29	4.40	10.86	133.10
820	56.03	315.28	3.33	4.40	11.37	133.06
821	56.08	312.45	3.28	4.40	11.60	132.92
822	56.14	307.08	3.17	4.40	11.73	132.73
823	56.22	299.39	3.13	4.40	11.94	132.53
824	56.28	293.01	3.09	4.49	12.14	132.38
825	56.33	290.28	3.03	4.40	12.22	132.35
826	56.38	294.23	3.11	4.40	12.04	132.26
827	56.45	297.47	2.97	4.40	11.65	132.30
828	56.52	312.14	3.01	4.40	11.06	132.37
829	56.62	327.93	3.08	4.40	10.51	132.50
830	56.66	335.32	3.02	4.40	9.79	132.45
831	56.73	351.82	2.83	4.40	9.62	132.89
832	56.81	362.85	3.53	4.49	9.77	133.43
833	56.95	356.47	3.65	4.40	10.06	134.06
834	57.00	370.75	3.68	4.40	10.03	134.48
835	57.09	389.98	4.06	4.40	10.22	134.71
836	57.19	358.40	4.02	4.59	10.60	134.88
837	57.27	357.18	4.00	4.49	11.00	134.55
838	57.35	346.35	3.69	4.59	10.13	133.80
839	57.44	369.23	2.85	4.49	9.47	132.97
840	57.50	352.73	2.88	4.59	8.69	132.46
841	57.52	370.95	2.99	4.30	8.68	133.16
842	57.58	410.42	3.60	4.30	8.49	134.41
843	57.63	446.56	4.36	4.30	8.42	135.32
844	57.72	439.07	4.21	4.40	8.40	135.58
845	57.77	431.17	3.97	4.40	8.22	135.14
846	57.82	430.77	3.67	4.40	7.74	134.36
847	57.91	426.51	3.05	4.40	6.86	133.51
848	57.96	452.73	2.75	4.40	6.01	132.56
849	58.02	449.09	2.48	4.40	5.35	132.23
850	58.09	474.69	2.59	4.49	5.13	132.30
851	58.16	483.80	2.77	4.49	4.92	132.61
852	58.25	495.95	2.73	4.49	5.00	132.98
853	58.30	493.42	2.98	4.49	5.44	133.54
854	58.40	473.38	3.46	4.49	5.94	133.95
855	58.50	471.86	3.32	4.49	6.39	134.14
856	58.56	460.12	3.32	4.49	6.35	134.03
857	58.64	470.34	3.32	4.49	6.52	134.15
858	58.73	463.76	3.50	4.68	6.66	134.73
859	58.78	490.08	4.08	4.68	6.43	134.94
860	58.88	510.42	3.53	4.68	6.01	135.03
861	58.97	519.43	3.50	4.78	5.46	134.39
862	59.07	503.03	3.11	4.78	5.31	133.97
863	59.13	496.05	2.99	4.78	5.28	133.42
864	59.23	481.47	2.88	4.78	5.21	132.95

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	59.31	476.41	2.60	4.78	5.30	132.24
866	59.38	435.32	2.31	4.78	5.27	131.56
867	59.41	439.12	2.27	4.78	5.38	131.23
868	59.46	442.91	2.34	4.78	5.29	131.28
869	59.51	448.48	2.34	4.78	5.27	131.25
870	59.57	439.07	2.23	4.78	5.63	132.20
871	59.66	467.91	3.25	4.87	5.58	132.94
872	59.75	505.97	3.06	4.97	6.03	134.45
873	59.80	502.83	4.04	4.97	6.32	135.37
874	59.85	510.42	4.53	4.97	6.89	136.20
875	59.91	512.45	4.44	4.97	7.09	136.30
876	59.99	489.57	4.24	4.97	7.40	136.48
877	60.05	494.33	4.91	4.87	8.36	136.97
878	60.09	458.80	5.56	4.78	9.17	137.25
879	60.14	440.99	5.00	4.78	9.81	137.14
880	60.19	433.30	4.90	4.78	9.70	136.76
881	60.22	439.07	4.84	4.78	9.61	136.51
882	60.28	430.16	4.56	4.78	10.15	136.19
883	60.33	369.53	4.52	4.78	11.14	135.77
884	60.38	343.82	4.41	4.78	12.93	135.37
885	60.42	303.34	4.35	4.68	14.24	134.92
886	60.48	281.88	4.12	4.68	14.94	133.83
887	60.57	260.63	2.98	4.59	14.40	131.99
888	60.66	244.74	2.02	4.59	13.41	129.58
889	60.68	226.11	1.72	4.49	12.77	127.88
890	60.69	225.45	1.67	4.01	12.50	126.95
891	60.74	224.80	1.43	4.11	12.59	126.30
892	60.79	202.83	1.36	4.21	12.85	125.42
893	60.84	190.99	1.24	4.11	13.42	124.52
894	60.89	182.49	1.05	4.11	13.76	123.73
895	60.98	173.38	1.04	4.01	14.35	123.40
896	61.03	167.00	1.14	4.01	16.66	125.09
897	61.08	163.66	1.94	4.01	20.32	128.00
898	61.18	163.76	3.09	3.92	22.76	129.84
899	61.23	166.29	2.90	3.92	24.31	131.32
900	61.31	174.39	3.66	3.92	20.35	131.18
901	61.42	241.39	2.47	3.92	15.65	131.06
902	61.47	293.32	2.18	4.01	10.48	129.51
903	61.51	326.62	1.66	3.92	7.95	129.12
904	61.54	373.78	1.86	3.73	6.66	129.28
905	61.57	397.87	2.12	3.73	6.17	130.14
906	61.58	415.68	2.20	3.54	5.00	130.33
907	61.61	442.20	1.90	3.54	6.02	129.76
908	61.63	322.26	1.78	2.77	6.49	129.08
909	61.63	338.36	1.80	2.77	11.34	128.31
910	61.66	112.95	1.97	2.20	16.91	128.00
911	61.67	122.67	2.10	2.20	26.40	127.65
912	61.70	152.93	2.30	2.20	22.91	128.46

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	61.71	183.20	2.33	2.20	19.72	129.29
914	61.76	206.48	2.50	2.10	17.47	129.99
915	61.80	229.45	2.69	2.01	15.78	130.50
916	61.84	250.50	2.60	2.01	13.82	130.39
917	61.86	271.15	2.16	2.01	11.07	129.64
918	61.93	317.51	1.72	2.01	8.65	128.83
919	61.98	348.28	1.71	2.01	5.00	128.76
920	62.04	407.39	1.86	2.01	5.00	130.00
921	62.09	460.93	2.44	2.10	5.00	130.94
922	62.14	486.94	2.29	2.01	4.65	131.59
923	62.19	497.77	2.32	2.01	4.30	131.67
924	62.24	512.55	2.43	2.01	4.19	131.86
925	62.26	516.39	2.43	2.01	4.03	131.99
926	62.29	528.94	2.40	2.10	4.03	131.96
927	62.38	511.74	2.40	2.20	4.39	132.48
928	62.44	506.37	2.97	2.10	5.19	132.83
929	62.46	452.63	2.92	2.10	5.89	133.06
930	62.47	448.12	2.80	1.24	6.21	132.63
931	62.51	443.62	2.61	1.43	5.98	132.52
932	62.56	469.23	2.76	1.53	5.91	132.86
933	62.60	479.04	3.12	1.53	5.80	133.25
934	62.65	484.51	2.99	1.53	5.69	133.25
935	62.70	481.58	2.73	1.53	5.44	132.87
936	62.75	480.87	2.67	1.53	5.25	132.60
937	62.80	486.64	2.68	1.62	4.98	132.62
938	62.85	516.90	2.69	1.62	4.37	132.78
939	62.89	572.26	2.69	1.72	3.80	133.35
940	62.97	618.32	3.10	1.82	3.40	134.28
941	63.04	668.31	3.58	1.82	3.09	135.14
942	63.09	716.80	3.59	1.82	2.87	135.70
943	63.13	724.18	3.74	1.91	2.94	136.16
944	63.19	705.46	4.21	1.91	3.36	136.94
945	63.23	719.83	4.89	1.91	3.84	137.28
946	63.28	735.32	5.37	1.91	4.17	137.28
947	63.32	725.10	5.58	2.01	3.85	137.28
948	63.38	727.02	3.92	2.10	2.64	135.83
949	63.44	724.79	1.47	2.10	1.89	134.28
950	63.52	728.13	3.49	2.29	1.92	134.03
951	63.57	693.42	3.66	2.68	2.71	135.18
952	63.66	670.44	3.03	2.68	3.13	134.92
953	63.73	614.77	3.31	2.77	4.81	133.80
954	63.76	319.53	2.86	3.15	6.52	133.28
955	63.76	432.39	2.88	3.15	7.53	132.72
956	63.78	483.50	2.92	3.15	6.10	133.35
957	63.81	499.59	3.22	3.15	5.61	134.22
958	63.85	555.36	3.75	3.15	5.72	134.88
959	63.86	524.19	3.76	3.15	6.14	135.34
960	63.91	488.05	3.95	3.25	6.96	135.56

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	63.94	481.37	4.28	3.06	7.58	135.81
962	63.95	481.78	4.31	2.96	7.84	136.00
963	64.00	477.73	4.30	2.96	7.92	135.94
964	64.02	469.13	4.22	2.96	7.88	135.77
965	64.05	472.67	4.05	2.96	7.62	135.55
966	64.09	485.42	3.89	2.96	7.39	135.35
967	64.11	476.31	3.87	3.06	7.15	135.11
968	64.15	478.34	3.65	3.06	6.89	134.84
969	64.20	492.00	3.47	3.06	6.53	134.82
970	64.25	512.45	3.75	3.06	6.14	134.94
971	64.29	533.19	3.70	3.06	5.78	135.26
972	64.34	561.33	3.79	3.25	5.01	135.28
973	64.43	616.49	3.54	3.25	4.34	135.35
974	64.48	639.47	3.59	3.35	3.80	135.20
975	64.53	636.74	3.43	3.35	3.33	134.70
976	64.58	651.72	2.78	3.35	3.10	134.64
977	64.63	676.61	3.45	3.44	2.91	135.01
978	64.68	713.46	3.79	3.44	3.16	136.27
979	64.73	738.66	4.50	3.44	3.23	136.63
980	64.77	703.94	3.99	3.44	3.00	136.64
981	64.82	764.06	3.71	3.63	2.55	136.18
982	64.87	785.42	3.67	3.63	2.65	135.90
983	64.89	648.27	3.66	3.82	2.87	135.82
984	64.93	708.09	3.69	3.82	3.20	135.78
985	64.94	712.24	3.73	3.92	2.93	135.98
986	64.98	726.92	3.83	3.92	2.86	136.11
987	64.99	737.75	3.84	4.01	2.79	136.19
988	65.03	737.24	3.82	4.01	2.77	136.10
989	65.08	721.96	3.70	4.11	2.68	135.79
990	65.13	721.76	3.39	4.01	2.53	135.18
991	65.17	702.63	3.00	4.21	2.31	134.38
992	65.22	686.23	2.70	4.30	2.22	133.76
993	65.23	678.84	2.70	4.30	2.19	133.47
994	65.28	679.40	2.71	4.40	2.24	133.50
995	65.32	679.40	2.75	4.49	2.48	134.03
996	65.37	679.95	3.32	4.49	2.63	134.36
997	65.42	680.97	3.11	4.49	2.78	134.78
998	65.47	692.71	3.26	4.49	2.89	134.63
999	65.48	641.09	3.19	4.40	3.08	134.58
1000	65.49	637.65	3.11	4.01	3.14	134.13
1001	65.52	637.65	2.79	4.40	3.09	133.95
1002	65.57	634.21	2.97	4.30	1.61	130.82
1003	65.62	664.97	0.00	4.40	0.17	126.03
1004	65.67	684.10	0.00	4.49	N/A	87.36
1005	65.69	698.07	0.00	4.59	N/A	87.36
1006	65.72	709.31	0.00	4.59	N/A	87.36
1007	65.77	749.49	0.00	4.59	N/A	87.36
1008	65.82	797.77	0.00	4.59	N/A	87.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1009	65.86	824.89	0.00	4.59	N/A	87.36
1010	65.86	813.05	0.00	4.59	N/A	87.36
1011	65.91	862.75	0.00	4.68	N/A	87.36
1012	65.96	886.13	0.00	4.78	N/A	87.36

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c:	Measured cone resistance (tsf)
f_s:	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.01	0.00	0.00	0.00	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
2	0.04	0.00	0.00	0.00	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
3	0.08	0.00	0.00	0.00	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
4	0.10	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
5	0.13	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
6	0.18	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
7	0.22	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
8	0.27	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
9	0.33	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
10	0.36	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
11	0.37	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
12	0.38	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
13	0.42	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
14	0.44	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
15	0.47	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
16	0.47	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
17	0.52	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
18	0.56	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
19	0.58	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
20	0.61	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
21	0.66	0.04	0.00	0.04	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
22	0.76	0.04	0.00	0.04	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
23	0.80	0.04	0.00	0.04	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
24	0.81	0.04	0.00	0.04	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
25	0.85	0.05	0.00	0.05	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
26	0.86	0.05	0.00	0.05	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
27	0.90	0.05	0.00	0.05	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
28	0.95	0.05	0.00	0.05	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
29	1.00	0.05	0.00	0.05	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
30	1.05	0.06	0.00	0.06	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
31	1.14	0.06	0.00	0.06	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
32	1.24	0.07	0.00	0.07	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
33	1.31	0.07	0.00	0.07	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
34	1.36	0.07	0.00	0.07	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
35	1.37	0.07	0.00	0.07	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
36	1.39	0.07	0.00	0.07	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
37	1.43	0.08	0.00	0.08	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
38	1.44	0.08	0.00	0.08	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
39	1.49	0.08	0.00	0.08	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
40	1.53	0.08	0.00	0.08	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
41	1.58	0.08	0.00	0.08	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
42	1.63	0.09	0.00	0.09	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
43	1.68	0.09	0.00	0.09	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
44	1.72	0.09	0.00	0.09	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
45	1.77	0.09	0.00	0.09	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
46	1.82	0.10	0.00	0.10	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
47	1.86	0.10	0.00	0.10	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
48	1.92	0.10	0.00	0.10	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	1.97	0.10	0.00	0.10	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
50	2.01	0.11	0.00	0.11	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
51	2.09	0.11	0.00	0.11	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
52	2.16	0.11	0.00	0.11	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
53	2.20	0.12	0.00	0.12	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
54	2.25	0.12	0.00	0.12	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
55	2.31	0.12	0.00	0.12	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
56	2.37	0.13	0.00	0.13	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
57	2.40	0.13	0.00	0.13	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
58	2.46	0.13	0.00	0.13	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
59	2.54	0.13	0.00	0.13	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
60	2.59	0.14	0.00	0.14	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
61	2.69	0.14	0.00	0.14	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
62	2.74	0.15	0.00	0.15	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
63	2.83	0.15	0.00	0.15	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
64	2.88	0.15	0.00	0.15	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
65	2.98	0.16	0.00	0.16	1.00	0.272	1.68	0.161	1.00	1.10	2.000	No
66	3.03	0.16	0.00	0.16	0.99	0.272	1.68	0.161	1.00	1.10	2.000	No
67	3.12	0.17	0.00	0.17	0.99	0.272	1.68	0.161	1.00	1.10	2.000	No
68	3.21	0.17	0.00	0.17	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
69	3.27	0.17	0.00	0.17	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
70	3.34	0.18	0.00	0.18	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
71	3.41	0.18	0.00	0.18	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
72	3.51	0.19	0.00	0.19	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
73	3.55	0.19	0.00	0.19	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
74	3.65	0.19	0.00	0.19	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
75	3.75	0.20	0.00	0.20	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
76	3.83	0.20	0.00	0.20	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
77	3.94	0.21	0.00	0.21	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
78	4.04	0.22	0.00	0.22	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
79	4.13	0.22	0.00	0.22	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
80	4.24	0.23	0.00	0.23	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
81	4.38	0.23	0.00	0.23	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
82	4.50	0.24	0.00	0.24	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
83	4.62	0.25	0.00	0.25	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
84	4.71	0.25	0.00	0.25	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
85	4.75	0.26	0.00	0.26	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
86	4.84	0.26	0.00	0.26	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
87	4.89	0.26	0.00	0.26	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
88	4.94	0.27	0.00	0.27	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
89	4.98	0.27	0.00	0.27	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
90	5.07	0.27	0.00	0.27	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
91	5.13	0.28	0.00	0.28	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
92	5.17	0.28	0.00	0.28	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
93	5.27	0.28	0.00	0.28	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
94	5.32	0.29	0.00	0.29	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
95	5.42	0.29	0.00	0.29	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
96	5.46	0.30	0.00	0.30	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	5.56	0.30	0.00	0.30	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
98	5.61	0.30	0.00	0.30	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
99	5.71	0.31	0.00	0.31	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
100	5.78	0.31	0.00	0.31	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
101	5.85	0.32	0.00	0.32	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
102	5.95	0.32	0.00	0.32	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
103	6.00	0.33	0.00	0.33	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
104	6.09	0.33	0.00	0.33	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
105	6.14	0.33	0.00	0.33	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
106	6.24	0.34	0.00	0.34	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
107	6.30	0.34	0.00	0.34	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
108	6.38	0.35	0.00	0.35	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
109	6.46	0.35	0.00	0.35	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
110	6.50	0.35	0.00	0.35	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
111	6.56	0.36	0.00	0.36	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
112	6.63	0.36	0.00	0.36	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
113	6.68	0.36	0.00	0.36	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
114	6.76	0.37	0.00	0.37	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
115	6.82	0.37	0.00	0.37	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
116	6.88	0.37	0.00	0.37	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
117	6.96	0.38	0.00	0.38	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
118	7.03	0.38	0.00	0.38	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
119	7.11	0.39	0.00	0.39	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
120	7.16	0.39	0.00	0.39	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
121	7.26	0.39	0.00	0.39	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
122	7.31	0.40	0.00	0.40	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
123	7.40	0.40	0.00	0.40	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
124	7.45	0.41	0.00	0.41	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
125	7.54	0.41	0.00	0.41	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
126	7.60	0.41	0.00	0.41	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
127	7.68	0.42	0.00	0.42	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
128	7.74	0.42	0.00	0.42	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
129	7.83	0.43	0.00	0.43	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
130	7.90	0.43	0.00	0.43	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
131	7.98	0.43	0.00	0.43	0.98	0.268	1.68	0.160	1.00	1.10	2.000	No
132	8.05	0.44	0.00	0.44	0.98	0.268	1.68	0.160	1.00	1.10	2.000	No
133	8.12	0.44	0.00	0.44	0.98	0.268	1.68	0.160	1.00	1.10	2.000	No
134	8.19	0.45	0.00	0.45	0.98	0.268	1.68	0.160	1.00	1.10	2.000	No
135	8.27	0.45	0.00	0.45	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
136	8.36	0.46	0.00	0.46	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
137	8.41	0.46	0.00	0.46	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
138	8.50	0.46	0.00	0.46	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
139	8.60	0.47	0.00	0.47	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
140	8.70	0.47	0.00	0.47	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
141	8.74	0.48	0.00	0.48	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
142	8.78	0.48	0.00	0.48	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
143	8.81	0.48	0.00	0.48	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
144	8.86	0.48	0.00	0.48	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	8.91	0.49	0.00	0.49	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
146	8.94	0.49	0.00	0.49	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
147	9.02	0.49	0.00	0.49	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
148	9.10	0.50	0.00	0.50	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
149	9.17	0.50	0.00	0.50	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
150	9.22	0.50	0.00	0.50	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
151	9.31	0.51	0.00	0.51	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
152	9.37	0.51	0.00	0.51	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
153	9.42	0.51	0.00	0.51	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
154	9.52	0.52	0.00	0.52	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
155	9.60	0.53	0.00	0.53	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
156	9.66	0.53	0.00	0.53	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
157	9.74	0.53	0.00	0.53	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
158	9.81	0.54	0.00	0.54	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
159	9.89	0.54	0.00	0.54	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
160	9.98	0.55	0.00	0.55	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
161	10.03	0.55	0.00	0.55	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
162	10.13	0.55	0.00	0.55	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
163	10.23	0.56	0.00	0.56	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
164	10.32	0.57	0.00	0.57	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
165	10.38	0.57	0.00	0.57	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
166	10.47	0.57	0.00	0.57	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
167	10.57	0.58	0.00	0.58	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
168	10.66	0.58	0.00	0.58	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
169	10.76	0.59	0.00	0.59	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
170	10.85	0.60	0.00	0.60	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
171	10.92	0.60	0.00	0.60	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
172	11.00	0.60	0.00	0.60	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
173	11.07	0.61	0.00	0.61	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
174	11.10	0.61	0.00	0.61	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
175	11.15	0.61	0.00	0.61	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
176	11.19	0.61	0.00	0.61	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
177	11.24	0.62	0.00	0.62	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
178	11.29	0.62	0.00	0.62	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
179	11.34	0.62	0.00	0.62	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
180	11.40	0.63	0.00	0.63	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
181	11.47	0.63	0.00	0.63	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
182	11.53	0.63	0.00	0.63	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
183	11.58	0.64	0.00	0.64	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
184	11.65	0.64	0.00	0.64	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
185	11.72	0.64	0.00	0.64	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
186	11.77	0.65	0.00	0.65	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
187	11.82	0.65	0.00	0.65	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
188	11.88	0.65	0.00	0.65	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
189	11.97	0.66	0.00	0.66	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
190	12.02	0.66	0.00	0.66	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
191	12.06	0.66	0.00	0.66	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
192	12.11	0.67	0.00	0.67	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	12.21	0.67	0.00	0.67	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
194	12.25	0.67	0.00	0.67	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
195	12.30	0.68	0.00	0.68	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
196	12.31	0.68	0.00	0.68	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
197	12.32	0.68	0.00	0.68	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
198	12.35	0.68	0.00	0.68	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
199	12.40	0.68	0.00	0.68	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
200	12.45	0.69	0.00	0.69	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
201	12.52	0.69	0.00	0.69	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
202	12.56	0.69	0.00	0.69	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
203	12.62	0.70	0.00	0.70	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
204	12.65	0.70	0.00	0.70	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
205	12.71	0.70	0.00	0.70	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
206	12.76	0.70	0.00	0.70	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
207	12.83	0.71	0.00	0.71	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
208	12.88	0.71	0.00	0.71	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
209	12.93	0.71	0.00	0.71	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
210	12.98	0.72	0.00	0.72	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
211	13.03	0.72	0.00	0.72	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
212	13.04	0.72	0.00	0.72	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
213	13.07	0.72	0.00	0.72	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
214	13.13	0.72	0.00	0.72	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
215	13.17	0.73	0.00	0.73	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
216	13.22	0.73	0.00	0.73	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
217	13.27	0.73	0.00	0.73	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
218	13.32	0.74	0.00	0.74	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
219	13.37	0.74	0.00	0.74	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
220	13.41	0.74	0.00	0.74	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
221	13.46	0.74	0.00	0.74	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
222	13.51	0.75	0.00	0.75	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
223	13.56	0.75	0.00	0.75	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
224	13.60	0.75	0.00	0.75	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
225	13.66	0.76	0.00	0.76	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
226	13.75	0.76	0.00	0.76	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
227	13.80	0.76	0.00	0.76	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
228	13.89	0.77	0.00	0.77	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
229	13.94	0.77	0.00	0.77	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
230	13.99	0.78	0.00	0.78	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
231	14.09	0.78	0.00	0.78	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
232	14.14	0.78	0.00	0.78	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
233	14.23	0.79	0.00	0.79	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
234	14.28	0.79	0.00	0.79	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
235	14.38	0.80	0.00	0.80	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
236	14.42	0.80	0.00	0.80	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
237	14.52	0.81	0.00	0.81	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
238	14.57	0.81	0.00	0.81	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
239	14.67	0.82	0.00	0.82	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
240	14.68	0.82	0.00	0.82	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	14.70	0.82	0.00	0.82	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
242	14.75	0.82	0.00	0.82	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
243	14.80	0.82	0.00	0.82	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
244	14.89	0.83	0.00	0.83	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
245	14.94	0.83	0.00	0.83	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
246	15.04	0.84	0.00	0.84	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
247	15.13	0.84	0.00	0.84	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
248	15.21	0.85	0.00	0.85	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
249	15.28	0.85	0.00	0.85	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
250	15.38	0.86	0.00	0.86	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
251	15.47	0.86	0.00	0.86	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
252	15.57	0.87	0.00	0.87	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
253	15.67	0.87	0.00	0.87	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
254	15.77	0.88	0.00	0.88	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
255	15.86	0.89	0.00	0.89	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
256	15.96	0.89	0.00	0.89	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
257	16.05	0.90	0.00	0.90	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
258	16.15	0.90	0.00	0.90	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
259	16.25	0.91	0.00	0.91	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
260	16.31	0.91	0.00	0.91	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
261	16.39	0.91	0.00	0.91	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
262	16.48	0.92	0.00	0.92	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
263	16.59	0.93	0.00	0.93	0.97	0.263	1.68	0.157	1.00	1.10	2.000	No
264	16.68	0.93	0.00	0.93	0.96	0.263	1.68	0.157	1.00	1.10	2.000	No
265	16.76	0.94	0.00	0.94	0.96	0.263	1.68	0.157	1.00	1.10	2.000	No
266	16.86	0.94	0.00	0.94	0.96	0.263	1.68	0.157	1.00	1.10	2.000	No
267	16.92	0.94	0.00	0.94	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
268	17.02	0.95	0.00	0.95	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
269	17.11	0.96	0.00	0.96	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
270	17.22	0.96	0.00	0.96	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
271	17.35	0.97	0.00	0.97	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
272	17.45	0.97	0.00	0.97	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
273	17.55	0.98	0.00	0.98	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
274	17.61	0.98	0.00	0.98	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
275	17.64	0.99	0.00	0.99	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
276	17.70	0.99	0.00	0.99	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
277	17.75	0.99	0.00	0.99	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
278	17.80	1.00	0.00	1.00	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
279	17.85	1.00	0.00	1.00	0.96	0.263	1.68	0.156	1.00	1.10	2.000	Yes
280	17.94	1.00	0.00	1.00	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
281	17.99	1.01	0.00	1.01	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
282	18.09	1.01	0.00	1.01	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
283	18.15	1.02	0.00	1.02	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
284	18.23	1.02	0.00	1.02	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
285	18.33	1.03	0.00	1.03	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
286	18.43	1.03	0.00	1.03	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
287	18.52	1.04	0.00	1.04	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
288	18.59	1.04	0.00	1.04	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	18.72	1.05	0.00	1.05	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
290	18.81	1.05	0.00	1.05	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
291	18.87	1.06	0.00	1.06	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
292	18.95	1.06	0.00	1.06	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
293	19.05	1.07	0.00	1.07	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
294	19.14	1.07	0.00	1.07	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
295	19.22	1.08	0.00	1.08	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
296	19.29	1.08	0.00	1.08	0.96	0.262	1.68	0.156	1.00	1.10	2.000	Yes
297	19.38	1.09	0.00	1.09	0.96	0.262	1.68	0.156	0.99	1.10	2.000	Yes
298	19.44	1.09	0.00	1.09	0.96	0.262	1.68	0.156	0.99	1.10	2.000	Yes
299	19.53	1.09	0.00	1.09	0.96	0.262	1.68	0.155	0.99	1.10	2.000	Yes
300	19.62	1.10	0.00	1.10	0.96	0.261	1.68	0.155	0.99	1.10	2.000	Yes
301	19.69	1.10	0.00	1.10	0.96	0.261	1.68	0.155	0.99	1.10	2.000	Yes
302	19.79	1.11	0.00	1.11	0.96	0.261	1.68	0.155	0.99	1.10	2.000	No
303	19.86	1.11	0.00	1.11	0.96	0.261	1.68	0.155	0.99	1.10	2.000	No
304	19.97	1.12	0.00	1.12	0.96	0.261	1.68	0.155	0.99	1.10	2.000	No
305	20.07	1.13	0.00	1.13	0.96	0.261	1.68	0.155	0.99	1.10	2.000	No
306	20.16	1.13	0.00	1.13	0.96	0.261	1.68	0.155	0.99	1.10	2.000	No
307	20.26	1.14	0.00	1.14	0.96	0.261	1.68	0.155	0.99	1.10	2.000	Yes
308	20.34	1.14	0.00	1.14	0.96	0.261	1.68	0.155	0.98	1.10	2.000	Yes
309	20.43	1.15	0.00	1.15	0.96	0.261	1.68	0.155	0.98	1.10	2.000	Yes
310	20.50	1.15	0.00	1.15	0.96	0.261	1.68	0.155	0.98	1.10	2.000	Yes
311	20.60	1.16	0.00	1.16	0.96	0.261	1.68	0.155	0.98	1.10	2.000	Yes
312	20.62	1.16	0.00	1.16	0.96	0.261	1.68	0.155	0.98	1.10	2.000	Yes
313	20.63	1.16	0.00	1.16	0.96	0.261	1.68	0.155	0.98	1.10	2.000	Yes
314	20.68	1.16	0.00	1.16	0.96	0.261	1.68	0.155	0.98	1.10	2.000	Yes
315	20.73	1.17	0.00	1.17	0.95	0.261	1.68	0.155	0.98	1.10	2.000	Yes
316	20.82	1.17	0.00	1.17	0.95	0.261	1.68	0.155	0.98	1.10	2.000	Yes
317	20.87	1.17	0.00	1.17	0.95	0.261	1.68	0.155	0.98	1.10	2.000	Yes
318	20.91	1.18	0.00	1.18	0.95	0.261	1.68	0.155	0.98	1.10	2.000	Yes
319	20.96	1.18	0.00	1.18	0.95	0.261	1.68	0.155	0.98	1.10	2.000	Yes
320	21.05	1.19	0.00	1.19	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
321	21.11	1.19	0.00	1.19	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
322	21.17	1.19	0.00	1.19	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
323	21.25	1.20	0.00	1.20	0.95	0.260	1.68	0.155	0.98	1.10	2.000	Yes
324	21.30	1.20	0.00	1.20	0.95	0.260	1.68	0.155	0.98	1.10	2.000	Yes
325	21.37	1.20	0.00	1.20	0.95	0.260	1.68	0.155	0.97	1.10	2.000	Yes
326	21.45	1.21	0.00	1.21	0.95	0.260	1.68	0.155	0.97	1.10	2.000	Yes
327	21.49	1.21	0.00	1.21	0.95	0.260	1.68	0.155	0.97	1.10	2.000	Yes
328	21.58	1.22	0.00	1.22	0.95	0.260	1.68	0.155	0.97	1.10	2.000	Yes
329	21.64	1.22	0.00	1.22	0.95	0.260	1.68	0.155	0.97	1.10	2.000	Yes
330	21.69	1.22	0.00	1.22	0.95	0.260	1.68	0.155	0.97	1.10	2.000	Yes
331	21.78	1.23	0.00	1.23	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
332	21.83	1.23	0.00	1.23	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
333	21.89	1.24	0.00	1.24	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
334	21.98	1.24	0.00	1.24	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
335	22.03	1.25	0.00	1.25	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
336	22.12	1.25	0.00	1.25	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	22.22	1.26	0.00	1.26	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
338	22.26	1.26	0.00	1.26	0.95	0.260	1.68	0.154	0.97	1.10	2.000	No
339	22.36	1.27	0.00	1.27	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
340	22.41	1.27	0.00	1.27	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
341	22.51	1.28	0.00	1.28	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
342	22.60	1.28	0.00	1.28	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
343	22.70	1.29	0.00	1.29	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
344	22.75	1.29	0.00	1.29	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
345	22.84	1.30	0.00	1.30	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
346	22.89	1.30	0.00	1.30	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
347	22.90	1.30	0.00	1.30	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
348	22.94	1.30	0.00	1.30	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
349	23.00	1.31	0.00	1.31	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
350	23.08	1.31	0.00	1.31	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
351	23.13	1.31	0.00	1.31	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
352	23.20	1.32	0.00	1.32	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
353	23.27	1.32	0.00	1.32	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
354	23.33	1.33	0.00	1.33	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
355	23.42	1.33	0.00	1.33	0.95	0.259	1.68	0.154	0.95	1.10	2.000	No
356	23.48	1.34	0.00	1.34	0.95	0.259	1.68	0.154	0.95	1.10	2.000	No
357	23.57	1.34	0.00	1.34	0.95	0.258	1.68	0.154	0.95	1.10	2.000	No
358	23.61	1.34	0.00	1.34	0.95	0.258	1.68	0.154	0.95	1.10	2.000	No
359	23.66	1.35	0.00	1.35	0.95	0.258	1.68	0.154	0.95	1.10	2.000	No
360	23.73	1.35	0.00	1.35	0.95	0.258	1.68	0.154	0.95	1.10	2.000	No
361	23.80	1.36	0.00	1.36	0.95	0.258	1.68	0.153	0.95	1.10	2.000	No
362	23.85	1.36	0.00	1.36	0.95	0.258	1.68	0.153	0.95	1.10	2.000	No
363	23.94	1.36	0.00	1.36	0.95	0.258	1.68	0.153	0.95	1.10	2.000	No
364	24.00	1.37	0.00	1.37	0.95	0.258	1.68	0.153	0.95	1.10	2.000	No
365	24.09	1.37	0.00	1.37	0.94	0.258	1.68	0.153	0.95	1.10	2.000	No
366	24.16	1.38	0.00	1.38	0.94	0.258	1.68	0.153	0.95	1.10	2.000	No
367	24.24	1.38	0.00	1.38	0.94	0.258	1.68	0.153	0.95	1.10	2.000	No
368	24.33	1.39	0.00	1.39	0.94	0.258	1.68	0.153	0.95	1.10	2.000	No
369	24.43	1.40	0.00	1.40	0.94	0.258	1.68	0.153	0.95	1.10	2.000	No
370	24.52	1.40	0.00	1.40	0.94	0.258	1.68	0.153	0.95	1.10	2.000	No
371	24.58	1.40	0.00	1.40	0.94	0.258	1.68	0.153	0.94	1.10	2.000	No
372	24.59	1.40	0.00	1.40	0.94	0.258	1.68	0.153	0.94	1.10	2.000	No
373	24.63	1.41	0.00	1.41	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
374	24.68	1.41	0.00	1.41	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
375	24.77	1.42	0.00	1.42	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
376	24.82	1.42	0.00	1.42	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
377	24.92	1.42	0.00	1.42	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
378	25.01	1.43	0.00	1.43	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
379	25.06	1.43	0.00	1.43	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
380	25.16	1.44	0.00	1.44	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
381	25.25	1.45	0.00	1.45	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
382	25.30	1.45	0.00	1.45	0.94	0.257	1.68	0.153	0.94	1.10	2.000	No
383	25.41	1.45	0.00	1.45	0.94	0.257	1.68	0.153	0.94	1.10	2.000	Yes
384	25.49	1.46	0.00	1.46	0.94	0.257	1.68	0.153	0.94	1.10	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	25.55	1.46	0.00	1.46	0.94	0.257	1.68	0.153	0.94	1.10	2.000	Yes
386	25.64	1.47	0.00	1.47	0.94	0.256	1.68	0.152	0.94	1.10	2.000	Yes
387	25.70	1.47	0.00	1.47	0.94	0.256	1.68	0.152	0.94	1.10	2.000	Yes
388	25.79	1.48	0.00	1.48	0.94	0.256	1.68	0.152	0.94	1.10	2.000	Yes
389	25.89	1.48	0.00	1.48	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
390	25.94	1.49	0.00	1.49	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
391	26.02	1.49	0.00	1.49	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
392	26.12	1.50	0.00	1.50	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
393	26.17	1.50	0.00	1.50	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
394	26.28	1.51	0.00	1.51	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
395	26.36	1.51	0.00	1.51	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
396	26.45	1.52	0.00	1.52	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
397	26.50	1.52	0.00	1.52	0.94	0.256	1.68	0.152	0.93	1.10	2.000	Yes
398	26.61	1.53	0.00	1.53	0.94	0.255	1.68	0.152	0.93	1.10	2.000	Yes
399	26.70	1.53	0.00	1.53	0.94	0.255	1.68	0.152	0.93	1.10	2.000	No
400	26.77	1.54	0.00	1.54	0.94	0.255	1.68	0.152	0.93	1.10	2.000	No
401	26.85	1.54	0.00	1.54	0.93	0.255	1.68	0.152	0.93	1.10	2.000	No
402	26.94	1.54	0.00	1.54	0.93	0.255	1.68	0.152	0.93	1.10	2.000	No
403	27.04	1.55	0.00	1.55	0.93	0.255	1.68	0.152	0.93	1.10	2.000	No
404	27.14	1.56	0.00	1.56	0.93	0.255	1.68	0.152	0.93	1.10	2.000	No
405	27.23	1.56	0.00	1.56	0.93	0.255	1.68	0.151	0.93	1.10	2.000	No
406	27.28	1.56	0.00	1.56	0.93	0.255	1.68	0.151	0.92	1.10	2.000	No
407	27.29	1.56	0.00	1.56	0.93	0.255	1.68	0.151	0.92	1.10	2.000	No
408	27.38	1.57	0.00	1.57	0.93	0.255	1.68	0.151	0.92	1.10	2.000	No
409	27.48	1.57	0.00	1.57	0.93	0.255	1.68	0.151	0.92	1.10	2.000	No
410	27.57	1.58	0.00	1.58	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
411	27.64	1.58	0.00	1.58	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
412	27.65	1.58	0.00	1.58	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
413	27.74	1.59	0.00	1.59	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
414	27.80	1.59	0.00	1.59	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
415	27.90	1.60	0.00	1.60	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
416	27.99	1.60	0.00	1.60	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
417	28.07	1.61	0.00	1.61	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
418	28.16	1.61	0.00	1.61	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
419	28.25	1.62	0.00	1.62	0.93	0.254	1.68	0.151	0.92	1.10	2.000	No
420	28.34	1.62	0.00	1.62	0.93	0.253	1.68	0.151	0.92	1.10	2.000	No
421	28.44	1.63	0.00	1.63	0.93	0.253	1.68	0.151	0.92	1.10	2.000	No
422	28.53	1.63	0.00	1.63	0.93	0.253	1.68	0.151	0.92	1.10	2.000	No
423	28.62	1.64	0.00	1.64	0.93	0.253	1.68	0.150	0.92	1.10	2.000	No
424	28.76	1.65	0.00	1.65	0.93	0.253	1.68	0.150	0.92	1.10	2.000	No
425	28.86	1.65	0.00	1.65	0.93	0.253	1.68	0.150	0.91	1.10	2.000	No
426	28.96	1.66	0.00	1.66	0.93	0.253	1.68	0.150	0.91	1.10	2.000	No
427	29.08	1.66	0.00	1.66	0.93	0.253	1.68	0.150	0.91	1.10	2.000	No
428	29.19	1.67	0.00	1.67	0.92	0.252	1.68	0.150	0.91	1.10	2.000	No
429	29.29	1.68	0.00	1.68	0.92	0.252	1.68	0.150	0.91	1.10	2.000	No
430	29.39	1.68	0.00	1.68	0.92	0.252	1.68	0.150	0.91	1.10	2.000	No
431	29.50	1.69	0.00	1.69	0.92	0.252	1.68	0.150	0.91	1.10	2.000	No
432	29.63	1.70	0.00	1.70	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	29.65	1.70	0.00	1.70	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
434	29.66	1.70	0.00	1.70	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
435	29.72	1.70	0.00	1.70	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
436	29.80	1.71	0.00	1.71	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
437	29.85	1.71	0.00	1.71	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
438	29.94	1.72	0.00	1.72	0.92	0.251	1.68	0.149	0.91	1.10	2.000	Yes
439	30.00	1.72	0.00	1.72	0.92	0.251	1.68	0.149	0.91	1.10	2.000	Yes
440	30.05	1.72	0.00	1.72	0.92	0.251	1.68	0.149	0.91	1.10	2.000	Yes
441	30.14	1.73	0.00	1.73	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
442	30.19	1.73	0.01	1.73	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
443	30.24	1.74	0.01	1.73	0.92	0.252	1.68	0.150	0.91	1.10	2.000	Yes
444	30.29	1.74	0.01	1.73	0.92	0.252	1.68	0.150	0.91	1.10	0.182	No
445	30.38	1.75	0.01	1.73	0.92	0.252	1.68	0.150	0.91	1.10	0.182	No
446	30.43	1.75	0.01	1.74	0.92	0.253	1.68	0.150	0.91	1.10	0.182	No
447	30.48	1.75	0.01	1.74	0.92	0.253	1.68	0.150	0.91	1.10	0.183	No
448	30.54	1.76	0.02	1.74	0.92	0.253	1.68	0.150	0.91	1.10	0.183	No
449	30.62	1.76	0.02	1.74	0.92	0.253	1.68	0.151	0.91	1.10	0.183	No
450	30.67	1.76	0.02	1.74	0.92	0.253	1.68	0.151	0.91	1.10	0.183	No
451	30.72	1.77	0.02	1.74	0.92	0.254	1.68	0.151	0.90	1.10	0.183	No
452	30.76	1.77	0.02	1.75	0.92	0.254	1.68	0.151	0.90	1.10	0.183	No
453	30.86	1.78	0.03	1.75	0.92	0.254	1.68	0.151	0.90	1.10	0.184	No
454	30.91	1.78	0.03	1.75	0.92	0.254	1.68	0.151	0.90	1.10	0.184	No
455	30.95	1.78	0.03	1.75	0.92	0.254	1.68	0.151	0.90	1.10	0.184	No
456	31.03	1.79	0.03	1.75	0.92	0.254	1.68	0.151	0.90	1.10	0.184	No
457	31.10	1.79	0.03	1.76	0.91	0.255	1.68	0.151	0.90	1.10	0.184	No
458	31.15	1.79	0.04	1.76	0.91	0.255	1.68	0.151	0.90	1.10	0.184	No
459	31.20	1.80	0.04	1.76	0.91	0.255	1.68	0.152	0.90	1.10	0.185	No
460	31.26	1.80	0.04	1.76	0.91	0.255	1.68	0.152	0.90	1.10	0.185	No
461	31.34	1.81	0.04	1.76	0.91	0.255	1.68	0.152	0.90	1.10	0.185	No
462	31.37	1.81	0.04	1.77	0.91	0.255	1.68	0.152	0.90	1.10	0.185	No
463	31.38	1.81	0.04	1.77	0.91	0.255	1.68	0.152	0.90	1.10	0.185	No
464	31.43	1.81	0.04	1.77	0.91	0.256	1.68	0.152	0.90	1.10	0.185	No
465	31.47	1.81	0.05	1.77	0.91	0.256	1.68	0.152	0.90	1.10	0.185	No
466	31.55	1.82	0.05	1.77	0.91	0.256	1.68	0.152	0.90	1.10	0.185	No
467	31.59	1.82	0.05	1.77	0.91	0.256	1.68	0.152	0.90	1.10	0.186	No
468	31.66	1.83	0.05	1.77	0.91	0.256	1.68	0.152	0.90	1.10	0.186	No
469	31.73	1.83	0.05	1.78	0.91	0.256	1.68	0.152	0.90	1.10	0.186	No
470	31.78	1.83	0.06	1.78	0.91	0.256	1.68	0.152	0.90	1.10	0.186	No
471	31.84	1.84	0.06	1.78	0.91	0.257	1.68	0.153	0.90	1.10	0.186	No
472	31.93	1.84	0.06	1.78	0.91	0.257	1.68	0.153	0.90	1.10	0.186	No
473	31.98	1.85	0.06	1.78	0.91	0.257	1.68	0.153	0.90	1.10	0.187	No
474	32.02	1.85	0.06	1.79	0.91	0.257	1.68	0.153	0.90	1.10	0.187	No
475	32.09	1.85	0.07	1.79	0.91	0.257	1.68	0.153	0.90	1.10	0.187	No
476	32.16	1.86	0.07	1.79	0.91	0.257	1.68	0.153	0.90	1.10	0.187	No
477	32.22	1.86	0.07	1.79	0.91	0.258	1.68	0.153	0.90	1.10	0.187	No
478	32.27	1.86	0.07	1.79	0.91	0.258	1.68	0.153	0.90	1.10	0.187	No
479	32.34	1.87	0.07	1.80	0.91	0.258	1.68	0.153	0.90	1.10	0.187	No
480	32.42	1.87	0.08	1.80	0.91	0.258	1.68	0.153	0.90	1.10	0.188	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	32.46	1.88	0.08	1.80	0.91	0.258	1.68	0.153	0.90	1.10	0.188	No
482	32.54	1.88	0.08	1.80	0.91	0.258	1.68	0.154	0.90	1.10	0.188	No
483	32.60	1.89	0.08	1.80	0.91	0.259	1.68	0.154	0.90	1.10	0.188	No
484	32.67	1.89	0.08	1.81	0.91	0.259	1.68	0.154	0.90	1.10	0.188	No
485	32.75	1.89	0.09	1.81	0.91	0.259	1.68	0.154	0.90	1.10	0.188	No
486	32.81	1.90	0.09	1.81	0.90	0.259	1.68	0.154	0.90	1.10	0.189	No
487	32.89	1.90	0.09	1.81	0.90	0.259	1.68	0.154	0.90	1.10	0.189	No
488	32.94	1.91	0.09	1.82	0.90	0.259	1.68	0.154	0.90	1.10	0.189	No
489	32.95	1.91	0.09	1.82	0.90	0.259	1.68	0.154	0.90	1.10	0.189	No
490	33.00	1.91	0.09	1.82	0.90	0.259	1.68	0.154	0.90	1.10	0.189	No
491	33.06	1.91	0.10	1.82	0.90	0.260	1.68	0.154	0.90	1.10	0.189	No
492	33.11	1.92	0.10	1.82	0.90	0.260	1.68	0.154	0.90	1.10	0.189	No
493	33.20	1.92	0.10	1.82	0.90	0.260	1.68	0.154	0.90	1.10	0.189	No
494	33.25	1.93	0.10	1.83	0.90	0.260	1.68	0.155	0.90	1.10	0.190	No
495	33.34	1.93	0.10	1.83	0.90	0.260	1.68	0.155	0.90	1.10	0.190	No
496	33.38	1.94	0.11	1.83	0.90	0.260	1.68	0.155	0.90	1.10	0.190	No
497	33.48	1.94	0.11	1.83	0.90	0.260	1.68	0.155	0.90	1.10	0.190	No
498	33.58	1.95	0.11	1.84	0.90	0.261	1.68	0.155	0.90	1.10	0.190	No
499	33.63	1.95	0.11	1.84	0.90	0.261	1.68	0.155	0.90	1.10	0.190	No
500	33.73	1.96	0.12	1.84	0.90	0.261	1.68	0.155	0.90	1.10	0.191	No
501	33.82	1.96	0.12	1.84	0.90	0.261	1.68	0.155	0.89	1.10	0.191	No
502	33.87	1.97	0.12	1.85	0.90	0.261	1.68	0.155	0.89	1.10	0.191	No
503	33.96	1.97	0.12	1.85	0.90	0.261	1.68	0.155	0.89	1.10	0.191	No
504	34.02	1.98	0.13	1.85	0.90	0.262	1.68	0.155	0.89	1.10	0.191	No
505	34.11	1.98	0.13	1.85	0.90	0.262	1.68	0.156	0.89	1.10	0.191	No
506	34.18	1.99	0.13	1.86	0.90	0.262	1.68	0.156	0.89	1.10	0.192	No
507	34.26	1.99	0.13	1.86	0.90	0.262	1.68	0.156	0.89	1.10	0.192	No
508	34.35	2.00	0.14	1.86	0.90	0.262	1.68	0.156	0.89	1.10	0.192	No
509	34.44	2.00	0.14	1.87	0.89	0.262	1.68	0.156	0.89	1.10	0.192	No
510	34.49	2.01	0.14	1.87	0.89	0.262	1.68	0.156	0.89	1.10	0.192	No
511	34.59	2.01	0.14	1.87	0.89	0.263	1.68	0.156	0.89	1.10	0.192	No
512	34.69	2.02	0.15	1.87	0.89	0.263	1.68	0.156	0.89	1.10	0.193	No
513	34.76	2.03	0.15	1.88	0.89	0.263	1.68	0.156	0.89	1.10	0.193	No
514	34.83	2.03	0.15	1.88	0.89	0.263	1.68	0.156	0.89	1.10	0.193	No
515	34.93	2.04	0.15	1.88	0.89	0.263	1.68	0.156	0.89	1.10	0.193	No
516	35.02	2.04	0.16	1.89	0.89	0.263	1.68	0.157	0.89	1.10	0.193	No
517	35.12	2.05	0.16	1.89	0.89	0.263	1.68	0.157	0.89	1.10	0.193	No
518	35.22	2.06	0.16	1.89	0.89	0.264	1.68	0.157	0.89	1.10	0.194	No
519	35.30	2.06	0.17	1.90	0.89	0.264	1.68	0.157	0.89	1.10	0.194	No
520	35.38	2.07	0.17	1.90	0.89	0.264	1.68	0.157	0.89	1.10	0.194	No
521	35.43	2.07	0.17	1.90	0.89	0.264	1.68	0.157	0.89	1.10	0.194	No
522	35.46	2.07	0.17	1.90	0.89	0.264	1.68	0.157	0.89	1.10	0.194	No
523	35.51	2.08	0.17	1.90	0.89	0.264	1.68	0.157	0.89	1.10	2.000	Yes
524	35.56	2.08	0.17	1.90	0.89	0.264	1.68	0.157	0.89	1.10	2.000	Yes
525	35.66	2.08	0.18	1.91	0.89	0.264	1.68	0.157	0.89	1.10	2.000	Yes
526	35.70	2.09	0.18	1.91	0.89	0.264	1.68	0.157	0.89	1.10	2.000	Yes
527	35.80	2.09	0.18	1.91	0.88	0.264	1.68	0.157	0.89	1.10	2.000	Yes
528	35.89	2.10	0.18	1.92	0.88	0.265	1.68	0.157	0.89	1.10	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	35.96	2.10	0.19	1.92	0.88	0.265	1.68	0.157	0.89	1.10	2.000	Yes
530	36.04	2.11	0.19	1.92	0.88	0.265	1.68	0.157	0.89	1.10	2.000	Yes
531	36.14	2.12	0.19	1.92	0.88	0.265	1.68	0.157	0.89	1.10	2.000	Yes
532	36.19	2.12	0.19	1.93	0.88	0.265	1.68	0.157	0.89	1.10	2.000	Yes
533	36.28	2.12	0.20	1.93	0.88	0.265	1.68	0.158	0.89	1.10	2.000	Yes
534	36.33	2.13	0.20	1.93	0.88	0.265	1.68	0.158	0.89	1.10	0.195	No
535	36.42	2.13	0.20	1.93	0.88	0.265	1.68	0.158	0.89	1.10	0.196	No
536	36.48	2.14	0.20	1.93	0.88	0.265	1.68	0.158	0.89	1.10	0.196	No
537	36.52	2.14	0.20	1.94	0.88	0.265	1.68	0.158	0.89	1.10	0.196	No
538	36.62	2.14	0.21	1.94	0.88	0.265	1.68	0.158	0.89	1.10	0.196	No
539	36.68	2.15	0.21	1.94	0.88	0.266	1.68	0.158	0.89	1.10	0.196	No
540	36.77	2.15	0.21	1.94	0.88	0.266	1.68	0.158	0.89	1.10	0.196	No
541	36.86	2.16	0.21	1.95	0.88	0.266	1.68	0.158	0.89	1.10	2.000	Yes
542	36.90	2.16	0.22	1.95	0.88	0.266	1.68	0.158	0.89	1.10	2.000	Yes
543	37.00	2.17	0.22	1.95	0.88	0.266	1.68	0.158	0.88	1.10	2.000	Yes
544	37.10	2.17	0.22	1.95	0.88	0.266	1.68	0.158	0.88	1.10	2.000	Yes
545	37.20	2.18	0.22	1.96	0.87	0.266	1.68	0.158	0.88	1.10	2.000	Yes
546	37.29	2.19	0.23	1.96	0.87	0.266	1.68	0.158	0.88	1.10	2.000	Yes
547	37.39	2.19	0.23	1.96	0.87	0.266	1.68	0.158	0.88	1.10	2.000	Yes
548	37.49	2.20	0.23	1.97	0.87	0.266	1.68	0.158	0.88	1.10	0.197	No
549	37.53	2.20	0.24	1.97	0.87	0.266	1.68	0.158	0.88	1.10	0.197	No
550	37.58	2.21	0.24	1.97	0.87	0.266	1.68	0.158	0.88	1.10	0.197	No
551	37.62	2.21	0.24	1.97	0.87	0.266	1.68	0.158	0.88	1.10	0.197	No
552	37.69	2.21	0.24	1.97	0.87	0.267	1.68	0.158	0.88	1.10	0.197	No
553	37.77	2.22	0.24	1.98	0.87	0.267	1.68	0.158	0.88	1.10	0.198	No
554	37.82	2.22	0.24	1.98	0.87	0.267	1.68	0.158	0.88	1.10	0.198	No
555	37.87	2.22	0.25	1.98	0.87	0.267	1.68	0.159	0.88	1.10	0.198	No
556	37.91	2.23	0.25	1.98	0.87	0.267	1.68	0.159	0.88	1.10	0.198	No
557	37.97	2.23	0.25	1.98	0.87	0.267	1.68	0.159	0.88	1.10	0.198	No
558	38.06	2.24	0.25	1.99	0.87	0.267	1.68	0.159	0.88	1.10	0.198	No
559	38.10	2.24	0.25	1.99	0.87	0.267	1.68	0.159	0.88	1.10	0.198	No
560	38.17	2.24	0.25	1.99	0.87	0.267	1.68	0.159	0.88	1.10	0.198	No
561	38.25	2.25	0.26	1.99	0.87	0.267	1.68	0.159	0.88	1.10	0.198	No
562	38.35	2.26	0.26	2.00	0.87	0.267	1.68	0.159	0.88	1.10	0.198	No
563	38.40	2.26	0.26	2.00	0.86	0.267	1.68	0.159	0.88	1.10	0.198	No
564	38.46	2.26	0.26	2.00	0.86	0.267	1.68	0.159	0.88	1.10	0.198	No
565	38.54	2.27	0.27	2.00	0.86	0.267	1.68	0.159	0.88	1.10	0.198	No
566	38.60	2.27	0.27	2.00	0.86	0.267	1.68	0.159	0.88	1.10	0.198	No
567	38.69	2.28	0.27	2.01	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
568	38.74	2.28	0.27	2.01	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
569	38.83	2.29	0.28	2.01	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
570	38.88	2.29	0.28	2.01	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
571	38.97	2.30	0.28	2.02	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
572	39.02	2.30	0.28	2.02	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
573	39.11	2.31	0.28	2.02	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
574	39.16	2.31	0.29	2.02	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
575	39.23	2.31	0.29	2.03	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
576	39.24	2.31	0.29	2.03	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	39.28	2.32	0.29	2.03	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
578	39.32	2.32	0.29	2.03	0.86	0.267	1.68	0.159	0.88	1.10	0.199	No
579	39.39	2.32	0.29	2.03	0.86	0.268	1.68	0.159	0.88	1.10	2.000	Yes
580	39.47	2.33	0.30	2.03	0.86	0.268	1.68	0.159	0.88	1.10	2.000	Yes
581	39.54	2.33	0.30	2.04	0.86	0.268	1.68	0.159	0.88	1.10	2.000	Yes
582	39.62	2.34	0.30	2.04	0.85	0.268	1.68	0.159	0.88	1.10	2.000	Yes
583	39.71	2.34	0.30	2.04	0.85	0.268	1.68	0.159	0.88	1.10	2.000	Yes
584	39.76	2.35	0.30	2.04	0.85	0.268	1.68	0.159	0.88	1.10	2.000	Yes
585	39.85	2.35	0.31	2.05	0.85	0.268	1.68	0.159	0.88	1.10	2.000	Yes
586	39.90	2.36	0.31	2.05	0.85	0.268	1.68	0.159	0.88	1.10	2.000	Yes
587	40.00	2.36	0.31	2.05	0.85	0.268	1.68	0.159	0.88	1.10	2.000	Yes
588	40.06	2.37	0.31	2.05	0.85	0.268	1.68	0.159	0.88	1.10	2.000	Yes
589	40.15	2.37	0.32	2.05	0.85	0.268	1.68	0.159	0.88	1.10	2.000	Yes
590	40.21	2.38	0.32	2.06	0.85	0.268	1.68	0.159	0.88	1.10	2.000	Yes
591	40.29	2.38	0.32	2.06	0.85	0.268	1.68	0.159	0.88	1.10	2.000	Yes
592	40.35	2.38	0.32	2.06	0.85	0.268	1.68	0.159	0.88	1.10	2.000	Yes
593	40.43	2.39	0.33	2.06	0.85	0.268	1.68	0.159	0.87	1.10	2.000	Yes
594	40.52	2.39	0.33	2.07	0.85	0.268	1.68	0.159	0.87	1.10	2.000	Yes
595	40.58	2.40	0.33	2.07	0.85	0.268	1.68	0.159	0.87	1.10	2.000	Yes
596	40.67	2.40	0.33	2.07	0.85	0.268	1.68	0.159	0.87	1.10	2.000	Yes
597	40.77	2.41	0.34	2.07	0.84	0.268	1.68	0.159	0.87	1.10	2.000	Yes
598	40.84	2.41	0.34	2.08	0.84	0.268	1.68	0.159	0.87	1.10	2.000	Yes
599	40.89	2.42	0.34	2.08	0.84	0.268	1.68	0.159	0.87	1.10	2.000	Yes
600	40.94	2.42	0.34	2.08	0.84	0.268	1.68	0.159	0.87	1.10	2.000	Yes
601	41.03	2.43	0.34	2.08	0.84	0.268	1.68	0.159	0.87	1.10	2.000	Yes
602	41.08	2.43	0.35	2.08	0.84	0.268	1.68	0.159	0.87	1.10	2.000	Yes
603	41.14	2.43	0.35	2.09	0.84	0.268	1.68	0.159	0.87	1.10	2.000	Yes
604	41.22	2.44	0.35	2.09	0.84	0.268	1.68	0.159	0.87	1.10	2.000	Yes
605	41.28	2.44	0.35	2.09	0.84	0.268	1.68	0.159	0.87	1.10	0.201	No
606	41.33	2.44	0.35	2.09	0.84	0.268	1.68	0.159	0.87	1.10	0.201	No
607	41.42	2.45	0.36	2.09	0.84	0.268	1.68	0.159	0.87	1.10	0.201	No
608	41.47	2.45	0.36	2.10	0.84	0.268	1.68	0.159	0.87	1.10	0.201	No
609	41.52	2.46	0.36	2.10	0.84	0.268	1.68	0.159	0.87	1.10	0.201	No
610	41.62	2.46	0.36	2.10	0.84	0.268	1.68	0.159	0.87	1.10	0.201	No
611	41.67	2.47	0.36	2.10	0.84	0.268	1.68	0.159	0.87	1.10	0.201	No
612	41.76	2.47	0.37	2.10	0.84	0.268	1.68	0.159	0.87	1.10	0.201	No
613	41.82	2.48	0.37	2.11	0.83	0.268	1.68	0.159	0.87	1.10	0.201	No
614	41.90	2.48	0.37	2.11	0.83	0.268	1.68	0.159	0.87	1.10	0.201	No
615	41.99	2.49	0.37	2.11	0.83	0.268	1.68	0.159	0.87	1.10	0.201	No
616	42.05	2.49	0.38	2.11	0.83	0.268	1.68	0.159	0.87	1.10	0.201	No
617	42.15	2.50	0.38	2.12	0.83	0.268	1.68	0.159	0.87	1.10	0.201	No
618	42.23	2.50	0.38	2.12	0.83	0.268	1.68	0.159	0.87	1.10	0.201	No
619	42.30	2.51	0.38	2.12	0.83	0.268	1.68	0.159	0.87	1.10	0.201	No
620	42.38	2.51	0.39	2.13	0.83	0.268	1.68	0.159	0.87	1.10	0.201	No
621	42.48	2.52	0.39	2.13	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
622	42.57	2.52	0.39	2.13	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
623	42.64	2.53	0.39	2.13	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
624	42.72	2.53	0.40	2.14	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	42.82	2.54	0.40	2.14	0.83	0.267	1.68	0.159	0.87	1.10	0.201	No
626	42.90	2.55	0.40	2.14	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
627	42.97	2.55	0.40	2.15	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
628	43.06	2.56	0.41	2.15	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
629	43.15	2.56	0.41	2.15	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
630	43.20	2.56	0.41	2.15	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
631	43.30	2.57	0.41	2.16	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
632	43.40	2.58	0.42	2.16	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
633	43.48	2.58	0.42	2.16	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
634	43.51	2.58	0.42	2.16	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
635	43.52	2.58	0.42	2.16	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
636	43.56	2.59	0.42	2.16	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
637	43.61	2.59	0.42	2.17	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
638	43.67	2.59	0.43	2.17	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
639	43.72	2.60	0.43	2.17	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
640	43.80	2.60	0.43	2.17	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
641	43.85	2.61	0.43	2.17	0.82	0.267	1.68	0.159	0.87	1.10	0.201	No
642	43.90	2.61	0.43	2.18	0.81	0.267	1.68	0.159	0.87	1.10	0.201	No
643	43.94	2.61	0.43	2.18	0.81	0.267	1.68	0.159	0.87	1.10	0.201	No
644	43.99	2.62	0.44	2.18	0.81	0.267	1.68	0.158	0.87	1.10	0.201	No
645	44.08	2.62	0.44	2.18	0.81	0.267	1.68	0.158	0.87	1.10	0.201	No
646	44.14	2.62	0.44	2.18	0.81	0.267	1.68	0.158	0.87	1.10	0.201	No
647	44.22	2.63	0.44	2.19	0.81	0.266	1.68	0.158	0.86	1.10	0.201	No
648	44.28	2.63	0.45	2.19	0.81	0.266	1.68	0.158	0.86	1.10	0.201	No
649	44.33	2.64	0.45	2.19	0.81	0.266	1.68	0.158	0.86	1.10	0.201	No
650	44.40	2.64	0.45	2.19	0.81	0.266	1.68	0.158	0.86	1.10	0.201	No
651	44.48	2.65	0.45	2.20	0.81	0.266	1.68	0.158	0.86	1.10	0.201	No
652	44.52	2.65	0.45	2.20	0.81	0.266	1.68	0.158	0.86	1.10	0.201	No
653	44.61	2.66	0.46	2.20	0.81	0.266	1.68	0.158	0.86	1.10	0.201	No
654	44.72	2.66	0.46	2.20	0.81	0.266	1.68	0.158	0.86	1.10	0.201	No
655	44.77	2.67	0.46	2.21	0.81	0.266	1.68	0.158	0.86	1.10	0.201	No
656	44.91	2.67	0.47	2.21	0.80	0.266	1.68	0.158	0.86	1.10	0.201	No
657	44.95	2.68	0.47	2.21	0.80	0.266	1.68	0.158	0.86	1.10	0.201	No
658	45.02	2.68	0.47	2.21	0.80	0.266	1.68	0.158	0.86	1.10	0.201	No
659	45.04	2.68	0.47	2.21	0.80	0.266	1.68	0.158	0.86	1.10	0.201	No
660	45.06	2.69	0.47	2.22	0.80	0.266	1.68	0.158	0.86	1.10	0.201	No
661	45.11	2.69	0.47	2.22	0.80	0.266	1.68	0.158	0.86	1.10	0.201	No
662	45.15	2.69	0.47	2.22	0.80	0.266	1.68	0.158	0.86	1.10	0.201	No
663	45.21	2.69	0.47	2.22	0.80	0.266	1.68	0.158	0.86	1.10	0.201	No
664	45.25	2.70	0.48	2.22	0.80	0.266	1.68	0.158	0.86	1.10	0.201	No
665	45.30	2.70	0.48	2.22	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
666	45.35	2.70	0.48	2.23	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
667	45.41	2.71	0.48	2.23	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
668	45.49	2.71	0.48	2.23	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
669	45.55	2.72	0.49	2.23	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
670	45.63	2.72	0.49	2.24	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
671	45.69	2.73	0.49	2.24	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No
672	45.78	2.73	0.49	2.24	0.80	0.265	1.68	0.158	0.86	1.10	0.201	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	45.84	2.74	0.49	2.24	0.80	0.265	1.68	0.157	0.86	1.10	0.201	No
674	45.93	2.74	0.50	2.25	0.79	0.265	1.68	0.157	0.86	1.10	0.201	No
675	46.02	2.75	0.50	2.25	0.79	0.265	1.68	0.157	0.86	1.10	2.000	Yes
676	46.08	2.75	0.50	2.25	0.79	0.265	1.68	0.157	0.86	1.10	2.000	Yes
677	46.16	2.76	0.50	2.25	0.79	0.265	1.68	0.157	0.86	1.10	2.000	Yes
678	46.24	2.76	0.51	2.26	0.79	0.265	1.68	0.157	0.86	1.10	2.000	Yes
679	46.31	2.77	0.51	2.26	0.79	0.264	1.68	0.157	0.86	1.10	2.000	Yes
680	46.41	2.77	0.51	2.26	0.79	0.264	1.68	0.157	0.86	1.10	2.000	Yes
681	46.48	2.78	0.51	2.26	0.79	0.264	1.68	0.157	0.86	1.10	2.000	Yes
682	46.56	2.78	0.52	2.27	0.79	0.264	1.68	0.157	0.86	1.10	2.000	Yes
683	46.65	2.79	0.52	2.27	0.79	0.264	1.68	0.157	0.86	1.10	2.000	Yes
684	46.75	2.79	0.52	2.27	0.79	0.264	1.68	0.157	0.86	1.10	2.000	Yes
685	46.84	2.80	0.53	2.27	0.78	0.264	1.68	0.157	0.86	1.10	2.000	Yes
686	46.94	2.81	0.53	2.28	0.78	0.264	1.68	0.157	0.86	1.10	0.201	No
687	47.02	2.81	0.53	2.28	0.78	0.264	1.68	0.157	0.86	1.10	0.201	No
688	47.08	2.81	0.53	2.28	0.78	0.264	1.68	0.157	0.86	1.10	0.201	No
689	47.12	2.82	0.53	2.28	0.78	0.264	1.68	0.157	0.86	1.10	0.201	No
690	47.16	2.82	0.54	2.28	0.78	0.263	1.68	0.157	0.86	1.10	0.201	No
691	47.21	2.82	0.54	2.28	0.78	0.263	1.68	0.157	0.86	1.10	0.201	No
692	47.27	2.82	0.54	2.29	0.78	0.263	1.68	0.157	0.86	1.10	0.201	No
693	47.35	2.83	0.54	2.29	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
694	47.40	2.83	0.54	2.29	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
695	47.50	2.84	0.55	2.29	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
696	47.55	2.84	0.55	2.29	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
697	47.61	2.84	0.55	2.29	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
698	47.69	2.85	0.55	2.30	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
699	47.76	2.85	0.55	2.30	0.78	0.263	1.68	0.156	0.86	1.10	0.201	No
700	47.83	2.85	0.56	2.30	0.77	0.263	1.68	0.156	0.86	1.10	0.201	No
701	47.93	2.86	0.56	2.30	0.77	0.263	1.68	0.156	0.86	1.10	0.201	No
702	48.02	2.87	0.56	2.30	0.77	0.263	1.68	0.156	0.86	1.10	0.201	No
703	48.09	2.87	0.56	2.30	0.77	0.262	1.68	0.156	0.86	1.10	0.201	No
704	48.18	2.87	0.57	2.31	0.77	0.262	1.68	0.156	0.86	1.10	0.200	No
705	48.27	2.88	0.57	2.31	0.77	0.262	1.68	0.156	0.86	1.10	0.200	No
706	48.37	2.88	0.57	2.31	0.77	0.262	1.68	0.156	0.86	1.10	0.200	No
707	48.46	2.89	0.58	2.31	0.77	0.262	1.68	0.156	0.86	1.10	0.200	No
708	48.52	2.89	0.58	2.31	0.77	0.262	1.68	0.156	0.86	1.10	0.200	No
709	48.60	2.90	0.58	2.32	0.77	0.262	1.68	0.156	0.85	1.10	0.200	No
710	48.70	2.90	0.58	2.32	0.77	0.262	1.68	0.156	0.85	1.10	0.200	No
711	48.79	2.91	0.59	2.32	0.77	0.262	1.68	0.156	0.85	1.10	0.200	No
712	48.85	2.91	0.59	2.32	0.76	0.262	1.68	0.155	0.85	1.10	0.200	No
713	48.94	2.92	0.59	2.32	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
714	49.04	2.92	0.59	2.33	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
715	49.13	2.93	0.60	2.33	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
716	49.23	2.93	0.60	2.33	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
717	49.33	2.94	0.60	2.33	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
718	49.38	2.94	0.60	2.34	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
719	49.42	2.94	0.61	2.34	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
720	49.48	2.95	0.61	2.34	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	49.53	2.95	0.61	2.34	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
722	49.58	2.95	0.61	2.34	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
723	49.63	2.96	0.61	2.34	0.76	0.261	1.68	0.155	0.85	1.10	0.200	No
724	49.72	2.96	0.62	2.35	0.76	0.260	1.68	0.155	0.85	1.10	0.200	No
725	49.77	2.96	0.62	2.35	0.76	0.260	1.68	0.155	0.85	1.10	0.200	No
726	49.83	2.97	0.62	2.35	0.75	0.260	1.68	0.155	0.85	1.10	0.200	No
727	49.92	2.97	0.62	2.35	0.75	0.260	1.68	0.155	0.85	1.10	0.200	No
728	49.97	2.98	0.62	2.35	0.75	0.260	1.68	0.155	0.85	1.10	0.199	No
729	50.04	2.98	0.63	2.36	0.75	0.260	1.68	0.154	0.85	1.10	0.199	No
730	50.11	2.99	0.63	2.36	0.75	0.260	1.68	0.154	0.85	1.10	0.199	No
731	50.20	2.99	0.63	2.36	0.75	0.260	1.68	0.154	0.85	1.10	0.199	No
732	50.27	3.00	0.63	2.36	0.75	0.260	1.68	0.154	0.85	1.10	0.199	No
733	50.34	3.00	0.63	2.36	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
734	50.45	3.01	0.64	2.37	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
735	50.54	3.01	0.64	2.37	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
736	50.59	3.01	0.64	2.37	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
737	50.68	3.02	0.65	2.37	0.75	0.259	1.68	0.154	0.85	1.10	0.199	No
738	50.79	3.03	0.65	2.38	0.74	0.259	1.68	0.154	0.85	1.10	0.199	No
739	50.88	3.03	0.65	2.38	0.74	0.259	1.68	0.154	0.85	1.10	0.199	No
740	50.98	3.04	0.65	2.38	0.74	0.259	1.68	0.154	0.85	1.10	0.199	No
741	51.07	3.04	0.66	2.38	0.74	0.258	1.68	0.154	0.85	1.10	0.199	No
742	51.17	3.05	0.66	2.39	0.74	0.258	1.68	0.153	0.85	1.10	0.199	No
743	51.24	3.05	0.66	2.39	0.74	0.258	1.68	0.153	0.85	1.10	0.199	No
744	51.33	3.06	0.67	2.39	0.74	0.258	1.68	0.153	0.85	1.10	0.199	No
745	51.46	3.06	0.67	2.39	0.74	0.258	1.68	0.153	0.85	1.10	0.198	No
746	51.46	3.06	0.67	2.39	0.74	0.258	1.68	0.153	0.85	1.10	0.198	No
747	51.51	3.07	0.67	2.40	0.74	0.258	1.68	0.153	0.85	1.10	0.198	No
748	51.56	3.07	0.67	2.40	0.74	0.258	1.68	0.153	0.85	1.10	0.198	No
749	51.65	3.07	0.68	2.40	0.74	0.258	1.68	0.153	0.85	1.10	0.198	No
750	51.71	3.08	0.68	2.40	0.74	0.257	1.68	0.153	0.85	1.10	0.198	No
751	51.79	3.08	0.68	2.40	0.73	0.257	1.68	0.153	0.85	1.10	0.198	No
752	51.85	3.09	0.68	2.40	0.73	0.257	1.68	0.153	0.85	1.10	0.198	No
753	51.94	3.09	0.68	2.41	0.73	0.257	1.68	0.153	0.85	1.10	0.198	No
754	51.99	3.09	0.69	2.41	0.73	0.257	1.68	0.153	0.85	1.10	0.198	No
755	52.09	3.10	0.69	2.41	0.73	0.257	1.68	0.153	0.85	1.10	0.198	No
756	52.19	3.11	0.69	2.41	0.73	0.257	1.68	0.153	0.85	1.10	0.198	No
757	52.28	3.11	0.70	2.42	0.73	0.257	1.68	0.152	0.85	1.10	0.198	No
758	52.35	3.12	0.70	2.42	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
759	52.43	3.12	0.70	2.42	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
760	52.52	3.13	0.70	2.42	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
761	52.62	3.13	0.71	2.43	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
762	52.72	3.14	0.71	2.43	0.73	0.256	1.68	0.152	0.85	1.10	0.198	No
763	52.81	3.14	0.71	2.43	0.72	0.256	1.68	0.152	0.85	1.10	0.197	No
764	52.91	3.15	0.71	2.44	0.72	0.255	1.68	0.152	0.85	1.10	0.197	No
765	53.00	3.16	0.72	2.44	0.72	0.255	1.68	0.152	0.85	1.10	0.197	No
766	53.10	3.16	0.72	2.44	0.72	0.255	1.68	0.152	0.85	1.10	2.000	Yes
767	53.20	3.17	0.72	2.45	0.72	0.255	1.68	0.152	0.85	1.10	2.000	Yes
768	53.29	3.18	0.73	2.45	0.72	0.255	1.68	0.151	0.85	1.10	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	53.38	3.18	0.73	2.45	0.72	0.255	1.68	0.151	0.85	1.10	2.000	Yes
770	53.46	3.19	0.73	2.46	0.72	0.254	1.68	0.151	0.85	1.10	2.000	Yes
771	53.53	3.19	0.73	2.46	0.72	0.254	1.68	0.151	0.84	1.10	2.000	Yes
772	53.63	3.20	0.74	2.46	0.72	0.254	1.68	0.151	0.84	1.10	2.000	Yes
773	53.73	3.21	0.74	2.47	0.72	0.254	1.68	0.151	0.84	1.10	2.000	Yes
774	53.82	3.21	0.74	2.47	0.71	0.254	1.68	0.151	0.84	1.10	2.000	Yes
775	53.92	3.22	0.75	2.47	0.71	0.254	1.68	0.151	0.84	1.10	2.000	Yes
776	53.94	3.22	0.75	2.47	0.71	0.254	1.68	0.151	0.84	1.10	0.196	No
777	53.96	3.22	0.75	2.47	0.71	0.254	1.68	0.151	0.84	1.10	0.196	No
778	53.97	3.22	0.75	2.47	0.71	0.254	1.68	0.151	0.84	1.10	0.196	No
779	54.05	3.23	0.75	2.48	0.71	0.253	1.68	0.151	0.84	1.10	0.196	No
780	54.08	3.23	0.75	2.48	0.71	0.253	1.68	0.151	0.84	1.10	0.196	No
781	54.13	3.23	0.75	2.48	0.71	0.253	1.68	0.151	0.84	1.10	0.196	No
782	54.19	3.24	0.75	2.48	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
783	54.25	3.24	0.76	2.48	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
784	54.28	3.24	0.76	2.49	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
785	54.29	3.24	0.76	2.49	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
786	54.34	3.25	0.76	2.49	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
787	54.35	3.25	0.76	2.49	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
788	54.40	3.25	0.76	2.49	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
789	54.44	3.25	0.76	2.49	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
790	54.49	3.26	0.76	2.49	0.71	0.253	1.68	0.150	0.84	1.10	0.196	No
791	54.53	3.26	0.77	2.50	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No
792	54.57	3.26	0.77	2.50	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No
793	54.58	3.26	0.77	2.50	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No
794	54.63	3.27	0.77	2.50	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No
795	54.68	3.27	0.77	2.50	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No
796	54.73	3.27	0.77	2.50	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No
797	54.78	3.28	0.77	2.50	0.71	0.252	1.68	0.150	0.84	1.10	0.196	No
798	54.83	3.28	0.77	2.51	0.70	0.252	1.68	0.150	0.84	1.10	0.196	No
799	54.88	3.28	0.78	2.51	0.70	0.252	1.68	0.150	0.84	1.10	0.196	No
800	54.92	3.29	0.78	2.51	0.70	0.252	1.68	0.150	0.84	1.10	0.196	No
801	54.97	3.29	0.78	2.51	0.70	0.252	1.68	0.150	0.84	1.10	0.196	No
802	55.02	3.29	0.78	2.51	0.70	0.252	1.68	0.150	0.84	1.10	0.196	No
803	55.12	3.30	0.78	2.52	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
804	55.17	3.30	0.79	2.52	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
805	55.25	3.31	0.79	2.52	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
806	55.31	3.31	0.79	2.52	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
807	55.36	3.32	0.79	2.53	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
808	55.45	3.32	0.79	2.53	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
809	55.50	3.33	0.80	2.53	0.70	0.251	1.68	0.149	0.84	1.10	0.195	No
810	55.60	3.33	0.80	2.53	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
811	55.65	3.34	0.80	2.54	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
812	55.71	3.34	0.80	2.54	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
813	55.75	3.34	0.80	2.54	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
814	55.79	3.35	0.80	2.54	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
815	55.84	3.35	0.81	2.54	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No
816	55.89	3.35	0.81	2.55	0.70	0.250	1.68	0.149	0.84	1.10	0.195	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	55.90	3.35	0.81	2.55	0.69	0.250	1.68	0.149	0.84	1.10	0.195	No
818	55.94	3.36	0.81	2.55	0.69	0.250	1.68	0.149	0.84	1.10	0.195	No
819	55.99	3.36	0.81	2.55	0.69	0.250	1.68	0.148	0.84	1.10	0.195	No
820	56.03	3.36	0.81	2.55	0.69	0.250	1.68	0.148	0.84	1.10	0.195	No
821	56.08	3.37	0.81	2.55	0.69	0.250	1.68	0.148	0.84	1.10	0.195	No
822	56.14	3.37	0.82	2.55	0.69	0.249	1.68	0.148	0.84	1.10	0.195	No
823	56.22	3.38	0.82	2.56	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
824	56.28	3.38	0.82	2.56	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
825	56.33	3.38	0.82	2.56	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
826	56.38	3.39	0.82	2.56	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
827	56.45	3.39	0.83	2.56	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
828	56.52	3.39	0.83	2.57	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
829	56.62	3.40	0.83	2.57	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
830	56.66	3.40	0.83	2.57	0.69	0.249	1.68	0.148	0.84	1.10	0.194	No
831	56.73	3.41	0.83	2.57	0.69	0.248	1.68	0.148	0.84	1.10	0.194	No
832	56.81	3.41	0.84	2.58	0.69	0.248	1.68	0.148	0.84	1.10	0.194	No
833	56.95	3.42	0.84	2.58	0.69	0.248	1.68	0.147	0.84	1.10	0.194	No
834	57.00	3.43	0.84	2.58	0.68	0.248	1.68	0.147	0.84	1.10	0.194	No
835	57.09	3.43	0.85	2.59	0.68	0.248	1.68	0.147	0.84	1.10	0.194	No
836	57.19	3.44	0.85	2.59	0.68	0.248	1.68	0.147	0.84	1.10	0.194	No
837	57.27	3.45	0.85	2.59	0.68	0.247	1.68	0.147	0.84	1.10	0.194	No
838	57.35	3.45	0.85	2.60	0.68	0.247	1.68	0.147	0.84	1.10	0.193	No
839	57.44	3.46	0.86	2.60	0.68	0.247	1.68	0.147	0.84	1.10	0.193	No
840	57.50	3.46	0.86	2.60	0.68	0.247	1.68	0.147	0.84	1.10	0.193	No
841	57.52	3.46	0.86	2.60	0.68	0.247	1.68	0.147	0.84	1.10	0.193	No
842	57.58	3.47	0.86	2.60	0.68	0.247	1.68	0.147	0.84	1.10	0.193	No
843	57.63	3.47	0.86	2.61	0.68	0.247	1.68	0.147	0.83	1.10	0.193	No
844	57.72	3.48	0.86	2.61	0.68	0.247	1.68	0.147	0.83	1.10	0.193	No
845	57.77	3.48	0.87	2.61	0.68	0.247	1.68	0.147	0.83	1.10	0.193	No
846	57.82	3.48	0.87	2.61	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
847	57.91	3.49	0.87	2.62	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
848	57.96	3.49	0.87	2.62	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
849	58.02	3.49	0.87	2.62	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
850	58.09	3.50	0.88	2.62	0.68	0.246	1.68	0.146	0.83	1.10	0.193	No
851	58.16	3.50	0.88	2.63	0.67	0.246	1.68	0.146	0.83	1.10	0.193	No
852	58.25	3.51	0.88	2.63	0.67	0.246	1.68	0.146	0.83	1.10	0.193	No
853	58.30	3.51	0.88	2.63	0.67	0.246	1.68	0.146	0.83	1.10	0.193	No
854	58.40	3.52	0.89	2.63	0.67	0.245	1.68	0.146	0.83	1.10	0.193	No
855	58.50	3.53	0.89	2.64	0.67	0.245	1.68	0.146	0.83	1.10	0.192	No
856	58.56	3.53	0.89	2.64	0.67	0.245	1.68	0.146	0.83	1.10	0.192	No
857	58.64	3.54	0.89	2.64	0.67	0.245	1.68	0.146	0.83	1.10	0.192	No
858	58.73	3.54	0.90	2.65	0.67	0.245	1.68	0.146	0.83	1.10	0.192	No
859	58.78	3.55	0.90	2.65	0.67	0.245	1.68	0.145	0.83	1.10	0.192	No
860	58.88	3.55	0.90	2.65	0.67	0.245	1.68	0.145	0.83	1.10	0.192	No
861	58.97	3.56	0.90	2.65	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
862	59.07	3.57	0.91	2.66	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
863	59.13	3.57	0.91	2.66	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No
864	59.23	3.58	0.91	2.66	0.67	0.244	1.68	0.145	0.83	1.10	0.192	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	59.31	3.58	0.91	2.67	0.66	0.244	1.68	0.145	0.83	1.10	0.192	No
866	59.38	3.59	0.92	2.67	0.66	0.244	1.68	0.145	0.83	1.10	0.192	No
867	59.41	3.59	0.92	2.67	0.66	0.244	1.68	0.145	0.83	1.10	0.192	No
868	59.46	3.59	0.92	2.67	0.66	0.244	1.68	0.145	0.83	1.10	0.192	No
869	59.51	3.59	0.92	2.67	0.66	0.243	1.68	0.145	0.83	1.10	0.192	No
870	59.57	3.60	0.92	2.68	0.66	0.243	1.68	0.145	0.83	1.10	0.192	No
871	59.66	3.60	0.93	2.68	0.66	0.243	1.68	0.145	0.83	1.10	0.191	No
872	59.75	3.61	0.93	2.68	0.66	0.243	1.68	0.144	0.83	1.10	0.191	No
873	59.80	3.61	0.93	2.68	0.66	0.243	1.68	0.144	0.83	1.10	0.191	No
874	59.85	3.62	0.93	2.69	0.66	0.243	1.68	0.144	0.83	1.10	0.191	No
875	59.91	3.62	0.93	2.69	0.66	0.243	1.68	0.144	0.83	1.10	0.191	No
876	59.99	3.63	0.94	2.69	0.66	0.243	1.68	0.144	0.83	1.10	0.191	No
877	60.05	3.63	0.94	2.69	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
878	60.09	3.63	0.94	2.69	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
879	60.14	3.64	0.94	2.70	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
880	60.19	3.64	0.94	2.70	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
881	60.22	3.64	0.94	2.70	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
882	60.28	3.65	0.94	2.70	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
883	60.33	3.65	0.95	2.70	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
884	60.38	3.65	0.95	2.71	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
885	60.42	3.66	0.95	2.71	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
886	60.48	3.66	0.95	2.71	0.66	0.242	1.68	0.144	0.83	1.10	0.191	No
887	60.57	3.67	0.95	2.71	0.65	0.242	1.68	0.144	0.83	1.10	0.191	No
888	60.66	3.67	0.96	2.72	0.65	0.241	1.68	0.143	0.83	1.10	0.191	No
889	60.68	3.67	0.96	2.72	0.65	0.241	1.68	0.143	0.83	1.10	0.191	No
890	60.69	3.67	0.96	2.72	0.65	0.241	1.68	0.143	0.83	1.10	0.191	No
891	60.74	3.68	0.96	2.72	0.65	0.241	1.68	0.143	0.83	1.10	0.191	No
892	60.79	3.68	0.96	2.72	0.65	0.241	1.68	0.143	0.83	1.10	0.190	No
893	60.84	3.68	0.96	2.72	0.65	0.241	1.68	0.143	0.83	1.10	0.190	No
894	60.89	3.69	0.96	2.72	0.65	0.241	1.68	0.143	0.83	1.10	0.190	No
895	60.98	3.69	0.97	2.73	0.65	0.241	1.68	0.143	0.83	1.10	0.190	No
896	61.03	3.69	0.97	2.73	0.65	0.241	1.68	0.143	0.83	1.10	0.190	No
897	61.08	3.70	0.97	2.73	0.65	0.241	1.68	0.143	0.83	1.10	0.190	No
898	61.18	3.70	0.97	2.73	0.65	0.241	1.68	0.143	0.83	1.10	0.190	No
899	61.23	3.71	0.97	2.73	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
900	61.31	3.71	0.98	2.74	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
901	61.42	3.72	0.98	2.74	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
902	61.47	3.72	0.98	2.74	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
903	61.51	3.73	0.98	2.74	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
904	61.54	3.73	0.98	2.74	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
905	61.57	3.73	0.98	2.74	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
906	61.58	3.73	0.99	2.75	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
907	61.61	3.73	0.99	2.75	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
908	61.63	3.73	0.99	2.75	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
909	61.63	3.73	0.99	2.75	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
910	61.66	3.74	0.99	2.75	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
911	61.67	3.74	0.99	2.75	0.65	0.240	1.68	0.143	0.83	1.10	0.190	No
912	61.70	3.74	0.99	2.75	0.65	0.240	1.68	0.142	0.83	1.10	0.190	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	61.71	3.74	0.99	2.75	0.65	0.240	1.68	0.142	0.83	1.10	0.190	No
914	61.76	3.74	0.99	2.75	0.65	0.240	1.68	0.142	0.83	1.10	0.190	No
915	61.80	3.75	0.99	2.75	0.65	0.240	1.68	0.142	0.83	1.10	0.190	No
916	61.84	3.75	0.99	2.75	0.64	0.239	1.68	0.142	0.83	1.10	0.190	No
917	61.86	3.75	0.99	2.75	0.64	0.239	1.68	0.142	0.83	1.10	0.190	No
918	61.93	3.75	1.00	2.76	0.64	0.239	1.68	0.142	0.83	1.10	0.190	No
919	61.98	3.76	1.00	2.76	0.64	0.239	1.68	0.142	0.83	1.10	0.189	No
920	62.04	3.76	1.00	2.76	0.64	0.239	1.68	0.142	0.83	1.10	0.189	No
921	62.09	3.76	1.00	2.76	0.64	0.239	1.68	0.142	0.83	1.10	0.189	No
922	62.14	3.77	1.00	2.76	0.64	0.239	1.68	0.142	0.83	1.10	0.189	No
923	62.19	3.77	1.00	2.77	0.64	0.239	1.68	0.142	0.83	1.10	0.189	No
924	62.24	3.77	1.01	2.77	0.64	0.239	1.68	0.142	0.83	1.10	0.189	No
925	62.26	3.77	1.01	2.77	0.64	0.239	1.68	0.142	0.83	1.10	0.189	No
926	62.29	3.78	1.01	2.77	0.64	0.239	1.68	0.142	0.82	1.10	0.189	No
927	62.38	3.78	1.01	2.77	0.64	0.239	1.68	0.142	0.82	1.10	0.189	No
928	62.44	3.79	1.01	2.77	0.64	0.239	1.68	0.142	0.82	1.10	0.189	No
929	62.46	3.79	1.01	2.78	0.64	0.239	1.68	0.142	0.82	1.10	0.189	No
930	62.47	3.79	1.01	2.78	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
931	62.51	3.79	1.01	2.78	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
932	62.56	3.79	1.02	2.78	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
933	62.60	3.80	1.02	2.78	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
934	62.65	3.80	1.02	2.78	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
935	62.70	3.80	1.02	2.78	0.64	0.238	1.68	0.142	0.82	1.10	0.189	No
936	62.75	3.81	1.02	2.79	0.64	0.238	1.68	0.141	0.82	1.10	0.189	No
937	62.80	3.81	1.02	2.79	0.64	0.238	1.68	0.141	0.82	1.10	0.189	No
938	62.85	3.81	1.02	2.79	0.64	0.238	1.68	0.141	0.82	1.10	0.189	No
939	62.89	3.82	1.03	2.79	0.64	0.238	1.68	0.141	0.82	1.10	0.189	No
940	62.97	3.82	1.03	2.79	0.64	0.238	1.68	0.141	0.82	1.10	0.189	No
941	63.04	3.83	1.03	2.80	0.64	0.238	1.68	0.141	0.82	1.10	0.189	No
942	63.09	3.83	1.03	2.80	0.64	0.237	1.68	0.141	0.82	1.10	0.189	No
943	63.13	3.83	1.03	2.80	0.64	0.237	1.68	0.141	0.82	1.10	0.189	No
944	63.19	3.84	1.04	2.80	0.63	0.237	1.68	0.141	0.82	1.10	0.189	No
945	63.23	3.84	1.04	2.80	0.63	0.237	1.68	0.141	0.82	1.10	0.189	No
946	63.28	3.84	1.04	2.81	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
947	63.32	3.85	1.04	2.81	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
948	63.38	3.85	1.04	2.81	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
949	63.44	3.85	1.04	2.81	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
950	63.52	3.86	1.05	2.81	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
951	63.57	3.86	1.05	2.82	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
952	63.66	3.87	1.05	2.82	0.63	0.237	1.68	0.141	0.82	1.10	0.188	No
953	63.73	3.87	1.05	2.82	0.63	0.236	1.68	0.141	0.82	1.10	0.188	No
954	63.76	3.88	1.05	2.82	0.63	0.236	1.68	0.141	0.82	1.10	0.188	No
955	63.76	3.88	1.05	2.82	0.63	0.236	1.68	0.141	0.82	1.10	0.188	No
956	63.78	3.88	1.05	2.82	0.63	0.236	1.68	0.141	0.82	1.10	0.188	No
957	63.81	3.88	1.05	2.82	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
958	63.85	3.88	1.06	2.83	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
959	63.86	3.88	1.06	2.83	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
960	63.91	3.89	1.06	2.83	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
961	63.94	3.89	1.06	2.83	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
962	63.95	3.89	1.06	2.83	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
963	64.00	3.89	1.06	2.83	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
964	64.02	3.89	1.06	2.83	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
965	64.05	3.90	1.06	2.83	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
966	64.09	3.90	1.06	2.83	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
967	64.11	3.90	1.06	2.84	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
968	64.15	3.90	1.07	2.84	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
969	64.20	3.91	1.07	2.84	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
970	64.25	3.91	1.07	2.84	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
971	64.29	3.91	1.07	2.84	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
972	64.34	3.92	1.07	2.84	0.63	0.236	1.68	0.140	0.82	1.10	0.188	No
973	64.43	3.92	1.07	2.85	0.63	0.235	1.68	0.140	0.82	1.10	0.188	No
974	64.48	3.92	1.08	2.85	0.63	0.235	1.68	0.140	0.82	1.10	0.188	No
975	64.53	3.93	1.08	2.85	0.63	0.235	1.68	0.140	0.82	1.10	0.188	No
976	64.58	3.93	1.08	2.85	0.62	0.235	1.68	0.140	0.82	1.10	0.187	No
977	64.63	3.93	1.08	2.85	0.62	0.235	1.68	0.140	0.82	1.10	0.187	No
978	64.68	3.94	1.08	2.86	0.62	0.235	1.68	0.140	0.82	1.10	0.187	No
979	64.73	3.94	1.08	2.86	0.62	0.235	1.68	0.140	0.82	1.10	0.187	No
980	64.77	3.94	1.08	2.86	0.62	0.235	1.68	0.140	0.82	1.10	0.187	No
981	64.82	3.95	1.09	2.86	0.62	0.235	1.68	0.140	0.82	1.10	0.187	No
982	64.87	3.95	1.09	2.86	0.62	0.235	1.68	0.140	0.82	1.10	0.187	No
983	64.89	3.95	1.09	2.86	0.62	0.235	1.68	0.139	0.82	1.10	0.187	No
984	64.93	3.95	1.09	2.86	0.62	0.235	1.68	0.139	0.82	1.10	0.187	No
985	64.94	3.96	1.09	2.87	0.62	0.235	1.68	0.139	0.82	1.10	0.187	No
986	64.98	3.96	1.09	2.87	0.62	0.235	1.68	0.139	0.82	1.10	0.187	No
987	64.99	3.96	1.09	2.87	0.62	0.235	1.68	0.139	0.82	1.10	0.187	No
988	65.03	3.96	1.09	2.87	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
989	65.08	3.96	1.09	2.87	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
990	65.13	3.97	1.10	2.87	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
991	65.17	3.97	1.10	2.87	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
992	65.22	3.97	1.10	2.88	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
993	65.23	3.98	1.10	2.88	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
994	65.28	3.98	1.10	2.88	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
995	65.32	3.98	1.10	2.88	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
996	65.37	3.98	1.10	2.88	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
997	65.42	3.99	1.10	2.88	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
998	65.47	3.99	1.11	2.88	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
999	65.48	3.99	1.11	2.88	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
1000	65.49	3.99	1.11	2.89	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
1001	65.52	3.99	1.11	2.89	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
1002	65.57	4.00	1.11	2.89	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
1003	65.62	4.00	1.11	2.89	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
1004	65.67	4.00	1.11	2.89	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
1005	65.69	4.00	1.11	2.89	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
1006	65.72	4.01	1.11	2.89	0.62	0.234	1.68	0.139	0.82	1.10	0.187	No
1007	65.77	4.01	1.12	2.89	0.62	0.233	1.68	0.139	0.82	1.10	0.187	No
1008	65.82	4.01	1.12	2.89	0.62	0.233	1.68	0.139	0.82	1.10	0.187	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1009	65.86	4.01	1.12	2.89	0.62	0.233	1.68	0.139	0.82	1.10	0.187	No
1010	65.86	4.01	1.12	2.89	0.62	0.233	1.68	0.139	0.82	1.10	0.187	No
1011	65.91	4.01	1.12	2.89	0.62	0.233	1.68	0.139	0.82	1.10	0.187	No
1012	65.96	4.02	1.12	2.89	0.62	0.233	1.68	0.139	0.82	1.10	0.187	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
σ_v: Total overburden pressure at test point (tsf)
u_0: Water pressure at test point (tsf)
σ_v': Effective overburden pressure based on GWT during earthquake (tsf)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.01	-0.03	N/A	-11.45	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
2	0.04	-0.03	N/A	-18.30	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
3	0.08	-0.07	N/A	-13.93	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
4	0.10	-0.03	N/A	-40.02	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
5	0.13	-0.03	N/A	-55.83	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
6	0.18	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
7	0.22	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
8	0.27	0.81	4.01	9.28	1.00	1.28	50.14	63.98	4.000	No	Yes	2.00
9	0.33	2.77	3.31	3.21	1.00	4.42	15.47	68.30	4.000	No	Yes	2.00
10	0.36	5.16	2.95	1.83	1.00	8.26	7.99	66.07	4.000	Yes	Yes	2.00
11	0.37	7.12	2.76	1.34	0.84	11.41	5.40	61.61	4.000	Yes	Yes	2.00
12	0.38	8.20	2.69	1.21	0.81	13.14	4.58	60.15	4.000	Yes	Yes	2.00
13	0.42	9.38	2.63	1.15	0.80	15.03	3.98	59.88	4.000	Yes	Yes	2.00
14	0.44	10.59	2.58	1.15	0.78	16.98	3.58	60.79	4.000	Yes	No	2.00
15	0.47	12.18	2.52	1.09	0.76	19.53	3.09	60.26	4.000	Yes	No	2.00
16	0.47	14.24	2.44	1.01	0.74	22.83	2.61	59.51	4.000	Yes	No	2.00
17	0.52	17.00	2.35	0.91	0.71	27.27	2.14	58.39	4.000	Yes	No	2.00
18	0.56	20.48	2.26	0.82	0.69	32.85	1.78	58.60	4.000	Yes	No	2.00
19	0.58	24.93	2.16	0.72	0.66	40.00	1.52	60.77	4.000	Yes	No	2.00
20	0.61	30.70	2.05	0.62	0.62	49.27	1.35	66.61	4.000	Yes	No	2.00
21	0.66	36.94	1.95	0.54	0.59	59.30	1.27	75.22	4.000	Yes	No	2.00
22	0.76	40.79	1.89	0.50	0.58	65.47	1.23	80.72	4.000	Yes	No	2.00
23	0.80	38.66	1.93	0.54	0.59	62.05	1.25	77.85	4.000	No	No	2.00
24	0.81	35.49	1.98	0.58	0.60	56.95	1.29	73.41	4.000	No	No	2.00
25	0.85	32.42	2.03	0.63	0.62	52.02	1.33	69.37	4.000	No	No	2.00
26	0.86	32.79	2.03	0.63	0.62	52.62	1.33	69.99	4.000	No	No	2.00
27	0.90	32.22	2.05	0.69	0.62	51.69	1.35	70.01	4.000	No	No	2.00
28	0.95	31.82	2.07	0.73	0.63	51.04	1.38	70.34	4.000	No	No	2.00
29	1.00	30.53	2.06	0.67	0.63	48.97	1.37	67.09	4.000	No	No	2.00
30	1.05	28.88	2.04	0.54	0.62	46.31	1.34	62.22	4.000	No	No	2.00
31	1.14	26.55	2.01	0.38	0.61	42.56	1.00	42.56	4.000	No	No	2.00
32	1.24	24.29	2.04	0.37	0.62	38.92	1.00	38.92	4.000	No	No	2.00
33	1.31	20.51	2.14	0.44	0.65	32.85	1.00	32.85	4.000	No	No	2.00
34	1.36	17.93	2.22	0.53	0.67	28.70	1.67	48.03	4.000	No	No	2.00
35	1.37	17.77	2.23	0.55	0.68	28.44	1.71	48.50	4.000	No	No	2.00
36	1.39	18.54	2.21	0.53	0.67	29.68	1.64	48.64	4.000	No	No	2.00
37	1.43	19.03	2.19	0.52	0.67	30.46	1.60	48.73	4.000	No	No	2.00
38	1.44	18.05	2.23	0.54	0.68	28.88	1.68	48.54	4.000	No	No	2.00
39	1.49	18.35	2.22	0.55	0.67	29.36	1.67	49.05	4.000	No	No	2.00
40	1.53	18.89	2.22	0.58	0.67	30.23	1.66	50.30	4.000	No	No	2.00
41	1.58	19.67	2.22	0.62	0.67	31.47	1.66	52.29	4.000	No	No	2.00
42	1.63	20.62	2.22	0.68	0.67	32.99	1.66	54.77	4.000	No	No	2.00
43	1.68	21.70	2.21	0.74	0.67	34.72	1.65	57.36	4.000	No	No	2.00
44	1.72	23.31	2.20	0.77	0.67	37.31	1.61	60.04	4.000	No	No	2.00
45	1.77	25.48	2.17	0.79	0.66	40.78	1.54	62.93	4.000	No	No	2.00
46	1.82	28.31	2.13	0.78	0.65	45.33	1.46	66.36	4.000	No	No	2.00
47	1.86	31.52	2.08	0.77	0.63	50.48	1.40	70.45	4.000	No	No	2.00
48	1.92	35.09	2.03	0.73	0.62	56.22	1.34	75.14	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	1.97	38.67	1.98	0.69	0.60	61.96	1.29	80.21	4.000	No	No	2.00
50	2.01	41.61	1.95	0.68	0.59	66.68	1.27	84.88	4.000	No	No	2.00
51	2.09	43.22	1.94	0.68	0.59	69.27	1.26	87.55	4.000	No	No	2.00
52	2.16	43.05	1.95	0.70	0.59	68.99	1.27	87.53	4.000	No	No	2.00
53	2.20	41.47	1.96	0.71	0.60	66.43	1.28	85.02	4.000	No	No	2.00
54	2.25	39.85	1.98	0.71	0.60	63.83	1.29	82.39	4.000	No	No	2.00
55	2.31	38.60	1.99	0.69	0.60	61.82	1.30	80.09	4.000	No	No	2.00
56	2.37	37.79	1.98	0.66	0.60	60.52	1.29	78.32	4.000	No	No	2.00
57	2.40	36.88	1.99	0.64	0.60	59.05	1.30	76.51	4.000	No	No	2.00
58	2.46	35.97	1.98	0.61	0.60	57.57	1.29	74.55	4.000	No	No	2.00
59	2.54	35.36	1.97	0.57	0.60	56.59	1.29	72.87	4.000	No	No	2.00
60	2.59	34.69	1.96	0.50	0.59	55.51	1.00	55.51	4.000	No	No	2.00
61	2.69	34.25	1.94	0.45	0.59	54.80	1.00	54.80	4.000	No	No	2.00
62	2.74	33.95	1.92	0.40	0.58	54.31	1.00	54.31	4.000	No	No	2.00
63	2.83	33.88	1.92	0.39	0.58	54.19	1.00	54.19	4.000	No	No	2.00
64	2.88	34.35	1.91	0.38	0.58	54.94	1.00	54.94	4.000	No	No	2.00
65	2.98	35.70	1.89	0.37	0.57	57.10	1.00	57.10	4.000	No	No	2.00
66	3.03	38.57	1.85	0.36	0.56	61.71	1.00	61.71	4.000	No	No	2.00
67	3.12	42.31	1.82	0.38	0.55	67.72	1.00	67.72	4.000	No	No	2.00
68	3.21	46.83	1.79	0.40	0.55	74.97	1.00	74.97	4.000	No	No	2.00
69	3.27	51.66	1.76	0.41	0.54	82.72	1.00	82.72	4.000	No	No	2.00
70	3.34	57.05	1.72	0.40	0.52	91.38	1.00	91.38	4.000	No	No	2.00
71	3.41	61.91	1.69	0.40	0.51	99.18	1.00	99.18	4.000	No	No	2.00
72	3.51	64.20	1.68	0.41	0.51	102.85	1.00	102.85	4.000	No	No	2.00
73	3.55	63.63	1.70	0.44	0.52	101.93	1.00	101.93	4.000	No	No	2.00
74	3.65	62.42	1.72	0.46	0.52	99.97	1.00	99.97	4.000	No	No	2.00
75	3.75	61.71	1.73	0.47	0.53	98.83	1.00	98.83	4.000	No	No	2.00
76	3.83	61.44	1.73	0.47	0.53	98.39	1.00	98.39	4.000	No	No	2.00
77	3.94	61.11	1.73	0.47	0.53	97.84	1.00	97.84	4.000	No	No	2.00
78	4.04	60.30	1.73	0.47	0.53	96.53	1.00	96.53	4.000	No	No	2.00
79	4.13	60.63	1.75	0.50	0.53	97.06	1.08	104.72	4.000	No	No	2.00
80	4.24	61.68	1.74	0.50	0.53	98.73	1.00	98.73	4.000	No	No	2.00
81	4.38	65.15	1.68	0.42	0.51	104.30	1.00	104.30	4.000	No	No	2.00
82	4.50	68.93	1.62	0.35	0.50	110.36	1.00	110.36	4.000	No	No	2.00
83	4.62	74.13	1.57	0.32	0.50	118.70	1.00	118.70	4.000	No	No	2.00
84	4.71	77.89	1.57	0.35	0.50	124.73	1.00	124.73	4.000	No	No	2.00
85	4.75	80.93	1.57	0.37	0.50	129.61	1.00	129.61	4.000	No	No	2.00
86	4.84	82.11	1.58	0.39	0.50	131.50	1.00	131.50	4.000	No	No	2.00
87	4.89	82.93	1.58	0.40	0.50	132.82	1.00	132.82	4.000	No	No	2.00
88	4.94	82.93	1.58	0.40	0.50	132.82	1.00	132.82	4.000	No	No	2.00
89	4.98	81.72	1.59	0.41	0.50	130.87	1.00	130.87	4.000	No	No	2.00
90	5.07	80.10	1.60	0.41	0.50	128.25	1.00	128.25	4.000	No	No	2.00
91	5.13	78.48	1.61	0.42	0.50	125.65	1.00	125.65	4.000	No	No	2.00
92	5.17	76.79	1.61	0.41	0.50	122.93	1.00	122.93	4.000	No	No	2.00
93	5.27	74.77	1.62	0.41	0.50	119.67	1.00	119.67	4.000	No	No	2.00
94	5.32	72.75	1.63	0.40	0.50	116.42	1.00	116.42	4.000	No	No	2.00
95	5.42	70.86	1.64	0.40	0.50	113.37	1.00	113.37	4.000	No	No	2.00
96	5.46	69.34	1.64	0.39	0.50	110.93	1.00	110.93	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	5.56	68.02	1.65	0.39	0.50	108.80	1.00	108.80	4.000	No	No	2.00
98	5.61	66.87	1.66	0.39	0.50	106.96	1.00	106.96	4.000	No	No	2.00
99	5.71	65.86	1.66	0.40	0.51	105.32	1.00	105.32	4.000	No	No	2.00
100	5.78	64.92	1.67	0.40	0.51	103.80	1.00	103.80	4.000	No	No	2.00
101	5.85	63.84	1.68	0.41	0.51	102.06	1.00	102.06	4.000	No	No	2.00
102	5.95	62.83	1.69	0.42	0.52	100.42	1.00	100.42	4.000	No	No	2.00
103	6.00	62.32	1.71	0.44	0.52	99.61	1.00	99.61	4.000	No	No	2.00
104	6.09	62.93	1.66	0.36	0.51	100.57	1.00	100.57	4.000	No	No	2.00
105	6.14	64.75	1.60	0.29	0.50	103.50	1.00	103.50	4.000	No	No	2.00
106	6.24	67.52	1.53	0.21	0.50	107.94	1.00	107.94	4.000	No	No	2.00
107	6.30	70.42	1.54	0.24	0.50	112.60	1.00	112.60	4.000	No	No	2.00
108	6.38	71.40	1.56	0.28	0.50	114.16	1.00	114.16	4.000	No	No	2.00
109	6.46	69.58	1.60	0.32	0.50	111.22	1.00	111.22	4.000	No	No	2.00
110	6.50	68.43	1.62	0.35	0.50	109.38	1.00	109.38	4.000	No	No	2.00
111	6.56	68.84	1.63	0.36	0.50	110.02	1.00	110.02	4.000	No	No	2.00
112	6.63	71.30	1.61	0.36	0.50	113.98	1.00	113.98	4.000	No	No	2.00
113	6.68	72.51	1.61	0.37	0.50	115.92	1.00	115.92	4.000	No	No	2.00
114	6.76	73.49	1.61	0.37	0.50	117.34	1.00	117.34	4.000	No	No	2.00
115	6.82	74.54	1.60	0.37	0.50	118.51	1.00	118.51	4.000	No	No	2.00
116	6.88	76.19	1.59	0.36	0.50	120.59	1.00	120.59	4.000	No	No	2.00
117	6.96	78.38	1.58	0.35	0.50	123.33	1.00	123.33	4.000	No	No	2.00
118	7.03	80.54	1.56	0.34	0.50	126.09	1.00	126.09	4.000	No	No	2.00
119	7.11	82.06	1.55	0.34	0.50	127.75	1.00	127.75	4.000	No	No	2.00
120	7.16	83.04	1.55	0.34	0.50	128.83	1.00	128.83	4.000	No	No	2.00
121	7.26	83.82	1.55	0.34	0.50	129.11	1.00	129.11	4.000	No	No	2.00
122	7.31	84.43	1.56	0.35	0.50	129.55	1.00	129.55	4.000	No	No	2.00
123	7.40	84.63	1.56	0.35	0.50	129.06	1.00	129.06	4.000	No	No	2.00
124	7.45	84.52	1.56	0.35	0.50	128.43	1.00	128.43	4.000	No	No	2.00
125	7.54	83.95	1.57	0.35	0.50	126.75	1.00	126.75	4.000	No	No	2.00
126	7.60	82.84	1.58	0.36	0.50	124.58	1.00	124.58	4.000	No	No	2.00
127	7.68	81.22	1.59	0.36	0.50	121.42	1.00	121.42	4.000	No	No	2.00
128	7.74	79.70	1.60	0.36	0.50	118.70	1.00	118.70	4.000	No	No	2.00
129	7.83	78.55	1.61	0.37	0.50	116.27	1.00	116.27	4.000	No	No	2.00
130	7.90	78.35	1.61	0.37	0.50	115.47	1.00	115.47	4.000	No	No	2.00
131	7.98	79.10	1.62	0.38	0.50	115.95	1.00	115.95	4.000	No	No	2.00
132	8.05	80.62	1.62	0.39	0.50	117.66	1.00	117.66	4.000	No	No	2.00
133	8.12	81.69	1.62	0.40	0.50	118.66	1.00	118.66	4.000	No	No	2.00
134	8.19	81.66	1.62	0.41	0.50	118.08	1.00	118.08	4.000	No	No	2.00
135	8.27	80.48	1.64	0.42	0.50	115.81	1.00	115.81	4.000	No	No	2.00
136	8.36	79.13	1.65	0.42	0.50	113.39	1.00	113.39	4.000	No	No	2.00
137	8.41	78.35	1.61	0.34	0.50	111.75	1.00	111.75	4.000	No	No	2.00
138	8.50	78.42	1.57	0.27	0.50	111.21	1.00	111.21	4.000	No	No	2.00
139	8.60	78.79	1.54	0.23	0.50	111.10	1.00	111.10	4.000	No	No	2.00
140	8.70	78.76	1.56	0.26	0.50	110.43	1.00	110.43	4.000	No	No	2.00
141	8.74	70.97	1.64	0.31	0.50	99.16	1.00	99.16	4.000	No	No	2.00
142	8.78	65.57	1.68	0.35	0.51	92.36	1.00	92.36	4.000	No	No	2.00
143	8.81	63.58	1.71	0.37	0.52	89.84	1.00	89.84	4.000	No	No	2.00
144	8.86	69.75	1.66	0.34	0.51	97.38	1.00	97.38	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	8.91	73.77	1.64	0.34	0.50	102.14	1.00	102.14	4.000	No	No	2.00
146	8.94	74.34	1.64	0.35	0.50	102.81	1.00	102.81	4.000	No	No	2.00
147	9.02	73.80	1.66	0.36	0.51	101.95	1.00	101.95	4.000	No	No	2.00
148	9.10	72.52	1.68	0.39	0.51	100.12	1.00	100.12	4.000	No	No	2.00
149	9.17	71.17	1.69	0.40	0.52	98.18	1.00	98.18	4.000	No	No	2.00
150	9.22	69.95	1.70	0.41	0.52	96.47	1.00	96.47	4.000	No	No	2.00
151	9.31	69.01	1.71	0.42	0.52	94.84	1.00	94.84	4.000	No	No	2.00
152	9.37	68.50	1.72	0.42	0.52	93.92	1.00	93.92	4.000	No	No	2.00
153	9.42	68.60	1.72	0.42	0.52	93.81	1.00	93.81	4.000	No	No	2.00
154	9.52	69.18	1.72	0.41	0.52	94.01	1.00	94.01	4.000	No	No	2.00
155	9.60	70.19	1.71	0.41	0.52	94.84	1.00	94.84	4.000	No	No	2.00
156	9.66	71.54	1.70	0.41	0.52	96.20	1.00	96.20	4.000	No	No	2.00
157	9.74	73.13	1.69	0.40	0.52	97.75	1.00	97.75	4.000	No	No	2.00
158	9.81	74.58	1.69	0.40	0.51	99.20	1.00	99.20	4.000	No	No	2.00
159	9.89	75.79	1.68	0.40	0.51	100.34	1.00	100.34	4.000	No	No	2.00
160	9.98	77.04	1.68	0.41	0.51	101.50	1.00	101.50	4.000	No	No	2.00
161	10.03	78.79	1.68	0.42	0.51	103.47	1.00	103.47	4.000	No	No	2.00
162	10.13	81.26	1.67	0.42	0.51	106.04	1.00	106.04	4.000	No	No	2.00
163	10.23	84.06	1.66	0.42	0.51	108.97	1.00	108.97	4.000	No	No	2.00
164	10.32	86.45	1.65	0.42	0.50	111.33	1.00	111.33	4.000	No	No	2.00
165	10.38	88.11	1.65	0.42	0.50	112.97	1.00	112.97	4.000	No	No	2.00
166	10.47	88.68	1.65	0.41	0.50	113.17	1.00	113.17	4.000	No	No	2.00
167	10.57	88.44	1.65	0.41	0.50	112.36	1.00	112.36	4.000	No	No	2.00
168	10.66	87.94	1.61	0.34	0.50	111.05	1.00	111.05	4.000	No	No	2.00
169	10.76	87.67	1.57	0.27	0.50	110.18	1.00	110.18	4.000	No	No	2.00
170	10.85	88.00	1.53	0.22	0.50	110.11	1.00	110.11	4.000	No	No	2.00
171	10.92	88.54	1.55	0.24	0.50	110.44	1.00	110.44	4.000	No	No	2.00
172	11.00	85.17	1.58	0.27	0.50	105.80	1.00	105.80	4.000	No	No	2.00
173	11.07	82.17	1.61	0.29	0.50	101.74	1.00	101.74	4.000	No	No	2.00
174	11.10	80.21	1.63	0.30	0.50	99.18	1.00	99.18	4.000	No	No	2.00
175	11.15	82.81	1.62	0.30	0.50	102.16	1.00	102.16	4.000	No	No	2.00
176	11.19	85.41	1.61	0.31	0.50	105.18	1.00	105.18	4.000	No	No	2.00
177	11.24	87.43	1.61	0.32	0.50	107.45	1.00	107.45	4.000	No	No	2.00
178	11.29	89.66	1.61	0.33	0.50	109.95	1.00	109.95	4.000	No	No	2.00
179	11.34	92.29	1.60	0.34	0.50	112.96	1.00	112.96	4.000	No	No	2.00
180	11.40	94.89	1.60	0.35	0.50	115.81	1.00	115.81	4.000	No	No	2.00
181	11.47	96.81	1.60	0.36	0.50	117.83	1.00	117.83	4.000	No	No	2.00
182	11.53	97.72	1.60	0.37	0.50	118.60	1.00	118.60	4.000	No	No	2.00
183	11.58	98.23	1.60	0.37	0.50	118.97	1.00	118.97	4.000	No	No	2.00
184	11.65	98.70	1.61	0.38	0.50	119.16	1.00	119.16	4.000	No	No	2.00
185	11.72	99.17	1.61	0.38	0.50	119.34	1.00	119.34	4.000	No	No	2.00
186	11.77	99.00	1.61	0.39	0.50	118.88	1.00	118.88	4.000	No	No	2.00
187	11.82	98.36	1.62	0.39	0.50	117.83	1.00	117.83	4.000	No	No	2.00
188	11.88	97.25	1.64	0.42	0.50	116.19	1.00	116.19	4.000	No	No	2.00
189	11.97	96.10	1.65	0.43	0.50	114.49	1.00	114.49	4.000	No	No	2.00
190	12.02	94.75	1.65	0.43	0.50	112.75	1.00	112.75	4.000	No	No	2.00
191	12.06	93.54	1.65	0.40	0.50	110.95	1.00	110.95	4.000	No	No	2.00
192	12.11	93.03	1.65	0.40	0.50	110.11	1.00	110.11	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	12.21	92.63	1.65	0.39	0.50	109.15	1.00	109.15	4.000	No	No	2.00
194	12.25	92.93	1.64	0.38	0.50	109.21	1.00	109.21	4.000	No	No	2.00
195	12.30	93.00	1.64	0.38	0.50	109.05	1.00	109.05	4.000	No	No	2.00
196	12.31	93.44	1.63	0.37	0.50	109.51	1.00	109.51	4.000	No	No	2.00
197	12.32	93.64	1.63	0.37	0.50	109.72	1.00	109.72	4.000	No	No	2.00
198	12.35	94.21	1.62	0.36	0.50	110.25	1.00	110.25	4.000	No	No	2.00
199	12.40	95.26	1.61	0.35	0.50	111.26	1.00	111.26	4.000	No	No	2.00
200	12.45	96.78	1.60	0.33	0.50	112.82	1.00	112.82	4.000	No	No	2.00
201	12.52	98.43	1.60	0.33	0.50	114.40	1.00	114.40	4.000	No	No	2.00
202	12.56	100.32	1.59	0.34	0.50	116.43	1.00	116.43	4.000	No	No	2.00
203	12.62	102.04	1.59	0.35	0.50	118.16	1.00	118.16	4.000	No	No	2.00
204	12.65	103.69	1.56	0.31	0.50	119.90	1.00	119.90	4.000	No	No	2.00
205	12.71	105.14	1.53	0.26	0.50	121.32	1.00	121.32	4.000	No	No	2.00
206	12.76	107.34	1.48	0.22	0.50	123.61	1.00	123.61	4.000	No	No	2.00
207	12.83	110.34	1.48	0.23	0.50	126.74	1.00	126.74	4.000	No	No	2.00
208	12.88	114.29	1.50	0.26	0.50	131.03	1.00	131.03	4.000	No	No	2.00
209	12.93	118.94	1.50	0.30	0.50	136.14	1.00	136.14	4.000	No	No	2.00
210	12.98	121.44	1.52	0.33	0.50	138.73	1.00	138.73	4.000	No	No	2.00
211	13.03	123.77	1.52	0.33	0.50	141.10	1.00	141.10	4.000	No	No	2.00
212	13.04	120.16	1.54	0.36	0.50	136.93	1.00	136.93	4.000	No	No	2.00
213	13.07	122.72	1.54	0.38	0.50	139.66	1.00	139.66	4.000	No	No	2.00
214	13.13	125.66	1.55	0.40	0.50	142.70	1.00	142.70	4.000	No	No	2.00
215	13.17	134.36	1.53	0.40	0.50	152.37	1.00	152.37	4.000	No	No	2.00
216	13.22	137.87	1.53	0.42	0.50	156.08	1.00	156.08	4.000	No	No	2.00
217	13.27	140.13	1.54	0.44	0.50	158.31	1.00	158.31	4.000	No	No	2.00
218	13.32	141.11	1.54	0.46	0.50	159.12	1.00	159.12	4.000	No	No	2.00
219	13.37	141.28	1.55	0.47	0.50	159.00	1.00	159.00	4.000	No	No	2.00
220	13.41	140.67	1.55	0.47	0.50	158.02	1.00	158.02	4.000	No	No	2.00
221	13.46	139.05	1.56	0.48	0.50	155.85	1.00	155.85	4.000	No	No	2.00
222	13.51	137.63	1.57	0.48	0.50	153.98	1.00	153.98	4.000	No	No	2.00
223	13.56	135.98	1.58	0.49	0.50	151.81	1.00	151.81	4.000	No	No	2.00
224	13.60	134.29	1.59	0.51	0.50	149.65	1.00	149.65	4.000	No	No	2.00
225	13.66	132.81	1.60	0.52	0.50	147.65	1.00	147.65	4.000	No	No	2.00
226	13.75	131.80	1.60	0.51	0.50	145.98	1.00	145.98	4.000	No	No	2.00
227	13.80	131.19	1.60	0.51	0.50	145.02	1.00	145.02	4.000	No	No	2.00
228	13.89	130.75	1.61	0.51	0.50	144.01	1.00	144.01	4.000	No	No	2.00
229	13.94	129.81	1.61	0.52	0.50	142.69	1.00	142.69	4.000	No	No	2.00
230	13.99	128.19	1.63	0.54	0.50	140.62	1.00	140.62	4.000	No	No	2.00
231	14.09	125.39	1.65	0.57	0.50	137.21	1.00	137.21	4.000	No	No	2.00
232	14.14	122.28	1.68	0.61	0.51	133.79	1.00	133.79	4.000	No	No	2.00
233	14.23	119.38	1.70	0.64	0.52	130.35	1.00	130.35	4.000	No	No	2.00
234	14.28	117.19	1.68	0.58	0.51	127.54	1.00	127.54	4.000	No	No	2.00
235	14.38	116.43	1.66	0.51	0.50	125.95	1.00	125.95	4.000	No	No	2.00
236	14.42	115.35	1.63	0.45	0.50	124.40	1.00	124.40	4.000	No	No	2.00
237	14.52	115.79	1.63	0.45	0.50	124.40	1.00	124.40	4.000	No	No	2.00
238	14.57	116.75	1.64	0.47	0.50	125.23	1.00	125.23	4.000	No	No	2.00
239	14.67	117.53	1.64	0.48	0.50	125.60	1.00	125.60	4.000	No	No	2.00
240	14.68	117.83	1.64	0.49	0.50	125.93	1.00	125.93	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	14.70	116.41	1.65	0.50	0.50	124.39	1.00	124.39	4.000	No	No	2.00
242	14.75	116.58	1.66	0.50	0.50	124.38	1.00	124.38	4.000	No	No	2.00
243	14.80	116.18	1.66	0.51	0.51	123.80	1.00	123.80	4.000	No	No	2.00
244	14.89	116.21	1.67	0.52	0.51	123.45	1.00	123.45	4.000	No	No	2.00
245	14.94	114.76	1.68	0.53	0.51	121.75	1.00	121.75	4.000	No	No	2.00
246	15.04	111.83	1.69	0.54	0.52	118.29	1.00	118.29	4.000	No	No	2.00
247	15.13	107.24	1.71	0.55	0.52	113.18	1.01	114.51	4.000	No	No	2.00
248	15.21	101.74	1.74	0.56	0.53	107.19	1.06	113.68	4.000	No	No	2.00
249	15.28	95.87	1.76	0.57	0.54	100.87	1.10	111.36	4.000	No	No	2.00
250	15.38	90.00	1.79	0.58	0.54	94.46	1.14	107.63	4.000	No	No	2.00
251	15.47	83.86	1.82	0.58	0.55	87.79	1.17	102.77	4.000	No	No	2.00
252	15.57	77.55	1.85	0.59	0.56	80.97	1.20	97.12	4.000	No	No	2.00
253	15.67	70.76	1.89	0.60	0.57	73.71	1.23	90.52	4.000	No	No	2.00
254	15.77	63.91	1.93	0.61	0.59	66.40	1.26	83.47	4.000	No	No	2.00
255	15.86	57.27	1.98	0.63	0.60	59.33	1.29	76.63	4.000	No	No	2.00
256	15.96	51.73	2.03	0.67	0.62	53.45	1.34	71.45	4.000	No	No	2.00
257	16.05	47.31	2.09	0.73	0.63	48.75	1.40	68.25	4.000	No	No	2.00
258	16.15	43.60	2.15	0.86	0.65	44.83	1.51	67.79	4.000	No	No	2.00
259	16.25	41.11	2.20	0.97	0.67	42.13	1.63	68.47	4.000	No	No	2.00
260	16.31	39.86	2.23	1.04	0.68	40.76	1.71	69.57	4.000	No	No	2.00
261	16.39	39.72	2.23	1.02	0.68	40.48	1.70	68.78	4.000	No	No	2.00
262	16.48	40.50	2.21	0.96	0.67	41.08	1.65	67.59	4.000	No	No	2.00
263	16.59	43.06	2.17	0.86	0.66	43.47	1.53	66.70	4.000	No	No	2.00
264	16.68	47.95	2.09	0.73	0.64	48.20	1.40	67.68	4.000	No	No	2.00
265	16.76	53.89	2.01	0.61	0.61	53.96	1.31	70.90	4.000	No	No	2.00
266	16.86	58.72	1.95	0.54	0.59	58.53	1.27	74.31	4.000	No	No	2.00
267	16.92	61.25	1.92	0.51	0.58	60.90	1.25	76.25	4.000	No	No	2.00
268	17.02	61.65	1.92	0.50	0.58	61.10	1.25	76.36	4.000	No	No	2.00
269	17.11	61.14	1.94	0.53	0.59	60.41	1.26	76.12	4.000	No	No	2.00
270	17.22	60.40	1.96	0.58	0.60	59.48	1.28	75.94	4.000	Yes	No	2.00
271	17.35	58.51	2.04	0.78	0.62	57.44	1.34	77.19	4.000	Yes	No	2.00
272	17.45	53.15	2.18	1.20	0.66	52.07	1.57	81.76	4.000	Yes	No	2.00
273	17.55	43.40	2.38	1.91	0.72	42.36	2.26	95.58	4.000	Yes	No	2.00
274	17.61	33.92	2.57	2.79	0.78	32.93	3.48	114.42	4.000	Yes	No	2.00
275	17.64	27.41	2.70	3.46	0.82	26.45	4.70	124.38	4.000	Yes	Yes	2.00
276	17.70	24.84	2.75	3.68	0.83	23.84	5.27	125.58	4.000	Yes	Yes	2.00
277	17.75	23.12	2.79	3.84	0.84	22.09	5.71	126.01	4.000	Yes	Yes	2.00
278	17.80	22.04	2.82	4.00	0.85	20.96	6.07	127.17	4.000	Yes	Yes	2.00
279	17.85	21.57	2.85	4.36	0.86	20.45	6.49	132.79	4.000	Yes	Yes	2.00
280	17.94	24.37	2.80	4.19	0.85	23.10	5.83	134.72	4.000	No	Yes	2.00
281	17.99	29.74	2.70	3.80	0.82	28.29	4.75	134.51	4.000	No	Yes	2.00
282	18.09	36.42	2.60	3.34	0.79	34.65	3.76	130.35	4.000	No	Yes	2.00
283	18.15	38.34	2.58	3.31	0.78	36.42	3.61	131.44	4.000	No	No	2.00
284	18.23	36.08	2.63	3.58	0.80	34.09	3.99	135.89	4.000	No	Yes	2.00
285	18.33	27.03	2.80	4.68	0.85	25.22	5.88	148.20	4.000	No	Yes	2.00
286	18.43	18.43	3.01	6.17	1.00	16.85	8.99	151.54	4.000	No	Yes	2.00
287	18.52	11.28	3.27	8.30	1.00	9.87	14.46	142.66	4.000	No	Yes	2.00
288	18.59	9.25	3.30	7.06	1.00	7.88	15.23	120.07	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	18.72	8.44	3.27	5.49	1.00	7.05	14.48	102.14	4.000	No	Yes	2.00
290	18.81	7.87	3.26	4.64	1.00	6.47	14.17	91.69	4.000	No	Yes	2.00
291	18.87	7.73	3.27	4.61	1.00	6.32	14.34	90.62	4.000	No	Yes	2.00
292	18.95	7.94	3.28	5.10	1.00	6.48	14.76	95.67	4.000	No	Yes	2.00
293	19.05	8.95	3.24	5.23	1.00	7.39	13.77	101.75	4.000	No	Yes	2.00
294	19.14	11.32	3.12	4.53	1.00	9.56	10.96	104.74	4.000	No	Yes	2.00
295	19.22	15.43	2.92	3.38	0.89	13.37	7.56	101.14	4.000	Yes	Yes	2.00
296	19.29	23.29	2.67	2.31	0.81	20.64	4.44	91.70	4.000	Yes	Yes	2.00
297	19.38	36.79	2.41	1.58	0.73	33.12	2.43	80.52	4.000	Yes	No	2.00
298	19.44	54.77	2.21	1.24	0.67	49.78	1.63	81.04	4.000	Yes	No	2.00
299	19.53	73.63	2.06	1.07	0.63	67.13	1.37	92.11	4.000	Yes	No	2.00
300	19.62	89.35	1.99	1.02	0.60	81.50	1.30	105.61	4.000	Yes	No	2.00
301	19.69	100.62	1.95	1.03	0.59	91.73	1.27	116.28	4.000	Yes	No	2.00
302	19.79	106.79	1.94	1.07	0.59	97.11	1.26	122.62	4.000	No	No	2.00
303	19.86	108.17	1.96	1.16	0.60	98.11	1.28	125.15	4.000	No	No	2.00
304	19.97	105.91	1.99	1.25	0.60	95.65	1.30	124.06	4.000	No	No	2.00
305	20.07	101.09	2.02	1.32	0.61	90.89	1.33	120.48	4.000	No	No	2.00
306	20.16	94.14	2.06	1.40	0.63	84.23	1.37	115.28	4.000	No	No	2.00
307	20.26	84.49	2.07	1.27	0.63	75.23	1.38	103.79	4.000	Yes	No	2.00
308	20.34	72.68	2.10	1.18	0.64	64.34	1.43	91.71	4.000	Yes	No	2.00
309	20.43	59.83	2.16	1.11	0.66	52.55	1.52	80.02	4.000	Yes	No	2.00
310	20.50	47.95	2.33	1.55	0.71	41.63	2.03	84.51	4.000	Yes	No	2.00
311	20.60	37.70	2.50	2.17	0.76	32.23	3.01	96.91	4.000	Yes	No	2.00
312	20.62	30.48	2.66	2.88	0.81	25.73	4.28	110.02	4.000	Yes	Yes	2.00
313	20.63	28.08	2.72	3.22	0.82	23.58	4.89	115.31	4.000	Yes	Yes	2.00
314	20.68	27.74	2.74	3.38	0.83	23.22	5.10	118.43	4.000	Yes	Yes	2.00
315	20.73	27.64	2.76	3.60	0.83	23.06	5.32	122.67	4.000	Yes	Yes	2.00
316	20.82	25.48	2.82	4.04	0.85	21.06	6.08	128.12	4.000	Yes	Yes	2.00
317	20.87	23.45	2.87	4.37	0.87	19.23	6.78	130.45	4.000	Yes	Yes	2.00
318	20.91	21.57	2.91	4.48	0.88	17.54	7.32	128.42	4.000	Yes	Yes	2.00
319	20.96	19.58	2.95	4.54	1.00	15.59	7.98	124.40	4.000	Yes	Yes	2.00
320	21.05	17.59	3.00	4.73	1.00	13.84	8.82	122.12	4.000	No	Yes	2.00
321	21.11	16.98	3.02	4.74	1.00	13.29	9.07	120.49	4.000	No	Yes	2.00
322	21.17	17.11	3.01	4.72	1.00	13.36	9.02	120.44	4.000	No	Yes	2.00
323	21.25	21.23	2.88	3.84	0.87	17.01	6.86	116.62	4.000	Yes	Yes	2.00
324	21.30	31.25	2.64	2.71	0.80	25.68	4.13	106.03	4.000	Yes	Yes	2.00
325	21.37	48.56	2.39	1.90	0.72	40.77	2.31	94.37	4.000	Yes	No	2.00
326	21.45	68.84	2.20	1.51	0.67	58.49	1.62	94.86	4.000	Yes	No	2.00
327	21.49	87.80	2.09	1.36	0.64	75.10	1.41	105.59	4.000	Yes	No	2.00
328	21.58	103.45	2.02	1.30	0.62	88.68	1.33	117.80	4.000	Yes	No	2.00
329	21.64	115.70	1.98	1.28	0.60	99.28	1.29	128.46	4.000	Yes	No	2.00
330	21.69	124.50	1.96	1.29	0.60	106.86	1.28	136.49	4.000	Yes	No	2.00
331	21.78	130.41	1.95	1.31	0.59	111.69	1.27	142.03	4.000	No	No	2.00
332	21.83	133.78	1.96	1.36	0.59	114.42	1.27	145.79	4.000	No	No	2.00
333	21.89	135.43	1.97	1.42	0.60	115.57	1.28	148.03	4.000	No	No	2.00
334	21.98	136.01	1.98	1.49	0.60	115.67	1.29	149.32	4.000	No	No	2.00
335	22.03	135.90	1.99	1.55	0.61	115.31	1.30	150.06	4.000	No	No	2.00
336	22.12	134.89	2.01	1.60	0.61	114.06	1.31	149.60	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	22.22	133.20	2.02	1.63	0.61	112.20	1.32	148.31	4.000	No	No	2.00
338	22.26	130.88	2.03	1.65	0.62	110.01	1.33	146.45	4.000	No	No	2.00
339	22.36	128.38	2.04	1.67	0.62	107.52	1.34	144.21	4.000	No	No	2.00
340	22.41	125.79	2.05	1.70	0.62	105.07	1.36	142.38	4.000	No	No	2.00
341	22.51	123.53	2.04	1.63	0.62	102.88	1.35	138.65	4.000	No	No	2.00
342	22.60	121.33	2.03	1.54	0.62	100.82	1.34	134.71	4.000	No	No	2.00
343	22.70	119.34	2.01	1.41	0.61	98.95	1.32	130.43	4.000	No	No	2.00
344	22.75	116.88	2.02	1.40	0.61	96.72	1.32	127.90	4.000	No	No	2.00
345	22.84	109.32	2.05	1.47	0.62	89.92	1.36	122.31	4.000	No	No	2.00
346	22.89	107.14	2.06	1.48	0.63	87.93	1.37	120.57	4.000	No	No	2.00
347	22.90	104.88	2.07	1.49	0.63	85.98	1.38	118.82	4.000	No	No	2.00
348	22.94	110.11	2.04	1.39	0.62	90.42	1.34	121.26	4.000	No	No	2.00
349	23.00	112.36	2.02	1.34	0.61	92.21	1.32	122.07	4.000	No	No	2.00
350	23.08	118.94	1.98	1.24	0.60	97.70	1.29	126.15	4.000	No	No	2.00
351	23.13	127.04	1.94	1.16	0.59	104.57	1.26	131.91	4.000	No	No	2.00
352	23.20	134.05	1.90	1.10	0.58	110.43	1.24	136.83	4.000	No	No	2.00
353	23.27	137.05	1.89	1.07	0.57	112.81	1.23	138.66	4.000	No	No	2.00
354	23.33	135.57	1.89	1.05	0.57	111.40	1.23	136.90	4.000	No	No	2.00
355	23.42	131.55	1.89	1.03	0.58	107.76	1.23	132.83	4.000	No	No	2.00
356	23.48	126.94	1.90	1.01	0.58	103.73	1.24	128.30	4.000	No	No	2.00
357	23.57	123.16	1.91	1.00	0.58	100.30	1.24	124.68	4.000	No	No	2.00
358	23.61	121.20	1.92	1.01	0.58	98.52	1.25	122.97	4.000	No	No	2.00
359	23.66	121.50	1.92	1.02	0.58	98.62	1.25	123.25	4.000	No	No	2.00
360	23.73	124.04	1.92	1.03	0.58	100.52	1.25	125.44	4.000	No	No	2.00
361	23.80	127.95	1.91	1.04	0.58	103.59	1.24	128.73	4.000	No	No	2.00
362	23.85	131.96	1.90	1.05	0.58	106.79	1.24	132.25	4.000	No	No	2.00
363	23.94	134.80	1.90	1.06	0.58	108.87	1.24	134.50	4.000	No	No	2.00
364	24.00	135.88	1.90	1.07	0.58	109.59	1.24	135.41	4.000	No	No	2.00
365	24.09	135.37	1.90	1.07	0.58	108.86	1.24	134.81	4.000	No	No	2.00
366	24.16	133.34	1.91	1.09	0.58	106.93	1.24	133.09	4.000	No	No	2.00
367	24.24	130.04	1.89	0.97	0.57	104.25	1.23	128.02	4.000	No	No	2.00
368	24.33	125.79	1.86	0.85	0.57	100.75	1.21	122.05	4.000	No	No	2.00
369	24.43	121.10	1.84	0.74	0.56	96.90	1.19	115.53	4.000	No	No	2.00
370	24.52	114.28	1.88	0.80	0.57	90.85	1.23	111.31	4.000	No	No	2.00
371	24.58	108.90	1.92	0.85	0.58	86.13	1.25	107.54	4.000	No	No	2.00
372	24.59	104.52	1.95	0.89	0.59	82.40	1.27	104.41	4.000	No	No	2.00
373	24.63	104.21	1.95	0.90	0.59	82.05	1.27	104.24	4.000	No	No	2.00
374	24.68	103.45	1.96	0.94	0.60	81.24	1.28	103.96	4.000	No	No	2.00
375	24.77	102.47	1.98	0.98	0.60	80.14	1.29	103.52	4.000	No	No	2.00
376	24.82	100.31	2.01	1.05	0.61	78.15	1.31	102.59	4.000	No	No	2.00
377	24.92	97.85	2.03	1.11	0.62	75.83	1.34	101.32	4.000	No	No	2.00
378	25.01	95.22	2.06	1.17	0.63	73.42	1.36	100.09	4.000	No	No	2.00
379	25.06	92.38	2.08	1.22	0.63	70.94	1.39	98.75	4.000	No	No	2.00
380	25.16	89.48	2.10	1.27	0.64	68.36	1.42	97.29	4.000	No	No	2.00
381	25.25	86.51	2.13	1.31	0.65	65.75	1.46	95.92	4.000	No	No	2.00
382	25.30	83.55	2.15	1.35	0.65	63.24	1.50	94.77	4.000	No	No	2.00
383	25.41	80.44	2.17	1.40	0.66	60.52	1.55	93.81	4.000	Yes	No	2.00
384	25.49	77.27	2.20	1.47	0.67	57.80	1.61	93.24	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	25.55	73.97	2.23	1.55	0.68	55.02	1.70	93.42	4.000	Yes	No	2.00
386	25.64	70.59	2.27	1.65	0.69	52.13	1.81	94.24	4.000	Yes	No	2.00
387	25.70	67.02	2.31	1.78	0.70	49.15	1.95	95.94	4.000	Yes	No	2.00
388	25.79	63.24	2.35	1.91	0.71	46.00	2.13	97.75	4.000	Yes	No	2.00
389	25.89	58.92	2.40	2.05	0.73	42.45	2.35	99.94	4.000	Yes	No	2.00
390	25.94	54.26	2.45	2.20	0.74	38.75	2.63	101.97	4.000	Yes	No	2.00
391	26.02	49.37	2.50	2.32	0.76	34.89	2.95	102.81	4.000	Yes	No	2.00
392	26.12	45.05	2.54	2.37	0.77	31.51	3.23	101.92	4.000	Yes	No	2.00
393	26.17	40.83	2.57	2.37	0.78	28.31	3.52	99.58	4.000	Yes	No	2.00
394	26.28	37.02	2.61	2.37	0.79	25.37	3.84	97.30	4.000	Yes	Yes	2.00
395	26.36	33.31	2.65	2.33	0.80	22.57	4.17	94.10	4.000	Yes	Yes	2.00
396	26.45	29.43	2.70	2.37	0.82	19.65	4.69	92.22	4.000	Yes	Yes	2.00
397	26.50	24.94	2.78	2.55	0.84	16.31	5.63	91.86	4.000	Yes	Yes	2.00
398	26.61	20.15	2.91	3.01	0.88	12.75	7.37	93.95	4.000	Yes	Yes	2.00
399	26.70	15.97	3.07	3.75	1.00	9.43	10.10	95.23	4.000	No	Yes	2.00
400	26.77	12.97	3.21	4.62	1.00	7.45	12.95	96.46	4.000	No	Yes	2.00
401	26.85	11.85	3.26	4.83	1.00	6.70	14.12	94.58	4.000	No	Yes	2.00
402	26.94	11.45	3.27	4.67	1.00	6.41	14.29	91.60	4.000	No	Yes	2.00
403	27.04	11.95	3.22	4.13	1.00	6.71	13.15	88.25	4.000	No	Yes	2.00
404	27.14	12.22	3.20	3.92	1.00	6.86	12.68	86.95	4.000	No	Yes	2.00
405	27.23	12.90	3.15	3.53	1.00	7.27	11.66	84.75	4.000	No	Yes	2.00
406	27.28	13.22	3.13	3.30	1.00	7.46	11.13	83.02	4.000	No	Yes	2.00
407	27.29	13.29	3.09	2.84	1.00	7.50	10.38	77.81	4.000	No	Yes	2.00
408	27.38	13.29	3.07	2.57	1.00	7.47	9.96	74.44	4.000	No	Yes	2.00
409	27.48	13.27	3.06	2.51	1.00	7.43	9.89	73.48	4.000	No	Yes	2.00
410	27.57	13.27	3.10	2.97	1.00	7.41	10.67	79.00	4.000	No	Yes	2.00
411	27.64	13.30	3.13	3.39	1.00	7.41	11.31	83.76	4.000	No	Yes	2.00
412	27.65	13.44	3.17	3.99	1.00	7.49	12.08	90.43	4.000	No	Yes	2.00
413	27.74	14.52	3.16	4.27	1.00	8.14	11.82	96.17	4.000	No	Yes	2.00
414	27.80	16.91	3.10	4.34	1.00	9.63	10.69	102.90	4.000	No	Yes	2.00
415	27.90	19.17	3.05	4.16	1.00	11.00	9.59	105.58	4.000	No	Yes	2.00
416	27.99	19.34	3.05	4.25	1.00	11.07	9.67	106.99	4.000	No	Yes	2.00
417	28.07	17.12	3.11	4.55	1.00	9.65	10.91	105.31	4.000	No	Yes	2.00
418	28.16	14.45	3.20	4.79	1.00	7.96	12.63	100.58	4.000	No	Yes	2.00
419	28.25	12.53	3.25	4.68	1.00	6.75	13.86	93.48	4.000	No	Yes	2.00
420	28.34	11.52	3.26	4.24	1.00	6.10	14.13	86.20	4.000	No	Yes	2.00
421	28.44	11.01	3.26	3.94	1.00	5.76	14.19	81.77	4.000	No	Yes	2.00
422	28.53	10.84	3.26	3.87	1.00	5.64	14.27	80.51	4.000	No	Yes	2.00
423	28.62	11.75	3.26	4.25	1.00	6.17	14.04	86.70	4.000	No	Yes	2.00
424	28.76	14.21	3.19	4.46	1.00	7.64	12.54	95.81	4.000	No	Yes	2.00
425	28.86	17.65	3.12	4.75	1.00	9.69	11.11	107.72	4.000	No	Yes	2.00
426	28.96	20.32	3.09	5.14	1.00	11.26	10.51	118.36	4.000	No	Yes	2.00
427	29.08	21.30	3.12	6.06	1.00	11.80	11.10	130.98	4.000	No	Yes	2.00
428	29.19	22.07	3.15	6.87	1.00	12.21	11.60	141.58	4.000	No	Yes	2.00
429	29.29	27.50	2.99	5.17	1.00	15.40	8.64	133.06	4.000	No	Yes	2.00
430	29.39	40.70	2.74	3.77	0.83	25.08	5.15	129.21	4.000	No	Yes	2.00
431	29.50	57.67	2.55	3.03	0.77	36.81	3.37	124.06	4.000	No	No	2.00
432	29.63	66.88	2.53	3.30	0.77	42.86	3.19	136.79	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	29.65	70.22	2.52	3.39	0.76	45.09	3.13	141.18	4.000	Yes	No	2.00
434	29.66	71.00	2.52	3.38	0.76	45.61	3.10	141.50	4.000	Yes	No	2.00
435	29.72	73.53	2.50	3.27	0.76	47.34	2.95	139.57	4.000	Yes	No	2.00
436	29.80	77.81	2.46	3.07	0.75	50.31	2.70	135.94	4.000	Yes	No	2.00
437	29.85	89.49	2.36	2.59	0.72	58.79	2.17	127.49	4.000	Yes	No	2.00
438	29.94	111.58	2.20	2.00	0.67	75.08	1.62	121.89	4.000	Yes	No	2.00
439	30.00	135.50	2.06	1.57	0.63	93.20	1.37	127.60	4.000	Yes	No	2.00
440	30.05	152.98	1.96	1.28	0.60	106.83	1.28	136.43	4.000	Yes	No	2.00
441	30.14	162.60	1.89	1.09	0.58	114.57	1.23	140.95	4.000	Yes	No	2.00
442	30.19	167.56	1.84	0.97	0.56	118.78	1.20	142.08	4.000	Yes	No	2.00
443	30.24	169.61	1.83	0.93	0.56	120.45	1.18	142.19	4.000	Yes	No	2.00
444	30.29	169.68	1.83	0.93	0.56	120.31	1.18	142.38	0.348	No	No	1.91
445	30.38	167.72	1.84	0.95	0.56	118.51	1.19	141.39	0.343	No	No	1.88
446	30.43	164.79	1.85	0.98	0.56	116.05	1.20	139.76	0.334	No	No	1.83
447	30.48	161.62	1.87	0.99	0.57	113.47	1.21	137.67	0.323	No	No	1.77
448	30.54	159.16	1.87	1.00	0.57	111.46	1.22	135.86	0.313	No	No	1.71
449	30.62	158.35	1.87	0.99	0.57	110.69	1.22	134.98	0.309	No	No	1.69
450	30.67	157.77	1.87	0.99	0.57	110.16	1.22	134.34	0.305	No	No	1.67
451	30.72	158.55	1.87	0.98	0.57	110.67	1.22	134.61	0.307	No	No	1.67
452	30.76	159.46	1.86	0.96	0.57	111.32	1.21	134.89	0.308	No	No	1.68
453	30.86	162.06	1.85	0.94	0.56	113.16	1.20	135.92	0.314	No	No	1.71
454	30.91	165.09	1.84	0.91	0.56	115.46	1.19	137.26	0.321	No	No	1.74
455	30.95	168.94	1.82	0.88	0.55	118.37	1.17	138.94	0.329	No	No	1.79
456	31.03	173.83	1.80	0.85	0.55	122.03	1.15	140.71	0.339	No	No	1.84
457	31.10	179.36	1.78	0.83	0.54	126.19	1.13	142.33	0.348	No	No	1.89
458	31.15	185.03	1.76	0.81	0.54	130.44	1.10	144.07	0.358	No	No	1.94
459	31.20	189.66	1.75	0.81	0.53	133.76	1.09	146.05	0.370	No	No	2.00
460	31.26	192.52	1.75	0.82	0.53	135.69	1.09	147.81	0.380	No	No	2.00
461	31.34	186.22	1.78	0.86	0.54	130.42	1.13	147.23	0.377	No	No	2.00
462	31.37	184.63	1.79	0.87	0.54	129.08	1.14	146.99	0.375	No	No	2.00
463	31.38	181.39	1.80	0.89	0.55	126.56	1.15	145.70	0.368	No	No	1.99
464	31.43	184.63	1.78	0.86	0.54	129.02	1.13	146.17	0.370	No	No	2.00
465	31.47	179.33	1.80	0.87	0.55	124.92	1.15	143.44	0.354	No	No	1.91
466	31.55	171.64	1.82	0.88	0.55	118.91	1.17	139.35	0.332	No	No	1.79
467	31.59	160.34	1.86	0.93	0.57	110.19	1.21	132.93	0.298	No	No	1.61
468	31.66	147.76	1.91	1.00	0.58	100.47	1.24	124.83	0.261	No	No	1.40
469	31.73	135.75	1.97	1.09	0.60	91.20	1.28	116.80	0.228	No	No	1.23
470	31.78	125.08	2.02	1.21	0.62	83.04	1.33	110.36	0.205	No	No	1.10
471	31.84	115.64	2.09	1.36	0.63	75.76	1.40	106.34	0.192	No	No	1.03
472	31.93	107.23	2.16	1.55	0.65	69.27	1.51	104.84	0.187	No	No	1.00
473	31.98	100.42	2.22	1.75	0.67	64.06	1.66	106.04	0.191	No	No	1.02
474	32.02	98.18	2.25	1.90	0.68	62.19	1.75	108.88	0.200	No	No	1.07
475	32.09	97.00	2.27	2.03	0.69	61.07	1.83	111.87	0.210	No	No	1.13
476	32.16	98.89	2.27	2.07	0.69	62.18	1.83	113.86	0.217	No	No	1.16
477	32.22	100.29	2.27	2.07	0.69	63.04	1.82	114.52	0.220	No	No	1.17
478	32.27	103.49	2.25	2.02	0.68	65.22	1.76	114.53	0.220	No	No	1.17
479	32.34	106.02	2.24	1.97	0.68	66.91	1.71	114.38	0.219	No	No	1.17
480	32.42	108.89	2.22	1.91	0.67	68.85	1.66	114.11	0.218	No	No	1.16

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	32.46	113.04	2.19	1.80	0.66	71.82	1.58	113.62	0.216	No	No	1.15
482	32.54	117.73	2.15	1.68	0.65	75.15	1.51	113.25	0.215	No	No	1.14
483	32.60	121.74	2.11	1.51	0.64	78.23	1.43	112.00	0.211	No	No	1.12
484	32.67	124.81	2.07	1.39	0.63	80.60	1.38	111.53	0.209	No	No	1.11
485	32.75	127.51	2.05	1.31	0.62	82.59	1.35	111.85	0.210	No	No	1.12
486	32.81	130.38	2.05	1.32	0.62	84.43	1.35	113.95	0.218	No	No	1.15
487	32.89	133.38	2.04	1.34	0.62	86.29	1.35	116.21	0.226	No	No	1.20
488	32.94	129.47	2.07	1.43	0.63	83.21	1.38	114.84	0.221	No	No	1.17
489	32.95	131.02	2.07	1.44	0.63	84.23	1.38	116.07	0.225	No	No	1.19
490	33.00	132.88	2.07	1.46	0.63	85.36	1.38	117.56	0.231	No	No	1.22
491	33.06	141.08	2.04	1.42	0.62	91.06	1.34	122.40	0.251	No	No	1.32
492	33.11	142.26	2.04	1.45	0.62	91.66	1.35	123.66	0.256	No	No	1.35
493	33.20	141.21	2.06	1.50	0.63	90.60	1.36	123.53	0.255	No	No	1.35
494	33.25	139.02	2.08	1.56	0.63	88.78	1.39	123.06	0.253	No	No	1.34
495	33.34	137.03	2.09	1.61	0.64	87.07	1.41	122.48	0.251	No	No	1.32
496	33.38	136.69	2.10	1.63	0.64	86.68	1.42	122.68	0.252	No	No	1.33
497	33.48	138.41	2.10	1.64	0.64	87.63	1.41	123.78	0.256	No	No	1.35
498	33.58	141.92	2.09	1.64	0.63	89.83	1.40	125.79	0.265	No	No	1.39
499	33.63	146.74	2.07	1.63	0.63	93.05	1.38	128.81	0.279	No	No	1.46
500	33.73	152.41	2.06	1.61	0.63	96.75	1.37	132.15	0.295	No	No	1.55
501	33.82	158.96	2.04	1.60	0.62	101.09	1.35	136.16	0.315	No	No	1.65
502	33.87	165.74	2.03	1.58	0.62	105.66	1.33	140.58	0.338	No	No	1.77
503	33.96	172.72	2.01	1.57	0.61	110.29	1.32	145.13	0.364	No	No	1.91
504	34.02	180.58	2.00	1.57	0.61	115.54	1.30	150.66	0.398	No	No	2.00
505	34.11	190.03	1.98	1.57	0.60	121.77	1.29	157.32	0.442	No	No	2.00
506	34.18	200.49	1.97	1.59	0.60	128.68	1.28	164.99	0.498	No	No	2.00
507	34.26	210.44	1.96	1.63	0.60	135.11	1.28	172.52	0.558	No	No	2.00
508	34.35	219.45	1.96	1.68	0.60	140.77	1.28	179.50	0.618	No	No	2.00
509	34.44	227.51	1.95	1.71	0.59	145.83	1.27	185.53	0.674	No	No	2.00
510	34.49	233.96	1.95	1.72	0.59	150.02	1.27	190.23	0.720	No	No	2.00
511	34.59	237.94	1.94	1.72	0.59	152.42	1.27	192.83	0.747	No	No	2.00
512	34.69	240.00	1.94	1.73	0.59	153.47	1.26	194.12	0.760	No	No	2.00
513	34.76	240.94	1.94	1.72	0.59	153.92	1.26	194.53	0.765	No	No	2.00
514	34.83	240.60	1.94	1.72	0.59	153.43	1.26	194.02	0.759	No	No	2.00
515	34.93	237.97	1.94	1.71	0.59	151.43	1.26	191.54	0.733	No	No	2.00
516	35.02	233.82	1.95	1.70	0.59	148.39	1.27	188.08	0.699	No	No	2.00
517	35.12	229.78	1.94	1.65	0.59	145.60	1.27	184.23	0.662	No	No	2.00
518	35.22	226.47	1.94	1.62	0.59	143.26	1.26	181.13	0.633	No	No	2.00
519	35.30	222.22	1.94	1.59	0.59	140.29	1.26	177.46	0.600	No	No	2.00
520	35.38	208.55	1.98	1.66	0.60	130.48	1.29	168.21	0.523	No	No	2.00
521	35.43	198.10	2.00	1.71	0.61	123.09	1.31	161.35	0.471	No	No	2.00
522	35.46	189.40	2.03	1.76	0.62	116.99	1.33	155.80	0.432	No	No	2.00
523	35.51	187.20	2.03	1.73	0.62	115.53	1.33	153.78	4.000	Yes	No	2.00
524	35.56	176.78	2.05	1.75	0.62	108.45	1.35	146.76	4.000	Yes	No	2.00
525	35.66	163.52	2.08	1.79	0.63	99.31	1.39	138.53	4.000	Yes	No	2.00
526	35.70	148.20	2.13	1.85	0.65	89.01	1.46	130.03	4.000	Yes	No	2.00
527	35.80	131.87	2.19	1.98	0.66	77.90	1.59	123.66	4.000	Yes	No	2.00
528	35.89	111.32	2.28	2.22	0.69	64.17	1.87	119.95	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	35.96	89.09	2.41	2.59	0.73	49.72	2.43	120.81	4.000	Yes	No	2.00
530	36.04	68.24	2.54	2.90	0.77	36.73	3.28	120.37	4.000	Yes	No	2.00
531	36.14	52.15	2.66	3.11	0.81	27.04	4.33	117.01	4.000	Yes	Yes	2.00
532	36.19	43.48	2.73	3.10	0.83	22.01	5.03	110.69	4.000	Yes	Yes	2.00
533	36.28	40.51	2.77	3.18	0.84	20.23	5.44	110.05	4.000	Yes	Yes	2.00
534	36.33	40.51	2.76	3.10	0.84	20.24	5.35	108.32	3.600	No	Yes	2.00
535	36.42	42.30	2.74	3.02	0.83	21.24	5.09	108.08	3.600	No	Yes	2.00
536	36.48	45.97	2.69	2.87	0.81	23.38	4.59	107.27	3.600	No	Yes	2.00
537	36.52	51.03	2.66	2.98	0.81	26.20	4.31	112.95	3.600	No	Yes	2.00
538	36.62	54.10	2.66	3.19	0.81	27.78	4.31	119.67	3.600	No	Yes	2.00
539	36.68	54.07	2.69	3.50	0.81	27.55	4.59	126.59	3.600	No	Yes	2.00
540	36.77	52.82	2.71	3.61	0.82	26.73	4.79	128.11	3.600	No	Yes	2.00
541	36.86	54.64	2.69	3.49	0.81	27.76	4.56	126.60	4.000	Yes	Yes	2.00
542	36.90	67.67	2.53	2.74	0.77	35.75	3.22	115.19	4.000	Yes	No	2.00
543	37.00	98.14	2.29	1.88	0.69	55.13	1.87	103.13	4.000	Yes	No	2.00
544	37.10	140.34	2.04	1.30	0.62	83.45	1.35	112.56	4.000	Yes	No	2.00
545	37.20	182.54	1.86	0.97	0.57	113.15	1.21	136.84	4.000	Yes	No	2.00
546	37.29	213.04	1.75	0.82	0.53	135.23	1.09	147.30	4.000	Yes	No	2.00
547	37.39	232.34	1.70	0.76	0.52	149.01	1.00	149.01	4.000	Yes	No	2.00
548	37.49	241.91	1.70	0.80	0.52	155.00	1.00	155.00	0.426	No	No	2.00
549	37.53	245.57	1.72	0.85	0.52	156.74	1.02	160.20	0.462	No	No	2.00
550	37.58	246.07	1.73	0.90	0.53	156.33	1.06	165.44	0.501	No	No	2.00
551	37.62	247.84	1.75	0.95	0.53	156.88	1.08	169.66	0.534	No	No	2.00
552	37.69	250.56	1.77	1.01	0.54	157.82	1.11	175.10	0.579	No	No	2.00
553	37.77	253.53	1.78	1.07	0.54	158.95	1.13	179.78	0.620	No	No	2.00
554	37.82	254.98	1.80	1.14	0.55	159.10	1.15	183.39	0.654	No	No	2.00
555	37.87	254.84	1.81	1.18	0.55	158.42	1.17	184.85	0.667	No	No	2.00
556	37.91	252.72	1.83	1.23	0.56	156.44	1.18	184.82	0.667	No	No	2.00
557	37.97	248.23	1.85	1.27	0.56	152.87	1.20	183.06	0.650	No	No	2.00
558	38.06	241.92	1.87	1.31	0.57	148.07	1.21	179.59	0.619	No	No	2.00
559	38.10	235.58	1.88	1.34	0.57	143.53	1.22	175.74	0.585	No	No	2.00
560	38.17	230.89	1.89	1.34	0.57	140.30	1.23	172.34	0.556	No	No	2.00
561	38.25	228.09	1.88	1.30	0.57	138.57	1.22	169.66	0.534	No	No	2.00
562	38.35	225.79	1.87	1.25	0.57	137.24	1.22	167.11	0.514	No	No	2.00
563	38.40	223.43	1.87	1.21	0.57	135.86	1.21	164.83	0.496	No	No	2.00
564	38.46	221.65	1.86	1.19	0.57	134.68	1.21	163.21	0.484	No	No	2.00
565	38.54	220.87	1.86	1.18	0.57	134.09	1.21	162.26	0.477	No	No	2.00
566	38.60	220.87	1.86	1.15	0.56	134.14	1.21	161.69	0.473	No	No	2.00
567	38.69	222.22	1.85	1.12	0.56	135.09	1.20	161.77	0.474	No	No	2.00
568	38.74	224.92	1.83	1.09	0.56	137.05	1.19	162.53	0.479	No	No	2.00
569	38.83	227.85	1.82	1.08	0.56	138.91	1.18	163.73	0.488	No	No	2.00
570	38.88	229.20	1.81	1.05	0.55	139.97	1.17	163.54	0.487	No	No	2.00
571	38.97	228.76	1.81	1.03	0.55	139.65	1.16	162.47	0.479	No	No	2.00
572	39.02	227.25	1.80	1.00	0.55	138.83	1.16	160.45	0.464	No	No	2.00
573	39.11	224.44	1.81	0.99	0.55	136.82	1.16	158.54	0.451	No	No	2.00
574	39.16	218.51	1.81	0.99	0.55	132.80	1.17	154.99	0.426	No	No	2.00
575	39.23	205.48	1.85	1.02	0.56	123.73	1.20	148.10	0.382	No	No	1.92
576	39.24	200.81	1.85	1.01	0.56	120.69	1.20	145.08	0.364	No	No	1.83

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	39.28	198.62	1.85	1.00	0.56	119.29	1.20	143.39	0.354	No	No	1.78
578	39.32	201.93	1.83	0.94	0.56	121.86	1.18	144.08	0.358	No	No	1.80
579	39.39	194.55	1.84	0.95	0.56	116.84	1.20	139.67	4.000	Yes	No	2.00
580	39.47	183.96	1.88	0.98	0.57	109.44	1.22	133.48	4.000	Yes	No	2.00
581	39.54	171.48	1.92	1.05	0.58	100.68	1.25	125.99	4.000	Yes	No	2.00
582	39.62	158.42	1.98	1.14	0.60	91.63	1.29	117.99	4.000	Yes	No	2.00
583	39.71	145.73	2.03	1.23	0.62	82.95	1.33	110.70	4.000	Yes	No	2.00
584	39.76	134.50	2.08	1.32	0.63	75.46	1.39	105.08	4.000	Yes	No	2.00
585	39.85	125.32	2.13	1.40	0.65	69.36	1.46	101.34	4.000	Yes	No	2.00
586	39.90	117.87	2.17	1.48	0.66	64.48	1.53	98.95	4.000	Yes	No	2.00
587	40.00	111.05	2.20	1.56	0.67	60.00	1.63	97.53	4.000	Yes	No	2.00
588	40.06	104.71	2.24	1.65	0.68	55.91	1.73	96.96	4.000	Yes	No	2.00
589	40.15	98.67	2.28	1.75	0.69	52.00	1.87	97.18	4.000	Yes	No	2.00
590	40.21	92.83	2.33	1.90	0.71	48.24	2.05	98.86	4.000	Yes	No	2.00
591	40.29	86.59	2.39	2.09	0.72	44.24	2.31	102.19	4.000	Yes	No	2.00
592	40.35	79.68	2.46	2.39	0.75	39.85	2.72	108.27	4.000	Yes	No	2.00
593	40.43	72.22	2.53	2.63	0.77	35.37	3.16	111.81	4.000	Yes	No	2.00
594	40.52	63.85	2.60	2.88	0.79	30.51	3.76	114.58	4.000	Yes	Yes	2.00
595	40.58	55.21	2.68	3.09	0.81	25.70	4.47	115.00	4.000	Yes	Yes	2.00
596	40.67	46.88	2.77	3.45	0.84	21.09	5.54	116.83	4.000	Yes	Yes	2.00
597	40.77	41.63	2.85	3.76	0.86	18.24	6.45	117.65	4.000	Yes	Yes	2.00
598	40.84	39.14	2.89	3.94	0.87	16.87	6.99	117.99	4.000	Yes	Yes	2.00
599	40.89	42.28	2.83	3.65	0.86	18.55	6.27	116.25	4.000	Yes	Yes	2.00
600	40.94	49.75	2.72	3.09	0.82	22.62	4.92	111.31	4.000	Yes	Yes	2.00
601	41.03	61.46	2.57	2.48	0.78	29.20	3.53	103.18	4.000	Yes	No	2.00
602	41.08	73.03	2.45	2.07	0.74	35.94	2.68	96.47	4.000	Yes	No	2.00
603	41.14	82.03	2.37	1.83	0.72	41.30	2.24	92.51	4.000	Yes	No	2.00
604	41.22	87.70	2.33	1.71	0.71	44.68	2.04	90.97	4.000	Yes	No	2.00
605	41.28	90.43	2.31	1.68	0.70	46.24	1.97	91.29	0.151	No	No	0.75
606	41.33	91.99	2.32	1.74	0.70	46.96	1.99	93.52	0.156	No	No	0.78
607	41.42	93.64	2.33	1.85	0.71	47.61	2.04	97.02	0.165	No	No	0.82
608	41.47	97.01	2.33	1.94	0.71	49.31	2.04	100.81	0.175	No	No	0.87
609	41.52	104.03	2.31	1.97	0.70	53.17	1.96	104.48	0.186	No	No	0.93
610	41.62	115.47	2.27	1.93	0.69	59.72	1.81	107.92	0.197	No	No	0.98
611	41.67	130.01	2.22	1.88	0.67	68.21	1.66	112.91	0.214	No	No	1.07
612	41.76	144.45	2.17	1.82	0.66	76.74	1.54	118.23	0.234	No	No	1.16
613	41.82	156.39	2.14	1.79	0.65	83.80	1.48	123.75	0.256	No	No	1.28
614	41.90	165.43	2.11	1.76	0.64	89.14	1.44	128.02	0.275	No	No	1.37
615	41.99	171.57	2.10	1.74	0.64	92.73	1.41	131.05	0.289	No	No	1.44
616	42.05	174.81	2.09	1.73	0.63	94.61	1.40	132.58	0.297	No	No	1.48
617	42.15	175.22	2.09	1.74	0.63	94.64	1.40	132.77	0.298	No	No	1.48
618	42.23	173.33	2.10	1.77	0.64	93.24	1.42	132.06	0.294	No	No	1.46
619	42.30	169.55	2.11	1.80	0.64	90.73	1.44	130.51	0.287	No	No	1.43
620	42.38	163.64	2.13	1.84	0.65	86.97	1.47	127.88	0.274	No	No	1.36
621	42.48	153.79	2.16	1.88	0.66	80.87	1.53	123.60	0.256	No	No	1.27
622	42.57	141.98	2.20	1.94	0.67	73.69	1.62	119.15	0.237	No	No	1.18
623	42.64	129.97	2.24	2.01	0.68	66.53	1.73	115.28	0.222	No	No	1.11
624	42.72	121.20	2.27	2.02	0.69	61.42	1.82	111.72	0.210	No	No	1.04

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	42.82	114.72	2.29	1.99	0.69	57.72	1.88	108.24	0.198	No	No	0.98
626	42.90	110.03	2.30	1.96	0.70	55.08	1.91	105.42	0.189	No	No	0.94
627	42.97	106.05	2.31	1.98	0.70	52.74	1.98	104.32	0.186	No	No	0.92
628	43.06	102.31	2.34	2.04	0.71	50.43	2.08	104.69	0.187	No	No	0.93
629	43.15	98.76	2.35	2.01	0.71	48.44	2.11	102.43	0.180	No	No	0.89
630	43.20	97.75	2.34	1.92	0.71	48.00	2.07	99.54	0.172	No	No	0.85
631	43.30	104.19	2.28	1.70	0.69	51.99	1.84	95.67	0.161	No	No	0.80
632	43.40	119.88	2.19	1.51	0.66	61.38	1.58	97.12	0.165	No	No	0.82
633	43.48	132.43	2.13	1.40	0.65	68.91	1.47	100.97	0.176	No	No	0.87
634	43.51	139.11	2.10	1.37	0.64	72.90	1.43	103.89	0.184	No	No	0.92
635	43.52	146.23	2.08	1.34	0.63	77.22	1.39	107.23	0.195	No	No	0.97
636	43.56	160.13	2.03	1.26	0.62	85.83	1.33	114.20	0.219	No	No	1.09
637	43.61	178.86	1.96	1.17	0.60	97.60	1.28	124.81	0.261	No	No	1.30
638	43.67	193.23	1.92	1.11	0.58	106.74	1.25	133.29	0.300	No	No	1.49
639	43.72	206.01	1.88	1.05	0.57	115.04	1.22	140.56	0.338	No	No	1.68
640	43.80	216.51	1.85	1.00	0.56	121.88	1.20	145.95	0.369	No	No	1.83
641	43.85	224.74	1.82	0.97	0.56	127.26	1.18	149.84	0.393	No	No	1.95
642	43.90	231.25	1.81	0.95	0.55	131.51	1.16	152.56	0.410	No	No	2.00
643	43.94	236.38	1.79	0.94	0.55	134.87	1.14	154.37	0.422	No	No	2.00
644	43.99	239.82	1.78	0.92	0.54	137.13	1.13	155.28	0.428	No	No	2.00
645	44.08	241.54	1.78	0.92	0.54	138.11	1.13	155.65	0.431	No	No	2.00
646	44.14	241.51	1.79	0.94	0.54	137.71	1.14	156.49	0.436	No	No	2.00
647	44.22	240.40	1.80	0.97	0.55	136.41	1.15	157.19	0.441	No	No	2.00
648	44.28	238.31	1.82	1.01	0.55	134.50	1.17	157.37	0.442	No	No	2.00
649	44.33	235.67	1.83	1.05	0.56	132.35	1.18	156.78	0.438	No	No	2.00
650	44.40	232.27	1.85	1.10	0.56	129.52	1.20	155.80	0.432	No	No	2.00
651	44.48	231.30	1.87	1.15	0.57	128.25	1.22	155.90	0.432	No	No	2.00
652	44.52	228.57	1.90	1.24	0.58	125.64	1.24	155.24	0.428	No	No	2.00
653	44.61	230.02	1.89	1.23	0.58	126.41	1.23	155.88	0.432	No	No	2.00
654	44.72	231.52	1.90	1.24	0.58	127.03	1.23	156.70	0.438	No	No	2.00
655	44.77	236.14	1.88	1.21	0.57	130.05	1.22	159.04	0.454	No	No	2.00
656	44.91	237.86	1.89	1.24	0.57	130.46	1.23	160.27	0.463	No	No	2.00
657	44.95	231.69	1.91	1.29	0.58	126.16	1.24	156.88	0.439	No	No	2.00
658	45.02	227.41	1.92	1.32	0.59	123.19	1.25	154.33	0.422	No	No	2.00
659	45.04	198.97	2.01	1.51	0.61	104.88	1.32	138.44	0.327	No	No	1.62
660	45.06	203.49	2.00	1.46	0.61	107.81	1.30	140.63	0.339	No	No	1.68
661	45.11	208.45	1.98	1.41	0.60	111.04	1.29	143.03	0.352	No	No	1.75
662	45.15	239.96	1.87	1.20	0.57	131.64	1.22	160.49	0.464	No	No	2.00
663	45.21	246.91	1.85	1.16	0.56	136.23	1.20	163.81	0.489	No	No	2.00
664	45.25	252.44	1.84	1.13	0.56	139.80	1.19	166.43	0.509	No	No	2.00
665	45.30	256.29	1.83	1.13	0.56	142.11	1.18	168.34	0.524	No	No	2.00
666	45.35	258.04	1.83	1.13	0.56	143.02	1.18	169.35	0.532	No	No	2.00
667	45.41	258.42	1.83	1.14	0.56	143.02	1.19	169.64	0.534	No	No	2.00
668	45.49	257.00	1.84	1.15	0.56	141.89	1.19	168.87	0.528	No	No	2.00
669	45.55	254.13	1.84	1.15	0.56	139.97	1.19	167.24	0.515	No	No	2.00
670	45.63	249.51	1.85	1.16	0.56	136.90	1.20	164.52	0.494	No	No	2.00
671	45.69	243.67	1.86	1.16	0.57	133.19	1.21	161.09	0.469	No	No	2.00
672	45.78	236.62	1.88	1.18	0.57	128.61	1.22	156.88	0.439	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	45.84	228.05	1.89	1.18	0.58	123.25	1.23	151.68	0.405	No	No	2.00
674	45.93	217.69	1.91	1.19	0.58	116.85	1.24	145.18	0.365	No	No	1.81
675	46.02	205.11	1.93	1.19	0.59	109.16	1.26	137.24	4.000	Yes	No	2.00
676	46.08	190.40	1.96	1.19	0.60	100.37	1.28	128.00	4.000	Yes	No	2.00
677	46.16	174.41	1.99	1.20	0.61	90.73	1.30	118.20	4.000	Yes	No	2.00
678	46.24	157.13	2.04	1.24	0.62	80.39	1.35	108.31	4.000	Yes	No	2.00
679	46.31	138.07	2.12	1.34	0.64	68.91	1.44	99.54	4.000	Yes	No	2.00
680	46.41	117.36	2.22	1.54	0.67	56.54	1.67	94.32	4.000	Yes	No	2.00
681	46.48	95.77	2.36	1.87	0.72	44.06	2.17	95.41	4.000	Yes	No	2.00
682	46.56	75.72	2.51	2.32	0.76	32.98	3.08	101.49	4.000	Yes	No	2.00
683	46.65	58.08	2.68	2.81	0.81	23.81	4.47	106.39	4.000	Yes	Yes	2.00
684	46.75	45.43	2.81	3.12	0.85	17.64	5.95	104.92	4.000	Yes	Yes	2.00
685	46.84	36.62	2.95	3.29	1.00	12.08	8.01	96.75	4.000	Yes	Yes	2.00
686	46.94	30.75	3.03	3.37	1.00	9.96	9.25	92.20	3.600	No	Yes	2.00
687	47.02	25.79	3.12	3.65	1.00	8.18	10.96	89.65	3.600	No	Yes	2.00
688	47.08	21.37	3.22	4.12	1.00	6.60	13.29	87.68	3.600	No	Yes	2.00
689	47.12	18.76	3.30	4.53	1.00	5.66	15.23	86.24	3.600	No	Yes	2.00
690	47.16	17.85	3.33	4.58	1.00	5.33	15.88	84.67	3.600	No	Yes	2.00
691	47.21	17.81	3.31	4.30	1.00	5.32	15.49	82.35	3.600	No	Yes	2.00
692	47.27	17.46	3.31	4.03	1.00	5.18	15.33	79.44	3.600	No	Yes	2.00
693	47.35	16.42	3.33	3.97	1.00	4.80	15.97	76.72	3.600	No	Yes	2.00
694	47.40	15.74	3.33	3.65	1.00	4.56	15.95	72.71	3.600	No	Yes	2.00
695	47.50	15.37	3.32	3.29	1.00	4.42	15.62	68.97	3.600	No	Yes	2.00
696	47.55	15.16	3.29	2.90	1.00	4.34	15.04	65.28	3.600	No	Yes	2.00
697	47.61	15.00	3.29	2.76	1.00	4.27	14.89	63.67	3.600	No	Yes	2.00
698	47.69	14.73	3.29	2.69	1.00	4.17	15.00	62.57	3.600	No	Yes	2.00
699	47.76	14.39	3.30	2.67	1.00	4.05	15.25	61.71	3.600	No	Yes	2.00
700	47.83	14.02	3.31	2.58	1.00	3.91	15.40	60.22	3.600	No	Yes	2.00
701	47.93	13.85	3.30	2.41	1.00	3.84	15.20	58.40	3.600	No	Yes	2.00
702	48.02	13.82	3.29	2.31	1.00	3.82	15.00	57.34	3.600	No	Yes	2.00
703	48.09	13.88	3.28	2.19	1.00	3.84	14.67	56.35	3.600	No	Yes	2.00
704	48.18	13.85	3.29	2.28	1.00	3.82	14.94	57.05	3.600	No	Yes	2.00
705	48.27	13.88	3.30	2.43	1.00	3.82	15.29	58.44	3.600	No	Yes	2.00
706	48.37	13.98	3.33	2.72	1.00	3.85	15.87	61.09	3.600	No	Yes	2.00
707	48.46	14.12	3.34	2.92	1.00	3.89	16.20	62.98	3.600	No	Yes	2.00
708	48.52	14.18	3.35	3.07	1.00	3.90	16.46	64.25	3.600	No	Yes	2.00
709	48.60	14.25	3.35	3.18	1.00	3.92	16.64	65.23	3.600	No	Yes	2.00
710	48.70	14.38	3.35	3.25	1.00	3.96	16.68	65.99	3.600	No	Yes	2.00
711	48.79	14.65	3.35	3.27	1.00	4.04	16.50	66.70	3.600	No	Yes	2.00
712	48.85	15.06	3.34	3.39	1.00	4.18	16.39	68.42	3.600	No	Yes	2.00
713	48.94	15.74	3.34	3.61	1.00	4.40	16.24	71.44	3.600	No	Yes	2.00
714	49.04	16.68	3.31	3.62	1.00	4.71	15.57	73.34	3.600	No	Yes	2.00
715	49.13	18.30	3.32	4.31	1.00	5.25	15.62	82.09	3.600	No	Yes	2.00
716	49.23	21.13	3.29	4.85	1.00	6.21	14.82	92.00	3.600	No	Yes	2.00
717	49.33	24.04	3.27	5.48	1.00	7.18	14.31	102.80	3.600	No	Yes	2.00
718	49.38	24.88	3.28	6.09	1.00	7.46	14.69	109.60	3.600	No	Yes	2.00
719	49.42	25.93	3.28	6.47	1.00	7.81	14.70	114.80	3.600	No	Yes	2.00
720	49.48	26.70	3.28	6.79	1.00	8.06	14.75	118.93	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	49.53	28.79	3.25	6.60	1.00	8.76	13.86	121.43	3.600	No	Yes	2.00
722	49.58	29.43	3.24	6.72	1.00	8.97	13.78	123.62	3.600	No	Yes	2.00
723	49.63	30.10	3.24	6.80	1.00	9.19	13.66	125.52	3.600	No	Yes	2.00
724	49.72	30.91	3.23	6.72	1.00	9.44	13.37	126.23	3.600	No	Yes	2.00
725	49.77	31.42	3.22	6.60	1.00	9.60	13.13	125.98	3.600	No	Yes	2.00
726	49.83	31.42	3.22	6.55	1.00	9.59	13.08	125.40	3.600	No	Yes	2.00
727	49.92	30.71	3.23	6.62	1.00	9.33	13.37	124.67	3.600	No	Yes	2.00
728	49.97	30.39	3.23	6.56	1.00	9.21	13.41	123.55	3.600	No	Yes	2.00
729	50.04	29.48	3.25	6.66	1.00	8.89	13.80	122.65	3.600	No	Yes	2.00
730	50.11	29.82	3.24	6.56	1.00	8.99	13.61	122.33	3.600	No	Yes	2.00
731	50.20	30.21	3.22	6.30	1.00	9.10	13.25	120.55	3.600	No	Yes	2.00
732	50.27	30.78	3.19	5.73	1.00	9.28	12.51	116.01	3.600	No	Yes	2.00
733	50.34	29.50	3.18	5.11	1.00	8.83	12.20	107.79	3.600	No	Yes	2.00
734	50.45	26.76	3.19	4.68	1.00	7.90	12.55	99.22	3.600	No	Yes	2.00
735	50.54	23.73	3.23	4.48	1.00	6.88	13.43	92.39	3.600	No	Yes	2.00
736	50.59	21.13	3.28	4.47	1.00	6.01	14.59	87.71	3.600	No	Yes	2.00
737	50.68	19.24	3.32	4.43	1.00	5.37	15.59	83.78	3.600	No	Yes	2.00
738	50.79	18.13	3.33	4.26	1.00	4.99	16.06	80.17	3.600	No	Yes	2.00
739	50.88	17.81	3.33	4.10	1.00	4.88	16.03	78.18	3.600	No	Yes	2.00
740	50.98	17.64	3.34	4.11	1.00	4.81	16.19	77.89	3.600	No	Yes	2.00
741	51.07	17.81	3.32	3.85	1.00	4.86	15.67	76.09	3.600	No	Yes	2.00
742	51.17	18.43	3.26	3.21	1.00	5.05	14.19	71.67	3.600	No	Yes	2.00
743	51.24	19.51	3.20	2.74	1.00	5.40	12.74	68.77	3.600	No	Yes	2.00
744	51.33	20.19	3.19	2.81	1.00	5.61	12.56	70.43	3.600	No	Yes	2.00
745	51.46	20.09	3.23	3.28	1.00	5.56	13.45	74.75	3.600	No	Yes	2.00
746	51.46	19.80	3.27	3.71	1.00	5.46	14.31	78.20	3.600	No	Yes	2.00
747	51.51	19.77	3.28	3.88	1.00	5.45	14.62	79.60	3.600	No	Yes	2.00
748	51.56	19.87	3.29	4.15	1.00	5.47	14.98	82.02	3.600	No	Yes	2.00
749	51.65	19.95	3.31	4.41	1.00	5.49	15.35	84.26	3.600	No	Yes	2.00
750	51.71	20.09	3.32	4.71	1.00	5.53	15.72	86.89	3.600	No	Yes	2.00
751	51.79	20.49	3.32	4.86	1.00	5.65	15.73	88.80	3.600	No	Yes	2.00
752	51.85	21.23	3.32	5.11	1.00	5.88	15.68	92.19	3.600	No	Yes	2.00
753	51.94	22.11	3.32	5.42	1.00	6.15	15.66	96.33	3.600	No	Yes	2.00
754	51.99	23.22	3.32	5.95	1.00	6.51	15.77	102.62	3.600	No	Yes	2.00
755	52.09	24.17	3.33	6.60	1.00	6.80	16.12	109.52	3.600	No	Yes	2.00
756	52.19	27.74	3.28	6.62	1.00	7.93	14.73	116.81	3.600	No	Yes	2.00
757	52.28	33.34	3.20	6.19	1.00	9.72	12.62	122.63	3.600	No	Yes	2.00
758	52.35	36.42	3.17	6.29	1.00	10.69	12.02	128.41	3.600	No	Yes	2.00
759	52.43	37.06	3.18	6.64	1.00	10.87	12.22	132.82	3.600	No	Yes	2.00
760	52.52	35.17	3.22	7.33	1.00	10.25	13.30	136.28	3.600	No	Yes	2.00
761	52.62	35.61	3.22	7.23	1.00	10.37	13.11	135.93	3.600	No	Yes	2.00
762	52.72	35.98	3.20	6.96	1.00	10.46	12.80	133.92	3.600	No	Yes	2.00
763	52.81	34.26	3.24	7.47	1.00	9.89	13.70	135.53	3.600	No	Yes	2.00
764	52.91	31.32	3.34	9.52	1.00	8.94	16.37	146.31	3.600	No	Yes	2.00
765	53.00	37.23	3.27	9.04	1.00	10.79	14.34	154.70	3.600	No	Yes	2.00
766	53.10	62.36	2.95	5.53	1.00	18.71	7.92	148.13	4.000	Yes	Yes	2.00
767	53.20	108.21	2.62	3.37	1.00	33.14	3.92	129.79	4.000	Yes	Yes	2.00
768	53.29	163.78	2.38	2.36	1.00	50.57	2.27	114.61	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	53.38	213.88	2.24	1.98	1.00	66.21	1.72	114.09	4.000	Yes	No	2.00
770	53.46	260.07	2.14	1.75	1.00	80.59	1.49	119.81	4.000	Yes	No	2.00
771	53.53	292.05	2.12	1.83	1.00	90.48	1.45	130.93	4.000	Yes	No	2.00
772	53.63	323.19	2.09	1.82	1.00	100.02	1.40	139.93	4.000	Yes	No	2.00
773	53.73	361.79	2.01	1.58	1.00	111.85	1.31	146.92	4.000	Yes	No	2.00
774	53.82	388.35	1.92	1.28	1.00	119.89	1.25	150.03	4.000	Yes	No	2.00
775	53.92	387.71	1.89	1.12	1.00	119.45	1.23	146.54	4.000	Yes	No	2.00
776	53.94	360.18	1.92	1.15	1.00	110.85	1.25	138.23	0.326	No	No	1.66
777	53.96	336.26	1.95	1.19	1.00	103.38	1.27	131.20	0.290	No	No	1.48
778	53.97	349.08	1.92	1.12	1.00	107.34	1.25	134.16	0.305	No	No	1.55
779	54.05	377.59	1.87	1.03	1.00	116.04	1.22	141.00	0.341	No	No	1.73
780	54.08	426.28	1.79	0.91	1.00	131.09	1.15	150.15	0.395	No	No	2.00
781	54.13	473.21	1.74	0.84	1.00	145.55	1.06	154.41	0.422	No	No	2.00
782	54.19	518.79	1.70	0.83	1.00	159.56	1.00	159.56	0.458	No	No	2.00
783	54.25	524.22	1.71	0.86	1.00	161.12	1.01	162.94	0.482	No	No	2.00
784	54.28	510.87	1.74	0.91	1.00	156.95	1.06	166.66	0.510	No	No	2.00
785	54.29	486.82	1.76	0.94	1.00	149.48	1.10	164.40	0.493	No	No	2.00
786	54.34	486.89	1.76	0.94	1.00	149.42	1.10	164.35	0.493	No	No	2.00
787	54.35	492.20	1.75	0.93	1.00	151.05	1.09	164.72	0.496	No	No	2.00
788	54.40	504.89	1.74	0.91	1.00	154.89	1.07	165.62	0.503	No	No	2.00
789	54.44	522.30	1.72	0.90	1.00	160.18	1.04	166.45	0.509	No	No	2.00
790	54.49	535.62	1.71	0.88	1.00	164.19	1.01	165.88	0.505	No	No	2.00
791	54.53	546.25	1.70	0.87	1.00	167.39	1.00	167.39	0.516	No	No	2.00
792	54.57	558.27	1.69	0.87	1.00	171.02	1.00	171.02	0.545	No	No	2.00
793	54.58	567.78	1.70	0.89	1.00	173.92	1.00	173.92	0.569	No	No	2.00
794	54.63	560.90	1.71	0.92	1.00	171.71	1.01	173.90	0.569	No	No	2.00
795	54.68	536.31	1.75	0.99	1.00	164.04	1.08	176.93	0.595	No	No	2.00
796	54.73	510.50	1.78	1.03	1.00	156.00	1.12	175.12	0.579	No	No	2.00
797	54.78	499.67	1.79	1.04	1.00	152.59	1.14	173.29	0.564	No	No	2.00
798	54.83	493.63	1.80	1.06	1.00	150.64	1.15	172.82	0.560	No	No	2.00
799	54.88	497.14	1.80	1.09	1.00	151.64	1.15	175.08	0.579	No	No	2.00
800	54.92	500.68	1.81	1.15	1.00	152.65	1.17	178.37	0.608	No	No	2.00
801	54.97	510.81	1.81	1.14	1.00	155.66	1.16	180.73	0.629	No	No	2.00
802	55.02	513.44	1.81	1.15	1.00	156.38	1.16	181.62	0.637	No	No	2.00
803	55.12	487.90	1.85	1.25	1.00	148.39	1.20	178.01	0.605	No	No	2.00
804	55.17	449.17	1.92	1.45	1.00	136.44	1.25	170.63	0.542	No	No	2.00
805	55.25	410.54	1.98	1.59	1.00	124.51	1.29	160.49	0.464	No	No	2.00
806	55.31	394.21	1.98	1.55	1.00	119.43	1.29	154.46	0.423	No	No	2.00
807	55.36	388.18	1.95	1.35	1.00	117.52	1.27	148.87	0.387	No	No	1.98
808	55.45	381.09	1.91	1.20	1.00	115.23	1.25	143.68	0.356	No	No	1.82
809	55.50	365.91	1.92	1.15	1.00	110.54	1.25	137.89	0.324	No	No	1.66
810	55.60	351.24	1.94	1.19	1.00	105.95	1.26	133.93	0.303	No	No	1.56
811	55.65	332.24	1.96	1.21	1.00	100.11	1.28	128.15	0.276	No	No	1.41
812	55.71	324.14	1.96	1.15	1.00	97.58	1.27	124.39	0.259	No	No	1.33
813	55.75	320.40	1.93	1.03	1.00	96.40	1.26	121.19	0.246	No	No	1.26
814	55.79	325.12	1.91	0.99	1.00	97.79	1.25	121.90	0.248	No	No	1.27
815	55.84	332.47	1.90	0.97	1.00	99.97	1.24	123.76	0.256	No	No	1.32
816	55.89	338.01	1.90	0.97	1.00	101.60	1.23	125.39	0.263	No	No	1.35

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	55.90	341.15	1.89	0.96	1.00	102.54	1.23	126.17	0.267	No	No	1.37
818	55.94	336.26	1.90	0.98	1.00	101.02	1.24	124.98	0.262	No	No	1.34
819	55.99	327.63	1.92	1.01	1.00	98.34	1.25	122.89	0.253	No	No	1.30
820	56.03	317.88	1.94	1.05	1.00	95.34	1.26	120.41	0.242	No	No	1.24
821	56.08	311.67	1.95	1.06	1.00	93.40	1.27	118.54	0.235	No	No	1.21
822	56.14	306.37	1.95	1.05	1.00	91.74	1.27	116.74	0.228	No	No	1.17
823	56.22	299.89	1.96	1.06	1.00	89.70	1.28	114.65	0.220	No	No	1.13
824	56.28	294.29	1.97	1.06	1.00	87.95	1.28	112.90	0.214	No	No	1.10
825	56.33	292.57	1.97	1.06	1.00	87.39	1.29	112.38	0.212	No	No	1.09
826	56.38	294.06	1.97	1.04	1.00	87.79	1.28	112.46	0.212	No	No	1.09
827	56.45	301.34	1.95	1.02	1.00	89.92	1.27	114.23	0.219	No	No	1.13
828	56.52	312.58	1.93	0.98	1.00	93.24	1.25	117.01	0.229	No	No	1.18
829	56.62	325.19	1.90	0.94	1.00	96.94	1.24	120.21	0.242	No	No	1.24
830	56.66	338.42	1.87	0.89	1.00	100.88	1.22	123.02	0.253	No	No	1.30
831	56.73	350.06	1.87	0.90	1.00	104.30	1.21	126.65	0.269	No	No	1.39
832	56.81	357.11	1.87	0.94	1.00	106.33	1.22	129.59	0.282	No	No	1.46
833	56.95	363.42	1.89	1.01	1.00	108.06	1.23	132.64	0.297	No	No	1.53
834	57.00	372.46	1.88	1.03	1.00	110.72	1.23	135.80	0.313	No	No	1.61
835	57.09	373.11	1.89	1.06	1.00	110.80	1.23	136.52	0.317	No	No	1.63
836	57.19	368.58	1.91	1.10	1.00	109.32	1.24	135.85	0.313	No	No	1.62
837	57.27	354.04	1.92	1.11	1.00	104.88	1.25	131.44	0.291	No	No	1.50
838	57.35	357.65	1.89	0.99	1.00	105.87	1.23	130.16	0.285	No	No	1.47
839	57.44	356.17	1.86	0.89	1.00	105.33	1.21	127.36	0.272	No	No	1.41
840	57.50	364.37	1.83	0.81	1.00	107.70	1.18	127.07	0.271	No	No	1.40
841	57.52	378.10	1.83	0.84	1.00	111.77	1.18	131.85	0.293	No	No	1.52
842	57.58	409.37	1.82	0.90	1.00	121.03	1.17	141.73	0.345	No	No	1.78
843	57.63	432.08	1.81	0.95	1.00	127.73	1.17	149.17	0.389	No	No	2.00
844	57.72	439.00	1.81	0.96	1.00	129.66	1.17	151.31	0.402	No	No	2.00
845	57.77	433.73	1.80	0.92	1.00	128.03	1.16	148.26	0.383	No	No	1.98
846	57.82	429.55	1.78	0.84	1.00	126.71	1.13	143.29	0.354	No	No	1.83
847	57.91	436.73	1.74	0.73	1.00	128.72	1.06	137.09	0.320	No	No	1.66
848	57.96	442.84	1.69	0.63	1.00	130.46	1.00	130.46	0.287	No	No	1.48
849	58.02	458.90	1.66	0.57	1.00	135.16	1.00	135.16	0.310	No	No	1.61
850	58.09	469.26	1.65	0.56	1.00	138.12	1.00	138.12	0.325	No	No	1.69
851	58.16	484.88	1.63	0.56	1.00	142.65	1.00	142.65	0.350	No	No	1.82
852	58.25	491.12	1.64	0.58	1.00	144.36	1.00	144.36	0.360	No	No	1.87
853	58.30	487.65	1.66	0.63	1.00	143.26	1.00	143.26	0.353	No	No	1.83
854	58.40	479.62	1.69	0.68	1.00	140.74	1.00	140.74	0.339	No	No	1.76
855	58.50	468.52	1.71	0.72	1.00	137.31	1.02	139.77	0.334	No	No	1.74
856	58.56	467.50	1.71	0.71	1.00	136.92	1.01	138.70	0.328	No	No	1.71
857	58.64	464.81	1.72	0.73	1.00	136.01	1.03	140.28	0.337	No	No	1.75
858	58.73	474.79	1.73	0.77	1.00	138.81	1.05	145.16	0.364	No	No	1.90
859	58.78	488.15	1.72	0.76	1.00	142.67	1.02	145.87	0.369	No	No	1.92
860	58.88	506.71	1.69	0.74	1.00	147.98	1.00	147.98	0.381	No	No	1.98
861	58.97	511.03	1.66	0.67	1.00	149.10	1.00	149.10	0.388	No	No	2.00
862	59.07	506.24	1.66	0.64	1.00	147.53	1.00	147.53	0.379	No	No	1.97
863	59.13	493.59	1.65	0.61	1.00	143.73	1.00	143.73	0.356	No	No	1.86
864	59.23	484.71	1.65	0.59	1.00	140.99	1.00	140.99	0.341	No	No	1.78

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	59.31	464.47	1.65	0.56	1.00	134.94	1.00	134.94	0.308	No	No	1.61
866	59.38	450.35	1.65	0.54	1.00	130.71	1.00	130.71	0.288	No	No	1.50
867	59.41	439.19	1.66	0.53	1.00	127.40	1.00	127.40	0.272	No	No	1.42
868	59.46	443.57	1.65	0.53	1.00	128.62	1.00	128.62	0.278	No	No	1.45
869	59.51	443.56	1.65	0.52	1.00	128.55	1.00	128.55	0.278	No	No	1.45
870	59.57	451.89	1.67	0.58	1.00	130.91	1.00	130.91	0.289	No	No	1.51
871	59.66	471.05	1.67	0.61	1.00	136.37	1.00	136.37	0.316	No	No	1.65
872	59.75	492.31	1.70	0.71	1.00	142.44	1.00	142.44	0.349	No	No	1.82
873	59.80	506.48	1.71	0.77	1.00	146.48	1.01	147.84	0.380	No	No	1.99
874	59.85	508.64	1.74	0.86	1.00	147.04	1.07	156.99	0.440	No	No	2.00
875	59.91	504.22	1.75	0.88	1.00	145.65	1.08	158.02	0.447	No	No	2.00
876	59.99	498.85	1.77	0.91	1.00	143.96	1.11	159.53	0.458	No	No	2.00
877	60.05	480.97	1.81	1.03	1.00	138.68	1.17	161.59	0.472	No	No	2.00
878	60.09	464.78	1.85	1.12	1.00	133.92	1.20	160.52	0.465	No	No	2.00
879	60.14	444.43	1.88	1.17	1.00	127.94	1.22	156.08	0.434	No	No	2.00
880	60.19	437.86	1.87	1.13	1.00	125.96	1.22	153.23	0.415	No	No	2.00
881	60.22	434.25	1.87	1.11	1.00	124.88	1.21	151.55	0.404	No	No	2.00
882	60.28	412.99	1.89	1.13	1.00	118.63	1.23	145.94	0.369	No	No	1.93
883	60.33	381.24	1.93	1.19	1.00	109.36	1.26	137.48	0.322	No	No	1.69
884	60.38	338.97	2.00	1.32	1.00	97.07	1.31	126.83	0.270	No	No	1.41
885	60.42	309.75	2.05	1.40	1.00	88.57	1.35	119.65	0.239	No	No	1.25
886	60.48	282.02	2.07	1.37	1.00	80.50	1.38	111.02	0.207	No	No	1.09
887	60.57	262.48	2.05	1.17	1.00	74.78	1.36	101.50	0.177	No	No	0.93
888	60.66	243.89	2.02	0.93	1.00	69.35	1.32	91.67	0.152	No	No	0.80
889	60.68	232.16	1.99	0.79	1.00	65.95	1.30	85.85	0.139	No	No	0.73
890	60.69	225.51	1.98	0.72	1.00	64.02	1.29	82.84	0.133	No	No	0.70
891	60.74	217.75	1.99	0.69	1.00	61.75	1.30	80.07	0.128	No	No	0.67
892	60.79	206.27	2.00	0.66	1.00	58.41	1.30	76.18	0.121	No	No	0.64
893	60.84	192.16	2.02	0.64	1.00	54.32	1.32	71.82	0.114	No	No	0.60
894	60.89	182.35	2.03	0.62	1.00	51.47	1.33	68.64	0.110	No	No	0.58
895	60.98	174.35	2.05	0.63	1.00	49.12	1.36	66.57	0.107	No	No	0.56
896	61.03	168.07	2.13	0.84	1.00	47.30	1.46	69.19	0.111	No	No	0.58
897	61.08	164.86	2.24	1.28	1.00	46.35	1.72	79.69	0.127	No	No	0.67
898	61.18	164.63	2.31	1.64	1.00	46.24	1.95	90.12	0.148	No	No	0.78
899	61.23	168.20	2.35	1.96	1.00	47.23	2.12	100.04	0.173	No	No	0.91
900	61.31	194.08	2.24	1.58	1.00	54.62	1.72	94.03	0.157	No	No	0.83
901	61.42	236.42	2.09	1.19	1.00	66.70	1.41	94.11	0.158	No	No	0.83
902	61.47	287.17	1.90	0.74	1.00	81.21	1.24	100.64	0.175	No	No	0.92
903	61.51	331.30	1.79	0.58	1.00	93.81	1.14	107.25	0.195	No	No	1.03
904	61.54	366.14	1.73	0.52	1.00	103.76	1.05	108.54	0.199	No	No	1.05
905	61.57	395.83	1.70	0.53	1.00	112.23	1.00	112.23	0.211	No	No	1.11
906	61.58	418.64	1.67	0.50	1.00	118.74	1.00	118.74	0.236	No	No	1.24
907	61.61	393.43	1.70	0.50	1.00	111.49	1.00	111.49	0.209	No	No	1.10
908	61.63	367.65	1.72	0.50	1.00	104.10	1.03	107.07	0.194	No	No	1.02
909	61.63	257.89	1.94	0.73	1.00	72.70	1.26	91.77	0.152	No	No	0.80
910	61.66	191.36	2.14	1.04	1.00	53.66	1.48	79.27	0.126	No	No	0.67
911	61.67	129.55	2.40	1.69	1.00	35.97	2.37	85.35	0.138	No	No	0.73
912	61.70	152.96	2.31	1.50	1.00	42.66	1.96	83.80	0.135	No	No	0.71

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	61.71	180.90	2.22	1.34	1.00	50.64	1.67	84.55	0.136	No	No	0.72
914	61.76	206.41	2.15	1.24	1.00	57.90	1.51	87.45	0.142	No	No	0.75
915	61.80	228.84	2.10	1.15	1.00	64.28	1.42	91.10	0.150	No	No	0.79
916	61.84	250.40	2.03	1.01	1.00	70.41	1.34	94.04	0.157	No	No	0.83
917	61.86	279.75	1.93	0.78	1.00	78.77	1.26	98.87	0.170	No	No	0.90
918	61.93	312.34	1.82	0.60	1.00	88.02	1.18	103.69	0.184	No	No	0.97
919	61.98	357.76	1.73	0.50	1.00	100.92	1.00	100.92	0.176	No	No	0.93
920	62.04	405.56	1.68	0.50	1.00	114.48	1.00	114.48	0.220	No	No	1.16
921	62.09	451.78	1.64	0.49	1.00	127.59	1.00	127.59	0.273	No	No	1.44
922	62.14	481.91	1.62	0.49	1.00	136.10	1.00	136.10	0.314	No	No	1.66
923	62.19	499.12	1.60	0.47	1.00	140.93	1.00	140.93	0.340	No	No	1.80
924	62.24	508.93	1.59	0.47	1.00	143.65	1.00	143.65	0.356	No	No	1.88
925	62.26	519.32	1.58	0.47	1.00	146.58	1.00	146.58	0.373	No	No	1.97
926	62.29	519.05	1.58	0.47	1.00	146.46	1.00	146.46	0.372	No	No	1.97
927	62.38	515.71	1.60	0.51	1.00	145.37	1.00	145.37	0.366	No	No	1.93
928	62.44	490.28	1.65	0.57	1.00	138.07	1.00	138.07	0.325	No	No	1.72
929	62.46	469.07	1.69	0.62	1.00	132.02	1.00	132.02	0.294	No	No	1.55
930	62.47	448.15	1.70	0.62	1.00	126.07	1.00	126.07	0.266	No	No	1.41
931	62.51	453.68	1.69	0.61	1.00	127.59	1.00	127.59	0.273	No	No	1.44
932	62.56	463.98	1.69	0.61	1.00	130.45	1.00	130.45	0.286	No	No	1.52
933	62.60	477.62	1.68	0.62	1.00	134.26	1.00	134.26	0.305	No	No	1.61
934	62.65	481.73	1.68	0.62	1.00	135.35	1.00	135.35	0.311	No	No	1.64
935	62.70	482.34	1.66	0.58	1.00	135.46	1.00	135.46	0.311	No	No	1.65
936	62.75	483.05	1.65	0.56	1.00	135.59	1.00	135.59	0.312	No	No	1.65
937	62.80	494.83	1.64	0.55	1.00	138.85	1.00	138.85	0.329	No	No	1.74
938	62.85	525.29	1.60	0.52	1.00	147.40	1.00	147.40	0.378	No	No	2.00
939	62.89	569.18	1.56	0.50	1.00	159.73	1.00	159.73	0.459	No	No	2.00
940	62.97	619.66	1.54	0.51	1.00	173.86	1.00	173.86	0.569	No	No	2.00
941	63.04	667.84	1.52	0.52	1.00	187.32	1.00	187.32	0.691	No	No	2.00
942	63.09	703.12	1.50	0.52	1.00	197.18	1.00	197.18	0.793	No	No	2.00
943	63.13	715.51	1.51	0.54	1.00	200.57	1.00	200.57	4.000	No	No	2.00
944	63.19	716.52	1.54	0.60	1.00	200.74	1.00	200.74	4.000	No	No	2.00
945	63.23	720.23	1.57	0.67	1.00	201.69	1.00	201.69	4.000	No	No	2.00
946	63.28	726.78	1.59	0.73	1.00	203.42	1.00	203.42	4.000	No	No	2.00
947	63.32	729.18	1.57	0.68	1.00	204.02	1.00	204.02	4.000	No	No	2.00
948	63.38	725.67	1.49	0.51	1.00	202.89	1.00	202.89	4.000	No	No	2.00
949	63.44	726.68	1.43	0.41	1.00	203.06	1.00	203.06	4.000	No	No	2.00
950	63.52	715.48	1.43	0.40	1.00	199.75	1.00	199.75	0.821	No	No	2.00
951	63.57	697.37	1.49	0.49	1.00	194.57	1.00	194.57	0.765	No	No	2.00
952	63.66	659.58	1.52	0.51	1.00	183.79	1.00	183.79	0.657	No	No	2.00
953	63.73	534.95	1.63	0.58	1.00	148.76	1.00	148.76	0.386	No	No	2.00
954	63.76	455.61	1.72	0.67	1.00	126.50	1.03	130.54	0.287	No	No	1.53
955	63.76	411.85	1.77	0.71	1.00	114.24	1.12	127.66	0.274	No	No	1.45
956	63.78	471.87	1.70	0.64	1.00	131.02	1.00	131.02	0.289	No	No	1.54
957	63.81	512.86	1.67	0.65	1.00	142.46	1.00	142.46	0.349	No	No	1.86
958	63.85	526.43	1.68	0.68	1.00	146.19	1.00	146.19	0.371	No	No	1.97
959	63.86	522.58	1.70	0.74	1.00	145.10	1.00	145.10	0.364	No	No	1.94
960	63.91	497.92	1.74	0.81	1.00	138.14	1.07	148.35	0.384	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
961	63.94	483.78	1.77	0.87	1.00	134.14	1.12	150.35	0.396	No	No	2.00
962	63.95	480.34	1.79	0.90	1.00	133.15	1.14	151.38	0.403	No	No	2.00
963	64.00	476.26	1.79	0.91	1.00	131.94	1.14	150.67	0.398	No	No	2.00
964	64.02	473.22	1.79	0.89	1.00	131.08	1.14	149.37	0.390	No	No	2.00
965	64.05	475.78	1.78	0.86	1.00	131.75	1.12	148.02	0.382	No	No	2.00
966	64.09	478.18	1.77	0.83	1.00	132.36	1.11	146.64	0.373	No	No	1.99
967	64.11	480.07	1.75	0.80	1.00	132.86	1.09	144.77	0.362	No	No	1.93
968	64.15	482.26	1.74	0.77	1.00	133.43	1.07	142.44	0.349	No	No	1.86
969	64.20	494.31	1.72	0.74	1.00	136.71	1.03	141.24	0.342	No	No	1.82
970	64.25	512.59	1.70	0.72	1.00	141.74	1.00	141.74	0.345	No	No	1.84
971	64.29	535.70	1.68	0.70	1.00	148.11	1.00	148.11	0.382	No	No	2.00
972	64.34	570.38	1.64	0.65	1.00	157.68	1.00	157.68	0.445	No	No	2.00
973	64.43	605.81	1.60	0.60	1.00	167.40	1.00	167.40	0.516	No	No	2.00
974	64.48	630.95	1.56	0.56	1.00	174.30	1.00	174.30	0.572	No	No	2.00
975	64.53	642.69	1.53	0.51	1.00	177.47	1.00	177.47	0.600	No	No	2.00
976	64.58	655.07	1.52	0.49	1.00	180.82	1.00	180.82	0.630	No	No	2.00
977	64.63	680.65	1.51	0.49	1.00	187.83	1.00	187.83	0.696	No	No	2.00
978	64.68	709.63	1.52	0.55	1.00	195.77	1.00	195.77	0.778	No	No	2.00
979	64.73	718.74	1.53	0.57	1.00	198.20	1.00	198.20	0.804	No	No	2.00
980	64.77	735.60	1.51	0.56	1.00	202.79	1.00	202.79	4.000	No	No	2.00
981	64.82	751.19	1.48	0.51	1.00	207.01	1.00	207.01	4.000	No	No	2.00
982	64.87	732.64	1.49	0.51	1.00	201.76	1.00	201.76	4.000	No	No	2.00
983	64.89	713.98	1.50	0.52	1.00	196.56	1.00	196.56	0.786	No	No	2.00
984	64.93	689.59	1.53	0.54	1.00	189.73	1.00	189.73	0.715	No	No	2.00
985	64.94	715.81	1.51	0.53	1.00	196.96	1.00	196.96	0.791	No	No	2.00
986	64.98	725.69	1.50	0.53	1.00	199.62	1.00	199.62	0.820	No	No	2.00
987	64.99	734.03	1.50	0.52	1.00	201.90	1.00	201.90	4.000	No	No	2.00
988	65.03	732.37	1.50	0.52	1.00	201.35	1.00	201.35	4.000	No	No	2.00
989	65.08	727.04	1.49	0.50	1.00	199.79	1.00	199.79	0.822	No	No	2.00
990	65.13	715.51	1.48	0.47	1.00	196.50	1.00	196.50	0.786	No	No	2.00
991	65.17	703.60	1.46	0.43	1.00	193.13	1.00	193.13	0.750	No	No	2.00
992	65.22	689.29	1.45	0.41	1.00	189.08	1.00	189.08	0.709	No	No	2.00
993	65.23	681.55	1.45	0.40	1.00	186.93	1.00	186.93	0.687	No	No	2.00
994	65.28	679.28	1.46	0.40	1.00	186.22	1.00	186.22	0.681	No	No	2.00
995	65.32	679.65	1.47	0.43	1.00	186.24	1.00	186.24	0.681	No	No	2.00
996	65.37	680.17	1.49	0.45	1.00	186.30	1.00	186.30	0.681	No	No	2.00
997	65.42	684.61	1.50	0.48	1.00	187.42	1.00	187.42	0.692	No	No	2.00
998	65.47	671.65	1.50	0.48	1.00	183.76	1.00	183.76	0.657	No	No	2.00
999	65.48	657.21	1.52	0.49	1.00	179.77	1.00	179.77	0.620	No	No	2.00
1000	65.49	638.86	1.52	0.48	1.00	174.70	1.00	174.70	0.576	No	No	2.00
1001	65.52	636.56	1.52	0.47	1.00	174.01	1.00	174.01	0.570	No	No	2.00
1002	65.57	645.67	1.41	0.30	1.00	176.43	1.00	176.43	0.591	No	No	2.00
1003	65.62	661.16	1.28	0.15	1.00	180.61	1.00	180.61	0.628	No	No	2.00
1004	65.67	682.44	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1005	65.69	697.23	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1006	65.72	719.02	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1007	65.77	752.26	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1008	65.82	790.78	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1009	65.86	811.97	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1010	65.86	833.63	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1011	65.91	854.04	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1012	65.96	878.41	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_t: Total cone resistance
I_c: Soil behavior type index
Fr: Normalized friction ratio (%)
n: Stress exponent
Q_{tn}: Normalized cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
0.01	2.00	0.00	0.00	0.03	0.00	0.04	2.00	0.00	0.00	0.03	0.00
0.08	2.00	0.00	0.00	0.04	0.00	0.10	2.00	0.00	0.00	0.02	0.00
0.13	2.00	0.00	0.00	0.03	0.00	0.18	2.00	0.00	0.00	0.04	0.00
0.22	2.00	0.00	0.00	0.05	0.00	0.27	2.00	0.00	0.00	0.05	0.00
0.33	2.00	0.00	0.00	0.05	0.00	0.36	2.00	0.00	0.00	0.03	0.00
0.37	2.00	0.00	0.00	0.01	0.00	0.38	2.00	0.00	0.00	0.01	0.00
0.42	2.00	0.00	0.00	0.04	0.00	0.44	2.00	0.00	0.00	0.03	0.00
0.47	2.00	0.00	0.00	0.02	0.00	0.47	2.00	0.00	0.00	0.01	0.00
0.52	2.00	0.00	0.00	0.04	0.00	0.56	2.00	0.00	0.00	0.05	0.00
0.58	2.00	0.00	0.00	0.01	0.00	0.61	2.00	0.00	0.00	0.03	0.00
0.66	2.00	0.00	0.00	0.05	0.00	0.76	2.00	0.00	0.00	0.09	0.00
0.80	2.00	0.00	0.00	0.05	0.00	0.81	2.00	0.00	0.00	0.01	0.00
0.85	2.00	0.00	0.00	0.04	0.00	0.86	2.00	0.00	0.00	0.01	0.00
0.90	2.00	0.00	0.00	0.04	0.00	0.95	2.00	0.00	0.00	0.04	0.00
1.00	2.00	0.00	0.00	0.05	0.00	1.05	2.00	0.00	0.00	0.06	0.00
1.14	2.00	0.00	0.00	0.09	0.00	1.24	2.00	0.00	0.00	0.09	0.00
1.31	2.00	0.00	0.00	0.08	0.00	1.36	2.00	0.00	0.00	0.05	0.00
1.37	2.00	0.00	0.00	0.01	0.00	1.39	2.00	0.00	0.00	0.02	0.00
1.43	2.00	0.00	0.00	0.04	0.00	1.44	2.00	0.00	0.00	0.01	0.00
1.49	2.00	0.00	0.00	0.06	0.00	1.53	2.00	0.00	0.00	0.04	0.00
1.58	2.00	0.00	0.00	0.05	0.00	1.63	2.00	0.00	0.00	0.05	0.00
1.68	2.00	0.00	0.00	0.05	0.00	1.72	2.00	0.00	0.00	0.05	0.00
1.77	2.00	0.00	0.00	0.05	0.00	1.82	2.00	0.00	0.00	0.05	0.00
1.86	2.00	0.00	0.00	0.04	0.00	1.92	2.00	0.00	0.00	0.05	0.00
1.97	2.00	0.00	0.00	0.05	0.00	2.01	2.00	0.00	0.00	0.05	0.00
2.09	2.00	0.00	0.00	0.07	0.00	2.16	2.00	0.00	0.00	0.07	0.00
2.20	2.00	0.00	0.00	0.04	0.00	2.25	2.00	0.00	0.00	0.05	0.00
2.31	2.00	0.00	0.00	0.06	0.00	2.37	2.00	0.00	0.00	0.06	0.00
2.40	2.00	0.00	0.00	0.03	0.00	2.46	2.00	0.00	0.00	0.06	0.00
2.54	2.00	0.00	0.00	0.08	0.00	2.59	2.00	0.00	0.00	0.05	0.00
2.69	2.00	0.00	0.00	0.10	0.00	2.74	2.00	0.00	0.00	0.05	0.00
2.83	2.00	0.00	0.00	0.10	0.00	2.88	2.00	0.00	0.00	0.05	0.00
2.98	2.00	0.00	0.00	0.10	0.00	3.03	2.00	0.00	0.00	0.05	0.00
3.12	2.00	0.00	0.00	0.08	0.00	3.21	2.00	0.00	0.00	0.09	0.00
3.27	2.00	0.00	0.00	0.06	0.00	3.34	2.00	0.00	0.00	0.08	0.00
3.41	2.00	0.00	0.00	0.07	0.00	3.51	2.00	0.00	0.00	0.10	0.00
3.55	2.00	0.00	0.00	0.05	0.00	3.65	2.00	0.00	0.00	0.10	0.00
3.75	2.00	0.00	0.00	0.10	0.00	3.83	2.00	0.00	0.00	0.09	0.00
3.94	2.00	0.00	0.00	0.10	0.00	4.04	2.00	0.00	0.00	0.10	0.00
4.13	2.00	0.00	0.00	0.09	0.00	4.24	2.00	0.00	0.00	0.11	0.00
4.38	2.00	0.00	0.00	0.13	0.00	4.50	2.00	0.00	0.00	0.12	0.00
4.62	2.00	0.00	0.00	0.12	0.00	4.71	2.00	0.00	0.00	0.10	0.00
4.75	2.00	0.00	0.00	0.04	0.00	4.84	2.00	0.00	0.00	0.08	0.00
4.89	2.00	0.00	0.00	0.05	0.00	4.94	2.00	0.00	0.00	0.05	0.00
4.98	2.00	0.00	0.00	0.04	0.00	5.07	2.00	0.00	0.00	0.09	0.00
5.13	2.00	0.00	0.00	0.05	0.00	5.17	2.00	0.00	0.00	0.05	0.00
5.27	2.00	0.00	0.00	0.09	0.00	5.32	2.00	0.00	0.00	0.05	0.00
5.42	2.00	0.00	0.00	0.10	0.00	5.46	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
5.56	2.00	0.00	0.00	0.10	0.00	5.61	2.00	0.00	0.00	0.05	0.00
5.71	2.00	0.00	0.00	0.09	0.00	5.78	2.00	0.00	0.00	0.08	0.00
5.85	2.00	0.00	0.00	0.07	0.00	5.95	2.00	0.00	0.00	0.10	0.00
6.00	2.00	0.00	0.00	0.05	0.00	6.09	2.00	0.00	0.00	0.10	0.00
6.14	2.00	0.00	0.00	0.05	0.00	6.24	2.00	0.00	0.00	0.09	0.00
6.30	2.00	0.00	0.00	0.06	0.00	6.38	2.00	0.00	0.00	0.09	0.00
6.46	2.00	0.00	0.00	0.08	0.00	6.50	2.00	0.00	0.00	0.04	0.00
6.56	2.00	0.00	0.00	0.07	0.00	6.63	2.00	0.00	0.00	0.06	0.00
6.68	2.00	0.00	0.00	0.05	0.00	6.76	2.00	0.00	0.00	0.08	0.00
6.82	2.00	0.00	0.00	0.06	0.00	6.88	2.00	0.00	0.00	0.06	0.00
6.96	2.00	0.00	0.00	0.08	0.00	7.03	2.00	0.00	0.00	0.07	0.00
7.11	2.00	0.00	0.00	0.08	0.00	7.16	2.00	0.00	0.00	0.05	0.00
7.26	2.00	0.00	0.00	0.10	0.00	7.31	2.00	0.00	0.00	0.05	0.00
7.40	2.00	0.00	0.00	0.09	0.00	7.45	2.00	0.00	0.00	0.05	0.00
7.54	2.00	0.00	0.00	0.09	0.00	7.60	2.00	0.00	0.00	0.06	0.00
7.68	2.00	0.00	0.00	0.09	0.00	7.74	2.00	0.00	0.00	0.05	0.00
7.83	2.00	0.00	0.00	0.09	0.00	7.90	2.00	0.00	0.00	0.07	0.00
7.98	2.00	0.00	0.00	0.08	0.00	8.05	2.00	0.00	0.00	0.07	0.00
8.12	2.00	0.00	0.00	0.08	0.00	8.19	2.00	0.00	0.00	0.07	0.00
8.27	2.00	0.00	0.00	0.07	0.00	8.36	2.00	0.00	0.00	0.10	0.00
8.41	2.00	0.00	0.00	0.05	0.00	8.50	2.00	0.00	0.00	0.09	0.00
8.60	2.00	0.00	0.00	0.10	0.00	8.70	2.00	0.00	0.00	0.09	0.00
8.74	2.00	0.00	0.00	0.05	0.00	8.78	2.00	0.00	0.00	0.03	0.00
8.81	2.00	0.00	0.00	0.03	0.00	8.86	2.00	0.00	0.00	0.05	0.00
8.91	2.00	0.00	0.00	0.04	0.00	8.94	2.00	0.00	0.00	0.04	0.00
9.02	2.00	0.00	0.00	0.08	0.00	9.10	2.00	0.00	0.00	0.07	0.00
9.17	2.00	0.00	0.00	0.07	0.00	9.22	2.00	0.00	0.00	0.05	0.00
9.31	2.00	0.00	0.00	0.09	0.00	9.37	2.00	0.00	0.00	0.06	0.00
9.42	2.00	0.00	0.00	0.05	0.00	9.52	2.00	0.00	0.00	0.10	0.00
9.60	2.00	0.00	0.00	0.08	0.00	9.66	2.00	0.00	0.00	0.06	0.00
9.74	2.00	0.00	0.00	0.08	0.00	9.81	2.00	0.00	0.00	0.07	0.00
9.89	2.00	0.00	0.00	0.08	0.00	9.98	2.00	0.00	0.00	0.09	0.00
10.03	2.00	0.00	0.00	0.06	0.00	10.13	2.00	0.00	0.00	0.09	0.00
10.23	2.00	0.00	0.00	0.10	0.00	10.32	2.00	0.00	0.00	0.09	0.00
10.38	2.00	0.00	0.00	0.06	0.00	10.47	2.00	0.00	0.00	0.09	0.00
10.57	2.00	0.00	0.00	0.10	0.00	10.66	2.00	0.00	0.00	0.09	0.00
10.76	2.00	0.00	0.00	0.10	0.00	10.85	2.00	0.00	0.00	0.10	0.00
10.92	2.00	0.00	0.00	0.07	0.00	11.00	2.00	0.00	0.00	0.08	0.00
11.07	2.00	0.00	0.00	0.06	0.00	11.10	2.00	0.00	0.00	0.03	0.00
11.15	2.00	0.00	0.00	0.05	0.00	11.19	2.00	0.00	0.00	0.04	0.00
11.24	2.00	0.00	0.00	0.05	0.00	11.29	2.00	0.00	0.00	0.05	0.00
11.34	2.00	0.00	0.00	0.05	0.00	11.40	2.00	0.00	0.00	0.07	0.00
11.47	2.00	0.00	0.00	0.06	0.00	11.53	2.00	0.00	0.00	0.06	0.00
11.58	2.00	0.00	0.00	0.04	0.00	11.65	2.00	0.00	0.00	0.07	0.00
11.72	2.00	0.00	0.00	0.07	0.00	11.77	2.00	0.00	0.00	0.05	0.00
11.82	2.00	0.00	0.00	0.05	0.00	11.88	2.00	0.00	0.00	0.06	0.00
11.97	2.00	0.00	0.00	0.09	0.00	12.02	2.00	0.00	0.00	0.05	0.00
12.06	2.00	0.00	0.00	0.05	0.00	12.11	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
12.21	2.00	0.00	0.00	0.10	0.00	12.25	2.00	0.00	0.00	0.04	0.00
12.30	2.00	0.00	0.00	0.05	0.00	12.31	2.00	0.00	0.00	0.01	0.00
12.32	2.00	0.00	0.00	0.01	0.00	12.35	2.00	0.00	0.00	0.03	0.00
12.40	2.00	0.00	0.00	0.05	0.00	12.45	2.00	0.00	0.00	0.05	0.00
12.52	2.00	0.00	0.00	0.08	0.00	12.56	2.00	0.00	0.00	0.04	0.00
12.62	2.00	0.00	0.00	0.06	0.00	12.65	2.00	0.00	0.00	0.04	0.00
12.71	2.00	0.00	0.00	0.05	0.00	12.76	2.00	0.00	0.00	0.05	0.00
12.83	2.00	0.00	0.00	0.07	0.00	12.88	2.00	0.00	0.00	0.05	0.00
12.93	2.00	0.00	0.00	0.05	0.00	12.98	2.00	0.00	0.00	0.05	0.00
13.03	2.00	0.00	0.00	0.05	0.00	13.04	2.00	0.00	0.00	0.01	0.00
13.07	2.00	0.00	0.00	0.04	0.00	13.13	2.00	0.00	0.00	0.05	0.00
13.17	2.00	0.00	0.00	0.04	0.00	13.22	2.00	0.00	0.00	0.05	0.00
13.27	2.00	0.00	0.00	0.05	0.00	13.32	2.00	0.00	0.00	0.04	0.00
13.37	2.00	0.00	0.00	0.05	0.00	13.41	2.00	0.00	0.00	0.04	0.00
13.46	2.00	0.00	0.00	0.05	0.00	13.51	2.00	0.00	0.00	0.04	0.00
13.56	2.00	0.00	0.00	0.05	0.00	13.60	2.00	0.00	0.00	0.04	0.00
13.66	2.00	0.00	0.00	0.06	0.00	13.75	2.00	0.00	0.00	0.09	0.00
13.80	2.00	0.00	0.00	0.05	0.00	13.89	2.00	0.00	0.00	0.09	0.00
13.94	2.00	0.00	0.00	0.05	0.00	13.99	2.00	0.00	0.00	0.05	0.00
14.09	2.00	0.00	0.00	0.09	0.00	14.14	2.00	0.00	0.00	0.06	0.00
14.23	2.00	0.00	0.00	0.09	0.00	14.28	2.00	0.00	0.00	0.05	0.00
14.38	2.00	0.00	0.00	0.10	0.00	14.42	2.00	0.00	0.00	0.04	0.00
14.52	2.00	0.00	0.00	0.10	0.00	14.57	2.00	0.00	0.00	0.05	0.00
14.67	2.00	0.00	0.00	0.10	0.00	14.68	2.00	0.00	0.00	0.01	0.00
14.70	2.00	0.00	0.00	0.02	0.00	14.75	2.00	0.00	0.00	0.05	0.00
14.80	2.00	0.00	0.00	0.04	0.00	14.89	2.00	0.00	0.00	0.10	0.00
14.94	2.00	0.00	0.00	0.05	0.00	15.04	2.00	0.00	0.00	0.10	0.00
15.13	2.00	0.00	0.00	0.09	0.00	15.21	2.00	0.00	0.00	0.08	0.00
15.28	2.00	0.00	0.00	0.07	0.00	15.38	2.00	0.00	0.00	0.10	0.00
15.47	2.00	0.00	0.00	0.09	0.00	15.57	2.00	0.00	0.00	0.10	0.00
15.67	2.00	0.00	0.00	0.09	0.00	15.77	2.00	0.00	0.00	0.10	0.00
15.86	2.00	0.00	0.00	0.10	0.00	15.96	2.00	0.00	0.00	0.09	0.00
16.05	2.00	0.00	0.00	0.10	0.00	16.15	2.00	0.00	0.00	0.09	0.00
16.25	2.00	0.00	0.00	0.10	0.00	16.31	2.00	0.00	0.00	0.06	0.00
16.39	2.00	0.00	0.00	0.08	0.00	16.48	2.00	0.00	0.00	0.10	0.00
16.59	2.00	0.00	0.00	0.10	0.00	16.68	2.00	0.00	0.00	0.09	0.00
16.76	2.00	0.00	0.00	0.08	0.00	16.86	2.00	0.00	0.00	0.10	0.00
16.92	2.00	0.00	0.00	0.06	0.00	17.02	2.00	0.00	0.00	0.09	0.00
17.11	2.00	0.00	0.00	0.10	0.00	17.22	2.00	0.00	0.00	0.11	0.00
17.35	2.00	0.00	0.00	0.13	0.00	17.45	2.00	0.00	0.00	0.10	0.00
17.55	2.00	0.00	0.00	0.10	0.00	17.61	2.00	0.00	0.00	0.07	0.00
17.64	2.00	0.00	0.00	0.03	0.00	17.70	2.00	0.00	0.00	0.06	0.00
17.75	2.00	0.00	0.00	0.04	0.00	17.80	2.00	0.00	0.00	0.05	0.00
17.85	2.00	0.00	0.00	0.05	0.00	17.94	2.00	0.00	0.00	0.10	0.00
17.99	2.00	0.00	0.00	0.04	0.00	18.09	2.00	0.00	0.00	0.10	0.00
18.15	2.00	0.00	0.00	0.06	0.00	18.23	2.00	0.00	0.00	0.08	0.00
18.33	2.00	0.00	0.00	0.10	0.00	18.43	2.00	0.00	0.00	0.10	0.00
18.52	2.00	0.00	0.00	0.10	0.00	18.59	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
18.72	2.00	0.00	0.00	0.13	0.00	18.81	2.00	0.00	0.00	0.09	0.00
18.87	2.00	0.00	0.00	0.06	0.00	18.95	2.00	0.00	0.00	0.08	0.00
19.05	2.00	0.00	0.00	0.10	0.00	19.14	2.00	0.00	0.00	0.09	0.00
19.22	2.00	0.00	0.00	0.07	0.00	19.29	2.00	0.00	0.00	0.08	0.00
19.38	2.00	0.00	0.00	0.09	0.00	19.44	2.00	0.00	0.00	0.06	0.00
19.53	2.00	0.00	0.00	0.09	0.00	19.62	2.00	0.00	0.00	0.09	0.00
19.69	2.00	0.00	0.00	0.07	0.00	19.79	2.00	0.00	0.00	0.10	0.00
19.86	2.00	0.00	0.00	0.07	0.00	19.97	2.00	0.00	0.00	0.10	0.00
20.07	2.00	0.00	0.00	0.10	0.00	20.16	2.00	0.00	0.00	0.09	0.00
20.26	2.00	0.00	0.00	0.10	0.00	20.34	2.00	0.00	0.00	0.08	0.00
20.43	2.00	0.00	0.00	0.09	0.00	20.50	2.00	0.00	0.00	0.07	0.00
20.60	2.00	0.00	0.00	0.10	0.00	20.62	2.00	0.00	0.00	0.02	0.00
20.63	2.00	0.00	0.00	0.01	0.00	20.68	2.00	0.00	0.00	0.05	0.00
20.73	2.00	0.00	0.00	0.05	0.00	20.82	2.00	0.00	0.00	0.09	0.00
20.87	2.00	0.00	0.00	0.05	0.00	20.91	2.00	0.00	0.00	0.05	0.00
20.96	2.00	0.00	0.00	0.05	0.00	21.05	2.00	0.00	0.00	0.09	0.00
21.11	2.00	0.00	0.00	0.06	0.00	21.17	2.00	0.00	0.00	0.06	0.00
21.25	2.00	0.00	0.00	0.08	0.00	21.30	2.00	0.00	0.00	0.06	0.00
21.37	2.00	0.00	0.00	0.06	0.00	21.45	2.00	0.00	0.00	0.08	0.00
21.49	2.00	0.00	0.00	0.05	0.00	21.58	2.00	0.00	0.00	0.09	0.00
21.64	2.00	0.00	0.00	0.06	0.00	21.69	2.00	0.00	0.00	0.05	0.00
21.78	2.00	0.00	0.00	0.09	0.00	21.83	2.00	0.00	0.00	0.05	0.00
21.89	2.00	0.00	0.00	0.06	0.00	21.98	2.00	0.00	0.00	0.09	0.00
22.03	2.00	0.00	0.00	0.05	0.00	22.12	2.00	0.00	0.00	0.09	0.00
22.22	2.00	0.00	0.00	0.10	0.00	22.26	2.00	0.00	0.00	0.05	0.00
22.36	2.00	0.00	0.00	0.09	0.00	22.41	2.00	0.00	0.00	0.05	0.00
22.51	2.00	0.00	0.00	0.10	0.00	22.60	2.00	0.00	0.00	0.09	0.00
22.70	2.00	0.00	0.00	0.10	0.00	22.75	2.00	0.00	0.00	0.05	0.00
22.84	2.00	0.00	0.00	0.10	0.00	22.89	2.00	0.00	0.00	0.05	0.00
22.90	2.00	0.00	0.00	0.01	0.00	22.94	2.00	0.00	0.00	0.04	0.00
23.00	2.00	0.00	0.00	0.06	0.00	23.08	2.00	0.00	0.00	0.08	0.00
23.13	2.00	0.00	0.00	0.05	0.00	23.20	2.00	0.00	0.00	0.07	0.00
23.27	2.00	0.00	0.00	0.07	0.00	23.33	2.00	0.00	0.00	0.06	0.00
23.42	2.00	0.00	0.00	0.09	0.00	23.48	2.00	0.00	0.00	0.06	0.00
23.57	2.00	0.00	0.00	0.09	0.00	23.61	2.00	0.00	0.00	0.04	0.00
23.66	2.00	0.00	0.00	0.05	0.00	23.73	2.00	0.00	0.00	0.07	0.00
23.80	2.00	0.00	0.00	0.07	0.00	23.85	2.00	0.00	0.00	0.05	0.00
23.94	2.00	0.00	0.00	0.09	0.00	24.00	2.00	0.00	0.00	0.05	0.00
24.09	2.00	0.00	0.00	0.09	0.00	24.16	2.00	0.00	0.00	0.07	0.00
24.24	2.00	0.00	0.00	0.07	0.00	24.33	2.00	0.00	0.00	0.10	0.00
24.43	2.00	0.00	0.00	0.10	0.00	24.52	2.00	0.00	0.00	0.09	0.00
24.58	2.00	0.00	0.00	0.06	0.00	24.59	2.00	0.00	0.00	0.01	0.00
24.63	2.00	0.00	0.00	0.04	0.00	24.68	2.00	0.00	0.00	0.05	0.00
24.77	2.00	0.00	0.00	0.10	0.00	24.82	2.00	0.00	0.00	0.05	0.00
24.92	2.00	0.00	0.00	0.10	0.00	25.01	2.00	0.00	0.00	0.09	0.00
25.06	2.00	0.00	0.00	0.06	0.00	25.16	2.00	0.00	0.00	0.09	0.00
25.25	2.00	0.00	0.00	0.09	0.00	25.30	2.00	0.00	0.00	0.05	0.00
25.41	2.00	0.00	0.00	0.11	0.00	25.49	2.00	0.00	0.00	0.09	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
25.55	2.00	0.00	0.00	0.05	0.00	25.64	2.00	0.00	0.00	0.09	0.00
25.70	2.00	0.00	0.00	0.06	0.00	25.79	2.00	0.00	0.00	0.09	0.00
25.89	2.00	0.00	0.00	0.10	0.00	25.94	2.00	0.00	0.00	0.06	0.00
26.02	2.00	0.00	0.00	0.08	0.00	26.12	2.00	0.00	0.00	0.09	0.00
26.17	2.00	0.00	0.00	0.05	0.00	26.28	2.00	0.00	0.00	0.11	0.00
26.36	2.00	0.00	0.00	0.09	0.00	26.45	2.00	0.00	0.00	0.09	0.00
26.50	2.00	0.00	0.00	0.05	0.00	26.61	2.00	0.00	0.00	0.11	0.00
26.70	2.00	0.00	0.00	0.09	0.00	26.77	2.00	0.00	0.00	0.07	0.00
26.85	2.00	0.00	0.00	0.08	0.00	26.94	2.00	0.00	0.00	0.09	0.00
27.04	2.00	0.00	0.00	0.09	0.00	27.14	2.00	0.00	0.00	0.10	0.00
27.23	2.00	0.00	0.00	0.09	0.00	27.28	2.00	0.00	0.00	0.05	0.00
27.29	2.00	0.00	0.00	0.01	0.00	27.38	2.00	0.00	0.00	0.09	0.00
27.48	2.00	0.00	0.00	0.10	0.00	27.57	2.00	0.00	0.00	0.09	0.00
27.64	2.00	0.00	0.00	0.07	0.00	27.65	2.00	0.00	0.00	0.01	0.00
27.74	2.00	0.00	0.00	0.09	0.00	27.80	2.00	0.00	0.00	0.06	0.00
27.90	2.00	0.00	0.00	0.10	0.00	27.99	2.00	0.00	0.00	0.09	0.00
28.07	2.00	0.00	0.00	0.08	0.00	28.16	2.00	0.00	0.00	0.09	0.00
28.25	2.00	0.00	0.00	0.09	0.00	28.34	2.00	0.00	0.00	0.09	0.00
28.44	2.00	0.00	0.00	0.10	0.00	28.53	2.00	0.00	0.00	0.09	0.00
28.62	2.00	0.00	0.00	0.09	0.00	28.76	2.00	0.00	0.00	0.14	0.00
28.86	2.00	0.00	0.00	0.10	0.00	28.96	2.00	0.00	0.00	0.10	0.00
29.08	2.00	0.00	0.00	0.11	0.00	29.19	2.00	0.00	0.00	0.12	0.00
29.29	2.00	0.00	0.00	0.10	0.00	29.39	2.00	0.00	0.00	0.09	0.00
29.50	2.00	0.00	0.00	0.11	0.00	29.63	2.00	0.00	0.00	0.13	0.00
29.65	2.00	0.00	0.00	0.02	0.00	29.66	2.00	0.00	0.00	0.01	0.00
29.72	2.00	0.00	0.00	0.06	0.00	29.80	2.00	0.00	0.00	0.09	0.00
29.85	2.00	0.00	0.00	0.05	0.00	29.94	2.00	0.00	0.00	0.09	0.00
30.00	2.00	0.00	0.00	0.06	0.00	30.05	2.00	0.00	0.00	0.05	0.00
30.14	2.00	0.00	0.00	0.09	0.00	30.19	2.00	0.00	0.00	0.05	0.00
30.24	2.00	0.00	0.00	0.05	0.00	30.29	1.91	0.00	0.00	0.05	0.00
30.38	1.88	0.00	0.00	0.09	0.00	30.43	1.83	0.00	0.00	0.05	0.00
30.48	1.77	0.00	0.00	0.05	0.00	30.54	1.71	0.00	0.00	0.06	0.00
30.62	1.69	0.00	0.00	0.08	0.00	30.67	1.67	0.00	0.00	0.05	0.00
30.72	1.67	0.00	0.00	0.05	0.00	30.76	1.68	0.00	0.00	0.04	0.00
30.86	1.71	0.00	0.00	0.10	0.00	30.91	1.74	0.00	0.00	0.05	0.00
30.95	1.79	0.00	0.00	0.05	0.00	31.03	1.84	0.00	0.00	0.07	0.00
31.10	1.89	0.00	0.00	0.07	0.00	31.15	1.94	0.00	0.00	0.05	0.00
31.20	2.00	0.00	0.00	0.05	0.00	31.26	2.00	0.00	0.00	0.06	0.00
31.34	2.00	0.00	0.00	0.08	0.00	31.37	2.00	0.00	0.00	0.02	0.00
31.38	1.99	0.00	0.00	0.01	0.00	31.43	2.00	0.00	0.00	0.05	0.00
31.47	1.91	0.00	0.00	0.05	0.00	31.55	1.79	0.00	0.00	0.07	0.00
31.59	1.61	0.00	0.00	0.05	0.00	31.66	1.40	0.00	0.00	0.06	0.00
31.73	1.23	0.00	0.00	0.08	0.00	31.78	1.10	0.00	0.00	0.05	0.00
31.84	1.03	0.00	0.00	0.06	0.00	31.93	1.00	0.00	0.00	0.09	0.00
31.98	1.02	0.00	0.00	0.05	0.00	32.02	1.07	0.00	0.00	0.05	0.00
32.09	1.13	0.00	0.00	0.07	0.00	32.16	1.16	0.00	0.00	0.07	0.00
32.22	1.17	0.00	0.00	0.05	0.00	32.27	1.17	0.00	0.00	0.05	0.00
32.34	1.17	0.00	0.00	0.07	0.00	32.42	1.16	0.00	0.00	0.08	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
32.46	1.15	0.00	0.00	0.04	0.00	32.54	1.14	0.00	0.00	0.09	0.00
32.60	1.12	0.00	0.00	0.06	0.00	32.67	1.11	0.00	0.00	0.07	0.00
32.75	1.12	0.00	0.00	0.08	0.00	32.81	1.15	0.00	0.00	0.06	0.00
32.89	1.20	0.00	0.00	0.08	0.00	32.94	1.17	0.00	0.00	0.05	0.00
32.95	1.19	0.00	0.00	0.01	0.00	33.00	1.22	0.00	0.00	0.05	0.00
33.06	1.32	0.00	0.00	0.06	0.00	33.11	1.35	0.00	0.00	0.05	0.00
33.20	1.35	0.00	0.00	0.09	0.00	33.25	1.34	0.00	0.00	0.05	0.00
33.34	1.32	0.00	0.00	0.09	0.00	33.38	1.33	0.00	0.00	0.04	0.00
33.48	1.35	0.00	0.00	0.10	0.00	33.58	1.39	0.00	0.00	0.10	0.00
33.63	1.46	0.00	0.00	0.04	0.00	33.73	1.55	0.00	0.00	0.10	0.00
33.82	1.65	0.00	0.00	0.09	0.00	33.87	1.77	0.00	0.00	0.05	0.00
33.96	1.91	0.00	0.00	0.09	0.00	34.02	2.00	0.00	0.00	0.06	0.00
34.11	2.00	0.00	0.00	0.09	0.00	34.18	2.00	0.00	0.00	0.07	0.00
34.26	2.00	0.00	0.00	0.08	0.00	34.35	2.00	0.00	0.00	0.09	0.00
34.44	2.00	0.00	0.00	0.09	0.00	34.49	2.00	0.00	0.00	0.05	0.00
34.59	2.00	0.00	0.00	0.10	0.00	34.69	2.00	0.00	0.00	0.09	0.00
34.76	2.00	0.00	0.00	0.07	0.00	34.83	2.00	0.00	0.00	0.08	0.00
34.93	2.00	0.00	0.00	0.10	0.00	35.02	2.00	0.00	0.00	0.09	0.00
35.12	2.00	0.00	0.00	0.10	0.00	35.22	2.00	0.00	0.00	0.10	0.00
35.30	2.00	0.00	0.00	0.08	0.00	35.38	2.00	0.00	0.00	0.08	0.00
35.43	2.00	0.00	0.00	0.04	0.00	35.46	2.00	0.00	0.00	0.04	0.00
35.51	2.00	0.00	0.00	0.05	0.00	35.56	2.00	0.00	0.00	0.04	0.00
35.66	2.00	0.00	0.00	0.10	0.00	35.70	2.00	0.00	0.00	0.05	0.00
35.80	2.00	0.00	0.00	0.10	0.00	35.89	2.00	0.00	0.00	0.09	0.00
35.96	2.00	0.00	0.00	0.07	0.00	36.04	2.00	0.00	0.00	0.08	0.00
36.14	2.00	0.00	0.00	0.10	0.00	36.19	2.00	0.00	0.00	0.05	0.00
36.28	2.00	0.00	0.00	0.09	0.00	36.33	2.00	0.00	0.00	0.04	0.00
36.42	2.00	0.00	0.00	0.09	0.00	36.48	2.00	0.00	0.00	0.05	0.00
36.52	2.00	0.00	0.00	0.05	0.00	36.62	2.00	0.00	0.00	0.10	0.00
36.68	2.00	0.00	0.00	0.06	0.00	36.77	2.00	0.00	0.00	0.09	0.00
36.86	2.00	0.00	0.00	0.09	0.00	36.90	2.00	0.00	0.00	0.05	0.00
37.00	2.00	0.00	0.00	0.10	0.00	37.10	2.00	0.00	0.00	0.10	0.00
37.20	2.00	0.00	0.00	0.10	0.00	37.29	2.00	0.00	0.00	0.09	0.00
37.39	2.00	0.00	0.00	0.10	0.00	37.49	2.00	0.00	0.00	0.10	0.00
37.53	2.00	0.00	0.00	0.05	0.00	37.58	2.00	0.00	0.00	0.04	0.00
37.62	2.00	0.00	0.00	0.05	0.00	37.69	2.00	0.00	0.00	0.07	0.00
37.77	2.00	0.00	0.00	0.08	0.00	37.82	2.00	0.00	0.00	0.05	0.00
37.87	2.00	0.00	0.00	0.05	0.00	37.91	2.00	0.00	0.00	0.05	0.00
37.97	2.00	0.00	0.00	0.06	0.00	38.06	2.00	0.00	0.00	0.09	0.00
38.10	2.00	0.00	0.00	0.04	0.00	38.17	2.00	0.00	0.00	0.07	0.00
38.25	2.00	0.00	0.00	0.08	0.00	38.35	2.00	0.00	0.00	0.09	0.00
38.40	2.00	0.00	0.00	0.05	0.00	38.46	2.00	0.00	0.00	0.06	0.00
38.54	2.00	0.00	0.00	0.08	0.00	38.60	2.00	0.00	0.00	0.06	0.00
38.69	2.00	0.00	0.00	0.08	0.00	38.74	2.00	0.00	0.00	0.05	0.00
38.83	2.00	0.00	0.00	0.09	0.00	38.88	2.00	0.00	0.00	0.05	0.00
38.97	2.00	0.00	0.00	0.09	0.00	39.02	2.00	0.00	0.00	0.05	0.00
39.11	2.00	0.00	0.00	0.09	0.00	39.16	2.00	0.00	0.00	0.06	0.00
39.23	1.92	0.00	0.00	0.06	0.00	39.24	1.83	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
39.28	1.78	0.00	0.00	0.04	0.00	39.32	1.80	0.00	0.00	0.05	0.00
39.39	2.00	0.00	0.00	0.06	0.00	39.47	2.00	0.00	0.00	0.08	0.00
39.54	2.00	0.00	0.00	0.07	0.00	39.62	2.00	0.00	0.00	0.08	0.00
39.71	2.00	0.00	0.00	0.09	0.00	39.76	2.00	0.00	0.00	0.05	0.00
39.85	2.00	0.00	0.00	0.09	0.00	39.90	2.00	0.00	0.00	0.06	0.00
40.00	2.00	0.00	0.00	0.10	0.00	40.06	2.00	0.00	0.00	0.06	0.00
40.15	2.00	0.00	0.00	0.09	0.00	40.21	2.00	0.00	0.00	0.06	0.00
40.29	2.00	0.00	0.00	0.08	0.00	40.35	2.00	0.00	0.00	0.06	0.00
40.43	2.00	0.00	0.00	0.08	0.00	40.52	2.00	0.00	0.00	0.09	0.00
40.58	2.00	0.00	0.00	0.05	0.00	40.67	2.00	0.00	0.00	0.10	0.00
40.77	2.00	0.00	0.00	0.09	0.00	40.84	2.00	0.00	0.00	0.07	0.00
40.89	2.00	0.00	0.00	0.05	0.00	40.94	2.00	0.00	0.00	0.05	0.00
41.03	2.00	0.00	0.00	0.10	0.00	41.08	2.00	0.00	0.00	0.05	0.00
41.14	2.00	0.00	0.00	0.06	0.00	41.22	2.00	0.00	0.00	0.08	0.00
41.28	0.75	0.25	1.20	0.06	0.02	41.33	0.78	0.22	1.41	0.05	0.01
41.42	0.82	0.18	2.00	0.09	0.02	41.47	0.87	0.13	3.68	0.05	0.01
41.52	0.93	0.07	13.55	0.06	0.00	41.62	0.98	0.02	23365.55	0.09	0.00
41.67	1.07	0.00	0.00	0.05	0.00	41.76	1.16	0.00	0.00	0.09	0.00
41.82	1.28	0.00	0.00	0.06	0.00	41.90	1.37	0.00	0.00	0.08	0.00
41.99	1.44	0.00	0.00	0.09	0.00	42.05	1.48	0.00	0.00	0.06	0.00
42.15	1.48	0.00	0.00	0.10	0.00	42.23	1.46	0.00	0.00	0.09	0.00
42.30	1.43	0.00	0.00	0.07	0.00	42.38	1.36	0.00	0.00	0.08	0.00
42.48	1.27	0.00	0.00	0.10	0.00	42.57	1.18	0.00	0.00	0.09	0.00
42.64	1.11	0.00	0.00	0.07	0.00	42.72	1.04	0.00	0.00	0.08	0.00
42.82	0.98	0.02	148889.56	0.10	0.00	42.90	0.94	0.06	23.51	0.08	0.01
42.97	0.92	0.08	11.30	0.07	0.01	43.06	0.93	0.07	13.85	0.09	0.01
43.15	0.89	0.11	5.32	0.09	0.01	43.20	0.85	0.15	2.78	0.05	0.01
43.30	0.80	0.20	1.68	0.10	0.02	43.40	0.82	0.18	1.97	0.10	0.02
43.48	0.87	0.13	3.65	0.08	0.01	43.51	0.92	0.08	9.02	0.03	0.00
43.52	0.97	0.03	357.31	0.01	0.00	43.56	1.09	0.00	0.00	0.04	0.00
43.61	1.30	0.00	0.00	0.05	0.00	43.67	1.49	0.00	0.00	0.06	0.00
43.72	1.68	0.00	0.00	0.05	0.00	43.80	1.83	0.00	0.00	0.08	0.00
43.85	1.95	0.00	0.00	0.05	0.00	43.90	2.00	0.00	0.00	0.05	0.00
43.94	2.00	0.00	0.00	0.05	0.00	43.99	2.00	0.00	0.00	0.05	0.00
44.08	2.00	0.00	0.00	0.09	0.00	44.14	2.00	0.00	0.00	0.06	0.00
44.22	2.00	0.00	0.00	0.08	0.00	44.28	2.00	0.00	0.00	0.05	0.00
44.33	2.00	0.00	0.00	0.05	0.00	44.40	2.00	0.00	0.00	0.07	0.00
44.48	2.00	0.00	0.00	0.08	0.00	44.52	2.00	0.00	0.00	0.05	0.00
44.61	2.00	0.00	0.00	0.09	0.00	44.72	2.00	0.00	0.00	0.11	0.00
44.77	2.00	0.00	0.00	0.05	0.00	44.91	2.00	0.00	0.00	0.14	0.00
44.95	2.00	0.00	0.00	0.05	0.00	45.02	2.00	0.00	0.00	0.07	0.00
45.04	1.62	0.00	0.00	0.02	0.00	45.06	1.68	0.00	0.00	0.02	0.00
45.11	1.75	0.00	0.00	0.05	0.00	45.15	2.00	0.00	0.00	0.05	0.00
45.21	2.00	0.00	0.00	0.05	0.00	45.25	2.00	0.00	0.00	0.04	0.00
45.30	2.00	0.00	0.00	0.05	0.00	45.35	2.00	0.00	0.00	0.05	0.00
45.41	2.00	0.00	0.00	0.06	0.00	45.49	2.00	0.00	0.00	0.08	0.00
45.55	2.00	0.00	0.00	0.05	0.00	45.63	2.00	0.00	0.00	0.09	0.00
45.69	2.00	0.00	0.00	0.05	0.00	45.78	2.00	0.00	0.00	0.09	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
45.84	2.00	0.00	0.00	0.06	0.00	45.93	1.81	0.00	0.00	0.09	0.00
46.02	2.00	0.00	0.00	0.09	0.00	46.08	2.00	0.00	0.00	0.05	0.00
46.16	2.00	0.00	0.00	0.09	0.00	46.24	2.00	0.00	0.00	0.07	0.00
46.31	2.00	0.00	0.00	0.07	0.00	46.41	2.00	0.00	0.00	0.10	0.00
46.48	2.00	0.00	0.00	0.06	0.00	46.56	2.00	0.00	0.00	0.09	0.00
46.65	2.00	0.00	0.00	0.09	0.00	46.75	2.00	0.00	0.00	0.10	0.00
46.84	2.00	0.00	0.00	0.09	0.00	46.94	2.00	0.00	0.00	0.09	0.00
47.02	2.00	0.00	0.00	0.08	0.00	47.08	2.00	0.00	0.00	0.06	0.00
47.12	2.00	0.00	0.00	0.04	0.00	47.16	2.00	0.00	0.00	0.04	0.00
47.21	2.00	0.00	0.00	0.05	0.00	47.27	2.00	0.00	0.00	0.06	0.00
47.35	2.00	0.00	0.00	0.08	0.00	47.40	2.00	0.00	0.00	0.05	0.00
47.50	2.00	0.00	0.00	0.10	0.00	47.55	2.00	0.00	0.00	0.05	0.00
47.61	2.00	0.00	0.00	0.06	0.00	47.69	2.00	0.00	0.00	0.08	0.00
47.76	2.00	0.00	0.00	0.08	0.00	47.83	2.00	0.00	0.00	0.07	0.00
47.93	2.00	0.00	0.00	0.10	0.00	48.02	2.00	0.00	0.00	0.09	0.00
48.09	2.00	0.00	0.00	0.07	0.00	48.18	2.00	0.00	0.00	0.09	0.00
48.27	2.00	0.00	0.00	0.09	0.00	48.37	2.00	0.00	0.00	0.10	0.00
48.46	2.00	0.00	0.00	0.09	0.00	48.52	2.00	0.00	0.00	0.07	0.00
48.60	2.00	0.00	0.00	0.08	0.00	48.70	2.00	0.00	0.00	0.10	0.00
48.79	2.00	0.00	0.00	0.09	0.00	48.85	2.00	0.00	0.00	0.06	0.00
48.94	2.00	0.00	0.00	0.09	0.00	49.04	2.00	0.00	0.00	0.09	0.00
49.13	2.00	0.00	0.00	0.09	0.00	49.23	2.00	0.00	0.00	0.10	0.00
49.33	2.00	0.00	0.00	0.09	0.00	49.38	2.00	0.00	0.00	0.05	0.00
49.42	2.00	0.00	0.00	0.04	0.00	49.48	2.00	0.00	0.00	0.06	0.00
49.53	2.00	0.00	0.00	0.04	0.00	49.58	2.00	0.00	0.00	0.05	0.00
49.63	2.00	0.00	0.00	0.05	0.00	49.72	2.00	0.00	0.00	0.10	0.00
49.77	2.00	0.00	0.00	0.05	0.00	49.83	2.00	0.00	0.00	0.05	0.00
49.92	2.00	0.00	0.00	0.09	0.00	49.97	2.00	0.00	0.00	0.05	0.00
50.04	2.00	0.00	0.00	0.07	0.00	50.11	2.00	0.00	0.00	0.07	0.00
50.20	2.00	0.00	0.00	0.09	0.00	50.27	2.00	0.00	0.00	0.07	0.00
50.34	2.00	0.00	0.00	0.07	0.00	50.45	2.00	0.00	0.00	0.10	0.00
50.54	2.00	0.00	0.00	0.09	0.00	50.59	2.00	0.00	0.00	0.05	0.00
50.68	2.00	0.00	0.00	0.09	0.00	50.79	2.00	0.00	0.00	0.10	0.00
50.88	2.00	0.00	0.00	0.09	0.00	50.98	2.00	0.00	0.00	0.10	0.00
51.07	2.00	0.00	0.00	0.09	0.00	51.17	2.00	0.00	0.00	0.10	0.00
51.24	2.00	0.00	0.00	0.07	0.00	51.33	2.00	0.00	0.00	0.09	0.00
51.46	2.00	0.00	0.00	0.13	0.00	51.46	2.00	0.00	0.00	0.00	0.00
51.51	2.00	0.00	0.00	0.05	0.00	51.56	2.00	0.00	0.00	0.05	0.00
51.65	2.00	0.00	0.00	0.09	0.00	51.71	2.00	0.00	0.00	0.06	0.00
51.79	2.00	0.00	0.00	0.09	0.00	51.85	2.00	0.00	0.00	0.05	0.00
51.94	2.00	0.00	0.00	0.09	0.00	51.99	2.00	0.00	0.00	0.05	0.00
52.09	2.00	0.00	0.00	0.10	0.00	52.19	2.00	0.00	0.00	0.10	0.00
52.28	2.00	0.00	0.00	0.09	0.00	52.35	2.00	0.00	0.00	0.07	0.00
52.43	2.00	0.00	0.00	0.08	0.00	52.52	2.00	0.00	0.00	0.09	0.00
52.62	2.00	0.00	0.00	0.11	0.00	52.72	2.00	0.00	0.00	0.09	0.00
52.81	2.00	0.00	0.00	0.09	0.00	52.91	2.00	0.00	0.00	0.10	0.00
53.00	2.00	0.00	0.00	0.09	0.00	53.10	2.00	0.00	0.00	0.10	0.00
53.20	2.00	0.00	0.00	0.09	0.00	53.29	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
53.38	2.00	0.00	0.00	0.09	0.00	53.46	2.00	0.00	0.00	0.08	0.00
53.53	2.00	0.00	0.00	0.07	0.00	53.63	2.00	0.00	0.00	0.10	0.00
53.73	2.00	0.00	0.00	0.10	0.00	53.82	2.00	0.00	0.00	0.09	0.00
53.92	2.00	0.00	0.00	0.10	0.00	53.94	1.66	0.00	0.00	0.02	0.00
53.96	1.48	0.00	0.00	0.02	0.00	53.97	1.55	0.00	0.00	0.01	0.00
54.05	1.73	0.00	0.00	0.08	0.00	54.08	2.00	0.00	0.00	0.02	0.00
54.13	2.00	0.00	0.00	0.05	0.00	54.19	2.00	0.00	0.00	0.06	0.00
54.25	2.00	0.00	0.00	0.06	0.00	54.28	2.00	0.00	0.00	0.03	0.00
54.29	2.00	0.00	0.00	0.02	0.00	54.34	2.00	0.00	0.00	0.05	0.00
54.35	2.00	0.00	0.00	0.01	0.00	54.40	2.00	0.00	0.00	0.05	0.00
54.44	2.00	0.00	0.00	0.04	0.00	54.49	2.00	0.00	0.00	0.05	0.00
54.53	2.00	0.00	0.00	0.04	0.00	54.57	2.00	0.00	0.00	0.03	0.00
54.58	2.00	0.00	0.00	0.02	0.00	54.63	2.00	0.00	0.00	0.04	0.00
54.68	2.00	0.00	0.00	0.05	0.00	54.73	2.00	0.00	0.00	0.05	0.00
54.78	2.00	0.00	0.00	0.05	0.00	54.83	2.00	0.00	0.00	0.05	0.00
54.88	2.00	0.00	0.00	0.05	0.00	54.92	2.00	0.00	0.00	0.05	0.00
54.97	2.00	0.00	0.00	0.05	0.00	55.02	2.00	0.00	0.00	0.05	0.00
55.12	2.00	0.00	0.00	0.09	0.00	55.17	2.00	0.00	0.00	0.05	0.00
55.25	2.00	0.00	0.00	0.08	0.00	55.31	2.00	0.00	0.00	0.06	0.00
55.36	1.98	0.00	0.00	0.05	0.00	55.45	1.82	0.00	0.00	0.09	0.00
55.50	1.66	0.00	0.00	0.05	0.00	55.60	1.56	0.00	0.00	0.10	0.00
55.65	1.41	0.00	0.00	0.05	0.00	55.71	1.33	0.00	0.00	0.06	0.00
55.75	1.26	0.00	0.00	0.04	0.00	55.79	1.27	0.00	0.00	0.04	0.00
55.84	1.32	0.00	0.00	0.05	0.00	55.89	1.35	0.00	0.00	0.05	0.00
55.90	1.37	0.00	0.00	0.01	0.00	55.94	1.34	0.00	0.00	0.03	0.00
55.99	1.30	0.00	0.00	0.05	0.00	56.03	1.24	0.00	0.00	0.05	0.00
56.08	1.21	0.00	0.00	0.05	0.00	56.14	1.17	0.00	0.00	0.06	0.00
56.22	1.13	0.00	0.00	0.08	0.00	56.28	1.10	0.00	0.00	0.05	0.00
56.33	1.09	0.00	0.00	0.05	0.00	56.38	1.09	0.00	0.00	0.05	0.00
56.45	1.13	0.00	0.00	0.07	0.00	56.52	1.18	0.00	0.00	0.07	0.00
56.62	1.24	0.00	0.00	0.10	0.00	56.66	1.30	0.00	0.00	0.05	0.00
56.73	1.39	0.00	0.00	0.07	0.00	56.81	1.46	0.00	0.00	0.08	0.00
56.95	1.53	0.00	0.00	0.14	0.00	57.00	1.61	0.00	0.00	0.04	0.00
57.09	1.63	0.00	0.00	0.10	0.00	57.19	1.62	0.00	0.00	0.10	0.00
57.27	1.50	0.00	0.00	0.08	0.00	57.35	1.47	0.00	0.00	0.07	0.00
57.44	1.41	0.00	0.00	0.09	0.00	57.50	1.40	0.00	0.00	0.07	0.00
57.52	1.52	0.00	0.00	0.02	0.00	57.58	1.78	0.00	0.00	0.05	0.00
57.63	2.00	0.00	0.00	0.05	0.00	57.72	2.00	0.00	0.00	0.09	0.00
57.77	1.98	0.00	0.00	0.04	0.00	57.82	1.83	0.00	0.00	0.05	0.00
57.91	1.66	0.00	0.00	0.09	0.00	57.96	1.48	0.00	0.00	0.05	0.00
58.02	1.61	0.00	0.00	0.05	0.00	58.09	1.69	0.00	0.00	0.08	0.00
58.16	1.82	0.00	0.00	0.06	0.00	58.25	1.87	0.00	0.00	0.10	0.00
58.30	1.83	0.00	0.00	0.05	0.00	58.40	1.76	0.00	0.00	0.10	0.00
58.50	1.74	0.00	0.00	0.10	0.00	58.56	1.71	0.00	0.00	0.06	0.00
58.64	1.75	0.00	0.00	0.08	0.00	58.73	1.90	0.00	0.00	0.09	0.00
58.78	1.92	0.00	0.00	0.05	0.00	58.88	1.98	0.00	0.00	0.09	0.00
58.97	2.00	0.00	0.00	0.09	0.00	59.07	1.97	0.00	0.00	0.10	0.00
59.13	1.86	0.00	0.00	0.05	0.00	59.23	1.78	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
59.31	1.61	0.00	0.00	0.09	0.00	59.38	1.50	0.00	0.00	0.07	0.00
59.41	1.42	0.00	0.00	0.03	0.00	59.46	1.45	0.00	0.00	0.05	0.00
59.51	1.45	0.00	0.00	0.05	0.00	59.57	1.51	0.00	0.00	0.05	0.00
59.66	1.65	0.00	0.00	0.09	0.00	59.75	1.82	0.00	0.00	0.09	0.00
59.80	1.99	0.00	0.00	0.05	0.00	59.85	2.00	0.00	0.00	0.05	0.00
59.91	2.00	0.00	0.00	0.06	0.00	59.99	2.00	0.00	0.00	0.08	0.00
60.05	2.00	0.00	0.00	0.05	0.00	60.09	2.00	0.00	0.00	0.04	0.00
60.14	2.00	0.00	0.00	0.05	0.00	60.19	2.00	0.00	0.00	0.05	0.00
60.22	2.00	0.00	0.00	0.03	0.00	60.28	1.93	0.00	0.00	0.06	0.00
60.33	1.69	0.00	0.00	0.05	0.00	60.38	1.41	0.00	0.00	0.05	0.00
60.42	1.25	0.00	0.00	0.04	0.00	60.48	1.09	0.00	0.00	0.06	0.00
60.57	0.93	0.07	15.13	0.09	0.00	60.66	0.80	0.20	1.61	0.09	0.00
60.68	0.73	0.27	1.06	0.03	0.00	60.69	0.70	0.30	0.91	0.01	0.00
60.74	0.67	0.33	0.81	0.05	0.00	60.79	0.64	0.36	0.71	0.05	0.00
60.84	0.60	0.40	0.63	0.05	0.00	60.89	0.58	0.42	0.59	0.05	0.00
60.98	0.56	0.44	0.57	0.09	0.01	61.03	0.58	0.42	0.60	0.04	0.00
61.08	0.67	0.33	0.80	0.06	0.00	61.18	0.78	0.22	1.42	0.09	0.00
61.23	0.91	0.09	7.91	0.06	0.00	61.31	0.83	0.17	2.12	0.08	0.00
61.42	0.83	0.17	2.14	0.10	0.00	61.47	0.92	0.08	10.64	0.05	0.00
61.51	1.03	0.00	0.00	0.05	0.00	61.54	1.05	0.00	0.00	0.02	0.00
61.57	1.11	0.00	0.00	0.03	0.00	61.58	1.24	0.00	0.00	0.02	0.00
61.61	1.10	0.00	0.00	0.03	0.00	61.63	1.02	0.00	0.00	0.01	0.00
61.63	0.80	0.20	1.66	0.01	0.00	61.66	0.67	0.33	0.80	0.02	0.00
61.67	0.73	0.27	1.04	0.01	0.00	61.70	0.71	0.29	0.96	0.03	0.00
61.71	0.72	0.28	1.00	0.01	0.00	61.76	0.75	0.25	1.18	0.04	0.00
61.80	0.79	0.21	1.57	0.05	0.00	61.84	0.83	0.17	2.16	0.04	0.00
61.86	0.90	0.10	5.56	0.02	0.00	61.93	0.97	0.03	567.87	0.07	0.00
61.98	0.93	0.07	13.38	0.05	0.00	62.04	1.16	0.00	0.00	0.06	0.00
62.09	1.44	0.00	0.00	0.05	0.00	62.14	1.66	0.00	0.00	0.05	0.00
62.19	1.80	0.00	0.00	0.05	0.00	62.24	1.88	0.00	0.00	0.05	0.00
62.26	1.97	0.00	0.00	0.02	0.00	62.29	1.97	0.00	0.00	0.03	0.00
62.38	1.93	0.00	0.00	0.09	0.00	62.44	1.72	0.00	0.00	0.06	0.00
62.46	1.55	0.00	0.00	0.02	0.00	62.47	1.41	0.00	0.00	0.01	0.00
62.51	1.44	0.00	0.00	0.04	0.00	62.56	1.52	0.00	0.00	0.05	0.00
62.60	1.61	0.00	0.00	0.04	0.00	62.65	1.64	0.00	0.00	0.05	0.00
62.70	1.65	0.00	0.00	0.05	0.00	62.75	1.65	0.00	0.00	0.05	0.00
62.80	1.74	0.00	0.00	0.05	0.00	62.85	2.00	0.00	0.00	0.05	0.00
62.89	2.00	0.00	0.00	0.05	0.00	62.97	2.00	0.00	0.00	0.07	0.00
63.04	2.00	0.00	0.00	0.07	0.00	63.09	2.00	0.00	0.00	0.05	0.00
63.13	2.00	0.00	0.00	0.05	0.00	63.19	2.00	0.00	0.00	0.05	0.00
63.23	2.00	0.00	0.00	0.04	0.00	63.28	2.00	0.00	0.00	0.05	0.00
63.32	2.00	0.00	0.00	0.04	0.00	63.38	2.00	0.00	0.00	0.06	0.00
63.44	2.00	0.00	0.00	0.06	0.00	63.52	2.00	0.00	0.00	0.08	0.00
63.57	2.00	0.00	0.00	0.05	0.00	63.66	2.00	0.00	0.00	0.09	0.00
63.73	2.00	0.00	0.00	0.06	0.00	63.76	1.53	0.00	0.00	0.03	0.00
63.76	1.45	0.00	0.00	0.01	0.00	63.78	1.54	0.00	0.00	0.02	0.00
63.81	1.86	0.00	0.00	0.03	0.00	63.85	1.97	0.00	0.00	0.04	0.00
63.86	1.94	0.00	0.00	0.01	0.00	63.91	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
63.94	2.00	0.00	0.00	0.03	0.00	63.95	2.00	0.00	0.00	0.02	0.00
64.00	2.00	0.00	0.00	0.05	0.00	64.02	2.00	0.00	0.00	0.01	0.00
64.05	2.00	0.00	0.00	0.03	0.00	64.09	1.99	0.00	0.00	0.04	0.00
64.11	1.93	0.00	0.00	0.02	0.00	64.15	1.86	0.00	0.00	0.04	0.00
64.20	1.82	0.00	0.00	0.05	0.00	64.25	1.84	0.00	0.00	0.05	0.00
64.29	2.00	0.00	0.00	0.04	0.00	64.34	2.00	0.00	0.00	0.05	0.00
64.43	2.00	0.00	0.00	0.08	0.00	64.48	2.00	0.00	0.00	0.05	0.00
64.53	2.00	0.00	0.00	0.05	0.00	64.58	2.00	0.00	0.00	0.05	0.00
64.63	2.00	0.00	0.00	0.05	0.00	64.68	2.00	0.00	0.00	0.05	0.00
64.73	2.00	0.00	0.00	0.05	0.00	64.77	2.00	0.00	0.00	0.05	0.00
64.82	2.00	0.00	0.00	0.04	0.00	64.87	2.00	0.00	0.00	0.05	0.00
64.89	2.00	0.00	0.00	0.02	0.00	64.93	2.00	0.00	0.00	0.04	0.00
64.94	2.00	0.00	0.00	0.01	0.00	64.98	2.00	0.00	0.00	0.04	0.00
64.99	2.00	0.00	0.00	0.01	0.00	65.03	2.00	0.00	0.00	0.05	0.00
65.08	2.00	0.00	0.00	0.05	0.00	65.13	2.00	0.00	0.00	0.05	0.00
65.17	2.00	0.00	0.00	0.04	0.00	65.22	2.00	0.00	0.00	0.05	0.00
65.23	2.00	0.00	0.00	0.01	0.00	65.28	2.00	0.00	0.00	0.05	0.00
65.32	2.00	0.00	0.00	0.04	0.00	65.37	2.00	0.00	0.00	0.05	0.00
65.42	2.00	0.00	0.00	0.05	0.00	65.47	2.00	0.00	0.00	0.05	0.00
65.48	2.00	0.00	0.00	0.01	0.00	65.49	2.00	0.00	0.00	0.01	0.00
65.52	2.00	0.00	0.00	0.03	0.00	65.57	2.00	0.00	0.00	0.05	0.00
65.62	2.00	0.00	0.00	0.05	0.00	65.67	2.00	0.00	0.00	0.05	0.00
65.69	2.00	0.00	0.00	0.01	0.00	65.72	2.00	0.00	0.00	0.03	0.00
65.77	2.00	0.00	0.00	0.05	0.00	65.82	2.00	0.00	0.00	0.05	0.00
65.86	2.00	0.00	0.00	0.04	0.00	65.86	2.00	0.00	0.00	0.01	0.00
65.91	2.00	0.00	0.00	0.05	0.00	65.96	2.00	0.00	0.00	0.04	0.00

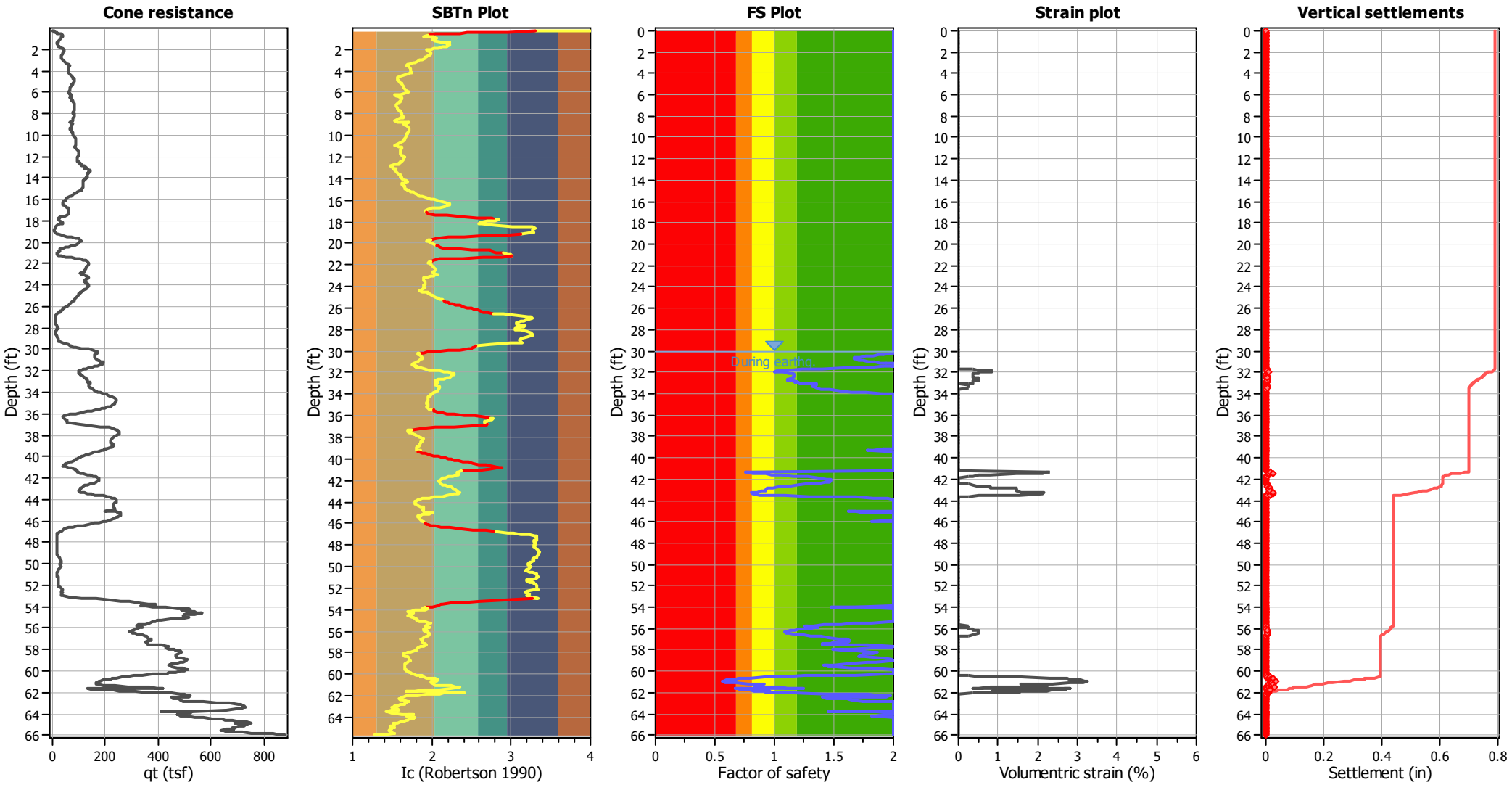
Overall liquefaction potential: 0.21

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
30.05	136.43	2.00	0.00	1.00	0.00	30.14	140.95	2.00	0.00	1.00	0.00
30.19	142.08	2.00	0.00	1.00	0.00	30.24	142.19	2.00	0.00	1.00	0.00
30.29	142.38	1.91	0.00	1.00	0.00	30.38	141.39	1.88	0.00	1.00	0.00
30.43	139.76	1.83	0.00	1.00	0.00	30.48	137.67	1.77	0.00	1.00	0.00
30.54	135.86	1.71	0.00	1.00	0.00	30.62	134.98	1.69	0.00	1.00	0.00
30.67	134.34	1.67	0.00	1.00	0.00	30.72	134.61	1.67	0.00	1.00	0.00
30.76	134.89	1.68	0.00	1.00	0.00	30.86	135.92	1.71	0.00	1.00	0.00
30.91	137.26	1.74	0.00	1.00	0.00	30.95	138.94	1.79	0.00	1.00	0.00
31.03	140.71	1.84	0.00	1.00	0.00	31.10	142.33	1.89	0.00	1.00	0.00
31.15	144.07	1.94	0.00	1.00	0.00	31.20	146.05	2.00	0.00	1.00	0.00
31.26	147.81	2.00	0.00	1.00	0.00	31.34	147.23	2.00	0.00	1.00	0.00
31.37	146.99	2.00	0.00	1.00	0.00	31.38	145.70	1.99	0.00	1.00	0.00
31.43	146.17	2.00	0.00	1.00	0.00	31.47	143.44	1.91	0.00	1.00	0.00
31.55	139.35	1.79	0.00	1.00	0.00	31.59	132.93	1.61	0.00	1.00	0.00
31.66	124.83	1.40	0.00	1.00	0.00	31.73	116.80	1.23	0.36	1.00	0.00
31.78	110.36	1.10	0.52	1.00	0.00	31.84	106.34	1.03	0.83	1.00	0.01
31.93	104.84	1.00	0.85	1.00	0.01	31.98	106.04	1.02	0.84	1.00	0.00
32.02	108.88	1.07	0.52	1.00	0.00	32.09	111.87	1.13	0.51	1.00	0.00
32.16	113.86	1.16	0.37	1.00	0.00	32.22	114.52	1.17	0.37	1.00	0.00
32.27	114.53	1.17	0.37	1.00	0.00	32.34	114.38	1.17	0.37	1.00	0.00
32.42	114.11	1.16	0.37	1.00	0.00	32.46	113.62	1.15	0.37	1.00	0.00
32.54	113.25	1.14	0.51	1.00	0.01	32.60	112.00	1.12	0.51	1.00	0.00
32.67	111.53	1.11	0.51	1.00	0.00	32.75	111.85	1.12	0.51	1.00	0.00
32.81	113.95	1.15	0.37	1.00	0.00	32.89	116.21	1.20	0.36	1.00	0.00
32.94	114.84	1.17	0.37	1.00	0.00	32.95	116.07	1.19	0.36	1.00	0.00
33.00	117.56	1.22	0.36	1.00	0.00	33.06	122.40	1.32	0.25	1.00	0.00
33.11	123.66	1.35	0.00	1.00	0.00	33.20	123.53	1.35	0.25	1.00	0.00
33.25	123.06	1.34	0.25	1.00	0.00	33.34	122.48	1.32	0.25	1.00	0.00
33.38	122.68	1.33	0.25	1.00	0.00	33.48	123.78	1.35	0.25	1.00	0.00
33.58	125.79	1.39	0.00	1.00	0.00	33.63	128.81	1.46	0.00	1.00	0.00
33.73	132.15	1.55	0.00	1.00	0.00	33.82	136.16	1.65	0.00	1.00	0.00
33.87	140.58	1.77	0.00	1.00	0.00	33.96	145.13	1.91	0.00	1.00	0.00
34.02	150.66	2.00	0.00	1.00	0.00	34.11	157.32	2.00	0.00	1.00	0.00
34.18	164.99	2.00	0.00	1.00	0.00	34.26	172.52	2.00	0.00	1.00	0.00
34.35	179.50	2.00	0.00	1.00	0.00	34.44	185.53	2.00	0.00	1.00	0.00
34.49	190.23	2.00	0.00	1.00	0.00	34.59	192.83	2.00	0.00	1.00	0.00
34.69	194.12	2.00	0.00	1.00	0.00	34.76	194.53	2.00	0.00	1.00	0.00
34.83	194.02	2.00	0.00	1.00	0.00	34.93	191.54	2.00	0.00	1.00	0.00
35.02	188.08	2.00	0.00	1.00	0.00	35.12	184.23	2.00	0.00	1.00	0.00
35.22	181.13	2.00	0.00	1.00	0.00	35.30	177.46	2.00	0.00	1.00	0.00
35.38	168.21	2.00	0.00	1.00	0.00	35.43	161.35	2.00	0.00	1.00	0.00
35.46	155.80	2.00	0.00	1.00	0.00	35.51	153.78	2.00	0.00	1.00	0.00
35.56	146.76	2.00	0.00	1.00	0.00	35.66	138.53	2.00	0.00	1.00	0.00
35.70	130.03	2.00	0.00	1.00	0.00	35.80	123.66	2.00	0.00	1.00	0.00
35.89	119.95	2.00	0.00	1.00	0.00	35.96	120.81	2.00	0.00	1.00	0.00
36.04	120.37	2.00	0.00	1.00	0.00	36.14	117.01	2.00	0.00	1.00	0.00
36.19	110.69	2.00	0.00	1.00	0.00	36.28	110.05	2.00	0.00	1.00	0.00
36.33	108.32	2.00	0.00	1.00	0.00	36.42	108.08	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
36.48	107.27	2.00	0.00	1.00	0.00	36.52	112.95	2.00	0.00	1.00	0.00
36.62	119.67	2.00	0.00	1.00	0.00	36.68	126.59	2.00	0.00	1.00	0.00
36.77	128.11	2.00	0.00	1.00	0.00	36.86	126.60	2.00	0.00	1.00	0.00
36.90	115.19	2.00	0.00	1.00	0.00	37.00	103.13	2.00	0.00	1.00	0.00
37.10	112.56	2.00	0.00	1.00	0.00	37.20	136.84	2.00	0.00	1.00	0.00
37.29	147.30	2.00	0.00	1.00	0.00	37.39	149.01	2.00	0.00	1.00	0.00
37.49	155.00	2.00	0.00	1.00	0.00	37.53	160.20	2.00	0.00	1.00	0.00
37.58	165.44	2.00	0.00	1.00	0.00	37.62	169.66	2.00	0.00	1.00	0.00
37.69	175.10	2.00	0.00	1.00	0.00	37.77	179.78	2.00	0.00	1.00	0.00
37.82	183.39	2.00	0.00	1.00	0.00	37.87	184.85	2.00	0.00	1.00	0.00
37.91	184.82	2.00	0.00	1.00	0.00	37.97	183.06	2.00	0.00	1.00	0.00
38.06	179.59	2.00	0.00	1.00	0.00	38.10	175.74	2.00	0.00	1.00	0.00
38.17	172.34	2.00	0.00	1.00	0.00	38.25	169.66	2.00	0.00	1.00	0.00
38.35	167.11	2.00	0.00	1.00	0.00	38.40	164.83	2.00	0.00	1.00	0.00
38.46	163.21	2.00	0.00	1.00	0.00	38.54	162.26	2.00	0.00	1.00	0.00
38.60	161.69	2.00	0.00	1.00	0.00	38.69	161.77	2.00	0.00	1.00	0.00
38.74	162.53	2.00	0.00	1.00	0.00	38.83	163.73	2.00	0.00	1.00	0.00
38.88	163.54	2.00	0.00	1.00	0.00	38.97	162.47	2.00	0.00	1.00	0.00
39.02	160.45	2.00	0.00	1.00	0.00	39.11	158.54	2.00	0.00	1.00	0.00
39.16	154.99	2.00	0.00	1.00	0.00	39.23	148.10	1.92	0.00	1.00	0.00
39.24	145.08	1.83	0.00	1.00	0.00	39.28	143.39	1.78	0.00	1.00	0.00
39.32	144.08	1.80	0.00	1.00	0.00	39.39	139.67	2.00	0.00	1.00	0.00
39.47	133.48	2.00	0.00	1.00	0.00	39.54	125.99	2.00	0.00	1.00	0.00
39.62	117.99	2.00	0.00	1.00	0.00	39.71	110.70	2.00	0.00	1.00	0.00
39.76	105.08	2.00	0.00	1.00	0.00	39.85	101.34	2.00	0.00	1.00	0.00
39.90	98.95	2.00	0.00	1.00	0.00	40.00	97.53	2.00	0.00	1.00	0.00
40.06	96.96	2.00	0.00	1.00	0.00	40.15	97.18	2.00	0.00	1.00	0.00
40.21	98.86	2.00	0.00	1.00	0.00	40.29	102.19	2.00	0.00	1.00	0.00
40.35	108.27	2.00	0.00	1.00	0.00	40.43	111.81	2.00	0.00	1.00	0.00
40.52	114.58	2.00	0.00	1.00	0.00	40.58	115.00	2.00	0.00	1.00	0.00
40.67	116.83	2.00	0.00	1.00	0.00	40.77	117.65	2.00	0.00	1.00	0.00
40.84	117.99	2.00	0.00	1.00	0.00	40.89	116.25	2.00	0.00	1.00	0.00
40.94	111.31	2.00	0.00	1.00	0.00	41.03	103.18	2.00	0.00	1.00	0.00
41.08	96.47	2.00	0.00	1.00	0.00	41.14	92.51	2.00	0.00	1.00	0.00
41.22	90.97	2.00	0.00	1.00	0.00	41.28	91.29	0.75	2.32	1.00	0.02
41.33	93.52	0.78	2.24	1.00	0.01	41.42	97.02	0.82	2.12	1.00	0.02
41.47	100.81	0.87	1.55	1.00	0.01	41.52	104.48	0.93	1.47	1.00	0.01
41.62	107.92	0.98	0.82	1.00	0.01	41.67	112.91	1.07	0.51	1.00	0.00
41.76	118.23	1.16	0.36	1.00	0.00	41.82	123.75	1.28	0.25	1.00	0.00
41.90	128.02	1.37	0.00	1.00	0.00	41.99	131.05	1.44	0.00	1.00	0.00
42.05	132.58	1.48	0.00	1.00	0.00	42.15	132.77	1.48	0.00	1.00	0.00
42.23	132.06	1.46	0.00	1.00	0.00	42.30	130.51	1.43	0.00	1.00	0.00
42.38	127.88	1.36	0.00	1.00	0.00	42.48	123.60	1.27	0.25	1.00	0.00
42.57	119.15	1.18	0.36	1.00	0.00	42.64	115.28	1.11	0.50	1.00	0.00
42.72	111.72	1.04	0.80	1.00	0.01	42.82	108.24	0.98	0.82	1.00	0.01
42.90	105.42	0.94	1.45	1.00	0.01	42.97	104.32	0.92	1.47	1.00	0.01
43.06	104.69	0.93	1.47	1.00	0.02	43.15	102.43	0.89	1.51	1.00	0.02
43.20	99.54	0.85	1.58	1.00	0.01	43.30	95.67	0.80	2.17	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
43.40	97.12	0.82	2.12	1.00	0.02	43.48	100.97	0.87	1.55	1.00	0.01
43.51	103.89	0.92	1.48	1.00	0.01	43.52	107.23	0.97	0.83	1.00	0.00
43.56	114.20	1.09	0.51	1.00	0.00	43.61	124.81	1.30	0.25	1.00	0.00
43.67	133.29	1.49	0.00	1.00	0.00	43.72	140.56	1.68	0.00	1.00	0.00
43.80	145.95	1.83	0.00	1.00	0.00	43.85	149.84	1.95	0.00	1.00	0.00
43.90	152.56	2.00	0.00	1.00	0.00	43.94	154.37	2.00	0.00	1.00	0.00
43.99	155.28	2.00	0.00	1.00	0.00	44.08	155.65	2.00	0.00	1.00	0.00
44.14	156.49	2.00	0.00	1.00	0.00	44.22	157.19	2.00	0.00	1.00	0.00
44.28	157.37	2.00	0.00	1.00	0.00	44.33	156.78	2.00	0.00	1.00	0.00
44.40	155.80	2.00	0.00	1.00	0.00	44.48	155.90	2.00	0.00	1.00	0.00
44.52	155.24	2.00	0.00	1.00	0.00	44.61	155.88	2.00	0.00	1.00	0.00
44.72	156.70	2.00	0.00	1.00	0.00	44.77	159.04	2.00	0.00	1.00	0.00
44.91	160.27	2.00	0.00	1.00	0.00	44.95	156.88	2.00	0.00	1.00	0.00
45.02	154.33	2.00	0.00	1.00	0.00	45.04	138.44	1.62	0.00	1.00	0.00
45.06	140.63	1.68	0.00	1.00	0.00	45.11	143.03	1.75	0.00	1.00	0.00
45.15	160.49	2.00	0.00	1.00	0.00	45.21	163.81	2.00	0.00	1.00	0.00
45.25	166.43	2.00	0.00	1.00	0.00	45.30	168.34	2.00	0.00	1.00	0.00
45.35	169.35	2.00	0.00	1.00	0.00	45.41	169.64	2.00	0.00	1.00	0.00
45.49	168.87	2.00	0.00	1.00	0.00	45.55	167.24	2.00	0.00	1.00	0.00
45.63	164.52	2.00	0.00	1.00	0.00	45.69	161.09	2.00	0.00	1.00	0.00
45.78	156.88	2.00	0.00	1.00	0.00	45.84	151.68	2.00	0.00	1.00	0.00
45.93	145.18	1.81	0.00	1.00	0.00	46.02	137.24	2.00	0.00	1.00	0.00
46.08	128.00	2.00	0.00	1.00	0.00	46.16	118.20	2.00	0.00	1.00	0.00
46.24	108.31	2.00	0.00	1.00	0.00	46.31	99.54	2.00	0.00	1.00	0.00
46.41	94.32	2.00	0.00	1.00	0.00	46.48	95.41	2.00	0.00	1.00	0.00
46.56	101.49	2.00	0.00	1.00	0.00	46.65	106.39	2.00	0.00	1.00	0.00
46.75	104.92	2.00	0.00	1.00	0.00	46.84	96.75	2.00	0.00	1.00	0.00
46.94	92.20	2.00	0.00	1.00	0.00	47.02	89.65	2.00	0.00	1.00	0.00
47.08	87.68	2.00	0.00	1.00	0.00	47.12	86.24	2.00	0.00	1.00	0.00
47.16	84.67	2.00	0.00	1.00	0.00	47.21	82.35	2.00	0.00	1.00	0.00
47.27	79.44	2.00	0.00	1.00	0.00	47.35	76.72	2.00	0.00	1.00	0.00
47.40	72.71	2.00	0.00	1.00	0.00	47.50	68.97	2.00	0.00	1.00	0.00
47.55	65.28	2.00	0.00	1.00	0.00	47.61	63.67	2.00	0.00	1.00	0.00
47.69	62.57	2.00	0.00	1.00	0.00	47.76	61.71	2.00	0.00	1.00	0.00
47.83	60.22	2.00	0.00	1.00	0.00	47.93	58.40	2.00	0.00	1.00	0.00
48.02	57.34	2.00	0.00	1.00	0.00	48.09	56.35	2.00	0.00	1.00	0.00
48.18	57.05	2.00	0.00	1.00	0.00	48.27	58.44	2.00	0.00	1.00	0.00
48.37	61.09	2.00	0.00	1.00	0.00	48.46	62.98	2.00	0.00	1.00	0.00
48.52	64.25	2.00	0.00	1.00	0.00	48.60	65.23	2.00	0.00	1.00	0.00
48.70	65.99	2.00	0.00	1.00	0.00	48.79	66.70	2.00	0.00	1.00	0.00
48.85	68.42	2.00	0.00	1.00	0.00	48.94	71.44	2.00	0.00	1.00	0.00
49.04	73.34	2.00	0.00	1.00	0.00	49.13	82.09	2.00	0.00	1.00	0.00
49.23	92.00	2.00	0.00	1.00	0.00	49.33	102.80	2.00	0.00	1.00	0.00
49.38	109.60	2.00	0.00	1.00	0.00	49.42	114.80	2.00	0.00	1.00	0.00
49.48	118.93	2.00	0.00	1.00	0.00	49.53	121.43	2.00	0.00	1.00	0.00
49.58	123.62	2.00	0.00	1.00	0.00	49.63	125.52	2.00	0.00	1.00	0.00
49.72	126.23	2.00	0.00	1.00	0.00	49.77	125.98	2.00	0.00	1.00	0.00
49.83	125.40	2.00	0.00	1.00	0.00	49.92	124.67	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
49.97	123.55	2.00	0.00	1.00	0.00	50.04	122.65	2.00	0.00	1.00	0.00
50.11	122.33	2.00	0.00	1.00	0.00	50.20	120.55	2.00	0.00	1.00	0.00
50.27	116.01	2.00	0.00	1.00	0.00	50.34	107.79	2.00	0.00	1.00	0.00
50.45	99.22	2.00	0.00	1.00	0.00	50.54	92.39	2.00	0.00	1.00	0.00
50.59	87.71	2.00	0.00	1.00	0.00	50.68	83.78	2.00	0.00	1.00	0.00
50.79	80.17	2.00	0.00	1.00	0.00	50.88	78.18	2.00	0.00	1.00	0.00
50.98	77.89	2.00	0.00	1.00	0.00	51.07	76.09	2.00	0.00	1.00	0.00
51.17	71.67	2.00	0.00	1.00	0.00	51.24	68.77	2.00	0.00	1.00	0.00
51.33	70.43	2.00	0.00	1.00	0.00	51.46	74.75	2.00	0.00	1.00	0.00
51.46	78.20	2.00	0.00	1.00	0.00	51.51	79.60	2.00	0.00	1.00	0.00
51.56	82.02	2.00	0.00	1.00	0.00	51.65	84.26	2.00	0.00	1.00	0.00
51.71	86.89	2.00	0.00	1.00	0.00	51.79	88.80	2.00	0.00	1.00	0.00
51.85	92.19	2.00	0.00	1.00	0.00	51.94	96.33	2.00	0.00	1.00	0.00
51.99	102.62	2.00	0.00	1.00	0.00	52.09	109.52	2.00	0.00	1.00	0.00
52.19	116.81	2.00	0.00	1.00	0.00	52.28	122.63	2.00	0.00	1.00	0.00
52.35	128.41	2.00	0.00	1.00	0.00	52.43	132.82	2.00	0.00	1.00	0.00
52.52	136.28	2.00	0.00	1.00	0.00	52.62	135.93	2.00	0.00	1.00	0.00
52.72	133.92	2.00	0.00	1.00	0.00	52.81	135.53	2.00	0.00	1.00	0.00
52.91	146.31	2.00	0.00	1.00	0.00	53.00	154.70	2.00	0.00	1.00	0.00
53.10	148.13	2.00	0.00	1.00	0.00	53.20	129.79	2.00	0.00	1.00	0.00
53.29	114.61	2.00	0.00	1.00	0.00	53.38	114.09	2.00	0.00	1.00	0.00
53.46	119.81	2.00	0.00	1.00	0.00	53.53	130.93	2.00	0.00	1.00	0.00
53.63	139.93	2.00	0.00	1.00	0.00	53.73	146.92	2.00	0.00	1.00	0.00
53.82	150.03	2.00	0.00	1.00	0.00	53.92	146.54	2.00	0.00	1.00	0.00
53.94	138.23	1.66	0.00	1.00	0.00	53.96	131.20	1.48	0.00	1.00	0.00
53.97	134.16	1.55	0.00	1.00	0.00	54.05	141.00	1.73	0.00	1.00	0.00
54.08	150.15	2.00	0.00	1.00	0.00	54.13	154.41	2.00	0.00	1.00	0.00
54.19	159.56	2.00	0.00	1.00	0.00	54.25	162.94	2.00	0.00	1.00	0.00
54.28	166.66	2.00	0.00	1.00	0.00	54.29	164.40	2.00	0.00	1.00	0.00
54.34	164.35	2.00	0.00	1.00	0.00	54.35	164.72	2.00	0.00	1.00	0.00
54.40	165.62	2.00	0.00	1.00	0.00	54.44	166.45	2.00	0.00	1.00	0.00
54.49	165.88	2.00	0.00	1.00	0.00	54.53	167.39	2.00	0.00	1.00	0.00
54.57	171.02	2.00	0.00	1.00	0.00	54.58	173.92	2.00	0.00	1.00	0.00
54.63	173.90	2.00	0.00	1.00	0.00	54.68	176.93	2.00	0.00	1.00	0.00
54.73	175.12	2.00	0.00	1.00	0.00	54.78	173.29	2.00	0.00	1.00	0.00
54.83	172.82	2.00	0.00	1.00	0.00	54.88	175.08	2.00	0.00	1.00	0.00
54.92	178.37	2.00	0.00	1.00	0.00	54.97	180.73	2.00	0.00	1.00	0.00
55.02	181.62	2.00	0.00	1.00	0.00	55.12	178.01	2.00	0.00	1.00	0.00
55.17	170.63	2.00	0.00	1.00	0.00	55.25	160.49	2.00	0.00	1.00	0.00
55.31	154.46	2.00	0.00	1.00	0.00	55.36	148.87	1.98	0.00	1.00	0.00
55.45	143.68	1.82	0.00	1.00	0.00	55.50	137.89	1.66	0.00	1.00	0.00
55.60	133.93	1.56	0.00	1.00	0.00	55.65	128.15	1.41	0.00	1.00	0.00
55.71	124.39	1.33	0.25	1.00	0.00	55.75	121.19	1.26	0.25	1.00	0.00
55.79	121.90	1.27	0.25	1.00	0.00	55.84	123.76	1.32	0.25	1.00	0.00
55.89	125.39	1.35	0.00	1.00	0.00	55.90	126.17	1.37	0.00	1.00	0.00
55.94	124.98	1.34	0.25	1.00	0.00	55.99	122.89	1.30	0.25	1.00	0.00
56.03	120.41	1.24	0.36	1.00	0.00	56.08	118.54	1.21	0.36	1.00	0.00
56.14	116.74	1.17	0.36	1.00	0.00	56.22	114.65	1.13	0.50	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
56.28	112.90	1.10	0.51	1.00	0.00	56.33	112.38	1.09	0.51	1.00	0.00
56.38	112.46	1.09	0.51	1.00	0.00	56.45	114.23	1.13	0.51	1.00	0.00
56.52	117.01	1.18	0.36	1.00	0.00	56.62	120.21	1.24	0.36	1.00	0.00
56.66	123.02	1.30	0.25	1.00	0.00	56.73	126.65	1.39	0.00	1.00	0.00
56.81	129.59	1.46	0.00	1.00	0.00	56.95	132.64	1.53	0.00	1.00	0.00
57.00	135.80	1.61	0.00	1.00	0.00	57.09	136.52	1.63	0.00	1.00	0.00
57.19	135.85	1.62	0.00	1.00	0.00	57.27	131.44	1.50	0.00	1.00	0.00
57.35	130.16	1.47	0.00	1.00	0.00	57.44	127.36	1.41	0.00	1.00	0.00
57.50	127.07	1.40	0.00	1.00	0.00	57.52	131.85	1.52	0.00	1.00	0.00
57.58	141.73	1.78	0.00	1.00	0.00	57.63	149.17	2.00	0.00	1.00	0.00
57.72	151.31	2.00	0.00	1.00	0.00	57.77	148.26	1.98	0.00	1.00	0.00
57.82	143.29	1.83	0.00	1.00	0.00	57.91	137.09	1.66	0.00	1.00	0.00
57.96	130.46	1.48	0.00	1.00	0.00	58.02	135.16	1.61	0.00	1.00	0.00
58.09	138.12	1.69	0.00	1.00	0.00	58.16	142.65	1.82	0.00	1.00	0.00
58.25	144.36	1.87	0.00	1.00	0.00	58.30	143.26	1.83	0.00	1.00	0.00
58.40	140.74	1.76	0.00	1.00	0.00	58.50	139.77	1.74	0.00	1.00	0.00
58.56	138.70	1.71	0.00	1.00	0.00	58.64	140.28	1.75	0.00	1.00	0.00
58.73	145.16	1.90	0.00	1.00	0.00	58.78	145.87	1.92	0.00	1.00	0.00
58.88	147.98	1.98	0.00	1.00	0.00	58.97	149.10	2.00	0.00	1.00	0.00
59.07	147.53	1.97	0.00	1.00	0.00	59.13	143.73	1.86	0.00	1.00	0.00
59.23	140.99	1.78	0.00	1.00	0.00	59.31	134.94	1.61	0.00	1.00	0.00
59.38	130.71	1.50	0.00	1.00	0.00	59.41	127.40	1.42	0.00	1.00	0.00
59.46	128.62	1.45	0.00	1.00	0.00	59.51	128.55	1.45	0.00	1.00	0.00
59.57	130.91	1.51	0.00	1.00	0.00	59.66	136.37	1.65	0.00	1.00	0.00
59.75	142.44	1.82	0.00	1.00	0.00	59.80	147.84	1.99	0.00	1.00	0.00
59.85	156.99	2.00	0.00	1.00	0.00	59.91	158.02	2.00	0.00	1.00	0.00
59.99	159.53	2.00	0.00	1.00	0.00	60.05	161.59	2.00	0.00	1.00	0.00
60.09	160.52	2.00	0.00	1.00	0.00	60.14	156.08	2.00	0.00	1.00	0.00
60.19	153.23	2.00	0.00	1.00	0.00	60.22	151.55	2.00	0.00	1.00	0.00
60.28	145.94	1.93	0.00	1.00	0.00	60.33	137.48	1.69	0.00	1.00	0.00
60.38	126.83	1.41	0.00	1.00	0.00	60.42	119.65	1.25	0.25	1.00	0.00
60.48	111.02	1.09	0.52	1.00	0.00	60.57	101.50	0.93	1.53	1.00	0.02
60.66	91.67	0.80	2.31	1.00	0.02	60.68	85.85	0.73	2.65	1.00	0.01
60.69	82.84	0.70	2.73	1.00	0.00	60.74	80.07	0.67	2.80	1.00	0.02
60.79	76.18	0.64	2.92	1.00	0.02	60.84	71.82	0.60	3.07	1.00	0.02
60.89	68.64	0.58	3.18	1.00	0.02	60.98	66.57	0.56	3.26	1.00	0.04
61.03	69.19	0.58	3.16	1.00	0.02	61.08	79.69	0.67	2.81	1.00	0.02
61.18	90.12	0.78	2.37	1.00	0.03	61.23	100.04	0.91	1.57	1.00	0.01
61.31	94.03	0.83	2.22	1.00	0.02	61.42	94.11	0.83	2.22	1.00	0.03
61.47	100.64	0.92	1.55	1.00	0.01	61.51	107.25	1.03	0.83	1.00	0.00
61.54	108.54	1.05	0.82	1.00	0.00	61.57	112.23	1.11	0.51	1.00	0.00
61.58	118.74	1.24	0.36	1.00	0.00	61.61	111.49	1.10	0.51	1.00	0.00
61.63	107.07	1.02	0.83	1.00	0.00	61.63	91.77	0.80	2.30	1.00	0.00
61.66	79.27	0.67	2.83	1.00	0.01	61.67	85.35	0.73	2.66	1.00	0.00
61.70	83.80	0.71	2.70	1.00	0.01	61.71	84.55	0.72	2.68	1.00	0.00
61.76	87.45	0.75	2.61	1.00	0.01	61.80	91.10	0.79	2.33	1.00	0.01
61.84	94.04	0.83	2.22	1.00	0.01	61.86	98.87	0.90	1.59	1.00	0.00
61.93	103.69	0.97	0.85	1.00	0.01	61.98	100.92	0.93	1.55	1.00	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
62.04	114.48	1.16	0.37	1.00	0.00	62.09	127.59	1.44	0.00	1.00	0.00
62.14	136.10	1.66	0.00	1.00	0.00	62.19	140.93	1.80	0.00	1.00	0.00
62.24	143.65	1.88	0.00	1.00	0.00	62.26	146.58	1.97	0.00	1.00	0.00
62.29	146.46	1.97	0.00	1.00	0.00	62.38	145.37	1.93	0.00	1.00	0.00
62.44	138.07	1.72	0.00	1.00	0.00	62.46	132.02	1.55	0.00	1.00	0.00
62.47	126.07	1.41	0.00	1.00	0.00	62.51	127.59	1.44	0.00	1.00	0.00
62.56	130.45	1.52	0.00	1.00	0.00	62.60	134.26	1.61	0.00	1.00	0.00
62.65	135.35	1.64	0.00	1.00	0.00	62.70	135.46	1.65	0.00	1.00	0.00
62.75	135.59	1.65	0.00	1.00	0.00	62.80	138.85	1.74	0.00	1.00	0.00
62.85	147.40	2.00	0.00	1.00	0.00	62.89	159.73	2.00	0.00	1.00	0.00
62.97	173.86	2.00	0.00	1.00	0.00	63.04	187.32	2.00	0.00	1.00	0.00
63.09	197.18	2.00	0.00	1.00	0.00	63.13	200.57	2.00	0.00	1.00	0.00
63.19	200.74	2.00	0.00	1.00	0.00	63.23	201.69	2.00	0.00	1.00	0.00
63.28	203.42	2.00	0.00	1.00	0.00	63.32	204.02	2.00	0.00	1.00	0.00
63.38	202.89	2.00	0.00	1.00	0.00	63.44	203.06	2.00	0.00	1.00	0.00
63.52	199.75	2.00	0.00	1.00	0.00	63.57	194.57	2.00	0.00	1.00	0.00
63.66	183.79	2.00	0.00	1.00	0.00	63.73	148.76	2.00	0.00	1.00	0.00
63.76	130.54	1.53	0.00	1.00	0.00	63.76	127.66	1.45	0.00	1.00	0.00
63.78	131.02	1.54	0.00	1.00	0.00	63.81	142.46	1.86	0.00	1.00	0.00
63.85	146.19	1.97	0.00	1.00	0.00	63.86	145.10	1.94	0.00	1.00	0.00
63.91	148.35	2.00	0.00	1.00	0.00	63.94	150.35	2.00	0.00	1.00	0.00
63.95	151.38	2.00	0.00	1.00	0.00	64.00	150.67	2.00	0.00	1.00	0.00
64.02	149.37	2.00	0.00	1.00	0.00	64.05	148.02	2.00	0.00	1.00	0.00
64.09	146.64	1.99	0.00	1.00	0.00	64.11	144.77	1.93	0.00	1.00	0.00
64.15	142.44	1.86	0.00	1.00	0.00	64.20	141.24	1.82	0.00	1.00	0.00
64.25	141.74	1.84	0.00	1.00	0.00	64.29	148.11	2.00	0.00	1.00	0.00
64.34	157.68	2.00	0.00	1.00	0.00	64.43	167.40	2.00	0.00	1.00	0.00
64.48	174.30	2.00	0.00	1.00	0.00	64.53	177.47	2.00	0.00	1.00	0.00
64.58	180.82	2.00	0.00	1.00	0.00	64.63	187.83	2.00	0.00	1.00	0.00
64.68	195.77	2.00	0.00	1.00	0.00	64.73	198.20	2.00	0.00	1.00	0.00
64.77	202.79	2.00	0.00	1.00	0.00	64.82	207.01	2.00	0.00	1.00	0.00
64.87	201.76	2.00	0.00	1.00	0.00	64.89	196.56	2.00	0.00	1.00	0.00
64.93	189.73	2.00	0.00	1.00	0.00	64.94	196.96	2.00	0.00	1.00	0.00
64.98	199.62	2.00	0.00	1.00	0.00	64.99	201.90	2.00	0.00	1.00	0.00
65.03	201.35	2.00	0.00	1.00	0.00	65.08	199.79	2.00	0.00	1.00	0.00
65.13	196.50	2.00	0.00	1.00	0.00	65.17	193.13	2.00	0.00	1.00	0.00
65.22	189.08	2.00	0.00	1.00	0.00	65.23	186.93	2.00	0.00	1.00	0.00
65.28	186.22	2.00	0.00	1.00	0.00	65.32	186.24	2.00	0.00	1.00	0.00
65.37	186.30	2.00	0.00	1.00	0.00	65.42	187.42	2.00	0.00	1.00	0.00
65.47	183.76	2.00	0.00	1.00	0.00	65.48	179.77	2.00	0.00	1.00	0.00
65.49	174.70	2.00	0.00	1.00	0.00	65.52	174.01	2.00	0.00	1.00	0.00
65.57	176.43	2.00	0.00	1.00	0.00	65.62	180.61	2.00	0.00	1.00	0.00
65.67	-1.00	2.00	0.00	1.00	0.00	65.69	-1.00	2.00	0.00	1.00	0.00
65.72	-1.00	2.00	0.00	1.00	0.00	65.77	-1.00	2.00	0.00	1.00	0.00
65.82	-1.00	2.00	0.00	1.00	0.00	65.86	-1.00	2.00	0.00	1.00	0.00
65.86	-1.00	2.00	0.00	1.00	0.00	65.91	-1.00	2.00	0.00	1.00	0.00
65.96	-1.00	2.00	0.00	1.00	0.00						

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)

Total estimated settlement: 0.79

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation (Robertson (2009) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.01	-0.03	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.04	-0.03	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.08	-0.07	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.10	-0.03	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.13	-0.03	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.18	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.22	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.27	0.81	1.28	50.14	63.98	4.01	4.89	3.60
0.33	2.77	4.42	15.47	68.30	3.31	5.08	10.70
0.36	5.16	8.26	7.99	66.07	2.95	0.18	0.67
0.37	7.12	11.41	5.40	61.61	2.76	0.13	0.66
0.38	8.20	13.14	4.58	60.15	2.69	0.11	0.66
0.42	9.38	15.03	3.98	59.88	2.63	0.11	0.66
0.44	10.59	16.98	3.58	60.79	2.58	0.12	0.66
0.47	12.18	19.53	3.09	60.26	2.52	0.12	0.66
0.47	14.24	22.83	2.61	59.51	2.44	0.11	0.66
0.52	17.00	27.27	2.14	58.39	2.35	0.10	0.65
0.56	20.48	32.85	1.78	58.60	2.26	0.10	0.65
0.58	24.93	40.00	1.52	60.77	2.16	0.12	0.66
0.61	30.70	49.27	1.35	66.61	2.05	0.19	0.67
0.66	36.94	59.30	1.27	75.22	1.95	0.39	0.70
0.76	40.79	65.47	1.23	80.72	1.89	0.62	0.71
0.80	38.66	62.05	1.25	77.85	1.93	0.49	0.70
0.81	35.49	56.95	1.29	73.41	1.98	0.34	0.69
0.85	32.42	52.02	1.33	69.37	2.03	0.24	0.68
0.86	32.79	52.62	1.33	69.99	2.03	0.25	0.68
0.90	32.22	51.69	1.35	70.01	2.05	0.25	0.68
0.95	31.82	51.04	1.38	70.34	2.07	0.26	0.68
1.00	30.53	48.97	1.37	67.09	2.06	0.20	0.68
1.05	28.88	46.31	1.34	62.22	2.04	0.14	0.66
1.14	26.55	42.56	1.00	42.56	2.01	0.03	0.62
1.24	24.29	38.92	1.00	38.92	2.04	0.03	0.62
1.31	20.51	32.85	1.00	32.85	2.14	0.02	0.62
1.36	17.93	28.70	1.67	48.03	2.22	0.05	0.62
1.37	17.77	28.44	1.71	48.50	2.23	0.05	0.62
1.39	18.54	29.68	1.64	48.64	2.21	0.05	0.62
1.43	19.03	30.46	1.60	48.73	2.19	0.05	0.62
1.44	18.05	28.88	1.68	48.54	2.23	0.05	0.62
1.49	18.35	29.36	1.67	49.05	2.22	0.05	0.62
1.53	18.89	30.23	1.66	50.30	2.22	0.05	0.63
1.58	19.67	31.47	1.66	52.29	2.22	0.06	0.63
1.63	20.62	32.99	1.66	54.77	2.22	0.08	0.64
1.68	21.70	34.72	1.65	57.36	2.21	0.09	0.65
1.72	23.31	37.31	1.61	60.04	2.20	0.11	0.66
1.77	25.48	40.78	1.54	62.93	2.17	0.14	0.66
1.82	28.31	45.33	1.46	66.36	2.13	0.19	0.67
1.86	31.52	50.48	1.40	70.45	2.08	0.26	0.68
1.92	35.09	56.22	1.34	75.14	2.03	0.39	0.70

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.97	38.67	61.96	1.29	80.21	1.98	0.59	0.71
2.01	41.61	66.68	1.27	84.88	1.95	0.72	0.72
2.09	43.22	69.27	1.26	87.55	1.94	0.72	0.72
2.16	43.05	68.99	1.27	87.53	1.95	0.72	0.72
2.20	41.47	66.43	1.28	85.02	1.96	0.72	0.72
2.25	39.85	63.83	1.29	82.39	1.98	0.71	0.71
2.31	38.60	61.82	1.30	80.09	1.99	0.59	0.71
2.37	37.79	60.52	1.29	78.32	1.98	0.51	0.70
2.40	36.88	59.05	1.30	76.51	1.99	0.44	0.70
2.46	35.97	57.57	1.29	74.55	1.98	0.37	0.69
2.54	35.36	56.59	1.29	72.87	1.97	0.32	0.69
2.59	34.69	55.51	1.00	55.51	1.96	0.08	0.64
2.69	34.25	54.80	1.00	54.80	1.94	0.08	0.64
2.74	33.95	54.31	1.00	54.31	1.92	0.07	0.64
2.83	33.88	54.19	1.00	54.19	1.92	0.07	0.64
2.88	34.35	54.94	1.00	54.94	1.91	0.08	0.64
2.98	35.70	57.10	1.00	57.10	1.89	0.09	0.65
3.03	38.57	61.71	1.00	61.71	1.85	0.13	0.66
3.12	42.31	67.72	1.00	67.72	1.82	0.21	0.68
3.21	46.83	74.97	1.00	74.97	1.79	0.38	0.70
3.27	51.66	82.72	1.00	82.72	1.76	0.71	0.71
3.34	57.05	91.38	1.00	91.38	1.72	0.73	0.73
3.41	61.91	99.18	1.00	99.18	1.69	0.75	0.75
3.51	64.20	102.85	1.00	102.85	1.68	0.75	0.75
3.55	63.63	101.93	1.00	101.93	1.70	0.75	0.75
3.65	62.42	99.97	1.00	99.97	1.72	0.75	0.75
3.75	61.71	98.83	1.00	98.83	1.73	0.75	0.75
3.83	61.44	98.39	1.00	98.39	1.73	0.75	0.75
3.94	61.11	97.84	1.00	97.84	1.73	0.74	0.74
4.04	60.30	96.53	1.00	96.53	1.73	0.74	0.74
4.13	60.63	97.06	1.08	104.72	1.75	0.76	0.76
4.24	61.68	98.73	1.00	98.73	1.74	0.75	0.75
4.38	65.15	104.30	1.00	104.30	1.68	0.76	0.76
4.50	68.93	110.36	1.00	110.36	1.62	0.77	0.77
4.62	74.13	118.70	1.00	118.70	1.57	0.78	0.78
4.71	77.89	124.73	1.00	124.73	1.57	0.79	0.79
4.75	80.93	129.61	1.00	129.61	1.57	0.80	0.80
4.84	82.11	131.50	1.00	131.50	1.58	0.80	0.80
4.89	82.93	132.82	1.00	132.82	1.58	0.80	0.80
4.94	82.93	132.82	1.00	132.82	1.58	0.80	0.80
4.98	81.72	130.87	1.00	130.87	1.59	0.80	0.80
5.07	80.10	128.25	1.00	128.25	1.60	0.80	0.80
5.13	78.48	125.65	1.00	125.65	1.61	0.79	0.79
5.17	76.79	122.93	1.00	122.93	1.61	0.79	0.79
5.27	74.77	119.67	1.00	119.67	1.62	0.78	0.78
5.32	72.75	116.42	1.00	116.42	1.63	0.78	0.78
5.42	70.86	113.37	1.00	113.37	1.64	0.77	0.77
5.46	69.34	110.93	1.00	110.93	1.64	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.56	68.02	108.80	1.00	108.80	1.65	0.76	0.76
5.61	66.87	106.96	1.00	106.96	1.66	0.76	0.76
5.71	65.86	105.32	1.00	105.32	1.66	0.76	0.76
5.78	64.92	103.80	1.00	103.80	1.67	0.76	0.76
5.85	63.84	102.06	1.00	102.06	1.68	0.75	0.75
5.95	62.83	100.42	1.00	100.42	1.69	0.75	0.75
6.00	62.32	99.61	1.00	99.61	1.71	0.75	0.75
6.09	62.93	100.57	1.00	100.57	1.66	0.75	0.75
6.14	64.75	103.50	1.00	103.50	1.60	0.75	0.75
6.24	67.52	107.94	1.00	107.94	1.53	0.76	0.76
6.30	70.42	112.60	1.00	112.60	1.54	0.77	0.77
6.38	71.40	114.16	1.00	114.16	1.56	0.77	0.77
6.46	69.58	111.22	1.00	111.22	1.60	0.77	0.77
6.50	68.43	109.38	1.00	109.38	1.62	0.77	0.77
6.56	68.84	110.02	1.00	110.02	1.63	0.77	0.77
6.63	71.30	113.98	1.00	113.98	1.61	0.77	0.77
6.68	72.51	115.92	1.00	115.92	1.61	0.78	0.78
6.76	73.49	117.34	1.00	117.34	1.61	0.78	0.78
6.82	74.54	118.51	1.00	118.51	1.60	0.78	0.78
6.88	76.19	120.59	1.00	120.59	1.59	0.78	0.78
6.96	78.38	123.33	1.00	123.33	1.58	0.79	0.79
7.03	80.54	126.09	1.00	126.09	1.56	0.79	0.79
7.11	82.06	127.75	1.00	127.75	1.55	0.80	0.80
7.16	83.04	128.83	1.00	128.83	1.55	0.80	0.80
7.26	83.82	129.11	1.00	129.11	1.55	0.80	0.80
7.31	84.43	129.55	1.00	129.55	1.56	0.80	0.80
7.40	84.63	129.06	1.00	129.06	1.56	0.80	0.80
7.45	84.52	128.43	1.00	128.43	1.56	0.80	0.80
7.54	83.95	126.75	1.00	126.75	1.57	0.79	0.79
7.60	82.84	124.58	1.00	124.58	1.58	0.79	0.79
7.68	81.22	121.42	1.00	121.42	1.59	0.79	0.79
7.74	79.70	118.70	1.00	118.70	1.60	0.78	0.78
7.83	78.55	116.27	1.00	116.27	1.61	0.78	0.78
7.90	78.35	115.47	1.00	115.47	1.61	0.78	0.78
7.98	79.10	115.95	1.00	115.95	1.62	0.78	0.78
8.05	80.62	117.66	1.00	117.66	1.62	0.78	0.78
8.12	81.69	118.66	1.00	118.66	1.62	0.78	0.78
8.19	81.66	118.08	1.00	118.08	1.62	0.78	0.78
8.27	80.48	115.81	1.00	115.81	1.64	0.78	0.78
8.36	79.13	113.39	1.00	113.39	1.65	0.77	0.77
8.41	78.35	111.75	1.00	111.75	1.61	0.77	0.77
8.50	78.42	111.21	1.00	111.21	1.57	0.77	0.77
8.60	78.79	111.10	1.00	111.10	1.54	0.77	0.77
8.70	78.76	110.43	1.00	110.43	1.56	0.77	0.77
8.74	70.97	99.16	1.00	99.16	1.64	0.75	0.75
8.78	65.57	92.36	1.00	92.36	1.68	0.73	0.73
8.81	63.58	89.84	1.00	89.84	1.71	0.73	0.73
8.86	69.75	97.38	1.00	97.38	1.66	0.74	0.74

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.91	73.77	102.14	1.00	102.14	1.64	0.75	0.75
8.94	74.34	102.81	1.00	102.81	1.64	0.75	0.75
9.02	73.80	101.95	1.00	101.95	1.66	0.75	0.75
9.10	72.52	100.12	1.00	100.12	1.68	0.75	0.75
9.17	71.17	98.18	1.00	98.18	1.69	0.74	0.74
9.22	69.95	96.47	1.00	96.47	1.70	0.74	0.74
9.31	69.01	94.84	1.00	94.84	1.71	0.74	0.74
9.37	68.50	93.92	1.00	93.92	1.72	0.74	0.74
9.42	68.60	93.81	1.00	93.81	1.72	0.74	0.74
9.52	69.18	94.01	1.00	94.01	1.72	0.74	0.74
9.60	70.19	94.84	1.00	94.84	1.71	0.74	0.74
9.66	71.54	96.20	1.00	96.20	1.70	0.74	0.74
9.74	73.13	97.75	1.00	97.75	1.69	0.74	0.74
9.81	74.58	99.20	1.00	99.20	1.69	0.75	0.75
9.89	75.79	100.34	1.00	100.34	1.68	0.75	0.75
9.98	77.04	101.50	1.00	101.50	1.68	0.75	0.75
10.03	78.79	103.47	1.00	103.47	1.68	0.75	0.75
10.13	81.26	106.04	1.00	106.04	1.67	0.76	0.76
10.23	84.06	108.97	1.00	108.97	1.66	0.76	0.76
10.32	86.45	111.33	1.00	111.33	1.65	0.77	0.77
10.38	88.11	112.97	1.00	112.97	1.65	0.77	0.77
10.47	88.68	113.17	1.00	113.17	1.65	0.77	0.77
10.57	88.44	112.36	1.00	112.36	1.65	0.77	0.77
10.66	87.94	111.05	1.00	111.05	1.61	0.77	0.77
10.76	87.67	110.18	1.00	110.18	1.57	0.77	0.77
10.85	88.00	110.11	1.00	110.11	1.53	0.77	0.77
10.92	88.54	110.44	1.00	110.44	1.55	0.77	0.77
11.00	85.17	105.80	1.00	105.80	1.58	0.76	0.76
11.07	82.17	101.74	1.00	101.74	1.61	0.75	0.75
11.10	80.21	99.18	1.00	99.18	1.63	0.75	0.75
11.15	82.81	102.16	1.00	102.16	1.62	0.75	0.75
11.19	85.41	105.18	1.00	105.18	1.61	0.76	0.76
11.24	87.43	107.45	1.00	107.45	1.61	0.76	0.76
11.29	89.66	109.95	1.00	109.95	1.61	0.77	0.77
11.34	92.29	112.96	1.00	112.96	1.60	0.77	0.77
11.40	94.89	115.81	1.00	115.81	1.60	0.78	0.78
11.47	96.81	117.83	1.00	117.83	1.60	0.78	0.78
11.53	97.72	118.60	1.00	118.60	1.60	0.78	0.78
11.58	98.23	118.97	1.00	118.97	1.60	0.78	0.78
11.65	98.70	119.16	1.00	119.16	1.61	0.78	0.78
11.72	99.17	119.34	1.00	119.34	1.61	0.78	0.78
11.77	99.00	118.88	1.00	118.88	1.61	0.78	0.78
11.82	98.36	117.83	1.00	117.83	1.62	0.78	0.78
11.88	97.25	116.19	1.00	116.19	1.64	0.78	0.78
11.97	96.10	114.49	1.00	114.49	1.65	0.77	0.77
12.02	94.75	112.75	1.00	112.75	1.65	0.77	0.77
12.06	93.54	110.95	1.00	110.95	1.65	0.77	0.77
12.11	93.03	110.11	1.00	110.11	1.65	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.21	92.63	109.15	1.00	109.15	1.65	0.76	0.76
12.25	92.93	109.21	1.00	109.21	1.64	0.76	0.76
12.30	93.00	109.05	1.00	109.05	1.64	0.76	0.76
12.31	93.44	109.51	1.00	109.51	1.63	0.77	0.77
12.32	93.64	109.72	1.00	109.72	1.63	0.77	0.77
12.35	94.21	110.25	1.00	110.25	1.62	0.77	0.77
12.40	95.26	111.26	1.00	111.26	1.61	0.77	0.77
12.45	96.78	112.82	1.00	112.82	1.60	0.77	0.77
12.52	98.43	114.40	1.00	114.40	1.60	0.77	0.77
12.56	100.32	116.43	1.00	116.43	1.59	0.78	0.78
12.62	102.04	118.16	1.00	118.16	1.59	0.78	0.78
12.65	103.69	119.90	1.00	119.90	1.56	0.78	0.78
12.71	105.14	121.32	1.00	121.32	1.53	0.78	0.78
12.76	107.34	123.61	1.00	123.61	1.48	0.79	0.79
12.83	110.34	126.74	1.00	126.74	1.48	0.79	0.79
12.88	114.29	131.03	1.00	131.03	1.50	0.80	0.80
12.93	118.94	136.14	1.00	136.14	1.50	0.81	0.81
12.98	121.44	138.73	1.00	138.73	1.52	0.81	0.81
13.03	123.77	141.10	1.00	141.10	1.52	0.81	0.81
13.04	120.16	136.93	1.00	136.93	1.54	0.81	0.81
13.07	122.72	139.66	1.00	139.66	1.54	0.81	0.81
13.13	125.66	142.70	1.00	142.70	1.55	0.82	0.82
13.17	134.36	152.37	1.00	152.37	1.53	0.83	0.83
13.22	137.87	156.08	1.00	156.08	1.53	0.84	0.84
13.27	140.13	158.31	1.00	158.31	1.54	0.84	0.84
13.32	141.11	159.12	1.00	159.12	1.54	0.84	0.84
13.37	141.28	159.00	1.00	159.00	1.55	0.84	0.84
13.41	140.67	158.02	1.00	158.02	1.55	0.84	0.84
13.46	139.05	155.85	1.00	155.85	1.56	0.83	0.83
13.51	137.63	153.98	1.00	153.98	1.57	0.83	0.83
13.56	135.98	151.81	1.00	151.81	1.58	0.83	0.83
13.60	134.29	149.65	1.00	149.65	1.59	0.83	0.83
13.66	132.81	147.65	1.00	147.65	1.60	0.82	0.82
13.75	131.80	145.98	1.00	145.98	1.60	0.82	0.82
13.80	131.19	145.02	1.00	145.02	1.60	0.82	0.82
13.89	130.75	144.01	1.00	144.01	1.61	0.82	0.82
13.94	129.81	142.69	1.00	142.69	1.61	0.82	0.82
13.99	128.19	140.62	1.00	140.62	1.63	0.81	0.81
14.09	125.39	137.21	1.00	137.21	1.65	0.81	0.81
14.14	122.28	133.79	1.00	133.79	1.68	0.80	0.80
14.23	119.38	130.35	1.00	130.35	1.70	0.80	0.80
14.28	117.19	127.54	1.00	127.54	1.68	0.79	0.79
14.38	116.43	125.95	1.00	125.95	1.66	0.79	0.79
14.42	115.35	124.40	1.00	124.40	1.63	0.79	0.79
14.52	115.79	124.40	1.00	124.40	1.63	0.79	0.79
14.57	116.75	125.23	1.00	125.23	1.64	0.79	0.79
14.67	117.53	125.60	1.00	125.60	1.64	0.79	0.79
14.68	117.83	125.93	1.00	125.93	1.64	0.79	0.79

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.70	116.41	124.39	1.00	124.39	1.65	0.79	0.79
14.75	116.58	124.38	1.00	124.38	1.66	0.79	0.79
14.80	116.18	123.80	1.00	123.80	1.66	0.79	0.79
14.89	116.21	123.45	1.00	123.45	1.67	0.79	0.79
14.94	114.76	121.75	1.00	121.75	1.68	0.79	0.79
15.04	111.83	118.29	1.00	118.29	1.69	0.78	0.78
15.13	107.24	113.18	1.01	114.51	1.71	0.77	0.77
15.21	101.74	107.19	1.06	113.68	1.74	0.77	0.77
15.28	95.87	100.87	1.10	111.36	1.76	0.77	0.77
15.38	90.00	94.46	1.14	107.63	1.79	0.76	0.76
15.47	83.86	87.79	1.17	102.77	1.82	0.75	0.75
15.57	77.55	80.97	1.20	97.12	1.85	0.74	0.74
15.67	70.76	73.71	1.23	90.52	1.89	0.73	0.73
15.77	63.91	66.40	1.26	83.47	1.93	0.71	0.71
15.86	57.27	59.33	1.29	76.63	1.98	0.44	0.70
15.96	51.73	53.45	1.34	71.45	2.03	0.29	0.69
16.05	47.31	48.75	1.40	68.25	2.09	0.22	0.68
16.15	43.60	44.83	1.51	67.79	2.15	0.21	0.68
16.25	41.11	42.13	1.63	68.47	2.20	0.22	0.68
16.31	39.86	40.76	1.71	69.57	2.23	0.25	0.68
16.39	39.72	40.48	1.70	68.78	2.23	0.23	0.68
16.48	40.50	41.08	1.65	67.59	2.21	0.21	0.68
16.59	43.06	43.47	1.53	66.70	2.17	0.19	0.67
16.68	47.95	48.20	1.40	67.68	2.09	0.21	0.68
16.76	53.89	53.96	1.31	70.90	2.01	0.27	0.69
16.86	58.72	58.53	1.27	74.31	1.95	0.36	0.69
16.92	61.25	60.90	1.25	76.25	1.92	0.43	0.70
17.02	61.65	61.10	1.25	76.36	1.92	0.43	0.70
17.11	61.14	60.41	1.26	76.12	1.94	0.42	0.70
17.22	60.40	59.48	1.28	75.94	1.96	0.42	0.70
17.35	58.51	57.44	1.34	77.19	2.04	0.46	0.70
17.45	53.15	52.07	1.57	81.76	2.18	0.68	0.71
17.55	43.40	42.36	2.26	95.58	2.38	0.74	0.74
17.61	33.92	32.93	3.48	114.42	2.57	0.77	0.77
17.64	27.41	26.45	4.70	124.38	2.70	0.79	0.79
17.70	24.84	23.84	5.27	125.58	2.75	0.79	0.79
17.75	23.12	22.09	5.71	126.01	2.79	0.79	0.79
17.80	22.04	20.96	6.07	127.17	2.82	0.79	0.79
17.85	21.57	20.45	6.49	132.79	2.85	0.80	0.80
17.94	24.37	23.10	5.83	134.72	2.80	0.81	0.81
17.99	29.74	28.29	4.75	134.51	2.70	0.81	0.81
18.09	36.42	34.65	3.76	130.35	2.60	0.80	0.80
18.15	38.34	36.42	3.61	131.44	2.58	0.80	0.80
18.23	36.08	34.09	3.99	135.89	2.63	0.81	0.81
18.33	27.03	25.22	5.88	148.20	2.80	0.82	0.82
18.43	18.43	16.85	8.99	151.54	3.01	1.12	1.20
18.52	11.28	9.87	14.46	142.66	3.27	0.79	0.70
18.59	9.25	7.88	15.23	120.07	3.30	0.54	0.56

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.72	8.44	7.05	14.48	102.14	3.27	0.33	0.50
18.81	7.87	6.47	14.17	91.69	3.26	0.29	0.46
18.87	7.73	6.32	14.34	90.62	3.27	0.28	0.45
18.95	7.94	6.48	14.76	95.67	3.28	0.31	0.46
19.05	8.95	7.39	13.77	101.75	3.24	0.40	0.53
19.14	11.32	9.56	10.96	104.74	3.12	0.45	0.68
19.22	15.43	13.37	7.56	101.14	2.92	0.75	0.75
19.29	23.29	20.64	4.44	91.70	2.67	0.73	0.73
19.38	36.79	33.12	2.43	80.52	2.41	0.61	0.71
19.44	54.77	49.78	1.63	81.04	2.21	0.64	0.71
19.53	73.63	67.13	1.37	92.11	2.06	0.73	0.73
19.62	89.35	81.50	1.30	105.61	1.99	0.76	0.76
19.69	100.62	91.73	1.27	116.28	1.95	0.78	0.78
19.79	106.79	97.11	1.26	122.62	1.94	0.79	0.79
19.86	108.17	98.11	1.28	125.15	1.96	0.79	0.79
19.97	105.91	95.65	1.30	124.06	1.99	0.79	0.79
20.07	101.09	90.89	1.33	120.48	2.02	0.78	0.78
20.16	94.14	84.23	1.37	115.28	2.06	0.78	0.78
20.26	84.49	75.23	1.38	103.79	2.07	0.76	0.76
20.34	72.68	64.34	1.43	91.71	2.10	0.73	0.73
20.43	59.83	52.55	1.52	80.02	2.16	0.58	0.71
20.50	47.95	41.63	2.03	84.51	2.33	0.72	0.72
20.60	37.70	32.23	3.01	96.91	2.50	0.74	0.74
20.62	30.48	25.73	4.28	110.02	2.66	0.77	0.77
20.63	28.08	23.58	4.89	115.31	2.72	0.78	0.78
20.68	27.74	23.22	5.10	118.43	2.74	0.78	0.78
20.73	27.64	23.06	5.32	122.67	2.76	0.79	0.79
20.82	25.48	21.06	6.08	128.12	2.82	0.80	0.80
20.87	23.45	19.23	6.78	130.45	2.87	0.80	0.80
20.91	21.57	17.54	7.32	128.42	2.91	0.80	0.80
20.96	19.58	15.59	7.98	124.40	2.95	0.79	0.79
21.05	17.59	13.84	8.82	122.12	3.00	0.63	0.99
21.11	16.98	13.29	9.07	120.49	3.02	0.63	0.95
21.17	17.11	13.36	9.02	120.44	3.01	0.63	0.95
21.25	21.23	17.01	6.86	116.62	2.88	0.78	0.78
21.30	31.25	25.68	4.13	106.03	2.64	0.76	0.76
21.37	48.56	40.77	2.31	94.37	2.39	0.74	0.74
21.45	68.84	58.49	1.62	94.86	2.20	0.74	0.74
21.49	87.80	75.10	1.41	105.59	2.09	0.76	0.76
21.58	103.45	88.68	1.33	117.80	2.02	0.78	0.78
21.64	115.70	99.28	1.29	128.46	1.98	0.80	0.80
21.69	124.50	106.86	1.28	136.49	1.96	0.81	0.81
21.78	130.41	111.69	1.27	142.03	1.95	0.82	0.82
21.83	133.78	114.42	1.27	145.79	1.96	0.82	0.82
21.89	135.43	115.57	1.28	148.03	1.97	0.82	0.82
21.98	136.01	115.67	1.29	149.32	1.98	0.83	0.83
22.03	135.90	115.31	1.30	150.06	1.99	0.83	0.83
22.12	134.89	114.06	1.31	149.60	2.01	0.83	0.83

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.22	133.20	112.20	1.32	148.31	2.02	0.82	0.82
22.26	130.88	110.01	1.33	146.45	2.03	0.82	0.82
22.36	128.38	107.52	1.34	144.21	2.04	0.82	0.82
22.41	125.79	105.07	1.36	142.38	2.05	0.82	0.82
22.51	123.53	102.88	1.35	138.65	2.04	0.81	0.81
22.60	121.33	100.82	1.34	134.71	2.03	0.81	0.81
22.70	119.34	98.95	1.32	130.43	2.01	0.80	0.80
22.75	116.88	96.72	1.32	127.90	2.02	0.80	0.80
22.84	109.32	89.92	1.36	122.31	2.05	0.79	0.79
22.89	107.14	87.93	1.37	120.57	2.06	0.78	0.78
22.90	104.88	85.98	1.38	118.82	2.07	0.78	0.78
22.94	110.11	90.42	1.34	121.26	2.04	0.78	0.78
23.00	112.36	92.21	1.32	122.07	2.02	0.79	0.79
23.08	118.94	97.70	1.29	126.15	1.98	0.79	0.79
23.13	127.04	104.57	1.26	131.91	1.94	0.80	0.80
23.20	134.05	110.43	1.24	136.83	1.90	0.81	0.81
23.27	137.05	112.81	1.23	138.66	1.89	0.81	0.81
23.33	135.57	111.40	1.23	136.90	1.89	0.81	0.81
23.42	131.55	107.76	1.23	132.83	1.89	0.80	0.80
23.48	126.94	103.73	1.24	128.30	1.90	0.80	0.80
23.57	123.16	100.30	1.24	124.68	1.91	0.79	0.79
23.61	121.20	98.52	1.25	122.97	1.92	0.79	0.79
23.66	121.50	98.62	1.25	123.25	1.92	0.79	0.79
23.73	124.04	100.52	1.25	125.44	1.92	0.79	0.79
23.80	127.95	103.59	1.24	128.73	1.91	0.80	0.80
23.85	131.96	106.79	1.24	132.25	1.90	0.80	0.80
23.94	134.80	108.87	1.24	134.50	1.90	0.81	0.81
24.00	135.88	109.59	1.24	135.41	1.90	0.81	0.81
24.09	135.37	108.86	1.24	134.81	1.90	0.81	0.81
24.16	133.34	106.93	1.24	133.09	1.91	0.80	0.80
24.24	130.04	104.25	1.23	128.02	1.89	0.80	0.80
24.33	125.79	100.75	1.21	122.05	1.86	0.79	0.79
24.43	121.10	96.90	1.19	115.53	1.84	0.78	0.78
24.52	114.28	90.85	1.23	111.31	1.88	0.77	0.77
24.58	108.90	86.13	1.25	107.54	1.92	0.76	0.76
24.59	104.52	82.40	1.27	104.41	1.95	0.76	0.76
24.63	104.21	82.05	1.27	104.24	1.95	0.76	0.76
24.68	103.45	81.24	1.28	103.96	1.96	0.76	0.76
24.77	102.47	80.14	1.29	103.52	1.98	0.75	0.75
24.82	100.31	78.15	1.31	102.59	2.01	0.75	0.75
24.92	97.85	75.83	1.34	101.32	2.03	0.75	0.75
25.01	95.22	73.42	1.36	100.09	2.06	0.75	0.75
25.06	92.38	70.94	1.39	98.75	2.08	0.75	0.75
25.16	89.48	68.36	1.42	97.29	2.10	0.74	0.74
25.25	86.51	65.75	1.46	95.92	2.13	0.74	0.74
25.30	83.55	63.24	1.50	94.77	2.15	0.74	0.74
25.41	80.44	60.52	1.55	93.81	2.17	0.74	0.74
25.49	77.27	57.80	1.61	93.24	2.20	0.74	0.74

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.55	73.97	55.02	1.70	93.42	2.23	0.74	0.74
25.64	70.59	52.13	1.81	94.24	2.27	0.74	0.74
25.70	67.02	49.15	1.95	95.94	2.31	0.74	0.74
25.79	63.24	46.00	2.13	97.75	2.35	0.74	0.74
25.89	58.92	42.45	2.35	99.94	2.40	0.75	0.75
25.94	54.26	38.75	2.63	101.97	2.45	0.75	0.75
26.02	49.37	34.89	2.95	102.81	2.50	0.75	0.75
26.12	45.05	31.51	3.23	101.92	2.54	0.75	0.75
26.17	40.83	28.31	3.52	99.58	2.57	0.75	0.75
26.28	37.02	25.37	3.84	97.30	2.61	0.74	0.74
26.36	33.31	22.57	4.17	94.10	2.65	0.74	0.74
26.45	29.43	19.65	4.69	92.22	2.70	0.73	0.73
26.50	24.94	16.31	5.63	91.86	2.78	0.73	0.73
26.61	20.15	12.75	7.37	93.95	2.91	0.74	0.74
26.70	15.97	9.43	10.10	95.23	3.07	0.35	0.67
26.77	12.97	7.45	12.95	96.46	3.21	0.35	0.53
26.85	11.85	6.70	14.12	94.58	3.26	0.34	0.48
26.94	11.45	6.41	14.29	91.60	3.27	0.29	0.46
27.04	11.95	6.71	13.15	88.25	3.22	0.28	0.48
27.14	12.22	6.86	12.68	86.95	3.20	0.27	0.49
27.23	12.90	7.27	11.66	84.75	3.15	0.26	0.52
27.28	13.22	7.46	11.13	83.02	3.13	0.24	0.53
27.29	13.29	7.50	10.38	77.81	3.09	0.24	0.54
27.38	13.29	7.47	9.96	74.44	3.07	0.16	0.53
27.48	13.27	7.43	9.89	73.48	3.06	0.18	0.53
27.57	13.27	7.41	10.67	79.00	3.10	0.22	0.53
27.64	13.30	7.41	11.31	83.76	3.13	0.26	0.53
27.65	13.44	7.49	12.08	90.43	3.17	0.27	0.53
27.74	14.52	8.14	11.82	96.17	3.16	0.36	0.58
27.80	16.91	9.63	10.69	102.90	3.10	0.41	0.69
27.90	19.17	11.00	9.59	105.58	3.05	0.48	0.79
27.99	19.34	11.07	9.67	106.99	3.05	0.48	0.79
28.07	17.12	9.65	10.91	105.31	3.11	0.45	0.69
28.16	14.45	7.96	12.63	100.58	3.20	0.39	0.57
28.25	12.53	6.75	13.86	93.48	3.25	0.31	0.48
28.34	11.52	6.10	14.13	86.20	3.26	0.25	0.44
28.44	11.01	5.76	14.19	81.77	3.26	0.21	0.41
28.53	10.84	5.64	14.27	80.51	3.26	0.21	0.40
28.62	11.75	6.17	14.04	86.70	3.26	0.23	0.44
28.76	14.21	7.64	12.54	95.81	3.19	0.35	0.55
28.86	17.65	9.69	11.11	107.72	3.12	0.45	0.69
28.96	20.32	11.26	10.51	118.36	3.09	0.58	0.80
29.08	21.30	11.80	11.10	130.98	3.12	0.70	0.84
29.19	22.07	12.21	11.60	141.58	3.15	0.86	0.87
29.29	27.50	15.40	8.64	133.06	2.99	0.80	0.80
29.39	40.70	25.08	5.15	129.21	2.74	0.80	0.80
29.50	57.67	36.81	3.37	124.06	2.55	0.79	0.79
29.63	66.88	42.86	3.19	136.79	2.53	0.81	0.81

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
29.65	70.22	45.09	3.13	141.18	2.52	0.81	0.81
29.66	71.00	45.61	3.10	141.50	2.52	0.82	0.82
29.72	73.53	47.34	2.95	139.57	2.50	0.81	0.81
29.80	77.81	50.31	2.70	135.94	2.46	0.81	0.81
29.85	89.49	58.79	2.17	127.49	2.36	0.79	0.79
29.94	111.58	75.08	1.62	121.89	2.20	0.79	0.79
30.00	135.50	93.20	1.37	127.60	2.06	0.79	0.79
30.05	152.98	106.83	1.28	136.43	1.96	0.81	0.81
30.14	162.60	114.57	1.23	140.95	1.89	0.81	0.81
30.19	167.56	118.78	1.20	142.08	1.84	0.82	0.82
30.24	169.61	120.45	1.18	142.19	1.83	0.82	0.82
30.29	169.68	120.31	1.18	142.38	1.83	0.82	0.82
30.38	167.72	118.51	1.19	141.39	1.84	0.82	0.82
30.43	164.79	116.05	1.20	139.76	1.85	0.81	0.81
30.48	161.62	113.47	1.21	137.67	1.87	0.81	0.81
30.54	159.16	111.46	1.22	135.86	1.87	0.81	0.81
30.62	158.35	110.69	1.22	134.98	1.87	0.81	0.81
30.67	157.77	110.16	1.22	134.34	1.87	0.80	0.80
30.72	158.55	110.67	1.22	134.61	1.87	0.81	0.81
30.76	159.46	111.32	1.21	134.89	1.86	0.81	0.81
30.86	162.06	113.16	1.20	135.92	1.85	0.81	0.81
30.91	165.09	115.46	1.19	137.26	1.84	0.81	0.81
30.95	168.94	118.37	1.17	138.94	1.82	0.81	0.81
31.03	173.83	122.03	1.15	140.71	1.80	0.81	0.81
31.10	179.36	126.19	1.13	142.33	1.78	0.82	0.82
31.15	185.03	130.44	1.10	144.07	1.76	0.82	0.82
31.20	189.66	133.76	1.09	146.05	1.75	0.82	0.82
31.26	192.52	135.69	1.09	147.81	1.75	0.82	0.82
31.34	186.22	130.42	1.13	147.23	1.78	0.82	0.82
31.37	184.63	129.08	1.14	146.99	1.79	0.82	0.82
31.38	181.39	126.56	1.15	145.70	1.80	0.82	0.82
31.43	184.63	129.02	1.13	146.17	1.78	0.82	0.82
31.47	179.33	124.92	1.15	143.44	1.80	0.82	0.82
31.55	171.64	118.91	1.17	139.35	1.82	0.81	0.81
31.59	160.34	110.19	1.21	132.93	1.86	0.80	0.80
31.66	147.76	100.47	1.24	124.83	1.91	0.79	0.79
31.73	135.75	91.20	1.28	116.80	1.97	0.78	0.78
31.78	125.08	83.04	1.33	110.36	2.02	0.77	0.77
31.84	115.64	75.76	1.40	106.34	2.09	0.76	0.76
31.93	107.23	69.27	1.51	104.84	2.16	0.76	0.76
31.98	100.42	64.06	1.66	106.04	2.22	0.76	0.76
32.02	98.18	62.19	1.75	108.88	2.25	0.76	0.76
32.09	97.00	61.07	1.83	111.87	2.27	0.77	0.77
32.16	98.89	62.18	1.83	113.86	2.27	0.77	0.77
32.22	100.29	63.04	1.82	114.52	2.27	0.77	0.77
32.27	103.49	65.22	1.76	114.53	2.25	0.77	0.77
32.34	106.02	66.91	1.71	114.38	2.24	0.77	0.77
32.42	108.89	68.85	1.66	114.11	2.22	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
32.46	113.04	71.82	1.58	113.62	2.19	0.77	0.77
32.54	117.73	75.15	1.51	113.25	2.15	0.77	0.77
32.60	121.74	78.23	1.43	112.00	2.11	0.77	0.77
32.67	124.81	80.60	1.38	111.53	2.07	0.77	0.77
32.75	127.51	82.59	1.35	111.85	2.05	0.77	0.77
32.81	130.38	84.43	1.35	113.95	2.05	0.77	0.77
32.89	133.38	86.29	1.35	116.21	2.04	0.78	0.78
32.94	129.47	83.21	1.38	114.84	2.07	0.77	0.77
32.95	131.02	84.23	1.38	116.07	2.07	0.78	0.78
33.00	132.88	85.36	1.38	117.56	2.07	0.78	0.78
33.06	141.08	91.06	1.34	122.40	2.04	0.79	0.79
33.11	142.26	91.66	1.35	123.66	2.04	0.79	0.79
33.20	141.21	90.60	1.36	123.53	2.06	0.79	0.79
33.25	139.02	88.78	1.39	123.06	2.08	0.79	0.79
33.34	137.03	87.07	1.41	122.48	2.09	0.79	0.79
33.38	136.69	86.68	1.42	122.68	2.10	0.79	0.79
33.48	138.41	87.63	1.41	123.78	2.10	0.79	0.79
33.58	141.92	89.83	1.40	125.79	2.09	0.79	0.79
33.63	146.74	93.05	1.38	128.81	2.07	0.80	0.80
33.73	152.41	96.75	1.37	132.15	2.06	0.80	0.80
33.82	158.96	101.09	1.35	136.16	2.04	0.81	0.81
33.87	165.74	105.66	1.33	140.58	2.03	0.81	0.81
33.96	172.72	110.29	1.32	145.13	2.01	0.82	0.82
34.02	180.58	115.54	1.30	150.66	2.00	0.83	0.83
34.11	190.03	121.77	1.29	157.32	1.98	0.84	0.84
34.18	200.49	128.68	1.28	164.99	1.97	0.85	0.85
34.26	210.44	135.11	1.28	172.52	1.96	0.86	0.86
34.35	219.45	140.77	1.28	179.50	1.96	0.86	0.86
34.44	227.51	145.83	1.27	185.53	1.95	0.87	0.87
34.49	233.96	150.02	1.27	190.23	1.95	0.88	0.88
34.59	237.94	152.42	1.27	192.83	1.94	0.88	0.88
34.69	240.00	153.47	1.26	194.12	1.94	0.88	0.88
34.76	240.94	153.92	1.26	194.53	1.94	0.88	0.88
34.83	240.60	153.43	1.26	194.02	1.94	0.88	0.88
34.93	237.97	151.43	1.26	191.54	1.94	0.88	0.88
35.02	233.82	148.39	1.27	188.08	1.95	0.87	0.87
35.12	229.78	145.60	1.27	184.23	1.94	0.87	0.87
35.22	226.47	143.26	1.26	181.13	1.94	0.87	0.87
35.30	222.22	140.29	1.26	177.46	1.94	0.86	0.86
35.38	208.55	130.48	1.29	168.21	1.98	0.85	0.85
35.43	198.10	123.09	1.31	161.35	2.00	0.84	0.84
35.46	189.40	116.99	1.33	155.80	2.03	0.83	0.83
35.51	187.20	115.53	1.33	153.78	2.03	0.83	0.83
35.56	176.78	108.45	1.35	146.76	2.05	0.82	0.82
35.66	163.52	99.31	1.39	138.53	2.08	0.81	0.81
35.70	148.20	89.01	1.46	130.03	2.13	0.80	0.80
35.80	131.87	77.90	1.59	123.66	2.19	0.79	0.79
35.89	111.32	64.17	1.87	119.95	2.28	0.78	0.78

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
35.96	89.09	49.72	2.43	120.81	2.41	0.78	0.78
36.04	68.24	36.73	3.28	120.37	2.54	0.78	0.78
36.14	52.15	27.04	4.33	117.01	2.66	0.78	0.78
36.19	43.48	22.01	5.03	110.69	2.73	0.77	0.77
36.28	40.51	20.23	5.44	110.05	2.77	0.77	0.77
36.33	40.51	20.24	5.35	108.32	2.76	0.76	0.76
36.42	42.30	21.24	5.09	108.08	2.74	0.76	0.76
36.48	45.97	23.38	4.59	107.27	2.69	0.76	0.76
36.52	51.03	26.20	4.31	112.95	2.66	0.77	0.77
36.62	54.10	27.78	4.31	119.67	2.66	0.78	0.78
36.68	54.07	27.55	4.59	126.59	2.69	0.79	0.79
36.77	52.82	26.73	4.79	128.11	2.71	0.80	0.80
36.86	54.64	27.76	4.56	126.60	2.69	0.79	0.79
36.90	67.67	35.75	3.22	115.19	2.53	0.77	0.77
37.00	98.14	55.13	1.87	103.13	2.29	0.75	0.75
37.10	140.34	83.45	1.35	112.56	2.04	0.77	0.77
37.20	182.54	113.15	1.21	136.84	1.86	0.81	0.81
37.29	213.04	135.23	1.09	147.30	1.75	0.82	0.82
37.39	232.34	149.01	1.00	149.01	1.70	0.83	0.83
37.49	241.91	155.00	1.00	155.00	1.70	0.83	0.83
37.53	245.57	156.74	1.02	160.20	1.72	0.84	0.84
37.58	246.07	156.33	1.06	165.44	1.73	0.85	0.85
37.62	247.84	156.88	1.08	169.66	1.75	0.85	0.85
37.69	250.56	157.82	1.11	175.10	1.77	0.86	0.86
37.77	253.53	158.95	1.13	179.78	1.78	0.86	0.86
37.82	254.98	159.10	1.15	183.39	1.80	0.87	0.87
37.87	254.84	158.42	1.17	184.85	1.81	0.87	0.87
37.91	252.72	156.44	1.18	184.82	1.83	0.87	0.87
37.97	248.23	152.87	1.20	183.06	1.85	0.87	0.87
38.06	241.92	148.07	1.21	179.59	1.87	0.86	0.86
38.10	235.58	143.53	1.22	175.74	1.88	0.86	0.86
38.17	230.89	140.30	1.23	172.34	1.89	0.86	0.86
38.25	228.09	138.57	1.22	169.66	1.88	0.85	0.85
38.35	225.79	137.24	1.22	167.11	1.87	0.85	0.85
38.40	223.43	135.86	1.21	164.83	1.87	0.85	0.85
38.46	221.65	134.68	1.21	163.21	1.86	0.84	0.84
38.54	220.87	134.09	1.21	162.26	1.86	0.84	0.84
38.60	220.87	134.14	1.21	161.69	1.86	0.84	0.84
38.69	222.22	135.09	1.20	161.77	1.85	0.84	0.84
38.74	224.92	137.05	1.19	162.53	1.83	0.84	0.84
38.83	227.85	138.91	1.18	163.73	1.82	0.84	0.84
38.88	229.20	139.97	1.17	163.54	1.81	0.84	0.84
38.97	228.76	139.65	1.16	162.47	1.81	0.84	0.84
39.02	227.25	138.83	1.16	160.45	1.80	0.84	0.84
39.11	224.44	136.82	1.16	158.54	1.81	0.84	0.84
39.16	218.51	132.80	1.17	154.99	1.81	0.83	0.83
39.23	205.48	123.73	1.20	148.10	1.85	0.82	0.82
39.24	200.81	120.69	1.20	145.08	1.85	0.82	0.82

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
39.28	198.62	119.29	1.20	143.39	1.85	0.82	0.82
39.32	201.93	121.86	1.18	144.08	1.83	0.82	0.82
39.39	194.55	116.84	1.20	139.67	1.84	0.81	0.81
39.47	183.96	109.44	1.22	133.48	1.88	0.80	0.80
39.54	171.48	100.68	1.25	125.99	1.92	0.79	0.79
39.62	158.42	91.63	1.29	117.99	1.98	0.78	0.78
39.71	145.73	82.95	1.33	110.70	2.03	0.77	0.77
39.76	134.50	75.46	1.39	105.08	2.08	0.76	0.76
39.85	125.32	69.36	1.46	101.34	2.13	0.75	0.75
39.90	117.87	64.48	1.53	98.95	2.17	0.75	0.75
40.00	111.05	60.00	1.63	97.53	2.20	0.74	0.74
40.06	104.71	55.91	1.73	96.96	2.24	0.74	0.74
40.15	98.67	52.00	1.87	97.18	2.28	0.74	0.74
40.21	92.83	48.24	2.05	98.86	2.33	0.75	0.75
40.29	86.59	44.24	2.31	102.19	2.39	0.75	0.75
40.35	79.68	39.85	2.72	108.27	2.46	0.76	0.76
40.43	72.22	35.37	3.16	111.81	2.53	0.77	0.77
40.52	63.85	30.51	3.76	114.58	2.60	0.77	0.77
40.58	55.21	25.70	4.47	115.00	2.68	0.77	0.77
40.67	46.88	21.09	5.54	116.83	2.77	0.78	0.78
40.77	41.63	18.24	6.45	117.65	2.85	0.78	0.78
40.84	39.14	16.87	6.99	117.99	2.89	0.78	0.78
40.89	42.28	18.55	6.27	116.25	2.83	0.78	0.78
40.94	49.75	22.62	4.92	111.31	2.72	0.77	0.77
41.03	61.46	29.20	3.53	103.18	2.57	0.75	0.75
41.08	73.03	35.94	2.68	96.47	2.45	0.74	0.74
41.14	82.03	41.30	2.24	92.51	2.37	0.73	0.73
41.22	87.70	44.68	2.04	90.97	2.33	0.73	0.73
41.28	90.43	46.24	1.97	91.29	2.31	0.73	0.73
41.33	91.99	46.96	1.99	93.52	2.32	0.74	0.74
41.42	93.64	47.61	2.04	97.02	2.33	0.74	0.74
41.47	97.01	49.31	2.04	100.81	2.33	0.75	0.75
41.52	104.03	53.17	1.96	104.48	2.31	0.76	0.76
41.62	115.47	59.72	1.81	107.92	2.27	0.76	0.76
41.67	130.01	68.21	1.66	112.91	2.22	0.77	0.77
41.76	144.45	76.74	1.54	118.23	2.17	0.78	0.78
41.82	156.39	83.80	1.48	123.75	2.14	0.79	0.79
41.90	165.43	89.14	1.44	128.02	2.11	0.80	0.80
41.99	171.57	92.73	1.41	131.05	2.10	0.80	0.80
42.05	174.81	94.61	1.40	132.58	2.09	0.80	0.80
42.15	175.22	94.64	1.40	132.77	2.09	0.80	0.80
42.23	173.33	93.24	1.42	132.06	2.10	0.80	0.80
42.30	169.55	90.73	1.44	130.51	2.11	0.80	0.80
42.38	163.64	86.97	1.47	127.88	2.13	0.80	0.80
42.48	153.79	80.87	1.53	123.60	2.16	0.79	0.79
42.57	141.98	73.69	1.62	119.15	2.20	0.78	0.78
42.64	129.97	66.53	1.73	115.28	2.24	0.78	0.78
42.72	121.20	61.42	1.82	111.72	2.27	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
42.82	114.72	57.72	1.88	108.24	2.29	0.76	0.76
42.90	110.03	55.08	1.91	105.42	2.30	0.76	0.76
42.97	106.05	52.74	1.98	104.32	2.31	0.76	0.76
43.06	102.31	50.43	2.08	104.69	2.34	0.76	0.76
43.15	98.76	48.44	2.11	102.43	2.35	0.75	0.75
43.20	97.75	48.00	2.07	99.54	2.34	0.75	0.75
43.30	104.19	51.99	1.84	95.67	2.28	0.74	0.74
43.40	119.88	61.38	1.58	97.12	2.19	0.74	0.74
43.48	132.43	68.91	1.47	100.97	2.13	0.75	0.75
43.51	139.11	72.90	1.43	103.89	2.10	0.76	0.76
43.52	146.23	77.22	1.39	107.23	2.08	0.76	0.76
43.56	160.13	85.83	1.33	114.20	2.03	0.77	0.77
43.61	178.86	97.60	1.28	124.81	1.96	0.79	0.79
43.67	193.23	106.74	1.25	133.29	1.92	0.80	0.80
43.72	206.01	115.04	1.22	140.56	1.88	0.81	0.81
43.80	216.51	121.88	1.20	145.95	1.85	0.82	0.82
43.85	224.74	127.26	1.18	149.84	1.82	0.83	0.83
43.90	231.25	131.51	1.16	152.56	1.81	0.83	0.83
43.94	236.38	134.87	1.14	154.37	1.79	0.83	0.83
43.99	239.82	137.13	1.13	155.28	1.78	0.83	0.83
44.08	241.54	138.11	1.13	155.65	1.78	0.83	0.83
44.14	241.51	137.71	1.14	156.49	1.79	0.84	0.84
44.22	240.40	136.41	1.15	157.19	1.80	0.84	0.84
44.28	238.31	134.50	1.17	157.37	1.82	0.84	0.84
44.33	235.67	132.35	1.18	156.78	1.83	0.84	0.84
44.40	232.27	129.52	1.20	155.80	1.85	0.83	0.83
44.48	231.30	128.25	1.22	155.90	1.87	0.83	0.83
44.52	228.57	125.64	1.24	155.24	1.90	0.83	0.83
44.61	230.02	126.41	1.23	155.88	1.89	0.83	0.83
44.72	231.52	127.03	1.23	156.70	1.90	0.84	0.84
44.77	236.14	130.05	1.22	159.04	1.88	0.84	0.84
44.91	237.86	130.46	1.23	160.27	1.89	0.84	0.84
44.95	231.69	126.16	1.24	156.88	1.91	0.84	0.84
45.02	227.41	123.19	1.25	154.33	1.92	0.83	0.83
45.04	198.97	104.88	1.32	138.44	2.01	0.81	0.81
45.06	203.49	107.81	1.30	140.63	2.00	0.81	0.81
45.11	208.45	111.04	1.29	143.03	1.98	0.82	0.82
45.15	239.96	131.64	1.22	160.49	1.87	0.84	0.84
45.21	246.91	136.23	1.20	163.81	1.85	0.84	0.84
45.25	252.44	139.80	1.19	166.43	1.84	0.85	0.85
45.30	256.29	142.11	1.18	168.34	1.83	0.85	0.85
45.35	258.04	143.02	1.18	169.35	1.83	0.85	0.85
45.41	258.42	143.02	1.19	169.64	1.83	0.85	0.85
45.49	257.00	141.89	1.19	168.87	1.84	0.85	0.85
45.55	254.13	139.97	1.19	167.24	1.84	0.85	0.85
45.63	249.51	136.90	1.20	164.52	1.85	0.85	0.85
45.69	243.67	133.19	1.21	161.09	1.86	0.84	0.84
45.78	236.62	128.61	1.22	156.88	1.88	0.84	0.84

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
45.84	228.05	123.25	1.23	151.68	1.89	0.83	0.83
45.93	217.69	116.85	1.24	145.18	1.91	0.82	0.82
46.02	205.11	109.16	1.26	137.24	1.93	0.81	0.81
46.08	190.40	100.37	1.28	128.00	1.96	0.80	0.80
46.16	174.41	90.73	1.30	118.20	1.99	0.78	0.78
46.24	157.13	80.39	1.35	108.31	2.04	0.76	0.76
46.31	138.07	68.91	1.44	99.54	2.12	0.75	0.75
46.41	117.36	56.54	1.67	94.32	2.22	0.74	0.74
46.48	95.77	44.06	2.17	95.41	2.36	0.74	0.74
46.56	75.72	32.98	3.08	101.49	2.51	0.75	0.75
46.65	58.08	23.81	4.47	106.39	2.68	0.76	0.76
46.75	45.43	17.64	5.95	104.92	2.81	0.76	0.76
46.84	36.62	12.08	8.01	96.75	2.95	0.74	0.74
46.94	30.75	9.96	9.25	92.20	3.03	0.42	0.71
47.02	25.79	8.18	10.96	89.65	3.12	0.36	0.58
47.08	21.37	6.60	13.29	87.68	3.22	0.33	0.47
47.12	18.76	5.66	15.23	86.24	3.30	0.32	0.40
47.16	17.85	5.33	15.88	84.67	3.33	0.30	0.38
47.21	17.81	5.32	15.49	82.35	3.31	0.28	0.38
47.27	17.46	5.18	15.33	79.44	3.31	0.26	0.37
47.35	16.42	4.80	15.97	76.72	3.33	0.23	0.34
47.40	15.74	4.56	15.95	72.71	3.33	0.22	0.33
47.50	15.37	4.42	15.62	68.97	3.32	0.17	0.32
47.55	15.16	4.34	15.04	65.28	3.29	0.16	0.31
47.61	15.00	4.27	14.89	63.67	3.29	0.14	0.31
47.69	14.73	4.17	15.00	62.57	3.29	0.14	0.30
47.76	14.39	4.05	15.25	61.71	3.30	0.13	0.29
47.83	14.02	3.91	15.40	60.22	3.31	0.13	0.28
47.93	13.85	3.84	15.20	58.40	3.30	0.11	0.27
48.02	13.82	3.82	15.00	57.34	3.29	0.10	0.27
48.09	13.88	3.84	14.67	56.35	3.28	0.11	0.27
48.18	13.85	3.82	14.94	57.05	3.29	0.10	0.27
48.27	13.88	3.82	15.29	58.44	3.30	0.12	0.27
48.37	13.98	3.85	15.87	61.09	3.33	0.13	0.27
48.46	14.12	3.89	16.20	62.98	3.34	0.14	0.28
48.52	14.18	3.90	16.46	64.25	3.35	0.15	0.28
48.60	14.25	3.92	16.64	65.23	3.35	0.16	0.28
48.70	14.38	3.96	16.68	65.99	3.35	0.16	0.28
48.79	14.65	4.04	16.50	66.70	3.35	0.16	0.29
48.85	15.06	4.18	16.39	68.42	3.34	0.17	0.30
48.94	15.74	4.40	16.24	71.44	3.34	0.20	0.31
49.04	16.68	4.71	15.57	73.34	3.31	0.23	0.34
49.13	18.30	5.25	15.62	82.09	3.32	0.22	0.38
49.23	21.13	6.21	14.82	92.00	3.29	0.41	0.44
49.33	24.04	7.18	14.31	102.80	3.27	0.51	0.51
49.38	24.88	7.46	14.69	109.60	3.28	0.57	0.53
49.42	25.93	7.81	14.70	114.80	3.28	0.64	0.56
49.48	26.70	8.06	14.75	118.93	3.28	0.70	0.58

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
49.53	28.79	8.76	13.86	121.43	3.25	0.73	0.63
49.58	29.43	8.97	13.78	123.62	3.24	0.76	0.64
49.63	30.10	9.19	13.66	125.52	3.24	0.79	0.66
49.72	30.91	9.44	13.37	126.23	3.23	0.81	0.67
49.77	31.42	9.60	13.13	125.98	3.22	0.80	0.69
49.83	31.42	9.59	13.08	125.40	3.22	0.79	0.68
49.92	30.71	9.33	13.37	124.67	3.23	0.79	0.67
49.97	30.39	9.21	13.41	123.55	3.23	0.76	0.66
50.04	29.48	8.89	13.80	122.65	3.25	0.74	0.64
50.11	29.82	8.99	13.61	122.33	3.24	0.74	0.64
50.20	30.21	9.10	13.25	120.55	3.22	0.76	0.65
50.27	30.78	9.28	12.51	116.01	3.19	0.68	0.66
50.34	29.50	8.83	12.20	107.79	3.18	0.58	0.63
50.45	26.76	7.90	12.55	99.22	3.19	0.45	0.56
50.54	23.73	6.88	13.43	92.39	3.23	0.38	0.49
50.59	21.13	6.01	14.59	87.71	3.28	0.35	0.43
50.68	19.24	5.37	15.59	83.78	3.32	0.30	0.38
50.79	18.13	4.99	16.06	80.17	3.33	0.26	0.36
50.88	17.81	4.88	16.03	78.18	3.33	0.25	0.35
50.98	17.64	4.81	16.19	77.89	3.34	0.25	0.34
51.07	17.81	4.86	15.67	76.09	3.32	0.25	0.35
51.17	18.43	5.05	14.19	71.67	3.26	0.21	0.36
51.24	19.51	5.40	12.74	68.77	3.20	0.16	0.39
51.33	20.19	5.61	12.56	70.43	3.19	0.20	0.40
51.46	20.09	5.56	13.45	74.75	3.23	0.25	0.40
51.46	19.80	5.46	14.31	78.20	3.27	0.25	0.39
51.51	19.77	5.45	14.62	79.60	3.28	0.28	0.39
51.56	19.87	5.47	14.98	82.02	3.29	0.28	0.39
51.65	19.95	5.49	15.35	84.26	3.31	0.31	0.39
51.71	20.09	5.53	15.72	86.89	3.32	0.33	0.39
51.79	20.49	5.65	15.73	88.80	3.32	0.35	0.40
51.85	21.23	5.88	15.68	92.19	3.32	0.37	0.42
51.94	22.11	6.15	15.66	96.33	3.32	0.43	0.44
51.99	23.22	6.51	15.77	102.62	3.32	0.48	0.46
52.09	24.17	6.80	16.12	109.52	3.33	0.57	0.49
52.19	27.74	7.93	14.73	116.81	3.28	0.67	0.57
52.28	33.34	9.72	12.62	122.63	3.20	0.78	0.69
52.35	36.42	10.69	12.02	128.41	3.17	0.87	0.76
52.43	37.06	10.87	12.22	132.82	3.18	0.95	0.78
52.52	35.17	10.25	13.30	136.28	3.22	0.97	0.73
52.62	35.61	10.37	13.11	135.93	3.22	0.98	0.74
52.72	35.98	10.46	12.80	133.92	3.20	0.94	0.75
52.81	34.26	9.89	13.70	135.53	3.24	0.89	0.71
52.91	31.32	8.94	16.37	146.31	3.34	1.03	0.64
53.00	37.23	10.79	14.34	154.70	3.27	1.38	0.77
53.10	62.36	18.71	7.92	148.13	2.95	0.82	0.82
53.20	108.21	33.14	3.92	129.79	2.62	0.80	0.80
53.29	163.78	50.57	2.27	114.61	2.38	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
53.38	213.88	66.21	1.72	114.09	2.24	0.77	0.77
53.46	260.07	80.59	1.49	119.81	2.14	0.78	0.78
53.53	292.05	90.48	1.45	130.93	2.12	0.80	0.80
53.63	323.19	100.02	1.40	139.93	2.09	0.81	0.81
53.73	361.79	111.85	1.31	146.92	2.01	0.82	0.82
53.82	388.35	119.89	1.25	150.03	1.92	0.83	0.83
53.92	387.71	119.45	1.23	146.54	1.89	0.82	0.82
53.94	360.18	110.85	1.25	138.23	1.92	0.81	0.81
53.96	336.26	103.38	1.27	131.20	1.95	0.80	0.80
53.97	349.08	107.34	1.25	134.16	1.92	0.80	0.80
54.05	377.59	116.04	1.22	141.00	1.87	0.81	0.81
54.08	426.28	131.09	1.15	150.15	1.79	0.83	0.83
54.13	473.21	145.55	1.06	154.41	1.74	0.83	0.83
54.19	518.79	159.56	1.00	159.56	1.70	0.84	0.84
54.25	524.22	161.12	1.01	162.94	1.71	0.84	0.84
54.28	510.87	156.95	1.06	166.66	1.74	0.85	0.85
54.29	486.82	149.48	1.10	164.40	1.76	0.85	0.85
54.34	486.89	149.42	1.10	164.35	1.76	0.85	0.85
54.35	492.20	151.05	1.09	164.72	1.75	0.85	0.85
54.40	504.89	154.89	1.07	165.62	1.74	0.85	0.85
54.44	522.30	160.18	1.04	166.45	1.72	0.85	0.85
54.49	535.62	164.19	1.01	165.88	1.71	0.85	0.85
54.53	546.25	167.39	1.00	167.39	1.70	0.85	0.85
54.57	558.27	171.02	1.00	171.02	1.69	0.85	0.85
54.58	567.78	173.92	1.00	173.92	1.70	0.86	0.86
54.63	560.90	171.71	1.01	173.90	1.71	0.86	0.86
54.68	536.31	164.04	1.08	176.93	1.75	0.86	0.86
54.73	510.50	156.00	1.12	175.12	1.78	0.86	0.86
54.78	499.67	152.59	1.14	173.29	1.79	0.86	0.86
54.83	493.63	150.64	1.15	172.82	1.80	0.86	0.86
54.88	497.14	151.64	1.15	175.08	1.80	0.86	0.86
54.92	500.68	152.65	1.17	178.37	1.81	0.86	0.86
54.97	510.81	155.66	1.16	180.73	1.81	0.87	0.87
55.02	513.44	156.38	1.16	181.62	1.81	0.87	0.87
55.12	487.90	148.39	1.20	178.01	1.85	0.86	0.86
55.17	449.17	136.44	1.25	170.63	1.92	0.85	0.85
55.25	410.54	124.51	1.29	160.49	1.98	0.84	0.84
55.31	394.21	119.43	1.29	154.46	1.98	0.83	0.83
55.36	388.18	117.52	1.27	148.87	1.95	0.83	0.83
55.45	381.09	115.23	1.25	143.68	1.91	0.82	0.82
55.50	365.91	110.54	1.25	137.89	1.92	0.81	0.81
55.60	351.24	105.95	1.26	133.93	1.94	0.80	0.80
55.65	332.24	100.11	1.28	128.15	1.96	0.80	0.80
55.71	324.14	97.58	1.27	124.39	1.96	0.79	0.79
55.75	320.40	96.40	1.26	121.19	1.93	0.78	0.78
55.79	325.12	97.79	1.25	121.90	1.91	0.79	0.79
55.84	332.47	99.97	1.24	123.76	1.90	0.79	0.79
55.89	338.01	101.60	1.23	125.39	1.90	0.79	0.79

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
55.90	341.15	102.54	1.23	126.17	1.89	0.79	0.79
55.94	336.26	101.02	1.24	124.98	1.90	0.79	0.79
55.99	327.63	98.34	1.25	122.89	1.92	0.79	0.79
56.03	317.88	95.34	1.26	120.41	1.94	0.78	0.78
56.08	311.67	93.40	1.27	118.54	1.95	0.78	0.78
56.14	306.37	91.74	1.27	116.74	1.95	0.78	0.78
56.22	299.89	89.70	1.28	114.65	1.96	0.77	0.77
56.28	294.29	87.95	1.28	112.90	1.97	0.77	0.77
56.33	292.57	87.39	1.29	112.38	1.97	0.77	0.77
56.38	294.06	87.79	1.28	112.46	1.97	0.77	0.77
56.45	301.34	89.92	1.27	114.23	1.95	0.77	0.77
56.52	312.58	93.24	1.25	117.01	1.93	0.78	0.78
56.62	325.19	96.94	1.24	120.21	1.90	0.78	0.78
56.66	338.42	100.88	1.22	123.02	1.87	0.79	0.79
56.73	350.06	104.30	1.21	126.65	1.87	0.79	0.79
56.81	357.11	106.33	1.22	129.59	1.87	0.80	0.80
56.95	363.42	108.06	1.23	132.64	1.89	0.80	0.80
57.00	372.46	110.72	1.23	135.80	1.88	0.81	0.81
57.09	373.11	110.80	1.23	136.52	1.89	0.81	0.81
57.19	368.58	109.32	1.24	135.85	1.91	0.81	0.81
57.27	354.04	104.88	1.25	131.44	1.92	0.80	0.80
57.35	357.65	105.87	1.23	130.16	1.89	0.80	0.80
57.44	356.17	105.33	1.21	127.36	1.86	0.79	0.79
57.50	364.37	107.70	1.18	127.07	1.83	0.79	0.79
57.52	378.10	111.77	1.18	131.85	1.83	0.80	0.80
57.58	409.37	121.03	1.17	141.73	1.82	0.82	0.82
57.63	432.08	127.73	1.17	149.17	1.81	0.83	0.83
57.72	439.00	129.66	1.17	151.31	1.81	0.83	0.83
57.77	433.73	128.03	1.16	148.26	1.80	0.82	0.82
57.82	429.55	126.71	1.13	143.29	1.78	0.82	0.82
57.91	436.73	128.72	1.06	137.09	1.74	0.81	0.81
57.96	442.84	130.46	1.00	130.46	1.69	0.80	0.80
58.02	458.90	135.16	1.00	135.16	1.66	0.81	0.81
58.09	469.26	138.12	1.00	138.12	1.65	0.81	0.81
58.16	484.88	142.65	1.00	142.65	1.63	0.82	0.82
58.25	491.12	144.36	1.00	144.36	1.64	0.82	0.82
58.30	487.65	143.26	1.00	143.26	1.66	0.82	0.82
58.40	479.62	140.74	1.00	140.74	1.69	0.81	0.81
58.50	468.52	137.31	1.02	139.77	1.71	0.81	0.81
58.56	467.50	136.92	1.01	138.70	1.71	0.81	0.81
58.64	464.81	136.01	1.03	140.28	1.72	0.81	0.81
58.73	474.79	138.81	1.05	145.16	1.73	0.82	0.82
58.78	488.15	142.67	1.02	145.87	1.72	0.82	0.82
58.88	506.71	147.98	1.00	147.98	1.69	0.82	0.82
58.97	511.03	149.10	1.00	149.10	1.66	0.83	0.83
59.07	506.24	147.53	1.00	147.53	1.66	0.82	0.82
59.13	493.59	143.73	1.00	143.73	1.65	0.82	0.82
59.23	484.71	140.99	1.00	140.99	1.65	0.81	0.81

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
59.31	464.47	134.94	1.00	134.94	1.65	0.81	0.81
59.38	450.35	130.71	1.00	130.71	1.65	0.80	0.80
59.41	439.19	127.40	1.00	127.40	1.66	0.79	0.79
59.46	443.57	128.62	1.00	128.62	1.65	0.80	0.80
59.51	443.56	128.55	1.00	128.55	1.65	0.80	0.80
59.57	451.89	130.91	1.00	130.91	1.67	0.80	0.80
59.66	471.05	136.37	1.00	136.37	1.67	0.81	0.81
59.75	492.31	142.44	1.00	142.44	1.70	0.82	0.82
59.80	506.48	146.48	1.01	147.84	1.71	0.82	0.82
59.85	508.64	147.04	1.07	156.99	1.74	0.84	0.84
59.91	504.22	145.65	1.08	158.02	1.75	0.84	0.84
59.99	498.85	143.96	1.11	159.53	1.77	0.84	0.84
60.05	480.97	138.68	1.17	161.59	1.81	0.84	0.84
60.09	464.78	133.92	1.20	160.52	1.85	0.84	0.84
60.14	444.43	127.94	1.22	156.08	1.88	0.84	0.84
60.19	437.86	125.96	1.22	153.23	1.87	0.83	0.83
60.22	434.25	124.88	1.21	151.55	1.87	0.83	0.83
60.28	412.99	118.63	1.23	145.94	1.89	0.82	0.82
60.33	381.24	109.36	1.26	137.48	1.93	0.81	0.81
60.38	338.97	97.07	1.31	126.83	2.00	0.79	0.79
60.42	309.75	88.57	1.35	119.65	2.05	0.78	0.78
60.48	282.02	80.50	1.38	111.02	2.07	0.77	0.77
60.57	262.48	74.78	1.36	101.50	2.05	0.75	0.75
60.66	243.89	69.35	1.32	91.67	2.02	0.73	0.73
60.68	232.16	65.95	1.30	85.85	1.99	0.72	0.72
60.69	225.51	64.02	1.29	82.84	1.98	0.71	0.71
60.74	217.75	61.75	1.30	80.07	1.99	0.59	0.71
60.79	206.27	58.41	1.30	76.18	2.00	0.42	0.70
60.84	192.16	54.32	1.32	71.82	2.02	0.30	0.69
60.89	182.35	51.47	1.33	68.64	2.03	0.23	0.68
60.98	174.35	49.12	1.36	66.57	2.05	0.19	0.67
61.03	168.07	47.30	1.46	69.19	2.13	0.24	0.68
61.08	164.86	46.35	1.72	79.69	2.24	0.57	0.71
61.18	164.63	46.24	1.95	90.12	2.31	0.73	0.73
61.23	168.20	47.23	2.12	100.04	2.35	0.75	0.75
61.31	194.08	54.62	1.72	94.03	2.24	0.74	0.74
61.42	236.42	66.70	1.41	94.11	2.09	0.74	0.74
61.47	287.17	81.21	1.24	100.64	1.90	0.75	0.75
61.51	331.30	93.81	1.14	107.25	1.79	0.76	0.76
61.54	366.14	103.76	1.05	108.54	1.73	0.76	0.76
61.57	395.83	112.23	1.00	112.23	1.70	0.77	0.77
61.58	418.64	118.74	1.00	118.74	1.67	0.78	0.78
61.61	393.43	111.49	1.00	111.49	1.70	0.77	0.77
61.63	367.65	104.10	1.03	107.07	1.72	0.76	0.76
61.63	257.89	72.70	1.26	91.77	1.94	0.73	0.73
61.66	191.36	53.66	1.48	79.27	2.14	0.55	0.71
61.67	129.55	35.97	2.37	85.35	2.40	0.72	0.72
61.70	152.96	42.66	1.96	83.80	2.31	0.72	0.72

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
61.71	180.90	50.64	1.67	84.55	2.22	0.72	0.72
61.76	206.41	57.90	1.51	87.45	2.15	0.72	0.72
61.80	228.84	64.28	1.42	91.10	2.10	0.73	0.73
61.84	250.40	70.41	1.34	94.04	2.03	0.74	0.74
61.86	279.75	78.77	1.26	98.87	1.93	0.75	0.75
61.93	312.34	88.02	1.18	103.69	1.82	0.75	0.75
61.98	357.76	100.92	1.00	100.92	1.73	0.75	0.75
62.04	405.56	114.48	1.00	114.48	1.68	0.77	0.77
62.09	451.78	127.59	1.00	127.59	1.64	0.79	0.79
62.14	481.91	136.10	1.00	136.10	1.62	0.81	0.81
62.19	499.12	140.93	1.00	140.93	1.60	0.81	0.81
62.24	508.93	143.65	1.00	143.65	1.59	0.82	0.82
62.26	519.32	146.58	1.00	146.58	1.58	0.82	0.82
62.29	519.05	146.46	1.00	146.46	1.58	0.82	0.82
62.38	515.71	145.37	1.00	145.37	1.60	0.82	0.82
62.44	490.28	138.07	1.00	138.07	1.65	0.81	0.81
62.46	469.07	132.02	1.00	132.02	1.69	0.80	0.80
62.47	448.15	126.07	1.00	126.07	1.70	0.79	0.79
62.51	453.68	127.59	1.00	127.59	1.69	0.79	0.79
62.56	463.98	130.45	1.00	130.45	1.69	0.80	0.80
62.60	477.62	134.26	1.00	134.26	1.68	0.80	0.80
62.65	481.73	135.35	1.00	135.35	1.68	0.81	0.81
62.70	482.34	135.46	1.00	135.46	1.66	0.81	0.81
62.75	483.05	135.59	1.00	135.59	1.65	0.81	0.81
62.80	494.83	138.85	1.00	138.85	1.64	0.81	0.81
62.85	525.29	147.40	1.00	147.40	1.60	0.82	0.82
62.89	569.18	159.73	1.00	159.73	1.56	0.84	0.84
62.97	619.66	173.86	1.00	173.86	1.54	0.86	0.86
63.04	667.84	187.32	1.00	187.32	1.52	0.87	0.87
63.09	703.12	197.18	1.00	197.18	1.50	0.88	0.88
63.13	715.51	200.57	1.00	200.57	1.51	0.89	0.89
63.19	716.52	200.74	1.00	200.74	1.54	0.89	0.89
63.23	720.23	201.69	1.00	201.69	1.57	0.89	0.89
63.28	726.78	203.42	1.00	203.42	1.59	0.89	0.89
63.32	729.18	204.02	1.00	204.02	1.57	0.89	0.89
63.38	725.67	202.89	1.00	202.89	1.49	0.89	0.89
63.44	726.68	203.06	1.00	203.06	1.43	0.89	0.89
63.52	715.48	199.75	1.00	199.75	1.43	0.89	0.89
63.57	697.37	194.57	1.00	194.57	1.49	0.88	0.88
63.66	659.58	183.79	1.00	183.79	1.52	0.87	0.87
63.73	534.95	148.76	1.00	148.76	1.63	0.83	0.83
63.76	455.61	126.50	1.03	130.54	1.72	0.80	0.80
63.76	411.85	114.24	1.12	127.66	1.77	0.79	0.79
63.78	471.87	131.02	1.00	131.02	1.70	0.80	0.80
63.81	512.86	142.46	1.00	142.46	1.67	0.82	0.82
63.85	526.43	146.19	1.00	146.19	1.68	0.82	0.82
63.86	522.58	145.10	1.00	145.10	1.70	0.82	0.82
63.91	497.92	138.14	1.07	148.35	1.74	0.82	0.82

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
63.94	483.78	134.14	1.12	150.35	1.77	0.83	0.83
63.95	480.34	133.15	1.14	151.38	1.79	0.83	0.83
64.00	476.26	131.94	1.14	150.67	1.79	0.83	0.83
64.02	473.22	131.08	1.14	149.37	1.79	0.83	0.83
64.05	475.78	131.75	1.12	148.02	1.78	0.82	0.82
64.09	478.18	132.36	1.11	146.64	1.77	0.82	0.82
64.11	480.07	132.86	1.09	144.77	1.75	0.82	0.82
64.15	482.26	133.43	1.07	142.44	1.74	0.82	0.82
64.20	494.31	136.71	1.03	141.24	1.72	0.81	0.81
64.25	512.59	141.74	1.00	141.74	1.70	0.82	0.82
64.29	535.70	148.11	1.00	148.11	1.68	0.82	0.82
64.34	570.38	157.68	1.00	157.68	1.64	0.84	0.84
64.43	605.81	167.40	1.00	167.40	1.60	0.85	0.85
64.48	630.95	174.30	1.00	174.30	1.56	0.86	0.86
64.53	642.69	177.47	1.00	177.47	1.53	0.86	0.86
64.58	655.07	180.82	1.00	180.82	1.52	0.87	0.87
64.63	680.65	187.83	1.00	187.83	1.51	0.87	0.87
64.68	709.63	195.77	1.00	195.77	1.52	0.88	0.88
64.73	718.74	198.20	1.00	198.20	1.53	0.88	0.88
64.77	735.60	202.79	1.00	202.79	1.51	0.89	0.89
64.82	751.19	207.01	1.00	207.01	1.48	0.89	0.89
64.87	732.64	201.76	1.00	201.76	1.49	0.89	0.89
64.89	713.98	196.56	1.00	196.56	1.50	0.88	0.88
64.93	689.59	189.73	1.00	189.73	1.53	0.88	0.88
64.94	715.81	196.96	1.00	196.96	1.51	0.88	0.88
64.98	725.69	199.62	1.00	199.62	1.50	0.89	0.89
64.99	734.03	201.90	1.00	201.90	1.50	0.89	0.89
65.03	732.37	201.35	1.00	201.35	1.50	0.89	0.89
65.08	727.04	199.79	1.00	199.79	1.49	0.89	0.89
65.13	715.51	196.50	1.00	196.50	1.48	0.88	0.88
65.17	703.60	193.13	1.00	193.13	1.46	0.88	0.88
65.22	689.29	189.08	1.00	189.08	1.45	0.87	0.87
65.23	681.55	186.93	1.00	186.93	1.45	0.87	0.87
65.28	679.28	186.22	1.00	186.22	1.46	0.87	0.87
65.32	679.65	186.24	1.00	186.24	1.47	0.87	0.87
65.37	680.17	186.30	1.00	186.30	1.49	0.87	0.87
65.42	684.61	187.42	1.00	187.42	1.50	0.87	0.87
65.47	671.65	183.76	1.00	183.76	1.50	0.87	0.87
65.48	657.21	179.77	1.00	179.77	1.52	0.86	0.86
65.49	638.86	174.70	1.00	174.70	1.52	0.86	0.86
65.52	636.56	174.01	1.00	174.01	1.52	0.86	0.86
65.57	645.67	176.43	1.00	176.43	1.41	0.86	0.86
65.62	661.16	180.61	1.00	180.61	1.28	0.87	0.87
65.67	682.44	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.69	697.23	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.72	719.02	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.77	752.26	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.82	790.78	-1.00	1.00	-1.00	-1.00	0.00	0.00

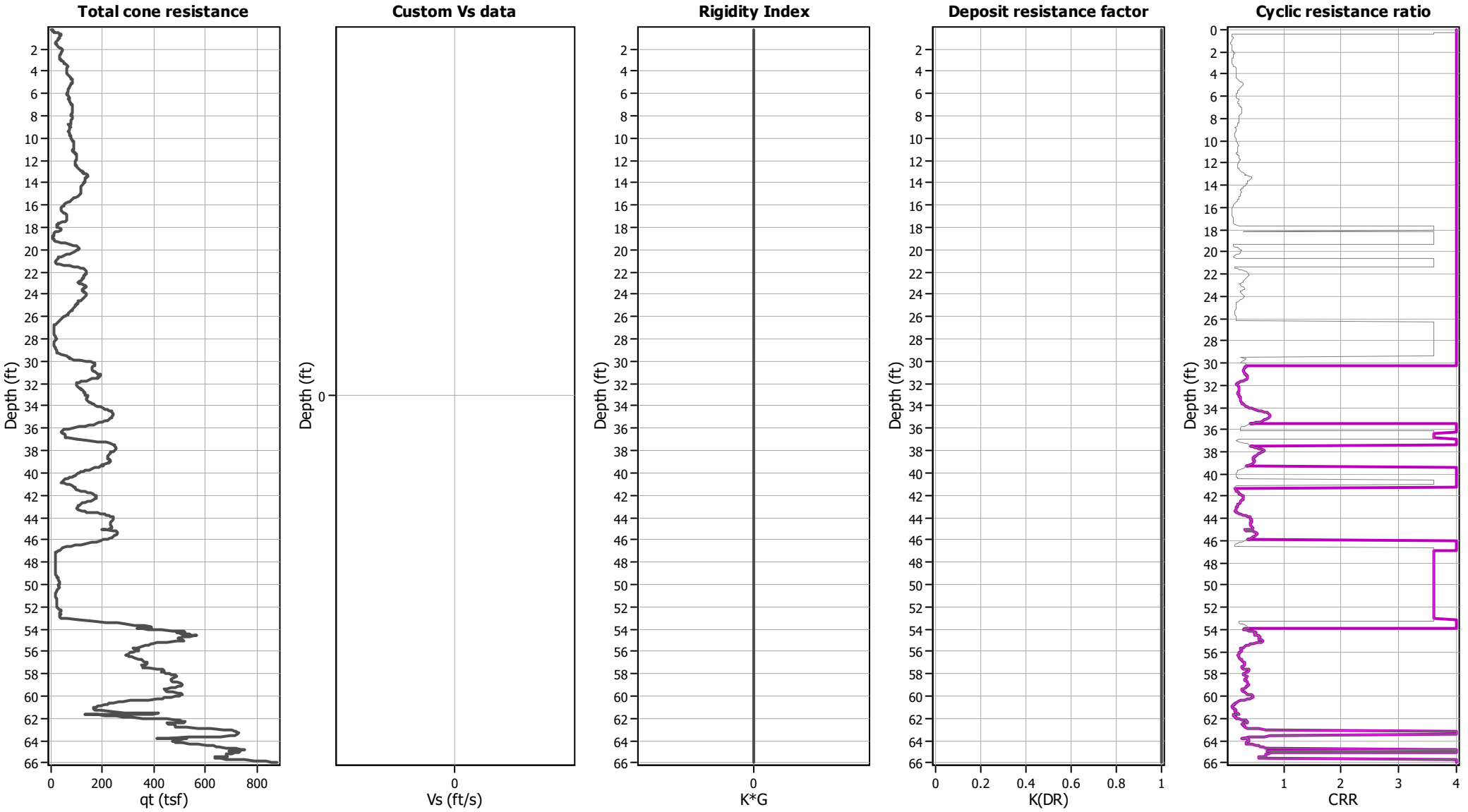
:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
65.86	811.97	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.86	833.63	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.91	854.04	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.96	878.41	-1.00	1.00	-1.00	-1.00	0.00	0.00

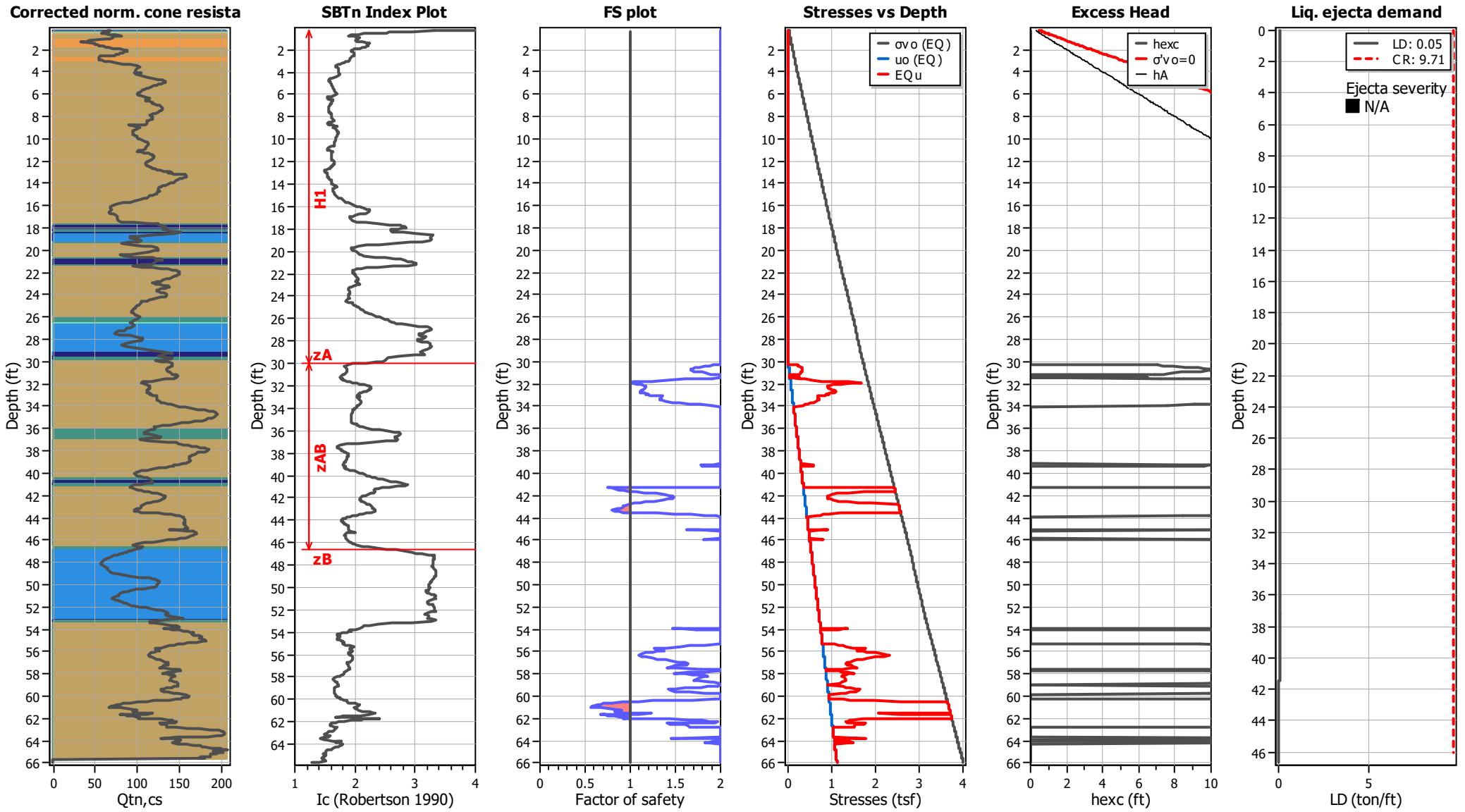
Abbreviations

q_t: Total cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Adjusted and corrected cone resistance due to fines
I_c: Soil behavior type index
$S_{u(liq)}/\sigma'_v$: Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$: Calculated peak undrained strength ratio

Aging Calculation Estimation



Ejecta Severity Estimation



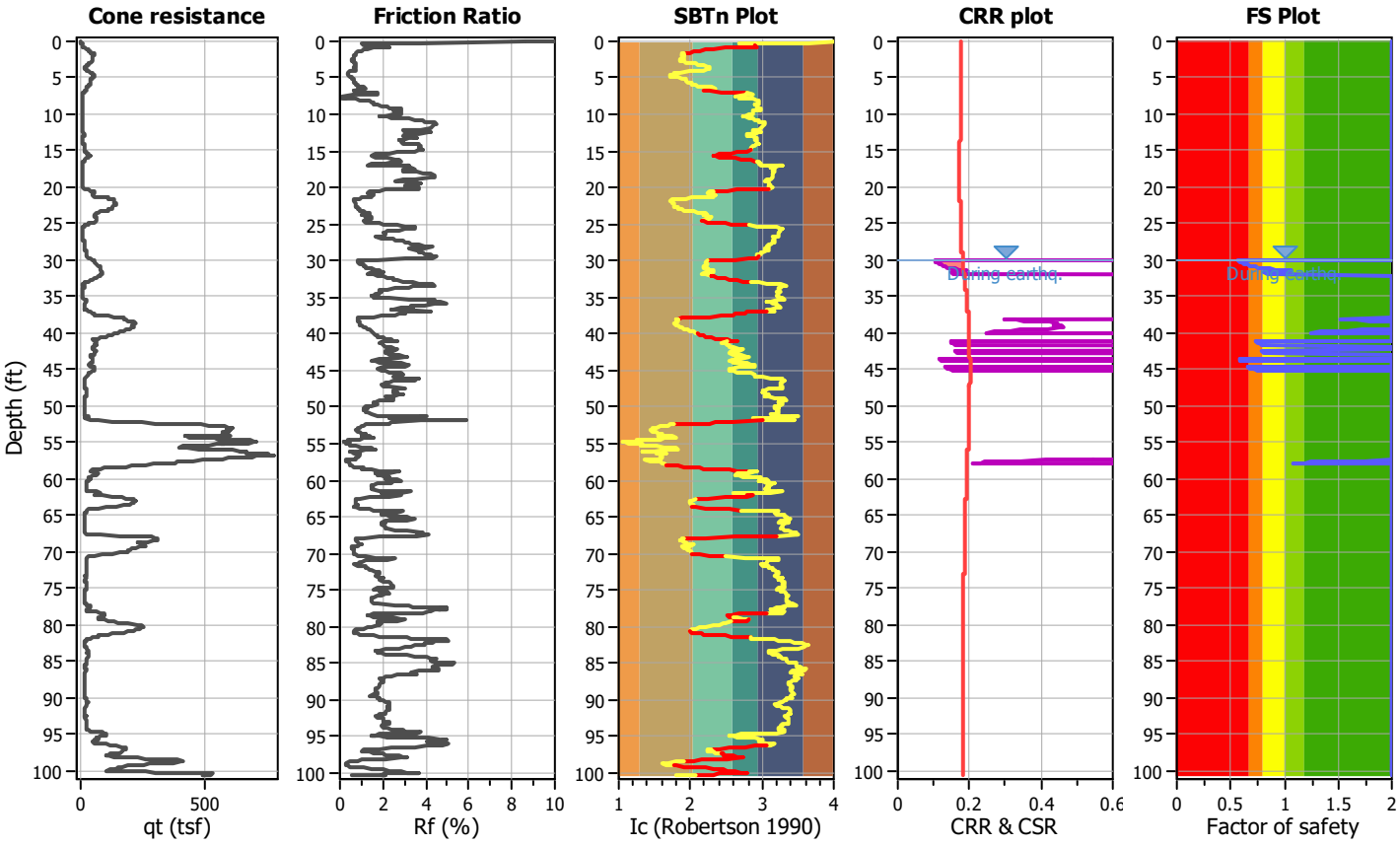
LIQUEFACTION ANALYSIS REPORT

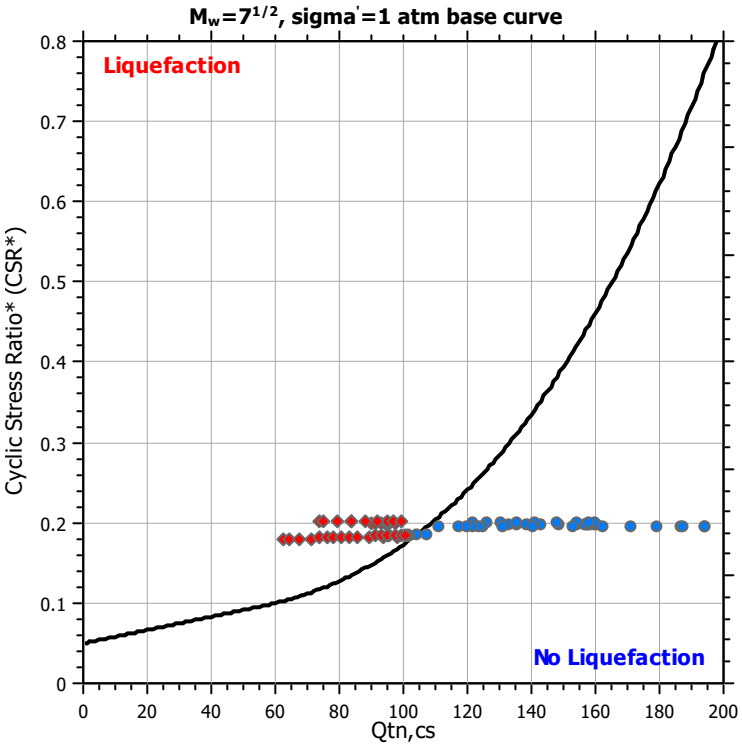
Project title : W1857-88-01 **Location : 331 The City Drive S**

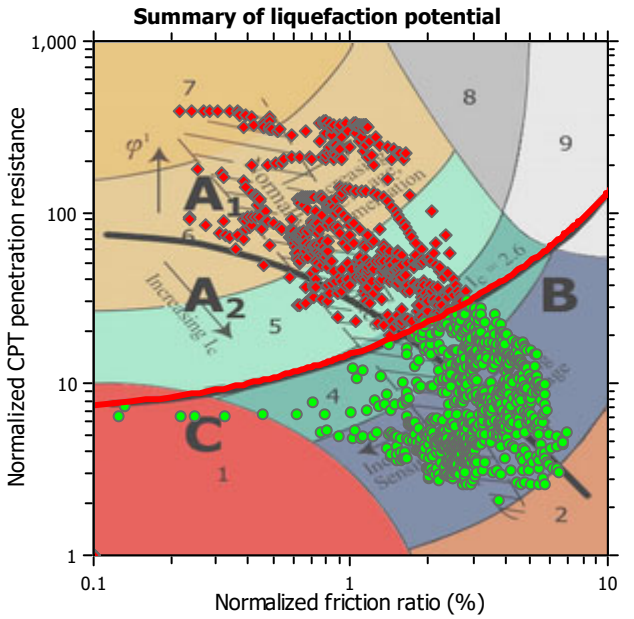
CPT file : CPT-3

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	54.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	30.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	62.00 ft
Earthquake magnitude M_w:	6.12	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.42	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

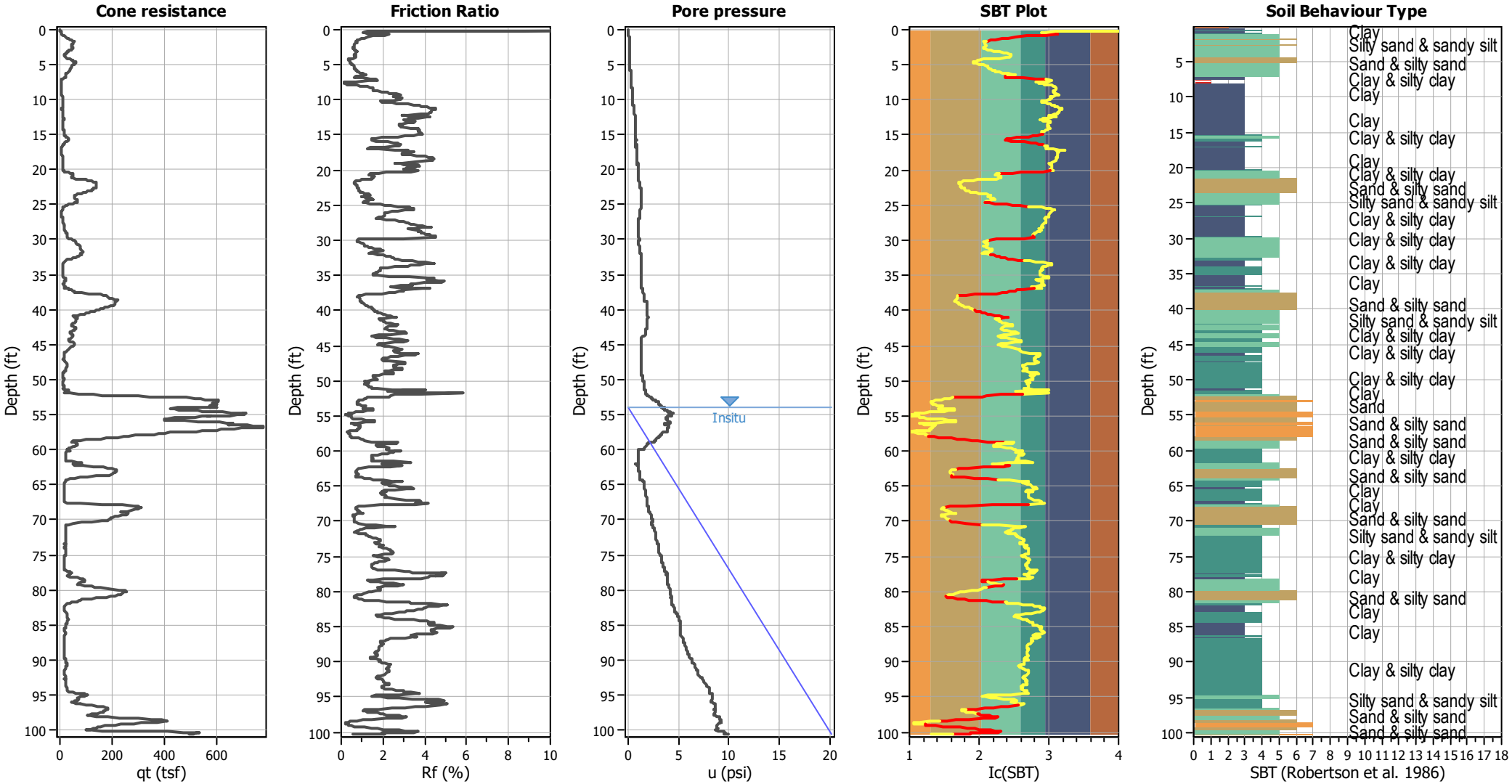






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



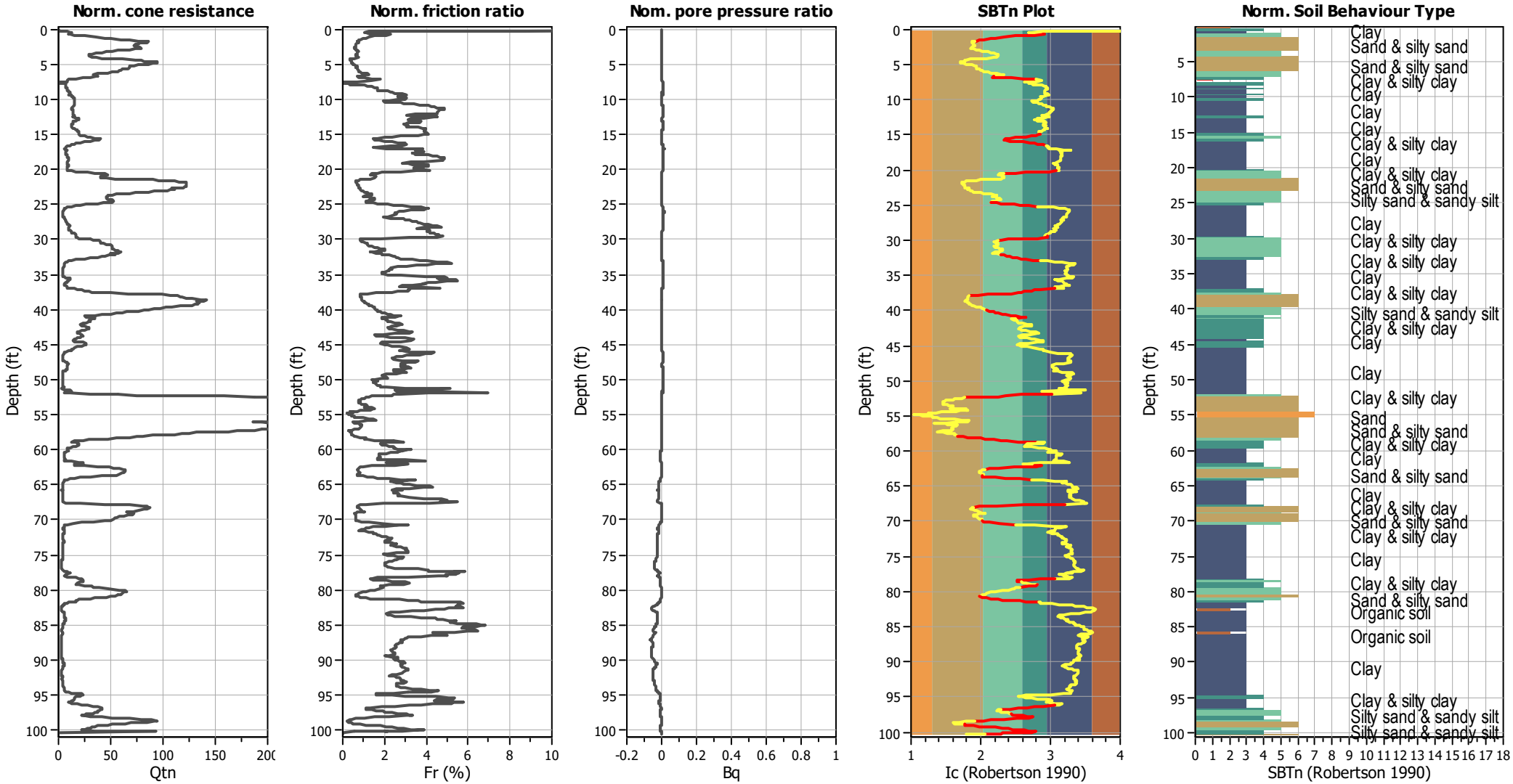
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	62.00 ft

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



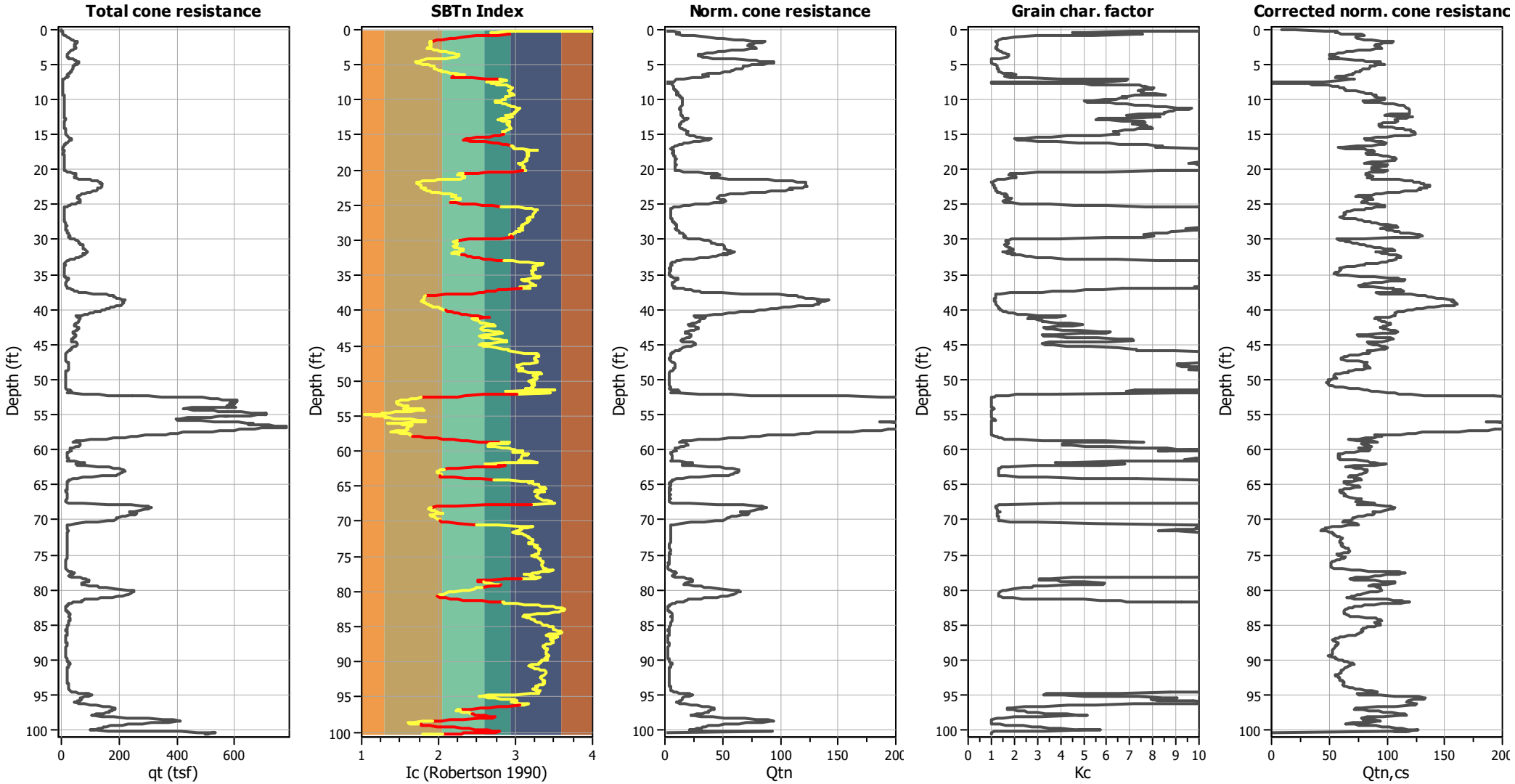
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	62.00 ft

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

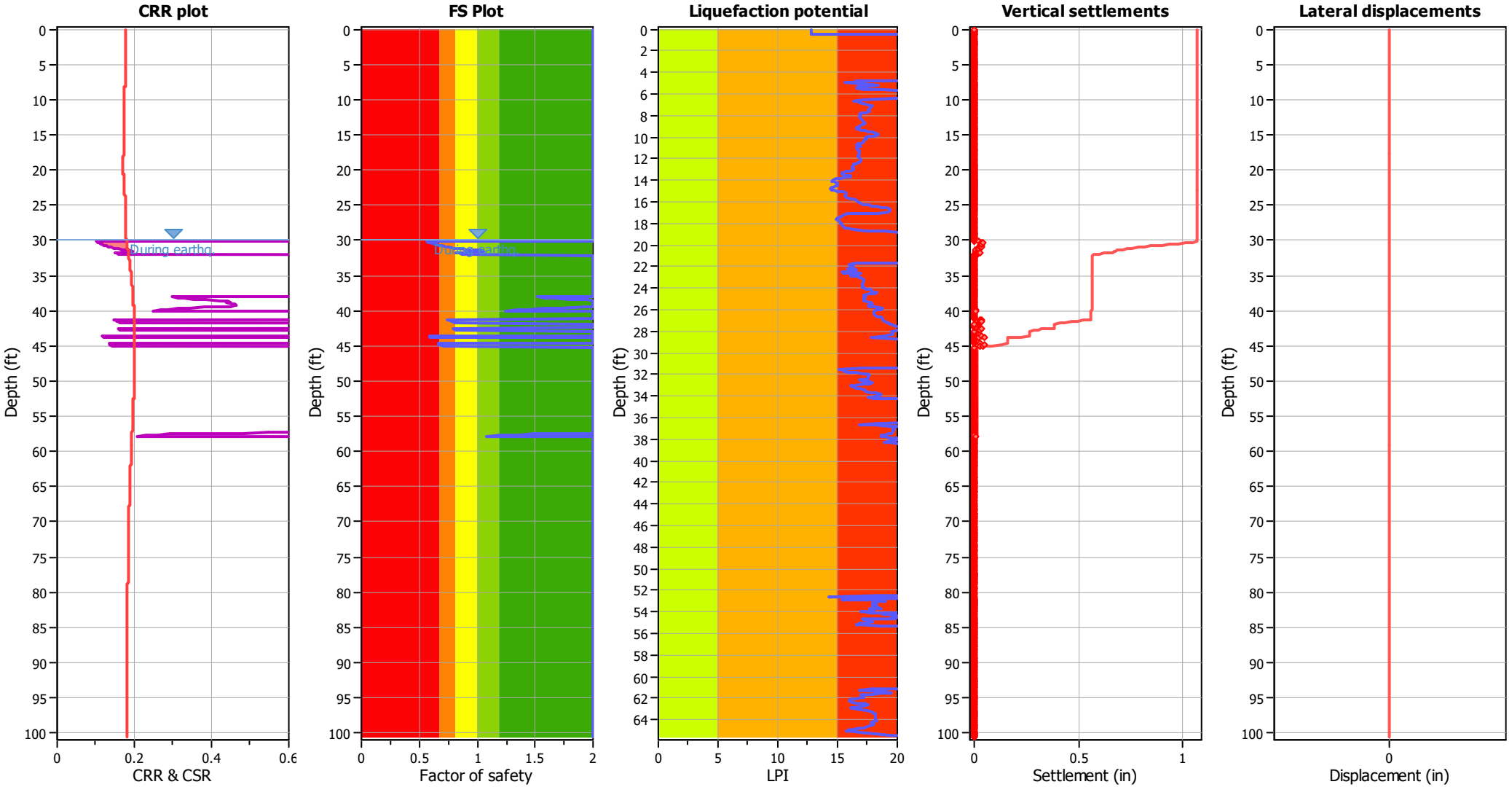
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	62.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	62.00 ft

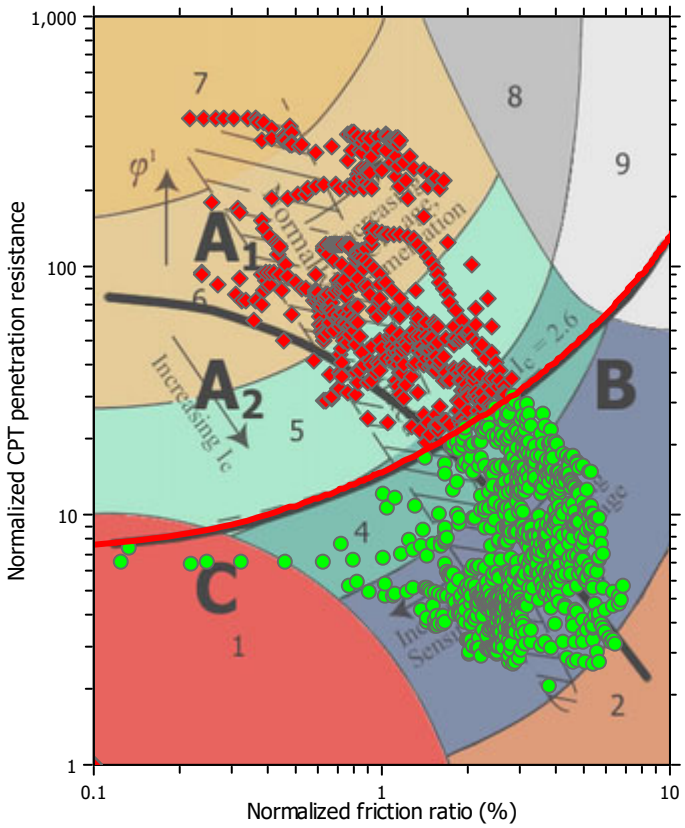
F.S. color scheme

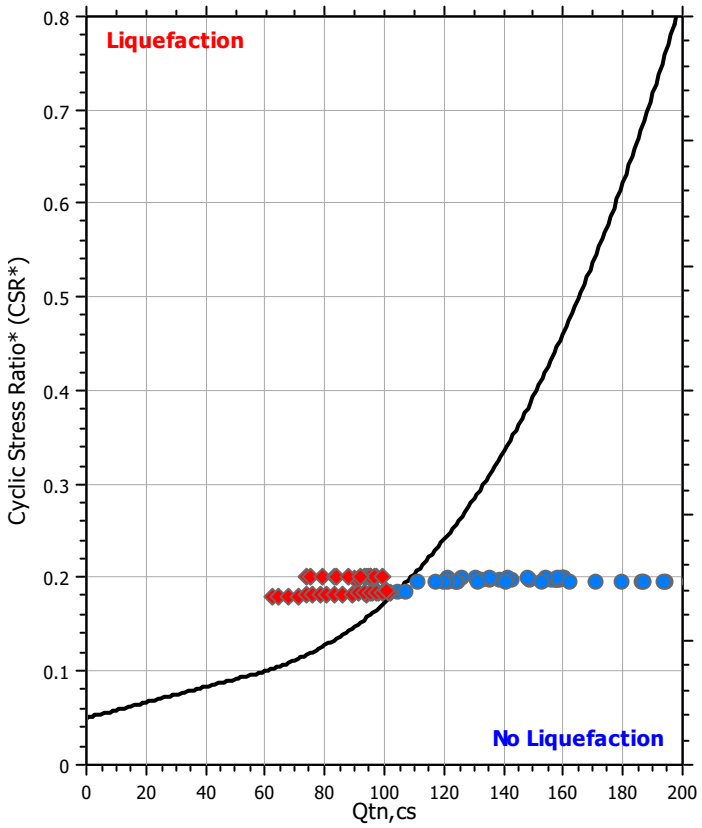
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

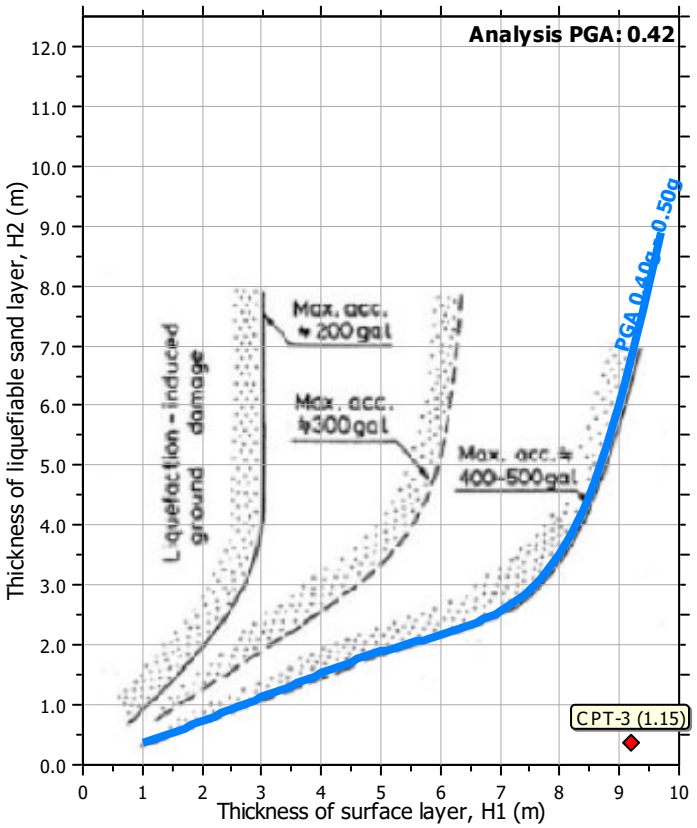
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



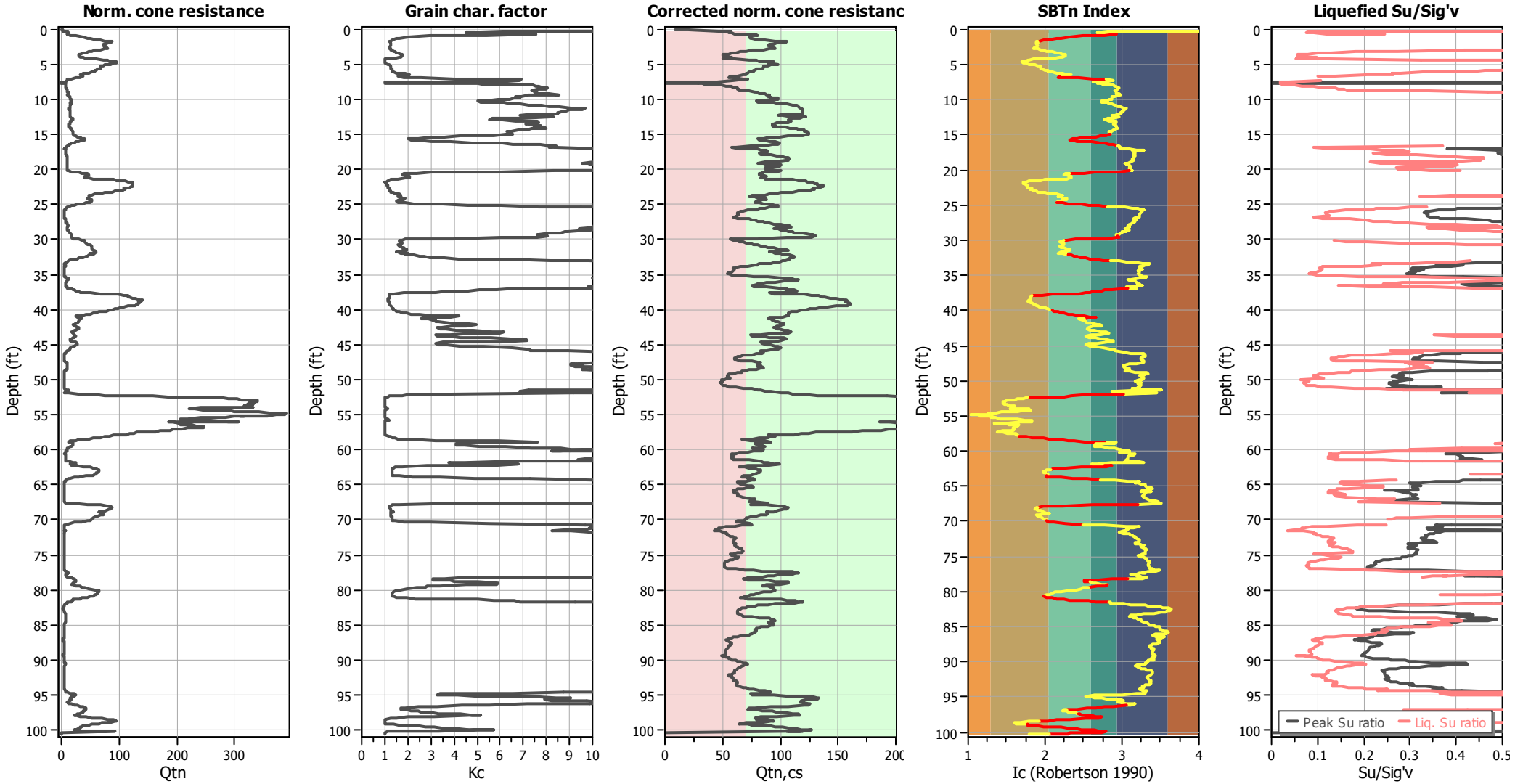




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	62.00 ft

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

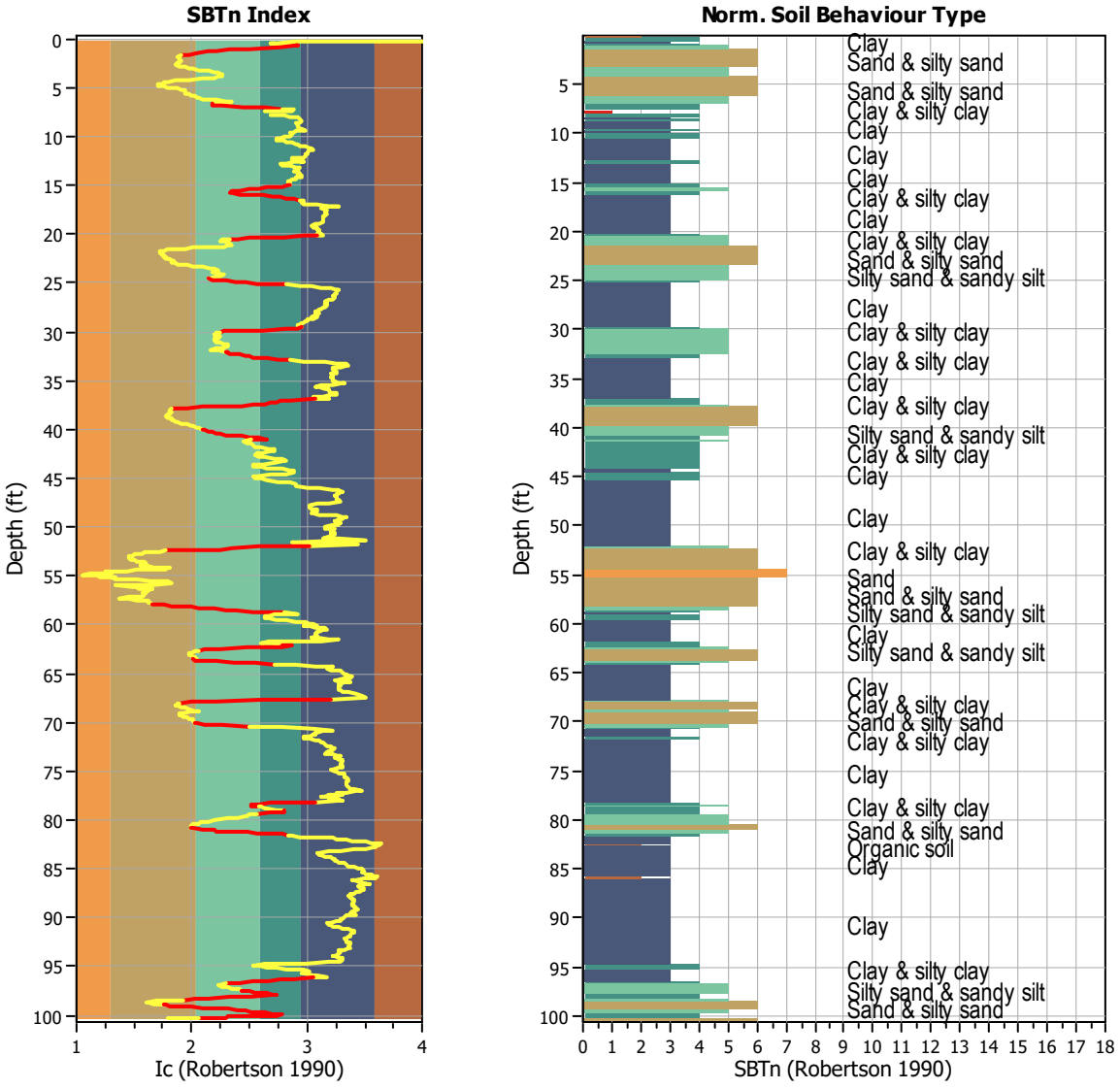
Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.12	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.42	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	62.00 ft

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between 1.80 < I_c < 3.0) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value:	1.70
I_c maximum check value:	3.00
I_c change ratio value:	0.0250
Minimum number of points in layer:	4

General statistics

Total points in CPT file:	1376
Total points excluded:	224
Exclusion percentage:	16.28%
Number of layers detected:	26

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	12	Start depth: 0.72 (ft)	3	Clay
		End depth: 1.74 (ft)	6	Sand & silty sand
Transition layer 2	6	Start depth: 6.76 (ft)	5	Silty sand & sandy silt
		End depth: 7.19 (ft)	4	Clay & silty clay
Transition layer 3	9	Start depth: 14.99 (ft)	3	Clay
		End depth: 15.67 (ft)	5	Silty sand & sandy silt
Transition layer 4	11	Start depth: 15.76 (ft)	5	Silty sand & sandy silt
		End depth: 16.58 (ft)	3	Clay
Transition layer 5	7	Start depth: 20.21 (ft)	3	Clay
		End depth: 20.60 (ft)	5	Silty sand & sandy silt
Transition layer 6	9	Start depth: 24.64 (ft)	5	Silty sand & sandy silt
		End depth: 25.27 (ft)	3	Clay
Transition layer 7	8	Start depth: 29.55 (ft)	3	Clay
		End depth: 30.13 (ft)	5	Silty sand & sandy silt
Transition layer 8	12	Start depth: 32.12 (ft)	5	Silty sand & sandy silt
		End depth: 32.98 (ft)	3	Clay
Transition layer 9	15	Start depth: 36.97 (ft)	3	Clay
		End depth: 37.97 (ft)	6	Sand & silty sand
Transition layer 10	12	Start depth: 40.09 (ft)	5	Silty sand & sandy silt
		End depth: 40.97 (ft)	4	Clay & silty clay
Transition layer 11	4	Start depth: 40.97 (ft)	4	Clay & silty clay
		End depth: 41.15 (ft)	5	Silty sand & sandy silt
Transition layer 12	8	Start depth: 52.01 (ft)	4	Clay & silty clay
		End depth: 52.45 (ft)	6	Sand & silty sand
Transition layer 13	14	Start depth: 57.92 (ft)	6	Sand & silty sand
		End depth: 58.84 (ft)	3	Clay
Transition layer 14	7	Start depth: 62.10 (ft)	3	Clay
		End depth: 62.74 (ft)	6	Sand & silty sand
Transition layer 15	7	Start depth: 63.61 (ft)	6	Sand & silty sand
		End depth: 64.15 (ft)	3	Clay
Transition layer 16	5	Start depth: 67.68 (ft)	4	Clay & silty clay
		End depth: 68.07 (ft)	6	Sand & silty sand
Transition layer 17	5	Start depth: 70.08 (ft)	6	Sand & silty sand
		End depth: 70.54 (ft)	4	Clay & silty clay
Transition layer 18	4	Start depth: 78.24 (ft)	4	Clay & silty clay
		End depth: 78.47 (ft)	5	Silty sand & sandy silt
Transition layer 19	4	Start depth: 78.53 (ft)	5	Silty sand & sandy silt
		End depth: 78.69 (ft)	4	Clay & silty clay
Transition layer 20	4	Start depth: 79.16 (ft)	4	Clay & silty clay
		End depth: 79.45 (ft)	5	Silty sand & sandy silt
Transition layer 21	15	Start depth: 80.83 (ft)	6	Sand & silty sand
		End depth: 81.56 (ft)	3	Clay
Transition layer 22	7	Start depth: 96.30 (ft)	3	Clay
		End depth: 96.87 (ft)	5	Silty sand & sandy silt
Transition layer 23	8	Start depth: 97.45 (ft)	5	Silty sand & sandy silt
		End depth: 97.88 (ft)	4	Clay & silty clay

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 24	8	Start depth: 97.88 (ft)	4	Clay & silty clay
		End depth: 98.47 (ft)	6	Sand & silty sand
Transition layer 25	14	Start depth: 98.98 (ft)	6	Sand & silty sand
		End depth: 99.95 (ft)	3	Clay
Transition layer 26	9	Start depth: 99.95 (ft)	3	Clay
		End depth: 100.28 (ft)	6	Sand & silty sand

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.04	0.10	0.03	0.00	100.00	87.36
2	0.10	0.10	0.04	0.00	100.00	87.36
3	0.11	0.20	0.05	0.00	100.00	87.36
4	0.16	0.40	0.05	0.00	100.00	87.36
5	0.19	1.01	0.05	0.00	100.00	88.74
6	0.24	2.43	0.05	0.00	71.90	91.34
7	0.31	5.06	0.06	0.00	51.48	93.80
8	0.38	7.29	0.07	0.00	42.56	95.48
9	0.43	7.69	0.08	0.00	39.63	96.43
10	0.49	7.69	0.08	0.00	41.35	96.84
11	0.58	6.58	0.09	0.00	44.64	97.26
12	0.63	6.17	0.10	0.00	49.07	97.85
13	0.67	5.97	0.11	0.00	51.93	98.72
14	0.72	6.02	0.13	0.00	53.54	99.42
15	0.72	6.07	0.13	0.00	52.47	101.17
16	0.84	8.00	0.20	0.00	44.02	103.62
17	0.96	13.76	0.25	0.00	30.61	106.61
18	1.06	25.71	0.28	0.10	23.44	108.76
19	1.24	28.44	0.33	0.10	19.50	109.81
20	1.30	29.76	0.31	0.10	17.10	110.05
21	1.48	36.23	0.28	0.10	14.00	110.41
22	1.59	45.85	0.33	0.10	12.36	111.13
23	1.69	44.33	0.37	0.10	11.12	112.10
24	1.69	52.02	0.37	0.10	10.74	112.65
25	1.74	53.04	0.39	0.10	9.92	112.99
26	1.79	54.66	0.40	0.10	9.87	113.14
27	1.84	53.64	0.39	0.10	10.04	113.01
28	1.88	50.40	0.38	0.10	10.26	112.64
29	1.93	49.70	0.35	0.10	10.40	112.09
30	1.99	48.28	0.32	0.10	10.27	111.60
31	2.03	48.08	0.31	0.10	10.19	111.23
32	2.08	47.87	0.31	0.10	10.14	110.98
33	2.13	47.06	0.29	0.10	10.28	110.80
34	2.22	45.65	0.30	0.10	10.49	110.61
35	2.27	44.84	0.29	0.10	10.68	110.44
36	2.33	44.43	0.28	0.10	10.61	110.26
37	2.42	45.04	0.28	0.10	10.34	110.23
38	2.48	46.86	0.28	0.10	9.95	110.30
39	2.56	48.28	0.28	0.10	9.56	110.53
40	2.65	50.10	0.29	0.10	9.36	110.70
41	2.72	49.90	0.29	0.10	9.62	110.74
42	2.80	46.15	0.29	0.10	10.31	110.44
43	2.89	42.00	0.28	0.10	11.29	109.97
44	2.94	39.17	0.26	0.10	12.40	109.53
45	3.04	35.93	0.26	0.10	13.48	109.00
46	3.14	32.59	0.24	0.10	14.78	108.19
47	3.23	28.44	0.21	0.10	15.91	107.05
48	3.31	26.01	0.18	0.10	17.31	105.88

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.37	22.77	0.17	0.10	18.64	104.75
50	3.48	20.34	0.15	0.10	20.16	103.47
51	3.57	18.02	0.12	0.10	20.83	102.23
52	3.65	18.02	0.11	0.10	20.99	101.38
53	3.71	18.02	0.11	0.10	20.91	101.29
54	3.82	18.02	0.11	0.10	20.93	102.11
55	3.91	19.84	0.15	0.10	20.16	103.21
56	4.00	22.67	0.16	0.10	18.85	104.71
57	4.10	25.91	0.19	0.10	15.53	104.42
58	4.19	30.57	0.11	0.10	5.00	104.40
59	4.26	37.15	0.13	0.10	5.00	104.51
60	4.35	46.05	0.17	0.10	5.00	106.46
61	4.44	53.64	0.20	0.19	5.00	107.75
62	4.52	49.70	0.21	0.19	5.00	108.36
63	4.53	50.81	0.21	0.19	5.00	108.59
64	4.58	56.27	0.21	0.19	5.00	108.81
65	4.63	58.00	0.22	0.19	5.00	109.16
66	4.68	59.01	0.23	0.19	5.00	109.49
67	4.72	59.51	0.24	0.19	5.00	109.83
68	4.77	59.31	0.25	0.19	5.00	110.07
69	4.82	58.40	0.26	0.19	5.00	110.22
70	4.88	56.48	0.26	0.19	5.00	110.30
71	4.96	53.74	0.27	0.19	7.94	110.33
72	5.01	50.61	0.27	0.19	8.80	110.33
73	5.08	47.27	0.28	0.19	9.75	110.30
74	5.16	44.43	0.28	0.19	10.61	110.22
75	5.21	42.71	0.28	0.19	11.15	110.15
76	5.30	42.66	0.28	0.19	11.35	110.11
77	5.37	42.66	0.28	0.19	11.37	110.11
78	5.45	42.61	0.28	0.19	11.35	110.10
79	5.52	42.81	0.28	0.19	11.43	110.08
80	5.59	41.90	0.28	0.19	11.67	109.99
81	5.65	40.38	0.27	0.19	12.17	109.79
82	5.74	38.16	0.27	0.19	12.78	109.59
83	5.83	36.84	0.27	0.19	13.36	109.47
84	5.89	36.23	0.27	0.29	13.78	109.49
85	5.97	35.83	0.27	0.29	14.10	109.46
86	6.07	34.92	0.27	0.29	14.65	109.36
87	6.12	32.79	0.27	0.29	15.67	109.20
88	6.22	29.96	0.27	0.29	17.39	109.00
89	6.28	26.52	0.27	0.29	19.71	108.75
90	6.36	23.18	0.27	0.29	22.24	108.30
91	6.46	20.65	0.26	0.29	24.09	107.75
92	6.52	20.04	0.24	0.29	23.83	106.97
93	6.60	21.46	0.20	0.29	21.15	106.06
94	6.70	24.70	0.16	0.29	18.41	104.86
95	6.76	24.49	0.14	0.29	18.15	104.05
96	6.84	19.84	0.15	0.29	21.31	103.55

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.94	14.57	0.15	0.29	28.13	103.13
98	7.03	10.32	0.15	0.29	36.85	102.17
99	7.13	7.69	0.14	0.29	45.33	101.02
100	7.19	6.68	0.13	0.29	50.80	99.02
101	7.32	5.47	0.08	0.29	50.53	95.58
102	7.42	5.16	0.02	0.29	46.05	89.63
103	7.49	4.86	0.01	0.29	36.85	87.36
104	7.57	4.76	-0.01	0.29	N/A	87.36
105	7.66	4.55	0.00	0.29	N/A	87.36
106	7.76	4.35	0.01	0.29	39.30	87.36
107	7.77	4.40	0.01	0.29	41.66	87.36
108	7.78	4.40	0.01	0.29	42.16	87.36
109	7.82	4.45	0.01	0.29	43.69	87.36
110	7.87	4.45	0.02	0.29	46.05	87.36
111	7.92	4.45	0.03	0.29	48.69	87.36
112	7.97	4.45	0.03	0.29	50.96	88.91
113	8.01	4.55	0.04	0.29	52.87	90.83
114	8.06	4.76	0.05	0.29	53.56	92.24
115	8.11	4.96	0.06	0.29	53.89	93.35
116	8.20	5.06	0.06	0.29	54.02	94.10
117	8.26	5.16	0.07	0.29	54.67	94.95
118	8.35	5.26	0.08	0.29	55.25	95.57
119	8.40	5.26	0.08	0.38	55.42	95.96
120	8.49	5.36	0.08	0.38	55.15	96.13
121	8.54	5.47	0.08	0.38	54.56	96.42
122	8.64	5.67	0.09	0.38	53.58	96.77
123	8.69	5.97	0.09	0.38	52.70	97.12
124	8.79	6.07	0.09	0.38	53.07	98.37
125	8.84	6.48	0.14	0.38	53.64	99.77
126	8.93	6.88	0.15	0.38	53.23	100.93
127	9.03	7.29	0.15	0.38	53.10	101.61
128	9.08	7.19	0.17	0.38	53.34	101.99
129	9.11	7.14	0.18	0.38	54.44	102.35
130	9.12	7.14	0.18	0.38	54.87	102.44
131	9.17	7.08	0.18	0.38	55.46	102.54
132	9.22	6.98	0.19	0.38	55.68	102.79
133	9.31	7.29	0.19	0.38	57.60	103.02
134	9.36	6.48	0.20	0.38	56.84	103.40
135	9.40	7.69	0.21	0.38	55.49	103.68
136	9.46	8.20	0.21	0.38	52.20	104.01
137	9.51	8.50	0.21	0.38	50.78	104.20
138	9.55	8.70	0.22	0.48	49.80	104.47
139	9.61	9.11	0.23	0.48	49.60	104.86
140	9.69	9.11	0.24	0.48	49.93	105.32
141	9.74	9.11	0.26	0.38	50.53	105.75
142	9.81	9.31	0.27	0.48	50.47	106.17
143	9.89	9.72	0.28	0.38	49.47	106.49
144	9.94	10.22	0.29	0.48	48.57	106.69

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	10.03	10.22	0.28	0.48	47.95	106.73
146	10.08	10.22	0.28	0.48	46.27	105.91
147	10.18	10.22	0.19	0.48	43.86	104.66
148	10.23	10.22	0.16	0.48	42.16	103.72
149	10.33	10.22	0.21	0.48	42.78	104.06
150	10.40	10.22	0.22	0.48	44.53	104.99
151	10.47	10.22	0.24	0.48	46.24	105.54
152	10.51	9.77	0.26	0.48	47.48	106.12
153	10.56	10.17	0.28	0.48	48.53	106.55
154	10.61	10.12	0.29	0.48	48.96	107.12
155	10.67	10.32	0.32	0.48	50.59	107.76
156	10.75	10.02	0.37	0.48	52.01	108.32
157	10.80	10.02	0.37	0.48	53.26	108.59
158	10.85	9.92	0.37	0.48	53.79	108.61
159	10.90	9.72	0.37	0.57	54.58	108.60
160	11.00	9.51	0.38	0.57	55.86	108.56
161	11.05	9.11	0.37	0.57	57.54	108.36
162	11.14	8.50	0.36	0.57	59.49	108.14
163	11.21	8.20	0.36	0.57	61.41	108.08
164	11.29	8.10	0.38	0.57	61.90	108.18
165	11.38	8.40	0.37	0.57	61.40	108.38
166	11.46	8.70	0.39	0.57	60.04	108.48
167	11.52	8.91	0.38	0.57	59.20	108.60
168	11.60	9.01	0.38	0.57	58.74	108.64
169	11.67	9.01	0.39	0.57	58.51	108.69
170	11.72	9.11	0.39	0.57	58.33	108.76
171	11.81	9.21	0.39	0.57	57.50	108.86
172	11.86	9.62	0.39	0.57	57.42	108.90
173	11.96	9.21	0.39	0.57	57.28	108.93
174	12.01	9.41	0.40	0.57	57.36	108.99
175	12.10	9.72	0.40	0.57	56.33	108.48
176	12.16	9.92	0.30	0.57	52.86	107.67
177	12.24	10.53	0.27	0.67	50.46	107.26
178	12.32	10.93	0.34	0.67	50.49	108.00
179	12.39	11.13	0.39	0.67	51.82	109.13
180	12.48	11.44	0.42	0.67	55.21	109.56
181	12.50	9.31	0.43	0.67	56.54	109.82
182	12.54	9.92	0.45	0.67	56.14	110.10
183	12.64	12.95	0.45	0.67	51.14	110.63
184	12.68	14.17	0.46	0.67	46.74	111.06
185	12.77	14.98	0.47	0.67	45.02	111.08
186	12.82	14.98	0.44	0.67	44.58	110.87
187	12.89	14.27	0.42	0.67	45.32	110.45
188	12.97	13.36	0.41	0.67	47.27	110.13
189	13.03	12.45	0.41	0.67	49.63	109.86
190	13.12	11.64	0.40	0.67	52.08	109.64
191	13.16	11.03	0.40	0.67	53.60	109.40
192	13.26	10.93	0.39	0.67	54.00	108.95

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	13.34	10.73	0.34	0.67	53.03	108.33
194	13.41	10.83	0.31	0.67	51.87	107.54
195	13.50	10.63	0.28	0.67	51.53	107.03
196	13.60	10.32	0.28	0.67	52.24	106.75
197	13.65	10.02	0.28	0.67	53.22	106.76
198	13.75	10.02	0.29	0.67	54.12	106.90
199	13.80	10.02	0.30	0.67	53.54	106.72
200	13.89	10.22	0.26	0.67	53.46	106.90
201	13.94	10.42	0.31	0.76	53.08	107.50
202	14.03	11.23	0.37	0.76	54.97	108.63
203	14.11	10.73	0.41	0.76	55.24	109.48
204	14.13	11.69	0.42	0.76	55.28	110.03
205	14.18	12.15	0.45	0.76	53.47	110.47
206	14.22	12.95	0.46	0.76	52.62	110.95
207	14.28	13.36	0.49	0.76	51.87	111.50
208	14.37	13.97	0.53	0.76	51.36	112.04
209	14.44	14.68	0.56	0.76	50.25	112.56
210	14.51	15.69	0.58	0.76	48.93	112.99
211	14.60	16.50	0.60	0.76	48.02	113.34
212	14.65	16.70	0.62	0.76	47.94	113.59
213	14.75	16.50	0.63	0.76	48.44	113.74
214	14.85	16.45	0.64	0.76	48.93	113.80
215	14.91	16.45	0.63	0.76	49.08	113.80
216	14.99	16.40	0.63	0.76	47.80	113.81
217	15.09	18.12	0.62	0.76	45.25	113.98
218	15.18	20.34	0.63	0.76	41.64	114.15
219	15.25	22.37	0.61	0.76	38.13	114.10
220	15.33	24.09	0.55	0.76	34.47	113.87
221	15.43	27.02	0.52	0.76	30.57	113.72
222	15.51	31.38	0.52	0.76	26.98	113.86
223	15.59	35.53	0.52	0.76	24.54	114.07
224	15.67	36.94	0.52	0.76	23.56	114.17
225	15.76	36.03	0.51	0.86	24.48	114.23
226	15.86	32.39	0.54	0.76	26.98	114.13
227	15.95	27.63	0.54	0.76	31.02	113.82
228	16.05	22.87	0.53	0.76	35.88	113.11
229	16.14	18.72	0.48	0.76	40.89	112.24
230	16.20	16.30	0.45	0.76	44.59	111.36
231	16.28	15.49	0.42	0.76	47.26	110.71
232	16.34	14.17	0.41	0.76	49.02	109.97
233	16.44	12.95	0.36	0.76	51.62	109.16
234	16.50	11.64	0.33	0.86	54.21	108.05
235	16.58	10.22	0.29	0.76	56.10	106.16
236	16.73	8.60	0.17	0.86	57.07	103.07
237	16.82	7.39	0.09	0.76	55.90	98.94
238	16.92	6.78	0.07	0.86	56.73	97.37
239	17.01	6.98	0.12	0.86	64.41	99.23
240	17.11	5.87	0.17	0.86	72.33	101.23

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	17.12	5.72	0.19	0.86	79.64	102.14
242	17.14	5.57	0.19	0.86	75.40	102.95
243	17.19	7.69	0.22	0.86	70.99	103.97
244	17.28	8.10	0.25	0.86	67.48	104.99
245	17.33	8.00	0.26	0.86	68.61	105.59
246	17.43	7.89	0.28	0.86	70.20	105.75
247	17.47	7.69	0.27	0.86	70.55	105.46
248	17.57	7.59	0.24	0.86	70.29	104.78
249	17.65	7.39	0.21	0.86	69.39	104.05
250	17.72	7.39	0.21	0.86	69.90	104.00
251	17.81	7.39	0.23	0.86	69.98	104.48
252	17.86	7.89	0.25	0.86	70.40	105.52
253	17.95	8.30	0.30	0.86	70.27	106.61
254	18.05	8.70	0.35	0.86	69.77	107.59
255	18.10	9.31	0.36	0.86	69.28	108.43
256	18.20	9.62	0.41	0.86	68.75	109.17
257	18.30	10.02	0.44	0.86	69.06	109.74
258	18.39	10.02	0.45	0.86	68.69	110.03
259	18.48	10.32	0.45	0.86	68.26	110.09
260	18.58	10.42	0.45	0.86	68.26	110.10
261	18.66	10.12	0.45	0.86	68.67	110.00
262	18.74	10.02	0.43	0.86	68.65	109.66
263	18.87	10.02	0.39	0.86	65.89	108.15
264	18.97	9.62	0.22	0.86	63.51	106.58
265	19.06	9.31	0.24	0.96	61.57	105.45
266	19.16	9.72	0.27	0.86	62.59	106.45
267	19.25	10.42	0.32	0.96	62.93	107.21
268	19.27	10.22	0.32	0.86	63.88	107.82
269	19.30	10.02	0.35	0.96	64.63	108.39
270	19.34	10.83	0.39	0.96	65.30	109.05
271	19.39	10.83	0.41	0.96	65.04	109.46
272	19.49	10.83	0.41	0.96	65.33	109.38
273	19.55	10.63	0.38	0.96	65.79	108.98
274	19.63	10.02	0.36	0.96	66.38	108.45
275	19.68	9.82	0.34	0.96	66.57	107.82
276	19.74	9.72	0.30	0.96	65.75	107.23
277	19.83	9.72	0.28	0.96	65.45	106.97
278	19.87	9.72	0.31	0.96	65.22	106.85
279	19.94	9.72	0.29	0.96	66.15	107.18
280	20.02	9.72	0.33	0.96	67.03	107.64
281	20.07	9.92	0.36	0.96	67.92	108.78
282	20.17	10.83	0.44	0.96	64.62	109.94
283	20.21	13.46	0.47	0.96	56.54	111.19
284	20.28	18.22	0.50	0.96	46.28	112.30
285	20.36	24.49	0.52	1.05	37.36	113.43
286	20.41	31.88	0.56	1.05	30.98	114.57
287	20.48	38.76	0.62	1.05	26.57	115.62
288	20.55	45.24	0.66	1.05	23.46	116.43

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	20.60	50.91	0.67	1.05	21.46	116.95
290	20.70	53.44	0.69	1.05	20.55	117.24
291	20.74	53.24	0.71	1.05	20.71	117.40
292	20.79	51.32	0.72	1.05	21.66	117.54
293	20.89	48.89	0.76	1.05	23.50	117.89
294	20.96	45.85	0.85	0.96	23.80	117.32
295	21.04	45.80	0.57	0.96	24.10	117.07
296	21.13	45.80	0.70	0.96	23.70	116.74
297	21.22	45.75	0.76	0.96	23.00	117.62
298	21.29	56.07	0.78	1.05	21.86	118.10
299	21.35	56.27	0.79	1.05	18.50	118.64
300	21.37	73.99	0.80	1.05	15.90	119.09
301	21.42	83.80	0.82	1.05	13.13	119.55
302	21.47	93.32	0.82	1.05	11.52	119.85
303	21.48	101.01	0.82	1.05	10.27	120.06
304	21.52	107.59	0.82	1.05	9.34	120.20
305	21.57	113.46	0.81	1.05	8.57	120.29
306	21.62	118.62	0.80	1.05	7.91	120.35
307	21.66	124.29	0.80	1.05	7.35	120.43
308	21.71	129.05	0.81	1.15	6.92	120.56
309	21.76	132.99	0.82	1.15	6.65	120.75
310	21.81	135.83	0.84	1.15	6.55	120.99
311	21.85	137.14	0.87	1.15	6.57	121.25
312	21.91	137.95	0.90	1.15	6.66	121.49
313	21.95	138.26	0.92	1.15	6.78	121.69
314	22.00	138.06	0.94	1.15	6.89	121.84
315	22.05	138.36	0.96	1.15	6.99	121.96
316	22.10	138.06	0.97	1.15	7.07	122.06
317	22.15	138.26	0.98	1.15	7.14	122.15
318	22.19	138.56	0.99	1.15	7.18	122.24
319	22.24	139.17	1.00	1.15	7.38	122.59
320	22.29	139.98	1.12	1.15	7.48	122.79
321	22.34	140.38	1.07	1.15	7.53	122.89
322	22.39	140.18	1.04	1.15	7.42	122.71
323	22.43	139.57	1.04	1.15	7.44	122.63
324	22.48	138.46	1.05	1.15	7.57	122.64
325	22.55	136.94	1.06	1.15	7.77	122.66
326	22.62	134.92	1.06	1.15	8.48	122.57
327	22.63	118.32	1.06	1.24	8.67	122.48
328	22.72	130.57	1.04	1.24	8.87	122.34
329	22.77	127.73	1.02	1.24	8.53	122.30
330	22.83	125.91	1.02	1.24	8.81	122.33
331	22.91	124.70	1.06	1.24	9.13	122.40
332	22.96	121.96	1.07	1.24	9.51	122.45
333	23.02	118.52	1.06	1.24	9.95	122.36
334	23.10	114.07	1.06	1.24	10.51	122.24
335	23.16	108.91	1.05	1.24	11.23	122.08
336	23.20	102.23	1.04	1.24	12.12	121.86

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	23.26	95.44	1.03	1.24	13.14	121.54
338	23.35	88.66	0.99	1.24	14.37	121.28
339	23.39	81.88	1.01	1.24	15.74	120.92
340	23.48	74.39	0.96	1.24	17.51	120.69
341	23.54	67.71	0.98	1.24	19.01	120.18
342	23.63	62.85	0.89	1.24	19.95	119.45
343	23.69	59.72	0.76	1.24	19.23	117.77
344	23.78	57.59	0.48	1.24	18.61	116.63
345	23.87	57.74	0.60	1.24	18.21	116.01
346	23.88	57.74	0.61	1.24	19.03	116.77
347	23.93	57.89	0.67	1.34	19.95	117.38
348	24.02	56.58	0.77	1.34	20.80	117.95
349	24.04	57.13	0.78	1.34	21.46	118.37
350	24.05	57.13	0.80	1.34	21.78	118.73
351	24.15	57.69	0.89	1.34	21.95	119.14
352	24.20	59.92	0.91	1.34	21.72	119.56
353	24.30	62.65	0.93	1.34	20.63	119.52
354	24.40	65.28	0.83	1.34	19.19	119.11
355	24.46	67.21	0.74	1.34	17.84	118.42
356	24.54	67.21	0.69	1.34	17.34	117.92
357	24.64	64.78	0.69	1.34	18.05	117.78
358	24.73	60.22	0.72	1.34	19.84	117.90
359	24.78	54.76	0.77	1.34	22.46	118.05
360	24.88	48.89	0.80	1.34	25.68	117.95
361	24.94	42.00	0.78	1.24	29.51	117.49
362	25.02	34.82	0.73	1.24	34.04	116.54
363	25.12	28.14	0.65	1.24	39.88	115.47
364	25.17	22.27	0.62	1.24	46.77	114.38
365	25.27	18.12	0.59	1.24	54.06	113.10
366	25.36	14.78	0.46	1.24	61.30	111.68
367	25.43	12.45	0.42	1.24	67.46	110.12
368	25.50	10.53	0.38	1.24	73.11	108.95
369	25.60	9.62	0.33	1.24	77.33	107.97
370	25.64	9.11	0.32	1.24	78.94	107.28
371	25.67	9.01	0.30	1.15	79.14	106.81
372	25.71	9.01	0.28	1.15	78.50	105.99
373	25.79	8.50	0.23	1.15	78.06	104.81
374	25.93	8.00	0.19	1.15	77.81	103.60
375	26.03	8.00	0.18	1.15	77.15	102.74
376	26.13	8.00	0.16	1.15	76.38	102.36
377	26.24	8.00	0.16	1.15	75.73	102.24
378	26.37	8.20	0.17	1.15	75.53	102.41
379	26.47	8.30	0.17	1.15	75.71	102.64
380	26.60	8.20	0.18	1.15	74.72	102.14
381	26.71	8.20	0.14	1.15	72.50	101.53
382	26.85	8.70	0.13	1.15	69.69	101.34
383	26.95	9.31	0.16	1.15	71.29	102.63
384	27.04	8.81	0.22	1.15	71.21	104.34

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	27.09	10.63	0.25	1.05	71.61	105.86
386	27.19	10.93	0.29	1.05	69.63	106.85
387	27.23	11.23	0.30	1.05	70.05	107.52
388	27.33	11.34	0.32	1.05	70.38	108.10
389	27.40	11.64	0.36	1.05	70.26	108.70
390	27.47	12.25	0.38	1.05	69.48	109.39
391	27.57	12.95	0.41	1.05	68.12	110.02
392	27.66	13.66	0.44	1.05	66.86	110.95
393	27.77	14.88	0.52	1.05	65.56	112.10
394	27.86	16.30	0.60	1.05	64.27	113.38
395	27.96	17.61	0.69	1.05	63.40	114.40
396	28.06	18.22	0.74	1.05	64.03	115.00
397	28.15	17.31	0.77	1.05	65.56	115.03
398	28.25	16.30	0.72	1.05	64.37	114.22
399	28.34	17.46	0.52	1.05	63.64	113.20
400	28.44	15.69	0.53	1.05	61.14	112.70
401	28.54	17.61	0.59	1.05	64.86	113.09
402	28.62	14.98	0.63	1.05	62.81	113.97
403	28.71	19.74	0.70	1.05	62.14	114.69
404	28.77	20.24	0.75	1.05	59.04	115.50
405	28.86	20.75	0.80	1.05	59.06	115.95
406	28.91	21.15	0.82	1.05	58.48	116.29
407	28.97	22.06	0.84	1.05	57.87	116.68
408	29.04	22.87	0.91	1.05	57.17	117.16
409	29.10	23.78	0.96	1.05	56.38	117.71
410	29.15	25.20	1.01	1.05	55.66	118.36
411	29.25	26.42	1.13	1.05	54.03	119.02
412	29.34	27.53	1.19	1.05	53.66	119.56
413	29.38	28.14	1.22	1.05	53.77	119.85
414	29.48	27.53	1.26	1.05	55.21	119.97
415	29.55	27.43	1.26	1.05	55.61	119.94
416	29.63	27.43	1.21	1.05	53.71	119.51
417	29.72	27.33	1.04	1.05	46.70	117.24
418	29.82	30.47	0.29	1.15	36.62	114.29
419	29.88	36.84	0.31	1.15	26.07	110.63
420	29.96	43.12	0.35	1.15	21.97	111.98
421	30.06	55.67	0.40	1.15	20.66	113.06
422	30.13	50.91	0.44	1.05	19.28	113.85
423	30.18	57.39	0.44	1.05	19.21	114.32
424	30.28	59.72	0.48	1.05	18.92	115.08
425	30.37	59.01	0.56	1.05	19.74	116.07
426	30.47	59.82	0.65	1.05	20.55	117.07
427	30.57	62.65	0.72	1.05	20.45	117.89
428	30.66	67.31	0.76	1.05	19.78	118.59
429	30.74	71.76	0.82	1.05	19.08	119.20
430	30.82	74.90	0.87	1.05	18.72	119.77
431	30.90	76.82	0.92	1.15	18.90	120.37
432	31.01	77.12	1.02	1.15	19.54	121.00

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	31.10	76.72	1.12	1.15	20.53	121.75
434	31.19	77.18	1.25	1.15	21.62	122.52
435	31.28	77.23	1.39	1.15	22.44	123.19
436	31.35	78.24	1.47	1.15	22.96	123.75
437	31.43	80.06	1.56	1.15	23.03	124.24
438	31.53	83.20	1.66	1.15	22.94	124.75
439	31.60	86.03	1.75	1.15	21.03	124.07
440	31.67	88.46	1.07	1.15	19.28	123.27
441	31.77	89.68	1.16	1.15	17.72	122.34
442	31.84	90.18	1.26	1.15	18.27	122.84
443	31.91	89.68	1.32	1.15	19.80	123.18
444	31.98	78.64	1.39	1.15	22.19	123.23
445	31.98	68.93	1.40	1.15	23.12	123.39
446	32.04	84.01	1.44	1.24	23.03	123.69
447	32.12	83.20	1.54	1.24	22.36	124.14
448	32.16	80.77	1.60	1.24	23.73	124.42
449	32.27	76.11	1.67	1.24	25.51	124.47
450	32.33	70.04	1.66	1.24	27.40	124.34
451	32.41	66.09	1.63	1.24	28.95	124.00
452	32.50	62.75	1.55	1.24	30.35	123.44
453	32.58	56.48	1.41	1.24	31.97	122.68
454	32.66	50.71	1.29	1.24	34.45	121.67
455	32.74	43.42	1.16	1.24	37.91	120.54
456	32.84	35.73	1.02	1.24	42.91	119.34
457	32.90	29.15	0.95	1.24	48.72	118.12
458	32.98	24.70	0.85	1.24	56.09	116.92
459	33.08	20.85	0.75	1.24	62.41	115.68
460	33.14	16.70	0.69	1.24	70.22	114.44
461	33.22	13.56	0.63	1.24	78.27	113.16
462	33.32	12.04	0.53	1.24	84.25	111.85
463	33.37	10.93	0.46	1.24	85.46	110.42
464	33.47	10.83	0.38	1.24	84.74	109.62
465	33.56	11.34	0.39	1.24	80.65	109.42
466	33.63	12.75	0.41	1.24	77.37	109.72
467	33.71	13.16	0.40	1.24	75.48	109.42
468	33.81	12.04	0.34	1.24	74.83	107.78
469	33.90	10.73	0.19	1.24	75.10	105.75
470	33.95	10.32	0.19	1.24	75.13	103.88
471	34.04	9.82	0.19	1.24	76.22	103.67
472	34.14	10.02	0.18	1.34	77.27	103.52
473	34.17	9.72	0.19	1.24	77.76	103.53
474	34.20	9.62	0.19	1.24	76.51	103.73
475	34.26	10.83	0.19	1.24	75.12	103.91
476	34.35	10.63	0.19	1.24	73.88	103.93
477	34.43	10.32	0.19	1.24	74.71	103.73
478	34.49	10.22	0.18	1.24	74.86	103.40
479	34.59	10.22	0.17	1.24	74.51	102.92
480	34.69	10.02	0.15	1.24	74.15	102.43

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	34.73	9.92	0.15	1.24	74.31	102.00
482	34.83	9.72	0.15	1.24	74.57	101.78
483	34.90	9.72	0.14	1.24	75.16	101.82
484	34.98	9.72	0.15	1.24	75.52	102.24
485	35.07	10.02	0.17	1.24	76.19	103.35
486	35.16	10.63	0.21	1.24	78.83	105.56
487	35.26	11.03	0.33	1.24	83.16	108.85
488	35.33	12.15	0.55	1.24	81.79	112.16
489	35.40	16.50	0.76	1.34	74.84	114.98
490	35.50	21.56	0.92	1.34	67.00	116.75
491	35.57	24.39	0.97	1.34	63.27	117.70
492	35.65	24.09	1.01	1.34	63.57	118.14
493	35.71	22.77	1.08	1.34	66.27	118.34
494	35.79	21.66	1.09	1.34	69.18	118.25
495	35.85	20.45	1.03	1.34	71.21	117.70
496	35.94	18.93	0.91	1.34	72.32	116.92
497	35.99	18.42	0.83	1.34	72.47	115.84
498	36.08	17.51	0.69	1.34	72.38	114.36
499	36.17	15.49	0.51	1.34	73.86	112.64
500	36.24	13.56	0.46	1.34	75.60	111.22
501	36.33	13.56	0.44	1.34	77.26	110.71
502	36.42	13.56	0.44	1.34	77.95	110.94
503	36.52	13.56	0.50	1.34	73.49	110.01
504	36.61	14.98	0.26	1.34	67.87	109.88
505	36.70	17.61	0.38	1.34	62.71	110.97
506	36.78	20.55	0.63	1.34	62.56	113.90
507	36.85	22.47	0.80	1.34	71.90	115.26
508	36.87	11.64	0.83	1.34	69.07	116.41
509	36.91	26.42	0.92	1.34	63.50	117.24
510	36.97	31.58	0.97	1.43	49.63	118.44
511	37.06	36.13	1.01	1.43	46.01	119.19
512	37.12	37.96	1.11	1.43	43.96	120.10
513	37.20	41.70	1.28	1.43	42.39	121.21
514	37.27	47.47	1.45	1.43	39.71	122.19
515	37.35	53.44	1.50	1.43	36.91	122.63
516	37.44	55.67	1.40	1.43	34.70	122.58
517	37.49	56.48	1.34	1.43	32.26	122.38
518	37.59	63.06	1.30	1.43	27.80	122.53
519	37.64	81.98	1.30	1.43	21.40	123.10
520	37.70	111.84	1.32	1.53	15.68	123.77
521	37.78	139.98	1.32	1.53	11.92	124.31
522	37.83	157.89	1.32	1.53	9.84	124.68
523	37.92	169.13	1.35	1.53	8.83	124.96
524	37.97	175.50	1.38	1.53	8.44	125.29
525	38.07	179.05	1.45	1.53	8.35	125.63
526	38.14	181.78	1.51	1.53	8.44	126.04
527	38.22	184.61	1.60	1.53	8.51	126.51
528	38.31	190.69	1.72	1.53	8.57	127.15

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	38.41	199.80	1.90	1.62	8.22	127.66
530	38.52	213.56	1.89	1.62	7.81	128.17
531	38.64	224.49	2.02	1.62	7.45	128.44
532	38.74	225.00	2.04	1.62	7.89	128.67
533	38.80	204.05	2.10	1.62	8.30	128.80
534	38.89	213.46	2.16	1.82	8.75	128.95
535	38.94	213.66	2.21	1.82	8.74	129.21
536	39.03	213.76	2.31	1.82	9.04	129.51
537	39.13	213.26	2.44	1.82	9.44	129.87
538	39.23	212.65	2.56	1.91	9.96	130.20
539	39.35	208.10	2.67	1.91	10.48	130.39
540	39.42	202.73	2.68	1.91	11.13	130.39
541	39.51	192.20	2.66	1.91	11.86	130.23
542	39.60	181.27	2.62	1.91	12.73	129.97
543	39.70	170.95	2.55	1.91	13.46	129.70
544	39.78	166.19	2.50	1.91	14.13	129.38
545	39.90	156.68	2.40	1.91	14.77	129.07
546	39.99	149.09	2.35	1.91	15.57	128.71
547	40.09	141.29	2.28	1.91	16.39	128.37
548	40.18	133.80	2.21	1.91	17.30	128.04
549	40.23	126.21	2.16	1.91	18.29	127.67
550	40.33	118.02	2.08	1.91	19.50	127.30
551	40.43	109.72	2.03	1.91	20.84	126.92
552	40.52	102.53	1.98	1.91	22.74	126.70
553	40.61	93.22	2.06	1.91	24.63	126.07
554	40.69	81.48	1.71	1.91	27.65	125.27
555	40.80	67.00	1.63	1.91	31.04	124.10
556	40.87	57.39	1.51	1.91	34.44	123.25
557	40.95	55.26	1.38	1.91	37.39	122.50
558	40.97	47.67	1.35	1.91	38.04	122.03
559	41.01	51.11	1.30	2.01	35.69	121.95
560	41.07	64.07	1.26	2.01	31.09	122.03
561	41.15	70.14	1.23	2.01	28.20	122.06
562	41.26	67.91	1.21	1.91	28.17	121.94
563	41.35	63.26	1.21	1.91	29.96	121.73
564	41.47	57.89	1.20	1.91	31.46	121.66
565	41.59	59.61	1.23	1.91	31.96	121.71
566	41.69	61.44	1.24	1.91	31.98	121.95
567	41.78	60.12	1.30	1.91	33.05	122.10
568	41.88	55.87	1.33	1.82	35.75	121.95
569	41.98	48.18	1.27	1.82	39.01	121.52
570	42.08	44.23	1.21	1.82	41.72	120.96
571	42.16	42.91	1.16	1.82	41.89	120.65
572	42.24	45.75	1.14	1.82	39.57	120.77
573	42.31	52.63	1.19	1.91	36.25	121.19
574	42.45	58.30	1.23	1.82	33.81	121.60
575	42.55	59.82	1.24	1.82	32.69	121.82
576	42.60	59.92	1.25	1.82	32.61	121.90

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	42.70	59.51	1.27	1.82	33.18	122.03
578	42.81	58.50	1.32	1.72	34.70	122.15
579	42.89	54.05	1.36	1.72	37.37	122.12
580	42.98	48.08	1.34	1.72	41.13	121.83
581	43.08	42.61	1.30	1.72	45.23	121.41
582	43.17	38.66	1.28	1.72	47.51	121.07
583	43.27	39.98	1.25	1.72	46.42	120.88
584	43.37	44.43	1.19	1.72	41.14	119.79
585	43.50	46.96	0.69	1.72	35.96	118.51
586	43.61	48.99	0.69	1.72	32.32	117.19
587	43.74	49.59	0.74	1.62	32.41	117.56
588	43.79	49.29	0.79	1.62	33.54	118.20
589	43.86	48.99	0.89	1.43	35.58	118.96
590	43.94	47.06	1.02	1.34	38.25	119.71
591	44.00	45.04	1.11	1.34	41.55	120.34
592	44.08	42.51	1.22	1.34	44.91	120.67
593	44.17	39.37	1.23	1.34	48.70	120.54
594	44.27	34.61	1.15	1.34	51.70	119.87
595	44.42	32.29	1.00	1.34	51.75	119.10
596	44.52	35.53	0.93	1.34	46.94	118.74
597	44.61	43.42	0.93	1.34	39.36	118.80
598	44.71	53.44	0.86	1.34	33.96	119.33
599	44.85	58.80	0.98	1.34	32.04	120.04
600	44.95	57.69	1.13	1.34	32.93	120.75
601	45.09	55.36	1.15	1.34	35.03	121.01
602	45.19	51.82	1.14	1.34	38.27	120.75
603	45.33	43.02	1.11	1.34	43.45	120.27
604	45.42	35.42	1.09	1.34	49.18	119.55
605	45.57	33.00	0.99	1.34	51.89	118.90
606	45.68	34.11	0.92	1.34	52.37	118.05
607	45.81	30.57	0.81	1.34	52.39	116.56
608	45.92	26.62	0.54	1.34	59.16	115.42
609	46.05	22.37	0.69	1.34	66.42	114.50
610	46.16	17.81	0.67	1.24	75.25	114.63
611	46.17	17.71	0.67	1.24	79.56	114.21
612	46.23	17.61	0.63	1.24	79.66	113.87
613	46.29	17.00	0.59	1.24	80.53	113.32
614	46.34	15.89	0.55	1.24	81.48	112.46
615	46.42	15.18	0.46	1.24	81.87	111.41
616	46.48	14.78	0.40	1.24	80.78	110.31
617	46.52	14.68	0.36	1.24	79.61	109.48
618	46.60	14.57	0.33	1.24	78.79	108.88
619	46.67	14.37	0.32	1.24	78.01	108.41
620	46.74	14.47	0.30	1.24	77.35	108.06
621	46.82	14.47	0.29	1.24	76.73	107.71
622	46.88	14.27	0.28	1.34	77.13	107.41
623	46.96	13.76	0.27	1.34	77.21	107.25
624	47.06	14.22	0.27	1.34	77.78	107.20

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	47.15	13.87	0.27	1.34	77.74	107.41
626	47.24	14.17	0.29	1.34	79.57	108.74
627	47.35	15.18	0.43	1.34	80.06	111.84
628	47.49	19.13	0.74	1.34	72.80	113.76
629	47.58	24.70	0.62	1.34	64.43	115.05
630	47.73	28.44	0.64	1.34	60.58	115.11
631	47.83	24.90	0.71	1.34	59.52	115.49
632	47.87	27.78	0.69	1.34	61.47	115.59
633	47.89	25.81	0.69	1.34	59.88	115.52
634	47.94	27.13	0.67	1.34	60.12	115.37
635	48.02	26.92	0.66	1.34	59.63	115.28
636	48.07	26.32	0.66	1.34	60.36	115.24
637	48.12	25.91	0.67	1.34	61.69	115.43
638	48.18	25.61	0.72	1.34	63.36	115.65
639	48.26	24.70	0.74	1.34	64.74	115.83
640	48.31	24.65	0.73	1.34	65.22	115.64
641	48.38	24.39	0.68	1.34	64.33	115.21
642	48.46	24.59	0.62	1.34	62.61	114.59
643	48.52	25.10	0.57	1.34	61.59	113.83
644	48.60	23.48	0.50	1.34	62.06	112.77
645	48.68	20.85	0.41	1.34	65.40	111.58
646	48.74	17.91	0.39	1.34	70.58	110.53
647	48.82	15.79	0.38	1.34	77.29	109.90
648	48.89	14.07	0.36	1.34	82.02	109.37
649	48.99	13.76	0.34	1.34	84.26	108.81
650	49.05	13.56	0.31	1.34	83.16	108.02
651	49.12	13.56	0.26	1.34	81.66	107.12
652	49.18	13.36	0.24	1.34	79.51	106.27
653	49.27	13.66	0.22	1.34	77.50	105.79
654	49.32	14.17	0.21	1.34	75.79	105.36
655	49.42	13.87	0.20	1.43	76.97	105.08
656	49.48	12.55	0.20	1.43	78.75	104.88
657	49.56	12.85	0.21	1.43	79.72	105.05
658	49.66	13.56	0.21	1.43	79.61	105.56
659	49.76	13.36	0.25	1.43	78.83	106.06
660	49.85	14.07	0.25	1.43	75.45	105.30
661	49.99	14.68	0.14	1.43	70.32	104.44
662	50.09	15.79	0.17	1.43	70.12	103.40
663	50.21	12.75	0.18	1.43	73.69	103.83
664	50.24	12.85	0.18	1.53	76.33	103.72
665	50.29	13.97	0.17	1.53	74.08	103.47
666	50.38	13.87	0.15	1.53	73.00	103.13
667	50.47	13.16	0.15	1.53	73.91	102.86
668	50.52	13.06	0.15	1.62	75.96	102.88
669	50.62	12.65	0.16	1.62	76.35	103.11
670	50.66	13.26	0.17	1.62	76.26	103.37
671	50.76	13.46	0.17	1.62	76.25	103.65
672	50.83	13.06	0.18	1.62	73.88	104.35

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	50.91	15.79	0.21	1.62	75.06	105.23
674	51.00	13.97	0.24	1.62	71.94	106.28
675	51.06	17.00	0.25	1.62	67.88	107.32
676	51.15	21.05	0.29	1.62	69.95	108.74
677	51.24	14.88	0.40	1.62	78.64	110.36
678	51.31	13.06	0.52	1.62	100.00	111.65
679	51.39	10.63	0.63	1.62	79.74	113.89
680	51.48	31.88	0.71	1.72	52.10	116.37
681	51.58	53.85	0.83	1.72	50.39	117.73
682	51.68	20.34	1.00	1.72	65.78	117.82
683	51.77	9.21	0.95	1.72	93.85	117.60
684	51.90	23.89	1.17	1.72	59.97	121.42
685	52.01	77.23	2.02	1.72	34.57	125.62
686	52.11	122.06	2.62	1.82	24.20	130.24
687	52.26	186.13	4.47	1.91	20.87	132.32
688	52.30	177.33	4.12	1.91	16.50	133.89
689	52.33	263.97	4.17	2.01	12.89	134.16
690	52.35	303.94	4.21	2.01	9.58	134.71
691	52.40	340.79	4.23	2.10	7.60	135.11
692	52.45	397.77	4.28	2.10	6.58	135.59
693	52.50	405.87	4.66	2.10	5.88	136.22
694	52.55	443.01	5.01	2.20	5.51	137.00
695	52.60	493.01	5.46	2.29	4.93	137.28
696	52.65	523.48	5.64	2.29	4.29	137.28
697	52.71	531.47	4.88	2.29	3.82	137.28
698	52.77	538.36	4.91	2.39	3.33	137.17
699	52.82	555.56	4.74	2.48	2.92	137.04
700	52.88	581.47	4.49	2.48	2.56	137.02
701	52.93	597.26	4.71	2.48	2.35	137.05
702	52.98	597.36	4.69	2.68	2.26	137.26
703	53.03	622.36	4.79	2.77	2.29	137.28
704	53.08	606.07	4.93	2.77	2.33	137.28
705	53.12	596.25	4.80	2.87	2.35	137.28
706	53.17	600.60	4.53	2.96	2.30	137.12
707	53.23	597.67	4.62	2.96	2.17	136.97
708	53.28	603.74	4.51	2.96	2.36	137.15
709	53.37	587.14	4.91	2.96	2.61	137.28
710	53.42	574.49	5.08	2.96	2.84	137.28
711	53.46	590.58	5.02	3.06	3.06	137.28
712	53.53	595.24	5.73	3.06	3.30	137.28
713	53.61	611.13	6.49	3.15	3.78	137.28
714	53.62	585.52	6.56	3.15	4.29	137.28
715	53.65	550.00	6.65	3.15	4.43	137.28
716	53.67	586.48	6.45	3.15	4.49	137.28
717	53.70	577.42	6.61	3.15	4.24	137.28
718	53.74	587.44	6.53	3.25	4.32	137.28
719	53.76	583.50	6.67	3.25	4.30	137.28
720	53.80	580.36	6.60	3.35	4.27	137.28

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	53.84	579.25	6.26	3.35	4.16	137.28
722	53.90	573.68	6.10	3.54	4.02	137.28
723	53.91	581.62	6.13	3.54	4.14	137.28
724	53.95	555.16	6.20	3.35	4.11	137.28
725	53.96	584.00	6.20	3.54	4.03	137.28
726	53.98	600.50	6.20	3.35	3.69	137.28
727	53.99	618.52	6.20	3.54	3.66	137.28
728	54.01	589.67	6.20	3.54	3.83	137.28
729	54.02	568.11	6.20	3.54	4.04	137.28
730	54.03	580.06	6.20	3.44	4.51	137.28
731	54.04	511.13	6.23	3.44	5.55	137.28
732	54.05	423.17	6.26	3.44	7.02	137.28
733	54.09	422.06	6.38	3.44	8.01	137.28
734	54.10	422.52	6.39	3.44	8.11	137.28
735	54.13	420.04	6.40	3.44	8.10	137.28
736	54.14	422.97	6.38	3.54	8.17	137.28
737	54.19	419.73	6.47	3.54	8.19	137.28
738	54.19	425.60	6.59	3.54	8.13	137.28
739	54.24	440.89	6.74	3.54	7.58	137.28
740	54.29	451.01	5.95	3.63	6.38	137.28
741	54.33	478.84	4.90	3.63	4.97	137.18
742	54.38	492.30	4.37	3.73	3.90	136.44
743	54.39	513.56	4.28	3.73	3.34	136.18
744	54.43	532.08	4.28	3.82	3.17	136.44
745	54.48	541.59	4.69	3.92	2.05	135.02
746	54.52	555.46	1.86	4.01	1.07	133.52
747	54.58	572.77	2.20	4.01	0.00	131.47
748	54.62	593.21	2.48	4.01	0.17	132.34
749	54.65	595.24	2.63	4.11	0.34	133.29
750	54.67	624.69	3.14	4.21	0.41	134.02
751	54.71	649.89	3.25	4.30	0.23	134.52
752	54.77	699.69	3.10	4.30	0.00	132.94
753	54.81	688.25	1.22	4.40	0.00	131.29
754	54.85	720.84	1.65	4.49	0.00	129.34
755	54.86	702.93	1.70	4.49	0.00	130.17
756	54.87	703.44	1.76	4.01	0.00	130.82
757	54.91	703.44	2.13	4.01	0.00	131.80
758	54.96	703.94	2.50	4.11	0.00	132.67
759	55.00	713.86	2.56	4.21	0.00	133.08
760	55.01	691.59	2.56	4.30	0.00	133.14
761	55.05	681.88	2.60	4.30	0.00	133.23
762	55.10	663.66	2.72	4.30	0.00	133.31
763	55.12	607.48	2.75	4.30	0.35	133.29
764	55.13	539.98	2.77	3.82	0.72	133.17
765	55.14	565.28	2.75	3.82	0.76	133.02
766	55.19	583.90	2.62	3.92	0.54	132.92
767	55.20	581.37	2.60	3.92	0.51	132.84
768	55.25	563.36	2.67	3.92	0.76	132.97

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	55.29	541.49	2.82	3.92	1.13	133.28
770	55.33	533.19	3.02	3.82	1.75	133.67
771	55.38	484.21	3.29	3.82	3.14	134.78
772	55.48	425.91	4.60	3.73	4.92	135.85
773	55.57	407.69	5.12	3.82	6.63	136.68
774	55.63	400.40	5.18	3.73	8.12	137.28
775	55.72	386.03	6.83	3.82	8.85	137.28
776	55.80	419.53	7.09	3.92	8.57	137.28
777	55.86	487.55	7.03	3.92	5.58	137.28
778	55.97	534.41	2.93	4.01	2.94	135.99
779	56.01	561.43	2.52	4.11	0.84	133.07
780	56.06	585.62	2.75	4.11	2.80	133.29
781	56.11	616.29	3.05	4.21	2.89	134.29
782	56.15	637.24	3.61	4.21	2.94	135.21
783	56.20	668.42	3.85	4.21	3.11	136.08
784	56.27	676.92	4.26	4.21	3.34	136.55
785	56.27	643.97	4.36	3.54	3.72	137.19
786	56.30	671.45	5.00	3.63	4.59	137.28
787	56.33	611.03	5.86	3.63	4.98	137.28
788	56.35	665.99	5.93	3.73	5.33	137.28
789	56.40	665.78	6.04	3.73	5.05	137.28
790	56.41	671.65	6.02	3.73	5.04	137.28
791	56.44	670.44	5.96	3.73	4.83	137.28
792	56.49	702.32	5.96	4.01	4.63	137.28
793	56.54	712.65	6.04	4.01	4.51	137.28
794	56.58	737.34	6.69	4.01	4.47	137.28
795	56.59	761.53	6.82	4.01	4.50	137.28
796	56.64	751.51	6.82	4.11	4.44	137.28
797	56.69	758.80	6.82	4.11	4.36	137.28
798	56.73	783.90	6.89	4.11	4.18	137.28
799	56.78	791.59	6.79	4.01	4.03	137.28
800	56.83	760.01	6.22	3.92	4.01	137.28
801	56.88	726.82	5.89	3.92	4.11	137.28
802	56.89	708.40	5.80	3.92	4.29	137.28
803	56.95	691.29	5.71	3.92	4.27	137.28
804	57.01	677.73	5.02	3.92	4.25	137.28
805	57.07	634.81	4.55	3.92	4.06	137.16
806	57.11	625.10	4.12	3.92	3.10	134.76
807	57.17	598.27	1.33	3.92	2.28	132.45
808	57.26	572.36	1.93	3.92	1.15	128.54
809	57.31	551.41	1.12	3.82	1.89	129.56
810	57.37	517.20	2.07	3.92	2.19	129.21
811	57.45	491.70	1.77	3.82	3.04	129.89
812	57.51	461.74	1.72	3.92	3.56	129.21
813	57.53	400.30	1.71	3.44	4.16	128.95
814	57.59	402.43	1.70	3.35	4.63	128.80
815	57.63	401.31	1.70	3.35	4.68	128.76
816	57.68	393.01	1.70	3.35	4.88	128.72

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	57.73	380.06	1.70	3.35	5.00	128.66
818	57.78	386.23	1.69	3.25	5.00	128.45
819	57.86	370.64	1.59	3.25	5.00	127.83
820	57.92	322.87	1.37	3.25	5.00	127.38
821	57.98	285.32	1.55	3.15	5.00	126.34
822	58.06	264.17	1.14	3.15	8.62	126.17
823	58.12	240.38	1.42	3.06	10.36	126.82
824	58.21	224.09	2.06	3.06	12.69	127.74
825	58.26	202.63	1.92	2.96	14.68	128.10
826	58.35	186.44	1.85	2.87	16.91	127.69
827	58.41	151.92	1.98	2.77	18.65	126.15
828	58.50	126.31	1.07	2.77	22.32	124.42
829	58.56	90.18	1.13	2.68	25.70	122.30
830	58.64	77.93	1.17	2.68	32.24	121.95
831	58.73	65.49	1.17	2.58	38.56	121.50
832	58.80	47.47	1.15	2.58	46.17	120.90
833	58.84	40.28	1.14	2.58	53.64	120.39
834	58.85	38.87	1.15	2.10	52.29	120.54
835	58.93	52.12	1.18	2.10	46.67	120.88
836	58.98	60.42	1.13	2.10	41.28	121.05
837	59.02	61.74	1.07	2.01	38.75	120.92
838	59.12	63.06	1.05	2.01	37.78	120.90
839	59.17	65.28	1.10	1.91	37.23	121.24
840	59.27	67.81	1.19	1.91	37.05	121.75
841	59.31	68.83	1.26	1.82	37.57	122.15
842	59.41	66.19	1.29	1.82	39.18	122.16
843	59.46	59.41	1.25	1.72	42.47	121.59
844	59.55	48.28	1.11	1.72	47.58	120.51
845	59.65	38.56	0.98	1.62	52.69	118.45
846	59.70	32.08	0.61	1.62	56.48	116.90
847	59.80	32.03	0.70	1.62	57.81	115.98
848	59.89	32.03	0.75	1.62	59.47	116.71
849	59.94	31.98	0.83	1.53	62.29	117.23
850	60.01	29.05	0.89	1.53	64.42	117.61
851	60.02	29.96	0.90	1.05	61.57	118.05
852	60.08	38.87	0.92	1.05	57.81	118.31
853	60.12	37.75	0.91	1.05	56.24	118.23
854	60.17	33.00	0.85	1.05	59.45	117.26
855	60.27	27.83	0.68	0.96	63.29	115.67
856	60.31	24.80	0.53	0.96	66.90	113.84
857	60.37	21.76	0.47	0.96	69.47	112.16
858	60.46	20.04	0.38	0.96	70.56	111.08
859	60.51	20.95	0.36	0.96	68.92	110.12
860	60.61	21.25	0.32	0.96	66.37	109.76
861	60.65	22.06	0.32	0.96	64.85	109.53
862	60.75	22.17	0.33	0.96	64.20	109.61
863	60.81	22.27	0.33	0.96	64.08	109.63
864	60.89	22.27	0.33	0.96	63.94	109.50

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	60.94	22.06	0.31	0.96	63.62	109.62
866	61.03	22.98	0.34	0.96	63.91	109.95
867	61.09	22.77	0.37	0.96	64.04	110.05
868	61.19	22.17	0.32	0.96	64.33	109.85
869	61.24	22.17	0.32	0.96	62.81	109.78
870	61.33	24.49	0.35	0.96	60.69	110.44
871	61.38	26.82	0.39	0.96	65.07	112.24
872	61.47	21.25	0.62	0.96	71.67	113.99
873	61.53	21.36	0.74	0.96	79.17	115.51
874	61.62	22.98	0.84	0.96	67.75	116.60
875	61.70	38.46	0.78	0.96	49.71	119.32
876	61.77	71.96	1.30	0.96	39.07	122.50
877	61.86	89.98	1.86	1.05	35.53	124.72
878	61.95	83.91	1.82	0.96	37.04	125.34
879	61.97	69.13	1.75	0.96	40.15	124.80
880	62.01	64.78	1.66	0.76	44.89	124.10
881	62.10	53.14	1.59	0.96	50.12	122.90
882	62.24	38.56	1.26	0.86	45.56	121.95
883	62.34	74.49	1.03	0.96	29.67	122.37
884	62.49	150.00	1.24	1.05	20.54	123.30
885	62.54	158.20	1.26	1.05	16.26	124.73
886	62.66	185.32	1.44	1.05	14.83	125.34
887	62.74	200.61	1.45	1.05	13.53	125.96
888	62.87	213.05	1.49	1.05	12.71	126.26
889	62.92	221.25	1.54	1.05	12.47	126.53
890	63.03	217.20	1.57	1.05	12.52	126.76
891	63.15	219.03	1.63	1.15	12.78	126.94
892	63.26	217.91	1.66	1.15	13.29	127.02
893	63.37	202.33	1.66	1.15	13.86	126.99
894	63.45	199.80	1.66	1.15	13.98	126.43
895	63.54	198.28	1.34	1.15	13.43	125.53
896	63.61	194.63	1.14	1.15	13.55	124.83
897	63.69	177.93	1.33	1.15	15.16	124.41
898	63.79	143.52	1.25	1.15	19.52	124.50
899	63.89	103.64	1.44	1.15	24.98	122.85
900	63.98	71.25	0.85	1.15	33.14	121.18
901	64.07	50.71	0.88	1.15	41.48	118.58
902	64.15	37.45	0.76	1.15	52.38	117.41
903	64.23	29.15	0.71	1.15	63.17	116.21
904	64.26	23.28	0.70	1.15	71.64	115.56
905	64.29	22.98	0.70	1.43	74.94	115.28
906	64.33	24.39	0.67	1.43	73.52	114.50
907	64.43	22.67	0.50	1.43	71.96	113.44
908	64.47	21.86	0.45	1.53	70.64	112.07
909	64.53	22.27	0.41	1.53	70.50	111.44
910	64.62	21.25	0.40	1.53	73.02	110.99
911	64.72	18.22	0.40	1.53	77.07	110.67
912	64.78	17.81	0.39	1.53	81.00	110.63

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	64.86	17.91	0.41	1.53	81.31	111.04
914	64.96	18.83	0.47	1.62	81.88	112.08
915	65.06	19.53	0.57	1.62	82.82	113.03
916	65.11	19.23	0.60	1.62	84.86	113.77
917	65.21	18.83	0.64	1.62	87.03	114.04
918	65.31	18.42	0.64	1.62	88.72	114.06
919	65.40	18.02	0.62	1.62	86.96	113.18
920	65.50	18.32	0.43	1.62	82.58	111.98
921	65.58	19.33	0.38	1.62	77.73	110.66
922	65.68	19.33	0.38	1.72	76.23	110.07
923	65.78	18.42	0.34	1.72	80.14	109.58
924	65.84	15.18	0.33	1.72	84.20	109.11
925	65.86	15.54	0.33	1.72	87.64	108.93
926	65.87	15.89	0.33	1.72	83.53	109.02
927	65.98	18.02	0.33	1.72	80.56	109.07
928	66.10	17.81	0.33	1.72	79.47	109.53
929	66.21	17.61	0.38	1.72	79.99	110.29
930	66.34	19.13	0.43	1.72	79.70	110.56
931	66.48	18.62	0.36	1.72	78.52	110.82
932	66.62	19.18	0.42	1.72	79.48	110.40
933	66.68	17.51	0.38	1.72	80.06	110.93
934	66.87	19.23	0.44	1.82	82.16	112.09
935	66.96	19.94	0.62	1.82	85.60	113.68
936	67.11	18.22	0.72	1.82	91.78	114.55
937	67.21	16.50	0.70	1.82	96.41	113.97
938	67.35	15.69	0.52	1.82	96.63	113.04
939	67.45	16.40	0.51	1.82	100.00	114.17
940	67.59	16.30	0.99	1.82	74.11	118.15
941	67.68	49.49	1.42	1.82	36.45	123.51
942	67.83	166.29	1.89	1.91	19.64	126.78
943	67.92	263.46	1.98	1.91	12.65	128.48
944	68.02	293.92	1.94	1.91	10.42	129.17
945	68.07	292.10	2.13	2.01	9.92	129.67
946	68.16	310.93	2.28	2.01	9.66	129.78
947	68.26	313.97	1.99	2.01	9.50	129.92
948	68.35	307.79	2.22	2.01	9.90	130.20
949	68.45	301.41	2.56	2.01	10.63	130.56
950	68.55	290.58	2.39	2.01	11.31	130.75
951	68.65	282.39	2.48	2.01	12.31	130.45
952	68.78	242.10	2.43	2.01	13.49	130.30
953	68.78	236.18	2.41	2.01	14.48	130.04
954	68.79	236.18	2.38	2.01	14.61	129.83
955	68.83	230.26	2.26	2.10	13.84	129.35
956	68.93	246.56	1.93	2.20	12.61	128.54
957	68.98	254.15	1.63	2.20	11.06	127.54
958	69.04	259.82	1.45	2.20	10.24	126.83
959	69.12	259.31	1.45	2.20	10.05	126.69
960	69.22	258.60	1.54	2.29	10.33	126.73

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	69.28	248.07	1.50	2.29	10.73	126.58
962	69.36	236.43	1.40	2.29	11.11	126.14
963	69.45	227.63	1.34	2.29	11.72	125.57
964	69.60	206.58	1.26	2.29	12.39	125.02
965	69.70	196.05	1.19	2.29	13.09	124.55
966	69.80	191.80	1.17	2.29	13.36	124.31
967	69.89	192.31	1.17	2.29	13.46	124.27
968	69.98	192.00	1.18	2.39	13.63	124.23
969	70.08	186.03	1.17	2.39	14.12	123.79
970	70.18	167.51	1.02	2.39	16.36	123.38
971	70.32	125.81	1.13	2.39	21.31	122.57
972	70.42	79.55	1.08	2.29	30.56	121.25
973	70.54	47.47	0.86	2.29	44.49	118.96
974	70.66	28.34	0.70	2.29	62.02	116.28
975	70.75	19.64	0.59	2.29	75.05	114.30
976	70.80	22.47	0.52	2.48	75.37	112.45
977	70.89	23.18	0.33	2.48	68.76	110.56
978	70.99	22.17	0.25	2.48	64.60	108.11
979	71.08	21.56	0.21	2.48	63.51	106.54
980	71.17	21.05	0.19	2.58	62.68	105.76
981	71.23	21.56	0.19	2.58	63.23	105.32
982	71.33	20.04	0.18	2.58	62.20	104.96
983	71.42	21.56	0.16	2.58	59.64	104.34
984	71.52	23.48	0.14	2.58	56.37	103.78
985	71.58	23.28	0.14	2.58	56.41	104.37
986	71.67	22.77	0.19	2.58	59.63	105.94
987	71.81	22.47	0.26	2.68	62.96	107.28
988	71.82	22.06	0.26	2.68	64.77	107.94
989	71.86	22.06	0.26	2.68	65.57	107.99
990	71.91	21.66	0.26	2.68	65.98	108.01
991	71.97	21.66	0.26	2.68	66.78	108.09
992	72.05	21.36	0.27	2.68	67.69	108.22
993	72.10	20.95	0.28	2.68	68.75	108.41
994	72.20	20.95	0.29	2.68	69.45	108.55
995	72.25	20.95	0.29	2.77	70.00	108.81
996	72.34	20.95	0.31	2.77	70.88	109.34
997	72.44	21.25	0.35	2.77	72.30	109.98
998	72.53	20.95	0.38	2.77	74.03	110.47
999	72.63	20.34	0.39	2.77	74.87	110.69
1000	72.69	20.95	0.39	2.77	75.74	110.64
1001	72.82	20.04	0.38	2.77	75.05	110.60
1002	72.92	20.95	0.38	2.77	73.32	110.41
1003	73.06	22.27	0.35	2.87	70.40	110.34
1004	73.16	22.98	0.35	2.87	70.10	110.49
1005	73.30	21.66	0.39	2.87	74.63	110.57
1006	73.35	17.81	0.39	2.87	78.07	110.69
1007	73.38	20.04	0.39	2.87	79.92	110.48
1008	73.47	19.64	0.37	2.87	77.08	110.44

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1009	73.53	20.24	0.37	2.96	76.55	110.30
1010	73.62	20.24	0.36	2.96	76.12	110.24
1011	73.71	19.94	0.36	2.96	77.10	110.31
1012	73.77	19.53	0.38	2.96	79.03	110.64
1013	73.86	19.23	0.42	3.06	81.15	111.10
1014	73.96	19.13	0.45	3.06	82.23	111.57
1015	74.06	19.64	0.47	3.06	82.36	111.89
1016	74.13	19.84	0.48	3.06	81.49	112.15
1017	74.24	20.45	0.48	3.06	80.85	112.33
1018	74.34	20.65	0.50	3.06	80.73	112.54
1019	74.44	20.45	0.51	3.06	81.57	112.67
1020	74.58	20.04	0.51	3.06	81.41	112.52
1021	74.68	20.50	0.47	3.06	78.40	111.21
1022	74.80	20.24	0.27	3.15	74.93	109.94
1023	74.92	20.55	0.31	3.15	73.80	109.11
1024	75.07	19.84	0.36	3.15	75.92	109.75
1025	75.08	19.64	0.36	3.15	77.59	110.03
1026	75.11	19.64	0.36	3.25	78.16	110.07
1027	75.16	19.43	0.37	3.25	78.98	110.30
1028	75.25	19.43	0.39	3.25	80.91	110.74
1029	75.32	18.93	0.43	3.35	82.63	111.17
1030	75.40	18.93	0.44	3.35	83.61	111.30
1031	75.50	18.93	0.42	3.35	83.49	110.99
1032	75.59	18.42	0.38	3.35	83.68	110.27
1033	75.69	17.41	0.34	3.35	84.66	109.43
1034	75.78	16.70	0.31	3.35	85.61	108.57
1035	75.88	16.30	0.28	3.35	85.84	107.84
1036	75.96	16.09	0.26	3.35	85.52	107.10
1037	76.05	15.79	0.24	3.35	84.67	106.59
1038	76.14	16.09	0.23	3.44	84.37	106.31
1039	76.26	15.89	0.23	3.44	84.09	106.37
1040	76.36	16.09	0.24	3.44	84.42	106.50
1041	76.41	16.09	0.24	3.44	84.56	106.55
1042	76.51	15.89	0.23	3.44	85.32	106.38
1043	76.65	15.38	0.23	3.44	86.78	106.27
1044	76.72	15.08	0.24	3.44	88.00	106.27
1045	76.79	15.18	0.24	3.54	88.79	106.37
1046	76.89	15.08	0.24	3.54	90.66	107.25
1047	76.98	15.28	0.33	3.54	97.45	110.24
1048	77.08	15.89	0.64	3.54	92.62	112.89
1049	77.18	22.67	0.68	3.54	84.18	115.44
1050	77.28	27.83	0.85	3.54	77.43	117.59
1051	77.37	29.55	1.20	3.63	80.05	119.52
1052	77.42	26.11	1.45	3.63	81.77	120.82
1053	77.42	30.47	1.49	3.73	80.76	121.59
1054	77.44	33.91	1.59	3.73	75.56	122.42
1055	77.48	37.45	1.79	3.73	72.09	123.26
1056	77.52	40.69	1.91	3.82	69.21	123.98

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1057	77.54	43.52	1.97	3.82	67.19	124.41
1058	77.57	44.43	2.03	3.82	67.13	124.60
1059	77.62	42.00	2.05	3.82	68.46	124.53
1060	77.65	40.18	1.97	3.82	70.82	124.28
1061	77.67	37.96	1.92	3.82	71.65	123.83
1062	77.71	37.85	1.76	3.82	71.90	123.46
1063	77.71	37.75	1.73	3.73	71.69	122.88
1064	77.76	35.32	1.55	3.82	73.39	122.11
1065	77.81	31.07	1.35	3.73	75.70	120.92
1066	77.90	28.74	1.16	3.82	78.54	119.86
1067	77.95	27.13	1.11	3.82	80.91	119.27
1068	78.01	25.91	1.14	3.82	82.45	118.93
1069	78.10	25.81	1.05	3.82	78.83	118.74
1070	78.16	30.87	0.98	3.82	63.10	119.02
1071	78.24	52.02	0.97	3.92	49.66	119.64
1072	78.29	63.76	1.00	3.92	39.63	120.51
1073	78.39	78.54	1.05	3.92	34.27	121.15
1074	78.47	89.78	1.06	3.92	31.50	121.96
1075	78.53	93.42	1.23	3.92	31.16	123.05
1076	78.62	94.84	1.51	3.92	32.43	124.23
1077	78.68	94.33	1.70	3.92	34.74	124.97
1078	78.69	84.31	1.76	3.92	35.67	125.92
1079	78.78	100.10	2.16	3.92	36.75	126.73
1080	78.81	97.27	2.34	3.92	38.10	127.66
1081	78.92	87.04	2.58	3.92	41.97	127.53
1082	79.03	71.36	2.29	3.92	46.36	126.48
1083	79.16	59.92	1.72	3.92	46.07	125.04
1084	79.26	73.78	1.52	4.01	39.53	124.49
1085	79.35	101.31	1.66	4.01	33.43	125.47
1086	79.45	116.80	2.02	4.01	30.53	126.98
1087	79.54	125.00	2.38	4.01	29.73	128.12
1088	79.64	130.77	2.50	4.01	29.16	128.84
1089	79.74	137.75	2.60	4.11	26.56	130.21
1090	79.88	191.60	3.45	4.21	23.02	131.59
1091	79.98	231.27	3.61	4.21	19.11	132.52
1092	80.12	263.76	3.19	4.21	17.02	132.38
1093	80.22	251.11	2.99	4.21	15.38	131.25
1094	80.36	244.53	2.16	4.21	14.66	129.87
1095	80.46	238.56	1.83	4.21	13.44	128.07
1096	80.60	233.20	1.51	4.21	12.69	126.55
1097	80.70	223.58	1.18	4.21	12.64	125.70
1098	80.83	214.78	1.39	4.30	13.47	125.59
1099	80.94	200.81	1.51	4.30	15.55	125.88
1100	81.01	167.71	1.47	4.21	17.35	125.78
1101	81.04	165.18	1.46	4.40	18.79	125.42
1102	81.09	159.61	1.41	4.40	19.43	125.22
1103	81.13	150.30	1.41	4.40	20.68	125.10
1104	81.18	138.66	1.47	4.40	23.02	125.16

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1105	81.23	121.46	1.58	4.40	26.12	125.34
1106	81.28	109.61	1.68	4.40	29.84	125.42
1107	81.33	96.96	1.71	4.40	33.69	125.60
1108	81.37	87.75	1.89	4.40	38.07	125.99
1109	81.42	80.57	2.17	4.40	42.18	126.42
1110	81.47	75.20	2.23	4.40	45.53	126.65
1111	81.52	71.36	2.25	4.40	47.80	126.68
1112	81.56	69.23	2.31	4.40	48.75	126.82
1113	81.61	72.17	2.40	4.40	49.37	126.98
1114	81.64	70.14	2.41	4.40	50.62	127.02
1115	81.70	63.87	2.40	4.40	54.71	126.72
1116	81.75	52.33	2.36	4.40	60.30	126.26
1117	81.79	46.76	2.28	4.40	66.56	125.58
1118	81.82	41.40	2.11	4.40	70.87	124.78
1119	81.86	37.35	1.89	4.40	74.63	123.79
1120	81.91	33.91	1.69	4.40	77.94	122.73
1121	81.95	30.57	1.50	4.40	81.32	121.53
1122	82.00	27.23	1.28	4.40	84.85	120.08
1123	82.09	23.99	1.02	4.40	88.86	118.54
1124	82.15	21.36	0.91	4.40	93.55	117.24
1125	82.19	19.43	0.86	4.49	97.46	116.22
1126	82.26	18.52	0.73	4.49	100.00	115.23
1127	82.34	17.00	0.65	4.49	100.00	114.22
1128	82.39	15.28	0.62	4.49	100.00	113.42
1129	82.48	14.47	0.58	4.59	100.00	112.80
1130	82.58	14.37	0.53	4.59	100.00	112.31
1131	82.62	14.88	0.51	4.59	100.00	111.87
1132	82.70	14.78	0.48	4.59	100.00	111.60
1133	82.77	14.78	0.47	4.59	100.00	111.26
1134	82.87	14.68	0.45	4.59	100.00	111.18
1135	82.96	15.59	0.46	4.68	100.00	111.16
1136	83.06	18.22	0.44	4.68	90.71	111.46
1137	83.16	20.65	0.45	4.68	79.92	111.87
1138	83.25	25.10	0.46	4.78	72.16	112.31
1139	83.34	27.43	0.46	4.78	66.55	112.65
1140	83.44	28.85	0.46	4.87	65.23	113.13
1141	83.54	28.54	0.53	4.87	65.41	113.57
1142	83.64	28.64	0.54	4.87	66.63	114.00
1143	83.73	28.44	0.56	4.87	69.35	114.34
1144	83.83	25.81	0.63	4.87	71.50	114.84
1145	83.85	27.33	0.67	5.07	74.13	115.50
1146	83.89	27.13	0.74	5.07	74.39	116.20
1147	83.94	27.73	0.82	5.07	76.21	117.47
1148	84.04	29.25	1.08	5.07	76.59	118.57
1149	84.09	30.57	1.13	5.07	76.69	119.51
1150	84.13	31.17	1.19	5.07	76.09	119.96
1151	84.18	31.88	1.26	5.07	76.24	120.30
1152	84.25	31.78	1.29	5.07	77.16	120.50

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1153	84.33	30.67	1.30	5.07	79.11	120.53
1154	84.37	29.25	1.31	5.07	81.52	120.45
1155	84.46	28.24	1.30	5.16	83.35	120.16
1156	84.52	27.33	1.20	5.16	84.37	119.78
1157	84.57	26.72	1.15	5.16	84.59	119.32
1158	84.67	26.42	1.10	5.16	84.79	119.04
1159	84.71	26.21	1.08	5.16	85.52	118.94
1160	84.81	25.61	1.12	5.16	87.61	119.09
1161	84.86	24.70	1.19	5.16	90.53	119.33
1162	84.91	23.99	1.23	5.16	93.50	119.49
1163	85.00	23.28	1.24	5.16	95.77	119.52
1164	85.05	22.77	1.24	5.16	97.25	119.32
1165	85.15	22.17	1.16	5.16	97.82	118.97
1166	85.19	21.86	1.09	5.16	97.66	118.30
1167	85.29	21.15	0.96	5.16	97.29	117.62
1168	85.35	20.75	0.90	5.16	97.56	116.95
1169	85.42	20.04	0.86	5.16	98.84	116.52
1170	85.48	19.23	0.83	5.16	100.00	116.19
1171	85.55	18.72	0.81	5.26	100.00	115.89
1172	85.63	18.12	0.79	5.26	100.00	115.64
1173	85.68	17.51	0.78	5.26	100.00	115.45
1174	85.77	17.00	0.77	5.26	100.00	115.34
1175	85.82	16.80	0.77	5.26	100.00	115.39
1176	85.89	17.10	0.80	5.26	100.00	115.55
1177	85.96	18.12	0.81	5.26	100.00	115.74
1178	86.03	19.53	0.79	5.26	98.42	115.81
1179	86.11	21.25	0.76	5.26	92.88	115.75
1180	86.16	22.17	0.74	5.26	88.74	115.62
1181	86.25	22.67	0.72	5.26	89.87	115.47
1182	86.36	19.94	0.73	5.26	94.60	114.88
1183	86.50	17.10	0.62	5.26	100.00	114.26
1184	86.51	17.21	0.61	5.26	100.00	113.63
1185	86.52	17.21	0.60	5.26	100.00	113.28
1186	86.57	17.31	0.54	5.26	100.00	112.52
1187	86.65	17.31	0.44	5.35	96.58	111.56
1188	86.71	17.31	0.41	5.35	94.30	110.68
1189	86.80	17.21	0.38	5.35	94.07	110.11
1190	86.90	16.50	0.35	5.45	95.37	109.44
1191	86.99	15.49	0.32	5.45	97.33	108.73
1192	87.04	15.08	0.30	5.45	98.63	108.13
1193	87.14	14.98	0.28	5.45	98.41	107.81
1194	87.19	15.18	0.28	5.45	97.17	107.78
1195	87.28	15.69	0.29	5.54	95.63	108.26
1196	87.38	16.50	0.33	5.54	93.79	108.83
1197	87.43	17.10	0.34	5.54	91.88	109.36
1198	87.52	17.71	0.35	5.54	89.95	109.63
1199	87.61	18.22	0.36	5.64	88.28	109.78
1200	87.66	18.52	0.36	5.64	87.04	109.79

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1201	87.76	18.62	0.35	5.64	86.65	109.67
1202	87.84	18.32	0.34	5.64	86.71	109.46
1203	87.91	18.12	0.33	5.64	87.47	109.24
1204	88.00	17.71	0.32	5.64	88.37	109.00
1205	88.11	17.31	0.31	5.73	89.54	108.84
1206	88.19	17.10	0.31	5.73	90.39	108.72
1207	88.25	17.00	0.31	5.73	90.81	108.62
1208	88.34	16.90	0.30	5.73	90.64	108.42
1209	88.44	16.90	0.29	5.83	90.17	108.15
1210	88.54	16.90	0.28	5.83	89.58	107.90
1211	88.64	16.90	0.27	5.83	89.37	107.73
1212	88.72	16.80	0.27	5.93	89.61	107.69
1213	88.82	16.70	0.28	5.93	90.07	107.73
1214	88.91	16.70	0.28	5.93	90.83	107.82
1215	89.01	16.50	0.28	5.93	91.58	107.90
1216	89.10	16.40	0.29	5.93	92.45	107.97
1217	89.19	16.30	0.29	6.02	93.00	107.82
1218	89.30	15.99	0.27	6.02	91.00	106.79
1219	89.39	16.09	0.18	6.12	89.02	106.17
1220	89.49	16.60	0.23	6.12	88.22	106.44
1221	89.59	16.90	0.29	6.12	90.32	107.86
1222	89.69	16.95	0.32	6.12	91.89	108.72
1223	89.73	17.00	0.33	6.21	90.02	109.17
1224	89.78	18.83	0.34	6.31	87.19	109.42
1225	89.83	19.33	0.34	6.31	84.28	109.67
1226	89.88	19.64	0.35	6.31	83.80	109.89
1227	89.93	19.64	0.36	6.31	83.63	110.18
1228	90.00	20.04	0.38	6.40	83.30	110.59
1229	90.07	20.75	0.41	6.40	82.14	111.03
1230	90.12	21.56	0.42	6.40	81.06	111.60
1231	90.22	22.27	0.46	6.40	80.51	112.20
1232	90.27	22.67	0.50	6.40	80.53	113.17
1233	90.36	23.89	0.60	6.40	77.53	114.19
1234	90.46	28.14	0.65	6.50	73.54	115.05
1235	90.50	30.06	0.66	6.50	70.62	115.50
1236	90.61	29.35	0.68	6.59	70.53	115.62
1237	90.66	28.74	0.68	6.59	71.78	115.45
1238	90.75	27.73	0.63	6.59	73.00	114.95
1239	90.84	26.11	0.57	6.59	74.84	114.27
1240	90.89	24.39	0.54	6.59	76.93	113.58
1241	90.99	23.38	0.50	6.59	79.28	113.09
1242	91.04	22.37	0.49	6.69	81.25	112.68
1243	91.14	21.46	0.48	6.69	83.54	112.40
1244	91.22	20.65	0.47	6.79	85.84	112.13
1245	91.28	19.84	0.46	6.79	88.45	111.80
1246	91.37	18.72	0.44	6.79	89.92	111.48
1247	91.47	18.93	0.42	6.88	90.14	111.12
1248	91.61	19.03	0.40	6.88	88.70	110.98

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1249	91.71	19.53	0.41	6.88	88.08	110.93
1250	91.81	19.33	0.41	6.88	87.81	110.97
1251	91.87	19.33	0.41	6.98	88.02	110.84
1252	92.00	19.13	0.39	6.98	86.12	110.10
1253	92.10	19.38	0.29	6.98	84.52	109.49
1254	92.20	19.43	0.32	7.07	83.14	109.22
1255	92.33	19.74	0.35	7.07	83.97	109.76
1256	92.38	19.79	0.37	7.07	84.45	110.16
1257	92.43	19.84	0.37	7.26	84.47	110.37
1258	92.48	20.14	0.38	7.26	85.19	110.58
1259	92.56	19.64	0.40	7.36	86.02	110.74
1260	92.63	19.53	0.40	7.36	87.16	110.82
1261	92.67	19.43	0.40	7.36	87.45	110.81
1262	92.72	19.43	0.40	7.36	87.55	110.79
1263	92.77	19.43	0.40	7.36	87.20	110.81
1264	92.86	19.74	0.40	7.46	86.63	110.88
1265	92.92	20.04	0.41	7.46	86.16	111.05
1266	92.97	20.14	0.42	7.55	86.69	111.44
1267	93.05	20.14	0.46	7.55	87.17	111.82
1268	93.10	20.45	0.47	7.55	87.05	112.15
1269	93.16	20.95	0.48	7.55	85.70	112.28
1270	93.25	21.56	0.48	7.65	83.79	112.35
1271	93.35	22.27	0.47	7.65	80.44	112.40
1272	93.40	24.19	0.47	7.65	78.94	112.28
1273	93.49	22.77	0.45	7.74	78.47	112.15
1274	93.56	22.47	0.45	7.74	79.73	111.99
1275	93.64	22.57	0.45	7.74	79.38	112.05
1276	93.73	23.28	0.46	7.74	78.34	112.52
1277	93.83	24.70	0.52	7.84	76.63	113.28
1278	93.88	26.42	0.57	8.03	75.40	114.39
1279	93.97	27.83	0.67	8.03	75.84	115.13
1280	94.07	26.42	0.70	8.03	78.80	115.71
1281	94.17	24.70	0.75	8.03	82.08	116.26
1282	94.26	25.81	0.86	8.03	80.59	116.63
1283	94.36	29.25	0.79	8.03	81.16	117.93
1284	94.45	28.24	1.17	8.03	80.92	119.20
1285	94.55	30.57	1.33	8.12	72.58	120.82
1286	94.64	48.48	1.34	8.12	58.20	121.86
1287	94.72	65.99	1.33	8.03	49.16	122.39
1288	94.74	64.98	1.34	8.03	41.37	122.92
1289	94.77	90.28	1.36	8.31	37.18	123.45
1290	94.85	97.87	1.44	8.31	33.27	124.10
1291	94.90	103.54	1.52	8.31	32.34	124.67
1292	94.95	106.48	1.62	8.31	32.54	125.32
1293	95.01	105.57	1.83	8.31	34.52	126.41
1294	95.09	101.62	2.33	8.31	37.59	127.40
1295	95.14	94.94	2.54	8.31	42.18	128.49
1296	95.23	86.54	3.07	8.31	47.11	129.05

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1297	95.29	77.43	3.22	8.31	52.64	129.44
1298	95.38	69.84	3.34	8.31	57.15	129.42
1299	95.43	65.69	3.35	8.31	59.57	129.33
1300	95.52	66.70	3.28	8.31	59.18	129.26
1301	95.57	70.75	3.23	8.31	56.95	129.08
1302	95.67	72.87	2.99	8.31	55.03	128.58
1303	95.77	69.74	2.61	8.22	56.22	127.67
1304	95.86	56.58	2.39	8.22	62.27	126.89
1305	95.95	44.23	2.56	8.22	64.67	126.27
1306	96.03	57.64	2.16	8.22	71.02	125.95
1307	96.11	37.96	2.38	8.31	66.58	126.41
1308	96.20	58.70	2.78	8.51	62.59	127.77
1309	96.30	80.57	3.26	8.60	51.74	129.50
1310	96.39	100.81	3.60	8.60	44.40	130.84
1311	96.50	122.37	3.84	8.70	38.62	131.75
1312	96.59	145.34	3.92	8.60	32.42	131.58
1313	96.69	166.80	2.74	8.60	26.91	130.69
1314	96.78	182.08	2.25	8.60	22.17	129.05
1315	96.87	191.29	1.93	8.60	20.37	128.23
1316	96.98	184.11	1.94	8.60	20.02	127.84
1317	97.02	180.06	1.94	8.51	21.02	127.82
1318	97.06	168.82	2.00	8.70	21.61	128.14
1319	97.12	179.96	2.21	8.70	22.39	128.67
1320	97.16	177.63	2.41	8.70	23.05	129.34
1321	97.21	172.97	2.61	8.70	24.45	129.98
1322	97.27	170.04	2.93	8.60	25.91	130.63
1323	97.33	168.12	3.21	8.60	27.09	131.15
1324	97.40	166.09	3.29	8.60	27.88	131.39
1325	97.45	163.36	3.29	8.60	28.36	131.45
1326	97.50	161.94	3.32	8.60	29.21	131.67
1327	97.58	158.50	3.65	8.60	30.75	131.92
1328	97.65	146.66	3.76	8.51	32.97	132.07
1329	97.69	135.32	3.76	8.51	35.59	131.79
1330	97.74	120.95	3.57	8.51	38.21	131.25
1331	97.81	108.60	3.32	8.51	40.74	130.65
1332	97.88	101.62	3.24	8.51	42.61	130.19
1333	97.93	98.68	3.18	8.60	40.27	130.07
1334	98.03	125.30	2.99	8.79	31.75	130.21
1335	98.15	191.80	2.67	9.08	23.53	130.24
1336	98.21	230.36	2.44	9.08	17.43	129.79
1337	98.32	262.75	1.96	9.08	13.84	129.24
1338	98.42	299.09	1.85	9.08	10.93	128.66
1339	98.47	343.32	1.71	9.08	5.00	127.75
1340	98.57	405.97	1.08	9.18	5.00	126.30
1341	98.70	416.60	0.89	9.18	4.53	124.66
1342	98.78	412.55	0.91	9.27	4.67	124.49
1343	98.85	382.49	1.03	9.27	5.00	124.66
1344	98.86	321.86	1.03	9.08	5.00	124.72

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1345	98.92	308.60	1.04	9.08	5.00	124.62
1346	98.98	337.35	1.04	9.18	5.00	124.75
1347	99.03	309.11	1.10	9.08	5.00	125.36
1348	99.11	281.37	1.35	8.98	5.00	126.14
1349	99.18	254.05	1.55	8.98	12.62	127.01
1350	99.23	230.16	1.76	8.89	15.59	128.18
1351	99.32	209.41	2.34	8.79	19.03	129.37
1352	99.37	189.57	2.77	8.79	22.90	130.41
1353	99.45	168.82	3.08	8.79	26.41	130.81
1354	99.56	152.93	3.11	8.79	29.20	131.00
1355	99.64	149.59	3.27	8.79	31.66	131.22
1356	99.71	139.27	3.58	8.79	34.06	131.59
1357	99.75	130.87	3.81	8.89	36.97	131.47
1358	99.90	114.27	3.39	8.79	40.25	131.23
1359	99.95	103.44	3.58	8.70	45.52	131.15
1360	100.04	87.25	4.17	8.70	42.09	132.11
1361	100.14	157.89	4.41	8.98	32.87	133.35
1362	100.14	232.39	4.40	8.98	26.10	134.08
1363	100.15	224.29	4.36	9.08	23.29	134.83
1364	100.19	250.30	5.18	9.18	22.57	136.06
1365	100.21	301.41	6.43	9.27	21.06	137.28
1366	100.24	342.10	7.12	9.27	14.70	135.60
1367	100.28	411.74	0.00	9.46	8.11	131.27
1368	100.31	477.42	0.00	9.56	N/A	87.36
1369	100.33	523.38	0.00	9.56	N/A	87.36
1370	100.38	524.49	0.00	9.56	N/A	87.36
1371	100.39	525.60	0.00	9.56	N/A	87.36
1372	100.43	529.15	0.00	9.65	N/A	87.36
1373	100.48	540.18	0.00	9.65	N/A	87.36
1374	100.53	496.96	0.00	9.56	N/A	87.36
1375	100.57	490.58	0.00	9.65	N/A	87.36
1376	100.60	500.40	0.00	9.94	N/A	87.36

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c:	Measured cone resistance (tsf)
f_s:	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.04	0.00	0.00	0.00	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
2	0.10	0.00	0.00	0.00	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
3	0.11	0.00	0.00	0.00	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
4	0.16	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
5	0.19	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
6	0.24	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
7	0.31	0.01	0.00	0.01	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
8	0.38	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
9	0.43	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
10	0.49	0.02	0.00	0.02	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
11	0.58	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
12	0.63	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
13	0.67	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	No
14	0.72	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
15	0.72	0.03	0.00	0.03	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
16	0.84	0.04	0.00	0.04	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
17	0.96	0.05	0.00	0.05	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
18	1.06	0.05	0.00	0.05	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
19	1.24	0.06	0.00	0.06	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
20	1.30	0.07	0.00	0.07	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
21	1.48	0.08	0.00	0.08	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
22	1.59	0.08	0.00	0.08	1.00	0.273	1.68	0.162	1.00	1.10	2.000	Yes
23	1.69	0.09	0.00	0.09	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
24	1.69	0.09	0.00	0.09	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
25	1.74	0.09	0.00	0.09	1.00	0.272	1.68	0.162	1.00	1.10	2.000	Yes
26	1.79	0.09	0.00	0.09	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
27	1.84	0.09	0.00	0.09	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
28	1.88	0.10	0.00	0.10	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
29	1.93	0.10	0.00	0.10	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
30	1.99	0.10	0.00	0.10	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
31	2.03	0.11	0.00	0.11	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
32	2.08	0.11	0.00	0.11	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
33	2.13	0.11	0.00	0.11	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
34	2.22	0.12	0.00	0.12	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
35	2.27	0.12	0.00	0.12	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
36	2.33	0.12	0.00	0.12	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
37	2.42	0.13	0.00	0.13	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
38	2.48	0.13	0.00	0.13	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
39	2.56	0.13	0.00	0.13	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
40	2.65	0.14	0.00	0.14	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
41	2.72	0.14	0.00	0.14	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
42	2.80	0.15	0.00	0.15	1.00	0.272	1.68	0.162	1.00	1.10	2.000	No
43	2.89	0.15	0.00	0.15	1.00	0.272	1.68	0.161	1.00	1.10	2.000	No
44	2.94	0.16	0.00	0.16	1.00	0.272	1.68	0.161	1.00	1.10	2.000	No
45	3.04	0.16	0.00	0.16	0.99	0.272	1.68	0.161	1.00	1.10	2.000	No
46	3.14	0.17	0.00	0.17	0.99	0.272	1.68	0.161	1.00	1.10	2.000	No
47	3.23	0.17	0.00	0.17	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
48	3.31	0.18	0.00	0.18	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	3.37	0.18	0.00	0.18	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
50	3.48	0.18	0.00	0.18	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
51	3.57	0.19	0.00	0.19	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
52	3.65	0.19	0.00	0.19	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
53	3.71	0.20	0.00	0.20	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
54	3.82	0.20	0.00	0.20	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
55	3.91	0.21	0.00	0.21	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
56	4.00	0.21	0.00	0.21	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
57	4.10	0.22	0.00	0.22	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
58	4.19	0.22	0.00	0.22	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
59	4.26	0.23	0.00	0.23	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
60	4.35	0.23	0.00	0.23	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
61	4.44	0.23	0.00	0.23	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
62	4.52	0.24	0.00	0.24	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
63	4.53	0.24	0.00	0.24	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
64	4.58	0.24	0.00	0.24	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
65	4.63	0.24	0.00	0.24	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
66	4.68	0.25	0.00	0.25	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
67	4.72	0.25	0.00	0.25	0.99	0.271	1.68	0.161	1.00	1.10	2.000	No
68	4.77	0.25	0.00	0.25	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
69	4.82	0.26	0.00	0.26	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
70	4.88	0.26	0.00	0.26	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
71	4.96	0.26	0.00	0.26	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
72	5.01	0.27	0.00	0.27	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
73	5.08	0.27	0.00	0.27	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
74	5.16	0.27	0.00	0.27	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
75	5.21	0.28	0.00	0.28	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
76	5.30	0.28	0.00	0.28	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
77	5.37	0.29	0.00	0.29	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
78	5.45	0.29	0.00	0.29	0.99	0.270	1.68	0.161	1.00	1.10	2.000	No
79	5.52	0.29	0.00	0.29	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
80	5.59	0.30	0.00	0.30	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
81	5.65	0.30	0.00	0.30	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
82	5.74	0.31	0.00	0.31	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
83	5.83	0.31	0.00	0.31	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
84	5.89	0.31	0.00	0.31	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
85	5.97	0.32	0.00	0.32	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
86	6.07	0.32	0.00	0.32	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
87	6.12	0.33	0.00	0.33	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
88	6.22	0.33	0.00	0.33	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
89	6.28	0.34	0.00	0.34	0.99	0.270	1.68	0.160	1.00	1.10	2.000	No
90	6.36	0.34	0.00	0.34	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
91	6.46	0.35	0.00	0.35	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
92	6.52	0.35	0.00	0.35	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
93	6.60	0.35	0.00	0.35	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
94	6.70	0.36	0.00	0.36	0.99	0.269	1.68	0.160	1.00	1.10	2.000	No
95	6.76	0.36	0.00	0.36	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
96	6.84	0.37	0.00	0.37	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	6.94	0.37	0.00	0.37	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
98	7.03	0.38	0.00	0.38	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
99	7.13	0.38	0.00	0.38	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
100	7.19	0.38	0.00	0.38	0.99	0.269	1.68	0.160	1.00	1.10	2.000	Yes
101	7.32	0.39	0.00	0.39	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
102	7.42	0.39	0.00	0.39	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
103	7.49	0.40	0.00	0.40	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
104	7.57	0.40	0.00	0.40	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
105	7.66	0.40	0.00	0.40	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
106	7.76	0.41	0.00	0.41	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
107	7.77	0.41	0.00	0.41	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
108	7.78	0.41	0.00	0.41	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
109	7.82	0.41	0.00	0.41	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
110	7.87	0.41	0.00	0.41	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
111	7.92	0.42	0.00	0.42	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
112	7.97	0.42	0.00	0.42	0.98	0.269	1.68	0.160	1.00	1.10	2.000	No
113	8.01	0.42	0.00	0.42	0.98	0.268	1.68	0.160	1.00	1.10	2.000	No
114	8.06	0.42	0.00	0.42	0.98	0.268	1.68	0.160	1.00	1.10	2.000	No
115	8.11	0.42	0.00	0.42	0.98	0.268	1.68	0.160	1.00	1.10	2.000	No
116	8.20	0.43	0.00	0.43	0.98	0.268	1.68	0.160	1.00	1.10	2.000	No
117	8.26	0.43	0.00	0.43	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
118	8.35	0.44	0.00	0.44	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
119	8.40	0.44	0.00	0.44	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
120	8.49	0.44	0.00	0.44	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
121	8.54	0.44	0.00	0.44	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
122	8.64	0.45	0.00	0.45	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
123	8.69	0.45	0.00	0.45	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
124	8.79	0.46	0.00	0.46	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
125	8.84	0.46	0.00	0.46	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
126	8.93	0.46	0.00	0.46	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
127	9.03	0.47	0.00	0.47	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
128	9.08	0.47	0.00	0.47	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
129	9.11	0.47	0.00	0.47	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
130	9.12	0.47	0.00	0.47	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
131	9.17	0.48	0.00	0.48	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
132	9.22	0.48	0.00	0.48	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
133	9.31	0.48	0.00	0.48	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
134	9.36	0.49	0.00	0.49	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
135	9.40	0.49	0.00	0.49	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
136	9.46	0.49	0.00	0.49	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
137	9.51	0.49	0.00	0.49	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
138	9.55	0.50	0.00	0.50	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
139	9.61	0.50	0.00	0.50	0.98	0.268	1.68	0.159	1.00	1.10	2.000	No
140	9.69	0.50	0.00	0.50	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
141	9.74	0.51	0.00	0.51	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
142	9.81	0.51	0.00	0.51	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
143	9.89	0.51	0.00	0.51	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
144	9.94	0.52	0.00	0.52	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	10.03	0.52	0.00	0.52	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
146	10.08	0.52	0.00	0.52	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
147	10.18	0.53	0.00	0.53	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
148	10.23	0.53	0.00	0.53	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
149	10.33	0.54	0.00	0.54	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
150	10.40	0.54	0.00	0.54	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
151	10.47	0.54	0.00	0.54	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
152	10.51	0.55	0.00	0.55	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
153	10.56	0.55	0.00	0.55	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
154	10.61	0.55	0.00	0.55	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
155	10.67	0.55	0.00	0.55	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
156	10.75	0.56	0.00	0.56	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
157	10.80	0.56	0.00	0.56	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
158	10.85	0.56	0.00	0.56	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
159	10.90	0.57	0.00	0.57	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
160	11.00	0.57	0.00	0.57	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
161	11.05	0.58	0.00	0.58	0.98	0.267	1.68	0.159	1.00	1.10	2.000	No
162	11.14	0.58	0.00	0.58	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
163	11.21	0.58	0.00	0.58	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
164	11.29	0.59	0.00	0.59	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
165	11.38	0.59	0.00	0.59	0.98	0.267	1.68	0.158	1.00	1.10	2.000	No
166	11.46	0.60	0.00	0.60	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
167	11.52	0.60	0.00	0.60	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
168	11.60	0.61	0.00	0.61	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
169	11.67	0.61	0.00	0.61	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
170	11.72	0.61	0.00	0.61	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
171	11.81	0.62	0.00	0.62	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
172	11.86	0.62	0.00	0.62	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
173	11.96	0.63	0.00	0.63	0.98	0.266	1.68	0.158	1.00	1.10	2.000	No
174	12.01	0.63	0.00	0.63	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
175	12.10	0.63	0.00	0.63	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
176	12.16	0.64	0.00	0.64	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
177	12.24	0.64	0.00	0.64	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
178	12.32	0.64	0.00	0.64	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
179	12.39	0.65	0.00	0.65	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
180	12.48	0.65	0.00	0.65	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
181	12.50	0.65	0.00	0.65	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
182	12.54	0.66	0.00	0.66	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
183	12.64	0.66	0.00	0.66	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
184	12.68	0.66	0.00	0.66	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
185	12.77	0.67	0.00	0.67	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
186	12.82	0.67	0.00	0.67	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
187	12.89	0.68	0.00	0.68	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
188	12.97	0.68	0.00	0.68	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
189	13.03	0.68	0.00	0.68	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
190	13.12	0.69	0.00	0.69	0.97	0.266	1.68	0.158	1.00	1.10	2.000	No
191	13.16	0.69	0.00	0.69	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
192	13.26	0.70	0.00	0.70	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	13.34	0.70	0.00	0.70	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
194	13.41	0.70	0.00	0.70	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
195	13.50	0.71	0.00	0.71	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
196	13.60	0.71	0.00	0.71	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
197	13.65	0.72	0.00	0.72	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
198	13.75	0.72	0.00	0.72	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
199	13.80	0.73	0.00	0.73	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
200	13.89	0.73	0.00	0.73	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
201	13.94	0.73	0.00	0.73	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
202	14.03	0.74	0.00	0.74	0.97	0.265	1.68	0.158	1.00	1.10	2.000	No
203	14.11	0.74	0.00	0.74	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
204	14.13	0.74	0.00	0.74	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
205	14.18	0.75	0.00	0.75	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
206	14.22	0.75	0.00	0.75	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
207	14.28	0.75	0.00	0.75	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
208	14.37	0.76	0.00	0.76	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
209	14.44	0.76	0.00	0.76	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
210	14.51	0.76	0.00	0.76	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
211	14.60	0.77	0.00	0.77	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
212	14.65	0.77	0.00	0.77	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
213	14.75	0.78	0.00	0.78	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
214	14.85	0.78	0.00	0.78	0.97	0.265	1.68	0.157	1.00	1.10	2.000	No
215	14.91	0.79	0.00	0.79	0.97	0.264	1.68	0.157	1.00	1.10	2.000	No
216	14.99	0.79	0.00	0.79	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
217	15.09	0.80	0.00	0.80	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
218	15.18	0.80	0.00	0.80	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
219	15.25	0.81	0.00	0.81	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
220	15.33	0.81	0.00	0.81	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
221	15.43	0.82	0.00	0.82	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
222	15.51	0.82	0.00	0.82	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
223	15.59	0.83	0.00	0.83	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
224	15.67	0.83	0.00	0.83	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
225	15.76	0.84	0.00	0.84	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
226	15.86	0.84	0.00	0.84	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
227	15.95	0.85	0.00	0.85	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
228	16.05	0.85	0.00	0.85	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
229	16.14	0.86	0.00	0.86	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
230	16.20	0.86	0.00	0.86	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
231	16.28	0.87	0.00	0.87	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
232	16.34	0.87	0.00	0.87	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
233	16.44	0.87	0.00	0.87	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
234	16.50	0.88	0.00	0.88	0.97	0.264	1.68	0.157	1.00	1.10	2.000	Yes
235	16.58	0.88	0.00	0.88	0.97	0.263	1.68	0.157	1.00	1.10	2.000	Yes
236	16.73	0.89	0.00	0.89	0.96	0.263	1.68	0.157	1.00	1.10	2.000	No
237	16.82	0.89	0.00	0.89	0.96	0.263	1.68	0.157	1.00	1.10	2.000	No
238	16.92	0.90	0.00	0.90	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
239	17.01	0.90	0.00	0.90	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
240	17.11	0.91	0.00	0.91	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	17.12	0.91	0.00	0.91	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
242	17.14	0.91	0.00	0.91	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
243	17.19	0.91	0.00	0.91	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
244	17.28	0.92	0.00	0.92	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
245	17.33	0.92	0.00	0.92	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
246	17.43	0.92	0.00	0.92	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
247	17.47	0.93	0.00	0.93	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
248	17.57	0.93	0.00	0.93	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
249	17.65	0.94	0.00	0.94	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
250	17.72	0.94	0.00	0.94	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
251	17.81	0.94	0.00	0.94	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
252	17.86	0.95	0.00	0.95	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
253	17.95	0.95	0.00	0.95	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
254	18.05	0.96	0.00	0.96	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
255	18.10	0.96	0.00	0.96	0.96	0.263	1.68	0.156	1.00	1.10	2.000	No
256	18.20	0.97	0.00	0.97	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
257	18.30	0.97	0.00	0.97	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
258	18.39	0.98	0.00	0.98	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
259	18.48	0.98	0.00	0.98	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
260	18.58	0.99	0.00	0.99	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
261	18.66	0.99	0.00	0.99	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
262	18.74	1.00	0.00	1.00	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
263	18.87	1.00	0.00	1.00	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
264	18.97	1.01	0.00	1.01	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
265	19.06	1.01	0.00	1.01	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
266	19.16	1.02	0.00	1.02	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
267	19.25	1.02	0.00	1.02	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
268	19.27	1.02	0.00	1.02	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
269	19.30	1.02	0.00	1.02	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
270	19.34	1.03	0.00	1.03	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
271	19.39	1.03	0.00	1.03	0.96	0.262	1.68	0.156	1.00	1.10	2.000	No
272	19.49	1.04	0.00	1.04	0.96	0.262	1.68	0.155	1.00	1.10	2.000	No
273	19.55	1.04	0.00	1.04	0.96	0.262	1.68	0.155	1.00	1.10	2.000	No
274	19.63	1.04	0.00	1.04	0.96	0.261	1.68	0.155	1.00	1.10	2.000	No
275	19.68	1.05	0.00	1.05	0.96	0.261	1.68	0.155	1.00	1.10	2.000	No
276	19.74	1.05	0.00	1.05	0.96	0.261	1.68	0.155	1.00	1.10	2.000	No
277	19.83	1.05	0.00	1.05	0.96	0.261	1.68	0.155	1.00	1.10	2.000	No
278	19.87	1.06	0.00	1.06	0.96	0.261	1.68	0.155	1.00	1.10	2.000	No
279	19.94	1.06	0.00	1.06	0.96	0.261	1.68	0.155	1.00	1.10	2.000	No
280	20.02	1.06	0.00	1.06	0.96	0.261	1.68	0.155	1.00	1.10	2.000	No
281	20.07	1.07	0.00	1.07	0.96	0.261	1.68	0.155	1.00	1.10	2.000	No
282	20.17	1.07	0.00	1.07	0.96	0.261	1.68	0.155	1.00	1.10	2.000	No
283	20.21	1.07	0.00	1.07	0.96	0.261	1.68	0.155	1.00	1.10	2.000	Yes
284	20.28	1.08	0.00	1.08	0.96	0.261	1.68	0.155	1.00	1.10	2.000	Yes
285	20.36	1.08	0.00	1.08	0.96	0.261	1.68	0.155	1.00	1.10	2.000	Yes
286	20.41	1.09	0.00	1.09	0.96	0.261	1.68	0.155	0.99	1.10	2.000	Yes
287	20.48	1.09	0.00	1.09	0.96	0.261	1.68	0.155	0.99	1.10	2.000	Yes
288	20.55	1.09	0.00	1.09	0.96	0.261	1.68	0.155	0.99	1.10	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	20.60	1.10	0.00	1.10	0.96	0.261	1.68	0.155	0.99	1.10	2.000	Yes
290	20.70	1.10	0.00	1.10	0.96	0.261	1.68	0.155	0.99	1.10	2.000	No
291	20.74	1.11	0.00	1.11	0.95	0.261	1.68	0.155	0.99	1.10	2.000	No
292	20.79	1.11	0.00	1.11	0.95	0.261	1.68	0.155	0.99	1.10	2.000	No
293	20.89	1.11	0.00	1.11	0.95	0.261	1.68	0.155	0.99	1.10	2.000	No
294	20.96	1.12	0.00	1.12	0.95	0.261	1.68	0.155	0.99	1.10	2.000	No
295	21.04	1.12	0.00	1.12	0.95	0.260	1.68	0.155	0.99	1.10	2.000	No
296	21.13	1.13	0.00	1.13	0.95	0.260	1.68	0.155	0.99	1.10	2.000	No
297	21.22	1.13	0.00	1.13	0.95	0.260	1.68	0.155	0.99	1.10	2.000	No
298	21.29	1.14	0.00	1.14	0.95	0.260	1.68	0.155	0.99	1.10	2.000	No
299	21.35	1.14	0.00	1.14	0.95	0.260	1.68	0.155	0.99	1.10	2.000	No
300	21.37	1.14	0.00	1.14	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
301	21.42	1.14	0.00	1.14	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
302	21.47	1.15	0.00	1.15	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
303	21.48	1.15	0.00	1.15	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
304	21.52	1.15	0.00	1.15	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
305	21.57	1.15	0.00	1.15	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
306	21.62	1.16	0.00	1.16	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
307	21.66	1.16	0.00	1.16	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
308	21.71	1.16	0.00	1.16	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
309	21.76	1.17	0.00	1.17	0.95	0.260	1.68	0.155	0.98	1.10	2.000	No
310	21.81	1.17	0.00	1.17	0.95	0.260	1.68	0.154	0.98	1.10	2.000	No
311	21.85	1.17	0.00	1.17	0.95	0.260	1.68	0.154	0.98	1.10	2.000	No
312	21.91	1.17	0.00	1.17	0.95	0.260	1.68	0.154	0.98	1.10	2.000	No
313	21.95	1.18	0.00	1.18	0.95	0.260	1.68	0.154	0.98	1.10	2.000	No
314	22.00	1.18	0.00	1.18	0.95	0.260	1.68	0.154	0.98	1.10	2.000	No
315	22.05	1.18	0.00	1.18	0.95	0.260	1.68	0.154	0.98	1.10	2.000	No
316	22.10	1.19	0.00	1.19	0.95	0.260	1.68	0.154	0.98	1.10	2.000	No
317	22.15	1.19	0.00	1.19	0.95	0.260	1.68	0.154	0.98	1.10	2.000	No
318	22.19	1.19	0.00	1.19	0.95	0.260	1.68	0.154	0.98	1.10	2.000	No
319	22.24	1.19	0.00	1.19	0.95	0.260	1.68	0.154	0.98	1.10	2.000	No
320	22.29	1.20	0.00	1.20	0.95	0.260	1.68	0.154	0.98	1.10	2.000	No
321	22.34	1.20	0.00	1.20	0.95	0.259	1.68	0.154	0.98	1.10	2.000	No
322	22.39	1.20	0.00	1.20	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
323	22.43	1.21	0.00	1.21	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
324	22.48	1.21	0.00	1.21	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
325	22.55	1.21	0.00	1.21	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
326	22.62	1.22	0.00	1.22	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
327	22.63	1.22	0.00	1.22	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
328	22.72	1.22	0.00	1.22	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
329	22.77	1.23	0.00	1.23	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
330	22.83	1.23	0.00	1.23	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
331	22.91	1.24	0.00	1.24	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
332	22.96	1.24	0.00	1.24	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
333	23.02	1.24	0.00	1.24	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
334	23.10	1.25	0.00	1.25	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
335	23.16	1.25	0.00	1.25	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
336	23.20	1.25	0.00	1.25	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	23.26	1.26	0.00	1.26	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
338	23.35	1.26	0.00	1.26	0.95	0.259	1.68	0.154	0.97	1.10	2.000	No
339	23.39	1.27	0.00	1.27	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
340	23.48	1.27	0.00	1.27	0.95	0.259	1.68	0.154	0.96	1.10	2.000	No
341	23.54	1.27	0.00	1.27	0.95	0.258	1.68	0.154	0.96	1.10	2.000	No
342	23.63	1.28	0.00	1.28	0.95	0.258	1.68	0.154	0.96	1.10	2.000	No
343	23.69	1.28	0.00	1.28	0.95	0.258	1.68	0.154	0.96	1.10	2.000	No
344	23.78	1.29	0.00	1.29	0.95	0.258	1.68	0.154	0.96	1.10	2.000	No
345	23.87	1.29	0.00	1.29	0.95	0.258	1.68	0.153	0.96	1.10	2.000	No
346	23.88	1.29	0.00	1.29	0.95	0.258	1.68	0.153	0.96	1.10	2.000	No
347	23.93	1.30	0.00	1.30	0.95	0.258	1.68	0.153	0.96	1.10	2.000	No
348	24.02	1.30	0.00	1.30	0.95	0.258	1.68	0.153	0.96	1.10	2.000	No
349	24.04	1.30	0.00	1.30	0.95	0.258	1.68	0.153	0.96	1.10	2.000	No
350	24.05	1.30	0.00	1.30	0.95	0.258	1.68	0.153	0.96	1.10	2.000	No
351	24.15	1.31	0.00	1.31	0.94	0.258	1.68	0.153	0.96	1.10	2.000	No
352	24.20	1.31	0.00	1.31	0.94	0.258	1.68	0.153	0.96	1.10	2.000	No
353	24.30	1.32	0.00	1.32	0.94	0.258	1.68	0.153	0.96	1.10	2.000	No
354	24.40	1.32	0.00	1.32	0.94	0.258	1.68	0.153	0.96	1.10	2.000	No
355	24.46	1.33	0.00	1.33	0.94	0.258	1.68	0.153	0.96	1.10	2.000	No
356	24.54	1.33	0.00	1.33	0.94	0.258	1.68	0.153	0.95	1.10	2.000	No
357	24.64	1.34	0.00	1.34	0.94	0.257	1.68	0.153	0.95	1.10	2.000	Yes
358	24.73	1.34	0.00	1.34	0.94	0.257	1.68	0.153	0.95	1.10	2.000	Yes
359	24.78	1.35	0.00	1.35	0.94	0.257	1.68	0.153	0.95	1.10	2.000	Yes
360	24.88	1.35	0.00	1.35	0.94	0.257	1.68	0.153	0.95	1.10	2.000	Yes
361	24.94	1.36	0.00	1.36	0.94	0.257	1.68	0.153	0.95	1.10	2.000	Yes
362	25.02	1.36	0.00	1.36	0.94	0.257	1.68	0.153	0.95	1.10	2.000	Yes
363	25.12	1.37	0.00	1.37	0.94	0.257	1.68	0.153	0.95	1.10	2.000	Yes
364	25.17	1.37	0.00	1.37	0.94	0.257	1.68	0.153	0.95	1.10	2.000	Yes
365	25.27	1.38	0.00	1.38	0.94	0.257	1.68	0.153	0.95	1.10	2.000	Yes
366	25.36	1.38	0.00	1.38	0.94	0.257	1.68	0.153	0.95	1.10	2.000	No
367	25.43	1.38	0.00	1.38	0.94	0.257	1.68	0.153	0.95	1.10	2.000	No
368	25.50	1.39	0.00	1.39	0.94	0.257	1.68	0.153	0.95	1.10	2.000	No
369	25.60	1.39	0.00	1.39	0.94	0.257	1.68	0.152	0.95	1.10	2.000	No
370	25.64	1.40	0.00	1.40	0.94	0.256	1.68	0.152	0.95	1.10	2.000	No
371	25.67	1.40	0.00	1.40	0.94	0.256	1.68	0.152	0.95	1.10	2.000	No
372	25.71	1.40	0.00	1.40	0.94	0.256	1.68	0.152	0.95	1.10	2.000	No
373	25.79	1.40	0.00	1.40	0.94	0.256	1.68	0.152	0.95	1.10	2.000	No
374	25.93	1.41	0.00	1.41	0.94	0.256	1.68	0.152	0.94	1.10	2.000	No
375	26.03	1.42	0.00	1.42	0.94	0.256	1.68	0.152	0.94	1.10	2.000	No
376	26.13	1.42	0.00	1.42	0.94	0.256	1.68	0.152	0.94	1.10	2.000	No
377	26.24	1.43	0.00	1.43	0.94	0.256	1.68	0.152	0.94	1.10	2.000	No
378	26.37	1.43	0.00	1.43	0.94	0.256	1.68	0.152	0.94	1.10	2.000	No
379	26.47	1.44	0.00	1.44	0.94	0.256	1.68	0.152	0.94	1.10	2.000	No
380	26.60	1.45	0.00	1.45	0.94	0.255	1.68	0.152	0.94	1.10	2.000	No
381	26.71	1.45	0.00	1.45	0.94	0.255	1.68	0.152	0.94	1.10	2.000	No
382	26.85	1.46	0.00	1.46	0.93	0.255	1.68	0.152	0.94	1.10	2.000	No
383	26.95	1.46	0.00	1.46	0.93	0.255	1.68	0.152	0.94	1.10	2.000	No
384	27.04	1.47	0.00	1.47	0.93	0.255	1.68	0.152	0.94	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	27.09	1.47	0.00	1.47	0.93	0.255	1.68	0.152	0.94	1.10	2.000	No
386	27.19	1.48	0.00	1.48	0.93	0.255	1.68	0.151	0.94	1.10	2.000	No
387	27.23	1.48	0.00	1.48	0.93	0.255	1.68	0.151	0.94	1.10	2.000	No
388	27.33	1.48	0.00	1.48	0.93	0.255	1.68	0.151	0.93	1.10	2.000	No
389	27.40	1.49	0.00	1.49	0.93	0.255	1.68	0.151	0.93	1.10	2.000	No
390	27.47	1.49	0.00	1.49	0.93	0.255	1.68	0.151	0.93	1.10	2.000	No
391	27.57	1.50	0.00	1.50	0.93	0.254	1.68	0.151	0.93	1.10	2.000	No
392	27.66	1.50	0.00	1.50	0.93	0.254	1.68	0.151	0.93	1.10	2.000	No
393	27.77	1.51	0.00	1.51	0.93	0.254	1.68	0.151	0.93	1.10	2.000	No
394	27.86	1.51	0.00	1.51	0.93	0.254	1.68	0.151	0.93	1.10	2.000	No
395	27.96	1.52	0.00	1.52	0.93	0.254	1.68	0.151	0.93	1.10	2.000	No
396	28.06	1.52	0.00	1.52	0.93	0.254	1.68	0.151	0.93	1.10	2.000	No
397	28.15	1.53	0.00	1.53	0.93	0.254	1.68	0.151	0.93	1.10	2.000	No
398	28.25	1.54	0.00	1.54	0.93	0.254	1.68	0.151	0.93	1.10	2.000	No
399	28.34	1.54	0.00	1.54	0.93	0.253	1.68	0.151	0.93	1.10	2.000	No
400	28.44	1.55	0.00	1.55	0.93	0.253	1.68	0.151	0.93	1.10	2.000	No
401	28.54	1.55	0.00	1.55	0.93	0.253	1.68	0.151	0.93	1.10	2.000	No
402	28.62	1.56	0.00	1.56	0.93	0.253	1.68	0.150	0.93	1.10	2.000	No
403	28.71	1.56	0.00	1.56	0.93	0.253	1.68	0.150	0.93	1.10	2.000	No
404	28.77	1.56	0.00	1.56	0.93	0.253	1.68	0.150	0.92	1.10	2.000	No
405	28.86	1.57	0.00	1.57	0.93	0.253	1.68	0.150	0.92	1.10	2.000	No
406	28.91	1.57	0.00	1.57	0.93	0.253	1.68	0.150	0.92	1.10	2.000	No
407	28.97	1.58	0.00	1.58	0.93	0.253	1.68	0.150	0.92	1.10	2.000	No
408	29.04	1.58	0.00	1.58	0.93	0.253	1.68	0.150	0.92	1.10	2.000	No
409	29.10	1.58	0.00	1.58	0.92	0.253	1.68	0.150	0.92	1.10	2.000	No
410	29.15	1.59	0.00	1.59	0.92	0.252	1.68	0.150	0.92	1.10	2.000	No
411	29.25	1.59	0.00	1.59	0.92	0.252	1.68	0.150	0.92	1.10	2.000	No
412	29.34	1.60	0.00	1.60	0.92	0.252	1.68	0.150	0.92	1.10	2.000	No
413	29.38	1.60	0.00	1.60	0.92	0.252	1.68	0.150	0.92	1.10	2.000	No
414	29.48	1.61	0.00	1.61	0.92	0.252	1.68	0.150	0.92	1.10	2.000	No
415	29.55	1.61	0.00	1.61	0.92	0.252	1.68	0.150	0.92	1.10	2.000	Yes
416	29.63	1.62	0.00	1.62	0.92	0.252	1.68	0.150	0.92	1.10	2.000	Yes
417	29.72	1.62	0.00	1.62	0.92	0.252	1.68	0.150	0.92	1.10	2.000	Yes
418	29.82	1.63	0.00	1.63	0.92	0.252	1.68	0.150	0.92	1.10	2.000	Yes
419	29.88	1.63	0.00	1.63	0.92	0.251	1.68	0.149	0.92	1.10	2.000	Yes
420	29.96	1.63	0.00	1.63	0.92	0.251	1.68	0.149	0.92	1.10	2.000	Yes
421	30.06	1.64	0.00	1.64	0.92	0.252	1.68	0.150	0.92	1.10	2.000	Yes
422	30.13	1.64	0.00	1.64	0.92	0.252	1.68	0.150	0.92	1.10	2.000	Yes
423	30.18	1.65	0.01	1.64	0.92	0.252	1.68	0.150	0.92	1.10	0.180	No
424	30.28	1.65	0.01	1.64	0.92	0.252	1.68	0.150	0.92	1.10	0.180	No
425	30.37	1.66	0.01	1.65	0.92	0.253	1.68	0.150	0.92	1.10	0.180	No
426	30.47	1.66	0.01	1.65	0.92	0.253	1.68	0.150	0.92	1.10	0.181	No
427	30.57	1.67	0.02	1.65	0.92	0.253	1.68	0.151	0.91	1.10	0.181	No
428	30.66	1.68	0.02	1.65	0.92	0.254	1.68	0.151	0.91	1.10	0.181	No
429	30.74	1.68	0.02	1.66	0.92	0.254	1.68	0.151	0.91	1.10	0.181	No
430	30.82	1.68	0.03	1.66	0.92	0.254	1.68	0.151	0.91	1.10	0.182	No
431	30.90	1.69	0.03	1.66	0.92	0.254	1.68	0.151	0.91	1.10	0.182	No
432	31.01	1.70	0.03	1.66	0.92	0.255	1.68	0.151	0.91	1.10	0.182	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	31.10	1.70	0.03	1.67	0.91	0.255	1.68	0.151	0.91	1.10	0.183	No
434	31.19	1.71	0.04	1.67	0.91	0.255	1.68	0.152	0.91	1.10	0.183	No
435	31.28	1.71	0.04	1.67	0.91	0.255	1.68	0.152	0.91	1.10	0.183	No
436	31.35	1.72	0.04	1.67	0.91	0.256	1.68	0.152	0.91	1.10	0.183	No
437	31.43	1.72	0.04	1.68	0.91	0.256	1.68	0.152	0.91	1.10	0.183	No
438	31.53	1.73	0.05	1.68	0.91	0.256	1.68	0.152	0.91	1.10	0.184	No
439	31.60	1.73	0.05	1.68	0.91	0.256	1.68	0.152	0.91	1.10	0.184	No
440	31.67	1.74	0.05	1.68	0.91	0.257	1.68	0.153	0.91	1.10	0.184	No
441	31.77	1.74	0.06	1.69	0.91	0.257	1.68	0.153	0.91	1.10	0.184	No
442	31.84	1.75	0.06	1.69	0.91	0.257	1.68	0.153	0.91	1.10	0.185	No
443	31.91	1.75	0.06	1.69	0.91	0.257	1.68	0.153	0.91	1.10	0.185	No
444	31.98	1.76	0.06	1.69	0.91	0.257	1.68	0.153	0.91	1.10	0.185	No
445	31.98	1.76	0.06	1.69	0.91	0.257	1.68	0.153	0.91	1.10	0.185	No
446	32.04	1.76	0.06	1.70	0.91	0.258	1.68	0.153	0.91	1.10	0.185	No
447	32.12	1.76	0.07	1.70	0.91	0.258	1.68	0.153	0.91	1.10	2.000	Yes
448	32.16	1.77	0.07	1.70	0.91	0.258	1.68	0.153	0.91	1.10	2.000	Yes
449	32.27	1.77	0.07	1.70	0.91	0.258	1.68	0.153	0.91	1.10	2.000	Yes
450	32.33	1.78	0.07	1.70	0.91	0.258	1.68	0.154	0.91	1.10	2.000	Yes
451	32.41	1.78	0.08	1.71	0.91	0.259	1.68	0.154	0.91	1.10	2.000	Yes
452	32.50	1.79	0.08	1.71	0.91	0.259	1.68	0.154	0.91	1.10	2.000	Yes
453	32.58	1.79	0.08	1.71	0.91	0.259	1.68	0.154	0.91	1.10	2.000	Yes
454	32.66	1.80	0.08	1.71	0.91	0.259	1.68	0.154	0.91	1.10	2.000	Yes
455	32.74	1.80	0.09	1.72	0.91	0.259	1.68	0.154	0.91	1.10	2.000	Yes
456	32.84	1.81	0.09	1.72	0.90	0.260	1.68	0.154	0.91	1.10	2.000	Yes
457	32.90	1.81	0.09	1.72	0.90	0.260	1.68	0.154	0.91	1.10	2.000	Yes
458	32.98	1.82	0.09	1.72	0.90	0.260	1.68	0.155	0.91	1.10	2.000	Yes
459	33.08	1.82	0.10	1.73	0.90	0.260	1.68	0.155	0.91	1.10	0.188	No
460	33.14	1.83	0.10	1.73	0.90	0.260	1.68	0.155	0.91	1.10	0.188	No
461	33.22	1.83	0.10	1.73	0.90	0.261	1.68	0.155	0.91	1.10	0.188	No
462	33.32	1.84	0.10	1.73	0.90	0.261	1.68	0.155	0.91	1.10	0.188	No
463	33.37	1.84	0.11	1.73	0.90	0.261	1.68	0.155	0.91	1.10	0.188	No
464	33.47	1.84	0.11	1.74	0.90	0.261	1.68	0.155	0.91	1.10	0.189	No
465	33.56	1.85	0.11	1.74	0.90	0.261	1.68	0.155	0.91	1.10	0.189	No
466	33.63	1.85	0.11	1.74	0.90	0.262	1.68	0.156	0.91	1.10	0.189	No
467	33.71	1.86	0.12	1.74	0.90	0.262	1.68	0.156	0.91	1.10	0.189	No
468	33.81	1.86	0.12	1.74	0.90	0.262	1.68	0.156	0.90	1.10	0.189	No
469	33.90	1.87	0.12	1.75	0.90	0.262	1.68	0.156	0.90	1.10	0.190	No
470	33.95	1.87	0.12	1.75	0.90	0.262	1.68	0.156	0.90	1.10	0.190	No
471	34.04	1.88	0.13	1.75	0.90	0.263	1.68	0.156	0.90	1.10	0.190	No
472	34.14	1.88	0.13	1.75	0.90	0.263	1.68	0.156	0.90	1.10	0.190	No
473	34.17	1.88	0.13	1.75	0.90	0.263	1.68	0.156	0.90	1.10	0.190	No
474	34.20	1.88	0.13	1.75	0.90	0.263	1.68	0.156	0.90	1.10	0.190	No
475	34.26	1.89	0.13	1.75	0.90	0.263	1.68	0.156	0.90	1.10	0.190	No
476	34.35	1.89	0.14	1.76	0.90	0.263	1.68	0.156	0.90	1.10	0.190	No
477	34.43	1.90	0.14	1.76	0.89	0.263	1.68	0.157	0.90	1.10	0.191	No
478	34.49	1.90	0.14	1.76	0.89	0.264	1.68	0.157	0.90	1.10	0.191	No
479	34.59	1.90	0.14	1.76	0.89	0.264	1.68	0.157	0.90	1.10	0.191	No
480	34.69	1.91	0.15	1.76	0.89	0.264	1.68	0.157	0.90	1.10	0.191	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	34.73	1.91	0.15	1.76	0.89	0.264	1.68	0.157	0.90	1.10	0.191	No
482	34.83	1.92	0.15	1.76	0.89	0.264	1.68	0.157	0.90	1.10	0.191	No
483	34.90	1.92	0.15	1.77	0.89	0.264	1.68	0.157	0.90	1.10	0.192	No
484	34.98	1.92	0.16	1.77	0.89	0.265	1.68	0.157	0.90	1.10	0.192	No
485	35.07	1.93	0.16	1.77	0.89	0.265	1.68	0.157	0.90	1.10	0.192	No
486	35.16	1.93	0.16	1.77	0.89	0.265	1.68	0.157	0.90	1.10	0.192	No
487	35.26	1.94	0.16	1.77	0.89	0.265	1.68	0.158	0.90	1.10	0.192	No
488	35.33	1.94	0.17	1.78	0.89	0.265	1.68	0.158	0.90	1.10	0.192	No
489	35.40	1.95	0.17	1.78	0.89	0.265	1.68	0.158	0.90	1.10	0.192	No
490	35.50	1.95	0.17	1.78	0.89	0.266	1.68	0.158	0.90	1.10	0.193	No
491	35.57	1.96	0.17	1.78	0.89	0.266	1.68	0.158	0.90	1.10	0.193	No
492	35.65	1.96	0.18	1.78	0.89	0.266	1.68	0.158	0.90	1.10	0.193	No
493	35.71	1.96	0.18	1.79	0.89	0.266	1.68	0.158	0.90	1.10	0.193	No
494	35.79	1.97	0.18	1.79	0.88	0.266	1.68	0.158	0.90	1.10	0.193	No
495	35.85	1.97	0.18	1.79	0.88	0.266	1.68	0.158	0.90	1.10	0.193	No
496	35.94	1.98	0.19	1.79	0.88	0.266	1.68	0.158	0.90	1.10	0.193	No
497	35.99	1.98	0.19	1.79	0.88	0.266	1.68	0.158	0.90	1.10	0.194	No
498	36.08	1.99	0.19	1.80	0.88	0.266	1.68	0.158	0.90	1.10	0.194	No
499	36.17	1.99	0.19	1.80	0.88	0.267	1.68	0.158	0.90	1.10	0.194	No
500	36.24	1.99	0.19	1.80	0.88	0.267	1.68	0.159	0.90	1.10	0.194	No
501	36.33	2.00	0.20	1.80	0.88	0.267	1.68	0.159	0.90	1.10	0.194	No
502	36.42	2.00	0.20	1.80	0.88	0.267	1.68	0.159	0.90	1.10	0.194	No
503	36.52	2.01	0.20	1.81	0.88	0.267	1.68	0.159	0.90	1.10	0.194	No
504	36.61	2.02	0.21	1.81	0.88	0.267	1.68	0.159	0.90	1.10	0.195	No
505	36.70	2.02	0.21	1.81	0.88	0.267	1.68	0.159	0.90	1.10	0.195	No
506	36.78	2.02	0.21	1.81	0.88	0.268	1.68	0.159	0.90	1.10	0.195	No
507	36.85	2.03	0.21	1.82	0.88	0.268	1.68	0.159	0.90	1.10	0.195	No
508	36.87	2.03	0.21	1.82	0.88	0.268	1.68	0.159	0.90	1.10	0.195	No
509	36.91	2.03	0.22	1.82	0.88	0.268	1.68	0.159	0.90	1.10	0.195	No
510	36.97	2.04	0.22	1.82	0.88	0.268	1.68	0.159	0.90	1.10	2.000	Yes
511	37.06	2.04	0.22	1.82	0.88	0.268	1.68	0.159	0.90	1.10	2.000	Yes
512	37.12	2.04	0.22	1.82	0.87	0.268	1.68	0.159	0.90	1.10	2.000	Yes
513	37.20	2.05	0.22	1.82	0.87	0.268	1.68	0.159	0.90	1.10	2.000	Yes
514	37.27	2.05	0.23	1.83	0.87	0.268	1.68	0.159	0.90	1.10	2.000	Yes
515	37.35	2.06	0.23	1.83	0.87	0.268	1.68	0.159	0.90	1.10	2.000	Yes
516	37.44	2.06	0.23	1.83	0.87	0.268	1.68	0.160	0.90	1.10	2.000	Yes
517	37.49	2.07	0.23	1.83	0.87	0.268	1.68	0.160	0.90	1.10	2.000	Yes
518	37.59	2.07	0.24	1.84	0.87	0.269	1.68	0.160	0.90	1.10	2.000	Yes
519	37.64	2.08	0.24	1.84	0.87	0.269	1.68	0.160	0.90	1.10	2.000	Yes
520	37.70	2.08	0.24	1.84	0.87	0.269	1.68	0.160	0.90	1.10	2.000	Yes
521	37.78	2.09	0.24	1.84	0.87	0.269	1.68	0.160	0.89	1.10	2.000	Yes
522	37.83	2.09	0.24	1.84	0.87	0.269	1.68	0.160	0.89	1.10	2.000	Yes
523	37.92	2.09	0.25	1.85	0.87	0.269	1.68	0.160	0.89	1.10	2.000	Yes
524	37.97	2.10	0.25	1.85	0.87	0.269	1.68	0.160	0.89	1.10	2.000	Yes
525	38.07	2.10	0.25	1.85	0.87	0.269	1.68	0.160	0.89	1.10	0.197	No
526	38.14	2.11	0.25	1.85	0.87	0.269	1.68	0.160	0.89	1.10	0.197	No
527	38.22	2.11	0.26	1.86	0.87	0.269	1.68	0.160	0.89	1.10	0.197	No
528	38.31	2.12	0.26	1.86	0.87	0.269	1.68	0.160	0.89	1.10	0.197	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	38.41	2.12	0.26	1.86	0.86	0.269	1.68	0.160	0.89	1.10	0.197	No
530	38.52	2.13	0.27	1.87	0.86	0.269	1.68	0.160	0.89	1.10	0.197	No
531	38.64	2.14	0.27	1.87	0.86	0.269	1.68	0.160	0.89	1.10	0.197	No
532	38.74	2.15	0.27	1.87	0.86	0.270	1.68	0.160	0.89	1.10	0.198	No
533	38.80	2.15	0.27	1.88	0.86	0.270	1.68	0.160	0.89	1.10	0.198	No
534	38.89	2.16	0.28	1.88	0.86	0.270	1.68	0.160	0.89	1.10	0.198	No
535	38.94	2.16	0.28	1.88	0.86	0.270	1.68	0.160	0.89	1.10	0.198	No
536	39.03	2.17	0.28	1.88	0.86	0.270	1.68	0.160	0.89	1.10	0.198	No
537	39.13	2.17	0.28	1.89	0.86	0.270	1.68	0.160	0.89	1.10	0.198	No
538	39.23	2.18	0.29	1.89	0.86	0.270	1.68	0.160	0.89	1.10	0.198	No
539	39.35	2.19	0.29	1.89	0.86	0.270	1.68	0.160	0.89	1.10	0.198	No
540	39.42	2.19	0.29	1.90	0.86	0.270	1.68	0.160	0.89	1.10	0.198	No
541	39.51	2.20	0.30	1.90	0.86	0.270	1.68	0.160	0.89	1.10	0.198	No
542	39.60	2.20	0.30	1.90	0.85	0.270	1.68	0.160	0.89	1.10	0.199	No
543	39.70	2.21	0.30	1.91	0.85	0.270	1.68	0.161	0.89	1.10	0.199	No
544	39.78	2.21	0.31	1.91	0.85	0.270	1.68	0.161	0.89	1.10	0.199	No
545	39.90	2.22	0.31	1.91	0.85	0.270	1.68	0.161	0.89	1.10	0.199	No
546	39.99	2.23	0.31	1.92	0.85	0.270	1.68	0.161	0.89	1.10	0.199	No
547	40.09	2.23	0.31	1.92	0.85	0.270	1.68	0.161	0.89	1.10	2.000	Yes
548	40.18	2.24	0.32	1.92	0.85	0.270	1.68	0.161	0.89	1.10	2.000	Yes
549	40.23	2.24	0.32	1.92	0.85	0.270	1.68	0.161	0.89	1.10	2.000	Yes
550	40.33	2.25	0.32	1.93	0.85	0.270	1.68	0.161	0.89	1.10	2.000	Yes
551	40.43	2.26	0.33	1.93	0.85	0.270	1.68	0.161	0.89	1.10	2.000	Yes
552	40.52	2.26	0.33	1.93	0.85	0.270	1.68	0.161	0.89	1.10	2.000	Yes
553	40.61	2.27	0.33	1.94	0.85	0.270	1.68	0.161	0.89	1.10	2.000	Yes
554	40.69	2.27	0.33	1.94	0.84	0.270	1.68	0.161	0.89	1.10	2.000	Yes
555	40.80	2.28	0.34	1.94	0.84	0.270	1.68	0.161	0.89	1.10	2.000	Yes
556	40.87	2.28	0.34	1.94	0.84	0.270	1.68	0.161	0.89	1.10	2.000	Yes
557	40.95	2.29	0.34	1.95	0.84	0.270	1.68	0.161	0.89	1.10	2.000	Yes
558	40.97	2.29	0.34	1.95	0.84	0.270	1.68	0.161	0.89	1.10	2.000	Yes
559	41.01	2.29	0.34	1.95	0.84	0.270	1.68	0.161	0.89	1.10	2.000	Yes
560	41.07	2.30	0.35	1.95	0.84	0.270	1.68	0.161	0.88	1.10	2.000	Yes
561	41.15	2.30	0.35	1.95	0.84	0.270	1.68	0.161	0.88	1.10	2.000	Yes
562	41.26	2.31	0.35	1.96	0.84	0.270	1.68	0.161	0.88	1.10	0.200	No
563	41.35	2.31	0.35	1.96	0.84	0.270	1.68	0.161	0.88	1.10	0.200	No
564	41.47	2.32	0.36	1.96	0.84	0.270	1.68	0.161	0.88	1.10	0.200	No
565	41.59	2.33	0.36	1.97	0.84	0.270	1.68	0.161	0.88	1.10	0.200	No
566	41.69	2.33	0.36	1.97	0.84	0.270	1.68	0.161	0.88	1.10	0.200	No
567	41.78	2.34	0.37	1.97	0.83	0.270	1.68	0.161	0.88	1.10	0.200	No
568	41.88	2.34	0.37	1.97	0.83	0.270	1.68	0.161	0.88	1.10	0.200	No
569	41.98	2.35	0.37	1.98	0.83	0.270	1.68	0.161	0.88	1.10	0.200	No
570	42.08	2.36	0.38	1.98	0.83	0.270	1.68	0.161	0.88	1.10	0.200	No
571	42.16	2.36	0.38	1.98	0.83	0.270	1.68	0.161	0.88	1.10	0.200	No
572	42.24	2.37	0.38	1.98	0.83	0.270	1.68	0.161	0.88	1.10	0.200	No
573	42.31	2.37	0.38	1.99	0.83	0.270	1.68	0.161	0.88	1.10	0.201	No
574	42.45	2.38	0.39	1.99	0.83	0.270	1.68	0.161	0.88	1.10	0.201	No
575	42.55	2.38	0.39	1.99	0.83	0.270	1.68	0.161	0.88	1.10	0.201	No
576	42.60	2.39	0.39	1.99	0.83	0.270	1.68	0.161	0.88	1.10	0.201	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	42.70	2.39	0.40	2.00	0.83	0.270	1.68	0.161	0.88	1.10	0.201	No
578	42.81	2.40	0.40	2.00	0.83	0.270	1.68	0.161	0.88	1.10	0.201	No
579	42.89	2.41	0.40	2.00	0.82	0.270	1.68	0.161	0.88	1.10	0.201	No
580	42.98	2.41	0.41	2.01	0.82	0.270	1.68	0.161	0.88	1.10	0.201	No
581	43.08	2.42	0.41	2.01	0.82	0.270	1.68	0.161	0.88	1.10	0.201	No
582	43.17	2.42	0.41	2.01	0.82	0.270	1.68	0.161	0.88	1.10	0.201	No
583	43.27	2.43	0.41	2.01	0.82	0.270	1.68	0.161	0.88	1.10	0.201	No
584	43.37	2.43	0.42	2.02	0.82	0.270	1.68	0.161	0.88	1.10	0.201	No
585	43.50	2.44	0.42	2.02	0.82	0.270	1.68	0.160	0.88	1.10	0.201	No
586	43.61	2.45	0.42	2.02	0.82	0.270	1.68	0.160	0.88	1.10	0.201	No
587	43.74	2.46	0.43	2.03	0.82	0.270	1.68	0.160	0.88	1.10	0.201	No
588	43.79	2.46	0.43	2.03	0.82	0.270	1.68	0.160	0.88	1.10	0.201	No
589	43.86	2.46	0.43	2.03	0.81	0.270	1.68	0.160	0.88	1.10	0.201	No
590	43.94	2.47	0.43	2.03	0.81	0.270	1.68	0.160	0.88	1.10	0.201	No
591	44.00	2.47	0.44	2.04	0.81	0.270	1.68	0.160	0.88	1.10	0.201	No
592	44.08	2.48	0.44	2.04	0.81	0.270	1.68	0.160	0.88	1.10	0.201	No
593	44.17	2.48	0.44	2.04	0.81	0.270	1.68	0.160	0.88	1.10	0.201	No
594	44.27	2.49	0.45	2.04	0.81	0.270	1.68	0.160	0.88	1.10	0.201	No
595	44.42	2.50	0.45	2.05	0.81	0.270	1.68	0.160	0.88	1.10	0.201	No
596	44.52	2.50	0.45	2.05	0.81	0.269	1.68	0.160	0.88	1.10	0.201	No
597	44.61	2.51	0.46	2.05	0.81	0.269	1.68	0.160	0.88	1.10	0.201	No
598	44.71	2.51	0.46	2.06	0.81	0.269	1.68	0.160	0.88	1.10	0.201	No
599	44.85	2.52	0.46	2.06	0.81	0.269	1.68	0.160	0.88	1.10	0.201	No
600	44.95	2.53	0.47	2.06	0.80	0.269	1.68	0.160	0.88	1.10	0.201	No
601	45.09	2.54	0.47	2.07	0.80	0.269	1.68	0.160	0.87	1.10	0.201	No
602	45.19	2.54	0.47	2.07	0.80	0.269	1.68	0.160	0.87	1.10	0.201	No
603	45.33	2.55	0.48	2.07	0.80	0.269	1.68	0.160	0.87	1.10	0.201	No
604	45.42	2.56	0.48	2.08	0.80	0.269	1.68	0.160	0.87	1.10	0.201	No
605	45.57	2.57	0.49	2.08	0.80	0.269	1.68	0.160	0.87	1.10	0.201	No
606	45.68	2.57	0.49	2.08	0.80	0.269	1.68	0.160	0.87	1.10	0.201	No
607	45.81	2.58	0.49	2.09	0.80	0.268	1.68	0.160	0.87	1.10	0.201	No
608	45.92	2.59	0.50	2.09	0.79	0.268	1.68	0.160	0.87	1.10	0.201	No
609	46.05	2.59	0.50	2.09	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
610	46.16	2.60	0.50	2.10	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
611	46.17	2.60	0.50	2.10	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
612	46.23	2.60	0.51	2.10	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
613	46.29	2.61	0.51	2.10	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
614	46.34	2.61	0.51	2.10	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
615	46.42	2.62	0.51	2.10	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
616	46.48	2.62	0.51	2.10	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
617	46.52	2.62	0.52	2.11	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
618	46.60	2.63	0.52	2.11	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
619	46.67	2.63	0.52	2.11	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
620	46.74	2.63	0.52	2.11	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
621	46.82	2.64	0.52	2.11	0.79	0.268	1.68	0.159	0.87	1.10	0.201	No
622	46.88	2.64	0.53	2.11	0.78	0.268	1.68	0.159	0.87	1.10	0.201	No
623	46.96	2.64	0.53	2.12	0.78	0.268	1.68	0.159	0.87	1.10	0.201	No
624	47.06	2.65	0.53	2.12	0.78	0.267	1.68	0.159	0.87	1.10	0.201	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	47.15	2.65	0.54	2.12	0.78	0.267	1.68	0.159	0.87	1.10	0.201	No
626	47.24	2.66	0.54	2.12	0.78	0.267	1.68	0.159	0.87	1.10	0.201	No
627	47.35	2.67	0.54	2.12	0.78	0.267	1.68	0.159	0.87	1.10	0.201	No
628	47.49	2.67	0.55	2.13	0.78	0.267	1.68	0.159	0.87	1.10	0.201	No
629	47.58	2.68	0.55	2.13	0.78	0.267	1.68	0.159	0.87	1.10	0.201	No
630	47.73	2.69	0.55	2.13	0.78	0.267	1.68	0.159	0.87	1.10	0.201	No
631	47.83	2.69	0.56	2.14	0.77	0.267	1.68	0.158	0.87	1.10	0.201	No
632	47.87	2.70	0.56	2.14	0.77	0.267	1.68	0.158	0.87	1.10	0.201	No
633	47.89	2.70	0.56	2.14	0.77	0.267	1.68	0.158	0.87	1.10	0.201	No
634	47.94	2.70	0.56	2.14	0.77	0.267	1.68	0.158	0.87	1.10	0.201	No
635	48.02	2.70	0.56	2.14	0.77	0.266	1.68	0.158	0.87	1.10	0.201	No
636	48.07	2.71	0.56	2.14	0.77	0.266	1.68	0.158	0.87	1.10	0.201	No
637	48.12	2.71	0.57	2.14	0.77	0.266	1.68	0.158	0.87	1.10	0.201	No
638	48.18	2.71	0.57	2.15	0.77	0.266	1.68	0.158	0.87	1.10	0.201	No
639	48.26	2.72	0.57	2.15	0.77	0.266	1.68	0.158	0.87	1.10	0.200	No
640	48.31	2.72	0.57	2.15	0.77	0.266	1.68	0.158	0.87	1.10	0.200	No
641	48.38	2.72	0.57	2.15	0.77	0.266	1.68	0.158	0.87	1.10	0.200	No
642	48.46	2.73	0.58	2.15	0.77	0.266	1.68	0.158	0.87	1.10	0.200	No
643	48.52	2.73	0.58	2.16	0.77	0.266	1.68	0.158	0.87	1.10	0.200	No
644	48.60	2.74	0.58	2.16	0.77	0.266	1.68	0.158	0.87	1.10	0.200	No
645	48.68	2.74	0.58	2.16	0.77	0.266	1.68	0.158	0.87	1.10	0.200	No
646	48.74	2.75	0.58	2.16	0.77	0.266	1.68	0.158	0.87	1.10	0.200	No
647	48.82	2.75	0.59	2.16	0.76	0.265	1.68	0.158	0.87	1.10	0.200	No
648	48.89	2.75	0.59	2.16	0.76	0.265	1.68	0.158	0.87	1.10	0.200	No
649	48.99	2.76	0.59	2.17	0.76	0.265	1.68	0.158	0.87	1.10	0.200	No
650	49.05	2.76	0.59	2.17	0.76	0.265	1.68	0.158	0.87	1.10	0.200	No
651	49.12	2.77	0.60	2.17	0.76	0.265	1.68	0.158	0.87	1.10	0.200	No
652	49.18	2.77	0.60	2.17	0.76	0.265	1.68	0.158	0.87	1.10	0.200	No
653	49.27	2.77	0.60	2.17	0.76	0.265	1.68	0.157	0.87	1.10	0.200	No
654	49.32	2.78	0.60	2.17	0.76	0.265	1.68	0.157	0.87	1.10	0.200	No
655	49.42	2.78	0.61	2.18	0.76	0.265	1.68	0.157	0.87	1.10	0.200	No
656	49.48	2.78	0.61	2.18	0.76	0.265	1.68	0.157	0.87	1.10	0.200	No
657	49.56	2.79	0.61	2.18	0.76	0.265	1.68	0.157	0.87	1.10	0.200	No
658	49.66	2.79	0.61	2.18	0.76	0.264	1.68	0.157	0.87	1.10	0.200	No
659	49.76	2.80	0.62	2.18	0.76	0.264	1.68	0.157	0.87	1.10	0.200	No
660	49.85	2.80	0.62	2.19	0.75	0.264	1.68	0.157	0.86	1.10	0.200	No
661	49.99	2.81	0.62	2.19	0.75	0.264	1.68	0.157	0.86	1.10	0.200	No
662	50.09	2.82	0.63	2.19	0.75	0.264	1.68	0.157	0.86	1.10	0.200	No
663	50.21	2.82	0.63	2.19	0.75	0.264	1.68	0.157	0.86	1.10	0.200	No
664	50.24	2.82	0.63	2.19	0.75	0.264	1.68	0.157	0.86	1.10	0.200	No
665	50.29	2.83	0.63	2.19	0.75	0.264	1.68	0.157	0.86	1.10	0.200	No
666	50.38	2.83	0.64	2.20	0.75	0.264	1.68	0.157	0.86	1.10	0.199	No
667	50.47	2.84	0.64	2.20	0.75	0.264	1.68	0.157	0.86	1.10	0.199	No
668	50.52	2.84	0.64	2.20	0.75	0.263	1.68	0.157	0.86	1.10	0.199	No
669	50.62	2.84	0.64	2.20	0.75	0.263	1.68	0.157	0.86	1.10	0.199	No
670	50.66	2.85	0.64	2.20	0.75	0.263	1.68	0.156	0.86	1.10	0.199	No
671	50.76	2.85	0.65	2.20	0.74	0.263	1.68	0.156	0.86	1.10	0.199	No
672	50.83	2.85	0.65	2.21	0.74	0.263	1.68	0.156	0.86	1.10	0.199	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	50.91	2.86	0.65	2.21	0.74	0.263	1.68	0.156	0.86	1.10	0.199	No
674	51.00	2.86	0.66	2.21	0.74	0.263	1.68	0.156	0.86	1.10	0.199	No
675	51.06	2.87	0.66	2.21	0.74	0.263	1.68	0.156	0.86	1.10	0.199	No
676	51.15	2.87	0.66	2.21	0.74	0.263	1.68	0.156	0.86	1.10	0.199	No
677	51.24	2.88	0.66	2.21	0.74	0.263	1.68	0.156	0.86	1.10	0.199	No
678	51.31	2.88	0.67	2.22	0.74	0.262	1.68	0.156	0.86	1.10	0.199	No
679	51.39	2.89	0.67	2.22	0.74	0.262	1.68	0.156	0.86	1.10	0.199	No
680	51.48	2.89	0.67	2.22	0.74	0.262	1.68	0.156	0.86	1.10	0.199	No
681	51.58	2.90	0.67	2.22	0.74	0.262	1.68	0.156	0.86	1.10	0.199	No
682	51.68	2.90	0.68	2.23	0.74	0.262	1.68	0.156	0.86	1.10	0.199	No
683	51.77	2.91	0.68	2.23	0.73	0.262	1.68	0.156	0.86	1.10	0.199	No
684	51.90	2.92	0.68	2.23	0.73	0.262	1.68	0.155	0.86	1.10	0.199	No
685	52.01	2.92	0.69	2.24	0.73	0.261	1.68	0.155	0.86	1.10	2.000	Yes
686	52.11	2.93	0.69	2.24	0.73	0.261	1.68	0.155	0.86	1.10	2.000	Yes
687	52.26	2.94	0.69	2.24	0.73	0.261	1.68	0.155	0.86	1.10	2.000	Yes
688	52.30	2.94	0.70	2.25	0.73	0.261	1.68	0.155	0.86	1.10	2.000	Yes
689	52.33	2.94	0.70	2.25	0.73	0.261	1.68	0.155	0.86	1.10	2.000	Yes
690	52.35	2.95	0.70	2.25	0.73	0.261	1.68	0.155	0.86	1.10	2.000	Yes
691	52.40	2.95	0.70	2.25	0.73	0.261	1.68	0.155	0.86	1.10	2.000	Yes
692	52.45	2.95	0.70	2.25	0.73	0.261	1.68	0.155	0.86	1.10	2.000	Yes
693	52.50	2.96	0.70	2.25	0.73	0.260	1.68	0.155	0.86	1.10	0.198	No
694	52.55	2.96	0.70	2.26	0.73	0.260	1.68	0.155	0.86	1.10	0.198	No
695	52.60	2.96	0.71	2.26	0.73	0.260	1.68	0.155	0.86	1.10	0.198	No
696	52.65	2.97	0.71	2.26	0.73	0.260	1.68	0.155	0.86	1.10	0.198	No
697	52.71	2.97	0.71	2.26	0.73	0.260	1.68	0.155	0.86	1.10	0.198	No
698	52.77	2.97	0.71	2.26	0.72	0.260	1.68	0.155	0.86	1.10	0.198	No
699	52.82	2.98	0.71	2.27	0.72	0.260	1.68	0.154	0.86	1.10	0.198	No
700	52.88	2.98	0.71	2.27	0.72	0.260	1.68	0.154	0.86	1.10	0.198	No
701	52.93	2.99	0.72	2.27	0.72	0.260	1.68	0.154	0.86	1.10	0.198	No
702	52.98	2.99	0.72	2.27	0.72	0.260	1.68	0.154	0.86	1.10	0.198	No
703	53.03	2.99	0.72	2.27	0.72	0.260	1.68	0.154	0.86	1.10	0.198	No
704	53.08	2.99	0.72	2.27	0.72	0.259	1.68	0.154	0.86	1.10	0.198	No
705	53.12	3.00	0.72	2.28	0.72	0.259	1.68	0.154	0.86	1.10	0.198	No
706	53.17	3.00	0.72	2.28	0.72	0.259	1.68	0.154	0.86	1.10	0.198	No
707	53.23	3.01	0.72	2.28	0.72	0.259	1.68	0.154	0.86	1.10	0.198	No
708	53.28	3.01	0.73	2.28	0.72	0.259	1.68	0.154	0.86	1.10	0.198	No
709	53.37	3.01	0.73	2.29	0.72	0.259	1.68	0.154	0.86	1.10	0.197	No
710	53.42	3.02	0.73	2.29	0.72	0.259	1.68	0.154	0.86	1.10	0.197	No
711	53.46	3.02	0.73	2.29	0.72	0.259	1.68	0.154	0.86	1.10	0.197	No
712	53.53	3.03	0.73	2.29	0.72	0.259	1.68	0.154	0.86	1.10	0.197	No
713	53.61	3.03	0.74	2.29	0.72	0.258	1.68	0.154	0.86	1.10	0.197	No
714	53.62	3.03	0.74	2.30	0.72	0.258	1.68	0.154	0.86	1.10	0.197	No
715	53.65	3.03	0.74	2.30	0.72	0.258	1.68	0.154	0.86	1.10	0.197	No
716	53.67	3.04	0.74	2.30	0.72	0.258	1.68	0.154	0.86	1.10	0.197	No
717	53.70	3.04	0.74	2.30	0.72	0.258	1.68	0.154	0.86	1.10	0.197	No
718	53.74	3.04	0.74	2.30	0.72	0.258	1.68	0.153	0.86	1.10	0.197	No
719	53.76	3.04	0.74	2.30	0.72	0.258	1.68	0.153	0.86	1.10	0.197	No
720	53.80	3.04	0.74	2.30	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	53.84	3.05	0.74	2.30	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
722	53.90	3.05	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
723	53.91	3.05	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
724	53.95	3.05	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
725	53.96	3.06	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
726	53.98	3.06	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
727	53.99	3.06	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
728	54.01	3.06	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
729	54.02	3.06	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
730	54.03	3.06	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
731	54.04	3.06	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
732	54.05	3.06	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
733	54.09	3.06	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
734	54.10	3.06	0.75	2.31	0.71	0.258	1.68	0.153	0.86	1.10	0.197	No
735	54.13	3.07	0.75	2.31	0.71	0.257	1.68	0.153	0.86	1.10	0.197	No
736	54.14	3.07	0.75	2.31	0.71	0.257	1.68	0.153	0.86	1.10	0.197	No
737	54.19	3.07	0.75	2.32	0.71	0.257	1.68	0.153	0.85	1.10	0.197	No
738	54.19	3.07	0.75	2.32	0.71	0.257	1.68	0.153	0.85	1.10	0.197	No
739	54.24	3.07	0.76	2.32	0.71	0.257	1.68	0.153	0.85	1.10	0.197	No
740	54.29	3.08	0.76	2.32	0.71	0.257	1.68	0.153	0.85	1.10	0.197	No
741	54.33	3.08	0.76	2.32	0.71	0.257	1.68	0.153	0.85	1.10	0.197	No
742	54.38	3.08	0.76	2.32	0.71	0.257	1.68	0.153	0.85	1.10	0.197	No
743	54.39	3.09	0.76	2.32	0.71	0.257	1.68	0.153	0.85	1.10	0.197	No
744	54.43	3.09	0.76	2.33	0.71	0.257	1.68	0.153	0.85	1.10	0.197	No
745	54.48	3.09	0.76	2.33	0.71	0.257	1.68	0.153	0.85	1.10	0.197	No
746	54.52	3.09	0.77	2.33	0.71	0.257	1.68	0.153	0.85	1.10	0.197	No
747	54.58	3.10	0.77	2.33	0.71	0.257	1.68	0.153	0.85	1.10	0.197	No
748	54.62	3.10	0.77	2.33	0.71	0.257	1.68	0.152	0.85	1.10	0.196	No
749	54.65	3.10	0.77	2.33	0.71	0.257	1.68	0.152	0.85	1.10	0.196	No
750	54.67	3.10	0.77	2.33	0.71	0.256	1.68	0.152	0.85	1.10	0.196	No
751	54.71	3.11	0.77	2.34	0.71	0.256	1.68	0.152	0.85	1.10	0.196	No
752	54.77	3.11	0.77	2.34	0.71	0.256	1.68	0.152	0.85	1.10	0.196	No
753	54.81	3.11	0.77	2.34	0.71	0.256	1.68	0.152	0.85	1.10	0.196	No
754	54.85	3.12	0.78	2.34	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
755	54.86	3.12	0.78	2.34	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
756	54.87	3.12	0.78	2.34	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
757	54.91	3.12	0.78	2.34	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
758	54.96	3.12	0.78	2.34	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
759	55.00	3.13	0.78	2.35	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
760	55.01	3.13	0.78	2.35	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
761	55.05	3.13	0.78	2.35	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
762	55.10	3.13	0.78	2.35	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
763	55.12	3.13	0.78	2.35	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
764	55.13	3.13	0.78	2.35	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
765	55.14	3.14	0.78	2.35	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
766	55.19	3.14	0.79	2.35	0.70	0.256	1.68	0.152	0.85	1.10	0.196	No
767	55.20	3.14	0.79	2.35	0.70	0.255	1.68	0.152	0.85	1.10	0.196	No
768	55.25	3.14	0.79	2.35	0.70	0.255	1.68	0.152	0.85	1.10	0.196	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	55.29	3.14	0.79	2.36	0.70	0.255	1.68	0.152	0.85	1.10	0.196	No
770	55.33	3.15	0.79	2.36	0.70	0.255	1.68	0.152	0.85	1.10	0.196	No
771	55.38	3.15	0.79	2.36	0.70	0.255	1.68	0.152	0.85	1.10	0.196	No
772	55.48	3.16	0.80	2.36	0.70	0.255	1.68	0.152	0.85	1.10	0.196	No
773	55.57	3.16	0.80	2.37	0.70	0.255	1.68	0.151	0.85	1.10	0.196	No
774	55.63	3.17	0.80	2.37	0.70	0.255	1.68	0.151	0.85	1.10	0.196	No
775	55.72	3.17	0.80	2.37	0.70	0.255	1.68	0.151	0.85	1.10	0.196	No
776	55.80	3.18	0.80	2.37	0.70	0.254	1.68	0.151	0.85	1.10	0.195	No
777	55.86	3.18	0.81	2.38	0.70	0.254	1.68	0.151	0.85	1.10	0.195	No
778	55.97	3.19	0.81	2.38	0.69	0.254	1.68	0.151	0.85	1.10	0.195	No
779	56.01	3.19	0.81	2.38	0.69	0.254	1.68	0.151	0.85	1.10	0.195	No
780	56.06	3.20	0.81	2.38	0.69	0.254	1.68	0.151	0.85	1.10	0.195	No
781	56.11	3.20	0.81	2.39	0.69	0.254	1.68	0.151	0.85	1.10	0.195	No
782	56.15	3.20	0.82	2.39	0.69	0.254	1.68	0.151	0.85	1.10	0.195	No
783	56.20	3.21	0.82	2.39	0.69	0.254	1.68	0.151	0.85	1.10	0.195	No
784	56.27	3.21	0.82	2.39	0.69	0.253	1.68	0.151	0.85	1.10	0.195	No
785	56.27	3.21	0.82	2.39	0.69	0.253	1.68	0.151	0.85	1.10	0.195	No
786	56.30	3.21	0.82	2.39	0.69	0.253	1.68	0.151	0.85	1.10	0.195	No
787	56.33	3.22	0.82	2.39	0.69	0.253	1.68	0.151	0.85	1.10	0.195	No
788	56.35	3.22	0.82	2.39	0.69	0.253	1.68	0.151	0.85	1.10	0.195	No
789	56.40	3.22	0.82	2.40	0.69	0.253	1.68	0.151	0.85	1.10	0.195	No
790	56.41	3.22	0.82	2.40	0.69	0.253	1.68	0.151	0.85	1.10	0.195	No
791	56.44	3.22	0.83	2.40	0.69	0.253	1.68	0.150	0.85	1.10	0.195	No
792	56.49	3.23	0.83	2.40	0.69	0.253	1.68	0.150	0.85	1.10	0.195	No
793	56.54	3.23	0.83	2.40	0.69	0.253	1.68	0.150	0.85	1.10	0.195	No
794	56.58	3.23	0.83	2.40	0.69	0.253	1.68	0.150	0.85	1.10	0.195	No
795	56.59	3.23	0.83	2.40	0.69	0.253	1.68	0.150	0.85	1.10	0.195	No
796	56.64	3.24	0.83	2.41	0.69	0.253	1.68	0.150	0.85	1.10	0.195	No
797	56.69	3.24	0.83	2.41	0.69	0.253	1.68	0.150	0.85	1.10	0.195	No
798	56.73	3.24	0.83	2.41	0.69	0.253	1.68	0.150	0.85	1.10	0.195	No
799	56.78	3.25	0.84	2.41	0.69	0.253	1.68	0.150	0.85	1.10	0.195	No
800	56.83	3.25	0.84	2.41	0.69	0.252	1.68	0.150	0.85	1.10	0.195	No
801	56.88	3.25	0.84	2.41	0.69	0.252	1.68	0.150	0.85	1.10	0.195	No
802	56.89	3.25	0.84	2.42	0.69	0.252	1.68	0.150	0.85	1.10	0.195	No
803	56.95	3.26	0.84	2.42	0.69	0.252	1.68	0.150	0.85	1.10	0.195	No
804	57.01	3.26	0.84	2.42	0.68	0.252	1.68	0.150	0.85	1.10	0.194	No
805	57.07	3.27	0.84	2.42	0.68	0.252	1.68	0.150	0.85	1.10	0.194	No
806	57.11	3.27	0.85	2.42	0.68	0.252	1.68	0.150	0.85	1.10	0.194	No
807	57.17	3.27	0.85	2.43	0.68	0.252	1.68	0.150	0.85	1.10	0.194	No
808	57.26	3.28	0.85	2.43	0.68	0.252	1.68	0.150	0.85	1.10	0.194	No
809	57.31	3.28	0.85	2.43	0.68	0.252	1.68	0.150	0.85	1.10	0.194	No
810	57.37	3.29	0.85	2.43	0.68	0.251	1.68	0.149	0.85	1.10	0.194	No
811	57.45	3.29	0.86	2.43	0.68	0.251	1.68	0.149	0.85	1.10	0.194	No
812	57.51	3.30	0.86	2.44	0.68	0.251	1.68	0.149	0.85	1.10	0.194	No
813	57.53	3.30	0.86	2.44	0.68	0.251	1.68	0.149	0.85	1.10	0.194	No
814	57.59	3.30	0.86	2.44	0.68	0.251	1.68	0.149	0.85	1.10	0.194	No
815	57.63	3.30	0.86	2.44	0.68	0.251	1.68	0.149	0.85	1.10	0.194	No
816	57.68	3.31	0.86	2.44	0.68	0.251	1.68	0.149	0.85	1.10	0.194	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	57.73	3.31	0.87	2.44	0.68	0.251	1.68	0.149	0.85	1.10	0.194	No
818	57.78	3.31	0.87	2.45	0.68	0.251	1.68	0.149	0.85	1.10	0.194	No
819	57.86	3.32	0.87	2.45	0.68	0.251	1.68	0.149	0.85	1.10	0.194	No
820	57.92	3.32	0.87	2.45	0.68	0.250	1.68	0.149	0.85	1.10	2.000	Yes
821	57.98	3.33	0.87	2.45	0.68	0.250	1.68	0.149	0.85	1.10	2.000	Yes
822	58.06	3.33	0.88	2.45	0.68	0.250	1.68	0.149	0.85	1.10	2.000	Yes
823	58.12	3.33	0.88	2.46	0.68	0.250	1.68	0.149	0.84	1.10	2.000	Yes
824	58.21	3.34	0.88	2.46	0.67	0.250	1.68	0.149	0.84	1.10	2.000	Yes
825	58.26	3.34	0.88	2.46	0.67	0.250	1.68	0.149	0.84	1.10	2.000	Yes
826	58.35	3.35	0.88	2.46	0.67	0.250	1.68	0.148	0.84	1.10	2.000	Yes
827	58.41	3.35	0.89	2.47	0.67	0.250	1.68	0.148	0.84	1.10	2.000	Yes
828	58.50	3.36	0.89	2.47	0.67	0.249	1.68	0.148	0.84	1.10	2.000	Yes
829	58.56	3.36	0.89	2.47	0.67	0.249	1.68	0.148	0.84	1.10	2.000	Yes
830	58.64	3.37	0.89	2.47	0.67	0.249	1.68	0.148	0.84	1.10	2.000	Yes
831	58.73	3.37	0.90	2.48	0.67	0.249	1.68	0.148	0.84	1.10	2.000	Yes
832	58.80	3.38	0.90	2.48	0.67	0.249	1.68	0.148	0.84	1.10	2.000	Yes
833	58.84	3.38	0.90	2.48	0.67	0.249	1.68	0.148	0.84	1.10	2.000	Yes
834	58.85	3.38	0.90	2.48	0.67	0.249	1.68	0.148	0.84	1.10	0.193	No
835	58.93	3.38	0.90	2.48	0.67	0.249	1.68	0.148	0.84	1.10	0.193	No
836	58.98	3.39	0.90	2.48	0.67	0.249	1.68	0.148	0.84	1.10	0.193	No
837	59.02	3.39	0.91	2.48	0.67	0.249	1.68	0.148	0.84	1.10	0.193	No
838	59.12	3.40	0.91	2.49	0.67	0.248	1.68	0.148	0.84	1.10	0.193	No
839	59.17	3.40	0.91	2.49	0.67	0.248	1.68	0.148	0.84	1.10	0.193	No
840	59.27	3.40	0.91	2.49	0.67	0.248	1.68	0.148	0.84	1.10	0.193	No
841	59.31	3.41	0.91	2.49	0.66	0.248	1.68	0.147	0.84	1.10	0.193	No
842	59.41	3.41	0.92	2.50	0.66	0.248	1.68	0.147	0.84	1.10	0.192	No
843	59.46	3.42	0.92	2.50	0.66	0.248	1.68	0.147	0.84	1.10	0.192	No
844	59.55	3.42	0.92	2.50	0.66	0.248	1.68	0.147	0.84	1.10	0.192	No
845	59.65	3.43	0.93	2.50	0.66	0.248	1.68	0.147	0.84	1.10	0.192	No
846	59.70	3.43	0.93	2.50	0.66	0.247	1.68	0.147	0.84	1.10	0.192	No
847	59.80	3.44	0.93	2.51	0.66	0.247	1.68	0.147	0.84	1.10	0.192	No
848	59.89	3.44	0.93	2.51	0.66	0.247	1.68	0.147	0.84	1.10	0.192	No
849	59.94	3.44	0.93	2.51	0.66	0.247	1.68	0.147	0.84	1.10	0.192	No
850	60.01	3.45	0.94	2.51	0.66	0.247	1.68	0.147	0.84	1.10	0.192	No
851	60.02	3.45	0.94	2.51	0.66	0.247	1.68	0.147	0.84	1.10	0.192	No
852	60.08	3.45	0.94	2.51	0.66	0.247	1.68	0.147	0.84	1.10	0.192	No
853	60.12	3.46	0.94	2.52	0.66	0.247	1.68	0.147	0.84	1.10	0.192	No
854	60.17	3.46	0.94	2.52	0.66	0.247	1.68	0.147	0.84	1.10	0.192	No
855	60.27	3.46	0.94	2.52	0.66	0.247	1.68	0.147	0.84	1.10	0.192	No
856	60.31	3.47	0.95	2.52	0.66	0.247	1.68	0.147	0.84	1.10	0.192	No
857	60.37	3.47	0.95	2.52	0.66	0.246	1.68	0.146	0.84	1.10	0.192	No
858	60.46	3.47	0.95	2.52	0.66	0.246	1.68	0.146	0.84	1.10	0.192	No
859	60.51	3.48	0.95	2.53	0.66	0.246	1.68	0.146	0.84	1.10	0.192	No
860	60.61	3.48	0.95	2.53	0.65	0.246	1.68	0.146	0.84	1.10	0.192	No
861	60.65	3.49	0.96	2.53	0.65	0.246	1.68	0.146	0.84	1.10	0.192	No
862	60.75	3.49	0.96	2.53	0.65	0.246	1.68	0.146	0.84	1.10	0.191	No
863	60.81	3.49	0.96	2.53	0.65	0.246	1.68	0.146	0.84	1.10	0.191	No
864	60.89	3.50	0.96	2.53	0.65	0.246	1.68	0.146	0.84	1.10	0.191	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	60.94	3.50	0.97	2.54	0.65	0.246	1.68	0.146	0.84	1.10	0.191	No
866	61.03	3.51	0.97	2.54	0.65	0.246	1.68	0.146	0.84	1.10	0.191	No
867	61.09	3.51	0.97	2.54	0.65	0.245	1.68	0.146	0.84	1.10	0.191	No
868	61.19	3.51	0.97	2.54	0.65	0.245	1.68	0.146	0.84	1.10	0.191	No
869	61.24	3.52	0.97	2.54	0.65	0.245	1.68	0.146	0.84	1.10	0.191	No
870	61.33	3.52	0.98	2.54	0.65	0.245	1.68	0.146	0.84	1.10	0.191	No
871	61.38	3.52	0.98	2.55	0.65	0.245	1.68	0.146	0.84	1.10	0.191	No
872	61.47	3.53	0.98	2.55	0.65	0.245	1.68	0.146	0.84	1.10	0.191	No
873	61.53	3.53	0.98	2.55	0.65	0.245	1.68	0.146	0.84	1.10	0.191	No
874	61.62	3.54	0.99	2.55	0.65	0.245	1.68	0.145	0.84	1.10	0.191	No
875	61.70	3.54	0.99	2.55	0.65	0.245	1.68	0.145	0.84	1.10	0.191	No
876	61.77	3.55	0.99	2.56	0.65	0.244	1.68	0.145	0.84	1.10	0.191	No
877	61.86	3.55	0.99	2.56	0.64	0.244	1.68	0.145	0.84	1.10	0.191	No
878	61.95	3.56	1.00	2.56	0.64	0.244	1.68	0.145	0.84	1.10	0.191	No
879	61.97	3.56	1.00	2.56	0.64	0.244	1.68	0.145	0.84	1.10	0.191	No
880	62.01	3.56	1.00	2.56	0.64	0.244	1.68	0.145	0.84	1.10	2.000	No
881	62.10	3.57	1.00	2.57	0.64	0.244	1.68	0.145	0.84	1.10	2.000	Yes
882	62.24	3.58	1.01	2.57	0.64	0.244	1.68	0.145	0.84	1.10	2.000	Yes
883	62.34	3.58	1.01	2.57	0.64	0.244	1.68	0.145	0.84	1.10	2.000	Yes
884	62.49	3.59	1.01	2.58	0.64	0.243	1.68	0.145	0.84	1.10	2.000	Yes
885	62.54	3.60	1.02	2.58	0.64	0.243	1.68	0.145	0.84	1.10	2.000	Yes
886	62.66	3.60	1.02	2.58	0.64	0.243	1.68	0.144	0.84	1.10	2.000	Yes
887	62.74	3.61	1.02	2.59	0.64	0.243	1.68	0.144	0.84	1.10	2.000	Yes
888	62.87	3.62	1.03	2.59	0.64	0.243	1.68	0.144	0.84	1.10	2.000	No
889	62.92	3.62	1.03	2.59	0.64	0.243	1.68	0.144	0.84	1.10	2.000	No
890	63.03	3.63	1.03	2.60	0.64	0.243	1.68	0.144	0.84	1.10	2.000	No
891	63.15	3.63	1.03	2.60	0.63	0.242	1.68	0.144	0.84	1.10	2.000	No
892	63.26	3.64	1.04	2.60	0.63	0.242	1.68	0.144	0.84	1.10	2.000	No
893	63.37	3.65	1.04	2.61	0.63	0.242	1.68	0.144	0.83	1.10	2.000	No
894	63.45	3.65	1.04	2.61	0.63	0.242	1.68	0.144	0.83	1.10	2.000	No
895	63.54	3.66	1.05	2.61	0.63	0.242	1.68	0.144	0.83	1.10	2.000	No
896	63.61	3.66	1.05	2.61	0.63	0.242	1.68	0.144	0.83	1.10	2.000	Yes
897	63.69	3.67	1.05	2.62	0.63	0.241	1.68	0.144	0.83	1.10	2.000	Yes
898	63.79	3.67	1.05	2.62	0.63	0.241	1.68	0.143	0.83	1.10	2.000	Yes
899	63.89	3.68	1.06	2.62	0.63	0.241	1.68	0.143	0.83	1.10	2.000	Yes
900	63.98	3.69	1.06	2.63	0.63	0.241	1.68	0.143	0.83	1.10	2.000	Yes
901	64.07	3.69	1.06	2.63	0.63	0.241	1.68	0.143	0.83	1.10	2.000	Yes
902	64.15	3.70	1.07	2.63	0.63	0.241	1.68	0.143	0.83	1.10	2.000	Yes
903	64.23	3.70	1.07	2.63	0.63	0.241	1.68	0.143	0.83	1.10	2.000	No
904	64.26	3.70	1.07	2.63	0.63	0.241	1.68	0.143	0.83	1.10	2.000	No
905	64.29	3.70	1.07	2.63	0.63	0.241	1.68	0.143	0.83	1.10	2.000	No
906	64.33	3.71	1.07	2.64	0.63	0.241	1.68	0.143	0.83	1.10	2.000	No
907	64.43	3.71	1.07	2.64	0.63	0.240	1.68	0.143	0.83	1.10	2.000	No
908	64.47	3.71	1.08	2.64	0.63	0.240	1.68	0.143	0.83	1.10	2.000	No
909	64.53	3.72	1.08	2.64	0.63	0.240	1.68	0.143	0.83	1.10	2.000	No
910	64.62	3.72	1.08	2.64	0.62	0.240	1.68	0.143	0.83	1.10	2.000	No
911	64.72	3.73	1.08	2.64	0.62	0.240	1.68	0.143	0.83	1.10	2.000	No
912	64.78	3.73	1.09	2.65	0.62	0.240	1.68	0.143	0.83	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	64.86	3.74	1.09	2.65	0.62	0.240	1.68	0.143	0.83	1.10	2.000	No
914	64.96	3.74	1.09	2.65	0.62	0.240	1.68	0.143	0.83	1.10	2.000	No
915	65.06	3.75	1.09	2.65	0.62	0.240	1.68	0.142	0.83	1.10	2.000	No
916	65.11	3.75	1.10	2.65	0.62	0.240	1.68	0.142	0.83	1.10	2.000	No
917	65.21	3.76	1.10	2.66	0.62	0.240	1.68	0.142	0.83	1.10	2.000	No
918	65.31	3.76	1.10	2.66	0.62	0.239	1.68	0.142	0.83	1.10	2.000	No
919	65.40	3.77	1.10	2.66	0.62	0.239	1.68	0.142	0.83	1.10	2.000	No
920	65.50	3.77	1.11	2.66	0.62	0.239	1.68	0.142	0.83	1.10	2.000	No
921	65.58	3.78	1.11	2.67	0.62	0.239	1.68	0.142	0.83	1.10	2.000	No
922	65.68	3.78	1.11	2.67	0.62	0.239	1.68	0.142	0.83	1.10	2.000	No
923	65.78	3.79	1.12	2.67	0.62	0.239	1.68	0.142	0.83	1.10	2.000	No
924	65.84	3.79	1.12	2.67	0.62	0.239	1.68	0.142	0.83	1.10	2.000	No
925	65.86	3.79	1.12	2.67	0.62	0.239	1.68	0.142	0.83	1.10	2.000	No
926	65.87	3.79	1.12	2.67	0.62	0.239	1.68	0.142	0.83	1.10	2.000	No
927	65.98	3.80	1.12	2.68	0.62	0.239	1.68	0.142	0.83	1.10	2.000	No
928	66.10	3.80	1.13	2.68	0.61	0.238	1.68	0.142	0.83	1.10	2.000	No
929	66.21	3.81	1.13	2.68	0.61	0.238	1.68	0.142	0.83	1.10	2.000	No
930	66.34	3.82	1.13	2.68	0.61	0.238	1.68	0.142	0.83	1.10	2.000	No
931	66.48	3.83	1.14	2.69	0.61	0.238	1.68	0.141	0.83	1.10	2.000	No
932	66.62	3.83	1.14	2.69	0.61	0.238	1.68	0.141	0.83	1.10	2.000	No
933	66.68	3.84	1.14	2.69	0.61	0.238	1.68	0.141	0.83	1.10	2.000	No
934	66.87	3.85	1.15	2.70	0.61	0.238	1.68	0.141	0.83	1.10	2.000	No
935	66.96	3.85	1.15	2.70	0.61	0.237	1.68	0.141	0.83	1.10	2.000	No
936	67.11	3.86	1.16	2.70	0.61	0.237	1.68	0.141	0.83	1.10	2.000	No
937	67.21	3.87	1.16	2.71	0.61	0.237	1.68	0.141	0.83	1.10	2.000	No
938	67.35	3.87	1.17	2.71	0.61	0.237	1.68	0.141	0.83	1.10	2.000	No
939	67.45	3.88	1.17	2.71	0.61	0.237	1.68	0.141	0.83	1.10	2.000	No
940	67.59	3.89	1.17	2.72	0.61	0.237	1.68	0.141	0.83	1.10	2.000	No
941	67.68	3.89	1.18	2.72	0.61	0.237	1.68	0.141	0.83	1.10	2.000	Yes
942	67.83	3.90	1.18	2.72	0.60	0.236	1.68	0.141	0.83	1.10	2.000	Yes
943	67.92	3.91	1.18	2.73	0.60	0.236	1.68	0.140	0.83	1.10	2.000	Yes
944	68.02	3.92	1.19	2.73	0.60	0.236	1.68	0.140	0.83	1.10	2.000	Yes
945	68.07	3.92	1.19	2.73	0.60	0.236	1.68	0.140	0.83	1.10	2.000	Yes
946	68.16	3.93	1.19	2.73	0.60	0.236	1.68	0.140	0.83	1.10	2.000	No
947	68.26	3.93	1.19	2.74	0.60	0.236	1.68	0.140	0.83	1.10	2.000	No
948	68.35	3.94	1.20	2.74	0.60	0.236	1.68	0.140	0.83	1.10	2.000	No
949	68.45	3.94	1.20	2.74	0.60	0.236	1.68	0.140	0.83	1.10	2.000	No
950	68.55	3.95	1.20	2.75	0.60	0.235	1.68	0.140	0.83	1.10	2.000	No
951	68.65	3.96	1.21	2.75	0.60	0.235	1.68	0.140	0.83	1.10	2.000	No
952	68.78	3.97	1.21	2.76	0.60	0.235	1.68	0.140	0.83	1.10	2.000	No
953	68.78	3.97	1.21	2.76	0.60	0.235	1.68	0.140	0.83	1.10	2.000	No
954	68.79	3.97	1.21	2.76	0.60	0.235	1.68	0.140	0.83	1.10	2.000	No
955	68.83	3.97	1.21	2.76	0.60	0.235	1.68	0.140	0.83	1.10	2.000	No
956	68.93	3.98	1.21	2.76	0.60	0.235	1.68	0.140	0.83	1.10	2.000	No
957	68.98	3.98	1.22	2.76	0.60	0.235	1.68	0.140	0.83	1.10	2.000	No
958	69.04	3.98	1.22	2.76	0.60	0.235	1.68	0.140	0.83	1.10	2.000	No
959	69.12	3.99	1.22	2.77	0.60	0.235	1.68	0.140	0.83	1.10	2.000	No
960	69.22	3.99	1.22	2.77	0.60	0.235	1.68	0.139	0.82	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
961	69.28	4.00	1.23	2.77	0.60	0.235	1.68	0.139	0.82	1.10	2.000	No
962	69.36	4.00	1.23	2.77	0.60	0.234	1.68	0.139	0.82	1.10	2.000	No
963	69.45	4.01	1.23	2.78	0.59	0.234	1.68	0.139	0.82	1.10	2.000	No
964	69.60	4.02	1.24	2.78	0.59	0.234	1.68	0.139	0.82	1.10	2.000	No
965	69.70	4.02	1.24	2.79	0.59	0.234	1.68	0.139	0.82	1.10	2.000	No
966	69.80	4.03	1.24	2.79	0.59	0.234	1.68	0.139	0.82	1.10	2.000	No
967	69.89	4.04	1.24	2.79	0.59	0.234	1.68	0.139	0.82	1.10	2.000	No
968	69.98	4.04	1.25	2.79	0.59	0.234	1.68	0.139	0.82	1.10	2.000	No
969	70.08	4.05	1.25	2.80	0.59	0.234	1.68	0.139	0.82	1.10	2.000	Yes
970	70.18	4.05	1.25	2.80	0.59	0.234	1.68	0.139	0.82	1.10	2.000	Yes
971	70.32	4.06	1.26	2.80	0.59	0.233	1.68	0.139	0.82	1.10	2.000	Yes
972	70.42	4.07	1.26	2.81	0.59	0.233	1.68	0.139	0.82	1.10	2.000	Yes
973	70.54	4.08	1.26	2.81	0.59	0.233	1.68	0.139	0.82	1.10	2.000	Yes
974	70.66	4.08	1.27	2.81	0.59	0.233	1.68	0.139	0.82	1.10	2.000	No
975	70.75	4.09	1.27	2.82	0.59	0.233	1.68	0.138	0.82	1.10	2.000	No
976	70.80	4.09	1.27	2.82	0.59	0.233	1.68	0.138	0.82	1.10	2.000	No
977	70.89	4.10	1.28	2.82	0.59	0.233	1.68	0.138	0.82	1.10	2.000	No
978	70.99	4.10	1.28	2.82	0.59	0.233	1.68	0.138	0.82	1.10	2.000	No
979	71.08	4.11	1.28	2.82	0.59	0.233	1.68	0.138	0.82	1.10	2.000	No
980	71.17	4.11	1.28	2.83	0.59	0.233	1.68	0.138	0.82	1.10	2.000	No
981	71.23	4.11	1.29	2.83	0.59	0.233	1.68	0.138	0.82	1.10	2.000	No
982	71.33	4.12	1.29	2.83	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
983	71.42	4.12	1.29	2.83	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
984	71.52	4.13	1.30	2.83	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
985	71.58	4.13	1.30	2.83	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
986	71.67	4.14	1.30	2.84	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
987	71.81	4.14	1.30	2.84	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
988	71.82	4.14	1.30	2.84	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
989	71.86	4.15	1.31	2.84	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
990	71.91	4.15	1.31	2.84	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
991	71.97	4.15	1.31	2.84	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
992	72.05	4.16	1.31	2.85	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
993	72.10	4.16	1.31	2.85	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
994	72.20	4.17	1.32	2.85	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
995	72.25	4.17	1.32	2.85	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
996	72.34	4.17	1.32	2.85	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
997	72.44	4.18	1.32	2.85	0.58	0.232	1.68	0.138	0.82	1.10	2.000	No
998	72.53	4.18	1.33	2.86	0.58	0.231	1.68	0.138	0.82	1.10	2.000	No
999	72.63	4.19	1.33	2.86	0.58	0.231	1.68	0.138	0.82	1.10	2.000	No
1000	72.69	4.19	1.33	2.86	0.58	0.231	1.68	0.138	0.82	1.10	2.000	No
1001	72.82	4.20	1.34	2.86	0.58	0.231	1.68	0.137	0.82	1.10	2.000	No
1002	72.92	4.20	1.34	2.87	0.58	0.231	1.68	0.137	0.82	1.10	2.000	No
1003	73.06	4.21	1.34	2.87	0.58	0.231	1.68	0.137	0.82	1.10	2.000	No
1004	73.16	4.22	1.35	2.87	0.58	0.231	1.68	0.137	0.82	1.10	2.000	No
1005	73.30	4.23	1.35	2.87	0.58	0.231	1.68	0.137	0.82	1.10	2.000	No
1006	73.35	4.23	1.35	2.88	0.58	0.231	1.68	0.137	0.82	1.10	2.000	No
1007	73.38	4.23	1.35	2.88	0.57	0.231	1.68	0.137	0.82	1.10	2.000	No
1008	73.47	4.24	1.36	2.88	0.57	0.231	1.68	0.137	0.82	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1009	73.53	4.24	1.36	2.88	0.57	0.231	1.68	0.137	0.82	1.10	2.000	No
1010	73.62	4.24	1.36	2.88	0.57	0.231	1.68	0.137	0.82	1.10	2.000	No
1011	73.71	4.25	1.36	2.88	0.57	0.231	1.68	0.137	0.82	1.10	2.000	No
1012	73.77	4.25	1.37	2.89	0.57	0.231	1.68	0.137	0.82	1.10	2.000	No
1013	73.86	4.26	1.37	2.89	0.57	0.230	1.68	0.137	0.82	1.10	2.000	No
1014	73.96	4.26	1.37	2.89	0.57	0.230	1.68	0.137	0.82	1.10	2.000	No
1015	74.06	4.27	1.37	2.89	0.57	0.230	1.68	0.137	0.82	1.10	2.000	No
1016	74.13	4.27	1.38	2.90	0.57	0.230	1.68	0.137	0.82	1.10	2.000	No
1017	74.24	4.28	1.38	2.90	0.57	0.230	1.68	0.137	0.82	1.10	2.000	No
1018	74.34	4.28	1.38	2.90	0.57	0.230	1.68	0.137	0.82	1.10	2.000	No
1019	74.44	4.29	1.39	2.90	0.57	0.230	1.68	0.137	0.82	1.10	2.000	No
1020	74.58	4.30	1.39	2.91	0.57	0.230	1.68	0.137	0.82	1.10	2.000	No
1021	74.68	4.30	1.39	2.91	0.57	0.230	1.68	0.137	0.82	1.10	2.000	No
1022	74.80	4.31	1.40	2.91	0.57	0.230	1.68	0.137	0.82	1.10	2.000	No
1023	74.92	4.32	1.40	2.91	0.57	0.230	1.68	0.136	0.82	1.10	2.000	No
1024	75.07	4.32	1.41	2.92	0.57	0.230	1.68	0.136	0.82	1.10	2.000	No
1025	75.08	4.32	1.41	2.92	0.57	0.230	1.68	0.136	0.82	1.10	2.000	No
1026	75.11	4.33	1.41	2.92	0.57	0.230	1.68	0.136	0.82	1.10	2.000	No
1027	75.16	4.33	1.41	2.92	0.57	0.229	1.68	0.136	0.82	1.10	2.000	No
1028	75.25	4.33	1.41	2.92	0.57	0.229	1.68	0.136	0.82	1.10	2.000	No
1029	75.32	4.34	1.41	2.92	0.57	0.229	1.68	0.136	0.82	1.10	2.000	No
1030	75.40	4.34	1.42	2.93	0.57	0.229	1.68	0.136	0.82	1.10	2.000	No
1031	75.50	4.35	1.42	2.93	0.57	0.229	1.68	0.136	0.82	1.10	2.000	No
1032	75.59	4.35	1.42	2.93	0.57	0.229	1.68	0.136	0.82	1.10	2.000	No
1033	75.69	4.36	1.43	2.93	0.56	0.229	1.68	0.136	0.82	1.10	2.000	No
1034	75.78	4.36	1.43	2.93	0.56	0.229	1.68	0.136	0.82	1.10	2.000	No
1035	75.88	4.37	1.43	2.94	0.56	0.229	1.68	0.136	0.82	1.10	2.000	No
1036	75.96	4.37	1.43	2.94	0.56	0.229	1.68	0.136	0.82	1.10	2.000	No
1037	76.05	4.38	1.44	2.94	0.56	0.229	1.68	0.136	0.82	1.10	2.000	No
1038	76.14	4.38	1.44	2.94	0.56	0.229	1.68	0.136	0.81	1.10	2.000	No
1039	76.26	4.39	1.44	2.95	0.56	0.229	1.68	0.136	0.81	1.10	2.000	No
1040	76.36	4.39	1.45	2.95	0.56	0.229	1.68	0.136	0.81	1.10	2.000	No
1041	76.41	4.40	1.45	2.95	0.56	0.229	1.68	0.136	0.81	1.10	2.000	No
1042	76.51	4.40	1.45	2.95	0.56	0.229	1.68	0.136	0.81	1.10	2.000	No
1043	76.65	4.41	1.46	2.95	0.56	0.229	1.68	0.136	0.81	1.10	2.000	No
1044	76.72	4.41	1.46	2.96	0.56	0.228	1.68	0.136	0.81	1.10	2.000	No
1045	76.79	4.42	1.46	2.96	0.56	0.228	1.68	0.136	0.81	1.10	2.000	No
1046	76.89	4.42	1.46	2.96	0.56	0.228	1.68	0.136	0.81	1.10	2.000	No
1047	76.98	4.43	1.47	2.96	0.56	0.228	1.68	0.136	0.81	1.10	2.000	No
1048	77.08	4.43	1.47	2.96	0.56	0.228	1.68	0.136	0.81	1.10	2.000	No
1049	77.18	4.44	1.47	2.97	0.56	0.228	1.68	0.136	0.81	1.10	2.000	No
1050	77.28	4.44	1.48	2.97	0.56	0.228	1.68	0.136	0.81	1.10	2.000	No
1051	77.37	4.45	1.48	2.97	0.56	0.228	1.68	0.136	0.81	1.10	2.000	No
1052	77.42	4.45	1.48	2.97	0.56	0.228	1.68	0.136	0.81	1.10	2.000	No
1053	77.42	4.45	1.48	2.97	0.56	0.228	1.68	0.136	0.81	1.10	2.000	No
1054	77.44	4.45	1.48	2.97	0.56	0.228	1.68	0.136	0.81	1.10	2.000	No
1055	77.48	4.46	1.48	2.98	0.56	0.228	1.68	0.136	0.81	1.10	2.000	No
1056	77.52	4.46	1.48	2.98	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1057	77.54	4.46	1.48	2.98	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1058	77.57	4.46	1.48	2.98	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1059	77.62	4.47	1.49	2.98	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1060	77.65	4.47	1.49	2.98	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1061	77.67	4.47	1.49	2.98	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1062	77.71	4.47	1.49	2.98	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1063	77.71	4.47	1.49	2.98	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1064	77.76	4.47	1.49	2.98	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1065	77.81	4.48	1.49	2.99	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1066	77.90	4.48	1.49	2.99	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1067	77.95	4.49	1.50	2.99	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1068	78.01	4.49	1.50	2.99	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1069	78.10	4.49	1.50	2.99	0.56	0.228	1.68	0.135	0.81	1.10	2.000	No
1070	78.16	4.50	1.50	3.00	0.55	0.227	1.68	0.135	0.81	1.10	2.000	No
1071	78.24	4.50	1.51	3.00	0.55	0.227	1.68	0.135	0.81	1.10	2.000	Yes
1072	78.29	4.51	1.51	3.00	0.55	0.227	1.68	0.135	0.81	1.10	2.000	Yes
1073	78.39	4.51	1.51	3.00	0.55	0.227	1.68	0.135	0.81	1.10	2.000	Yes
1074	78.47	4.52	1.51	3.00	0.55	0.227	1.68	0.135	0.81	1.10	2.000	Yes
1075	78.53	4.52	1.51	3.01	0.55	0.227	1.68	0.135	0.81	1.10	2.000	Yes
1076	78.62	4.53	1.52	3.01	0.55	0.227	1.68	0.135	0.81	1.10	2.000	Yes
1077	78.68	4.53	1.52	3.01	0.55	0.227	1.68	0.135	0.81	1.10	2.000	Yes
1078	78.69	4.53	1.52	3.01	0.55	0.227	1.68	0.135	0.81	1.10	2.000	Yes
1079	78.78	4.54	1.52	3.01	0.55	0.227	1.68	0.135	0.81	1.10	2.000	No
1080	78.81	4.54	1.52	3.02	0.55	0.227	1.68	0.135	0.81	1.10	2.000	No
1081	78.92	4.55	1.53	3.02	0.55	0.227	1.68	0.135	0.81	1.10	2.000	No
1082	79.03	4.55	1.53	3.02	0.55	0.227	1.68	0.135	0.81	1.10	2.000	No
1083	79.16	4.56	1.53	3.03	0.55	0.227	1.68	0.135	0.81	1.10	2.000	Yes
1084	79.26	4.57	1.54	3.03	0.55	0.227	1.68	0.135	0.81	1.10	2.000	Yes
1085	79.35	4.57	1.54	3.03	0.55	0.227	1.68	0.135	0.81	1.10	2.000	Yes
1086	79.45	4.58	1.54	3.04	0.55	0.227	1.68	0.135	0.81	1.10	2.000	Yes
1087	79.54	4.58	1.55	3.04	0.55	0.226	1.68	0.135	0.81	1.10	2.000	No
1088	79.64	4.59	1.55	3.04	0.55	0.226	1.68	0.135	0.81	1.10	2.000	No
1089	79.74	4.60	1.55	3.05	0.55	0.226	1.68	0.135	0.81	1.10	2.000	No
1090	79.88	4.61	1.56	3.05	0.55	0.226	1.68	0.134	0.81	1.10	2.000	No
1091	79.98	4.61	1.56	3.05	0.55	0.226	1.68	0.134	0.81	1.10	2.000	No
1092	80.12	4.62	1.56	3.06	0.55	0.226	1.68	0.134	0.81	1.10	2.000	No
1093	80.22	4.63	1.57	3.06	0.55	0.226	1.68	0.134	0.81	1.10	2.000	No
1094	80.36	4.64	1.57	3.07	0.55	0.226	1.68	0.134	0.81	1.10	2.000	No
1095	80.46	4.64	1.57	3.07	0.55	0.226	1.68	0.134	0.81	1.10	2.000	No
1096	80.60	4.65	1.58	3.07	0.55	0.226	1.68	0.134	0.81	1.10	2.000	No
1097	80.70	4.66	1.58	3.08	0.55	0.226	1.68	0.134	0.81	1.10	2.000	No
1098	80.83	4.67	1.59	3.08	0.55	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1099	80.94	4.67	1.59	3.09	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1100	81.01	4.68	1.59	3.09	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1101	81.04	4.68	1.59	3.09	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1102	81.09	4.68	1.59	3.09	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1103	81.13	4.69	1.60	3.09	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1104	81.18	4.69	1.60	3.09	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1105	81.23	4.69	1.60	3.09	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1106	81.28	4.70	1.60	3.10	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1107	81.33	4.70	1.60	3.10	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1108	81.37	4.70	1.60	3.10	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1109	81.42	4.70	1.60	3.10	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1110	81.47	4.71	1.61	3.10	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1111	81.52	4.71	1.61	3.10	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1112	81.56	4.71	1.61	3.10	0.54	0.225	1.68	0.134	0.81	1.10	2.000	Yes
1113	81.61	4.72	1.61	3.11	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1114	81.64	4.72	1.61	3.11	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1115	81.70	4.72	1.61	3.11	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1116	81.75	4.73	1.61	3.11	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1117	81.79	4.73	1.62	3.11	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1118	81.82	4.73	1.62	3.11	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1119	81.86	4.73	1.62	3.11	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1120	81.91	4.74	1.62	3.12	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1121	81.95	4.74	1.62	3.12	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1122	82.00	4.74	1.62	3.12	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1123	82.09	4.75	1.63	3.12	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1124	82.15	4.75	1.63	3.12	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1125	82.19	4.75	1.63	3.12	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1126	82.26	4.76	1.63	3.13	0.54	0.225	1.68	0.134	0.81	1.10	2.000	No
1127	82.34	4.76	1.63	3.13	0.54	0.225	1.68	0.133	0.81	1.10	2.000	No
1128	82.39	4.76	1.63	3.13	0.54	0.225	1.68	0.133	0.81	1.10	2.000	No
1129	82.48	4.77	1.64	3.13	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1130	82.58	4.77	1.64	3.13	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1131	82.62	4.78	1.64	3.13	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1132	82.70	4.78	1.64	3.14	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1133	82.77	4.78	1.65	3.14	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1134	82.87	4.79	1.65	3.14	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1135	82.96	4.80	1.65	3.14	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1136	83.06	4.80	1.66	3.15	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1137	83.16	4.81	1.66	3.15	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1138	83.25	4.81	1.66	3.15	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1139	83.34	4.82	1.66	3.15	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1140	83.44	4.82	1.67	3.15	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1141	83.54	4.83	1.67	3.16	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1142	83.64	4.83	1.67	3.16	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1143	83.73	4.84	1.68	3.16	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1144	83.83	4.84	1.68	3.16	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1145	83.85	4.85	1.68	3.17	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1146	83.89	4.85	1.68	3.17	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1147	83.94	4.85	1.68	3.17	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1148	84.04	4.86	1.69	3.17	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1149	84.09	4.86	1.69	3.17	0.54	0.224	1.68	0.133	0.80	1.10	2.000	No
1150	84.13	4.86	1.69	3.17	0.53	0.224	1.68	0.133	0.80	1.10	2.000	No
1151	84.18	4.87	1.69	3.17	0.53	0.224	1.68	0.133	0.80	1.10	2.000	No
1152	84.25	4.87	1.69	3.18	0.53	0.224	1.68	0.133	0.80	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1153	84.33	4.87	1.69	3.18	0.53	0.224	1.68	0.133	0.80	1.10	2.000	No
1154	84.37	4.88	1.70	3.18	0.53	0.224	1.68	0.133	0.80	1.10	2.000	No
1155	84.46	4.88	1.70	3.18	0.53	0.224	1.68	0.133	0.80	1.10	2.000	No
1156	84.52	4.89	1.70	3.18	0.53	0.224	1.68	0.133	0.80	1.10	2.000	No
1157	84.57	4.89	1.70	3.19	0.53	0.224	1.68	0.133	0.80	1.10	2.000	No
1158	84.67	4.89	1.71	3.19	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1159	84.71	4.90	1.71	3.19	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1160	84.81	4.90	1.71	3.19	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1161	84.86	4.91	1.71	3.19	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1162	84.91	4.91	1.71	3.20	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1163	85.00	4.91	1.72	3.20	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1164	85.05	4.92	1.72	3.20	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1165	85.15	4.92	1.72	3.20	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1166	85.19	4.93	1.72	3.20	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1167	85.29	4.93	1.73	3.21	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1168	85.35	4.94	1.73	3.21	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1169	85.42	4.94	1.73	3.21	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1170	85.48	4.94	1.73	3.21	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1171	85.55	4.95	1.73	3.21	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1172	85.63	4.95	1.74	3.22	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1173	85.68	4.95	1.74	3.22	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1174	85.77	4.96	1.74	3.22	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1175	85.82	4.96	1.74	3.22	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1176	85.89	4.97	1.74	3.22	0.53	0.223	1.68	0.133	0.80	1.10	2.000	No
1177	85.96	4.97	1.75	3.22	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1178	86.03	4.97	1.75	3.23	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1179	86.11	4.98	1.75	3.23	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1180	86.16	4.98	1.75	3.23	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1181	86.25	4.99	1.76	3.23	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1182	86.36	4.99	1.76	3.23	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1183	86.50	5.00	1.76	3.24	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1184	86.51	5.00	1.76	3.24	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1185	86.52	5.00	1.76	3.24	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1186	86.57	5.01	1.76	3.24	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1187	86.65	5.01	1.77	3.24	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1188	86.71	5.01	1.77	3.24	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1189	86.80	5.02	1.77	3.25	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1190	86.90	5.02	1.78	3.25	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1191	86.99	5.03	1.78	3.25	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1192	87.04	5.03	1.78	3.25	0.53	0.223	1.68	0.132	0.80	1.10	2.000	No
1193	87.14	5.04	1.78	3.25	0.53	0.222	1.68	0.132	0.80	1.10	2.000	No
1194	87.19	5.04	1.78	3.26	0.53	0.222	1.68	0.132	0.80	1.10	2.000	No
1195	87.28	5.04	1.79	3.26	0.53	0.222	1.68	0.132	0.80	1.10	2.000	No
1196	87.38	5.05	1.79	3.26	0.53	0.222	1.68	0.132	0.80	1.10	2.000	No
1197	87.43	5.05	1.79	3.26	0.53	0.222	1.68	0.132	0.80	1.10	2.000	No
1198	87.52	5.06	1.79	3.26	0.53	0.222	1.68	0.132	0.80	1.10	2.000	No
1199	87.61	5.06	1.80	3.26	0.53	0.222	1.68	0.132	0.80	1.10	2.000	No
1200	87.66	5.07	1.80	3.27	0.53	0.222	1.68	0.132	0.80	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1201	87.76	5.07	1.80	3.27	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1202	87.84	5.07	1.80	3.27	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1203	87.91	5.08	1.81	3.27	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1204	88.00	5.08	1.81	3.27	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1205	88.11	5.09	1.81	3.28	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1206	88.19	5.09	1.82	3.28	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1207	88.25	5.10	1.82	3.28	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1208	88.34	5.10	1.82	3.28	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1209	88.44	5.11	1.82	3.28	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1210	88.54	5.11	1.83	3.29	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1211	88.64	5.12	1.83	3.29	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1212	88.72	5.12	1.83	3.29	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1213	88.82	5.13	1.84	3.29	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1214	88.91	5.13	1.84	3.29	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1215	89.01	5.14	1.84	3.30	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1216	89.10	5.14	1.84	3.30	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1217	89.19	5.15	1.85	3.30	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1218	89.30	5.15	1.85	3.30	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1219	89.39	5.16	1.85	3.31	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1220	89.49	5.16	1.86	3.31	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1221	89.59	5.17	1.86	3.31	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1222	89.69	5.17	1.86	3.31	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1223	89.73	5.18	1.86	3.31	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1224	89.78	5.18	1.87	3.31	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1225	89.83	5.18	1.87	3.32	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1226	89.88	5.19	1.87	3.32	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1227	89.93	5.19	1.87	3.32	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1228	90.00	5.19	1.87	3.32	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1229	90.07	5.20	1.87	3.32	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1230	90.12	5.20	1.88	3.32	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1231	90.22	5.20	1.88	3.33	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1232	90.27	5.21	1.88	3.33	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1233	90.36	5.21	1.88	3.33	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1234	90.46	5.22	1.89	3.33	0.52	0.222	1.68	0.132	0.80	1.10	2.000	No
1235	90.50	5.22	1.89	3.33	0.52	0.222	1.68	0.132	0.79	1.10	2.000	No
1236	90.61	5.23	1.89	3.34	0.52	0.222	1.68	0.132	0.79	1.10	2.000	No
1237	90.66	5.23	1.89	3.34	0.52	0.221	1.68	0.132	0.79	1.10	2.000	No
1238	90.75	5.23	1.90	3.34	0.52	0.221	1.68	0.132	0.79	1.10	2.000	No
1239	90.84	5.24	1.90	3.34	0.52	0.221	1.68	0.132	0.79	1.10	2.000	No
1240	90.89	5.24	1.90	3.34	0.52	0.221	1.68	0.132	0.79	1.10	2.000	No
1241	90.99	5.25	1.90	3.35	0.52	0.221	1.68	0.132	0.79	1.10	2.000	No
1242	91.04	5.25	1.90	3.35	0.52	0.221	1.68	0.132	0.79	1.10	2.000	No
1243	91.14	5.26	1.91	3.35	0.52	0.221	1.68	0.132	0.79	1.10	2.000	No
1244	91.22	5.26	1.91	3.35	0.52	0.221	1.68	0.132	0.79	1.10	2.000	No
1245	91.28	5.26	1.91	3.35	0.52	0.221	1.68	0.132	0.79	1.10	2.000	No
1246	91.37	5.27	1.91	3.35	0.52	0.221	1.68	0.132	0.79	1.10	2.000	No
1247	91.47	5.28	1.92	3.36	0.52	0.221	1.68	0.132	0.79	1.10	2.000	No
1248	91.61	5.28	1.92	3.36	0.52	0.221	1.68	0.132	0.79	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1249	91.71	5.29	1.93	3.36	0.52	0.221	1.68	0.131	0.79	1.10	2.000	No
1250	91.81	5.29	1.93	3.37	0.52	0.221	1.68	0.131	0.79	1.10	2.000	No
1251	91.87	5.30	1.93	3.37	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1252	92.00	5.30	1.93	3.37	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1253	92.10	5.31	1.94	3.37	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1254	92.20	5.32	1.94	3.37	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1255	92.33	5.32	1.94	3.38	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1256	92.38	5.33	1.95	3.38	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1257	92.43	5.33	1.95	3.38	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1258	92.48	5.33	1.95	3.38	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1259	92.56	5.33	1.95	3.38	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1260	92.63	5.34	1.95	3.38	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1261	92.67	5.34	1.96	3.39	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1262	92.72	5.34	1.96	3.39	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1263	92.77	5.35	1.96	3.39	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1264	92.86	5.35	1.96	3.39	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1265	92.92	5.35	1.96	3.39	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1266	92.97	5.36	1.96	3.39	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1267	93.05	5.36	1.97	3.39	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1268	93.10	5.37	1.97	3.40	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1269	93.16	5.37	1.97	3.40	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1270	93.25	5.37	1.97	3.40	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1271	93.35	5.38	1.98	3.40	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1272	93.40	5.38	1.98	3.40	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1273	93.49	5.39	1.98	3.41	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1274	93.56	5.39	1.98	3.41	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1275	93.64	5.40	1.99	3.41	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1276	93.73	5.40	1.99	3.41	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1277	93.83	5.41	1.99	3.41	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1278	93.88	5.41	1.99	3.42	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1279	93.97	5.41	2.00	3.42	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1280	94.07	5.42	2.00	3.42	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1281	94.17	5.43	2.00	3.42	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1282	94.26	5.43	2.01	3.43	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1283	94.36	5.44	2.01	3.43	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1284	94.45	5.44	2.01	3.43	0.51	0.221	1.68	0.131	0.79	1.10	2.000	No
1285	94.55	5.45	2.01	3.43	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1286	94.64	5.45	2.02	3.44	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1287	94.72	5.46	2.02	3.44	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1288	94.74	5.46	2.02	3.44	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1289	94.77	5.46	2.02	3.44	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1290	94.85	5.47	2.02	3.44	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1291	94.90	5.47	2.02	3.44	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1292	94.95	5.47	2.03	3.45	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1293	95.01	5.48	2.03	3.45	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1294	95.09	5.48	2.03	3.45	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1295	95.14	5.48	2.03	3.45	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1296	95.23	5.49	2.04	3.46	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1297	95.29	5.49	2.04	3.46	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1298	95.38	5.50	2.04	3.46	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1299	95.43	5.50	2.04	3.46	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1300	95.52	5.51	2.04	3.47	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1301	95.57	5.51	2.05	3.47	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1302	95.67	5.52	2.05	3.47	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1303	95.77	5.53	2.05	3.47	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1304	95.86	5.53	2.05	3.48	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1305	95.95	5.54	2.06	3.48	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1306	96.03	5.54	2.06	3.48	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1307	96.11	5.55	2.06	3.48	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1308	96.20	5.55	2.07	3.49	0.51	0.220	1.68	0.131	0.79	1.10	2.000	No
1309	96.30	5.56	2.07	3.49	0.51	0.220	1.68	0.131	0.79	1.10	2.000	Yes
1310	96.39	5.57	2.07	3.49	0.51	0.220	1.68	0.131	0.79	1.10	2.000	Yes
1311	96.50	5.57	2.07	3.50	0.51	0.220	1.68	0.131	0.79	1.10	2.000	Yes
1312	96.59	5.58	2.08	3.50	0.50	0.220	1.68	0.131	0.79	1.10	2.000	Yes
1313	96.69	5.58	2.08	3.50	0.50	0.220	1.68	0.131	0.79	1.10	2.000	Yes
1314	96.78	5.59	2.08	3.51	0.50	0.220	1.68	0.131	0.79	1.10	2.000	Yes
1315	96.87	5.60	2.09	3.51	0.50	0.220	1.68	0.131	0.79	1.10	2.000	Yes
1316	96.98	5.60	2.09	3.51	0.50	0.220	1.68	0.130	0.79	1.10	2.000	No
1317	97.02	5.61	2.09	3.51	0.50	0.220	1.68	0.130	0.79	1.10	2.000	No
1318	97.06	5.61	2.09	3.52	0.50	0.219	1.68	0.130	0.79	1.10	2.000	No
1319	97.12	5.61	2.09	3.52	0.50	0.219	1.68	0.130	0.79	1.10	2.000	No
1320	97.16	5.62	2.10	3.52	0.50	0.219	1.68	0.130	0.79	1.10	2.000	No
1321	97.21	5.62	2.10	3.52	0.50	0.219	1.68	0.130	0.79	1.10	2.000	No
1322	97.27	5.62	2.10	3.52	0.50	0.219	1.68	0.130	0.79	1.10	2.000	No
1323	97.33	5.63	2.10	3.53	0.50	0.219	1.68	0.130	0.79	1.10	2.000	No
1324	97.40	5.63	2.10	3.53	0.50	0.219	1.68	0.130	0.79	1.10	2.000	No
1325	97.45	5.63	2.10	3.53	0.50	0.219	1.68	0.130	0.79	1.10	2.000	Yes
1326	97.50	5.64	2.11	3.53	0.50	0.219	1.68	0.130	0.79	1.10	2.000	Yes
1327	97.58	5.64	2.11	3.53	0.50	0.219	1.68	0.130	0.79	1.10	2.000	Yes
1328	97.65	5.65	2.11	3.54	0.50	0.219	1.68	0.130	0.79	1.10	2.000	Yes
1329	97.69	5.65	2.11	3.54	0.50	0.219	1.68	0.130	0.79	1.10	2.000	Yes
1330	97.74	5.65	2.11	3.54	0.50	0.219	1.68	0.130	0.79	1.10	2.000	Yes
1331	97.81	5.66	2.12	3.54	0.50	0.219	1.68	0.130	0.79	1.10	2.000	Yes
1332	97.88	5.66	2.12	3.54	0.50	0.219	1.68	0.130	0.79	1.10	2.000	Yes
1333	97.93	5.67	2.12	3.55	0.50	0.219	1.68	0.130	0.79	1.10	2.000	Yes
1334	98.03	5.67	2.12	3.55	0.50	0.219	1.68	0.130	0.79	1.10	2.000	Yes
1335	98.15	5.68	2.13	3.55	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1336	98.21	5.68	2.13	3.56	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1337	98.32	5.69	2.13	3.56	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1338	98.42	5.70	2.13	3.56	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1339	98.47	5.70	2.14	3.56	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1340	98.57	5.71	2.14	3.57	0.50	0.219	1.68	0.130	0.78	1.10	2.000	No
1341	98.70	5.71	2.14	3.57	0.50	0.219	1.68	0.130	0.78	1.10	2.000	No
1342	98.78	5.72	2.15	3.57	0.50	0.219	1.68	0.130	0.78	1.10	2.000	No
1343	98.85	5.72	2.15	3.58	0.50	0.219	1.68	0.130	0.78	1.10	2.000	No
1344	98.86	5.72	2.15	3.58	0.50	0.219	1.68	0.130	0.78	1.10	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1345	98.92	5.73	2.15	3.58	0.50	0.219	1.68	0.130	0.78	1.10	2.000	No
1346	98.98	5.73	2.15	3.58	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1347	99.03	5.74	2.15	3.58	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1348	99.11	5.74	2.16	3.58	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1349	99.18	5.74	2.16	3.59	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1350	99.23	5.75	2.16	3.59	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1351	99.32	5.75	2.16	3.59	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1352	99.37	5.76	2.16	3.59	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1353	99.45	5.76	2.17	3.60	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1354	99.56	5.77	2.17	3.60	0.50	0.219	1.68	0.130	0.78	1.10	2.000	Yes
1355	99.64	5.77	2.17	3.60	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1356	99.71	5.78	2.17	3.60	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1357	99.75	5.78	2.18	3.61	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1358	99.90	5.79	2.18	3.61	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1359	99.95	5.80	2.18	3.61	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1360	100.04	5.80	2.19	3.62	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1361	100.14	5.81	2.19	3.62	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1362	100.14	5.81	2.19	3.62	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1363	100.15	5.81	2.19	3.62	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1364	100.19	5.81	2.19	3.62	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1365	100.21	5.81	2.19	3.62	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1366	100.24	5.81	2.19	3.62	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1367	100.28	5.82	2.19	3.62	0.50	0.218	1.68	0.130	0.78	1.10	2.000	Yes
1368	100.31	5.82	2.19	3.63	0.50	0.218	1.68	0.130	0.78	1.10	2.000	No
1369	100.33	5.82	2.19	3.63	0.50	0.218	1.68	0.130	0.78	1.10	2.000	No
1370	100.38	5.82	2.20	3.63	0.50	0.218	1.68	0.130	0.78	1.10	2.000	No
1371	100.39	5.82	2.20	3.63	0.50	0.218	1.68	0.130	0.78	1.10	2.000	No
1372	100.43	5.82	2.20	3.63	0.50	0.218	1.68	0.130	0.78	1.10	2.000	No
1373	100.48	5.83	2.20	3.63	0.50	0.218	1.68	0.130	0.78	1.10	2.000	No
1374	100.53	5.83	2.20	3.63	0.50	0.218	1.68	0.130	0.78	1.10	2.000	No
1375	100.57	5.83	2.20	3.63	0.50	0.218	1.68	0.130	0.78	1.10	2.000	No
1376	100.60	5.83	2.20	3.63	0.50	0.218	1.68	0.130	0.78	1.10	2.000	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
σ_v: Total overburden pressure at test point (tsf)
u_0: Water pressure at test point (tsf)
σ_v': Effective overburden pressure based on GWT during earthquake (tsf)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.04	0.10	4.06	37.76	1.00	0.16	54.25	8.56	4.000	No	Yes	2.00
2	0.10	0.13	4.06	31.79	1.00	0.21	54.25	11.25	4.000	No	Yes	2.00
3	0.11	0.23	4.06	19.95	1.00	0.37	54.25	19.92	4.000	No	Yes	2.00
4	0.16	0.54	4.06	8.78	1.00	0.85	54.25	46.18	4.000	No	Yes	2.00
5	0.19	1.28	3.64	3.82	1.00	2.04	26.86	54.86	4.000	No	Yes	2.00
6	0.24	2.83	3.19	1.88	1.00	4.54	12.41	56.29	4.000	No	Yes	2.00
7	0.31	4.93	2.89	1.26	0.88	7.89	7.08	55.92	4.000	No	Yes	2.00
8	0.38	6.68	2.74	1.06	0.83	10.70	5.13	54.91	4.000	No	Yes	2.00
9	0.43	7.56	2.68	1.02	0.81	12.11	4.55	55.04	4.000	No	Yes	2.00
10	0.49	7.32	2.72	1.13	0.82	11.72	4.88	57.26	4.000	No	Yes	2.00
11	0.58	6.81	2.78	1.31	0.84	10.90	5.56	60.65	4.000	No	Yes	2.00
12	0.63	6.24	2.85	1.60	0.86	9.98	6.53	65.19	4.000	No	Yes	2.00
13	0.67	6.05	2.90	1.88	0.88	9.68	7.19	69.56	4.000	No	Yes	2.00
14	0.72	6.02	2.92	2.08	0.89	9.62	7.57	72.80	4.000	Yes	Yes	2.00
15	0.72	6.70	2.91	2.29	0.88	10.70	7.32	78.32	4.000	Yes	Yes	2.00
16	0.84	9.28	2.77	2.08	0.84	14.84	5.43	80.63	4.000	Yes	Yes	2.00
17	0.96	15.82	2.50	1.53	0.76	25.35	2.97	75.23	4.000	Yes	No	2.00
18	1.06	22.64	2.32	1.27	0.71	36.29	2.02	73.35	4.000	Yes	No	2.00
19	1.24	27.97	2.21	1.11	0.67	44.84	1.65	74.08	4.000	Yes	No	2.00
20	1.30	31.48	2.14	0.98	0.65	50.47	1.49	75.12	4.000	Yes	No	2.00
21	1.48	37.28	2.04	0.82	0.62	59.78	1.34	80.22	4.000	Yes	No	2.00
22	1.59	42.14	1.98	0.77	0.60	67.57	1.29	87.16	4.000	Yes	No	2.00
23	1.69	47.40	1.93	0.75	0.59	76.02	1.26	95.52	4.000	Yes	No	2.00
24	1.69	49.80	1.91	0.76	0.58	79.87	1.25	99.55	4.000	Yes	No	2.00
25	1.74	53.24	1.88	0.73	0.57	85.40	1.22	104.46	4.000	Yes	No	2.00
26	1.79	53.78	1.88	0.73	0.57	86.26	1.22	105.40	4.000	No	No	2.00
27	1.84	52.90	1.89	0.73	0.57	84.84	1.23	104.08	4.000	No	No	2.00
28	1.88	51.25	1.89	0.73	0.58	82.18	1.23	101.34	4.000	No	No	2.00
29	1.93	49.46	1.90	0.71	0.58	79.31	1.24	98.11	4.000	No	No	2.00
30	1.99	48.69	1.90	0.68	0.58	78.06	1.23	96.29	4.000	No	No	2.00
31	2.03	48.08	1.89	0.65	0.58	77.07	1.23	94.90	4.000	No	No	2.00
32	2.08	47.67	1.89	0.64	0.57	76.42	1.23	93.98	4.000	No	No	2.00
33	2.13	46.86	1.90	0.64	0.58	75.11	1.23	92.67	4.000	No	No	2.00
34	2.22	45.85	1.90	0.64	0.58	73.48	1.24	91.09	4.000	No	No	2.00
35	2.27	44.97	1.91	0.64	0.58	72.07	1.24	89.70	4.000	No	No	2.00
36	2.33	44.77	1.91	0.63	0.58	71.74	1.24	89.16	4.000	No	No	2.00
37	2.42	45.44	1.90	0.61	0.58	72.81	1.24	89.96	4.000	No	No	2.00
38	2.48	46.73	1.88	0.60	0.57	74.86	1.22	91.66	4.000	No	No	2.00
39	2.56	48.41	1.86	0.59	0.57	77.57	1.21	94.03	4.000	No	No	2.00
40	2.65	49.43	1.86	0.59	0.56	79.19	1.21	95.47	4.000	No	No	2.00
41	2.72	48.72	1.87	0.60	0.57	78.04	1.21	94.74	4.000	No	No	2.00
42	2.80	46.02	1.90	0.62	0.58	73.70	1.23	90.99	4.000	No	No	2.00
43	2.89	42.44	1.94	0.65	0.59	67.94	1.26	85.67	4.000	No	No	2.00
44	2.94	39.03	1.98	0.69	0.60	62.46	1.29	80.64	4.000	No	No	2.00
45	3.04	35.90	2.02	0.71	0.61	57.42	1.32	76.04	4.000	No	No	2.00
46	3.14	32.32	2.07	0.73	0.63	51.66	1.37	70.91	4.000	No	No	2.00
47	3.23	29.01	2.10	0.73	0.64	46.34	1.42	65.97	4.000	No	No	2.00
48	3.31	25.74	2.15	0.73	0.65	41.07	1.50	61.64	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	3.37	23.04	2.19	0.72	0.66	36.73	1.59	58.33	4.000	No	No	2.00
50	3.48	20.38	2.23	0.72	0.68	32.44	1.71	55.35	4.000	No	No	2.00
51	3.57	18.79	2.25	0.67	0.68	29.89	1.76	52.71	4.000	No	No	2.00
52	3.65	18.02	2.26	0.63	0.69	28.64	1.78	50.93	4.000	No	No	2.00
53	3.71	18.02	2.26	0.63	0.68	28.64	1.77	50.70	4.000	No	No	2.00
54	3.82	18.63	2.26	0.67	0.68	29.60	1.77	52.47	4.000	No	No	2.00
55	3.91	20.18	2.23	0.70	0.68	32.09	1.71	54.73	4.000	No	No	2.00
56	4.00	22.81	2.20	0.73	0.67	36.30	1.60	58.22	4.000	No	No	2.00
57	4.10	26.38	2.09	0.58	0.64	42.04	1.41	59.10	4.000	No	No	2.00
58	4.19	31.21	1.98	0.46	0.60	49.79	1.00	49.79	4.000	No	No	2.00
59	4.26	37.92	1.86	0.36	0.57	60.57	1.00	60.57	4.000	No	No	2.00
60	4.35	45.62	1.79	0.37	0.54	72.92	1.00	72.92	4.000	No	No	2.00
61	4.44	49.80	1.77	0.39	0.54	79.63	1.00	79.63	4.000	No	No	2.00
62	4.52	51.39	1.76	0.41	0.54	82.17	1.00	82.17	4.000	No	No	2.00
63	4.53	52.26	1.76	0.41	0.54	83.58	1.00	83.58	4.000	No	No	2.00
64	4.58	55.03	1.73	0.39	0.53	88.02	1.00	88.02	4.000	No	No	2.00
65	4.63	57.76	1.71	0.39	0.52	92.41	1.00	92.41	4.000	No	No	2.00
66	4.68	58.84	1.70	0.39	0.52	94.14	1.00	94.14	4.000	No	No	2.00
67	4.72	59.28	1.71	0.41	0.52	94.84	1.00	94.84	4.000	No	No	2.00
68	4.77	59.08	1.72	0.42	0.52	94.51	1.00	94.51	4.000	No	No	2.00
69	4.82	58.07	1.73	0.44	0.53	92.88	1.00	92.88	4.000	No	No	2.00
70	4.88	56.21	1.76	0.47	0.54	89.89	1.00	89.89	4.000	No	No	2.00
71	4.96	53.61	1.79	0.50	0.55	85.71	1.14	97.96	4.000	No	No	2.00
72	5.01	50.54	1.83	0.54	0.56	80.78	1.18	95.67	4.000	No	No	2.00
73	5.08	47.44	1.87	0.59	0.57	75.78	1.22	92.32	4.000	No	No	2.00
74	5.16	44.81	1.91	0.63	0.58	71.55	1.24	88.93	4.000	No	No	2.00
75	5.21	43.27	1.93	0.65	0.59	69.07	1.26	86.85	4.000	No	No	2.00
76	5.30	42.68	1.94	0.66	0.59	68.12	1.26	86.01	4.000	No	No	2.00
77	5.37	42.65	1.94	0.66	0.59	68.06	1.26	85.96	4.000	No	No	2.00
78	5.45	42.70	1.94	0.66	0.59	68.13	1.26	86.01	4.000	No	No	2.00
79	5.52	42.44	1.94	0.66	0.59	67.72	1.26	85.64	4.000	No	No	2.00
80	5.59	41.70	1.95	0.67	0.59	66.52	1.27	84.54	4.000	No	No	2.00
81	5.65	40.15	1.97	0.69	0.60	64.02	1.28	82.25	4.000	No	No	2.00
82	5.74	38.46	1.99	0.71	0.61	61.30	1.30	79.83	4.000	No	No	2.00
83	5.83	37.08	2.02	0.73	0.61	59.07	1.32	77.99	4.000	No	No	2.00
84	5.89	36.30	2.03	0.75	0.62	57.82	1.33	77.16	4.000	No	No	2.00
85	5.97	35.66	2.04	0.77	0.62	56.79	1.35	76.43	4.000	No	No	2.00
86	6.07	34.52	2.06	0.79	0.63	54.94	1.37	75.11	4.000	No	No	2.00
87	6.12	32.56	2.10	0.84	0.64	51.79	1.41	73.14	4.000	No	No	2.00
88	6.22	29.76	2.15	0.92	0.65	47.28	1.51	71.19	4.000	No	No	2.00
89	6.28	26.56	2.22	1.04	0.67	42.13	1.67	70.33	4.000	No	No	2.00
90	6.36	23.45	2.29	1.15	0.70	37.14	1.90	70.41	4.000	No	No	2.00
91	6.46	21.29	2.34	1.22	0.71	33.66	2.09	70.43	4.000	No	No	2.00
92	6.52	20.72	2.33	1.14	0.71	32.73	2.06	67.56	4.000	No	No	2.00
93	6.60	22.07	2.26	0.92	0.69	34.89	1.79	62.55	4.000	No	No	2.00
94	6.70	23.55	2.18	0.72	0.66	37.27	1.57	58.59	4.000	No	No	2.00
95	6.76	23.01	2.17	0.66	0.66	36.39	1.55	56.58	4.000	Yes	No	2.00
96	6.84	19.64	2.27	0.77	0.69	30.96	1.81	55.94	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	6.94	14.91	2.44	1.05	0.74	23.37	2.60	60.83	4.000	Yes	No	2.00
98	7.03	10.86	2.63	1.42	0.80	16.85	4.02	67.75	4.000	Yes	Yes	2.00
99	7.13	8.23	2.79	1.78	0.84	12.62	5.71	72.04	4.000	Yes	Yes	2.00
100	7.19	6.62	2.88	1.83	0.87	10.02	6.93	69.39	4.000	Yes	Yes	2.00
101	7.32	5.77	2.88	1.39	0.87	8.65	6.87	59.40	4.000	No	Yes	2.00
102	7.42	5.17	2.80	0.72	0.85	7.67	5.87	44.99	4.000	No	Yes	2.00
103	7.49	4.93	2.63	0.13	0.80	7.28	4.02	29.29	4.000	No	Yes	2.00
104	7.57	4.73	N/A	-0.03	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
105	7.66	4.56	N/A	-0.01	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
106	7.76	4.44	2.68	0.13	0.81	6.47	4.48	29.00	4.000	No	Yes	2.00
107	7.77	4.39	2.72	0.22	0.82	6.39	4.95	31.63	4.000	No	Yes	2.00
108	7.78	4.42	2.73	0.25	0.83	6.44	5.05	32.53	4.000	No	Yes	2.00
109	7.82	4.44	2.76	0.33	0.84	6.47	5.36	34.69	4.000	No	Yes	2.00
110	7.87	4.45	2.80	0.46	0.85	6.49	5.86	38.07	4.000	No	Yes	2.00
111	7.92	4.45	2.85	0.63	0.86	6.49	6.45	41.83	4.000	No	Yes	2.00
112	7.97	4.49	2.88	0.80	0.87	6.54	6.96	45.53	4.000	No	Yes	2.00
113	8.01	4.59	2.91	1.01	0.88	6.70	7.41	49.66	4.000	No	Yes	2.00
114	8.06	4.76	2.92	1.17	0.89	6.97	7.58	52.81	4.000	No	Yes	2.00
115	8.11	4.93	2.93	1.29	0.89	7.24	7.65	55.42	4.000	No	Yes	2.00
116	8.20	5.06	2.93	1.38	0.89	7.45	7.68	57.24	4.000	No	Yes	2.00
117	8.26	5.16	2.94	1.51	0.89	7.60	7.84	59.63	4.000	No	Yes	2.00
118	8.35	5.23	2.95	1.61	1.00	7.70	7.98	61.50	4.000	No	Yes	2.00
119	8.40	5.30	2.95	1.67	1.00	7.81	8.02	62.65	4.000	No	Yes	2.00
120	8.49	5.37	2.95	1.68	0.89	7.91	7.96	62.99	4.000	No	Yes	2.00
121	8.54	5.51	2.94	1.69	0.89	8.13	7.81	63.54	4.000	No	Yes	2.00
122	8.64	5.71	2.93	1.68	0.89	8.45	7.58	64.06	4.000	No	Yes	2.00
123	8.69	5.91	2.91	1.68	0.88	8.77	7.37	64.63	4.000	No	Yes	2.00
124	8.79	6.18	2.92	1.87	0.88	9.19	7.46	68.57	4.000	No	Yes	2.00
125	8.84	6.48	2.93	2.12	0.89	9.68	7.59	73.49	4.000	No	Yes	2.00
126	8.93	6.89	2.92	2.28	0.88	10.32	7.50	77.37	4.000	No	Yes	2.00
127	9.03	7.13	2.92	2.39	0.88	10.69	7.46	79.83	4.000	No	Yes	2.00
128	9.08	7.21	2.92	2.47	0.88	10.83	7.52	81.47	4.000	No	Yes	2.00
129	9.11	7.16	2.94	2.63	0.89	10.75	7.78	83.66	4.000	No	Yes	2.00
130	9.12	7.13	2.95	2.68	0.89	10.69	7.89	84.32	4.000	No	Yes	2.00
131	9.17	7.07	2.95	2.75	1.00	10.60	8.03	85.13	4.000	No	Yes	2.00
132	9.22	7.12	2.96	2.81	1.00	10.67	8.09	86.32	4.000	No	Yes	2.00
133	9.31	6.92	2.99	3.02	1.00	10.34	8.56	88.56	4.000	No	Yes	2.00
134	9.36	7.16	2.98	3.04	1.00	10.72	8.37	89.76	4.000	No	Yes	2.00
135	9.40	7.46	2.95	2.98	1.00	11.20	8.04	90.10	4.000	No	Yes	2.00
136	9.46	8.14	2.90	2.76	0.88	12.28	7.25	89.07	4.000	No	Yes	2.00
137	9.51	8.47	2.88	2.68	0.87	12.82	6.92	88.75	4.000	No	Yes	2.00
138	9.55	8.78	2.86	2.65	0.87	13.30	6.70	89.10	4.000	No	Yes	2.00
139	9.61	8.98	2.86	2.71	0.87	13.63	6.65	90.65	4.000	No	Yes	2.00
140	9.69	9.12	2.87	2.83	0.87	13.84	6.73	93.09	4.000	No	Yes	2.00
141	9.74	9.18	2.88	2.97	0.87	13.94	6.87	95.71	4.000	No	Yes	2.00
142	9.81	9.39	2.88	3.05	0.87	14.26	6.85	97.70	4.000	No	Yes	2.00
143	9.89	9.76	2.86	3.02	0.87	14.85	6.62	98.33	4.000	No	Yes	2.00
144	9.94	10.06	2.84	2.98	0.86	15.33	6.42	98.43	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	10.03	10.23	2.83	2.93	0.86	15.59	6.28	97.94	4.000	No	Yes	2.00
146	10.08	10.23	2.80	2.62	0.85	15.59	5.91	92.18	4.000	No	Yes	2.00
147	10.18	10.23	2.76	2.21	0.84	15.58	5.40	84.12	4.000	No	Yes	2.00
148	10.23	10.23	2.73	1.94	0.83	15.58	5.05	78.62	4.000	No	Yes	2.00
149	10.33	10.23	2.74	2.03	0.83	15.57	5.17	80.55	4.000	No	Yes	2.00
150	10.40	10.23	2.77	2.31	0.84	15.56	5.54	86.20	4.000	No	Yes	2.00
151	10.47	10.08	2.80	2.55	0.85	15.32	5.91	90.44	4.000	No	Yes	2.00
152	10.51	10.06	2.83	2.76	0.86	15.28	6.18	94.42	4.000	No	Yes	2.00
153	10.56	10.03	2.84	2.94	0.86	15.23	6.41	97.63	4.000	No	Yes	2.00
154	10.61	10.21	2.85	3.10	0.86	15.52	6.51	100.97	4.000	No	Yes	2.00
155	10.67	10.16	2.88	3.41	0.87	15.43	6.88	106.14	4.000	No	Yes	2.00
156	10.75	10.13	2.90	3.70	0.88	15.37	7.21	110.80	4.000	No	Yes	2.00
157	10.80	9.99	2.92	3.91	0.88	15.15	7.50	113.70	4.000	No	Yes	2.00
158	10.85	9.89	2.93	3.98	0.89	14.99	7.63	114.35	4.000	No	Yes	2.00
159	10.90	9.72	2.94	4.07	0.89	14.71	7.82	115.05	4.000	No	Yes	2.00
160	11.00	9.45	2.96	4.21	1.00	14.27	8.13	116.05	4.000	No	Yes	2.00
161	11.05	9.05	2.99	4.36	1.00	13.61	8.55	116.32	4.000	No	Yes	2.00
162	11.14	8.61	3.01	4.54	1.00	12.90	9.04	116.64	4.000	No	Yes	2.00
163	11.21	8.27	3.04	4.77	1.00	12.36	9.53	117.80	4.000	No	Yes	2.00
164	11.29	8.24	3.05	4.86	1.00	12.30	9.66	118.79	4.000	No	Yes	2.00
165	11.38	8.41	3.04	4.86	1.00	12.56	9.53	119.67	4.000	No	Yes	2.00
166	11.46	8.68	3.02	4.71	1.00	12.98	9.18	119.19	4.000	No	Yes	2.00
167	11.52	8.88	3.01	4.64	1.00	13.30	8.96	119.26	4.000	No	Yes	2.00
168	11.60	8.98	3.00	4.60	1.00	13.46	8.85	119.12	4.000	No	Yes	2.00
169	11.67	9.05	3.00	4.58	1.00	13.56	8.79	119.24	4.000	No	Yes	2.00
170	11.72	9.12	3.00	4.58	1.00	13.67	8.75	119.52	4.000	No	Yes	2.00
171	11.81	9.32	2.99	4.50	1.00	13.98	8.54	119.37	4.000	No	Yes	2.00
172	11.86	9.35	2.98	4.50	1.00	14.03	8.52	119.54	4.000	No	Yes	2.00
173	11.96	9.42	2.98	4.48	1.00	14.07	8.48	119.37	4.000	No	Yes	2.00
174	12.01	9.45	2.98	4.50	1.00	14.06	8.50	119.58	4.000	No	Yes	2.00
175	12.10	9.69	2.97	4.05	0.89	13.55	8.25	111.75	4.000	No	Yes	2.00
176	12.16	10.07	2.91	3.44	0.88	13.97	7.41	103.51	4.000	No	Yes	2.00
177	12.24	10.47	2.88	3.08	0.87	14.38	6.85	98.49	4.000	No	Yes	2.00
178	12.32	10.87	2.88	3.24	0.87	14.89	6.86	102.09	4.000	No	Yes	2.00
179	12.39	11.18	2.90	3.63	0.88	15.29	7.16	109.53	4.000	No	Yes	2.00
180	12.48	10.64	2.95	4.13	0.89	14.47	7.97	115.36	4.000	No	Yes	2.00
181	12.50	10.23	2.97	4.52	1.00	14.64	8.30	121.50	4.000	No	Yes	2.00
182	12.54	10.74	2.96	4.40	0.89	14.58	8.20	119.55	4.000	No	Yes	2.00
183	12.64	12.36	2.89	3.89	0.87	16.65	7.01	116.68	4.000	No	Yes	2.00
184	12.68	14.04	2.81	3.45	0.85	18.79	6.01	113.05	4.000	No	Yes	2.00
185	12.77	14.72	2.78	3.24	0.84	19.54	5.64	110.30	4.000	No	Yes	2.00
186	12.82	14.75	2.78	3.14	0.84	19.48	5.55	108.15	4.000	No	Yes	2.00
187	12.89	14.21	2.79	3.12	0.84	18.67	5.71	106.60	4.000	No	Yes	2.00
188	12.97	13.37	2.82	3.26	0.85	17.49	6.13	107.25	4.000	No	Yes	2.00
189	13.03	12.49	2.86	3.45	0.87	16.30	6.66	108.51	4.000	No	Yes	2.00
190	13.12	11.72	2.90	3.66	0.88	15.20	7.22	109.85	4.000	No	Yes	2.00
191	13.16	11.21	2.93	3.77	0.89	14.50	7.58	109.96	4.000	No	Yes	2.00
192	13.26	10.91	2.93	3.69	0.89	13.99	7.68	107.43	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	13.34	10.84	2.92	3.42	0.88	13.79	7.45	102.72	4.000	No	Yes	2.00
194	13.41	10.74	2.90	3.11	0.88	13.56	7.18	97.27	4.000	No	Yes	2.00
195	13.50	10.60	2.89	2.96	0.88	13.27	7.10	94.19	4.000	No	Yes	2.00
196	13.60	10.33	2.90	2.95	0.88	12.84	7.26	93.25	4.000	No	Yes	2.00
197	13.65	10.13	2.92	3.04	0.88	12.55	7.49	94.05	4.000	No	Yes	2.00
198	13.75	10.03	2.93	3.14	0.89	12.35	7.71	95.17	4.000	No	Yes	2.00
199	13.80	10.10	2.92	3.04	0.89	12.37	7.57	93.67	4.000	No	Yes	2.00
200	13.89	10.23	2.92	3.06	0.89	12.47	7.55	94.18	4.000	No	Yes	2.00
201	13.94	10.63	2.92	3.15	0.88	12.95	7.46	96.59	4.000	No	Yes	2.00
202	14.03	10.80	2.95	3.59	0.89	13.13	7.91	103.87	4.000	No	Yes	2.00
203	14.11	11.23	2.95	3.82	0.89	13.59	7.98	108.45	4.000	No	Yes	2.00
204	14.13	11.53	2.95	3.97	0.89	13.97	7.99	111.61	4.000	No	Yes	2.00
205	14.18	12.27	2.92	3.86	0.89	14.85	7.55	112.19	4.000	No	Yes	2.00
206	14.22	12.83	2.91	3.88	0.88	15.50	7.35	113.98	4.000	No	Yes	2.00
207	14.28	13.44	2.90	3.92	0.88	16.19	7.18	116.20	4.000	No	Yes	2.00
208	14.37	14.01	2.89	3.98	0.88	16.81	7.06	118.62	4.000	No	Yes	2.00
209	14.44	14.79	2.87	3.97	0.87	17.68	6.80	120.24	4.000	No	Yes	2.00
210	14.51	15.63	2.85	3.90	0.86	18.60	6.50	120.95	4.000	No	Yes	2.00
211	14.60	16.31	2.83	3.86	0.86	19.30	6.30	121.55	4.000	No	Yes	2.00
212	14.65	16.58	2.83	3.91	0.86	19.57	6.28	122.89	4.000	No	Yes	2.00
213	14.75	16.56	2.84	3.99	0.86	19.44	6.39	124.23	4.000	No	Yes	2.00
214	14.85	16.48	2.85	4.06	0.86	19.22	6.50	124.95	4.000	No	Yes	2.00
215	14.91	16.44	2.85	4.07	0.86	19.11	6.54	124.89	4.000	No	Yes	2.00
216	14.99	17.00	2.83	3.89	0.86	19.64	6.25	122.73	4.000	Yes	Yes	2.00
217	15.09	18.30	2.79	3.60	0.84	21.01	5.69	119.59	4.000	Yes	Yes	2.00
218	15.18	20.29	2.72	3.20	0.82	23.13	4.94	114.33	4.000	Yes	Yes	2.00
219	15.25	22.28	2.66	2.79	0.80	25.25	4.26	107.53	4.000	Yes	Yes	2.00
220	15.33	24.50	2.58	2.38	0.78	27.58	3.60	99.22	4.000	Yes	No	2.00
221	15.43	27.51	2.50	1.99	0.76	30.70	2.96	90.92	4.000	Yes	No	2.00
222	15.51	31.32	2.41	1.70	0.73	34.70	2.45	84.95	4.000	Yes	No	2.00
223	15.59	34.63	2.35	1.53	0.71	38.13	2.14	81.77	4.000	Yes	No	2.00
224	15.67	36.18	2.33	1.46	0.71	39.65	2.03	80.65	4.000	Yes	No	2.00
225	15.76	35.13	2.35	1.53	0.71	38.36	2.14	81.98	4.000	Yes	No	2.00
226	15.86	32.03	2.41	1.71	0.73	34.86	2.45	85.36	4.000	Yes	No	2.00
227	15.95	27.64	2.51	2.00	0.76	30.01	3.03	90.95	4.000	Yes	No	2.00
228	16.05	23.08	2.61	2.33	0.79	24.94	3.85	95.91	4.000	Yes	Yes	2.00
229	16.14	19.31	2.71	2.64	0.82	20.73	4.79	99.32	4.000	Yes	Yes	2.00
230	16.20	16.85	2.78	2.83	0.84	17.98	5.55	99.84	4.000	Yes	Yes	2.00
231	16.28	15.33	2.82	2.95	0.85	16.24	6.13	99.52	4.000	Yes	Yes	2.00
232	16.34	14.21	2.85	2.97	0.86	14.97	6.52	97.62	4.000	Yes	Yes	2.00
233	16.44	12.93	2.89	3.04	0.88	13.48	7.12	95.96	4.000	Yes	Yes	2.00
234	16.50	11.61	2.93	3.03	0.89	12.00	7.73	92.73	4.000	Yes	Yes	2.00
235	16.58	10.17	2.96	2.83	1.00	10.54	8.19	86.31	4.000	Yes	Yes	2.00
236	16.73	8.75	2.98	2.31	1.00	8.85	8.43	74.57	4.000	No	Yes	2.00
237	16.82	7.60	2.96	1.61	1.00	7.51	8.14	61.14	4.000	No	Yes	2.00
238	16.92	7.06	2.97	1.45	1.00	6.86	8.35	57.29	4.000	No	Yes	2.00
239	17.01	6.56	3.09	2.09	1.00	6.26	10.33	64.67	4.000	No	Yes	2.00
240	17.11	6.20	3.19	2.99	1.00	5.84	12.54	73.17	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	17.12	5.73	3.28	3.81	1.00	5.31	14.74	78.30	4.000	No	Yes	2.00
242	17.14	6.34	3.23	3.66	1.00	5.97	13.44	80.31	4.000	No	Yes	2.00
243	17.19	7.13	3.17	3.53	1.00	6.82	12.15	82.92	4.000	No	Yes	2.00
244	17.28	7.94	3.13	3.46	1.00	7.67	11.16	85.58	4.000	No	Yes	2.00
245	17.33	8.01	3.14	3.72	1.00	7.71	11.48	88.52	4.000	No	Yes	2.00
246	17.43	7.87	3.16	3.90	1.00	7.52	11.93	89.67	4.000	No	Yes	2.00
247	17.47	7.74	3.17	3.85	1.00	7.35	12.03	88.37	4.000	No	Yes	2.00
248	17.57	7.57	3.16	3.62	1.00	7.12	11.95	85.14	4.000	No	Yes	2.00
249	17.65	7.47	3.15	3.35	1.00	6.98	11.70	81.63	4.000	No	Yes	2.00
250	17.72	7.40	3.16	3.37	1.00	6.88	11.84	81.46	4.000	No	Yes	2.00
251	17.81	7.57	3.16	3.48	1.00	7.02	11.86	83.22	4.000	No	Yes	2.00
252	17.86	7.87	3.17	3.79	1.00	7.32	11.98	87.65	4.000	No	Yes	2.00
253	17.95	8.31	3.16	4.07	1.00	7.73	11.95	92.32	4.000	No	Yes	2.00
254	18.05	8.78	3.16	4.29	1.00	8.18	11.81	96.52	4.000	No	Yes	2.00
255	18.10	9.22	3.15	4.49	1.00	8.61	11.67	100.43	4.000	No	Yes	2.00
256	18.20	9.66	3.14	4.65	1.00	9.01	11.52	103.80	4.000	No	Yes	2.00
257	18.30	9.90	3.15	4.85	1.00	9.20	11.60	106.76	4.000	No	Yes	2.00
258	18.39	10.13	3.14	4.89	1.00	9.38	11.50	107.91	4.000	No	Yes	2.00
259	18.48	10.27	3.14	4.83	1.00	9.47	11.38	107.71	4.000	No	Yes	2.00
260	18.58	10.30	3.14	4.82	1.00	9.44	11.38	107.46	4.000	No	Yes	2.00
261	18.66	10.20	3.14	4.82	1.00	9.30	11.49	106.87	4.000	No	Yes	2.00
262	18.74	10.07	3.14	4.69	1.00	9.12	11.49	104.74	4.000	No	Yes	2.00
263	18.87	9.90	3.11	3.92	1.00	8.88	10.73	95.26	4.000	No	Yes	2.00
264	18.97	9.66	3.07	3.27	1.00	8.59	10.09	86.69	4.000	No	Yes	2.00
265	19.06	9.56	3.05	2.85	1.00	8.45	9.58	80.90	4.000	No	Yes	2.00
266	19.16	9.83	3.06	3.14	1.00	8.66	9.84	85.25	4.000	No	Yes	2.00
267	19.25	10.13	3.06	3.34	1.00	8.91	9.93	88.50	4.000	No	Yes	2.00
268	19.27	10.23	3.08	3.58	1.00	9.00	10.18	91.69	4.000	No	Yes	2.00
269	19.30	10.37	3.09	3.79	1.00	9.12	10.39	94.70	4.000	No	Yes	2.00
270	19.34	10.57	3.10	4.04	1.00	9.29	10.57	98.19	4.000	No	Yes	2.00
271	19.39	10.84	3.09	4.12	1.00	9.53	10.50	100.00	4.000	No	Yes	2.00
272	19.49	10.78	3.10	4.12	1.00	9.41	10.57	99.51	4.000	No	Yes	2.00
273	19.55	10.51	3.10	4.04	1.00	9.12	10.70	97.54	4.000	No	Yes	2.00
274	19.63	10.17	3.11	3.94	1.00	8.75	10.86	95.04	4.000	No	Yes	2.00
275	19.68	9.87	3.11	3.78	1.00	8.43	10.91	92.04	4.000	No	Yes	2.00
276	19.74	9.77	3.10	3.54	1.00	8.31	10.69	88.83	4.000	No	Yes	2.00
277	19.83	9.73	3.10	3.44	1.00	8.24	10.61	87.40	4.000	No	Yes	2.00
278	19.87	9.73	3.10	3.38	1.00	8.22	10.55	86.67	4.000	No	Yes	2.00
279	19.94	9.73	3.11	3.54	1.00	8.19	10.80	88.39	4.000	No	Yes	2.00
280	20.02	9.80	3.12	3.73	1.00	8.21	11.04	90.64	4.000	No	Yes	2.00
281	20.07	10.17	3.13	4.13	1.00	8.54	11.28	96.33	4.000	No	Yes	2.00
282	20.17	11.42	3.09	4.10	1.00	9.65	10.38	100.21	4.000	No	Yes	2.00
283	20.21	14.18	2.97	3.57	1.00	12.20	8.30	101.25	4.000	Yes	Yes	2.00
284	20.28	18.74	2.80	2.81	0.85	16.43	5.92	97.16	4.000	Yes	Yes	2.00
285	20.36	24.88	2.64	2.22	0.80	22.08	4.11	90.84	4.000	Yes	Yes	2.00
286	20.41	31.73	2.51	1.86	0.76	28.40	3.02	85.89	4.000	Yes	No	2.00
287	20.48	38.64	2.40	1.64	0.73	34.74	2.39	83.15	4.000	Yes	No	2.00
288	20.55	44.99	2.33	1.49	0.71	40.52	2.02	82.00	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	20.60	49.88	2.27	1.39	0.69	44.99	1.82	81.90	4.000	Yes	No	2.00
290	20.70	52.55	2.25	1.34	0.68	47.28	1.74	82.23	4.000	No	No	2.00
291	20.74	52.68	2.25	1.37	0.68	47.32	1.75	82.97	4.000	No	No	2.00
292	20.79	51.17	2.28	1.45	0.69	45.83	1.84	84.31	4.000	No	No	2.00
293	20.89	48.70	2.33	1.63	0.71	43.39	2.03	87.95	4.000	No	No	2.00
294	20.96	46.86	2.33	1.59	0.71	41.58	2.06	85.66	4.000	No	No	2.00
295	21.04	45.83	2.34	1.58	0.71	40.52	2.09	84.84	4.000	No	No	2.00
296	21.13	45.80	2.33	1.51	0.71	40.36	2.05	82.71	4.000	No	No	2.00
297	21.22	49.22	2.31	1.55	0.70	43.31	1.97	85.52	4.000	No	No	2.00
298	21.29	52.71	2.28	1.51	0.69	46.38	1.86	86.23	4.000	No	No	2.00
299	21.35	62.13	2.19	1.30	0.66	54.84	1.58	86.56	4.000	No	No	2.00
300	21.37	71.37	2.10	1.15	0.64	63.21	1.42	89.97	4.000	No	No	2.00
301	21.42	83.72	2.01	0.98	0.61	74.37	1.31	97.64	4.000	No	No	2.00
302	21.47	92.73	1.95	0.89	0.59	82.47	1.27	104.48	4.000	No	No	2.00
303	21.48	100.66	1.90	0.82	0.58	89.69	1.23	110.65	4.000	No	No	2.00
304	21.52	107.37	1.85	0.77	0.56	95.73	1.20	115.32	4.000	No	No	2.00
305	21.57	113.24	1.82	0.73	0.55	100.98	1.17	118.63	4.000	No	No	2.00
306	21.62	118.81	1.79	0.69	0.54	105.91	1.14	120.85	4.000	No	No	2.00
307	21.66	124.00	1.76	0.65	0.54	110.52	1.10	122.11	4.000	No	No	2.00
308	21.71	128.79	1.74	0.63	0.53	114.75	1.07	122.79	4.000	No	No	2.00
309	21.76	132.64	1.73	0.62	0.53	118.10	1.04	123.42	4.000	No	No	2.00
310	21.81	135.34	1.72	0.63	0.52	120.38	1.03	124.51	4.000	No	No	2.00
311	21.85	136.99	1.72	0.64	0.53	121.70	1.04	126.15	4.000	No	No	2.00
312	21.91	137.80	1.73	0.66	0.53	122.24	1.05	127.87	4.000	No	No	2.00
313	21.95	138.11	1.73	0.67	0.53	122.32	1.06	129.40	4.000	No	No	2.00
314	22.00	138.24	1.74	0.69	0.53	122.26	1.07	130.49	4.000	No	No	2.00
315	22.05	138.18	1.75	0.70	0.53	122.02	1.08	131.33	4.000	No	No	2.00
316	22.10	138.24	1.75	0.71	0.53	121.90	1.08	132.00	4.000	No	No	2.00
317	22.15	138.31	1.75	0.72	0.53	121.77	1.09	132.56	4.000	No	No	2.00
318	22.19	138.68	1.75	0.72	0.53	121.94	1.09	133.12	4.000	No	No	2.00
319	22.24	139.25	1.76	0.75	0.54	122.24	1.11	135.35	4.000	No	No	2.00
320	22.29	139.86	1.77	0.77	0.54	122.58	1.11	136.60	4.000	No	No	2.00
321	22.34	140.20	1.77	0.78	0.54	122.70	1.12	137.16	4.000	No	No	2.00
322	22.39	140.06	1.77	0.76	0.54	122.45	1.11	135.89	4.000	No	No	2.00
323	22.43	139.42	1.77	0.76	0.54	121.72	1.11	135.26	4.000	No	No	2.00
324	22.48	138.34	1.77	0.76	0.54	120.56	1.12	135.08	4.000	No	No	2.00
325	22.55	136.79	1.78	0.78	0.54	118.95	1.13	134.76	4.000	No	No	2.00
326	22.62	130.08	1.82	0.82	0.55	112.68	1.17	131.90	4.000	No	No	2.00
327	22.63	127.95	1.83	0.83	0.56	110.75	1.18	130.57	4.000	No	No	2.00
328	22.72	125.56	1.83	0.84	0.56	108.31	1.19	128.61	4.000	No	No	2.00
329	22.77	128.09	1.82	0.81	0.55	110.46	1.17	129.57	4.000	No	No	2.00
330	22.83	126.13	1.83	0.83	0.56	108.51	1.19	128.59	4.000	No	No	2.00
331	22.91	124.21	1.85	0.86	0.56	106.52	1.20	127.55	4.000	No	No	2.00
332	22.96	121.74	1.86	0.88	0.57	104.15	1.21	126.09	4.000	No	No	2.00
333	23.02	118.20	1.88	0.91	0.57	100.84	1.22	123.45	4.000	No	No	2.00
334	23.10	113.85	1.90	0.94	0.58	96.74	1.24	119.96	4.000	No	No	2.00
335	23.16	108.42	1.93	0.98	0.59	91.79	1.26	115.60	4.000	No	No	2.00
336	23.20	102.21	1.97	1.03	0.60	86.20	1.28	110.62	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	23.26	95.46	2.01	1.08	0.61	80.15	1.31	105.23	4.000	No	No	2.00
338	23.35	88.68	2.05	1.15	0.62	74.00	1.36	100.36	4.000	No	No	2.00
339	23.39	81.66	2.10	1.23	0.64	67.80	1.42	95.97	4.000	No	No	2.00
340	23.48	74.68	2.15	1.34	0.65	61.55	1.51	93.11	4.000	No	No	2.00
341	23.54	68.33	2.20	1.41	0.67	55.99	1.61	90.41	4.000	No	No	2.00
342	23.63	63.44	2.23	1.41	0.68	51.67	1.69	87.24	4.000	No	No	2.00
343	23.69	60.07	2.21	1.21	0.67	48.84	1.63	79.68	4.000	No	No	2.00
344	23.78	58.37	2.19	1.08	0.66	47.34	1.59	75.09	4.000	No	No	2.00
345	23.87	57.71	2.18	1.00	0.66	46.70	1.56	72.76	4.000	No	No	2.00
346	23.88	57.81	2.20	1.11	0.67	46.69	1.62	75.51	4.000	No	No	2.00
347	23.93	57.42	2.23	1.22	0.68	46.23	1.69	78.05	4.000	No	No	2.00
348	24.02	57.22	2.25	1.33	0.68	45.85	1.76	80.73	4.000	No	No	2.00
349	24.04	56.97	2.27	1.41	0.69	45.57	1.82	82.98	4.000	No	No	2.00
350	24.05	57.34	2.28	1.47	0.69	45.82	1.85	84.83	4.000	No	No	2.00
351	24.15	58.27	2.28	1.52	0.69	46.42	1.87	86.71	4.000	No	No	2.00
352	24.20	60.11	2.28	1.55	0.69	47.86	1.85	88.32	4.000	No	No	2.00
353	24.30	62.64	2.25	1.45	0.68	49.86	1.75	87.06	4.000	No	No	2.00
354	24.40	65.07	2.21	1.31	0.67	51.83	1.63	84.41	4.000	No	No	2.00
355	24.46	66.59	2.16	1.15	0.66	53.10	1.53	81.44	4.000	No	No	2.00
356	24.54	66.42	2.15	1.08	0.65	52.90	1.50	79.49	4.000	No	No	2.00
357	24.64	64.09	2.17	1.11	0.66	50.78	1.55	78.59	4.000	Yes	No	2.00
358	24.73	59.94	2.22	1.24	0.68	47.12	1.68	79.13	4.000	Yes	No	2.00
359	24.78	54.64	2.30	1.43	0.70	42.55	1.92	81.62	4.000	Yes	No	2.00
360	24.88	48.57	2.38	1.66	0.72	37.36	2.28	85.25	4.000	Yes	No	2.00
361	24.94	41.92	2.47	1.90	0.75	31.81	2.80	89.16	4.000	Yes	No	2.00
362	25.02	35.00	2.57	2.14	0.78	26.12	3.52	92.04	4.000	Yes	No	2.00
363	25.12	28.43	2.69	2.46	0.81	20.76	4.59	95.35	4.000	Yes	Yes	2.00
364	25.17	22.86	2.81	2.88	0.85	16.30	6.02	98.17	4.000	Yes	Yes	2.00
365	25.27	18.41	2.93	3.27	0.89	12.75	7.69	98.13	4.000	Yes	Yes	2.00
366	25.36	15.13	3.04	3.56	1.00	9.96	9.50	94.69	4.000	No	Yes	2.00
367	25.43	12.60	3.13	3.75	1.00	8.11	11.16	90.44	4.000	No	Yes	2.00
368	25.50	10.88	3.20	3.97	1.00	6.84	12.76	87.31	4.000	No	Yes	2.00
369	25.60	9.77	3.25	4.08	1.00	6.01	14.03	84.31	4.000	No	Yes	2.00
370	25.64	9.26	3.27	4.02	1.00	5.64	14.52	81.86	4.000	No	Yes	2.00
371	25.67	9.06	3.28	3.90	1.00	5.48	14.58	79.98	4.000	No	Yes	2.00
372	25.71	8.86	3.27	3.61	1.00	5.33	14.38	76.65	4.000	No	Yes	2.00
373	25.79	8.52	3.26	3.26	1.00	5.07	14.25	72.22	4.000	No	Yes	2.00
374	25.93	8.18	3.26	2.95	1.00	4.80	14.17	68.01	4.000	No	Yes	2.00
375	26.03	8.02	3.25	2.70	1.00	4.66	13.97	65.11	4.000	No	Yes	2.00
376	26.13	8.02	3.24	2.57	1.00	4.64	13.74	63.74	4.000	No	Yes	2.00
377	26.24	8.08	3.23	2.50	1.00	4.67	13.54	63.18	4.000	No	Yes	2.00
378	26.37	8.18	3.23	2.51	1.00	4.71	13.48	63.49	4.000	No	Yes	2.00
379	26.47	8.25	3.23	2.56	1.00	4.73	13.53	64.09	4.000	No	Yes	2.00
380	26.60	8.25	3.22	2.39	1.00	4.71	13.24	62.33	4.000	No	Yes	2.00
381	26.71	8.38	3.19	2.15	1.00	4.78	12.59	60.15	4.000	No	Yes	2.00
382	26.85	8.75	3.16	1.96	1.00	5.00	11.78	58.94	4.000	No	Yes	2.00
383	26.95	8.96	3.18	2.26	1.00	5.12	12.24	62.69	4.000	No	Yes	2.00
384	27.04	9.60	3.18	2.57	1.00	5.54	12.21	67.66	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	27.09	10.14	3.18	2.92	1.00	5.90	12.33	72.68	4.000	No	Yes	2.00
386	27.19	10.95	3.16	2.98	1.00	6.42	11.76	75.49	4.000	No	Yes	2.00
387	27.23	11.18	3.16	3.16	1.00	6.56	11.88	78.01	4.000	No	Yes	2.00
388	27.33	11.42	3.17	3.32	1.00	6.70	11.98	80.22	4.000	No	Yes	2.00
389	27.40	11.76	3.16	3.46	1.00	6.91	11.94	82.48	4.000	No	Yes	2.00
390	27.47	12.30	3.15	3.56	1.00	7.25	11.72	84.94	4.000	No	Yes	2.00
391	27.57	12.97	3.14	3.59	1.00	7.66	11.34	86.93	4.000	No	Yes	2.00
392	27.66	13.85	3.12	3.70	1.00	8.22	10.99	90.36	4.000	No	Yes	2.00
393	27.77	14.96	3.10	3.87	1.00	8.93	10.64	94.93	4.000	No	Yes	2.00
394	27.86	16.28	3.08	4.09	1.00	9.76	10.29	100.42	4.000	No	Yes	2.00
395	27.96	17.39	3.07	4.27	1.00	10.45	10.06	105.14	4.000	No	Yes	2.00
396	28.06	17.73	3.08	4.52	1.00	10.63	10.22	108.70	4.000	No	Yes	2.00
397	28.15	17.29	3.10	4.70	1.00	10.31	10.64	109.63	4.000	No	Yes	2.00
398	28.25	17.04	3.08	4.30	1.00	10.10	10.32	104.18	4.000	No	Yes	2.00
399	28.34	16.50	3.07	3.92	1.00	9.71	10.12	98.29	4.000	No	Yes	2.00
400	28.44	16.94	3.04	3.53	1.00	9.96	9.46	94.21	4.000	No	Yes	2.00
401	28.54	16.11	3.09	4.00	1.00	9.38	10.45	98.03	4.000	No	Yes	2.00
402	28.62	17.46	3.06	4.02	1.00	10.22	9.90	101.19	4.000	No	Yes	2.00
403	28.71	18.34	3.05	4.14	1.00	10.74	9.72	104.45	4.000	No	Yes	2.00
404	28.77	20.26	3.01	4.01	1.00	11.95	8.92	106.63	4.000	No	Yes	2.00
405	28.86	20.73	3.01	4.13	1.00	12.21	8.93	109.00	4.000	No	Yes	2.00
406	28.91	21.34	3.00	4.15	1.00	12.56	8.78	110.37	4.000	No	Yes	2.00
407	28.97	22.04	2.99	4.19	1.00	12.99	8.63	112.06	4.000	No	Yes	2.00
408	29.04	22.92	2.98	4.23	1.00	13.50	8.45	114.13	4.000	No	Yes	2.00
409	29.10	23.97	2.97	4.28	1.00	14.13	8.26	116.69	4.000	No	Yes	2.00
410	29.15	25.15	2.96	4.38	1.00	14.85	8.08	120.01	4.000	No	Yes	2.00
411	29.25	26.40	2.93	4.48	0.89	16.30	7.69	125.36	4.000	No	Yes	2.00
412	29.34	27.38	2.93	4.58	0.89	16.91	7.60	128.48	4.000	No	Yes	2.00
413	29.38	27.75	2.93	4.68	0.89	17.12	7.63	130.55	4.000	No	Yes	2.00
414	29.48	27.72	2.95	4.76	1.00	16.25	7.97	129.55	4.000	No	Yes	2.00
415	29.55	27.48	2.96	4.80	1.00	16.06	8.07	129.61	4.000	Yes	Yes	2.00
416	29.63	27.41	2.93	4.54	0.89	16.75	7.61	127.50	4.000	Yes	Yes	2.00
417	29.72	28.43	2.81	3.17	0.85	17.61	6.01	105.80	4.000	Yes	Yes	2.00
418	29.82	31.56	2.63	1.83	0.80	20.09	3.98	79.94	4.000	Yes	Yes	2.00
419	29.88	36.83	2.39	0.90	0.73	24.31	2.33	56.65	4.000	Yes	No	2.00
420	29.96	45.23	2.29	0.81	0.69	30.47	1.87	56.98	4.000	Yes	No	2.00
421	30.06	49.92	2.25	0.82	0.68	33.83	1.75	59.16	4.000	Yes	No	2.00
422	30.13	54.67	2.21	0.81	0.67	37.29	1.64	60.99	4.000	Yes	No	2.00
423	30.18	56.02	2.21	0.84	0.67	38.21	1.63	62.30	0.102	No	No	0.57
424	30.28	58.72	2.20	0.87	0.67	40.06	1.61	64.44	0.105	No	No	0.58
425	30.37	59.53	2.22	0.98	0.67	40.40	1.67	67.53	0.109	No	No	0.60
426	30.47	60.51	2.25	1.10	0.68	40.85	1.74	71.05	0.113	No	No	0.63
427	30.57	63.28	2.24	1.15	0.68	42.69	1.73	73.87	0.117	No	No	0.65
428	30.66	67.26	2.22	1.17	0.67	45.46	1.67	76.12	0.121	No	No	0.67
429	30.74	71.34	2.20	1.17	0.67	48.33	1.62	78.31	0.125	No	No	0.69
430	30.82	74.51	2.19	1.19	0.67	50.51	1.59	80.52	0.129	No	No	0.71
431	30.90	76.30	2.20	1.26	0.67	51.60	1.61	82.93	0.133	No	No	0.73
432	31.01	76.90	2.22	1.35	0.67	51.74	1.66	85.67	0.138	No	No	0.76

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	31.10	77.02	2.24	1.50	0.68	51.51	1.74	89.47	0.147	No	No	0.80
434	31.19	77.06	2.28	1.66	0.69	51.19	1.84	93.96	0.157	No	No	0.86
435	31.28	77.57	2.30	1.81	0.70	51.24	1.92	98.21	0.168	No	No	0.92
436	31.35	78.53	2.31	1.92	0.70	51.70	1.97	101.82	0.178	No	No	0.97
437	31.43	80.52	2.31	1.98	0.70	52.90	1.98	104.59	0.186	No	No	1.02
438	31.53	83.11	2.31	2.04	0.70	54.53	1.97	107.28	0.195	No	No	1.06
439	31.60	85.91	2.26	1.77	0.69	56.74	1.78	101.10	0.176	No	No	0.96
440	31.67	88.07	2.21	1.54	0.67	58.52	1.64	95.74	0.162	No	No	0.88
441	31.77	89.46	2.16	1.33	0.66	59.74	1.53	91.18	0.150	No	No	0.82
442	31.84	89.86	2.18	1.41	0.66	59.77	1.56	93.40	0.156	No	No	0.84
443	31.91	86.18	2.22	1.57	0.68	56.78	1.68	95.19	0.160	No	No	0.87
444	31.98	79.10	2.29	1.77	0.70	51.41	1.89	97.23	0.165	No	No	0.89
445	31.98	77.21	2.32	1.87	0.70	49.95	1.99	99.23	0.171	No	No	0.92
446	32.04	78.73	2.31	1.90	0.70	50.91	1.98	100.65	0.175	No	No	0.94
447	32.12	82.68	2.30	1.89	0.70	53.56	1.91	102.19	4.000	Yes	No	2.00
448	32.16	80.04	2.33	2.05	0.71	51.46	2.05	105.63	4.000	Yes	No	2.00
449	32.27	75.66	2.38	2.23	0.72	48.11	2.26	108.77	4.000	Yes	No	2.00
450	32.33	70.76	2.42	2.40	0.74	44.53	2.50	111.51	4.000	Yes	No	2.00
451	32.41	66.31	2.46	2.50	0.75	41.33	2.72	112.40	4.000	Yes	No	2.00
452	32.50	61.79	2.49	2.55	0.76	38.14	2.93	111.66	4.000	Yes	No	2.00
453	32.58	56.66	2.53	2.59	0.77	34.61	3.18	110.12	4.000	Yes	No	2.00
454	32.66	50.22	2.58	2.66	0.78	30.23	3.59	108.68	4.000	Yes	No	2.00
455	32.74	43.30	2.65	2.79	0.80	25.56	4.22	107.79	4.000	Yes	Yes	2.00
456	32.84	36.12	2.75	3.04	0.83	20.76	5.20	107.96	4.000	Yes	Yes	2.00
457	32.90	29.88	2.85	3.36	0.86	16.68	6.45	107.62	4.000	Yes	Yes	2.00
458	32.98	24.92	2.96	3.68	1.00	12.71	8.19	104.08	4.000	Yes	Yes	2.00
459	33.08	20.77	3.06	4.02	1.00	10.40	9.80	101.84	3.600	No	Yes	2.00
460	33.14	17.05	3.16	4.51	1.00	8.34	11.93	99.50	3.600	No	Yes	2.00
461	33.22	14.12	3.27	5.00	1.00	6.71	14.31	96.06	3.600	No	Yes	2.00
462	33.32	12.19	3.34	5.20	1.00	5.64	16.21	91.43	3.600	No	Yes	2.00
463	33.37	11.28	3.35	4.81	1.00	5.14	16.60	85.28	3.600	No	Yes	2.00
464	33.47	11.05	3.34	4.46	1.00	4.99	16.37	81.70	3.600	No	Yes	2.00
465	33.56	11.66	3.30	4.00	1.00	5.30	15.06	79.85	3.600	No	Yes	2.00
466	33.63	12.43	3.26	3.78	1.00	5.71	14.04	80.15	3.600	No	Yes	2.00
467	33.71	12.67	3.23	3.53	1.00	5.82	13.47	78.37	3.600	No	Yes	2.00
468	33.81	11.99	3.22	3.07	1.00	5.44	13.27	72.19	3.600	No	Yes	2.00
469	33.90	11.05	3.23	2.64	1.00	4.92	13.35	65.65	3.600	No	Yes	2.00
470	33.95	10.31	3.23	2.27	1.00	4.51	13.36	60.28	3.600	No	Yes	2.00
471	34.04	10.07	3.24	2.29	1.00	4.37	13.69	59.84	3.600	No	Yes	2.00
472	34.14	9.87	3.25	2.32	1.00	4.25	14.01	59.54	3.600	No	Yes	2.00
473	34.17	9.81	3.26	2.35	1.00	4.21	14.16	59.63	3.600	No	Yes	2.00
474	34.20	10.07	3.24	2.31	1.00	4.35	13.78	59.92	3.600	No	Yes	2.00
475	34.26	10.38	3.23	2.26	1.00	4.50	13.36	60.14	3.600	No	Yes	2.00
476	34.35	10.61	3.21	2.19	1.00	4.61	12.99	59.91	3.600	No	Yes	2.00
477	34.43	10.41	3.22	2.20	1.00	4.49	13.24	59.45	3.600	No	Yes	2.00
478	34.49	10.27	3.22	2.15	1.00	4.41	13.28	58.59	3.600	No	Yes	2.00
479	34.59	10.17	3.22	2.05	1.00	4.34	13.18	57.25	3.600	No	Yes	2.00
480	34.69	10.07	3.21	1.94	1.00	4.28	13.07	55.91	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	34.73	9.90	3.22	1.88	1.00	4.18	13.12	54.88	3.600	No	Yes	2.00
482	34.83	9.80	3.22	1.86	1.00	4.12	13.19	54.34	3.600	No	Yes	2.00
483	34.90	9.74	3.23	1.89	1.00	4.07	13.37	54.48	3.600	No	Yes	2.00
484	34.98	9.84	3.23	1.97	1.00	4.12	13.48	55.47	3.600	No	Yes	2.00
485	35.07	10.14	3.24	2.18	1.00	4.26	13.68	58.28	3.600	No	Yes	2.00
486	35.16	10.58	3.27	2.77	1.00	4.47	14.49	64.79	3.600	No	Yes	2.00
487	35.26	11.29	3.32	3.92	1.00	4.82	15.85	76.48	3.600	No	Yes	2.00
488	35.33	13.25	3.31	4.84	1.00	5.82	15.42	89.71	3.600	No	Yes	2.00
489	35.40	16.76	3.22	5.02	1.00	7.61	13.28	101.03	3.600	No	Yes	2.00
490	35.50	20.84	3.12	4.66	1.00	9.67	11.03	106.70	3.600	No	Yes	2.00
491	35.57	23.37	3.07	4.51	1.00	10.95	10.02	109.72	3.600	No	Yes	2.00
492	35.65	23.77	3.07	4.67	1.00	11.12	10.10	112.36	3.600	No	Yes	2.00
493	35.71	22.86	3.11	5.08	1.00	10.64	10.83	115.22	3.600	No	Yes	2.00
494	35.79	21.65	3.15	5.43	1.00	9.99	11.64	116.27	3.600	No	Yes	2.00
495	35.85	20.37	3.18	5.49	1.00	9.32	12.22	113.90	3.600	No	Yes	2.00
496	35.94	19.29	3.19	5.34	1.00	8.75	12.53	109.71	3.600	No	Yes	2.00
497	35.99	18.31	3.19	4.97	1.00	8.24	12.58	103.66	3.600	No	Yes	2.00
498	36.08	17.16	3.19	4.47	1.00	7.64	12.55	95.94	3.600	No	Yes	2.00
499	36.17	15.54	3.21	4.09	1.00	6.80	12.98	88.35	3.600	No	Yes	2.00
500	36.24	14.22	3.23	3.84	1.00	6.13	13.50	82.76	3.600	No	Yes	2.00
501	36.33	13.58	3.25	3.84	1.00	5.79	14.00	81.11	3.600	No	Yes	2.00
502	36.42	13.58	3.26	3.97	1.00	5.77	14.22	82.08	3.600	No	Yes	2.00
503	36.52	14.05	3.21	3.32	1.00	5.99	12.88	77.16	3.600	No	Yes	2.00
504	36.61	15.40	3.13	2.85	1.00	6.64	11.27	74.88	3.600	No	Yes	2.00
505	36.70	17.73	3.06	2.69	1.00	7.78	9.87	76.79	3.600	No	Yes	2.00
506	36.78	20.23	3.06	3.31	1.00	8.99	9.83	88.43	3.600	No	Yes	2.00
507	36.85	18.24	3.19	4.64	1.00	7.99	12.41	99.18	3.600	No	Yes	2.00
508	36.87	20.20	3.15	4.68	1.00	8.95	11.61	103.88	3.600	No	Yes	2.00
509	36.91	23.23	3.07	4.28	1.00	10.43	10.08	105.17	3.600	No	Yes	2.00
510	36.97	31.40	2.86	3.30	0.87	15.73	6.66	104.77	4.000	Yes	Yes	2.00
511	37.06	35.24	2.80	3.11	0.85	17.97	5.86	105.20	4.000	Yes	Yes	2.00
512	37.12	38.62	2.76	3.10	0.84	19.91	5.42	107.91	4.000	Yes	Yes	2.00
513	37.20	42.40	2.74	3.17	0.83	22.04	5.10	112.33	4.000	Yes	Yes	2.00
514	37.27	47.56	2.69	3.09	0.81	25.06	4.56	114.30	4.000	Yes	Yes	2.00
515	37.35	52.21	2.63	2.89	0.80	27.88	4.03	112.42	4.000	Yes	Yes	2.00
516	37.44	55.22	2.59	2.66	0.78	29.75	3.64	108.21	4.000	Yes	No	2.00
517	37.49	58.42	2.53	2.39	0.77	31.83	3.23	102.76	4.000	Yes	No	2.00
518	37.59	67.19	2.43	2.02	0.74	37.46	2.56	95.81	4.000	Yes	No	2.00
519	37.64	85.65	2.27	1.57	0.69	49.64	1.82	90.11	4.000	Yes	No	2.00
520	37.70	111.29	2.10	1.20	0.64	67.10	1.41	94.79	4.000	Yes	No	2.00
521	37.78	136.59	1.96	0.98	0.60	84.81	1.28	108.37	4.000	Yes	No	2.00
522	37.83	155.69	1.88	0.87	0.57	98.45	1.22	120.19	4.000	Yes	No	2.00
523	37.92	167.53	1.83	0.82	0.56	106.83	1.19	126.68	4.000	Yes	No	2.00
524	37.97	174.58	1.81	0.81	0.55	111.69	1.17	130.53	4.000	Yes	No	2.00
525	38.07	178.80	1.81	0.82	0.55	114.34	1.16	133.13	0.299	No	No	1.52
526	38.14	181.84	1.81	0.85	0.55	116.07	1.17	135.64	0.312	No	No	1.59
527	38.22	185.72	1.82	0.88	0.55	118.33	1.17	138.68	0.328	No	No	1.67
528	38.31	191.72	1.82	0.92	0.55	121.94	1.17	143.23	0.353	No	No	1.79

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	38.41	201.37	1.80	0.92	0.55	128.37	1.16	148.66	0.386	No	No	1.96
530	38.52	212.64	1.79	0.92	0.54	135.94	1.14	154.32	0.422	No	No	2.00
531	38.64	221.04	1.77	0.91	0.54	141.59	1.11	157.41	0.443	No	No	2.00
532	38.74	217.87	1.79	0.95	0.54	138.67	1.14	158.10	0.448	No	No	2.00
533	38.80	214.19	1.81	0.99	0.55	135.62	1.16	157.57	0.444	No	No	2.00
534	38.89	210.42	1.83	1.04	0.56	132.43	1.18	156.57	0.437	No	No	2.00
535	38.94	213.65	1.83	1.05	0.56	134.37	1.18	158.84	0.453	No	No	2.00
536	39.03	213.59	1.84	1.10	0.56	133.74	1.19	159.69	0.459	No	No	2.00
537	39.13	213.25	1.86	1.15	0.57	132.81	1.21	160.46	0.464	No	No	2.00
538	39.23	211.36	1.88	1.22	0.57	130.76	1.22	160.12	0.462	No	No	2.00
539	39.35	207.85	1.90	1.28	0.58	127.69	1.24	158.27	0.449	No	No	2.00
540	39.42	201.04	1.93	1.34	0.59	122.59	1.26	154.08	0.420	No	No	2.00
541	39.51	192.09	1.96	1.40	0.60	116.15	1.28	148.22	0.383	No	No	1.93
542	39.60	181.50	1.99	1.45	0.61	108.71	1.30	141.37	0.343	No	No	1.73
543	39.70	172.83	2.02	1.50	0.61	102.65	1.32	135.85	0.313	No	No	1.58
544	39.78	164.63	2.04	1.53	0.62	97.07	1.35	130.75	0.288	No	No	1.45
545	39.90	157.35	2.06	1.56	0.63	92.05	1.37	126.28	0.267	No	No	1.34
546	39.99	149.05	2.09	1.60	0.64	86.44	1.41	121.65	0.247	No	No	1.24
547	40.09	141.42	2.12	1.64	0.64	81.31	1.45	117.75	4.000	Yes	No	2.00
548	40.18	133.79	2.15	1.68	0.65	76.23	1.50	114.33	4.000	Yes	No	2.00
549	40.23	126.04	2.18	1.74	0.66	71.16	1.56	111.30	4.000	Yes	No	2.00
550	40.33	118.01	2.22	1.81	0.67	65.88	1.65	108.90	4.000	Yes	No	2.00
551	40.43	110.12	2.25	1.88	0.68	60.74	1.76	107.17	4.000	Yes	No	2.00
552	40.52	101.85	2.31	2.03	0.70	55.31	1.95	107.68	4.000	Yes	No	2.00
553	40.61	92.44	2.36	2.12	0.71	49.44	2.15	106.53	4.000	Yes	No	2.00
554	40.69	80.59	2.43	2.30	0.74	42.14	2.54	106.96	4.000	Yes	No	2.00
555	40.80	68.65	2.51	2.44	0.76	35.01	3.03	106.21	4.000	Yes	No	2.00
556	40.87	59.91	2.58	2.61	0.78	29.84	3.59	107.20	4.000	Yes	No	2.00
557	40.95	53.47	2.64	2.76	0.80	26.09	4.12	107.50	4.000	Yes	Yes	2.00
558	40.97	51.37	2.65	2.73	0.80	24.94	4.24	105.79	4.000	Yes	Yes	2.00
559	41.01	54.31	2.61	2.50	0.79	26.70	3.81	101.77	4.000	Yes	Yes	2.00
560	41.07	61.80	2.51	2.12	0.76	31.20	3.04	94.92	4.000	Yes	No	2.00
561	41.15	67.40	2.44	1.89	0.74	34.61	2.61	90.47	4.000	Yes	No	2.00
562	41.26	67.13	2.44	1.87	0.74	34.39	2.61	89.74	0.147	No	No	0.74
563	41.35	63.05	2.48	1.98	0.75	31.86	2.87	91.40	0.151	No	No	0.76
564	41.47	60.28	2.52	2.09	0.76	30.09	3.10	93.27	0.155	No	No	0.78
565	41.59	59.67	2.53	2.13	0.77	29.62	3.18	94.19	0.158	No	No	0.79
566	41.69	60.42	2.53	2.16	0.77	29.94	3.18	95.29	0.160	No	No	0.80
567	41.78	59.17	2.55	2.27	0.77	29.08	3.36	97.63	0.167	No	No	0.83
568	41.88	54.75	2.61	2.48	0.79	26.41	3.82	100.94	3.600	No	Yes	2.00
569	41.98	49.45	2.67	2.69	0.81	23.32	4.43	103.21	3.600	No	Yes	2.00
570	42.08	45.13	2.72	2.83	0.83	20.88	4.96	103.54	3.600	No	Yes	2.00
571	42.16	44.32	2.73	2.78	0.83	20.43	4.99	102.01	3.600	No	Yes	2.00
572	42.24	47.12	2.68	2.60	0.81	21.98	4.53	99.69	3.600	No	Yes	2.00
573	42.31	52.25	2.62	2.38	0.79	24.86	3.91	97.23	3.600	No	Yes	2.00
574	42.45	56.94	2.57	2.24	0.78	27.44	3.48	95.61	0.161	No	No	0.80
575	42.55	59.37	2.54	2.18	0.77	28.78	3.30	94.91	0.160	No	No	0.80
576	42.60	59.78	2.54	2.18	0.77	28.96	3.29	95.14	0.160	No	No	0.80

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	42.70	59.34	2.55	2.25	0.77	28.59	3.38	96.60	0.164	No	No	0.82
578	42.81	57.38	2.59	2.39	0.78	27.33	3.64	99.43	0.171	No	No	0.85
579	42.89	53.57	2.64	2.62	0.80	25.06	4.12	103.15	3.600	No	Yes	2.00
580	42.98	48.27	2.71	2.91	0.82	22.02	4.84	106.61	3.600	No	Yes	2.00
581	43.08	43.14	2.79	3.21	0.84	19.16	5.69	108.99	3.600	No	Yes	2.00
582	43.17	40.44	2.83	3.35	0.86	17.68	6.18	109.35	3.600	No	Yes	2.00
583	43.27	41.05	2.81	3.20	0.85	18.01	5.94	107.03	3.600	No	Yes	2.00
584	43.37	43.81	2.71	2.52	0.82	19.71	4.84	95.48	3.600	No	Yes	2.00
585	43.50	46.82	2.61	1.93	0.79	21.62	3.86	83.44	3.600	No	Yes	2.00
586	43.61	48.54	2.54	1.53	0.77	22.85	3.24	73.95	0.118	No	No	0.59
587	43.74	49.31	2.54	1.57	0.77	23.16	3.25	75.29	0.120	No	No	0.60
588	43.79	49.31	2.56	1.72	0.78	22.99	3.44	79.06	0.126	No	No	0.63
589	43.86	48.47	2.60	1.95	0.79	22.31	3.79	84.59	3.600	No	Yes	2.00
590	43.94	47.05	2.66	2.26	0.81	21.30	4.28	91.16	3.600	No	Yes	2.00
591	44.00	44.89	2.72	2.63	0.82	19.92	4.92	98.08	3.600	No	Yes	2.00
592	44.08	42.33	2.78	2.98	0.84	18.39	5.62	103.37	3.600	No	Yes	2.00
593	44.17	38.85	2.85	3.30	0.86	16.48	6.45	106.26	3.600	No	Yes	2.00
594	44.27	35.44	2.90	3.43	0.88	14.71	7.14	105.00	3.600	No	Yes	2.00
595	44.42	34.16	2.90	3.25	0.88	14.09	7.15	100.72	3.600	No	Yes	2.00
596	44.52	37.10	2.82	2.76	0.85	15.69	6.06	95.03	3.600	No	Yes	2.00
597	44.61	44.15	2.68	2.18	0.81	19.52	4.49	87.72	3.600	No	Yes	2.00
598	44.71	51.91	2.57	1.87	0.78	23.77	3.51	83.46	0.134	No	No	0.67
599	44.85	56.66	2.53	1.83	0.77	26.27	3.19	83.87	0.135	No	No	0.67
600	44.95	57.30	2.55	1.98	0.77	26.40	3.34	88.11	0.144	No	No	0.71
601	45.09	54.98	2.59	2.17	0.79	24.92	3.69	92.06	0.153	No	No	0.76
602	45.19	50.09	2.66	2.39	0.81	22.17	4.29	95.00	3.600	No	Yes	2.00
603	45.33	43.44	2.76	2.73	0.83	18.53	5.31	98.48	3.600	No	Yes	2.00
604	45.42	37.17	2.85	3.08	0.86	15.25	6.56	100.02	3.600	No	Yes	2.00
605	45.57	34.20	2.90	3.17	0.88	13.74	7.18	98.64	3.600	No	Yes	2.00
606	45.68	32.58	2.91	3.02	0.88	12.98	7.29	94.66	3.600	No	Yes	2.00
607	45.81	30.45	2.91	2.71	0.88	12.02	7.30	87.72	3.600	No	Yes	2.00
608	45.92	26.54	3.01	2.83	1.00	9.26	8.96	82.93	3.600	No	Yes	2.00
609	46.05	22.29	3.11	3.22	1.00	7.59	10.87	82.51	3.600	No	Yes	2.00
610	46.16	19.32	3.23	4.05	1.00	6.43	13.40	86.12	3.600	No	Yes	2.00
611	46.17	17.73	3.28	4.34	1.00	5.82	14.71	85.57	3.600	No	Yes	2.00
612	46.23	17.46	3.28	4.24	1.00	5.70	14.75	84.09	3.600	No	Yes	2.00
613	46.29	16.85	3.29	4.16	1.00	5.46	15.02	82.02	3.600	No	Yes	2.00
614	46.34	16.04	3.31	3.98	1.00	5.15	15.32	78.81	3.600	No	Yes	2.00
615	46.42	15.30	3.31	3.71	1.00	4.85	15.44	74.90	3.600	No	Yes	2.00
616	46.48	14.90	3.30	3.33	1.00	4.69	15.10	70.80	3.600	No	Yes	2.00
617	46.52	14.69	3.28	3.04	1.00	4.61	14.73	67.86	3.600	No	Yes	2.00
618	46.60	14.56	3.27	2.84	1.00	4.55	14.47	65.79	3.600	No	Yes	2.00
619	46.67	14.49	3.26	2.68	1.00	4.51	14.23	64.21	3.600	No	Yes	2.00
620	46.74	14.45	3.25	2.57	1.00	4.49	14.03	63.02	3.600	No	Yes	2.00
621	46.82	14.42	3.25	2.46	1.00	4.47	13.84	61.88	3.600	No	Yes	2.00
622	46.88	14.19	3.25	2.42	1.00	4.37	13.96	61.07	3.600	No	Yes	2.00
623	46.96	14.10	3.25	2.39	1.00	4.33	13.99	60.61	3.600	No	Yes	2.00
624	47.06	13.97	3.26	2.41	1.00	4.27	14.16	60.52	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	47.15	14.11	3.26	2.45	1.00	4.31	14.15	61.03	3.600	No	Yes	2.00
626	47.24	14.43	3.28	2.83	1.00	4.42	14.72	65.10	3.600	No	Yes	2.00
627	47.35	16.18	3.29	3.62	1.00	5.07	14.87	75.39	3.600	No	Yes	2.00
628	47.49	19.69	3.20	3.51	1.00	6.36	12.67	80.67	3.600	No	Yes	2.00
629	47.58	24.11	3.09	3.10	1.00	8.00	10.33	82.65	3.600	No	Yes	2.00
630	47.73	26.03	3.03	2.80	1.00	8.69	9.32	80.95	3.600	No	Yes	2.00
631	47.83	27.06	3.02	2.79	1.00	9.05	9.05	81.84	3.600	No	Yes	2.00
632	47.87	26.18	3.04	2.97	1.00	8.71	9.55	83.19	3.600	No	Yes	2.00
633	47.89	26.93	3.02	2.82	1.00	8.98	9.14	82.12	3.600	No	Yes	2.00
634	47.94	26.64	3.02	2.81	1.00	8.87	9.20	81.59	3.600	No	Yes	2.00
635	48.02	26.81	3.02	2.75	1.00	8.91	9.08	80.90	3.600	No	Yes	2.00
636	48.07	26.40	3.03	2.79	1.00	8.75	9.26	81.07	3.600	No	Yes	2.00
637	48.12	25.97	3.05	2.94	1.00	8.58	9.61	82.45	3.600	No	Yes	2.00
638	48.18	25.43	3.07	3.12	1.00	8.37	10.05	84.09	3.600	No	Yes	2.00
639	48.26	25.01	3.09	3.28	1.00	8.20	10.42	85.42	3.600	No	Yes	2.00
640	48.31	24.60	3.10	3.27	1.00	8.04	10.54	84.77	3.600	No	Yes	2.00
641	48.38	24.56	3.08	3.09	1.00	8.01	10.30	82.58	3.600	No	Yes	2.00
642	48.46	24.71	3.06	2.82	1.00	8.05	9.85	79.31	3.600	No	Yes	2.00
643	48.52	24.41	3.05	2.59	1.00	7.93	9.58	75.99	3.600	No	Yes	2.00
644	48.60	23.16	3.05	2.42	1.00	7.46	9.70	72.40	3.600	No	Yes	2.00
645	48.68	20.77	3.10	2.41	1.00	6.57	10.59	69.64	3.600	No	Yes	2.00
646	48.74	18.20	3.17	2.55	1.00	5.63	12.04	67.76	3.600	No	Yes	2.00
647	48.82	15.94	3.25	2.86	1.00	4.80	14.01	67.24	3.600	No	Yes	2.00
648	48.89	14.56	3.31	3.07	1.00	4.29	15.49	66.41	3.600	No	Yes	2.00
649	48.99	13.82	3.34	3.08	1.00	4.01	16.21	64.98	3.600	No	Yes	2.00
650	49.05	13.65	3.32	2.83	1.00	3.94	15.85	62.48	3.600	No	Yes	2.00
651	49.12	13.51	3.31	2.54	1.00	3.89	15.38	59.74	3.600	No	Yes	2.00
652	49.18	13.55	3.28	2.25	1.00	3.89	14.70	57.20	3.600	No	Yes	2.00
653	49.27	13.75	3.26	2.06	1.00	3.96	14.08	55.71	3.600	No	Yes	2.00
654	49.32	13.92	3.24	1.91	1.00	4.01	13.56	54.42	3.600	No	Yes	2.00
655	49.42	13.55	3.25	1.92	1.00	3.87	13.92	53.88	3.600	No	Yes	2.00
656	49.48	13.11	3.27	1.97	1.00	3.71	14.46	53.63	3.600	No	Yes	2.00
657	49.56	13.01	3.28	2.04	1.00	3.66	14.76	54.09	3.600	No	Yes	2.00
658	49.66	13.28	3.28	2.12	1.00	3.75	14.73	55.25	3.600	No	Yes	2.00
659	49.76	13.68	3.27	2.16	1.00	3.89	14.49	56.33	3.600	No	Yes	2.00
660	49.85	14.06	3.23	1.87	1.00	4.01	13.46	54.00	3.600	No	Yes	2.00
661	49.99	14.87	3.17	1.52	1.00	4.29	11.96	51.28	3.600	No	Yes	2.00
662	50.09	14.43	3.16	1.38	1.00	4.12	11.90	49.07	3.600	No	Yes	2.00
663	50.21	13.82	3.21	1.57	1.00	3.89	12.94	50.39	3.600	No	Yes	2.00
664	50.24	13.21	3.24	1.66	1.00	3.68	13.72	50.47	3.600	No	Yes	2.00
665	50.29	13.59	3.21	1.54	1.00	3.81	13.05	49.66	3.600	No	Yes	2.00
666	50.38	13.69	3.20	1.45	1.00	3.83	12.73	48.82	3.600	No	Yes	2.00
667	50.47	13.39	3.21	1.45	1.00	3.72	13.00	48.36	3.600	No	Yes	2.00
668	50.52	12.98	3.24	1.53	1.00	3.57	13.61	48.61	3.600	No	Yes	2.00
669	50.62	13.01	3.24	1.57	1.00	3.58	13.73	49.09	3.600	No	Yes	2.00
670	50.66	13.15	3.24	1.60	1.00	3.62	13.70	49.58	3.600	No	Yes	2.00
671	50.76	13.28	3.24	1.64	1.00	3.66	13.70	50.11	3.600	No	Yes	2.00
672	50.83	14.13	3.21	1.63	1.00	3.95	12.99	51.29	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	50.91	14.30	3.23	1.81	1.00	4.00	13.34	53.36	3.600	No	Yes	2.00
674	51.00	15.61	3.19	1.82	1.00	4.45	12.42	55.29	3.600	No	Yes	2.00
675	51.06	17.36	3.13	1.78	1.00	5.06	11.27	56.99	3.600	No	Yes	2.00
676	51.15	17.67	3.16	2.10	1.00	5.15	11.86	61.08	3.600	No	Yes	2.00
677	51.24	16.35	3.27	2.96	1.00	4.68	14.43	67.57	3.600	No	Yes	2.00
678	51.31	12.88	3.51	5.15	1.00	3.47	21.69	75.27	3.600	No	Yes	2.00
679	51.39	18.55	3.28	3.96	1.00	5.43	14.77	80.15	3.600	No	Yes	2.00
680	51.48	32.14	2.90	2.47	0.88	11.43	7.23	82.64	3.600	No	Yes	2.00
681	51.58	35.38	2.87	2.60	0.87	12.78	6.83	87.30	3.600	No	Yes	2.00
682	51.68	27.82	3.10	3.71	1.00	8.59	10.70	91.85	3.600	No	Yes	2.00
683	51.77	17.84	3.45	6.98	1.00	5.13	19.49	100.06	3.600	No	Yes	2.00
684	51.90	36.80	3.02	4.07	1.00	11.62	9.16	106.47	3.600	No	Yes	2.00
685	52.01	74.42	2.58	2.71	0.78	30.49	3.61	110.20	4.000	Yes	No	2.00
686	52.11	128.50	2.34	2.42	0.71	57.50	2.11	121.05	4.000	Yes	No	2.00
687	52.26	161.87	2.25	2.35	0.68	74.64	1.77	131.90	4.000	Yes	No	2.00
688	52.30	209.17	2.12	2.06	0.65	100.78	1.45	146.55	4.000	Yes	No	2.00
689	52.33	248.44	2.00	1.70	0.61	124.60	1.31	162.63	4.000	Yes	No	2.00
690	52.35	302.93	1.87	1.40	0.57	158.50	1.21	192.22	4.000	Yes	No	2.00
691	52.40	347.53	1.78	1.23	0.54	187.07	1.12	209.95	4.000	Yes	No	2.00
692	52.45	381.51	1.72	1.16	0.53	208.63	1.04	216.58	4.000	Yes	No	2.00
693	52.50	415.58	1.69	1.13	0.51	229.89	1.00	229.89	4.000	No	No	2.00
694	52.55	447.33	1.67	1.14	0.51	248.98	1.00	248.98	4.000	No	No	2.00
695	52.60	486.53	1.63	1.11	0.50	273.15	1.00	273.15	4.000	No	No	2.00
696	52.65	516.02	1.60	1.04	0.50	289.64	1.00	289.64	4.000	No	No	2.00
697	52.71	531.14	1.57	0.97	0.50	297.95	1.00	297.95	4.000	No	No	2.00
698	52.77	541.83	1.53	0.90	0.50	303.79	1.00	303.79	4.000	No	No	2.00
699	52.82	558.50	1.51	0.85	0.50	312.99	1.00	312.99	4.000	No	No	2.00
700	52.88	578.13	1.48	0.81	0.50	323.84	1.00	323.84	4.000	No	No	2.00
701	52.93	592.07	1.46	0.79	0.50	331.46	1.00	331.46	4.000	No	No	2.00
702	52.98	605.70	1.46	0.78	0.50	338.95	1.00	338.95	4.000	No	No	2.00
703	53.03	608.64	1.46	0.79	0.50	340.39	1.00	340.39	4.000	No	No	2.00
704	53.08	608.27	1.46	0.80	0.50	340.01	1.00	340.01	4.000	No	No	2.00
705	53.12	601.01	1.47	0.80	0.50	335.78	1.00	335.78	4.000	No	No	2.00
706	53.17	598.22	1.46	0.78	0.50	333.99	1.00	333.99	4.000	No	No	2.00
707	53.23	600.71	1.45	0.76	0.50	335.19	1.00	335.19	4.000	No	No	2.00
708	53.28	596.23	1.47	0.79	0.50	332.45	1.00	332.45	4.000	No	No	2.00
709	53.37	588.50	1.48	0.83	0.50	327.80	1.00	327.80	4.000	No	No	2.00
710	53.42	584.11	1.50	0.86	0.50	325.17	1.00	325.17	4.000	No	No	2.00
711	53.46	586.81	1.52	0.90	0.50	326.50	1.00	326.50	4.000	No	No	2.00
712	53.53	599.03	1.53	0.96	0.50	333.09	1.00	333.09	4.000	No	No	2.00
713	53.61	597.34	1.56	1.05	0.50	331.84	1.00	331.84	4.000	No	No	2.00
714	53.62	582.26	1.60	1.13	0.50	323.39	1.00	323.39	4.000	No	No	2.00
715	53.65	574.05	1.60	1.15	0.50	318.67	1.00	318.67	4.000	No	No	2.00
716	53.67	571.35	1.61	1.16	0.50	317.12	1.00	317.12	4.000	No	No	2.00
717	53.70	583.83	1.59	1.12	0.50	323.95	1.00	323.95	4.000	No	No	2.00
718	53.74	582.83	1.60	1.14	0.50	323.26	1.00	323.26	4.000	No	No	2.00
719	53.76	583.81	1.60	1.14	0.50	323.74	1.00	323.74	4.000	No	No	2.00
720	53.80	581.08	1.59	1.13	0.50	322.06	1.00	322.06	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	53.84	577.81	1.59	1.10	0.50	320.07	1.00	320.07	4.000	No	No	2.00
722	53.90	578.23	1.58	1.07	0.50	320.12	1.00	320.12	4.000	No	No	2.00
723	53.91	570.20	1.59	1.08	0.50	315.61	1.00	315.61	4.000	No	No	2.00
724	53.95	573.64	1.58	1.08	0.50	317.38	1.00	317.38	4.000	No	No	2.00
725	53.96	579.94	1.58	1.07	0.50	320.83	1.00	320.83	4.000	No	No	2.00
726	53.98	601.06	1.56	1.04	0.50	332.48	1.00	332.48	4.000	No	No	2.00
727	53.99	602.95	1.56	1.03	0.50	333.50	1.00	333.50	4.000	No	No	2.00
728	54.01	592.15	1.57	1.05	0.50	327.46	1.00	327.46	4.000	No	No	2.00
729	54.02	579.33	1.58	1.08	0.50	320.31	1.00	320.31	4.000	No	No	2.00
730	54.03	553.15	1.61	1.13	0.50	305.74	1.00	305.74	4.000	No	No	2.00
731	54.04	504.84	1.67	1.24	0.51	276.21	1.00	276.21	4.000	No	No	2.00
732	54.05	452.17	1.75	1.40	0.53	241.19	1.08	260.14	4.000	No	No	2.00
733	54.09	422.63	1.79	1.51	0.55	221.81	1.15	254.46	4.000	No	No	2.00
734	54.10	421.59	1.80	1.53	0.55	220.94	1.15	254.57	4.000	No	No	2.00
735	54.13	421.89	1.80	1.53	0.55	221.06	1.15	254.64	4.000	No	No	2.00
736	54.14	420.96	1.80	1.54	0.55	220.34	1.16	254.59	4.000	No	No	2.00
737	54.19	422.82	1.80	1.54	0.55	221.19	1.16	255.77	4.000	No	No	2.00
738	54.19	428.79	1.80	1.55	0.55	224.52	1.15	258.95	4.000	No	No	2.00
739	54.24	439.22	1.77	1.47	0.54	231.86	1.12	259.93	4.000	No	No	2.00
740	54.29	456.97	1.71	1.29	0.52	245.94	1.02	249.88	4.000	No	No	2.00
741	54.33	474.10	1.64	1.08	0.50	261.31	1.00	261.31	4.000	No	No	2.00
742	54.38	494.95	1.57	0.92	0.50	272.80	1.00	272.80	4.000	No	No	2.00
743	54.39	512.70	1.53	0.85	0.50	282.62	1.00	282.62	4.000	No	No	2.00
744	54.43	529.13	1.52	0.84	0.50	291.66	1.00	291.66	4.000	No	No	2.00
745	54.48	543.10	1.44	0.67	0.50	299.32	1.00	299.32	4.000	No	No	2.00
746	54.52	556.66	1.36	0.53	0.50	306.76	1.00	306.76	4.000	No	No	2.00
747	54.58	573.87	1.26	0.38	0.50	316.20	1.00	316.20	4.000	No	No	2.00
748	54.62	587.13	1.28	0.42	0.50	323.46	1.00	323.46	4.000	No	No	2.00
749	54.65	604.44	1.29	0.46	0.50	333.00	1.00	333.00	4.000	No	No	2.00
750	54.67	623.33	1.30	0.48	0.50	343.41	1.00	343.41	4.000	No	No	2.00
751	54.71	658.15	1.28	0.48	0.50	362.60	1.00	362.60	4.000	No	No	2.00
752	54.77	679.34	1.20	0.37	0.50	374.21	1.00	374.21	4.000	No	No	2.00
753	54.81	702.99	1.11	0.28	0.50	387.19	1.00	387.19	4.000	No	No	2.00
754	54.85	704.07	1.04	0.22	0.50	387.70	1.00	387.70	4.000	No	No	2.00
755	54.86	709.13	1.06	0.24	0.50	390.48	1.00	390.48	4.000	No	No	2.00
756	54.87	703.33	1.09	0.27	0.50	387.26	1.00	387.26	4.000	No	No	2.00
757	54.91	703.66	1.13	0.30	0.50	387.35	1.00	387.35	4.000	No	No	2.00
758	54.96	707.14	1.16	0.34	0.50	389.17	1.00	389.17	4.000	No	No	2.00
759	55.00	703.19	1.18	0.36	0.50	386.89	1.00	386.89	4.000	No	No	2.00
760	55.01	695.84	1.19	0.37	0.50	382.82	1.00	382.82	4.000	No	No	2.00
761	55.05	679.11	1.21	0.39	0.50	373.47	1.00	373.47	4.000	No	No	2.00
762	55.10	651.07	1.24	0.42	0.50	357.87	1.00	357.87	4.000	No	No	2.00
763	55.12	603.77	1.29	0.46	0.50	331.72	1.00	331.72	4.000	No	No	2.00
764	55.13	570.97	1.33	0.49	0.50	313.58	1.00	313.58	4.000	No	No	2.00
765	55.14	563.11	1.33	0.48	0.50	309.22	1.00	309.22	4.000	No	No	2.00
766	55.19	576.91	1.31	0.46	0.50	316.75	1.00	316.75	4.000	No	No	2.00
767	55.20	576.27	1.31	0.46	0.50	316.38	1.00	316.38	4.000	No	No	2.00
768	55.25	562.13	1.33	0.48	0.50	308.48	1.00	308.48	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	55.29	546.07	1.37	0.52	0.50	299.55	1.00	299.55	4.000	No	No	2.00
770	55.33	519.69	1.42	0.59	0.50	284.92	1.00	284.92	4.000	No	No	2.00
771	55.38	481.16	1.52	0.76	0.50	263.59	1.00	263.59	4.000	No	No	2.00
772	55.48	439.32	1.63	0.99	0.50	240.38	1.00	240.38	4.000	No	No	2.00
773	55.57	411.39	1.73	1.22	0.53	218.55	1.04	227.87	4.000	No	No	2.00
774	55.63	398.09	1.80	1.45	0.55	206.42	1.15	237.94	4.000	No	No	2.00
775	55.72	402.04	1.83	1.60	0.56	206.08	1.19	244.53	4.000	No	No	2.00
776	55.80	431.09	1.82	1.63	0.55	221.88	1.17	260.68	4.000	No	No	2.00
777	55.86	480.55	1.67	1.19	0.51	259.76	1.00	259.76	4.000	No	No	2.00
778	55.97	527.85	1.51	0.79	0.50	288.32	1.00	288.32	4.000	No	No	2.00
779	56.01	560.55	1.34	0.49	0.50	306.20	1.00	306.20	4.000	No	No	2.00
780	56.06	587.84	1.50	0.47	1.00	186.61	1.00	186.61	0.684	No	No	2.00
781	56.11	613.11	1.50	0.51	1.00	194.57	1.00	194.57	0.765	No	No	2.00
782	56.15	640.71	1.51	0.55	1.00	203.27	1.00	203.27	4.000	No	No	2.00
783	56.20	660.92	1.52	0.59	1.00	209.60	1.00	209.60	4.000	No	No	2.00
784	56.27	663.16	1.53	0.63	1.00	210.15	1.00	210.15	4.000	No	No	2.00
785	56.27	664.17	1.56	0.69	1.00	210.45	1.00	210.45	4.000	No	No	2.00
786	56.30	642.20	1.61	0.79	1.00	203.39	1.00	203.39	4.000	No	No	2.00
787	56.33	649.54	1.64	0.87	1.00	205.64	1.00	205.64	4.000	No	No	2.00
788	56.35	647.65	1.66	0.92	1.00	205.00	1.00	205.00	4.000	No	No	2.00
789	56.40	667.86	1.64	0.90	1.00	211.31	1.00	211.31	4.000	No	No	2.00
790	56.41	669.34	1.64	0.90	1.00	211.76	1.00	211.76	4.000	No	No	2.00
791	56.44	681.53	1.63	0.88	1.00	215.53	1.00	215.53	4.000	No	No	2.00
792	56.49	695.19	1.62	0.87	1.00	219.75	1.00	219.75	4.000	No	No	2.00
793	56.54	717.49	1.61	0.87	1.00	226.71	1.00	226.71	4.000	No	No	2.00
794	56.58	737.23	1.61	0.89	1.00	232.85	1.00	232.85	4.000	No	No	2.00
795	56.59	750.18	1.61	0.91	1.00	236.93	1.00	236.93	4.000	No	No	2.00
796	56.64	757.34	1.60	0.90	1.00	239.07	1.00	239.07	4.000	No	No	2.00
797	56.69	764.80	1.60	0.90	1.00	241.29	1.00	241.29	4.000	No	No	2.00
798	56.73	778.16	1.59	0.88	1.00	245.40	1.00	245.40	4.000	No	No	2.00
799	56.78	778.56	1.58	0.86	1.00	245.38	1.00	245.38	4.000	No	No	2.00
800	56.83	759.53	1.58	0.83	1.00	239.22	1.00	239.22	4.000	No	No	2.00
801	56.88	731.80	1.58	0.82	1.00	230.32	1.00	230.32	4.000	No	No	2.00
802	56.89	708.89	1.60	0.82	1.00	223.03	1.00	223.03	4.000	No	No	2.00
803	56.95	692.53	1.59	0.80	1.00	217.71	1.00	217.71	4.000	No	No	2.00
804	57.01	668.00	1.59	0.77	1.00	209.81	1.00	209.81	4.000	No	No	2.00
805	57.07	645.94	1.58	0.71	1.00	202.70	1.00	202.70	4.000	No	No	2.00
806	57.11	619.45	1.52	0.54	1.00	194.25	1.00	194.25	0.762	No	No	2.00
807	57.17	598.63	1.46	0.41	1.00	187.56	1.00	187.56	0.694	No	No	2.00
808	57.26	574.07	1.37	0.26	1.00	179.66	1.00	179.66	0.619	No	No	2.00
809	57.31	547.05	1.43	0.31	1.00	171.06	1.00	171.06	0.546	No	No	2.00
810	57.37	520.16	1.45	0.32	1.00	162.50	1.00	162.50	0.479	No	No	2.00
811	57.45	490.27	1.51	0.38	1.00	152.96	1.00	152.96	0.413	No	No	2.00
812	57.51	451.30	1.55	0.39	1.00	140.63	1.00	140.63	0.339	No	No	1.75
813	57.53	421.54	1.59	0.41	1.00	131.27	1.00	131.27	0.290	No	No	1.50
814	57.59	401.40	1.62	0.43	1.00	124.87	1.00	124.87	0.261	No	No	1.35
815	57.63	398.96	1.62	0.43	1.00	124.05	1.00	124.05	0.258	No	No	1.33
816	57.68	391.51	1.63	0.44	1.00	121.66	1.00	121.66	0.247	No	No	1.28

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	57.73	386.48	1.64	0.44	1.00	120.01	1.00	120.01	0.241	No	No	1.24
818	57.78	379.02	1.65	0.44	1.00	117.62	1.00	117.62	0.231	No	No	1.19
819	57.86	359.96	1.66	0.43	1.00	111.55	1.00	111.55	0.209	No	No	1.08
820	57.92	326.32	1.71	0.47	1.00	100.97	1.00	100.97	4.000	Yes	No	2.00
821	57.98	290.83	1.76	0.47	1.00	89.82	1.00	89.82	4.000	Yes	No	2.00
822	58.06	263.33	1.82	0.53	1.00	81.16	1.18	95.51	4.000	Yes	No	2.00
823	58.12	242.92	1.90	0.64	1.00	74.75	1.24	92.39	4.000	Yes	No	2.00
824	58.21	222.41	1.99	0.82	1.00	68.28	1.30	88.73	4.000	Yes	No	2.00
825	58.26	204.43	2.06	0.97	1.00	62.64	1.37	85.71	4.000	Yes	No	2.00
826	58.35	180.37	2.14	1.08	1.00	55.10	1.48	81.38	4.000	Yes	No	2.00
827	58.41	154.93	2.19	1.08	1.00	47.15	1.59	74.91	4.000	Yes	No	2.00
828	58.50	122.84	2.29	1.16	1.00	37.13	1.90	70.73	4.000	Yes	No	2.00
829	58.56	98.18	2.38	1.18	1.00	29.45	2.28	67.27	4.000	Yes	No	2.00
830	58.64	77.90	2.53	1.55	1.00	23.14	3.23	74.61	4.000	Yes	No	2.00
831	58.73	63.67	2.66	1.93	1.00	18.70	4.34	81.15	4.000	Yes	Yes	2.00
832	58.80	51.12	2.80	2.41	1.00	14.80	5.89	87.16	4.000	Yes	Yes	2.00
833	58.84	42.24	2.93	2.94	1.00	12.04	7.59	91.44	4.000	Yes	Yes	2.00
834	58.85	43.79	2.90	2.86	1.00	12.52	7.27	91.06	3.600	No	Yes	2.00
835	58.93	50.50	2.81	2.45	1.00	14.59	6.00	87.49	3.600	No	Yes	2.00
836	58.98	58.12	2.72	2.06	1.00	16.94	4.87	82.49	3.600	No	Yes	2.00
837	59.02	61.77	2.67	1.86	1.00	18.06	4.38	79.02	3.600	No	Yes	2.00
838	59.12	63.39	2.65	1.79	1.00	18.54	4.19	77.74	3.600	No	Yes	2.00
839	59.17	65.41	2.64	1.79	1.00	19.15	4.09	78.34	3.600	No	Yes	2.00
840	59.27	67.33	2.63	1.85	1.00	19.73	4.06	80.06	3.600	No	Yes	2.00
841	59.31	67.64	2.64	1.94	1.00	19.81	4.15	82.31	3.600	No	Yes	2.00
842	59.41	64.84	2.68	2.06	1.00	18.93	4.46	84.40	3.600	No	Yes	2.00
843	59.46	57.99	2.74	2.22	1.00	16.81	5.11	85.91	3.600	No	Yes	2.00
844	59.55	48.77	2.83	2.45	1.00	13.96	6.20	86.53	3.600	No	Yes	2.00
845	59.65	39.66	2.91	2.48	1.00	11.14	7.37	82.12	3.600	No	Yes	2.00
846	59.70	34.25	2.97	2.47	1.00	9.47	8.28	78.48	3.600	No	Yes	2.00
847	59.80	32.07	2.99	2.40	1.00	8.80	8.61	75.77	3.600	No	Yes	2.00
848	59.89	32.04	3.01	2.66	1.00	8.78	9.03	79.29	3.600	No	Yes	2.00
849	59.94	31.04	3.06	2.98	1.00	8.47	9.76	82.68	3.600	No	Yes	2.00
850	60.01	30.35	3.09	3.25	1.00	8.25	10.33	85.21	3.600	No	Yes	2.00
851	60.02	32.64	3.04	3.10	1.00	8.95	9.57	85.70	3.600	No	Yes	2.00
852	60.08	35.54	2.99	2.84	1.00	9.83	8.61	84.70	3.600	No	Yes	2.00
853	60.12	36.56	2.97	2.70	1.00	10.14	8.23	83.40	3.600	No	Yes	2.00
854	60.17	32.87	3.01	2.76	1.00	9.01	9.03	81.32	3.600	No	Yes	2.00
855	60.27	28.56	3.07	2.73	1.00	7.68	10.03	76.99	3.600	No	Yes	2.00
856	60.31	24.81	3.12	2.61	1.00	6.53	11.00	71.83	3.600	No	Yes	2.00
857	60.37	22.21	3.15	2.46	1.00	5.73	11.72	67.16	3.600	No	Yes	2.00
858	60.46	20.93	3.17	2.32	1.00	5.33	12.03	64.16	3.600	No	Yes	2.00
859	60.51	20.76	3.15	2.06	1.00	5.28	11.57	61.05	3.600	No	Yes	2.00
860	60.61	21.43	3.11	1.87	1.00	5.48	10.86	59.48	3.600	No	Yes	2.00
861	60.65	21.84	3.09	1.76	1.00	5.60	10.44	58.49	3.600	No	Yes	2.00
862	60.75	22.18	3.08	1.74	1.00	5.70	10.27	58.52	3.600	No	Yes	2.00
863	60.81	22.25	3.08	1.74	1.00	5.72	10.24	58.52	3.600	No	Yes	2.00
864	60.89	22.21	3.08	1.71	1.00	5.70	10.20	58.14	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	60.94	22.45	3.07	1.71	1.00	5.77	10.12	58.37	3.600	No	Yes	2.00
866	61.03	22.62	3.08	1.77	1.00	5.81	10.19	59.27	3.600	No	Yes	2.00
867	61.09	22.65	3.08	1.79	1.00	5.82	10.23	59.56	3.600	No	Yes	2.00
868	61.19	22.38	3.08	1.78	1.00	5.74	10.30	59.09	3.600	No	Yes	2.00
869	61.24	22.96	3.06	1.69	1.00	5.91	9.90	58.48	3.600	No	Yes	2.00
870	61.33	24.51	3.03	1.68	1.00	6.37	9.35	59.55	3.600	No	Yes	2.00
871	61.38	24.20	3.09	2.19	1.00	6.28	10.50	65.92	3.600	No	Yes	2.00
872	61.47	23.16	3.18	2.97	1.00	5.95	12.35	73.50	3.600	No	Yes	2.00
873	61.53	21.88	3.28	3.99	1.00	5.56	14.59	81.14	3.600	No	Yes	2.00
874	61.62	27.61	3.13	3.27	1.00	7.29	11.24	81.97	3.600	No	Yes	2.00
875	61.70	44.48	2.86	2.37	1.00	12.39	6.68	82.73	3.600	No	Yes	2.00
876	61.77	66.81	2.67	2.07	1.00	19.14	4.44	84.93	3.600	No	Yes	2.00
877	61.86	81.96	2.60	2.12	1.00	23.70	3.78	89.66	3.600	No	Yes	2.00
878	61.95	81.02	2.63	2.34	1.00	23.39	4.06	94.89	3.600	No	Yes	2.00
879	61.97	72.62	2.69	2.53	1.00	20.85	4.65	96.91	3.600	No	Yes	2.00
880	62.01	62.36	2.78	2.84	1.00	17.75	5.62	99.66	4.000	No	Yes	2.00
881	62.10	52.17	2.87	3.09	1.00	14.66	6.77	99.23	4.000	Yes	Yes	2.00
882	62.24	55.41	2.79	2.50	1.00	15.61	5.76	89.92	4.000	Yes	Yes	2.00
883	62.34	87.70	2.48	1.40	1.00	25.31	2.83	71.54	4.000	Yes	No	2.00
884	62.49	127.58	2.25	0.95	1.00	37.26	1.74	64.77	4.000	Yes	No	2.00
885	62.54	164.52	2.11	0.82	1.00	48.34	1.44	69.68	4.000	Yes	No	2.00
886	62.66	181.39	2.07	0.78	1.00	53.35	1.37	73.33	4.000	Yes	No	2.00
887	62.74	199.68	2.02	0.75	1.00	58.78	1.33	77.94	4.000	Yes	No	2.00
888	62.87	211.65	1.99	0.72	1.00	62.29	1.30	80.99	4.000	No	No	2.00
889	62.92	217.18	1.98	0.72	1.00	63.92	1.29	82.65	4.000	No	No	2.00
890	63.03	219.18	1.98	0.73	1.00	64.44	1.29	83.41	4.000	No	No	2.00
891	63.15	218.06	1.99	0.76	1.00	64.03	1.30	83.38	4.000	No	No	2.00
892	63.26	213.11	2.01	0.79	1.00	62.49	1.32	82.35	4.000	No	No	2.00
893	63.37	206.70	2.03	0.82	1.00	60.51	1.34	80.92	4.000	No	No	2.00
894	63.45	200.15	2.04	0.79	1.00	58.51	1.34	78.49	4.000	No	No	2.00
895	63.54	197.59	2.02	0.71	1.00	57.70	1.32	76.31	4.000	No	No	2.00
896	63.61	190.30	2.02	0.68	1.00	55.49	1.33	73.61	4.000	Yes	No	2.00
897	63.69	172.04	2.08	0.74	1.00	50.02	1.39	69.47	4.000	Yes	No	2.00
898	63.79	141.71	2.22	0.97	1.00	40.98	1.65	67.77	4.000	Yes	No	2.00
899	63.89	106.15	2.36	1.15	1.00	30.39	2.20	66.74	4.000	Yes	No	2.00
900	63.98	75.22	2.55	1.47	1.00	21.20	3.37	71.48	4.000	Yes	No	2.00
901	64.07	53.15	2.72	1.67	1.00	14.65	4.91	71.91	4.000	Yes	Yes	2.00
902	64.15	39.12	2.91	2.21	1.00	10.48	7.30	76.48	4.000	Yes	Yes	2.00
903	64.23	29.98	3.07	2.76	1.00	7.77	10.00	77.68	4.000	No	Yes	2.00
904	64.26	25.15	3.18	3.28	1.00	6.34	12.34	78.26	4.000	No	Yes	2.00
905	64.29	23.57	3.22	3.48	1.00	5.87	13.31	78.14	4.000	No	Yes	2.00
906	64.33	23.37	3.21	3.17	1.00	5.81	12.89	74.86	4.000	No	Yes	2.00
907	64.43	22.99	3.19	2.81	1.00	5.69	12.43	70.78	4.000	No	Yes	2.00
908	64.47	22.29	3.17	2.45	1.00	5.48	12.05	66.07	4.000	No	Yes	2.00
909	64.53	21.82	3.17	2.32	1.00	5.34	12.01	64.15	4.000	No	Yes	2.00
910	64.62	20.60	3.20	2.39	1.00	4.98	12.74	63.40	4.000	No	Yes	2.00
911	64.72	19.12	3.25	2.57	1.00	4.53	13.95	63.23	4.000	No	Yes	2.00
912	64.78	18.00	3.30	2.81	1.00	4.20	15.17	63.74	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	64.86	18.21	3.30	2.92	1.00	4.26	15.26	65.01	4.000	No	Yes	2.00
914	64.96	18.78	3.31	3.20	1.00	4.42	15.44	68.31	4.000	No	Yes	2.00
915	65.06	19.22	3.32	3.52	1.00	4.55	15.74	71.61	4.000	No	Yes	2.00
916	65.11	19.22	3.34	3.90	1.00	4.55	16.41	74.58	4.000	No	Yes	2.00
917	65.21	18.85	3.37	4.16	1.00	4.43	17.13	75.90	4.000	No	Yes	2.00
918	65.31	18.45	3.39	4.32	1.00	4.31	17.70	76.26	4.000	No	Yes	2.00
919	65.40	18.28	3.37	3.90	1.00	4.25	17.10	72.77	4.000	No	Yes	2.00
920	65.50	18.58	3.32	3.22	1.00	4.34	15.67	67.97	4.000	No	Yes	2.00
921	65.58	19.02	3.26	2.59	1.00	4.46	14.15	63.13	4.000	No	Yes	2.00
922	65.68	19.05	3.24	2.38	1.00	4.47	13.69	61.17	4.000	No	Yes	2.00
923	65.78	17.67	3.29	2.52	1.00	4.06	14.89	60.45	4.000	No	Yes	2.00
924	65.84	16.40	3.34	2.66	1.00	3.69	16.19	59.69	4.000	No	Yes	2.00
925	65.86	15.56	3.38	2.83	1.00	3.44	17.33	59.62	4.000	No	Yes	2.00
926	65.87	16.51	3.33	2.60	1.00	3.72	15.97	59.36	4.000	No	Yes	2.00
927	65.98	17.26	3.29	2.44	1.00	3.93	15.03	59.09	4.000	No	Yes	2.00
928	66.10	17.84	3.28	2.46	1.00	4.09	14.69	60.13	4.000	No	Yes	2.00
929	66.21	18.21	3.29	2.65	1.00	4.20	14.85	62.32	4.000	No	Yes	2.00
930	66.34	18.48	3.28	2.68	1.00	4.27	14.76	63.01	4.000	No	Yes	2.00
931	66.48	19.00	3.27	2.66	1.00	4.42	14.39	63.55	4.000	No	Yes	2.00
932	66.62	18.46	3.28	2.63	1.00	4.25	14.69	62.45	4.000	No	Yes	2.00
933	66.68	18.67	3.29	2.78	1.00	4.31	14.87	64.07	4.000	No	Yes	2.00
934	66.87	18.92	3.31	3.19	1.00	4.37	15.53	67.94	4.000	No	Yes	2.00
935	66.96	19.16	3.35	3.89	1.00	4.44	16.65	73.89	4.000	No	Yes	2.00
936	67.11	18.25	3.42	4.74	1.00	4.17	18.76	78.15	4.000	No	Yes	2.00
937	67.21	16.83	3.47	4.99	1.00	3.75	20.42	76.60	4.000	No	Yes	2.00
938	67.35	16.22	3.48	4.67	1.00	3.57	20.50	73.18	4.000	No	Yes	2.00
939	67.45	16.16	3.52	5.49	1.00	3.55	21.95	77.86	4.000	No	Yes	2.00
940	67.59	27.42	3.21	4.13	1.00	6.79	13.06	88.71	4.000	No	Yes	2.00
941	67.68	77.39	2.62	1.95	1.00	21.19	3.95	83.67	4.000	Yes	Yes	2.00
942	67.83	159.77	2.22	1.13	1.00	44.89	1.66	74.68	4.000	Yes	No	2.00
943	67.92	241.25	1.99	0.82	1.00	68.29	1.30	88.64	4.000	Yes	No	2.00
944	68.02	283.19	1.90	0.72	1.00	80.28	1.24	99.35	4.000	Yes	No	2.00
945	68.07	299.01	1.88	0.72	1.00	84.78	1.22	103.71	4.000	Yes	No	2.00
946	68.16	305.70	1.87	0.71	1.00	86.62	1.22	105.26	4.000	No	No	2.00
947	68.26	310.93	1.86	0.70	1.00	88.04	1.21	106.54	4.000	No	No	2.00
948	68.35	307.75	1.88	0.74	1.00	87.05	1.22	106.44	4.000	No	No	2.00
949	68.45	299.96	1.91	0.81	1.00	84.74	1.24	105.37	4.000	No	No	2.00
950	68.55	291.49	1.94	0.86	1.00	82.23	1.26	103.72	4.000	No	No	2.00
951	68.65	271.72	1.98	0.91	1.00	76.50	1.29	98.57	4.000	No	No	2.00
952	68.78	253.59	2.02	0.98	1.00	71.23	1.32	94.35	4.000	No	No	2.00
953	68.78	238.18	2.05	1.03	1.00	66.83	1.36	90.91	4.000	No	No	2.00
954	68.79	234.24	2.06	1.02	1.00	65.70	1.37	89.70	4.000	No	No	2.00
955	68.83	237.70	2.03	0.94	1.00	66.66	1.34	89.08	4.000	No	No	2.00
956	68.93	243.69	1.99	0.81	1.00	68.30	1.30	88.59	4.000	No	No	2.00
957	68.98	253.54	1.93	0.67	1.00	71.08	1.25	89.18	4.000	No	No	2.00
958	69.04	257.79	1.89	0.60	1.00	72.25	1.23	89.05	4.000	No	No	2.00
959	69.12	259.28	1.89	0.58	1.00	72.61	1.23	89.10	4.000	No	No	2.00
960	69.22	255.36	1.90	0.59	1.00	71.43	1.24	88.23	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
961	69.28	247.73	1.91	0.61	1.00	69.22	1.25	86.25	4.000	No	No	2.00
962	69.36	237.41	1.93	0.61	1.00	66.24	1.26	83.22	4.000	No	No	2.00
963	69.45	223.58	1.95	0.61	1.00	62.26	1.27	79.21	4.000	No	No	2.00
964	69.60	210.12	1.98	0.61	1.00	58.37	1.29	75.34	4.000	No	No	2.00
965	69.70	198.18	2.01	0.62	1.00	54.94	1.31	72.05	4.000	No	No	2.00
966	69.80	193.42	2.01	0.62	1.00	53.54	1.32	70.68	4.000	No	No	2.00
967	69.89	192.07	2.02	0.62	1.00	53.12	1.32	70.30	4.000	No	No	2.00
968	69.98	190.15	2.02	0.63	1.00	52.53	1.33	69.82	4.000	No	No	2.00
969	70.08	181.88	2.04	0.63	1.00	50.15	1.35	67.53	4.000	Yes	No	2.00
970	70.18	159.82	2.12	0.71	1.00	43.89	1.45	63.51	4.000	Yes	No	2.00
971	70.32	124.32	2.27	0.89	1.00	33.85	1.81	61.16	4.000	Yes	No	2.00
972	70.42	84.31	2.50	1.27	1.00	22.56	2.96	66.77	4.000	Yes	No	2.00
973	70.54	51.82	2.77	1.84	1.00	13.41	5.53	74.19	4.000	Yes	Yes	2.00
974	70.66	31.85	3.05	2.58	1.00	7.79	9.69	75.54	4.000	No	Yes	2.00
975	70.75	23.52	3.23	3.11	1.00	5.45	13.34	72.70	4.000	No	Yes	2.00
976	70.80	21.80	3.23	2.72	1.00	4.97	13.43	66.71	4.000	No	Yes	2.00
977	70.89	22.64	3.14	1.98	1.00	5.20	11.52	59.87	4.000	No	Yes	2.00
978	70.99	22.34	3.09	1.45	1.00	5.11	10.38	53.00	4.000	No	Yes	2.00
979	71.08	21.63	3.07	1.23	1.00	4.90	10.09	49.46	4.000	No	Yes	2.00
980	71.17	21.43	3.06	1.12	1.00	4.84	9.87	47.79	4.000	No	Yes	2.00
981	71.23	20.92	3.07	1.10	1.00	4.70	10.01	47.05	4.000	No	Yes	2.00
982	71.33	21.09	3.05	1.03	1.00	4.74	9.74	46.20	4.000	No	Yes	2.00
983	71.42	21.73	3.02	0.90	1.00	4.92	9.08	44.64	4.000	No	Yes	2.00
984	71.52	22.81	2.97	0.78	1.00	5.22	8.26	43.06	4.000	No	Yes	2.00
985	71.58	23.21	2.97	0.82	1.00	5.33	8.27	44.01	4.000	No	Yes	2.00
986	71.67	22.88	3.02	1.04	1.00	5.23	9.07	47.43	4.000	No	Yes	2.00
987	71.81	22.47	3.06	1.28	1.00	5.11	9.94	50.76	4.000	No	Yes	2.00
988	71.82	22.24	3.09	1.43	1.00	5.04	10.42	52.55	4.000	No	Yes	2.00
989	71.86	21.97	3.10	1.47	1.00	4.96	10.64	52.82	4.000	No	Yes	2.00
990	71.91	21.83	3.11	1.49	1.00	4.92	10.75	52.95	4.000	No	Yes	2.00
991	71.97	21.60	3.12	1.53	1.00	4.86	10.97	53.27	4.000	No	Yes	2.00
992	72.05	21.36	3.13	1.58	1.00	4.79	11.22	53.72	4.000	No	Yes	2.00
993	72.10	21.13	3.14	1.65	1.00	4.72	11.52	54.35	4.000	No	Yes	2.00
994	72.20	20.99	3.15	1.70	1.00	4.68	11.71	54.79	4.000	No	Yes	2.00
995	72.25	20.99	3.16	1.76	1.00	4.67	11.87	55.49	4.000	No	Yes	2.00
996	72.34	21.09	3.17	1.88	1.00	4.70	12.12	56.94	4.000	No	Yes	2.00
997	72.44	21.09	3.19	2.06	1.00	4.69	12.53	58.80	4.000	No	Yes	2.00
998	72.53	20.89	3.21	2.23	1.00	4.63	13.04	60.40	4.000	No	Yes	2.00
999	72.63	20.79	3.22	2.32	1.00	4.60	13.29	61.13	4.000	No	Yes	2.00
1000	72.69	20.48	3.23	2.36	1.00	4.51	13.55	61.14	4.000	No	Yes	2.00
1001	72.82	20.69	3.23	2.31	1.00	4.56	13.34	60.87	4.000	No	Yes	2.00
1002	72.92	21.13	3.20	2.18	1.00	4.68	12.83	60.05	4.000	No	Yes	2.00
1003	73.06	22.11	3.17	2.01	1.00	4.95	11.98	59.27	4.000	No	Yes	2.00
1004	73.16	22.34	3.16	2.02	1.00	5.01	11.90	59.57	4.000	No	Yes	2.00
1005	73.30	20.86	3.22	2.28	1.00	4.59	13.21	60.65	4.000	No	Yes	2.00
1006	73.35	19.88	3.26	2.50	1.00	4.32	14.25	61.53	4.000	No	Yes	2.00
1007	73.38	19.20	3.29	2.56	1.00	4.13	14.83	61.23	4.000	No	Yes	2.00
1008	73.47	20.02	3.25	2.39	1.00	4.35	13.95	60.67	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1009	73.53	20.08	3.24	2.33	1.00	4.37	13.79	60.20	4.000	No	Yes	2.00
1010	73.62	20.18	3.24	2.30	1.00	4.39	13.66	59.95	4.000	No	Yes	2.00
1011	73.71	19.95	3.25	2.36	1.00	4.32	13.95	60.28	4.000	No	Yes	2.00
1012	73.77	19.61	3.28	2.54	1.00	4.23	14.55	61.46	4.000	No	Yes	2.00
1013	73.86	19.34	3.30	2.76	1.00	4.15	15.21	63.08	4.000	No	Yes	2.00
1014	73.96	19.38	3.31	2.94	1.00	4.15	15.56	64.61	4.000	No	Yes	2.00
1015	74.06	19.58	3.32	3.02	1.00	4.20	15.60	65.59	4.000	No	Yes	2.00
1016	74.13	20.02	3.31	3.02	1.00	4.32	15.32	66.22	4.000	No	Yes	2.00
1017	74.24	20.36	3.30	3.02	1.00	4.41	15.12	66.66	4.000	No	Yes	2.00
1018	74.34	20.56	3.30	3.06	1.00	4.46	15.08	67.26	4.000	No	Yes	2.00
1019	74.44	20.42	3.31	3.15	1.00	4.42	15.35	67.81	4.000	No	Yes	2.00
1020	74.58	20.37	3.30	3.10	1.00	4.40	15.30	67.28	4.000	No	Yes	2.00
1021	74.68	20.30	3.27	2.60	1.00	4.38	14.35	62.80	4.000	No	Yes	2.00
1022	74.80	20.47	3.22	2.16	1.00	4.42	13.30	58.74	4.000	No	Yes	2.00
1023	74.92	20.26	3.21	1.96	1.00	4.35	12.97	56.43	4.000	No	Yes	2.00
1024	75.07	20.06	3.24	2.18	1.00	4.29	13.60	58.35	4.000	No	Yes	2.00
1025	75.08	19.75	3.26	2.32	1.00	4.21	14.10	59.34	4.000	No	Yes	2.00
1026	75.11	19.62	3.26	2.36	1.00	4.17	14.28	59.53	4.000	No	Yes	2.00
1027	75.16	19.55	3.27	2.45	1.00	4.15	14.53	60.28	4.000	No	Yes	2.00
1028	75.25	19.31	3.30	2.65	1.00	4.08	15.14	61.74	4.000	No	Yes	2.00
1029	75.32	19.14	3.32	2.86	1.00	4.03	15.69	63.23	4.000	No	Yes	2.00
1030	75.40	18.98	3.33	2.95	1.00	3.98	16.00	63.73	4.000	No	Yes	2.00
1031	75.50	18.81	3.33	2.87	1.00	3.93	15.96	62.77	4.000	No	Yes	2.00
1032	75.59	18.30	3.33	2.72	1.00	3.79	16.02	60.75	4.000	No	Yes	2.00
1033	75.69	17.56	3.34	2.60	1.00	3.59	16.34	58.60	4.000	No	Yes	2.00
1034	75.78	16.85	3.35	2.48	1.00	3.39	16.66	56.46	4.000	No	Yes	2.00
1035	75.88	16.41	3.36	2.34	1.00	3.27	16.73	54.66	4.000	No	Yes	2.00
1036	75.96	16.11	3.35	2.19	1.00	3.18	16.62	52.90	4.000	No	Yes	2.00
1037	76.05	16.04	3.34	2.06	1.00	3.16	16.34	51.65	4.000	No	Yes	2.00
1038	76.14	15.97	3.34	1.99	1.00	3.14	16.25	51.00	4.000	No	Yes	2.00
1039	76.26	16.07	3.34	1.99	1.00	3.16	16.16	51.09	4.000	No	Yes	2.00
1040	76.36	16.07	3.34	2.03	1.00	3.16	16.26	51.38	4.000	No	Yes	2.00
1041	76.41	16.07	3.34	2.04	1.00	3.16	16.31	51.50	4.000	No	Yes	2.00
1042	76.51	15.84	3.35	2.05	1.00	3.09	16.56	51.17	4.000	No	Yes	2.00
1043	76.65	15.50	3.37	2.09	1.00	2.99	17.04	51.04	4.000	No	Yes	2.00
1044	76.72	15.26	3.38	2.15	1.00	2.93	17.45	51.12	4.000	No	Yes	2.00
1045	76.79	15.16	3.39	2.21	1.00	2.90	17.72	51.39	4.000	No	Yes	2.00
1046	76.89	15.23	3.41	2.47	1.00	2.91	18.36	53.53	4.000	No	Yes	2.00
1047	76.98	15.47	3.48	3.62	1.00	2.98	20.80	61.89	4.000	No	Yes	2.00
1048	77.08	18.00	3.43	4.02	1.00	3.65	19.05	69.60	4.000	No	Yes	2.00
1049	77.18	22.18	3.34	4.06	1.00	4.77	16.19	77.29	4.000	No	Yes	2.00
1050	77.28	26.73	3.26	4.08	1.00	5.99	14.06	84.26	4.000	No	Yes	2.00
1051	77.37	27.88	3.29	4.98	1.00	6.30	14.87	93.62	4.000	No	Yes	2.00
1052	77.42	28.76	3.31	5.68	1.00	6.53	15.41	100.64	4.000	No	Yes	2.00
1053	77.42	30.22	3.30	5.86	1.00	6.92	15.09	104.44	4.000	No	Yes	2.00
1054	77.44	34.00	3.23	5.50	1.00	7.94	13.49	107.05	4.000	No	Yes	2.00
1055	77.48	37.40	3.19	5.36	1.00	8.85	12.47	110.31	4.000	No	Yes	2.00
1056	77.52	40.61	3.15	5.24	1.00	9.70	11.65	113.00	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1057	77.54	42.94	3.12	5.12	1.00	10.33	11.08	114.44	4.000	No	Yes	2.00
1058	77.57	43.37	3.12	5.18	1.00	10.44	11.07	115.54	4.000	No	Yes	2.00
1059	77.62	42.26	3.14	5.33	1.00	10.14	11.44	115.93	4.000	No	Yes	2.00
1060	77.65	40.10	3.17	5.56	1.00	9.55	12.10	115.64	4.000	No	Yes	2.00
1061	77.67	38.72	3.18	5.50	1.00	9.18	12.34	113.32	4.000	No	Yes	2.00
1062	77.71	37.91	3.19	5.40	1.00	8.96	12.41	111.24	4.000	No	Yes	2.00
1063	77.71	37.03	3.18	5.16	1.00	8.73	12.35	107.78	4.000	No	Yes	2.00
1064	77.76	34.77	3.20	5.10	1.00	8.12	12.85	104.25	4.000	No	Yes	2.00
1065	77.81	31.76	3.23	4.96	1.00	7.31	13.53	98.88	4.000	No	Yes	2.00
1066	77.90	29.03	3.27	4.92	1.00	6.57	14.40	94.60	4.000	No	Yes	2.00
1067	77.95	27.32	3.30	4.97	1.00	6.11	15.14	92.44	4.000	No	Yes	2.00
1068	78.01	26.34	3.32	5.03	1.00	5.84	15.63	91.29	4.000	No	Yes	2.00
1069	78.10	27.59	3.27	4.56	1.00	6.17	14.49	89.37	4.000	No	Yes	2.00
1070	78.16	36.29	3.07	3.14	1.00	8.49	9.98	84.71	4.000	No	Yes	2.00
1071	78.24	48.94	2.86	2.21	1.00	11.86	6.66	79.05	4.000	Yes	Yes	2.00
1072	78.29	64.83	2.68	1.67	1.00	16.10	4.54	73.14	4.000	Yes	Yes	2.00
1073	78.39	77.42	2.58	1.42	1.00	19.44	3.56	69.27	4.000	Yes	No	2.00
1074	78.47	87.30	2.52	1.35	1.00	22.06	3.11	68.51	4.000	Yes	No	2.00
1075	78.53	92.74	2.51	1.44	1.00	23.49	3.05	71.72	4.000	Yes	No	2.00
1076	78.62	94.25	2.54	1.65	1.00	23.88	3.25	77.71	4.000	Yes	No	2.00
1077	78.68	91.22	2.59	1.91	1.00	23.06	3.64	84.02	4.000	Yes	No	2.00
1078	78.69	92.97	2.61	2.12	1.00	23.52	3.81	89.57	4.000	Yes	Yes	2.00
1079	78.78	93.95	2.63	2.33	1.00	23.76	4.00	95.10	4.000	No	Yes	2.00
1080	78.81	94.86	2.65	2.61	1.00	24.00	4.25	102.04	4.000	No	Yes	2.00
1081	78.92	85.28	2.73	2.97	1.00	21.43	5.01	107.35	4.000	No	Yes	2.00
1082	79.03	72.83	2.81	3.21	1.00	18.11	5.93	107.43	4.000	No	Yes	2.00
1083	79.16	68.41	2.80	2.88	1.00	16.91	5.87	99.26	4.000	Yes	Yes	2.00
1084	79.26	78.39	2.68	2.21	1.00	19.54	4.53	88.45	4.000	Yes	Yes	2.00
1085	79.35	97.35	2.56	1.87	1.00	24.54	3.42	83.92	4.000	Yes	No	2.00
1086	79.45	114.43	2.50	1.84	1.00	29.03	2.95	85.78	4.000	Yes	No	2.00
1087	79.54	124.25	2.48	1.92	1.00	31.60	2.84	89.58	4.000	No	No	2.00
1088	79.64	131.23	2.47	1.97	1.00	33.41	2.75	91.91	4.000	No	No	2.00
1089	79.74	153.43	2.40	1.91	1.00	39.23	2.39	93.85	4.000	No	No	2.00
1090	79.88	186.93	2.31	1.77	1.00	48.00	1.98	94.86	4.000	No	No	2.00
1091	79.98	228.94	2.20	1.52	1.00	59.00	1.62	95.73	4.000	No	No	2.00
1092	80.12	248.77	2.14	1.34	1.00	64.13	1.48	95.14	4.000	No	No	2.00
1093	80.22	253.19	2.09	1.12	1.00	65.23	1.40	91.22	4.000	No	No	2.00
1094	80.36	244.79	2.06	0.97	1.00	62.94	1.37	86.07	4.000	No	No	2.00
1095	80.46	238.82	2.02	0.78	1.00	61.33	1.32	81.11	4.000	No	No	2.00
1096	80.60	231.84	1.99	0.66	1.00	59.42	1.30	77.21	4.000	No	No	2.00
1097	80.70	223.91	1.99	0.62	1.00	57.30	1.30	74.37	4.000	No	No	2.00
1098	80.83	213.12	2.02	0.65	1.00	54.42	1.32	72.04	4.000	Yes	No	2.00
1099	80.94	194.49	2.09	0.77	1.00	49.51	1.41	69.62	4.000	Yes	No	2.00
1100	81.01	177.96	2.15	0.85	1.00	45.17	1.50	67.91	4.000	Yes	No	2.00
1101	81.04	164.23	2.19	0.91	1.00	41.58	1.60	66.50	4.000	Yes	No	2.00
1102	81.09	158.43	2.21	0.93	1.00	40.05	1.65	65.97	4.000	Yes	No	2.00
1103	81.13	149.59	2.25	0.99	1.00	37.74	1.75	66.04	4.000	Yes	No	2.00
1104	81.18	136.87	2.31	1.12	1.00	34.41	1.98	67.98	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1105	81.23	123.31	2.39	1.33	1.00	30.87	2.34	72.13	4.000	Yes	No	2.00
1106	81.28	109.41	2.48	1.58	1.00	27.24	2.85	77.64	4.000	Yes	No	2.00
1107	81.33	98.17	2.57	1.89	1.00	24.30	3.46	84.19	4.000	Yes	No	2.00
1108	81.37	88.49	2.65	2.30	1.00	21.78	4.25	92.48	4.000	Yes	Yes	2.00
1109	81.42	81.24	2.73	2.74	1.00	19.88	5.05	100.46	4.000	Yes	Yes	2.00
1110	81.47	75.77	2.79	3.12	1.00	18.46	5.75	106.15	4.000	Yes	Yes	2.00
1111	81.52	71.99	2.83	3.36	1.00	17.47	6.25	109.13	4.000	Yes	Yes	2.00
1112	81.56	70.98	2.85	3.50	1.00	17.20	6.46	111.09	4.000	Yes	Yes	2.00
1113	81.61	70.58	2.86	3.61	1.00	17.08	6.60	112.75	4.000	No	Yes	2.00
1114	81.64	68.79	2.88	3.76	1.00	16.62	6.89	114.41	4.000	No	Yes	2.00
1115	81.70	62.18	2.94	4.16	1.00	14.89	7.85	116.91	4.000	No	Yes	2.00
1116	81.75	54.38	3.03	4.72	1.00	12.87	9.25	118.94	4.000	No	Yes	2.00
1117	81.79	46.89	3.11	5.33	1.00	10.92	10.91	119.14	4.000	No	Yes	2.00
1118	81.82	41.90	3.17	5.62	1.00	9.62	12.12	116.62	4.000	No	Yes	2.00
1119	81.86	37.62	3.22	5.76	1.00	8.51	13.21	112.49	4.000	No	Yes	2.00
1120	81.91	34.01	3.26	5.79	1.00	7.57	14.21	107.66	4.000	No	Yes	2.00
1121	81.95	30.63	3.30	5.75	1.00	6.70	15.27	102.27	4.000	No	Yes	2.00
1122	82.00	27.33	3.34	5.61	1.00	5.84	16.41	95.81	4.000	No	Yes	2.00
1123	82.09	24.26	3.39	5.48	1.00	5.04	17.74	89.46	4.000	No	Yes	2.00
1124	82.15	21.66	3.44	5.50	1.00	4.37	19.38	84.64	4.000	No	Yes	2.00
1125	82.19	19.83	3.48	5.52	1.00	3.89	20.80	81.03	4.000	No	Yes	2.00
1126	82.26	18.38	3.52	5.48	1.00	3.52	22.06	77.56	4.000	No	Yes	2.00
1127	82.34	17.00	3.56	5.45	1.00	3.16	23.49	74.17	4.000	No	Yes	2.00
1128	82.39	15.65	3.61	5.65	1.00	2.81	25.58	71.81	4.000	No	Yes	2.00
1129	82.48	14.77	3.64	5.76	1.00	2.58	27.14	69.97	4.000	No	Yes	2.00
1130	82.58	14.64	3.64	5.47	1.00	2.54	26.84	68.21	4.000	No	Yes	2.00
1131	82.62	14.74	3.62	5.09	1.00	2.57	25.95	66.60	4.000	No	Yes	2.00
1132	82.70	14.88	3.60	4.83	1.00	2.60	25.23	65.56	4.000	No	Yes	2.00
1133	82.77	14.81	3.59	4.65	1.00	2.58	24.98	64.46	4.000	No	Yes	2.00
1134	82.87	15.08	3.57	4.45	1.00	2.65	24.19	64.01	4.000	No	Yes	2.00
1135	82.96	16.23	3.51	3.90	1.00	2.94	21.57	63.38	4.000	No	Yes	2.00
1136	83.06	18.22	3.41	3.33	1.00	3.45	18.38	63.34	4.000	No	Yes	2.00
1137	83.16	21.39	3.29	2.70	1.00	4.26	14.82	63.10	4.000	No	Yes	2.00
1138	83.25	24.46	3.19	2.32	1.00	5.04	12.49	62.94	4.000	No	Yes	2.00
1139	83.34	27.20	3.11	2.06	1.00	5.74	10.91	62.57	4.000	No	Yes	2.00
1140	83.44	28.34	3.10	2.06	1.00	6.03	10.55	63.55	4.000	No	Yes	2.00
1141	83.54	28.75	3.10	2.14	1.00	6.12	10.60	64.89	4.000	No	Yes	2.00
1142	83.64	28.61	3.12	2.29	1.00	6.08	10.93	66.49	4.000	No	Yes	2.00
1143	83.73	27.70	3.15	2.52	1.00	5.84	11.68	68.29	4.000	No	Yes	2.00
1144	83.83	27.26	3.18	2.77	1.00	5.73	12.30	70.46	4.000	No	Yes	2.00
1145	83.85	26.83	3.21	3.11	1.00	5.62	13.07	73.38	4.000	No	Yes	2.00
1146	83.89	27.47	3.22	3.29	1.00	5.78	13.14	75.93	4.000	No	Yes	2.00
1147	83.94	28.11	3.24	3.78	1.00	5.94	13.69	81.26	4.000	No	Yes	2.00
1148	84.04	29.26	3.25	4.14	1.00	6.23	13.80	85.92	4.000	No	Yes	2.00
1149	84.09	30.40	3.25	4.44	1.00	6.51	13.83	90.10	4.000	No	Yes	2.00
1150	84.13	31.28	3.24	4.51	1.00	6.74	13.65	91.94	4.000	No	Yes	2.00
1151	84.18	31.68	3.24	4.64	1.00	6.83	13.70	93.61	4.000	No	Yes	2.00
1152	84.25	31.52	3.25	4.81	1.00	6.79	13.97	94.85	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1153	84.33	30.64	3.28	5.04	1.00	6.56	14.57	95.60	4.000	No	Yes	2.00
1154	84.37	29.46	3.31	5.29	1.00	6.26	15.33	95.90	4.000	No	Yes	2.00
1155	84.46	28.35	3.33	5.40	1.00	5.97	15.91	94.98	4.000	No	Yes	2.00
1156	84.52	27.50	3.34	5.37	1.00	5.75	16.25	93.43	4.000	No	Yes	2.00
1157	84.57	26.90	3.34	5.22	1.00	5.59	16.32	91.27	4.000	No	Yes	2.00
1158	84.67	26.52	3.34	5.14	1.00	5.49	16.38	90.00	4.000	No	Yes	2.00
1159	84.71	26.15	3.35	5.18	1.00	5.40	16.62	89.72	4.000	No	Yes	2.00
1160	84.81	25.58	3.38	5.48	1.00	5.25	17.32	90.86	4.000	No	Yes	2.00
1161	84.86	24.84	3.41	5.93	1.00	5.06	18.32	92.62	4.000	No	Yes	2.00
1162	84.91	24.06	3.44	6.37	1.00	4.86	19.36	94.03	4.000	No	Yes	2.00
1163	85.00	23.42	3.47	6.69	1.00	4.69	20.18	94.63	4.000	No	Yes	2.00
1164	85.05	22.81	3.48	6.79	1.00	4.53	20.72	93.94	4.000	No	Yes	2.00
1165	85.15	22.34	3.49	6.69	1.00	4.41	20.94	92.30	4.000	No	Yes	2.00
1166	85.19	21.80	3.49	6.36	1.00	4.27	20.88	89.13	4.000	No	Yes	2.00
1167	85.29	21.33	3.48	6.00	1.00	4.15	20.74	85.98	4.000	No	Yes	2.00
1168	85.35	20.72	3.49	5.75	1.00	3.99	20.84	83.14	4.000	No	Yes	2.00
1169	85.42	20.08	3.50	5.71	1.00	3.82	21.32	81.54	4.000	No	Yes	2.00
1170	85.48	19.40	3.52	5.78	1.00	3.65	22.03	80.45	4.000	No	Yes	2.00
1171	85.55	18.77	3.54	5.87	1.00	3.49	22.80	79.50	4.000	No	Yes	2.00
1172	85.63	18.19	3.56	5.98	1.00	3.34	23.58	78.76	4.000	No	Yes	2.00
1173	85.68	17.62	3.58	6.16	1.00	3.19	24.50	78.25	4.000	No	Yes	2.00
1174	85.77	17.18	3.60	6.34	1.00	3.08	25.34	78.03	4.000	No	Yes	2.00
1175	85.82	17.04	3.61	6.47	1.00	3.04	25.74	78.34	4.000	No	Yes	2.00
1176	85.89	17.42	3.60	6.38	1.00	3.13	25.13	78.79	4.000	No	Yes	2.00
1177	85.96	18.33	3.56	5.99	1.00	3.36	23.51	79.01	4.000	No	Yes	2.00
1178	86.03	19.71	3.49	5.35	1.00	3.71	21.16	78.44	4.000	No	Yes	2.00
1179	86.11	21.06	3.44	4.76	1.00	4.04	19.14	77.40	4.000	No	Yes	2.00
1180	86.16	22.11	3.39	4.32	1.00	4.30	17.71	76.21	4.000	No	Yes	2.00
1181	86.25	21.67	3.40	4.38	1.00	4.19	18.09	75.81	4.000	No	Yes	2.00
1182	86.36	19.98	3.45	4.62	1.00	3.76	19.76	74.32	4.000	No	Yes	2.00
1183	86.50	18.16	3.52	4.99	1.00	3.30	22.08	72.85	4.000	No	Yes	2.00
1184	86.51	17.25	3.55	5.00	1.00	3.07	23.09	70.91	4.000	No	Yes	2.00
1185	86.52	17.32	3.53	4.74	1.00	3.09	22.53	69.58	4.000	No	Yes	2.00
1186	86.57	17.35	3.51	4.25	1.00	3.10	21.58	66.80	4.000	No	Yes	2.00
1187	86.65	17.39	3.48	3.72	1.00	3.10	20.48	63.50	4.000	No	Yes	2.00
1188	86.71	17.35	3.45	3.31	1.00	3.09	19.65	60.73	4.000	No	Yes	2.00
1189	86.80	17.08	3.45	3.15	1.00	3.02	19.57	59.11	4.000	No	Yes	2.00
1190	86.90	16.48	3.46	3.06	1.00	2.87	20.04	57.42	4.000	No	Yes	2.00
1191	86.99	15.77	3.48	3.01	1.00	2.69	20.75	55.74	4.000	No	Yes	2.00
1192	87.04	15.26	3.50	2.94	1.00	2.56	21.24	54.32	4.000	No	Yes	2.00
1193	87.14	15.16	3.49	2.85	1.00	2.53	21.16	53.51	4.000	No	Yes	2.00
1194	87.19	15.36	3.48	2.77	1.00	2.58	20.70	53.36	4.000	No	Yes	2.00
1195	87.28	15.87	3.46	2.79	1.00	2.70	20.13	54.40	4.000	No	Yes	2.00
1196	87.38	16.51	3.45	2.81	1.00	2.86	19.47	55.67	4.000	No	Yes	2.00
1197	87.43	17.18	3.42	2.82	1.00	3.03	18.79	56.85	4.000	No	Yes	2.00
1198	87.52	17.76	3.40	2.76	1.00	3.17	18.12	57.36	4.000	No	Yes	2.00
1199	87.61	18.23	3.38	2.70	1.00	3.28	17.55	57.58	4.000	No	Yes	2.00
1200	87.66	18.53	3.37	2.63	1.00	3.35	17.13	57.47	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1201	87.76	18.57	3.37	2.58	1.00	3.36	17.00	57.12	4.000	No	Yes	2.00
1202	87.84	18.43	3.37	2.54	1.00	3.32	17.02	56.58	4.000	No	Yes	2.00
1203	87.91	18.13	3.37	2.53	1.00	3.25	17.27	56.08	4.000	No	Yes	2.00
1204	88.00	17.79	3.39	2.53	1.00	3.16	17.58	55.54	4.000	No	Yes	2.00
1205	88.11	17.46	3.40	2.56	1.00	3.07	17.98	55.23	4.000	No	Yes	2.00
1206	88.19	17.22	3.41	2.58	1.00	3.01	18.27	55.01	4.000	No	Yes	2.00
1207	88.25	17.08	3.41	2.59	1.00	2.98	18.42	54.79	4.000	No	Yes	2.00
1208	88.34	17.02	3.41	2.53	1.00	2.96	18.36	54.27	4.000	No	Yes	2.00
1209	88.44	16.98	3.41	2.45	1.00	2.94	18.20	53.59	4.000	No	Yes	2.00
1210	88.54	16.98	3.40	2.37	1.00	2.94	17.99	52.93	4.000	No	Yes	2.00
1211	88.64	16.95	3.40	2.33	1.00	2.93	17.92	52.52	4.000	No	Yes	2.00
1212	88.72	16.88	3.40	2.33	1.00	2.91	18.00	52.42	4.000	No	Yes	2.00
1213	88.82	16.82	3.40	2.36	1.00	2.89	18.16	52.53	4.000	No	Yes	2.00
1214	88.91	16.72	3.41	2.41	1.00	2.87	18.42	52.79	4.000	No	Yes	2.00
1215	89.01	16.62	3.42	2.47	1.00	2.84	18.68	53.02	4.000	No	Yes	2.00
1216	89.10	16.49	3.43	2.53	1.00	2.80	18.99	53.22	4.000	No	Yes	2.00
1217	89.19	16.32	3.44	2.53	1.00	2.76	19.19	52.91	4.000	No	Yes	2.00
1218	89.30	16.21	3.41	2.22	1.00	2.73	18.48	50.44	4.000	No	Yes	2.00
1219	89.39	16.31	3.39	2.02	1.00	2.75	17.80	48.98	4.000	No	Yes	2.00
1220	89.49	16.62	3.38	2.03	1.00	2.82	17.53	49.49	4.000	No	Yes	2.00
1221	89.59	16.90	3.41	2.39	1.00	2.89	18.25	52.76	4.000	No	Yes	2.00
1222	89.69	17.04	3.42	2.65	1.00	2.92	18.79	54.90	4.000	No	Yes	2.00
1223	89.73	17.68	3.40	2.64	1.00	3.08	18.14	55.86	4.000	No	Yes	2.00
1224	89.78	18.48	3.37	2.53	1.00	3.27	17.18	56.23	4.000	No	Yes	2.00
1225	89.83	19.36	3.34	2.42	1.00	3.49	16.22	56.56	4.000	No	Yes	2.00
1226	89.88	19.63	3.33	2.44	1.00	3.55	16.06	57.05	4.000	No	Yes	2.00
1227	89.93	19.86	3.33	2.48	1.00	3.61	16.01	57.77	4.000	No	Yes	2.00
1228	90.00	20.24	3.33	2.55	1.00	3.70	15.90	58.79	4.000	No	Yes	2.00
1229	90.07	20.88	3.31	2.57	1.00	3.85	15.53	59.82	4.000	No	Yes	2.00
1230	90.12	21.62	3.30	2.62	1.00	4.03	15.19	61.24	4.000	No	Yes	2.00
1231	90.22	22.26	3.29	2.71	1.00	4.19	15.01	62.84	4.000	No	Yes	2.00
1232	90.27	23.04	3.29	2.93	1.00	4.37	15.02	65.70	4.000	No	Yes	2.00
1233	90.36	24.99	3.26	2.95	1.00	4.85	14.09	68.34	4.000	No	Yes	2.00
1234	90.46	27.46	3.21	2.86	1.00	5.45	12.89	70.27	4.000	No	Yes	2.00
1235	90.50	29.28	3.17	2.76	1.00	5.89	12.05	71.01	4.000	No	Yes	2.00
1236	90.61	29.48	3.17	2.77	1.00	5.94	12.02	71.39	4.000	No	Yes	2.00
1237	90.66	28.70	3.18	2.82	1.00	5.75	12.38	71.12	4.000	No	Yes	2.00
1238	90.75	27.62	3.20	2.80	1.00	5.48	12.73	69.74	4.000	No	Yes	2.00
1239	90.84	26.17	3.22	2.78	1.00	5.12	13.28	67.94	4.000	No	Yes	2.00
1240	90.89	24.72	3.25	2.77	1.00	4.76	13.90	66.20	4.000	No	Yes	2.00
1241	90.99	23.48	3.28	2.82	1.00	4.45	14.63	65.12	4.000	No	Yes	2.00
1242	91.04	22.50	3.30	2.86	1.00	4.21	15.24	64.21	4.000	No	Yes	2.00
1243	91.14	21.59	3.33	2.94	1.00	3.99	15.98	63.69	4.000	No	Yes	2.00
1244	91.22	20.75	3.36	3.03	1.00	3.78	16.73	63.19	4.000	No	Yes	2.00
1245	91.28	19.83	3.39	3.13	1.00	3.55	17.61	62.55	4.000	No	Yes	2.00
1246	91.37	19.26	3.40	3.14	1.00	3.41	18.11	61.75	4.000	No	Yes	2.00
1247	91.47	18.99	3.40	3.07	1.00	3.34	18.18	60.75	4.000	No	Yes	2.00
1248	91.61	19.26	3.39	2.94	1.00	3.40	17.69	60.19	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1249	91.71	19.40	3.38	2.89	1.00	3.43	17.48	59.97	4.000	No	Yes	2.00
1250	91.81	19.50	3.38	2.88	1.00	3.45	17.39	60.03	4.000	No	Yes	2.00
1251	91.87	19.36	3.38	2.86	1.00	3.42	17.46	59.68	4.000	No	Yes	2.00
1252	92.00	19.38	3.36	2.58	1.00	3.42	16.82	57.50	4.000	No	Yes	2.00
1253	92.10	19.41	3.34	2.37	1.00	3.42	16.30	55.77	4.000	No	Yes	2.00
1254	92.20	19.62	3.32	2.25	1.00	3.47	15.85	54.98	4.000	No	Yes	2.00
1255	92.33	19.76	3.33	2.39	1.00	3.50	16.12	56.37	4.000	No	Yes	2.00
1256	92.38	19.89	3.34	2.50	1.00	3.53	16.27	57.43	4.000	No	Yes	2.00
1257	92.43	20.03	3.34	2.54	1.00	3.56	16.28	57.96	4.000	No	Yes	2.00
1258	92.48	19.98	3.35	2.62	1.00	3.55	16.52	58.57	4.000	No	Yes	2.00
1259	92.56	19.88	3.36	2.71	1.00	3.52	16.79	59.09	4.000	No	Yes	2.00
1260	92.63	19.64	3.37	2.79	1.00	3.46	17.17	59.41	4.000	No	Yes	2.00
1261	92.67	19.57	3.37	2.81	1.00	3.44	17.27	59.42	4.000	No	Yes	2.00
1262	92.72	19.54	3.38	2.81	1.00	3.43	17.30	59.38	4.000	No	Yes	2.00
1263	92.77	19.64	3.37	2.79	1.00	3.46	17.18	59.37	4.000	No	Yes	2.00
1264	92.86	19.84	3.37	2.77	1.00	3.50	16.99	59.49	4.000	No	Yes	2.00
1265	92.92	20.08	3.36	2.78	1.00	3.56	16.84	59.88	4.000	No	Yes	2.00
1266	92.97	20.21	3.37	2.90	1.00	3.59	17.01	61.03	4.000	No	Yes	2.00
1267	93.05	20.35	3.37	3.02	1.00	3.62	17.17	62.12	4.000	No	Yes	2.00
1268	93.10	20.62	3.37	3.09	1.00	3.68	17.13	63.07	4.000	No	Yes	2.00
1269	93.16	21.10	3.35	3.03	1.00	3.79	16.68	63.28	4.000	No	Yes	2.00
1270	93.25	21.70	3.33	2.92	1.00	3.94	16.06	63.20	4.000	No	Yes	2.00
1271	93.35	22.78	3.29	2.71	1.00	4.19	14.99	62.84	4.000	No	Yes	2.00
1272	93.40	23.19	3.27	2.59	1.00	4.29	14.52	62.27	4.000	No	Yes	2.00
1273	93.49	23.25	3.27	2.54	1.00	4.30	14.38	61.82	4.000	No	Yes	2.00
1274	93.56	22.71	3.28	2.58	1.00	4.17	14.77	61.55	4.000	No	Yes	2.00
1275	93.64	22.88	3.28	2.57	1.00	4.21	14.66	61.65	4.000	No	Yes	2.00
1276	93.73	23.63	3.27	2.60	1.00	4.38	14.34	62.81	4.000	No	Yes	2.00
1277	93.83	24.91	3.25	2.65	1.00	4.69	13.81	64.72	4.000	No	Yes	2.00
1278	93.88	26.43	3.23	2.80	1.00	5.05	13.44	67.85	4.000	No	Yes	2.00
1279	93.97	27.01	3.24	3.00	1.00	5.18	13.58	70.35	4.000	No	Yes	2.00
1280	94.07	26.43	3.27	3.36	1.00	5.04	14.48	72.95	4.000	No	Yes	2.00
1281	94.17	25.76	3.31	3.78	1.00	4.87	15.51	75.57	4.000	No	Yes	2.00
1282	94.26	26.70	3.29	3.75	1.00	5.09	15.04	76.60	4.000	No	Yes	2.00
1283	94.36	27.88	3.30	4.18	1.00	5.37	15.22	81.75	4.000	No	Yes	2.00
1284	94.45	29.47	3.30	4.56	1.00	5.75	15.14	87.02	4.000	No	Yes	2.00
1285	94.55	35.88	3.19	4.21	1.00	7.27	12.61	91.74	4.000	No	Yes	2.00
1286	94.64	48.46	3.00	3.11	1.00	10.27	8.71	89.52	4.000	No	Yes	2.00
1287	94.72	59.93	2.85	2.46	1.00	13.01	6.55	85.22	4.000	No	Yes	2.00
1288	94.74	73.87	2.72	1.96	1.00	16.33	4.89	79.85	4.000	No	Yes	2.00
1289	94.77	84.50	2.64	1.75	1.00	18.86	4.08	76.98	4.000	No	Yes	2.00
1290	94.85	97.35	2.56	1.57	1.00	21.92	3.39	74.39	4.000	No	No	2.00
1291	94.90	102.75	2.54	1.57	1.00	23.20	3.24	75.17	4.000	No	No	2.00
1292	94.95	105.32	2.54	1.66	1.00	23.80	3.27	77.89	4.000	No	No	2.00
1293	95.01	104.68	2.58	1.94	1.00	23.63	3.61	85.22	4.000	No	No	2.00
1294	95.09	100.83	2.64	2.34	1.00	22.70	4.16	94.37	4.000	No	Yes	2.00
1295	95.14	94.49	2.73	2.97	1.00	21.18	5.05	107.02	4.000	No	Yes	2.00
1296	95.23	86.42	2.82	3.64	1.00	19.25	6.10	117.34	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1297	95.29	78.06	2.91	4.43	1.00	17.25	7.36	126.89	4.000	No	Yes	2.00
1298	95.38	71.11	2.98	5.04	1.00	15.59	8.45	131.69	4.000	No	Yes	2.00
1299	95.43	67.53	3.02	5.36	1.00	14.73	9.06	133.43	4.000	No	Yes	2.00
1300	95.52	67.83	3.01	5.27	1.00	14.79	8.96	132.50	4.000	No	Yes	2.00
1301	95.57	70.23	2.98	4.89	1.00	15.35	8.40	128.95	4.000	No	Yes	2.00
1302	95.67	71.24	2.95	4.48	1.00	15.58	7.93	123.49	4.000	No	Yes	2.00
1303	95.77	66.52	2.97	4.36	1.00	14.45	8.22	118.72	4.000	No	Yes	2.00
1304	95.86	56.97	3.06	4.90	1.00	12.17	9.76	118.80	4.000	No	Yes	2.00
1305	95.95	52.94	3.09	5.00	1.00	11.21	10.40	116.56	4.000	No	Yes	2.00
1306	96.03	46.73	3.17	5.75	1.00	9.74	12.16	118.40	4.000	No	Yes	2.00
1307	96.11	51.55	3.12	5.30	1.00	10.87	10.92	118.64	4.000	No	Yes	2.00
1308	96.20	59.20	3.06	5.23	1.00	12.66	9.84	124.65	4.000	No	Yes	2.00
1309	96.30	80.15	2.90	4.31	1.00	17.59	7.15	125.73	4.000	Yes	Yes	2.00
1310	96.39	101.37	2.77	3.72	1.00	22.58	5.51	124.50	4.000	Yes	Yes	2.00
1311	96.50	122.96	2.67	3.23	1.00	27.64	4.35	120.31	4.000	Yes	Yes	2.00
1312	96.59	144.96	2.54	2.51	1.00	32.80	3.25	106.72	4.000	Yes	No	2.00
1313	96.69	164.86	2.41	1.87	1.00	37.45	2.44	91.36	4.000	Yes	No	2.00
1314	96.78	180.18	2.29	1.32	1.00	41.02	1.89	77.51	4.000	Yes	No	2.00
1315	96.87	185.95	2.24	1.13	1.00	42.35	1.72	72.98	4.000	Yes	No	2.00
1316	96.98	185.28	2.23	1.08	1.00	42.15	1.69	71.40	4.000	No	No	2.00
1317	97.02	177.79	2.26	1.14	1.00	40.38	1.78	71.90	4.000	No	No	2.00
1318	97.06	176.40	2.27	1.20	1.00	40.04	1.83	73.47	4.000	No	No	2.00
1319	97.12	175.60	2.30	1.30	1.00	39.84	1.91	76.16	4.000	No	No	2.00
1320	97.16	176.98	2.31	1.41	1.00	40.15	1.98	79.48	4.000	No	No	2.00
1321	97.21	173.67	2.35	1.58	1.00	39.35	2.13	83.99	4.000	No	No	2.00
1322	97.27	170.50	2.39	1.77	1.00	38.59	2.31	89.17	4.000	No	No	2.00
1323	97.33	168.21	2.42	1.93	1.00	38.04	2.46	93.67	4.000	No	No	2.00
1324	97.40	165.98	2.44	2.03	1.00	37.49	2.57	96.33	4.000	No	No	2.00
1325	97.45	163.92	2.45	2.09	1.00	37.00	2.64	97.51	4.000	Yes	No	2.00
1326	97.50	161.39	2.47	2.20	1.00	36.39	2.76	100.38	4.000	Yes	No	2.00
1327	97.58	155.82	2.50	2.38	1.00	35.06	2.99	104.78	4.000	Yes	No	2.00
1328	97.65	146.95	2.55	2.64	1.00	32.97	3.34	110.26	4.000	Yes	No	2.00
1329	97.69	134.43	2.60	2.87	1.00	30.04	3.79	113.95	4.000	Yes	Yes	2.00
1330	97.74	121.75	2.66	3.06	1.00	27.07	4.27	115.68	4.000	Yes	Yes	2.00
1331	97.81	110.51	2.71	3.22	1.00	24.44	4.76	116.42	4.000	Yes	Yes	2.00
1332	97.88	103.09	2.74	3.33	1.00	22.69	5.14	116.63	4.000	Yes	Yes	2.00
1333	97.93	108.66	2.70	3.05	1.00	23.98	4.67	111.98	4.000	Yes	Yes	2.00
1334	98.03	138.72	2.52	2.22	1.00	30.95	3.15	97.35	4.000	Yes	No	2.00
1335	98.15	182.62	2.33	1.53	1.00	41.12	2.03	83.50	4.000	Yes	No	2.00
1336	98.21	228.43	2.15	1.06	1.00	51.75	1.51	78.05	4.000	Yes	No	2.00
1337	98.32	264.20	2.03	0.81	1.00	60.00	1.34	80.19	4.000	Yes	No	2.00
1338	98.42	301.85	1.92	0.62	1.00	68.69	1.25	85.96	4.000	Yes	No	2.00
1339	98.47	349.59	1.79	0.45	1.00	79.73	1.00	79.73	4.000	Yes	No	2.00
1340	98.57	388.76	1.69	0.32	1.00	88.75	1.00	88.75	4.000	No	No	2.00
1341	98.70	411.84	1.61	0.24	1.00	94.00	1.00	94.00	4.000	No	No	2.00
1342	98.78	404.01	1.62	0.24	1.00	92.13	1.00	92.13	4.000	No	No	2.00
1343	98.85	372.43	1.67	0.27	1.00	84.79	1.00	84.79	4.000	No	No	2.00
1344	98.86	337.78	1.74	0.31	1.00	76.77	1.00	76.77	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1345	98.92	322.73	1.77	0.33	1.00	73.26	1.00	73.26	4.000	No	No	2.00
1346	98.98	318.48	1.78	0.34	1.00	72.24	1.00	72.24	4.000	Yes	No	2.00
1347	99.03	309.41	1.81	0.38	1.00	70.12	1.00	70.12	4.000	Yes	No	2.00
1348	99.11	281.64	1.90	0.48	1.00	63.67	1.00	63.67	4.000	Yes	No	2.00
1349	99.18	255.32	1.99	0.62	1.00	57.57	1.30	74.69	4.000	Yes	No	2.00
1350	99.23	231.33	2.09	0.83	1.00	52.01	1.41	73.25	4.000	Yes	No	2.00
1351	99.32	209.84	2.20	1.12	1.00	47.02	1.62	76.01	4.000	Yes	No	2.00
1352	99.37	189.39	2.31	1.49	1.00	42.29	1.96	83.05	4.000	Yes	No	2.00
1353	99.45	170.57	2.40	1.81	1.00	37.93	2.37	90.04	4.000	Yes	No	2.00
1354	99.56	157.24	2.47	2.08	1.00	34.83	2.76	96.01	4.000	Yes	No	2.00
1355	99.64	147.39	2.52	2.34	1.00	32.55	3.13	101.90	4.000	Yes	No	2.00
1356	99.71	140.04	2.57	2.64	1.00	30.84	3.53	108.77	4.000	Yes	No	2.00
1357	99.75	128.26	2.63	2.93	1.00	28.12	4.04	113.72	4.000	Yes	Yes	2.00
1358	99.90	116.32	2.70	3.25	1.00	25.35	4.67	118.27	4.000	Yes	Yes	2.00
1359	99.95	101.78	2.79	3.87	1.00	22.01	5.75	126.55	4.000	Yes	Yes	2.00
1360	100.04	116.32	2.73	3.67	1.00	25.32	5.03	127.45	4.000	Yes	Yes	2.00
1361	100.14	159.30	2.55	2.82	1.00	35.14	3.33	116.89	4.000	Yes	No	2.00
1362	100.14	204.99	2.39	2.20	1.00	45.59	2.33	106.43	4.000	Yes	No	2.00
1363	100.15	235.79	2.32	2.02	1.00	52.64	2.00	105.52	4.000	Yes	No	2.00
1364	100.19	258.80	2.30	2.10	1.00	57.89	1.93	111.71	4.000	Yes	No	2.00
1365	100.21	298.07	2.26	2.14	1.00	66.86	1.78	119.29	4.000	Yes	No	2.00
1366	100.24	351.88	2.06	1.31	1.00	79.16	1.37	108.37	4.000	Yes	No	2.00
1367	100.28	410.56	1.80	0.59	1.00	92.54	1.15	106.62	4.000	Yes	No	2.00
1368	100.31	470.98	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1369	100.33	508.57	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1370	100.38	524.63	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1371	100.39	526.55	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1372	100.43	531.78	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1373	100.48	522.24	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1374	100.53	509.38	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1375	100.57	496.12	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1376	100.60	497.27	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_t: Total cone resistance
I_c: Soil behavior type index
Fr: Normalized friction ratio (%)
n: Stress exponent
Q_{tn}: Normalized cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
0.04	2.00	0.00	0.00	0.06	0.00	0.10	2.00	0.00	0.00	0.06	0.00
0.11	2.00	0.00	0.00	0.01	0.00	0.16	2.00	0.00	0.00	0.05	0.00
0.19	2.00	0.00	0.00	0.04	0.00	0.24	2.00	0.00	0.00	0.05	0.00
0.31	2.00	0.00	0.00	0.07	0.00	0.38	2.00	0.00	0.00	0.07	0.00
0.43	2.00	0.00	0.00	0.05	0.00	0.49	2.00	0.00	0.00	0.06	0.00
0.58	2.00	0.00	0.00	0.09	0.00	0.63	2.00	0.00	0.00	0.05	0.00
0.67	2.00	0.00	0.00	0.04	0.00	0.72	2.00	0.00	0.00	0.05	0.00
0.72	2.00	0.00	0.00	0.01	0.00	0.84	2.00	0.00	0.00	0.12	0.00
0.96	2.00	0.00	0.00	0.12	0.00	1.06	2.00	0.00	0.00	0.09	0.00
1.24	2.00	0.00	0.00	0.19	0.00	1.30	2.00	0.00	0.00	0.06	0.00
1.48	2.00	0.00	0.00	0.18	0.00	1.59	2.00	0.00	0.00	0.10	0.00
1.69	2.00	0.00	0.00	0.10	0.00	1.69	2.00	0.00	0.00	0.01	0.00
1.74	2.00	0.00	0.00	0.05	0.00	1.79	2.00	0.00	0.00	0.04	0.00
1.84	2.00	0.00	0.00	0.05	0.00	1.88	2.00	0.00	0.00	0.05	0.00
1.93	2.00	0.00	0.00	0.05	0.00	1.99	2.00	0.00	0.00	0.06	0.00
2.03	2.00	0.00	0.00	0.04	0.00	2.08	2.00	0.00	0.00	0.05	0.00
2.13	2.00	0.00	0.00	0.05	0.00	2.22	2.00	0.00	0.00	0.09	0.00
2.27	2.00	0.00	0.00	0.06	0.00	2.33	2.00	0.00	0.00	0.05	0.00
2.42	2.00	0.00	0.00	0.09	0.00	2.48	2.00	0.00	0.00	0.07	0.00
2.56	2.00	0.00	0.00	0.07	0.00	2.65	2.00	0.00	0.00	0.10	0.00
2.72	2.00	0.00	0.00	0.07	0.00	2.80	2.00	0.00	0.00	0.08	0.00
2.89	2.00	0.00	0.00	0.09	0.00	2.94	2.00	0.00	0.00	0.05	0.00
3.04	2.00	0.00	0.00	0.10	0.00	3.14	2.00	0.00	0.00	0.10	0.00
3.23	2.00	0.00	0.00	0.10	0.00	3.31	2.00	0.00	0.00	0.07	0.00
3.37	2.00	0.00	0.00	0.06	0.00	3.48	2.00	0.00	0.00	0.11	0.00
3.57	2.00	0.00	0.00	0.09	0.00	3.65	2.00	0.00	0.00	0.09	0.00
3.71	2.00	0.00	0.00	0.06	0.00	3.82	2.00	0.00	0.00	0.11	0.00
3.91	2.00	0.00	0.00	0.09	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.09	0.00	4.19	2.00	0.00	0.00	0.10	0.00
4.26	2.00	0.00	0.00	0.07	0.00	4.35	2.00	0.00	0.00	0.09	0.00
4.44	2.00	0.00	0.00	0.10	0.00	4.52	2.00	0.00	0.00	0.08	0.00
4.53	2.00	0.00	0.00	0.01	0.00	4.58	2.00	0.00	0.00	0.05	0.00
4.63	2.00	0.00	0.00	0.05	0.00	4.68	2.00	0.00	0.00	0.05	0.00
4.72	2.00	0.00	0.00	0.04	0.00	4.77	2.00	0.00	0.00	0.05	0.00
4.82	2.00	0.00	0.00	0.05	0.00	4.88	2.00	0.00	0.00	0.06	0.00
4.96	2.00	0.00	0.00	0.08	0.00	5.01	2.00	0.00	0.00	0.05	0.00
5.08	2.00	0.00	0.00	0.07	0.00	5.16	2.00	0.00	0.00	0.08	0.00
5.21	2.00	0.00	0.00	0.05	0.00	5.30	2.00	0.00	0.00	0.09	0.00
5.37	2.00	0.00	0.00	0.07	0.00	5.45	2.00	0.00	0.00	0.08	0.00
5.52	2.00	0.00	0.00	0.07	0.00	5.59	2.00	0.00	0.00	0.07	0.00
5.65	2.00	0.00	0.00	0.06	0.00	5.74	2.00	0.00	0.00	0.08	0.00
5.83	2.00	0.00	0.00	0.09	0.00	5.89	2.00	0.00	0.00	0.06	0.00
5.97	2.00	0.00	0.00	0.08	0.00	6.07	2.00	0.00	0.00	0.09	0.00
6.12	2.00	0.00	0.00	0.05	0.00	6.22	2.00	0.00	0.00	0.10	0.00
6.28	2.00	0.00	0.00	0.06	0.00	6.36	2.00	0.00	0.00	0.08	0.00
6.46	2.00	0.00	0.00	0.10	0.00	6.52	2.00	0.00	0.00	0.06	0.00
6.60	2.00	0.00	0.00	0.09	0.00	6.70	2.00	0.00	0.00	0.09	0.00
6.76	2.00	0.00	0.00	0.07	0.00	6.84	2.00	0.00	0.00	0.08	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
6.94	2.00	0.00	0.00	0.10	0.00	7.03	2.00	0.00	0.00	0.09	0.00
7.13	2.00	0.00	0.00	0.09	0.00	7.19	2.00	0.00	0.00	0.06	0.00
7.32	2.00	0.00	0.00	0.13	0.00	7.42	2.00	0.00	0.00	0.10	0.00
7.49	2.00	0.00	0.00	0.07	0.00	7.57	2.00	0.00	0.00	0.08	0.00
7.66	2.00	0.00	0.00	0.09	0.00	7.76	2.00	0.00	0.00	0.10	0.00
7.77	2.00	0.00	0.00	0.01	0.00	7.78	2.00	0.00	0.00	0.00	0.00
7.82	2.00	0.00	0.00	0.04	0.00	7.87	2.00	0.00	0.00	0.05	0.00
7.92	2.00	0.00	0.00	0.04	0.00	7.97	2.00	0.00	0.00	0.05	0.00
8.01	2.00	0.00	0.00	0.04	0.00	8.06	2.00	0.00	0.00	0.05	0.00
8.11	2.00	0.00	0.00	0.05	0.00	8.20	2.00	0.00	0.00	0.09	0.00
8.26	2.00	0.00	0.00	0.06	0.00	8.35	2.00	0.00	0.00	0.09	0.00
8.40	2.00	0.00	0.00	0.06	0.00	8.49	2.00	0.00	0.00	0.09	0.00
8.54	2.00	0.00	0.00	0.05	0.00	8.64	2.00	0.00	0.00	0.09	0.00
8.69	2.00	0.00	0.00	0.05	0.00	8.79	2.00	0.00	0.00	0.10	0.00
8.84	2.00	0.00	0.00	0.05	0.00	8.93	2.00	0.00	0.00	0.09	0.00
9.03	2.00	0.00	0.00	0.10	0.00	9.08	2.00	0.00	0.00	0.06	0.00
9.11	2.00	0.00	0.00	0.02	0.00	9.12	2.00	0.00	0.00	0.01	0.00
9.17	2.00	0.00	0.00	0.05	0.00	9.22	2.00	0.00	0.00	0.05	0.00
9.31	2.00	0.00	0.00	0.10	0.00	9.36	2.00	0.00	0.00	0.05	0.00
9.40	2.00	0.00	0.00	0.03	0.00	9.46	2.00	0.00	0.00	0.06	0.00
9.51	2.00	0.00	0.00	0.05	0.00	9.55	2.00	0.00	0.00	0.04	0.00
9.61	2.00	0.00	0.00	0.06	0.00	9.69	2.00	0.00	0.00	0.09	0.00
9.74	2.00	0.00	0.00	0.05	0.00	9.81	2.00	0.00	0.00	0.07	0.00
9.89	2.00	0.00	0.00	0.07	0.00	9.94	2.00	0.00	0.00	0.05	0.00
10.03	2.00	0.00	0.00	0.09	0.00	10.08	2.00	0.00	0.00	0.05	0.00
10.18	2.00	0.00	0.00	0.11	0.00	10.23	2.00	0.00	0.00	0.04	0.00
10.33	2.00	0.00	0.00	0.10	0.00	10.40	2.00	0.00	0.00	0.07	0.00
10.47	2.00	0.00	0.00	0.07	0.00	10.51	2.00	0.00	0.00	0.04	0.00
10.56	2.00	0.00	0.00	0.05	0.00	10.61	2.00	0.00	0.00	0.05	0.00
10.67	2.00	0.00	0.00	0.05	0.00	10.75	2.00	0.00	0.00	0.08	0.00
10.80	2.00	0.00	0.00	0.05	0.00	10.85	2.00	0.00	0.00	0.05	0.00
10.90	2.00	0.00	0.00	0.04	0.00	11.00	2.00	0.00	0.00	0.10	0.00
11.05	2.00	0.00	0.00	0.06	0.00	11.14	2.00	0.00	0.00	0.09	0.00
11.21	2.00	0.00	0.00	0.07	0.00	11.29	2.00	0.00	0.00	0.08	0.00
11.38	2.00	0.00	0.00	0.09	0.00	11.46	2.00	0.00	0.00	0.08	0.00
11.52	2.00	0.00	0.00	0.06	0.00	11.60	2.00	0.00	0.00	0.08	0.00
11.67	2.00	0.00	0.00	0.07	0.00	11.72	2.00	0.00	0.00	0.05	0.00
11.81	2.00	0.00	0.00	0.09	0.00	11.86	2.00	0.00	0.00	0.05	0.00
11.96	2.00	0.00	0.00	0.10	0.00	12.01	2.00	0.00	0.00	0.05	0.00
12.10	2.00	0.00	0.00	0.09	0.00	12.16	2.00	0.00	0.00	0.06	0.00
12.24	2.00	0.00	0.00	0.09	0.00	12.32	2.00	0.00	0.00	0.07	0.00
12.39	2.00	0.00	0.00	0.08	0.00	12.48	2.00	0.00	0.00	0.09	0.00
12.50	2.00	0.00	0.00	0.01	0.00	12.54	2.00	0.00	0.00	0.04	0.00
12.64	2.00	0.00	0.00	0.10	0.00	12.68	2.00	0.00	0.00	0.05	0.00
12.77	2.00	0.00	0.00	0.08	0.00	12.82	2.00	0.00	0.00	0.06	0.00
12.89	2.00	0.00	0.00	0.07	0.00	12.97	2.00	0.00	0.00	0.08	0.00
13.03	2.00	0.00	0.00	0.06	0.00	13.12	2.00	0.00	0.00	0.09	0.00
13.16	2.00	0.00	0.00	0.05	0.00	13.26	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
13.34	2.00	0.00	0.00	0.08	0.00	13.41	2.00	0.00	0.00	0.06	0.00
13.50	2.00	0.00	0.00	0.09	0.00	13.60	2.00	0.00	0.00	0.10	0.00
13.65	2.00	0.00	0.00	0.05	0.00	13.75	2.00	0.00	0.00	0.10	0.00
13.80	2.00	0.00	0.00	0.06	0.00	13.89	2.00	0.00	0.00	0.09	0.00
13.94	2.00	0.00	0.00	0.05	0.00	14.03	2.00	0.00	0.00	0.09	0.00
14.11	2.00	0.00	0.00	0.07	0.00	14.13	2.00	0.00	0.00	0.02	0.00
14.18	2.00	0.00	0.00	0.05	0.00	14.22	2.00	0.00	0.00	0.04	0.00
14.28	2.00	0.00	0.00	0.06	0.00	14.37	2.00	0.00	0.00	0.09	0.00
14.44	2.00	0.00	0.00	0.07	0.00	14.51	2.00	0.00	0.00	0.08	0.00
14.60	2.00	0.00	0.00	0.09	0.00	14.65	2.00	0.00	0.00	0.05	0.00
14.75	2.00	0.00	0.00	0.10	0.00	14.85	2.00	0.00	0.00	0.10	0.00
14.91	2.00	0.00	0.00	0.06	0.00	14.99	2.00	0.00	0.00	0.08	0.00
15.09	2.00	0.00	0.00	0.09	0.00	15.18	2.00	0.00	0.00	0.09	0.00
15.25	2.00	0.00	0.00	0.07	0.00	15.33	2.00	0.00	0.00	0.08	0.00
15.43	2.00	0.00	0.00	0.10	0.00	15.51	2.00	0.00	0.00	0.09	0.00
15.59	2.00	0.00	0.00	0.08	0.00	15.67	2.00	0.00	0.00	0.08	0.00
15.76	2.00	0.00	0.00	0.09	0.00	15.86	2.00	0.00	0.00	0.10	0.00
15.95	2.00	0.00	0.00	0.09	0.00	16.05	2.00	0.00	0.00	0.10	0.00
16.14	2.00	0.00	0.00	0.09	0.00	16.20	2.00	0.00	0.00	0.06	0.00
16.28	2.00	0.00	0.00	0.09	0.00	16.34	2.00	0.00	0.00	0.05	0.00
16.44	2.00	0.00	0.00	0.10	0.00	16.50	2.00	0.00	0.00	0.06	0.00
16.58	2.00	0.00	0.00	0.08	0.00	16.73	2.00	0.00	0.00	0.15	0.00
16.82	2.00	0.00	0.00	0.09	0.00	16.92	2.00	0.00	0.00	0.10	0.00
17.01	2.00	0.00	0.00	0.09	0.00	17.11	2.00	0.00	0.00	0.09	0.00
17.12	2.00	0.00	0.00	0.01	0.00	17.14	2.00	0.00	0.00	0.02	0.00
17.19	2.00	0.00	0.00	0.05	0.00	17.28	2.00	0.00	0.00	0.09	0.00
17.33	2.00	0.00	0.00	0.05	0.00	17.43	2.00	0.00	0.00	0.10	0.00
17.47	2.00	0.00	0.00	0.05	0.00	17.57	2.00	0.00	0.00	0.10	0.00
17.65	2.00	0.00	0.00	0.08	0.00	17.72	2.00	0.00	0.00	0.06	0.00
17.81	2.00	0.00	0.00	0.09	0.00	17.86	2.00	0.00	0.00	0.05	0.00
17.95	2.00	0.00	0.00	0.10	0.00	18.05	2.00	0.00	0.00	0.10	0.00
18.10	2.00	0.00	0.00	0.05	0.00	18.20	2.00	0.00	0.00	0.10	0.00
18.30	2.00	0.00	0.00	0.10	0.00	18.39	2.00	0.00	0.00	0.10	0.00
18.48	2.00	0.00	0.00	0.09	0.00	18.58	2.00	0.00	0.00	0.10	0.00
18.66	2.00	0.00	0.00	0.08	0.00	18.74	2.00	0.00	0.00	0.08	0.00
18.87	2.00	0.00	0.00	0.13	0.00	18.97	2.00	0.00	0.00	0.10	0.00
19.06	2.00	0.00	0.00	0.10	0.00	19.16	2.00	0.00	0.00	0.10	0.00
19.25	2.00	0.00	0.00	0.10	0.00	19.27	2.00	0.00	0.00	0.01	0.00
19.30	2.00	0.00	0.00	0.03	0.00	19.34	2.00	0.00	0.00	0.04	0.00
19.39	2.00	0.00	0.00	0.05	0.00	19.49	2.00	0.00	0.00	0.10	0.00
19.55	2.00	0.00	0.00	0.06	0.00	19.63	2.00	0.00	0.00	0.08	0.00
19.68	2.00	0.00	0.00	0.05	0.00	19.74	2.00	0.00	0.00	0.06	0.00
19.83	2.00	0.00	0.00	0.08	0.00	19.87	2.00	0.00	0.00	0.05	0.00
19.94	2.00	0.00	0.00	0.07	0.00	20.02	2.00	0.00	0.00	0.08	0.00
20.07	2.00	0.00	0.00	0.05	0.00	20.17	2.00	0.00	0.00	0.10	0.00
20.21	2.00	0.00	0.00	0.05	0.00	20.28	2.00	0.00	0.00	0.07	0.00
20.36	2.00	0.00	0.00	0.08	0.00	20.41	2.00	0.00	0.00	0.05	0.00
20.48	2.00	0.00	0.00	0.07	0.00	20.55	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
20.60	2.00	0.00	0.00	0.05	0.00	20.70	2.00	0.00	0.00	0.10	0.00
20.74	2.00	0.00	0.00	0.05	0.00	20.79	2.00	0.00	0.00	0.05	0.00
20.89	2.00	0.00	0.00	0.09	0.00	20.96	2.00	0.00	0.00	0.08	0.00
21.04	2.00	0.00	0.00	0.07	0.00	21.13	2.00	0.00	0.00	0.09	0.00
21.22	2.00	0.00	0.00	0.09	0.00	21.29	2.00	0.00	0.00	0.06	0.00
21.35	2.00	0.00	0.00	0.06	0.00	21.37	2.00	0.00	0.00	0.03	0.00
21.42	2.00	0.00	0.00	0.05	0.00	21.47	2.00	0.00	0.00	0.05	0.00
21.48	2.00	0.00	0.00	0.01	0.00	21.52	2.00	0.00	0.00	0.04	0.00
21.57	2.00	0.00	0.00	0.05	0.00	21.62	2.00	0.00	0.00	0.05	0.00
21.66	2.00	0.00	0.00	0.05	0.00	21.71	2.00	0.00	0.00	0.05	0.00
21.76	2.00	0.00	0.00	0.05	0.00	21.81	2.00	0.00	0.00	0.05	0.00
21.85	2.00	0.00	0.00	0.04	0.00	21.91	2.00	0.00	0.00	0.05	0.00
21.95	2.00	0.00	0.00	0.05	0.00	22.00	2.00	0.00	0.00	0.05	0.00
22.05	2.00	0.00	0.00	0.04	0.00	22.10	2.00	0.00	0.00	0.05	0.00
22.15	2.00	0.00	0.00	0.05	0.00	22.19	2.00	0.00	0.00	0.05	0.00
22.24	2.00	0.00	0.00	0.05	0.00	22.29	2.00	0.00	0.00	0.05	0.00
22.34	2.00	0.00	0.00	0.05	0.00	22.39	2.00	0.00	0.00	0.05	0.00
22.43	2.00	0.00	0.00	0.05	0.00	22.48	2.00	0.00	0.00	0.05	0.00
22.55	2.00	0.00	0.00	0.06	0.00	22.62	2.00	0.00	0.00	0.07	0.00
22.63	2.00	0.00	0.00	0.01	0.00	22.72	2.00	0.00	0.00	0.10	0.00
22.77	2.00	0.00	0.00	0.04	0.00	22.83	2.00	0.00	0.00	0.06	0.00
22.91	2.00	0.00	0.00	0.08	0.00	22.96	2.00	0.00	0.00	0.05	0.00
23.02	2.00	0.00	0.00	0.05	0.00	23.10	2.00	0.00	0.00	0.09	0.00
23.16	2.00	0.00	0.00	0.06	0.00	23.20	2.00	0.00	0.00	0.05	0.00
23.26	2.00	0.00	0.00	0.06	0.00	23.35	2.00	0.00	0.00	0.09	0.00
23.39	2.00	0.00	0.00	0.04	0.00	23.48	2.00	0.00	0.00	0.09	0.00
23.54	2.00	0.00	0.00	0.06	0.00	23.63	2.00	0.00	0.00	0.09	0.00
23.69	2.00	0.00	0.00	0.06	0.00	23.78	2.00	0.00	0.00	0.09	0.00
23.87	2.00	0.00	0.00	0.09	0.00	23.88	2.00	0.00	0.00	0.01	0.00
23.93	2.00	0.00	0.00	0.05	0.00	24.02	2.00	0.00	0.00	0.10	0.00
24.04	2.00	0.00	0.00	0.01	0.00	24.05	2.00	0.00	0.00	0.02	0.00
24.15	2.00	0.00	0.00	0.10	0.00	24.20	2.00	0.00	0.00	0.05	0.00
24.30	2.00	0.00	0.00	0.10	0.00	24.40	2.00	0.00	0.00	0.09	0.00
24.46	2.00	0.00	0.00	0.07	0.00	24.54	2.00	0.00	0.00	0.08	0.00
24.64	2.00	0.00	0.00	0.10	0.00	24.73	2.00	0.00	0.00	0.09	0.00
24.78	2.00	0.00	0.00	0.06	0.00	24.88	2.00	0.00	0.00	0.09	0.00
24.94	2.00	0.00	0.00	0.06	0.00	25.02	2.00	0.00	0.00	0.08	0.00
25.12	2.00	0.00	0.00	0.10	0.00	25.17	2.00	0.00	0.00	0.05	0.00
25.27	2.00	0.00	0.00	0.10	0.00	25.36	2.00	0.00	0.00	0.09	0.00
25.43	2.00	0.00	0.00	0.07	0.00	25.50	2.00	0.00	0.00	0.08	0.00
25.60	2.00	0.00	0.00	0.10	0.00	25.64	2.00	0.00	0.00	0.04	0.00
25.67	2.00	0.00	0.00	0.03	0.00	25.71	2.00	0.00	0.00	0.04	0.00
25.79	2.00	0.00	0.00	0.09	0.00	25.93	2.00	0.00	0.00	0.14	0.00
26.03	2.00	0.00	0.00	0.10	0.00	26.13	2.00	0.00	0.00	0.10	0.00
26.24	2.00	0.00	0.00	0.11	0.00	26.37	2.00	0.00	0.00	0.13	0.00
26.47	2.00	0.00	0.00	0.10	0.00	26.60	2.00	0.00	0.00	0.13	0.00
26.71	2.00	0.00	0.00	0.11	0.00	26.85	2.00	0.00	0.00	0.15	0.00
26.95	2.00	0.00	0.00	0.09	0.00	27.04	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
27.09	2.00	0.00	0.00	0.05	0.00	27.19	2.00	0.00	0.00	0.10	0.00
27.23	2.00	0.00	0.00	0.05	0.00	27.33	2.00	0.00	0.00	0.10	0.00
27.40	2.00	0.00	0.00	0.07	0.00	27.47	2.00	0.00	0.00	0.07	0.00
27.57	2.00	0.00	0.00	0.11	0.00	27.66	2.00	0.00	0.00	0.09	0.00
27.77	2.00	0.00	0.00	0.10	0.00	27.86	2.00	0.00	0.00	0.10	0.00
27.96	2.00	0.00	0.00	0.10	0.00	28.06	2.00	0.00	0.00	0.10	0.00
28.15	2.00	0.00	0.00	0.09	0.00	28.25	2.00	0.00	0.00	0.10	0.00
28.34	2.00	0.00	0.00	0.09	0.00	28.44	2.00	0.00	0.00	0.10	0.00
28.54	2.00	0.00	0.00	0.10	0.00	28.62	2.00	0.00	0.00	0.08	0.00
28.71	2.00	0.00	0.00	0.09	0.00	28.77	2.00	0.00	0.00	0.05	0.00
28.86	2.00	0.00	0.00	0.09	0.00	28.91	2.00	0.00	0.00	0.05	0.00
28.97	2.00	0.00	0.00	0.05	0.00	29.04	2.00	0.00	0.00	0.08	0.00
29.10	2.00	0.00	0.00	0.06	0.00	29.15	2.00	0.00	0.00	0.05	0.00
29.25	2.00	0.00	0.00	0.10	0.00	29.34	2.00	0.00	0.00	0.09	0.00
29.38	2.00	0.00	0.00	0.04	0.00	29.48	2.00	0.00	0.00	0.10	0.00
29.55	2.00	0.00	0.00	0.06	0.00	29.63	2.00	0.00	0.00	0.09	0.00
29.72	2.00	0.00	0.00	0.09	0.00	29.82	2.00	0.00	0.00	0.10	0.00
29.88	2.00	0.00	0.00	0.06	0.00	29.96	2.00	0.00	0.00	0.08	0.00
30.06	2.00	0.00	0.00	0.09	0.00	30.13	2.00	0.00	0.00	0.07	0.00
30.18	0.57	0.00	0.00	0.04	0.03	30.28	0.58	0.00	0.00	0.10	0.07
30.37	0.60	0.00	0.00	0.09	0.06	30.47	0.63	0.00	0.00	0.10	0.06
30.57	0.65	0.00	0.00	0.10	0.06	30.66	0.67	0.00	0.00	0.10	0.05
30.74	0.69	0.00	0.00	0.08	0.04	30.82	0.71	0.00	0.00	0.08	0.04
30.90	0.73	0.00	0.00	0.08	0.04	31.01	0.76	0.00	0.00	0.11	0.04
31.10	0.80	0.00	0.00	0.08	0.03	31.19	0.86	0.00	0.00	0.09	0.02
31.28	0.92	0.00	0.00	0.09	0.01	31.35	0.97	0.00	0.00	0.06	0.00
31.43	1.02	0.00	0.00	0.09	0.00	31.53	1.06	0.00	0.00	0.09	0.00
31.60	0.96	0.00	0.00	0.07	0.00	31.67	0.88	0.00	0.00	0.08	0.01
31.77	0.82	0.00	0.00	0.10	0.03	31.84	0.84	0.00	0.00	0.07	0.02
31.91	0.87	0.00	0.00	0.07	0.01	31.98	0.89	0.00	0.00	0.07	0.01
31.98	0.92	0.00	0.00	0.01	0.00	32.04	0.94	0.00	0.00	0.05	0.00
32.12	2.00	0.00	0.00	0.08	0.00	32.16	2.00	0.00	0.00	0.05	0.00
32.27	2.00	0.00	0.00	0.10	0.00	32.33	2.00	0.00	0.00	0.06	0.00
32.41	2.00	0.00	0.00	0.08	0.00	32.50	2.00	0.00	0.00	0.09	0.00
32.58	2.00	0.00	0.00	0.08	0.00	32.66	2.00	0.00	0.00	0.07	0.00
32.74	2.00	0.00	0.00	0.09	0.00	32.84	2.00	0.00	0.00	0.10	0.00
32.90	2.00	0.00	0.00	0.06	0.00	32.98	2.00	0.00	0.00	0.09	0.00
33.08	2.00	0.00	0.00	0.09	0.00	33.14	2.00	0.00	0.00	0.07	0.00
33.22	2.00	0.00	0.00	0.08	0.00	33.32	2.00	0.00	0.00	0.10	0.00
33.37	2.00	0.00	0.00	0.05	0.00	33.47	2.00	0.00	0.00	0.10	0.00
33.56	2.00	0.00	0.00	0.09	0.00	33.63	2.00	0.00	0.00	0.07	0.00
33.71	2.00	0.00	0.00	0.08	0.00	33.81	2.00	0.00	0.00	0.09	0.00
33.90	2.00	0.00	0.00	0.09	0.00	33.95	2.00	0.00	0.00	0.05	0.00
34.04	2.00	0.00	0.00	0.09	0.00	34.14	2.00	0.00	0.00	0.10	0.00
34.17	2.00	0.00	0.00	0.02	0.00	34.20	2.00	0.00	0.00	0.04	0.00
34.26	2.00	0.00	0.00	0.05	0.00	34.35	2.00	0.00	0.00	0.09	0.00
34.43	2.00	0.00	0.00	0.08	0.00	34.49	2.00	0.00	0.00	0.06	0.00
34.59	2.00	0.00	0.00	0.09	0.00	34.69	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
34.73	2.00	0.00	0.00	0.05	0.00	34.83	2.00	0.00	0.00	0.10	0.00
34.90	2.00	0.00	0.00	0.07	0.00	34.98	2.00	0.00	0.00	0.08	0.00
35.07	2.00	0.00	0.00	0.09	0.00	35.16	2.00	0.00	0.00	0.10	0.00
35.26	2.00	0.00	0.00	0.10	0.00	35.33	2.00	0.00	0.00	0.07	0.00
35.40	2.00	0.00	0.00	0.07	0.00	35.50	2.00	0.00	0.00	0.10	0.00
35.57	2.00	0.00	0.00	0.06	0.00	35.65	2.00	0.00	0.00	0.08	0.00
35.71	2.00	0.00	0.00	0.06	0.00	35.79	2.00	0.00	0.00	0.09	0.00
35.85	2.00	0.00	0.00	0.06	0.00	35.94	2.00	0.00	0.00	0.08	0.00
35.99	2.00	0.00	0.00	0.06	0.00	36.08	2.00	0.00	0.00	0.08	0.00
36.17	2.00	0.00	0.00	0.10	0.00	36.24	2.00	0.00	0.00	0.07	0.00
36.33	2.00	0.00	0.00	0.08	0.00	36.42	2.00	0.00	0.00	0.09	0.00
36.52	2.00	0.00	0.00	0.10	0.00	36.61	2.00	0.00	0.00	0.09	0.00
36.70	2.00	0.00	0.00	0.09	0.00	36.78	2.00	0.00	0.00	0.08	0.00
36.85	2.00	0.00	0.00	0.07	0.00	36.87	2.00	0.00	0.00	0.01	0.00
36.91	2.00	0.00	0.00	0.05	0.00	36.97	2.00	0.00	0.00	0.06	0.00
37.06	2.00	0.00	0.00	0.09	0.00	37.12	2.00	0.00	0.00	0.06	0.00
37.20	2.00	0.00	0.00	0.08	0.00	37.27	2.00	0.00	0.00	0.08	0.00
37.35	2.00	0.00	0.00	0.07	0.00	37.44	2.00	0.00	0.00	0.09	0.00
37.49	2.00	0.00	0.00	0.05	0.00	37.59	2.00	0.00	0.00	0.10	0.00
37.64	2.00	0.00	0.00	0.05	0.00	37.70	2.00	0.00	0.00	0.07	0.00
37.78	2.00	0.00	0.00	0.08	0.00	37.83	2.00	0.00	0.00	0.05	0.00
37.92	2.00	0.00	0.00	0.09	0.00	37.97	2.00	0.00	0.00	0.05	0.00
38.07	1.52	0.00	0.00	0.09	0.00	38.14	1.59	0.00	0.00	0.07	0.00
38.22	1.67	0.00	0.00	0.08	0.00	38.31	1.79	0.00	0.00	0.09	0.00
38.41	1.96	0.00	0.00	0.09	0.00	38.52	2.00	0.00	0.00	0.11	0.00
38.64	2.00	0.00	0.00	0.13	0.00	38.74	2.00	0.00	0.00	0.10	0.00
38.80	2.00	0.00	0.00	0.06	0.00	38.89	2.00	0.00	0.00	0.08	0.00
38.94	2.00	0.00	0.00	0.05	0.00	39.03	2.00	0.00	0.00	0.09	0.00
39.13	2.00	0.00	0.00	0.10	0.00	39.23	2.00	0.00	0.00	0.10	0.00
39.35	2.00	0.00	0.00	0.12	0.00	39.42	2.00	0.00	0.00	0.07	0.00
39.51	1.93	0.00	0.00	0.09	0.00	39.60	1.73	0.00	0.00	0.09	0.00
39.70	1.58	0.00	0.00	0.10	0.00	39.78	1.45	0.00	0.00	0.07	0.00
39.90	1.34	0.00	0.00	0.12	0.00	39.99	1.24	0.00	0.00	0.09	0.00
40.09	2.00	0.00	0.00	0.10	0.00	40.18	2.00	0.00	0.00	0.09	0.00
40.23	2.00	0.00	0.00	0.05	0.00	40.33	2.00	0.00	0.00	0.10	0.00
40.43	2.00	0.00	0.00	0.10	0.00	40.52	2.00	0.00	0.00	0.09	0.00
40.61	2.00	0.00	0.00	0.08	0.00	40.69	2.00	0.00	0.00	0.09	0.00
40.80	2.00	0.00	0.00	0.10	0.00	40.87	2.00	0.00	0.00	0.08	0.00
40.95	2.00	0.00	0.00	0.08	0.00	40.97	2.00	0.00	0.00	0.02	0.00
41.01	2.00	0.00	0.00	0.04	0.00	41.07	2.00	0.00	0.00	0.06	0.00
41.15	2.00	0.00	0.00	0.08	0.00	41.26	0.74	0.00	0.00	0.11	0.03
41.35	0.76	0.00	0.00	0.09	0.02	41.47	0.78	0.00	0.00	0.12	0.03
41.59	0.79	0.00	0.00	0.12	0.03	41.69	0.80	0.00	0.00	0.10	0.02
41.78	0.83	0.00	0.00	0.09	0.02	41.88	2.00	0.00	0.00	0.10	0.00
41.98	2.00	0.00	0.00	0.10	0.00	42.08	2.00	0.00	0.00	0.10	0.00
42.16	2.00	0.00	0.00	0.08	0.00	42.24	2.00	0.00	0.00	0.08	0.00
42.31	2.00	0.00	0.00	0.07	0.00	42.45	0.80	0.00	0.00	0.14	0.03
42.55	0.80	0.00	0.00	0.09	0.02	42.60	0.80	0.00	0.00	0.05	0.01

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
42.70	0.82	0.00	0.00	0.10	0.02	42.81	0.85	0.00	0.00	0.11	0.02
42.89	2.00	0.00	0.00	0.08	0.00	42.98	2.00	0.00	0.00	0.10	0.00
43.08	2.00	0.00	0.00	0.10	0.00	43.17	2.00	0.00	0.00	0.09	0.00
43.27	2.00	0.00	0.00	0.10	0.00	43.37	2.00	0.00	0.00	0.09	0.00
43.50	2.00	0.00	0.00	0.14	0.00	43.61	0.59	0.00	0.00	0.10	0.04
43.74	0.60	0.00	0.00	0.13	0.06	43.79	0.63	0.00	0.00	0.05	0.02
43.86	2.00	0.00	0.00	0.07	0.00	43.94	2.00	0.00	0.00	0.07	0.00
44.00	2.00	0.00	0.00	0.06	0.00	44.08	2.00	0.00	0.00	0.08	0.00
44.17	2.00	0.00	0.00	0.09	0.00	44.27	2.00	0.00	0.00	0.10	0.00
44.42	2.00	0.00	0.00	0.14	0.00	44.52	2.00	0.00	0.00	0.10	0.00
44.61	2.00	0.00	0.00	0.10	0.00	44.71	0.67	0.00	0.00	0.09	0.03
44.85	0.67	0.00	0.00	0.14	0.05	44.95	0.71	0.00	0.00	0.10	0.03
45.09	0.76	0.00	0.00	0.14	0.03	45.19	2.00	0.00	0.00	0.10	0.00
45.33	2.00	0.00	0.00	0.14	0.00	45.42	2.00	0.00	0.00	0.10	0.00
45.57	2.00	0.00	0.00	0.14	0.00	45.68	2.00	0.00	0.00	0.11	0.00
45.81	2.00	0.00	0.00	0.14	0.00	45.92	2.00	0.00	0.00	0.11	0.00
46.05	2.00	0.00	0.00	0.13	0.00	46.16	2.00	0.00	0.00	0.10	0.00
46.17	2.00	0.00	0.00	0.01	0.00	46.23	2.00	0.00	0.00	0.06	0.00
46.29	2.00	0.00	0.00	0.05	0.00	46.34	2.00	0.00	0.00	0.05	0.00
46.42	2.00	0.00	0.00	0.09	0.00	46.48	2.00	0.00	0.00	0.05	0.00
46.52	2.00	0.00	0.00	0.05	0.00	46.60	2.00	0.00	0.00	0.08	0.00
46.67	2.00	0.00	0.00	0.07	0.00	46.74	2.00	0.00	0.00	0.07	0.00
46.82	2.00	0.00	0.00	0.08	0.00	46.88	2.00	0.00	0.00	0.06	0.00
46.96	2.00	0.00	0.00	0.09	0.00	47.06	2.00	0.00	0.00	0.09	0.00
47.15	2.00	0.00	0.00	0.10	0.00	47.24	2.00	0.00	0.00	0.09	0.00
47.35	2.00	0.00	0.00	0.10	0.00	47.49	2.00	0.00	0.00	0.14	0.00
47.58	2.00	0.00	0.00	0.09	0.00	47.73	2.00	0.00	0.00	0.15	0.00
47.83	2.00	0.00	0.00	0.10	0.00	47.87	2.00	0.00	0.00	0.04	0.00
47.89	2.00	0.00	0.00	0.02	0.00	47.94	2.00	0.00	0.00	0.05	0.00
48.02	2.00	0.00	0.00	0.08	0.00	48.07	2.00	0.00	0.00	0.05	0.00
48.12	2.00	0.00	0.00	0.05	0.00	48.18	2.00	0.00	0.00	0.06	0.00
48.26	2.00	0.00	0.00	0.08	0.00	48.31	2.00	0.00	0.00	0.06	0.00
48.38	2.00	0.00	0.00	0.06	0.00	48.46	2.00	0.00	0.00	0.08	0.00
48.52	2.00	0.00	0.00	0.06	0.00	48.60	2.00	0.00	0.00	0.08	0.00
48.68	2.00	0.00	0.00	0.08	0.00	48.74	2.00	0.00	0.00	0.06	0.00
48.82	2.00	0.00	0.00	0.08	0.00	48.89	2.00	0.00	0.00	0.07	0.00
48.99	2.00	0.00	0.00	0.10	0.00	49.05	2.00	0.00	0.00	0.06	0.00
49.12	2.00	0.00	0.00	0.08	0.00	49.18	2.00	0.00	0.00	0.06	0.00
49.27	2.00	0.00	0.00	0.09	0.00	49.32	2.00	0.00	0.00	0.05	0.00
49.42	2.00	0.00	0.00	0.09	0.00	49.48	2.00	0.00	0.00	0.06	0.00
49.56	2.00	0.00	0.00	0.09	0.00	49.66	2.00	0.00	0.00	0.10	0.00
49.76	2.00	0.00	0.00	0.09	0.00	49.85	2.00	0.00	0.00	0.09	0.00
49.99	2.00	0.00	0.00	0.14	0.00	50.09	2.00	0.00	0.00	0.10	0.00
50.21	2.00	0.00	0.00	0.12	0.00	50.24	2.00	0.00	0.00	0.03	0.00
50.29	2.00	0.00	0.00	0.05	0.00	50.38	2.00	0.00	0.00	0.09	0.00
50.47	2.00	0.00	0.00	0.09	0.00	50.52	2.00	0.00	0.00	0.05	0.00
50.62	2.00	0.00	0.00	0.10	0.00	50.66	2.00	0.00	0.00	0.05	0.00
50.76	2.00	0.00	0.00	0.10	0.00	50.83	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
50.91	2.00	0.00	0.00	0.09	0.00	51.00	2.00	0.00	0.00	0.09	0.00
51.06	2.00	0.00	0.00	0.06	0.00	51.15	2.00	0.00	0.00	0.08	0.00
51.24	2.00	0.00	0.00	0.10	0.00	51.31	2.00	0.00	0.00	0.07	0.00
51.39	2.00	0.00	0.00	0.08	0.00	51.48	2.00	0.00	0.00	0.09	0.00
51.58	2.00	0.00	0.00	0.10	0.00	51.68	2.00	0.00	0.00	0.10	0.00
51.77	2.00	0.00	0.00	0.10	0.00	51.90	2.00	0.00	0.00	0.13	0.00
52.01	2.00	0.00	0.00	0.11	0.00	52.11	2.00	0.00	0.00	0.10	0.00
52.26	2.00	0.00	0.00	0.14	0.00	52.30	2.00	0.00	0.00	0.05	0.00
52.33	2.00	0.00	0.00	0.03	0.00	52.35	2.00	0.00	0.00	0.02	0.00
52.40	2.00	0.00	0.00	0.05	0.00	52.45	2.00	0.00	0.00	0.05	0.00
52.50	2.00	0.00	0.00	0.05	0.00	52.55	2.00	0.00	0.00	0.05	0.00
52.60	2.00	0.00	0.00	0.05	0.00	52.65	2.00	0.00	0.00	0.05	0.00
52.71	2.00	0.00	0.00	0.07	0.00	52.77	2.00	0.00	0.00	0.05	0.00
52.82	2.00	0.00	0.00	0.05	0.00	52.88	2.00	0.00	0.00	0.06	0.00
52.93	2.00	0.00	0.00	0.06	0.00	52.98	2.00	0.00	0.00	0.05	0.00
53.03	2.00	0.00	0.00	0.05	0.00	53.08	2.00	0.00	0.00	0.05	0.00
53.12	2.00	0.00	0.00	0.04	0.00	53.17	2.00	0.00	0.00	0.05	0.00
53.23	2.00	0.00	0.00	0.05	0.00	53.28	2.00	0.00	0.00	0.06	0.00
53.37	2.00	0.00	0.00	0.09	0.00	53.42	2.00	0.00	0.00	0.05	0.00
53.46	2.00	0.00	0.00	0.05	0.00	53.53	2.00	0.00	0.00	0.06	0.00
53.61	2.00	0.00	0.00	0.08	0.00	53.62	2.00	0.00	0.00	0.01	0.00
53.65	2.00	0.00	0.00	0.04	0.00	53.67	2.00	0.00	0.00	0.01	0.00
53.70	2.00	0.00	0.00	0.04	0.00	53.74	2.00	0.00	0.00	0.04	0.00
53.76	2.00	0.00	0.00	0.02	0.00	53.80	2.00	0.00	0.00	0.04	0.00
53.84	2.00	0.00	0.00	0.05	0.00	53.90	2.00	0.00	0.00	0.05	0.00
53.91	2.00	0.00	0.00	0.01	0.00	53.95	2.00	0.00	0.00	0.04	0.00
53.96	2.00	0.00	0.00	0.01	0.00	53.98	2.00	0.00	0.00	0.02	0.00
53.99	2.00	0.00	0.00	0.01	0.00	54.01	2.00	0.00	0.00	0.01	0.00
54.02	2.00	0.00	0.00	0.01	0.00	54.03	2.00	0.00	0.00	0.01	0.00
54.04	2.00	0.00	0.00	0.01	0.00	54.05	2.00	0.00	0.00	0.01	0.00
54.09	2.00	0.00	0.00	0.04	0.00	54.10	2.00	0.00	0.00	0.01	0.00
54.13	2.00	0.00	0.00	0.04	0.00	54.14	2.00	0.00	0.00	0.01	0.00
54.19	2.00	0.00	0.00	0.05	0.00	54.19	2.00	0.00	0.00	0.01	0.00
54.24	2.00	0.00	0.00	0.05	0.00	54.29	2.00	0.00	0.00	0.04	0.00
54.33	2.00	0.00	0.00	0.05	0.00	54.38	2.00	0.00	0.00	0.05	0.00
54.39	2.00	0.00	0.00	0.01	0.00	54.43	2.00	0.00	0.00	0.04	0.00
54.48	2.00	0.00	0.00	0.05	0.00	54.52	2.00	0.00	0.00	0.05	0.00
54.58	2.00	0.00	0.00	0.05	0.00	54.62	2.00	0.00	0.00	0.04	0.00
54.65	2.00	0.00	0.00	0.03	0.00	54.67	2.00	0.00	0.00	0.02	0.00
54.71	2.00	0.00	0.00	0.04	0.00	54.77	2.00	0.00	0.00	0.05	0.00
54.81	2.00	0.00	0.00	0.05	0.00	54.85	2.00	0.00	0.00	0.04	0.00
54.86	2.00	0.00	0.00	0.01	0.00	54.87	2.00	0.00	0.00	0.01	0.00
54.91	2.00	0.00	0.00	0.04	0.00	54.96	2.00	0.00	0.00	0.04	0.00
55.00	2.00	0.00	0.00	0.04	0.00	55.01	2.00	0.00	0.00	0.01	0.00
55.05	2.00	0.00	0.00	0.05	0.00	55.10	2.00	0.00	0.00	0.05	0.00
55.12	2.00	0.00	0.00	0.01	0.00	55.13	2.00	0.00	0.00	0.02	0.00
55.14	2.00	0.00	0.00	0.01	0.00	55.19	2.00	0.00	0.00	0.05	0.00
55.20	2.00	0.00	0.00	0.01	0.00	55.25	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
55.29	2.00	0.00	0.00	0.04	0.00	55.33	2.00	0.00	0.00	0.04	0.00
55.38	2.00	0.00	0.00	0.05	0.00	55.48	2.00	0.00	0.00	0.10	0.00
55.57	2.00	0.00	0.00	0.09	0.00	55.63	2.00	0.00	0.00	0.05	0.00
55.72	2.00	0.00	0.00	0.10	0.00	55.80	2.00	0.00	0.00	0.08	0.00
55.86	2.00	0.00	0.00	0.06	0.00	55.97	2.00	0.00	0.00	0.10	0.00
56.01	2.00	0.00	0.00	0.05	0.00	56.06	2.00	0.00	0.00	0.05	0.00
56.11	2.00	0.00	0.00	0.05	0.00	56.15	2.00	0.00	0.00	0.04	0.00
56.20	2.00	0.00	0.00	0.05	0.00	56.27	2.00	0.00	0.00	0.06	0.00
56.27	2.00	0.00	0.00	0.01	0.00	56.30	2.00	0.00	0.00	0.03	0.00
56.33	2.00	0.00	0.00	0.03	0.00	56.35	2.00	0.00	0.00	0.01	0.00
56.40	2.00	0.00	0.00	0.05	0.00	56.41	2.00	0.00	0.00	0.01	0.00
56.44	2.00	0.00	0.00	0.04	0.00	56.49	2.00	0.00	0.00	0.05	0.00
56.54	2.00	0.00	0.00	0.04	0.00	56.58	2.00	0.00	0.00	0.05	0.00
56.59	2.00	0.00	0.00	0.01	0.00	56.64	2.00	0.00	0.00	0.05	0.00
56.69	2.00	0.00	0.00	0.05	0.00	56.73	2.00	0.00	0.00	0.04	0.00
56.78	2.00	0.00	0.00	0.05	0.00	56.83	2.00	0.00	0.00	0.05	0.00
56.88	2.00	0.00	0.00	0.05	0.00	56.89	2.00	0.00	0.00	0.02	0.00
56.95	2.00	0.00	0.00	0.06	0.00	57.01	2.00	0.00	0.00	0.06	0.00
57.07	2.00	0.00	0.00	0.06	0.00	57.11	2.00	0.00	0.00	0.05	0.00
57.17	2.00	0.00	0.00	0.06	0.00	57.26	2.00	0.00	0.00	0.09	0.00
57.31	2.00	0.00	0.00	0.05	0.00	57.37	2.00	0.00	0.00	0.06	0.00
57.45	2.00	0.00	0.00	0.08	0.00	57.51	1.75	0.00	0.00	0.06	0.00
57.53	1.50	0.00	0.00	0.02	0.00	57.59	1.35	0.00	0.00	0.05	0.00
57.63	1.33	0.00	0.00	0.05	0.00	57.68	1.28	0.00	0.00	0.05	0.00
57.73	1.24	0.00	0.00	0.05	0.00	57.78	1.19	0.00	0.00	0.05	0.00
57.86	1.08	0.00	0.00	0.08	0.00	57.92	2.00	0.00	0.00	0.06	0.00
57.98	2.00	0.00	0.00	0.06	0.00	58.06	2.00	0.00	0.00	0.08	0.00
58.12	2.00	0.00	0.00	0.05	0.00	58.21	2.00	0.00	0.00	0.09	0.00
58.26	2.00	0.00	0.00	0.05	0.00	58.35	2.00	0.00	0.00	0.09	0.00
58.41	2.00	0.00	0.00	0.06	0.00	58.50	2.00	0.00	0.00	0.09	0.00
58.56	2.00	0.00	0.00	0.06	0.00	58.64	2.00	0.00	0.00	0.08	0.00
58.73	2.00	0.00	0.00	0.09	0.00	58.80	2.00	0.00	0.00	0.07	0.00
58.84	2.00	0.00	0.00	0.03	0.00	58.85	2.00	0.00	0.00	0.01	0.00
58.93	2.00	0.00	0.00	0.08	0.00	58.98	2.00	0.00	0.00	0.05	0.00
59.02	2.00	0.00	0.00	0.05	0.00	59.12	2.00	0.00	0.00	0.10	0.00
59.17	2.00	0.00	0.00	0.05	0.00	59.27	2.00	0.00	0.00	0.09	0.00
59.31	2.00	0.00	0.00	0.05	0.00	59.41	2.00	0.00	0.00	0.09	0.00
59.46	2.00	0.00	0.00	0.05	0.00	59.55	2.00	0.00	0.00	0.09	0.00
59.65	2.00	0.00	0.00	0.10	0.00	59.70	2.00	0.00	0.00	0.05	0.00
59.80	2.00	0.00	0.00	0.10	0.00	59.89	2.00	0.00	0.00	0.09	0.00
59.94	2.00	0.00	0.00	0.05	0.00	60.01	2.00	0.00	0.00	0.07	0.00
60.02	2.00	0.00	0.00	0.02	0.00	60.08	2.00	0.00	0.00	0.05	0.00
60.12	2.00	0.00	0.00	0.04	0.00	60.17	2.00	0.00	0.00	0.05	0.00
60.27	2.00	0.00	0.00	0.10	0.00	60.31	2.00	0.00	0.00	0.04	0.00
60.37	2.00	0.00	0.00	0.06	0.00	60.46	2.00	0.00	0.00	0.09	0.00
60.51	2.00	0.00	0.00	0.05	0.00	60.61	2.00	0.00	0.00	0.10	0.00
60.65	2.00	0.00	0.00	0.05	0.00	60.75	2.00	0.00	0.00	0.10	0.00
60.81	2.00	0.00	0.00	0.05	0.00	60.89	2.00	0.00	0.00	0.08	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
60.94	2.00	0.00	0.00	0.05	0.00	61.03	2.00	0.00	0.00	0.09	0.00
61.09	2.00	0.00	0.00	0.06	0.00	61.19	2.00	0.00	0.00	0.09	0.00
61.24	2.00	0.00	0.00	0.06	0.00	61.33	2.00	0.00	0.00	0.08	0.00
61.38	2.00	0.00	0.00	0.05	0.00	61.47	2.00	0.00	0.00	0.10	0.00
61.53	2.00	0.00	0.00	0.06	0.00	61.62	2.00	0.00	0.00	0.09	0.00
61.70	2.00	0.00	0.00	0.09	0.00	61.77	2.00	0.00	0.00	0.06	0.00
61.86	2.00	0.00	0.00	0.09	0.00	61.95	2.00	0.00	0.00	0.10	0.00
61.97	2.00	0.00	0.00	0.02	0.00	62.01	2.00	0.00	0.00	0.04	0.00
62.10	2.00	0.00	0.00	0.09	0.00	62.24	2.00	0.00	0.00	0.14	0.00
62.34	2.00	0.00	0.00	0.10	0.00	62.49	2.00	0.00	0.00	0.14	0.00
62.54	2.00	0.00	0.00	0.05	0.00	62.66	2.00	0.00	0.00	0.12	0.00
62.74	2.00	0.00	0.00	0.08	0.00	62.87	2.00	0.00	0.00	0.13	0.00
62.92	2.00	0.00	0.00	0.05	0.00	63.03	2.00	0.00	0.00	0.11	0.00
63.15	2.00	0.00	0.00	0.12	0.00	63.26	2.00	0.00	0.00	0.11	0.00
63.37	2.00	0.00	0.00	0.11	0.00	63.45	2.00	0.00	0.00	0.08	0.00
63.54	2.00	0.00	0.00	0.10	0.00	63.61	2.00	0.00	0.00	0.07	0.00
63.69	2.00	0.00	0.00	0.08	0.00	63.79	2.00	0.00	0.00	0.09	0.00
63.89	2.00	0.00	0.00	0.10	0.00	63.98	2.00	0.00	0.00	0.09	0.00
64.07	2.00	0.00	0.00	0.09	0.00	64.15	2.00	0.00	0.00	0.08	0.00
64.23	2.00	0.00	0.00	0.08	0.00	64.26	2.00	0.00	0.00	0.03	0.00
64.29	2.00	0.00	0.00	0.02	0.00	64.33	2.00	0.00	0.00	0.05	0.00
64.43	2.00	0.00	0.00	0.10	0.00	64.47	2.00	0.00	0.00	0.04	0.00
64.53	2.00	0.00	0.00	0.05	0.00	64.62	2.00	0.00	0.00	0.10	0.00
64.72	2.00	0.00	0.00	0.09	0.00	64.78	2.00	0.00	0.00	0.06	0.00
64.86	2.00	0.00	0.00	0.09	0.00	64.96	2.00	0.00	0.00	0.10	0.00
65.06	2.00	0.00	0.00	0.09	0.00	65.11	2.00	0.00	0.00	0.05	0.00
65.21	2.00	0.00	0.00	0.10	0.00	65.31	2.00	0.00	0.00	0.10	0.00
65.40	2.00	0.00	0.00	0.09	0.00	65.50	2.00	0.00	0.00	0.10	0.00
65.58	2.00	0.00	0.00	0.09	0.00	65.68	2.00	0.00	0.00	0.10	0.00
65.78	2.00	0.00	0.00	0.10	0.00	65.84	2.00	0.00	0.00	0.07	0.00
65.86	2.00	0.00	0.00	0.01	0.00	65.87	2.00	0.00	0.00	0.01	0.00
65.98	2.00	0.00	0.00	0.11	0.00	66.10	2.00	0.00	0.00	0.12	0.00
66.21	2.00	0.00	0.00	0.11	0.00	66.34	2.00	0.00	0.00	0.13	0.00
66.48	2.00	0.00	0.00	0.14	0.00	66.62	2.00	0.00	0.00	0.14	0.00
66.68	2.00	0.00	0.00	0.06	0.00	66.87	2.00	0.00	0.00	0.19	0.00
66.96	2.00	0.00	0.00	0.09	0.00	67.11	2.00	0.00	0.00	0.15	0.00
67.21	2.00	0.00	0.00	0.10	0.00	67.35	2.00	0.00	0.00	0.14	0.00
67.45	2.00	0.00	0.00	0.10	0.00	67.59	2.00	0.00	0.00	0.14	0.00
67.68	2.00	0.00	0.00	0.09	0.00	67.83	2.00	0.00	0.00	0.15	0.00
67.92	2.00	0.00	0.00	0.10	0.00	68.02	2.00	0.00	0.00	0.09	0.00
68.07	2.00	0.00	0.00	0.05	0.00	68.16	2.00	0.00	0.00	0.09	0.00
68.26	2.00	0.00	0.00	0.10	0.00	68.35	2.00	0.00	0.00	0.09	0.00
68.45	2.00	0.00	0.00	0.10	0.00	68.55	2.00	0.00	0.00	0.10	0.00
68.65	2.00	0.00	0.00	0.10	0.00	68.78	2.00	0.00	0.00	0.13	0.00
68.78	2.00	0.00	0.00	0.01	0.00	68.79	2.00	0.00	0.00	0.01	0.00
68.83	2.00	0.00	0.00	0.04	0.00	68.93	2.00	0.00	0.00	0.09	0.00
68.98	2.00	0.00	0.00	0.05	0.00	69.04	2.00	0.00	0.00	0.06	0.00
69.12	2.00	0.00	0.00	0.08	0.00	69.22	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
69.28	2.00	0.00	0.00	0.07	0.00	69.36	2.00	0.00	0.00	0.08	0.00
69.45	2.00	0.00	0.00	0.09	0.00	69.60	2.00	0.00	0.00	0.14	0.00
69.70	2.00	0.00	0.00	0.10	0.00	69.80	2.00	0.00	0.00	0.09	0.00
69.89	2.00	0.00	0.00	0.10	0.00	69.98	2.00	0.00	0.00	0.09	0.00
70.08	2.00	0.00	0.00	0.10	0.00	70.18	2.00	0.00	0.00	0.10	0.00
70.32	2.00	0.00	0.00	0.14	0.00	70.42	2.00	0.00	0.00	0.10	0.00
70.54	2.00	0.00	0.00	0.12	0.00	70.66	2.00	0.00	0.00	0.12	0.00
70.75	2.00	0.00	0.00	0.09	0.00	70.80	2.00	0.00	0.00	0.05	0.00
70.89	2.00	0.00	0.00	0.09	0.00	70.99	2.00	0.00	0.00	0.10	0.00
71.08	2.00	0.00	0.00	0.09	0.00	71.17	2.00	0.00	0.00	0.09	0.00
71.23	2.00	0.00	0.00	0.05	0.00	71.33	2.00	0.00	0.00	0.10	0.00
71.42	2.00	0.00	0.00	0.09	0.00	71.52	2.00	0.00	0.00	0.10	0.00
71.58	2.00	0.00	0.00	0.06	0.00	71.67	2.00	0.00	0.00	0.08	0.00
71.81	2.00	0.00	0.00	0.14	0.00	71.82	2.00	0.00	0.00	0.01	0.00
71.86	2.00	0.00	0.00	0.04	0.00	71.91	2.00	0.00	0.00	0.05	0.00
71.97	2.00	0.00	0.00	0.06	0.00	72.05	2.00	0.00	0.00	0.08	0.00
72.10	2.00	0.00	0.00	0.05	0.00	72.20	2.00	0.00	0.00	0.10	0.00
72.25	2.00	0.00	0.00	0.05	0.00	72.34	2.00	0.00	0.00	0.10	0.00
72.44	2.00	0.00	0.00	0.10	0.00	72.53	2.00	0.00	0.00	0.09	0.00
72.63	2.00	0.00	0.00	0.10	0.00	72.69	2.00	0.00	0.00	0.06	0.00
72.82	2.00	0.00	0.00	0.13	0.00	72.92	2.00	0.00	0.00	0.09	0.00
73.06	2.00	0.00	0.00	0.14	0.00	73.16	2.00	0.00	0.00	0.10	0.00
73.30	2.00	0.00	0.00	0.14	0.00	73.35	2.00	0.00	0.00	0.05	0.00
73.38	2.00	0.00	0.00	0.03	0.00	73.47	2.00	0.00	0.00	0.09	0.00
73.53	2.00	0.00	0.00	0.06	0.00	73.62	2.00	0.00	0.00	0.09	0.00
73.71	2.00	0.00	0.00	0.09	0.00	73.77	2.00	0.00	0.00	0.06	0.00
73.86	2.00	0.00	0.00	0.09	0.00	73.96	2.00	0.00	0.00	0.09	0.00
74.06	2.00	0.00	0.00	0.10	0.00	74.13	2.00	0.00	0.00	0.07	0.00
74.24	2.00	0.00	0.00	0.11	0.00	74.34	2.00	0.00	0.00	0.10	0.00
74.44	2.00	0.00	0.00	0.10	0.00	74.58	2.00	0.00	0.00	0.14	0.00
74.68	2.00	0.00	0.00	0.10	0.00	74.80	2.00	0.00	0.00	0.13	0.00
74.92	2.00	0.00	0.00	0.12	0.00	75.07	2.00	0.00	0.00	0.14	0.00
75.08	2.00	0.00	0.00	0.01	0.00	75.11	2.00	0.00	0.00	0.03	0.00
75.16	2.00	0.00	0.00	0.05	0.00	75.25	2.00	0.00	0.00	0.09	0.00
75.32	2.00	0.00	0.00	0.07	0.00	75.40	2.00	0.00	0.00	0.08	0.00
75.50	2.00	0.00	0.00	0.10	0.00	75.59	2.00	0.00	0.00	0.09	0.00
75.69	2.00	0.00	0.00	0.10	0.00	75.78	2.00	0.00	0.00	0.09	0.00
75.88	2.00	0.00	0.00	0.09	0.00	75.96	2.00	0.00	0.00	0.09	0.00
76.05	2.00	0.00	0.00	0.08	0.00	76.14	2.00	0.00	0.00	0.09	0.00
76.26	2.00	0.00	0.00	0.12	0.00	76.36	2.00	0.00	0.00	0.10	0.00
76.41	2.00	0.00	0.00	0.05	0.00	76.51	2.00	0.00	0.00	0.10	0.00
76.65	2.00	0.00	0.00	0.14	0.00	76.72	2.00	0.00	0.00	0.07	0.00
76.79	2.00	0.00	0.00	0.07	0.00	76.89	2.00	0.00	0.00	0.10	0.00
76.98	2.00	0.00	0.00	0.09	0.00	77.08	2.00	0.00	0.00	0.10	0.00
77.18	2.00	0.00	0.00	0.10	0.00	77.28	2.00	0.00	0.00	0.10	0.00
77.37	2.00	0.00	0.00	0.10	0.00	77.42	2.00	0.00	0.00	0.04	0.00
77.42	2.00	0.00	0.00	0.01	0.00	77.44	2.00	0.00	0.00	0.01	0.00
77.48	2.00	0.00	0.00	0.04	0.00	77.52	2.00	0.00	0.00	0.04	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
77.54	2.00	0.00	0.00	0.02	0.00	77.57	2.00	0.00	0.00	0.03	0.00
77.62	2.00	0.00	0.00	0.05	0.00	77.65	2.00	0.00	0.00	0.04	0.00
77.67	2.00	0.00	0.00	0.01	0.00	77.71	2.00	0.00	0.00	0.04	0.00
77.71	2.00	0.00	0.00	0.01	0.00	77.76	2.00	0.00	0.00	0.05	0.00
77.81	2.00	0.00	0.00	0.05	0.00	77.90	2.00	0.00	0.00	0.09	0.00
77.95	2.00	0.00	0.00	0.05	0.00	78.01	2.00	0.00	0.00	0.06	0.00
78.10	2.00	0.00	0.00	0.09	0.00	78.16	2.00	0.00	0.00	0.06	0.00
78.24	2.00	0.00	0.00	0.08	0.00	78.29	2.00	0.00	0.00	0.05	0.00
78.39	2.00	0.00	0.00	0.10	0.00	78.47	2.00	0.00	0.00	0.08	0.00
78.53	2.00	0.00	0.00	0.06	0.00	78.62	2.00	0.00	0.00	0.09	0.00
78.68	2.00	0.00	0.00	0.05	0.00	78.69	2.00	0.00	0.00	0.01	0.00
78.78	2.00	0.00	0.00	0.09	0.00	78.81	2.00	0.00	0.00	0.04	0.00
78.92	2.00	0.00	0.00	0.11	0.00	79.03	2.00	0.00	0.00	0.11	0.00
79.16	2.00	0.00	0.00	0.13	0.00	79.26	2.00	0.00	0.00	0.10	0.00
79.35	2.00	0.00	0.00	0.09	0.00	79.45	2.00	0.00	0.00	0.10	0.00
79.54	2.00	0.00	0.00	0.09	0.00	79.64	2.00	0.00	0.00	0.10	0.00
79.74	2.00	0.00	0.00	0.10	0.00	79.88	2.00	0.00	0.00	0.14	0.00
79.98	2.00	0.00	0.00	0.10	0.00	80.12	2.00	0.00	0.00	0.14	0.00
80.22	2.00	0.00	0.00	0.09	0.00	80.36	2.00	0.00	0.00	0.14	0.00
80.46	2.00	0.00	0.00	0.10	0.00	80.60	2.00	0.00	0.00	0.14	0.00
80.70	2.00	0.00	0.00	0.10	0.00	80.83	2.00	0.00	0.00	0.13	0.00
80.94	2.00	0.00	0.00	0.11	0.00	81.01	2.00	0.00	0.00	0.07	0.00
81.04	2.00	0.00	0.00	0.03	0.00	81.09	2.00	0.00	0.00	0.06	0.00
81.13	2.00	0.00	0.00	0.04	0.00	81.18	2.00	0.00	0.00	0.05	0.00
81.23	2.00	0.00	0.00	0.05	0.00	81.28	2.00	0.00	0.00	0.05	0.00
81.33	2.00	0.00	0.00	0.05	0.00	81.37	2.00	0.00	0.00	0.05	0.00
81.42	2.00	0.00	0.00	0.04	0.00	81.47	2.00	0.00	0.00	0.05	0.00
81.52	2.00	0.00	0.00	0.05	0.00	81.56	2.00	0.00	0.00	0.05	0.00
81.61	2.00	0.00	0.00	0.04	0.00	81.64	2.00	0.00	0.00	0.04	0.00
81.70	2.00	0.00	0.00	0.06	0.00	81.75	2.00	0.00	0.00	0.05	0.00
81.79	2.00	0.00	0.00	0.04	0.00	81.82	2.00	0.00	0.00	0.03	0.00
81.86	2.00	0.00	0.00	0.04	0.00	81.91	2.00	0.00	0.00	0.05	0.00
81.95	2.00	0.00	0.00	0.04	0.00	82.00	2.00	0.00	0.00	0.05	0.00
82.09	2.00	0.00	0.00	0.09	0.00	82.15	2.00	0.00	0.00	0.06	0.00
82.19	2.00	0.00	0.00	0.04	0.00	82.26	2.00	0.00	0.00	0.07	0.00
82.34	2.00	0.00	0.00	0.08	0.00	82.39	2.00	0.00	0.00	0.05	0.00
82.48	2.00	0.00	0.00	0.10	0.00	82.58	2.00	0.00	0.00	0.09	0.00
82.62	2.00	0.00	0.00	0.04	0.00	82.70	2.00	0.00	0.00	0.08	0.00
82.77	2.00	0.00	0.00	0.07	0.00	82.87	2.00	0.00	0.00	0.10	0.00
82.96	2.00	0.00	0.00	0.09	0.00	83.06	2.00	0.00	0.00	0.10	0.00
83.16	2.00	0.00	0.00	0.10	0.00	83.25	2.00	0.00	0.00	0.09	0.00
83.34	2.00	0.00	0.00	0.09	0.00	83.44	2.00	0.00	0.00	0.10	0.00
83.54	2.00	0.00	0.00	0.10	0.00	83.64	2.00	0.00	0.00	0.09	0.00
83.73	2.00	0.00	0.00	0.10	0.00	83.83	2.00	0.00	0.00	0.09	0.00
83.85	2.00	0.00	0.00	0.02	0.00	83.89	2.00	0.00	0.00	0.04	0.00
83.94	2.00	0.00	0.00	0.05	0.00	84.04	2.00	0.00	0.00	0.10	0.00
84.09	2.00	0.00	0.00	0.05	0.00	84.13	2.00	0.00	0.00	0.04	0.00
84.18	2.00	0.00	0.00	0.05	0.00	84.25	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
84.33	2.00	0.00	0.00	0.08	0.00	84.37	2.00	0.00	0.00	0.05	0.00
84.46	2.00	0.00	0.00	0.08	0.00	84.52	2.00	0.00	0.00	0.06	0.00
84.57	2.00	0.00	0.00	0.05	0.00	84.67	2.00	0.00	0.00	0.10	0.00
84.71	2.00	0.00	0.00	0.04	0.00	84.81	2.00	0.00	0.00	0.10	0.00
84.86	2.00	0.00	0.00	0.05	0.00	84.91	2.00	0.00	0.00	0.06	0.00
85.00	2.00	0.00	0.00	0.09	0.00	85.05	2.00	0.00	0.00	0.05	0.00
85.15	2.00	0.00	0.00	0.10	0.00	85.19	2.00	0.00	0.00	0.05	0.00
85.29	2.00	0.00	0.00	0.10	0.00	85.35	2.00	0.00	0.00	0.06	0.00
85.42	2.00	0.00	0.00	0.07	0.00	85.48	2.00	0.00	0.00	0.06	0.00
85.55	2.00	0.00	0.00	0.06	0.00	85.63	2.00	0.00	0.00	0.08	0.00
85.68	2.00	0.00	0.00	0.05	0.00	85.77	2.00	0.00	0.00	0.09	0.00
85.82	2.00	0.00	0.00	0.05	0.00	85.89	2.00	0.00	0.00	0.07	0.00
85.96	2.00	0.00	0.00	0.08	0.00	86.03	2.00	0.00	0.00	0.07	0.00
86.11	2.00	0.00	0.00	0.07	0.00	86.16	2.00	0.00	0.00	0.06	0.00
86.25	2.00	0.00	0.00	0.09	0.00	86.36	2.00	0.00	0.00	0.11	0.00
86.50	2.00	0.00	0.00	0.14	0.00	86.51	2.00	0.00	0.00	0.01	0.00
86.52	2.00	0.00	0.00	0.01	0.00	86.57	2.00	0.00	0.00	0.05	0.00
86.65	2.00	0.00	0.00	0.09	0.00	86.71	2.00	0.00	0.00	0.06	0.00
86.80	2.00	0.00	0.00	0.09	0.00	86.90	2.00	0.00	0.00	0.09	0.00
86.99	2.00	0.00	0.00	0.09	0.00	87.04	2.00	0.00	0.00	0.05	0.00
87.14	2.00	0.00	0.00	0.09	0.00	87.19	2.00	0.00	0.00	0.06	0.00
87.28	2.00	0.00	0.00	0.09	0.00	87.38	2.00	0.00	0.00	0.09	0.00
87.43	2.00	0.00	0.00	0.06	0.00	87.52	2.00	0.00	0.00	0.09	0.00
87.61	2.00	0.00	0.00	0.09	0.00	87.66	2.00	0.00	0.00	0.05	0.00
87.76	2.00	0.00	0.00	0.10	0.00	87.84	2.00	0.00	0.00	0.08	0.00
87.91	2.00	0.00	0.00	0.07	0.00	88.00	2.00	0.00	0.00	0.09	0.00
88.11	2.00	0.00	0.00	0.11	0.00	88.19	2.00	0.00	0.00	0.08	0.00
88.25	2.00	0.00	0.00	0.06	0.00	88.34	2.00	0.00	0.00	0.09	0.00
88.44	2.00	0.00	0.00	0.10	0.00	88.54	2.00	0.00	0.00	0.11	0.00
88.64	2.00	0.00	0.00	0.10	0.00	88.72	2.00	0.00	0.00	0.09	0.00
88.82	2.00	0.00	0.00	0.10	0.00	88.91	2.00	0.00	0.00	0.09	0.00
89.01	2.00	0.00	0.00	0.10	0.00	89.10	2.00	0.00	0.00	0.09	0.00
89.19	2.00	0.00	0.00	0.09	0.00	89.30	2.00	0.00	0.00	0.11	0.00
89.39	2.00	0.00	0.00	0.09	0.00	89.49	2.00	0.00	0.00	0.10	0.00
89.59	2.00	0.00	0.00	0.09	0.00	89.69	2.00	0.00	0.00	0.10	0.00
89.73	2.00	0.00	0.00	0.05	0.00	89.78	2.00	0.00	0.00	0.04	0.00
89.83	2.00	0.00	0.00	0.06	0.00	89.88	2.00	0.00	0.00	0.05	0.00
89.93	2.00	0.00	0.00	0.05	0.00	90.00	2.00	0.00	0.00	0.07	0.00
90.07	2.00	0.00	0.00	0.08	0.00	90.12	2.00	0.00	0.00	0.05	0.00
90.22	2.00	0.00	0.00	0.09	0.00	90.27	2.00	0.00	0.00	0.05	0.00
90.36	2.00	0.00	0.00	0.09	0.00	90.46	2.00	0.00	0.00	0.10	0.00
90.50	2.00	0.00	0.00	0.04	0.00	90.61	2.00	0.00	0.00	0.10	0.00
90.66	2.00	0.00	0.00	0.05	0.00	90.75	2.00	0.00	0.00	0.09	0.00
90.84	2.00	0.00	0.00	0.09	0.00	90.89	2.00	0.00	0.00	0.05	0.00
90.99	2.00	0.00	0.00	0.10	0.00	91.04	2.00	0.00	0.00	0.05	0.00
91.14	2.00	0.00	0.00	0.09	0.00	91.22	2.00	0.00	0.00	0.09	0.00
91.28	2.00	0.00	0.00	0.06	0.00	91.37	2.00	0.00	0.00	0.09	0.00
91.47	2.00	0.00	0.00	0.10	0.00	91.61	2.00	0.00	0.00	0.14	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
91.71	2.00	0.00	0.00	0.10	0.00	91.81	2.00	0.00	0.00	0.10	0.00
91.87	2.00	0.00	0.00	0.06	0.00	92.00	2.00	0.00	0.00	0.13	0.00
92.10	2.00	0.00	0.00	0.10	0.00	92.20	2.00	0.00	0.00	0.10	0.00
92.33	2.00	0.00	0.00	0.13	0.00	92.38	2.00	0.00	0.00	0.05	0.00
92.43	2.00	0.00	0.00	0.05	0.00	92.48	2.00	0.00	0.00	0.05	0.00
92.56	2.00	0.00	0.00	0.08	0.00	92.63	2.00	0.00	0.00	0.07	0.00
92.67	2.00	0.00	0.00	0.05	0.00	92.72	2.00	0.00	0.00	0.04	0.00
92.77	2.00	0.00	0.00	0.05	0.00	92.86	2.00	0.00	0.00	0.10	0.00
92.92	2.00	0.00	0.00	0.05	0.00	92.97	2.00	0.00	0.00	0.05	0.00
93.05	2.00	0.00	0.00	0.08	0.00	93.10	2.00	0.00	0.00	0.06	0.00
93.16	2.00	0.00	0.00	0.06	0.00	93.25	2.00	0.00	0.00	0.09	0.00
93.35	2.00	0.00	0.00	0.10	0.00	93.40	2.00	0.00	0.00	0.05	0.00
93.49	2.00	0.00	0.00	0.10	0.00	93.56	2.00	0.00	0.00	0.07	0.00
93.64	2.00	0.00	0.00	0.08	0.00	93.73	2.00	0.00	0.00	0.09	0.00
93.83	2.00	0.00	0.00	0.10	0.00	93.88	2.00	0.00	0.00	0.05	0.00
93.97	2.00	0.00	0.00	0.09	0.00	94.07	2.00	0.00	0.00	0.10	0.00
94.17	2.00	0.00	0.00	0.10	0.00	94.26	2.00	0.00	0.00	0.10	0.00
94.36	2.00	0.00	0.00	0.09	0.00	94.45	2.00	0.00	0.00	0.09	0.00
94.55	2.00	0.00	0.00	0.10	0.00	94.64	2.00	0.00	0.00	0.09	0.00
94.72	2.00	0.00	0.00	0.07	0.00	94.74	2.00	0.00	0.00	0.03	0.00
94.77	2.00	0.00	0.00	0.02	0.00	94.85	2.00	0.00	0.00	0.08	0.00
94.90	2.00	0.00	0.00	0.05	0.00	94.95	2.00	0.00	0.00	0.05	0.00
95.01	2.00	0.00	0.00	0.06	0.00	95.09	2.00	0.00	0.00	0.08	0.00
95.14	2.00	0.00	0.00	0.05	0.00	95.23	2.00	0.00	0.00	0.09	0.00
95.29	2.00	0.00	0.00	0.06	0.00	95.38	2.00	0.00	0.00	0.09	0.00
95.43	2.00	0.00	0.00	0.05	0.00	95.52	2.00	0.00	0.00	0.09	0.00
95.57	2.00	0.00	0.00	0.05	0.00	95.67	2.00	0.00	0.00	0.10	0.00
95.77	2.00	0.00	0.00	0.09	0.00	95.86	2.00	0.00	0.00	0.10	0.00
95.95	2.00	0.00	0.00	0.09	0.00	96.03	2.00	0.00	0.00	0.08	0.00
96.11	2.00	0.00	0.00	0.08	0.00	96.20	2.00	0.00	0.00	0.09	0.00
96.30	2.00	0.00	0.00	0.10	0.00	96.39	2.00	0.00	0.00	0.09	0.00
96.50	2.00	0.00	0.00	0.11	0.00	96.59	2.00	0.00	0.00	0.09	0.00
96.69	2.00	0.00	0.00	0.10	0.00	96.78	2.00	0.00	0.00	0.09	0.00
96.87	2.00	0.00	0.00	0.09	0.00	96.98	2.00	0.00	0.00	0.11	0.00
97.02	2.00	0.00	0.00	0.04	0.00	97.06	2.00	0.00	0.00	0.05	0.00
97.12	2.00	0.00	0.00	0.05	0.00	97.16	2.00	0.00	0.00	0.04	0.00
97.21	2.00	0.00	0.00	0.05	0.00	97.27	2.00	0.00	0.00	0.06	0.00
97.33	2.00	0.00	0.00	0.06	0.00	97.40	2.00	0.00	0.00	0.07	0.00
97.45	2.00	0.00	0.00	0.05	0.00	97.50	2.00	0.00	0.00	0.05	0.00
97.58	2.00	0.00	0.00	0.08	0.00	97.65	2.00	0.00	0.00	0.07	0.00
97.69	2.00	0.00	0.00	0.04	0.00	97.74	2.00	0.00	0.00	0.05	0.00
97.81	2.00	0.00	0.00	0.07	0.00	97.88	2.00	0.00	0.00	0.08	0.00
97.93	2.00	0.00	0.00	0.05	0.00	98.03	2.00	0.00	0.00	0.10	0.00
98.15	2.00	0.00	0.00	0.12	0.00	98.21	2.00	0.00	0.00	0.06	0.00
98.32	2.00	0.00	0.00	0.11	0.00	98.42	2.00	0.00	0.00	0.09	0.00
98.47	2.00	0.00	0.00	0.05	0.00	98.57	2.00	0.00	0.00	0.10	0.00
98.70	2.00	0.00	0.00	0.13	0.00	98.78	2.00	0.00	0.00	0.08	0.00
98.85	2.00	0.00	0.00	0.06	0.00	98.86	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
98.92	2.00	0.00	0.00	0.06	0.00	98.98	2.00	0.00	0.00	0.06	0.00
99.03	2.00	0.00	0.00	0.05	0.00	99.11	2.00	0.00	0.00	0.07	0.00
99.18	2.00	0.00	0.00	0.07	0.00	99.23	2.00	0.00	0.00	0.05	0.00
99.32	2.00	0.00	0.00	0.09	0.00	99.37	2.00	0.00	0.00	0.05	0.00
99.45	2.00	0.00	0.00	0.08	0.00	99.56	2.00	0.00	0.00	0.11	0.00
99.64	2.00	0.00	0.00	0.07	0.00	99.71	2.00	0.00	0.00	0.07	0.00
99.75	2.00	0.00	0.00	0.04	0.00	99.90	2.00	0.00	0.00	0.15	0.00
99.95	2.00	0.00	0.00	0.05	0.00	100.04	2.00	0.00	0.00	0.09	0.00
100.14	2.00	0.00	0.00	0.09	0.00	100.14	2.00	0.00	0.00	0.00	0.00
100.15	2.00	0.00	0.00	0.01	0.00	100.19	2.00	0.00	0.00	0.03	0.00
100.21	2.00	0.00	0.00	0.02	0.00	100.24	2.00	0.00	0.00	0.03	0.00
100.28	2.00	0.00	0.00	0.05	0.00	100.31	2.00	0.00	0.00	0.02	0.00
100.33	2.00	0.00	0.00	0.02	0.00	100.38	2.00	0.00	0.00	0.05	0.00
100.39	2.00	0.00	0.00	0.01	0.00	100.43	2.00	0.00	0.00	0.03	0.00
100.48	2.00	0.00	0.00	0.05	0.00	100.53	2.00	0.00	0.00	0.05	0.00
100.57	2.00	0.00	0.00	0.05	0.00	100.60	2.00	0.00	0.00	0.02	0.00

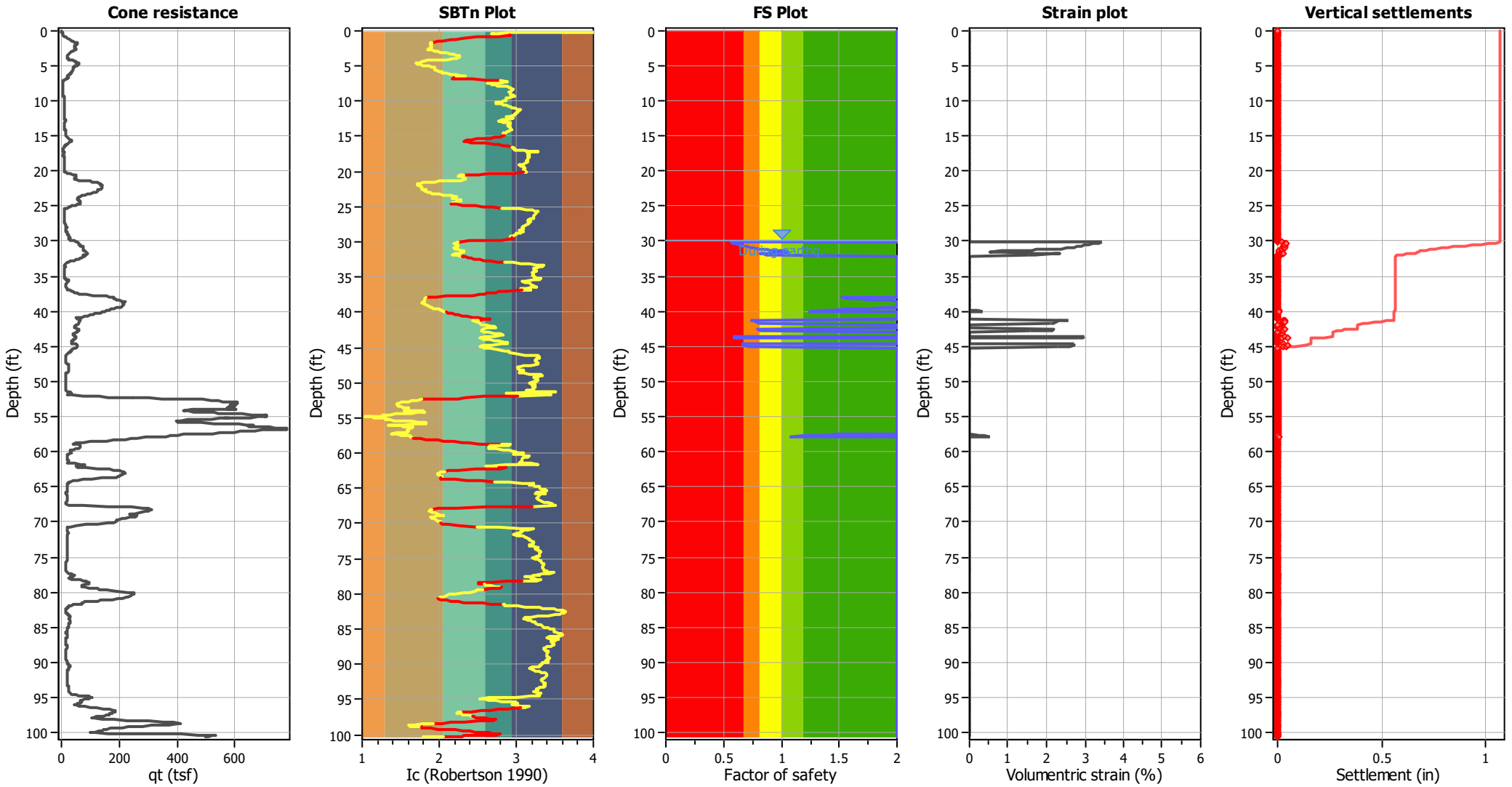
Overall liquefaction potential: 1.15

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
30.06	59.16	2.00	0.00	1.00	0.00	30.13	60.99	2.00	0.00	1.00	0.00
30.18	62.30	0.57	3.44	1.00	0.02	30.28	64.44	0.58	3.35	1.00	0.04
30.37	67.53	0.60	3.22	1.00	0.04	30.47	71.05	0.63	3.09	1.00	0.04
30.57	73.87	0.65	3.00	1.00	0.04	30.66	76.12	0.67	2.92	1.00	0.03
30.74	78.31	0.69	2.86	1.00	0.03	30.82	80.52	0.71	2.79	1.00	0.03
30.90	82.93	0.73	2.72	1.00	0.03	31.01	85.67	0.76	2.55	1.00	0.03
31.10	89.47	0.80	2.39	1.00	0.02	31.19	93.96	0.86	1.72	1.00	0.02
31.28	98.21	0.92	1.61	1.00	0.02	31.35	101.82	0.97	0.87	1.00	0.01
31.43	104.59	1.02	0.85	1.00	0.01	31.53	107.28	1.06	0.53	1.00	0.01
31.60	101.10	0.96	0.87	1.00	0.01	31.67	95.74	0.88	1.67	1.00	0.02
31.77	91.18	0.82	2.33	1.00	0.03	31.84	93.40	0.84	2.24	1.00	0.02
31.91	95.19	0.87	1.69	1.00	0.01	31.98	97.23	0.89	1.63	1.00	0.01
31.98	99.23	0.92	1.59	1.00	0.00	32.04	100.65	0.94	1.55	1.00	0.01
32.12	102.19	2.00	0.00	1.00	0.00	32.16	105.63	2.00	0.00	1.00	0.00
32.27	108.77	2.00	0.00	1.00	0.00	32.33	111.51	2.00	0.00	1.00	0.00
32.41	112.40	2.00	0.00	1.00	0.00	32.50	111.66	2.00	0.00	1.00	0.00
32.58	110.12	2.00	0.00	1.00	0.00	32.66	108.68	2.00	0.00	1.00	0.00
32.74	107.79	2.00	0.00	1.00	0.00	32.84	107.96	2.00	0.00	1.00	0.00
32.90	107.62	2.00	0.00	1.00	0.00	32.98	104.08	2.00	0.00	1.00	0.00
33.08	101.84	2.00	0.00	1.00	0.00	33.14	99.50	2.00	0.00	1.00	0.00
33.22	96.06	2.00	0.00	1.00	0.00	33.32	91.43	2.00	0.00	1.00	0.00
33.37	85.28	2.00	0.00	1.00	0.00	33.47	81.70	2.00	0.00	1.00	0.00
33.56	79.85	2.00	0.00	1.00	0.00	33.63	80.15	2.00	0.00	1.00	0.00
33.71	78.37	2.00	0.00	1.00	0.00	33.81	72.19	2.00	0.00	1.00	0.00
33.90	65.65	2.00	0.00	1.00	0.00	33.95	60.28	2.00	0.00	1.00	0.00
34.04	59.84	2.00	0.00	1.00	0.00	34.14	59.54	2.00	0.00	1.00	0.00
34.17	59.63	2.00	0.00	1.00	0.00	34.20	59.92	2.00	0.00	1.00	0.00
34.26	60.14	2.00	0.00	1.00	0.00	34.35	59.91	2.00	0.00	1.00	0.00
34.43	59.45	2.00	0.00	1.00	0.00	34.49	58.59	2.00	0.00	1.00	0.00
34.59	57.25	2.00	0.00	1.00	0.00	34.69	55.91	2.00	0.00	1.00	0.00
34.73	54.88	2.00	0.00	1.00	0.00	34.83	54.34	2.00	0.00	1.00	0.00
34.90	54.48	2.00	0.00	1.00	0.00	34.98	55.47	2.00	0.00	1.00	0.00
35.07	58.28	2.00	0.00	1.00	0.00	35.16	64.79	2.00	0.00	1.00	0.00
35.26	76.48	2.00	0.00	1.00	0.00	35.33	89.71	2.00	0.00	1.00	0.00
35.40	101.03	2.00	0.00	1.00	0.00	35.50	106.70	2.00	0.00	1.00	0.00
35.57	109.72	2.00	0.00	1.00	0.00	35.65	112.36	2.00	0.00	1.00	0.00
35.71	115.22	2.00	0.00	1.00	0.00	35.79	116.27	2.00	0.00	1.00	0.00
35.85	113.90	2.00	0.00	1.00	0.00	35.94	109.71	2.00	0.00	1.00	0.00
35.99	103.66	2.00	0.00	1.00	0.00	36.08	95.94	2.00	0.00	1.00	0.00
36.17	88.35	2.00	0.00	1.00	0.00	36.24	82.76	2.00	0.00	1.00	0.00
36.33	81.11	2.00	0.00	1.00	0.00	36.42	82.08	2.00	0.00	1.00	0.00
36.52	77.16	2.00	0.00	1.00	0.00	36.61	74.88	2.00	0.00	1.00	0.00
36.70	76.79	2.00	0.00	1.00	0.00	36.78	88.43	2.00	0.00	1.00	0.00
36.85	99.18	2.00	0.00	1.00	0.00	36.87	103.88	2.00	0.00	1.00	0.00
36.91	105.17	2.00	0.00	1.00	0.00	36.97	104.77	2.00	0.00	1.00	0.00
37.06	105.20	2.00	0.00	1.00	0.00	37.12	107.91	2.00	0.00	1.00	0.00
37.20	112.33	2.00	0.00	1.00	0.00	37.27	114.30	2.00	0.00	1.00	0.00
37.35	112.42	2.00	0.00	1.00	0.00	37.44	108.21	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
37.49	102.76	2.00	0.00	1.00	0.00	37.59	95.81	2.00	0.00	1.00	0.00
37.64	90.11	2.00	0.00	1.00	0.00	37.70	94.79	2.00	0.00	1.00	0.00
37.78	108.37	2.00	0.00	1.00	0.00	37.83	120.19	2.00	0.00	1.00	0.00
37.92	126.68	2.00	0.00	1.00	0.00	37.97	130.53	2.00	0.00	1.00	0.00
38.07	133.13	1.52	0.00	1.00	0.00	38.14	135.64	1.59	0.00	1.00	0.00
38.22	138.68	1.67	0.00	1.00	0.00	38.31	143.23	1.79	0.00	1.00	0.00
38.41	148.66	1.96	0.00	1.00	0.00	38.52	154.32	2.00	0.00	1.00	0.00
38.64	157.41	2.00	0.00	1.00	0.00	38.74	158.10	2.00	0.00	1.00	0.00
38.80	157.57	2.00	0.00	1.00	0.00	38.89	156.57	2.00	0.00	1.00	0.00
38.94	158.84	2.00	0.00	1.00	0.00	39.03	159.69	2.00	0.00	1.00	0.00
39.13	160.46	2.00	0.00	1.00	0.00	39.23	160.12	2.00	0.00	1.00	0.00
39.35	158.27	2.00	0.00	1.00	0.00	39.42	154.08	2.00	0.00	1.00	0.00
39.51	148.22	1.93	0.00	1.00	0.00	39.60	141.37	1.73	0.00	1.00	0.00
39.70	135.85	1.58	0.00	1.00	0.00	39.78	130.75	1.45	0.00	1.00	0.00
39.90	126.28	1.34	0.24	1.00	0.00	39.99	121.65	1.24	0.35	1.00	0.00
40.09	117.75	2.00	0.00	1.00	0.00	40.18	114.33	2.00	0.00	1.00	0.00
40.23	111.30	2.00	0.00	1.00	0.00	40.33	108.90	2.00	0.00	1.00	0.00
40.43	107.17	2.00	0.00	1.00	0.00	40.52	107.68	2.00	0.00	1.00	0.00
40.61	106.53	2.00	0.00	1.00	0.00	40.69	106.96	2.00	0.00	1.00	0.00
40.80	106.21	2.00	0.00	1.00	0.00	40.87	107.20	2.00	0.00	1.00	0.00
40.95	107.50	2.00	0.00	1.00	0.00	40.97	105.79	2.00	0.00	1.00	0.00
41.01	101.77	2.00	0.00	1.00	0.00	41.07	94.92	2.00	0.00	1.00	0.00
41.15	90.47	2.00	0.00	1.00	0.00	41.26	89.74	0.74	2.55	1.00	0.03
41.35	91.40	0.76	2.32	1.00	0.02	41.47	93.27	0.78	2.25	1.00	0.03
41.59	94.19	0.79	2.22	1.00	0.03	41.69	95.29	0.80	2.18	1.00	0.03
41.78	97.63	0.83	2.10	1.00	0.02	41.88	100.94	2.00	0.00	1.00	0.00
41.98	103.21	2.00	0.00	1.00	0.00	42.08	103.54	2.00	0.00	1.00	0.00
42.16	102.01	2.00	0.00	1.00	0.00	42.24	99.69	2.00	0.00	1.00	0.00
42.31	97.23	2.00	0.00	1.00	0.00	42.45	95.61	0.80	2.17	1.00	0.04
42.55	94.91	0.80	2.19	1.00	0.02	42.60	95.14	0.80	2.19	1.00	0.01
42.70	96.60	0.82	2.14	1.00	0.03	42.81	99.43	0.85	1.58	1.00	0.02
42.89	103.15	2.00	0.00	1.00	0.00	42.98	106.61	2.00	0.00	1.00	0.00
43.08	108.99	2.00	0.00	1.00	0.00	43.17	109.35	2.00	0.00	1.00	0.00
43.27	107.03	2.00	0.00	1.00	0.00	43.37	95.48	2.00	0.00	1.00	0.00
43.50	83.44	2.00	0.00	1.00	0.00	43.61	73.95	0.59	2.99	1.00	0.04
43.74	75.29	0.60	2.95	1.00	0.05	43.79	79.06	0.63	2.83	1.00	0.02
43.86	84.59	2.00	0.00	1.00	0.00	43.94	91.16	2.00	0.00	1.00	0.00
44.00	98.08	2.00	0.00	1.00	0.00	44.08	103.37	2.00	0.00	1.00	0.00
44.17	106.26	2.00	0.00	1.00	0.00	44.27	105.00	2.00	0.00	1.00	0.00
44.42	100.72	2.00	0.00	1.00	0.00	44.52	95.03	2.00	0.00	1.00	0.00
44.61	87.72	2.00	0.00	1.00	0.00	44.71	83.46	0.67	2.71	1.00	0.03
44.85	83.87	0.67	2.70	1.00	0.05	44.95	88.11	0.71	2.59	1.00	0.03
45.09	92.06	0.76	2.29	1.00	0.04	45.19	95.00	2.00	0.00	1.00	0.00
45.33	98.48	2.00	0.00	1.00	0.00	45.42	100.02	2.00	0.00	1.00	0.00
45.57	98.64	2.00	0.00	1.00	0.00	45.68	94.66	2.00	0.00	1.00	0.00
45.81	87.72	2.00	0.00	1.00	0.00	45.92	82.93	2.00	0.00	1.00	0.00
46.05	82.51	2.00	0.00	1.00	0.00	46.16	86.12	2.00	0.00	1.00	0.00
46.17	85.57	2.00	0.00	1.00	0.00	46.23	84.09	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
46.29	82.02	2.00	0.00	1.00	0.00	46.34	78.81	2.00	0.00	1.00	0.00
46.42	74.90	2.00	0.00	1.00	0.00	46.48	70.80	2.00	0.00	1.00	0.00
46.52	67.86	2.00	0.00	1.00	0.00	46.60	65.79	2.00	0.00	1.00	0.00
46.67	64.21	2.00	0.00	1.00	0.00	46.74	63.02	2.00	0.00	1.00	0.00
46.82	61.88	2.00	0.00	1.00	0.00	46.88	61.07	2.00	0.00	1.00	0.00
46.96	60.61	2.00	0.00	1.00	0.00	47.06	60.52	2.00	0.00	1.00	0.00
47.15	61.03	2.00	0.00	1.00	0.00	47.24	65.10	2.00	0.00	1.00	0.00
47.35	75.39	2.00	0.00	1.00	0.00	47.49	80.67	2.00	0.00	1.00	0.00
47.58	82.65	2.00	0.00	1.00	0.00	47.73	80.95	2.00	0.00	1.00	0.00
47.83	81.84	2.00	0.00	1.00	0.00	47.87	83.19	2.00	0.00	1.00	0.00
47.89	82.12	2.00	0.00	1.00	0.00	47.94	81.59	2.00	0.00	1.00	0.00
48.02	80.90	2.00	0.00	1.00	0.00	48.07	81.07	2.00	0.00	1.00	0.00
48.12	82.45	2.00	0.00	1.00	0.00	48.18	84.09	2.00	0.00	1.00	0.00
48.26	85.42	2.00	0.00	1.00	0.00	48.31	84.77	2.00	0.00	1.00	0.00
48.38	82.58	2.00	0.00	1.00	0.00	48.46	79.31	2.00	0.00	1.00	0.00
48.52	75.99	2.00	0.00	1.00	0.00	48.60	72.40	2.00	0.00	1.00	0.00
48.68	69.64	2.00	0.00	1.00	0.00	48.74	67.76	2.00	0.00	1.00	0.00
48.82	67.24	2.00	0.00	1.00	0.00	48.89	66.41	2.00	0.00	1.00	0.00
48.99	64.98	2.00	0.00	1.00	0.00	49.05	62.48	2.00	0.00	1.00	0.00
49.12	59.74	2.00	0.00	1.00	0.00	49.18	57.20	2.00	0.00	1.00	0.00
49.27	55.71	2.00	0.00	1.00	0.00	49.32	54.42	2.00	0.00	1.00	0.00
49.42	53.88	2.00	0.00	1.00	0.00	49.48	53.63	2.00	0.00	1.00	0.00
49.56	54.09	2.00	0.00	1.00	0.00	49.66	55.25	2.00	0.00	1.00	0.00
49.76	56.33	2.00	0.00	1.00	0.00	49.85	54.00	2.00	0.00	1.00	0.00
49.99	51.28	2.00	0.00	1.00	0.00	50.09	49.07	2.00	0.00	1.00	0.00
50.21	50.39	2.00	0.00	1.00	0.00	50.24	50.47	2.00	0.00	1.00	0.00
50.29	49.66	2.00	0.00	1.00	0.00	50.38	48.82	2.00	0.00	1.00	0.00
50.47	48.36	2.00	0.00	1.00	0.00	50.52	48.61	2.00	0.00	1.00	0.00
50.62	49.09	2.00	0.00	1.00	0.00	50.66	49.58	2.00	0.00	1.00	0.00
50.76	50.11	2.00	0.00	1.00	0.00	50.83	51.29	2.00	0.00	1.00	0.00
50.91	53.36	2.00	0.00	1.00	0.00	51.00	55.29	2.00	0.00	1.00	0.00
51.06	56.99	2.00	0.00	1.00	0.00	51.15	61.08	2.00	0.00	1.00	0.00
51.24	67.57	2.00	0.00	1.00	0.00	51.31	75.27	2.00	0.00	1.00	0.00
51.39	80.15	2.00	0.00	1.00	0.00	51.48	82.64	2.00	0.00	1.00	0.00
51.58	87.30	2.00	0.00	1.00	0.00	51.68	91.85	2.00	0.00	1.00	0.00
51.77	100.06	2.00	0.00	1.00	0.00	51.90	106.47	2.00	0.00	1.00	0.00
52.01	110.20	2.00	0.00	1.00	0.00	52.11	121.05	2.00	0.00	1.00	0.00
52.26	131.90	2.00	0.00	1.00	0.00	52.30	146.55	2.00	0.00	1.00	0.00
52.33	162.63	2.00	0.00	1.00	0.00	52.35	192.22	2.00	0.00	1.00	0.00
52.40	209.95	2.00	0.00	1.00	0.00	52.45	216.58	2.00	0.00	1.00	0.00
52.50	229.89	2.00	0.00	1.00	0.00	52.55	248.98	2.00	0.00	1.00	0.00
52.60	273.15	2.00	0.00	1.00	0.00	52.65	289.64	2.00	0.00	1.00	0.00
52.71	297.95	2.00	0.00	1.00	0.00	52.77	303.79	2.00	0.00	1.00	0.00
52.82	312.99	2.00	0.00	1.00	0.00	52.88	323.84	2.00	0.00	1.00	0.00
52.93	331.46	2.00	0.00	1.00	0.00	52.98	338.95	2.00	0.00	1.00	0.00
53.03	340.39	2.00	0.00	1.00	0.00	53.08	340.01	2.00	0.00	1.00	0.00
53.12	335.78	2.00	0.00	1.00	0.00	53.17	333.99	2.00	0.00	1.00	0.00
53.23	335.19	2.00	0.00	1.00	0.00	53.28	332.45	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
53.37	327.80	2.00	0.00	1.00	0.00	53.42	325.17	2.00	0.00	1.00	0.00
53.46	326.50	2.00	0.00	1.00	0.00	53.53	333.09	2.00	0.00	1.00	0.00
53.61	331.84	2.00	0.00	1.00	0.00	53.62	323.39	2.00	0.00	1.00	0.00
53.65	318.67	2.00	0.00	1.00	0.00	53.67	317.12	2.00	0.00	1.00	0.00
53.70	323.95	2.00	0.00	1.00	0.00	53.74	323.26	2.00	0.00	1.00	0.00
53.76	323.74	2.00	0.00	1.00	0.00	53.80	322.06	2.00	0.00	1.00	0.00
53.84	320.07	2.00	0.00	1.00	0.00	53.90	320.12	2.00	0.00	1.00	0.00
53.91	315.61	2.00	0.00	1.00	0.00	53.95	317.38	2.00	0.00	1.00	0.00
53.96	320.83	2.00	0.00	1.00	0.00	53.98	332.48	2.00	0.00	1.00	0.00
53.99	333.50	2.00	0.00	1.00	0.00	54.01	327.46	2.00	0.00	1.00	0.00
54.02	320.31	2.00	0.00	1.00	0.00	54.03	305.74	2.00	0.00	1.00	0.00
54.04	276.21	2.00	0.00	1.00	0.00	54.05	260.14	2.00	0.00	1.00	0.00
54.09	254.46	2.00	0.00	1.00	0.00	54.10	254.57	2.00	0.00	1.00	0.00
54.13	254.64	2.00	0.00	1.00	0.00	54.14	254.59	2.00	0.00	1.00	0.00
54.19	255.77	2.00	0.00	1.00	0.00	54.19	258.95	2.00	0.00	1.00	0.00
54.24	259.93	2.00	0.00	1.00	0.00	54.29	249.88	2.00	0.00	1.00	0.00
54.33	261.31	2.00	0.00	1.00	0.00	54.38	272.80	2.00	0.00	1.00	0.00
54.39	282.62	2.00	0.00	1.00	0.00	54.43	291.66	2.00	0.00	1.00	0.00
54.48	299.32	2.00	0.00	1.00	0.00	54.52	306.76	2.00	0.00	1.00	0.00
54.58	316.20	2.00	0.00	1.00	0.00	54.62	323.46	2.00	0.00	1.00	0.00
54.65	333.00	2.00	0.00	1.00	0.00	54.67	343.41	2.00	0.00	1.00	0.00
54.71	362.60	2.00	0.00	1.00	0.00	54.77	374.21	2.00	0.00	1.00	0.00
54.81	387.19	2.00	0.00	1.00	0.00	54.85	387.70	2.00	0.00	1.00	0.00
54.86	390.48	2.00	0.00	1.00	0.00	54.87	387.26	2.00	0.00	1.00	0.00
54.91	387.35	2.00	0.00	1.00	0.00	54.96	389.17	2.00	0.00	1.00	0.00
55.00	386.89	2.00	0.00	1.00	0.00	55.01	382.82	2.00	0.00	1.00	0.00
55.05	373.47	2.00	0.00	1.00	0.00	55.10	357.87	2.00	0.00	1.00	0.00
55.12	331.72	2.00	0.00	1.00	0.00	55.13	313.58	2.00	0.00	1.00	0.00
55.14	309.22	2.00	0.00	1.00	0.00	55.19	316.75	2.00	0.00	1.00	0.00
55.20	316.38	2.00	0.00	1.00	0.00	55.25	308.48	2.00	0.00	1.00	0.00
55.29	299.55	2.00	0.00	1.00	0.00	55.33	284.92	2.00	0.00	1.00	0.00
55.38	263.59	2.00	0.00	1.00	0.00	55.48	240.38	2.00	0.00	1.00	0.00
55.57	227.87	2.00	0.00	1.00	0.00	55.63	237.94	2.00	0.00	1.00	0.00
55.72	244.53	2.00	0.00	1.00	0.00	55.80	260.68	2.00	0.00	1.00	0.00
55.86	259.76	2.00	0.00	1.00	0.00	55.97	288.32	2.00	0.00	1.00	0.00
56.01	306.20	2.00	0.00	1.00	0.00	56.06	186.61	2.00	0.00	1.00	0.00
56.11	194.57	2.00	0.00	1.00	0.00	56.15	203.27	2.00	0.00	1.00	0.00
56.20	209.60	2.00	0.00	1.00	0.00	56.27	210.15	2.00	0.00	1.00	0.00
56.27	210.45	2.00	0.00	1.00	0.00	56.30	203.39	2.00	0.00	1.00	0.00
56.33	205.64	2.00	0.00	1.00	0.00	56.35	205.00	2.00	0.00	1.00	0.00
56.40	211.31	2.00	0.00	1.00	0.00	56.41	211.76	2.00	0.00	1.00	0.00
56.44	215.53	2.00	0.00	1.00	0.00	56.49	219.75	2.00	0.00	1.00	0.00
56.54	226.71	2.00	0.00	1.00	0.00	56.58	232.85	2.00	0.00	1.00	0.00
56.59	236.93	2.00	0.00	1.00	0.00	56.64	239.07	2.00	0.00	1.00	0.00
56.69	241.29	2.00	0.00	1.00	0.00	56.73	245.40	2.00	0.00	1.00	0.00
56.78	245.38	2.00	0.00	1.00	0.00	56.83	239.22	2.00	0.00	1.00	0.00
56.88	230.32	2.00	0.00	1.00	0.00	56.89	223.03	2.00	0.00	1.00	0.00
56.95	217.71	2.00	0.00	1.00	0.00	57.01	209.81	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
57.07	202.70	2.00	0.00	1.00	0.00	57.11	194.25	2.00	0.00	1.00	0.00
57.17	187.56	2.00	0.00	1.00	0.00	57.26	179.66	2.00	0.00	1.00	0.00
57.31	171.06	2.00	0.00	1.00	0.00	57.37	162.50	2.00	0.00	1.00	0.00
57.45	152.96	2.00	0.00	1.00	0.00	57.51	140.63	1.75	0.00	1.00	0.00
57.53	131.27	1.50	0.00	1.00	0.00	57.59	124.87	1.35	0.25	1.00	0.00
57.63	124.05	1.33	0.25	1.00	0.00	57.68	121.66	1.28	0.25	1.00	0.00
57.73	120.01	1.24	0.36	1.00	0.00	57.78	117.62	1.19	0.36	1.00	0.00
57.86	111.55	1.08	0.51	1.00	0.01	57.92	100.97	2.00	0.00	1.00	0.00
57.98	89.82	2.00	0.00	1.00	0.00	58.06	95.51	2.00	0.00	1.00	0.00
58.12	92.39	2.00	0.00	1.00	0.00	58.21	88.73	2.00	0.00	1.00	0.00
58.26	85.71	2.00	0.00	1.00	0.00	58.35	81.38	2.00	0.00	1.00	0.00
58.41	74.91	2.00	0.00	1.00	0.00	58.50	70.73	2.00	0.00	1.00	0.00
58.56	67.27	2.00	0.00	1.00	0.00	58.64	74.61	2.00	0.00	1.00	0.00
58.73	81.15	2.00	0.00	1.00	0.00	58.80	87.16	2.00	0.00	1.00	0.00
58.84	91.44	2.00	0.00	1.00	0.00	58.85	91.06	2.00	0.00	1.00	0.00
58.93	87.49	2.00	0.00	1.00	0.00	58.98	82.49	2.00	0.00	1.00	0.00
59.02	79.02	2.00	0.00	1.00	0.00	59.12	77.74	2.00	0.00	1.00	0.00
59.17	78.34	2.00	0.00	1.00	0.00	59.27	80.06	2.00	0.00	1.00	0.00
59.31	82.31	2.00	0.00	1.00	0.00	59.41	84.40	2.00	0.00	1.00	0.00
59.46	85.91	2.00	0.00	1.00	0.00	59.55	86.53	2.00	0.00	1.00	0.00
59.65	82.12	2.00	0.00	1.00	0.00	59.70	78.48	2.00	0.00	1.00	0.00
59.80	75.77	2.00	0.00	1.00	0.00	59.89	79.29	2.00	0.00	1.00	0.00
59.94	82.68	2.00	0.00	1.00	0.00	60.01	85.21	2.00	0.00	1.00	0.00
60.02	85.70	2.00	0.00	1.00	0.00	60.08	84.70	2.00	0.00	1.00	0.00
60.12	83.40	2.00	0.00	1.00	0.00	60.17	81.32	2.00	0.00	1.00	0.00
60.27	76.99	2.00	0.00	1.00	0.00	60.31	71.83	2.00	0.00	1.00	0.00
60.37	67.16	2.00	0.00	1.00	0.00	60.46	64.16	2.00	0.00	1.00	0.00
60.51	61.05	2.00	0.00	1.00	0.00	60.61	59.48	2.00	0.00	1.00	0.00
60.65	58.49	2.00	0.00	1.00	0.00	60.75	58.52	2.00	0.00	1.00	0.00
60.81	58.52	2.00	0.00	1.00	0.00	60.89	58.14	2.00	0.00	1.00	0.00
60.94	58.37	2.00	0.00	1.00	0.00	61.03	59.27	2.00	0.00	1.00	0.00
61.09	59.56	2.00	0.00	1.00	0.00	61.19	59.09	2.00	0.00	1.00	0.00
61.24	58.48	2.00	0.00	1.00	0.00	61.33	59.55	2.00	0.00	1.00	0.00
61.38	65.92	2.00	0.00	1.00	0.00	61.47	73.50	2.00	0.00	1.00	0.00
61.53	81.14	2.00	0.00	1.00	0.00	61.62	81.97	2.00	0.00	1.00	0.00
61.70	82.73	2.00	0.00	1.00	0.00	61.77	84.93	2.00	0.00	1.00	0.00
61.86	89.66	2.00	0.00	1.00	0.00	61.95	94.89	2.00	0.00	1.00	0.00
61.97	96.91	2.00	0.00	1.00	0.00	62.01	99.66	2.00	0.00	1.00	0.00
62.10	99.23	2.00	0.00	1.00	0.00	62.24	89.92	2.00	0.00	1.00	0.00
62.34	71.54	2.00	0.00	1.00	0.00	62.49	64.77	2.00	0.00	1.00	0.00
62.54	69.68	2.00	0.00	1.00	0.00	62.66	73.33	2.00	0.00	1.00	0.00
62.74	77.94	2.00	0.00	1.00	0.00	62.87	80.99	2.00	0.00	1.00	0.00
62.92	82.65	2.00	0.00	1.00	0.00	63.03	83.41	2.00	0.00	1.00	0.00
63.15	83.38	2.00	0.00	1.00	0.00	63.26	82.35	2.00	0.00	1.00	0.00
63.37	80.92	2.00	0.00	1.00	0.00	63.45	78.49	2.00	0.00	1.00	0.00
63.54	76.31	2.00	0.00	1.00	0.00	63.61	73.61	2.00	0.00	1.00	0.00
63.69	69.47	2.00	0.00	1.00	0.00	63.79	67.77	2.00	0.00	1.00	0.00
63.89	66.74	2.00	0.00	1.00	0.00	63.98	71.48	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
64.07	71.91	2.00	0.00	1.00	0.00	64.15	76.48	2.00	0.00	1.00	0.00
64.23	77.68	2.00	0.00	1.00	0.00	64.26	78.26	2.00	0.00	1.00	0.00
64.29	78.14	2.00	0.00	1.00	0.00	64.33	74.86	2.00	0.00	1.00	0.00
64.43	70.78	2.00	0.00	1.00	0.00	64.47	66.07	2.00	0.00	1.00	0.00
64.53	64.15	2.00	0.00	1.00	0.00	64.62	63.40	2.00	0.00	1.00	0.00
64.72	63.23	2.00	0.00	1.00	0.00	64.78	63.74	2.00	0.00	1.00	0.00
64.86	65.01	2.00	0.00	1.00	0.00	64.96	68.31	2.00	0.00	1.00	0.00
65.06	71.61	2.00	0.00	1.00	0.00	65.11	74.58	2.00	0.00	1.00	0.00
65.21	75.90	2.00	0.00	1.00	0.00	65.31	76.26	2.00	0.00	1.00	0.00
65.40	72.77	2.00	0.00	1.00	0.00	65.50	67.97	2.00	0.00	1.00	0.00
65.58	63.13	2.00	0.00	1.00	0.00	65.68	61.17	2.00	0.00	1.00	0.00
65.78	60.45	2.00	0.00	1.00	0.00	65.84	59.69	2.00	0.00	1.00	0.00
65.86	59.62	2.00	0.00	1.00	0.00	65.87	59.36	2.00	0.00	1.00	0.00
65.98	59.09	2.00	0.00	1.00	0.00	66.10	60.13	2.00	0.00	1.00	0.00
66.21	62.32	2.00	0.00	1.00	0.00	66.34	63.01	2.00	0.00	1.00	0.00
66.48	63.55	2.00	0.00	1.00	0.00	66.62	62.45	2.00	0.00	1.00	0.00
66.68	64.07	2.00	0.00	1.00	0.00	66.87	67.94	2.00	0.00	1.00	0.00
66.96	73.89	2.00	0.00	1.00	0.00	67.11	78.15	2.00	0.00	1.00	0.00
67.21	76.60	2.00	0.00	1.00	0.00	67.35	73.18	2.00	0.00	1.00	0.00
67.45	77.86	2.00	0.00	1.00	0.00	67.59	88.71	2.00	0.00	1.00	0.00
67.68	83.67	2.00	0.00	1.00	0.00	67.83	74.68	2.00	0.00	1.00	0.00
67.92	88.64	2.00	0.00	1.00	0.00	68.02	99.35	2.00	0.00	1.00	0.00
68.07	103.71	2.00	0.00	1.00	0.00	68.16	105.26	2.00	0.00	1.00	0.00
68.26	106.54	2.00	0.00	1.00	0.00	68.35	106.44	2.00	0.00	1.00	0.00
68.45	105.37	2.00	0.00	1.00	0.00	68.55	103.72	2.00	0.00	1.00	0.00
68.65	98.57	2.00	0.00	1.00	0.00	68.78	94.35	2.00	0.00	1.00	0.00
68.78	90.91	2.00	0.00	1.00	0.00	68.79	89.70	2.00	0.00	1.00	0.00
68.83	89.08	2.00	0.00	1.00	0.00	68.93	88.59	2.00	0.00	1.00	0.00
68.98	89.18	2.00	0.00	1.00	0.00	69.04	89.05	2.00	0.00	1.00	0.00
69.12	89.10	2.00	0.00	1.00	0.00	69.22	88.23	2.00	0.00	1.00	0.00
69.28	86.25	2.00	0.00	1.00	0.00	69.36	83.22	2.00	0.00	1.00	0.00
69.45	79.21	2.00	0.00	1.00	0.00	69.60	75.34	2.00	0.00	1.00	0.00
69.70	72.05	2.00	0.00	1.00	0.00	69.80	70.68	2.00	0.00	1.00	0.00
69.89	70.30	2.00	0.00	1.00	0.00	69.98	69.82	2.00	0.00	1.00	0.00
70.08	67.53	2.00	0.00	1.00	0.00	70.18	63.51	2.00	0.00	1.00	0.00
70.32	61.16	2.00	0.00	1.00	0.00	70.42	66.77	2.00	0.00	1.00	0.00
70.54	74.19	2.00	0.00	1.00	0.00	70.66	75.54	2.00	0.00	1.00	0.00
70.75	72.70	2.00	0.00	1.00	0.00	70.80	66.71	2.00	0.00	1.00	0.00
70.89	59.87	2.00	0.00	1.00	0.00	70.99	53.00	2.00	0.00	1.00	0.00
71.08	49.46	2.00	0.00	1.00	0.00	71.17	47.79	2.00	0.00	1.00	0.00
71.23	47.05	2.00	0.00	1.00	0.00	71.33	46.20	2.00	0.00	1.00	0.00
71.42	44.64	2.00	0.00	1.00	0.00	71.52	43.06	2.00	0.00	1.00	0.00
71.58	44.01	2.00	0.00	1.00	0.00	71.67	47.43	2.00	0.00	1.00	0.00
71.81	50.76	2.00	0.00	1.00	0.00	71.82	52.55	2.00	0.00	1.00	0.00
71.86	52.82	2.00	0.00	1.00	0.00	71.91	52.95	2.00	0.00	1.00	0.00
71.97	53.27	2.00	0.00	1.00	0.00	72.05	53.72	2.00	0.00	1.00	0.00
72.10	54.35	2.00	0.00	1.00	0.00	72.20	54.79	2.00	0.00	1.00	0.00
72.25	55.49	2.00	0.00	1.00	0.00	72.34	56.94	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
72.44	58.80	2.00	0.00	1.00	0.00	72.53	60.40	2.00	0.00	1.00	0.00
72.63	61.13	2.00	0.00	1.00	0.00	72.69	61.14	2.00	0.00	1.00	0.00
72.82	60.87	2.00	0.00	1.00	0.00	72.92	60.05	2.00	0.00	1.00	0.00
73.06	59.27	2.00	0.00	1.00	0.00	73.16	59.57	2.00	0.00	1.00	0.00
73.30	60.65	2.00	0.00	1.00	0.00	73.35	61.53	2.00	0.00	1.00	0.00
73.38	61.23	2.00	0.00	1.00	0.00	73.47	60.67	2.00	0.00	1.00	0.00
73.53	60.20	2.00	0.00	1.00	0.00	73.62	59.95	2.00	0.00	1.00	0.00
73.71	60.28	2.00	0.00	1.00	0.00	73.77	61.46	2.00	0.00	1.00	0.00
73.86	63.08	2.00	0.00	1.00	0.00	73.96	64.61	2.00	0.00	1.00	0.00
74.06	65.59	2.00	0.00	1.00	0.00	74.13	66.22	2.00	0.00	1.00	0.00
74.24	66.66	2.00	0.00	1.00	0.00	74.34	67.26	2.00	0.00	1.00	0.00
74.44	67.81	2.00	0.00	1.00	0.00	74.58	67.28	2.00	0.00	1.00	0.00
74.68	62.80	2.00	0.00	1.00	0.00	74.80	58.74	2.00	0.00	1.00	0.00
74.92	56.43	2.00	0.00	1.00	0.00	75.07	58.35	2.00	0.00	1.00	0.00
75.08	59.34	2.00	0.00	1.00	0.00	75.11	59.53	2.00	0.00	1.00	0.00
75.16	60.28	2.00	0.00	1.00	0.00	75.25	61.74	2.00	0.00	1.00	0.00
75.32	63.23	2.00	0.00	1.00	0.00	75.40	63.73	2.00	0.00	1.00	0.00
75.50	62.77	2.00	0.00	1.00	0.00	75.59	60.75	2.00	0.00	1.00	0.00
75.69	58.60	2.00	0.00	1.00	0.00	75.78	56.46	2.00	0.00	1.00	0.00
75.88	54.66	2.00	0.00	1.00	0.00	75.96	52.90	2.00	0.00	1.00	0.00
76.05	51.65	2.00	0.00	1.00	0.00	76.14	51.00	2.00	0.00	1.00	0.00
76.26	51.09	2.00	0.00	1.00	0.00	76.36	51.38	2.00	0.00	1.00	0.00
76.41	51.50	2.00	0.00	1.00	0.00	76.51	51.17	2.00	0.00	1.00	0.00
76.65	51.04	2.00	0.00	1.00	0.00	76.72	51.12	2.00	0.00	1.00	0.00
76.79	51.39	2.00	0.00	1.00	0.00	76.89	53.53	2.00	0.00	1.00	0.00
76.98	61.89	2.00	0.00	1.00	0.00	77.08	69.60	2.00	0.00	1.00	0.00
77.18	77.29	2.00	0.00	1.00	0.00	77.28	84.26	2.00	0.00	1.00	0.00
77.37	93.62	2.00	0.00	1.00	0.00	77.42	100.64	2.00	0.00	1.00	0.00
77.42	104.44	2.00	0.00	1.00	0.00	77.44	107.05	2.00	0.00	1.00	0.00
77.48	110.31	2.00	0.00	1.00	0.00	77.52	113.00	2.00	0.00	1.00	0.00
77.54	114.44	2.00	0.00	1.00	0.00	77.57	115.54	2.00	0.00	1.00	0.00
77.62	115.93	2.00	0.00	1.00	0.00	77.65	115.64	2.00	0.00	1.00	0.00
77.67	113.32	2.00	0.00	1.00	0.00	77.71	111.24	2.00	0.00	1.00	0.00
77.71	107.78	2.00	0.00	1.00	0.00	77.76	104.25	2.00	0.00	1.00	0.00
77.81	98.88	2.00	0.00	1.00	0.00	77.90	94.60	2.00	0.00	1.00	0.00
77.95	92.44	2.00	0.00	1.00	0.00	78.01	91.29	2.00	0.00	1.00	0.00
78.10	89.37	2.00	0.00	1.00	0.00	78.16	84.71	2.00	0.00	1.00	0.00
78.24	79.05	2.00	0.00	1.00	0.00	78.29	73.14	2.00	0.00	1.00	0.00
78.39	69.27	2.00	0.00	1.00	0.00	78.47	68.51	2.00	0.00	1.00	0.00
78.53	71.72	2.00	0.00	1.00	0.00	78.62	77.71	2.00	0.00	1.00	0.00
78.68	84.02	2.00	0.00	1.00	0.00	78.69	89.57	2.00	0.00	1.00	0.00
78.78	95.10	2.00	0.00	1.00	0.00	78.81	102.04	2.00	0.00	1.00	0.00
78.92	107.35	2.00	0.00	1.00	0.00	79.03	107.43	2.00	0.00	1.00	0.00
79.16	99.26	2.00	0.00	1.00	0.00	79.26	88.45	2.00	0.00	1.00	0.00
79.35	83.92	2.00	0.00	1.00	0.00	79.45	85.78	2.00	0.00	1.00	0.00
79.54	89.58	2.00	0.00	1.00	0.00	79.64	91.91	2.00	0.00	1.00	0.00
79.74	93.85	2.00	0.00	1.00	0.00	79.88	94.86	2.00	0.00	1.00	0.00
79.98	95.73	2.00	0.00	1.00	0.00	80.12	95.14	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
80.22	91.22	2.00	0.00	1.00	0.00	80.36	86.07	2.00	0.00	1.00	0.00
80.46	81.11	2.00	0.00	1.00	0.00	80.60	77.21	2.00	0.00	1.00	0.00
80.70	74.37	2.00	0.00	1.00	0.00	80.83	72.04	2.00	0.00	1.00	0.00
80.94	69.62	2.00	0.00	1.00	0.00	81.01	67.91	2.00	0.00	1.00	0.00
81.04	66.50	2.00	0.00	1.00	0.00	81.09	65.97	2.00	0.00	1.00	0.00
81.13	66.04	2.00	0.00	1.00	0.00	81.18	67.98	2.00	0.00	1.00	0.00
81.23	72.13	2.00	0.00	1.00	0.00	81.28	77.64	2.00	0.00	1.00	0.00
81.33	84.19	2.00	0.00	1.00	0.00	81.37	92.48	2.00	0.00	1.00	0.00
81.42	100.46	2.00	0.00	1.00	0.00	81.47	106.15	2.00	0.00	1.00	0.00
81.52	109.13	2.00	0.00	1.00	0.00	81.56	111.09	2.00	0.00	1.00	0.00
81.61	112.75	2.00	0.00	1.00	0.00	81.64	114.41	2.00	0.00	1.00	0.00
81.70	116.91	2.00	0.00	1.00	0.00	81.75	118.94	2.00	0.00	1.00	0.00
81.79	119.14	2.00	0.00	1.00	0.00	81.82	116.62	2.00	0.00	1.00	0.00
81.86	112.49	2.00	0.00	1.00	0.00	81.91	107.66	2.00	0.00	1.00	0.00
81.95	102.27	2.00	0.00	1.00	0.00	82.00	95.81	2.00	0.00	1.00	0.00
82.09	89.46	2.00	0.00	1.00	0.00	82.15	84.64	2.00	0.00	1.00	0.00
82.19	81.03	2.00	0.00	1.00	0.00	82.26	77.56	2.00	0.00	1.00	0.00
82.34	74.17	2.00	0.00	1.00	0.00	82.39	71.81	2.00	0.00	1.00	0.00
82.48	69.97	2.00	0.00	1.00	0.00	82.58	68.21	2.00	0.00	1.00	0.00
82.62	66.60	2.00	0.00	1.00	0.00	82.70	65.56	2.00	0.00	1.00	0.00
82.77	64.46	2.00	0.00	1.00	0.00	82.87	64.01	2.00	0.00	1.00	0.00
82.96	63.38	2.00	0.00	1.00	0.00	83.06	63.34	2.00	0.00	1.00	0.00
83.16	63.10	2.00	0.00	1.00	0.00	83.25	62.94	2.00	0.00	1.00	0.00
83.34	62.57	2.00	0.00	1.00	0.00	83.44	63.55	2.00	0.00	1.00	0.00
83.54	64.89	2.00	0.00	1.00	0.00	83.64	66.49	2.00	0.00	1.00	0.00
83.73	68.29	2.00	0.00	1.00	0.00	83.83	70.46	2.00	0.00	1.00	0.00
83.85	73.38	2.00	0.00	1.00	0.00	83.89	75.93	2.00	0.00	1.00	0.00
83.94	81.26	2.00	0.00	1.00	0.00	84.04	85.92	2.00	0.00	1.00	0.00
84.09	90.10	2.00	0.00	1.00	0.00	84.13	91.94	2.00	0.00	1.00	0.00
84.18	93.61	2.00	0.00	1.00	0.00	84.25	94.85	2.00	0.00	1.00	0.00
84.33	95.60	2.00	0.00	1.00	0.00	84.37	95.90	2.00	0.00	1.00	0.00
84.46	94.98	2.00	0.00	1.00	0.00	84.52	93.43	2.00	0.00	1.00	0.00
84.57	91.27	2.00	0.00	1.00	0.00	84.67	90.00	2.00	0.00	1.00	0.00
84.71	89.72	2.00	0.00	1.00	0.00	84.81	90.86	2.00	0.00	1.00	0.00
84.86	92.62	2.00	0.00	1.00	0.00	84.91	94.03	2.00	0.00	1.00	0.00
85.00	94.63	2.00	0.00	1.00	0.00	85.05	93.94	2.00	0.00	1.00	0.00
85.15	92.30	2.00	0.00	1.00	0.00	85.19	89.13	2.00	0.00	1.00	0.00
85.29	85.98	2.00	0.00	1.00	0.00	85.35	83.14	2.00	0.00	1.00	0.00
85.42	81.54	2.00	0.00	1.00	0.00	85.48	80.45	2.00	0.00	1.00	0.00
85.55	79.50	2.00	0.00	1.00	0.00	85.63	78.76	2.00	0.00	1.00	0.00
85.68	78.25	2.00	0.00	1.00	0.00	85.77	78.03	2.00	0.00	1.00	0.00
85.82	78.34	2.00	0.00	1.00	0.00	85.89	78.79	2.00	0.00	1.00	0.00
85.96	79.01	2.00	0.00	1.00	0.00	86.03	78.44	2.00	0.00	1.00	0.00
86.11	77.40	2.00	0.00	1.00	0.00	86.16	76.21	2.00	0.00	1.00	0.00
86.25	75.81	2.00	0.00	1.00	0.00	86.36	74.32	2.00	0.00	1.00	0.00
86.50	72.85	2.00	0.00	1.00	0.00	86.51	70.91	2.00	0.00	1.00	0.00
86.52	69.58	2.00	0.00	1.00	0.00	86.57	66.80	2.00	0.00	1.00	0.00
86.65	63.50	2.00	0.00	1.00	0.00	86.71	60.73	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
86.80	59.11	2.00	0.00	1.00	0.00	86.90	57.42	2.00	0.00	1.00	0.00
86.99	55.74	2.00	0.00	1.00	0.00	87.04	54.32	2.00	0.00	1.00	0.00
87.14	53.51	2.00	0.00	1.00	0.00	87.19	53.36	2.00	0.00	1.00	0.00
87.28	54.40	2.00	0.00	1.00	0.00	87.38	55.67	2.00	0.00	1.00	0.00
87.43	56.85	2.00	0.00	1.00	0.00	87.52	57.36	2.00	0.00	1.00	0.00
87.61	57.58	2.00	0.00	1.00	0.00	87.66	57.47	2.00	0.00	1.00	0.00
87.76	57.12	2.00	0.00	1.00	0.00	87.84	56.58	2.00	0.00	1.00	0.00
87.91	56.08	2.00	0.00	1.00	0.00	88.00	55.54	2.00	0.00	1.00	0.00
88.11	55.23	2.00	0.00	1.00	0.00	88.19	55.01	2.00	0.00	1.00	0.00
88.25	54.79	2.00	0.00	1.00	0.00	88.34	54.27	2.00	0.00	1.00	0.00
88.44	53.59	2.00	0.00	1.00	0.00	88.54	52.93	2.00	0.00	1.00	0.00
88.64	52.52	2.00	0.00	1.00	0.00	88.72	52.42	2.00	0.00	1.00	0.00
88.82	52.53	2.00	0.00	1.00	0.00	88.91	52.79	2.00	0.00	1.00	0.00
89.01	53.02	2.00	0.00	1.00	0.00	89.10	53.22	2.00	0.00	1.00	0.00
89.19	52.91	2.00	0.00	1.00	0.00	89.30	50.44	2.00	0.00	1.00	0.00
89.39	48.98	2.00	0.00	1.00	0.00	89.49	49.49	2.00	0.00	1.00	0.00
89.59	52.76	2.00	0.00	1.00	0.00	89.69	54.90	2.00	0.00	1.00	0.00
89.73	55.86	2.00	0.00	1.00	0.00	89.78	56.23	2.00	0.00	1.00	0.00
89.83	56.56	2.00	0.00	1.00	0.00	89.88	57.05	2.00	0.00	1.00	0.00
89.93	57.77	2.00	0.00	1.00	0.00	90.00	58.79	2.00	0.00	1.00	0.00
90.07	59.82	2.00	0.00	1.00	0.00	90.12	61.24	2.00	0.00	1.00	0.00
90.22	62.84	2.00	0.00	1.00	0.00	90.27	65.70	2.00	0.00	1.00	0.00
90.36	68.34	2.00	0.00	1.00	0.00	90.46	70.27	2.00	0.00	1.00	0.00
90.50	71.01	2.00	0.00	1.00	0.00	90.61	71.39	2.00	0.00	1.00	0.00
90.66	71.12	2.00	0.00	1.00	0.00	90.75	69.74	2.00	0.00	1.00	0.00
90.84	67.94	2.00	0.00	1.00	0.00	90.89	66.20	2.00	0.00	1.00	0.00
90.99	65.12	2.00	0.00	1.00	0.00	91.04	64.21	2.00	0.00	1.00	0.00
91.14	63.69	2.00	0.00	1.00	0.00	91.22	63.19	2.00	0.00	1.00	0.00
91.28	62.55	2.00	0.00	1.00	0.00	91.37	61.75	2.00	0.00	1.00	0.00
91.47	60.75	2.00	0.00	1.00	0.00	91.61	60.19	2.00	0.00	1.00	0.00
91.71	59.97	2.00	0.00	1.00	0.00	91.81	60.03	2.00	0.00	1.00	0.00
91.87	59.68	2.00	0.00	1.00	0.00	92.00	57.50	2.00	0.00	1.00	0.00
92.10	55.77	2.00	0.00	1.00	0.00	92.20	54.98	2.00	0.00	1.00	0.00
92.33	56.37	2.00	0.00	1.00	0.00	92.38	57.43	2.00	0.00	1.00	0.00
92.43	57.96	2.00	0.00	1.00	0.00	92.48	58.57	2.00	0.00	1.00	0.00
92.56	59.09	2.00	0.00	1.00	0.00	92.63	59.41	2.00	0.00	1.00	0.00
92.67	59.42	2.00	0.00	1.00	0.00	92.72	59.38	2.00	0.00	1.00	0.00
92.77	59.37	2.00	0.00	1.00	0.00	92.86	59.49	2.00	0.00	1.00	0.00
92.92	59.88	2.00	0.00	1.00	0.00	92.97	61.03	2.00	0.00	1.00	0.00
93.05	62.12	2.00	0.00	1.00	0.00	93.10	63.07	2.00	0.00	1.00	0.00
93.16	63.28	2.00	0.00	1.00	0.00	93.25	63.20	2.00	0.00	1.00	0.00
93.35	62.84	2.00	0.00	1.00	0.00	93.40	62.27	2.00	0.00	1.00	0.00
93.49	61.82	2.00	0.00	1.00	0.00	93.56	61.55	2.00	0.00	1.00	0.00
93.64	61.65	2.00	0.00	1.00	0.00	93.73	62.81	2.00	0.00	1.00	0.00
93.83	64.72	2.00	0.00	1.00	0.00	93.88	67.85	2.00	0.00	1.00	0.00
93.97	70.35	2.00	0.00	1.00	0.00	94.07	72.95	2.00	0.00	1.00	0.00
94.17	75.57	2.00	0.00	1.00	0.00	94.26	76.60	2.00	0.00	1.00	0.00
94.36	81.75	2.00	0.00	1.00	0.00	94.45	87.02	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
94.55	91.74	2.00	0.00	1.00	0.00	94.64	89.52	2.00	0.00	1.00	0.00
94.72	85.22	2.00	0.00	1.00	0.00	94.74	79.85	2.00	0.00	1.00	0.00
94.77	76.98	2.00	0.00	1.00	0.00	94.85	74.39	2.00	0.00	1.00	0.00
94.90	75.17	2.00	0.00	1.00	0.00	94.95	77.89	2.00	0.00	1.00	0.00
95.01	85.22	2.00	0.00	1.00	0.00	95.09	94.37	2.00	0.00	1.00	0.00
95.14	107.02	2.00	0.00	1.00	0.00	95.23	117.34	2.00	0.00	1.00	0.00
95.29	126.89	2.00	0.00	1.00	0.00	95.38	131.69	2.00	0.00	1.00	0.00
95.43	133.43	2.00	0.00	1.00	0.00	95.52	132.50	2.00	0.00	1.00	0.00
95.57	128.95	2.00	0.00	1.00	0.00	95.67	123.49	2.00	0.00	1.00	0.00
95.77	118.72	2.00	0.00	1.00	0.00	95.86	118.80	2.00	0.00	1.00	0.00
95.95	116.56	2.00	0.00	1.00	0.00	96.03	118.40	2.00	0.00	1.00	0.00
96.11	118.64	2.00	0.00	1.00	0.00	96.20	124.65	2.00	0.00	1.00	0.00
96.30	125.73	2.00	0.00	1.00	0.00	96.39	124.50	2.00	0.00	1.00	0.00
96.50	120.31	2.00	0.00	1.00	0.00	96.59	106.72	2.00	0.00	1.00	0.00
96.69	91.36	2.00	0.00	1.00	0.00	96.78	77.51	2.00	0.00	1.00	0.00
96.87	72.98	2.00	0.00	1.00	0.00	96.98	71.40	2.00	0.00	1.00	0.00
97.02	71.90	2.00	0.00	1.00	0.00	97.06	73.47	2.00	0.00	1.00	0.00
97.12	76.16	2.00	0.00	1.00	0.00	97.16	79.48	2.00	0.00	1.00	0.00
97.21	83.99	2.00	0.00	1.00	0.00	97.27	89.17	2.00	0.00	1.00	0.00
97.33	93.67	2.00	0.00	1.00	0.00	97.40	96.33	2.00	0.00	1.00	0.00
97.45	97.51	2.00	0.00	1.00	0.00	97.50	100.38	2.00	0.00	1.00	0.00
97.58	104.78	2.00	0.00	1.00	0.00	97.65	110.26	2.00	0.00	1.00	0.00
97.69	113.95	2.00	0.00	1.00	0.00	97.74	115.68	2.00	0.00	1.00	0.00
97.81	116.42	2.00	0.00	1.00	0.00	97.88	116.63	2.00	0.00	1.00	0.00
97.93	111.98	2.00	0.00	1.00	0.00	98.03	97.35	2.00	0.00	1.00	0.00
98.15	83.50	2.00	0.00	1.00	0.00	98.21	78.05	2.00	0.00	1.00	0.00
98.32	80.19	2.00	0.00	1.00	0.00	98.42	85.96	2.00	0.00	1.00	0.00
98.47	79.73	2.00	0.00	1.00	0.00	98.57	88.75	2.00	0.00	1.00	0.00
98.70	94.00	2.00	0.00	1.00	0.00	98.78	92.13	2.00	0.00	1.00	0.00
98.85	84.79	2.00	0.00	1.00	0.00	98.86	76.77	2.00	0.00	1.00	0.00
98.92	73.26	2.00	0.00	1.00	0.00	98.98	72.24	2.00	0.00	1.00	0.00
99.03	70.12	2.00	0.00	1.00	0.00	99.11	63.67	2.00	0.00	1.00	0.00
99.18	74.69	2.00	0.00	1.00	0.00	99.23	73.25	2.00	0.00	1.00	0.00
99.32	76.01	2.00	0.00	1.00	0.00	99.37	83.05	2.00	0.00	1.00	0.00
99.45	90.04	2.00	0.00	1.00	0.00	99.56	96.01	2.00	0.00	1.00	0.00
99.64	101.90	2.00	0.00	1.00	0.00	99.71	108.77	2.00	0.00	1.00	0.00
99.75	113.72	2.00	0.00	1.00	0.00	99.90	118.27	2.00	0.00	1.00	0.00
99.95	126.55	2.00	0.00	1.00	0.00	100.04	127.45	2.00	0.00	1.00	0.00
100.14	116.89	2.00	0.00	1.00	0.00	100.14	106.43	2.00	0.00	1.00	0.00
100.15	105.52	2.00	0.00	1.00	0.00	100.19	111.71	2.00	0.00	1.00	0.00
100.21	119.29	2.00	0.00	1.00	0.00	100.24	108.37	2.00	0.00	1.00	0.00
100.28	106.62	2.00	0.00	1.00	0.00	100.31	-1.00	2.00	0.00	1.00	0.00
100.33	-1.00	2.00	0.00	1.00	0.00	100.38	-1.00	2.00	0.00	1.00	0.00
100.39	-1.00	2.00	0.00	1.00	0.00	100.43	-1.00	2.00	0.00	1.00	0.00
100.48	-1.00	2.00	0.00	1.00	0.00	100.53	-1.00	2.00	0.00	1.00	0.00
100.57	-1.00	2.00	0.00	1.00	0.00	100.60	-1.00	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)

Total estimated settlement: 1.07

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation (Robertson (2009) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.04	0.10	0.16	54.25	8.56	4.06	18.21	3.82
0.10	0.13	0.21	54.25	11.25	4.06	10.48	2.18
0.11	0.23	0.37	54.25	19.92	4.06	9.43	3.40
0.16	0.54	0.85	54.25	46.18	4.06	6.91	5.55
0.19	1.28	2.04	26.86	54.86	3.64	5.54	10.68
0.24	2.83	4.54	12.41	56.29	3.19	4.85	19.02
0.31	4.93	7.89	7.08	55.92	2.89	0.08	0.64
0.38	6.68	10.70	5.13	54.91	2.74	0.08	0.64
0.43	7.56	12.11	4.55	55.04	2.68	0.08	0.64
0.49	7.32	11.72	4.88	57.26	2.72	0.09	0.65
0.58	6.81	10.90	5.56	60.65	2.78	0.12	0.66
0.63	6.24	9.98	6.53	65.19	2.85	0.17	0.67
0.67	6.05	9.68	7.19	69.56	2.90	0.25	0.68
0.72	6.02	9.62	7.57	72.80	2.92	0.32	0.69
0.72	6.70	10.70	7.32	78.32	2.91	0.51	0.70
0.84	9.28	14.84	5.43	80.63	2.77	0.62	0.71
0.96	15.82	25.35	2.97	75.23	2.50	0.39	0.70
1.06	22.64	36.29	2.02	73.35	2.32	0.34	0.69
1.24	27.97	44.84	1.65	74.08	2.21	0.36	0.69
1.30	31.48	50.47	1.49	75.12	2.14	0.39	0.70
1.48	37.28	59.78	1.34	80.22	2.04	0.59	0.71
1.59	42.14	67.57	1.29	87.16	1.98	0.72	0.72
1.69	47.40	76.02	1.26	95.52	1.93	0.74	0.74
1.69	49.80	79.87	1.25	99.55	1.91	0.75	0.75
1.74	53.24	85.40	1.22	104.46	1.88	0.76	0.76
1.79	53.78	86.26	1.22	105.40	1.88	0.76	0.76
1.84	52.90	84.84	1.23	104.08	1.89	0.76	0.76
1.88	51.25	82.18	1.23	101.34	1.89	0.75	0.75
1.93	49.46	79.31	1.24	98.11	1.90	0.74	0.74
1.99	48.69	78.06	1.23	96.29	1.90	0.74	0.74
2.03	48.08	77.07	1.23	94.90	1.89	0.74	0.74
2.08	47.67	76.42	1.23	93.98	1.89	0.74	0.74
2.13	46.86	75.11	1.23	92.67	1.90	0.73	0.73
2.22	45.85	73.48	1.24	91.09	1.90	0.73	0.73
2.27	44.97	72.07	1.24	89.70	1.91	0.73	0.73
2.33	44.77	71.74	1.24	89.16	1.91	0.73	0.73
2.42	45.44	72.81	1.24	89.96	1.90	0.73	0.73
2.48	46.73	74.86	1.22	91.66	1.88	0.73	0.73
2.56	48.41	77.57	1.21	94.03	1.86	0.74	0.74
2.65	49.43	79.19	1.21	95.47	1.86	0.74	0.74
2.72	48.72	78.04	1.21	94.74	1.87	0.74	0.74
2.80	46.02	73.70	1.23	90.99	1.90	0.73	0.73
2.89	42.44	67.94	1.26	85.67	1.94	0.72	0.72
2.94	39.03	62.46	1.29	80.64	1.98	0.62	0.71
3.04	35.90	57.42	1.32	76.04	2.02	0.42	0.70
3.14	32.32	51.66	1.37	70.91	2.07	0.27	0.69
3.23	29.01	46.34	1.42	65.97	2.10	0.18	0.67
3.31	25.74	41.07	1.50	61.64	2.15	0.13	0.66

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.37	23.04	36.73	1.59	58.33	2.19	0.10	0.65
3.48	20.38	32.44	1.71	55.35	2.23	0.08	0.64
3.57	18.79	29.89	1.76	52.71	2.25	0.06	0.63
3.65	18.02	28.64	1.78	50.93	2.26	0.06	0.63
3.71	18.02	28.64	1.77	50.70	2.26	0.06	0.63
3.82	18.63	29.60	1.77	52.47	2.26	0.06	0.63
3.91	20.18	32.09	1.71	54.73	2.23	0.07	0.64
4.00	22.81	36.30	1.60	58.22	2.20	0.10	0.65
4.10	26.38	42.04	1.41	59.10	2.09	0.11	0.65
4.19	31.21	49.79	1.00	49.79	1.98	0.05	0.62
4.26	37.92	60.57	1.00	60.57	1.86	0.12	0.66
4.35	45.62	72.92	1.00	72.92	1.79	0.32	0.69
4.44	49.80	79.63	1.00	79.63	1.77	0.57	0.71
4.52	51.39	82.17	1.00	82.17	1.76	0.70	0.71
4.53	52.26	83.58	1.00	83.58	1.76	0.72	0.72
4.58	55.03	88.02	1.00	88.02	1.73	0.72	0.72
4.63	57.76	92.41	1.00	92.41	1.71	0.73	0.73
4.68	58.84	94.14	1.00	94.14	1.70	0.74	0.74
4.72	59.28	94.84	1.00	94.84	1.71	0.74	0.74
4.77	59.08	94.51	1.00	94.51	1.72	0.74	0.74
4.82	58.07	92.88	1.00	92.88	1.73	0.73	0.73
4.88	56.21	89.89	1.00	89.89	1.76	0.73	0.73
4.96	53.61	85.71	1.14	97.96	1.79	0.74	0.74
5.01	50.54	80.78	1.18	95.67	1.83	0.74	0.74
5.08	47.44	75.78	1.22	92.32	1.87	0.73	0.73
5.16	44.81	71.55	1.24	88.93	1.91	0.73	0.73
5.21	43.27	69.07	1.26	86.85	1.93	0.72	0.72
5.30	42.68	68.12	1.26	86.01	1.94	0.72	0.72
5.37	42.65	68.06	1.26	85.96	1.94	0.72	0.72
5.45	42.70	68.13	1.26	86.01	1.94	0.72	0.72
5.52	42.44	67.72	1.26	85.64	1.94	0.72	0.72
5.59	41.70	66.52	1.27	84.54	1.95	0.72	0.72
5.65	40.15	64.02	1.28	82.25	1.97	0.70	0.71
5.74	38.46	61.30	1.30	79.83	1.99	0.58	0.71
5.83	37.08	59.07	1.32	77.99	2.02	0.49	0.70
5.89	36.30	57.82	1.33	77.16	2.03	0.46	0.70
5.97	35.66	56.79	1.35	76.43	2.04	0.43	0.70
6.07	34.52	54.94	1.37	75.11	2.06	0.39	0.70
6.12	32.56	51.79	1.41	73.14	2.10	0.33	0.69
6.22	29.76	47.28	1.51	71.19	2.15	0.28	0.69
6.28	26.56	42.13	1.67	70.33	2.22	0.26	0.68
6.36	23.45	37.14	1.90	70.41	2.29	0.26	0.68
6.46	21.29	33.66	2.09	70.43	2.34	0.26	0.68
6.52	20.72	32.73	2.06	67.56	2.33	0.21	0.68
6.60	22.07	34.89	1.79	62.55	2.26	0.14	0.66
6.70	23.55	37.27	1.57	58.59	2.18	0.10	0.65
6.76	23.01	36.39	1.55	56.58	2.17	0.09	0.65
6.84	19.64	30.96	1.81	55.94	2.27	0.08	0.64

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.94	14.91	23.37	2.60	60.83	2.44	0.12	0.66
7.03	10.86	16.85	4.02	67.75	2.63	0.21	0.68
7.13	8.23	12.62	5.71	72.04	2.79	0.30	0.69
7.19	6.62	10.02	6.93	69.39	2.88	0.24	0.68
7.32	5.77	8.65	6.87	59.40	2.88	0.11	0.65
7.42	5.17	7.67	5.87	44.99	2.80	0.04	0.62
7.49	4.93	7.28	4.02	29.29	2.63	0.02	0.62
7.57	4.73	-1.00	1.00	-1.00	-1.00	0.00	0.00
7.66	4.56	-1.00	1.00	-1.00	-1.00	0.00	0.00
7.76	4.44	6.47	4.48	29.00	2.68	0.02	0.62
7.77	4.39	6.39	4.95	31.63	2.72	0.02	0.62
7.78	4.42	6.44	5.05	32.53	2.73	0.02	0.62
7.82	4.44	6.47	5.36	34.69	2.76	0.02	0.62
7.87	4.45	6.49	5.86	38.07	2.80	0.03	0.62
7.92	4.45	6.49	6.45	41.83	2.85	0.03	0.62
7.97	4.49	6.54	6.96	45.53	2.88	0.04	0.62
8.01	4.59	6.70	7.41	49.66	2.91	0.05	0.62
8.06	4.76	6.97	7.58	52.81	2.92	0.06	0.63
8.11	4.93	7.24	7.65	55.42	2.93	0.08	0.64
8.20	5.06	7.45	7.68	57.24	2.93	0.09	0.65
8.26	5.16	7.60	7.84	59.63	2.94	0.11	0.66
8.35	5.23	7.70	7.98	61.50	2.95	0.13	0.66
8.40	5.30	7.81	8.02	62.65	2.95	0.14	0.66
8.49	5.37	7.91	7.96	62.99	2.95	0.14	0.66
8.54	5.51	8.13	7.81	63.54	2.94	0.15	0.67
8.64	5.71	8.45	7.58	64.06	2.93	0.16	0.67
8.69	5.91	8.77	7.37	64.63	2.91	0.16	0.67
8.79	6.18	9.19	7.46	68.57	2.92	0.23	0.68
8.84	6.48	9.68	7.59	73.49	2.93	0.34	0.69
8.93	6.89	10.32	7.50	77.37	2.92	0.47	0.70
9.03	7.13	10.69	7.46	79.83	2.92	0.58	0.71
9.08	7.21	10.83	7.52	81.47	2.92	0.66	0.71
9.11	7.16	10.75	7.78	83.66	2.94	0.72	0.72
9.12	7.13	10.69	7.89	84.32	2.95	0.72	0.72
9.17	7.07	10.60	8.03	85.13	2.95	0.72	0.72
9.22	7.12	10.67	8.09	86.32	2.96	0.72	0.72
9.31	6.92	10.34	8.56	88.56	2.99	0.73	0.73
9.36	7.16	10.72	8.37	89.76	2.98	0.73	0.73
9.40	7.46	11.20	8.04	90.10	2.95	0.73	0.73
9.46	8.14	12.28	7.25	89.07	2.90	0.73	0.73
9.51	8.47	12.82	6.92	88.75	2.88	0.73	0.73
9.55	8.78	13.30	6.70	89.10	2.86	0.73	0.73
9.61	8.98	13.63	6.65	90.65	2.86	0.73	0.73
9.69	9.12	13.84	6.73	93.09	2.87	0.73	0.73
9.74	9.18	13.94	6.87	95.71	2.88	0.74	0.74
9.81	9.39	14.26	6.85	97.70	2.88	0.74	0.74
9.89	9.76	14.85	6.62	98.33	2.86	0.74	0.74
9.94	10.06	15.33	6.42	98.43	2.84	0.75	0.75

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.03	10.23	15.59	6.28	97.94	2.83	0.74	0.74
10.08	10.23	15.59	5.91	92.18	2.80	0.73	0.73
10.18	10.23	15.58	5.40	84.12	2.76	0.72	0.72
10.23	10.23	15.58	5.05	78.62	2.73	0.52	0.70
10.33	10.23	15.57	5.17	80.55	2.74	0.61	0.71
10.40	10.23	15.56	5.54	86.20	2.77	0.72	0.72
10.47	10.08	15.32	5.91	90.44	2.80	0.73	0.73
10.51	10.06	15.28	6.18	94.42	2.83	0.74	0.74
10.56	10.03	15.23	6.41	97.63	2.84	0.74	0.74
10.61	10.21	15.52	6.51	100.97	2.85	0.75	0.75
10.67	10.16	15.43	6.88	106.14	2.88	0.76	0.76
10.75	10.13	15.37	7.21	110.80	2.90	0.77	0.77
10.80	9.99	15.15	7.50	113.70	2.92	0.77	0.77
10.85	9.89	14.99	7.63	114.35	2.93	0.77	0.77
10.90	9.72	14.71	7.82	115.05	2.94	0.77	0.77
11.00	9.45	14.27	8.13	116.05	2.96	0.78	0.78
11.05	9.05	13.61	8.55	116.32	2.99	0.78	0.78
11.14	8.61	12.90	9.04	116.64	3.01	0.62	0.99
11.21	8.27	12.36	9.53	117.80	3.04	0.62	0.94
11.29	8.24	12.30	9.66	118.79	3.05	0.65	0.93
11.38	8.41	12.56	9.53	119.67	3.04	0.63	0.94
11.46	8.68	12.98	9.18	119.19	3.02	0.64	0.97
11.52	8.88	13.30	8.96	119.26	3.01	0.64	0.98
11.60	8.98	13.46	8.85	119.12	3.00	0.64	0.99
11.67	9.05	13.56	8.79	119.24	3.00	0.64	0.99
11.72	9.12	13.67	8.75	119.52	3.00	0.78	0.78
11.81	9.32	13.98	8.54	119.37	2.99	0.78	0.78
11.86	9.35	14.03	8.52	119.54	2.98	0.78	0.78
11.96	9.42	14.07	8.48	119.37	2.98	0.78	0.78
12.01	9.45	14.06	8.50	119.58	2.98	0.78	0.78
12.10	9.69	13.55	8.25	111.75	2.97	0.77	0.77
12.16	10.07	13.97	7.41	103.51	2.91	0.75	0.75
12.24	10.47	14.38	6.85	98.49	2.88	0.75	0.75
12.32	10.87	14.89	6.86	102.09	2.88	0.75	0.75
12.39	11.18	15.29	7.16	109.53	2.90	0.77	0.77
12.48	10.64	14.47	7.97	115.36	2.95	0.78	0.78
12.50	10.23	14.64	8.30	121.50	2.97	0.79	0.79
12.54	10.74	14.58	8.20	119.55	2.96	0.78	0.78
12.64	12.36	16.65	7.01	116.68	2.89	0.78	0.78
12.68	14.04	18.79	6.01	113.05	2.81	0.77	0.77
12.77	14.72	19.54	5.64	110.30	2.78	0.77	0.77
12.82	14.75	19.48	5.55	108.15	2.78	0.76	0.76
12.89	14.21	18.67	5.71	106.60	2.79	0.76	0.76
12.97	13.37	17.49	6.13	107.25	2.82	0.76	0.76
13.03	12.49	16.30	6.66	108.51	2.86	0.76	0.76
13.12	11.72	15.20	7.22	109.85	2.90	0.77	0.77
13.16	11.21	14.50	7.58	109.96	2.93	0.77	0.77
13.26	10.91	13.99	7.68	107.43	2.93	0.76	0.76

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.34	10.84	13.79	7.45	102.72	2.92	0.75	0.75
13.41	10.74	13.56	7.18	97.27	2.90	0.74	0.74
13.50	10.60	13.27	7.10	94.19	2.89	0.74	0.74
13.60	10.33	12.84	7.26	93.25	2.90	0.74	0.74
13.65	10.13	12.55	7.49	94.05	2.92	0.74	0.74
13.75	10.03	12.35	7.71	95.17	2.93	0.74	0.74
13.80	10.10	12.37	7.57	93.67	2.92	0.74	0.74
13.89	10.23	12.47	7.55	94.18	2.92	0.74	0.74
13.94	10.63	12.95	7.46	96.59	2.92	0.74	0.74
14.03	10.80	13.13	7.91	103.87	2.95	0.76	0.76
14.11	11.23	13.59	7.98	108.45	2.95	0.76	0.76
14.13	11.53	13.97	7.99	111.61	2.95	0.77	0.77
14.18	12.27	14.85	7.55	112.19	2.92	0.77	0.77
14.22	12.83	15.50	7.35	113.98	2.91	0.77	0.77
14.28	13.44	16.19	7.18	116.20	2.90	0.78	0.78
14.37	14.01	16.81	7.06	118.62	2.89	0.78	0.78
14.44	14.79	17.68	6.80	120.24	2.87	0.78	0.78
14.51	15.63	18.60	6.50	120.95	2.85	0.78	0.78
14.60	16.31	19.30	6.30	121.55	2.83	0.79	0.79
14.65	16.58	19.57	6.28	122.89	2.83	0.79	0.79
14.75	16.56	19.44	6.39	124.23	2.84	0.79	0.79
14.85	16.48	19.22	6.50	124.95	2.85	0.79	0.79
14.91	16.44	19.11	6.54	124.89	2.85	0.79	0.79
14.99	17.00	19.64	6.25	122.73	2.83	0.79	0.79
15.09	18.30	21.01	5.69	119.59	2.79	0.78	0.78
15.18	20.29	23.13	4.94	114.33	2.72	0.77	0.77
15.25	22.28	25.25	4.26	107.53	2.66	0.76	0.76
15.33	24.50	27.58	3.60	99.22	2.58	0.75	0.75
15.43	27.51	30.70	2.96	90.92	2.50	0.73	0.73
15.51	31.32	34.70	2.45	84.95	2.41	0.72	0.72
15.59	34.63	38.13	2.14	81.77	2.35	0.68	0.71
15.67	36.18	39.65	2.03	80.65	2.33	0.62	0.71
15.76	35.13	38.36	2.14	81.98	2.35	0.69	0.71
15.86	32.03	34.86	2.45	85.36	2.41	0.72	0.72
15.95	27.64	30.01	3.03	90.95	2.51	0.73	0.73
16.05	23.08	24.94	3.85	95.91	2.61	0.74	0.74
16.14	19.31	20.73	4.79	99.32	2.71	0.75	0.75
16.20	16.85	17.98	5.55	99.84	2.78	0.75	0.75
16.28	15.33	16.24	6.13	99.52	2.82	0.75	0.75
16.34	14.21	14.97	6.52	97.62	2.85	0.74	0.74
16.44	12.93	13.48	7.12	95.96	2.89	0.74	0.74
16.50	11.61	12.00	7.73	92.73	2.93	0.73	0.73
16.58	10.17	10.54	8.19	86.31	2.96	0.72	0.72
16.73	8.75	8.85	8.43	74.57	2.98	0.37	0.69
16.82	7.60	7.51	8.14	61.14	2.96	0.12	0.66
16.92	7.06	6.86	8.35	57.29	2.97	0.09	0.65
17.01	6.56	6.26	10.33	64.67	3.09	0.13	0.45
17.11	6.20	5.84	12.54	73.17	3.19	0.19	0.42

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
17.12	5.73	5.31	14.74	78.30	3.28	0.20	0.38
17.14	6.34	5.97	13.44	80.31	3.23	0.21	0.43
17.19	7.13	6.82	12.15	82.92	3.17	0.24	0.49
17.28	7.94	7.67	11.16	85.58	3.13	0.27	0.55
17.33	8.01	7.71	11.48	88.52	3.14	0.29	0.55
17.43	7.87	7.52	11.93	89.67	3.16	0.30	0.54
17.47	7.74	7.35	12.03	88.37	3.17	0.29	0.52
17.57	7.57	7.12	11.95	85.14	3.16	0.25	0.51
17.65	7.47	6.98	11.70	81.63	3.15	0.23	0.50
17.72	7.40	6.88	11.84	81.46	3.16	0.22	0.49
17.81	7.57	7.02	11.86	83.22	3.16	0.25	0.50
17.86	7.87	7.32	11.98	87.65	3.17	0.27	0.52
17.95	8.31	7.73	11.95	92.32	3.16	0.32	0.55
18.05	8.78	8.18	11.81	96.52	3.16	0.36	0.58
18.10	9.22	8.61	11.67	100.43	3.15	0.38	0.61
18.20	9.66	9.01	11.52	103.80	3.14	0.42	0.64
18.30	9.90	9.20	11.60	106.76	3.15	0.46	0.66
18.39	10.13	9.38	11.50	107.91	3.14	0.46	0.67
18.48	10.27	9.47	11.38	107.71	3.14	0.46	0.68
18.58	10.30	9.44	11.38	107.46	3.14	0.46	0.67
18.66	10.20	9.30	11.49	106.87	3.14	0.45	0.66
18.74	10.07	9.12	11.49	104.74	3.14	0.44	0.65
18.87	9.90	8.88	10.73	95.26	3.11	0.39	0.63
18.97	9.66	8.59	10.09	86.69	3.07	0.22	0.61
19.06	9.56	8.45	9.58	80.90	3.05	0.24	0.60
19.16	9.83	8.66	9.84	85.25	3.06	0.27	0.62
19.25	10.13	8.91	9.93	88.50	3.06	0.31	0.64
19.27	10.23	9.00	10.18	91.69	3.08	0.31	0.64
19.30	10.37	9.12	10.39	94.70	3.09	0.34	0.65
19.34	10.57	9.29	10.57	98.19	3.10	0.38	0.66
19.39	10.84	9.53	10.50	100.00	3.09	0.40	0.68
19.49	10.78	9.41	10.57	99.51	3.10	0.39	0.67
19.55	10.51	9.12	10.70	97.54	3.10	0.37	0.65
19.63	10.17	8.75	10.86	95.04	3.11	0.34	0.63
19.68	9.87	8.43	10.91	92.04	3.11	0.32	0.60
19.74	9.77	8.31	10.69	88.83	3.10	0.29	0.59
19.83	9.73	8.24	10.61	87.40	3.10	0.27	0.59
19.87	9.73	8.22	10.55	86.67	3.10	0.29	0.59
19.94	9.73	8.19	10.80	88.39	3.11	0.27	0.58
20.02	9.80	8.21	11.04	90.64	3.12	0.31	0.59
20.07	10.17	8.54	11.28	96.33	3.13	0.34	0.61
20.17	11.42	9.65	10.38	100.21	3.09	0.41	0.69
20.21	14.18	12.20	8.30	101.25	2.97	0.75	0.75
20.28	18.74	16.43	5.92	97.16	2.80	0.74	0.74
20.36	24.88	22.08	4.11	90.84	2.64	0.73	0.73
20.41	31.73	28.40	3.02	85.89	2.51	0.72	0.72
20.48	38.64	34.74	2.39	83.15	2.40	0.71	0.71
20.55	44.99	40.52	2.02	82.00	2.33	0.69	0.71

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
20.60	49.88	44.99	1.82	81.90	2.27	0.68	0.71
20.70	52.55	47.28	1.74	82.23	2.25	0.70	0.71
20.74	52.68	47.32	1.75	82.97	2.25	0.71	0.71
20.79	51.17	45.83	1.84	84.31	2.28	0.72	0.72
20.89	48.70	43.39	2.03	87.95	2.33	0.72	0.72
20.96	46.86	41.58	2.06	85.66	2.33	0.72	0.72
21.04	45.83	40.52	2.09	84.84	2.34	0.72	0.72
21.13	45.80	40.36	2.05	82.71	2.33	0.71	0.71
21.22	49.22	43.31	1.97	85.52	2.31	0.72	0.72
21.29	52.71	46.38	1.86	86.23	2.28	0.72	0.72
21.35	62.13	54.84	1.58	86.56	2.19	0.72	0.72
21.37	71.37	63.21	1.42	89.97	2.10	0.73	0.73
21.42	83.72	74.37	1.31	97.64	2.01	0.74	0.74
21.47	92.73	82.47	1.27	104.48	1.95	0.76	0.76
21.48	100.66	89.69	1.23	110.65	1.90	0.77	0.77
21.52	107.37	95.73	1.20	115.32	1.85	0.78	0.78
21.57	113.24	100.98	1.17	118.63	1.82	0.78	0.78
21.62	118.81	105.91	1.14	120.85	1.79	0.78	0.78
21.66	124.00	110.52	1.10	122.11	1.76	0.79	0.79
21.71	128.79	114.75	1.07	122.79	1.74	0.79	0.79
21.76	132.64	118.10	1.04	123.42	1.73	0.79	0.79
21.81	135.34	120.38	1.03	124.51	1.72	0.79	0.79
21.85	136.99	121.70	1.04	126.15	1.72	0.79	0.79
21.91	137.80	122.24	1.05	127.87	1.73	0.80	0.80
21.95	138.11	122.32	1.06	129.40	1.73	0.80	0.80
22.00	138.24	122.26	1.07	130.49	1.74	0.80	0.80
22.05	138.18	122.02	1.08	131.33	1.75	0.80	0.80
22.10	138.24	121.90	1.08	132.00	1.75	0.80	0.80
22.15	138.31	121.77	1.09	132.56	1.75	0.80	0.80
22.19	138.68	121.94	1.09	133.12	1.75	0.80	0.80
22.24	139.25	122.24	1.11	135.35	1.76	0.81	0.81
22.29	139.86	122.58	1.11	136.60	1.77	0.81	0.81
22.34	140.20	122.70	1.12	137.16	1.77	0.81	0.81
22.39	140.06	122.45	1.11	135.89	1.77	0.81	0.81
22.43	139.42	121.72	1.11	135.26	1.77	0.81	0.81
22.48	138.34	120.56	1.12	135.08	1.77	0.81	0.81
22.55	136.79	118.95	1.13	134.76	1.78	0.81	0.81
22.62	130.08	112.68	1.17	131.90	1.82	0.80	0.80
22.63	127.95	110.75	1.18	130.57	1.83	0.80	0.80
22.72	125.56	108.31	1.19	128.61	1.83	0.80	0.80
22.77	128.09	110.46	1.17	129.57	1.82	0.80	0.80
22.83	126.13	108.51	1.19	128.59	1.83	0.80	0.80
22.91	124.21	106.52	1.20	127.55	1.85	0.79	0.79
22.96	121.74	104.15	1.21	126.09	1.86	0.79	0.79
23.02	118.20	100.84	1.22	123.45	1.88	0.79	0.79
23.10	113.85	96.74	1.24	119.96	1.90	0.78	0.78
23.16	108.42	91.79	1.26	115.60	1.93	0.78	0.78
23.20	102.21	86.20	1.28	110.62	1.97	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
23.26	95.46	80.15	1.31	105.23	2.01	0.76	0.76
23.35	88.68	74.00	1.36	100.36	2.05	0.75	0.75
23.39	81.66	67.80	1.42	95.97	2.10	0.74	0.74
23.48	74.68	61.55	1.51	93.11	2.15	0.73	0.73
23.54	68.33	55.99	1.61	90.41	2.20	0.73	0.73
23.63	63.44	51.67	1.69	87.24	2.23	0.72	0.72
23.69	60.07	48.84	1.63	79.68	2.21	0.57	0.71
23.78	58.37	47.34	1.59	75.09	2.19	0.39	0.70
23.87	57.71	46.70	1.56	72.76	2.18	0.32	0.69
23.88	57.81	46.69	1.62	75.51	2.20	0.40	0.70
23.93	57.42	46.23	1.69	78.05	2.23	0.50	0.70
24.02	57.22	45.85	1.76	80.73	2.25	0.62	0.71
24.04	56.97	45.57	1.82	82.98	2.27	0.71	0.71
24.05	57.34	45.82	1.85	84.83	2.28	0.72	0.72
24.15	58.27	46.42	1.87	86.71	2.28	0.72	0.72
24.20	60.11	47.86	1.85	88.32	2.28	0.73	0.73
24.30	62.64	49.86	1.75	87.06	2.25	0.72	0.72
24.40	65.07	51.83	1.63	84.41	2.21	0.72	0.72
24.46	66.59	53.10	1.53	81.44	2.16	0.66	0.71
24.54	66.42	52.90	1.50	79.49	2.15	0.56	0.71
24.64	64.09	50.78	1.55	78.59	2.17	0.52	0.70
24.73	59.94	47.12	1.68	79.13	2.22	0.54	0.71
24.78	54.64	42.55	1.92	81.62	2.30	0.67	0.71
24.88	48.57	37.36	2.28	85.25	2.38	0.72	0.72
24.94	41.92	31.81	2.80	89.16	2.47	0.73	0.73
25.02	35.00	26.12	3.52	92.04	2.57	0.73	0.73
25.12	28.43	20.76	4.59	95.35	2.69	0.74	0.74
25.17	22.86	16.30	6.02	98.17	2.81	0.74	0.74
25.27	18.41	12.75	7.69	98.13	2.93	0.74	0.74
25.36	15.13	9.96	9.50	94.69	3.04	0.34	0.71
25.43	12.60	8.11	11.16	90.44	3.13	0.30	0.58
25.50	10.88	6.84	12.76	87.31	3.20	0.27	0.49
25.60	9.77	6.01	14.03	84.31	3.25	0.24	0.43
25.64	9.26	5.64	14.52	81.86	3.27	0.23	0.40
25.67	9.06	5.48	14.58	79.98	3.28	0.22	0.39
25.71	8.86	5.33	14.38	76.65	3.27	0.20	0.38
25.79	8.52	5.07	14.25	72.22	3.26	0.16	0.36
25.93	8.18	4.80	14.17	68.01	3.26	0.14	0.34
26.03	8.02	4.66	13.97	65.11	3.25	0.13	0.33
26.13	8.02	4.64	13.74	63.74	3.24	0.11	0.33
26.24	8.08	4.67	13.54	63.18	3.23	0.12	0.33
26.37	8.18	4.71	13.48	63.49	3.23	0.12	0.34
26.47	8.25	4.73	13.53	64.09	3.23	0.12	0.34
26.60	8.25	4.71	13.24	62.33	3.22	0.12	0.34
26.71	8.38	4.78	12.59	60.15	3.19	0.09	0.34
26.85	8.75	5.00	11.78	58.94	3.16	0.09	0.36
26.95	8.96	5.12	12.24	62.69	3.18	0.11	0.37
27.04	9.60	5.54	12.21	67.66	3.18	0.15	0.40

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
27.09	10.14	5.90	12.33	72.68	3.18	0.17	0.42
27.19	10.95	6.42	11.76	75.49	3.16	0.20	0.46
27.23	11.18	6.56	11.88	78.01	3.16	0.21	0.47
27.33	11.42	6.70	11.98	80.22	3.17	0.22	0.48
27.40	11.76	6.91	11.94	82.48	3.16	0.24	0.49
27.47	12.30	7.25	11.72	84.94	3.15	0.25	0.52
27.57	12.97	7.66	11.34	86.93	3.14	0.28	0.55
27.66	13.85	8.22	10.99	90.36	3.12	0.30	0.59
27.77	14.96	8.93	10.64	94.93	3.10	0.34	0.64
27.86	16.28	9.76	10.29	100.42	3.08	0.40	0.70
27.96	17.39	10.45	10.06	105.14	3.07	0.45	0.75
28.06	17.73	10.63	10.22	108.70	3.08	0.49	0.76
28.15	17.29	10.31	10.64	109.63	3.10	0.50	0.74
28.25	17.04	10.10	10.32	104.18	3.08	0.47	0.72
28.34	16.50	9.71	10.12	98.29	3.07	0.34	0.69
28.44	16.94	9.96	9.46	94.21	3.04	0.34	0.71
28.54	16.11	9.38	10.45	98.03	3.09	0.38	0.67
28.62	17.46	10.22	9.90	101.19	3.06	0.41	0.73
28.71	18.34	10.74	9.72	104.45	3.05	0.45	0.77
28.77	20.26	11.95	8.92	106.63	3.01	0.48	0.85
28.86	20.73	12.21	8.93	109.00	3.01	0.51	0.87
28.91	21.34	12.56	8.78	110.37	3.00	0.52	0.90
28.97	22.04	12.99	8.63	112.06	2.99	0.77	0.77
29.04	22.92	13.50	8.45	114.13	2.98	0.77	0.77
29.10	23.97	14.13	8.26	116.69	2.97	0.78	0.78
29.15	25.15	14.85	8.08	120.01	2.96	0.78	0.78
29.25	26.40	16.30	7.69	125.36	2.93	0.79	0.79
29.34	27.38	16.91	7.60	128.48	2.93	0.80	0.80
29.38	27.75	17.12	7.63	130.55	2.93	0.80	0.80
29.48	27.72	16.25	7.97	129.55	2.95	0.80	0.80
29.55	27.48	16.06	8.07	129.61	2.96	0.80	0.80
29.63	27.41	16.75	7.61	127.50	2.93	0.79	0.79
29.72	28.43	17.61	6.01	105.80	2.81	0.76	0.76
29.82	31.56	20.09	3.98	79.94	2.63	0.58	0.71
29.88	36.83	24.31	2.33	56.65	2.39	0.09	0.65
29.96	45.23	30.47	1.87	56.98	2.29	0.09	0.65
30.06	49.92	33.83	1.75	59.16	2.25	0.11	0.65
30.13	54.67	37.29	1.64	60.99	2.21	0.12	0.66
30.18	56.02	38.21	1.63	62.30	2.21	0.14	0.66
30.28	58.72	40.06	1.61	64.44	2.20	0.16	0.67
30.37	59.53	40.40	1.67	67.53	2.22	0.21	0.68
30.47	60.51	40.85	1.74	71.05	2.25	0.28	0.69
30.57	63.28	42.69	1.73	73.87	2.24	0.35	0.69
30.66	67.26	45.46	1.67	76.12	2.22	0.42	0.70
30.74	71.34	48.33	1.62	78.31	2.20	0.51	0.70
30.82	74.51	50.51	1.59	80.52	2.19	0.61	0.71
30.90	76.30	51.60	1.61	82.93	2.20	0.71	0.71
31.01	76.90	51.74	1.66	85.67	2.22	0.72	0.72

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
31.10	77.02	51.51	1.74	89.47	2.24	0.73	0.73
31.19	77.06	51.19	1.84	93.96	2.28	0.74	0.74
31.28	77.57	51.24	1.92	98.21	2.30	0.74	0.74
31.35	78.53	51.70	1.97	101.82	2.31	0.75	0.75
31.43	80.52	52.90	1.98	104.59	2.31	0.76	0.76
31.53	83.11	54.53	1.97	107.28	2.31	0.76	0.76
31.60	85.91	56.74	1.78	101.10	2.26	0.75	0.75
31.67	88.07	58.52	1.64	95.74	2.21	0.74	0.74
31.77	89.46	59.74	1.53	91.18	2.16	0.73	0.73
31.84	89.86	59.77	1.56	93.40	2.18	0.74	0.74
31.91	86.18	56.78	1.68	95.19	2.22	0.74	0.74
31.98	79.10	51.41	1.89	97.23	2.29	0.74	0.74
31.98	77.21	49.95	1.99	99.23	2.32	0.75	0.75
32.04	78.73	50.91	1.98	100.65	2.31	0.75	0.75
32.12	82.68	53.56	1.91	102.19	2.30	0.75	0.75
32.16	80.04	51.46	2.05	105.63	2.33	0.76	0.76
32.27	75.66	48.11	2.26	108.77	2.38	0.76	0.76
32.33	70.76	44.53	2.50	111.51	2.42	0.77	0.77
32.41	66.31	41.33	2.72	112.40	2.46	0.77	0.77
32.50	61.79	38.14	2.93	111.66	2.49	0.77	0.77
32.58	56.66	34.61	3.18	110.12	2.53	0.77	0.77
32.66	50.22	30.23	3.59	108.68	2.58	0.76	0.76
32.74	43.30	25.56	4.22	107.79	2.65	0.76	0.76
32.84	36.12	20.76	5.20	107.96	2.75	0.76	0.76
32.90	29.88	16.68	6.45	107.62	2.85	0.76	0.76
32.98	24.92	12.71	8.19	104.08	2.96	0.76	0.76
33.08	20.77	10.40	9.80	101.84	3.06	0.43	0.74
33.14	17.05	8.34	11.93	99.50	3.16	0.40	0.60
33.22	14.12	6.71	14.31	96.06	3.27	0.36	0.48
33.32	12.19	5.64	16.21	91.43	3.34	0.30	0.40
33.37	11.28	5.14	16.60	85.28	3.35	0.27	0.37
33.47	11.05	4.99	16.37	81.70	3.34	0.22	0.36
33.56	11.66	5.30	15.06	79.85	3.30	0.23	0.38
33.63	12.43	5.71	14.04	80.15	3.26	0.23	0.41
33.71	12.67	5.82	13.47	78.37	3.23	0.23	0.42
33.81	11.99	5.44	13.27	72.19	3.22	0.19	0.39
33.90	11.05	4.92	13.35	65.65	3.23	0.11	0.35
33.95	10.31	4.51	13.36	60.28	3.23	0.11	0.32
34.04	10.07	4.37	13.69	59.84	3.24	0.11	0.31
34.14	9.87	4.25	14.01	59.54	3.25	0.10	0.30
34.17	9.81	4.21	14.16	59.63	3.26	0.11	0.30
34.20	10.07	4.35	13.78	59.92	3.24	0.11	0.31
34.26	10.38	4.50	13.36	60.14	3.23	0.11	0.32
34.35	10.61	4.61	12.99	59.91	3.21	0.11	0.33
34.43	10.41	4.49	13.24	59.45	3.22	0.11	0.32
34.49	10.27	4.41	13.28	58.59	3.22	0.10	0.32
34.59	10.17	4.34	13.18	57.25	3.22	0.10	0.31
34.69	10.07	4.28	13.07	55.91	3.21	0.09	0.31

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
34.73	9.90	4.18	13.12	54.88	3.22	0.08	0.30
34.83	9.80	4.12	13.19	54.34	3.22	0.08	0.29
34.90	9.74	4.07	13.37	54.48	3.23	0.08	0.29
34.98	9.84	4.12	13.48	55.47	3.23	0.09	0.29
35.07	10.14	4.26	13.68	58.28	3.24	0.10	0.30
35.16	10.58	4.47	14.49	64.79	3.27	0.12	0.32
35.26	11.29	4.82	15.85	76.48	3.32	0.19	0.34
35.33	13.25	5.82	15.42	89.71	3.31	0.31	0.42
35.40	16.76	7.61	13.28	101.03	3.22	0.42	0.54
35.50	20.84	9.67	11.03	106.70	3.12	0.52	0.69
35.57	23.37	10.95	10.02	109.72	3.07	0.54	0.78
35.65	23.77	11.12	10.10	112.36	3.07	0.57	0.79
35.71	22.86	10.64	10.83	115.22	3.11	0.61	0.76
35.79	21.65	9.99	11.64	116.27	3.15	0.61	0.71
35.85	20.37	9.32	12.22	113.90	3.18	0.57	0.67
35.94	19.29	8.75	12.53	109.71	3.19	0.51	0.63
35.99	18.31	8.24	12.58	103.66	3.19	0.46	0.59
36.08	17.16	7.64	12.55	95.94	3.19	0.38	0.55
36.17	15.54	6.80	12.98	88.35	3.21	0.28	0.49
36.24	14.22	6.13	13.50	82.76	3.23	0.26	0.44
36.33	13.58	5.79	14.00	81.11	3.25	0.24	0.41
36.42	13.58	5.77	14.22	82.08	3.26	0.24	0.41
36.52	14.05	5.99	12.88	77.16	3.21	0.28	0.43
36.61	15.40	6.64	11.27	74.88	3.13	0.14	0.47
36.70	17.73	7.78	9.87	76.79	3.06	0.21	0.56
36.78	20.23	8.99	9.83	88.43	3.06	0.34	0.64
36.85	18.24	7.99	12.41	99.18	3.19	0.44	0.57
36.87	20.20	8.95	11.61	103.88	3.15	0.46	0.64
36.91	23.23	10.43	10.08	105.17	3.07	0.51	0.75
36.97	31.40	15.73	6.66	104.77	2.86	0.76	0.76
37.06	35.24	17.97	5.86	105.20	2.80	0.76	0.76
37.12	38.62	19.91	5.42	107.91	2.76	0.76	0.76
37.20	42.40	22.04	5.10	112.33	2.74	0.77	0.77
37.27	47.56	25.06	4.56	114.30	2.69	0.77	0.77
37.35	52.21	27.88	4.03	112.42	2.63	0.77	0.77
37.44	55.22	29.75	3.64	108.21	2.59	0.76	0.76
37.49	58.42	31.83	3.23	102.76	2.53	0.75	0.75
37.59	67.19	37.46	2.56	95.81	2.43	0.74	0.74
37.64	85.65	49.64	1.82	90.11	2.27	0.73	0.73
37.70	111.29	67.10	1.41	94.79	2.10	0.74	0.74
37.78	136.59	84.81	1.28	108.37	1.96	0.76	0.76
37.83	155.69	98.45	1.22	120.19	1.88	0.78	0.78
37.92	167.53	106.83	1.19	126.68	1.83	0.79	0.79
37.97	174.58	111.69	1.17	130.53	1.81	0.80	0.80
38.07	178.80	114.34	1.16	133.13	1.81	0.80	0.80
38.14	181.84	116.07	1.17	135.64	1.81	0.81	0.81
38.22	185.72	118.33	1.17	138.68	1.82	0.81	0.81
38.31	191.72	121.94	1.17	143.23	1.82	0.82	0.82

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.41	201.37	128.37	1.16	148.66	1.80	0.83	0.83
38.52	212.64	135.94	1.14	154.32	1.79	0.83	0.83
38.64	221.04	141.59	1.11	157.41	1.77	0.84	0.84
38.74	217.87	138.67	1.14	158.10	1.79	0.84	0.84
38.80	214.19	135.62	1.16	157.57	1.81	0.84	0.84
38.89	210.42	132.43	1.18	156.57	1.83	0.84	0.84
38.94	213.65	134.37	1.18	158.84	1.83	0.84	0.84
39.03	213.59	133.74	1.19	159.69	1.84	0.84	0.84
39.13	213.25	132.81	1.21	160.46	1.86	0.84	0.84
39.23	211.36	130.76	1.22	160.12	1.88	0.84	0.84
39.35	207.85	127.69	1.24	158.27	1.90	0.84	0.84
39.42	201.04	122.59	1.26	154.08	1.93	0.83	0.83
39.51	192.09	116.15	1.28	148.22	1.96	0.82	0.82
39.60	181.50	108.71	1.30	141.37	1.99	0.82	0.82
39.70	172.83	102.65	1.32	135.85	2.02	0.81	0.81
39.78	164.63	97.07	1.35	130.75	2.04	0.80	0.80
39.90	157.35	92.05	1.37	126.28	2.06	0.79	0.79
39.99	149.05	86.44	1.41	121.65	2.09	0.79	0.79
40.09	141.42	81.31	1.45	117.75	2.12	0.78	0.78
40.18	133.79	76.23	1.50	114.33	2.15	0.77	0.77
40.23	126.04	71.16	1.56	111.30	2.18	0.77	0.77
40.33	118.01	65.88	1.65	108.90	2.22	0.76	0.76
40.43	110.12	60.74	1.76	107.17	2.25	0.76	0.76
40.52	101.85	55.31	1.95	107.68	2.31	0.76	0.76
40.61	92.44	49.44	2.15	106.53	2.36	0.76	0.76
40.69	80.59	42.14	2.54	106.96	2.43	0.76	0.76
40.80	68.65	35.01	3.03	106.21	2.51	0.76	0.76
40.87	59.91	29.84	3.59	107.20	2.58	0.76	0.76
40.95	53.47	26.09	4.12	107.50	2.64	0.76	0.76
40.97	51.37	24.94	4.24	105.79	2.65	0.76	0.76
41.01	54.31	26.70	3.81	101.77	2.61	0.75	0.75
41.07	61.80	31.20	3.04	94.92	2.51	0.74	0.74
41.15	67.40	34.61	2.61	90.47	2.44	0.73	0.73
41.26	67.13	34.39	2.61	89.74	2.44	0.73	0.73
41.35	63.05	31.86	2.87	91.40	2.48	0.73	0.73
41.47	60.28	30.09	3.10	93.27	2.52	0.74	0.74
41.59	59.67	29.62	3.18	94.19	2.53	0.74	0.74
41.69	60.42	29.94	3.18	95.29	2.53	0.74	0.74
41.78	59.17	29.08	3.36	97.63	2.55	0.74	0.74
41.88	54.75	26.41	3.82	100.94	2.61	0.75	0.75
41.98	49.45	23.32	4.43	103.21	2.67	0.75	0.75
42.08	45.13	20.88	4.96	103.54	2.72	0.75	0.75
42.16	44.32	20.43	4.99	102.01	2.73	0.75	0.75
42.24	47.12	21.98	4.53	99.69	2.68	0.75	0.75
42.31	52.25	24.86	3.91	97.23	2.62	0.74	0.74
42.45	56.94	27.44	3.48	95.61	2.57	0.74	0.74
42.55	59.37	28.78	3.30	94.91	2.54	0.74	0.74
42.60	59.78	28.96	3.29	95.14	2.54	0.74	0.74

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
42.70	59.34	28.59	3.38	96.60	2.55	0.74	0.74
42.81	57.38	27.33	3.64	99.43	2.59	0.75	0.75
42.89	53.57	25.06	4.12	103.15	2.64	0.75	0.75
42.98	48.27	22.02	4.84	106.61	2.71	0.76	0.76
43.08	43.14	19.16	5.69	108.99	2.79	0.76	0.76
43.17	40.44	17.68	6.18	109.35	2.83	0.76	0.76
43.27	41.05	18.01	5.94	107.03	2.81	0.76	0.76
43.37	43.81	19.71	4.84	95.48	2.71	0.74	0.74
43.50	46.82	21.62	3.86	83.44	2.61	0.71	0.71
43.61	48.54	22.85	3.24	73.95	2.54	0.35	0.69
43.74	49.31	23.16	3.25	75.29	2.54	0.39	0.70
43.79	49.31	22.99	3.44	79.06	2.56	0.54	0.71
43.86	48.47	22.31	3.79	84.59	2.60	0.72	0.72
43.94	47.05	21.30	4.28	91.16	2.66	0.73	0.73
44.00	44.89	19.92	4.92	98.08	2.72	0.74	0.74
44.08	42.33	18.39	5.62	103.37	2.78	0.75	0.75
44.17	38.85	16.48	6.45	106.26	2.85	0.76	0.76
44.27	35.44	14.71	7.14	105.00	2.90	0.76	0.76
44.42	34.16	14.09	7.15	100.72	2.90	0.75	0.75
44.52	37.10	15.69	6.06	95.03	2.82	0.74	0.74
44.61	44.15	19.52	4.49	87.72	2.68	0.72	0.72
44.71	51.91	23.77	3.51	83.46	2.57	0.71	0.71
44.85	56.66	26.27	3.19	83.87	2.53	0.72	0.72
44.95	57.30	26.40	3.34	88.11	2.55	0.72	0.72
45.09	54.98	24.92	3.69	92.06	2.59	0.73	0.73
45.19	50.09	22.17	4.29	95.00	2.66	0.74	0.74
45.33	43.44	18.53	5.31	98.48	2.76	0.75	0.75
45.42	37.17	15.25	6.56	100.02	2.85	0.75	0.75
45.57	34.20	13.74	7.18	98.64	2.90	0.75	0.75
45.68	32.58	12.98	7.29	94.66	2.91	0.74	0.74
45.81	30.45	12.02	7.30	87.72	2.91	0.72	0.72
45.92	26.54	9.26	8.96	82.93	3.01	0.26	0.66
46.05	22.29	7.59	10.87	82.51	3.11	0.33	0.54
46.16	19.32	6.43	13.40	86.12	3.23	0.32	0.46
46.17	17.73	5.82	14.71	85.57	3.28	0.32	0.42
46.23	17.46	5.70	14.75	84.09	3.28	0.30	0.41
46.29	16.85	5.46	15.02	82.02	3.29	0.28	0.39
46.34	16.04	5.15	15.32	78.81	3.31	0.26	0.37
46.42	15.30	4.85	15.44	74.90	3.31	0.22	0.35
46.48	14.90	4.69	15.10	70.80	3.30	0.19	0.34
46.52	14.69	4.61	14.73	67.86	3.28	0.17	0.33
46.60	14.56	4.55	14.47	65.79	3.27	0.16	0.32
46.67	14.49	4.51	14.23	64.21	3.26	0.15	0.32
46.74	14.45	4.49	14.03	63.02	3.25	0.14	0.32
46.82	14.42	4.47	13.84	61.88	3.25	0.14	0.32
46.88	14.19	4.37	13.96	61.07	3.25	0.13	0.31
46.96	14.10	4.33	13.99	60.61	3.25	0.13	0.31
47.06	13.97	4.27	14.16	60.52	3.26	0.13	0.31

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
47.15	14.11	4.31	14.15	61.03	3.26	0.13	0.31
47.24	14.43	4.42	14.72	65.10	3.28	0.14	0.32
47.35	16.18	5.07	14.87	75.39	3.29	0.20	0.36
47.49	19.69	6.36	12.67	80.67	3.20	0.35	0.45
47.58	24.11	8.00	10.33	82.65	3.09	0.29	0.57
47.73	26.03	8.69	9.32	80.95	3.03	0.30	0.62
47.83	27.06	9.05	9.05	81.84	3.02	0.33	0.65
47.87	26.18	8.71	9.55	83.19	3.04	0.32	0.62
47.89	26.93	8.98	9.14	82.12	3.02	0.32	0.64
47.94	26.64	8.87	9.20	81.59	3.02	0.31	0.63
48.02	26.81	8.91	9.08	80.90	3.02	0.31	0.64
48.07	26.40	8.75	9.26	81.07	3.03	0.31	0.63
48.12	25.97	8.58	9.61	82.45	3.05	0.31	0.61
48.18	25.43	8.37	10.05	84.09	3.07	0.34	0.60
48.26	25.01	8.20	10.42	85.42	3.09	0.34	0.59
48.31	24.60	8.04	10.54	84.77	3.10	0.34	0.57
48.38	24.56	8.01	10.30	82.58	3.08	0.31	0.57
48.46	24.71	8.05	9.85	79.31	3.06	0.29	0.58
48.52	24.41	7.93	9.58	75.99	3.05	0.26	0.57
48.60	23.16	7.46	9.70	72.40	3.05	0.23	0.53
48.68	20.77	6.57	10.59	69.64	3.10	0.19	0.47
48.74	18.20	5.63	12.04	67.76	3.17	0.18	0.40
48.82	15.94	4.80	14.01	67.24	3.25	0.17	0.34
48.89	14.56	4.29	15.49	66.41	3.31	0.17	0.31
48.99	13.82	4.01	16.21	64.98	3.34	0.16	0.29
49.05	13.65	3.94	15.85	62.48	3.32	0.14	0.28
49.12	13.51	3.89	15.38	59.74	3.31	0.12	0.28
49.18	13.55	3.89	14.70	57.20	3.28	0.11	0.28
49.27	13.75	3.96	14.08	55.71	3.26	0.10	0.28
49.32	13.92	4.01	13.56	54.42	3.24	0.10	0.29
49.42	13.55	3.87	13.92	53.88	3.25	0.09	0.28
49.48	13.11	3.71	14.46	53.63	3.27	0.09	0.26
49.56	13.01	3.66	14.76	54.09	3.28	0.09	0.26
49.66	13.28	3.75	14.73	55.25	3.28	0.10	0.27
49.76	13.68	3.89	14.49	56.33	3.27	0.11	0.28
49.85	14.06	4.01	13.46	54.00	3.23	0.11	0.29
49.99	14.87	4.29	11.96	51.28	3.17	0.06	0.31
50.09	14.43	4.12	11.90	49.07	3.16	0.08	0.29
50.21	13.82	3.89	12.94	50.39	3.21	0.08	0.28
50.24	13.21	3.68	13.72	50.47	3.24	0.08	0.26
50.29	13.59	3.81	13.05	49.66	3.21	0.08	0.27
50.38	13.69	3.83	12.73	48.82	3.20	0.07	0.27
50.47	13.39	3.72	13.00	48.36	3.21	0.07	0.27
50.52	12.98	3.57	13.61	48.61	3.24	0.07	0.26
50.62	13.01	3.58	13.73	49.09	3.24	0.07	0.26
50.66	13.15	3.62	13.70	49.58	3.24	0.08	0.26
50.76	13.28	3.66	13.70	50.11	3.24	0.08	0.26
50.83	14.13	3.95	12.99	51.29	3.21	0.08	0.28

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
50.91	14.30	4.00	13.34	53.36	3.23	0.09	0.29
51.00	15.61	4.45	12.42	55.29	3.19	0.11	0.32
51.06	17.36	5.06	11.27	56.99	3.13	0.11	0.36
51.15	17.67	5.15	11.86	61.08	3.16	0.13	0.37
51.24	16.35	4.68	14.43	67.57	3.27	0.18	0.33
51.31	12.88	3.47	21.69	75.27	3.51	0.23	0.25
51.39	18.55	5.43	14.77	80.15	3.28	0.29	0.39
51.48	32.14	11.43	7.23	82.64	2.90	0.71	0.71
51.58	35.38	12.78	6.83	87.30	2.87	0.72	0.72
51.68	27.82	8.59	10.70	91.85	3.10	0.45	0.61
51.77	17.84	5.13	19.49	100.06	3.45	0.43	0.37
51.90	36.80	11.62	9.16	106.47	3.02	0.53	0.83
52.01	74.42	30.49	3.61	110.20	2.58	0.77	0.77
52.11	128.50	57.50	2.11	121.05	2.34	0.78	0.78
52.26	161.87	74.64	1.77	131.90	2.25	0.80	0.80
52.30	209.17	100.78	1.45	146.55	2.12	0.82	0.82
52.33	248.44	124.60	1.31	162.63	2.00	0.84	0.84
52.35	302.93	158.50	1.21	192.22	1.87	0.88	0.88
52.40	347.53	187.07	1.12	209.95	1.78	0.90	0.90
52.45	381.51	208.63	1.04	216.58	1.72	0.90	0.90
52.50	415.58	229.89	1.00	229.89	1.69	0.92	0.92
52.55	447.33	248.98	1.00	248.98	1.67	0.93	0.93
52.60	486.53	273.15	1.00	273.15	1.63	0.96	0.96
52.65	516.02	289.64	1.00	289.64	1.60	0.97	0.97
52.71	531.14	297.95	1.00	297.95	1.57	0.98	0.98
52.77	541.83	303.79	1.00	303.79	1.53	0.98	0.98
52.82	558.50	312.99	1.00	312.99	1.51	0.99	0.99
52.88	578.13	323.84	1.00	323.84	1.48	1.00	1.00
52.93	592.07	331.46	1.00	331.46	1.46	1.00	1.00
52.98	605.70	338.95	1.00	338.95	1.46	1.01	1.01
53.03	608.64	340.39	1.00	340.39	1.46	1.01	1.01
53.08	608.27	340.01	1.00	340.01	1.46	1.01	1.01
53.12	601.01	335.78	1.00	335.78	1.47	1.00	1.00
53.17	598.22	333.99	1.00	333.99	1.46	1.00	1.00
53.23	600.71	335.19	1.00	335.19	1.45	1.00	1.00
53.28	596.23	332.45	1.00	332.45	1.47	1.00	1.00
53.37	588.50	327.80	1.00	327.80	1.48	1.00	1.00
53.42	584.11	325.17	1.00	325.17	1.50	1.00	1.00
53.46	586.81	326.50	1.00	326.50	1.52	1.00	1.00
53.53	599.03	333.09	1.00	333.09	1.53	1.00	1.00
53.61	597.34	331.84	1.00	331.84	1.56	1.00	1.00
53.62	582.26	323.39	1.00	323.39	1.60	1.00	1.00
53.65	574.05	318.67	1.00	318.67	1.60	0.99	0.99
53.67	571.35	317.12	1.00	317.12	1.61	0.99	0.99
53.70	583.83	323.95	1.00	323.95	1.59	1.00	1.00
53.74	582.83	323.26	1.00	323.26	1.60	1.00	1.00
53.76	583.81	323.74	1.00	323.74	1.60	1.00	1.00
53.80	581.08	322.06	1.00	322.06	1.59	0.99	0.99

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
53.84	577.81	320.07	1.00	320.07	1.59	0.99	0.99
53.90	578.23	320.12	1.00	320.12	1.58	0.99	0.99
53.91	570.20	315.61	1.00	315.61	1.59	0.99	0.99
53.95	573.64	317.38	1.00	317.38	1.58	0.99	0.99
53.96	579.94	320.83	1.00	320.83	1.58	0.99	0.99
53.98	601.06	332.48	1.00	332.48	1.56	1.00	1.00
53.99	602.95	333.50	1.00	333.50	1.56	1.00	1.00
54.01	592.15	327.46	1.00	327.46	1.57	1.00	1.00
54.02	579.33	320.31	1.00	320.31	1.58	0.99	0.99
54.03	553.15	305.74	1.00	305.74	1.61	0.98	0.98
54.04	504.84	276.21	1.00	276.21	1.67	0.96	0.96
54.05	452.17	241.19	1.08	260.14	1.75	0.94	0.94
54.09	422.63	221.81	1.15	254.46	1.79	0.94	0.94
54.10	421.59	220.94	1.15	254.57	1.80	0.94	0.94
54.13	421.89	221.06	1.15	254.64	1.80	0.94	0.94
54.14	420.96	220.34	1.16	254.59	1.80	0.94	0.94
54.19	422.82	221.19	1.16	255.77	1.80	0.94	0.94
54.19	428.79	224.52	1.15	258.95	1.80	0.94	0.94
54.24	439.22	231.86	1.12	259.93	1.77	0.94	0.94
54.29	456.97	245.94	1.02	249.88	1.71	0.94	0.94
54.33	474.10	261.31	1.00	261.31	1.64	0.95	0.95
54.38	494.95	272.80	1.00	272.80	1.57	0.96	0.96
54.39	512.70	282.62	1.00	282.62	1.53	0.96	0.96
54.43	529.13	291.66	1.00	291.66	1.52	0.97	0.97
54.48	543.10	299.32	1.00	299.32	1.44	0.98	0.98
54.52	556.66	306.76	1.00	306.76	1.36	0.98	0.98
54.58	573.87	316.20	1.00	316.20	1.26	0.99	0.99
54.62	587.13	323.46	1.00	323.46	1.28	1.00	1.00
54.65	604.44	333.00	1.00	333.00	1.29	1.00	1.00
54.67	623.33	343.41	1.00	343.41	1.30	1.01	1.01
54.71	658.15	362.60	1.00	362.60	1.28	1.02	1.02
54.77	679.34	374.21	1.00	374.21	1.20	1.03	1.03
54.81	702.99	387.19	1.00	387.19	1.11	1.04	1.04
54.85	704.07	387.70	1.00	387.70	1.04	1.04	1.04
54.86	709.13	390.48	1.00	390.48	1.06	1.04	1.04
54.87	703.33	387.26	1.00	387.26	1.09	1.04	1.04
54.91	703.66	387.35	1.00	387.35	1.13	1.04	1.04
54.96	707.14	389.17	1.00	389.17	1.16	1.04	1.04
55.00	703.19	386.89	1.00	386.89	1.18	1.04	1.04
55.01	695.84	382.82	1.00	382.82	1.19	1.04	1.04
55.05	679.11	373.47	1.00	373.47	1.21	1.03	1.03
55.10	651.07	357.87	1.00	357.87	1.24	1.02	1.02
55.12	603.77	331.72	1.00	331.72	1.29	1.00	1.00
55.13	570.97	313.58	1.00	313.58	1.33	0.99	0.99
55.14	563.11	309.22	1.00	309.22	1.33	0.98	0.98
55.19	576.91	316.75	1.00	316.75	1.31	0.99	0.99
55.20	576.27	316.38	1.00	316.38	1.31	0.99	0.99
55.25	562.13	308.48	1.00	308.48	1.33	0.98	0.98

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
55.29	546.07	299.55	1.00	299.55	1.37	0.98	0.98
55.33	519.69	284.92	1.00	284.92	1.42	0.97	0.97
55.38	481.16	263.59	1.00	263.59	1.52	0.95	0.95
55.48	439.32	240.38	1.00	240.38	1.63	0.93	0.93
55.57	411.39	218.55	1.04	227.87	1.73	0.92	0.92
55.63	398.09	206.42	1.15	237.94	1.80	0.92	0.92
55.72	402.04	206.08	1.19	244.53	1.83	0.93	0.93
55.80	431.09	221.88	1.17	260.68	1.82	0.95	0.95
55.86	480.55	259.76	1.00	259.76	1.67	0.94	0.94
55.97	527.85	288.32	1.00	288.32	1.51	0.97	0.97
56.01	560.55	306.20	1.00	306.20	1.34	0.98	0.98
56.06	587.84	186.61	1.00	186.61	1.50	0.87	0.87
56.11	613.11	194.57	1.00	194.57	1.50	0.88	0.88
56.15	640.71	203.27	1.00	203.27	1.51	0.89	0.89
56.20	660.92	209.60	1.00	209.60	1.52	0.90	0.90
56.27	663.16	210.15	1.00	210.15	1.53	0.90	0.90
56.27	664.17	210.45	1.00	210.45	1.56	0.90	0.90
56.30	642.20	203.39	1.00	203.39	1.61	0.89	0.89
56.33	649.54	205.64	1.00	205.64	1.64	0.89	0.89
56.35	647.65	205.00	1.00	205.00	1.66	0.89	0.89
56.40	667.86	211.31	1.00	211.31	1.64	0.90	0.90
56.41	669.34	211.76	1.00	211.76	1.64	0.90	0.90
56.44	681.53	215.53	1.00	215.53	1.63	0.90	0.90
56.49	695.19	219.75	1.00	219.75	1.62	0.91	0.91
56.54	717.49	226.71	1.00	226.71	1.61	0.91	0.91
56.58	737.23	232.85	1.00	232.85	1.61	0.92	0.92
56.59	750.18	236.93	1.00	236.93	1.61	0.92	0.92
56.64	757.34	239.07	1.00	239.07	1.60	0.93	0.93
56.69	764.80	241.29	1.00	241.29	1.60	0.93	0.93
56.73	778.16	245.40	1.00	245.40	1.59	0.93	0.93
56.78	778.56	245.38	1.00	245.38	1.58	0.93	0.93
56.83	759.53	239.22	1.00	239.22	1.58	0.93	0.93
56.88	731.80	230.32	1.00	230.32	1.58	0.92	0.92
56.89	708.89	223.03	1.00	223.03	1.60	0.91	0.91
56.95	692.53	217.71	1.00	217.71	1.59	0.91	0.91
57.01	668.00	209.81	1.00	209.81	1.59	0.90	0.90
57.07	645.94	202.70	1.00	202.70	1.58	0.89	0.89
57.11	619.45	194.25	1.00	194.25	1.52	0.88	0.88
57.17	598.63	187.56	1.00	187.56	1.46	0.87	0.87
57.26	574.07	179.66	1.00	179.66	1.37	0.86	0.86
57.31	547.05	171.06	1.00	171.06	1.43	0.85	0.85
57.37	520.16	162.50	1.00	162.50	1.45	0.84	0.84
57.45	490.27	152.96	1.00	152.96	1.51	0.83	0.83
57.51	451.30	140.63	1.00	140.63	1.55	0.81	0.81
57.53	421.54	131.27	1.00	131.27	1.59	0.80	0.80
57.59	401.40	124.87	1.00	124.87	1.62	0.79	0.79
57.63	398.96	124.05	1.00	124.05	1.62	0.79	0.79
57.68	391.51	121.66	1.00	121.66	1.63	0.79	0.79

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
57.73	386.48	120.01	1.00	120.01	1.64	0.78	0.78
57.78	379.02	117.62	1.00	117.62	1.65	0.78	0.78
57.86	359.96	111.55	1.00	111.55	1.66	0.77	0.77
57.92	326.32	100.97	1.00	100.97	1.71	0.75	0.75
57.98	290.83	89.82	1.00	89.82	1.76	0.73	0.73
58.06	263.33	81.16	1.18	95.51	1.82	0.74	0.74
58.12	242.92	74.75	1.24	92.39	1.90	0.73	0.73
58.21	222.41	68.28	1.30	88.73	1.99	0.73	0.73
58.26	204.43	62.64	1.37	85.71	2.06	0.72	0.72
58.35	180.37	55.10	1.48	81.38	2.14	0.65	0.71
58.41	154.93	47.15	1.59	74.91	2.19	0.38	0.70
58.50	122.84	37.13	1.90	70.73	2.29	0.27	0.69
58.56	98.18	29.45	2.28	67.27	2.38	0.20	0.68
58.64	77.90	23.14	3.23	74.61	2.53	0.37	0.69
58.73	63.67	18.70	4.34	81.15	2.66	0.64	0.71
58.80	51.12	14.80	5.89	87.16	2.80	0.72	0.72
58.84	42.24	12.04	7.59	91.44	2.93	0.73	0.73
58.85	43.79	12.52	7.27	91.06	2.90	0.73	0.73
58.93	50.50	14.59	6.00	87.49	2.81	0.72	0.72
58.98	58.12	16.94	4.87	82.49	2.72	0.71	0.71
59.02	61.77	18.06	4.38	79.02	2.67	0.54	0.70
59.12	63.39	18.54	4.19	77.74	2.65	0.48	0.70
59.17	65.41	19.15	4.09	78.34	2.64	0.51	0.70
59.27	67.33	19.73	4.06	80.06	2.63	0.59	0.71
59.31	67.64	19.81	4.15	82.31	2.64	0.71	0.71
59.41	64.84	18.93	4.46	84.40	2.68	0.72	0.72
59.46	57.99	16.81	5.11	85.91	2.74	0.72	0.72
59.55	48.77	13.96	6.20	86.53	2.83	0.72	0.72
59.65	39.66	11.14	7.37	82.12	2.91	0.70	0.71
59.70	34.25	9.47	8.28	78.48	2.97	0.51	0.70
59.80	32.07	8.80	8.61	75.77	2.99	0.41	0.70
59.89	32.04	8.78	9.03	79.29	3.01	0.30	0.63
59.94	31.04	8.47	9.76	82.68	3.06	0.33	0.60
60.01	30.35	8.25	10.33	85.21	3.09	0.36	0.59
60.02	32.64	8.95	9.57	85.70	3.04	0.36	0.64
60.08	35.54	9.83	8.61	84.70	2.99	0.72	0.72
60.12	36.56	10.14	8.23	83.40	2.97	0.71	0.71
60.17	32.87	9.01	9.03	81.32	3.01	0.34	0.64
60.27	28.56	7.68	10.03	76.99	3.07	0.27	0.55
60.31	24.81	6.53	11.00	71.83	3.12	0.21	0.47
60.37	22.21	5.73	11.72	67.16	3.15	0.19	0.41
60.46	20.93	5.33	12.03	64.16	3.17	0.15	0.38
60.51	20.76	5.28	11.57	61.05	3.15	0.14	0.38
60.61	21.43	5.48	10.86	59.48	3.11	0.13	0.39
60.65	21.84	5.60	10.44	58.49	3.09	0.13	0.40
60.75	22.18	5.70	10.27	58.52	3.08	0.13	0.41
60.81	22.25	5.72	10.24	58.52	3.08	0.13	0.41
60.89	22.21	5.70	10.20	58.14	3.08	0.13	0.41

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
60.94	22.45	5.77	10.12	58.37	3.07	0.12	0.41
61.03	22.62	5.81	10.19	59.27	3.08	0.13	0.42
61.09	22.65	5.82	10.23	59.56	3.08	0.14	0.42
61.19	22.38	5.74	10.30	59.09	3.08	0.13	0.41
61.24	22.96	5.91	9.90	58.48	3.06	0.12	0.42
61.33	24.51	6.37	9.35	59.55	3.03	0.14	0.46
61.38	24.20	6.28	10.50	65.92	3.09	0.15	0.45
61.47	23.16	5.95	12.35	73.50	3.18	0.24	0.43
61.53	21.88	5.56	14.59	81.14	3.28	0.29	0.40
61.62	27.61	7.29	11.24	81.97	3.13	0.33	0.52
61.70	44.48	12.39	6.68	82.73	2.86	0.71	0.71
61.77	66.81	19.14	4.44	84.93	2.67	0.72	0.72
61.86	81.96	23.70	3.78	89.66	2.60	0.73	0.73
61.95	81.02	23.39	4.06	94.89	2.63	0.74	0.74
61.97	72.62	20.85	4.65	96.91	2.69	0.74	0.74
62.01	62.36	17.75	5.62	99.66	2.78	0.75	0.75
62.10	52.17	14.66	6.77	99.23	2.87	0.75	0.75
62.24	55.41	15.61	5.76	89.92	2.79	0.73	0.73
62.34	87.70	25.31	2.83	71.54	2.48	0.29	0.69
62.49	127.58	37.26	1.74	64.77	2.25	0.17	0.67
62.54	164.52	48.34	1.44	69.68	2.11	0.25	0.68
62.66	181.39	53.35	1.37	73.33	2.07	0.34	0.69
62.74	199.68	58.78	1.33	77.94	2.02	0.49	0.70
62.87	211.65	62.29	1.30	80.99	1.99	0.63	0.71
62.92	217.18	63.92	1.29	82.65	1.98	0.71	0.71
63.03	219.18	64.44	1.29	83.41	1.98	0.71	0.71
63.15	218.06	64.03	1.30	83.38	1.99	0.71	0.71
63.26	213.11	62.49	1.32	82.35	2.01	0.71	0.71
63.37	206.70	60.51	1.34	80.92	2.03	0.63	0.71
63.45	200.15	58.51	1.34	78.49	2.04	0.51	0.70
63.54	197.59	57.70	1.32	76.31	2.02	0.43	0.70
63.61	190.30	55.49	1.33	73.61	2.02	0.34	0.69
63.69	172.04	50.02	1.39	69.47	2.08	0.24	0.68
63.79	141.71	40.98	1.65	67.77	2.22	0.21	0.68
63.89	106.15	30.39	2.20	66.74	2.36	0.19	0.67
63.98	75.22	21.20	3.37	71.48	2.55	0.29	0.69
64.07	53.15	14.65	4.91	71.91	2.72	0.30	0.69
64.15	39.12	10.48	7.30	76.48	2.91	0.44	0.70
64.23	29.98	7.77	10.00	77.68	3.07	0.27	0.56
64.26	25.15	6.34	12.34	78.26	3.18	0.27	0.45
64.29	23.57	5.87	13.31	78.14	3.22	0.26	0.42
64.33	23.37	5.81	12.89	74.86	3.21	0.26	0.41
64.43	22.99	5.69	12.43	70.78	3.19	0.19	0.41
64.47	22.29	5.48	12.05	66.07	3.17	0.17	0.39
64.53	21.82	5.34	12.01	64.15	3.17	0.16	0.38
64.62	20.60	4.98	12.74	63.40	3.20	0.15	0.36
64.72	19.12	4.53	13.95	63.23	3.25	0.15	0.32
64.78	18.00	4.20	15.17	63.74	3.30	0.15	0.30

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
64.86	18.21	4.26	15.26	65.01	3.30	0.16	0.30
64.96	18.78	4.42	15.44	68.31	3.31	0.18	0.32
65.06	19.22	4.55	15.74	71.61	3.32	0.21	0.32
65.11	19.22	4.55	16.41	74.58	3.34	0.23	0.32
65.21	18.85	4.43	17.13	75.90	3.37	0.24	0.32
65.31	18.45	4.31	17.70	76.26	3.39	0.24	0.31
65.40	18.28	4.25	17.10	72.77	3.37	0.23	0.30
65.50	18.58	4.34	15.67	67.97	3.32	0.16	0.31
65.58	19.02	4.46	14.15	63.13	3.26	0.14	0.32
65.68	19.05	4.47	13.69	61.17	3.24	0.14	0.32
65.78	17.67	4.06	14.89	60.45	3.29	0.13	0.29
65.84	16.40	3.69	16.19	59.69	3.34	0.13	0.26
65.86	15.56	3.44	17.33	59.62	3.38	0.12	0.25
65.87	16.51	3.72	15.97	59.36	3.33	0.12	0.27
65.98	17.26	3.93	15.03	59.09	3.29	0.12	0.28
66.10	17.84	4.09	14.69	60.13	3.28	0.12	0.29
66.21	18.21	4.20	14.85	62.32	3.29	0.14	0.30
66.34	18.48	4.27	14.76	63.01	3.28	0.16	0.31
66.48	19.00	4.42	14.39	63.55	3.27	0.13	0.32
66.62	18.46	4.25	14.69	62.45	3.28	0.15	0.30
66.68	18.67	4.31	14.87	64.07	3.29	0.14	0.31
66.87	18.92	4.37	15.53	67.94	3.31	0.16	0.31
66.96	19.16	4.44	16.65	73.89	3.35	0.23	0.32
67.11	18.25	4.17	18.76	78.15	3.42	0.27	0.30
67.21	16.83	3.75	20.42	76.60	3.47	0.26	0.27
67.35	16.22	3.57	20.50	73.18	3.48	0.19	0.26
67.45	16.16	3.55	21.95	77.86	3.52	0.19	0.25
67.59	27.42	6.79	13.06	88.71	3.21	0.37	0.49
67.68	77.39	21.19	3.95	83.67	2.62	0.72	0.72
67.83	159.77	44.89	1.66	74.68	2.22	0.38	0.69
67.92	241.25	68.29	1.30	88.64	1.99	0.73	0.73
68.02	283.19	80.28	1.24	99.35	1.90	0.75	0.75
68.07	299.01	84.78	1.22	103.71	1.88	0.75	0.75
68.16	305.70	86.62	1.22	105.26	1.87	0.76	0.76
68.26	310.93	88.04	1.21	106.54	1.86	0.76	0.76
68.35	307.75	87.05	1.22	106.44	1.88	0.76	0.76
68.45	299.96	84.74	1.24	105.37	1.91	0.76	0.76
68.55	291.49	82.23	1.26	103.72	1.94	0.75	0.75
68.65	271.72	76.50	1.29	98.57	1.98	0.75	0.75
68.78	253.59	71.23	1.32	94.35	2.02	0.74	0.74
68.78	238.18	66.83	1.36	90.91	2.05	0.73	0.73
68.79	234.24	65.70	1.37	89.70	2.06	0.73	0.73
68.83	237.70	66.66	1.34	89.08	2.03	0.73	0.73
68.93	243.69	68.30	1.30	88.59	1.99	0.73	0.73
68.98	253.54	71.08	1.25	89.18	1.93	0.73	0.73
69.04	257.79	72.25	1.23	89.05	1.89	0.73	0.73
69.12	259.28	72.61	1.23	89.10	1.89	0.73	0.73
69.22	255.36	71.43	1.24	88.23	1.90	0.72	0.72

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
69.28	247.73	69.22	1.25	86.25	1.91	0.72	0.72
69.36	237.41	66.24	1.26	83.22	1.93	0.71	0.71
69.45	223.58	62.26	1.27	79.21	1.95	0.55	0.71
69.60	210.12	58.37	1.29	75.34	1.98	0.40	0.70
69.70	198.18	54.94	1.31	72.05	2.01	0.30	0.69
69.80	193.42	53.54	1.32	70.68	2.01	0.27	0.69
69.89	192.07	53.12	1.32	70.30	2.02	0.26	0.68
69.98	190.15	52.53	1.33	69.82	2.02	0.25	0.68
70.08	181.88	50.15	1.35	67.53	2.04	0.21	0.68
70.18	159.82	43.89	1.45	63.51	2.12	0.15	0.67
70.32	124.32	33.85	1.81	61.16	2.27	0.12	0.66
70.42	84.31	22.56	2.96	66.77	2.50	0.20	0.68
70.54	51.82	13.41	5.53	74.19	2.77	0.36	0.69
70.66	31.85	7.79	9.69	75.54	3.05	0.25	0.56
70.75	23.52	5.45	13.34	72.70	3.23	0.21	0.39
70.80	21.80	4.97	13.43	66.71	3.23	0.18	0.35
70.89	22.64	5.20	11.52	59.87	3.14	0.12	0.37
70.99	22.34	5.11	10.38	53.00	3.09	0.09	0.36
71.08	21.63	4.90	10.09	49.46	3.07	0.07	0.35
71.17	21.43	4.84	9.87	47.79	3.06	0.07	0.35
71.23	20.92	4.70	10.01	47.05	3.07	0.07	0.34
71.33	21.09	4.74	9.74	46.20	3.05	0.06	0.34
71.42	21.73	4.92	9.08	44.64	3.02	0.06	0.35
71.52	22.81	5.22	8.26	43.06	2.97	0.03	0.62
71.58	23.21	5.33	8.27	44.01	2.97	0.04	0.62
71.67	22.88	5.23	9.07	47.43	3.02	0.07	0.37
71.81	22.47	5.11	9.94	50.76	3.06	0.09	0.36
71.82	22.24	5.04	10.42	52.55	3.09	0.09	0.36
71.86	21.97	4.96	10.64	52.82	3.10	0.09	0.35
71.91	21.83	4.92	10.75	52.95	3.11	0.09	0.35
71.97	21.60	4.86	10.97	53.27	3.12	0.09	0.35
72.05	21.36	4.79	11.22	53.72	3.13	0.10	0.34
72.10	21.13	4.72	11.52	54.35	3.14	0.10	0.34
72.20	20.99	4.68	11.71	54.79	3.15	0.10	0.33
72.25	20.99	4.67	11.87	55.49	3.16	0.10	0.33
72.34	21.09	4.70	12.12	56.94	3.17	0.11	0.34
72.44	21.09	4.69	12.53	58.80	3.19	0.12	0.34
72.53	20.89	4.63	13.04	60.40	3.21	0.13	0.33
72.63	20.79	4.60	13.29	61.13	3.22	0.14	0.33
72.69	20.48	4.51	13.55	61.14	3.23	0.14	0.32
72.82	20.69	4.56	13.34	60.87	3.23	0.13	0.33
72.92	21.13	4.68	12.83	60.05	3.20	0.13	0.33
73.06	22.11	4.95	11.98	59.27	3.17	0.12	0.35
73.16	22.34	5.01	11.90	59.57	3.16	0.12	0.36
73.30	20.86	4.59	13.21	60.65	3.22	0.14	0.33
73.35	19.88	4.32	14.25	61.53	3.26	0.14	0.31
73.38	19.20	4.13	14.83	61.23	3.29	0.13	0.30
73.47	20.02	4.35	13.95	60.67	3.25	0.13	0.31

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
73.53	20.08	4.37	13.79	60.20	3.24	0.13	0.31
73.62	20.18	4.39	13.66	59.95	3.24	0.13	0.31
73.71	19.95	4.32	13.95	60.28	3.25	0.13	0.31
73.77	19.61	4.23	14.55	61.46	3.28	0.13	0.30
73.86	19.34	4.15	15.21	63.08	3.30	0.15	0.30
73.96	19.38	4.15	15.56	64.61	3.31	0.15	0.30
74.06	19.58	4.20	15.60	65.59	3.32	0.16	0.30
74.13	20.02	4.32	15.32	66.22	3.31	0.16	0.31
74.24	20.36	4.41	15.12	66.66	3.30	0.17	0.31
74.34	20.56	4.46	15.08	67.26	3.30	0.17	0.32
74.44	20.42	4.42	15.35	67.81	3.31	0.18	0.32
74.58	20.37	4.40	15.30	67.28	3.30	0.18	0.31
74.68	20.30	4.38	14.35	62.80	3.27	0.16	0.31
74.80	20.47	4.42	13.30	58.74	3.22	0.09	0.32
74.92	20.26	4.35	12.97	56.43	3.21	0.11	0.31
75.07	20.06	4.29	13.60	58.35	3.24	0.12	0.31
75.08	19.75	4.21	14.10	59.34	3.26	0.12	0.30
75.11	19.62	4.17	14.28	59.53	3.26	0.12	0.30
75.16	19.55	4.15	14.53	60.28	3.27	0.13	0.30
75.25	19.31	4.08	15.14	61.74	3.30	0.13	0.29
75.32	19.14	4.03	15.69	63.23	3.32	0.15	0.29
75.40	18.98	3.98	16.00	63.73	3.33	0.15	0.28
75.50	18.81	3.93	15.96	62.77	3.33	0.14	0.28
75.59	18.30	3.79	16.02	60.75	3.33	0.13	0.27
75.69	17.56	3.59	16.34	58.60	3.34	0.11	0.26
75.78	16.85	3.39	16.66	56.46	3.35	0.11	0.24
75.88	16.41	3.27	16.73	54.66	3.36	0.10	0.23
75.96	16.11	3.18	16.62	52.90	3.35	0.09	0.23
76.05	16.04	3.16	16.34	51.65	3.34	0.08	0.23
76.14	15.97	3.14	16.25	51.00	3.34	0.08	0.22
76.26	16.07	3.16	16.16	51.09	3.34	0.08	0.23
76.36	16.07	3.16	16.26	51.38	3.34	0.08	0.23
76.41	16.07	3.16	16.31	51.50	3.34	0.08	0.23
76.51	15.84	3.09	16.56	51.17	3.35	0.08	0.22
76.65	15.50	2.99	17.04	51.04	3.37	0.08	0.21
76.72	15.26	2.93	17.45	51.12	3.38	0.08	0.21
76.79	15.16	2.90	17.72	51.39	3.39	0.08	0.21
76.89	15.23	2.91	18.36	53.53	3.41	0.08	0.21
76.98	15.47	2.98	20.80	61.89	3.48	0.11	0.21
77.08	18.00	3.65	19.05	69.60	3.43	0.21	0.26
77.18	22.18	4.77	16.19	77.29	3.34	0.23	0.34
77.28	26.73	5.99	14.06	84.26	3.26	0.29	0.43
77.37	27.88	6.30	14.87	93.62	3.29	0.40	0.45
77.42	28.76	6.53	15.41	100.64	3.31	0.49	0.47
77.42	30.22	6.92	15.09	104.44	3.30	0.50	0.49
77.44	34.00	7.94	13.49	107.05	3.23	0.53	0.57
77.48	37.40	8.85	12.47	110.31	3.19	0.60	0.63
77.52	40.61	9.70	11.65	113.00	3.15	0.64	0.69

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
77.54	42.94	10.33	11.08	114.44	3.12	0.66	0.74
77.57	43.37	10.44	11.07	115.54	3.12	0.68	0.75
77.62	42.26	10.14	11.44	115.93	3.14	0.69	0.72
77.65	40.10	9.55	12.10	115.64	3.17	0.66	0.68
77.67	38.72	9.18	12.34	113.32	3.18	0.65	0.66
77.71	37.91	8.96	12.41	111.24	3.19	0.59	0.64
77.71	37.03	8.73	12.35	107.78	3.18	0.58	0.62
77.76	34.77	8.12	12.85	104.25	3.20	0.52	0.58
77.81	31.76	7.31	13.53	98.88	3.23	0.45	0.52
77.90	29.03	6.57	14.40	94.60	3.27	0.39	0.47
77.95	27.32	6.11	15.14	92.44	3.30	0.37	0.44
78.01	26.34	5.84	15.63	91.29	3.32	0.38	0.42
78.10	27.59	6.17	14.49	89.37	3.27	0.35	0.44
78.16	36.29	8.49	9.98	84.71	3.07	0.33	0.61
78.24	48.94	11.86	6.66	79.05	2.86	0.54	0.70
78.29	64.83	16.10	4.54	73.14	2.68	0.33	0.69
78.39	77.42	19.44	3.56	69.27	2.58	0.24	0.68
78.47	87.30	22.06	3.11	68.51	2.52	0.23	0.68
78.53	92.74	23.49	3.05	71.72	2.51	0.29	0.69
78.62	94.25	23.88	3.25	77.71	2.54	0.48	0.70
78.68	91.22	23.06	3.64	84.02	2.59	0.72	0.72
78.69	92.97	23.52	3.81	89.57	2.61	0.73	0.73
78.78	93.95	23.76	4.00	95.10	2.63	0.74	0.74
78.81	94.86	24.00	4.25	102.04	2.65	0.75	0.75
78.92	85.28	21.43	5.01	107.35	2.73	0.76	0.76
79.03	72.83	18.11	5.93	107.43	2.81	0.76	0.76
79.16	68.41	16.91	5.87	99.26	2.80	0.75	0.75
79.26	78.39	19.54	4.53	88.45	2.68	0.73	0.73
79.35	97.35	24.54	3.42	83.92	2.56	0.72	0.72
79.45	114.43	29.03	2.95	85.78	2.50	0.72	0.72
79.54	124.25	31.60	2.84	89.58	2.48	0.73	0.73
79.64	131.23	33.41	2.75	91.91	2.47	0.73	0.73
79.74	153.43	39.23	2.39	93.85	2.40	0.74	0.74
79.88	186.93	48.00	1.98	94.86	2.31	0.74	0.74
79.98	228.94	59.00	1.62	95.73	2.20	0.74	0.74
80.12	248.77	64.13	1.48	95.14	2.14	0.74	0.74
80.22	253.19	65.23	1.40	91.22	2.09	0.73	0.73
80.36	244.79	62.94	1.37	86.07	2.06	0.72	0.72
80.46	238.82	61.33	1.32	81.11	2.02	0.64	0.71
80.60	231.84	59.42	1.30	77.21	1.99	0.46	0.70
80.70	223.91	57.30	1.30	74.37	1.99	0.37	0.69
80.83	213.12	54.42	1.32	72.04	2.02	0.30	0.69
80.94	194.49	49.51	1.41	69.62	2.09	0.25	0.68
81.01	177.96	45.17	1.50	67.91	2.15	0.21	0.68
81.04	164.23	41.58	1.60	66.50	2.19	0.19	0.67
81.09	158.43	40.05	1.65	65.97	2.21	0.18	0.67
81.13	149.59	37.74	1.75	66.04	2.25	0.18	0.67
81.18	136.87	34.41	1.98	67.98	2.31	0.22	0.68

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
81.23	123.31	30.87	2.34	72.13	2.39	0.30	0.69
81.28	109.41	27.24	2.85	77.64	2.48	0.48	0.70
81.33	98.17	24.30	3.46	84.19	2.57	0.72	0.72
81.37	88.49	21.78	4.25	92.48	2.65	0.73	0.73
81.42	81.24	19.88	5.05	100.46	2.73	0.75	0.75
81.47	75.77	18.46	5.75	106.15	2.79	0.76	0.76
81.52	71.99	17.47	6.25	109.13	2.83	0.76	0.76
81.56	70.98	17.20	6.46	111.09	2.85	0.77	0.77
81.61	70.58	17.08	6.60	112.75	2.86	0.77	0.77
81.64	68.79	16.62	6.89	114.41	2.88	0.77	0.77
81.70	62.18	14.89	7.85	116.91	2.94	0.78	0.78
81.75	54.38	12.87	9.25	118.94	3.03	0.76	0.92
81.79	46.89	10.92	10.91	119.14	3.11	0.73	0.78
81.82	41.90	9.62	12.12	116.62	3.17	0.68	0.69
81.86	37.62	8.51	13.21	112.49	3.22	0.61	0.61
81.91	34.01	7.57	14.21	107.66	3.26	0.54	0.54
81.95	30.63	6.70	15.27	102.27	3.30	0.48	0.48
82.00	27.33	5.84	16.41	95.81	3.34	0.41	0.42
82.09	24.26	5.04	17.74	89.46	3.39	0.33	0.36
82.15	21.66	4.37	19.38	84.64	3.44	0.29	0.31
82.19	19.83	3.89	20.80	81.03	3.48	0.27	0.28
82.26	18.38	3.52	22.06	77.56	3.52	0.23	0.25
82.34	17.00	3.16	23.49	74.17	3.56	0.21	0.23
82.39	15.65	2.81	25.58	71.81	3.61	0.20	0.20
82.48	14.77	2.58	27.14	69.97	3.64	0.18	0.18
82.58	14.64	2.54	26.84	68.21	3.64	0.17	0.18
82.62	14.74	2.57	25.95	66.60	3.62	0.16	0.18
82.70	14.88	2.60	25.23	65.56	3.60	0.15	0.19
82.77	14.81	2.58	24.98	64.46	3.59	0.15	0.18
82.87	15.08	2.65	24.19	64.01	3.57	0.14	0.19
82.96	16.23	2.94	21.57	63.38	3.51	0.14	0.21
83.06	18.22	3.45	18.38	63.34	3.41	0.14	0.25
83.16	21.39	4.26	14.82	63.10	3.29	0.14	0.30
83.25	24.46	5.04	12.49	62.94	3.19	0.15	0.36
83.34	27.20	5.74	10.91	62.57	3.11	0.15	0.41
83.44	28.34	6.03	10.55	63.55	3.10	0.15	0.43
83.54	28.75	6.12	10.60	64.89	3.10	0.17	0.44
83.64	28.61	6.08	10.93	66.49	3.12	0.17	0.43
83.73	27.70	5.84	11.68	68.29	3.15	0.18	0.42
83.83	27.26	5.73	12.30	70.46	3.18	0.20	0.41
83.85	26.83	5.62	13.07	73.38	3.21	0.21	0.40
83.89	27.47	5.78	13.14	75.93	3.22	0.24	0.41
83.94	28.11	5.94	13.69	81.26	3.24	0.26	0.42
84.04	29.26	6.23	13.80	85.92	3.25	0.34	0.44
84.09	30.40	6.51	13.83	90.10	3.25	0.36	0.47
84.13	31.28	6.74	13.65	91.94	3.24	0.37	0.48
84.18	31.68	6.83	13.70	93.61	3.24	0.40	0.49
84.25	31.52	6.79	13.97	94.85	3.25	0.41	0.48

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
84.33	30.64	6.56	14.57	95.60	3.28	0.41	0.47
84.37	29.46	6.26	15.33	95.90	3.31	0.41	0.45
84.46	28.35	5.97	15.91	94.98	3.33	0.41	0.43
84.52	27.50	5.75	16.25	93.43	3.34	0.38	0.41
84.57	26.90	5.59	16.32	91.27	3.34	0.36	0.40
84.67	26.52	5.49	16.38	90.00	3.34	0.34	0.39
84.71	26.15	5.40	16.62	89.72	3.35	0.34	0.39
84.81	25.58	5.25	17.32	90.86	3.38	0.35	0.37
84.86	24.84	5.06	18.32	92.62	3.41	0.37	0.36
84.91	24.06	4.86	19.36	94.03	3.44	0.38	0.35
85.00	23.42	4.69	20.18	94.63	3.47	0.39	0.33
85.05	22.81	4.53	20.72	93.94	3.48	0.39	0.32
85.15	22.34	4.41	20.94	92.30	3.49	0.36	0.31
85.19	21.80	4.27	20.88	89.13	3.49	0.34	0.30
85.29	21.33	4.15	20.74	85.98	3.48	0.30	0.30
85.35	20.72	3.99	20.84	83.14	3.49	0.28	0.28
85.42	20.08	3.82	21.32	81.54	3.50	0.27	0.27
85.48	19.40	3.65	22.03	80.45	3.52	0.26	0.26
85.55	18.77	3.49	22.80	79.50	3.54	0.25	0.25
85.63	18.19	3.34	23.58	78.76	3.56	0.25	0.24
85.68	17.62	3.19	24.50	78.25	3.58	0.24	0.23
85.77	17.18	3.08	25.34	78.03	3.60	0.24	0.22
85.82	17.04	3.04	25.74	78.34	3.61	0.24	0.22
85.89	17.42	3.13	25.13	78.79	3.60	0.25	0.22
85.96	18.33	3.36	23.51	79.01	3.56	0.25	0.24
86.03	19.71	3.71	21.16	78.44	3.49	0.25	0.26
86.11	21.06	4.04	19.14	77.40	3.44	0.24	0.29
86.16	22.11	4.30	17.71	76.21	3.39	0.23	0.31
86.25	21.67	4.19	18.09	75.81	3.40	0.22	0.30
86.36	19.98	3.76	19.76	74.32	3.45	0.23	0.27
86.50	18.16	3.30	22.08	72.85	3.52	0.19	0.24
86.51	17.25	3.07	23.09	70.91	3.55	0.19	0.22
86.52	17.32	3.09	22.53	69.58	3.53	0.19	0.22
86.57	17.35	3.10	21.58	66.80	3.51	0.17	0.22
86.65	17.39	3.10	20.48	63.50	3.48	0.13	0.22
86.71	17.35	3.09	19.65	60.73	3.45	0.13	0.22
86.80	17.08	3.02	19.57	59.11	3.45	0.12	0.22
86.90	16.48	2.87	20.04	57.42	3.46	0.11	0.20
86.99	15.77	2.69	20.75	55.74	3.48	0.10	0.19
87.04	15.26	2.56	21.24	54.32	3.50	0.09	0.18
87.14	15.16	2.53	21.16	53.51	3.49	0.09	0.18
87.19	15.36	2.58	20.70	53.36	3.48	0.09	0.18
87.28	15.87	2.70	20.13	54.40	3.46	0.09	0.19
87.38	16.51	2.86	19.47	55.67	3.45	0.10	0.20
87.43	17.18	3.03	18.79	56.85	3.42	0.11	0.22
87.52	17.76	3.17	18.12	57.36	3.40	0.11	0.23
87.61	18.23	3.28	17.55	57.58	3.38	0.11	0.23
87.66	18.53	3.35	17.13	57.47	3.37	0.11	0.24

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
87.76	18.57	3.36	17.00	57.12	3.37	0.11	0.24
87.84	18.43	3.32	17.02	56.58	3.37	0.10	0.24
87.91	18.13	3.25	17.27	56.08	3.37	0.10	0.23
88.00	17.79	3.16	17.58	55.54	3.39	0.10	0.23
88.11	17.46	3.07	17.98	55.23	3.40	0.10	0.22
88.19	17.22	3.01	18.27	55.01	3.41	0.10	0.22
88.25	17.08	2.98	18.42	54.79	3.41	0.10	0.21
88.34	17.02	2.96	18.36	54.27	3.41	0.09	0.21
88.44	16.98	2.94	18.20	53.59	3.41	0.09	0.21
88.54	16.98	2.94	17.99	52.93	3.40	0.09	0.21
88.64	16.95	2.93	17.92	52.52	3.40	0.08	0.21
88.72	16.88	2.91	18.00	52.42	3.40	0.08	0.21
88.82	16.82	2.89	18.16	52.53	3.40	0.08	0.21
88.91	16.72	2.87	18.42	52.79	3.41	0.08	0.20
89.01	16.62	2.84	18.68	53.02	3.42	0.09	0.20
89.10	16.49	2.80	18.99	53.22	3.43	0.09	0.20
89.19	16.32	2.76	19.19	52.91	3.44	0.09	0.20
89.30	16.21	2.73	18.48	50.44	3.41	0.08	0.19
89.39	16.31	2.75	17.80	48.98	3.39	0.05	0.20
89.49	16.62	2.82	17.53	49.49	3.38	0.07	0.20
89.59	16.90	2.89	18.25	52.76	3.41	0.09	0.21
89.69	17.04	2.92	18.79	54.90	3.42	0.10	0.21
89.73	17.68	3.08	18.14	55.86	3.40	0.10	0.22
89.78	18.48	3.27	17.18	56.23	3.37	0.10	0.23
89.83	19.36	3.49	16.22	56.56	3.34	0.10	0.25
89.88	19.63	3.55	16.06	57.05	3.33	0.11	0.25
89.93	19.86	3.61	16.01	57.77	3.33	0.11	0.26
90.00	20.24	3.70	15.90	58.79	3.33	0.11	0.26
90.07	20.88	3.85	15.53	59.82	3.31	0.12	0.28
90.12	21.62	4.03	15.19	61.24	3.30	0.13	0.29
90.22	22.26	4.19	15.01	62.84	3.29	0.14	0.30
90.27	23.04	4.37	15.02	65.70	3.29	0.15	0.31
90.36	24.99	4.85	14.09	68.34	3.26	0.18	0.35
90.46	27.46	5.45	12.89	70.27	3.21	0.20	0.39
90.50	29.28	5.89	12.05	71.01	3.17	0.20	0.42
90.61	29.48	5.94	12.02	71.39	3.17	0.20	0.42
90.66	28.70	5.75	12.38	71.12	3.18	0.20	0.41
90.75	27.62	5.48	12.73	69.74	3.20	0.19	0.39
90.84	26.17	5.12	13.28	67.94	3.22	0.17	0.37
90.89	24.72	4.76	13.90	66.20	3.25	0.16	0.34
90.99	23.48	4.45	14.63	65.12	3.28	0.15	0.32
91.04	22.50	4.21	15.24	64.21	3.30	0.15	0.30
91.14	21.59	3.99	15.98	63.69	3.33	0.14	0.28
91.22	20.75	3.78	16.73	63.19	3.36	0.14	0.27
91.28	19.83	3.55	17.61	62.55	3.39	0.14	0.25
91.37	19.26	3.41	18.11	61.75	3.40	0.13	0.24
91.47	18.99	3.34	18.18	60.75	3.40	0.13	0.24
91.61	19.26	3.40	17.69	60.19	3.39	0.12	0.24

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
91.71	19.40	3.43	17.48	59.97	3.38	0.12	0.25
91.81	19.50	3.45	17.39	60.03	3.38	0.12	0.25
91.87	19.36	3.42	17.46	59.68	3.38	0.12	0.24
92.00	19.38	3.42	16.82	57.50	3.36	0.12	0.24
92.10	19.41	3.42	16.30	55.77	3.34	0.09	0.24
92.20	19.62	3.47	15.85	54.98	3.32	0.09	0.25
92.33	19.76	3.50	16.12	56.37	3.33	0.10	0.25
92.38	19.89	3.53	16.27	57.43	3.34	0.11	0.25
92.43	20.03	3.56	16.28	57.96	3.34	0.11	0.25
92.48	19.98	3.55	16.52	58.57	3.35	0.11	0.25
92.56	19.88	3.52	16.79	59.09	3.36	0.12	0.25
92.63	19.64	3.46	17.17	59.41	3.37	0.12	0.25
92.67	19.57	3.44	17.27	59.42	3.37	0.12	0.25
92.72	19.54	3.43	17.30	59.38	3.38	0.12	0.25
92.77	19.64	3.46	17.18	59.37	3.37	0.12	0.25
92.86	19.84	3.50	16.99	59.49	3.37	0.12	0.25
92.92	20.08	3.56	16.84	59.88	3.36	0.12	0.25
92.97	20.21	3.59	17.01	61.03	3.37	0.12	0.26
93.05	20.35	3.62	17.17	62.12	3.37	0.14	0.26
93.10	20.62	3.68	17.13	63.07	3.37	0.14	0.26
93.16	21.10	3.79	16.68	63.28	3.35	0.14	0.27
93.25	21.70	3.94	16.06	63.20	3.33	0.14	0.28
93.35	22.78	4.19	14.99	62.84	3.29	0.14	0.30
93.40	23.19	4.29	14.52	62.27	3.27	0.14	0.31
93.49	23.25	4.30	14.38	61.82	3.27	0.13	0.31
93.56	22.71	4.17	14.77	61.55	3.28	0.13	0.30
93.64	22.88	4.21	14.66	61.65	3.28	0.13	0.30
93.73	23.63	4.38	14.34	62.81	3.27	0.13	0.31
93.83	24.91	4.69	13.81	64.72	3.25	0.15	0.33
93.88	26.43	5.05	13.44	67.85	3.23	0.17	0.36
93.97	27.01	5.18	13.58	70.35	3.24	0.20	0.37
94.07	26.43	5.04	14.48	72.95	3.27	0.20	0.36
94.17	25.76	4.87	15.51	75.57	3.31	0.22	0.35
94.26	26.70	5.09	15.04	76.60	3.29	0.25	0.36
94.36	27.88	5.37	15.22	81.75	3.30	0.23	0.38
94.45	29.47	5.75	15.14	87.02	3.30	0.34	0.41
94.55	35.88	7.27	12.61	91.74	3.19	0.39	0.52
94.64	48.46	10.27	8.71	89.52	3.00	0.73	0.73
94.72	59.93	13.01	6.55	85.22	2.85	0.72	0.72
94.74	73.87	16.33	4.89	79.85	2.72	0.58	0.71
94.77	84.50	18.86	4.08	76.98	2.64	0.45	0.70
94.85	97.35	21.92	3.39	74.39	2.56	0.37	0.69
94.90	102.75	23.20	3.24	75.17	2.54	0.39	0.70
94.95	105.32	23.80	3.27	77.89	2.54	0.49	0.70
95.01	104.68	23.63	3.61	85.22	2.58	0.72	0.72
95.09	100.83	22.70	4.16	94.37	2.64	0.74	0.74
95.14	94.49	21.18	5.05	107.02	2.73	0.76	0.76
95.23	86.42	19.25	6.10	117.34	2.82	0.78	0.78

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
95.29	78.06	17.25	7.36	126.89	2.91	0.79	0.79
95.38	71.11	15.59	8.45	131.69	2.98	0.80	0.80
95.43	67.53	14.73	9.06	133.43	3.02	0.97	1.05
95.52	67.83	14.79	8.96	132.50	3.01	0.95	1.06
95.57	70.23	15.35	8.40	128.95	2.98	0.80	0.80
95.67	71.24	15.58	7.93	123.49	2.95	0.79	0.79
95.77	66.52	14.45	8.22	118.72	2.97	0.78	0.78
95.86	56.97	12.17	9.76	118.80	3.06	0.69	0.87
95.95	52.94	11.21	10.40	116.56	3.09	0.74	0.80
96.03	46.73	9.74	12.16	118.40	3.17	0.62	0.70
96.11	51.55	10.87	10.92	118.64	3.12	0.68	0.78
96.20	59.20	12.66	9.84	124.65	3.06	0.80	0.90
96.30	80.15	17.59	7.15	125.73	2.90	0.79	0.79
96.39	101.37	22.58	5.51	124.50	2.77	0.79	0.79
96.50	122.96	27.64	4.35	120.31	2.67	0.78	0.78
96.59	144.96	32.80	3.25	106.72	2.54	0.76	0.76
96.69	164.86	37.45	2.44	91.36	2.41	0.73	0.73
96.78	180.18	41.02	1.89	77.51	2.29	0.47	0.70
96.87	185.95	42.35	1.72	72.98	2.24	0.33	0.69
96.98	185.28	42.15	1.69	71.40	2.23	0.29	0.69
97.02	177.79	40.38	1.78	71.90	2.26	0.30	0.69
97.06	176.40	40.04	1.83	73.47	2.27	0.34	0.69
97.12	175.60	39.84	1.91	76.16	2.30	0.42	0.70
97.16	176.98	40.15	1.98	79.48	2.31	0.56	0.71
97.21	173.67	39.35	2.13	83.99	2.35	0.72	0.72
97.27	170.50	38.59	2.31	89.17	2.39	0.73	0.73
97.33	168.21	38.04	2.46	93.67	2.42	0.74	0.74
97.40	165.98	37.49	2.57	96.33	2.44	0.74	0.74
97.45	163.92	37.00	2.64	97.51	2.45	0.74	0.74
97.50	161.39	36.39	2.76	100.38	2.47	0.75	0.75
97.58	155.82	35.06	2.99	104.78	2.50	0.76	0.76
97.65	146.95	32.97	3.34	110.26	2.55	0.77	0.77
97.69	134.43	30.04	3.79	113.95	2.60	0.77	0.77
97.74	121.75	27.07	4.27	115.68	2.66	0.78	0.78
97.81	110.51	24.44	4.76	116.42	2.71	0.78	0.78
97.88	103.09	22.69	5.14	116.63	2.74	0.78	0.78
97.93	108.66	23.98	4.67	111.98	2.70	0.77	0.77
98.03	138.72	30.95	3.15	97.35	2.52	0.74	0.74
98.15	182.62	41.12	2.03	83.50	2.33	0.71	0.71
98.21	228.43	51.75	1.51	78.05	2.15	0.50	0.70
98.32	264.20	60.00	1.34	80.19	2.03	0.59	0.71
98.42	301.85	68.69	1.25	85.96	1.92	0.72	0.72
98.47	349.59	79.73	1.00	79.73	1.79	0.57	0.71
98.57	388.76	88.75	1.00	88.75	1.69	0.73	0.73
98.70	411.84	94.00	1.00	94.00	1.61	0.74	0.74
98.78	404.01	92.13	1.00	92.13	1.62	0.73	0.73
98.85	372.43	84.79	1.00	84.79	1.67	0.72	0.72
98.86	337.78	76.77	1.00	76.77	1.74	0.45	0.70

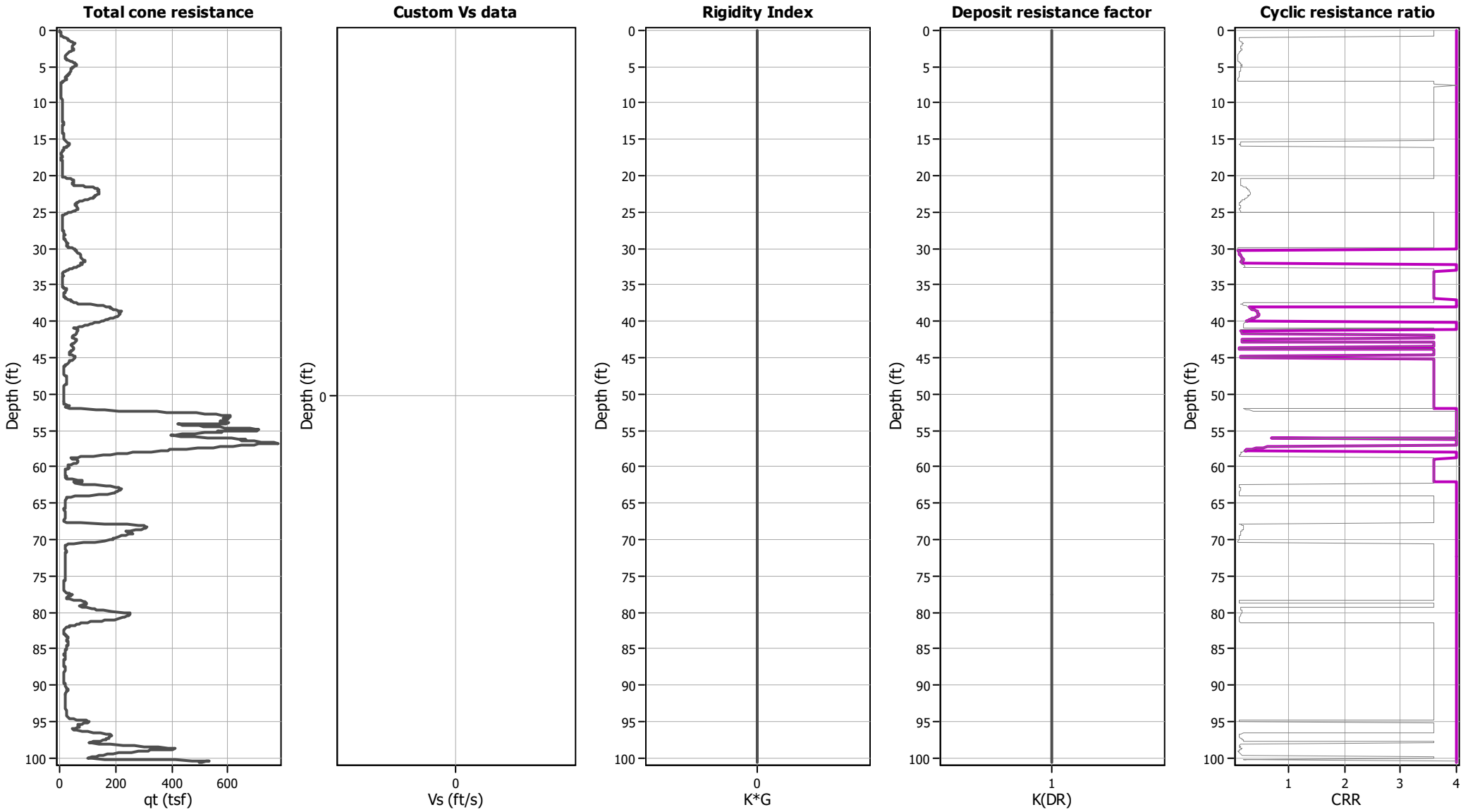
:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
98.92	322.73	73.26	1.00	73.26	1.77	0.33	0.69
98.98	318.48	72.24	1.00	72.24	1.78	0.31	0.69
99.03	309.41	70.12	1.00	70.12	1.81	0.26	0.68
99.11	281.64	63.67	1.00	63.67	1.90	0.15	0.67
99.18	255.32	57.57	1.30	74.69	1.99	0.38	0.69
99.23	231.33	52.01	1.41	73.25	2.09	0.33	0.69
99.32	209.84	47.02	1.62	76.01	2.20	0.42	0.70
99.37	189.39	42.29	1.96	83.05	2.31	0.71	0.71
99.45	170.57	37.93	2.37	90.04	2.40	0.73	0.73
99.56	157.24	34.83	2.76	96.01	2.47	0.74	0.74
99.64	147.39	32.55	3.13	101.90	2.52	0.75	0.75
99.71	140.04	30.84	3.53	108.77	2.57	0.76	0.76
99.75	128.26	28.12	4.04	113.72	2.63	0.77	0.77
99.90	116.32	25.35	4.67	118.27	2.70	0.78	0.78
99.95	101.78	22.01	5.75	126.55	2.79	0.79	0.79
100.04	116.32	25.32	5.03	127.45	2.73	0.79	0.79
100.14	159.30	35.14	3.33	116.89	2.55	0.78	0.78
100.14	204.99	45.59	2.33	106.43	2.39	0.76	0.76
100.15	235.79	52.64	2.00	105.52	2.32	0.76	0.76
100.19	258.80	57.89	1.93	111.71	2.30	0.77	0.77
100.21	298.07	66.86	1.78	119.29	2.26	0.78	0.78
100.24	351.88	79.16	1.37	108.37	2.06	0.76	0.76
100.28	410.56	92.54	1.15	106.62	1.80	0.76	0.76
100.31	470.98	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.33	508.57	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.38	524.63	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.39	526.55	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.43	531.78	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.48	522.24	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.53	509.38	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.57	496.12	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.60	497.27	-1.00	1.00	-1.00	-1.00	0.00	0.00

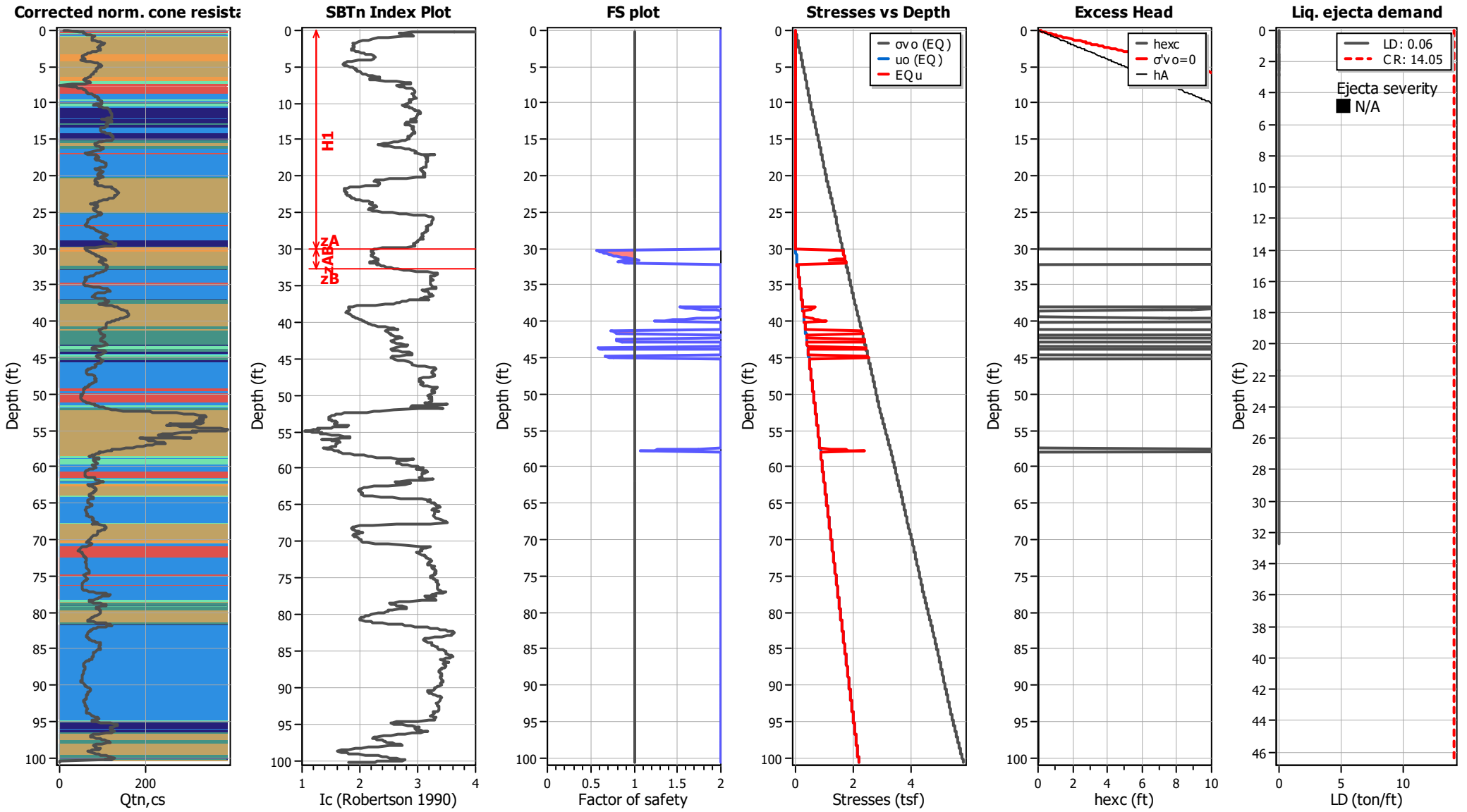
Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Aging Calculation Estimation

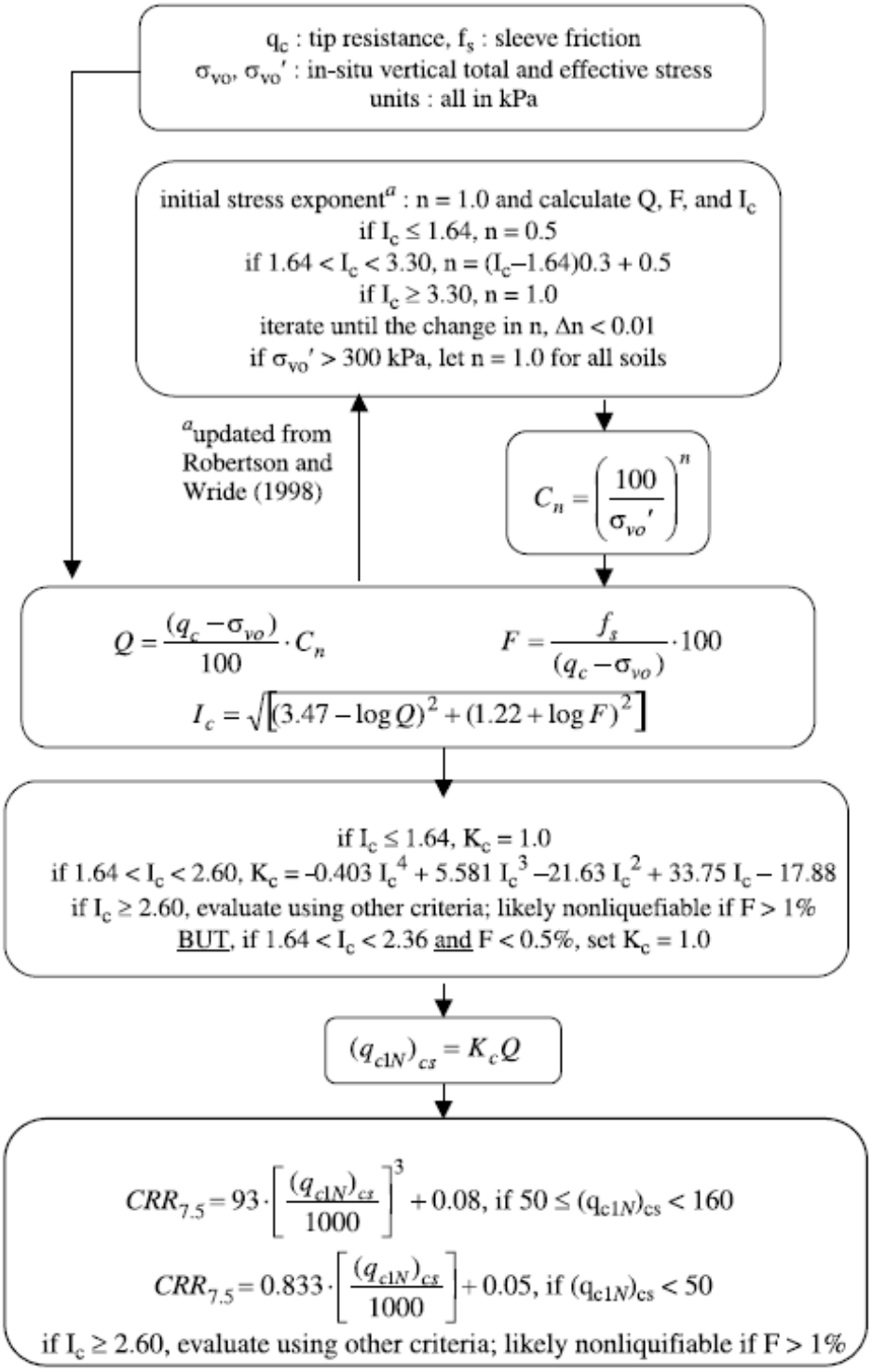


Ejecta Severity Estimation



Procedure for the evaluation of soil liquefaction resistance, NCEER (1998)

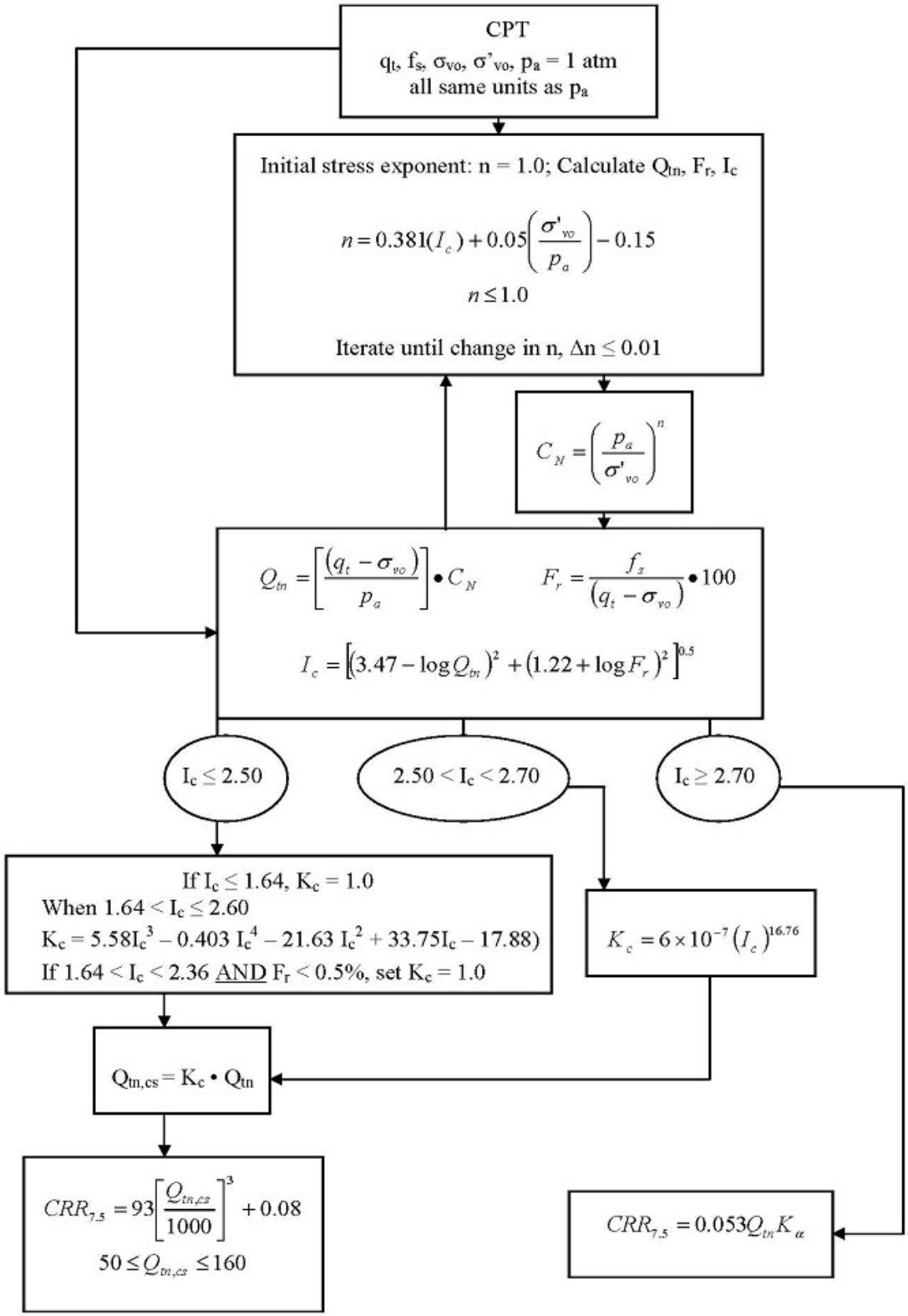
Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. The procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart[1]:



[1] "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

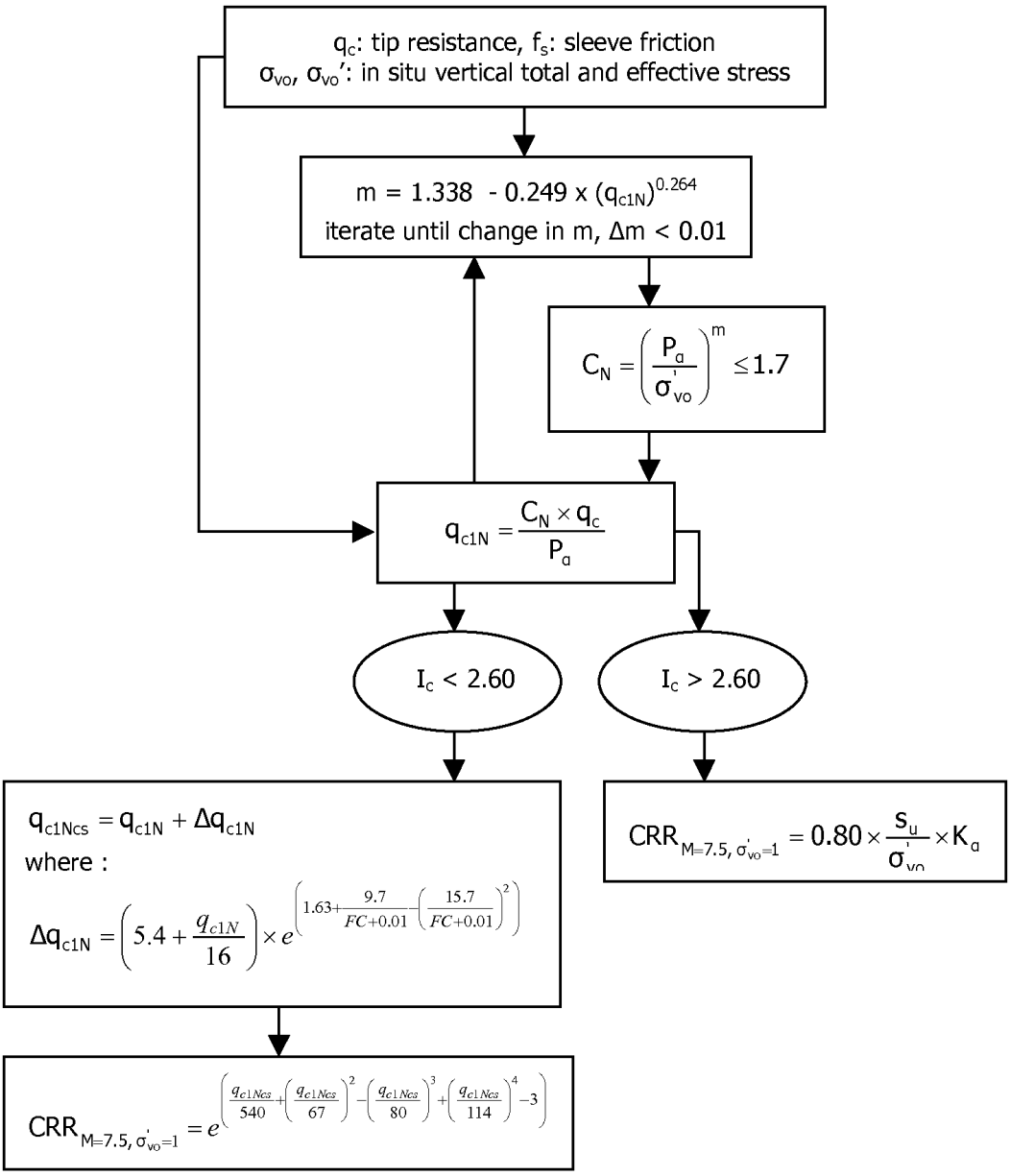
Procedure for the evaluation of soil liquefaction resistance (all soils), Robertson (2010)

Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. This procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart[1]:

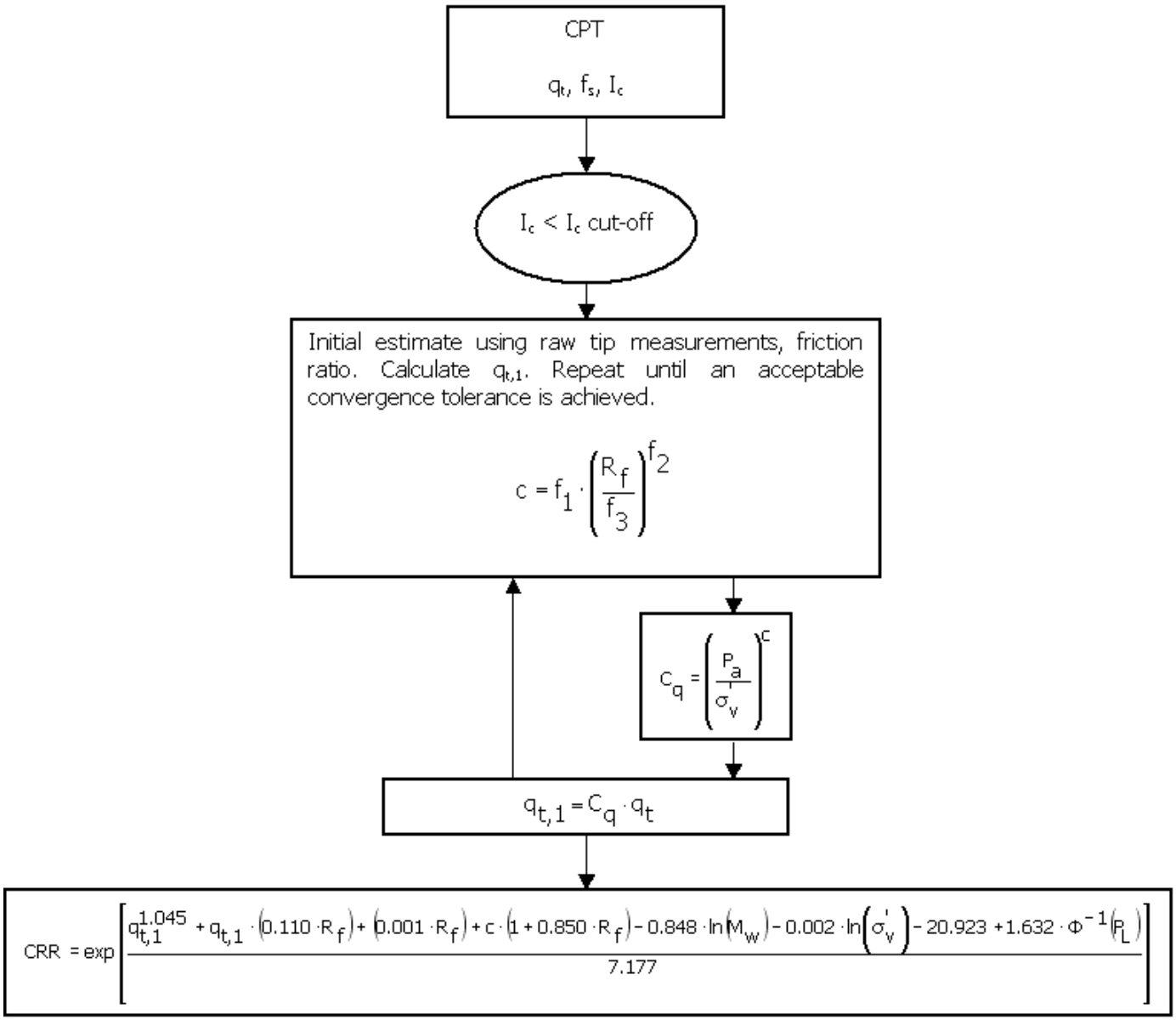


[1] P.K. Robertson, 2009. "Performance based earthquake design using the CPT", Keynote Lecture, International Conference on Performance-based Design in Earthquake Geotechnical Engineering – from case history to practice, IS-Tokyo, June 2009

Procedure for the evaluation of soil liquefaction resistance, Idriss & Boulanger (2008)



Procedure for the evaluation of soil liquefaction resistance (sandy soils), Moss et al. (2006)



Procedure for the evaluation of soil liquefaction resistance, Boulanger & Idriss(2014)

$$FS_{liq} = \frac{CRR_{M=7.5,\sigma'_v=1atm}}{CSR_{M=7.5,\sigma'_v=1atm}}$$

$$CSR_{M=7.5,\sigma'_v=1atm} = 0.65 \frac{\sigma_v}{\sigma'_v} \frac{a_{max}}{g} r_d \frac{1}{MSF} \frac{1}{K_\sigma}$$

$$r_d = \exp\left[\alpha(z) + \beta(z) \cdot M\right]$$

$$\alpha(z) = -1.012 - 1.126 \sin\left(\frac{z}{11.73} + 5.133\right)$$

$$\beta(z) = 0.106 + 0.118 \sin\left(\frac{z}{11.28} + 5.142\right)$$

$$K_\sigma = 1 - C_\sigma \ln\left(\frac{\sigma'_v}{P_a}\right) \le 1.1$$

$$C_\sigma = \frac{1}{37.3 - 8.27\left(q_{c1Ncs}\right)^{0.264}} \le 0.3$$

$$MSF = 1 + \left(MSF_{max} - 1\right)\left(8.64 \exp\left(\frac{-M}{4}\right) - 1.325\right)$$

$$MSF_{max} = 1.09 + \left(\frac{q_{C1Ncs}}{180}\right)^3 \le 2.2$$

σ'_v *and* σ_v *at start of earthquake shaking*

$$CRR_{M=7.5,\sigma'_v=1atm} = \exp\left(\frac{q_{c1Ncs}}{113} + \left(\frac{q_{c1Ncs}}{1000}\right)^2 - \left(\frac{q_{c1Ncs}}{140}\right)^3 + \left(\frac{q_{c1Ncs}}{137}\right)^4 - 2.80\right)$$

$$q_{c1Ncs} = q_{c1N} + \Delta q_{c1N}$$

$$\Delta q_{c1N} = \left(11.9 + \frac{q_{c1N}}{14.6}\right) \exp\left(1.63 - \frac{9.7}{FC+2} - \left(\frac{15.7}{FC+2}\right)^2\right)$$

$$q_{c1N} = C_{Ne} \frac{q_c}{P_a}$$

$$C_{Ne} = \left(\frac{P_a}{\sigma'_v}\right)^m \le 1.7$$

$$m = 1.338 - 0.249\left(q_{c1Ncs}\right)^{0.264} \quad with \quad 0.264 \le m \le 0.782$$

$$FC = 80\left(I_C + C_{FC}\right) - 137 \quad with \quad 0\% \le FC \le 100\%$$

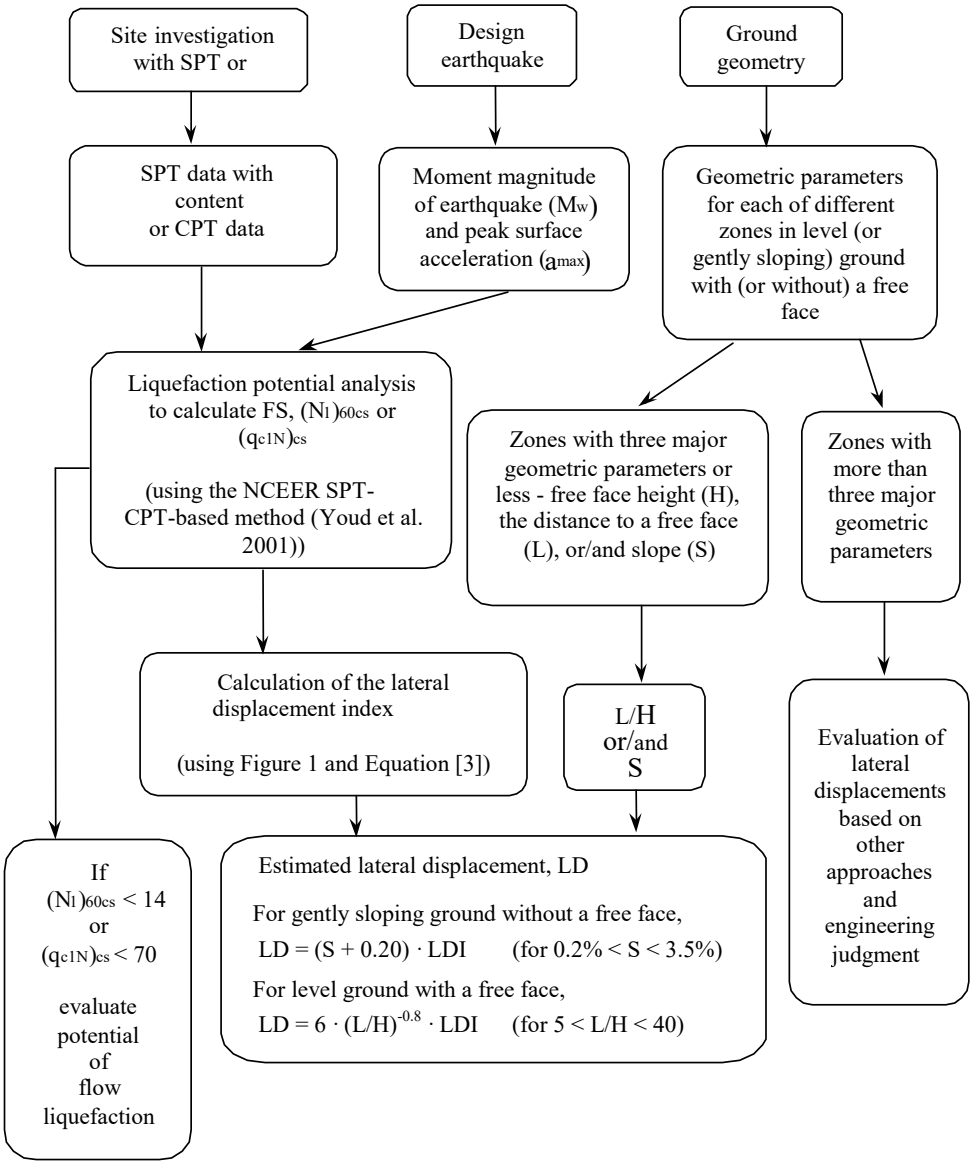
$$I_c = \left[\left(3.47 - \log\left(Q\right)\right)^2 + \left(1.22 + \log\left(F\right)\right)^2\right]^{0.5}$$

$$Q = \left(\frac{q_c - \sigma_{vc}}{P_a}\right)\left(\frac{P_a}{\sigma'_{vc}}\right)^n \; with \; 0.5 \le n \le 1.0 \; per \; Robertson \; \& \; Wride \; (1998)$$

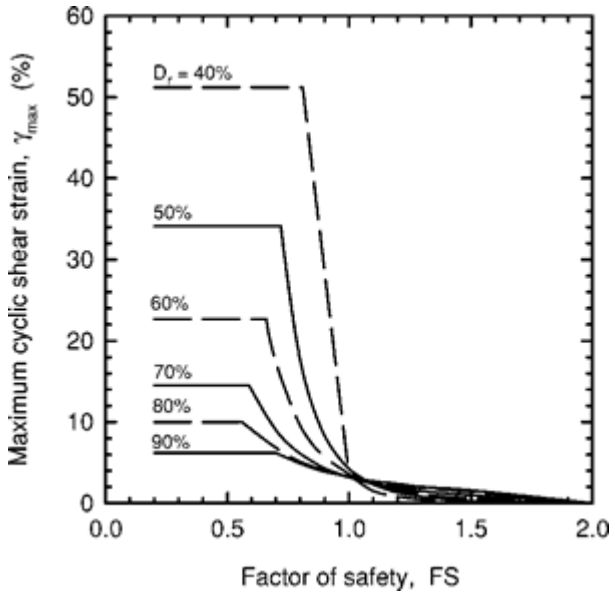
$$F = \left(\frac{f_s}{q_c - \sigma_{vc}}\right) \cdot 100\%$$

σ'_v *at time of CPT sounding*

Procedure for the evaluation of liquefaction-induced lateral spreading displacements



[1] Flow chart illustrating major steps in estimating liquefaction-induced lateral spreading displacements using the proposed approach



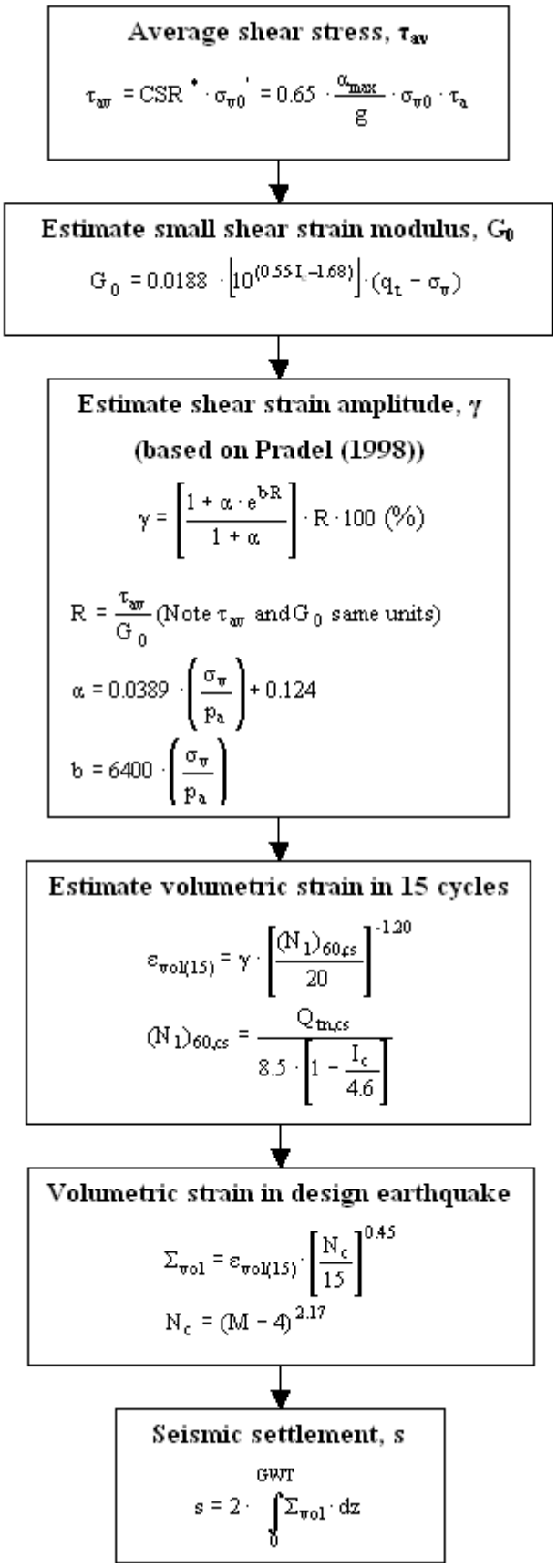
[1] Figure 1

$$LDI = \int_0^{z_{max}} \gamma_{max} dz$$

[1] Equation [3]

[1] "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

Procedure for the estimation of seismic induced settlements in dry sands



Robertson, P.K. and Lisheng, S., 2010, "Estimation of seismic compression in dry soils using the CPT" FIFTH INTERNATIONAL CONFERENCE ON RECENT ADVANCES IN GEOTECHNICAL EARTHQUAKE ENGINEERING AND SOIL DYNAMICS, Symposium in honor of professor I. M. Idriss, San Diego, CA

Liquefaction Potential Index (LPI) calculation procedure

Calculation of the Liquefaction Potential Index (LPI) is used to interpret the liquefaction assessment calculations in terms of severity over depth. The calculation procedure is based on the methology developed by Iwasaki (1982) and is adopted by AFPS.

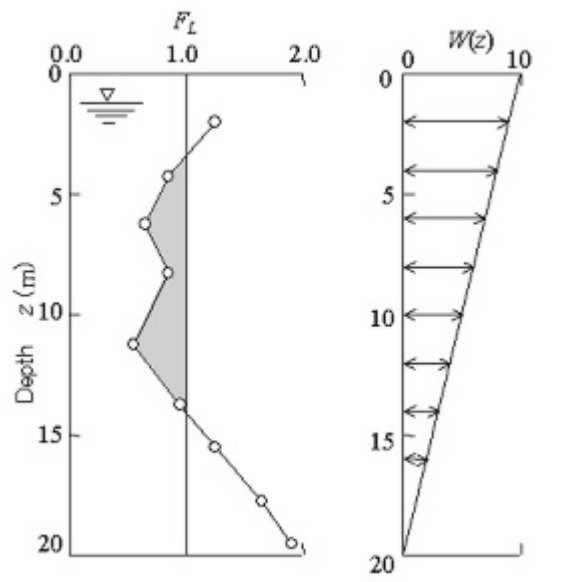
To estimate the severity of liquefaction extent at a given site, LPI is calculated based on the following equation:

$$\mathbf{LPI} = \int_0^{20} (10 - 0{,}5z) \times F_L \times dz$$

where:
F_L = 1 - F.S. when F.S. less than 1
F_L = 0 when F.S. greater than 1
z depth of measurment in meters

Values of LPI range between zero (0) when no test point is characterized as liquefiable and 100 when all points are characterized as susceptible to liquefaction. Iwasaki proposed four (4) discrete categories based on the numeric value of LPI:

- LPI = 0 : Liquefaction risk is very low
- 0 < LPI <= 5 : Liquefaction risk is low
- 5 < LPI <= 15 : Liquefaction risk is high
- LPI > 15 : Liquefaction risk is very high



Graphical presentation of the LPI calculation procedure

Shear-Induced Building Settlement (Ds) calculation procedure

The shear-induced building settlement (Ds) due to liquefaction below the building can be estimated using the relationship developed by Bray and Macedo (2017):

$$Ln(Ds) = c1 + c2 * LBS + 0.58 * Ln\left(Tanh\left(\frac{HL}{6}\right)\right) + 4.59 * Ln(Q) - 0.42 * Ln(Q)^2 - 0.02 * B + 0.84 * Ln(CAVdp) + 0.41 * Ln(Sa1) + \varepsilon$$

where Ds is in the units of mm, c1= -8.35 and c2= 0.072 for LBS ≤ 16, and c1= -7.48 and c2= 0.014 otherwise. Q is the building contact pressure in units of kPa, HL is the cumulative thickness of the liquefiable layers in the units of m, B is the building width in the units of m, CAVdp is a standardized version of the cumulative absolute velocity in the units of g-s, Sa1 is 5%-damped pseudo-acceleration response spectral value at a period of 1 s in the units of g, and ε is a normal random variable with zero mean and 0.50 standard deviation in Ln units. The liquefaction-induced building settlement index (LBS) is:

$$LBS = \sum W * \frac{\varepsilon_{shear}}{z} dz$$

where z (m) is the depth measured from the ground surface > 0, W is a foundation-weighting factor wherein W = 0.0 for z less than Df, which is the embedment depth of the foundation, and W = 1.0 otherwise. The shear strain parameter (ε_shear) is the liquefaction-induced free-field shear strain (in %) estimated using Zhang et al. (2004). It is calculated based on the estimated Dr of the liquefied soil layer and the calculated safety factor against liquefaction triggering (FSL).

References

- Lunne, T., Robertson, P.K., and Powell, J.J.M 1997. Cone penetration testing in geotechnical practice, E & FN Spon Routledge, 352 p, ISBN 0-7514-0393-8.
- Boulanger, R.W. and Idriss, I. M., 2007. Evaluation of Cyclic Softening in Silts and Clays. ASCE Journal of Geotechnical and Geoenvironmental Engineering June, Vol. 133, No. 6 pp 641-652
- Boulanger, R.W. and Idriss, I. M., 2014. CPT AND SPT BASED LIQUEFACTION TRIGGERING PROCEDURES. DEPARTMENT OF CIVIL & ENVIRONMENTAL ENGINEERING COLLEGE OF ENGINEERING UNIVERSITY OF CALIFORNIA AT DAVIS
- Robertson, P.K. and Cabal, K.L., 2007, Guide to Cone Penetration Testing for Geotechnical Engineering. Available at no cost at http://www.geologismiki.gr/
- Robertson, P.K. 1990. Soil classification using the cone penetration test. Canadian Geotechnical Journal, 27 (1), 151-8.
- Robertson, P.K. and Wride, C.E., 1998. Cyclic Liquefaction and its Evaluation based on the CPT Canadian Geotechnical Journal, 1998, Vol. 35, August.
- Youd, T.L., Idriss, I.M., Andrus, R.D., Arango, I., Castro, G., Christian, J.T., Dobry, R., Finn, W.D.L., Harder, L.F., Hynes, M.E., Ishihara, K., Koester, J., Liao, S., Marcuson III, W.F., Martin, G.R., Mitchell, J.K., Moriwaki, Y., Power, M.S., Robertson, P.K., Seed, R., and Stokoe, K.H., Liquefaction Resistance of Soils: Summary Report from the 1996 NCEER and 1998 NCEER/NSF Workshop on Evaluation of Liquefaction Resistance of Soils, ASCE, Journal of Geotechnical & Geoenvironmental Engineering, Vol. 127, October, pp 817-833
- Zhang, G., Robertson. P.K., Brachman, R., 2002, Estimating Liquefaction Induced Ground Settlements from the CPT, Canadian Geotechnical Journal, 39: pp 1168-1180
- Zhang, G., Robertson. P.K., Brachman, R., 2004, Estimating Liquefaction Induced Lateral Displacements using the SPT and CPT, ASCE, Journal of Geotechnical & Geoenvironmental Engineering, Vol. 130, No. 8, 861-871
- Pradel, D., 1998, Procedure to Evaluate Earthquake-Induced Settlements in Dry Sandy Soils, ASCE, Journal of Geotechnical & Geoenvironmental Engineering, Vol. 124, No. 4, 364-368
- Iwasaki, T., 1986, Soil liquefaction studies in Japan: state-of-the-art, Soil Dynamics and Earthquake Engineering, Vol. 5, No. 1, 2-70
- Papathanassiou G., 2008, LPI-based approach for calibrating the severity of liquefaction-induced failures and for assessing the probability of liquefaction surface evidence, Eng. Geol. 96:94–104
- P.K. Robertson, 2009, Interpretation of Cone Penetration Tests - a unified approach., Canadian Geotechnical Journal, Vol. 46, No. 11, pp 1337-1355
- P.K. Robertson, 2009. "Performance based earthquake design using the CPT", Keynote Lecture, International Conference on Performance-based Design in Earthquake Geotechnical Engineering - from case history to practice, IS-Tokyo, June 2009
- Robertson, P.K. and Lisheng, S., 2010, "Estimation of seismic compression in dry soils using the CPT" FIFTH INTERNATIONAL CONFERENCE ON RECENT ADVANCES IN GEOTECHNICAL EARTHQUAKE ENGINEERING AND SOIL DYNAMICS, *Symposium in honor of professor I. M. Idriss,* SAN diego, CA
- R. E. S. Moss, R. B. Seed, R. E. Kayen, J. P. Stewart, A. Der Kiureghian, K. O. Cetin, CPT-Based Probabilistic and Deterministic Assessment of In Situ Seismic Soil Liquefaction Potential, Journal of Geotechnical and Geoenvironmental Engineering, Vol. 132, No. 8, August 1, 2006
- I. M. Idriss and R. W. Boulanger, 2008. Soil liquefaction during earthquakes, Earthquake Engineering Research Institute MNO-12
- Jonathan D. Bray & Jorge Macedo, Department of Civil & Environmental Engineering, Univ. of California, Berkeley, CA, USA, Simplified procedure for estimating liquefaction-induced building settlement, *Proceedings of the 19th International Conference on Soil Mechanics and Geotechnical Engineering, Seoul 201*

TABLE OF CONTENTS

CPT-1 results

Summary data report	1
Transition layer aglorithm summary report	8
Transition layer aglorithm data report	9
Input field data	10
Cyclic stress resistance results	33
Cyclic resistance ratio results	56
Liquefaction potential index data	79
Vertical settlements summary report	91
Vertical settlements data report	92
Strength loss data report	99

CPT-2 results

Summary data report	124
Transition layer aglorithm summary report	131
Transition layer aglorithm data report	132
Input field data	133
Cyclic stress resistance results	155
Cyclic resistance ratio results	177
Liquefaction potential index data	199
Vertical settlements summary report	210
Vertical settlements data report	211
Strength loss data report	218

CPT-3 results

Summary data report	242
Transition layer aglorithm summary report	249
Transition layer aglorithm data report	250
Input field data	252
Cyclic stress resistance results	281
Cyclic resistance ratio results	310
Liquefaction potential index data	339
Vertical settlements summary report	354
Vertical settlements data report	355
Strength loss data report	366

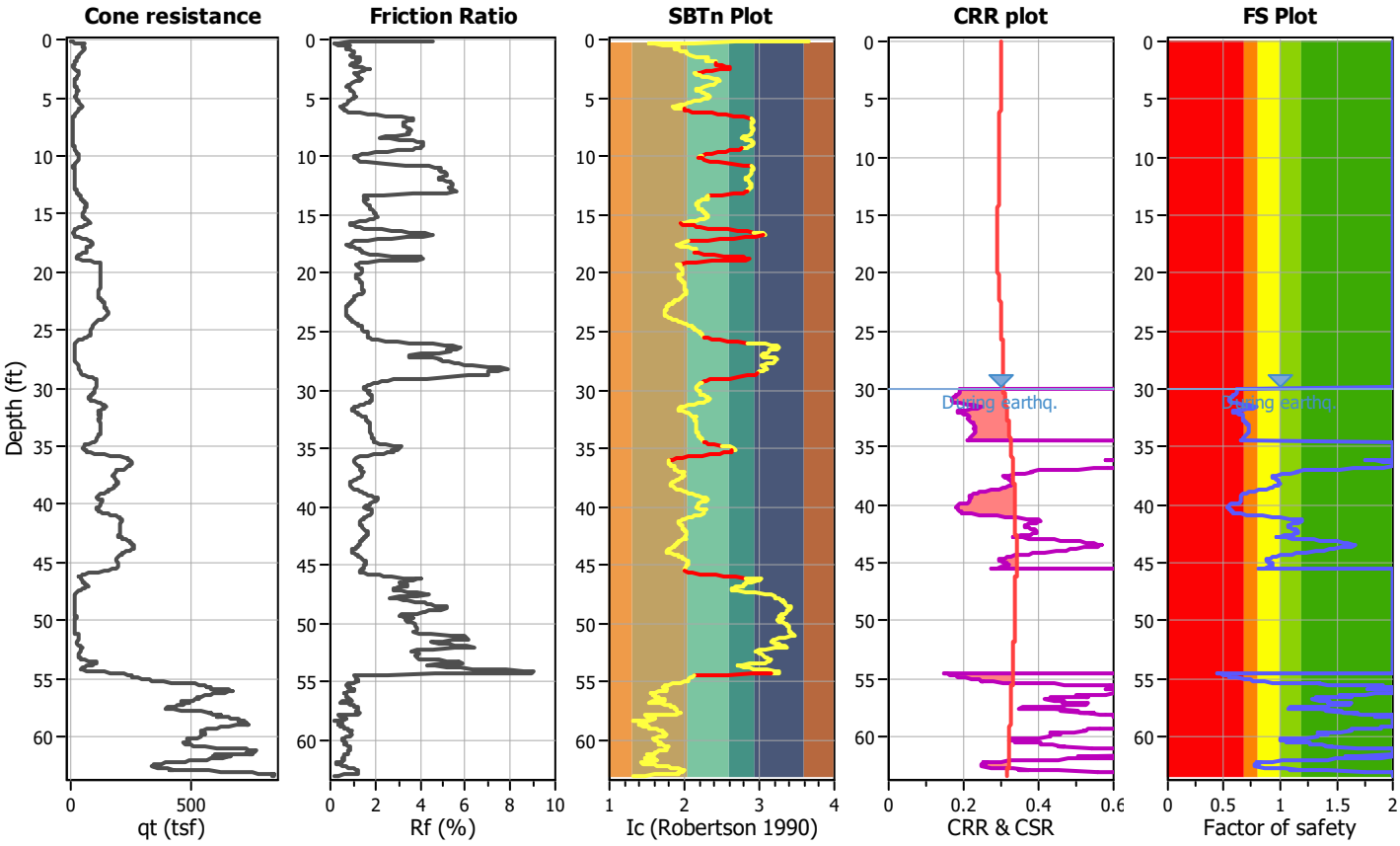
LIQUEFACTION ANALYSIS REPORT

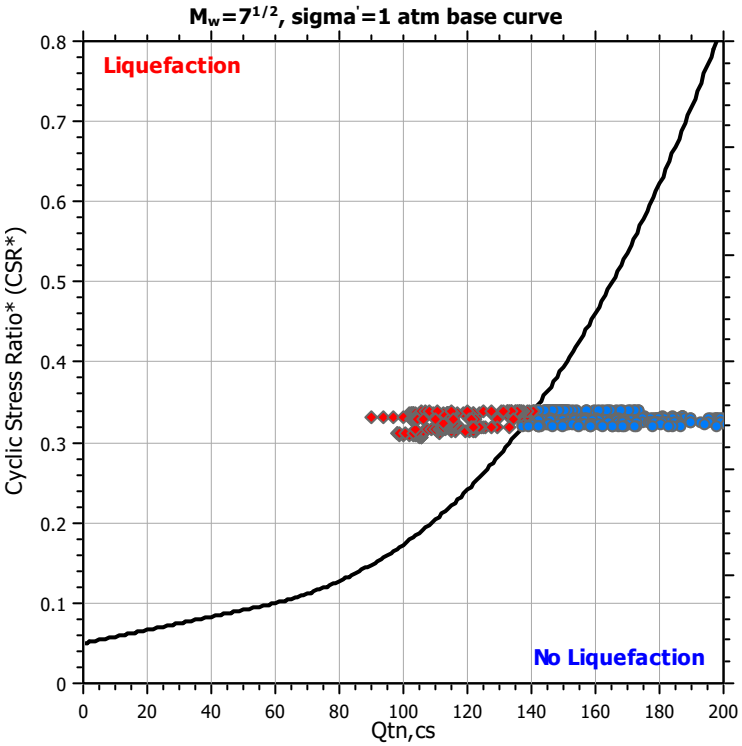
Project title : W1857-88-01 **Location : 331 The City Drive S**

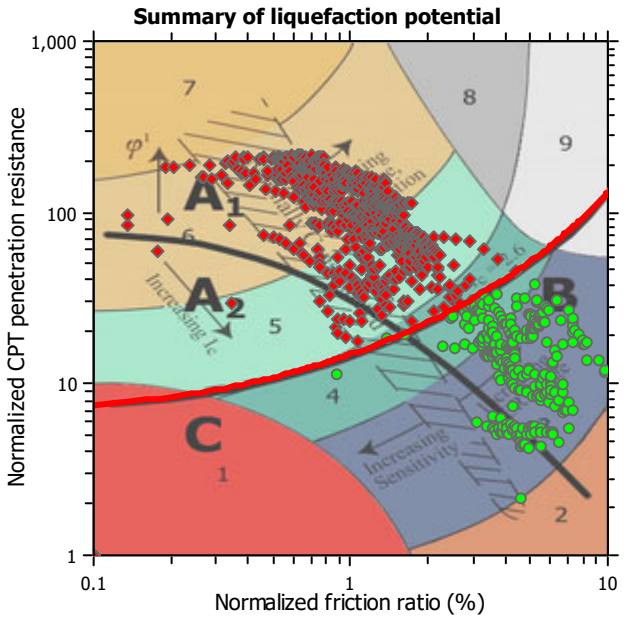
CPT file : CPT-1

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	54.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	30.00 ft	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.65	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.63	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

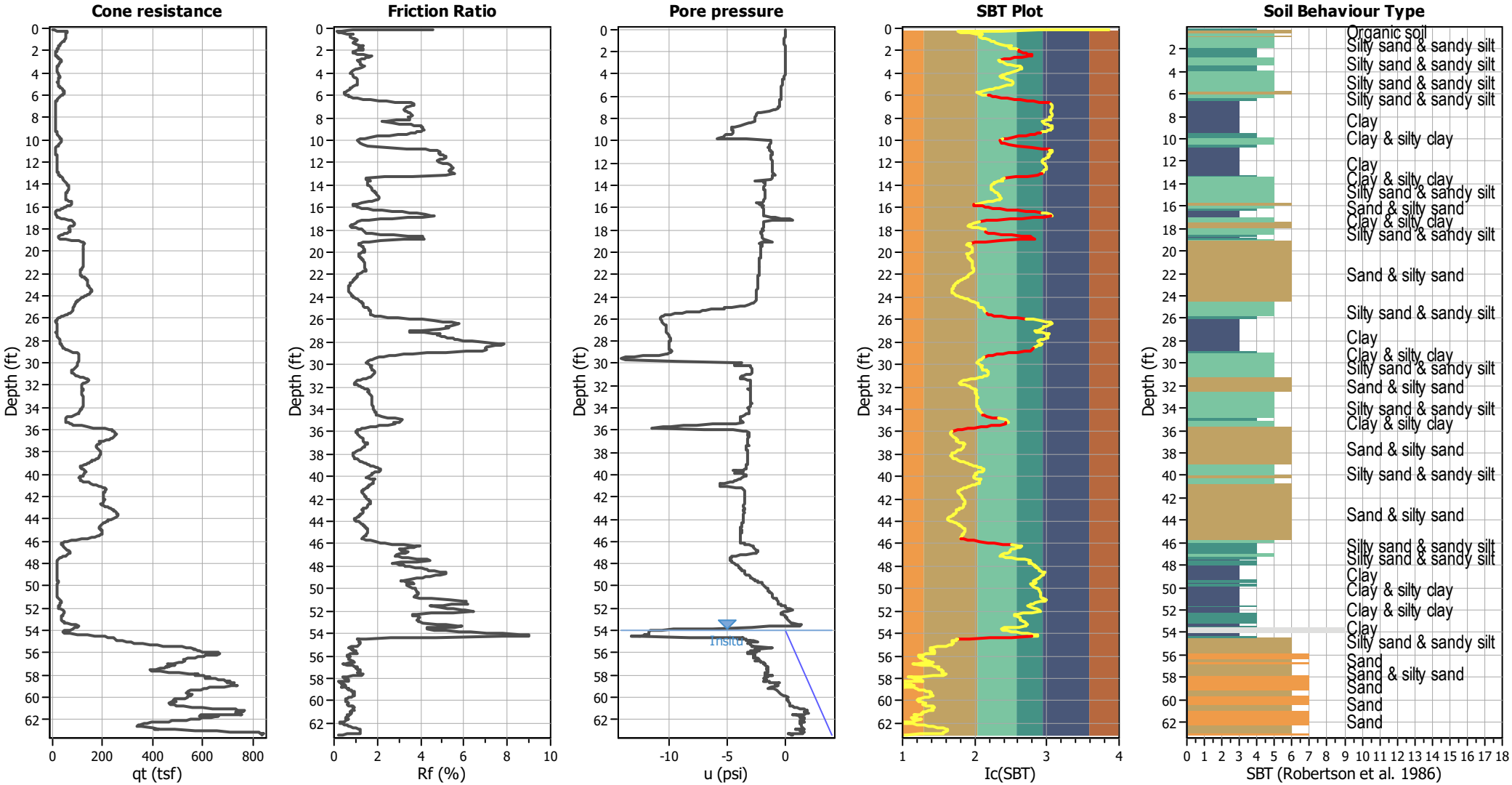






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



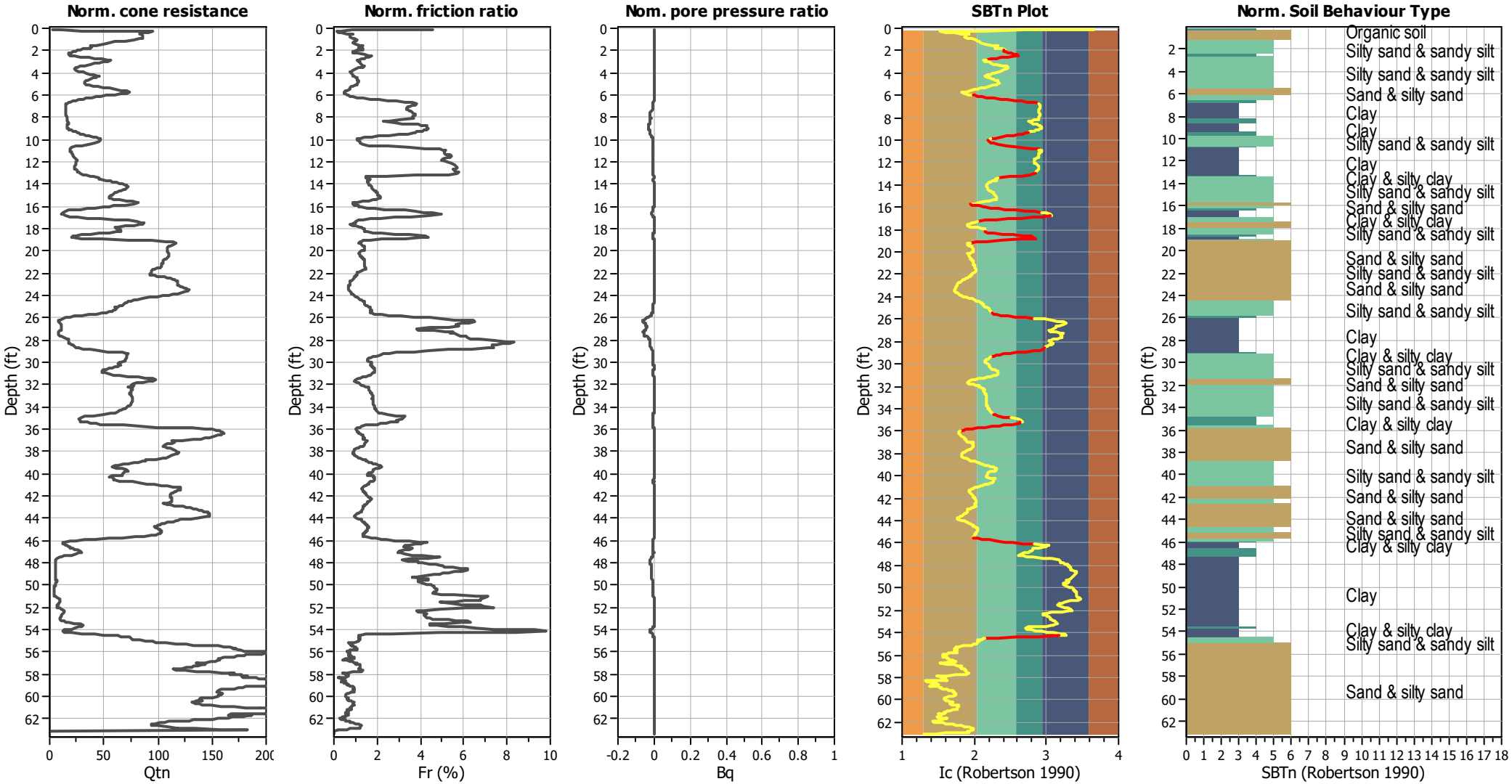
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



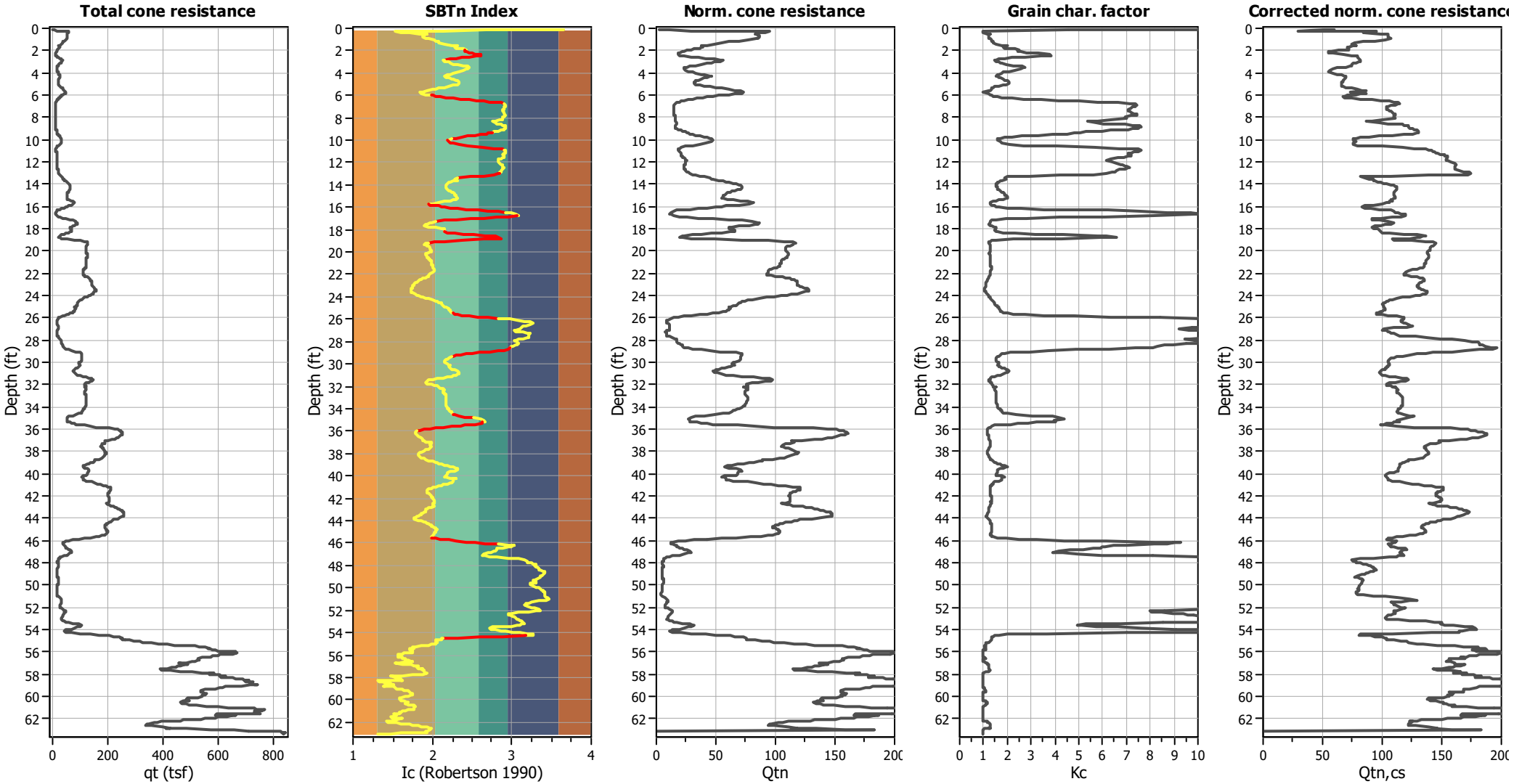
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

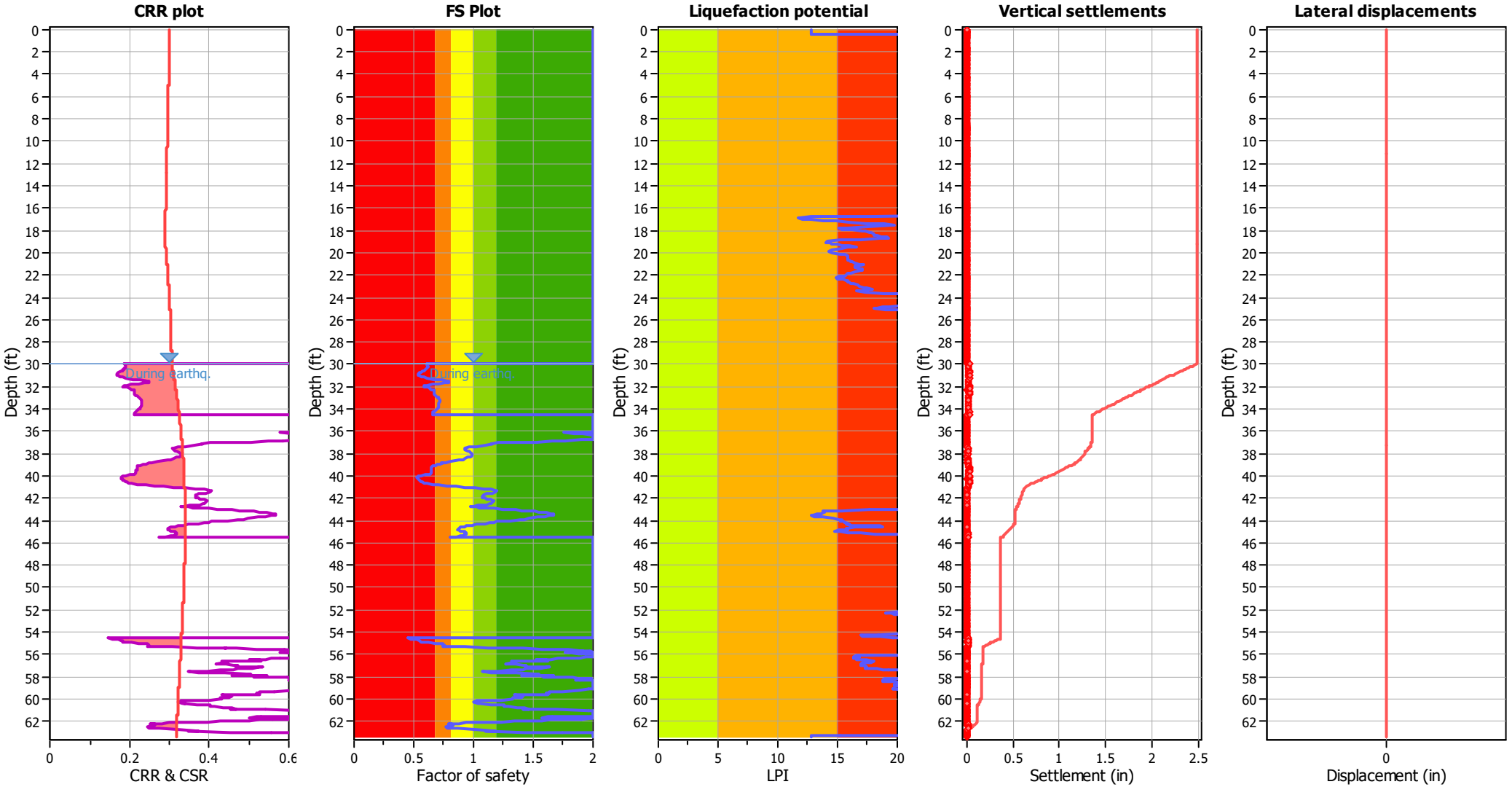
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

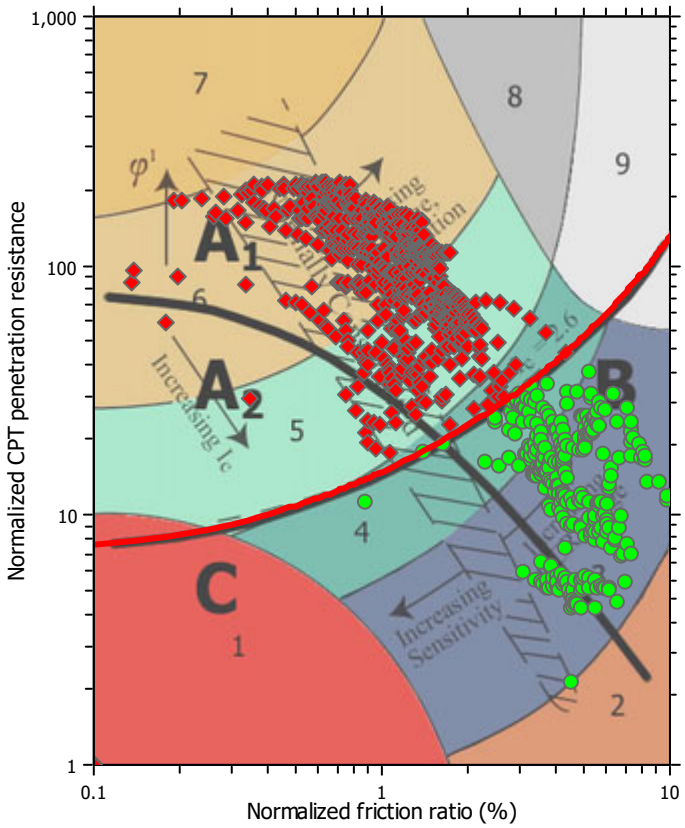
F.S. color scheme

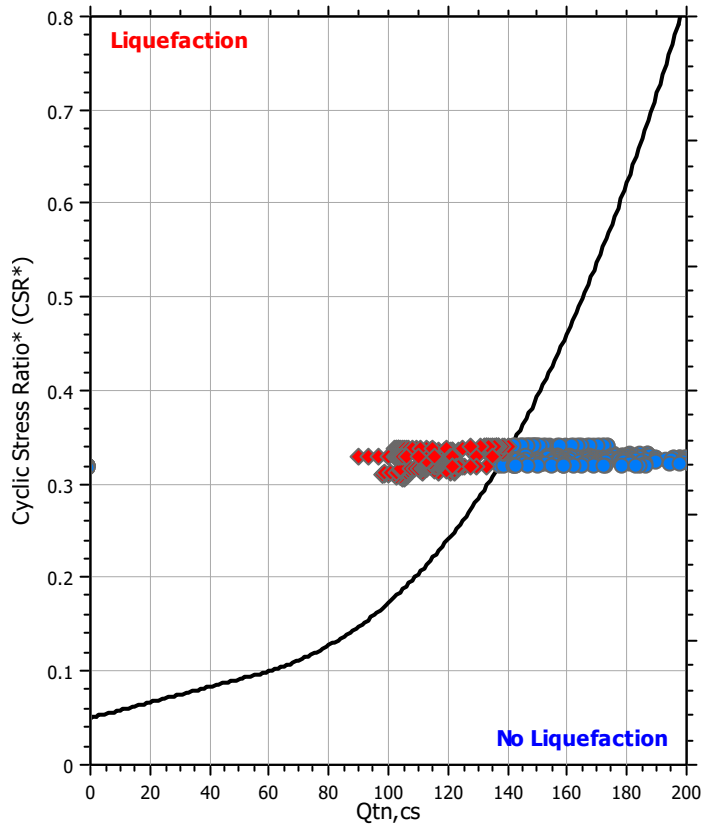
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

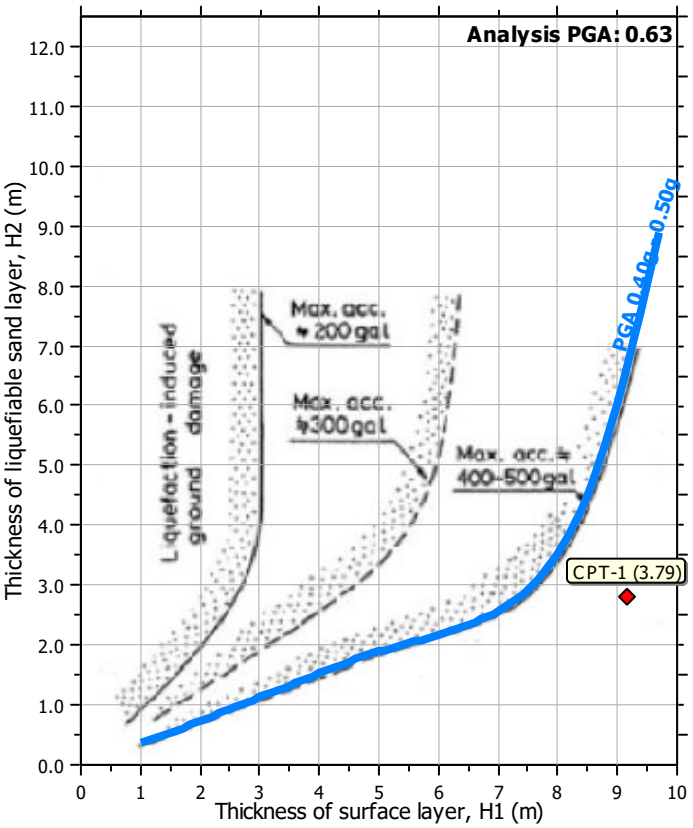
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



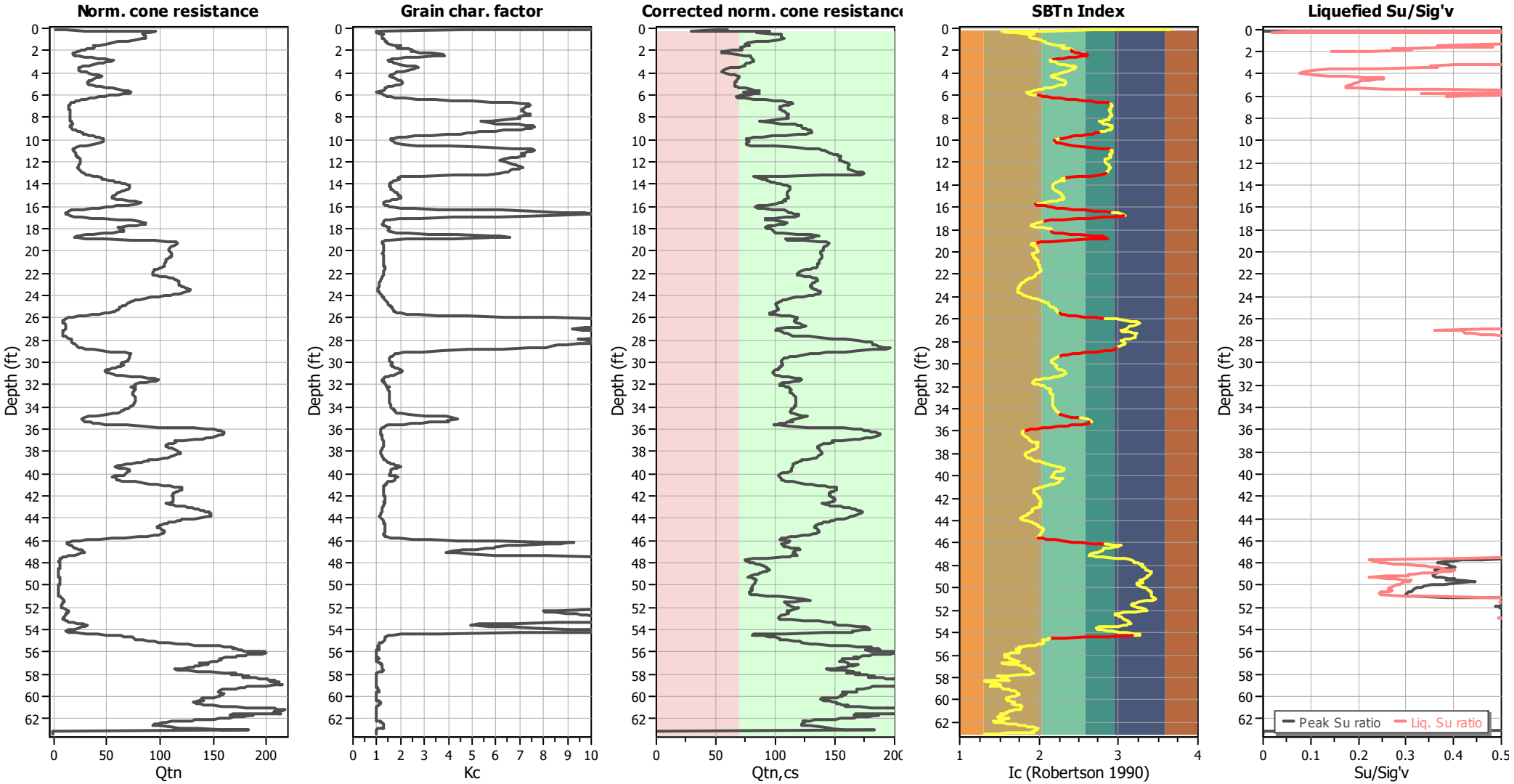




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

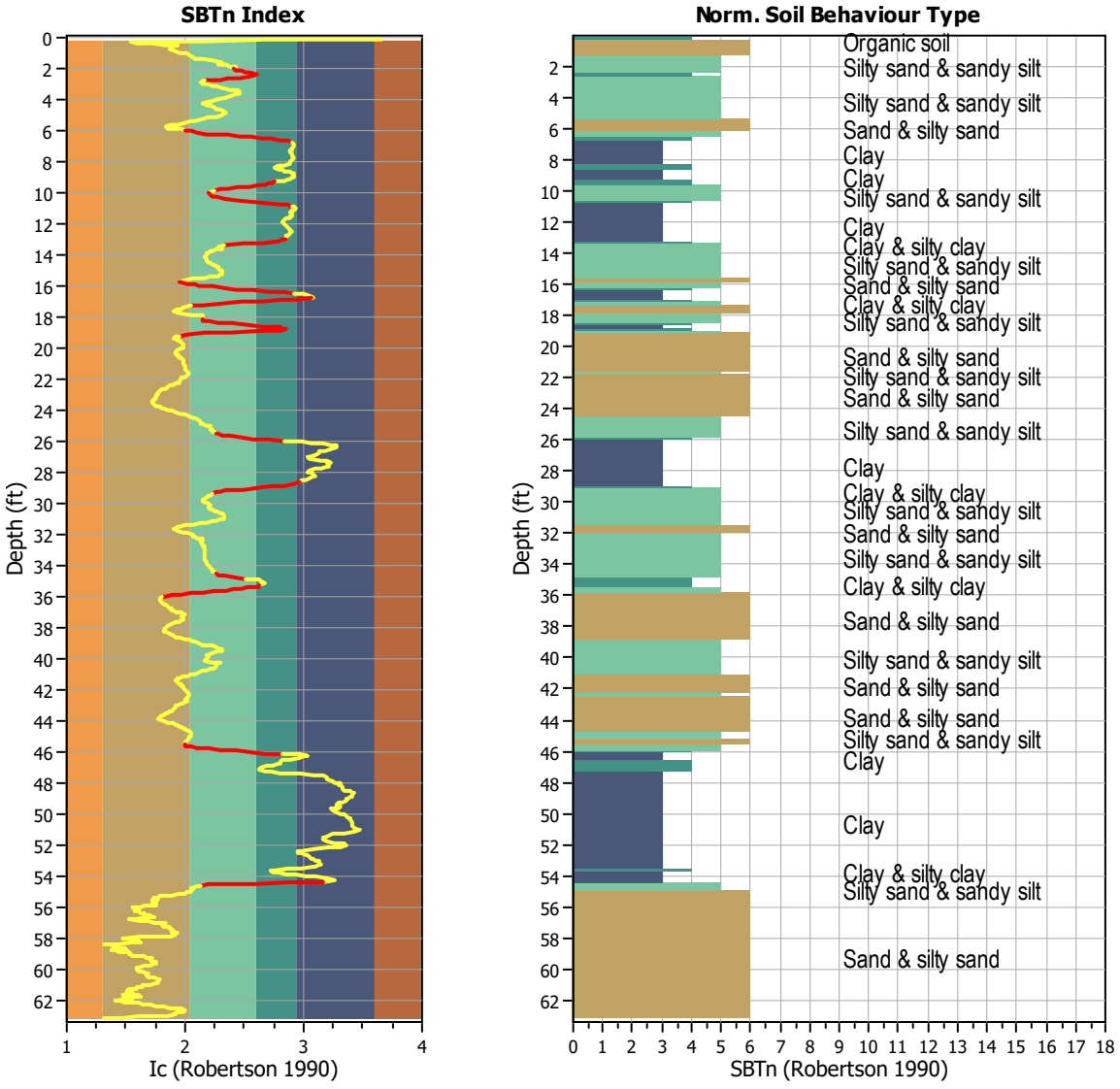
Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between 1.80 < I_c < 3.0) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	1063
I_c maximum check value:	3.00	Total points excluded:	146
I_c change ratio value:	0.0250	Exclusion percentage:	13.73%
Minimum number of points in layer:	4	Number of layers detected:	16

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	6	Start depth: 2.05 (ft)	5	Silty sand & sandy silt
		End depth: 2.34 (ft)	4	Clay & silty clay
Transition layer 2	8	Start depth: 2.44 (ft)	4	Clay & silty clay
		End depth: 2.89 (ft)	5	Silty sand & sandy silt
Transition layer 3	14	Start depth: 6.02 (ft)	6	Sand & silty sand
		End depth: 6.83 (ft)	3	Clay
Transition layer 4	10	Start depth: 9.38 (ft)	4	Clay & silty clay
		End depth: 9.97 (ft)	5	Silty sand & sandy silt
Transition layer 5	10	Start depth: 10.20 (ft)	5	Silty sand & sandy silt
		End depth: 10.89 (ft)	3	Clay
Transition layer 6	6	Start depth: 13.04 (ft)	3	Clay
		End depth: 13.47 (ft)	5	Silty sand & sandy silt
Transition layer 7	13	Start depth: 15.79 (ft)	6	Sand & silty sand
		End depth: 16.54 (ft)	3	Clay
Transition layer 8	8	Start depth: 16.86 (ft)	3	Clay
		End depth: 17.34 (ft)	6	Sand & silty sand
Transition layer 9	9	Start depth: 18.22 (ft)	5	Silty sand & sandy silt
		End depth: 18.76 (ft)	3	Clay
Transition layer 10	8	Start depth: 18.76 (ft)	3	Clay
		End depth: 19.24 (ft)	6	Sand & silty sand
Transition layer 11	8	Start depth: 25.52 (ft)	5	Silty sand & sandy silt
		End depth: 26.02 (ft)	3	Clay
Transition layer 12	12	Start depth: 28.67 (ft)	3	Clay
		End depth: 29.43 (ft)	5	Silty sand & sandy silt
Transition layer 13	5	Start depth: 34.55 (ft)	5	Silty sand & sandy silt
		End depth: 34.90 (ft)	4	Clay & silty clay
Transition layer 14	13	Start depth: 35.33 (ft)	4	Clay & silty clay
		End depth: 36.06 (ft)	6	Sand & silty sand
Transition layer 15	10	Start depth: 45.56 (ft)	6	Sand & silty sand
		End depth: 46.15 (ft)	3	Clay
Transition layer 16	6	Start depth: 54.34 (ft)	3	Clay
		End depth: 54.53 (ft)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.01	0.00	0.01	0.00	N/A	120.90
2	0.04	0.00	0.03	0.00	N/A	120.90
3	0.09	0.00	0.06	0.00	N/A	120.90
4	0.11	0.00	0.06	0.00	N/A	120.90
5	0.14	0.00	0.06	0.00	N/A	120.90
6	0.14	0.00	0.06	0.00	100.00	90.58
7	0.18	4.04	0.06	0.00	39.81	94.62
8	0.23	16.88	0.06	0.00	5.00	97.10
9	0.24	33.66	0.06	0.00	5.00	99.09
10	0.28	59.84	0.07	0.00	4.02	100.70
11	0.33	65.70	0.08	0.00	3.32	101.83
12	0.38	52.26	0.09	0.00	4.29	104.01
13	0.42	51.86	0.16	0.00	5.00	107.23
14	0.47	52.21	0.28	0.00	8.85	111.04
15	0.51	51.45	0.45	0.00	10.39	113.09
16	0.52	52.16	0.45	0.00	11.07	113.95
17	0.57	52.66	0.42	0.00	10.65	113.68
18	0.61	53.17	0.40	0.00	10.18	113.34
19	0.67	53.88	0.39	0.00	9.91	113.08
20	0.73	53.37	0.38	0.00	9.72	112.99
21	0.81	54.28	0.39	-0.10	9.70	112.87
22	0.86	53.22	0.37	-0.10	10.78	114.14
23	0.98	53.07	0.60	-0.10	11.85	114.82
24	1.05	50.14	0.53	-0.10	13.47	114.97
25	1.15	41.44	0.44	-0.10	14.02	113.60
26	1.24	39.42	0.37	-0.10	14.97	111.74
27	1.34	32.75	0.28	-0.10	15.41	110.26
28	1.43	31.24	0.27	0.00	17.53	109.89
29	1.53	27.90	0.36	0.00	20.70	109.99
30	1.58	21.43	0.33	0.00	23.01	110.04
31	1.62	24.36	0.30	0.00	23.24	109.31
32	1.67	24.66	0.28	0.00	21.78	108.90
33	1.75	24.06	0.27	0.00	21.84	108.54
34	1.77	22.95	0.27	0.00	22.45	108.33
35	1.81	22.24	0.27	0.00	23.98	108.08
36	1.86	19.31	0.26	0.00	25.81	107.68
37	1.91	17.59	0.25	0.00	27.51	107.00
38	1.95	16.98	0.22	0.00	27.58	105.88
39	2.00	16.38	0.17	0.00	26.85	104.31
40	2.05	15.26	0.13	0.00	26.79	102.37
41	2.11	13.04	0.11	0.00	27.77	100.94
42	2.20	12.23	0.11	0.00	29.43	100.17
43	2.24	11.73	0.11	0.00	30.90	100.15
44	2.29	11.22	0.11	0.00	32.65	100.53
45	2.34	10.82	0.13	0.00	35.39	102.57
46	2.44	11.93	0.22	0.00	35.96	104.47
47	2.48	13.75	0.24	0.00	33.48	106.65
48	2.58	17.99	0.29	0.00	29.16	108.19

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	2.63	22.34	0.33	0.00	25.09	109.71
50	2.71	26.89	0.36	0.00	22.48	110.79
51	2.78	29.01	0.39	0.00	19.70	111.55
52	2.82	35.08	0.39	0.00	17.69	111.93
53	2.89	37.10	0.38	0.00	16.81	111.84
54	2.96	32.65	0.36	0.00	17.52	111.71
55	3.03	31.13	0.39	0.00	19.08	111.39
56	3.11	28.91	0.36	0.00	20.03	110.91
57	3.19	26.89	0.31	0.00	21.15	109.99
58	3.25	23.55	0.29	0.00	22.96	109.06
59	3.35	20.12	0.28	0.00	25.68	108.30
60	3.41	17.79	0.26	0.00	28.08	107.14
61	3.50	15.47	0.20	0.00	29.06	105.47
62	3.59	14.46	0.15	0.00	28.55	103.57
63	3.69	14.56	0.13	0.00	27.72	102.55
64	3.79	14.76	0.14	0.00	26.19	102.21
65	3.88	16.27	0.13	0.00	24.04	102.29
66	3.97	18.60	0.13	0.00	21.42	103.22
67	4.07	22.54	0.17	0.00	20.94	104.68
68	4.14	21.33	0.21	-0.08	19.71	106.20
69	4.17	26.59	0.22	-0.08	18.89	107.22
70	4.26	28.61	0.25	-0.08	17.51	107.99
71	4.32	29.21	0.26	-0.09	17.59	108.49
72	4.37	28.30	0.27	-0.09	18.27	108.68
73	4.42	26.79	0.27	-0.10	19.47	108.64
74	4.51	24.77	0.27	-0.19	20.53	108.32
75	4.61	23.65	0.25	-0.19	21.42	107.89
76	4.65	22.64	0.24	-0.19	22.24	107.37
77	4.74	20.82	0.23	-0.19	23.28	106.98
78	4.80	19.81	0.22	-0.19	23.69	106.69
79	4.89	20.82	0.22	-0.19	24.07	106.54
80	4.95	19.51	0.22	-0.19	23.69	106.58
81	5.04	20.82	0.22	-0.19	23.00	106.70
82	5.13	22.84	0.22	-0.29	21.27	106.93
83	5.18	24.77	0.22	-0.29	19.16	107.22
84	5.28	28.20	0.23	-0.29	17.18	107.58
85	5.32	31.24	0.23	-0.29	15.37	108.17
86	5.42	34.97	0.25	-0.29	14.24	109.03
87	5.51	37.81	0.29	-0.29	13.16	109.85
88	5.60	41.65	0.30	-0.29	11.39	109.42
89	5.66	44.38	0.19	-0.29	9.82	108.84
90	5.76	46.70	0.21	-0.29	5.00	108.20
91	5.85	46.50	0.23	-0.29	9.42	108.60
92	5.92	41.55	0.23	-0.29	10.81	108.56
93	5.95	35.28	0.23	-0.33	11.91	108.38
94	5.97	37.81	0.23	-0.33	12.79	108.24
95	6.02	35.38	0.23	-0.33	13.11	108.15
96	6.06	32.95	0.23	-0.38	14.35	107.90

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.16	29.92	0.22	-0.38	15.93	107.69
98	6.21	27.09	0.23	-0.38	18.25	107.74
99	6.26	23.96	0.26	-0.38	21.09	108.07
100	6.31	21.83	0.28	-0.48	24.86	108.67
101	6.40	19.10	0.33	-0.48	28.84	109.09
102	6.44	16.78	0.34	-0.48	33.47	109.42
103	6.52	14.86	0.37	-0.48	37.59	109.55
104	6.57	13.75	0.38	-0.48	41.98	109.58
105	6.64	11.83	0.39	-0.48	45.80	109.43
106	6.69	10.92	0.39	-0.48	49.59	109.18
107	6.78	10.21	0.38	-0.48	51.74	108.94
108	6.83	9.91	0.38	-0.48	52.73	108.51
109	6.92	9.60	0.34	-0.48	53.03	108.02
110	6.97	9.30	0.32	-0.57	52.79	107.48
111	7.03	9.30	0.31	-0.57	52.62	107.19
112	7.12	9.30	0.30	-0.57	52.17	107.05
113	7.22	9.40	0.30	-0.86	51.84	107.03
114	7.27	9.50	0.31	-0.95	51.49	107.14
115	7.36	9.70	0.31	-1.34	51.37	107.36
116	7.43	9.81	0.33	-2.10	51.48	107.59
117	7.50	9.81	0.33	-2.39	51.81	107.80
118	7.59	9.81	0.34	-2.48	52.08	107.91
119	7.64	9.81	0.34	-2.48	52.59	107.98
120	7.75	9.60	0.35	-2.48	53.06	108.03
121	7.79	9.60	0.35	-2.48	52.94	108.11
122	7.89	10.01	0.35	-2.58	51.93	108.20
123	7.99	10.41	0.35	-2.58	51.00	108.32
124	8.04	10.41	0.36	-2.58	50.93	108.47
125	8.13	10.31	0.37	-2.58	51.23	108.53
126	8.23	10.31	0.36	-2.67	48.25	107.10
127	8.32	10.31	0.16	-2.96	45.66	105.82
128	8.37	10.31	0.23	-3.15	43.57	105.27
129	8.46	11.12	0.30	-3.44	45.48	107.20
130	8.56	11.83	0.36	-3.53	46.89	108.35
131	8.59	11.12	0.37	-3.93	48.24	108.98
132	8.61	11.12	0.39	-3.93	49.87	109.23
133	8.67	11.02	0.41	-3.93	51.01	109.48
134	8.71	10.71	0.41	-4.39	52.13	109.59
135	8.72	10.51	0.42	-4.49	53.07	109.66
136	8.78	10.51	0.43	-4.58	53.51	109.72
137	8.80	10.51	0.43	-4.58	53.62	109.76
138	8.86	10.51	0.43	-4.58	53.65	109.77
139	8.90	10.51	0.43	-4.58	53.45	109.87
140	8.95	10.82	0.44	-4.58	53.21	110.02
141	8.96	10.92	0.45	-4.58	52.79	110.21
142	9.00	11.12	0.45	-4.58	52.52	110.39
143	9.05	11.32	0.47	-4.49	52.13	110.62
144	9.09	11.62	0.48	-4.49	51.55	110.83

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	9.10	11.93	0.48	-4.49	50.65	111.10
146	9.14	12.53	0.51	-4.49	49.64	111.46
147	9.20	13.14	0.53	-4.49	48.16	111.91
148	9.24	14.15	0.55	-4.49	46.46	112.37
149	9.29	15.16	0.57	-4.49	44.67	112.78
150	9.31	15.97	0.59	-4.49	43.27	113.20
151	9.38	16.78	0.62	-4.58	42.21	113.51
152	9.41	17.29	0.63	-4.77	40.91	113.67
153	9.47	18.09	0.60	-5.15	39.32	113.64
154	9.53	18.90	0.58	-5.25	36.22	113.38
155	9.62	21.23	0.52	-5.34	32.67	113.07
156	9.67	23.35	0.49	-5.54	28.33	112.63
157	9.77	26.79	0.43	-5.92	25.15	112.27
158	9.81	28.81	0.41	-3.34	22.18	111.77
159	9.90	31.03	0.36	-1.43	20.30	111.35
160	9.97	32.25	0.34	-1.24	18.94	111.09
161	10.06	33.56	0.35	-1.24	18.88	111.19
162	10.20	32.14	0.37	-1.24	19.84	111.65
163	10.30	30.73	0.42	-1.34	21.09	110.81
164	10.44	25.07	0.26	-1.34	23.79	110.16
165	10.54	20.82	0.33	-1.43	28.52	109.42
166	10.63	16.27	0.39	-1.40	37.17	110.42
167	10.74	12.64	0.49	-1.40	45.02	111.01
168	10.78	12.64	0.51	-1.37	49.84	111.50
169	10.83	12.64	0.53	-1.37	50.94	111.75
170	10.88	12.23	0.55	-1.34	52.01	111.93
171	10.89	12.13	0.55	-1.24	53.26	112.19
172	10.97	12.13	0.60	-1.24	53.74	112.49
173	11.02	12.53	0.61	-1.15	53.76	112.83
174	11.07	12.84	0.63	-1.15	53.28	113.04
175	11.11	13.04	0.63	-1.15	52.89	113.23
176	11.16	13.34	0.65	-1.05	52.38	113.46
177	11.21	13.85	0.67	-1.15	51.91	113.73
178	11.26	14.15	0.69	-1.15	51.53	114.03
179	11.30	14.46	0.72	-1.24	51.55	114.31
180	11.36	14.56	0.74	-1.24	51.71	114.56
181	11.40	14.66	0.76	-1.24	51.84	114.75
182	11.45	14.86	0.77	-1.24	51.87	114.90
183	11.50	14.96	0.78	-1.24	51.65	115.06
184	11.55	15.36	0.79	-1.24	51.39	115.24
185	11.60	15.67	0.81	-1.24	50.61	115.51
186	11.66	16.58	0.84	-1.24	49.52	115.80
187	11.74	17.49	0.86	-1.15	48.09	116.04
188	11.84	18.19	0.85	-1.15	47.34	116.23
189	11.93	18.30	0.88	-1.15	47.43	116.42
190	12.04	18.09	0.91	-1.15	48.38	116.63
191	12.13	17.79	0.93	-1.15	49.30	116.79
192	12.22	17.79	0.95	-1.15	50.08	116.85

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.27	17.49	0.95	-1.15	50.46	116.81
194	12.37	17.29	0.93	-1.15	51.02	116.74
195	12.41	17.08	0.93	-1.15	51.24	116.69
196	12.51	17.18	0.94	-1.15	51.67	116.70
197	12.56	16.98	0.94	-1.15	51.47	116.76
198	12.65	17.59	0.95	-1.05	50.92	116.90
199	12.71	18.40	0.97	-1.05	49.81	117.22
200	12.79	19.41	1.02	-1.05	49.34	117.71
201	12.89	19.91	1.11	-0.95	48.93	118.28
202	12.96	21.03	1.17	-0.95	48.62	118.87
203	13.04	22.04	1.25	-0.86	47.37	119.33
204	13.13	23.65	1.26	-1.05	44.91	119.65
205	13.23	26.69	1.23	-1.05	37.79	118.14
206	13.30	30.12	0.44	-1.05	30.22	116.19
207	13.37	34.27	0.48	-1.15	23.39	113.77
208	13.47	38.11	0.56	-1.24	22.02	114.92
209	13.57	42.66	0.63	-2.58	22.72	115.65
210	13.61	35.68	0.65	-1.72	23.01	116.05
211	13.62	39.32	0.66	-1.72	22.69	116.34
212	13.68	45.99	0.69	-1.72	21.00	116.83
213	13.73	47.71	0.72	-1.91	19.82	117.32
214	13.77	49.83	0.75	-1.72	19.40	117.84
215	13.87	52.77	0.82	-1.72	18.89	118.41
216	13.93	56.20	0.87	-1.72	18.50	119.05
217	14.00	58.43	0.92	-1.72	18.11	119.60
218	14.06	61.05	0.98	-1.72	17.96	120.09
219	14.12	62.47	1.02	-1.81	17.96	120.53
220	14.21	63.18	1.08	-1.81	18.11	120.86
221	14.25	63.58	1.10	-1.81	18.27	121.08
222	14.35	63.68	1.12	-1.81	18.46	121.16
223	14.45	62.87	1.11	-1.72	18.76	121.14
224	14.50	61.36	1.11	-1.72	19.22	121.02
225	14.59	59.03	1.09	-1.72	19.83	120.88
226	14.64	57.21	1.08	-1.72	20.46	120.71
227	14.74	55.39	1.07	-1.72	21.03	120.57
228	14.80	54.28	1.06	-1.72	21.53	120.45
229	14.88	53.07	1.06	-1.72	21.95	120.36
230	14.97	52.26	1.05	-1.72	22.36	120.29
231	15.05	51.45	1.05	-1.72	22.79	120.27
232	15.13	50.64	1.07	-1.72	23.16	120.29
233	15.21	50.54	1.07	-1.72	23.18	120.30
234	15.28	51.76	1.05	-1.81	22.62	120.34
235	15.36	54.48	1.06	-1.91	21.45	120.45
236	15.41	59.13	1.06	-1.91	19.60	120.68
237	15.50	67.12	1.06	-2.00	17.73	120.96
238	15.55	72.98	1.07	-2.48	14.99	120.29
239	15.65	78.34	0.69	-2.00	12.97	119.36
240	15.71	79.55	0.68	-2.29	11.49	118.07

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	15.79	76.72	0.66	-2.00	11.94	117.74
242	15.89	69.04	0.63	-1.81	13.58	117.28
243	15.90	56.20	0.63	-1.93	15.06	116.86
244	15.94	58.12	0.62	-1.93	16.49	116.54
245	16.00	54.38	0.60	-1.93	17.46	116.33
246	16.06	47.31	0.61	-1.81	19.74	116.08
247	16.14	41.44	0.62	-1.81	23.40	115.82
248	16.19	33.56	0.63	-1.81	27.82	115.40
249	16.26	27.39	0.61	-1.81	33.97	114.66
250	16.33	20.42	0.58	-1.81	40.60	113.74
251	16.38	16.88	0.54	-1.81	47.75	112.60
252	16.47	13.95	0.48	-1.81	53.58	111.81
253	16.54	12.53	0.50	-1.81	58.20	111.16
254	16.62	11.52	0.48	-1.81	61.95	111.19
255	16.70	11.42	0.52	-1.81	63.86	111.41
256	16.76	11.73	0.55	-1.72	62.72	112.21
257	16.86	13.75	0.62	-1.24	55.66	113.21
258	16.90	19.21	0.65	-0.86	46.99	114.45
259	16.98	25.07	0.71	-0.29	37.95	115.60
260	17.05	33.26	0.75	0.38	29.58	116.88
261	17.14	47.91	0.80	0.67	22.70	117.88
262	17.20	61.46	0.80	-1.15	17.44	118.65
263	17.29	75.11	0.79	-1.91	14.33	119.10
264	17.34	82.59	0.81	-1.91	12.57	119.56
265	17.44	88.35	0.86	-1.91	12.10	120.15
266	17.50	89.76	0.95	-1.91	11.17	119.56
267	17.58	88.65	0.59	-1.91	10.61	118.74
268	17.64	86.12	0.61	-1.91	10.36	117.68
269	17.75	80.36	0.68	-1.91	11.68	118.09
270	17.82	75.11	0.73	-1.91	14.12	118.45
271	17.89	60.85	0.79	-1.94	16.11	118.58
272	17.89	62.17	0.79	-1.94	17.43	118.74
273	17.96	65.10	0.82	-1.94	17.29	119.02
274	18.02	65.00	0.86	-1.91	17.38	119.46
275	18.07	66.01	0.93	-2.00	17.40	119.89
276	18.17	69.65	0.96	-2.00	17.19	120.21
277	18.22	70.76	0.96	-2.10	17.38	120.34
278	18.30	65.91	0.98	-2.10	18.63	120.33
279	18.36	59.03	1.01	-2.10	21.57	120.25
280	18.42	48.22	1.05	-2.00	25.82	120.15
281	18.50	40.43	1.10	-2.00	31.86	119.89
282	18.56	31.34	1.11	-2.00	38.47	119.44
283	18.62	25.47	1.08	-2.00	45.73	118.51
284	18.69	20.42	0.95	-2.00	47.28	117.84
285	18.76	26.08	0.90	-2.00	49.35	117.26
286	18.84	20.22	0.92	-1.91	46.20	117.56
287	18.89	26.69	0.98	-1.81	38.13	118.84
288	18.98	48.82	1.15	-1.53	25.23	120.89

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	19.05	83.09	1.28	-1.15	17.63	122.71
290	19.12	103.41	1.40	-2.00	13.45	123.88
291	19.18	118.98	1.44	-2.19	11.63	124.47
292	19.24	125.34	1.44	-2.00	10.70	124.75
293	19.32	127.97	1.47	-2.10	10.50	124.90
294	19.38	127.06	1.50	-2.00	10.78	125.14
295	19.46	124.64	1.59	-2.00	11.28	125.37
296	19.54	122.82	1.64	-2.10	11.83	125.56
297	19.62	120.49	1.66	-2.10	12.18	125.64
298	19.70	119.78	1.66	-2.10	12.37	125.65
299	19.80	119.78	1.65	-2.10	12.42	125.63
300	19.85	119.78	1.65	-2.10	12.39	125.59
301	19.94	119.78	1.64	-2.10	12.46	125.66
302	20.03	120.39	1.70	-2.10	11.91	125.24
303	20.13	122.11	1.36	-2.10	11.37	124.85
304	20.19	123.12	1.38	-2.10	10.74	124.42
305	20.29	124.84	1.43	-2.10	10.87	124.64
306	20.39	124.28	1.47	-2.15	11.01	124.81
307	20.43	124.49	1.48	-2.15	11.19	124.93
308	20.47	123.73	1.51	-2.15	11.32	125.04
309	20.52	124.13	1.54	-2.19	11.55	125.23
310	20.61	124.13	1.61	-2.19	11.79	125.44
311	20.66	123.73	1.64	-2.19	12.08	125.60
312	20.71	122.01	1.65	-2.19	12.32	125.65
313	20.77	121.00	1.66	-2.19	12.55	125.68
314	20.85	120.09	1.67	-2.19	12.67	125.69
315	20.91	120.59	1.67	-2.19	12.69	125.72
316	21.00	121.30	1.67	-2.19	12.68	125.74
317	21.05	121.20	1.68	-2.19	12.72	125.75
318	21.11	120.39	1.68	-2.19	12.82	125.76
319	21.19	119.99	1.69	-2.19	12.93	125.79
320	21.24	120.19	1.70	-2.19	12.99	125.84
321	21.34	120.59	1.71	-2.19	13.03	125.87
322	21.39	120.49	1.71	-2.19	13.11	125.88
323	21.48	118.98	1.71	-2.19	13.31	125.83
324	21.53	116.65	1.70	-2.19	13.57	125.71
325	21.64	113.62	1.66	-2.19	13.84	125.53
326	21.72	111.39	1.62	-2.19	13.51	124.89
327	21.81	110.48	1.31	-2.19	12.90	124.15
328	21.89	110.59	1.24	-2.29	12.18	123.40
329	21.97	110.59	1.21	-2.29	11.93	123.16
330	22.05	110.99	1.19	-2.29	11.80	123.03
331	22.12	110.94	1.17	-2.34	11.72	122.95
332	22.13	110.94	1.17	-2.34	11.70	122.93
333	22.18	110.89	1.18	-2.34	11.57	122.96
334	22.22	114.22	1.18	-2.39	11.23	123.02
335	22.28	118.47	1.17	-2.39	10.74	123.13
336	22.33	122.82	1.19	-2.39	10.28	123.26

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.38	126.46	1.20	-2.39	9.90	123.41
338	22.41	129.89	1.21	-2.39	9.50	123.49
339	22.51	133.73	1.20	-2.39	9.14	123.51
340	22.56	135.96	1.18	-2.39	8.79	123.46
341	22.61	137.98	1.16	-2.39	8.51	123.37
342	22.65	139.19	1.14	-2.39	8.23	123.24
343	22.71	140.61	1.11	-2.39	8.00	123.09
344	22.76	141.21	1.08	-2.39	7.75	122.87
345	22.85	141.72	1.03	-2.39	7.57	122.67
346	22.89	141.82	1.02	-2.39	7.41	122.48
347	22.99	141.92	1.00	-2.39	7.34	122.38
348	23.04	141.92	0.99	-2.39	7.26	122.31
349	23.12	142.83	0.99	-2.39	7.17	122.30
350	23.18	145.06	0.99	-2.39	7.02	122.35
351	23.24	147.58	1.00	-2.39	6.88	122.47
352	23.33	150.11	1.02	-2.39	6.74	122.61
353	23.38	153.24	1.03	-2.48	6.65	122.79
354	23.47	155.06	1.05	-2.48	6.58	122.94
355	23.52	156.58	1.07	-2.48	6.66	123.16
356	23.61	156.07	1.12	-2.48	6.86	123.36
357	23.68	153.95	1.15	-2.48	7.23	123.57
358	23.76	150.31	1.19	-2.48	7.68	123.69
359	23.83	145.46	1.20	-2.48	8.20	123.74
360	23.90	140.61	1.21	-2.48	8.71	123.73
361	23.97	136.36	1.22	-2.48	9.28	123.71
362	24.05	131.21	1.23	-2.48	9.97	123.67
363	24.10	123.63	1.24	-2.48	10.81	123.59
364	24.19	116.75	1.24	-2.48	11.87	123.44
365	24.27	108.16	1.24	-2.48	12.89	123.28
366	24.34	103.31	1.24	-2.48	13.89	123.13
367	24.43	98.56	1.23	-2.58	14.65	123.04
368	24.48	96.03	1.24	-2.58	15.39	123.04
369	24.57	93.50	1.28	-2.77	16.07	123.15
370	24.62	91.89	1.32	-2.86	16.33	122.96
371	24.72	90.17	1.17	-3.15	16.56	122.82
372	24.81	89.06	1.23	-3.53	16.74	122.68
373	24.86	88.15	1.26	-3.91	17.34	122.92
374	24.95	86.83	1.31	-4.58	18.26	123.01
375	25.01	80.77	1.32	-5.22	19.01	123.05
376	25.02	81.12	1.32	-5.22	19.54	123.03
377	25.05	81.47	1.33	-5.22	19.39	123.10
378	25.11	83.09	1.34	-6.01	19.35	123.16
379	25.15	82.69	1.35	-6.39	19.38	123.22
380	25.21	82.08	1.36	-6.87	19.61	123.23
381	25.25	81.27	1.36	-7.16	19.86	123.21
382	25.30	80.16	1.35	-7.45	20.12	123.10
383	25.40	78.24	1.31	-8.49	20.43	122.88
384	25.45	76.01	1.27	-8.88	20.89	122.49

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.52	71.57	1.20	-9.54	21.58	121.99
386	25.60	66.92	1.12	-9.93	23.10	121.43
387	25.66	58.73	1.10	-10.40	25.37	120.85
388	25.74	51.45	1.05	-10.50	29.28	120.35
389	25.80	42.15	1.06	-10.69	34.11	119.74
390	25.88	34.67	1.01	-10.79	40.89	119.02
391	25.94	26.89	0.97	-10.79	48.17	118.23
392	26.02	22.64	0.95	-10.79	56.96	117.39
393	26.09	19.00	0.88	-10.79	63.54	116.56
394	26.17	16.38	0.82	-10.69	70.12	115.68
395	26.23	14.15	0.78	-10.69	75.56	115.05
396	26.29	13.44	0.77	-10.69	79.02	114.78
397	26.37	13.55	0.78	-10.50	78.84	114.95
398	26.46	14.66	0.82	-10.50	75.43	115.54
399	26.55	17.08	0.90	-10.40	71.32	116.21
400	26.60	18.40	0.93	-10.31	68.23	116.84
401	26.70	19.10	0.98	-10.31	67.29	117.29
402	26.78	19.31	1.04	-10.31	67.28	117.57
403	26.87	19.31	1.03	-10.31	65.46	116.94
404	26.94	19.31	0.72	-10.31	62.21	115.56
405	27.03	19.00	0.56	-10.31	60.24	114.24
406	27.13	17.99	0.66	-10.31	61.72	113.90
407	27.18	16.98	0.66	-10.31	68.38	114.01
408	27.27	13.14	0.67	-10.20	73.05	113.89
409	27.32	14.15	0.68	-10.20	75.75	113.91
410	27.37	15.16	0.70	-10.20	73.86	114.24
411	27.41	15.16	0.73	-10.12	73.36	114.52
412	27.46	15.16	0.75	-10.12	74.03	114.74
413	27.51	15.16	0.76	-10.02	74.31	115.06
414	27.61	15.67	0.82	-10.02	73.92	115.57
415	27.66	16.68	0.89	-9.93	72.75	116.57
416	27.73	18.50	1.06	-9.93	69.00	118.04
417	27.80	23.15	1.28	-9.93	64.92	119.84
418	27.88	27.09	1.57	-9.93	61.75	121.59
419	27.96	29.72	1.88	-9.93	61.15	122.86
420	28.04	29.82	2.03	-10.02	62.65	123.82
421	28.12	29.21	2.29	-10.02	64.46	124.33
422	28.18	29.31	2.33	-10.02	64.94	124.77
423	28.27	31.24	2.40	-10.02	63.60	125.01
424	28.32	32.85	2.43	-10.02	61.44	125.31
425	28.42	34.87	2.48	-10.02	59.28	125.61
426	28.47	37.40	2.56	-10.02	57.63	126.07
427	28.61	39.22	2.75	-10.02	56.63	126.53
428	28.67	40.43	2.86	-10.02	55.75	127.05
429	28.75	43.16	3.02	-10.02	52.70	127.47
430	28.81	47.71	3.06	-9.93	47.96	127.92
431	28.90	58.12	3.04	-9.83	41.37	128.35
432	29.00	72.07	3.02	-9.93	35.34	128.76

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	29.05	82.28	3.02	-10.02	30.50	129.11
434	29.10	94.11	3.00	-10.21	27.19	129.31
435	29.15	101.79	2.92	-10.31	24.40	129.24
436	29.24	107.76	2.68	-10.98	22.48	128.87
437	29.29	108.56	2.46	-12.31	21.04	128.21
438	29.37	106.54	2.19	-13.08	20.19	127.50
439	29.43	105.43	2.02	-13.84	19.39	126.74
440	29.53	104.93	1.82	-14.22	18.65	126.11
441	29.62	104.93	1.70	-13.79	18.12	125.67
442	29.68	104.93	1.71	-13.74	17.48	125.18
443	29.80	104.93	1.48	-9.45	17.32	124.98
444	29.91	103.81	1.57	-4.29	17.30	124.83
445	30.00	102.90	1.62	-3.72	18.66	124.98
446	30.07	90.77	1.65	-4.39	19.24	125.07
447	30.15	98.76	1.66	-4.39	19.60	125.10
448	30.21	99.47	1.66	-4.39	19.01	125.18
449	30.26	99.06	1.66	-2.96	19.09	125.17
450	30.31	97.75	1.66	-2.96	19.36	125.12
451	30.38	95.83	1.65	-2.96	19.77	125.02
452	30.45	93.10	1.62	-2.86	20.38	124.87
453	30.50	89.06	1.61	-2.86	21.16	124.68
454	30.55	85.31	1.58	-2.86	22.05	124.38
455	30.64	80.56	1.51	-2.86	22.84	124.05
456	30.70	77.83	1.46	-2.86	23.38	123.62
457	30.79	75.51	1.39	-2.86	23.69	123.34
458	30.84	74.90	1.38	-2.86	23.72	123.20
459	30.93	76.12	1.39	-2.96	23.33	123.30
460	30.98	79.96	1.42	-3.05	22.53	123.52
461	31.05	84.51	1.45	-3.34	21.39	123.92
462	31.13	91.68	1.54	-3.63	20.20	124.38
463	31.17	98.66	1.60	-3.72	18.55	124.91
464	31.27	111.19	1.64	-3.91	16.70	125.32
465	31.32	123.12	1.65	-3.82	14.63	125.57
466	31.41	135.55	1.59	-3.44	13.02	125.62
467	31.46	141.82	1.54	-3.25	11.83	125.51
468	31.52	145.46	1.49	-3.05	11.07	125.22
469	31.61	145.97	1.37	-3.05	10.64	124.85
470	31.66	143.74	1.32	-3.05	10.61	124.43
471	31.75	136.87	1.28	-3.05	11.17	124.24
472	31.80	129.59	1.32	-3.05	12.39	124.35
473	31.90	121.10	1.46	-2.96	13.62	124.39
474	31.94	115.44	1.39	-2.96	14.62	124.45
475	32.04	114.12	1.42	-2.96	14.97	124.60
476	32.09	118.67	1.55	-2.96	15.15	125.24
477	32.20	124.84	1.74	-3.02	15.99	125.83
478	32.24	112.71	1.82	-3.02	16.70	126.23
479	32.28	115.74	1.85	-3.07	17.46	126.32
480	32.29	115.74	1.86	-3.07	17.17	126.42

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	32.30	118.77	1.87	-3.25	16.87	126.53
482	32.40	122.41	1.90	-3.05	16.70	126.62
483	32.45	120.49	1.91	-3.05	16.81	126.69
484	32.55	118.67	1.92	-3.05	17.10	126.69
485	32.59	118.37	1.92	-3.05	17.33	126.73
486	32.69	118.07	1.95	-3.05	17.51	126.82
487	32.76	118.07	1.99	-2.96	17.74	126.96
488	32.84	118.27	2.04	-2.96	17.92	127.13
489	32.90	118.98	2.08	-2.96	18.01	127.28
490	32.98	119.89	2.11	-2.96	17.99	127.39
491	33.06	121.10	2.12	-3.05	17.91	127.48
492	33.12	122.21	2.13	-3.05	17.81	127.55
493	33.22	123.12	2.15	-3.05	17.76	127.60
494	33.31	123.32	2.16	-3.05	17.76	127.64
495	33.37	123.32	2.16	-2.96	17.77	127.65
496	33.46	123.32	2.16	-2.96	17.80	127.65
497	33.55	123.32	2.17	-2.86	17.87	127.68
498	33.65	123.02	2.18	-2.96	17.99	127.72
499	33.70	122.72	2.20	-2.96	18.14	127.75
500	33.79	122.11	2.21	-2.96	18.29	127.77
501	33.89	121.40	2.21	-3.05	18.48	127.74
502	33.99	119.89	2.19	-3.25	18.70	127.68
503	34.04	118.17	2.18	-3.25	18.98	127.58
504	34.13	115.44	2.15	-3.15	19.34	127.46
505	34.23	113.01	2.13	-3.15	19.82	127.32
506	34.32	109.78	2.11	-3.15	20.27	127.22
507	34.37	108.16	2.10	-3.15	20.65	127.13
508	34.47	106.85	2.09	-3.15	21.01	127.08
509	34.55	104.93	2.10	-3.34	21.77	127.01
510	34.63	98.76	2.11	-3.53	23.58	126.91
511	34.73	86.43	2.14	-3.72	26.59	126.63
512	34.80	74.09	2.10	-3.91	31.19	126.00
513	34.90	57.92	1.93	-3.91	36.19	125.07
514	35.00	49.53	1.74	-3.91	37.59	123.92
515	35.12	57.47	1.42	-3.91	38.98	122.90
516	35.20	44.27	1.40	-3.72	36.68	122.71
517	35.33	57.01	1.55	-3.63	36.87	123.05
518	35.41	59.84	1.61	-4.20	32.11	123.80
519	35.44	73.57	1.62	-6.27	29.94	124.11
520	35.48	72.58	1.63	-6.27	26.74	124.41
521	35.57	84.61	1.62	-7.64	24.34	124.63
522	35.62	95.42	1.62	-8.78	20.42	125.05
523	35.67	116.45	1.64	-9.93	17.13	125.56
524	35.71	134.74	1.71	-10.60	14.14	126.40
525	35.82	161.84	1.91	-11.55	12.01	127.28
526	35.86	183.57	2.03	-11.17	10.22	128.24
527	35.93	210.36	2.20	-6.97	8.94	129.00
528	36.01	229.56	2.33	-4.49	8.16	129.62

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	36.06	236.44	2.41	-3.63	7.85	130.06
530	36.12	240.88	2.52	-3.34	7.80	130.37
531	36.18	244.83	2.59	-3.15	7.84	130.72
532	36.25	249.58	2.73	-3.15	7.88	131.01
533	36.30	251.80	2.80	-3.15	8.05	131.37
534	36.39	253.32	2.97	-3.25	8.23	131.64
535	36.44	253.52	3.03	-3.15	8.49	131.92
536	36.53	252.51	3.13	-3.25	8.77	132.08
537	36.59	248.57	3.20	-3.15	9.37	132.44
538	36.68	244.22	3.54	-3.25	9.70	132.41
539	36.75	237.75	3.16	-3.25	9.93	132.25
540	36.83	233.20	3.05	-3.25	9.92	131.78
541	36.90	225.32	3.02	-3.25	10.25	131.57
542	36.97	217.43	2.99	-3.25	10.78	131.42
543	37.02	208.94	2.97	-3.25	11.95	131.17
544	37.04	178.92	2.94	-3.25	12.56	130.99
545	37.08	193.37	2.89	-3.25	12.85	130.76
546	37.17	193.68	2.77	-3.25	12.27	130.55
547	37.27	188.42	2.66	-3.25	12.36	130.20
548	37.37	179.93	2.56	-3.15	12.63	129.85
549	37.42	175.89	2.48	-3.34	12.60	129.41
550	37.51	175.94	2.26	-3.34	12.21	128.93
551	37.58	175.99	2.11	-3.34	11.53	128.42
552	37.66	179.12	2.01	-3.34	10.87	128.00
553	37.76	182.05	1.88	-3.34	10.12	127.61
554	37.85	186.70	1.77	-3.25	9.43	127.24
555	37.93	189.63	1.70	-3.25	8.90	127.02
556	38.04	192.67	1.69	-3.25	8.61	126.94
557	38.13	194.59	1.69	-3.25	8.49	126.94
558	38.18	194.49	1.69	-3.25	8.53	126.96
559	38.28	191.76	1.70	-3.25	8.89	127.11
560	38.37	187.61	1.81	-3.25	9.47	127.34
561	38.47	182.96	1.89	-3.25	10.26	127.74
562	38.57	180.23	2.05	-3.25	10.93	128.06
563	38.62	178.11	2.10	-3.25	11.67	128.38
564	38.72	172.15	2.20	-3.25	12.92	128.49
565	38.78	152.33	2.27	-3.26	13.99	128.58
566	38.81	156.28	2.28	-3.25	14.73	128.61
567	38.86	157.49	2.30	-3.25	14.82	128.67
568	38.91	151.93	2.32	-3.25	15.34	128.70
569	38.95	146.77	2.36	-3.25	16.32	128.70
570	39.05	139.19	2.39	-3.25	17.39	128.67
571	39.09	132.82	2.40	-3.34	18.62	128.58
572	39.14	125.24	2.40	-3.34	19.92	128.44
573	39.24	117.26	2.39	-3.34	21.20	128.25
574	39.29	112.20	2.35	-3.34	22.35	128.02
575	39.39	107.15	2.30	-3.34	23.14	127.89
576	39.43	106.24	2.34	-3.34	23.05	127.94

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	39.53	114.22	2.38	-3.53	21.86	128.13
578	39.57	124.74	2.36	-3.63	20.02	128.31
579	39.68	133.73	2.34	-4.49	18.81	128.39
580	39.73	133.63	2.33	-3.67	18.53	128.37
581	39.81	128.68	2.32	-4.39	18.86	128.23
582	39.89	125.85	2.25	-3.72	18.82	127.76
583	39.96	124.74	1.96	-3.44	18.19	127.14
584	40.06	125.34	1.81	-3.34	17.66	126.63
585	40.15	123.63	1.86	-3.34	17.93	126.54
586	40.20	119.28	1.91	-3.44	19.75	126.53
587	40.24	100.48	1.93	-3.71	21.16	126.50
588	40.26	106.09	1.93	-3.71	22.23	126.44
589	40.27	106.09	1.94	-3.71	21.47	126.59
590	40.37	111.70	1.99	-3.91	21.22	126.73
591	40.42	111.70	2.01	-4.01	21.04	126.91
592	40.52	111.70	2.06	-4.20	21.09	127.05
593	40.56	113.92	2.09	-4.39	20.77	127.30
594	40.66	120.39	2.17	-4.49	19.70	127.64
595	40.70	132.62	2.24	-4.77	18.40	128.08
596	40.75	141.82	2.32	-5.25	17.09	128.59
597	40.85	153.55	2.47	-5.63	16.06	129.13
598	40.91	165.07	2.59	-5.63	15.13	129.61
599	40.96	173.76	2.65	-5.63	14.17	129.97
600	41.04	185.49	2.68	-5.63	13.29	130.19
601	41.09	193.78	2.70	-4.96	12.46	130.39
602	41.18	202.77	2.73	-4.20	11.82	130.54
603	41.23	209.35	2.74	-3.72	11.36	130.66
604	41.29	211.97	2.74	-3.63	11.10	130.71
605	41.38	213.59	2.74	-3.63	11.02	130.73
606	41.42	212.88	2.74	-3.53	11.10	130.74
607	41.52	209.95	2.77	-3.53	11.32	130.76
608	41.57	207.42	2.79	-3.53	11.64	130.80
609	41.62	204.59	2.83	-3.44	11.95	130.86
610	41.71	202.88	2.87	-3.44	12.22	130.92
611	41.76	202.07	2.89	-3.44	12.42	131.01
612	41.84	201.66	2.94	-3.44	12.59	131.09
613	41.91	201.36	2.97	-3.44	12.74	131.20
614	41.95	201.76	3.03	-3.53	12.88	131.32
615	42.01	202.27	3.09	-3.53	13.08	131.54
616	42.10	203.68	3.24	-3.53	13.30	131.80
617	42.15	204.90	3.34	-3.53	13.56	132.12
618	42.24	206.51	3.49	-3.53	13.76	132.35
619	42.28	206.82	3.55	-3.53	13.82	132.43
620	42.39	206.21	3.45	-3.53	13.78	132.37
621	42.43	205.91	3.41	-3.53	13.60	132.21
622	42.50	206.26	3.33	-3.53	13.33	131.99
623	42.58	206.31	3.14	-3.53	12.97	131.71
624	42.65	206.41	3.03	-3.53	13.30	131.34

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	42.70	184.28	2.97	-3.61	13.40	131.14
626	42.73	197.11	2.95	-3.61	13.48	131.01
627	42.77	199.94	2.91	-3.61	12.77	131.00
628	42.82	203.68	2.86	-3.62	12.36	130.97
629	42.87	208.03	2.85	-3.62	11.87	131.00
630	42.91	215.81	2.87	-3.63	11.40	131.10
631	42.97	222.69	2.90	-3.53	11.00	131.25
632	43.02	226.93	2.94	-3.44	10.78	131.43
633	43.06	230.98	3.03	-3.53	10.72	131.66
634	43.11	233.71	3.13	-3.53	10.67	131.89
635	43.17	238.46	3.19	-3.63	10.57	132.05
636	43.21	241.79	3.19	-3.63	10.32	132.13
637	43.29	246.54	3.17	-3.63	10.05	132.16
638	43.34	250.39	3.16	-3.63	9.74	132.17
639	43.39	254.83	3.15	-3.53	9.49	132.17
640	43.45	257.26	3.12	-3.53	9.24	132.11
641	43.51	258.67	3.05	-3.63	8.93	131.89
642	43.59	258.98	2.87	-3.63	8.66	131.64
643	43.64	258.27	2.81	-3.63	8.23	131.24
644	43.70	260.49	2.58	-3.63	7.80	130.79
645	43.78	259.28	2.37	-3.63	7.50	130.39
646	43.88	255.44	2.40	-3.63	7.60	130.26
647	43.94	250.99	2.49	-3.63	8.46	130.43
648	44.04	228.05	2.65	-3.66	9.36	130.60
649	44.07	225.92	2.69	-3.63	10.23	130.73
650	44.12	223.80	2.73	-3.66	10.49	130.79
651	44.16	221.17	2.75	-3.63	10.73	130.81
652	44.21	218.64	2.74	-3.63	11.01	130.81
653	44.26	214.50	2.77	-3.63	11.32	130.81
654	44.31	210.96	2.79	-3.63	11.70	130.81
655	44.35	207.12	2.80	-3.72	12.07	130.81
656	44.40	202.98	2.81	-3.72	12.44	130.79
657	44.45	199.84	2.82	-3.72	12.75	130.78
658	44.50	197.82	2.82	-3.72	12.98	130.76
659	44.54	196.00	2.82	-3.72	13.20	130.75
660	44.60	193.78	2.85	-3.72	13.50	130.78
661	44.64	190.75	2.88	-3.72	13.86	130.82
662	44.69	188.52	2.92	-3.72	14.21	130.87
663	44.74	186.60	2.94	-3.82	14.38	130.92
664	44.79	188.37	2.96	-3.82	14.49	130.94
665	44.83	186.70	2.95	-3.82	14.44	130.96
666	44.88	188.22	2.95	-3.82	14.34	130.97
667	44.93	191.76	2.96	-3.82	14.12	131.02
668	44.98	193.78	2.97	-3.72	13.90	131.07
669	45.03	195.70	2.97	-3.82	13.77	131.11
670	45.08	196.61	2.98	-3.72	13.68	131.13
671	45.16	197.32	2.98	-3.82	13.57	131.13
672	45.19	198.83	2.96	-3.72	13.41	131.06

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	45.27	198.73	2.88	-3.82	13.22	130.92
674	45.32	197.92	2.81	-3.82	13.07	130.71
675	45.37	196.20	2.73	-3.82	12.89	130.37
676	45.45	192.77	2.52	-3.82	12.75	129.96
677	45.51	188.52	2.41	-3.82	12.79	129.49
678	45.56	180.54	2.32	-3.82	13.16	129.13
679	45.61	172.65	2.26	-3.82	14.11	128.81
680	45.69	156.48	2.24	-3.82	15.78	128.59
681	45.75	140.00	2.30	-3.82	18.95	128.52
682	45.81	115.94	2.49	-3.91	22.57	127.65
683	45.89	90.17	1.83	-3.91	27.28	126.48
684	45.94	73.89	1.73	-3.91	32.45	124.69
685	46.04	56.20	1.58	-3.91	38.98	123.71
686	46.08	47.71	1.52	-3.91	47.47	122.68
687	46.15	36.09	1.45	-3.82	56.21	122.08
688	46.17	36.19	1.44	-3.53	60.34	121.69
689	46.18	36.19	1.43	-3.53	60.04	121.61
690	46.23	36.29	1.40	-3.53	59.44	121.53
691	46.27	37.10	1.38	-3.44	58.23	121.42
692	46.32	38.31	1.34	-3.15	56.14	121.33
693	46.41	40.64	1.30	-2.86	51.16	121.34
694	46.47	43.06	1.32	-2.77	48.66	121.54
695	46.52	45.89	1.37	-2.77	47.10	121.93
696	46.56	47.51	1.45	-2.77	46.43	122.56
697	46.65	49.43	1.62	-2.67	46.28	123.25
698	46.71	51.45	1.75	-2.58	46.04	123.95
699	46.76	53.78	1.86	-2.48	44.89	124.54
700	46.85	58.12	1.95	-2.39	42.94	124.99
701	46.90	62.77	1.97	-2.39	40.08	125.34
702	46.99	69.04	1.98	-2.48	37.61	125.55
703	47.04	71.97	1.98	-2.48	36.35	125.63
704	47.10	70.15	1.97	-2.77	36.71	125.56
705	47.16	66.51	1.95	-3.34	38.66	125.31
706	47.23	59.84	1.90	-3.82	41.64	124.83
707	47.30	52.66	1.77	-4.20	46.53	124.02
708	47.38	42.05	1.62	-4.58	55.83	123.02
709	47.43	33.76	1.52	-4.58	63.91	121.70
710	47.52	27.09	1.27	-4.77	70.43	120.03
711	47.59	23.86	0.95	-4.77	72.90	117.35
712	47.66	21.03	0.52	-4.77	72.89	114.76
713	47.77	19.51	0.53	-4.68	73.13	112.86
714	47.82	18.80	0.54	-4.58	76.41	112.94
715	47.91	18.19	0.56	-4.58	78.15	113.07
716	47.93	18.35	0.57	-4.36	81.01	113.17
717	47.97	16.68	0.58	-4.36	81.15	113.36
718	48.02	18.50	0.60	-4.36	81.66	113.65
719	48.07	18.60	0.64	-4.23	80.69	114.13
720	48.12	18.60	0.68	-4.10	82.08	114.75

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	48.19	18.80	0.77	-4.01	83.29	115.28
722	48.23	18.90	0.79	-4.01	83.94	115.75
723	48.31	19.21	0.82	-4.01	83.94	116.02
724	48.35	19.51	0.84	-3.91	83.94	116.26
725	48.40	19.51	0.86	-3.91	84.74	116.39
726	48.45	18.90	0.88	-3.91	86.54	116.45
727	48.50	18.19	0.88	-3.82	89.36	116.43
728	48.55	17.29	0.89	-3.72	90.62	116.47
729	48.59	18.09	0.90	-3.72	91.76	116.60
730	48.67	17.69	0.94	-3.53	91.23	116.72
731	48.73	17.99	0.92	-3.53	91.27	116.67
732	48.78	17.99	0.89	-3.53	89.99	116.42
733	48.83	18.09	0.84	-3.53	88.84	116.04
734	48.91	17.99	0.79	-3.44	87.70	115.60
735	48.98	17.89	0.74	-3.34	86.94	115.19
736	49.03	17.79	0.72	-3.15	86.65	114.95
737	49.12	17.69	0.72	-3.05	85.60	114.48
738	49.17	17.69	0.61	-2.96	83.33	113.76
739	49.27	17.99	0.53	-2.96	80.70	113.14
740	49.31	18.50	0.56	-2.86	79.11	113.26
741	49.38	19.31	0.62	-2.77	78.69	113.92
742	49.45	19.91	0.66	-2.67	78.67	114.51
743	49.51	20.01	0.70	-2.67	81.86	114.78
744	49.54	17.18	0.72	-2.34	81.23	115.10
745	49.59	21.23	0.74	-2.34	79.36	115.30
746	49.64	22.24	0.73	-2.34	75.47	115.37
747	49.73	21.23	0.70	-2.00	76.06	115.20
748	49.83	20.22	0.70	-2.00	78.94	114.89
749	49.92	18.70	0.68	-1.91	82.21	114.64
750	49.98	17.79	0.67	-1.81	85.18	114.35
751	50.07	17.18	0.66	-1.72	86.78	114.13
752	50.16	17.08	0.64	-1.62	87.78	113.97
753	50.24	16.78	0.64	-1.53	88.72	113.83
754	50.32	16.27	0.63	-1.43	89.58	113.75
755	50.41	16.38	0.63	-1.43	90.32	113.77
756	50.50	16.38	0.65	-1.34	90.32	113.80
757	50.56	16.38	0.64	-1.34	90.32	113.63
758	50.66	16.07	0.59	-1.24	90.38	113.36
759	50.74	15.87	0.59	-1.15	90.68	113.17
760	50.84	15.87	0.60	-1.15	92.49	113.65
761	50.93	15.87	0.71	-1.05	95.02	114.60
762	50.98	16.17	0.85	-1.05	96.87	116.37
763	51.08	18.30	1.14	-0.95	92.70	118.68
764	51.17	24.36	1.53	-0.76	84.52	120.98
765	51.24	30.73	1.80	-0.76	77.19	122.97
766	51.34	35.28	2.14	-0.57	74.02	124.16
767	51.41	34.97	2.26	-0.57	71.12	123.46
768	51.51	32.25	1.21	-0.57	70.63	122.43

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	51.58	31.24	1.48	-0.57	69.74	121.04
770	51.68	30.12	1.47	-0.38	72.97	121.32
771	51.79	28.51	1.42	-0.38	77.64	121.01
772	51.82	23.55	1.42	0.00	80.70	120.81
773	51.85	25.57	1.43	0.00	84.43	120.74
774	51.91	24.06	1.47	0.10	84.06	121.14
775	52.00	25.37	1.63	0.19	85.77	121.55
776	52.05	25.17	1.70	0.48	82.19	122.20
777	52.10	30.63	1.77	0.67	73.91	122.79
778	52.19	39.52	1.77	0.67	64.23	123.22
779	52.28	45.29	1.67	0.19	57.68	123.38
780	52.34	47.31	1.65	-0.10	55.15	123.36
781	52.42	46.50	1.68	-0.38	55.52	123.38
782	52.48	44.48	1.70	-0.29	57.37	123.35
783	52.57	42.05	1.69	-0.29	59.26	123.14
784	52.62	40.43	1.61	-0.19	60.78	122.72
785	52.69	38.31	1.49	0.00	61.59	122.10
786	52.77	36.79	1.37	0.10	62.55	121.57
787	52.87	35.58	1.36	0.19	63.92	121.31
788	52.91	34.27	1.39	0.19	65.28	120.93
789	53.01	32.35	1.22	0.19	67.19	120.67
790	53.10	31.03	1.28	0.29	68.16	120.77
791	53.16	33.16	1.47	0.38	69.53	122.45
792	53.25	37.91	2.14	0.48	67.34	124.27
793	53.29	44.98	2.40	0.57	65.53	126.29
794	53.38	49.94	3.03	0.67	63.67	127.54
795	53.42	51.76	3.26	1.15	57.59	128.96
796	53.47	76.22	3.60	1.34	50.04	130.26
797	53.52	95.93	4.09	1.43	43.49	131.46
798	53.58	106.44	4.29	1.24	41.58	132.45
799	53.66	106.44	4.88	-1.34	42.62	133.05
800	53.75	98.56	5.19	-2.86	45.49	133.37
801	53.81	91.08	5.18	-6.30	49.54	133.18
802	53.87	77.43	5.01	-9.74	53.77	132.67
803	53.95	68.54	4.74	-10.69	59.61	131.92
804	54.01	56.20	4.47	-11.74	65.69	131.12
805	54.06	47.81	4.22	-11.84	72.92	129.99
806	54.15	39.02	3.56	-11.84	77.78	129.07
807	54.20	39.02	3.50	-11.84	78.61	128.77
808	54.29	44.27	3.87	-11.84	70.76	129.29
809	54.34	59.94	3.77	-11.84	51.11	129.21
810	54.43	104.52	2.08	-12.22	34.79	128.49
811	54.45	137.17	1.94	-11.93	23.26	127.27
812	54.48	170.33	1.92	-12.60	19.04	127.74
813	54.52	191.25	2.08	-13.36	17.01	128.18
814	54.53	195.50	2.08	-13.08	16.36	128.98
815	54.58	210.36	2.46	-12.79	16.17	129.67
816	54.62	218.44	2.63	-8.30	15.74	130.34

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	54.65	230.47	2.63	-4.01	14.88	130.73
818	54.70	251.70	2.72	-3.63	14.37	131.15
819	54.76	252.00	2.98	-4.09	14.25	131.53
820	54.77	249.83	2.99	-3.42	14.61	131.77
821	54.82	247.96	3.02	-3.42	14.54	131.82
822	54.87	256.85	3.02	-3.42	14.47	131.87
823	54.88	254.53	3.03	-2.96	14.29	131.89
824	54.91	255.64	3.02	-3.09	14.24	131.96
825	54.96	261.81	3.08	-2.96	13.92	132.10
826	54.97	272.93	3.13	-2.77	13.35	132.49
827	55.03	295.47	3.37	-2.39	12.75	133.09
828	55.09	316.39	3.69	-2.96	11.80	133.38
829	55.15	333.88	3.31	-3.25	10.23	132.43
830	55.20	333.38	2.00	-3.05	9.28	131.93
831	55.25	347.93	3.01	-3.05	7.69	130.99
832	55.30	393.32	2.16	-3.05	7.43	132.16
833	55.34	419.40	3.03	-2.96	6.93	132.95
834	55.39	439.92	3.71	-2.77	7.32	134.46
835	55.40	460.94	4.01	-2.86	7.35	135.39
836	55.44	486.11	4.30	-2.67	7.07	135.83
837	55.44	501.48	4.26	-2.67	6.42	136.02
838	55.49	546.16	4.10	-2.64	6.52	136.38
839	55.54	505.72	4.89	-1.24	6.65	137.08
840	55.59	548.48	5.43	-1.05	7.22	137.28
841	55.63	550.81	5.64	-2.46	7.14	137.28
842	55.64	554.04	5.65	-2.46	7.12	137.28
843	55.68	555.66	5.52	-2.67	6.77	137.28
844	55.69	591.24	5.48	-2.60	6.62	137.28
845	55.69	564.35	5.44	-2.60	6.75	137.28
846	55.71	543.02	5.64	-2.53	7.10	137.28
847	55.76	577.59	6.17	-2.53	7.22	137.28
848	55.78	581.33	6.12	-2.39	7.02	137.28
849	55.81	581.74	5.86	-2.19	6.58	137.28
850	55.85	580.73	4.95	-2.67	5.96	137.28
851	55.86	590.13	4.53	-2.96	5.19	136.82
852	55.91	594.27	4.00	-2.96	4.62	136.29
853	55.92	611.66	3.93	-2.58	4.30	135.90
854	55.96	600.94	3.86	-2.48	3.98	135.87
855	55.97	644.61	3.85	-2.96	3.85	136.11
856	56.00	656.84	4.22	-3.15	3.75	136.51
857	56.01	661.80	4.40	-3.25	4.03	137.12
858	56.03	661.85	4.90	-3.25	4.27	137.28
859	56.05	661.85	5.01	-3.05	4.38	137.28
860	56.10	661.90	4.73	-2.86	4.31	137.28
861	56.12	671.50	4.82	-2.77	4.05	137.28
862	56.16	670.79	4.37	-2.67	3.91	137.12
863	56.17	660.89	4.28	-2.77	3.94	136.81
864	56.20	632.79	4.35	-2.77	4.25	136.76

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	56.22	611.76	4.41	-2.77	4.54	136.69
866	56.24	608.02	4.27	-2.67	4.60	136.52
867	56.30	605.70	4.12	-2.77	4.63	136.39
868	56.31	594.48	4.22	-2.67	4.86	136.51
869	56.34	587.00	4.54	-2.67	5.22	136.76
870	56.39	577.29	4.62	-2.67	5.42	136.81
871	56.45	572.94	4.38	-2.77	5.52	136.73
872	56.48	566.78	4.44	-2.58	5.63	136.67
873	56.49	556.57	4.57	-2.48	6.11	137.00
874	56.53	543.12	5.08	-2.39	6.65	137.27
875	56.58	526.85	5.09	-2.29	7.00	137.27
876	56.63	517.25	4.68	-2.39	5.57	135.21
877	56.68	530.19	1.47	-2.67	4.07	132.85
878	56.73	530.69	1.99	-2.19	3.28	131.52
879	56.78	533.22	3.31	-2.10	4.70	133.92
880	56.83	515.12	4.11	-2.10	5.98	135.53
881	56.89	505.72	4.38	-1.81	6.76	136.05
882	56.95	489.35	4.29	-1.72	7.57	136.39
883	56.99	460.13	4.89	-1.77	8.27	136.67
884	57.01	461.35	5.04	-1.81	8.73	136.83
885	57.04	461.35	4.71	-1.77	8.64	136.75
886	57.09	462.56	4.73	-1.77	8.37	136.69
887	57.11	480.76	4.85	-1.72	8.26	136.91
888	57.13	489.04	5.06	-1.72	8.28	137.28
889	57.18	496.12	5.48	-1.72	8.57	137.28
890	57.19	481.26	5.56	-1.72	9.17	137.28
891	57.21	456.09	5.75	-1.53	9.62	137.28
892	57.24	456.14	5.61	-1.53	9.80	137.28
893	57.28	456.19	5.36	-1.53	9.62	137.28
894	57.32	457.91	5.35	-1.53	9.68	137.28
895	57.35	438.71	5.32	-1.62	9.84	137.28
896	57.38	439.61	5.31	-1.43	10.12	137.28
897	57.43	428.50	5.24	-1.43	10.11	137.06
898	57.48	423.44	4.91	-1.62	10.27	136.57
899	57.52	392.11	4.48	-1.53	10.16	135.74
900	57.57	380.28	3.84	-1.53	10.70	135.89
901	57.62	396.35	5.29	-1.53	11.26	136.75
902	57.68	413.43	6.11	-1.53	10.99	137.28
903	57.76	472.77	5.74	-1.43	9.99	137.28
904	57.81	500.57	5.68	-1.72	7.13	136.51
905	57.86	543.23	2.17	-1.72	4.79	134.57
906	57.89	587.00	2.33	-1.72	2.67	131.65
907	57.91	587.40	2.22	-1.72	2.56	131.81
908	57.92	576.28	2.27	-1.72	2.86	132.23
909	57.95	567.79	2.76	-1.72	3.35	132.94
910	57.99	563.14	3.00	-1.72	3.71	133.65
911	58.01	581.13	3.08	-1.72	3.92	134.30
912	58.05	591.95	3.53	-1.72	3.96	134.78

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	58.05	600.54	3.58	-1.05	4.23	135.48
914	58.10	604.18	4.04	-1.43	4.36	135.85
915	58.13	609.64	4.08	-1.53	4.44	136.17
916	58.15	619.75	4.05	-1.53	4.30	136.16
917	58.17	626.22	3.98	-1.53	4.19	136.18
918	58.20	629.45	4.07	-1.53	4.24	136.22
919	58.21	614.69	4.13	-1.72	4.37	136.30
920	58.21	614.14	4.14	-1.72	4.48	136.33
921	58.23	614.14	4.16	-1.72	4.50	136.34
922	58.24	613.58	4.15	-1.81	4.62	136.36
923	58.25	596.70	4.21	-1.81	3.41	134.35
924	58.29	617.42	1.15	-1.72	2.07	131.70
925	58.31	627.93	1.23	-1.72	0.59	127.71
926	58.33	636.43	1.41	-1.72	0.81	129.01
927	58.38	652.70	1.86	-1.62	1.14	130.50
928	58.39	665.03	2.22	-1.70	1.43	131.67
929	58.43	667.96	2.33	-1.62	1.54	132.23
930	58.43	678.68	2.34	-1.70	1.38	132.20
931	58.48	701.62	2.15	-1.62	1.49	132.66
932	58.53	683.83	2.76	-1.62	1.70	133.35
933	58.56	697.78	3.03	-1.81	2.25	134.65
934	58.58	707.59	3.68	-1.91	2.48	135.33
935	58.59	707.99	3.65	-1.73	2.66	135.86
936	58.63	717.19	3.78	-1.54	2.76	135.95
937	58.63	696.42	3.83	-1.37	2.82	136.12
938	58.63	714.06	3.90	-1.37	2.92	135.93
939	58.68	675.65	3.56	-1.03	2.66	135.58
940	58.69	710.92	3.27	-1.03	2.12	134.51
941	58.72	719.11	2.44	-1.03	1.55	133.64
942	58.73	723.56	2.46	-0.91	1.34	133.28
943	58.74	726.19	2.85	-0.48	1.62	134.13
944	58.77	736.20	3.38	-0.85	2.06	135.06
945	58.81	718.51	3.65	-0.85	2.44	135.72
946	58.82	713.35	3.81	-0.85	2.73	136.05
947	58.83	710.01	3.91	-0.86	2.96	136.52
948	58.87	724.07	4.41	-0.86	3.17	137.07
949	58.91	732.96	4.71	-0.86	3.32	137.28
950	58.92	738.02	4.73	-0.76	3.35	137.28
951	58.93	742.66	4.76	-0.67	3.28	137.28
952	58.96	740.95	4.59	-0.57	3.26	137.28
953	59.01	733.57	4.60	-0.57	3.68	137.28
954	59.06	674.43	5.18	-1.24	4.25	137.28
955	59.08	653.91	5.10	-1.24	4.86	137.28
956	59.11	637.54	4.96	-1.24	5.19	137.28
957	59.15	625.41	5.36	-1.24	5.74	137.28
958	59.21	618.74	6.10	-1.43	6.20	137.28
959	59.26	610.75	5.85	-0.95	6.43	137.28
960	59.30	588.81	5.33	-0.67	6.35	137.28

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	59.35	577.39	5.07	-0.67	6.33	137.28
962	59.40	573.45	5.09	-0.67	6.60	137.28
963	59.42	537.46	5.10	-0.62	6.81	137.28
964	59.47	542.01	4.94	-0.62	7.03	137.28
965	59.51	538.58	4.99	-0.62	7.10	137.28
966	59.56	537.67	5.28	-0.48	7.14	137.28
967	59.61	537.67	4.95	-0.48	6.86	137.10
968	59.67	536.76	4.21	-0.48	6.15	136.33
969	59.71	551.52	3.80	-0.29	5.22	135.39
970	59.80	572.94	3.30	-0.29	4.51	134.34
971	59.85	543.02	2.68	-0.10	4.17	133.65
972	59.90	541.41	2.94	0.00	4.17	133.27
973	60.00	542.21	2.91	0.29	4.27	133.47
974	60.04	545.35	2.91	0.19	4.40	133.64
975	60.10	537.57	3.16	0.19	4.95	133.98
976	60.15	496.63	3.43	0.19	5.55	134.23
977	60.19	490.76	3.36	0.19	6.05	134.17
978	60.23	474.79	3.20	0.19	5.92	133.82
979	60.28	484.90	2.99	0.29	5.71	133.46
980	60.33	488.14	2.90	0.29	5.51	133.41
981	60.38	493.90	3.10	0.29	5.65	133.73
982	60.42	493.85	3.38	0.29	5.89	134.17
983	60.44	493.80	3.46	0.29	6.33	134.53
984	60.47	473.88	3.65	0.38	6.98	134.97
985	60.52	460.13	4.12	0.48	7.63	135.40
986	60.56	462.56	4.23	0.38	8.01	135.74
987	60.57	465.39	4.25	0.38	7.98	135.80
988	60.61	467.11	4.21	0.38	7.76	135.74
989	60.66	479.34	4.08	0.38	7.57	135.77
990	60.71	485.41	4.24	0.38	7.40	135.90
991	60.76	495.21	4.35	0.48	7.47	136.31
992	60.81	505.12	4.72	0.67	7.48	136.65
993	60.86	513.91	4.79	0.76	7.09	136.81
994	60.91	550.10	4.48	0.95	6.19	136.86
995	60.95	615.30	4.50	1.05	5.45	137.13
996	61.00	639.05	4.99	1.24	5.05	137.28
997	61.02	658.56	5.11	1.72	5.00	137.28
998	61.05	675.54	5.33	1.72	4.74	137.28
999	61.08	721.13	5.51	1.62	4.50	137.28
1000	61.09	733.97	5.54	1.62	4.27	137.28
1001	61.13	740.34	5.59	1.81	4.24	137.28
1002	61.14	739.43	5.66	1.91	4.28	137.28
1003	61.16	738.52	5.76	1.91	4.32	137.28
1004	61.20	746.30	5.81	1.91	4.05	137.28
1005	61.23	767.73	5.15	1.91	3.75	137.28
1006	61.24	772.28	5.21	1.81	3.14	137.28
1007	61.29	760.66	3.90	1.81	2.97	137.28
1008	61.30	743.57	4.26	1.72	3.09	137.25

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1009	61.33	728.41	5.05	1.81	3.50	137.28
1010	61.38	731.65	4.85	2.00	3.57	137.28
1011	61.43	732.56	4.32	1.81	3.24	137.17
1012	61.48	728.92	3.98	1.81	2.87	136.68
1013	61.53	753.18	3.97	1.62	2.61	136.51
1014	61.56	770.56	3.96	1.72	2.53	136.46
1015	61.58	740.54	3.88	1.72	2.82	136.29
1016	61.59	669.61	3.85	1.46	3.07	136.12
1017	61.62	696.97	3.82	0.67	4.53	135.66
1018	61.63	435.47	3.76	0.86	4.59	135.59
1019	61.67	653.41	3.77	1.34	4.68	135.51
1020	61.71	676.15	3.74	1.43	3.52	135.82
1021	61.76	658.36	3.79	1.34	3.57	135.69
1022	61.81	631.98	3.61	1.34	3.48	134.89
1023	61.86	611.66	2.70	1.53	3.19	133.76
1024	61.87	601.35	2.42	1.62	2.51	131.84
1025	61.91	589.42	1.65	1.72	2.08	130.34
1026	61.95	575.78	1.49	1.72	1.72	128.91
1027	61.96	568.80	1.46	1.62	1.77	128.59
1028	62.00	555.56	1.48	1.53	2.11	128.99
1029	62.04	536.66	1.77	1.43	2.73	129.80
1030	62.06	513.20	2.07	1.34	3.63	130.78
1031	62.10	482.98	2.34	1.34	4.36	131.39
1032	62.14	478.73	2.39	1.34	4.98	131.79
1033	62.20	464.78	2.54	1.34	5.42	131.98
1034	62.22	445.68	2.60	1.62	6.21	132.17
1035	62.27	407.07	2.72	1.43	7.02	132.25
1036	62.29	393.62	2.77	1.34	7.80	132.39
1037	62.34	388.36	2.89	1.43	8.52	132.51
1038	62.39	358.75	2.98	1.24	9.48	132.97
1039	62.43	352.68	3.46	1.43	11.11	133.79
1040	62.49	331.86	4.17	1.43	12.15	134.44
1041	62.57	335.80	4.05	1.43	12.81	134.86
1042	62.68	341.56	4.21	1.43	12.34	135.49
1043	62.75	394.13	5.02	1.53	11.19	136.33
1044	62.87	459.02	5.12	1.62	10.57	136.91
1045	62.88	425.46	5.04	1.53	11.01	136.62
1046	62.89	343.08	4.64	0.86	9.46	135.64
1047	62.93	504.41	3.12	1.53	6.80	134.88
1048	62.98	608.73	3.27	1.24	4.56	134.66
1049	63.02	602.56	3.75	1.53	2.42	132.17
1050	63.07	649.36	0.00	1.53	0.48	127.73
1051	63.12	723.66	0.00	1.62	N/A	87.36
1052	63.14	759.24	0.00	1.62	N/A	87.36
1053	63.17	774.10	0.00	1.72	N/A	87.36
1054	63.17	810.49	0.00	1.53	N/A	87.36
1055	63.20	813.42	0.00	1.53	N/A	87.36
1056	63.21	853.96	0.00	1.53	N/A	87.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1057	63.23	825.05	0.00	1.43	N/A	87.36
1058	63.26	849.66	0.00	0.99	N/A	87.36
1059	63.28	829.50	0.00	0.99	N/A	87.36
1060	63.31	845.37	0.00	0.29	N/A	87.36
1061	63.32	839.40	0.00	0.48	N/A	87.36
1062	63.36	833.34	0.00	0.57	N/A	87.36
1063	63.40	838.59	0.00	0.67	N/A	87.36

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c:	Measured cone resistance (tsf)
f_s:	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.01	0.00	0.00	0.00	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
2	0.04	0.00	0.00	0.00	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
3	0.09	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
4	0.11	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
5	0.14	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
6	0.14	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
7	0.18	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
8	0.23	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
9	0.24	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
10	0.28	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
11	0.33	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
12	0.38	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
13	0.42	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
14	0.47	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
15	0.51	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
16	0.52	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
17	0.57	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
18	0.61	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
19	0.67	0.04	0.00	0.04	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
20	0.73	0.04	0.00	0.04	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
21	0.81	0.04	0.00	0.04	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
22	0.86	0.05	0.00	0.05	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
23	0.98	0.05	0.00	0.05	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
24	1.05	0.06	0.00	0.06	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
25	1.15	0.06	0.00	0.06	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
26	1.24	0.07	0.00	0.07	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
27	1.34	0.07	0.00	0.07	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
28	1.43	0.08	0.00	0.08	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
29	1.53	0.09	0.00	0.09	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
30	1.58	0.09	0.00	0.09	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
31	1.62	0.09	0.00	0.09	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
32	1.67	0.09	0.00	0.09	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
33	1.75	0.10	0.00	0.10	1.00	0.409	1.36	0.300	1.00	1.00	2.000	No
34	1.77	0.10	0.00	0.10	1.00	0.409	1.36	0.300	1.00	1.00	2.000	No
35	1.81	0.10	0.00	0.10	1.00	0.409	1.36	0.300	1.00	1.00	2.000	No
36	1.86	0.10	0.00	0.10	1.00	0.409	1.36	0.300	1.00	1.00	2.000	No
37	1.91	0.11	0.00	0.11	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
38	1.95	0.11	0.00	0.11	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
39	2.00	0.11	0.00	0.11	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
40	2.05	0.11	0.00	0.11	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
41	2.11	0.12	0.00	0.12	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
42	2.20	0.12	0.00	0.12	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
43	2.24	0.12	0.00	0.12	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
44	2.29	0.13	0.00	0.13	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
45	2.34	0.13	0.00	0.13	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
46	2.44	0.13	0.00	0.13	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
47	2.48	0.13	0.00	0.13	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
48	2.58	0.14	0.00	0.14	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	2.63	0.14	0.00	0.14	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
50	2.71	0.15	0.00	0.15	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
51	2.78	0.15	0.00	0.15	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
52	2.82	0.15	0.00	0.15	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
53	2.89	0.16	0.00	0.16	1.00	0.408	1.36	0.300	1.00	1.00	2.000	Yes
54	2.96	0.16	0.00	0.16	1.00	0.407	1.36	0.300	1.00	1.00	2.000	No
55	3.03	0.17	0.00	0.17	0.99	0.407	1.36	0.300	1.00	1.00	2.000	No
56	3.11	0.17	0.00	0.17	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
57	3.19	0.17	0.00	0.17	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
58	3.25	0.18	0.00	0.18	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
59	3.35	0.18	0.00	0.18	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
60	3.41	0.19	0.00	0.19	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
61	3.50	0.19	0.00	0.19	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
62	3.59	0.20	0.00	0.20	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
63	3.69	0.20	0.00	0.20	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
64	3.79	0.21	0.00	0.21	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
65	3.88	0.21	0.00	0.21	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
66	3.97	0.22	0.00	0.22	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
67	4.07	0.22	0.00	0.22	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
68	4.14	0.22	0.00	0.22	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
69	4.17	0.23	0.00	0.23	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
70	4.26	0.23	0.00	0.23	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
71	4.32	0.23	0.00	0.23	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
72	4.37	0.24	0.00	0.24	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
73	4.42	0.24	0.00	0.24	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
74	4.51	0.24	0.00	0.24	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
75	4.61	0.25	0.00	0.25	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
76	4.65	0.25	0.00	0.25	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
77	4.74	0.26	0.00	0.26	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
78	4.80	0.26	0.00	0.26	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
79	4.89	0.26	0.00	0.26	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
80	4.95	0.27	0.00	0.27	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
81	5.04	0.27	0.00	0.27	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
82	5.13	0.28	0.00	0.28	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
83	5.18	0.28	0.00	0.28	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
84	5.28	0.29	0.00	0.29	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
85	5.32	0.29	0.00	0.29	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
86	5.42	0.29	0.00	0.29	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
87	5.51	0.30	0.00	0.30	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
88	5.60	0.30	0.00	0.30	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
89	5.66	0.31	0.00	0.31	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
90	5.76	0.31	0.00	0.31	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
91	5.85	0.32	0.00	0.32	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
92	5.92	0.32	0.00	0.32	0.99	0.405	1.36	0.297	1.00	1.00	2.000	No
93	5.95	0.32	0.00	0.32	0.99	0.405	1.36	0.297	1.00	1.00	2.000	No
94	5.97	0.32	0.00	0.32	0.99	0.405	1.36	0.297	1.00	1.00	2.000	No
95	6.02	0.33	0.00	0.33	0.99	0.405	1.36	0.297	1.00	1.00	2.000	Yes
96	6.06	0.33	0.00	0.33	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	6.16	0.33	0.00	0.33	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
98	6.21	0.34	0.00	0.34	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
99	6.26	0.34	0.00	0.34	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
100	6.31	0.34	0.00	0.34	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
101	6.40	0.35	0.00	0.35	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
102	6.44	0.35	0.00	0.35	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
103	6.52	0.35	0.00	0.35	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
104	6.57	0.36	0.00	0.36	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
105	6.64	0.36	0.00	0.36	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
106	6.69	0.36	0.00	0.36	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
107	6.78	0.37	0.00	0.37	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
108	6.83	0.37	0.00	0.37	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
109	6.92	0.37	0.00	0.37	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
110	6.97	0.38	0.00	0.38	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
111	7.03	0.38	0.00	0.38	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
112	7.12	0.38	0.00	0.38	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
113	7.22	0.39	0.00	0.39	0.99	0.403	1.36	0.297	1.00	1.00	2.000	No
114	7.27	0.39	0.00	0.39	0.99	0.403	1.36	0.297	1.00	1.00	2.000	No
115	7.36	0.40	0.00	0.40	0.98	0.403	1.36	0.297	1.00	1.00	2.000	No
116	7.43	0.40	0.00	0.40	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
117	7.50	0.41	0.00	0.41	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
118	7.59	0.41	0.00	0.41	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
119	7.64	0.41	0.00	0.41	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
120	7.75	0.42	0.00	0.42	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
121	7.79	0.42	0.00	0.42	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
122	7.89	0.43	0.00	0.43	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
123	7.99	0.43	0.00	0.43	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
124	8.04	0.43	0.00	0.43	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
125	8.13	0.44	0.00	0.44	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
126	8.23	0.44	0.00	0.44	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
127	8.32	0.45	0.00	0.45	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
128	8.37	0.45	0.00	0.45	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
129	8.46	0.46	0.00	0.46	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
130	8.56	0.46	0.00	0.46	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
131	8.59	0.46	0.00	0.46	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
132	8.61	0.47	0.00	0.47	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
133	8.67	0.47	0.00	0.47	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
134	8.71	0.47	0.00	0.47	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
135	8.72	0.47	0.00	0.47	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
136	8.78	0.47	0.00	0.47	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
137	8.80	0.48	0.00	0.48	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
138	8.86	0.48	0.00	0.48	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
139	8.90	0.48	0.00	0.48	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
140	8.95	0.48	0.00	0.48	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
141	8.96	0.48	0.00	0.48	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
142	9.00	0.49	0.00	0.49	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
143	9.05	0.49	0.00	0.49	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
144	9.09	0.49	0.00	0.49	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	9.10	0.49	0.00	0.49	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
146	9.14	0.49	0.00	0.49	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
147	9.20	0.50	0.00	0.50	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
148	9.24	0.50	0.00	0.50	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
149	9.29	0.50	0.00	0.50	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
150	9.31	0.50	0.00	0.50	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
151	9.38	0.51	0.00	0.51	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
152	9.41	0.51	0.00	0.51	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
153	9.47	0.51	0.00	0.51	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
154	9.53	0.52	0.00	0.52	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
155	9.62	0.52	0.00	0.52	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
156	9.67	0.52	0.00	0.52	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
157	9.77	0.53	0.00	0.53	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
158	9.81	0.53	0.00	0.53	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
159	9.90	0.54	0.00	0.54	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
160	9.97	0.54	0.00	0.54	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
161	10.06	0.55	0.00	0.55	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
162	10.20	0.55	0.00	0.55	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
163	10.30	0.56	0.00	0.56	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
164	10.44	0.57	0.00	0.57	0.98	0.401	1.36	0.295	1.00	1.00	2.000	Yes
165	10.54	0.57	0.00	0.57	0.98	0.400	1.36	0.294	1.00	1.00	2.000	Yes
166	10.63	0.58	0.00	0.58	0.98	0.400	1.36	0.294	1.00	1.00	2.000	Yes
167	10.74	0.58	0.00	0.58	0.98	0.400	1.36	0.294	1.00	1.00	2.000	Yes
168	10.78	0.59	0.00	0.59	0.98	0.400	1.36	0.294	1.00	1.00	2.000	Yes
169	10.83	0.59	0.00	0.59	0.98	0.400	1.36	0.294	1.00	1.00	2.000	Yes
170	10.88	0.59	0.00	0.59	0.98	0.400	1.36	0.294	1.00	1.00	2.000	Yes
171	10.89	0.59	0.00	0.59	0.98	0.400	1.36	0.294	1.00	1.00	2.000	Yes
172	10.97	0.60	0.00	0.60	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
173	11.02	0.60	0.00	0.60	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
174	11.07	0.60	0.00	0.60	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
175	11.11	0.60	0.00	0.60	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
176	11.16	0.61	0.00	0.61	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
177	11.21	0.61	0.00	0.61	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
178	11.26	0.61	0.00	0.61	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
179	11.30	0.62	0.00	0.62	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
180	11.36	0.62	0.00	0.62	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
181	11.40	0.62	0.00	0.62	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
182	11.45	0.62	0.00	0.62	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
183	11.50	0.63	0.00	0.63	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
184	11.55	0.63	0.00	0.63	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
185	11.60	0.63	0.00	0.63	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
186	11.66	0.64	0.00	0.64	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
187	11.74	0.64	0.00	0.64	0.98	0.399	1.36	0.294	1.00	1.00	2.000	No
188	11.84	0.65	0.00	0.65	0.98	0.399	1.36	0.294	1.00	1.00	2.000	No
189	11.93	0.65	0.00	0.65	0.98	0.399	1.36	0.294	1.00	1.00	2.000	No
190	12.04	0.66	0.00	0.66	0.97	0.399	1.36	0.294	1.00	1.00	2.000	No
191	12.13	0.66	0.00	0.66	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
192	12.22	0.67	0.00	0.67	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	12.27	0.67	0.00	0.67	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
194	12.37	0.68	0.00	0.68	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
195	12.41	0.68	0.00	0.68	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
196	12.51	0.69	0.00	0.69	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
197	12.56	0.69	0.00	0.69	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
198	12.65	0.69	0.00	0.69	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
199	12.71	0.70	0.00	0.70	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
200	12.79	0.70	0.00	0.70	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
201	12.89	0.71	0.00	0.71	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
202	12.96	0.71	0.00	0.71	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
203	13.04	0.72	0.00	0.72	0.97	0.398	1.36	0.293	1.00	1.00	2.000	Yes
204	13.13	0.72	0.00	0.72	0.97	0.398	1.36	0.293	1.00	1.00	2.000	Yes
205	13.23	0.73	0.00	0.73	0.97	0.398	1.36	0.293	1.00	1.00	2.000	Yes
206	13.30	0.73	0.00	0.73	0.97	0.398	1.36	0.293	1.00	1.00	2.000	Yes
207	13.37	0.74	0.00	0.74	0.97	0.398	1.36	0.293	1.00	1.00	2.000	Yes
208	13.47	0.74	0.00	0.74	0.97	0.398	1.36	0.293	1.00	1.00	2.000	Yes
209	13.57	0.75	0.00	0.75	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
210	13.61	0.75	0.00	0.75	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
211	13.62	0.75	0.00	0.75	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
212	13.68	0.75	0.00	0.75	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
213	13.73	0.76	0.00	0.76	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
214	13.77	0.76	0.00	0.76	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
215	13.87	0.77	0.00	0.77	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
216	13.93	0.77	0.00	0.77	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
217	14.00	0.77	0.00	0.77	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
218	14.06	0.78	0.00	0.78	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
219	14.12	0.78	0.00	0.78	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
220	14.21	0.79	0.00	0.79	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
221	14.25	0.79	0.00	0.79	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
222	14.35	0.79	0.00	0.79	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
223	14.45	0.80	0.00	0.80	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
224	14.50	0.80	0.00	0.80	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
225	14.59	0.81	0.00	0.81	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
226	14.64	0.81	0.00	0.81	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
227	14.74	0.82	0.00	0.82	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
228	14.80	0.82	0.00	0.82	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
229	14.88	0.83	0.00	0.83	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
230	14.97	0.83	0.00	0.83	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
231	15.05	0.84	0.00	0.84	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
232	15.13	0.84	0.00	0.84	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
233	15.21	0.85	0.00	0.85	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
234	15.28	0.85	0.00	0.85	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
235	15.36	0.86	0.00	0.86	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
236	15.41	0.86	0.00	0.86	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
237	15.50	0.86	0.00	0.86	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
238	15.55	0.87	0.00	0.87	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
239	15.65	0.87	0.00	0.87	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
240	15.71	0.88	0.00	0.88	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	15.79	0.88	0.00	0.88	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
242	15.89	0.89	0.00	0.89	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
243	15.90	0.89	0.00	0.89	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
244	15.94	0.89	0.00	0.89	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
245	16.00	0.89	0.00	0.89	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
246	16.06	0.90	0.00	0.90	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
247	16.14	0.90	0.00	0.90	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
248	16.19	0.90	0.00	0.90	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
249	16.26	0.91	0.00	0.91	0.97	0.395	1.36	0.291	1.00	1.00	2.000	Yes
250	16.33	0.91	0.00	0.91	0.97	0.395	1.36	0.291	1.00	1.00	2.000	Yes
251	16.38	0.91	0.00	0.91	0.97	0.395	1.36	0.291	1.00	1.00	2.000	Yes
252	16.47	0.92	0.00	0.92	0.97	0.395	1.36	0.291	1.00	1.00	2.000	Yes
253	16.54	0.92	0.00	0.92	0.97	0.395	1.36	0.291	1.00	1.00	2.000	Yes
254	16.62	0.93	0.00	0.93	0.97	0.395	1.36	0.291	1.00	1.00	2.000	No
255	16.70	0.93	0.00	0.93	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
256	16.76	0.94	0.00	0.94	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
257	16.86	0.94	0.00	0.94	0.96	0.395	1.36	0.290	1.00	1.00	2.000	Yes
258	16.90	0.94	0.00	0.94	0.96	0.395	1.36	0.290	1.00	1.00	2.000	Yes
259	16.98	0.95	0.00	0.95	0.96	0.395	1.36	0.290	1.00	1.00	2.000	Yes
260	17.05	0.95	0.00	0.95	0.96	0.395	1.36	0.290	1.00	1.00	2.000	Yes
261	17.14	0.96	0.00	0.96	0.96	0.395	1.36	0.290	1.00	1.00	2.000	Yes
262	17.20	0.96	0.00	0.96	0.96	0.395	1.36	0.290	1.00	1.00	2.000	Yes
263	17.29	0.97	0.00	0.97	0.96	0.395	1.36	0.290	1.00	1.00	2.000	Yes
264	17.34	0.97	0.00	0.97	0.96	0.394	1.36	0.290	1.00	1.00	2.000	Yes
265	17.44	0.98	0.00	0.98	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
266	17.50	0.98	0.00	0.98	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
267	17.58	0.98	0.00	0.98	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
268	17.64	0.99	0.00	0.99	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
269	17.75	0.99	0.00	0.99	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
270	17.82	1.00	0.00	1.00	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
271	17.89	1.00	0.00	1.00	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
272	17.89	1.00	0.00	1.00	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
273	17.96	1.01	0.00	1.01	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
274	18.02	1.01	0.00	1.01	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
275	18.07	1.01	0.00	1.01	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
276	18.17	1.02	0.00	1.02	0.96	0.394	1.36	0.289	1.00	1.00	2.000	No
277	18.22	1.02	0.00	1.02	0.96	0.394	1.36	0.289	1.00	1.00	2.000	Yes
278	18.30	1.03	0.00	1.03	0.96	0.394	1.36	0.289	1.00	1.00	2.000	Yes
279	18.36	1.03	0.00	1.03	0.96	0.394	1.36	0.289	1.00	1.00	2.000	Yes
280	18.42	1.03	0.00	1.03	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
281	18.50	1.04	0.00	1.04	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
282	18.56	1.04	0.00	1.04	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
283	18.62	1.05	0.00	1.05	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
284	18.69	1.05	0.00	1.05	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
285	18.76	1.05	0.00	1.05	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
286	18.84	1.06	0.00	1.06	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
287	18.89	1.06	0.00	1.06	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
288	18.98	1.07	0.00	1.07	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	19.05	1.07	0.00	1.07	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
290	19.12	1.08	0.00	1.08	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
291	19.18	1.08	0.00	1.08	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
292	19.24	1.08	0.00	1.08	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
293	19.32	1.09	0.00	1.09	0.96	0.393	1.36	0.289	0.99	1.00	2.000	No
294	19.38	1.09	0.00	1.09	0.96	0.392	1.36	0.289	0.99	1.00	2.000	No
295	19.46	1.10	0.00	1.10	0.96	0.392	1.36	0.289	0.99	1.00	2.000	No
296	19.54	1.10	0.00	1.10	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
297	19.62	1.11	0.00	1.11	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
298	19.70	1.11	0.00	1.11	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
299	19.80	1.12	0.00	1.12	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
300	19.85	1.12	0.00	1.12	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
301	19.94	1.13	0.00	1.13	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
302	20.03	1.13	0.00	1.13	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
303	20.13	1.14	0.00	1.14	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
304	20.19	1.14	0.00	1.14	0.96	0.392	1.36	0.288	0.98	1.00	2.000	No
305	20.29	1.15	0.00	1.15	0.96	0.392	1.36	0.288	0.98	1.00	2.000	No
306	20.39	1.16	0.00	1.16	0.96	0.391	1.36	0.288	0.98	1.00	2.000	No
307	20.43	1.16	0.00	1.16	0.96	0.391	1.36	0.288	0.98	1.00	2.000	No
308	20.47	1.16	0.00	1.16	0.96	0.391	1.36	0.288	0.98	1.00	2.000	No
309	20.52	1.16	0.00	1.16	0.96	0.391	1.36	0.288	0.98	1.00	2.000	No
310	20.61	1.17	0.00	1.17	0.96	0.391	1.36	0.288	0.98	1.00	2.000	No
311	20.66	1.17	0.00	1.17	0.96	0.391	1.36	0.288	0.98	1.00	2.000	No
312	20.71	1.18	0.00	1.18	0.96	0.391	1.36	0.288	0.98	1.00	2.000	No
313	20.77	1.18	0.00	1.18	0.95	0.391	1.36	0.287	0.98	1.00	2.000	No
314	20.85	1.18	0.00	1.18	0.95	0.391	1.36	0.287	0.98	1.00	2.000	No
315	20.91	1.19	0.00	1.19	0.95	0.391	1.36	0.287	0.98	1.00	2.000	No
316	21.00	1.19	0.00	1.19	0.95	0.391	1.36	0.287	0.98	1.00	2.000	No
317	21.05	1.20	0.00	1.20	0.95	0.391	1.36	0.287	0.98	1.00	2.000	No
318	21.11	1.20	0.00	1.20	0.95	0.391	1.36	0.287	0.97	1.00	2.000	No
319	21.19	1.21	0.00	1.21	0.95	0.391	1.36	0.287	0.97	1.00	2.000	No
320	21.24	1.21	0.00	1.21	0.95	0.390	1.36	0.287	0.97	1.00	2.000	No
321	21.34	1.22	0.00	1.22	0.95	0.390	1.36	0.287	0.97	1.00	2.000	No
322	21.39	1.22	0.00	1.22	0.95	0.390	1.36	0.287	0.97	1.00	2.000	No
323	21.48	1.22	0.00	1.22	0.95	0.390	1.36	0.287	0.97	1.00	2.000	No
324	21.53	1.23	0.00	1.23	0.95	0.390	1.36	0.287	0.97	1.00	2.000	No
325	21.64	1.23	0.00	1.23	0.95	0.390	1.36	0.287	0.97	1.00	2.000	No
326	21.72	1.24	0.00	1.24	0.95	0.390	1.36	0.287	0.97	1.00	2.000	No
327	21.81	1.24	0.00	1.24	0.95	0.390	1.36	0.287	0.97	1.00	2.000	No
328	21.89	1.25	0.00	1.25	0.95	0.390	1.36	0.287	0.97	1.00	2.000	No
329	21.97	1.25	0.00	1.25	0.95	0.390	1.36	0.286	0.97	1.00	2.000	No
330	22.05	1.26	0.00	1.26	0.95	0.390	1.36	0.286	0.97	1.00	2.000	No
331	22.12	1.26	0.00	1.26	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
332	22.13	1.26	0.00	1.26	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
333	22.18	1.27	0.00	1.27	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
334	22.22	1.27	0.00	1.27	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
335	22.28	1.27	0.00	1.27	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
336	22.33	1.28	0.00	1.28	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	22.38	1.28	0.00	1.28	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
338	22.41	1.28	0.00	1.28	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
339	22.51	1.29	0.00	1.29	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
340	22.56	1.29	0.00	1.29	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
341	22.61	1.29	0.00	1.29	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
342	22.65	1.30	0.00	1.30	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
343	22.71	1.30	0.00	1.30	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
344	22.76	1.30	0.00	1.30	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
345	22.85	1.31	0.00	1.31	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
346	22.89	1.31	0.00	1.31	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
347	22.99	1.32	0.00	1.32	0.95	0.388	1.36	0.286	0.96	1.00	2.000	No
348	23.04	1.32	0.00	1.32	0.95	0.388	1.36	0.286	0.96	1.00	2.000	No
349	23.12	1.33	0.00	1.33	0.95	0.388	1.36	0.285	0.96	1.00	2.000	No
350	23.18	1.33	0.00	1.33	0.95	0.388	1.36	0.285	0.96	1.00	2.000	No
351	23.24	1.33	0.00	1.33	0.95	0.388	1.36	0.285	0.95	1.00	2.000	No
352	23.33	1.34	0.00	1.34	0.95	0.388	1.36	0.285	0.95	1.00	2.000	No
353	23.38	1.34	0.00	1.34	0.95	0.388	1.36	0.285	0.95	1.00	2.000	No
354	23.47	1.35	0.00	1.35	0.95	0.388	1.36	0.285	0.95	1.00	2.000	No
355	23.52	1.35	0.00	1.35	0.95	0.388	1.36	0.285	0.95	1.00	2.000	No
356	23.61	1.36	0.00	1.36	0.95	0.388	1.36	0.285	0.95	1.00	2.000	No
357	23.68	1.36	0.00	1.36	0.95	0.388	1.36	0.285	0.95	1.00	2.000	No
358	23.76	1.36	0.00	1.36	0.95	0.387	1.36	0.285	0.95	1.00	2.000	No
359	23.83	1.37	0.00	1.37	0.95	0.387	1.36	0.285	0.95	1.00	2.000	No
360	23.90	1.37	0.00	1.37	0.95	0.387	1.36	0.285	0.95	1.00	2.000	No
361	23.97	1.38	0.00	1.38	0.95	0.387	1.36	0.285	0.95	1.00	2.000	No
362	24.05	1.38	0.00	1.38	0.95	0.387	1.36	0.285	0.95	1.00	2.000	No
363	24.10	1.39	0.00	1.39	0.94	0.387	1.36	0.284	0.95	1.00	2.000	No
364	24.19	1.39	0.00	1.39	0.94	0.387	1.36	0.284	0.95	1.00	2.000	No
365	24.27	1.40	0.00	1.40	0.94	0.387	1.36	0.284	0.95	1.00	2.000	No
366	24.34	1.40	0.00	1.40	0.94	0.387	1.36	0.284	0.95	1.00	2.000	No
367	24.43	1.41	0.00	1.41	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
368	24.48	1.41	0.00	1.41	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
369	24.57	1.41	0.00	1.41	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
370	24.62	1.42	0.00	1.42	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
371	24.72	1.42	0.00	1.42	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
372	24.81	1.43	0.00	1.43	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
373	24.86	1.43	0.00	1.43	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
374	24.95	1.44	0.00	1.44	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
375	25.01	1.44	0.00	1.44	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
376	25.02	1.44	0.00	1.44	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
377	25.05	1.44	0.00	1.44	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
378	25.11	1.45	0.00	1.45	0.94	0.386	1.36	0.283	0.94	1.00	2.000	No
379	25.15	1.45	0.00	1.45	0.94	0.385	1.36	0.283	0.94	1.00	2.000	No
380	25.21	1.45	0.00	1.45	0.94	0.385	1.36	0.283	0.94	1.00	2.000	No
381	25.25	1.46	0.00	1.46	0.94	0.385	1.36	0.283	0.94	1.00	2.000	No
382	25.30	1.46	0.00	1.46	0.94	0.385	1.36	0.283	0.94	1.00	2.000	No
383	25.40	1.47	0.00	1.47	0.94	0.385	1.36	0.283	0.94	1.00	2.000	No
384	25.45	1.47	0.00	1.47	0.94	0.385	1.36	0.283	0.94	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	25.52	1.47	0.00	1.47	0.94	0.385	1.36	0.283	0.94	1.00	2.000	Yes
386	25.60	1.48	0.00	1.48	0.94	0.385	1.36	0.283	0.94	1.00	2.000	Yes
387	25.66	1.48	0.00	1.48	0.94	0.385	1.36	0.283	0.93	1.00	2.000	Yes
388	25.74	1.49	0.00	1.49	0.94	0.385	1.36	0.283	0.93	1.00	2.000	Yes
389	25.80	1.49	0.00	1.49	0.94	0.384	1.36	0.283	0.93	1.00	2.000	Yes
390	25.88	1.49	0.00	1.49	0.94	0.384	1.36	0.283	0.93	1.00	2.000	Yes
391	25.94	1.50	0.00	1.50	0.94	0.384	1.36	0.283	0.93	1.00	2.000	Yes
392	26.02	1.50	0.00	1.50	0.94	0.384	1.36	0.282	0.93	1.00	2.000	Yes
393	26.09	1.51	0.00	1.51	0.94	0.384	1.36	0.282	0.93	1.00	2.000	No
394	26.17	1.51	0.00	1.51	0.94	0.384	1.36	0.282	0.93	1.00	2.000	No
395	26.23	1.52	0.00	1.52	0.94	0.384	1.36	0.282	0.93	1.00	2.000	No
396	26.29	1.52	0.00	1.52	0.94	0.384	1.36	0.282	0.93	1.00	2.000	No
397	26.37	1.52	0.00	1.52	0.94	0.384	1.36	0.282	0.93	1.00	2.000	No
398	26.46	1.53	0.00	1.53	0.94	0.383	1.36	0.282	0.93	1.00	2.000	No
399	26.55	1.53	0.00	1.53	0.94	0.383	1.36	0.282	0.93	1.00	2.000	No
400	26.60	1.54	0.00	1.54	0.94	0.383	1.36	0.282	0.93	1.00	2.000	No
401	26.70	1.54	0.00	1.54	0.94	0.383	1.36	0.282	0.93	1.00	2.000	No
402	26.78	1.55	0.00	1.55	0.94	0.383	1.36	0.282	0.93	1.00	2.000	No
403	26.87	1.55	0.00	1.55	0.93	0.383	1.36	0.281	0.93	1.00	2.000	No
404	26.94	1.56	0.00	1.56	0.93	0.383	1.36	0.281	0.93	1.00	2.000	No
405	27.03	1.56	0.00	1.56	0.93	0.383	1.36	0.281	0.93	1.00	2.000	No
406	27.13	1.57	0.00	1.57	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
407	27.18	1.57	0.00	1.57	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
408	27.27	1.58	0.00	1.58	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
409	27.32	1.58	0.00	1.58	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
410	27.37	1.58	0.00	1.58	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
411	27.41	1.58	0.00	1.58	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
412	27.46	1.59	0.00	1.59	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
413	27.51	1.59	0.00	1.59	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
414	27.61	1.59	0.00	1.59	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
415	27.66	1.60	0.00	1.60	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
416	27.73	1.60	0.00	1.60	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
417	27.80	1.61	0.00	1.61	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
418	27.88	1.61	0.00	1.61	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
419	27.96	1.62	0.00	1.62	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
420	28.04	1.62	0.00	1.62	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
421	28.12	1.63	0.00	1.63	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
422	28.18	1.63	0.00	1.63	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
423	28.27	1.64	0.00	1.64	0.93	0.380	1.36	0.280	0.92	1.00	2.000	No
424	28.32	1.64	0.00	1.64	0.93	0.380	1.36	0.280	0.92	1.00	2.000	No
425	28.42	1.64	0.00	1.64	0.93	0.380	1.36	0.279	0.92	1.00	2.000	No
426	28.47	1.65	0.00	1.65	0.93	0.380	1.36	0.279	0.92	1.00	2.000	No
427	28.61	1.66	0.00	1.66	0.93	0.380	1.36	0.279	0.91	1.00	2.000	No
428	28.67	1.66	0.00	1.66	0.93	0.380	1.36	0.279	0.91	1.00	2.000	Yes
429	28.75	1.67	0.00	1.67	0.93	0.379	1.36	0.279	0.91	1.00	2.000	Yes
430	28.81	1.67	0.00	1.67	0.93	0.379	1.36	0.279	0.91	1.00	2.000	Yes
431	28.90	1.68	0.00	1.68	0.93	0.379	1.36	0.279	0.91	1.00	2.000	Yes
432	29.00	1.68	0.00	1.68	0.93	0.379	1.36	0.279	0.91	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	29.05	1.68	0.00	1.68	0.93	0.379	1.36	0.279	0.91	1.00	2.000	Yes
434	29.10	1.69	0.00	1.69	0.93	0.379	1.36	0.278	0.91	1.00	2.000	Yes
435	29.15	1.69	0.00	1.69	0.92	0.379	1.36	0.278	0.91	1.00	2.000	Yes
436	29.24	1.70	0.00	1.70	0.92	0.379	1.36	0.278	0.91	1.00	2.000	Yes
437	29.29	1.70	0.00	1.70	0.92	0.378	1.36	0.278	0.91	1.00	2.000	Yes
438	29.37	1.71	0.00	1.71	0.92	0.378	1.36	0.278	0.91	1.00	2.000	Yes
439	29.43	1.71	0.00	1.71	0.92	0.378	1.36	0.278	0.91	1.00	2.000	Yes
440	29.53	1.72	0.00	1.72	0.92	0.378	1.36	0.278	0.91	1.00	2.000	No
441	29.62	1.72	0.00	1.72	0.92	0.378	1.36	0.278	0.91	1.00	2.000	No
442	29.68	1.72	0.00	1.72	0.92	0.378	1.36	0.278	0.91	1.00	2.000	No
443	29.80	1.73	0.00	1.73	0.92	0.377	1.36	0.277	0.91	1.00	2.000	No
444	29.91	1.74	0.00	1.74	0.92	0.377	1.36	0.277	0.91	1.00	2.000	No
445	30.00	1.74	0.00	1.74	0.92	0.377	1.36	0.277	0.90	1.00	0.306	No
446	30.07	1.75	0.00	1.75	0.92	0.377	1.36	0.277	0.90	1.00	0.307	No
447	30.15	1.75	0.00	1.75	0.92	0.378	1.36	0.278	0.90	1.00	0.307	No
448	30.21	1.76	0.01	1.75	0.92	0.378	1.36	0.278	0.90	1.00	0.307	No
449	30.26	1.76	0.01	1.75	0.92	0.378	1.36	0.278	0.90	1.00	0.308	No
450	30.31	1.76	0.01	1.75	0.92	0.378	1.36	0.278	0.90	1.00	0.308	No
451	30.38	1.77	0.01	1.76	0.92	0.379	1.36	0.278	0.90	1.00	0.308	No
452	30.45	1.77	0.01	1.76	0.92	0.379	1.36	0.279	0.90	1.00	0.308	No
453	30.50	1.78	0.02	1.76	0.92	0.379	1.36	0.279	0.90	1.00	0.309	No
454	30.55	1.78	0.02	1.76	0.92	0.379	1.36	0.279	0.90	1.00	0.309	No
455	30.64	1.78	0.02	1.76	0.92	0.380	1.36	0.279	0.90	1.00	0.309	No
456	30.70	1.79	0.02	1.77	0.92	0.380	1.36	0.279	0.90	1.00	0.310	No
457	30.79	1.79	0.02	1.77	0.92	0.381	1.36	0.280	0.90	1.00	0.310	No
458	30.84	1.80	0.03	1.77	0.92	0.381	1.36	0.280	0.90	1.00	0.310	No
459	30.93	1.80	0.03	1.77	0.92	0.381	1.36	0.280	0.90	1.00	0.311	No
460	30.98	1.81	0.03	1.78	0.92	0.381	1.36	0.280	0.90	1.00	0.311	No
461	31.05	1.81	0.03	1.78	0.92	0.382	1.36	0.281	0.90	1.00	0.311	No
462	31.13	1.81	0.04	1.78	0.91	0.382	1.36	0.281	0.90	1.00	0.312	No
463	31.17	1.82	0.04	1.78	0.91	0.382	1.36	0.281	0.90	1.00	0.312	No
464	31.27	1.82	0.04	1.78	0.91	0.383	1.36	0.281	0.90	1.00	0.312	No
465	31.32	1.83	0.04	1.79	0.91	0.383	1.36	0.281	0.90	1.00	0.312	No
466	31.41	1.83	0.04	1.79	0.91	0.383	1.36	0.282	0.90	1.00	0.313	No
467	31.46	1.84	0.05	1.79	0.91	0.383	1.36	0.282	0.90	1.00	0.313	No
468	31.52	1.84	0.05	1.79	0.91	0.384	1.36	0.282	0.90	1.00	0.313	No
469	31.61	1.84	0.05	1.79	0.91	0.384	1.36	0.282	0.90	1.00	0.314	No
470	31.66	1.85	0.05	1.80	0.91	0.384	1.36	0.282	0.90	1.00	0.314	No
471	31.75	1.85	0.05	1.80	0.91	0.384	1.36	0.283	0.90	1.00	0.314	No
472	31.80	1.86	0.06	1.80	0.91	0.385	1.36	0.283	0.90	1.00	0.315	No
473	31.90	1.86	0.06	1.80	0.91	0.385	1.36	0.283	0.90	1.00	0.315	No
474	31.94	1.87	0.06	1.81	0.91	0.385	1.36	0.283	0.90	1.00	0.315	No
475	32.04	1.87	0.06	1.81	0.91	0.386	1.36	0.283	0.90	1.00	0.316	No
476	32.09	1.87	0.07	1.81	0.91	0.386	1.36	0.284	0.90	1.00	0.316	No
477	32.20	1.88	0.07	1.81	0.91	0.386	1.36	0.284	0.90	1.00	0.316	No
478	32.24	1.88	0.07	1.81	0.91	0.386	1.36	0.284	0.90	1.00	0.316	No
479	32.28	1.89	0.07	1.82	0.91	0.386	1.36	0.284	0.90	1.00	0.317	No
480	32.29	1.89	0.07	1.82	0.91	0.386	1.36	0.284	0.90	1.00	0.317	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	32.30	1.89	0.07	1.82	0.91	0.387	1.36	0.284	0.90	1.00	0.317	No
482	32.40	1.89	0.07	1.82	0.91	0.387	1.36	0.284	0.90	1.00	0.317	No
483	32.45	1.90	0.08	1.82	0.91	0.387	1.36	0.285	0.90	1.00	0.317	No
484	32.55	1.90	0.08	1.82	0.91	0.387	1.36	0.285	0.90	1.00	0.318	No
485	32.59	1.91	0.08	1.83	0.91	0.388	1.36	0.285	0.90	1.00	0.318	No
486	32.69	1.91	0.08	1.83	0.91	0.388	1.36	0.285	0.90	1.00	0.318	No
487	32.76	1.92	0.09	1.83	0.91	0.388	1.36	0.285	0.90	1.00	0.318	No
488	32.84	1.92	0.09	1.83	0.90	0.388	1.36	0.286	0.90	1.00	0.319	No
489	32.90	1.93	0.09	1.84	0.90	0.389	1.36	0.286	0.90	1.00	0.319	No
490	32.98	1.93	0.09	1.84	0.90	0.389	1.36	0.286	0.90	1.00	0.319	No
491	33.06	1.94	0.10	1.84	0.90	0.389	1.36	0.286	0.90	1.00	0.320	No
492	33.12	1.94	0.10	1.84	0.90	0.389	1.36	0.286	0.89	1.00	0.320	No
493	33.22	1.95	0.10	1.85	0.90	0.390	1.36	0.286	0.89	1.00	0.320	No
494	33.31	1.95	0.10	1.85	0.90	0.390	1.36	0.287	0.89	1.00	0.321	No
495	33.37	1.96	0.10	1.85	0.90	0.390	1.36	0.287	0.89	1.00	0.321	No
496	33.46	1.96	0.11	1.85	0.90	0.390	1.36	0.287	0.89	1.00	0.321	No
497	33.55	1.97	0.11	1.86	0.90	0.391	1.36	0.287	0.89	1.00	0.321	No
498	33.65	1.97	0.11	1.86	0.90	0.391	1.36	0.287	0.89	1.00	0.322	No
499	33.70	1.98	0.12	1.86	0.90	0.391	1.36	0.288	0.89	1.00	0.322	No
500	33.79	1.98	0.12	1.86	0.90	0.391	1.36	0.288	0.89	1.00	0.322	No
501	33.89	1.99	0.12	1.87	0.90	0.392	1.36	0.288	0.89	1.00	0.323	No
502	33.99	2.00	0.12	1.87	0.90	0.392	1.36	0.288	0.89	1.00	0.323	No
503	34.04	2.00	0.13	1.87	0.90	0.392	1.36	0.288	0.89	1.00	0.323	No
504	34.13	2.00	0.13	1.88	0.90	0.392	1.36	0.288	0.89	1.00	0.323	No
505	34.23	2.01	0.13	1.88	0.90	0.393	1.36	0.289	0.89	1.00	0.324	No
506	34.32	2.02	0.13	1.88	0.90	0.393	1.36	0.289	0.89	1.00	0.324	No
507	34.37	2.02	0.14	1.88	0.89	0.393	1.36	0.289	0.89	1.00	0.324	No
508	34.47	2.03	0.14	1.89	0.89	0.393	1.36	0.289	0.89	1.00	0.325	No
509	34.55	2.03	0.14	1.89	0.89	0.393	1.36	0.289	0.89	1.00	2.000	Yes
510	34.63	2.04	0.14	1.89	0.89	0.394	1.36	0.289	0.89	1.00	2.000	Yes
511	34.73	2.04	0.15	1.90	0.89	0.394	1.36	0.290	0.89	1.00	2.000	Yes
512	34.80	2.05	0.15	1.90	0.89	0.394	1.36	0.290	0.89	1.00	2.000	Yes
513	34.90	2.05	0.15	1.90	0.89	0.394	1.36	0.290	0.89	1.00	2.000	Yes
514	35.00	2.06	0.16	1.90	0.89	0.395	1.36	0.290	0.89	1.00	0.326	No
515	35.12	2.07	0.16	1.91	0.89	0.395	1.36	0.290	0.89	1.00	0.327	No
516	35.20	2.07	0.16	1.91	0.89	0.395	1.36	0.290	0.89	1.00	0.327	No
517	35.33	2.08	0.17	1.91	0.89	0.395	1.36	0.291	0.89	1.00	2.000	Yes
518	35.41	2.08	0.17	1.92	0.89	0.396	1.36	0.291	0.89	1.00	2.000	Yes
519	35.44	2.09	0.17	1.92	0.89	0.396	1.36	0.291	0.89	1.00	2.000	Yes
520	35.48	2.09	0.17	1.92	0.89	0.396	1.36	0.291	0.89	1.00	2.000	Yes
521	35.57	2.10	0.17	1.92	0.89	0.396	1.36	0.291	0.89	1.00	2.000	Yes
522	35.62	2.10	0.18	1.92	0.89	0.396	1.36	0.291	0.89	1.00	2.000	Yes
523	35.67	2.10	0.18	1.92	0.89	0.396	1.36	0.291	0.89	1.00	2.000	Yes
524	35.71	2.10	0.18	1.93	0.89	0.396	1.36	0.291	0.89	1.00	2.000	Yes
525	35.82	2.11	0.18	1.93	0.88	0.396	1.36	0.291	0.89	1.00	2.000	Yes
526	35.86	2.11	0.18	1.93	0.88	0.397	1.36	0.292	0.89	1.00	2.000	Yes
527	35.93	2.12	0.19	1.93	0.88	0.397	1.36	0.292	0.89	1.00	2.000	Yes
528	36.01	2.12	0.19	1.94	0.88	0.397	1.36	0.292	0.89	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	36.06	2.13	0.19	1.94	0.88	0.397	1.36	0.292	0.89	1.00	2.000	Yes
530	36.12	2.13	0.19	1.94	0.88	0.397	1.36	0.292	0.89	1.00	0.329	No
531	36.18	2.13	0.19	1.94	0.88	0.397	1.36	0.292	0.89	1.00	0.330	No
532	36.25	2.14	0.19	1.94	0.88	0.397	1.36	0.292	0.89	1.00	0.330	No
533	36.30	2.14	0.20	1.95	0.88	0.397	1.36	0.292	0.89	1.00	0.330	No
534	36.39	2.15	0.20	1.95	0.88	0.397	1.36	0.292	0.89	1.00	0.330	No
535	36.44	2.15	0.20	1.95	0.88	0.398	1.36	0.292	0.88	1.00	0.330	No
536	36.53	2.16	0.20	1.95	0.88	0.398	1.36	0.292	0.88	1.00	0.331	No
537	36.59	2.16	0.21	1.96	0.88	0.398	1.36	0.292	0.88	1.00	0.331	No
538	36.68	2.17	0.21	1.96	0.88	0.398	1.36	0.293	0.88	1.00	0.331	No
539	36.75	2.17	0.21	1.96	0.88	0.398	1.36	0.293	0.88	1.00	0.331	No
540	36.83	2.18	0.21	1.96	0.88	0.398	1.36	0.293	0.88	1.00	0.331	No
541	36.90	2.18	0.22	1.97	0.88	0.398	1.36	0.293	0.88	1.00	0.331	No
542	36.97	2.19	0.22	1.97	0.88	0.398	1.36	0.293	0.88	1.00	0.332	No
543	37.02	2.19	0.22	1.97	0.88	0.398	1.36	0.293	0.88	1.00	0.332	No
544	37.04	2.19	0.22	1.97	0.88	0.399	1.36	0.293	0.88	1.00	0.332	No
545	37.08	2.19	0.22	1.97	0.88	0.399	1.36	0.293	0.88	1.00	0.332	No
546	37.17	2.20	0.22	1.98	0.87	0.399	1.36	0.293	0.88	1.00	0.332	No
547	37.27	2.21	0.23	1.98	0.87	0.399	1.36	0.293	0.88	1.00	0.332	No
548	37.37	2.21	0.23	1.98	0.87	0.399	1.36	0.293	0.88	1.00	0.333	No
549	37.42	2.22	0.23	1.98	0.87	0.399	1.36	0.293	0.88	1.00	0.333	No
550	37.51	2.22	0.23	1.99	0.87	0.399	1.36	0.293	0.88	1.00	0.333	No
551	37.58	2.23	0.24	1.99	0.87	0.399	1.36	0.294	0.88	1.00	0.333	No
552	37.66	2.23	0.24	1.99	0.87	0.399	1.36	0.294	0.88	1.00	0.333	No
553	37.76	2.24	0.24	1.99	0.87	0.399	1.36	0.294	0.88	1.00	0.333	No
554	37.85	2.24	0.24	2.00	0.87	0.400	1.36	0.294	0.88	1.00	0.334	No
555	37.93	2.25	0.25	2.00	0.87	0.400	1.36	0.294	0.88	1.00	0.334	No
556	38.04	2.26	0.25	2.00	0.87	0.400	1.36	0.294	0.88	1.00	0.334	No
557	38.13	2.26	0.25	2.01	0.87	0.400	1.36	0.294	0.88	1.00	0.334	No
558	38.18	2.26	0.26	2.01	0.87	0.400	1.36	0.294	0.88	1.00	0.334	No
559	38.28	2.27	0.26	2.01	0.87	0.400	1.36	0.294	0.88	1.00	0.334	No
560	38.37	2.28	0.26	2.01	0.86	0.400	1.36	0.294	0.88	1.00	0.335	No
561	38.47	2.28	0.26	2.02	0.86	0.400	1.36	0.294	0.88	1.00	0.335	No
562	38.57	2.29	0.27	2.02	0.86	0.400	1.36	0.294	0.88	1.00	0.335	No
563	38.62	2.29	0.27	2.02	0.86	0.400	1.36	0.294	0.88	1.00	0.335	No
564	38.72	2.30	0.27	2.03	0.86	0.400	1.36	0.294	0.88	1.00	0.335	No
565	38.78	2.30	0.27	2.03	0.86	0.400	1.36	0.294	0.88	1.00	0.335	No
566	38.81	2.30	0.27	2.03	0.86	0.400	1.36	0.294	0.88	1.00	0.335	No
567	38.86	2.31	0.28	2.03	0.86	0.401	1.36	0.294	0.88	1.00	0.335	No
568	38.91	2.31	0.28	2.03	0.86	0.401	1.36	0.294	0.88	1.00	0.336	No
569	38.95	2.31	0.28	2.03	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
570	39.05	2.32	0.28	2.04	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
571	39.09	2.32	0.28	2.04	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
572	39.14	2.33	0.29	2.04	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
573	39.24	2.33	0.29	2.04	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
574	39.29	2.33	0.29	2.05	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
575	39.39	2.34	0.29	2.05	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
576	39.43	2.34	0.29	2.05	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	39.53	2.35	0.30	2.05	0.86	0.401	1.36	0.295	0.88	1.00	0.337	No
578	39.57	2.35	0.30	2.05	0.85	0.401	1.36	0.295	0.88	1.00	0.337	No
579	39.68	2.36	0.30	2.06	0.85	0.401	1.36	0.295	0.88	1.00	0.337	No
580	39.73	2.36	0.30	2.06	0.85	0.401	1.36	0.295	0.88	1.00	0.337	No
581	39.81	2.37	0.31	2.06	0.85	0.401	1.36	0.295	0.88	1.00	0.337	No
582	39.89	2.37	0.31	2.07	0.85	0.401	1.36	0.295	0.87	1.00	0.337	No
583	39.96	2.38	0.31	2.07	0.85	0.401	1.36	0.295	0.87	1.00	0.337	No
584	40.06	2.38	0.31	2.07	0.85	0.401	1.36	0.295	0.87	1.00	0.337	No
585	40.15	2.39	0.32	2.07	0.85	0.401	1.36	0.295	0.87	1.00	0.337	No
586	40.20	2.39	0.32	2.07	0.85	0.401	1.36	0.295	0.87	1.00	0.337	No
587	40.24	2.40	0.32	2.08	0.85	0.401	1.36	0.295	0.87	1.00	0.337	No
588	40.26	2.40	0.32	2.08	0.85	0.401	1.36	0.295	0.87	1.00	0.337	No
589	40.27	2.40	0.32	2.08	0.85	0.401	1.36	0.295	0.87	1.00	0.338	No
590	40.37	2.40	0.32	2.08	0.85	0.401	1.36	0.295	0.87	1.00	0.338	No
591	40.42	2.41	0.32	2.08	0.85	0.401	1.36	0.295	0.87	1.00	0.338	No
592	40.52	2.41	0.33	2.09	0.85	0.401	1.36	0.295	0.87	1.00	0.338	No
593	40.56	2.42	0.33	2.09	0.85	0.401	1.36	0.295	0.87	1.00	0.338	No
594	40.66	2.42	0.33	2.09	0.85	0.401	1.36	0.295	0.87	1.00	0.338	No
595	40.70	2.43	0.33	2.09	0.84	0.401	1.36	0.295	0.87	1.00	0.338	No
596	40.75	2.43	0.34	2.09	0.84	0.401	1.36	0.295	0.87	1.00	0.338	No
597	40.85	2.43	0.34	2.10	0.84	0.401	1.36	0.295	0.87	1.00	0.338	No
598	40.91	2.44	0.34	2.10	0.84	0.401	1.36	0.295	0.87	1.00	0.338	No
599	40.96	2.44	0.34	2.10	0.84	0.401	1.36	0.295	0.87	1.00	0.338	No
600	41.04	2.45	0.34	2.10	0.84	0.401	1.36	0.295	0.87	1.00	0.338	No
601	41.09	2.45	0.35	2.10	0.84	0.401	1.36	0.295	0.87	1.00	0.338	No
602	41.18	2.46	0.35	2.11	0.84	0.401	1.36	0.295	0.87	1.00	0.338	No
603	41.23	2.46	0.35	2.11	0.84	0.401	1.36	0.295	0.87	1.00	0.339	No
604	41.29	2.46	0.35	2.11	0.84	0.401	1.36	0.295	0.87	1.00	0.339	No
605	41.38	2.47	0.36	2.11	0.84	0.401	1.36	0.295	0.87	1.00	0.339	No
606	41.42	2.47	0.36	2.12	0.84	0.401	1.36	0.295	0.87	1.00	0.339	No
607	41.52	2.48	0.36	2.12	0.84	0.401	1.36	0.295	0.87	1.00	0.339	No
608	41.57	2.48	0.36	2.12	0.84	0.401	1.36	0.295	0.87	1.00	0.339	No
609	41.62	2.49	0.36	2.12	0.84	0.401	1.36	0.295	0.87	1.00	0.339	No
610	41.71	2.49	0.37	2.13	0.84	0.401	1.36	0.295	0.87	1.00	0.339	No
611	41.76	2.49	0.37	2.13	0.84	0.401	1.36	0.295	0.87	1.00	0.339	No
612	41.84	2.50	0.37	2.13	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
613	41.91	2.50	0.37	2.13	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
614	41.95	2.51	0.37	2.13	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
615	42.01	2.51	0.37	2.14	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
616	42.10	2.52	0.38	2.14	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
617	42.15	2.52	0.38	2.14	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
618	42.24	2.53	0.38	2.14	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
619	42.28	2.53	0.38	2.15	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
620	42.39	2.54	0.39	2.15	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
621	42.43	2.54	0.39	2.15	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
622	42.50	2.54	0.39	2.15	0.83	0.401	1.36	0.294	0.87	1.00	0.339	No
623	42.58	2.55	0.39	2.16	0.83	0.400	1.36	0.294	0.87	1.00	0.339	No
624	42.65	2.55	0.39	2.16	0.83	0.400	1.36	0.294	0.87	1.00	0.340	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	42.70	2.56	0.40	2.16	0.83	0.400	1.36	0.294	0.87	1.00	0.340	No
626	42.73	2.56	0.40	2.16	0.83	0.400	1.36	0.294	0.87	1.00	0.340	No
627	42.77	2.56	0.40	2.16	0.83	0.400	1.36	0.294	0.87	1.00	0.340	No
628	42.82	2.56	0.40	2.16	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
629	42.87	2.57	0.40	2.17	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
630	42.91	2.57	0.40	2.17	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
631	42.97	2.57	0.40	2.17	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
632	43.02	2.58	0.41	2.17	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
633	43.06	2.58	0.41	2.17	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
634	43.11	2.58	0.41	2.17	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
635	43.17	2.59	0.41	2.18	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
636	43.21	2.59	0.41	2.18	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
637	43.29	2.59	0.41	2.18	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
638	43.34	2.60	0.42	2.18	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
639	43.39	2.60	0.42	2.18	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
640	43.45	2.61	0.42	2.19	0.82	0.400	1.36	0.294	0.86	1.00	0.340	No
641	43.51	2.61	0.42	2.19	0.82	0.400	1.36	0.294	0.86	1.00	0.340	No
642	43.59	2.61	0.42	2.19	0.82	0.400	1.36	0.294	0.86	1.00	0.340	No
643	43.64	2.62	0.43	2.19	0.82	0.400	1.36	0.294	0.86	1.00	0.340	No
644	43.70	2.62	0.43	2.19	0.82	0.399	1.36	0.294	0.86	1.00	0.340	No
645	43.78	2.63	0.43	2.20	0.82	0.399	1.36	0.294	0.86	1.00	0.340	No
646	43.88	2.63	0.43	2.20	0.81	0.399	1.36	0.294	0.86	1.00	0.340	No
647	43.94	2.64	0.43	2.20	0.81	0.399	1.36	0.294	0.86	1.00	0.340	No
648	44.04	2.64	0.44	2.21	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
649	44.07	2.65	0.44	2.21	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
650	44.12	2.65	0.44	2.21	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
651	44.16	2.65	0.44	2.21	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
652	44.21	2.65	0.44	2.21	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
653	44.26	2.66	0.44	2.21	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
654	44.31	2.66	0.45	2.22	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
655	44.35	2.66	0.45	2.22	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
656	44.40	2.67	0.45	2.22	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
657	44.45	2.67	0.45	2.22	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
658	44.50	2.67	0.45	2.22	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
659	44.54	2.68	0.45	2.22	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
660	44.60	2.68	0.46	2.22	0.81	0.398	1.36	0.293	0.86	1.00	0.340	No
661	44.64	2.68	0.46	2.23	0.81	0.398	1.36	0.293	0.86	1.00	0.340	No
662	44.69	2.69	0.46	2.23	0.81	0.398	1.36	0.293	0.86	1.00	0.340	No
663	44.74	2.69	0.46	2.23	0.81	0.398	1.36	0.293	0.86	1.00	0.340	No
664	44.79	2.69	0.46	2.23	0.81	0.398	1.36	0.293	0.86	1.00	0.340	No
665	44.83	2.70	0.46	2.23	0.81	0.398	1.36	0.293	0.86	1.00	0.340	No
666	44.88	2.70	0.46	2.23	0.80	0.398	1.36	0.293	0.86	1.00	0.340	No
667	44.93	2.70	0.47	2.24	0.80	0.398	1.36	0.293	0.86	1.00	0.340	No
668	44.98	2.71	0.47	2.24	0.80	0.398	1.36	0.293	0.86	1.00	0.340	No
669	45.03	2.71	0.47	2.24	0.80	0.398	1.36	0.293	0.86	1.00	0.340	No
670	45.08	2.71	0.47	2.24	0.80	0.398	1.36	0.292	0.86	1.00	0.340	No
671	45.16	2.72	0.47	2.24	0.80	0.398	1.36	0.292	0.86	1.00	0.340	No
672	45.19	2.72	0.47	2.25	0.80	0.398	1.36	0.292	0.86	1.00	0.340	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	45.27	2.72	0.48	2.25	0.80	0.397	1.36	0.292	0.86	1.00	0.340	No
674	45.32	2.73	0.48	2.25	0.80	0.397	1.36	0.292	0.86	1.00	0.340	No
675	45.37	2.73	0.48	2.25	0.80	0.397	1.36	0.292	0.86	1.00	0.340	No
676	45.45	2.74	0.48	2.25	0.80	0.397	1.36	0.292	0.86	1.00	0.340	No
677	45.51	2.74	0.48	2.26	0.80	0.397	1.36	0.292	0.86	1.00	0.340	No
678	45.56	2.74	0.49	2.26	0.80	0.397	1.36	0.292	0.86	1.00	2.000	Yes
679	45.61	2.75	0.49	2.26	0.80	0.397	1.36	0.292	0.86	1.00	2.000	Yes
680	45.69	2.75	0.49	2.26	0.80	0.397	1.36	0.292	0.86	1.00	2.000	Yes
681	45.75	2.76	0.49	2.26	0.80	0.397	1.36	0.292	0.86	1.00	2.000	Yes
682	45.81	2.76	0.49	2.27	0.80	0.397	1.36	0.292	0.86	1.00	2.000	Yes
683	45.89	2.76	0.50	2.27	0.79	0.397	1.36	0.292	0.86	1.00	2.000	Yes
684	45.94	2.77	0.50	2.27	0.79	0.396	1.36	0.291	0.86	1.00	2.000	Yes
685	46.04	2.77	0.50	2.27	0.79	0.396	1.36	0.291	0.86	1.00	2.000	Yes
686	46.08	2.78	0.50	2.27	0.79	0.396	1.36	0.291	0.86	1.00	2.000	Yes
687	46.15	2.78	0.50	2.28	0.79	0.396	1.36	0.291	0.86	1.00	2.000	Yes
688	46.17	2.78	0.50	2.28	0.79	0.396	1.36	0.291	0.86	1.00	0.339	No
689	46.18	2.78	0.50	2.28	0.79	0.396	1.36	0.291	0.86	1.00	0.339	No
690	46.23	2.79	0.51	2.28	0.79	0.396	1.36	0.291	0.86	1.00	0.339	No
691	46.27	2.79	0.51	2.28	0.79	0.396	1.36	0.291	0.86	1.00	0.339	No
692	46.32	2.79	0.51	2.28	0.79	0.396	1.36	0.291	0.86	1.00	0.339	No
693	46.41	2.80	0.51	2.28	0.79	0.396	1.36	0.291	0.86	1.00	0.339	No
694	46.47	2.80	0.51	2.29	0.79	0.396	1.36	0.291	0.86	1.00	0.339	No
695	46.52	2.80	0.52	2.29	0.79	0.396	1.36	0.291	0.86	1.00	0.339	No
696	46.56	2.81	0.52	2.29	0.79	0.395	1.36	0.291	0.86	1.00	0.339	No
697	46.65	2.81	0.52	2.29	0.79	0.395	1.36	0.291	0.86	1.00	0.339	No
698	46.71	2.81	0.52	2.29	0.79	0.395	1.36	0.291	0.86	1.00	0.339	No
699	46.76	2.82	0.52	2.29	0.79	0.395	1.36	0.291	0.86	1.00	0.339	No
700	46.85	2.82	0.53	2.30	0.78	0.395	1.36	0.290	0.86	1.00	0.339	No
701	46.90	2.83	0.53	2.30	0.78	0.395	1.36	0.290	0.86	1.00	0.339	No
702	46.99	2.83	0.53	2.30	0.78	0.395	1.36	0.290	0.86	1.00	0.339	No
703	47.04	2.84	0.53	2.30	0.78	0.395	1.36	0.290	0.86	1.00	0.339	No
704	47.10	2.84	0.53	2.31	0.78	0.395	1.36	0.290	0.86	1.00	0.339	No
705	47.16	2.84	0.54	2.31	0.78	0.394	1.36	0.290	0.86	1.00	0.339	No
706	47.23	2.85	0.54	2.31	0.78	0.394	1.36	0.290	0.86	1.00	0.339	No
707	47.30	2.85	0.54	2.31	0.78	0.394	1.36	0.290	0.86	1.00	0.339	No
708	47.38	2.86	0.54	2.31	0.78	0.394	1.36	0.290	0.86	1.00	0.339	No
709	47.43	2.86	0.54	2.32	0.78	0.394	1.36	0.290	0.86	1.00	0.339	No
710	47.52	2.86	0.55	2.32	0.78	0.394	1.36	0.289	0.85	1.00	0.339	No
711	47.59	2.87	0.55	2.32	0.78	0.394	1.36	0.289	0.85	1.00	0.339	No
712	47.66	2.87	0.55	2.32	0.78	0.394	1.36	0.289	0.85	1.00	0.339	No
713	47.77	2.88	0.55	2.32	0.78	0.393	1.36	0.289	0.85	1.00	0.338	No
714	47.82	2.88	0.56	2.33	0.77	0.393	1.36	0.289	0.85	1.00	0.338	No
715	47.91	2.89	0.56	2.33	0.77	0.393	1.36	0.289	0.85	1.00	0.338	No
716	47.93	2.89	0.56	2.33	0.77	0.393	1.36	0.289	0.85	1.00	0.338	No
717	47.97	2.89	0.56	2.33	0.77	0.393	1.36	0.289	0.85	1.00	0.338	No
718	48.02	2.89	0.56	2.33	0.77	0.393	1.36	0.289	0.85	1.00	0.338	No
719	48.07	2.90	0.56	2.33	0.77	0.393	1.36	0.289	0.85	1.00	0.338	No
720	48.12	2.90	0.57	2.33	0.77	0.393	1.36	0.289	0.85	1.00	0.338	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	48.19	2.90	0.57	2.34	0.77	0.393	1.36	0.289	0.85	1.00	0.338	No
722	48.23	2.91	0.57	2.34	0.77	0.392	1.36	0.289	0.85	1.00	0.338	No
723	48.31	2.91	0.57	2.34	0.77	0.392	1.36	0.288	0.85	1.00	0.338	No
724	48.35	2.91	0.57	2.34	0.77	0.392	1.36	0.288	0.85	1.00	0.338	No
725	48.40	2.92	0.57	2.34	0.77	0.392	1.36	0.288	0.85	1.00	0.338	No
726	48.45	2.92	0.58	2.34	0.77	0.392	1.36	0.288	0.85	1.00	0.338	No
727	48.50	2.92	0.58	2.34	0.77	0.392	1.36	0.288	0.85	1.00	0.338	No
728	48.55	2.92	0.58	2.35	0.77	0.392	1.36	0.288	0.85	1.00	0.338	No
729	48.59	2.93	0.58	2.35	0.77	0.392	1.36	0.288	0.85	1.00	0.338	No
730	48.67	2.93	0.58	2.35	0.77	0.392	1.36	0.288	0.85	1.00	0.338	No
731	48.73	2.93	0.58	2.35	0.77	0.392	1.36	0.288	0.85	1.00	0.338	No
732	48.78	2.94	0.59	2.35	0.77	0.391	1.36	0.288	0.85	1.00	0.338	No
733	48.83	2.94	0.59	2.35	0.76	0.391	1.36	0.288	0.85	1.00	0.338	No
734	48.91	2.94	0.59	2.35	0.76	0.391	1.36	0.288	0.85	1.00	0.337	No
735	48.98	2.95	0.59	2.36	0.76	0.391	1.36	0.287	0.85	1.00	0.337	No
736	49.03	2.95	0.59	2.36	0.76	0.391	1.36	0.287	0.85	1.00	0.337	No
737	49.12	2.96	0.60	2.36	0.76	0.391	1.36	0.287	0.85	1.00	0.337	No
738	49.17	2.96	0.60	2.36	0.76	0.391	1.36	0.287	0.85	1.00	0.337	No
739	49.27	2.97	0.60	2.36	0.76	0.390	1.36	0.287	0.85	1.00	0.337	No
740	49.31	2.97	0.60	2.37	0.76	0.390	1.36	0.287	0.85	1.00	0.337	No
741	49.38	2.97	0.60	2.37	0.76	0.390	1.36	0.287	0.85	1.00	0.337	No
742	49.45	2.98	0.61	2.37	0.76	0.390	1.36	0.287	0.85	1.00	0.337	No
743	49.51	2.98	0.61	2.37	0.76	0.390	1.36	0.287	0.85	1.00	0.337	No
744	49.54	2.98	0.61	2.37	0.76	0.390	1.36	0.287	0.85	1.00	0.337	No
745	49.59	2.98	0.61	2.37	0.76	0.390	1.36	0.287	0.85	1.00	0.337	No
746	49.64	2.99	0.61	2.37	0.76	0.390	1.36	0.287	0.85	1.00	0.337	No
747	49.73	2.99	0.62	2.38	0.76	0.389	1.36	0.286	0.85	1.00	0.337	No
748	49.83	3.00	0.62	2.38	0.75	0.389	1.36	0.286	0.85	1.00	0.337	No
749	49.92	3.00	0.62	2.38	0.75	0.389	1.36	0.286	0.85	1.00	0.336	No
750	49.98	3.01	0.62	2.38	0.75	0.389	1.36	0.286	0.85	1.00	0.336	No
751	50.07	3.01	0.63	2.39	0.75	0.389	1.36	0.286	0.85	1.00	0.336	No
752	50.16	3.02	0.63	2.39	0.75	0.389	1.36	0.286	0.85	1.00	0.336	No
753	50.24	3.02	0.63	2.39	0.75	0.388	1.36	0.286	0.85	1.00	0.336	No
754	50.32	3.03	0.63	2.39	0.75	0.388	1.36	0.285	0.85	1.00	0.336	No
755	50.41	3.03	0.64	2.39	0.75	0.388	1.36	0.285	0.85	1.00	0.336	No
756	50.50	3.04	0.64	2.40	0.75	0.388	1.36	0.285	0.85	1.00	0.336	No
757	50.56	3.04	0.64	2.40	0.75	0.388	1.36	0.285	0.85	1.00	0.336	No
758	50.66	3.04	0.64	2.40	0.75	0.388	1.36	0.285	0.85	1.00	0.336	No
759	50.74	3.05	0.65	2.40	0.75	0.387	1.36	0.285	0.85	1.00	0.336	No
760	50.84	3.05	0.65	2.40	0.74	0.387	1.36	0.285	0.85	1.00	0.335	No
761	50.93	3.06	0.65	2.41	0.74	0.387	1.36	0.284	0.85	1.00	0.335	No
762	50.98	3.06	0.65	2.41	0.74	0.387	1.36	0.284	0.85	1.00	0.335	No
763	51.08	3.07	0.66	2.41	0.74	0.387	1.36	0.284	0.85	1.00	0.335	No
764	51.17	3.07	0.66	2.41	0.74	0.386	1.36	0.284	0.85	1.00	0.335	No
765	51.24	3.08	0.66	2.42	0.74	0.386	1.36	0.284	0.85	1.00	0.335	No
766	51.34	3.09	0.67	2.42	0.74	0.386	1.36	0.284	0.85	1.00	0.335	No
767	51.41	3.09	0.67	2.42	0.74	0.386	1.36	0.284	0.85	1.00	0.335	No
768	51.51	3.10	0.67	2.42	0.74	0.386	1.36	0.283	0.85	1.00	0.335	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	51.58	3.10	0.67	2.43	0.74	0.385	1.36	0.283	0.85	1.00	0.335	No
770	51.68	3.11	0.68	2.43	0.74	0.385	1.36	0.283	0.85	1.00	0.334	No
771	51.79	3.11	0.68	2.43	0.73	0.385	1.36	0.283	0.85	1.00	0.334	No
772	51.82	3.11	0.68	2.43	0.73	0.385	1.36	0.283	0.85	1.00	0.334	No
773	51.85	3.12	0.68	2.43	0.73	0.385	1.36	0.283	0.85	1.00	0.334	No
774	51.91	3.12	0.68	2.44	0.73	0.385	1.36	0.283	0.85	1.00	0.334	No
775	52.00	3.13	0.69	2.44	0.73	0.384	1.36	0.283	0.85	1.00	0.334	No
776	52.05	3.13	0.69	2.44	0.73	0.384	1.36	0.283	0.85	1.00	0.334	No
777	52.10	3.13	0.69	2.44	0.73	0.384	1.36	0.282	0.85	1.00	0.334	No
778	52.19	3.14	0.69	2.44	0.73	0.384	1.36	0.282	0.85	1.00	0.334	No
779	52.28	3.14	0.70	2.45	0.73	0.384	1.36	0.282	0.85	1.00	0.334	No
780	52.34	3.15	0.70	2.45	0.73	0.384	1.36	0.282	0.85	1.00	0.334	No
781	52.42	3.15	0.70	2.45	0.73	0.383	1.36	0.282	0.85	1.00	0.333	No
782	52.48	3.15	0.70	2.45	0.73	0.383	1.36	0.282	0.85	1.00	0.333	No
783	52.57	3.16	0.70	2.46	0.73	0.383	1.36	0.282	0.84	1.00	0.333	No
784	52.62	3.16	0.71	2.46	0.73	0.383	1.36	0.281	0.84	1.00	0.333	No
785	52.69	3.17	0.71	2.46	0.73	0.383	1.36	0.281	0.84	1.00	0.333	No
786	52.77	3.17	0.71	2.46	0.72	0.382	1.36	0.281	0.84	1.00	0.333	No
787	52.87	3.18	0.71	2.46	0.72	0.382	1.36	0.281	0.84	1.00	0.333	No
788	52.91	3.18	0.71	2.47	0.72	0.382	1.36	0.281	0.84	1.00	0.333	No
789	53.01	3.19	0.72	2.47	0.72	0.382	1.36	0.281	0.84	1.00	0.333	No
790	53.10	3.19	0.72	2.47	0.72	0.382	1.36	0.281	0.84	1.00	0.333	No
791	53.16	3.20	0.72	2.47	0.72	0.382	1.36	0.281	0.84	1.00	0.332	No
792	53.25	3.20	0.73	2.48	0.72	0.381	1.36	0.280	0.84	1.00	0.332	No
793	53.29	3.20	0.73	2.48	0.72	0.381	1.36	0.280	0.84	1.00	0.332	No
794	53.38	3.21	0.73	2.48	0.72	0.381	1.36	0.280	0.84	1.00	0.332	No
795	53.42	3.21	0.73	2.48	0.72	0.381	1.36	0.280	0.84	1.00	0.332	No
796	53.47	3.22	0.73	2.48	0.72	0.381	1.36	0.280	0.84	1.00	0.332	No
797	53.52	3.22	0.73	2.49	0.72	0.381	1.36	0.280	0.84	1.00	0.332	No
798	53.58	3.22	0.74	2.49	0.72	0.380	1.36	0.280	0.84	1.00	0.332	No
799	53.66	3.23	0.74	2.49	0.72	0.380	1.36	0.280	0.84	1.00	0.332	No
800	53.75	3.23	0.74	2.49	0.72	0.380	1.36	0.279	0.84	1.00	0.332	No
801	53.81	3.24	0.74	2.50	0.71	0.380	1.36	0.279	0.84	1.00	0.332	No
802	53.87	3.24	0.74	2.50	0.71	0.380	1.36	0.279	0.84	1.00	0.331	No
803	53.95	3.25	0.75	2.50	0.71	0.379	1.36	0.279	0.84	1.00	0.331	No
804	54.01	3.25	0.75	2.50	0.71	0.379	1.36	0.279	0.84	1.00	0.331	No
805	54.06	3.26	0.75	2.50	0.71	0.379	1.36	0.279	0.84	1.00	0.331	No
806	54.15	3.26	0.75	2.51	0.71	0.379	1.36	0.279	0.84	1.00	0.331	No
807	54.20	3.26	0.76	2.51	0.71	0.379	1.36	0.278	0.84	1.00	0.331	No
808	54.29	3.27	0.76	2.51	0.71	0.379	1.36	0.278	0.84	1.00	0.331	No
809	54.34	3.27	0.76	2.51	0.71	0.378	1.36	0.278	0.84	1.00	2.000	Yes
810	54.43	3.28	0.76	2.52	0.71	0.378	1.36	0.278	0.84	1.00	2.000	Yes
811	54.45	3.28	0.76	2.52	0.71	0.378	1.36	0.278	0.84	1.00	2.000	Yes
812	54.48	3.28	0.76	2.52	0.71	0.378	1.36	0.278	0.84	1.00	2.000	Yes
813	54.52	3.28	0.76	2.52	0.71	0.378	1.36	0.278	0.84	1.00	2.000	Yes
814	54.53	3.29	0.77	2.52	0.71	0.378	1.36	0.278	0.84	1.00	2.000	Yes
815	54.58	3.29	0.77	2.52	0.71	0.378	1.36	0.278	0.84	1.00	0.330	No
816	54.62	3.29	0.77	2.52	0.71	0.378	1.36	0.278	0.84	1.00	0.330	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	54.65	3.29	0.77	2.52	0.71	0.378	1.36	0.278	0.84	1.00	0.330	No
818	54.70	3.30	0.77	2.53	0.71	0.377	1.36	0.277	0.84	1.00	0.330	No
819	54.76	3.30	0.77	2.53	0.71	0.377	1.36	0.277	0.84	1.00	0.330	No
820	54.77	3.30	0.77	2.53	0.71	0.377	1.36	0.277	0.84	1.00	0.330	No
821	54.82	3.30	0.77	2.53	0.71	0.377	1.36	0.277	0.84	1.00	0.330	No
822	54.87	3.31	0.78	2.53	0.70	0.377	1.36	0.277	0.84	1.00	0.330	No
823	54.88	3.31	0.78	2.53	0.70	0.377	1.36	0.277	0.84	1.00	0.330	No
824	54.91	3.31	0.78	2.53	0.70	0.377	1.36	0.277	0.84	1.00	0.330	No
825	54.96	3.31	0.78	2.53	0.70	0.377	1.36	0.277	0.84	1.00	0.330	No
826	54.97	3.31	0.78	2.53	0.70	0.377	1.36	0.277	0.84	1.00	0.330	No
827	55.03	3.32	0.78	2.54	0.70	0.377	1.36	0.277	0.84	1.00	0.330	No
828	55.09	3.32	0.78	2.54	0.70	0.376	1.36	0.277	0.84	1.00	0.330	No
829	55.15	3.33	0.78	2.54	0.70	0.376	1.36	0.277	0.84	1.00	0.330	No
830	55.20	3.33	0.79	2.54	0.70	0.376	1.36	0.276	0.84	1.00	0.329	No
831	55.25	3.33	0.79	2.54	0.70	0.376	1.36	0.276	0.84	1.00	0.329	No
832	55.30	3.34	0.79	2.55	0.70	0.376	1.36	0.276	0.84	1.00	0.329	No
833	55.34	3.34	0.79	2.55	0.70	0.376	1.36	0.276	0.84	1.00	0.329	No
834	55.39	3.34	0.79	2.55	0.70	0.376	1.36	0.276	0.84	1.00	0.329	No
835	55.40	3.34	0.79	2.55	0.70	0.376	1.36	0.276	0.84	1.00	0.329	No
836	55.44	3.34	0.79	2.55	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No
837	55.44	3.35	0.79	2.55	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No
838	55.49	3.35	0.80	2.55	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No
839	55.54	3.35	0.80	2.56	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No
840	55.59	3.36	0.80	2.56	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No
841	55.63	3.36	0.80	2.56	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No
842	55.64	3.36	0.80	2.56	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No
843	55.68	3.36	0.80	2.56	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No
844	55.69	3.36	0.80	2.56	0.70	0.375	1.36	0.275	0.84	1.00	0.329	No
845	55.69	3.36	0.80	2.56	0.70	0.375	1.36	0.275	0.84	1.00	0.329	No
846	55.71	3.36	0.80	2.56	0.70	0.375	1.36	0.275	0.84	1.00	0.329	No
847	55.76	3.37	0.80	2.56	0.70	0.374	1.36	0.275	0.84	1.00	0.329	No
848	55.78	3.37	0.80	2.56	0.70	0.374	1.36	0.275	0.84	1.00	0.329	No
849	55.81	3.37	0.81	2.57	0.70	0.374	1.36	0.275	0.84	1.00	0.329	No
850	55.85	3.37	0.81	2.57	0.70	0.374	1.36	0.275	0.84	1.00	0.328	No
851	55.86	3.37	0.81	2.57	0.70	0.374	1.36	0.275	0.84	1.00	0.328	No
852	55.91	3.38	0.81	2.57	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
853	55.92	3.38	0.81	2.57	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
854	55.96	3.38	0.81	2.57	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
855	55.97	3.38	0.81	2.57	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
856	56.00	3.38	0.81	2.57	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
857	56.01	3.38	0.81	2.57	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
858	56.03	3.39	0.81	2.57	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
859	56.05	3.39	0.81	2.57	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
860	56.10	3.39	0.81	2.58	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
861	56.12	3.39	0.81	2.58	0.69	0.373	1.36	0.275	0.84	1.00	0.328	No
862	56.16	3.39	0.82	2.58	0.69	0.373	1.36	0.275	0.84	1.00	0.328	No
863	56.17	3.40	0.82	2.58	0.69	0.373	1.36	0.274	0.84	1.00	0.328	No
864	56.20	3.40	0.82	2.58	0.69	0.373	1.36	0.274	0.84	1.00	0.328	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	56.22	3.40	0.82	2.58	0.69	0.373	1.36	0.274	0.84	1.00	0.328	No
866	56.24	3.40	0.82	2.58	0.69	0.373	1.36	0.274	0.84	1.00	0.328	No
867	56.30	3.40	0.82	2.58	0.69	0.373	1.36	0.274	0.84	1.00	0.328	No
868	56.31	3.40	0.82	2.58	0.69	0.373	1.36	0.274	0.84	1.00	0.328	No
869	56.34	3.41	0.82	2.59	0.69	0.373	1.36	0.274	0.84	1.00	0.328	No
870	56.39	3.41	0.82	2.59	0.69	0.373	1.36	0.274	0.84	1.00	0.328	No
871	56.45	3.41	0.83	2.59	0.69	0.373	1.36	0.274	0.84	1.00	0.328	No
872	56.48	3.42	0.83	2.59	0.69	0.372	1.36	0.274	0.84	1.00	0.328	No
873	56.49	3.42	0.83	2.59	0.69	0.372	1.36	0.274	0.84	1.00	0.328	No
874	56.53	3.42	0.83	2.59	0.69	0.372	1.36	0.274	0.84	1.00	0.327	No
875	56.58	3.42	0.83	2.59	0.69	0.372	1.36	0.274	0.84	1.00	0.327	No
876	56.63	3.43	0.83	2.60	0.69	0.372	1.36	0.274	0.84	1.00	0.327	No
877	56.68	3.43	0.83	2.60	0.69	0.372	1.36	0.273	0.84	1.00	0.327	No
878	56.73	3.43	0.83	2.60	0.69	0.372	1.36	0.273	0.84	1.00	0.327	No
879	56.78	3.44	0.84	2.60	0.69	0.372	1.36	0.273	0.84	1.00	0.327	No
880	56.83	3.44	0.84	2.60	0.69	0.372	1.36	0.273	0.84	1.00	0.327	No
881	56.89	3.44	0.84	2.61	0.69	0.371	1.36	0.273	0.84	1.00	0.327	No
882	56.95	3.45	0.84	2.61	0.69	0.371	1.36	0.273	0.83	1.00	0.327	No
883	56.99	3.45	0.84	2.61	0.68	0.371	1.36	0.273	0.83	1.00	0.327	No
884	57.01	3.45	0.84	2.61	0.68	0.371	1.36	0.273	0.83	1.00	0.327	No
885	57.04	3.45	0.84	2.61	0.68	0.371	1.36	0.273	0.83	1.00	0.327	No
886	57.09	3.46	0.85	2.61	0.68	0.371	1.36	0.273	0.83	1.00	0.327	No
887	57.11	3.46	0.85	2.61	0.68	0.371	1.36	0.273	0.83	1.00	0.327	No
888	57.13	3.46	0.85	2.61	0.68	0.371	1.36	0.273	0.83	1.00	0.327	No
889	57.18	3.46	0.85	2.62	0.68	0.371	1.36	0.272	0.83	1.00	0.326	No
890	57.19	3.46	0.85	2.62	0.68	0.371	1.36	0.272	0.83	1.00	0.326	No
891	57.21	3.47	0.85	2.62	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
892	57.24	3.47	0.85	2.62	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
893	57.28	3.47	0.85	2.62	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
894	57.32	3.47	0.85	2.62	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
895	57.35	3.48	0.85	2.62	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
896	57.38	3.48	0.85	2.62	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
897	57.43	3.48	0.86	2.63	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
898	57.48	3.48	0.86	2.63	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
899	57.52	3.49	0.86	2.63	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
900	57.57	3.49	0.86	2.63	0.68	0.369	1.36	0.272	0.83	1.00	0.326	No
901	57.62	3.49	0.86	2.63	0.68	0.369	1.36	0.272	0.83	1.00	0.326	No
902	57.68	3.50	0.86	2.63	0.68	0.369	1.36	0.271	0.83	1.00	0.326	No
903	57.76	3.50	0.87	2.64	0.68	0.369	1.36	0.271	0.83	1.00	0.326	No
904	57.81	3.51	0.87	2.64	0.68	0.369	1.36	0.271	0.83	1.00	0.326	No
905	57.86	3.51	0.87	2.64	0.68	0.369	1.36	0.271	0.83	1.00	0.325	No
906	57.89	3.51	0.87	2.64	0.68	0.369	1.36	0.271	0.83	1.00	0.325	No
907	57.91	3.51	0.87	2.64	0.68	0.369	1.36	0.271	0.83	1.00	0.325	No
908	57.92	3.51	0.87	2.64	0.68	0.368	1.36	0.271	0.83	1.00	0.325	No
909	57.95	3.52	0.87	2.64	0.68	0.368	1.36	0.271	0.83	1.00	0.325	No
910	57.99	3.52	0.87	2.65	0.68	0.368	1.36	0.271	0.83	1.00	0.325	No
911	58.01	3.52	0.87	2.65	0.68	0.368	1.36	0.271	0.83	1.00	0.325	No
912	58.05	3.52	0.88	2.65	0.68	0.368	1.36	0.271	0.83	1.00	0.325	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	58.05	3.52	0.88	2.65	0.68	0.368	1.36	0.271	0.83	1.00	0.325	No
914	58.10	3.53	0.88	2.65	0.68	0.368	1.36	0.271	0.83	1.00	0.325	No
915	58.13	3.53	0.88	2.65	0.67	0.368	1.36	0.270	0.83	1.00	0.325	No
916	58.15	3.53	0.88	2.65	0.67	0.368	1.36	0.270	0.83	1.00	0.325	No
917	58.17	3.53	0.88	2.65	0.67	0.368	1.36	0.270	0.83	1.00	0.325	No
918	58.20	3.53	0.88	2.65	0.67	0.368	1.36	0.270	0.83	1.00	0.325	No
919	58.21	3.53	0.88	2.65	0.67	0.368	1.36	0.270	0.83	1.00	0.325	No
920	58.21	3.53	0.88	2.65	0.67	0.368	1.36	0.270	0.83	1.00	0.325	No
921	58.23	3.54	0.88	2.65	0.67	0.368	1.36	0.270	0.83	1.00	0.325	No
922	58.24	3.54	0.88	2.66	0.67	0.368	1.36	0.270	0.83	1.00	0.325	No
923	58.25	3.54	0.88	2.66	0.67	0.368	1.36	0.270	0.83	1.00	0.325	No
924	58.29	3.54	0.88	2.66	0.67	0.367	1.36	0.270	0.83	1.00	0.325	No
925	58.31	3.54	0.88	2.66	0.67	0.367	1.36	0.270	0.83	1.00	0.325	No
926	58.33	3.54	0.88	2.66	0.67	0.367	1.36	0.270	0.83	1.00	0.325	No
927	58.38	3.55	0.89	2.66	0.67	0.367	1.36	0.270	0.83	1.00	0.325	No
928	58.39	3.55	0.89	2.66	0.67	0.367	1.36	0.270	0.83	1.00	0.325	No
929	58.43	3.55	0.89	2.66	0.67	0.367	1.36	0.270	0.83	1.00	0.325	No
930	58.43	3.55	0.89	2.66	0.67	0.367	1.36	0.270	0.83	1.00	0.325	No
931	58.48	3.55	0.89	2.66	0.67	0.367	1.36	0.270	0.83	1.00	0.324	No
932	58.53	3.56	0.89	2.67	0.67	0.367	1.36	0.270	0.83	1.00	0.324	No
933	58.56	3.56	0.89	2.67	0.67	0.367	1.36	0.270	0.83	1.00	0.324	No
934	58.58	3.56	0.89	2.67	0.67	0.367	1.36	0.270	0.83	1.00	0.324	No
935	58.59	3.56	0.89	2.67	0.67	0.367	1.36	0.270	0.83	1.00	0.324	No
936	58.63	3.56	0.89	2.67	0.67	0.367	1.36	0.270	0.83	1.00	0.324	No
937	58.63	3.56	0.89	2.67	0.67	0.367	1.36	0.270	0.83	1.00	0.324	No
938	58.63	3.56	0.89	2.67	0.67	0.367	1.36	0.269	0.83	1.00	0.324	No
939	58.68	3.57	0.89	2.67	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
940	58.69	3.57	0.90	2.67	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
941	58.72	3.57	0.90	2.67	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
942	58.73	3.57	0.90	2.67	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
943	58.74	3.57	0.90	2.67	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
944	58.77	3.57	0.90	2.67	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
945	58.81	3.57	0.90	2.68	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
946	58.82	3.57	0.90	2.68	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
947	58.83	3.58	0.90	2.68	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
948	58.87	3.58	0.90	2.68	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
949	58.91	3.58	0.90	2.68	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
950	58.92	3.58	0.90	2.68	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
951	58.93	3.58	0.90	2.68	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
952	58.96	3.58	0.90	2.68	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
953	59.01	3.59	0.91	2.68	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
954	59.06	3.59	0.91	2.68	0.67	0.365	1.36	0.269	0.83	1.00	0.324	No
955	59.08	3.59	0.91	2.69	0.67	0.365	1.36	0.269	0.83	1.00	0.324	No
956	59.11	3.59	0.91	2.69	0.67	0.365	1.36	0.269	0.83	1.00	0.324	No
957	59.15	3.60	0.91	2.69	0.67	0.365	1.36	0.268	0.83	1.00	0.323	No
958	59.21	3.60	0.91	2.69	0.67	0.365	1.36	0.268	0.83	1.00	0.323	No
959	59.26	3.60	0.91	2.69	0.67	0.365	1.36	0.268	0.83	1.00	0.323	No
960	59.30	3.61	0.91	2.69	0.66	0.365	1.36	0.268	0.83	1.00	0.323	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
961	59.35	3.61	0.92	2.70	0.66	0.365	1.36	0.268	0.83	1.00	0.323	No
962	59.40	3.61	0.92	2.70	0.66	0.364	1.36	0.268	0.83	1.00	0.323	No
963	59.42	3.62	0.92	2.70	0.66	0.364	1.36	0.268	0.83	1.00	0.323	No
964	59.47	3.62	0.92	2.70	0.66	0.364	1.36	0.268	0.83	1.00	0.323	No
965	59.51	3.62	0.92	2.70	0.66	0.364	1.36	0.268	0.83	1.00	0.323	No
966	59.56	3.63	0.92	2.70	0.66	0.364	1.36	0.268	0.83	1.00	0.323	No
967	59.61	3.63	0.92	2.71	0.66	0.364	1.36	0.268	0.83	1.00	0.323	No
968	59.67	3.63	0.93	2.71	0.66	0.364	1.36	0.267	0.83	1.00	0.323	No
969	59.71	3.64	0.93	2.71	0.66	0.364	1.36	0.267	0.83	1.00	0.323	No
970	59.80	3.64	0.93	2.71	0.66	0.363	1.36	0.267	0.83	1.00	0.323	No
971	59.85	3.65	0.93	2.71	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
972	59.90	3.65	0.93	2.72	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
973	60.00	3.65	0.94	2.72	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
974	60.04	3.66	0.94	2.72	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
975	60.10	3.66	0.94	2.72	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
976	60.15	3.67	0.94	2.72	0.66	0.362	1.36	0.267	0.83	1.00	0.322	No
977	60.19	3.67	0.94	2.73	0.66	0.362	1.36	0.266	0.83	1.00	0.322	No
978	60.23	3.67	0.94	2.73	0.66	0.362	1.36	0.266	0.83	1.00	0.322	No
979	60.28	3.67	0.94	2.73	0.66	0.362	1.36	0.266	0.83	1.00	0.322	No
980	60.33	3.68	0.95	2.73	0.66	0.362	1.36	0.266	0.83	1.00	0.322	No
981	60.38	3.68	0.95	2.73	0.66	0.362	1.36	0.266	0.83	1.00	0.322	No
982	60.42	3.68	0.95	2.73	0.66	0.362	1.36	0.266	0.83	1.00	0.322	No
983	60.44	3.68	0.95	2.73	0.66	0.362	1.36	0.266	0.83	1.00	0.322	No
984	60.47	3.69	0.95	2.74	0.66	0.362	1.36	0.266	0.83	1.00	0.322	No
985	60.52	3.69	0.95	2.74	0.66	0.362	1.36	0.266	0.83	1.00	0.321	No
986	60.56	3.69	0.95	2.74	0.65	0.361	1.36	0.266	0.83	1.00	0.321	No
987	60.57	3.69	0.95	2.74	0.65	0.361	1.36	0.266	0.83	1.00	0.321	No
988	60.61	3.70	0.96	2.74	0.65	0.361	1.36	0.266	0.83	1.00	0.321	No
989	60.66	3.70	0.96	2.74	0.65	0.361	1.36	0.266	0.83	1.00	0.321	No
990	60.71	3.70	0.96	2.74	0.65	0.361	1.36	0.265	0.83	1.00	0.321	No
991	60.76	3.71	0.96	2.75	0.65	0.361	1.36	0.265	0.83	1.00	0.321	No
992	60.81	3.71	0.96	2.75	0.65	0.361	1.36	0.265	0.83	1.00	0.321	No
993	60.86	3.71	0.96	2.75	0.65	0.361	1.36	0.265	0.83	1.00	0.321	No
994	60.91	3.72	0.96	2.75	0.65	0.361	1.36	0.265	0.83	1.00	0.321	No
995	60.95	3.72	0.97	2.75	0.65	0.360	1.36	0.265	0.83	1.00	0.321	No
996	61.00	3.72	0.97	2.76	0.65	0.360	1.36	0.265	0.83	1.00	0.321	No
997	61.02	3.72	0.97	2.76	0.65	0.360	1.36	0.265	0.83	1.00	0.321	No
998	61.05	3.73	0.97	2.76	0.65	0.360	1.36	0.265	0.83	1.00	0.321	No
999	61.08	3.73	0.97	2.76	0.65	0.360	1.36	0.265	0.83	1.00	0.321	No
1000	61.09	3.73	0.97	2.76	0.65	0.360	1.36	0.265	0.83	1.00	0.321	No
1001	61.13	3.73	0.97	2.76	0.65	0.360	1.36	0.265	0.83	1.00	0.321	No
1002	61.14	3.73	0.97	2.76	0.65	0.360	1.36	0.265	0.83	1.00	0.321	No
1003	61.16	3.73	0.97	2.76	0.65	0.360	1.36	0.265	0.83	1.00	0.321	No
1004	61.20	3.74	0.97	2.76	0.65	0.360	1.36	0.265	0.83	1.00	0.320	No
1005	61.23	3.74	0.97	2.76	0.65	0.360	1.36	0.264	0.83	1.00	0.320	No
1006	61.24	3.74	0.97	2.76	0.65	0.360	1.36	0.264	0.83	1.00	0.320	No
1007	61.29	3.74	0.98	2.77	0.65	0.360	1.36	0.264	0.83	1.00	0.320	No
1008	61.30	3.74	0.98	2.77	0.65	0.360	1.36	0.264	0.83	1.00	0.320	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1009	61.33	3.75	0.98	2.77	0.65	0.359	1.36	0.264	0.83	1.00	0.320	No
1010	61.38	3.75	0.98	2.77	0.65	0.359	1.36	0.264	0.82	1.00	0.320	No
1011	61.43	3.75	0.98	2.77	0.65	0.359	1.36	0.264	0.82	1.00	0.320	No
1012	61.48	3.76	0.98	2.77	0.65	0.359	1.36	0.264	0.82	1.00	0.320	No
1013	61.53	3.76	0.98	2.78	0.65	0.359	1.36	0.264	0.82	1.00	0.320	No
1014	61.56	3.76	0.98	2.78	0.65	0.359	1.36	0.264	0.82	1.00	0.320	No
1015	61.58	3.76	0.99	2.78	0.65	0.359	1.36	0.264	0.82	1.00	0.320	No
1016	61.59	3.76	0.99	2.78	0.65	0.359	1.36	0.264	0.82	1.00	0.320	No
1017	61.62	3.76	0.99	2.78	0.65	0.359	1.36	0.264	0.82	1.00	0.320	No
1018	61.63	3.77	0.99	2.78	0.65	0.359	1.36	0.264	0.82	1.00	0.320	No
1019	61.67	3.77	0.99	2.78	0.65	0.359	1.36	0.264	0.82	1.00	0.320	No
1020	61.71	3.77	0.99	2.78	0.65	0.358	1.36	0.264	0.82	1.00	0.320	No
1021	61.76	3.77	0.99	2.78	0.65	0.358	1.36	0.263	0.82	1.00	0.320	No
1022	61.81	3.78	0.99	2.79	0.64	0.358	1.36	0.263	0.82	1.00	0.320	No
1023	61.86	3.78	0.99	2.79	0.64	0.358	1.36	0.263	0.82	1.00	0.320	No
1024	61.87	3.78	0.99	2.79	0.64	0.358	1.36	0.263	0.82	1.00	0.320	No
1025	61.91	3.78	1.00	2.79	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
1026	61.95	3.79	1.00	2.79	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
1027	61.96	3.79	1.00	2.79	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
1028	62.00	3.79	1.00	2.79	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
1029	62.04	3.79	1.00	2.79	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
1030	62.06	3.79	1.00	2.79	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
1031	62.10	3.80	1.00	2.80	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
1032	62.14	3.80	1.00	2.80	0.64	0.357	1.36	0.263	0.82	1.00	0.319	No
1033	62.20	3.80	1.00	2.80	0.64	0.357	1.36	0.263	0.82	1.00	0.319	No
1034	62.22	3.80	1.01	2.80	0.64	0.357	1.36	0.263	0.82	1.00	0.319	No
1035	62.27	3.81	1.01	2.80	0.64	0.357	1.36	0.263	0.82	1.00	0.319	No
1036	62.29	3.81	1.01	2.80	0.64	0.357	1.36	0.263	0.82	1.00	0.319	No
1037	62.34	3.81	1.01	2.80	0.64	0.357	1.36	0.262	0.82	1.00	0.319	No
1038	62.39	3.82	1.01	2.81	0.64	0.357	1.36	0.262	0.82	1.00	0.319	No
1039	62.43	3.82	1.01	2.81	0.64	0.357	1.36	0.262	0.82	1.00	0.319	No
1040	62.49	3.82	1.01	2.81	0.64	0.357	1.36	0.262	0.82	1.00	0.319	No
1041	62.57	3.83	1.02	2.81	0.64	0.356	1.36	0.262	0.82	1.00	0.319	No
1042	62.68	3.84	1.02	2.82	0.64	0.356	1.36	0.262	0.82	1.00	0.318	No
1043	62.75	3.84	1.02	2.82	0.64	0.356	1.36	0.262	0.82	1.00	0.318	No
1044	62.87	3.85	1.03	2.82	0.64	0.356	1.36	0.261	0.82	1.00	0.318	No
1045	62.88	3.85	1.03	2.82	0.64	0.356	1.36	0.261	0.82	1.00	0.318	No
1046	62.89	3.85	1.03	2.82	0.64	0.356	1.36	0.261	0.82	1.00	0.318	No
1047	62.93	3.85	1.03	2.83	0.64	0.355	1.36	0.261	0.82	1.00	0.318	No
1048	62.98	3.86	1.03	2.83	0.64	0.355	1.36	0.261	0.82	1.00	0.318	No
1049	63.02	3.86	1.03	2.83	0.64	0.355	1.36	0.261	0.82	1.00	0.318	No
1050	63.07	3.86	1.03	2.83	0.64	0.355	1.36	0.261	0.82	1.00	0.318	No
1051	63.12	3.86	1.03	2.83	0.64	0.355	1.36	0.261	0.82	1.00	0.318	No
1052	63.14	3.86	1.03	2.83	0.64	0.355	1.36	0.261	0.82	1.00	0.318	No
1053	63.17	3.87	1.03	2.83	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No
1054	63.17	3.87	1.04	2.83	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No
1055	63.20	3.87	1.04	2.83	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No
1056	63.21	3.87	1.04	2.83	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1057	63.23	3.87	1.04	2.83	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No
1058	63.26	3.87	1.04	2.83	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No
1059	63.28	3.87	1.04	2.83	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No
1060	63.31	3.87	1.04	2.83	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No
1061	63.32	3.87	1.04	2.83	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No
1062	63.36	3.87	1.04	2.83	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No
1063	63.40	3.88	1.04	2.83	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
σ_v: Total overburden pressure at test point (tsf)
u_0: Water pressure at test point (tsf)
σ_v': Effective overburden pressure based on GWT during earthquake (tsf)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.01	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
2	0.04	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
3	0.09	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
4	0.11	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
5	0.14	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
6	0.14	1.35	3.66	4.59	1.00	2.15	27.82	59.81	4.000	No	Yes	2.00
7	0.18	6.97	2.69	0.89	0.81	11.19	4.58	51.24	4.000	No	Yes	2.00
8	0.23	18.19	2.14	0.35	0.65	29.21	1.00	29.21	4.000	No	No	2.00
9	0.24	36.79	1.76	0.18	0.54	59.09	1.00	59.09	4.000	No	No	2.00
10	0.28	53.07	1.58	0.14	0.50	85.23	1.00	85.23	4.000	No	No	2.00
11	0.33	59.27	1.53	0.14	0.50	95.19	1.00	95.19	4.000	No	No	2.00
12	0.38	56.61	1.60	0.20	0.50	90.91	1.00	90.91	4.000	No	No	2.00
13	0.42	52.11	1.72	0.34	0.52	83.69	1.00	83.69	4.000	No	No	2.00
14	0.47	51.84	1.83	0.58	0.56	83.25	1.19	98.77	4.000	No	No	2.00
15	0.51	51.94	1.90	0.76	0.58	83.40	1.24	103.16	4.000	No	No	2.00
16	0.52	52.09	1.93	0.85	0.59	83.64	1.26	104.99	4.000	No	No	2.00
17	0.57	52.66	1.91	0.81	0.58	84.56	1.24	105.20	4.000	No	No	2.00
18	0.61	53.24	1.89	0.76	0.58	85.48	1.23	105.23	4.000	No	No	2.00
19	0.67	53.47	1.88	0.73	0.57	85.85	1.22	105.00	4.000	No	No	2.00
20	0.73	53.84	1.87	0.71	0.57	86.44	1.22	105.23	4.000	No	No	2.00
21	0.81	53.62	1.87	0.71	0.57	86.08	1.22	104.72	4.000	No	No	2.00
22	0.86	53.52	1.92	0.84	0.58	85.91	1.25	107.16	4.000	No	No	2.00
23	0.98	52.14	1.96	0.96	0.60	83.69	1.28	106.78	4.000	No	No	2.00
24	1.05	48.22	2.02	1.08	0.61	77.37	1.32	102.42	4.000	No	No	2.00
25	1.15	43.67	2.04	1.03	0.62	70.05	1.34	94.07	4.000	No	No	2.00
26	1.24	37.87	2.07	0.96	0.63	60.73	1.38	83.84	4.000	No	No	2.00
27	1.34	34.47	2.09	0.89	0.63	55.26	1.40	77.37	4.000	No	No	2.00
28	1.43	30.63	2.16	0.99	0.65	49.08	1.51	74.33	4.000	No	No	2.00
29	1.53	26.86	2.25	1.20	0.68	43.01	1.75	75.37	4.000	No	No	2.00
30	1.58	24.56	2.31	1.36	0.70	39.32	1.98	77.68	4.000	No	No	2.00
31	1.62	23.48	2.32	1.31	0.70	37.59	2.00	75.15	4.000	No	No	2.00
32	1.67	24.36	2.28	1.18	0.69	38.99	1.85	72.19	4.000	No	No	2.00
33	1.75	23.89	2.28	1.15	0.69	38.23	1.86	70.99	4.000	No	No	2.00
34	1.77	23.08	2.30	1.17	0.70	36.93	1.92	70.79	4.000	No	No	2.00
35	1.81	21.50	2.34	1.25	0.71	34.38	2.08	71.55	4.000	No	No	2.00
36	1.86	19.71	2.39	1.32	0.72	31.51	2.30	72.37	4.000	No	No	2.00
37	1.91	17.96	2.43	1.37	0.74	28.69	2.52	72.24	4.000	No	No	2.00
38	1.95	16.98	2.43	1.26	0.74	27.11	2.53	68.54	4.000	No	No	2.00
39	2.00	16.21	2.41	1.09	0.73	25.86	2.43	62.85	4.000	No	No	2.00
40	2.05	14.89	2.41	0.93	0.73	23.75	2.42	57.52	4.000	Yes	No	2.00
41	2.11	13.51	2.43	0.88	0.74	21.52	2.55	54.95	4.000	Yes	No	2.00
42	2.20	12.33	2.47	0.89	0.75	19.62	2.79	54.76	4.000	Yes	No	2.00
43	2.24	11.73	2.50	0.95	0.76	18.64	3.01	56.15	4.000	Yes	No	2.00
44	2.29	11.26	2.54	1.06	0.77	17.88	3.29	58.85	4.000	Yes	No	2.00
45	2.34	11.32	2.60	1.39	0.79	17.99	3.76	67.59	4.000	Yes	Yes	2.00
46	2.44	12.17	2.61	1.64	0.79	19.33	3.86	74.63	4.000	Yes	Yes	2.00
47	2.48	14.56	2.56	1.73	0.78	23.17	3.43	79.44	4.000	Yes	No	2.00
48	2.58	18.03	2.47	1.60	0.75	28.74	2.75	79.05	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	2.63	22.41	2.37	1.48	0.72	35.77	2.21	79.01	4.000	Yes	No	2.00
50	2.71	26.08	2.30	1.39	0.70	41.66	1.92	80.03	4.000	Yes	No	2.00
51	2.78	30.33	2.22	1.27	0.67	48.48	1.67	80.89	4.000	Yes	No	2.00
52	2.82	33.73	2.16	1.16	0.66	53.95	1.52	82.21	4.000	Yes	No	2.00
53	2.89	34.94	2.13	1.09	0.65	55.89	1.47	82.24	4.000	Yes	No	2.00
54	2.96	33.63	2.16	1.13	0.65	53.77	1.51	81.39	4.000	No	No	2.00
55	3.03	30.90	2.20	1.21	0.67	49.37	1.62	80.00	4.000	No	No	2.00
56	3.11	28.98	2.23	1.23	0.68	46.28	1.70	78.46	4.000	No	No	2.00
57	3.19	26.45	2.26	1.23	0.69	42.22	1.79	75.65	4.000	No	No	2.00
58	3.25	23.52	2.31	1.27	0.70	37.50	1.97	73.87	4.000	No	No	2.00
59	3.35	20.49	2.38	1.38	0.72	32.62	2.28	74.42	4.000	No	No	2.00
60	3.41	17.79	2.44	1.42	0.74	28.29	2.60	73.49	4.000	No	No	2.00
61	3.50	15.91	2.46	1.31	0.75	25.25	2.74	69.10	4.000	No	No	2.00
62	3.59	14.83	2.45	1.11	0.74	23.51	2.66	62.63	4.000	No	No	2.00
63	3.69	14.59	2.43	0.99	0.74	23.12	2.55	58.90	4.000	No	No	2.00
64	3.79	15.20	2.39	0.89	0.73	24.09	2.35	56.48	4.000	No	No	2.00
65	3.88	16.54	2.34	0.81	0.71	26.24	2.09	54.78	4.000	No	No	2.00
66	3.97	19.14	2.27	0.75	0.69	30.40	1.82	55.25	4.000	No	No	2.00
67	4.07	20.82	2.26	0.82	0.68	33.10	1.77	58.69	4.000	No	No	2.00
68	4.14	23.49	2.22	0.86	0.67	37.37	1.67	62.38	4.000	No	No	2.00
69	4.17	25.51	2.20	0.89	0.67	40.62	1.61	65.25	4.000	No	No	2.00
70	4.26	28.14	2.15	0.86	0.65	44.83	1.51	67.83	4.000	No	No	2.00
71	4.32	28.71	2.16	0.90	0.66	45.74	1.52	69.43	4.000	No	No	2.00
72	4.37	28.10	2.18	0.95	0.66	44.77	1.56	69.94	4.000	No	No	2.00
73	4.42	26.62	2.21	1.02	0.67	42.38	1.65	69.93	4.000	No	No	2.00
74	4.51	25.07	2.24	1.05	0.68	39.88	1.74	69.30	4.000	No	No	2.00
75	4.61	23.68	2.27	1.07	0.69	37.65	1.82	68.42	4.000	No	No	2.00
76	4.65	22.37	2.29	1.08	0.70	35.53	1.90	67.38	4.000	No	No	2.00
77	4.74	21.09	2.32	1.11	0.70	33.47	2.00	67.06	4.000	No	No	2.00
78	4.80	20.48	2.33	1.11	0.71	32.49	2.05	66.55	4.000	No	No	2.00
79	4.89	20.04	2.34	1.12	0.71	31.78	2.09	66.46	4.000	No	No	2.00
80	4.95	20.38	2.33	1.10	0.71	32.32	2.05	66.20	4.000	No	No	2.00
81	5.04	21.05	2.31	1.07	0.70	33.39	1.97	65.92	4.000	No	No	2.00
82	5.13	22.81	2.27	0.99	0.69	36.20	1.80	65.26	4.000	No	No	2.00
83	5.18	25.27	2.20	0.90	0.67	40.14	1.63	65.28	4.000	No	No	2.00
84	5.28	28.07	2.14	0.82	0.65	44.63	1.49	66.64	4.000	No	No	2.00
85	5.32	31.47	2.09	0.76	0.63	50.09	1.40	70.04	4.000	No	No	2.00
86	5.42	34.67	2.05	0.75	0.62	55.23	1.35	74.62	4.000	No	No	2.00
87	5.51	38.14	2.01	0.74	0.61	60.80	1.31	79.86	4.000	No	No	2.00
88	5.60	41.28	1.94	0.63	0.59	65.83	1.26	83.18	4.000	No	No	2.00
89	5.66	44.24	1.88	0.53	0.57	70.58	1.22	86.14	4.000	No	No	2.00
90	5.76	45.86	1.83	0.46	0.56	73.17	1.00	73.17	4.000	No	No	2.00
91	5.85	44.91	1.86	0.50	0.57	71.65	1.21	86.53	4.000	No	No	2.00
92	5.92	41.11	1.92	0.56	0.58	65.53	1.25	81.79	4.000	No	No	2.00
93	5.95	38.21	1.96	0.61	0.60	60.87	1.28	77.76	4.000	No	No	2.00
94	5.97	36.15	1.99	0.64	0.61	57.56	1.30	74.97	4.000	No	No	2.00
95	6.02	35.37	2.01	0.65	0.61	56.31	1.31	73.90	4.000	Yes	No	2.00
96	6.06	32.74	2.05	0.70	0.62	52.08	1.36	70.59	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	6.16	29.98	2.10	0.76	0.64	47.63	1.42	67.87	4.000	Yes	No	2.00
98	6.21	26.98	2.18	0.88	0.66	42.82	1.56	66.83	4.000	Yes	No	2.00
99	6.26	24.29	2.26	1.07	0.69	38.48	1.79	68.74	4.000	Yes	No	2.00
100	6.31	21.62	2.36	1.35	0.72	34.19	2.18	74.63	4.000	Yes	No	2.00
101	6.40	19.23	2.46	1.68	0.75	30.34	2.70	82.06	4.000	Yes	No	2.00
102	6.44	16.91	2.56	2.09	0.78	26.60	3.43	91.18	4.000	Yes	No	2.00
103	6.52	15.12	2.64	2.48	0.80	23.73	4.16	98.65	4.000	Yes	Yes	2.00
104	6.57	13.47	2.73	2.91	0.83	21.08	5.01	105.63	4.000	Yes	Yes	2.00
105	6.64	12.16	2.80	3.29	0.85	18.96	5.81	110.19	4.000	Yes	Yes	2.00
106	6.69	10.98	2.86	3.65	0.87	17.06	6.65	113.46	4.000	Yes	Yes	2.00
107	6.78	10.34	2.90	3.84	0.88	16.02	7.15	114.49	4.000	Yes	Yes	2.00
108	6.83	9.90	2.91	3.84	0.88	15.31	7.38	112.96	4.000	Yes	Yes	2.00
109	6.92	9.60	2.92	3.75	0.88	14.82	7.45	110.37	4.000	No	Yes	2.00
110	6.97	9.39	2.91	3.59	0.88	14.48	7.39	107.07	4.000	No	Yes	2.00
111	7.03	9.29	2.91	3.50	0.88	14.32	7.35	105.27	4.000	No	Yes	2.00
112	7.12	9.32	2.90	3.42	0.88	14.36	7.25	104.07	4.000	No	Yes	2.00
113	7.22	9.39	2.90	3.38	0.88	14.46	7.17	103.64	4.000	No	Yes	2.00
114	7.27	9.52	2.89	3.37	0.88	14.66	7.09	103.89	4.000	No	Yes	2.00
115	7.36	9.65	2.89	3.41	0.87	14.86	7.06	104.93	4.000	No	Yes	2.00
116	7.43	9.75	2.89	3.48	0.88	15.01	7.08	106.34	4.000	No	Yes	2.00
117	7.50	9.78	2.90	3.56	0.88	15.06	7.16	107.82	4.000	No	Yes	2.00
118	7.59	9.77	2.90	3.61	0.88	15.04	7.22	108.69	4.000	No	Yes	2.00
119	7.64	9.70	2.91	3.69	0.88	14.93	7.34	109.64	4.000	No	Yes	2.00
120	7.75	9.63	2.92	3.75	0.88	14.81	7.46	110.40	4.000	No	Yes	2.00
121	7.79	9.70	2.92	3.76	0.88	14.91	7.43	110.74	4.000	No	Yes	2.00
122	7.89	9.97	2.90	3.67	0.88	15.33	7.19	110.22	4.000	No	Yes	2.00
123	7.99	10.24	2.88	3.59	0.87	15.76	6.97	109.89	4.000	No	Yes	2.00
124	8.04	10.34	2.88	3.62	0.87	15.91	6.96	110.71	4.000	No	Yes	2.00
125	8.13	10.31	2.89	3.67	0.87	15.85	7.03	111.39	4.000	No	Yes	2.00
126	8.23	10.27	2.84	3.03	0.86	15.79	6.35	100.23	4.000	No	Yes	2.00
127	8.32	10.27	2.79	2.55	0.85	15.77	5.78	91.18	4.000	No	Yes	2.00
128	8.37	10.53	2.76	2.28	0.84	16.20	5.34	86.47	4.000	No	Yes	2.00
129	8.46	11.04	2.79	2.79	0.85	17.00	5.74	97.61	4.000	No	Yes	2.00
130	8.56	11.30	2.82	3.16	0.85	17.42	6.05	105.35	4.000	No	Yes	2.00
131	8.59	11.30	2.84	3.44	0.86	17.41	6.35	110.51	4.000	No	Yes	2.00
132	8.61	11.03	2.87	3.69	0.87	16.97	6.71	113.97	4.000	No	Yes	2.00
133	8.67	10.89	2.88	3.88	0.87	16.75	6.98	116.82	4.000	No	Yes	2.00
134	8.71	10.69	2.90	4.05	0.88	16.41	7.24	118.78	4.000	No	Yes	2.00
135	8.72	10.51	2.92	4.18	0.88	16.13	7.46	120.30	4.000	No	Yes	2.00
136	8.78	10.44	2.92	4.25	0.89	16.02	7.56	121.13	4.000	No	Yes	2.00
137	8.80	10.44	2.93	4.28	0.89	16.02	7.59	121.54	4.000	No	Yes	2.00
138	8.86	10.44	2.93	4.29	0.89	16.01	7.60	121.62	4.000	No	Yes	2.00
139	8.90	10.55	2.92	4.29	0.88	16.17	7.55	122.08	4.000	No	Yes	2.00
140	8.95	10.68	2.92	4.30	0.88	16.39	7.49	122.77	4.000	No	Yes	2.00
141	8.96	10.89	2.91	4.30	0.88	16.71	7.39	123.54	4.000	No	Yes	2.00
142	9.00	11.05	2.91	4.31	0.88	16.98	7.33	124.43	4.000	No	Yes	2.00
143	9.05	11.29	2.90	4.33	0.88	17.35	7.24	125.55	4.000	No	Yes	2.00
144	9.09	11.56	2.89	4.31	0.88	17.78	7.10	126.26	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	9.10	11.96	2.88	4.27	0.87	18.43	6.89	127.03	4.000	No	Yes	2.00
146	9.14	12.47	2.86	4.24	0.87	19.24	6.66	128.15	4.000	No	Yes	2.00
147	9.20	13.21	2.84	4.16	0.86	20.42	6.33	129.23	4.000	No	Yes	2.00
148	9.24	14.09	2.81	4.06	0.85	21.83	5.95	129.98	4.000	No	Yes	2.00
149	9.29	15.03	2.78	3.93	0.84	23.34	5.57	129.97	4.000	No	Yes	2.00
150	9.31	15.90	2.75	3.85	0.83	24.74	5.28	130.54	4.000	No	Yes	2.00
151	9.38	16.61	2.73	3.79	0.83	25.88	5.06	130.87	4.000	Yes	Yes	2.00
152	9.41	17.32	2.71	3.66	0.82	27.00	4.80	129.53	4.000	Yes	Yes	2.00
153	9.47	18.02	2.68	3.45	0.81	28.13	4.48	126.15	4.000	Yes	Yes	2.00
154	9.53	19.33	2.62	3.03	0.79	30.23	3.91	118.10	4.000	Yes	Yes	2.00
155	9.62	21.08	2.54	2.58	0.77	33.03	3.29	108.83	4.000	Yes	No	2.00
156	9.67	23.71	2.45	2.07	0.74	36.88	2.63	97.08	4.000	Yes	No	2.00
157	9.77	26.25	2.37	1.72	0.72	39.96	2.22	88.55	4.000	Yes	No	2.00
158	9.81	28.83	2.29	1.42	0.70	43.12	1.89	81.52	4.000	Yes	No	2.00
159	9.90	30.67	2.24	1.23	0.68	45.16	1.72	77.57	4.000	Yes	No	2.00
160	9.97	32.26	2.20	1.11	0.67	46.92	1.61	75.55	4.000	Yes	No	2.00
161	10.06	32.63	2.20	1.11	0.67	47.13	1.61	75.67	4.000	No	No	2.00
162	10.20	32.13	2.22	1.20	0.68	46.19	1.68	77.59	4.000	Yes	No	2.00
163	10.30	29.29	2.26	1.22	0.69	42.06	1.79	75.15	4.000	Yes	No	2.00
164	10.44	25.52	2.33	1.34	0.71	36.67	2.06	75.52	4.000	Yes	No	2.00
165	10.54	20.70	2.45	1.61	0.74	30.03	2.66	79.87	4.000	Yes	No	2.00
166	10.63	16.56	2.64	2.51	0.80	24.49	4.08	99.92	4.000	Yes	Yes	2.00
167	10.74	13.83	2.78	3.48	0.84	20.66	5.64	116.62	4.000	Yes	Yes	2.00
168	10.78	12.62	2.86	4.22	0.87	18.99	6.71	127.39	4.000	Yes	Yes	2.00
169	10.83	12.48	2.88	4.44	0.87	18.76	6.96	130.59	4.000	Yes	Yes	2.00
170	10.88	12.31	2.90	4.63	0.88	18.47	7.21	133.16	4.000	Yes	Yes	2.00
171	10.89	12.15	2.92	4.89	0.88	18.24	7.50	136.86	4.000	Yes	Yes	2.00
172	10.97	12.25	2.93	5.04	0.89	18.30	7.62	139.36	4.000	No	Yes	2.00
173	11.02	12.48	2.93	5.14	0.89	18.59	7.62	141.70	4.000	No	Yes	2.00
174	11.07	12.79	2.92	5.12	0.88	18.96	7.51	142.37	4.000	No	Yes	2.00
175	11.11	13.06	2.91	5.11	0.88	19.28	7.42	143.00	4.000	No	Yes	2.00
176	11.16	13.39	2.91	5.09	0.88	19.70	7.30	143.71	4.000	No	Yes	2.00
177	11.21	13.76	2.90	5.09	0.88	20.15	7.19	144.81	4.000	No	Yes	2.00
178	11.26	14.14	2.89	5.11	0.88	20.62	7.10	146.37	4.000	No	Yes	2.00
179	11.30	14.37	2.89	5.20	0.88	20.90	7.10	148.42	4.000	No	Yes	2.00
180	11.36	14.54	2.90	5.29	0.88	21.07	7.14	150.43	4.000	No	Yes	2.00
181	11.40	14.68	2.90	5.36	0.88	21.19	7.17	151.92	4.000	No	Yes	2.00
182	11.45	14.81	2.90	5.40	0.88	21.32	7.18	152.97	4.000	No	Yes	2.00
183	11.50	15.04	2.89	5.41	0.88	21.57	7.12	153.64	4.000	No	Yes	2.00
184	11.55	15.31	2.89	5.41	0.88	21.86	7.06	154.44	4.000	No	Yes	2.00
185	11.60	15.85	2.88	5.35	0.87	22.53	6.88	155.07	4.000	No	Yes	2.00
186	11.66	16.56	2.86	5.25	0.87	23.39	6.63	155.14	4.000	No	Yes	2.00
187	11.74	17.40	2.84	5.06	0.86	24.38	6.31	153.92	4.000	No	Yes	2.00
188	11.84	17.98	2.82	4.98	0.86	24.97	6.15	153.46	4.000	No	Yes	2.00
189	11.93	18.18	2.82	5.03	0.86	25.08	6.17	154.65	4.000	No	Yes	2.00
190	12.04	18.04	2.84	5.23	0.86	24.73	6.38	157.76	4.000	No	Yes	2.00
191	12.13	17.87	2.86	5.42	0.87	24.37	6.58	160.42	4.000	No	Yes	2.00
192	12.22	17.67	2.87	5.55	0.87	23.94	6.76	161.87	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	12.27	17.51	2.88	5.59	0.87	23.64	6.85	161.93	4.000	No	Yes	2.00
194	12.37	17.27	2.88	5.64	0.87	23.16	6.98	161.58	4.000	No	Yes	2.00
195	12.41	17.17	2.89	5.65	0.87	22.94	7.03	161.26	4.000	No	Yes	2.00
196	12.51	17.06	2.89	5.71	0.88	22.65	7.13	161.48	4.000	No	Yes	2.00
197	12.56	17.23	2.89	5.68	0.88	22.78	7.08	161.37	4.000	No	Yes	2.00
198	12.65	17.64	2.88	5.61	0.87	23.15	6.96	161.03	4.000	No	Yes	2.00
199	12.71	18.45	2.86	5.51	0.87	24.09	6.70	161.44	4.000	No	Yes	2.00
200	12.79	19.23	2.86	5.57	0.87	24.96	6.59	164.56	4.000	No	Yes	2.00
201	12.89	20.10	2.85	5.67	0.86	25.92	6.50	168.54	4.000	No	Yes	2.00
202	12.96	20.98	2.84	5.80	0.86	26.96	6.43	173.33	4.000	No	Yes	2.00
203	13.04	22.23	2.82	5.70	0.86	28.37	6.15	174.57	4.000	Yes	Yes	2.00
204	13.13	24.11	2.78	5.33	0.84	30.49	5.62	171.40	4.000	Yes	Yes	2.00
205	13.23	26.80	2.65	3.76	0.80	33.27	4.19	139.58	4.000	Yes	Yes	2.00
206	13.30	30.34	2.49	2.43	0.76	36.95	2.91	107.47	4.000	Yes	No	2.00
207	13.37	34.15	2.32	1.49	0.70	40.77	2.02	82.17	4.000	Yes	No	2.00
208	13.47	38.32	2.29	1.49	0.69	45.44	1.87	85.15	4.000	Yes	No	2.00
209	13.57	38.79	2.31	1.62	0.70	45.84	1.94	89.15	4.000	No	No	2.00
210	13.61	39.19	2.31	1.69	0.70	46.27	1.98	91.39	4.000	No	No	2.00
211	13.62	40.31	2.30	1.69	0.70	47.52	1.94	92.31	4.000	No	No	2.00
212	13.68	44.31	2.26	1.59	0.69	51.92	1.78	92.36	4.000	No	No	2.00
213	13.73	47.82	2.22	1.53	0.68	55.76	1.68	93.57	4.000	No	No	2.00
214	13.77	50.08	2.21	1.55	0.67	58.23	1.65	95.79	4.000	No	No	2.00
215	13.87	52.91	2.20	1.55	0.67	61.16	1.61	98.26	4.000	No	No	2.00
216	13.93	55.78	2.19	1.58	0.66	64.26	1.58	101.41	4.000	No	No	2.00
217	14.00	58.54	2.17	1.60	0.66	67.15	1.55	104.21	4.000	No	No	2.00
218	14.06	60.62	2.17	1.63	0.66	69.33	1.54	106.89	4.000	No	No	2.00
219	14.12	62.21	2.17	1.67	0.66	70.95	1.54	109.37	4.000	No	No	2.00
220	14.21	63.05	2.17	1.71	0.66	71.63	1.55	111.13	4.000	No	No	2.00
221	14.25	63.45	2.18	1.75	0.66	71.96	1.56	112.44	4.000	No	No	2.00
222	14.35	63.35	2.18	1.78	0.66	71.51	1.58	112.67	4.000	No	No	2.00
223	14.45	62.61	2.19	1.80	0.67	70.37	1.60	112.38	4.000	No	No	2.00
224	14.50	61.06	2.21	1.83	0.67	68.50	1.63	111.75	4.000	No	No	2.00
225	14.59	59.18	2.22	1.87	0.68	66.15	1.68	111.04	4.000	No	No	2.00
226	14.64	57.19	2.24	1.92	0.68	63.82	1.73	110.49	4.000	No	No	2.00
227	14.74	55.60	2.26	1.95	0.69	61.79	1.78	110.08	4.000	No	No	2.00
228	14.80	54.22	2.27	1.99	0.69	60.12	1.83	109.86	4.000	No	No	2.00
229	14.88	53.18	2.28	2.02	0.69	58.73	1.87	109.70	4.000	No	No	2.00
230	14.97	52.24	2.30	2.05	0.70	57.45	1.91	109.62	4.000	No	No	2.00
231	15.05	51.43	2.31	2.08	0.70	56.38	1.95	110.04	4.000	No	No	2.00
232	15.13	50.85	2.32	2.12	0.70	55.53	1.99	110.56	4.000	No	No	2.00
233	15.21	50.95	2.32	2.12	0.70	55.42	1.99	110.46	4.000	No	No	2.00
234	15.28	52.23	2.30	2.06	0.70	56.58	1.93	109.48	4.000	No	No	2.00
235	15.36	55.10	2.27	1.95	0.69	59.37	1.82	108.07	4.000	No	No	2.00
236	15.41	60.22	2.22	1.78	0.67	64.61	1.66	107.30	4.000	No	No	2.00
237	15.50	66.38	2.16	1.62	0.66	70.74	1.53	108.00	4.000	No	No	2.00
238	15.55	72.78	2.07	1.31	0.63	77.07	1.38	106.45	4.000	No	No	2.00
239	15.65	76.92	2.00	1.07	0.61	80.83	1.31	105.71	4.000	No	No	2.00
240	15.71	78.17	1.94	0.88	0.59	81.68	1.27	103.43	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	15.79	75.07	1.96	0.89	0.60	78.22	1.28	99.99	4.000	Yes	No	2.00
242	15.89	67.29	2.02	0.97	0.61	69.97	1.33	92.88	4.000	Yes	No	2.00
243	15.90	61.09	2.07	1.04	0.63	63.58	1.38	88.03	4.000	Yes	No	2.00
244	15.94	56.21	2.12	1.11	0.64	58.47	1.45	84.99	4.000	Yes	No	2.00
245	16.00	53.24	2.15	1.16	0.65	55.28	1.51	83.45	4.000	Yes	No	2.00
246	16.06	47.68	2.22	1.30	0.67	49.45	1.67	82.65	4.000	Yes	No	2.00
247	16.14	40.74	2.32	1.56	0.71	42.17	2.02	85.02	4.000	Yes	No	2.00
248	16.19	34.10	2.43	1.87	0.74	35.24	2.56	90.26	4.000	Yes	No	2.00
249	16.26	27.10	2.57	2.32	0.78	27.88	3.51	97.89	4.000	Yes	No	2.00
250	16.33	21.54	2.70	2.80	0.82	22.01	4.74	104.24	4.000	Yes	Yes	2.00
251	16.38	17.06	2.83	3.31	0.86	17.28	6.24	107.80	4.000	Yes	Yes	2.00
252	16.47	14.43	2.93	3.75	0.89	14.45	7.58	109.50	4.000	Yes	Yes	2.00
253	16.54	12.64	3.00	4.14	1.00	12.69	8.71	110.54	4.000	Yes	Yes	2.00
254	16.62	11.80	3.05	4.58	1.00	11.71	9.67	113.31	4.000	No	Yes	2.00
255	16.70	11.53	3.08	4.88	1.00	11.36	10.18	115.66	4.000	No	Yes	2.00
256	16.76	12.28	3.06	4.98	1.00	12.12	9.88	119.66	4.000	No	Yes	2.00
257	16.86	14.88	2.96	4.36	1.00	14.80	8.08	119.59	4.000	Yes	Yes	2.00
258	16.90	19.33	2.82	3.59	0.85	19.15	6.07	116.24	4.000	Yes	Yes	2.00
259	16.98	25.84	2.65	2.82	0.80	25.69	4.22	108.51	4.000	Yes	Yes	2.00
260	17.05	35.42	2.48	2.18	0.75	35.23	2.81	99.11	4.000	Yes	No	2.00
261	17.14	47.54	2.30	1.68	0.70	47.19	1.94	91.71	4.000	Yes	No	2.00
262	17.20	61.48	2.15	1.32	0.65	60.90	1.51	91.88	4.000	Yes	No	2.00
263	17.29	73.03	2.05	1.11	0.62	72.03	1.35	97.56	4.000	Yes	No	2.00
264	17.34	81.99	1.99	1.01	0.60	80.70	1.30	104.58	4.000	Yes	No	2.00
265	17.44	86.87	1.97	1.01	0.60	85.21	1.28	109.31	4.000	No	No	2.00
266	17.50	88.89	1.93	0.91	0.59	86.96	1.26	109.36	4.000	No	No	2.00
267	17.58	88.15	1.91	0.82	0.58	85.91	1.24	106.78	4.000	No	No	2.00
268	17.64	85.02	1.90	0.75	0.58	82.63	1.24	102.13	4.000	No	No	2.00
269	17.75	80.50	1.95	0.85	0.59	77.97	1.27	99.12	4.000	No	No	2.00
270	17.82	72.08	2.04	1.03	0.62	69.66	1.35	93.80	4.000	No	No	2.00
271	17.89	66.02	2.11	1.19	0.64	63.60	1.43	91.18	4.000	No	No	2.00
272	17.89	62.68	2.15	1.30	0.65	60.37	1.51	91.04	4.000	No	No	2.00
273	17.96	64.06	2.15	1.31	0.65	61.55	1.50	92.30	4.000	No	No	2.00
274	18.02	65.34	2.15	1.35	0.65	62.67	1.51	94.33	4.000	No	No	2.00
275	18.07	66.86	2.15	1.39	0.65	64.01	1.51	96.43	4.000	No	No	2.00
276	18.17	68.78	2.14	1.40	0.65	65.62	1.49	98.02	4.000	No	No	2.00
277	18.22	68.74	2.15	1.43	0.65	65.47	1.51	98.54	4.000	Yes	No	2.00
278	18.30	65.20	2.19	1.53	0.66	61.85	1.59	98.20	4.000	Yes	No	2.00
279	18.36	57.69	2.27	1.79	0.69	54.52	1.83	99.83	4.000	Yes	No	2.00
280	18.42	49.20	2.39	2.19	0.72	46.28	2.30	106.36	4.000	Yes	No	2.00
281	18.50	39.97	2.53	2.80	0.77	37.31	3.16	118.00	4.000	Yes	No	2.00
282	18.56	32.38	2.66	3.50	0.81	29.97	4.32	129.55	4.000	Yes	Yes	2.00
283	18.62	25.71	2.80	4.24	0.85	23.53	5.80	136.40	4.000	Yes	Yes	2.00
284	18.69	23.96	2.82	4.26	0.85	21.78	6.13	133.60	4.000	Yes	Yes	2.00
285	18.76	22.21	2.86	4.37	0.87	20.05	6.60	132.24	4.000	Yes	Yes	2.00
286	18.84	24.30	2.80	4.02	0.85	21.95	5.90	129.41	4.000	Yes	Yes	2.00
287	18.89	31.88	2.66	3.30	0.80	29.04	4.26	123.66	4.000	Yes	Yes	2.00
288	18.98	52.85	2.37	2.20	0.72	48.61	2.23	108.20	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	19.05	78.42	2.16	1.65	0.66	72.48	1.52	110.23	4.000	Yes	No	2.00
290	19.12	101.80	2.02	1.36	0.61	94.21	1.32	124.65	4.000	Yes	No	2.00
291	19.18	115.88	1.95	1.24	0.59	107.18	1.27	136.09	4.000	Yes	No	2.00
292	19.24	124.07	1.91	1.18	0.58	114.61	1.25	142.72	4.000	Yes	No	2.00
293	19.32	126.76	1.90	1.17	0.58	116.83	1.24	144.84	4.000	No	No	2.00
294	19.38	126.53	1.92	1.21	0.58	116.38	1.25	145.16	4.000	No	No	2.00
295	19.46	124.81	1.94	1.27	0.59	114.42	1.26	144.25	4.000	No	No	2.00
296	19.54	122.62	1.96	1.34	0.60	112.08	1.28	142.92	4.000	No	No	2.00
297	19.62	121.00	1.97	1.38	0.60	110.26	1.28	141.68	4.000	No	No	2.00
298	19.70	119.99	1.98	1.40	0.60	109.01	1.29	140.65	4.000	No	No	2.00
299	19.80	119.75	1.98	1.39	0.60	108.41	1.29	140.01	4.000	No	No	2.00
300	19.85	119.75	1.98	1.39	0.60	108.23	1.29	139.71	4.000	No	No	2.00
301	19.94	119.95	1.98	1.40	0.60	108.07	1.29	139.71	4.000	No	No	2.00
302	20.03	120.73	1.96	1.31	0.60	108.50	1.28	138.61	4.000	No	No	2.00
303	20.13	121.84	1.94	1.23	0.59	109.19	1.26	137.92	4.000	No	No	2.00
304	20.19	123.33	1.91	1.14	0.58	110.40	1.25	137.60	4.000	No	No	2.00
305	20.29	124.05	1.92	1.16	0.58	110.67	1.25	138.32	4.000	No	No	2.00
306	20.39	124.51	1.93	1.18	0.59	110.70	1.25	138.76	4.000	No	No	2.00
307	20.43	124.14	1.93	1.21	0.59	110.23	1.26	138.70	4.000	No	No	2.00
308	20.47	124.09	1.94	1.23	0.59	109.99	1.26	138.78	4.000	No	No	2.00
309	20.52	123.97	1.95	1.26	0.59	109.69	1.27	139.06	4.000	No	No	2.00
310	20.61	123.97	1.96	1.30	0.59	109.33	1.27	139.29	4.000	No	No	2.00
311	20.66	123.26	1.97	1.34	0.60	108.48	1.28	139.08	4.000	No	No	2.00
312	20.71	122.22	1.98	1.36	0.60	107.35	1.29	138.34	4.000	No	No	2.00
313	20.77	121.00	1.99	1.39	0.60	106.04	1.30	137.35	4.000	No	No	2.00
314	20.85	120.53	1.99	1.40	0.60	105.33	1.30	136.79	4.000	No	No	2.00
315	20.91	120.63	1.99	1.40	0.61	105.23	1.30	136.74	4.000	No	No	2.00
316	21.00	121.00	1.99	1.40	0.61	105.23	1.30	136.71	4.000	No	No	2.00
317	21.05	120.93	1.99	1.40	0.61	105.01	1.30	136.53	4.000	No	No	2.00
318	21.11	120.50	2.00	1.41	0.61	104.40	1.30	136.06	4.000	No	No	2.00
319	21.19	120.16	2.00	1.42	0.61	103.82	1.31	135.66	4.000	No	No	2.00
320	21.24	120.23	2.00	1.43	0.61	103.70	1.31	135.67	4.000	No	No	2.00
321	21.34	120.39	2.00	1.43	0.61	103.52	1.31	135.57	4.000	No	No	2.00
322	21.39	119.99	2.01	1.44	0.61	103.00	1.31	135.16	4.000	No	No	2.00
323	21.48	118.68	2.01	1.45	0.61	101.52	1.32	133.84	4.000	No	No	2.00
324	21.53	116.39	2.02	1.47	0.61	99.34	1.33	131.86	4.000	No	No	2.00
325	21.64	113.86	2.03	1.47	0.62	96.79	1.34	129.36	4.000	No	No	2.00
326	21.72	111.80	2.02	1.38	0.61	94.83	1.33	125.65	4.000	No	No	2.00
327	21.81	110.79	2.00	1.27	0.61	93.80	1.31	122.48	4.000	No	No	2.00
328	21.89	110.52	1.97	1.15	0.60	93.48	1.28	120.09	4.000	No	No	2.00
329	21.97	110.69	1.96	1.11	0.60	93.44	1.28	119.40	4.000	No	No	2.00
330	22.05	110.81	1.96	1.09	0.60	93.32	1.27	118.94	4.000	No	No	2.00
331	22.12	110.92	1.95	1.07	0.59	93.25	1.27	118.64	4.000	No	No	2.00
332	22.13	110.89	1.95	1.07	0.59	93.20	1.27	118.54	4.000	No	No	2.00
333	22.18	111.98	1.95	1.06	0.59	94.01	1.27	119.22	4.000	No	No	2.00
334	22.22	114.49	1.93	1.04	0.59	96.10	1.26	121.02	4.000	No	No	2.00
335	22.28	118.47	1.91	1.01	0.58	99.41	1.25	123.90	4.000	No	No	2.00
336	22.33	122.55	1.90	0.98	0.58	102.85	1.23	126.89	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	22.38	126.36	1.88	0.96	0.57	106.02	1.22	129.64	4.000	No	No	2.00
338	22.41	129.99	1.86	0.93	0.57	109.11	1.21	132.05	4.000	No	No	2.00
339	22.51	133.16	1.85	0.91	0.56	111.59	1.20	133.67	4.000	No	No	2.00
340	22.56	135.86	1.83	0.88	0.56	113.83	1.18	134.77	4.000	No	No	2.00
341	22.61	137.68	1.82	0.85	0.55	115.29	1.17	135.13	4.000	No	No	2.00
342	22.65	139.23	1.81	0.82	0.55	116.56	1.16	135.07	4.000	No	No	2.00
343	22.71	140.30	1.79	0.80	0.55	117.38	1.15	134.57	4.000	No	No	2.00
344	22.76	141.15	1.78	0.77	0.54	118.01	1.13	133.54	4.000	No	No	2.00
345	22.85	141.55	1.77	0.74	0.54	118.16	1.12	132.33	4.000	No	No	2.00
346	22.89	141.79	1.77	0.72	0.54	118.28	1.11	131.19	4.000	No	No	2.00
347	22.99	141.85	1.76	0.71	0.54	118.07	1.10	130.38	4.000	No	No	2.00
348	23.04	142.19	1.76	0.71	0.54	118.24	1.10	129.89	4.000	No	No	2.00
349	23.12	143.24	1.75	0.70	0.53	118.92	1.09	129.72	4.000	No	No	2.00
350	23.18	145.12	1.75	0.69	0.53	120.36	1.08	129.86	4.000	No	No	2.00
351	23.24	147.55	1.74	0.69	0.53	122.28	1.07	130.48	4.000	No	No	2.00
352	23.33	150.28	1.73	0.68	0.53	124.35	1.05	131.06	4.000	No	No	2.00
353	23.38	152.77	1.73	0.68	0.53	126.31	1.04	131.98	4.000	No	No	2.00
354	23.47	154.92	1.72	0.68	0.53	127.86	1.04	132.70	4.000	No	No	2.00
355	23.52	155.87	1.73	0.70	0.53	128.46	1.05	134.34	4.000	No	No	2.00
356	23.61	155.50	1.74	0.72	0.53	127.76	1.06	136.02	4.000	No	No	2.00
357	23.68	153.41	1.76	0.76	0.54	125.65	1.10	137.67	4.000	No	No	2.00
358	23.76	149.87	1.78	0.79	0.54	122.29	1.13	137.84	4.000	No	No	2.00
359	23.83	145.42	1.80	0.83	0.55	118.19	1.16	136.72	4.000	No	No	2.00
360	23.90	140.77	1.83	0.87	0.56	113.95	1.18	134.56	4.000	No	No	2.00
361	23.97	136.02	1.85	0.91	0.56	109.66	1.20	131.87	4.000	No	No	2.00
362	24.05	130.36	1.88	0.95	0.57	104.58	1.22	128.11	4.000	No	No	2.00
363	24.10	123.83	1.92	1.01	0.58	98.86	1.25	123.41	4.000	No	No	2.00
364	24.19	116.14	1.96	1.08	0.60	92.13	1.28	117.58	4.000	No	No	2.00
365	24.27	109.37	2.00	1.15	0.61	86.22	1.31	112.54	4.000	No	No	2.00
366	24.34	103.31	2.03	1.21	0.62	80.98	1.34	108.37	4.000	No	No	2.00
367	24.43	99.26	2.06	1.26	0.63	77.39	1.37	105.81	4.000	No	No	2.00
368	24.48	95.99	2.09	1.32	0.63	74.54	1.40	104.29	4.000	No	No	2.00
369	24.57	93.77	2.11	1.39	0.64	72.46	1.43	103.72	4.000	No	No	2.00
370	24.62	91.81	2.12	1.39	0.64	70.77	1.45	102.28	4.000	No	No	2.00
371	24.72	90.33	2.12	1.39	0.65	69.37	1.46	101.12	4.000	No	No	2.00
372	24.81	89.08	2.13	1.39	0.65	68.17	1.47	100.03	4.000	No	No	2.00
373	24.86	87.96	2.15	1.46	0.65	67.09	1.50	100.81	4.000	No	No	2.00
374	24.95	85.18	2.18	1.55	0.66	64.60	1.56	100.88	4.000	No	No	2.00
375	25.01	82.83	2.20	1.62	0.67	62.55	1.62	101.05	4.000	No	No	2.00
376	25.02	81.04	2.22	1.66	0.67	61.07	1.66	101.09	4.000	No	No	2.00
377	25.05	81.81	2.21	1.65	0.67	61.63	1.64	101.34	4.000	No	No	2.00
378	25.11	82.33	2.21	1.65	0.67	61.92	1.64	101.59	4.000	No	No	2.00
379	25.15	82.53	2.21	1.66	0.67	61.99	1.64	101.87	4.000	No	No	2.00
380	25.21	81.92	2.22	1.68	0.67	61.38	1.66	101.94	4.000	No	No	2.00
381	25.25	81.07	2.23	1.70	0.68	60.61	1.68	101.90	4.000	No	No	2.00
382	25.30	79.78	2.23	1.71	0.68	59.50	1.70	101.32	4.000	No	No	2.00
383	25.40	78.02	2.24	1.71	0.68	57.95	1.73	100.17	4.000	No	No	2.00
384	25.45	75.14	2.25	1.71	0.68	55.63	1.77	98.38	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	25.52	71.36	2.27	1.71	0.69	52.56	1.83	96.28	4.000	Yes	No	2.00
386	25.60	65.60	2.32	1.78	0.70	47.92	1.99	95.12	4.000	Yes	No	2.00
387	25.66	58.89	2.37	1.90	0.72	42.57	2.24	95.48	4.000	Yes	No	2.00
388	25.74	50.63	2.47	2.18	0.75	36.01	2.77	99.69	4.000	Yes	No	2.00
389	25.80	42.60	2.57	2.54	0.78	29.74	3.54	105.15	4.000	Yes	No	2.00
390	25.88	34.42	2.71	3.09	0.82	23.44	4.79	112.31	4.000	Yes	Yes	2.00
391	25.94	27.91	2.84	3.70	0.86	18.51	6.33	117.20	4.000	Yes	Yes	2.00
392	26.02	22.69	2.98	4.41	1.00	14.10	8.40	118.43	4.000	Yes	Yes	2.00
393	26.09	19.19	3.07	4.99	1.00	11.73	10.09	118.41	4.000	No	Yes	2.00
394	26.17	16.36	3.16	5.56	1.00	9.82	11.90	116.89	4.000	No	Yes	2.00
395	26.23	14.50	3.23	6.07	1.00	8.57	13.49	115.61	4.000	No	Yes	2.00
396	26.29	13.56	3.28	6.45	1.00	7.93	14.54	115.33	4.000	No	Yes	2.00
397	26.37	13.73	3.27	6.48	1.00	8.01	14.49	116.10	4.000	No	Yes	2.00
398	26.46	14.95	3.23	6.22	1.00	8.78	13.45	118.10	4.000	No	Yes	2.00
399	26.55	16.56	3.18	5.88	1.00	9.80	12.25	120.00	4.000	No	Yes	2.00
400	26.60	18.04	3.14	5.67	1.00	10.74	11.37	122.14	4.000	No	Yes	2.00
401	26.70	18.79	3.12	5.69	1.00	11.18	11.11	124.24	4.000	No	Yes	2.00
402	26.78	19.09	3.12	5.78	1.00	11.34	11.11	125.96	4.000	No	Yes	2.00
403	26.87	19.16	3.10	5.28	1.00	11.34	10.61	120.33	4.000	No	Yes	2.00
404	26.94	19.06	3.05	4.41	1.00	11.25	9.74	109.55	4.000	No	Yes	2.00
405	27.03	18.62	3.03	3.81	1.00	10.92	9.23	100.80	4.000	No	Yes	2.00
406	27.13	17.84	3.05	3.86	1.00	10.38	9.61	99.83	4.000	No	Yes	2.00
407	27.18	15.89	3.14	4.63	1.00	9.12	11.41	104.10	4.000	No	Yes	2.00
408	27.27	14.61	3.20	5.14	1.00	8.27	12.75	105.48	4.000	No	Yes	2.00
409	27.32	14.00	3.23	5.49	1.00	7.87	13.55	106.67	4.000	No	Yes	2.00
410	27.37	14.68	3.21	5.36	1.00	8.28	12.99	107.59	4.000	No	Yes	2.00
411	27.41	15.01	3.20	5.40	1.00	8.48	12.84	108.89	4.000	No	Yes	2.00
412	27.46	15.01	3.21	5.56	1.00	8.47	13.04	110.36	4.000	No	Yes	2.00
413	27.51	15.19	3.22	5.71	1.00	8.56	13.12	112.25	4.000	No	Yes	2.00
414	27.61	15.69	3.21	5.85	1.00	8.84	13.00	114.96	4.000	No	Yes	2.00
415	27.66	16.81	3.20	6.07	1.00	9.52	12.66	120.53	4.000	No	Yes	2.00
416	27.73	19.30	3.15	6.09	1.00	11.05	11.59	128.02	4.000	No	Yes	2.00
417	27.80	22.77	3.09	6.16	1.00	13.18	10.46	137.91	4.000	No	Yes	2.00
418	27.88	26.51	3.05	6.33	1.00	15.46	9.62	148.75	4.000	No	Yes	2.00
419	27.96	28.73	3.04	6.73	1.00	16.78	9.46	158.82	4.000	No	Yes	2.00
420	28.04	29.44	3.06	7.42	1.00	17.16	9.86	169.19	4.000	No	Yes	2.00
421	28.12	29.30	3.09	8.01	1.00	17.02	10.34	175.99	4.000	No	Yes	2.00
422	28.18	29.78	3.09	8.32	1.00	17.27	10.47	180.83	4.000	No	Yes	2.00
423	28.27	30.99	3.07	8.13	1.00	17.95	10.11	181.45	4.000	No	Yes	2.00
424	28.32	32.84	3.04	7.81	1.00	19.04	9.54	181.70	4.000	No	Yes	2.00
425	28.42	34.90	3.01	7.49	1.00	20.22	8.98	181.66	4.000	No	Yes	2.00
426	28.47	37.02	2.99	7.35	1.00	21.47	8.57	183.98	4.000	No	Yes	2.00
427	28.61	38.87	2.97	7.32	1.00	22.47	8.32	186.93	4.000	No	Yes	2.00
428	28.67	40.79	2.96	7.36	1.00	23.57	8.10	190.99	4.000	Yes	Yes	2.00
429	28.75	43.62	2.91	7.10	0.88	26.58	7.37	195.90	4.000	Yes	Yes	2.00
430	28.81	49.52	2.83	6.35	0.86	30.58	6.28	192.19	4.000	Yes	Yes	2.00
431	28.90	59.16	2.72	5.28	0.82	37.21	4.89	181.92	4.000	Yes	Yes	2.00
432	29.00	70.68	2.60	4.38	0.79	45.27	3.75	169.71	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	29.05	82.68	2.50	3.72	0.76	53.82	2.95	158.84	4.000	Yes	No	2.00
434	29.10	92.58	2.42	3.28	0.73	60.99	2.48	151.03	4.000	Yes	No	2.00
435	29.15	101.07	2.35	2.88	0.71	67.24	2.13	143.11	4.000	Yes	No	2.00
436	29.24	105.88	2.30	2.58	0.70	70.82	1.92	136.02	4.000	Yes	No	2.00
437	29.29	107.45	2.26	2.31	0.69	72.19	1.78	128.66	4.000	Yes	No	2.00
438	29.37	106.66	2.23	2.12	0.68	71.76	1.71	122.57	4.000	Yes	No	2.00
439	29.43	105.44	2.21	1.94	0.67	71.05	1.64	116.77	4.000	Yes	No	2.00
440	29.53	104.90	2.19	1.79	0.66	70.72	1.59	112.38	4.000	No	No	2.00
441	29.62	104.73	2.17	1.69	0.66	70.61	1.55	109.62	4.000	No	No	2.00
442	29.68	104.75	2.15	1.58	0.65	70.73	1.51	106.89	4.000	No	No	2.00
443	29.80	104.42	2.15	1.54	0.65	70.36	1.50	105.63	4.000	No	No	2.00
444	29.91	103.80	2.15	1.52	0.65	69.74	1.50	104.61	4.000	No	No	2.00
445	30.00	99.10	2.19	1.66	0.66	65.97	1.59	104.86	0.187	No	No	0.61
446	30.07	97.42	2.21	1.72	0.67	64.55	1.63	105.36	0.189	No	No	0.62
447	30.15	96.27	2.22	1.75	0.67	63.56	1.66	105.54	0.189	No	No	0.62
448	30.21	99.04	2.20	1.70	0.67	65.49	1.62	105.77	0.190	No	No	0.62
449	30.26	98.71	2.20	1.71	0.67	65.16	1.62	105.66	0.190	No	No	0.62
450	30.31	97.50	2.21	1.73	0.67	64.21	1.64	105.39	0.189	No	No	0.61
451	30.38	95.52	2.22	1.75	0.67	62.65	1.67	104.86	0.187	No	No	0.61
452	30.45	92.62	2.24	1.79	0.68	60.44	1.72	104.23	0.185	No	No	0.60
453	30.50	89.12	2.26	1.84	0.69	57.84	1.79	103.72	0.184	No	No	0.60
454	30.55	84.94	2.29	1.88	0.69	54.79	1.88	102.88	0.181	No	No	0.59
455	30.64	81.19	2.31	1.91	0.70	52.03	1.96	101.83	0.178	No	No	0.58
456	30.70	77.93	2.32	1.91	0.70	49.71	2.01	100.16	0.173	No	No	0.56
457	30.79	76.04	2.33	1.90	0.71	48.30	2.05	98.96	0.170	No	No	0.55
458	30.84	75.47	2.33	1.88	0.71	47.86	2.05	98.19	0.168	No	No	0.54
459	30.93	76.95	2.32	1.86	0.70	48.79	2.01	98.05	0.168	No	No	0.54
460	30.98	80.15	2.30	1.81	0.70	50.98	1.93	98.14	0.168	No	No	0.54
461	31.05	85.34	2.27	1.76	0.69	54.54	1.81	98.98	0.170	No	No	0.55
462	31.13	91.57	2.24	1.70	0.68	58.82	1.71	100.51	0.174	No	No	0.56
463	31.17	100.46	2.19	1.61	0.66	65.08	1.58	102.97	0.182	No	No	0.58
464	31.27	110.94	2.13	1.49	0.65	72.52	1.47	106.25	0.192	No	No	0.61
465	31.32	123.23	2.06	1.34	0.63	81.52	1.37	111.37	0.208	No	No	0.67
466	31.41	133.45	2.00	1.21	0.61	89.03	1.31	116.56	0.227	No	No	0.73
467	31.46	140.90	1.96	1.11	0.60	94.67	1.28	120.72	0.244	No	No	0.78
468	31.52	144.37	1.93	1.03	0.59	97.40	1.26	122.24	0.250	No	No	0.80
469	31.61	145.01	1.91	0.97	0.58	97.95	1.24	121.83	0.248	No	No	0.79
470	31.66	142.15	1.91	0.95	0.58	95.90	1.24	119.20	0.238	No	No	0.76
471	31.75	136.69	1.93	0.97	0.59	91.66	1.26	115.29	0.223	No	No	0.71
472	31.80	129.14	1.98	1.06	0.60	85.76	1.29	110.68	0.206	No	No	0.66
473	31.90	122.00	2.02	1.16	0.62	80.16	1.33	106.52	0.192	No	No	0.61
474	31.94	116.84	2.06	1.24	0.63	76.18	1.37	104.07	0.185	No	No	0.59
475	32.04	116.03	2.07	1.27	0.63	75.33	1.38	104.00	0.185	No	No	0.59
476	32.09	119.17	2.08	1.34	0.63	77.25	1.39	107.23	0.195	No	No	0.62
477	32.20	118.70	2.11	1.46	0.64	76.38	1.43	109.06	0.201	No	No	0.63
478	32.24	117.72	2.13	1.56	0.65	75.37	1.47	110.44	0.205	No	No	0.65
479	32.28	114.69	2.15	1.64	0.65	73.02	1.51	110.26	0.205	No	No	0.65
480	32.29	116.70	2.14	1.62	0.65	74.43	1.49	111.09	0.207	No	No	0.66

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	32.30	118.93	2.13	1.60	0.65	75.98	1.47	112.06	0.211	No	No	0.67
482	32.40	120.51	2.13	1.59	0.65	76.91	1.47	112.71	0.213	No	No	0.67
483	32.45	120.48	2.13	1.61	0.65	76.77	1.47	112.95	0.214	No	No	0.67
484	32.55	119.13	2.14	1.63	0.65	75.61	1.49	112.51	0.212	No	No	0.67
485	32.59	118.33	2.15	1.66	0.65	74.91	1.50	112.50	0.212	No	No	0.67
486	32.69	118.13	2.15	1.68	0.65	74.54	1.51	112.79	0.213	No	No	0.67
487	32.76	118.09	2.16	1.72	0.66	74.31	1.53	113.51	0.216	No	No	0.68
488	32.84	118.40	2.17	1.75	0.66	74.31	1.54	114.35	0.219	No	No	0.69
489	32.90	119.00	2.17	1.77	0.66	74.55	1.55	115.19	0.222	No	No	0.70
490	32.98	119.95	2.17	1.78	0.66	75.02	1.54	115.83	0.225	No	No	0.70
491	33.06	121.02	2.17	1.78	0.66	75.61	1.54	116.33	0.226	No	No	0.71
492	33.12	122.10	2.16	1.78	0.66	76.23	1.53	116.77	0.228	No	No	0.71
493	33.22	122.84	2.16	1.78	0.66	76.56	1.53	117.03	0.229	No	No	0.72
494	33.31	123.21	2.16	1.78	0.66	76.64	1.53	117.14	0.229	No	No	0.72
495	33.37	123.28	2.16	1.78	0.66	76.59	1.53	117.11	0.229	No	No	0.72
496	33.46	123.28	2.16	1.78	0.66	76.41	1.53	117.00	0.229	No	No	0.71
497	33.55	123.18	2.17	1.79	0.66	76.17	1.54	117.00	0.229	No	No	0.71
498	33.65	122.98	2.17	1.80	0.66	75.83	1.54	117.07	0.229	No	No	0.71
499	33.70	122.57	2.17	1.82	0.66	75.42	1.55	117.18	0.230	No	No	0.71
500	33.79	122.03	2.18	1.84	0.66	74.86	1.56	117.10	0.229	No	No	0.71
501	33.89	121.09	2.18	1.85	0.66	74.04	1.58	116.76	0.228	No	No	0.71
502	33.99	119.77	2.19	1.86	0.67	72.98	1.59	116.20	0.226	No	No	0.70
503	34.04	117.79	2.20	1.88	0.67	71.55	1.61	115.43	0.223	No	No	0.69
504	34.13	115.49	2.21	1.89	0.67	69.85	1.64	114.59	0.220	No	No	0.68
505	34.23	112.70	2.22	1.92	0.68	67.80	1.68	113.76	0.217	No	No	0.67
506	34.32	110.27	2.24	1.95	0.68	66.01	1.71	113.20	0.215	No	No	0.66
507	34.37	108.22	2.25	1.98	0.68	64.55	1.75	112.84	0.214	No	No	0.66
508	34.47	106.60	2.26	2.00	0.69	63.31	1.78	112.69	0.213	No	No	0.66
509	34.55	103.47	2.28	2.07	0.69	61.05	1.85	112.96	4.000	Yes	No	2.00
510	34.63	96.66	2.33	2.24	0.71	56.31	2.04	114.64	4.000	Yes	No	2.00
511	34.73	86.37	2.40	2.51	0.73	49.33	2.40	118.21	4.000	Yes	No	2.00
512	34.80	72.76	2.51	2.91	0.76	40.42	3.06	123.59	4.000	Yes	No	2.00
513	34.90	60.46	2.62	3.30	0.79	32.62	3.90	127.28	4.000	Yes	Yes	2.00
514	35.00	54.92	2.64	3.21	0.80	29.29	4.16	121.79	3.600	No	Yes	2.00
515	35.12	50.37	2.67	3.15	0.81	26.54	4.42	117.31	3.600	No	Yes	2.00
516	35.20	52.86	2.63	2.87	0.80	28.11	3.99	112.19	3.600	No	Yes	2.00
517	35.33	53.65	2.63	2.95	0.80	28.43	4.02	114.42	4.000	Yes	Yes	2.00
518	35.41	63.41	2.53	2.60	0.77	34.44	3.20	110.34	4.000	Yes	No	2.00
519	35.44	68.58	2.48	2.43	0.75	37.68	2.87	108.02	4.000	Yes	No	2.00
520	35.48	76.82	2.41	2.17	0.73	42.96	2.42	103.82	4.000	Yes	No	2.00
521	35.57	84.09	2.35	1.98	0.71	47.63	2.12	101.05	4.000	Yes	No	2.00
522	35.62	98.70	2.24	1.69	0.68	57.30	1.73	98.99	4.000	Yes	No	2.00
523	35.67	115.40	2.14	1.46	0.65	68.51	1.49	102.07	4.000	Yes	No	2.00
524	35.71	137.52	2.04	1.30	0.62	83.52	1.35	112.52	4.000	Yes	No	2.00
525	35.82	159.89	1.96	1.19	0.60	98.71	1.28	126.36	4.000	Yes	No	2.00
526	35.86	185.11	1.89	1.12	0.58	116.11	1.23	143.07	4.000	Yes	No	2.00
527	35.93	207.72	1.84	1.06	0.56	131.80	1.19	156.85	4.000	Yes	No	2.00
528	36.01	225.38	1.80	1.04	0.55	144.00	1.16	166.33	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	36.06	235.57	1.79	1.04	0.54	150.92	1.14	171.69	4.000	Yes	No	2.00
530	36.12	240.67	1.78	1.05	0.54	154.12	1.13	174.89	0.578	No	No	1.75
531	36.18	245.05	1.79	1.08	0.54	156.73	1.14	178.20	0.606	No	No	1.84
532	36.25	248.69	1.79	1.10	0.54	158.84	1.14	180.98	0.631	No	No	1.91
533	36.30	251.52	1.80	1.14	0.55	160.26	1.15	184.12	0.661	No	No	2.00
534	36.39	252.83	1.81	1.17	0.55	160.54	1.16	185.99	0.678	No	No	2.00
535	36.44	253.07	1.82	1.21	0.55	160.15	1.17	187.57	0.694	No	No	2.00
536	36.53	251.49	1.83	1.25	0.56	158.45	1.18	187.51	0.693	No	No	2.00
537	36.59	248.39	1.86	1.34	0.57	155.45	1.21	187.43	0.692	No	No	2.00
538	36.68	243.47	1.87	1.37	0.57	151.62	1.22	184.49	0.664	No	No	2.00
539	36.75	238.34	1.88	1.38	0.57	147.93	1.22	180.99	0.631	No	No	1.91
540	36.83	232.04	1.88	1.34	0.57	143.78	1.22	175.91	0.586	No	No	1.77
541	36.90	225.27	1.89	1.35	0.58	138.95	1.23	171.34	0.548	No	No	1.65
542	36.97	217.18	1.92	1.39	0.58	133.11	1.25	166.05	0.506	No	No	1.53
543	37.02	201.72	1.96	1.49	0.60	122.19	1.28	156.23	0.435	No	No	1.31
544	37.04	193.70	1.99	1.53	0.60	116.64	1.30	151.13	0.401	No	No	1.21
545	37.08	188.61	2.00	1.54	0.61	113.19	1.30	147.61	0.379	No	No	1.14
546	37.17	191.78	1.97	1.46	0.60	115.46	1.29	148.65	0.385	No	No	1.16
547	37.27	187.30	1.98	1.44	0.60	112.45	1.29	145.04	0.364	No	No	1.09
548	37.37	181.37	1.99	1.43	0.60	108.42	1.30	140.68	0.339	No	No	1.02
549	37.42	177.21	1.99	1.39	0.60	105.83	1.30	137.22	0.320	No	No	0.96
550	37.51	175.89	1.97	1.32	0.60	105.19	1.29	135.25	0.310	No	No	0.93
551	37.58	176.97	1.95	1.22	0.59	106.34	1.27	134.76	0.308	No	No	0.92
552	37.66	179.01	1.92	1.13	0.58	108.07	1.25	135.08	0.309	No	No	0.93
553	37.76	182.58	1.89	1.05	0.57	110.83	1.23	136.26	0.315	No	No	0.95
554	37.85	186.08	1.86	0.97	0.57	113.57	1.21	137.18	0.320	No	No	0.96
555	37.93	189.62	1.84	0.92	0.56	116.22	1.19	138.14	0.325	No	No	0.97
556	38.04	192.25	1.82	0.89	0.55	117.99	1.18	138.80	0.329	No	No	0.98
557	38.13	193.87	1.82	0.88	0.55	118.97	1.17	139.30	0.331	No	No	0.99
558	38.18	193.57	1.82	0.88	0.55	118.63	1.17	139.16	0.331	No	No	0.99
559	38.28	191.24	1.84	0.92	0.56	116.58	1.19	138.51	0.327	No	No	0.98
560	38.37	187.40	1.86	0.97	0.57	113.37	1.21	137.08	0.320	No	No	0.95
561	38.47	183.55	1.89	1.06	0.58	109.99	1.23	135.63	0.312	No	No	0.93
562	38.57	180.39	1.92	1.13	0.58	107.19	1.25	134.14	0.304	No	No	0.91
563	38.62	176.78	1.95	1.21	0.59	104.23	1.27	132.48	0.296	No	No	0.88
564	38.72	167.48	2.00	1.33	0.61	97.43	1.31	127.27	0.272	No	No	0.81
565	38.78	160.21	2.04	1.42	0.62	92.19	1.34	123.72	0.256	No	No	0.76
566	38.81	155.32	2.06	1.49	0.63	88.77	1.37	121.63	0.247	No	No	0.74
567	38.86	155.19	2.07	1.50	0.63	88.54	1.37	121.68	0.248	No	No	0.74
568	38.91	152.02	2.08	1.55	0.63	86.27	1.40	120.51	0.243	No	No	0.72
569	38.95	145.92	2.12	1.64	0.64	82.06	1.44	118.55	0.235	No	No	0.70
570	39.05	139.55	2.15	1.74	0.65	77.66	1.51	116.91	0.229	No	No	0.68
571	39.09	132.37	2.19	1.84	0.66	72.88	1.59	115.64	0.224	No	No	0.67
572	39.14	125.06	2.23	1.95	0.68	68.10	1.69	114.83	0.221	No	No	0.66
573	39.24	118.19	2.26	2.05	0.69	63.61	1.80	114.32	0.219	No	No	0.65
574	39.29	112.16	2.30	2.14	0.70	59.80	1.91	114.03	0.218	No	No	0.65
575	39.39	108.48	2.32	2.20	0.70	57.39	1.99	114.16	0.218	No	No	0.65
576	39.43	109.15	2.31	2.19	0.70	57.74	1.98	114.28	0.219	No	No	0.65

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	39.53	115.02	2.28	2.10	0.69	61.25	1.86	113.89	0.217	No	No	0.65
578	39.57	124.17	2.23	1.94	0.68	67.01	1.69	113.55	0.216	No	No	0.64
579	39.68	130.64	2.19	1.83	0.67	71.04	1.60	113.69	0.217	No	No	0.64
580	39.73	131.95	2.19	1.80	0.66	71.83	1.58	113.53	0.216	No	No	0.64
581	39.81	129.33	2.20	1.81	0.67	70.10	1.60	112.48	0.212	No	No	0.63
582	39.89	126.37	2.19	1.75	0.67	68.39	1.60	109.51	0.202	No	No	0.60
583	39.96	125.26	2.18	1.63	0.66	68.01	1.56	105.89	0.190	No	No	0.56
584	40.06	124.52	2.16	1.53	0.66	67.75	1.52	103.14	0.182	No	No	0.54
585	40.15	122.70	2.17	1.55	0.66	66.50	1.54	102.38	0.180	No	No	0.53
586	40.20	114.41	2.22	1.70	0.67	61.03	1.67	102.07	0.179	No	No	0.53
587	40.24	108.56	2.26	1.81	0.69	57.23	1.79	102.62	0.181	No	No	0.53
588	40.26	104.17	2.29	1.90	0.70	54.45	1.90	103.22	0.182	No	No	0.54
589	40.27	107.91	2.27	1.85	0.69	56.72	1.82	103.36	0.183	No	No	0.54
590	40.37	109.77	2.26	1.84	0.69	57.73	1.80	103.81	0.184	No	No	0.55
591	40.42	111.64	2.26	1.85	0.69	58.75	1.78	104.71	0.187	No	No	0.55
592	40.52	112.38	2.26	1.87	0.69	59.02	1.79	105.44	0.189	No	No	0.56
593	40.56	115.27	2.25	1.87	0.68	60.66	1.76	106.63	0.193	No	No	0.57
594	40.66	122.24	2.22	1.81	0.67	64.78	1.67	108.06	0.197	No	No	0.58
595	40.70	131.54	2.18	1.74	0.66	70.42	1.57	110.67	0.206	No	No	0.61
596	40.75	142.59	2.14	1.67	0.65	77.15	1.49	114.79	0.221	No	No	0.65
597	40.85	153.40	2.11	1.63	0.64	83.66	1.43	119.75	0.240	No	No	0.71
598	40.91	164.05	2.08	1.59	0.63	90.16	1.39	125.10	0.262	No	No	0.77
599	40.96	174.69	2.04	1.53	0.62	96.83	1.35	130.56	0.287	No	No	0.85
600	41.04	184.27	2.01	1.47	0.61	102.87	1.32	135.59	0.312	No	No	0.92
601	41.09	193.94	1.98	1.41	0.60	109.10	1.29	141.03	0.341	No	No	1.01
602	41.18	201.90	1.96	1.36	0.60	114.17	1.28	145.57	0.367	No	No	1.08
603	41.23	207.97	1.94	1.33	0.59	118.08	1.26	149.12	0.388	No	No	1.15
604	41.29	211.58	1.93	1.31	0.59	120.37	1.26	151.17	0.401	No	No	1.19
605	41.38	212.76	1.93	1.30	0.59	120.98	1.25	151.67	0.404	No	No	1.19
606	41.42	212.09	1.93	1.31	0.59	120.40	1.26	151.21	0.402	No	No	1.19
607	41.52	210.03	1.94	1.33	0.59	118.76	1.26	149.86	0.393	No	No	1.16
608	41.57	207.27	1.95	1.36	0.59	116.72	1.27	148.26	0.383	No	No	1.13
609	41.62	204.91	1.96	1.40	0.60	114.93	1.28	146.93	0.375	No	No	1.11
610	41.71	203.13	1.97	1.43	0.60	113.45	1.29	145.89	0.369	No	No	1.09
611	41.76	202.15	1.98	1.45	0.60	112.60	1.29	145.43	0.366	No	No	1.08
612	41.84	201.65	1.99	1.47	0.60	111.98	1.30	145.17	0.364	No	No	1.08
613	41.91	201.54	1.99	1.50	0.61	111.64	1.30	145.22	0.365	No	No	1.08
614	41.95	201.75	2.00	1.52	0.61	111.52	1.31	145.53	0.367	No	No	1.08
615	42.01	202.52	2.00	1.56	0.61	111.63	1.31	146.36	0.372	No	No	1.10
616	42.10	203.57	2.01	1.60	0.61	111.82	1.32	147.40	0.378	No	No	1.11
617	42.15	204.98	2.02	1.66	0.61	112.23	1.33	148.90	0.387	No	No	1.14
618	42.24	206.03	2.03	1.70	0.62	112.44	1.33	149.94	0.394	No	No	1.16
619	42.28	206.46	2.03	1.71	0.62	112.53	1.34	150.31	0.396	No	No	1.17
620	42.39	206.26	2.03	1.70	0.62	112.27	1.33	149.81	0.393	No	No	1.16
621	42.43	206.08	2.02	1.67	0.62	112.28	1.33	149.14	0.389	No	No	1.14
622	42.50	206.11	2.01	1.62	0.61	112.45	1.32	148.36	0.384	No	No	1.13
623	42.58	206.28	2.00	1.56	0.61	112.80	1.31	147.54	0.379	No	No	1.12
624	42.65	198.95	2.01	1.55	0.61	108.28	1.32	142.73	0.350	No	No	1.03

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	42.70	195.88	2.02	1.54	0.61	106.39	1.32	140.58	0.338	No	No	1.00
626	42.73	193.72	2.02	1.54	0.61	105.08	1.32	139.14	0.331	No	No	0.97
627	42.77	200.19	1.99	1.47	0.61	109.31	1.30	142.31	0.348	No	No	1.02
628	42.82	203.83	1.98	1.43	0.60	111.68	1.29	144.06	0.358	No	No	1.05
629	42.87	209.12	1.96	1.39	0.60	115.10	1.28	146.92	0.375	No	No	1.10
630	42.91	215.46	1.94	1.35	0.59	119.14	1.26	150.57	0.397	No	No	1.17
631	42.97	221.76	1.92	1.32	0.59	123.09	1.25	154.27	0.421	No	No	1.24
632	43.02	226.82	1.92	1.32	0.58	126.14	1.25	157.35	0.442	No	No	1.30
633	43.06	230.49	1.91	1.33	0.58	128.19	1.25	159.72	0.459	No	No	1.35
634	43.11	234.33	1.91	1.34	0.58	130.34	1.24	162.21	0.477	No	No	1.40
635	43.17	237.93	1.91	1.35	0.58	132.40	1.24	164.40	0.493	No	No	1.45
636	43.21	242.21	1.90	1.33	0.58	135.09	1.23	166.83	0.512	No	No	1.51
637	43.29	246.19	1.89	1.30	0.57	137.59	1.23	168.85	0.528	No	No	1.55
638	43.34	250.53	1.87	1.28	0.57	140.43	1.22	171.05	0.545	No	No	1.61
639	43.39	254.11	1.86	1.25	0.57	142.76	1.21	172.71	0.559	No	No	1.65
640	43.45	256.87	1.85	1.22	0.56	144.64	1.20	173.74	0.568	No	No	1.67
641	43.51	258.25	1.84	1.18	0.56	145.84	1.19	173.50	0.566	No	No	1.66
642	43.59	258.59	1.82	1.14	0.56	146.35	1.18	172.47	0.557	No	No	1.64
643	43.64	259.19	1.80	1.07	0.55	147.38	1.16	170.73	0.543	No	No	1.60
644	43.70	259.29	1.78	1.01	0.54	148.12	1.13	168.10	0.522	No	No	1.54
645	43.78	258.35	1.77	0.96	0.54	147.98	1.12	165.08	0.498	No	No	1.47
646	43.88	255.18	1.77	0.96	0.54	145.77	1.12	163.55	0.487	No	No	1.43
647	43.94	244.77	1.82	1.04	0.55	138.10	1.17	161.52	0.472	No	No	1.39
648	44.04	234.93	1.86	1.12	0.57	130.84	1.21	157.74	0.445	No	No	1.31
649	44.07	225.87	1.89	1.21	0.58	124.41	1.23	153.31	0.415	No	No	1.22
650	44.12	223.58	1.90	1.23	0.58	122.68	1.24	152.08	0.407	No	No	1.20
651	44.16	221.15	1.91	1.25	0.58	120.94	1.25	150.70	0.398	No	No	1.17
652	44.21	218.05	1.93	1.28	0.59	118.76	1.25	148.86	0.387	No	No	1.14
653	44.26	214.65	1.94	1.30	0.59	116.39	1.26	146.86	0.375	No	No	1.10
654	44.31	210.81	1.95	1.34	0.59	113.73	1.27	144.63	0.361	No	No	1.06
655	44.35	206.97	1.97	1.37	0.60	111.11	1.28	142.44	0.349	No	No	1.03
656	44.40	203.26	1.98	1.40	0.60	108.60	1.29	140.32	0.337	No	No	0.99
657	44.45	200.16	1.99	1.43	0.61	106.49	1.30	138.56	0.327	No	No	0.96
658	44.50	197.83	2.00	1.45	0.61	104.91	1.31	137.24	0.320	No	No	0.94
659	44.54	195.81	2.01	1.47	0.61	103.53	1.32	136.15	0.315	No	No	0.93
660	44.60	193.46	2.02	1.49	0.61	101.86	1.32	134.97	0.309	No	No	0.91
661	44.64	190.96	2.03	1.53	0.62	100.11	1.34	133.85	0.303	No	No	0.89
662	44.69	188.57	2.05	1.57	0.62	98.42	1.35	132.85	0.298	No	No	0.88
663	44.74	187.78	2.05	1.59	0.62	97.76	1.36	132.59	0.297	No	No	0.87
664	44.79	187.17	2.06	1.60	0.62	97.27	1.36	132.34	0.296	No	No	0.87
665	44.83	187.71	2.05	1.60	0.62	97.52	1.36	132.53	0.296	No	No	0.87
666	44.88	188.84	2.05	1.59	0.62	98.15	1.35	132.96	0.299	No	No	0.88
667	44.93	191.20	2.04	1.57	0.62	99.52	1.35	134.02	0.304	No	No	0.89
668	44.98	193.69	2.03	1.55	0.62	100.99	1.34	135.20	0.310	No	No	0.91
669	45.03	195.31	2.03	1.54	0.62	101.90	1.33	135.95	0.314	No	No	0.92
670	45.08	196.49	2.03	1.54	0.62	102.54	1.33	136.45	0.316	No	No	0.93
671	45.16	197.53	2.02	1.52	0.62	103.08	1.33	136.81	0.318	No	No	0.94
672	45.19	198.24	2.02	1.50	0.61	103.58	1.32	136.91	0.319	No	No	0.94

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	45.27	198.44	2.01	1.47	0.61	103.76	1.32	136.53	0.317	No	No	0.93
674	45.32	197.56	2.00	1.44	0.61	103.38	1.31	135.53	0.312	No	No	0.92
675	45.37	195.58	2.00	1.39	0.61	102.45	1.31	133.73	0.302	No	No	0.89
676	45.45	192.44	1.99	1.35	0.61	100.80	1.30	131.17	0.290	No	No	0.85
677	45.51	187.22	1.99	1.31	0.61	97.91	1.30	127.52	0.273	No	No	0.80
678	45.56	180.52	2.01	1.31	0.61	93.92	1.31	123.37	4.000	Yes	No	2.00
679	45.61	169.84	2.04	1.36	0.62	87.34	1.35	117.60	4.000	Yes	No	2.00
680	45.69	156.32	2.10	1.48	0.64	78.89	1.42	111.79	4.000	Yes	No	2.00
681	45.75	137.42	2.20	1.74	0.67	67.17	1.61	108.19	4.000	Yes	No	2.00
682	45.81	115.31	2.30	1.96	0.70	54.45	1.93	105.04	4.000	Yes	No	2.00
683	45.89	93.28	2.42	2.23	0.73	42.25	2.49	105.10	4.000	Yes	No	2.00
684	45.94	73.36	2.54	2.43	0.77	31.83	3.26	103.73	4.000	Yes	No	2.00
685	46.04	59.21	2.67	2.85	0.81	24.44	4.42	108.05	4.000	Yes	Yes	2.00
686	46.08	46.61	2.83	3.46	0.86	18.15	6.18	112.07	4.000	Yes	Yes	2.00
687	46.15	39.94	2.97	3.96	1.00	13.37	8.22	109.85	4.000	Yes	Yes	2.00
688	46.17	36.10	3.03	4.33	1.00	11.98	9.26	110.89	3.600	No	Yes	2.00
689	46.18	36.17	3.02	4.27	1.00	12.00	9.18	110.17	3.600	No	Yes	2.00
690	46.23	36.48	3.01	4.17	1.00	12.10	9.03	109.18	3.600	No	Yes	2.00
691	46.27	37.18	3.00	4.00	1.00	12.34	8.72	107.58	3.600	No	Yes	2.00
692	46.32	38.64	2.96	3.74	1.00	12.85	8.20	105.33	3.600	No	Yes	2.00
693	46.41	40.63	2.89	3.49	0.87	15.29	7.01	107.19	3.600	No	Yes	2.00
694	46.47	43.16	2.85	3.30	0.86	16.49	6.44	106.19	3.600	No	Yes	2.00
695	46.52	45.45	2.82	3.23	0.85	17.54	6.09	106.89	3.600	No	Yes	2.00
696	46.56	47.57	2.81	3.31	0.85	18.46	5.95	109.81	3.600	No	Yes	2.00
697	46.65	49.42	2.80	3.44	0.85	19.21	5.91	113.60	3.600	No	Yes	2.00
698	46.71	51.52	2.80	3.58	0.85	20.07	5.86	117.68	3.600	No	Yes	2.00
699	46.76	54.41	2.78	3.59	0.84	21.37	5.62	120.04	3.600	No	Yes	2.00
700	46.85	58.19	2.75	3.48	0.83	23.13	5.21	120.43	3.600	No	Yes	2.00
701	46.90	63.28	2.69	3.26	0.82	25.63	4.63	118.71	3.600	No	Yes	2.00
702	46.99	67.89	2.65	3.04	0.80	27.93	4.16	116.19	3.600	No	Yes	2.00
703	47.04	70.35	2.62	2.93	0.79	29.16	3.93	114.63	3.600	No	Yes	2.00
704	47.10	69.50	2.63	2.95	0.80	28.71	4.00	114.71	3.600	No	Yes	2.00
705	47.16	65.45	2.67	3.09	0.81	26.63	4.36	116.10	3.600	No	Yes	2.00
706	47.23	59.62	2.72	3.30	0.82	23.71	4.94	117.23	3.600	No	Yes	2.00
707	47.30	51.46	2.81	3.62	0.85	19.76	5.97	117.96	3.600	No	Yes	2.00
708	47.38	42.76	2.96	4.09	1.00	13.97	8.12	113.48	3.600	No	Yes	2.00
709	47.43	34.23	3.08	4.68	1.00	10.97	10.19	111.84	3.600	No	Yes	2.00
710	47.52	28.17	3.17	4.93	1.00	8.83	11.99	105.92	3.600	No	Yes	2.00
711	47.59	23.92	3.20	4.34	1.00	7.34	12.70	93.23	3.600	No	Yes	2.00
712	47.66	21.40	3.20	3.59	1.00	6.45	12.70	81.89	3.600	No	Yes	2.00
713	47.77	19.71	3.20	3.13	1.00	5.85	12.77	74.67	3.600	No	Yes	2.00
714	47.82	18.77	3.24	3.41	1.00	5.51	13.75	75.76	3.600	No	Yes	2.00
715	47.91	18.38	3.26	3.59	1.00	5.37	14.28	76.63	3.600	No	Yes	2.00
716	47.93	17.68	3.30	3.86	1.00	5.12	15.17	77.65	3.600	No	Yes	2.00
717	47.97	17.78	3.30	3.92	1.00	5.15	15.21	78.37	3.600	No	Yes	2.00
718	48.02	17.86	3.31	4.05	1.00	5.17	15.38	79.56	3.600	No	Yes	2.00
719	48.07	18.51	3.30	4.11	1.00	5.39	15.07	81.21	3.600	No	Yes	2.00
720	48.12	18.61	3.31	4.43	1.00	5.42	15.51	84.04	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	48.19	18.71	3.33	4.73	1.00	5.44	15.90	86.54	3.600	No	Yes	2.00
722	48.23	18.91	3.33	4.96	1.00	5.51	16.11	88.74	3.600	No	Yes	2.00
723	48.31	19.15	3.33	5.05	1.00	5.58	16.11	89.88	3.600	No	Yes	2.00
724	48.35	19.35	3.33	5.13	1.00	5.64	16.11	90.92	3.600	No	Yes	2.00
725	48.40	19.25	3.34	5.27	1.00	5.60	16.37	91.72	3.600	No	Yes	2.00
726	48.45	18.81	3.36	5.50	1.00	5.45	16.96	92.39	3.600	No	Yes	2.00
727	48.50	18.07	3.40	5.83	1.00	5.19	17.92	92.93	3.600	No	Yes	2.00
728	48.55	17.80	3.41	6.00	1.00	5.09	18.35	93.37	3.600	No	Yes	2.00
729	48.59	17.64	3.42	6.20	1.00	5.03	18.75	94.24	3.600	No	Yes	2.00
730	48.67	17.87	3.42	6.18	1.00	5.10	18.56	94.62	3.600	No	Yes	2.00
731	48.73	17.84	3.42	6.16	1.00	5.08	18.58	94.36	3.600	No	Yes	2.00
732	48.78	17.97	3.40	5.89	1.00	5.12	18.13	92.80	3.600	No	Yes	2.00
733	48.83	17.97	3.39	5.58	1.00	5.11	17.74	90.68	3.600	No	Yes	2.00
734	48.91	17.94	3.38	5.27	1.00	5.09	17.35	88.35	3.600	No	Yes	2.00
735	48.98	17.84	3.37	5.04	1.00	5.05	17.10	86.35	3.600	No	Yes	2.00
736	49.03	17.74	3.37	4.91	1.00	5.01	17.00	85.19	3.600	No	Yes	2.00
737	49.12	17.68	3.35	4.63	1.00	4.98	16.65	82.90	3.600	No	Yes	2.00
738	49.17	17.75	3.33	4.17	1.00	5.00	15.91	79.48	3.600	No	Yes	2.00
739	49.27	18.02	3.30	3.75	1.00	5.08	15.07	76.51	3.600	No	Yes	2.00
740	49.31	18.56	3.28	3.65	1.00	5.25	14.57	76.55	3.600	No	Yes	2.00
741	49.38	19.20	3.27	3.79	1.00	5.46	14.44	78.88	3.600	No	Yes	2.00
742	49.45	19.70	3.27	3.95	1.00	5.62	14.44	81.15	3.600	No	Yes	2.00
743	49.51	19.00	3.31	4.33	1.00	5.38	15.44	83.00	3.600	No	Yes	2.00
744	49.54	19.44	3.30	4.37	1.00	5.52	15.24	84.13	3.600	No	Yes	2.00
745	49.59	20.18	3.28	4.25	1.00	5.76	14.65	84.45	3.600	No	Yes	2.00
746	49.64	21.53	3.23	3.89	1.00	6.21	13.47	83.63	3.600	No	Yes	2.00
747	49.73	21.20	3.24	3.89	1.00	6.09	13.64	83.01	3.600	No	Yes	2.00
748	49.83	20.02	3.27	4.07	1.00	5.68	14.52	82.47	3.600	No	Yes	2.00
749	49.92	18.88	3.31	4.30	1.00	5.29	15.55	82.19	3.600	No	Yes	2.00
750	49.98	17.86	3.35	4.49	1.00	4.94	16.51	81.62	3.600	No	Yes	2.00
751	50.07	17.33	3.37	4.57	1.00	4.75	17.04	81.01	3.600	No	Yes	2.00
752	50.16	16.99	3.38	4.61	1.00	4.63	17.38	80.51	3.600	No	Yes	2.00
753	50.24	16.69	3.39	4.65	1.00	4.52	17.70	80.06	3.600	No	Yes	2.00
754	50.32	16.46	3.40	4.71	1.00	4.44	17.99	79.87	3.600	No	Yes	2.00
755	50.41	16.32	3.41	4.79	1.00	4.39	18.25	80.02	3.600	No	Yes	2.00
756	50.50	16.36	3.41	4.79	1.00	4.39	18.25	80.09	3.600	No	Yes	2.00
757	50.56	16.26	3.41	4.73	1.00	4.35	18.25	79.36	3.600	No	Yes	2.00
758	50.66	16.09	3.41	4.63	1.00	4.28	18.27	78.27	3.600	No	Yes	2.00
759	50.74	15.92	3.41	4.59	1.00	4.22	18.37	77.53	3.600	No	Yes	2.00
760	50.84	15.85	3.43	4.94	1.00	4.19	19.00	79.62	3.600	No	Yes	2.00
761	50.93	15.95	3.46	5.57	1.00	4.21	19.91	83.88	3.600	No	Yes	2.00
762	50.98	16.77	3.48	6.56	1.00	4.47	20.59	92.08	3.600	No	Yes	2.00
763	51.08	19.60	3.43	7.08	1.00	5.39	19.08	102.75	3.600	No	Yes	2.00
764	51.17	24.45	3.34	6.97	1.00	6.95	16.30	113.31	3.600	No	Yes	2.00
765	51.24	30.11	3.25	6.75	1.00	8.78	13.98	122.80	3.600	No	Yes	2.00
766	51.34	33.65	3.21	6.76	1.00	9.91	13.03	129.12	3.600	No	Yes	2.00
767	51.41	34.16	3.18	6.01	1.00	10.06	12.19	122.59	3.600	No	Yes	2.00
768	51.51	32.81	3.17	5.54	1.00	9.60	12.05	115.66	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	51.58	31.20	3.16	4.92	1.00	9.06	11.80	106.93	3.600	No	Yes	2.00
770	51.68	29.95	3.20	5.43	1.00	8.64	12.73	109.98	3.600	No	Yes	2.00
771	51.79	27.39	3.26	5.93	1.00	7.80	14.12	110.16	3.600	No	Yes	2.00
772	51.82	25.87	3.30	6.27	1.00	7.31	15.07	110.15	3.600	No	Yes	2.00
773	51.85	24.39	3.34	6.78	1.00	6.83	16.27	111.07	3.600	No	Yes	2.00
774	51.91	25.00	3.34	6.90	1.00	7.01	16.14	113.23	3.600	No	Yes	2.00
775	52.00	24.87	3.36	7.36	1.00	6.96	16.71	116.25	3.600	No	Yes	2.00
776	52.05	27.06	3.31	7.10	1.00	7.65	15.54	118.92	3.600	No	Yes	2.00
777	52.10	31.78	3.21	6.10	1.00	9.15	13.00	118.95	3.600	No	Yes	2.00
778	52.19	38.49	3.08	4.92	1.00	11.27	10.28	115.81	3.600	No	Yes	2.00
779	52.28	44.04	2.99	4.15	1.00	13.02	8.58	111.69	3.600	No	Yes	2.00
780	52.34	46.37	2.95	3.85	1.00	13.74	7.96	109.32	3.600	No	Yes	2.00
781	52.42	46.09	2.96	3.90	1.00	13.63	8.05	109.66	3.600	No	Yes	2.00
782	52.48	44.34	2.98	4.10	1.00	13.05	8.50	111.03	3.600	No	Yes	2.00
783	52.57	42.32	3.01	4.26	1.00	12.39	8.98	111.27	3.600	No	Yes	2.00
784	52.62	40.26	3.03	4.31	1.00	11.73	9.37	109.88	3.600	No	Yes	2.00
785	52.69	38.51	3.05	4.22	1.00	11.16	9.58	106.89	3.600	No	Yes	2.00
786	52.77	36.89	3.06	4.17	1.00	10.63	9.83	104.50	3.600	No	Yes	2.00
787	52.87	35.55	3.08	4.24	1.00	10.19	10.19	103.83	3.600	No	Yes	2.00
788	52.91	34.07	3.10	4.28	1.00	9.71	10.56	102.56	3.600	No	Yes	2.00
789	53.01	32.55	3.12	4.42	1.00	9.21	11.08	102.13	3.600	No	Yes	2.00
790	53.10	32.18	3.14	4.56	1.00	9.08	11.35	103.11	3.600	No	Yes	2.00
791	53.16	34.04	3.15	5.28	1.00	9.65	11.74	113.26	3.600	No	Yes	2.00
792	53.25	38.69	3.13	5.64	1.00	11.08	11.13	123.32	3.600	No	Yes	2.00
793	53.29	44.28	3.10	6.15	1.00	12.82	10.63	136.25	3.600	No	Yes	2.00
794	53.38	48.90	3.07	6.34	1.00	14.23	10.13	144.18	3.600	No	Yes	2.00
795	53.42	59.32	2.99	5.88	1.00	17.47	8.56	149.47	3.600	No	Yes	2.00
796	53.47	74.66	2.87	5.11	1.00	22.21	6.75	150.02	3.600	No	Yes	2.00
797	53.52	92.88	2.76	4.46	1.00	27.85	5.32	148.22	3.600	No	Yes	2.00
798	53.58	102.94	2.72	4.44	1.00	30.94	4.93	152.55	3.600	No	Yes	2.00
799	53.66	103.80	2.74	4.76	1.00	31.15	5.14	160.18	3.600	No	Yes	2.00
800	53.75	98.64	2.79	5.33	1.00	29.50	5.74	169.41	3.600	No	Yes	2.00
801	53.81	88.93	2.86	5.98	1.00	26.46	6.64	175.67	3.600	No	Yes	2.00
802	53.87	78.89	2.93	6.58	1.00	23.33	7.63	177.89	3.600	No	Yes	2.00
803	53.95	67.24	3.02	7.41	1.00	19.70	9.07	178.71	3.600	No	Yes	2.00
804	54.01	57.35	3.10	8.28	1.00	16.64	10.67	177.57	3.600	No	Yes	2.00
805	54.06	47.51	3.20	9.23	1.00	13.60	12.71	172.90	3.600	No	Yes	2.00
806	54.15	41.78	3.26	9.77	1.00	11.83	14.16	167.57	3.600	No	Yes	2.00
807	54.20	40.60	3.27	9.77	1.00	11.46	14.42	165.24	3.600	No	Yes	2.00
808	54.29	47.57	3.17	8.38	1.00	13.59	12.09	164.23	3.600	No	Yes	2.00
809	54.34	69.40	2.89	4.90	1.00	20.27	7.00	141.87	4.000	Yes	Yes	2.00
810	54.43	100.37	2.59	2.67	1.00	29.73	3.65	108.63	4.000	Yes	No	2.00
811	54.45	137.16	2.32	1.48	1.00	41.00	2.00	82.07	4.000	Yes	No	2.00
812	54.48	166.07	2.20	1.22	1.00	49.83	1.62	80.59	4.000	Yes	No	2.00
813	54.52	185.51	2.14	1.11	1.00	55.76	1.48	82.69	4.000	Yes	No	2.00
814	54.53	198.85	2.12	1.13	1.00	59.83	1.45	86.57	4.000	Yes	No	2.00
815	54.58	207.94	2.11	1.17	1.00	62.58	1.44	89.91	0.148	No	No	0.45
816	54.62	219.64	2.10	1.19	1.00	66.13	1.42	93.59	0.156	No	No	0.47

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	54.65	233.46	2.07	1.16	1.00	70.33	1.38	96.81	0.164	No	No	0.50
818	54.70	244.67	2.05	1.15	1.00	73.72	1.36	99.98	0.173	No	No	0.52
819	54.76	251.12	2.05	1.17	1.00	75.64	1.35	102.23	0.179	No	No	0.54
820	54.77	249.88	2.06	1.22	1.00	75.25	1.37	102.77	0.181	No	No	0.55
821	54.82	251.50	2.06	1.21	1.00	75.71	1.36	103.16	0.182	No	No	0.55
822	54.87	253.07	2.05	1.21	1.00	76.14	1.36	103.55	0.183	No	No	0.56
823	54.88	255.63	2.05	1.20	1.00	76.92	1.35	104.08	0.185	No	No	0.56
824	54.91	257.28	2.05	1.20	1.00	77.39	1.35	104.56	0.186	No	No	0.56
825	54.96	263.42	2.04	1.18	1.00	79.22	1.34	106.09	0.191	No	No	0.58
826	54.97	276.70	2.01	1.17	1.00	83.26	1.32	109.90	0.203	No	No	0.62
827	55.03	294.89	1.99	1.17	1.00	88.74	1.30	115.47	0.223	No	No	0.68
828	55.09	315.21	1.96	1.11	1.00	94.86	1.27	120.89	0.244	No	No	0.74
829	55.15	327.84	1.89	0.92	1.00	98.63	1.23	121.55	0.247	No	No	0.75
830	55.20	338.35	1.85	0.83	1.00	101.77	1.20	122.41	0.251	No	No	0.76
831	55.25	358.17	1.78	0.67	1.00	107.74	1.13	121.49	0.247	No	No	0.75
832	55.30	386.84	1.77	0.71	1.00	116.38	1.11	129.28	0.281	No	No	0.85
833	55.34	417.50	1.74	0.72	1.00	125.63	1.07	134.62	0.307	No	No	0.93
834	55.39	440.05	1.76	0.82	1.00	132.40	1.10	146.03	0.370	No	No	1.12
835	55.40	462.28	1.76	0.87	1.00	139.13	1.10	153.71	0.418	No	No	1.27
836	55.44	482.80	1.75	0.87	1.00	145.29	1.08	157.35	0.442	No	No	1.34
837	55.44	511.21	1.72	0.83	1.00	153.88	1.02	157.04	0.440	No	No	1.34
838	55.49	517.76	1.72	0.86	1.00	155.78	1.03	160.78	0.467	No	No	1.42
839	55.54	533.43	1.73	0.91	1.00	160.44	1.05	167.71	0.519	No	No	1.58
840	55.59	534.98	1.76	1.00	1.00	160.82	1.10	176.17	0.588	No	No	1.79
841	55.63	551.08	1.75	1.02	1.00	165.61	1.09	180.34	0.625	No	No	1.90
842	55.64	553.47	1.75	1.02	1.00	166.31	1.09	180.79	0.630	No	No	1.91
843	55.68	566.94	1.73	0.98	1.00	170.31	1.06	179.92	0.622	No	No	1.89
844	55.69	570.38	1.73	0.97	1.00	171.33	1.04	178.50	0.609	No	No	1.85
845	55.69	566.17	1.73	0.98	1.00	170.04	1.05	179.38	0.617	No	No	1.88
846	55.71	561.62	1.75	1.03	1.00	168.63	1.09	183.08	0.651	No	No	1.98
847	55.76	567.28	1.76	1.06	1.00	170.25	1.10	186.45	0.683	No	No	2.00
848	55.78	580.19	1.75	1.05	1.00	174.11	1.08	187.85	0.696	No	No	2.00
849	55.81	581.23	1.72	0.98	1.00	174.36	1.04	180.96	0.631	No	No	1.92
850	55.85	584.16	1.69	0.88	1.00	175.16	1.00	175.16	0.580	No	No	1.77
851	55.86	588.34	1.65	0.77	1.00	176.41	1.00	176.41	0.591	No	No	1.80
852	55.91	598.65	1.62	0.70	1.00	179.42	1.00	179.42	0.617	No	No	1.88
853	55.92	602.25	1.60	0.66	1.00	180.48	1.00	180.48	0.627	No	No	1.91
854	55.96	619.03	1.58	0.63	1.00	185.46	1.00	185.46	0.673	No	No	2.00
855	55.97	634.09	1.57	0.63	1.00	189.98	1.00	189.98	0.718	No	No	2.00
856	56.00	654.37	1.56	0.64	1.00	196.01	1.00	196.01	0.780	No	No	2.00
857	56.01	660.12	1.58	0.69	1.00	197.72	1.00	197.72	0.799	No	No	2.00
858	56.03	661.79	1.59	0.72	1.00	198.18	1.00	198.18	0.804	No	No	2.00
859	56.05	661.82	1.60	0.74	1.00	198.14	1.00	198.14	0.803	No	No	2.00
860	56.10	665.04	1.60	0.73	1.00	198.99	1.00	198.99	0.813	No	No	2.00
861	56.12	668.02	1.58	0.70	1.00	199.86	1.00	199.86	0.822	No	No	2.00
862	56.16	667.69	1.57	0.68	1.00	199.67	1.00	199.67	0.820	No	No	2.00
863	56.17	654.78	1.57	0.67	1.00	195.76	1.00	195.76	0.778	No	No	2.00
864	56.20	635.11	1.59	0.69	1.00	189.78	1.00	189.78	0.716	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	56.22	617.48	1.61	0.71	1.00	184.46	1.00	184.46	0.664	No	No	2.00
866	56.24	608.45	1.61	0.71	1.00	181.69	1.00	181.69	0.638	No	No	1.95
867	56.30	602.69	1.62	0.70	1.00	179.84	1.00	179.84	0.621	No	No	1.89
868	56.31	595.69	1.63	0.72	1.00	177.72	1.00	177.72	0.602	No	No	1.84
869	56.34	586.22	1.65	0.77	1.00	174.82	1.00	174.82	0.577	No	No	1.76
870	56.39	579.04	1.66	0.78	1.00	172.57	1.00	172.57	0.558	No	No	1.70
871	56.45	572.30	1.67	0.79	1.00	170.44	1.00	170.44	0.540	No	No	1.65
872	56.48	565.39	1.67	0.79	1.00	168.31	1.00	168.31	0.523	No	No	1.60
873	56.49	555.45	1.70	0.85	1.00	165.32	1.00	165.32	0.500	No	No	1.53
874	56.53	542.15	1.73	0.91	1.00	161.25	1.05	168.57	0.525	No	No	1.60
875	56.58	529.04	1.75	0.94	1.00	157.24	1.08	169.38	0.532	No	No	1.62
876	56.63	524.73	1.67	0.72	1.00	155.86	1.00	155.86	0.432	No	No	1.32
877	56.68	526.01	1.58	0.52	1.00	156.17	1.00	156.17	0.434	No	No	1.33
878	56.73	531.33	1.53	0.43	1.00	157.68	1.00	157.68	0.445	No	No	1.36
879	56.78	526.31	1.62	0.60	1.00	156.09	1.00	156.09	0.434	No	No	1.33
880	56.83	517.99	1.69	0.76	1.00	153.53	1.00	153.53	0.417	No	No	1.27
881	56.89	503.37	1.73	0.85	1.00	149.05	1.06	157.35	0.442	No	No	1.35
882	56.95	485.04	1.77	0.94	1.00	143.50	1.12	160.76	0.466	No	No	1.43
883	56.99	470.25	1.81	1.02	1.00	139.02	1.16	161.37	0.471	No	No	1.44
884	57.01	460.92	1.83	1.07	1.00	136.23	1.18	160.98	0.468	No	No	1.43
885	57.04	461.73	1.82	1.05	1.00	136.41	1.18	160.65	0.466	No	No	1.43
886	57.09	468.20	1.81	1.02	1.00	138.26	1.17	161.13	0.469	No	No	1.44
887	57.11	477.43	1.81	1.03	1.00	140.98	1.16	163.57	0.487	No	No	1.49
888	57.13	488.62	1.81	1.06	1.00	144.26	1.16	167.47	0.517	No	No	1.58
889	57.18	488.78	1.82	1.11	1.00	144.24	1.17	169.44	0.532	No	No	1.63
890	57.19	477.80	1.85	1.18	1.00	140.96	1.20	168.95	0.529	No	No	1.62
891	57.21	464.47	1.87	1.22	1.00	136.96	1.21	166.30	0.508	No	No	1.56
892	57.24	456.12	1.88	1.23	1.00	134.45	1.22	164.00	0.490	No	No	1.50
893	57.28	456.72	1.87	1.20	1.00	134.56	1.21	163.35	0.485	No	No	1.49
894	57.32	450.91	1.87	1.19	1.00	132.78	1.22	161.45	0.471	No	No	1.44
895	57.35	445.39	1.88	1.21	1.00	131.08	1.22	160.03	0.461	No	No	1.41
896	57.38	435.59	1.89	1.22	1.00	128.14	1.23	157.50	0.443	No	No	1.36
897	57.43	430.50	1.89	1.21	1.00	126.56	1.23	155.53	0.430	No	No	1.32
898	57.48	414.66	1.90	1.19	1.00	121.80	1.23	150.26	0.396	No	No	1.21
899	57.52	398.59	1.89	1.12	1.00	116.98	1.23	143.92	0.357	No	No	1.10
900	57.57	389.56	1.91	1.18	1.00	114.25	1.25	142.28	0.348	No	No	1.07
901	57.62	396.66	1.94	1.29	1.00	116.29	1.26	146.53	0.373	No	No	1.14
902	57.68	427.50	1.92	1.35	1.00	125.32	1.25	157.03	0.440	No	No	1.35
903	57.76	462.23	1.88	1.27	1.00	135.46	1.23	166.00	0.505	No	No	1.55
904	57.81	505.50	1.75	0.90	1.00	148.16	1.09	161.17	0.469	No	No	1.44
905	57.86	543.58	1.63	0.63	1.00	159.31	1.00	159.31	0.456	No	No	1.40
906	57.89	572.52	1.49	0.39	1.00	167.80	1.00	167.80	0.519	No	No	1.60
907	57.91	583.54	1.48	0.39	1.00	171.02	1.00	171.02	0.545	No	No	1.68
908	57.92	577.13	1.50	0.42	1.00	169.11	1.00	169.11	0.530	No	No	1.63
909	57.95	569.05	1.54	0.47	1.00	166.67	1.00	166.67	0.511	No	No	1.57
910	57.99	570.66	1.56	0.52	1.00	167.08	1.00	167.08	0.514	No	No	1.58
911	58.01	578.72	1.57	0.56	1.00	169.42	1.00	169.42	0.532	No	No	1.64
912	58.05	591.19	1.58	0.58	1.00	173.02	1.00	173.02	0.562	No	No	1.73

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	58.05	598.87	1.59	0.62	1.00	175.27	1.00	175.27	0.581	No	No	1.79
914	58.10	604.77	1.60	0.65	1.00	176.91	1.00	176.91	0.595	No	No	1.83
915	58.13	611.17	1.60	0.67	1.00	178.73	1.00	178.73	0.611	No	No	1.88
916	58.15	618.51	1.60	0.66	1.00	180.87	1.00	180.87	0.630	No	No	1.94
917	58.17	625.12	1.59	0.65	1.00	182.75	1.00	182.75	0.648	No	No	1.99
918	58.20	623.43	1.59	0.66	1.00	182.21	1.00	182.21	0.643	No	No	1.98
919	58.21	619.40	1.60	0.67	1.00	181.00	1.00	181.00	0.632	No	No	1.94
920	58.21	614.30	1.61	0.68	1.00	179.50	1.00	179.50	0.618	No	No	1.90
921	58.23	613.93	1.61	0.68	1.00	179.34	1.00	179.34	0.616	No	No	1.90
922	58.24	608.11	1.62	0.69	1.00	177.62	1.00	177.62	0.601	No	No	1.85
923	58.25	609.21	1.54	0.52	1.00	177.92	1.00	177.92	0.604	No	No	1.86
924	58.29	613.99	1.44	0.36	1.00	179.26	1.00	179.26	0.616	No	No	1.90
925	58.31	627.24	1.32	0.20	1.00	183.11	1.00	183.11	0.651	No	No	2.00
926	58.33	639.00	1.34	0.24	1.00	186.52	1.00	186.52	0.683	No	No	2.00
927	58.38	651.36	1.37	0.28	1.00	190.06	1.00	190.06	0.718	No	No	2.00
928	58.39	661.87	1.39	0.32	1.00	193.13	1.00	193.13	0.750	No	No	2.00
929	58.43	670.53	1.40	0.34	1.00	195.59	1.00	195.59	0.776	No	No	2.00
930	58.43	682.73	1.39	0.33	1.00	199.15	1.00	199.15	0.815	No	No	2.00
931	58.48	688.02	1.40	0.35	1.00	200.60	1.00	200.60	4.000	No	No	2.00
932	58.53	694.39	1.41	0.38	1.00	202.36	1.00	202.36	4.000	No	No	2.00
933	58.56	696.37	1.46	0.46	1.00	202.90	1.00	202.90	4.000	No	No	2.00
934	58.58	704.43	1.47	0.49	1.00	205.20	1.00	205.20	4.000	No	No	2.00
935	58.59	710.90	1.49	0.52	1.00	207.06	1.00	207.06	4.000	No	No	2.00
936	58.63	707.18	1.49	0.53	1.00	205.90	1.00	205.90	4.000	No	No	2.00
937	58.63	709.20	1.50	0.54	1.00	206.49	1.00	206.49	4.000	No	No	2.00
938	58.63	695.36	1.51	0.54	1.00	202.42	1.00	202.42	4.000	No	No	2.00
939	58.68	700.19	1.49	0.51	1.00	203.74	1.00	203.74	4.000	No	No	2.00
940	58.69	701.88	1.45	0.44	1.00	204.22	1.00	204.22	4.000	No	No	2.00
941	58.72	717.85	1.40	0.38	1.00	208.81	1.00	208.81	4.000	No	No	2.00
942	58.73	722.94	1.38	0.36	1.00	210.28	1.00	210.28	4.000	No	No	2.00
943	58.74	728.64	1.41	0.40	1.00	211.92	1.00	211.92	4.000	No	No	2.00
944	58.77	726.96	1.44	0.45	1.00	211.36	1.00	211.36	4.000	No	No	2.00
945	58.81	722.67	1.47	0.50	1.00	210.02	1.00	210.02	4.000	No	No	2.00
946	58.82	713.94	1.49	0.53	1.00	207.44	1.00	207.44	4.000	No	No	2.00
947	58.83	715.80	1.51	0.57	1.00	207.97	1.00	207.97	4.000	No	No	2.00
948	58.87	722.33	1.52	0.60	1.00	209.78	1.00	209.78	4.000	No	No	2.00
949	58.91	731.67	1.53	0.63	1.00	212.41	1.00	212.41	4.000	No	No	2.00
950	58.92	737.87	1.54	0.64	1.00	214.21	1.00	214.21	4.000	No	No	2.00
951	58.93	740.53	1.53	0.64	1.00	214.95	1.00	214.95	4.000	No	No	2.00
952	58.96	739.05	1.53	0.63	1.00	214.44	1.00	214.44	4.000	No	No	2.00
953	59.01	716.31	1.56	0.67	1.00	207.70	1.00	207.70	4.000	No	No	2.00
954	59.06	687.29	1.59	0.73	1.00	199.13	1.00	199.13	0.814	No	No	2.00
955	59.08	655.28	1.63	0.78	1.00	189.77	1.00	189.77	0.716	No	No	2.00
956	59.11	638.94	1.65	0.81	1.00	184.95	1.00	184.95	0.668	No	No	2.00
957	59.15	627.21	1.68	0.88	1.00	181.46	1.00	181.46	0.636	No	No	1.96
958	59.21	618.28	1.70	0.94	1.00	178.75	1.00	178.75	0.611	No	No	1.89
959	59.26	606.09	1.72	0.96	1.00	175.11	1.02	178.89	0.612	No	No	1.89
960	59.30	592.31	1.71	0.92	1.00	171.02	1.01	173.20	0.563	No	No	1.74

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
961	59.35	579.87	1.71	0.90	1.00	167.32	1.01	169.07	0.529	No	No	1.64
962	59.40	562.76	1.73	0.91	1.00	162.26	1.04	168.73	0.527	No	No	1.63
963	59.42	550.96	1.74	0.92	1.00	158.81	1.06	168.34	0.524	No	No	1.62
964	59.47	539.34	1.75	0.93	1.00	155.35	1.08	167.78	0.519	No	No	1.61
965	59.51	539.41	1.75	0.95	1.00	155.29	1.09	168.63	0.526	No	No	1.63
966	59.56	537.97	1.75	0.95	1.00	154.79	1.09	168.59	0.526	No	No	1.63
967	59.61	537.36	1.74	0.90	1.00	154.53	1.06	164.50	0.494	No	No	1.53
968	59.67	541.98	1.70	0.80	1.00	155.77	1.00	155.77	0.432	No	No	1.34
969	59.71	553.73	1.65	0.69	1.00	159.11	1.00	159.11	0.455	No	No	1.41
970	59.80	555.82	1.61	0.59	1.00	159.56	1.00	159.56	0.458	No	No	1.42
971	59.85	552.45	1.59	0.54	1.00	158.50	1.00	158.50	0.450	No	No	1.40
972	59.90	542.21	1.59	0.53	1.00	155.47	1.00	155.47	0.429	No	No	1.33
973	60.00	542.99	1.59	0.54	1.00	155.53	1.00	155.53	0.430	No	No	1.33
974	60.04	541.71	1.60	0.56	1.00	155.09	1.00	155.09	0.427	No	No	1.33
975	60.10	526.52	1.63	0.60	1.00	150.62	1.00	150.62	0.398	No	No	1.23
976	60.15	508.32	1.67	0.66	1.00	145.30	1.00	145.30	0.365	No	No	1.13
977	60.19	487.40	1.70	0.69	1.00	139.22	1.00	139.22	0.331	No	No	1.03
978	60.23	483.49	1.69	0.66	1.00	138.03	1.00	138.03	0.325	No	No	1.01
979	60.28	482.61	1.68	0.63	1.00	137.71	1.00	137.71	0.323	No	No	1.00
980	60.33	488.98	1.67	0.62	1.00	139.47	1.00	139.47	0.332	No	No	1.03
981	60.38	491.97	1.67	0.64	1.00	140.26	1.00	140.26	0.337	No	No	1.05
982	60.42	493.85	1.69	0.68	1.00	140.74	1.00	140.74	0.339	No	No	1.05
983	60.44	487.18	1.71	0.72	1.00	138.79	1.01	140.24	0.337	No	No	1.05
984	60.47	475.94	1.74	0.79	1.00	135.53	1.08	145.72	0.368	No	No	1.14
985	60.52	465.53	1.78	0.87	1.00	132.47	1.12	148.94	0.387	No	No	1.20
986	60.56	462.70	1.79	0.92	1.00	131.60	1.15	150.90	0.400	No	No	1.24
987	60.57	465.03	1.79	0.92	1.00	132.25	1.15	151.48	0.403	No	No	1.25
988	60.61	470.62	1.78	0.89	1.00	133.80	1.13	151.48	0.403	No	No	1.25
989	60.66	477.29	1.77	0.88	1.00	135.64	1.12	151.98	0.406	No	No	1.27
990	60.71	486.66	1.77	0.87	1.00	138.25	1.11	153.21	0.414	No	No	1.29
991	60.76	495.25	1.77	0.90	1.00	140.63	1.11	156.59	0.437	No	No	1.36
992	60.81	504.76	1.77	0.92	1.00	143.27	1.11	159.58	0.458	No	No	1.43
993	60.86	523.05	1.75	0.90	1.00	148.43	1.08	161.02	0.468	No	No	1.46
994	60.91	559.78	1.70	0.83	1.00	158.84	1.00	158.84	0.453	No	No	1.41
995	60.95	601.50	1.66	0.78	1.00	170.69	1.00	170.69	0.542	No	No	1.69
996	61.00	637.66	1.64	0.77	1.00	180.91	1.00	180.91	0.631	No	No	1.97
997	61.02	657.74	1.64	0.79	1.00	186.60	1.00	186.60	0.684	No	No	2.00
998	61.05	685.10	1.62	0.78	1.00	194.34	1.00	194.34	0.763	No	No	2.00
999	61.08	710.24	1.61	0.77	1.00	201.44	1.00	201.44	4.000	No	No	2.00
1000	61.09	731.84	1.59	0.76	1.00	207.57	1.00	207.57	4.000	No	No	2.00
1001	61.13	737.94	1.59	0.76	1.00	209.24	1.00	209.24	4.000	No	No	2.00
1002	61.14	739.46	1.60	0.77	1.00	209.63	1.00	209.63	4.000	No	No	2.00
1003	61.16	741.44	1.60	0.78	1.00	210.15	1.00	210.15	4.000	No	No	2.00
1004	61.20	750.88	1.58	0.75	1.00	212.77	1.00	212.77	4.000	No	No	2.00
1005	61.23	762.13	1.56	0.71	1.00	215.88	1.00	215.88	4.000	No	No	2.00
1006	61.24	766.92	1.52	0.62	1.00	217.23	1.00	217.23	4.000	No	No	2.00
1007	61.29	758.86	1.51	0.59	1.00	214.83	1.00	214.83	4.000	No	No	2.00
1008	61.30	744.24	1.52	0.59	1.00	210.65	1.00	210.65	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1009	61.33	734.57	1.55	0.65	1.00	207.82	1.00	207.82	4.000	No	No	2.00
1010	61.38	730.90	1.55	0.65	1.00	206.66	1.00	206.66	4.000	No	No	2.00
1011	61.43	731.07	1.53	0.60	1.00	206.60	1.00	206.60	4.000	No	No	2.00
1012	61.48	738.25	1.50	0.56	1.00	208.54	1.00	208.54	4.000	No	No	2.00
1013	61.53	750.91	1.48	0.53	1.00	212.02	1.00	212.02	4.000	No	No	2.00
1014	61.56	754.78	1.48	0.52	1.00	213.05	1.00	213.05	4.000	No	No	2.00
1015	61.58	726.93	1.50	0.54	1.00	205.10	1.00	205.10	4.000	No	No	2.00
1016	61.59	702.39	1.52	0.55	1.00	198.13	1.00	198.13	0.803	No	No	2.00
1017	61.62	600.70	1.61	0.64	1.00	169.24	1.00	169.24	0.531	No	No	1.66
1018	61.63	595.30	1.61	0.64	1.00	167.67	1.00	167.67	0.518	No	No	1.62
1019	61.67	588.36	1.62	0.64	1.00	165.65	1.00	165.65	0.503	No	No	1.57
1020	61.71	662.66	1.55	0.57	1.00	186.61	1.00	186.61	0.684	No	No	2.00
1021	61.76	655.52	1.55	0.57	1.00	184.50	1.00	184.50	0.664	No	No	2.00
1022	61.81	634.02	1.54	0.53	1.00	178.32	1.00	178.32	0.607	No	No	1.90
1023	61.86	615.02	1.52	0.48	1.00	172.85	1.00	172.85	0.560	No	No	1.75
1024	61.87	600.83	1.48	0.38	1.00	168.83	1.00	168.83	0.528	No	No	1.65
1025	61.91	588.87	1.44	0.32	1.00	165.39	1.00	165.39	0.501	No	No	1.57
1026	61.95	578.02	1.42	0.27	1.00	162.25	1.00	162.25	0.477	No	No	1.49
1027	61.96	566.74	1.42	0.26	1.00	159.04	1.00	159.04	0.454	No	No	1.42
1028	62.00	553.70	1.45	0.29	1.00	155.30	1.00	155.30	0.428	No	No	1.34
1029	62.04	535.16	1.49	0.33	1.00	150.01	1.00	150.01	0.394	No	No	1.23
1030	62.06	510.97	1.55	0.41	1.00	143.15	1.00	143.15	0.353	No	No	1.11
1031	62.10	491.66	1.60	0.47	1.00	137.65	1.00	137.65	0.323	No	No	1.01
1032	62.14	475.52	1.64	0.51	1.00	133.04	1.00	133.04	0.299	No	No	0.94
1033	62.20	463.08	1.66	0.55	1.00	129.46	1.00	129.46	0.282	No	No	0.88
1034	62.22	439.20	1.71	0.60	1.00	122.70	1.00	122.70	0.252	No	No	0.79
1035	62.27	415.48	1.75	0.66	1.00	115.96	1.08	125.13	0.262	No	No	0.82
1036	62.29	396.37	1.78	0.71	1.00	110.55	1.13	125.44	0.264	No	No	0.83
1037	62.34	380.26	1.82	0.77	1.00	105.96	1.17	124.22	0.258	No	No	0.81
1038	62.39	366.62	1.86	0.86	1.00	102.08	1.21	123.46	0.255	No	No	0.80
1039	62.43	347.78	1.93	1.03	1.00	96.73	1.26	121.51	0.247	No	No	0.77
1040	62.49	340.13	1.97	1.16	1.00	94.52	1.28	121.38	0.246	No	No	0.77
1041	62.57	336.43	1.99	1.25	1.00	93.40	1.30	121.70	0.248	No	No	0.78
1042	62.68	357.18	1.98	1.25	1.00	99.12	1.29	127.79	0.274	No	No	0.86
1043	62.75	398.26	1.93	1.21	1.00	110.56	1.26	139.12	0.330	No	No	1.04
1044	62.87	426.23	1.91	1.20	1.00	118.25	1.24	146.86	0.375	No	No	1.18
1045	62.88	409.21	1.93	1.22	1.00	113.48	1.25	142.25	0.348	No	No	1.09
1046	62.89	424.34	1.86	1.01	1.00	117.70	1.21	142.29	0.348	No	No	1.09
1047	62.93	485.42	1.74	0.76	1.00	134.75	1.06	142.80	0.351	No	No	1.10
1048	62.98	571.92	1.61	0.59	1.00	158.87	1.00	158.87	0.453	No	No	1.42
1049	63.02	620.24	1.47	0.38	1.00	172.30	1.00	172.30	0.556	No	No	1.75
1050	63.07	658.55	1.31	0.19	1.00	182.93	1.00	182.93	0.649	No	No	2.00
1051	63.12	710.78	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1052	63.14	752.36	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1053	63.17	781.30	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1054	63.17	799.36	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1055	63.20	825.98	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1056	63.21	830.83	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1057	63.23	842.91	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1058	63.26	834.75	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1059	63.28	841.52	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1060	63.31	838.10	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1061	63.32	839.38	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1062	63.36	837.12	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1063	63.40	836.85	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_t: Total cone resistance
I_c: Soil behavior type index
Fr: Normalized friction ratio (%)
n: Stress exponent
Q_{tn}: Normalized cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
0.01	2.00	0.00	0.00	0.02	0.00	0.04	2.00	0.00	0.00	0.02	0.00
0.09	2.00	0.00	0.00	0.05	0.00	0.11	2.00	0.00	0.00	0.02	0.00
0.14	2.00	0.00	0.00	0.03	0.00	0.14	2.00	0.00	0.00	0.01	0.00
0.18	2.00	0.00	0.00	0.04	0.00	0.23	2.00	0.00	0.00	0.05	0.00
0.24	2.00	0.00	0.00	0.01	0.00	0.28	2.00	0.00	0.00	0.04	0.00
0.33	2.00	0.00	0.00	0.05	0.00	0.38	2.00	0.00	0.00	0.05	0.00
0.42	2.00	0.00	0.00	0.05	0.00	0.47	2.00	0.00	0.00	0.05	0.00
0.51	2.00	0.00	0.00	0.04	0.00	0.52	2.00	0.00	0.00	0.01	0.00
0.57	2.00	0.00	0.00	0.05	0.00	0.61	2.00	0.00	0.00	0.04	0.00
0.67	2.00	0.00	0.00	0.05	0.00	0.73	2.00	0.00	0.00	0.06	0.00
0.81	2.00	0.00	0.00	0.08	0.00	0.86	2.00	0.00	0.00	0.05	0.00
0.98	2.00	0.00	0.00	0.12	0.00	1.05	2.00	0.00	0.00	0.07	0.00
1.15	2.00	0.00	0.00	0.10	0.00	1.24	2.00	0.00	0.00	0.09	0.00
1.34	2.00	0.00	0.00	0.10	0.00	1.43	2.00	0.00	0.00	0.09	0.00
1.53	2.00	0.00	0.00	0.10	0.00	1.58	2.00	0.00	0.00	0.05	0.00
1.62	2.00	0.00	0.00	0.04	0.00	1.67	2.00	0.00	0.00	0.05	0.00
1.75	2.00	0.00	0.00	0.07	0.00	1.77	2.00	0.00	0.00	0.03	0.00
1.81	2.00	0.00	0.00	0.04	0.00	1.86	2.00	0.00	0.00	0.04	0.00
1.91	2.00	0.00	0.00	0.05	0.00	1.95	2.00	0.00	0.00	0.04	0.00
2.00	2.00	0.00	0.00	0.05	0.00	2.05	2.00	0.00	0.00	0.05	0.00
2.11	2.00	0.00	0.00	0.06	0.00	2.20	2.00	0.00	0.00	0.09	0.00
2.24	2.00	0.00	0.00	0.05	0.00	2.29	2.00	0.00	0.00	0.05	0.00
2.34	2.00	0.00	0.00	0.05	0.00	2.44	2.00	0.00	0.00	0.10	0.00
2.48	2.00	0.00	0.00	0.05	0.00	2.58	2.00	0.00	0.00	0.10	0.00
2.63	2.00	0.00	0.00	0.05	0.00	2.71	2.00	0.00	0.00	0.08	0.00
2.78	2.00	0.00	0.00	0.07	0.00	2.82	2.00	0.00	0.00	0.04	0.00
2.89	2.00	0.00	0.00	0.07	0.00	2.96	2.00	0.00	0.00	0.08	0.00
3.03	2.00	0.00	0.00	0.07	0.00	3.11	2.00	0.00	0.00	0.08	0.00
3.19	2.00	0.00	0.00	0.09	0.00	3.25	2.00	0.00	0.00	0.06	0.00
3.35	2.00	0.00	0.00	0.10	0.00	3.41	2.00	0.00	0.00	0.05	0.00
3.50	2.00	0.00	0.00	0.09	0.00	3.59	2.00	0.00	0.00	0.09	0.00
3.69	2.00	0.00	0.00	0.10	0.00	3.79	2.00	0.00	0.00	0.09	0.00
3.88	2.00	0.00	0.00	0.09	0.00	3.97	2.00	0.00	0.00	0.10	0.00
4.07	2.00	0.00	0.00	0.09	0.00	4.14	2.00	0.00	0.00	0.07	0.00
4.17	2.00	0.00	0.00	0.04	0.00	4.26	2.00	0.00	0.00	0.09	0.00
4.32	2.00	0.00	0.00	0.05	0.00	4.37	2.00	0.00	0.00	0.05	0.00
4.42	2.00	0.00	0.00	0.06	0.00	4.51	2.00	0.00	0.00	0.08	0.00
4.61	2.00	0.00	0.00	0.10	0.00	4.65	2.00	0.00	0.00	0.05	0.00
4.74	2.00	0.00	0.00	0.09	0.00	4.80	2.00	0.00	0.00	0.06	0.00
4.89	2.00	0.00	0.00	0.09	0.00	4.95	2.00	0.00	0.00	0.05	0.00
5.04	2.00	0.00	0.00	0.09	0.00	5.13	2.00	0.00	0.00	0.09	0.00
5.18	2.00	0.00	0.00	0.05	0.00	5.28	2.00	0.00	0.00	0.10	0.00
5.32	2.00	0.00	0.00	0.04	0.00	5.42	2.00	0.00	0.00	0.10	0.00
5.51	2.00	0.00	0.00	0.09	0.00	5.60	2.00	0.00	0.00	0.09	0.00
5.66	2.00	0.00	0.00	0.06	0.00	5.76	2.00	0.00	0.00	0.09	0.00
5.85	2.00	0.00	0.00	0.09	0.00	5.92	2.00	0.00	0.00	0.07	0.00
5.95	2.00	0.00	0.00	0.03	0.00	5.97	2.00	0.00	0.00	0.02	0.00
6.02	2.00	0.00	0.00	0.06	0.00	6.06	2.00	0.00	0.00	0.04	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
6.16	2.00	0.00	0.00	0.10	0.00	6.21	2.00	0.00	0.00	0.04	0.00
6.26	2.00	0.00	0.00	0.06	0.00	6.31	2.00	0.00	0.00	0.04	0.00
6.40	2.00	0.00	0.00	0.09	0.00	6.44	2.00	0.00	0.00	0.04	0.00
6.52	2.00	0.00	0.00	0.08	0.00	6.57	2.00	0.00	0.00	0.05	0.00
6.64	2.00	0.00	0.00	0.07	0.00	6.69	2.00	0.00	0.00	0.05	0.00
6.78	2.00	0.00	0.00	0.09	0.00	6.83	2.00	0.00	0.00	0.05	0.00
6.92	2.00	0.00	0.00	0.09	0.00	6.97	2.00	0.00	0.00	0.05	0.00
7.03	2.00	0.00	0.00	0.05	0.00	7.12	2.00	0.00	0.00	0.09	0.00
7.22	2.00	0.00	0.00	0.10	0.00	7.27	2.00	0.00	0.00	0.05	0.00
7.36	2.00	0.00	0.00	0.09	0.00	7.43	2.00	0.00	0.00	0.08	0.00
7.50	2.00	0.00	0.00	0.07	0.00	7.59	2.00	0.00	0.00	0.09	0.00
7.64	2.00	0.00	0.00	0.05	0.00	7.75	2.00	0.00	0.00	0.10	0.00
7.79	2.00	0.00	0.00	0.04	0.00	7.89	2.00	0.00	0.00	0.10	0.00
7.99	2.00	0.00	0.00	0.10	0.00	8.04	2.00	0.00	0.00	0.05	0.00
8.13	2.00	0.00	0.00	0.09	0.00	8.23	2.00	0.00	0.00	0.10	0.00
8.32	2.00	0.00	0.00	0.09	0.00	8.37	2.00	0.00	0.00	0.05	0.00
8.46	2.00	0.00	0.00	0.09	0.00	8.56	2.00	0.00	0.00	0.10	0.00
8.59	2.00	0.00	0.00	0.02	0.00	8.61	2.00	0.00	0.00	0.03	0.00
8.67	2.00	0.00	0.00	0.05	0.00	8.71	2.00	0.00	0.00	0.04	0.00
8.72	2.00	0.00	0.00	0.01	0.00	8.78	2.00	0.00	0.00	0.06	0.00
8.80	2.00	0.00	0.00	0.02	0.00	8.86	2.00	0.00	0.00	0.05	0.00
8.90	2.00	0.00	0.00	0.04	0.00	8.95	2.00	0.00	0.00	0.05	0.00
8.96	2.00	0.00	0.00	0.01	0.00	9.00	2.00	0.00	0.00	0.04	0.00
9.05	2.00	0.00	0.00	0.05	0.00	9.09	2.00	0.00	0.00	0.04	0.00
9.10	2.00	0.00	0.00	0.01	0.00	9.14	2.00	0.00	0.00	0.05	0.00
9.20	2.00	0.00	0.00	0.05	0.00	9.24	2.00	0.00	0.00	0.04	0.00
9.29	2.00	0.00	0.00	0.05	0.00	9.31	2.00	0.00	0.00	0.02	0.00
9.38	2.00	0.00	0.00	0.07	0.00	9.41	2.00	0.00	0.00	0.03	0.00
9.47	2.00	0.00	0.00	0.06	0.00	9.53	2.00	0.00	0.00	0.05	0.00
9.62	2.00	0.00	0.00	0.09	0.00	9.67	2.00	0.00	0.00	0.05	0.00
9.77	2.00	0.00	0.00	0.10	0.00	9.81	2.00	0.00	0.00	0.05	0.00
9.90	2.00	0.00	0.00	0.08	0.00	9.97	2.00	0.00	0.00	0.08	0.00
10.06	2.00	0.00	0.00	0.09	0.00	10.20	2.00	0.00	0.00	0.14	0.00
10.30	2.00	0.00	0.00	0.09	0.00	10.44	2.00	0.00	0.00	0.14	0.00
10.54	2.00	0.00	0.00	0.10	0.00	10.63	2.00	0.00	0.00	0.09	0.00
10.74	2.00	0.00	0.00	0.11	0.00	10.78	2.00	0.00	0.00	0.04	0.00
10.83	2.00	0.00	0.00	0.05	0.00	10.88	2.00	0.00	0.00	0.05	0.00
10.89	2.00	0.00	0.00	0.02	0.00	10.97	2.00	0.00	0.00	0.08	0.00
11.02	2.00	0.00	0.00	0.05	0.00	11.07	2.00	0.00	0.00	0.05	0.00
11.11	2.00	0.00	0.00	0.05	0.00	11.16	2.00	0.00	0.00	0.05	0.00
11.21	2.00	0.00	0.00	0.05	0.00	11.26	2.00	0.00	0.00	0.04	0.00
11.30	2.00	0.00	0.00	0.05	0.00	11.36	2.00	0.00	0.00	0.05	0.00
11.40	2.00	0.00	0.00	0.05	0.00	11.45	2.00	0.00	0.00	0.04	0.00
11.50	2.00	0.00	0.00	0.05	0.00	11.55	2.00	0.00	0.00	0.05	0.00
11.60	2.00	0.00	0.00	0.05	0.00	11.66	2.00	0.00	0.00	0.07	0.00
11.74	2.00	0.00	0.00	0.08	0.00	11.84	2.00	0.00	0.00	0.10	0.00
11.93	2.00	0.00	0.00	0.09	0.00	12.04	2.00	0.00	0.00	0.11	0.00
12.13	2.00	0.00	0.00	0.09	0.00	12.22	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
12.27	2.00	0.00	0.00	0.04	0.00	12.37	2.00	0.00	0.00	0.10	0.00
12.41	2.00	0.00	0.00	0.05	0.00	12.51	2.00	0.00	0.00	0.09	0.00
12.56	2.00	0.00	0.00	0.05	0.00	12.65	2.00	0.00	0.00	0.09	0.00
12.71	2.00	0.00	0.00	0.06	0.00	12.79	2.00	0.00	0.00	0.08	0.00
12.89	2.00	0.00	0.00	0.10	0.00	12.96	2.00	0.00	0.00	0.06	0.00
13.04	2.00	0.00	0.00	0.08	0.00	13.13	2.00	0.00	0.00	0.09	0.00
13.23	2.00	0.00	0.00	0.10	0.00	13.30	2.00	0.00	0.00	0.07	0.00
13.37	2.00	0.00	0.00	0.07	0.00	13.47	2.00	0.00	0.00	0.10	0.00
13.57	2.00	0.00	0.00	0.10	0.00	13.61	2.00	0.00	0.00	0.04	0.00
13.62	2.00	0.00	0.00	0.02	0.00	13.68	2.00	0.00	0.00	0.06	0.00
13.73	2.00	0.00	0.00	0.05	0.00	13.77	2.00	0.00	0.00	0.04	0.00
13.87	2.00	0.00	0.00	0.10	0.00	13.93	2.00	0.00	0.00	0.06	0.00
14.00	2.00	0.00	0.00	0.07	0.00	14.06	2.00	0.00	0.00	0.06	0.00
14.12	2.00	0.00	0.00	0.06	0.00	14.21	2.00	0.00	0.00	0.09	0.00
14.25	2.00	0.00	0.00	0.05	0.00	14.35	2.00	0.00	0.00	0.10	0.00
14.45	2.00	0.00	0.00	0.09	0.00	14.50	2.00	0.00	0.00	0.05	0.00
14.59	2.00	0.00	0.00	0.09	0.00	14.64	2.00	0.00	0.00	0.05	0.00
14.74	2.00	0.00	0.00	0.10	0.00	14.80	2.00	0.00	0.00	0.06	0.00
14.88	2.00	0.00	0.00	0.09	0.00	14.97	2.00	0.00	0.00	0.09	0.00
15.05	2.00	0.00	0.00	0.08	0.00	15.13	2.00	0.00	0.00	0.09	0.00
15.21	2.00	0.00	0.00	0.08	0.00	15.28	2.00	0.00	0.00	0.07	0.00
15.36	2.00	0.00	0.00	0.08	0.00	15.41	2.00	0.00	0.00	0.04	0.00
15.50	2.00	0.00	0.00	0.10	0.00	15.55	2.00	0.00	0.00	0.05	0.00
15.65	2.00	0.00	0.00	0.10	0.00	15.71	2.00	0.00	0.00	0.06	0.00
15.79	2.00	0.00	0.00	0.08	0.00	15.89	2.00	0.00	0.00	0.10	0.00
15.90	2.00	0.00	0.00	0.01	0.00	15.94	2.00	0.00	0.00	0.04	0.00
16.00	2.00	0.00	0.00	0.06	0.00	16.06	2.00	0.00	0.00	0.06	0.00
16.14	2.00	0.00	0.00	0.08	0.00	16.19	2.00	0.00	0.00	0.05	0.00
16.26	2.00	0.00	0.00	0.07	0.00	16.33	2.00	0.00	0.00	0.07	0.00
16.38	2.00	0.00	0.00	0.05	0.00	16.47	2.00	0.00	0.00	0.09	0.00
16.54	2.00	0.00	0.00	0.06	0.00	16.62	2.00	0.00	0.00	0.08	0.00
16.70	2.00	0.00	0.00	0.09	0.00	16.76	2.00	0.00	0.00	0.06	0.00
16.86	2.00	0.00	0.00	0.10	0.00	16.90	2.00	0.00	0.00	0.04	0.00
16.98	2.00	0.00	0.00	0.08	0.00	17.05	2.00	0.00	0.00	0.07	0.00
17.14	2.00	0.00	0.00	0.09	0.00	17.20	2.00	0.00	0.00	0.05	0.00
17.29	2.00	0.00	0.00	0.10	0.00	17.34	2.00	0.00	0.00	0.05	0.00
17.44	2.00	0.00	0.00	0.10	0.00	17.50	2.00	0.00	0.00	0.06	0.00
17.58	2.00	0.00	0.00	0.09	0.00	17.64	2.00	0.00	0.00	0.06	0.00
17.75	2.00	0.00	0.00	0.11	0.00	17.82	2.00	0.00	0.00	0.06	0.00
17.89	2.00	0.00	0.00	0.07	0.00	17.89	2.00	0.00	0.00	0.00	0.00
17.96	2.00	0.00	0.00	0.07	0.00	18.02	2.00	0.00	0.00	0.05	0.00
18.07	2.00	0.00	0.00	0.05	0.00	18.17	2.00	0.00	0.00	0.10	0.00
18.22	2.00	0.00	0.00	0.05	0.00	18.30	2.00	0.00	0.00	0.09	0.00
18.36	2.00	0.00	0.00	0.06	0.00	18.42	2.00	0.00	0.00	0.06	0.00
18.50	2.00	0.00	0.00	0.08	0.00	18.56	2.00	0.00	0.00	0.06	0.00
18.62	2.00	0.00	0.00	0.06	0.00	18.69	2.00	0.00	0.00	0.07	0.00
18.76	2.00	0.00	0.00	0.07	0.00	18.84	2.00	0.00	0.00	0.08	0.00
18.89	2.00	0.00	0.00	0.05	0.00	18.98	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
19.05	2.00	0.00	0.00	0.06	0.00	19.12	2.00	0.00	0.00	0.07	0.00
19.18	2.00	0.00	0.00	0.06	0.00	19.24	2.00	0.00	0.00	0.06	0.00
19.32	2.00	0.00	0.00	0.07	0.00	19.38	2.00	0.00	0.00	0.06	0.00
19.46	2.00	0.00	0.00	0.09	0.00	19.54	2.00	0.00	0.00	0.07	0.00
19.62	2.00	0.00	0.00	0.08	0.00	19.70	2.00	0.00	0.00	0.08	0.00
19.80	2.00	0.00	0.00	0.10	0.00	19.85	2.00	0.00	0.00	0.05	0.00
19.94	2.00	0.00	0.00	0.09	0.00	20.03	2.00	0.00	0.00	0.09	0.00
20.13	2.00	0.00	0.00	0.10	0.00	20.19	2.00	0.00	0.00	0.06	0.00
20.29	2.00	0.00	0.00	0.10	0.00	20.39	2.00	0.00	0.00	0.10	0.00
20.43	2.00	0.00	0.00	0.03	0.00	20.47	2.00	0.00	0.00	0.05	0.00
20.52	2.00	0.00	0.00	0.05	0.00	20.61	2.00	0.00	0.00	0.09	0.00
20.66	2.00	0.00	0.00	0.05	0.00	20.71	2.00	0.00	0.00	0.05	0.00
20.77	2.00	0.00	0.00	0.06	0.00	20.85	2.00	0.00	0.00	0.08	0.00
20.91	2.00	0.00	0.00	0.05	0.00	21.00	2.00	0.00	0.00	0.09	0.00
21.05	2.00	0.00	0.00	0.05	0.00	21.11	2.00	0.00	0.00	0.06	0.00
21.19	2.00	0.00	0.00	0.08	0.00	21.24	2.00	0.00	0.00	0.05	0.00
21.34	2.00	0.00	0.00	0.09	0.00	21.39	2.00	0.00	0.00	0.05	0.00
21.48	2.00	0.00	0.00	0.10	0.00	21.53	2.00	0.00	0.00	0.05	0.00
21.64	2.00	0.00	0.00	0.11	0.00	21.72	2.00	0.00	0.00	0.08	0.00
21.81	2.00	0.00	0.00	0.09	0.00	21.89	2.00	0.00	0.00	0.08	0.00
21.97	2.00	0.00	0.00	0.08	0.00	22.05	2.00	0.00	0.00	0.09	0.00
22.12	2.00	0.00	0.00	0.07	0.00	22.13	2.00	0.00	0.00	0.01	0.00
22.18	2.00	0.00	0.00	0.05	0.00	22.22	2.00	0.00	0.00	0.04	0.00
22.28	2.00	0.00	0.00	0.06	0.00	22.33	2.00	0.00	0.00	0.05	0.00
22.38	2.00	0.00	0.00	0.05	0.00	22.41	2.00	0.00	0.00	0.03	0.00
22.51	2.00	0.00	0.00	0.10	0.00	22.56	2.00	0.00	0.00	0.05	0.00
22.61	2.00	0.00	0.00	0.05	0.00	22.65	2.00	0.00	0.00	0.04	0.00
22.71	2.00	0.00	0.00	0.05	0.00	22.76	2.00	0.00	0.00	0.06	0.00
22.85	2.00	0.00	0.00	0.08	0.00	22.89	2.00	0.00	0.00	0.05	0.00
22.99	2.00	0.00	0.00	0.10	0.00	23.04	2.00	0.00	0.00	0.05	0.00
23.12	2.00	0.00	0.00	0.08	0.00	23.18	2.00	0.00	0.00	0.07	0.00
23.24	2.00	0.00	0.00	0.06	0.00	23.33	2.00	0.00	0.00	0.09	0.00
23.38	2.00	0.00	0.00	0.05	0.00	23.47	2.00	0.00	0.00	0.09	0.00
23.52	2.00	0.00	0.00	0.05	0.00	23.61	2.00	0.00	0.00	0.09	0.00
23.68	2.00	0.00	0.00	0.07	0.00	23.76	2.00	0.00	0.00	0.08	0.00
23.83	2.00	0.00	0.00	0.07	0.00	23.90	2.00	0.00	0.00	0.08	0.00
23.97	2.00	0.00	0.00	0.07	0.00	24.05	2.00	0.00	0.00	0.08	0.00
24.10	2.00	0.00	0.00	0.05	0.00	24.19	2.00	0.00	0.00	0.09	0.00
24.27	2.00	0.00	0.00	0.08	0.00	24.34	2.00	0.00	0.00	0.07	0.00
24.43	2.00	0.00	0.00	0.09	0.00	24.48	2.00	0.00	0.00	0.05	0.00
24.57	2.00	0.00	0.00	0.09	0.00	24.62	2.00	0.00	0.00	0.05	0.00
24.72	2.00	0.00	0.00	0.09	0.00	24.81	2.00	0.00	0.00	0.10	0.00
24.86	2.00	0.00	0.00	0.05	0.00	24.95	2.00	0.00	0.00	0.09	0.00
25.01	2.00	0.00	0.00	0.06	0.00	25.02	2.00	0.00	0.00	0.01	0.00
25.05	2.00	0.00	0.00	0.03	0.00	25.11	2.00	0.00	0.00	0.06	0.00
25.15	2.00	0.00	0.00	0.04	0.00	25.21	2.00	0.00	0.00	0.06	0.00
25.25	2.00	0.00	0.00	0.04	0.00	25.30	2.00	0.00	0.00	0.05	0.00
25.40	2.00	0.00	0.00	0.10	0.00	25.45	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
25.52	2.00	0.00	0.00	0.07	0.00	25.60	2.00	0.00	0.00	0.07	0.00
25.66	2.00	0.00	0.00	0.06	0.00	25.74	2.00	0.00	0.00	0.08	0.00
25.80	2.00	0.00	0.00	0.06	0.00	25.88	2.00	0.00	0.00	0.07	0.00
25.94	2.00	0.00	0.00	0.07	0.00	26.02	2.00	0.00	0.00	0.08	0.00
26.09	2.00	0.00	0.00	0.07	0.00	26.17	2.00	0.00	0.00	0.08	0.00
26.23	2.00	0.00	0.00	0.06	0.00	26.29	2.00	0.00	0.00	0.06	0.00
26.37	2.00	0.00	0.00	0.08	0.00	26.46	2.00	0.00	0.00	0.08	0.00
26.55	2.00	0.00	0.00	0.09	0.00	26.60	2.00	0.00	0.00	0.05	0.00
26.70	2.00	0.00	0.00	0.10	0.00	26.78	2.00	0.00	0.00	0.08	0.00
26.87	2.00	0.00	0.00	0.09	0.00	26.94	2.00	0.00	0.00	0.06	0.00
27.03	2.00	0.00	0.00	0.10	0.00	27.13	2.00	0.00	0.00	0.10	0.00
27.18	2.00	0.00	0.00	0.05	0.00	27.27	2.00	0.00	0.00	0.09	0.00
27.32	2.00	0.00	0.00	0.05	0.00	27.37	2.00	0.00	0.00	0.05	0.00
27.41	2.00	0.00	0.00	0.05	0.00	27.46	2.00	0.00	0.00	0.05	0.00
27.51	2.00	0.00	0.00	0.05	0.00	27.61	2.00	0.00	0.00	0.09	0.00
27.66	2.00	0.00	0.00	0.05	0.00	27.73	2.00	0.00	0.00	0.07	0.00
27.80	2.00	0.00	0.00	0.07	0.00	27.88	2.00	0.00	0.00	0.08	0.00
27.96	2.00	0.00	0.00	0.09	0.00	28.04	2.00	0.00	0.00	0.08	0.00
28.12	2.00	0.00	0.00	0.08	0.00	28.18	2.00	0.00	0.00	0.06	0.00
28.27	2.00	0.00	0.00	0.09	0.00	28.32	2.00	0.00	0.00	0.05	0.00
28.42	2.00	0.00	0.00	0.10	0.00	28.47	2.00	0.00	0.00	0.05	0.00
28.61	2.00	0.00	0.00	0.14	0.00	28.67	2.00	0.00	0.00	0.06	0.00
28.75	2.00	0.00	0.00	0.09	0.00	28.81	2.00	0.00	0.00	0.05	0.00
28.90	2.00	0.00	0.00	0.10	0.00	29.00	2.00	0.00	0.00	0.09	0.00
29.05	2.00	0.00	0.00	0.05	0.00	29.10	2.00	0.00	0.00	0.05	0.00
29.15	2.00	0.00	0.00	0.05	0.00	29.24	2.00	0.00	0.00	0.09	0.00
29.29	2.00	0.00	0.00	0.05	0.00	29.37	2.00	0.00	0.00	0.07	0.00
29.43	2.00	0.00	0.00	0.06	0.00	29.53	2.00	0.00	0.00	0.10	0.00
29.62	2.00	0.00	0.00	0.09	0.00	29.68	2.00	0.00	0.00	0.06	0.00
29.80	2.00	0.00	0.00	0.12	0.00	29.91	2.00	0.00	0.00	0.12	0.00
30.00	0.61	0.00	0.00	0.09	0.06	30.07	0.62	0.00	0.00	0.07	0.04
30.15	0.62	0.00	0.00	0.08	0.05	30.21	0.62	0.00	0.00	0.07	0.04
30.26	0.62	0.00	0.00	0.05	0.03	30.31	0.61	0.00	0.00	0.05	0.03
30.38	0.61	0.00	0.00	0.07	0.05	30.45	0.60	0.00	0.00	0.07	0.05
30.50	0.60	0.00	0.00	0.05	0.03	30.55	0.59	0.00	0.00	0.05	0.03
30.64	0.58	0.00	0.00	0.09	0.06	30.70	0.56	0.00	0.00	0.05	0.04
30.79	0.55	0.00	0.00	0.09	0.07	30.84	0.54	0.00	0.00	0.05	0.04
30.93	0.54	0.00	0.00	0.09	0.07	30.98	0.54	0.00	0.00	0.05	0.04
31.05	0.55	0.00	0.00	0.06	0.05	31.13	0.56	0.00	0.00	0.08	0.06
31.17	0.58	0.00	0.00	0.05	0.03	31.27	0.61	0.00	0.00	0.10	0.06
31.32	0.67	0.00	0.00	0.05	0.03	31.41	0.73	0.00	0.00	0.10	0.04
31.46	0.78	0.00	0.00	0.05	0.02	31.52	0.80	0.00	0.00	0.06	0.02
31.61	0.79	0.00	0.00	0.08	0.03	31.66	0.76	0.00	0.00	0.06	0.02
31.75	0.71	0.00	0.00	0.09	0.04	31.80	0.66	0.00	0.00	0.05	0.03
31.90	0.61	0.00	0.00	0.10	0.06	31.94	0.59	0.00	0.00	0.05	0.03
32.04	0.59	0.00	0.00	0.10	0.06	32.09	0.62	0.00	0.00	0.04	0.03
32.20	0.63	0.00	0.00	0.11	0.06	32.24	0.65	0.00	0.00	0.04	0.02
32.28	0.65	0.00	0.00	0.04	0.02	32.29	0.66	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
32.30	0.67	0.00	0.00	0.01	0.01	32.40	0.67	0.00	0.00	0.10	0.05
32.45	0.67	0.00	0.00	0.04	0.02	32.55	0.67	0.00	0.00	0.10	0.05
32.59	0.67	0.00	0.00	0.05	0.02	32.69	0.67	0.00	0.00	0.10	0.05
32.76	0.68	0.00	0.00	0.07	0.03	32.84	0.69	0.00	0.00	0.08	0.04
32.90	0.70	0.00	0.00	0.07	0.03	32.98	0.70	0.00	0.00	0.08	0.03
33.06	0.71	0.00	0.00	0.08	0.03	33.12	0.71	0.00	0.00	0.06	0.03
33.22	0.72	0.00	0.00	0.10	0.04	33.31	0.72	0.00	0.00	0.09	0.04
33.37	0.72	0.00	0.00	0.05	0.02	33.46	0.71	0.00	0.00	0.09	0.04
33.55	0.71	0.00	0.00	0.09	0.04	33.65	0.71	0.00	0.00	0.10	0.04
33.70	0.71	0.00	0.00	0.05	0.02	33.79	0.71	0.00	0.00	0.09	0.04
33.89	0.71	0.00	0.00	0.10	0.04	33.99	0.70	0.00	0.00	0.09	0.04
34.04	0.69	0.00	0.00	0.05	0.02	34.13	0.68	0.00	0.00	0.09	0.04
34.23	0.67	0.00	0.00	0.10	0.05	34.32	0.66	0.00	0.00	0.09	0.05
34.37	0.66	0.00	0.00	0.05	0.02	34.47	0.66	0.00	0.00	0.10	0.05
34.55	2.00	0.00	0.00	0.08	0.00	34.63	2.00	0.00	0.00	0.08	0.00
34.73	2.00	0.00	0.00	0.10	0.00	34.80	2.00	0.00	0.00	0.08	0.00
34.90	2.00	0.00	0.00	0.09	0.00	35.00	2.00	0.00	0.00	0.10	0.00
35.12	2.00	0.00	0.00	0.13	0.00	35.20	2.00	0.00	0.00	0.07	0.00
35.33	2.00	0.00	0.00	0.13	0.00	35.41	2.00	0.00	0.00	0.07	0.00
35.44	2.00	0.00	0.00	0.03	0.00	35.48	2.00	0.00	0.00	0.05	0.00
35.57	2.00	0.00	0.00	0.09	0.00	35.62	2.00	0.00	0.00	0.05	0.00
35.67	2.00	0.00	0.00	0.05	0.00	35.71	2.00	0.00	0.00	0.04	0.00
35.82	2.00	0.00	0.00	0.10	0.00	35.86	2.00	0.00	0.00	0.05	0.00
35.93	2.00	0.00	0.00	0.07	0.00	36.01	2.00	0.00	0.00	0.08	0.00
36.06	2.00	0.00	0.00	0.05	0.00	36.12	1.75	0.00	0.00	0.06	0.00
36.18	1.84	0.00	0.00	0.06	0.00	36.25	1.91	0.00	0.00	0.07	0.00
36.30	2.00	0.00	0.00	0.05	0.00	36.39	2.00	0.00	0.00	0.10	0.00
36.44	2.00	0.00	0.00	0.05	0.00	36.53	2.00	0.00	0.00	0.09	0.00
36.59	2.00	0.00	0.00	0.05	0.00	36.68	2.00	0.00	0.00	0.09	0.00
36.75	1.91	0.00	0.00	0.07	0.00	36.83	1.77	0.00	0.00	0.08	0.00
36.90	1.65	0.00	0.00	0.07	0.00	36.97	1.53	0.00	0.00	0.07	0.00
37.02	1.31	0.00	0.00	0.05	0.00	37.04	1.21	0.00	0.00	0.02	0.00
37.08	1.14	0.00	0.00	0.04	0.00	37.17	1.16	0.00	0.00	0.09	0.00
37.27	1.09	0.00	0.00	0.10	0.00	37.37	1.02	0.00	0.00	0.09	0.00
37.42	0.96	0.00	0.00	0.05	0.00	37.51	0.93	0.00	0.00	0.09	0.01
37.58	0.92	0.00	0.00	0.07	0.01	37.66	0.93	0.00	0.00	0.07	0.01
37.76	0.95	0.00	0.00	0.10	0.01	37.85	0.96	0.00	0.00	0.09	0.00
37.93	0.97	0.00	0.00	0.08	0.00	38.04	0.98	0.00	0.00	0.11	0.00
38.13	0.99	0.00	0.00	0.09	0.00	38.18	0.99	0.00	0.00	0.05	0.00
38.28	0.98	0.00	0.00	0.10	0.00	38.37	0.95	0.00	0.00	0.09	0.01
38.47	0.93	0.00	0.00	0.09	0.01	38.57	0.91	0.00	0.00	0.10	0.01
38.62	0.88	0.00	0.00	0.04	0.01	38.72	0.81	0.00	0.00	0.10	0.02
38.78	0.76	0.00	0.00	0.06	0.02	38.81	0.74	0.00	0.00	0.02	0.01
38.86	0.74	0.00	0.00	0.05	0.02	38.91	0.72	0.00	0.00	0.05	0.02
38.95	0.70	0.00	0.00	0.05	0.02	39.05	0.68	0.00	0.00	0.10	0.04
39.09	0.67	0.00	0.00	0.05	0.02	39.14	0.66	0.00	0.00	0.05	0.02
39.24	0.65	0.00	0.00	0.10	0.04	39.29	0.65	0.00	0.00	0.05	0.02
39.39	0.65	0.00	0.00	0.10	0.04	39.43	0.65	0.00	0.00	0.05	0.02

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
39.53	0.65	0.00	0.00	0.10	0.04	39.57	0.64	0.00	0.00	0.04	0.02
39.68	0.64	0.00	0.00	0.10	0.04	39.73	0.64	0.00	0.00	0.05	0.02
39.81	0.63	0.00	0.00	0.08	0.04	39.89	0.60	0.00	0.00	0.08	0.04
39.96	0.56	0.00	0.00	0.07	0.03	40.06	0.54	0.00	0.00	0.10	0.05
40.15	0.53	0.00	0.00	0.09	0.05	40.20	0.53	0.00	0.00	0.06	0.03
40.24	0.53	0.00	0.00	0.04	0.02	40.26	0.54	0.00	0.00	0.01	0.01
40.27	0.54	0.00	0.00	0.02	0.01	40.37	0.55	0.00	0.00	0.09	0.05
40.42	0.55	0.00	0.00	0.05	0.02	40.52	0.56	0.00	0.00	0.10	0.05
40.56	0.57	0.00	0.00	0.04	0.02	40.66	0.58	0.00	0.00	0.10	0.05
40.70	0.61	0.00	0.00	0.05	0.02	40.75	0.65	0.00	0.00	0.05	0.02
40.85	0.71	0.00	0.00	0.10	0.03	40.91	0.77	0.00	0.00	0.06	0.01
40.96	0.85	0.00	0.00	0.05	0.01	41.04	0.92	0.00	0.00	0.08	0.01
41.09	1.01	0.00	0.00	0.05	0.00	41.18	1.08	0.00	0.00	0.09	0.00
41.23	1.15	0.00	0.00	0.05	0.00	41.29	1.19	0.00	0.00	0.06	0.00
41.38	1.19	0.00	0.00	0.09	0.00	41.42	1.19	0.00	0.00	0.05	0.00
41.52	1.16	0.00	0.00	0.10	0.00	41.57	1.13	0.00	0.00	0.05	0.00
41.62	1.11	0.00	0.00	0.05	0.00	41.71	1.09	0.00	0.00	0.09	0.00
41.76	1.08	0.00	0.00	0.04	0.00	41.84	1.08	0.00	0.00	0.09	0.00
41.91	1.08	0.00	0.00	0.07	0.00	41.95	1.08	0.00	0.00	0.05	0.00
42.01	1.10	0.00	0.00	0.06	0.00	42.10	1.11	0.00	0.00	0.08	0.00
42.15	1.14	0.00	0.00	0.05	0.00	42.24	1.16	0.00	0.00	0.09	0.00
42.28	1.17	0.00	0.00	0.04	0.00	42.39	1.16	0.00	0.00	0.10	0.00
42.43	1.14	0.00	0.00	0.04	0.00	42.50	1.13	0.00	0.00	0.07	0.00
42.58	1.12	0.00	0.00	0.08	0.00	42.65	1.03	0.00	0.00	0.07	0.00
42.70	1.00	0.00	0.00	0.06	0.00	42.73	0.97	0.00	0.00	0.02	0.00
42.77	1.02	0.00	0.00	0.04	0.00	42.82	1.05	0.00	0.00	0.05	0.00
42.87	1.10	0.00	0.00	0.05	0.00	42.91	1.17	0.00	0.00	0.04	0.00
42.97	1.24	0.00	0.00	0.05	0.00	43.02	1.30	0.00	0.00	0.05	0.00
43.06	1.35	0.00	0.00	0.05	0.00	43.11	1.40	0.00	0.00	0.04	0.00
43.17	1.45	0.00	0.00	0.06	0.00	43.21	1.51	0.00	0.00	0.04	0.00
43.29	1.55	0.00	0.00	0.08	0.00	43.34	1.61	0.00	0.00	0.05	0.00
43.39	1.65	0.00	0.00	0.06	0.00	43.45	1.67	0.00	0.00	0.05	0.00
43.51	1.66	0.00	0.00	0.06	0.00	43.59	1.64	0.00	0.00	0.08	0.00
43.64	1.60	0.00	0.00	0.05	0.00	43.70	1.54	0.00	0.00	0.06	0.00
43.78	1.47	0.00	0.00	0.09	0.00	43.88	1.43	0.00	0.00	0.10	0.00
43.94	1.39	0.00	0.00	0.06	0.00	44.04	1.31	0.00	0.00	0.10	0.00
44.07	1.22	0.00	0.00	0.03	0.00	44.12	1.20	0.00	0.00	0.05	0.00
44.16	1.17	0.00	0.00	0.04	0.00	44.21	1.14	0.00	0.00	0.05	0.00
44.26	1.10	0.00	0.00	0.05	0.00	44.31	1.06	0.00	0.00	0.05	0.00
44.35	1.03	0.00	0.00	0.04	0.00	44.40	0.99	0.00	0.00	0.05	0.00
44.45	0.96	0.00	0.00	0.05	0.00	44.50	0.94	0.00	0.00	0.05	0.00
44.54	0.93	0.00	0.00	0.04	0.00	44.60	0.91	0.00	0.00	0.06	0.01
44.64	0.89	0.00	0.00	0.05	0.00	44.69	0.88	0.00	0.00	0.05	0.01
44.74	0.87	0.00	0.00	0.05	0.01	44.79	0.87	0.00	0.00	0.04	0.01
44.83	0.87	0.00	0.00	0.05	0.01	44.88	0.88	0.00	0.00	0.05	0.01
44.93	0.89	0.00	0.00	0.05	0.01	44.98	0.91	0.00	0.00	0.05	0.00
45.03	0.92	0.00	0.00	0.05	0.00	45.08	0.93	0.00	0.00	0.06	0.00
45.16	0.94	0.00	0.00	0.08	0.00	45.19	0.94	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
45.27	0.93	0.00	0.00	0.08	0.01	45.32	0.92	0.00	0.00	0.05	0.00
45.37	0.89	0.00	0.00	0.05	0.00	45.45	0.85	0.00	0.00	0.09	0.01
45.51	0.80	0.00	0.00	0.05	0.01	45.56	2.00	0.00	0.00	0.05	0.00
45.61	2.00	0.00	0.00	0.05	0.00	45.69	2.00	0.00	0.00	0.08	0.00
45.75	2.00	0.00	0.00	0.06	0.00	45.81	2.00	0.00	0.00	0.07	0.00
45.89	2.00	0.00	0.00	0.08	0.00	45.94	2.00	0.00	0.00	0.05	0.00
46.04	2.00	0.00	0.00	0.10	0.00	46.08	2.00	0.00	0.00	0.04	0.00
46.15	2.00	0.00	0.00	0.06	0.00	46.17	2.00	0.00	0.00	0.02	0.00
46.18	2.00	0.00	0.00	0.01	0.00	46.23	2.00	0.00	0.00	0.05	0.00
46.27	2.00	0.00	0.00	0.05	0.00	46.32	2.00	0.00	0.00	0.05	0.00
46.41	2.00	0.00	0.00	0.09	0.00	46.47	2.00	0.00	0.00	0.06	0.00
46.52	2.00	0.00	0.00	0.05	0.00	46.56	2.00	0.00	0.00	0.04	0.00
46.65	2.00	0.00	0.00	0.09	0.00	46.71	2.00	0.00	0.00	0.06	0.00
46.76	2.00	0.00	0.00	0.05	0.00	46.85	2.00	0.00	0.00	0.09	0.00
46.90	2.00	0.00	0.00	0.05	0.00	46.99	2.00	0.00	0.00	0.09	0.00
47.04	2.00	0.00	0.00	0.06	0.00	47.10	2.00	0.00	0.00	0.05	0.00
47.16	2.00	0.00	0.00	0.06	0.00	47.23	2.00	0.00	0.00	0.07	0.00
47.30	2.00	0.00	0.00	0.06	0.00	47.38	2.00	0.00	0.00	0.09	0.00
47.43	2.00	0.00	0.00	0.05	0.00	47.52	2.00	0.00	0.00	0.09	0.00
47.59	2.00	0.00	0.00	0.07	0.00	47.66	2.00	0.00	0.00	0.07	0.00
47.77	2.00	0.00	0.00	0.10	0.00	47.82	2.00	0.00	0.00	0.05	0.00
47.91	2.00	0.00	0.00	0.08	0.00	47.93	2.00	0.00	0.00	0.03	0.00
47.97	2.00	0.00	0.00	0.04	0.00	48.02	2.00	0.00	0.00	0.05	0.00
48.07	2.00	0.00	0.00	0.05	0.00	48.12	2.00	0.00	0.00	0.05	0.00
48.19	2.00	0.00	0.00	0.07	0.00	48.23	2.00	0.00	0.00	0.04	0.00
48.31	2.00	0.00	0.00	0.08	0.00	48.35	2.00	0.00	0.00	0.05	0.00
48.40	2.00	0.00	0.00	0.05	0.00	48.45	2.00	0.00	0.00	0.05	0.00
48.50	2.00	0.00	0.00	0.05	0.00	48.55	2.00	0.00	0.00	0.05	0.00
48.59	2.00	0.00	0.00	0.04	0.00	48.67	2.00	0.00	0.00	0.08	0.00
48.73	2.00	0.00	0.00	0.05	0.00	48.78	2.00	0.00	0.00	0.06	0.00
48.83	2.00	0.00	0.00	0.05	0.00	48.91	2.00	0.00	0.00	0.07	0.00
48.98	2.00	0.00	0.00	0.07	0.00	49.03	2.00	0.00	0.00	0.05	0.00
49.12	2.00	0.00	0.00	0.09	0.00	49.17	2.00	0.00	0.00	0.05	0.00
49.27	2.00	0.00	0.00	0.09	0.00	49.31	2.00	0.00	0.00	0.05	0.00
49.38	2.00	0.00	0.00	0.06	0.00	49.45	2.00	0.00	0.00	0.08	0.00
49.51	2.00	0.00	0.00	0.05	0.00	49.54	2.00	0.00	0.00	0.03	0.00
49.59	2.00	0.00	0.00	0.05	0.00	49.64	2.00	0.00	0.00	0.05	0.00
49.73	2.00	0.00	0.00	0.10	0.00	49.83	2.00	0.00	0.00	0.10	0.00
49.92	2.00	0.00	0.00	0.10	0.00	49.98	2.00	0.00	0.00	0.05	0.00
50.07	2.00	0.00	0.00	0.09	0.00	50.16	2.00	0.00	0.00	0.09	0.00
50.24	2.00	0.00	0.00	0.09	0.00	50.32	2.00	0.00	0.00	0.08	0.00
50.41	2.00	0.00	0.00	0.09	0.00	50.50	2.00	0.00	0.00	0.09	0.00
50.56	2.00	0.00	0.00	0.06	0.00	50.66	2.00	0.00	0.00	0.10	0.00
50.74	2.00	0.00	0.00	0.09	0.00	50.84	2.00	0.00	0.00	0.10	0.00
50.93	2.00	0.00	0.00	0.09	0.00	50.98	2.00	0.00	0.00	0.05	0.00
51.08	2.00	0.00	0.00	0.09	0.00	51.17	2.00	0.00	0.00	0.10	0.00
51.24	2.00	0.00	0.00	0.06	0.00	51.34	2.00	0.00	0.00	0.10	0.00
51.41	2.00	0.00	0.00	0.07	0.00	51.51	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
51.58	2.00	0.00	0.00	0.07	0.00	51.68	2.00	0.00	0.00	0.10	0.00
51.79	2.00	0.00	0.00	0.11	0.00	51.82	2.00	0.00	0.00	0.03	0.00
51.85	2.00	0.00	0.00	0.03	0.00	51.91	2.00	0.00	0.00	0.06	0.00
52.00	2.00	0.00	0.00	0.09	0.00	52.05	2.00	0.00	0.00	0.05	0.00
52.10	2.00	0.00	0.00	0.06	0.00	52.19	2.00	0.00	0.00	0.09	0.00
52.28	2.00	0.00	0.00	0.09	0.00	52.34	2.00	0.00	0.00	0.06	0.00
52.42	2.00	0.00	0.00	0.08	0.00	52.48	2.00	0.00	0.00	0.06	0.00
52.57	2.00	0.00	0.00	0.09	0.00	52.62	2.00	0.00	0.00	0.05	0.00
52.69	2.00	0.00	0.00	0.07	0.00	52.77	2.00	0.00	0.00	0.08	0.00
52.87	2.00	0.00	0.00	0.10	0.00	52.91	2.00	0.00	0.00	0.04	0.00
53.01	2.00	0.00	0.00	0.10	0.00	53.10	2.00	0.00	0.00	0.09	0.00
53.16	2.00	0.00	0.00	0.06	0.00	53.25	2.00	0.00	0.00	0.09	0.00
53.29	2.00	0.00	0.00	0.04	0.00	53.38	2.00	0.00	0.00	0.09	0.00
53.42	2.00	0.00	0.00	0.04	0.00	53.47	2.00	0.00	0.00	0.05	0.00
53.52	2.00	0.00	0.00	0.05	0.00	53.58	2.00	0.00	0.00	0.05	0.00
53.66	2.00	0.00	0.00	0.08	0.00	53.75	2.00	0.00	0.00	0.09	0.00
53.81	2.00	0.00	0.00	0.05	0.00	53.87	2.00	0.00	0.00	0.06	0.00
53.95	2.00	0.00	0.00	0.08	0.00	54.01	2.00	0.00	0.00	0.06	0.00
54.06	2.00	0.00	0.00	0.05	0.00	54.15	2.00	0.00	0.00	0.08	0.00
54.20	2.00	0.00	0.00	0.06	0.00	54.29	2.00	0.00	0.00	0.08	0.00
54.34	2.00	0.00	0.00	0.05	0.00	54.43	2.00	0.00	0.00	0.09	0.00
54.45	2.00	0.00	0.00	0.02	0.00	54.48	2.00	0.00	0.00	0.03	0.00
54.52	2.00	0.00	0.00	0.03	0.00	54.53	2.00	0.00	0.00	0.01	0.00
54.58	0.45	0.00	0.00	0.05	0.01	54.62	0.47	0.00	0.00	0.04	0.01
54.65	0.50	0.00	0.00	0.03	0.01	54.70	0.52	0.00	0.00	0.04	0.01
54.76	0.54	0.00	0.00	0.06	0.01	54.77	0.55	0.00	0.00	0.01	0.00
54.82	0.55	0.00	0.00	0.05	0.01	54.87	0.56	0.00	0.00	0.05	0.01
54.88	0.56	0.00	0.00	0.01	0.00	54.91	0.56	0.00	0.00	0.03	0.01
54.96	0.58	0.00	0.00	0.05	0.01	54.97	0.62	0.00	0.00	0.01	0.00
55.03	0.68	0.00	0.00	0.06	0.01	55.09	0.74	0.00	0.00	0.06	0.01
55.15	0.75	0.00	0.00	0.06	0.01	55.20	0.76	0.00	0.00	0.05	0.01
55.25	0.75	0.00	0.00	0.05	0.01	55.30	0.85	0.00	0.00	0.05	0.00
55.34	0.93	0.00	0.00	0.05	0.00	55.39	1.12	0.00	0.00	0.04	0.00
55.40	1.27	0.00	0.00	0.01	0.00	55.44	1.34	0.00	0.00	0.04	0.00
55.44	1.34	0.00	0.00	0.01	0.00	55.49	1.42	0.00	0.00	0.05	0.00
55.54	1.58	0.00	0.00	0.05	0.00	55.59	1.79	0.00	0.00	0.05	0.00
55.63	1.90	0.00	0.00	0.04	0.00	55.64	1.91	0.00	0.00	0.01	0.00
55.68	1.89	0.00	0.00	0.04	0.00	55.69	1.85	0.00	0.00	0.01	0.00
55.69	1.88	0.00	0.00	0.01	0.00	55.71	1.98	0.00	0.00	0.02	0.00
55.76	2.00	0.00	0.00	0.05	0.00	55.78	2.00	0.00	0.00	0.02	0.00
55.81	1.92	0.00	0.00	0.04	0.00	55.85	1.77	0.00	0.00	0.04	0.00
55.86	1.80	0.00	0.00	0.01	0.00	55.91	1.88	0.00	0.00	0.05	0.00
55.92	1.91	0.00	0.00	0.01	0.00	55.96	2.00	0.00	0.00	0.04	0.00
55.97	2.00	0.00	0.00	0.01	0.00	56.00	2.00	0.00	0.00	0.03	0.00
56.01	2.00	0.00	0.00	0.01	0.00	56.03	2.00	0.00	0.00	0.02	0.00
56.05	2.00	0.00	0.00	0.02	0.00	56.10	2.00	0.00	0.00	0.05	0.00
56.12	2.00	0.00	0.00	0.02	0.00	56.16	2.00	0.00	0.00	0.04	0.00
56.17	2.00	0.00	0.00	0.02	0.00	56.20	2.00	0.00	0.00	0.03	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
56.22	2.00	0.00	0.00	0.02	0.00	56.24	1.95	0.00	0.00	0.03	0.00
56.30	1.89	0.00	0.00	0.06	0.00	56.31	1.84	0.00	0.00	0.01	0.00
56.34	1.76	0.00	0.00	0.03	0.00	56.39	1.70	0.00	0.00	0.05	0.00
56.45	1.65	0.00	0.00	0.06	0.00	56.48	1.60	0.00	0.00	0.03	0.00
56.49	1.53	0.00	0.00	0.01	0.00	56.53	1.60	0.00	0.00	0.04	0.00
56.58	1.62	0.00	0.00	0.05	0.00	56.63	1.32	0.00	0.00	0.05	0.00
56.68	1.33	0.00	0.00	0.04	0.00	56.73	1.36	0.00	0.00	0.05	0.00
56.78	1.33	0.00	0.00	0.05	0.00	56.83	1.27	0.00	0.00	0.05	0.00
56.89	1.35	0.00	0.00	0.07	0.00	56.95	1.43	0.00	0.00	0.06	0.00
56.99	1.44	0.00	0.00	0.04	0.00	57.01	1.43	0.00	0.00	0.01	0.00
57.04	1.43	0.00	0.00	0.04	0.00	57.09	1.44	0.00	0.00	0.05	0.00
57.11	1.49	0.00	0.00	0.02	0.00	57.13	1.58	0.00	0.00	0.03	0.00
57.18	1.63	0.00	0.00	0.04	0.00	57.19	1.62	0.00	0.00	0.01	0.00
57.21	1.56	0.00	0.00	0.03	0.00	57.24	1.50	0.00	0.00	0.02	0.00
57.28	1.49	0.00	0.00	0.05	0.00	57.32	1.44	0.00	0.00	0.04	0.00
57.35	1.41	0.00	0.00	0.04	0.00	57.38	1.36	0.00	0.00	0.03	0.00
57.43	1.32	0.00	0.00	0.04	0.00	57.48	1.21	0.00	0.00	0.05	0.00
57.52	1.10	0.00	0.00	0.05	0.00	57.57	1.07	0.00	0.00	0.05	0.00
57.62	1.14	0.00	0.00	0.05	0.00	57.68	1.35	0.00	0.00	0.06	0.00
57.76	1.55	0.00	0.00	0.08	0.00	57.81	1.44	0.00	0.00	0.05	0.00
57.86	1.40	0.00	0.00	0.05	0.00	57.89	1.60	0.00	0.00	0.03	0.00
57.91	1.68	0.00	0.00	0.02	0.00	57.92	1.63	0.00	0.00	0.01	0.00
57.95	1.57	0.00	0.00	0.03	0.00	57.99	1.58	0.00	0.00	0.04	0.00
58.01	1.64	0.00	0.00	0.02	0.00	58.05	1.73	0.00	0.00	0.04	0.00
58.05	1.79	0.00	0.00	0.01	0.00	58.10	1.83	0.00	0.00	0.05	0.00
58.13	1.88	0.00	0.00	0.03	0.00	58.15	1.94	0.00	0.00	0.01	0.00
58.17	1.99	0.00	0.00	0.03	0.00	58.20	1.98	0.00	0.00	0.02	0.00
58.21	1.94	0.00	0.00	0.01	0.00	58.21	1.90	0.00	0.00	0.00	0.00
58.23	1.90	0.00	0.00	0.02	0.00	58.24	1.85	0.00	0.00	0.01	0.00
58.25	1.86	0.00	0.00	0.01	0.00	58.29	1.90	0.00	0.00	0.04	0.00
58.31	2.00	0.00	0.00	0.02	0.00	58.33	2.00	0.00	0.00	0.02	0.00
58.38	2.00	0.00	0.00	0.05	0.00	58.39	2.00	0.00	0.00	0.01	0.00
58.43	2.00	0.00	0.00	0.04	0.00	58.43	2.00	0.00	0.00	0.01	0.00
58.48	2.00	0.00	0.00	0.05	0.00	58.53	2.00	0.00	0.00	0.05	0.00
58.56	2.00	0.00	0.00	0.02	0.00	58.58	2.00	0.00	0.00	0.03	0.00
58.59	2.00	0.00	0.00	0.01	0.00	58.63	2.00	0.00	0.00	0.03	0.00
58.63	2.00	0.00	0.00	0.00	0.00	58.63	2.00	0.00	0.00	0.01	0.00
58.68	2.00	0.00	0.00	0.04	0.00	58.69	2.00	0.00	0.00	0.01	0.00
58.72	2.00	0.00	0.00	0.03	0.00	58.73	2.00	0.00	0.00	0.01	0.00
58.74	2.00	0.00	0.00	0.01	0.00	58.77	2.00	0.00	0.00	0.03	0.00
58.81	2.00	0.00	0.00	0.04	0.00	58.82	2.00	0.00	0.00	0.01	0.00
58.83	2.00	0.00	0.00	0.01	0.00	58.87	2.00	0.00	0.00	0.04	0.00
58.91	2.00	0.00	0.00	0.04	0.00	58.92	2.00	0.00	0.00	0.01	0.00
58.93	2.00	0.00	0.00	0.01	0.00	58.96	2.00	0.00	0.00	0.03	0.00
59.01	2.00	0.00	0.00	0.05	0.00	59.06	2.00	0.00	0.00	0.05	0.00
59.08	2.00	0.00	0.00	0.02	0.00	59.11	2.00	0.00	0.00	0.03	0.00
59.15	1.96	0.00	0.00	0.04	0.00	59.21	1.89	0.00	0.00	0.05	0.00
59.26	1.89	0.00	0.00	0.05	0.00	59.30	1.74	0.00	0.00	0.04	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
59.35	1.64	0.00	0.00	0.05	0.00	59.40	1.63	0.00	0.00	0.05	0.00
59.42	1.62	0.00	0.00	0.02	0.00	59.47	1.61	0.00	0.00	0.05	0.00
59.51	1.63	0.00	0.00	0.05	0.00	59.56	1.63	0.00	0.00	0.05	0.00
59.61	1.53	0.00	0.00	0.05	0.00	59.67	1.34	0.00	0.00	0.05	0.00
59.71	1.41	0.00	0.00	0.04	0.00	59.80	1.42	0.00	0.00	0.09	0.00
59.85	1.40	0.00	0.00	0.05	0.00	59.90	1.33	0.00	0.00	0.05	0.00
60.00	1.33	0.00	0.00	0.10	0.00	60.04	1.33	0.00	0.00	0.05	0.00
60.10	1.23	0.00	0.00	0.06	0.00	60.15	1.13	0.00	0.00	0.05	0.00
60.19	1.03	0.00	0.00	0.03	0.00	60.23	1.01	0.00	0.00	0.05	0.00
60.28	1.00	0.00	0.00	0.05	0.00	60.33	1.03	0.00	0.00	0.05	0.00
60.38	1.05	0.00	0.00	0.04	0.00	60.42	1.05	0.00	0.00	0.04	0.00
60.44	1.05	0.00	0.00	0.02	0.00	60.47	1.14	0.00	0.00	0.02	0.00
60.52	1.20	0.00	0.00	0.05	0.00	60.56	1.24	0.00	0.00	0.04	0.00
60.57	1.25	0.00	0.00	0.01	0.00	60.61	1.25	0.00	0.00	0.04	0.00
60.66	1.27	0.00	0.00	0.05	0.00	60.71	1.29	0.00	0.00	0.05	0.00
60.76	1.36	0.00	0.00	0.05	0.00	60.81	1.43	0.00	0.00	0.05	0.00
60.86	1.46	0.00	0.00	0.05	0.00	60.91	1.41	0.00	0.00	0.05	0.00
60.95	1.69	0.00	0.00	0.04	0.00	61.00	1.97	0.00	0.00	0.05	0.00
61.02	2.00	0.00	0.00	0.02	0.00	61.05	2.00	0.00	0.00	0.03	0.00
61.08	2.00	0.00	0.00	0.03	0.00	61.09	2.00	0.00	0.00	0.02	0.00
61.13	2.00	0.00	0.00	0.03	0.00	61.14	2.00	0.00	0.00	0.02	0.00
61.16	2.00	0.00	0.00	0.02	0.00	61.20	2.00	0.00	0.00	0.03	0.00
61.23	2.00	0.00	0.00	0.04	0.00	61.24	2.00	0.00	0.00	0.01	0.00
61.29	2.00	0.00	0.00	0.05	0.00	61.30	2.00	0.00	0.00	0.01	0.00
61.33	2.00	0.00	0.00	0.04	0.00	61.38	2.00	0.00	0.00	0.05	0.00
61.43	2.00	0.00	0.00	0.05	0.00	61.48	2.00	0.00	0.00	0.04	0.00
61.53	2.00	0.00	0.00	0.05	0.00	61.56	2.00	0.00	0.00	0.03	0.00
61.58	2.00	0.00	0.00	0.02	0.00	61.59	2.00	0.00	0.00	0.01	0.00
61.62	1.66	0.00	0.00	0.03	0.00	61.63	1.62	0.00	0.00	0.02	0.00
61.67	1.57	0.00	0.00	0.03	0.00	61.71	2.00	0.00	0.00	0.05	0.00
61.76	2.00	0.00	0.00	0.05	0.00	61.81	1.90	0.00	0.00	0.05	0.00
61.86	1.75	0.00	0.00	0.05	0.00	61.87	1.65	0.00	0.00	0.01	0.00
61.91	1.57	0.00	0.00	0.04	0.00	61.95	1.49	0.00	0.00	0.04	0.00
61.96	1.42	0.00	0.00	0.01	0.00	62.00	1.34	0.00	0.00	0.04	0.00
62.04	1.23	0.00	0.00	0.04	0.00	62.06	1.11	0.00	0.00	0.02	0.00
62.10	1.01	0.00	0.00	0.04	0.00	62.14	0.94	0.00	0.00	0.04	0.00
62.20	0.88	0.00	0.00	0.05	0.00	62.22	0.79	0.00	0.00	0.02	0.00
62.27	0.82	0.00	0.00	0.05	0.00	62.29	0.83	0.00	0.00	0.02	0.00
62.34	0.81	0.00	0.00	0.05	0.00	62.39	0.80	0.00	0.00	0.04	0.00
62.43	0.77	0.00	0.00	0.05	0.00	62.49	0.77	0.00	0.00	0.06	0.00
62.57	0.78	0.00	0.00	0.08	0.00	62.68	0.86	0.00	0.00	0.10	0.00
62.75	1.04	0.00	0.00	0.08	0.00	62.87	1.18	0.00	0.00	0.12	0.00
62.88	1.09	0.00	0.00	0.01	0.00	62.89	1.09	0.00	0.00	0.01	0.00
62.93	1.10	0.00	0.00	0.04	0.00	62.98	1.42	0.00	0.00	0.05	0.00
63.02	1.75	0.00	0.00	0.05	0.00	63.07	2.00	0.00	0.00	0.05	0.00
63.12	2.00	0.00	0.00	0.05	0.00	63.14	2.00	0.00	0.00	0.02	0.00
63.17	2.00	0.00	0.00	0.03	0.00	63.17	2.00	0.00	0.00	0.01	0.00
63.20	2.00	0.00	0.00	0.02	0.00	63.21	2.00	0.00	0.00	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
63.23	2.00	0.00	0.00	0.02	0.00	63.26	2.00	0.00	0.00	0.03	0.00
63.28	2.00	0.00	0.00	0.02	0.00	63.31	2.00	0.00	0.00	0.03	0.00
63.32	2.00	0.00	0.00	0.01	0.00	63.36	2.00	0.00	0.00	0.04	0.00
63.40	2.00	0.00	0.00	0.04	0.00						

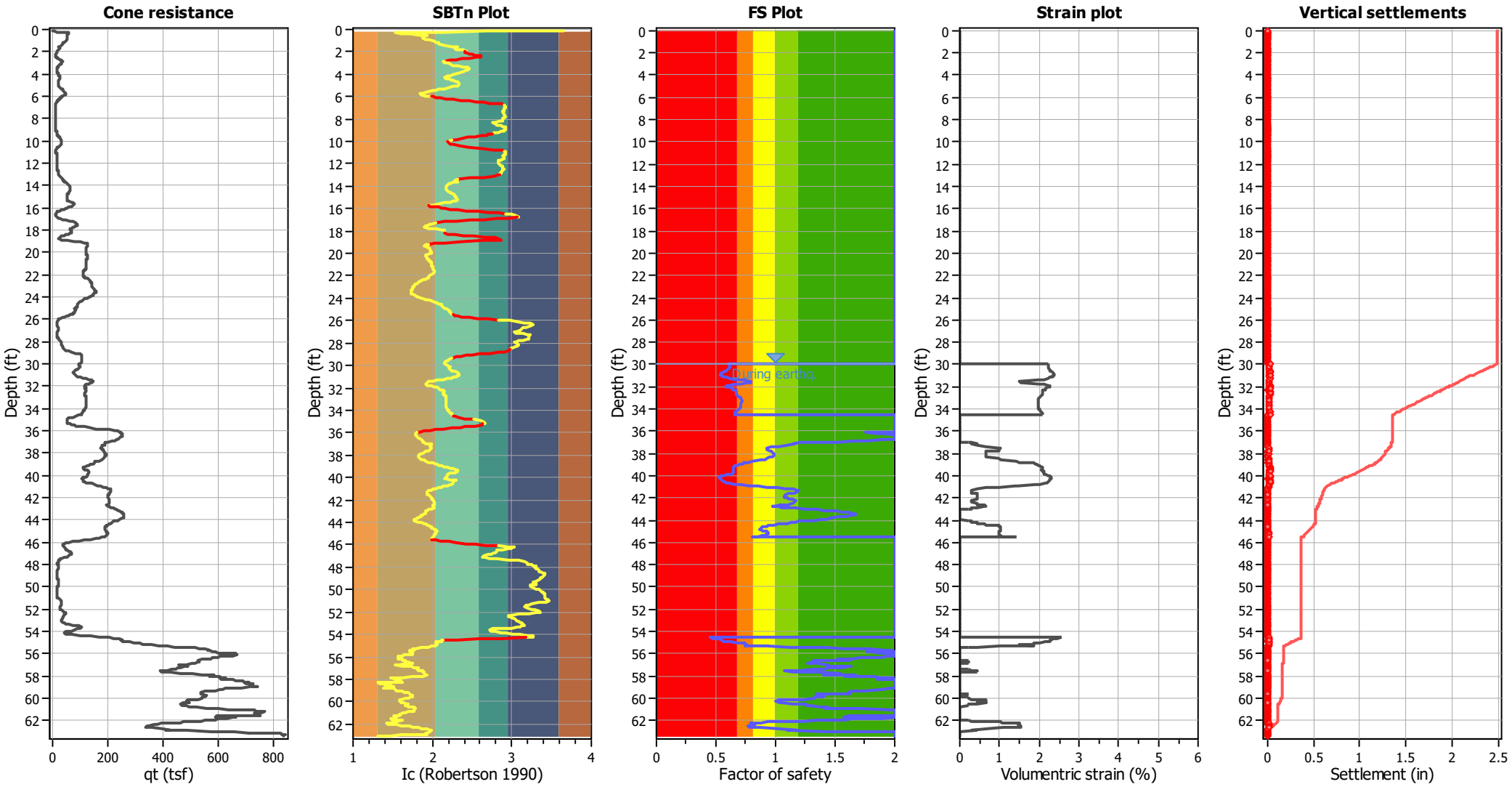
Overall liquefaction potential: 3.79

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
30.00	104.86	0.61	2.25	1.00	0.02	30.07	105.36	0.62	2.24	1.00	0.02
30.15	105.54	0.62	2.24	1.00	0.02	30.21	105.77	0.62	2.23	1.00	0.02
30.26	105.66	0.62	2.23	1.00	0.01	30.31	105.39	0.61	2.24	1.00	0.01
30.38	104.86	0.61	2.25	1.00	0.02	30.45	104.23	0.60	2.26	1.00	0.02
30.50	103.72	0.60	2.27	1.00	0.01	30.55	102.88	0.59	2.28	1.00	0.01
30.64	101.83	0.58	2.30	1.00	0.03	30.70	100.16	0.56	2.33	1.00	0.01
30.79	98.96	0.55	2.36	1.00	0.03	30.84	98.19	0.54	2.37	1.00	0.01
30.93	98.05	0.54	2.37	1.00	0.03	30.98	98.14	0.54	2.37	1.00	0.01
31.05	98.98	0.55	2.36	1.00	0.02	31.13	100.51	0.56	2.33	1.00	0.02
31.17	102.97	0.58	2.28	1.00	0.01	31.27	106.25	0.61	2.22	1.00	0.03
31.32	111.37	0.67	2.11	1.00	0.01	31.41	116.56	0.73	1.98	1.00	0.02
31.46	120.72	0.78	1.54	1.00	0.01	31.52	122.24	0.80	1.52	1.00	0.01
31.61	121.83	0.79	1.52	1.00	0.02	31.66	119.20	0.76	1.57	1.00	0.01
31.75	115.29	0.71	2.01	1.00	0.02	31.80	110.68	0.66	2.13	1.00	0.01
31.90	106.52	0.61	2.22	1.00	0.03	31.94	104.07	0.59	2.26	1.00	0.01
32.04	104.00	0.59	2.26	1.00	0.03	32.09	107.23	0.62	2.21	1.00	0.01
32.20	109.06	0.63	2.18	1.00	0.03	32.24	110.44	0.65	2.15	1.00	0.01
32.28	110.26	0.65	2.16	1.00	0.01	32.29	111.09	0.66	2.12	1.00	0.00
32.30	112.06	0.67	2.09	1.00	0.00	32.40	112.71	0.67	2.07	1.00	0.02
32.45	112.95	0.67	2.07	1.00	0.01	32.55	112.51	0.67	2.08	1.00	0.02
32.59	112.50	0.67	2.08	1.00	0.01	32.69	112.79	0.67	2.07	1.00	0.02
32.76	113.51	0.68	2.05	1.00	0.02	32.84	114.35	0.69	2.03	1.00	0.02
32.90	115.19	0.70	2.01	1.00	0.02	32.98	115.83	0.70	2.00	1.00	0.02
33.06	116.33	0.71	1.98	1.00	0.02	33.12	116.77	0.71	1.97	1.00	0.02
33.22	117.03	0.72	1.97	1.00	0.02	33.31	117.14	0.72	1.96	1.00	0.02
33.37	117.11	0.72	1.96	1.00	0.01	33.46	117.00	0.71	1.97	1.00	0.02
33.55	117.00	0.71	1.97	1.00	0.02	33.65	117.07	0.71	1.97	1.00	0.02
33.70	117.18	0.71	1.96	1.00	0.01	33.79	117.10	0.71	1.97	1.00	0.02
33.89	116.76	0.71	1.97	1.00	0.02	33.99	116.20	0.70	1.99	1.00	0.02
34.04	115.43	0.69	2.01	1.00	0.01	34.13	114.59	0.68	2.03	1.00	0.02
34.23	113.76	0.67	2.05	1.00	0.02	34.32	113.20	0.66	2.06	1.00	0.02
34.37	112.84	0.66	2.07	1.00	0.01	34.47	112.69	0.66	2.08	1.00	0.02
34.55	112.96	2.00	0.00	1.00	0.00	34.63	114.64	2.00	0.00	1.00	0.00
34.73	118.21	2.00	0.00	1.00	0.00	34.80	123.59	2.00	0.00	1.00	0.00
34.90	127.28	2.00	0.00	1.00	0.00	35.00	121.79	2.00	0.00	1.00	0.00
35.12	117.31	2.00	0.00	1.00	0.00	35.20	112.19	2.00	0.00	1.00	0.00
35.33	114.42	2.00	0.00	1.00	0.00	35.41	110.34	2.00	0.00	1.00	0.00
35.44	108.02	2.00	0.00	1.00	0.00	35.48	103.82	2.00	0.00	1.00	0.00
35.57	101.05	2.00	0.00	1.00	0.00	35.62	98.99	2.00	0.00	1.00	0.00
35.67	102.07	2.00	0.00	1.00	0.00	35.71	112.52	2.00	0.00	1.00	0.00
35.82	126.36	2.00	0.00	1.00	0.00	35.86	143.07	2.00	0.00	1.00	0.00
35.93	156.85	2.00	0.00	1.00	0.00	36.01	166.33	2.00	0.00	1.00	0.00
36.06	171.69	2.00	0.00	1.00	0.00	36.12	174.89	1.75	0.00	1.00	0.00
36.18	178.20	1.84	0.00	1.00	0.00	36.25	180.98	1.91	0.00	1.00	0.00
36.30	184.12	2.00	0.00	1.00	0.00	36.39	185.99	2.00	0.00	1.00	0.00
36.44	187.57	2.00	0.00	1.00	0.00	36.53	187.51	2.00	0.00	1.00	0.00
36.59	187.43	2.00	0.00	1.00	0.00	36.68	184.49	2.00	0.00	1.00	0.00
36.75	180.99	1.91	0.00	1.00	0.00	36.83	175.91	1.77	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
36.90	171.34	1.65	0.00	1.00	0.00	36.97	166.05	1.53	0.00	1.00	0.00
37.02	156.23	1.31	0.21	1.00	0.00	37.04	151.13	1.21	0.30	1.00	0.00
37.08	147.61	1.14	0.43	1.00	0.00	37.17	148.65	1.16	0.31	1.00	0.00
37.27	145.04	1.09	0.43	1.00	0.01	37.37	140.68	1.02	0.64	1.00	0.01
37.42	137.22	0.96	0.66	1.00	0.00	37.51	135.25	0.93	1.00	1.00	0.01
37.58	134.76	0.92	1.01	1.00	0.01	37.66	135.08	0.93	1.00	1.00	0.01
37.76	136.26	0.95	0.99	1.00	0.01	37.85	137.18	0.96	0.66	1.00	0.01
37.93	138.14	0.97	0.65	1.00	0.01	38.04	138.80	0.98	0.65	1.00	0.01
38.13	139.30	0.99	0.65	1.00	0.01	38.18	139.16	0.99	0.65	1.00	0.00
38.28	138.51	0.98	0.65	1.00	0.01	38.37	137.08	0.95	0.66	1.00	0.01
38.47	135.63	0.93	1.00	1.00	0.01	38.57	134.14	0.91	1.02	1.00	0.01
38.62	132.48	0.88	1.03	1.00	0.01	38.72	127.27	0.81	1.43	1.00	0.02
38.78	123.72	0.76	1.49	1.00	0.01	38.81	121.63	0.74	1.86	1.00	0.01
38.86	121.68	0.74	1.86	1.00	0.01	38.91	120.51	0.72	1.89	1.00	0.01
38.95	118.55	0.70	1.93	1.00	0.01	39.05	116.91	0.68	1.97	1.00	0.02
39.09	115.64	0.67	2.00	1.00	0.01	39.14	114.83	0.66	2.02	1.00	0.01
39.24	114.32	0.65	2.03	1.00	0.02	39.29	114.03	0.65	2.10	1.00	0.01
39.39	114.16	0.65	2.10	1.00	0.02	39.43	114.28	0.65	2.03	1.00	0.01
39.53	113.89	0.65	2.10	1.00	0.03	39.57	113.55	0.64	2.11	1.00	0.01
39.68	113.69	0.64	2.10	1.00	0.03	39.73	113.53	0.64	2.11	1.00	0.01
39.81	112.48	0.63	2.12	1.00	0.02	39.89	109.51	0.60	2.17	1.00	0.02
39.96	105.89	0.56	2.23	1.00	0.02	40.06	103.14	0.54	2.28	1.00	0.03
40.15	102.38	0.53	2.29	1.00	0.02	40.20	102.07	0.53	2.30	1.00	0.02
40.24	102.62	0.53	2.29	1.00	0.01	40.26	103.22	0.54	2.28	1.00	0.00
40.27	103.36	0.54	2.27	1.00	0.00	40.37	103.81	0.55	2.27	1.00	0.03
40.42	104.71	0.55	2.25	1.00	0.01	40.52	105.44	0.56	2.24	1.00	0.03
40.56	106.63	0.57	2.22	1.00	0.01	40.66	108.06	0.58	2.19	1.00	0.03
40.70	110.67	0.61	2.15	1.00	0.01	40.75	114.79	0.65	2.02	1.00	0.01
40.85	119.75	0.71	1.90	1.00	0.02	40.91	125.10	0.77	1.47	1.00	0.01
40.96	130.56	0.85	1.38	1.00	0.01	41.04	135.59	0.92	1.00	1.00	0.01
41.09	141.03	1.01	0.64	1.00	0.00	41.18	145.57	1.08	0.43	1.00	0.00
41.23	149.12	1.15	0.43	1.00	0.00	41.29	151.17	1.19	0.30	1.00	0.00
41.38	151.67	1.19	0.30	1.00	0.00	41.42	151.21	1.19	0.30	1.00	0.00
41.52	149.86	1.16	0.31	1.00	0.00	41.57	148.26	1.13	0.43	1.00	0.00
41.62	146.93	1.11	0.43	1.00	0.00	41.71	145.89	1.09	0.43	1.00	0.00
41.76	145.43	1.08	0.43	1.00	0.00	41.84	145.17	1.08	0.43	1.00	0.00
41.91	145.22	1.08	0.43	1.00	0.00	41.95	145.53	1.08	0.43	1.00	0.00
42.01	146.36	1.10	0.43	1.00	0.00	42.10	147.40	1.11	0.43	1.00	0.00
42.15	148.90	1.14	0.43	1.00	0.00	42.24	149.94	1.16	0.31	1.00	0.00
42.28	150.31	1.17	0.31	1.00	0.00	42.39	149.81	1.16	0.31	1.00	0.00
42.43	149.14	1.14	0.43	1.00	0.00	42.50	148.36	1.13	0.43	1.00	0.00
42.58	147.54	1.12	0.43	1.00	0.00	42.65	142.73	1.03	0.63	1.00	0.01
42.70	140.58	1.00	0.64	1.00	0.00	42.73	139.14	0.97	0.65	1.00	0.00
42.77	142.31	1.02	0.64	1.00	0.00	42.82	144.06	1.05	0.43	1.00	0.00
42.87	146.92	1.10	0.43	1.00	0.00	42.91	150.57	1.17	0.30	1.00	0.00
42.97	154.27	1.24	0.30	1.00	0.00	43.02	157.35	1.30	0.21	1.00	0.00
43.06	159.72	1.35	0.00	1.00	0.00	43.11	162.21	1.40	0.00	1.00	0.00
43.17	164.40	1.45	0.00	1.00	0.00	43.21	166.83	1.51	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
43.29	168.85	1.55	0.00	1.00	0.00	43.34	171.05	1.61	0.00	1.00	0.00
43.39	172.71	1.65	0.00	1.00	0.00	43.45	173.74	1.67	0.00	1.00	0.00
43.51	173.50	1.66	0.00	1.00	0.00	43.59	172.47	1.64	0.00	1.00	0.00
43.64	170.73	1.60	0.00	1.00	0.00	43.70	168.10	1.54	0.00	1.00	0.00
43.78	165.08	1.47	0.00	1.00	0.00	43.88	163.55	1.43	0.00	1.00	0.00
43.94	161.52	1.39	0.00	1.00	0.00	44.04	157.74	1.31	0.21	1.00	0.00
44.07	153.31	1.22	0.30	1.00	0.00	44.12	152.08	1.20	0.30	1.00	0.00
44.16	150.70	1.17	0.30	1.00	0.00	44.21	148.86	1.14	0.43	1.00	0.00
44.26	146.86	1.10	0.43	1.00	0.00	44.31	144.63	1.06	0.43	1.00	0.00
44.35	142.44	1.03	0.64	1.00	0.00	44.40	140.32	0.99	0.64	1.00	0.00
44.45	138.56	0.96	0.65	1.00	0.00	44.50	137.24	0.94	0.98	1.00	0.01
44.54	136.15	0.93	0.99	1.00	0.00	44.60	134.97	0.91	1.01	1.00	0.01
44.64	133.85	0.89	1.02	1.00	0.01	44.69	132.85	0.88	1.03	1.00	0.01
44.74	132.59	0.87	1.03	1.00	0.01	44.79	132.34	0.87	1.04	1.00	0.01
44.83	132.53	0.87	1.03	1.00	0.01	44.88	132.96	0.88	1.03	1.00	0.01
44.93	134.02	0.89	1.02	1.00	0.01	44.98	135.20	0.91	1.00	1.00	0.01
45.03	135.95	0.92	1.00	1.00	0.01	45.08	136.45	0.93	0.99	1.00	0.01
45.16	136.81	0.94	0.99	1.00	0.01	45.19	136.91	0.94	0.98	1.00	0.00
45.27	136.53	0.93	0.99	1.00	0.01	45.32	135.53	0.92	1.00	1.00	0.01
45.37	133.73	0.89	1.02	1.00	0.01	45.45	131.17	0.85	1.05	1.00	0.01
45.51	127.52	0.80	1.42	1.00	0.01	45.56	123.37	2.00	0.00	1.00	0.00
45.61	117.60	2.00	0.00	1.00	0.00	45.69	111.79	2.00	0.00	1.00	0.00
45.75	108.19	2.00	0.00	1.00	0.00	45.81	105.04	2.00	0.00	1.00	0.00
45.89	105.10	2.00	0.00	1.00	0.00	45.94	103.73	2.00	0.00	1.00	0.00
46.04	108.05	2.00	0.00	1.00	0.00	46.08	112.07	2.00	0.00	1.00	0.00
46.15	109.85	2.00	0.00	1.00	0.00	46.17	110.89	2.00	0.00	1.00	0.00
46.18	110.17	2.00	0.00	1.00	0.00	46.23	109.18	2.00	0.00	1.00	0.00
46.27	107.58	2.00	0.00	1.00	0.00	46.32	105.33	2.00	0.00	1.00	0.00
46.41	107.19	2.00	0.00	1.00	0.00	46.47	106.19	2.00	0.00	1.00	0.00
46.52	106.89	2.00	0.00	1.00	0.00	46.56	109.81	2.00	0.00	1.00	0.00
46.65	113.60	2.00	0.00	1.00	0.00	46.71	117.68	2.00	0.00	1.00	0.00
46.76	120.04	2.00	0.00	1.00	0.00	46.85	120.43	2.00	0.00	1.00	0.00
46.90	118.71	2.00	0.00	1.00	0.00	46.99	116.19	2.00	0.00	1.00	0.00
47.04	114.63	2.00	0.00	1.00	0.00	47.10	114.71	2.00	0.00	1.00	0.00
47.16	116.10	2.00	0.00	1.00	0.00	47.23	117.23	2.00	0.00	1.00	0.00
47.30	117.96	2.00	0.00	1.00	0.00	47.38	113.48	2.00	0.00	1.00	0.00
47.43	111.84	2.00	0.00	1.00	0.00	47.52	105.92	2.00	0.00	1.00	0.00
47.59	93.23	2.00	0.00	1.00	0.00	47.66	81.89	2.00	0.00	1.00	0.00
47.77	74.67	2.00	0.00	1.00	0.00	47.82	75.76	2.00	0.00	1.00	0.00
47.91	76.63	2.00	0.00	1.00	0.00	47.93	77.65	2.00	0.00	1.00	0.00
47.97	78.37	2.00	0.00	1.00	0.00	48.02	79.56	2.00	0.00	1.00	0.00
48.07	81.21	2.00	0.00	1.00	0.00	48.12	84.04	2.00	0.00	1.00	0.00
48.19	86.54	2.00	0.00	1.00	0.00	48.23	88.74	2.00	0.00	1.00	0.00
48.31	89.88	2.00	0.00	1.00	0.00	48.35	90.92	2.00	0.00	1.00	0.00
48.40	91.72	2.00	0.00	1.00	0.00	48.45	92.39	2.00	0.00	1.00	0.00
48.50	92.93	2.00	0.00	1.00	0.00	48.55	93.37	2.00	0.00	1.00	0.00
48.59	94.24	2.00	0.00	1.00	0.00	48.67	94.62	2.00	0.00	1.00	0.00
48.73	94.36	2.00	0.00	1.00	0.00	48.78	92.80	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
48.83	90.68	2.00	0.00	1.00	0.00	48.91	88.35	2.00	0.00	1.00	0.00
48.98	86.35	2.00	0.00	1.00	0.00	49.03	85.19	2.00	0.00	1.00	0.00
49.12	82.90	2.00	0.00	1.00	0.00	49.17	79.48	2.00	0.00	1.00	0.00
49.27	76.51	2.00	0.00	1.00	0.00	49.31	76.55	2.00	0.00	1.00	0.00
49.38	78.88	2.00	0.00	1.00	0.00	49.45	81.15	2.00	0.00	1.00	0.00
49.51	83.00	2.00	0.00	1.00	0.00	49.54	84.13	2.00	0.00	1.00	0.00
49.59	84.45	2.00	0.00	1.00	0.00	49.64	83.63	2.00	0.00	1.00	0.00
49.73	83.01	2.00	0.00	1.00	0.00	49.83	82.47	2.00	0.00	1.00	0.00
49.92	82.19	2.00	0.00	1.00	0.00	49.98	81.62	2.00	0.00	1.00	0.00
50.07	81.01	2.00	0.00	1.00	0.00	50.16	80.51	2.00	0.00	1.00	0.00
50.24	80.06	2.00	0.00	1.00	0.00	50.32	79.87	2.00	0.00	1.00	0.00
50.41	80.02	2.00	0.00	1.00	0.00	50.50	80.09	2.00	0.00	1.00	0.00
50.56	79.36	2.00	0.00	1.00	0.00	50.66	78.27	2.00	0.00	1.00	0.00
50.74	77.53	2.00	0.00	1.00	0.00	50.84	79.62	2.00	0.00	1.00	0.00
50.93	83.88	2.00	0.00	1.00	0.00	50.98	92.08	2.00	0.00	1.00	0.00
51.08	102.75	2.00	0.00	1.00	0.00	51.17	113.31	2.00	0.00	1.00	0.00
51.24	122.80	2.00	0.00	1.00	0.00	51.34	129.12	2.00	0.00	1.00	0.00
51.41	122.59	2.00	0.00	1.00	0.00	51.51	115.66	2.00	0.00	1.00	0.00
51.58	106.93	2.00	0.00	1.00	0.00	51.68	109.98	2.00	0.00	1.00	0.00
51.79	110.16	2.00	0.00	1.00	0.00	51.82	110.15	2.00	0.00	1.00	0.00
51.85	111.07	2.00	0.00	1.00	0.00	51.91	113.23	2.00	0.00	1.00	0.00
52.00	116.25	2.00	0.00	1.00	0.00	52.05	118.92	2.00	0.00	1.00	0.00
52.10	118.95	2.00	0.00	1.00	0.00	52.19	115.81	2.00	0.00	1.00	0.00
52.28	111.69	2.00	0.00	1.00	0.00	52.34	109.32	2.00	0.00	1.00	0.00
52.42	109.66	2.00	0.00	1.00	0.00	52.48	111.03	2.00	0.00	1.00	0.00
52.57	111.27	2.00	0.00	1.00	0.00	52.62	109.88	2.00	0.00	1.00	0.00
52.69	106.89	2.00	0.00	1.00	0.00	52.77	104.50	2.00	0.00	1.00	0.00
52.87	103.83	2.00	0.00	1.00	0.00	52.91	102.56	2.00	0.00	1.00	0.00
53.01	102.13	2.00	0.00	1.00	0.00	53.10	103.11	2.00	0.00	1.00	0.00
53.16	113.26	2.00	0.00	1.00	0.00	53.25	123.32	2.00	0.00	1.00	0.00
53.29	136.25	2.00	0.00	1.00	0.00	53.38	144.18	2.00	0.00	1.00	0.00
53.42	149.47	2.00	0.00	1.00	0.00	53.47	150.02	2.00	0.00	1.00	0.00
53.52	148.22	2.00	0.00	1.00	0.00	53.58	152.55	2.00	0.00	1.00	0.00
53.66	160.18	2.00	0.00	1.00	0.00	53.75	169.41	2.00	0.00	1.00	0.00
53.81	175.67	2.00	0.00	1.00	0.00	53.87	177.89	2.00	0.00	1.00	0.00
53.95	178.71	2.00	0.00	1.00	0.00	54.01	177.57	2.00	0.00	1.00	0.00
54.06	172.90	2.00	0.00	1.00	0.00	54.15	167.57	2.00	0.00	1.00	0.00
54.20	165.24	2.00	0.00	1.00	0.00	54.29	164.23	2.00	0.00	1.00	0.00
54.34	141.87	2.00	0.00	1.00	0.00	54.43	108.63	2.00	0.00	1.00	0.00
54.45	82.07	2.00	0.00	1.00	0.00	54.48	80.59	2.00	0.00	1.00	0.00
54.52	82.69	2.00	0.00	1.00	0.00	54.53	86.57	2.00	0.00	1.00	0.00
54.58	89.91	0.45	2.55	1.00	0.01	54.62	93.59	0.47	2.47	1.00	0.01
54.65	96.81	0.50	2.40	1.00	0.01	54.70	99.98	0.52	2.34	1.00	0.01
54.76	102.23	0.54	2.29	1.00	0.02	54.77	102.77	0.55	2.28	1.00	0.00
54.82	103.16	0.55	2.28	1.00	0.01	54.87	103.55	0.56	2.27	1.00	0.01
54.88	104.08	0.56	2.26	1.00	0.00	54.91	104.56	0.56	2.25	1.00	0.01
54.96	106.09	0.58	2.23	1.00	0.01	54.97	109.90	0.62	2.16	1.00	0.00
55.03	115.47	0.68	2.00	1.00	0.02	55.09	120.89	0.74	1.88	1.00	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
55.15	121.55	0.75	1.86	1.00	0.01	55.20	122.41	0.76	1.51	1.00	0.01
55.25	121.49	0.75	1.86	1.00	0.01	55.30	129.28	0.85	1.07	1.00	0.01
55.34	134.62	0.93	1.01	1.00	0.01	55.39	146.03	1.12	0.43	1.00	0.00
55.40	153.71	1.27	0.21	1.00	0.00	55.44	157.35	1.34	0.21	1.00	0.00
55.44	157.04	1.34	0.21	1.00	0.00	55.49	160.78	1.42	0.00	1.00	0.00
55.54	167.71	1.58	0.00	1.00	0.00	55.59	176.17	1.79	0.00	1.00	0.00
55.63	180.34	1.90	0.00	1.00	0.00	55.64	180.79	1.91	0.00	1.00	0.00
55.68	179.92	1.89	0.00	1.00	0.00	55.69	178.50	1.85	0.00	1.00	0.00
55.69	179.38	1.88	0.00	1.00	0.00	55.71	183.08	1.98	0.00	1.00	0.00
55.76	186.45	2.00	0.00	1.00	0.00	55.78	187.85	2.00	0.00	1.00	0.00
55.81	180.96	1.92	0.00	1.00	0.00	55.85	175.16	1.77	0.00	1.00	0.00
55.86	176.41	1.80	0.00	1.00	0.00	55.91	179.42	1.88	0.00	1.00	0.00
55.92	180.48	1.91	0.00	1.00	0.00	55.96	185.46	2.00	0.00	1.00	0.00
55.97	189.98	2.00	0.00	1.00	0.00	56.00	196.01	2.00	0.00	1.00	0.00
56.01	197.72	2.00	0.00	1.00	0.00	56.03	198.18	2.00	0.00	1.00	0.00
56.05	198.14	2.00	0.00	1.00	0.00	56.10	198.99	2.00	0.00	1.00	0.00
56.12	199.86	2.00	0.00	1.00	0.00	56.16	199.67	2.00	0.00	1.00	0.00
56.17	195.76	2.00	0.00	1.00	0.00	56.20	189.78	2.00	0.00	1.00	0.00
56.22	184.46	2.00	0.00	1.00	0.00	56.24	181.69	1.95	0.00	1.00	0.00
56.30	179.84	1.89	0.00	1.00	0.00	56.31	177.72	1.84	0.00	1.00	0.00
56.34	174.82	1.76	0.00	1.00	0.00	56.39	172.57	1.70	0.00	1.00	0.00
56.45	170.44	1.65	0.00	1.00	0.00	56.48	168.31	1.60	0.00	1.00	0.00
56.49	165.32	1.53	0.00	1.00	0.00	56.53	168.57	1.60	0.00	1.00	0.00
56.58	169.38	1.62	0.00	1.00	0.00	56.63	155.86	1.32	0.21	1.00	0.00
56.68	156.17	1.33	0.21	1.00	0.00	56.73	157.68	1.36	0.00	1.00	0.00
56.78	156.09	1.33	0.21	1.00	0.00	56.83	153.53	1.27	0.21	1.00	0.00
56.89	157.35	1.35	0.00	1.00	0.00	56.95	160.76	1.43	0.00	1.00	0.00
56.99	161.37	1.44	0.00	1.00	0.00	57.01	160.98	1.43	0.00	1.00	0.00
57.04	160.65	1.43	0.00	1.00	0.00	57.09	161.13	1.44	0.00	1.00	0.00
57.11	163.57	1.49	0.00	1.00	0.00	57.13	167.47	1.58	0.00	1.00	0.00
57.18	169.44	1.63	0.00	1.00	0.00	57.19	168.95	1.62	0.00	1.00	0.00
57.21	166.30	1.56	0.00	1.00	0.00	57.24	164.00	1.50	0.00	1.00	0.00
57.28	163.35	1.49	0.00	1.00	0.00	57.32	161.45	1.44	0.00	1.00	0.00
57.35	160.03	1.41	0.00	1.00	0.00	57.38	157.50	1.36	0.00	1.00	0.00
57.43	155.53	1.32	0.21	1.00	0.00	57.48	150.26	1.21	0.31	1.00	0.00
57.52	143.92	1.10	0.44	1.00	0.00	57.57	142.28	1.07	0.44	1.00	0.00
57.62	146.53	1.14	0.43	1.00	0.00	57.68	157.03	1.35	0.00	1.00	0.00
57.76	166.00	1.55	0.00	1.00	0.00	57.81	161.17	1.44	0.00	1.00	0.00
57.86	159.31	1.40	0.00	1.00	0.00	57.89	167.80	1.60	0.00	1.00	0.00
57.91	171.02	1.68	0.00	1.00	0.00	57.92	169.11	1.63	0.00	1.00	0.00
57.95	166.67	1.57	0.00	1.00	0.00	57.99	167.08	1.58	0.00	1.00	0.00
58.01	169.42	1.64	0.00	1.00	0.00	58.05	173.02	1.73	0.00	1.00	0.00
58.05	175.27	1.79	0.00	1.00	0.00	58.10	176.91	1.83	0.00	1.00	0.00
58.13	178.73	1.88	0.00	1.00	0.00	58.15	180.87	1.94	0.00	1.00	0.00
58.17	182.75	1.99	0.00	1.00	0.00	58.20	182.21	1.98	0.00	1.00	0.00
58.21	181.00	1.94	0.00	1.00	0.00	58.21	179.50	1.90	0.00	1.00	0.00
58.23	179.34	1.90	0.00	1.00	0.00	58.24	177.62	1.85	0.00	1.00	0.00
58.25	177.92	1.86	0.00	1.00	0.00	58.29	179.26	1.90	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
58.31	183.11	2.00	0.00	1.00	0.00	58.33	186.52	2.00	0.00	1.00	0.00
58.38	190.06	2.00	0.00	1.00	0.00	58.39	193.13	2.00	0.00	1.00	0.00
58.43	195.59	2.00	0.00	1.00	0.00	58.43	199.15	2.00	0.00	1.00	0.00
58.48	200.60	2.00	0.00	1.00	0.00	58.53	202.36	2.00	0.00	1.00	0.00
58.56	202.90	2.00	0.00	1.00	0.00	58.58	205.20	2.00	0.00	1.00	0.00
58.59	207.06	2.00	0.00	1.00	0.00	58.63	205.90	2.00	0.00	1.00	0.00
58.63	206.49	2.00	0.00	1.00	0.00	58.63	202.42	2.00	0.00	1.00	0.00
58.68	203.74	2.00	0.00	1.00	0.00	58.69	204.22	2.00	0.00	1.00	0.00
58.72	208.81	2.00	0.00	1.00	0.00	58.73	210.28	2.00	0.00	1.00	0.00
58.74	211.92	2.00	0.00	1.00	0.00	58.77	211.36	2.00	0.00	1.00	0.00
58.81	210.02	2.00	0.00	1.00	0.00	58.82	207.44	2.00	0.00	1.00	0.00
58.83	207.97	2.00	0.00	1.00	0.00	58.87	209.78	2.00	0.00	1.00	0.00
58.91	212.41	2.00	0.00	1.00	0.00	58.92	214.21	2.00	0.00	1.00	0.00
58.93	214.95	2.00	0.00	1.00	0.00	58.96	214.44	2.00	0.00	1.00	0.00
59.01	207.70	2.00	0.00	1.00	0.00	59.06	199.13	2.00	0.00	1.00	0.00
59.08	189.77	2.00	0.00	1.00	0.00	59.11	184.95	2.00	0.00	1.00	0.00
59.15	181.46	1.96	0.00	1.00	0.00	59.21	178.75	1.89	0.00	1.00	0.00
59.26	178.89	1.89	0.00	1.00	0.00	59.30	173.20	1.74	0.00	1.00	0.00
59.35	169.07	1.64	0.00	1.00	0.00	59.40	168.73	1.63	0.00	1.00	0.00
59.42	168.34	1.62	0.00	1.00	0.00	59.47	167.78	1.61	0.00	1.00	0.00
59.51	168.63	1.63	0.00	1.00	0.00	59.56	168.59	1.63	0.00	1.00	0.00
59.61	164.50	1.53	0.00	1.00	0.00	59.67	155.77	1.34	0.21	1.00	0.00
59.71	159.11	1.41	0.00	1.00	0.00	59.80	159.56	1.42	0.00	1.00	0.00
59.85	158.50	1.40	0.00	1.00	0.00	59.90	155.47	1.33	0.21	1.00	0.00
60.00	155.53	1.33	0.21	1.00	0.00	60.04	155.09	1.33	0.21	1.00	0.00
60.10	150.62	1.23	0.30	1.00	0.00	60.15	145.30	1.13	0.43	1.00	0.00
60.19	139.22	1.03	0.65	1.00	0.00	60.23	138.03	1.01	0.65	1.00	0.00
60.28	137.71	1.00	0.66	1.00	0.00	60.33	139.47	1.03	0.65	1.00	0.00
60.38	140.26	1.05	0.64	1.00	0.00	60.42	140.74	1.05	0.44	1.00	0.00
60.44	140.24	1.05	0.65	1.00	0.00	60.47	145.72	1.14	0.43	1.00	0.00
60.52	148.94	1.20	0.31	1.00	0.00	60.56	150.90	1.24	0.30	1.00	0.00
60.57	151.48	1.25	0.22	1.00	0.00	60.61	151.48	1.25	0.22	1.00	0.00
60.66	151.98	1.27	0.21	1.00	0.00	60.71	153.21	1.29	0.21	1.00	0.00
60.76	156.59	1.36	0.00	1.00	0.00	60.81	159.58	1.43	0.00	1.00	0.00
60.86	161.02	1.46	0.00	1.00	0.00	60.91	158.84	1.41	0.00	1.00	0.00
60.95	170.69	1.69	0.00	1.00	0.00	61.00	180.91	1.97	0.00	1.00	0.00
61.02	186.60	2.00	0.00	1.00	0.00	61.05	194.34	2.00	0.00	1.00	0.00
61.08	201.44	2.00	0.00	1.00	0.00	61.09	207.57	2.00	0.00	1.00	0.00
61.13	209.24	2.00	0.00	1.00	0.00	61.14	209.63	2.00	0.00	1.00	0.00
61.16	210.15	2.00	0.00	1.00	0.00	61.20	212.77	2.00	0.00	1.00	0.00
61.23	215.88	2.00	0.00	1.00	0.00	61.24	217.23	2.00	0.00	1.00	0.00
61.29	214.83	2.00	0.00	1.00	0.00	61.30	210.65	2.00	0.00	1.00	0.00
61.33	207.82	2.00	0.00	1.00	0.00	61.38	206.66	2.00	0.00	1.00	0.00
61.43	206.60	2.00	0.00	1.00	0.00	61.48	208.54	2.00	0.00	1.00	0.00
61.53	212.02	2.00	0.00	1.00	0.00	61.56	213.05	2.00	0.00	1.00	0.00
61.58	205.10	2.00	0.00	1.00	0.00	61.59	198.13	2.00	0.00	1.00	0.00
61.62	169.24	1.66	0.00	1.00	0.00	61.63	167.67	1.62	0.00	1.00	0.00
61.67	165.65	1.57	0.00	1.00	0.00	61.71	186.61	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
61.76	184.50	2.00	0.00	1.00	0.00	61.81	178.32	1.90	0.00	1.00	0.00
61.86	172.85	1.75	0.00	1.00	0.00	61.87	168.83	1.65	0.00	1.00	0.00
61.91	165.39	1.57	0.00	1.00	0.00	61.95	162.25	1.49	0.00	1.00	0.00
61.96	159.04	1.42	0.00	1.00	0.00	62.00	155.30	1.34	0.21	1.00	0.00
62.04	150.01	1.23	0.31	1.00	0.00	62.06	143.15	1.11	0.44	1.00	0.00
62.10	137.65	1.01	0.66	1.00	0.00	62.14	133.04	0.94	1.03	1.00	0.01
62.20	129.46	0.88	1.07	1.00	0.01	62.22	122.70	0.79	1.51	1.00	0.00
62.27	125.13	0.82	1.46	1.00	0.01	62.29	125.44	0.83	1.46	1.00	0.00
62.34	124.22	0.81	1.48	1.00	0.01	62.39	123.46	0.80	1.49	1.00	0.01
62.43	121.51	0.77	1.53	1.00	0.01	62.49	121.38	0.77	1.53	1.00	0.01
62.57	121.70	0.78	1.53	1.00	0.02	62.68	127.79	0.86	1.09	1.00	0.01
62.75	139.12	1.04	0.65	1.00	0.01	62.87	146.86	1.18	0.31	1.00	0.00
62.88	142.25	1.09	0.44	1.00	0.00	62.89	142.29	1.09	0.44	1.00	0.00
62.93	142.80	1.10	0.44	1.00	0.00	62.98	158.87	1.42	0.00	1.00	0.00
63.02	172.30	1.75	0.00	1.00	0.00	63.07	182.93	2.00	0.00	1.00	0.00
63.12	-1.00	2.00	0.00	1.00	0.00	63.14	-1.00	2.00	0.00	1.00	0.00
63.17	-1.00	2.00	0.00	1.00	0.00	63.17	-1.00	2.00	0.00	1.00	0.00
63.20	-1.00	2.00	0.00	1.00	0.00	63.21	-1.00	2.00	0.00	1.00	0.00
63.23	-1.00	2.00	0.00	1.00	0.00	63.26	-1.00	2.00	0.00	1.00	0.00
63.28	-1.00	2.00	0.00	1.00	0.00	63.31	-1.00	2.00	0.00	1.00	0.00
63.32	-1.00	2.00	0.00	1.00	0.00	63.36	-1.00	2.00	0.00	1.00	0.00
63.40	-1.00	2.00	0.00	1.00	0.00						

Total estimated settlement: 2.49

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation (Robertson (2009) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.01	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.04	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.09	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.11	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.14	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.14	1.35	2.15	27.82	59.81	3.66	7.03	11.25
0.18	6.97	11.19	4.58	51.24	2.69	0.06	0.63
0.23	18.19	29.21	1.00	29.21	2.14	0.02	0.62
0.24	36.79	59.09	1.00	59.09	1.76	0.11	0.65
0.28	53.07	85.23	1.00	85.23	1.58	0.72	0.72
0.33	59.27	95.19	1.00	95.19	1.53	0.74	0.74
0.38	56.61	90.91	1.00	90.91	1.60	0.73	0.73
0.42	52.11	83.69	1.00	83.69	1.72	0.72	0.72
0.47	51.84	83.25	1.19	98.77	1.83	0.75	0.75
0.51	51.94	83.40	1.24	103.16	1.90	0.75	0.75
0.52	52.09	83.64	1.26	104.99	1.93	0.76	0.76
0.57	52.66	84.56	1.24	105.20	1.91	0.76	0.76
0.61	53.24	85.48	1.23	105.23	1.89	0.76	0.76
0.67	53.47	85.85	1.22	105.00	1.88	0.76	0.76
0.73	53.84	86.44	1.22	105.23	1.87	0.76	0.76
0.81	53.62	86.08	1.22	104.72	1.87	0.76	0.76
0.86	53.52	85.91	1.25	107.16	1.92	0.76	0.76
0.98	52.14	83.69	1.28	106.78	1.96	0.76	0.76
1.05	48.22	77.37	1.32	102.42	2.02	0.75	0.75
1.15	43.67	70.05	1.34	94.07	2.04	0.74	0.74
1.24	37.87	60.73	1.38	83.84	2.07	0.72	0.72
1.34	34.47	55.26	1.40	77.37	2.09	0.47	0.70
1.43	30.63	49.08	1.51	74.33	2.16	0.36	0.69
1.53	26.86	43.01	1.75	75.37	2.25	0.40	0.70
1.58	24.56	39.32	1.98	77.68	2.31	0.48	0.70
1.62	23.48	37.59	2.00	75.15	2.32	0.39	0.70
1.67	24.36	38.99	1.85	72.19	2.28	0.31	0.69
1.75	23.89	38.23	1.86	70.99	2.28	0.28	0.69
1.77	23.08	36.93	1.92	70.79	2.30	0.27	0.69
1.81	21.50	34.38	2.08	71.55	2.34	0.29	0.69
1.86	19.71	31.51	2.30	72.37	2.39	0.31	0.69
1.91	17.96	28.69	2.52	72.24	2.43	0.31	0.69
1.95	16.98	27.11	2.53	68.54	2.43	0.23	0.68
2.00	16.21	25.86	2.43	62.85	2.41	0.14	0.66
2.05	14.89	23.75	2.42	57.52	2.41	0.09	0.65
2.11	13.51	21.52	2.55	54.95	2.43	0.08	0.64
2.20	12.33	19.62	2.79	54.76	2.47	0.08	0.64
2.24	11.73	18.64	3.01	56.15	2.50	0.08	0.65
2.29	11.26	17.88	3.29	58.85	2.54	0.10	0.65
2.34	11.32	17.99	3.76	67.59	2.60	0.21	0.68
2.44	12.17	19.33	3.86	74.63	2.61	0.37	0.69
2.48	14.56	23.17	3.43	79.44	2.56	0.56	0.71
2.58	18.03	28.74	2.75	79.05	2.47	0.54	0.70

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.63	22.41	35.77	2.21	79.01	2.37	0.54	0.70
2.71	26.08	41.66	1.92	80.03	2.30	0.59	0.71
2.78	30.33	48.48	1.67	80.89	2.22	0.63	0.71
2.82	33.73	53.95	1.52	82.21	2.16	0.70	0.71
2.89	34.94	55.89	1.47	82.24	2.13	0.70	0.71
2.96	33.63	53.77	1.51	81.39	2.16	0.66	0.71
3.03	30.90	49.37	1.62	80.00	2.20	0.58	0.71
3.11	28.98	46.28	1.70	78.46	2.23	0.51	0.70
3.19	26.45	42.22	1.79	75.65	2.26	0.41	0.70
3.25	23.52	37.50	1.97	73.87	2.31	0.35	0.69
3.35	20.49	32.62	2.28	74.42	2.38	0.37	0.69
3.41	17.79	28.29	2.60	73.49	2.44	0.34	0.69
3.50	15.91	25.25	2.74	69.10	2.46	0.24	0.68
3.59	14.83	23.51	2.66	62.63	2.45	0.14	0.66
3.69	14.59	23.12	2.55	58.90	2.43	0.10	0.65
3.79	15.20	24.09	2.35	56.48	2.39	0.09	0.65
3.88	16.54	26.24	2.09	54.78	2.34	0.08	0.64
3.97	19.14	30.40	1.82	55.25	2.27	0.08	0.64
4.07	20.82	33.10	1.77	58.69	2.26	0.10	0.65
4.14	23.49	37.37	1.67	62.38	2.22	0.14	0.66
4.17	25.51	40.62	1.61	65.25	2.20	0.17	0.67
4.26	28.14	44.83	1.51	67.83	2.15	0.21	0.68
4.32	28.71	45.74	1.52	69.43	2.16	0.24	0.68
4.37	28.10	44.77	1.56	69.94	2.18	0.25	0.68
4.42	26.62	42.38	1.65	69.93	2.21	0.25	0.68
4.51	25.07	39.88	1.74	69.30	2.24	0.24	0.68
4.61	23.68	37.65	1.82	68.42	2.27	0.22	0.68
4.65	22.37	35.53	1.90	67.38	2.29	0.21	0.68
4.74	21.09	33.47	2.00	67.06	2.32	0.20	0.68
4.80	20.48	32.49	2.05	66.55	2.33	0.19	0.67
4.89	20.04	31.78	2.09	66.46	2.34	0.19	0.67
4.95	20.38	32.32	2.05	66.20	2.33	0.19	0.67
5.04	21.05	33.39	1.97	65.92	2.31	0.18	0.67
5.13	22.81	36.20	1.80	65.26	2.27	0.17	0.67
5.18	25.27	40.14	1.63	65.28	2.20	0.17	0.67
5.28	28.07	44.63	1.49	66.64	2.14	0.19	0.67
5.32	31.47	50.09	1.40	70.04	2.09	0.26	0.68
5.42	34.67	55.23	1.35	74.62	2.05	0.37	0.69
5.51	38.14	60.80	1.31	79.86	2.01	0.58	0.71
5.60	41.28	65.83	1.26	83.18	1.94	0.71	0.71
5.66	44.24	70.58	1.22	86.14	1.88	0.72	0.72
5.76	45.86	73.17	1.00	73.17	1.83	0.33	0.69
5.85	44.91	71.65	1.21	86.53	1.86	0.72	0.72
5.92	41.11	65.53	1.25	81.79	1.92	0.68	0.71
5.95	38.21	60.87	1.28	77.76	1.96	0.48	0.70
5.97	36.15	57.56	1.30	74.97	1.99	0.38	0.70
6.02	35.37	56.31	1.31	73.90	2.01	0.35	0.69
6.06	32.74	52.08	1.36	70.59	2.05	0.27	0.68

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.16	29.98	47.63	1.42	67.87	2.10	0.21	0.68
6.21	26.98	42.82	1.56	66.83	2.18	0.20	0.68
6.26	24.29	38.48	1.79	68.74	2.26	0.23	0.68
6.31	21.62	34.19	2.18	74.63	2.36	0.37	0.69
6.40	19.23	30.34	2.70	82.06	2.46	0.69	0.71
6.44	16.91	26.60	3.43	91.18	2.56	0.73	0.73
6.52	15.12	23.73	4.16	98.65	2.64	0.75	0.75
6.57	13.47	21.08	5.01	105.63	2.73	0.76	0.76
6.64	12.16	18.96	5.81	110.19	2.80	0.77	0.77
6.69	10.98	17.06	6.65	113.46	2.86	0.77	0.77
6.78	10.34	16.02	7.15	114.49	2.90	0.77	0.77
6.83	9.90	15.31	7.38	112.96	2.91	0.77	0.77
6.92	9.60	14.82	7.45	110.37	2.92	0.77	0.77
6.97	9.39	14.48	7.39	107.07	2.91	0.76	0.76
7.03	9.29	14.32	7.35	105.27	2.91	0.76	0.76
7.12	9.32	14.36	7.25	104.07	2.90	0.76	0.76
7.22	9.39	14.46	7.17	103.64	2.90	0.75	0.75
7.27	9.52	14.66	7.09	103.89	2.89	0.76	0.76
7.36	9.65	14.86	7.06	104.93	2.89	0.76	0.76
7.43	9.75	15.01	7.08	106.34	2.89	0.76	0.76
7.50	9.78	15.06	7.16	107.82	2.90	0.76	0.76
7.59	9.77	15.04	7.22	108.69	2.90	0.76	0.76
7.64	9.70	14.93	7.34	109.64	2.91	0.77	0.77
7.75	9.63	14.81	7.46	110.40	2.92	0.77	0.77
7.79	9.70	14.91	7.43	110.74	2.92	0.77	0.77
7.89	9.97	15.33	7.19	110.22	2.90	0.77	0.77
7.99	10.24	15.76	6.97	109.89	2.88	0.77	0.77
8.04	10.34	15.91	6.96	110.71	2.88	0.77	0.77
8.13	10.31	15.85	7.03	111.39	2.89	0.77	0.77
8.23	10.27	15.79	6.35	100.23	2.84	0.75	0.75
8.32	10.27	15.77	5.78	91.18	2.79	0.73	0.73
8.37	10.53	16.20	5.34	86.47	2.76	0.72	0.72
8.46	11.04	17.00	5.74	97.61	2.79	0.74	0.74
8.56	11.30	17.42	6.05	105.35	2.82	0.76	0.76
8.59	11.30	17.41	6.35	110.51	2.84	0.77	0.77
8.61	11.03	16.97	6.71	113.97	2.87	0.77	0.77
8.67	10.89	16.75	6.98	116.82	2.88	0.78	0.78
8.71	10.69	16.41	7.24	118.78	2.90	0.78	0.78
8.72	10.51	16.13	7.46	120.30	2.92	0.78	0.78
8.78	10.44	16.02	7.56	121.13	2.92	0.78	0.78
8.80	10.44	16.02	7.59	121.54	2.93	0.79	0.79
8.86	10.44	16.01	7.60	121.62	2.93	0.79	0.79
8.90	10.55	16.17	7.55	122.08	2.92	0.79	0.79
8.95	10.68	16.39	7.49	122.77	2.92	0.79	0.79
8.96	10.89	16.71	7.39	123.54	2.91	0.79	0.79
9.00	11.05	16.98	7.33	124.43	2.91	0.79	0.79
9.05	11.29	17.35	7.24	125.55	2.90	0.79	0.79
9.09	11.56	17.78	7.10	126.26	2.89	0.79	0.79

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.10	11.96	18.43	6.89	127.03	2.88	0.79	0.79
9.14	12.47	19.24	6.66	128.15	2.86	0.80	0.80
9.20	13.21	20.42	6.33	129.23	2.84	0.80	0.80
9.24	14.09	21.83	5.95	129.98	2.81	0.80	0.80
9.29	15.03	23.34	5.57	129.97	2.78	0.80	0.80
9.31	15.90	24.74	5.28	130.54	2.75	0.80	0.80
9.38	16.61	25.88	5.06	130.87	2.73	0.80	0.80
9.41	17.32	27.00	4.80	129.53	2.71	0.80	0.80
9.47	18.02	28.13	4.48	126.15	2.68	0.79	0.79
9.53	19.33	30.23	3.91	118.10	2.62	0.78	0.78
9.62	21.08	33.03	3.29	108.83	2.54	0.76	0.76
9.67	23.71	36.88	2.63	97.08	2.45	0.74	0.74
9.77	26.25	39.96	2.22	88.55	2.37	0.73	0.73
9.81	28.83	43.12	1.89	81.52	2.29	0.66	0.71
9.90	30.67	45.16	1.72	77.57	2.24	0.48	0.70
9.97	32.26	46.92	1.61	75.55	2.20	0.40	0.70
10.06	32.63	47.13	1.61	75.67	2.20	0.41	0.70
10.20	32.13	46.19	1.68	77.59	2.22	0.48	0.70
10.30	29.29	42.06	1.79	75.15	2.26	0.39	0.70
10.44	25.52	36.67	2.06	75.52	2.33	0.40	0.70
10.54	20.70	30.03	2.66	79.87	2.45	0.58	0.71
10.63	16.56	24.49	4.08	99.92	2.64	0.75	0.75
10.74	13.83	20.66	5.64	116.62	2.78	0.78	0.78
10.78	12.62	18.99	6.71	127.39	2.86	0.79	0.79
10.83	12.48	18.76	6.96	130.59	2.88	0.80	0.80
10.88	12.31	18.47	7.21	133.16	2.90	0.80	0.80
10.89	12.15	18.24	7.50	136.86	2.92	0.81	0.81
10.97	12.25	18.30	7.62	139.36	2.93	0.81	0.81
11.02	12.48	18.59	7.62	141.70	2.93	0.82	0.82
11.07	12.79	18.96	7.51	142.37	2.92	0.82	0.82
11.11	13.06	19.28	7.42	143.00	2.91	0.82	0.82
11.16	13.39	19.70	7.30	143.71	2.91	0.82	0.82
11.21	13.76	20.15	7.19	144.81	2.90	0.82	0.82
11.26	14.14	20.62	7.10	146.37	2.89	0.82	0.82
11.30	14.37	20.90	7.10	148.42	2.89	0.82	0.82
11.36	14.54	21.07	7.14	150.43	2.90	0.83	0.83
11.40	14.68	21.19	7.17	151.92	2.90	0.83	0.83
11.45	14.81	21.32	7.18	152.97	2.90	0.83	0.83
11.50	15.04	21.57	7.12	153.64	2.89	0.83	0.83
11.55	15.31	21.86	7.06	154.44	2.89	0.83	0.83
11.60	15.85	22.53	6.88	155.07	2.88	0.83	0.83
11.66	16.56	23.39	6.63	155.14	2.86	0.83	0.83
11.74	17.40	24.38	6.31	153.92	2.84	0.83	0.83
11.84	17.98	24.97	6.15	153.46	2.82	0.83	0.83
11.93	18.18	25.08	6.17	154.65	2.82	0.83	0.83
12.04	18.04	24.73	6.38	157.76	2.84	0.84	0.84
12.13	17.87	24.37	6.58	160.42	2.86	0.84	0.84
12.22	17.67	23.94	6.76	161.87	2.87	0.84	0.84

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.27	17.51	23.64	6.85	161.93	2.88	0.84	0.84
12.37	17.27	23.16	6.98	161.58	2.88	0.84	0.84
12.41	17.17	22.94	7.03	161.26	2.89	0.84	0.84
12.51	17.06	22.65	7.13	161.48	2.89	0.84	0.84
12.56	17.23	22.78	7.08	161.37	2.89	0.84	0.84
12.65	17.64	23.15	6.96	161.03	2.88	0.84	0.84
12.71	18.45	24.09	6.70	161.44	2.86	0.84	0.84
12.79	19.23	24.96	6.59	164.56	2.86	0.85	0.85
12.89	20.10	25.92	6.50	168.54	2.85	0.85	0.85
12.96	20.98	26.96	6.43	173.33	2.84	0.86	0.86
13.04	22.23	28.37	6.15	174.57	2.82	0.86	0.86
13.13	24.11	30.49	5.62	171.40	2.78	0.85	0.85
13.23	26.80	33.27	4.19	139.58	2.65	0.81	0.81
13.30	30.34	36.95	2.91	107.47	2.49	0.76	0.76
13.37	34.15	40.77	2.02	82.17	2.32	0.70	0.71
13.47	38.32	45.44	1.87	85.15	2.29	0.72	0.72
13.57	38.79	45.84	1.94	89.15	2.31	0.73	0.73
13.61	39.19	46.27	1.98	91.39	2.31	0.73	0.73
13.62	40.31	47.52	1.94	92.31	2.30	0.73	0.73
13.68	44.31	51.92	1.78	92.36	2.26	0.73	0.73
13.73	47.82	55.76	1.68	93.57	2.22	0.74	0.74
13.77	50.08	58.23	1.65	95.79	2.21	0.74	0.74
13.87	52.91	61.16	1.61	98.26	2.20	0.74	0.74
13.93	55.78	64.26	1.58	101.41	2.19	0.75	0.75
14.00	58.54	67.15	1.55	104.21	2.17	0.76	0.76
14.06	60.62	69.33	1.54	106.89	2.17	0.76	0.76
14.12	62.21	70.95	1.54	109.37	2.17	0.77	0.77
14.21	63.05	71.63	1.55	111.13	2.17	0.77	0.77
14.25	63.45	71.96	1.56	112.44	2.18	0.77	0.77
14.35	63.35	71.51	1.58	112.67	2.18	0.77	0.77
14.45	62.61	70.37	1.60	112.38	2.19	0.77	0.77
14.50	61.06	68.50	1.63	111.75	2.21	0.77	0.77
14.59	59.18	66.15	1.68	111.04	2.22	0.77	0.77
14.64	57.19	63.82	1.73	110.49	2.24	0.77	0.77
14.74	55.60	61.79	1.78	110.08	2.26	0.77	0.77
14.80	54.22	60.12	1.83	109.86	2.27	0.77	0.77
14.88	53.18	58.73	1.87	109.70	2.28	0.77	0.77
14.97	52.24	57.45	1.91	109.62	2.30	0.77	0.77
15.05	51.43	56.38	1.95	110.04	2.31	0.77	0.77
15.13	50.85	55.53	1.99	110.56	2.32	0.77	0.77
15.21	50.95	55.42	1.99	110.46	2.32	0.77	0.77
15.28	52.23	56.58	1.93	109.48	2.30	0.77	0.77
15.36	55.10	59.37	1.82	108.07	2.27	0.76	0.76
15.41	60.22	64.61	1.66	107.30	2.22	0.76	0.76
15.50	66.38	70.74	1.53	108.00	2.16	0.76	0.76
15.55	72.78	77.07	1.38	106.45	2.07	0.76	0.76
15.65	76.92	80.83	1.31	105.71	2.00	0.76	0.76
15.71	78.17	81.68	1.27	103.43	1.94	0.75	0.75

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.79	75.07	78.22	1.28	99.99	1.96	0.75	0.75
15.89	67.29	69.97	1.33	92.88	2.02	0.73	0.73
15.90	61.09	63.58	1.38	88.03	2.07	0.72	0.72
15.94	56.21	58.47	1.45	84.99	2.12	0.72	0.72
16.00	53.24	55.28	1.51	83.45	2.15	0.71	0.71
16.06	47.68	49.45	1.67	82.65	2.22	0.71	0.71
16.14	40.74	42.17	2.02	85.02	2.32	0.72	0.72
16.19	34.10	35.24	2.56	90.26	2.43	0.73	0.73
16.26	27.10	27.88	3.51	97.89	2.57	0.74	0.74
16.33	21.54	22.01	4.74	104.24	2.70	0.76	0.76
16.38	17.06	17.28	6.24	107.80	2.83	0.76	0.76
16.47	14.43	14.45	7.58	109.50	2.93	0.77	0.77
16.54	12.64	12.69	8.71	110.54	3.00	0.77	0.77
16.62	11.80	11.71	9.67	113.31	3.05	0.52	0.84
16.70	11.53	11.36	10.18	115.66	3.08	0.56	0.81
16.76	12.28	12.12	9.88	119.66	3.06	0.59	0.87
16.86	14.88	14.80	8.08	119.59	2.96	0.78	0.78
16.90	19.33	19.15	6.07	116.24	2.82	0.78	0.78
16.98	25.84	25.69	4.22	108.51	2.65	0.76	0.76
17.05	35.42	35.23	2.81	99.11	2.48	0.75	0.75
17.14	47.54	47.19	1.94	91.71	2.30	0.73	0.73
17.20	61.48	60.90	1.51	91.88	2.15	0.73	0.73
17.29	73.03	72.03	1.35	97.56	2.05	0.74	0.74
17.34	81.99	80.70	1.30	104.58	1.99	0.76	0.76
17.44	86.87	85.21	1.28	109.31	1.97	0.76	0.76
17.50	88.89	86.96	1.26	109.36	1.93	0.76	0.76
17.58	88.15	85.91	1.24	106.78	1.91	0.76	0.76
17.64	85.02	82.63	1.24	102.13	1.90	0.75	0.75
17.75	80.50	77.97	1.27	99.12	1.95	0.75	0.75
17.82	72.08	69.66	1.35	93.80	2.04	0.74	0.74
17.89	66.02	63.60	1.43	91.18	2.11	0.73	0.73
17.89	62.68	60.37	1.51	91.04	2.15	0.73	0.73
17.96	64.06	61.55	1.50	92.30	2.15	0.73	0.73
18.02	65.34	62.67	1.51	94.33	2.15	0.74	0.74
18.07	66.86	64.01	1.51	96.43	2.15	0.74	0.74
18.17	68.78	65.62	1.49	98.02	2.14	0.74	0.74
18.22	68.74	65.47	1.51	98.54	2.15	0.75	0.75
18.30	65.20	61.85	1.59	98.20	2.19	0.74	0.74
18.36	57.69	54.52	1.83	99.83	2.27	0.75	0.75
18.42	49.20	46.28	2.30	106.36	2.39	0.76	0.76
18.50	39.97	37.31	3.16	118.00	2.53	0.78	0.78
18.56	32.38	29.97	4.32	129.55	2.66	0.80	0.80
18.62	25.71	23.53	5.80	136.40	2.80	0.81	0.81
18.69	23.96	21.78	6.13	133.60	2.82	0.80	0.80
18.76	22.21	20.05	6.60	132.24	2.86	0.80	0.80
18.84	24.30	21.95	5.90	129.41	2.80	0.80	0.80
18.89	31.88	29.04	4.26	123.66	2.66	0.79	0.79
18.98	52.85	48.61	2.23	108.20	2.37	0.76	0.76

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
19.05	78.42	72.48	1.52	110.23	2.16	0.77	0.77
19.12	101.80	94.21	1.32	124.65	2.02	0.79	0.79
19.18	115.88	107.18	1.27	136.09	1.95	0.81	0.81
19.24	124.07	114.61	1.25	142.72	1.91	0.82	0.82
19.32	126.76	116.83	1.24	144.84	1.90	0.82	0.82
19.38	126.53	116.38	1.25	145.16	1.92	0.82	0.82
19.46	124.81	114.42	1.26	144.25	1.94	0.82	0.82
19.54	122.62	112.08	1.28	142.92	1.96	0.82	0.82
19.62	121.00	110.26	1.28	141.68	1.97	0.82	0.82
19.70	119.99	109.01	1.29	140.65	1.98	0.81	0.81
19.80	119.75	108.41	1.29	140.01	1.98	0.81	0.81
19.85	119.75	108.23	1.29	139.71	1.98	0.81	0.81
19.94	119.95	108.07	1.29	139.71	1.98	0.81	0.81
20.03	120.73	108.50	1.28	138.61	1.96	0.81	0.81
20.13	121.84	109.19	1.26	137.92	1.94	0.81	0.81
20.19	123.33	110.40	1.25	137.60	1.91	0.81	0.81
20.29	124.05	110.67	1.25	138.32	1.92	0.81	0.81
20.39	124.51	110.70	1.25	138.76	1.93	0.81	0.81
20.43	124.14	110.23	1.26	138.70	1.93	0.81	0.81
20.47	124.09	109.99	1.26	138.78	1.94	0.81	0.81
20.52	123.97	109.69	1.27	139.06	1.95	0.81	0.81
20.61	123.97	109.33	1.27	139.29	1.96	0.81	0.81
20.66	123.26	108.48	1.28	139.08	1.97	0.81	0.81
20.71	122.22	107.35	1.29	138.34	1.98	0.81	0.81
20.77	121.00	106.04	1.30	137.35	1.99	0.81	0.81
20.85	120.53	105.33	1.30	136.79	1.99	0.81	0.81
20.91	120.63	105.23	1.30	136.74	1.99	0.81	0.81
21.00	121.00	105.23	1.30	136.71	1.99	0.81	0.81
21.05	120.93	105.01	1.30	136.53	1.99	0.81	0.81
21.11	120.50	104.40	1.30	136.06	2.00	0.81	0.81
21.19	120.16	103.82	1.31	135.66	2.00	0.81	0.81
21.24	120.23	103.70	1.31	135.67	2.00	0.81	0.81
21.34	120.39	103.52	1.31	135.57	2.00	0.81	0.81
21.39	119.99	103.00	1.31	135.16	2.01	0.81	0.81
21.48	118.68	101.52	1.32	133.84	2.01	0.80	0.80
21.53	116.39	99.34	1.33	131.86	2.02	0.80	0.80
21.64	113.86	96.79	1.34	129.36	2.03	0.80	0.80
21.72	111.80	94.83	1.33	125.65	2.02	0.79	0.79
21.81	110.79	93.80	1.31	122.48	2.00	0.79	0.79
21.89	110.52	93.48	1.28	120.09	1.97	0.78	0.78
21.97	110.69	93.44	1.28	119.40	1.96	0.78	0.78
22.05	110.81	93.32	1.27	118.94	1.96	0.78	0.78
22.12	110.92	93.25	1.27	118.64	1.95	0.78	0.78
22.13	110.89	93.20	1.27	118.54	1.95	0.78	0.78
22.18	111.98	94.01	1.27	119.22	1.95	0.78	0.78
22.22	114.49	96.10	1.26	121.02	1.93	0.78	0.78
22.28	118.47	99.41	1.25	123.90	1.91	0.79	0.79
22.33	122.55	102.85	1.23	126.89	1.90	0.79	0.79

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.38	126.36	106.02	1.22	129.64	1.88	0.80	0.80
22.41	129.99	109.11	1.21	132.05	1.86	0.80	0.80
22.51	133.16	111.59	1.20	133.67	1.85	0.80	0.80
22.56	135.86	113.83	1.18	134.77	1.83	0.81	0.81
22.61	137.68	115.29	1.17	135.13	1.82	0.81	0.81
22.65	139.23	116.56	1.16	135.07	1.81	0.81	0.81
22.71	140.30	117.38	1.15	134.57	1.79	0.81	0.81
22.76	141.15	118.01	1.13	133.54	1.78	0.80	0.80
22.85	141.55	118.16	1.12	132.33	1.77	0.80	0.80
22.89	141.79	118.28	1.11	131.19	1.77	0.80	0.80
22.99	141.85	118.07	1.10	130.38	1.76	0.80	0.80
23.04	142.19	118.24	1.10	129.89	1.76	0.80	0.80
23.12	143.24	118.92	1.09	129.72	1.75	0.80	0.80
23.18	145.12	120.36	1.08	129.86	1.75	0.80	0.80
23.24	147.55	122.28	1.07	130.48	1.74	0.80	0.80
23.33	150.28	124.35	1.05	131.06	1.73	0.80	0.80
23.38	152.77	126.31	1.04	131.98	1.73	0.80	0.80
23.47	154.92	127.86	1.04	132.70	1.72	0.80	0.80
23.52	155.87	128.46	1.05	134.34	1.73	0.80	0.80
23.61	155.50	127.76	1.06	136.02	1.74	0.81	0.81
23.68	153.41	125.65	1.10	137.67	1.76	0.81	0.81
23.76	149.87	122.29	1.13	137.84	1.78	0.81	0.81
23.83	145.42	118.19	1.16	136.72	1.80	0.81	0.81
23.90	140.77	113.95	1.18	134.56	1.83	0.81	0.81
23.97	136.02	109.66	1.20	131.87	1.85	0.80	0.80
24.05	130.36	104.58	1.22	128.11	1.88	0.80	0.80
24.10	123.83	98.86	1.25	123.41	1.92	0.79	0.79
24.19	116.14	92.13	1.28	117.58	1.96	0.78	0.78
24.27	109.37	86.22	1.31	112.54	2.00	0.77	0.77
24.34	103.31	80.98	1.34	108.37	2.03	0.76	0.76
24.43	99.26	77.39	1.37	105.81	2.06	0.76	0.76
24.48	95.99	74.54	1.40	104.29	2.09	0.76	0.76
24.57	93.77	72.46	1.43	103.72	2.11	0.75	0.75
24.62	91.81	70.77	1.45	102.28	2.12	0.75	0.75
24.72	90.33	69.37	1.46	101.12	2.12	0.75	0.75
24.81	89.08	68.17	1.47	100.03	2.13	0.75	0.75
24.86	87.96	67.09	1.50	100.81	2.15	0.75	0.75
24.95	85.18	64.60	1.56	100.88	2.18	0.75	0.75
25.01	82.83	62.55	1.62	101.05	2.20	0.75	0.75
25.02	81.04	61.07	1.66	101.09	2.22	0.75	0.75
25.05	81.81	61.63	1.64	101.34	2.21	0.75	0.75
25.11	82.33	61.92	1.64	101.59	2.21	0.75	0.75
25.15	82.53	61.99	1.64	101.87	2.21	0.75	0.75
25.21	81.92	61.38	1.66	101.94	2.22	0.75	0.75
25.25	81.07	60.61	1.68	101.90	2.23	0.75	0.75
25.30	79.78	59.50	1.70	101.32	2.23	0.75	0.75
25.40	78.02	57.95	1.73	100.17	2.24	0.75	0.75
25.45	75.14	55.63	1.77	98.38	2.25	0.75	0.75

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.52	71.36	52.56	1.83	96.28	2.27	0.74	0.74
25.60	65.60	47.92	1.99	95.12	2.32	0.74	0.74
25.66	58.89	42.57	2.24	95.48	2.37	0.74	0.74
25.74	50.63	36.01	2.77	99.69	2.47	0.75	0.75
25.80	42.60	29.74	3.54	105.15	2.57	0.76	0.76
25.88	34.42	23.44	4.79	112.31	2.71	0.77	0.77
25.94	27.91	18.51	6.33	117.20	2.84	0.78	0.78
26.02	22.69	14.10	8.40	118.43	2.98	0.78	0.78
26.09	19.19	11.73	10.09	118.41	3.07	0.59	0.84
26.17	16.36	9.82	11.90	116.89	3.16	0.54	0.70
26.23	14.50	8.57	13.49	115.61	3.23	0.51	0.61
26.29	13.56	7.93	14.54	115.33	3.28	0.51	0.57
26.37	13.73	8.01	14.49	116.10	3.27	0.51	0.57
26.46	14.95	8.78	13.45	118.10	3.23	0.54	0.63
26.55	16.56	9.80	12.25	120.00	3.18	0.59	0.70
26.60	18.04	10.74	11.37	122.14	3.14	0.60	0.77
26.70	18.79	11.18	11.11	124.24	3.12	0.63	0.80
26.78	19.09	11.34	11.11	125.96	3.12	0.67	0.81
26.87	19.16	11.34	10.61	120.33	3.10	0.66	0.81
26.94	19.06	11.25	9.74	109.55	3.05	0.47	0.80
27.03	18.62	10.92	9.23	100.80	3.03	0.36	0.78
27.13	17.84	10.38	9.61	99.83	3.05	0.42	0.74
27.18	15.89	9.12	11.41	104.10	3.14	0.42	0.65
27.27	14.61	8.27	12.75	105.48	3.20	0.42	0.59
27.32	14.00	7.87	13.55	106.67	3.23	0.43	0.56
27.37	14.68	8.28	12.99	107.59	3.21	0.44	0.59
27.41	15.01	8.48	12.84	108.89	3.20	0.46	0.61
27.46	15.01	8.47	13.04	110.36	3.21	0.47	0.60
27.51	15.19	8.56	13.12	112.25	3.22	0.48	0.61
27.61	15.69	8.84	13.00	114.96	3.21	0.51	0.63
27.66	16.81	9.52	12.66	120.53	3.20	0.56	0.68
27.73	19.30	11.05	11.59	128.02	3.15	0.66	0.79
27.80	22.77	13.18	10.46	137.91	3.09	0.80	0.94
27.88	26.51	15.46	9.62	148.75	3.05	0.98	1.10
27.96	28.73	16.78	9.46	158.82	3.04	1.16	1.20
28.04	29.44	17.16	9.86	169.19	3.06	1.25	1.23
28.12	29.30	17.02	10.34	175.99	3.09	1.41	1.22
28.18	29.78	17.27	10.47	180.83	3.09	1.43	1.23
28.27	30.99	17.95	10.11	181.45	3.07	1.47	1.28
28.32	32.84	19.04	9.54	181.70	3.04	1.48	1.36
28.42	34.90	20.22	8.98	181.66	3.01	1.51	1.44
28.47	37.02	21.47	8.57	183.98	2.99	0.87	0.87
28.61	38.87	22.47	8.32	186.93	2.97	0.87	0.87
28.67	40.79	23.57	8.10	190.99	2.96	0.88	0.88
28.75	43.62	26.58	7.37	195.90	2.91	0.88	0.88
28.81	49.52	30.58	6.28	192.19	2.83	0.88	0.88
28.90	59.16	37.21	4.89	181.92	2.72	0.87	0.87
29.00	70.68	45.27	3.75	169.71	2.60	0.85	0.85

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
29.05	82.68	53.82	2.95	158.84	2.50	0.84	0.84
29.10	92.58	60.99	2.48	151.03	2.42	0.83	0.83
29.15	101.07	67.24	2.13	143.11	2.35	0.82	0.82
29.24	105.88	70.82	1.92	136.02	2.30	0.81	0.81
29.29	107.45	72.19	1.78	128.66	2.26	0.80	0.80
29.37	106.66	71.76	1.71	122.57	2.23	0.79	0.79
29.43	105.44	71.05	1.64	116.77	2.21	0.78	0.78
29.53	104.90	70.72	1.59	112.38	2.19	0.77	0.77
29.62	104.73	70.61	1.55	109.62	2.17	0.77	0.77
29.68	104.75	70.73	1.51	106.89	2.15	0.76	0.76
29.80	104.42	70.36	1.50	105.63	2.15	0.76	0.76
29.91	103.80	69.74	1.50	104.61	2.15	0.76	0.76
30.00	99.10	65.97	1.59	104.86	2.19	0.76	0.76
30.07	97.42	64.55	1.63	105.36	2.21	0.76	0.76
30.15	96.27	63.56	1.66	105.54	2.22	0.76	0.76
30.21	99.04	65.49	1.62	105.77	2.20	0.76	0.76
30.26	98.71	65.16	1.62	105.66	2.20	0.76	0.76
30.31	97.50	64.21	1.64	105.39	2.21	0.76	0.76
30.38	95.52	62.65	1.67	104.86	2.22	0.76	0.76
30.45	92.62	60.44	1.72	104.23	2.24	0.76	0.76
30.50	89.12	57.84	1.79	103.72	2.26	0.75	0.75
30.55	84.94	54.79	1.88	102.88	2.29	0.75	0.75
30.64	81.19	52.03	1.96	101.83	2.31	0.75	0.75
30.70	77.93	49.71	2.01	100.16	2.32	0.75	0.75
30.79	76.04	48.30	2.05	98.96	2.33	0.75	0.75
30.84	75.47	47.86	2.05	98.19	2.33	0.74	0.74
30.93	76.95	48.79	2.01	98.05	2.32	0.74	0.74
30.98	80.15	50.98	1.93	98.14	2.30	0.74	0.74
31.05	85.34	54.54	1.81	98.98	2.27	0.75	0.75
31.13	91.57	58.82	1.71	100.51	2.24	0.75	0.75
31.17	100.46	65.08	1.58	102.97	2.19	0.75	0.75
31.27	110.94	72.52	1.47	106.25	2.13	0.76	0.76
31.32	123.23	81.52	1.37	111.37	2.06	0.77	0.77
31.41	133.45	89.03	1.31	116.56	2.00	0.78	0.78
31.46	140.90	94.67	1.28	120.72	1.96	0.78	0.78
31.52	144.37	97.40	1.26	122.24	1.93	0.79	0.79
31.61	145.01	97.95	1.24	121.83	1.91	0.79	0.79
31.66	142.15	95.90	1.24	119.20	1.91	0.78	0.78
31.75	136.69	91.66	1.26	115.29	1.93	0.78	0.78
31.80	129.14	85.76	1.29	110.68	1.98	0.77	0.77
31.90	122.00	80.16	1.33	106.52	2.02	0.76	0.76
31.94	116.84	76.18	1.37	104.07	2.06	0.76	0.76
32.04	116.03	75.33	1.38	104.00	2.07	0.76	0.76
32.09	119.17	77.25	1.39	107.23	2.08	0.76	0.76
32.20	118.70	76.38	1.43	109.06	2.11	0.76	0.76
32.24	117.72	75.37	1.47	110.44	2.13	0.77	0.77
32.28	114.69	73.02	1.51	110.26	2.15	0.77	0.77
32.29	116.70	74.43	1.49	111.09	2.14	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
32.30	118.93	75.98	1.47	112.06	2.13	0.77	0.77
32.40	120.51	76.91	1.47	112.71	2.13	0.77	0.77
32.45	120.48	76.77	1.47	112.95	2.13	0.77	0.77
32.55	119.13	75.61	1.49	112.51	2.14	0.77	0.77
32.59	118.33	74.91	1.50	112.50	2.15	0.77	0.77
32.69	118.13	74.54	1.51	112.79	2.15	0.77	0.77
32.76	118.09	74.31	1.53	113.51	2.16	0.77	0.77
32.84	118.40	74.31	1.54	114.35	2.17	0.77	0.77
32.90	119.00	74.55	1.55	115.19	2.17	0.77	0.77
32.98	119.95	75.02	1.54	115.83	2.17	0.78	0.78
33.06	121.02	75.61	1.54	116.33	2.17	0.78	0.78
33.12	122.10	76.23	1.53	116.77	2.16	0.78	0.78
33.22	122.84	76.56	1.53	117.03	2.16	0.78	0.78
33.31	123.21	76.64	1.53	117.14	2.16	0.78	0.78
33.37	123.28	76.59	1.53	117.11	2.16	0.78	0.78
33.46	123.28	76.41	1.53	117.00	2.16	0.78	0.78
33.55	123.18	76.17	1.54	117.00	2.17	0.78	0.78
33.65	122.98	75.83	1.54	117.07	2.17	0.78	0.78
33.70	122.57	75.42	1.55	117.18	2.17	0.78	0.78
33.79	122.03	74.86	1.56	117.10	2.18	0.78	0.78
33.89	121.09	74.04	1.58	116.76	2.18	0.78	0.78
33.99	119.77	72.98	1.59	116.20	2.19	0.78	0.78
34.04	117.79	71.55	1.61	115.43	2.20	0.78	0.78
34.13	115.49	69.85	1.64	114.59	2.21	0.77	0.77
34.23	112.70	67.80	1.68	113.76	2.22	0.77	0.77
34.32	110.27	66.01	1.71	113.20	2.24	0.77	0.77
34.37	108.22	64.55	1.75	112.84	2.25	0.77	0.77
34.47	106.60	63.31	1.78	112.69	2.26	0.77	0.77
34.55	103.47	61.05	1.85	112.96	2.28	0.77	0.77
34.63	96.66	56.31	2.04	114.64	2.33	0.77	0.77
34.73	86.37	49.33	2.40	118.21	2.40	0.78	0.78
34.80	72.76	40.42	3.06	123.59	2.51	0.79	0.79
34.90	60.46	32.62	3.90	127.28	2.62	0.79	0.79
35.00	54.92	29.29	4.16	121.79	2.64	0.79	0.79
35.12	50.37	26.54	4.42	117.31	2.67	0.78	0.78
35.20	52.86	28.11	3.99	112.19	2.63	0.77	0.77
35.33	53.65	28.43	4.02	114.42	2.63	0.77	0.77
35.41	63.41	34.44	3.20	110.34	2.53	0.77	0.77
35.44	68.58	37.68	2.87	108.02	2.48	0.76	0.76
35.48	76.82	42.96	2.42	103.82	2.41	0.76	0.76
35.57	84.09	47.63	2.12	101.05	2.35	0.75	0.75
35.62	98.70	57.30	1.73	98.99	2.24	0.75	0.75
35.67	115.40	68.51	1.49	102.07	2.14	0.75	0.75
35.71	137.52	83.52	1.35	112.52	2.04	0.77	0.77
35.82	159.89	98.71	1.28	126.36	1.96	0.79	0.79
35.86	185.11	116.11	1.23	143.07	1.89	0.82	0.82
35.93	207.72	131.80	1.19	156.85	1.84	0.84	0.84
36.01	225.38	144.00	1.16	166.33	1.80	0.85	0.85

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
36.06	235.57	150.92	1.14	171.69	1.79	0.85	0.85
36.12	240.67	154.12	1.13	174.89	1.78	0.86	0.86
36.18	245.05	156.73	1.14	178.20	1.79	0.86	0.86
36.25	248.69	158.84	1.14	180.98	1.79	0.87	0.87
36.30	251.52	160.26	1.15	184.12	1.80	0.87	0.87
36.39	252.83	160.54	1.16	185.99	1.81	0.87	0.87
36.44	253.07	160.15	1.17	187.57	1.82	0.87	0.87
36.53	251.49	158.45	1.18	187.51	1.83	0.87	0.87
36.59	248.39	155.45	1.21	187.43	1.86	0.87	0.87
36.68	243.47	151.62	1.22	184.49	1.87	0.87	0.87
36.75	238.34	147.93	1.22	180.99	1.88	0.87	0.87
36.83	232.04	143.78	1.22	175.91	1.88	0.86	0.86
36.90	225.27	138.95	1.23	171.34	1.89	0.85	0.85
36.97	217.18	133.11	1.25	166.05	1.92	0.85	0.85
37.02	201.72	122.19	1.28	156.23	1.96	0.84	0.84
37.04	193.70	116.64	1.30	151.13	1.99	0.83	0.83
37.08	188.61	113.19	1.30	147.61	2.00	0.82	0.82
37.17	191.78	115.46	1.29	148.65	1.97	0.83	0.83
37.27	187.30	112.45	1.29	145.04	1.98	0.82	0.82
37.37	181.37	108.42	1.30	140.68	1.99	0.81	0.81
37.42	177.21	105.83	1.30	137.22	1.99	0.81	0.81
37.51	175.89	105.19	1.29	135.25	1.97	0.81	0.81
37.58	176.97	106.34	1.27	134.76	1.95	0.81	0.81
37.66	179.01	108.07	1.25	135.08	1.92	0.81	0.81
37.76	182.58	110.83	1.23	136.26	1.89	0.81	0.81
37.85	186.08	113.57	1.21	137.18	1.86	0.81	0.81
37.93	189.62	116.22	1.19	138.14	1.84	0.81	0.81
38.04	192.25	117.99	1.18	138.80	1.82	0.81	0.81
38.13	193.87	118.97	1.17	139.30	1.82	0.81	0.81
38.18	193.57	118.63	1.17	139.16	1.82	0.81	0.81
38.28	191.24	116.58	1.19	138.51	1.84	0.81	0.81
38.37	187.40	113.37	1.21	137.08	1.86	0.81	0.81
38.47	183.55	109.99	1.23	135.63	1.89	0.81	0.81
38.57	180.39	107.19	1.25	134.14	1.92	0.80	0.80
38.62	176.78	104.23	1.27	132.48	1.95	0.80	0.80
38.72	167.48	97.43	1.31	127.27	2.00	0.79	0.79
38.78	160.21	92.19	1.34	123.72	2.04	0.79	0.79
38.81	155.32	88.77	1.37	121.63	2.06	0.79	0.79
38.86	155.19	88.54	1.37	121.68	2.07	0.79	0.79
38.91	152.02	86.27	1.40	120.51	2.08	0.78	0.78
38.95	145.92	82.06	1.44	118.55	2.12	0.78	0.78
39.05	139.55	77.66	1.51	116.91	2.15	0.78	0.78
39.09	132.37	72.88	1.59	115.64	2.19	0.78	0.78
39.14	125.06	68.10	1.69	114.83	2.23	0.77	0.77
39.24	118.19	63.61	1.80	114.32	2.26	0.77	0.77
39.29	112.16	59.80	1.91	114.03	2.30	0.77	0.77
39.39	108.48	57.39	1.99	114.16	2.32	0.77	0.77
39.43	109.15	57.74	1.98	114.28	2.31	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
39.53	115.02	61.25	1.86	113.89	2.28	0.77	0.77
39.57	124.17	67.01	1.69	113.55	2.23	0.77	0.77
39.68	130.64	71.04	1.60	113.69	2.19	0.77	0.77
39.73	131.95	71.83	1.58	113.53	2.19	0.77	0.77
39.81	129.33	70.10	1.60	112.48	2.20	0.77	0.77
39.89	126.37	68.39	1.60	109.51	2.19	0.77	0.77
39.96	125.26	68.01	1.56	105.89	2.18	0.76	0.76
40.06	124.52	67.75	1.52	103.14	2.16	0.75	0.75
40.15	122.70	66.50	1.54	102.38	2.17	0.75	0.75
40.20	114.41	61.03	1.67	102.07	2.22	0.75	0.75
40.24	108.56	57.23	1.79	102.62	2.26	0.75	0.75
40.26	104.17	54.45	1.90	103.22	2.29	0.75	0.75
40.27	107.91	56.72	1.82	103.36	2.27	0.75	0.75
40.37	109.77	57.73	1.80	103.81	2.26	0.76	0.76
40.42	111.64	58.75	1.78	104.71	2.26	0.76	0.76
40.52	112.38	59.02	1.79	105.44	2.26	0.76	0.76
40.56	115.27	60.66	1.76	106.63	2.25	0.76	0.76
40.66	122.24	64.78	1.67	108.06	2.22	0.76	0.76
40.70	131.54	70.42	1.57	110.67	2.18	0.77	0.77
40.75	142.59	77.15	1.49	114.79	2.14	0.77	0.77
40.85	153.40	83.66	1.43	119.75	2.11	0.78	0.78
40.91	164.05	90.16	1.39	125.10	2.08	0.79	0.79
40.96	174.69	96.83	1.35	130.56	2.04	0.80	0.80
41.04	184.27	102.87	1.32	135.59	2.01	0.81	0.81
41.09	193.94	109.10	1.29	141.03	1.98	0.81	0.81
41.18	201.90	114.17	1.28	145.57	1.96	0.82	0.82
41.23	207.97	118.08	1.26	149.12	1.94	0.83	0.83
41.29	211.58	120.37	1.26	151.17	1.93	0.83	0.83
41.38	212.76	120.98	1.25	151.67	1.93	0.83	0.83
41.42	212.09	120.40	1.26	151.21	1.93	0.83	0.83
41.52	210.03	118.76	1.26	149.86	1.94	0.83	0.83
41.57	207.27	116.72	1.27	148.26	1.95	0.82	0.82
41.62	204.91	114.93	1.28	146.93	1.96	0.82	0.82
41.71	203.13	113.45	1.29	145.89	1.97	0.82	0.82
41.76	202.15	112.60	1.29	145.43	1.98	0.82	0.82
41.84	201.65	111.98	1.30	145.17	1.99	0.82	0.82
41.91	201.54	111.64	1.30	145.22	1.99	0.82	0.82
41.95	201.75	111.52	1.31	145.53	2.00	0.82	0.82
42.01	202.52	111.63	1.31	146.36	2.00	0.82	0.82
42.10	203.57	111.82	1.32	147.40	2.01	0.82	0.82
42.15	204.98	112.23	1.33	148.90	2.02	0.83	0.83
42.24	206.03	112.44	1.33	149.94	2.03	0.83	0.83
42.28	206.46	112.53	1.34	150.31	2.03	0.83	0.83
42.39	206.26	112.27	1.33	149.81	2.03	0.83	0.83
42.43	206.08	112.28	1.33	149.14	2.02	0.83	0.83
42.50	206.11	112.45	1.32	148.36	2.01	0.82	0.82
42.58	206.28	112.80	1.31	147.54	2.00	0.82	0.82
42.65	198.95	108.28	1.32	142.73	2.01	0.82	0.82

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
42.70	195.88	106.39	1.32	140.58	2.02	0.81	0.81
42.73	193.72	105.08	1.32	139.14	2.02	0.81	0.81
42.77	200.19	109.31	1.30	142.31	1.99	0.82	0.82
42.82	203.83	111.68	1.29	144.06	1.98	0.82	0.82
42.87	209.12	115.10	1.28	146.92	1.96	0.82	0.82
42.91	215.46	119.14	1.26	150.57	1.94	0.83	0.83
42.97	221.76	123.09	1.25	154.27	1.92	0.83	0.83
43.02	226.82	126.14	1.25	157.35	1.92	0.84	0.84
43.06	230.49	128.19	1.25	159.72	1.91	0.84	0.84
43.11	234.33	130.34	1.24	162.21	1.91	0.84	0.84
43.17	237.93	132.40	1.24	164.40	1.91	0.85	0.85
43.21	242.21	135.09	1.23	166.83	1.90	0.85	0.85
43.29	246.19	137.59	1.23	168.85	1.89	0.85	0.85
43.34	250.53	140.43	1.22	171.05	1.87	0.85	0.85
43.39	254.11	142.76	1.21	172.71	1.86	0.86	0.86
43.45	256.87	144.64	1.20	173.74	1.85	0.86	0.86
43.51	258.25	145.84	1.19	173.50	1.84	0.86	0.86
43.59	258.59	146.35	1.18	172.47	1.82	0.86	0.86
43.64	259.19	147.38	1.16	170.73	1.80	0.85	0.85
43.70	259.29	148.12	1.13	168.10	1.78	0.85	0.85
43.78	258.35	147.98	1.12	165.08	1.77	0.85	0.85
43.88	255.18	145.77	1.12	163.55	1.77	0.84	0.84
43.94	244.77	138.10	1.17	161.52	1.82	0.84	0.84
44.04	234.93	130.84	1.21	157.74	1.86	0.84	0.84
44.07	225.87	124.41	1.23	153.31	1.89	0.83	0.83
44.12	223.58	122.68	1.24	152.08	1.90	0.83	0.83
44.16	221.15	120.94	1.25	150.70	1.91	0.83	0.83
44.21	218.05	118.76	1.25	148.86	1.93	0.83	0.83
44.26	214.65	116.39	1.26	146.86	1.94	0.82	0.82
44.31	210.81	113.73	1.27	144.63	1.95	0.82	0.82
44.35	206.97	111.11	1.28	142.44	1.97	0.82	0.82
44.40	203.26	108.60	1.29	140.32	1.98	0.81	0.81
44.45	200.16	106.49	1.30	138.56	1.99	0.81	0.81
44.50	197.83	104.91	1.31	137.24	2.00	0.81	0.81
44.54	195.81	103.53	1.32	136.15	2.01	0.81	0.81
44.60	193.46	101.86	1.32	134.97	2.02	0.81	0.81
44.64	190.96	100.11	1.34	133.85	2.03	0.80	0.80
44.69	188.57	98.42	1.35	132.85	2.05	0.80	0.80
44.74	187.78	97.76	1.36	132.59	2.05	0.80	0.80
44.79	187.17	97.27	1.36	132.34	2.06	0.80	0.80
44.83	187.71	97.52	1.36	132.53	2.05	0.80	0.80
44.88	188.84	98.15	1.35	132.96	2.05	0.80	0.80
44.93	191.20	99.52	1.35	134.02	2.04	0.80	0.80
44.98	193.69	100.99	1.34	135.20	2.03	0.81	0.81
45.03	195.31	101.90	1.33	135.95	2.03	0.81	0.81
45.08	196.49	102.54	1.33	136.45	2.03	0.81	0.81
45.16	197.53	103.08	1.33	136.81	2.02	0.81	0.81
45.19	198.24	103.58	1.32	136.91	2.02	0.81	0.81

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
45.27	198.44	103.76	1.32	136.53	2.01	0.81	0.81
45.32	197.56	103.38	1.31	135.53	2.00	0.81	0.81
45.37	195.58	102.45	1.31	133.73	2.00	0.80	0.80
45.45	192.44	100.80	1.30	131.17	1.99	0.80	0.80
45.51	187.22	97.91	1.30	127.52	1.99	0.79	0.79
45.56	180.52	93.92	1.31	123.37	2.01	0.79	0.79
45.61	169.84	87.34	1.35	117.60	2.04	0.78	0.78
45.69	156.32	78.89	1.42	111.79	2.10	0.77	0.77
45.75	137.42	67.17	1.61	108.19	2.20	0.76	0.76
45.81	115.31	54.45	1.93	105.04	2.30	0.76	0.76
45.89	93.28	42.25	2.49	105.10	2.42	0.76	0.76
45.94	73.36	31.83	3.26	103.73	2.54	0.75	0.75
46.04	59.21	24.44	4.42	108.05	2.67	0.76	0.76
46.08	46.61	18.15	6.18	112.07	2.83	0.77	0.77
46.15	39.94	13.37	8.22	109.85	2.97	0.77	0.77
46.17	36.10	11.98	9.26	110.89	3.03	0.63	0.86
46.18	36.17	12.00	9.18	110.17	3.02	0.63	0.86
46.23	36.48	12.10	9.03	109.18	3.01	0.62	0.86
46.27	37.18	12.34	8.72	107.58	3.00	0.76	0.76
46.32	38.64	12.85	8.20	105.33	2.96	0.76	0.76
46.41	40.63	15.29	7.01	107.19	2.89	0.76	0.76
46.47	43.16	16.49	6.44	106.19	2.85	0.76	0.76
46.52	45.45	17.54	6.09	106.89	2.82	0.76	0.76
46.56	47.57	18.46	5.95	109.81	2.81	0.77	0.77
46.65	49.42	19.21	5.91	113.60	2.80	0.77	0.77
46.71	51.52	20.07	5.86	117.68	2.80	0.78	0.78
46.76	54.41	21.37	5.62	120.04	2.78	0.78	0.78
46.85	58.19	23.13	5.21	120.43	2.75	0.78	0.78
46.90	63.28	25.63	4.63	118.71	2.69	0.78	0.78
46.99	67.89	27.93	4.16	116.19	2.65	0.78	0.78
47.04	70.35	29.16	3.93	114.63	2.62	0.77	0.77
47.10	69.50	28.71	4.00	114.71	2.63	0.77	0.77
47.16	65.45	26.63	4.36	116.10	2.67	0.78	0.78
47.23	59.62	23.71	4.94	117.23	2.72	0.78	0.78
47.30	51.46	19.76	5.97	117.96	2.81	0.78	0.78
47.38	42.76	13.97	8.12	113.48	2.96	0.77	0.77
47.43	34.23	10.97	10.19	111.84	3.08	0.65	0.78
47.52	28.17	8.83	11.99	105.92	3.17	0.55	0.63
47.59	23.92	7.34	12.70	93.23	3.20	0.41	0.52
47.66	21.40	6.45	12.70	81.89	3.20	0.22	0.46
47.77	19.71	5.85	12.77	74.67	3.20	0.23	0.42
47.82	18.77	5.51	13.75	75.76	3.24	0.23	0.39
47.91	18.38	5.37	14.28	76.63	3.26	0.24	0.38
47.93	17.68	5.12	15.17	77.65	3.30	0.24	0.37
47.97	17.78	5.15	15.21	78.37	3.30	0.25	0.37
48.02	17.86	5.17	15.38	79.56	3.31	0.26	0.37
48.07	18.51	5.39	15.07	81.21	3.30	0.27	0.38
48.12	18.61	5.42	15.51	84.04	3.31	0.29	0.39

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
48.19	18.71	5.44	15.90	86.54	3.33	0.33	0.39
48.23	18.91	5.51	16.11	88.74	3.33	0.34	0.39
48.31	19.15	5.58	16.11	89.88	3.33	0.35	0.40
48.35	19.35	5.64	16.11	90.92	3.33	0.36	0.40
48.40	19.25	5.60	16.37	91.72	3.34	0.37	0.40
48.45	18.81	5.45	16.96	92.39	3.36	0.37	0.39
48.50	18.07	5.19	17.92	92.93	3.40	0.38	0.37
48.55	17.80	5.09	18.35	93.37	3.41	0.38	0.36
48.59	17.64	5.03	18.75	94.24	3.42	0.39	0.36
48.67	17.87	5.10	18.56	94.62	3.42	0.40	0.36
48.73	17.84	5.08	18.58	94.36	3.42	0.39	0.36
48.78	17.97	5.12	18.13	92.80	3.40	0.38	0.37
48.83	17.97	5.11	17.74	90.68	3.39	0.36	0.37
48.91	17.94	5.09	17.35	88.35	3.38	0.33	0.36
48.98	17.84	5.05	17.10	86.35	3.37	0.32	0.36
49.03	17.74	5.01	17.00	85.19	3.37	0.31	0.36
49.12	17.68	4.98	16.65	82.90	3.35	0.30	0.36
49.17	17.75	5.00	15.91	79.48	3.33	0.26	0.36
49.27	18.02	5.08	15.07	76.51	3.30	0.22	0.36
49.31	18.56	5.25	14.57	76.55	3.28	0.24	0.38
49.38	19.20	5.46	14.44	78.88	3.27	0.26	0.39
49.45	19.70	5.62	14.44	81.15	3.27	0.28	0.40
49.51	19.00	5.38	15.44	83.00	3.31	0.29	0.38
49.54	19.44	5.52	15.24	84.13	3.30	0.30	0.39
49.59	20.18	5.76	14.65	84.45	3.28	0.31	0.41
49.64	21.53	6.21	13.47	83.63	3.23	0.31	0.44
49.73	21.20	6.09	13.64	83.01	3.24	0.29	0.43
49.83	20.02	5.68	14.52	82.47	3.27	0.29	0.41
49.92	18.88	5.29	15.55	82.19	3.31	0.29	0.38
49.98	17.86	4.94	16.51	81.62	3.35	0.28	0.35
50.07	17.33	4.75	17.04	81.01	3.37	0.27	0.34
50.16	16.99	4.63	17.38	80.51	3.38	0.27	0.33
50.24	16.69	4.52	17.70	80.06	3.39	0.27	0.32
50.32	16.46	4.44	17.99	79.87	3.40	0.26	0.32
50.41	16.32	4.39	18.25	80.02	3.41	0.26	0.31
50.50	16.36	4.39	18.25	80.09	3.41	0.27	0.31
50.56	16.26	4.35	18.25	79.36	3.41	0.27	0.31
50.66	16.09	4.28	18.27	78.27	3.41	0.25	0.31
50.74	15.92	4.22	18.37	77.53	3.41	0.24	0.30
50.84	15.85	4.19	19.00	79.62	3.43	0.25	0.30
50.93	15.95	4.21	19.91	83.88	3.46	0.30	0.30
50.98	16.77	4.47	20.59	92.08	3.48	0.35	0.32
51.08	19.60	5.39	19.08	102.75	3.43	0.47	0.38
51.17	24.45	6.95	16.30	113.31	3.34	0.63	0.50
51.24	30.11	8.78	13.98	122.80	3.25	0.75	0.63
51.34	33.65	9.91	13.03	129.12	3.21	0.89	0.71
51.41	34.16	10.06	12.19	122.59	3.18	0.93	0.72
51.51	32.81	9.60	12.05	115.66	3.17	0.50	0.69

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
51.58	31.20	9.06	11.80	106.93	3.16	0.61	0.65
51.68	29.95	8.64	12.73	109.98	3.20	0.60	0.62
51.79	27.39	7.80	14.12	110.16	3.26	0.59	0.56
51.82	25.87	7.31	15.07	110.15	3.30	0.59	0.52
51.85	24.39	6.83	16.27	111.07	3.34	0.59	0.49
51.91	25.00	7.01	16.14	113.23	3.34	0.60	0.50
52.00	24.87	6.96	16.71	116.25	3.36	0.67	0.50
52.05	27.06	7.65	15.54	118.92	3.31	0.70	0.55
52.10	31.78	9.15	13.00	118.95	3.21	0.72	0.65
52.19	38.49	11.27	10.28	115.81	3.08	0.73	0.80
52.28	44.04	13.02	8.58	111.69	2.99	0.77	0.77
52.34	46.37	13.74	7.96	109.32	2.95	0.76	0.76
52.42	46.09	13.63	8.05	109.66	2.96	0.77	0.77
52.48	44.34	13.05	8.50	111.03	2.98	0.77	0.77
52.57	42.32	12.39	8.98	111.27	3.01	0.69	0.88
52.62	40.26	11.73	9.37	109.88	3.03	0.66	0.84
52.69	38.51	11.16	9.58	106.89	3.05	0.61	0.80
52.77	36.89	10.63	9.83	104.50	3.06	0.56	0.76
52.87	35.55	10.19	10.19	103.83	3.08	0.55	0.73
52.91	34.07	9.71	10.56	102.56	3.10	0.57	0.69
53.01	32.55	9.21	11.08	102.13	3.12	0.49	0.66
53.10	32.18	9.08	11.35	103.11	3.14	0.52	0.65
53.16	34.04	9.65	11.74	113.26	3.15	0.59	0.69
53.25	38.69	11.08	11.13	123.32	3.13	0.87	0.79
53.29	44.28	12.82	10.63	136.25	3.10	0.97	0.92
53.38	48.90	14.23	10.13	144.18	3.07	1.22	1.02
53.42	59.32	17.47	8.56	149.47	2.99	0.83	0.83
53.47	74.66	22.21	6.75	150.02	2.87	0.83	0.83
53.52	92.88	27.85	5.32	148.22	2.76	0.82	0.82
53.58	102.94	30.94	4.93	152.55	2.72	0.83	0.83
53.66	103.80	31.15	5.14	160.18	2.74	0.84	0.84
53.75	98.64	29.50	5.74	169.41	2.79	0.85	0.85
53.81	88.93	26.46	6.64	175.67	2.86	0.86	0.86
53.87	78.89	23.33	7.63	177.89	2.93	0.86	0.86
53.95	67.24	19.70	9.07	178.71	3.02	1.90	1.41
54.01	57.35	16.64	10.67	177.57	3.10	1.79	1.19
54.06	47.51	13.60	12.71	172.90	3.20	1.68	0.97
54.15	41.78	11.83	14.16	167.57	3.26	1.42	0.85
54.20	40.60	11.46	14.42	165.24	3.27	1.40	0.82
54.29	47.57	13.59	12.09	164.23	3.17	1.54	0.97
54.34	69.40	20.27	7.00	141.87	2.89	0.82	0.82
54.43	100.37	29.73	3.65	108.63	2.59	0.76	0.76
54.45	137.16	41.00	2.00	82.07	2.32	0.69	0.71
54.48	166.07	49.83	1.62	80.59	2.20	0.61	0.71
54.52	185.51	55.76	1.48	82.69	2.14	0.71	0.71
54.53	198.85	59.83	1.45	86.57	2.12	0.72	0.72
54.58	207.94	62.58	1.44	89.91	2.11	0.73	0.73
54.62	219.64	66.13	1.42	93.59	2.10	0.74	0.74

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
54.65	233.46	70.33	1.38	96.81	2.07	0.74	0.74
54.70	244.67	73.72	1.36	99.98	2.05	0.75	0.75
54.76	251.12	75.64	1.35	102.23	2.05	0.75	0.75
54.77	249.88	75.25	1.37	102.77	2.06	0.75	0.75
54.82	251.50	75.71	1.36	103.16	2.06	0.75	0.75
54.87	253.07	76.14	1.36	103.55	2.05	0.75	0.75
54.88	255.63	76.92	1.35	104.08	2.05	0.76	0.76
54.91	257.28	77.39	1.35	104.56	2.05	0.76	0.76
54.96	263.42	79.22	1.34	106.09	2.04	0.76	0.76
54.97	276.70	83.26	1.32	109.90	2.01	0.77	0.77
55.03	294.89	88.74	1.30	115.47	1.99	0.78	0.78
55.09	315.21	94.86	1.27	120.89	1.96	0.78	0.78
55.15	327.84	98.63	1.23	121.55	1.89	0.79	0.79
55.20	338.35	101.77	1.20	122.41	1.85	0.79	0.79
55.25	358.17	107.74	1.13	121.49	1.78	0.79	0.79
55.30	386.84	116.38	1.11	129.28	1.77	0.80	0.80
55.34	417.50	125.63	1.07	134.62	1.74	0.81	0.81
55.39	440.05	132.40	1.10	146.03	1.76	0.82	0.82
55.40	462.28	139.13	1.10	153.71	1.76	0.83	0.83
55.44	482.80	145.29	1.08	157.35	1.75	0.84	0.84
55.44	511.21	153.88	1.02	157.04	1.72	0.84	0.84
55.49	517.76	155.78	1.03	160.78	1.72	0.84	0.84
55.54	533.43	160.44	1.05	167.71	1.73	0.85	0.85
55.59	534.98	160.82	1.10	176.17	1.76	0.86	0.86
55.63	551.08	165.61	1.09	180.34	1.75	0.86	0.86
55.64	553.47	166.31	1.09	180.79	1.75	0.87	0.87
55.68	566.94	170.31	1.06	179.92	1.73	0.86	0.86
55.69	570.38	171.33	1.04	178.50	1.73	0.86	0.86
55.69	566.17	170.04	1.05	179.38	1.73	0.86	0.86
55.71	561.62	168.63	1.09	183.08	1.75	0.87	0.87
55.76	567.28	170.25	1.10	186.45	1.76	0.87	0.87
55.78	580.19	174.11	1.08	187.85	1.75	0.87	0.87
55.81	581.23	174.36	1.04	180.96	1.72	0.87	0.87
55.85	584.16	175.16	1.00	175.16	1.69	0.86	0.86
55.86	588.34	176.41	1.00	176.41	1.65	0.86	0.86
55.91	598.65	179.42	1.00	179.42	1.62	0.86	0.86
55.92	602.25	180.48	1.00	180.48	1.60	0.87	0.87
55.96	619.03	185.46	1.00	185.46	1.58	0.87	0.87
55.97	634.09	189.98	1.00	189.98	1.57	0.88	0.88
56.00	654.37	196.01	1.00	196.01	1.56	0.88	0.88
56.01	660.12	197.72	1.00	197.72	1.58	0.88	0.88
56.03	661.79	198.18	1.00	198.18	1.59	0.88	0.88
56.05	661.82	198.14	1.00	198.14	1.60	0.88	0.88
56.10	665.04	198.99	1.00	198.99	1.60	0.89	0.89
56.12	668.02	199.86	1.00	199.86	1.58	0.89	0.89
56.16	667.69	199.67	1.00	199.67	1.57	0.89	0.89
56.17	654.78	195.76	1.00	195.76	1.57	0.88	0.88
56.20	635.11	189.78	1.00	189.78	1.59	0.88	0.88

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
56.22	617.48	184.46	1.00	184.46	1.61	0.87	0.87
56.24	608.45	181.69	1.00	181.69	1.61	0.87	0.87
56.30	602.69	179.84	1.00	179.84	1.62	0.86	0.86
56.31	595.69	177.72	1.00	177.72	1.63	0.86	0.86
56.34	586.22	174.82	1.00	174.82	1.65	0.86	0.86
56.39	579.04	172.57	1.00	172.57	1.66	0.86	0.86
56.45	572.30	170.44	1.00	170.44	1.67	0.85	0.85
56.48	565.39	168.31	1.00	168.31	1.67	0.85	0.85
56.49	555.45	165.32	1.00	165.32	1.70	0.85	0.85
56.53	542.15	161.25	1.05	168.57	1.73	0.85	0.85
56.58	529.04	157.24	1.08	169.38	1.75	0.85	0.85
56.63	524.73	155.86	1.00	155.86	1.67	0.83	0.83
56.68	526.01	156.17	1.00	156.17	1.58	0.84	0.84
56.73	531.33	157.68	1.00	157.68	1.53	0.84	0.84
56.78	526.31	156.09	1.00	156.09	1.62	0.84	0.84
56.83	517.99	153.53	1.00	153.53	1.69	0.83	0.83
56.89	503.37	149.05	1.06	157.35	1.73	0.84	0.84
56.95	485.04	143.50	1.12	160.76	1.77	0.84	0.84
56.99	470.25	139.02	1.16	161.37	1.81	0.84	0.84
57.01	460.92	136.23	1.18	160.98	1.83	0.84	0.84
57.04	461.73	136.41	1.18	160.65	1.82	0.84	0.84
57.09	468.20	138.26	1.17	161.13	1.81	0.84	0.84
57.11	477.43	140.98	1.16	163.57	1.81	0.84	0.84
57.13	488.62	144.26	1.16	167.47	1.81	0.85	0.85
57.18	488.78	144.24	1.17	169.44	1.82	0.85	0.85
57.19	477.80	140.96	1.20	168.95	1.85	0.85	0.85
57.21	464.47	136.96	1.21	166.30	1.87	0.85	0.85
57.24	456.12	134.45	1.22	164.00	1.88	0.85	0.85
57.28	456.72	134.56	1.21	163.35	1.87	0.84	0.84
57.32	450.91	132.78	1.22	161.45	1.87	0.84	0.84
57.35	445.39	131.08	1.22	160.03	1.88	0.84	0.84
57.38	435.59	128.14	1.23	157.50	1.89	0.84	0.84
57.43	430.50	126.56	1.23	155.53	1.89	0.83	0.83
57.48	414.66	121.80	1.23	150.26	1.90	0.83	0.83
57.52	398.59	116.98	1.23	143.92	1.89	0.82	0.82
57.57	389.56	114.25	1.25	142.28	1.91	0.82	0.82
57.62	396.66	116.29	1.26	146.53	1.94	0.82	0.82
57.68	427.50	125.32	1.25	157.03	1.92	0.84	0.84
57.76	462.23	135.46	1.23	166.00	1.88	0.85	0.85
57.81	505.50	148.16	1.09	161.17	1.75	0.84	0.84
57.86	543.58	159.31	1.00	159.31	1.63	0.84	0.84
57.89	572.52	167.80	1.00	167.80	1.49	0.85	0.85
57.91	583.54	171.02	1.00	171.02	1.48	0.85	0.85
57.92	577.13	169.11	1.00	169.11	1.50	0.85	0.85
57.95	569.05	166.67	1.00	166.67	1.54	0.85	0.85
57.99	570.66	167.08	1.00	167.08	1.56	0.85	0.85
58.01	578.72	169.42	1.00	169.42	1.57	0.85	0.85
58.05	591.19	173.02	1.00	173.02	1.58	0.86	0.86

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
58.05	598.87	175.27	1.00	175.27	1.59	0.86	0.86
58.10	604.77	176.91	1.00	176.91	1.60	0.86	0.86
58.13	611.17	178.73	1.00	178.73	1.60	0.86	0.86
58.15	618.51	180.87	1.00	180.87	1.60	0.87	0.87
58.17	625.12	182.75	1.00	182.75	1.59	0.87	0.87
58.20	623.43	182.21	1.00	182.21	1.59	0.87	0.87
58.21	619.40	181.00	1.00	181.00	1.60	0.87	0.87
58.21	614.30	179.50	1.00	179.50	1.61	0.86	0.86
58.23	613.93	179.34	1.00	179.34	1.61	0.86	0.86
58.24	608.11	177.62	1.00	177.62	1.62	0.86	0.86
58.25	609.21	177.92	1.00	177.92	1.54	0.86	0.86
58.29	613.99	179.26	1.00	179.26	1.44	0.86	0.86
58.31	627.24	183.11	1.00	183.11	1.32	0.87	0.87
58.33	639.00	186.52	1.00	186.52	1.34	0.87	0.87
58.38	651.36	190.06	1.00	190.06	1.37	0.88	0.88
58.39	661.87	193.13	1.00	193.13	1.39	0.88	0.88
58.43	670.53	195.59	1.00	195.59	1.40	0.88	0.88
58.43	682.73	199.15	1.00	199.15	1.39	0.89	0.89
58.48	688.02	200.60	1.00	200.60	1.40	0.89	0.89
58.53	694.39	202.36	1.00	202.36	1.41	0.89	0.89
58.56	696.37	202.90	1.00	202.90	1.46	0.89	0.89
58.58	704.43	205.20	1.00	205.20	1.47	0.89	0.89
58.59	710.90	207.06	1.00	207.06	1.49	0.89	0.89
58.63	707.18	205.90	1.00	205.90	1.49	0.89	0.89
58.63	709.20	206.49	1.00	206.49	1.50	0.89	0.89
58.63	695.36	202.42	1.00	202.42	1.51	0.89	0.89
58.68	700.19	203.74	1.00	203.74	1.49	0.89	0.89
58.69	701.88	204.22	1.00	204.22	1.45	0.89	0.89
58.72	717.85	208.81	1.00	208.81	1.40	0.90	0.90
58.73	722.94	210.28	1.00	210.28	1.38	0.90	0.90
58.74	728.64	211.92	1.00	211.92	1.41	0.90	0.90
58.77	726.96	211.36	1.00	211.36	1.44	0.90	0.90
58.81	722.67	210.02	1.00	210.02	1.47	0.90	0.90
58.82	713.94	207.44	1.00	207.44	1.49	0.89	0.89
58.83	715.80	207.97	1.00	207.97	1.51	0.90	0.90
58.87	722.33	209.78	1.00	209.78	1.52	0.90	0.90
58.91	731.67	212.41	1.00	212.41	1.53	0.90	0.90
58.92	737.87	214.21	1.00	214.21	1.54	0.90	0.90
58.93	740.53	214.95	1.00	214.95	1.53	0.90	0.90
58.96	739.05	214.44	1.00	214.44	1.53	0.90	0.90
59.01	716.31	207.70	1.00	207.70	1.56	0.89	0.89
59.06	687.29	199.13	1.00	199.13	1.59	0.89	0.89
59.08	655.28	189.77	1.00	189.77	1.63	0.88	0.88
59.11	638.94	184.95	1.00	184.95	1.65	0.87	0.87
59.15	627.21	181.46	1.00	181.46	1.68	0.87	0.87
59.21	618.28	178.75	1.00	178.75	1.70	0.86	0.86
59.26	606.09	175.11	1.02	178.89	1.72	0.86	0.86
59.30	592.31	171.02	1.01	173.20	1.71	0.86	0.86

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
59.35	579.87	167.32	1.01	169.07	1.71	0.85	0.85
59.40	562.76	162.26	1.04	168.73	1.73	0.85	0.85
59.42	550.96	158.81	1.06	168.34	1.74	0.85	0.85
59.47	539.34	155.35	1.08	167.78	1.75	0.85	0.85
59.51	539.41	155.29	1.09	168.63	1.75	0.85	0.85
59.56	537.97	154.79	1.09	168.59	1.75	0.85	0.85
59.61	537.36	154.53	1.06	164.50	1.74	0.85	0.85
59.67	541.98	155.77	1.00	155.77	1.70	0.83	0.83
59.71	553.73	159.11	1.00	159.11	1.65	0.84	0.84
59.80	555.82	159.56	1.00	159.56	1.61	0.84	0.84
59.85	552.45	158.50	1.00	158.50	1.59	0.84	0.84
59.90	542.21	155.47	1.00	155.47	1.59	0.83	0.83
60.00	542.99	155.53	1.00	155.53	1.59	0.83	0.83
60.04	541.71	155.09	1.00	155.09	1.60	0.83	0.83
60.10	526.52	150.62	1.00	150.62	1.63	0.83	0.83
60.15	508.32	145.30	1.00	145.30	1.67	0.82	0.82
60.19	487.40	139.22	1.00	139.22	1.70	0.81	0.81
60.23	483.49	138.03	1.00	138.03	1.69	0.81	0.81
60.28	482.61	137.71	1.00	137.71	1.68	0.81	0.81
60.33	488.98	139.47	1.00	139.47	1.67	0.81	0.81
60.38	491.97	140.26	1.00	140.26	1.67	0.81	0.81
60.42	493.85	140.74	1.00	140.74	1.69	0.81	0.81
60.44	487.18	138.79	1.01	140.24	1.71	0.81	0.81
60.47	475.94	135.53	1.08	145.72	1.74	0.82	0.82
60.52	465.53	132.47	1.12	148.94	1.78	0.83	0.83
60.56	462.70	131.60	1.15	150.90	1.79	0.83	0.83
60.57	465.03	132.25	1.15	151.48	1.79	0.83	0.83
60.61	470.62	133.80	1.13	151.48	1.78	0.83	0.83
60.66	477.29	135.64	1.12	151.98	1.77	0.83	0.83
60.71	486.66	138.25	1.11	153.21	1.77	0.83	0.83
60.76	495.25	140.63	1.11	156.59	1.77	0.84	0.84
60.81	504.76	143.27	1.11	159.58	1.77	0.84	0.84
60.86	523.05	148.43	1.08	161.02	1.75	0.84	0.84
60.91	559.78	158.84	1.00	158.84	1.70	0.84	0.84
60.95	601.50	170.69	1.00	170.69	1.66	0.85	0.85
61.00	637.66	180.91	1.00	180.91	1.64	0.87	0.87
61.02	657.74	186.60	1.00	186.60	1.64	0.87	0.87
61.05	685.10	194.34	1.00	194.34	1.62	0.88	0.88
61.08	710.24	201.44	1.00	201.44	1.61	0.89	0.89
61.09	731.84	207.57	1.00	207.57	1.59	0.89	0.89
61.13	737.94	209.24	1.00	209.24	1.59	0.90	0.90
61.14	739.46	209.63	1.00	209.63	1.60	0.90	0.90
61.16	741.44	210.15	1.00	210.15	1.60	0.90	0.90
61.20	750.88	212.77	1.00	212.77	1.58	0.90	0.90
61.23	762.13	215.88	1.00	215.88	1.56	0.90	0.90
61.24	766.92	217.23	1.00	217.23	1.52	0.90	0.90
61.29	758.86	214.83	1.00	214.83	1.51	0.90	0.90
61.30	744.24	210.65	1.00	210.65	1.52	0.90	0.90

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
61.33	734.57	207.82	1.00	207.82	1.55	0.90	0.90
61.38	730.90	206.66	1.00	206.66	1.55	0.89	0.89
61.43	731.07	206.60	1.00	206.60	1.53	0.89	0.89
61.48	738.25	208.54	1.00	208.54	1.50	0.90	0.90
61.53	750.91	212.02	1.00	212.02	1.48	0.90	0.90
61.56	754.78	213.05	1.00	213.05	1.48	0.90	0.90
61.58	726.93	205.10	1.00	205.10	1.50	0.89	0.89
61.59	702.39	198.13	1.00	198.13	1.52	0.88	0.88
61.62	600.70	169.24	1.00	169.24	1.61	0.85	0.85
61.63	595.30	167.67	1.00	167.67	1.61	0.85	0.85
61.67	588.36	165.65	1.00	165.65	1.62	0.85	0.85
61.71	662.66	186.61	1.00	186.61	1.55	0.87	0.87
61.76	655.52	184.50	1.00	184.50	1.55	0.87	0.87
61.81	634.02	178.32	1.00	178.32	1.54	0.86	0.86
61.86	615.02	172.85	1.00	172.85	1.52	0.86	0.86
61.87	600.83	168.83	1.00	168.83	1.48	0.85	0.85
61.91	588.87	165.39	1.00	165.39	1.44	0.85	0.85
61.95	578.02	162.25	1.00	162.25	1.42	0.84	0.84
61.96	566.74	159.04	1.00	159.04	1.42	0.84	0.84
62.00	553.70	155.30	1.00	155.30	1.45	0.83	0.83
62.04	535.16	150.01	1.00	150.01	1.49	0.83	0.83
62.06	510.97	143.15	1.00	143.15	1.55	0.82	0.82
62.10	491.66	137.65	1.00	137.65	1.60	0.81	0.81
62.14	475.52	133.04	1.00	133.04	1.64	0.80	0.80
62.20	463.08	129.46	1.00	129.46	1.66	0.80	0.80
62.22	439.20	122.70	1.00	122.70	1.71	0.79	0.79
62.27	415.48	115.96	1.08	125.13	1.75	0.79	0.79
62.29	396.37	110.55	1.13	125.44	1.78	0.79	0.79
62.34	380.26	105.96	1.17	124.22	1.82	0.79	0.79
62.39	366.62	102.08	1.21	123.46	1.86	0.79	0.79
62.43	347.78	96.73	1.26	121.51	1.93	0.79	0.79
62.49	340.13	94.52	1.28	121.38	1.97	0.79	0.79
62.57	336.43	93.40	1.30	121.70	1.99	0.79	0.79
62.68	357.18	99.12	1.29	127.79	1.98	0.80	0.80
62.75	398.26	110.56	1.26	139.12	1.93	0.81	0.81
62.87	426.23	118.25	1.24	146.86	1.91	0.82	0.82
62.88	409.21	113.48	1.25	142.25	1.93	0.82	0.82
62.89	424.34	117.70	1.21	142.29	1.86	0.82	0.82
62.93	485.42	134.75	1.06	142.80	1.74	0.82	0.82
62.98	571.92	158.87	1.00	158.87	1.61	0.84	0.84
63.02	620.24	172.30	1.00	172.30	1.47	0.86	0.86
63.07	658.55	182.93	1.00	182.93	1.31	0.87	0.87
63.12	710.78	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.14	752.36	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.17	781.30	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.17	799.36	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.20	825.98	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.21	830.83	-1.00	1.00	-1.00	-1.00	0.00	0.00

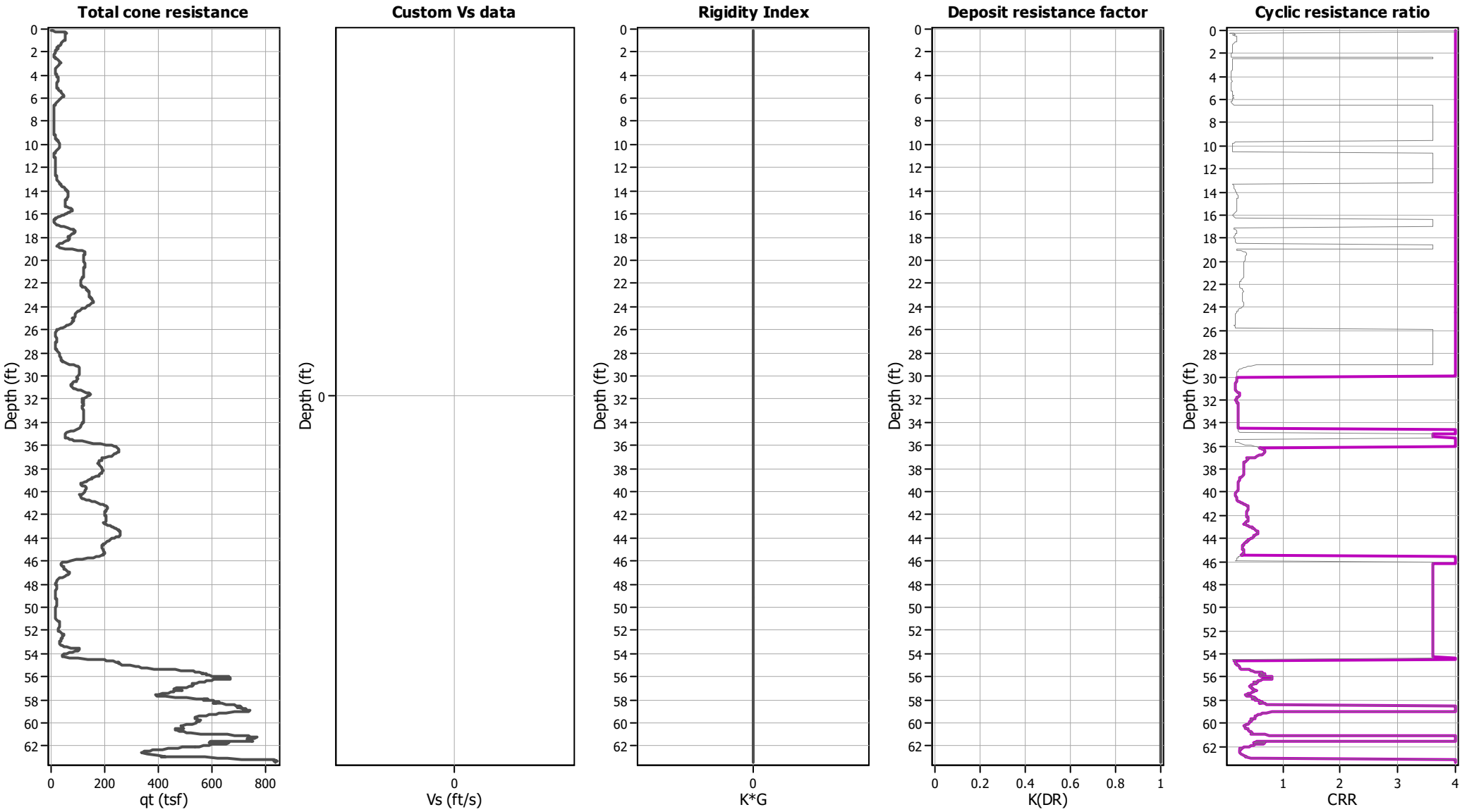
:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
63.23	842.91	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.26	834.75	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.28	841.52	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.31	838.10	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.32	839.38	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.36	837.12	-1.00	1.00	-1.00	-1.00	0.00	0.00
63.40	836.85	-1.00	1.00	-1.00	-1.00	0.00	0.00

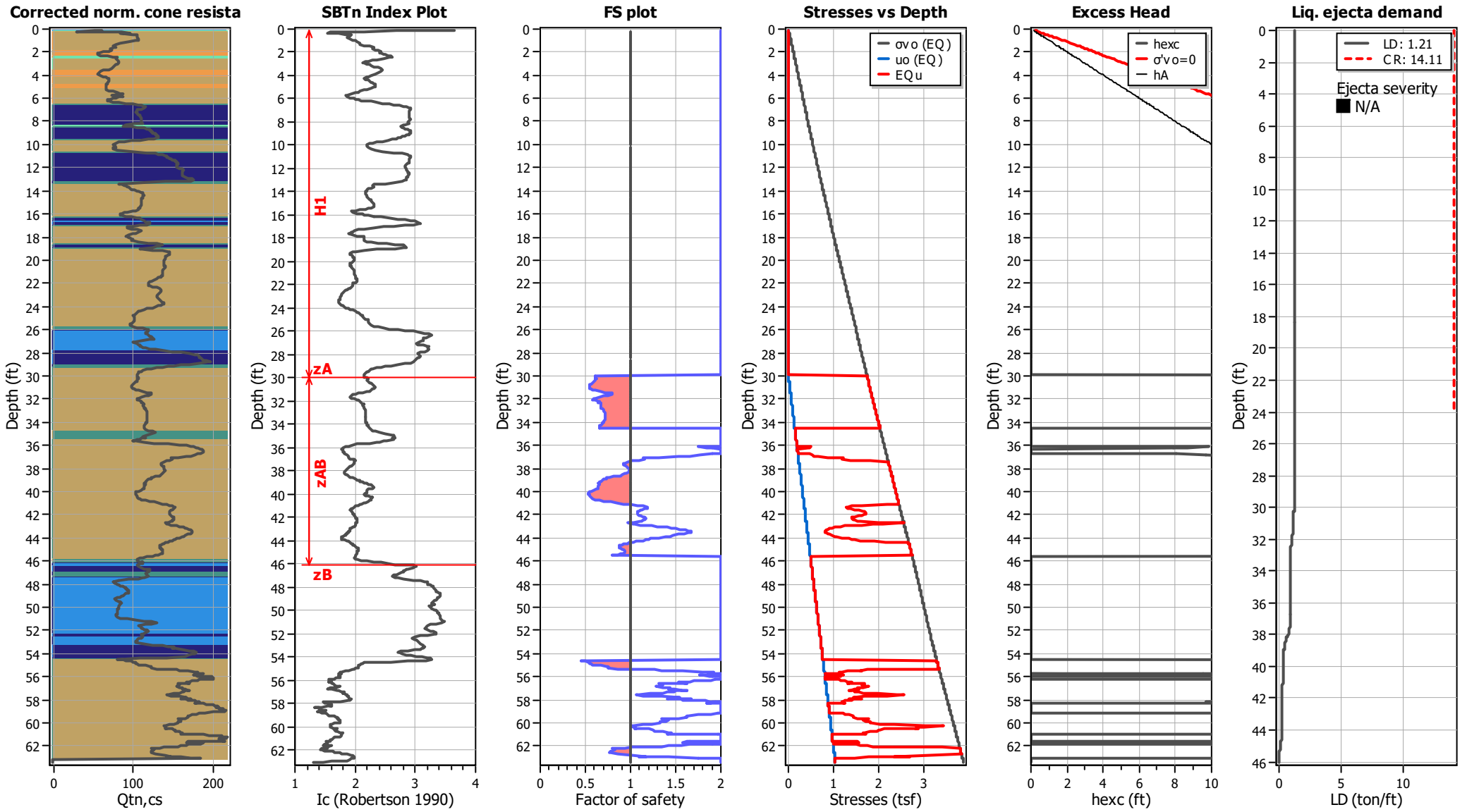
Abbreviations

q_t: Total cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Adjusted and corrected cone resistance due to fines
I_c: Soil behavior type index
$S_{u(liq)}/\sigma'_v$: Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$: Calculated peak undrained strength ratio

Aging Calculation Estimation



Ejecta Severity Estimation



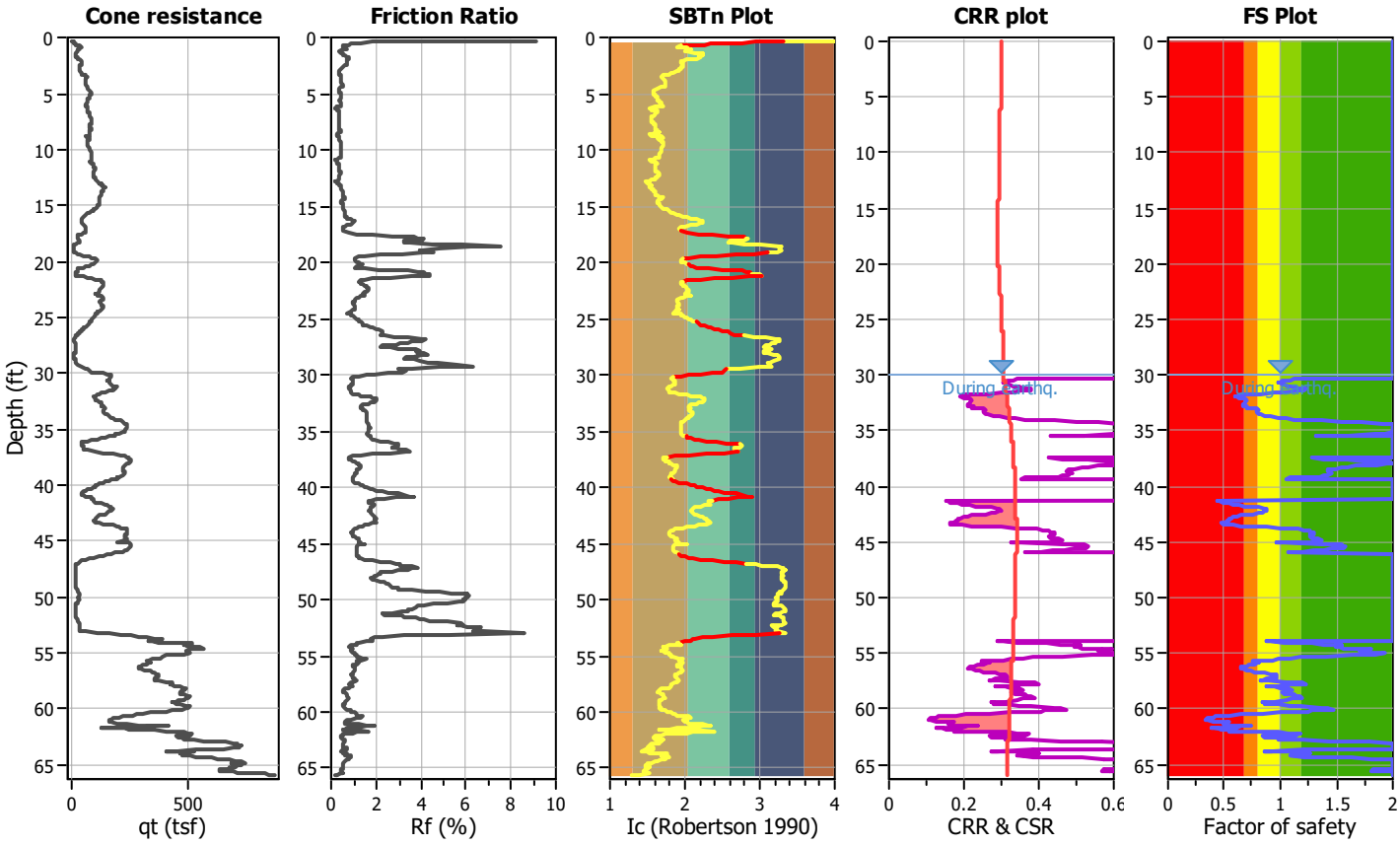
LIQUEFACTION ANALYSIS REPORT

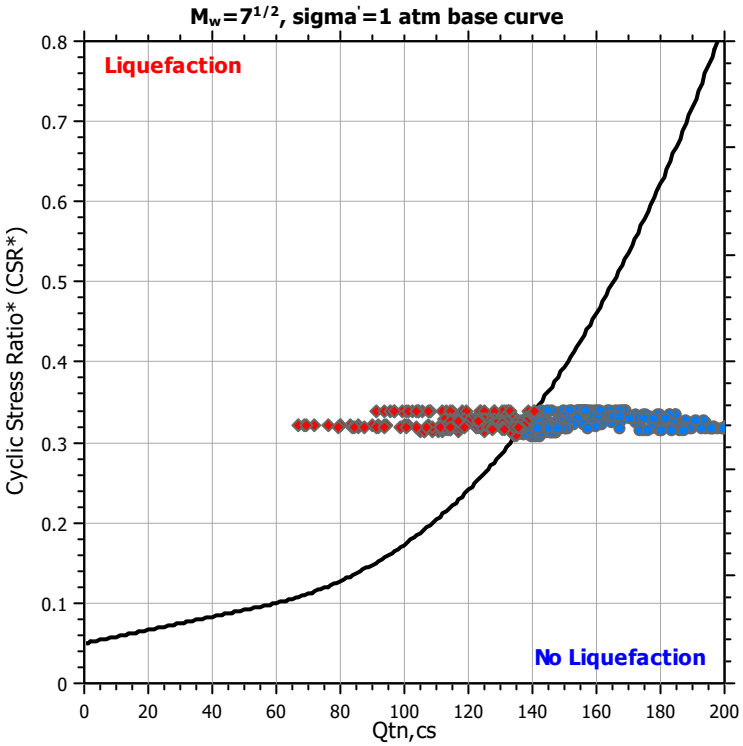
Project title : W1857-88-01 **Location : 331 The City Drive S**

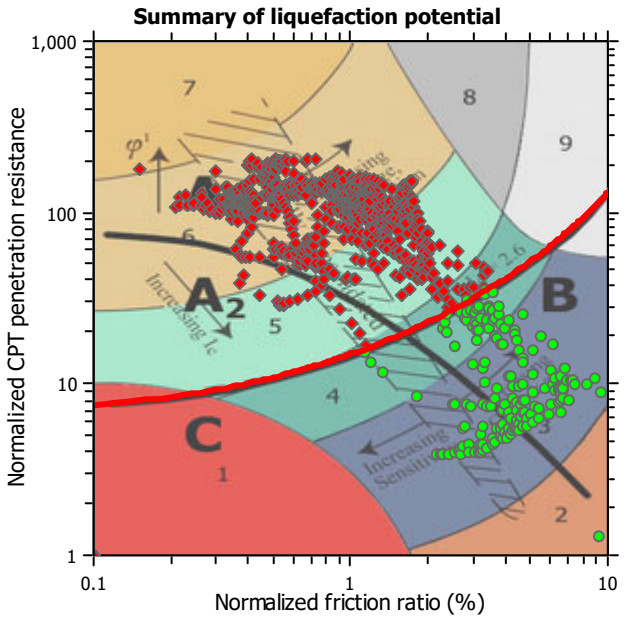
CPT file : CPT-2

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	54.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	30.00 ft	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.65	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.63	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

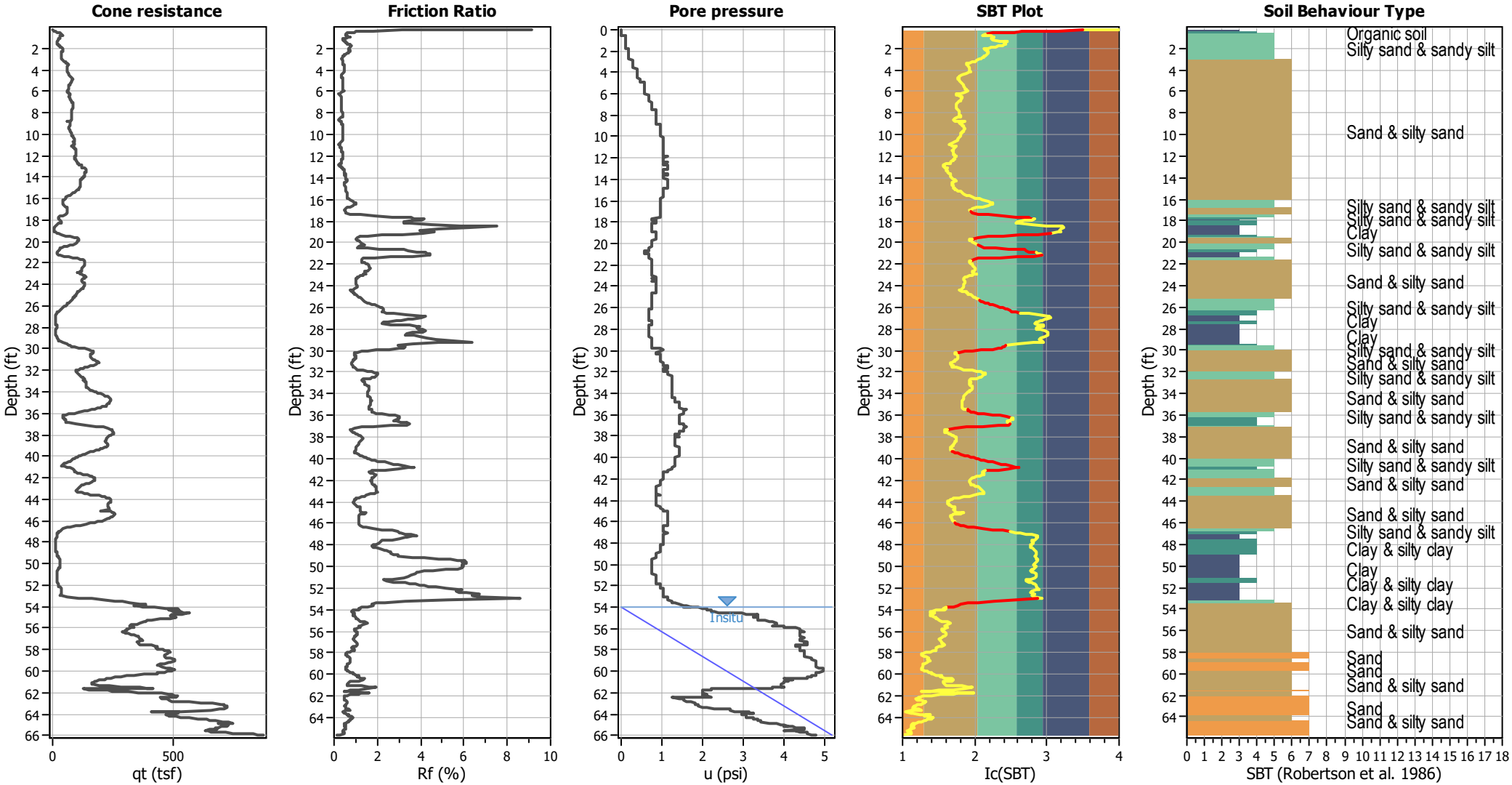






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



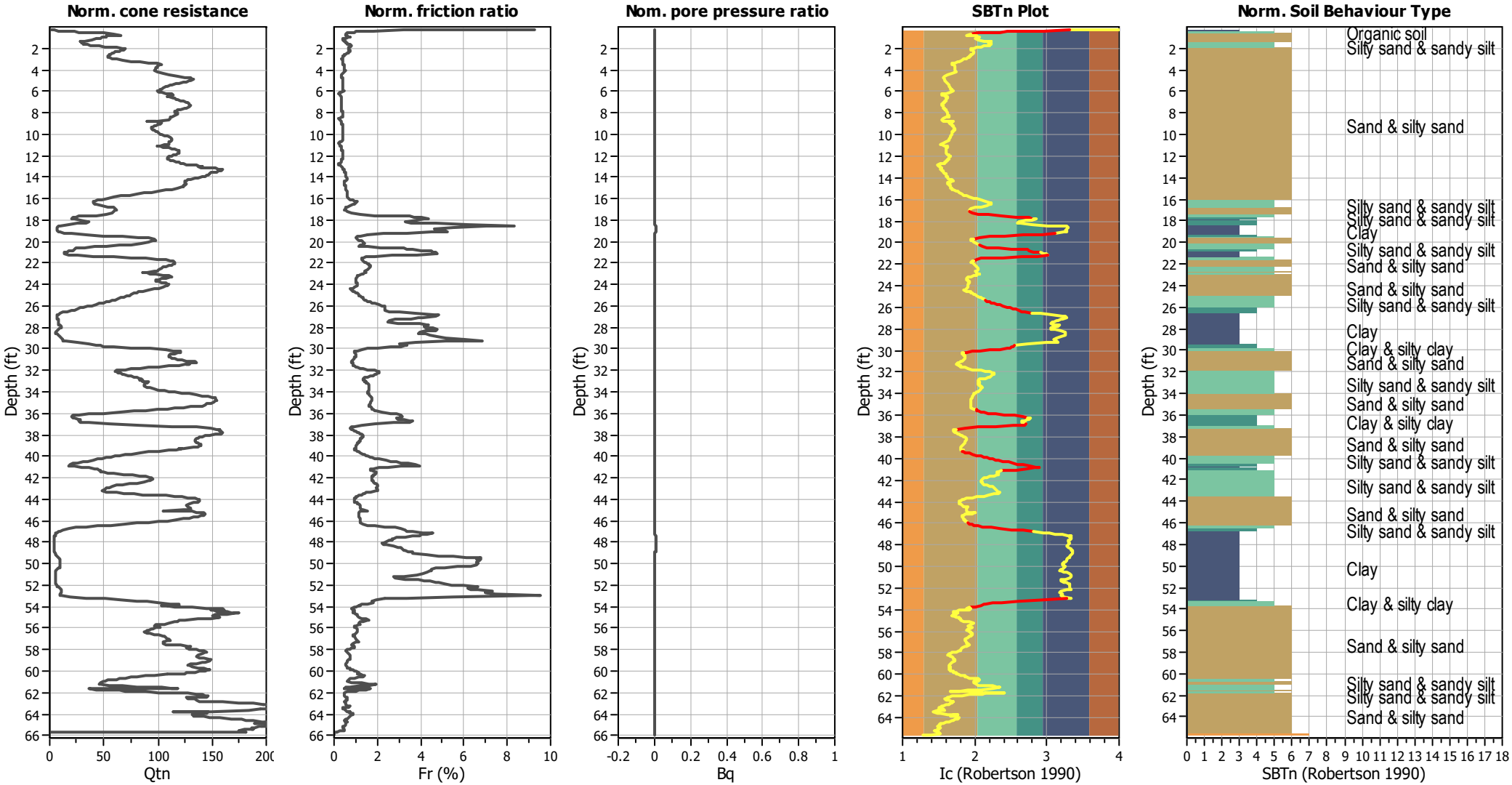
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



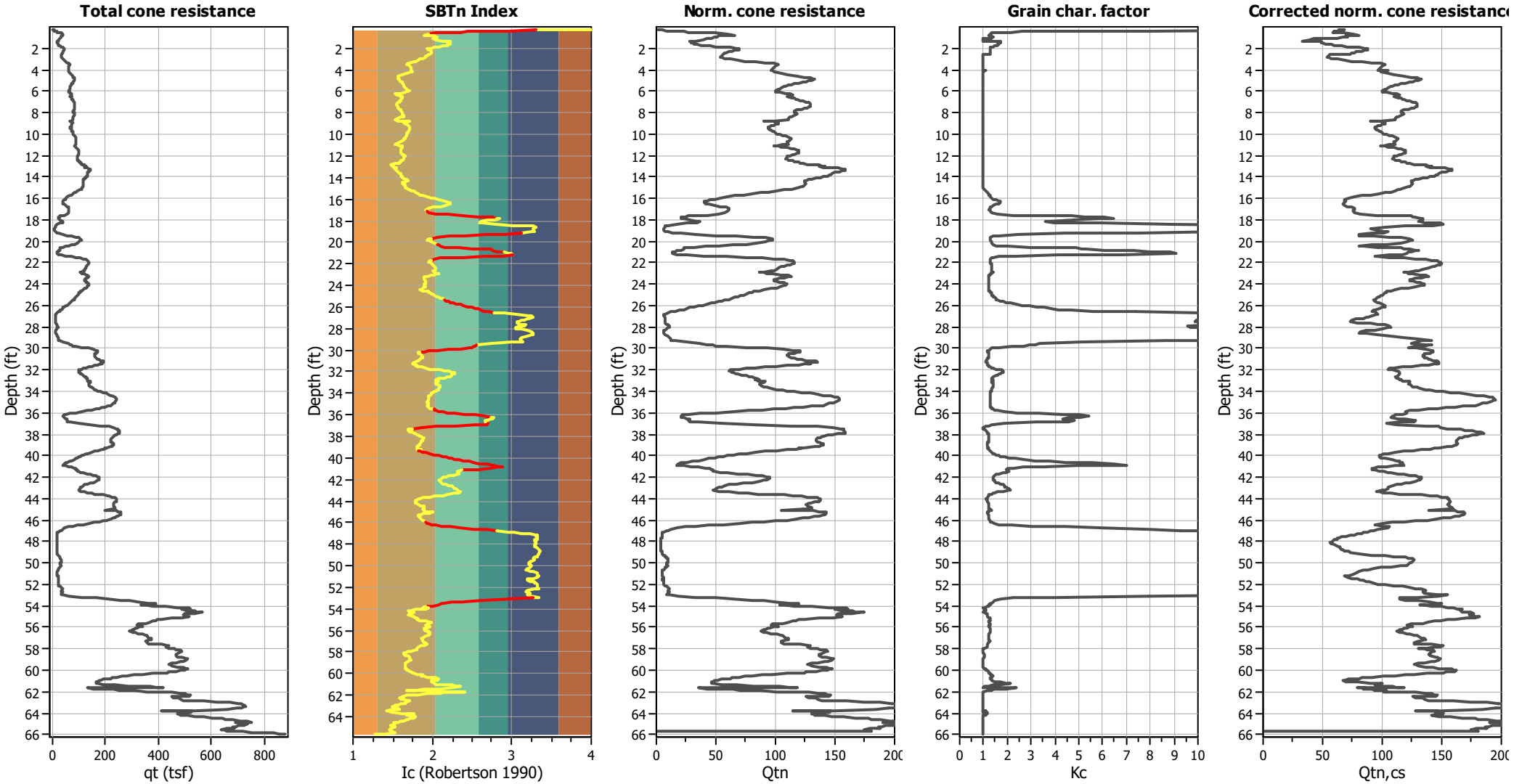
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

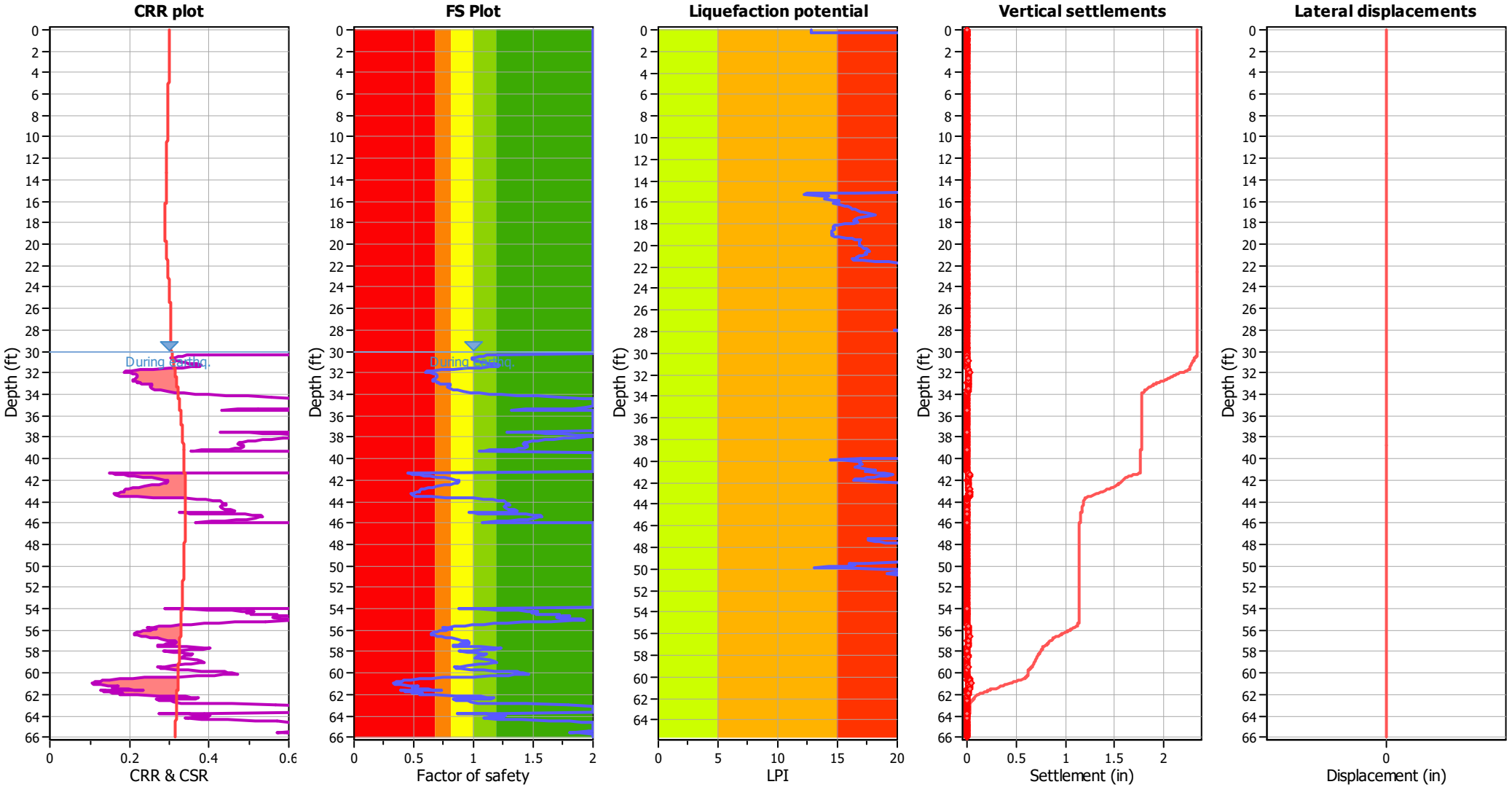
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

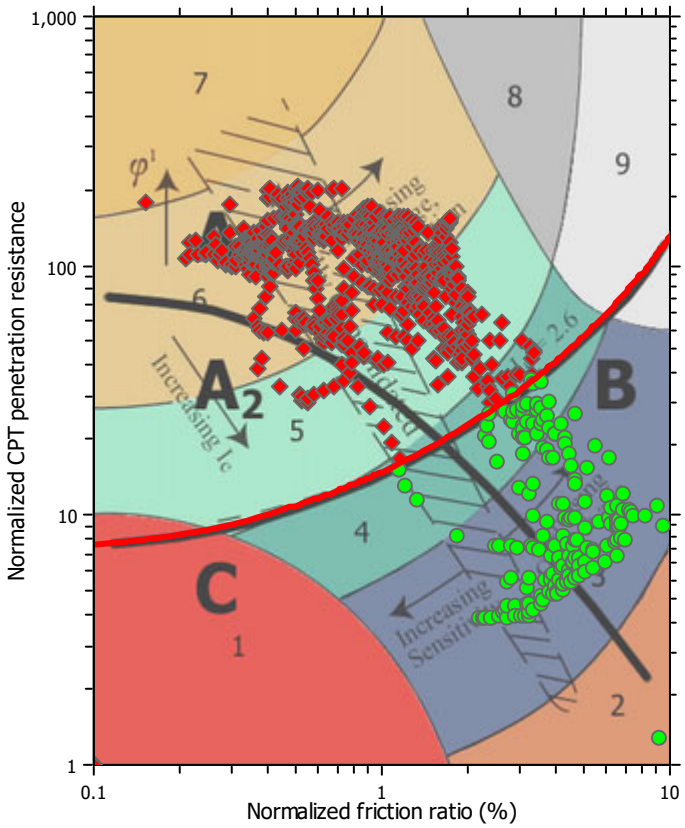
F.S. color scheme

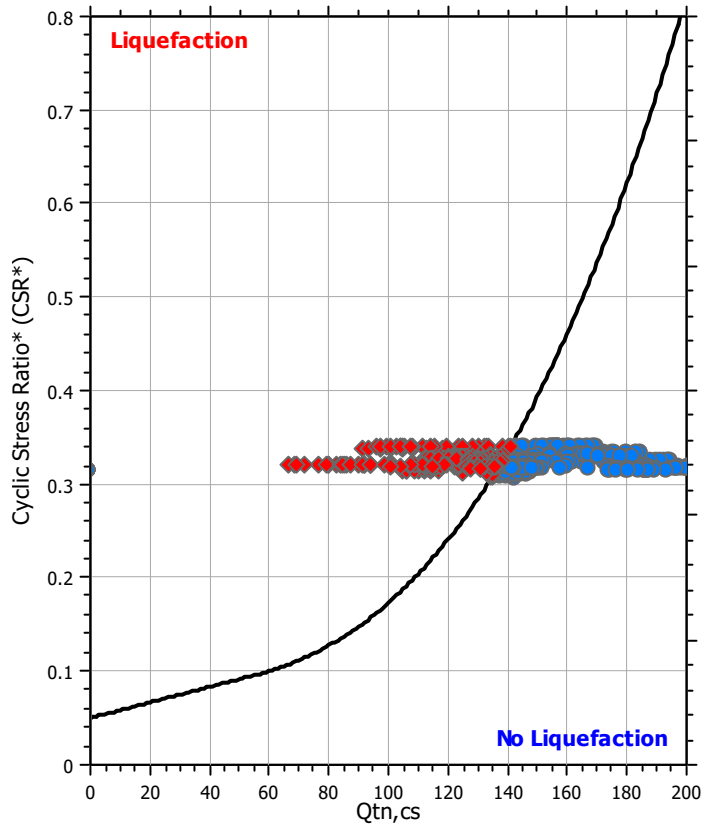
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

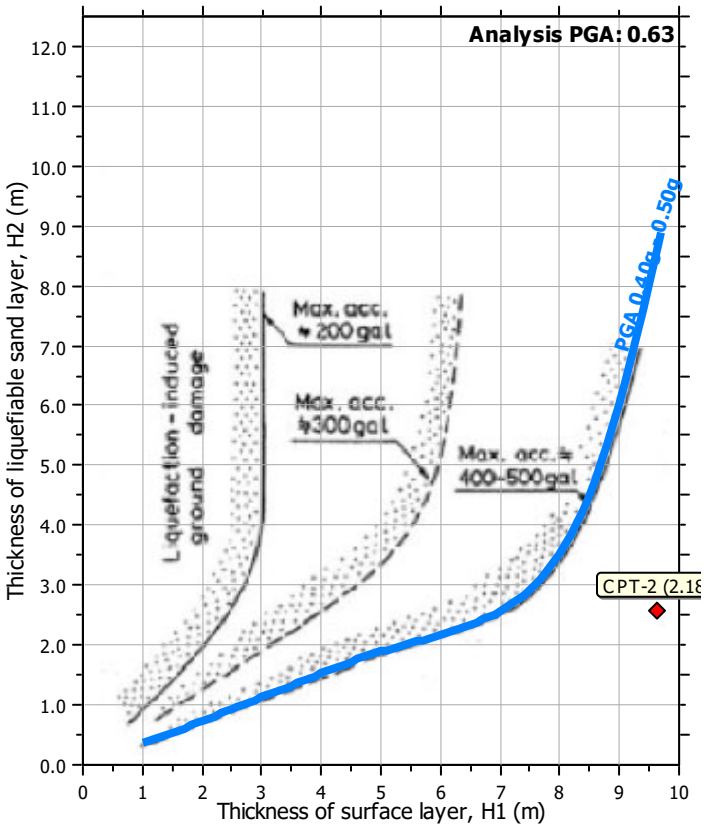
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



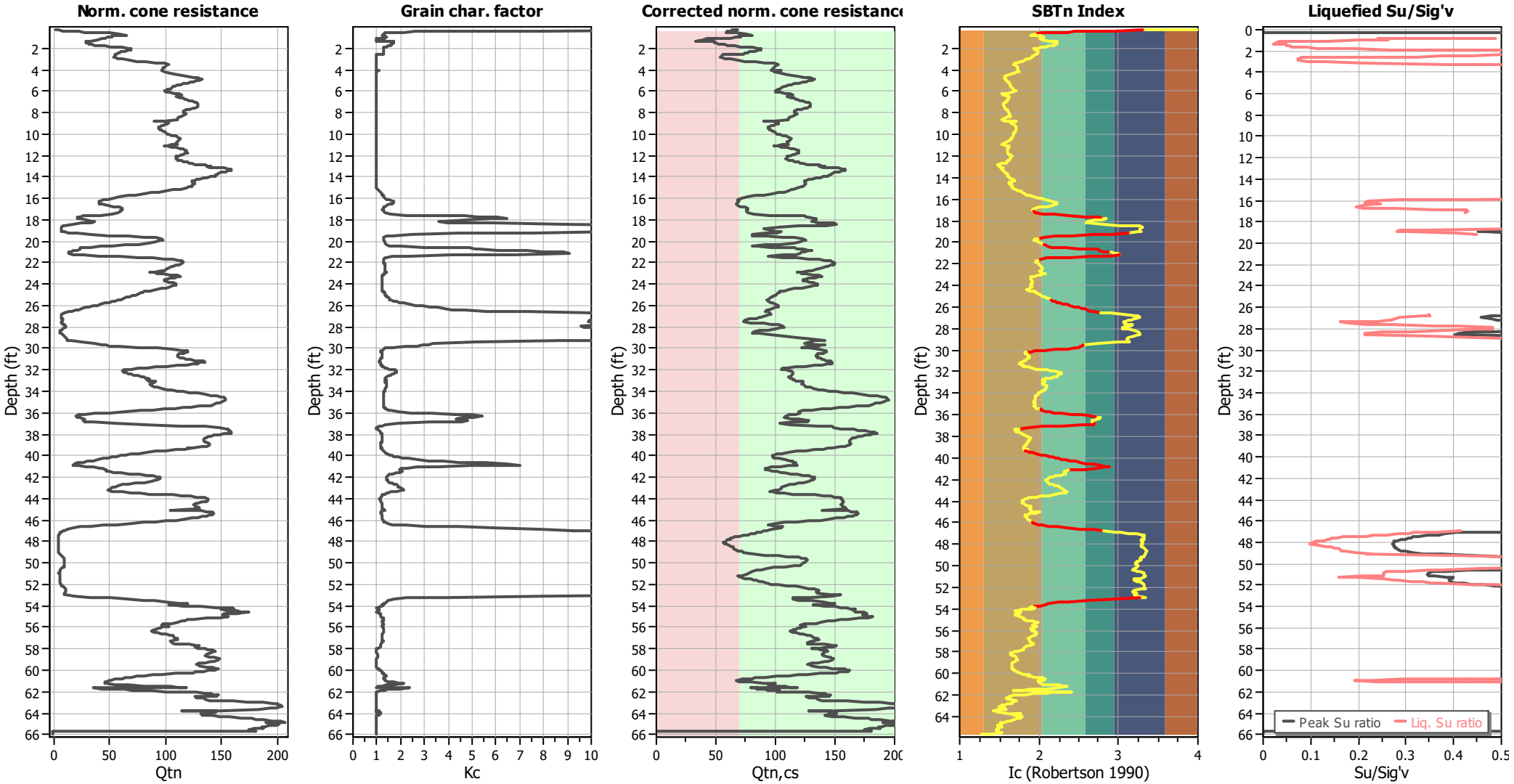




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

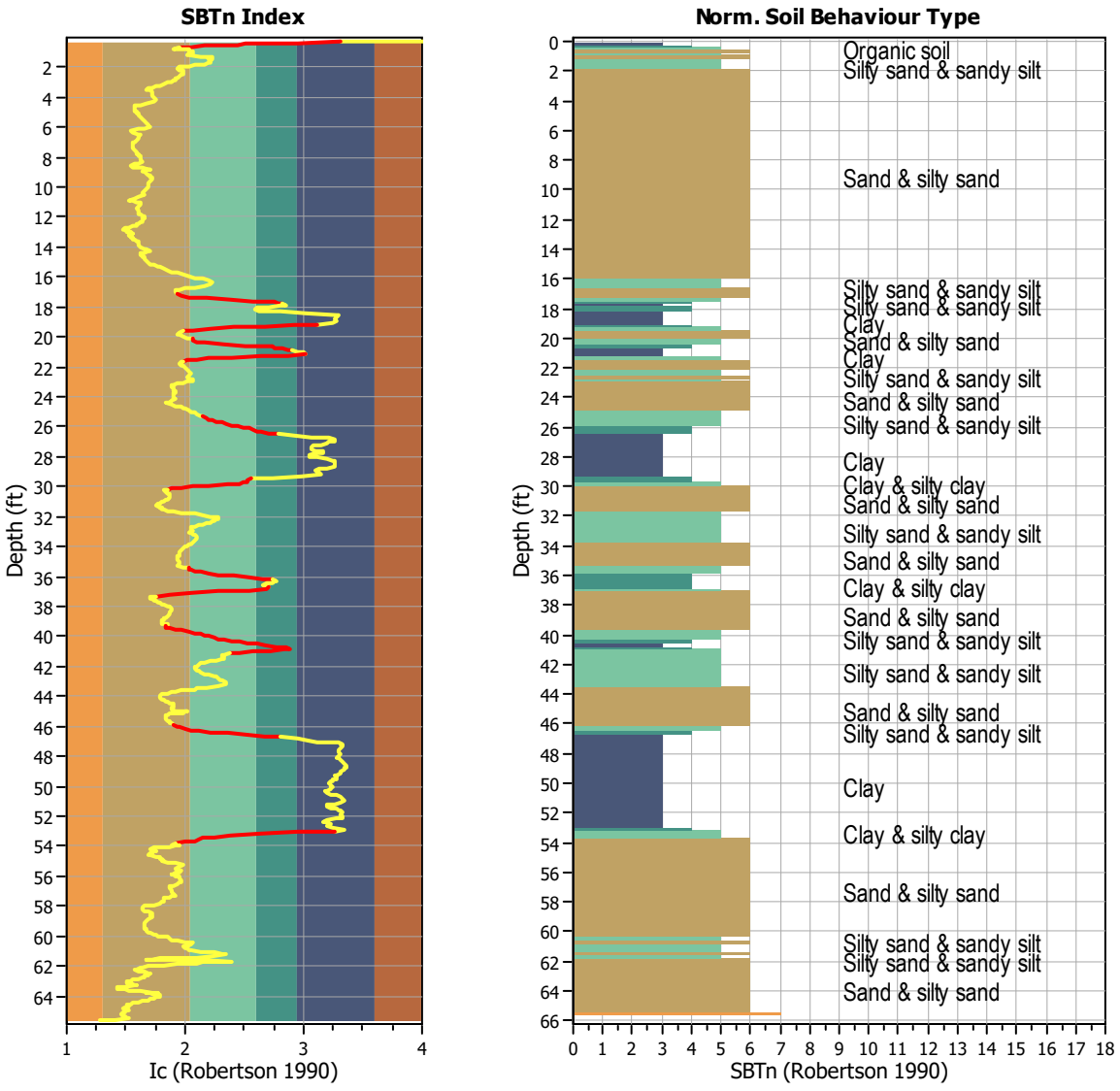
Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	1012
I_c maximum check value:	3.00	Total points excluded:	145
I_c change ratio value:	0.0250	Exclusion percentage:	14.33%
Minimum number of points in layer:	4	Number of layers detected:	13

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	13	Start depth: 0.36 (ft)	3	Clay
		End depth: 0.76 (ft)	6	Sand & silty sand
Transition layer 2	10	Start depth: 17.22 (ft)	6	Sand & silty sand
		End depth: 17.85 (ft)	3	Clay
Transition layer 3	7	Start depth: 19.22 (ft)	3	Clay
		End depth: 19.69 (ft)	6	Sand & silty sand
Transition layer 4	13	Start depth: 20.26 (ft)	5	Silty sand & sandy silt
		End depth: 20.96 (ft)	3	Clay
Transition layer 5	8	Start depth: 21.25 (ft)	3	Clay
		End depth: 21.69 (ft)	6	Sand & silty sand
Transition layer 6	16	Start depth: 25.41 (ft)	5	Silty sand & sandy silt
		End depth: 26.61 (ft)	3	Clay
Transition layer 7	12	Start depth: 29.63 (ft)	4	Clay & silty clay
		End depth: 30.24 (ft)	6	Sand & silty sand
Transition layer 8	11	Start depth: 35.51 (ft)	5	Silty sand & sandy silt
		End depth: 36.28 (ft)	4	Clay & silty clay
Transition layer 9	7	Start depth: 36.86 (ft)	4	Clay & silty clay
		End depth: 37.39 (ft)	6	Sand & silty sand
Transition layer 10	20	Start depth: 39.39 (ft)	6	Sand & silty sand
		End depth: 40.84 (ft)	3	Clay
Transition layer 11	7	Start depth: 40.84 (ft)	3	Clay
		End depth: 41.22 (ft)	5	Silty sand & sandy silt
Transition layer 12	11	Start depth: 46.02 (ft)	6	Sand & silty sand
		End depth: 46.84 (ft)	3	Clay
Transition layer 13	10	Start depth: 53.10 (ft)	3	Clay
		End depth: 53.92 (ft)	6	Sand & silty sand

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.01	0.00	0.00	0.00	N/A	120.90
2	0.04	-0.10	0.01	0.00	N/A	120.90
3	0.08	0.00	0.01	0.00	N/A	120.90
4	0.10	-0.10	0.01	0.00	N/A	120.90
5	0.13	0.00	0.02	0.00	N/A	120.90
6	0.18	0.00	0.03	0.00	N/A	120.90
7	0.22	0.00	0.05	0.00	N/A	120.90
8	0.27	0.00	0.08	0.00	100.00	90.68
9	0.33	2.43	0.09	0.00	81.96	94.98
10	0.36	5.87	0.09	0.00	55.30	96.98
11	0.37	7.19	0.09	0.00	43.87	97.82
12	0.38	8.30	0.10	0.00	39.79	98.46
13	0.42	9.11	0.11	0.00	36.64	99.41
14	0.44	10.73	0.12	0.00	34.37	100.58
15	0.47	11.94	0.14	0.00	31.37	101.55
16	0.47	13.87	0.14	0.00	28.15	102.58
17	0.52	16.90	0.16	0.00	24.51	103.55
18	0.56	20.24	0.17	0.00	21.06	104.60
19	0.58	24.29	0.18	0.00	17.61	105.59
20	0.61	30.26	0.19	0.10	14.26	106.54
21	0.66	37.55	0.20	0.10	11.58	107.34
22	0.76	43.02	0.21	0.10	10.25	107.74
23	0.80	41.80	0.21	0.10	11.05	107.65
24	0.81	31.17	0.21	0.10	12.33	107.41
25	0.85	33.50	0.20	0.10	13.76	107.15
26	0.86	32.59	0.20	0.10	13.66	107.29
27	0.90	32.29	0.22	0.10	14.33	107.68
28	0.95	31.78	0.24	0.10	14.92	108.07
29	1.00	31.38	0.24	0.10	14.72	106.94
30	1.05	28.44	0.12	0.10	14.03	104.83
31	1.14	26.82	0.10	0.10	5.00	101.56
32	1.24	24.39	0.08	0.10	5.00	100.45
33	1.31	21.66	0.09	0.10	5.00	100.02
34	1.36	15.49	0.10	0.10	19.77	100.07
35	1.37	16.65	0.10	0.10	20.16	100.28
36	1.39	21.17	0.10	0.10	19.32	100.40
37	1.43	17.81	0.10	0.10	18.80	100.44
38	1.44	18.12	0.10	0.10	19.86	100.33
39	1.49	18.22	0.10	0.10	19.73	100.60
40	1.53	18.72	0.11	0.10	19.64	101.22
41	1.58	19.74	0.12	0.10	19.61	102.17
42	1.63	20.55	0.14	0.10	19.60	103.26
43	1.68	21.56	0.16	0.10	19.49	104.34
44	1.72	22.98	0.18	0.10	18.93	105.39
45	1.77	25.40	0.20	0.10	17.98	106.40
46	1.82	28.04	0.22	0.19	16.68	107.38
47	1.86	31.48	0.24	0.19	15.32	108.26
48	1.92	35.02	0.26	0.19	13.84	108.95

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	1.97	38.77	0.26	0.19	12.52	109.50
50	2.01	42.21	0.27	0.19	11.75	110.13
51	2.09	43.83	0.31	0.19	11.40	110.51
52	2.16	43.62	0.30	0.19	11.59	110.65
53	2.20	41.70	0.29	0.19	12.00	110.35
54	2.25	39.07	0.28	0.19	12.39	109.98
55	2.31	38.77	0.27	0.19	12.55	109.49
56	2.37	37.96	0.25	0.19	12.51	108.98
57	2.40	36.64	0.24	0.19	12.56	108.51
58	2.46	36.03	0.23	0.19	12.53	107.92
59	2.54	35.22	0.20	0.19	12.28	107.21
60	2.59	34.82	0.18	0.19	5.00	106.07
61	2.69	34.01	0.14	0.19	5.00	105.12
62	2.74	33.91	0.14	0.19	5.00	104.27
63	2.83	33.91	0.13	0.29	5.00	104.04
64	2.88	33.81	0.13	0.29	5.00	103.96
65	2.98	35.32	0.13	0.29	5.00	104.13
66	3.03	37.96	0.13	0.29	5.00	104.69
67	3.12	42.41	0.15	0.29	5.00	105.94
68	3.21	46.56	0.19	0.29	5.00	107.29
69	3.27	51.52	0.21	0.29	5.00	108.51
70	3.34	56.88	0.23	0.29	5.00	109.32
71	3.41	62.75	0.24	0.29	5.00	110.12
72	3.51	66.09	0.27	0.29	5.00	110.66
73	3.55	63.76	0.28	0.29	5.00	111.08
74	3.65	61.03	0.29	0.38	5.00	111.24
75	3.75	62.45	0.30	0.38	5.00	111.31
76	3.83	61.64	0.29	0.38	5.00	111.22
77	3.94	60.22	0.28	0.38	5.00	111.12
78	4.04	61.44	0.28	0.38	5.00	111.07
79	4.13	59.21	0.29	0.38	7.02	111.59
80	4.24	61.23	0.34	0.38	5.00	111.65
81	4.38	64.57	0.29	0.38	5.00	110.97
82	4.50	69.64	0.19	0.38	4.69	110.20
83	4.62	72.57	0.25	0.48	3.95	110.29
84	4.71	80.16	0.28	0.48	3.93	111.40
85	4.75	80.92	0.29	0.48	3.90	112.19
86	4.84	81.68	0.33	0.48	3.97	112.65
87	4.89	83.70	0.33	0.57	4.02	112.99
88	4.94	83.40	0.33	0.57	4.04	113.02
89	4.98	81.68	0.33	0.57	4.17	112.97
90	5.07	80.06	0.33	0.57	4.33	112.85
91	5.13	78.54	0.33	0.57	4.49	112.71
92	5.17	76.82	0.32	0.57	4.57	112.40
93	5.27	75.00	0.30	0.57	4.72	112.10
94	5.32	72.47	0.30	0.57	4.84	111.72
95	5.42	70.75	0.28	0.57	4.99	111.41
96	5.46	69.33	0.27	0.57	5.00	111.08

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	5.56	67.91	0.26	0.57	5.00	110.88
98	5.61	66.80	0.26	0.57	5.00	110.75
99	5.71	65.89	0.26	0.57	5.00	110.68
100	5.78	64.88	0.26	0.57	5.00	110.63
101	5.85	63.97	0.26	0.57	5.00	110.57
102	5.95	62.65	0.26	0.57	5.00	110.53
103	6.00	61.84	0.26	0.57	5.00	110.86
104	6.09	62.45	0.30	0.67	5.00	109.42
105	6.14	64.47	0.11	0.67	4.43	108.06
106	6.24	67.31	0.14	0.67	3.33	106.15
107	6.30	70.75	0.17	0.67	3.46	107.71
108	6.38	73.18	0.20	0.67	3.76	108.87
109	6.46	70.24	0.23	0.67	4.34	109.63
110	6.50	65.28	0.24	0.67	4.73	110.08
111	6.56	69.74	0.25	0.67	4.82	110.41
112	6.63	71.46	0.26	0.67	4.59	110.75
113	6.68	72.67	0.26	0.67	4.51	110.97
114	6.76	73.38	0.27	0.76	4.44	111.12
115	6.82	74.39	0.27	0.76	4.37	111.23
116	6.88	75.81	0.27	0.76	4.21	111.32
117	6.96	78.34	0.27	0.76	3.98	111.40
118	7.03	80.97	0.27	0.76	3.77	111.49
119	7.11	82.29	0.27	0.76	3.64	111.55
120	7.16	82.89	0.27	0.76	3.60	111.70
121	7.26	83.91	0.29	0.76	3.62	111.86
122	7.31	84.62	0.29	0.76	3.65	112.04
123	7.40	84.72	0.29	0.76	3.70	112.13
124	7.45	84.51	0.30	0.76	3.76	112.18
125	7.54	84.31	0.30	0.86	3.86	112.16
126	7.60	83.00	0.30	0.86	3.98	112.07
127	7.68	81.17	0.29	0.86	4.16	111.94
128	7.74	79.45	0.29	0.86	4.33	111.82
129	7.83	78.44	0.29	0.86	4.51	111.77
130	7.90	77.73	0.29	0.86	4.60	111.85
131	7.98	78.85	0.30	0.86	4.65	112.09
132	8.05	80.67	0.31	0.86	4.62	112.42
133	8.12	82.29	0.32	0.86	4.65	112.70
134	8.19	82.08	0.33	0.86	4.77	112.88
135	8.27	80.57	0.34	0.86	5.03	113.00
136	8.36	78.74	0.34	0.86	5.00	112.80
137	8.41	78.04	0.31	0.86	4.51	111.23
138	8.50	78.24	0.15	0.86	3.85	109.61
139	8.60	78.95	0.18	0.86	3.40	108.40
140	8.70	79.15	0.21	0.86	3.76	109.30
141	8.74	78.14	0.22	0.86	4.96	109.52
142	8.78	55.57	0.22	0.86	5.00	109.55
143	8.81	62.96	0.23	0.96	5.00	109.69
144	8.86	72.17	0.24	0.96	5.00	110.13

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	8.91	74.09	0.25	0.96	5.00	110.49
146	8.94	75.00	0.25	0.96	5.00	110.79
147	9.02	73.89	0.27	0.96	5.00	111.08
148	9.10	72.47	0.28	0.96	5.00	111.34
149	9.17	71.15	0.28	0.96	5.00	111.44
150	9.22	69.84	0.28	0.96	5.00	111.44
151	9.31	68.83	0.28	0.96	5.00	111.41
152	9.37	68.32	0.28	0.96	5.00	111.39
153	9.42	68.32	0.28	0.96	5.00	111.39
154	9.52	69.13	0.28	0.96	5.00	111.41
155	9.60	70.04	0.28	0.96	5.00	111.49
156	9.66	71.36	0.29	0.96	5.00	111.61
157	9.74	73.18	0.29	0.96	5.00	111.74
158	9.81	74.80	0.29	0.96	5.00	111.88
159	9.89	75.71	0.30	0.96	5.00	112.10
160	9.98	76.82	0.32	0.96	5.00	112.42
161	10.03	78.54	0.33	1.05	5.00	112.78
162	10.13	80.97	0.34	1.05	5.00	113.14
163	10.23	84.21	0.35	1.05	5.00	113.45
164	10.32	86.94	0.36	1.05	5.00	113.68
165	10.38	88.16	0.36	1.05	5.00	113.80
166	10.47	89.17	0.37	1.05	5.00	113.83
167	10.57	88.66	0.36	1.05	5.00	113.81
168	10.66	87.45	0.36	1.05	4.50	112.22
169	10.76	87.65	0.16	1.05	3.90	110.65
170	10.85	87.85	0.19	1.05	3.30	108.99
171	10.92	88.46	0.22	1.05	3.57	109.92
172	11.00	89.27	0.23	1.05	4.11	110.26
173	11.07	77.73	0.23	1.05	4.54	110.35
174	11.10	79.45	0.23	1.05	4.87	110.48
175	11.15	83.40	0.25	1.05	4.71	110.88
176	11.19	85.53	0.26	1.05	4.61	111.40
177	11.24	87.25	0.28	1.05	4.59	111.90
178	11.29	89.47	0.30	1.05	4.51	112.30
179	11.34	92.21	0.31	1.05	4.40	112.73
180	11.40	95.14	0.33	1.05	4.33	113.17
181	11.47	97.27	0.35	1.05	4.32	113.59
182	11.53	97.98	0.36	1.05	4.38	113.88
183	11.58	97.87	0.36	1.05	4.42	114.06
184	11.65	98.78	0.37	1.05	4.46	114.22
185	11.72	99.39	0.38	1.05	4.50	114.36
186	11.77	99.29	0.38	1.05	4.57	114.43
187	11.82	98.28	0.38	1.05	4.67	114.45
188	11.88	97.47	0.38	1.15	5.03	114.87
189	11.97	95.95	0.45	1.05	5.00	114.84
190	12.02	94.84	0.38	1.05	5.00	114.75
191	12.06	93.42	0.38	1.05	5.00	114.18
192	12.11	92.31	0.37	1.05	5.00	114.03

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	12.21	93.32	0.36	1.05	5.00	113.85
194	12.25	92.21	0.35	1.05	5.00	113.70
195	12.30	93.22	0.35	1.05	5.01	113.58
196	12.31	93.52	0.35	1.05	4.95	113.56
197	12.32	93.52	0.35	1.05	4.93	113.57
198	12.35	93.83	0.35	1.05	4.77	113.38
199	12.40	95.24	0.32	1.05	4.60	113.25
200	12.45	96.66	0.32	1.15	4.38	113.11
201	12.52	98.38	0.32	1.05	4.29	113.28
202	12.56	100.20	0.33	1.05	4.25	113.61
203	12.62	102.33	0.36	1.05	4.25	113.99
204	12.65	103.54	0.37	1.05	3.77	113.26
205	12.71	105.16	0.23	1.15	3.23	112.19
206	12.76	106.68	0.23	1.15	2.62	110.90
207	12.83	110.12	0.23	1.15	2.60	111.55
208	12.88	114.17	0.28	1.15	2.77	112.94
209	12.93	118.52	0.37	1.15	2.90	114.26
210	12.98	124.09	0.40	1.15	3.08	115.17
211	13.03	121.66	0.41	1.15	3.06	115.51
212	13.04	125.50	0.42	1.15	3.47	115.78
213	13.07	113.26	0.46	1.05	3.50	116.29
214	13.13	129.35	0.50	1.05	3.58	116.95
215	13.17	134.31	0.54	1.05	3.26	117.70
216	13.22	139.37	0.58	1.05	3.29	118.28
217	13.27	139.88	0.62	1.05	3.36	118.74
218	13.32	141.09	0.64	1.05	3.46	119.07
219	13.37	142.31	0.66	1.05	3.56	119.26
220	13.41	140.38	0.67	1.05	3.64	119.30
221	13.46	139.27	0.66	1.05	3.75	119.26
222	13.51	137.45	0.66	1.15	3.85	119.23
223	13.56	136.13	0.66	1.15	4.04	119.31
224	13.60	134.31	0.69	1.05	4.26	119.44
225	13.66	132.39	0.70	1.05	4.38	119.40
226	13.75	131.68	0.66	1.05	4.42	119.28
227	13.80	131.27	0.66	1.05	4.39	119.11
228	13.89	130.57	0.66	1.05	4.46	119.13
229	13.94	130.36	0.67	1.05	4.60	119.22
230	13.99	128.44	0.69	1.15	4.88	119.41
231	14.09	125.71	0.72	1.15	5.27	119.59
232	14.14	121.96	0.73	1.15	5.70	119.79
233	14.23	119.13	0.76	1.15	6.08	119.87
234	14.28	117.00	0.76	1.15	5.80	119.04
235	14.38	115.38	0.51	1.15	5.31	118.06
236	14.42	116.85	0.51	1.15	4.82	116.96
237	14.52	113.76	0.52	1.15	4.88	117.10
238	14.57	116.70	0.53	1.15	4.95	117.39
239	14.67	119.74	0.57	1.15	5.03	117.62
240	14.68	116.09	0.57	1.15	5.00	117.81

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	14.70	117.61	0.58	1.15	5.00	117.84
242	14.75	115.48	0.58	1.15	5.31	117.93
243	14.80	116.60	0.59	1.15	5.43	118.05
244	14.89	116.40	0.61	1.05	5.52	118.17
245	14.94	115.59	0.61	1.05	5.70	118.20
246	15.04	112.25	0.60	1.05	5.96	118.05
247	15.13	107.59	0.59	1.05	6.34	117.77
248	15.21	101.82	0.57	1.05	6.81	117.40
249	15.28	95.75	0.55	1.05	7.34	116.95
250	15.38	89.98	0.52	1.05	7.88	116.40
251	15.47	84.21	0.48	1.05	8.48	115.75
252	15.57	77.33	0.45	1.05	9.19	115.05
253	15.67	71.05	0.42	1.05	10.08	114.27
254	15.77	63.87	0.38	0.96	11.15	113.43
255	15.86	56.78	0.35	0.96	12.43	112.60
256	15.96	51.11	0.33	0.96	13.84	112.03
257	16.05	47.27	0.34	0.96	15.41	111.80
258	16.15	43.52	0.35	0.96	17.50	112.16
259	16.25	39.98	0.42	0.96	19.14	112.43
260	16.31	39.78	0.40	0.96	20.17	112.68
261	16.39	39.78	0.40	0.96	20.08	112.48
262	16.48	39.57	0.38	0.96	19.41	112.23
263	16.59	42.10	0.35	0.96	17.84	112.02
264	16.68	47.47	0.35	0.96	15.50	111.89
265	16.76	54.25	0.33	0.96	13.16	111.73
266	16.86	59.92	0.29	0.96	11.62	111.63
267	16.92	61.94	0.31	0.96	10.95	111.65
268	17.02	61.84	0.32	0.96	10.86	111.63
269	17.11	61.13	0.29	0.96	11.26	111.95
270	17.22	60.42	0.35	0.96	11.88	112.47
271	17.35	59.61	0.39	0.96	14.04	114.30
272	17.45	55.47	0.60	0.96	18.38	116.52
273	17.55	44.33	0.88	0.96	25.48	117.93
274	17.61	30.36	0.95	0.96	33.75	118.25
275	17.64	27.02	0.93	0.76	40.43	117.69
276	17.70	24.80	0.87	0.76	43.23	117.15
277	17.75	22.67	0.84	0.76	45.31	116.73
278	17.80	21.86	0.84	0.76	46.98	116.55
279	17.85	21.56	0.84	0.86	48.89	116.96
280	17.94	21.26	1.00	0.86	45.90	117.91
281	17.99	30.26	1.09	0.86	40.69	119.19
282	18.09	37.65	1.19	0.86	35.41	120.26
283	18.15	41.30	1.27	0.76	34.54	120.72
284	18.23	36.03	1.26	0.76	36.66	120.67
285	18.33	30.87	1.23	0.76	46.11	119.75
286	18.43	14.17	1.16	0.76	59.31	117.89
287	18.52	10.22	0.82	0.76	78.74	114.99
288	18.59	9.41	0.56	0.76	81.21	111.71

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	18.72	8.10	0.35	0.76	78.82	108.87
290	18.81	7.79	0.30	0.76	77.80	106.89
291	18.87	7.69	0.30	0.76	78.37	106.65
292	18.95	7.69	0.32	0.86	79.72	107.66
293	19.05	8.40	0.43	0.86	76.48	109.13
294	19.14	10.73	0.48	0.86	66.73	110.57
295	19.22	14.78	0.48	0.86	53.52	111.65
296	19.29	20.75	0.49	0.86	39.10	113.06
297	19.38	34.31	0.56	0.86	26.85	114.86
298	19.44	55.26	0.63	0.86	19.18	117.03
299	19.53	74.70	0.80	0.86	14.77	118.92
300	19.62	90.89	0.91	0.86	12.57	120.49
301	19.69	102.43	1.00	0.76	11.54	121.67
302	19.79	108.50	1.15	0.76	11.36	122.57
303	19.86	109.41	1.24	0.76	11.84	123.28
304	19.97	106.58	1.33	0.76	12.61	123.60
305	20.07	101.72	1.35	0.76	13.52	123.57
306	20.16	94.94	1.29	0.76	14.68	123.29
307	20.26	85.73	1.27	0.76	14.95	121.49
308	20.34	72.77	0.61	0.67	15.95	119.48
309	20.43	59.51	0.65	0.67	17.67	117.13
310	20.50	47.17	0.70	0.67	23.52	117.36
311	20.60	37.15	0.83	0.67	30.86	117.42
312	20.62	28.74	0.85	0.67	38.22	117.36
313	20.63	25.51	0.86	0.57	41.38	117.35
314	20.68	29.96	0.89	0.57	42.41	117.60
315	20.73	27.73	0.95	0.57	43.48	118.01
316	20.82	25.20	1.01	0.57	47.06	118.03
317	20.87	23.48	0.98	0.57	50.17	117.77
318	20.91	21.66	0.93	0.57	52.49	117.09
319	20.96	19.53	0.83	0.67	55.24	116.20
320	21.05	17.51	0.75	0.67	58.65	115.41
321	21.11	15.69	0.75	0.67	59.61	115.06
322	21.17	17.71	0.75	0.67	59.41	115.10
323	21.25	17.91	0.76	0.67	50.49	115.80
324	21.30	28.04	0.80	0.67	37.44	117.17
325	21.37	47.77	0.89	0.67	25.95	118.97
326	21.45	69.84	1.01	0.76	19.10	120.73
327	21.49	88.87	1.16	0.76	15.54	122.37
328	21.58	104.65	1.36	0.76	13.61	123.67
329	21.64	116.80	1.47	0.76	12.50	124.67
330	21.69	125.61	1.57	0.76	11.91	125.41
331	21.78	131.07	1.71	0.76	11.69	126.01
332	21.83	134.51	1.80	0.76	11.79	126.54
333	21.89	135.73	1.90	0.76	12.04	126.96
334	21.98	136.03	2.02	0.76	12.40	127.34
335	22.03	136.23	2.09	0.76	12.75	127.63
336	22.12	135.42	2.15	0.76	13.09	127.77

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	22.22	132.99	2.16	0.76	13.41	127.81
338	22.26	131.17	2.15	0.76	13.69	127.73
339	22.36	128.44	2.12	0.76	13.97	127.61
340	22.41	125.51	2.10	0.76	14.35	127.56
341	22.51	123.38	2.14	0.76	14.15	127.06
342	22.60	121.66	1.74	0.76	13.83	126.45
343	22.70	118.93	1.65	0.76	13.30	125.68
344	22.75	117.41	1.61	0.76	13.43	125.41
345	22.84	114.27	1.59	0.76	14.48	125.10
346	22.89	96.25	1.56	0.76	14.75	124.96
347	22.90	110.88	1.55	0.76	15.01	124.78
348	22.94	107.49	1.51	0.76	13.97	124.76
349	23.00	111.94	1.47	0.76	13.47	124.67
350	23.08	117.61	1.47	0.86	12.40	124.71
351	23.13	127.23	1.45	0.86	11.31	124.84
352	23.20	136.23	1.45	0.86	10.47	124.96
353	23.27	138.66	1.46	0.86	10.12	124.97
354	23.33	136.23	1.43	0.76	10.11	124.75
355	23.42	131.78	1.34	0.86	10.24	124.32
356	23.48	126.62	1.25	0.76	10.39	123.80
357	23.57	122.37	1.20	0.86	10.62	123.46
358	23.61	120.44	1.20	0.86	10.81	123.34
359	23.66	120.75	1.21	0.86	10.87	123.44
360	23.73	123.28	1.25	0.86	10.80	123.73
361	23.80	128.04	1.32	0.86	10.61	124.10
362	23.85	132.49	1.37	0.86	10.45	124.49
363	23.94	135.32	1.42	0.86	10.34	124.75
364	24.00	136.54	1.44	0.86	10.35	124.89
365	24.09	135.73	1.44	0.86	10.44	124.90
366	24.16	133.80	1.43	0.86	10.68	124.85
367	24.24	130.46	1.43	0.86	10.08	123.73
368	24.33	125.81	0.86	0.86	9.54	122.48
369	24.43	121.05	0.88	0.86	8.99	121.06
370	24.52	116.40	0.91	0.86	9.98	121.07
371	24.58	105.36	0.92	0.86	10.82	121.05
372	24.59	104.91	0.92	0.86	11.52	121.00
373	24.63	103.24	0.93	0.76	11.65	121.07
374	24.68	104.45	0.95	0.76	11.99	121.27
375	24.77	102.63	1.00	0.76	12.42	121.51
376	24.82	100.30	1.03	0.76	13.12	121.77
377	24.92	97.98	1.08	0.76	13.83	121.94
378	25.01	95.24	1.10	0.76	14.55	122.06
379	25.06	92.41	1.11	0.76	15.23	122.08
380	25.16	89.47	1.12	0.76	15.90	122.02
381	25.25	86.54	1.11	0.76	16.59	121.94
382	25.30	83.50	1.11	0.76	17.28	121.83
383	25.41	80.57	1.11	0.76	18.09	121.73
384	25.49	77.23	1.11	0.76	18.98	121.65

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	25.55	73.99	1.11	0.76	20.07	121.62
386	25.64	70.65	1.15	0.76	21.32	121.62
387	25.70	67.11	1.16	0.76	22.79	121.64
388	25.79	63.26	1.19	0.76	24.37	121.58
389	25.89	59.31	1.18	0.76	26.26	121.42
390	25.94	54.15	1.17	0.76	28.33	121.11
391	26.02	49.29	1.13	0.76	30.48	120.54
392	26.12	44.64	1.03	0.76	32.30	119.79
393	26.17	41.19	0.94	0.67	34.00	118.80
394	26.28	36.64	0.83	0.67	35.82	117.81
395	26.36	33.20	0.76	0.67	37.65	116.64
396	26.45	30.06	0.64	0.67	40.39	115.51
397	26.50	25.00	0.59	0.67	44.96	114.33
398	26.61	19.74	0.56	0.67	52.70	113.36
399	26.70	15.69	0.53	0.67	63.56	112.54
400	26.77	12.45	0.54	0.67	73.76	111.85
401	26.85	10.73	0.52	0.67	77.64	111.21
402	26.94	12.35	0.44	0.67	78.19	110.57
403	27.04	11.23	0.43	0.67	74.40	110.13
404	27.14	12.25	0.42	0.67	72.81	110.00
405	27.23	13.16	0.41	0.76	69.26	109.81
406	27.28	13.26	0.38	0.76	67.37	109.59
407	27.29	13.21	0.37	0.76	64.60	108.54
408	27.38	13.36	0.25	0.76	63.04	107.81
409	27.48	13.26	0.28	0.76	62.75	107.60
410	27.57	13.16	0.35	0.76	65.67	108.83
411	27.64	13.36	0.41	0.76	68.02	109.83
412	27.65	13.36	0.43	0.67	70.74	111.13
413	27.74	13.56	0.57	0.67	69.81	112.46
414	27.80	16.60	0.65	0.67	65.76	114.19
415	27.90	20.55	0.77	0.67	61.65	115.18
416	27.99	20.34	0.77	0.67	61.92	115.44
417	28.07	17.11	0.72	0.67	66.57	114.64
418	28.16	13.87	0.62	0.67	72.64	113.23
419	28.25	12.35	0.50	0.67	76.77	111.52
420	28.34	11.34	0.41	0.67	77.68	109.88
421	28.44	10.83	0.35	0.67	77.85	108.83
422	28.53	10.83	0.35	0.67	78.14	108.53
423	28.62	10.83	0.37	0.67	77.38	110.10
424	28.76	13.56	0.57	0.67	72.35	112.51
425	28.86	18.22	0.74	0.76	67.30	115.27
426	28.96	21.15	0.97	0.76	65.09	117.31
427	29.08	21.56	1.17	0.76	67.25	119.00
428	29.19	21.15	1.43	0.76	69.03	120.29
429	29.29	23.48	1.60	0.76	57.91	120.47
430	29.39	37.85	0.97	0.76	42.67	122.13
431	29.50	60.73	1.83	0.76	33.13	124.03
432	29.63	74.39	2.28	0.76	32.04	126.13

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	29.65	65.49	2.34	0.76	31.66	126.80
434	29.66	70.75	2.34	0.76	31.48	126.90
435	29.72	76.72	2.35	0.76	30.48	126.99
436	29.80	73.08	2.34	0.76	28.82	127.09
437	29.85	83.60	2.30	0.96	24.74	127.25
438	29.94	111.74	2.18	1.05	19.12	127.53
439	30.00	139.37	2.11	0.96	14.70	127.66
440	30.05	155.36	1.99	0.96	11.90	127.40
441	30.14	164.17	1.72	0.86	10.16	126.80
442	30.19	168.22	1.55	0.86	9.10	126.23
443	30.24	170.24	1.55	0.86	8.70	126.01
444	30.29	170.34	1.56	0.86	8.77	126.09
445	30.38	168.42	1.60	0.96	9.02	126.13
446	30.43	164.37	1.60	0.96	9.33	126.13
447	30.48	161.54	1.59	0.96	9.59	126.05
448	30.54	158.91	1.58	0.96	9.78	125.95
449	30.62	156.98	1.55	0.96	9.79	125.86
450	30.67	159.11	1.54	0.96	9.79	125.78
451	30.72	157.18	1.54	0.96	9.69	125.76
452	30.76	159.31	1.53	0.96	9.55	125.70
453	30.86	161.84	1.49	0.96	9.23	125.64
454	30.91	164.98	1.48	0.96	8.91	125.62
455	30.95	168.42	1.49	0.96	8.55	125.64
456	31.03	173.38	1.47	0.96	8.12	125.67
457	31.10	179.65	1.45	1.05	7.69	125.73
458	31.15	185.02	1.48	1.05	7.34	125.89
459	31.20	190.38	1.52	1.05	7.18	126.13
460	31.26	193.52	1.57	1.05	7.15	126.36
461	31.34	193.62	1.60	1.05	7.71	126.40
462	31.37	171.46	1.60	1.05	7.87	126.43
463	31.38	188.76	1.60	1.15	8.09	126.36
464	31.43	183.91	1.58	1.15	7.77	126.31
465	31.47	181.17	1.53	1.15	8.03	126.07
466	31.55	172.87	1.49	1.15	8.51	125.78
467	31.59	160.83	1.47	1.15	9.39	125.48
468	31.66	147.27	1.45	1.15	10.59	125.21
469	31.73	135.12	1.45	1.05	12.03	125.03
470	31.78	124.80	1.48	1.05	13.62	124.95
471	31.84	115.28	1.53	1.05	15.49	125.08
472	31.93	106.78	1.65	1.05	17.52	125.26
473	31.98	99.59	1.73	1.15	19.53	125.52
474	32.02	94.84	1.82	1.15	20.69	125.90
475	32.09	100.05	1.96	1.15	21.58	126.26
476	32.16	96.05	2.03	1.15	21.57	126.59
477	32.22	100.51	2.04	1.15	21.42	126.73
478	32.27	104.25	2.05	1.15	20.75	126.84
479	32.34	105.67	2.06	1.24	20.20	126.90
480	32.42	108.10	2.04	1.24	19.56	126.93

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	32.46	112.85	2.02	1.24	18.55	126.88
482	32.54	118.12	1.95	1.24	17.41	126.77
483	32.60	122.16	1.87	1.24	16.07	126.34
484	32.67	124.90	1.62	1.24	15.05	125.97
485	32.75	127.33	1.63	1.24	14.32	125.74
486	32.81	130.26	1.68	1.24	14.20	126.03
487	32.89	133.50	1.79	1.24	14.12	126.37
488	32.94	136.34	1.83	1.24	14.96	126.52
489	32.95	118.52	1.84	1.24	14.91	126.69
490	33.00	138.16	1.90	1.24	14.89	126.92
491	33.06	141.90	1.98	1.24	14.05	127.30
492	33.11	143.12	2.03	1.24	14.18	127.55
493	33.20	141.70	2.09	1.24	14.56	127.71
494	33.25	138.76	2.13	1.24	15.10	127.86
495	33.34	136.54	2.19	1.24	15.55	127.94
496	33.38	135.73	2.19	1.24	15.74	128.03
497	33.48	137.75	2.22	1.24	15.68	128.19
498	33.58	141.70	2.30	1.24	15.42	128.42
499	33.63	146.25	2.34	1.24	15.06	128.72
500	33.73	152.23	2.43	1.24	14.62	129.02
501	33.82	158.70	2.51	1.24	14.13	129.36
502	33.87	165.89	2.57	1.24	13.67	129.70
503	33.96	172.57	2.69	1.24	13.23	130.04
504	34.02	179.65	2.77	1.24	12.84	130.48
505	34.11	189.47	2.95	1.24	12.43	131.00
506	34.18	200.91	3.15	1.24	12.08	131.61
507	34.26	211.03	3.36	1.24	11.89	132.25
508	34.35	219.33	3.65	1.24	11.82	132.88
509	34.44	227.93	3.92	1.34	11.72	133.37
510	34.49	235.22	3.98	1.34	11.56	133.69
511	34.59	238.66	4.05	1.34	11.45	133.86
512	34.69	239.88	4.13	1.34	11.44	133.98
513	34.76	241.39	4.15	1.34	11.40	134.01
514	34.83	241.50	4.07	1.43	11.43	134.00
515	34.93	238.86	4.12	1.43	11.44	133.81
516	35.02	233.50	3.89	1.43	11.54	133.60
517	35.12	229.05	3.79	1.43	11.46	133.22
518	35.22	226.72	3.60	1.43	11.42	132.94
519	35.30	223.58	3.51	1.43	11.44	132.63
520	35.38	216.29	3.41	1.43	12.34	132.31
521	35.43	185.73	3.36	1.43	13.07	132.03
522	35.46	192.21	3.30	1.53	13.71	131.78
523	35.51	190.18	3.21	1.62	13.68	131.56
524	35.56	179.15	3.11	1.62	14.30	131.05
525	35.66	160.93	2.83	1.53	15.30	130.47
526	35.70	150.40	2.73	1.53	16.62	129.73
527	35.80	133.20	2.53	1.53	18.63	129.08
528	35.89	111.94	2.45	1.53	21.97	128.26

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	35.96	88.76	2.31	1.53	26.84	127.15
530	36.04	66.50	1.99	1.43	32.56	125.33
531	36.14	49.39	1.45	1.43	38.50	123.16
532	36.19	40.49	1.23	1.43	42.06	121.28
533	36.28	40.49	1.16	1.43	44.05	120.76
534	36.33	40.49	1.27	1.43	43.63	120.56
535	36.42	40.49	1.14	1.43	42.36	120.82
536	36.48	45.85	1.23	1.43	39.85	121.28
537	36.52	51.52	1.40	1.43	38.41	122.62
538	36.62	55.67	1.74	1.43	38.39	123.71
539	36.68	55.06	1.84	1.43	39.88	124.37
540	36.77	51.42	1.88	1.43	40.89	124.37
541	36.86	51.92	1.78	1.43	39.71	124.46
542	36.90	60.53	1.84	1.53	32.23	124.83
543	37.00	90.49	1.76	1.53	21.98	125.79
544	37.10	143.32	1.82	1.62	14.18	126.63
545	37.20	187.14	1.82	1.53	9.48	127.07
546	37.29	217.10	1.62	1.53	7.15	127.31
547	37.39	234.82	1.72	1.53	6.16	127.69
548	37.49	245.04	1.93	1.53	6.15	128.39
549	37.53	245.80	2.08	1.53	6.43	129.01
550	37.58	245.80	2.19	1.43	6.79	129.47
551	37.62	246.56	2.33	1.43	7.05	129.90
552	37.69	251.11	2.46	1.43	7.41	130.49
553	37.77	253.95	2.76	1.43	7.74	131.04
554	37.82	255.46	2.89	1.34	8.12	131.53
555	37.87	255.46	3.00	1.34	8.40	131.80
556	37.91	253.54	3.09	1.34	8.73	131.98
557	37.97	249.09	3.14	1.34	9.14	132.07
558	38.06	242.00	3.17	1.43	9.58	132.05
559	38.10	234.61	3.14	1.34	9.96	131.95
560	38.17	230.06	3.08	1.34	10.09	131.72
561	38.25	227.93	2.95	1.34	9.95	131.37
562	38.35	226.21	2.75	1.34	9.74	130.98
563	38.40	223.18	2.65	1.34	9.59	130.66
564	38.46	220.85	2.61	1.34	9.55	130.46
565	38.54	220.85	2.57	1.34	9.50	130.34
566	38.60	220.85	2.53	1.34	9.36	130.20
567	38.69	220.85	2.46	1.34	9.14	130.07
568	38.74	224.90	2.42	1.34	8.84	129.97
569	38.83	228.95	2.40	1.34	8.66	130.01
570	38.88	229.65	2.47	1.34	8.43	129.87
571	38.97	228.95	2.27	1.43	8.33	129.71
572	39.02	227.63	2.26	1.43	8.17	129.42
573	39.11	225.10	2.21	1.43	8.23	129.25
574	39.16	220.54	2.14	1.43	8.40	128.95
575	39.23	209.82	2.04	1.43	9.12	128.58
576	39.24	186.03	2.02	1.43	9.26	128.31

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	39.28	206.53	1.96	1.43	9.26	128.10
578	39.32	203.24	1.90	1.43	8.75	127.86
579	39.39	195.95	1.80	1.43	9.08	127.52
580	39.47	184.41	1.77	1.43	9.80	127.22
581	39.54	171.46	1.78	1.43	10.93	127.03
582	39.62	158.50	1.78	1.43	12.28	126.82
583	39.71	145.24	1.76	1.43	13.78	126.57
584	39.76	133.40	1.75	1.43	15.25	126.29
585	39.85	124.80	1.72	1.43	16.63	126.05
586	39.90	117.71	1.71	1.43	17.85	125.82
587	40.00	111.03	1.69	1.34	19.15	125.63
588	40.06	104.35	1.69	1.34	20.49	125.46
589	40.15	98.68	1.69	1.34	21.96	125.31
590	40.21	92.91	1.69	1.34	23.70	125.27
591	40.29	86.84	1.76	1.34	25.91	125.29
592	40.35	79.96	1.83	1.34	28.93	125.45
593	40.43	72.17	1.95	1.34	31.85	125.15
594	40.52	64.47	1.72	1.34	35.38	124.58
595	40.58	54.86	1.64	1.34	39.26	123.64
596	40.67	46.25	1.54	1.34	44.53	122.80
597	40.77	39.47	1.43	1.34	48.71	122.20
598	40.84	39.12	1.45	1.34	51.09	121.91
599	40.89	38.77	1.46	1.24	47.89	122.14
600	40.94	48.89	1.45	1.24	41.53	122.58
601	41.03	61.54	1.47	1.24	34.10	123.11
602	41.08	73.89	1.47	1.24	28.70	123.52
603	41.14	83.60	1.45	1.15	25.34	123.76
604	41.22	88.56	1.45	1.15	23.58	123.93
605	41.28	90.89	1.47	1.15	23.00	124.13
606	41.33	91.80	1.53	1.05	23.16	124.56
607	41.42	93.22	1.69	1.05	23.59	125.16
608	41.47	95.85	1.84	1.05	23.66	125.86
609	41.52	101.92	1.97	1.05	22.91	126.69
610	41.62	114.27	2.20	1.05	21.31	127.57
611	41.67	130.16	2.38	1.05	19.54	128.55
612	41.76	145.55	2.62	1.05	17.95	129.34
613	41.82	157.59	2.74	1.05	16.90	130.00
614	41.90	165.99	2.90	1.05	16.15	130.44
615	41.99	172.67	2.96	1.05	15.70	130.73
616	42.05	176.01	2.98	1.05	15.44	130.86
617	42.15	175.71	3.00	0.96	15.47	130.91
618	42.23	173.89	3.02	0.96	15.76	130.92
619	42.30	170.34	3.03	0.96	16.20	130.85
620	42.38	164.37	2.97	0.96	16.79	130.64
621	42.48	156.17	2.87	0.96	17.75	130.21
622	42.57	140.79	2.70	0.96	19.03	129.66
623	42.64	128.95	2.56	0.86	20.48	129.02
624	42.72	120.14	2.42	0.86	21.44	128.37

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	42.82	114.47	2.21	0.86	22.03	127.72
626	42.90	109.51	2.08	0.86	22.42	127.19
627	42.97	106.07	2.04	0.86	23.04	126.89
628	43.06	102.53	2.03	0.86	23.94	126.76
629	43.15	98.28	2.05	0.86	24.28	126.30
630	43.20	95.44	1.73	0.86	23.92	125.87
631	43.30	99.49	1.72	0.86	21.66	125.62
632	43.40	117.61	1.75	0.86	18.56	126.10
633	43.48	142.51	1.83	0.96	16.70	126.59
634	43.51	137.14	1.89	0.96	15.94	126.91
635	43.52	137.65	1.91	0.86	15.16	127.23
636	43.56	163.87	1.98	0.86	13.67	127.68
637	43.61	178.84	2.08	0.86	11.96	128.22
638	43.67	193.82	2.13	0.86	10.83	128.59
639	43.72	206.98	2.13	0.86	9.87	128.82
640	43.80	217.20	2.15	0.86	9.14	128.98
641	43.85	225.30	2.16	0.86	8.63	129.13
642	43.90	231.68	2.18	0.86	8.26	129.25
643	43.94	236.74	2.19	0.86	7.97	129.33
644	43.99	240.69	2.18	0.86	7.76	129.35
645	44.08	242.00	2.18	0.86	7.68	129.38
646	44.14	241.90	2.20	0.86	7.83	129.54
647	44.22	240.59	2.33	0.86	8.11	129.75
648	44.28	238.66	2.39	0.86	8.47	129.97
649	44.33	235.63	2.43	0.86	8.80	130.11
650	44.40	232.69	2.50	0.86	9.29	130.33
651	44.48	228.44	2.64	0.86	9.67	130.62
652	44.52	232.74	2.75	0.86	10.35	131.05
653	44.61	224.49	3.00	0.96	10.26	131.06
654	44.72	232.79	2.65	0.96	10.27	131.18
655	44.77	237.24	2.86	0.96	9.91	131.18
656	44.91	238.36	2.94	1.05	10.09	131.47
657	44.95	237.95	2.96	1.05	10.63	131.50
658	45.02	218.72	2.98	1.05	10.98	131.47
659	45.04	225.50	2.97	1.15	13.35	131.14
660	45.06	152.63	2.96	1.15	12.86	131.13
661	45.11	232.29	2.89	1.15	12.30	131.08
662	45.15	240.38	2.84	1.15	9.78	131.30
663	45.21	247.16	2.81	1.15	9.27	131.31
664	45.25	253.14	2.82	1.15	8.95	131.37
665	45.30	256.98	2.86	1.15	8.80	131.48
666	45.35	258.70	2.90	1.15	8.79	131.59
667	45.41	258.40	2.92	1.15	8.84	131.65
668	45.49	258.10	2.93	1.15	8.94	131.65
669	45.55	254.45	2.91	1.15	9.06	131.57
670	45.63	249.80	2.86	1.15	9.25	131.42
671	45.69	244.23	2.81	1.15	9.48	131.22
672	45.78	236.94	2.74	1.15	9.80	131.01

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	45.84	228.64	2.69	1.15	10.17	130.69
674	45.93	218.52	2.57	1.15	10.59	130.25
675	46.02	205.87	2.39	1.15	11.15	129.68
676	46.08	190.89	2.26	1.15	11.83	128.94
677	46.16	174.39	2.03	1.15	12.80	128.17
678	46.24	157.89	1.90	1.15	14.14	127.35
679	46.31	139.07	1.81	1.15	16.32	126.66
680	46.41	117.21	1.75	1.05	19.70	126.05
681	46.48	95.75	1.74	1.05	24.72	125.44
682	46.56	74.29	1.72	1.05	31.32	124.66
683	46.65	57.08	1.60	1.05	39.23	123.40
684	46.75	42.81	1.33	1.05	46.43	121.67
685	46.84	36.34	1.06	1.05	55.36	119.83
686	46.94	30.67	0.95	1.05	60.33	118.19
687	47.02	25.20	0.82	1.15	66.74	116.92
688	47.08	21.46	0.75	1.15	74.89	115.79
689	47.12	17.41	0.72	1.15	81.21	115.04
690	47.16	17.36	0.69	1.05	83.23	114.56
691	47.21	18.72	0.65	1.05	82.03	114.08
692	47.27	17.31	0.59	1.05	81.52	113.39
693	47.35	16.30	0.53	1.05	83.53	112.58
694	47.40	15.59	0.49	1.05	83.45	111.48
695	47.50	15.28	0.39	1.05	82.43	110.45
696	47.55	15.18	0.36	1.05	80.62	109.38
697	47.61	14.98	0.33	1.05	80.14	108.87
698	47.69	14.78	0.32	1.05	80.47	108.49
699	47.76	14.37	0.31	1.05	81.28	108.16
700	47.83	13.97	0.29	1.05	81.76	107.60
701	47.93	13.66	0.26	1.05	81.12	106.97
702	48.02	13.87	0.24	1.05	80.49	106.61
703	48.09	13.87	0.26	1.05	79.44	106.28
704	48.18	13.87	0.22	0.96	80.27	106.53
705	48.27	13.76	0.27	0.96	81.39	107.03
706	48.37	13.97	0.31	0.96	83.22	107.94
707	48.46	14.17	0.33	0.96	84.23	108.58
708	48.52	14.17	0.35	0.96	85.01	108.99
709	48.60	14.17	0.36	0.96	85.57	109.30
710	48.70	14.37	0.37	0.96	85.68	109.56
711	48.79	14.57	0.38	0.96	85.16	109.83
712	48.85	14.98	0.40	0.96	84.80	110.40
713	48.94	15.59	0.45	0.86	84.36	111.35
714	49.04	16.60	0.53	0.86	82.26	112.03
715	49.13	17.81	0.50	0.86	82.44	114.35
716	49.23	20.45	0.95	0.86	79.90	116.80
717	49.33	25.10	1.19	0.86	78.26	119.08
718	49.38	26.52	1.32	0.86	79.49	120.23
719	49.42	22.98	1.49	0.86	79.52	121.11
720	49.48	28.24	1.64	0.76	79.69	121.78

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	49.53	28.85	1.70	0.76	76.78	122.38
722	49.58	29.25	1.78	0.76	76.54	122.73
723	49.63	30.16	1.86	0.76	76.14	123.06
724	49.72	30.87	1.90	0.76	75.17	123.25
725	49.77	31.68	1.88	0.76	74.33	123.29
726	49.83	31.68	1.86	0.76	74.18	123.23
727	49.92	30.87	1.85	0.76	75.14	123.07
728	49.97	29.55	1.80	0.76	75.30	122.90
729	50.04	30.72	1.75	0.76	76.58	122.68
730	50.11	28.14	1.74	0.76	75.95	122.69
731	50.20	30.57	1.79	0.76	74.75	122.53
732	50.27	31.88	1.62	0.76	72.22	122.03
733	50.34	29.86	1.37	0.76	71.16	120.74
734	50.45	26.72	1.07	0.76	72.38	119.07
735	50.54	23.68	0.89	0.76	75.35	117.45
736	50.59	20.75	0.82	0.76	79.17	116.17
737	50.68	18.93	0.71	0.76	82.34	115.07
738	50.79	18.02	0.62	0.76	83.79	114.12
739	50.88	17.41	0.60	0.76	83.70	113.63
740	50.98	17.97	0.60	0.86	84.20	113.54
741	51.07	17.51	0.60	0.86	82.59	113.17
742	51.17	17.91	0.50	0.86	77.88	112.22
743	51.24	19.84	0.38	0.86	73.04	111.69
744	51.33	20.75	0.47	0.86	72.41	112.26
745	51.46	19.94	0.60	0.86	75.43	113.32
746	51.46	19.53	0.60	0.86	78.27	114.06
747	51.51	19.89	0.66	0.86	79.25	114.37
748	51.56	19.84	0.68	0.86	80.43	114.92
749	51.65	19.84	0.75	0.86	81.58	115.41
750	51.71	20.14	0.80	0.86	82.75	115.96
751	51.79	20.24	0.85	0.86	82.76	116.41
752	51.85	21.05	0.88	0.96	82.60	117.17
753	51.94	22.37	1.05	0.96	82.55	118.05
754	51.99	22.87	1.16	0.96	82.91	119.26
755	52.09	24.39	1.38	0.96	83.97	120.45
756	52.19	25.20	1.63	0.96	79.61	121.96
757	52.28	33.60	1.89	1.05	72.62	123.41
758	52.35	41.19	2.10	1.05	70.52	124.45
759	52.43	34.41	2.30	1.05	71.21	125.03
760	52.52	35.53	2.36	1.05	74.91	125.21
761	52.62	35.53	2.39	1.05	74.30	125.23
762	52.72	35.73	2.30	1.05	73.23	125.06
763	52.81	36.64	2.18	1.05	76.25	125.06
764	52.91	30.36	2.50	1.05	84.74	125.89
765	53.00	26.92	3.37	1.05	78.34	127.32
766	53.10	54.35	3.37	1.15	54.98	129.03
767	53.20	105.77	3.09	1.15	36.28	130.96
768	53.29	164.47	4.18	1.15	25.56	132.47

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	53.38	221.05	4.12	1.24	20.37	133.80
770	53.46	256.07	4.20	1.24	17.07	134.82
771	53.53	303.03	5.14	1.24	16.36	136.29
772	53.63	317.00	6.49	1.34	15.39	137.26
773	53.73	349.49	5.84	1.43	13.15	137.28
774	53.82	418.82	4.63	1.53	10.93	136.47
775	53.92	396.66	4.29	1.62	10.04	135.51
776	53.94	347.57	4.04	1.72	10.76	134.94
777	53.96	336.23	3.96	1.53	11.60	134.54
778	53.97	324.90	3.90	1.82	10.87	134.48
779	54.05	386.03	3.80	1.91	9.65	134.60
780	54.08	421.76	3.84	2.01	7.98	134.88
781	54.13	470.95	3.88	2.01	6.82	135.32
782	54.19	526.82	4.09	2.10	6.18	136.15
783	54.25	558.50	4.85	2.10	6.33	136.53
784	54.28	487.24	4.52	2.20	6.83	136.70
785	54.29	486.79	4.52	2.20	7.28	136.40
786	54.34	486.33	4.52	2.20	7.28	136.41
787	54.35	487.45	4.52	2.20	7.16	136.45
788	54.40	502.73	4.55	2.29	6.91	136.58
789	54.44	524.39	4.66	2.29	6.59	136.78
790	54.49	539.67	4.74	2.39	6.33	136.88
791	54.53	542.71	4.62	2.39	6.16	137.00
792	54.57	556.27	4.81	2.68	6.01	137.19
793	54.58	575.70	5.00	2.96	6.08	137.28
794	54.63	571.25	5.32	3.06	6.35	137.28
795	54.68	535.62	5.13	3.15	7.02	137.28
796	54.73	501.92	5.33	3.35	7.61	137.28
797	54.78	493.82	5.24	3.25	7.81	137.28
798	54.83	503.13	4.96	3.35	8.02	137.28
799	54.88	483.80	5.42	3.25	8.15	137.28
800	54.92	504.35	5.80	3.35	8.44	137.28
801	54.97	513.76	5.91	3.35	8.28	137.28
802	55.02	514.17	5.71	3.35	8.29	137.28
803	55.12	512.24	5.99	3.35	9.19	137.28
804	55.17	437.14	6.44	3.35	10.90	137.28
805	55.25	397.97	6.94	3.54	12.33	137.28
806	55.31	396.35	6.00	3.63	12.48	137.28
807	55.36	388.16	5.24	3.73	11.51	136.87
808	55.45	379.86	4.35	3.82	10.76	135.80
809	55.50	375.10	3.96	3.82	10.78	135.09
810	55.60	342.61	4.16	3.82	11.41	134.98
811	55.65	335.83	4.33	3.82	12.01	134.55
812	55.71	318.11	3.48	3.73	11.81	133.90
813	55.75	318.32	3.23	4.01	11.15	133.00
814	55.79	324.59	3.09	4.01	10.75	132.84
815	55.84	332.28	3.22	4.01	10.43	132.92
816	55.89	340.38	3.26	4.11	10.29	133.07

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	55.90	341.19	3.24	4.30	10.16	133.10
818	55.94	341.70	3.23	4.30	10.40	133.09
819	55.99	325.71	3.29	4.40	10.86	133.10
820	56.03	315.28	3.33	4.40	11.37	133.06
821	56.08	312.45	3.28	4.40	11.60	132.92
822	56.14	307.08	3.17	4.40	11.73	132.73
823	56.22	299.39	3.13	4.40	11.94	132.53
824	56.28	293.01	3.09	4.49	12.14	132.38
825	56.33	290.28	3.03	4.40	12.22	132.35
826	56.38	294.23	3.11	4.40	12.04	132.26
827	56.45	297.47	2.97	4.40	11.65	132.30
828	56.52	312.14	3.01	4.40	11.06	132.37
829	56.62	327.93	3.08	4.40	10.51	132.50
830	56.66	335.32	3.02	4.40	9.79	132.45
831	56.73	351.82	2.83	4.40	9.62	132.89
832	56.81	362.85	3.53	4.49	9.77	133.43
833	56.95	356.47	3.65	4.40	10.06	134.06
834	57.00	370.75	3.68	4.40	10.03	134.48
835	57.09	389.98	4.06	4.40	10.22	134.71
836	57.19	358.40	4.02	4.59	10.60	134.88
837	57.27	357.18	4.00	4.49	11.00	134.55
838	57.35	346.35	3.69	4.59	10.13	133.80
839	57.44	369.23	2.85	4.49	9.47	132.97
840	57.50	352.73	2.88	4.59	8.69	132.46
841	57.52	370.95	2.99	4.30	8.68	133.16
842	57.58	410.42	3.60	4.30	8.49	134.41
843	57.63	446.56	4.36	4.30	8.42	135.32
844	57.72	439.07	4.21	4.40	8.40	135.58
845	57.77	431.17	3.97	4.40	8.22	135.14
846	57.82	430.77	3.67	4.40	7.74	134.36
847	57.91	426.51	3.05	4.40	6.86	133.51
848	57.96	452.73	2.75	4.40	6.01	132.56
849	58.02	449.09	2.48	4.40	5.35	132.23
850	58.09	474.69	2.59	4.49	5.13	132.30
851	58.16	483.80	2.77	4.49	4.92	132.61
852	58.25	495.95	2.73	4.49	5.00	132.98
853	58.30	493.42	2.98	4.49	5.44	133.54
854	58.40	473.38	3.46	4.49	5.94	133.95
855	58.50	471.86	3.32	4.49	6.39	134.14
856	58.56	460.12	3.32	4.49	6.35	134.03
857	58.64	470.34	3.32	4.49	6.52	134.15
858	58.73	463.76	3.50	4.68	6.66	134.73
859	58.78	490.08	4.08	4.68	6.43	134.94
860	58.88	510.42	3.53	4.68	6.01	135.03
861	58.97	519.43	3.50	4.78	5.46	134.39
862	59.07	503.03	3.11	4.78	5.31	133.97
863	59.13	496.05	2.99	4.78	5.28	133.42
864	59.23	481.47	2.88	4.78	5.21	132.95

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	59.31	476.41	2.60	4.78	5.30	132.24
866	59.38	435.32	2.31	4.78	5.27	131.56
867	59.41	439.12	2.27	4.78	5.38	131.23
868	59.46	442.91	2.34	4.78	5.29	131.28
869	59.51	448.48	2.34	4.78	5.27	131.25
870	59.57	439.07	2.23	4.78	5.63	132.20
871	59.66	467.91	3.25	4.87	5.58	132.94
872	59.75	505.97	3.06	4.97	6.03	134.45
873	59.80	502.83	4.04	4.97	6.32	135.37
874	59.85	510.42	4.53	4.97	6.89	136.20
875	59.91	512.45	4.44	4.97	7.09	136.30
876	59.99	489.57	4.24	4.97	7.40	136.48
877	60.05	494.33	4.91	4.87	8.36	136.97
878	60.09	458.80	5.56	4.78	9.17	137.25
879	60.14	440.99	5.00	4.78	9.81	137.14
880	60.19	433.30	4.90	4.78	9.70	136.76
881	60.22	439.07	4.84	4.78	9.61	136.51
882	60.28	430.16	4.56	4.78	10.15	136.19
883	60.33	369.53	4.52	4.78	11.14	135.77
884	60.38	343.82	4.41	4.78	12.93	135.37
885	60.42	303.34	4.35	4.68	14.24	134.92
886	60.48	281.88	4.12	4.68	14.94	133.83
887	60.57	260.63	2.98	4.59	14.40	131.99
888	60.66	244.74	2.02	4.59	13.41	129.58
889	60.68	226.11	1.72	4.49	12.77	127.88
890	60.69	225.45	1.67	4.01	12.50	126.95
891	60.74	224.80	1.43	4.11	12.59	126.30
892	60.79	202.83	1.36	4.21	12.85	125.42
893	60.84	190.99	1.24	4.11	13.42	124.52
894	60.89	182.49	1.05	4.11	13.76	123.73
895	60.98	173.38	1.04	4.01	14.35	123.40
896	61.03	167.00	1.14	4.01	16.66	125.09
897	61.08	163.66	1.94	4.01	20.32	128.00
898	61.18	163.76	3.09	3.92	22.76	129.84
899	61.23	166.29	2.90	3.92	24.31	131.32
900	61.31	174.39	3.66	3.92	20.35	131.18
901	61.42	241.39	2.47	3.92	15.65	131.06
902	61.47	293.32	2.18	4.01	10.48	129.51
903	61.51	326.62	1.66	3.92	7.95	129.12
904	61.54	373.78	1.86	3.73	6.66	129.28
905	61.57	397.87	2.12	3.73	6.17	130.14
906	61.58	415.68	2.20	3.54	5.00	130.33
907	61.61	442.20	1.90	3.54	6.02	129.76
908	61.63	322.26	1.78	2.77	6.49	129.08
909	61.63	338.36	1.80	2.77	11.34	128.31
910	61.66	112.95	1.97	2.20	16.91	128.00
911	61.67	122.67	2.10	2.20	26.40	127.65
912	61.70	152.93	2.30	2.20	22.91	128.46

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	61.71	183.20	2.33	2.20	19.72	129.29
914	61.76	206.48	2.50	2.10	17.47	129.99
915	61.80	229.45	2.69	2.01	15.78	130.50
916	61.84	250.50	2.60	2.01	13.82	130.39
917	61.86	271.15	2.16	2.01	11.07	129.64
918	61.93	317.51	1.72	2.01	8.65	128.83
919	61.98	348.28	1.71	2.01	5.00	128.76
920	62.04	407.39	1.86	2.01	5.00	130.00
921	62.09	460.93	2.44	2.10	5.00	130.94
922	62.14	486.94	2.29	2.01	4.65	131.59
923	62.19	497.77	2.32	2.01	4.30	131.67
924	62.24	512.55	2.43	2.01	4.19	131.86
925	62.26	516.39	2.43	2.01	4.03	131.99
926	62.29	528.94	2.40	2.10	4.03	131.96
927	62.38	511.74	2.40	2.20	4.39	132.48
928	62.44	506.37	2.97	2.10	5.19	132.83
929	62.46	452.63	2.92	2.10	5.89	133.06
930	62.47	448.12	2.80	1.24	6.21	132.63
931	62.51	443.62	2.61	1.43	5.98	132.52
932	62.56	469.23	2.76	1.53	5.91	132.86
933	62.60	479.04	3.12	1.53	5.80	133.25
934	62.65	484.51	2.99	1.53	5.69	133.25
935	62.70	481.58	2.73	1.53	5.44	132.87
936	62.75	480.87	2.67	1.53	5.25	132.60
937	62.80	486.64	2.68	1.62	4.98	132.62
938	62.85	516.90	2.69	1.62	4.37	132.78
939	62.89	572.26	2.69	1.72	3.80	133.35
940	62.97	618.32	3.10	1.82	3.40	134.28
941	63.04	668.31	3.58	1.82	3.09	135.14
942	63.09	716.80	3.59	1.82	2.87	135.70
943	63.13	724.18	3.74	1.91	2.94	136.16
944	63.19	705.46	4.21	1.91	3.36	136.94
945	63.23	719.83	4.89	1.91	3.84	137.28
946	63.28	735.32	5.37	1.91	4.17	137.28
947	63.32	725.10	5.58	2.01	3.85	137.28
948	63.38	727.02	3.92	2.10	2.64	135.83
949	63.44	724.79	1.47	2.10	1.89	134.28
950	63.52	728.13	3.49	2.29	1.92	134.03
951	63.57	693.42	3.66	2.68	2.71	135.18
952	63.66	670.44	3.03	2.68	3.13	134.92
953	63.73	614.77	3.31	2.77	4.81	133.80
954	63.76	319.53	2.86	3.15	6.52	133.28
955	63.76	432.39	2.88	3.15	7.53	132.72
956	63.78	483.50	2.92	3.15	6.10	133.35
957	63.81	499.59	3.22	3.15	5.61	134.22
958	63.85	555.36	3.75	3.15	5.72	134.88
959	63.86	524.19	3.76	3.15	6.14	135.34
960	63.91	488.05	3.95	3.25	6.96	135.56

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	63.94	481.37	4.28	3.06	7.58	135.81
962	63.95	481.78	4.31	2.96	7.84	136.00
963	64.00	477.73	4.30	2.96	7.92	135.94
964	64.02	469.13	4.22	2.96	7.88	135.77
965	64.05	472.67	4.05	2.96	7.62	135.55
966	64.09	485.42	3.89	2.96	7.39	135.35
967	64.11	476.31	3.87	3.06	7.15	135.11
968	64.15	478.34	3.65	3.06	6.89	134.84
969	64.20	492.00	3.47	3.06	6.53	134.82
970	64.25	512.45	3.75	3.06	6.14	134.94
971	64.29	533.19	3.70	3.06	5.78	135.26
972	64.34	561.33	3.79	3.25	5.01	135.28
973	64.43	616.49	3.54	3.25	4.34	135.35
974	64.48	639.47	3.59	3.35	3.80	135.20
975	64.53	636.74	3.43	3.35	3.33	134.70
976	64.58	651.72	2.78	3.35	3.10	134.64
977	64.63	676.61	3.45	3.44	2.91	135.01
978	64.68	713.46	3.79	3.44	3.16	136.27
979	64.73	738.66	4.50	3.44	3.23	136.63
980	64.77	703.94	3.99	3.44	3.00	136.64
981	64.82	764.06	3.71	3.63	2.55	136.18
982	64.87	785.42	3.67	3.63	2.65	135.90
983	64.89	648.27	3.66	3.82	2.87	135.82
984	64.93	708.09	3.69	3.82	3.20	135.78
985	64.94	712.24	3.73	3.92	2.93	135.98
986	64.98	726.92	3.83	3.92	2.86	136.11
987	64.99	737.75	3.84	4.01	2.79	136.19
988	65.03	737.24	3.82	4.01	2.77	136.10
989	65.08	721.96	3.70	4.11	2.68	135.79
990	65.13	721.76	3.39	4.01	2.53	135.18
991	65.17	702.63	3.00	4.21	2.31	134.38
992	65.22	686.23	2.70	4.30	2.22	133.76
993	65.23	678.84	2.70	4.30	2.19	133.47
994	65.28	679.40	2.71	4.40	2.24	133.50
995	65.32	679.40	2.75	4.49	2.48	134.03
996	65.37	679.95	3.32	4.49	2.63	134.36
997	65.42	680.97	3.11	4.49	2.78	134.78
998	65.47	692.71	3.26	4.49	2.89	134.63
999	65.48	641.09	3.19	4.40	3.08	134.58
1000	65.49	637.65	3.11	4.01	3.14	134.13
1001	65.52	637.65	2.79	4.40	3.09	133.95
1002	65.57	634.21	2.97	4.30	1.61	130.82
1003	65.62	664.97	0.00	4.40	0.17	126.03
1004	65.67	684.10	0.00	4.49	N/A	87.36
1005	65.69	698.07	0.00	4.59	N/A	87.36
1006	65.72	709.31	0.00	4.59	N/A	87.36
1007	65.77	749.49	0.00	4.59	N/A	87.36
1008	65.82	797.77	0.00	4.59	N/A	87.36

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1009	65.86	824.89	0.00	4.59	N/A	87.36
1010	65.86	813.05	0.00	4.59	N/A	87.36
1011	65.91	862.75	0.00	4.68	N/A	87.36
1012	65.96	886.13	0.00	4.78	N/A	87.36

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c:	Measured cone resistance (tsf)
f_s:	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.01	0.00	0.00	0.00	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
2	0.04	0.00	0.00	0.00	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
3	0.08	0.00	0.00	0.00	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
4	0.10	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
5	0.13	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
6	0.18	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
7	0.22	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
8	0.27	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
9	0.33	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
10	0.36	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
11	0.37	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
12	0.38	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
13	0.42	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
14	0.44	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
15	0.47	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
16	0.47	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
17	0.52	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
18	0.56	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
19	0.58	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
20	0.61	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
21	0.66	0.04	0.00	0.04	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
22	0.76	0.04	0.00	0.04	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
23	0.80	0.04	0.00	0.04	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
24	0.81	0.04	0.00	0.04	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
25	0.85	0.05	0.00	0.05	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
26	0.86	0.05	0.00	0.05	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
27	0.90	0.05	0.00	0.05	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
28	0.95	0.05	0.00	0.05	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
29	1.00	0.05	0.00	0.05	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
30	1.05	0.06	0.00	0.06	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
31	1.14	0.06	0.00	0.06	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
32	1.24	0.07	0.00	0.07	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
33	1.31	0.07	0.00	0.07	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
34	1.36	0.07	0.00	0.07	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
35	1.37	0.07	0.00	0.07	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
36	1.39	0.07	0.00	0.07	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
37	1.43	0.08	0.00	0.08	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
38	1.44	0.08	0.00	0.08	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
39	1.49	0.08	0.00	0.08	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
40	1.53	0.08	0.00	0.08	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
41	1.58	0.08	0.00	0.08	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
42	1.63	0.09	0.00	0.09	1.00	0.409	1.36	0.301	1.00	1.00	2.000	No
43	1.68	0.09	0.00	0.09	1.00	0.409	1.36	0.300	1.00	1.00	2.000	No
44	1.72	0.09	0.00	0.09	1.00	0.409	1.36	0.300	1.00	1.00	2.000	No
45	1.77	0.09	0.00	0.09	1.00	0.409	1.36	0.300	1.00	1.00	2.000	No
46	1.82	0.10	0.00	0.10	1.00	0.409	1.36	0.300	1.00	1.00	2.000	No
47	1.86	0.10	0.00	0.10	1.00	0.409	1.36	0.300	1.00	1.00	2.000	No
48	1.92	0.10	0.00	0.10	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	1.97	0.10	0.00	0.10	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
50	2.01	0.11	0.00	0.11	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
51	2.09	0.11	0.00	0.11	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
52	2.16	0.11	0.00	0.11	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
53	2.20	0.12	0.00	0.12	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
54	2.25	0.12	0.00	0.12	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
55	2.31	0.12	0.00	0.12	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
56	2.37	0.13	0.00	0.13	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
57	2.40	0.13	0.00	0.13	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
58	2.46	0.13	0.00	0.13	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
59	2.54	0.13	0.00	0.13	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
60	2.59	0.14	0.00	0.14	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
61	2.69	0.14	0.00	0.14	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
62	2.74	0.15	0.00	0.15	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
63	2.83	0.15	0.00	0.15	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
64	2.88	0.15	0.00	0.15	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
65	2.98	0.16	0.00	0.16	1.00	0.407	1.36	0.300	1.00	1.00	2.000	No
66	3.03	0.16	0.00	0.16	0.99	0.407	1.36	0.300	1.00	1.00	2.000	No
67	3.12	0.17	0.00	0.17	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
68	3.21	0.17	0.00	0.17	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
69	3.27	0.17	0.00	0.17	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
70	3.34	0.18	0.00	0.18	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
71	3.41	0.18	0.00	0.18	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
72	3.51	0.19	0.00	0.19	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
73	3.55	0.19	0.00	0.19	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
74	3.65	0.19	0.00	0.19	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
75	3.75	0.20	0.00	0.20	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
76	3.83	0.20	0.00	0.20	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
77	3.94	0.21	0.00	0.21	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
78	4.04	0.22	0.00	0.22	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
79	4.13	0.22	0.00	0.22	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
80	4.24	0.23	0.00	0.23	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
81	4.38	0.23	0.00	0.23	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
82	4.50	0.24	0.00	0.24	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
83	4.62	0.25	0.00	0.25	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
84	4.71	0.25	0.00	0.25	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
85	4.75	0.26	0.00	0.26	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
86	4.84	0.26	0.00	0.26	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
87	4.89	0.26	0.00	0.26	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
88	4.94	0.27	0.00	0.27	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
89	4.98	0.27	0.00	0.27	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
90	5.07	0.27	0.00	0.27	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
91	5.13	0.28	0.00	0.28	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
92	5.17	0.28	0.00	0.28	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
93	5.27	0.28	0.00	0.28	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
94	5.32	0.29	0.00	0.29	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
95	5.42	0.29	0.00	0.29	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
96	5.46	0.30	0.00	0.30	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	5.56	0.30	0.00	0.30	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
98	5.61	0.30	0.00	0.30	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
99	5.71	0.31	0.00	0.31	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
100	5.78	0.31	0.00	0.31	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
101	5.85	0.32	0.00	0.32	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
102	5.95	0.32	0.00	0.32	0.99	0.405	1.36	0.297	1.00	1.00	2.000	No
103	6.00	0.33	0.00	0.33	0.99	0.405	1.36	0.297	1.00	1.00	2.000	No
104	6.09	0.33	0.00	0.33	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
105	6.14	0.33	0.00	0.33	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
106	6.24	0.34	0.00	0.34	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
107	6.30	0.34	0.00	0.34	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
108	6.38	0.35	0.00	0.35	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
109	6.46	0.35	0.00	0.35	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
110	6.50	0.35	0.00	0.35	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
111	6.56	0.36	0.00	0.36	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
112	6.63	0.36	0.00	0.36	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
113	6.68	0.36	0.00	0.36	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
114	6.76	0.37	0.00	0.37	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
115	6.82	0.37	0.00	0.37	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
116	6.88	0.37	0.00	0.37	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
117	6.96	0.38	0.00	0.38	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
118	7.03	0.38	0.00	0.38	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
119	7.11	0.39	0.00	0.39	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
120	7.16	0.39	0.00	0.39	0.99	0.403	1.36	0.297	1.00	1.00	2.000	No
121	7.26	0.39	0.00	0.39	0.99	0.403	1.36	0.297	1.00	1.00	2.000	No
122	7.31	0.40	0.00	0.40	0.98	0.403	1.36	0.297	1.00	1.00	2.000	No
123	7.40	0.40	0.00	0.40	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
124	7.45	0.41	0.00	0.41	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
125	7.54	0.41	0.00	0.41	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
126	7.60	0.41	0.00	0.41	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
127	7.68	0.42	0.00	0.42	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
128	7.74	0.42	0.00	0.42	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
129	7.83	0.43	0.00	0.43	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
130	7.90	0.43	0.00	0.43	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
131	7.98	0.43	0.00	0.43	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
132	8.05	0.44	0.00	0.44	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
133	8.12	0.44	0.00	0.44	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
134	8.19	0.45	0.00	0.45	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
135	8.27	0.45	0.00	0.45	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
136	8.36	0.46	0.00	0.46	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
137	8.41	0.46	0.00	0.46	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
138	8.50	0.46	0.00	0.46	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
139	8.60	0.47	0.00	0.47	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
140	8.70	0.47	0.00	0.47	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
141	8.74	0.48	0.00	0.48	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
142	8.78	0.48	0.00	0.48	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
143	8.81	0.48	0.00	0.48	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
144	8.86	0.48	0.00	0.48	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	8.91	0.49	0.00	0.49	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
146	8.94	0.49	0.00	0.49	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
147	9.02	0.49	0.00	0.49	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
148	9.10	0.50	0.00	0.50	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
149	9.17	0.50	0.00	0.50	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
150	9.22	0.50	0.00	0.50	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
151	9.31	0.51	0.00	0.51	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
152	9.37	0.51	0.00	0.51	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
153	9.42	0.51	0.00	0.51	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
154	9.52	0.52	0.00	0.52	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
155	9.60	0.53	0.00	0.53	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
156	9.66	0.53	0.00	0.53	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
157	9.74	0.53	0.00	0.53	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
158	9.81	0.54	0.00	0.54	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
159	9.89	0.54	0.00	0.54	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
160	9.98	0.55	0.00	0.55	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
161	10.03	0.55	0.00	0.55	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
162	10.13	0.55	0.00	0.55	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
163	10.23	0.56	0.00	0.56	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
164	10.32	0.57	0.00	0.57	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
165	10.38	0.57	0.00	0.57	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
166	10.47	0.57	0.00	0.57	0.98	0.401	1.36	0.294	1.00	1.00	2.000	No
167	10.57	0.58	0.00	0.58	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
168	10.66	0.58	0.00	0.58	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
169	10.76	0.59	0.00	0.59	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
170	10.85	0.60	0.00	0.60	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
171	10.92	0.60	0.00	0.60	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
172	11.00	0.60	0.00	0.60	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
173	11.07	0.61	0.00	0.61	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
174	11.10	0.61	0.00	0.61	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
175	11.15	0.61	0.00	0.61	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
176	11.19	0.61	0.00	0.61	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
177	11.24	0.62	0.00	0.62	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
178	11.29	0.62	0.00	0.62	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
179	11.34	0.62	0.00	0.62	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
180	11.40	0.63	0.00	0.63	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
181	11.47	0.63	0.00	0.63	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
182	11.53	0.63	0.00	0.63	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
183	11.58	0.64	0.00	0.64	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
184	11.65	0.64	0.00	0.64	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
185	11.72	0.64	0.00	0.64	0.98	0.399	1.36	0.294	1.00	1.00	2.000	No
186	11.77	0.65	0.00	0.65	0.98	0.399	1.36	0.294	1.00	1.00	2.000	No
187	11.82	0.65	0.00	0.65	0.98	0.399	1.36	0.294	1.00	1.00	2.000	No
188	11.88	0.65	0.00	0.65	0.98	0.399	1.36	0.294	1.00	1.00	2.000	No
189	11.97	0.66	0.00	0.66	0.97	0.399	1.36	0.294	1.00	1.00	2.000	No
190	12.02	0.66	0.00	0.66	0.97	0.399	1.36	0.294	1.00	1.00	2.000	No
191	12.06	0.66	0.00	0.66	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
192	12.11	0.67	0.00	0.67	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	12.21	0.67	0.00	0.67	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
194	12.25	0.67	0.00	0.67	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
195	12.30	0.68	0.00	0.68	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
196	12.31	0.68	0.00	0.68	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
197	12.32	0.68	0.00	0.68	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
198	12.35	0.68	0.00	0.68	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
199	12.40	0.68	0.00	0.68	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
200	12.45	0.69	0.00	0.69	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
201	12.52	0.69	0.00	0.69	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
202	12.56	0.69	0.00	0.69	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
203	12.62	0.70	0.00	0.70	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
204	12.65	0.70	0.00	0.70	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
205	12.71	0.70	0.00	0.70	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
206	12.76	0.70	0.00	0.70	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
207	12.83	0.71	0.00	0.71	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
208	12.88	0.71	0.00	0.71	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
209	12.93	0.71	0.00	0.71	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
210	12.98	0.72	0.00	0.72	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
211	13.03	0.72	0.00	0.72	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
212	13.04	0.72	0.00	0.72	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
213	13.07	0.72	0.00	0.72	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
214	13.13	0.72	0.00	0.72	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
215	13.17	0.73	0.00	0.73	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
216	13.22	0.73	0.00	0.73	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
217	13.27	0.73	0.00	0.73	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
218	13.32	0.74	0.00	0.74	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
219	13.37	0.74	0.00	0.74	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
220	13.41	0.74	0.00	0.74	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
221	13.46	0.74	0.00	0.74	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
222	13.51	0.75	0.00	0.75	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
223	13.56	0.75	0.00	0.75	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
224	13.60	0.75	0.00	0.75	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
225	13.66	0.76	0.00	0.76	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
226	13.75	0.76	0.00	0.76	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
227	13.80	0.76	0.00	0.76	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
228	13.89	0.77	0.00	0.77	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
229	13.94	0.77	0.00	0.77	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
230	13.99	0.78	0.00	0.78	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
231	14.09	0.78	0.00	0.78	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
232	14.14	0.78	0.00	0.78	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
233	14.23	0.79	0.00	0.79	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
234	14.28	0.79	0.00	0.79	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
235	14.38	0.80	0.00	0.80	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
236	14.42	0.80	0.00	0.80	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
237	14.52	0.81	0.00	0.81	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
238	14.57	0.81	0.00	0.81	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
239	14.67	0.82	0.00	0.82	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
240	14.68	0.82	0.00	0.82	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	14.70	0.82	0.00	0.82	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
242	14.75	0.82	0.00	0.82	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
243	14.80	0.82	0.00	0.82	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
244	14.89	0.83	0.00	0.83	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
245	14.94	0.83	0.00	0.83	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
246	15.04	0.84	0.00	0.84	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
247	15.13	0.84	0.00	0.84	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
248	15.21	0.85	0.00	0.85	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
249	15.28	0.85	0.00	0.85	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
250	15.38	0.86	0.00	0.86	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
251	15.47	0.86	0.00	0.86	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
252	15.57	0.87	0.00	0.87	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
253	15.67	0.87	0.00	0.87	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
254	15.77	0.88	0.00	0.88	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
255	15.86	0.89	0.00	0.89	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
256	15.96	0.89	0.00	0.89	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
257	16.05	0.90	0.00	0.90	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
258	16.15	0.90	0.00	0.90	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
259	16.25	0.91	0.00	0.91	0.97	0.396	1.36	0.291	1.00	1.00	2.000	No
260	16.31	0.91	0.00	0.91	0.97	0.395	1.36	0.291	1.00	1.00	2.000	No
261	16.39	0.91	0.00	0.91	0.97	0.395	1.36	0.291	1.00	1.00	2.000	No
262	16.48	0.92	0.00	0.92	0.97	0.395	1.36	0.291	1.00	1.00	2.000	No
263	16.59	0.93	0.00	0.93	0.97	0.395	1.36	0.291	1.00	1.00	2.000	No
264	16.68	0.93	0.00	0.93	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
265	16.76	0.94	0.00	0.94	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
266	16.86	0.94	0.00	0.94	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
267	16.92	0.94	0.00	0.94	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
268	17.02	0.95	0.00	0.95	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
269	17.11	0.96	0.00	0.96	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
270	17.22	0.96	0.00	0.96	0.96	0.395	1.36	0.290	1.00	1.00	2.000	Yes
271	17.35	0.97	0.00	0.97	0.96	0.394	1.36	0.290	1.00	1.00	2.000	Yes
272	17.45	0.97	0.00	0.97	0.96	0.394	1.36	0.290	1.00	1.00	2.000	Yes
273	17.55	0.98	0.00	0.98	0.96	0.394	1.36	0.290	1.00	1.00	2.000	Yes
274	17.61	0.98	0.00	0.98	0.96	0.394	1.36	0.290	1.00	1.00	2.000	Yes
275	17.64	0.99	0.00	0.99	0.96	0.394	1.36	0.290	1.00	1.00	2.000	Yes
276	17.70	0.99	0.00	0.99	0.96	0.394	1.36	0.290	1.00	1.00	2.000	Yes
277	17.75	0.99	0.00	0.99	0.96	0.394	1.36	0.290	1.00	1.00	2.000	Yes
278	17.80	1.00	0.00	1.00	0.96	0.394	1.36	0.290	1.00	1.00	2.000	Yes
279	17.85	1.00	0.00	1.00	0.96	0.394	1.36	0.290	1.00	1.00	2.000	Yes
280	17.94	1.00	0.00	1.00	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
281	17.99	1.01	0.00	1.01	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
282	18.09	1.01	0.00	1.01	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
283	18.15	1.02	0.00	1.02	0.96	0.394	1.36	0.289	1.00	1.00	2.000	No
284	18.23	1.02	0.00	1.02	0.96	0.394	1.36	0.289	1.00	1.00	2.000	No
285	18.33	1.03	0.00	1.03	0.96	0.394	1.36	0.289	1.00	1.00	2.000	No
286	18.43	1.03	0.00	1.03	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
287	18.52	1.04	0.00	1.04	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
288	18.59	1.04	0.00	1.04	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	18.72	1.05	0.00	1.05	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
290	18.81	1.05	0.00	1.05	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
291	18.87	1.06	0.00	1.06	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
292	18.95	1.06	0.00	1.06	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
293	19.05	1.07	0.00	1.07	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
294	19.14	1.07	0.00	1.07	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
295	19.22	1.08	0.00	1.08	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
296	19.29	1.08	0.00	1.08	0.96	0.393	1.36	0.289	1.00	1.00	2.000	Yes
297	19.38	1.09	0.00	1.09	0.96	0.392	1.36	0.289	0.99	1.00	2.000	Yes
298	19.44	1.09	0.00	1.09	0.96	0.392	1.36	0.289	0.99	1.00	2.000	Yes
299	19.53	1.09	0.00	1.09	0.96	0.392	1.36	0.288	0.99	1.00	2.000	Yes
300	19.62	1.10	0.00	1.10	0.96	0.392	1.36	0.288	0.99	1.00	2.000	Yes
301	19.69	1.10	0.00	1.10	0.96	0.392	1.36	0.288	0.99	1.00	2.000	Yes
302	19.79	1.11	0.00	1.11	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
303	19.86	1.11	0.00	1.11	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
304	19.97	1.12	0.00	1.12	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
305	20.07	1.13	0.00	1.13	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
306	20.16	1.13	0.00	1.13	0.96	0.392	1.36	0.288	0.99	1.00	2.000	No
307	20.26	1.14	0.00	1.14	0.96	0.392	1.36	0.288	0.99	1.00	2.000	Yes
308	20.34	1.14	0.00	1.14	0.96	0.391	1.36	0.288	0.98	1.00	2.000	Yes
309	20.43	1.15	0.00	1.15	0.96	0.391	1.36	0.288	0.98	1.00	2.000	Yes
310	20.50	1.15	0.00	1.15	0.96	0.391	1.36	0.288	0.98	1.00	2.000	Yes
311	20.60	1.16	0.00	1.16	0.96	0.391	1.36	0.288	0.98	1.00	2.000	Yes
312	20.62	1.16	0.00	1.16	0.96	0.391	1.36	0.288	0.98	1.00	2.000	Yes
313	20.63	1.16	0.00	1.16	0.96	0.391	1.36	0.288	0.98	1.00	2.000	Yes
314	20.68	1.16	0.00	1.16	0.96	0.391	1.36	0.288	0.98	1.00	2.000	Yes
315	20.73	1.17	0.00	1.17	0.95	0.391	1.36	0.288	0.98	1.00	2.000	Yes
316	20.82	1.17	0.00	1.17	0.95	0.391	1.36	0.287	0.98	1.00	2.000	Yes
317	20.87	1.17	0.00	1.17	0.95	0.391	1.36	0.287	0.98	1.00	2.000	Yes
318	20.91	1.18	0.00	1.18	0.95	0.391	1.36	0.287	0.98	1.00	2.000	Yes
319	20.96	1.18	0.00	1.18	0.95	0.391	1.36	0.287	0.98	1.00	2.000	Yes
320	21.05	1.19	0.00	1.19	0.95	0.391	1.36	0.287	0.98	1.00	2.000	No
321	21.11	1.19	0.00	1.19	0.95	0.391	1.36	0.287	0.98	1.00	2.000	No
322	21.17	1.19	0.00	1.19	0.95	0.391	1.36	0.287	0.98	1.00	2.000	No
323	21.25	1.20	0.00	1.20	0.95	0.390	1.36	0.287	0.98	1.00	2.000	Yes
324	21.30	1.20	0.00	1.20	0.95	0.390	1.36	0.287	0.98	1.00	2.000	Yes
325	21.37	1.20	0.00	1.20	0.95	0.390	1.36	0.287	0.97	1.00	2.000	Yes
326	21.45	1.21	0.00	1.21	0.95	0.390	1.36	0.287	0.97	1.00	2.000	Yes
327	21.49	1.21	0.00	1.21	0.95	0.390	1.36	0.287	0.97	1.00	2.000	Yes
328	21.58	1.22	0.00	1.22	0.95	0.390	1.36	0.287	0.97	1.00	2.000	Yes
329	21.64	1.22	0.00	1.22	0.95	0.390	1.36	0.287	0.97	1.00	2.000	Yes
330	21.69	1.22	0.00	1.22	0.95	0.390	1.36	0.287	0.97	1.00	2.000	Yes
331	21.78	1.23	0.00	1.23	0.95	0.390	1.36	0.287	0.97	1.00	2.000	No
332	21.83	1.23	0.00	1.23	0.95	0.390	1.36	0.287	0.97	1.00	2.000	No
333	21.89	1.24	0.00	1.24	0.95	0.390	1.36	0.287	0.97	1.00	2.000	No
334	21.98	1.24	0.00	1.24	0.95	0.390	1.36	0.286	0.97	1.00	2.000	No
335	22.03	1.25	0.00	1.25	0.95	0.390	1.36	0.286	0.97	1.00	2.000	No
336	22.12	1.25	0.00	1.25	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	22.22	1.26	0.00	1.26	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
338	22.26	1.26	0.00	1.26	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
339	22.36	1.27	0.00	1.27	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
340	22.41	1.27	0.00	1.27	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
341	22.51	1.28	0.00	1.28	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
342	22.60	1.28	0.00	1.28	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
343	22.70	1.29	0.00	1.29	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
344	22.75	1.29	0.00	1.29	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
345	22.84	1.30	0.00	1.30	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
346	22.89	1.30	0.00	1.30	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
347	22.90	1.30	0.00	1.30	0.95	0.389	1.36	0.286	0.96	1.00	2.000	No
348	22.94	1.30	0.00	1.30	0.95	0.388	1.36	0.286	0.96	1.00	2.000	No
349	23.00	1.31	0.00	1.31	0.95	0.388	1.36	0.286	0.96	1.00	2.000	No
350	23.08	1.31	0.00	1.31	0.95	0.388	1.36	0.285	0.96	1.00	2.000	No
351	23.13	1.31	0.00	1.31	0.95	0.388	1.36	0.285	0.96	1.00	2.000	No
352	23.20	1.32	0.00	1.32	0.95	0.388	1.36	0.285	0.96	1.00	2.000	No
353	23.27	1.32	0.00	1.32	0.95	0.388	1.36	0.285	0.96	1.00	2.000	No
354	23.33	1.33	0.00	1.33	0.95	0.388	1.36	0.285	0.96	1.00	2.000	No
355	23.42	1.33	0.00	1.33	0.95	0.388	1.36	0.285	0.95	1.00	2.000	No
356	23.48	1.34	0.00	1.34	0.95	0.388	1.36	0.285	0.95	1.00	2.000	No
357	23.57	1.34	0.00	1.34	0.95	0.388	1.36	0.285	0.95	1.00	2.000	No
358	23.61	1.34	0.00	1.34	0.95	0.388	1.36	0.285	0.95	1.00	2.000	No
359	23.66	1.35	0.00	1.35	0.95	0.388	1.36	0.285	0.95	1.00	2.000	No
360	23.73	1.35	0.00	1.35	0.95	0.387	1.36	0.285	0.95	1.00	2.000	No
361	23.80	1.36	0.00	1.36	0.95	0.387	1.36	0.285	0.95	1.00	2.000	No
362	23.85	1.36	0.00	1.36	0.95	0.387	1.36	0.285	0.95	1.00	2.000	No
363	23.94	1.36	0.00	1.36	0.95	0.387	1.36	0.285	0.95	1.00	2.000	No
364	24.00	1.37	0.00	1.37	0.95	0.387	1.36	0.285	0.95	1.00	2.000	No
365	24.09	1.37	0.00	1.37	0.94	0.387	1.36	0.285	0.95	1.00	2.000	No
366	24.16	1.38	0.00	1.38	0.94	0.387	1.36	0.284	0.95	1.00	2.000	No
367	24.24	1.38	0.00	1.38	0.94	0.387	1.36	0.284	0.95	1.00	2.000	No
368	24.33	1.39	0.00	1.39	0.94	0.387	1.36	0.284	0.95	1.00	2.000	No
369	24.43	1.40	0.00	1.40	0.94	0.386	1.36	0.284	0.95	1.00	2.000	No
370	24.52	1.40	0.00	1.40	0.94	0.386	1.36	0.284	0.95	1.00	2.000	No
371	24.58	1.40	0.00	1.40	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
372	24.59	1.40	0.00	1.40	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
373	24.63	1.41	0.00	1.41	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
374	24.68	1.41	0.00	1.41	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
375	24.77	1.42	0.00	1.42	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
376	24.82	1.42	0.00	1.42	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
377	24.92	1.42	0.00	1.42	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
378	25.01	1.43	0.00	1.43	0.94	0.386	1.36	0.284	0.94	1.00	2.000	No
379	25.06	1.43	0.00	1.43	0.94	0.386	1.36	0.283	0.94	1.00	2.000	No
380	25.16	1.44	0.00	1.44	0.94	0.385	1.36	0.283	0.94	1.00	2.000	No
381	25.25	1.45	0.00	1.45	0.94	0.385	1.36	0.283	0.94	1.00	2.000	No
382	25.30	1.45	0.00	1.45	0.94	0.385	1.36	0.283	0.94	1.00	2.000	No
383	25.41	1.45	0.00	1.45	0.94	0.385	1.36	0.283	0.94	1.00	2.000	Yes
384	25.49	1.46	0.00	1.46	0.94	0.385	1.36	0.283	0.94	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	25.55	1.46	0.00	1.46	0.94	0.385	1.36	0.283	0.94	1.00	2.000	Yes
386	25.64	1.47	0.00	1.47	0.94	0.385	1.36	0.283	0.94	1.00	2.000	Yes
387	25.70	1.47	0.00	1.47	0.94	0.385	1.36	0.283	0.94	1.00	2.000	Yes
388	25.79	1.48	0.00	1.48	0.94	0.385	1.36	0.283	0.94	1.00	2.000	Yes
389	25.89	1.48	0.00	1.48	0.94	0.384	1.36	0.283	0.93	1.00	2.000	Yes
390	25.94	1.49	0.00	1.49	0.94	0.384	1.36	0.283	0.93	1.00	2.000	Yes
391	26.02	1.49	0.00	1.49	0.94	0.384	1.36	0.282	0.93	1.00	2.000	Yes
392	26.12	1.50	0.00	1.50	0.94	0.384	1.36	0.282	0.93	1.00	2.000	Yes
393	26.17	1.50	0.00	1.50	0.94	0.384	1.36	0.282	0.93	1.00	2.000	Yes
394	26.28	1.51	0.00	1.51	0.94	0.384	1.36	0.282	0.93	1.00	2.000	Yes
395	26.36	1.51	0.00	1.51	0.94	0.384	1.36	0.282	0.93	1.00	2.000	Yes
396	26.45	1.52	0.00	1.52	0.94	0.383	1.36	0.282	0.93	1.00	2.000	Yes
397	26.50	1.52	0.00	1.52	0.94	0.383	1.36	0.282	0.93	1.00	2.000	Yes
398	26.61	1.53	0.00	1.53	0.94	0.383	1.36	0.282	0.93	1.00	2.000	Yes
399	26.70	1.53	0.00	1.53	0.94	0.383	1.36	0.282	0.93	1.00	2.000	No
400	26.77	1.54	0.00	1.54	0.94	0.383	1.36	0.282	0.93	1.00	2.000	No
401	26.85	1.54	0.00	1.54	0.93	0.383	1.36	0.281	0.93	1.00	2.000	No
402	26.94	1.54	0.00	1.54	0.93	0.383	1.36	0.281	0.93	1.00	2.000	No
403	27.04	1.55	0.00	1.55	0.93	0.383	1.36	0.281	0.93	1.00	2.000	No
404	27.14	1.56	0.00	1.56	0.93	0.382	1.36	0.281	0.93	1.00	2.000	No
405	27.23	1.56	0.00	1.56	0.93	0.382	1.36	0.281	0.93	1.00	2.000	No
406	27.28	1.56	0.00	1.56	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
407	27.29	1.56	0.00	1.56	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
408	27.38	1.57	0.00	1.57	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
409	27.48	1.57	0.00	1.57	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
410	27.57	1.58	0.00	1.58	0.93	0.382	1.36	0.281	0.92	1.00	2.000	No
411	27.64	1.58	0.00	1.58	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
412	27.65	1.58	0.00	1.58	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
413	27.74	1.59	0.00	1.59	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
414	27.80	1.59	0.00	1.59	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
415	27.90	1.60	0.00	1.60	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
416	27.99	1.60	0.00	1.60	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
417	28.07	1.61	0.00	1.61	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
418	28.16	1.61	0.00	1.61	0.93	0.381	1.36	0.280	0.92	1.00	2.000	No
419	28.25	1.62	0.00	1.62	0.93	0.380	1.36	0.280	0.92	1.00	2.000	No
420	28.34	1.62	0.00	1.62	0.93	0.380	1.36	0.280	0.92	1.00	2.000	No
421	28.44	1.63	0.00	1.63	0.93	0.380	1.36	0.279	0.92	1.00	2.000	No
422	28.53	1.63	0.00	1.63	0.93	0.380	1.36	0.279	0.92	1.00	2.000	No
423	28.62	1.64	0.00	1.64	0.93	0.380	1.36	0.279	0.92	1.00	2.000	No
424	28.76	1.65	0.00	1.65	0.93	0.379	1.36	0.279	0.92	1.00	2.000	No
425	28.86	1.65	0.00	1.65	0.93	0.379	1.36	0.279	0.91	1.00	2.000	No
426	28.96	1.66	0.00	1.66	0.93	0.379	1.36	0.279	0.91	1.00	2.000	No
427	29.08	1.66	0.00	1.66	0.93	0.379	1.36	0.279	0.91	1.00	2.000	No
428	29.19	1.67	0.00	1.67	0.92	0.379	1.36	0.278	0.91	1.00	2.000	No
429	29.29	1.68	0.00	1.68	0.92	0.378	1.36	0.278	0.91	1.00	2.000	No
430	29.39	1.68	0.00	1.68	0.92	0.378	1.36	0.278	0.91	1.00	2.000	No
431	29.50	1.69	0.00	1.69	0.92	0.378	1.36	0.278	0.91	1.00	2.000	No
432	29.63	1.70	0.00	1.70	0.92	0.378	1.36	0.278	0.91	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	29.65	1.70	0.00	1.70	0.92	0.378	1.36	0.278	0.91	1.00	2.000	Yes
434	29.66	1.70	0.00	1.70	0.92	0.378	1.36	0.278	0.91	1.00	2.000	Yes
435	29.72	1.70	0.00	1.70	0.92	0.378	1.36	0.278	0.91	1.00	2.000	Yes
436	29.80	1.71	0.00	1.71	0.92	0.377	1.36	0.277	0.91	1.00	2.000	Yes
437	29.85	1.71	0.00	1.71	0.92	0.377	1.36	0.277	0.91	1.00	2.000	Yes
438	29.94	1.72	0.00	1.72	0.92	0.377	1.36	0.277	0.91	1.00	2.000	Yes
439	30.00	1.72	0.00	1.72	0.92	0.377	1.36	0.277	0.91	1.00	2.000	Yes
440	30.05	1.72	0.00	1.72	0.92	0.377	1.36	0.277	0.91	1.00	2.000	Yes
441	30.14	1.73	0.00	1.73	0.92	0.378	1.36	0.278	0.91	1.00	2.000	Yes
442	30.19	1.73	0.01	1.73	0.92	0.378	1.36	0.278	0.91	1.00	2.000	Yes
443	30.24	1.74	0.01	1.73	0.92	0.378	1.36	0.278	0.91	1.00	2.000	Yes
444	30.29	1.74	0.01	1.73	0.92	0.378	1.36	0.278	0.91	1.00	0.307	No
445	30.38	1.75	0.01	1.73	0.92	0.379	1.36	0.278	0.91	1.00	0.307	No
446	30.43	1.75	0.01	1.74	0.92	0.379	1.36	0.279	0.91	1.00	0.308	No
447	30.48	1.75	0.01	1.74	0.92	0.379	1.36	0.279	0.91	1.00	0.308	No
448	30.54	1.76	0.02	1.74	0.92	0.379	1.36	0.279	0.91	1.00	0.308	No
449	30.62	1.76	0.02	1.74	0.92	0.380	1.36	0.279	0.91	1.00	0.309	No
450	30.67	1.76	0.02	1.74	0.92	0.380	1.36	0.279	0.91	1.00	0.309	No
451	30.72	1.77	0.02	1.74	0.92	0.380	1.36	0.280	0.90	1.00	0.309	No
452	30.76	1.77	0.02	1.75	0.92	0.380	1.36	0.280	0.90	1.00	0.309	No
453	30.86	1.78	0.03	1.75	0.92	0.381	1.36	0.280	0.90	1.00	0.310	No
454	30.91	1.78	0.03	1.75	0.92	0.381	1.36	0.280	0.90	1.00	0.310	No
455	30.95	1.78	0.03	1.75	0.92	0.381	1.36	0.280	0.90	1.00	0.310	No
456	31.03	1.79	0.03	1.75	0.92	0.382	1.36	0.281	0.90	1.00	0.310	No
457	31.10	1.79	0.03	1.76	0.91	0.382	1.36	0.281	0.90	1.00	0.311	No
458	31.15	1.79	0.04	1.76	0.91	0.382	1.36	0.281	0.90	1.00	0.311	No
459	31.20	1.80	0.04	1.76	0.91	0.382	1.36	0.281	0.90	1.00	0.311	No
460	31.26	1.80	0.04	1.76	0.91	0.383	1.36	0.281	0.90	1.00	0.311	No
461	31.34	1.81	0.04	1.76	0.91	0.383	1.36	0.282	0.90	1.00	0.312	No
462	31.37	1.81	0.04	1.77	0.91	0.383	1.36	0.282	0.90	1.00	0.312	No
463	31.38	1.81	0.04	1.77	0.91	0.383	1.36	0.282	0.90	1.00	0.312	No
464	31.43	1.81	0.04	1.77	0.91	0.383	1.36	0.282	0.90	1.00	0.312	No
465	31.47	1.81	0.05	1.77	0.91	0.383	1.36	0.282	0.90	1.00	0.312	No
466	31.55	1.82	0.05	1.77	0.91	0.384	1.36	0.282	0.90	1.00	0.313	No
467	31.59	1.82	0.05	1.77	0.91	0.384	1.36	0.282	0.90	1.00	0.313	No
468	31.66	1.83	0.05	1.77	0.91	0.384	1.36	0.282	0.90	1.00	0.313	No
469	31.73	1.83	0.05	1.78	0.91	0.385	1.36	0.283	0.90	1.00	0.314	No
470	31.78	1.83	0.06	1.78	0.91	0.385	1.36	0.283	0.90	1.00	0.314	No
471	31.84	1.84	0.06	1.78	0.91	0.385	1.36	0.283	0.90	1.00	0.314	No
472	31.93	1.84	0.06	1.78	0.91	0.385	1.36	0.283	0.90	1.00	0.314	No
473	31.98	1.85	0.06	1.78	0.91	0.385	1.36	0.283	0.90	1.00	0.315	No
474	32.02	1.85	0.06	1.79	0.91	0.386	1.36	0.284	0.90	1.00	0.315	No
475	32.09	1.85	0.07	1.79	0.91	0.386	1.36	0.284	0.90	1.00	0.315	No
476	32.16	1.86	0.07	1.79	0.91	0.386	1.36	0.284	0.90	1.00	0.315	No
477	32.22	1.86	0.07	1.79	0.91	0.386	1.36	0.284	0.90	1.00	0.316	No
478	32.27	1.86	0.07	1.79	0.91	0.387	1.36	0.284	0.90	1.00	0.316	No
479	32.34	1.87	0.07	1.80	0.91	0.387	1.36	0.284	0.90	1.00	0.316	No
480	32.42	1.87	0.08	1.80	0.91	0.387	1.36	0.285	0.90	1.00	0.316	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	32.46	1.88	0.08	1.80	0.91	0.387	1.36	0.285	0.90	1.00	0.317	No
482	32.54	1.88	0.08	1.80	0.91	0.388	1.36	0.285	0.90	1.00	0.317	No
483	32.60	1.89	0.08	1.80	0.91	0.388	1.36	0.285	0.90	1.00	0.317	No
484	32.67	1.89	0.08	1.81	0.91	0.388	1.36	0.285	0.90	1.00	0.317	No
485	32.75	1.89	0.09	1.81	0.91	0.388	1.36	0.285	0.90	1.00	0.318	No
486	32.81	1.90	0.09	1.81	0.90	0.389	1.36	0.286	0.90	1.00	0.318	No
487	32.89	1.90	0.09	1.81	0.90	0.389	1.36	0.286	0.90	1.00	0.318	No
488	32.94	1.91	0.09	1.82	0.90	0.389	1.36	0.286	0.90	1.00	0.319	No
489	32.95	1.91	0.09	1.82	0.90	0.389	1.36	0.286	0.90	1.00	0.319	No
490	33.00	1.91	0.09	1.82	0.90	0.389	1.36	0.286	0.90	1.00	0.319	No
491	33.06	1.91	0.10	1.82	0.90	0.389	1.36	0.286	0.90	1.00	0.319	No
492	33.11	1.92	0.10	1.82	0.90	0.390	1.36	0.286	0.90	1.00	0.319	No
493	33.20	1.92	0.10	1.82	0.90	0.390	1.36	0.287	0.90	1.00	0.320	No
494	33.25	1.93	0.10	1.83	0.90	0.390	1.36	0.287	0.90	1.00	0.320	No
495	33.34	1.93	0.10	1.83	0.90	0.390	1.36	0.287	0.90	1.00	0.320	No
496	33.38	1.94	0.11	1.83	0.90	0.390	1.36	0.287	0.90	1.00	0.320	No
497	33.48	1.94	0.11	1.83	0.90	0.391	1.36	0.287	0.90	1.00	0.321	No
498	33.58	1.95	0.11	1.84	0.90	0.391	1.36	0.287	0.90	1.00	0.321	No
499	33.63	1.95	0.11	1.84	0.90	0.391	1.36	0.288	0.90	1.00	0.321	No
500	33.73	1.96	0.12	1.84	0.90	0.391	1.36	0.288	0.90	1.00	0.322	No
501	33.82	1.96	0.12	1.84	0.90	0.392	1.36	0.288	0.89	1.00	0.322	No
502	33.87	1.97	0.12	1.85	0.90	0.392	1.36	0.288	0.89	1.00	0.322	No
503	33.96	1.97	0.12	1.85	0.90	0.392	1.36	0.288	0.89	1.00	0.322	No
504	34.02	1.98	0.13	1.85	0.90	0.392	1.36	0.288	0.89	1.00	0.323	No
505	34.11	1.98	0.13	1.85	0.90	0.393	1.36	0.289	0.89	1.00	0.323	No
506	34.18	1.99	0.13	1.86	0.90	0.393	1.36	0.289	0.89	1.00	0.323	No
507	34.26	1.99	0.13	1.86	0.90	0.393	1.36	0.289	0.89	1.00	0.323	No
508	34.35	2.00	0.14	1.86	0.90	0.393	1.36	0.289	0.89	1.00	0.324	No
509	34.44	2.00	0.14	1.87	0.89	0.393	1.36	0.289	0.89	1.00	0.324	No
510	34.49	2.01	0.14	1.87	0.89	0.394	1.36	0.289	0.89	1.00	0.324	No
511	34.59	2.01	0.14	1.87	0.89	0.394	1.36	0.290	0.89	1.00	0.325	No
512	34.69	2.02	0.15	1.87	0.89	0.394	1.36	0.290	0.89	1.00	0.325	No
513	34.76	2.03	0.15	1.88	0.89	0.394	1.36	0.290	0.89	1.00	0.325	No
514	34.83	2.03	0.15	1.88	0.89	0.394	1.36	0.290	0.89	1.00	0.325	No
515	34.93	2.04	0.15	1.88	0.89	0.395	1.36	0.290	0.89	1.00	0.326	No
516	35.02	2.04	0.16	1.89	0.89	0.395	1.36	0.290	0.89	1.00	0.326	No
517	35.12	2.05	0.16	1.89	0.89	0.395	1.36	0.291	0.89	1.00	0.326	No
518	35.22	2.06	0.16	1.89	0.89	0.395	1.36	0.291	0.89	1.00	0.327	No
519	35.30	2.06	0.17	1.90	0.89	0.396	1.36	0.291	0.89	1.00	0.327	No
520	35.38	2.07	0.17	1.90	0.89	0.396	1.36	0.291	0.89	1.00	0.327	No
521	35.43	2.07	0.17	1.90	0.89	0.396	1.36	0.291	0.89	1.00	0.327	No
522	35.46	2.07	0.17	1.90	0.89	0.396	1.36	0.291	0.89	1.00	0.327	No
523	35.51	2.08	0.17	1.90	0.89	0.396	1.36	0.291	0.89	1.00	2.000	Yes
524	35.56	2.08	0.17	1.90	0.89	0.396	1.36	0.291	0.89	1.00	2.000	Yes
525	35.66	2.08	0.18	1.91	0.89	0.396	1.36	0.291	0.89	1.00	2.000	Yes
526	35.70	2.09	0.18	1.91	0.89	0.396	1.36	0.291	0.89	1.00	2.000	Yes
527	35.80	2.09	0.18	1.91	0.88	0.397	1.36	0.292	0.89	1.00	2.000	Yes
528	35.89	2.10	0.18	1.92	0.88	0.397	1.36	0.292	0.89	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	35.96	2.10	0.19	1.92	0.88	0.397	1.36	0.292	0.89	1.00	2.000	Yes
530	36.04	2.11	0.19	1.92	0.88	0.397	1.36	0.292	0.89	1.00	2.000	Yes
531	36.14	2.12	0.19	1.92	0.88	0.397	1.36	0.292	0.89	1.00	2.000	Yes
532	36.19	2.12	0.19	1.93	0.88	0.397	1.36	0.292	0.89	1.00	2.000	Yes
533	36.28	2.12	0.20	1.93	0.88	0.398	1.36	0.292	0.89	1.00	2.000	Yes
534	36.33	2.13	0.20	1.93	0.88	0.398	1.36	0.292	0.89	1.00	0.330	No
535	36.42	2.13	0.20	1.93	0.88	0.398	1.36	0.293	0.89	1.00	0.330	No
536	36.48	2.14	0.20	1.93	0.88	0.398	1.36	0.293	0.89	1.00	0.330	No
537	36.52	2.14	0.20	1.94	0.88	0.398	1.36	0.293	0.89	1.00	0.330	No
538	36.62	2.14	0.21	1.94	0.88	0.398	1.36	0.293	0.89	1.00	0.330	No
539	36.68	2.15	0.21	1.94	0.88	0.398	1.36	0.293	0.89	1.00	0.331	No
540	36.77	2.15	0.21	1.94	0.88	0.398	1.36	0.293	0.89	1.00	0.331	No
541	36.86	2.16	0.21	1.95	0.88	0.399	1.36	0.293	0.89	1.00	2.000	Yes
542	36.90	2.16	0.22	1.95	0.88	0.399	1.36	0.293	0.89	1.00	2.000	Yes
543	37.00	2.17	0.22	1.95	0.88	0.399	1.36	0.293	0.88	1.00	2.000	Yes
544	37.10	2.17	0.22	1.95	0.88	0.399	1.36	0.293	0.88	1.00	2.000	Yes
545	37.20	2.18	0.22	1.96	0.87	0.399	1.36	0.293	0.88	1.00	2.000	Yes
546	37.29	2.19	0.23	1.96	0.87	0.399	1.36	0.294	0.88	1.00	2.000	Yes
547	37.39	2.19	0.23	1.96	0.87	0.399	1.36	0.294	0.88	1.00	2.000	Yes
548	37.49	2.20	0.23	1.97	0.87	0.400	1.36	0.294	0.88	1.00	0.333	No
549	37.53	2.20	0.24	1.97	0.87	0.400	1.36	0.294	0.88	1.00	0.333	No
550	37.58	2.21	0.24	1.97	0.87	0.400	1.36	0.294	0.88	1.00	0.333	No
551	37.62	2.21	0.24	1.97	0.87	0.400	1.36	0.294	0.88	1.00	0.333	No
552	37.69	2.21	0.24	1.97	0.87	0.400	1.36	0.294	0.88	1.00	0.333	No
553	37.77	2.22	0.24	1.98	0.87	0.400	1.36	0.294	0.88	1.00	0.333	No
554	37.82	2.22	0.24	1.98	0.87	0.400	1.36	0.294	0.88	1.00	0.333	No
555	37.87	2.22	0.25	1.98	0.87	0.400	1.36	0.294	0.88	1.00	0.333	No
556	37.91	2.23	0.25	1.98	0.87	0.400	1.36	0.294	0.88	1.00	0.333	No
557	37.97	2.23	0.25	1.98	0.87	0.400	1.36	0.294	0.88	1.00	0.334	No
558	38.06	2.24	0.25	1.99	0.87	0.400	1.36	0.294	0.88	1.00	0.334	No
559	38.10	2.24	0.25	1.99	0.87	0.400	1.36	0.294	0.88	1.00	0.334	No
560	38.17	2.24	0.25	1.99	0.87	0.400	1.36	0.294	0.88	1.00	0.334	No
561	38.25	2.25	0.26	1.99	0.87	0.400	1.36	0.294	0.88	1.00	0.334	No
562	38.35	2.26	0.26	2.00	0.87	0.401	1.36	0.294	0.88	1.00	0.334	No
563	38.40	2.26	0.26	2.00	0.86	0.401	1.36	0.295	0.88	1.00	0.334	No
564	38.46	2.26	0.26	2.00	0.86	0.401	1.36	0.295	0.88	1.00	0.335	No
565	38.54	2.27	0.27	2.00	0.86	0.401	1.36	0.295	0.88	1.00	0.335	No
566	38.60	2.27	0.27	2.00	0.86	0.401	1.36	0.295	0.88	1.00	0.335	No
567	38.69	2.28	0.27	2.01	0.86	0.401	1.36	0.295	0.88	1.00	0.335	No
568	38.74	2.28	0.27	2.01	0.86	0.401	1.36	0.295	0.88	1.00	0.335	No
569	38.83	2.29	0.28	2.01	0.86	0.401	1.36	0.295	0.88	1.00	0.335	No
570	38.88	2.29	0.28	2.01	0.86	0.401	1.36	0.295	0.88	1.00	0.335	No
571	38.97	2.30	0.28	2.02	0.86	0.401	1.36	0.295	0.88	1.00	0.335	No
572	39.02	2.30	0.28	2.02	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
573	39.11	2.31	0.28	2.02	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
574	39.16	2.31	0.29	2.02	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
575	39.23	2.31	0.29	2.03	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
576	39.24	2.31	0.29	2.03	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	39.28	2.32	0.29	2.03	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
578	39.32	2.32	0.29	2.03	0.86	0.401	1.36	0.295	0.88	1.00	0.336	No
579	39.39	2.32	0.29	2.03	0.86	0.401	1.36	0.295	0.88	1.00	2.000	Yes
580	39.47	2.33	0.30	2.03	0.86	0.401	1.36	0.295	0.88	1.00	2.000	Yes
581	39.54	2.33	0.30	2.04	0.86	0.401	1.36	0.295	0.88	1.00	2.000	Yes
582	39.62	2.34	0.30	2.04	0.85	0.401	1.36	0.295	0.88	1.00	2.000	Yes
583	39.71	2.34	0.30	2.04	0.85	0.401	1.36	0.295	0.88	1.00	2.000	Yes
584	39.76	2.35	0.30	2.04	0.85	0.401	1.36	0.295	0.88	1.00	2.000	Yes
585	39.85	2.35	0.31	2.05	0.85	0.401	1.36	0.295	0.88	1.00	2.000	Yes
586	39.90	2.36	0.31	2.05	0.85	0.402	1.36	0.295	0.88	1.00	2.000	Yes
587	40.00	2.36	0.31	2.05	0.85	0.402	1.36	0.295	0.88	1.00	2.000	Yes
588	40.06	2.37	0.31	2.05	0.85	0.402	1.36	0.295	0.88	1.00	2.000	Yes
589	40.15	2.37	0.32	2.05	0.85	0.402	1.36	0.295	0.88	1.00	2.000	Yes
590	40.21	2.38	0.32	2.06	0.85	0.402	1.36	0.295	0.88	1.00	2.000	Yes
591	40.29	2.38	0.32	2.06	0.85	0.402	1.36	0.295	0.88	1.00	2.000	Yes
592	40.35	2.38	0.32	2.06	0.85	0.402	1.36	0.295	0.88	1.00	2.000	Yes
593	40.43	2.39	0.33	2.06	0.85	0.402	1.36	0.295	0.87	1.00	2.000	Yes
594	40.52	2.39	0.33	2.07	0.85	0.402	1.36	0.295	0.87	1.00	2.000	Yes
595	40.58	2.40	0.33	2.07	0.85	0.402	1.36	0.295	0.87	1.00	2.000	Yes
596	40.67	2.40	0.33	2.07	0.85	0.402	1.36	0.295	0.87	1.00	2.000	Yes
597	40.77	2.41	0.34	2.07	0.84	0.402	1.36	0.295	0.87	1.00	2.000	Yes
598	40.84	2.41	0.34	2.08	0.84	0.402	1.36	0.295	0.87	1.00	2.000	Yes
599	40.89	2.42	0.34	2.08	0.84	0.402	1.36	0.295	0.87	1.00	2.000	Yes
600	40.94	2.42	0.34	2.08	0.84	0.402	1.36	0.295	0.87	1.00	2.000	Yes
601	41.03	2.43	0.34	2.08	0.84	0.402	1.36	0.295	0.87	1.00	2.000	Yes
602	41.08	2.43	0.35	2.08	0.84	0.402	1.36	0.295	0.87	1.00	2.000	Yes
603	41.14	2.43	0.35	2.09	0.84	0.402	1.36	0.295	0.87	1.00	2.000	Yes
604	41.22	2.44	0.35	2.09	0.84	0.402	1.36	0.295	0.87	1.00	2.000	Yes
605	41.28	2.44	0.35	2.09	0.84	0.402	1.36	0.295	0.87	1.00	0.338	No
606	41.33	2.44	0.35	2.09	0.84	0.402	1.36	0.295	0.87	1.00	0.338	No
607	41.42	2.45	0.36	2.09	0.84	0.402	1.36	0.295	0.87	1.00	0.339	No
608	41.47	2.45	0.36	2.10	0.84	0.402	1.36	0.295	0.87	1.00	0.339	No
609	41.52	2.46	0.36	2.10	0.84	0.402	1.36	0.295	0.87	1.00	0.339	No
610	41.62	2.46	0.36	2.10	0.84	0.402	1.36	0.295	0.87	1.00	0.339	No
611	41.67	2.47	0.36	2.10	0.84	0.402	1.36	0.295	0.87	1.00	0.339	No
612	41.76	2.47	0.37	2.10	0.84	0.402	1.36	0.295	0.87	1.00	0.339	No
613	41.82	2.48	0.37	2.11	0.83	0.402	1.36	0.295	0.87	1.00	0.339	No
614	41.90	2.48	0.37	2.11	0.83	0.402	1.36	0.295	0.87	1.00	0.339	No
615	41.99	2.49	0.37	2.11	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
616	42.05	2.49	0.38	2.11	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
617	42.15	2.50	0.38	2.12	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
618	42.23	2.50	0.38	2.12	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
619	42.30	2.51	0.38	2.12	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
620	42.38	2.51	0.39	2.13	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
621	42.48	2.52	0.39	2.13	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
622	42.57	2.52	0.39	2.13	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
623	42.64	2.53	0.39	2.13	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
624	42.72	2.53	0.40	2.14	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	42.82	2.54	0.40	2.14	0.83	0.401	1.36	0.295	0.87	1.00	0.339	No
626	42.90	2.55	0.40	2.14	0.82	0.401	1.36	0.295	0.87	1.00	0.339	No
627	42.97	2.55	0.40	2.15	0.82	0.401	1.36	0.295	0.87	1.00	0.339	No
628	43.06	2.56	0.41	2.15	0.82	0.401	1.36	0.295	0.87	1.00	0.340	No
629	43.15	2.56	0.41	2.15	0.82	0.401	1.36	0.295	0.87	1.00	0.340	No
630	43.20	2.56	0.41	2.15	0.82	0.401	1.36	0.295	0.87	1.00	0.340	No
631	43.30	2.57	0.41	2.16	0.82	0.401	1.36	0.295	0.87	1.00	0.340	No
632	43.40	2.58	0.42	2.16	0.82	0.401	1.36	0.294	0.87	1.00	0.340	No
633	43.48	2.58	0.42	2.16	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
634	43.51	2.58	0.42	2.16	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
635	43.52	2.58	0.42	2.16	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
636	43.56	2.59	0.42	2.16	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
637	43.61	2.59	0.42	2.17	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
638	43.67	2.59	0.43	2.17	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
639	43.72	2.60	0.43	2.17	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
640	43.80	2.60	0.43	2.17	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
641	43.85	2.61	0.43	2.17	0.82	0.400	1.36	0.294	0.87	1.00	0.340	No
642	43.90	2.61	0.43	2.18	0.81	0.400	1.36	0.294	0.87	1.00	0.340	No
643	43.94	2.61	0.43	2.18	0.81	0.400	1.36	0.294	0.87	1.00	0.340	No
644	43.99	2.62	0.44	2.18	0.81	0.400	1.36	0.294	0.87	1.00	0.340	No
645	44.08	2.62	0.44	2.18	0.81	0.400	1.36	0.294	0.87	1.00	0.340	No
646	44.14	2.62	0.44	2.18	0.81	0.400	1.36	0.294	0.87	1.00	0.340	No
647	44.22	2.63	0.44	2.19	0.81	0.400	1.36	0.294	0.86	1.00	0.340	No
648	44.28	2.63	0.45	2.19	0.81	0.400	1.36	0.294	0.86	1.00	0.340	No
649	44.33	2.64	0.45	2.19	0.81	0.400	1.36	0.294	0.86	1.00	0.340	No
650	44.40	2.64	0.45	2.19	0.81	0.399	1.36	0.294	0.86	1.00	0.340	No
651	44.48	2.65	0.45	2.20	0.81	0.399	1.36	0.294	0.86	1.00	0.340	No
652	44.52	2.65	0.45	2.20	0.81	0.399	1.36	0.294	0.86	1.00	0.340	No
653	44.61	2.66	0.46	2.20	0.81	0.399	1.36	0.294	0.86	1.00	0.340	No
654	44.72	2.66	0.46	2.20	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
655	44.77	2.67	0.46	2.21	0.81	0.399	1.36	0.293	0.86	1.00	0.340	No
656	44.91	2.67	0.47	2.21	0.80	0.399	1.36	0.293	0.86	1.00	0.340	No
657	44.95	2.68	0.47	2.21	0.80	0.399	1.36	0.293	0.86	1.00	0.340	No
658	45.02	2.68	0.47	2.21	0.80	0.399	1.36	0.293	0.86	1.00	0.340	No
659	45.04	2.68	0.47	2.21	0.80	0.399	1.36	0.293	0.86	1.00	0.340	No
660	45.06	2.69	0.47	2.22	0.80	0.399	1.36	0.293	0.86	1.00	0.340	No
661	45.11	2.69	0.47	2.22	0.80	0.399	1.36	0.293	0.86	1.00	0.340	No
662	45.15	2.69	0.47	2.22	0.80	0.398	1.36	0.293	0.86	1.00	0.340	No
663	45.21	2.69	0.47	2.22	0.80	0.398	1.36	0.293	0.86	1.00	0.340	No
664	45.25	2.70	0.48	2.22	0.80	0.398	1.36	0.293	0.86	1.00	0.340	No
665	45.30	2.70	0.48	2.22	0.80	0.398	1.36	0.293	0.86	1.00	0.340	No
666	45.35	2.70	0.48	2.23	0.80	0.398	1.36	0.293	0.86	1.00	0.340	No
667	45.41	2.71	0.48	2.23	0.80	0.398	1.36	0.293	0.86	1.00	0.340	No
668	45.49	2.71	0.48	2.23	0.80	0.398	1.36	0.293	0.86	1.00	0.340	No
669	45.55	2.72	0.49	2.23	0.80	0.398	1.36	0.293	0.86	1.00	0.340	No
670	45.63	2.72	0.49	2.24	0.80	0.398	1.36	0.292	0.86	1.00	0.340	No
671	45.69	2.73	0.49	2.24	0.80	0.398	1.36	0.292	0.86	1.00	0.340	No
672	45.78	2.73	0.49	2.24	0.80	0.397	1.36	0.292	0.86	1.00	0.340	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	45.84	2.74	0.49	2.24	0.80	0.397	1.36	0.292	0.86	1.00	0.340	No
674	45.93	2.74	0.50	2.25	0.79	0.397	1.36	0.292	0.86	1.00	0.339	No
675	46.02	2.75	0.50	2.25	0.79	0.397	1.36	0.292	0.86	1.00	2.000	Yes
676	46.08	2.75	0.50	2.25	0.79	0.397	1.36	0.292	0.86	1.00	2.000	Yes
677	46.16	2.76	0.50	2.25	0.79	0.397	1.36	0.292	0.86	1.00	2.000	Yes
678	46.24	2.76	0.51	2.26	0.79	0.397	1.36	0.292	0.86	1.00	2.000	Yes
679	46.31	2.77	0.51	2.26	0.79	0.397	1.36	0.292	0.86	1.00	2.000	Yes
680	46.41	2.77	0.51	2.26	0.79	0.396	1.36	0.291	0.86	1.00	2.000	Yes
681	46.48	2.78	0.51	2.26	0.79	0.396	1.36	0.291	0.86	1.00	2.000	Yes
682	46.56	2.78	0.52	2.27	0.79	0.396	1.36	0.291	0.86	1.00	2.000	Yes
683	46.65	2.79	0.52	2.27	0.79	0.396	1.36	0.291	0.86	1.00	2.000	Yes
684	46.75	2.79	0.52	2.27	0.79	0.396	1.36	0.291	0.86	1.00	2.000	Yes
685	46.84	2.80	0.53	2.27	0.78	0.396	1.36	0.291	0.86	1.00	2.000	Yes
686	46.94	2.81	0.53	2.28	0.78	0.396	1.36	0.291	0.86	1.00	0.339	No
687	47.02	2.81	0.53	2.28	0.78	0.395	1.36	0.291	0.86	1.00	0.339	No
688	47.08	2.81	0.53	2.28	0.78	0.395	1.36	0.291	0.86	1.00	0.339	No
689	47.12	2.82	0.53	2.28	0.78	0.395	1.36	0.291	0.86	1.00	0.339	No
690	47.16	2.82	0.54	2.28	0.78	0.395	1.36	0.291	0.86	1.00	0.339	No
691	47.21	2.82	0.54	2.28	0.78	0.395	1.36	0.291	0.86	1.00	0.339	No
692	47.27	2.82	0.54	2.29	0.78	0.395	1.36	0.290	0.86	1.00	0.339	No
693	47.35	2.83	0.54	2.29	0.78	0.395	1.36	0.290	0.86	1.00	0.339	No
694	47.40	2.83	0.54	2.29	0.78	0.395	1.36	0.290	0.86	1.00	0.339	No
695	47.50	2.84	0.55	2.29	0.78	0.395	1.36	0.290	0.86	1.00	0.339	No
696	47.55	2.84	0.55	2.29	0.78	0.395	1.36	0.290	0.86	1.00	0.339	No
697	47.61	2.84	0.55	2.29	0.78	0.394	1.36	0.290	0.86	1.00	0.339	No
698	47.69	2.85	0.55	2.30	0.78	0.394	1.36	0.290	0.86	1.00	0.339	No
699	47.76	2.85	0.55	2.30	0.78	0.394	1.36	0.290	0.86	1.00	0.338	No
700	47.83	2.85	0.56	2.30	0.77	0.394	1.36	0.290	0.86	1.00	0.338	No
701	47.93	2.86	0.56	2.30	0.77	0.394	1.36	0.290	0.86	1.00	0.338	No
702	48.02	2.87	0.56	2.30	0.77	0.394	1.36	0.290	0.86	1.00	0.338	No
703	48.09	2.87	0.56	2.30	0.77	0.394	1.36	0.289	0.86	1.00	0.338	No
704	48.18	2.87	0.57	2.31	0.77	0.394	1.36	0.289	0.86	1.00	0.338	No
705	48.27	2.88	0.57	2.31	0.77	0.393	1.36	0.289	0.86	1.00	0.338	No
706	48.37	2.88	0.57	2.31	0.77	0.393	1.36	0.289	0.86	1.00	0.338	No
707	48.46	2.89	0.58	2.31	0.77	0.393	1.36	0.289	0.86	1.00	0.338	No
708	48.52	2.89	0.58	2.31	0.77	0.393	1.36	0.289	0.86	1.00	0.338	No
709	48.60	2.90	0.58	2.32	0.77	0.393	1.36	0.289	0.85	1.00	0.338	No
710	48.70	2.90	0.58	2.32	0.77	0.393	1.36	0.289	0.85	1.00	0.338	No
711	48.79	2.91	0.59	2.32	0.77	0.392	1.36	0.289	0.85	1.00	0.338	No
712	48.85	2.91	0.59	2.32	0.76	0.392	1.36	0.288	0.85	1.00	0.338	No
713	48.94	2.92	0.59	2.32	0.76	0.392	1.36	0.288	0.85	1.00	0.337	No
714	49.04	2.92	0.59	2.33	0.76	0.392	1.36	0.288	0.85	1.00	0.337	No
715	49.13	2.93	0.60	2.33	0.76	0.392	1.36	0.288	0.85	1.00	0.337	No
716	49.23	2.93	0.60	2.33	0.76	0.392	1.36	0.288	0.85	1.00	0.337	No
717	49.33	2.94	0.60	2.33	0.76	0.391	1.36	0.288	0.85	1.00	0.337	No
718	49.38	2.94	0.60	2.34	0.76	0.391	1.36	0.288	0.85	1.00	0.337	No
719	49.42	2.94	0.61	2.34	0.76	0.391	1.36	0.288	0.85	1.00	0.337	No
720	49.48	2.95	0.61	2.34	0.76	0.391	1.36	0.288	0.85	1.00	0.337	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	49.53	2.95	0.61	2.34	0.76	0.391	1.36	0.287	0.85	1.00	0.337	No
722	49.58	2.95	0.61	2.34	0.76	0.391	1.36	0.287	0.85	1.00	0.337	No
723	49.63	2.96	0.61	2.34	0.76	0.391	1.36	0.287	0.85	1.00	0.337	No
724	49.72	2.96	0.62	2.35	0.76	0.391	1.36	0.287	0.85	1.00	0.337	No
725	49.77	2.96	0.62	2.35	0.76	0.390	1.36	0.287	0.85	1.00	0.337	No
726	49.83	2.97	0.62	2.35	0.75	0.390	1.36	0.287	0.85	1.00	0.337	No
727	49.92	2.97	0.62	2.35	0.75	0.390	1.36	0.287	0.85	1.00	0.337	No
728	49.97	2.98	0.62	2.35	0.75	0.390	1.36	0.287	0.85	1.00	0.336	No
729	50.04	2.98	0.63	2.36	0.75	0.390	1.36	0.287	0.85	1.00	0.336	No
730	50.11	2.99	0.63	2.36	0.75	0.390	1.36	0.287	0.85	1.00	0.336	No
731	50.20	2.99	0.63	2.36	0.75	0.389	1.36	0.286	0.85	1.00	0.336	No
732	50.27	3.00	0.63	2.36	0.75	0.389	1.36	0.286	0.85	1.00	0.336	No
733	50.34	3.00	0.63	2.36	0.75	0.389	1.36	0.286	0.85	1.00	0.336	No
734	50.45	3.01	0.64	2.37	0.75	0.389	1.36	0.286	0.85	1.00	0.336	No
735	50.54	3.01	0.64	2.37	0.75	0.389	1.36	0.286	0.85	1.00	0.336	No
736	50.59	3.01	0.64	2.37	0.75	0.389	1.36	0.286	0.85	1.00	0.336	No
737	50.68	3.02	0.65	2.37	0.75	0.388	1.36	0.286	0.85	1.00	0.336	No
738	50.79	3.03	0.65	2.38	0.74	0.388	1.36	0.285	0.85	1.00	0.336	No
739	50.88	3.03	0.65	2.38	0.74	0.388	1.36	0.285	0.85	1.00	0.335	No
740	50.98	3.04	0.65	2.38	0.74	0.388	1.36	0.285	0.85	1.00	0.335	No
741	51.07	3.04	0.66	2.38	0.74	0.388	1.36	0.285	0.85	1.00	0.335	No
742	51.17	3.05	0.66	2.39	0.74	0.387	1.36	0.285	0.85	1.00	0.335	No
743	51.24	3.05	0.66	2.39	0.74	0.387	1.36	0.285	0.85	1.00	0.335	No
744	51.33	3.06	0.67	2.39	0.74	0.387	1.36	0.285	0.85	1.00	0.335	No
745	51.46	3.06	0.67	2.39	0.74	0.387	1.36	0.284	0.85	1.00	0.335	No
746	51.46	3.06	0.67	2.39	0.74	0.387	1.36	0.284	0.85	1.00	0.335	No
747	51.51	3.07	0.67	2.40	0.74	0.387	1.36	0.284	0.85	1.00	0.335	No
748	51.56	3.07	0.67	2.40	0.74	0.386	1.36	0.284	0.85	1.00	0.335	No
749	51.65	3.07	0.68	2.40	0.74	0.386	1.36	0.284	0.85	1.00	0.335	No
750	51.71	3.08	0.68	2.40	0.74	0.386	1.36	0.284	0.85	1.00	0.334	No
751	51.79	3.08	0.68	2.40	0.73	0.386	1.36	0.284	0.85	1.00	0.334	No
752	51.85	3.09	0.68	2.40	0.73	0.386	1.36	0.284	0.85	1.00	0.334	No
753	51.94	3.09	0.68	2.41	0.73	0.386	1.36	0.284	0.85	1.00	0.334	No
754	51.99	3.09	0.69	2.41	0.73	0.385	1.36	0.283	0.85	1.00	0.334	No
755	52.09	3.10	0.69	2.41	0.73	0.385	1.36	0.283	0.85	1.00	0.334	No
756	52.19	3.11	0.69	2.41	0.73	0.385	1.36	0.283	0.85	1.00	0.334	No
757	52.28	3.11	0.70	2.42	0.73	0.385	1.36	0.283	0.85	1.00	0.334	No
758	52.35	3.12	0.70	2.42	0.73	0.385	1.36	0.283	0.85	1.00	0.334	No
759	52.43	3.12	0.70	2.42	0.73	0.384	1.36	0.283	0.85	1.00	0.334	No
760	52.52	3.13	0.70	2.42	0.73	0.384	1.36	0.282	0.85	1.00	0.333	No
761	52.62	3.13	0.71	2.43	0.73	0.384	1.36	0.282	0.85	1.00	0.333	No
762	52.72	3.14	0.71	2.43	0.73	0.384	1.36	0.282	0.85	1.00	0.333	No
763	52.81	3.14	0.71	2.43	0.72	0.383	1.36	0.282	0.85	1.00	0.333	No
764	52.91	3.15	0.71	2.44	0.72	0.383	1.36	0.282	0.85	1.00	0.333	No
765	53.00	3.16	0.72	2.44	0.72	0.383	1.36	0.282	0.85	1.00	0.333	No
766	53.10	3.16	0.72	2.44	0.72	0.383	1.36	0.281	0.85	1.00	2.000	Yes
767	53.20	3.17	0.72	2.45	0.72	0.382	1.36	0.281	0.85	1.00	2.000	Yes
768	53.29	3.18	0.73	2.45	0.72	0.382	1.36	0.281	0.85	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	53.38	3.18	0.73	2.45	0.72	0.382	1.36	0.281	0.85	1.00	2.000	Yes
770	53.46	3.19	0.73	2.46	0.72	0.382	1.36	0.281	0.85	1.00	2.000	Yes
771	53.53	3.19	0.73	2.46	0.72	0.382	1.36	0.281	0.84	1.00	2.000	Yes
772	53.63	3.20	0.74	2.46	0.72	0.381	1.36	0.280	0.84	1.00	2.000	Yes
773	53.73	3.21	0.74	2.47	0.72	0.381	1.36	0.280	0.84	1.00	2.000	Yes
774	53.82	3.21	0.74	2.47	0.71	0.381	1.36	0.280	0.84	1.00	2.000	Yes
775	53.92	3.22	0.75	2.47	0.71	0.380	1.36	0.280	0.84	1.00	2.000	Yes
776	53.94	3.22	0.75	2.47	0.71	0.380	1.36	0.280	0.84	1.00	0.331	No
777	53.96	3.22	0.75	2.47	0.71	0.380	1.36	0.280	0.84	1.00	0.331	No
778	53.97	3.22	0.75	2.47	0.71	0.380	1.36	0.280	0.84	1.00	0.331	No
779	54.05	3.23	0.75	2.48	0.71	0.380	1.36	0.279	0.84	1.00	0.331	No
780	54.08	3.23	0.75	2.48	0.71	0.380	1.36	0.279	0.84	1.00	0.331	No
781	54.13	3.23	0.75	2.48	0.71	0.380	1.36	0.279	0.84	1.00	0.331	No
782	54.19	3.24	0.75	2.48	0.71	0.380	1.36	0.279	0.84	1.00	0.331	No
783	54.25	3.24	0.76	2.48	0.71	0.380	1.36	0.279	0.84	1.00	0.331	No
784	54.28	3.24	0.76	2.49	0.71	0.379	1.36	0.279	0.84	1.00	0.331	No
785	54.29	3.24	0.76	2.49	0.71	0.379	1.36	0.279	0.84	1.00	0.331	No
786	54.34	3.25	0.76	2.49	0.71	0.379	1.36	0.279	0.84	1.00	0.331	No
787	54.35	3.25	0.76	2.49	0.71	0.379	1.36	0.279	0.84	1.00	0.331	No
788	54.40	3.25	0.76	2.49	0.71	0.379	1.36	0.279	0.84	1.00	0.331	No
789	54.44	3.25	0.76	2.49	0.71	0.379	1.36	0.279	0.84	1.00	0.331	No
790	54.49	3.26	0.76	2.49	0.71	0.379	1.36	0.279	0.84	1.00	0.331	No
791	54.53	3.26	0.77	2.50	0.71	0.379	1.36	0.278	0.84	1.00	0.331	No
792	54.57	3.26	0.77	2.50	0.71	0.379	1.36	0.278	0.84	1.00	0.331	No
793	54.58	3.26	0.77	2.50	0.71	0.379	1.36	0.278	0.84	1.00	0.331	No
794	54.63	3.27	0.77	2.50	0.71	0.378	1.36	0.278	0.84	1.00	0.330	No
795	54.68	3.27	0.77	2.50	0.71	0.378	1.36	0.278	0.84	1.00	0.330	No
796	54.73	3.27	0.77	2.50	0.71	0.378	1.36	0.278	0.84	1.00	0.330	No
797	54.78	3.28	0.77	2.50	0.71	0.378	1.36	0.278	0.84	1.00	0.330	No
798	54.83	3.28	0.77	2.51	0.70	0.378	1.36	0.278	0.84	1.00	0.330	No
799	54.88	3.28	0.78	2.51	0.70	0.378	1.36	0.278	0.84	1.00	0.330	No
800	54.92	3.29	0.78	2.51	0.70	0.378	1.36	0.278	0.84	1.00	0.330	No
801	54.97	3.29	0.78	2.51	0.70	0.378	1.36	0.278	0.84	1.00	0.330	No
802	55.02	3.29	0.78	2.51	0.70	0.377	1.36	0.277	0.84	1.00	0.330	No
803	55.12	3.30	0.78	2.52	0.70	0.377	1.36	0.277	0.84	1.00	0.330	No
804	55.17	3.30	0.79	2.52	0.70	0.377	1.36	0.277	0.84	1.00	0.330	No
805	55.25	3.31	0.79	2.52	0.70	0.377	1.36	0.277	0.84	1.00	0.330	No
806	55.31	3.31	0.79	2.52	0.70	0.377	1.36	0.277	0.84	1.00	0.329	No
807	55.36	3.32	0.79	2.53	0.70	0.376	1.36	0.277	0.84	1.00	0.329	No
808	55.45	3.32	0.79	2.53	0.70	0.376	1.36	0.277	0.84	1.00	0.329	No
809	55.50	3.33	0.80	2.53	0.70	0.376	1.36	0.276	0.84	1.00	0.329	No
810	55.60	3.33	0.80	2.53	0.70	0.376	1.36	0.276	0.84	1.00	0.329	No
811	55.65	3.34	0.80	2.54	0.70	0.376	1.36	0.276	0.84	1.00	0.329	No
812	55.71	3.34	0.80	2.54	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No
813	55.75	3.34	0.80	2.54	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No
814	55.79	3.35	0.80	2.54	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No
815	55.84	3.35	0.81	2.54	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No
816	55.89	3.35	0.81	2.55	0.70	0.375	1.36	0.276	0.84	1.00	0.329	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	55.90	3.35	0.81	2.55	0.69	0.375	1.36	0.276	0.84	1.00	0.329	No
818	55.94	3.36	0.81	2.55	0.69	0.375	1.36	0.276	0.84	1.00	0.328	No
819	55.99	3.36	0.81	2.55	0.69	0.375	1.36	0.275	0.84	1.00	0.328	No
820	56.03	3.36	0.81	2.55	0.69	0.375	1.36	0.275	0.84	1.00	0.328	No
821	56.08	3.37	0.81	2.55	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
822	56.14	3.37	0.82	2.55	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
823	56.22	3.38	0.82	2.56	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
824	56.28	3.38	0.82	2.56	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
825	56.33	3.38	0.82	2.56	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
826	56.38	3.39	0.82	2.56	0.69	0.374	1.36	0.275	0.84	1.00	0.328	No
827	56.45	3.39	0.83	2.56	0.69	0.373	1.36	0.275	0.84	1.00	0.328	No
828	56.52	3.39	0.83	2.57	0.69	0.373	1.36	0.274	0.84	1.00	0.328	No
829	56.62	3.40	0.83	2.57	0.69	0.373	1.36	0.274	0.84	1.00	0.327	No
830	56.66	3.40	0.83	2.57	0.69	0.373	1.36	0.274	0.84	1.00	0.327	No
831	56.73	3.41	0.83	2.57	0.69	0.373	1.36	0.274	0.84	1.00	0.327	No
832	56.81	3.41	0.84	2.58	0.69	0.372	1.36	0.274	0.84	1.00	0.327	No
833	56.95	3.42	0.84	2.58	0.69	0.372	1.36	0.274	0.84	1.00	0.327	No
834	57.00	3.43	0.84	2.58	0.68	0.372	1.36	0.273	0.84	1.00	0.327	No
835	57.09	3.43	0.85	2.59	0.68	0.372	1.36	0.273	0.84	1.00	0.327	No
836	57.19	3.44	0.85	2.59	0.68	0.371	1.36	0.273	0.84	1.00	0.327	No
837	57.27	3.45	0.85	2.59	0.68	0.371	1.36	0.273	0.84	1.00	0.326	No
838	57.35	3.45	0.85	2.60	0.68	0.371	1.36	0.273	0.84	1.00	0.326	No
839	57.44	3.46	0.86	2.60	0.68	0.371	1.36	0.273	0.84	1.00	0.326	No
840	57.50	3.46	0.86	2.60	0.68	0.371	1.36	0.272	0.84	1.00	0.326	No
841	57.52	3.46	0.86	2.60	0.68	0.370	1.36	0.272	0.84	1.00	0.326	No
842	57.58	3.47	0.86	2.60	0.68	0.370	1.36	0.272	0.84	1.00	0.326	No
843	57.63	3.47	0.86	2.61	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
844	57.72	3.48	0.86	2.61	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
845	57.77	3.48	0.87	2.61	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
846	57.82	3.48	0.87	2.61	0.68	0.370	1.36	0.272	0.83	1.00	0.326	No
847	57.91	3.49	0.87	2.62	0.68	0.369	1.36	0.272	0.83	1.00	0.326	No
848	57.96	3.49	0.87	2.62	0.68	0.369	1.36	0.271	0.83	1.00	0.325	No
849	58.02	3.49	0.87	2.62	0.68	0.369	1.36	0.271	0.83	1.00	0.325	No
850	58.09	3.50	0.88	2.62	0.68	0.369	1.36	0.271	0.83	1.00	0.325	No
851	58.16	3.50	0.88	2.63	0.67	0.369	1.36	0.271	0.83	1.00	0.325	No
852	58.25	3.51	0.88	2.63	0.67	0.368	1.36	0.271	0.83	1.00	0.325	No
853	58.30	3.51	0.88	2.63	0.67	0.368	1.36	0.271	0.83	1.00	0.325	No
854	58.40	3.52	0.89	2.63	0.67	0.368	1.36	0.271	0.83	1.00	0.325	No
855	58.50	3.53	0.89	2.64	0.67	0.368	1.36	0.270	0.83	1.00	0.325	No
856	58.56	3.53	0.89	2.64	0.67	0.368	1.36	0.270	0.83	1.00	0.325	No
857	58.64	3.54	0.89	2.64	0.67	0.367	1.36	0.270	0.83	1.00	0.324	No
858	58.73	3.54	0.90	2.65	0.67	0.367	1.36	0.270	0.83	1.00	0.324	No
859	58.78	3.55	0.90	2.65	0.67	0.367	1.36	0.270	0.83	1.00	0.324	No
860	58.88	3.55	0.90	2.65	0.67	0.367	1.36	0.270	0.83	1.00	0.324	No
861	58.97	3.56	0.90	2.65	0.67	0.367	1.36	0.269	0.83	1.00	0.324	No
862	59.07	3.57	0.91	2.66	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
863	59.13	3.57	0.91	2.66	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No
864	59.23	3.58	0.91	2.66	0.67	0.366	1.36	0.269	0.83	1.00	0.324	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	59.31	3.58	0.91	2.67	0.66	0.366	1.36	0.269	0.83	1.00	0.323	No
866	59.38	3.59	0.92	2.67	0.66	0.365	1.36	0.269	0.83	1.00	0.323	No
867	59.41	3.59	0.92	2.67	0.66	0.365	1.36	0.269	0.83	1.00	0.323	No
868	59.46	3.59	0.92	2.67	0.66	0.365	1.36	0.269	0.83	1.00	0.323	No
869	59.51	3.59	0.92	2.67	0.66	0.365	1.36	0.268	0.83	1.00	0.323	No
870	59.57	3.60	0.92	2.68	0.66	0.365	1.36	0.268	0.83	1.00	0.323	No
871	59.66	3.60	0.93	2.68	0.66	0.365	1.36	0.268	0.83	1.00	0.323	No
872	59.75	3.61	0.93	2.68	0.66	0.365	1.36	0.268	0.83	1.00	0.323	No
873	59.80	3.61	0.93	2.68	0.66	0.364	1.36	0.268	0.83	1.00	0.323	No
874	59.85	3.62	0.93	2.69	0.66	0.364	1.36	0.268	0.83	1.00	0.323	No
875	59.91	3.62	0.93	2.69	0.66	0.364	1.36	0.268	0.83	1.00	0.323	No
876	59.99	3.63	0.94	2.69	0.66	0.364	1.36	0.268	0.83	1.00	0.322	No
877	60.05	3.63	0.94	2.69	0.66	0.364	1.36	0.267	0.83	1.00	0.322	No
878	60.09	3.63	0.94	2.69	0.66	0.364	1.36	0.267	0.83	1.00	0.322	No
879	60.14	3.64	0.94	2.70	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
880	60.19	3.64	0.94	2.70	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
881	60.22	3.64	0.94	2.70	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
882	60.28	3.65	0.94	2.70	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
883	60.33	3.65	0.95	2.70	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
884	60.38	3.65	0.95	2.71	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
885	60.42	3.66	0.95	2.71	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
886	60.48	3.66	0.95	2.71	0.66	0.363	1.36	0.267	0.83	1.00	0.322	No
887	60.57	3.67	0.95	2.71	0.65	0.362	1.36	0.266	0.83	1.00	0.322	No
888	60.66	3.67	0.96	2.72	0.65	0.362	1.36	0.266	0.83	1.00	0.321	No
889	60.68	3.67	0.96	2.72	0.65	0.362	1.36	0.266	0.83	1.00	0.321	No
890	60.69	3.67	0.96	2.72	0.65	0.362	1.36	0.266	0.83	1.00	0.321	No
891	60.74	3.68	0.96	2.72	0.65	0.362	1.36	0.266	0.83	1.00	0.321	No
892	60.79	3.68	0.96	2.72	0.65	0.362	1.36	0.266	0.83	1.00	0.321	No
893	60.84	3.68	0.96	2.72	0.65	0.362	1.36	0.266	0.83	1.00	0.321	No
894	60.89	3.69	0.96	2.72	0.65	0.362	1.36	0.266	0.83	1.00	0.321	No
895	60.98	3.69	0.97	2.73	0.65	0.361	1.36	0.266	0.83	1.00	0.321	No
896	61.03	3.69	0.97	2.73	0.65	0.361	1.36	0.266	0.83	1.00	0.321	No
897	61.08	3.70	0.97	2.73	0.65	0.361	1.36	0.265	0.83	1.00	0.321	No
898	61.18	3.70	0.97	2.73	0.65	0.361	1.36	0.265	0.83	1.00	0.321	No
899	61.23	3.71	0.97	2.73	0.65	0.361	1.36	0.265	0.83	1.00	0.321	No
900	61.31	3.71	0.98	2.74	0.65	0.361	1.36	0.265	0.83	1.00	0.321	No
901	61.42	3.72	0.98	2.74	0.65	0.360	1.36	0.265	0.83	1.00	0.320	No
902	61.47	3.72	0.98	2.74	0.65	0.360	1.36	0.265	0.83	1.00	0.320	No
903	61.51	3.73	0.98	2.74	0.65	0.360	1.36	0.265	0.83	1.00	0.320	No
904	61.54	3.73	0.98	2.74	0.65	0.360	1.36	0.265	0.83	1.00	0.320	No
905	61.57	3.73	0.98	2.74	0.65	0.360	1.36	0.265	0.83	1.00	0.320	No
906	61.58	3.73	0.99	2.75	0.65	0.360	1.36	0.265	0.83	1.00	0.320	No
907	61.61	3.73	0.99	2.75	0.65	0.360	1.36	0.265	0.83	1.00	0.320	No
908	61.63	3.73	0.99	2.75	0.65	0.360	1.36	0.265	0.83	1.00	0.320	No
909	61.63	3.73	0.99	2.75	0.65	0.360	1.36	0.264	0.83	1.00	0.320	No
910	61.66	3.74	0.99	2.75	0.65	0.360	1.36	0.264	0.83	1.00	0.320	No
911	61.67	3.74	0.99	2.75	0.65	0.360	1.36	0.264	0.83	1.00	0.320	No
912	61.70	3.74	0.99	2.75	0.65	0.360	1.36	0.264	0.83	1.00	0.320	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	61.71	3.74	0.99	2.75	0.65	0.360	1.36	0.264	0.83	1.00	0.320	No
914	61.76	3.74	0.99	2.75	0.65	0.359	1.36	0.264	0.83	1.00	0.320	No
915	61.80	3.75	0.99	2.75	0.65	0.359	1.36	0.264	0.83	1.00	0.320	No
916	61.84	3.75	0.99	2.75	0.64	0.359	1.36	0.264	0.83	1.00	0.320	No
917	61.86	3.75	0.99	2.75	0.64	0.359	1.36	0.264	0.83	1.00	0.320	No
918	61.93	3.75	1.00	2.76	0.64	0.359	1.36	0.264	0.83	1.00	0.320	No
919	61.98	3.76	1.00	2.76	0.64	0.359	1.36	0.264	0.83	1.00	0.320	No
920	62.04	3.76	1.00	2.76	0.64	0.359	1.36	0.264	0.83	1.00	0.320	No
921	62.09	3.76	1.00	2.76	0.64	0.359	1.36	0.264	0.83	1.00	0.319	No
922	62.14	3.77	1.00	2.76	0.64	0.359	1.36	0.264	0.83	1.00	0.319	No
923	62.19	3.77	1.00	2.77	0.64	0.358	1.36	0.264	0.83	1.00	0.319	No
924	62.24	3.77	1.01	2.77	0.64	0.358	1.36	0.263	0.83	1.00	0.319	No
925	62.26	3.77	1.01	2.77	0.64	0.358	1.36	0.263	0.83	1.00	0.319	No
926	62.29	3.78	1.01	2.77	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
927	62.38	3.78	1.01	2.77	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
928	62.44	3.79	1.01	2.77	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
929	62.46	3.79	1.01	2.78	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
930	62.47	3.79	1.01	2.78	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
931	62.51	3.79	1.01	2.78	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
932	62.56	3.79	1.02	2.78	0.64	0.358	1.36	0.263	0.82	1.00	0.319	No
933	62.60	3.80	1.02	2.78	0.64	0.357	1.36	0.263	0.82	1.00	0.319	No
934	62.65	3.80	1.02	2.78	0.64	0.357	1.36	0.263	0.82	1.00	0.319	No
935	62.70	3.80	1.02	2.78	0.64	0.357	1.36	0.263	0.82	1.00	0.319	No
936	62.75	3.81	1.02	2.79	0.64	0.357	1.36	0.263	0.82	1.00	0.319	No
937	62.80	3.81	1.02	2.79	0.64	0.357	1.36	0.262	0.82	1.00	0.319	No
938	62.85	3.81	1.02	2.79	0.64	0.357	1.36	0.262	0.82	1.00	0.318	No
939	62.89	3.82	1.03	2.79	0.64	0.357	1.36	0.262	0.82	1.00	0.318	No
940	62.97	3.82	1.03	2.79	0.64	0.357	1.36	0.262	0.82	1.00	0.318	No
941	63.04	3.83	1.03	2.80	0.64	0.356	1.36	0.262	0.82	1.00	0.318	No
942	63.09	3.83	1.03	2.80	0.64	0.356	1.36	0.262	0.82	1.00	0.318	No
943	63.13	3.83	1.03	2.80	0.64	0.356	1.36	0.262	0.82	1.00	0.318	No
944	63.19	3.84	1.04	2.80	0.63	0.356	1.36	0.262	0.82	1.00	0.318	No
945	63.23	3.84	1.04	2.80	0.63	0.356	1.36	0.262	0.82	1.00	0.318	No
946	63.28	3.84	1.04	2.81	0.63	0.356	1.36	0.262	0.82	1.00	0.318	No
947	63.32	3.85	1.04	2.81	0.63	0.356	1.36	0.261	0.82	1.00	0.318	No
948	63.38	3.85	1.04	2.81	0.63	0.356	1.36	0.261	0.82	1.00	0.318	No
949	63.44	3.85	1.04	2.81	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No
950	63.52	3.86	1.05	2.81	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No
951	63.57	3.86	1.05	2.82	0.63	0.355	1.36	0.261	0.82	1.00	0.318	No
952	63.66	3.87	1.05	2.82	0.63	0.355	1.36	0.261	0.82	1.00	0.317	No
953	63.73	3.87	1.05	2.82	0.63	0.355	1.36	0.261	0.82	1.00	0.317	No
954	63.76	3.88	1.05	2.82	0.63	0.355	1.36	0.261	0.82	1.00	0.317	No
955	63.76	3.88	1.05	2.82	0.63	0.355	1.36	0.261	0.82	1.00	0.317	No
956	63.78	3.88	1.05	2.82	0.63	0.355	1.36	0.261	0.82	1.00	0.317	No
957	63.81	3.88	1.05	2.82	0.63	0.355	1.36	0.261	0.82	1.00	0.317	No
958	63.85	3.88	1.06	2.83	0.63	0.354	1.36	0.261	0.82	1.00	0.317	No
959	63.86	3.88	1.06	2.83	0.63	0.354	1.36	0.261	0.82	1.00	0.317	No
960	63.91	3.89	1.06	2.83	0.63	0.354	1.36	0.260	0.82	1.00	0.317	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
961	63.94	3.89	1.06	2.83	0.63	0.354	1.36	0.260	0.82	1.00	0.317	No
962	63.95	3.89	1.06	2.83	0.63	0.354	1.36	0.260	0.82	1.00	0.317	No
963	64.00	3.89	1.06	2.83	0.63	0.354	1.36	0.260	0.82	1.00	0.317	No
964	64.02	3.89	1.06	2.83	0.63	0.354	1.36	0.260	0.82	1.00	0.317	No
965	64.05	3.90	1.06	2.83	0.63	0.354	1.36	0.260	0.82	1.00	0.317	No
966	64.09	3.90	1.06	2.83	0.63	0.354	1.36	0.260	0.82	1.00	0.317	No
967	64.11	3.90	1.06	2.84	0.63	0.354	1.36	0.260	0.82	1.00	0.317	No
968	64.15	3.90	1.07	2.84	0.63	0.354	1.36	0.260	0.82	1.00	0.317	No
969	64.20	3.91	1.07	2.84	0.63	0.354	1.36	0.260	0.82	1.00	0.317	No
970	64.25	3.91	1.07	2.84	0.63	0.353	1.36	0.260	0.82	1.00	0.317	No
971	64.29	3.91	1.07	2.84	0.63	0.353	1.36	0.260	0.82	1.00	0.317	No
972	64.34	3.92	1.07	2.84	0.63	0.353	1.36	0.260	0.82	1.00	0.317	No
973	64.43	3.92	1.07	2.85	0.63	0.353	1.36	0.260	0.82	1.00	0.316	No
974	64.48	3.92	1.08	2.85	0.63	0.353	1.36	0.259	0.82	1.00	0.316	No
975	64.53	3.93	1.08	2.85	0.63	0.353	1.36	0.259	0.82	1.00	0.316	No
976	64.58	3.93	1.08	2.85	0.62	0.353	1.36	0.259	0.82	1.00	0.316	No
977	64.63	3.93	1.08	2.85	0.62	0.353	1.36	0.259	0.82	1.00	0.316	No
978	64.68	3.94	1.08	2.86	0.62	0.352	1.36	0.259	0.82	1.00	0.316	No
979	64.73	3.94	1.08	2.86	0.62	0.352	1.36	0.259	0.82	1.00	0.316	No
980	64.77	3.94	1.08	2.86	0.62	0.352	1.36	0.259	0.82	1.00	0.316	No
981	64.82	3.95	1.09	2.86	0.62	0.352	1.36	0.259	0.82	1.00	0.316	No
982	64.87	3.95	1.09	2.86	0.62	0.352	1.36	0.259	0.82	1.00	0.316	No
983	64.89	3.95	1.09	2.86	0.62	0.352	1.36	0.259	0.82	1.00	0.316	No
984	64.93	3.95	1.09	2.86	0.62	0.352	1.36	0.259	0.82	1.00	0.316	No
985	64.94	3.96	1.09	2.87	0.62	0.352	1.36	0.259	0.82	1.00	0.316	No
986	64.98	3.96	1.09	2.87	0.62	0.352	1.36	0.259	0.82	1.00	0.316	No
987	64.99	3.96	1.09	2.87	0.62	0.352	1.36	0.259	0.82	1.00	0.316	No
988	65.03	3.96	1.09	2.87	0.62	0.352	1.36	0.259	0.82	1.00	0.316	No
989	65.08	3.96	1.09	2.87	0.62	0.352	1.36	0.258	0.82	1.00	0.316	No
990	65.13	3.97	1.10	2.87	0.62	0.351	1.36	0.258	0.82	1.00	0.316	No
991	65.17	3.97	1.10	2.87	0.62	0.351	1.36	0.258	0.82	1.00	0.315	No
992	65.22	3.97	1.10	2.88	0.62	0.351	1.36	0.258	0.82	1.00	0.315	No
993	65.23	3.98	1.10	2.88	0.62	0.351	1.36	0.258	0.82	1.00	0.315	No
994	65.28	3.98	1.10	2.88	0.62	0.351	1.36	0.258	0.82	1.00	0.315	No
995	65.32	3.98	1.10	2.88	0.62	0.351	1.36	0.258	0.82	1.00	0.315	No
996	65.37	3.98	1.10	2.88	0.62	0.351	1.36	0.258	0.82	1.00	0.315	No
997	65.42	3.99	1.10	2.88	0.62	0.351	1.36	0.258	0.82	1.00	0.315	No
998	65.47	3.99	1.11	2.88	0.62	0.351	1.36	0.258	0.82	1.00	0.315	No
999	65.48	3.99	1.11	2.88	0.62	0.351	1.36	0.258	0.82	1.00	0.315	No
1000	65.49	3.99	1.11	2.89	0.62	0.351	1.36	0.258	0.82	1.00	0.315	No
1001	65.52	3.99	1.11	2.89	0.62	0.351	1.36	0.258	0.82	1.00	0.315	No
1002	65.57	4.00	1.11	2.89	0.62	0.350	1.36	0.258	0.82	1.00	0.315	No
1003	65.62	4.00	1.11	2.89	0.62	0.350	1.36	0.258	0.82	1.00	0.315	No
1004	65.67	4.00	1.11	2.89	0.62	0.350	1.36	0.258	0.82	1.00	0.315	No
1005	65.69	4.00	1.11	2.89	0.62	0.350	1.36	0.258	0.82	1.00	0.315	No
1006	65.72	4.01	1.11	2.89	0.62	0.350	1.36	0.258	0.82	1.00	0.315	No
1007	65.77	4.01	1.12	2.89	0.62	0.350	1.36	0.257	0.82	1.00	0.315	No
1008	65.82	4.01	1.12	2.89	0.62	0.350	1.36	0.257	0.82	1.00	0.315	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1009	65.86	4.01	1.12	2.89	0.62	0.350	1.36	0.257	0.82	1.00	0.315	No
1010	65.86	4.01	1.12	2.89	0.62	0.350	1.36	0.257	0.82	1.00	0.315	No
1011	65.91	4.01	1.12	2.89	0.62	0.350	1.36	0.257	0.82	1.00	0.315	No
1012	65.96	4.02	1.12	2.89	0.62	0.350	1.36	0.257	0.82	1.00	0.315	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
σ_v: Total overburden pressure at test point (tsf)
u_0: Water pressure at test point (tsf)
σ_v': Effective overburden pressure based on GWT during earthquake (tsf)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.01	-0.03	N/A	-11.45	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
2	0.04	-0.03	N/A	-18.30	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
3	0.08	-0.07	N/A	-13.93	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
4	0.10	-0.03	N/A	-40.02	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
5	0.13	-0.03	N/A	-55.83	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
6	0.18	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
7	0.22	0.00	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
8	0.27	0.81	4.01	9.28	1.00	1.28	50.14	63.98	4.000	No	Yes	2.00
9	0.33	2.77	3.31	3.21	1.00	4.42	15.47	68.30	4.000	No	Yes	2.00
10	0.36	5.16	2.95	1.83	1.00	8.26	7.99	66.07	4.000	Yes	Yes	2.00
11	0.37	7.12	2.76	1.34	0.84	11.41	5.40	61.61	4.000	Yes	Yes	2.00
12	0.38	8.20	2.69	1.21	0.81	13.14	4.58	60.15	4.000	Yes	Yes	2.00
13	0.42	9.38	2.63	1.15	0.80	15.03	3.98	59.88	4.000	Yes	Yes	2.00
14	0.44	10.59	2.58	1.15	0.78	16.98	3.58	60.79	4.000	Yes	No	2.00
15	0.47	12.18	2.52	1.09	0.76	19.53	3.09	60.26	4.000	Yes	No	2.00
16	0.47	14.24	2.44	1.01	0.74	22.83	2.61	59.51	4.000	Yes	No	2.00
17	0.52	17.00	2.35	0.91	0.71	27.27	2.14	58.39	4.000	Yes	No	2.00
18	0.56	20.48	2.26	0.82	0.69	32.85	1.78	58.60	4.000	Yes	No	2.00
19	0.58	24.93	2.16	0.72	0.66	40.00	1.52	60.77	4.000	Yes	No	2.00
20	0.61	30.70	2.05	0.62	0.62	49.27	1.35	66.61	4.000	Yes	No	2.00
21	0.66	36.94	1.95	0.54	0.59	59.30	1.27	75.22	4.000	Yes	No	2.00
22	0.76	40.79	1.89	0.50	0.58	65.47	1.23	80.72	4.000	Yes	No	2.00
23	0.80	38.66	1.93	0.54	0.59	62.05	1.25	77.85	4.000	No	No	2.00
24	0.81	35.49	1.98	0.58	0.60	56.95	1.29	73.41	4.000	No	No	2.00
25	0.85	32.42	2.03	0.63	0.62	52.02	1.33	69.37	4.000	No	No	2.00
26	0.86	32.79	2.03	0.63	0.62	52.62	1.33	69.99	4.000	No	No	2.00
27	0.90	32.22	2.05	0.69	0.62	51.69	1.35	70.01	4.000	No	No	2.00
28	0.95	31.82	2.07	0.73	0.63	51.04	1.38	70.34	4.000	No	No	2.00
29	1.00	30.53	2.06	0.67	0.63	48.97	1.37	67.09	4.000	No	No	2.00
30	1.05	28.88	2.04	0.54	0.62	46.31	1.34	62.22	4.000	No	No	2.00
31	1.14	26.55	2.01	0.38	0.61	42.56	1.00	42.56	4.000	No	No	2.00
32	1.24	24.29	2.04	0.37	0.62	38.92	1.00	38.92	4.000	No	No	2.00
33	1.31	20.51	2.14	0.44	0.65	32.85	1.00	32.85	4.000	No	No	2.00
34	1.36	17.93	2.22	0.53	0.67	28.70	1.67	48.03	4.000	No	No	2.00
35	1.37	17.77	2.23	0.55	0.68	28.44	1.71	48.50	4.000	No	No	2.00
36	1.39	18.54	2.21	0.53	0.67	29.68	1.64	48.64	4.000	No	No	2.00
37	1.43	19.03	2.19	0.52	0.67	30.46	1.60	48.73	4.000	No	No	2.00
38	1.44	18.05	2.23	0.54	0.68	28.88	1.68	48.54	4.000	No	No	2.00
39	1.49	18.35	2.22	0.55	0.67	29.36	1.67	49.05	4.000	No	No	2.00
40	1.53	18.89	2.22	0.58	0.67	30.23	1.66	50.30	4.000	No	No	2.00
41	1.58	19.67	2.22	0.62	0.67	31.47	1.66	52.29	4.000	No	No	2.00
42	1.63	20.62	2.22	0.68	0.67	32.99	1.66	54.77	4.000	No	No	2.00
43	1.68	21.70	2.21	0.74	0.67	34.72	1.65	57.36	4.000	No	No	2.00
44	1.72	23.31	2.20	0.77	0.67	37.31	1.61	60.04	4.000	No	No	2.00
45	1.77	25.48	2.17	0.79	0.66	40.78	1.54	62.93	4.000	No	No	2.00
46	1.82	28.31	2.13	0.78	0.65	45.33	1.46	66.36	4.000	No	No	2.00
47	1.86	31.52	2.08	0.77	0.63	50.48	1.40	70.45	4.000	No	No	2.00
48	1.92	35.09	2.03	0.73	0.62	56.22	1.34	75.14	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	1.97	38.67	1.98	0.69	0.60	61.96	1.29	80.21	4.000	No	No	2.00
50	2.01	41.61	1.95	0.68	0.59	66.68	1.27	84.88	4.000	No	No	2.00
51	2.09	43.22	1.94	0.68	0.59	69.27	1.26	87.55	4.000	No	No	2.00
52	2.16	43.05	1.95	0.70	0.59	68.99	1.27	87.53	4.000	No	No	2.00
53	2.20	41.47	1.96	0.71	0.60	66.43	1.28	85.02	4.000	No	No	2.00
54	2.25	39.85	1.98	0.71	0.60	63.83	1.29	82.39	4.000	No	No	2.00
55	2.31	38.60	1.99	0.69	0.60	61.82	1.30	80.09	4.000	No	No	2.00
56	2.37	37.79	1.98	0.66	0.60	60.52	1.29	78.32	4.000	No	No	2.00
57	2.40	36.88	1.99	0.64	0.60	59.05	1.30	76.51	4.000	No	No	2.00
58	2.46	35.97	1.98	0.61	0.60	57.57	1.29	74.55	4.000	No	No	2.00
59	2.54	35.36	1.97	0.57	0.60	56.59	1.29	72.87	4.000	No	No	2.00
60	2.59	34.69	1.96	0.50	0.59	55.51	1.00	55.51	4.000	No	No	2.00
61	2.69	34.25	1.94	0.45	0.59	54.80	1.00	54.80	4.000	No	No	2.00
62	2.74	33.95	1.92	0.40	0.58	54.31	1.00	54.31	4.000	No	No	2.00
63	2.83	33.88	1.92	0.39	0.58	54.19	1.00	54.19	4.000	No	No	2.00
64	2.88	34.35	1.91	0.38	0.58	54.94	1.00	54.94	4.000	No	No	2.00
65	2.98	35.70	1.89	0.37	0.57	57.10	1.00	57.10	4.000	No	No	2.00
66	3.03	38.57	1.85	0.36	0.56	61.71	1.00	61.71	4.000	No	No	2.00
67	3.12	42.31	1.82	0.38	0.55	67.72	1.00	67.72	4.000	No	No	2.00
68	3.21	46.83	1.79	0.40	0.55	74.97	1.00	74.97	4.000	No	No	2.00
69	3.27	51.66	1.76	0.41	0.54	82.72	1.00	82.72	4.000	No	No	2.00
70	3.34	57.05	1.72	0.40	0.52	91.38	1.00	91.38	4.000	No	No	2.00
71	3.41	61.91	1.69	0.40	0.51	99.18	1.00	99.18	4.000	No	No	2.00
72	3.51	64.20	1.68	0.41	0.51	102.85	1.00	102.85	4.000	No	No	2.00
73	3.55	63.63	1.70	0.44	0.52	101.93	1.00	101.93	4.000	No	No	2.00
74	3.65	62.42	1.72	0.46	0.52	99.97	1.00	99.97	4.000	No	No	2.00
75	3.75	61.71	1.73	0.47	0.53	98.83	1.00	98.83	4.000	No	No	2.00
76	3.83	61.44	1.73	0.47	0.53	98.39	1.00	98.39	4.000	No	No	2.00
77	3.94	61.11	1.73	0.47	0.53	97.84	1.00	97.84	4.000	No	No	2.00
78	4.04	60.30	1.73	0.47	0.53	96.53	1.00	96.53	4.000	No	No	2.00
79	4.13	60.63	1.75	0.50	0.53	97.06	1.08	104.72	4.000	No	No	2.00
80	4.24	61.68	1.74	0.50	0.53	98.73	1.00	98.73	4.000	No	No	2.00
81	4.38	65.15	1.68	0.42	0.51	104.30	1.00	104.30	4.000	No	No	2.00
82	4.50	68.93	1.62	0.35	0.50	110.36	1.00	110.36	4.000	No	No	2.00
83	4.62	74.13	1.57	0.32	0.50	118.70	1.00	118.70	4.000	No	No	2.00
84	4.71	77.89	1.57	0.35	0.50	124.73	1.00	124.73	4.000	No	No	2.00
85	4.75	80.93	1.57	0.37	0.50	129.61	1.00	129.61	4.000	No	No	2.00
86	4.84	82.11	1.58	0.39	0.50	131.50	1.00	131.50	4.000	No	No	2.00
87	4.89	82.93	1.58	0.40	0.50	132.82	1.00	132.82	4.000	No	No	2.00
88	4.94	82.93	1.58	0.40	0.50	132.82	1.00	132.82	4.000	No	No	2.00
89	4.98	81.72	1.59	0.41	0.50	130.87	1.00	130.87	4.000	No	No	2.00
90	5.07	80.10	1.60	0.41	0.50	128.25	1.00	128.25	4.000	No	No	2.00
91	5.13	78.48	1.61	0.42	0.50	125.65	1.00	125.65	4.000	No	No	2.00
92	5.17	76.79	1.61	0.41	0.50	122.93	1.00	122.93	4.000	No	No	2.00
93	5.27	74.77	1.62	0.41	0.50	119.67	1.00	119.67	4.000	No	No	2.00
94	5.32	72.75	1.63	0.40	0.50	116.42	1.00	116.42	4.000	No	No	2.00
95	5.42	70.86	1.64	0.40	0.50	113.37	1.00	113.37	4.000	No	No	2.00
96	5.46	69.34	1.64	0.39	0.50	110.93	1.00	110.93	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	5.56	68.02	1.65	0.39	0.50	108.80	1.00	108.80	4.000	No	No	2.00
98	5.61	66.87	1.66	0.39	0.50	106.96	1.00	106.96	4.000	No	No	2.00
99	5.71	65.86	1.66	0.40	0.51	105.32	1.00	105.32	4.000	No	No	2.00
100	5.78	64.92	1.67	0.40	0.51	103.80	1.00	103.80	4.000	No	No	2.00
101	5.85	63.84	1.68	0.41	0.51	102.06	1.00	102.06	4.000	No	No	2.00
102	5.95	62.83	1.69	0.42	0.52	100.42	1.00	100.42	4.000	No	No	2.00
103	6.00	62.32	1.71	0.44	0.52	99.61	1.00	99.61	4.000	No	No	2.00
104	6.09	62.93	1.66	0.36	0.51	100.57	1.00	100.57	4.000	No	No	2.00
105	6.14	64.75	1.60	0.29	0.50	103.50	1.00	103.50	4.000	No	No	2.00
106	6.24	67.52	1.53	0.21	0.50	107.94	1.00	107.94	4.000	No	No	2.00
107	6.30	70.42	1.54	0.24	0.50	112.60	1.00	112.60	4.000	No	No	2.00
108	6.38	71.40	1.56	0.28	0.50	114.16	1.00	114.16	4.000	No	No	2.00
109	6.46	69.58	1.60	0.32	0.50	111.22	1.00	111.22	4.000	No	No	2.00
110	6.50	68.43	1.62	0.35	0.50	109.38	1.00	109.38	4.000	No	No	2.00
111	6.56	68.84	1.63	0.36	0.50	110.02	1.00	110.02	4.000	No	No	2.00
112	6.63	71.30	1.61	0.36	0.50	113.98	1.00	113.98	4.000	No	No	2.00
113	6.68	72.51	1.61	0.37	0.50	115.92	1.00	115.92	4.000	No	No	2.00
114	6.76	73.49	1.61	0.37	0.50	117.34	1.00	117.34	4.000	No	No	2.00
115	6.82	74.54	1.60	0.37	0.50	118.51	1.00	118.51	4.000	No	No	2.00
116	6.88	76.19	1.59	0.36	0.50	120.59	1.00	120.59	4.000	No	No	2.00
117	6.96	78.38	1.58	0.35	0.50	123.33	1.00	123.33	4.000	No	No	2.00
118	7.03	80.54	1.56	0.34	0.50	126.09	1.00	126.09	4.000	No	No	2.00
119	7.11	82.06	1.55	0.34	0.50	127.75	1.00	127.75	4.000	No	No	2.00
120	7.16	83.04	1.55	0.34	0.50	128.83	1.00	128.83	4.000	No	No	2.00
121	7.26	83.82	1.55	0.34	0.50	129.11	1.00	129.11	4.000	No	No	2.00
122	7.31	84.43	1.56	0.35	0.50	129.55	1.00	129.55	4.000	No	No	2.00
123	7.40	84.63	1.56	0.35	0.50	129.06	1.00	129.06	4.000	No	No	2.00
124	7.45	84.52	1.56	0.35	0.50	128.43	1.00	128.43	4.000	No	No	2.00
125	7.54	83.95	1.57	0.35	0.50	126.75	1.00	126.75	4.000	No	No	2.00
126	7.60	82.84	1.58	0.36	0.50	124.58	1.00	124.58	4.000	No	No	2.00
127	7.68	81.22	1.59	0.36	0.50	121.42	1.00	121.42	4.000	No	No	2.00
128	7.74	79.70	1.60	0.36	0.50	118.70	1.00	118.70	4.000	No	No	2.00
129	7.83	78.55	1.61	0.37	0.50	116.27	1.00	116.27	4.000	No	No	2.00
130	7.90	78.35	1.61	0.37	0.50	115.47	1.00	115.47	4.000	No	No	2.00
131	7.98	79.10	1.62	0.38	0.50	115.95	1.00	115.95	4.000	No	No	2.00
132	8.05	80.62	1.62	0.39	0.50	117.66	1.00	117.66	4.000	No	No	2.00
133	8.12	81.69	1.62	0.40	0.50	118.66	1.00	118.66	4.000	No	No	2.00
134	8.19	81.66	1.62	0.41	0.50	118.08	1.00	118.08	4.000	No	No	2.00
135	8.27	80.48	1.64	0.42	0.50	115.81	1.00	115.81	4.000	No	No	2.00
136	8.36	79.13	1.65	0.42	0.50	113.39	1.00	113.39	4.000	No	No	2.00
137	8.41	78.35	1.61	0.34	0.50	111.75	1.00	111.75	4.000	No	No	2.00
138	8.50	78.42	1.57	0.27	0.50	111.21	1.00	111.21	4.000	No	No	2.00
139	8.60	78.79	1.54	0.23	0.50	111.10	1.00	111.10	4.000	No	No	2.00
140	8.70	78.76	1.56	0.26	0.50	110.43	1.00	110.43	4.000	No	No	2.00
141	8.74	70.97	1.64	0.31	0.50	99.16	1.00	99.16	4.000	No	No	2.00
142	8.78	65.57	1.68	0.35	0.51	92.36	1.00	92.36	4.000	No	No	2.00
143	8.81	63.58	1.71	0.37	0.52	89.84	1.00	89.84	4.000	No	No	2.00
144	8.86	69.75	1.66	0.34	0.51	97.38	1.00	97.38	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	8.91	73.77	1.64	0.34	0.50	102.14	1.00	102.14	4.000	No	No	2.00
146	8.94	74.34	1.64	0.35	0.50	102.81	1.00	102.81	4.000	No	No	2.00
147	9.02	73.80	1.66	0.36	0.51	101.95	1.00	101.95	4.000	No	No	2.00
148	9.10	72.52	1.68	0.39	0.51	100.12	1.00	100.12	4.000	No	No	2.00
149	9.17	71.17	1.69	0.40	0.52	98.18	1.00	98.18	4.000	No	No	2.00
150	9.22	69.95	1.70	0.41	0.52	96.47	1.00	96.47	4.000	No	No	2.00
151	9.31	69.01	1.71	0.42	0.52	94.84	1.00	94.84	4.000	No	No	2.00
152	9.37	68.50	1.72	0.42	0.52	93.92	1.00	93.92	4.000	No	No	2.00
153	9.42	68.60	1.72	0.42	0.52	93.81	1.00	93.81	4.000	No	No	2.00
154	9.52	69.18	1.72	0.41	0.52	94.01	1.00	94.01	4.000	No	No	2.00
155	9.60	70.19	1.71	0.41	0.52	94.84	1.00	94.84	4.000	No	No	2.00
156	9.66	71.54	1.70	0.41	0.52	96.20	1.00	96.20	4.000	No	No	2.00
157	9.74	73.13	1.69	0.40	0.52	97.75	1.00	97.75	4.000	No	No	2.00
158	9.81	74.58	1.69	0.40	0.51	99.20	1.00	99.20	4.000	No	No	2.00
159	9.89	75.79	1.68	0.40	0.51	100.34	1.00	100.34	4.000	No	No	2.00
160	9.98	77.04	1.68	0.41	0.51	101.50	1.00	101.50	4.000	No	No	2.00
161	10.03	78.79	1.68	0.42	0.51	103.47	1.00	103.47	4.000	No	No	2.00
162	10.13	81.26	1.67	0.42	0.51	106.04	1.00	106.04	4.000	No	No	2.00
163	10.23	84.06	1.66	0.42	0.51	108.97	1.00	108.97	4.000	No	No	2.00
164	10.32	86.45	1.65	0.42	0.50	111.33	1.00	111.33	4.000	No	No	2.00
165	10.38	88.11	1.65	0.42	0.50	112.97	1.00	112.97	4.000	No	No	2.00
166	10.47	88.68	1.65	0.41	0.50	113.17	1.00	113.17	4.000	No	No	2.00
167	10.57	88.44	1.65	0.41	0.50	112.36	1.00	112.36	4.000	No	No	2.00
168	10.66	87.94	1.61	0.34	0.50	111.05	1.00	111.05	4.000	No	No	2.00
169	10.76	87.67	1.57	0.27	0.50	110.18	1.00	110.18	4.000	No	No	2.00
170	10.85	88.00	1.53	0.22	0.50	110.11	1.00	110.11	4.000	No	No	2.00
171	10.92	88.54	1.55	0.24	0.50	110.44	1.00	110.44	4.000	No	No	2.00
172	11.00	85.17	1.58	0.27	0.50	105.80	1.00	105.80	4.000	No	No	2.00
173	11.07	82.17	1.61	0.29	0.50	101.74	1.00	101.74	4.000	No	No	2.00
174	11.10	80.21	1.63	0.30	0.50	99.18	1.00	99.18	4.000	No	No	2.00
175	11.15	82.81	1.62	0.30	0.50	102.16	1.00	102.16	4.000	No	No	2.00
176	11.19	85.41	1.61	0.31	0.50	105.18	1.00	105.18	4.000	No	No	2.00
177	11.24	87.43	1.61	0.32	0.50	107.45	1.00	107.45	4.000	No	No	2.00
178	11.29	89.66	1.61	0.33	0.50	109.95	1.00	109.95	4.000	No	No	2.00
179	11.34	92.29	1.60	0.34	0.50	112.96	1.00	112.96	4.000	No	No	2.00
180	11.40	94.89	1.60	0.35	0.50	115.81	1.00	115.81	4.000	No	No	2.00
181	11.47	96.81	1.60	0.36	0.50	117.83	1.00	117.83	4.000	No	No	2.00
182	11.53	97.72	1.60	0.37	0.50	118.60	1.00	118.60	4.000	No	No	2.00
183	11.58	98.23	1.60	0.37	0.50	118.97	1.00	118.97	4.000	No	No	2.00
184	11.65	98.70	1.61	0.38	0.50	119.16	1.00	119.16	4.000	No	No	2.00
185	11.72	99.17	1.61	0.38	0.50	119.34	1.00	119.34	4.000	No	No	2.00
186	11.77	99.00	1.61	0.39	0.50	118.88	1.00	118.88	4.000	No	No	2.00
187	11.82	98.36	1.62	0.39	0.50	117.83	1.00	117.83	4.000	No	No	2.00
188	11.88	97.25	1.64	0.42	0.50	116.19	1.00	116.19	4.000	No	No	2.00
189	11.97	96.10	1.65	0.43	0.50	114.49	1.00	114.49	4.000	No	No	2.00
190	12.02	94.75	1.65	0.43	0.50	112.75	1.00	112.75	4.000	No	No	2.00
191	12.06	93.54	1.65	0.40	0.50	110.95	1.00	110.95	4.000	No	No	2.00
192	12.11	93.03	1.65	0.40	0.50	110.11	1.00	110.11	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	12.21	92.63	1.65	0.39	0.50	109.15	1.00	109.15	4.000	No	No	2.00
194	12.25	92.93	1.64	0.38	0.50	109.21	1.00	109.21	4.000	No	No	2.00
195	12.30	93.00	1.64	0.38	0.50	109.05	1.00	109.05	4.000	No	No	2.00
196	12.31	93.44	1.63	0.37	0.50	109.51	1.00	109.51	4.000	No	No	2.00
197	12.32	93.64	1.63	0.37	0.50	109.72	1.00	109.72	4.000	No	No	2.00
198	12.35	94.21	1.62	0.36	0.50	110.25	1.00	110.25	4.000	No	No	2.00
199	12.40	95.26	1.61	0.35	0.50	111.26	1.00	111.26	4.000	No	No	2.00
200	12.45	96.78	1.60	0.33	0.50	112.82	1.00	112.82	4.000	No	No	2.00
201	12.52	98.43	1.60	0.33	0.50	114.40	1.00	114.40	4.000	No	No	2.00
202	12.56	100.32	1.59	0.34	0.50	116.43	1.00	116.43	4.000	No	No	2.00
203	12.62	102.04	1.59	0.35	0.50	118.16	1.00	118.16	4.000	No	No	2.00
204	12.65	103.69	1.56	0.31	0.50	119.90	1.00	119.90	4.000	No	No	2.00
205	12.71	105.14	1.53	0.26	0.50	121.32	1.00	121.32	4.000	No	No	2.00
206	12.76	107.34	1.48	0.22	0.50	123.61	1.00	123.61	4.000	No	No	2.00
207	12.83	110.34	1.48	0.23	0.50	126.74	1.00	126.74	4.000	No	No	2.00
208	12.88	114.29	1.50	0.26	0.50	131.03	1.00	131.03	4.000	No	No	2.00
209	12.93	118.94	1.50	0.30	0.50	136.14	1.00	136.14	4.000	No	No	2.00
210	12.98	121.44	1.52	0.33	0.50	138.73	1.00	138.73	4.000	No	No	2.00
211	13.03	123.77	1.52	0.33	0.50	141.10	1.00	141.10	4.000	No	No	2.00
212	13.04	120.16	1.54	0.36	0.50	136.93	1.00	136.93	4.000	No	No	2.00
213	13.07	122.72	1.54	0.38	0.50	139.66	1.00	139.66	4.000	No	No	2.00
214	13.13	125.66	1.55	0.40	0.50	142.70	1.00	142.70	4.000	No	No	2.00
215	13.17	134.36	1.53	0.40	0.50	152.37	1.00	152.37	4.000	No	No	2.00
216	13.22	137.87	1.53	0.42	0.50	156.08	1.00	156.08	4.000	No	No	2.00
217	13.27	140.13	1.54	0.44	0.50	158.31	1.00	158.31	4.000	No	No	2.00
218	13.32	141.11	1.54	0.46	0.50	159.12	1.00	159.12	4.000	No	No	2.00
219	13.37	141.28	1.55	0.47	0.50	159.00	1.00	159.00	4.000	No	No	2.00
220	13.41	140.67	1.55	0.47	0.50	158.02	1.00	158.02	4.000	No	No	2.00
221	13.46	139.05	1.56	0.48	0.50	155.85	1.00	155.85	4.000	No	No	2.00
222	13.51	137.63	1.57	0.48	0.50	153.98	1.00	153.98	4.000	No	No	2.00
223	13.56	135.98	1.58	0.49	0.50	151.81	1.00	151.81	4.000	No	No	2.00
224	13.60	134.29	1.59	0.51	0.50	149.65	1.00	149.65	4.000	No	No	2.00
225	13.66	132.81	1.60	0.52	0.50	147.65	1.00	147.65	4.000	No	No	2.00
226	13.75	131.80	1.60	0.51	0.50	145.98	1.00	145.98	4.000	No	No	2.00
227	13.80	131.19	1.60	0.51	0.50	145.02	1.00	145.02	4.000	No	No	2.00
228	13.89	130.75	1.61	0.51	0.50	144.01	1.00	144.01	4.000	No	No	2.00
229	13.94	129.81	1.61	0.52	0.50	142.69	1.00	142.69	4.000	No	No	2.00
230	13.99	128.19	1.63	0.54	0.50	140.62	1.00	140.62	4.000	No	No	2.00
231	14.09	125.39	1.65	0.57	0.50	137.21	1.00	137.21	4.000	No	No	2.00
232	14.14	122.28	1.68	0.61	0.51	133.79	1.00	133.79	4.000	No	No	2.00
233	14.23	119.38	1.70	0.64	0.52	130.35	1.00	130.35	4.000	No	No	2.00
234	14.28	117.19	1.68	0.58	0.51	127.54	1.00	127.54	4.000	No	No	2.00
235	14.38	116.43	1.66	0.51	0.50	125.95	1.00	125.95	4.000	No	No	2.00
236	14.42	115.35	1.63	0.45	0.50	124.40	1.00	124.40	4.000	No	No	2.00
237	14.52	115.79	1.63	0.45	0.50	124.40	1.00	124.40	4.000	No	No	2.00
238	14.57	116.75	1.64	0.47	0.50	125.23	1.00	125.23	4.000	No	No	2.00
239	14.67	117.53	1.64	0.48	0.50	125.60	1.00	125.60	4.000	No	No	2.00
240	14.68	117.83	1.64	0.49	0.50	125.93	1.00	125.93	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	14.70	116.41	1.65	0.50	0.50	124.39	1.00	124.39	4.000	No	No	2.00
242	14.75	116.58	1.66	0.50	0.50	124.38	1.00	124.38	4.000	No	No	2.00
243	14.80	116.18	1.66	0.51	0.51	123.80	1.00	123.80	4.000	No	No	2.00
244	14.89	116.21	1.67	0.52	0.51	123.45	1.00	123.45	4.000	No	No	2.00
245	14.94	114.76	1.68	0.53	0.51	121.75	1.00	121.75	4.000	No	No	2.00
246	15.04	111.83	1.69	0.54	0.52	118.29	1.00	118.29	4.000	No	No	2.00
247	15.13	107.24	1.71	0.55	0.52	113.18	1.01	114.51	4.000	No	No	2.00
248	15.21	101.74	1.74	0.56	0.53	107.19	1.06	113.68	4.000	No	No	2.00
249	15.28	95.87	1.76	0.57	0.54	100.87	1.10	111.36	4.000	No	No	2.00
250	15.38	90.00	1.79	0.58	0.54	94.46	1.14	107.63	4.000	No	No	2.00
251	15.47	83.86	1.82	0.58	0.55	87.79	1.17	102.77	4.000	No	No	2.00
252	15.57	77.55	1.85	0.59	0.56	80.97	1.20	97.12	4.000	No	No	2.00
253	15.67	70.76	1.89	0.60	0.57	73.71	1.23	90.52	4.000	No	No	2.00
254	15.77	63.91	1.93	0.61	0.59	66.40	1.26	83.47	4.000	No	No	2.00
255	15.86	57.27	1.98	0.63	0.60	59.33	1.29	76.63	4.000	No	No	2.00
256	15.96	51.73	2.03	0.67	0.62	53.45	1.34	71.45	4.000	No	No	2.00
257	16.05	47.31	2.09	0.73	0.63	48.75	1.40	68.25	4.000	No	No	2.00
258	16.15	43.60	2.15	0.86	0.65	44.83	1.51	67.79	4.000	No	No	2.00
259	16.25	41.11	2.20	0.97	0.67	42.13	1.63	68.47	4.000	No	No	2.00
260	16.31	39.86	2.23	1.04	0.68	40.76	1.71	69.57	4.000	No	No	2.00
261	16.39	39.72	2.23	1.02	0.68	40.48	1.70	68.78	4.000	No	No	2.00
262	16.48	40.50	2.21	0.96	0.67	41.08	1.65	67.59	4.000	No	No	2.00
263	16.59	43.06	2.17	0.86	0.66	43.47	1.53	66.70	4.000	No	No	2.00
264	16.68	47.95	2.09	0.73	0.64	48.20	1.40	67.68	4.000	No	No	2.00
265	16.76	53.89	2.01	0.61	0.61	53.96	1.31	70.90	4.000	No	No	2.00
266	16.86	58.72	1.95	0.54	0.59	58.53	1.27	74.31	4.000	No	No	2.00
267	16.92	61.25	1.92	0.51	0.58	60.90	1.25	76.25	4.000	No	No	2.00
268	17.02	61.65	1.92	0.50	0.58	61.10	1.25	76.36	4.000	No	No	2.00
269	17.11	61.14	1.94	0.53	0.59	60.41	1.26	76.12	4.000	No	No	2.00
270	17.22	60.40	1.96	0.58	0.60	59.48	1.28	75.94	4.000	Yes	No	2.00
271	17.35	58.51	2.04	0.78	0.62	57.44	1.34	77.19	4.000	Yes	No	2.00
272	17.45	53.15	2.18	1.20	0.66	52.07	1.57	81.76	4.000	Yes	No	2.00
273	17.55	43.40	2.38	1.91	0.72	42.36	2.26	95.58	4.000	Yes	No	2.00
274	17.61	33.92	2.57	2.79	0.78	32.93	3.48	114.42	4.000	Yes	No	2.00
275	17.64	27.41	2.70	3.46	0.82	26.45	4.70	124.38	4.000	Yes	Yes	2.00
276	17.70	24.84	2.75	3.68	0.83	23.84	5.27	125.58	4.000	Yes	Yes	2.00
277	17.75	23.12	2.79	3.84	0.84	22.09	5.71	126.01	4.000	Yes	Yes	2.00
278	17.80	22.04	2.82	4.00	0.85	20.96	6.07	127.17	4.000	Yes	Yes	2.00
279	17.85	21.57	2.85	4.36	0.86	20.45	6.49	132.79	4.000	Yes	Yes	2.00
280	17.94	24.37	2.80	4.19	0.85	23.10	5.83	134.72	4.000	No	Yes	2.00
281	17.99	29.74	2.70	3.80	0.82	28.29	4.75	134.51	4.000	No	Yes	2.00
282	18.09	36.42	2.60	3.34	0.79	34.65	3.76	130.35	4.000	No	Yes	2.00
283	18.15	38.34	2.58	3.31	0.78	36.42	3.61	131.44	4.000	No	No	2.00
284	18.23	36.08	2.63	3.58	0.80	34.09	3.99	135.89	4.000	No	Yes	2.00
285	18.33	27.03	2.80	4.68	0.85	25.22	5.88	148.20	4.000	No	Yes	2.00
286	18.43	18.43	3.01	6.17	1.00	16.85	8.99	151.54	4.000	No	Yes	2.00
287	18.52	11.28	3.27	8.30	1.00	9.87	14.46	142.66	4.000	No	Yes	2.00
288	18.59	9.25	3.30	7.06	1.00	7.88	15.23	120.07	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	18.72	8.44	3.27	5.49	1.00	7.05	14.48	102.14	4.000	No	Yes	2.00
290	18.81	7.87	3.26	4.64	1.00	6.47	14.17	91.69	4.000	No	Yes	2.00
291	18.87	7.73	3.27	4.61	1.00	6.32	14.34	90.62	4.000	No	Yes	2.00
292	18.95	7.94	3.28	5.10	1.00	6.48	14.76	95.67	4.000	No	Yes	2.00
293	19.05	8.95	3.24	5.23	1.00	7.39	13.77	101.75	4.000	No	Yes	2.00
294	19.14	11.32	3.12	4.53	1.00	9.56	10.96	104.74	4.000	No	Yes	2.00
295	19.22	15.43	2.92	3.38	0.89	13.37	7.56	101.14	4.000	Yes	Yes	2.00
296	19.29	23.29	2.67	2.31	0.81	20.64	4.44	91.70	4.000	Yes	Yes	2.00
297	19.38	36.79	2.41	1.58	0.73	33.12	2.43	80.52	4.000	Yes	No	2.00
298	19.44	54.77	2.21	1.24	0.67	49.78	1.63	81.04	4.000	Yes	No	2.00
299	19.53	73.63	2.06	1.07	0.63	67.13	1.37	92.11	4.000	Yes	No	2.00
300	19.62	89.35	1.99	1.02	0.60	81.50	1.30	105.61	4.000	Yes	No	2.00
301	19.69	100.62	1.95	1.03	0.59	91.73	1.27	116.28	4.000	Yes	No	2.00
302	19.79	106.79	1.94	1.07	0.59	97.11	1.26	122.62	4.000	No	No	2.00
303	19.86	108.17	1.96	1.16	0.60	98.11	1.28	125.15	4.000	No	No	2.00
304	19.97	105.91	1.99	1.25	0.60	95.65	1.30	124.06	4.000	No	No	2.00
305	20.07	101.09	2.02	1.32	0.61	90.89	1.33	120.48	4.000	No	No	2.00
306	20.16	94.14	2.06	1.40	0.63	84.23	1.37	115.28	4.000	No	No	2.00
307	20.26	84.49	2.07	1.27	0.63	75.23	1.38	103.79	4.000	Yes	No	2.00
308	20.34	72.68	2.10	1.18	0.64	64.34	1.43	91.71	4.000	Yes	No	2.00
309	20.43	59.83	2.16	1.11	0.66	52.55	1.52	80.02	4.000	Yes	No	2.00
310	20.50	47.95	2.33	1.55	0.71	41.63	2.03	84.51	4.000	Yes	No	2.00
311	20.60	37.70	2.50	2.17	0.76	32.23	3.01	96.91	4.000	Yes	No	2.00
312	20.62	30.48	2.66	2.88	0.81	25.73	4.28	110.02	4.000	Yes	Yes	2.00
313	20.63	28.08	2.72	3.22	0.82	23.58	4.89	115.31	4.000	Yes	Yes	2.00
314	20.68	27.74	2.74	3.38	0.83	23.22	5.10	118.43	4.000	Yes	Yes	2.00
315	20.73	27.64	2.76	3.60	0.83	23.06	5.32	122.67	4.000	Yes	Yes	2.00
316	20.82	25.48	2.82	4.04	0.85	21.06	6.08	128.12	4.000	Yes	Yes	2.00
317	20.87	23.45	2.87	4.37	0.87	19.23	6.78	130.45	4.000	Yes	Yes	2.00
318	20.91	21.57	2.91	4.48	0.88	17.54	7.32	128.42	4.000	Yes	Yes	2.00
319	20.96	19.58	2.95	4.54	1.00	15.59	7.98	124.40	4.000	Yes	Yes	2.00
320	21.05	17.59	3.00	4.73	1.00	13.84	8.82	122.12	4.000	No	Yes	2.00
321	21.11	16.98	3.02	4.74	1.00	13.29	9.07	120.49	4.000	No	Yes	2.00
322	21.17	17.11	3.01	4.72	1.00	13.36	9.02	120.44	4.000	No	Yes	2.00
323	21.25	21.23	2.88	3.84	0.87	17.01	6.86	116.62	4.000	Yes	Yes	2.00
324	21.30	31.25	2.64	2.71	0.80	25.68	4.13	106.03	4.000	Yes	Yes	2.00
325	21.37	48.56	2.39	1.90	0.72	40.77	2.31	94.37	4.000	Yes	No	2.00
326	21.45	68.84	2.20	1.51	0.67	58.49	1.62	94.86	4.000	Yes	No	2.00
327	21.49	87.80	2.09	1.36	0.64	75.10	1.41	105.59	4.000	Yes	No	2.00
328	21.58	103.45	2.02	1.30	0.62	88.68	1.33	117.80	4.000	Yes	No	2.00
329	21.64	115.70	1.98	1.28	0.60	99.28	1.29	128.46	4.000	Yes	No	2.00
330	21.69	124.50	1.96	1.29	0.60	106.86	1.28	136.49	4.000	Yes	No	2.00
331	21.78	130.41	1.95	1.31	0.59	111.69	1.27	142.03	4.000	No	No	2.00
332	21.83	133.78	1.96	1.36	0.59	114.42	1.27	145.79	4.000	No	No	2.00
333	21.89	135.43	1.97	1.42	0.60	115.57	1.28	148.03	4.000	No	No	2.00
334	21.98	136.01	1.98	1.49	0.60	115.67	1.29	149.32	4.000	No	No	2.00
335	22.03	135.90	1.99	1.55	0.61	115.31	1.30	150.06	4.000	No	No	2.00
336	22.12	134.89	2.01	1.60	0.61	114.06	1.31	149.60	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	22.22	133.20	2.02	1.63	0.61	112.20	1.32	148.31	4.000	No	No	2.00
338	22.26	130.88	2.03	1.65	0.62	110.01	1.33	146.45	4.000	No	No	2.00
339	22.36	128.38	2.04	1.67	0.62	107.52	1.34	144.21	4.000	No	No	2.00
340	22.41	125.79	2.05	1.70	0.62	105.07	1.36	142.38	4.000	No	No	2.00
341	22.51	123.53	2.04	1.63	0.62	102.88	1.35	138.65	4.000	No	No	2.00
342	22.60	121.33	2.03	1.54	0.62	100.82	1.34	134.71	4.000	No	No	2.00
343	22.70	119.34	2.01	1.41	0.61	98.95	1.32	130.43	4.000	No	No	2.00
344	22.75	116.88	2.02	1.40	0.61	96.72	1.32	127.90	4.000	No	No	2.00
345	22.84	109.32	2.05	1.47	0.62	89.92	1.36	122.31	4.000	No	No	2.00
346	22.89	107.14	2.06	1.48	0.63	87.93	1.37	120.57	4.000	No	No	2.00
347	22.90	104.88	2.07	1.49	0.63	85.98	1.38	118.82	4.000	No	No	2.00
348	22.94	110.11	2.04	1.39	0.62	90.42	1.34	121.26	4.000	No	No	2.00
349	23.00	112.36	2.02	1.34	0.61	92.21	1.32	122.07	4.000	No	No	2.00
350	23.08	118.94	1.98	1.24	0.60	97.70	1.29	126.15	4.000	No	No	2.00
351	23.13	127.04	1.94	1.16	0.59	104.57	1.26	131.91	4.000	No	No	2.00
352	23.20	134.05	1.90	1.10	0.58	110.43	1.24	136.83	4.000	No	No	2.00
353	23.27	137.05	1.89	1.07	0.57	112.81	1.23	138.66	4.000	No	No	2.00
354	23.33	135.57	1.89	1.05	0.57	111.40	1.23	136.90	4.000	No	No	2.00
355	23.42	131.55	1.89	1.03	0.58	107.76	1.23	132.83	4.000	No	No	2.00
356	23.48	126.94	1.90	1.01	0.58	103.73	1.24	128.30	4.000	No	No	2.00
357	23.57	123.16	1.91	1.00	0.58	100.30	1.24	124.68	4.000	No	No	2.00
358	23.61	121.20	1.92	1.01	0.58	98.52	1.25	122.97	4.000	No	No	2.00
359	23.66	121.50	1.92	1.02	0.58	98.62	1.25	123.25	4.000	No	No	2.00
360	23.73	124.04	1.92	1.03	0.58	100.52	1.25	125.44	4.000	No	No	2.00
361	23.80	127.95	1.91	1.04	0.58	103.59	1.24	128.73	4.000	No	No	2.00
362	23.85	131.96	1.90	1.05	0.58	106.79	1.24	132.25	4.000	No	No	2.00
363	23.94	134.80	1.90	1.06	0.58	108.87	1.24	134.50	4.000	No	No	2.00
364	24.00	135.88	1.90	1.07	0.58	109.59	1.24	135.41	4.000	No	No	2.00
365	24.09	135.37	1.90	1.07	0.58	108.86	1.24	134.81	4.000	No	No	2.00
366	24.16	133.34	1.91	1.09	0.58	106.93	1.24	133.09	4.000	No	No	2.00
367	24.24	130.04	1.89	0.97	0.57	104.25	1.23	128.02	4.000	No	No	2.00
368	24.33	125.79	1.86	0.85	0.57	100.75	1.21	122.05	4.000	No	No	2.00
369	24.43	121.10	1.84	0.74	0.56	96.90	1.19	115.53	4.000	No	No	2.00
370	24.52	114.28	1.88	0.80	0.57	90.85	1.23	111.31	4.000	No	No	2.00
371	24.58	108.90	1.92	0.85	0.58	86.13	1.25	107.54	4.000	No	No	2.00
372	24.59	104.52	1.95	0.89	0.59	82.40	1.27	104.41	4.000	No	No	2.00
373	24.63	104.21	1.95	0.90	0.59	82.05	1.27	104.24	4.000	No	No	2.00
374	24.68	103.45	1.96	0.94	0.60	81.24	1.28	103.96	4.000	No	No	2.00
375	24.77	102.47	1.98	0.98	0.60	80.14	1.29	103.52	4.000	No	No	2.00
376	24.82	100.31	2.01	1.05	0.61	78.15	1.31	102.59	4.000	No	No	2.00
377	24.92	97.85	2.03	1.11	0.62	75.83	1.34	101.32	4.000	No	No	2.00
378	25.01	95.22	2.06	1.17	0.63	73.42	1.36	100.09	4.000	No	No	2.00
379	25.06	92.38	2.08	1.22	0.63	70.94	1.39	98.75	4.000	No	No	2.00
380	25.16	89.48	2.10	1.27	0.64	68.36	1.42	97.29	4.000	No	No	2.00
381	25.25	86.51	2.13	1.31	0.65	65.75	1.46	95.92	4.000	No	No	2.00
382	25.30	83.55	2.15	1.35	0.65	63.24	1.50	94.77	4.000	No	No	2.00
383	25.41	80.44	2.17	1.40	0.66	60.52	1.55	93.81	4.000	Yes	No	2.00
384	25.49	77.27	2.20	1.47	0.67	57.80	1.61	93.24	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	25.55	73.97	2.23	1.55	0.68	55.02	1.70	93.42	4.000	Yes	No	2.00
386	25.64	70.59	2.27	1.65	0.69	52.13	1.81	94.24	4.000	Yes	No	2.00
387	25.70	67.02	2.31	1.78	0.70	49.15	1.95	95.94	4.000	Yes	No	2.00
388	25.79	63.24	2.35	1.91	0.71	46.00	2.13	97.75	4.000	Yes	No	2.00
389	25.89	58.92	2.40	2.05	0.73	42.45	2.35	99.94	4.000	Yes	No	2.00
390	25.94	54.26	2.45	2.20	0.74	38.75	2.63	101.97	4.000	Yes	No	2.00
391	26.02	49.37	2.50	2.32	0.76	34.89	2.95	102.81	4.000	Yes	No	2.00
392	26.12	45.05	2.54	2.37	0.77	31.51	3.23	101.92	4.000	Yes	No	2.00
393	26.17	40.83	2.57	2.37	0.78	28.31	3.52	99.58	4.000	Yes	No	2.00
394	26.28	37.02	2.61	2.37	0.79	25.37	3.84	97.30	4.000	Yes	Yes	2.00
395	26.36	33.31	2.65	2.33	0.80	22.57	4.17	94.10	4.000	Yes	Yes	2.00
396	26.45	29.43	2.70	2.37	0.82	19.65	4.69	92.22	4.000	Yes	Yes	2.00
397	26.50	24.94	2.78	2.55	0.84	16.31	5.63	91.86	4.000	Yes	Yes	2.00
398	26.61	20.15	2.91	3.01	0.88	12.75	7.37	93.95	4.000	Yes	Yes	2.00
399	26.70	15.97	3.07	3.75	1.00	9.43	10.10	95.23	4.000	No	Yes	2.00
400	26.77	12.97	3.21	4.62	1.00	7.45	12.95	96.46	4.000	No	Yes	2.00
401	26.85	11.85	3.26	4.83	1.00	6.70	14.12	94.58	4.000	No	Yes	2.00
402	26.94	11.45	3.27	4.67	1.00	6.41	14.29	91.60	4.000	No	Yes	2.00
403	27.04	11.95	3.22	4.13	1.00	6.71	13.15	88.25	4.000	No	Yes	2.00
404	27.14	12.22	3.20	3.92	1.00	6.86	12.68	86.95	4.000	No	Yes	2.00
405	27.23	12.90	3.15	3.53	1.00	7.27	11.66	84.75	4.000	No	Yes	2.00
406	27.28	13.22	3.13	3.30	1.00	7.46	11.13	83.02	4.000	No	Yes	2.00
407	27.29	13.29	3.09	2.84	1.00	7.50	10.38	77.81	4.000	No	Yes	2.00
408	27.38	13.29	3.07	2.57	1.00	7.47	9.96	74.44	4.000	No	Yes	2.00
409	27.48	13.27	3.06	2.51	1.00	7.43	9.89	73.48	4.000	No	Yes	2.00
410	27.57	13.27	3.10	2.97	1.00	7.41	10.67	79.00	4.000	No	Yes	2.00
411	27.64	13.30	3.13	3.39	1.00	7.41	11.31	83.76	4.000	No	Yes	2.00
412	27.65	13.44	3.17	3.99	1.00	7.49	12.08	90.43	4.000	No	Yes	2.00
413	27.74	14.52	3.16	4.27	1.00	8.14	11.82	96.17	4.000	No	Yes	2.00
414	27.80	16.91	3.10	4.34	1.00	9.63	10.69	102.90	4.000	No	Yes	2.00
415	27.90	19.17	3.05	4.16	1.00	11.00	9.59	105.58	4.000	No	Yes	2.00
416	27.99	19.34	3.05	4.25	1.00	11.07	9.67	106.99	4.000	No	Yes	2.00
417	28.07	17.12	3.11	4.55	1.00	9.65	10.91	105.31	4.000	No	Yes	2.00
418	28.16	14.45	3.20	4.79	1.00	7.96	12.63	100.58	4.000	No	Yes	2.00
419	28.25	12.53	3.25	4.68	1.00	6.75	13.86	93.48	4.000	No	Yes	2.00
420	28.34	11.52	3.26	4.24	1.00	6.10	14.13	86.20	4.000	No	Yes	2.00
421	28.44	11.01	3.26	3.94	1.00	5.76	14.19	81.77	4.000	No	Yes	2.00
422	28.53	10.84	3.26	3.87	1.00	5.64	14.27	80.51	4.000	No	Yes	2.00
423	28.62	11.75	3.26	4.25	1.00	6.17	14.04	86.70	4.000	No	Yes	2.00
424	28.76	14.21	3.19	4.46	1.00	7.64	12.54	95.81	4.000	No	Yes	2.00
425	28.86	17.65	3.12	4.75	1.00	9.69	11.11	107.72	4.000	No	Yes	2.00
426	28.96	20.32	3.09	5.14	1.00	11.26	10.51	118.36	4.000	No	Yes	2.00
427	29.08	21.30	3.12	6.06	1.00	11.80	11.10	130.98	4.000	No	Yes	2.00
428	29.19	22.07	3.15	6.87	1.00	12.21	11.60	141.58	4.000	No	Yes	2.00
429	29.29	27.50	2.99	5.17	1.00	15.40	8.64	133.06	4.000	No	Yes	2.00
430	29.39	40.70	2.74	3.77	0.83	25.08	5.15	129.21	4.000	No	Yes	2.00
431	29.50	57.67	2.55	3.03	0.77	36.81	3.37	124.06	4.000	No	No	2.00
432	29.63	66.88	2.53	3.30	0.77	42.86	3.19	136.79	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	29.65	70.22	2.52	3.39	0.76	45.09	3.13	141.18	4.000	Yes	No	2.00
434	29.66	71.00	2.52	3.38	0.76	45.61	3.10	141.50	4.000	Yes	No	2.00
435	29.72	73.53	2.50	3.27	0.76	47.34	2.95	139.57	4.000	Yes	No	2.00
436	29.80	77.81	2.46	3.07	0.75	50.31	2.70	135.94	4.000	Yes	No	2.00
437	29.85	89.49	2.36	2.59	0.72	58.79	2.17	127.49	4.000	Yes	No	2.00
438	29.94	111.58	2.20	2.00	0.67	75.08	1.62	121.89	4.000	Yes	No	2.00
439	30.00	135.50	2.06	1.57	0.63	93.20	1.37	127.60	4.000	Yes	No	2.00
440	30.05	152.98	1.96	1.28	0.60	106.83	1.28	136.43	4.000	Yes	No	2.00
441	30.14	162.60	1.89	1.09	0.58	114.57	1.23	140.95	4.000	Yes	No	2.00
442	30.19	167.56	1.84	0.97	0.56	118.78	1.20	142.08	4.000	Yes	No	2.00
443	30.24	169.61	1.83	0.93	0.56	120.45	1.18	142.19	4.000	Yes	No	2.00
444	30.29	169.68	1.83	0.93	0.56	120.31	1.18	142.38	0.348	No	No	1.14
445	30.38	167.72	1.84	0.95	0.56	118.51	1.19	141.39	0.343	No	No	1.12
446	30.43	164.79	1.85	0.98	0.56	116.05	1.20	139.76	0.334	No	No	1.09
447	30.48	161.62	1.87	0.99	0.57	113.47	1.21	137.67	0.323	No	No	1.05
448	30.54	159.16	1.87	1.00	0.57	111.46	1.22	135.86	0.313	No	No	1.02
449	30.62	158.35	1.87	0.99	0.57	110.69	1.22	134.98	0.309	No	No	1.00
450	30.67	157.77	1.87	0.99	0.57	110.16	1.22	134.34	0.305	No	No	0.99
451	30.72	158.55	1.87	0.98	0.57	110.67	1.22	134.61	0.307	No	No	0.99
452	30.76	159.46	1.86	0.96	0.57	111.32	1.21	134.89	0.308	No	No	1.00
453	30.86	162.06	1.85	0.94	0.56	113.16	1.20	135.92	0.314	No	No	1.01
454	30.91	165.09	1.84	0.91	0.56	115.46	1.19	137.26	0.321	No	No	1.03
455	30.95	168.94	1.82	0.88	0.55	118.37	1.17	138.94	0.329	No	No	1.06
456	31.03	173.83	1.80	0.85	0.55	122.03	1.15	140.71	0.339	No	No	1.09
457	31.10	179.36	1.78	0.83	0.54	126.19	1.13	142.33	0.348	No	No	1.12
458	31.15	185.03	1.76	0.81	0.54	130.44	1.10	144.07	0.358	No	No	1.15
459	31.20	189.66	1.75	0.81	0.53	133.76	1.09	146.05	0.370	No	No	1.19
460	31.26	192.52	1.75	0.82	0.53	135.69	1.09	147.81	0.380	No	No	1.22
461	31.34	186.22	1.78	0.86	0.54	130.42	1.13	147.23	0.377	No	No	1.21
462	31.37	184.63	1.79	0.87	0.54	129.08	1.14	146.99	0.375	No	No	1.20
463	31.38	181.39	1.80	0.89	0.55	126.56	1.15	145.70	0.368	No	No	1.18
464	31.43	184.63	1.78	0.86	0.54	129.02	1.13	146.17	0.370	No	No	1.19
465	31.47	179.33	1.80	0.87	0.55	124.92	1.15	143.44	0.354	No	No	1.13
466	31.55	171.64	1.82	0.88	0.55	118.91	1.17	139.35	0.332	No	No	1.06
467	31.59	160.34	1.86	0.93	0.57	110.19	1.21	132.93	0.298	No	No	0.95
468	31.66	147.76	1.91	1.00	0.58	100.47	1.24	124.83	0.261	No	No	0.83
469	31.73	135.75	1.97	1.09	0.60	91.20	1.28	116.80	0.228	No	No	0.73
470	31.78	125.08	2.02	1.21	0.62	83.04	1.33	110.36	0.205	No	No	0.65
471	31.84	115.64	2.09	1.36	0.63	75.76	1.40	106.34	0.192	No	No	0.61
472	31.93	107.23	2.16	1.55	0.65	69.27	1.51	104.84	0.187	No	No	0.60
473	31.98	100.42	2.22	1.75	0.67	64.06	1.66	106.04	0.191	No	No	0.61
474	32.02	98.18	2.25	1.90	0.68	62.19	1.75	108.88	0.200	No	No	0.64
475	32.09	97.00	2.27	2.03	0.69	61.07	1.83	111.87	0.210	No	No	0.67
476	32.16	98.89	2.27	2.07	0.69	62.18	1.83	113.86	0.217	No	No	0.69
477	32.22	100.29	2.27	2.07	0.69	63.04	1.82	114.52	0.220	No	No	0.70
478	32.27	103.49	2.25	2.02	0.68	65.22	1.76	114.53	0.220	No	No	0.70
479	32.34	106.02	2.24	1.97	0.68	66.91	1.71	114.38	0.219	No	No	0.69
480	32.42	108.89	2.22	1.91	0.67	68.85	1.66	114.11	0.218	No	No	0.69

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	32.46	113.04	2.19	1.80	0.66	71.82	1.58	113.62	0.216	No	No	0.68
482	32.54	117.73	2.15	1.68	0.65	75.15	1.51	113.25	0.215	No	No	0.68
483	32.60	121.74	2.11	1.51	0.64	78.23	1.43	112.00	0.211	No	No	0.66
484	32.67	124.81	2.07	1.39	0.63	80.60	1.38	111.53	0.209	No	No	0.66
485	32.75	127.51	2.05	1.31	0.62	82.59	1.35	111.85	0.210	No	No	0.66
486	32.81	130.38	2.05	1.32	0.62	84.43	1.35	113.95	0.218	No	No	0.68
487	32.89	133.38	2.04	1.34	0.62	86.29	1.35	116.21	0.226	No	No	0.71
488	32.94	129.47	2.07	1.43	0.63	83.21	1.38	114.84	0.221	No	No	0.69
489	32.95	131.02	2.07	1.44	0.63	84.23	1.38	116.07	0.225	No	No	0.71
490	33.00	132.88	2.07	1.46	0.63	85.36	1.38	117.56	0.231	No	No	0.72
491	33.06	141.08	2.04	1.42	0.62	91.06	1.34	122.40	0.251	No	No	0.79
492	33.11	142.26	2.04	1.45	0.62	91.66	1.35	123.66	0.256	No	No	0.80
493	33.20	141.21	2.06	1.50	0.63	90.60	1.36	123.53	0.255	No	No	0.80
494	33.25	139.02	2.08	1.56	0.63	88.78	1.39	123.06	0.253	No	No	0.79
495	33.34	137.03	2.09	1.61	0.64	87.07	1.41	122.48	0.251	No	No	0.78
496	33.38	136.69	2.10	1.63	0.64	86.68	1.42	122.68	0.252	No	No	0.79
497	33.48	138.41	2.10	1.64	0.64	87.63	1.41	123.78	0.256	No	No	0.80
498	33.58	141.92	2.09	1.64	0.63	89.83	1.40	125.79	0.265	No	No	0.83
499	33.63	146.74	2.07	1.63	0.63	93.05	1.38	128.81	0.279	No	No	0.87
500	33.73	152.41	2.06	1.61	0.63	96.75	1.37	132.15	0.295	No	No	0.92
501	33.82	158.96	2.04	1.60	0.62	101.09	1.35	136.16	0.315	No	No	0.98
502	33.87	165.74	2.03	1.58	0.62	105.66	1.33	140.58	0.338	No	No	1.05
503	33.96	172.72	2.01	1.57	0.61	110.29	1.32	145.13	0.364	No	No	1.13
504	34.02	180.58	2.00	1.57	0.61	115.54	1.30	150.66	0.398	No	No	1.23
505	34.11	190.03	1.98	1.57	0.60	121.77	1.29	157.32	0.442	No	No	1.37
506	34.18	200.49	1.97	1.59	0.60	128.68	1.28	164.99	0.498	No	No	1.54
507	34.26	210.44	1.96	1.63	0.60	135.11	1.28	172.52	0.558	No	No	1.72
508	34.35	219.45	1.96	1.68	0.60	140.77	1.28	179.50	0.618	No	No	1.91
509	34.44	227.51	1.95	1.71	0.59	145.83	1.27	185.53	0.674	No	No	2.00
510	34.49	233.96	1.95	1.72	0.59	150.02	1.27	190.23	0.720	No	No	2.00
511	34.59	237.94	1.94	1.72	0.59	152.42	1.27	192.83	0.747	No	No	2.00
512	34.69	240.00	1.94	1.73	0.59	153.47	1.26	194.12	0.760	No	No	2.00
513	34.76	240.94	1.94	1.72	0.59	153.92	1.26	194.53	0.765	No	No	2.00
514	34.83	240.60	1.94	1.72	0.59	153.43	1.26	194.02	0.759	No	No	2.00
515	34.93	237.97	1.94	1.71	0.59	151.43	1.26	191.54	0.733	No	No	2.00
516	35.02	233.82	1.95	1.70	0.59	148.39	1.27	188.08	0.699	No	No	2.00
517	35.12	229.78	1.94	1.65	0.59	145.60	1.27	184.23	0.662	No	No	2.00
518	35.22	226.47	1.94	1.62	0.59	143.26	1.26	181.13	0.633	No	No	1.94
519	35.30	222.22	1.94	1.59	0.59	140.29	1.26	177.46	0.600	No	No	1.83
520	35.38	208.55	1.98	1.66	0.60	130.48	1.29	168.21	0.523	No	No	1.60
521	35.43	198.10	2.00	1.71	0.61	123.09	1.31	161.35	0.471	No	No	1.44
522	35.46	189.40	2.03	1.76	0.62	116.99	1.33	155.80	0.432	No	No	1.32
523	35.51	187.20	2.03	1.73	0.62	115.53	1.33	153.78	4.000	Yes	No	2.00
524	35.56	176.78	2.05	1.75	0.62	108.45	1.35	146.76	4.000	Yes	No	2.00
525	35.66	163.52	2.08	1.79	0.63	99.31	1.39	138.53	4.000	Yes	No	2.00
526	35.70	148.20	2.13	1.85	0.65	89.01	1.46	130.03	4.000	Yes	No	2.00
527	35.80	131.87	2.19	1.98	0.66	77.90	1.59	123.66	4.000	Yes	No	2.00
528	35.89	111.32	2.28	2.22	0.69	64.17	1.87	119.95	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	35.96	89.09	2.41	2.59	0.73	49.72	2.43	120.81	4.000	Yes	No	2.00
530	36.04	68.24	2.54	2.90	0.77	36.73	3.28	120.37	4.000	Yes	No	2.00
531	36.14	52.15	2.66	3.11	0.81	27.04	4.33	117.01	4.000	Yes	Yes	2.00
532	36.19	43.48	2.73	3.10	0.83	22.01	5.03	110.69	4.000	Yes	Yes	2.00
533	36.28	40.51	2.77	3.18	0.84	20.23	5.44	110.05	4.000	Yes	Yes	2.00
534	36.33	40.51	2.76	3.10	0.84	20.24	5.35	108.32	3.600	No	Yes	2.00
535	36.42	42.30	2.74	3.02	0.83	21.24	5.09	108.08	3.600	No	Yes	2.00
536	36.48	45.97	2.69	2.87	0.81	23.38	4.59	107.27	3.600	No	Yes	2.00
537	36.52	51.03	2.66	2.98	0.81	26.20	4.31	112.95	3.600	No	Yes	2.00
538	36.62	54.10	2.66	3.19	0.81	27.78	4.31	119.67	3.600	No	Yes	2.00
539	36.68	54.07	2.69	3.50	0.81	27.55	4.59	126.59	3.600	No	Yes	2.00
540	36.77	52.82	2.71	3.61	0.82	26.73	4.79	128.11	3.600	No	Yes	2.00
541	36.86	54.64	2.69	3.49	0.81	27.76	4.56	126.60	4.000	Yes	Yes	2.00
542	36.90	67.67	2.53	2.74	0.77	35.75	3.22	115.19	4.000	Yes	No	2.00
543	37.00	98.14	2.29	1.88	0.69	55.13	1.87	103.13	4.000	Yes	No	2.00
544	37.10	140.34	2.04	1.30	0.62	83.45	1.35	112.56	4.000	Yes	No	2.00
545	37.20	182.54	1.86	0.97	0.57	113.15	1.21	136.84	4.000	Yes	No	2.00
546	37.29	213.04	1.75	0.82	0.53	135.23	1.09	147.30	4.000	Yes	No	2.00
547	37.39	232.34	1.70	0.76	0.52	149.01	1.00	149.01	4.000	Yes	No	2.00
548	37.49	241.91	1.70	0.80	0.52	155.00	1.00	155.00	0.426	No	No	1.28
549	37.53	245.57	1.72	0.85	0.52	156.74	1.02	160.20	0.462	No	No	1.39
550	37.58	246.07	1.73	0.90	0.53	156.33	1.06	165.44	0.501	No	No	1.51
551	37.62	247.84	1.75	0.95	0.53	156.88	1.08	169.66	0.534	No	No	1.60
552	37.69	250.56	1.77	1.01	0.54	157.82	1.11	175.10	0.579	No	No	1.74
553	37.77	253.53	1.78	1.07	0.54	158.95	1.13	179.78	0.620	No	No	1.86
554	37.82	254.98	1.80	1.14	0.55	159.10	1.15	183.39	0.654	No	No	1.96
555	37.87	254.84	1.81	1.18	0.55	158.42	1.17	184.85	0.667	No	No	2.00
556	37.91	252.72	1.83	1.23	0.56	156.44	1.18	184.82	0.667	No	No	2.00
557	37.97	248.23	1.85	1.27	0.56	152.87	1.20	183.06	0.650	No	No	1.95
558	38.06	241.92	1.87	1.31	0.57	148.07	1.21	179.59	0.619	No	No	1.85
559	38.10	235.58	1.88	1.34	0.57	143.53	1.22	175.74	0.585	No	No	1.75
560	38.17	230.89	1.89	1.34	0.57	140.30	1.23	172.34	0.556	No	No	1.67
561	38.25	228.09	1.88	1.30	0.57	138.57	1.22	169.66	0.534	No	No	1.60
562	38.35	225.79	1.87	1.25	0.57	137.24	1.22	167.11	0.514	No	No	1.54
563	38.40	223.43	1.87	1.21	0.57	135.86	1.21	164.83	0.496	No	No	1.48
564	38.46	221.65	1.86	1.19	0.57	134.68	1.21	163.21	0.484	No	No	1.45
565	38.54	220.87	1.86	1.18	0.57	134.09	1.21	162.26	0.477	No	No	1.43
566	38.60	220.87	1.86	1.15	0.56	134.14	1.21	161.69	0.473	No	No	1.41
567	38.69	222.22	1.85	1.12	0.56	135.09	1.20	161.77	0.474	No	No	1.41
568	38.74	224.92	1.83	1.09	0.56	137.05	1.19	162.53	0.479	No	No	1.43
569	38.83	227.85	1.82	1.08	0.56	138.91	1.18	163.73	0.488	No	No	1.46
570	38.88	229.20	1.81	1.05	0.55	139.97	1.17	163.54	0.487	No	No	1.45
571	38.97	228.76	1.81	1.03	0.55	139.65	1.16	162.47	0.479	No	No	1.43
572	39.02	227.25	1.80	1.00	0.55	138.83	1.16	160.45	0.464	No	No	1.38
573	39.11	224.44	1.81	0.99	0.55	136.82	1.16	158.54	0.451	No	No	1.34
574	39.16	218.51	1.81	0.99	0.55	132.80	1.17	154.99	0.426	No	No	1.27
575	39.23	205.48	1.85	1.02	0.56	123.73	1.20	148.10	0.382	No	No	1.14
576	39.24	200.81	1.85	1.01	0.56	120.69	1.20	145.08	0.364	No	No	1.08

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	39.28	198.62	1.85	1.00	0.56	119.29	1.20	143.39	0.354	No	No	1.05
578	39.32	201.93	1.83	0.94	0.56	121.86	1.18	144.08	0.358	No	No	1.07
579	39.39	194.55	1.84	0.95	0.56	116.84	1.20	139.67	4.000	Yes	No	2.00
580	39.47	183.96	1.88	0.98	0.57	109.44	1.22	133.48	4.000	Yes	No	2.00
581	39.54	171.48	1.92	1.05	0.58	100.68	1.25	125.99	4.000	Yes	No	2.00
582	39.62	158.42	1.98	1.14	0.60	91.63	1.29	117.99	4.000	Yes	No	2.00
583	39.71	145.73	2.03	1.23	0.62	82.95	1.33	110.70	4.000	Yes	No	2.00
584	39.76	134.50	2.08	1.32	0.63	75.46	1.39	105.08	4.000	Yes	No	2.00
585	39.85	125.32	2.13	1.40	0.65	69.36	1.46	101.34	4.000	Yes	No	2.00
586	39.90	117.87	2.17	1.48	0.66	64.48	1.53	98.95	4.000	Yes	No	2.00
587	40.00	111.05	2.20	1.56	0.67	60.00	1.63	97.53	4.000	Yes	No	2.00
588	40.06	104.71	2.24	1.65	0.68	55.91	1.73	96.96	4.000	Yes	No	2.00
589	40.15	98.67	2.28	1.75	0.69	52.00	1.87	97.18	4.000	Yes	No	2.00
590	40.21	92.83	2.33	1.90	0.71	48.24	2.05	98.86	4.000	Yes	No	2.00
591	40.29	86.59	2.39	2.09	0.72	44.24	2.31	102.19	4.000	Yes	No	2.00
592	40.35	79.68	2.46	2.39	0.75	39.85	2.72	108.27	4.000	Yes	No	2.00
593	40.43	72.22	2.53	2.63	0.77	35.37	3.16	111.81	4.000	Yes	No	2.00
594	40.52	63.85	2.60	2.88	0.79	30.51	3.76	114.58	4.000	Yes	Yes	2.00
595	40.58	55.21	2.68	3.09	0.81	25.70	4.47	115.00	4.000	Yes	Yes	2.00
596	40.67	46.88	2.77	3.45	0.84	21.09	5.54	116.83	4.000	Yes	Yes	2.00
597	40.77	41.63	2.85	3.76	0.86	18.24	6.45	117.65	4.000	Yes	Yes	2.00
598	40.84	39.14	2.89	3.94	0.87	16.87	6.99	117.99	4.000	Yes	Yes	2.00
599	40.89	42.28	2.83	3.65	0.86	18.55	6.27	116.25	4.000	Yes	Yes	2.00
600	40.94	49.75	2.72	3.09	0.82	22.62	4.92	111.31	4.000	Yes	Yes	2.00
601	41.03	61.46	2.57	2.48	0.78	29.20	3.53	103.18	4.000	Yes	No	2.00
602	41.08	73.03	2.45	2.07	0.74	35.94	2.68	96.47	4.000	Yes	No	2.00
603	41.14	82.03	2.37	1.83	0.72	41.30	2.24	92.51	4.000	Yes	No	2.00
604	41.22	87.70	2.33	1.71	0.71	44.68	2.04	90.97	4.000	Yes	No	2.00
605	41.28	90.43	2.31	1.68	0.70	46.24	1.97	91.29	0.151	No	No	0.45
606	41.33	91.99	2.32	1.74	0.70	46.96	1.99	93.52	0.156	No	No	0.46
607	41.42	93.64	2.33	1.85	0.71	47.61	2.04	97.02	0.165	No	No	0.49
608	41.47	97.01	2.33	1.94	0.71	49.31	2.04	100.81	0.175	No	No	0.52
609	41.52	104.03	2.31	1.97	0.70	53.17	1.96	104.48	0.186	No	No	0.55
610	41.62	115.47	2.27	1.93	0.69	59.72	1.81	107.92	0.197	No	No	0.58
611	41.67	130.01	2.22	1.88	0.67	68.21	1.66	112.91	0.214	No	No	0.63
612	41.76	144.45	2.17	1.82	0.66	76.74	1.54	118.23	0.234	No	No	0.69
613	41.82	156.39	2.14	1.79	0.65	83.80	1.48	123.75	0.256	No	No	0.76
614	41.90	165.43	2.11	1.76	0.64	89.14	1.44	128.02	0.275	No	No	0.81
615	41.99	171.57	2.10	1.74	0.64	92.73	1.41	131.05	0.289	No	No	0.85
616	42.05	174.81	2.09	1.73	0.63	94.61	1.40	132.58	0.297	No	No	0.88
617	42.15	175.22	2.09	1.74	0.63	94.64	1.40	132.77	0.298	No	No	0.88
618	42.23	173.33	2.10	1.77	0.64	93.24	1.42	132.06	0.294	No	No	0.87
619	42.30	169.55	2.11	1.80	0.64	90.73	1.44	130.51	0.287	No	No	0.85
620	42.38	163.64	2.13	1.84	0.65	86.97	1.47	127.88	0.274	No	No	0.81
621	42.48	153.79	2.16	1.88	0.66	80.87	1.53	123.60	0.256	No	No	0.75
622	42.57	141.98	2.20	1.94	0.67	73.69	1.62	119.15	0.237	No	No	0.70
623	42.64	129.97	2.24	2.01	0.68	66.53	1.73	115.28	0.222	No	No	0.66
624	42.72	121.20	2.27	2.02	0.69	61.42	1.82	111.72	0.210	No	No	0.62

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	42.82	114.72	2.29	1.99	0.69	57.72	1.88	108.24	0.198	No	No	0.58
626	42.90	110.03	2.30	1.96	0.70	55.08	1.91	105.42	0.189	No	No	0.56
627	42.97	106.05	2.31	1.98	0.70	52.74	1.98	104.32	0.186	No	No	0.55
628	43.06	102.31	2.34	2.04	0.71	50.43	2.08	104.69	0.187	No	No	0.55
629	43.15	98.76	2.35	2.01	0.71	48.44	2.11	102.43	0.180	No	No	0.53
630	43.20	97.75	2.34	1.92	0.71	48.00	2.07	99.54	0.172	No	No	0.51
631	43.30	104.19	2.28	1.70	0.69	51.99	1.84	95.67	0.161	No	No	0.48
632	43.40	119.88	2.19	1.51	0.66	61.38	1.58	97.12	0.165	No	No	0.49
633	43.48	132.43	2.13	1.40	0.65	68.91	1.47	100.97	0.176	No	No	0.52
634	43.51	139.11	2.10	1.37	0.64	72.90	1.43	103.89	0.184	No	No	0.54
635	43.52	146.23	2.08	1.34	0.63	77.22	1.39	107.23	0.195	No	No	0.57
636	43.56	160.13	2.03	1.26	0.62	85.83	1.33	114.20	0.219	No	No	0.64
637	43.61	178.86	1.96	1.17	0.60	97.60	1.28	124.81	0.261	No	No	0.77
638	43.67	193.23	1.92	1.11	0.58	106.74	1.25	133.29	0.300	No	No	0.88
639	43.72	206.01	1.88	1.05	0.57	115.04	1.22	140.56	0.338	No	No	1.00
640	43.80	216.51	1.85	1.00	0.56	121.88	1.20	145.95	0.369	No	No	1.09
641	43.85	224.74	1.82	0.97	0.56	127.26	1.18	149.84	0.393	No	No	1.16
642	43.90	231.25	1.81	0.95	0.55	131.51	1.16	152.56	0.410	No	No	1.21
643	43.94	236.38	1.79	0.94	0.55	134.87	1.14	154.37	0.422	No	No	1.24
644	43.99	239.82	1.78	0.92	0.54	137.13	1.13	155.28	0.428	No	No	1.26
645	44.08	241.54	1.78	0.92	0.54	138.11	1.13	155.65	0.431	No	No	1.27
646	44.14	241.51	1.79	0.94	0.54	137.71	1.14	156.49	0.436	No	No	1.28
647	44.22	240.40	1.80	0.97	0.55	136.41	1.15	157.19	0.441	No	No	1.30
648	44.28	238.31	1.82	1.01	0.55	134.50	1.17	157.37	0.442	No	No	1.30
649	44.33	235.67	1.83	1.05	0.56	132.35	1.18	156.78	0.438	No	No	1.29
650	44.40	232.27	1.85	1.10	0.56	129.52	1.20	155.80	0.432	No	No	1.27
651	44.48	231.30	1.87	1.15	0.57	128.25	1.22	155.90	0.432	No	No	1.27
652	44.52	228.57	1.90	1.24	0.58	125.64	1.24	155.24	0.428	No	No	1.26
653	44.61	230.02	1.89	1.23	0.58	126.41	1.23	155.88	0.432	No	No	1.27
654	44.72	231.52	1.90	1.24	0.58	127.03	1.23	156.70	0.438	No	No	1.29
655	44.77	236.14	1.88	1.21	0.57	130.05	1.22	159.04	0.454	No	No	1.34
656	44.91	237.86	1.89	1.24	0.57	130.46	1.23	160.27	0.463	No	No	1.36
657	44.95	231.69	1.91	1.29	0.58	126.16	1.24	156.88	0.439	No	No	1.29
658	45.02	227.41	1.92	1.32	0.59	123.19	1.25	154.33	0.422	No	No	1.24
659	45.04	198.97	2.01	1.51	0.61	104.88	1.32	138.44	0.327	No	No	0.96
660	45.06	203.49	2.00	1.46	0.61	107.81	1.30	140.63	0.339	No	No	1.00
661	45.11	208.45	1.98	1.41	0.60	111.04	1.29	143.03	0.352	No	No	1.04
662	45.15	239.96	1.87	1.20	0.57	131.64	1.22	160.49	0.464	No	No	1.37
663	45.21	246.91	1.85	1.16	0.56	136.23	1.20	163.81	0.489	No	No	1.44
664	45.25	252.44	1.84	1.13	0.56	139.80	1.19	166.43	0.509	No	No	1.50
665	45.30	256.29	1.83	1.13	0.56	142.11	1.18	168.34	0.524	No	No	1.54
666	45.35	258.04	1.83	1.13	0.56	143.02	1.18	169.35	0.532	No	No	1.57
667	45.41	258.42	1.83	1.14	0.56	143.02	1.19	169.64	0.534	No	No	1.57
668	45.49	257.00	1.84	1.15	0.56	141.89	1.19	168.87	0.528	No	No	1.55
669	45.55	254.13	1.84	1.15	0.56	139.97	1.19	167.24	0.515	No	No	1.52
670	45.63	249.51	1.85	1.16	0.56	136.90	1.20	164.52	0.494	No	No	1.46
671	45.69	243.67	1.86	1.16	0.57	133.19	1.21	161.09	0.469	No	No	1.38
672	45.78	236.62	1.88	1.18	0.57	128.61	1.22	156.88	0.439	No	No	1.29

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	45.84	228.05	1.89	1.18	0.58	123.25	1.23	151.68	0.405	No	No	1.19
674	45.93	217.69	1.91	1.19	0.58	116.85	1.24	145.18	0.365	No	No	1.07
675	46.02	205.11	1.93	1.19	0.59	109.16	1.26	137.24	4.000	Yes	No	2.00
676	46.08	190.40	1.96	1.19	0.60	100.37	1.28	128.00	4.000	Yes	No	2.00
677	46.16	174.41	1.99	1.20	0.61	90.73	1.30	118.20	4.000	Yes	No	2.00
678	46.24	157.13	2.04	1.24	0.62	80.39	1.35	108.31	4.000	Yes	No	2.00
679	46.31	138.07	2.12	1.34	0.64	68.91	1.44	99.54	4.000	Yes	No	2.00
680	46.41	117.36	2.22	1.54	0.67	56.54	1.67	94.32	4.000	Yes	No	2.00
681	46.48	95.77	2.36	1.87	0.72	44.06	2.17	95.41	4.000	Yes	No	2.00
682	46.56	75.72	2.51	2.32	0.76	32.98	3.08	101.49	4.000	Yes	No	2.00
683	46.65	58.08	2.68	2.81	0.81	23.81	4.47	106.39	4.000	Yes	Yes	2.00
684	46.75	45.43	2.81	3.12	0.85	17.64	5.95	104.92	4.000	Yes	Yes	2.00
685	46.84	36.62	2.95	3.29	1.00	12.08	8.01	96.75	4.000	Yes	Yes	2.00
686	46.94	30.75	3.03	3.37	1.00	9.96	9.25	92.20	3.600	No	Yes	2.00
687	47.02	25.79	3.12	3.65	1.00	8.18	10.96	89.65	3.600	No	Yes	2.00
688	47.08	21.37	3.22	4.12	1.00	6.60	13.29	87.68	3.600	No	Yes	2.00
689	47.12	18.76	3.30	4.53	1.00	5.66	15.23	86.24	3.600	No	Yes	2.00
690	47.16	17.85	3.33	4.58	1.00	5.33	15.88	84.67	3.600	No	Yes	2.00
691	47.21	17.81	3.31	4.30	1.00	5.32	15.49	82.35	3.600	No	Yes	2.00
692	47.27	17.46	3.31	4.03	1.00	5.18	15.33	79.44	3.600	No	Yes	2.00
693	47.35	16.42	3.33	3.97	1.00	4.80	15.97	76.72	3.600	No	Yes	2.00
694	47.40	15.74	3.33	3.65	1.00	4.56	15.95	72.71	3.600	No	Yes	2.00
695	47.50	15.37	3.32	3.29	1.00	4.42	15.62	68.97	3.600	No	Yes	2.00
696	47.55	15.16	3.29	2.90	1.00	4.34	15.04	65.28	3.600	No	Yes	2.00
697	47.61	15.00	3.29	2.76	1.00	4.27	14.89	63.67	3.600	No	Yes	2.00
698	47.69	14.73	3.29	2.69	1.00	4.17	15.00	62.57	3.600	No	Yes	2.00
699	47.76	14.39	3.30	2.67	1.00	4.05	15.25	61.71	3.600	No	Yes	2.00
700	47.83	14.02	3.31	2.58	1.00	3.91	15.40	60.22	3.600	No	Yes	2.00
701	47.93	13.85	3.30	2.41	1.00	3.84	15.20	58.40	3.600	No	Yes	2.00
702	48.02	13.82	3.29	2.31	1.00	3.82	15.00	57.34	3.600	No	Yes	2.00
703	48.09	13.88	3.28	2.19	1.00	3.84	14.67	56.35	3.600	No	Yes	2.00
704	48.18	13.85	3.29	2.28	1.00	3.82	14.94	57.05	3.600	No	Yes	2.00
705	48.27	13.88	3.30	2.43	1.00	3.82	15.29	58.44	3.600	No	Yes	2.00
706	48.37	13.98	3.33	2.72	1.00	3.85	15.87	61.09	3.600	No	Yes	2.00
707	48.46	14.12	3.34	2.92	1.00	3.89	16.20	62.98	3.600	No	Yes	2.00
708	48.52	14.18	3.35	3.07	1.00	3.90	16.46	64.25	3.600	No	Yes	2.00
709	48.60	14.25	3.35	3.18	1.00	3.92	16.64	65.23	3.600	No	Yes	2.00
710	48.70	14.38	3.35	3.25	1.00	3.96	16.68	65.99	3.600	No	Yes	2.00
711	48.79	14.65	3.35	3.27	1.00	4.04	16.50	66.70	3.600	No	Yes	2.00
712	48.85	15.06	3.34	3.39	1.00	4.18	16.39	68.42	3.600	No	Yes	2.00
713	48.94	15.74	3.34	3.61	1.00	4.40	16.24	71.44	3.600	No	Yes	2.00
714	49.04	16.68	3.31	3.62	1.00	4.71	15.57	73.34	3.600	No	Yes	2.00
715	49.13	18.30	3.32	4.31	1.00	5.25	15.62	82.09	3.600	No	Yes	2.00
716	49.23	21.13	3.29	4.85	1.00	6.21	14.82	92.00	3.600	No	Yes	2.00
717	49.33	24.04	3.27	5.48	1.00	7.18	14.31	102.80	3.600	No	Yes	2.00
718	49.38	24.88	3.28	6.09	1.00	7.46	14.69	109.60	3.600	No	Yes	2.00
719	49.42	25.93	3.28	6.47	1.00	7.81	14.70	114.80	3.600	No	Yes	2.00
720	49.48	26.70	3.28	6.79	1.00	8.06	14.75	118.93	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	49.53	28.79	3.25	6.60	1.00	8.76	13.86	121.43	3.600	No	Yes	2.00
722	49.58	29.43	3.24	6.72	1.00	8.97	13.78	123.62	3.600	No	Yes	2.00
723	49.63	30.10	3.24	6.80	1.00	9.19	13.66	125.52	3.600	No	Yes	2.00
724	49.72	30.91	3.23	6.72	1.00	9.44	13.37	126.23	3.600	No	Yes	2.00
725	49.77	31.42	3.22	6.60	1.00	9.60	13.13	125.98	3.600	No	Yes	2.00
726	49.83	31.42	3.22	6.55	1.00	9.59	13.08	125.40	3.600	No	Yes	2.00
727	49.92	30.71	3.23	6.62	1.00	9.33	13.37	124.67	3.600	No	Yes	2.00
728	49.97	30.39	3.23	6.56	1.00	9.21	13.41	123.55	3.600	No	Yes	2.00
729	50.04	29.48	3.25	6.66	1.00	8.89	13.80	122.65	3.600	No	Yes	2.00
730	50.11	29.82	3.24	6.56	1.00	8.99	13.61	122.33	3.600	No	Yes	2.00
731	50.20	30.21	3.22	6.30	1.00	9.10	13.25	120.55	3.600	No	Yes	2.00
732	50.27	30.78	3.19	5.73	1.00	9.28	12.51	116.01	3.600	No	Yes	2.00
733	50.34	29.50	3.18	5.11	1.00	8.83	12.20	107.79	3.600	No	Yes	2.00
734	50.45	26.76	3.19	4.68	1.00	7.90	12.55	99.22	3.600	No	Yes	2.00
735	50.54	23.73	3.23	4.48	1.00	6.88	13.43	92.39	3.600	No	Yes	2.00
736	50.59	21.13	3.28	4.47	1.00	6.01	14.59	87.71	3.600	No	Yes	2.00
737	50.68	19.24	3.32	4.43	1.00	5.37	15.59	83.78	3.600	No	Yes	2.00
738	50.79	18.13	3.33	4.26	1.00	4.99	16.06	80.17	3.600	No	Yes	2.00
739	50.88	17.81	3.33	4.10	1.00	4.88	16.03	78.18	3.600	No	Yes	2.00
740	50.98	17.64	3.34	4.11	1.00	4.81	16.19	77.89	3.600	No	Yes	2.00
741	51.07	17.81	3.32	3.85	1.00	4.86	15.67	76.09	3.600	No	Yes	2.00
742	51.17	18.43	3.26	3.21	1.00	5.05	14.19	71.67	3.600	No	Yes	2.00
743	51.24	19.51	3.20	2.74	1.00	5.40	12.74	68.77	3.600	No	Yes	2.00
744	51.33	20.19	3.19	2.81	1.00	5.61	12.56	70.43	3.600	No	Yes	2.00
745	51.46	20.09	3.23	3.28	1.00	5.56	13.45	74.75	3.600	No	Yes	2.00
746	51.46	19.80	3.27	3.71	1.00	5.46	14.31	78.20	3.600	No	Yes	2.00
747	51.51	19.77	3.28	3.88	1.00	5.45	14.62	79.60	3.600	No	Yes	2.00
748	51.56	19.87	3.29	4.15	1.00	5.47	14.98	82.02	3.600	No	Yes	2.00
749	51.65	19.95	3.31	4.41	1.00	5.49	15.35	84.26	3.600	No	Yes	2.00
750	51.71	20.09	3.32	4.71	1.00	5.53	15.72	86.89	3.600	No	Yes	2.00
751	51.79	20.49	3.32	4.86	1.00	5.65	15.73	88.80	3.600	No	Yes	2.00
752	51.85	21.23	3.32	5.11	1.00	5.88	15.68	92.19	3.600	No	Yes	2.00
753	51.94	22.11	3.32	5.42	1.00	6.15	15.66	96.33	3.600	No	Yes	2.00
754	51.99	23.22	3.32	5.95	1.00	6.51	15.77	102.62	3.600	No	Yes	2.00
755	52.09	24.17	3.33	6.60	1.00	6.80	16.12	109.52	3.600	No	Yes	2.00
756	52.19	27.74	3.28	6.62	1.00	7.93	14.73	116.81	3.600	No	Yes	2.00
757	52.28	33.34	3.20	6.19	1.00	9.72	12.62	122.63	3.600	No	Yes	2.00
758	52.35	36.42	3.17	6.29	1.00	10.69	12.02	128.41	3.600	No	Yes	2.00
759	52.43	37.06	3.18	6.64	1.00	10.87	12.22	132.82	3.600	No	Yes	2.00
760	52.52	35.17	3.22	7.33	1.00	10.25	13.30	136.28	3.600	No	Yes	2.00
761	52.62	35.61	3.22	7.23	1.00	10.37	13.11	135.93	3.600	No	Yes	2.00
762	52.72	35.98	3.20	6.96	1.00	10.46	12.80	133.92	3.600	No	Yes	2.00
763	52.81	34.26	3.24	7.47	1.00	9.89	13.70	135.53	3.600	No	Yes	2.00
764	52.91	31.32	3.34	9.52	1.00	8.94	16.37	146.31	3.600	No	Yes	2.00
765	53.00	37.23	3.27	9.04	1.00	10.79	14.34	154.70	3.600	No	Yes	2.00
766	53.10	62.36	2.95	5.53	1.00	18.71	7.92	148.13	4.000	Yes	Yes	2.00
767	53.20	108.21	2.62	3.37	1.00	33.14	3.92	129.79	4.000	Yes	Yes	2.00
768	53.29	163.78	2.38	2.36	1.00	50.57	2.27	114.61	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	53.38	213.88	2.24	1.98	1.00	66.21	1.72	114.09	4.000	Yes	No	2.00
770	53.46	260.07	2.14	1.75	1.00	80.59	1.49	119.81	4.000	Yes	No	2.00
771	53.53	292.05	2.12	1.83	1.00	90.48	1.45	130.93	4.000	Yes	No	2.00
772	53.63	323.19	2.09	1.82	1.00	100.02	1.40	139.93	4.000	Yes	No	2.00
773	53.73	361.79	2.01	1.58	1.00	111.85	1.31	146.92	4.000	Yes	No	2.00
774	53.82	388.35	1.92	1.28	1.00	119.89	1.25	150.03	4.000	Yes	No	2.00
775	53.92	387.71	1.89	1.12	1.00	119.45	1.23	146.54	4.000	Yes	No	2.00
776	53.94	360.18	1.92	1.15	1.00	110.85	1.25	138.23	0.326	No	No	0.98
777	53.96	336.26	1.95	1.19	1.00	103.38	1.27	131.20	0.290	No	No	0.88
778	53.97	349.08	1.92	1.12	1.00	107.34	1.25	134.16	0.305	No	No	0.92
779	54.05	377.59	1.87	1.03	1.00	116.04	1.22	141.00	0.341	No	No	1.03
780	54.08	426.28	1.79	0.91	1.00	131.09	1.15	150.15	0.395	No	No	1.19
781	54.13	473.21	1.74	0.84	1.00	145.55	1.06	154.41	0.422	No	No	1.28
782	54.19	518.79	1.70	0.83	1.00	159.56	1.00	159.56	0.458	No	No	1.38
783	54.25	524.22	1.71	0.86	1.00	161.12	1.01	162.94	0.482	No	No	1.46
784	54.28	510.87	1.74	0.91	1.00	156.95	1.06	166.66	0.510	No	No	1.54
785	54.29	486.82	1.76	0.94	1.00	149.48	1.10	164.40	0.493	No	No	1.49
786	54.34	486.89	1.76	0.94	1.00	149.42	1.10	164.35	0.493	No	No	1.49
787	54.35	492.20	1.75	0.93	1.00	151.05	1.09	164.72	0.496	No	No	1.50
788	54.40	504.89	1.74	0.91	1.00	154.89	1.07	165.62	0.503	No	No	1.52
789	54.44	522.30	1.72	0.90	1.00	160.18	1.04	166.45	0.509	No	No	1.54
790	54.49	535.62	1.71	0.88	1.00	164.19	1.01	165.88	0.505	No	No	1.53
791	54.53	546.25	1.70	0.87	1.00	167.39	1.00	167.39	0.516	No	No	1.56
792	54.57	558.27	1.69	0.87	1.00	171.02	1.00	171.02	0.545	No	No	1.65
793	54.58	567.78	1.70	0.89	1.00	173.92	1.00	173.92	0.569	No	No	1.72
794	54.63	560.90	1.71	0.92	1.00	171.71	1.01	173.90	0.569	No	No	1.72
795	54.68	536.31	1.75	0.99	1.00	164.04	1.08	176.93	0.595	No	No	1.80
796	54.73	510.50	1.78	1.03	1.00	156.00	1.12	175.12	0.579	No	No	1.75
797	54.78	499.67	1.79	1.04	1.00	152.59	1.14	173.29	0.564	No	No	1.71
798	54.83	493.63	1.80	1.06	1.00	150.64	1.15	172.82	0.560	No	No	1.70
799	54.88	497.14	1.80	1.09	1.00	151.64	1.15	175.08	0.579	No	No	1.75
800	54.92	500.68	1.81	1.15	1.00	152.65	1.17	178.37	0.608	No	No	1.84
801	54.97	510.81	1.81	1.14	1.00	155.66	1.16	180.73	0.629	No	No	1.91
802	55.02	513.44	1.81	1.15	1.00	156.38	1.16	181.62	0.637	No	No	1.93
803	55.12	487.90	1.85	1.25	1.00	148.39	1.20	178.01	0.605	No	No	1.83
804	55.17	449.17	1.92	1.45	1.00	136.44	1.25	170.63	0.542	No	No	1.64
805	55.25	410.54	1.98	1.59	1.00	124.51	1.29	160.49	0.464	No	No	1.41
806	55.31	394.21	1.98	1.55	1.00	119.43	1.29	154.46	0.423	No	No	1.28
807	55.36	388.18	1.95	1.35	1.00	117.52	1.27	148.87	0.387	No	No	1.17
808	55.45	381.09	1.91	1.20	1.00	115.23	1.25	143.68	0.356	No	No	1.08
809	55.50	365.91	1.92	1.15	1.00	110.54	1.25	137.89	0.324	No	No	0.98
810	55.60	351.24	1.94	1.19	1.00	105.95	1.26	133.93	0.303	No	No	0.92
811	55.65	332.24	1.96	1.21	1.00	100.11	1.28	128.15	0.276	No	No	0.84
812	55.71	324.14	1.96	1.15	1.00	97.58	1.27	124.39	0.259	No	No	0.79
813	55.75	320.40	1.93	1.03	1.00	96.40	1.26	121.19	0.246	No	No	0.75
814	55.79	325.12	1.91	0.99	1.00	97.79	1.25	121.90	0.248	No	No	0.76
815	55.84	332.47	1.90	0.97	1.00	99.97	1.24	123.76	0.256	No	No	0.78
816	55.89	338.01	1.90	0.97	1.00	101.60	1.23	125.39	0.263	No	No	0.80

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	55.90	341.15	1.89	0.96	1.00	102.54	1.23	126.17	0.267	No	No	0.81
818	55.94	336.26	1.90	0.98	1.00	101.02	1.24	124.98	0.262	No	No	0.80
819	55.99	327.63	1.92	1.01	1.00	98.34	1.25	122.89	0.253	No	No	0.77
820	56.03	317.88	1.94	1.05	1.00	95.34	1.26	120.41	0.242	No	No	0.74
821	56.08	311.67	1.95	1.06	1.00	93.40	1.27	118.54	0.235	No	No	0.72
822	56.14	306.37	1.95	1.05	1.00	91.74	1.27	116.74	0.228	No	No	0.69
823	56.22	299.89	1.96	1.06	1.00	89.70	1.28	114.65	0.220	No	No	0.67
824	56.28	294.29	1.97	1.06	1.00	87.95	1.28	112.90	0.214	No	No	0.65
825	56.33	292.57	1.97	1.06	1.00	87.39	1.29	112.38	0.212	No	No	0.65
826	56.38	294.06	1.97	1.04	1.00	87.79	1.28	112.46	0.212	No	No	0.65
827	56.45	301.34	1.95	1.02	1.00	89.92	1.27	114.23	0.219	No	No	0.67
828	56.52	312.58	1.93	0.98	1.00	93.24	1.25	117.01	0.229	No	No	0.70
829	56.62	325.19	1.90	0.94	1.00	96.94	1.24	120.21	0.242	No	No	0.74
830	56.66	338.42	1.87	0.89	1.00	100.88	1.22	123.02	0.253	No	No	0.77
831	56.73	350.06	1.87	0.90	1.00	104.30	1.21	126.65	0.269	No	No	0.82
832	56.81	357.11	1.87	0.94	1.00	106.33	1.22	129.59	0.282	No	No	0.86
833	56.95	363.42	1.89	1.01	1.00	108.06	1.23	132.64	0.297	No	No	0.91
834	57.00	372.46	1.88	1.03	1.00	110.72	1.23	135.80	0.313	No	No	0.96
835	57.09	373.11	1.89	1.06	1.00	110.80	1.23	136.52	0.317	No	No	0.97
836	57.19	368.58	1.91	1.10	1.00	109.32	1.24	135.85	0.313	No	No	0.96
837	57.27	354.04	1.92	1.11	1.00	104.88	1.25	131.44	0.291	No	No	0.89
838	57.35	357.65	1.89	0.99	1.00	105.87	1.23	130.16	0.285	No	No	0.87
839	57.44	356.17	1.86	0.89	1.00	105.33	1.21	127.36	0.272	No	No	0.83
840	57.50	364.37	1.83	0.81	1.00	107.70	1.18	127.07	0.271	No	No	0.83
841	57.52	378.10	1.83	0.84	1.00	111.77	1.18	131.85	0.293	No	No	0.90
842	57.58	409.37	1.82	0.90	1.00	121.03	1.17	141.73	0.345	No	No	1.06
843	57.63	432.08	1.81	0.95	1.00	127.73	1.17	149.17	0.389	No	No	1.19
844	57.72	439.00	1.81	0.96	1.00	129.66	1.17	151.31	0.402	No	No	1.23
845	57.77	433.73	1.80	0.92	1.00	128.03	1.16	148.26	0.383	No	No	1.18
846	57.82	429.55	1.78	0.84	1.00	126.71	1.13	143.29	0.354	No	No	1.09
847	57.91	436.73	1.74	0.73	1.00	128.72	1.06	137.09	0.320	No	No	0.98
848	57.96	442.84	1.69	0.63	1.00	130.46	1.00	130.46	0.287	No	No	0.88
849	58.02	458.90	1.66	0.57	1.00	135.16	1.00	135.16	0.310	No	No	0.95
850	58.09	469.26	1.65	0.56	1.00	138.12	1.00	138.12	0.325	No	No	1.00
851	58.16	484.88	1.63	0.56	1.00	142.65	1.00	142.65	0.350	No	No	1.08
852	58.25	491.12	1.64	0.58	1.00	144.36	1.00	144.36	0.360	No	No	1.11
853	58.30	487.65	1.66	0.63	1.00	143.26	1.00	143.26	0.353	No	No	1.09
854	58.40	479.62	1.69	0.68	1.00	140.74	1.00	140.74	0.339	No	No	1.04
855	58.50	468.52	1.71	0.72	1.00	137.31	1.02	139.77	0.334	No	No	1.03
856	58.56	467.50	1.71	0.71	1.00	136.92	1.01	138.70	0.328	No	No	1.01
857	58.64	464.81	1.72	0.73	1.00	136.01	1.03	140.28	0.337	No	No	1.04
858	58.73	474.79	1.73	0.77	1.00	138.81	1.05	145.16	0.364	No	No	1.12
859	58.78	488.15	1.72	0.76	1.00	142.67	1.02	145.87	0.369	No	No	1.14
860	58.88	506.71	1.69	0.74	1.00	147.98	1.00	147.98	0.381	No	No	1.18
861	58.97	511.03	1.66	0.67	1.00	149.10	1.00	149.10	0.388	No	No	1.20
862	59.07	506.24	1.66	0.64	1.00	147.53	1.00	147.53	0.379	No	No	1.17
863	59.13	493.59	1.65	0.61	1.00	143.73	1.00	143.73	0.356	No	No	1.10
864	59.23	484.71	1.65	0.59	1.00	140.99	1.00	140.99	0.341	No	No	1.05

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	59.31	464.47	1.65	0.56	1.00	134.94	1.00	134.94	0.308	No	No	0.95
866	59.38	450.35	1.65	0.54	1.00	130.71	1.00	130.71	0.288	No	No	0.89
867	59.41	439.19	1.66	0.53	1.00	127.40	1.00	127.40	0.272	No	No	0.84
868	59.46	443.57	1.65	0.53	1.00	128.62	1.00	128.62	0.278	No	No	0.86
869	59.51	443.56	1.65	0.52	1.00	128.55	1.00	128.55	0.278	No	No	0.86
870	59.57	451.89	1.67	0.58	1.00	130.91	1.00	130.91	0.289	No	No	0.89
871	59.66	471.05	1.67	0.61	1.00	136.37	1.00	136.37	0.316	No	No	0.98
872	59.75	492.31	1.70	0.71	1.00	142.44	1.00	142.44	0.349	No	No	1.08
873	59.80	506.48	1.71	0.77	1.00	146.48	1.01	147.84	0.380	No	No	1.18
874	59.85	508.64	1.74	0.86	1.00	147.04	1.07	156.99	0.440	No	No	1.36
875	59.91	504.22	1.75	0.88	1.00	145.65	1.08	158.02	0.447	No	No	1.39
876	59.99	498.85	1.77	0.91	1.00	143.96	1.11	159.53	0.458	No	No	1.42
877	60.05	480.97	1.81	1.03	1.00	138.68	1.17	161.59	0.472	No	No	1.47
878	60.09	464.78	1.85	1.12	1.00	133.92	1.20	160.52	0.465	No	No	1.44
879	60.14	444.43	1.88	1.17	1.00	127.94	1.22	156.08	0.434	No	No	1.35
880	60.19	437.86	1.87	1.13	1.00	125.96	1.22	153.23	0.415	No	No	1.29
881	60.22	434.25	1.87	1.11	1.00	124.88	1.21	151.55	0.404	No	No	1.25
882	60.28	412.99	1.89	1.13	1.00	118.63	1.23	145.94	0.369	No	No	1.15
883	60.33	381.24	1.93	1.19	1.00	109.36	1.26	137.48	0.322	No	No	1.00
884	60.38	338.97	2.00	1.32	1.00	97.07	1.31	126.83	0.270	No	No	0.84
885	60.42	309.75	2.05	1.40	1.00	88.57	1.35	119.65	0.239	No	No	0.74
886	60.48	282.02	2.07	1.37	1.00	80.50	1.38	111.02	0.207	No	No	0.64
887	60.57	262.48	2.05	1.17	1.00	74.78	1.36	101.50	0.177	No	No	0.55
888	60.66	243.89	2.02	0.93	1.00	69.35	1.32	91.67	0.152	No	No	0.47
889	60.68	232.16	1.99	0.79	1.00	65.95	1.30	85.85	0.139	No	No	0.43
890	60.69	225.51	1.98	0.72	1.00	64.02	1.29	82.84	0.133	No	No	0.41
891	60.74	217.75	1.99	0.69	1.00	61.75	1.30	80.07	0.128	No	No	0.40
892	60.79	206.27	2.00	0.66	1.00	58.41	1.30	76.18	0.121	No	No	0.38
893	60.84	192.16	2.02	0.64	1.00	54.32	1.32	71.82	0.114	No	No	0.36
894	60.89	182.35	2.03	0.62	1.00	51.47	1.33	68.64	0.110	No	No	0.34
895	60.98	174.35	2.05	0.63	1.00	49.12	1.36	66.57	0.107	No	No	0.33
896	61.03	168.07	2.13	0.84	1.00	47.30	1.46	69.19	0.111	No	No	0.35
897	61.08	164.86	2.24	1.28	1.00	46.35	1.72	79.69	0.127	No	No	0.40
898	61.18	164.63	2.31	1.64	1.00	46.24	1.95	90.12	0.148	No	No	0.46
899	61.23	168.20	2.35	1.96	1.00	47.23	2.12	100.04	0.173	No	No	0.54
900	61.31	194.08	2.24	1.58	1.00	54.62	1.72	94.03	0.157	No	No	0.49
901	61.42	236.42	2.09	1.19	1.00	66.70	1.41	94.11	0.158	No	No	0.49
902	61.47	287.17	1.90	0.74	1.00	81.21	1.24	100.64	0.175	No	No	0.55
903	61.51	331.30	1.79	0.58	1.00	93.81	1.14	107.25	0.195	No	No	0.61
904	61.54	366.14	1.73	0.52	1.00	103.76	1.05	108.54	0.199	No	No	0.62
905	61.57	395.83	1.70	0.53	1.00	112.23	1.00	112.23	0.211	No	No	0.66
906	61.58	418.64	1.67	0.50	1.00	118.74	1.00	118.74	0.236	No	No	0.74
907	61.61	393.43	1.70	0.50	1.00	111.49	1.00	111.49	0.209	No	No	0.65
908	61.63	367.65	1.72	0.50	1.00	104.10	1.03	107.07	0.194	No	No	0.61
909	61.63	257.89	1.94	0.73	1.00	72.70	1.26	91.77	0.152	No	No	0.47
910	61.66	191.36	2.14	1.04	1.00	53.66	1.48	79.27	0.126	No	No	0.39
911	61.67	129.55	2.40	1.69	1.00	35.97	2.37	85.35	0.138	No	No	0.43
912	61.70	152.96	2.31	1.50	1.00	42.66	1.96	83.80	0.135	No	No	0.42

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	61.71	180.90	2.22	1.34	1.00	50.64	1.67	84.55	0.136	No	No	0.43
914	61.76	206.41	2.15	1.24	1.00	57.90	1.51	87.45	0.142	No	No	0.44
915	61.80	228.84	2.10	1.15	1.00	64.28	1.42	91.10	0.150	No	No	0.47
916	61.84	250.40	2.03	1.01	1.00	70.41	1.34	94.04	0.157	No	No	0.49
917	61.86	279.75	1.93	0.78	1.00	78.77	1.26	98.87	0.170	No	No	0.53
918	61.93	312.34	1.82	0.60	1.00	88.02	1.18	103.69	0.184	No	No	0.57
919	61.98	357.76	1.73	0.50	1.00	100.92	1.00	100.92	0.176	No	No	0.55
920	62.04	405.56	1.68	0.50	1.00	114.48	1.00	114.48	0.220	No	No	0.69
921	62.09	451.78	1.64	0.49	1.00	127.59	1.00	127.59	0.273	No	No	0.86
922	62.14	481.91	1.62	0.49	1.00	136.10	1.00	136.10	0.314	No	No	0.98
923	62.19	499.12	1.60	0.47	1.00	140.93	1.00	140.93	0.340	No	No	1.07
924	62.24	508.93	1.59	0.47	1.00	143.65	1.00	143.65	0.356	No	No	1.11
925	62.26	519.32	1.58	0.47	1.00	146.58	1.00	146.58	0.373	No	No	1.17
926	62.29	519.05	1.58	0.47	1.00	146.46	1.00	146.46	0.372	No	No	1.17
927	62.38	515.71	1.60	0.51	1.00	145.37	1.00	145.37	0.366	No	No	1.15
928	62.44	490.28	1.65	0.57	1.00	138.07	1.00	138.07	0.325	No	No	1.02
929	62.46	469.07	1.69	0.62	1.00	132.02	1.00	132.02	0.294	No	No	0.92
930	62.47	448.15	1.70	0.62	1.00	126.07	1.00	126.07	0.266	No	No	0.84
931	62.51	453.68	1.69	0.61	1.00	127.59	1.00	127.59	0.273	No	No	0.86
932	62.56	463.98	1.69	0.61	1.00	130.45	1.00	130.45	0.286	No	No	0.90
933	62.60	477.62	1.68	0.62	1.00	134.26	1.00	134.26	0.305	No	No	0.96
934	62.65	481.73	1.68	0.62	1.00	135.35	1.00	135.35	0.311	No	No	0.97
935	62.70	482.34	1.66	0.58	1.00	135.46	1.00	135.46	0.311	No	No	0.98
936	62.75	483.05	1.65	0.56	1.00	135.59	1.00	135.59	0.312	No	No	0.98
937	62.80	494.83	1.64	0.55	1.00	138.85	1.00	138.85	0.329	No	No	1.03
938	62.85	525.29	1.60	0.52	1.00	147.40	1.00	147.40	0.378	No	No	1.19
939	62.89	569.18	1.56	0.50	1.00	159.73	1.00	159.73	0.459	No	No	1.44
940	62.97	619.66	1.54	0.51	1.00	173.86	1.00	173.86	0.569	No	No	1.79
941	63.04	667.84	1.52	0.52	1.00	187.32	1.00	187.32	0.691	No	No	2.00
942	63.09	703.12	1.50	0.52	1.00	197.18	1.00	197.18	0.793	No	No	2.00
943	63.13	715.51	1.51	0.54	1.00	200.57	1.00	200.57	4.000	No	No	2.00
944	63.19	716.52	1.54	0.60	1.00	200.74	1.00	200.74	4.000	No	No	2.00
945	63.23	720.23	1.57	0.67	1.00	201.69	1.00	201.69	4.000	No	No	2.00
946	63.28	726.78	1.59	0.73	1.00	203.42	1.00	203.42	4.000	No	No	2.00
947	63.32	729.18	1.57	0.68	1.00	204.02	1.00	204.02	4.000	No	No	2.00
948	63.38	725.67	1.49	0.51	1.00	202.89	1.00	202.89	4.000	No	No	2.00
949	63.44	726.68	1.43	0.41	1.00	203.06	1.00	203.06	4.000	No	No	2.00
950	63.52	715.48	1.43	0.40	1.00	199.75	1.00	199.75	0.821	No	No	2.00
951	63.57	697.37	1.49	0.49	1.00	194.57	1.00	194.57	0.765	No	No	2.00
952	63.66	659.58	1.52	0.51	1.00	183.79	1.00	183.79	0.657	No	No	2.00
953	63.73	534.95	1.63	0.58	1.00	148.76	1.00	148.76	0.386	No	No	1.22
954	63.76	455.61	1.72	0.67	1.00	126.50	1.03	130.54	0.287	No	No	0.90
955	63.76	411.85	1.77	0.71	1.00	114.24	1.12	127.66	0.274	No	No	0.86
956	63.78	471.87	1.70	0.64	1.00	131.02	1.00	131.02	0.289	No	No	0.91
957	63.81	512.86	1.67	0.65	1.00	142.46	1.00	142.46	0.349	No	No	1.10
958	63.85	526.43	1.68	0.68	1.00	146.19	1.00	146.19	0.371	No	No	1.17
959	63.86	522.58	1.70	0.74	1.00	145.10	1.00	145.10	0.364	No	No	1.15
960	63.91	497.92	1.74	0.81	1.00	138.14	1.07	148.35	0.384	No	No	1.21

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
961	63.94	483.78	1.77	0.87	1.00	134.14	1.12	150.35	0.396	No	No	1.25
962	63.95	480.34	1.79	0.90	1.00	133.15	1.14	151.38	0.403	No	No	1.27
963	64.00	476.26	1.79	0.91	1.00	131.94	1.14	150.67	0.398	No	No	1.26
964	64.02	473.22	1.79	0.89	1.00	131.08	1.14	149.37	0.390	No	No	1.23
965	64.05	475.78	1.78	0.86	1.00	131.75	1.12	148.02	0.382	No	No	1.20
966	64.09	478.18	1.77	0.83	1.00	132.36	1.11	146.64	0.373	No	No	1.18
967	64.11	480.07	1.75	0.80	1.00	132.86	1.09	144.77	0.362	No	No	1.14
968	64.15	482.26	1.74	0.77	1.00	133.43	1.07	142.44	0.349	No	No	1.10
969	64.20	494.31	1.72	0.74	1.00	136.71	1.03	141.24	0.342	No	No	1.08
970	64.25	512.59	1.70	0.72	1.00	141.74	1.00	141.74	0.345	No	No	1.09
971	64.29	535.70	1.68	0.70	1.00	148.11	1.00	148.11	0.382	No	No	1.21
972	64.34	570.38	1.64	0.65	1.00	157.68	1.00	157.68	0.445	No	No	1.40
973	64.43	605.81	1.60	0.60	1.00	167.40	1.00	167.40	0.516	No	No	1.63
974	64.48	630.95	1.56	0.56	1.00	174.30	1.00	174.30	0.572	No	No	1.81
975	64.53	642.69	1.53	0.51	1.00	177.47	1.00	177.47	0.600	No	No	1.90
976	64.58	655.07	1.52	0.49	1.00	180.82	1.00	180.82	0.630	No	No	1.99
977	64.63	680.65	1.51	0.49	1.00	187.83	1.00	187.83	0.696	No	No	2.00
978	64.68	709.63	1.52	0.55	1.00	195.77	1.00	195.77	0.778	No	No	2.00
979	64.73	718.74	1.53	0.57	1.00	198.20	1.00	198.20	0.804	No	No	2.00
980	64.77	735.60	1.51	0.56	1.00	202.79	1.00	202.79	4.000	No	No	2.00
981	64.82	751.19	1.48	0.51	1.00	207.01	1.00	207.01	4.000	No	No	2.00
982	64.87	732.64	1.49	0.51	1.00	201.76	1.00	201.76	4.000	No	No	2.00
983	64.89	713.98	1.50	0.52	1.00	196.56	1.00	196.56	0.786	No	No	2.00
984	64.93	689.59	1.53	0.54	1.00	189.73	1.00	189.73	0.715	No	No	2.00
985	64.94	715.81	1.51	0.53	1.00	196.96	1.00	196.96	0.791	No	No	2.00
986	64.98	725.69	1.50	0.53	1.00	199.62	1.00	199.62	0.820	No	No	2.00
987	64.99	734.03	1.50	0.52	1.00	201.90	1.00	201.90	4.000	No	No	2.00
988	65.03	732.37	1.50	0.52	1.00	201.35	1.00	201.35	4.000	No	No	2.00
989	65.08	727.04	1.49	0.50	1.00	199.79	1.00	199.79	0.822	No	No	2.00
990	65.13	715.51	1.48	0.47	1.00	196.50	1.00	196.50	0.786	No	No	2.00
991	65.17	703.60	1.46	0.43	1.00	193.13	1.00	193.13	0.750	No	No	2.00
992	65.22	689.29	1.45	0.41	1.00	189.08	1.00	189.08	0.709	No	No	2.00
993	65.23	681.55	1.45	0.40	1.00	186.93	1.00	186.93	0.687	No	No	2.00
994	65.28	679.28	1.46	0.40	1.00	186.22	1.00	186.22	0.681	No	No	2.00
995	65.32	679.65	1.47	0.43	1.00	186.24	1.00	186.24	0.681	No	No	2.00
996	65.37	680.17	1.49	0.45	1.00	186.30	1.00	186.30	0.681	No	No	2.00
997	65.42	684.61	1.50	0.48	1.00	187.42	1.00	187.42	0.692	No	No	2.00
998	65.47	671.65	1.50	0.48	1.00	183.76	1.00	183.76	0.657	No	No	2.00
999	65.48	657.21	1.52	0.49	1.00	179.77	1.00	179.77	0.620	No	No	1.97
1000	65.49	638.86	1.52	0.48	1.00	174.70	1.00	174.70	0.576	No	No	1.83
1001	65.52	636.56	1.52	0.47	1.00	174.01	1.00	174.01	0.570	No	No	1.81
1002	65.57	645.67	1.41	0.30	1.00	176.43	1.00	176.43	0.591	No	No	1.88
1003	65.62	661.16	1.28	0.15	1.00	180.61	1.00	180.61	0.628	No	No	1.99
1004	65.67	682.44	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1005	65.69	697.23	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1006	65.72	719.02	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1007	65.77	752.26	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1008	65.82	790.78	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1009	65.86	811.97	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1010	65.86	833.63	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1011	65.91	854.04	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1012	65.96	878.41	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_t: Total cone resistance
I_c: Soil behavior type index
Fr: Normalized friction ratio (%)
n: Stress exponent
Q_{tn}: Normalized cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
0.01	2.00	0.00	0.00	0.03	0.00	0.04	2.00	0.00	0.00	0.03	0.00
0.08	2.00	0.00	0.00	0.04	0.00	0.10	2.00	0.00	0.00	0.02	0.00
0.13	2.00	0.00	0.00	0.03	0.00	0.18	2.00	0.00	0.00	0.04	0.00
0.22	2.00	0.00	0.00	0.05	0.00	0.27	2.00	0.00	0.00	0.05	0.00
0.33	2.00	0.00	0.00	0.05	0.00	0.36	2.00	0.00	0.00	0.03	0.00
0.37	2.00	0.00	0.00	0.01	0.00	0.38	2.00	0.00	0.00	0.01	0.00
0.42	2.00	0.00	0.00	0.04	0.00	0.44	2.00	0.00	0.00	0.03	0.00
0.47	2.00	0.00	0.00	0.02	0.00	0.47	2.00	0.00	0.00	0.01	0.00
0.52	2.00	0.00	0.00	0.04	0.00	0.56	2.00	0.00	0.00	0.05	0.00
0.58	2.00	0.00	0.00	0.01	0.00	0.61	2.00	0.00	0.00	0.03	0.00
0.66	2.00	0.00	0.00	0.05	0.00	0.76	2.00	0.00	0.00	0.09	0.00
0.80	2.00	0.00	0.00	0.05	0.00	0.81	2.00	0.00	0.00	0.01	0.00
0.85	2.00	0.00	0.00	0.04	0.00	0.86	2.00	0.00	0.00	0.01	0.00
0.90	2.00	0.00	0.00	0.04	0.00	0.95	2.00	0.00	0.00	0.04	0.00
1.00	2.00	0.00	0.00	0.05	0.00	1.05	2.00	0.00	0.00	0.06	0.00
1.14	2.00	0.00	0.00	0.09	0.00	1.24	2.00	0.00	0.00	0.09	0.00
1.31	2.00	0.00	0.00	0.08	0.00	1.36	2.00	0.00	0.00	0.05	0.00
1.37	2.00	0.00	0.00	0.01	0.00	1.39	2.00	0.00	0.00	0.02	0.00
1.43	2.00	0.00	0.00	0.04	0.00	1.44	2.00	0.00	0.00	0.01	0.00
1.49	2.00	0.00	0.00	0.06	0.00	1.53	2.00	0.00	0.00	0.04	0.00
1.58	2.00	0.00	0.00	0.05	0.00	1.63	2.00	0.00	0.00	0.05	0.00
1.68	2.00	0.00	0.00	0.05	0.00	1.72	2.00	0.00	0.00	0.05	0.00
1.77	2.00	0.00	0.00	0.05	0.00	1.82	2.00	0.00	0.00	0.05	0.00
1.86	2.00	0.00	0.00	0.04	0.00	1.92	2.00	0.00	0.00	0.05	0.00
1.97	2.00	0.00	0.00	0.05	0.00	2.01	2.00	0.00	0.00	0.05	0.00
2.09	2.00	0.00	0.00	0.07	0.00	2.16	2.00	0.00	0.00	0.07	0.00
2.20	2.00	0.00	0.00	0.04	0.00	2.25	2.00	0.00	0.00	0.05	0.00
2.31	2.00	0.00	0.00	0.06	0.00	2.37	2.00	0.00	0.00	0.06	0.00
2.40	2.00	0.00	0.00	0.03	0.00	2.46	2.00	0.00	0.00	0.06	0.00
2.54	2.00	0.00	0.00	0.08	0.00	2.59	2.00	0.00	0.00	0.05	0.00
2.69	2.00	0.00	0.00	0.10	0.00	2.74	2.00	0.00	0.00	0.05	0.00
2.83	2.00	0.00	0.00	0.10	0.00	2.88	2.00	0.00	0.00	0.05	0.00
2.98	2.00	0.00	0.00	0.10	0.00	3.03	2.00	0.00	0.00	0.05	0.00
3.12	2.00	0.00	0.00	0.08	0.00	3.21	2.00	0.00	0.00	0.09	0.00
3.27	2.00	0.00	0.00	0.06	0.00	3.34	2.00	0.00	0.00	0.08	0.00
3.41	2.00	0.00	0.00	0.07	0.00	3.51	2.00	0.00	0.00	0.10	0.00
3.55	2.00	0.00	0.00	0.05	0.00	3.65	2.00	0.00	0.00	0.10	0.00
3.75	2.00	0.00	0.00	0.10	0.00	3.83	2.00	0.00	0.00	0.09	0.00
3.94	2.00	0.00	0.00	0.10	0.00	4.04	2.00	0.00	0.00	0.10	0.00
4.13	2.00	0.00	0.00	0.09	0.00	4.24	2.00	0.00	0.00	0.11	0.00
4.38	2.00	0.00	0.00	0.13	0.00	4.50	2.00	0.00	0.00	0.12	0.00
4.62	2.00	0.00	0.00	0.12	0.00	4.71	2.00	0.00	0.00	0.10	0.00
4.75	2.00	0.00	0.00	0.04	0.00	4.84	2.00	0.00	0.00	0.08	0.00
4.89	2.00	0.00	0.00	0.05	0.00	4.94	2.00	0.00	0.00	0.05	0.00
4.98	2.00	0.00	0.00	0.04	0.00	5.07	2.00	0.00	0.00	0.09	0.00
5.13	2.00	0.00	0.00	0.05	0.00	5.17	2.00	0.00	0.00	0.05	0.00
5.27	2.00	0.00	0.00	0.09	0.00	5.32	2.00	0.00	0.00	0.05	0.00
5.42	2.00	0.00	0.00	0.10	0.00	5.46	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
5.56	2.00	0.00	0.00	0.10	0.00	5.61	2.00	0.00	0.00	0.05	0.00
5.71	2.00	0.00	0.00	0.09	0.00	5.78	2.00	0.00	0.00	0.08	0.00
5.85	2.00	0.00	0.00	0.07	0.00	5.95	2.00	0.00	0.00	0.10	0.00
6.00	2.00	0.00	0.00	0.05	0.00	6.09	2.00	0.00	0.00	0.10	0.00
6.14	2.00	0.00	0.00	0.05	0.00	6.24	2.00	0.00	0.00	0.09	0.00
6.30	2.00	0.00	0.00	0.06	0.00	6.38	2.00	0.00	0.00	0.09	0.00
6.46	2.00	0.00	0.00	0.08	0.00	6.50	2.00	0.00	0.00	0.04	0.00
6.56	2.00	0.00	0.00	0.07	0.00	6.63	2.00	0.00	0.00	0.06	0.00
6.68	2.00	0.00	0.00	0.05	0.00	6.76	2.00	0.00	0.00	0.08	0.00
6.82	2.00	0.00	0.00	0.06	0.00	6.88	2.00	0.00	0.00	0.06	0.00
6.96	2.00	0.00	0.00	0.08	0.00	7.03	2.00	0.00	0.00	0.07	0.00
7.11	2.00	0.00	0.00	0.08	0.00	7.16	2.00	0.00	0.00	0.05	0.00
7.26	2.00	0.00	0.00	0.10	0.00	7.31	2.00	0.00	0.00	0.05	0.00
7.40	2.00	0.00	0.00	0.09	0.00	7.45	2.00	0.00	0.00	0.05	0.00
7.54	2.00	0.00	0.00	0.09	0.00	7.60	2.00	0.00	0.00	0.06	0.00
7.68	2.00	0.00	0.00	0.09	0.00	7.74	2.00	0.00	0.00	0.05	0.00
7.83	2.00	0.00	0.00	0.09	0.00	7.90	2.00	0.00	0.00	0.07	0.00
7.98	2.00	0.00	0.00	0.08	0.00	8.05	2.00	0.00	0.00	0.07	0.00
8.12	2.00	0.00	0.00	0.08	0.00	8.19	2.00	0.00	0.00	0.07	0.00
8.27	2.00	0.00	0.00	0.07	0.00	8.36	2.00	0.00	0.00	0.10	0.00
8.41	2.00	0.00	0.00	0.05	0.00	8.50	2.00	0.00	0.00	0.09	0.00
8.60	2.00	0.00	0.00	0.10	0.00	8.70	2.00	0.00	0.00	0.09	0.00
8.74	2.00	0.00	0.00	0.05	0.00	8.78	2.00	0.00	0.00	0.03	0.00
8.81	2.00	0.00	0.00	0.03	0.00	8.86	2.00	0.00	0.00	0.05	0.00
8.91	2.00	0.00	0.00	0.04	0.00	8.94	2.00	0.00	0.00	0.04	0.00
9.02	2.00	0.00	0.00	0.08	0.00	9.10	2.00	0.00	0.00	0.07	0.00
9.17	2.00	0.00	0.00	0.07	0.00	9.22	2.00	0.00	0.00	0.05	0.00
9.31	2.00	0.00	0.00	0.09	0.00	9.37	2.00	0.00	0.00	0.06	0.00
9.42	2.00	0.00	0.00	0.05	0.00	9.52	2.00	0.00	0.00	0.10	0.00
9.60	2.00	0.00	0.00	0.08	0.00	9.66	2.00	0.00	0.00	0.06	0.00
9.74	2.00	0.00	0.00	0.08	0.00	9.81	2.00	0.00	0.00	0.07	0.00
9.89	2.00	0.00	0.00	0.08	0.00	9.98	2.00	0.00	0.00	0.09	0.00
10.03	2.00	0.00	0.00	0.06	0.00	10.13	2.00	0.00	0.00	0.09	0.00
10.23	2.00	0.00	0.00	0.10	0.00	10.32	2.00	0.00	0.00	0.09	0.00
10.38	2.00	0.00	0.00	0.06	0.00	10.47	2.00	0.00	0.00	0.09	0.00
10.57	2.00	0.00	0.00	0.10	0.00	10.66	2.00	0.00	0.00	0.09	0.00
10.76	2.00	0.00	0.00	0.10	0.00	10.85	2.00	0.00	0.00	0.10	0.00
10.92	2.00	0.00	0.00	0.07	0.00	11.00	2.00	0.00	0.00	0.08	0.00
11.07	2.00	0.00	0.00	0.06	0.00	11.10	2.00	0.00	0.00	0.03	0.00
11.15	2.00	0.00	0.00	0.05	0.00	11.19	2.00	0.00	0.00	0.04	0.00
11.24	2.00	0.00	0.00	0.05	0.00	11.29	2.00	0.00	0.00	0.05	0.00
11.34	2.00	0.00	0.00	0.05	0.00	11.40	2.00	0.00	0.00	0.07	0.00
11.47	2.00	0.00	0.00	0.06	0.00	11.53	2.00	0.00	0.00	0.06	0.00
11.58	2.00	0.00	0.00	0.04	0.00	11.65	2.00	0.00	0.00	0.07	0.00
11.72	2.00	0.00	0.00	0.07	0.00	11.77	2.00	0.00	0.00	0.05	0.00
11.82	2.00	0.00	0.00	0.05	0.00	11.88	2.00	0.00	0.00	0.06	0.00
11.97	2.00	0.00	0.00	0.09	0.00	12.02	2.00	0.00	0.00	0.05	0.00
12.06	2.00	0.00	0.00	0.05	0.00	12.11	2.00	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
12.21	2.00	0.00	0.00	0.10	0.00	12.25	2.00	0.00	0.00	0.04	0.00
12.30	2.00	0.00	0.00	0.05	0.00	12.31	2.00	0.00	0.00	0.01	0.00
12.32	2.00	0.00	0.00	0.01	0.00	12.35	2.00	0.00	0.00	0.03	0.00
12.40	2.00	0.00	0.00	0.05	0.00	12.45	2.00	0.00	0.00	0.05	0.00
12.52	2.00	0.00	0.00	0.08	0.00	12.56	2.00	0.00	0.00	0.04	0.00
12.62	2.00	0.00	0.00	0.06	0.00	12.65	2.00	0.00	0.00	0.04	0.00
12.71	2.00	0.00	0.00	0.05	0.00	12.76	2.00	0.00	0.00	0.05	0.00
12.83	2.00	0.00	0.00	0.07	0.00	12.88	2.00	0.00	0.00	0.05	0.00
12.93	2.00	0.00	0.00	0.05	0.00	12.98	2.00	0.00	0.00	0.05	0.00
13.03	2.00	0.00	0.00	0.05	0.00	13.04	2.00	0.00	0.00	0.01	0.00
13.07	2.00	0.00	0.00	0.04	0.00	13.13	2.00	0.00	0.00	0.05	0.00
13.17	2.00	0.00	0.00	0.04	0.00	13.22	2.00	0.00	0.00	0.05	0.00
13.27	2.00	0.00	0.00	0.05	0.00	13.32	2.00	0.00	0.00	0.04	0.00
13.37	2.00	0.00	0.00	0.05	0.00	13.41	2.00	0.00	0.00	0.04	0.00
13.46	2.00	0.00	0.00	0.05	0.00	13.51	2.00	0.00	0.00	0.04	0.00
13.56	2.00	0.00	0.00	0.05	0.00	13.60	2.00	0.00	0.00	0.04	0.00
13.66	2.00	0.00	0.00	0.06	0.00	13.75	2.00	0.00	0.00	0.09	0.00
13.80	2.00	0.00	0.00	0.05	0.00	13.89	2.00	0.00	0.00	0.09	0.00
13.94	2.00	0.00	0.00	0.05	0.00	13.99	2.00	0.00	0.00	0.05	0.00
14.09	2.00	0.00	0.00	0.09	0.00	14.14	2.00	0.00	0.00	0.06	0.00
14.23	2.00	0.00	0.00	0.09	0.00	14.28	2.00	0.00	0.00	0.05	0.00
14.38	2.00	0.00	0.00	0.10	0.00	14.42	2.00	0.00	0.00	0.04	0.00
14.52	2.00	0.00	0.00	0.10	0.00	14.57	2.00	0.00	0.00	0.05	0.00
14.67	2.00	0.00	0.00	0.10	0.00	14.68	2.00	0.00	0.00	0.01	0.00
14.70	2.00	0.00	0.00	0.02	0.00	14.75	2.00	0.00	0.00	0.05	0.00
14.80	2.00	0.00	0.00	0.04	0.00	14.89	2.00	0.00	0.00	0.10	0.00
14.94	2.00	0.00	0.00	0.05	0.00	15.04	2.00	0.00	0.00	0.10	0.00
15.13	2.00	0.00	0.00	0.09	0.00	15.21	2.00	0.00	0.00	0.08	0.00
15.28	2.00	0.00	0.00	0.07	0.00	15.38	2.00	0.00	0.00	0.10	0.00
15.47	2.00	0.00	0.00	0.09	0.00	15.57	2.00	0.00	0.00	0.10	0.00
15.67	2.00	0.00	0.00	0.09	0.00	15.77	2.00	0.00	0.00	0.10	0.00
15.86	2.00	0.00	0.00	0.10	0.00	15.96	2.00	0.00	0.00	0.09	0.00
16.05	2.00	0.00	0.00	0.10	0.00	16.15	2.00	0.00	0.00	0.09	0.00
16.25	2.00	0.00	0.00	0.10	0.00	16.31	2.00	0.00	0.00	0.06	0.00
16.39	2.00	0.00	0.00	0.08	0.00	16.48	2.00	0.00	0.00	0.10	0.00
16.59	2.00	0.00	0.00	0.10	0.00	16.68	2.00	0.00	0.00	0.09	0.00
16.76	2.00	0.00	0.00	0.08	0.00	16.86	2.00	0.00	0.00	0.10	0.00
16.92	2.00	0.00	0.00	0.06	0.00	17.02	2.00	0.00	0.00	0.09	0.00
17.11	2.00	0.00	0.00	0.10	0.00	17.22	2.00	0.00	0.00	0.11	0.00
17.35	2.00	0.00	0.00	0.13	0.00	17.45	2.00	0.00	0.00	0.10	0.00
17.55	2.00	0.00	0.00	0.10	0.00	17.61	2.00	0.00	0.00	0.07	0.00
17.64	2.00	0.00	0.00	0.03	0.00	17.70	2.00	0.00	0.00	0.06	0.00
17.75	2.00	0.00	0.00	0.04	0.00	17.80	2.00	0.00	0.00	0.05	0.00
17.85	2.00	0.00	0.00	0.05	0.00	17.94	2.00	0.00	0.00	0.10	0.00
17.99	2.00	0.00	0.00	0.04	0.00	18.09	2.00	0.00	0.00	0.10	0.00
18.15	2.00	0.00	0.00	0.06	0.00	18.23	2.00	0.00	0.00	0.08	0.00
18.33	2.00	0.00	0.00	0.10	0.00	18.43	2.00	0.00	0.00	0.10	0.00
18.52	2.00	0.00	0.00	0.10	0.00	18.59	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
18.72	2.00	0.00	0.00	0.13	0.00	18.81	2.00	0.00	0.00	0.09	0.00
18.87	2.00	0.00	0.00	0.06	0.00	18.95	2.00	0.00	0.00	0.08	0.00
19.05	2.00	0.00	0.00	0.10	0.00	19.14	2.00	0.00	0.00	0.09	0.00
19.22	2.00	0.00	0.00	0.07	0.00	19.29	2.00	0.00	0.00	0.08	0.00
19.38	2.00	0.00	0.00	0.09	0.00	19.44	2.00	0.00	0.00	0.06	0.00
19.53	2.00	0.00	0.00	0.09	0.00	19.62	2.00	0.00	0.00	0.09	0.00
19.69	2.00	0.00	0.00	0.07	0.00	19.79	2.00	0.00	0.00	0.10	0.00
19.86	2.00	0.00	0.00	0.07	0.00	19.97	2.00	0.00	0.00	0.10	0.00
20.07	2.00	0.00	0.00	0.10	0.00	20.16	2.00	0.00	0.00	0.09	0.00
20.26	2.00	0.00	0.00	0.10	0.00	20.34	2.00	0.00	0.00	0.08	0.00
20.43	2.00	0.00	0.00	0.09	0.00	20.50	2.00	0.00	0.00	0.07	0.00
20.60	2.00	0.00	0.00	0.10	0.00	20.62	2.00	0.00	0.00	0.02	0.00
20.63	2.00	0.00	0.00	0.01	0.00	20.68	2.00	0.00	0.00	0.05	0.00
20.73	2.00	0.00	0.00	0.05	0.00	20.82	2.00	0.00	0.00	0.09	0.00
20.87	2.00	0.00	0.00	0.05	0.00	20.91	2.00	0.00	0.00	0.05	0.00
20.96	2.00	0.00	0.00	0.05	0.00	21.05	2.00	0.00	0.00	0.09	0.00
21.11	2.00	0.00	0.00	0.06	0.00	21.17	2.00	0.00	0.00	0.06	0.00
21.25	2.00	0.00	0.00	0.08	0.00	21.30	2.00	0.00	0.00	0.06	0.00
21.37	2.00	0.00	0.00	0.06	0.00	21.45	2.00	0.00	0.00	0.08	0.00
21.49	2.00	0.00	0.00	0.05	0.00	21.58	2.00	0.00	0.00	0.09	0.00
21.64	2.00	0.00	0.00	0.06	0.00	21.69	2.00	0.00	0.00	0.05	0.00
21.78	2.00	0.00	0.00	0.09	0.00	21.83	2.00	0.00	0.00	0.05	0.00
21.89	2.00	0.00	0.00	0.06	0.00	21.98	2.00	0.00	0.00	0.09	0.00
22.03	2.00	0.00	0.00	0.05	0.00	22.12	2.00	0.00	0.00	0.09	0.00
22.22	2.00	0.00	0.00	0.10	0.00	22.26	2.00	0.00	0.00	0.05	0.00
22.36	2.00	0.00	0.00	0.09	0.00	22.41	2.00	0.00	0.00	0.05	0.00
22.51	2.00	0.00	0.00	0.10	0.00	22.60	2.00	0.00	0.00	0.09	0.00
22.70	2.00	0.00	0.00	0.10	0.00	22.75	2.00	0.00	0.00	0.05	0.00
22.84	2.00	0.00	0.00	0.10	0.00	22.89	2.00	0.00	0.00	0.05	0.00
22.90	2.00	0.00	0.00	0.01	0.00	22.94	2.00	0.00	0.00	0.04	0.00
23.00	2.00	0.00	0.00	0.06	0.00	23.08	2.00	0.00	0.00	0.08	0.00
23.13	2.00	0.00	0.00	0.05	0.00	23.20	2.00	0.00	0.00	0.07	0.00
23.27	2.00	0.00	0.00	0.07	0.00	23.33	2.00	0.00	0.00	0.06	0.00
23.42	2.00	0.00	0.00	0.09	0.00	23.48	2.00	0.00	0.00	0.06	0.00
23.57	2.00	0.00	0.00	0.09	0.00	23.61	2.00	0.00	0.00	0.04	0.00
23.66	2.00	0.00	0.00	0.05	0.00	23.73	2.00	0.00	0.00	0.07	0.00
23.80	2.00	0.00	0.00	0.07	0.00	23.85	2.00	0.00	0.00	0.05	0.00
23.94	2.00	0.00	0.00	0.09	0.00	24.00	2.00	0.00	0.00	0.05	0.00
24.09	2.00	0.00	0.00	0.09	0.00	24.16	2.00	0.00	0.00	0.07	0.00
24.24	2.00	0.00	0.00	0.07	0.00	24.33	2.00	0.00	0.00	0.10	0.00
24.43	2.00	0.00	0.00	0.10	0.00	24.52	2.00	0.00	0.00	0.09	0.00
24.58	2.00	0.00	0.00	0.06	0.00	24.59	2.00	0.00	0.00	0.01	0.00
24.63	2.00	0.00	0.00	0.04	0.00	24.68	2.00	0.00	0.00	0.05	0.00
24.77	2.00	0.00	0.00	0.10	0.00	24.82	2.00	0.00	0.00	0.05	0.00
24.92	2.00	0.00	0.00	0.10	0.00	25.01	2.00	0.00	0.00	0.09	0.00
25.06	2.00	0.00	0.00	0.06	0.00	25.16	2.00	0.00	0.00	0.09	0.00
25.25	2.00	0.00	0.00	0.09	0.00	25.30	2.00	0.00	0.00	0.05	0.00
25.41	2.00	0.00	0.00	0.11	0.00	25.49	2.00	0.00	0.00	0.09	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
25.55	2.00	0.00	0.00	0.05	0.00	25.64	2.00	0.00	0.00	0.09	0.00
25.70	2.00	0.00	0.00	0.06	0.00	25.79	2.00	0.00	0.00	0.09	0.00
25.89	2.00	0.00	0.00	0.10	0.00	25.94	2.00	0.00	0.00	0.06	0.00
26.02	2.00	0.00	0.00	0.08	0.00	26.12	2.00	0.00	0.00	0.09	0.00
26.17	2.00	0.00	0.00	0.05	0.00	26.28	2.00	0.00	0.00	0.11	0.00
26.36	2.00	0.00	0.00	0.09	0.00	26.45	2.00	0.00	0.00	0.09	0.00
26.50	2.00	0.00	0.00	0.05	0.00	26.61	2.00	0.00	0.00	0.11	0.00
26.70	2.00	0.00	0.00	0.09	0.00	26.77	2.00	0.00	0.00	0.07	0.00
26.85	2.00	0.00	0.00	0.08	0.00	26.94	2.00	0.00	0.00	0.09	0.00
27.04	2.00	0.00	0.00	0.09	0.00	27.14	2.00	0.00	0.00	0.10	0.00
27.23	2.00	0.00	0.00	0.09	0.00	27.28	2.00	0.00	0.00	0.05	0.00
27.29	2.00	0.00	0.00	0.01	0.00	27.38	2.00	0.00	0.00	0.09	0.00
27.48	2.00	0.00	0.00	0.10	0.00	27.57	2.00	0.00	0.00	0.09	0.00
27.64	2.00	0.00	0.00	0.07	0.00	27.65	2.00	0.00	0.00	0.01	0.00
27.74	2.00	0.00	0.00	0.09	0.00	27.80	2.00	0.00	0.00	0.06	0.00
27.90	2.00	0.00	0.00	0.10	0.00	27.99	2.00	0.00	0.00	0.09	0.00
28.07	2.00	0.00	0.00	0.08	0.00	28.16	2.00	0.00	0.00	0.09	0.00
28.25	2.00	0.00	0.00	0.09	0.00	28.34	2.00	0.00	0.00	0.09	0.00
28.44	2.00	0.00	0.00	0.10	0.00	28.53	2.00	0.00	0.00	0.09	0.00
28.62	2.00	0.00	0.00	0.09	0.00	28.76	2.00	0.00	0.00	0.14	0.00
28.86	2.00	0.00	0.00	0.10	0.00	28.96	2.00	0.00	0.00	0.10	0.00
29.08	2.00	0.00	0.00	0.11	0.00	29.19	2.00	0.00	0.00	0.12	0.00
29.29	2.00	0.00	0.00	0.10	0.00	29.39	2.00	0.00	0.00	0.09	0.00
29.50	2.00	0.00	0.00	0.11	0.00	29.63	2.00	0.00	0.00	0.13	0.00
29.65	2.00	0.00	0.00	0.02	0.00	29.66	2.00	0.00	0.00	0.01	0.00
29.72	2.00	0.00	0.00	0.06	0.00	29.80	2.00	0.00	0.00	0.09	0.00
29.85	2.00	0.00	0.00	0.05	0.00	29.94	2.00	0.00	0.00	0.09	0.00
30.00	2.00	0.00	0.00	0.06	0.00	30.05	2.00	0.00	0.00	0.05	0.00
30.14	2.00	0.00	0.00	0.09	0.00	30.19	2.00	0.00	0.00	0.05	0.00
30.24	2.00	0.00	0.00	0.05	0.00	30.29	1.14	0.00	0.00	0.05	0.00
30.38	1.12	0.00	0.00	0.09	0.00	30.43	1.09	0.00	0.00	0.05	0.00
30.48	1.05	0.00	0.00	0.05	0.00	30.54	1.02	0.00	0.00	0.06	0.00
30.62	1.00	0.00	0.00	0.08	0.00	30.67	0.99	0.01	90006887.17	0.05	0.00
30.72	0.99	0.01	161806562 5614.33	0.05	0.00	30.76	1.00	0.00	811703898	0.04	0.00
30.86	1.01	0.00	0.00	0.10	0.00	30.91	1.03	0.00	0.00	0.05	0.00
30.95	1.06	0.00	0.00	0.05	0.00	31.03	1.09	0.00	0.00	0.07	0.00
31.10	1.12	0.00	0.00	0.07	0.00	31.15	1.15	0.00	0.00	0.05	0.00
31.20	1.19	0.00	0.00	0.05	0.00	31.26	1.22	0.00	0.00	0.06	0.00
31.34	1.21	0.00	0.00	0.08	0.00	31.37	1.20	0.00	0.00	0.02	0.00
31.38	1.18	0.00	0.00	0.01	0.00	31.43	1.19	0.00	0.00	0.05	0.00
31.47	1.13	0.00	0.00	0.05	0.00	31.55	1.06	0.00	0.00	0.07	0.00
31.59	0.95	0.05	66.65	0.05	0.00	31.66	0.83	0.17	2.22	0.06	0.02
31.73	0.73	0.27	1.05	0.08	0.03	31.78	0.65	0.35	0.76	0.05	0.03
31.84	0.61	0.39	0.65	0.06	0.04	31.93	0.60	0.40	0.62	0.09	0.06
31.98	0.61	0.39	0.64	0.05	0.03	32.02	0.64	0.36	0.71	0.05	0.03
32.09	0.67	0.33	0.80	0.07	0.03	32.16	0.69	0.31	0.87	0.07	0.03
32.22	0.70	0.30	0.90	0.05	0.03	32.27	0.70	0.30	0.90	0.05	0.02
32.34	0.69	0.31	0.89	0.07	0.03	32.42	0.69	0.31	0.88	0.08	0.04

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
32.46	0.68	0.32	0.86	0.04	0.02	32.54	0.68	0.32	0.84	0.09	0.04
32.60	0.66	0.34	0.79	0.06	0.03	32.67	0.66	0.34	0.77	0.07	0.03
32.75	0.66	0.34	0.78	0.08	0.04	32.81	0.68	0.32	0.86	0.06	0.03
32.89	0.71	0.29	0.96	0.08	0.04	32.94	0.69	0.31	0.89	0.05	0.02
32.95	0.71	0.29	0.95	0.01	0.00	33.00	0.72	0.28	1.04	0.05	0.02
33.06	0.79	0.21	1.49	0.06	0.02	33.11	0.80	0.20	1.68	0.05	0.01
33.20	0.80	0.20	1.65	0.09	0.03	33.25	0.79	0.21	1.56	0.05	0.02
33.34	0.78	0.22	1.47	0.09	0.03	33.38	0.79	0.21	1.49	0.04	0.01
33.48	0.80	0.20	1.65	0.10	0.03	33.58	0.83	0.17	2.07	0.10	0.03
33.63	0.87	0.13	3.40	0.04	0.01	33.73	0.92	0.08	9.37	0.10	0.01
33.82	0.98	0.02	7362.55	0.09	0.00	33.87	1.05	0.00	0.00	0.05	0.00
33.96	1.13	0.00	0.00	0.09	0.00	34.02	1.23	0.00	0.00	0.06	0.00
34.11	1.37	0.00	0.00	0.09	0.00	34.18	1.54	0.00	0.00	0.07	0.00
34.26	1.72	0.00	0.00	0.08	0.00	34.35	1.91	0.00	0.00	0.09	0.00
34.44	2.00	0.00	0.00	0.09	0.00	34.49	2.00	0.00	0.00	0.05	0.00
34.59	2.00	0.00	0.00	0.10	0.00	34.69	2.00	0.00	0.00	0.09	0.00
34.76	2.00	0.00	0.00	0.07	0.00	34.83	2.00	0.00	0.00	0.08	0.00
34.93	2.00	0.00	0.00	0.10	0.00	35.02	2.00	0.00	0.00	0.09	0.00
35.12	2.00	0.00	0.00	0.10	0.00	35.22	1.94	0.00	0.00	0.10	0.00
35.30	1.83	0.00	0.00	0.08	0.00	35.38	1.60	0.00	0.00	0.08	0.00
35.43	1.44	0.00	0.00	0.04	0.00	35.46	1.32	0.00	0.00	0.04	0.00
35.51	2.00	0.00	0.00	0.05	0.00	35.56	2.00	0.00	0.00	0.04	0.00
35.66	2.00	0.00	0.00	0.10	0.00	35.70	2.00	0.00	0.00	0.05	0.00
35.80	2.00	0.00	0.00	0.10	0.00	35.89	2.00	0.00	0.00	0.09	0.00
35.96	2.00	0.00	0.00	0.07	0.00	36.04	2.00	0.00	0.00	0.08	0.00
36.14	2.00	0.00	0.00	0.10	0.00	36.19	2.00	0.00	0.00	0.05	0.00
36.28	2.00	0.00	0.00	0.09	0.00	36.33	2.00	0.00	0.00	0.04	0.00
36.42	2.00	0.00	0.00	0.09	0.00	36.48	2.00	0.00	0.00	0.05	0.00
36.52	2.00	0.00	0.00	0.05	0.00	36.62	2.00	0.00	0.00	0.10	0.00
36.68	2.00	0.00	0.00	0.06	0.00	36.77	2.00	0.00	0.00	0.09	0.00
36.86	2.00	0.00	0.00	0.09	0.00	36.90	2.00	0.00	0.00	0.05	0.00
37.00	2.00	0.00	0.00	0.10	0.00	37.10	2.00	0.00	0.00	0.10	0.00
37.20	2.00	0.00	0.00	0.10	0.00	37.29	2.00	0.00	0.00	0.09	0.00
37.39	2.00	0.00	0.00	0.10	0.00	37.49	1.28	0.00	0.00	0.10	0.00
37.53	1.39	0.00	0.00	0.05	0.00	37.58	1.51	0.00	0.00	0.04	0.00
37.62	1.60	0.00	0.00	0.05	0.00	37.69	1.74	0.00	0.00	0.07	0.00
37.77	1.86	0.00	0.00	0.08	0.00	37.82	1.96	0.00	0.00	0.05	0.00
37.87	2.00	0.00	0.00	0.05	0.00	37.91	2.00	0.00	0.00	0.05	0.00
37.97	1.95	0.00	0.00	0.06	0.00	38.06	1.85	0.00	0.00	0.09	0.00
38.10	1.75	0.00	0.00	0.04	0.00	38.17	1.67	0.00	0.00	0.07	0.00
38.25	1.60	0.00	0.00	0.08	0.00	38.35	1.54	0.00	0.00	0.09	0.00
38.40	1.48	0.00	0.00	0.05	0.00	38.46	1.45	0.00	0.00	0.06	0.00
38.54	1.43	0.00	0.00	0.08	0.00	38.60	1.41	0.00	0.00	0.06	0.00
38.69	1.41	0.00	0.00	0.08	0.00	38.74	1.43	0.00	0.00	0.05	0.00
38.83	1.46	0.00	0.00	0.09	0.00	38.88	1.45	0.00	0.00	0.05	0.00
38.97	1.43	0.00	0.00	0.09	0.00	39.02	1.38	0.00	0.00	0.05	0.00
39.11	1.34	0.00	0.00	0.09	0.00	39.16	1.27	0.00	0.00	0.06	0.00
39.23	1.14	0.00	0.00	0.06	0.00	39.24	1.08	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
39.28	1.05	0.00	0.00	0.04	0.00	39.32	1.07	0.00	0.00	0.05	0.00
39.39	2.00	0.00	0.00	0.06	0.00	39.47	2.00	0.00	0.00	0.08	0.00
39.54	2.00	0.00	0.00	0.07	0.00	39.62	2.00	0.00	0.00	0.08	0.00
39.71	2.00	0.00	0.00	0.09	0.00	39.76	2.00	0.00	0.00	0.05	0.00
39.85	2.00	0.00	0.00	0.09	0.00	39.90	2.00	0.00	0.00	0.06	0.00
40.00	2.00	0.00	0.00	0.10	0.00	40.06	2.00	0.00	0.00	0.06	0.00
40.15	2.00	0.00	0.00	0.09	0.00	40.21	2.00	0.00	0.00	0.06	0.00
40.29	2.00	0.00	0.00	0.08	0.00	40.35	2.00	0.00	0.00	0.06	0.00
40.43	2.00	0.00	0.00	0.08	0.00	40.52	2.00	0.00	0.00	0.09	0.00
40.58	2.00	0.00	0.00	0.05	0.00	40.67	2.00	0.00	0.00	0.10	0.00
40.77	2.00	0.00	0.00	0.09	0.00	40.84	2.00	0.00	0.00	0.07	0.00
40.89	2.00	0.00	0.00	0.05	0.00	40.94	2.00	0.00	0.00	0.05	0.00
41.03	2.00	0.00	0.00	0.10	0.00	41.08	2.00	0.00	0.00	0.05	0.00
41.14	2.00	0.00	0.00	0.06	0.00	41.22	2.00	0.00	0.00	0.08	0.00
41.28	0.45	0.55	0.42	0.06	0.03	41.33	0.46	0.54	0.44	0.05	0.03
41.42	0.49	0.51	0.46	0.09	0.05	41.47	0.52	0.48	0.50	0.05	0.03
41.52	0.55	0.45	0.54	0.06	0.03	41.62	0.58	0.42	0.60	0.09	0.04
41.67	0.63	0.37	0.70	0.05	0.02	41.76	0.69	0.31	0.88	0.09	0.03
41.82	0.76	0.24	1.23	0.06	0.02	41.90	0.81	0.19	1.83	0.08	0.02
41.99	0.85	0.15	2.80	0.09	0.01	42.05	0.88	0.12	3.80	0.06	0.01
42.15	0.88	0.12	3.96	0.10	0.01	42.23	0.87	0.13	3.38	0.09	0.01
42.30	0.85	0.15	2.55	0.07	0.01	42.38	0.81	0.19	1.79	0.08	0.02
42.48	0.75	0.25	1.21	0.10	0.03	42.57	0.70	0.30	0.92	0.09	0.03
42.64	0.66	0.34	0.76	0.07	0.02	42.72	0.62	0.38	0.67	0.08	0.03
42.82	0.58	0.42	0.60	0.10	0.04	42.90	0.56	0.44	0.55	0.08	0.04
42.97	0.55	0.45	0.54	0.07	0.03	43.06	0.55	0.45	0.54	0.09	0.04
43.15	0.53	0.47	0.52	0.09	0.05	43.20	0.51	0.49	0.49	0.05	0.03
43.30	0.48	0.52	0.45	0.10	0.05	43.40	0.49	0.51	0.46	0.10	0.05
43.48	0.52	0.48	0.50	0.08	0.04	43.51	0.54	0.46	0.53	0.03	0.02
43.52	0.57	0.43	0.58	0.01	0.00	43.56	0.64	0.36	0.73	0.04	0.01
43.61	0.77	0.23	1.32	0.05	0.01	43.67	0.88	0.12	4.39	0.06	0.01
43.72	1.00	0.00	797274697	0.05	0.00	43.80	1.09	0.00	0.00	0.08	0.00
43.85	1.16	0.00	0.00	0.05	0.00	43.90	1.21	0.00	0.00	0.05	0.00
43.94	1.24	0.00	0.00	0.05	0.00	43.99	1.26	0.00	0.00	0.05	0.00
44.08	1.27	0.00	0.00	0.09	0.00	44.14	1.28	0.00	0.00	0.06	0.00
44.22	1.30	0.00	0.00	0.08	0.00	44.28	1.30	0.00	0.00	0.05	0.00
44.33	1.29	0.00	0.00	0.05	0.00	44.40	1.27	0.00	0.00	0.07	0.00
44.48	1.27	0.00	0.00	0.08	0.00	44.52	1.26	0.00	0.00	0.05	0.00
44.61	1.27	0.00	0.00	0.09	0.00	44.72	1.29	0.00	0.00	0.11	0.00
44.77	1.34	0.00	0.00	0.05	0.00	44.91	1.36	0.00	0.00	0.14	0.00
44.95	1.29	0.00	0.00	0.05	0.00	45.02	1.24	0.00	0.00	0.07	0.00
45.04	0.96	0.04	168.59	0.02	0.00	45.06	1.00	0.00	814329101	0.02	0.00
45.11	1.04	0.00	0.00	0.05	0.00	45.15	1.37	0.00	0.00	0.05	0.00
45.21	1.44	0.00	0.00	0.05	0.00	45.25	1.50	0.00	0.00	0.04	0.00
45.30	1.54	0.00	0.00	0.05	0.00	45.35	1.57	0.00	0.00	0.05	0.00
45.41	1.57	0.00	0.00	0.06	0.00	45.49	1.55	0.00	0.00	0.08	0.00
45.55	1.52	0.00	0.00	0.05	0.00	45.63	1.46	0.00	0.00	0.09	0.00
45.69	1.38	0.00	0.00	0.05	0.00	45.78	1.29	0.00	0.00	0.09	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
45.84	1.19	0.00	0.00	0.06	0.00	45.93	1.07	0.00	0.00	0.09	0.00
46.02	2.00	0.00	0.00	0.09	0.00	46.08	2.00	0.00	0.00	0.05	0.00
46.16	2.00	0.00	0.00	0.09	0.00	46.24	2.00	0.00	0.00	0.07	0.00
46.31	2.00	0.00	0.00	0.07	0.00	46.41	2.00	0.00	0.00	0.10	0.00
46.48	2.00	0.00	0.00	0.06	0.00	46.56	2.00	0.00	0.00	0.09	0.00
46.65	2.00	0.00	0.00	0.09	0.00	46.75	2.00	0.00	0.00	0.10	0.00
46.84	2.00	0.00	0.00	0.09	0.00	46.94	2.00	0.00	0.00	0.09	0.00
47.02	2.00	0.00	0.00	0.08	0.00	47.08	2.00	0.00	0.00	0.06	0.00
47.12	2.00	0.00	0.00	0.04	0.00	47.16	2.00	0.00	0.00	0.04	0.00
47.21	2.00	0.00	0.00	0.05	0.00	47.27	2.00	0.00	0.00	0.06	0.00
47.35	2.00	0.00	0.00	0.08	0.00	47.40	2.00	0.00	0.00	0.05	0.00
47.50	2.00	0.00	0.00	0.10	0.00	47.55	2.00	0.00	0.00	0.05	0.00
47.61	2.00	0.00	0.00	0.06	0.00	47.69	2.00	0.00	0.00	0.08	0.00
47.76	2.00	0.00	0.00	0.08	0.00	47.83	2.00	0.00	0.00	0.07	0.00
47.93	2.00	0.00	0.00	0.10	0.00	48.02	2.00	0.00	0.00	0.09	0.00
48.09	2.00	0.00	0.00	0.07	0.00	48.18	2.00	0.00	0.00	0.09	0.00
48.27	2.00	0.00	0.00	0.09	0.00	48.37	2.00	0.00	0.00	0.10	0.00
48.46	2.00	0.00	0.00	0.09	0.00	48.52	2.00	0.00	0.00	0.07	0.00
48.60	2.00	0.00	0.00	0.08	0.00	48.70	2.00	0.00	0.00	0.10	0.00
48.79	2.00	0.00	0.00	0.09	0.00	48.85	2.00	0.00	0.00	0.06	0.00
48.94	2.00	0.00	0.00	0.09	0.00	49.04	2.00	0.00	0.00	0.09	0.00
49.13	2.00	0.00	0.00	0.09	0.00	49.23	2.00	0.00	0.00	0.10	0.00
49.33	2.00	0.00	0.00	0.09	0.00	49.38	2.00	0.00	0.00	0.05	0.00
49.42	2.00	0.00	0.00	0.04	0.00	49.48	2.00	0.00	0.00	0.06	0.00
49.53	2.00	0.00	0.00	0.04	0.00	49.58	2.00	0.00	0.00	0.05	0.00
49.63	2.00	0.00	0.00	0.05	0.00	49.72	2.00	0.00	0.00	0.10	0.00
49.77	2.00	0.00	0.00	0.05	0.00	49.83	2.00	0.00	0.00	0.05	0.00
49.92	2.00	0.00	0.00	0.09	0.00	49.97	2.00	0.00	0.00	0.05	0.00
50.04	2.00	0.00	0.00	0.07	0.00	50.11	2.00	0.00	0.00	0.07	0.00
50.20	2.00	0.00	0.00	0.09	0.00	50.27	2.00	0.00	0.00	0.07	0.00
50.34	2.00	0.00	0.00	0.07	0.00	50.45	2.00	0.00	0.00	0.10	0.00
50.54	2.00	0.00	0.00	0.09	0.00	50.59	2.00	0.00	0.00	0.05	0.00
50.68	2.00	0.00	0.00	0.09	0.00	50.79	2.00	0.00	0.00	0.10	0.00
50.88	2.00	0.00	0.00	0.09	0.00	50.98	2.00	0.00	0.00	0.10	0.00
51.07	2.00	0.00	0.00	0.09	0.00	51.17	2.00	0.00	0.00	0.10	0.00
51.24	2.00	0.00	0.00	0.07	0.00	51.33	2.00	0.00	0.00	0.09	0.00
51.46	2.00	0.00	0.00	0.13	0.00	51.46	2.00	0.00	0.00	0.00	0.00
51.51	2.00	0.00	0.00	0.05	0.00	51.56	2.00	0.00	0.00	0.05	0.00
51.65	2.00	0.00	0.00	0.09	0.00	51.71	2.00	0.00	0.00	0.06	0.00
51.79	2.00	0.00	0.00	0.09	0.00	51.85	2.00	0.00	0.00	0.05	0.00
51.94	2.00	0.00	0.00	0.09	0.00	51.99	2.00	0.00	0.00	0.05	0.00
52.09	2.00	0.00	0.00	0.10	0.00	52.19	2.00	0.00	0.00	0.10	0.00
52.28	2.00	0.00	0.00	0.09	0.00	52.35	2.00	0.00	0.00	0.07	0.00
52.43	2.00	0.00	0.00	0.08	0.00	52.52	2.00	0.00	0.00	0.09	0.00
52.62	2.00	0.00	0.00	0.11	0.00	52.72	2.00	0.00	0.00	0.09	0.00
52.81	2.00	0.00	0.00	0.09	0.00	52.91	2.00	0.00	0.00	0.10	0.00
53.00	2.00	0.00	0.00	0.09	0.00	53.10	2.00	0.00	0.00	0.10	0.00
53.20	2.00	0.00	0.00	0.09	0.00	53.29	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
53.38	2.00	0.00	0.00	0.09	0.00	53.46	2.00	0.00	0.00	0.08	0.00
53.53	2.00	0.00	0.00	0.07	0.00	53.63	2.00	0.00	0.00	0.10	0.00
53.73	2.00	0.00	0.00	0.10	0.00	53.82	2.00	0.00	0.00	0.09	0.00
53.92	2.00	0.00	0.00	0.10	0.00	53.94	0.98	0.02	70981.95	0.02	0.00
53.96	0.88	0.12	3.79	0.02	0.00	53.97	0.92	0.08	10.21	0.01	0.00
54.05	1.03	0.00	0.00	0.08	0.00	54.08	1.19	0.00	0.00	0.02	0.00
54.13	1.28	0.00	0.00	0.05	0.00	54.19	1.38	0.00	0.00	0.06	0.00
54.25	1.46	0.00	0.00	0.06	0.00	54.28	1.54	0.00	0.00	0.03	0.00
54.29	1.49	0.00	0.00	0.02	0.00	54.34	1.49	0.00	0.00	0.05	0.00
54.35	1.50	0.00	0.00	0.01	0.00	54.40	1.52	0.00	0.00	0.05	0.00
54.44	1.54	0.00	0.00	0.04	0.00	54.49	1.53	0.00	0.00	0.05	0.00
54.53	1.56	0.00	0.00	0.04	0.00	54.57	1.65	0.00	0.00	0.03	0.00
54.58	1.72	0.00	0.00	0.02	0.00	54.63	1.72	0.00	0.00	0.04	0.00
54.68	1.80	0.00	0.00	0.05	0.00	54.73	1.75	0.00	0.00	0.05	0.00
54.78	1.71	0.00	0.00	0.05	0.00	54.83	1.70	0.00	0.00	0.05	0.00
54.88	1.75	0.00	0.00	0.05	0.00	54.92	1.84	0.00	0.00	0.05	0.00
54.97	1.91	0.00	0.00	0.05	0.00	55.02	1.93	0.00	0.00	0.05	0.00
55.12	1.83	0.00	0.00	0.09	0.00	55.17	1.64	0.00	0.00	0.05	0.00
55.25	1.41	0.00	0.00	0.08	0.00	55.31	1.28	0.00	0.00	0.06	0.00
55.36	1.17	0.00	0.00	0.05	0.00	55.45	1.08	0.00	0.00	0.09	0.00
55.50	0.98	0.02	192664.19	0.05	0.00	55.60	0.92	0.08	11.38	0.10	0.00
55.65	0.84	0.16	2.35	0.05	0.00	55.71	0.79	0.21	1.51	0.06	0.01
55.75	0.75	0.25	1.17	0.04	0.00	55.79	0.76	0.24	1.23	0.04	0.00
55.84	0.78	0.22	1.43	0.05	0.01	55.89	0.80	0.20	1.68	0.05	0.00
55.90	0.81	0.19	1.83	0.01	0.00	55.94	0.80	0.20	1.61	0.03	0.00
55.99	0.77	0.23	1.33	0.05	0.01	56.03	0.74	0.26	1.11	0.05	0.01
56.08	0.72	0.28	0.99	0.05	0.01	56.14	0.69	0.31	0.90	0.06	0.01
56.22	0.67	0.33	0.81	0.08	0.01	56.28	0.65	0.35	0.75	0.05	0.01
56.33	0.65	0.35	0.74	0.05	0.01	56.38	0.65	0.35	0.74	0.05	0.01
56.45	0.67	0.33	0.80	0.07	0.01	56.52	0.70	0.30	0.91	0.07	0.01
56.62	0.74	0.26	1.11	0.10	0.01	56.66	0.77	0.23	1.37	0.05	0.00
56.73	0.82	0.18	1.99	0.07	0.01	56.81	0.86	0.14	3.17	0.08	0.00
56.95	0.91	0.09	7.48	0.14	0.01	57.00	0.96	0.04	95.74	0.04	0.00
57.09	0.97	0.03	549.52	0.10	0.00	57.19	0.96	0.04	115.26	0.10	0.00
57.27	0.89	0.11	5.10	0.08	0.00	57.35	0.87	0.13	3.70	0.07	0.00
57.44	0.83	0.17	2.25	0.09	0.01	57.50	0.83	0.17	2.17	0.07	0.00
57.52	0.90	0.10	5.94	0.02	0.00	57.58	1.06	0.00	0.00	0.05	0.00
57.63	1.19	0.00	0.00	0.05	0.00	57.72	1.23	0.00	0.00	0.09	0.00
57.77	1.18	0.00	0.00	0.04	0.00	57.82	1.09	0.00	0.00	0.05	0.00
57.91	0.98	0.02	45128.57	0.09	0.00	57.96	0.88	0.12	4.13	0.05	0.00
58.02	0.95	0.05	55.89	0.05	0.00	58.09	1.00	0.00	176603202	0.08	0.00
58.16	1.08	0.00	0.00	0.06	0.00	58.25	1.11	0.00	0.00	0.10	0.00
58.30	1.09	0.00	0.00	0.05	0.00	58.40	1.04	0.00	0.00	0.10	0.00
58.50	1.03	0.00	0.00	0.10	0.00	58.56	1.01	0.00	0.00	0.06	0.00
58.64	1.04	0.00	0.00	0.08	0.00	58.73	1.12	0.00	0.00	0.09	0.00
58.78	1.14	0.00	0.00	0.05	0.00	58.88	1.18	0.00	0.00	0.09	0.00
58.97	1.20	0.00	0.00	0.09	0.00	59.07	1.17	0.00	0.00	0.10	0.00
59.13	1.10	0.00	0.00	0.05	0.00	59.23	1.05	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
59.31	0.95	0.05	67.96	0.09	0.00	59.38	0.89	0.11	4.90	0.07	0.00
59.41	0.84	0.16	2.46	0.03	0.00	59.46	0.86	0.14	3.03	0.05	0.00
59.51	0.86	0.14	3.00	0.05	0.00	59.57	0.89	0.11	5.27	0.05	0.00
59.66	0.98	0.02	7667.36	0.09	0.00	59.75	1.08	0.00	0.00	0.09	0.00
59.80	1.18	0.00	0.00	0.05	0.00	59.85	1.36	0.00	0.00	0.05	0.00
59.91	1.39	0.00	0.00	0.06	0.00	59.99	1.42	0.00	0.00	0.08	0.00
60.05	1.47	0.00	0.00	0.05	0.00	60.09	1.44	0.00	0.00	0.04	0.00
60.14	1.35	0.00	0.00	0.05	0.00	60.19	1.29	0.00	0.00	0.05	0.00
60.22	1.25	0.00	0.00	0.03	0.00	60.28	1.15	0.00	0.00	0.06	0.00
60.33	1.00	0.00	370871701	0.05	0.00	60.38	0.84	0.16	2.34	0.05	0.00
60.42	0.74	0.26	1.15	0.04	0.00	60.48	0.64	0.36	0.73	0.06	0.01
60.57	0.55	0.45	0.55	0.09	0.01	60.66	0.47	0.53	0.45	0.09	0.01
60.68	0.43	0.57	0.41	0.03	0.00	60.69	0.41	0.59	0.40	0.01	0.00
60.74	0.40	0.60	0.38	0.05	0.01	60.79	0.38	0.62	0.37	0.05	0.01
60.84	0.36	0.64	0.36	0.05	0.01	60.89	0.34	0.66	0.35	0.05	0.01
60.98	0.33	0.67	0.34	0.09	0.01	61.03	0.35	0.65	0.35	0.04	0.01
61.08	0.40	0.60	0.38	0.06	0.01	61.18	0.46	0.54	0.44	0.09	0.01
61.23	0.54	0.46	0.53	0.06	0.01	61.31	0.49	0.51	0.47	0.08	0.01
61.42	0.49	0.51	0.47	0.10	0.01	61.47	0.55	0.45	0.54	0.05	0.00
61.51	0.61	0.39	0.65	0.05	0.00	61.54	0.62	0.38	0.68	0.02	0.00
61.57	0.66	0.34	0.78	0.03	0.00	61.58	0.74	0.26	1.10	0.02	0.00
61.61	0.65	0.35	0.76	0.03	0.00	61.63	0.61	0.39	0.64	0.01	0.00
61.63	0.47	0.53	0.45	0.01	0.00	61.66	0.39	0.61	0.38	0.02	0.00
61.67	0.43	0.57	0.41	0.01	0.00	61.70	0.42	0.58	0.40	0.03	0.00
61.71	0.43	0.57	0.41	0.01	0.00	61.76	0.44	0.56	0.42	0.04	0.00
61.80	0.47	0.53	0.45	0.05	0.00	61.84	0.49	0.51	0.47	0.04	0.00
61.86	0.53	0.47	0.52	0.02	0.00	61.93	0.57	0.43	0.58	0.07	0.01
61.98	0.55	0.45	0.54	0.05	0.00	62.04	0.69	0.31	0.87	0.06	0.00
62.09	0.86	0.14	2.85	0.05	0.00	62.14	0.98	0.02	303039.98	0.05	0.00
62.19	1.07	0.00	0.00	0.05	0.00	62.24	1.11	0.00	0.00	0.05	0.00
62.26	1.17	0.00	0.00	0.02	0.00	62.29	1.17	0.00	0.00	0.03	0.00
62.38	1.15	0.00	0.00	0.09	0.00	62.44	1.02	0.00	0.00	0.06	0.00
62.46	0.92	0.08	11.18	0.02	0.00	62.47	0.84	0.16	2.27	0.01	0.00
62.51	0.86	0.14	2.91	0.04	0.00	62.56	0.90	0.10	5.86	0.05	0.00
62.60	0.96	0.04	92.83	0.04	0.00	62.65	0.97	0.03	2178.99	0.05	0.00
62.70	0.98	0.02	4021.39	0.05	0.00	62.75	0.98	0.02	10362.26	0.05	0.00
62.80	1.03	0.00	0.00	0.05	0.00	62.85	1.19	0.00	0.00	0.05	0.00
62.89	1.44	0.00	0.00	0.05	0.00	62.97	1.79	0.00	0.00	0.07	0.00
63.04	2.00	0.00	0.00	0.07	0.00	63.09	2.00	0.00	0.00	0.05	0.00
63.13	2.00	0.00	0.00	0.05	0.00	63.19	2.00	0.00	0.00	0.05	0.00
63.23	2.00	0.00	0.00	0.04	0.00	63.28	2.00	0.00	0.00	0.05	0.00
63.32	2.00	0.00	0.00	0.04	0.00	63.38	2.00	0.00	0.00	0.06	0.00
63.44	2.00	0.00	0.00	0.06	0.00	63.52	2.00	0.00	0.00	0.08	0.00
63.57	2.00	0.00	0.00	0.05	0.00	63.66	2.00	0.00	0.00	0.09	0.00
63.73	1.22	0.00	0.00	0.06	0.00	63.76	0.90	0.10	6.71	0.03	0.00
63.76	0.86	0.14	3.13	0.01	0.00	63.78	0.91	0.09	8.14	0.02	0.00
63.81	1.10	0.00	0.00	0.03	0.00	63.85	1.17	0.00	0.00	0.04	0.00
63.86	1.15	0.00	0.00	0.01	0.00	63.91	1.21	0.00	0.00	0.05	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
63.94	1.25	0.00	0.00	0.03	0.00	63.95	1.27	0.00	0.00	0.02	0.00
64.00	1.26	0.00	0.00	0.05	0.00	64.02	1.23	0.00	0.00	0.01	0.00
64.05	1.20	0.00	0.00	0.03	0.00	64.09	1.18	0.00	0.00	0.04	0.00
64.11	1.14	0.00	0.00	0.02	0.00	64.15	1.10	0.00	0.00	0.04	0.00
64.20	1.08	0.00	0.00	0.05	0.00	64.25	1.09	0.00	0.00	0.05	0.00
64.29	1.21	0.00	0.00	0.04	0.00	64.34	1.40	0.00	0.00	0.05	0.00
64.43	1.63	0.00	0.00	0.08	0.00	64.48	1.81	0.00	0.00	0.05	0.00
64.53	1.90	0.00	0.00	0.05	0.00	64.58	1.99	0.00	0.00	0.05	0.00
64.63	2.00	0.00	0.00	0.05	0.00	64.68	2.00	0.00	0.00	0.05	0.00
64.73	2.00	0.00	0.00	0.05	0.00	64.77	2.00	0.00	0.00	0.05	0.00
64.82	2.00	0.00	0.00	0.04	0.00	64.87	2.00	0.00	0.00	0.05	0.00
64.89	2.00	0.00	0.00	0.02	0.00	64.93	2.00	0.00	0.00	0.04	0.00
64.94	2.00	0.00	0.00	0.01	0.00	64.98	2.00	0.00	0.00	0.04	0.00
64.99	2.00	0.00	0.00	0.01	0.00	65.03	2.00	0.00	0.00	0.05	0.00
65.08	2.00	0.00	0.00	0.05	0.00	65.13	2.00	0.00	0.00	0.05	0.00
65.17	2.00	0.00	0.00	0.04	0.00	65.22	2.00	0.00	0.00	0.05	0.00
65.23	2.00	0.00	0.00	0.01	0.00	65.28	2.00	0.00	0.00	0.05	0.00
65.32	2.00	0.00	0.00	0.04	0.00	65.37	2.00	0.00	0.00	0.05	0.00
65.42	2.00	0.00	0.00	0.05	0.00	65.47	2.00	0.00	0.00	0.05	0.00
65.48	1.97	0.00	0.00	0.01	0.00	65.49	1.83	0.00	0.00	0.01	0.00
65.52	1.81	0.00	0.00	0.03	0.00	65.57	1.88	0.00	0.00	0.05	0.00
65.62	1.99	0.00	0.00	0.05	0.00	65.67	2.00	0.00	0.00	0.05	0.00
65.69	2.00	0.00	0.00	0.01	0.00	65.72	2.00	0.00	0.00	0.03	0.00
65.77	2.00	0.00	0.00	0.05	0.00	65.82	2.00	0.00	0.00	0.05	0.00
65.86	2.00	0.00	0.00	0.04	0.00	65.86	2.00	0.00	0.00	0.01	0.00
65.91	2.00	0.00	0.00	0.05	0.00	65.96	2.00	0.00	0.00	0.04	0.00

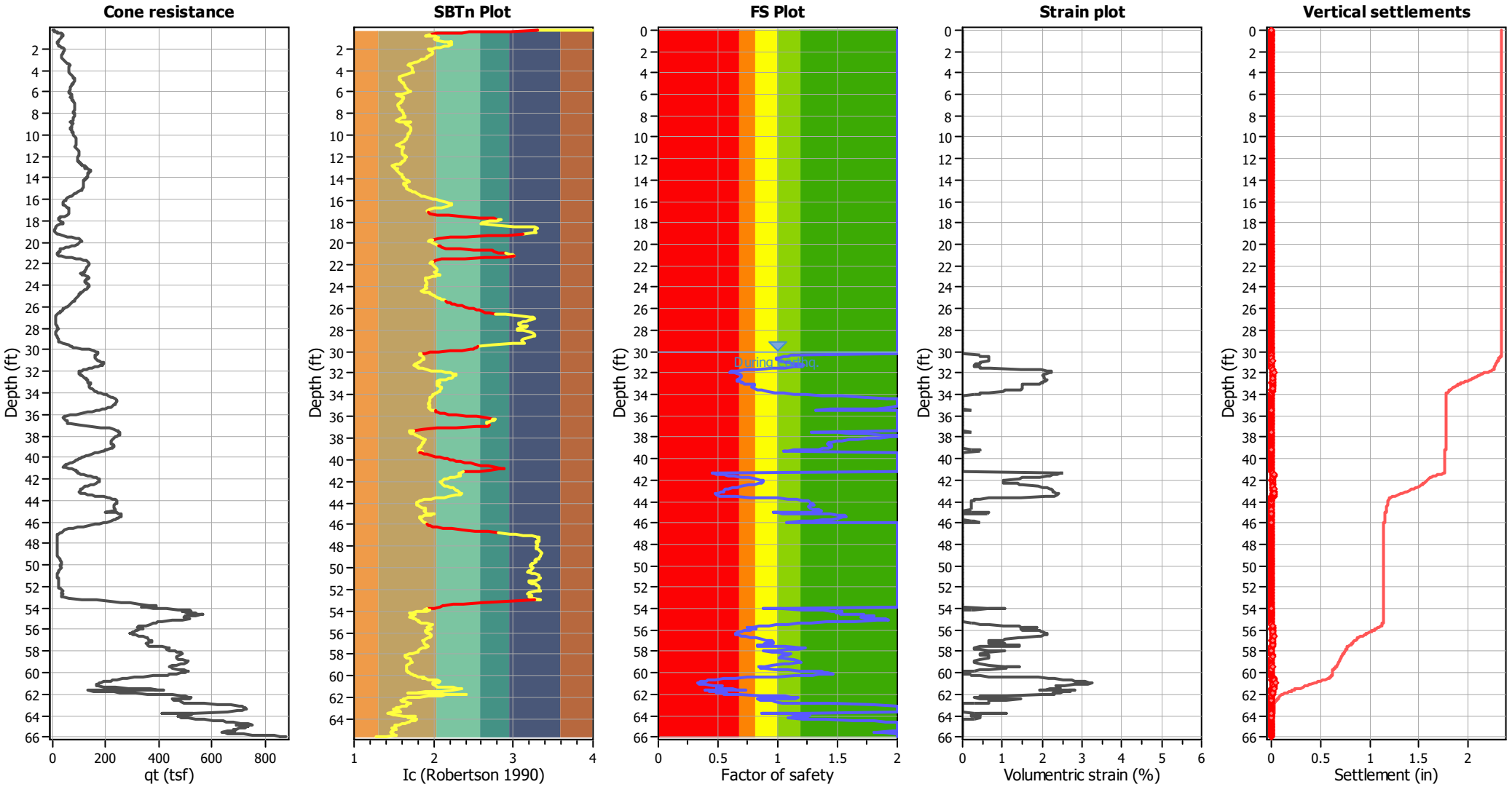
Overall liquefaction potential: 2.18

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
30.05	136.43	2.00	0.00	1.00	0.00	30.14	140.95	2.00	0.00	1.00	0.00
30.19	142.08	2.00	0.00	1.00	0.00	30.24	142.19	2.00	0.00	1.00	0.00
30.29	142.38	1.14	0.44	1.00	0.00	30.38	141.39	1.12	0.44	1.00	0.00
30.43	139.76	1.09	0.44	1.00	0.00	30.48	137.67	1.05	0.66	1.00	0.00
30.54	135.86	1.02	0.66	1.00	0.00	30.62	134.98	1.00	0.67	1.00	0.01
30.67	134.34	0.99	0.67	1.00	0.00	30.72	134.61	0.99	0.67	1.00	0.00
30.76	134.89	1.00	0.67	1.00	0.00	30.86	135.92	1.01	0.66	1.00	0.01
30.91	137.26	1.03	0.66	1.00	0.00	30.95	138.94	1.06	0.45	1.00	0.00
31.03	140.71	1.09	0.44	1.00	0.00	31.10	142.33	1.12	0.44	1.00	0.00
31.15	144.07	1.15	0.31	1.00	0.00	31.20	146.05	1.19	0.31	1.00	0.00
31.26	147.81	1.22	0.31	1.00	0.00	31.34	147.23	1.21	0.31	1.00	0.00
31.37	146.99	1.20	0.31	1.00	0.00	31.38	145.70	1.18	0.31	1.00	0.00
31.43	146.17	1.19	0.31	1.00	0.00	31.47	143.44	1.13	0.44	1.00	0.00
31.55	139.35	1.06	0.44	1.00	0.00	31.59	132.93	0.95	0.68	1.00	0.00
31.66	124.83	0.83	1.47	1.00	0.01	31.73	116.80	0.73	1.97	1.00	0.02
31.78	110.36	0.65	2.14	1.00	0.01	31.84	106.34	0.61	2.22	1.00	0.02
31.93	104.84	0.60	2.25	1.00	0.02	31.98	106.04	0.61	2.23	1.00	0.01
32.02	108.88	0.64	2.18	1.00	0.01	32.09	111.87	0.67	2.10	1.00	0.02
32.16	113.86	0.69	2.04	1.00	0.02	32.22	114.52	0.70	2.03	1.00	0.01
32.27	114.53	0.70	2.03	1.00	0.01	32.34	114.38	0.69	2.03	1.00	0.02
32.42	114.11	0.69	2.04	1.00	0.02	32.46	113.62	0.68	2.05	1.00	0.01
32.54	113.25	0.68	2.06	1.00	0.02	32.60	112.00	0.66	2.09	1.00	0.02
32.67	111.53	0.66	2.11	1.00	0.02	32.75	111.85	0.66	2.10	1.00	0.02
32.81	113.95	0.68	2.04	1.00	0.01	32.89	116.21	0.71	1.99	1.00	0.02
32.94	114.84	0.69	2.02	1.00	0.01	32.95	116.07	0.71	1.99	1.00	0.00
33.00	117.56	0.72	1.95	1.00	0.01	33.06	122.40	0.79	1.51	1.00	0.01
33.11	123.66	0.80	1.49	1.00	0.01	33.20	123.53	0.80	1.49	1.00	0.02
33.25	123.06	0.79	1.50	1.00	0.01	33.34	122.48	0.78	1.51	1.00	0.02
33.38	122.68	0.79	1.51	1.00	0.01	33.48	123.78	0.80	1.49	1.00	0.02
33.58	125.79	0.83	1.45	1.00	0.02	33.63	128.81	0.87	1.08	1.00	0.01
33.73	132.15	0.92	1.04	1.00	0.01	33.82	136.16	0.98	0.66	1.00	0.01
33.87	140.58	1.05	0.44	1.00	0.00	33.96	145.13	1.13	0.43	1.00	0.00
34.02	150.66	1.23	0.30	1.00	0.00	34.11	157.32	1.37	0.00	1.00	0.00
34.18	164.99	1.54	0.00	1.00	0.00	34.26	172.52	1.72	0.00	1.00	0.00
34.35	179.50	1.91	0.00	1.00	0.00	34.44	185.53	2.00	0.00	1.00	0.00
34.49	190.23	2.00	0.00	1.00	0.00	34.59	192.83	2.00	0.00	1.00	0.00
34.69	194.12	2.00	0.00	1.00	0.00	34.76	194.53	2.00	0.00	1.00	0.00
34.83	194.02	2.00	0.00	1.00	0.00	34.93	191.54	2.00	0.00	1.00	0.00
35.02	188.08	2.00	0.00	1.00	0.00	35.12	184.23	2.00	0.00	1.00	0.00
35.22	181.13	1.94	0.00	1.00	0.00	35.30	177.46	1.83	0.00	1.00	0.00
35.38	168.21	1.60	0.00	1.00	0.00	35.43	161.35	1.44	0.00	1.00	0.00
35.46	155.80	1.32	0.21	1.00	0.00	35.51	153.78	2.00	0.00	1.00	0.00
35.56	146.76	2.00	0.00	1.00	0.00	35.66	138.53	2.00	0.00	1.00	0.00
35.70	130.03	2.00	0.00	1.00	0.00	35.80	123.66	2.00	0.00	1.00	0.00
35.89	119.95	2.00	0.00	1.00	0.00	35.96	120.81	2.00	0.00	1.00	0.00
36.04	120.37	2.00	0.00	1.00	0.00	36.14	117.01	2.00	0.00	1.00	0.00
36.19	110.69	2.00	0.00	1.00	0.00	36.28	110.05	2.00	0.00	1.00	0.00
36.33	108.32	2.00	0.00	1.00	0.00	36.42	108.08	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
36.48	107.27	2.00	0.00	1.00	0.00	36.52	112.95	2.00	0.00	1.00	0.00
36.62	119.67	2.00	0.00	1.00	0.00	36.68	126.59	2.00	0.00	1.00	0.00
36.77	128.11	2.00	0.00	1.00	0.00	36.86	126.60	2.00	0.00	1.00	0.00
36.90	115.19	2.00	0.00	1.00	0.00	37.00	103.13	2.00	0.00	1.00	0.00
37.10	112.56	2.00	0.00	1.00	0.00	37.20	136.84	2.00	0.00	1.00	0.00
37.29	147.30	2.00	0.00	1.00	0.00	37.39	149.01	2.00	0.00	1.00	0.00
37.49	155.00	1.28	0.21	1.00	0.00	37.53	160.20	1.39	0.00	1.00	0.00
37.58	165.44	1.51	0.00	1.00	0.00	37.62	169.66	1.60	0.00	1.00	0.00
37.69	175.10	1.74	0.00	1.00	0.00	37.77	179.78	1.86	0.00	1.00	0.00
37.82	183.39	1.96	0.00	1.00	0.00	37.87	184.85	2.00	0.00	1.00	0.00
37.91	184.82	2.00	0.00	1.00	0.00	37.97	183.06	1.95	0.00	1.00	0.00
38.06	179.59	1.85	0.00	1.00	0.00	38.10	175.74	1.75	0.00	1.00	0.00
38.17	172.34	1.67	0.00	1.00	0.00	38.25	169.66	1.60	0.00	1.00	0.00
38.35	167.11	1.54	0.00	1.00	0.00	38.40	164.83	1.48	0.00	1.00	0.00
38.46	163.21	1.45	0.00	1.00	0.00	38.54	162.26	1.43	0.00	1.00	0.00
38.60	161.69	1.41	0.00	1.00	0.00	38.69	161.77	1.41	0.00	1.00	0.00
38.74	162.53	1.43	0.00	1.00	0.00	38.83	163.73	1.46	0.00	1.00	0.00
38.88	163.54	1.45	0.00	1.00	0.00	38.97	162.47	1.43	0.00	1.00	0.00
39.02	160.45	1.38	0.00	1.00	0.00	39.11	158.54	1.34	0.21	1.00	0.00
39.16	154.99	1.27	0.21	1.00	0.00	39.23	148.10	1.14	0.43	1.00	0.00
39.24	145.08	1.08	0.43	1.00	0.00	39.28	143.39	1.05	0.44	1.00	0.00
39.32	144.08	1.07	0.43	1.00	0.00	39.39	139.67	2.00	0.00	1.00	0.00
39.47	133.48	2.00	0.00	1.00	0.00	39.54	125.99	2.00	0.00	1.00	0.00
39.62	117.99	2.00	0.00	1.00	0.00	39.71	110.70	2.00	0.00	1.00	0.00
39.76	105.08	2.00	0.00	1.00	0.00	39.85	101.34	2.00	0.00	1.00	0.00
39.90	98.95	2.00	0.00	1.00	0.00	40.00	97.53	2.00	0.00	1.00	0.00
40.06	96.96	2.00	0.00	1.00	0.00	40.15	97.18	2.00	0.00	1.00	0.00
40.21	98.86	2.00	0.00	1.00	0.00	40.29	102.19	2.00	0.00	1.00	0.00
40.35	108.27	2.00	0.00	1.00	0.00	40.43	111.81	2.00	0.00	1.00	0.00
40.52	114.58	2.00	0.00	1.00	0.00	40.58	115.00	2.00	0.00	1.00	0.00
40.67	116.83	2.00	0.00	1.00	0.00	40.77	117.65	2.00	0.00	1.00	0.00
40.84	117.99	2.00	0.00	1.00	0.00	40.89	116.25	2.00	0.00	1.00	0.00
40.94	111.31	2.00	0.00	1.00	0.00	41.03	103.18	2.00	0.00	1.00	0.00
41.08	96.47	2.00	0.00	1.00	0.00	41.14	92.51	2.00	0.00	1.00	0.00
41.22	90.97	2.00	0.00	1.00	0.00	41.28	91.29	0.45	2.52	1.00	0.02
41.33	93.52	0.46	2.47	1.00	0.01	41.42	97.02	0.49	2.40	1.00	0.03
41.47	100.81	0.52	2.32	1.00	0.01	41.52	104.48	0.55	2.25	1.00	0.02
41.62	107.92	0.58	2.20	1.00	0.02	41.67	112.91	0.63	2.12	1.00	0.01
41.76	118.23	0.69	1.94	1.00	0.02	41.82	123.75	0.76	1.49	1.00	0.01
41.90	128.02	0.81	1.42	1.00	0.01	41.99	131.05	0.85	1.05	1.00	0.01
42.05	132.58	0.88	1.03	1.00	0.01	42.15	132.77	0.88	1.03	1.00	0.01
42.23	132.06	0.87	1.04	1.00	0.01	42.30	130.51	0.85	1.38	1.00	0.01
42.38	127.88	0.81	1.42	1.00	0.01	42.48	123.60	0.75	1.49	1.00	0.02
42.57	119.15	0.70	1.92	1.00	0.02	42.64	115.28	0.66	2.01	1.00	0.02
42.72	111.72	0.62	2.13	1.00	0.02	42.82	108.24	0.58	2.19	1.00	0.03
42.90	105.42	0.56	2.24	1.00	0.02	42.97	104.32	0.55	2.26	1.00	0.02
43.06	104.69	0.55	2.25	1.00	0.02	43.15	102.43	0.53	2.29	1.00	0.03
43.20	99.54	0.51	2.35	1.00	0.01	43.30	95.67	0.48	2.42	1.00	0.03

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
43.40	97.12	0.49	2.39	1.00	0.03	43.48	100.97	0.52	2.32	1.00	0.02
43.51	103.89	0.54	2.26	1.00	0.01	43.52	107.23	0.57	2.21	1.00	0.00
43.56	114.20	0.64	2.10	1.00	0.01	43.61	124.81	0.77	1.47	1.00	0.01
43.67	133.29	0.88	1.02	1.00	0.01	43.72	140.56	1.00	0.64	1.00	0.00
43.80	145.95	1.09	0.43	1.00	0.00	43.85	149.84	1.16	0.31	1.00	0.00
43.90	152.56	1.21	0.30	1.00	0.00	43.94	154.37	1.24	0.30	1.00	0.00
43.99	155.28	1.26	0.21	1.00	0.00	44.08	155.65	1.27	0.21	1.00	0.00
44.14	156.49	1.28	0.21	1.00	0.00	44.22	157.19	1.30	0.21	1.00	0.00
44.28	157.37	1.30	0.21	1.00	0.00	44.33	156.78	1.29	0.21	1.00	0.00
44.40	155.80	1.27	0.21	1.00	0.00	44.48	155.90	1.27	0.21	1.00	0.00
44.52	155.24	1.26	0.21	1.00	0.00	44.61	155.88	1.27	0.21	1.00	0.00
44.72	156.70	1.29	0.21	1.00	0.00	44.77	159.04	1.34	0.21	1.00	0.00
44.91	160.27	1.36	0.00	1.00	0.00	44.95	156.88	1.29	0.21	1.00	0.00
45.02	154.33	1.24	0.30	1.00	0.00	45.04	138.44	0.96	0.65	1.00	0.00
45.06	140.63	1.00	0.64	1.00	0.00	45.11	143.03	1.04	0.63	1.00	0.00
45.15	160.49	1.37	0.00	1.00	0.00	45.21	163.81	1.44	0.00	1.00	0.00
45.25	166.43	1.50	0.00	1.00	0.00	45.30	168.34	1.54	0.00	1.00	0.00
45.35	169.35	1.57	0.00	1.00	0.00	45.41	169.64	1.57	0.00	1.00	0.00
45.49	168.87	1.55	0.00	1.00	0.00	45.55	167.24	1.52	0.00	1.00	0.00
45.63	164.52	1.46	0.00	1.00	0.00	45.69	161.09	1.38	0.00	1.00	0.00
45.78	156.88	1.29	0.21	1.00	0.00	45.84	151.68	1.19	0.30	1.00	0.00
45.93	145.18	1.07	0.43	1.00	0.00	46.02	137.24	2.00	0.00	1.00	0.00
46.08	128.00	2.00	0.00	1.00	0.00	46.16	118.20	2.00	0.00	1.00	0.00
46.24	108.31	2.00	0.00	1.00	0.00	46.31	99.54	2.00	0.00	1.00	0.00
46.41	94.32	2.00	0.00	1.00	0.00	46.48	95.41	2.00	0.00	1.00	0.00
46.56	101.49	2.00	0.00	1.00	0.00	46.65	106.39	2.00	0.00	1.00	0.00
46.75	104.92	2.00	0.00	1.00	0.00	46.84	96.75	2.00	0.00	1.00	0.00
46.94	92.20	2.00	0.00	1.00	0.00	47.02	89.65	2.00	0.00	1.00	0.00
47.08	87.68	2.00	0.00	1.00	0.00	47.12	86.24	2.00	0.00	1.00	0.00
47.16	84.67	2.00	0.00	1.00	0.00	47.21	82.35	2.00	0.00	1.00	0.00
47.27	79.44	2.00	0.00	1.00	0.00	47.35	76.72	2.00	0.00	1.00	0.00
47.40	72.71	2.00	0.00	1.00	0.00	47.50	68.97	2.00	0.00	1.00	0.00
47.55	65.28	2.00	0.00	1.00	0.00	47.61	63.67	2.00	0.00	1.00	0.00
47.69	62.57	2.00	0.00	1.00	0.00	47.76	61.71	2.00	0.00	1.00	0.00
47.83	60.22	2.00	0.00	1.00	0.00	47.93	58.40	2.00	0.00	1.00	0.00
48.02	57.34	2.00	0.00	1.00	0.00	48.09	56.35	2.00	0.00	1.00	0.00
48.18	57.05	2.00	0.00	1.00	0.00	48.27	58.44	2.00	0.00	1.00	0.00
48.37	61.09	2.00	0.00	1.00	0.00	48.46	62.98	2.00	0.00	1.00	0.00
48.52	64.25	2.00	0.00	1.00	0.00	48.60	65.23	2.00	0.00	1.00	0.00
48.70	65.99	2.00	0.00	1.00	0.00	48.79	66.70	2.00	0.00	1.00	0.00
48.85	68.42	2.00	0.00	1.00	0.00	48.94	71.44	2.00	0.00	1.00	0.00
49.04	73.34	2.00	0.00	1.00	0.00	49.13	82.09	2.00	0.00	1.00	0.00
49.23	92.00	2.00	0.00	1.00	0.00	49.33	102.80	2.00	0.00	1.00	0.00
49.38	109.60	2.00	0.00	1.00	0.00	49.42	114.80	2.00	0.00	1.00	0.00
49.48	118.93	2.00	0.00	1.00	0.00	49.53	121.43	2.00	0.00	1.00	0.00
49.58	123.62	2.00	0.00	1.00	0.00	49.63	125.52	2.00	0.00	1.00	0.00
49.72	126.23	2.00	0.00	1.00	0.00	49.77	125.98	2.00	0.00	1.00	0.00
49.83	125.40	2.00	0.00	1.00	0.00	49.92	124.67	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
49.97	123.55	2.00	0.00	1.00	0.00	50.04	122.65	2.00	0.00	1.00	0.00
50.11	122.33	2.00	0.00	1.00	0.00	50.20	120.55	2.00	0.00	1.00	0.00
50.27	116.01	2.00	0.00	1.00	0.00	50.34	107.79	2.00	0.00	1.00	0.00
50.45	99.22	2.00	0.00	1.00	0.00	50.54	92.39	2.00	0.00	1.00	0.00
50.59	87.71	2.00	0.00	1.00	0.00	50.68	83.78	2.00	0.00	1.00	0.00
50.79	80.17	2.00	0.00	1.00	0.00	50.88	78.18	2.00	0.00	1.00	0.00
50.98	77.89	2.00	0.00	1.00	0.00	51.07	76.09	2.00	0.00	1.00	0.00
51.17	71.67	2.00	0.00	1.00	0.00	51.24	68.77	2.00	0.00	1.00	0.00
51.33	70.43	2.00	0.00	1.00	0.00	51.46	74.75	2.00	0.00	1.00	0.00
51.46	78.20	2.00	0.00	1.00	0.00	51.51	79.60	2.00	0.00	1.00	0.00
51.56	82.02	2.00	0.00	1.00	0.00	51.65	84.26	2.00	0.00	1.00	0.00
51.71	86.89	2.00	0.00	1.00	0.00	51.79	88.80	2.00	0.00	1.00	0.00
51.85	92.19	2.00	0.00	1.00	0.00	51.94	96.33	2.00	0.00	1.00	0.00
51.99	102.62	2.00	0.00	1.00	0.00	52.09	109.52	2.00	0.00	1.00	0.00
52.19	116.81	2.00	0.00	1.00	0.00	52.28	122.63	2.00	0.00	1.00	0.00
52.35	128.41	2.00	0.00	1.00	0.00	52.43	132.82	2.00	0.00	1.00	0.00
52.52	136.28	2.00	0.00	1.00	0.00	52.62	135.93	2.00	0.00	1.00	0.00
52.72	133.92	2.00	0.00	1.00	0.00	52.81	135.53	2.00	0.00	1.00	0.00
52.91	146.31	2.00	0.00	1.00	0.00	53.00	154.70	2.00	0.00	1.00	0.00
53.10	148.13	2.00	0.00	1.00	0.00	53.20	129.79	2.00	0.00	1.00	0.00
53.29	114.61	2.00	0.00	1.00	0.00	53.38	114.09	2.00	0.00	1.00	0.00
53.46	119.81	2.00	0.00	1.00	0.00	53.53	130.93	2.00	0.00	1.00	0.00
53.63	139.93	2.00	0.00	1.00	0.00	53.73	146.92	2.00	0.00	1.00	0.00
53.82	150.03	2.00	0.00	1.00	0.00	53.92	146.54	2.00	0.00	1.00	0.00
53.94	138.23	0.98	0.65	1.00	0.00	53.96	131.20	0.88	1.05	1.00	0.00
53.97	134.16	0.92	1.01	1.00	0.00	54.05	141.00	1.03	0.64	1.00	0.01
54.08	150.15	1.19	0.31	1.00	0.00	54.13	154.41	1.28	0.21	1.00	0.00
54.19	159.56	1.38	0.00	1.00	0.00	54.25	162.94	1.46	0.00	1.00	0.00
54.28	166.66	1.54	0.00	1.00	0.00	54.29	164.40	1.49	0.00	1.00	0.00
54.34	164.35	1.49	0.00	1.00	0.00	54.35	164.72	1.50	0.00	1.00	0.00
54.40	165.62	1.52	0.00	1.00	0.00	54.44	166.45	1.54	0.00	1.00	0.00
54.49	165.88	1.53	0.00	1.00	0.00	54.53	167.39	1.56	0.00	1.00	0.00
54.57	171.02	1.65	0.00	1.00	0.00	54.58	173.92	1.72	0.00	1.00	0.00
54.63	173.90	1.72	0.00	1.00	0.00	54.68	176.93	1.80	0.00	1.00	0.00
54.73	175.12	1.75	0.00	1.00	0.00	54.78	173.29	1.71	0.00	1.00	0.00
54.83	172.82	1.70	0.00	1.00	0.00	54.88	175.08	1.75	0.00	1.00	0.00
54.92	178.37	1.84	0.00	1.00	0.00	54.97	180.73	1.91	0.00	1.00	0.00
55.02	181.62	1.93	0.00	1.00	0.00	55.12	178.01	1.83	0.00	1.00	0.00
55.17	170.63	1.64	0.00	1.00	0.00	55.25	160.49	1.41	0.00	1.00	0.00
55.31	154.46	1.28	0.21	1.00	0.00	55.36	148.87	1.17	0.31	1.00	0.00
55.45	143.68	1.08	0.44	1.00	0.00	55.50	137.89	0.98	0.66	1.00	0.00
55.60	133.93	0.92	1.02	1.00	0.01	55.65	128.15	0.84	1.41	1.00	0.01
55.71	124.39	0.79	1.48	1.00	0.01	55.75	121.19	0.75	1.87	1.00	0.01
55.79	121.90	0.76	1.52	1.00	0.01	55.84	123.76	0.78	1.49	1.00	0.01
55.89	125.39	0.80	1.46	1.00	0.01	55.90	126.17	0.81	1.45	1.00	0.00
55.94	124.98	0.80	1.47	1.00	0.01	55.99	122.89	0.77	1.50	1.00	0.01
56.03	120.41	0.74	1.89	1.00	0.01	56.08	118.54	0.72	1.93	1.00	0.01
56.14	116.74	0.69	1.97	1.00	0.01	56.22	114.65	0.67	2.02	1.00	0.02

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
56.28	112.90	0.65	2.07	1.00	0.01	56.33	112.38	0.65	2.12	1.00	0.01
56.38	112.46	0.65	2.12	1.00	0.01	56.45	114.23	0.67	2.04	1.00	0.02
56.52	117.01	0.70	1.97	1.00	0.02	56.62	120.21	0.74	1.89	1.00	0.02
56.66	123.02	0.77	1.50	1.00	0.01	56.73	126.65	0.82	1.44	1.00	0.01
56.81	129.59	0.86	1.07	1.00	0.01	56.95	132.64	0.91	1.03	1.00	0.02
57.00	135.80	0.96	0.66	1.00	0.00	57.09	136.52	0.97	0.66	1.00	0.01
57.19	135.85	0.96	0.66	1.00	0.01	57.27	131.44	0.89	1.05	1.00	0.01
57.35	130.16	0.87	1.06	1.00	0.01	57.44	127.36	0.83	1.43	1.00	0.02
57.50	127.07	0.83	1.43	1.00	0.01	57.52	131.85	0.90	1.04	1.00	0.00
57.58	141.73	1.06	0.44	1.00	0.00	57.63	149.17	1.19	0.31	1.00	0.00
57.72	151.31	1.23	0.30	1.00	0.00	57.77	148.26	1.18	0.31	1.00	0.00
57.82	143.29	1.09	0.44	1.00	0.00	57.91	137.09	0.98	0.66	1.00	0.01
57.96	130.46	0.88	1.06	1.00	0.01	58.02	135.16	0.95	0.67	1.00	0.00
58.09	138.12	1.00	0.65	1.00	0.01	58.16	142.65	1.08	0.44	1.00	0.00
58.25	144.36	1.11	0.43	1.00	0.01	58.30	143.26	1.09	0.44	1.00	0.00
58.40	140.74	1.04	0.64	1.00	0.01	58.50	139.77	1.03	0.65	1.00	0.01
58.56	138.70	1.01	0.65	1.00	0.00	58.64	140.28	1.04	0.64	1.00	0.01
58.73	145.16	1.12	0.43	1.00	0.00	58.78	145.87	1.14	0.43	1.00	0.00
58.88	147.98	1.18	0.31	1.00	0.00	58.97	149.10	1.20	0.31	1.00	0.00
59.07	147.53	1.17	0.31	1.00	0.00	59.13	143.73	1.10	0.44	1.00	0.00
59.23	140.99	1.05	0.44	1.00	0.01	59.31	134.94	0.95	0.67	1.00	0.01
59.38	130.71	0.89	1.05	1.00	0.01	59.41	127.40	0.84	1.43	1.00	0.01
59.46	128.62	0.86	1.08	1.00	0.01	59.51	128.55	0.86	1.08	1.00	0.01
59.57	130.91	0.89	1.05	1.00	0.01	59.66	136.37	0.98	0.66	1.00	0.01
59.75	142.44	1.08	0.44	1.00	0.00	59.80	147.84	1.18	0.31	1.00	0.00
59.85	156.99	1.36	0.00	1.00	0.00	59.91	158.02	1.39	0.00	1.00	0.00
59.99	159.53	1.42	0.00	1.00	0.00	60.05	161.59	1.47	0.00	1.00	0.00
60.09	160.52	1.44	0.00	1.00	0.00	60.14	156.08	1.35	0.21	1.00	0.00
60.19	153.23	1.29	0.21	1.00	0.00	60.22	151.55	1.25	0.22	1.00	0.00
60.28	145.94	1.15	0.43	1.00	0.00	60.33	137.48	1.00	0.66	1.00	0.00
60.38	126.83	0.84	1.44	1.00	0.01	60.42	119.65	0.74	1.91	1.00	0.01
60.48	111.02	0.64	2.14	1.00	0.02	60.57	101.50	0.55	2.31	1.00	0.02
60.66	91.67	0.47	2.51	1.00	0.03	60.68	85.85	0.43	2.65	1.00	0.01
60.69	82.84	0.41	2.73	1.00	0.00	60.74	80.07	0.40	2.80	1.00	0.02
60.79	76.18	0.38	2.92	1.00	0.02	60.84	71.82	0.36	3.07	1.00	0.02
60.89	68.64	0.34	3.18	1.00	0.02	60.98	66.57	0.33	3.26	1.00	0.04
61.03	69.19	0.35	3.16	1.00	0.02	61.08	79.69	0.40	2.81	1.00	0.02
61.18	90.12	0.46	2.54	1.00	0.03	61.23	100.04	0.54	2.34	1.00	0.02
61.31	94.03	0.49	2.46	1.00	0.02	61.42	94.11	0.49	2.46	1.00	0.03
61.47	100.64	0.55	2.32	1.00	0.01	61.51	107.25	0.61	2.21	1.00	0.01
61.54	108.54	0.62	2.18	1.00	0.01	61.57	112.23	0.66	2.09	1.00	0.01
61.58	118.74	0.74	1.93	1.00	0.00	61.61	111.49	0.65	2.11	1.00	0.01
61.63	107.07	0.61	2.21	1.00	0.00	61.63	91.77	0.47	2.51	1.00	0.00
61.66	79.27	0.39	2.83	1.00	0.01	61.67	85.35	0.43	2.66	1.00	0.00
61.70	83.80	0.42	2.70	1.00	0.01	61.71	84.55	0.43	2.68	1.00	0.00
61.76	87.45	0.44	2.61	1.00	0.01	61.80	91.10	0.47	2.52	1.00	0.01
61.84	94.04	0.49	2.46	1.00	0.01	61.86	98.87	0.53	2.36	1.00	0.01
61.93	103.69	0.57	2.27	1.00	0.02	61.98	100.92	0.55	2.32	1.00	0.01

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
62.04	114.48	0.69	2.03	1.00	0.01	62.09	127.59	0.86	1.09	1.00	0.01
62.14	136.10	0.98	0.66	1.00	0.00	62.19	140.93	1.07	0.44	1.00	0.00
62.24	143.65	1.11	0.44	1.00	0.00	62.26	146.58	1.17	0.31	1.00	0.00
62.29	146.46	1.17	0.31	1.00	0.00	62.38	145.37	1.15	0.43	1.00	0.00
62.44	138.07	1.02	0.65	1.00	0.00	62.46	132.02	0.92	1.04	1.00	0.00
62.47	126.07	0.84	1.45	1.00	0.00	62.51	127.59	0.86	1.09	1.00	0.01
62.56	130.45	0.90	1.06	1.00	0.01	62.60	134.26	0.96	0.67	1.00	0.00
62.65	135.35	0.97	0.67	1.00	0.00	62.70	135.46	0.98	0.67	1.00	0.00
62.75	135.59	0.98	0.67	1.00	0.00	62.80	138.85	1.03	0.65	1.00	0.00
62.85	147.40	1.19	0.31	1.00	0.00	62.89	159.73	1.44	0.00	1.00	0.00
62.97	173.86	1.79	0.00	1.00	0.00	63.04	187.32	2.00	0.00	1.00	0.00
63.09	197.18	2.00	0.00	1.00	0.00	63.13	200.57	2.00	0.00	1.00	0.00
63.19	200.74	2.00	0.00	1.00	0.00	63.23	201.69	2.00	0.00	1.00	0.00
63.28	203.42	2.00	0.00	1.00	0.00	63.32	204.02	2.00	0.00	1.00	0.00
63.38	202.89	2.00	0.00	1.00	0.00	63.44	203.06	2.00	0.00	1.00	0.00
63.52	199.75	2.00	0.00	1.00	0.00	63.57	194.57	2.00	0.00	1.00	0.00
63.66	183.79	2.00	0.00	1.00	0.00	63.73	148.76	1.22	0.31	1.00	0.00
63.76	130.54	0.90	1.06	1.00	0.00	63.76	127.66	0.86	1.09	1.00	0.00
63.78	131.02	0.91	1.05	1.00	0.00	63.81	142.46	1.10	0.44	1.00	0.00
63.85	146.19	1.17	0.31	1.00	0.00	63.86	145.10	1.15	0.43	1.00	0.00
63.91	148.35	1.21	0.31	1.00	0.00	63.94	150.35	1.25	0.31	1.00	0.00
63.95	151.38	1.27	0.22	1.00	0.00	64.00	150.67	1.26	0.22	1.00	0.00
64.02	149.37	1.23	0.31	1.00	0.00	64.05	148.02	1.20	0.31	1.00	0.00
64.09	146.64	1.18	0.31	1.00	0.00	64.11	144.77	1.14	0.43	1.00	0.00
64.15	142.44	1.10	0.44	1.00	0.00	64.20	141.24	1.08	0.44	1.00	0.00
64.25	141.74	1.09	0.44	1.00	0.00	64.29	148.11	1.21	0.31	1.00	0.00
64.34	157.68	1.40	0.00	1.00	0.00	64.43	167.40	1.63	0.00	1.00	0.00
64.48	174.30	1.81	0.00	1.00	0.00	64.53	177.47	1.90	0.00	1.00	0.00
64.58	180.82	1.99	0.00	1.00	0.00	64.63	187.83	2.00	0.00	1.00	0.00
64.68	195.77	2.00	0.00	1.00	0.00	64.73	198.20	2.00	0.00	1.00	0.00
64.77	202.79	2.00	0.00	1.00	0.00	64.82	207.01	2.00	0.00	1.00	0.00
64.87	201.76	2.00	0.00	1.00	0.00	64.89	196.56	2.00	0.00	1.00	0.00
64.93	189.73	2.00	0.00	1.00	0.00	64.94	196.96	2.00	0.00	1.00	0.00
64.98	199.62	2.00	0.00	1.00	0.00	64.99	201.90	2.00	0.00	1.00	0.00
65.03	201.35	2.00	0.00	1.00	0.00	65.08	199.79	2.00	0.00	1.00	0.00
65.13	196.50	2.00	0.00	1.00	0.00	65.17	193.13	2.00	0.00	1.00	0.00
65.22	189.08	2.00	0.00	1.00	0.00	65.23	186.93	2.00	0.00	1.00	0.00
65.28	186.22	2.00	0.00	1.00	0.00	65.32	186.24	2.00	0.00	1.00	0.00
65.37	186.30	2.00	0.00	1.00	0.00	65.42	187.42	2.00	0.00	1.00	0.00
65.47	183.76	2.00	0.00	1.00	0.00	65.48	179.77	1.97	0.00	1.00	0.00
65.49	174.70	1.83	0.00	1.00	0.00	65.52	174.01	1.81	0.00	1.00	0.00
65.57	176.43	1.88	0.00	1.00	0.00	65.62	180.61	1.99	0.00	1.00	0.00
65.67	-1.00	2.00	0.00	1.00	0.00	65.69	-1.00	2.00	0.00	1.00	0.00
65.72	-1.00	2.00	0.00	1.00	0.00	65.77	-1.00	2.00	0.00	1.00	0.00
65.82	-1.00	2.00	0.00	1.00	0.00	65.86	-1.00	2.00	0.00	1.00	0.00
65.86	-1.00	2.00	0.00	1.00	0.00	65.91	-1.00	2.00	0.00	1.00	0.00
65.96	-1.00	2.00	0.00	1.00	0.00						

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)

Total estimated settlement: 2.34

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation (Robertson (2009) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.01	-0.03	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.04	-0.03	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.08	-0.07	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.10	-0.03	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.13	-0.03	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.18	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.22	0.00	-1.00	1.00	-1.00	-1.00	0.00	0.00
0.27	0.81	1.28	50.14	63.98	4.01	4.89	3.60
0.33	2.77	4.42	15.47	68.30	3.31	5.08	10.70
0.36	5.16	8.26	7.99	66.07	2.95	0.18	0.67
0.37	7.12	11.41	5.40	61.61	2.76	0.13	0.66
0.38	8.20	13.14	4.58	60.15	2.69	0.11	0.66
0.42	9.38	15.03	3.98	59.88	2.63	0.11	0.66
0.44	10.59	16.98	3.58	60.79	2.58	0.12	0.66
0.47	12.18	19.53	3.09	60.26	2.52	0.12	0.66
0.47	14.24	22.83	2.61	59.51	2.44	0.11	0.66
0.52	17.00	27.27	2.14	58.39	2.35	0.10	0.65
0.56	20.48	32.85	1.78	58.60	2.26	0.10	0.65
0.58	24.93	40.00	1.52	60.77	2.16	0.12	0.66
0.61	30.70	49.27	1.35	66.61	2.05	0.19	0.67
0.66	36.94	59.30	1.27	75.22	1.95	0.39	0.70
0.76	40.79	65.47	1.23	80.72	1.89	0.62	0.71
0.80	38.66	62.05	1.25	77.85	1.93	0.49	0.70
0.81	35.49	56.95	1.29	73.41	1.98	0.34	0.69
0.85	32.42	52.02	1.33	69.37	2.03	0.24	0.68
0.86	32.79	52.62	1.33	69.99	2.03	0.25	0.68
0.90	32.22	51.69	1.35	70.01	2.05	0.25	0.68
0.95	31.82	51.04	1.38	70.34	2.07	0.26	0.68
1.00	30.53	48.97	1.37	67.09	2.06	0.20	0.68
1.05	28.88	46.31	1.34	62.22	2.04	0.14	0.66
1.14	26.55	42.56	1.00	42.56	2.01	0.03	0.62
1.24	24.29	38.92	1.00	38.92	2.04	0.03	0.62
1.31	20.51	32.85	1.00	32.85	2.14	0.02	0.62
1.36	17.93	28.70	1.67	48.03	2.22	0.05	0.62
1.37	17.77	28.44	1.71	48.50	2.23	0.05	0.62
1.39	18.54	29.68	1.64	48.64	2.21	0.05	0.62
1.43	19.03	30.46	1.60	48.73	2.19	0.05	0.62
1.44	18.05	28.88	1.68	48.54	2.23	0.05	0.62
1.49	18.35	29.36	1.67	49.05	2.22	0.05	0.62
1.53	18.89	30.23	1.66	50.30	2.22	0.05	0.63
1.58	19.67	31.47	1.66	52.29	2.22	0.06	0.63
1.63	20.62	32.99	1.66	54.77	2.22	0.08	0.64
1.68	21.70	34.72	1.65	57.36	2.21	0.09	0.65
1.72	23.31	37.31	1.61	60.04	2.20	0.11	0.66
1.77	25.48	40.78	1.54	62.93	2.17	0.14	0.66
1.82	28.31	45.33	1.46	66.36	2.13	0.19	0.67
1.86	31.52	50.48	1.40	70.45	2.08	0.26	0.68
1.92	35.09	56.22	1.34	75.14	2.03	0.39	0.70

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.97	38.67	61.96	1.29	80.21	1.98	0.59	0.71
2.01	41.61	66.68	1.27	84.88	1.95	0.72	0.72
2.09	43.22	69.27	1.26	87.55	1.94	0.72	0.72
2.16	43.05	68.99	1.27	87.53	1.95	0.72	0.72
2.20	41.47	66.43	1.28	85.02	1.96	0.72	0.72
2.25	39.85	63.83	1.29	82.39	1.98	0.71	0.71
2.31	38.60	61.82	1.30	80.09	1.99	0.59	0.71
2.37	37.79	60.52	1.29	78.32	1.98	0.51	0.70
2.40	36.88	59.05	1.30	76.51	1.99	0.44	0.70
2.46	35.97	57.57	1.29	74.55	1.98	0.37	0.69
2.54	35.36	56.59	1.29	72.87	1.97	0.32	0.69
2.59	34.69	55.51	1.00	55.51	1.96	0.08	0.64
2.69	34.25	54.80	1.00	54.80	1.94	0.08	0.64
2.74	33.95	54.31	1.00	54.31	1.92	0.07	0.64
2.83	33.88	54.19	1.00	54.19	1.92	0.07	0.64
2.88	34.35	54.94	1.00	54.94	1.91	0.08	0.64
2.98	35.70	57.10	1.00	57.10	1.89	0.09	0.65
3.03	38.57	61.71	1.00	61.71	1.85	0.13	0.66
3.12	42.31	67.72	1.00	67.72	1.82	0.21	0.68
3.21	46.83	74.97	1.00	74.97	1.79	0.38	0.70
3.27	51.66	82.72	1.00	82.72	1.76	0.71	0.71
3.34	57.05	91.38	1.00	91.38	1.72	0.73	0.73
3.41	61.91	99.18	1.00	99.18	1.69	0.75	0.75
3.51	64.20	102.85	1.00	102.85	1.68	0.75	0.75
3.55	63.63	101.93	1.00	101.93	1.70	0.75	0.75
3.65	62.42	99.97	1.00	99.97	1.72	0.75	0.75
3.75	61.71	98.83	1.00	98.83	1.73	0.75	0.75
3.83	61.44	98.39	1.00	98.39	1.73	0.75	0.75
3.94	61.11	97.84	1.00	97.84	1.73	0.74	0.74
4.04	60.30	96.53	1.00	96.53	1.73	0.74	0.74
4.13	60.63	97.06	1.08	104.72	1.75	0.76	0.76
4.24	61.68	98.73	1.00	98.73	1.74	0.75	0.75
4.38	65.15	104.30	1.00	104.30	1.68	0.76	0.76
4.50	68.93	110.36	1.00	110.36	1.62	0.77	0.77
4.62	74.13	118.70	1.00	118.70	1.57	0.78	0.78
4.71	77.89	124.73	1.00	124.73	1.57	0.79	0.79
4.75	80.93	129.61	1.00	129.61	1.57	0.80	0.80
4.84	82.11	131.50	1.00	131.50	1.58	0.80	0.80
4.89	82.93	132.82	1.00	132.82	1.58	0.80	0.80
4.94	82.93	132.82	1.00	132.82	1.58	0.80	0.80
4.98	81.72	130.87	1.00	130.87	1.59	0.80	0.80
5.07	80.10	128.25	1.00	128.25	1.60	0.80	0.80
5.13	78.48	125.65	1.00	125.65	1.61	0.79	0.79
5.17	76.79	122.93	1.00	122.93	1.61	0.79	0.79
5.27	74.77	119.67	1.00	119.67	1.62	0.78	0.78
5.32	72.75	116.42	1.00	116.42	1.63	0.78	0.78
5.42	70.86	113.37	1.00	113.37	1.64	0.77	0.77
5.46	69.34	110.93	1.00	110.93	1.64	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.56	68.02	108.80	1.00	108.80	1.65	0.76	0.76
5.61	66.87	106.96	1.00	106.96	1.66	0.76	0.76
5.71	65.86	105.32	1.00	105.32	1.66	0.76	0.76
5.78	64.92	103.80	1.00	103.80	1.67	0.76	0.76
5.85	63.84	102.06	1.00	102.06	1.68	0.75	0.75
5.95	62.83	100.42	1.00	100.42	1.69	0.75	0.75
6.00	62.32	99.61	1.00	99.61	1.71	0.75	0.75
6.09	62.93	100.57	1.00	100.57	1.66	0.75	0.75
6.14	64.75	103.50	1.00	103.50	1.60	0.75	0.75
6.24	67.52	107.94	1.00	107.94	1.53	0.76	0.76
6.30	70.42	112.60	1.00	112.60	1.54	0.77	0.77
6.38	71.40	114.16	1.00	114.16	1.56	0.77	0.77
6.46	69.58	111.22	1.00	111.22	1.60	0.77	0.77
6.50	68.43	109.38	1.00	109.38	1.62	0.77	0.77
6.56	68.84	110.02	1.00	110.02	1.63	0.77	0.77
6.63	71.30	113.98	1.00	113.98	1.61	0.77	0.77
6.68	72.51	115.92	1.00	115.92	1.61	0.78	0.78
6.76	73.49	117.34	1.00	117.34	1.61	0.78	0.78
6.82	74.54	118.51	1.00	118.51	1.60	0.78	0.78
6.88	76.19	120.59	1.00	120.59	1.59	0.78	0.78
6.96	78.38	123.33	1.00	123.33	1.58	0.79	0.79
7.03	80.54	126.09	1.00	126.09	1.56	0.79	0.79
7.11	82.06	127.75	1.00	127.75	1.55	0.80	0.80
7.16	83.04	128.83	1.00	128.83	1.55	0.80	0.80
7.26	83.82	129.11	1.00	129.11	1.55	0.80	0.80
7.31	84.43	129.55	1.00	129.55	1.56	0.80	0.80
7.40	84.63	129.06	1.00	129.06	1.56	0.80	0.80
7.45	84.52	128.43	1.00	128.43	1.56	0.80	0.80
7.54	83.95	126.75	1.00	126.75	1.57	0.79	0.79
7.60	82.84	124.58	1.00	124.58	1.58	0.79	0.79
7.68	81.22	121.42	1.00	121.42	1.59	0.79	0.79
7.74	79.70	118.70	1.00	118.70	1.60	0.78	0.78
7.83	78.55	116.27	1.00	116.27	1.61	0.78	0.78
7.90	78.35	115.47	1.00	115.47	1.61	0.78	0.78
7.98	79.10	115.95	1.00	115.95	1.62	0.78	0.78
8.05	80.62	117.66	1.00	117.66	1.62	0.78	0.78
8.12	81.69	118.66	1.00	118.66	1.62	0.78	0.78
8.19	81.66	118.08	1.00	118.08	1.62	0.78	0.78
8.27	80.48	115.81	1.00	115.81	1.64	0.78	0.78
8.36	79.13	113.39	1.00	113.39	1.65	0.77	0.77
8.41	78.35	111.75	1.00	111.75	1.61	0.77	0.77
8.50	78.42	111.21	1.00	111.21	1.57	0.77	0.77
8.60	78.79	111.10	1.00	111.10	1.54	0.77	0.77
8.70	78.76	110.43	1.00	110.43	1.56	0.77	0.77
8.74	70.97	99.16	1.00	99.16	1.64	0.75	0.75
8.78	65.57	92.36	1.00	92.36	1.68	0.73	0.73
8.81	63.58	89.84	1.00	89.84	1.71	0.73	0.73
8.86	69.75	97.38	1.00	97.38	1.66	0.74	0.74

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.91	73.77	102.14	1.00	102.14	1.64	0.75	0.75
8.94	74.34	102.81	1.00	102.81	1.64	0.75	0.75
9.02	73.80	101.95	1.00	101.95	1.66	0.75	0.75
9.10	72.52	100.12	1.00	100.12	1.68	0.75	0.75
9.17	71.17	98.18	1.00	98.18	1.69	0.74	0.74
9.22	69.95	96.47	1.00	96.47	1.70	0.74	0.74
9.31	69.01	94.84	1.00	94.84	1.71	0.74	0.74
9.37	68.50	93.92	1.00	93.92	1.72	0.74	0.74
9.42	68.60	93.81	1.00	93.81	1.72	0.74	0.74
9.52	69.18	94.01	1.00	94.01	1.72	0.74	0.74
9.60	70.19	94.84	1.00	94.84	1.71	0.74	0.74
9.66	71.54	96.20	1.00	96.20	1.70	0.74	0.74
9.74	73.13	97.75	1.00	97.75	1.69	0.74	0.74
9.81	74.58	99.20	1.00	99.20	1.69	0.75	0.75
9.89	75.79	100.34	1.00	100.34	1.68	0.75	0.75
9.98	77.04	101.50	1.00	101.50	1.68	0.75	0.75
10.03	78.79	103.47	1.00	103.47	1.68	0.75	0.75
10.13	81.26	106.04	1.00	106.04	1.67	0.76	0.76
10.23	84.06	108.97	1.00	108.97	1.66	0.76	0.76
10.32	86.45	111.33	1.00	111.33	1.65	0.77	0.77
10.38	88.11	112.97	1.00	112.97	1.65	0.77	0.77
10.47	88.68	113.17	1.00	113.17	1.65	0.77	0.77
10.57	88.44	112.36	1.00	112.36	1.65	0.77	0.77
10.66	87.94	111.05	1.00	111.05	1.61	0.77	0.77
10.76	87.67	110.18	1.00	110.18	1.57	0.77	0.77
10.85	88.00	110.11	1.00	110.11	1.53	0.77	0.77
10.92	88.54	110.44	1.00	110.44	1.55	0.77	0.77
11.00	85.17	105.80	1.00	105.80	1.58	0.76	0.76
11.07	82.17	101.74	1.00	101.74	1.61	0.75	0.75
11.10	80.21	99.18	1.00	99.18	1.63	0.75	0.75
11.15	82.81	102.16	1.00	102.16	1.62	0.75	0.75
11.19	85.41	105.18	1.00	105.18	1.61	0.76	0.76
11.24	87.43	107.45	1.00	107.45	1.61	0.76	0.76
11.29	89.66	109.95	1.00	109.95	1.61	0.77	0.77
11.34	92.29	112.96	1.00	112.96	1.60	0.77	0.77
11.40	94.89	115.81	1.00	115.81	1.60	0.78	0.78
11.47	96.81	117.83	1.00	117.83	1.60	0.78	0.78
11.53	97.72	118.60	1.00	118.60	1.60	0.78	0.78
11.58	98.23	118.97	1.00	118.97	1.60	0.78	0.78
11.65	98.70	119.16	1.00	119.16	1.61	0.78	0.78
11.72	99.17	119.34	1.00	119.34	1.61	0.78	0.78
11.77	99.00	118.88	1.00	118.88	1.61	0.78	0.78
11.82	98.36	117.83	1.00	117.83	1.62	0.78	0.78
11.88	97.25	116.19	1.00	116.19	1.64	0.78	0.78
11.97	96.10	114.49	1.00	114.49	1.65	0.77	0.77
12.02	94.75	112.75	1.00	112.75	1.65	0.77	0.77
12.06	93.54	110.95	1.00	110.95	1.65	0.77	0.77
12.11	93.03	110.11	1.00	110.11	1.65	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.21	92.63	109.15	1.00	109.15	1.65	0.76	0.76
12.25	92.93	109.21	1.00	109.21	1.64	0.76	0.76
12.30	93.00	109.05	1.00	109.05	1.64	0.76	0.76
12.31	93.44	109.51	1.00	109.51	1.63	0.77	0.77
12.32	93.64	109.72	1.00	109.72	1.63	0.77	0.77
12.35	94.21	110.25	1.00	110.25	1.62	0.77	0.77
12.40	95.26	111.26	1.00	111.26	1.61	0.77	0.77
12.45	96.78	112.82	1.00	112.82	1.60	0.77	0.77
12.52	98.43	114.40	1.00	114.40	1.60	0.77	0.77
12.56	100.32	116.43	1.00	116.43	1.59	0.78	0.78
12.62	102.04	118.16	1.00	118.16	1.59	0.78	0.78
12.65	103.69	119.90	1.00	119.90	1.56	0.78	0.78
12.71	105.14	121.32	1.00	121.32	1.53	0.78	0.78
12.76	107.34	123.61	1.00	123.61	1.48	0.79	0.79
12.83	110.34	126.74	1.00	126.74	1.48	0.79	0.79
12.88	114.29	131.03	1.00	131.03	1.50	0.80	0.80
12.93	118.94	136.14	1.00	136.14	1.50	0.81	0.81
12.98	121.44	138.73	1.00	138.73	1.52	0.81	0.81
13.03	123.77	141.10	1.00	141.10	1.52	0.81	0.81
13.04	120.16	136.93	1.00	136.93	1.54	0.81	0.81
13.07	122.72	139.66	1.00	139.66	1.54	0.81	0.81
13.13	125.66	142.70	1.00	142.70	1.55	0.82	0.82
13.17	134.36	152.37	1.00	152.37	1.53	0.83	0.83
13.22	137.87	156.08	1.00	156.08	1.53	0.84	0.84
13.27	140.13	158.31	1.00	158.31	1.54	0.84	0.84
13.32	141.11	159.12	1.00	159.12	1.54	0.84	0.84
13.37	141.28	159.00	1.00	159.00	1.55	0.84	0.84
13.41	140.67	158.02	1.00	158.02	1.55	0.84	0.84
13.46	139.05	155.85	1.00	155.85	1.56	0.83	0.83
13.51	137.63	153.98	1.00	153.98	1.57	0.83	0.83
13.56	135.98	151.81	1.00	151.81	1.58	0.83	0.83
13.60	134.29	149.65	1.00	149.65	1.59	0.83	0.83
13.66	132.81	147.65	1.00	147.65	1.60	0.82	0.82
13.75	131.80	145.98	1.00	145.98	1.60	0.82	0.82
13.80	131.19	145.02	1.00	145.02	1.60	0.82	0.82
13.89	130.75	144.01	1.00	144.01	1.61	0.82	0.82
13.94	129.81	142.69	1.00	142.69	1.61	0.82	0.82
13.99	128.19	140.62	1.00	140.62	1.63	0.81	0.81
14.09	125.39	137.21	1.00	137.21	1.65	0.81	0.81
14.14	122.28	133.79	1.00	133.79	1.68	0.80	0.80
14.23	119.38	130.35	1.00	130.35	1.70	0.80	0.80
14.28	117.19	127.54	1.00	127.54	1.68	0.79	0.79
14.38	116.43	125.95	1.00	125.95	1.66	0.79	0.79
14.42	115.35	124.40	1.00	124.40	1.63	0.79	0.79
14.52	115.79	124.40	1.00	124.40	1.63	0.79	0.79
14.57	116.75	125.23	1.00	125.23	1.64	0.79	0.79
14.67	117.53	125.60	1.00	125.60	1.64	0.79	0.79
14.68	117.83	125.93	1.00	125.93	1.64	0.79	0.79

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.70	116.41	124.39	1.00	124.39	1.65	0.79	0.79
14.75	116.58	124.38	1.00	124.38	1.66	0.79	0.79
14.80	116.18	123.80	1.00	123.80	1.66	0.79	0.79
14.89	116.21	123.45	1.00	123.45	1.67	0.79	0.79
14.94	114.76	121.75	1.00	121.75	1.68	0.79	0.79
15.04	111.83	118.29	1.00	118.29	1.69	0.78	0.78
15.13	107.24	113.18	1.01	114.51	1.71	0.77	0.77
15.21	101.74	107.19	1.06	113.68	1.74	0.77	0.77
15.28	95.87	100.87	1.10	111.36	1.76	0.77	0.77
15.38	90.00	94.46	1.14	107.63	1.79	0.76	0.76
15.47	83.86	87.79	1.17	102.77	1.82	0.75	0.75
15.57	77.55	80.97	1.20	97.12	1.85	0.74	0.74
15.67	70.76	73.71	1.23	90.52	1.89	0.73	0.73
15.77	63.91	66.40	1.26	83.47	1.93	0.71	0.71
15.86	57.27	59.33	1.29	76.63	1.98	0.44	0.70
15.96	51.73	53.45	1.34	71.45	2.03	0.29	0.69
16.05	47.31	48.75	1.40	68.25	2.09	0.22	0.68
16.15	43.60	44.83	1.51	67.79	2.15	0.21	0.68
16.25	41.11	42.13	1.63	68.47	2.20	0.22	0.68
16.31	39.86	40.76	1.71	69.57	2.23	0.25	0.68
16.39	39.72	40.48	1.70	68.78	2.23	0.23	0.68
16.48	40.50	41.08	1.65	67.59	2.21	0.21	0.68
16.59	43.06	43.47	1.53	66.70	2.17	0.19	0.67
16.68	47.95	48.20	1.40	67.68	2.09	0.21	0.68
16.76	53.89	53.96	1.31	70.90	2.01	0.27	0.69
16.86	58.72	58.53	1.27	74.31	1.95	0.36	0.69
16.92	61.25	60.90	1.25	76.25	1.92	0.43	0.70
17.02	61.65	61.10	1.25	76.36	1.92	0.43	0.70
17.11	61.14	60.41	1.26	76.12	1.94	0.42	0.70
17.22	60.40	59.48	1.28	75.94	1.96	0.42	0.70
17.35	58.51	57.44	1.34	77.19	2.04	0.46	0.70
17.45	53.15	52.07	1.57	81.76	2.18	0.68	0.71
17.55	43.40	42.36	2.26	95.58	2.38	0.74	0.74
17.61	33.92	32.93	3.48	114.42	2.57	0.77	0.77
17.64	27.41	26.45	4.70	124.38	2.70	0.79	0.79
17.70	24.84	23.84	5.27	125.58	2.75	0.79	0.79
17.75	23.12	22.09	5.71	126.01	2.79	0.79	0.79
17.80	22.04	20.96	6.07	127.17	2.82	0.79	0.79
17.85	21.57	20.45	6.49	132.79	2.85	0.80	0.80
17.94	24.37	23.10	5.83	134.72	2.80	0.81	0.81
17.99	29.74	28.29	4.75	134.51	2.70	0.81	0.81
18.09	36.42	34.65	3.76	130.35	2.60	0.80	0.80
18.15	38.34	36.42	3.61	131.44	2.58	0.80	0.80
18.23	36.08	34.09	3.99	135.89	2.63	0.81	0.81
18.33	27.03	25.22	5.88	148.20	2.80	0.82	0.82
18.43	18.43	16.85	8.99	151.54	3.01	1.12	1.20
18.52	11.28	9.87	14.46	142.66	3.27	0.79	0.70
18.59	9.25	7.88	15.23	120.07	3.30	0.54	0.56

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
18.72	8.44	7.05	14.48	102.14	3.27	0.33	0.50
18.81	7.87	6.47	14.17	91.69	3.26	0.29	0.46
18.87	7.73	6.32	14.34	90.62	3.27	0.28	0.45
18.95	7.94	6.48	14.76	95.67	3.28	0.31	0.46
19.05	8.95	7.39	13.77	101.75	3.24	0.40	0.53
19.14	11.32	9.56	10.96	104.74	3.12	0.45	0.68
19.22	15.43	13.37	7.56	101.14	2.92	0.75	0.75
19.29	23.29	20.64	4.44	91.70	2.67	0.73	0.73
19.38	36.79	33.12	2.43	80.52	2.41	0.61	0.71
19.44	54.77	49.78	1.63	81.04	2.21	0.64	0.71
19.53	73.63	67.13	1.37	92.11	2.06	0.73	0.73
19.62	89.35	81.50	1.30	105.61	1.99	0.76	0.76
19.69	100.62	91.73	1.27	116.28	1.95	0.78	0.78
19.79	106.79	97.11	1.26	122.62	1.94	0.79	0.79
19.86	108.17	98.11	1.28	125.15	1.96	0.79	0.79
19.97	105.91	95.65	1.30	124.06	1.99	0.79	0.79
20.07	101.09	90.89	1.33	120.48	2.02	0.78	0.78
20.16	94.14	84.23	1.37	115.28	2.06	0.78	0.78
20.26	84.49	75.23	1.38	103.79	2.07	0.76	0.76
20.34	72.68	64.34	1.43	91.71	2.10	0.73	0.73
20.43	59.83	52.55	1.52	80.02	2.16	0.58	0.71
20.50	47.95	41.63	2.03	84.51	2.33	0.72	0.72
20.60	37.70	32.23	3.01	96.91	2.50	0.74	0.74
20.62	30.48	25.73	4.28	110.02	2.66	0.77	0.77
20.63	28.08	23.58	4.89	115.31	2.72	0.78	0.78
20.68	27.74	23.22	5.10	118.43	2.74	0.78	0.78
20.73	27.64	23.06	5.32	122.67	2.76	0.79	0.79
20.82	25.48	21.06	6.08	128.12	2.82	0.80	0.80
20.87	23.45	19.23	6.78	130.45	2.87	0.80	0.80
20.91	21.57	17.54	7.32	128.42	2.91	0.80	0.80
20.96	19.58	15.59	7.98	124.40	2.95	0.79	0.79
21.05	17.59	13.84	8.82	122.12	3.00	0.63	0.99
21.11	16.98	13.29	9.07	120.49	3.02	0.63	0.95
21.17	17.11	13.36	9.02	120.44	3.01	0.63	0.95
21.25	21.23	17.01	6.86	116.62	2.88	0.78	0.78
21.30	31.25	25.68	4.13	106.03	2.64	0.76	0.76
21.37	48.56	40.77	2.31	94.37	2.39	0.74	0.74
21.45	68.84	58.49	1.62	94.86	2.20	0.74	0.74
21.49	87.80	75.10	1.41	105.59	2.09	0.76	0.76
21.58	103.45	88.68	1.33	117.80	2.02	0.78	0.78
21.64	115.70	99.28	1.29	128.46	1.98	0.80	0.80
21.69	124.50	106.86	1.28	136.49	1.96	0.81	0.81
21.78	130.41	111.69	1.27	142.03	1.95	0.82	0.82
21.83	133.78	114.42	1.27	145.79	1.96	0.82	0.82
21.89	135.43	115.57	1.28	148.03	1.97	0.82	0.82
21.98	136.01	115.67	1.29	149.32	1.98	0.83	0.83
22.03	135.90	115.31	1.30	150.06	1.99	0.83	0.83
22.12	134.89	114.06	1.31	149.60	2.01	0.83	0.83

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
22.22	133.20	112.20	1.32	148.31	2.02	0.82	0.82
22.26	130.88	110.01	1.33	146.45	2.03	0.82	0.82
22.36	128.38	107.52	1.34	144.21	2.04	0.82	0.82
22.41	125.79	105.07	1.36	142.38	2.05	0.82	0.82
22.51	123.53	102.88	1.35	138.65	2.04	0.81	0.81
22.60	121.33	100.82	1.34	134.71	2.03	0.81	0.81
22.70	119.34	98.95	1.32	130.43	2.01	0.80	0.80
22.75	116.88	96.72	1.32	127.90	2.02	0.80	0.80
22.84	109.32	89.92	1.36	122.31	2.05	0.79	0.79
22.89	107.14	87.93	1.37	120.57	2.06	0.78	0.78
22.90	104.88	85.98	1.38	118.82	2.07	0.78	0.78
22.94	110.11	90.42	1.34	121.26	2.04	0.78	0.78
23.00	112.36	92.21	1.32	122.07	2.02	0.79	0.79
23.08	118.94	97.70	1.29	126.15	1.98	0.79	0.79
23.13	127.04	104.57	1.26	131.91	1.94	0.80	0.80
23.20	134.05	110.43	1.24	136.83	1.90	0.81	0.81
23.27	137.05	112.81	1.23	138.66	1.89	0.81	0.81
23.33	135.57	111.40	1.23	136.90	1.89	0.81	0.81
23.42	131.55	107.76	1.23	132.83	1.89	0.80	0.80
23.48	126.94	103.73	1.24	128.30	1.90	0.80	0.80
23.57	123.16	100.30	1.24	124.68	1.91	0.79	0.79
23.61	121.20	98.52	1.25	122.97	1.92	0.79	0.79
23.66	121.50	98.62	1.25	123.25	1.92	0.79	0.79
23.73	124.04	100.52	1.25	125.44	1.92	0.79	0.79
23.80	127.95	103.59	1.24	128.73	1.91	0.80	0.80
23.85	131.96	106.79	1.24	132.25	1.90	0.80	0.80
23.94	134.80	108.87	1.24	134.50	1.90	0.81	0.81
24.00	135.88	109.59	1.24	135.41	1.90	0.81	0.81
24.09	135.37	108.86	1.24	134.81	1.90	0.81	0.81
24.16	133.34	106.93	1.24	133.09	1.91	0.80	0.80
24.24	130.04	104.25	1.23	128.02	1.89	0.80	0.80
24.33	125.79	100.75	1.21	122.05	1.86	0.79	0.79
24.43	121.10	96.90	1.19	115.53	1.84	0.78	0.78
24.52	114.28	90.85	1.23	111.31	1.88	0.77	0.77
24.58	108.90	86.13	1.25	107.54	1.92	0.76	0.76
24.59	104.52	82.40	1.27	104.41	1.95	0.76	0.76
24.63	104.21	82.05	1.27	104.24	1.95	0.76	0.76
24.68	103.45	81.24	1.28	103.96	1.96	0.76	0.76
24.77	102.47	80.14	1.29	103.52	1.98	0.75	0.75
24.82	100.31	78.15	1.31	102.59	2.01	0.75	0.75
24.92	97.85	75.83	1.34	101.32	2.03	0.75	0.75
25.01	95.22	73.42	1.36	100.09	2.06	0.75	0.75
25.06	92.38	70.94	1.39	98.75	2.08	0.75	0.75
25.16	89.48	68.36	1.42	97.29	2.10	0.74	0.74
25.25	86.51	65.75	1.46	95.92	2.13	0.74	0.74
25.30	83.55	63.24	1.50	94.77	2.15	0.74	0.74
25.41	80.44	60.52	1.55	93.81	2.17	0.74	0.74
25.49	77.27	57.80	1.61	93.24	2.20	0.74	0.74

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
25.55	73.97	55.02	1.70	93.42	2.23	0.74	0.74
25.64	70.59	52.13	1.81	94.24	2.27	0.74	0.74
25.70	67.02	49.15	1.95	95.94	2.31	0.74	0.74
25.79	63.24	46.00	2.13	97.75	2.35	0.74	0.74
25.89	58.92	42.45	2.35	99.94	2.40	0.75	0.75
25.94	54.26	38.75	2.63	101.97	2.45	0.75	0.75
26.02	49.37	34.89	2.95	102.81	2.50	0.75	0.75
26.12	45.05	31.51	3.23	101.92	2.54	0.75	0.75
26.17	40.83	28.31	3.52	99.58	2.57	0.75	0.75
26.28	37.02	25.37	3.84	97.30	2.61	0.74	0.74
26.36	33.31	22.57	4.17	94.10	2.65	0.74	0.74
26.45	29.43	19.65	4.69	92.22	2.70	0.73	0.73
26.50	24.94	16.31	5.63	91.86	2.78	0.73	0.73
26.61	20.15	12.75	7.37	93.95	2.91	0.74	0.74
26.70	15.97	9.43	10.10	95.23	3.07	0.35	0.67
26.77	12.97	7.45	12.95	96.46	3.21	0.35	0.53
26.85	11.85	6.70	14.12	94.58	3.26	0.34	0.48
26.94	11.45	6.41	14.29	91.60	3.27	0.29	0.46
27.04	11.95	6.71	13.15	88.25	3.22	0.28	0.48
27.14	12.22	6.86	12.68	86.95	3.20	0.27	0.49
27.23	12.90	7.27	11.66	84.75	3.15	0.26	0.52
27.28	13.22	7.46	11.13	83.02	3.13	0.24	0.53
27.29	13.29	7.50	10.38	77.81	3.09	0.24	0.54
27.38	13.29	7.47	9.96	74.44	3.07	0.16	0.53
27.48	13.27	7.43	9.89	73.48	3.06	0.18	0.53
27.57	13.27	7.41	10.67	79.00	3.10	0.22	0.53
27.64	13.30	7.41	11.31	83.76	3.13	0.26	0.53
27.65	13.44	7.49	12.08	90.43	3.17	0.27	0.53
27.74	14.52	8.14	11.82	96.17	3.16	0.36	0.58
27.80	16.91	9.63	10.69	102.90	3.10	0.41	0.69
27.90	19.17	11.00	9.59	105.58	3.05	0.48	0.79
27.99	19.34	11.07	9.67	106.99	3.05	0.48	0.79
28.07	17.12	9.65	10.91	105.31	3.11	0.45	0.69
28.16	14.45	7.96	12.63	100.58	3.20	0.39	0.57
28.25	12.53	6.75	13.86	93.48	3.25	0.31	0.48
28.34	11.52	6.10	14.13	86.20	3.26	0.25	0.44
28.44	11.01	5.76	14.19	81.77	3.26	0.21	0.41
28.53	10.84	5.64	14.27	80.51	3.26	0.21	0.40
28.62	11.75	6.17	14.04	86.70	3.26	0.23	0.44
28.76	14.21	7.64	12.54	95.81	3.19	0.35	0.55
28.86	17.65	9.69	11.11	107.72	3.12	0.45	0.69
28.96	20.32	11.26	10.51	118.36	3.09	0.58	0.80
29.08	21.30	11.80	11.10	130.98	3.12	0.70	0.84
29.19	22.07	12.21	11.60	141.58	3.15	0.86	0.87
29.29	27.50	15.40	8.64	133.06	2.99	0.80	0.80
29.39	40.70	25.08	5.15	129.21	2.74	0.80	0.80
29.50	57.67	36.81	3.37	124.06	2.55	0.79	0.79
29.63	66.88	42.86	3.19	136.79	2.53	0.81	0.81

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
29.65	70.22	45.09	3.13	141.18	2.52	0.81	0.81
29.66	71.00	45.61	3.10	141.50	2.52	0.82	0.82
29.72	73.53	47.34	2.95	139.57	2.50	0.81	0.81
29.80	77.81	50.31	2.70	135.94	2.46	0.81	0.81
29.85	89.49	58.79	2.17	127.49	2.36	0.79	0.79
29.94	111.58	75.08	1.62	121.89	2.20	0.79	0.79
30.00	135.50	93.20	1.37	127.60	2.06	0.79	0.79
30.05	152.98	106.83	1.28	136.43	1.96	0.81	0.81
30.14	162.60	114.57	1.23	140.95	1.89	0.81	0.81
30.19	167.56	118.78	1.20	142.08	1.84	0.82	0.82
30.24	169.61	120.45	1.18	142.19	1.83	0.82	0.82
30.29	169.68	120.31	1.18	142.38	1.83	0.82	0.82
30.38	167.72	118.51	1.19	141.39	1.84	0.82	0.82
30.43	164.79	116.05	1.20	139.76	1.85	0.81	0.81
30.48	161.62	113.47	1.21	137.67	1.87	0.81	0.81
30.54	159.16	111.46	1.22	135.86	1.87	0.81	0.81
30.62	158.35	110.69	1.22	134.98	1.87	0.81	0.81
30.67	157.77	110.16	1.22	134.34	1.87	0.80	0.80
30.72	158.55	110.67	1.22	134.61	1.87	0.81	0.81
30.76	159.46	111.32	1.21	134.89	1.86	0.81	0.81
30.86	162.06	113.16	1.20	135.92	1.85	0.81	0.81
30.91	165.09	115.46	1.19	137.26	1.84	0.81	0.81
30.95	168.94	118.37	1.17	138.94	1.82	0.81	0.81
31.03	173.83	122.03	1.15	140.71	1.80	0.81	0.81
31.10	179.36	126.19	1.13	142.33	1.78	0.82	0.82
31.15	185.03	130.44	1.10	144.07	1.76	0.82	0.82
31.20	189.66	133.76	1.09	146.05	1.75	0.82	0.82
31.26	192.52	135.69	1.09	147.81	1.75	0.82	0.82
31.34	186.22	130.42	1.13	147.23	1.78	0.82	0.82
31.37	184.63	129.08	1.14	146.99	1.79	0.82	0.82
31.38	181.39	126.56	1.15	145.70	1.80	0.82	0.82
31.43	184.63	129.02	1.13	146.17	1.78	0.82	0.82
31.47	179.33	124.92	1.15	143.44	1.80	0.82	0.82
31.55	171.64	118.91	1.17	139.35	1.82	0.81	0.81
31.59	160.34	110.19	1.21	132.93	1.86	0.80	0.80
31.66	147.76	100.47	1.24	124.83	1.91	0.79	0.79
31.73	135.75	91.20	1.28	116.80	1.97	0.78	0.78
31.78	125.08	83.04	1.33	110.36	2.02	0.77	0.77
31.84	115.64	75.76	1.40	106.34	2.09	0.76	0.76
31.93	107.23	69.27	1.51	104.84	2.16	0.76	0.76
31.98	100.42	64.06	1.66	106.04	2.22	0.76	0.76
32.02	98.18	62.19	1.75	108.88	2.25	0.76	0.76
32.09	97.00	61.07	1.83	111.87	2.27	0.77	0.77
32.16	98.89	62.18	1.83	113.86	2.27	0.77	0.77
32.22	100.29	63.04	1.82	114.52	2.27	0.77	0.77
32.27	103.49	65.22	1.76	114.53	2.25	0.77	0.77
32.34	106.02	66.91	1.71	114.38	2.24	0.77	0.77
32.42	108.89	68.85	1.66	114.11	2.22	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
32.46	113.04	71.82	1.58	113.62	2.19	0.77	0.77
32.54	117.73	75.15	1.51	113.25	2.15	0.77	0.77
32.60	121.74	78.23	1.43	112.00	2.11	0.77	0.77
32.67	124.81	80.60	1.38	111.53	2.07	0.77	0.77
32.75	127.51	82.59	1.35	111.85	2.05	0.77	0.77
32.81	130.38	84.43	1.35	113.95	2.05	0.77	0.77
32.89	133.38	86.29	1.35	116.21	2.04	0.78	0.78
32.94	129.47	83.21	1.38	114.84	2.07	0.77	0.77
32.95	131.02	84.23	1.38	116.07	2.07	0.78	0.78
33.00	132.88	85.36	1.38	117.56	2.07	0.78	0.78
33.06	141.08	91.06	1.34	122.40	2.04	0.79	0.79
33.11	142.26	91.66	1.35	123.66	2.04	0.79	0.79
33.20	141.21	90.60	1.36	123.53	2.06	0.79	0.79
33.25	139.02	88.78	1.39	123.06	2.08	0.79	0.79
33.34	137.03	87.07	1.41	122.48	2.09	0.79	0.79
33.38	136.69	86.68	1.42	122.68	2.10	0.79	0.79
33.48	138.41	87.63	1.41	123.78	2.10	0.79	0.79
33.58	141.92	89.83	1.40	125.79	2.09	0.79	0.79
33.63	146.74	93.05	1.38	128.81	2.07	0.80	0.80
33.73	152.41	96.75	1.37	132.15	2.06	0.80	0.80
33.82	158.96	101.09	1.35	136.16	2.04	0.81	0.81
33.87	165.74	105.66	1.33	140.58	2.03	0.81	0.81
33.96	172.72	110.29	1.32	145.13	2.01	0.82	0.82
34.02	180.58	115.54	1.30	150.66	2.00	0.83	0.83
34.11	190.03	121.77	1.29	157.32	1.98	0.84	0.84
34.18	200.49	128.68	1.28	164.99	1.97	0.85	0.85
34.26	210.44	135.11	1.28	172.52	1.96	0.86	0.86
34.35	219.45	140.77	1.28	179.50	1.96	0.86	0.86
34.44	227.51	145.83	1.27	185.53	1.95	0.87	0.87
34.49	233.96	150.02	1.27	190.23	1.95	0.88	0.88
34.59	237.94	152.42	1.27	192.83	1.94	0.88	0.88
34.69	240.00	153.47	1.26	194.12	1.94	0.88	0.88
34.76	240.94	153.92	1.26	194.53	1.94	0.88	0.88
34.83	240.60	153.43	1.26	194.02	1.94	0.88	0.88
34.93	237.97	151.43	1.26	191.54	1.94	0.88	0.88
35.02	233.82	148.39	1.27	188.08	1.95	0.87	0.87
35.12	229.78	145.60	1.27	184.23	1.94	0.87	0.87
35.22	226.47	143.26	1.26	181.13	1.94	0.87	0.87
35.30	222.22	140.29	1.26	177.46	1.94	0.86	0.86
35.38	208.55	130.48	1.29	168.21	1.98	0.85	0.85
35.43	198.10	123.09	1.31	161.35	2.00	0.84	0.84
35.46	189.40	116.99	1.33	155.80	2.03	0.83	0.83
35.51	187.20	115.53	1.33	153.78	2.03	0.83	0.83
35.56	176.78	108.45	1.35	146.76	2.05	0.82	0.82
35.66	163.52	99.31	1.39	138.53	2.08	0.81	0.81
35.70	148.20	89.01	1.46	130.03	2.13	0.80	0.80
35.80	131.87	77.90	1.59	123.66	2.19	0.79	0.79
35.89	111.32	64.17	1.87	119.95	2.28	0.78	0.78

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
35.96	89.09	49.72	2.43	120.81	2.41	0.78	0.78
36.04	68.24	36.73	3.28	120.37	2.54	0.78	0.78
36.14	52.15	27.04	4.33	117.01	2.66	0.78	0.78
36.19	43.48	22.01	5.03	110.69	2.73	0.77	0.77
36.28	40.51	20.23	5.44	110.05	2.77	0.77	0.77
36.33	40.51	20.24	5.35	108.32	2.76	0.76	0.76
36.42	42.30	21.24	5.09	108.08	2.74	0.76	0.76
36.48	45.97	23.38	4.59	107.27	2.69	0.76	0.76
36.52	51.03	26.20	4.31	112.95	2.66	0.77	0.77
36.62	54.10	27.78	4.31	119.67	2.66	0.78	0.78
36.68	54.07	27.55	4.59	126.59	2.69	0.79	0.79
36.77	52.82	26.73	4.79	128.11	2.71	0.80	0.80
36.86	54.64	27.76	4.56	126.60	2.69	0.79	0.79
36.90	67.67	35.75	3.22	115.19	2.53	0.77	0.77
37.00	98.14	55.13	1.87	103.13	2.29	0.75	0.75
37.10	140.34	83.45	1.35	112.56	2.04	0.77	0.77
37.20	182.54	113.15	1.21	136.84	1.86	0.81	0.81
37.29	213.04	135.23	1.09	147.30	1.75	0.82	0.82
37.39	232.34	149.01	1.00	149.01	1.70	0.83	0.83
37.49	241.91	155.00	1.00	155.00	1.70	0.83	0.83
37.53	245.57	156.74	1.02	160.20	1.72	0.84	0.84
37.58	246.07	156.33	1.06	165.44	1.73	0.85	0.85
37.62	247.84	156.88	1.08	169.66	1.75	0.85	0.85
37.69	250.56	157.82	1.11	175.10	1.77	0.86	0.86
37.77	253.53	158.95	1.13	179.78	1.78	0.86	0.86
37.82	254.98	159.10	1.15	183.39	1.80	0.87	0.87
37.87	254.84	158.42	1.17	184.85	1.81	0.87	0.87
37.91	252.72	156.44	1.18	184.82	1.83	0.87	0.87
37.97	248.23	152.87	1.20	183.06	1.85	0.87	0.87
38.06	241.92	148.07	1.21	179.59	1.87	0.86	0.86
38.10	235.58	143.53	1.22	175.74	1.88	0.86	0.86
38.17	230.89	140.30	1.23	172.34	1.89	0.86	0.86
38.25	228.09	138.57	1.22	169.66	1.88	0.85	0.85
38.35	225.79	137.24	1.22	167.11	1.87	0.85	0.85
38.40	223.43	135.86	1.21	164.83	1.87	0.85	0.85
38.46	221.65	134.68	1.21	163.21	1.86	0.84	0.84
38.54	220.87	134.09	1.21	162.26	1.86	0.84	0.84
38.60	220.87	134.14	1.21	161.69	1.86	0.84	0.84
38.69	222.22	135.09	1.20	161.77	1.85	0.84	0.84
38.74	224.92	137.05	1.19	162.53	1.83	0.84	0.84
38.83	227.85	138.91	1.18	163.73	1.82	0.84	0.84
38.88	229.20	139.97	1.17	163.54	1.81	0.84	0.84
38.97	228.76	139.65	1.16	162.47	1.81	0.84	0.84
39.02	227.25	138.83	1.16	160.45	1.80	0.84	0.84
39.11	224.44	136.82	1.16	158.54	1.81	0.84	0.84
39.16	218.51	132.80	1.17	154.99	1.81	0.83	0.83
39.23	205.48	123.73	1.20	148.10	1.85	0.82	0.82
39.24	200.81	120.69	1.20	145.08	1.85	0.82	0.82

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
39.28	198.62	119.29	1.20	143.39	1.85	0.82	0.82
39.32	201.93	121.86	1.18	144.08	1.83	0.82	0.82
39.39	194.55	116.84	1.20	139.67	1.84	0.81	0.81
39.47	183.96	109.44	1.22	133.48	1.88	0.80	0.80
39.54	171.48	100.68	1.25	125.99	1.92	0.79	0.79
39.62	158.42	91.63	1.29	117.99	1.98	0.78	0.78
39.71	145.73	82.95	1.33	110.70	2.03	0.77	0.77
39.76	134.50	75.46	1.39	105.08	2.08	0.76	0.76
39.85	125.32	69.36	1.46	101.34	2.13	0.75	0.75
39.90	117.87	64.48	1.53	98.95	2.17	0.75	0.75
40.00	111.05	60.00	1.63	97.53	2.20	0.74	0.74
40.06	104.71	55.91	1.73	96.96	2.24	0.74	0.74
40.15	98.67	52.00	1.87	97.18	2.28	0.74	0.74
40.21	92.83	48.24	2.05	98.86	2.33	0.75	0.75
40.29	86.59	44.24	2.31	102.19	2.39	0.75	0.75
40.35	79.68	39.85	2.72	108.27	2.46	0.76	0.76
40.43	72.22	35.37	3.16	111.81	2.53	0.77	0.77
40.52	63.85	30.51	3.76	114.58	2.60	0.77	0.77
40.58	55.21	25.70	4.47	115.00	2.68	0.77	0.77
40.67	46.88	21.09	5.54	116.83	2.77	0.78	0.78
40.77	41.63	18.24	6.45	117.65	2.85	0.78	0.78
40.84	39.14	16.87	6.99	117.99	2.89	0.78	0.78
40.89	42.28	18.55	6.27	116.25	2.83	0.78	0.78
40.94	49.75	22.62	4.92	111.31	2.72	0.77	0.77
41.03	61.46	29.20	3.53	103.18	2.57	0.75	0.75
41.08	73.03	35.94	2.68	96.47	2.45	0.74	0.74
41.14	82.03	41.30	2.24	92.51	2.37	0.73	0.73
41.22	87.70	44.68	2.04	90.97	2.33	0.73	0.73
41.28	90.43	46.24	1.97	91.29	2.31	0.73	0.73
41.33	91.99	46.96	1.99	93.52	2.32	0.74	0.74
41.42	93.64	47.61	2.04	97.02	2.33	0.74	0.74
41.47	97.01	49.31	2.04	100.81	2.33	0.75	0.75
41.52	104.03	53.17	1.96	104.48	2.31	0.76	0.76
41.62	115.47	59.72	1.81	107.92	2.27	0.76	0.76
41.67	130.01	68.21	1.66	112.91	2.22	0.77	0.77
41.76	144.45	76.74	1.54	118.23	2.17	0.78	0.78
41.82	156.39	83.80	1.48	123.75	2.14	0.79	0.79
41.90	165.43	89.14	1.44	128.02	2.11	0.80	0.80
41.99	171.57	92.73	1.41	131.05	2.10	0.80	0.80
42.05	174.81	94.61	1.40	132.58	2.09	0.80	0.80
42.15	175.22	94.64	1.40	132.77	2.09	0.80	0.80
42.23	173.33	93.24	1.42	132.06	2.10	0.80	0.80
42.30	169.55	90.73	1.44	130.51	2.11	0.80	0.80
42.38	163.64	86.97	1.47	127.88	2.13	0.80	0.80
42.48	153.79	80.87	1.53	123.60	2.16	0.79	0.79
42.57	141.98	73.69	1.62	119.15	2.20	0.78	0.78
42.64	129.97	66.53	1.73	115.28	2.24	0.78	0.78
42.72	121.20	61.42	1.82	111.72	2.27	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
42.82	114.72	57.72	1.88	108.24	2.29	0.76	0.76
42.90	110.03	55.08	1.91	105.42	2.30	0.76	0.76
42.97	106.05	52.74	1.98	104.32	2.31	0.76	0.76
43.06	102.31	50.43	2.08	104.69	2.34	0.76	0.76
43.15	98.76	48.44	2.11	102.43	2.35	0.75	0.75
43.20	97.75	48.00	2.07	99.54	2.34	0.75	0.75
43.30	104.19	51.99	1.84	95.67	2.28	0.74	0.74
43.40	119.88	61.38	1.58	97.12	2.19	0.74	0.74
43.48	132.43	68.91	1.47	100.97	2.13	0.75	0.75
43.51	139.11	72.90	1.43	103.89	2.10	0.76	0.76
43.52	146.23	77.22	1.39	107.23	2.08	0.76	0.76
43.56	160.13	85.83	1.33	114.20	2.03	0.77	0.77
43.61	178.86	97.60	1.28	124.81	1.96	0.79	0.79
43.67	193.23	106.74	1.25	133.29	1.92	0.80	0.80
43.72	206.01	115.04	1.22	140.56	1.88	0.81	0.81
43.80	216.51	121.88	1.20	145.95	1.85	0.82	0.82
43.85	224.74	127.26	1.18	149.84	1.82	0.83	0.83
43.90	231.25	131.51	1.16	152.56	1.81	0.83	0.83
43.94	236.38	134.87	1.14	154.37	1.79	0.83	0.83
43.99	239.82	137.13	1.13	155.28	1.78	0.83	0.83
44.08	241.54	138.11	1.13	155.65	1.78	0.83	0.83
44.14	241.51	137.71	1.14	156.49	1.79	0.84	0.84
44.22	240.40	136.41	1.15	157.19	1.80	0.84	0.84
44.28	238.31	134.50	1.17	157.37	1.82	0.84	0.84
44.33	235.67	132.35	1.18	156.78	1.83	0.84	0.84
44.40	232.27	129.52	1.20	155.80	1.85	0.83	0.83
44.48	231.30	128.25	1.22	155.90	1.87	0.83	0.83
44.52	228.57	125.64	1.24	155.24	1.90	0.83	0.83
44.61	230.02	126.41	1.23	155.88	1.89	0.83	0.83
44.72	231.52	127.03	1.23	156.70	1.90	0.84	0.84
44.77	236.14	130.05	1.22	159.04	1.88	0.84	0.84
44.91	237.86	130.46	1.23	160.27	1.89	0.84	0.84
44.95	231.69	126.16	1.24	156.88	1.91	0.84	0.84
45.02	227.41	123.19	1.25	154.33	1.92	0.83	0.83
45.04	198.97	104.88	1.32	138.44	2.01	0.81	0.81
45.06	203.49	107.81	1.30	140.63	2.00	0.81	0.81
45.11	208.45	111.04	1.29	143.03	1.98	0.82	0.82
45.15	239.96	131.64	1.22	160.49	1.87	0.84	0.84
45.21	246.91	136.23	1.20	163.81	1.85	0.84	0.84
45.25	252.44	139.80	1.19	166.43	1.84	0.85	0.85
45.30	256.29	142.11	1.18	168.34	1.83	0.85	0.85
45.35	258.04	143.02	1.18	169.35	1.83	0.85	0.85
45.41	258.42	143.02	1.19	169.64	1.83	0.85	0.85
45.49	257.00	141.89	1.19	168.87	1.84	0.85	0.85
45.55	254.13	139.97	1.19	167.24	1.84	0.85	0.85
45.63	249.51	136.90	1.20	164.52	1.85	0.85	0.85
45.69	243.67	133.19	1.21	161.09	1.86	0.84	0.84
45.78	236.62	128.61	1.22	156.88	1.88	0.84	0.84

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
45.84	228.05	123.25	1.23	151.68	1.89	0.83	0.83
45.93	217.69	116.85	1.24	145.18	1.91	0.82	0.82
46.02	205.11	109.16	1.26	137.24	1.93	0.81	0.81
46.08	190.40	100.37	1.28	128.00	1.96	0.80	0.80
46.16	174.41	90.73	1.30	118.20	1.99	0.78	0.78
46.24	157.13	80.39	1.35	108.31	2.04	0.76	0.76
46.31	138.07	68.91	1.44	99.54	2.12	0.75	0.75
46.41	117.36	56.54	1.67	94.32	2.22	0.74	0.74
46.48	95.77	44.06	2.17	95.41	2.36	0.74	0.74
46.56	75.72	32.98	3.08	101.49	2.51	0.75	0.75
46.65	58.08	23.81	4.47	106.39	2.68	0.76	0.76
46.75	45.43	17.64	5.95	104.92	2.81	0.76	0.76
46.84	36.62	12.08	8.01	96.75	2.95	0.74	0.74
46.94	30.75	9.96	9.25	92.20	3.03	0.42	0.71
47.02	25.79	8.18	10.96	89.65	3.12	0.36	0.58
47.08	21.37	6.60	13.29	87.68	3.22	0.33	0.47
47.12	18.76	5.66	15.23	86.24	3.30	0.32	0.40
47.16	17.85	5.33	15.88	84.67	3.33	0.30	0.38
47.21	17.81	5.32	15.49	82.35	3.31	0.28	0.38
47.27	17.46	5.18	15.33	79.44	3.31	0.26	0.37
47.35	16.42	4.80	15.97	76.72	3.33	0.23	0.34
47.40	15.74	4.56	15.95	72.71	3.33	0.22	0.33
47.50	15.37	4.42	15.62	68.97	3.32	0.17	0.32
47.55	15.16	4.34	15.04	65.28	3.29	0.16	0.31
47.61	15.00	4.27	14.89	63.67	3.29	0.14	0.31
47.69	14.73	4.17	15.00	62.57	3.29	0.14	0.30
47.76	14.39	4.05	15.25	61.71	3.30	0.13	0.29
47.83	14.02	3.91	15.40	60.22	3.31	0.13	0.28
47.93	13.85	3.84	15.20	58.40	3.30	0.11	0.27
48.02	13.82	3.82	15.00	57.34	3.29	0.10	0.27
48.09	13.88	3.84	14.67	56.35	3.28	0.11	0.27
48.18	13.85	3.82	14.94	57.05	3.29	0.10	0.27
48.27	13.88	3.82	15.29	58.44	3.30	0.12	0.27
48.37	13.98	3.85	15.87	61.09	3.33	0.13	0.27
48.46	14.12	3.89	16.20	62.98	3.34	0.14	0.28
48.52	14.18	3.90	16.46	64.25	3.35	0.15	0.28
48.60	14.25	3.92	16.64	65.23	3.35	0.16	0.28
48.70	14.38	3.96	16.68	65.99	3.35	0.16	0.28
48.79	14.65	4.04	16.50	66.70	3.35	0.16	0.29
48.85	15.06	4.18	16.39	68.42	3.34	0.17	0.30
48.94	15.74	4.40	16.24	71.44	3.34	0.20	0.31
49.04	16.68	4.71	15.57	73.34	3.31	0.23	0.34
49.13	18.30	5.25	15.62	82.09	3.32	0.22	0.38
49.23	21.13	6.21	14.82	92.00	3.29	0.41	0.44
49.33	24.04	7.18	14.31	102.80	3.27	0.51	0.51
49.38	24.88	7.46	14.69	109.60	3.28	0.57	0.53
49.42	25.93	7.81	14.70	114.80	3.28	0.64	0.56
49.48	26.70	8.06	14.75	118.93	3.28	0.70	0.58

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
49.53	28.79	8.76	13.86	121.43	3.25	0.73	0.63
49.58	29.43	8.97	13.78	123.62	3.24	0.76	0.64
49.63	30.10	9.19	13.66	125.52	3.24	0.79	0.66
49.72	30.91	9.44	13.37	126.23	3.23	0.81	0.67
49.77	31.42	9.60	13.13	125.98	3.22	0.80	0.69
49.83	31.42	9.59	13.08	125.40	3.22	0.79	0.68
49.92	30.71	9.33	13.37	124.67	3.23	0.79	0.67
49.97	30.39	9.21	13.41	123.55	3.23	0.76	0.66
50.04	29.48	8.89	13.80	122.65	3.25	0.74	0.64
50.11	29.82	8.99	13.61	122.33	3.24	0.74	0.64
50.20	30.21	9.10	13.25	120.55	3.22	0.76	0.65
50.27	30.78	9.28	12.51	116.01	3.19	0.68	0.66
50.34	29.50	8.83	12.20	107.79	3.18	0.58	0.63
50.45	26.76	7.90	12.55	99.22	3.19	0.45	0.56
50.54	23.73	6.88	13.43	92.39	3.23	0.38	0.49
50.59	21.13	6.01	14.59	87.71	3.28	0.35	0.43
50.68	19.24	5.37	15.59	83.78	3.32	0.30	0.38
50.79	18.13	4.99	16.06	80.17	3.33	0.26	0.36
50.88	17.81	4.88	16.03	78.18	3.33	0.25	0.35
50.98	17.64	4.81	16.19	77.89	3.34	0.25	0.34
51.07	17.81	4.86	15.67	76.09	3.32	0.25	0.35
51.17	18.43	5.05	14.19	71.67	3.26	0.21	0.36
51.24	19.51	5.40	12.74	68.77	3.20	0.16	0.39
51.33	20.19	5.61	12.56	70.43	3.19	0.20	0.40
51.46	20.09	5.56	13.45	74.75	3.23	0.25	0.40
51.46	19.80	5.46	14.31	78.20	3.27	0.25	0.39
51.51	19.77	5.45	14.62	79.60	3.28	0.28	0.39
51.56	19.87	5.47	14.98	82.02	3.29	0.28	0.39
51.65	19.95	5.49	15.35	84.26	3.31	0.31	0.39
51.71	20.09	5.53	15.72	86.89	3.32	0.33	0.39
51.79	20.49	5.65	15.73	88.80	3.32	0.35	0.40
51.85	21.23	5.88	15.68	92.19	3.32	0.37	0.42
51.94	22.11	6.15	15.66	96.33	3.32	0.43	0.44
51.99	23.22	6.51	15.77	102.62	3.32	0.48	0.46
52.09	24.17	6.80	16.12	109.52	3.33	0.57	0.49
52.19	27.74	7.93	14.73	116.81	3.28	0.67	0.57
52.28	33.34	9.72	12.62	122.63	3.20	0.78	0.69
52.35	36.42	10.69	12.02	128.41	3.17	0.87	0.76
52.43	37.06	10.87	12.22	132.82	3.18	0.95	0.78
52.52	35.17	10.25	13.30	136.28	3.22	0.97	0.73
52.62	35.61	10.37	13.11	135.93	3.22	0.98	0.74
52.72	35.98	10.46	12.80	133.92	3.20	0.94	0.75
52.81	34.26	9.89	13.70	135.53	3.24	0.89	0.71
52.91	31.32	8.94	16.37	146.31	3.34	1.03	0.64
53.00	37.23	10.79	14.34	154.70	3.27	1.38	0.77
53.10	62.36	18.71	7.92	148.13	2.95	0.82	0.82
53.20	108.21	33.14	3.92	129.79	2.62	0.80	0.80
53.29	163.78	50.57	2.27	114.61	2.38	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
53.38	213.88	66.21	1.72	114.09	2.24	0.77	0.77
53.46	260.07	80.59	1.49	119.81	2.14	0.78	0.78
53.53	292.05	90.48	1.45	130.93	2.12	0.80	0.80
53.63	323.19	100.02	1.40	139.93	2.09	0.81	0.81
53.73	361.79	111.85	1.31	146.92	2.01	0.82	0.82
53.82	388.35	119.89	1.25	150.03	1.92	0.83	0.83
53.92	387.71	119.45	1.23	146.54	1.89	0.82	0.82
53.94	360.18	110.85	1.25	138.23	1.92	0.81	0.81
53.96	336.26	103.38	1.27	131.20	1.95	0.80	0.80
53.97	349.08	107.34	1.25	134.16	1.92	0.80	0.80
54.05	377.59	116.04	1.22	141.00	1.87	0.81	0.81
54.08	426.28	131.09	1.15	150.15	1.79	0.83	0.83
54.13	473.21	145.55	1.06	154.41	1.74	0.83	0.83
54.19	518.79	159.56	1.00	159.56	1.70	0.84	0.84
54.25	524.22	161.12	1.01	162.94	1.71	0.84	0.84
54.28	510.87	156.95	1.06	166.66	1.74	0.85	0.85
54.29	486.82	149.48	1.10	164.40	1.76	0.85	0.85
54.34	486.89	149.42	1.10	164.35	1.76	0.85	0.85
54.35	492.20	151.05	1.09	164.72	1.75	0.85	0.85
54.40	504.89	154.89	1.07	165.62	1.74	0.85	0.85
54.44	522.30	160.18	1.04	166.45	1.72	0.85	0.85
54.49	535.62	164.19	1.01	165.88	1.71	0.85	0.85
54.53	546.25	167.39	1.00	167.39	1.70	0.85	0.85
54.57	558.27	171.02	1.00	171.02	1.69	0.85	0.85
54.58	567.78	173.92	1.00	173.92	1.70	0.86	0.86
54.63	560.90	171.71	1.01	173.90	1.71	0.86	0.86
54.68	536.31	164.04	1.08	176.93	1.75	0.86	0.86
54.73	510.50	156.00	1.12	175.12	1.78	0.86	0.86
54.78	499.67	152.59	1.14	173.29	1.79	0.86	0.86
54.83	493.63	150.64	1.15	172.82	1.80	0.86	0.86
54.88	497.14	151.64	1.15	175.08	1.80	0.86	0.86
54.92	500.68	152.65	1.17	178.37	1.81	0.86	0.86
54.97	510.81	155.66	1.16	180.73	1.81	0.87	0.87
55.02	513.44	156.38	1.16	181.62	1.81	0.87	0.87
55.12	487.90	148.39	1.20	178.01	1.85	0.86	0.86
55.17	449.17	136.44	1.25	170.63	1.92	0.85	0.85
55.25	410.54	124.51	1.29	160.49	1.98	0.84	0.84
55.31	394.21	119.43	1.29	154.46	1.98	0.83	0.83
55.36	388.18	117.52	1.27	148.87	1.95	0.83	0.83
55.45	381.09	115.23	1.25	143.68	1.91	0.82	0.82
55.50	365.91	110.54	1.25	137.89	1.92	0.81	0.81
55.60	351.24	105.95	1.26	133.93	1.94	0.80	0.80
55.65	332.24	100.11	1.28	128.15	1.96	0.80	0.80
55.71	324.14	97.58	1.27	124.39	1.96	0.79	0.79
55.75	320.40	96.40	1.26	121.19	1.93	0.78	0.78
55.79	325.12	97.79	1.25	121.90	1.91	0.79	0.79
55.84	332.47	99.97	1.24	123.76	1.90	0.79	0.79
55.89	338.01	101.60	1.23	125.39	1.90	0.79	0.79

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
55.90	341.15	102.54	1.23	126.17	1.89	0.79	0.79
55.94	336.26	101.02	1.24	124.98	1.90	0.79	0.79
55.99	327.63	98.34	1.25	122.89	1.92	0.79	0.79
56.03	317.88	95.34	1.26	120.41	1.94	0.78	0.78
56.08	311.67	93.40	1.27	118.54	1.95	0.78	0.78
56.14	306.37	91.74	1.27	116.74	1.95	0.78	0.78
56.22	299.89	89.70	1.28	114.65	1.96	0.77	0.77
56.28	294.29	87.95	1.28	112.90	1.97	0.77	0.77
56.33	292.57	87.39	1.29	112.38	1.97	0.77	0.77
56.38	294.06	87.79	1.28	112.46	1.97	0.77	0.77
56.45	301.34	89.92	1.27	114.23	1.95	0.77	0.77
56.52	312.58	93.24	1.25	117.01	1.93	0.78	0.78
56.62	325.19	96.94	1.24	120.21	1.90	0.78	0.78
56.66	338.42	100.88	1.22	123.02	1.87	0.79	0.79
56.73	350.06	104.30	1.21	126.65	1.87	0.79	0.79
56.81	357.11	106.33	1.22	129.59	1.87	0.80	0.80
56.95	363.42	108.06	1.23	132.64	1.89	0.80	0.80
57.00	372.46	110.72	1.23	135.80	1.88	0.81	0.81
57.09	373.11	110.80	1.23	136.52	1.89	0.81	0.81
57.19	368.58	109.32	1.24	135.85	1.91	0.81	0.81
57.27	354.04	104.88	1.25	131.44	1.92	0.80	0.80
57.35	357.65	105.87	1.23	130.16	1.89	0.80	0.80
57.44	356.17	105.33	1.21	127.36	1.86	0.79	0.79
57.50	364.37	107.70	1.18	127.07	1.83	0.79	0.79
57.52	378.10	111.77	1.18	131.85	1.83	0.80	0.80
57.58	409.37	121.03	1.17	141.73	1.82	0.82	0.82
57.63	432.08	127.73	1.17	149.17	1.81	0.83	0.83
57.72	439.00	129.66	1.17	151.31	1.81	0.83	0.83
57.77	433.73	128.03	1.16	148.26	1.80	0.82	0.82
57.82	429.55	126.71	1.13	143.29	1.78	0.82	0.82
57.91	436.73	128.72	1.06	137.09	1.74	0.81	0.81
57.96	442.84	130.46	1.00	130.46	1.69	0.80	0.80
58.02	458.90	135.16	1.00	135.16	1.66	0.81	0.81
58.09	469.26	138.12	1.00	138.12	1.65	0.81	0.81
58.16	484.88	142.65	1.00	142.65	1.63	0.82	0.82
58.25	491.12	144.36	1.00	144.36	1.64	0.82	0.82
58.30	487.65	143.26	1.00	143.26	1.66	0.82	0.82
58.40	479.62	140.74	1.00	140.74	1.69	0.81	0.81
58.50	468.52	137.31	1.02	139.77	1.71	0.81	0.81
58.56	467.50	136.92	1.01	138.70	1.71	0.81	0.81
58.64	464.81	136.01	1.03	140.28	1.72	0.81	0.81
58.73	474.79	138.81	1.05	145.16	1.73	0.82	0.82
58.78	488.15	142.67	1.02	145.87	1.72	0.82	0.82
58.88	506.71	147.98	1.00	147.98	1.69	0.82	0.82
58.97	511.03	149.10	1.00	149.10	1.66	0.83	0.83
59.07	506.24	147.53	1.00	147.53	1.66	0.82	0.82
59.13	493.59	143.73	1.00	143.73	1.65	0.82	0.82
59.23	484.71	140.99	1.00	140.99	1.65	0.81	0.81

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
59.31	464.47	134.94	1.00	134.94	1.65	0.81	0.81
59.38	450.35	130.71	1.00	130.71	1.65	0.80	0.80
59.41	439.19	127.40	1.00	127.40	1.66	0.79	0.79
59.46	443.57	128.62	1.00	128.62	1.65	0.80	0.80
59.51	443.56	128.55	1.00	128.55	1.65	0.80	0.80
59.57	451.89	130.91	1.00	130.91	1.67	0.80	0.80
59.66	471.05	136.37	1.00	136.37	1.67	0.81	0.81
59.75	492.31	142.44	1.00	142.44	1.70	0.82	0.82
59.80	506.48	146.48	1.01	147.84	1.71	0.82	0.82
59.85	508.64	147.04	1.07	156.99	1.74	0.84	0.84
59.91	504.22	145.65	1.08	158.02	1.75	0.84	0.84
59.99	498.85	143.96	1.11	159.53	1.77	0.84	0.84
60.05	480.97	138.68	1.17	161.59	1.81	0.84	0.84
60.09	464.78	133.92	1.20	160.52	1.85	0.84	0.84
60.14	444.43	127.94	1.22	156.08	1.88	0.84	0.84
60.19	437.86	125.96	1.22	153.23	1.87	0.83	0.83
60.22	434.25	124.88	1.21	151.55	1.87	0.83	0.83
60.28	412.99	118.63	1.23	145.94	1.89	0.82	0.82
60.33	381.24	109.36	1.26	137.48	1.93	0.81	0.81
60.38	338.97	97.07	1.31	126.83	2.00	0.79	0.79
60.42	309.75	88.57	1.35	119.65	2.05	0.78	0.78
60.48	282.02	80.50	1.38	111.02	2.07	0.77	0.77
60.57	262.48	74.78	1.36	101.50	2.05	0.75	0.75
60.66	243.89	69.35	1.32	91.67	2.02	0.73	0.73
60.68	232.16	65.95	1.30	85.85	1.99	0.72	0.72
60.69	225.51	64.02	1.29	82.84	1.98	0.71	0.71
60.74	217.75	61.75	1.30	80.07	1.99	0.59	0.71
60.79	206.27	58.41	1.30	76.18	2.00	0.42	0.70
60.84	192.16	54.32	1.32	71.82	2.02	0.30	0.69
60.89	182.35	51.47	1.33	68.64	2.03	0.23	0.68
60.98	174.35	49.12	1.36	66.57	2.05	0.19	0.67
61.03	168.07	47.30	1.46	69.19	2.13	0.24	0.68
61.08	164.86	46.35	1.72	79.69	2.24	0.57	0.71
61.18	164.63	46.24	1.95	90.12	2.31	0.73	0.73
61.23	168.20	47.23	2.12	100.04	2.35	0.75	0.75
61.31	194.08	54.62	1.72	94.03	2.24	0.74	0.74
61.42	236.42	66.70	1.41	94.11	2.09	0.74	0.74
61.47	287.17	81.21	1.24	100.64	1.90	0.75	0.75
61.51	331.30	93.81	1.14	107.25	1.79	0.76	0.76
61.54	366.14	103.76	1.05	108.54	1.73	0.76	0.76
61.57	395.83	112.23	1.00	112.23	1.70	0.77	0.77
61.58	418.64	118.74	1.00	118.74	1.67	0.78	0.78
61.61	393.43	111.49	1.00	111.49	1.70	0.77	0.77
61.63	367.65	104.10	1.03	107.07	1.72	0.76	0.76
61.63	257.89	72.70	1.26	91.77	1.94	0.73	0.73
61.66	191.36	53.66	1.48	79.27	2.14	0.55	0.71
61.67	129.55	35.97	2.37	85.35	2.40	0.72	0.72
61.70	152.96	42.66	1.96	83.80	2.31	0.72	0.72

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
61.71	180.90	50.64	1.67	84.55	2.22	0.72	0.72
61.76	206.41	57.90	1.51	87.45	2.15	0.72	0.72
61.80	228.84	64.28	1.42	91.10	2.10	0.73	0.73
61.84	250.40	70.41	1.34	94.04	2.03	0.74	0.74
61.86	279.75	78.77	1.26	98.87	1.93	0.75	0.75
61.93	312.34	88.02	1.18	103.69	1.82	0.75	0.75
61.98	357.76	100.92	1.00	100.92	1.73	0.75	0.75
62.04	405.56	114.48	1.00	114.48	1.68	0.77	0.77
62.09	451.78	127.59	1.00	127.59	1.64	0.79	0.79
62.14	481.91	136.10	1.00	136.10	1.62	0.81	0.81
62.19	499.12	140.93	1.00	140.93	1.60	0.81	0.81
62.24	508.93	143.65	1.00	143.65	1.59	0.82	0.82
62.26	519.32	146.58	1.00	146.58	1.58	0.82	0.82
62.29	519.05	146.46	1.00	146.46	1.58	0.82	0.82
62.38	515.71	145.37	1.00	145.37	1.60	0.82	0.82
62.44	490.28	138.07	1.00	138.07	1.65	0.81	0.81
62.46	469.07	132.02	1.00	132.02	1.69	0.80	0.80
62.47	448.15	126.07	1.00	126.07	1.70	0.79	0.79
62.51	453.68	127.59	1.00	127.59	1.69	0.79	0.79
62.56	463.98	130.45	1.00	130.45	1.69	0.80	0.80
62.60	477.62	134.26	1.00	134.26	1.68	0.80	0.80
62.65	481.73	135.35	1.00	135.35	1.68	0.81	0.81
62.70	482.34	135.46	1.00	135.46	1.66	0.81	0.81
62.75	483.05	135.59	1.00	135.59	1.65	0.81	0.81
62.80	494.83	138.85	1.00	138.85	1.64	0.81	0.81
62.85	525.29	147.40	1.00	147.40	1.60	0.82	0.82
62.89	569.18	159.73	1.00	159.73	1.56	0.84	0.84
62.97	619.66	173.86	1.00	173.86	1.54	0.86	0.86
63.04	667.84	187.32	1.00	187.32	1.52	0.87	0.87
63.09	703.12	197.18	1.00	197.18	1.50	0.88	0.88
63.13	715.51	200.57	1.00	200.57	1.51	0.89	0.89
63.19	716.52	200.74	1.00	200.74	1.54	0.89	0.89
63.23	720.23	201.69	1.00	201.69	1.57	0.89	0.89
63.28	726.78	203.42	1.00	203.42	1.59	0.89	0.89
63.32	729.18	204.02	1.00	204.02	1.57	0.89	0.89
63.38	725.67	202.89	1.00	202.89	1.49	0.89	0.89
63.44	726.68	203.06	1.00	203.06	1.43	0.89	0.89
63.52	715.48	199.75	1.00	199.75	1.43	0.89	0.89
63.57	697.37	194.57	1.00	194.57	1.49	0.88	0.88
63.66	659.58	183.79	1.00	183.79	1.52	0.87	0.87
63.73	534.95	148.76	1.00	148.76	1.63	0.83	0.83
63.76	455.61	126.50	1.03	130.54	1.72	0.80	0.80
63.76	411.85	114.24	1.12	127.66	1.77	0.79	0.79
63.78	471.87	131.02	1.00	131.02	1.70	0.80	0.80
63.81	512.86	142.46	1.00	142.46	1.67	0.82	0.82
63.85	526.43	146.19	1.00	146.19	1.68	0.82	0.82
63.86	522.58	145.10	1.00	145.10	1.70	0.82	0.82
63.91	497.92	138.14	1.07	148.35	1.74	0.82	0.82

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
63.94	483.78	134.14	1.12	150.35	1.77	0.83	0.83
63.95	480.34	133.15	1.14	151.38	1.79	0.83	0.83
64.00	476.26	131.94	1.14	150.67	1.79	0.83	0.83
64.02	473.22	131.08	1.14	149.37	1.79	0.83	0.83
64.05	475.78	131.75	1.12	148.02	1.78	0.82	0.82
64.09	478.18	132.36	1.11	146.64	1.77	0.82	0.82
64.11	480.07	132.86	1.09	144.77	1.75	0.82	0.82
64.15	482.26	133.43	1.07	142.44	1.74	0.82	0.82
64.20	494.31	136.71	1.03	141.24	1.72	0.81	0.81
64.25	512.59	141.74	1.00	141.74	1.70	0.82	0.82
64.29	535.70	148.11	1.00	148.11	1.68	0.82	0.82
64.34	570.38	157.68	1.00	157.68	1.64	0.84	0.84
64.43	605.81	167.40	1.00	167.40	1.60	0.85	0.85
64.48	630.95	174.30	1.00	174.30	1.56	0.86	0.86
64.53	642.69	177.47	1.00	177.47	1.53	0.86	0.86
64.58	655.07	180.82	1.00	180.82	1.52	0.87	0.87
64.63	680.65	187.83	1.00	187.83	1.51	0.87	0.87
64.68	709.63	195.77	1.00	195.77	1.52	0.88	0.88
64.73	718.74	198.20	1.00	198.20	1.53	0.88	0.88
64.77	735.60	202.79	1.00	202.79	1.51	0.89	0.89
64.82	751.19	207.01	1.00	207.01	1.48	0.89	0.89
64.87	732.64	201.76	1.00	201.76	1.49	0.89	0.89
64.89	713.98	196.56	1.00	196.56	1.50	0.88	0.88
64.93	689.59	189.73	1.00	189.73	1.53	0.88	0.88
64.94	715.81	196.96	1.00	196.96	1.51	0.88	0.88
64.98	725.69	199.62	1.00	199.62	1.50	0.89	0.89
64.99	734.03	201.90	1.00	201.90	1.50	0.89	0.89
65.03	732.37	201.35	1.00	201.35	1.50	0.89	0.89
65.08	727.04	199.79	1.00	199.79	1.49	0.89	0.89
65.13	715.51	196.50	1.00	196.50	1.48	0.88	0.88
65.17	703.60	193.13	1.00	193.13	1.46	0.88	0.88
65.22	689.29	189.08	1.00	189.08	1.45	0.87	0.87
65.23	681.55	186.93	1.00	186.93	1.45	0.87	0.87
65.28	679.28	186.22	1.00	186.22	1.46	0.87	0.87
65.32	679.65	186.24	1.00	186.24	1.47	0.87	0.87
65.37	680.17	186.30	1.00	186.30	1.49	0.87	0.87
65.42	684.61	187.42	1.00	187.42	1.50	0.87	0.87
65.47	671.65	183.76	1.00	183.76	1.50	0.87	0.87
65.48	657.21	179.77	1.00	179.77	1.52	0.86	0.86
65.49	638.86	174.70	1.00	174.70	1.52	0.86	0.86
65.52	636.56	174.01	1.00	174.01	1.52	0.86	0.86
65.57	645.67	176.43	1.00	176.43	1.41	0.86	0.86
65.62	661.16	180.61	1.00	180.61	1.28	0.87	0.87
65.67	682.44	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.69	697.23	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.72	719.02	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.77	752.26	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.82	790.78	-1.00	1.00	-1.00	-1.00	0.00	0.00

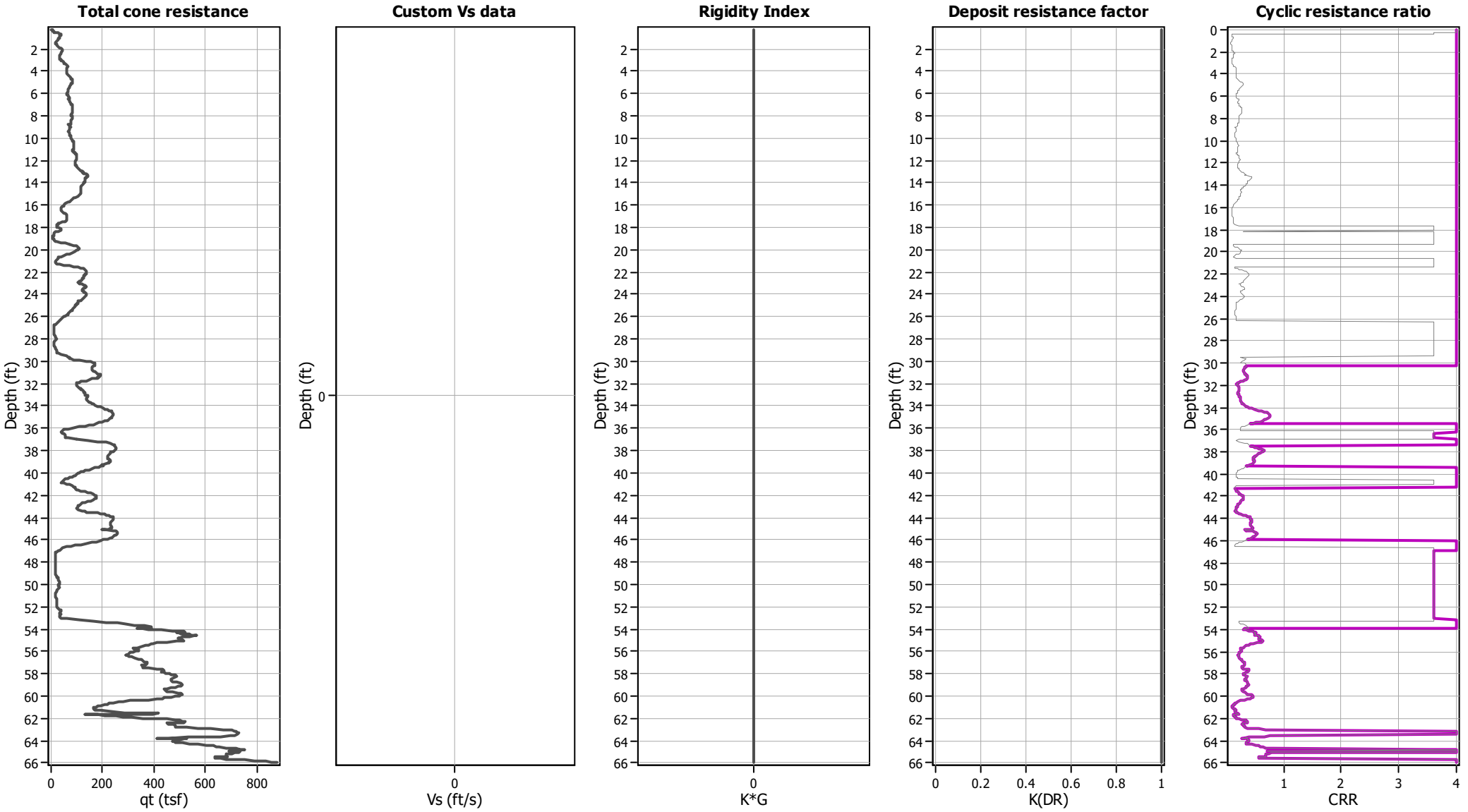
:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
65.86	811.97	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.86	833.63	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.91	854.04	-1.00	1.00	-1.00	-1.00	0.00	0.00
65.96	878.41	-1.00	1.00	-1.00	-1.00	0.00	0.00

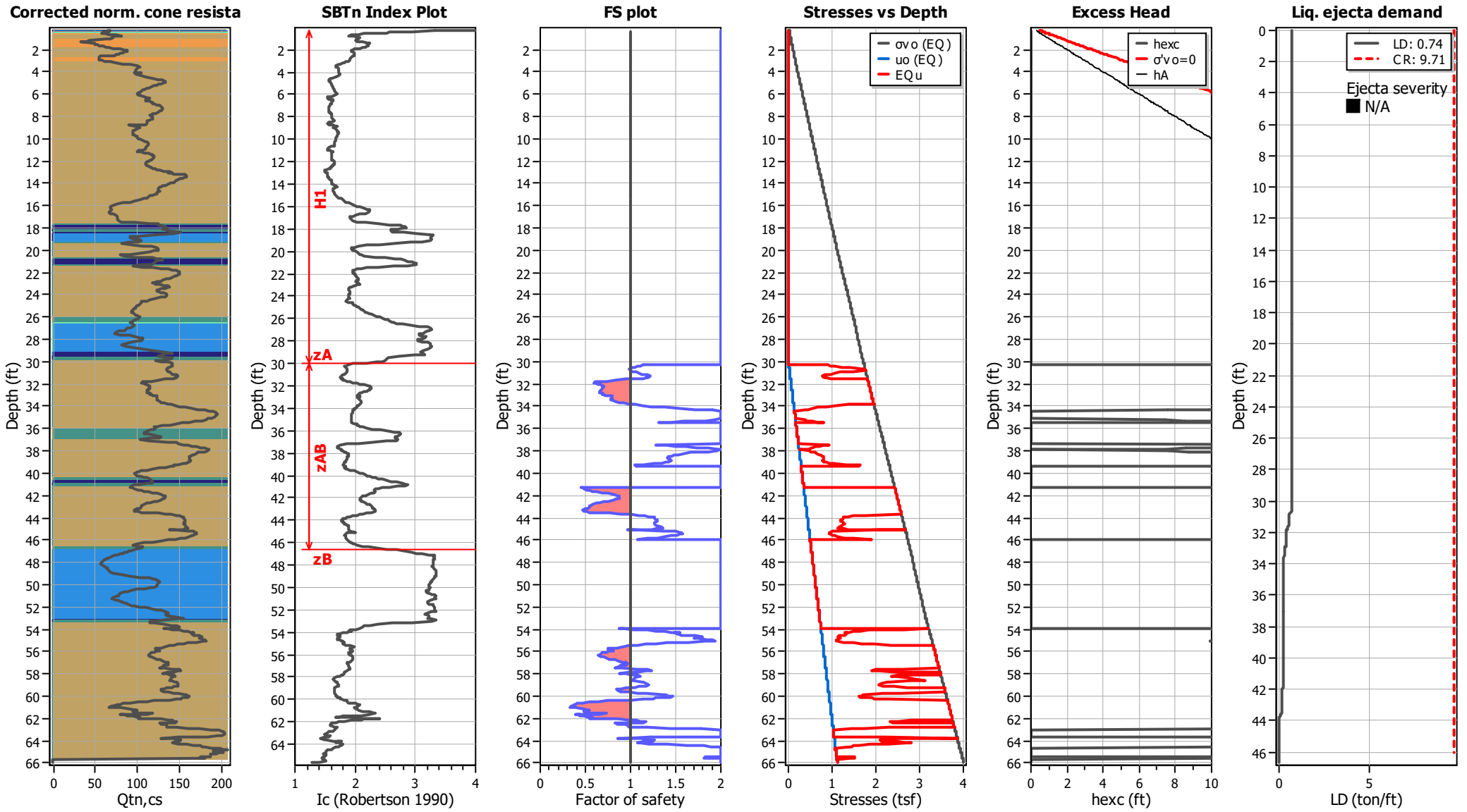
Abbreviations

q_t: Total cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Adjusted and corrected cone resistance due to fines
I_c: Soil behavior type index
$S_{u(liq)}/\sigma'_v$: Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$: Calculated peak undrained strength ratio

Aging Calculation Estimation



Ejecta Severity Estimation



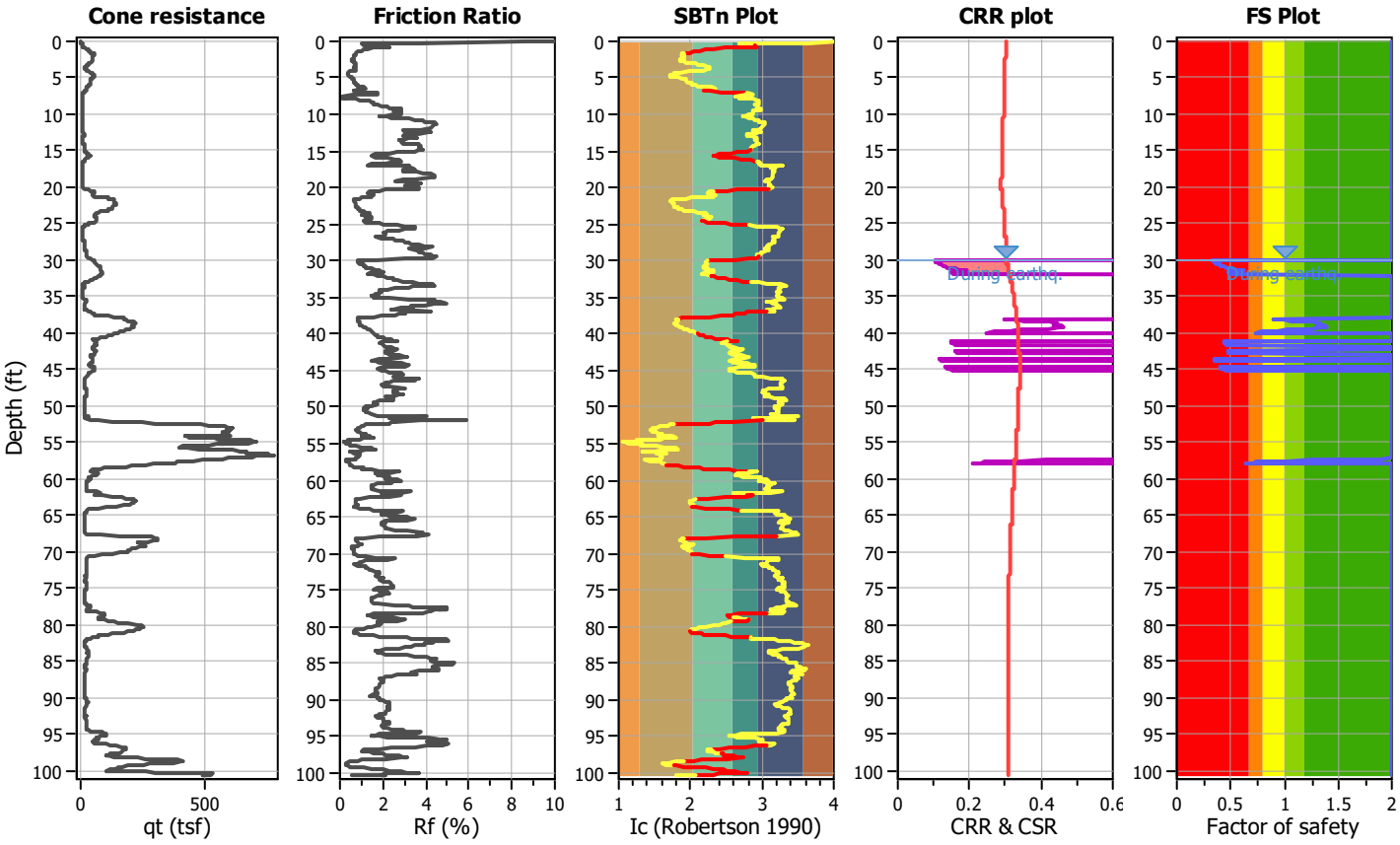
LIQUEFACTION ANALYSIS REPORT

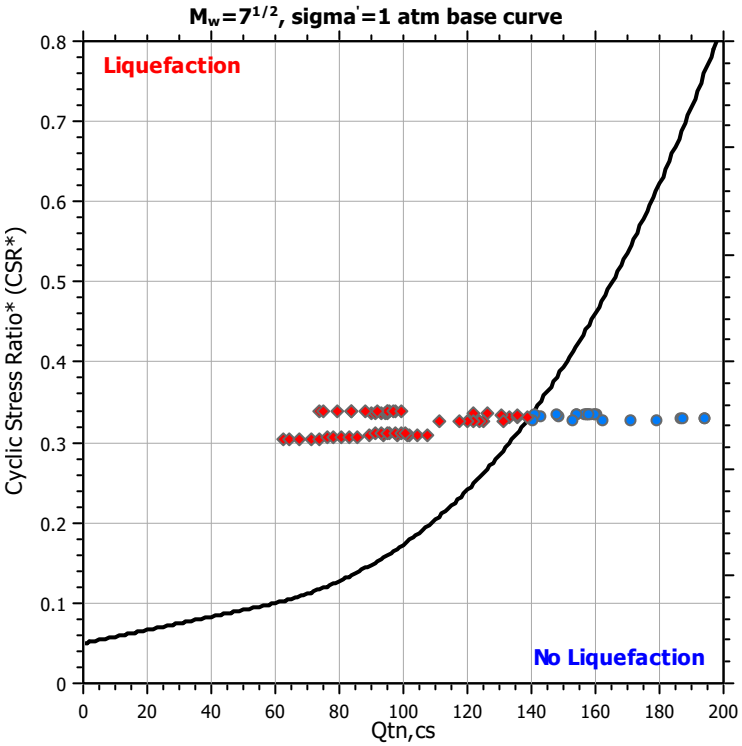
Project title : W1857-88-01 **Location : 331 The City Drive S**

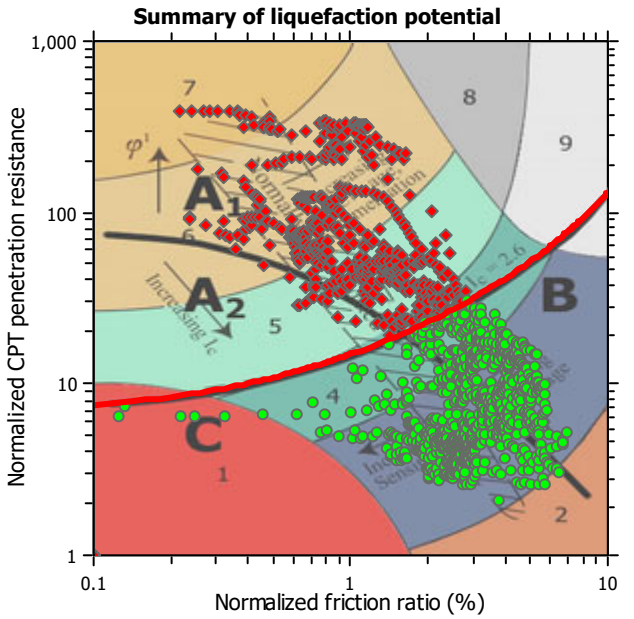
CPT file : CPT-3

Input parameters and analysis data

Analysis method:	NCEER (1998)	G.W.T. (in-situ):	54.00 ft	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	NCEER (1998)	G.W.T. (earthq.):	30.00 ft	Fill height:	N/A	Limit depth applied:	Yes
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	62.00 ft
Earthquake magnitude M_w:	6.65	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.63	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

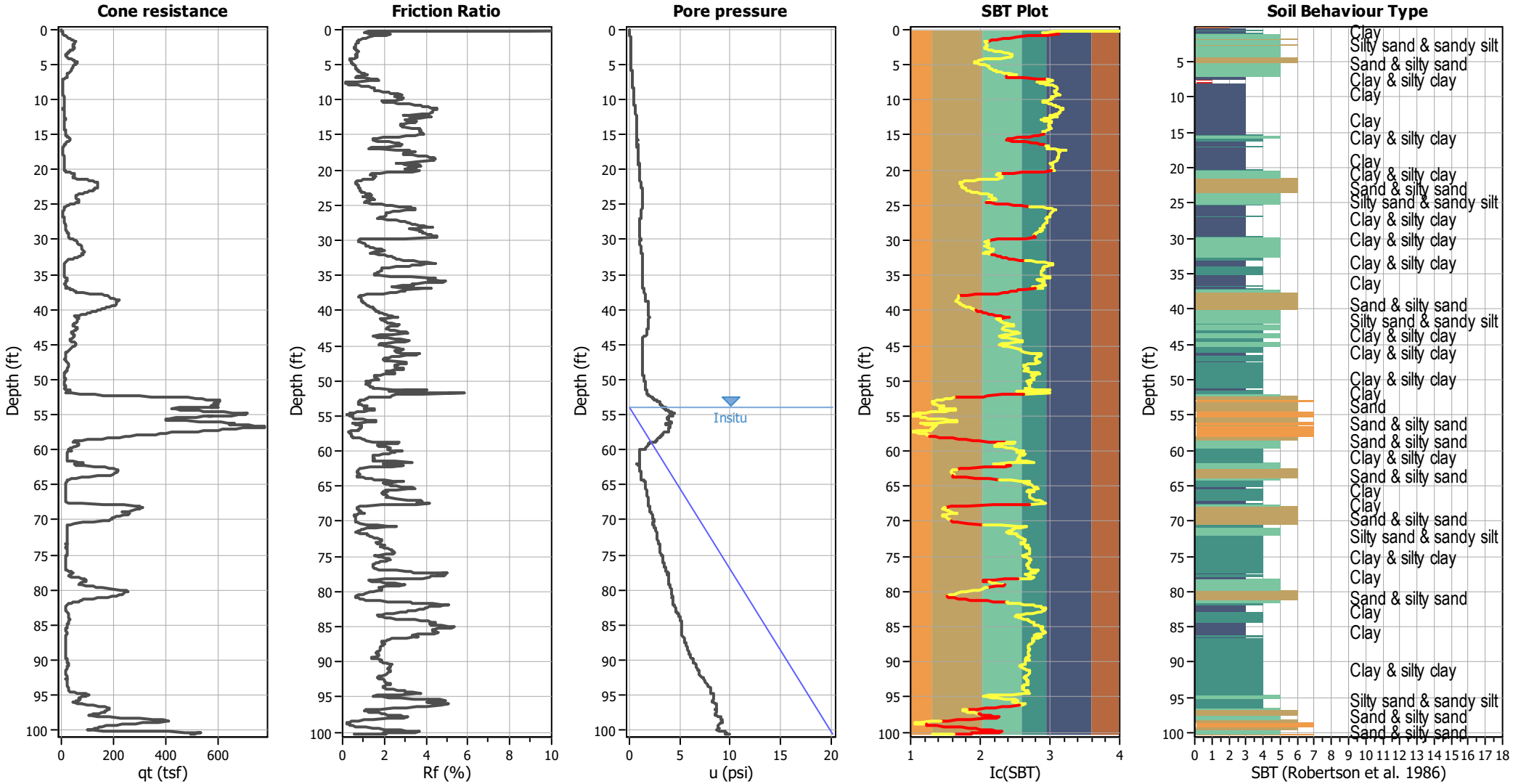






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



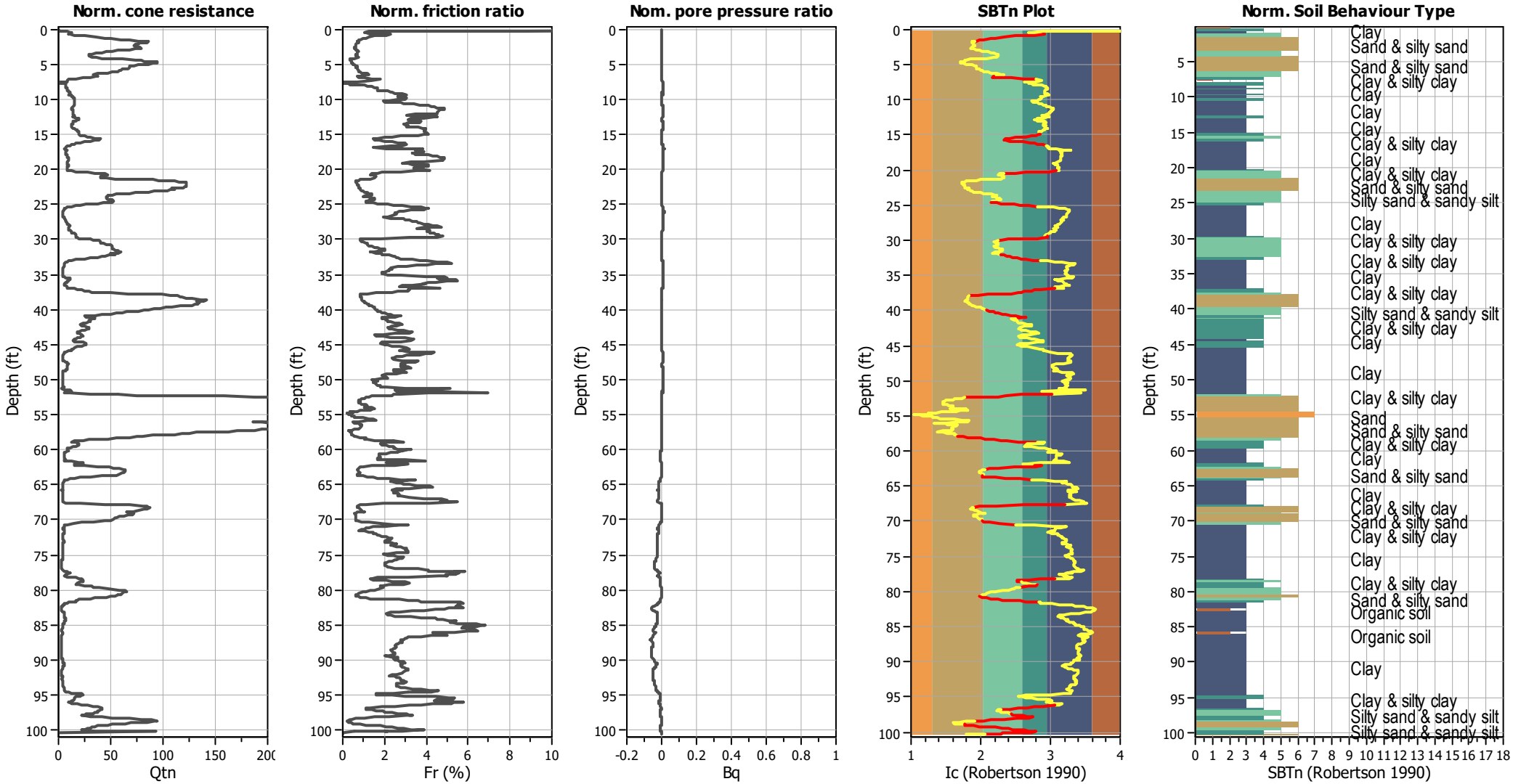
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	62.00 ft

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



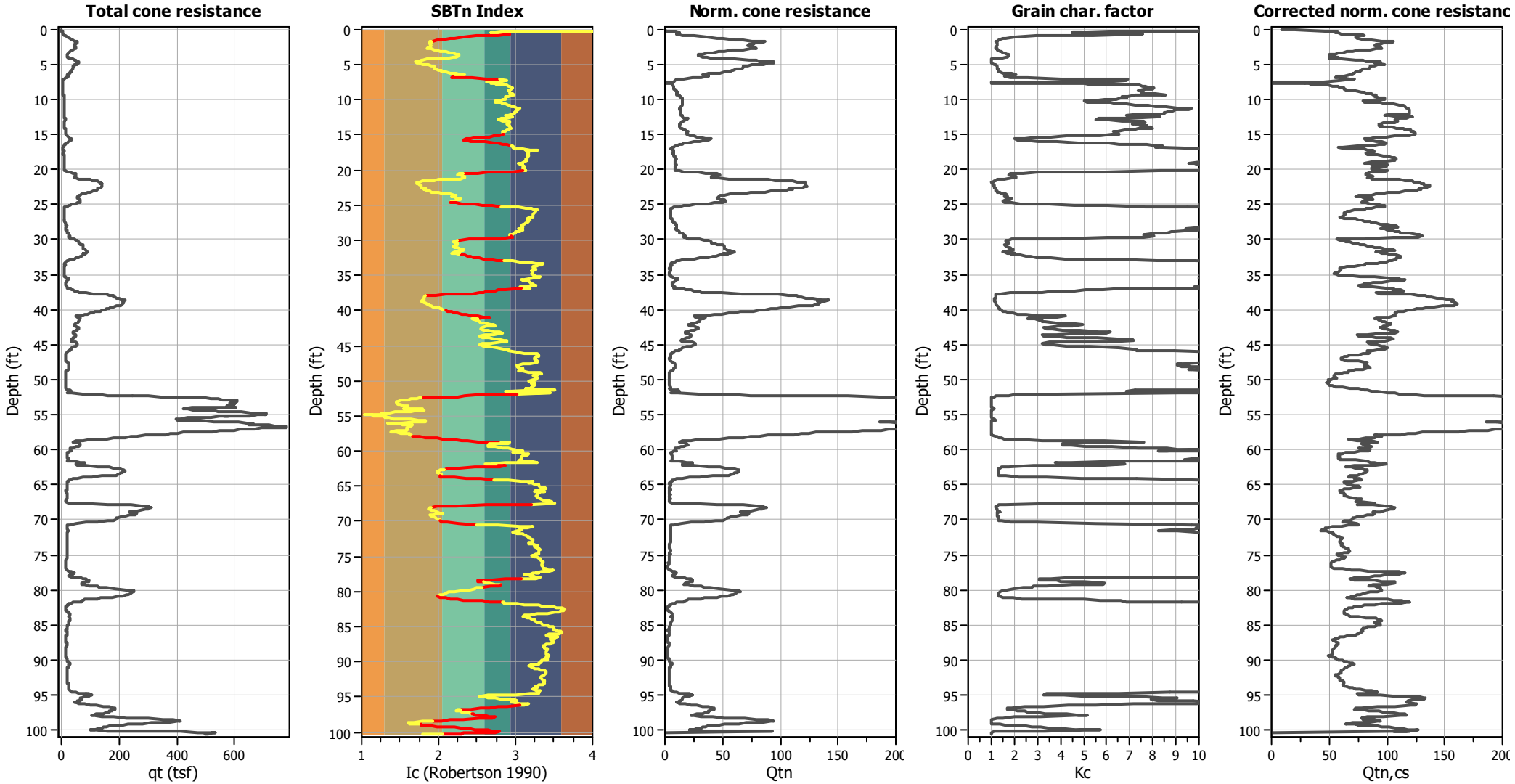
Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	62.00 ft

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

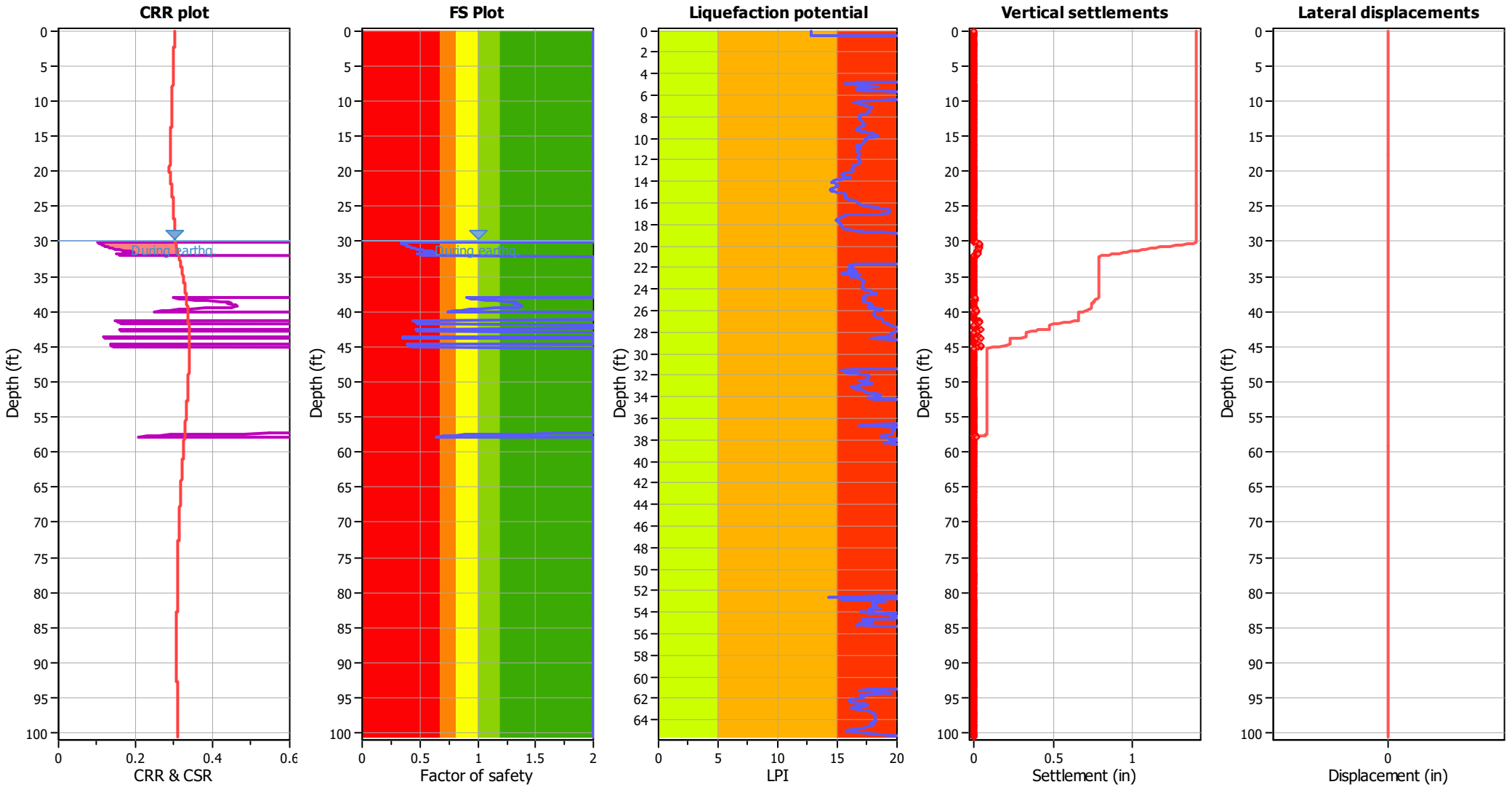
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	62.00 ft

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	62.00 ft

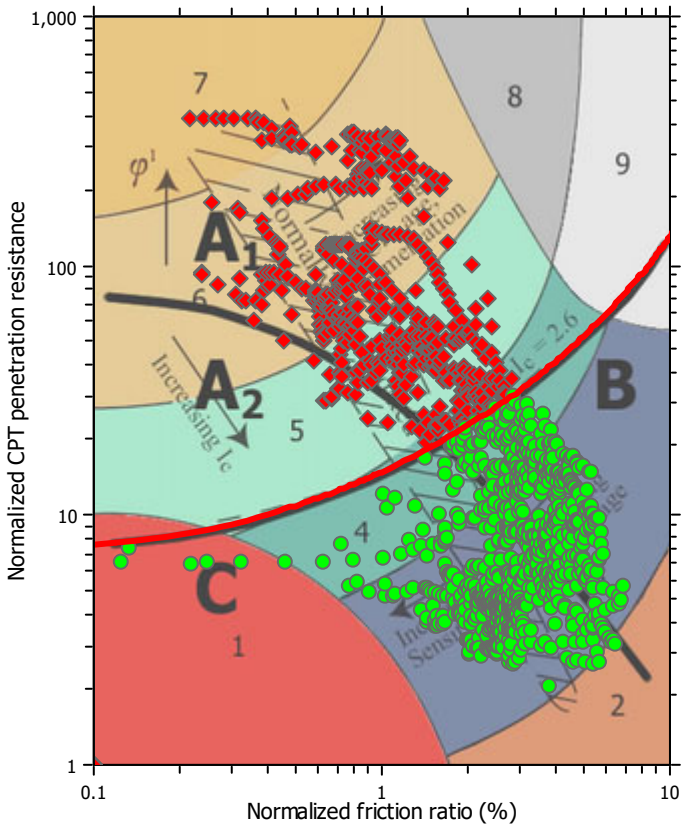
F.S. color scheme

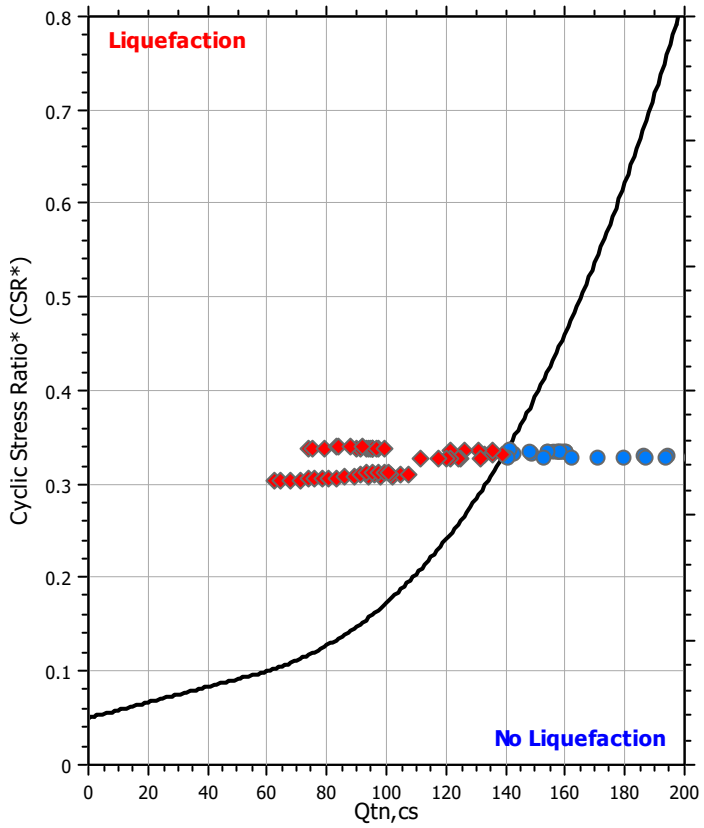
- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

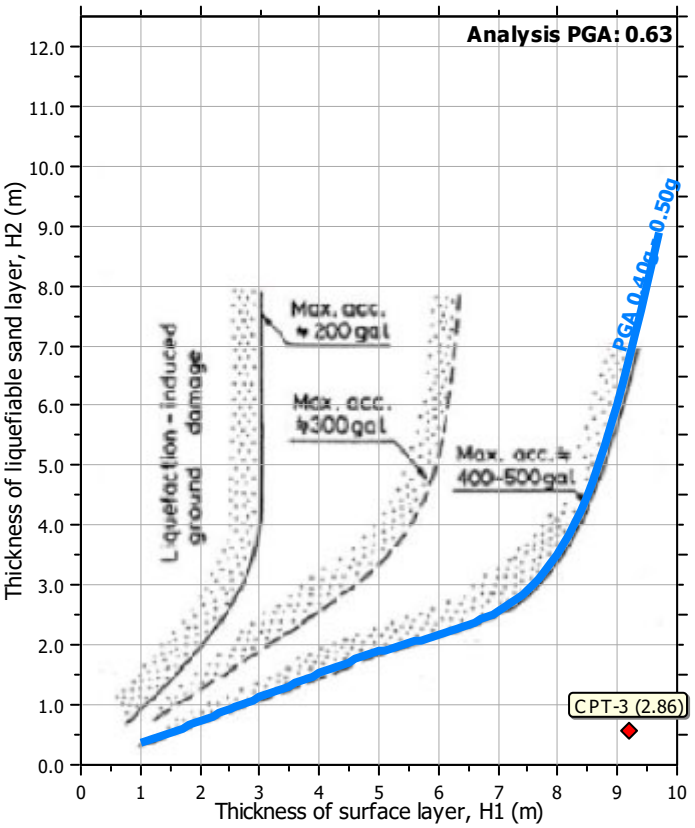
LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis summary plots



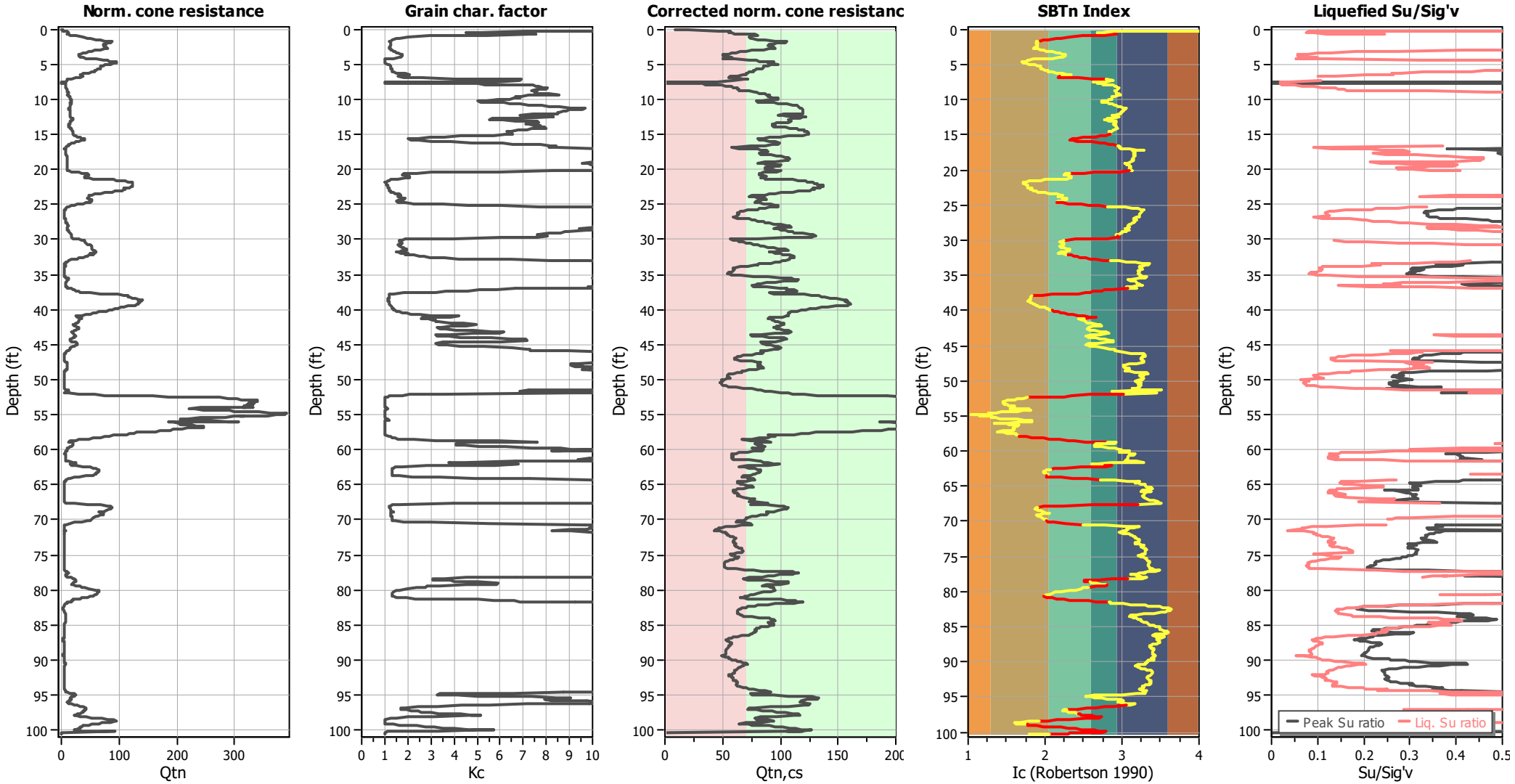




Input parameters and analysis data

Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	62.00 ft

Check for strength loss plots (Robertson (2010))



Input parameters and analysis data

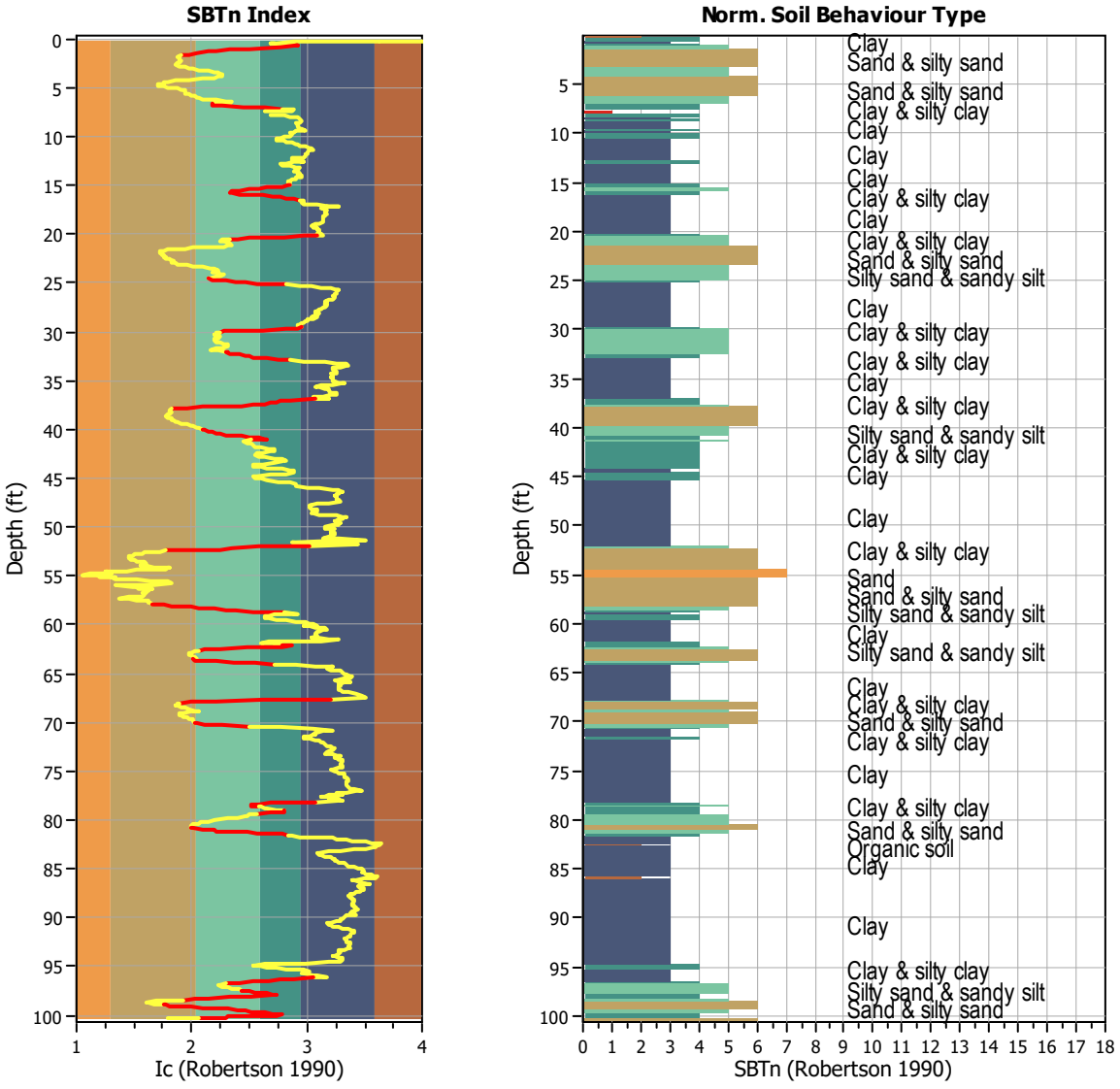
Analysis method:	NCEER (1998)	Depth to water table (erthq.):	30.00 ft	Fill weight:	N/A
Fines correction method:	NCEER (1998)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.65	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.63	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	54.00 ft	Fill height:	N/A	Limit depth:	62.00 ft

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between 1.80 < I_c < 3.0) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties

I_c minimum check value:	1.70
I_c maximum check value:	3.00
I_c change ratio value:	0.0250
Minimum number of points in layer:	4

General statistics

Total points in CPT file:	1376
Total points excluded:	224
Exclusion percentage:	16.28%
Number of layers detected:	26

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	12	Start depth: 0.72 (ft)	3	Clay
		End depth: 1.74 (ft)	6	Sand & silty sand
Transition layer 2	6	Start depth: 6.76 (ft)	5	Silty sand & sandy silt
		End depth: 7.19 (ft)	4	Clay & silty clay
Transition layer 3	9	Start depth: 14.99 (ft)	3	Clay
		End depth: 15.67 (ft)	5	Silty sand & sandy silt
Transition layer 4	11	Start depth: 15.76 (ft)	5	Silty sand & sandy silt
		End depth: 16.58 (ft)	3	Clay
Transition layer 5	7	Start depth: 20.21 (ft)	3	Clay
		End depth: 20.60 (ft)	5	Silty sand & sandy silt
Transition layer 6	9	Start depth: 24.64 (ft)	5	Silty sand & sandy silt
		End depth: 25.27 (ft)	3	Clay
Transition layer 7	8	Start depth: 29.55 (ft)	3	Clay
		End depth: 30.13 (ft)	5	Silty sand & sandy silt
Transition layer 8	12	Start depth: 32.12 (ft)	5	Silty sand & sandy silt
		End depth: 32.98 (ft)	3	Clay
Transition layer 9	15	Start depth: 36.97 (ft)	3	Clay
		End depth: 37.97 (ft)	6	Sand & silty sand
Transition layer 10	12	Start depth: 40.09 (ft)	5	Silty sand & sandy silt
		End depth: 40.97 (ft)	4	Clay & silty clay
Transition layer 11	4	Start depth: 40.97 (ft)	4	Clay & silty clay
		End depth: 41.15 (ft)	5	Silty sand & sandy silt
Transition layer 12	8	Start depth: 52.01 (ft)	4	Clay & silty clay
		End depth: 52.45 (ft)	6	Sand & silty sand
Transition layer 13	14	Start depth: 57.92 (ft)	6	Sand & silty sand
		End depth: 58.84 (ft)	3	Clay
Transition layer 14	7	Start depth: 62.10 (ft)	3	Clay
		End depth: 62.74 (ft)	6	Sand & silty sand
Transition layer 15	7	Start depth: 63.61 (ft)	6	Sand & silty sand
		End depth: 64.15 (ft)	3	Clay
Transition layer 16	5	Start depth: 67.68 (ft)	4	Clay & silty clay
		End depth: 68.07 (ft)	6	Sand & silty sand
Transition layer 17	5	Start depth: 70.08 (ft)	6	Sand & silty sand
		End depth: 70.54 (ft)	4	Clay & silty clay
Transition layer 18	4	Start depth: 78.24 (ft)	4	Clay & silty clay
		End depth: 78.47 (ft)	5	Silty sand & sandy silt
Transition layer 19	4	Start depth: 78.53 (ft)	5	Silty sand & sandy silt
		End depth: 78.69 (ft)	4	Clay & silty clay
Transition layer 20	4	Start depth: 79.16 (ft)	4	Clay & silty clay
		End depth: 79.45 (ft)	5	Silty sand & sandy silt
Transition layer 21	15	Start depth: 80.83 (ft)	6	Sand & silty sand
		End depth: 81.56 (ft)	3	Clay
Transition layer 22	7	Start depth: 96.30 (ft)	3	Clay
		End depth: 96.87 (ft)	5	Silty sand & sandy silt
Transition layer 23	8	Start depth: 97.45 (ft)	5	Silty sand & sandy silt
		End depth: 97.88 (ft)	4	Clay & silty clay

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 24	8	Start depth: 97.88 (ft)	4	Clay & silty clay
		End depth: 98.47 (ft)	6	Sand & silty sand
Transition layer 25	14	Start depth: 98.98 (ft)	6	Sand & silty sand
		End depth: 99.95 (ft)	3	Clay
Transition layer 26	9	Start depth: 99.95 (ft)	3	Clay
		End depth: 100.28 (ft)	6	Sand & silty sand

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1	0.04	0.10	0.03	0.00	100.00	87.36
2	0.10	0.10	0.04	0.00	100.00	87.36
3	0.11	0.20	0.05	0.00	100.00	87.36
4	0.16	0.40	0.05	0.00	100.00	87.36
5	0.19	1.01	0.05	0.00	100.00	88.74
6	0.24	2.43	0.05	0.00	71.90	91.34
7	0.31	5.06	0.06	0.00	51.48	93.80
8	0.38	7.29	0.07	0.00	42.56	95.48
9	0.43	7.69	0.08	0.00	39.63	96.43
10	0.49	7.69	0.08	0.00	41.35	96.84
11	0.58	6.58	0.09	0.00	44.64	97.26
12	0.63	6.17	0.10	0.00	49.07	97.85
13	0.67	5.97	0.11	0.00	51.93	98.72
14	0.72	6.02	0.13	0.00	53.54	99.42
15	0.72	6.07	0.13	0.00	52.47	101.17
16	0.84	8.00	0.20	0.00	44.02	103.62
17	0.96	13.76	0.25	0.00	30.61	106.61
18	1.06	25.71	0.28	0.10	23.44	108.76
19	1.24	28.44	0.33	0.10	19.50	109.81
20	1.30	29.76	0.31	0.10	17.10	110.05
21	1.48	36.23	0.28	0.10	14.00	110.41
22	1.59	45.85	0.33	0.10	12.36	111.13
23	1.69	44.33	0.37	0.10	11.12	112.10
24	1.69	52.02	0.37	0.10	10.74	112.65
25	1.74	53.04	0.39	0.10	9.92	112.99
26	1.79	54.66	0.40	0.10	9.87	113.14
27	1.84	53.64	0.39	0.10	10.04	113.01
28	1.88	50.40	0.38	0.10	10.26	112.64
29	1.93	49.70	0.35	0.10	10.40	112.09
30	1.99	48.28	0.32	0.10	10.27	111.60
31	2.03	48.08	0.31	0.10	10.19	111.23
32	2.08	47.87	0.31	0.10	10.14	110.98
33	2.13	47.06	0.29	0.10	10.28	110.80
34	2.22	45.65	0.30	0.10	10.49	110.61
35	2.27	44.84	0.29	0.10	10.68	110.44
36	2.33	44.43	0.28	0.10	10.61	110.26
37	2.42	45.04	0.28	0.10	10.34	110.23
38	2.48	46.86	0.28	0.10	9.95	110.30
39	2.56	48.28	0.28	0.10	9.56	110.53
40	2.65	50.10	0.29	0.10	9.36	110.70
41	2.72	49.90	0.29	0.10	9.62	110.74
42	2.80	46.15	0.29	0.10	10.31	110.44
43	2.89	42.00	0.28	0.10	11.29	109.97
44	2.94	39.17	0.26	0.10	12.40	109.53
45	3.04	35.93	0.26	0.10	13.48	109.00
46	3.14	32.59	0.24	0.10	14.78	108.19
47	3.23	28.44	0.21	0.10	15.91	107.05
48	3.31	26.01	0.18	0.10	17.31	105.88

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
49	3.37	22.77	0.17	0.10	18.64	104.75
50	3.48	20.34	0.15	0.10	20.16	103.47
51	3.57	18.02	0.12	0.10	20.83	102.23
52	3.65	18.02	0.11	0.10	20.99	101.38
53	3.71	18.02	0.11	0.10	20.91	101.29
54	3.82	18.02	0.11	0.10	20.93	102.11
55	3.91	19.84	0.15	0.10	20.16	103.21
56	4.00	22.67	0.16	0.10	18.85	104.71
57	4.10	25.91	0.19	0.10	15.53	104.42
58	4.19	30.57	0.11	0.10	5.00	104.40
59	4.26	37.15	0.13	0.10	5.00	104.51
60	4.35	46.05	0.17	0.10	5.00	106.46
61	4.44	53.64	0.20	0.19	5.00	107.75
62	4.52	49.70	0.21	0.19	5.00	108.36
63	4.53	50.81	0.21	0.19	5.00	108.59
64	4.58	56.27	0.21	0.19	5.00	108.81
65	4.63	58.00	0.22	0.19	5.00	109.16
66	4.68	59.01	0.23	0.19	5.00	109.49
67	4.72	59.51	0.24	0.19	5.00	109.83
68	4.77	59.31	0.25	0.19	5.00	110.07
69	4.82	58.40	0.26	0.19	5.00	110.22
70	4.88	56.48	0.26	0.19	5.00	110.30
71	4.96	53.74	0.27	0.19	7.94	110.33
72	5.01	50.61	0.27	0.19	8.80	110.33
73	5.08	47.27	0.28	0.19	9.75	110.30
74	5.16	44.43	0.28	0.19	10.61	110.22
75	5.21	42.71	0.28	0.19	11.15	110.15
76	5.30	42.66	0.28	0.19	11.35	110.11
77	5.37	42.66	0.28	0.19	11.37	110.11
78	5.45	42.61	0.28	0.19	11.35	110.10
79	5.52	42.81	0.28	0.19	11.43	110.08
80	5.59	41.90	0.28	0.19	11.67	109.99
81	5.65	40.38	0.27	0.19	12.17	109.79
82	5.74	38.16	0.27	0.19	12.78	109.59
83	5.83	36.84	0.27	0.19	13.36	109.47
84	5.89	36.23	0.27	0.29	13.78	109.49
85	5.97	35.83	0.27	0.29	14.10	109.46
86	6.07	34.92	0.27	0.29	14.65	109.36
87	6.12	32.79	0.27	0.29	15.67	109.20
88	6.22	29.96	0.27	0.29	17.39	109.00
89	6.28	26.52	0.27	0.29	19.71	108.75
90	6.36	23.18	0.27	0.29	22.24	108.30
91	6.46	20.65	0.26	0.29	24.09	107.75
92	6.52	20.04	0.24	0.29	23.83	106.97
93	6.60	21.46	0.20	0.29	21.15	106.06
94	6.70	24.70	0.16	0.29	18.41	104.86
95	6.76	24.49	0.14	0.29	18.15	104.05
96	6.84	19.84	0.15	0.29	21.31	103.55

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
97	6.94	14.57	0.15	0.29	28.13	103.13
98	7.03	10.32	0.15	0.29	36.85	102.17
99	7.13	7.69	0.14	0.29	45.33	101.02
100	7.19	6.68	0.13	0.29	50.80	99.02
101	7.32	5.47	0.08	0.29	50.53	95.58
102	7.42	5.16	0.02	0.29	46.05	89.63
103	7.49	4.86	0.01	0.29	36.85	87.36
104	7.57	4.76	-0.01	0.29	N/A	87.36
105	7.66	4.55	0.00	0.29	N/A	87.36
106	7.76	4.35	0.01	0.29	39.30	87.36
107	7.77	4.40	0.01	0.29	41.66	87.36
108	7.78	4.40	0.01	0.29	42.16	87.36
109	7.82	4.45	0.01	0.29	43.69	87.36
110	7.87	4.45	0.02	0.29	46.05	87.36
111	7.92	4.45	0.03	0.29	48.69	87.36
112	7.97	4.45	0.03	0.29	50.96	88.91
113	8.01	4.55	0.04	0.29	52.87	90.83
114	8.06	4.76	0.05	0.29	53.56	92.24
115	8.11	4.96	0.06	0.29	53.89	93.35
116	8.20	5.06	0.06	0.29	54.02	94.10
117	8.26	5.16	0.07	0.29	54.67	94.95
118	8.35	5.26	0.08	0.29	55.25	95.57
119	8.40	5.26	0.08	0.38	55.42	95.96
120	8.49	5.36	0.08	0.38	55.15	96.13
121	8.54	5.47	0.08	0.38	54.56	96.42
122	8.64	5.67	0.09	0.38	53.58	96.77
123	8.69	5.97	0.09	0.38	52.70	97.12
124	8.79	6.07	0.09	0.38	53.07	98.37
125	8.84	6.48	0.14	0.38	53.64	99.77
126	8.93	6.88	0.15	0.38	53.23	100.93
127	9.03	7.29	0.15	0.38	53.10	101.61
128	9.08	7.19	0.17	0.38	53.34	101.99
129	9.11	7.14	0.18	0.38	54.44	102.35
130	9.12	7.14	0.18	0.38	54.87	102.44
131	9.17	7.08	0.18	0.38	55.46	102.54
132	9.22	6.98	0.19	0.38	55.68	102.79
133	9.31	7.29	0.19	0.38	57.60	103.02
134	9.36	6.48	0.20	0.38	56.84	103.40
135	9.40	7.69	0.21	0.38	55.49	103.68
136	9.46	8.20	0.21	0.38	52.20	104.01
137	9.51	8.50	0.21	0.38	50.78	104.20
138	9.55	8.70	0.22	0.48	49.80	104.47
139	9.61	9.11	0.23	0.48	49.60	104.86
140	9.69	9.11	0.24	0.48	49.93	105.32
141	9.74	9.11	0.26	0.38	50.53	105.75
142	9.81	9.31	0.27	0.48	50.47	106.17
143	9.89	9.72	0.28	0.38	49.47	106.49
144	9.94	10.22	0.29	0.48	48.57	106.69

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
145	10.03	10.22	0.28	0.48	47.95	106.73
146	10.08	10.22	0.28	0.48	46.27	105.91
147	10.18	10.22	0.19	0.48	43.86	104.66
148	10.23	10.22	0.16	0.48	42.16	103.72
149	10.33	10.22	0.21	0.48	42.78	104.06
150	10.40	10.22	0.22	0.48	44.53	104.99
151	10.47	10.22	0.24	0.48	46.24	105.54
152	10.51	9.77	0.26	0.48	47.48	106.12
153	10.56	10.17	0.28	0.48	48.53	106.55
154	10.61	10.12	0.29	0.48	48.96	107.12
155	10.67	10.32	0.32	0.48	50.59	107.76
156	10.75	10.02	0.37	0.48	52.01	108.32
157	10.80	10.02	0.37	0.48	53.26	108.59
158	10.85	9.92	0.37	0.48	53.79	108.61
159	10.90	9.72	0.37	0.57	54.58	108.60
160	11.00	9.51	0.38	0.57	55.86	108.56
161	11.05	9.11	0.37	0.57	57.54	108.36
162	11.14	8.50	0.36	0.57	59.49	108.14
163	11.21	8.20	0.36	0.57	61.41	108.08
164	11.29	8.10	0.38	0.57	61.90	108.18
165	11.38	8.40	0.37	0.57	61.40	108.38
166	11.46	8.70	0.39	0.57	60.04	108.48
167	11.52	8.91	0.38	0.57	59.20	108.60
168	11.60	9.01	0.38	0.57	58.74	108.64
169	11.67	9.01	0.39	0.57	58.51	108.69
170	11.72	9.11	0.39	0.57	58.33	108.76
171	11.81	9.21	0.39	0.57	57.50	108.86
172	11.86	9.62	0.39	0.57	57.42	108.90
173	11.96	9.21	0.39	0.57	57.28	108.93
174	12.01	9.41	0.40	0.57	57.36	108.99
175	12.10	9.72	0.40	0.57	56.33	108.48
176	12.16	9.92	0.30	0.57	52.86	107.67
177	12.24	10.53	0.27	0.67	50.46	107.26
178	12.32	10.93	0.34	0.67	50.49	108.00
179	12.39	11.13	0.39	0.67	51.82	109.13
180	12.48	11.44	0.42	0.67	55.21	109.56
181	12.50	9.31	0.43	0.67	56.54	109.82
182	12.54	9.92	0.45	0.67	56.14	110.10
183	12.64	12.95	0.45	0.67	51.14	110.63
184	12.68	14.17	0.46	0.67	46.74	111.06
185	12.77	14.98	0.47	0.67	45.02	111.08
186	12.82	14.98	0.44	0.67	44.58	110.87
187	12.89	14.27	0.42	0.67	45.32	110.45
188	12.97	13.36	0.41	0.67	47.27	110.13
189	13.03	12.45	0.41	0.67	49.63	109.86
190	13.12	11.64	0.40	0.67	52.08	109.64
191	13.16	11.03	0.40	0.67	53.60	109.40
192	13.26	10.93	0.39	0.67	54.00	108.95

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
193	13.34	10.73	0.34	0.67	53.03	108.33
194	13.41	10.83	0.31	0.67	51.87	107.54
195	13.50	10.63	0.28	0.67	51.53	107.03
196	13.60	10.32	0.28	0.67	52.24	106.75
197	13.65	10.02	0.28	0.67	53.22	106.76
198	13.75	10.02	0.29	0.67	54.12	106.90
199	13.80	10.02	0.30	0.67	53.54	106.72
200	13.89	10.22	0.26	0.67	53.46	106.90
201	13.94	10.42	0.31	0.76	53.08	107.50
202	14.03	11.23	0.37	0.76	54.97	108.63
203	14.11	10.73	0.41	0.76	55.24	109.48
204	14.13	11.69	0.42	0.76	55.28	110.03
205	14.18	12.15	0.45	0.76	53.47	110.47
206	14.22	12.95	0.46	0.76	52.62	110.95
207	14.28	13.36	0.49	0.76	51.87	111.50
208	14.37	13.97	0.53	0.76	51.36	112.04
209	14.44	14.68	0.56	0.76	50.25	112.56
210	14.51	15.69	0.58	0.76	48.93	112.99
211	14.60	16.50	0.60	0.76	48.02	113.34
212	14.65	16.70	0.62	0.76	47.94	113.59
213	14.75	16.50	0.63	0.76	48.44	113.74
214	14.85	16.45	0.64	0.76	48.93	113.80
215	14.91	16.45	0.63	0.76	49.08	113.80
216	14.99	16.40	0.63	0.76	47.80	113.81
217	15.09	18.12	0.62	0.76	45.25	113.98
218	15.18	20.34	0.63	0.76	41.64	114.15
219	15.25	22.37	0.61	0.76	38.13	114.10
220	15.33	24.09	0.55	0.76	34.47	113.87
221	15.43	27.02	0.52	0.76	30.57	113.72
222	15.51	31.38	0.52	0.76	26.98	113.86
223	15.59	35.53	0.52	0.76	24.54	114.07
224	15.67	36.94	0.52	0.76	23.56	114.17
225	15.76	36.03	0.51	0.86	24.48	114.23
226	15.86	32.39	0.54	0.76	26.98	114.13
227	15.95	27.63	0.54	0.76	31.02	113.82
228	16.05	22.87	0.53	0.76	35.88	113.11
229	16.14	18.72	0.48	0.76	40.89	112.24
230	16.20	16.30	0.45	0.76	44.59	111.36
231	16.28	15.49	0.42	0.76	47.26	110.71
232	16.34	14.17	0.41	0.76	49.02	109.97
233	16.44	12.95	0.36	0.76	51.62	109.16
234	16.50	11.64	0.33	0.86	54.21	108.05
235	16.58	10.22	0.29	0.76	56.10	106.16
236	16.73	8.60	0.17	0.86	57.07	103.07
237	16.82	7.39	0.09	0.76	55.90	98.94
238	16.92	6.78	0.07	0.86	56.73	97.37
239	17.01	6.98	0.12	0.86	64.41	99.23
240	17.11	5.87	0.17	0.86	72.33	101.23

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
241	17.12	5.72	0.19	0.86	79.64	102.14
242	17.14	5.57	0.19	0.86	75.40	102.95
243	17.19	7.69	0.22	0.86	70.99	103.97
244	17.28	8.10	0.25	0.86	67.48	104.99
245	17.33	8.00	0.26	0.86	68.61	105.59
246	17.43	7.89	0.28	0.86	70.20	105.75
247	17.47	7.69	0.27	0.86	70.55	105.46
248	17.57	7.59	0.24	0.86	70.29	104.78
249	17.65	7.39	0.21	0.86	69.39	104.05
250	17.72	7.39	0.21	0.86	69.90	104.00
251	17.81	7.39	0.23	0.86	69.98	104.48
252	17.86	7.89	0.25	0.86	70.40	105.52
253	17.95	8.30	0.30	0.86	70.27	106.61
254	18.05	8.70	0.35	0.86	69.77	107.59
255	18.10	9.31	0.36	0.86	69.28	108.43
256	18.20	9.62	0.41	0.86	68.75	109.17
257	18.30	10.02	0.44	0.86	69.06	109.74
258	18.39	10.02	0.45	0.86	68.69	110.03
259	18.48	10.32	0.45	0.86	68.26	110.09
260	18.58	10.42	0.45	0.86	68.26	110.10
261	18.66	10.12	0.45	0.86	68.67	110.00
262	18.74	10.02	0.43	0.86	68.65	109.66
263	18.87	10.02	0.39	0.86	65.89	108.15
264	18.97	9.62	0.22	0.86	63.51	106.58
265	19.06	9.31	0.24	0.96	61.57	105.45
266	19.16	9.72	0.27	0.86	62.59	106.45
267	19.25	10.42	0.32	0.96	62.93	107.21
268	19.27	10.22	0.32	0.86	63.88	107.82
269	19.30	10.02	0.35	0.96	64.63	108.39
270	19.34	10.83	0.39	0.96	65.30	109.05
271	19.39	10.83	0.41	0.96	65.04	109.46
272	19.49	10.83	0.41	0.96	65.33	109.38
273	19.55	10.63	0.38	0.96	65.79	108.98
274	19.63	10.02	0.36	0.96	66.38	108.45
275	19.68	9.82	0.34	0.96	66.57	107.82
276	19.74	9.72	0.30	0.96	65.75	107.23
277	19.83	9.72	0.28	0.96	65.45	106.97
278	19.87	9.72	0.31	0.96	65.22	106.85
279	19.94	9.72	0.29	0.96	66.15	107.18
280	20.02	9.72	0.33	0.96	67.03	107.64
281	20.07	9.92	0.36	0.96	67.92	108.78
282	20.17	10.83	0.44	0.96	64.62	109.94
283	20.21	13.46	0.47	0.96	56.54	111.19
284	20.28	18.22	0.50	0.96	46.28	112.30
285	20.36	24.49	0.52	1.05	37.36	113.43
286	20.41	31.88	0.56	1.05	30.98	114.57
287	20.48	38.76	0.62	1.05	26.57	115.62
288	20.55	45.24	0.66	1.05	23.46	116.43

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
289	20.60	50.91	0.67	1.05	21.46	116.95
290	20.70	53.44	0.69	1.05	20.55	117.24
291	20.74	53.24	0.71	1.05	20.71	117.40
292	20.79	51.32	0.72	1.05	21.66	117.54
293	20.89	48.89	0.76	1.05	23.50	117.89
294	20.96	45.85	0.85	0.96	23.80	117.32
295	21.04	45.80	0.57	0.96	24.10	117.07
296	21.13	45.80	0.70	0.96	23.70	116.74
297	21.22	45.75	0.76	0.96	23.00	117.62
298	21.29	56.07	0.78	1.05	21.86	118.10
299	21.35	56.27	0.79	1.05	18.50	118.64
300	21.37	73.99	0.80	1.05	15.90	119.09
301	21.42	83.80	0.82	1.05	13.13	119.55
302	21.47	93.32	0.82	1.05	11.52	119.85
303	21.48	101.01	0.82	1.05	10.27	120.06
304	21.52	107.59	0.82	1.05	9.34	120.20
305	21.57	113.46	0.81	1.05	8.57	120.29
306	21.62	118.62	0.80	1.05	7.91	120.35
307	21.66	124.29	0.80	1.05	7.35	120.43
308	21.71	129.05	0.81	1.15	6.92	120.56
309	21.76	132.99	0.82	1.15	6.65	120.75
310	21.81	135.83	0.84	1.15	6.55	120.99
311	21.85	137.14	0.87	1.15	6.57	121.25
312	21.91	137.95	0.90	1.15	6.66	121.49
313	21.95	138.26	0.92	1.15	6.78	121.69
314	22.00	138.06	0.94	1.15	6.89	121.84
315	22.05	138.36	0.96	1.15	6.99	121.96
316	22.10	138.06	0.97	1.15	7.07	122.06
317	22.15	138.26	0.98	1.15	7.14	122.15
318	22.19	138.56	0.99	1.15	7.18	122.24
319	22.24	139.17	1.00	1.15	7.38	122.59
320	22.29	139.98	1.12	1.15	7.48	122.79
321	22.34	140.38	1.07	1.15	7.53	122.89
322	22.39	140.18	1.04	1.15	7.42	122.71
323	22.43	139.57	1.04	1.15	7.44	122.63
324	22.48	138.46	1.05	1.15	7.57	122.64
325	22.55	136.94	1.06	1.15	7.77	122.66
326	22.62	134.92	1.06	1.15	8.48	122.57
327	22.63	118.32	1.06	1.24	8.67	122.48
328	22.72	130.57	1.04	1.24	8.87	122.34
329	22.77	127.73	1.02	1.24	8.53	122.30
330	22.83	125.91	1.02	1.24	8.81	122.33
331	22.91	124.70	1.06	1.24	9.13	122.40
332	22.96	121.96	1.07	1.24	9.51	122.45
333	23.02	118.52	1.06	1.24	9.95	122.36
334	23.10	114.07	1.06	1.24	10.51	122.24
335	23.16	108.91	1.05	1.24	11.23	122.08
336	23.20	102.23	1.04	1.24	12.12	121.86

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
337	23.26	95.44	1.03	1.24	13.14	121.54
338	23.35	88.66	0.99	1.24	14.37	121.28
339	23.39	81.88	1.01	1.24	15.74	120.92
340	23.48	74.39	0.96	1.24	17.51	120.69
341	23.54	67.71	0.98	1.24	19.01	120.18
342	23.63	62.85	0.89	1.24	19.95	119.45
343	23.69	59.72	0.76	1.24	19.23	117.77
344	23.78	57.59	0.48	1.24	18.61	116.63
345	23.87	57.74	0.60	1.24	18.21	116.01
346	23.88	57.74	0.61	1.24	19.03	116.77
347	23.93	57.89	0.67	1.34	19.95	117.38
348	24.02	56.58	0.77	1.34	20.80	117.95
349	24.04	57.13	0.78	1.34	21.46	118.37
350	24.05	57.13	0.80	1.34	21.78	118.73
351	24.15	57.69	0.89	1.34	21.95	119.14
352	24.20	59.92	0.91	1.34	21.72	119.56
353	24.30	62.65	0.93	1.34	20.63	119.52
354	24.40	65.28	0.83	1.34	19.19	119.11
355	24.46	67.21	0.74	1.34	17.84	118.42
356	24.54	67.21	0.69	1.34	17.34	117.92
357	24.64	64.78	0.69	1.34	18.05	117.78
358	24.73	60.22	0.72	1.34	19.84	117.90
359	24.78	54.76	0.77	1.34	22.46	118.05
360	24.88	48.89	0.80	1.34	25.68	117.95
361	24.94	42.00	0.78	1.24	29.51	117.49
362	25.02	34.82	0.73	1.24	34.04	116.54
363	25.12	28.14	0.65	1.24	39.88	115.47
364	25.17	22.27	0.62	1.24	46.77	114.38
365	25.27	18.12	0.59	1.24	54.06	113.10
366	25.36	14.78	0.46	1.24	61.30	111.68
367	25.43	12.45	0.42	1.24	67.46	110.12
368	25.50	10.53	0.38	1.24	73.11	108.95
369	25.60	9.62	0.33	1.24	77.33	107.97
370	25.64	9.11	0.32	1.24	78.94	107.28
371	25.67	9.01	0.30	1.15	79.14	106.81
372	25.71	9.01	0.28	1.15	78.50	105.99
373	25.79	8.50	0.23	1.15	78.06	104.81
374	25.93	8.00	0.19	1.15	77.81	103.60
375	26.03	8.00	0.18	1.15	77.15	102.74
376	26.13	8.00	0.16	1.15	76.38	102.36
377	26.24	8.00	0.16	1.15	75.73	102.24
378	26.37	8.20	0.17	1.15	75.53	102.41
379	26.47	8.30	0.17	1.15	75.71	102.64
380	26.60	8.20	0.18	1.15	74.72	102.14
381	26.71	8.20	0.14	1.15	72.50	101.53
382	26.85	8.70	0.13	1.15	69.69	101.34
383	26.95	9.31	0.16	1.15	71.29	102.63
384	27.04	8.81	0.22	1.15	71.21	104.34

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
385	27.09	10.63	0.25	1.05	71.61	105.86
386	27.19	10.93	0.29	1.05	69.63	106.85
387	27.23	11.23	0.30	1.05	70.05	107.52
388	27.33	11.34	0.32	1.05	70.38	108.10
389	27.40	11.64	0.36	1.05	70.26	108.70
390	27.47	12.25	0.38	1.05	69.48	109.39
391	27.57	12.95	0.41	1.05	68.12	110.02
392	27.66	13.66	0.44	1.05	66.86	110.95
393	27.77	14.88	0.52	1.05	65.56	112.10
394	27.86	16.30	0.60	1.05	64.27	113.38
395	27.96	17.61	0.69	1.05	63.40	114.40
396	28.06	18.22	0.74	1.05	64.03	115.00
397	28.15	17.31	0.77	1.05	65.56	115.03
398	28.25	16.30	0.72	1.05	64.37	114.22
399	28.34	17.46	0.52	1.05	63.64	113.20
400	28.44	15.69	0.53	1.05	61.14	112.70
401	28.54	17.61	0.59	1.05	64.86	113.09
402	28.62	14.98	0.63	1.05	62.81	113.97
403	28.71	19.74	0.70	1.05	62.14	114.69
404	28.77	20.24	0.75	1.05	59.04	115.50
405	28.86	20.75	0.80	1.05	59.06	115.95
406	28.91	21.15	0.82	1.05	58.48	116.29
407	28.97	22.06	0.84	1.05	57.87	116.68
408	29.04	22.87	0.91	1.05	57.17	117.16
409	29.10	23.78	0.96	1.05	56.38	117.71
410	29.15	25.20	1.01	1.05	55.66	118.36
411	29.25	26.42	1.13	1.05	54.03	119.02
412	29.34	27.53	1.19	1.05	53.66	119.56
413	29.38	28.14	1.22	1.05	53.77	119.85
414	29.48	27.53	1.26	1.05	55.21	119.97
415	29.55	27.43	1.26	1.05	55.61	119.94
416	29.63	27.43	1.21	1.05	53.71	119.51
417	29.72	27.33	1.04	1.05	46.70	117.24
418	29.82	30.47	0.29	1.15	36.62	114.29
419	29.88	36.84	0.31	1.15	26.07	110.63
420	29.96	43.12	0.35	1.15	21.97	111.98
421	30.06	55.67	0.40	1.15	20.66	113.06
422	30.13	50.91	0.44	1.05	19.28	113.85
423	30.18	57.39	0.44	1.05	19.21	114.32
424	30.28	59.72	0.48	1.05	18.92	115.08
425	30.37	59.01	0.56	1.05	19.74	116.07
426	30.47	59.82	0.65	1.05	20.55	117.07
427	30.57	62.65	0.72	1.05	20.45	117.89
428	30.66	67.31	0.76	1.05	19.78	118.59
429	30.74	71.76	0.82	1.05	19.08	119.20
430	30.82	74.90	0.87	1.05	18.72	119.77
431	30.90	76.82	0.92	1.15	18.90	120.37
432	31.01	77.12	1.02	1.15	19.54	121.00

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
433	31.10	76.72	1.12	1.15	20.53	121.75
434	31.19	77.18	1.25	1.15	21.62	122.52
435	31.28	77.23	1.39	1.15	22.44	123.19
436	31.35	78.24	1.47	1.15	22.96	123.75
437	31.43	80.06	1.56	1.15	23.03	124.24
438	31.53	83.20	1.66	1.15	22.94	124.75
439	31.60	86.03	1.75	1.15	21.03	124.07
440	31.67	88.46	1.07	1.15	19.28	123.27
441	31.77	89.68	1.16	1.15	17.72	122.34
442	31.84	90.18	1.26	1.15	18.27	122.84
443	31.91	89.68	1.32	1.15	19.80	123.18
444	31.98	78.64	1.39	1.15	22.19	123.23
445	31.98	68.93	1.40	1.15	23.12	123.39
446	32.04	84.01	1.44	1.24	23.03	123.69
447	32.12	83.20	1.54	1.24	22.36	124.14
448	32.16	80.77	1.60	1.24	23.73	124.42
449	32.27	76.11	1.67	1.24	25.51	124.47
450	32.33	70.04	1.66	1.24	27.40	124.34
451	32.41	66.09	1.63	1.24	28.95	124.00
452	32.50	62.75	1.55	1.24	30.35	123.44
453	32.58	56.48	1.41	1.24	31.97	122.68
454	32.66	50.71	1.29	1.24	34.45	121.67
455	32.74	43.42	1.16	1.24	37.91	120.54
456	32.84	35.73	1.02	1.24	42.91	119.34
457	32.90	29.15	0.95	1.24	48.72	118.12
458	32.98	24.70	0.85	1.24	56.09	116.92
459	33.08	20.85	0.75	1.24	62.41	115.68
460	33.14	16.70	0.69	1.24	70.22	114.44
461	33.22	13.56	0.63	1.24	78.27	113.16
462	33.32	12.04	0.53	1.24	84.25	111.85
463	33.37	10.93	0.46	1.24	85.46	110.42
464	33.47	10.83	0.38	1.24	84.74	109.62
465	33.56	11.34	0.39	1.24	80.65	109.42
466	33.63	12.75	0.41	1.24	77.37	109.72
467	33.71	13.16	0.40	1.24	75.48	109.42
468	33.81	12.04	0.34	1.24	74.83	107.78
469	33.90	10.73	0.19	1.24	75.10	105.75
470	33.95	10.32	0.19	1.24	75.13	103.88
471	34.04	9.82	0.19	1.24	76.22	103.67
472	34.14	10.02	0.18	1.34	77.27	103.52
473	34.17	9.72	0.19	1.24	77.76	103.53
474	34.20	9.62	0.19	1.24	76.51	103.73
475	34.26	10.83	0.19	1.24	75.12	103.91
476	34.35	10.63	0.19	1.24	73.88	103.93
477	34.43	10.32	0.19	1.24	74.71	103.73
478	34.49	10.22	0.18	1.24	74.86	103.40
479	34.59	10.22	0.17	1.24	74.51	102.92
480	34.69	10.02	0.15	1.24	74.15	102.43

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
481	34.73	9.92	0.15	1.24	74.31	102.00
482	34.83	9.72	0.15	1.24	74.57	101.78
483	34.90	9.72	0.14	1.24	75.16	101.82
484	34.98	9.72	0.15	1.24	75.52	102.24
485	35.07	10.02	0.17	1.24	76.19	103.35
486	35.16	10.63	0.21	1.24	78.83	105.56
487	35.26	11.03	0.33	1.24	83.16	108.85
488	35.33	12.15	0.55	1.24	81.79	112.16
489	35.40	16.50	0.76	1.34	74.84	114.98
490	35.50	21.56	0.92	1.34	67.00	116.75
491	35.57	24.39	0.97	1.34	63.27	117.70
492	35.65	24.09	1.01	1.34	63.57	118.14
493	35.71	22.77	1.08	1.34	66.27	118.34
494	35.79	21.66	1.09	1.34	69.18	118.25
495	35.85	20.45	1.03	1.34	71.21	117.70
496	35.94	18.93	0.91	1.34	72.32	116.92
497	35.99	18.42	0.83	1.34	72.47	115.84
498	36.08	17.51	0.69	1.34	72.38	114.36
499	36.17	15.49	0.51	1.34	73.86	112.64
500	36.24	13.56	0.46	1.34	75.60	111.22
501	36.33	13.56	0.44	1.34	77.26	110.71
502	36.42	13.56	0.44	1.34	77.95	110.94
503	36.52	13.56	0.50	1.34	73.49	110.01
504	36.61	14.98	0.26	1.34	67.87	109.88
505	36.70	17.61	0.38	1.34	62.71	110.97
506	36.78	20.55	0.63	1.34	62.56	113.90
507	36.85	22.47	0.80	1.34	71.90	115.26
508	36.87	11.64	0.83	1.34	69.07	116.41
509	36.91	26.42	0.92	1.34	63.50	117.24
510	36.97	31.58	0.97	1.43	49.63	118.44
511	37.06	36.13	1.01	1.43	46.01	119.19
512	37.12	37.96	1.11	1.43	43.96	120.10
513	37.20	41.70	1.28	1.43	42.39	121.21
514	37.27	47.47	1.45	1.43	39.71	122.19
515	37.35	53.44	1.50	1.43	36.91	122.63
516	37.44	55.67	1.40	1.43	34.70	122.58
517	37.49	56.48	1.34	1.43	32.26	122.38
518	37.59	63.06	1.30	1.43	27.80	122.53
519	37.64	81.98	1.30	1.43	21.40	123.10
520	37.70	111.84	1.32	1.53	15.68	123.77
521	37.78	139.98	1.32	1.53	11.92	124.31
522	37.83	157.89	1.32	1.53	9.84	124.68
523	37.92	169.13	1.35	1.53	8.83	124.96
524	37.97	175.50	1.38	1.53	8.44	125.29
525	38.07	179.05	1.45	1.53	8.35	125.63
526	38.14	181.78	1.51	1.53	8.44	126.04
527	38.22	184.61	1.60	1.53	8.51	126.51
528	38.31	190.69	1.72	1.53	8.57	127.15

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
529	38.41	199.80	1.90	1.62	8.22	127.66
530	38.52	213.56	1.89	1.62	7.81	128.17
531	38.64	224.49	2.02	1.62	7.45	128.44
532	38.74	225.00	2.04	1.62	7.89	128.67
533	38.80	204.05	2.10	1.62	8.30	128.80
534	38.89	213.46	2.16	1.82	8.75	128.95
535	38.94	213.66	2.21	1.82	8.74	129.21
536	39.03	213.76	2.31	1.82	9.04	129.51
537	39.13	213.26	2.44	1.82	9.44	129.87
538	39.23	212.65	2.56	1.91	9.96	130.20
539	39.35	208.10	2.67	1.91	10.48	130.39
540	39.42	202.73	2.68	1.91	11.13	130.39
541	39.51	192.20	2.66	1.91	11.86	130.23
542	39.60	181.27	2.62	1.91	12.73	129.97
543	39.70	170.95	2.55	1.91	13.46	129.70
544	39.78	166.19	2.50	1.91	14.13	129.38
545	39.90	156.68	2.40	1.91	14.77	129.07
546	39.99	149.09	2.35	1.91	15.57	128.71
547	40.09	141.29	2.28	1.91	16.39	128.37
548	40.18	133.80	2.21	1.91	17.30	128.04
549	40.23	126.21	2.16	1.91	18.29	127.67
550	40.33	118.02	2.08	1.91	19.50	127.30
551	40.43	109.72	2.03	1.91	20.84	126.92
552	40.52	102.53	1.98	1.91	22.74	126.70
553	40.61	93.22	2.06	1.91	24.63	126.07
554	40.69	81.48	1.71	1.91	27.65	125.27
555	40.80	67.00	1.63	1.91	31.04	124.10
556	40.87	57.39	1.51	1.91	34.44	123.25
557	40.95	55.26	1.38	1.91	37.39	122.50
558	40.97	47.67	1.35	1.91	38.04	122.03
559	41.01	51.11	1.30	2.01	35.69	121.95
560	41.07	64.07	1.26	2.01	31.09	122.03
561	41.15	70.14	1.23	2.01	28.20	122.06
562	41.26	67.91	1.21	1.91	28.17	121.94
563	41.35	63.26	1.21	1.91	29.96	121.73
564	41.47	57.89	1.20	1.91	31.46	121.66
565	41.59	59.61	1.23	1.91	31.96	121.71
566	41.69	61.44	1.24	1.91	31.98	121.95
567	41.78	60.12	1.30	1.91	33.05	122.10
568	41.88	55.87	1.33	1.82	35.75	121.95
569	41.98	48.18	1.27	1.82	39.01	121.52
570	42.08	44.23	1.21	1.82	41.72	120.96
571	42.16	42.91	1.16	1.82	41.89	120.65
572	42.24	45.75	1.14	1.82	39.57	120.77
573	42.31	52.63	1.19	1.91	36.25	121.19
574	42.45	58.30	1.23	1.82	33.81	121.60
575	42.55	59.82	1.24	1.82	32.69	121.82
576	42.60	59.92	1.25	1.82	32.61	121.90

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
577	42.70	59.51	1.27	1.82	33.18	122.03
578	42.81	58.50	1.32	1.72	34.70	122.15
579	42.89	54.05	1.36	1.72	37.37	122.12
580	42.98	48.08	1.34	1.72	41.13	121.83
581	43.08	42.61	1.30	1.72	45.23	121.41
582	43.17	38.66	1.28	1.72	47.51	121.07
583	43.27	39.98	1.25	1.72	46.42	120.88
584	43.37	44.43	1.19	1.72	41.14	119.79
585	43.50	46.96	0.69	1.72	35.96	118.51
586	43.61	48.99	0.69	1.72	32.32	117.19
587	43.74	49.59	0.74	1.62	32.41	117.56
588	43.79	49.29	0.79	1.62	33.54	118.20
589	43.86	48.99	0.89	1.43	35.58	118.96
590	43.94	47.06	1.02	1.34	38.25	119.71
591	44.00	45.04	1.11	1.34	41.55	120.34
592	44.08	42.51	1.22	1.34	44.91	120.67
593	44.17	39.37	1.23	1.34	48.70	120.54
594	44.27	34.61	1.15	1.34	51.70	119.87
595	44.42	32.29	1.00	1.34	51.75	119.10
596	44.52	35.53	0.93	1.34	46.94	118.74
597	44.61	43.42	0.93	1.34	39.36	118.80
598	44.71	53.44	0.86	1.34	33.96	119.33
599	44.85	58.80	0.98	1.34	32.04	120.04
600	44.95	57.69	1.13	1.34	32.93	120.75
601	45.09	55.36	1.15	1.34	35.03	121.01
602	45.19	51.82	1.14	1.34	38.27	120.75
603	45.33	43.02	1.11	1.34	43.45	120.27
604	45.42	35.42	1.09	1.34	49.18	119.55
605	45.57	33.00	0.99	1.34	51.89	118.90
606	45.68	34.11	0.92	1.34	52.37	118.05
607	45.81	30.57	0.81	1.34	52.39	116.56
608	45.92	26.62	0.54	1.34	59.16	115.42
609	46.05	22.37	0.69	1.34	66.42	114.50
610	46.16	17.81	0.67	1.24	75.25	114.63
611	46.17	17.71	0.67	1.24	79.56	114.21
612	46.23	17.61	0.63	1.24	79.66	113.87
613	46.29	17.00	0.59	1.24	80.53	113.32
614	46.34	15.89	0.55	1.24	81.48	112.46
615	46.42	15.18	0.46	1.24	81.87	111.41
616	46.48	14.78	0.40	1.24	80.78	110.31
617	46.52	14.68	0.36	1.24	79.61	109.48
618	46.60	14.57	0.33	1.24	78.79	108.88
619	46.67	14.37	0.32	1.24	78.01	108.41
620	46.74	14.47	0.30	1.24	77.35	108.06
621	46.82	14.47	0.29	1.24	76.73	107.71
622	46.88	14.27	0.28	1.34	77.13	107.41
623	46.96	13.76	0.27	1.34	77.21	107.25
624	47.06	14.22	0.27	1.34	77.78	107.20

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
625	47.15	13.87	0.27	1.34	77.74	107.41
626	47.24	14.17	0.29	1.34	79.57	108.74
627	47.35	15.18	0.43	1.34	80.06	111.84
628	47.49	19.13	0.74	1.34	72.80	113.76
629	47.58	24.70	0.62	1.34	64.43	115.05
630	47.73	28.44	0.64	1.34	60.58	115.11
631	47.83	24.90	0.71	1.34	59.52	115.49
632	47.87	27.78	0.69	1.34	61.47	115.59
633	47.89	25.81	0.69	1.34	59.88	115.52
634	47.94	27.13	0.67	1.34	60.12	115.37
635	48.02	26.92	0.66	1.34	59.63	115.28
636	48.07	26.32	0.66	1.34	60.36	115.24
637	48.12	25.91	0.67	1.34	61.69	115.43
638	48.18	25.61	0.72	1.34	63.36	115.65
639	48.26	24.70	0.74	1.34	64.74	115.83
640	48.31	24.65	0.73	1.34	65.22	115.64
641	48.38	24.39	0.68	1.34	64.33	115.21
642	48.46	24.59	0.62	1.34	62.61	114.59
643	48.52	25.10	0.57	1.34	61.59	113.83
644	48.60	23.48	0.50	1.34	62.06	112.77
645	48.68	20.85	0.41	1.34	65.40	111.58
646	48.74	17.91	0.39	1.34	70.58	110.53
647	48.82	15.79	0.38	1.34	77.29	109.90
648	48.89	14.07	0.36	1.34	82.02	109.37
649	48.99	13.76	0.34	1.34	84.26	108.81
650	49.05	13.56	0.31	1.34	83.16	108.02
651	49.12	13.56	0.26	1.34	81.66	107.12
652	49.18	13.36	0.24	1.34	79.51	106.27
653	49.27	13.66	0.22	1.34	77.50	105.79
654	49.32	14.17	0.21	1.34	75.79	105.36
655	49.42	13.87	0.20	1.43	76.97	105.08
656	49.48	12.55	0.20	1.43	78.75	104.88
657	49.56	12.85	0.21	1.43	79.72	105.05
658	49.66	13.56	0.21	1.43	79.61	105.56
659	49.76	13.36	0.25	1.43	78.83	106.06
660	49.85	14.07	0.25	1.43	75.45	105.30
661	49.99	14.68	0.14	1.43	70.32	104.44
662	50.09	15.79	0.17	1.43	70.12	103.40
663	50.21	12.75	0.18	1.43	73.69	103.83
664	50.24	12.85	0.18	1.53	76.33	103.72
665	50.29	13.97	0.17	1.53	74.08	103.47
666	50.38	13.87	0.15	1.53	73.00	103.13
667	50.47	13.16	0.15	1.53	73.91	102.86
668	50.52	13.06	0.15	1.62	75.96	102.88
669	50.62	12.65	0.16	1.62	76.35	103.11
670	50.66	13.26	0.17	1.62	76.26	103.37
671	50.76	13.46	0.17	1.62	76.25	103.65
672	50.83	13.06	0.18	1.62	73.88	104.35

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
673	50.91	15.79	0.21	1.62	75.06	105.23
674	51.00	13.97	0.24	1.62	71.94	106.28
675	51.06	17.00	0.25	1.62	67.88	107.32
676	51.15	21.05	0.29	1.62	69.95	108.74
677	51.24	14.88	0.40	1.62	78.64	110.36
678	51.31	13.06	0.52	1.62	100.00	111.65
679	51.39	10.63	0.63	1.62	79.74	113.89
680	51.48	31.88	0.71	1.72	52.10	116.37
681	51.58	53.85	0.83	1.72	50.39	117.73
682	51.68	20.34	1.00	1.72	65.78	117.82
683	51.77	9.21	0.95	1.72	93.85	117.60
684	51.90	23.89	1.17	1.72	59.97	121.42
685	52.01	77.23	2.02	1.72	34.57	125.62
686	52.11	122.06	2.62	1.82	24.20	130.24
687	52.26	186.13	4.47	1.91	20.87	132.32
688	52.30	177.33	4.12	1.91	16.50	133.89
689	52.33	263.97	4.17	2.01	12.89	134.16
690	52.35	303.94	4.21	2.01	9.58	134.71
691	52.40	340.79	4.23	2.10	7.60	135.11
692	52.45	397.77	4.28	2.10	6.58	135.59
693	52.50	405.87	4.66	2.10	5.88	136.22
694	52.55	443.01	5.01	2.20	5.51	137.00
695	52.60	493.01	5.46	2.29	4.93	137.28
696	52.65	523.48	5.64	2.29	4.29	137.28
697	52.71	531.47	4.88	2.29	3.82	137.28
698	52.77	538.36	4.91	2.39	3.33	137.17
699	52.82	555.56	4.74	2.48	2.92	137.04
700	52.88	581.47	4.49	2.48	2.56	137.02
701	52.93	597.26	4.71	2.48	2.35	137.05
702	52.98	597.36	4.69	2.68	2.26	137.26
703	53.03	622.36	4.79	2.77	2.29	137.28
704	53.08	606.07	4.93	2.77	2.33	137.28
705	53.12	596.25	4.80	2.87	2.35	137.28
706	53.17	600.60	4.53	2.96	2.30	137.12
707	53.23	597.67	4.62	2.96	2.17	136.97
708	53.28	603.74	4.51	2.96	2.36	137.15
709	53.37	587.14	4.91	2.96	2.61	137.28
710	53.42	574.49	5.08	2.96	2.84	137.28
711	53.46	590.58	5.02	3.06	3.06	137.28
712	53.53	595.24	5.73	3.06	3.30	137.28
713	53.61	611.13	6.49	3.15	3.78	137.28
714	53.62	585.52	6.56	3.15	4.29	137.28
715	53.65	550.00	6.65	3.15	4.43	137.28
716	53.67	586.48	6.45	3.15	4.49	137.28
717	53.70	577.42	6.61	3.15	4.24	137.28
718	53.74	587.44	6.53	3.25	4.32	137.28
719	53.76	583.50	6.67	3.25	4.30	137.28
720	53.80	580.36	6.60	3.35	4.27	137.28

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
721	53.84	579.25	6.26	3.35	4.16	137.28
722	53.90	573.68	6.10	3.54	4.02	137.28
723	53.91	581.62	6.13	3.54	4.14	137.28
724	53.95	555.16	6.20	3.35	4.11	137.28
725	53.96	584.00	6.20	3.54	4.03	137.28
726	53.98	600.50	6.20	3.35	3.69	137.28
727	53.99	618.52	6.20	3.54	3.66	137.28
728	54.01	589.67	6.20	3.54	3.83	137.28
729	54.02	568.11	6.20	3.54	4.04	137.28
730	54.03	580.06	6.20	3.44	4.51	137.28
731	54.04	511.13	6.23	3.44	5.55	137.28
732	54.05	423.17	6.26	3.44	7.02	137.28
733	54.09	422.06	6.38	3.44	8.01	137.28
734	54.10	422.52	6.39	3.44	8.11	137.28
735	54.13	420.04	6.40	3.44	8.10	137.28
736	54.14	422.97	6.38	3.54	8.17	137.28
737	54.19	419.73	6.47	3.54	8.19	137.28
738	54.19	425.60	6.59	3.54	8.13	137.28
739	54.24	440.89	6.74	3.54	7.58	137.28
740	54.29	451.01	5.95	3.63	6.38	137.28
741	54.33	478.84	4.90	3.63	4.97	137.18
742	54.38	492.30	4.37	3.73	3.90	136.44
743	54.39	513.56	4.28	3.73	3.34	136.18
744	54.43	532.08	4.28	3.82	3.17	136.44
745	54.48	541.59	4.69	3.92	2.05	135.02
746	54.52	555.46	1.86	4.01	1.07	133.52
747	54.58	572.77	2.20	4.01	0.00	131.47
748	54.62	593.21	2.48	4.01	0.17	132.34
749	54.65	595.24	2.63	4.11	0.34	133.29
750	54.67	624.69	3.14	4.21	0.41	134.02
751	54.71	649.89	3.25	4.30	0.23	134.52
752	54.77	699.69	3.10	4.30	0.00	132.94
753	54.81	688.25	1.22	4.40	0.00	131.29
754	54.85	720.84	1.65	4.49	0.00	129.34
755	54.86	702.93	1.70	4.49	0.00	130.17
756	54.87	703.44	1.76	4.01	0.00	130.82
757	54.91	703.44	2.13	4.01	0.00	131.80
758	54.96	703.94	2.50	4.11	0.00	132.67
759	55.00	713.86	2.56	4.21	0.00	133.08
760	55.01	691.59	2.56	4.30	0.00	133.14
761	55.05	681.88	2.60	4.30	0.00	133.23
762	55.10	663.66	2.72	4.30	0.00	133.31
763	55.12	607.48	2.75	4.30	0.35	133.29
764	55.13	539.98	2.77	3.82	0.72	133.17
765	55.14	565.28	2.75	3.82	0.76	133.02
766	55.19	583.90	2.62	3.92	0.54	132.92
767	55.20	581.37	2.60	3.92	0.51	132.84
768	55.25	563.36	2.67	3.92	0.76	132.97

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
769	55.29	541.49	2.82	3.92	1.13	133.28
770	55.33	533.19	3.02	3.82	1.75	133.67
771	55.38	484.21	3.29	3.82	3.14	134.78
772	55.48	425.91	4.60	3.73	4.92	135.85
773	55.57	407.69	5.12	3.82	6.63	136.68
774	55.63	400.40	5.18	3.73	8.12	137.28
775	55.72	386.03	6.83	3.82	8.85	137.28
776	55.80	419.53	7.09	3.92	8.57	137.28
777	55.86	487.55	7.03	3.92	5.58	137.28
778	55.97	534.41	2.93	4.01	2.94	135.99
779	56.01	561.43	2.52	4.11	0.84	133.07
780	56.06	585.62	2.75	4.11	2.80	133.29
781	56.11	616.29	3.05	4.21	2.89	134.29
782	56.15	637.24	3.61	4.21	2.94	135.21
783	56.20	668.42	3.85	4.21	3.11	136.08
784	56.27	676.92	4.26	4.21	3.34	136.55
785	56.27	643.97	4.36	3.54	3.72	137.19
786	56.30	671.45	5.00	3.63	4.59	137.28
787	56.33	611.03	5.86	3.63	4.98	137.28
788	56.35	665.99	5.93	3.73	5.33	137.28
789	56.40	665.78	6.04	3.73	5.05	137.28
790	56.41	671.65	6.02	3.73	5.04	137.28
791	56.44	670.44	5.96	3.73	4.83	137.28
792	56.49	702.32	5.96	4.01	4.63	137.28
793	56.54	712.65	6.04	4.01	4.51	137.28
794	56.58	737.34	6.69	4.01	4.47	137.28
795	56.59	761.53	6.82	4.01	4.50	137.28
796	56.64	751.51	6.82	4.11	4.44	137.28
797	56.69	758.80	6.82	4.11	4.36	137.28
798	56.73	783.90	6.89	4.11	4.18	137.28
799	56.78	791.59	6.79	4.01	4.03	137.28
800	56.83	760.01	6.22	3.92	4.01	137.28
801	56.88	726.82	5.89	3.92	4.11	137.28
802	56.89	708.40	5.80	3.92	4.29	137.28
803	56.95	691.29	5.71	3.92	4.27	137.28
804	57.01	677.73	5.02	3.92	4.25	137.28
805	57.07	634.81	4.55	3.92	4.06	137.16
806	57.11	625.10	4.12	3.92	3.10	134.76
807	57.17	598.27	1.33	3.92	2.28	132.45
808	57.26	572.36	1.93	3.92	1.15	128.54
809	57.31	551.41	1.12	3.82	1.89	129.56
810	57.37	517.20	2.07	3.92	2.19	129.21
811	57.45	491.70	1.77	3.82	3.04	129.89
812	57.51	461.74	1.72	3.92	3.56	129.21
813	57.53	400.30	1.71	3.44	4.16	128.95
814	57.59	402.43	1.70	3.35	4.63	128.80
815	57.63	401.31	1.70	3.35	4.68	128.76
816	57.68	393.01	1.70	3.35	4.88	128.72

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
817	57.73	380.06	1.70	3.35	5.00	128.66
818	57.78	386.23	1.69	3.25	5.00	128.45
819	57.86	370.64	1.59	3.25	5.00	127.83
820	57.92	322.87	1.37	3.25	5.00	127.38
821	57.98	285.32	1.55	3.15	5.00	126.34
822	58.06	264.17	1.14	3.15	8.62	126.17
823	58.12	240.38	1.42	3.06	10.36	126.82
824	58.21	224.09	2.06	3.06	12.69	127.74
825	58.26	202.63	1.92	2.96	14.68	128.10
826	58.35	186.44	1.85	2.87	16.91	127.69
827	58.41	151.92	1.98	2.77	18.65	126.15
828	58.50	126.31	1.07	2.77	22.32	124.42
829	58.56	90.18	1.13	2.68	25.70	122.30
830	58.64	77.93	1.17	2.68	32.24	121.95
831	58.73	65.49	1.17	2.58	38.56	121.50
832	58.80	47.47	1.15	2.58	46.17	120.90
833	58.84	40.28	1.14	2.58	53.64	120.39
834	58.85	38.87	1.15	2.10	52.29	120.54
835	58.93	52.12	1.18	2.10	46.67	120.88
836	58.98	60.42	1.13	2.10	41.28	121.05
837	59.02	61.74	1.07	2.01	38.75	120.92
838	59.12	63.06	1.05	2.01	37.78	120.90
839	59.17	65.28	1.10	1.91	37.23	121.24
840	59.27	67.81	1.19	1.91	37.05	121.75
841	59.31	68.83	1.26	1.82	37.57	122.15
842	59.41	66.19	1.29	1.82	39.18	122.16
843	59.46	59.41	1.25	1.72	42.47	121.59
844	59.55	48.28	1.11	1.72	47.58	120.51
845	59.65	38.56	0.98	1.62	52.69	118.45
846	59.70	32.08	0.61	1.62	56.48	116.90
847	59.80	32.03	0.70	1.62	57.81	115.98
848	59.89	32.03	0.75	1.62	59.47	116.71
849	59.94	31.98	0.83	1.53	62.29	117.23
850	60.01	29.05	0.89	1.53	64.42	117.61
851	60.02	29.96	0.90	1.05	61.57	118.05
852	60.08	38.87	0.92	1.05	57.81	118.31
853	60.12	37.75	0.91	1.05	56.24	118.23
854	60.17	33.00	0.85	1.05	59.45	117.26
855	60.27	27.83	0.68	0.96	63.29	115.67
856	60.31	24.80	0.53	0.96	66.90	113.84
857	60.37	21.76	0.47	0.96	69.47	112.16
858	60.46	20.04	0.38	0.96	70.56	111.08
859	60.51	20.95	0.36	0.96	68.92	110.12
860	60.61	21.25	0.32	0.96	66.37	109.76
861	60.65	22.06	0.32	0.96	64.85	109.53
862	60.75	22.17	0.33	0.96	64.20	109.61
863	60.81	22.27	0.33	0.96	64.08	109.63
864	60.89	22.27	0.33	0.96	63.94	109.50

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
865	60.94	22.06	0.31	0.96	63.62	109.62
866	61.03	22.98	0.34	0.96	63.91	109.95
867	61.09	22.77	0.37	0.96	64.04	110.05
868	61.19	22.17	0.32	0.96	64.33	109.85
869	61.24	22.17	0.32	0.96	62.81	109.78
870	61.33	24.49	0.35	0.96	60.69	110.44
871	61.38	26.82	0.39	0.96	65.07	112.24
872	61.47	21.25	0.62	0.96	71.67	113.99
873	61.53	21.36	0.74	0.96	79.17	115.51
874	61.62	22.98	0.84	0.96	67.75	116.60
875	61.70	38.46	0.78	0.96	49.71	119.32
876	61.77	71.96	1.30	0.96	39.07	122.50
877	61.86	89.98	1.86	1.05	35.53	124.72
878	61.95	83.91	1.82	0.96	37.04	125.34
879	61.97	69.13	1.75	0.96	40.15	124.80
880	62.01	64.78	1.66	0.76	44.89	124.10
881	62.10	53.14	1.59	0.96	50.12	122.90
882	62.24	38.56	1.26	0.86	45.56	121.95
883	62.34	74.49	1.03	0.96	29.67	122.37
884	62.49	150.00	1.24	1.05	20.54	123.30
885	62.54	158.20	1.26	1.05	16.26	124.73
886	62.66	185.32	1.44	1.05	14.83	125.34
887	62.74	200.61	1.45	1.05	13.53	125.96
888	62.87	213.05	1.49	1.05	12.71	126.26
889	62.92	221.25	1.54	1.05	12.47	126.53
890	63.03	217.20	1.57	1.05	12.52	126.76
891	63.15	219.03	1.63	1.15	12.78	126.94
892	63.26	217.91	1.66	1.15	13.29	127.02
893	63.37	202.33	1.66	1.15	13.86	126.99
894	63.45	199.80	1.66	1.15	13.98	126.43
895	63.54	198.28	1.34	1.15	13.43	125.53
896	63.61	194.63	1.14	1.15	13.55	124.83
897	63.69	177.93	1.33	1.15	15.16	124.41
898	63.79	143.52	1.25	1.15	19.52	124.50
899	63.89	103.64	1.44	1.15	24.98	122.85
900	63.98	71.25	0.85	1.15	33.14	121.18
901	64.07	50.71	0.88	1.15	41.48	118.58
902	64.15	37.45	0.76	1.15	52.38	117.41
903	64.23	29.15	0.71	1.15	63.17	116.21
904	64.26	23.28	0.70	1.15	71.64	115.56
905	64.29	22.98	0.70	1.43	74.94	115.28
906	64.33	24.39	0.67	1.43	73.52	114.50
907	64.43	22.67	0.50	1.43	71.96	113.44
908	64.47	21.86	0.45	1.53	70.64	112.07
909	64.53	22.27	0.41	1.53	70.50	111.44
910	64.62	21.25	0.40	1.53	73.02	110.99
911	64.72	18.22	0.40	1.53	77.07	110.67
912	64.78	17.81	0.39	1.53	81.00	110.63

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
913	64.86	17.91	0.41	1.53	81.31	111.04
914	64.96	18.83	0.47	1.62	81.88	112.08
915	65.06	19.53	0.57	1.62	82.82	113.03
916	65.11	19.23	0.60	1.62	84.86	113.77
917	65.21	18.83	0.64	1.62	87.03	114.04
918	65.31	18.42	0.64	1.62	88.72	114.06
919	65.40	18.02	0.62	1.62	86.96	113.18
920	65.50	18.32	0.43	1.62	82.58	111.98
921	65.58	19.33	0.38	1.62	77.73	110.66
922	65.68	19.33	0.38	1.72	76.23	110.07
923	65.78	18.42	0.34	1.72	80.14	109.58
924	65.84	15.18	0.33	1.72	84.20	109.11
925	65.86	15.54	0.33	1.72	87.64	108.93
926	65.87	15.89	0.33	1.72	83.53	109.02
927	65.98	18.02	0.33	1.72	80.56	109.07
928	66.10	17.81	0.33	1.72	79.47	109.53
929	66.21	17.61	0.38	1.72	79.99	110.29
930	66.34	19.13	0.43	1.72	79.70	110.56
931	66.48	18.62	0.36	1.72	78.52	110.82
932	66.62	19.18	0.42	1.72	79.48	110.40
933	66.68	17.51	0.38	1.72	80.06	110.93
934	66.87	19.23	0.44	1.82	82.16	112.09
935	66.96	19.94	0.62	1.82	85.60	113.68
936	67.11	18.22	0.72	1.82	91.78	114.55
937	67.21	16.50	0.70	1.82	96.41	113.97
938	67.35	15.69	0.52	1.82	96.63	113.04
939	67.45	16.40	0.51	1.82	100.00	114.17
940	67.59	16.30	0.99	1.82	74.11	118.15
941	67.68	49.49	1.42	1.82	36.45	123.51
942	67.83	166.29	1.89	1.91	19.64	126.78
943	67.92	263.46	1.98	1.91	12.65	128.48
944	68.02	293.92	1.94	1.91	10.42	129.17
945	68.07	292.10	2.13	2.01	9.92	129.67
946	68.16	310.93	2.28	2.01	9.66	129.78
947	68.26	313.97	1.99	2.01	9.50	129.92
948	68.35	307.79	2.22	2.01	9.90	130.20
949	68.45	301.41	2.56	2.01	10.63	130.56
950	68.55	290.58	2.39	2.01	11.31	130.75
951	68.65	282.39	2.48	2.01	12.31	130.45
952	68.78	242.10	2.43	2.01	13.49	130.30
953	68.78	236.18	2.41	2.01	14.48	130.04
954	68.79	236.18	2.38	2.01	14.61	129.83
955	68.83	230.26	2.26	2.10	13.84	129.35
956	68.93	246.56	1.93	2.20	12.61	128.54
957	68.98	254.15	1.63	2.20	11.06	127.54
958	69.04	259.82	1.45	2.20	10.24	126.83
959	69.12	259.31	1.45	2.20	10.05	126.69
960	69.22	258.60	1.54	2.29	10.33	126.73

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
961	69.28	248.07	1.50	2.29	10.73	126.58
962	69.36	236.43	1.40	2.29	11.11	126.14
963	69.45	227.63	1.34	2.29	11.72	125.57
964	69.60	206.58	1.26	2.29	12.39	125.02
965	69.70	196.05	1.19	2.29	13.09	124.55
966	69.80	191.80	1.17	2.29	13.36	124.31
967	69.89	192.31	1.17	2.29	13.46	124.27
968	69.98	192.00	1.18	2.39	13.63	124.23
969	70.08	186.03	1.17	2.39	14.12	123.79
970	70.18	167.51	1.02	2.39	16.36	123.38
971	70.32	125.81	1.13	2.39	21.31	122.57
972	70.42	79.55	1.08	2.29	30.56	121.25
973	70.54	47.47	0.86	2.29	44.49	118.96
974	70.66	28.34	0.70	2.29	62.02	116.28
975	70.75	19.64	0.59	2.29	75.05	114.30
976	70.80	22.47	0.52	2.48	75.37	112.45
977	70.89	23.18	0.33	2.48	68.76	110.56
978	70.99	22.17	0.25	2.48	64.60	108.11
979	71.08	21.56	0.21	2.48	63.51	106.54
980	71.17	21.05	0.19	2.58	62.68	105.76
981	71.23	21.56	0.19	2.58	63.23	105.32
982	71.33	20.04	0.18	2.58	62.20	104.96
983	71.42	21.56	0.16	2.58	59.64	104.34
984	71.52	23.48	0.14	2.58	56.37	103.78
985	71.58	23.28	0.14	2.58	56.41	104.37
986	71.67	22.77	0.19	2.58	59.63	105.94
987	71.81	22.47	0.26	2.68	62.96	107.28
988	71.82	22.06	0.26	2.68	64.77	107.94
989	71.86	22.06	0.26	2.68	65.57	107.99
990	71.91	21.66	0.26	2.68	65.98	108.01
991	71.97	21.66	0.26	2.68	66.78	108.09
992	72.05	21.36	0.27	2.68	67.69	108.22
993	72.10	20.95	0.28	2.68	68.75	108.41
994	72.20	20.95	0.29	2.68	69.45	108.55
995	72.25	20.95	0.29	2.77	70.00	108.81
996	72.34	20.95	0.31	2.77	70.88	109.34
997	72.44	21.25	0.35	2.77	72.30	109.98
998	72.53	20.95	0.38	2.77	74.03	110.47
999	72.63	20.34	0.39	2.77	74.87	110.69
1000	72.69	20.95	0.39	2.77	75.74	110.64
1001	72.82	20.04	0.38	2.77	75.05	110.60
1002	72.92	20.95	0.38	2.77	73.32	110.41
1003	73.06	22.27	0.35	2.87	70.40	110.34
1004	73.16	22.98	0.35	2.87	70.10	110.49
1005	73.30	21.66	0.39	2.87	74.63	110.57
1006	73.35	17.81	0.39	2.87	78.07	110.69
1007	73.38	20.04	0.39	2.87	79.92	110.48
1008	73.47	19.64	0.37	2.87	77.08	110.44

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1009	73.53	20.24	0.37	2.96	76.55	110.30
1010	73.62	20.24	0.36	2.96	76.12	110.24
1011	73.71	19.94	0.36	2.96	77.10	110.31
1012	73.77	19.53	0.38	2.96	79.03	110.64
1013	73.86	19.23	0.42	3.06	81.15	111.10
1014	73.96	19.13	0.45	3.06	82.23	111.57
1015	74.06	19.64	0.47	3.06	82.36	111.89
1016	74.13	19.84	0.48	3.06	81.49	112.15
1017	74.24	20.45	0.48	3.06	80.85	112.33
1018	74.34	20.65	0.50	3.06	80.73	112.54
1019	74.44	20.45	0.51	3.06	81.57	112.67
1020	74.58	20.04	0.51	3.06	81.41	112.52
1021	74.68	20.50	0.47	3.06	78.40	111.21
1022	74.80	20.24	0.27	3.15	74.93	109.94
1023	74.92	20.55	0.31	3.15	73.80	109.11
1024	75.07	19.84	0.36	3.15	75.92	109.75
1025	75.08	19.64	0.36	3.15	77.59	110.03
1026	75.11	19.64	0.36	3.25	78.16	110.07
1027	75.16	19.43	0.37	3.25	78.98	110.30
1028	75.25	19.43	0.39	3.25	80.91	110.74
1029	75.32	18.93	0.43	3.35	82.63	111.17
1030	75.40	18.93	0.44	3.35	83.61	111.30
1031	75.50	18.93	0.42	3.35	83.49	110.99
1032	75.59	18.42	0.38	3.35	83.68	110.27
1033	75.69	17.41	0.34	3.35	84.66	109.43
1034	75.78	16.70	0.31	3.35	85.61	108.57
1035	75.88	16.30	0.28	3.35	85.84	107.84
1036	75.96	16.09	0.26	3.35	85.52	107.10
1037	76.05	15.79	0.24	3.35	84.67	106.59
1038	76.14	16.09	0.23	3.44	84.37	106.31
1039	76.26	15.89	0.23	3.44	84.09	106.37
1040	76.36	16.09	0.24	3.44	84.42	106.50
1041	76.41	16.09	0.24	3.44	84.56	106.55
1042	76.51	15.89	0.23	3.44	85.32	106.38
1043	76.65	15.38	0.23	3.44	86.78	106.27
1044	76.72	15.08	0.24	3.44	88.00	106.27
1045	76.79	15.18	0.24	3.54	88.79	106.37
1046	76.89	15.08	0.24	3.54	90.66	107.25
1047	76.98	15.28	0.33	3.54	97.45	110.24
1048	77.08	15.89	0.64	3.54	92.62	112.89
1049	77.18	22.67	0.68	3.54	84.18	115.44
1050	77.28	27.83	0.85	3.54	77.43	117.59
1051	77.37	29.55	1.20	3.63	80.05	119.52
1052	77.42	26.11	1.45	3.63	81.77	120.82
1053	77.42	30.47	1.49	3.73	80.76	121.59
1054	77.44	33.91	1.59	3.73	75.56	122.42
1055	77.48	37.45	1.79	3.73	72.09	123.26
1056	77.52	40.69	1.91	3.82	69.21	123.98

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1057	77.54	43.52	1.97	3.82	67.19	124.41
1058	77.57	44.43	2.03	3.82	67.13	124.60
1059	77.62	42.00	2.05	3.82	68.46	124.53
1060	77.65	40.18	1.97	3.82	70.82	124.28
1061	77.67	37.96	1.92	3.82	71.65	123.83
1062	77.71	37.85	1.76	3.82	71.90	123.46
1063	77.71	37.75	1.73	3.73	71.69	122.88
1064	77.76	35.32	1.55	3.82	73.39	122.11
1065	77.81	31.07	1.35	3.73	75.70	120.92
1066	77.90	28.74	1.16	3.82	78.54	119.86
1067	77.95	27.13	1.11	3.82	80.91	119.27
1068	78.01	25.91	1.14	3.82	82.45	118.93
1069	78.10	25.81	1.05	3.82	78.83	118.74
1070	78.16	30.87	0.98	3.82	63.10	119.02
1071	78.24	52.02	0.97	3.92	49.66	119.64
1072	78.29	63.76	1.00	3.92	39.63	120.51
1073	78.39	78.54	1.05	3.92	34.27	121.15
1074	78.47	89.78	1.06	3.92	31.50	121.96
1075	78.53	93.42	1.23	3.92	31.16	123.05
1076	78.62	94.84	1.51	3.92	32.43	124.23
1077	78.68	94.33	1.70	3.92	34.74	124.97
1078	78.69	84.31	1.76	3.92	35.67	125.92
1079	78.78	100.10	2.16	3.92	36.75	126.73
1080	78.81	97.27	2.34	3.92	38.10	127.66
1081	78.92	87.04	2.58	3.92	41.97	127.53
1082	79.03	71.36	2.29	3.92	46.36	126.48
1083	79.16	59.92	1.72	3.92	46.07	125.04
1084	79.26	73.78	1.52	4.01	39.53	124.49
1085	79.35	101.31	1.66	4.01	33.43	125.47
1086	79.45	116.80	2.02	4.01	30.53	126.98
1087	79.54	125.00	2.38	4.01	29.73	128.12
1088	79.64	130.77	2.50	4.01	29.16	128.84
1089	79.74	137.75	2.60	4.11	26.56	130.21
1090	79.88	191.60	3.45	4.21	23.02	131.59
1091	79.98	231.27	3.61	4.21	19.11	132.52
1092	80.12	263.76	3.19	4.21	17.02	132.38
1093	80.22	251.11	2.99	4.21	15.38	131.25
1094	80.36	244.53	2.16	4.21	14.66	129.87
1095	80.46	238.56	1.83	4.21	13.44	128.07
1096	80.60	233.20	1.51	4.21	12.69	126.55
1097	80.70	223.58	1.18	4.21	12.64	125.70
1098	80.83	214.78	1.39	4.30	13.47	125.59
1099	80.94	200.81	1.51	4.30	15.55	125.88
1100	81.01	167.71	1.47	4.21	17.35	125.78
1101	81.04	165.18	1.46	4.40	18.79	125.42
1102	81.09	159.61	1.41	4.40	19.43	125.22
1103	81.13	150.30	1.41	4.40	20.68	125.10
1104	81.18	138.66	1.47	4.40	23.02	125.16

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1105	81.23	121.46	1.58	4.40	26.12	125.34
1106	81.28	109.61	1.68	4.40	29.84	125.42
1107	81.33	96.96	1.71	4.40	33.69	125.60
1108	81.37	87.75	1.89	4.40	38.07	125.99
1109	81.42	80.57	2.17	4.40	42.18	126.42
1110	81.47	75.20	2.23	4.40	45.53	126.65
1111	81.52	71.36	2.25	4.40	47.80	126.68
1112	81.56	69.23	2.31	4.40	48.75	126.82
1113	81.61	72.17	2.40	4.40	49.37	126.98
1114	81.64	70.14	2.41	4.40	50.62	127.02
1115	81.70	63.87	2.40	4.40	54.71	126.72
1116	81.75	52.33	2.36	4.40	60.30	126.26
1117	81.79	46.76	2.28	4.40	66.56	125.58
1118	81.82	41.40	2.11	4.40	70.87	124.78
1119	81.86	37.35	1.89	4.40	74.63	123.79
1120	81.91	33.91	1.69	4.40	77.94	122.73
1121	81.95	30.57	1.50	4.40	81.32	121.53
1122	82.00	27.23	1.28	4.40	84.85	120.08
1123	82.09	23.99	1.02	4.40	88.86	118.54
1124	82.15	21.36	0.91	4.40	93.55	117.24
1125	82.19	19.43	0.86	4.49	97.46	116.22
1126	82.26	18.52	0.73	4.49	100.00	115.23
1127	82.34	17.00	0.65	4.49	100.00	114.22
1128	82.39	15.28	0.62	4.49	100.00	113.42
1129	82.48	14.47	0.58	4.59	100.00	112.80
1130	82.58	14.37	0.53	4.59	100.00	112.31
1131	82.62	14.88	0.51	4.59	100.00	111.87
1132	82.70	14.78	0.48	4.59	100.00	111.60
1133	82.77	14.78	0.47	4.59	100.00	111.26
1134	82.87	14.68	0.45	4.59	100.00	111.18
1135	82.96	15.59	0.46	4.68	100.00	111.16
1136	83.06	18.22	0.44	4.68	90.71	111.46
1137	83.16	20.65	0.45	4.68	79.92	111.87
1138	83.25	25.10	0.46	4.78	72.16	112.31
1139	83.34	27.43	0.46	4.78	66.55	112.65
1140	83.44	28.85	0.46	4.87	65.23	113.13
1141	83.54	28.54	0.53	4.87	65.41	113.57
1142	83.64	28.64	0.54	4.87	66.63	114.00
1143	83.73	28.44	0.56	4.87	69.35	114.34
1144	83.83	25.81	0.63	4.87	71.50	114.84
1145	83.85	27.33	0.67	5.07	74.13	115.50
1146	83.89	27.13	0.74	5.07	74.39	116.20
1147	83.94	27.73	0.82	5.07	76.21	117.47
1148	84.04	29.25	1.08	5.07	76.59	118.57
1149	84.09	30.57	1.13	5.07	76.69	119.51
1150	84.13	31.17	1.19	5.07	76.09	119.96
1151	84.18	31.88	1.26	5.07	76.24	120.30
1152	84.25	31.78	1.29	5.07	77.16	120.50

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1153	84.33	30.67	1.30	5.07	79.11	120.53
1154	84.37	29.25	1.31	5.07	81.52	120.45
1155	84.46	28.24	1.30	5.16	83.35	120.16
1156	84.52	27.33	1.20	5.16	84.37	119.78
1157	84.57	26.72	1.15	5.16	84.59	119.32
1158	84.67	26.42	1.10	5.16	84.79	119.04
1159	84.71	26.21	1.08	5.16	85.52	118.94
1160	84.81	25.61	1.12	5.16	87.61	119.09
1161	84.86	24.70	1.19	5.16	90.53	119.33
1162	84.91	23.99	1.23	5.16	93.50	119.49
1163	85.00	23.28	1.24	5.16	95.77	119.52
1164	85.05	22.77	1.24	5.16	97.25	119.32
1165	85.15	22.17	1.16	5.16	97.82	118.97
1166	85.19	21.86	1.09	5.16	97.66	118.30
1167	85.29	21.15	0.96	5.16	97.29	117.62
1168	85.35	20.75	0.90	5.16	97.56	116.95
1169	85.42	20.04	0.86	5.16	98.84	116.52
1170	85.48	19.23	0.83	5.16	100.00	116.19
1171	85.55	18.72	0.81	5.26	100.00	115.89
1172	85.63	18.12	0.79	5.26	100.00	115.64
1173	85.68	17.51	0.78	5.26	100.00	115.45
1174	85.77	17.00	0.77	5.26	100.00	115.34
1175	85.82	16.80	0.77	5.26	100.00	115.39
1176	85.89	17.10	0.80	5.26	100.00	115.55
1177	85.96	18.12	0.81	5.26	100.00	115.74
1178	86.03	19.53	0.79	5.26	98.42	115.81
1179	86.11	21.25	0.76	5.26	92.88	115.75
1180	86.16	22.17	0.74	5.26	88.74	115.62
1181	86.25	22.67	0.72	5.26	89.87	115.47
1182	86.36	19.94	0.73	5.26	94.60	114.88
1183	86.50	17.10	0.62	5.26	100.00	114.26
1184	86.51	17.21	0.61	5.26	100.00	113.63
1185	86.52	17.21	0.60	5.26	100.00	113.28
1186	86.57	17.31	0.54	5.26	100.00	112.52
1187	86.65	17.31	0.44	5.35	96.58	111.56
1188	86.71	17.31	0.41	5.35	94.30	110.68
1189	86.80	17.21	0.38	5.35	94.07	110.11
1190	86.90	16.50	0.35	5.45	95.37	109.44
1191	86.99	15.49	0.32	5.45	97.33	108.73
1192	87.04	15.08	0.30	5.45	98.63	108.13
1193	87.14	14.98	0.28	5.45	98.41	107.81
1194	87.19	15.18	0.28	5.45	97.17	107.78
1195	87.28	15.69	0.29	5.54	95.63	108.26
1196	87.38	16.50	0.33	5.54	93.79	108.83
1197	87.43	17.10	0.34	5.54	91.88	109.36
1198	87.52	17.71	0.35	5.54	89.95	109.63
1199	87.61	18.22	0.36	5.64	88.28	109.78
1200	87.66	18.52	0.36	5.64	87.04	109.79

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1201	87.76	18.62	0.35	5.64	86.65	109.67
1202	87.84	18.32	0.34	5.64	86.71	109.46
1203	87.91	18.12	0.33	5.64	87.47	109.24
1204	88.00	17.71	0.32	5.64	88.37	109.00
1205	88.11	17.31	0.31	5.73	89.54	108.84
1206	88.19	17.10	0.31	5.73	90.39	108.72
1207	88.25	17.00	0.31	5.73	90.81	108.62
1208	88.34	16.90	0.30	5.73	90.64	108.42
1209	88.44	16.90	0.29	5.83	90.17	108.15
1210	88.54	16.90	0.28	5.83	89.58	107.90
1211	88.64	16.90	0.27	5.83	89.37	107.73
1212	88.72	16.80	0.27	5.93	89.61	107.69
1213	88.82	16.70	0.28	5.93	90.07	107.73
1214	88.91	16.70	0.28	5.93	90.83	107.82
1215	89.01	16.50	0.28	5.93	91.58	107.90
1216	89.10	16.40	0.29	5.93	92.45	107.97
1217	89.19	16.30	0.29	6.02	93.00	107.82
1218	89.30	15.99	0.27	6.02	91.00	106.79
1219	89.39	16.09	0.18	6.12	89.02	106.17
1220	89.49	16.60	0.23	6.12	88.22	106.44
1221	89.59	16.90	0.29	6.12	90.32	107.86
1222	89.69	16.95	0.32	6.12	91.89	108.72
1223	89.73	17.00	0.33	6.21	90.02	109.17
1224	89.78	18.83	0.34	6.31	87.19	109.42
1225	89.83	19.33	0.34	6.31	84.28	109.67
1226	89.88	19.64	0.35	6.31	83.80	109.89
1227	89.93	19.64	0.36	6.31	83.63	110.18
1228	90.00	20.04	0.38	6.40	83.30	110.59
1229	90.07	20.75	0.41	6.40	82.14	111.03
1230	90.12	21.56	0.42	6.40	81.06	111.60
1231	90.22	22.27	0.46	6.40	80.51	112.20
1232	90.27	22.67	0.50	6.40	80.53	113.17
1233	90.36	23.89	0.60	6.40	77.53	114.19
1234	90.46	28.14	0.65	6.50	73.54	115.05
1235	90.50	30.06	0.66	6.50	70.62	115.50
1236	90.61	29.35	0.68	6.59	70.53	115.62
1237	90.66	28.74	0.68	6.59	71.78	115.45
1238	90.75	27.73	0.63	6.59	73.00	114.95
1239	90.84	26.11	0.57	6.59	74.84	114.27
1240	90.89	24.39	0.54	6.59	76.93	113.58
1241	90.99	23.38	0.50	6.59	79.28	113.09
1242	91.04	22.37	0.49	6.69	81.25	112.68
1243	91.14	21.46	0.48	6.69	83.54	112.40
1244	91.22	20.65	0.47	6.79	85.84	112.13
1245	91.28	19.84	0.46	6.79	88.45	111.80
1246	91.37	18.72	0.44	6.79	89.92	111.48
1247	91.47	18.93	0.42	6.88	90.14	111.12
1248	91.61	19.03	0.40	6.88	88.70	110.98

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1249	91.71	19.53	0.41	6.88	88.08	110.93
1250	91.81	19.33	0.41	6.88	87.81	110.97
1251	91.87	19.33	0.41	6.98	88.02	110.84
1252	92.00	19.13	0.39	6.98	86.12	110.10
1253	92.10	19.38	0.29	6.98	84.52	109.49
1254	92.20	19.43	0.32	7.07	83.14	109.22
1255	92.33	19.74	0.35	7.07	83.97	109.76
1256	92.38	19.79	0.37	7.07	84.45	110.16
1257	92.43	19.84	0.37	7.26	84.47	110.37
1258	92.48	20.14	0.38	7.26	85.19	110.58
1259	92.56	19.64	0.40	7.36	86.02	110.74
1260	92.63	19.53	0.40	7.36	87.16	110.82
1261	92.67	19.43	0.40	7.36	87.45	110.81
1262	92.72	19.43	0.40	7.36	87.55	110.79
1263	92.77	19.43	0.40	7.36	87.20	110.81
1264	92.86	19.74	0.40	7.46	86.63	110.88
1265	92.92	20.04	0.41	7.46	86.16	111.05
1266	92.97	20.14	0.42	7.55	86.69	111.44
1267	93.05	20.14	0.46	7.55	87.17	111.82
1268	93.10	20.45	0.47	7.55	87.05	112.15
1269	93.16	20.95	0.48	7.55	85.70	112.28
1270	93.25	21.56	0.48	7.65	83.79	112.35
1271	93.35	22.27	0.47	7.65	80.44	112.40
1272	93.40	24.19	0.47	7.65	78.94	112.28
1273	93.49	22.77	0.45	7.74	78.47	112.15
1274	93.56	22.47	0.45	7.74	79.73	111.99
1275	93.64	22.57	0.45	7.74	79.38	112.05
1276	93.73	23.28	0.46	7.74	78.34	112.52
1277	93.83	24.70	0.52	7.84	76.63	113.28
1278	93.88	26.42	0.57	8.03	75.40	114.39
1279	93.97	27.83	0.67	8.03	75.84	115.13
1280	94.07	26.42	0.70	8.03	78.80	115.71
1281	94.17	24.70	0.75	8.03	82.08	116.26
1282	94.26	25.81	0.86	8.03	80.59	116.63
1283	94.36	29.25	0.79	8.03	81.16	117.93
1284	94.45	28.24	1.17	8.03	80.92	119.20
1285	94.55	30.57	1.33	8.12	72.58	120.82
1286	94.64	48.48	1.34	8.12	58.20	121.86
1287	94.72	65.99	1.33	8.03	49.16	122.39
1288	94.74	64.98	1.34	8.03	41.37	122.92
1289	94.77	90.28	1.36	8.31	37.18	123.45
1290	94.85	97.87	1.44	8.31	33.27	124.10
1291	94.90	103.54	1.52	8.31	32.34	124.67
1292	94.95	106.48	1.62	8.31	32.54	125.32
1293	95.01	105.57	1.83	8.31	34.52	126.41
1294	95.09	101.62	2.33	8.31	37.59	127.40
1295	95.14	94.94	2.54	8.31	42.18	128.49
1296	95.23	86.54	3.07	8.31	47.11	129.05

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1297	95.29	77.43	3.22	8.31	52.64	129.44
1298	95.38	69.84	3.34	8.31	57.15	129.42
1299	95.43	65.69	3.35	8.31	59.57	129.33
1300	95.52	66.70	3.28	8.31	59.18	129.26
1301	95.57	70.75	3.23	8.31	56.95	129.08
1302	95.67	72.87	2.99	8.31	55.03	128.58
1303	95.77	69.74	2.61	8.22	56.22	127.67
1304	95.86	56.58	2.39	8.22	62.27	126.89
1305	95.95	44.23	2.56	8.22	64.67	126.27
1306	96.03	57.64	2.16	8.22	71.02	125.95
1307	96.11	37.96	2.38	8.31	66.58	126.41
1308	96.20	58.70	2.78	8.51	62.59	127.77
1309	96.30	80.57	3.26	8.60	51.74	129.50
1310	96.39	100.81	3.60	8.60	44.40	130.84
1311	96.50	122.37	3.84	8.70	38.62	131.75
1312	96.59	145.34	3.92	8.60	32.42	131.58
1313	96.69	166.80	2.74	8.60	26.91	130.69
1314	96.78	182.08	2.25	8.60	22.17	129.05
1315	96.87	191.29	1.93	8.60	20.37	128.23
1316	96.98	184.11	1.94	8.60	20.02	127.84
1317	97.02	180.06	1.94	8.51	21.02	127.82
1318	97.06	168.82	2.00	8.70	21.61	128.14
1319	97.12	179.96	2.21	8.70	22.39	128.67
1320	97.16	177.63	2.41	8.70	23.05	129.34
1321	97.21	172.97	2.61	8.70	24.45	129.98
1322	97.27	170.04	2.93	8.60	25.91	130.63
1323	97.33	168.12	3.21	8.60	27.09	131.15
1324	97.40	166.09	3.29	8.60	27.88	131.39
1325	97.45	163.36	3.29	8.60	28.36	131.45
1326	97.50	161.94	3.32	8.60	29.21	131.67
1327	97.58	158.50	3.65	8.60	30.75	131.92
1328	97.65	146.66	3.76	8.51	32.97	132.07
1329	97.69	135.32	3.76	8.51	35.59	131.79
1330	97.74	120.95	3.57	8.51	38.21	131.25
1331	97.81	108.60	3.32	8.51	40.74	130.65
1332	97.88	101.62	3.24	8.51	42.61	130.19
1333	97.93	98.68	3.18	8.60	40.27	130.07
1334	98.03	125.30	2.99	8.79	31.75	130.21
1335	98.15	191.80	2.67	9.08	23.53	130.24
1336	98.21	230.36	2.44	9.08	17.43	129.79
1337	98.32	262.75	1.96	9.08	13.84	129.24
1338	98.42	299.09	1.85	9.08	10.93	128.66
1339	98.47	343.32	1.71	9.08	5.00	127.75
1340	98.57	405.97	1.08	9.18	5.00	126.30
1341	98.70	416.60	0.89	9.18	4.53	124.66
1342	98.78	412.55	0.91	9.27	4.67	124.49
1343	98.85	382.49	1.03	9.27	5.00	124.66
1344	98.86	321.86	1.03	9.08	5.00	124.72

:: Field input data :: (continued)

Point ID	Depth (ft)	q_c (tsf)	f_s (tsf)	u (tsf)	Fines content (%)	Unit weight (pcf)
1345	98.92	308.60	1.04	9.08	5.00	124.62
1346	98.98	337.35	1.04	9.18	5.00	124.75
1347	99.03	309.11	1.10	9.08	5.00	125.36
1348	99.11	281.37	1.35	8.98	5.00	126.14
1349	99.18	254.05	1.55	8.98	12.62	127.01
1350	99.23	230.16	1.76	8.89	15.59	128.18
1351	99.32	209.41	2.34	8.79	19.03	129.37
1352	99.37	189.57	2.77	8.79	22.90	130.41
1353	99.45	168.82	3.08	8.79	26.41	130.81
1354	99.56	152.93	3.11	8.79	29.20	131.00
1355	99.64	149.59	3.27	8.79	31.66	131.22
1356	99.71	139.27	3.58	8.79	34.06	131.59
1357	99.75	130.87	3.81	8.89	36.97	131.47
1358	99.90	114.27	3.39	8.79	40.25	131.23
1359	99.95	103.44	3.58	8.70	45.52	131.15
1360	100.04	87.25	4.17	8.70	42.09	132.11
1361	100.14	157.89	4.41	8.98	32.87	133.35
1362	100.14	232.39	4.40	8.98	26.10	134.08
1363	100.15	224.29	4.36	9.08	23.29	134.83
1364	100.19	250.30	5.18	9.18	22.57	136.06
1365	100.21	301.41	6.43	9.27	21.06	137.28
1366	100.24	342.10	7.12	9.27	14.70	135.60
1367	100.28	411.74	0.00	9.46	8.11	131.27
1368	100.31	477.42	0.00	9.56	N/A	87.36
1369	100.33	523.38	0.00	9.56	N/A	87.36
1370	100.38	524.49	0.00	9.56	N/A	87.36
1371	100.39	525.60	0.00	9.56	N/A	87.36
1372	100.43	529.15	0.00	9.65	N/A	87.36
1373	100.48	540.18	0.00	9.65	N/A	87.36
1374	100.53	496.96	0.00	9.56	N/A	87.36
1375	100.57	490.58	0.00	9.65	N/A	87.36
1376	100.60	500.40	0.00	9.94	N/A	87.36

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (ft)
q_c:	Measured cone resistance (tsf)
f_s:	Sleeve friction resistance (tsf)
u:	Pore pressure (tsf)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (pcf)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.04	0.00	0.00	0.00	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
2	0.10	0.00	0.00	0.00	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
3	0.11	0.00	0.00	0.00	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
4	0.16	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
5	0.19	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
6	0.24	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
7	0.31	0.01	0.00	0.01	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
8	0.38	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
9	0.43	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
10	0.49	0.02	0.00	0.02	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
11	0.58	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
12	0.63	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
13	0.67	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	No
14	0.72	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
15	0.72	0.03	0.00	0.03	1.00	0.410	1.36	0.301	1.00	1.00	2.000	Yes
16	0.84	0.04	0.00	0.04	1.00	0.409	1.36	0.301	1.00	1.00	2.000	Yes
17	0.96	0.05	0.00	0.05	1.00	0.409	1.36	0.301	1.00	1.00	2.000	Yes
18	1.06	0.05	0.00	0.05	1.00	0.409	1.36	0.301	1.00	1.00	2.000	Yes
19	1.24	0.06	0.00	0.06	1.00	0.409	1.36	0.301	1.00	1.00	2.000	Yes
20	1.30	0.07	0.00	0.07	1.00	0.409	1.36	0.301	1.00	1.00	2.000	Yes
21	1.48	0.08	0.00	0.08	1.00	0.409	1.36	0.301	1.00	1.00	2.000	Yes
22	1.59	0.08	0.00	0.08	1.00	0.409	1.36	0.301	1.00	1.00	2.000	Yes
23	1.69	0.09	0.00	0.09	1.00	0.409	1.36	0.300	1.00	1.00	2.000	Yes
24	1.69	0.09	0.00	0.09	1.00	0.409	1.36	0.300	1.00	1.00	2.000	Yes
25	1.74	0.09	0.00	0.09	1.00	0.409	1.36	0.300	1.00	1.00	2.000	Yes
26	1.79	0.09	0.00	0.09	1.00	0.409	1.36	0.300	1.00	1.00	2.000	No
27	1.84	0.09	0.00	0.09	1.00	0.409	1.36	0.300	1.00	1.00	2.000	No
28	1.88	0.10	0.00	0.10	1.00	0.409	1.36	0.300	1.00	1.00	2.000	No
29	1.93	0.10	0.00	0.10	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
30	1.99	0.10	0.00	0.10	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
31	2.03	0.11	0.00	0.11	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
32	2.08	0.11	0.00	0.11	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
33	2.13	0.11	0.00	0.11	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
34	2.22	0.12	0.00	0.12	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
35	2.27	0.12	0.00	0.12	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
36	2.33	0.12	0.00	0.12	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
37	2.42	0.13	0.00	0.13	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
38	2.48	0.13	0.00	0.13	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
39	2.56	0.13	0.00	0.13	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
40	2.65	0.14	0.00	0.14	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
41	2.72	0.14	0.00	0.14	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
42	2.80	0.15	0.00	0.15	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
43	2.89	0.15	0.00	0.15	1.00	0.408	1.36	0.300	1.00	1.00	2.000	No
44	2.94	0.16	0.00	0.16	1.00	0.407	1.36	0.300	1.00	1.00	2.000	No
45	3.04	0.16	0.00	0.16	0.99	0.407	1.36	0.300	1.00	1.00	2.000	No
46	3.14	0.17	0.00	0.17	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
47	3.23	0.17	0.00	0.17	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
48	3.31	0.18	0.00	0.18	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	3.37	0.18	0.00	0.18	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
50	3.48	0.18	0.00	0.18	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
51	3.57	0.19	0.00	0.19	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
52	3.65	0.19	0.00	0.19	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
53	3.71	0.20	0.00	0.20	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
54	3.82	0.20	0.00	0.20	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
55	3.91	0.21	0.00	0.21	0.99	0.407	1.36	0.299	1.00	1.00	2.000	No
56	4.00	0.21	0.00	0.21	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
57	4.10	0.22	0.00	0.22	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
58	4.19	0.22	0.00	0.22	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
59	4.26	0.23	0.00	0.23	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
60	4.35	0.23	0.00	0.23	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
61	4.44	0.23	0.00	0.23	0.99	0.406	1.36	0.299	1.00	1.00	2.000	No
62	4.52	0.24	0.00	0.24	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
63	4.53	0.24	0.00	0.24	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
64	4.58	0.24	0.00	0.24	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
65	4.63	0.24	0.00	0.24	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
66	4.68	0.25	0.00	0.25	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
67	4.72	0.25	0.00	0.25	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
68	4.77	0.25	0.00	0.25	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
69	4.82	0.26	0.00	0.26	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
70	4.88	0.26	0.00	0.26	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
71	4.96	0.26	0.00	0.26	0.99	0.406	1.36	0.298	1.00	1.00	2.000	No
72	5.01	0.27	0.00	0.27	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
73	5.08	0.27	0.00	0.27	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
74	5.16	0.27	0.00	0.27	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
75	5.21	0.28	0.00	0.28	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
76	5.30	0.28	0.00	0.28	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
77	5.37	0.29	0.00	0.29	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
78	5.45	0.29	0.00	0.29	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
79	5.52	0.29	0.00	0.29	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
80	5.59	0.30	0.00	0.30	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
81	5.65	0.30	0.00	0.30	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
82	5.74	0.31	0.00	0.31	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
83	5.83	0.31	0.00	0.31	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
84	5.89	0.31	0.00	0.31	0.99	0.405	1.36	0.298	1.00	1.00	2.000	No
85	5.97	0.32	0.00	0.32	0.99	0.405	1.36	0.297	1.00	1.00	2.000	No
86	6.07	0.32	0.00	0.32	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
87	6.12	0.33	0.00	0.33	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
88	6.22	0.33	0.00	0.33	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
89	6.28	0.34	0.00	0.34	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
90	6.36	0.34	0.00	0.34	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
91	6.46	0.35	0.00	0.35	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
92	6.52	0.35	0.00	0.35	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
93	6.60	0.35	0.00	0.35	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
94	6.70	0.36	0.00	0.36	0.99	0.404	1.36	0.297	1.00	1.00	2.000	No
95	6.76	0.36	0.00	0.36	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
96	6.84	0.37	0.00	0.37	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	6.94	0.37	0.00	0.37	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
98	7.03	0.38	0.00	0.38	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
99	7.13	0.38	0.00	0.38	0.99	0.404	1.36	0.297	1.00	1.00	2.000	Yes
100	7.19	0.38	0.00	0.38	0.99	0.403	1.36	0.297	1.00	1.00	2.000	Yes
101	7.32	0.39	0.00	0.39	0.98	0.403	1.36	0.297	1.00	1.00	2.000	No
102	7.42	0.39	0.00	0.39	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
103	7.49	0.40	0.00	0.40	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
104	7.57	0.40	0.00	0.40	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
105	7.66	0.40	0.00	0.40	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
106	7.76	0.41	0.00	0.41	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
107	7.77	0.41	0.00	0.41	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
108	7.78	0.41	0.00	0.41	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
109	7.82	0.41	0.00	0.41	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
110	7.87	0.41	0.00	0.41	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
111	7.92	0.42	0.00	0.42	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
112	7.97	0.42	0.00	0.42	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
113	8.01	0.42	0.00	0.42	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
114	8.06	0.42	0.00	0.42	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
115	8.11	0.42	0.00	0.42	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
116	8.20	0.43	0.00	0.43	0.98	0.403	1.36	0.296	1.00	1.00	2.000	No
117	8.26	0.43	0.00	0.43	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
118	8.35	0.44	0.00	0.44	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
119	8.40	0.44	0.00	0.44	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
120	8.49	0.44	0.00	0.44	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
121	8.54	0.44	0.00	0.44	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
122	8.64	0.45	0.00	0.45	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
123	8.69	0.45	0.00	0.45	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
124	8.79	0.46	0.00	0.46	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
125	8.84	0.46	0.00	0.46	0.98	0.402	1.36	0.296	1.00	1.00	2.000	No
126	8.93	0.46	0.00	0.46	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
127	9.03	0.47	0.00	0.47	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
128	9.08	0.47	0.00	0.47	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
129	9.11	0.47	0.00	0.47	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
130	9.12	0.47	0.00	0.47	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
131	9.17	0.48	0.00	0.48	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
132	9.22	0.48	0.00	0.48	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
133	9.31	0.48	0.00	0.48	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
134	9.36	0.49	0.00	0.49	0.98	0.402	1.36	0.295	1.00	1.00	2.000	No
135	9.40	0.49	0.00	0.49	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
136	9.46	0.49	0.00	0.49	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
137	9.51	0.49	0.00	0.49	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
138	9.55	0.50	0.00	0.50	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
139	9.61	0.50	0.00	0.50	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
140	9.69	0.50	0.00	0.50	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
141	9.74	0.51	0.00	0.51	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
142	9.81	0.51	0.00	0.51	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
143	9.89	0.51	0.00	0.51	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
144	9.94	0.52	0.00	0.52	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	10.03	0.52	0.00	0.52	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
146	10.08	0.52	0.00	0.52	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
147	10.18	0.53	0.00	0.53	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
148	10.23	0.53	0.00	0.53	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
149	10.33	0.54	0.00	0.54	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
150	10.40	0.54	0.00	0.54	0.98	0.401	1.36	0.295	1.00	1.00	2.000	No
151	10.47	0.54	0.00	0.54	0.98	0.401	1.36	0.294	1.00	1.00	2.000	No
152	10.51	0.55	0.00	0.55	0.98	0.401	1.36	0.294	1.00	1.00	2.000	No
153	10.56	0.55	0.00	0.55	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
154	10.61	0.55	0.00	0.55	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
155	10.67	0.55	0.00	0.55	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
156	10.75	0.56	0.00	0.56	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
157	10.80	0.56	0.00	0.56	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
158	10.85	0.56	0.00	0.56	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
159	10.90	0.57	0.00	0.57	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
160	11.00	0.57	0.00	0.57	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
161	11.05	0.58	0.00	0.58	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
162	11.14	0.58	0.00	0.58	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
163	11.21	0.58	0.00	0.58	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
164	11.29	0.59	0.00	0.59	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
165	11.38	0.59	0.00	0.59	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
166	11.46	0.60	0.00	0.60	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
167	11.52	0.60	0.00	0.60	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
168	11.60	0.61	0.00	0.61	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
169	11.67	0.61	0.00	0.61	0.98	0.400	1.36	0.294	1.00	1.00	2.000	No
170	11.72	0.61	0.00	0.61	0.98	0.399	1.36	0.294	1.00	1.00	2.000	No
171	11.81	0.62	0.00	0.62	0.98	0.399	1.36	0.294	1.00	1.00	2.000	No
172	11.86	0.62	0.00	0.62	0.98	0.399	1.36	0.294	1.00	1.00	2.000	No
173	11.96	0.63	0.00	0.63	0.98	0.399	1.36	0.294	1.00	1.00	2.000	No
174	12.01	0.63	0.00	0.63	0.97	0.399	1.36	0.294	1.00	1.00	2.000	No
175	12.10	0.63	0.00	0.63	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
176	12.16	0.64	0.00	0.64	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
177	12.24	0.64	0.00	0.64	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
178	12.32	0.64	0.00	0.64	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
179	12.39	0.65	0.00	0.65	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
180	12.48	0.65	0.00	0.65	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
181	12.50	0.65	0.00	0.65	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
182	12.54	0.66	0.00	0.66	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
183	12.64	0.66	0.00	0.66	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
184	12.68	0.66	0.00	0.66	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
185	12.77	0.67	0.00	0.67	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
186	12.82	0.67	0.00	0.67	0.97	0.399	1.36	0.293	1.00	1.00	2.000	No
187	12.89	0.68	0.00	0.68	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
188	12.97	0.68	0.00	0.68	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
189	13.03	0.68	0.00	0.68	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
190	13.12	0.69	0.00	0.69	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
191	13.16	0.69	0.00	0.69	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
192	13.26	0.70	0.00	0.70	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	13.34	0.70	0.00	0.70	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
194	13.41	0.70	0.00	0.70	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
195	13.50	0.71	0.00	0.71	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
196	13.60	0.71	0.00	0.71	0.97	0.398	1.36	0.293	1.00	1.00	2.000	No
197	13.65	0.72	0.00	0.72	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
198	13.75	0.72	0.00	0.72	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
199	13.80	0.73	0.00	0.73	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
200	13.89	0.73	0.00	0.73	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
201	13.94	0.73	0.00	0.73	0.97	0.398	1.36	0.292	1.00	1.00	2.000	No
202	14.03	0.74	0.00	0.74	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
203	14.11	0.74	0.00	0.74	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
204	14.13	0.74	0.00	0.74	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
205	14.18	0.75	0.00	0.75	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
206	14.22	0.75	0.00	0.75	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
207	14.28	0.75	0.00	0.75	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
208	14.37	0.76	0.00	0.76	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
209	14.44	0.76	0.00	0.76	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
210	14.51	0.76	0.00	0.76	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
211	14.60	0.77	0.00	0.77	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
212	14.65	0.77	0.00	0.77	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
213	14.75	0.78	0.00	0.78	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
214	14.85	0.78	0.00	0.78	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
215	14.91	0.79	0.00	0.79	0.97	0.397	1.36	0.292	1.00	1.00	2.000	No
216	14.99	0.79	0.00	0.79	0.97	0.397	1.36	0.292	1.00	1.00	2.000	Yes
217	15.09	0.80	0.00	0.80	0.97	0.397	1.36	0.292	1.00	1.00	2.000	Yes
218	15.18	0.80	0.00	0.80	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
219	15.25	0.81	0.00	0.81	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
220	15.33	0.81	0.00	0.81	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
221	15.43	0.82	0.00	0.82	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
222	15.51	0.82	0.00	0.82	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
223	15.59	0.83	0.00	0.83	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
224	15.67	0.83	0.00	0.83	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
225	15.76	0.84	0.00	0.84	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
226	15.86	0.84	0.00	0.84	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
227	15.95	0.85	0.00	0.85	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
228	16.05	0.85	0.00	0.85	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
229	16.14	0.86	0.00	0.86	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
230	16.20	0.86	0.00	0.86	0.97	0.396	1.36	0.291	1.00	1.00	2.000	Yes
231	16.28	0.87	0.00	0.87	0.97	0.395	1.36	0.291	1.00	1.00	2.000	Yes
232	16.34	0.87	0.00	0.87	0.97	0.395	1.36	0.291	1.00	1.00	2.000	Yes
233	16.44	0.87	0.00	0.87	0.97	0.395	1.36	0.291	1.00	1.00	2.000	Yes
234	16.50	0.88	0.00	0.88	0.97	0.395	1.36	0.291	1.00	1.00	2.000	Yes
235	16.58	0.88	0.00	0.88	0.97	0.395	1.36	0.291	1.00	1.00	2.000	Yes
236	16.73	0.89	0.00	0.89	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
237	16.82	0.89	0.00	0.89	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
238	16.92	0.90	0.00	0.90	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
239	17.01	0.90	0.00	0.90	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
240	17.11	0.91	0.00	0.91	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	17.12	0.91	0.00	0.91	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
242	17.14	0.91	0.00	0.91	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
243	17.19	0.91	0.00	0.91	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
244	17.28	0.92	0.00	0.92	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
245	17.33	0.92	0.00	0.92	0.96	0.395	1.36	0.290	1.00	1.00	2.000	No
246	17.43	0.92	0.00	0.92	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
247	17.47	0.93	0.00	0.93	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
248	17.57	0.93	0.00	0.93	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
249	17.65	0.94	0.00	0.94	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
250	17.72	0.94	0.00	0.94	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
251	17.81	0.94	0.00	0.94	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
252	17.86	0.95	0.00	0.95	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
253	17.95	0.95	0.00	0.95	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
254	18.05	0.96	0.00	0.96	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
255	18.10	0.96	0.00	0.96	0.96	0.394	1.36	0.290	1.00	1.00	2.000	No
256	18.20	0.97	0.00	0.97	0.96	0.394	1.36	0.289	1.00	1.00	2.000	No
257	18.30	0.97	0.00	0.97	0.96	0.394	1.36	0.289	1.00	1.00	2.000	No
258	18.39	0.98	0.00	0.98	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
259	18.48	0.98	0.00	0.98	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
260	18.58	0.99	0.00	0.99	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
261	18.66	0.99	0.00	0.99	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
262	18.74	1.00	0.00	1.00	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
263	18.87	1.00	0.00	1.00	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
264	18.97	1.01	0.00	1.01	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
265	19.06	1.01	0.00	1.01	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
266	19.16	1.02	0.00	1.02	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
267	19.25	1.02	0.00	1.02	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
268	19.27	1.02	0.00	1.02	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
269	19.30	1.02	0.00	1.02	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
270	19.34	1.03	0.00	1.03	0.96	0.393	1.36	0.289	1.00	1.00	2.000	No
271	19.39	1.03	0.00	1.03	0.96	0.392	1.36	0.289	1.00	1.00	2.000	No
272	19.49	1.04	0.00	1.04	0.96	0.392	1.36	0.288	1.00	1.00	2.000	No
273	19.55	1.04	0.00	1.04	0.96	0.392	1.36	0.288	1.00	1.00	2.000	No
274	19.63	1.04	0.00	1.04	0.96	0.392	1.36	0.288	1.00	1.00	2.000	No
275	19.68	1.05	0.00	1.05	0.96	0.392	1.36	0.288	1.00	1.00	2.000	No
276	19.74	1.05	0.00	1.05	0.96	0.392	1.36	0.288	1.00	1.00	2.000	No
277	19.83	1.05	0.00	1.05	0.96	0.392	1.36	0.288	1.00	1.00	2.000	No
278	19.87	1.06	0.00	1.06	0.96	0.392	1.36	0.288	1.00	1.00	2.000	No
279	19.94	1.06	0.00	1.06	0.96	0.392	1.36	0.288	1.00	1.00	2.000	No
280	20.02	1.06	0.00	1.06	0.96	0.392	1.36	0.288	1.00	1.00	2.000	No
281	20.07	1.07	0.00	1.07	0.96	0.392	1.36	0.288	1.00	1.00	2.000	No
282	20.17	1.07	0.00	1.07	0.96	0.392	1.36	0.288	1.00	1.00	2.000	No
283	20.21	1.07	0.00	1.07	0.96	0.392	1.36	0.288	1.00	1.00	2.000	Yes
284	20.28	1.08	0.00	1.08	0.96	0.392	1.36	0.288	1.00	1.00	2.000	Yes
285	20.36	1.08	0.00	1.08	0.96	0.391	1.36	0.288	1.00	1.00	2.000	Yes
286	20.41	1.09	0.00	1.09	0.96	0.391	1.36	0.288	0.99	1.00	2.000	Yes
287	20.48	1.09	0.00	1.09	0.96	0.391	1.36	0.288	0.99	1.00	2.000	Yes
288	20.55	1.09	0.00	1.09	0.96	0.391	1.36	0.288	0.99	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	20.60	1.10	0.00	1.10	0.96	0.391	1.36	0.288	0.99	1.00	2.000	Yes
290	20.70	1.10	0.00	1.10	0.96	0.391	1.36	0.288	0.99	1.00	2.000	No
291	20.74	1.11	0.00	1.11	0.95	0.391	1.36	0.288	0.99	1.00	2.000	No
292	20.79	1.11	0.00	1.11	0.95	0.391	1.36	0.287	0.99	1.00	2.000	No
293	20.89	1.11	0.00	1.11	0.95	0.391	1.36	0.287	0.99	1.00	2.000	No
294	20.96	1.12	0.00	1.12	0.95	0.391	1.36	0.287	0.99	1.00	2.000	No
295	21.04	1.12	0.00	1.12	0.95	0.391	1.36	0.287	0.99	1.00	2.000	No
296	21.13	1.13	0.00	1.13	0.95	0.391	1.36	0.287	0.99	1.00	2.000	No
297	21.22	1.13	0.00	1.13	0.95	0.391	1.36	0.287	0.99	1.00	2.000	No
298	21.29	1.14	0.00	1.14	0.95	0.390	1.36	0.287	0.99	1.00	2.000	No
299	21.35	1.14	0.00	1.14	0.95	0.390	1.36	0.287	0.99	1.00	2.000	No
300	21.37	1.14	0.00	1.14	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
301	21.42	1.14	0.00	1.14	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
302	21.47	1.15	0.00	1.15	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
303	21.48	1.15	0.00	1.15	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
304	21.52	1.15	0.00	1.15	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
305	21.57	1.15	0.00	1.15	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
306	21.62	1.16	0.00	1.16	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
307	21.66	1.16	0.00	1.16	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
308	21.71	1.16	0.00	1.16	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
309	21.76	1.17	0.00	1.17	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
310	21.81	1.17	0.00	1.17	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
311	21.85	1.17	0.00	1.17	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
312	21.91	1.17	0.00	1.17	0.95	0.390	1.36	0.287	0.98	1.00	2.000	No
313	21.95	1.18	0.00	1.18	0.95	0.390	1.36	0.286	0.98	1.00	2.000	No
314	22.00	1.18	0.00	1.18	0.95	0.390	1.36	0.286	0.98	1.00	2.000	No
315	22.05	1.18	0.00	1.18	0.95	0.390	1.36	0.286	0.98	1.00	2.000	No
316	22.10	1.19	0.00	1.19	0.95	0.389	1.36	0.286	0.98	1.00	2.000	No
317	22.15	1.19	0.00	1.19	0.95	0.389	1.36	0.286	0.98	1.00	2.000	No
318	22.19	1.19	0.00	1.19	0.95	0.389	1.36	0.286	0.98	1.00	2.000	No
319	22.24	1.19	0.00	1.19	0.95	0.389	1.36	0.286	0.98	1.00	2.000	No
320	22.29	1.20	0.00	1.20	0.95	0.389	1.36	0.286	0.98	1.00	2.000	No
321	22.34	1.20	0.00	1.20	0.95	0.389	1.36	0.286	0.98	1.00	2.000	No
322	22.39	1.20	0.00	1.20	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
323	22.43	1.21	0.00	1.21	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
324	22.48	1.21	0.00	1.21	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
325	22.55	1.21	0.00	1.21	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
326	22.62	1.22	0.00	1.22	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
327	22.63	1.22	0.00	1.22	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
328	22.72	1.22	0.00	1.22	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
329	22.77	1.23	0.00	1.23	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
330	22.83	1.23	0.00	1.23	0.95	0.389	1.36	0.286	0.97	1.00	2.000	No
331	22.91	1.24	0.00	1.24	0.95	0.388	1.36	0.286	0.97	1.00	2.000	No
332	22.96	1.24	0.00	1.24	0.95	0.388	1.36	0.286	0.97	1.00	2.000	No
333	23.02	1.24	0.00	1.24	0.95	0.388	1.36	0.286	0.97	1.00	2.000	No
334	23.10	1.25	0.00	1.25	0.95	0.388	1.36	0.285	0.97	1.00	2.000	No
335	23.16	1.25	0.00	1.25	0.95	0.388	1.36	0.285	0.97	1.00	2.000	No
336	23.20	1.25	0.00	1.25	0.95	0.388	1.36	0.285	0.97	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	23.26	1.26	0.00	1.26	0.95	0.388	1.36	0.285	0.97	1.00	2.000	No
338	23.35	1.26	0.00	1.26	0.95	0.388	1.36	0.285	0.97	1.00	2.000	No
339	23.39	1.27	0.00	1.27	0.95	0.388	1.36	0.285	0.96	1.00	2.000	No
340	23.48	1.27	0.00	1.27	0.95	0.388	1.36	0.285	0.96	1.00	2.000	No
341	23.54	1.27	0.00	1.27	0.95	0.388	1.36	0.285	0.96	1.00	2.000	No
342	23.63	1.28	0.00	1.28	0.95	0.388	1.36	0.285	0.96	1.00	2.000	No
343	23.69	1.28	0.00	1.28	0.95	0.387	1.36	0.285	0.96	1.00	2.000	No
344	23.78	1.29	0.00	1.29	0.95	0.387	1.36	0.285	0.96	1.00	2.000	No
345	23.87	1.29	0.00	1.29	0.95	0.387	1.36	0.285	0.96	1.00	2.000	No
346	23.88	1.29	0.00	1.29	0.95	0.387	1.36	0.285	0.96	1.00	2.000	No
347	23.93	1.30	0.00	1.30	0.95	0.387	1.36	0.285	0.96	1.00	2.000	No
348	24.02	1.30	0.00	1.30	0.95	0.387	1.36	0.285	0.96	1.00	2.000	No
349	24.04	1.30	0.00	1.30	0.95	0.387	1.36	0.285	0.96	1.00	2.000	No
350	24.05	1.30	0.00	1.30	0.95	0.387	1.36	0.285	0.96	1.00	2.000	No
351	24.15	1.31	0.00	1.31	0.94	0.387	1.36	0.284	0.96	1.00	2.000	No
352	24.20	1.31	0.00	1.31	0.94	0.387	1.36	0.284	0.96	1.00	2.000	No
353	24.30	1.32	0.00	1.32	0.94	0.387	1.36	0.284	0.96	1.00	2.000	No
354	24.40	1.32	0.00	1.32	0.94	0.387	1.36	0.284	0.96	1.00	2.000	No
355	24.46	1.33	0.00	1.33	0.94	0.386	1.36	0.284	0.96	1.00	2.000	No
356	24.54	1.33	0.00	1.33	0.94	0.386	1.36	0.284	0.95	1.00	2.000	No
357	24.64	1.34	0.00	1.34	0.94	0.386	1.36	0.284	0.95	1.00	2.000	Yes
358	24.73	1.34	0.00	1.34	0.94	0.386	1.36	0.284	0.95	1.00	2.000	Yes
359	24.78	1.35	0.00	1.35	0.94	0.386	1.36	0.284	0.95	1.00	2.000	Yes
360	24.88	1.35	0.00	1.35	0.94	0.386	1.36	0.284	0.95	1.00	2.000	Yes
361	24.94	1.36	0.00	1.36	0.94	0.386	1.36	0.284	0.95	1.00	2.000	Yes
362	25.02	1.36	0.00	1.36	0.94	0.386	1.36	0.284	0.95	1.00	2.000	Yes
363	25.12	1.37	0.00	1.37	0.94	0.386	1.36	0.283	0.95	1.00	2.000	Yes
364	25.17	1.37	0.00	1.37	0.94	0.385	1.36	0.283	0.95	1.00	2.000	Yes
365	25.27	1.38	0.00	1.38	0.94	0.385	1.36	0.283	0.95	1.00	2.000	Yes
366	25.36	1.38	0.00	1.38	0.94	0.385	1.36	0.283	0.95	1.00	2.000	No
367	25.43	1.38	0.00	1.38	0.94	0.385	1.36	0.283	0.95	1.00	2.000	No
368	25.50	1.39	0.00	1.39	0.94	0.385	1.36	0.283	0.95	1.00	2.000	No
369	25.60	1.39	0.00	1.39	0.94	0.385	1.36	0.283	0.95	1.00	2.000	No
370	25.64	1.40	0.00	1.40	0.94	0.385	1.36	0.283	0.95	1.00	2.000	No
371	25.67	1.40	0.00	1.40	0.94	0.385	1.36	0.283	0.95	1.00	2.000	No
372	25.71	1.40	0.00	1.40	0.94	0.385	1.36	0.283	0.95	1.00	2.000	No
373	25.79	1.40	0.00	1.40	0.94	0.384	1.36	0.283	0.95	1.00	2.000	No
374	25.93	1.41	0.00	1.41	0.94	0.384	1.36	0.283	0.94	1.00	2.000	No
375	26.03	1.42	0.00	1.42	0.94	0.384	1.36	0.282	0.94	1.00	2.000	No
376	26.13	1.42	0.00	1.42	0.94	0.384	1.36	0.282	0.94	1.00	2.000	No
377	26.24	1.43	0.00	1.43	0.94	0.384	1.36	0.282	0.94	1.00	2.000	No
378	26.37	1.43	0.00	1.43	0.94	0.384	1.36	0.282	0.94	1.00	2.000	No
379	26.47	1.44	0.00	1.44	0.94	0.383	1.36	0.282	0.94	1.00	2.000	No
380	26.60	1.45	0.00	1.45	0.94	0.383	1.36	0.282	0.94	1.00	2.000	No
381	26.71	1.45	0.00	1.45	0.94	0.383	1.36	0.282	0.94	1.00	2.000	No
382	26.85	1.46	0.00	1.46	0.93	0.383	1.36	0.281	0.94	1.00	2.000	No
383	26.95	1.46	0.00	1.46	0.93	0.383	1.36	0.281	0.94	1.00	2.000	No
384	27.04	1.47	0.00	1.47	0.93	0.382	1.36	0.281	0.94	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	27.09	1.47	0.00	1.47	0.93	0.382	1.36	0.281	0.94	1.00	2.000	No
386	27.19	1.48	0.00	1.48	0.93	0.382	1.36	0.281	0.94	1.00	2.000	No
387	27.23	1.48	0.00	1.48	0.93	0.382	1.36	0.281	0.94	1.00	2.000	No
388	27.33	1.48	0.00	1.48	0.93	0.382	1.36	0.281	0.93	1.00	2.000	No
389	27.40	1.49	0.00	1.49	0.93	0.382	1.36	0.281	0.93	1.00	2.000	No
390	27.47	1.49	0.00	1.49	0.93	0.382	1.36	0.281	0.93	1.00	2.000	No
391	27.57	1.50	0.00	1.50	0.93	0.382	1.36	0.281	0.93	1.00	2.000	No
392	27.66	1.50	0.00	1.50	0.93	0.381	1.36	0.280	0.93	1.00	2.000	No
393	27.77	1.51	0.00	1.51	0.93	0.381	1.36	0.280	0.93	1.00	2.000	No
394	27.86	1.51	0.00	1.51	0.93	0.381	1.36	0.280	0.93	1.00	2.000	No
395	27.96	1.52	0.00	1.52	0.93	0.381	1.36	0.280	0.93	1.00	2.000	No
396	28.06	1.52	0.00	1.52	0.93	0.381	1.36	0.280	0.93	1.00	2.000	No
397	28.15	1.53	0.00	1.53	0.93	0.381	1.36	0.280	0.93	1.00	2.000	No
398	28.25	1.54	0.00	1.54	0.93	0.380	1.36	0.280	0.93	1.00	2.000	No
399	28.34	1.54	0.00	1.54	0.93	0.380	1.36	0.280	0.93	1.00	2.000	No
400	28.44	1.55	0.00	1.55	0.93	0.380	1.36	0.279	0.93	1.00	2.000	No
401	28.54	1.55	0.00	1.55	0.93	0.380	1.36	0.279	0.93	1.00	2.000	No
402	28.62	1.56	0.00	1.56	0.93	0.380	1.36	0.279	0.93	1.00	2.000	No
403	28.71	1.56	0.00	1.56	0.93	0.380	1.36	0.279	0.93	1.00	2.000	No
404	28.77	1.56	0.00	1.56	0.93	0.379	1.36	0.279	0.92	1.00	2.000	No
405	28.86	1.57	0.00	1.57	0.93	0.379	1.36	0.279	0.92	1.00	2.000	No
406	28.91	1.57	0.00	1.57	0.93	0.379	1.36	0.279	0.92	1.00	2.000	No
407	28.97	1.58	0.00	1.58	0.93	0.379	1.36	0.279	0.92	1.00	2.000	No
408	29.04	1.58	0.00	1.58	0.93	0.379	1.36	0.279	0.92	1.00	2.000	No
409	29.10	1.58	0.00	1.58	0.92	0.379	1.36	0.278	0.92	1.00	2.000	No
410	29.15	1.59	0.00	1.59	0.92	0.379	1.36	0.278	0.92	1.00	2.000	No
411	29.25	1.59	0.00	1.59	0.92	0.378	1.36	0.278	0.92	1.00	2.000	No
412	29.34	1.60	0.00	1.60	0.92	0.378	1.36	0.278	0.92	1.00	2.000	No
413	29.38	1.60	0.00	1.60	0.92	0.378	1.36	0.278	0.92	1.00	2.000	No
414	29.48	1.61	0.00	1.61	0.92	0.378	1.36	0.278	0.92	1.00	2.000	No
415	29.55	1.61	0.00	1.61	0.92	0.378	1.36	0.278	0.92	1.00	2.000	Yes
416	29.63	1.62	0.00	1.62	0.92	0.378	1.36	0.278	0.92	1.00	2.000	Yes
417	29.72	1.62	0.00	1.62	0.92	0.378	1.36	0.278	0.92	1.00	2.000	Yes
418	29.82	1.63	0.00	1.63	0.92	0.377	1.36	0.277	0.92	1.00	2.000	Yes
419	29.88	1.63	0.00	1.63	0.92	0.377	1.36	0.277	0.92	1.00	2.000	Yes
420	29.96	1.63	0.00	1.63	0.92	0.377	1.36	0.277	0.92	1.00	2.000	Yes
421	30.06	1.64	0.00	1.64	0.92	0.377	1.36	0.277	0.92	1.00	2.000	Yes
422	30.13	1.64	0.00	1.64	0.92	0.378	1.36	0.278	0.92	1.00	2.000	Yes
423	30.18	1.65	0.01	1.64	0.92	0.378	1.36	0.278	0.92	1.00	0.303	No
424	30.28	1.65	0.01	1.64	0.92	0.378	1.36	0.278	0.92	1.00	0.304	No
425	30.37	1.66	0.01	1.65	0.92	0.379	1.36	0.279	0.92	1.00	0.304	No
426	30.47	1.66	0.01	1.65	0.92	0.379	1.36	0.279	0.92	1.00	0.305	No
427	30.57	1.67	0.02	1.65	0.92	0.380	1.36	0.279	0.91	1.00	0.305	No
428	30.66	1.68	0.02	1.65	0.92	0.380	1.36	0.280	0.91	1.00	0.306	No
429	30.74	1.68	0.02	1.66	0.92	0.381	1.36	0.280	0.91	1.00	0.306	No
430	30.82	1.68	0.03	1.66	0.92	0.381	1.36	0.280	0.91	1.00	0.306	No
431	30.90	1.69	0.03	1.66	0.92	0.381	1.36	0.280	0.91	1.00	0.307	No
432	31.01	1.70	0.03	1.66	0.92	0.382	1.36	0.281	0.91	1.00	0.307	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	31.10	1.70	0.03	1.67	0.91	0.382	1.36	0.281	0.91	1.00	0.308	No
434	31.19	1.71	0.04	1.67	0.91	0.383	1.36	0.281	0.91	1.00	0.308	No
435	31.28	1.71	0.04	1.67	0.91	0.383	1.36	0.282	0.91	1.00	0.309	No
436	31.35	1.72	0.04	1.67	0.91	0.383	1.36	0.282	0.91	1.00	0.309	No
437	31.43	1.72	0.04	1.68	0.91	0.384	1.36	0.282	0.91	1.00	0.309	No
438	31.53	1.73	0.05	1.68	0.91	0.384	1.36	0.283	0.91	1.00	0.310	No
439	31.60	1.73	0.05	1.68	0.91	0.385	1.36	0.283	0.91	1.00	0.310	No
440	31.67	1.74	0.05	1.68	0.91	0.385	1.36	0.283	0.91	1.00	0.311	No
441	31.77	1.74	0.06	1.69	0.91	0.385	1.36	0.283	0.91	1.00	0.311	No
442	31.84	1.75	0.06	1.69	0.91	0.386	1.36	0.283	0.91	1.00	0.311	No
443	31.91	1.75	0.06	1.69	0.91	0.386	1.36	0.284	0.91	1.00	0.312	No
444	31.98	1.76	0.06	1.69	0.91	0.386	1.36	0.284	0.91	1.00	0.312	No
445	31.98	1.76	0.06	1.69	0.91	0.386	1.36	0.284	0.91	1.00	0.312	No
446	32.04	1.76	0.06	1.70	0.91	0.386	1.36	0.284	0.91	1.00	0.312	No
447	32.12	1.76	0.07	1.70	0.91	0.387	1.36	0.284	0.91	1.00	2.000	Yes
448	32.16	1.77	0.07	1.70	0.91	0.387	1.36	0.284	0.91	1.00	2.000	Yes
449	32.27	1.77	0.07	1.70	0.91	0.387	1.36	0.285	0.91	1.00	2.000	Yes
450	32.33	1.78	0.07	1.70	0.91	0.388	1.36	0.285	0.91	1.00	2.000	Yes
451	32.41	1.78	0.08	1.71	0.91	0.388	1.36	0.285	0.91	1.00	2.000	Yes
452	32.50	1.79	0.08	1.71	0.91	0.388	1.36	0.285	0.91	1.00	2.000	Yes
453	32.58	1.79	0.08	1.71	0.91	0.389	1.36	0.286	0.91	1.00	2.000	Yes
454	32.66	1.80	0.08	1.71	0.91	0.389	1.36	0.286	0.91	1.00	2.000	Yes
455	32.74	1.80	0.09	1.72	0.91	0.389	1.36	0.286	0.91	1.00	2.000	Yes
456	32.84	1.81	0.09	1.72	0.90	0.390	1.36	0.286	0.91	1.00	2.000	Yes
457	32.90	1.81	0.09	1.72	0.90	0.390	1.36	0.287	0.91	1.00	2.000	Yes
458	32.98	1.82	0.09	1.72	0.90	0.390	1.36	0.287	0.91	1.00	2.000	Yes
459	33.08	1.82	0.10	1.73	0.90	0.390	1.36	0.287	0.91	1.00	0.317	No
460	33.14	1.83	0.10	1.73	0.90	0.391	1.36	0.287	0.91	1.00	0.317	No
461	33.22	1.83	0.10	1.73	0.90	0.391	1.36	0.287	0.91	1.00	0.317	No
462	33.32	1.84	0.10	1.73	0.90	0.391	1.36	0.288	0.91	1.00	0.318	No
463	33.37	1.84	0.11	1.73	0.90	0.392	1.36	0.288	0.91	1.00	0.318	No
464	33.47	1.84	0.11	1.74	0.90	0.392	1.36	0.288	0.91	1.00	0.318	No
465	33.56	1.85	0.11	1.74	0.90	0.392	1.36	0.288	0.91	1.00	0.318	No
466	33.63	1.85	0.11	1.74	0.90	0.392	1.36	0.289	0.91	1.00	0.319	No
467	33.71	1.86	0.12	1.74	0.90	0.393	1.36	0.289	0.91	1.00	0.319	No
468	33.81	1.86	0.12	1.74	0.90	0.393	1.36	0.289	0.90	1.00	0.319	No
469	33.90	1.87	0.12	1.75	0.90	0.393	1.36	0.289	0.90	1.00	0.320	No
470	33.95	1.87	0.12	1.75	0.90	0.394	1.36	0.289	0.90	1.00	0.320	No
471	34.04	1.88	0.13	1.75	0.90	0.394	1.36	0.290	0.90	1.00	0.320	No
472	34.14	1.88	0.13	1.75	0.90	0.394	1.36	0.290	0.90	1.00	0.321	No
473	34.17	1.88	0.13	1.75	0.90	0.394	1.36	0.290	0.90	1.00	0.321	No
474	34.20	1.88	0.13	1.75	0.90	0.394	1.36	0.290	0.90	1.00	0.321	No
475	34.26	1.89	0.13	1.75	0.90	0.395	1.36	0.290	0.90	1.00	0.321	No
476	34.35	1.89	0.14	1.76	0.90	0.395	1.36	0.290	0.90	1.00	0.321	No
477	34.43	1.90	0.14	1.76	0.89	0.395	1.36	0.291	0.90	1.00	0.322	No
478	34.49	1.90	0.14	1.76	0.89	0.395	1.36	0.291	0.90	1.00	0.322	No
479	34.59	1.90	0.14	1.76	0.89	0.396	1.36	0.291	0.90	1.00	0.322	No
480	34.69	1.91	0.15	1.76	0.89	0.396	1.36	0.291	0.90	1.00	0.322	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	34.73	1.91	0.15	1.76	0.89	0.396	1.36	0.291	0.90	1.00	0.323	No
482	34.83	1.92	0.15	1.76	0.89	0.396	1.36	0.291	0.90	1.00	0.323	No
483	34.90	1.92	0.15	1.77	0.89	0.397	1.36	0.292	0.90	1.00	0.323	No
484	34.98	1.92	0.16	1.77	0.89	0.397	1.36	0.292	0.90	1.00	0.323	No
485	35.07	1.93	0.16	1.77	0.89	0.397	1.36	0.292	0.90	1.00	0.324	No
486	35.16	1.93	0.16	1.77	0.89	0.397	1.36	0.292	0.90	1.00	0.324	No
487	35.26	1.94	0.16	1.77	0.89	0.398	1.36	0.292	0.90	1.00	0.324	No
488	35.33	1.94	0.17	1.78	0.89	0.398	1.36	0.292	0.90	1.00	0.324	No
489	35.40	1.95	0.17	1.78	0.89	0.398	1.36	0.293	0.90	1.00	0.325	No
490	35.50	1.95	0.17	1.78	0.89	0.398	1.36	0.293	0.90	1.00	0.325	No
491	35.57	1.96	0.17	1.78	0.89	0.398	1.36	0.293	0.90	1.00	0.325	No
492	35.65	1.96	0.18	1.78	0.89	0.399	1.36	0.293	0.90	1.00	0.325	No
493	35.71	1.96	0.18	1.79	0.89	0.399	1.36	0.293	0.90	1.00	0.326	No
494	35.79	1.97	0.18	1.79	0.88	0.399	1.36	0.293	0.90	1.00	0.326	No
495	35.85	1.97	0.18	1.79	0.88	0.399	1.36	0.293	0.90	1.00	0.326	No
496	35.94	1.98	0.19	1.79	0.88	0.399	1.36	0.294	0.90	1.00	0.326	No
497	35.99	1.98	0.19	1.79	0.88	0.400	1.36	0.294	0.90	1.00	0.326	No
498	36.08	1.99	0.19	1.80	0.88	0.400	1.36	0.294	0.90	1.00	0.327	No
499	36.17	1.99	0.19	1.80	0.88	0.400	1.36	0.294	0.90	1.00	0.327	No
500	36.24	1.99	0.19	1.80	0.88	0.400	1.36	0.294	0.90	1.00	0.327	No
501	36.33	2.00	0.20	1.80	0.88	0.400	1.36	0.294	0.90	1.00	0.327	No
502	36.42	2.00	0.20	1.80	0.88	0.401	1.36	0.294	0.90	1.00	0.328	No
503	36.52	2.01	0.20	1.81	0.88	0.401	1.36	0.295	0.90	1.00	0.328	No
504	36.61	2.02	0.21	1.81	0.88	0.401	1.36	0.295	0.90	1.00	0.328	No
505	36.70	2.02	0.21	1.81	0.88	0.401	1.36	0.295	0.90	1.00	0.328	No
506	36.78	2.02	0.21	1.81	0.88	0.401	1.36	0.295	0.90	1.00	0.329	No
507	36.85	2.03	0.21	1.82	0.88	0.401	1.36	0.295	0.90	1.00	0.329	No
508	36.87	2.03	0.21	1.82	0.88	0.401	1.36	0.295	0.90	1.00	0.329	No
509	36.91	2.03	0.22	1.82	0.88	0.402	1.36	0.295	0.90	1.00	0.329	No
510	36.97	2.04	0.22	1.82	0.88	0.402	1.36	0.295	0.90	1.00	2.000	Yes
511	37.06	2.04	0.22	1.82	0.88	0.402	1.36	0.295	0.90	1.00	2.000	Yes
512	37.12	2.04	0.22	1.82	0.87	0.402	1.36	0.296	0.90	1.00	2.000	Yes
513	37.20	2.05	0.22	1.82	0.87	0.402	1.36	0.296	0.90	1.00	2.000	Yes
514	37.27	2.05	0.23	1.83	0.87	0.402	1.36	0.296	0.90	1.00	2.000	Yes
515	37.35	2.06	0.23	1.83	0.87	0.402	1.36	0.296	0.90	1.00	2.000	Yes
516	37.44	2.06	0.23	1.83	0.87	0.403	1.36	0.296	0.90	1.00	2.000	Yes
517	37.49	2.07	0.23	1.83	0.87	0.403	1.36	0.296	0.90	1.00	2.000	Yes
518	37.59	2.07	0.24	1.84	0.87	0.403	1.36	0.296	0.90	1.00	2.000	Yes
519	37.64	2.08	0.24	1.84	0.87	0.403	1.36	0.296	0.90	1.00	2.000	Yes
520	37.70	2.08	0.24	1.84	0.87	0.403	1.36	0.296	0.90	1.00	2.000	Yes
521	37.78	2.09	0.24	1.84	0.87	0.403	1.36	0.296	0.89	1.00	2.000	Yes
522	37.83	2.09	0.24	1.84	0.87	0.403	1.36	0.296	0.89	1.00	2.000	Yes
523	37.92	2.09	0.25	1.85	0.87	0.403	1.36	0.297	0.89	1.00	2.000	Yes
524	37.97	2.10	0.25	1.85	0.87	0.403	1.36	0.297	0.89	1.00	2.000	Yes
525	38.07	2.10	0.25	1.85	0.87	0.403	1.36	0.297	0.89	1.00	0.332	No
526	38.14	2.11	0.25	1.85	0.87	0.404	1.36	0.297	0.89	1.00	0.332	No
527	38.22	2.11	0.26	1.86	0.87	0.404	1.36	0.297	0.89	1.00	0.332	No
528	38.31	2.12	0.26	1.86	0.87	0.404	1.36	0.297	0.89	1.00	0.332	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	38.41	2.12	0.26	1.86	0.86	0.404	1.36	0.297	0.89	1.00	0.333	No
530	38.52	2.13	0.27	1.87	0.86	0.404	1.36	0.297	0.89	1.00	0.333	No
531	38.64	2.14	0.27	1.87	0.86	0.404	1.36	0.297	0.89	1.00	0.333	No
532	38.74	2.15	0.27	1.87	0.86	0.404	1.36	0.297	0.89	1.00	0.333	No
533	38.80	2.15	0.27	1.88	0.86	0.404	1.36	0.297	0.89	1.00	0.333	No
534	38.89	2.16	0.28	1.88	0.86	0.404	1.36	0.297	0.89	1.00	0.334	No
535	38.94	2.16	0.28	1.88	0.86	0.405	1.36	0.297	0.89	1.00	0.334	No
536	39.03	2.17	0.28	1.88	0.86	0.405	1.36	0.297	0.89	1.00	0.334	No
537	39.13	2.17	0.28	1.89	0.86	0.405	1.36	0.298	0.89	1.00	0.334	No
538	39.23	2.18	0.29	1.89	0.86	0.405	1.36	0.298	0.89	1.00	0.334	No
539	39.35	2.19	0.29	1.89	0.86	0.405	1.36	0.298	0.89	1.00	0.334	No
540	39.42	2.19	0.29	1.90	0.86	0.405	1.36	0.298	0.89	1.00	0.335	No
541	39.51	2.20	0.30	1.90	0.86	0.405	1.36	0.298	0.89	1.00	0.335	No
542	39.60	2.20	0.30	1.90	0.85	0.405	1.36	0.298	0.89	1.00	0.335	No
543	39.70	2.21	0.30	1.91	0.85	0.405	1.36	0.298	0.89	1.00	0.335	No
544	39.78	2.21	0.31	1.91	0.85	0.405	1.36	0.298	0.89	1.00	0.335	No
545	39.90	2.22	0.31	1.91	0.85	0.405	1.36	0.298	0.89	1.00	0.335	No
546	39.99	2.23	0.31	1.92	0.85	0.405	1.36	0.298	0.89	1.00	0.336	No
547	40.09	2.23	0.31	1.92	0.85	0.405	1.36	0.298	0.89	1.00	2.000	Yes
548	40.18	2.24	0.32	1.92	0.85	0.405	1.36	0.298	0.89	1.00	2.000	Yes
549	40.23	2.24	0.32	1.92	0.85	0.405	1.36	0.298	0.89	1.00	2.000	Yes
550	40.33	2.25	0.32	1.93	0.85	0.405	1.36	0.298	0.89	1.00	2.000	Yes
551	40.43	2.26	0.33	1.93	0.85	0.405	1.36	0.298	0.89	1.00	2.000	Yes
552	40.52	2.26	0.33	1.93	0.85	0.405	1.36	0.298	0.89	1.00	2.000	Yes
553	40.61	2.27	0.33	1.94	0.85	0.405	1.36	0.298	0.89	1.00	2.000	Yes
554	40.69	2.27	0.33	1.94	0.84	0.406	1.36	0.298	0.89	1.00	2.000	Yes
555	40.80	2.28	0.34	1.94	0.84	0.406	1.36	0.298	0.89	1.00	2.000	Yes
556	40.87	2.28	0.34	1.94	0.84	0.406	1.36	0.298	0.89	1.00	2.000	Yes
557	40.95	2.29	0.34	1.95	0.84	0.406	1.36	0.298	0.89	1.00	2.000	Yes
558	40.97	2.29	0.34	1.95	0.84	0.406	1.36	0.298	0.89	1.00	2.000	Yes
559	41.01	2.29	0.34	1.95	0.84	0.406	1.36	0.298	0.89	1.00	2.000	Yes
560	41.07	2.30	0.35	1.95	0.84	0.406	1.36	0.298	0.88	1.00	2.000	Yes
561	41.15	2.30	0.35	1.95	0.84	0.406	1.36	0.298	0.88	1.00	2.000	Yes
562	41.26	2.31	0.35	1.96	0.84	0.406	1.36	0.298	0.88	1.00	0.337	No
563	41.35	2.31	0.35	1.96	0.84	0.406	1.36	0.298	0.88	1.00	0.337	No
564	41.47	2.32	0.36	1.96	0.84	0.406	1.36	0.298	0.88	1.00	0.337	No
565	41.59	2.33	0.36	1.97	0.84	0.406	1.36	0.298	0.88	1.00	0.338	No
566	41.69	2.33	0.36	1.97	0.84	0.406	1.36	0.298	0.88	1.00	0.338	No
567	41.78	2.34	0.37	1.97	0.83	0.406	1.36	0.298	0.88	1.00	0.338	No
568	41.88	2.34	0.37	1.97	0.83	0.406	1.36	0.298	0.88	1.00	0.338	No
569	41.98	2.35	0.37	1.98	0.83	0.406	1.36	0.298	0.88	1.00	0.338	No
570	42.08	2.36	0.38	1.98	0.83	0.406	1.36	0.298	0.88	1.00	0.338	No
571	42.16	2.36	0.38	1.98	0.83	0.406	1.36	0.298	0.88	1.00	0.338	No
572	42.24	2.37	0.38	1.98	0.83	0.406	1.36	0.298	0.88	1.00	0.338	No
573	42.31	2.37	0.38	1.99	0.83	0.406	1.36	0.298	0.88	1.00	0.338	No
574	42.45	2.38	0.39	1.99	0.83	0.406	1.36	0.298	0.88	1.00	0.338	No
575	42.55	2.38	0.39	1.99	0.83	0.405	1.36	0.298	0.88	1.00	0.338	No
576	42.60	2.39	0.39	1.99	0.83	0.405	1.36	0.298	0.88	1.00	0.338	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	42.70	2.39	0.40	2.00	0.83	0.405	1.36	0.298	0.88	1.00	0.338	No
578	42.81	2.40	0.40	2.00	0.83	0.405	1.36	0.298	0.88	1.00	0.339	No
579	42.89	2.41	0.40	2.00	0.82	0.405	1.36	0.298	0.88	1.00	0.339	No
580	42.98	2.41	0.41	2.01	0.82	0.405	1.36	0.298	0.88	1.00	0.339	No
581	43.08	2.42	0.41	2.01	0.82	0.405	1.36	0.298	0.88	1.00	0.339	No
582	43.17	2.42	0.41	2.01	0.82	0.405	1.36	0.298	0.88	1.00	0.339	No
583	43.27	2.43	0.41	2.01	0.82	0.405	1.36	0.298	0.88	1.00	0.339	No
584	43.37	2.43	0.42	2.02	0.82	0.405	1.36	0.298	0.88	1.00	0.339	No
585	43.50	2.44	0.42	2.02	0.82	0.405	1.36	0.298	0.88	1.00	0.339	No
586	43.61	2.45	0.42	2.02	0.82	0.405	1.36	0.298	0.88	1.00	0.339	No
587	43.74	2.46	0.43	2.03	0.82	0.405	1.36	0.298	0.88	1.00	0.339	No
588	43.79	2.46	0.43	2.03	0.82	0.405	1.36	0.298	0.88	1.00	0.339	No
589	43.86	2.46	0.43	2.03	0.81	0.405	1.36	0.298	0.88	1.00	0.339	No
590	43.94	2.47	0.43	2.03	0.81	0.405	1.36	0.298	0.88	1.00	0.339	No
591	44.00	2.47	0.44	2.04	0.81	0.405	1.36	0.298	0.88	1.00	0.339	No
592	44.08	2.48	0.44	2.04	0.81	0.405	1.36	0.297	0.88	1.00	0.339	No
593	44.17	2.48	0.44	2.04	0.81	0.404	1.36	0.297	0.88	1.00	0.339	No
594	44.27	2.49	0.45	2.04	0.81	0.404	1.36	0.297	0.88	1.00	0.339	No
595	44.42	2.50	0.45	2.05	0.81	0.404	1.36	0.297	0.88	1.00	0.339	No
596	44.52	2.50	0.45	2.05	0.81	0.404	1.36	0.297	0.88	1.00	0.339	No
597	44.61	2.51	0.46	2.05	0.81	0.404	1.36	0.297	0.88	1.00	0.339	No
598	44.71	2.51	0.46	2.06	0.81	0.404	1.36	0.297	0.88	1.00	0.339	No
599	44.85	2.52	0.46	2.06	0.81	0.404	1.36	0.297	0.88	1.00	0.339	No
600	44.95	2.53	0.47	2.06	0.80	0.404	1.36	0.297	0.88	1.00	0.339	No
601	45.09	2.54	0.47	2.07	0.80	0.404	1.36	0.297	0.87	1.00	0.339	No
602	45.19	2.54	0.47	2.07	0.80	0.403	1.36	0.297	0.87	1.00	0.339	No
603	45.33	2.55	0.48	2.07	0.80	0.403	1.36	0.297	0.87	1.00	0.339	No
604	45.42	2.56	0.48	2.08	0.80	0.403	1.36	0.296	0.87	1.00	0.339	No
605	45.57	2.57	0.49	2.08	0.80	0.403	1.36	0.296	0.87	1.00	0.339	No
606	45.68	2.57	0.49	2.08	0.80	0.403	1.36	0.296	0.87	1.00	0.339	No
607	45.81	2.58	0.49	2.09	0.80	0.403	1.36	0.296	0.87	1.00	0.339	No
608	45.92	2.59	0.50	2.09	0.79	0.403	1.36	0.296	0.87	1.00	0.339	No
609	46.05	2.59	0.50	2.09	0.79	0.402	1.36	0.296	0.87	1.00	0.339	No
610	46.16	2.60	0.50	2.10	0.79	0.402	1.36	0.296	0.87	1.00	0.339	No
611	46.17	2.60	0.50	2.10	0.79	0.402	1.36	0.296	0.87	1.00	0.339	No
612	46.23	2.60	0.51	2.10	0.79	0.402	1.36	0.296	0.87	1.00	0.339	No
613	46.29	2.61	0.51	2.10	0.79	0.402	1.36	0.296	0.87	1.00	0.339	No
614	46.34	2.61	0.51	2.10	0.79	0.402	1.36	0.296	0.87	1.00	0.339	No
615	46.42	2.62	0.51	2.10	0.79	0.402	1.36	0.296	0.87	1.00	0.339	No
616	46.48	2.62	0.51	2.10	0.79	0.402	1.36	0.295	0.87	1.00	0.339	No
617	46.52	2.62	0.52	2.11	0.79	0.402	1.36	0.295	0.87	1.00	0.339	No
618	46.60	2.63	0.52	2.11	0.79	0.402	1.36	0.295	0.87	1.00	0.339	No
619	46.67	2.63	0.52	2.11	0.79	0.402	1.36	0.295	0.87	1.00	0.339	No
620	46.74	2.63	0.52	2.11	0.79	0.402	1.36	0.295	0.87	1.00	0.339	No
621	46.82	2.64	0.52	2.11	0.79	0.401	1.36	0.295	0.87	1.00	0.339	No
622	46.88	2.64	0.53	2.11	0.78	0.401	1.36	0.295	0.87	1.00	0.339	No
623	46.96	2.64	0.53	2.12	0.78	0.401	1.36	0.295	0.87	1.00	0.339	No
624	47.06	2.65	0.53	2.12	0.78	0.401	1.36	0.295	0.87	1.00	0.339	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	47.15	2.65	0.54	2.12	0.78	0.401	1.36	0.295	0.87	1.00	0.339	No
626	47.24	2.66	0.54	2.12	0.78	0.401	1.36	0.295	0.87	1.00	0.339	No
627	47.35	2.67	0.54	2.12	0.78	0.401	1.36	0.295	0.87	1.00	0.339	No
628	47.49	2.67	0.55	2.13	0.78	0.400	1.36	0.294	0.87	1.00	0.339	No
629	47.58	2.68	0.55	2.13	0.78	0.400	1.36	0.294	0.87	1.00	0.339	No
630	47.73	2.69	0.55	2.13	0.78	0.400	1.36	0.294	0.87	1.00	0.338	No
631	47.83	2.69	0.56	2.14	0.77	0.400	1.36	0.294	0.87	1.00	0.338	No
632	47.87	2.70	0.56	2.14	0.77	0.400	1.36	0.294	0.87	1.00	0.338	No
633	47.89	2.70	0.56	2.14	0.77	0.400	1.36	0.294	0.87	1.00	0.338	No
634	47.94	2.70	0.56	2.14	0.77	0.400	1.36	0.294	0.87	1.00	0.338	No
635	48.02	2.70	0.56	2.14	0.77	0.400	1.36	0.294	0.87	1.00	0.338	No
636	48.07	2.71	0.56	2.14	0.77	0.400	1.36	0.294	0.87	1.00	0.338	No
637	48.12	2.71	0.57	2.14	0.77	0.399	1.36	0.294	0.87	1.00	0.338	No
638	48.18	2.71	0.57	2.15	0.77	0.399	1.36	0.294	0.87	1.00	0.338	No
639	48.26	2.72	0.57	2.15	0.77	0.399	1.36	0.294	0.87	1.00	0.338	No
640	48.31	2.72	0.57	2.15	0.77	0.399	1.36	0.293	0.87	1.00	0.338	No
641	48.38	2.72	0.57	2.15	0.77	0.399	1.36	0.293	0.87	1.00	0.338	No
642	48.46	2.73	0.58	2.15	0.77	0.399	1.36	0.293	0.87	1.00	0.338	No
643	48.52	2.73	0.58	2.16	0.77	0.399	1.36	0.293	0.87	1.00	0.338	No
644	48.60	2.74	0.58	2.16	0.77	0.399	1.36	0.293	0.87	1.00	0.338	No
645	48.68	2.74	0.58	2.16	0.77	0.398	1.36	0.293	0.87	1.00	0.338	No
646	48.74	2.75	0.58	2.16	0.77	0.398	1.36	0.293	0.87	1.00	0.338	No
647	48.82	2.75	0.59	2.16	0.76	0.398	1.36	0.293	0.87	1.00	0.338	No
648	48.89	2.75	0.59	2.16	0.76	0.398	1.36	0.293	0.87	1.00	0.338	No
649	48.99	2.76	0.59	2.17	0.76	0.398	1.36	0.293	0.87	1.00	0.338	No
650	49.05	2.76	0.59	2.17	0.76	0.398	1.36	0.292	0.87	1.00	0.338	No
651	49.12	2.77	0.60	2.17	0.76	0.398	1.36	0.292	0.87	1.00	0.338	No
652	49.18	2.77	0.60	2.17	0.76	0.398	1.36	0.292	0.87	1.00	0.337	No
653	49.27	2.77	0.60	2.17	0.76	0.397	1.36	0.292	0.87	1.00	0.337	No
654	49.32	2.78	0.60	2.17	0.76	0.397	1.36	0.292	0.87	1.00	0.337	No
655	49.42	2.78	0.61	2.18	0.76	0.397	1.36	0.292	0.87	1.00	0.337	No
656	49.48	2.78	0.61	2.18	0.76	0.397	1.36	0.292	0.87	1.00	0.337	No
657	49.56	2.79	0.61	2.18	0.76	0.397	1.36	0.292	0.87	1.00	0.337	No
658	49.66	2.79	0.61	2.18	0.76	0.397	1.36	0.292	0.87	1.00	0.337	No
659	49.76	2.80	0.62	2.18	0.76	0.397	1.36	0.292	0.87	1.00	0.337	No
660	49.85	2.80	0.62	2.19	0.75	0.396	1.36	0.291	0.86	1.00	0.337	No
661	49.99	2.81	0.62	2.19	0.75	0.396	1.36	0.291	0.86	1.00	0.337	No
662	50.09	2.82	0.63	2.19	0.75	0.396	1.36	0.291	0.86	1.00	0.337	No
663	50.21	2.82	0.63	2.19	0.75	0.396	1.36	0.291	0.86	1.00	0.337	No
664	50.24	2.82	0.63	2.19	0.75	0.396	1.36	0.291	0.86	1.00	0.337	No
665	50.29	2.83	0.63	2.19	0.75	0.396	1.36	0.291	0.86	1.00	0.337	No
666	50.38	2.83	0.64	2.20	0.75	0.395	1.36	0.291	0.86	1.00	0.336	No
667	50.47	2.84	0.64	2.20	0.75	0.395	1.36	0.291	0.86	1.00	0.336	No
668	50.52	2.84	0.64	2.20	0.75	0.395	1.36	0.291	0.86	1.00	0.336	No
669	50.62	2.84	0.64	2.20	0.75	0.395	1.36	0.290	0.86	1.00	0.336	No
670	50.66	2.85	0.64	2.20	0.75	0.395	1.36	0.290	0.86	1.00	0.336	No
671	50.76	2.85	0.65	2.20	0.74	0.395	1.36	0.290	0.86	1.00	0.336	No
672	50.83	2.85	0.65	2.21	0.74	0.395	1.36	0.290	0.86	1.00	0.336	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	50.91	2.86	0.65	2.21	0.74	0.394	1.36	0.290	0.86	1.00	0.336	No
674	51.00	2.86	0.66	2.21	0.74	0.394	1.36	0.290	0.86	1.00	0.336	No
675	51.06	2.87	0.66	2.21	0.74	0.394	1.36	0.290	0.86	1.00	0.336	No
676	51.15	2.87	0.66	2.21	0.74	0.394	1.36	0.290	0.86	1.00	0.336	No
677	51.24	2.88	0.66	2.21	0.74	0.394	1.36	0.290	0.86	1.00	0.336	No
678	51.31	2.88	0.67	2.22	0.74	0.394	1.36	0.289	0.86	1.00	0.336	No
679	51.39	2.89	0.67	2.22	0.74	0.393	1.36	0.289	0.86	1.00	0.335	No
680	51.48	2.89	0.67	2.22	0.74	0.393	1.36	0.289	0.86	1.00	0.335	No
681	51.58	2.90	0.67	2.22	0.74	0.393	1.36	0.289	0.86	1.00	0.335	No
682	51.68	2.90	0.68	2.23	0.74	0.393	1.36	0.289	0.86	1.00	0.335	No
683	51.77	2.91	0.68	2.23	0.73	0.393	1.36	0.289	0.86	1.00	0.335	No
684	51.90	2.92	0.68	2.23	0.73	0.392	1.36	0.288	0.86	1.00	0.335	No
685	52.01	2.92	0.69	2.24	0.73	0.392	1.36	0.288	0.86	1.00	2.000	Yes
686	52.11	2.93	0.69	2.24	0.73	0.392	1.36	0.288	0.86	1.00	2.000	Yes
687	52.26	2.94	0.69	2.24	0.73	0.391	1.36	0.288	0.86	1.00	2.000	Yes
688	52.30	2.94	0.70	2.25	0.73	0.391	1.36	0.288	0.86	1.00	2.000	Yes
689	52.33	2.94	0.70	2.25	0.73	0.391	1.36	0.288	0.86	1.00	2.000	Yes
690	52.35	2.95	0.70	2.25	0.73	0.391	1.36	0.288	0.86	1.00	2.000	Yes
691	52.40	2.95	0.70	2.25	0.73	0.391	1.36	0.287	0.86	1.00	2.000	Yes
692	52.45	2.95	0.70	2.25	0.73	0.391	1.36	0.287	0.86	1.00	2.000	Yes
693	52.50	2.96	0.70	2.25	0.73	0.391	1.36	0.287	0.86	1.00	0.334	No
694	52.55	2.96	0.70	2.26	0.73	0.391	1.36	0.287	0.86	1.00	0.334	No
695	52.60	2.96	0.71	2.26	0.73	0.390	1.36	0.287	0.86	1.00	0.334	No
696	52.65	2.97	0.71	2.26	0.73	0.390	1.36	0.287	0.86	1.00	0.334	No
697	52.71	2.97	0.71	2.26	0.73	0.390	1.36	0.287	0.86	1.00	0.334	No
698	52.77	2.97	0.71	2.26	0.72	0.390	1.36	0.287	0.86	1.00	0.334	No
699	52.82	2.98	0.71	2.27	0.72	0.390	1.36	0.287	0.86	1.00	0.334	No
700	52.88	2.98	0.71	2.27	0.72	0.390	1.36	0.287	0.86	1.00	0.334	No
701	52.93	2.99	0.72	2.27	0.72	0.390	1.36	0.286	0.86	1.00	0.334	No
702	52.98	2.99	0.72	2.27	0.72	0.389	1.36	0.286	0.86	1.00	0.334	No
703	53.03	2.99	0.72	2.27	0.72	0.389	1.36	0.286	0.86	1.00	0.334	No
704	53.08	2.99	0.72	2.27	0.72	0.389	1.36	0.286	0.86	1.00	0.333	No
705	53.12	3.00	0.72	2.28	0.72	0.389	1.36	0.286	0.86	1.00	0.333	No
706	53.17	3.00	0.72	2.28	0.72	0.389	1.36	0.286	0.86	1.00	0.333	No
707	53.23	3.01	0.72	2.28	0.72	0.389	1.36	0.286	0.86	1.00	0.333	No
708	53.28	3.01	0.73	2.28	0.72	0.389	1.36	0.286	0.86	1.00	0.333	No
709	53.37	3.01	0.73	2.29	0.72	0.388	1.36	0.286	0.86	1.00	0.333	No
710	53.42	3.02	0.73	2.29	0.72	0.388	1.36	0.285	0.86	1.00	0.333	No
711	53.46	3.02	0.73	2.29	0.72	0.388	1.36	0.285	0.86	1.00	0.333	No
712	53.53	3.03	0.73	2.29	0.72	0.388	1.36	0.285	0.86	1.00	0.333	No
713	53.61	3.03	0.74	2.29	0.72	0.388	1.36	0.285	0.86	1.00	0.333	No
714	53.62	3.03	0.74	2.30	0.72	0.388	1.36	0.285	0.86	1.00	0.333	No
715	53.65	3.03	0.74	2.30	0.72	0.388	1.36	0.285	0.86	1.00	0.333	No
716	53.67	3.04	0.74	2.30	0.72	0.388	1.36	0.285	0.86	1.00	0.333	No
717	53.70	3.04	0.74	2.30	0.72	0.387	1.36	0.285	0.86	1.00	0.333	No
718	53.74	3.04	0.74	2.30	0.72	0.387	1.36	0.285	0.86	1.00	0.333	No
719	53.76	3.04	0.74	2.30	0.72	0.387	1.36	0.285	0.86	1.00	0.333	No
720	53.80	3.04	0.74	2.30	0.71	0.387	1.36	0.285	0.86	1.00	0.333	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	53.84	3.05	0.74	2.30	0.71	0.387	1.36	0.285	0.86	1.00	0.332	No
722	53.90	3.05	0.75	2.31	0.71	0.387	1.36	0.284	0.86	1.00	0.332	No
723	53.91	3.05	0.75	2.31	0.71	0.387	1.36	0.284	0.86	1.00	0.332	No
724	53.95	3.05	0.75	2.31	0.71	0.387	1.36	0.284	0.86	1.00	0.332	No
725	53.96	3.06	0.75	2.31	0.71	0.387	1.36	0.284	0.86	1.00	0.332	No
726	53.98	3.06	0.75	2.31	0.71	0.387	1.36	0.284	0.86	1.00	0.332	No
727	53.99	3.06	0.75	2.31	0.71	0.387	1.36	0.284	0.86	1.00	0.332	No
728	54.01	3.06	0.75	2.31	0.71	0.387	1.36	0.284	0.86	1.00	0.332	No
729	54.02	3.06	0.75	2.31	0.71	0.387	1.36	0.284	0.86	1.00	0.332	No
730	54.03	3.06	0.75	2.31	0.71	0.386	1.36	0.284	0.86	1.00	0.332	No
731	54.04	3.06	0.75	2.31	0.71	0.386	1.36	0.284	0.86	1.00	0.332	No
732	54.05	3.06	0.75	2.31	0.71	0.386	1.36	0.284	0.86	1.00	0.332	No
733	54.09	3.06	0.75	2.31	0.71	0.386	1.36	0.284	0.86	1.00	0.332	No
734	54.10	3.06	0.75	2.31	0.71	0.386	1.36	0.284	0.86	1.00	0.332	No
735	54.13	3.07	0.75	2.31	0.71	0.386	1.36	0.284	0.86	1.00	0.332	No
736	54.14	3.07	0.75	2.31	0.71	0.386	1.36	0.284	0.86	1.00	0.332	No
737	54.19	3.07	0.75	2.32	0.71	0.386	1.36	0.284	0.85	1.00	0.332	No
738	54.19	3.07	0.75	2.32	0.71	0.386	1.36	0.284	0.85	1.00	0.332	No
739	54.24	3.07	0.76	2.32	0.71	0.386	1.36	0.284	0.85	1.00	0.332	No
740	54.29	3.08	0.76	2.32	0.71	0.386	1.36	0.284	0.85	1.00	0.332	No
741	54.33	3.08	0.76	2.32	0.71	0.386	1.36	0.284	0.85	1.00	0.332	No
742	54.38	3.08	0.76	2.32	0.71	0.385	1.36	0.283	0.85	1.00	0.332	No
743	54.39	3.09	0.76	2.32	0.71	0.385	1.36	0.283	0.85	1.00	0.332	No
744	54.43	3.09	0.76	2.33	0.71	0.385	1.36	0.283	0.85	1.00	0.332	No
745	54.48	3.09	0.76	2.33	0.71	0.385	1.36	0.283	0.85	1.00	0.332	No
746	54.52	3.09	0.77	2.33	0.71	0.385	1.36	0.283	0.85	1.00	0.332	No
747	54.58	3.10	0.77	2.33	0.71	0.385	1.36	0.283	0.85	1.00	0.331	No
748	54.62	3.10	0.77	2.33	0.71	0.385	1.36	0.283	0.85	1.00	0.331	No
749	54.65	3.10	0.77	2.33	0.71	0.385	1.36	0.283	0.85	1.00	0.331	No
750	54.67	3.10	0.77	2.33	0.71	0.385	1.36	0.283	0.85	1.00	0.331	No
751	54.71	3.11	0.77	2.34	0.71	0.385	1.36	0.283	0.85	1.00	0.331	No
752	54.77	3.11	0.77	2.34	0.71	0.384	1.36	0.283	0.85	1.00	0.331	No
753	54.81	3.11	0.77	2.34	0.71	0.384	1.36	0.283	0.85	1.00	0.331	No
754	54.85	3.12	0.78	2.34	0.70	0.384	1.36	0.282	0.85	1.00	0.331	No
755	54.86	3.12	0.78	2.34	0.70	0.384	1.36	0.282	0.85	1.00	0.331	No
756	54.87	3.12	0.78	2.34	0.70	0.384	1.36	0.282	0.85	1.00	0.331	No
757	54.91	3.12	0.78	2.34	0.70	0.384	1.36	0.282	0.85	1.00	0.331	No
758	54.96	3.12	0.78	2.34	0.70	0.384	1.36	0.282	0.85	1.00	0.331	No
759	55.00	3.13	0.78	2.35	0.70	0.384	1.36	0.282	0.85	1.00	0.331	No
760	55.01	3.13	0.78	2.35	0.70	0.384	1.36	0.282	0.85	1.00	0.331	No
761	55.05	3.13	0.78	2.35	0.70	0.384	1.36	0.282	0.85	1.00	0.331	No
762	55.10	3.13	0.78	2.35	0.70	0.384	1.36	0.282	0.85	1.00	0.331	No
763	55.12	3.13	0.78	2.35	0.70	0.383	1.36	0.282	0.85	1.00	0.331	No
764	55.13	3.13	0.78	2.35	0.70	0.383	1.36	0.282	0.85	1.00	0.331	No
765	55.14	3.14	0.78	2.35	0.70	0.383	1.36	0.282	0.85	1.00	0.331	No
766	55.19	3.14	0.79	2.35	0.70	0.383	1.36	0.282	0.85	1.00	0.331	No
767	55.20	3.14	0.79	2.35	0.70	0.383	1.36	0.282	0.85	1.00	0.331	No
768	55.25	3.14	0.79	2.35	0.70	0.383	1.36	0.282	0.85	1.00	0.331	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	55.29	3.14	0.79	2.36	0.70	0.383	1.36	0.282	0.85	1.00	0.330	No
770	55.33	3.15	0.79	2.36	0.70	0.383	1.36	0.281	0.85	1.00	0.330	No
771	55.38	3.15	0.79	2.36	0.70	0.383	1.36	0.281	0.85	1.00	0.330	No
772	55.48	3.16	0.80	2.36	0.70	0.382	1.36	0.281	0.85	1.00	0.330	No
773	55.57	3.16	0.80	2.37	0.70	0.382	1.36	0.281	0.85	1.00	0.330	No
774	55.63	3.17	0.80	2.37	0.70	0.382	1.36	0.281	0.85	1.00	0.330	No
775	55.72	3.17	0.80	2.37	0.70	0.382	1.36	0.281	0.85	1.00	0.330	No
776	55.80	3.18	0.80	2.37	0.70	0.382	1.36	0.281	0.85	1.00	0.330	No
777	55.86	3.18	0.81	2.38	0.70	0.381	1.36	0.280	0.85	1.00	0.330	No
778	55.97	3.19	0.81	2.38	0.69	0.381	1.36	0.280	0.85	1.00	0.330	No
779	56.01	3.19	0.81	2.38	0.69	0.381	1.36	0.280	0.85	1.00	0.329	No
780	56.06	3.20	0.81	2.38	0.69	0.381	1.36	0.280	0.85	1.00	0.329	No
781	56.11	3.20	0.81	2.39	0.69	0.381	1.36	0.280	0.85	1.00	0.329	No
782	56.15	3.20	0.82	2.39	0.69	0.381	1.36	0.280	0.85	1.00	0.329	No
783	56.20	3.21	0.82	2.39	0.69	0.380	1.36	0.280	0.85	1.00	0.329	No
784	56.27	3.21	0.82	2.39	0.69	0.380	1.36	0.280	0.85	1.00	0.329	No
785	56.27	3.21	0.82	2.39	0.69	0.380	1.36	0.280	0.85	1.00	0.329	No
786	56.30	3.21	0.82	2.39	0.69	0.380	1.36	0.279	0.85	1.00	0.329	No
787	56.33	3.22	0.82	2.39	0.69	0.380	1.36	0.279	0.85	1.00	0.329	No
788	56.35	3.22	0.82	2.39	0.69	0.380	1.36	0.279	0.85	1.00	0.329	No
789	56.40	3.22	0.82	2.40	0.69	0.380	1.36	0.279	0.85	1.00	0.329	No
790	56.41	3.22	0.82	2.40	0.69	0.380	1.36	0.279	0.85	1.00	0.329	No
791	56.44	3.22	0.83	2.40	0.69	0.380	1.36	0.279	0.85	1.00	0.329	No
792	56.49	3.23	0.83	2.40	0.69	0.380	1.36	0.279	0.85	1.00	0.329	No
793	56.54	3.23	0.83	2.40	0.69	0.379	1.36	0.279	0.85	1.00	0.329	No
794	56.58	3.23	0.83	2.40	0.69	0.379	1.36	0.279	0.85	1.00	0.329	No
795	56.59	3.23	0.83	2.40	0.69	0.379	1.36	0.279	0.85	1.00	0.329	No
796	56.64	3.24	0.83	2.41	0.69	0.379	1.36	0.279	0.85	1.00	0.329	No
797	56.69	3.24	0.83	2.41	0.69	0.379	1.36	0.279	0.85	1.00	0.328	No
798	56.73	3.24	0.83	2.41	0.69	0.379	1.36	0.279	0.85	1.00	0.328	No
799	56.78	3.25	0.84	2.41	0.69	0.379	1.36	0.278	0.85	1.00	0.328	No
800	56.83	3.25	0.84	2.41	0.69	0.379	1.36	0.278	0.85	1.00	0.328	No
801	56.88	3.25	0.84	2.41	0.69	0.378	1.36	0.278	0.85	1.00	0.328	No
802	56.89	3.25	0.84	2.42	0.69	0.378	1.36	0.278	0.85	1.00	0.328	No
803	56.95	3.26	0.84	2.42	0.69	0.378	1.36	0.278	0.85	1.00	0.328	No
804	57.01	3.26	0.84	2.42	0.68	0.378	1.36	0.278	0.85	1.00	0.328	No
805	57.07	3.27	0.84	2.42	0.68	0.378	1.36	0.278	0.85	1.00	0.328	No
806	57.11	3.27	0.85	2.42	0.68	0.378	1.36	0.278	0.85	1.00	0.328	No
807	57.17	3.27	0.85	2.43	0.68	0.378	1.36	0.278	0.85	1.00	0.328	No
808	57.26	3.28	0.85	2.43	0.68	0.377	1.36	0.277	0.85	1.00	0.328	No
809	57.31	3.28	0.85	2.43	0.68	0.377	1.36	0.277	0.85	1.00	0.328	No
810	57.37	3.29	0.85	2.43	0.68	0.377	1.36	0.277	0.85	1.00	0.327	No
811	57.45	3.29	0.86	2.43	0.68	0.377	1.36	0.277	0.85	1.00	0.327	No
812	57.51	3.30	0.86	2.44	0.68	0.377	1.36	0.277	0.85	1.00	0.327	No
813	57.53	3.30	0.86	2.44	0.68	0.377	1.36	0.277	0.85	1.00	0.327	No
814	57.59	3.30	0.86	2.44	0.68	0.377	1.36	0.277	0.85	1.00	0.327	No
815	57.63	3.30	0.86	2.44	0.68	0.376	1.36	0.277	0.85	1.00	0.327	No
816	57.68	3.31	0.86	2.44	0.68	0.376	1.36	0.277	0.85	1.00	0.327	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
817	57.73	3.31	0.87	2.44	0.68	0.376	1.36	0.277	0.85	1.00	0.327	No
818	57.78	3.31	0.87	2.45	0.68	0.376	1.36	0.276	0.85	1.00	0.327	No
819	57.86	3.32	0.87	2.45	0.68	0.376	1.36	0.276	0.85	1.00	0.327	No
820	57.92	3.32	0.87	2.45	0.68	0.376	1.36	0.276	0.85	1.00	2.000	Yes
821	57.98	3.33	0.87	2.45	0.68	0.376	1.36	0.276	0.85	1.00	2.000	Yes
822	58.06	3.33	0.88	2.45	0.68	0.375	1.36	0.276	0.85	1.00	2.000	Yes
823	58.12	3.33	0.88	2.46	0.68	0.375	1.36	0.276	0.84	1.00	2.000	Yes
824	58.21	3.34	0.88	2.46	0.67	0.375	1.36	0.276	0.84	1.00	2.000	Yes
825	58.26	3.34	0.88	2.46	0.67	0.375	1.36	0.276	0.84	1.00	2.000	Yes
826	58.35	3.35	0.88	2.46	0.67	0.375	1.36	0.275	0.84	1.00	2.000	Yes
827	58.41	3.35	0.89	2.47	0.67	0.374	1.36	0.275	0.84	1.00	2.000	Yes
828	58.50	3.36	0.89	2.47	0.67	0.374	1.36	0.275	0.84	1.00	2.000	Yes
829	58.56	3.36	0.89	2.47	0.67	0.374	1.36	0.275	0.84	1.00	2.000	Yes
830	58.64	3.37	0.89	2.47	0.67	0.374	1.36	0.275	0.84	1.00	2.000	Yes
831	58.73	3.37	0.90	2.48	0.67	0.374	1.36	0.275	0.84	1.00	2.000	Yes
832	58.80	3.38	0.90	2.48	0.67	0.373	1.36	0.275	0.84	1.00	2.000	Yes
833	58.84	3.38	0.90	2.48	0.67	0.373	1.36	0.274	0.84	1.00	2.000	Yes
834	58.85	3.38	0.90	2.48	0.67	0.373	1.36	0.274	0.84	1.00	0.325	No
835	58.93	3.38	0.90	2.48	0.67	0.373	1.36	0.274	0.84	1.00	0.325	No
836	58.98	3.39	0.90	2.48	0.67	0.373	1.36	0.274	0.84	1.00	0.325	No
837	59.02	3.39	0.91	2.48	0.67	0.373	1.36	0.274	0.84	1.00	0.325	No
838	59.12	3.40	0.91	2.49	0.67	0.373	1.36	0.274	0.84	1.00	0.325	No
839	59.17	3.40	0.91	2.49	0.67	0.373	1.36	0.274	0.84	1.00	0.325	No
840	59.27	3.40	0.91	2.49	0.67	0.372	1.36	0.274	0.84	1.00	0.325	No
841	59.31	3.41	0.91	2.49	0.66	0.372	1.36	0.274	0.84	1.00	0.325	No
842	59.41	3.41	0.92	2.50	0.66	0.372	1.36	0.273	0.84	1.00	0.325	No
843	59.46	3.42	0.92	2.50	0.66	0.372	1.36	0.273	0.84	1.00	0.325	No
844	59.55	3.42	0.92	2.50	0.66	0.372	1.36	0.273	0.84	1.00	0.324	No
845	59.65	3.43	0.93	2.50	0.66	0.371	1.36	0.273	0.84	1.00	0.324	No
846	59.70	3.43	0.93	2.50	0.66	0.371	1.36	0.273	0.84	1.00	0.324	No
847	59.80	3.44	0.93	2.51	0.66	0.371	1.36	0.273	0.84	1.00	0.324	No
848	59.89	3.44	0.93	2.51	0.66	0.371	1.36	0.273	0.84	1.00	0.324	No
849	59.94	3.44	0.93	2.51	0.66	0.371	1.36	0.273	0.84	1.00	0.324	No
850	60.01	3.45	0.94	2.51	0.66	0.371	1.36	0.272	0.84	1.00	0.324	No
851	60.02	3.45	0.94	2.51	0.66	0.370	1.36	0.272	0.84	1.00	0.324	No
852	60.08	3.45	0.94	2.51	0.66	0.370	1.36	0.272	0.84	1.00	0.324	No
853	60.12	3.46	0.94	2.52	0.66	0.370	1.36	0.272	0.84	1.00	0.324	No
854	60.17	3.46	0.94	2.52	0.66	0.370	1.36	0.272	0.84	1.00	0.324	No
855	60.27	3.46	0.94	2.52	0.66	0.370	1.36	0.272	0.84	1.00	0.324	No
856	60.31	3.47	0.95	2.52	0.66	0.370	1.36	0.272	0.84	1.00	0.323	No
857	60.37	3.47	0.95	2.52	0.66	0.370	1.36	0.272	0.84	1.00	0.323	No
858	60.46	3.47	0.95	2.52	0.66	0.369	1.36	0.272	0.84	1.00	0.323	No
859	60.51	3.48	0.95	2.53	0.66	0.369	1.36	0.272	0.84	1.00	0.323	No
860	60.61	3.48	0.95	2.53	0.65	0.369	1.36	0.271	0.84	1.00	0.323	No
861	60.65	3.49	0.96	2.53	0.65	0.369	1.36	0.271	0.84	1.00	0.323	No
862	60.75	3.49	0.96	2.53	0.65	0.369	1.36	0.271	0.84	1.00	0.323	No
863	60.81	3.49	0.96	2.53	0.65	0.369	1.36	0.271	0.84	1.00	0.323	No
864	60.89	3.50	0.96	2.53	0.65	0.369	1.36	0.271	0.84	1.00	0.323	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
865	60.94	3.50	0.97	2.54	0.65	0.368	1.36	0.271	0.84	1.00	0.323	No
866	61.03	3.51	0.97	2.54	0.65	0.368	1.36	0.271	0.84	1.00	0.323	No
867	61.09	3.51	0.97	2.54	0.65	0.368	1.36	0.271	0.84	1.00	0.322	No
868	61.19	3.51	0.97	2.54	0.65	0.368	1.36	0.271	0.84	1.00	0.322	No
869	61.24	3.52	0.97	2.54	0.65	0.368	1.36	0.270	0.84	1.00	0.322	No
870	61.33	3.52	0.98	2.54	0.65	0.368	1.36	0.270	0.84	1.00	0.322	No
871	61.38	3.52	0.98	2.55	0.65	0.368	1.36	0.270	0.84	1.00	0.322	No
872	61.47	3.53	0.98	2.55	0.65	0.367	1.36	0.270	0.84	1.00	0.322	No
873	61.53	3.53	0.98	2.55	0.65	0.367	1.36	0.270	0.84	1.00	0.322	No
874	61.62	3.54	0.99	2.55	0.65	0.367	1.36	0.270	0.84	1.00	0.322	No
875	61.70	3.54	0.99	2.55	0.65	0.367	1.36	0.270	0.84	1.00	0.322	No
876	61.77	3.55	0.99	2.56	0.65	0.367	1.36	0.270	0.84	1.00	0.322	No
877	61.86	3.55	0.99	2.56	0.64	0.366	1.36	0.269	0.84	1.00	0.322	No
878	61.95	3.56	1.00	2.56	0.64	0.366	1.36	0.269	0.84	1.00	0.321	No
879	61.97	3.56	1.00	2.56	0.64	0.366	1.36	0.269	0.84	1.00	0.321	No
880	62.01	3.56	1.00	2.56	0.64	0.366	1.36	0.269	0.84	1.00	2.000	No
881	62.10	3.57	1.00	2.57	0.64	0.366	1.36	0.269	0.84	1.00	2.000	Yes
882	62.24	3.58	1.01	2.57	0.64	0.366	1.36	0.269	0.84	1.00	2.000	Yes
883	62.34	3.58	1.01	2.57	0.64	0.365	1.36	0.269	0.84	1.00	2.000	Yes
884	62.49	3.59	1.01	2.58	0.64	0.365	1.36	0.268	0.84	1.00	2.000	Yes
885	62.54	3.60	1.02	2.58	0.64	0.365	1.36	0.268	0.84	1.00	2.000	Yes
886	62.66	3.60	1.02	2.58	0.64	0.365	1.36	0.268	0.84	1.00	2.000	Yes
887	62.74	3.61	1.02	2.59	0.64	0.364	1.36	0.268	0.84	1.00	2.000	Yes
888	62.87	3.62	1.03	2.59	0.64	0.364	1.36	0.268	0.84	1.00	2.000	No
889	62.92	3.62	1.03	2.59	0.64	0.364	1.36	0.268	0.84	1.00	2.000	No
890	63.03	3.63	1.03	2.60	0.64	0.364	1.36	0.267	0.84	1.00	2.000	No
891	63.15	3.63	1.03	2.60	0.63	0.363	1.36	0.267	0.84	1.00	2.000	No
892	63.26	3.64	1.04	2.60	0.63	0.363	1.36	0.267	0.84	1.00	2.000	No
893	63.37	3.65	1.04	2.61	0.63	0.363	1.36	0.267	0.83	1.00	2.000	No
894	63.45	3.65	1.04	2.61	0.63	0.363	1.36	0.267	0.83	1.00	2.000	No
895	63.54	3.66	1.05	2.61	0.63	0.363	1.36	0.267	0.83	1.00	2.000	No
896	63.61	3.66	1.05	2.61	0.63	0.362	1.36	0.266	0.83	1.00	2.000	Yes
897	63.69	3.67	1.05	2.62	0.63	0.362	1.36	0.266	0.83	1.00	2.000	Yes
898	63.79	3.67	1.05	2.62	0.63	0.362	1.36	0.266	0.83	1.00	2.000	Yes
899	63.89	3.68	1.06	2.62	0.63	0.362	1.36	0.266	0.83	1.00	2.000	Yes
900	63.98	3.69	1.06	2.63	0.63	0.362	1.36	0.266	0.83	1.00	2.000	Yes
901	64.07	3.69	1.06	2.63	0.63	0.361	1.36	0.266	0.83	1.00	2.000	Yes
902	64.15	3.70	1.07	2.63	0.63	0.361	1.36	0.266	0.83	1.00	2.000	Yes
903	64.23	3.70	1.07	2.63	0.63	0.361	1.36	0.266	0.83	1.00	2.000	No
904	64.26	3.70	1.07	2.63	0.63	0.361	1.36	0.265	0.83	1.00	2.000	No
905	64.29	3.70	1.07	2.63	0.63	0.361	1.36	0.265	0.83	1.00	2.000	No
906	64.33	3.71	1.07	2.64	0.63	0.361	1.36	0.265	0.83	1.00	2.000	No
907	64.43	3.71	1.07	2.64	0.63	0.361	1.36	0.265	0.83	1.00	2.000	No
908	64.47	3.71	1.08	2.64	0.63	0.361	1.36	0.265	0.83	1.00	2.000	No
909	64.53	3.72	1.08	2.64	0.63	0.361	1.36	0.265	0.83	1.00	2.000	No
910	64.62	3.72	1.08	2.64	0.62	0.360	1.36	0.265	0.83	1.00	2.000	No
911	64.72	3.73	1.08	2.64	0.62	0.360	1.36	0.265	0.83	1.00	2.000	No
912	64.78	3.73	1.09	2.65	0.62	0.360	1.36	0.265	0.83	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
913	64.86	3.74	1.09	2.65	0.62	0.360	1.36	0.265	0.83	1.00	2.000	No
914	64.96	3.74	1.09	2.65	0.62	0.360	1.36	0.264	0.83	1.00	2.000	No
915	65.06	3.75	1.09	2.65	0.62	0.360	1.36	0.264	0.83	1.00	2.000	No
916	65.11	3.75	1.10	2.65	0.62	0.359	1.36	0.264	0.83	1.00	2.000	No
917	65.21	3.76	1.10	2.66	0.62	0.359	1.36	0.264	0.83	1.00	2.000	No
918	65.31	3.76	1.10	2.66	0.62	0.359	1.36	0.264	0.83	1.00	2.000	No
919	65.40	3.77	1.10	2.66	0.62	0.359	1.36	0.264	0.83	1.00	2.000	No
920	65.50	3.77	1.11	2.66	0.62	0.359	1.36	0.264	0.83	1.00	2.000	No
921	65.58	3.78	1.11	2.67	0.62	0.359	1.36	0.264	0.83	1.00	2.000	No
922	65.68	3.78	1.11	2.67	0.62	0.358	1.36	0.264	0.83	1.00	2.000	No
923	65.78	3.79	1.12	2.67	0.62	0.358	1.36	0.263	0.83	1.00	2.000	No
924	65.84	3.79	1.12	2.67	0.62	0.358	1.36	0.263	0.83	1.00	2.000	No
925	65.86	3.79	1.12	2.67	0.62	0.358	1.36	0.263	0.83	1.00	2.000	No
926	65.87	3.79	1.12	2.67	0.62	0.358	1.36	0.263	0.83	1.00	2.000	No
927	65.98	3.80	1.12	2.68	0.62	0.358	1.36	0.263	0.83	1.00	2.000	No
928	66.10	3.80	1.13	2.68	0.61	0.358	1.36	0.263	0.83	1.00	2.000	No
929	66.21	3.81	1.13	2.68	0.61	0.357	1.36	0.263	0.83	1.00	2.000	No
930	66.34	3.82	1.13	2.68	0.61	0.357	1.36	0.263	0.83	1.00	2.000	No
931	66.48	3.83	1.14	2.69	0.61	0.357	1.36	0.262	0.83	1.00	2.000	No
932	66.62	3.83	1.14	2.69	0.61	0.357	1.36	0.262	0.83	1.00	2.000	No
933	66.68	3.84	1.14	2.69	0.61	0.357	1.36	0.262	0.83	1.00	2.000	No
934	66.87	3.85	1.15	2.70	0.61	0.356	1.36	0.262	0.83	1.00	2.000	No
935	66.96	3.85	1.15	2.70	0.61	0.356	1.36	0.262	0.83	1.00	2.000	No
936	67.11	3.86	1.16	2.70	0.61	0.356	1.36	0.262	0.83	1.00	2.000	No
937	67.21	3.87	1.16	2.71	0.61	0.356	1.36	0.262	0.83	1.00	2.000	No
938	67.35	3.87	1.17	2.71	0.61	0.356	1.36	0.261	0.83	1.00	2.000	No
939	67.45	3.88	1.17	2.71	0.61	0.355	1.36	0.261	0.83	1.00	2.000	No
940	67.59	3.89	1.17	2.72	0.61	0.355	1.36	0.261	0.83	1.00	2.000	No
941	67.68	3.89	1.18	2.72	0.61	0.355	1.36	0.261	0.83	1.00	2.000	Yes
942	67.83	3.90	1.18	2.72	0.60	0.355	1.36	0.261	0.83	1.00	2.000	Yes
943	67.92	3.91	1.18	2.73	0.60	0.354	1.36	0.261	0.83	1.00	2.000	Yes
944	68.02	3.92	1.19	2.73	0.60	0.354	1.36	0.260	0.83	1.00	2.000	Yes
945	68.07	3.92	1.19	2.73	0.60	0.354	1.36	0.260	0.83	1.00	2.000	Yes
946	68.16	3.93	1.19	2.73	0.60	0.354	1.36	0.260	0.83	1.00	2.000	No
947	68.26	3.93	1.19	2.74	0.60	0.354	1.36	0.260	0.83	1.00	2.000	No
948	68.35	3.94	1.20	2.74	0.60	0.354	1.36	0.260	0.83	1.00	2.000	No
949	68.45	3.94	1.20	2.74	0.60	0.353	1.36	0.260	0.83	1.00	2.000	No
950	68.55	3.95	1.20	2.75	0.60	0.353	1.36	0.260	0.83	1.00	2.000	No
951	68.65	3.96	1.21	2.75	0.60	0.353	1.36	0.260	0.83	1.00	2.000	No
952	68.78	3.97	1.21	2.76	0.60	0.353	1.36	0.259	0.83	1.00	2.000	No
953	68.78	3.97	1.21	2.76	0.60	0.353	1.36	0.259	0.83	1.00	2.000	No
954	68.79	3.97	1.21	2.76	0.60	0.353	1.36	0.259	0.83	1.00	2.000	No
955	68.83	3.97	1.21	2.76	0.60	0.353	1.36	0.259	0.83	1.00	2.000	No
956	68.93	3.98	1.21	2.76	0.60	0.353	1.36	0.259	0.83	1.00	2.000	No
957	68.98	3.98	1.22	2.76	0.60	0.352	1.36	0.259	0.83	1.00	2.000	No
958	69.04	3.98	1.22	2.76	0.60	0.352	1.36	0.259	0.83	1.00	2.000	No
959	69.12	3.99	1.22	2.77	0.60	0.352	1.36	0.259	0.83	1.00	2.000	No
960	69.22	3.99	1.22	2.77	0.60	0.352	1.36	0.259	0.82	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
961	69.28	4.00	1.23	2.77	0.60	0.352	1.36	0.259	0.82	1.00	2.000	No
962	69.36	4.00	1.23	2.77	0.60	0.352	1.36	0.259	0.82	1.00	2.000	No
963	69.45	4.01	1.23	2.78	0.59	0.352	1.36	0.258	0.82	1.00	2.000	No
964	69.60	4.02	1.24	2.78	0.59	0.351	1.36	0.258	0.82	1.00	2.000	No
965	69.70	4.02	1.24	2.79	0.59	0.351	1.36	0.258	0.82	1.00	2.000	No
966	69.80	4.03	1.24	2.79	0.59	0.351	1.36	0.258	0.82	1.00	2.000	No
967	69.89	4.04	1.24	2.79	0.59	0.351	1.36	0.258	0.82	1.00	2.000	No
968	69.98	4.04	1.25	2.79	0.59	0.351	1.36	0.258	0.82	1.00	2.000	No
969	70.08	4.05	1.25	2.80	0.59	0.350	1.36	0.258	0.82	1.00	2.000	Yes
970	70.18	4.05	1.25	2.80	0.59	0.350	1.36	0.258	0.82	1.00	2.000	Yes
971	70.32	4.06	1.26	2.80	0.59	0.350	1.36	0.257	0.82	1.00	2.000	Yes
972	70.42	4.07	1.26	2.81	0.59	0.350	1.36	0.257	0.82	1.00	2.000	Yes
973	70.54	4.08	1.26	2.81	0.59	0.350	1.36	0.257	0.82	1.00	2.000	Yes
974	70.66	4.08	1.27	2.81	0.59	0.350	1.36	0.257	0.82	1.00	2.000	No
975	70.75	4.09	1.27	2.82	0.59	0.349	1.36	0.257	0.82	1.00	2.000	No
976	70.80	4.09	1.27	2.82	0.59	0.349	1.36	0.257	0.82	1.00	2.000	No
977	70.89	4.10	1.28	2.82	0.59	0.349	1.36	0.257	0.82	1.00	2.000	No
978	70.99	4.10	1.28	2.82	0.59	0.349	1.36	0.257	0.82	1.00	2.000	No
979	71.08	4.11	1.28	2.82	0.59	0.349	1.36	0.257	0.82	1.00	2.000	No
980	71.17	4.11	1.28	2.83	0.59	0.349	1.36	0.257	0.82	1.00	2.000	No
981	71.23	4.11	1.29	2.83	0.59	0.349	1.36	0.256	0.82	1.00	2.000	No
982	71.33	4.12	1.29	2.83	0.58	0.349	1.36	0.256	0.82	1.00	2.000	No
983	71.42	4.12	1.29	2.83	0.58	0.349	1.36	0.256	0.82	1.00	2.000	No
984	71.52	4.13	1.30	2.83	0.58	0.348	1.36	0.256	0.82	1.00	2.000	No
985	71.58	4.13	1.30	2.83	0.58	0.348	1.36	0.256	0.82	1.00	2.000	No
986	71.67	4.14	1.30	2.84	0.58	0.348	1.36	0.256	0.82	1.00	2.000	No
987	71.81	4.14	1.30	2.84	0.58	0.348	1.36	0.256	0.82	1.00	2.000	No
988	71.82	4.14	1.30	2.84	0.58	0.348	1.36	0.256	0.82	1.00	2.000	No
989	71.86	4.15	1.31	2.84	0.58	0.348	1.36	0.256	0.82	1.00	2.000	No
990	71.91	4.15	1.31	2.84	0.58	0.348	1.36	0.256	0.82	1.00	2.000	No
991	71.97	4.15	1.31	2.84	0.58	0.348	1.36	0.256	0.82	1.00	2.000	No
992	72.05	4.16	1.31	2.85	0.58	0.348	1.36	0.256	0.82	1.00	2.000	No
993	72.10	4.16	1.31	2.85	0.58	0.348	1.36	0.256	0.82	1.00	2.000	No
994	72.20	4.17	1.32	2.85	0.58	0.348	1.36	0.256	0.82	1.00	2.000	No
995	72.25	4.17	1.32	2.85	0.58	0.348	1.36	0.256	0.82	1.00	2.000	No
996	72.34	4.17	1.32	2.85	0.58	0.347	1.36	0.255	0.82	1.00	2.000	No
997	72.44	4.18	1.32	2.85	0.58	0.347	1.36	0.255	0.82	1.00	2.000	No
998	72.53	4.18	1.33	2.86	0.58	0.347	1.36	0.255	0.82	1.00	2.000	No
999	72.63	4.19	1.33	2.86	0.58	0.347	1.36	0.255	0.82	1.00	2.000	No
1000	72.69	4.19	1.33	2.86	0.58	0.347	1.36	0.255	0.82	1.00	2.000	No
1001	72.82	4.20	1.34	2.86	0.58	0.347	1.36	0.255	0.82	1.00	2.000	No
1002	72.92	4.20	1.34	2.87	0.58	0.347	1.36	0.255	0.82	1.00	2.000	No
1003	73.06	4.21	1.34	2.87	0.58	0.347	1.36	0.255	0.82	1.00	2.000	No
1004	73.16	4.22	1.35	2.87	0.58	0.346	1.36	0.255	0.82	1.00	2.000	No
1005	73.30	4.23	1.35	2.87	0.58	0.346	1.36	0.255	0.82	1.00	2.000	No
1006	73.35	4.23	1.35	2.88	0.58	0.346	1.36	0.255	0.82	1.00	2.000	No
1007	73.38	4.23	1.35	2.88	0.57	0.346	1.36	0.255	0.82	1.00	2.000	No
1008	73.47	4.24	1.36	2.88	0.57	0.346	1.36	0.254	0.82	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1009	73.53	4.24	1.36	2.88	0.57	0.346	1.36	0.254	0.82	1.00	2.000	No
1010	73.62	4.24	1.36	2.88	0.57	0.346	1.36	0.254	0.82	1.00	2.000	No
1011	73.71	4.25	1.36	2.88	0.57	0.346	1.36	0.254	0.82	1.00	2.000	No
1012	73.77	4.25	1.37	2.89	0.57	0.346	1.36	0.254	0.82	1.00	2.000	No
1013	73.86	4.26	1.37	2.89	0.57	0.346	1.36	0.254	0.82	1.00	2.000	No
1014	73.96	4.26	1.37	2.89	0.57	0.346	1.36	0.254	0.82	1.00	2.000	No
1015	74.06	4.27	1.37	2.89	0.57	0.345	1.36	0.254	0.82	1.00	2.000	No
1016	74.13	4.27	1.38	2.90	0.57	0.345	1.36	0.254	0.82	1.00	2.000	No
1017	74.24	4.28	1.38	2.90	0.57	0.345	1.36	0.254	0.82	1.00	2.000	No
1018	74.34	4.28	1.38	2.90	0.57	0.345	1.36	0.254	0.82	1.00	2.000	No
1019	74.44	4.29	1.39	2.90	0.57	0.345	1.36	0.254	0.82	1.00	2.000	No
1020	74.58	4.30	1.39	2.91	0.57	0.345	1.36	0.254	0.82	1.00	2.000	No
1021	74.68	4.30	1.39	2.91	0.57	0.345	1.36	0.253	0.82	1.00	2.000	No
1022	74.80	4.31	1.40	2.91	0.57	0.345	1.36	0.253	0.82	1.00	2.000	No
1023	74.92	4.32	1.40	2.91	0.57	0.344	1.36	0.253	0.82	1.00	2.000	No
1024	75.07	4.32	1.41	2.92	0.57	0.344	1.36	0.253	0.82	1.00	2.000	No
1025	75.08	4.32	1.41	2.92	0.57	0.344	1.36	0.253	0.82	1.00	2.000	No
1026	75.11	4.33	1.41	2.92	0.57	0.344	1.36	0.253	0.82	1.00	2.000	No
1027	75.16	4.33	1.41	2.92	0.57	0.344	1.36	0.253	0.82	1.00	2.000	No
1028	75.25	4.33	1.41	2.92	0.57	0.344	1.36	0.253	0.82	1.00	2.000	No
1029	75.32	4.34	1.41	2.92	0.57	0.344	1.36	0.253	0.82	1.00	2.000	No
1030	75.40	4.34	1.42	2.93	0.57	0.344	1.36	0.253	0.82	1.00	2.000	No
1031	75.50	4.35	1.42	2.93	0.57	0.344	1.36	0.253	0.82	1.00	2.000	No
1032	75.59	4.35	1.42	2.93	0.57	0.344	1.36	0.253	0.82	1.00	2.000	No
1033	75.69	4.36	1.43	2.93	0.56	0.344	1.36	0.253	0.82	1.00	2.000	No
1034	75.78	4.36	1.43	2.93	0.56	0.344	1.36	0.253	0.82	1.00	2.000	No
1035	75.88	4.37	1.43	2.94	0.56	0.343	1.36	0.253	0.82	1.00	2.000	No
1036	75.96	4.37	1.43	2.94	0.56	0.343	1.36	0.252	0.82	1.00	2.000	No
1037	76.05	4.38	1.44	2.94	0.56	0.343	1.36	0.252	0.82	1.00	2.000	No
1038	76.14	4.38	1.44	2.94	0.56	0.343	1.36	0.252	0.81	1.00	2.000	No
1039	76.26	4.39	1.44	2.95	0.56	0.343	1.36	0.252	0.81	1.00	2.000	No
1040	76.36	4.39	1.45	2.95	0.56	0.343	1.36	0.252	0.81	1.00	2.000	No
1041	76.41	4.40	1.45	2.95	0.56	0.343	1.36	0.252	0.81	1.00	2.000	No
1042	76.51	4.40	1.45	2.95	0.56	0.343	1.36	0.252	0.81	1.00	2.000	No
1043	76.65	4.41	1.46	2.95	0.56	0.343	1.36	0.252	0.81	1.00	2.000	No
1044	76.72	4.41	1.46	2.96	0.56	0.343	1.36	0.252	0.81	1.00	2.000	No
1045	76.79	4.42	1.46	2.96	0.56	0.343	1.36	0.252	0.81	1.00	2.000	No
1046	76.89	4.42	1.46	2.96	0.56	0.343	1.36	0.252	0.81	1.00	2.000	No
1047	76.98	4.43	1.47	2.96	0.56	0.342	1.36	0.252	0.81	1.00	2.000	No
1048	77.08	4.43	1.47	2.96	0.56	0.342	1.36	0.252	0.81	1.00	2.000	No
1049	77.18	4.44	1.47	2.97	0.56	0.342	1.36	0.252	0.81	1.00	2.000	No
1050	77.28	4.44	1.48	2.97	0.56	0.342	1.36	0.252	0.81	1.00	2.000	No
1051	77.37	4.45	1.48	2.97	0.56	0.342	1.36	0.252	0.81	1.00	2.000	No
1052	77.42	4.45	1.48	2.97	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1053	77.42	4.45	1.48	2.97	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1054	77.44	4.45	1.48	2.97	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1055	77.48	4.46	1.48	2.98	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1056	77.52	4.46	1.48	2.98	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1057	77.54	4.46	1.48	2.98	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1058	77.57	4.46	1.48	2.98	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1059	77.62	4.47	1.49	2.98	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1060	77.65	4.47	1.49	2.98	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1061	77.67	4.47	1.49	2.98	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1062	77.71	4.47	1.49	2.98	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1063	77.71	4.47	1.49	2.98	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1064	77.76	4.47	1.49	2.98	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1065	77.81	4.48	1.49	2.99	0.56	0.342	1.36	0.251	0.81	1.00	2.000	No
1066	77.90	4.48	1.49	2.99	0.56	0.341	1.36	0.251	0.81	1.00	2.000	No
1067	77.95	4.49	1.50	2.99	0.56	0.341	1.36	0.251	0.81	1.00	2.000	No
1068	78.01	4.49	1.50	2.99	0.56	0.341	1.36	0.251	0.81	1.00	2.000	No
1069	78.10	4.49	1.50	2.99	0.56	0.341	1.36	0.251	0.81	1.00	2.000	No
1070	78.16	4.50	1.50	3.00	0.55	0.341	1.36	0.251	0.81	1.00	2.000	No
1071	78.24	4.50	1.51	3.00	0.55	0.341	1.36	0.251	0.81	1.00	2.000	Yes
1072	78.29	4.51	1.51	3.00	0.55	0.341	1.36	0.251	0.81	1.00	2.000	Yes
1073	78.39	4.51	1.51	3.00	0.55	0.341	1.36	0.251	0.81	1.00	2.000	Yes
1074	78.47	4.52	1.51	3.00	0.55	0.341	1.36	0.251	0.81	1.00	2.000	Yes
1075	78.53	4.52	1.51	3.01	0.55	0.341	1.36	0.251	0.81	1.00	2.000	Yes
1076	78.62	4.53	1.52	3.01	0.55	0.341	1.36	0.251	0.81	1.00	2.000	Yes
1077	78.68	4.53	1.52	3.01	0.55	0.341	1.36	0.250	0.81	1.00	2.000	Yes
1078	78.69	4.53	1.52	3.01	0.55	0.341	1.36	0.250	0.81	1.00	2.000	Yes
1079	78.78	4.54	1.52	3.01	0.55	0.341	1.36	0.250	0.81	1.00	2.000	No
1080	78.81	4.54	1.52	3.02	0.55	0.340	1.36	0.250	0.81	1.00	2.000	No
1081	78.92	4.55	1.53	3.02	0.55	0.340	1.36	0.250	0.81	1.00	2.000	No
1082	79.03	4.55	1.53	3.02	0.55	0.340	1.36	0.250	0.81	1.00	2.000	No
1083	79.16	4.56	1.53	3.03	0.55	0.340	1.36	0.250	0.81	1.00	2.000	Yes
1084	79.26	4.57	1.54	3.03	0.55	0.340	1.36	0.250	0.81	1.00	2.000	Yes
1085	79.35	4.57	1.54	3.03	0.55	0.340	1.36	0.250	0.81	1.00	2.000	Yes
1086	79.45	4.58	1.54	3.04	0.55	0.340	1.36	0.250	0.81	1.00	2.000	Yes
1087	79.54	4.58	1.55	3.04	0.55	0.340	1.36	0.250	0.81	1.00	2.000	No
1088	79.64	4.59	1.55	3.04	0.55	0.340	1.36	0.250	0.81	1.00	2.000	No
1089	79.74	4.60	1.55	3.05	0.55	0.339	1.36	0.250	0.81	1.00	2.000	No
1090	79.88	4.61	1.56	3.05	0.55	0.339	1.36	0.249	0.81	1.00	2.000	No
1091	79.98	4.61	1.56	3.05	0.55	0.339	1.36	0.249	0.81	1.00	2.000	No
1092	80.12	4.62	1.56	3.06	0.55	0.339	1.36	0.249	0.81	1.00	2.000	No
1093	80.22	4.63	1.57	3.06	0.55	0.339	1.36	0.249	0.81	1.00	2.000	No
1094	80.36	4.64	1.57	3.07	0.55	0.339	1.36	0.249	0.81	1.00	2.000	No
1095	80.46	4.64	1.57	3.07	0.55	0.339	1.36	0.249	0.81	1.00	2.000	No
1096	80.60	4.65	1.58	3.07	0.55	0.338	1.36	0.249	0.81	1.00	2.000	No
1097	80.70	4.66	1.58	3.08	0.55	0.338	1.36	0.249	0.81	1.00	2.000	No
1098	80.83	4.67	1.59	3.08	0.55	0.338	1.36	0.249	0.81	1.00	2.000	Yes
1099	80.94	4.67	1.59	3.09	0.54	0.338	1.36	0.249	0.81	1.00	2.000	Yes
1100	81.01	4.68	1.59	3.09	0.54	0.338	1.36	0.249	0.81	1.00	2.000	Yes
1101	81.04	4.68	1.59	3.09	0.54	0.338	1.36	0.249	0.81	1.00	2.000	Yes
1102	81.09	4.68	1.59	3.09	0.54	0.338	1.36	0.248	0.81	1.00	2.000	Yes
1103	81.13	4.69	1.60	3.09	0.54	0.338	1.36	0.248	0.81	1.00	2.000	Yes
1104	81.18	4.69	1.60	3.09	0.54	0.338	1.36	0.248	0.81	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1105	81.23	4.69	1.60	3.09	0.54	0.338	1.36	0.248	0.81	1.00	2.000	Yes
1106	81.28	4.70	1.60	3.10	0.54	0.338	1.36	0.248	0.81	1.00	2.000	Yes
1107	81.33	4.70	1.60	3.10	0.54	0.338	1.36	0.248	0.81	1.00	2.000	Yes
1108	81.37	4.70	1.60	3.10	0.54	0.338	1.36	0.248	0.81	1.00	2.000	Yes
1109	81.42	4.70	1.60	3.10	0.54	0.338	1.36	0.248	0.81	1.00	2.000	Yes
1110	81.47	4.71	1.61	3.10	0.54	0.338	1.36	0.248	0.81	1.00	2.000	Yes
1111	81.52	4.71	1.61	3.10	0.54	0.338	1.36	0.248	0.81	1.00	2.000	Yes
1112	81.56	4.71	1.61	3.10	0.54	0.338	1.36	0.248	0.81	1.00	2.000	Yes
1113	81.61	4.72	1.61	3.11	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1114	81.64	4.72	1.61	3.11	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1115	81.70	4.72	1.61	3.11	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1116	81.75	4.73	1.61	3.11	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1117	81.79	4.73	1.62	3.11	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1118	81.82	4.73	1.62	3.11	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1119	81.86	4.73	1.62	3.11	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1120	81.91	4.74	1.62	3.12	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1121	81.95	4.74	1.62	3.12	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1122	82.00	4.74	1.62	3.12	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1123	82.09	4.75	1.63	3.12	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1124	82.15	4.75	1.63	3.12	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1125	82.19	4.75	1.63	3.12	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1126	82.26	4.76	1.63	3.13	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1127	82.34	4.76	1.63	3.13	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1128	82.39	4.76	1.63	3.13	0.54	0.337	1.36	0.248	0.81	1.00	2.000	No
1129	82.48	4.77	1.64	3.13	0.54	0.337	1.36	0.248	0.80	1.00	2.000	No
1130	82.58	4.77	1.64	3.13	0.54	0.337	1.36	0.248	0.80	1.00	2.000	No
1131	82.62	4.78	1.64	3.13	0.54	0.337	1.36	0.248	0.80	1.00	2.000	No
1132	82.70	4.78	1.64	3.14	0.54	0.337	1.36	0.247	0.80	1.00	2.000	No
1133	82.77	4.78	1.65	3.14	0.54	0.337	1.36	0.247	0.80	1.00	2.000	No
1134	82.87	4.79	1.65	3.14	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1135	82.96	4.80	1.65	3.14	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1136	83.06	4.80	1.66	3.15	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1137	83.16	4.81	1.66	3.15	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1138	83.25	4.81	1.66	3.15	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1139	83.34	4.82	1.66	3.15	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1140	83.44	4.82	1.67	3.15	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1141	83.54	4.83	1.67	3.16	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1142	83.64	4.83	1.67	3.16	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1143	83.73	4.84	1.68	3.16	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1144	83.83	4.84	1.68	3.16	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1145	83.85	4.85	1.68	3.17	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1146	83.89	4.85	1.68	3.17	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1147	83.94	4.85	1.68	3.17	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1148	84.04	4.86	1.69	3.17	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1149	84.09	4.86	1.69	3.17	0.54	0.336	1.36	0.247	0.80	1.00	2.000	No
1150	84.13	4.86	1.69	3.17	0.53	0.336	1.36	0.247	0.80	1.00	2.000	No
1151	84.18	4.87	1.69	3.17	0.53	0.336	1.36	0.247	0.80	1.00	2.000	No
1152	84.25	4.87	1.69	3.18	0.53	0.336	1.36	0.247	0.80	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1153	84.33	4.87	1.69	3.18	0.53	0.335	1.36	0.247	0.80	1.00	2.000	No
1154	84.37	4.88	1.70	3.18	0.53	0.335	1.36	0.247	0.80	1.00	2.000	No
1155	84.46	4.88	1.70	3.18	0.53	0.335	1.36	0.247	0.80	1.00	2.000	No
1156	84.52	4.89	1.70	3.18	0.53	0.335	1.36	0.247	0.80	1.00	2.000	No
1157	84.57	4.89	1.70	3.19	0.53	0.335	1.36	0.247	0.80	1.00	2.000	No
1158	84.67	4.89	1.71	3.19	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1159	84.71	4.90	1.71	3.19	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1160	84.81	4.90	1.71	3.19	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1161	84.86	4.91	1.71	3.19	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1162	84.91	4.91	1.71	3.20	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1163	85.00	4.91	1.72	3.20	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1164	85.05	4.92	1.72	3.20	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1165	85.15	4.92	1.72	3.20	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1166	85.19	4.93	1.72	3.20	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1167	85.29	4.93	1.73	3.21	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1168	85.35	4.94	1.73	3.21	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1169	85.42	4.94	1.73	3.21	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1170	85.48	4.94	1.73	3.21	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1171	85.55	4.95	1.73	3.21	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1172	85.63	4.95	1.74	3.22	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1173	85.68	4.95	1.74	3.22	0.53	0.335	1.36	0.246	0.80	1.00	2.000	No
1174	85.77	4.96	1.74	3.22	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1175	85.82	4.96	1.74	3.22	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1176	85.89	4.97	1.74	3.22	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1177	85.96	4.97	1.75	3.22	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1178	86.03	4.97	1.75	3.23	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1179	86.11	4.98	1.75	3.23	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1180	86.16	4.98	1.75	3.23	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1181	86.25	4.99	1.76	3.23	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1182	86.36	4.99	1.76	3.23	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1183	86.50	5.00	1.76	3.24	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1184	86.51	5.00	1.76	3.24	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1185	86.52	5.00	1.76	3.24	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1186	86.57	5.01	1.76	3.24	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1187	86.65	5.01	1.77	3.24	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1188	86.71	5.01	1.77	3.24	0.53	0.334	1.36	0.246	0.80	1.00	2.000	No
1189	86.80	5.02	1.77	3.25	0.53	0.334	1.36	0.245	0.80	1.00	2.000	No
1190	86.90	5.02	1.78	3.25	0.53	0.334	1.36	0.245	0.80	1.00	2.000	No
1191	86.99	5.03	1.78	3.25	0.53	0.334	1.36	0.245	0.80	1.00	2.000	No
1192	87.04	5.03	1.78	3.25	0.53	0.334	1.36	0.245	0.80	1.00	2.000	No
1193	87.14	5.04	1.78	3.25	0.53	0.334	1.36	0.245	0.80	1.00	2.000	No
1194	87.19	5.04	1.78	3.26	0.53	0.334	1.36	0.245	0.80	1.00	2.000	No
1195	87.28	5.04	1.79	3.26	0.53	0.334	1.36	0.245	0.80	1.00	2.000	No
1196	87.38	5.05	1.79	3.26	0.53	0.334	1.36	0.245	0.80	1.00	2.000	No
1197	87.43	5.05	1.79	3.26	0.53	0.334	1.36	0.245	0.80	1.00	2.000	No
1198	87.52	5.06	1.79	3.26	0.53	0.334	1.36	0.245	0.80	1.00	2.000	No
1199	87.61	5.06	1.80	3.26	0.53	0.334	1.36	0.245	0.80	1.00	2.000	No
1200	87.66	5.07	1.80	3.27	0.53	0.333	1.36	0.245	0.80	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1201	87.76	5.07	1.80	3.27	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1202	87.84	5.07	1.80	3.27	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1203	87.91	5.08	1.81	3.27	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1204	88.00	5.08	1.81	3.27	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1205	88.11	5.09	1.81	3.28	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1206	88.19	5.09	1.82	3.28	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1207	88.25	5.10	1.82	3.28	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1208	88.34	5.10	1.82	3.28	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1209	88.44	5.11	1.82	3.28	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1210	88.54	5.11	1.83	3.29	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1211	88.64	5.12	1.83	3.29	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1212	88.72	5.12	1.83	3.29	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1213	88.82	5.13	1.84	3.29	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1214	88.91	5.13	1.84	3.29	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1215	89.01	5.14	1.84	3.30	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1216	89.10	5.14	1.84	3.30	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1217	89.19	5.15	1.85	3.30	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1218	89.30	5.15	1.85	3.30	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1219	89.39	5.16	1.85	3.31	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1220	89.49	5.16	1.86	3.31	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1221	89.59	5.17	1.86	3.31	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1222	89.69	5.17	1.86	3.31	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1223	89.73	5.18	1.86	3.31	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1224	89.78	5.18	1.87	3.31	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1225	89.83	5.18	1.87	3.32	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1226	89.88	5.19	1.87	3.32	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1227	89.93	5.19	1.87	3.32	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1228	90.00	5.19	1.87	3.32	0.52	0.333	1.36	0.245	0.80	1.00	2.000	No
1229	90.07	5.20	1.87	3.32	0.52	0.333	1.36	0.244	0.80	1.00	2.000	No
1230	90.12	5.20	1.88	3.32	0.52	0.332	1.36	0.244	0.80	1.00	2.000	No
1231	90.22	5.20	1.88	3.33	0.52	0.332	1.36	0.244	0.80	1.00	2.000	No
1232	90.27	5.21	1.88	3.33	0.52	0.332	1.36	0.244	0.80	1.00	2.000	No
1233	90.36	5.21	1.88	3.33	0.52	0.332	1.36	0.244	0.80	1.00	2.000	No
1234	90.46	5.22	1.89	3.33	0.52	0.332	1.36	0.244	0.80	1.00	2.000	No
1235	90.50	5.22	1.89	3.33	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1236	90.61	5.23	1.89	3.34	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1237	90.66	5.23	1.89	3.34	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1238	90.75	5.23	1.90	3.34	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1239	90.84	5.24	1.90	3.34	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1240	90.89	5.24	1.90	3.34	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1241	90.99	5.25	1.90	3.35	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1242	91.04	5.25	1.90	3.35	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1243	91.14	5.26	1.91	3.35	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1244	91.22	5.26	1.91	3.35	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1245	91.28	5.26	1.91	3.35	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1246	91.37	5.27	1.91	3.35	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1247	91.47	5.28	1.92	3.36	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1248	91.61	5.28	1.92	3.36	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1249	91.71	5.29	1.93	3.36	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1250	91.81	5.29	1.93	3.37	0.52	0.332	1.36	0.244	0.79	1.00	2.000	No
1251	91.87	5.30	1.93	3.37	0.51	0.332	1.36	0.244	0.79	1.00	2.000	No
1252	92.00	5.30	1.93	3.37	0.51	0.332	1.36	0.244	0.79	1.00	2.000	No
1253	92.10	5.31	1.94	3.37	0.51	0.332	1.36	0.244	0.79	1.00	2.000	No
1254	92.20	5.32	1.94	3.37	0.51	0.332	1.36	0.244	0.79	1.00	2.000	No
1255	92.33	5.32	1.94	3.38	0.51	0.332	1.36	0.244	0.79	1.00	2.000	No
1256	92.38	5.33	1.95	3.38	0.51	0.332	1.36	0.244	0.79	1.00	2.000	No
1257	92.43	5.33	1.95	3.38	0.51	0.332	1.36	0.244	0.79	1.00	2.000	No
1258	92.48	5.33	1.95	3.38	0.51	0.332	1.36	0.244	0.79	1.00	2.000	No
1259	92.56	5.33	1.95	3.38	0.51	0.332	1.36	0.244	0.79	1.00	2.000	No
1260	92.63	5.34	1.95	3.38	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1261	92.67	5.34	1.96	3.39	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1262	92.72	5.34	1.96	3.39	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1263	92.77	5.35	1.96	3.39	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1264	92.86	5.35	1.96	3.39	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1265	92.92	5.35	1.96	3.39	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1266	92.97	5.36	1.96	3.39	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1267	93.05	5.36	1.97	3.39	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1268	93.10	5.37	1.97	3.40	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1269	93.16	5.37	1.97	3.40	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1270	93.25	5.37	1.97	3.40	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1271	93.35	5.38	1.98	3.40	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1272	93.40	5.38	1.98	3.40	0.51	0.331	1.36	0.244	0.79	1.00	2.000	No
1273	93.49	5.39	1.98	3.41	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1274	93.56	5.39	1.98	3.41	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1275	93.64	5.40	1.99	3.41	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1276	93.73	5.40	1.99	3.41	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1277	93.83	5.41	1.99	3.41	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1278	93.88	5.41	1.99	3.42	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1279	93.97	5.41	2.00	3.42	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1280	94.07	5.42	2.00	3.42	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1281	94.17	5.43	2.00	3.42	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1282	94.26	5.43	2.01	3.43	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1283	94.36	5.44	2.01	3.43	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1284	94.45	5.44	2.01	3.43	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1285	94.55	5.45	2.01	3.43	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1286	94.64	5.45	2.02	3.44	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1287	94.72	5.46	2.02	3.44	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1288	94.74	5.46	2.02	3.44	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1289	94.77	5.46	2.02	3.44	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1290	94.85	5.47	2.02	3.44	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1291	94.90	5.47	2.02	3.44	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1292	94.95	5.47	2.03	3.45	0.51	0.331	1.36	0.243	0.79	1.00	2.000	No
1293	95.01	5.48	2.03	3.45	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1294	95.09	5.48	2.03	3.45	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1295	95.14	5.48	2.03	3.45	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1296	95.23	5.49	2.04	3.46	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1297	95.29	5.49	2.04	3.46	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1298	95.38	5.50	2.04	3.46	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1299	95.43	5.50	2.04	3.46	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1300	95.52	5.51	2.04	3.47	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1301	95.57	5.51	2.05	3.47	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1302	95.67	5.52	2.05	3.47	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1303	95.77	5.53	2.05	3.47	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1304	95.86	5.53	2.05	3.48	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1305	95.95	5.54	2.06	3.48	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1306	96.03	5.54	2.06	3.48	0.51	0.330	1.36	0.243	0.79	1.00	2.000	No
1307	96.11	5.55	2.06	3.48	0.51	0.330	1.36	0.242	0.79	1.00	2.000	No
1308	96.20	5.55	2.07	3.49	0.51	0.330	1.36	0.242	0.79	1.00	2.000	No
1309	96.30	5.56	2.07	3.49	0.51	0.330	1.36	0.242	0.79	1.00	2.000	Yes
1310	96.39	5.57	2.07	3.49	0.51	0.330	1.36	0.242	0.79	1.00	2.000	Yes
1311	96.50	5.57	2.07	3.50	0.51	0.330	1.36	0.242	0.79	1.00	2.000	Yes
1312	96.59	5.58	2.08	3.50	0.50	0.330	1.36	0.242	0.79	1.00	2.000	Yes
1313	96.69	5.58	2.08	3.50	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1314	96.78	5.59	2.08	3.51	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1315	96.87	5.60	2.09	3.51	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1316	96.98	5.60	2.09	3.51	0.50	0.329	1.36	0.242	0.79	1.00	2.000	No
1317	97.02	5.61	2.09	3.51	0.50	0.329	1.36	0.242	0.79	1.00	2.000	No
1318	97.06	5.61	2.09	3.52	0.50	0.329	1.36	0.242	0.79	1.00	2.000	No
1319	97.12	5.61	2.09	3.52	0.50	0.329	1.36	0.242	0.79	1.00	2.000	No
1320	97.16	5.62	2.10	3.52	0.50	0.329	1.36	0.242	0.79	1.00	2.000	No
1321	97.21	5.62	2.10	3.52	0.50	0.329	1.36	0.242	0.79	1.00	2.000	No
1322	97.27	5.62	2.10	3.52	0.50	0.329	1.36	0.242	0.79	1.00	2.000	No
1323	97.33	5.63	2.10	3.53	0.50	0.329	1.36	0.242	0.79	1.00	2.000	No
1324	97.40	5.63	2.10	3.53	0.50	0.329	1.36	0.242	0.79	1.00	2.000	No
1325	97.45	5.63	2.10	3.53	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1326	97.50	5.64	2.11	3.53	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1327	97.58	5.64	2.11	3.53	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1328	97.65	5.65	2.11	3.54	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1329	97.69	5.65	2.11	3.54	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1330	97.74	5.65	2.11	3.54	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1331	97.81	5.66	2.12	3.54	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1332	97.88	5.66	2.12	3.54	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1333	97.93	5.67	2.12	3.55	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1334	98.03	5.67	2.12	3.55	0.50	0.329	1.36	0.242	0.79	1.00	2.000	Yes
1335	98.15	5.68	2.13	3.55	0.50	0.329	1.36	0.242	0.78	1.00	2.000	Yes
1336	98.21	5.68	2.13	3.56	0.50	0.329	1.36	0.242	0.78	1.00	2.000	Yes
1337	98.32	5.69	2.13	3.56	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1338	98.42	5.70	2.13	3.56	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1339	98.47	5.70	2.14	3.56	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1340	98.57	5.71	2.14	3.57	0.50	0.328	1.36	0.241	0.78	1.00	2.000	No
1341	98.70	5.71	2.14	3.57	0.50	0.328	1.36	0.241	0.78	1.00	2.000	No
1342	98.78	5.72	2.15	3.57	0.50	0.328	1.36	0.241	0.78	1.00	2.000	No
1343	98.85	5.72	2.15	3.58	0.50	0.328	1.36	0.241	0.78	1.00	2.000	No
1344	98.86	5.72	2.15	3.58	0.50	0.328	1.36	0.241	0.78	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (ft)	σ_v (tsf)	u_0 (tsf)	σ_v' (tsf)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1345	98.92	5.73	2.15	3.58	0.50	0.328	1.36	0.241	0.78	1.00	2.000	No
1346	98.98	5.73	2.15	3.58	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1347	99.03	5.74	2.15	3.58	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1348	99.11	5.74	2.16	3.58	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1349	99.18	5.74	2.16	3.59	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1350	99.23	5.75	2.16	3.59	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1351	99.32	5.75	2.16	3.59	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1352	99.37	5.76	2.16	3.59	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1353	99.45	5.76	2.17	3.60	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1354	99.56	5.77	2.17	3.60	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1355	99.64	5.77	2.17	3.60	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1356	99.71	5.78	2.17	3.60	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1357	99.75	5.78	2.18	3.61	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1358	99.90	5.79	2.18	3.61	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1359	99.95	5.80	2.18	3.61	0.50	0.328	1.36	0.241	0.78	1.00	2.000	Yes
1360	100.04	5.80	2.19	3.62	0.50	0.327	1.36	0.241	0.78	1.00	2.000	Yes
1361	100.14	5.81	2.19	3.62	0.50	0.327	1.36	0.241	0.78	1.00	2.000	Yes
1362	100.14	5.81	2.19	3.62	0.50	0.327	1.36	0.241	0.78	1.00	2.000	Yes
1363	100.15	5.81	2.19	3.62	0.50	0.327	1.36	0.241	0.78	1.00	2.000	Yes
1364	100.19	5.81	2.19	3.62	0.50	0.327	1.36	0.241	0.78	1.00	2.000	Yes
1365	100.21	5.81	2.19	3.62	0.50	0.327	1.36	0.241	0.78	1.00	2.000	Yes
1366	100.24	5.81	2.19	3.62	0.50	0.327	1.36	0.241	0.78	1.00	2.000	Yes
1367	100.28	5.82	2.19	3.62	0.50	0.327	1.36	0.241	0.78	1.00	2.000	Yes
1368	100.31	5.82	2.19	3.63	0.50	0.327	1.36	0.241	0.78	1.00	2.000	No
1369	100.33	5.82	2.19	3.63	0.50	0.327	1.36	0.241	0.78	1.00	2.000	No
1370	100.38	5.82	2.20	3.63	0.50	0.327	1.36	0.241	0.78	1.00	2.000	No
1371	100.39	5.82	2.20	3.63	0.50	0.327	1.36	0.241	0.78	1.00	2.000	No
1372	100.43	5.82	2.20	3.63	0.50	0.327	1.36	0.241	0.78	1.00	2.000	No
1373	100.48	5.83	2.20	3.63	0.50	0.327	1.36	0.241	0.78	1.00	2.000	No
1374	100.53	5.83	2.20	3.63	0.50	0.327	1.36	0.241	0.78	1.00	2.000	No
1375	100.57	5.83	2.20	3.63	0.50	0.327	1.36	0.241	0.78	1.00	2.000	No
1376	100.60	5.83	2.20	3.63	0.50	0.327	1.36	0.241	0.78	1.00	2.000	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
σ_v: Total overburden pressure at test point (tsf)
u_0: Water pressure at test point (tsf)
σ_v': Effective overburden pressure based on GWT during earthquake (tsf)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.04	0.10	4.06	37.76	1.00	0.16	54.25	8.56	4.000	No	Yes	2.00
2	0.10	0.13	4.06	31.79	1.00	0.21	54.25	11.25	4.000	No	Yes	2.00
3	0.11	0.23	4.06	19.95	1.00	0.37	54.25	19.92	4.000	No	Yes	2.00
4	0.16	0.54	4.06	8.78	1.00	0.85	54.25	46.18	4.000	No	Yes	2.00
5	0.19	1.28	3.64	3.82	1.00	2.04	26.86	54.86	4.000	No	Yes	2.00
6	0.24	2.83	3.19	1.88	1.00	4.54	12.41	56.29	4.000	No	Yes	2.00
7	0.31	4.93	2.89	1.26	0.88	7.89	7.08	55.92	4.000	No	Yes	2.00
8	0.38	6.68	2.74	1.06	0.83	10.70	5.13	54.91	4.000	No	Yes	2.00
9	0.43	7.56	2.68	1.02	0.81	12.11	4.55	55.04	4.000	No	Yes	2.00
10	0.49	7.32	2.72	1.13	0.82	11.72	4.88	57.26	4.000	No	Yes	2.00
11	0.58	6.81	2.78	1.31	0.84	10.90	5.56	60.65	4.000	No	Yes	2.00
12	0.63	6.24	2.85	1.60	0.86	9.98	6.53	65.19	4.000	No	Yes	2.00
13	0.67	6.05	2.90	1.88	0.88	9.68	7.19	69.56	4.000	No	Yes	2.00
14	0.72	6.02	2.92	2.08	0.89	9.62	7.57	72.80	4.000	Yes	Yes	2.00
15	0.72	6.70	2.91	2.29	0.88	10.70	7.32	78.32	4.000	Yes	Yes	2.00
16	0.84	9.28	2.77	2.08	0.84	14.84	5.43	80.63	4.000	Yes	Yes	2.00
17	0.96	15.82	2.50	1.53	0.76	25.35	2.97	75.23	4.000	Yes	No	2.00
18	1.06	22.64	2.32	1.27	0.71	36.29	2.02	73.35	4.000	Yes	No	2.00
19	1.24	27.97	2.21	1.11	0.67	44.84	1.65	74.08	4.000	Yes	No	2.00
20	1.30	31.48	2.14	0.98	0.65	50.47	1.49	75.12	4.000	Yes	No	2.00
21	1.48	37.28	2.04	0.82	0.62	59.78	1.34	80.22	4.000	Yes	No	2.00
22	1.59	42.14	1.98	0.77	0.60	67.57	1.29	87.16	4.000	Yes	No	2.00
23	1.69	47.40	1.93	0.75	0.59	76.02	1.26	95.52	4.000	Yes	No	2.00
24	1.69	49.80	1.91	0.76	0.58	79.87	1.25	99.55	4.000	Yes	No	2.00
25	1.74	53.24	1.88	0.73	0.57	85.40	1.22	104.46	4.000	Yes	No	2.00
26	1.79	53.78	1.88	0.73	0.57	86.26	1.22	105.40	4.000	No	No	2.00
27	1.84	52.90	1.89	0.73	0.57	84.84	1.23	104.08	4.000	No	No	2.00
28	1.88	51.25	1.89	0.73	0.58	82.18	1.23	101.34	4.000	No	No	2.00
29	1.93	49.46	1.90	0.71	0.58	79.31	1.24	98.11	4.000	No	No	2.00
30	1.99	48.69	1.90	0.68	0.58	78.06	1.23	96.29	4.000	No	No	2.00
31	2.03	48.08	1.89	0.65	0.58	77.07	1.23	94.90	4.000	No	No	2.00
32	2.08	47.67	1.89	0.64	0.57	76.42	1.23	93.98	4.000	No	No	2.00
33	2.13	46.86	1.90	0.64	0.58	75.11	1.23	92.67	4.000	No	No	2.00
34	2.22	45.85	1.90	0.64	0.58	73.48	1.24	91.09	4.000	No	No	2.00
35	2.27	44.97	1.91	0.64	0.58	72.07	1.24	89.70	4.000	No	No	2.00
36	2.33	44.77	1.91	0.63	0.58	71.74	1.24	89.16	4.000	No	No	2.00
37	2.42	45.44	1.90	0.61	0.58	72.81	1.24	89.96	4.000	No	No	2.00
38	2.48	46.73	1.88	0.60	0.57	74.86	1.22	91.66	4.000	No	No	2.00
39	2.56	48.41	1.86	0.59	0.57	77.57	1.21	94.03	4.000	No	No	2.00
40	2.65	49.43	1.86	0.59	0.56	79.19	1.21	95.47	4.000	No	No	2.00
41	2.72	48.72	1.87	0.60	0.57	78.04	1.21	94.74	4.000	No	No	2.00
42	2.80	46.02	1.90	0.62	0.58	73.70	1.23	90.99	4.000	No	No	2.00
43	2.89	42.44	1.94	0.65	0.59	67.94	1.26	85.67	4.000	No	No	2.00
44	2.94	39.03	1.98	0.69	0.60	62.46	1.29	80.64	4.000	No	No	2.00
45	3.04	35.90	2.02	0.71	0.61	57.42	1.32	76.04	4.000	No	No	2.00
46	3.14	32.32	2.07	0.73	0.63	51.66	1.37	70.91	4.000	No	No	2.00
47	3.23	29.01	2.10	0.73	0.64	46.34	1.42	65.97	4.000	No	No	2.00
48	3.31	25.74	2.15	0.73	0.65	41.07	1.50	61.64	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	3.37	23.04	2.19	0.72	0.66	36.73	1.59	58.33	4.000	No	No	2.00
50	3.48	20.38	2.23	0.72	0.68	32.44	1.71	55.35	4.000	No	No	2.00
51	3.57	18.79	2.25	0.67	0.68	29.89	1.76	52.71	4.000	No	No	2.00
52	3.65	18.02	2.26	0.63	0.69	28.64	1.78	50.93	4.000	No	No	2.00
53	3.71	18.02	2.26	0.63	0.68	28.64	1.77	50.70	4.000	No	No	2.00
54	3.82	18.63	2.26	0.67	0.68	29.60	1.77	52.47	4.000	No	No	2.00
55	3.91	20.18	2.23	0.70	0.68	32.09	1.71	54.73	4.000	No	No	2.00
56	4.00	22.81	2.20	0.73	0.67	36.30	1.60	58.22	4.000	No	No	2.00
57	4.10	26.38	2.09	0.58	0.64	42.04	1.41	59.10	4.000	No	No	2.00
58	4.19	31.21	1.98	0.46	0.60	49.79	1.00	49.79	4.000	No	No	2.00
59	4.26	37.92	1.86	0.36	0.57	60.57	1.00	60.57	4.000	No	No	2.00
60	4.35	45.62	1.79	0.37	0.54	72.92	1.00	72.92	4.000	No	No	2.00
61	4.44	49.80	1.77	0.39	0.54	79.63	1.00	79.63	4.000	No	No	2.00
62	4.52	51.39	1.76	0.41	0.54	82.17	1.00	82.17	4.000	No	No	2.00
63	4.53	52.26	1.76	0.41	0.54	83.58	1.00	83.58	4.000	No	No	2.00
64	4.58	55.03	1.73	0.39	0.53	88.02	1.00	88.02	4.000	No	No	2.00
65	4.63	57.76	1.71	0.39	0.52	92.41	1.00	92.41	4.000	No	No	2.00
66	4.68	58.84	1.70	0.39	0.52	94.14	1.00	94.14	4.000	No	No	2.00
67	4.72	59.28	1.71	0.41	0.52	94.84	1.00	94.84	4.000	No	No	2.00
68	4.77	59.08	1.72	0.42	0.52	94.51	1.00	94.51	4.000	No	No	2.00
69	4.82	58.07	1.73	0.44	0.53	92.88	1.00	92.88	4.000	No	No	2.00
70	4.88	56.21	1.76	0.47	0.54	89.89	1.00	89.89	4.000	No	No	2.00
71	4.96	53.61	1.79	0.50	0.55	85.71	1.14	97.96	4.000	No	No	2.00
72	5.01	50.54	1.83	0.54	0.56	80.78	1.18	95.67	4.000	No	No	2.00
73	5.08	47.44	1.87	0.59	0.57	75.78	1.22	92.32	4.000	No	No	2.00
74	5.16	44.81	1.91	0.63	0.58	71.55	1.24	88.93	4.000	No	No	2.00
75	5.21	43.27	1.93	0.65	0.59	69.07	1.26	86.85	4.000	No	No	2.00
76	5.30	42.68	1.94	0.66	0.59	68.12	1.26	86.01	4.000	No	No	2.00
77	5.37	42.65	1.94	0.66	0.59	68.06	1.26	85.96	4.000	No	No	2.00
78	5.45	42.70	1.94	0.66	0.59	68.13	1.26	86.01	4.000	No	No	2.00
79	5.52	42.44	1.94	0.66	0.59	67.72	1.26	85.64	4.000	No	No	2.00
80	5.59	41.70	1.95	0.67	0.59	66.52	1.27	84.54	4.000	No	No	2.00
81	5.65	40.15	1.97	0.69	0.60	64.02	1.28	82.25	4.000	No	No	2.00
82	5.74	38.46	1.99	0.71	0.61	61.30	1.30	79.83	4.000	No	No	2.00
83	5.83	37.08	2.02	0.73	0.61	59.07	1.32	77.99	4.000	No	No	2.00
84	5.89	36.30	2.03	0.75	0.62	57.82	1.33	77.16	4.000	No	No	2.00
85	5.97	35.66	2.04	0.77	0.62	56.79	1.35	76.43	4.000	No	No	2.00
86	6.07	34.52	2.06	0.79	0.63	54.94	1.37	75.11	4.000	No	No	2.00
87	6.12	32.56	2.10	0.84	0.64	51.79	1.41	73.14	4.000	No	No	2.00
88	6.22	29.76	2.15	0.92	0.65	47.28	1.51	71.19	4.000	No	No	2.00
89	6.28	26.56	2.22	1.04	0.67	42.13	1.67	70.33	4.000	No	No	2.00
90	6.36	23.45	2.29	1.15	0.70	37.14	1.90	70.41	4.000	No	No	2.00
91	6.46	21.29	2.34	1.22	0.71	33.66	2.09	70.43	4.000	No	No	2.00
92	6.52	20.72	2.33	1.14	0.71	32.73	2.06	67.56	4.000	No	No	2.00
93	6.60	22.07	2.26	0.92	0.69	34.89	1.79	62.55	4.000	No	No	2.00
94	6.70	23.55	2.18	0.72	0.66	37.27	1.57	58.59	4.000	No	No	2.00
95	6.76	23.01	2.17	0.66	0.66	36.39	1.55	56.58	4.000	Yes	No	2.00
96	6.84	19.64	2.27	0.77	0.69	30.96	1.81	55.94	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	6.94	14.91	2.44	1.05	0.74	23.37	2.60	60.83	4.000	Yes	No	2.00
98	7.03	10.86	2.63	1.42	0.80	16.85	4.02	67.75	4.000	Yes	Yes	2.00
99	7.13	8.23	2.79	1.78	0.84	12.62	5.71	72.04	4.000	Yes	Yes	2.00
100	7.19	6.62	2.88	1.83	0.87	10.02	6.93	69.39	4.000	Yes	Yes	2.00
101	7.32	5.77	2.88	1.39	0.87	8.65	6.87	59.40	4.000	No	Yes	2.00
102	7.42	5.17	2.80	0.72	0.85	7.67	5.87	44.99	4.000	No	Yes	2.00
103	7.49	4.93	2.63	0.13	0.80	7.28	4.02	29.29	4.000	No	Yes	2.00
104	7.57	4.73	N/A	-0.03	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
105	7.66	4.56	N/A	-0.01	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
106	7.76	4.44	2.68	0.13	0.81	6.47	4.48	29.00	4.000	No	Yes	2.00
107	7.77	4.39	2.72	0.22	0.82	6.39	4.95	31.63	4.000	No	Yes	2.00
108	7.78	4.42	2.73	0.25	0.83	6.44	5.05	32.53	4.000	No	Yes	2.00
109	7.82	4.44	2.76	0.33	0.84	6.47	5.36	34.69	4.000	No	Yes	2.00
110	7.87	4.45	2.80	0.46	0.85	6.49	5.86	38.07	4.000	No	Yes	2.00
111	7.92	4.45	2.85	0.63	0.86	6.49	6.45	41.83	4.000	No	Yes	2.00
112	7.97	4.49	2.88	0.80	0.87	6.54	6.96	45.53	4.000	No	Yes	2.00
113	8.01	4.59	2.91	1.01	0.88	6.70	7.41	49.66	4.000	No	Yes	2.00
114	8.06	4.76	2.92	1.17	0.89	6.97	7.58	52.81	4.000	No	Yes	2.00
115	8.11	4.93	2.93	1.29	0.89	7.24	7.65	55.42	4.000	No	Yes	2.00
116	8.20	5.06	2.93	1.38	0.89	7.45	7.68	57.24	4.000	No	Yes	2.00
117	8.26	5.16	2.94	1.51	0.89	7.60	7.84	59.63	4.000	No	Yes	2.00
118	8.35	5.23	2.95	1.61	1.00	7.70	7.98	61.50	4.000	No	Yes	2.00
119	8.40	5.30	2.95	1.67	1.00	7.81	8.02	62.65	4.000	No	Yes	2.00
120	8.49	5.37	2.95	1.68	0.89	7.91	7.96	62.99	4.000	No	Yes	2.00
121	8.54	5.51	2.94	1.69	0.89	8.13	7.81	63.54	4.000	No	Yes	2.00
122	8.64	5.71	2.93	1.68	0.89	8.45	7.58	64.06	4.000	No	Yes	2.00
123	8.69	5.91	2.91	1.68	0.88	8.77	7.37	64.63	4.000	No	Yes	2.00
124	8.79	6.18	2.92	1.87	0.88	9.19	7.46	68.57	4.000	No	Yes	2.00
125	8.84	6.48	2.93	2.12	0.89	9.68	7.59	73.49	4.000	No	Yes	2.00
126	8.93	6.89	2.92	2.28	0.88	10.32	7.50	77.37	4.000	No	Yes	2.00
127	9.03	7.13	2.92	2.39	0.88	10.69	7.46	79.83	4.000	No	Yes	2.00
128	9.08	7.21	2.92	2.47	0.88	10.83	7.52	81.47	4.000	No	Yes	2.00
129	9.11	7.16	2.94	2.63	0.89	10.75	7.78	83.66	4.000	No	Yes	2.00
130	9.12	7.13	2.95	2.68	0.89	10.69	7.89	84.32	4.000	No	Yes	2.00
131	9.17	7.07	2.95	2.75	1.00	10.60	8.03	85.13	4.000	No	Yes	2.00
132	9.22	7.12	2.96	2.81	1.00	10.67	8.09	86.32	4.000	No	Yes	2.00
133	9.31	6.92	2.99	3.02	1.00	10.34	8.56	88.56	4.000	No	Yes	2.00
134	9.36	7.16	2.98	3.04	1.00	10.72	8.37	89.76	4.000	No	Yes	2.00
135	9.40	7.46	2.95	2.98	1.00	11.20	8.04	90.10	4.000	No	Yes	2.00
136	9.46	8.14	2.90	2.76	0.88	12.28	7.25	89.07	4.000	No	Yes	2.00
137	9.51	8.47	2.88	2.68	0.87	12.82	6.92	88.75	4.000	No	Yes	2.00
138	9.55	8.78	2.86	2.65	0.87	13.30	6.70	89.10	4.000	No	Yes	2.00
139	9.61	8.98	2.86	2.71	0.87	13.63	6.65	90.65	4.000	No	Yes	2.00
140	9.69	9.12	2.87	2.83	0.87	13.84	6.73	93.09	4.000	No	Yes	2.00
141	9.74	9.18	2.88	2.97	0.87	13.94	6.87	95.71	4.000	No	Yes	2.00
142	9.81	9.39	2.88	3.05	0.87	14.26	6.85	97.70	4.000	No	Yes	2.00
143	9.89	9.76	2.86	3.02	0.87	14.85	6.62	98.33	4.000	No	Yes	2.00
144	9.94	10.06	2.84	2.98	0.86	15.33	6.42	98.43	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	10.03	10.23	2.83	2.93	0.86	15.59	6.28	97.94	4.000	No	Yes	2.00
146	10.08	10.23	2.80	2.62	0.85	15.59	5.91	92.18	4.000	No	Yes	2.00
147	10.18	10.23	2.76	2.21	0.84	15.58	5.40	84.12	4.000	No	Yes	2.00
148	10.23	10.23	2.73	1.94	0.83	15.58	5.05	78.62	4.000	No	Yes	2.00
149	10.33	10.23	2.74	2.03	0.83	15.57	5.17	80.55	4.000	No	Yes	2.00
150	10.40	10.23	2.77	2.31	0.84	15.56	5.54	86.20	4.000	No	Yes	2.00
151	10.47	10.08	2.80	2.55	0.85	15.32	5.91	90.44	4.000	No	Yes	2.00
152	10.51	10.06	2.83	2.76	0.86	15.28	6.18	94.42	4.000	No	Yes	2.00
153	10.56	10.03	2.84	2.94	0.86	15.23	6.41	97.63	4.000	No	Yes	2.00
154	10.61	10.21	2.85	3.10	0.86	15.52	6.51	100.97	4.000	No	Yes	2.00
155	10.67	10.16	2.88	3.41	0.87	15.43	6.88	106.14	4.000	No	Yes	2.00
156	10.75	10.13	2.90	3.70	0.88	15.37	7.21	110.80	4.000	No	Yes	2.00
157	10.80	9.99	2.92	3.91	0.88	15.15	7.50	113.70	4.000	No	Yes	2.00
158	10.85	9.89	2.93	3.98	0.89	14.99	7.63	114.35	4.000	No	Yes	2.00
159	10.90	9.72	2.94	4.07	0.89	14.71	7.82	115.05	4.000	No	Yes	2.00
160	11.00	9.45	2.96	4.21	1.00	14.27	8.13	116.05	4.000	No	Yes	2.00
161	11.05	9.05	2.99	4.36	1.00	13.61	8.55	116.32	4.000	No	Yes	2.00
162	11.14	8.61	3.01	4.54	1.00	12.90	9.04	116.64	4.000	No	Yes	2.00
163	11.21	8.27	3.04	4.77	1.00	12.36	9.53	117.80	4.000	No	Yes	2.00
164	11.29	8.24	3.05	4.86	1.00	12.30	9.66	118.79	4.000	No	Yes	2.00
165	11.38	8.41	3.04	4.86	1.00	12.56	9.53	119.67	4.000	No	Yes	2.00
166	11.46	8.68	3.02	4.71	1.00	12.98	9.18	119.19	4.000	No	Yes	2.00
167	11.52	8.88	3.01	4.64	1.00	13.30	8.96	119.26	4.000	No	Yes	2.00
168	11.60	8.98	3.00	4.60	1.00	13.46	8.85	119.12	4.000	No	Yes	2.00
169	11.67	9.05	3.00	4.58	1.00	13.56	8.79	119.24	4.000	No	Yes	2.00
170	11.72	9.12	3.00	4.58	1.00	13.67	8.75	119.52	4.000	No	Yes	2.00
171	11.81	9.32	2.99	4.50	1.00	13.98	8.54	119.37	4.000	No	Yes	2.00
172	11.86	9.35	2.98	4.50	1.00	14.03	8.52	119.54	4.000	No	Yes	2.00
173	11.96	9.42	2.98	4.48	1.00	14.07	8.48	119.37	4.000	No	Yes	2.00
174	12.01	9.45	2.98	4.50	1.00	14.06	8.50	119.58	4.000	No	Yes	2.00
175	12.10	9.69	2.97	4.05	0.89	13.55	8.25	111.75	4.000	No	Yes	2.00
176	12.16	10.07	2.91	3.44	0.88	13.97	7.41	103.51	4.000	No	Yes	2.00
177	12.24	10.47	2.88	3.08	0.87	14.38	6.85	98.49	4.000	No	Yes	2.00
178	12.32	10.87	2.88	3.24	0.87	14.89	6.86	102.09	4.000	No	Yes	2.00
179	12.39	11.18	2.90	3.63	0.88	15.29	7.16	109.53	4.000	No	Yes	2.00
180	12.48	10.64	2.95	4.13	0.89	14.47	7.97	115.36	4.000	No	Yes	2.00
181	12.50	10.23	2.97	4.52	1.00	14.64	8.30	121.50	4.000	No	Yes	2.00
182	12.54	10.74	2.96	4.40	0.89	14.58	8.20	119.55	4.000	No	Yes	2.00
183	12.64	12.36	2.89	3.89	0.87	16.65	7.01	116.68	4.000	No	Yes	2.00
184	12.68	14.04	2.81	3.45	0.85	18.79	6.01	113.05	4.000	No	Yes	2.00
185	12.77	14.72	2.78	3.24	0.84	19.54	5.64	110.30	4.000	No	Yes	2.00
186	12.82	14.75	2.78	3.14	0.84	19.48	5.55	108.15	4.000	No	Yes	2.00
187	12.89	14.21	2.79	3.12	0.84	18.67	5.71	106.60	4.000	No	Yes	2.00
188	12.97	13.37	2.82	3.26	0.85	17.49	6.13	107.25	4.000	No	Yes	2.00
189	13.03	12.49	2.86	3.45	0.87	16.30	6.66	108.51	4.000	No	Yes	2.00
190	13.12	11.72	2.90	3.66	0.88	15.20	7.22	109.85	4.000	No	Yes	2.00
191	13.16	11.21	2.93	3.77	0.89	14.50	7.58	109.96	4.000	No	Yes	2.00
192	13.26	10.91	2.93	3.69	0.89	13.99	7.68	107.43	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	13.34	10.84	2.92	3.42	0.88	13.79	7.45	102.72	4.000	No	Yes	2.00
194	13.41	10.74	2.90	3.11	0.88	13.56	7.18	97.27	4.000	No	Yes	2.00
195	13.50	10.60	2.89	2.96	0.88	13.27	7.10	94.19	4.000	No	Yes	2.00
196	13.60	10.33	2.90	2.95	0.88	12.84	7.26	93.25	4.000	No	Yes	2.00
197	13.65	10.13	2.92	3.04	0.88	12.55	7.49	94.05	4.000	No	Yes	2.00
198	13.75	10.03	2.93	3.14	0.89	12.35	7.71	95.17	4.000	No	Yes	2.00
199	13.80	10.10	2.92	3.04	0.89	12.37	7.57	93.67	4.000	No	Yes	2.00
200	13.89	10.23	2.92	3.06	0.89	12.47	7.55	94.18	4.000	No	Yes	2.00
201	13.94	10.63	2.92	3.15	0.88	12.95	7.46	96.59	4.000	No	Yes	2.00
202	14.03	10.80	2.95	3.59	0.89	13.13	7.91	103.87	4.000	No	Yes	2.00
203	14.11	11.23	2.95	3.82	0.89	13.59	7.98	108.45	4.000	No	Yes	2.00
204	14.13	11.53	2.95	3.97	0.89	13.97	7.99	111.61	4.000	No	Yes	2.00
205	14.18	12.27	2.92	3.86	0.89	14.85	7.55	112.19	4.000	No	Yes	2.00
206	14.22	12.83	2.91	3.88	0.88	15.50	7.35	113.98	4.000	No	Yes	2.00
207	14.28	13.44	2.90	3.92	0.88	16.19	7.18	116.20	4.000	No	Yes	2.00
208	14.37	14.01	2.89	3.98	0.88	16.81	7.06	118.62	4.000	No	Yes	2.00
209	14.44	14.79	2.87	3.97	0.87	17.68	6.80	120.24	4.000	No	Yes	2.00
210	14.51	15.63	2.85	3.90	0.86	18.60	6.50	120.95	4.000	No	Yes	2.00
211	14.60	16.31	2.83	3.86	0.86	19.30	6.30	121.55	4.000	No	Yes	2.00
212	14.65	16.58	2.83	3.91	0.86	19.57	6.28	122.89	4.000	No	Yes	2.00
213	14.75	16.56	2.84	3.99	0.86	19.44	6.39	124.23	4.000	No	Yes	2.00
214	14.85	16.48	2.85	4.06	0.86	19.22	6.50	124.95	4.000	No	Yes	2.00
215	14.91	16.44	2.85	4.07	0.86	19.11	6.54	124.89	4.000	No	Yes	2.00
216	14.99	17.00	2.83	3.89	0.86	19.64	6.25	122.73	4.000	Yes	Yes	2.00
217	15.09	18.30	2.79	3.60	0.84	21.01	5.69	119.59	4.000	Yes	Yes	2.00
218	15.18	20.29	2.72	3.20	0.82	23.13	4.94	114.33	4.000	Yes	Yes	2.00
219	15.25	22.28	2.66	2.79	0.80	25.25	4.26	107.53	4.000	Yes	Yes	2.00
220	15.33	24.50	2.58	2.38	0.78	27.58	3.60	99.22	4.000	Yes	No	2.00
221	15.43	27.51	2.50	1.99	0.76	30.70	2.96	90.92	4.000	Yes	No	2.00
222	15.51	31.32	2.41	1.70	0.73	34.70	2.45	84.95	4.000	Yes	No	2.00
223	15.59	34.63	2.35	1.53	0.71	38.13	2.14	81.77	4.000	Yes	No	2.00
224	15.67	36.18	2.33	1.46	0.71	39.65	2.03	80.65	4.000	Yes	No	2.00
225	15.76	35.13	2.35	1.53	0.71	38.36	2.14	81.98	4.000	Yes	No	2.00
226	15.86	32.03	2.41	1.71	0.73	34.86	2.45	85.36	4.000	Yes	No	2.00
227	15.95	27.64	2.51	2.00	0.76	30.01	3.03	90.95	4.000	Yes	No	2.00
228	16.05	23.08	2.61	2.33	0.79	24.94	3.85	95.91	4.000	Yes	Yes	2.00
229	16.14	19.31	2.71	2.64	0.82	20.73	4.79	99.32	4.000	Yes	Yes	2.00
230	16.20	16.85	2.78	2.83	0.84	17.98	5.55	99.84	4.000	Yes	Yes	2.00
231	16.28	15.33	2.82	2.95	0.85	16.24	6.13	99.52	4.000	Yes	Yes	2.00
232	16.34	14.21	2.85	2.97	0.86	14.97	6.52	97.62	4.000	Yes	Yes	2.00
233	16.44	12.93	2.89	3.04	0.88	13.48	7.12	95.96	4.000	Yes	Yes	2.00
234	16.50	11.61	2.93	3.03	0.89	12.00	7.73	92.73	4.000	Yes	Yes	2.00
235	16.58	10.17	2.96	2.83	1.00	10.54	8.19	86.31	4.000	Yes	Yes	2.00
236	16.73	8.75	2.98	2.31	1.00	8.85	8.43	74.57	4.000	No	Yes	2.00
237	16.82	7.60	2.96	1.61	1.00	7.51	8.14	61.14	4.000	No	Yes	2.00
238	16.92	7.06	2.97	1.45	1.00	6.86	8.35	57.29	4.000	No	Yes	2.00
239	17.01	6.56	3.09	2.09	1.00	6.26	10.33	64.67	4.000	No	Yes	2.00
240	17.11	6.20	3.19	2.99	1.00	5.84	12.54	73.17	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	17.12	5.73	3.28	3.81	1.00	5.31	14.74	78.30	4.000	No	Yes	2.00
242	17.14	6.34	3.23	3.66	1.00	5.97	13.44	80.31	4.000	No	Yes	2.00
243	17.19	7.13	3.17	3.53	1.00	6.82	12.15	82.92	4.000	No	Yes	2.00
244	17.28	7.94	3.13	3.46	1.00	7.67	11.16	85.58	4.000	No	Yes	2.00
245	17.33	8.01	3.14	3.72	1.00	7.71	11.48	88.52	4.000	No	Yes	2.00
246	17.43	7.87	3.16	3.90	1.00	7.52	11.93	89.67	4.000	No	Yes	2.00
247	17.47	7.74	3.17	3.85	1.00	7.35	12.03	88.37	4.000	No	Yes	2.00
248	17.57	7.57	3.16	3.62	1.00	7.12	11.95	85.14	4.000	No	Yes	2.00
249	17.65	7.47	3.15	3.35	1.00	6.98	11.70	81.63	4.000	No	Yes	2.00
250	17.72	7.40	3.16	3.37	1.00	6.88	11.84	81.46	4.000	No	Yes	2.00
251	17.81	7.57	3.16	3.48	1.00	7.02	11.86	83.22	4.000	No	Yes	2.00
252	17.86	7.87	3.17	3.79	1.00	7.32	11.98	87.65	4.000	No	Yes	2.00
253	17.95	8.31	3.16	4.07	1.00	7.73	11.95	92.32	4.000	No	Yes	2.00
254	18.05	8.78	3.16	4.29	1.00	8.18	11.81	96.52	4.000	No	Yes	2.00
255	18.10	9.22	3.15	4.49	1.00	8.61	11.67	100.43	4.000	No	Yes	2.00
256	18.20	9.66	3.14	4.65	1.00	9.01	11.52	103.80	4.000	No	Yes	2.00
257	18.30	9.90	3.15	4.85	1.00	9.20	11.60	106.76	4.000	No	Yes	2.00
258	18.39	10.13	3.14	4.89	1.00	9.38	11.50	107.91	4.000	No	Yes	2.00
259	18.48	10.27	3.14	4.83	1.00	9.47	11.38	107.71	4.000	No	Yes	2.00
260	18.58	10.30	3.14	4.82	1.00	9.44	11.38	107.46	4.000	No	Yes	2.00
261	18.66	10.20	3.14	4.82	1.00	9.30	11.49	106.87	4.000	No	Yes	2.00
262	18.74	10.07	3.14	4.69	1.00	9.12	11.49	104.74	4.000	No	Yes	2.00
263	18.87	9.90	3.11	3.92	1.00	8.88	10.73	95.26	4.000	No	Yes	2.00
264	18.97	9.66	3.07	3.27	1.00	8.59	10.09	86.69	4.000	No	Yes	2.00
265	19.06	9.56	3.05	2.85	1.00	8.45	9.58	80.90	4.000	No	Yes	2.00
266	19.16	9.83	3.06	3.14	1.00	8.66	9.84	85.25	4.000	No	Yes	2.00
267	19.25	10.13	3.06	3.34	1.00	8.91	9.93	88.50	4.000	No	Yes	2.00
268	19.27	10.23	3.08	3.58	1.00	9.00	10.18	91.69	4.000	No	Yes	2.00
269	19.30	10.37	3.09	3.79	1.00	9.12	10.39	94.70	4.000	No	Yes	2.00
270	19.34	10.57	3.10	4.04	1.00	9.29	10.57	98.19	4.000	No	Yes	2.00
271	19.39	10.84	3.09	4.12	1.00	9.53	10.50	100.00	4.000	No	Yes	2.00
272	19.49	10.78	3.10	4.12	1.00	9.41	10.57	99.51	4.000	No	Yes	2.00
273	19.55	10.51	3.10	4.04	1.00	9.12	10.70	97.54	4.000	No	Yes	2.00
274	19.63	10.17	3.11	3.94	1.00	8.75	10.86	95.04	4.000	No	Yes	2.00
275	19.68	9.87	3.11	3.78	1.00	8.43	10.91	92.04	4.000	No	Yes	2.00
276	19.74	9.77	3.10	3.54	1.00	8.31	10.69	88.83	4.000	No	Yes	2.00
277	19.83	9.73	3.10	3.44	1.00	8.24	10.61	87.40	4.000	No	Yes	2.00
278	19.87	9.73	3.10	3.38	1.00	8.22	10.55	86.67	4.000	No	Yes	2.00
279	19.94	9.73	3.11	3.54	1.00	8.19	10.80	88.39	4.000	No	Yes	2.00
280	20.02	9.80	3.12	3.73	1.00	8.21	11.04	90.64	4.000	No	Yes	2.00
281	20.07	10.17	3.13	4.13	1.00	8.54	11.28	96.33	4.000	No	Yes	2.00
282	20.17	11.42	3.09	4.10	1.00	9.65	10.38	100.21	4.000	No	Yes	2.00
283	20.21	14.18	2.97	3.57	1.00	12.20	8.30	101.25	4.000	Yes	Yes	2.00
284	20.28	18.74	2.80	2.81	0.85	16.43	5.92	97.16	4.000	Yes	Yes	2.00
285	20.36	24.88	2.64	2.22	0.80	22.08	4.11	90.84	4.000	Yes	Yes	2.00
286	20.41	31.73	2.51	1.86	0.76	28.40	3.02	85.89	4.000	Yes	No	2.00
287	20.48	38.64	2.40	1.64	0.73	34.74	2.39	83.15	4.000	Yes	No	2.00
288	20.55	44.99	2.33	1.49	0.71	40.52	2.02	82.00	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	20.60	49.88	2.27	1.39	0.69	44.99	1.82	81.90	4.000	Yes	No	2.00
290	20.70	52.55	2.25	1.34	0.68	47.28	1.74	82.23	4.000	No	No	2.00
291	20.74	52.68	2.25	1.37	0.68	47.32	1.75	82.97	4.000	No	No	2.00
292	20.79	51.17	2.28	1.45	0.69	45.83	1.84	84.31	4.000	No	No	2.00
293	20.89	48.70	2.33	1.63	0.71	43.39	2.03	87.95	4.000	No	No	2.00
294	20.96	46.86	2.33	1.59	0.71	41.58	2.06	85.66	4.000	No	No	2.00
295	21.04	45.83	2.34	1.58	0.71	40.52	2.09	84.84	4.000	No	No	2.00
296	21.13	45.80	2.33	1.51	0.71	40.36	2.05	82.71	4.000	No	No	2.00
297	21.22	49.22	2.31	1.55	0.70	43.31	1.97	85.52	4.000	No	No	2.00
298	21.29	52.71	2.28	1.51	0.69	46.38	1.86	86.23	4.000	No	No	2.00
299	21.35	62.13	2.19	1.30	0.66	54.84	1.58	86.56	4.000	No	No	2.00
300	21.37	71.37	2.10	1.15	0.64	63.21	1.42	89.97	4.000	No	No	2.00
301	21.42	83.72	2.01	0.98	0.61	74.37	1.31	97.64	4.000	No	No	2.00
302	21.47	92.73	1.95	0.89	0.59	82.47	1.27	104.48	4.000	No	No	2.00
303	21.48	100.66	1.90	0.82	0.58	89.69	1.23	110.65	4.000	No	No	2.00
304	21.52	107.37	1.85	0.77	0.56	95.73	1.20	115.32	4.000	No	No	2.00
305	21.57	113.24	1.82	0.73	0.55	100.98	1.17	118.63	4.000	No	No	2.00
306	21.62	118.81	1.79	0.69	0.54	105.91	1.14	120.85	4.000	No	No	2.00
307	21.66	124.00	1.76	0.65	0.54	110.52	1.10	122.11	4.000	No	No	2.00
308	21.71	128.79	1.74	0.63	0.53	114.75	1.07	122.79	4.000	No	No	2.00
309	21.76	132.64	1.73	0.62	0.53	118.10	1.04	123.42	4.000	No	No	2.00
310	21.81	135.34	1.72	0.63	0.52	120.38	1.03	124.51	4.000	No	No	2.00
311	21.85	136.99	1.72	0.64	0.53	121.70	1.04	126.15	4.000	No	No	2.00
312	21.91	137.80	1.73	0.66	0.53	122.24	1.05	127.87	4.000	No	No	2.00
313	21.95	138.11	1.73	0.67	0.53	122.32	1.06	129.40	4.000	No	No	2.00
314	22.00	138.24	1.74	0.69	0.53	122.26	1.07	130.49	4.000	No	No	2.00
315	22.05	138.18	1.75	0.70	0.53	122.02	1.08	131.33	4.000	No	No	2.00
316	22.10	138.24	1.75	0.71	0.53	121.90	1.08	132.00	4.000	No	No	2.00
317	22.15	138.31	1.75	0.72	0.53	121.77	1.09	132.56	4.000	No	No	2.00
318	22.19	138.68	1.75	0.72	0.53	121.94	1.09	133.12	4.000	No	No	2.00
319	22.24	139.25	1.76	0.75	0.54	122.24	1.11	135.35	4.000	No	No	2.00
320	22.29	139.86	1.77	0.77	0.54	122.58	1.11	136.60	4.000	No	No	2.00
321	22.34	140.20	1.77	0.78	0.54	122.70	1.12	137.16	4.000	No	No	2.00
322	22.39	140.06	1.77	0.76	0.54	122.45	1.11	135.89	4.000	No	No	2.00
323	22.43	139.42	1.77	0.76	0.54	121.72	1.11	135.26	4.000	No	No	2.00
324	22.48	138.34	1.77	0.76	0.54	120.56	1.12	135.08	4.000	No	No	2.00
325	22.55	136.79	1.78	0.78	0.54	118.95	1.13	134.76	4.000	No	No	2.00
326	22.62	130.08	1.82	0.82	0.55	112.68	1.17	131.90	4.000	No	No	2.00
327	22.63	127.95	1.83	0.83	0.56	110.75	1.18	130.57	4.000	No	No	2.00
328	22.72	125.56	1.83	0.84	0.56	108.31	1.19	128.61	4.000	No	No	2.00
329	22.77	128.09	1.82	0.81	0.55	110.46	1.17	129.57	4.000	No	No	2.00
330	22.83	126.13	1.83	0.83	0.56	108.51	1.19	128.59	4.000	No	No	2.00
331	22.91	124.21	1.85	0.86	0.56	106.52	1.20	127.55	4.000	No	No	2.00
332	22.96	121.74	1.86	0.88	0.57	104.15	1.21	126.09	4.000	No	No	2.00
333	23.02	118.20	1.88	0.91	0.57	100.84	1.22	123.45	4.000	No	No	2.00
334	23.10	113.85	1.90	0.94	0.58	96.74	1.24	119.96	4.000	No	No	2.00
335	23.16	108.42	1.93	0.98	0.59	91.79	1.26	115.60	4.000	No	No	2.00
336	23.20	102.21	1.97	1.03	0.60	86.20	1.28	110.62	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	23.26	95.46	2.01	1.08	0.61	80.15	1.31	105.23	4.000	No	No	2.00
338	23.35	88.68	2.05	1.15	0.62	74.00	1.36	100.36	4.000	No	No	2.00
339	23.39	81.66	2.10	1.23	0.64	67.80	1.42	95.97	4.000	No	No	2.00
340	23.48	74.68	2.15	1.34	0.65	61.55	1.51	93.11	4.000	No	No	2.00
341	23.54	68.33	2.20	1.41	0.67	55.99	1.61	90.41	4.000	No	No	2.00
342	23.63	63.44	2.23	1.41	0.68	51.67	1.69	87.24	4.000	No	No	2.00
343	23.69	60.07	2.21	1.21	0.67	48.84	1.63	79.68	4.000	No	No	2.00
344	23.78	58.37	2.19	1.08	0.66	47.34	1.59	75.09	4.000	No	No	2.00
345	23.87	57.71	2.18	1.00	0.66	46.70	1.56	72.76	4.000	No	No	2.00
346	23.88	57.81	2.20	1.11	0.67	46.69	1.62	75.51	4.000	No	No	2.00
347	23.93	57.42	2.23	1.22	0.68	46.23	1.69	78.05	4.000	No	No	2.00
348	24.02	57.22	2.25	1.33	0.68	45.85	1.76	80.73	4.000	No	No	2.00
349	24.04	56.97	2.27	1.41	0.69	45.57	1.82	82.98	4.000	No	No	2.00
350	24.05	57.34	2.28	1.47	0.69	45.82	1.85	84.83	4.000	No	No	2.00
351	24.15	58.27	2.28	1.52	0.69	46.42	1.87	86.71	4.000	No	No	2.00
352	24.20	60.11	2.28	1.55	0.69	47.86	1.85	88.32	4.000	No	No	2.00
353	24.30	62.64	2.25	1.45	0.68	49.86	1.75	87.06	4.000	No	No	2.00
354	24.40	65.07	2.21	1.31	0.67	51.83	1.63	84.41	4.000	No	No	2.00
355	24.46	66.59	2.16	1.15	0.66	53.10	1.53	81.44	4.000	No	No	2.00
356	24.54	66.42	2.15	1.08	0.65	52.90	1.50	79.49	4.000	No	No	2.00
357	24.64	64.09	2.17	1.11	0.66	50.78	1.55	78.59	4.000	Yes	No	2.00
358	24.73	59.94	2.22	1.24	0.68	47.12	1.68	79.13	4.000	Yes	No	2.00
359	24.78	54.64	2.30	1.43	0.70	42.55	1.92	81.62	4.000	Yes	No	2.00
360	24.88	48.57	2.38	1.66	0.72	37.36	2.28	85.25	4.000	Yes	No	2.00
361	24.94	41.92	2.47	1.90	0.75	31.81	2.80	89.16	4.000	Yes	No	2.00
362	25.02	35.00	2.57	2.14	0.78	26.12	3.52	92.04	4.000	Yes	No	2.00
363	25.12	28.43	2.69	2.46	0.81	20.76	4.59	95.35	4.000	Yes	Yes	2.00
364	25.17	22.86	2.81	2.88	0.85	16.30	6.02	98.17	4.000	Yes	Yes	2.00
365	25.27	18.41	2.93	3.27	0.89	12.75	7.69	98.13	4.000	Yes	Yes	2.00
366	25.36	15.13	3.04	3.56	1.00	9.96	9.50	94.69	4.000	No	Yes	2.00
367	25.43	12.60	3.13	3.75	1.00	8.11	11.16	90.44	4.000	No	Yes	2.00
368	25.50	10.88	3.20	3.97	1.00	6.84	12.76	87.31	4.000	No	Yes	2.00
369	25.60	9.77	3.25	4.08	1.00	6.01	14.03	84.31	4.000	No	Yes	2.00
370	25.64	9.26	3.27	4.02	1.00	5.64	14.52	81.86	4.000	No	Yes	2.00
371	25.67	9.06	3.28	3.90	1.00	5.48	14.58	79.98	4.000	No	Yes	2.00
372	25.71	8.86	3.27	3.61	1.00	5.33	14.38	76.65	4.000	No	Yes	2.00
373	25.79	8.52	3.26	3.26	1.00	5.07	14.25	72.22	4.000	No	Yes	2.00
374	25.93	8.18	3.26	2.95	1.00	4.80	14.17	68.01	4.000	No	Yes	2.00
375	26.03	8.02	3.25	2.70	1.00	4.66	13.97	65.11	4.000	No	Yes	2.00
376	26.13	8.02	3.24	2.57	1.00	4.64	13.74	63.74	4.000	No	Yes	2.00
377	26.24	8.08	3.23	2.50	1.00	4.67	13.54	63.18	4.000	No	Yes	2.00
378	26.37	8.18	3.23	2.51	1.00	4.71	13.48	63.49	4.000	No	Yes	2.00
379	26.47	8.25	3.23	2.56	1.00	4.73	13.53	64.09	4.000	No	Yes	2.00
380	26.60	8.25	3.22	2.39	1.00	4.71	13.24	62.33	4.000	No	Yes	2.00
381	26.71	8.38	3.19	2.15	1.00	4.78	12.59	60.15	4.000	No	Yes	2.00
382	26.85	8.75	3.16	1.96	1.00	5.00	11.78	58.94	4.000	No	Yes	2.00
383	26.95	8.96	3.18	2.26	1.00	5.12	12.24	62.69	4.000	No	Yes	2.00
384	27.04	9.60	3.18	2.57	1.00	5.54	12.21	67.66	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	27.09	10.14	3.18	2.92	1.00	5.90	12.33	72.68	4.000	No	Yes	2.00
386	27.19	10.95	3.16	2.98	1.00	6.42	11.76	75.49	4.000	No	Yes	2.00
387	27.23	11.18	3.16	3.16	1.00	6.56	11.88	78.01	4.000	No	Yes	2.00
388	27.33	11.42	3.17	3.32	1.00	6.70	11.98	80.22	4.000	No	Yes	2.00
389	27.40	11.76	3.16	3.46	1.00	6.91	11.94	82.48	4.000	No	Yes	2.00
390	27.47	12.30	3.15	3.56	1.00	7.25	11.72	84.94	4.000	No	Yes	2.00
391	27.57	12.97	3.14	3.59	1.00	7.66	11.34	86.93	4.000	No	Yes	2.00
392	27.66	13.85	3.12	3.70	1.00	8.22	10.99	90.36	4.000	No	Yes	2.00
393	27.77	14.96	3.10	3.87	1.00	8.93	10.64	94.93	4.000	No	Yes	2.00
394	27.86	16.28	3.08	4.09	1.00	9.76	10.29	100.42	4.000	No	Yes	2.00
395	27.96	17.39	3.07	4.27	1.00	10.45	10.06	105.14	4.000	No	Yes	2.00
396	28.06	17.73	3.08	4.52	1.00	10.63	10.22	108.70	4.000	No	Yes	2.00
397	28.15	17.29	3.10	4.70	1.00	10.31	10.64	109.63	4.000	No	Yes	2.00
398	28.25	17.04	3.08	4.30	1.00	10.10	10.32	104.18	4.000	No	Yes	2.00
399	28.34	16.50	3.07	3.92	1.00	9.71	10.12	98.29	4.000	No	Yes	2.00
400	28.44	16.94	3.04	3.53	1.00	9.96	9.46	94.21	4.000	No	Yes	2.00
401	28.54	16.11	3.09	4.00	1.00	9.38	10.45	98.03	4.000	No	Yes	2.00
402	28.62	17.46	3.06	4.02	1.00	10.22	9.90	101.19	4.000	No	Yes	2.00
403	28.71	18.34	3.05	4.14	1.00	10.74	9.72	104.45	4.000	No	Yes	2.00
404	28.77	20.26	3.01	4.01	1.00	11.95	8.92	106.63	4.000	No	Yes	2.00
405	28.86	20.73	3.01	4.13	1.00	12.21	8.93	109.00	4.000	No	Yes	2.00
406	28.91	21.34	3.00	4.15	1.00	12.56	8.78	110.37	4.000	No	Yes	2.00
407	28.97	22.04	2.99	4.19	1.00	12.99	8.63	112.06	4.000	No	Yes	2.00
408	29.04	22.92	2.98	4.23	1.00	13.50	8.45	114.13	4.000	No	Yes	2.00
409	29.10	23.97	2.97	4.28	1.00	14.13	8.26	116.69	4.000	No	Yes	2.00
410	29.15	25.15	2.96	4.38	1.00	14.85	8.08	120.01	4.000	No	Yes	2.00
411	29.25	26.40	2.93	4.48	0.89	16.30	7.69	125.36	4.000	No	Yes	2.00
412	29.34	27.38	2.93	4.58	0.89	16.91	7.60	128.48	4.000	No	Yes	2.00
413	29.38	27.75	2.93	4.68	0.89	17.12	7.63	130.55	4.000	No	Yes	2.00
414	29.48	27.72	2.95	4.76	1.00	16.25	7.97	129.55	4.000	No	Yes	2.00
415	29.55	27.48	2.96	4.80	1.00	16.06	8.07	129.61	4.000	Yes	Yes	2.00
416	29.63	27.41	2.93	4.54	0.89	16.75	7.61	127.50	4.000	Yes	Yes	2.00
417	29.72	28.43	2.81	3.17	0.85	17.61	6.01	105.80	4.000	Yes	Yes	2.00
418	29.82	31.56	2.63	1.83	0.80	20.09	3.98	79.94	4.000	Yes	Yes	2.00
419	29.88	36.83	2.39	0.90	0.73	24.31	2.33	56.65	4.000	Yes	No	2.00
420	29.96	45.23	2.29	0.81	0.69	30.47	1.87	56.98	4.000	Yes	No	2.00
421	30.06	49.92	2.25	0.82	0.68	33.83	1.75	59.16	4.000	Yes	No	2.00
422	30.13	54.67	2.21	0.81	0.67	37.29	1.64	60.99	4.000	Yes	No	2.00
423	30.18	56.02	2.21	0.84	0.67	38.21	1.63	62.30	0.102	No	No	0.34
424	30.28	58.72	2.20	0.87	0.67	40.06	1.61	64.44	0.105	No	No	0.35
425	30.37	59.53	2.22	0.98	0.67	40.40	1.67	67.53	0.109	No	No	0.36
426	30.47	60.51	2.25	1.10	0.68	40.85	1.74	71.05	0.113	No	No	0.37
427	30.57	63.28	2.24	1.15	0.68	42.69	1.73	73.87	0.117	No	No	0.38
428	30.66	67.26	2.22	1.17	0.67	45.46	1.67	76.12	0.121	No	No	0.40
429	30.74	71.34	2.20	1.17	0.67	48.33	1.62	78.31	0.125	No	No	0.41
430	30.82	74.51	2.19	1.19	0.67	50.51	1.59	80.52	0.129	No	No	0.42
431	30.90	76.30	2.20	1.26	0.67	51.60	1.61	82.93	0.133	No	No	0.43
432	31.01	76.90	2.22	1.35	0.67	51.74	1.66	85.67	0.138	No	No	0.45

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	31.10	77.02	2.24	1.50	0.68	51.51	1.74	89.47	0.147	No	No	0.48
434	31.19	77.06	2.28	1.66	0.69	51.19	1.84	93.96	0.157	No	No	0.51
435	31.28	77.57	2.30	1.81	0.70	51.24	1.92	98.21	0.168	No	No	0.54
436	31.35	78.53	2.31	1.92	0.70	51.70	1.97	101.82	0.178	No	No	0.58
437	31.43	80.52	2.31	1.98	0.70	52.90	1.98	104.59	0.186	No	No	0.60
438	31.53	83.11	2.31	2.04	0.70	54.53	1.97	107.28	0.195	No	No	0.63
439	31.60	85.91	2.26	1.77	0.69	56.74	1.78	101.10	0.176	No	No	0.57
440	31.67	88.07	2.21	1.54	0.67	58.52	1.64	95.74	0.162	No	No	0.52
441	31.77	89.46	2.16	1.33	0.66	59.74	1.53	91.18	0.150	No	No	0.48
442	31.84	89.86	2.18	1.41	0.66	59.77	1.56	93.40	0.156	No	No	0.50
443	31.91	86.18	2.22	1.57	0.68	56.78	1.68	95.19	0.160	No	No	0.51
444	31.98	79.10	2.29	1.77	0.70	51.41	1.89	97.23	0.165	No	No	0.53
445	31.98	77.21	2.32	1.87	0.70	49.95	1.99	99.23	0.171	No	No	0.55
446	32.04	78.73	2.31	1.90	0.70	50.91	1.98	100.65	0.175	No	No	0.56
447	32.12	82.68	2.30	1.89	0.70	53.56	1.91	102.19	4.000	Yes	No	2.00
448	32.16	80.04	2.33	2.05	0.71	51.46	2.05	105.63	4.000	Yes	No	2.00
449	32.27	75.66	2.38	2.23	0.72	48.11	2.26	108.77	4.000	Yes	No	2.00
450	32.33	70.76	2.42	2.40	0.74	44.53	2.50	111.51	4.000	Yes	No	2.00
451	32.41	66.31	2.46	2.50	0.75	41.33	2.72	112.40	4.000	Yes	No	2.00
452	32.50	61.79	2.49	2.55	0.76	38.14	2.93	111.66	4.000	Yes	No	2.00
453	32.58	56.66	2.53	2.59	0.77	34.61	3.18	110.12	4.000	Yes	No	2.00
454	32.66	50.22	2.58	2.66	0.78	30.23	3.59	108.68	4.000	Yes	No	2.00
455	32.74	43.30	2.65	2.79	0.80	25.56	4.22	107.79	4.000	Yes	Yes	2.00
456	32.84	36.12	2.75	3.04	0.83	20.76	5.20	107.96	4.000	Yes	Yes	2.00
457	32.90	29.88	2.85	3.36	0.86	16.68	6.45	107.62	4.000	Yes	Yes	2.00
458	32.98	24.92	2.96	3.68	1.00	12.71	8.19	104.08	4.000	Yes	Yes	2.00
459	33.08	20.77	3.06	4.02	1.00	10.40	9.80	101.84	3.600	No	Yes	2.00
460	33.14	17.05	3.16	4.51	1.00	8.34	11.93	99.50	3.600	No	Yes	2.00
461	33.22	14.12	3.27	5.00	1.00	6.71	14.31	96.06	3.600	No	Yes	2.00
462	33.32	12.19	3.34	5.20	1.00	5.64	16.21	91.43	3.600	No	Yes	2.00
463	33.37	11.28	3.35	4.81	1.00	5.14	16.60	85.28	3.600	No	Yes	2.00
464	33.47	11.05	3.34	4.46	1.00	4.99	16.37	81.70	3.600	No	Yes	2.00
465	33.56	11.66	3.30	4.00	1.00	5.30	15.06	79.85	3.600	No	Yes	2.00
466	33.63	12.43	3.26	3.78	1.00	5.71	14.04	80.15	3.600	No	Yes	2.00
467	33.71	12.67	3.23	3.53	1.00	5.82	13.47	78.37	3.600	No	Yes	2.00
468	33.81	11.99	3.22	3.07	1.00	5.44	13.27	72.19	3.600	No	Yes	2.00
469	33.90	11.05	3.23	2.64	1.00	4.92	13.35	65.65	3.600	No	Yes	2.00
470	33.95	10.31	3.23	2.27	1.00	4.51	13.36	60.28	3.600	No	Yes	2.00
471	34.04	10.07	3.24	2.29	1.00	4.37	13.69	59.84	3.600	No	Yes	2.00
472	34.14	9.87	3.25	2.32	1.00	4.25	14.01	59.54	3.600	No	Yes	2.00
473	34.17	9.81	3.26	2.35	1.00	4.21	14.16	59.63	3.600	No	Yes	2.00
474	34.20	10.07	3.24	2.31	1.00	4.35	13.78	59.92	3.600	No	Yes	2.00
475	34.26	10.38	3.23	2.26	1.00	4.50	13.36	60.14	3.600	No	Yes	2.00
476	34.35	10.61	3.21	2.19	1.00	4.61	12.99	59.91	3.600	No	Yes	2.00
477	34.43	10.41	3.22	2.20	1.00	4.49	13.24	59.45	3.600	No	Yes	2.00
478	34.49	10.27	3.22	2.15	1.00	4.41	13.28	58.59	3.600	No	Yes	2.00
479	34.59	10.17	3.22	2.05	1.00	4.34	13.18	57.25	3.600	No	Yes	2.00
480	34.69	10.07	3.21	1.94	1.00	4.28	13.07	55.91	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	34.73	9.90	3.22	1.88	1.00	4.18	13.12	54.88	3.600	No	Yes	2.00
482	34.83	9.80	3.22	1.86	1.00	4.12	13.19	54.34	3.600	No	Yes	2.00
483	34.90	9.74	3.23	1.89	1.00	4.07	13.37	54.48	3.600	No	Yes	2.00
484	34.98	9.84	3.23	1.97	1.00	4.12	13.48	55.47	3.600	No	Yes	2.00
485	35.07	10.14	3.24	2.18	1.00	4.26	13.68	58.28	3.600	No	Yes	2.00
486	35.16	10.58	3.27	2.77	1.00	4.47	14.49	64.79	3.600	No	Yes	2.00
487	35.26	11.29	3.32	3.92	1.00	4.82	15.85	76.48	3.600	No	Yes	2.00
488	35.33	13.25	3.31	4.84	1.00	5.82	15.42	89.71	3.600	No	Yes	2.00
489	35.40	16.76	3.22	5.02	1.00	7.61	13.28	101.03	3.600	No	Yes	2.00
490	35.50	20.84	3.12	4.66	1.00	9.67	11.03	106.70	3.600	No	Yes	2.00
491	35.57	23.37	3.07	4.51	1.00	10.95	10.02	109.72	3.600	No	Yes	2.00
492	35.65	23.77	3.07	4.67	1.00	11.12	10.10	112.36	3.600	No	Yes	2.00
493	35.71	22.86	3.11	5.08	1.00	10.64	10.83	115.22	3.600	No	Yes	2.00
494	35.79	21.65	3.15	5.43	1.00	9.99	11.64	116.27	3.600	No	Yes	2.00
495	35.85	20.37	3.18	5.49	1.00	9.32	12.22	113.90	3.600	No	Yes	2.00
496	35.94	19.29	3.19	5.34	1.00	8.75	12.53	109.71	3.600	No	Yes	2.00
497	35.99	18.31	3.19	4.97	1.00	8.24	12.58	103.66	3.600	No	Yes	2.00
498	36.08	17.16	3.19	4.47	1.00	7.64	12.55	95.94	3.600	No	Yes	2.00
499	36.17	15.54	3.21	4.09	1.00	6.80	12.98	88.35	3.600	No	Yes	2.00
500	36.24	14.22	3.23	3.84	1.00	6.13	13.50	82.76	3.600	No	Yes	2.00
501	36.33	13.58	3.25	3.84	1.00	5.79	14.00	81.11	3.600	No	Yes	2.00
502	36.42	13.58	3.26	3.97	1.00	5.77	14.22	82.08	3.600	No	Yes	2.00
503	36.52	14.05	3.21	3.32	1.00	5.99	12.88	77.16	3.600	No	Yes	2.00
504	36.61	15.40	3.13	2.85	1.00	6.64	11.27	74.88	3.600	No	Yes	2.00
505	36.70	17.73	3.06	2.69	1.00	7.78	9.87	76.79	3.600	No	Yes	2.00
506	36.78	20.23	3.06	3.31	1.00	8.99	9.83	88.43	3.600	No	Yes	2.00
507	36.85	18.24	3.19	4.64	1.00	7.99	12.41	99.18	3.600	No	Yes	2.00
508	36.87	20.20	3.15	4.68	1.00	8.95	11.61	103.88	3.600	No	Yes	2.00
509	36.91	23.23	3.07	4.28	1.00	10.43	10.08	105.17	3.600	No	Yes	2.00
510	36.97	31.40	2.86	3.30	0.87	15.73	6.66	104.77	4.000	Yes	Yes	2.00
511	37.06	35.24	2.80	3.11	0.85	17.97	5.86	105.20	4.000	Yes	Yes	2.00
512	37.12	38.62	2.76	3.10	0.84	19.91	5.42	107.91	4.000	Yes	Yes	2.00
513	37.20	42.40	2.74	3.17	0.83	22.04	5.10	112.33	4.000	Yes	Yes	2.00
514	37.27	47.56	2.69	3.09	0.81	25.06	4.56	114.30	4.000	Yes	Yes	2.00
515	37.35	52.21	2.63	2.89	0.80	27.88	4.03	112.42	4.000	Yes	Yes	2.00
516	37.44	55.22	2.59	2.66	0.78	29.75	3.64	108.21	4.000	Yes	No	2.00
517	37.49	58.42	2.53	2.39	0.77	31.83	3.23	102.76	4.000	Yes	No	2.00
518	37.59	67.19	2.43	2.02	0.74	37.46	2.56	95.81	4.000	Yes	No	2.00
519	37.64	85.65	2.27	1.57	0.69	49.64	1.82	90.11	4.000	Yes	No	2.00
520	37.70	111.29	2.10	1.20	0.64	67.10	1.41	94.79	4.000	Yes	No	2.00
521	37.78	136.59	1.96	0.98	0.60	84.81	1.28	108.37	4.000	Yes	No	2.00
522	37.83	155.69	1.88	0.87	0.57	98.45	1.22	120.19	4.000	Yes	No	2.00
523	37.92	167.53	1.83	0.82	0.56	106.83	1.19	126.68	4.000	Yes	No	2.00
524	37.97	174.58	1.81	0.81	0.55	111.69	1.17	130.53	4.000	Yes	No	2.00
525	38.07	178.80	1.81	0.82	0.55	114.34	1.16	133.13	0.299	No	No	0.90
526	38.14	181.84	1.81	0.85	0.55	116.07	1.17	135.64	0.312	No	No	0.94
527	38.22	185.72	1.82	0.88	0.55	118.33	1.17	138.68	0.328	No	No	0.99
528	38.31	191.72	1.82	0.92	0.55	121.94	1.17	143.23	0.353	No	No	1.06

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	38.41	201.37	1.80	0.92	0.55	128.37	1.16	148.66	0.386	No	No	1.16
530	38.52	212.64	1.79	0.92	0.54	135.94	1.14	154.32	0.422	No	No	1.27
531	38.64	221.04	1.77	0.91	0.54	141.59	1.11	157.41	0.443	No	No	1.33
532	38.74	217.87	1.79	0.95	0.54	138.67	1.14	158.10	0.448	No	No	1.34
533	38.80	214.19	1.81	0.99	0.55	135.62	1.16	157.57	0.444	No	No	1.33
534	38.89	210.42	1.83	1.04	0.56	132.43	1.18	156.57	0.437	No	No	1.31
535	38.94	213.65	1.83	1.05	0.56	134.37	1.18	158.84	0.453	No	No	1.36
536	39.03	213.59	1.84	1.10	0.56	133.74	1.19	159.69	0.459	No	No	1.37
537	39.13	213.25	1.86	1.15	0.57	132.81	1.21	160.46	0.464	No	No	1.39
538	39.23	211.36	1.88	1.22	0.57	130.76	1.22	160.12	0.462	No	No	1.38
539	39.35	207.85	1.90	1.28	0.58	127.69	1.24	158.27	0.449	No	No	1.34
540	39.42	201.04	1.93	1.34	0.59	122.59	1.26	154.08	0.420	No	No	1.26
541	39.51	192.09	1.96	1.40	0.60	116.15	1.28	148.22	0.383	No	No	1.14
542	39.60	181.50	1.99	1.45	0.61	108.71	1.30	141.37	0.343	No	No	1.02
543	39.70	172.83	2.02	1.50	0.61	102.65	1.32	135.85	0.313	No	No	0.93
544	39.78	164.63	2.04	1.53	0.62	97.07	1.35	130.75	0.288	No	No	0.86
545	39.90	157.35	2.06	1.56	0.63	92.05	1.37	126.28	0.267	No	No	0.80
546	39.99	149.05	2.09	1.60	0.64	86.44	1.41	121.65	0.247	No	No	0.74
547	40.09	141.42	2.12	1.64	0.64	81.31	1.45	117.75	4.000	Yes	No	2.00
548	40.18	133.79	2.15	1.68	0.65	76.23	1.50	114.33	4.000	Yes	No	2.00
549	40.23	126.04	2.18	1.74	0.66	71.16	1.56	111.30	4.000	Yes	No	2.00
550	40.33	118.01	2.22	1.81	0.67	65.88	1.65	108.90	4.000	Yes	No	2.00
551	40.43	110.12	2.25	1.88	0.68	60.74	1.76	107.17	4.000	Yes	No	2.00
552	40.52	101.85	2.31	2.03	0.70	55.31	1.95	107.68	4.000	Yes	No	2.00
553	40.61	92.44	2.36	2.12	0.71	49.44	2.15	106.53	4.000	Yes	No	2.00
554	40.69	80.59	2.43	2.30	0.74	42.14	2.54	106.96	4.000	Yes	No	2.00
555	40.80	68.65	2.51	2.44	0.76	35.01	3.03	106.21	4.000	Yes	No	2.00
556	40.87	59.91	2.58	2.61	0.78	29.84	3.59	107.20	4.000	Yes	No	2.00
557	40.95	53.47	2.64	2.76	0.80	26.09	4.12	107.50	4.000	Yes	Yes	2.00
558	40.97	51.37	2.65	2.73	0.80	24.94	4.24	105.79	4.000	Yes	Yes	2.00
559	41.01	54.31	2.61	2.50	0.79	26.70	3.81	101.77	4.000	Yes	Yes	2.00
560	41.07	61.80	2.51	2.12	0.76	31.20	3.04	94.92	4.000	Yes	No	2.00
561	41.15	67.40	2.44	1.89	0.74	34.61	2.61	90.47	4.000	Yes	No	2.00
562	41.26	67.13	2.44	1.87	0.74	34.39	2.61	89.74	0.147	No	No	0.44
563	41.35	63.05	2.48	1.98	0.75	31.86	2.87	91.40	0.151	No	No	0.45
564	41.47	60.28	2.52	2.09	0.76	30.09	3.10	93.27	0.155	No	No	0.46
565	41.59	59.67	2.53	2.13	0.77	29.62	3.18	94.19	0.158	No	No	0.47
566	41.69	60.42	2.53	2.16	0.77	29.94	3.18	95.29	0.160	No	No	0.48
567	41.78	59.17	2.55	2.27	0.77	29.08	3.36	97.63	0.167	No	No	0.49
568	41.88	54.75	2.61	2.48	0.79	26.41	3.82	100.94	3.600	No	Yes	2.00
569	41.98	49.45	2.67	2.69	0.81	23.32	4.43	103.21	3.600	No	Yes	2.00
570	42.08	45.13	2.72	2.83	0.83	20.88	4.96	103.54	3.600	No	Yes	2.00
571	42.16	44.32	2.73	2.78	0.83	20.43	4.99	102.01	3.600	No	Yes	2.00
572	42.24	47.12	2.68	2.60	0.81	21.98	4.53	99.69	3.600	No	Yes	2.00
573	42.31	52.25	2.62	2.38	0.79	24.86	3.91	97.23	3.600	No	Yes	2.00
574	42.45	56.94	2.57	2.24	0.78	27.44	3.48	95.61	0.161	No	No	0.48
575	42.55	59.37	2.54	2.18	0.77	28.78	3.30	94.91	0.160	No	No	0.47
576	42.60	59.78	2.54	2.18	0.77	28.96	3.29	95.14	0.160	No	No	0.47

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	42.70	59.34	2.55	2.25	0.77	28.59	3.38	96.60	0.164	No	No	0.48
578	42.81	57.38	2.59	2.39	0.78	27.33	3.64	99.43	0.171	No	No	0.51
579	42.89	53.57	2.64	2.62	0.80	25.06	4.12	103.15	3.600	No	Yes	2.00
580	42.98	48.27	2.71	2.91	0.82	22.02	4.84	106.61	3.600	No	Yes	2.00
581	43.08	43.14	2.79	3.21	0.84	19.16	5.69	108.99	3.600	No	Yes	2.00
582	43.17	40.44	2.83	3.35	0.86	17.68	6.18	109.35	3.600	No	Yes	2.00
583	43.27	41.05	2.81	3.20	0.85	18.01	5.94	107.03	3.600	No	Yes	2.00
584	43.37	43.81	2.71	2.52	0.82	19.71	4.84	95.48	3.600	No	Yes	2.00
585	43.50	46.82	2.61	1.93	0.79	21.62	3.86	83.44	3.600	No	Yes	2.00
586	43.61	48.54	2.54	1.53	0.77	22.85	3.24	73.95	0.118	No	No	0.35
587	43.74	49.31	2.54	1.57	0.77	23.16	3.25	75.29	0.120	No	No	0.35
588	43.79	49.31	2.56	1.72	0.78	22.99	3.44	79.06	0.126	No	No	0.37
589	43.86	48.47	2.60	1.95	0.79	22.31	3.79	84.59	3.600	No	Yes	2.00
590	43.94	47.05	2.66	2.26	0.81	21.30	4.28	91.16	3.600	No	Yes	2.00
591	44.00	44.89	2.72	2.63	0.82	19.92	4.92	98.08	3.600	No	Yes	2.00
592	44.08	42.33	2.78	2.98	0.84	18.39	5.62	103.37	3.600	No	Yes	2.00
593	44.17	38.85	2.85	3.30	0.86	16.48	6.45	106.26	3.600	No	Yes	2.00
594	44.27	35.44	2.90	3.43	0.88	14.71	7.14	105.00	3.600	No	Yes	2.00
595	44.42	34.16	2.90	3.25	0.88	14.09	7.15	100.72	3.600	No	Yes	2.00
596	44.52	37.10	2.82	2.76	0.85	15.69	6.06	95.03	3.600	No	Yes	2.00
597	44.61	44.15	2.68	2.18	0.81	19.52	4.49	87.72	3.600	No	Yes	2.00
598	44.71	51.91	2.57	1.87	0.78	23.77	3.51	83.46	0.134	No	No	0.40
599	44.85	56.66	2.53	1.83	0.77	26.27	3.19	83.87	0.135	No	No	0.40
600	44.95	57.30	2.55	1.98	0.77	26.40	3.34	88.11	0.144	No	No	0.42
601	45.09	54.98	2.59	2.17	0.79	24.92	3.69	92.06	0.153	No	No	0.45
602	45.19	50.09	2.66	2.39	0.81	22.17	4.29	95.00	3.600	No	Yes	2.00
603	45.33	43.44	2.76	2.73	0.83	18.53	5.31	98.48	3.600	No	Yes	2.00
604	45.42	37.17	2.85	3.08	0.86	15.25	6.56	100.02	3.600	No	Yes	2.00
605	45.57	34.20	2.90	3.17	0.88	13.74	7.18	98.64	3.600	No	Yes	2.00
606	45.68	32.58	2.91	3.02	0.88	12.98	7.29	94.66	3.600	No	Yes	2.00
607	45.81	30.45	2.91	2.71	0.88	12.02	7.30	87.72	3.600	No	Yes	2.00
608	45.92	26.54	3.01	2.83	1.00	9.26	8.96	82.93	3.600	No	Yes	2.00
609	46.05	22.29	3.11	3.22	1.00	7.59	10.87	82.51	3.600	No	Yes	2.00
610	46.16	19.32	3.23	4.05	1.00	6.43	13.40	86.12	3.600	No	Yes	2.00
611	46.17	17.73	3.28	4.34	1.00	5.82	14.71	85.57	3.600	No	Yes	2.00
612	46.23	17.46	3.28	4.24	1.00	5.70	14.75	84.09	3.600	No	Yes	2.00
613	46.29	16.85	3.29	4.16	1.00	5.46	15.02	82.02	3.600	No	Yes	2.00
614	46.34	16.04	3.31	3.98	1.00	5.15	15.32	78.81	3.600	No	Yes	2.00
615	46.42	15.30	3.31	3.71	1.00	4.85	15.44	74.90	3.600	No	Yes	2.00
616	46.48	14.90	3.30	3.33	1.00	4.69	15.10	70.80	3.600	No	Yes	2.00
617	46.52	14.69	3.28	3.04	1.00	4.61	14.73	67.86	3.600	No	Yes	2.00
618	46.60	14.56	3.27	2.84	1.00	4.55	14.47	65.79	3.600	No	Yes	2.00
619	46.67	14.49	3.26	2.68	1.00	4.51	14.23	64.21	3.600	No	Yes	2.00
620	46.74	14.45	3.25	2.57	1.00	4.49	14.03	63.02	3.600	No	Yes	2.00
621	46.82	14.42	3.25	2.46	1.00	4.47	13.84	61.88	3.600	No	Yes	2.00
622	46.88	14.19	3.25	2.42	1.00	4.37	13.96	61.07	3.600	No	Yes	2.00
623	46.96	14.10	3.25	2.39	1.00	4.33	13.99	60.61	3.600	No	Yes	2.00
624	47.06	13.97	3.26	2.41	1.00	4.27	14.16	60.52	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	47.15	14.11	3.26	2.45	1.00	4.31	14.15	61.03	3.600	No	Yes	2.00
626	47.24	14.43	3.28	2.83	1.00	4.42	14.72	65.10	3.600	No	Yes	2.00
627	47.35	16.18	3.29	3.62	1.00	5.07	14.87	75.39	3.600	No	Yes	2.00
628	47.49	19.69	3.20	3.51	1.00	6.36	12.67	80.67	3.600	No	Yes	2.00
629	47.58	24.11	3.09	3.10	1.00	8.00	10.33	82.65	3.600	No	Yes	2.00
630	47.73	26.03	3.03	2.80	1.00	8.69	9.32	80.95	3.600	No	Yes	2.00
631	47.83	27.06	3.02	2.79	1.00	9.05	9.05	81.84	3.600	No	Yes	2.00
632	47.87	26.18	3.04	2.97	1.00	8.71	9.55	83.19	3.600	No	Yes	2.00
633	47.89	26.93	3.02	2.82	1.00	8.98	9.14	82.12	3.600	No	Yes	2.00
634	47.94	26.64	3.02	2.81	1.00	8.87	9.20	81.59	3.600	No	Yes	2.00
635	48.02	26.81	3.02	2.75	1.00	8.91	9.08	80.90	3.600	No	Yes	2.00
636	48.07	26.40	3.03	2.79	1.00	8.75	9.26	81.07	3.600	No	Yes	2.00
637	48.12	25.97	3.05	2.94	1.00	8.58	9.61	82.45	3.600	No	Yes	2.00
638	48.18	25.43	3.07	3.12	1.00	8.37	10.05	84.09	3.600	No	Yes	2.00
639	48.26	25.01	3.09	3.28	1.00	8.20	10.42	85.42	3.600	No	Yes	2.00
640	48.31	24.60	3.10	3.27	1.00	8.04	10.54	84.77	3.600	No	Yes	2.00
641	48.38	24.56	3.08	3.09	1.00	8.01	10.30	82.58	3.600	No	Yes	2.00
642	48.46	24.71	3.06	2.82	1.00	8.05	9.85	79.31	3.600	No	Yes	2.00
643	48.52	24.41	3.05	2.59	1.00	7.93	9.58	75.99	3.600	No	Yes	2.00
644	48.60	23.16	3.05	2.42	1.00	7.46	9.70	72.40	3.600	No	Yes	2.00
645	48.68	20.77	3.10	2.41	1.00	6.57	10.59	69.64	3.600	No	Yes	2.00
646	48.74	18.20	3.17	2.55	1.00	5.63	12.04	67.76	3.600	No	Yes	2.00
647	48.82	15.94	3.25	2.86	1.00	4.80	14.01	67.24	3.600	No	Yes	2.00
648	48.89	14.56	3.31	3.07	1.00	4.29	15.49	66.41	3.600	No	Yes	2.00
649	48.99	13.82	3.34	3.08	1.00	4.01	16.21	64.98	3.600	No	Yes	2.00
650	49.05	13.65	3.32	2.83	1.00	3.94	15.85	62.48	3.600	No	Yes	2.00
651	49.12	13.51	3.31	2.54	1.00	3.89	15.38	59.74	3.600	No	Yes	2.00
652	49.18	13.55	3.28	2.25	1.00	3.89	14.70	57.20	3.600	No	Yes	2.00
653	49.27	13.75	3.26	2.06	1.00	3.96	14.08	55.71	3.600	No	Yes	2.00
654	49.32	13.92	3.24	1.91	1.00	4.01	13.56	54.42	3.600	No	Yes	2.00
655	49.42	13.55	3.25	1.92	1.00	3.87	13.92	53.88	3.600	No	Yes	2.00
656	49.48	13.11	3.27	1.97	1.00	3.71	14.46	53.63	3.600	No	Yes	2.00
657	49.56	13.01	3.28	2.04	1.00	3.66	14.76	54.09	3.600	No	Yes	2.00
658	49.66	13.28	3.28	2.12	1.00	3.75	14.73	55.25	3.600	No	Yes	2.00
659	49.76	13.68	3.27	2.16	1.00	3.89	14.49	56.33	3.600	No	Yes	2.00
660	49.85	14.06	3.23	1.87	1.00	4.01	13.46	54.00	3.600	No	Yes	2.00
661	49.99	14.87	3.17	1.52	1.00	4.29	11.96	51.28	3.600	No	Yes	2.00
662	50.09	14.43	3.16	1.38	1.00	4.12	11.90	49.07	3.600	No	Yes	2.00
663	50.21	13.82	3.21	1.57	1.00	3.89	12.94	50.39	3.600	No	Yes	2.00
664	50.24	13.21	3.24	1.66	1.00	3.68	13.72	50.47	3.600	No	Yes	2.00
665	50.29	13.59	3.21	1.54	1.00	3.81	13.05	49.66	3.600	No	Yes	2.00
666	50.38	13.69	3.20	1.45	1.00	3.83	12.73	48.82	3.600	No	Yes	2.00
667	50.47	13.39	3.21	1.45	1.00	3.72	13.00	48.36	3.600	No	Yes	2.00
668	50.52	12.98	3.24	1.53	1.00	3.57	13.61	48.61	3.600	No	Yes	2.00
669	50.62	13.01	3.24	1.57	1.00	3.58	13.73	49.09	3.600	No	Yes	2.00
670	50.66	13.15	3.24	1.60	1.00	3.62	13.70	49.58	3.600	No	Yes	2.00
671	50.76	13.28	3.24	1.64	1.00	3.66	13.70	50.11	3.600	No	Yes	2.00
672	50.83	14.13	3.21	1.63	1.00	3.95	12.99	51.29	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	50.91	14.30	3.23	1.81	1.00	4.00	13.34	53.36	3.600	No	Yes	2.00
674	51.00	15.61	3.19	1.82	1.00	4.45	12.42	55.29	3.600	No	Yes	2.00
675	51.06	17.36	3.13	1.78	1.00	5.06	11.27	56.99	3.600	No	Yes	2.00
676	51.15	17.67	3.16	2.10	1.00	5.15	11.86	61.08	3.600	No	Yes	2.00
677	51.24	16.35	3.27	2.96	1.00	4.68	14.43	67.57	3.600	No	Yes	2.00
678	51.31	12.88	3.51	5.15	1.00	3.47	21.69	75.27	3.600	No	Yes	2.00
679	51.39	18.55	3.28	3.96	1.00	5.43	14.77	80.15	3.600	No	Yes	2.00
680	51.48	32.14	2.90	2.47	0.88	11.43	7.23	82.64	3.600	No	Yes	2.00
681	51.58	35.38	2.87	2.60	0.87	12.78	6.83	87.30	3.600	No	Yes	2.00
682	51.68	27.82	3.10	3.71	1.00	8.59	10.70	91.85	3.600	No	Yes	2.00
683	51.77	17.84	3.45	6.98	1.00	5.13	19.49	100.06	3.600	No	Yes	2.00
684	51.90	36.80	3.02	4.07	1.00	11.62	9.16	106.47	3.600	No	Yes	2.00
685	52.01	74.42	2.58	2.71	0.78	30.49	3.61	110.20	4.000	Yes	No	2.00
686	52.11	128.50	2.34	2.42	0.71	57.50	2.11	121.05	4.000	Yes	No	2.00
687	52.26	161.87	2.25	2.35	0.68	74.64	1.77	131.90	4.000	Yes	No	2.00
688	52.30	209.17	2.12	2.06	0.65	100.78	1.45	146.55	4.000	Yes	No	2.00
689	52.33	248.44	2.00	1.70	0.61	124.60	1.31	162.63	4.000	Yes	No	2.00
690	52.35	302.93	1.87	1.40	0.57	158.50	1.21	192.22	4.000	Yes	No	2.00
691	52.40	347.53	1.78	1.23	0.54	187.07	1.12	209.95	4.000	Yes	No	2.00
692	52.45	381.51	1.72	1.16	0.53	208.63	1.04	216.58	4.000	Yes	No	2.00
693	52.50	415.58	1.69	1.13	0.51	229.89	1.00	229.89	4.000	No	No	2.00
694	52.55	447.33	1.67	1.14	0.51	248.98	1.00	248.98	4.000	No	No	2.00
695	52.60	486.53	1.63	1.11	0.50	273.15	1.00	273.15	4.000	No	No	2.00
696	52.65	516.02	1.60	1.04	0.50	289.64	1.00	289.64	4.000	No	No	2.00
697	52.71	531.14	1.57	0.97	0.50	297.95	1.00	297.95	4.000	No	No	2.00
698	52.77	541.83	1.53	0.90	0.50	303.79	1.00	303.79	4.000	No	No	2.00
699	52.82	558.50	1.51	0.85	0.50	312.99	1.00	312.99	4.000	No	No	2.00
700	52.88	578.13	1.48	0.81	0.50	323.84	1.00	323.84	4.000	No	No	2.00
701	52.93	592.07	1.46	0.79	0.50	331.46	1.00	331.46	4.000	No	No	2.00
702	52.98	605.70	1.46	0.78	0.50	338.95	1.00	338.95	4.000	No	No	2.00
703	53.03	608.64	1.46	0.79	0.50	340.39	1.00	340.39	4.000	No	No	2.00
704	53.08	608.27	1.46	0.80	0.50	340.01	1.00	340.01	4.000	No	No	2.00
705	53.12	601.01	1.47	0.80	0.50	335.78	1.00	335.78	4.000	No	No	2.00
706	53.17	598.22	1.46	0.78	0.50	333.99	1.00	333.99	4.000	No	No	2.00
707	53.23	600.71	1.45	0.76	0.50	335.19	1.00	335.19	4.000	No	No	2.00
708	53.28	596.23	1.47	0.79	0.50	332.45	1.00	332.45	4.000	No	No	2.00
709	53.37	588.50	1.48	0.83	0.50	327.80	1.00	327.80	4.000	No	No	2.00
710	53.42	584.11	1.50	0.86	0.50	325.17	1.00	325.17	4.000	No	No	2.00
711	53.46	586.81	1.52	0.90	0.50	326.50	1.00	326.50	4.000	No	No	2.00
712	53.53	599.03	1.53	0.96	0.50	333.09	1.00	333.09	4.000	No	No	2.00
713	53.61	597.34	1.56	1.05	0.50	331.84	1.00	331.84	4.000	No	No	2.00
714	53.62	582.26	1.60	1.13	0.50	323.39	1.00	323.39	4.000	No	No	2.00
715	53.65	574.05	1.60	1.15	0.50	318.67	1.00	318.67	4.000	No	No	2.00
716	53.67	571.35	1.61	1.16	0.50	317.12	1.00	317.12	4.000	No	No	2.00
717	53.70	583.83	1.59	1.12	0.50	323.95	1.00	323.95	4.000	No	No	2.00
718	53.74	582.83	1.60	1.14	0.50	323.26	1.00	323.26	4.000	No	No	2.00
719	53.76	583.81	1.60	1.14	0.50	323.74	1.00	323.74	4.000	No	No	2.00
720	53.80	581.08	1.59	1.13	0.50	322.06	1.00	322.06	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	53.84	577.81	1.59	1.10	0.50	320.07	1.00	320.07	4.000	No	No	2.00
722	53.90	578.23	1.58	1.07	0.50	320.12	1.00	320.12	4.000	No	No	2.00
723	53.91	570.20	1.59	1.08	0.50	315.61	1.00	315.61	4.000	No	No	2.00
724	53.95	573.64	1.58	1.08	0.50	317.38	1.00	317.38	4.000	No	No	2.00
725	53.96	579.94	1.58	1.07	0.50	320.83	1.00	320.83	4.000	No	No	2.00
726	53.98	601.06	1.56	1.04	0.50	332.48	1.00	332.48	4.000	No	No	2.00
727	53.99	602.95	1.56	1.03	0.50	333.50	1.00	333.50	4.000	No	No	2.00
728	54.01	592.15	1.57	1.05	0.50	327.46	1.00	327.46	4.000	No	No	2.00
729	54.02	579.33	1.58	1.08	0.50	320.31	1.00	320.31	4.000	No	No	2.00
730	54.03	553.15	1.61	1.13	0.50	305.74	1.00	305.74	4.000	No	No	2.00
731	54.04	504.84	1.67	1.24	0.51	276.21	1.00	276.21	4.000	No	No	2.00
732	54.05	452.17	1.75	1.40	0.53	241.19	1.08	260.14	4.000	No	No	2.00
733	54.09	422.63	1.79	1.51	0.55	221.81	1.15	254.46	4.000	No	No	2.00
734	54.10	421.59	1.80	1.53	0.55	220.94	1.15	254.57	4.000	No	No	2.00
735	54.13	421.89	1.80	1.53	0.55	221.06	1.15	254.64	4.000	No	No	2.00
736	54.14	420.96	1.80	1.54	0.55	220.34	1.16	254.59	4.000	No	No	2.00
737	54.19	422.82	1.80	1.54	0.55	221.19	1.16	255.77	4.000	No	No	2.00
738	54.19	428.79	1.80	1.55	0.55	224.52	1.15	258.95	4.000	No	No	2.00
739	54.24	439.22	1.77	1.47	0.54	231.86	1.12	259.93	4.000	No	No	2.00
740	54.29	456.97	1.71	1.29	0.52	245.94	1.02	249.88	4.000	No	No	2.00
741	54.33	474.10	1.64	1.08	0.50	261.31	1.00	261.31	4.000	No	No	2.00
742	54.38	494.95	1.57	0.92	0.50	272.80	1.00	272.80	4.000	No	No	2.00
743	54.39	512.70	1.53	0.85	0.50	282.62	1.00	282.62	4.000	No	No	2.00
744	54.43	529.13	1.52	0.84	0.50	291.66	1.00	291.66	4.000	No	No	2.00
745	54.48	543.10	1.44	0.67	0.50	299.32	1.00	299.32	4.000	No	No	2.00
746	54.52	556.66	1.36	0.53	0.50	306.76	1.00	306.76	4.000	No	No	2.00
747	54.58	573.87	1.26	0.38	0.50	316.20	1.00	316.20	4.000	No	No	2.00
748	54.62	587.13	1.28	0.42	0.50	323.46	1.00	323.46	4.000	No	No	2.00
749	54.65	604.44	1.29	0.46	0.50	333.00	1.00	333.00	4.000	No	No	2.00
750	54.67	623.33	1.30	0.48	0.50	343.41	1.00	343.41	4.000	No	No	2.00
751	54.71	658.15	1.28	0.48	0.50	362.60	1.00	362.60	4.000	No	No	2.00
752	54.77	679.34	1.20	0.37	0.50	374.21	1.00	374.21	4.000	No	No	2.00
753	54.81	702.99	1.11	0.28	0.50	387.19	1.00	387.19	4.000	No	No	2.00
754	54.85	704.07	1.04	0.22	0.50	387.70	1.00	387.70	4.000	No	No	2.00
755	54.86	709.13	1.06	0.24	0.50	390.48	1.00	390.48	4.000	No	No	2.00
756	54.87	703.33	1.09	0.27	0.50	387.26	1.00	387.26	4.000	No	No	2.00
757	54.91	703.66	1.13	0.30	0.50	387.35	1.00	387.35	4.000	No	No	2.00
758	54.96	707.14	1.16	0.34	0.50	389.17	1.00	389.17	4.000	No	No	2.00
759	55.00	703.19	1.18	0.36	0.50	386.89	1.00	386.89	4.000	No	No	2.00
760	55.01	695.84	1.19	0.37	0.50	382.82	1.00	382.82	4.000	No	No	2.00
761	55.05	679.11	1.21	0.39	0.50	373.47	1.00	373.47	4.000	No	No	2.00
762	55.10	651.07	1.24	0.42	0.50	357.87	1.00	357.87	4.000	No	No	2.00
763	55.12	603.77	1.29	0.46	0.50	331.72	1.00	331.72	4.000	No	No	2.00
764	55.13	570.97	1.33	0.49	0.50	313.58	1.00	313.58	4.000	No	No	2.00
765	55.14	563.11	1.33	0.48	0.50	309.22	1.00	309.22	4.000	No	No	2.00
766	55.19	576.91	1.31	0.46	0.50	316.75	1.00	316.75	4.000	No	No	2.00
767	55.20	576.27	1.31	0.46	0.50	316.38	1.00	316.38	4.000	No	No	2.00
768	55.25	562.13	1.33	0.48	0.50	308.48	1.00	308.48	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	55.29	546.07	1.37	0.52	0.50	299.55	1.00	299.55	4.000	No	No	2.00
770	55.33	519.69	1.42	0.59	0.50	284.92	1.00	284.92	4.000	No	No	2.00
771	55.38	481.16	1.52	0.76	0.50	263.59	1.00	263.59	4.000	No	No	2.00
772	55.48	439.32	1.63	0.99	0.50	240.38	1.00	240.38	4.000	No	No	2.00
773	55.57	411.39	1.73	1.22	0.53	218.55	1.04	227.87	4.000	No	No	2.00
774	55.63	398.09	1.80	1.45	0.55	206.42	1.15	237.94	4.000	No	No	2.00
775	55.72	402.04	1.83	1.60	0.56	206.08	1.19	244.53	4.000	No	No	2.00
776	55.80	431.09	1.82	1.63	0.55	221.88	1.17	260.68	4.000	No	No	2.00
777	55.86	480.55	1.67	1.19	0.51	259.76	1.00	259.76	4.000	No	No	2.00
778	55.97	527.85	1.51	0.79	0.50	288.32	1.00	288.32	4.000	No	No	2.00
779	56.01	560.55	1.34	0.49	0.50	306.20	1.00	306.20	4.000	No	No	2.00
780	56.06	587.84	1.50	0.47	1.00	186.61	1.00	186.61	0.684	No	No	2.00
781	56.11	613.11	1.50	0.51	1.00	194.57	1.00	194.57	0.765	No	No	2.00
782	56.15	640.71	1.51	0.55	1.00	203.27	1.00	203.27	4.000	No	No	2.00
783	56.20	660.92	1.52	0.59	1.00	209.60	1.00	209.60	4.000	No	No	2.00
784	56.27	663.16	1.53	0.63	1.00	210.15	1.00	210.15	4.000	No	No	2.00
785	56.27	664.17	1.56	0.69	1.00	210.45	1.00	210.45	4.000	No	No	2.00
786	56.30	642.20	1.61	0.79	1.00	203.39	1.00	203.39	4.000	No	No	2.00
787	56.33	649.54	1.64	0.87	1.00	205.64	1.00	205.64	4.000	No	No	2.00
788	56.35	647.65	1.66	0.92	1.00	205.00	1.00	205.00	4.000	No	No	2.00
789	56.40	667.86	1.64	0.90	1.00	211.31	1.00	211.31	4.000	No	No	2.00
790	56.41	669.34	1.64	0.90	1.00	211.76	1.00	211.76	4.000	No	No	2.00
791	56.44	681.53	1.63	0.88	1.00	215.53	1.00	215.53	4.000	No	No	2.00
792	56.49	695.19	1.62	0.87	1.00	219.75	1.00	219.75	4.000	No	No	2.00
793	56.54	717.49	1.61	0.87	1.00	226.71	1.00	226.71	4.000	No	No	2.00
794	56.58	737.23	1.61	0.89	1.00	232.85	1.00	232.85	4.000	No	No	2.00
795	56.59	750.18	1.61	0.91	1.00	236.93	1.00	236.93	4.000	No	No	2.00
796	56.64	757.34	1.60	0.90	1.00	239.07	1.00	239.07	4.000	No	No	2.00
797	56.69	764.80	1.60	0.90	1.00	241.29	1.00	241.29	4.000	No	No	2.00
798	56.73	778.16	1.59	0.88	1.00	245.40	1.00	245.40	4.000	No	No	2.00
799	56.78	778.56	1.58	0.86	1.00	245.38	1.00	245.38	4.000	No	No	2.00
800	56.83	759.53	1.58	0.83	1.00	239.22	1.00	239.22	4.000	No	No	2.00
801	56.88	731.80	1.58	0.82	1.00	230.32	1.00	230.32	4.000	No	No	2.00
802	56.89	708.89	1.60	0.82	1.00	223.03	1.00	223.03	4.000	No	No	2.00
803	56.95	692.53	1.59	0.80	1.00	217.71	1.00	217.71	4.000	No	No	2.00
804	57.01	668.00	1.59	0.77	1.00	209.81	1.00	209.81	4.000	No	No	2.00
805	57.07	645.94	1.58	0.71	1.00	202.70	1.00	202.70	4.000	No	No	2.00
806	57.11	619.45	1.52	0.54	1.00	194.25	1.00	194.25	0.762	No	No	2.00
807	57.17	598.63	1.46	0.41	1.00	187.56	1.00	187.56	0.694	No	No	2.00
808	57.26	574.07	1.37	0.26	1.00	179.66	1.00	179.66	0.619	No	No	1.89
809	57.31	547.05	1.43	0.31	1.00	171.06	1.00	171.06	0.546	No	No	1.67
810	57.37	520.16	1.45	0.32	1.00	162.50	1.00	162.50	0.479	No	No	1.46
811	57.45	490.27	1.51	0.38	1.00	152.96	1.00	152.96	0.413	No	No	1.26
812	57.51	451.30	1.55	0.39	1.00	140.63	1.00	140.63	0.339	No	No	1.03
813	57.53	421.54	1.59	0.41	1.00	131.27	1.00	131.27	0.290	No	No	0.89
814	57.59	401.40	1.62	0.43	1.00	124.87	1.00	124.87	0.261	No	No	0.80
815	57.63	398.96	1.62	0.43	1.00	124.05	1.00	124.05	0.258	No	No	0.79
816	57.68	391.51	1.63	0.44	1.00	121.66	1.00	121.66	0.247	No	No	0.76

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
817	57.73	386.48	1.64	0.44	1.00	120.01	1.00	120.01	0.241	No	No	0.74
818	57.78	379.02	1.65	0.44	1.00	117.62	1.00	117.62	0.231	No	No	0.71
819	57.86	359.96	1.66	0.43	1.00	111.55	1.00	111.55	0.209	No	No	0.64
820	57.92	326.32	1.71	0.47	1.00	100.97	1.00	100.97	4.000	Yes	No	2.00
821	57.98	290.83	1.76	0.47	1.00	89.82	1.00	89.82	4.000	Yes	No	2.00
822	58.06	263.33	1.82	0.53	1.00	81.16	1.18	95.51	4.000	Yes	No	2.00
823	58.12	242.92	1.90	0.64	1.00	74.75	1.24	92.39	4.000	Yes	No	2.00
824	58.21	222.41	1.99	0.82	1.00	68.28	1.30	88.73	4.000	Yes	No	2.00
825	58.26	204.43	2.06	0.97	1.00	62.64	1.37	85.71	4.000	Yes	No	2.00
826	58.35	180.37	2.14	1.08	1.00	55.10	1.48	81.38	4.000	Yes	No	2.00
827	58.41	154.93	2.19	1.08	1.00	47.15	1.59	74.91	4.000	Yes	No	2.00
828	58.50	122.84	2.29	1.16	1.00	37.13	1.90	70.73	4.000	Yes	No	2.00
829	58.56	98.18	2.38	1.18	1.00	29.45	2.28	67.27	4.000	Yes	No	2.00
830	58.64	77.90	2.53	1.55	1.00	23.14	3.23	74.61	4.000	Yes	No	2.00
831	58.73	63.67	2.66	1.93	1.00	18.70	4.34	81.15	4.000	Yes	Yes	2.00
832	58.80	51.12	2.80	2.41	1.00	14.80	5.89	87.16	4.000	Yes	Yes	2.00
833	58.84	42.24	2.93	2.94	1.00	12.04	7.59	91.44	4.000	Yes	Yes	2.00
834	58.85	43.79	2.90	2.86	1.00	12.52	7.27	91.06	3.600	No	Yes	2.00
835	58.93	50.50	2.81	2.45	1.00	14.59	6.00	87.49	3.600	No	Yes	2.00
836	58.98	58.12	2.72	2.06	1.00	16.94	4.87	82.49	3.600	No	Yes	2.00
837	59.02	61.77	2.67	1.86	1.00	18.06	4.38	79.02	3.600	No	Yes	2.00
838	59.12	63.39	2.65	1.79	1.00	18.54	4.19	77.74	3.600	No	Yes	2.00
839	59.17	65.41	2.64	1.79	1.00	19.15	4.09	78.34	3.600	No	Yes	2.00
840	59.27	67.33	2.63	1.85	1.00	19.73	4.06	80.06	3.600	No	Yes	2.00
841	59.31	67.64	2.64	1.94	1.00	19.81	4.15	82.31	3.600	No	Yes	2.00
842	59.41	64.84	2.68	2.06	1.00	18.93	4.46	84.40	3.600	No	Yes	2.00
843	59.46	57.99	2.74	2.22	1.00	16.81	5.11	85.91	3.600	No	Yes	2.00
844	59.55	48.77	2.83	2.45	1.00	13.96	6.20	86.53	3.600	No	Yes	2.00
845	59.65	39.66	2.91	2.48	1.00	11.14	7.37	82.12	3.600	No	Yes	2.00
846	59.70	34.25	2.97	2.47	1.00	9.47	8.28	78.48	3.600	No	Yes	2.00
847	59.80	32.07	2.99	2.40	1.00	8.80	8.61	75.77	3.600	No	Yes	2.00
848	59.89	32.04	3.01	2.66	1.00	8.78	9.03	79.29	3.600	No	Yes	2.00
849	59.94	31.04	3.06	2.98	1.00	8.47	9.76	82.68	3.600	No	Yes	2.00
850	60.01	30.35	3.09	3.25	1.00	8.25	10.33	85.21	3.600	No	Yes	2.00
851	60.02	32.64	3.04	3.10	1.00	8.95	9.57	85.70	3.600	No	Yes	2.00
852	60.08	35.54	2.99	2.84	1.00	9.83	8.61	84.70	3.600	No	Yes	2.00
853	60.12	36.56	2.97	2.70	1.00	10.14	8.23	83.40	3.600	No	Yes	2.00
854	60.17	32.87	3.01	2.76	1.00	9.01	9.03	81.32	3.600	No	Yes	2.00
855	60.27	28.56	3.07	2.73	1.00	7.68	10.03	76.99	3.600	No	Yes	2.00
856	60.31	24.81	3.12	2.61	1.00	6.53	11.00	71.83	3.600	No	Yes	2.00
857	60.37	22.21	3.15	2.46	1.00	5.73	11.72	67.16	3.600	No	Yes	2.00
858	60.46	20.93	3.17	2.32	1.00	5.33	12.03	64.16	3.600	No	Yes	2.00
859	60.51	20.76	3.15	2.06	1.00	5.28	11.57	61.05	3.600	No	Yes	2.00
860	60.61	21.43	3.11	1.87	1.00	5.48	10.86	59.48	3.600	No	Yes	2.00
861	60.65	21.84	3.09	1.76	1.00	5.60	10.44	58.49	3.600	No	Yes	2.00
862	60.75	22.18	3.08	1.74	1.00	5.70	10.27	58.52	3.600	No	Yes	2.00
863	60.81	22.25	3.08	1.74	1.00	5.72	10.24	58.52	3.600	No	Yes	2.00
864	60.89	22.21	3.08	1.71	1.00	5.70	10.20	58.14	3.600	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
865	60.94	22.45	3.07	1.71	1.00	5.77	10.12	58.37	3.600	No	Yes	2.00
866	61.03	22.62	3.08	1.77	1.00	5.81	10.19	59.27	3.600	No	Yes	2.00
867	61.09	22.65	3.08	1.79	1.00	5.82	10.23	59.56	3.600	No	Yes	2.00
868	61.19	22.38	3.08	1.78	1.00	5.74	10.30	59.09	3.600	No	Yes	2.00
869	61.24	22.96	3.06	1.69	1.00	5.91	9.90	58.48	3.600	No	Yes	2.00
870	61.33	24.51	3.03	1.68	1.00	6.37	9.35	59.55	3.600	No	Yes	2.00
871	61.38	24.20	3.09	2.19	1.00	6.28	10.50	65.92	3.600	No	Yes	2.00
872	61.47	23.16	3.18	2.97	1.00	5.95	12.35	73.50	3.600	No	Yes	2.00
873	61.53	21.88	3.28	3.99	1.00	5.56	14.59	81.14	3.600	No	Yes	2.00
874	61.62	27.61	3.13	3.27	1.00	7.29	11.24	81.97	3.600	No	Yes	2.00
875	61.70	44.48	2.86	2.37	1.00	12.39	6.68	82.73	3.600	No	Yes	2.00
876	61.77	66.81	2.67	2.07	1.00	19.14	4.44	84.93	3.600	No	Yes	2.00
877	61.86	81.96	2.60	2.12	1.00	23.70	3.78	89.66	3.600	No	Yes	2.00
878	61.95	81.02	2.63	2.34	1.00	23.39	4.06	94.89	3.600	No	Yes	2.00
879	61.97	72.62	2.69	2.53	1.00	20.85	4.65	96.91	3.600	No	Yes	2.00
880	62.01	62.36	2.78	2.84	1.00	17.75	5.62	99.66	4.000	No	Yes	2.00
881	62.10	52.17	2.87	3.09	1.00	14.66	6.77	99.23	4.000	Yes	Yes	2.00
882	62.24	55.41	2.79	2.50	1.00	15.61	5.76	89.92	4.000	Yes	Yes	2.00
883	62.34	87.70	2.48	1.40	1.00	25.31	2.83	71.54	4.000	Yes	No	2.00
884	62.49	127.58	2.25	0.95	1.00	37.26	1.74	64.77	4.000	Yes	No	2.00
885	62.54	164.52	2.11	0.82	1.00	48.34	1.44	69.68	4.000	Yes	No	2.00
886	62.66	181.39	2.07	0.78	1.00	53.35	1.37	73.33	4.000	Yes	No	2.00
887	62.74	199.68	2.02	0.75	1.00	58.78	1.33	77.94	4.000	Yes	No	2.00
888	62.87	211.65	1.99	0.72	1.00	62.29	1.30	80.99	4.000	No	No	2.00
889	62.92	217.18	1.98	0.72	1.00	63.92	1.29	82.65	4.000	No	No	2.00
890	63.03	219.18	1.98	0.73	1.00	64.44	1.29	83.41	4.000	No	No	2.00
891	63.15	218.06	1.99	0.76	1.00	64.03	1.30	83.38	4.000	No	No	2.00
892	63.26	213.11	2.01	0.79	1.00	62.49	1.32	82.35	4.000	No	No	2.00
893	63.37	206.70	2.03	0.82	1.00	60.51	1.34	80.92	4.000	No	No	2.00
894	63.45	200.15	2.04	0.79	1.00	58.51	1.34	78.49	4.000	No	No	2.00
895	63.54	197.59	2.02	0.71	1.00	57.70	1.32	76.31	4.000	No	No	2.00
896	63.61	190.30	2.02	0.68	1.00	55.49	1.33	73.61	4.000	Yes	No	2.00
897	63.69	172.04	2.08	0.74	1.00	50.02	1.39	69.47	4.000	Yes	No	2.00
898	63.79	141.71	2.22	0.97	1.00	40.98	1.65	67.77	4.000	Yes	No	2.00
899	63.89	106.15	2.36	1.15	1.00	30.39	2.20	66.74	4.000	Yes	No	2.00
900	63.98	75.22	2.55	1.47	1.00	21.20	3.37	71.48	4.000	Yes	No	2.00
901	64.07	53.15	2.72	1.67	1.00	14.65	4.91	71.91	4.000	Yes	Yes	2.00
902	64.15	39.12	2.91	2.21	1.00	10.48	7.30	76.48	4.000	Yes	Yes	2.00
903	64.23	29.98	3.07	2.76	1.00	7.77	10.00	77.68	4.000	No	Yes	2.00
904	64.26	25.15	3.18	3.28	1.00	6.34	12.34	78.26	4.000	No	Yes	2.00
905	64.29	23.57	3.22	3.48	1.00	5.87	13.31	78.14	4.000	No	Yes	2.00
906	64.33	23.37	3.21	3.17	1.00	5.81	12.89	74.86	4.000	No	Yes	2.00
907	64.43	22.99	3.19	2.81	1.00	5.69	12.43	70.78	4.000	No	Yes	2.00
908	64.47	22.29	3.17	2.45	1.00	5.48	12.05	66.07	4.000	No	Yes	2.00
909	64.53	21.82	3.17	2.32	1.00	5.34	12.01	64.15	4.000	No	Yes	2.00
910	64.62	20.60	3.20	2.39	1.00	4.98	12.74	63.40	4.000	No	Yes	2.00
911	64.72	19.12	3.25	2.57	1.00	4.53	13.95	63.23	4.000	No	Yes	2.00
912	64.78	18.00	3.30	2.81	1.00	4.20	15.17	63.74	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
913	64.86	18.21	3.30	2.92	1.00	4.26	15.26	65.01	4.000	No	Yes	2.00
914	64.96	18.78	3.31	3.20	1.00	4.42	15.44	68.31	4.000	No	Yes	2.00
915	65.06	19.22	3.32	3.52	1.00	4.55	15.74	71.61	4.000	No	Yes	2.00
916	65.11	19.22	3.34	3.90	1.00	4.55	16.41	74.58	4.000	No	Yes	2.00
917	65.21	18.85	3.37	4.16	1.00	4.43	17.13	75.90	4.000	No	Yes	2.00
918	65.31	18.45	3.39	4.32	1.00	4.31	17.70	76.26	4.000	No	Yes	2.00
919	65.40	18.28	3.37	3.90	1.00	4.25	17.10	72.77	4.000	No	Yes	2.00
920	65.50	18.58	3.32	3.22	1.00	4.34	15.67	67.97	4.000	No	Yes	2.00
921	65.58	19.02	3.26	2.59	1.00	4.46	14.15	63.13	4.000	No	Yes	2.00
922	65.68	19.05	3.24	2.38	1.00	4.47	13.69	61.17	4.000	No	Yes	2.00
923	65.78	17.67	3.29	2.52	1.00	4.06	14.89	60.45	4.000	No	Yes	2.00
924	65.84	16.40	3.34	2.66	1.00	3.69	16.19	59.69	4.000	No	Yes	2.00
925	65.86	15.56	3.38	2.83	1.00	3.44	17.33	59.62	4.000	No	Yes	2.00
926	65.87	16.51	3.33	2.60	1.00	3.72	15.97	59.36	4.000	No	Yes	2.00
927	65.98	17.26	3.29	2.44	1.00	3.93	15.03	59.09	4.000	No	Yes	2.00
928	66.10	17.84	3.28	2.46	1.00	4.09	14.69	60.13	4.000	No	Yes	2.00
929	66.21	18.21	3.29	2.65	1.00	4.20	14.85	62.32	4.000	No	Yes	2.00
930	66.34	18.48	3.28	2.68	1.00	4.27	14.76	63.01	4.000	No	Yes	2.00
931	66.48	19.00	3.27	2.66	1.00	4.42	14.39	63.55	4.000	No	Yes	2.00
932	66.62	18.46	3.28	2.63	1.00	4.25	14.69	62.45	4.000	No	Yes	2.00
933	66.68	18.67	3.29	2.78	1.00	4.31	14.87	64.07	4.000	No	Yes	2.00
934	66.87	18.92	3.31	3.19	1.00	4.37	15.53	67.94	4.000	No	Yes	2.00
935	66.96	19.16	3.35	3.89	1.00	4.44	16.65	73.89	4.000	No	Yes	2.00
936	67.11	18.25	3.42	4.74	1.00	4.17	18.76	78.15	4.000	No	Yes	2.00
937	67.21	16.83	3.47	4.99	1.00	3.75	20.42	76.60	4.000	No	Yes	2.00
938	67.35	16.22	3.48	4.67	1.00	3.57	20.50	73.18	4.000	No	Yes	2.00
939	67.45	16.16	3.52	5.49	1.00	3.55	21.95	77.86	4.000	No	Yes	2.00
940	67.59	27.42	3.21	4.13	1.00	6.79	13.06	88.71	4.000	No	Yes	2.00
941	67.68	77.39	2.62	1.95	1.00	21.19	3.95	83.67	4.000	Yes	Yes	2.00
942	67.83	159.77	2.22	1.13	1.00	44.89	1.66	74.68	4.000	Yes	No	2.00
943	67.92	241.25	1.99	0.82	1.00	68.29	1.30	88.64	4.000	Yes	No	2.00
944	68.02	283.19	1.90	0.72	1.00	80.28	1.24	99.35	4.000	Yes	No	2.00
945	68.07	299.01	1.88	0.72	1.00	84.78	1.22	103.71	4.000	Yes	No	2.00
946	68.16	305.70	1.87	0.71	1.00	86.62	1.22	105.26	4.000	No	No	2.00
947	68.26	310.93	1.86	0.70	1.00	88.04	1.21	106.54	4.000	No	No	2.00
948	68.35	307.75	1.88	0.74	1.00	87.05	1.22	106.44	4.000	No	No	2.00
949	68.45	299.96	1.91	0.81	1.00	84.74	1.24	105.37	4.000	No	No	2.00
950	68.55	291.49	1.94	0.86	1.00	82.23	1.26	103.72	4.000	No	No	2.00
951	68.65	271.72	1.98	0.91	1.00	76.50	1.29	98.57	4.000	No	No	2.00
952	68.78	253.59	2.02	0.98	1.00	71.23	1.32	94.35	4.000	No	No	2.00
953	68.78	238.18	2.05	1.03	1.00	66.83	1.36	90.91	4.000	No	No	2.00
954	68.79	234.24	2.06	1.02	1.00	65.70	1.37	89.70	4.000	No	No	2.00
955	68.83	237.70	2.03	0.94	1.00	66.66	1.34	89.08	4.000	No	No	2.00
956	68.93	243.69	1.99	0.81	1.00	68.30	1.30	88.59	4.000	No	No	2.00
957	68.98	253.54	1.93	0.67	1.00	71.08	1.25	89.18	4.000	No	No	2.00
958	69.04	257.79	1.89	0.60	1.00	72.25	1.23	89.05	4.000	No	No	2.00
959	69.12	259.28	1.89	0.58	1.00	72.61	1.23	89.10	4.000	No	No	2.00
960	69.22	255.36	1.90	0.59	1.00	71.43	1.24	88.23	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
961	69.28	247.73	1.91	0.61	1.00	69.22	1.25	86.25	4.000	No	No	2.00
962	69.36	237.41	1.93	0.61	1.00	66.24	1.26	83.22	4.000	No	No	2.00
963	69.45	223.58	1.95	0.61	1.00	62.26	1.27	79.21	4.000	No	No	2.00
964	69.60	210.12	1.98	0.61	1.00	58.37	1.29	75.34	4.000	No	No	2.00
965	69.70	198.18	2.01	0.62	1.00	54.94	1.31	72.05	4.000	No	No	2.00
966	69.80	193.42	2.01	0.62	1.00	53.54	1.32	70.68	4.000	No	No	2.00
967	69.89	192.07	2.02	0.62	1.00	53.12	1.32	70.30	4.000	No	No	2.00
968	69.98	190.15	2.02	0.63	1.00	52.53	1.33	69.82	4.000	No	No	2.00
969	70.08	181.88	2.04	0.63	1.00	50.15	1.35	67.53	4.000	Yes	No	2.00
970	70.18	159.82	2.12	0.71	1.00	43.89	1.45	63.51	4.000	Yes	No	2.00
971	70.32	124.32	2.27	0.89	1.00	33.85	1.81	61.16	4.000	Yes	No	2.00
972	70.42	84.31	2.50	1.27	1.00	22.56	2.96	66.77	4.000	Yes	No	2.00
973	70.54	51.82	2.77	1.84	1.00	13.41	5.53	74.19	4.000	Yes	Yes	2.00
974	70.66	31.85	3.05	2.58	1.00	7.79	9.69	75.54	4.000	No	Yes	2.00
975	70.75	23.52	3.23	3.11	1.00	5.45	13.34	72.70	4.000	No	Yes	2.00
976	70.80	21.80	3.23	2.72	1.00	4.97	13.43	66.71	4.000	No	Yes	2.00
977	70.89	22.64	3.14	1.98	1.00	5.20	11.52	59.87	4.000	No	Yes	2.00
978	70.99	22.34	3.09	1.45	1.00	5.11	10.38	53.00	4.000	No	Yes	2.00
979	71.08	21.63	3.07	1.23	1.00	4.90	10.09	49.46	4.000	No	Yes	2.00
980	71.17	21.43	3.06	1.12	1.00	4.84	9.87	47.79	4.000	No	Yes	2.00
981	71.23	20.92	3.07	1.10	1.00	4.70	10.01	47.05	4.000	No	Yes	2.00
982	71.33	21.09	3.05	1.03	1.00	4.74	9.74	46.20	4.000	No	Yes	2.00
983	71.42	21.73	3.02	0.90	1.00	4.92	9.08	44.64	4.000	No	Yes	2.00
984	71.52	22.81	2.97	0.78	1.00	5.22	8.26	43.06	4.000	No	Yes	2.00
985	71.58	23.21	2.97	0.82	1.00	5.33	8.27	44.01	4.000	No	Yes	2.00
986	71.67	22.88	3.02	1.04	1.00	5.23	9.07	47.43	4.000	No	Yes	2.00
987	71.81	22.47	3.06	1.28	1.00	5.11	9.94	50.76	4.000	No	Yes	2.00
988	71.82	22.24	3.09	1.43	1.00	5.04	10.42	52.55	4.000	No	Yes	2.00
989	71.86	21.97	3.10	1.47	1.00	4.96	10.64	52.82	4.000	No	Yes	2.00
990	71.91	21.83	3.11	1.49	1.00	4.92	10.75	52.95	4.000	No	Yes	2.00
991	71.97	21.60	3.12	1.53	1.00	4.86	10.97	53.27	4.000	No	Yes	2.00
992	72.05	21.36	3.13	1.58	1.00	4.79	11.22	53.72	4.000	No	Yes	2.00
993	72.10	21.13	3.14	1.65	1.00	4.72	11.52	54.35	4.000	No	Yes	2.00
994	72.20	20.99	3.15	1.70	1.00	4.68	11.71	54.79	4.000	No	Yes	2.00
995	72.25	20.99	3.16	1.76	1.00	4.67	11.87	55.49	4.000	No	Yes	2.00
996	72.34	21.09	3.17	1.88	1.00	4.70	12.12	56.94	4.000	No	Yes	2.00
997	72.44	21.09	3.19	2.06	1.00	4.69	12.53	58.80	4.000	No	Yes	2.00
998	72.53	20.89	3.21	2.23	1.00	4.63	13.04	60.40	4.000	No	Yes	2.00
999	72.63	20.79	3.22	2.32	1.00	4.60	13.29	61.13	4.000	No	Yes	2.00
1000	72.69	20.48	3.23	2.36	1.00	4.51	13.55	61.14	4.000	No	Yes	2.00
1001	72.82	20.69	3.23	2.31	1.00	4.56	13.34	60.87	4.000	No	Yes	2.00
1002	72.92	21.13	3.20	2.18	1.00	4.68	12.83	60.05	4.000	No	Yes	2.00
1003	73.06	22.11	3.17	2.01	1.00	4.95	11.98	59.27	4.000	No	Yes	2.00
1004	73.16	22.34	3.16	2.02	1.00	5.01	11.90	59.57	4.000	No	Yes	2.00
1005	73.30	20.86	3.22	2.28	1.00	4.59	13.21	60.65	4.000	No	Yes	2.00
1006	73.35	19.88	3.26	2.50	1.00	4.32	14.25	61.53	4.000	No	Yes	2.00
1007	73.38	19.20	3.29	2.56	1.00	4.13	14.83	61.23	4.000	No	Yes	2.00
1008	73.47	20.02	3.25	2.39	1.00	4.35	13.95	60.67	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1009	73.53	20.08	3.24	2.33	1.00	4.37	13.79	60.20	4.000	No	Yes	2.00
1010	73.62	20.18	3.24	2.30	1.00	4.39	13.66	59.95	4.000	No	Yes	2.00
1011	73.71	19.95	3.25	2.36	1.00	4.32	13.95	60.28	4.000	No	Yes	2.00
1012	73.77	19.61	3.28	2.54	1.00	4.23	14.55	61.46	4.000	No	Yes	2.00
1013	73.86	19.34	3.30	2.76	1.00	4.15	15.21	63.08	4.000	No	Yes	2.00
1014	73.96	19.38	3.31	2.94	1.00	4.15	15.56	64.61	4.000	No	Yes	2.00
1015	74.06	19.58	3.32	3.02	1.00	4.20	15.60	65.59	4.000	No	Yes	2.00
1016	74.13	20.02	3.31	3.02	1.00	4.32	15.32	66.22	4.000	No	Yes	2.00
1017	74.24	20.36	3.30	3.02	1.00	4.41	15.12	66.66	4.000	No	Yes	2.00
1018	74.34	20.56	3.30	3.06	1.00	4.46	15.08	67.26	4.000	No	Yes	2.00
1019	74.44	20.42	3.31	3.15	1.00	4.42	15.35	67.81	4.000	No	Yes	2.00
1020	74.58	20.37	3.30	3.10	1.00	4.40	15.30	67.28	4.000	No	Yes	2.00
1021	74.68	20.30	3.27	2.60	1.00	4.38	14.35	62.80	4.000	No	Yes	2.00
1022	74.80	20.47	3.22	2.16	1.00	4.42	13.30	58.74	4.000	No	Yes	2.00
1023	74.92	20.26	3.21	1.96	1.00	4.35	12.97	56.43	4.000	No	Yes	2.00
1024	75.07	20.06	3.24	2.18	1.00	4.29	13.60	58.35	4.000	No	Yes	2.00
1025	75.08	19.75	3.26	2.32	1.00	4.21	14.10	59.34	4.000	No	Yes	2.00
1026	75.11	19.62	3.26	2.36	1.00	4.17	14.28	59.53	4.000	No	Yes	2.00
1027	75.16	19.55	3.27	2.45	1.00	4.15	14.53	60.28	4.000	No	Yes	2.00
1028	75.25	19.31	3.30	2.65	1.00	4.08	15.14	61.74	4.000	No	Yes	2.00
1029	75.32	19.14	3.32	2.86	1.00	4.03	15.69	63.23	4.000	No	Yes	2.00
1030	75.40	18.98	3.33	2.95	1.00	3.98	16.00	63.73	4.000	No	Yes	2.00
1031	75.50	18.81	3.33	2.87	1.00	3.93	15.96	62.77	4.000	No	Yes	2.00
1032	75.59	18.30	3.33	2.72	1.00	3.79	16.02	60.75	4.000	No	Yes	2.00
1033	75.69	17.56	3.34	2.60	1.00	3.59	16.34	58.60	4.000	No	Yes	2.00
1034	75.78	16.85	3.35	2.48	1.00	3.39	16.66	56.46	4.000	No	Yes	2.00
1035	75.88	16.41	3.36	2.34	1.00	3.27	16.73	54.66	4.000	No	Yes	2.00
1036	75.96	16.11	3.35	2.19	1.00	3.18	16.62	52.90	4.000	No	Yes	2.00
1037	76.05	16.04	3.34	2.06	1.00	3.16	16.34	51.65	4.000	No	Yes	2.00
1038	76.14	15.97	3.34	1.99	1.00	3.14	16.25	51.00	4.000	No	Yes	2.00
1039	76.26	16.07	3.34	1.99	1.00	3.16	16.16	51.09	4.000	No	Yes	2.00
1040	76.36	16.07	3.34	2.03	1.00	3.16	16.26	51.38	4.000	No	Yes	2.00
1041	76.41	16.07	3.34	2.04	1.00	3.16	16.31	51.50	4.000	No	Yes	2.00
1042	76.51	15.84	3.35	2.05	1.00	3.09	16.56	51.17	4.000	No	Yes	2.00
1043	76.65	15.50	3.37	2.09	1.00	2.99	17.04	51.04	4.000	No	Yes	2.00
1044	76.72	15.26	3.38	2.15	1.00	2.93	17.45	51.12	4.000	No	Yes	2.00
1045	76.79	15.16	3.39	2.21	1.00	2.90	17.72	51.39	4.000	No	Yes	2.00
1046	76.89	15.23	3.41	2.47	1.00	2.91	18.36	53.53	4.000	No	Yes	2.00
1047	76.98	15.47	3.48	3.62	1.00	2.98	20.80	61.89	4.000	No	Yes	2.00
1048	77.08	18.00	3.43	4.02	1.00	3.65	19.05	69.60	4.000	No	Yes	2.00
1049	77.18	22.18	3.34	4.06	1.00	4.77	16.19	77.29	4.000	No	Yes	2.00
1050	77.28	26.73	3.26	4.08	1.00	5.99	14.06	84.26	4.000	No	Yes	2.00
1051	77.37	27.88	3.29	4.98	1.00	6.30	14.87	93.62	4.000	No	Yes	2.00
1052	77.42	28.76	3.31	5.68	1.00	6.53	15.41	100.64	4.000	No	Yes	2.00
1053	77.42	30.22	3.30	5.86	1.00	6.92	15.09	104.44	4.000	No	Yes	2.00
1054	77.44	34.00	3.23	5.50	1.00	7.94	13.49	107.05	4.000	No	Yes	2.00
1055	77.48	37.40	3.19	5.36	1.00	8.85	12.47	110.31	4.000	No	Yes	2.00
1056	77.52	40.61	3.15	5.24	1.00	9.70	11.65	113.00	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1057	77.54	42.94	3.12	5.12	1.00	10.33	11.08	114.44	4.000	No	Yes	2.00
1058	77.57	43.37	3.12	5.18	1.00	10.44	11.07	115.54	4.000	No	Yes	2.00
1059	77.62	42.26	3.14	5.33	1.00	10.14	11.44	115.93	4.000	No	Yes	2.00
1060	77.65	40.10	3.17	5.56	1.00	9.55	12.10	115.64	4.000	No	Yes	2.00
1061	77.67	38.72	3.18	5.50	1.00	9.18	12.34	113.32	4.000	No	Yes	2.00
1062	77.71	37.91	3.19	5.40	1.00	8.96	12.41	111.24	4.000	No	Yes	2.00
1063	77.71	37.03	3.18	5.16	1.00	8.73	12.35	107.78	4.000	No	Yes	2.00
1064	77.76	34.77	3.20	5.10	1.00	8.12	12.85	104.25	4.000	No	Yes	2.00
1065	77.81	31.76	3.23	4.96	1.00	7.31	13.53	98.88	4.000	No	Yes	2.00
1066	77.90	29.03	3.27	4.92	1.00	6.57	14.40	94.60	4.000	No	Yes	2.00
1067	77.95	27.32	3.30	4.97	1.00	6.11	15.14	92.44	4.000	No	Yes	2.00
1068	78.01	26.34	3.32	5.03	1.00	5.84	15.63	91.29	4.000	No	Yes	2.00
1069	78.10	27.59	3.27	4.56	1.00	6.17	14.49	89.37	4.000	No	Yes	2.00
1070	78.16	36.29	3.07	3.14	1.00	8.49	9.98	84.71	4.000	No	Yes	2.00
1071	78.24	48.94	2.86	2.21	1.00	11.86	6.66	79.05	4.000	Yes	Yes	2.00
1072	78.29	64.83	2.68	1.67	1.00	16.10	4.54	73.14	4.000	Yes	Yes	2.00
1073	78.39	77.42	2.58	1.42	1.00	19.44	3.56	69.27	4.000	Yes	No	2.00
1074	78.47	87.30	2.52	1.35	1.00	22.06	3.11	68.51	4.000	Yes	No	2.00
1075	78.53	92.74	2.51	1.44	1.00	23.49	3.05	71.72	4.000	Yes	No	2.00
1076	78.62	94.25	2.54	1.65	1.00	23.88	3.25	77.71	4.000	Yes	No	2.00
1077	78.68	91.22	2.59	1.91	1.00	23.06	3.64	84.02	4.000	Yes	No	2.00
1078	78.69	92.97	2.61	2.12	1.00	23.52	3.81	89.57	4.000	Yes	Yes	2.00
1079	78.78	93.95	2.63	2.33	1.00	23.76	4.00	95.10	4.000	No	Yes	2.00
1080	78.81	94.86	2.65	2.61	1.00	24.00	4.25	102.04	4.000	No	Yes	2.00
1081	78.92	85.28	2.73	2.97	1.00	21.43	5.01	107.35	4.000	No	Yes	2.00
1082	79.03	72.83	2.81	3.21	1.00	18.11	5.93	107.43	4.000	No	Yes	2.00
1083	79.16	68.41	2.80	2.88	1.00	16.91	5.87	99.26	4.000	Yes	Yes	2.00
1084	79.26	78.39	2.68	2.21	1.00	19.54	4.53	88.45	4.000	Yes	Yes	2.00
1085	79.35	97.35	2.56	1.87	1.00	24.54	3.42	83.92	4.000	Yes	No	2.00
1086	79.45	114.43	2.50	1.84	1.00	29.03	2.95	85.78	4.000	Yes	No	2.00
1087	79.54	124.25	2.48	1.92	1.00	31.60	2.84	89.58	4.000	No	No	2.00
1088	79.64	131.23	2.47	1.97	1.00	33.41	2.75	91.91	4.000	No	No	2.00
1089	79.74	153.43	2.40	1.91	1.00	39.23	2.39	93.85	4.000	No	No	2.00
1090	79.88	186.93	2.31	1.77	1.00	48.00	1.98	94.86	4.000	No	No	2.00
1091	79.98	228.94	2.20	1.52	1.00	59.00	1.62	95.73	4.000	No	No	2.00
1092	80.12	248.77	2.14	1.34	1.00	64.13	1.48	95.14	4.000	No	No	2.00
1093	80.22	253.19	2.09	1.12	1.00	65.23	1.40	91.22	4.000	No	No	2.00
1094	80.36	244.79	2.06	0.97	1.00	62.94	1.37	86.07	4.000	No	No	2.00
1095	80.46	238.82	2.02	0.78	1.00	61.33	1.32	81.11	4.000	No	No	2.00
1096	80.60	231.84	1.99	0.66	1.00	59.42	1.30	77.21	4.000	No	No	2.00
1097	80.70	223.91	1.99	0.62	1.00	57.30	1.30	74.37	4.000	No	No	2.00
1098	80.83	213.12	2.02	0.65	1.00	54.42	1.32	72.04	4.000	Yes	No	2.00
1099	80.94	194.49	2.09	0.77	1.00	49.51	1.41	69.62	4.000	Yes	No	2.00
1100	81.01	177.96	2.15	0.85	1.00	45.17	1.50	67.91	4.000	Yes	No	2.00
1101	81.04	164.23	2.19	0.91	1.00	41.58	1.60	66.50	4.000	Yes	No	2.00
1102	81.09	158.43	2.21	0.93	1.00	40.05	1.65	65.97	4.000	Yes	No	2.00
1103	81.13	149.59	2.25	0.99	1.00	37.74	1.75	66.04	4.000	Yes	No	2.00
1104	81.18	136.87	2.31	1.12	1.00	34.41	1.98	67.98	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1105	81.23	123.31	2.39	1.33	1.00	30.87	2.34	72.13	4.000	Yes	No	2.00
1106	81.28	109.41	2.48	1.58	1.00	27.24	2.85	77.64	4.000	Yes	No	2.00
1107	81.33	98.17	2.57	1.89	1.00	24.30	3.46	84.19	4.000	Yes	No	2.00
1108	81.37	88.49	2.65	2.30	1.00	21.78	4.25	92.48	4.000	Yes	Yes	2.00
1109	81.42	81.24	2.73	2.74	1.00	19.88	5.05	100.46	4.000	Yes	Yes	2.00
1110	81.47	75.77	2.79	3.12	1.00	18.46	5.75	106.15	4.000	Yes	Yes	2.00
1111	81.52	71.99	2.83	3.36	1.00	17.47	6.25	109.13	4.000	Yes	Yes	2.00
1112	81.56	70.98	2.85	3.50	1.00	17.20	6.46	111.09	4.000	Yes	Yes	2.00
1113	81.61	70.58	2.86	3.61	1.00	17.08	6.60	112.75	4.000	No	Yes	2.00
1114	81.64	68.79	2.88	3.76	1.00	16.62	6.89	114.41	4.000	No	Yes	2.00
1115	81.70	62.18	2.94	4.16	1.00	14.89	7.85	116.91	4.000	No	Yes	2.00
1116	81.75	54.38	3.03	4.72	1.00	12.87	9.25	118.94	4.000	No	Yes	2.00
1117	81.79	46.89	3.11	5.33	1.00	10.92	10.91	119.14	4.000	No	Yes	2.00
1118	81.82	41.90	3.17	5.62	1.00	9.62	12.12	116.62	4.000	No	Yes	2.00
1119	81.86	37.62	3.22	5.76	1.00	8.51	13.21	112.49	4.000	No	Yes	2.00
1120	81.91	34.01	3.26	5.79	1.00	7.57	14.21	107.66	4.000	No	Yes	2.00
1121	81.95	30.63	3.30	5.75	1.00	6.70	15.27	102.27	4.000	No	Yes	2.00
1122	82.00	27.33	3.34	5.61	1.00	5.84	16.41	95.81	4.000	No	Yes	2.00
1123	82.09	24.26	3.39	5.48	1.00	5.04	17.74	89.46	4.000	No	Yes	2.00
1124	82.15	21.66	3.44	5.50	1.00	4.37	19.38	84.64	4.000	No	Yes	2.00
1125	82.19	19.83	3.48	5.52	1.00	3.89	20.80	81.03	4.000	No	Yes	2.00
1126	82.26	18.38	3.52	5.48	1.00	3.52	22.06	77.56	4.000	No	Yes	2.00
1127	82.34	17.00	3.56	5.45	1.00	3.16	23.49	74.17	4.000	No	Yes	2.00
1128	82.39	15.65	3.61	5.65	1.00	2.81	25.58	71.81	4.000	No	Yes	2.00
1129	82.48	14.77	3.64	5.76	1.00	2.58	27.14	69.97	4.000	No	Yes	2.00
1130	82.58	14.64	3.64	5.47	1.00	2.54	26.84	68.21	4.000	No	Yes	2.00
1131	82.62	14.74	3.62	5.09	1.00	2.57	25.95	66.60	4.000	No	Yes	2.00
1132	82.70	14.88	3.60	4.83	1.00	2.60	25.23	65.56	4.000	No	Yes	2.00
1133	82.77	14.81	3.59	4.65	1.00	2.58	24.98	64.46	4.000	No	Yes	2.00
1134	82.87	15.08	3.57	4.45	1.00	2.65	24.19	64.01	4.000	No	Yes	2.00
1135	82.96	16.23	3.51	3.90	1.00	2.94	21.57	63.38	4.000	No	Yes	2.00
1136	83.06	18.22	3.41	3.33	1.00	3.45	18.38	63.34	4.000	No	Yes	2.00
1137	83.16	21.39	3.29	2.70	1.00	4.26	14.82	63.10	4.000	No	Yes	2.00
1138	83.25	24.46	3.19	2.32	1.00	5.04	12.49	62.94	4.000	No	Yes	2.00
1139	83.34	27.20	3.11	2.06	1.00	5.74	10.91	62.57	4.000	No	Yes	2.00
1140	83.44	28.34	3.10	2.06	1.00	6.03	10.55	63.55	4.000	No	Yes	2.00
1141	83.54	28.75	3.10	2.14	1.00	6.12	10.60	64.89	4.000	No	Yes	2.00
1142	83.64	28.61	3.12	2.29	1.00	6.08	10.93	66.49	4.000	No	Yes	2.00
1143	83.73	27.70	3.15	2.52	1.00	5.84	11.68	68.29	4.000	No	Yes	2.00
1144	83.83	27.26	3.18	2.77	1.00	5.73	12.30	70.46	4.000	No	Yes	2.00
1145	83.85	26.83	3.21	3.11	1.00	5.62	13.07	73.38	4.000	No	Yes	2.00
1146	83.89	27.47	3.22	3.29	1.00	5.78	13.14	75.93	4.000	No	Yes	2.00
1147	83.94	28.11	3.24	3.78	1.00	5.94	13.69	81.26	4.000	No	Yes	2.00
1148	84.04	29.26	3.25	4.14	1.00	6.23	13.80	85.92	4.000	No	Yes	2.00
1149	84.09	30.40	3.25	4.44	1.00	6.51	13.83	90.10	4.000	No	Yes	2.00
1150	84.13	31.28	3.24	4.51	1.00	6.74	13.65	91.94	4.000	No	Yes	2.00
1151	84.18	31.68	3.24	4.64	1.00	6.83	13.70	93.61	4.000	No	Yes	2.00
1152	84.25	31.52	3.25	4.81	1.00	6.79	13.97	94.85	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1153	84.33	30.64	3.28	5.04	1.00	6.56	14.57	95.60	4.000	No	Yes	2.00
1154	84.37	29.46	3.31	5.29	1.00	6.26	15.33	95.90	4.000	No	Yes	2.00
1155	84.46	28.35	3.33	5.40	1.00	5.97	15.91	94.98	4.000	No	Yes	2.00
1156	84.52	27.50	3.34	5.37	1.00	5.75	16.25	93.43	4.000	No	Yes	2.00
1157	84.57	26.90	3.34	5.22	1.00	5.59	16.32	91.27	4.000	No	Yes	2.00
1158	84.67	26.52	3.34	5.14	1.00	5.49	16.38	90.00	4.000	No	Yes	2.00
1159	84.71	26.15	3.35	5.18	1.00	5.40	16.62	89.72	4.000	No	Yes	2.00
1160	84.81	25.58	3.38	5.48	1.00	5.25	17.32	90.86	4.000	No	Yes	2.00
1161	84.86	24.84	3.41	5.93	1.00	5.06	18.32	92.62	4.000	No	Yes	2.00
1162	84.91	24.06	3.44	6.37	1.00	4.86	19.36	94.03	4.000	No	Yes	2.00
1163	85.00	23.42	3.47	6.69	1.00	4.69	20.18	94.63	4.000	No	Yes	2.00
1164	85.05	22.81	3.48	6.79	1.00	4.53	20.72	93.94	4.000	No	Yes	2.00
1165	85.15	22.34	3.49	6.69	1.00	4.41	20.94	92.30	4.000	No	Yes	2.00
1166	85.19	21.80	3.49	6.36	1.00	4.27	20.88	89.13	4.000	No	Yes	2.00
1167	85.29	21.33	3.48	6.00	1.00	4.15	20.74	85.98	4.000	No	Yes	2.00
1168	85.35	20.72	3.49	5.75	1.00	3.99	20.84	83.14	4.000	No	Yes	2.00
1169	85.42	20.08	3.50	5.71	1.00	3.82	21.32	81.54	4.000	No	Yes	2.00
1170	85.48	19.40	3.52	5.78	1.00	3.65	22.03	80.45	4.000	No	Yes	2.00
1171	85.55	18.77	3.54	5.87	1.00	3.49	22.80	79.50	4.000	No	Yes	2.00
1172	85.63	18.19	3.56	5.98	1.00	3.34	23.58	78.76	4.000	No	Yes	2.00
1173	85.68	17.62	3.58	6.16	1.00	3.19	24.50	78.25	4.000	No	Yes	2.00
1174	85.77	17.18	3.60	6.34	1.00	3.08	25.34	78.03	4.000	No	Yes	2.00
1175	85.82	17.04	3.61	6.47	1.00	3.04	25.74	78.34	4.000	No	Yes	2.00
1176	85.89	17.42	3.60	6.38	1.00	3.13	25.13	78.79	4.000	No	Yes	2.00
1177	85.96	18.33	3.56	5.99	1.00	3.36	23.51	79.01	4.000	No	Yes	2.00
1178	86.03	19.71	3.49	5.35	1.00	3.71	21.16	78.44	4.000	No	Yes	2.00
1179	86.11	21.06	3.44	4.76	1.00	4.04	19.14	77.40	4.000	No	Yes	2.00
1180	86.16	22.11	3.39	4.32	1.00	4.30	17.71	76.21	4.000	No	Yes	2.00
1181	86.25	21.67	3.40	4.38	1.00	4.19	18.09	75.81	4.000	No	Yes	2.00
1182	86.36	19.98	3.45	4.62	1.00	3.76	19.76	74.32	4.000	No	Yes	2.00
1183	86.50	18.16	3.52	4.99	1.00	3.30	22.08	72.85	4.000	No	Yes	2.00
1184	86.51	17.25	3.55	5.00	1.00	3.07	23.09	70.91	4.000	No	Yes	2.00
1185	86.52	17.32	3.53	4.74	1.00	3.09	22.53	69.58	4.000	No	Yes	2.00
1186	86.57	17.35	3.51	4.25	1.00	3.10	21.58	66.80	4.000	No	Yes	2.00
1187	86.65	17.39	3.48	3.72	1.00	3.10	20.48	63.50	4.000	No	Yes	2.00
1188	86.71	17.35	3.45	3.31	1.00	3.09	19.65	60.73	4.000	No	Yes	2.00
1189	86.80	17.08	3.45	3.15	1.00	3.02	19.57	59.11	4.000	No	Yes	2.00
1190	86.90	16.48	3.46	3.06	1.00	2.87	20.04	57.42	4.000	No	Yes	2.00
1191	86.99	15.77	3.48	3.01	1.00	2.69	20.75	55.74	4.000	No	Yes	2.00
1192	87.04	15.26	3.50	2.94	1.00	2.56	21.24	54.32	4.000	No	Yes	2.00
1193	87.14	15.16	3.49	2.85	1.00	2.53	21.16	53.51	4.000	No	Yes	2.00
1194	87.19	15.36	3.48	2.77	1.00	2.58	20.70	53.36	4.000	No	Yes	2.00
1195	87.28	15.87	3.46	2.79	1.00	2.70	20.13	54.40	4.000	No	Yes	2.00
1196	87.38	16.51	3.45	2.81	1.00	2.86	19.47	55.67	4.000	No	Yes	2.00
1197	87.43	17.18	3.42	2.82	1.00	3.03	18.79	56.85	4.000	No	Yes	2.00
1198	87.52	17.76	3.40	2.76	1.00	3.17	18.12	57.36	4.000	No	Yes	2.00
1199	87.61	18.23	3.38	2.70	1.00	3.28	17.55	57.58	4.000	No	Yes	2.00
1200	87.66	18.53	3.37	2.63	1.00	3.35	17.13	57.47	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1201	87.76	18.57	3.37	2.58	1.00	3.36	17.00	57.12	4.000	No	Yes	2.00
1202	87.84	18.43	3.37	2.54	1.00	3.32	17.02	56.58	4.000	No	Yes	2.00
1203	87.91	18.13	3.37	2.53	1.00	3.25	17.27	56.08	4.000	No	Yes	2.00
1204	88.00	17.79	3.39	2.53	1.00	3.16	17.58	55.54	4.000	No	Yes	2.00
1205	88.11	17.46	3.40	2.56	1.00	3.07	17.98	55.23	4.000	No	Yes	2.00
1206	88.19	17.22	3.41	2.58	1.00	3.01	18.27	55.01	4.000	No	Yes	2.00
1207	88.25	17.08	3.41	2.59	1.00	2.98	18.42	54.79	4.000	No	Yes	2.00
1208	88.34	17.02	3.41	2.53	1.00	2.96	18.36	54.27	4.000	No	Yes	2.00
1209	88.44	16.98	3.41	2.45	1.00	2.94	18.20	53.59	4.000	No	Yes	2.00
1210	88.54	16.98	3.40	2.37	1.00	2.94	17.99	52.93	4.000	No	Yes	2.00
1211	88.64	16.95	3.40	2.33	1.00	2.93	17.92	52.52	4.000	No	Yes	2.00
1212	88.72	16.88	3.40	2.33	1.00	2.91	18.00	52.42	4.000	No	Yes	2.00
1213	88.82	16.82	3.40	2.36	1.00	2.89	18.16	52.53	4.000	No	Yes	2.00
1214	88.91	16.72	3.41	2.41	1.00	2.87	18.42	52.79	4.000	No	Yes	2.00
1215	89.01	16.62	3.42	2.47	1.00	2.84	18.68	53.02	4.000	No	Yes	2.00
1216	89.10	16.49	3.43	2.53	1.00	2.80	18.99	53.22	4.000	No	Yes	2.00
1217	89.19	16.32	3.44	2.53	1.00	2.76	19.19	52.91	4.000	No	Yes	2.00
1218	89.30	16.21	3.41	2.22	1.00	2.73	18.48	50.44	4.000	No	Yes	2.00
1219	89.39	16.31	3.39	2.02	1.00	2.75	17.80	48.98	4.000	No	Yes	2.00
1220	89.49	16.62	3.38	2.03	1.00	2.82	17.53	49.49	4.000	No	Yes	2.00
1221	89.59	16.90	3.41	2.39	1.00	2.89	18.25	52.76	4.000	No	Yes	2.00
1222	89.69	17.04	3.42	2.65	1.00	2.92	18.79	54.90	4.000	No	Yes	2.00
1223	89.73	17.68	3.40	2.64	1.00	3.08	18.14	55.86	4.000	No	Yes	2.00
1224	89.78	18.48	3.37	2.53	1.00	3.27	17.18	56.23	4.000	No	Yes	2.00
1225	89.83	19.36	3.34	2.42	1.00	3.49	16.22	56.56	4.000	No	Yes	2.00
1226	89.88	19.63	3.33	2.44	1.00	3.55	16.06	57.05	4.000	No	Yes	2.00
1227	89.93	19.86	3.33	2.48	1.00	3.61	16.01	57.77	4.000	No	Yes	2.00
1228	90.00	20.24	3.33	2.55	1.00	3.70	15.90	58.79	4.000	No	Yes	2.00
1229	90.07	20.88	3.31	2.57	1.00	3.85	15.53	59.82	4.000	No	Yes	2.00
1230	90.12	21.62	3.30	2.62	1.00	4.03	15.19	61.24	4.000	No	Yes	2.00
1231	90.22	22.26	3.29	2.71	1.00	4.19	15.01	62.84	4.000	No	Yes	2.00
1232	90.27	23.04	3.29	2.93	1.00	4.37	15.02	65.70	4.000	No	Yes	2.00
1233	90.36	24.99	3.26	2.95	1.00	4.85	14.09	68.34	4.000	No	Yes	2.00
1234	90.46	27.46	3.21	2.86	1.00	5.45	12.89	70.27	4.000	No	Yes	2.00
1235	90.50	29.28	3.17	2.76	1.00	5.89	12.05	71.01	4.000	No	Yes	2.00
1236	90.61	29.48	3.17	2.77	1.00	5.94	12.02	71.39	4.000	No	Yes	2.00
1237	90.66	28.70	3.18	2.82	1.00	5.75	12.38	71.12	4.000	No	Yes	2.00
1238	90.75	27.62	3.20	2.80	1.00	5.48	12.73	69.74	4.000	No	Yes	2.00
1239	90.84	26.17	3.22	2.78	1.00	5.12	13.28	67.94	4.000	No	Yes	2.00
1240	90.89	24.72	3.25	2.77	1.00	4.76	13.90	66.20	4.000	No	Yes	2.00
1241	90.99	23.48	3.28	2.82	1.00	4.45	14.63	65.12	4.000	No	Yes	2.00
1242	91.04	22.50	3.30	2.86	1.00	4.21	15.24	64.21	4.000	No	Yes	2.00
1243	91.14	21.59	3.33	2.94	1.00	3.99	15.98	63.69	4.000	No	Yes	2.00
1244	91.22	20.75	3.36	3.03	1.00	3.78	16.73	63.19	4.000	No	Yes	2.00
1245	91.28	19.83	3.39	3.13	1.00	3.55	17.61	62.55	4.000	No	Yes	2.00
1246	91.37	19.26	3.40	3.14	1.00	3.41	18.11	61.75	4.000	No	Yes	2.00
1247	91.47	18.99	3.40	3.07	1.00	3.34	18.18	60.75	4.000	No	Yes	2.00
1248	91.61	19.26	3.39	2.94	1.00	3.40	17.69	60.19	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1249	91.71	19.40	3.38	2.89	1.00	3.43	17.48	59.97	4.000	No	Yes	2.00
1250	91.81	19.50	3.38	2.88	1.00	3.45	17.39	60.03	4.000	No	Yes	2.00
1251	91.87	19.36	3.38	2.86	1.00	3.42	17.46	59.68	4.000	No	Yes	2.00
1252	92.00	19.38	3.36	2.58	1.00	3.42	16.82	57.50	4.000	No	Yes	2.00
1253	92.10	19.41	3.34	2.37	1.00	3.42	16.30	55.77	4.000	No	Yes	2.00
1254	92.20	19.62	3.32	2.25	1.00	3.47	15.85	54.98	4.000	No	Yes	2.00
1255	92.33	19.76	3.33	2.39	1.00	3.50	16.12	56.37	4.000	No	Yes	2.00
1256	92.38	19.89	3.34	2.50	1.00	3.53	16.27	57.43	4.000	No	Yes	2.00
1257	92.43	20.03	3.34	2.54	1.00	3.56	16.28	57.96	4.000	No	Yes	2.00
1258	92.48	19.98	3.35	2.62	1.00	3.55	16.52	58.57	4.000	No	Yes	2.00
1259	92.56	19.88	3.36	2.71	1.00	3.52	16.79	59.09	4.000	No	Yes	2.00
1260	92.63	19.64	3.37	2.79	1.00	3.46	17.17	59.41	4.000	No	Yes	2.00
1261	92.67	19.57	3.37	2.81	1.00	3.44	17.27	59.42	4.000	No	Yes	2.00
1262	92.72	19.54	3.38	2.81	1.00	3.43	17.30	59.38	4.000	No	Yes	2.00
1263	92.77	19.64	3.37	2.79	1.00	3.46	17.18	59.37	4.000	No	Yes	2.00
1264	92.86	19.84	3.37	2.77	1.00	3.50	16.99	59.49	4.000	No	Yes	2.00
1265	92.92	20.08	3.36	2.78	1.00	3.56	16.84	59.88	4.000	No	Yes	2.00
1266	92.97	20.21	3.37	2.90	1.00	3.59	17.01	61.03	4.000	No	Yes	2.00
1267	93.05	20.35	3.37	3.02	1.00	3.62	17.17	62.12	4.000	No	Yes	2.00
1268	93.10	20.62	3.37	3.09	1.00	3.68	17.13	63.07	4.000	No	Yes	2.00
1269	93.16	21.10	3.35	3.03	1.00	3.79	16.68	63.28	4.000	No	Yes	2.00
1270	93.25	21.70	3.33	2.92	1.00	3.94	16.06	63.20	4.000	No	Yes	2.00
1271	93.35	22.78	3.29	2.71	1.00	4.19	14.99	62.84	4.000	No	Yes	2.00
1272	93.40	23.19	3.27	2.59	1.00	4.29	14.52	62.27	4.000	No	Yes	2.00
1273	93.49	23.25	3.27	2.54	1.00	4.30	14.38	61.82	4.000	No	Yes	2.00
1274	93.56	22.71	3.28	2.58	1.00	4.17	14.77	61.55	4.000	No	Yes	2.00
1275	93.64	22.88	3.28	2.57	1.00	4.21	14.66	61.65	4.000	No	Yes	2.00
1276	93.73	23.63	3.27	2.60	1.00	4.38	14.34	62.81	4.000	No	Yes	2.00
1277	93.83	24.91	3.25	2.65	1.00	4.69	13.81	64.72	4.000	No	Yes	2.00
1278	93.88	26.43	3.23	2.80	1.00	5.05	13.44	67.85	4.000	No	Yes	2.00
1279	93.97	27.01	3.24	3.00	1.00	5.18	13.58	70.35	4.000	No	Yes	2.00
1280	94.07	26.43	3.27	3.36	1.00	5.04	14.48	72.95	4.000	No	Yes	2.00
1281	94.17	25.76	3.31	3.78	1.00	4.87	15.51	75.57	4.000	No	Yes	2.00
1282	94.26	26.70	3.29	3.75	1.00	5.09	15.04	76.60	4.000	No	Yes	2.00
1283	94.36	27.88	3.30	4.18	1.00	5.37	15.22	81.75	4.000	No	Yes	2.00
1284	94.45	29.47	3.30	4.56	1.00	5.75	15.14	87.02	4.000	No	Yes	2.00
1285	94.55	35.88	3.19	4.21	1.00	7.27	12.61	91.74	4.000	No	Yes	2.00
1286	94.64	48.46	3.00	3.11	1.00	10.27	8.71	89.52	4.000	No	Yes	2.00
1287	94.72	59.93	2.85	2.46	1.00	13.01	6.55	85.22	4.000	No	Yes	2.00
1288	94.74	73.87	2.72	1.96	1.00	16.33	4.89	79.85	4.000	No	Yes	2.00
1289	94.77	84.50	2.64	1.75	1.00	18.86	4.08	76.98	4.000	No	Yes	2.00
1290	94.85	97.35	2.56	1.57	1.00	21.92	3.39	74.39	4.000	No	No	2.00
1291	94.90	102.75	2.54	1.57	1.00	23.20	3.24	75.17	4.000	No	No	2.00
1292	94.95	105.32	2.54	1.66	1.00	23.80	3.27	77.89	4.000	No	No	2.00
1293	95.01	104.68	2.58	1.94	1.00	23.63	3.61	85.22	4.000	No	No	2.00
1294	95.09	100.83	2.64	2.34	1.00	22.70	4.16	94.37	4.000	No	Yes	2.00
1295	95.14	94.49	2.73	2.97	1.00	21.18	5.05	107.02	4.000	No	Yes	2.00
1296	95.23	86.42	2.82	3.64	1.00	19.25	6.10	117.34	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1297	95.29	78.06	2.91	4.43	1.00	17.25	7.36	126.89	4.000	No	Yes	2.00
1298	95.38	71.11	2.98	5.04	1.00	15.59	8.45	131.69	4.000	No	Yes	2.00
1299	95.43	67.53	3.02	5.36	1.00	14.73	9.06	133.43	4.000	No	Yes	2.00
1300	95.52	67.83	3.01	5.27	1.00	14.79	8.96	132.50	4.000	No	Yes	2.00
1301	95.57	70.23	2.98	4.89	1.00	15.35	8.40	128.95	4.000	No	Yes	2.00
1302	95.67	71.24	2.95	4.48	1.00	15.58	7.93	123.49	4.000	No	Yes	2.00
1303	95.77	66.52	2.97	4.36	1.00	14.45	8.22	118.72	4.000	No	Yes	2.00
1304	95.86	56.97	3.06	4.90	1.00	12.17	9.76	118.80	4.000	No	Yes	2.00
1305	95.95	52.94	3.09	5.00	1.00	11.21	10.40	116.56	4.000	No	Yes	2.00
1306	96.03	46.73	3.17	5.75	1.00	9.74	12.16	118.40	4.000	No	Yes	2.00
1307	96.11	51.55	3.12	5.30	1.00	10.87	10.92	118.64	4.000	No	Yes	2.00
1308	96.20	59.20	3.06	5.23	1.00	12.66	9.84	124.65	4.000	No	Yes	2.00
1309	96.30	80.15	2.90	4.31	1.00	17.59	7.15	125.73	4.000	Yes	Yes	2.00
1310	96.39	101.37	2.77	3.72	1.00	22.58	5.51	124.50	4.000	Yes	Yes	2.00
1311	96.50	122.96	2.67	3.23	1.00	27.64	4.35	120.31	4.000	Yes	Yes	2.00
1312	96.59	144.96	2.54	2.51	1.00	32.80	3.25	106.72	4.000	Yes	No	2.00
1313	96.69	164.86	2.41	1.87	1.00	37.45	2.44	91.36	4.000	Yes	No	2.00
1314	96.78	180.18	2.29	1.32	1.00	41.02	1.89	77.51	4.000	Yes	No	2.00
1315	96.87	185.95	2.24	1.13	1.00	42.35	1.72	72.98	4.000	Yes	No	2.00
1316	96.98	185.28	2.23	1.08	1.00	42.15	1.69	71.40	4.000	No	No	2.00
1317	97.02	177.79	2.26	1.14	1.00	40.38	1.78	71.90	4.000	No	No	2.00
1318	97.06	176.40	2.27	1.20	1.00	40.04	1.83	73.47	4.000	No	No	2.00
1319	97.12	175.60	2.30	1.30	1.00	39.84	1.91	76.16	4.000	No	No	2.00
1320	97.16	176.98	2.31	1.41	1.00	40.15	1.98	79.48	4.000	No	No	2.00
1321	97.21	173.67	2.35	1.58	1.00	39.35	2.13	83.99	4.000	No	No	2.00
1322	97.27	170.50	2.39	1.77	1.00	38.59	2.31	89.17	4.000	No	No	2.00
1323	97.33	168.21	2.42	1.93	1.00	38.04	2.46	93.67	4.000	No	No	2.00
1324	97.40	165.98	2.44	2.03	1.00	37.49	2.57	96.33	4.000	No	No	2.00
1325	97.45	163.92	2.45	2.09	1.00	37.00	2.64	97.51	4.000	Yes	No	2.00
1326	97.50	161.39	2.47	2.20	1.00	36.39	2.76	100.38	4.000	Yes	No	2.00
1327	97.58	155.82	2.50	2.38	1.00	35.06	2.99	104.78	4.000	Yes	No	2.00
1328	97.65	146.95	2.55	2.64	1.00	32.97	3.34	110.26	4.000	Yes	No	2.00
1329	97.69	134.43	2.60	2.87	1.00	30.04	3.79	113.95	4.000	Yes	Yes	2.00
1330	97.74	121.75	2.66	3.06	1.00	27.07	4.27	115.68	4.000	Yes	Yes	2.00
1331	97.81	110.51	2.71	3.22	1.00	24.44	4.76	116.42	4.000	Yes	Yes	2.00
1332	97.88	103.09	2.74	3.33	1.00	22.69	5.14	116.63	4.000	Yes	Yes	2.00
1333	97.93	108.66	2.70	3.05	1.00	23.98	4.67	111.98	4.000	Yes	Yes	2.00
1334	98.03	138.72	2.52	2.22	1.00	30.95	3.15	97.35	4.000	Yes	No	2.00
1335	98.15	182.62	2.33	1.53	1.00	41.12	2.03	83.50	4.000	Yes	No	2.00
1336	98.21	228.43	2.15	1.06	1.00	51.75	1.51	78.05	4.000	Yes	No	2.00
1337	98.32	264.20	2.03	0.81	1.00	60.00	1.34	80.19	4.000	Yes	No	2.00
1338	98.42	301.85	1.92	0.62	1.00	68.69	1.25	85.96	4.000	Yes	No	2.00
1339	98.47	349.59	1.79	0.45	1.00	79.73	1.00	79.73	4.000	Yes	No	2.00
1340	98.57	388.76	1.69	0.32	1.00	88.75	1.00	88.75	4.000	No	No	2.00
1341	98.70	411.84	1.61	0.24	1.00	94.00	1.00	94.00	4.000	No	No	2.00
1342	98.78	404.01	1.62	0.24	1.00	92.13	1.00	92.13	4.000	No	No	2.00
1343	98.85	372.43	1.67	0.27	1.00	84.79	1.00	84.79	4.000	No	No	2.00
1344	98.86	337.78	1.74	0.31	1.00	76.77	1.00	76.77	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (ft)	q_t (tsf)	I_c	Fr (%)	n	Q_{tn}	K_c	$Q_{tn,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1345	98.92	322.73	1.77	0.33	1.00	73.26	1.00	73.26	4.000	No	No	2.00
1346	98.98	318.48	1.78	0.34	1.00	72.24	1.00	72.24	4.000	Yes	No	2.00
1347	99.03	309.41	1.81	0.38	1.00	70.12	1.00	70.12	4.000	Yes	No	2.00
1348	99.11	281.64	1.90	0.48	1.00	63.67	1.00	63.67	4.000	Yes	No	2.00
1349	99.18	255.32	1.99	0.62	1.00	57.57	1.30	74.69	4.000	Yes	No	2.00
1350	99.23	231.33	2.09	0.83	1.00	52.01	1.41	73.25	4.000	Yes	No	2.00
1351	99.32	209.84	2.20	1.12	1.00	47.02	1.62	76.01	4.000	Yes	No	2.00
1352	99.37	189.39	2.31	1.49	1.00	42.29	1.96	83.05	4.000	Yes	No	2.00
1353	99.45	170.57	2.40	1.81	1.00	37.93	2.37	90.04	4.000	Yes	No	2.00
1354	99.56	157.24	2.47	2.08	1.00	34.83	2.76	96.01	4.000	Yes	No	2.00
1355	99.64	147.39	2.52	2.34	1.00	32.55	3.13	101.90	4.000	Yes	No	2.00
1356	99.71	140.04	2.57	2.64	1.00	30.84	3.53	108.77	4.000	Yes	No	2.00
1357	99.75	128.26	2.63	2.93	1.00	28.12	4.04	113.72	4.000	Yes	Yes	2.00
1358	99.90	116.32	2.70	3.25	1.00	25.35	4.67	118.27	4.000	Yes	Yes	2.00
1359	99.95	101.78	2.79	3.87	1.00	22.01	5.75	126.55	4.000	Yes	Yes	2.00
1360	100.04	116.32	2.73	3.67	1.00	25.32	5.03	127.45	4.000	Yes	Yes	2.00
1361	100.14	159.30	2.55	2.82	1.00	35.14	3.33	116.89	4.000	Yes	No	2.00
1362	100.14	204.99	2.39	2.20	1.00	45.59	2.33	106.43	4.000	Yes	No	2.00
1363	100.15	235.79	2.32	2.02	1.00	52.64	2.00	105.52	4.000	Yes	No	2.00
1364	100.19	258.80	2.30	2.10	1.00	57.89	1.93	111.71	4.000	Yes	No	2.00
1365	100.21	298.07	2.26	2.14	1.00	66.86	1.78	119.29	4.000	Yes	No	2.00
1366	100.24	351.88	2.06	1.31	1.00	79.16	1.37	108.37	4.000	Yes	No	2.00
1367	100.28	410.56	1.80	0.59	1.00	92.54	1.15	106.62	4.000	Yes	No	2.00
1368	100.31	470.98	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1369	100.33	508.57	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1370	100.38	524.63	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1371	100.39	526.55	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1372	100.43	531.78	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1373	100.48	522.24	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1374	100.53	509.38	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1375	100.57	496.12	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00
1376	100.60	497.27	N/A	0.00	1.00	-1.00	1.00	N/A	4.000	No	No	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (ft)
q_t: Total cone resistance
I_c: Soil behavior type index
Fr: Normalized friction ratio (%)
n: Stress exponent
Q_{tn}: Normalized cone resistance
K_c: Cone resistance correction factor due to fines
$Q_{tn,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
0.04	2.00	0.00	0.00	0.06	0.00	0.10	2.00	0.00	0.00	0.06	0.00
0.11	2.00	0.00	0.00	0.01	0.00	0.16	2.00	0.00	0.00	0.05	0.00
0.19	2.00	0.00	0.00	0.04	0.00	0.24	2.00	0.00	0.00	0.05	0.00
0.31	2.00	0.00	0.00	0.07	0.00	0.38	2.00	0.00	0.00	0.07	0.00
0.43	2.00	0.00	0.00	0.05	0.00	0.49	2.00	0.00	0.00	0.06	0.00
0.58	2.00	0.00	0.00	0.09	0.00	0.63	2.00	0.00	0.00	0.05	0.00
0.67	2.00	0.00	0.00	0.04	0.00	0.72	2.00	0.00	0.00	0.05	0.00
0.72	2.00	0.00	0.00	0.01	0.00	0.84	2.00	0.00	0.00	0.12	0.00
0.96	2.00	0.00	0.00	0.12	0.00	1.06	2.00	0.00	0.00	0.09	0.00
1.24	2.00	0.00	0.00	0.19	0.00	1.30	2.00	0.00	0.00	0.06	0.00
1.48	2.00	0.00	0.00	0.18	0.00	1.59	2.00	0.00	0.00	0.10	0.00
1.69	2.00	0.00	0.00	0.10	0.00	1.69	2.00	0.00	0.00	0.01	0.00
1.74	2.00	0.00	0.00	0.05	0.00	1.79	2.00	0.00	0.00	0.04	0.00
1.84	2.00	0.00	0.00	0.05	0.00	1.88	2.00	0.00	0.00	0.05	0.00
1.93	2.00	0.00	0.00	0.05	0.00	1.99	2.00	0.00	0.00	0.06	0.00
2.03	2.00	0.00	0.00	0.04	0.00	2.08	2.00	0.00	0.00	0.05	0.00
2.13	2.00	0.00	0.00	0.05	0.00	2.22	2.00	0.00	0.00	0.09	0.00
2.27	2.00	0.00	0.00	0.06	0.00	2.33	2.00	0.00	0.00	0.05	0.00
2.42	2.00	0.00	0.00	0.09	0.00	2.48	2.00	0.00	0.00	0.07	0.00
2.56	2.00	0.00	0.00	0.07	0.00	2.65	2.00	0.00	0.00	0.10	0.00
2.72	2.00	0.00	0.00	0.07	0.00	2.80	2.00	0.00	0.00	0.08	0.00
2.89	2.00	0.00	0.00	0.09	0.00	2.94	2.00	0.00	0.00	0.05	0.00
3.04	2.00	0.00	0.00	0.10	0.00	3.14	2.00	0.00	0.00	0.10	0.00
3.23	2.00	0.00	0.00	0.10	0.00	3.31	2.00	0.00	0.00	0.07	0.00
3.37	2.00	0.00	0.00	0.06	0.00	3.48	2.00	0.00	0.00	0.11	0.00
3.57	2.00	0.00	0.00	0.09	0.00	3.65	2.00	0.00	0.00	0.09	0.00
3.71	2.00	0.00	0.00	0.06	0.00	3.82	2.00	0.00	0.00	0.11	0.00
3.91	2.00	0.00	0.00	0.09	0.00	4.00	2.00	0.00	0.00	0.10	0.00
4.10	2.00	0.00	0.00	0.09	0.00	4.19	2.00	0.00	0.00	0.10	0.00
4.26	2.00	0.00	0.00	0.07	0.00	4.35	2.00	0.00	0.00	0.09	0.00
4.44	2.00	0.00	0.00	0.10	0.00	4.52	2.00	0.00	0.00	0.08	0.00
4.53	2.00	0.00	0.00	0.01	0.00	4.58	2.00	0.00	0.00	0.05	0.00
4.63	2.00	0.00	0.00	0.05	0.00	4.68	2.00	0.00	0.00	0.05	0.00
4.72	2.00	0.00	0.00	0.04	0.00	4.77	2.00	0.00	0.00	0.05	0.00
4.82	2.00	0.00	0.00	0.05	0.00	4.88	2.00	0.00	0.00	0.06	0.00
4.96	2.00	0.00	0.00	0.08	0.00	5.01	2.00	0.00	0.00	0.05	0.00
5.08	2.00	0.00	0.00	0.07	0.00	5.16	2.00	0.00	0.00	0.08	0.00
5.21	2.00	0.00	0.00	0.05	0.00	5.30	2.00	0.00	0.00	0.09	0.00
5.37	2.00	0.00	0.00	0.07	0.00	5.45	2.00	0.00	0.00	0.08	0.00
5.52	2.00	0.00	0.00	0.07	0.00	5.59	2.00	0.00	0.00	0.07	0.00
5.65	2.00	0.00	0.00	0.06	0.00	5.74	2.00	0.00	0.00	0.08	0.00
5.83	2.00	0.00	0.00	0.09	0.00	5.89	2.00	0.00	0.00	0.06	0.00
5.97	2.00	0.00	0.00	0.08	0.00	6.07	2.00	0.00	0.00	0.09	0.00
6.12	2.00	0.00	0.00	0.05	0.00	6.22	2.00	0.00	0.00	0.10	0.00
6.28	2.00	0.00	0.00	0.06	0.00	6.36	2.00	0.00	0.00	0.08	0.00
6.46	2.00	0.00	0.00	0.10	0.00	6.52	2.00	0.00	0.00	0.06	0.00
6.60	2.00	0.00	0.00	0.09	0.00	6.70	2.00	0.00	0.00	0.09	0.00
6.76	2.00	0.00	0.00	0.07	0.00	6.84	2.00	0.00	0.00	0.08	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
6.94	2.00	0.00	0.00	0.10	0.00	7.03	2.00	0.00	0.00	0.09	0.00
7.13	2.00	0.00	0.00	0.09	0.00	7.19	2.00	0.00	0.00	0.06	0.00
7.32	2.00	0.00	0.00	0.13	0.00	7.42	2.00	0.00	0.00	0.10	0.00
7.49	2.00	0.00	0.00	0.07	0.00	7.57	2.00	0.00	0.00	0.08	0.00
7.66	2.00	0.00	0.00	0.09	0.00	7.76	2.00	0.00	0.00	0.10	0.00
7.77	2.00	0.00	0.00	0.01	0.00	7.78	2.00	0.00	0.00	0.00	0.00
7.82	2.00	0.00	0.00	0.04	0.00	7.87	2.00	0.00	0.00	0.05	0.00
7.92	2.00	0.00	0.00	0.04	0.00	7.97	2.00	0.00	0.00	0.05	0.00
8.01	2.00	0.00	0.00	0.04	0.00	8.06	2.00	0.00	0.00	0.05	0.00
8.11	2.00	0.00	0.00	0.05	0.00	8.20	2.00	0.00	0.00	0.09	0.00
8.26	2.00	0.00	0.00	0.06	0.00	8.35	2.00	0.00	0.00	0.09	0.00
8.40	2.00	0.00	0.00	0.06	0.00	8.49	2.00	0.00	0.00	0.09	0.00
8.54	2.00	0.00	0.00	0.05	0.00	8.64	2.00	0.00	0.00	0.09	0.00
8.69	2.00	0.00	0.00	0.05	0.00	8.79	2.00	0.00	0.00	0.10	0.00
8.84	2.00	0.00	0.00	0.05	0.00	8.93	2.00	0.00	0.00	0.09	0.00
9.03	2.00	0.00	0.00	0.10	0.00	9.08	2.00	0.00	0.00	0.06	0.00
9.11	2.00	0.00	0.00	0.02	0.00	9.12	2.00	0.00	0.00	0.01	0.00
9.17	2.00	0.00	0.00	0.05	0.00	9.22	2.00	0.00	0.00	0.05	0.00
9.31	2.00	0.00	0.00	0.10	0.00	9.36	2.00	0.00	0.00	0.05	0.00
9.40	2.00	0.00	0.00	0.03	0.00	9.46	2.00	0.00	0.00	0.06	0.00
9.51	2.00	0.00	0.00	0.05	0.00	9.55	2.00	0.00	0.00	0.04	0.00
9.61	2.00	0.00	0.00	0.06	0.00	9.69	2.00	0.00	0.00	0.09	0.00
9.74	2.00	0.00	0.00	0.05	0.00	9.81	2.00	0.00	0.00	0.07	0.00
9.89	2.00	0.00	0.00	0.07	0.00	9.94	2.00	0.00	0.00	0.05	0.00
10.03	2.00	0.00	0.00	0.09	0.00	10.08	2.00	0.00	0.00	0.05	0.00
10.18	2.00	0.00	0.00	0.11	0.00	10.23	2.00	0.00	0.00	0.04	0.00
10.33	2.00	0.00	0.00	0.10	0.00	10.40	2.00	0.00	0.00	0.07	0.00
10.47	2.00	0.00	0.00	0.07	0.00	10.51	2.00	0.00	0.00	0.04	0.00
10.56	2.00	0.00	0.00	0.05	0.00	10.61	2.00	0.00	0.00	0.05	0.00
10.67	2.00	0.00	0.00	0.05	0.00	10.75	2.00	0.00	0.00	0.08	0.00
10.80	2.00	0.00	0.00	0.05	0.00	10.85	2.00	0.00	0.00	0.05	0.00
10.90	2.00	0.00	0.00	0.04	0.00	11.00	2.00	0.00	0.00	0.10	0.00
11.05	2.00	0.00	0.00	0.06	0.00	11.14	2.00	0.00	0.00	0.09	0.00
11.21	2.00	0.00	0.00	0.07	0.00	11.29	2.00	0.00	0.00	0.08	0.00
11.38	2.00	0.00	0.00	0.09	0.00	11.46	2.00	0.00	0.00	0.08	0.00
11.52	2.00	0.00	0.00	0.06	0.00	11.60	2.00	0.00	0.00	0.08	0.00
11.67	2.00	0.00	0.00	0.07	0.00	11.72	2.00	0.00	0.00	0.05	0.00
11.81	2.00	0.00	0.00	0.09	0.00	11.86	2.00	0.00	0.00	0.05	0.00
11.96	2.00	0.00	0.00	0.10	0.00	12.01	2.00	0.00	0.00	0.05	0.00
12.10	2.00	0.00	0.00	0.09	0.00	12.16	2.00	0.00	0.00	0.06	0.00
12.24	2.00	0.00	0.00	0.09	0.00	12.32	2.00	0.00	0.00	0.07	0.00
12.39	2.00	0.00	0.00	0.08	0.00	12.48	2.00	0.00	0.00	0.09	0.00
12.50	2.00	0.00	0.00	0.01	0.00	12.54	2.00	0.00	0.00	0.04	0.00
12.64	2.00	0.00	0.00	0.10	0.00	12.68	2.00	0.00	0.00	0.05	0.00
12.77	2.00	0.00	0.00	0.08	0.00	12.82	2.00	0.00	0.00	0.06	0.00
12.89	2.00	0.00	0.00	0.07	0.00	12.97	2.00	0.00	0.00	0.08	0.00
13.03	2.00	0.00	0.00	0.06	0.00	13.12	2.00	0.00	0.00	0.09	0.00
13.16	2.00	0.00	0.00	0.05	0.00	13.26	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
13.34	2.00	0.00	0.00	0.08	0.00	13.41	2.00	0.00	0.00	0.06	0.00
13.50	2.00	0.00	0.00	0.09	0.00	13.60	2.00	0.00	0.00	0.10	0.00
13.65	2.00	0.00	0.00	0.05	0.00	13.75	2.00	0.00	0.00	0.10	0.00
13.80	2.00	0.00	0.00	0.06	0.00	13.89	2.00	0.00	0.00	0.09	0.00
13.94	2.00	0.00	0.00	0.05	0.00	14.03	2.00	0.00	0.00	0.09	0.00
14.11	2.00	0.00	0.00	0.07	0.00	14.13	2.00	0.00	0.00	0.02	0.00
14.18	2.00	0.00	0.00	0.05	0.00	14.22	2.00	0.00	0.00	0.04	0.00
14.28	2.00	0.00	0.00	0.06	0.00	14.37	2.00	0.00	0.00	0.09	0.00
14.44	2.00	0.00	0.00	0.07	0.00	14.51	2.00	0.00	0.00	0.08	0.00
14.60	2.00	0.00	0.00	0.09	0.00	14.65	2.00	0.00	0.00	0.05	0.00
14.75	2.00	0.00	0.00	0.10	0.00	14.85	2.00	0.00	0.00	0.10	0.00
14.91	2.00	0.00	0.00	0.06	0.00	14.99	2.00	0.00	0.00	0.08	0.00
15.09	2.00	0.00	0.00	0.09	0.00	15.18	2.00	0.00	0.00	0.09	0.00
15.25	2.00	0.00	0.00	0.07	0.00	15.33	2.00	0.00	0.00	0.08	0.00
15.43	2.00	0.00	0.00	0.10	0.00	15.51	2.00	0.00	0.00	0.09	0.00
15.59	2.00	0.00	0.00	0.08	0.00	15.67	2.00	0.00	0.00	0.08	0.00
15.76	2.00	0.00	0.00	0.09	0.00	15.86	2.00	0.00	0.00	0.10	0.00
15.95	2.00	0.00	0.00	0.09	0.00	16.05	2.00	0.00	0.00	0.10	0.00
16.14	2.00	0.00	0.00	0.09	0.00	16.20	2.00	0.00	0.00	0.06	0.00
16.28	2.00	0.00	0.00	0.09	0.00	16.34	2.00	0.00	0.00	0.05	0.00
16.44	2.00	0.00	0.00	0.10	0.00	16.50	2.00	0.00	0.00	0.06	0.00
16.58	2.00	0.00	0.00	0.08	0.00	16.73	2.00	0.00	0.00	0.15	0.00
16.82	2.00	0.00	0.00	0.09	0.00	16.92	2.00	0.00	0.00	0.10	0.00
17.01	2.00	0.00	0.00	0.09	0.00	17.11	2.00	0.00	0.00	0.09	0.00
17.12	2.00	0.00	0.00	0.01	0.00	17.14	2.00	0.00	0.00	0.02	0.00
17.19	2.00	0.00	0.00	0.05	0.00	17.28	2.00	0.00	0.00	0.09	0.00
17.33	2.00	0.00	0.00	0.05	0.00	17.43	2.00	0.00	0.00	0.10	0.00
17.47	2.00	0.00	0.00	0.05	0.00	17.57	2.00	0.00	0.00	0.10	0.00
17.65	2.00	0.00	0.00	0.08	0.00	17.72	2.00	0.00	0.00	0.06	0.00
17.81	2.00	0.00	0.00	0.09	0.00	17.86	2.00	0.00	0.00	0.05	0.00
17.95	2.00	0.00	0.00	0.10	0.00	18.05	2.00	0.00	0.00	0.10	0.00
18.10	2.00	0.00	0.00	0.05	0.00	18.20	2.00	0.00	0.00	0.10	0.00
18.30	2.00	0.00	0.00	0.10	0.00	18.39	2.00	0.00	0.00	0.10	0.00
18.48	2.00	0.00	0.00	0.09	0.00	18.58	2.00	0.00	0.00	0.10	0.00
18.66	2.00	0.00	0.00	0.08	0.00	18.74	2.00	0.00	0.00	0.08	0.00
18.87	2.00	0.00	0.00	0.13	0.00	18.97	2.00	0.00	0.00	0.10	0.00
19.06	2.00	0.00	0.00	0.10	0.00	19.16	2.00	0.00	0.00	0.10	0.00
19.25	2.00	0.00	0.00	0.10	0.00	19.27	2.00	0.00	0.00	0.01	0.00
19.30	2.00	0.00	0.00	0.03	0.00	19.34	2.00	0.00	0.00	0.04	0.00
19.39	2.00	0.00	0.00	0.05	0.00	19.49	2.00	0.00	0.00	0.10	0.00
19.55	2.00	0.00	0.00	0.06	0.00	19.63	2.00	0.00	0.00	0.08	0.00
19.68	2.00	0.00	0.00	0.05	0.00	19.74	2.00	0.00	0.00	0.06	0.00
19.83	2.00	0.00	0.00	0.08	0.00	19.87	2.00	0.00	0.00	0.05	0.00
19.94	2.00	0.00	0.00	0.07	0.00	20.02	2.00	0.00	0.00	0.08	0.00
20.07	2.00	0.00	0.00	0.05	0.00	20.17	2.00	0.00	0.00	0.10	0.00
20.21	2.00	0.00	0.00	0.05	0.00	20.28	2.00	0.00	0.00	0.07	0.00
20.36	2.00	0.00	0.00	0.08	0.00	20.41	2.00	0.00	0.00	0.05	0.00
20.48	2.00	0.00	0.00	0.07	0.00	20.55	2.00	0.00	0.00	0.07	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
20.60	2.00	0.00	0.00	0.05	0.00	20.70	2.00	0.00	0.00	0.10	0.00
20.74	2.00	0.00	0.00	0.05	0.00	20.79	2.00	0.00	0.00	0.05	0.00
20.89	2.00	0.00	0.00	0.09	0.00	20.96	2.00	0.00	0.00	0.08	0.00
21.04	2.00	0.00	0.00	0.07	0.00	21.13	2.00	0.00	0.00	0.09	0.00
21.22	2.00	0.00	0.00	0.09	0.00	21.29	2.00	0.00	0.00	0.06	0.00
21.35	2.00	0.00	0.00	0.06	0.00	21.37	2.00	0.00	0.00	0.03	0.00
21.42	2.00	0.00	0.00	0.05	0.00	21.47	2.00	0.00	0.00	0.05	0.00
21.48	2.00	0.00	0.00	0.01	0.00	21.52	2.00	0.00	0.00	0.04	0.00
21.57	2.00	0.00	0.00	0.05	0.00	21.62	2.00	0.00	0.00	0.05	0.00
21.66	2.00	0.00	0.00	0.05	0.00	21.71	2.00	0.00	0.00	0.05	0.00
21.76	2.00	0.00	0.00	0.05	0.00	21.81	2.00	0.00	0.00	0.05	0.00
21.85	2.00	0.00	0.00	0.04	0.00	21.91	2.00	0.00	0.00	0.05	0.00
21.95	2.00	0.00	0.00	0.05	0.00	22.00	2.00	0.00	0.00	0.05	0.00
22.05	2.00	0.00	0.00	0.04	0.00	22.10	2.00	0.00	0.00	0.05	0.00
22.15	2.00	0.00	0.00	0.05	0.00	22.19	2.00	0.00	0.00	0.05	0.00
22.24	2.00	0.00	0.00	0.05	0.00	22.29	2.00	0.00	0.00	0.05	0.00
22.34	2.00	0.00	0.00	0.05	0.00	22.39	2.00	0.00	0.00	0.05	0.00
22.43	2.00	0.00	0.00	0.05	0.00	22.48	2.00	0.00	0.00	0.05	0.00
22.55	2.00	0.00	0.00	0.06	0.00	22.62	2.00	0.00	0.00	0.07	0.00
22.63	2.00	0.00	0.00	0.01	0.00	22.72	2.00	0.00	0.00	0.10	0.00
22.77	2.00	0.00	0.00	0.04	0.00	22.83	2.00	0.00	0.00	0.06	0.00
22.91	2.00	0.00	0.00	0.08	0.00	22.96	2.00	0.00	0.00	0.05	0.00
23.02	2.00	0.00	0.00	0.05	0.00	23.10	2.00	0.00	0.00	0.09	0.00
23.16	2.00	0.00	0.00	0.06	0.00	23.20	2.00	0.00	0.00	0.05	0.00
23.26	2.00	0.00	0.00	0.06	0.00	23.35	2.00	0.00	0.00	0.09	0.00
23.39	2.00	0.00	0.00	0.04	0.00	23.48	2.00	0.00	0.00	0.09	0.00
23.54	2.00	0.00	0.00	0.06	0.00	23.63	2.00	0.00	0.00	0.09	0.00
23.69	2.00	0.00	0.00	0.06	0.00	23.78	2.00	0.00	0.00	0.09	0.00
23.87	2.00	0.00	0.00	0.09	0.00	23.88	2.00	0.00	0.00	0.01	0.00
23.93	2.00	0.00	0.00	0.05	0.00	24.02	2.00	0.00	0.00	0.10	0.00
24.04	2.00	0.00	0.00	0.01	0.00	24.05	2.00	0.00	0.00	0.02	0.00
24.15	2.00	0.00	0.00	0.10	0.00	24.20	2.00	0.00	0.00	0.05	0.00
24.30	2.00	0.00	0.00	0.10	0.00	24.40	2.00	0.00	0.00	0.09	0.00
24.46	2.00	0.00	0.00	0.07	0.00	24.54	2.00	0.00	0.00	0.08	0.00
24.64	2.00	0.00	0.00	0.10	0.00	24.73	2.00	0.00	0.00	0.09	0.00
24.78	2.00	0.00	0.00	0.06	0.00	24.88	2.00	0.00	0.00	0.09	0.00
24.94	2.00	0.00	0.00	0.06	0.00	25.02	2.00	0.00	0.00	0.08	0.00
25.12	2.00	0.00	0.00	0.10	0.00	25.17	2.00	0.00	0.00	0.05	0.00
25.27	2.00	0.00	0.00	0.10	0.00	25.36	2.00	0.00	0.00	0.09	0.00
25.43	2.00	0.00	0.00	0.07	0.00	25.50	2.00	0.00	0.00	0.08	0.00
25.60	2.00	0.00	0.00	0.10	0.00	25.64	2.00	0.00	0.00	0.04	0.00
25.67	2.00	0.00	0.00	0.03	0.00	25.71	2.00	0.00	0.00	0.04	0.00
25.79	2.00	0.00	0.00	0.09	0.00	25.93	2.00	0.00	0.00	0.14	0.00
26.03	2.00	0.00	0.00	0.10	0.00	26.13	2.00	0.00	0.00	0.10	0.00
26.24	2.00	0.00	0.00	0.11	0.00	26.37	2.00	0.00	0.00	0.13	0.00
26.47	2.00	0.00	0.00	0.10	0.00	26.60	2.00	0.00	0.00	0.13	0.00
26.71	2.00	0.00	0.00	0.11	0.00	26.85	2.00	0.00	0.00	0.15	0.00
26.95	2.00	0.00	0.00	0.09	0.00	27.04	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
27.09	2.00	0.00	0.00	0.05	0.00	27.19	2.00	0.00	0.00	0.10	0.00
27.23	2.00	0.00	0.00	0.05	0.00	27.33	2.00	0.00	0.00	0.10	0.00
27.40	2.00	0.00	0.00	0.07	0.00	27.47	2.00	0.00	0.00	0.07	0.00
27.57	2.00	0.00	0.00	0.11	0.00	27.66	2.00	0.00	0.00	0.09	0.00
27.77	2.00	0.00	0.00	0.10	0.00	27.86	2.00	0.00	0.00	0.10	0.00
27.96	2.00	0.00	0.00	0.10	0.00	28.06	2.00	0.00	0.00	0.10	0.00
28.15	2.00	0.00	0.00	0.09	0.00	28.25	2.00	0.00	0.00	0.10	0.00
28.34	2.00	0.00	0.00	0.09	0.00	28.44	2.00	0.00	0.00	0.10	0.00
28.54	2.00	0.00	0.00	0.10	0.00	28.62	2.00	0.00	0.00	0.08	0.00
28.71	2.00	0.00	0.00	0.09	0.00	28.77	2.00	0.00	0.00	0.05	0.00
28.86	2.00	0.00	0.00	0.09	0.00	28.91	2.00	0.00	0.00	0.05	0.00
28.97	2.00	0.00	0.00	0.05	0.00	29.04	2.00	0.00	0.00	0.08	0.00
29.10	2.00	0.00	0.00	0.06	0.00	29.15	2.00	0.00	0.00	0.05	0.00
29.25	2.00	0.00	0.00	0.10	0.00	29.34	2.00	0.00	0.00	0.09	0.00
29.38	2.00	0.00	0.00	0.04	0.00	29.48	2.00	0.00	0.00	0.10	0.00
29.55	2.00	0.00	0.00	0.06	0.00	29.63	2.00	0.00	0.00	0.09	0.00
29.72	2.00	0.00	0.00	0.09	0.00	29.82	2.00	0.00	0.00	0.10	0.00
29.88	2.00	0.00	0.00	0.06	0.00	29.96	2.00	0.00	0.00	0.08	0.00
30.06	2.00	0.00	0.00	0.09	0.00	30.13	2.00	0.00	0.00	0.07	0.00
30.18	0.34	0.00	0.00	0.04	0.05	30.28	0.35	0.00	0.00	0.10	0.11
30.37	0.36	0.00	0.00	0.09	0.10	30.47	0.37	0.00	0.00	0.10	0.10
30.57	0.38	0.00	0.00	0.10	0.10	30.66	0.40	0.00	0.00	0.10	0.10
30.74	0.41	0.00	0.00	0.08	0.07	30.82	0.42	0.00	0.00	0.08	0.07
30.90	0.43	0.00	0.00	0.08	0.07	31.01	0.45	0.00	0.00	0.11	0.10
31.10	0.48	0.00	0.00	0.08	0.07	31.19	0.51	0.00	0.00	0.09	0.07
31.28	0.54	0.00	0.00	0.09	0.07	31.35	0.58	0.00	0.00	0.06	0.04
31.43	0.60	0.00	0.00	0.09	0.06	31.53	0.63	0.00	0.00	0.09	0.05
31.60	0.57	0.00	0.00	0.07	0.05	31.67	0.52	0.00	0.00	0.08	0.06
31.77	0.48	0.00	0.00	0.10	0.08	31.84	0.50	0.00	0.00	0.07	0.05
31.91	0.51	0.00	0.00	0.07	0.05	31.98	0.53	0.00	0.00	0.07	0.05
31.98	0.55	0.00	0.00	0.01	0.01	32.04	0.56	0.00	0.00	0.05	0.04
32.12	2.00	0.00	0.00	0.08	0.00	32.16	2.00	0.00	0.00	0.05	0.00
32.27	2.00	0.00	0.00	0.10	0.00	32.33	2.00	0.00	0.00	0.06	0.00
32.41	2.00	0.00	0.00	0.08	0.00	32.50	2.00	0.00	0.00	0.09	0.00
32.58	2.00	0.00	0.00	0.08	0.00	32.66	2.00	0.00	0.00	0.07	0.00
32.74	2.00	0.00	0.00	0.09	0.00	32.84	2.00	0.00	0.00	0.10	0.00
32.90	2.00	0.00	0.00	0.06	0.00	32.98	2.00	0.00	0.00	0.09	0.00
33.08	2.00	0.00	0.00	0.09	0.00	33.14	2.00	0.00	0.00	0.07	0.00
33.22	2.00	0.00	0.00	0.08	0.00	33.32	2.00	0.00	0.00	0.10	0.00
33.37	2.00	0.00	0.00	0.05	0.00	33.47	2.00	0.00	0.00	0.10	0.00
33.56	2.00	0.00	0.00	0.09	0.00	33.63	2.00	0.00	0.00	0.07	0.00
33.71	2.00	0.00	0.00	0.08	0.00	33.81	2.00	0.00	0.00	0.09	0.00
33.90	2.00	0.00	0.00	0.09	0.00	33.95	2.00	0.00	0.00	0.05	0.00
34.04	2.00	0.00	0.00	0.09	0.00	34.14	2.00	0.00	0.00	0.10	0.00
34.17	2.00	0.00	0.00	0.02	0.00	34.20	2.00	0.00	0.00	0.04	0.00
34.26	2.00	0.00	0.00	0.05	0.00	34.35	2.00	0.00	0.00	0.09	0.00
34.43	2.00	0.00	0.00	0.08	0.00	34.49	2.00	0.00	0.00	0.06	0.00
34.59	2.00	0.00	0.00	0.09	0.00	34.69	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
34.73	2.00	0.00	0.00	0.05	0.00	34.83	2.00	0.00	0.00	0.10	0.00
34.90	2.00	0.00	0.00	0.07	0.00	34.98	2.00	0.00	0.00	0.08	0.00
35.07	2.00	0.00	0.00	0.09	0.00	35.16	2.00	0.00	0.00	0.10	0.00
35.26	2.00	0.00	0.00	0.10	0.00	35.33	2.00	0.00	0.00	0.07	0.00
35.40	2.00	0.00	0.00	0.07	0.00	35.50	2.00	0.00	0.00	0.10	0.00
35.57	2.00	0.00	0.00	0.06	0.00	35.65	2.00	0.00	0.00	0.08	0.00
35.71	2.00	0.00	0.00	0.06	0.00	35.79	2.00	0.00	0.00	0.09	0.00
35.85	2.00	0.00	0.00	0.06	0.00	35.94	2.00	0.00	0.00	0.08	0.00
35.99	2.00	0.00	0.00	0.06	0.00	36.08	2.00	0.00	0.00	0.08	0.00
36.17	2.00	0.00	0.00	0.10	0.00	36.24	2.00	0.00	0.00	0.07	0.00
36.33	2.00	0.00	0.00	0.08	0.00	36.42	2.00	0.00	0.00	0.09	0.00
36.52	2.00	0.00	0.00	0.10	0.00	36.61	2.00	0.00	0.00	0.09	0.00
36.70	2.00	0.00	0.00	0.09	0.00	36.78	2.00	0.00	0.00	0.08	0.00
36.85	2.00	0.00	0.00	0.07	0.00	36.87	2.00	0.00	0.00	0.01	0.00
36.91	2.00	0.00	0.00	0.05	0.00	36.97	2.00	0.00	0.00	0.06	0.00
37.06	2.00	0.00	0.00	0.09	0.00	37.12	2.00	0.00	0.00	0.06	0.00
37.20	2.00	0.00	0.00	0.08	0.00	37.27	2.00	0.00	0.00	0.08	0.00
37.35	2.00	0.00	0.00	0.07	0.00	37.44	2.00	0.00	0.00	0.09	0.00
37.49	2.00	0.00	0.00	0.05	0.00	37.59	2.00	0.00	0.00	0.10	0.00
37.64	2.00	0.00	0.00	0.05	0.00	37.70	2.00	0.00	0.00	0.07	0.00
37.78	2.00	0.00	0.00	0.08	0.00	37.83	2.00	0.00	0.00	0.05	0.00
37.92	2.00	0.00	0.00	0.09	0.00	37.97	2.00	0.00	0.00	0.05	0.00
38.07	0.90	0.00	0.00	0.09	0.01	38.14	0.94	0.00	0.00	0.07	0.01
38.22	0.99	0.00	0.00	0.08	0.00	38.31	1.06	0.00	0.00	0.09	0.00
38.41	1.16	0.00	0.00	0.09	0.00	38.52	1.27	0.00	0.00	0.11	0.00
38.64	1.33	0.00	0.00	0.13	0.00	38.74	1.34	0.00	0.00	0.10	0.00
38.80	1.33	0.00	0.00	0.06	0.00	38.89	1.31	0.00	0.00	0.08	0.00
38.94	1.36	0.00	0.00	0.05	0.00	39.03	1.37	0.00	0.00	0.09	0.00
39.13	1.39	0.00	0.00	0.10	0.00	39.23	1.38	0.00	0.00	0.10	0.00
39.35	1.34	0.00	0.00	0.12	0.00	39.42	1.26	0.00	0.00	0.07	0.00
39.51	1.14	0.00	0.00	0.09	0.00	39.60	1.02	0.00	0.00	0.09	0.00
39.70	0.93	0.00	0.00	0.10	0.01	39.78	0.86	0.00	0.00	0.07	0.01
39.90	0.80	0.00	0.00	0.12	0.03	39.99	0.74	0.00	0.00	0.09	0.03
40.09	2.00	0.00	0.00	0.10	0.00	40.18	2.00	0.00	0.00	0.09	0.00
40.23	2.00	0.00	0.00	0.05	0.00	40.33	2.00	0.00	0.00	0.10	0.00
40.43	2.00	0.00	0.00	0.10	0.00	40.52	2.00	0.00	0.00	0.09	0.00
40.61	2.00	0.00	0.00	0.08	0.00	40.69	2.00	0.00	0.00	0.09	0.00
40.80	2.00	0.00	0.00	0.10	0.00	40.87	2.00	0.00	0.00	0.08	0.00
40.95	2.00	0.00	0.00	0.08	0.00	40.97	2.00	0.00	0.00	0.02	0.00
41.01	2.00	0.00	0.00	0.04	0.00	41.07	2.00	0.00	0.00	0.06	0.00
41.15	2.00	0.00	0.00	0.08	0.00	41.26	0.44	0.00	0.00	0.11	0.07
41.35	0.45	0.00	0.00	0.09	0.06	41.47	0.46	0.00	0.00	0.12	0.08
41.59	0.47	0.00	0.00	0.12	0.07	41.69	0.48	0.00	0.00	0.10	0.06
41.78	0.49	0.00	0.00	0.09	0.05	41.88	2.00	0.00	0.00	0.10	0.00
41.98	2.00	0.00	0.00	0.10	0.00	42.08	2.00	0.00	0.00	0.10	0.00
42.16	2.00	0.00	0.00	0.08	0.00	42.24	2.00	0.00	0.00	0.08	0.00
42.31	2.00	0.00	0.00	0.07	0.00	42.45	0.48	0.00	0.00	0.14	0.08
42.55	0.47	0.00	0.00	0.09	0.05	42.60	0.47	0.00	0.00	0.05	0.03

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
42.70	0.48	0.00	0.00	0.10	0.06	42.81	0.51	0.00	0.00	0.11	0.06
42.89	2.00	0.00	0.00	0.08	0.00	42.98	2.00	0.00	0.00	0.10	0.00
43.08	2.00	0.00	0.00	0.10	0.00	43.17	2.00	0.00	0.00	0.09	0.00
43.27	2.00	0.00	0.00	0.10	0.00	43.37	2.00	0.00	0.00	0.09	0.00
43.50	2.00	0.00	0.00	0.14	0.00	43.61	0.35	0.00	0.00	0.10	0.07
43.74	0.35	0.00	0.00	0.13	0.09	43.79	0.37	0.00	0.00	0.05	0.03
43.86	2.00	0.00	0.00	0.07	0.00	43.94	2.00	0.00	0.00	0.07	0.00
44.00	2.00	0.00	0.00	0.06	0.00	44.08	2.00	0.00	0.00	0.08	0.00
44.17	2.00	0.00	0.00	0.09	0.00	44.27	2.00	0.00	0.00	0.10	0.00
44.42	2.00	0.00	0.00	0.14	0.00	44.52	2.00	0.00	0.00	0.10	0.00
44.61	2.00	0.00	0.00	0.10	0.00	44.71	0.40	0.00	0.00	0.09	0.06
44.85	0.40	0.00	0.00	0.14	0.08	44.95	0.42	0.00	0.00	0.10	0.06
45.09	0.45	0.00	0.00	0.14	0.07	45.19	2.00	0.00	0.00	0.10	0.00
45.33	2.00	0.00	0.00	0.14	0.00	45.42	2.00	0.00	0.00	0.10	0.00
45.57	2.00	0.00	0.00	0.14	0.00	45.68	2.00	0.00	0.00	0.11	0.00
45.81	2.00	0.00	0.00	0.14	0.00	45.92	2.00	0.00	0.00	0.11	0.00
46.05	2.00	0.00	0.00	0.13	0.00	46.16	2.00	0.00	0.00	0.10	0.00
46.17	2.00	0.00	0.00	0.01	0.00	46.23	2.00	0.00	0.00	0.06	0.00
46.29	2.00	0.00	0.00	0.05	0.00	46.34	2.00	0.00	0.00	0.05	0.00
46.42	2.00	0.00	0.00	0.09	0.00	46.48	2.00	0.00	0.00	0.05	0.00
46.52	2.00	0.00	0.00	0.05	0.00	46.60	2.00	0.00	0.00	0.08	0.00
46.67	2.00	0.00	0.00	0.07	0.00	46.74	2.00	0.00	0.00	0.07	0.00
46.82	2.00	0.00	0.00	0.08	0.00	46.88	2.00	0.00	0.00	0.06	0.00
46.96	2.00	0.00	0.00	0.09	0.00	47.06	2.00	0.00	0.00	0.09	0.00
47.15	2.00	0.00	0.00	0.10	0.00	47.24	2.00	0.00	0.00	0.09	0.00
47.35	2.00	0.00	0.00	0.10	0.00	47.49	2.00	0.00	0.00	0.14	0.00
47.58	2.00	0.00	0.00	0.09	0.00	47.73	2.00	0.00	0.00	0.15	0.00
47.83	2.00	0.00	0.00	0.10	0.00	47.87	2.00	0.00	0.00	0.04	0.00
47.89	2.00	0.00	0.00	0.02	0.00	47.94	2.00	0.00	0.00	0.05	0.00
48.02	2.00	0.00	0.00	0.08	0.00	48.07	2.00	0.00	0.00	0.05	0.00
48.12	2.00	0.00	0.00	0.05	0.00	48.18	2.00	0.00	0.00	0.06	0.00
48.26	2.00	0.00	0.00	0.08	0.00	48.31	2.00	0.00	0.00	0.06	0.00
48.38	2.00	0.00	0.00	0.06	0.00	48.46	2.00	0.00	0.00	0.08	0.00
48.52	2.00	0.00	0.00	0.06	0.00	48.60	2.00	0.00	0.00	0.08	0.00
48.68	2.00	0.00	0.00	0.08	0.00	48.74	2.00	0.00	0.00	0.06	0.00
48.82	2.00	0.00	0.00	0.08	0.00	48.89	2.00	0.00	0.00	0.07	0.00
48.99	2.00	0.00	0.00	0.10	0.00	49.05	2.00	0.00	0.00	0.06	0.00
49.12	2.00	0.00	0.00	0.08	0.00	49.18	2.00	0.00	0.00	0.06	0.00
49.27	2.00	0.00	0.00	0.09	0.00	49.32	2.00	0.00	0.00	0.05	0.00
49.42	2.00	0.00	0.00	0.09	0.00	49.48	2.00	0.00	0.00	0.06	0.00
49.56	2.00	0.00	0.00	0.09	0.00	49.66	2.00	0.00	0.00	0.10	0.00
49.76	2.00	0.00	0.00	0.09	0.00	49.85	2.00	0.00	0.00	0.09	0.00
49.99	2.00	0.00	0.00	0.14	0.00	50.09	2.00	0.00	0.00	0.10	0.00
50.21	2.00	0.00	0.00	0.12	0.00	50.24	2.00	0.00	0.00	0.03	0.00
50.29	2.00	0.00	0.00	0.05	0.00	50.38	2.00	0.00	0.00	0.09	0.00
50.47	2.00	0.00	0.00	0.09	0.00	50.52	2.00	0.00	0.00	0.05	0.00
50.62	2.00	0.00	0.00	0.10	0.00	50.66	2.00	0.00	0.00	0.05	0.00
50.76	2.00	0.00	0.00	0.10	0.00	50.83	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
50.91	2.00	0.00	0.00	0.09	0.00	51.00	2.00	0.00	0.00	0.09	0.00
51.06	2.00	0.00	0.00	0.06	0.00	51.15	2.00	0.00	0.00	0.08	0.00
51.24	2.00	0.00	0.00	0.10	0.00	51.31	2.00	0.00	0.00	0.07	0.00
51.39	2.00	0.00	0.00	0.08	0.00	51.48	2.00	0.00	0.00	0.09	0.00
51.58	2.00	0.00	0.00	0.10	0.00	51.68	2.00	0.00	0.00	0.10	0.00
51.77	2.00	0.00	0.00	0.10	0.00	51.90	2.00	0.00	0.00	0.13	0.00
52.01	2.00	0.00	0.00	0.11	0.00	52.11	2.00	0.00	0.00	0.10	0.00
52.26	2.00	0.00	0.00	0.14	0.00	52.30	2.00	0.00	0.00	0.05	0.00
52.33	2.00	0.00	0.00	0.03	0.00	52.35	2.00	0.00	0.00	0.02	0.00
52.40	2.00	0.00	0.00	0.05	0.00	52.45	2.00	0.00	0.00	0.05	0.00
52.50	2.00	0.00	0.00	0.05	0.00	52.55	2.00	0.00	0.00	0.05	0.00
52.60	2.00	0.00	0.00	0.05	0.00	52.65	2.00	0.00	0.00	0.05	0.00
52.71	2.00	0.00	0.00	0.07	0.00	52.77	2.00	0.00	0.00	0.05	0.00
52.82	2.00	0.00	0.00	0.05	0.00	52.88	2.00	0.00	0.00	0.06	0.00
52.93	2.00	0.00	0.00	0.06	0.00	52.98	2.00	0.00	0.00	0.05	0.00
53.03	2.00	0.00	0.00	0.05	0.00	53.08	2.00	0.00	0.00	0.05	0.00
53.12	2.00	0.00	0.00	0.04	0.00	53.17	2.00	0.00	0.00	0.05	0.00
53.23	2.00	0.00	0.00	0.05	0.00	53.28	2.00	0.00	0.00	0.06	0.00
53.37	2.00	0.00	0.00	0.09	0.00	53.42	2.00	0.00	0.00	0.05	0.00
53.46	2.00	0.00	0.00	0.05	0.00	53.53	2.00	0.00	0.00	0.06	0.00
53.61	2.00	0.00	0.00	0.08	0.00	53.62	2.00	0.00	0.00	0.01	0.00
53.65	2.00	0.00	0.00	0.04	0.00	53.67	2.00	0.00	0.00	0.01	0.00
53.70	2.00	0.00	0.00	0.04	0.00	53.74	2.00	0.00	0.00	0.04	0.00
53.76	2.00	0.00	0.00	0.02	0.00	53.80	2.00	0.00	0.00	0.04	0.00
53.84	2.00	0.00	0.00	0.05	0.00	53.90	2.00	0.00	0.00	0.05	0.00
53.91	2.00	0.00	0.00	0.01	0.00	53.95	2.00	0.00	0.00	0.04	0.00
53.96	2.00	0.00	0.00	0.01	0.00	53.98	2.00	0.00	0.00	0.02	0.00
53.99	2.00	0.00	0.00	0.01	0.00	54.01	2.00	0.00	0.00	0.01	0.00
54.02	2.00	0.00	0.00	0.01	0.00	54.03	2.00	0.00	0.00	0.01	0.00
54.04	2.00	0.00	0.00	0.01	0.00	54.05	2.00	0.00	0.00	0.01	0.00
54.09	2.00	0.00	0.00	0.04	0.00	54.10	2.00	0.00	0.00	0.01	0.00
54.13	2.00	0.00	0.00	0.04	0.00	54.14	2.00	0.00	0.00	0.01	0.00
54.19	2.00	0.00	0.00	0.05	0.00	54.19	2.00	0.00	0.00	0.01	0.00
54.24	2.00	0.00	0.00	0.05	0.00	54.29	2.00	0.00	0.00	0.04	0.00
54.33	2.00	0.00	0.00	0.05	0.00	54.38	2.00	0.00	0.00	0.05	0.00
54.39	2.00	0.00	0.00	0.01	0.00	54.43	2.00	0.00	0.00	0.04	0.00
54.48	2.00	0.00	0.00	0.05	0.00	54.52	2.00	0.00	0.00	0.05	0.00
54.58	2.00	0.00	0.00	0.05	0.00	54.62	2.00	0.00	0.00	0.04	0.00
54.65	2.00	0.00	0.00	0.03	0.00	54.67	2.00	0.00	0.00	0.02	0.00
54.71	2.00	0.00	0.00	0.04	0.00	54.77	2.00	0.00	0.00	0.05	0.00
54.81	2.00	0.00	0.00	0.05	0.00	54.85	2.00	0.00	0.00	0.04	0.00
54.86	2.00	0.00	0.00	0.01	0.00	54.87	2.00	0.00	0.00	0.01	0.00
54.91	2.00	0.00	0.00	0.04	0.00	54.96	2.00	0.00	0.00	0.04	0.00
55.00	2.00	0.00	0.00	0.04	0.00	55.01	2.00	0.00	0.00	0.01	0.00
55.05	2.00	0.00	0.00	0.05	0.00	55.10	2.00	0.00	0.00	0.05	0.00
55.12	2.00	0.00	0.00	0.01	0.00	55.13	2.00	0.00	0.00	0.02	0.00
55.14	2.00	0.00	0.00	0.01	0.00	55.19	2.00	0.00	0.00	0.05	0.00
55.20	2.00	0.00	0.00	0.01	0.00	55.25	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
55.29	2.00	0.00	0.00	0.04	0.00	55.33	2.00	0.00	0.00	0.04	0.00
55.38	2.00	0.00	0.00	0.05	0.00	55.48	2.00	0.00	0.00	0.10	0.00
55.57	2.00	0.00	0.00	0.09	0.00	55.63	2.00	0.00	0.00	0.05	0.00
55.72	2.00	0.00	0.00	0.10	0.00	55.80	2.00	0.00	0.00	0.08	0.00
55.86	2.00	0.00	0.00	0.06	0.00	55.97	2.00	0.00	0.00	0.10	0.00
56.01	2.00	0.00	0.00	0.05	0.00	56.06	2.00	0.00	0.00	0.05	0.00
56.11	2.00	0.00	0.00	0.05	0.00	56.15	2.00	0.00	0.00	0.04	0.00
56.20	2.00	0.00	0.00	0.05	0.00	56.27	2.00	0.00	0.00	0.06	0.00
56.27	2.00	0.00	0.00	0.01	0.00	56.30	2.00	0.00	0.00	0.03	0.00
56.33	2.00	0.00	0.00	0.03	0.00	56.35	2.00	0.00	0.00	0.01	0.00
56.40	2.00	0.00	0.00	0.05	0.00	56.41	2.00	0.00	0.00	0.01	0.00
56.44	2.00	0.00	0.00	0.04	0.00	56.49	2.00	0.00	0.00	0.05	0.00
56.54	2.00	0.00	0.00	0.04	0.00	56.58	2.00	0.00	0.00	0.05	0.00
56.59	2.00	0.00	0.00	0.01	0.00	56.64	2.00	0.00	0.00	0.05	0.00
56.69	2.00	0.00	0.00	0.05	0.00	56.73	2.00	0.00	0.00	0.04	0.00
56.78	2.00	0.00	0.00	0.05	0.00	56.83	2.00	0.00	0.00	0.05	0.00
56.88	2.00	0.00	0.00	0.05	0.00	56.89	2.00	0.00	0.00	0.02	0.00
56.95	2.00	0.00	0.00	0.06	0.00	57.01	2.00	0.00	0.00	0.06	0.00
57.07	2.00	0.00	0.00	0.06	0.00	57.11	2.00	0.00	0.00	0.05	0.00
57.17	2.00	0.00	0.00	0.06	0.00	57.26	1.89	0.00	0.00	0.09	0.00
57.31	1.67	0.00	0.00	0.05	0.00	57.37	1.46	0.00	0.00	0.06	0.00
57.45	1.26	0.00	0.00	0.08	0.00	57.51	1.03	0.00	0.00	0.06	0.00
57.53	0.89	0.00	0.00	0.02	0.00	57.59	0.80	0.00	0.00	0.05	0.00
57.63	0.79	0.00	0.00	0.05	0.00	57.68	0.76	0.00	0.00	0.05	0.00
57.73	0.74	0.00	0.00	0.05	0.01	57.78	0.71	0.00	0.00	0.05	0.01
57.86	0.64	0.00	0.00	0.08	0.01	57.92	2.00	0.00	0.00	0.06	0.00
57.98	2.00	0.00	0.00	0.06	0.00	58.06	2.00	0.00	0.00	0.08	0.00
58.12	2.00	0.00	0.00	0.05	0.00	58.21	2.00	0.00	0.00	0.09	0.00
58.26	2.00	0.00	0.00	0.05	0.00	58.35	2.00	0.00	0.00	0.09	0.00
58.41	2.00	0.00	0.00	0.06	0.00	58.50	2.00	0.00	0.00	0.09	0.00
58.56	2.00	0.00	0.00	0.06	0.00	58.64	2.00	0.00	0.00	0.08	0.00
58.73	2.00	0.00	0.00	0.09	0.00	58.80	2.00	0.00	0.00	0.07	0.00
58.84	2.00	0.00	0.00	0.03	0.00	58.85	2.00	0.00	0.00	0.01	0.00
58.93	2.00	0.00	0.00	0.08	0.00	58.98	2.00	0.00	0.00	0.05	0.00
59.02	2.00	0.00	0.00	0.05	0.00	59.12	2.00	0.00	0.00	0.10	0.00
59.17	2.00	0.00	0.00	0.05	0.00	59.27	2.00	0.00	0.00	0.09	0.00
59.31	2.00	0.00	0.00	0.05	0.00	59.41	2.00	0.00	0.00	0.09	0.00
59.46	2.00	0.00	0.00	0.05	0.00	59.55	2.00	0.00	0.00	0.09	0.00
59.65	2.00	0.00	0.00	0.10	0.00	59.70	2.00	0.00	0.00	0.05	0.00
59.80	2.00	0.00	0.00	0.10	0.00	59.89	2.00	0.00	0.00	0.09	0.00
59.94	2.00	0.00	0.00	0.05	0.00	60.01	2.00	0.00	0.00	0.07	0.00
60.02	2.00	0.00	0.00	0.02	0.00	60.08	2.00	0.00	0.00	0.05	0.00
60.12	2.00	0.00	0.00	0.04	0.00	60.17	2.00	0.00	0.00	0.05	0.00
60.27	2.00	0.00	0.00	0.10	0.00	60.31	2.00	0.00	0.00	0.04	0.00
60.37	2.00	0.00	0.00	0.06	0.00	60.46	2.00	0.00	0.00	0.09	0.00
60.51	2.00	0.00	0.00	0.05	0.00	60.61	2.00	0.00	0.00	0.10	0.00
60.65	2.00	0.00	0.00	0.05	0.00	60.75	2.00	0.00	0.00	0.10	0.00
60.81	2.00	0.00	0.00	0.05	0.00	60.89	2.00	0.00	0.00	0.08	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
60.94	2.00	0.00	0.00	0.05	0.00	61.03	2.00	0.00	0.00	0.09	0.00
61.09	2.00	0.00	0.00	0.06	0.00	61.19	2.00	0.00	0.00	0.09	0.00
61.24	2.00	0.00	0.00	0.06	0.00	61.33	2.00	0.00	0.00	0.08	0.00
61.38	2.00	0.00	0.00	0.05	0.00	61.47	2.00	0.00	0.00	0.10	0.00
61.53	2.00	0.00	0.00	0.06	0.00	61.62	2.00	0.00	0.00	0.09	0.00
61.70	2.00	0.00	0.00	0.09	0.00	61.77	2.00	0.00	0.00	0.06	0.00
61.86	2.00	0.00	0.00	0.09	0.00	61.95	2.00	0.00	0.00	0.10	0.00
61.97	2.00	0.00	0.00	0.02	0.00	62.01	2.00	0.00	0.00	0.04	0.00
62.10	2.00	0.00	0.00	0.09	0.00	62.24	2.00	0.00	0.00	0.14	0.00
62.34	2.00	0.00	0.00	0.10	0.00	62.49	2.00	0.00	0.00	0.14	0.00
62.54	2.00	0.00	0.00	0.05	0.00	62.66	2.00	0.00	0.00	0.12	0.00
62.74	2.00	0.00	0.00	0.08	0.00	62.87	2.00	0.00	0.00	0.13	0.00
62.92	2.00	0.00	0.00	0.05	0.00	63.03	2.00	0.00	0.00	0.11	0.00
63.15	2.00	0.00	0.00	0.12	0.00	63.26	2.00	0.00	0.00	0.11	0.00
63.37	2.00	0.00	0.00	0.11	0.00	63.45	2.00	0.00	0.00	0.08	0.00
63.54	2.00	0.00	0.00	0.10	0.00	63.61	2.00	0.00	0.00	0.07	0.00
63.69	2.00	0.00	0.00	0.08	0.00	63.79	2.00	0.00	0.00	0.09	0.00
63.89	2.00	0.00	0.00	0.10	0.00	63.98	2.00	0.00	0.00	0.09	0.00
64.07	2.00	0.00	0.00	0.09	0.00	64.15	2.00	0.00	0.00	0.08	0.00
64.23	2.00	0.00	0.00	0.08	0.00	64.26	2.00	0.00	0.00	0.03	0.00
64.29	2.00	0.00	0.00	0.02	0.00	64.33	2.00	0.00	0.00	0.05	0.00
64.43	2.00	0.00	0.00	0.10	0.00	64.47	2.00	0.00	0.00	0.04	0.00
64.53	2.00	0.00	0.00	0.05	0.00	64.62	2.00	0.00	0.00	0.10	0.00
64.72	2.00	0.00	0.00	0.09	0.00	64.78	2.00	0.00	0.00	0.06	0.00
64.86	2.00	0.00	0.00	0.09	0.00	64.96	2.00	0.00	0.00	0.10	0.00
65.06	2.00	0.00	0.00	0.09	0.00	65.11	2.00	0.00	0.00	0.05	0.00
65.21	2.00	0.00	0.00	0.10	0.00	65.31	2.00	0.00	0.00	0.10	0.00
65.40	2.00	0.00	0.00	0.09	0.00	65.50	2.00	0.00	0.00	0.10	0.00
65.58	2.00	0.00	0.00	0.09	0.00	65.68	2.00	0.00	0.00	0.10	0.00
65.78	2.00	0.00	0.00	0.10	0.00	65.84	2.00	0.00	0.00	0.07	0.00
65.86	2.00	0.00	0.00	0.01	0.00	65.87	2.00	0.00	0.00	0.01	0.00
65.98	2.00	0.00	0.00	0.11	0.00	66.10	2.00	0.00	0.00	0.12	0.00
66.21	2.00	0.00	0.00	0.11	0.00	66.34	2.00	0.00	0.00	0.13	0.00
66.48	2.00	0.00	0.00	0.14	0.00	66.62	2.00	0.00	0.00	0.14	0.00
66.68	2.00	0.00	0.00	0.06	0.00	66.87	2.00	0.00	0.00	0.19	0.00
66.96	2.00	0.00	0.00	0.09	0.00	67.11	2.00	0.00	0.00	0.15	0.00
67.21	2.00	0.00	0.00	0.10	0.00	67.35	2.00	0.00	0.00	0.14	0.00
67.45	2.00	0.00	0.00	0.10	0.00	67.59	2.00	0.00	0.00	0.14	0.00
67.68	2.00	0.00	0.00	0.09	0.00	67.83	2.00	0.00	0.00	0.15	0.00
67.92	2.00	0.00	0.00	0.10	0.00	68.02	2.00	0.00	0.00	0.09	0.00
68.07	2.00	0.00	0.00	0.05	0.00	68.16	2.00	0.00	0.00	0.09	0.00
68.26	2.00	0.00	0.00	0.10	0.00	68.35	2.00	0.00	0.00	0.09	0.00
68.45	2.00	0.00	0.00	0.10	0.00	68.55	2.00	0.00	0.00	0.10	0.00
68.65	2.00	0.00	0.00	0.10	0.00	68.78	2.00	0.00	0.00	0.13	0.00
68.78	2.00	0.00	0.00	0.01	0.00	68.79	2.00	0.00	0.00	0.01	0.00
68.83	2.00	0.00	0.00	0.04	0.00	68.93	2.00	0.00	0.00	0.09	0.00
68.98	2.00	0.00	0.00	0.05	0.00	69.04	2.00	0.00	0.00	0.06	0.00
69.12	2.00	0.00	0.00	0.08	0.00	69.22	2.00	0.00	0.00	0.10	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
69.28	2.00	0.00	0.00	0.07	0.00	69.36	2.00	0.00	0.00	0.08	0.00
69.45	2.00	0.00	0.00	0.09	0.00	69.60	2.00	0.00	0.00	0.14	0.00
69.70	2.00	0.00	0.00	0.10	0.00	69.80	2.00	0.00	0.00	0.09	0.00
69.89	2.00	0.00	0.00	0.10	0.00	69.98	2.00	0.00	0.00	0.09	0.00
70.08	2.00	0.00	0.00	0.10	0.00	70.18	2.00	0.00	0.00	0.10	0.00
70.32	2.00	0.00	0.00	0.14	0.00	70.42	2.00	0.00	0.00	0.10	0.00
70.54	2.00	0.00	0.00	0.12	0.00	70.66	2.00	0.00	0.00	0.12	0.00
70.75	2.00	0.00	0.00	0.09	0.00	70.80	2.00	0.00	0.00	0.05	0.00
70.89	2.00	0.00	0.00	0.09	0.00	70.99	2.00	0.00	0.00	0.10	0.00
71.08	2.00	0.00	0.00	0.09	0.00	71.17	2.00	0.00	0.00	0.09	0.00
71.23	2.00	0.00	0.00	0.05	0.00	71.33	2.00	0.00	0.00	0.10	0.00
71.42	2.00	0.00	0.00	0.09	0.00	71.52	2.00	0.00	0.00	0.10	0.00
71.58	2.00	0.00	0.00	0.06	0.00	71.67	2.00	0.00	0.00	0.08	0.00
71.81	2.00	0.00	0.00	0.14	0.00	71.82	2.00	0.00	0.00	0.01	0.00
71.86	2.00	0.00	0.00	0.04	0.00	71.91	2.00	0.00	0.00	0.05	0.00
71.97	2.00	0.00	0.00	0.06	0.00	72.05	2.00	0.00	0.00	0.08	0.00
72.10	2.00	0.00	0.00	0.05	0.00	72.20	2.00	0.00	0.00	0.10	0.00
72.25	2.00	0.00	0.00	0.05	0.00	72.34	2.00	0.00	0.00	0.10	0.00
72.44	2.00	0.00	0.00	0.10	0.00	72.53	2.00	0.00	0.00	0.09	0.00
72.63	2.00	0.00	0.00	0.10	0.00	72.69	2.00	0.00	0.00	0.06	0.00
72.82	2.00	0.00	0.00	0.13	0.00	72.92	2.00	0.00	0.00	0.09	0.00
73.06	2.00	0.00	0.00	0.14	0.00	73.16	2.00	0.00	0.00	0.10	0.00
73.30	2.00	0.00	0.00	0.14	0.00	73.35	2.00	0.00	0.00	0.05	0.00
73.38	2.00	0.00	0.00	0.03	0.00	73.47	2.00	0.00	0.00	0.09	0.00
73.53	2.00	0.00	0.00	0.06	0.00	73.62	2.00	0.00	0.00	0.09	0.00
73.71	2.00	0.00	0.00	0.09	0.00	73.77	2.00	0.00	0.00	0.06	0.00
73.86	2.00	0.00	0.00	0.09	0.00	73.96	2.00	0.00	0.00	0.09	0.00
74.06	2.00	0.00	0.00	0.10	0.00	74.13	2.00	0.00	0.00	0.07	0.00
74.24	2.00	0.00	0.00	0.11	0.00	74.34	2.00	0.00	0.00	0.10	0.00
74.44	2.00	0.00	0.00	0.10	0.00	74.58	2.00	0.00	0.00	0.14	0.00
74.68	2.00	0.00	0.00	0.10	0.00	74.80	2.00	0.00	0.00	0.13	0.00
74.92	2.00	0.00	0.00	0.12	0.00	75.07	2.00	0.00	0.00	0.14	0.00
75.08	2.00	0.00	0.00	0.01	0.00	75.11	2.00	0.00	0.00	0.03	0.00
75.16	2.00	0.00	0.00	0.05	0.00	75.25	2.00	0.00	0.00	0.09	0.00
75.32	2.00	0.00	0.00	0.07	0.00	75.40	2.00	0.00	0.00	0.08	0.00
75.50	2.00	0.00	0.00	0.10	0.00	75.59	2.00	0.00	0.00	0.09	0.00
75.69	2.00	0.00	0.00	0.10	0.00	75.78	2.00	0.00	0.00	0.09	0.00
75.88	2.00	0.00	0.00	0.09	0.00	75.96	2.00	0.00	0.00	0.09	0.00
76.05	2.00	0.00	0.00	0.08	0.00	76.14	2.00	0.00	0.00	0.09	0.00
76.26	2.00	0.00	0.00	0.12	0.00	76.36	2.00	0.00	0.00	0.10	0.00
76.41	2.00	0.00	0.00	0.05	0.00	76.51	2.00	0.00	0.00	0.10	0.00
76.65	2.00	0.00	0.00	0.14	0.00	76.72	2.00	0.00	0.00	0.07	0.00
76.79	2.00	0.00	0.00	0.07	0.00	76.89	2.00	0.00	0.00	0.10	0.00
76.98	2.00	0.00	0.00	0.09	0.00	77.08	2.00	0.00	0.00	0.10	0.00
77.18	2.00	0.00	0.00	0.10	0.00	77.28	2.00	0.00	0.00	0.10	0.00
77.37	2.00	0.00	0.00	0.10	0.00	77.42	2.00	0.00	0.00	0.04	0.00
77.42	2.00	0.00	0.00	0.01	0.00	77.44	2.00	0.00	0.00	0.01	0.00
77.48	2.00	0.00	0.00	0.04	0.00	77.52	2.00	0.00	0.00	0.04	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
77.54	2.00	0.00	0.00	0.02	0.00	77.57	2.00	0.00	0.00	0.03	0.00
77.62	2.00	0.00	0.00	0.05	0.00	77.65	2.00	0.00	0.00	0.04	0.00
77.67	2.00	0.00	0.00	0.01	0.00	77.71	2.00	0.00	0.00	0.04	0.00
77.71	2.00	0.00	0.00	0.01	0.00	77.76	2.00	0.00	0.00	0.05	0.00
77.81	2.00	0.00	0.00	0.05	0.00	77.90	2.00	0.00	0.00	0.09	0.00
77.95	2.00	0.00	0.00	0.05	0.00	78.01	2.00	0.00	0.00	0.06	0.00
78.10	2.00	0.00	0.00	0.09	0.00	78.16	2.00	0.00	0.00	0.06	0.00
78.24	2.00	0.00	0.00	0.08	0.00	78.29	2.00	0.00	0.00	0.05	0.00
78.39	2.00	0.00	0.00	0.10	0.00	78.47	2.00	0.00	0.00	0.08	0.00
78.53	2.00	0.00	0.00	0.06	0.00	78.62	2.00	0.00	0.00	0.09	0.00
78.68	2.00	0.00	0.00	0.05	0.00	78.69	2.00	0.00	0.00	0.01	0.00
78.78	2.00	0.00	0.00	0.09	0.00	78.81	2.00	0.00	0.00	0.04	0.00
78.92	2.00	0.00	0.00	0.11	0.00	79.03	2.00	0.00	0.00	0.11	0.00
79.16	2.00	0.00	0.00	0.13	0.00	79.26	2.00	0.00	0.00	0.10	0.00
79.35	2.00	0.00	0.00	0.09	0.00	79.45	2.00	0.00	0.00	0.10	0.00
79.54	2.00	0.00	0.00	0.09	0.00	79.64	2.00	0.00	0.00	0.10	0.00
79.74	2.00	0.00	0.00	0.10	0.00	79.88	2.00	0.00	0.00	0.14	0.00
79.98	2.00	0.00	0.00	0.10	0.00	80.12	2.00	0.00	0.00	0.14	0.00
80.22	2.00	0.00	0.00	0.09	0.00	80.36	2.00	0.00	0.00	0.14	0.00
80.46	2.00	0.00	0.00	0.10	0.00	80.60	2.00	0.00	0.00	0.14	0.00
80.70	2.00	0.00	0.00	0.10	0.00	80.83	2.00	0.00	0.00	0.13	0.00
80.94	2.00	0.00	0.00	0.11	0.00	81.01	2.00	0.00	0.00	0.07	0.00
81.04	2.00	0.00	0.00	0.03	0.00	81.09	2.00	0.00	0.00	0.06	0.00
81.13	2.00	0.00	0.00	0.04	0.00	81.18	2.00	0.00	0.00	0.05	0.00
81.23	2.00	0.00	0.00	0.05	0.00	81.28	2.00	0.00	0.00	0.05	0.00
81.33	2.00	0.00	0.00	0.05	0.00	81.37	2.00	0.00	0.00	0.05	0.00
81.42	2.00	0.00	0.00	0.04	0.00	81.47	2.00	0.00	0.00	0.05	0.00
81.52	2.00	0.00	0.00	0.05	0.00	81.56	2.00	0.00	0.00	0.05	0.00
81.61	2.00	0.00	0.00	0.04	0.00	81.64	2.00	0.00	0.00	0.04	0.00
81.70	2.00	0.00	0.00	0.06	0.00	81.75	2.00	0.00	0.00	0.05	0.00
81.79	2.00	0.00	0.00	0.04	0.00	81.82	2.00	0.00	0.00	0.03	0.00
81.86	2.00	0.00	0.00	0.04	0.00	81.91	2.00	0.00	0.00	0.05	0.00
81.95	2.00	0.00	0.00	0.04	0.00	82.00	2.00	0.00	0.00	0.05	0.00
82.09	2.00	0.00	0.00	0.09	0.00	82.15	2.00	0.00	0.00	0.06	0.00
82.19	2.00	0.00	0.00	0.04	0.00	82.26	2.00	0.00	0.00	0.07	0.00
82.34	2.00	0.00	0.00	0.08	0.00	82.39	2.00	0.00	0.00	0.05	0.00
82.48	2.00	0.00	0.00	0.10	0.00	82.58	2.00	0.00	0.00	0.09	0.00
82.62	2.00	0.00	0.00	0.04	0.00	82.70	2.00	0.00	0.00	0.08	0.00
82.77	2.00	0.00	0.00	0.07	0.00	82.87	2.00	0.00	0.00	0.10	0.00
82.96	2.00	0.00	0.00	0.09	0.00	83.06	2.00	0.00	0.00	0.10	0.00
83.16	2.00	0.00	0.00	0.10	0.00	83.25	2.00	0.00	0.00	0.09	0.00
83.34	2.00	0.00	0.00	0.09	0.00	83.44	2.00	0.00	0.00	0.10	0.00
83.54	2.00	0.00	0.00	0.10	0.00	83.64	2.00	0.00	0.00	0.09	0.00
83.73	2.00	0.00	0.00	0.10	0.00	83.83	2.00	0.00	0.00	0.09	0.00
83.85	2.00	0.00	0.00	0.02	0.00	83.89	2.00	0.00	0.00	0.04	0.00
83.94	2.00	0.00	0.00	0.05	0.00	84.04	2.00	0.00	0.00	0.10	0.00
84.09	2.00	0.00	0.00	0.05	0.00	84.13	2.00	0.00	0.00	0.04	0.00
84.18	2.00	0.00	0.00	0.05	0.00	84.25	2.00	0.00	0.00	0.06	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
84.33	2.00	0.00	0.00	0.08	0.00	84.37	2.00	0.00	0.00	0.05	0.00
84.46	2.00	0.00	0.00	0.08	0.00	84.52	2.00	0.00	0.00	0.06	0.00
84.57	2.00	0.00	0.00	0.05	0.00	84.67	2.00	0.00	0.00	0.10	0.00
84.71	2.00	0.00	0.00	0.04	0.00	84.81	2.00	0.00	0.00	0.10	0.00
84.86	2.00	0.00	0.00	0.05	0.00	84.91	2.00	0.00	0.00	0.06	0.00
85.00	2.00	0.00	0.00	0.09	0.00	85.05	2.00	0.00	0.00	0.05	0.00
85.15	2.00	0.00	0.00	0.10	0.00	85.19	2.00	0.00	0.00	0.05	0.00
85.29	2.00	0.00	0.00	0.10	0.00	85.35	2.00	0.00	0.00	0.06	0.00
85.42	2.00	0.00	0.00	0.07	0.00	85.48	2.00	0.00	0.00	0.06	0.00
85.55	2.00	0.00	0.00	0.06	0.00	85.63	2.00	0.00	0.00	0.08	0.00
85.68	2.00	0.00	0.00	0.05	0.00	85.77	2.00	0.00	0.00	0.09	0.00
85.82	2.00	0.00	0.00	0.05	0.00	85.89	2.00	0.00	0.00	0.07	0.00
85.96	2.00	0.00	0.00	0.08	0.00	86.03	2.00	0.00	0.00	0.07	0.00
86.11	2.00	0.00	0.00	0.07	0.00	86.16	2.00	0.00	0.00	0.06	0.00
86.25	2.00	0.00	0.00	0.09	0.00	86.36	2.00	0.00	0.00	0.11	0.00
86.50	2.00	0.00	0.00	0.14	0.00	86.51	2.00	0.00	0.00	0.01	0.00
86.52	2.00	0.00	0.00	0.01	0.00	86.57	2.00	0.00	0.00	0.05	0.00
86.65	2.00	0.00	0.00	0.09	0.00	86.71	2.00	0.00	0.00	0.06	0.00
86.80	2.00	0.00	0.00	0.09	0.00	86.90	2.00	0.00	0.00	0.09	0.00
86.99	2.00	0.00	0.00	0.09	0.00	87.04	2.00	0.00	0.00	0.05	0.00
87.14	2.00	0.00	0.00	0.09	0.00	87.19	2.00	0.00	0.00	0.06	0.00
87.28	2.00	0.00	0.00	0.09	0.00	87.38	2.00	0.00	0.00	0.09	0.00
87.43	2.00	0.00	0.00	0.06	0.00	87.52	2.00	0.00	0.00	0.09	0.00
87.61	2.00	0.00	0.00	0.09	0.00	87.66	2.00	0.00	0.00	0.05	0.00
87.76	2.00	0.00	0.00	0.10	0.00	87.84	2.00	0.00	0.00	0.08	0.00
87.91	2.00	0.00	0.00	0.07	0.00	88.00	2.00	0.00	0.00	0.09	0.00
88.11	2.00	0.00	0.00	0.11	0.00	88.19	2.00	0.00	0.00	0.08	0.00
88.25	2.00	0.00	0.00	0.06	0.00	88.34	2.00	0.00	0.00	0.09	0.00
88.44	2.00	0.00	0.00	0.10	0.00	88.54	2.00	0.00	0.00	0.11	0.00
88.64	2.00	0.00	0.00	0.10	0.00	88.72	2.00	0.00	0.00	0.09	0.00
88.82	2.00	0.00	0.00	0.10	0.00	88.91	2.00	0.00	0.00	0.09	0.00
89.01	2.00	0.00	0.00	0.10	0.00	89.10	2.00	0.00	0.00	0.09	0.00
89.19	2.00	0.00	0.00	0.09	0.00	89.30	2.00	0.00	0.00	0.11	0.00
89.39	2.00	0.00	0.00	0.09	0.00	89.49	2.00	0.00	0.00	0.10	0.00
89.59	2.00	0.00	0.00	0.09	0.00	89.69	2.00	0.00	0.00	0.10	0.00
89.73	2.00	0.00	0.00	0.05	0.00	89.78	2.00	0.00	0.00	0.04	0.00
89.83	2.00	0.00	0.00	0.06	0.00	89.88	2.00	0.00	0.00	0.05	0.00
89.93	2.00	0.00	0.00	0.05	0.00	90.00	2.00	0.00	0.00	0.07	0.00
90.07	2.00	0.00	0.00	0.08	0.00	90.12	2.00	0.00	0.00	0.05	0.00
90.22	2.00	0.00	0.00	0.09	0.00	90.27	2.00	0.00	0.00	0.05	0.00
90.36	2.00	0.00	0.00	0.09	0.00	90.46	2.00	0.00	0.00	0.10	0.00
90.50	2.00	0.00	0.00	0.04	0.00	90.61	2.00	0.00	0.00	0.10	0.00
90.66	2.00	0.00	0.00	0.05	0.00	90.75	2.00	0.00	0.00	0.09	0.00
90.84	2.00	0.00	0.00	0.09	0.00	90.89	2.00	0.00	0.00	0.05	0.00
90.99	2.00	0.00	0.00	0.10	0.00	91.04	2.00	0.00	0.00	0.05	0.00
91.14	2.00	0.00	0.00	0.09	0.00	91.22	2.00	0.00	0.00	0.09	0.00
91.28	2.00	0.00	0.00	0.06	0.00	91.37	2.00	0.00	0.00	0.09	0.00
91.47	2.00	0.00	0.00	0.10	0.00	91.61	2.00	0.00	0.00	0.14	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
91.71	2.00	0.00	0.00	0.10	0.00	91.81	2.00	0.00	0.00	0.10	0.00
91.87	2.00	0.00	0.00	0.06	0.00	92.00	2.00	0.00	0.00	0.13	0.00
92.10	2.00	0.00	0.00	0.10	0.00	92.20	2.00	0.00	0.00	0.10	0.00
92.33	2.00	0.00	0.00	0.13	0.00	92.38	2.00	0.00	0.00	0.05	0.00
92.43	2.00	0.00	0.00	0.05	0.00	92.48	2.00	0.00	0.00	0.05	0.00
92.56	2.00	0.00	0.00	0.08	0.00	92.63	2.00	0.00	0.00	0.07	0.00
92.67	2.00	0.00	0.00	0.05	0.00	92.72	2.00	0.00	0.00	0.04	0.00
92.77	2.00	0.00	0.00	0.05	0.00	92.86	2.00	0.00	0.00	0.10	0.00
92.92	2.00	0.00	0.00	0.05	0.00	92.97	2.00	0.00	0.00	0.05	0.00
93.05	2.00	0.00	0.00	0.08	0.00	93.10	2.00	0.00	0.00	0.06	0.00
93.16	2.00	0.00	0.00	0.06	0.00	93.25	2.00	0.00	0.00	0.09	0.00
93.35	2.00	0.00	0.00	0.10	0.00	93.40	2.00	0.00	0.00	0.05	0.00
93.49	2.00	0.00	0.00	0.10	0.00	93.56	2.00	0.00	0.00	0.07	0.00
93.64	2.00	0.00	0.00	0.08	0.00	93.73	2.00	0.00	0.00	0.09	0.00
93.83	2.00	0.00	0.00	0.10	0.00	93.88	2.00	0.00	0.00	0.05	0.00
93.97	2.00	0.00	0.00	0.09	0.00	94.07	2.00	0.00	0.00	0.10	0.00
94.17	2.00	0.00	0.00	0.10	0.00	94.26	2.00	0.00	0.00	0.10	0.00
94.36	2.00	0.00	0.00	0.09	0.00	94.45	2.00	0.00	0.00	0.09	0.00
94.55	2.00	0.00	0.00	0.10	0.00	94.64	2.00	0.00	0.00	0.09	0.00
94.72	2.00	0.00	0.00	0.07	0.00	94.74	2.00	0.00	0.00	0.03	0.00
94.77	2.00	0.00	0.00	0.02	0.00	94.85	2.00	0.00	0.00	0.08	0.00
94.90	2.00	0.00	0.00	0.05	0.00	94.95	2.00	0.00	0.00	0.05	0.00
95.01	2.00	0.00	0.00	0.06	0.00	95.09	2.00	0.00	0.00	0.08	0.00
95.14	2.00	0.00	0.00	0.05	0.00	95.23	2.00	0.00	0.00	0.09	0.00
95.29	2.00	0.00	0.00	0.06	0.00	95.38	2.00	0.00	0.00	0.09	0.00
95.43	2.00	0.00	0.00	0.05	0.00	95.52	2.00	0.00	0.00	0.09	0.00
95.57	2.00	0.00	0.00	0.05	0.00	95.67	2.00	0.00	0.00	0.10	0.00
95.77	2.00	0.00	0.00	0.09	0.00	95.86	2.00	0.00	0.00	0.10	0.00
95.95	2.00	0.00	0.00	0.09	0.00	96.03	2.00	0.00	0.00	0.08	0.00
96.11	2.00	0.00	0.00	0.08	0.00	96.20	2.00	0.00	0.00	0.09	0.00
96.30	2.00	0.00	0.00	0.10	0.00	96.39	2.00	0.00	0.00	0.09	0.00
96.50	2.00	0.00	0.00	0.11	0.00	96.59	2.00	0.00	0.00	0.09	0.00
96.69	2.00	0.00	0.00	0.10	0.00	96.78	2.00	0.00	0.00	0.09	0.00
96.87	2.00	0.00	0.00	0.09	0.00	96.98	2.00	0.00	0.00	0.11	0.00
97.02	2.00	0.00	0.00	0.04	0.00	97.06	2.00	0.00	0.00	0.05	0.00
97.12	2.00	0.00	0.00	0.05	0.00	97.16	2.00	0.00	0.00	0.04	0.00
97.21	2.00	0.00	0.00	0.05	0.00	97.27	2.00	0.00	0.00	0.06	0.00
97.33	2.00	0.00	0.00	0.06	0.00	97.40	2.00	0.00	0.00	0.07	0.00
97.45	2.00	0.00	0.00	0.05	0.00	97.50	2.00	0.00	0.00	0.05	0.00
97.58	2.00	0.00	0.00	0.08	0.00	97.65	2.00	0.00	0.00	0.07	0.00
97.69	2.00	0.00	0.00	0.04	0.00	97.74	2.00	0.00	0.00	0.05	0.00
97.81	2.00	0.00	0.00	0.07	0.00	97.88	2.00	0.00	0.00	0.08	0.00
97.93	2.00	0.00	0.00	0.05	0.00	98.03	2.00	0.00	0.00	0.10	0.00
98.15	2.00	0.00	0.00	0.12	0.00	98.21	2.00	0.00	0.00	0.06	0.00
98.32	2.00	0.00	0.00	0.11	0.00	98.42	2.00	0.00	0.00	0.09	0.00
98.47	2.00	0.00	0.00	0.05	0.00	98.57	2.00	0.00	0.00	0.10	0.00
98.70	2.00	0.00	0.00	0.13	0.00	98.78	2.00	0.00	0.00	0.08	0.00
98.85	2.00	0.00	0.00	0.06	0.00	98.86	2.00	0.00	0.00	0.01	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (ft)	FS	F_L	w_z	d_z	LPI	Depth (ft)	FS	F_L	w_z	d_z	LPI
98.92	2.00	0.00	0.00	0.06	0.00	98.98	2.00	0.00	0.00	0.06	0.00
99.03	2.00	0.00	0.00	0.05	0.00	99.11	2.00	0.00	0.00	0.07	0.00
99.18	2.00	0.00	0.00	0.07	0.00	99.23	2.00	0.00	0.00	0.05	0.00
99.32	2.00	0.00	0.00	0.09	0.00	99.37	2.00	0.00	0.00	0.05	0.00
99.45	2.00	0.00	0.00	0.08	0.00	99.56	2.00	0.00	0.00	0.11	0.00
99.64	2.00	0.00	0.00	0.07	0.00	99.71	2.00	0.00	0.00	0.07	0.00
99.75	2.00	0.00	0.00	0.04	0.00	99.90	2.00	0.00	0.00	0.15	0.00
99.95	2.00	0.00	0.00	0.05	0.00	100.04	2.00	0.00	0.00	0.09	0.00
100.14	2.00	0.00	0.00	0.09	0.00	100.14	2.00	0.00	0.00	0.00	0.00
100.15	2.00	0.00	0.00	0.01	0.00	100.19	2.00	0.00	0.00	0.03	0.00
100.21	2.00	0.00	0.00	0.02	0.00	100.24	2.00	0.00	0.00	0.03	0.00
100.28	2.00	0.00	0.00	0.05	0.00	100.31	2.00	0.00	0.00	0.02	0.00
100.33	2.00	0.00	0.00	0.02	0.00	100.38	2.00	0.00	0.00	0.05	0.00
100.39	2.00	0.00	0.00	0.01	0.00	100.43	2.00	0.00	0.00	0.03	0.00
100.48	2.00	0.00	0.00	0.05	0.00	100.53	2.00	0.00	0.00	0.05	0.00
100.57	2.00	0.00	0.00	0.05	0.00	100.60	2.00	0.00	0.00	0.02	0.00

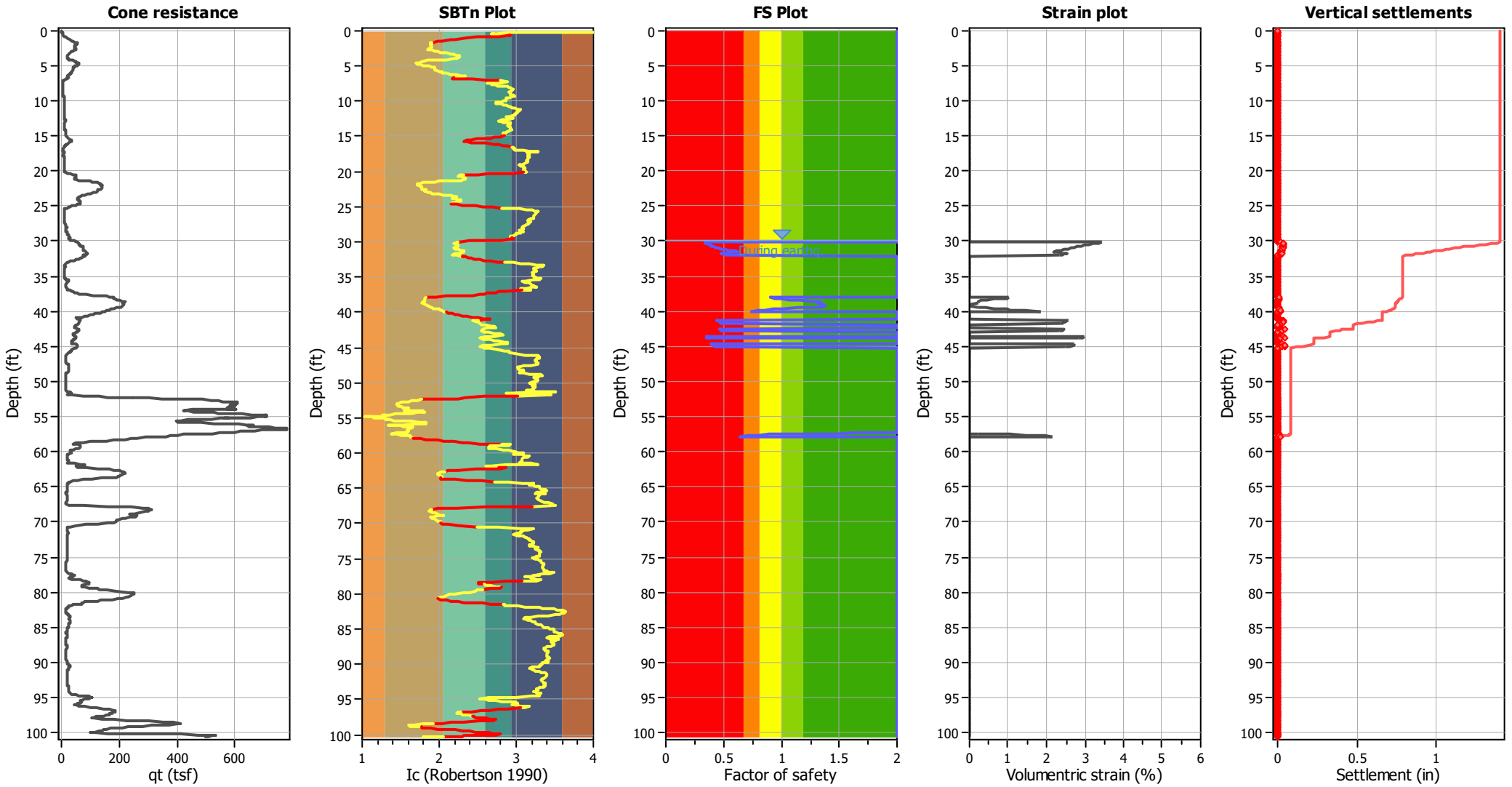
Overall liquefaction potential: 2.86

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (ft)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
30.06	59.16	2.00	0.00	1.00	0.00	30.13	60.99	2.00	0.00	1.00	0.00
30.18	62.30	0.34	3.44	1.00	0.02	30.28	64.44	0.35	3.35	1.00	0.04
30.37	67.53	0.36	3.22	1.00	0.04	30.47	71.05	0.37	3.09	1.00	0.04
30.57	73.87	0.38	3.00	1.00	0.04	30.66	76.12	0.40	2.92	1.00	0.03
30.74	78.31	0.41	2.86	1.00	0.03	30.82	80.52	0.42	2.79	1.00	0.03
30.90	82.93	0.43	2.72	1.00	0.03	31.01	85.67	0.45	2.65	1.00	0.04
31.10	89.47	0.48	2.56	1.00	0.03	31.19	93.96	0.51	2.46	1.00	0.03
31.28	98.21	0.54	2.37	1.00	0.03	31.35	101.82	0.58	2.30	1.00	0.02
31.43	104.59	0.60	2.25	1.00	0.02	31.53	107.28	0.63	2.21	1.00	0.02
31.60	101.10	0.57	2.32	1.00	0.02	31.67	95.74	0.52	2.42	1.00	0.02
31.77	91.18	0.48	2.52	1.00	0.03	31.84	93.40	0.50	2.47	1.00	0.02
31.91	95.19	0.51	2.43	1.00	0.02	31.98	97.23	0.53	2.39	1.00	0.02
31.98	99.23	0.55	2.35	1.00	0.00	32.04	100.65	0.56	2.32	1.00	0.02
32.12	102.19	2.00	0.00	1.00	0.00	32.16	105.63	2.00	0.00	1.00	0.00
32.27	108.77	2.00	0.00	1.00	0.00	32.33	111.51	2.00	0.00	1.00	0.00
32.41	112.40	2.00	0.00	1.00	0.00	32.50	111.66	2.00	0.00	1.00	0.00
32.58	110.12	2.00	0.00	1.00	0.00	32.66	108.68	2.00	0.00	1.00	0.00
32.74	107.79	2.00	0.00	1.00	0.00	32.84	107.96	2.00	0.00	1.00	0.00
32.90	107.62	2.00	0.00	1.00	0.00	32.98	104.08	2.00	0.00	1.00	0.00
33.08	101.84	2.00	0.00	1.00	0.00	33.14	99.50	2.00	0.00	1.00	0.00
33.22	96.06	2.00	0.00	1.00	0.00	33.32	91.43	2.00	0.00	1.00	0.00
33.37	85.28	2.00	0.00	1.00	0.00	33.47	81.70	2.00	0.00	1.00	0.00
33.56	79.85	2.00	0.00	1.00	0.00	33.63	80.15	2.00	0.00	1.00	0.00
33.71	78.37	2.00	0.00	1.00	0.00	33.81	72.19	2.00	0.00	1.00	0.00
33.90	65.65	2.00	0.00	1.00	0.00	33.95	60.28	2.00	0.00	1.00	0.00
34.04	59.84	2.00	0.00	1.00	0.00	34.14	59.54	2.00	0.00	1.00	0.00
34.17	59.63	2.00	0.00	1.00	0.00	34.20	59.92	2.00	0.00	1.00	0.00
34.26	60.14	2.00	0.00	1.00	0.00	34.35	59.91	2.00	0.00	1.00	0.00
34.43	59.45	2.00	0.00	1.00	0.00	34.49	58.59	2.00	0.00	1.00	0.00
34.59	57.25	2.00	0.00	1.00	0.00	34.69	55.91	2.00	0.00	1.00	0.00
34.73	54.88	2.00	0.00	1.00	0.00	34.83	54.34	2.00	0.00	1.00	0.00
34.90	54.48	2.00	0.00	1.00	0.00	34.98	55.47	2.00	0.00	1.00	0.00
35.07	58.28	2.00	0.00	1.00	0.00	35.16	64.79	2.00	0.00	1.00	0.00
35.26	76.48	2.00	0.00	1.00	0.00	35.33	89.71	2.00	0.00	1.00	0.00
35.40	101.03	2.00	0.00	1.00	0.00	35.50	106.70	2.00	0.00	1.00	0.00
35.57	109.72	2.00	0.00	1.00	0.00	35.65	112.36	2.00	0.00	1.00	0.00
35.71	115.22	2.00	0.00	1.00	0.00	35.79	116.27	2.00	0.00	1.00	0.00
35.85	113.90	2.00	0.00	1.00	0.00	35.94	109.71	2.00	0.00	1.00	0.00
35.99	103.66	2.00	0.00	1.00	0.00	36.08	95.94	2.00	0.00	1.00	0.00
36.17	88.35	2.00	0.00	1.00	0.00	36.24	82.76	2.00	0.00	1.00	0.00
36.33	81.11	2.00	0.00	1.00	0.00	36.42	82.08	2.00	0.00	1.00	0.00
36.52	77.16	2.00	0.00	1.00	0.00	36.61	74.88	2.00	0.00	1.00	0.00
36.70	76.79	2.00	0.00	1.00	0.00	36.78	88.43	2.00	0.00	1.00	0.00
36.85	99.18	2.00	0.00	1.00	0.00	36.87	103.88	2.00	0.00	1.00	0.00
36.91	105.17	2.00	0.00	1.00	0.00	36.97	104.77	2.00	0.00	1.00	0.00
37.06	105.20	2.00	0.00	1.00	0.00	37.12	107.91	2.00	0.00	1.00	0.00
37.20	112.33	2.00	0.00	1.00	0.00	37.27	114.30	2.00	0.00	1.00	0.00
37.35	112.42	2.00	0.00	1.00	0.00	37.44	108.21	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
37.49	102.76	2.00	0.00	1.00	0.00	37.59	95.81	2.00	0.00	1.00	0.00
37.64	90.11	2.00	0.00	1.00	0.00	37.70	94.79	2.00	0.00	1.00	0.00
37.78	108.37	2.00	0.00	1.00	0.00	37.83	120.19	2.00	0.00	1.00	0.00
37.92	126.68	2.00	0.00	1.00	0.00	37.97	130.53	2.00	0.00	1.00	0.00
38.07	133.13	0.90	1.03	1.00	0.01	38.14	135.64	0.94	1.00	1.00	0.01
38.22	138.68	0.99	0.65	1.00	0.01	38.31	143.23	1.06	0.44	1.00	0.00
38.41	148.66	1.16	0.31	1.00	0.00	38.52	154.32	1.27	0.21	1.00	0.00
38.64	157.41	1.33	0.21	1.00	0.00	38.74	158.10	1.34	0.21	1.00	0.00
38.80	157.57	1.33	0.21	1.00	0.00	38.89	156.57	1.31	0.21	1.00	0.00
38.94	158.84	1.36	0.00	1.00	0.00	39.03	159.69	1.37	0.00	1.00	0.00
39.13	160.46	1.39	0.00	1.00	0.00	39.23	160.12	1.38	0.00	1.00	0.00
39.35	158.27	1.34	0.21	1.00	0.00	39.42	154.08	1.26	0.21	1.00	0.00
39.51	148.22	1.14	0.43	1.00	0.00	39.60	141.37	1.02	0.64	1.00	0.01
39.70	135.85	0.93	1.00	1.00	0.01	39.78	130.75	0.86	1.05	1.00	0.01
39.90	126.28	0.80	1.45	1.00	0.02	39.99	121.65	0.74	1.86	1.00	0.02
40.09	117.75	2.00	0.00	1.00	0.00	40.18	114.33	2.00	0.00	1.00	0.00
40.23	111.30	2.00	0.00	1.00	0.00	40.33	108.90	2.00	0.00	1.00	0.00
40.43	107.17	2.00	0.00	1.00	0.00	40.52	107.68	2.00	0.00	1.00	0.00
40.61	106.53	2.00	0.00	1.00	0.00	40.69	106.96	2.00	0.00	1.00	0.00
40.80	106.21	2.00	0.00	1.00	0.00	40.87	107.20	2.00	0.00	1.00	0.00
40.95	107.50	2.00	0.00	1.00	0.00	40.97	105.79	2.00	0.00	1.00	0.00
41.01	101.77	2.00	0.00	1.00	0.00	41.07	94.92	2.00	0.00	1.00	0.00
41.15	90.47	2.00	0.00	1.00	0.00	41.26	89.74	0.44	2.55	1.00	0.03
41.35	91.40	0.45	2.52	1.00	0.03	41.47	93.27	0.46	2.47	1.00	0.04
41.59	94.19	0.47	2.45	1.00	0.03	41.69	95.29	0.48	2.43	1.00	0.03
41.78	97.63	0.49	2.38	1.00	0.03	41.88	100.94	2.00	0.00	1.00	0.00
41.98	103.21	2.00	0.00	1.00	0.00	42.08	103.54	2.00	0.00	1.00	0.00
42.16	102.01	2.00	0.00	1.00	0.00	42.24	99.69	2.00	0.00	1.00	0.00
42.31	97.23	2.00	0.00	1.00	0.00	42.45	95.61	0.48	2.42	1.00	0.04
42.55	94.91	0.47	2.44	1.00	0.03	42.60	95.14	0.47	2.43	1.00	0.01
42.70	96.60	0.48	2.40	1.00	0.03	42.81	99.43	0.51	2.35	1.00	0.03
42.89	103.15	2.00	0.00	1.00	0.00	42.98	106.61	2.00	0.00	1.00	0.00
43.08	108.99	2.00	0.00	1.00	0.00	43.17	109.35	2.00	0.00	1.00	0.00
43.27	107.03	2.00	0.00	1.00	0.00	43.37	95.48	2.00	0.00	1.00	0.00
43.50	83.44	2.00	0.00	1.00	0.00	43.61	73.95	0.35	2.99	1.00	0.04
43.74	75.29	0.35	2.95	1.00	0.05	43.79	79.06	0.37	2.83	1.00	0.02
43.86	84.59	2.00	0.00	1.00	0.00	43.94	91.16	2.00	0.00	1.00	0.00
44.00	98.08	2.00	0.00	1.00	0.00	44.08	103.37	2.00	0.00	1.00	0.00
44.17	106.26	2.00	0.00	1.00	0.00	44.27	105.00	2.00	0.00	1.00	0.00
44.42	100.72	2.00	0.00	1.00	0.00	44.52	95.03	2.00	0.00	1.00	0.00
44.61	87.72	2.00	0.00	1.00	0.00	44.71	83.46	0.40	2.71	1.00	0.03
44.85	83.87	0.40	2.70	1.00	0.05	44.95	88.11	0.42	2.59	1.00	0.03
45.09	92.06	0.45	2.50	1.00	0.04	45.19	95.00	2.00	0.00	1.00	0.00
45.33	98.48	2.00	0.00	1.00	0.00	45.42	100.02	2.00	0.00	1.00	0.00
45.57	98.64	2.00	0.00	1.00	0.00	45.68	94.66	2.00	0.00	1.00	0.00
45.81	87.72	2.00	0.00	1.00	0.00	45.92	82.93	2.00	0.00	1.00	0.00
46.05	82.51	2.00	0.00	1.00	0.00	46.16	86.12	2.00	0.00	1.00	0.00
46.17	85.57	2.00	0.00	1.00	0.00	46.23	84.09	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
46.29	82.02	2.00	0.00	1.00	0.00	46.34	78.81	2.00	0.00	1.00	0.00
46.42	74.90	2.00	0.00	1.00	0.00	46.48	70.80	2.00	0.00	1.00	0.00
46.52	67.86	2.00	0.00	1.00	0.00	46.60	65.79	2.00	0.00	1.00	0.00
46.67	64.21	2.00	0.00	1.00	0.00	46.74	63.02	2.00	0.00	1.00	0.00
46.82	61.88	2.00	0.00	1.00	0.00	46.88	61.07	2.00	0.00	1.00	0.00
46.96	60.61	2.00	0.00	1.00	0.00	47.06	60.52	2.00	0.00	1.00	0.00
47.15	61.03	2.00	0.00	1.00	0.00	47.24	65.10	2.00	0.00	1.00	0.00
47.35	75.39	2.00	0.00	1.00	0.00	47.49	80.67	2.00	0.00	1.00	0.00
47.58	82.65	2.00	0.00	1.00	0.00	47.73	80.95	2.00	0.00	1.00	0.00
47.83	81.84	2.00	0.00	1.00	0.00	47.87	83.19	2.00	0.00	1.00	0.00
47.89	82.12	2.00	0.00	1.00	0.00	47.94	81.59	2.00	0.00	1.00	0.00
48.02	80.90	2.00	0.00	1.00	0.00	48.07	81.07	2.00	0.00	1.00	0.00
48.12	82.45	2.00	0.00	1.00	0.00	48.18	84.09	2.00	0.00	1.00	0.00
48.26	85.42	2.00	0.00	1.00	0.00	48.31	84.77	2.00	0.00	1.00	0.00
48.38	82.58	2.00	0.00	1.00	0.00	48.46	79.31	2.00	0.00	1.00	0.00
48.52	75.99	2.00	0.00	1.00	0.00	48.60	72.40	2.00	0.00	1.00	0.00
48.68	69.64	2.00	0.00	1.00	0.00	48.74	67.76	2.00	0.00	1.00	0.00
48.82	67.24	2.00	0.00	1.00	0.00	48.89	66.41	2.00	0.00	1.00	0.00
48.99	64.98	2.00	0.00	1.00	0.00	49.05	62.48	2.00	0.00	1.00	0.00
49.12	59.74	2.00	0.00	1.00	0.00	49.18	57.20	2.00	0.00	1.00	0.00
49.27	55.71	2.00	0.00	1.00	0.00	49.32	54.42	2.00	0.00	1.00	0.00
49.42	53.88	2.00	0.00	1.00	0.00	49.48	53.63	2.00	0.00	1.00	0.00
49.56	54.09	2.00	0.00	1.00	0.00	49.66	55.25	2.00	0.00	1.00	0.00
49.76	56.33	2.00	0.00	1.00	0.00	49.85	54.00	2.00	0.00	1.00	0.00
49.99	51.28	2.00	0.00	1.00	0.00	50.09	49.07	2.00	0.00	1.00	0.00
50.21	50.39	2.00	0.00	1.00	0.00	50.24	50.47	2.00	0.00	1.00	0.00
50.29	49.66	2.00	0.00	1.00	0.00	50.38	48.82	2.00	0.00	1.00	0.00
50.47	48.36	2.00	0.00	1.00	0.00	50.52	48.61	2.00	0.00	1.00	0.00
50.62	49.09	2.00	0.00	1.00	0.00	50.66	49.58	2.00	0.00	1.00	0.00
50.76	50.11	2.00	0.00	1.00	0.00	50.83	51.29	2.00	0.00	1.00	0.00
50.91	53.36	2.00	0.00	1.00	0.00	51.00	55.29	2.00	0.00	1.00	0.00
51.06	56.99	2.00	0.00	1.00	0.00	51.15	61.08	2.00	0.00	1.00	0.00
51.24	67.57	2.00	0.00	1.00	0.00	51.31	75.27	2.00	0.00	1.00	0.00
51.39	80.15	2.00	0.00	1.00	0.00	51.48	82.64	2.00	0.00	1.00	0.00
51.58	87.30	2.00	0.00	1.00	0.00	51.68	91.85	2.00	0.00	1.00	0.00
51.77	100.06	2.00	0.00	1.00	0.00	51.90	106.47	2.00	0.00	1.00	0.00
52.01	110.20	2.00	0.00	1.00	0.00	52.11	121.05	2.00	0.00	1.00	0.00
52.26	131.90	2.00	0.00	1.00	0.00	52.30	146.55	2.00	0.00	1.00	0.00
52.33	162.63	2.00	0.00	1.00	0.00	52.35	192.22	2.00	0.00	1.00	0.00
52.40	209.95	2.00	0.00	1.00	0.00	52.45	216.58	2.00	0.00	1.00	0.00
52.50	229.89	2.00	0.00	1.00	0.00	52.55	248.98	2.00	0.00	1.00	0.00
52.60	273.15	2.00	0.00	1.00	0.00	52.65	289.64	2.00	0.00	1.00	0.00
52.71	297.95	2.00	0.00	1.00	0.00	52.77	303.79	2.00	0.00	1.00	0.00
52.82	312.99	2.00	0.00	1.00	0.00	52.88	323.84	2.00	0.00	1.00	0.00
52.93	331.46	2.00	0.00	1.00	0.00	52.98	338.95	2.00	0.00	1.00	0.00
53.03	340.39	2.00	0.00	1.00	0.00	53.08	340.01	2.00	0.00	1.00	0.00
53.12	335.78	2.00	0.00	1.00	0.00	53.17	333.99	2.00	0.00	1.00	0.00
53.23	335.19	2.00	0.00	1.00	0.00	53.28	332.45	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
53.37	327.80	2.00	0.00	1.00	0.00	53.42	325.17	2.00	0.00	1.00	0.00
53.46	326.50	2.00	0.00	1.00	0.00	53.53	333.09	2.00	0.00	1.00	0.00
53.61	331.84	2.00	0.00	1.00	0.00	53.62	323.39	2.00	0.00	1.00	0.00
53.65	318.67	2.00	0.00	1.00	0.00	53.67	317.12	2.00	0.00	1.00	0.00
53.70	323.95	2.00	0.00	1.00	0.00	53.74	323.26	2.00	0.00	1.00	0.00
53.76	323.74	2.00	0.00	1.00	0.00	53.80	322.06	2.00	0.00	1.00	0.00
53.84	320.07	2.00	0.00	1.00	0.00	53.90	320.12	2.00	0.00	1.00	0.00
53.91	315.61	2.00	0.00	1.00	0.00	53.95	317.38	2.00	0.00	1.00	0.00
53.96	320.83	2.00	0.00	1.00	0.00	53.98	332.48	2.00	0.00	1.00	0.00
53.99	333.50	2.00	0.00	1.00	0.00	54.01	327.46	2.00	0.00	1.00	0.00
54.02	320.31	2.00	0.00	1.00	0.00	54.03	305.74	2.00	0.00	1.00	0.00
54.04	276.21	2.00	0.00	1.00	0.00	54.05	260.14	2.00	0.00	1.00	0.00
54.09	254.46	2.00	0.00	1.00	0.00	54.10	254.57	2.00	0.00	1.00	0.00
54.13	254.64	2.00	0.00	1.00	0.00	54.14	254.59	2.00	0.00	1.00	0.00
54.19	255.77	2.00	0.00	1.00	0.00	54.19	258.95	2.00	0.00	1.00	0.00
54.24	259.93	2.00	0.00	1.00	0.00	54.29	249.88	2.00	0.00	1.00	0.00
54.33	261.31	2.00	0.00	1.00	0.00	54.38	272.80	2.00	0.00	1.00	0.00
54.39	282.62	2.00	0.00	1.00	0.00	54.43	291.66	2.00	0.00	1.00	0.00
54.48	299.32	2.00	0.00	1.00	0.00	54.52	306.76	2.00	0.00	1.00	0.00
54.58	316.20	2.00	0.00	1.00	0.00	54.62	323.46	2.00	0.00	1.00	0.00
54.65	333.00	2.00	0.00	1.00	0.00	54.67	343.41	2.00	0.00	1.00	0.00
54.71	362.60	2.00	0.00	1.00	0.00	54.77	374.21	2.00	0.00	1.00	0.00
54.81	387.19	2.00	0.00	1.00	0.00	54.85	387.70	2.00	0.00	1.00	0.00
54.86	390.48	2.00	0.00	1.00	0.00	54.87	387.26	2.00	0.00	1.00	0.00
54.91	387.35	2.00	0.00	1.00	0.00	54.96	389.17	2.00	0.00	1.00	0.00
55.00	386.89	2.00	0.00	1.00	0.00	55.01	382.82	2.00	0.00	1.00	0.00
55.05	373.47	2.00	0.00	1.00	0.00	55.10	357.87	2.00	0.00	1.00	0.00
55.12	331.72	2.00	0.00	1.00	0.00	55.13	313.58	2.00	0.00	1.00	0.00
55.14	309.22	2.00	0.00	1.00	0.00	55.19	316.75	2.00	0.00	1.00	0.00
55.20	316.38	2.00	0.00	1.00	0.00	55.25	308.48	2.00	0.00	1.00	0.00
55.29	299.55	2.00	0.00	1.00	0.00	55.33	284.92	2.00	0.00	1.00	0.00
55.38	263.59	2.00	0.00	1.00	0.00	55.48	240.38	2.00	0.00	1.00	0.00
55.57	227.87	2.00	0.00	1.00	0.00	55.63	237.94	2.00	0.00	1.00	0.00
55.72	244.53	2.00	0.00	1.00	0.00	55.80	260.68	2.00	0.00	1.00	0.00
55.86	259.76	2.00	0.00	1.00	0.00	55.97	288.32	2.00	0.00	1.00	0.00
56.01	306.20	2.00	0.00	1.00	0.00	56.06	186.61	2.00	0.00	1.00	0.00
56.11	194.57	2.00	0.00	1.00	0.00	56.15	203.27	2.00	0.00	1.00	0.00
56.20	209.60	2.00	0.00	1.00	0.00	56.27	210.15	2.00	0.00	1.00	0.00
56.27	210.45	2.00	0.00	1.00	0.00	56.30	203.39	2.00	0.00	1.00	0.00
56.33	205.64	2.00	0.00	1.00	0.00	56.35	205.00	2.00	0.00	1.00	0.00
56.40	211.31	2.00	0.00	1.00	0.00	56.41	211.76	2.00	0.00	1.00	0.00
56.44	215.53	2.00	0.00	1.00	0.00	56.49	219.75	2.00	0.00	1.00	0.00
56.54	226.71	2.00	0.00	1.00	0.00	56.58	232.85	2.00	0.00	1.00	0.00
56.59	236.93	2.00	0.00	1.00	0.00	56.64	239.07	2.00	0.00	1.00	0.00
56.69	241.29	2.00	0.00	1.00	0.00	56.73	245.40	2.00	0.00	1.00	0.00
56.78	245.38	2.00	0.00	1.00	0.00	56.83	239.22	2.00	0.00	1.00	0.00
56.88	230.32	2.00	0.00	1.00	0.00	56.89	223.03	2.00	0.00	1.00	0.00
56.95	217.71	2.00	0.00	1.00	0.00	57.01	209.81	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
57.07	202.70	2.00	0.00	1.00	0.00	57.11	194.25	2.00	0.00	1.00	0.00
57.17	187.56	2.00	0.00	1.00	0.00	57.26	179.66	1.89	0.00	1.00	0.00
57.31	171.06	1.67	0.00	1.00	0.00	57.37	162.50	1.46	0.00	1.00	0.00
57.45	152.96	1.26	0.21	1.00	0.00	57.51	140.63	1.03	0.64	1.00	0.00
57.53	131.27	0.89	1.05	1.00	0.00	57.59	124.87	0.80	1.47	1.00	0.01
57.63	124.05	0.79	1.48	1.00	0.01	57.68	121.66	0.76	1.53	1.00	0.01
57.73	120.01	0.74	1.90	1.00	0.01	57.78	117.62	0.71	1.95	1.00	0.01
57.86	111.55	0.64	2.14	1.00	0.02	57.92	100.97	2.00	0.00	1.00	0.00
57.98	89.82	2.00	0.00	1.00	0.00	58.06	95.51	2.00	0.00	1.00	0.00
58.12	92.39	2.00	0.00	1.00	0.00	58.21	88.73	2.00	0.00	1.00	0.00
58.26	85.71	2.00	0.00	1.00	0.00	58.35	81.38	2.00	0.00	1.00	0.00
58.41	74.91	2.00	0.00	1.00	0.00	58.50	70.73	2.00	0.00	1.00	0.00
58.56	67.27	2.00	0.00	1.00	0.00	58.64	74.61	2.00	0.00	1.00	0.00
58.73	81.15	2.00	0.00	1.00	0.00	58.80	87.16	2.00	0.00	1.00	0.00
58.84	91.44	2.00	0.00	1.00	0.00	58.85	91.06	2.00	0.00	1.00	0.00
58.93	87.49	2.00	0.00	1.00	0.00	58.98	82.49	2.00	0.00	1.00	0.00
59.02	79.02	2.00	0.00	1.00	0.00	59.12	77.74	2.00	0.00	1.00	0.00
59.17	78.34	2.00	0.00	1.00	0.00	59.27	80.06	2.00	0.00	1.00	0.00
59.31	82.31	2.00	0.00	1.00	0.00	59.41	84.40	2.00	0.00	1.00	0.00
59.46	85.91	2.00	0.00	1.00	0.00	59.55	86.53	2.00	0.00	1.00	0.00
59.65	82.12	2.00	0.00	1.00	0.00	59.70	78.48	2.00	0.00	1.00	0.00
59.80	75.77	2.00	0.00	1.00	0.00	59.89	79.29	2.00	0.00	1.00	0.00
59.94	82.68	2.00	0.00	1.00	0.00	60.01	85.21	2.00	0.00	1.00	0.00
60.02	85.70	2.00	0.00	1.00	0.00	60.08	84.70	2.00	0.00	1.00	0.00
60.12	83.40	2.00	0.00	1.00	0.00	60.17	81.32	2.00	0.00	1.00	0.00
60.27	76.99	2.00	0.00	1.00	0.00	60.31	71.83	2.00	0.00	1.00	0.00
60.37	67.16	2.00	0.00	1.00	0.00	60.46	64.16	2.00	0.00	1.00	0.00
60.51	61.05	2.00	0.00	1.00	0.00	60.61	59.48	2.00	0.00	1.00	0.00
60.65	58.49	2.00	0.00	1.00	0.00	60.75	58.52	2.00	0.00	1.00	0.00
60.81	58.52	2.00	0.00	1.00	0.00	60.89	58.14	2.00	0.00	1.00	0.00
60.94	58.37	2.00	0.00	1.00	0.00	61.03	59.27	2.00	0.00	1.00	0.00
61.09	59.56	2.00	0.00	1.00	0.00	61.19	59.09	2.00	0.00	1.00	0.00
61.24	58.48	2.00	0.00	1.00	0.00	61.33	59.55	2.00	0.00	1.00	0.00
61.38	65.92	2.00	0.00	1.00	0.00	61.47	73.50	2.00	0.00	1.00	0.00
61.53	81.14	2.00	0.00	1.00	0.00	61.62	81.97	2.00	0.00	1.00	0.00
61.70	82.73	2.00	0.00	1.00	0.00	61.77	84.93	2.00	0.00	1.00	0.00
61.86	89.66	2.00	0.00	1.00	0.00	61.95	94.89	2.00	0.00	1.00	0.00
61.97	96.91	2.00	0.00	1.00	0.00	62.01	99.66	2.00	0.00	1.00	0.00
62.10	99.23	2.00	0.00	1.00	0.00	62.24	89.92	2.00	0.00	1.00	0.00
62.34	71.54	2.00	0.00	1.00	0.00	62.49	64.77	2.00	0.00	1.00	0.00
62.54	69.68	2.00	0.00	1.00	0.00	62.66	73.33	2.00	0.00	1.00	0.00
62.74	77.94	2.00	0.00	1.00	0.00	62.87	80.99	2.00	0.00	1.00	0.00
62.92	82.65	2.00	0.00	1.00	0.00	63.03	83.41	2.00	0.00	1.00	0.00
63.15	83.38	2.00	0.00	1.00	0.00	63.26	82.35	2.00	0.00	1.00	0.00
63.37	80.92	2.00	0.00	1.00	0.00	63.45	78.49	2.00	0.00	1.00	0.00
63.54	76.31	2.00	0.00	1.00	0.00	63.61	73.61	2.00	0.00	1.00	0.00
63.69	69.47	2.00	0.00	1.00	0.00	63.79	67.77	2.00	0.00	1.00	0.00
63.89	66.74	2.00	0.00	1.00	0.00	63.98	71.48	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
64.07	71.91	2.00	0.00	1.00	0.00	64.15	76.48	2.00	0.00	1.00	0.00
64.23	77.68	2.00	0.00	1.00	0.00	64.26	78.26	2.00	0.00	1.00	0.00
64.29	78.14	2.00	0.00	1.00	0.00	64.33	74.86	2.00	0.00	1.00	0.00
64.43	70.78	2.00	0.00	1.00	0.00	64.47	66.07	2.00	0.00	1.00	0.00
64.53	64.15	2.00	0.00	1.00	0.00	64.62	63.40	2.00	0.00	1.00	0.00
64.72	63.23	2.00	0.00	1.00	0.00	64.78	63.74	2.00	0.00	1.00	0.00
64.86	65.01	2.00	0.00	1.00	0.00	64.96	68.31	2.00	0.00	1.00	0.00
65.06	71.61	2.00	0.00	1.00	0.00	65.11	74.58	2.00	0.00	1.00	0.00
65.21	75.90	2.00	0.00	1.00	0.00	65.31	76.26	2.00	0.00	1.00	0.00
65.40	72.77	2.00	0.00	1.00	0.00	65.50	67.97	2.00	0.00	1.00	0.00
65.58	63.13	2.00	0.00	1.00	0.00	65.68	61.17	2.00	0.00	1.00	0.00
65.78	60.45	2.00	0.00	1.00	0.00	65.84	59.69	2.00	0.00	1.00	0.00
65.86	59.62	2.00	0.00	1.00	0.00	65.87	59.36	2.00	0.00	1.00	0.00
65.98	59.09	2.00	0.00	1.00	0.00	66.10	60.13	2.00	0.00	1.00	0.00
66.21	62.32	2.00	0.00	1.00	0.00	66.34	63.01	2.00	0.00	1.00	0.00
66.48	63.55	2.00	0.00	1.00	0.00	66.62	62.45	2.00	0.00	1.00	0.00
66.68	64.07	2.00	0.00	1.00	0.00	66.87	67.94	2.00	0.00	1.00	0.00
66.96	73.89	2.00	0.00	1.00	0.00	67.11	78.15	2.00	0.00	1.00	0.00
67.21	76.60	2.00	0.00	1.00	0.00	67.35	73.18	2.00	0.00	1.00	0.00
67.45	77.86	2.00	0.00	1.00	0.00	67.59	88.71	2.00	0.00	1.00	0.00
67.68	83.67	2.00	0.00	1.00	0.00	67.83	74.68	2.00	0.00	1.00	0.00
67.92	88.64	2.00	0.00	1.00	0.00	68.02	99.35	2.00	0.00	1.00	0.00
68.07	103.71	2.00	0.00	1.00	0.00	68.16	105.26	2.00	0.00	1.00	0.00
68.26	106.54	2.00	0.00	1.00	0.00	68.35	106.44	2.00	0.00	1.00	0.00
68.45	105.37	2.00	0.00	1.00	0.00	68.55	103.72	2.00	0.00	1.00	0.00
68.65	98.57	2.00	0.00	1.00	0.00	68.78	94.35	2.00	0.00	1.00	0.00
68.78	90.91	2.00	0.00	1.00	0.00	68.79	89.70	2.00	0.00	1.00	0.00
68.83	89.08	2.00	0.00	1.00	0.00	68.93	88.59	2.00	0.00	1.00	0.00
68.98	89.18	2.00	0.00	1.00	0.00	69.04	89.05	2.00	0.00	1.00	0.00
69.12	89.10	2.00	0.00	1.00	0.00	69.22	88.23	2.00	0.00	1.00	0.00
69.28	86.25	2.00	0.00	1.00	0.00	69.36	83.22	2.00	0.00	1.00	0.00
69.45	79.21	2.00	0.00	1.00	0.00	69.60	75.34	2.00	0.00	1.00	0.00
69.70	72.05	2.00	0.00	1.00	0.00	69.80	70.68	2.00	0.00	1.00	0.00
69.89	70.30	2.00	0.00	1.00	0.00	69.98	69.82	2.00	0.00	1.00	0.00
70.08	67.53	2.00	0.00	1.00	0.00	70.18	63.51	2.00	0.00	1.00	0.00
70.32	61.16	2.00	0.00	1.00	0.00	70.42	66.77	2.00	0.00	1.00	0.00
70.54	74.19	2.00	0.00	1.00	0.00	70.66	75.54	2.00	0.00	1.00	0.00
70.75	72.70	2.00	0.00	1.00	0.00	70.80	66.71	2.00	0.00	1.00	0.00
70.89	59.87	2.00	0.00	1.00	0.00	70.99	53.00	2.00	0.00	1.00	0.00
71.08	49.46	2.00	0.00	1.00	0.00	71.17	47.79	2.00	0.00	1.00	0.00
71.23	47.05	2.00	0.00	1.00	0.00	71.33	46.20	2.00	0.00	1.00	0.00
71.42	44.64	2.00	0.00	1.00	0.00	71.52	43.06	2.00	0.00	1.00	0.00
71.58	44.01	2.00	0.00	1.00	0.00	71.67	47.43	2.00	0.00	1.00	0.00
71.81	50.76	2.00	0.00	1.00	0.00	71.82	52.55	2.00	0.00	1.00	0.00
71.86	52.82	2.00	0.00	1.00	0.00	71.91	52.95	2.00	0.00	1.00	0.00
71.97	53.27	2.00	0.00	1.00	0.00	72.05	53.72	2.00	0.00	1.00	0.00
72.10	54.35	2.00	0.00	1.00	0.00	72.20	54.79	2.00	0.00	1.00	0.00
72.25	55.49	2.00	0.00	1.00	0.00	72.34	56.94	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
72.44	58.80	2.00	0.00	1.00	0.00	72.53	60.40	2.00	0.00	1.00	0.00
72.63	61.13	2.00	0.00	1.00	0.00	72.69	61.14	2.00	0.00	1.00	0.00
72.82	60.87	2.00	0.00	1.00	0.00	72.92	60.05	2.00	0.00	1.00	0.00
73.06	59.27	2.00	0.00	1.00	0.00	73.16	59.57	2.00	0.00	1.00	0.00
73.30	60.65	2.00	0.00	1.00	0.00	73.35	61.53	2.00	0.00	1.00	0.00
73.38	61.23	2.00	0.00	1.00	0.00	73.47	60.67	2.00	0.00	1.00	0.00
73.53	60.20	2.00	0.00	1.00	0.00	73.62	59.95	2.00	0.00	1.00	0.00
73.71	60.28	2.00	0.00	1.00	0.00	73.77	61.46	2.00	0.00	1.00	0.00
73.86	63.08	2.00	0.00	1.00	0.00	73.96	64.61	2.00	0.00	1.00	0.00
74.06	65.59	2.00	0.00	1.00	0.00	74.13	66.22	2.00	0.00	1.00	0.00
74.24	66.66	2.00	0.00	1.00	0.00	74.34	67.26	2.00	0.00	1.00	0.00
74.44	67.81	2.00	0.00	1.00	0.00	74.58	67.28	2.00	0.00	1.00	0.00
74.68	62.80	2.00	0.00	1.00	0.00	74.80	58.74	2.00	0.00	1.00	0.00
74.92	56.43	2.00	0.00	1.00	0.00	75.07	58.35	2.00	0.00	1.00	0.00
75.08	59.34	2.00	0.00	1.00	0.00	75.11	59.53	2.00	0.00	1.00	0.00
75.16	60.28	2.00	0.00	1.00	0.00	75.25	61.74	2.00	0.00	1.00	0.00
75.32	63.23	2.00	0.00	1.00	0.00	75.40	63.73	2.00	0.00	1.00	0.00
75.50	62.77	2.00	0.00	1.00	0.00	75.59	60.75	2.00	0.00	1.00	0.00
75.69	58.60	2.00	0.00	1.00	0.00	75.78	56.46	2.00	0.00	1.00	0.00
75.88	54.66	2.00	0.00	1.00	0.00	75.96	52.90	2.00	0.00	1.00	0.00
76.05	51.65	2.00	0.00	1.00	0.00	76.14	51.00	2.00	0.00	1.00	0.00
76.26	51.09	2.00	0.00	1.00	0.00	76.36	51.38	2.00	0.00	1.00	0.00
76.41	51.50	2.00	0.00	1.00	0.00	76.51	51.17	2.00	0.00	1.00	0.00
76.65	51.04	2.00	0.00	1.00	0.00	76.72	51.12	2.00	0.00	1.00	0.00
76.79	51.39	2.00	0.00	1.00	0.00	76.89	53.53	2.00	0.00	1.00	0.00
76.98	61.89	2.00	0.00	1.00	0.00	77.08	69.60	2.00	0.00	1.00	0.00
77.18	77.29	2.00	0.00	1.00	0.00	77.28	84.26	2.00	0.00	1.00	0.00
77.37	93.62	2.00	0.00	1.00	0.00	77.42	100.64	2.00	0.00	1.00	0.00
77.42	104.44	2.00	0.00	1.00	0.00	77.44	107.05	2.00	0.00	1.00	0.00
77.48	110.31	2.00	0.00	1.00	0.00	77.52	113.00	2.00	0.00	1.00	0.00
77.54	114.44	2.00	0.00	1.00	0.00	77.57	115.54	2.00	0.00	1.00	0.00
77.62	115.93	2.00	0.00	1.00	0.00	77.65	115.64	2.00	0.00	1.00	0.00
77.67	113.32	2.00	0.00	1.00	0.00	77.71	111.24	2.00	0.00	1.00	0.00
77.71	107.78	2.00	0.00	1.00	0.00	77.76	104.25	2.00	0.00	1.00	0.00
77.81	98.88	2.00	0.00	1.00	0.00	77.90	94.60	2.00	0.00	1.00	0.00
77.95	92.44	2.00	0.00	1.00	0.00	78.01	91.29	2.00	0.00	1.00	0.00
78.10	89.37	2.00	0.00	1.00	0.00	78.16	84.71	2.00	0.00	1.00	0.00
78.24	79.05	2.00	0.00	1.00	0.00	78.29	73.14	2.00	0.00	1.00	0.00
78.39	69.27	2.00	0.00	1.00	0.00	78.47	68.51	2.00	0.00	1.00	0.00
78.53	71.72	2.00	0.00	1.00	0.00	78.62	77.71	2.00	0.00	1.00	0.00
78.68	84.02	2.00	0.00	1.00	0.00	78.69	89.57	2.00	0.00	1.00	0.00
78.78	95.10	2.00	0.00	1.00	0.00	78.81	102.04	2.00	0.00	1.00	0.00
78.92	107.35	2.00	0.00	1.00	0.00	79.03	107.43	2.00	0.00	1.00	0.00
79.16	99.26	2.00	0.00	1.00	0.00	79.26	88.45	2.00	0.00	1.00	0.00
79.35	83.92	2.00	0.00	1.00	0.00	79.45	85.78	2.00	0.00	1.00	0.00
79.54	89.58	2.00	0.00	1.00	0.00	79.64	91.91	2.00	0.00	1.00	0.00
79.74	93.85	2.00	0.00	1.00	0.00	79.88	94.86	2.00	0.00	1.00	0.00
79.98	95.73	2.00	0.00	1.00	0.00	80.12	95.14	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
80.22	91.22	2.00	0.00	1.00	0.00	80.36	86.07	2.00	0.00	1.00	0.00
80.46	81.11	2.00	0.00	1.00	0.00	80.60	77.21	2.00	0.00	1.00	0.00
80.70	74.37	2.00	0.00	1.00	0.00	80.83	72.04	2.00	0.00	1.00	0.00
80.94	69.62	2.00	0.00	1.00	0.00	81.01	67.91	2.00	0.00	1.00	0.00
81.04	66.50	2.00	0.00	1.00	0.00	81.09	65.97	2.00	0.00	1.00	0.00
81.13	66.04	2.00	0.00	1.00	0.00	81.18	67.98	2.00	0.00	1.00	0.00
81.23	72.13	2.00	0.00	1.00	0.00	81.28	77.64	2.00	0.00	1.00	0.00
81.33	84.19	2.00	0.00	1.00	0.00	81.37	92.48	2.00	0.00	1.00	0.00
81.42	100.46	2.00	0.00	1.00	0.00	81.47	106.15	2.00	0.00	1.00	0.00
81.52	109.13	2.00	0.00	1.00	0.00	81.56	111.09	2.00	0.00	1.00	0.00
81.61	112.75	2.00	0.00	1.00	0.00	81.64	114.41	2.00	0.00	1.00	0.00
81.70	116.91	2.00	0.00	1.00	0.00	81.75	118.94	2.00	0.00	1.00	0.00
81.79	119.14	2.00	0.00	1.00	0.00	81.82	116.62	2.00	0.00	1.00	0.00
81.86	112.49	2.00	0.00	1.00	0.00	81.91	107.66	2.00	0.00	1.00	0.00
81.95	102.27	2.00	0.00	1.00	0.00	82.00	95.81	2.00	0.00	1.00	0.00
82.09	89.46	2.00	0.00	1.00	0.00	82.15	84.64	2.00	0.00	1.00	0.00
82.19	81.03	2.00	0.00	1.00	0.00	82.26	77.56	2.00	0.00	1.00	0.00
82.34	74.17	2.00	0.00	1.00	0.00	82.39	71.81	2.00	0.00	1.00	0.00
82.48	69.97	2.00	0.00	1.00	0.00	82.58	68.21	2.00	0.00	1.00	0.00
82.62	66.60	2.00	0.00	1.00	0.00	82.70	65.56	2.00	0.00	1.00	0.00
82.77	64.46	2.00	0.00	1.00	0.00	82.87	64.01	2.00	0.00	1.00	0.00
82.96	63.38	2.00	0.00	1.00	0.00	83.06	63.34	2.00	0.00	1.00	0.00
83.16	63.10	2.00	0.00	1.00	0.00	83.25	62.94	2.00	0.00	1.00	0.00
83.34	62.57	2.00	0.00	1.00	0.00	83.44	63.55	2.00	0.00	1.00	0.00
83.54	64.89	2.00	0.00	1.00	0.00	83.64	66.49	2.00	0.00	1.00	0.00
83.73	68.29	2.00	0.00	1.00	0.00	83.83	70.46	2.00	0.00	1.00	0.00
83.85	73.38	2.00	0.00	1.00	0.00	83.89	75.93	2.00	0.00	1.00	0.00
83.94	81.26	2.00	0.00	1.00	0.00	84.04	85.92	2.00	0.00	1.00	0.00
84.09	90.10	2.00	0.00	1.00	0.00	84.13	91.94	2.00	0.00	1.00	0.00
84.18	93.61	2.00	0.00	1.00	0.00	84.25	94.85	2.00	0.00	1.00	0.00
84.33	95.60	2.00	0.00	1.00	0.00	84.37	95.90	2.00	0.00	1.00	0.00
84.46	94.98	2.00	0.00	1.00	0.00	84.52	93.43	2.00	0.00	1.00	0.00
84.57	91.27	2.00	0.00	1.00	0.00	84.67	90.00	2.00	0.00	1.00	0.00
84.71	89.72	2.00	0.00	1.00	0.00	84.81	90.86	2.00	0.00	1.00	0.00
84.86	92.62	2.00	0.00	1.00	0.00	84.91	94.03	2.00	0.00	1.00	0.00
85.00	94.63	2.00	0.00	1.00	0.00	85.05	93.94	2.00	0.00	1.00	0.00
85.15	92.30	2.00	0.00	1.00	0.00	85.19	89.13	2.00	0.00	1.00	0.00
85.29	85.98	2.00	0.00	1.00	0.00	85.35	83.14	2.00	0.00	1.00	0.00
85.42	81.54	2.00	0.00	1.00	0.00	85.48	80.45	2.00	0.00	1.00	0.00
85.55	79.50	2.00	0.00	1.00	0.00	85.63	78.76	2.00	0.00	1.00	0.00
85.68	78.25	2.00	0.00	1.00	0.00	85.77	78.03	2.00	0.00	1.00	0.00
85.82	78.34	2.00	0.00	1.00	0.00	85.89	78.79	2.00	0.00	1.00	0.00
85.96	79.01	2.00	0.00	1.00	0.00	86.03	78.44	2.00	0.00	1.00	0.00
86.11	77.40	2.00	0.00	1.00	0.00	86.16	76.21	2.00	0.00	1.00	0.00
86.25	75.81	2.00	0.00	1.00	0.00	86.36	74.32	2.00	0.00	1.00	0.00
86.50	72.85	2.00	0.00	1.00	0.00	86.51	70.91	2.00	0.00	1.00	0.00
86.52	69.58	2.00	0.00	1.00	0.00	86.57	66.80	2.00	0.00	1.00	0.00
86.65	63.50	2.00	0.00	1.00	0.00	86.71	60.73	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
86.80	59.11	2.00	0.00	1.00	0.00	86.90	57.42	2.00	0.00	1.00	0.00
86.99	55.74	2.00	0.00	1.00	0.00	87.04	54.32	2.00	0.00	1.00	0.00
87.14	53.51	2.00	0.00	1.00	0.00	87.19	53.36	2.00	0.00	1.00	0.00
87.28	54.40	2.00	0.00	1.00	0.00	87.38	55.67	2.00	0.00	1.00	0.00
87.43	56.85	2.00	0.00	1.00	0.00	87.52	57.36	2.00	0.00	1.00	0.00
87.61	57.58	2.00	0.00	1.00	0.00	87.66	57.47	2.00	0.00	1.00	0.00
87.76	57.12	2.00	0.00	1.00	0.00	87.84	56.58	2.00	0.00	1.00	0.00
87.91	56.08	2.00	0.00	1.00	0.00	88.00	55.54	2.00	0.00	1.00	0.00
88.11	55.23	2.00	0.00	1.00	0.00	88.19	55.01	2.00	0.00	1.00	0.00
88.25	54.79	2.00	0.00	1.00	0.00	88.34	54.27	2.00	0.00	1.00	0.00
88.44	53.59	2.00	0.00	1.00	0.00	88.54	52.93	2.00	0.00	1.00	0.00
88.64	52.52	2.00	0.00	1.00	0.00	88.72	52.42	2.00	0.00	1.00	0.00
88.82	52.53	2.00	0.00	1.00	0.00	88.91	52.79	2.00	0.00	1.00	0.00
89.01	53.02	2.00	0.00	1.00	0.00	89.10	53.22	2.00	0.00	1.00	0.00
89.19	52.91	2.00	0.00	1.00	0.00	89.30	50.44	2.00	0.00	1.00	0.00
89.39	48.98	2.00	0.00	1.00	0.00	89.49	49.49	2.00	0.00	1.00	0.00
89.59	52.76	2.00	0.00	1.00	0.00	89.69	54.90	2.00	0.00	1.00	0.00
89.73	55.86	2.00	0.00	1.00	0.00	89.78	56.23	2.00	0.00	1.00	0.00
89.83	56.56	2.00	0.00	1.00	0.00	89.88	57.05	2.00	0.00	1.00	0.00
89.93	57.77	2.00	0.00	1.00	0.00	90.00	58.79	2.00	0.00	1.00	0.00
90.07	59.82	2.00	0.00	1.00	0.00	90.12	61.24	2.00	0.00	1.00	0.00
90.22	62.84	2.00	0.00	1.00	0.00	90.27	65.70	2.00	0.00	1.00	0.00
90.36	68.34	2.00	0.00	1.00	0.00	90.46	70.27	2.00	0.00	1.00	0.00
90.50	71.01	2.00	0.00	1.00	0.00	90.61	71.39	2.00	0.00	1.00	0.00
90.66	71.12	2.00	0.00	1.00	0.00	90.75	69.74	2.00	0.00	1.00	0.00
90.84	67.94	2.00	0.00	1.00	0.00	90.89	66.20	2.00	0.00	1.00	0.00
90.99	65.12	2.00	0.00	1.00	0.00	91.04	64.21	2.00	0.00	1.00	0.00
91.14	63.69	2.00	0.00	1.00	0.00	91.22	63.19	2.00	0.00	1.00	0.00
91.28	62.55	2.00	0.00	1.00	0.00	91.37	61.75	2.00	0.00	1.00	0.00
91.47	60.75	2.00	0.00	1.00	0.00	91.61	60.19	2.00	0.00	1.00	0.00
91.71	59.97	2.00	0.00	1.00	0.00	91.81	60.03	2.00	0.00	1.00	0.00
91.87	59.68	2.00	0.00	1.00	0.00	92.00	57.50	2.00	0.00	1.00	0.00
92.10	55.77	2.00	0.00	1.00	0.00	92.20	54.98	2.00	0.00	1.00	0.00
92.33	56.37	2.00	0.00	1.00	0.00	92.38	57.43	2.00	0.00	1.00	0.00
92.43	57.96	2.00	0.00	1.00	0.00	92.48	58.57	2.00	0.00	1.00	0.00
92.56	59.09	2.00	0.00	1.00	0.00	92.63	59.41	2.00	0.00	1.00	0.00
92.67	59.42	2.00	0.00	1.00	0.00	92.72	59.38	2.00	0.00	1.00	0.00
92.77	59.37	2.00	0.00	1.00	0.00	92.86	59.49	2.00	0.00	1.00	0.00
92.92	59.88	2.00	0.00	1.00	0.00	92.97	61.03	2.00	0.00	1.00	0.00
93.05	62.12	2.00	0.00	1.00	0.00	93.10	63.07	2.00	0.00	1.00	0.00
93.16	63.28	2.00	0.00	1.00	0.00	93.25	63.20	2.00	0.00	1.00	0.00
93.35	62.84	2.00	0.00	1.00	0.00	93.40	62.27	2.00	0.00	1.00	0.00
93.49	61.82	2.00	0.00	1.00	0.00	93.56	61.55	2.00	0.00	1.00	0.00
93.64	61.65	2.00	0.00	1.00	0.00	93.73	62.81	2.00	0.00	1.00	0.00
93.83	64.72	2.00	0.00	1.00	0.00	93.88	67.85	2.00	0.00	1.00	0.00
93.97	70.35	2.00	0.00	1.00	0.00	94.07	72.95	2.00	0.00	1.00	0.00
94.17	75.57	2.00	0.00	1.00	0.00	94.26	76.60	2.00	0.00	1.00	0.00
94.36	81.75	2.00	0.00	1.00	0.00	94.45	87.02	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)
94.55	91.74	2.00	0.00	1.00	0.00	94.64	89.52	2.00	0.00	1.00	0.00
94.72	85.22	2.00	0.00	1.00	0.00	94.74	79.85	2.00	0.00	1.00	0.00
94.77	76.98	2.00	0.00	1.00	0.00	94.85	74.39	2.00	0.00	1.00	0.00
94.90	75.17	2.00	0.00	1.00	0.00	94.95	77.89	2.00	0.00	1.00	0.00
95.01	85.22	2.00	0.00	1.00	0.00	95.09	94.37	2.00	0.00	1.00	0.00
95.14	107.02	2.00	0.00	1.00	0.00	95.23	117.34	2.00	0.00	1.00	0.00
95.29	126.89	2.00	0.00	1.00	0.00	95.38	131.69	2.00	0.00	1.00	0.00
95.43	133.43	2.00	0.00	1.00	0.00	95.52	132.50	2.00	0.00	1.00	0.00
95.57	128.95	2.00	0.00	1.00	0.00	95.67	123.49	2.00	0.00	1.00	0.00
95.77	118.72	2.00	0.00	1.00	0.00	95.86	118.80	2.00	0.00	1.00	0.00
95.95	116.56	2.00	0.00	1.00	0.00	96.03	118.40	2.00	0.00	1.00	0.00
96.11	118.64	2.00	0.00	1.00	0.00	96.20	124.65	2.00	0.00	1.00	0.00
96.30	125.73	2.00	0.00	1.00	0.00	96.39	124.50	2.00	0.00	1.00	0.00
96.50	120.31	2.00	0.00	1.00	0.00	96.59	106.72	2.00	0.00	1.00	0.00
96.69	91.36	2.00	0.00	1.00	0.00	96.78	77.51	2.00	0.00	1.00	0.00
96.87	72.98	2.00	0.00	1.00	0.00	96.98	71.40	2.00	0.00	1.00	0.00
97.02	71.90	2.00	0.00	1.00	0.00	97.06	73.47	2.00	0.00	1.00	0.00
97.12	76.16	2.00	0.00	1.00	0.00	97.16	79.48	2.00	0.00	1.00	0.00
97.21	83.99	2.00	0.00	1.00	0.00	97.27	89.17	2.00	0.00	1.00	0.00
97.33	93.67	2.00	0.00	1.00	0.00	97.40	96.33	2.00	0.00	1.00	0.00
97.45	97.51	2.00	0.00	1.00	0.00	97.50	100.38	2.00	0.00	1.00	0.00
97.58	104.78	2.00	0.00	1.00	0.00	97.65	110.26	2.00	0.00	1.00	0.00
97.69	113.95	2.00	0.00	1.00	0.00	97.74	115.68	2.00	0.00	1.00	0.00
97.81	116.42	2.00	0.00	1.00	0.00	97.88	116.63	2.00	0.00	1.00	0.00
97.93	111.98	2.00	0.00	1.00	0.00	98.03	97.35	2.00	0.00	1.00	0.00
98.15	83.50	2.00	0.00	1.00	0.00	98.21	78.05	2.00	0.00	1.00	0.00
98.32	80.19	2.00	0.00	1.00	0.00	98.42	85.96	2.00	0.00	1.00	0.00
98.47	79.73	2.00	0.00	1.00	0.00	98.57	88.75	2.00	0.00	1.00	0.00
98.70	94.00	2.00	0.00	1.00	0.00	98.78	92.13	2.00	0.00	1.00	0.00
98.85	84.79	2.00	0.00	1.00	0.00	98.86	76.77	2.00	0.00	1.00	0.00
98.92	73.26	2.00	0.00	1.00	0.00	98.98	72.24	2.00	0.00	1.00	0.00
99.03	70.12	2.00	0.00	1.00	0.00	99.11	63.67	2.00	0.00	1.00	0.00
99.18	74.69	2.00	0.00	1.00	0.00	99.23	73.25	2.00	0.00	1.00	0.00
99.32	76.01	2.00	0.00	1.00	0.00	99.37	83.05	2.00	0.00	1.00	0.00
99.45	90.04	2.00	0.00	1.00	0.00	99.56	96.01	2.00	0.00	1.00	0.00
99.64	101.90	2.00	0.00	1.00	0.00	99.71	108.77	2.00	0.00	1.00	0.00
99.75	113.72	2.00	0.00	1.00	0.00	99.90	118.27	2.00	0.00	1.00	0.00
99.95	126.55	2.00	0.00	1.00	0.00	100.04	127.45	2.00	0.00	1.00	0.00
100.14	116.89	2.00	0.00	1.00	0.00	100.14	106.43	2.00	0.00	1.00	0.00
100.15	105.52	2.00	0.00	1.00	0.00	100.19	111.71	2.00	0.00	1.00	0.00
100.21	119.29	2.00	0.00	1.00	0.00	100.24	108.37	2.00	0.00	1.00	0.00
100.28	106.62	2.00	0.00	1.00	0.00	100.31	-1.00	2.00	0.00	1.00	0.00
100.33	-1.00	2.00	0.00	1.00	0.00	100.38	-1.00	2.00	0.00	1.00	0.00
100.39	-1.00	2.00	0.00	1.00	0.00	100.43	-1.00	2.00	0.00	1.00	0.00
100.48	-1.00	2.00	0.00	1.00	0.00	100.53	-1.00	2.00	0.00	1.00	0.00
100.57	-1.00	2.00	0.00	1.00	0.00	100.60	-1.00	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)	Depth (ft)	$Q_{tn,cs}$	FS	e_v (%)	DF	Settlement (in)

Total estimated settlement: 1.40

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation (Robertson (2009) ::

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.04	0.10	0.16	54.25	8.56	4.06	18.21	3.82
0.10	0.13	0.21	54.25	11.25	4.06	10.48	2.18
0.11	0.23	0.37	54.25	19.92	4.06	9.43	3.40
0.16	0.54	0.85	54.25	46.18	4.06	6.91	5.55
0.19	1.28	2.04	26.86	54.86	3.64	5.54	10.68
0.24	2.83	4.54	12.41	56.29	3.19	4.85	19.02
0.31	4.93	7.89	7.08	55.92	2.89	0.08	0.64
0.38	6.68	10.70	5.13	54.91	2.74	0.08	0.64
0.43	7.56	12.11	4.55	55.04	2.68	0.08	0.64
0.49	7.32	11.72	4.88	57.26	2.72	0.09	0.65
0.58	6.81	10.90	5.56	60.65	2.78	0.12	0.66
0.63	6.24	9.98	6.53	65.19	2.85	0.17	0.67
0.67	6.05	9.68	7.19	69.56	2.90	0.25	0.68
0.72	6.02	9.62	7.57	72.80	2.92	0.32	0.69
0.72	6.70	10.70	7.32	78.32	2.91	0.51	0.70
0.84	9.28	14.84	5.43	80.63	2.77	0.62	0.71
0.96	15.82	25.35	2.97	75.23	2.50	0.39	0.70
1.06	22.64	36.29	2.02	73.35	2.32	0.34	0.69
1.24	27.97	44.84	1.65	74.08	2.21	0.36	0.69
1.30	31.48	50.47	1.49	75.12	2.14	0.39	0.70
1.48	37.28	59.78	1.34	80.22	2.04	0.59	0.71
1.59	42.14	67.57	1.29	87.16	1.98	0.72	0.72
1.69	47.40	76.02	1.26	95.52	1.93	0.74	0.74
1.69	49.80	79.87	1.25	99.55	1.91	0.75	0.75
1.74	53.24	85.40	1.22	104.46	1.88	0.76	0.76
1.79	53.78	86.26	1.22	105.40	1.88	0.76	0.76
1.84	52.90	84.84	1.23	104.08	1.89	0.76	0.76
1.88	51.25	82.18	1.23	101.34	1.89	0.75	0.75
1.93	49.46	79.31	1.24	98.11	1.90	0.74	0.74
1.99	48.69	78.06	1.23	96.29	1.90	0.74	0.74
2.03	48.08	77.07	1.23	94.90	1.89	0.74	0.74
2.08	47.67	76.42	1.23	93.98	1.89	0.74	0.74
2.13	46.86	75.11	1.23	92.67	1.90	0.73	0.73
2.22	45.85	73.48	1.24	91.09	1.90	0.73	0.73
2.27	44.97	72.07	1.24	89.70	1.91	0.73	0.73
2.33	44.77	71.74	1.24	89.16	1.91	0.73	0.73
2.42	45.44	72.81	1.24	89.96	1.90	0.73	0.73
2.48	46.73	74.86	1.22	91.66	1.88	0.73	0.73
2.56	48.41	77.57	1.21	94.03	1.86	0.74	0.74
2.65	49.43	79.19	1.21	95.47	1.86	0.74	0.74
2.72	48.72	78.04	1.21	94.74	1.87	0.74	0.74
2.80	46.02	73.70	1.23	90.99	1.90	0.73	0.73
2.89	42.44	67.94	1.26	85.67	1.94	0.72	0.72
2.94	39.03	62.46	1.29	80.64	1.98	0.62	0.71
3.04	35.90	57.42	1.32	76.04	2.02	0.42	0.70
3.14	32.32	51.66	1.37	70.91	2.07	0.27	0.69
3.23	29.01	46.34	1.42	65.97	2.10	0.18	0.67
3.31	25.74	41.07	1.50	61.64	2.15	0.13	0.66

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.37	23.04	36.73	1.59	58.33	2.19	0.10	0.65
3.48	20.38	32.44	1.71	55.35	2.23	0.08	0.64
3.57	18.79	29.89	1.76	52.71	2.25	0.06	0.63
3.65	18.02	28.64	1.78	50.93	2.26	0.06	0.63
3.71	18.02	28.64	1.77	50.70	2.26	0.06	0.63
3.82	18.63	29.60	1.77	52.47	2.26	0.06	0.63
3.91	20.18	32.09	1.71	54.73	2.23	0.07	0.64
4.00	22.81	36.30	1.60	58.22	2.20	0.10	0.65
4.10	26.38	42.04	1.41	59.10	2.09	0.11	0.65
4.19	31.21	49.79	1.00	49.79	1.98	0.05	0.62
4.26	37.92	60.57	1.00	60.57	1.86	0.12	0.66
4.35	45.62	72.92	1.00	72.92	1.79	0.32	0.69
4.44	49.80	79.63	1.00	79.63	1.77	0.57	0.71
4.52	51.39	82.17	1.00	82.17	1.76	0.70	0.71
4.53	52.26	83.58	1.00	83.58	1.76	0.72	0.72
4.58	55.03	88.02	1.00	88.02	1.73	0.72	0.72
4.63	57.76	92.41	1.00	92.41	1.71	0.73	0.73
4.68	58.84	94.14	1.00	94.14	1.70	0.74	0.74
4.72	59.28	94.84	1.00	94.84	1.71	0.74	0.74
4.77	59.08	94.51	1.00	94.51	1.72	0.74	0.74
4.82	58.07	92.88	1.00	92.88	1.73	0.73	0.73
4.88	56.21	89.89	1.00	89.89	1.76	0.73	0.73
4.96	53.61	85.71	1.14	97.96	1.79	0.74	0.74
5.01	50.54	80.78	1.18	95.67	1.83	0.74	0.74
5.08	47.44	75.78	1.22	92.32	1.87	0.73	0.73
5.16	44.81	71.55	1.24	88.93	1.91	0.73	0.73
5.21	43.27	69.07	1.26	86.85	1.93	0.72	0.72
5.30	42.68	68.12	1.26	86.01	1.94	0.72	0.72
5.37	42.65	68.06	1.26	85.96	1.94	0.72	0.72
5.45	42.70	68.13	1.26	86.01	1.94	0.72	0.72
5.52	42.44	67.72	1.26	85.64	1.94	0.72	0.72
5.59	41.70	66.52	1.27	84.54	1.95	0.72	0.72
5.65	40.15	64.02	1.28	82.25	1.97	0.70	0.71
5.74	38.46	61.30	1.30	79.83	1.99	0.58	0.71
5.83	37.08	59.07	1.32	77.99	2.02	0.49	0.70
5.89	36.30	57.82	1.33	77.16	2.03	0.46	0.70
5.97	35.66	56.79	1.35	76.43	2.04	0.43	0.70
6.07	34.52	54.94	1.37	75.11	2.06	0.39	0.70
6.12	32.56	51.79	1.41	73.14	2.10	0.33	0.69
6.22	29.76	47.28	1.51	71.19	2.15	0.28	0.69
6.28	26.56	42.13	1.67	70.33	2.22	0.26	0.68
6.36	23.45	37.14	1.90	70.41	2.29	0.26	0.68
6.46	21.29	33.66	2.09	70.43	2.34	0.26	0.68
6.52	20.72	32.73	2.06	67.56	2.33	0.21	0.68
6.60	22.07	34.89	1.79	62.55	2.26	0.14	0.66
6.70	23.55	37.27	1.57	58.59	2.18	0.10	0.65
6.76	23.01	36.39	1.55	56.58	2.17	0.09	0.65
6.84	19.64	30.96	1.81	55.94	2.27	0.08	0.64

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.94	14.91	23.37	2.60	60.83	2.44	0.12	0.66
7.03	10.86	16.85	4.02	67.75	2.63	0.21	0.68
7.13	8.23	12.62	5.71	72.04	2.79	0.30	0.69
7.19	6.62	10.02	6.93	69.39	2.88	0.24	0.68
7.32	5.77	8.65	6.87	59.40	2.88	0.11	0.65
7.42	5.17	7.67	5.87	44.99	2.80	0.04	0.62
7.49	4.93	7.28	4.02	29.29	2.63	0.02	0.62
7.57	4.73	-1.00	1.00	-1.00	-1.00	0.00	0.00
7.66	4.56	-1.00	1.00	-1.00	-1.00	0.00	0.00
7.76	4.44	6.47	4.48	29.00	2.68	0.02	0.62
7.77	4.39	6.39	4.95	31.63	2.72	0.02	0.62
7.78	4.42	6.44	5.05	32.53	2.73	0.02	0.62
7.82	4.44	6.47	5.36	34.69	2.76	0.02	0.62
7.87	4.45	6.49	5.86	38.07	2.80	0.03	0.62
7.92	4.45	6.49	6.45	41.83	2.85	0.03	0.62
7.97	4.49	6.54	6.96	45.53	2.88	0.04	0.62
8.01	4.59	6.70	7.41	49.66	2.91	0.05	0.62
8.06	4.76	6.97	7.58	52.81	2.92	0.06	0.63
8.11	4.93	7.24	7.65	55.42	2.93	0.08	0.64
8.20	5.06	7.45	7.68	57.24	2.93	0.09	0.65
8.26	5.16	7.60	7.84	59.63	2.94	0.11	0.66
8.35	5.23	7.70	7.98	61.50	2.95	0.13	0.66
8.40	5.30	7.81	8.02	62.65	2.95	0.14	0.66
8.49	5.37	7.91	7.96	62.99	2.95	0.14	0.66
8.54	5.51	8.13	7.81	63.54	2.94	0.15	0.67
8.64	5.71	8.45	7.58	64.06	2.93	0.16	0.67
8.69	5.91	8.77	7.37	64.63	2.91	0.16	0.67
8.79	6.18	9.19	7.46	68.57	2.92	0.23	0.68
8.84	6.48	9.68	7.59	73.49	2.93	0.34	0.69
8.93	6.89	10.32	7.50	77.37	2.92	0.47	0.70
9.03	7.13	10.69	7.46	79.83	2.92	0.58	0.71
9.08	7.21	10.83	7.52	81.47	2.92	0.66	0.71
9.11	7.16	10.75	7.78	83.66	2.94	0.72	0.72
9.12	7.13	10.69	7.89	84.32	2.95	0.72	0.72
9.17	7.07	10.60	8.03	85.13	2.95	0.72	0.72
9.22	7.12	10.67	8.09	86.32	2.96	0.72	0.72
9.31	6.92	10.34	8.56	88.56	2.99	0.73	0.73
9.36	7.16	10.72	8.37	89.76	2.98	0.73	0.73
9.40	7.46	11.20	8.04	90.10	2.95	0.73	0.73
9.46	8.14	12.28	7.25	89.07	2.90	0.73	0.73
9.51	8.47	12.82	6.92	88.75	2.88	0.73	0.73
9.55	8.78	13.30	6.70	89.10	2.86	0.73	0.73
9.61	8.98	13.63	6.65	90.65	2.86	0.73	0.73
9.69	9.12	13.84	6.73	93.09	2.87	0.73	0.73
9.74	9.18	13.94	6.87	95.71	2.88	0.74	0.74
9.81	9.39	14.26	6.85	97.70	2.88	0.74	0.74
9.89	9.76	14.85	6.62	98.33	2.86	0.74	0.74
9.94	10.06	15.33	6.42	98.43	2.84	0.75	0.75

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.03	10.23	15.59	6.28	97.94	2.83	0.74	0.74
10.08	10.23	15.59	5.91	92.18	2.80	0.73	0.73
10.18	10.23	15.58	5.40	84.12	2.76	0.72	0.72
10.23	10.23	15.58	5.05	78.62	2.73	0.52	0.70
10.33	10.23	15.57	5.17	80.55	2.74	0.61	0.71
10.40	10.23	15.56	5.54	86.20	2.77	0.72	0.72
10.47	10.08	15.32	5.91	90.44	2.80	0.73	0.73
10.51	10.06	15.28	6.18	94.42	2.83	0.74	0.74
10.56	10.03	15.23	6.41	97.63	2.84	0.74	0.74
10.61	10.21	15.52	6.51	100.97	2.85	0.75	0.75
10.67	10.16	15.43	6.88	106.14	2.88	0.76	0.76
10.75	10.13	15.37	7.21	110.80	2.90	0.77	0.77
10.80	9.99	15.15	7.50	113.70	2.92	0.77	0.77
10.85	9.89	14.99	7.63	114.35	2.93	0.77	0.77
10.90	9.72	14.71	7.82	115.05	2.94	0.77	0.77
11.00	9.45	14.27	8.13	116.05	2.96	0.78	0.78
11.05	9.05	13.61	8.55	116.32	2.99	0.78	0.78
11.14	8.61	12.90	9.04	116.64	3.01	0.62	0.99
11.21	8.27	12.36	9.53	117.80	3.04	0.62	0.94
11.29	8.24	12.30	9.66	118.79	3.05	0.65	0.93
11.38	8.41	12.56	9.53	119.67	3.04	0.63	0.94
11.46	8.68	12.98	9.18	119.19	3.02	0.64	0.97
11.52	8.88	13.30	8.96	119.26	3.01	0.64	0.98
11.60	8.98	13.46	8.85	119.12	3.00	0.64	0.99
11.67	9.05	13.56	8.79	119.24	3.00	0.64	0.99
11.72	9.12	13.67	8.75	119.52	3.00	0.78	0.78
11.81	9.32	13.98	8.54	119.37	2.99	0.78	0.78
11.86	9.35	14.03	8.52	119.54	2.98	0.78	0.78
11.96	9.42	14.07	8.48	119.37	2.98	0.78	0.78
12.01	9.45	14.06	8.50	119.58	2.98	0.78	0.78
12.10	9.69	13.55	8.25	111.75	2.97	0.77	0.77
12.16	10.07	13.97	7.41	103.51	2.91	0.75	0.75
12.24	10.47	14.38	6.85	98.49	2.88	0.75	0.75
12.32	10.87	14.89	6.86	102.09	2.88	0.75	0.75
12.39	11.18	15.29	7.16	109.53	2.90	0.77	0.77
12.48	10.64	14.47	7.97	115.36	2.95	0.78	0.78
12.50	10.23	14.64	8.30	121.50	2.97	0.79	0.79
12.54	10.74	14.58	8.20	119.55	2.96	0.78	0.78
12.64	12.36	16.65	7.01	116.68	2.89	0.78	0.78
12.68	14.04	18.79	6.01	113.05	2.81	0.77	0.77
12.77	14.72	19.54	5.64	110.30	2.78	0.77	0.77
12.82	14.75	19.48	5.55	108.15	2.78	0.76	0.76
12.89	14.21	18.67	5.71	106.60	2.79	0.76	0.76
12.97	13.37	17.49	6.13	107.25	2.82	0.76	0.76
13.03	12.49	16.30	6.66	108.51	2.86	0.76	0.76
13.12	11.72	15.20	7.22	109.85	2.90	0.77	0.77
13.16	11.21	14.50	7.58	109.96	2.93	0.77	0.77
13.26	10.91	13.99	7.68	107.43	2.93	0.76	0.76

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.34	10.84	13.79	7.45	102.72	2.92	0.75	0.75
13.41	10.74	13.56	7.18	97.27	2.90	0.74	0.74
13.50	10.60	13.27	7.10	94.19	2.89	0.74	0.74
13.60	10.33	12.84	7.26	93.25	2.90	0.74	0.74
13.65	10.13	12.55	7.49	94.05	2.92	0.74	0.74
13.75	10.03	12.35	7.71	95.17	2.93	0.74	0.74
13.80	10.10	12.37	7.57	93.67	2.92	0.74	0.74
13.89	10.23	12.47	7.55	94.18	2.92	0.74	0.74
13.94	10.63	12.95	7.46	96.59	2.92	0.74	0.74
14.03	10.80	13.13	7.91	103.87	2.95	0.76	0.76
14.11	11.23	13.59	7.98	108.45	2.95	0.76	0.76
14.13	11.53	13.97	7.99	111.61	2.95	0.77	0.77
14.18	12.27	14.85	7.55	112.19	2.92	0.77	0.77
14.22	12.83	15.50	7.35	113.98	2.91	0.77	0.77
14.28	13.44	16.19	7.18	116.20	2.90	0.78	0.78
14.37	14.01	16.81	7.06	118.62	2.89	0.78	0.78
14.44	14.79	17.68	6.80	120.24	2.87	0.78	0.78
14.51	15.63	18.60	6.50	120.95	2.85	0.78	0.78
14.60	16.31	19.30	6.30	121.55	2.83	0.79	0.79
14.65	16.58	19.57	6.28	122.89	2.83	0.79	0.79
14.75	16.56	19.44	6.39	124.23	2.84	0.79	0.79
14.85	16.48	19.22	6.50	124.95	2.85	0.79	0.79
14.91	16.44	19.11	6.54	124.89	2.85	0.79	0.79
14.99	17.00	19.64	6.25	122.73	2.83	0.79	0.79
15.09	18.30	21.01	5.69	119.59	2.79	0.78	0.78
15.18	20.29	23.13	4.94	114.33	2.72	0.77	0.77
15.25	22.28	25.25	4.26	107.53	2.66	0.76	0.76
15.33	24.50	27.58	3.60	99.22	2.58	0.75	0.75
15.43	27.51	30.70	2.96	90.92	2.50	0.73	0.73
15.51	31.32	34.70	2.45	84.95	2.41	0.72	0.72
15.59	34.63	38.13	2.14	81.77	2.35	0.68	0.71
15.67	36.18	39.65	2.03	80.65	2.33	0.62	0.71
15.76	35.13	38.36	2.14	81.98	2.35	0.69	0.71
15.86	32.03	34.86	2.45	85.36	2.41	0.72	0.72
15.95	27.64	30.01	3.03	90.95	2.51	0.73	0.73
16.05	23.08	24.94	3.85	95.91	2.61	0.74	0.74
16.14	19.31	20.73	4.79	99.32	2.71	0.75	0.75
16.20	16.85	17.98	5.55	99.84	2.78	0.75	0.75
16.28	15.33	16.24	6.13	99.52	2.82	0.75	0.75
16.34	14.21	14.97	6.52	97.62	2.85	0.74	0.74
16.44	12.93	13.48	7.12	95.96	2.89	0.74	0.74
16.50	11.61	12.00	7.73	92.73	2.93	0.73	0.73
16.58	10.17	10.54	8.19	86.31	2.96	0.72	0.72
16.73	8.75	8.85	8.43	74.57	2.98	0.37	0.69
16.82	7.60	7.51	8.14	61.14	2.96	0.12	0.66
16.92	7.06	6.86	8.35	57.29	2.97	0.09	0.65
17.01	6.56	6.26	10.33	64.67	3.09	0.13	0.45
17.11	6.20	5.84	12.54	73.17	3.19	0.19	0.42

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
17.12	5.73	5.31	14.74	78.30	3.28	0.20	0.38
17.14	6.34	5.97	13.44	80.31	3.23	0.21	0.43
17.19	7.13	6.82	12.15	82.92	3.17	0.24	0.49
17.28	7.94	7.67	11.16	85.58	3.13	0.27	0.55
17.33	8.01	7.71	11.48	88.52	3.14	0.29	0.55
17.43	7.87	7.52	11.93	89.67	3.16	0.30	0.54
17.47	7.74	7.35	12.03	88.37	3.17	0.29	0.52
17.57	7.57	7.12	11.95	85.14	3.16	0.25	0.51
17.65	7.47	6.98	11.70	81.63	3.15	0.23	0.50
17.72	7.40	6.88	11.84	81.46	3.16	0.22	0.49
17.81	7.57	7.02	11.86	83.22	3.16	0.25	0.50
17.86	7.87	7.32	11.98	87.65	3.17	0.27	0.52
17.95	8.31	7.73	11.95	92.32	3.16	0.32	0.55
18.05	8.78	8.18	11.81	96.52	3.16	0.36	0.58
18.10	9.22	8.61	11.67	100.43	3.15	0.38	0.61
18.20	9.66	9.01	11.52	103.80	3.14	0.42	0.64
18.30	9.90	9.20	11.60	106.76	3.15	0.46	0.66
18.39	10.13	9.38	11.50	107.91	3.14	0.46	0.67
18.48	10.27	9.47	11.38	107.71	3.14	0.46	0.68
18.58	10.30	9.44	11.38	107.46	3.14	0.46	0.67
18.66	10.20	9.30	11.49	106.87	3.14	0.45	0.66
18.74	10.07	9.12	11.49	104.74	3.14	0.44	0.65
18.87	9.90	8.88	10.73	95.26	3.11	0.39	0.63
18.97	9.66	8.59	10.09	86.69	3.07	0.22	0.61
19.06	9.56	8.45	9.58	80.90	3.05	0.24	0.60
19.16	9.83	8.66	9.84	85.25	3.06	0.27	0.62
19.25	10.13	8.91	9.93	88.50	3.06	0.31	0.64
19.27	10.23	9.00	10.18	91.69	3.08	0.31	0.64
19.30	10.37	9.12	10.39	94.70	3.09	0.34	0.65
19.34	10.57	9.29	10.57	98.19	3.10	0.38	0.66
19.39	10.84	9.53	10.50	100.00	3.09	0.40	0.68
19.49	10.78	9.41	10.57	99.51	3.10	0.39	0.67
19.55	10.51	9.12	10.70	97.54	3.10	0.37	0.65
19.63	10.17	8.75	10.86	95.04	3.11	0.34	0.63
19.68	9.87	8.43	10.91	92.04	3.11	0.32	0.60
19.74	9.77	8.31	10.69	88.83	3.10	0.29	0.59
19.83	9.73	8.24	10.61	87.40	3.10	0.27	0.59
19.87	9.73	8.22	10.55	86.67	3.10	0.29	0.59
19.94	9.73	8.19	10.80	88.39	3.11	0.27	0.58
20.02	9.80	8.21	11.04	90.64	3.12	0.31	0.59
20.07	10.17	8.54	11.28	96.33	3.13	0.34	0.61
20.17	11.42	9.65	10.38	100.21	3.09	0.41	0.69
20.21	14.18	12.20	8.30	101.25	2.97	0.75	0.75
20.28	18.74	16.43	5.92	97.16	2.80	0.74	0.74
20.36	24.88	22.08	4.11	90.84	2.64	0.73	0.73
20.41	31.73	28.40	3.02	85.89	2.51	0.72	0.72
20.48	38.64	34.74	2.39	83.15	2.40	0.71	0.71
20.55	44.99	40.52	2.02	82.00	2.33	0.69	0.71

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
20.60	49.88	44.99	1.82	81.90	2.27	0.68	0.71
20.70	52.55	47.28	1.74	82.23	2.25	0.70	0.71
20.74	52.68	47.32	1.75	82.97	2.25	0.71	0.71
20.79	51.17	45.83	1.84	84.31	2.28	0.72	0.72
20.89	48.70	43.39	2.03	87.95	2.33	0.72	0.72
20.96	46.86	41.58	2.06	85.66	2.33	0.72	0.72
21.04	45.83	40.52	2.09	84.84	2.34	0.72	0.72
21.13	45.80	40.36	2.05	82.71	2.33	0.71	0.71
21.22	49.22	43.31	1.97	85.52	2.31	0.72	0.72
21.29	52.71	46.38	1.86	86.23	2.28	0.72	0.72
21.35	62.13	54.84	1.58	86.56	2.19	0.72	0.72
21.37	71.37	63.21	1.42	89.97	2.10	0.73	0.73
21.42	83.72	74.37	1.31	97.64	2.01	0.74	0.74
21.47	92.73	82.47	1.27	104.48	1.95	0.76	0.76
21.48	100.66	89.69	1.23	110.65	1.90	0.77	0.77
21.52	107.37	95.73	1.20	115.32	1.85	0.78	0.78
21.57	113.24	100.98	1.17	118.63	1.82	0.78	0.78
21.62	118.81	105.91	1.14	120.85	1.79	0.78	0.78
21.66	124.00	110.52	1.10	122.11	1.76	0.79	0.79
21.71	128.79	114.75	1.07	122.79	1.74	0.79	0.79
21.76	132.64	118.10	1.04	123.42	1.73	0.79	0.79
21.81	135.34	120.38	1.03	124.51	1.72	0.79	0.79
21.85	136.99	121.70	1.04	126.15	1.72	0.79	0.79
21.91	137.80	122.24	1.05	127.87	1.73	0.80	0.80
21.95	138.11	122.32	1.06	129.40	1.73	0.80	0.80
22.00	138.24	122.26	1.07	130.49	1.74	0.80	0.80
22.05	138.18	122.02	1.08	131.33	1.75	0.80	0.80
22.10	138.24	121.90	1.08	132.00	1.75	0.80	0.80
22.15	138.31	121.77	1.09	132.56	1.75	0.80	0.80
22.19	138.68	121.94	1.09	133.12	1.75	0.80	0.80
22.24	139.25	122.24	1.11	135.35	1.76	0.81	0.81
22.29	139.86	122.58	1.11	136.60	1.77	0.81	0.81
22.34	140.20	122.70	1.12	137.16	1.77	0.81	0.81
22.39	140.06	122.45	1.11	135.89	1.77	0.81	0.81
22.43	139.42	121.72	1.11	135.26	1.77	0.81	0.81
22.48	138.34	120.56	1.12	135.08	1.77	0.81	0.81
22.55	136.79	118.95	1.13	134.76	1.78	0.81	0.81
22.62	130.08	112.68	1.17	131.90	1.82	0.80	0.80
22.63	127.95	110.75	1.18	130.57	1.83	0.80	0.80
22.72	125.56	108.31	1.19	128.61	1.83	0.80	0.80
22.77	128.09	110.46	1.17	129.57	1.82	0.80	0.80
22.83	126.13	108.51	1.19	128.59	1.83	0.80	0.80
22.91	124.21	106.52	1.20	127.55	1.85	0.79	0.79
22.96	121.74	104.15	1.21	126.09	1.86	0.79	0.79
23.02	118.20	100.84	1.22	123.45	1.88	0.79	0.79
23.10	113.85	96.74	1.24	119.96	1.90	0.78	0.78
23.16	108.42	91.79	1.26	115.60	1.93	0.78	0.78
23.20	102.21	86.20	1.28	110.62	1.97	0.77	0.77

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
23.26	95.46	80.15	1.31	105.23	2.01	0.76	0.76
23.35	88.68	74.00	1.36	100.36	2.05	0.75	0.75
23.39	81.66	67.80	1.42	95.97	2.10	0.74	0.74
23.48	74.68	61.55	1.51	93.11	2.15	0.73	0.73
23.54	68.33	55.99	1.61	90.41	2.20	0.73	0.73
23.63	63.44	51.67	1.69	87.24	2.23	0.72	0.72
23.69	60.07	48.84	1.63	79.68	2.21	0.57	0.71
23.78	58.37	47.34	1.59	75.09	2.19	0.39	0.70
23.87	57.71	46.70	1.56	72.76	2.18	0.32	0.69
23.88	57.81	46.69	1.62	75.51	2.20	0.40	0.70
23.93	57.42	46.23	1.69	78.05	2.23	0.50	0.70
24.02	57.22	45.85	1.76	80.73	2.25	0.62	0.71
24.04	56.97	45.57	1.82	82.98	2.27	0.71	0.71
24.05	57.34	45.82	1.85	84.83	2.28	0.72	0.72
24.15	58.27	46.42	1.87	86.71	2.28	0.72	0.72
24.20	60.11	47.86	1.85	88.32	2.28	0.73	0.73
24.30	62.64	49.86	1.75	87.06	2.25	0.72	0.72
24.40	65.07	51.83	1.63	84.41	2.21	0.72	0.72
24.46	66.59	53.10	1.53	81.44	2.16	0.66	0.71
24.54	66.42	52.90	1.50	79.49	2.15	0.56	0.71
24.64	64.09	50.78	1.55	78.59	2.17	0.52	0.70
24.73	59.94	47.12	1.68	79.13	2.22	0.54	0.71
24.78	54.64	42.55	1.92	81.62	2.30	0.67	0.71
24.88	48.57	37.36	2.28	85.25	2.38	0.72	0.72
24.94	41.92	31.81	2.80	89.16	2.47	0.73	0.73
25.02	35.00	26.12	3.52	92.04	2.57	0.73	0.73
25.12	28.43	20.76	4.59	95.35	2.69	0.74	0.74
25.17	22.86	16.30	6.02	98.17	2.81	0.74	0.74
25.27	18.41	12.75	7.69	98.13	2.93	0.74	0.74
25.36	15.13	9.96	9.50	94.69	3.04	0.34	0.71
25.43	12.60	8.11	11.16	90.44	3.13	0.30	0.58
25.50	10.88	6.84	12.76	87.31	3.20	0.27	0.49
25.60	9.77	6.01	14.03	84.31	3.25	0.24	0.43
25.64	9.26	5.64	14.52	81.86	3.27	0.23	0.40
25.67	9.06	5.48	14.58	79.98	3.28	0.22	0.39
25.71	8.86	5.33	14.38	76.65	3.27	0.20	0.38
25.79	8.52	5.07	14.25	72.22	3.26	0.16	0.36
25.93	8.18	4.80	14.17	68.01	3.26	0.14	0.34
26.03	8.02	4.66	13.97	65.11	3.25	0.13	0.33
26.13	8.02	4.64	13.74	63.74	3.24	0.11	0.33
26.24	8.08	4.67	13.54	63.18	3.23	0.12	0.33
26.37	8.18	4.71	13.48	63.49	3.23	0.12	0.34
26.47	8.25	4.73	13.53	64.09	3.23	0.12	0.34
26.60	8.25	4.71	13.24	62.33	3.22	0.12	0.34
26.71	8.38	4.78	12.59	60.15	3.19	0.09	0.34
26.85	8.75	5.00	11.78	58.94	3.16	0.09	0.36
26.95	8.96	5.12	12.24	62.69	3.18	0.11	0.37
27.04	9.60	5.54	12.21	67.66	3.18	0.15	0.40

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
27.09	10.14	5.90	12.33	72.68	3.18	0.17	0.42
27.19	10.95	6.42	11.76	75.49	3.16	0.20	0.46
27.23	11.18	6.56	11.88	78.01	3.16	0.21	0.47
27.33	11.42	6.70	11.98	80.22	3.17	0.22	0.48
27.40	11.76	6.91	11.94	82.48	3.16	0.24	0.49
27.47	12.30	7.25	11.72	84.94	3.15	0.25	0.52
27.57	12.97	7.66	11.34	86.93	3.14	0.28	0.55
27.66	13.85	8.22	10.99	90.36	3.12	0.30	0.59
27.77	14.96	8.93	10.64	94.93	3.10	0.34	0.64
27.86	16.28	9.76	10.29	100.42	3.08	0.40	0.70
27.96	17.39	10.45	10.06	105.14	3.07	0.45	0.75
28.06	17.73	10.63	10.22	108.70	3.08	0.49	0.76
28.15	17.29	10.31	10.64	109.63	3.10	0.50	0.74
28.25	17.04	10.10	10.32	104.18	3.08	0.47	0.72
28.34	16.50	9.71	10.12	98.29	3.07	0.34	0.69
28.44	16.94	9.96	9.46	94.21	3.04	0.34	0.71
28.54	16.11	9.38	10.45	98.03	3.09	0.38	0.67
28.62	17.46	10.22	9.90	101.19	3.06	0.41	0.73
28.71	18.34	10.74	9.72	104.45	3.05	0.45	0.77
28.77	20.26	11.95	8.92	106.63	3.01	0.48	0.85
28.86	20.73	12.21	8.93	109.00	3.01	0.51	0.87
28.91	21.34	12.56	8.78	110.37	3.00	0.52	0.90
28.97	22.04	12.99	8.63	112.06	2.99	0.77	0.77
29.04	22.92	13.50	8.45	114.13	2.98	0.77	0.77
29.10	23.97	14.13	8.26	116.69	2.97	0.78	0.78
29.15	25.15	14.85	8.08	120.01	2.96	0.78	0.78
29.25	26.40	16.30	7.69	125.36	2.93	0.79	0.79
29.34	27.38	16.91	7.60	128.48	2.93	0.80	0.80
29.38	27.75	17.12	7.63	130.55	2.93	0.80	0.80
29.48	27.72	16.25	7.97	129.55	2.95	0.80	0.80
29.55	27.48	16.06	8.07	129.61	2.96	0.80	0.80
29.63	27.41	16.75	7.61	127.50	2.93	0.79	0.79
29.72	28.43	17.61	6.01	105.80	2.81	0.76	0.76
29.82	31.56	20.09	3.98	79.94	2.63	0.58	0.71
29.88	36.83	24.31	2.33	56.65	2.39	0.09	0.65
29.96	45.23	30.47	1.87	56.98	2.29	0.09	0.65
30.06	49.92	33.83	1.75	59.16	2.25	0.11	0.65
30.13	54.67	37.29	1.64	60.99	2.21	0.12	0.66
30.18	56.02	38.21	1.63	62.30	2.21	0.14	0.66
30.28	58.72	40.06	1.61	64.44	2.20	0.16	0.67
30.37	59.53	40.40	1.67	67.53	2.22	0.21	0.68
30.47	60.51	40.85	1.74	71.05	2.25	0.28	0.69
30.57	63.28	42.69	1.73	73.87	2.24	0.35	0.69
30.66	67.26	45.46	1.67	76.12	2.22	0.42	0.70
30.74	71.34	48.33	1.62	78.31	2.20	0.51	0.70
30.82	74.51	50.51	1.59	80.52	2.19	0.61	0.71
30.90	76.30	51.60	1.61	82.93	2.20	0.71	0.71
31.01	76.90	51.74	1.66	85.67	2.22	0.72	0.72

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
31.10	77.02	51.51	1.74	89.47	2.24	0.73	0.73
31.19	77.06	51.19	1.84	93.96	2.28	0.74	0.74
31.28	77.57	51.24	1.92	98.21	2.30	0.74	0.74
31.35	78.53	51.70	1.97	101.82	2.31	0.75	0.75
31.43	80.52	52.90	1.98	104.59	2.31	0.76	0.76
31.53	83.11	54.53	1.97	107.28	2.31	0.76	0.76
31.60	85.91	56.74	1.78	101.10	2.26	0.75	0.75
31.67	88.07	58.52	1.64	95.74	2.21	0.74	0.74
31.77	89.46	59.74	1.53	91.18	2.16	0.73	0.73
31.84	89.86	59.77	1.56	93.40	2.18	0.74	0.74
31.91	86.18	56.78	1.68	95.19	2.22	0.74	0.74
31.98	79.10	51.41	1.89	97.23	2.29	0.74	0.74
31.98	77.21	49.95	1.99	99.23	2.32	0.75	0.75
32.04	78.73	50.91	1.98	100.65	2.31	0.75	0.75
32.12	82.68	53.56	1.91	102.19	2.30	0.75	0.75
32.16	80.04	51.46	2.05	105.63	2.33	0.76	0.76
32.27	75.66	48.11	2.26	108.77	2.38	0.76	0.76
32.33	70.76	44.53	2.50	111.51	2.42	0.77	0.77
32.41	66.31	41.33	2.72	112.40	2.46	0.77	0.77
32.50	61.79	38.14	2.93	111.66	2.49	0.77	0.77
32.58	56.66	34.61	3.18	110.12	2.53	0.77	0.77
32.66	50.22	30.23	3.59	108.68	2.58	0.76	0.76
32.74	43.30	25.56	4.22	107.79	2.65	0.76	0.76
32.84	36.12	20.76	5.20	107.96	2.75	0.76	0.76
32.90	29.88	16.68	6.45	107.62	2.85	0.76	0.76
32.98	24.92	12.71	8.19	104.08	2.96	0.76	0.76
33.08	20.77	10.40	9.80	101.84	3.06	0.43	0.74
33.14	17.05	8.34	11.93	99.50	3.16	0.40	0.60
33.22	14.12	6.71	14.31	96.06	3.27	0.36	0.48
33.32	12.19	5.64	16.21	91.43	3.34	0.30	0.40
33.37	11.28	5.14	16.60	85.28	3.35	0.27	0.37
33.47	11.05	4.99	16.37	81.70	3.34	0.22	0.36
33.56	11.66	5.30	15.06	79.85	3.30	0.23	0.38
33.63	12.43	5.71	14.04	80.15	3.26	0.23	0.41
33.71	12.67	5.82	13.47	78.37	3.23	0.23	0.42
33.81	11.99	5.44	13.27	72.19	3.22	0.19	0.39
33.90	11.05	4.92	13.35	65.65	3.23	0.11	0.35
33.95	10.31	4.51	13.36	60.28	3.23	0.11	0.32
34.04	10.07	4.37	13.69	59.84	3.24	0.11	0.31
34.14	9.87	4.25	14.01	59.54	3.25	0.10	0.30
34.17	9.81	4.21	14.16	59.63	3.26	0.11	0.30
34.20	10.07	4.35	13.78	59.92	3.24	0.11	0.31
34.26	10.38	4.50	13.36	60.14	3.23	0.11	0.32
34.35	10.61	4.61	12.99	59.91	3.21	0.11	0.33
34.43	10.41	4.49	13.24	59.45	3.22	0.11	0.32
34.49	10.27	4.41	13.28	58.59	3.22	0.10	0.32
34.59	10.17	4.34	13.18	57.25	3.22	0.10	0.31
34.69	10.07	4.28	13.07	55.91	3.21	0.09	0.31

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
34.73	9.90	4.18	13.12	54.88	3.22	0.08	0.30
34.83	9.80	4.12	13.19	54.34	3.22	0.08	0.29
34.90	9.74	4.07	13.37	54.48	3.23	0.08	0.29
34.98	9.84	4.12	13.48	55.47	3.23	0.09	0.29
35.07	10.14	4.26	13.68	58.28	3.24	0.10	0.30
35.16	10.58	4.47	14.49	64.79	3.27	0.12	0.32
35.26	11.29	4.82	15.85	76.48	3.32	0.19	0.34
35.33	13.25	5.82	15.42	89.71	3.31	0.31	0.42
35.40	16.76	7.61	13.28	101.03	3.22	0.42	0.54
35.50	20.84	9.67	11.03	106.70	3.12	0.52	0.69
35.57	23.37	10.95	10.02	109.72	3.07	0.54	0.78
35.65	23.77	11.12	10.10	112.36	3.07	0.57	0.79
35.71	22.86	10.64	10.83	115.22	3.11	0.61	0.76
35.79	21.65	9.99	11.64	116.27	3.15	0.61	0.71
35.85	20.37	9.32	12.22	113.90	3.18	0.57	0.67
35.94	19.29	8.75	12.53	109.71	3.19	0.51	0.63
35.99	18.31	8.24	12.58	103.66	3.19	0.46	0.59
36.08	17.16	7.64	12.55	95.94	3.19	0.38	0.55
36.17	15.54	6.80	12.98	88.35	3.21	0.28	0.49
36.24	14.22	6.13	13.50	82.76	3.23	0.26	0.44
36.33	13.58	5.79	14.00	81.11	3.25	0.24	0.41
36.42	13.58	5.77	14.22	82.08	3.26	0.24	0.41
36.52	14.05	5.99	12.88	77.16	3.21	0.28	0.43
36.61	15.40	6.64	11.27	74.88	3.13	0.14	0.47
36.70	17.73	7.78	9.87	76.79	3.06	0.21	0.56
36.78	20.23	8.99	9.83	88.43	3.06	0.34	0.64
36.85	18.24	7.99	12.41	99.18	3.19	0.44	0.57
36.87	20.20	8.95	11.61	103.88	3.15	0.46	0.64
36.91	23.23	10.43	10.08	105.17	3.07	0.51	0.75
36.97	31.40	15.73	6.66	104.77	2.86	0.76	0.76
37.06	35.24	17.97	5.86	105.20	2.80	0.76	0.76
37.12	38.62	19.91	5.42	107.91	2.76	0.76	0.76
37.20	42.40	22.04	5.10	112.33	2.74	0.77	0.77
37.27	47.56	25.06	4.56	114.30	2.69	0.77	0.77
37.35	52.21	27.88	4.03	112.42	2.63	0.77	0.77
37.44	55.22	29.75	3.64	108.21	2.59	0.76	0.76
37.49	58.42	31.83	3.23	102.76	2.53	0.75	0.75
37.59	67.19	37.46	2.56	95.81	2.43	0.74	0.74
37.64	85.65	49.64	1.82	90.11	2.27	0.73	0.73
37.70	111.29	67.10	1.41	94.79	2.10	0.74	0.74
37.78	136.59	84.81	1.28	108.37	1.96	0.76	0.76
37.83	155.69	98.45	1.22	120.19	1.88	0.78	0.78
37.92	167.53	106.83	1.19	126.68	1.83	0.79	0.79
37.97	174.58	111.69	1.17	130.53	1.81	0.80	0.80
38.07	178.80	114.34	1.16	133.13	1.81	0.80	0.80
38.14	181.84	116.07	1.17	135.64	1.81	0.81	0.81
38.22	185.72	118.33	1.17	138.68	1.82	0.81	0.81
38.31	191.72	121.94	1.17	143.23	1.82	0.82	0.82

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
38.41	201.37	128.37	1.16	148.66	1.80	0.83	0.83
38.52	212.64	135.94	1.14	154.32	1.79	0.83	0.83
38.64	221.04	141.59	1.11	157.41	1.77	0.84	0.84
38.74	217.87	138.67	1.14	158.10	1.79	0.84	0.84
38.80	214.19	135.62	1.16	157.57	1.81	0.84	0.84
38.89	210.42	132.43	1.18	156.57	1.83	0.84	0.84
38.94	213.65	134.37	1.18	158.84	1.83	0.84	0.84
39.03	213.59	133.74	1.19	159.69	1.84	0.84	0.84
39.13	213.25	132.81	1.21	160.46	1.86	0.84	0.84
39.23	211.36	130.76	1.22	160.12	1.88	0.84	0.84
39.35	207.85	127.69	1.24	158.27	1.90	0.84	0.84
39.42	201.04	122.59	1.26	154.08	1.93	0.83	0.83
39.51	192.09	116.15	1.28	148.22	1.96	0.82	0.82
39.60	181.50	108.71	1.30	141.37	1.99	0.82	0.82
39.70	172.83	102.65	1.32	135.85	2.02	0.81	0.81
39.78	164.63	97.07	1.35	130.75	2.04	0.80	0.80
39.90	157.35	92.05	1.37	126.28	2.06	0.79	0.79
39.99	149.05	86.44	1.41	121.65	2.09	0.79	0.79
40.09	141.42	81.31	1.45	117.75	2.12	0.78	0.78
40.18	133.79	76.23	1.50	114.33	2.15	0.77	0.77
40.23	126.04	71.16	1.56	111.30	2.18	0.77	0.77
40.33	118.01	65.88	1.65	108.90	2.22	0.76	0.76
40.43	110.12	60.74	1.76	107.17	2.25	0.76	0.76
40.52	101.85	55.31	1.95	107.68	2.31	0.76	0.76
40.61	92.44	49.44	2.15	106.53	2.36	0.76	0.76
40.69	80.59	42.14	2.54	106.96	2.43	0.76	0.76
40.80	68.65	35.01	3.03	106.21	2.51	0.76	0.76
40.87	59.91	29.84	3.59	107.20	2.58	0.76	0.76
40.95	53.47	26.09	4.12	107.50	2.64	0.76	0.76
40.97	51.37	24.94	4.24	105.79	2.65	0.76	0.76
41.01	54.31	26.70	3.81	101.77	2.61	0.75	0.75
41.07	61.80	31.20	3.04	94.92	2.51	0.74	0.74
41.15	67.40	34.61	2.61	90.47	2.44	0.73	0.73
41.26	67.13	34.39	2.61	89.74	2.44	0.73	0.73
41.35	63.05	31.86	2.87	91.40	2.48	0.73	0.73
41.47	60.28	30.09	3.10	93.27	2.52	0.74	0.74
41.59	59.67	29.62	3.18	94.19	2.53	0.74	0.74
41.69	60.42	29.94	3.18	95.29	2.53	0.74	0.74
41.78	59.17	29.08	3.36	97.63	2.55	0.74	0.74
41.88	54.75	26.41	3.82	100.94	2.61	0.75	0.75
41.98	49.45	23.32	4.43	103.21	2.67	0.75	0.75
42.08	45.13	20.88	4.96	103.54	2.72	0.75	0.75
42.16	44.32	20.43	4.99	102.01	2.73	0.75	0.75
42.24	47.12	21.98	4.53	99.69	2.68	0.75	0.75
42.31	52.25	24.86	3.91	97.23	2.62	0.74	0.74
42.45	56.94	27.44	3.48	95.61	2.57	0.74	0.74
42.55	59.37	28.78	3.30	94.91	2.54	0.74	0.74
42.60	59.78	28.96	3.29	95.14	2.54	0.74	0.74

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
42.70	59.34	28.59	3.38	96.60	2.55	0.74	0.74
42.81	57.38	27.33	3.64	99.43	2.59	0.75	0.75
42.89	53.57	25.06	4.12	103.15	2.64	0.75	0.75
42.98	48.27	22.02	4.84	106.61	2.71	0.76	0.76
43.08	43.14	19.16	5.69	108.99	2.79	0.76	0.76
43.17	40.44	17.68	6.18	109.35	2.83	0.76	0.76
43.27	41.05	18.01	5.94	107.03	2.81	0.76	0.76
43.37	43.81	19.71	4.84	95.48	2.71	0.74	0.74
43.50	46.82	21.62	3.86	83.44	2.61	0.71	0.71
43.61	48.54	22.85	3.24	73.95	2.54	0.35	0.69
43.74	49.31	23.16	3.25	75.29	2.54	0.39	0.70
43.79	49.31	22.99	3.44	79.06	2.56	0.54	0.71
43.86	48.47	22.31	3.79	84.59	2.60	0.72	0.72
43.94	47.05	21.30	4.28	91.16	2.66	0.73	0.73
44.00	44.89	19.92	4.92	98.08	2.72	0.74	0.74
44.08	42.33	18.39	5.62	103.37	2.78	0.75	0.75
44.17	38.85	16.48	6.45	106.26	2.85	0.76	0.76
44.27	35.44	14.71	7.14	105.00	2.90	0.76	0.76
44.42	34.16	14.09	7.15	100.72	2.90	0.75	0.75
44.52	37.10	15.69	6.06	95.03	2.82	0.74	0.74
44.61	44.15	19.52	4.49	87.72	2.68	0.72	0.72
44.71	51.91	23.77	3.51	83.46	2.57	0.71	0.71
44.85	56.66	26.27	3.19	83.87	2.53	0.72	0.72
44.95	57.30	26.40	3.34	88.11	2.55	0.72	0.72
45.09	54.98	24.92	3.69	92.06	2.59	0.73	0.73
45.19	50.09	22.17	4.29	95.00	2.66	0.74	0.74
45.33	43.44	18.53	5.31	98.48	2.76	0.75	0.75
45.42	37.17	15.25	6.56	100.02	2.85	0.75	0.75
45.57	34.20	13.74	7.18	98.64	2.90	0.75	0.75
45.68	32.58	12.98	7.29	94.66	2.91	0.74	0.74
45.81	30.45	12.02	7.30	87.72	2.91	0.72	0.72
45.92	26.54	9.26	8.96	82.93	3.01	0.26	0.66
46.05	22.29	7.59	10.87	82.51	3.11	0.33	0.54
46.16	19.32	6.43	13.40	86.12	3.23	0.32	0.46
46.17	17.73	5.82	14.71	85.57	3.28	0.32	0.42
46.23	17.46	5.70	14.75	84.09	3.28	0.30	0.41
46.29	16.85	5.46	15.02	82.02	3.29	0.28	0.39
46.34	16.04	5.15	15.32	78.81	3.31	0.26	0.37
46.42	15.30	4.85	15.44	74.90	3.31	0.22	0.35
46.48	14.90	4.69	15.10	70.80	3.30	0.19	0.34
46.52	14.69	4.61	14.73	67.86	3.28	0.17	0.33
46.60	14.56	4.55	14.47	65.79	3.27	0.16	0.32
46.67	14.49	4.51	14.23	64.21	3.26	0.15	0.32
46.74	14.45	4.49	14.03	63.02	3.25	0.14	0.32
46.82	14.42	4.47	13.84	61.88	3.25	0.14	0.32
46.88	14.19	4.37	13.96	61.07	3.25	0.13	0.31
46.96	14.10	4.33	13.99	60.61	3.25	0.13	0.31
47.06	13.97	4.27	14.16	60.52	3.26	0.13	0.31

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
47.15	14.11	4.31	14.15	61.03	3.26	0.13	0.31
47.24	14.43	4.42	14.72	65.10	3.28	0.14	0.32
47.35	16.18	5.07	14.87	75.39	3.29	0.20	0.36
47.49	19.69	6.36	12.67	80.67	3.20	0.35	0.45
47.58	24.11	8.00	10.33	82.65	3.09	0.29	0.57
47.73	26.03	8.69	9.32	80.95	3.03	0.30	0.62
47.83	27.06	9.05	9.05	81.84	3.02	0.33	0.65
47.87	26.18	8.71	9.55	83.19	3.04	0.32	0.62
47.89	26.93	8.98	9.14	82.12	3.02	0.32	0.64
47.94	26.64	8.87	9.20	81.59	3.02	0.31	0.63
48.02	26.81	8.91	9.08	80.90	3.02	0.31	0.64
48.07	26.40	8.75	9.26	81.07	3.03	0.31	0.63
48.12	25.97	8.58	9.61	82.45	3.05	0.31	0.61
48.18	25.43	8.37	10.05	84.09	3.07	0.34	0.60
48.26	25.01	8.20	10.42	85.42	3.09	0.34	0.59
48.31	24.60	8.04	10.54	84.77	3.10	0.34	0.57
48.38	24.56	8.01	10.30	82.58	3.08	0.31	0.57
48.46	24.71	8.05	9.85	79.31	3.06	0.29	0.58
48.52	24.41	7.93	9.58	75.99	3.05	0.26	0.57
48.60	23.16	7.46	9.70	72.40	3.05	0.23	0.53
48.68	20.77	6.57	10.59	69.64	3.10	0.19	0.47
48.74	18.20	5.63	12.04	67.76	3.17	0.18	0.40
48.82	15.94	4.80	14.01	67.24	3.25	0.17	0.34
48.89	14.56	4.29	15.49	66.41	3.31	0.17	0.31
48.99	13.82	4.01	16.21	64.98	3.34	0.16	0.29
49.05	13.65	3.94	15.85	62.48	3.32	0.14	0.28
49.12	13.51	3.89	15.38	59.74	3.31	0.12	0.28
49.18	13.55	3.89	14.70	57.20	3.28	0.11	0.28
49.27	13.75	3.96	14.08	55.71	3.26	0.10	0.28
49.32	13.92	4.01	13.56	54.42	3.24	0.10	0.29
49.42	13.55	3.87	13.92	53.88	3.25	0.09	0.28
49.48	13.11	3.71	14.46	53.63	3.27	0.09	0.26
49.56	13.01	3.66	14.76	54.09	3.28	0.09	0.26
49.66	13.28	3.75	14.73	55.25	3.28	0.10	0.27
49.76	13.68	3.89	14.49	56.33	3.27	0.11	0.28
49.85	14.06	4.01	13.46	54.00	3.23	0.11	0.29
49.99	14.87	4.29	11.96	51.28	3.17	0.06	0.31
50.09	14.43	4.12	11.90	49.07	3.16	0.08	0.29
50.21	13.82	3.89	12.94	50.39	3.21	0.08	0.28
50.24	13.21	3.68	13.72	50.47	3.24	0.08	0.26
50.29	13.59	3.81	13.05	49.66	3.21	0.08	0.27
50.38	13.69	3.83	12.73	48.82	3.20	0.07	0.27
50.47	13.39	3.72	13.00	48.36	3.21	0.07	0.27
50.52	12.98	3.57	13.61	48.61	3.24	0.07	0.26
50.62	13.01	3.58	13.73	49.09	3.24	0.07	0.26
50.66	13.15	3.62	13.70	49.58	3.24	0.08	0.26
50.76	13.28	3.66	13.70	50.11	3.24	0.08	0.26
50.83	14.13	3.95	12.99	51.29	3.21	0.08	0.28

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
50.91	14.30	4.00	13.34	53.36	3.23	0.09	0.29
51.00	15.61	4.45	12.42	55.29	3.19	0.11	0.32
51.06	17.36	5.06	11.27	56.99	3.13	0.11	0.36
51.15	17.67	5.15	11.86	61.08	3.16	0.13	0.37
51.24	16.35	4.68	14.43	67.57	3.27	0.18	0.33
51.31	12.88	3.47	21.69	75.27	3.51	0.23	0.25
51.39	18.55	5.43	14.77	80.15	3.28	0.29	0.39
51.48	32.14	11.43	7.23	82.64	2.90	0.71	0.71
51.58	35.38	12.78	6.83	87.30	2.87	0.72	0.72
51.68	27.82	8.59	10.70	91.85	3.10	0.45	0.61
51.77	17.84	5.13	19.49	100.06	3.45	0.43	0.37
51.90	36.80	11.62	9.16	106.47	3.02	0.53	0.83
52.01	74.42	30.49	3.61	110.20	2.58	0.77	0.77
52.11	128.50	57.50	2.11	121.05	2.34	0.78	0.78
52.26	161.87	74.64	1.77	131.90	2.25	0.80	0.80
52.30	209.17	100.78	1.45	146.55	2.12	0.82	0.82
52.33	248.44	124.60	1.31	162.63	2.00	0.84	0.84
52.35	302.93	158.50	1.21	192.22	1.87	0.88	0.88
52.40	347.53	187.07	1.12	209.95	1.78	0.90	0.90
52.45	381.51	208.63	1.04	216.58	1.72	0.90	0.90
52.50	415.58	229.89	1.00	229.89	1.69	0.92	0.92
52.55	447.33	248.98	1.00	248.98	1.67	0.93	0.93
52.60	486.53	273.15	1.00	273.15	1.63	0.96	0.96
52.65	516.02	289.64	1.00	289.64	1.60	0.97	0.97
52.71	531.14	297.95	1.00	297.95	1.57	0.98	0.98
52.77	541.83	303.79	1.00	303.79	1.53	0.98	0.98
52.82	558.50	312.99	1.00	312.99	1.51	0.99	0.99
52.88	578.13	323.84	1.00	323.84	1.48	1.00	1.00
52.93	592.07	331.46	1.00	331.46	1.46	1.00	1.00
52.98	605.70	338.95	1.00	338.95	1.46	1.01	1.01
53.03	608.64	340.39	1.00	340.39	1.46	1.01	1.01
53.08	608.27	340.01	1.00	340.01	1.46	1.01	1.01
53.12	601.01	335.78	1.00	335.78	1.47	1.00	1.00
53.17	598.22	333.99	1.00	333.99	1.46	1.00	1.00
53.23	600.71	335.19	1.00	335.19	1.45	1.00	1.00
53.28	596.23	332.45	1.00	332.45	1.47	1.00	1.00
53.37	588.50	327.80	1.00	327.80	1.48	1.00	1.00
53.42	584.11	325.17	1.00	325.17	1.50	1.00	1.00
53.46	586.81	326.50	1.00	326.50	1.52	1.00	1.00
53.53	599.03	333.09	1.00	333.09	1.53	1.00	1.00
53.61	597.34	331.84	1.00	331.84	1.56	1.00	1.00
53.62	582.26	323.39	1.00	323.39	1.60	1.00	1.00
53.65	574.05	318.67	1.00	318.67	1.60	0.99	0.99
53.67	571.35	317.12	1.00	317.12	1.61	0.99	0.99
53.70	583.83	323.95	1.00	323.95	1.59	1.00	1.00
53.74	582.83	323.26	1.00	323.26	1.60	1.00	1.00
53.76	583.81	323.74	1.00	323.74	1.60	1.00	1.00
53.80	581.08	322.06	1.00	322.06	1.59	0.99	0.99

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
53.84	577.81	320.07	1.00	320.07	1.59	0.99	0.99
53.90	578.23	320.12	1.00	320.12	1.58	0.99	0.99
53.91	570.20	315.61	1.00	315.61	1.59	0.99	0.99
53.95	573.64	317.38	1.00	317.38	1.58	0.99	0.99
53.96	579.94	320.83	1.00	320.83	1.58	0.99	0.99
53.98	601.06	332.48	1.00	332.48	1.56	1.00	1.00
53.99	602.95	333.50	1.00	333.50	1.56	1.00	1.00
54.01	592.15	327.46	1.00	327.46	1.57	1.00	1.00
54.02	579.33	320.31	1.00	320.31	1.58	0.99	0.99
54.03	553.15	305.74	1.00	305.74	1.61	0.98	0.98
54.04	504.84	276.21	1.00	276.21	1.67	0.96	0.96
54.05	452.17	241.19	1.08	260.14	1.75	0.94	0.94
54.09	422.63	221.81	1.15	254.46	1.79	0.94	0.94
54.10	421.59	220.94	1.15	254.57	1.80	0.94	0.94
54.13	421.89	221.06	1.15	254.64	1.80	0.94	0.94
54.14	420.96	220.34	1.16	254.59	1.80	0.94	0.94
54.19	422.82	221.19	1.16	255.77	1.80	0.94	0.94
54.19	428.79	224.52	1.15	258.95	1.80	0.94	0.94
54.24	439.22	231.86	1.12	259.93	1.77	0.94	0.94
54.29	456.97	245.94	1.02	249.88	1.71	0.94	0.94
54.33	474.10	261.31	1.00	261.31	1.64	0.95	0.95
54.38	494.95	272.80	1.00	272.80	1.57	0.96	0.96
54.39	512.70	282.62	1.00	282.62	1.53	0.96	0.96
54.43	529.13	291.66	1.00	291.66	1.52	0.97	0.97
54.48	543.10	299.32	1.00	299.32	1.44	0.98	0.98
54.52	556.66	306.76	1.00	306.76	1.36	0.98	0.98
54.58	573.87	316.20	1.00	316.20	1.26	0.99	0.99
54.62	587.13	323.46	1.00	323.46	1.28	1.00	1.00
54.65	604.44	333.00	1.00	333.00	1.29	1.00	1.00
54.67	623.33	343.41	1.00	343.41	1.30	1.01	1.01
54.71	658.15	362.60	1.00	362.60	1.28	1.02	1.02
54.77	679.34	374.21	1.00	374.21	1.20	1.03	1.03
54.81	702.99	387.19	1.00	387.19	1.11	1.04	1.04
54.85	704.07	387.70	1.00	387.70	1.04	1.04	1.04
54.86	709.13	390.48	1.00	390.48	1.06	1.04	1.04
54.87	703.33	387.26	1.00	387.26	1.09	1.04	1.04
54.91	703.66	387.35	1.00	387.35	1.13	1.04	1.04
54.96	707.14	389.17	1.00	389.17	1.16	1.04	1.04
55.00	703.19	386.89	1.00	386.89	1.18	1.04	1.04
55.01	695.84	382.82	1.00	382.82	1.19	1.04	1.04
55.05	679.11	373.47	1.00	373.47	1.21	1.03	1.03
55.10	651.07	357.87	1.00	357.87	1.24	1.02	1.02
55.12	603.77	331.72	1.00	331.72	1.29	1.00	1.00
55.13	570.97	313.58	1.00	313.58	1.33	0.99	0.99
55.14	563.11	309.22	1.00	309.22	1.33	0.98	0.98
55.19	576.91	316.75	1.00	316.75	1.31	0.99	0.99
55.20	576.27	316.38	1.00	316.38	1.31	0.99	0.99
55.25	562.13	308.48	1.00	308.48	1.33	0.98	0.98

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
55.29	546.07	299.55	1.00	299.55	1.37	0.98	0.98
55.33	519.69	284.92	1.00	284.92	1.42	0.97	0.97
55.38	481.16	263.59	1.00	263.59	1.52	0.95	0.95
55.48	439.32	240.38	1.00	240.38	1.63	0.93	0.93
55.57	411.39	218.55	1.04	227.87	1.73	0.92	0.92
55.63	398.09	206.42	1.15	237.94	1.80	0.92	0.92
55.72	402.04	206.08	1.19	244.53	1.83	0.93	0.93
55.80	431.09	221.88	1.17	260.68	1.82	0.95	0.95
55.86	480.55	259.76	1.00	259.76	1.67	0.94	0.94
55.97	527.85	288.32	1.00	288.32	1.51	0.97	0.97
56.01	560.55	306.20	1.00	306.20	1.34	0.98	0.98
56.06	587.84	186.61	1.00	186.61	1.50	0.87	0.87
56.11	613.11	194.57	1.00	194.57	1.50	0.88	0.88
56.15	640.71	203.27	1.00	203.27	1.51	0.89	0.89
56.20	660.92	209.60	1.00	209.60	1.52	0.90	0.90
56.27	663.16	210.15	1.00	210.15	1.53	0.90	0.90
56.27	664.17	210.45	1.00	210.45	1.56	0.90	0.90
56.30	642.20	203.39	1.00	203.39	1.61	0.89	0.89
56.33	649.54	205.64	1.00	205.64	1.64	0.89	0.89
56.35	647.65	205.00	1.00	205.00	1.66	0.89	0.89
56.40	667.86	211.31	1.00	211.31	1.64	0.90	0.90
56.41	669.34	211.76	1.00	211.76	1.64	0.90	0.90
56.44	681.53	215.53	1.00	215.53	1.63	0.90	0.90
56.49	695.19	219.75	1.00	219.75	1.62	0.91	0.91
56.54	717.49	226.71	1.00	226.71	1.61	0.91	0.91
56.58	737.23	232.85	1.00	232.85	1.61	0.92	0.92
56.59	750.18	236.93	1.00	236.93	1.61	0.92	0.92
56.64	757.34	239.07	1.00	239.07	1.60	0.93	0.93
56.69	764.80	241.29	1.00	241.29	1.60	0.93	0.93
56.73	778.16	245.40	1.00	245.40	1.59	0.93	0.93
56.78	778.56	245.38	1.00	245.38	1.58	0.93	0.93
56.83	759.53	239.22	1.00	239.22	1.58	0.93	0.93
56.88	731.80	230.32	1.00	230.32	1.58	0.92	0.92
56.89	708.89	223.03	1.00	223.03	1.60	0.91	0.91
56.95	692.53	217.71	1.00	217.71	1.59	0.91	0.91
57.01	668.00	209.81	1.00	209.81	1.59	0.90	0.90
57.07	645.94	202.70	1.00	202.70	1.58	0.89	0.89
57.11	619.45	194.25	1.00	194.25	1.52	0.88	0.88
57.17	598.63	187.56	1.00	187.56	1.46	0.87	0.87
57.26	574.07	179.66	1.00	179.66	1.37	0.86	0.86
57.31	547.05	171.06	1.00	171.06	1.43	0.85	0.85
57.37	520.16	162.50	1.00	162.50	1.45	0.84	0.84
57.45	490.27	152.96	1.00	152.96	1.51	0.83	0.83
57.51	451.30	140.63	1.00	140.63	1.55	0.81	0.81
57.53	421.54	131.27	1.00	131.27	1.59	0.80	0.80
57.59	401.40	124.87	1.00	124.87	1.62	0.79	0.79
57.63	398.96	124.05	1.00	124.05	1.62	0.79	0.79
57.68	391.51	121.66	1.00	121.66	1.63	0.79	0.79

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
57.73	386.48	120.01	1.00	120.01	1.64	0.78	0.78
57.78	379.02	117.62	1.00	117.62	1.65	0.78	0.78
57.86	359.96	111.55	1.00	111.55	1.66	0.77	0.77
57.92	326.32	100.97	1.00	100.97	1.71	0.75	0.75
57.98	290.83	89.82	1.00	89.82	1.76	0.73	0.73
58.06	263.33	81.16	1.18	95.51	1.82	0.74	0.74
58.12	242.92	74.75	1.24	92.39	1.90	0.73	0.73
58.21	222.41	68.28	1.30	88.73	1.99	0.73	0.73
58.26	204.43	62.64	1.37	85.71	2.06	0.72	0.72
58.35	180.37	55.10	1.48	81.38	2.14	0.65	0.71
58.41	154.93	47.15	1.59	74.91	2.19	0.38	0.70
58.50	122.84	37.13	1.90	70.73	2.29	0.27	0.69
58.56	98.18	29.45	2.28	67.27	2.38	0.20	0.68
58.64	77.90	23.14	3.23	74.61	2.53	0.37	0.69
58.73	63.67	18.70	4.34	81.15	2.66	0.64	0.71
58.80	51.12	14.80	5.89	87.16	2.80	0.72	0.72
58.84	42.24	12.04	7.59	91.44	2.93	0.73	0.73
58.85	43.79	12.52	7.27	91.06	2.90	0.73	0.73
58.93	50.50	14.59	6.00	87.49	2.81	0.72	0.72
58.98	58.12	16.94	4.87	82.49	2.72	0.71	0.71
59.02	61.77	18.06	4.38	79.02	2.67	0.54	0.70
59.12	63.39	18.54	4.19	77.74	2.65	0.48	0.70
59.17	65.41	19.15	4.09	78.34	2.64	0.51	0.70
59.27	67.33	19.73	4.06	80.06	2.63	0.59	0.71
59.31	67.64	19.81	4.15	82.31	2.64	0.71	0.71
59.41	64.84	18.93	4.46	84.40	2.68	0.72	0.72
59.46	57.99	16.81	5.11	85.91	2.74	0.72	0.72
59.55	48.77	13.96	6.20	86.53	2.83	0.72	0.72
59.65	39.66	11.14	7.37	82.12	2.91	0.70	0.71
59.70	34.25	9.47	8.28	78.48	2.97	0.51	0.70
59.80	32.07	8.80	8.61	75.77	2.99	0.41	0.70
59.89	32.04	8.78	9.03	79.29	3.01	0.30	0.63
59.94	31.04	8.47	9.76	82.68	3.06	0.33	0.60
60.01	30.35	8.25	10.33	85.21	3.09	0.36	0.59
60.02	32.64	8.95	9.57	85.70	3.04	0.36	0.64
60.08	35.54	9.83	8.61	84.70	2.99	0.72	0.72
60.12	36.56	10.14	8.23	83.40	2.97	0.71	0.71
60.17	32.87	9.01	9.03	81.32	3.01	0.34	0.64
60.27	28.56	7.68	10.03	76.99	3.07	0.27	0.55
60.31	24.81	6.53	11.00	71.83	3.12	0.21	0.47
60.37	22.21	5.73	11.72	67.16	3.15	0.19	0.41
60.46	20.93	5.33	12.03	64.16	3.17	0.15	0.38
60.51	20.76	5.28	11.57	61.05	3.15	0.14	0.38
60.61	21.43	5.48	10.86	59.48	3.11	0.13	0.39
60.65	21.84	5.60	10.44	58.49	3.09	0.13	0.40
60.75	22.18	5.70	10.27	58.52	3.08	0.13	0.41
60.81	22.25	5.72	10.24	58.52	3.08	0.13	0.41
60.89	22.21	5.70	10.20	58.14	3.08	0.13	0.41

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
60.94	22.45	5.77	10.12	58.37	3.07	0.12	0.41
61.03	22.62	5.81	10.19	59.27	3.08	0.13	0.42
61.09	22.65	5.82	10.23	59.56	3.08	0.14	0.42
61.19	22.38	5.74	10.30	59.09	3.08	0.13	0.41
61.24	22.96	5.91	9.90	58.48	3.06	0.12	0.42
61.33	24.51	6.37	9.35	59.55	3.03	0.14	0.46
61.38	24.20	6.28	10.50	65.92	3.09	0.15	0.45
61.47	23.16	5.95	12.35	73.50	3.18	0.24	0.43
61.53	21.88	5.56	14.59	81.14	3.28	0.29	0.40
61.62	27.61	7.29	11.24	81.97	3.13	0.33	0.52
61.70	44.48	12.39	6.68	82.73	2.86	0.71	0.71
61.77	66.81	19.14	4.44	84.93	2.67	0.72	0.72
61.86	81.96	23.70	3.78	89.66	2.60	0.73	0.73
61.95	81.02	23.39	4.06	94.89	2.63	0.74	0.74
61.97	72.62	20.85	4.65	96.91	2.69	0.74	0.74
62.01	62.36	17.75	5.62	99.66	2.78	0.75	0.75
62.10	52.17	14.66	6.77	99.23	2.87	0.75	0.75
62.24	55.41	15.61	5.76	89.92	2.79	0.73	0.73
62.34	87.70	25.31	2.83	71.54	2.48	0.29	0.69
62.49	127.58	37.26	1.74	64.77	2.25	0.17	0.67
62.54	164.52	48.34	1.44	69.68	2.11	0.25	0.68
62.66	181.39	53.35	1.37	73.33	2.07	0.34	0.69
62.74	199.68	58.78	1.33	77.94	2.02	0.49	0.70
62.87	211.65	62.29	1.30	80.99	1.99	0.63	0.71
62.92	217.18	63.92	1.29	82.65	1.98	0.71	0.71
63.03	219.18	64.44	1.29	83.41	1.98	0.71	0.71
63.15	218.06	64.03	1.30	83.38	1.99	0.71	0.71
63.26	213.11	62.49	1.32	82.35	2.01	0.71	0.71
63.37	206.70	60.51	1.34	80.92	2.03	0.63	0.71
63.45	200.15	58.51	1.34	78.49	2.04	0.51	0.70
63.54	197.59	57.70	1.32	76.31	2.02	0.43	0.70
63.61	190.30	55.49	1.33	73.61	2.02	0.34	0.69
63.69	172.04	50.02	1.39	69.47	2.08	0.24	0.68
63.79	141.71	40.98	1.65	67.77	2.22	0.21	0.68
63.89	106.15	30.39	2.20	66.74	2.36	0.19	0.67
63.98	75.22	21.20	3.37	71.48	2.55	0.29	0.69
64.07	53.15	14.65	4.91	71.91	2.72	0.30	0.69
64.15	39.12	10.48	7.30	76.48	2.91	0.44	0.70
64.23	29.98	7.77	10.00	77.68	3.07	0.27	0.56
64.26	25.15	6.34	12.34	78.26	3.18	0.27	0.45
64.29	23.57	5.87	13.31	78.14	3.22	0.26	0.42
64.33	23.37	5.81	12.89	74.86	3.21	0.26	0.41
64.43	22.99	5.69	12.43	70.78	3.19	0.19	0.41
64.47	22.29	5.48	12.05	66.07	3.17	0.17	0.39
64.53	21.82	5.34	12.01	64.15	3.17	0.16	0.38
64.62	20.60	4.98	12.74	63.40	3.20	0.15	0.36
64.72	19.12	4.53	13.95	63.23	3.25	0.15	0.32
64.78	18.00	4.20	15.17	63.74	3.30	0.15	0.30

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
64.86	18.21	4.26	15.26	65.01	3.30	0.16	0.30
64.96	18.78	4.42	15.44	68.31	3.31	0.18	0.32
65.06	19.22	4.55	15.74	71.61	3.32	0.21	0.32
65.11	19.22	4.55	16.41	74.58	3.34	0.23	0.32
65.21	18.85	4.43	17.13	75.90	3.37	0.24	0.32
65.31	18.45	4.31	17.70	76.26	3.39	0.24	0.31
65.40	18.28	4.25	17.10	72.77	3.37	0.23	0.30
65.50	18.58	4.34	15.67	67.97	3.32	0.16	0.31
65.58	19.02	4.46	14.15	63.13	3.26	0.14	0.32
65.68	19.05	4.47	13.69	61.17	3.24	0.14	0.32
65.78	17.67	4.06	14.89	60.45	3.29	0.13	0.29
65.84	16.40	3.69	16.19	59.69	3.34	0.13	0.26
65.86	15.56	3.44	17.33	59.62	3.38	0.12	0.25
65.87	16.51	3.72	15.97	59.36	3.33	0.12	0.27
65.98	17.26	3.93	15.03	59.09	3.29	0.12	0.28
66.10	17.84	4.09	14.69	60.13	3.28	0.12	0.29
66.21	18.21	4.20	14.85	62.32	3.29	0.14	0.30
66.34	18.48	4.27	14.76	63.01	3.28	0.16	0.31
66.48	19.00	4.42	14.39	63.55	3.27	0.13	0.32
66.62	18.46	4.25	14.69	62.45	3.28	0.15	0.30
66.68	18.67	4.31	14.87	64.07	3.29	0.14	0.31
66.87	18.92	4.37	15.53	67.94	3.31	0.16	0.31
66.96	19.16	4.44	16.65	73.89	3.35	0.23	0.32
67.11	18.25	4.17	18.76	78.15	3.42	0.27	0.30
67.21	16.83	3.75	20.42	76.60	3.47	0.26	0.27
67.35	16.22	3.57	20.50	73.18	3.48	0.19	0.26
67.45	16.16	3.55	21.95	77.86	3.52	0.19	0.25
67.59	27.42	6.79	13.06	88.71	3.21	0.37	0.49
67.68	77.39	21.19	3.95	83.67	2.62	0.72	0.72
67.83	159.77	44.89	1.66	74.68	2.22	0.38	0.69
67.92	241.25	68.29	1.30	88.64	1.99	0.73	0.73
68.02	283.19	80.28	1.24	99.35	1.90	0.75	0.75
68.07	299.01	84.78	1.22	103.71	1.88	0.75	0.75
68.16	305.70	86.62	1.22	105.26	1.87	0.76	0.76
68.26	310.93	88.04	1.21	106.54	1.86	0.76	0.76
68.35	307.75	87.05	1.22	106.44	1.88	0.76	0.76
68.45	299.96	84.74	1.24	105.37	1.91	0.76	0.76
68.55	291.49	82.23	1.26	103.72	1.94	0.75	0.75
68.65	271.72	76.50	1.29	98.57	1.98	0.75	0.75
68.78	253.59	71.23	1.32	94.35	2.02	0.74	0.74
68.78	238.18	66.83	1.36	90.91	2.05	0.73	0.73
68.79	234.24	65.70	1.37	89.70	2.06	0.73	0.73
68.83	237.70	66.66	1.34	89.08	2.03	0.73	0.73
68.93	243.69	68.30	1.30	88.59	1.99	0.73	0.73
68.98	253.54	71.08	1.25	89.18	1.93	0.73	0.73
69.04	257.79	72.25	1.23	89.05	1.89	0.73	0.73
69.12	259.28	72.61	1.23	89.10	1.89	0.73	0.73
69.22	255.36	71.43	1.24	88.23	1.90	0.72	0.72

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
69.28	247.73	69.22	1.25	86.25	1.91	0.72	0.72
69.36	237.41	66.24	1.26	83.22	1.93	0.71	0.71
69.45	223.58	62.26	1.27	79.21	1.95	0.55	0.71
69.60	210.12	58.37	1.29	75.34	1.98	0.40	0.70
69.70	198.18	54.94	1.31	72.05	2.01	0.30	0.69
69.80	193.42	53.54	1.32	70.68	2.01	0.27	0.69
69.89	192.07	53.12	1.32	70.30	2.02	0.26	0.68
69.98	190.15	52.53	1.33	69.82	2.02	0.25	0.68
70.08	181.88	50.15	1.35	67.53	2.04	0.21	0.68
70.18	159.82	43.89	1.45	63.51	2.12	0.15	0.67
70.32	124.32	33.85	1.81	61.16	2.27	0.12	0.66
70.42	84.31	22.56	2.96	66.77	2.50	0.20	0.68
70.54	51.82	13.41	5.53	74.19	2.77	0.36	0.69
70.66	31.85	7.79	9.69	75.54	3.05	0.25	0.56
70.75	23.52	5.45	13.34	72.70	3.23	0.21	0.39
70.80	21.80	4.97	13.43	66.71	3.23	0.18	0.35
70.89	22.64	5.20	11.52	59.87	3.14	0.12	0.37
70.99	22.34	5.11	10.38	53.00	3.09	0.09	0.36
71.08	21.63	4.90	10.09	49.46	3.07	0.07	0.35
71.17	21.43	4.84	9.87	47.79	3.06	0.07	0.35
71.23	20.92	4.70	10.01	47.05	3.07	0.07	0.34
71.33	21.09	4.74	9.74	46.20	3.05	0.06	0.34
71.42	21.73	4.92	9.08	44.64	3.02	0.06	0.35
71.52	22.81	5.22	8.26	43.06	2.97	0.03	0.62
71.58	23.21	5.33	8.27	44.01	2.97	0.04	0.62
71.67	22.88	5.23	9.07	47.43	3.02	0.07	0.37
71.81	22.47	5.11	9.94	50.76	3.06	0.09	0.36
71.82	22.24	5.04	10.42	52.55	3.09	0.09	0.36
71.86	21.97	4.96	10.64	52.82	3.10	0.09	0.35
71.91	21.83	4.92	10.75	52.95	3.11	0.09	0.35
71.97	21.60	4.86	10.97	53.27	3.12	0.09	0.35
72.05	21.36	4.79	11.22	53.72	3.13	0.10	0.34
72.10	21.13	4.72	11.52	54.35	3.14	0.10	0.34
72.20	20.99	4.68	11.71	54.79	3.15	0.10	0.33
72.25	20.99	4.67	11.87	55.49	3.16	0.10	0.33
72.34	21.09	4.70	12.12	56.94	3.17	0.11	0.34
72.44	21.09	4.69	12.53	58.80	3.19	0.12	0.34
72.53	20.89	4.63	13.04	60.40	3.21	0.13	0.33
72.63	20.79	4.60	13.29	61.13	3.22	0.14	0.33
72.69	20.48	4.51	13.55	61.14	3.23	0.14	0.32
72.82	20.69	4.56	13.34	60.87	3.23	0.13	0.33
72.92	21.13	4.68	12.83	60.05	3.20	0.13	0.33
73.06	22.11	4.95	11.98	59.27	3.17	0.12	0.35
73.16	22.34	5.01	11.90	59.57	3.16	0.12	0.36
73.30	20.86	4.59	13.21	60.65	3.22	0.14	0.33
73.35	19.88	4.32	14.25	61.53	3.26	0.14	0.31
73.38	19.20	4.13	14.83	61.23	3.29	0.13	0.30
73.47	20.02	4.35	13.95	60.67	3.25	0.13	0.31

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
73.53	20.08	4.37	13.79	60.20	3.24	0.13	0.31
73.62	20.18	4.39	13.66	59.95	3.24	0.13	0.31
73.71	19.95	4.32	13.95	60.28	3.25	0.13	0.31
73.77	19.61	4.23	14.55	61.46	3.28	0.13	0.30
73.86	19.34	4.15	15.21	63.08	3.30	0.15	0.30
73.96	19.38	4.15	15.56	64.61	3.31	0.15	0.30
74.06	19.58	4.20	15.60	65.59	3.32	0.16	0.30
74.13	20.02	4.32	15.32	66.22	3.31	0.16	0.31
74.24	20.36	4.41	15.12	66.66	3.30	0.17	0.31
74.34	20.56	4.46	15.08	67.26	3.30	0.17	0.32
74.44	20.42	4.42	15.35	67.81	3.31	0.18	0.32
74.58	20.37	4.40	15.30	67.28	3.30	0.18	0.31
74.68	20.30	4.38	14.35	62.80	3.27	0.16	0.31
74.80	20.47	4.42	13.30	58.74	3.22	0.09	0.32
74.92	20.26	4.35	12.97	56.43	3.21	0.11	0.31
75.07	20.06	4.29	13.60	58.35	3.24	0.12	0.31
75.08	19.75	4.21	14.10	59.34	3.26	0.12	0.30
75.11	19.62	4.17	14.28	59.53	3.26	0.12	0.30
75.16	19.55	4.15	14.53	60.28	3.27	0.13	0.30
75.25	19.31	4.08	15.14	61.74	3.30	0.13	0.29
75.32	19.14	4.03	15.69	63.23	3.32	0.15	0.29
75.40	18.98	3.98	16.00	63.73	3.33	0.15	0.28
75.50	18.81	3.93	15.96	62.77	3.33	0.14	0.28
75.59	18.30	3.79	16.02	60.75	3.33	0.13	0.27
75.69	17.56	3.59	16.34	58.60	3.34	0.11	0.26
75.78	16.85	3.39	16.66	56.46	3.35	0.11	0.24
75.88	16.41	3.27	16.73	54.66	3.36	0.10	0.23
75.96	16.11	3.18	16.62	52.90	3.35	0.09	0.23
76.05	16.04	3.16	16.34	51.65	3.34	0.08	0.23
76.14	15.97	3.14	16.25	51.00	3.34	0.08	0.22
76.26	16.07	3.16	16.16	51.09	3.34	0.08	0.23
76.36	16.07	3.16	16.26	51.38	3.34	0.08	0.23
76.41	16.07	3.16	16.31	51.50	3.34	0.08	0.23
76.51	15.84	3.09	16.56	51.17	3.35	0.08	0.22
76.65	15.50	2.99	17.04	51.04	3.37	0.08	0.21
76.72	15.26	2.93	17.45	51.12	3.38	0.08	0.21
76.79	15.16	2.90	17.72	51.39	3.39	0.08	0.21
76.89	15.23	2.91	18.36	53.53	3.41	0.08	0.21
76.98	15.47	2.98	20.80	61.89	3.48	0.11	0.21
77.08	18.00	3.65	19.05	69.60	3.43	0.21	0.26
77.18	22.18	4.77	16.19	77.29	3.34	0.23	0.34
77.28	26.73	5.99	14.06	84.26	3.26	0.29	0.43
77.37	27.88	6.30	14.87	93.62	3.29	0.40	0.45
77.42	28.76	6.53	15.41	100.64	3.31	0.49	0.47
77.42	30.22	6.92	15.09	104.44	3.30	0.50	0.49
77.44	34.00	7.94	13.49	107.05	3.23	0.53	0.57
77.48	37.40	8.85	12.47	110.31	3.19	0.60	0.63
77.52	40.61	9.70	11.65	113.00	3.15	0.64	0.69

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
77.54	42.94	10.33	11.08	114.44	3.12	0.66	0.74
77.57	43.37	10.44	11.07	115.54	3.12	0.68	0.75
77.62	42.26	10.14	11.44	115.93	3.14	0.69	0.72
77.65	40.10	9.55	12.10	115.64	3.17	0.66	0.68
77.67	38.72	9.18	12.34	113.32	3.18	0.65	0.66
77.71	37.91	8.96	12.41	111.24	3.19	0.59	0.64
77.71	37.03	8.73	12.35	107.78	3.18	0.58	0.62
77.76	34.77	8.12	12.85	104.25	3.20	0.52	0.58
77.81	31.76	7.31	13.53	98.88	3.23	0.45	0.52
77.90	29.03	6.57	14.40	94.60	3.27	0.39	0.47
77.95	27.32	6.11	15.14	92.44	3.30	0.37	0.44
78.01	26.34	5.84	15.63	91.29	3.32	0.38	0.42
78.10	27.59	6.17	14.49	89.37	3.27	0.35	0.44
78.16	36.29	8.49	9.98	84.71	3.07	0.33	0.61
78.24	48.94	11.86	6.66	79.05	2.86	0.54	0.70
78.29	64.83	16.10	4.54	73.14	2.68	0.33	0.69
78.39	77.42	19.44	3.56	69.27	2.58	0.24	0.68
78.47	87.30	22.06	3.11	68.51	2.52	0.23	0.68
78.53	92.74	23.49	3.05	71.72	2.51	0.29	0.69
78.62	94.25	23.88	3.25	77.71	2.54	0.48	0.70
78.68	91.22	23.06	3.64	84.02	2.59	0.72	0.72
78.69	92.97	23.52	3.81	89.57	2.61	0.73	0.73
78.78	93.95	23.76	4.00	95.10	2.63	0.74	0.74
78.81	94.86	24.00	4.25	102.04	2.65	0.75	0.75
78.92	85.28	21.43	5.01	107.35	2.73	0.76	0.76
79.03	72.83	18.11	5.93	107.43	2.81	0.76	0.76
79.16	68.41	16.91	5.87	99.26	2.80	0.75	0.75
79.26	78.39	19.54	4.53	88.45	2.68	0.73	0.73
79.35	97.35	24.54	3.42	83.92	2.56	0.72	0.72
79.45	114.43	29.03	2.95	85.78	2.50	0.72	0.72
79.54	124.25	31.60	2.84	89.58	2.48	0.73	0.73
79.64	131.23	33.41	2.75	91.91	2.47	0.73	0.73
79.74	153.43	39.23	2.39	93.85	2.40	0.74	0.74
79.88	186.93	48.00	1.98	94.86	2.31	0.74	0.74
79.98	228.94	59.00	1.62	95.73	2.20	0.74	0.74
80.12	248.77	64.13	1.48	95.14	2.14	0.74	0.74
80.22	253.19	65.23	1.40	91.22	2.09	0.73	0.73
80.36	244.79	62.94	1.37	86.07	2.06	0.72	0.72
80.46	238.82	61.33	1.32	81.11	2.02	0.64	0.71
80.60	231.84	59.42	1.30	77.21	1.99	0.46	0.70
80.70	223.91	57.30	1.30	74.37	1.99	0.37	0.69
80.83	213.12	54.42	1.32	72.04	2.02	0.30	0.69
80.94	194.49	49.51	1.41	69.62	2.09	0.25	0.68
81.01	177.96	45.17	1.50	67.91	2.15	0.21	0.68
81.04	164.23	41.58	1.60	66.50	2.19	0.19	0.67
81.09	158.43	40.05	1.65	65.97	2.21	0.18	0.67
81.13	149.59	37.74	1.75	66.04	2.25	0.18	0.67
81.18	136.87	34.41	1.98	67.98	2.31	0.22	0.68

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
81.23	123.31	30.87	2.34	72.13	2.39	0.30	0.69
81.28	109.41	27.24	2.85	77.64	2.48	0.48	0.70
81.33	98.17	24.30	3.46	84.19	2.57	0.72	0.72
81.37	88.49	21.78	4.25	92.48	2.65	0.73	0.73
81.42	81.24	19.88	5.05	100.46	2.73	0.75	0.75
81.47	75.77	18.46	5.75	106.15	2.79	0.76	0.76
81.52	71.99	17.47	6.25	109.13	2.83	0.76	0.76
81.56	70.98	17.20	6.46	111.09	2.85	0.77	0.77
81.61	70.58	17.08	6.60	112.75	2.86	0.77	0.77
81.64	68.79	16.62	6.89	114.41	2.88	0.77	0.77
81.70	62.18	14.89	7.85	116.91	2.94	0.78	0.78
81.75	54.38	12.87	9.25	118.94	3.03	0.76	0.92
81.79	46.89	10.92	10.91	119.14	3.11	0.73	0.78
81.82	41.90	9.62	12.12	116.62	3.17	0.68	0.69
81.86	37.62	8.51	13.21	112.49	3.22	0.61	0.61
81.91	34.01	7.57	14.21	107.66	3.26	0.54	0.54
81.95	30.63	6.70	15.27	102.27	3.30	0.48	0.48
82.00	27.33	5.84	16.41	95.81	3.34	0.41	0.42
82.09	24.26	5.04	17.74	89.46	3.39	0.33	0.36
82.15	21.66	4.37	19.38	84.64	3.44	0.29	0.31
82.19	19.83	3.89	20.80	81.03	3.48	0.27	0.28
82.26	18.38	3.52	22.06	77.56	3.52	0.23	0.25
82.34	17.00	3.16	23.49	74.17	3.56	0.21	0.23
82.39	15.65	2.81	25.58	71.81	3.61	0.20	0.20
82.48	14.77	2.58	27.14	69.97	3.64	0.18	0.18
82.58	14.64	2.54	26.84	68.21	3.64	0.17	0.18
82.62	14.74	2.57	25.95	66.60	3.62	0.16	0.18
82.70	14.88	2.60	25.23	65.56	3.60	0.15	0.19
82.77	14.81	2.58	24.98	64.46	3.59	0.15	0.18
82.87	15.08	2.65	24.19	64.01	3.57	0.14	0.19
82.96	16.23	2.94	21.57	63.38	3.51	0.14	0.21
83.06	18.22	3.45	18.38	63.34	3.41	0.14	0.25
83.16	21.39	4.26	14.82	63.10	3.29	0.14	0.30
83.25	24.46	5.04	12.49	62.94	3.19	0.15	0.36
83.34	27.20	5.74	10.91	62.57	3.11	0.15	0.41
83.44	28.34	6.03	10.55	63.55	3.10	0.15	0.43
83.54	28.75	6.12	10.60	64.89	3.10	0.17	0.44
83.64	28.61	6.08	10.93	66.49	3.12	0.17	0.43
83.73	27.70	5.84	11.68	68.29	3.15	0.18	0.42
83.83	27.26	5.73	12.30	70.46	3.18	0.20	0.41
83.85	26.83	5.62	13.07	73.38	3.21	0.21	0.40
83.89	27.47	5.78	13.14	75.93	3.22	0.24	0.41
83.94	28.11	5.94	13.69	81.26	3.24	0.26	0.42
84.04	29.26	6.23	13.80	85.92	3.25	0.34	0.44
84.09	30.40	6.51	13.83	90.10	3.25	0.36	0.47
84.13	31.28	6.74	13.65	91.94	3.24	0.37	0.48
84.18	31.68	6.83	13.70	93.61	3.24	0.40	0.49
84.25	31.52	6.79	13.97	94.85	3.25	0.41	0.48

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
84.33	30.64	6.56	14.57	95.60	3.28	0.41	0.47
84.37	29.46	6.26	15.33	95.90	3.31	0.41	0.45
84.46	28.35	5.97	15.91	94.98	3.33	0.41	0.43
84.52	27.50	5.75	16.25	93.43	3.34	0.38	0.41
84.57	26.90	5.59	16.32	91.27	3.34	0.36	0.40
84.67	26.52	5.49	16.38	90.00	3.34	0.34	0.39
84.71	26.15	5.40	16.62	89.72	3.35	0.34	0.39
84.81	25.58	5.25	17.32	90.86	3.38	0.35	0.37
84.86	24.84	5.06	18.32	92.62	3.41	0.37	0.36
84.91	24.06	4.86	19.36	94.03	3.44	0.38	0.35
85.00	23.42	4.69	20.18	94.63	3.47	0.39	0.33
85.05	22.81	4.53	20.72	93.94	3.48	0.39	0.32
85.15	22.34	4.41	20.94	92.30	3.49	0.36	0.31
85.19	21.80	4.27	20.88	89.13	3.49	0.34	0.30
85.29	21.33	4.15	20.74	85.98	3.48	0.30	0.30
85.35	20.72	3.99	20.84	83.14	3.49	0.28	0.28
85.42	20.08	3.82	21.32	81.54	3.50	0.27	0.27
85.48	19.40	3.65	22.03	80.45	3.52	0.26	0.26
85.55	18.77	3.49	22.80	79.50	3.54	0.25	0.25
85.63	18.19	3.34	23.58	78.76	3.56	0.25	0.24
85.68	17.62	3.19	24.50	78.25	3.58	0.24	0.23
85.77	17.18	3.08	25.34	78.03	3.60	0.24	0.22
85.82	17.04	3.04	25.74	78.34	3.61	0.24	0.22
85.89	17.42	3.13	25.13	78.79	3.60	0.25	0.22
85.96	18.33	3.36	23.51	79.01	3.56	0.25	0.24
86.03	19.71	3.71	21.16	78.44	3.49	0.25	0.26
86.11	21.06	4.04	19.14	77.40	3.44	0.24	0.29
86.16	22.11	4.30	17.71	76.21	3.39	0.23	0.31
86.25	21.67	4.19	18.09	75.81	3.40	0.22	0.30
86.36	19.98	3.76	19.76	74.32	3.45	0.23	0.27
86.50	18.16	3.30	22.08	72.85	3.52	0.19	0.24
86.51	17.25	3.07	23.09	70.91	3.55	0.19	0.22
86.52	17.32	3.09	22.53	69.58	3.53	0.19	0.22
86.57	17.35	3.10	21.58	66.80	3.51	0.17	0.22
86.65	17.39	3.10	20.48	63.50	3.48	0.13	0.22
86.71	17.35	3.09	19.65	60.73	3.45	0.13	0.22
86.80	17.08	3.02	19.57	59.11	3.45	0.12	0.22
86.90	16.48	2.87	20.04	57.42	3.46	0.11	0.20
86.99	15.77	2.69	20.75	55.74	3.48	0.10	0.19
87.04	15.26	2.56	21.24	54.32	3.50	0.09	0.18
87.14	15.16	2.53	21.16	53.51	3.49	0.09	0.18
87.19	15.36	2.58	20.70	53.36	3.48	0.09	0.18
87.28	15.87	2.70	20.13	54.40	3.46	0.09	0.19
87.38	16.51	2.86	19.47	55.67	3.45	0.10	0.20
87.43	17.18	3.03	18.79	56.85	3.42	0.11	0.22
87.52	17.76	3.17	18.12	57.36	3.40	0.11	0.23
87.61	18.23	3.28	17.55	57.58	3.38	0.11	0.23
87.66	18.53	3.35	17.13	57.47	3.37	0.11	0.24

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
87.76	18.57	3.36	17.00	57.12	3.37	0.11	0.24
87.84	18.43	3.32	17.02	56.58	3.37	0.10	0.24
87.91	18.13	3.25	17.27	56.08	3.37	0.10	0.23
88.00	17.79	3.16	17.58	55.54	3.39	0.10	0.23
88.11	17.46	3.07	17.98	55.23	3.40	0.10	0.22
88.19	17.22	3.01	18.27	55.01	3.41	0.10	0.22
88.25	17.08	2.98	18.42	54.79	3.41	0.10	0.21
88.34	17.02	2.96	18.36	54.27	3.41	0.09	0.21
88.44	16.98	2.94	18.20	53.59	3.41	0.09	0.21
88.54	16.98	2.94	17.99	52.93	3.40	0.09	0.21
88.64	16.95	2.93	17.92	52.52	3.40	0.08	0.21
88.72	16.88	2.91	18.00	52.42	3.40	0.08	0.21
88.82	16.82	2.89	18.16	52.53	3.40	0.08	0.21
88.91	16.72	2.87	18.42	52.79	3.41	0.08	0.20
89.01	16.62	2.84	18.68	53.02	3.42	0.09	0.20
89.10	16.49	2.80	18.99	53.22	3.43	0.09	0.20
89.19	16.32	2.76	19.19	52.91	3.44	0.09	0.20
89.30	16.21	2.73	18.48	50.44	3.41	0.08	0.19
89.39	16.31	2.75	17.80	48.98	3.39	0.05	0.20
89.49	16.62	2.82	17.53	49.49	3.38	0.07	0.20
89.59	16.90	2.89	18.25	52.76	3.41	0.09	0.21
89.69	17.04	2.92	18.79	54.90	3.42	0.10	0.21
89.73	17.68	3.08	18.14	55.86	3.40	0.10	0.22
89.78	18.48	3.27	17.18	56.23	3.37	0.10	0.23
89.83	19.36	3.49	16.22	56.56	3.34	0.10	0.25
89.88	19.63	3.55	16.06	57.05	3.33	0.11	0.25
89.93	19.86	3.61	16.01	57.77	3.33	0.11	0.26
90.00	20.24	3.70	15.90	58.79	3.33	0.11	0.26
90.07	20.88	3.85	15.53	59.82	3.31	0.12	0.28
90.12	21.62	4.03	15.19	61.24	3.30	0.13	0.29
90.22	22.26	4.19	15.01	62.84	3.29	0.14	0.30
90.27	23.04	4.37	15.02	65.70	3.29	0.15	0.31
90.36	24.99	4.85	14.09	68.34	3.26	0.18	0.35
90.46	27.46	5.45	12.89	70.27	3.21	0.20	0.39
90.50	29.28	5.89	12.05	71.01	3.17	0.20	0.42
90.61	29.48	5.94	12.02	71.39	3.17	0.20	0.42
90.66	28.70	5.75	12.38	71.12	3.18	0.20	0.41
90.75	27.62	5.48	12.73	69.74	3.20	0.19	0.39
90.84	26.17	5.12	13.28	67.94	3.22	0.17	0.37
90.89	24.72	4.76	13.90	66.20	3.25	0.16	0.34
90.99	23.48	4.45	14.63	65.12	3.28	0.15	0.32
91.04	22.50	4.21	15.24	64.21	3.30	0.15	0.30
91.14	21.59	3.99	15.98	63.69	3.33	0.14	0.28
91.22	20.75	3.78	16.73	63.19	3.36	0.14	0.27
91.28	19.83	3.55	17.61	62.55	3.39	0.14	0.25
91.37	19.26	3.41	18.11	61.75	3.40	0.13	0.24
91.47	18.99	3.34	18.18	60.75	3.40	0.13	0.24
91.61	19.26	3.40	17.69	60.19	3.39	0.12	0.24

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
91.71	19.40	3.43	17.48	59.97	3.38	0.12	0.25
91.81	19.50	3.45	17.39	60.03	3.38	0.12	0.25
91.87	19.36	3.42	17.46	59.68	3.38	0.12	0.24
92.00	19.38	3.42	16.82	57.50	3.36	0.12	0.24
92.10	19.41	3.42	16.30	55.77	3.34	0.09	0.24
92.20	19.62	3.47	15.85	54.98	3.32	0.09	0.25
92.33	19.76	3.50	16.12	56.37	3.33	0.10	0.25
92.38	19.89	3.53	16.27	57.43	3.34	0.11	0.25
92.43	20.03	3.56	16.28	57.96	3.34	0.11	0.25
92.48	19.98	3.55	16.52	58.57	3.35	0.11	0.25
92.56	19.88	3.52	16.79	59.09	3.36	0.12	0.25
92.63	19.64	3.46	17.17	59.41	3.37	0.12	0.25
92.67	19.57	3.44	17.27	59.42	3.37	0.12	0.25
92.72	19.54	3.43	17.30	59.38	3.38	0.12	0.25
92.77	19.64	3.46	17.18	59.37	3.37	0.12	0.25
92.86	19.84	3.50	16.99	59.49	3.37	0.12	0.25
92.92	20.08	3.56	16.84	59.88	3.36	0.12	0.25
92.97	20.21	3.59	17.01	61.03	3.37	0.12	0.26
93.05	20.35	3.62	17.17	62.12	3.37	0.14	0.26
93.10	20.62	3.68	17.13	63.07	3.37	0.14	0.26
93.16	21.10	3.79	16.68	63.28	3.35	0.14	0.27
93.25	21.70	3.94	16.06	63.20	3.33	0.14	0.28
93.35	22.78	4.19	14.99	62.84	3.29	0.14	0.30
93.40	23.19	4.29	14.52	62.27	3.27	0.14	0.31
93.49	23.25	4.30	14.38	61.82	3.27	0.13	0.31
93.56	22.71	4.17	14.77	61.55	3.28	0.13	0.30
93.64	22.88	4.21	14.66	61.65	3.28	0.13	0.30
93.73	23.63	4.38	14.34	62.81	3.27	0.13	0.31
93.83	24.91	4.69	13.81	64.72	3.25	0.15	0.33
93.88	26.43	5.05	13.44	67.85	3.23	0.17	0.36
93.97	27.01	5.18	13.58	70.35	3.24	0.20	0.37
94.07	26.43	5.04	14.48	72.95	3.27	0.20	0.36
94.17	25.76	4.87	15.51	75.57	3.31	0.22	0.35
94.26	26.70	5.09	15.04	76.60	3.29	0.25	0.36
94.36	27.88	5.37	15.22	81.75	3.30	0.23	0.38
94.45	29.47	5.75	15.14	87.02	3.30	0.34	0.41
94.55	35.88	7.27	12.61	91.74	3.19	0.39	0.52
94.64	48.46	10.27	8.71	89.52	3.00	0.73	0.73
94.72	59.93	13.01	6.55	85.22	2.85	0.72	0.72
94.74	73.87	16.33	4.89	79.85	2.72	0.58	0.71
94.77	84.50	18.86	4.08	76.98	2.64	0.45	0.70
94.85	97.35	21.92	3.39	74.39	2.56	0.37	0.69
94.90	102.75	23.20	3.24	75.17	2.54	0.39	0.70
94.95	105.32	23.80	3.27	77.89	2.54	0.49	0.70
95.01	104.68	23.63	3.61	85.22	2.58	0.72	0.72
95.09	100.83	22.70	4.16	94.37	2.64	0.74	0.74
95.14	94.49	21.18	5.05	107.02	2.73	0.76	0.76
95.23	86.42	19.25	6.10	117.34	2.82	0.78	0.78

:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
95.29	78.06	17.25	7.36	126.89	2.91	0.79	0.79
95.38	71.11	15.59	8.45	131.69	2.98	0.80	0.80
95.43	67.53	14.73	9.06	133.43	3.02	0.97	1.05
95.52	67.83	14.79	8.96	132.50	3.01	0.95	1.06
95.57	70.23	15.35	8.40	128.95	2.98	0.80	0.80
95.67	71.24	15.58	7.93	123.49	2.95	0.79	0.79
95.77	66.52	14.45	8.22	118.72	2.97	0.78	0.78
95.86	56.97	12.17	9.76	118.80	3.06	0.69	0.87
95.95	52.94	11.21	10.40	116.56	3.09	0.74	0.80
96.03	46.73	9.74	12.16	118.40	3.17	0.62	0.70
96.11	51.55	10.87	10.92	118.64	3.12	0.68	0.78
96.20	59.20	12.66	9.84	124.65	3.06	0.80	0.90
96.30	80.15	17.59	7.15	125.73	2.90	0.79	0.79
96.39	101.37	22.58	5.51	124.50	2.77	0.79	0.79
96.50	122.96	27.64	4.35	120.31	2.67	0.78	0.78
96.59	144.96	32.80	3.25	106.72	2.54	0.76	0.76
96.69	164.86	37.45	2.44	91.36	2.41	0.73	0.73
96.78	180.18	41.02	1.89	77.51	2.29	0.47	0.70
96.87	185.95	42.35	1.72	72.98	2.24	0.33	0.69
96.98	185.28	42.15	1.69	71.40	2.23	0.29	0.69
97.02	177.79	40.38	1.78	71.90	2.26	0.30	0.69
97.06	176.40	40.04	1.83	73.47	2.27	0.34	0.69
97.12	175.60	39.84	1.91	76.16	2.30	0.42	0.70
97.16	176.98	40.15	1.98	79.48	2.31	0.56	0.71
97.21	173.67	39.35	2.13	83.99	2.35	0.72	0.72
97.27	170.50	38.59	2.31	89.17	2.39	0.73	0.73
97.33	168.21	38.04	2.46	93.67	2.42	0.74	0.74
97.40	165.98	37.49	2.57	96.33	2.44	0.74	0.74
97.45	163.92	37.00	2.64	97.51	2.45	0.74	0.74
97.50	161.39	36.39	2.76	100.38	2.47	0.75	0.75
97.58	155.82	35.06	2.99	104.78	2.50	0.76	0.76
97.65	146.95	32.97	3.34	110.26	2.55	0.77	0.77
97.69	134.43	30.04	3.79	113.95	2.60	0.77	0.77
97.74	121.75	27.07	4.27	115.68	2.66	0.78	0.78
97.81	110.51	24.44	4.76	116.42	2.71	0.78	0.78
97.88	103.09	22.69	5.14	116.63	2.74	0.78	0.78
97.93	108.66	23.98	4.67	111.98	2.70	0.77	0.77
98.03	138.72	30.95	3.15	97.35	2.52	0.74	0.74
98.15	182.62	41.12	2.03	83.50	2.33	0.71	0.71
98.21	228.43	51.75	1.51	78.05	2.15	0.50	0.70
98.32	264.20	60.00	1.34	80.19	2.03	0.59	0.71
98.42	301.85	68.69	1.25	85.96	1.92	0.72	0.72
98.47	349.59	79.73	1.00	79.73	1.79	0.57	0.71
98.57	388.76	88.75	1.00	88.75	1.69	0.73	0.73
98.70	411.84	94.00	1.00	94.00	1.61	0.74	0.74
98.78	404.01	92.13	1.00	92.13	1.62	0.73	0.73
98.85	372.43	84.79	1.00	84.79	1.67	0.72	0.72
98.86	337.78	76.77	1.00	76.77	1.74	0.45	0.70

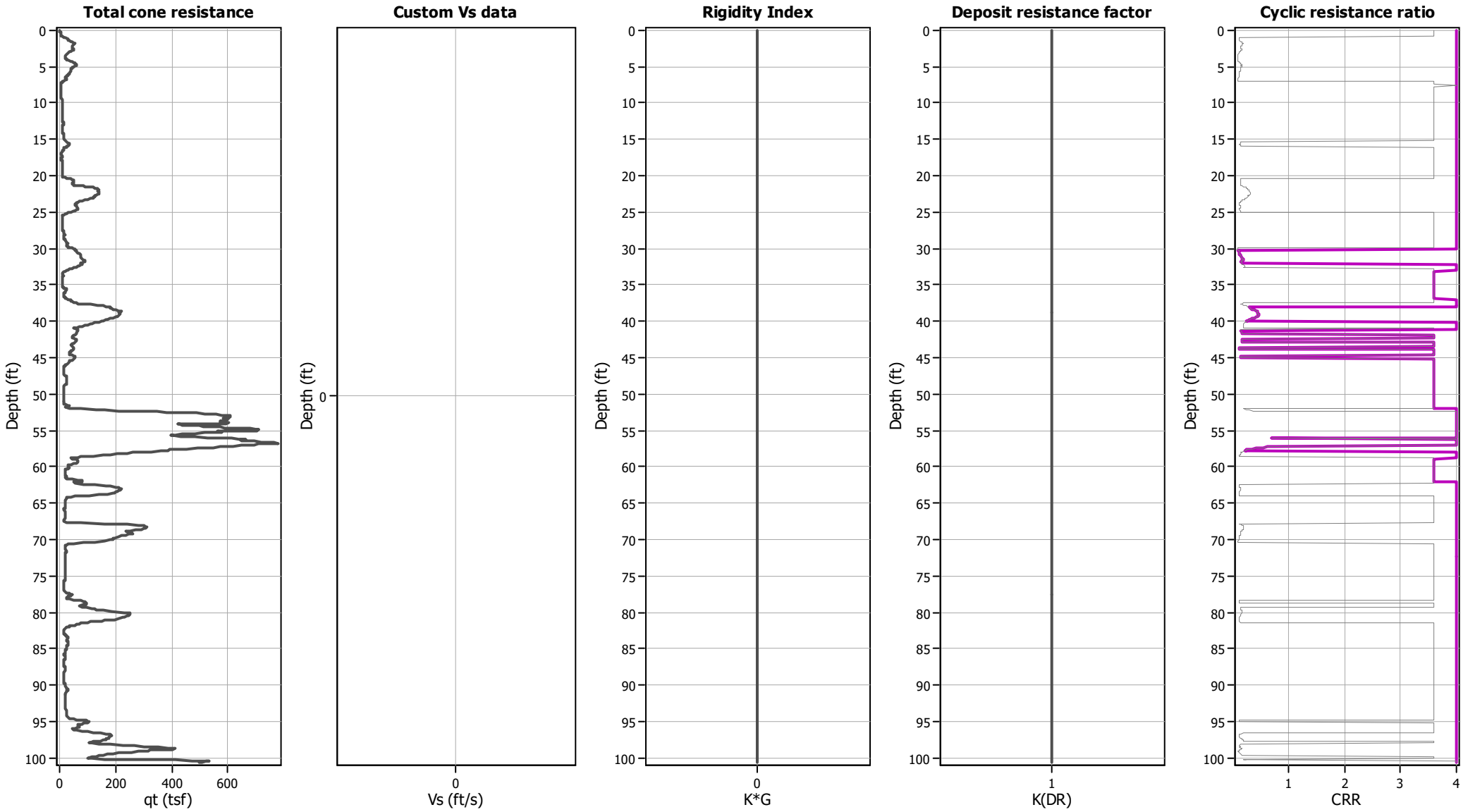
:: Strength loss calculation (Robertson (2009) :: (continued)

Depth (ft)	q_t (tsf)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
98.92	322.73	73.26	1.00	73.26	1.77	0.33	0.69
98.98	318.48	72.24	1.00	72.24	1.78	0.31	0.69
99.03	309.41	70.12	1.00	70.12	1.81	0.26	0.68
99.11	281.64	63.67	1.00	63.67	1.90	0.15	0.67
99.18	255.32	57.57	1.30	74.69	1.99	0.38	0.69
99.23	231.33	52.01	1.41	73.25	2.09	0.33	0.69
99.32	209.84	47.02	1.62	76.01	2.20	0.42	0.70
99.37	189.39	42.29	1.96	83.05	2.31	0.71	0.71
99.45	170.57	37.93	2.37	90.04	2.40	0.73	0.73
99.56	157.24	34.83	2.76	96.01	2.47	0.74	0.74
99.64	147.39	32.55	3.13	101.90	2.52	0.75	0.75
99.71	140.04	30.84	3.53	108.77	2.57	0.76	0.76
99.75	128.26	28.12	4.04	113.72	2.63	0.77	0.77
99.90	116.32	25.35	4.67	118.27	2.70	0.78	0.78
99.95	101.78	22.01	5.75	126.55	2.79	0.79	0.79
100.04	116.32	25.32	5.03	127.45	2.73	0.79	0.79
100.14	159.30	35.14	3.33	116.89	2.55	0.78	0.78
100.14	204.99	45.59	2.33	106.43	2.39	0.76	0.76
100.15	235.79	52.64	2.00	105.52	2.32	0.76	0.76
100.19	258.80	57.89	1.93	111.71	2.30	0.77	0.77
100.21	298.07	66.86	1.78	119.29	2.26	0.78	0.78
100.24	351.88	79.16	1.37	108.37	2.06	0.76	0.76
100.28	410.56	92.54	1.15	106.62	1.80	0.76	0.76
100.31	470.98	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.33	508.57	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.38	524.63	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.39	526.55	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.43	531.78	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.48	522.24	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.53	509.38	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.57	496.12	-1.00	1.00	-1.00	-1.00	0.00	0.00
100.60	497.27	-1.00	1.00	-1.00	-1.00	0.00	0.00

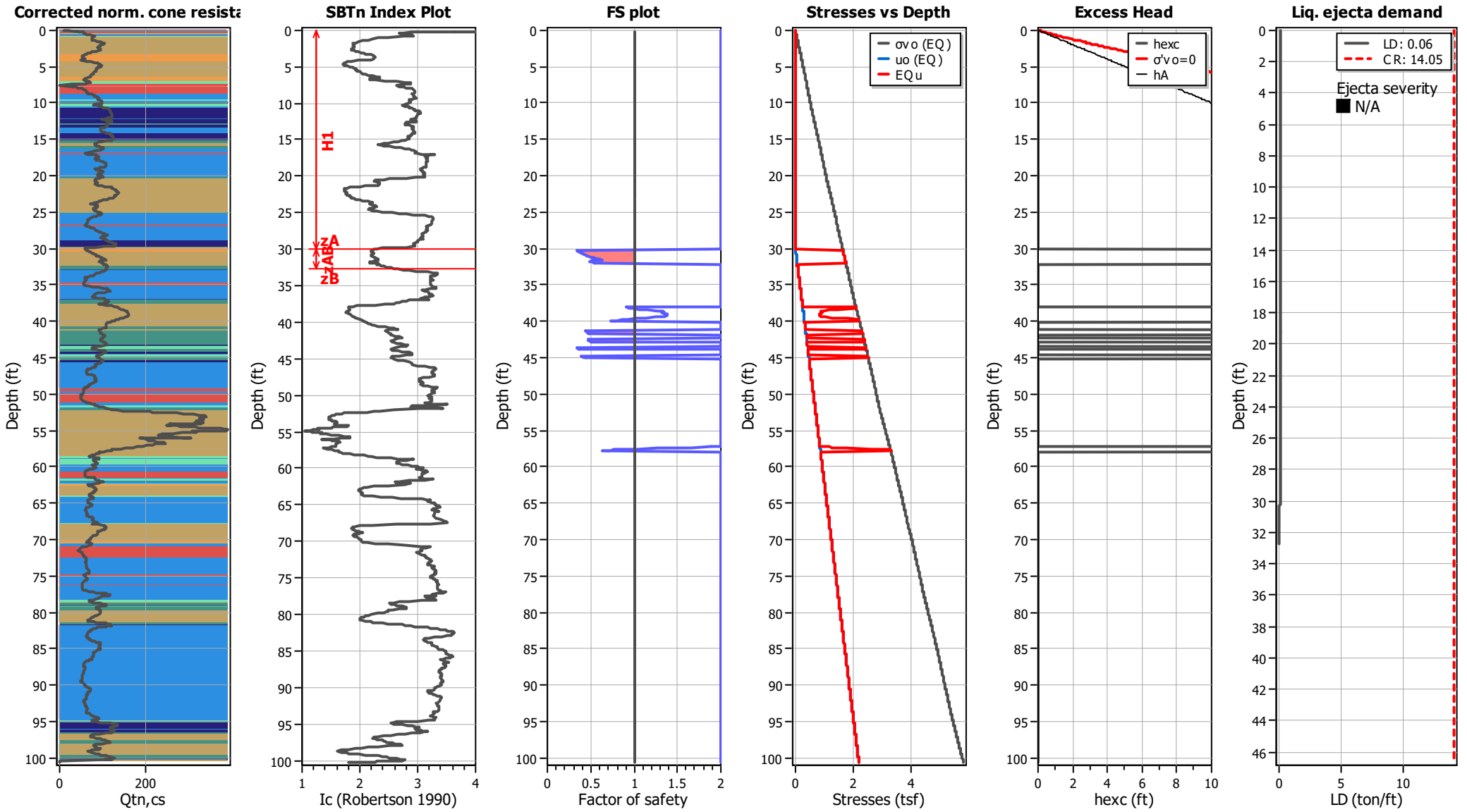
Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Aging Calculation Estimation

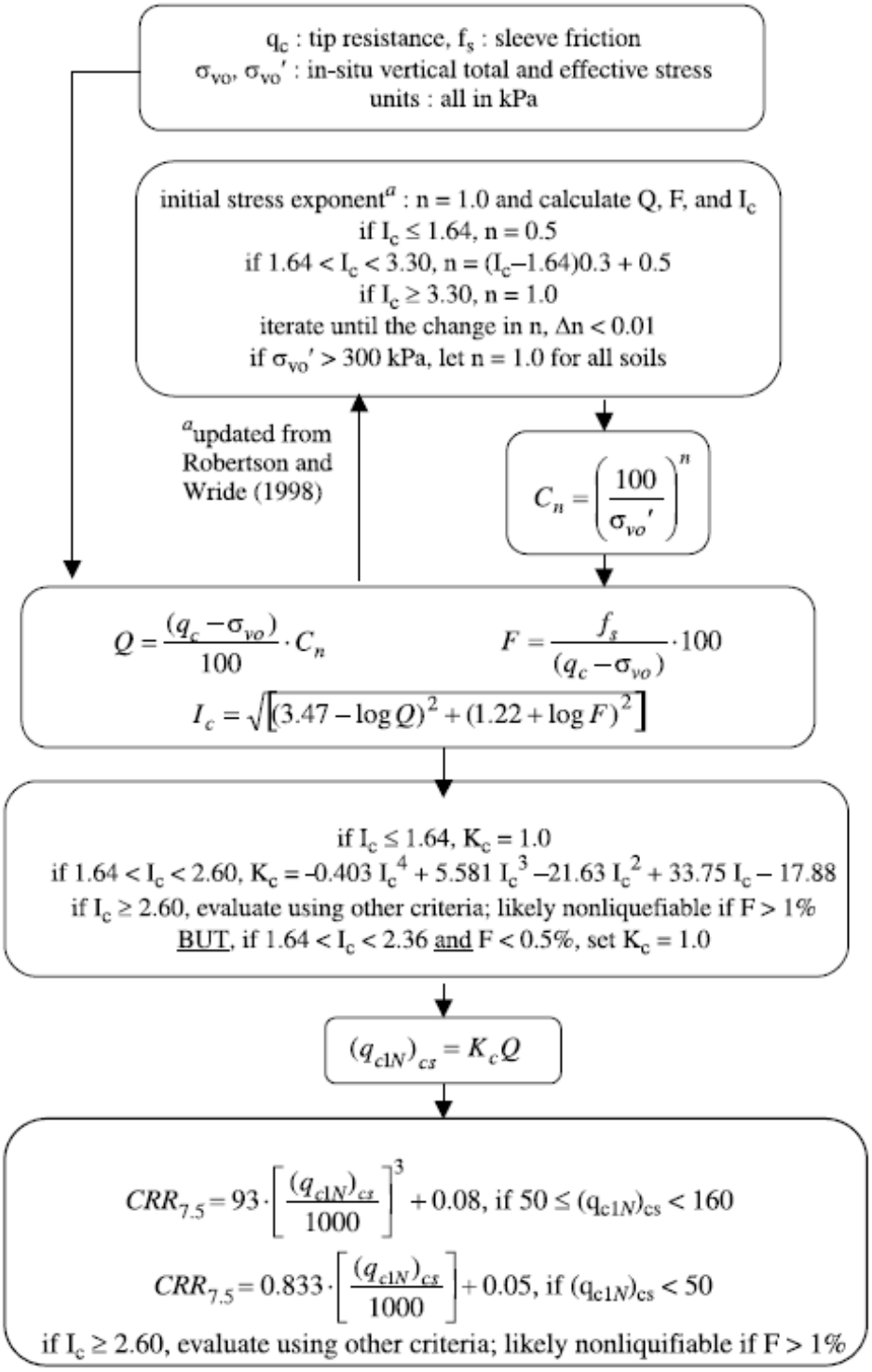


Ejecta Severity Estimation



Procedure for the evaluation of soil liquefaction resistance, NCEER (1998)

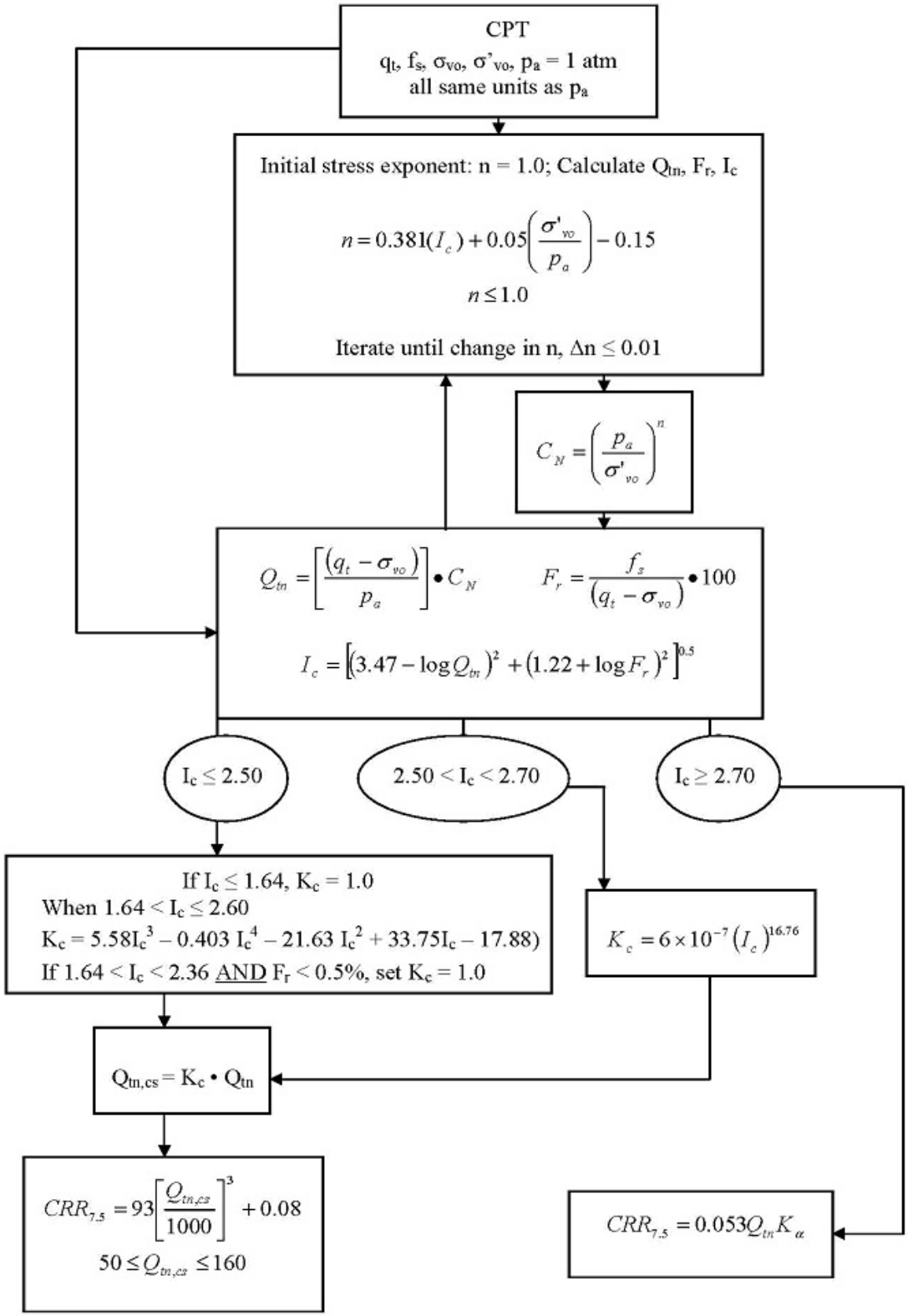
Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. The procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart[1]:



[1] "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

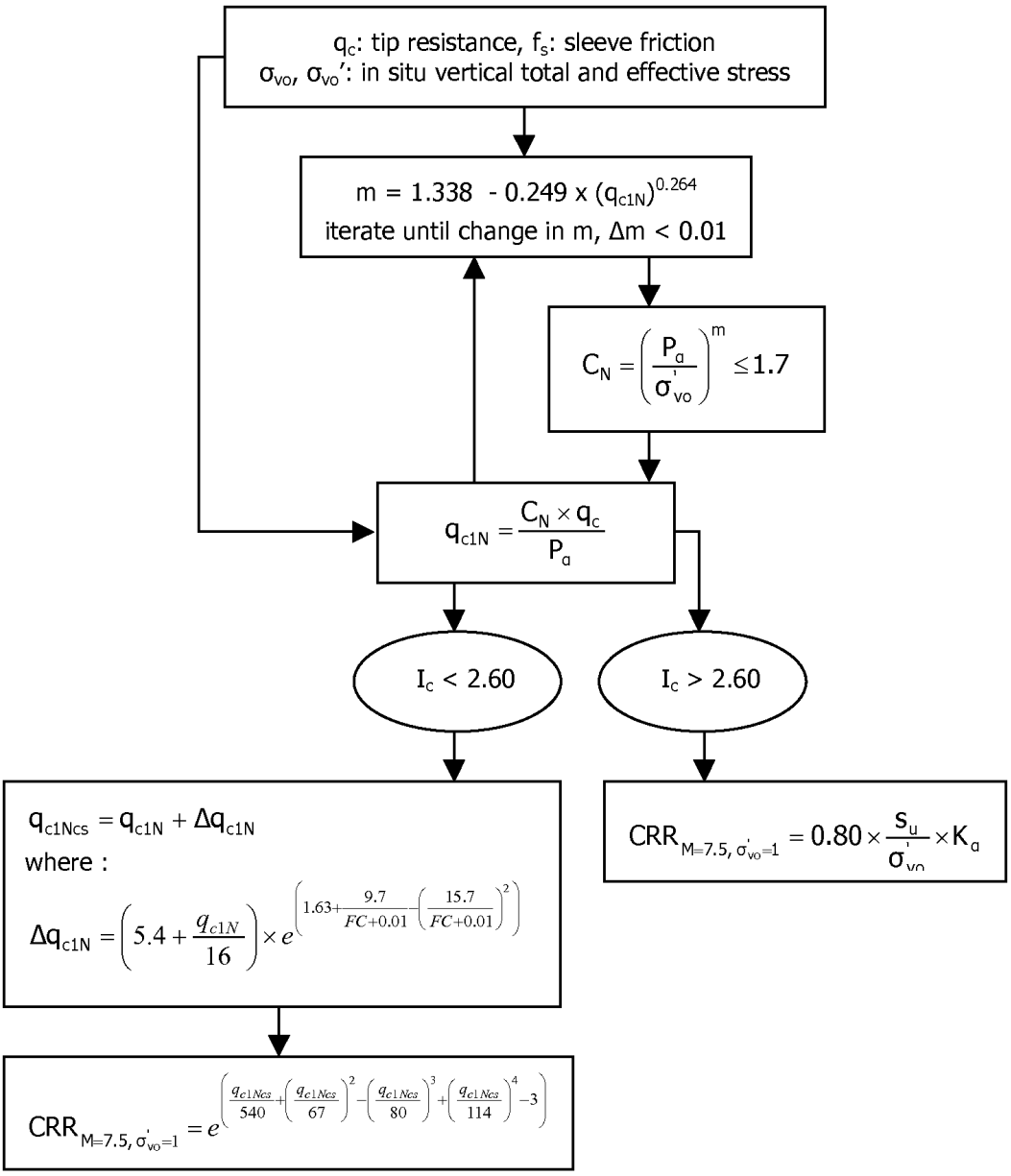
Procedure for the evaluation of soil liquefaction resistance (all soils), Robertson (2010)

Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. This procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart[1]:

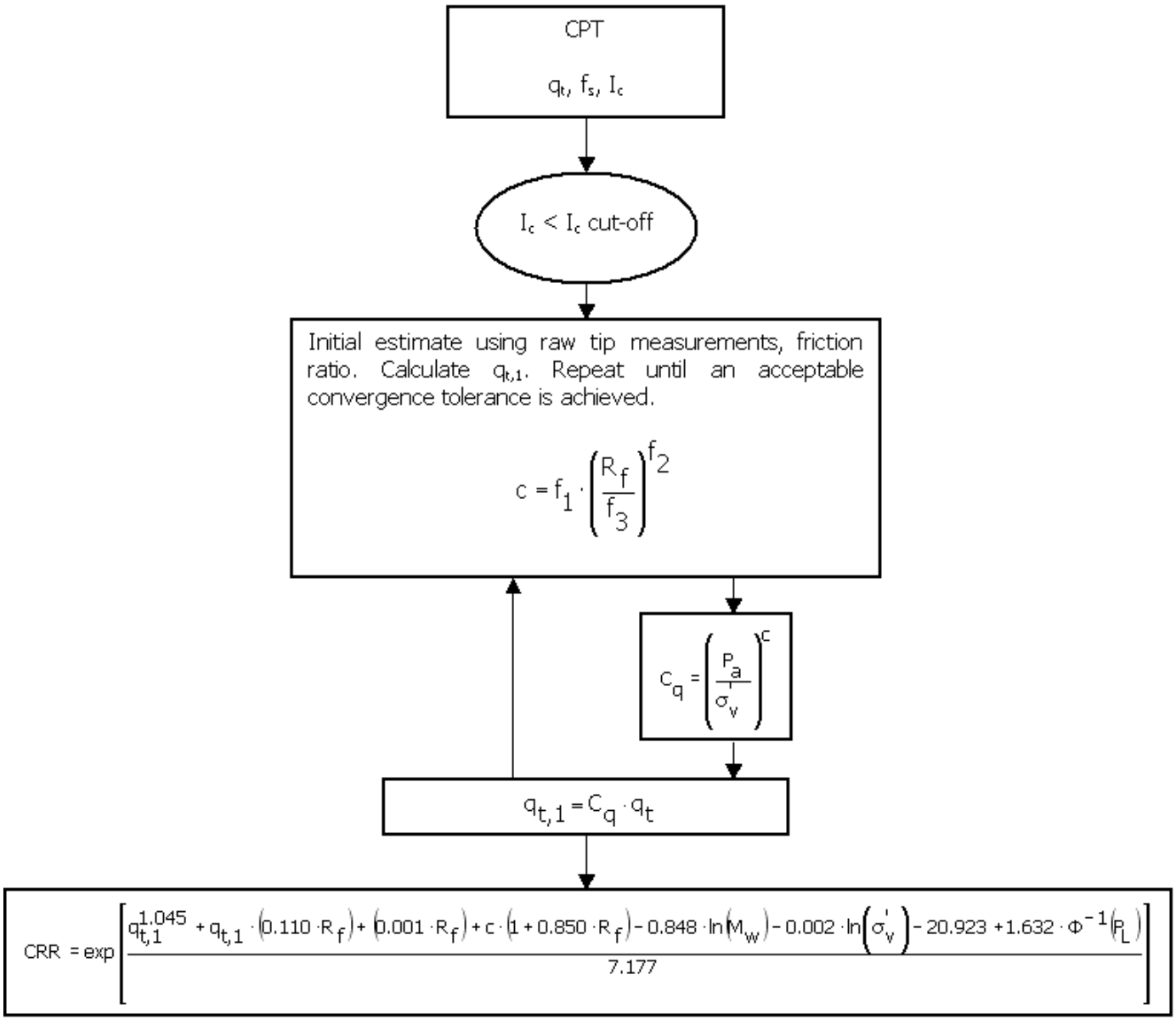


[1] P.K. Robertson, 2009. "Performance based earthquake design using the CPT", Keynote Lecture, International Conference on Performance-based Design in Earthquake Geotechnical Engineering – from case history to practice, IS-Tokyo, June 2009

Procedure for the evaluation of soil liquefaction resistance, Idriss & Boulanger (2008)



Procedure for the evaluation of soil liquefaction resistance (sandy soils), Moss et al. (2006)



Procedure for the evaluation of soil liquefaction resistance, Boulanger & Idriss(2014)

$$FS_{liq} = \frac{CRR_{M=7.5,\sigma'_v=1atm}}{CSR_{M=7.5,\sigma'_v=1atm}}$$

$$CSR_{M=7.5,\sigma'_v=1atm} = 0.65 \frac{\sigma_v}{\sigma'_v} \frac{a_{max}}{g} r_d \frac{1}{MSF} \frac{1}{K_\sigma}$$

$$r_d = \exp\left[\alpha(z) + \beta(z) \cdot M\right]$$

$$\alpha(z) = -1.012 - 1.126 \sin\left(\frac{z}{11.73} + 5.133\right)$$

$$\beta(z) = 0.106 + 0.118 \sin\left(\frac{z}{11.28} + 5.142\right)$$

$$K_\sigma = 1 - C_\sigma \ln\left(\frac{\sigma'_v}{P_a}\right) \le 1.1$$

$$C_\sigma = \frac{1}{37.3 - 8.27\left(q_{c1Ncs}\right)^{0.264}} \le 0.3$$

$$MSF = 1 + \left(MSF_{max} - 1\right)\left(8.64 \exp\left(\frac{-M}{4}\right) - 1.325\right)$$

$$MSF_{max} = 1.09 + \left(\frac{q_{C1Ncs}}{180}\right)^3 \le 2.2$$

σ'_v *and* σ_v *at start of earthquake shaking*

$$CRR_{M=7.5,\sigma'_v=1atm} = \exp\left(\frac{q_{c1Ncs}}{113} + \left(\frac{q_{c1Ncs}}{1000}\right)^2 - \left(\frac{q_{c1Ncs}}{140}\right)^3 + \left(\frac{q_{c1Ncs}}{137}\right)^4 - 2.80\right)$$

$$q_{c1Ncs} = q_{c1N} + \Delta q_{c1N}$$

$$\Delta q_{c1N} = \left(11.9 + \frac{q_{c1N}}{14.6}\right) \exp\left(1.63 - \frac{9.7}{FC+2} - \left(\frac{15.7}{FC+2}\right)^2\right)$$

$$q_{c1N} = C_{Ne} \frac{q_c}{P_a}$$

$$C_{Ne} = \left(\frac{P_a}{\sigma'_v}\right)^m \le 1.7$$

$$m = 1.338 - 0.249\left(q_{c1Ncs}\right)^{0.264} \quad with \quad 0.264 \le m \le 0.782$$

$$FC = 80\left(I_C + C_{FC}\right) - 137 \quad with \quad 0\% \le FC \le 100\%$$

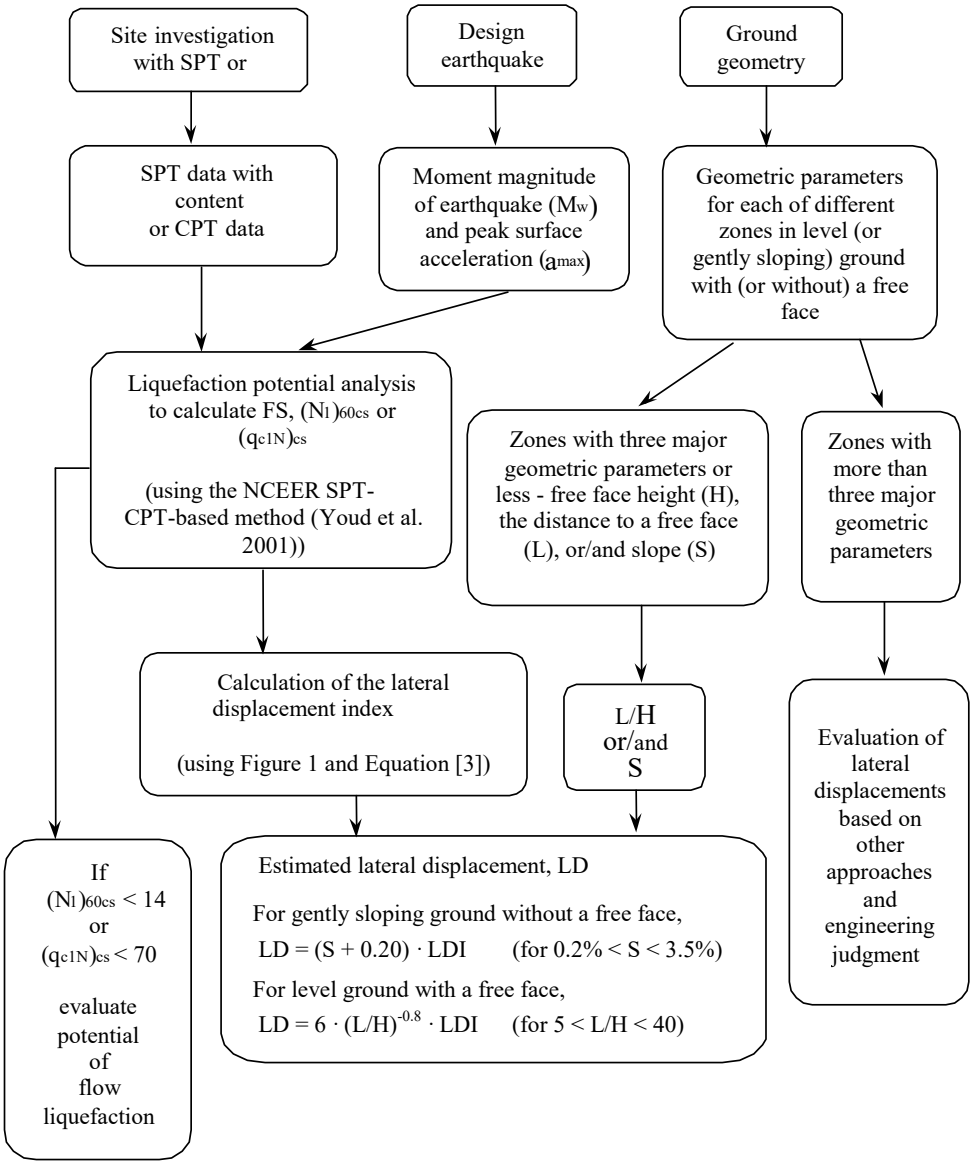
$$I_c = \left[\left(3.47 - \log\left(Q\right)\right)^2 + \left(1.22 + \log\left(F\right)\right)^2\right]^{0.5}$$

$$Q = \left(\frac{q_c - \sigma_{vc}}{P_a}\right)\left(\frac{P_a}{\sigma'_{vc}}\right)^n \; with \; 0.5 \le n \le 1.0 \; per \; Robertson \; \& \; Wride \; (1998)$$

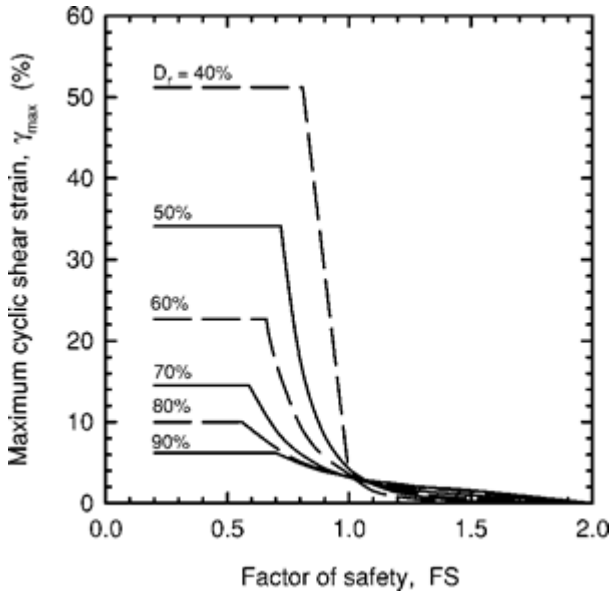
$$F = \left(\frac{f_s}{q_c - \sigma_{vc}}\right) \cdot 100\%$$

σ'_v *at time of CPT sounding*

Procedure for the evaluation of liquefaction-induced lateral spreading displacements



[1] Flow chart illustrating major steps in estimating liquefaction-induced lateral spreading displacements using the proposed approach



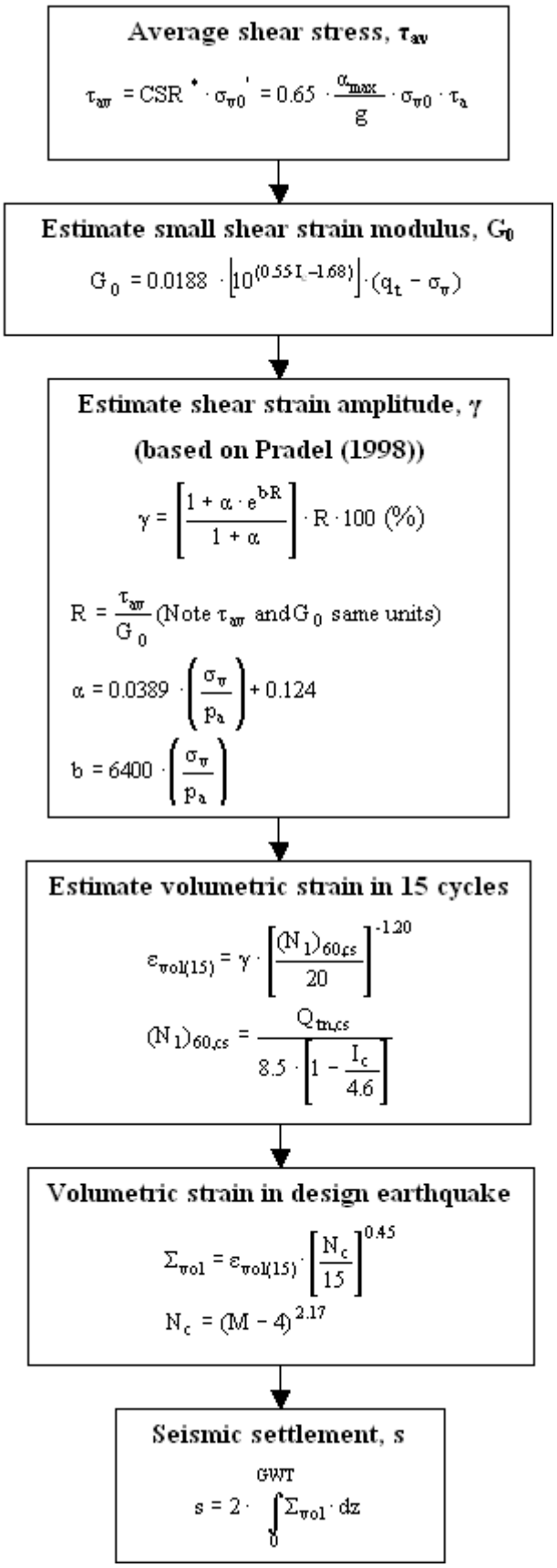
[1] Figure 1

$$LDI = \int_0^{z_{max}} \gamma_{max} dz$$

[1] Equation [3]

[1] "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

Procedure for the estimation of seismic induced settlements in dry sands



Robertson, P.K. and Lisheng, S., 2010, "Estimation of seismic compression in dry soils using the CPT" FIFTH INTERNATIONAL CONFERENCE ON RECENT ADVANCES IN GEOTECHNICAL EARTHQUAKE ENGINEERING AND SOIL DYNAMICS, Symposium in honor of professor I. M. Idriss, San Diego, CA

Liquefaction Potential Index (LPI) calculation procedure

Calculation of the Liquefaction Potential Index (LPI) is used to interpret the liquefaction assessment calculations in terms of severity over depth. The calculation procedure is based on the methology developed by Iwasaki (1982) and is adopted by AFPS.

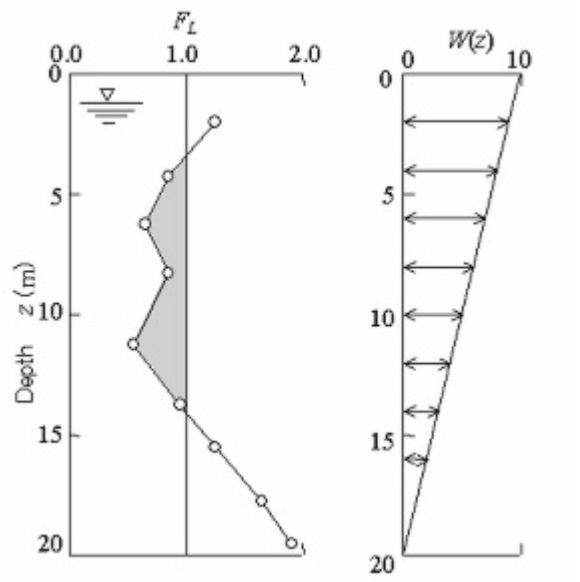
To estimate the severity of liquefaction extent at a given site, LPI is calculated based on the following equation:

$$\mathbf{LPI} = \int_0^{20} (10 - 0{,}5z) \times F_L \times dz$$

where:
F_L = 1 - F.S. when F.S. less than 1
F_L = 0 when F.S. greater than 1
z depth of measurment in meters

Values of LPI range between zero (0) when no test point is characterized as liquefiable and 100 when all points are characterized as susceptible to liquefaction. Iwasaki proposed four (4) discrete categories based on the numeric value of LPI:

- LPI = 0 : Liquefaction risk is very low
- 0 < LPI <= 5 : Liquefaction risk is low
- 5 < LPI <= 15 : Liquefaction risk is high
- LPI > 15 : Liquefaction risk is very high



Graphical presentation of the LPI calculation procedure

Shear-Induced Building Settlement (Ds) calculation procedure

The shear-induced building settlement (Ds) due to liquefaction below the building can be estimated using the relationship developed by Bray and Macedo (2017):

$$Ln(Ds) = c1 + c2 * LBS + 0.58 * Ln\left(Tanh\left(\frac{HL}{6}\right)\right) + 4.59 * Ln(Q) - 0.42 * Ln(Q)^2 - 0.02 * B + 0.84 * Ln(CAVdp) + 0.41 * Ln(Sa1) + \varepsilon$$

where Ds is in the units of mm, c1= -8.35 and c2= 0.072 for LBS ≤ 16, and c1= -7.48 and c2= 0.014 otherwise. Q is the building contact pressure in units of kPa, HL is the cumulative thickness of the liquefiable layers in the units of m, B is the building width in the units of m, CAVdp is a standardized version of the cumulative absolute velocity in the units of g-s, Sa1 is 5%-damped pseudo-acceleration response spectral value at a period of 1 s in the units of g, and ε is a normal random variable with zero mean and 0.50 standard deviation in Ln units. The liquefaction-induced building settlement index (LBS) is:

$$LBS = \sum W * \frac{\varepsilon_{shear}}{z} dz$$

where z (m) is the depth measured from the ground surface > 0, W is a foundation-weighting factor wherein W = 0.0 for z less than Df, which is the embedment depth of the foundation, and W = 1.0 otherwise. The shear strain parameter (ε_shear) is the liquefaction-induced free-field shear strain (in %) estimated using Zhang et al. (2004). It is calculated based on the estimated Dr of the liquefied soil layer and the calculated safety factor against liquefaction triggering (FSL).

References

- Lunne, T., Robertson, P.K., and Powell, J.J.M 1997. Cone penetration testing in geotechnical practice, E & FN Spon Routledge, 352 p, ISBN 0-7514-0393-8.
- Boulanger, R.W. and Idriss, I. M., 2007. Evaluation of Cyclic Softening in Silts and Clays. ASCE Journal of Geotechnical and Geoenvironmental Engineering June, Vol. 133, No. 6 pp 641-652
- Boulanger, R.W. and Idriss, I. M., 2014. CPT AND SPT BASED LIQUEFACTION TRIGGERING PROCEDURES. DEPARTMENT OF CIVIL & ENVIRONMENTAL ENGINEERING COLLEGE OF ENGINEERING UNIVERSITY OF CALIFORNIA AT DAVIS
- Robertson, P.K. and Cabal, K.L., 2007, Guide to Cone Penetration Testing for Geotechnical Engineering. Available at no cost at http://www.geologismiki.gr/
- Robertson, P.K. 1990. Soil classification using the cone penetration test. Canadian Geotechnical Journal, 27 (1), 151-8.
- Robertson, P.K. and Wride, C.E., 1998. Cyclic Liquefaction and its Evaluation based on the CPT Canadian Geotechnical Journal, 1998, Vol. 35, August.
- Youd, T.L., Idriss, I.M., Andrus, R.D., Arango, I., Castro, G., Christian, J.T., Dobry, R., Finn, W.D.L., Harder, L.F., Hynes, M.E., Ishihara, K., Koester, J., Liao, S., Marcuson III, W.F., Martin, G.R., Mitchell, J.K., Moriwaki, Y., Power, M.S., Robertson, P.K., Seed, R., and Stokoe, K.H., Liquefaction Resistance of Soils: Summary Report from the 1996 NCEER and 1998 NCEER/NSF Workshop on Evaluation of Liquefaction Resistance of Soils, ASCE, Journal of Geotechnical & Geoenvironmental Engineering, Vol. 127, October, pp 817-833
- Zhang, G., Robertson. P.K., Brachman, R., 2002, Estimating Liquefaction Induced Ground Settlements from the CPT, Canadian Geotechnical Journal, 39: pp 1168-1180
- Zhang, G., Robertson. P.K., Brachman, R., 2004, Estimating Liquefaction Induced Lateral Displacements using the SPT and CPT, ASCE, Journal of Geotechnical & Geoenvironmental Engineering, Vol. 130, No. 8, 861-871
- Pradel, D., 1998, Procedure to Evaluate Earthquake-Induced Settlements in Dry Sandy Soils, ASCE, Journal of Geotechnical & Geoenvironmental Engineering, Vol. 124, No. 4, 364-368
- Iwasaki, T., 1986, Soil liquefaction studies in Japan: state-of-the-art, Soil Dynamics and Earthquake Engineering, Vol. 5, No. 1, 2-70
- Papathanassiou G., 2008, LPI-based approach for calibrating the severity of liquefaction-induced failures and for assessing the probability of liquefaction surface evidence, Eng. Geol. 96:94–104
- P.K. Robertson, 2009, Interpretation of Cone Penetration Tests - a unified approach., Canadian Geotechnical Journal, Vol. 46, No. 11, pp 1337-1355
- P.K. Robertson, 2009. "Performance based earthquake design using the CPT", Keynote Lecture, International Conference on Performance-based Design in Earthquake Geotechnical Engineering - from case history to practice, IS-Tokyo, June 2009
- Robertson, P.K. and Lisheng, S., 2010, "Estimation of seismic compression in dry soils using the CPT" FIFTH INTERNATIONAL CONFERENCE ON RECENT ADVANCES IN GEOTECHNICAL EARTHQUAKE ENGINEERING AND SOIL DYNAMICS, *Symposium in honor of professor I. M. Idriss,* SAN diego, CA
- R. E. S. Moss, R. B. Seed, R. E. Kayen, J. P. Stewart, A. Der Kiureghian, K. O. Cetin, CPT-Based Probabilistic and Deterministic Assessment of In Situ Seismic Soil Liquefaction Potential, Journal of Geotechnical and Geoenvironmental Engineering, Vol. 132, No. 8, August 1, 2006
- I. M. Idriss and R. W. Boulanger, 2008. Soil liquefaction during earthquakes, Earthquake Engineering Research Institute MNO-12
- Jonathan D. Bray & Jorge Macedo, Department of Civil & Environmental Engineering, Univ. of California, Berkeley, CA, USA, Simplified procedure for estimating liquefaction-induced building settlement, *Proceedings of the 19th International Conference on Soil Mechanics and Geotechnical Engineering, Seoul 201*

Attachment 2

WIHMP Criteria and Opportunities (NOC Only)

Stormwater Requirements
INSERT PROJECT FILE NO. HERE

A WIHMP is not applicable for this project.

Attachment 3

Additional DMA and BMP Summary Tables

Table 15-1 DMA Summary

DMA ID	Total Area	Imperviousness	DCV
	ac	%	ac-ft
Phase 1 – DMA 1, Behavioral Health	0.289	100%	0.02
Phase 1 – DMA 2, Kitchen	0.096	100%	0.01
Phase 1 – DMA 3, Vocation	0.253	100%	0.01
Phase 1 – DMA 4, Duplex	0.278	100%	0.02
Phase 1 – DMA 5, Triplex	0.273	100%	0.02
Phase 1 – DMA 6, Site	5.382	20%	0.10
Phase 2A – DMA 1, Long-Term Housing	1.409	65%	0.06
Phase 2B – DMA 1, Independent Living	1.083	75%	0.05

Table 15-2 BMP Summary

BMP ID	Infiltration Feasibility			Associated DMA(s)	Total DCV
	Full	Partial	No Infiltration	-	ac-ft
BH	☐	☐	☒	Phase 1 – DMA 1, Behavioral Health	0.02
K	☐	☐	☒	Phase 1 – DMA 2, Kitchen	0.01
V	☐	☐	☒	Phase 1 – DMA 3, Vocation	0.01
D	☐	☐	☒	Phase 1 – DMA 4, Duplex	0.02
T	☐	☐	☒	Phase 1 – DMA 5, Triplex	0.02
LTH	☐	☐	☒	Phase 2A – DMA 1, Long-Term Housing	0.234
IL	☐	☐	☒	Phase 2B – DMA 1, Independent Living	0.201
	☐	☐	☐		
	☐	☐	☐		
	☐	☐	☐	

Attachment 4

DCV Calculations

PHASE 1 – DCV CALCULATIONS

Building: Transitional Living & Behavioral Health

Site info:

$$Total\ Building\ Area = 12{,}600\ sq.ft\ (0.29\ acres)$$

$$\%\ Impervious = 100\%$$

Simple DCV:

$$C = (0.75)(imp) + 0.15 = (0.75)(1.0) + 0.15 = 0.90$$

$$V = (C)(d)(A)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right)$$

$$V = (0.90)(0.75\ in.)(0.29\ acres)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right) = 708.75\ ft^3$$

BMP ID	Planter Height (ft)	Planter Area (sq.ft)	Volume(cu.ft)
BH1	3	115	345
BH2	3	115	345
BH3	3	120	360
		TOTAL:	1050

Building: Kitchen

Site info:

$$Total\ Building\ Area = 4{,}200\ sq.ft\ (0.10\ acres)$$

$$\%\ Impervious = 100\%$$

Simple DCV:

$$C = (0.75)(imp) + 0.15 = (0.75)(1.0) + 0.15 = 0.90$$

$$V = (C)(d)(A)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right)$$

$$V = (0.90)(0.75\ in.)(0.10\ acres)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right) = 236.25\ ft^3$$

BMP ID	Planter Height (ft)	Planter Area (sq.ft)	Volume(cu.ft)
1	4	60	240
		TOTAL:	240

Building: Education & Vocational Education

Site info:

$$Total\ Building\ Area = 11{,}000\ sq.ft\ (0.25\ acres)$$

$$\%\ Impervious = 100\%$$

Simple DCV:

$$C = (0.75)(imp) + 0.15 = (0.75)(1.0) + 0.15 = 0.90$$

$$V = (C)(d)(A)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right)$$

$$V = (0.90)(0.75\ in.)(0.25\ acres)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right) = 618.75\ ft^3$$

BMP ID	Planter Height (ft)	Planter Area (sq.ft)	Volume(cu.ft)
V1	3	96	288
V2	3	144	432
V3	3	48	144
		TOTAL:	864

Building: Duplex Housing

Site info:

$$Total\ Building\ Area = 12{,}100\ sq.ft\ (0.28\ acres)$$

$$\%\ Impervious = 100\%$$

Simple DCV:

$$C = (0.75)(imp) + 0.15 = (0.75)(1.0) + 0.15 = 0.90$$

$$V = (C)(d)(A)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right)$$

$$V = (0.90)(0.75\ in.)(0.28\ acres)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right) = 680.63\ ft^3$$

BMP ID	Planter Height (ft)	Planter Area (sq.ft)	Volume(cu.ft)
D1	3	50	150
D2	3	49	147
D3	3	49	147
D4	3	50	150
D5	3	48	144
D6	3	48	144
		TOTAL:	882

Building: Triplex Housing

Site info:

$$Total\ Building\ Area = 19{,}000\ sq.ft\ (0.44\ acres)$$

$$\%\ Impervious = 100\%$$

Simple DCV:

$$C = (0.75)(imp) + 0.15 = (0.75)(1.0) + 0.15 = 0.90$$

$$V = (C)(d)(A)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right)$$

$$V = (0.90)(0.75\ in.)(0.44\ acres)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right) = 1{,}068.75\ ft^3$$

BMP ID	Planter Height (ft)	Planter Area (sq.ft)	Volume(cu.ft)
T1	3	28	84
T2	3	24	72
T3	3	40	119
T4	3	42	125
T5	3	24	72
T6	3	49	147
T7	3	70	210
T8	3	67	201
T9	3	66	198
T10	3	67	201
T11	3	71	213
		TOTAL:	1,428

Building: Remaining Site

Site info:

$$Total\ Area = 234{,}447.9\ sq.ft\ (5.38\ acres)$$

$$\%\ Impervious = 20\%$$

Simple DCV:

$$C = (0.75)(imp) + 0.15 = (0.75)(0.20) + 0.15 = 0.30$$

$$V = (C)(d)(A)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right)$$

$$V = (0.30)(0.75\ in.)(5.38\ acres)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right) = 4{,}395.7\ ft^3$$

PHASE 2 – DCV CALCULATIONS

Phase 2A													
Drainage Area Name / DMA	**BMP ID, Feature or Land Use Type**	**Total Drainage Area (ft^2)**	**Total Drainage Area (acres)**	**Total Pervious Area (ft^2)**	**Calculated % impervious**	**Assumed % impervious**	**Runoff Coefficient**	**Design Storm Depth (in)**	**Average or Estimated Tc (min)**	**Rainfall Intensity (in/hr)**	**Simple Method DCV (ft^3)**	**Q_{Design} (cfs)**	**Acre-Feet (ac-ft)**
Phase 2A – DMA 1	Long-Term Housing	61,381.8	1.409	22,140.3	63.9%	65%	0.638	0.8	5	0.26	**2,610.5**	**0.234**	**0.060**

Phase 2B													
Drainage Area Name / DMA	**BMP ID, Feature or Land Use Type**	**Total Drainage Area (ft^2)**	**Total Drainage Area (acres)**	**Total Pervious Area (ft^2)**	**Calculated % impervious**	**Assumed % impervious**	**Runoff Coefficient**	**Design Storm Depth (in)**	**Average or Estimated Tc (min)**	**Rainfall Intensity (in/hr)**	**Simple Method DCV (ft^3)**	**Q_{Design} (cfs)**	**Acre-Feet (ac-ft)**
Phase 2B – DMA 1	Independent Living	47,190.7	1.083	12,299.8	73.9%	75%	0.713	0.8	5	0.26	**2,242.4**	**0.201**	**0.051**

Attachment 5

Supplementary Infiltration Investigation Report

Attachment 6

Additional Infiltration and Harvest and Use Feasibility Tables

Stormwater Requirements
INSERT PROJECT FILE NO. HERE

BMP ID	Infiltration Feasibility			Harvest and Use Feasibility		
	Full	Partial	No Infiltration	Feasible	Not Feasible	NA
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐
	☐	☐	☐	☐	☐	☐

Attachment 7

Priority Project BMP Conformance Analysis Tables

NOC PRIORITY PROJECT BMP CONFORMANCE ANALYSIS

DMA ID:	**DCV =**	0 ac-ft

Hydrologic Source Controls

Included	Site Design BMP	Fact Sheet	DCV Reduction
☐	Localized On-Lot Infiltration[4]	HSC-1	0 ac-ft
☐	Impervious Area Dispersion[5]	HSC-2	0 ac-ft
☐	Street Trees[6]	HSC-3	0 ac-ft
☐	Residential Rain Barrels (Not Actively Managed)	HSC-4	0 ac-ft
☐	Amended Soils Over Tight Underlying Soils[7]	MISC-2	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	HSCs will not be implemented, as selected LID BMPs will sufficiently treat the DCV for this DMA.	-	0 ac-ft
		Total DCV Reduction =	**0 ac-ft**
		Remaining DCV = DCV – Total DCV Reduction =	**0 ac-ft**

Check only one of the two boxes below:

☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the hydrologic source controls checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable. The conformance analysis for this DMA is complete, and the rest of this table can remain blank.
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by hydrologic source controls. Additional BMPs are necessary and will be implemented. The conformance analysis for this DMA continues below.

Low Impact Development BMPs | Infiltration

Included	Site Design BMP	Fact Sheet	DCV Reduction
☐	Infiltration Basin[8]	INF-1	0 ac-ft
☐	Infiltration Trench[9]	INF-2	0 ac-ft
☐	Bioretention with no Underdrain[10]	INF-3	0 ac-ft
☐	Bioinfiltration with Raised Underdrain	INF-4	0 ac-ft
☐	Drywell[11]	INF-5	0 ac-ft

[4] Also known as Downspout Infiltration, Retention Grading, French Drains, or On-Lot Rain Gardens.
[5] Also known as Downspout Dispersion, Downspout Disconnection, Impervious Area Disconnection, or Sheet Flow Dispersion.
[6] Also known as Canopy Interception.
[7] No DCV Reduction credit is allowed for amended soils alone. Amended soils must be used as part of HSC-2 – Impervious Area Dispersion, and to increase the retention volume of Infiltration and Biotreatment BMPs.
[8] Also known as Recharge Basin or Infiltration Pond.
[9] Also known as French Drain, Rock Trench, Exfiltration trench, Soak-Aways or Soakage Trench.
[10] Also known as Rain Garden or Infiltration Planter.
[11] Also known as Soak-Away Pits, Infiltration Sumps, Rock Sumps, or Underground Injection Controls. Calculations for determining DCV reduction provided by drywells is highly site-specific. No template is

☐	Permeable Pavement[12]	INF-6	0 ac-ft
☐	Underground Infiltration[13]	INF-7	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
	Total DCV Reduction =		0 **ac-ft**
	Remaining DCV = DCV –Total DCV Reduction =		0 **ac-ft**
Check only one of the two boxes below:			
☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the infiltration LID BMP(s) checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable. The conformance analysis for this DMA is complete, and the rest of this table can remain blank.		
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by infiltration LID BMPs. Additional BMPs are necessary and will be implemented. The conformance analysis for this DMA continues below.		
Low Impact Development BMPs | Harvest and Use			
Included	Site Design BMP	Fact Sheet	DCV Reduction
☐	Above-Ground Cisterns and Rain Barrels	HU-1	0 ac-ft
☐	Underground Detention[14]	HU-2	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
	Total DCV Reduction =		0 **ac-ft**
	Remaining DCV = DCV –Total DCV Reduction =		0 **ac-ft**
Check only one of the two boxes below:			
☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the harvest and use LID BMP(s) checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable. The conformance analysis for this DMA is complete, and the rest of this table can remain blank.		
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by harvest and use LID BMPs. Additional BMPs are necessary and will be implemented. The conformance analysis for this DMA continues below.		

provided. Drywells must be designed to ensure a drawdown time of 48 hours. Calculations for DCV reduction are to be provided as **Attachment 8**.

[12] Also known as Pervious Pavement, Porous Concrete, Pavers, or Permeable Asphalt.

[13] Also known as Subsurface Infiltration Galleries, Infiltration Vault, or Recharge Vault. For underground infiltration devices with open pore volume (e.g. vaults, crates, pipe sections, etc.), refer to the Infiltration Basin BMP Template. For underground infiltration devices with pore space (e.g. aggregate reservoirs), refer to the permeable Pavement BMP Template.

[14] Refer to the Above-Ground Cisterns and Rain Barrels calculation template.

Low Impact Development BMPs | Evapotranspiration			
Included	Site Design BMP	Fact Sheet	DCV Reduction
☐	Green Roof / Brown Roof	HSC-5	0 ac-ft
☐	Blue Roof	HSC-6	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
	Total DCV Reduction =		0 **ac-ft**
	Remaining DCV = DCV –Total DCV Reduction =		0 **ac-ft**
Check only one of the two boxes below:			
☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the evapotranspiration LID BMP(s) checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable. The conformance analysis for this DMA is complete, and the rest of this table can remain blank.		
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by evapotranspiration LID BMPs. Additional BMPs are necessary and will be implemented. The conformance analysis for this DMA continues below.		

Low Impact Development BMPs | Biotreatment			
Included	Site Design BMP	Fact Sheet	DCV Reduction
☐	Bioretention with Underdrains[15]	BIO-1	0 ac-ft
☐	Vegetated Swale[16]	BIO-2	0 ac-ft
☐	Vegetated Filter Strip[17]	BIO-3	0 ac-ft
☐	Wet Detention Basin[18]	BIO-4	0 ac-ft
☐	Constructed Wetlands[19]	BIO-5	0 ac-ft
☐	Dry Extended Detention Basin[20]	BIO-6	0 ac-ft
☐	Proprietary Biotreatment[21]	BIO-7	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
	Total DCV Reduction =		0 **ac-ft**
	Remaining DCV = DCV –Total DCV Reduction =		0 **ac-ft**

[15] Also known as Rain Gardens with Underdrains, Vegetated Media Filter, or Downspout Planter Boxes.
[16] Also known as Bioswale, Biofiltration Swale, or Grass Swale.
[17] Also known as Buffer Strip or Vegetated Buffer.
[18] Also known as Wet Ponds or Retention Ponds. A calculation template is not provided for wet detention basins. If implemented, calculations are required to be included in **Attachment 8**.
[19] Also known as Stormwater Wetlands, Wetland Basins, or Treatment Wetland. A calculation template is not provided for Constructed Wetlands. If implemented, calculates are required to be included in **Attachment 8**.
[20] Also known as Dry Ponds or Detention Ponds.
[21] Also known as Catch Basin Planter Box, Bioretention Vault, or Tree Box Filter. A calculation template is not provided for Proprietary Biotreatment. If implemented, calculations are required to be included in **Attachment 8**.

Check only one of the two boxes below:	
☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the biotreatment LID BMP(s) checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable. The conformance analysis for this DMA is complete, and the rest of this table can remain blank.
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by biotreatment LID BMPs. Additional BMPs are necessary and will be implemented. The conformance analysis for this DMA continues below.

Treatment Control BMPs

Treatment Control BMPs can only be considered if the BMP Conformance Analysis indicates that it is not feasible to retain the full design capture volume with LID BMPs.

Included	Site Design BMP	Fact Sheet	DCV Reduction
☐	Sand Filter[22]	TRT-1	0 ac-ft
☐	Cartridge Media Filter[23]	TRT-2	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
	Total DCV Reduction =		0 **ac-ft**
	Remaining DCV = DCV –Total DCV Reduction =		0 **ac-ft**

Check only one of the two boxes below:	
☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the treatment BMP(s) checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable. The conformance analysis for this DMA is complete, and the rest of this table can remain blank.
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by treatment control BMPs. Additional BMPs are necessary and will be implemented. The conformance analysis for this DMA continues below.

Regional/Sub-Regional LID BMPs

Off-site Regional/Sub-Regional LID BMPs can only be considered if the BMP Conformance Analysis indicates that it is not feasible to retain the full design capture volume with on-site LID BMPs and with Treatment Control BMPs. Describe regional/sub-regional LID BMPs in which the Project will participate. Refer to Section 7.II-2.4.3.2 of the Model WQMP.

INSERT DESCRIPTION HERE

DMA ID: INSERT DMA ID HERE	**Final Remaining DCV =**	0 ac-ft

[22] Also known as Bed Media Filter.
[23] Also known as Manufactured Media Filters.

SOC PRIORITY PROJECT BMP CONFORMANCE ANALYSIS

DMA ID: INSERT DMA ID HERE	**DCV =**	0 ac-ft

Hydrologic Source Controls

Included	Site Design BMP	Fact Sheet	DCV Reduction
☐	Localized On-Lot Infiltration[1]	HSC-1	0 ac-ft
☐	Impervious Area Dispersion[2]	HSC-2	0 ac-ft
☐	Street Trees[3]	HSC-3	0 ac-ft
☐	Residential Rain Barrels (Not Actively Managed)	HSC-4	0 ac-ft
☐	Amended Soils Over Tight Underlying Soils[4]	MISC-2	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	HSCs will not be implemented, as selected LID BMPs will sufficiently treat the DCV for this DMA.	-	0 ac-ft
		Total DCV Reduction =	**0 ac-ft**
		Remaining DCV = DCV – Total DCV Reduction =	**0 ac-ft**

Check only one of the two boxes below:

☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the hydrologic source controls checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable. The conformance analysis for this DMA is complete, and the rest of this table can remain blank.
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by hydrologic source controls. Additional BMPs are necessary and will be implemented. The conformance analysis for this DMA continues below.

Low Impact Development BMPs | Infiltration

Included	Site Design BMP	Fact Sheet	DCV Reduction
☐	Infiltration Basin[5]	INF-1	0 ac-ft
☐	Infiltration Trench[6]	INF-2	0 ac-ft
☐	Bioretention with no Underdrain[7]	INF-3	0 ac-ft
☐	Bioinfiltration with Raised Underdrain	INF-4	0 ac-ft
☐	Drywell[8]	INF-5	0 ac-ft

[1] Also known as Downspout Infiltration, Retention Grading, French Drains, or On-Lot Rain Gardens.
[2] Also known as Downspout Dispersion, Downspout Disconnection, Impervious Area Disconnection, or Sheet Flow Dispersion.
[3] Also known as Canopy Interception.
[4] No DCV Reduction credit is allowed for amended soils alone. Amended soils must be used as part of HSC-2 – Impervious Area Dispersion, and to increase the retention volume of Infiltration and Biotreatment BMPs.
[5] Also known as Recharge Basin or Infiltration Pond.
[6] Also known as French Drain, Rock Trench, Exfiltration trench, Soak-Aways or Soakage Trench.
[7] Also known as Rain Garden or Infiltration Planter.
[8] Also known as Soak-Away Pits, Infiltration Sumps, Rock Sumps, or Underground Injection Controls. Calculations for determining DCV reduction provided by drywells is highly site-specific. No template is

☐	Permeable Pavement[9]	INF-6	0 ac-ft
☐	Underground Infiltration[10]	INF-7	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
	Total DCV Reduction =		0 **ac-ft**
	Remaining DCV = DCV –Total DCV Reduction =		0 **ac-ft**
Check only one of the two boxes below:			
☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the infiltration LID BMP(s) checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable. The conformance analysis for this DMA is complete, and the rest of this table can remain blank.		
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by infiltration LID BMPs. Additional BMPs are necessary and will be implemented. The conformance analysis for this DMA continues below.		
Low Impact Development BMPs | Harvest and Use			
Included	Site Design BMP	Fact Sheet	DCV Reduction
☐	Above-Ground Cisterns and Rain Barrels	HU-1	0 ac-ft
☐	Underground Detention[11]	HU-2	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
	Total DCV Reduction =		0 **ac-ft**
	Remaining DCV = DCV –Total DCV Reduction =		0 **ac-ft**
Check only one of the two boxes below:			
☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the harvest and use LID BMP(s) checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable. The conformance analysis for this DMA is complete, and the rest of this table can remain blank.		
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by harvest and use LID BMPs. Additional BMPs are necessary and will be implemented. The conformance analysis for this DMA continues below.		

provided. Drywells must be designed to ensure a drawdown time of 48 hours. Calculations for DCV reduction are to be provided as **Attachment 8**.

[9] Also known as Pervious Pavement, Porous Concrete, Pavers, or Permeable Asphalt.

[10] Also known as Subsurface Infiltration Galleries, Infiltration Vault, or Recharge Vault. For underground infiltration devices with open pore volume (e.g. vaults, crates, pipe sections, etc.), refer to the Infiltration Basin BMP Template. For underground infiltration devices with pore space (e.g. aggregate reservoirs), refer to the permeable Pavement BMP Template.

[11] Refer to the Above-Ground Cisterns and Rain Barrels calculation template.

Low Impact Development BMPs | Evapotranspiration			
Included	Site Design BMP	Fact Sheet	DCV Reduction
☐	Green Roof / Brown Roof	HSC-5	0 ac-ft
☐	Blue Roof	HSC-6	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
	Total DCV Reduction =		0 **ac-ft**
	Remaining DCV = DCV –Total DCV Reduction =		0 **ac-ft**
Check only one of the two boxes below:			
☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the evapotranspiration LID BMP(s) checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable. The conformance analysis for this DMA is complete, and the rest of this table can remain blank.		
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by evapotranspiration LID BMPs. Additional BMPs are necessary and will be implemented. The conformance analysis for this DMA continues below.		

Low Impact Development BMPs | Biotreatment			
Included	Site Design BMP	Fact Sheet	DCV Reduction
☐	Bioretention with Underdrains[12]	BIO-1	0 ac-ft
☐	Proprietary Biotreatment[13]	BIO-7	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
	Total DCV Reduction =		0 **ac-ft**
	Remaining DCV = DCV –Total DCV Reduction =		0 **ac-ft**
Check only one of the two boxes below:			
☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the biotreatment LID BMP(s) checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable. The conformance analysis for this DMA is complete, and the rest of this table can remain blank.		
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by biotreatment LID BMPs. Additional BMPs are necessary and will be implemented. The conformance analysis for this DMA continues below.		

[12] Also known as Rain Gardens with Underdrains, Vegetated Media Filter, or Downspout Planter Boxes.
[13] Also known as Catch Basin Planter Box, Bioretention Vault, or Tree Box Filter. A calculation template is not provided for Proprietary Biotreatment. If implemented, calculations are required to be included in **Attachment 8**.

Treatment Control BMPs			
Treatment Control BMPs can only be considered if the BMP Conformance Analysis indicates that it is not feasible to retain the full design capture volume with LID BMPs.			
Included	Site Design BMP	Fact Sheet	DCV Reduction
☐	Vegetated Swale[14]	BIO-2	0 ac-ft
☐	Vegetated Filter Strip[15]	BIO-3	0 ac-ft
☐	Wet Detention Basin[16]	BIO-4	0 ac-ft
☐	Constructed Wetlands[17]	BIO-5	0 ac-ft
☐	Dry Extended Detention Basin[18]	BIO-6	0 ac-ft
☐	Sand Filter[19]	TRT-1	0 ac-ft
☐	Cartridge Media Filter[20]	TRT-2	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
☐	Other: Insert Other Infiltration BMP Here	-	0 ac-ft
		Total DCV Reduction =	0 **ac-ft**
		Remaining DCV = DCV –Total DCV Reduction =	0 **ac-ft**
Check only one of the two boxes below:			
☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the treatment BMP(s) checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable. The conformance analysis for this DMA is complete, and the rest of this table can remain blank.		
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by treatment control BMPs. Additional BMPs are necessary and will be implemented. The conformance analysis for this DMA continues below.		

[14] Also known as Bioswale, Biofiltration Swale, or Grass Swale.
[15] Also known as Buffer Strip or Vegetated Buffer.
[16] Also known as Wet Ponds or Retention Ponds. A calculation template is not provided for wet detention basins. If implemented, calculations are required to be included in **Attachment 8**.
[17] Also known as Stormwater Wetlands, Wetland Basins, or Treatment Wetland. A calculation template is not provided for Constructed Wetlands. If implemented, calculates are required to be included in **Attachment 8**.
[18] Also known as Dry Ponds or Detention Ponds.
[19] Also known as Bed Media Filter.
[20] Also known as Manufactured Media Filters.

Regional/Sub-Regional LID BMPs		
Off-site Regional/Sub-Regional LID BMPs can only be considered if the BMP Conformance Analysis indicates that it is not feasible to retain the full design capture volume with on-site LID BMPs and with Treatment Control BMPs. Describe regional/sub-regional LID BMPs in which the Project will participate. Refer to Section 7.II-2.4.3.2 of the Model WQMP.		
INSERT DESCRIPTION HERE		
DMA ID: INSERT DMA ID HERE	**Final Remaining DCV =**	0 ac-ft

Attachment 8

DCV Reduction Calculations

PHASE 1 – DCV REDUCTION CALCULATIONS

Building: Transitional Living & Behavioral Health

Site info:

$$Total\ Building\ Area = 12{,}600\ sq.ft\ (0.29\ acres)$$

$$\%\ Impervious = 100\%$$

Simple DCV:

$$C = (0.75)(imp) + 0.15 = (0.75)(1.0) + 0.15 = 0.90$$

$$V = (C)(d)(A)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right)$$

$$V = (0.90)(0.75\ in.)(0.29\ acres)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right) = 708.75\ ft^3$$

BMP ID	Planter Height (ft)	Planter Area (sq.ft)	Volume(cu.ft)
BH1	3	115	345
BH2	3	115	345
BH3	3	120	360
		TOTAL:	1050

Building: Kitchen

Site info:

$$Total\ Building\ Area = 4{,}200\ sq.ft\ (0.10\ acres)$$

$$\%\ Impervious = 100\%$$

Simple DCV:

$$C = (0.75)(imp) + 0.15 = (0.75)(1.0) + 0.15 = 0.90$$

$$V = (C)(d)(A)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right)$$

$$V = (0.90)(0.75\ in.)(0.10\ acres)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right) = 236.25\ ft^3$$

BMP ID	Planter Height (ft)	Planter Area (sq.ft)	Volume(cu.ft)
1	4	60	240
		TOTAL:	240

Building: Education & Vocational Education

Site info:

$$Total\ Building\ Area = 11{,}000\ sq.ft\ (0.25\ acres)$$

$$\%\ Impervious = 100\%$$

Simple DCV:

$$C = (0.75)(imp) + 0.15 = (0.75)(1.0) + 0.15 = 0.90$$

$$V = (C)(d)(A)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right)$$

$$V = (0.90)(0.75\ in.)(0.25\ acres)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right) = 618.75\ ft^3$$

BMP ID	Planter Height (ft)	Planter Area (sq.ft)	Volume(cu.ft)
V1	3	96	288
V2	3	144	432
V3	3	48	144
		TOTAL:	864

Building: Duplex Housing

Site info:

$$Total\ Building\ Area = 12{,}100\ sq.ft\ (0.28\ acres)$$

$$\%\ Impervious = 100\%$$

Simple DCV:

$$C = (0.75)(imp) + 0.15 = (0.75)(1.0) + 0.15 = 0.90$$

$$V = (C)(d)(A)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right)$$

$$V = (0.90)(0.75\ in.)(0.28\ acres)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right) = 680.63\ ft^3$$

BMP ID	Planter Height (ft)	Planter Area (sq.ft)	Volume(cu.ft)
D1	3	50	150
D2	3	49	147
D3	3	49	147
D4	3	50	150
D5	3	48	144
D6	3	48	144
		TOTAL:	882

Building: Triplex Housing

Site info:

$$Total\ Building\ Area = 19{,}000\ sq.ft\ (0.44\ acres)$$

$$\%\ Impervious = 100\%$$

Simple DCV:

$$C = (0.75)(imp) + 0.15 = (0.75)(1.0) + 0.15 = 0.90$$

$$V = (C)(d)(A)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right)$$

$$V = (0.90)(0.75\ in.)(0.44\ acres)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right) = 1{,}068.75\ ft^3$$

BMP ID	Planter Height (ft)	Planter Area (sq.ft)	Volume(cu.ft)
T1	3	28	84
T2	3	24	72
T3	3	40	119
T4	3	42	125
T5	3	24	72
T6	3	49	147
T7	3	70	210
T8	3	67	201
T9	3	66	198
T10	3	67	201
T11	3	71	213
		TOTAL:	1,428

Building: Remaining Site

Site info:

$$Total\ Area = 234{,}447.9\ sq.ft\ (5.38\ acres)$$

$$\%\ Impervious = 20\%$$

Simple DCV:

$$C = (0.75)(imp) + 0.15 = (0.75)(0.20) + 0.15 = 0.30$$

$$V = (C)(d)(A)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right)$$

$$V = (0.30)(0.75\ in.)(5.38\ acres)\left(\frac{43{,}560\ sq.ft}{1\ acre}\right)\left(\frac{1\ ft}{12\ in}\right) = 4{,}395.7\ ft^3$$

PHASE 2 – DCV REDUCTION CALCULATIONS

			Phase 2A - DMA 1	Phase 2B - DMA 1	
Step 1: Determine the design capture storm depth used for calculating volume					
1	Enter design capture storm depth from Figure III.1, *d* (inches)	d=	0.80	0.80	inches
2	Enter calculated drawdown time of the proposed BMP based on equation provided in applicable BMP Fact Sheet, *T* (hours)	T=	9.64	9.64	hours
3	Using Figure III.2, determine the "fraction of design capture storm depth" at which the BMP drawdown time (T) line achieves 80% capture efficiency, X_1	X_1=	0.50	0.50	
4	Enter the effect depth of provided HSCs upstream, d_{HSC} (inches) (Worksheet A)	d_{HSC}=	0	0	inches
5	Enter capture efficiency corresponding to d_{HSC}, Y_2 (Worksheet A)	Y_2=	0%	0%	%
6	Using Figure III.2, determine the fraction of "design capture storm depth" at which the drawdown time (T) achieves the equivalent of the upstream capture efficiency (Y_2), X_2	X_2=	0.00	0.00	
7	Calculate the fraction of design volume that must be provided by BMP, *fraction* = X_1 - X_2	fraction=	0.50	0.50	
8	Calculate the resultant design capture storm depth (inches), $d_{fraction}$= *fraction* × *d*	$d_{fraction}$=	0.40	0.40	inches
Step 2: Calculate the DCV					
1	Enter Project area tributary to BMP(s), *A* (acres)	A=	1.41	1.08	acres
2	Enter Project Imperviousness, *imp* (unitless)	imp=	65%	75%	%
3	Calculate runoff coefficient, *C= (0.75 x imp) + 0.15*	C=	0.638	0.713	
4	Calculate runoff volume, V_{design}= *(C x* $d_{fraction}$ *x A x 43560 x (1/12))*	V_{design}=	1,305	1,121	cu-ft

Supporting Calculations

Describe System:		*Phase 2A - DMA 1*	*Phase 2B - DMA 1*	
	Bioretention Without Underdrain	-	-	
	Ponding Depth (d_p) =	*0.5*	*0.5*	ft
	Media Depth (d_M) =	*3*	*3*	ft
	Media Porosity (η_M) =	*20%*	*20%*	
	Gravel Reservoir Depth (d_G) =			ft
	Gravel Porosity (η_G) =	*35%*	*35%*	
	Effective Depth ($d_{Effective}$) =	*1.10*	*1.10*	ft
	Design Infiltration Rate (K_{Design}) =	*1.4*	*1.4*	in/hr
	Minimum Surface Area Required (A_{Min}) =	*1,187*	*1,019*	ft^2
	Total Infiltrating Surface Area Provided =	*1,190*	*1,020*	ft^2
	Total Volume Stored =	*1,309*	*1,122*	ft^3

Provide drawdown time calculations per applicable BMP Fact Sheet:				
	Drawdown (DD or T) = ($d_{Effective}$) / (K_{Design}) x 12			
	Time to Drawdown Effective Depth (T) =	*9.6*	*9.6*	hours

Attachment 9

Green Street Project BMP Conformance Analysis Tables

GREEN STREET PROJECT BMP CONFORMANCE ANALYSIS

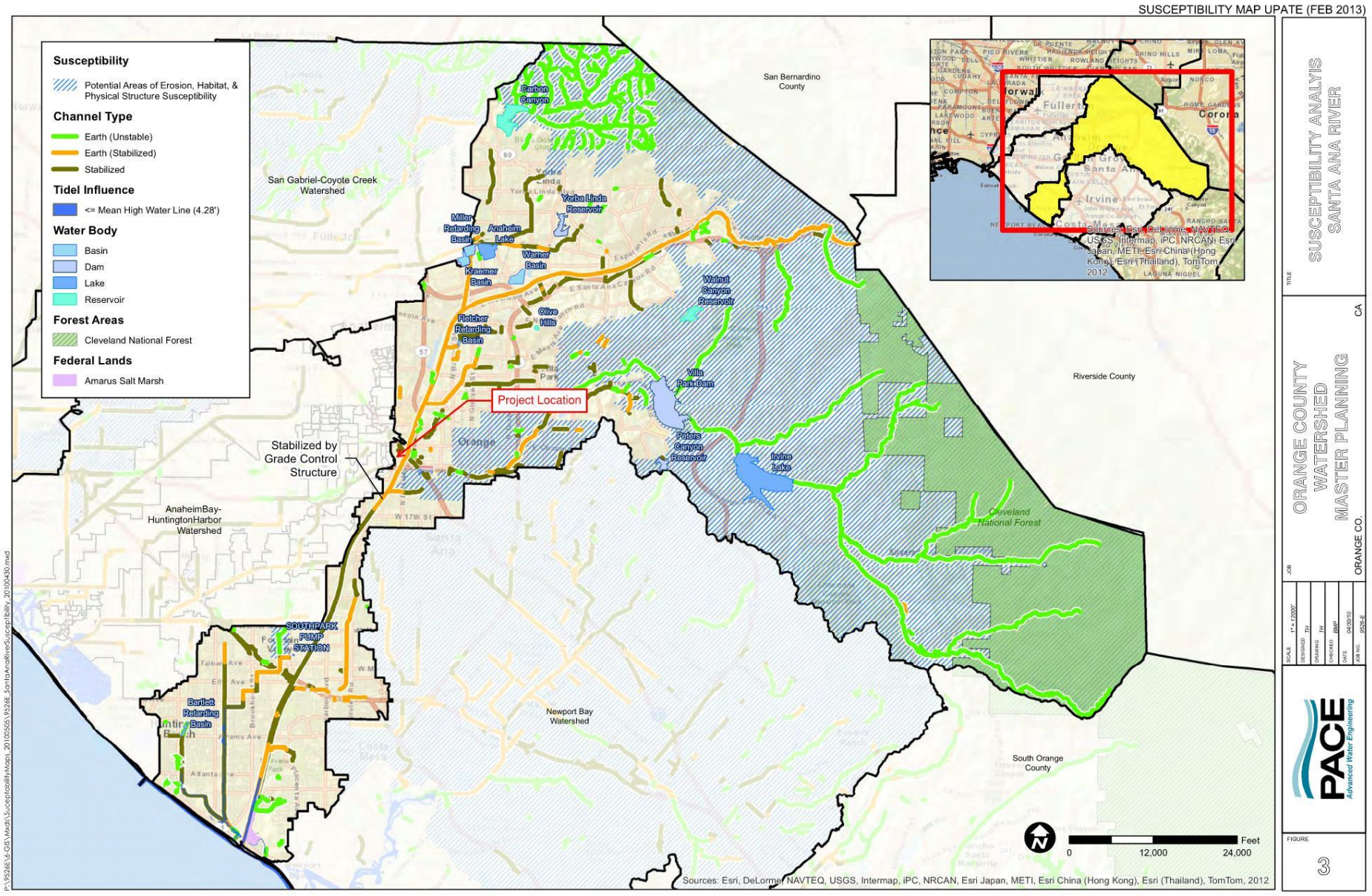
DMA ID: INSERT DMA ID HERE		**DCV =**	0 ac-ft	
Hydrologic Source Controls				
Included	Site Design BMP	Fact Sheet	DCV Reduction	
☐	Street Trees[1]	HSC-3	0 ac-ft	
Low Impact Development BMPs | Infiltration				
☐	Infiltration Trench[2]	INF-2	0 ac-ft	
☐	Bioretention with no Underdrain[3]	INF-3	0 ac-ft	
☐	Bioinfiltration with Raised Underdrain	INF-4	0 ac-ft	
☐	Drywell[4]	INF-5	0 ac-ft	
☐	Permeable Pavement[5]	INF-6	0 ac-ft	
☐	Underground Infiltration[6]	INF-7	0 ac-ft	
Low Impact Development BMPs | Biotreatment				
☐	Bioretention with Underdrains[7]	BIO-1	0 ac-ft	
☐	Vegetated Swale[8]	BIO-2	0 ac-ft	
☐	Vegetated Filter Strip[9]	BIO-3	0 ac-ft	
☐	Proprietary Biotreatment[10]	BIO-7	0 ac-ft	
Treatment Control BMPs				
☐	Sand Filter[11]	TRT-1	0 ac-ft	
☐	Cartridge Media Filter[12]	TRT-2	0 ac-ft	
		Total DCV Reduction =	0	**ac-ft**
		Remaining DCV = DCV –Total DCV Reduction =	0	**ac-ft**

[1] Also known as Canopy Interception.
[2] Also known as French Drain, Rock Trench, Exfiltration Trench, Soak-Aways, or Soakage Trench.
[3] Also known as Rain Garden or Infiltration Planter.
[4] Also known as Soak-Away Pits, Infiltration Sumps, Rock Sumps, or Underground Injection Controls. Calculations for determining DCV reduction provided by drywells is highly site-specific. No template is provided. Drywells must be designed to ensure a drawdown time of 48 hours. Calculations for DCV reduction are to be provided in **Attachment 8**.
[5] Also known as Pervious Pavement, Porous Concrete, Pavers, or Permeable Asphalt.
[6] Also known as Subsurface Infiltration Galleries, Infiltration Vault, or Recharge Vault. For underground infiltration devices with open pore volume (e.g. vaults, crates, pipe sections, etc.), refer to the Infiltration Basin BMP Template. For underground infiltration devices with pore space (e.g. aggregate reservoirs), refer to the permeable Pavement BMP Template.
[7] Also known as Rain Gardens with Underdrains, Vegetated Media Filter, or Downspout Planter Boxes.
[8] Also known as Bioswale, Biofiltration Swale, or Grass Swale.
[9] Also known as Buffer Strip or Vegetated Buffer.
[10] Also known as Catch Basin Planter Box, Bioretention Vault, or Tree Box Filter. A calculation template is not provided for Proprietary Biotreatment. If implemented, calculations are required to be included in **Attachment 8**.
[11] Also known as Bed Media Filter.
[12] Also known as Manufactured Media Filters.

Check only one of the two boxes below:	
☐ Remaining DCV = 0 ac-ft	The DCV for this DMA is fully captured by the LID BMP(s) checked above. No additional BMPs are necessary, except hydromodification control BMPs if applicable.
☐ Remaining DCV > 0 ac-ft	The DCV for this DMA cannot feasibly be fully captured by LID BMPs. If LID or hydromodification sizing criteria cannot be achieved, document the constraints here.

Attachment 10

Hydromodification Exhibits and Calculations


SUSCEPTIBILITY MAP UPATE (FEB 2013)
Susceptibility
Potential Areas of Erosion, Habitat, & Physical Structure Susceptibility
Channel Type
Earth (Unstable)
Earth (Stabilized)
Stabilized
Tidel Influence
<= Mean High Water Line (4.28')
Water Body
Basin
Dam
Lake
Reservoir
Forest Areas
Cleveland National Forest
Federal Lands
Amarus Salt Marsh
San Gabriel-Coyote Creek Watershed
San Bernardino County
Riverside County
Carbon Canyon
Yorba Linda Reservoir
Miller Retarding Basin
Anaheim Lake
Warner Basin
Kraemer Basin
Walnut Canyon Reservoir
Olive Hills
Fletcher Retarding Basin
Villa Park Dam
Project Location
Stabilized by Grade Control Structure
Peters Canyon Reservoir
Irvine Lake
Cleveland National Forest
AnaheimBay-HuntingtonHarbor Watershed
SOUTHPARK PUMP STATION
Bartlett Retarding Basin
Newport Bay Watershed
South Orange County
Sources: Esri, DeLorme, NAVTEQ, USGS, Intermap, iPC, NRCAN, Esri Japan, METI, Esri China (Hong Kong), Esri (Thailand), TomTom, 2012
0
12,000
24,000
Feet
SUSCEPTIBILITY ANALYIS
SANTA ANA RIVER
ORANGE COUNTY
WATERSHED
MASTER PLANNING
ORANGE CO.
CA
PACE
Advanced Water Engineering
FIGURE
3

Attachment 11

Hydromodification Management Plan

Attachment 12

BMP Exhibit

HYDROLOGIC SOIL GROUP: "A"

LEGEND

	MAJOR DRAINAGE BOUNDARY
	SUB-DRAINAGE BOUNDARY
	FLOWLINE
	DRAINAGE FLOW DIRECTION
(SD)	STORM DRAIN LINE
A1 / 0.12AC	SUBAREA DESIGNATION / SUBAREA (ACRES)
10	NODE NUMBER
123.4FS	PROPOSED FINISHED SURFACE ELEV.
123.4FG	PROPOSED FINISHED GRADE ELEV.
123.4INV	INVERT ELEV.
Q25	CALCULATED RUNOFF FOR 25 YR FREQ.
Tc	TIME OF CONCENTRATION
SD	STORM DRAIN
S	SLOPE
L	FLOW PATH LENGTH (SURFACE)
NAP	NOT A PART

Youth Transition Center

Long Term Housing

Classroom and Library Building

Independent Living

2A-1 0.97AC

2A-2 0.44AC

2B 1.08AC

Proposed Bioretention with No Underdrain (INF-3); 1,190 SF

Proposed Bioretention with No Underdrain (INF-3); 1,020 SF

SERVICE WAY

SIDWELL WAY

HOSPITAL FRONTAGE RD

JUSTICE CENTER WAY

ORANGEWOOD CHILDREN'S HOME

ORANGE COUNTY COURT MANCHESTER OFFICE

A.C. PARKING LOT

BREAK ROOM

ADMIN

MEDICAL UNIT

UNIT M

DENTAL

UNIT T

UNIT Q

UNIT B

UNIT C

UNIT Z

UNIT Y

ALLEY

LAMOREAUX JUSTICE CENTER

JUSTICE CENTER

CLASSROOMS

YLA 1

YLA 2

YLA ADMIN

AC PARKING LOT

BASKETBALL COURT

UTILITY ENCLOSURE

NORTH FIELD

SOCCER FIELD

M.R.C. BUILDING

LAUNDRY

KITCHEN

SUB STATION

SANTA ANA RIVER

SANTA ANA FWY (5)

SCALE: 1" = 40'

DRAINAGE CONDITIONS TABLE

Subarea	Area (SF)	Area (AC)	Pervious Area (SF)	Impervious Rate (%)	Soil Type	Pervious Rate (AES)
Existing Phase 2A	61,381.78	1.41	15,644.66	74.51%	A	25%
Proposed Phase 2A	61,381.78	1.41	22,140.30	63.93%	A	35%
Existing Phase 2B	47,190.68	1.08	7,860.61	83.34%	A	20%
Proposed Phase 2B	47,190.68	1.08	12,299.84	73.94%	A	25%

DRAINAGE CALCULATIONS TABLE

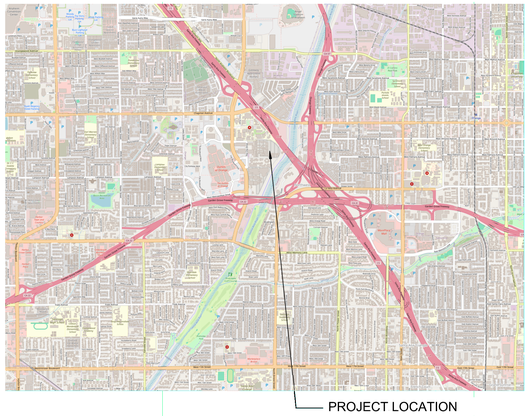
Subarea	Q_2 (CFS)	TC (Min)	Q_{10} (CFS)	TC (Min)	Q_{25} (CFS)	TC (Min)	Q_{100} (CFS)	TC (Min)
Existing Phase 2A	1.88	9.32	3.48	9.32	4.18	9.32	5.37	9.32
Proposed Phase 2A	1.75	9.98	3.29	9.98	3.96	9.98	5.10	9.98
Change	-0.13	0.66	-0.19	0.66	-0.22	0.66	-0.27	0.66
Existing Phase 2B	1.65	7.60	3.03	7.60	3.62	7.60	4.65	7.60
Proposed Phase 2B	1.60	7.88	2.94	7.88	3.53	7.88	4.54	7.88
Change	-0.05	0.28	-0.09	0.28	-0.09	0.28	-0.11	0.28

PREPARED FOR:
The County of Orange
601 N. ROSS STREET
SANTA ANA, CA 92701

PREPARED BY:
FUSCOE ENGINEERING
15535 Sand Canyon Ave, Suite 100
Irvine, California 92618
949.474.1960 fuscoe.com

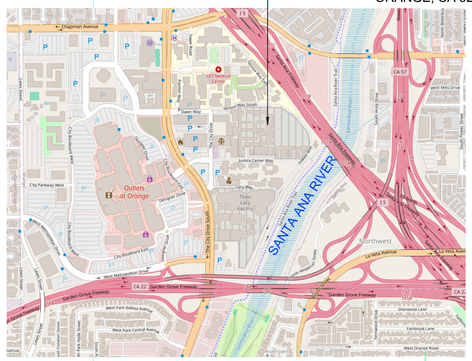
County of Orange
OC Public Works
PROPOSED DRAINAGE AND LID BMP CONCEPTUAL PLAN
ORANGE COUNTY JUVENILE HALL
ORANGE COUNTY, CA
11/18/2024

E:\USERS\DRAINAGE\WORK\ENGINEERING\DOCUMENTS\OC_VISTA\OC_TOPO_2023-BASE_11072024-HYD.DWG [11-18-24 5:52:54PM] Plotted By: dsanchez



VICINITY MAP

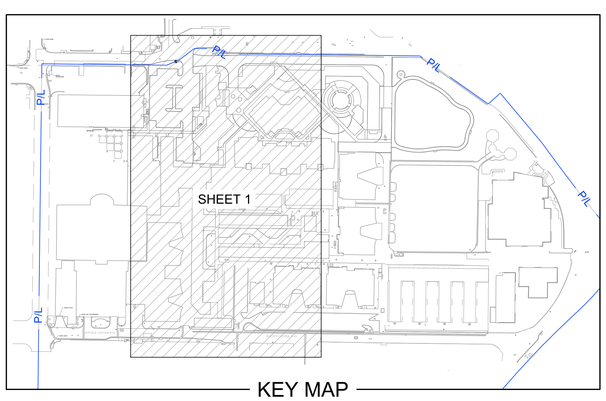
PROJECT LOCATION
ADDRESS: 331 SIDWELL WAY,
ORANGE, CA 92868



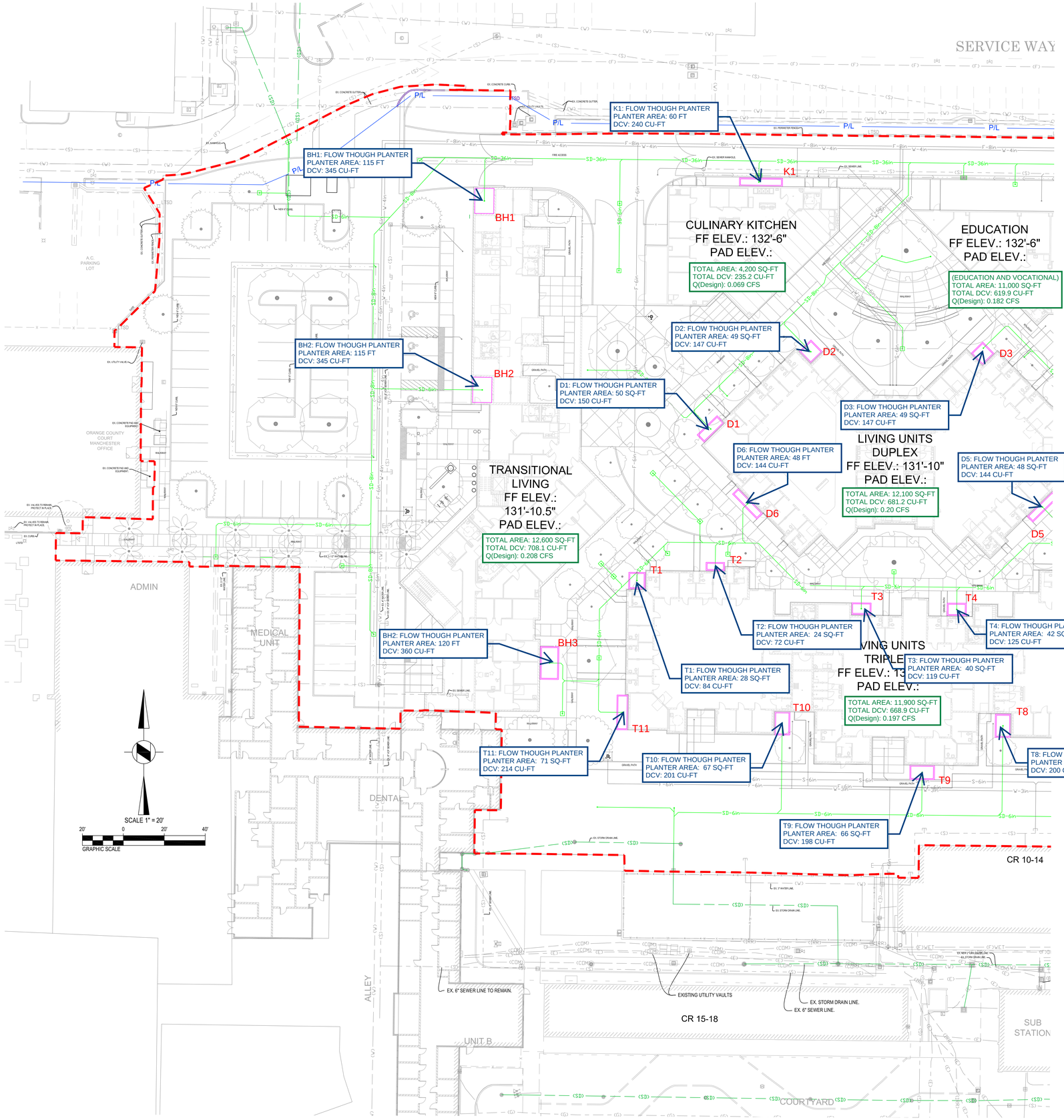
SITE MAP

LEGEND

P/L	PROPERTY LINE
	LIMITS OF WORK
SD	NEW STORM DRAIN LINE
(SD)	EXISTING STORM DRAIN LINE
	NEW FLOW THROUGH PLANTER
BMP ID#	



KEY MAP



County of Orange
PUBLIC WORKS
OC Facilities Design & Construction

Revisions

01	08/19/2024	PLAN CHECK COMMENTS
A	08/19/2024	PLAN CHANGES

Consultants
COFFMAN ENGINEERS
17781 Sky Park Circle, Suite F
Irvine, CA 92614-6417
(949) 660-1911
www.coffman.com

A-E Seal
PROFESSIONAL ENGINEER
STEVE WITHERSPOON
No. C-58311
Exp. 06-30-26
CIVIL
STATE OF CALIFORNIA

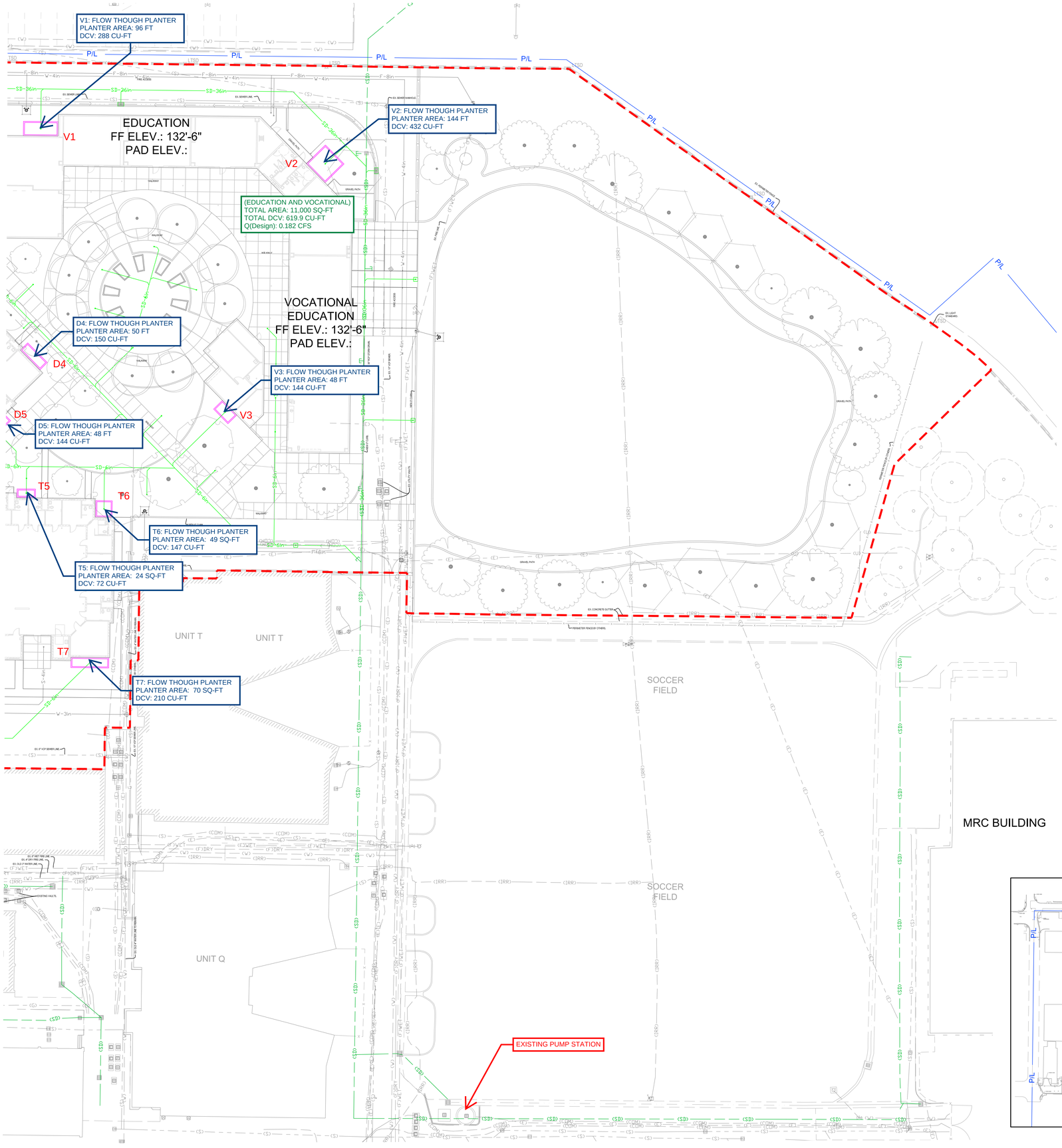
DLRGROUP
300 S. FLOWER ST.
SUITE 1000
LOS ANGELES, CA 90017
© DLR Group

Balfour Beatty

A-E

Sht Title: OC YOUTH TRANSITION CENTER - BMP EXHIBIT
Project: COUNTY OF ORANGE - YOUTH TRANSITION CENTER
331 THE CITY DRIVE S.
ORANGE, CA 92868
Package: -
PROJ. NO. -
DATE 11/06/24

Approve In Concept
Project Manager: _____
Section Manager: _____
OC PUBLIC WORKS
OC FACILITIES DESIGN & CONSTRUCTION
Date: _____
Plan No.
-
Sheet
01



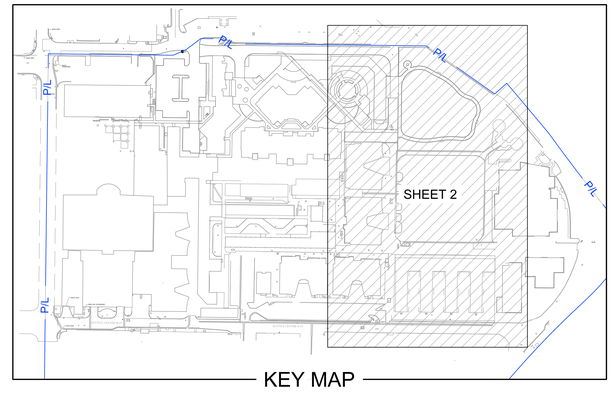
LEGEND

- P/L — PROPERTY LINE
- LIMITS OF WORK
- SD — NEW STORM DRAIN LINE
- (SD) — EXISTING STORM DRAIN LINE
- NEW FLOW THROUGH PLANTER
- BMP ID#

SCALE 1" = 20'

20' 0 20' 40'

GRAPHIC SCALE



KEY MAP

County of Orange

PUBLIC WORKS

OC Facilities Design & Construction

Revisions

01	08/19/2024	PLAN CHECK COMMENTS
A	08/19/2024	PLAN CHANGES

Consultants

COFFMAN ENGINEERS
17272 NEWHOPE STREET
SUITE 100
FOUNTAIN VALLEY, CA 92677
(714) 435-8100
www.coffman.com

A-E Seal

A-E

Balfour Beatty

DLRGROUP
700 S. FLOWER ST.
SUITE 2100
LOS ANGELES, CA 90017
© DLR Group

Sht Title OC YOUTH TRANSITION CENTER - BMP EXHIBIT

Project: COUNTY OF ORANGE - YOUTH TRANSITION CENTER
331 THE CITY DRIVE S.
ORANGE, CA 92868

Package: -

DATE 11/06/24

PROJ. NO. -

Approve In Concept

Project Manager: _____

Section Manager: _____

OC PUBLIC WORKS
OC FACILITIES DESIGN & CONSTRUCTION

Date: _____

Plan No.
-

Sheet
02

Attachment 13

Additional Educational Material

No additional education materials have been identified for the project.

Attachment 14

Additional BMP Inspection and Maintenance Responsibility Tables

Table 12-1 BMP Inspection and Maintenance Responsibilities

BMP	DMA	Reponsible Party(s)	Inspection/ Maintenance Activities Required	Minimum Frequency of Activities

Attachment 15

Operations and Maintenance Plan

Attachment 16

BMP Inspection Record

Attachment 17

Conceptual Hydrology Report for Phase 1 and Phase 2 (Separate Reports)

COFFMAN ENGINEERS

PRELIMINARY HYDROLOGY REPORT

ORANGE COUNTY TRANSITIONAL YOUTH CENTER |
CITY OF ORANGE, CA

Prepared by: Coffman Engineers, Inc.
626 Wilshire Blvd., Suite 700, Los Angeles, CA 90017
Job No. 232144
Date Prepared: November 15, 2024

Table of Contents

A. INTRODUCTION 3

1. Project Description 3
2. Location 3
3. Focus of Report 4

B. Methodology 4

1. Hydrology Manual 4
2. Existing Site Conditions 4
3. Proposed Site Condition 4

C. Summary 5

D. References 5

APPENDIX A – Site Plan 7

A. INTRODUCTION

1. Project Description

The County of Orange plans to undertake a multi-phase project to demolish and rebuild several structures, along with associated infrastructure and landscaping, within the Orange County Juvenile Hall Campus. This portion of the report will focus on phase 1 of the project focusing on the northern part of the campus, improving about 5.8 acres of the approximate overall 17-acre property.

2. Location

The project site is located at 331 The City Drive South in the City of Orange, California. The site is located near the 5 Freeway, the 22 Freeway, and The City Drive Street and sits on parcel number 231-271-10. Additionally this project is located west of the Santa Ana River.



Vicinity Map

3. Focus of Report

This preliminary report will focus on the area impacted by phase 1 improvements by identifying changes to existing and post project conditions. This study will outline the general project characteristics and methodology used in water treatment.

B. Methodology

1. Hydrology Manual

The post-development hydrology analysis for the site will be determined using the methodology outlined in the Orange County Hydrology Manual for post-developed conditions, using the Rational Method, in accordance with the manual.

2. Existing Site Conditions

Phase 1 of the project occupies approximately 5.8 acres of the site. The project site is relatively level and slopes from the northwest to the southeast. Site drainage flows into existing 36in RCP storm drain between the existing library and baseball field. The existing storm drain flows off campus and eventually discharges into the Santa Ana River Channel.

3. Proposed Site Condition

Phase 1 of the project will leverage the existing storm drain system to manage new drainage flows. The site will be divided into multiple drainage areas, encompassing both the buildings and the overall site. Roof runoff from each building will be directed into flow-through planters for water treatment. Any surface runoff not treated by the flow-through planters will be managed and treated using an underground treatment unit.

Phase 1 – Drainage Area	Area (sq-ft)	Area (acres)	Impervious Area (sq-ft)	Percent Impervious
Behavioral Health	12,600	0.29	0	100%
Kitchen	4,200	5.81	0	100%
Education and Vocational Ed.	11,000	0.25	0	100%
Duplex	12,100	0.28	0	100%
Triplex	11,900	0.27	0	100%
Non-Building Area	234,448	5.38	187,638	20%

C. Summary

We are expecting a difference in peak flow rates between pre-development and post-development conditions which will primarily be attributed to the decrease in impervious surface area, which will decrease by approximately 33% in post-development conditions. See below for the summary table for the entire site, comparing pre-development and post-development conditions:

Phase 1	Area (sq-ft)	Area (acres)	Impervious Area (acres)	Percent Impervious
Existing Conditions	252,999.45	5.81	3.41	58.7%
Proposed Conditions	252.999.45	5.81	1.51	32.8%

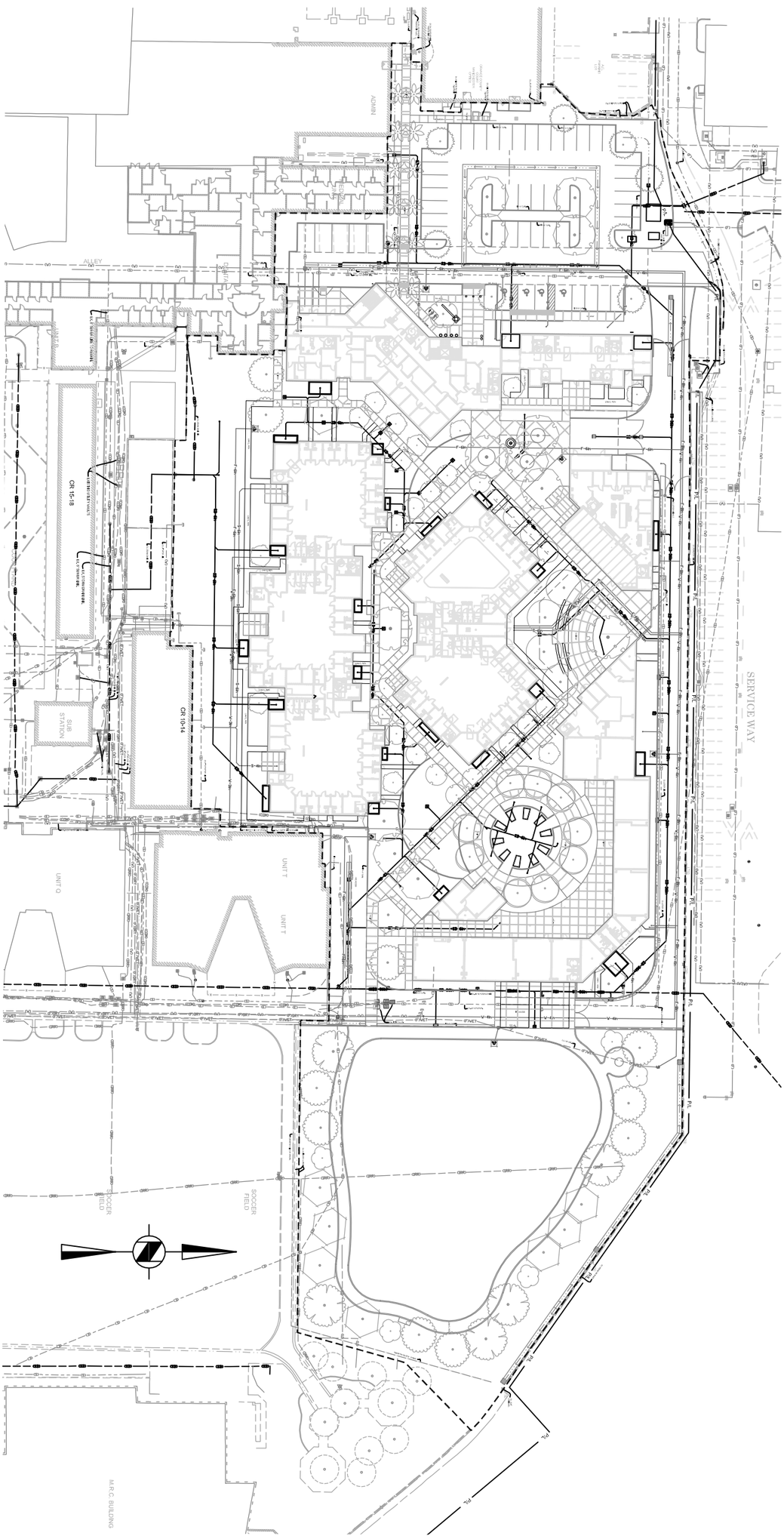
This report is based off a preliminary hydrology study for phase 1 of this project.

D. References

- Orange County Hydrology Manual (October 1986)

- Orange County Hydrology Manual Addendum No. 1 (1996)

APPENDIX A – Site Plan



VICINITY MAP

PROJECT LOCATION

SITE MAP

SANTA ANA RIVER

PROJECT LOCATION
ADDRESS: 331 THE CITY DRIVE S.
ORANGE, CA 92868

LEGEND

P/L — PROPERTY LINE

SD — STORM DRAIN

GSD — GRAY WATER STORM DRAIN

ELECTRIC UNDERGROUND

Sheet

Plan No.

OC PUBLIC WORKS
OC FACILITIES DESIGN & CONSTRUCTION

Date:

Approve In Concept

Project Manager:

Section Manager:

Sht Title

Project: COUNTY OF ORANGE - YOUTH TRANSITION CENTER
331 THE CITY DRIVE S.
ORANGE, CA 92868

Package:

PROJ. NO.

DATE 11/06/24

A-E

Balfour Beatty DLRGROUP
550 S. FLOWER ST.
SUITE 1000
LOS ANGELES, CA 90017
© DLR Group

A-E Seal

Consultants

COFFMAN ENGINEERS
3 JON VILLIERS BLVD
SUITE 1010
LOS ANGELES, CA 90017
www.coffman.com

Revisions

01	05/19/2024	PLAN CHECK COMMENTS
A	05/19/2024	PLAN CHANGES

County of Orange

OC PUBLIC WORKS

OC Facilities Design & Construction

PRELIMINARY HYDROLOGY REPORT

Orange County Juvenile Hall

Orange County, California

PREPARED BY:

Fuscoe Engineering, Inc.

15535 Sand Canyon Ave, Suite 100

Irvine, CA 92618

(949) 474-1960

Project Number:

309-026-01

Date Prepared:

November 2024

Table of Contents

1.0 INTRODUCTION 3

1.1 Geographic Setting 3

1.2 Purpose of this Report 4

1.3 References 4

2.0 HYDROLOGY 5

2.1 Existing Condition 5

2.2 Proposed Condition 5

3.0 FEMA 6

4.0 RESULTS AND CONCLUSIONS 6

5.0 APPENDICESS 7

Appendix A Architect's Site Plan

Appendix B Existing Storm Drain Information

Appendix C Existing Hydrology

Appendix D Proposed Hydrology

Appendix E FEMA Map

1.0 INTRODUCTION

1.1 Geographic Setting

The County of Orange (County) proposes to demolish and replace ten buildings and associated infrastructure within the existing Orange County Juvenile Hall Campus (campus) located in the City of Orange (City), California, which occupies an approximately 17-acre property located at 331 The City Drive South (project site). The study area is bounded by Justice Way to the south, Hospital Frontage Road to the west, Interstate 5 freeway and Santa Ana River to the east and Service Way to the north. A Vicinity Map is shown below.



VICINITY MAP

The proposed site improvements will be divided into three phases. The architect's Overall Site Plan is included in this report as Appendix 1. This portion of the site will focus on Phases 2A and 2B of the development. Phase 2A comprises of Long Term Housing and Classroom and Library

Building, located adjacent to the south of Phase 1. Phase 2B comprises of Independent Living, located near the southeast edged of the property.

1.2 Purpose of this Report

The purpose of this analysis is to identify and analyze the pre- and post-project drainage conditions in order to provide adequate drainage facilities for the proposed development located in the County of Orange, California.

This Drainage Study will analyze and compare the 2-, 10-, 25- and 100-year storm events for the existing and proposed conditions. Outcomes of the analysis will facilitate the conceptual layout of a drainage system to adequately convey storm runoff through the site without adversely impacting surrounding areas. The project is HCOC exempt and therefore Hydromodification requirements are not applicable.

The project is within Soil Type "A", based on the County of Orange Hydrology Manual.

All hydrology and hydrologic calculations would be performed and verified for protection in a 100-year storm event according to the Orange County Hydrology Manual (1986) and its Addendum (1996) during final design. All calculations will be based on AES Rational Method and will follow requirements per Orange County Hydrology Manual. Impervious rates will be calculated per existing and proposed plans. AES does now offer specific impervious rates but rather it utilizes pre-determined rates based on estimated land use. For these calculations, similar pre-determined rates were selected that conservatively follows the hand calculations.

1.3 References

The following references were used to evaluate hydrologic conditions and water quality requirements:

- Orange County Hydrology Manual (October 1986)
- Orange County Hydrology Manual Addendum No. 1 (1996)
- Orange County Local Drainage Manual (January 1996)
- AES (Advanced Engineering Software), Rational Method (July 2016)

2.0 HYDROLOGY

2.1 Existing Condition

The approximate overall 17-acre study area is a developed site that contains the Orange County Juvenile Hall Campus. The existing site generally slopes in a southerly direction to southerly area of the property.

An existing 33-inch RCP storm drain drains from the north to the south and bisects the project site, allowing for a collection point for on-site stormwater. This storm drain connects to an existing 42-inch RCP that is located offsite and adjacent to the south which runs south along The City Drive and discharges into the Santa Ana River Channel, and ultimately the Pacific Ocean.

Phases 2A and 2B will be analyzed for existing hydrological conditions using AES Rational Method to generate storm runoff rates using calculated existing impervious rates. Hydrology Calculations are located in Existing Hydrology (Appendix C).

2.2 Proposed Condition

The proposed project improvements will maintain the existing drainage patterns.

Phases 2A and 2B will be analyzed for proposed hydrological conditions using AES Rational Method to generate storm runoff rates using calculated proposed impervious rates based on the Overall Site Plan. Hydrology Calculations are located in Proposed Hydrology (Appendix D).

The overall drainage strategy is to convey onsite stormwater runoff into an onsite storm drain system that mitigates the proposed runoff's water quality, hydraulic and volumetric parameters per the regulating agencies (County of Orange) drainage codes. There will be several drainage management areas defined in the water quality analysis. The proposed project would provide a series of proposed bioretention with underdrain planter systems to capture and treat stormwater runoff.

As discussed in the existing condition, the drainage conveyance will similarly connect to the existing 33-inch RCP storm drain drains from the north to the south, ultimately connecting to an

existing 42-inch RCP location off-site to the south, that discharges into the Santa Ana River Channel, and ultimately the Pacific Ocean.

3.0 FEMA

The project site is located at FEMA flood zone 'X' per FEMA Flood Insurance Rate Map (FIRM) No. 06059C0142J, map revised December 3, 2021. The site is entirely within Zone X, which depicts area of reduced flood risk due to levee. A CLOMR or LOMR will not be required. A FEMA Map (Firmette) is included in this report as Appendix E.

4.0 RESULTS AND CONCLUSIONS

The results of the hydrologic analyses are shown on the following table.

Tabe A - Phase 2 Drainage Conditions

Subarea	Area (SF)	Area (AC)	Pervious Area (SF)	Impervious Rate (%)	Soil Type	Pervious Rate (AES)
Existing Phase 2A	61,381.78	1.41	15,644.66	74.51%	A	25%
Proposed Phase 2A	61,381.78	1.41	22,140.30	63.93%	A	35%
Existing Phase 2B	47,190.68	1.08	7,860.61	83.34%	A	20%
Proposed Phase 2B	47,190.68	1.08	12,299.84	73.94%	A	25%

Tabe B - Phase 2 Drainage Calculations

Subarea	Q_2 (CFS)	TC (Min)	Q_{10} (CFS)	TC (Min)	Q_{25} (CFS)	TC (Min)	Q_{100} (CFS)	TC (Min)
Existing Phase 2A	1.88	9.32	3.48	9.32	4.18	9.32	5.37	9.32
Proposed Phase 2A	1.75	9.98	3.29	9.98	3.96	9.98	5.10	9.98
Change	-0.13	0.66	-0.19	0.66	-0.22	0.66	-0.27	0.66
Existing Phase 2B	1.65	7.60	3.03	7.60	3.62	7.60	4.65	7.60
Proposed Phase 2B	1.60	7.88	2.94	7.88	3.53	7.88	4.54	7.88
Change	-0.05	0.28	-0.09	0.28	-0.09	0.28	-0.11	0.28

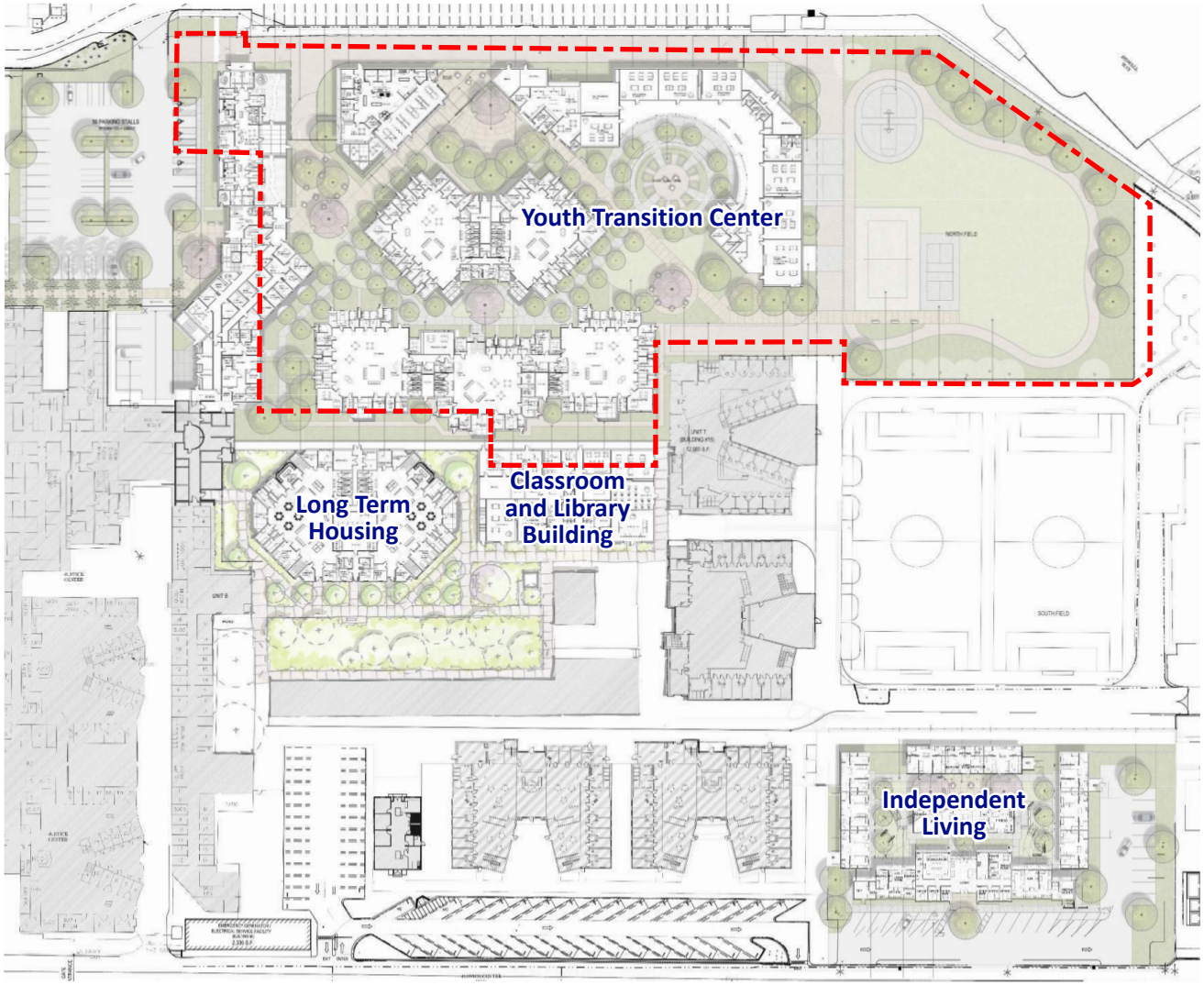
When comparing the Q allowable to the proposed condition, the proposed condition discharges less than expected. This is mostly due to the increase in pervious areas when comparing pre vs. post-development. Based on the hydrologic analyses included in this report, the proposed project will not adversely impact the drainage systems.

5.0 APPENDICESS

Appendix 1 Architect's Site Plan
Appendix 2 Existing Storm Drain Information
Appendix 3 Existing Hydrology
Appendix 4 Proposed Hydrology
Appendix 5 FEMA Map

APPENDIX A

Architect's Site Plan



LSA

LEGEND

Youth Transition Boundary

FIGURE 2-6

N

NO SCALE

SOURCE: DLR Group, Balfour Beatty, OC Dept of Public Works

I:\O\OCY2001.48\G\Overall_Site_Plan.ai (10/17/2024)

Orange County Youth Transition Center
Juvenile Hall Replacement Project
Overall Site Plan

APPENDIX B

Existing Storm Drain Information

SUBJECT TO FURTHER REVISION

PROJECT LOCATION

LOS ANGELES COUNTY
ORANGE COUNTY
SAN BERNARDINO COUNTY
ORANGE COUNTY
RIVERSIDE COUNTY
ORANGE COUNTY
LOS ANGELES COUNTY
ORANGE COUNTY

LEGEND

City Boundaries

Hydrologic Soil Groups

- A Soils
- B Soils
- C Soils
- D Soils

Source:
Soils: Natural Resources Conservation Service (NRCS)
Soil Survey - soil_ca678, Orange County & Western Riverside
Date of publication: 2006-02-08
http://websoilsurvey.nrcs.usda.gov/app/HomePage.htm

0 2.5 5 10 Kilometers
0 1.8 3.6 7.2 Miles

P:\95226E\6-GIS\Mxds\Reports\InfiltrationFeasability_20110215\95226E_FigureXVI-2a_HydroSoils_20110215.mxd

TITLE
NRCS HYDROLOGIC SOILS GROUPS

JOB
ORANGE COUNTY INFILTRATION STUDY
ORANGE CO. CA

SCALE	1" = 1.8 miles
DESIGNED	TH
DRAWING	TH
CHECKED	BMP
DATE	02/09/11
JOB NO.	95226-E

PACE
Advanced Water Engineering

FIGURE
XVI-2a

Susceptibility

Potential Areas of Erosion, Habitat, & Physical Structure Susceptibility

Channel Type

Earth (Unstable)
Earth (Stabilized)
Stabilized

Tidel Influence

<= Mean High Water Line (4.28')

Water Body

Basin
Dam
Lake
Reservoir

Forest Areas

Cleveland National Forest

Federal Lands

Amarus Salt Marsh

PROJECT LOCATION

Stabilized by Grade Control Structure

San Gabriel-Coyote Creek Watershed

San Bernardino County

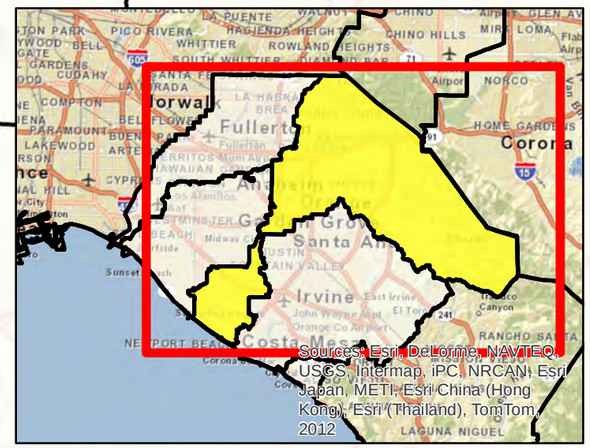
Riverside County

South Orange County

Newport Bay Watershed

AnaheimBay-HuntingtonHarbor Watershed

Carbon Canyon
Yorba Linda Reservoir
Miller Retarding Basin
Anaheim Lake
Warner Basin
Kraemer Basin
Olive Hills
Fletcher Retarding Basin
Walnut Canyon Reservoir
Villa Park Dam
Peters Canyon Reservoir
Irvine Lake
SOUTHPARK PUMP STATION
Bartlett Retarding Basin
Cleveland National Forest



0 12,000 24,000 Feet

Sources: Esri, DeLorme, NAVTEQ, USGS, Intermap, iPC, NRCAN, Esri Japan, METI, Esri China (Hong Kong), Esri (Thailand), TomTom, 2012

P:\9526E\16-GIS\Mxds\SuceptabilityMaps_20100505\9526E_SantaAnaRiverSusceptibility_20100430.mxd

TITLE
SUSCEPTIBILITY ANALYIS
SANTA ANA RIVER

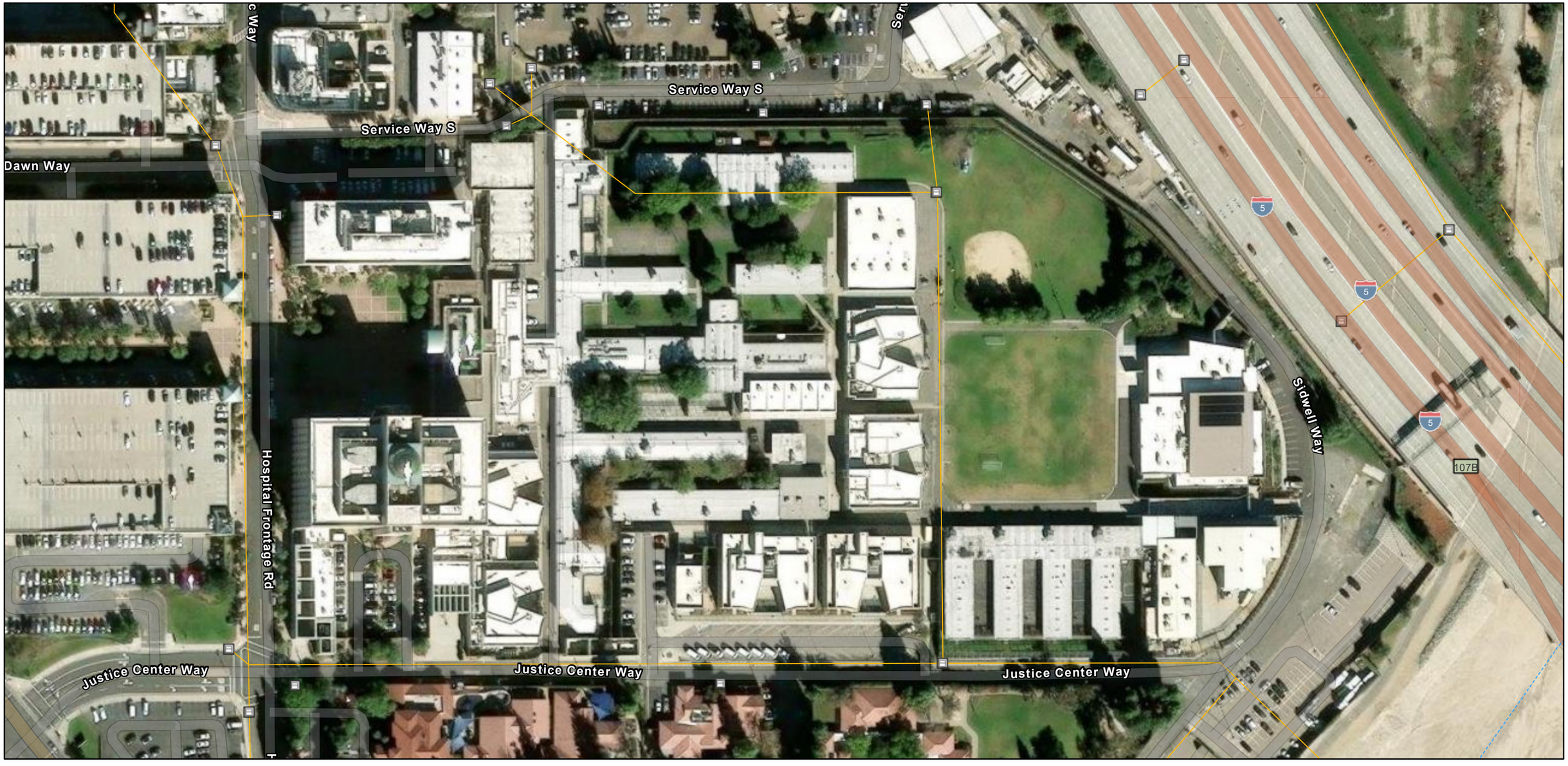
JOB
ORANGE COUNTY
WATERSHED
MASTER PLANNING
ORANGE CO. CA

SCALE	1" = 12000'
DESIGNED	TH
DRAWING	TH
CHECKED	BMP
DATE	04/30/10
JOB NO.	9526-E

PACE
Advanced Water Engineering

FIGURE
3

OC - YTC Storm Drain Layout



11/4/2024

Inlets

Local Drainage

Closed Conveyance

Regional Channels

Open Conveyance

1:1,869

0 0.02 0.04 0.07 mi

0 0.03 0.06 0.11 km

Esri Community Maps Contributors, County of Los Angeles, California State Parks, © OpenStreetMap, Microsoft, Esri, TomTom, Garmin, SafeGraph, GeoTechnologies, Inc, METI/NASA, USGS, Bureau of Land Management, EPA, NPS, US Census Bureau, USDA, USFWS, Maxar

APPENDIX C

Existing Hydrology

HYDROLOGIC SOIL GROUP: "A"

LEGEND

	MAJOR DRAINAGE BOUNDARY
	SUB-DRAINAGE BOUNDARY
	FLOWLINE
	DRAINAGE FLOW DIRECTION
(SD)	STORM DRAIN LINE
A1 / 0.12AC	SUBAREA DESIGNATION / SUBAREA (ACRES)
10	NODE NUMBER
123.4FS	PROPOSED FINISHED SURFACE ELEV.
123.4FG	PROPOSED FINISHED GRADE ELEV.
123.4INV	INVERT ELEV.
Q25	CALCULATED RUNOFF FOR 25 YR FREQ.
Tc	TIME OF CONCENTRATION
SD	STORM DRAIN
S	SLOPE
L	FLOW PATH LENGTH (SURFACE)
NAP	NOT A PART

PHASE DESIGNATION:

- PHASE 1
- PHASE 2
- PHASE 3

N

40' 0' 20' 40' 80'

SCALE: 1" = 40'

DRAINAGE CONDITIONS TABLE

Subarea	Area (SF)	Area (AC)	Pervious Area (SF)	Impervious Rate (%)	Soil Type	Pervious Rate (AES)
Existing Phase 2A	61,381.78	1.41	15,644.66	74.51%	A	25%
Proposed Phase 2A	61,381.78	1.41	22,140.30	63.93%	A	35%
Existing Phase 2B	47,190.68	1.08	7,860.61	83.34%	A	20%
Proposed Phase 2B	47,190.68	1.08	12,299.84	73.94%	A	25%

DRAINAGE CALCULATIONS TABLE

Subarea	Q_2 (CFS)	TC (Min)	Q_{10} (CFS)	TC (Min)	Q_{25} (CFS)	TC (Min)	Q_{100} (CFS)	TC (Min)
Existing Phase 2A	1.88	9.32	3.48	9.32	4.18	9.32	5.37	9.32
Proposed Phase 2A	1.75	9.98	3.29	9.98	3.96	9.98	5.10	9.98
Change	-0.13	0.66	-0.19	0.66	-0.22	0.66	-0.27	0.66
Existing Phase 2B	1.65	7.60	3.03	7.60	3.62	7.60	4.65	7.60
Proposed Phase 2B	1.60	7.88	2.94	7.88	3.53	7.88	4.54	7.88
Change	-0.05	0.28	-0.09	0.28	-0.09	0.28	-0.11	0.28

PREPARED FOR:	PREPARED BY:	County of Orange OC Public Works
The County of Orange 601 N. ROSS STREET SANTA ANA, CA 92701	FUSCOE ENGINEERING 15535 Sand Canyon Ave, Suite 100 Irvine, California 92618 949.474.1960 fuscoe.com	EXISTING DRAINAGE CONDITIONS ORANGE COUNTY JUVENILE HALL ORANGE COUNTY, CA 11/18/2024

C:\USERS\CMASON\DOWNLOADS\EXHIBIT - FUSCOE ENGINEERING\DOCUMENTS\OC_VITL\VITL_TOPO_2023-BASE_11072024-HYD.DWG [11-18-24 8:25:17PM] Plotted by: cmason

Phase 2A

Existing Conditions

```
**************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2A                                                               *
* EXISTING 2-YEAR STORM                                                  *
 ************************************************************************

  FILE NAME: YTC2A.DAT
  TIME/DATE OF STUDY: 17:45 11/12/2024
========================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
========================================================================
                    --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =    2.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)  (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0313 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

**************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
==========================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   423.27
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    9.319
  *   2 YEAR RAINFALL INTENSITY(INCH/HR) =  1.583
  SUBAREA Tc AND LOSS RATE DATA(AMC  I ):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  MOBILE HOME PARK           A        0.97      0.40     0.250    17    9.32
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.250
  SUBAREA RUNOFF(CFS) =      1.30
  TOTAL AREA(ACRES) =      0.97   PEAK FLOW RATE(CFS) =      1.30

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =    9.32
  RAINFALL INTENSITY(INCH/HR) =   1.58
  AREA-AVERAGED Fm(INCH/HR) =  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.25
  EFFECTIVE STREAM AREA(ACRES) =       0.97
  TOTAL STREAM AREA(ACRES) =       0.97
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       1.30

****************************************************************************
  FLOW PROCESS FROM NODE      1.10 TO NODE      2.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
============================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   302.28
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.615
  *   2 YEAR RAINFALL INTENSITY(INCH/HR) =  1.778
  SUBAREA Tc AND LOSS RATE DATA(AMC  I ):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
  MOBILE HOME PARK           A        0.44      0.40     0.250    17    7.61
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.250
  SUBAREA RUNOFF(CFS) =      0.66
  TOTAL AREA(ACRES) =      0.44   PEAK FLOW RATE(CFS) =      0.66

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =    7.61
  RAINFALL INTENSITY(INCH/HR) =   1.78
  AREA-AVERAGED Fm(INCH/HR) =  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.25
  EFFECTIVE STREAM AREA(ACRES) =       0.44
  TOTAL STREAM AREA(ACRES) =       0.44
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       0.66

  ** CONFLUENCE DATA **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap      Ae      HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)          (ACRES)    NODE
```

```
    1        1.30    9.32    1.583  0.40( 0.10) 0.25       1.0       1.00
    2        0.66    7.61    1.778  0.40( 0.10) 0.25       0.4       1.10

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        1.86    7.61    1.778  0.40( 0.10) 0.25       1.2       1.10
      2        1.88    9.32    1.583  0.40( 0.10) 0.25       1.4       1.00

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =       1.88    Tc(MIN.) =     9.32
  EFFECTIVE AREA(ACRES) =       1.41   AREA-AVERAGED Fm(INCH/HR) =  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap =  0.25
  TOTAL AREA(ACRES) =        1.4
  LONGEST FLOWPATH FROM NODE      1.00 TO NODE      2.00 =     423.27 FEET.
============================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.4  TC(MIN.) =      9.32
  EFFECTIVE AREA(ACRES) =      1.41  AREA-AVERAGED Fm(INCH/HR)=  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.250
  PEAK FLOW RATE(CFS)   =       1.88

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        1.86    7.61    1.778  0.40( 0.10) 0.25       1.2       1.10
      2        1.88    9.32    1.583  0.40( 0.10) 0.25       1.4       1.00
============================================================================
============================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
**************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                 *
* PHASE 2A                                                              *
* EXISTING 10-YEAR STORM                                                *
 ************************************************************************

  FILE NAME: YTC2A10.DAT
  TIME/DATE OF STUDY: 17:47 11/12/2024
========================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
========================================================================
                    --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =   10.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)   (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0312 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

**************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
========================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   423.27
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    9.319
  *  10 YEAR RAINFALL INTENSITY(INCH/HR) =  2.841
  SUBAREA Tc AND LOSS RATE DATA(AMC  II):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  MOBILE HOME PARK           A        0.97      0.40     0.250    32    9.32
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.250
  SUBAREA RUNOFF(CFS) =      2.39
  TOTAL AREA(ACRES) =      0.97   PEAK FLOW RATE(CFS) =      2.39

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =    9.32
  RAINFALL INTENSITY(INCH/HR) =   2.84
  AREA-AVERAGED Fm(INCH/HR) =  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.25
  EFFECTIVE STREAM AREA(ACRES) =       0.97
  TOTAL STREAM AREA(ACRES) =       0.97
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       2.39

****************************************************************************
  FLOW PROCESS FROM NODE      1.10 TO NODE      2.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
============================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   302.28
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.615
  *  10 YEAR RAINFALL INTENSITY(INCH/HR) =  3.190
  SUBAREA Tc AND LOSS RATE DATA(AMC  II):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
  MOBILE HOME PARK           A        0.44      0.40     0.250    32    7.61
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.250
  SUBAREA RUNOFF(CFS) =      1.22
  TOTAL AREA(ACRES) =      0.44   PEAK FLOW RATE(CFS) =      1.22

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =    7.61
  RAINFALL INTENSITY(INCH/HR) =   3.19
  AREA-AVERAGED Fm(INCH/HR) =  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.25
  EFFECTIVE STREAM AREA(ACRES) =       0.44
  TOTAL STREAM AREA(ACRES) =       0.44
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       1.22

  ** CONFLUENCE DATA **
   STREAM       Q      Tc   Intensity   Fp(Fm)      Ap      Ae      HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)          (ACRES)     NODE
```

```
    1        2.39    9.32    2.841  0.40( 0.10) 0.25       1.0       1.00
    2        1.22    7.61    3.190  0.40( 0.10) 0.25       0.4       1.10

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        3.43    7.61    3.190  0.40( 0.10) 0.25       1.2       1.10
      2        3.48    9.32    2.841  0.40( 0.10) 0.25       1.4       1.00

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =       3.48    Tc(MIN.) =     9.32
  EFFECTIVE AREA(ACRES) =       1.41   AREA-AVERAGED Fm(INCH/HR) =  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap =  0.25
  TOTAL AREA(ACRES) =        1.4
  LONGEST FLOWPATH FROM NODE      1.00 TO NODE      2.00 =     423.27 FEET.
============================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.4  TC(MIN.) =      9.32
  EFFECTIVE AREA(ACRES) =      1.41  AREA-AVERAGED Fm(INCH/HR)=  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.250
  PEAK FLOW RATE(CFS)   =       3.48

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        3.43    7.61    3.190  0.40( 0.10) 0.25       1.2       1.10
      2        3.48    9.32    2.841  0.40( 0.10) 0.25       1.4       1.00
============================================================================
============================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
**************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2B                                                               *
* EXISTING 25-YEAR STORM                                                 *
 ************************************************************************

  FILE NAME: YTC2A25.DAT
  TIME/DATE OF STUDY: 17:48 11/12/2024
========================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
========================================================================
                     --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =   25.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)   (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0312 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

**************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
==========================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   423.27
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    9.319
  *  25 YEAR RAINFALL INTENSITY(INCH/HR) =  3.391
  SUBAREA Tc AND LOSS RATE DATA(AMC  II):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  MOBILE HOME PARK           A        0.97      0.40     0.250    32    9.32
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.250
  SUBAREA RUNOFF(CFS) =      2.87
  TOTAL AREA(ACRES) =      0.97   PEAK FLOW RATE(CFS) =      2.87

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =    9.32
  RAINFALL INTENSITY(INCH/HR) =   3.39
  AREA-AVERAGED Fm(INCH/HR) =  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.25
  EFFECTIVE STREAM AREA(ACRES) =       0.97
  TOTAL STREAM AREA(ACRES) =       0.97
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       2.87

****************************************************************************
  FLOW PROCESS FROM NODE      1.10 TO NODE      2.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
============================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   302.28
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.615
  *  25 YEAR RAINFALL INTENSITY(INCH/HR) =  3.802
  SUBAREA Tc AND LOSS RATE DATA(AMC  II):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
  MOBILE HOME PARK           A        0.44      0.40     0.250    32    7.61
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.250
  SUBAREA RUNOFF(CFS) =      1.47
  TOTAL AREA(ACRES) =      0.44   PEAK FLOW RATE(CFS) =      1.47

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =    7.61
  RAINFALL INTENSITY(INCH/HR) =   3.80
  AREA-AVERAGED Fm(INCH/HR) =  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.25
  EFFECTIVE STREAM AREA(ACRES) =       0.44
  TOTAL STREAM AREA(ACRES) =       0.44
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       1.47

  ** CONFLUENCE DATA **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap      Ae      HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)          (ACRES)    NODE
```

```
    1        2.87    9.32    3.391  0.40( 0.10) 0.25       1.0       1.00
    2        1.47    7.61    3.802  0.40( 0.10) 0.25       0.4       1.10

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        4.11    7.61    3.802  0.40( 0.10) 0.25       1.2       1.10
      2        4.18    9.32    3.391  0.40( 0.10) 0.25       1.4       1.00

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =       4.18    Tc(MIN.) =     9.32
  EFFECTIVE AREA(ACRES) =       1.41   AREA-AVERAGED Fm(INCH/HR) =  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap =  0.25
  TOTAL AREA(ACRES) =        1.4
  LONGEST FLOWPATH FROM NODE      1.00 TO NODE      2.00 =     423.27 FEET.
============================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.4  TC(MIN.) =      9.32
  EFFECTIVE AREA(ACRES) =      1.41  AREA-AVERAGED Fm(INCH/HR)=  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.250
  PEAK FLOW RATE(CFS)   =       4.18

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        4.11    7.61    3.802  0.40( 0.10) 0.25       1.2       1.10
      2        4.18    9.32    3.391  0.40( 0.10) 0.25       1.4       1.00
============================================================================
============================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
******************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2A                                                               *
* EXISTING 100-YEAR STORM                                                *
 ************************************************************************

  FILE NAME: YTC2A100.DAT
  TIME/DATE OF STUDY: 17:50 11/12/2024
================================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
================================================================================
                     --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =  100.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)  (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0312 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

******************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
------------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
================================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   423.27
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    9.319
  * 100 YEAR RAINFALL INTENSITY(INCH/HR) =  4.331
  SUBAREA Tc AND LOSS RATE DATA(AMC III):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  MOBILE HOME PARK           A        0.97      0.40     0.250    52    9.32
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.250
  SUBAREA RUNOFF(CFS) =      3.69
  TOTAL AREA(ACRES) =      0.97   PEAK FLOW RATE(CFS) =      3.69

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =    9.32
  RAINFALL INTENSITY(INCH/HR) =   4.33
  AREA-AVERAGED Fm(INCH/HR) =  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.25
  EFFECTIVE STREAM AREA(ACRES) =       0.97
  TOTAL STREAM AREA(ACRES) =       0.97
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       3.69

****************************************************************************
  FLOW PROCESS FROM NODE      1.10 TO NODE      2.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
============================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   302.28
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.615
  * 100 YEAR RAINFALL INTENSITY(INCH/HR) =  4.862
  SUBAREA Tc AND LOSS RATE DATA(AMC III):
   DEVELOPMENT TYPE/       SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE             GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
  MOBILE HOME PARK            A        0.44      0.40     0.250    52    7.61
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.250
  SUBAREA RUNOFF(CFS) =      1.89
  TOTAL AREA(ACRES) =      0.44   PEAK FLOW RATE(CFS) =      1.89

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =    7.61
  RAINFALL INTENSITY(INCH/HR) =   4.86
  AREA-AVERAGED Fm(INCH/HR) =  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.25
  EFFECTIVE STREAM AREA(ACRES) =       0.44
  TOTAL STREAM AREA(ACRES) =       0.44
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       1.89

  ** CONFLUENCE DATA **
   STREAM       Q      Tc   Intensity   Fp(Fm)      Ap      Ae      HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)          (ACRES)     NODE
```

```
    1        3.69    9.32    4.331  0.40( 0.10) 0.25       1.0       1.00
    2        1.89    7.61    4.862  0.40( 0.10) 0.25       0.4       1.10

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        5.28    7.61    4.862  0.40( 0.10) 0.25       1.2       1.10
      2        5.37    9.32    4.331  0.40( 0.10) 0.25       1.4       1.00

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =       5.37    Tc(MIN.) =     9.32
  EFFECTIVE AREA(ACRES) =       1.41   AREA-AVERAGED Fm(INCH/HR) =  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap =  0.25
  TOTAL AREA(ACRES) =        1.4
  LONGEST FLOWPATH FROM NODE      1.00 TO NODE      2.00 =     423.27 FEET.
============================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.4  TC(MIN.) =      9.32
  EFFECTIVE AREA(ACRES) =      1.41  AREA-AVERAGED Fm(INCH/HR)=  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.250
  PEAK FLOW RATE(CFS)   =       5.37

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        5.28    7.61    4.862  0.40( 0.10) 0.25       1.2       1.10
      2        5.37    9.32    4.331  0.40( 0.10) 0.25       1.4       1.00
============================================================================
============================================================================
  END OF RATIONAL METHOD ANALYSIS
```

Phase 2B

Existing Conditions

```
**************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2B                                                               *
* EXISTING 2-YEAR STORM                                                  *
 **************************************************************************

  FILE NAME: YTC2B.DAT
  TIME/DATE OF STUDY: 17:22 11/11/2024
==========================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
==========================================================================
                     --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =    2.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)  (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0313 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

**************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
==========================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   300.00
  ELEVATION DATA: UPSTREAM(FEET) =    131.80  DOWNSTREAM(FEET) =    128.00

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.601
  *   2 YEAR RAINFALL INTENSITY(INCH/HR) =  1.780
  SUBAREA Tc AND LOSS RATE DATA(AMC  I ):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  APARTMENTS                  A        1.08      0.40     0.200    17    7.60
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.200
  SUBAREA RUNOFF(CFS) =      1.65
  TOTAL AREA(ACRES) =      1.08   PEAK FLOW RATE(CFS) =      1.65
================================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.1  TC(MIN.) =      7.60
  EFFECTIVE AREA(ACRES) =      1.08  AREA-AVERAGED Fm(INCH/HR)=  0.08
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.200
  PEAK FLOW RATE(CFS)   =       1.65
================================================================================
================================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
**************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2B                                                               *
* EXISTING 10-YEAR STORM                                                 *
 **************************************************************************

  FILE NAME: YTC2B10.DAT
  TIME/DATE OF STUDY: 17:28 11/11/2024
==========================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
==========================================================================
                     --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =   10.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)  (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0313 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

**************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
==========================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   300.00
  ELEVATION DATA: UPSTREAM(FEET) =    131.80  DOWNSTREAM(FEET) =    128.00

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.601
  *  10 YEAR RAINFALL INTENSITY(INCH/HR) =  3.193
  SUBAREA Tc AND LOSS RATE DATA(AMC  II):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  APARTMENTS                  A        1.08      0.40     0.200    32    7.60
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.200
  SUBAREA RUNOFF(CFS) =      3.03
  TOTAL AREA(ACRES) =      1.08   PEAK FLOW RATE(CFS) =      3.03
================================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.1  TC(MIN.) =      7.60
  EFFECTIVE AREA(ACRES) =      1.08  AREA-AVERAGED Fm(INCH/HR)=  0.08
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.200
  PEAK FLOW RATE(CFS)   =       3.03
================================================================================
================================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
**************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2B                                                               *
* EXISTING 25-YEAR STORM                                                 *
 ************************************************************************

  FILE NAME: YTC2B25.DAT
  TIME/DATE OF STUDY: 17:37 11/11/2024
========================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
========================================================================
                    --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =   25.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)   (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0313 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

**************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
==========================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   300.00
  ELEVATION DATA: UPSTREAM(FEET) =    131.80  DOWNSTREAM(FEET) =    128.00

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.601
  *  25 YEAR RAINFALL INTENSITY(INCH/HR) =  3.806
  SUBAREA Tc AND LOSS RATE DATA(AMC  II):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  APARTMENTS                  A        1.08      0.40     0.200    32    7.60
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.200
  SUBAREA RUNOFF(CFS) =      3.62
  TOTAL AREA(ACRES) =      1.08   PEAK FLOW RATE(CFS) =      3.62
================================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.1  TC(MIN.) =      7.60
  EFFECTIVE AREA(ACRES) =      1.08  AREA-AVERAGED Fm(INCH/HR)=  0.08
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.200
  PEAK FLOW RATE(CFS)   =       3.62
================================================================================
================================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
******************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2B                                                               *
* EXISTING 100-YEAR STORM                                                *
 ************************************************************************

  FILE NAME: YTC2B100.DAT
  TIME/DATE OF STUDY: 17:42 11/11/2024
================================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
================================================================================
                     --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =  100.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)  (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0313 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

******************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
------------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
================================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   300.00
  ELEVATION DATA: UPSTREAM(FEET) =    131.80  DOWNSTREAM(FEET) =    128.00

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.601
  * 100 YEAR RAINFALL INTENSITY(INCH/HR) =  4.867
  SUBAREA Tc AND LOSS RATE DATA(AMC III):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  APARTMENTS                  A        1.08      0.40     0.200    52    7.60
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.200
  SUBAREA RUNOFF(CFS) =      4.65
  TOTAL AREA(ACRES) =      1.08   PEAK FLOW RATE(CFS) =      4.65
================================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.1  TC(MIN.) =      7.60
  EFFECTIVE AREA(ACRES) =      1.08  AREA-AVERAGED Fm(INCH/HR)=  0.08
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.200
  PEAK FLOW RATE(CFS)   =       4.65
================================================================================
================================================================================
  END OF RATIONAL METHOD ANALYSIS
```

APPENDIX D

Proposed Hydrology

HYDROLOGIC SOIL GROUP: "A"

LEGEND

	MAJOR DRAINAGE BOUNDARY
	SUB-DRAINAGE BOUNDARY
	FLOWLINE
	DRAINAGE FLOW DIRECTION
(SD)	STORM DRAIN LINE
A1 / 0.12AC	SUBAREA DESIGNATION / SUBAREA (ACRES)
10	NODE NUMBER
123.4FS	PROPOSED FINISHED SURFACE ELEV.
123.4FG	PROPOSED FINISHED GRADE ELEV.
123.4INV	INVERT ELEV.
Q25	CALCULATED RUNOFF FOR 25 YR FREQ.
Tc	TIME OF CONCENTRATION
SD	STORM DRAIN
S	SLOPE
L	FLOW PATH LENGTH (SURFACE)
NAP	NOT A PART

Youth Transition Center

Long Term Housing

Classroom and Library Building

Independent Living

2A-1 0.97AC

2A-2 0.44AC

2B 1.08AC

Proposed Bioretention with No Underdrain (INF-3); 1,190 SF

Proposed Bioretention with No Underdrain (INF-3); 1,020 SF

SERVICE WAY

SIDWELL WAY

HOSPITAL FRONTAGE RD

JUSTICE CENTER WAY

ORANGEWOOD CHILDREN'S HOME

ORANGE COUNTY COURT MANCHESTER OFFICE

A.C. PARKING LOT

BREAK ROOM

ADMIN

MEDICAL UNIT

UNIT M

DENTAL

UNIT T

UNIT Q

UNIT B

UNIT C

UNIT Z

UNIT Y

ALLEY

LAMOREAUX JUSTICE CENTER

JUSTICE CENTER

CLASSROOMS

YLA 1

YLA 2

YLA ADMIN

AC PARKING LOT

BASKETBALL COURT

UTILITY ENCLOSURE

NORTH FIELD

SOCCER FIELD

M.R.C. BUILDING

LAUNDRY

KITCHEN

SUB STATION

SANTA ANA RIVER

SANTA ANA FWY (5)

SCALE: 1" = 40'

DRAINAGE CONDITIONS TABLE

Subarea	Area (SF)	Area (AC)	Pervious Area (SF)	Impervious Rate (%)	Soil Type	Pervious Rate (AES)
Existing Phase 2A	61,381.78	1.41	15,644.66	74.51%	A	25%
Proposed Phase 2A	61,381.78	1.41	22,140.30	63.93%	A	35%
Existing Phase 2B	47,190.68	1.08	7,860.61	83.34%	A	20%
Proposed Phase 2B	47,190.68	1.08	12,299.84	73.94%	A	25%

DRAINAGE CALCULATIONS TABLE

Subarea	Q_2 (CFS)	TC (Min)	Q_{10} (CFS)	TC (Min)	Q_{25} (CFS)	TC (Min)	Q_{100} (CFS)	TC (Min)
Existing Phase 2A	1.88	9.32	3.48	9.32	4.18	9.32	5.37	9.32
Proposed Phase 2A	1.75	9.98	3.29	9.98	3.96	9.98	5.10	9.98
Change	-0.13	0.66	-0.19	0.66	-0.22	0.66	-0.27	0.66
Existing Phase 2B	1.65	7.60	3.03	7.60	3.62	7.60	4.65	7.60
Proposed Phase 2B	1.60	7.88	2.94	7.88	3.53	7.88	4.54	7.88
Change	-0.05	0.28	-0.09	0.28	-0.09	0.28	-0.11	0.28

PREPARED FOR:
The County of Orange
601 N. ROSS STREET
SANTA ANA, CA 92701

PREPARED BY:
FUSCOE ENGINEERING
15535 Sand Canyon Ave, Suite 100
Irvine, California 92618
949.474.1960 fuscoe.com

County of Orange
OC Public Works
PROPOSED DRAINAGE AND LID BMP CONCEPTUAL PLAN
ORANGE COUNTY JUVENILE HALL
ORANGE COUNTY, CA
11/18/2024

E:\USERS\DRAINAGE\WORK\ENGINEERING\DOCUMENTS\OC_VISTA\OC_TOPO_2023-BASE_11072024-HYD.DWG [11-18-24 5:52:54PM] Plotted By: dsanchez

Phase 2A

Proposed Conditions

```
**************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2A                                                               *
* PROPOSED 2-YEAR STORM                                                  *
 **************************************************************************

  FILE NAME: YTC2AP.DAT
  TIME/DATE OF STUDY: 18:37 11/12/2024
==========================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
==========================================================================
                    --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =    2.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)   (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0313 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

**************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
==========================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   423.27
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    9.985
  *   2 YEAR RAINFALL INTENSITY(INCH/HR) =  1.522
  SUBAREA Tc AND LOSS RATE DATA(AMC  I ):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  CONDOMINIUMS                A        0.97      0.40     0.350    17    9.98
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.350
  SUBAREA RUNOFF(CFS) =      1.21
  TOTAL AREA(ACRES) =      0.97   PEAK FLOW RATE(CFS) =      1.21

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =    9.98
  RAINFALL INTENSITY(INCH/HR) =   1.52
  AREA-AVERAGED Fm(INCH/HR) =  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.35
  EFFECTIVE STREAM AREA(ACRES) =       0.97
  TOTAL STREAM AREA(ACRES) =       0.97
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       1.21

****************************************************************************
  FLOW PROCESS FROM NODE      1.10 TO NODE      2.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
============================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   302.28
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    8.159
  *   2 YEAR RAINFALL INTENSITY(INCH/HR) =  1.709
  SUBAREA Tc AND LOSS RATE DATA(AMC  I ):
   DEVELOPMENT TYPE/       SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE             GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
  CONDOMINIUMS                A        0.44      0.40     0.350    17    8.16
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.350
  SUBAREA RUNOFF(CFS) =      0.62
  TOTAL AREA(ACRES) =      0.44   PEAK FLOW RATE(CFS) =      0.62

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =    8.16
  RAINFALL INTENSITY(INCH/HR) =   1.71
  AREA-AVERAGED Fm(INCH/HR) =  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.35
  EFFECTIVE STREAM AREA(ACRES) =       0.44
  TOTAL STREAM AREA(ACRES) =       0.44
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       0.62

  ** CONFLUENCE DATA **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap      Ae      HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)          (ACRES)     NODE
```

```
    1        1.21    9.98    1.522  0.40( 0.14) 0.35       1.0       1.00
    2        0.62    8.16    1.709  0.40( 0.14) 0.35       0.4       1.10

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        1.74    8.16    1.709  0.40( 0.14) 0.35       1.2       1.10
      2        1.75    9.98    1.522  0.40( 0.14) 0.35       1.4       1.00

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =       1.75    Tc(MIN.) =     9.98
  EFFECTIVE AREA(ACRES) =       1.41   AREA-AVERAGED Fm(INCH/HR) =  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap =  0.35
  TOTAL AREA(ACRES) =        1.4
  LONGEST FLOWPATH FROM NODE      1.00 TO NODE      2.00 =     423.27 FEET.
============================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.4  TC(MIN.) =      9.98
  EFFECTIVE AREA(ACRES) =      1.41  AREA-AVERAGED Fm(INCH/HR)=  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.350
  PEAK FLOW RATE(CFS)   =       1.75

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        1.74    8.16    1.709  0.40( 0.14) 0.35       1.2       1.10
      2        1.75    9.98    1.522  0.40( 0.14) 0.35       1.4       1.00
============================================================================
============================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
**************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2A                                                               *
* PROPOSED 10-YEAR STORM                                                 *
 ************************************************************************

  FILE NAME: YTC2A10P.DAT
  TIME/DATE OF STUDY: 18:40 11/12/2024
========================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
========================================================================
                     --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =   10.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)   (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0312 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

**************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
==========================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   423.27
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    9.985
  *  10 YEAR RAINFALL INTENSITY(INCH/HR) =  2.731
  SUBAREA Tc AND LOSS RATE DATA(AMC  II):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  CONDOMINIUMS                A        0.97      0.40     0.350    32    9.98
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.350
  SUBAREA RUNOFF(CFS) =      2.26
  TOTAL AREA(ACRES) =      0.97   PEAK FLOW RATE(CFS) =      2.26

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =    9.98
  RAINFALL INTENSITY(INCH/HR) =   2.73
  AREA-AVERAGED Fm(INCH/HR) =  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.35
  EFFECTIVE STREAM AREA(ACRES) =       0.97
  TOTAL STREAM AREA(ACRES) =       0.97
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       2.26

****************************************************************************
  FLOW PROCESS FROM NODE      1.10 TO NODE      2.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
============================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   302.28
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    8.159
  *  10 YEAR RAINFALL INTENSITY(INCH/HR) =  3.066
  SUBAREA Tc AND LOSS RATE DATA(AMC  II):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
  CONDOMINIUMS                A        0.44      0.40     0.350    32    8.16
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.350
  SUBAREA RUNOFF(CFS) =      1.16
  TOTAL AREA(ACRES) =      0.44   PEAK FLOW RATE(CFS) =      1.16

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =    8.16
  RAINFALL INTENSITY(INCH/HR) =   3.07
  AREA-AVERAGED Fm(INCH/HR) =  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.35
  EFFECTIVE STREAM AREA(ACRES) =       0.44
  TOTAL STREAM AREA(ACRES) =       0.44
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       1.16

  ** CONFLUENCE DATA **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap      Ae      HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)          (ACRES)     NODE
```

```
    1        2.26    9.98    2.731  0.40( 0.14) 0.35       1.0       1.00
    2        1.16    8.16    3.066  0.40( 0.14) 0.35       0.4       1.10

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        3.25    8.16    3.066  0.40( 0.14) 0.35       1.2       1.10
      2        3.29    9.98    2.731  0.40( 0.14) 0.35       1.4       1.00

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =       3.29    Tc(MIN.) =     9.98
  EFFECTIVE AREA(ACRES) =       1.41   AREA-AVERAGED Fm(INCH/HR) =  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap =  0.35
  TOTAL AREA(ACRES) =        1.4
  LONGEST FLOWPATH FROM NODE      1.00 TO NODE      2.00 =     423.27 FEET.
============================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.4  TC(MIN.) =      9.98
  EFFECTIVE AREA(ACRES) =      1.41  AREA-AVERAGED Fm(INCH/HR)=  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.350
  PEAK FLOW RATE(CFS)   =       3.29

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        3.25    8.16    3.066  0.40( 0.14) 0.35       1.2       1.10
      2        3.29    9.98    2.731  0.40( 0.14) 0.35       1.4       1.00
============================================================================
============================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
**************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2A                                                               *
* PROPOSED 25-YEAR STORM                                                 *
 **************************************************************************

  FILE NAME: YTC2A25P.DAT
  TIME/DATE OF STUDY: 18:41 11/12/2024
==========================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
==========================================================================
                     --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =   25.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)   (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0312 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

**************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
==========================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   423.27
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    9.985
  *  25 YEAR RAINFALL INTENSITY(INCH/HR) =  3.261
  SUBAREA Tc AND LOSS RATE DATA(AMC  II):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  CONDOMINIUMS                A        0.97      0.40     0.350    32    9.98
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.350
  SUBAREA RUNOFF(CFS) =      2.72
  TOTAL AREA(ACRES) =      0.97   PEAK FLOW RATE(CFS) =      2.72

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =    9.98
  RAINFALL INTENSITY(INCH/HR) =   3.26
  AREA-AVERAGED Fm(INCH/HR) =  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.35
  EFFECTIVE STREAM AREA(ACRES) =       0.97
  TOTAL STREAM AREA(ACRES) =       0.97
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       2.72

****************************************************************************
  FLOW PROCESS FROM NODE      1.10 TO NODE      2.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
============================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   302.28
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    8.159
  *  25 YEAR RAINFALL INTENSITY(INCH/HR) =  3.656
  SUBAREA Tc AND LOSS RATE DATA(AMC  II):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
  CONDOMINIUMS                A        0.44      0.40     0.350    32    8.16
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.350
  SUBAREA RUNOFF(CFS) =      1.39
  TOTAL AREA(ACRES) =      0.44   PEAK FLOW RATE(CFS) =      1.39

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =    8.16
  RAINFALL INTENSITY(INCH/HR) =   3.66
  AREA-AVERAGED Fm(INCH/HR) =  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.35
  EFFECTIVE STREAM AREA(ACRES) =       0.44
  TOTAL STREAM AREA(ACRES) =       0.44
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       1.39

  ** CONFLUENCE DATA **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap      Ae      HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)          (ACRES)    NODE
```

```
    1        2.72    9.98    3.261  0.40( 0.14) 0.35       1.0       1.00
    2        1.39    8.16    3.656  0.40( 0.14) 0.35       0.4       1.10

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        3.90    8.16    3.656  0.40( 0.14) 0.35       1.2       1.10
      2        3.96    9.98    3.261  0.40( 0.14) 0.35       1.4       1.00

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =       3.96    Tc(MIN.) =     9.98
  EFFECTIVE AREA(ACRES) =       1.41   AREA-AVERAGED Fm(INCH/HR) =  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap =  0.35
  TOTAL AREA(ACRES) =        1.4
  LONGEST FLOWPATH FROM NODE      1.00 TO NODE      2.00 =     423.27 FEET.
============================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.4  TC(MIN.) =      9.98
  EFFECTIVE AREA(ACRES) =      1.41  AREA-AVERAGED Fm(INCH/HR)=  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.350
  PEAK FLOW RATE(CFS)   =       3.96

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        3.90    8.16    3.656  0.40( 0.14) 0.35       1.2       1.10
      2        3.96    9.98    3.261  0.40( 0.14) 0.35       1.4       1.00
============================================================================
============================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
******************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2A                                                               *
* PROPOSED 100-YEAR STORM                                                *
 ************************************************************************

  FILE NAME: YT2A100P.DAT
  TIME/DATE OF STUDY: 18:44 11/12/2024
==============================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
==============================================================================
                    --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =  100.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)   (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0312 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

******************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
------------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
==============================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   423.27
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    9.985
  * 100 YEAR RAINFALL INTENSITY(INCH/HR) =  4.163
  SUBAREA Tc AND LOSS RATE DATA(AMC III):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  CONDOMINIUMS                A        0.97      0.40     0.350    52    9.98
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.350
  SUBAREA RUNOFF(CFS) =      3.51
  TOTAL AREA(ACRES) =      0.97   PEAK FLOW RATE(CFS) =      3.51

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
  TIME OF CONCENTRATION(MIN.) =    9.98
  RAINFALL INTENSITY(INCH/HR) =   4.16
  AREA-AVERAGED Fm(INCH/HR) =  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.35
  EFFECTIVE STREAM AREA(ACRES) =       0.97
  TOTAL STREAM AREA(ACRES) =       0.97
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       3.51

****************************************************************************
  FLOW PROCESS FROM NODE      1.10 TO NODE      2.00 IS CODE =  21
----------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
============================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   302.28
  ELEVATION DATA: UPSTREAM(FEET) =    131.50  DOWNSTREAM(FEET) =    126.88

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    8.159
  * 100 YEAR RAINFALL INTENSITY(INCH/HR) =  4.674
  SUBAREA Tc AND LOSS RATE DATA(AMC III):
   DEVELOPMENT TYPE/       SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE             GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
  CONDOMINIUMS                A        0.44      0.40     0.350    52    8.16
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.350
  SUBAREA RUNOFF(CFS) =      1.80
  TOTAL AREA(ACRES) =      0.44   PEAK FLOW RATE(CFS) =      1.80

****************************************************************************
  FLOW PROCESS FROM NODE      2.00 TO NODE      2.00 IS CODE =   1
----------------------------------------------------------------------------
  >>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
  >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
============================================================================
  TOTAL NUMBER OF STREAMS =  2
  CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  2 ARE:
  TIME OF CONCENTRATION(MIN.) =    8.16
  RAINFALL INTENSITY(INCH/HR) =   4.67
  AREA-AVERAGED Fm(INCH/HR) =  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40
  AREA-AVERAGED Ap =  0.35
  EFFECTIVE STREAM AREA(ACRES) =       0.44
  TOTAL STREAM AREA(ACRES) =       0.44
  PEAK FLOW RATE(CFS) AT CONFLUENCE =       1.80

  ** CONFLUENCE DATA **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap      Ae      HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)          (ACRES)     NODE
```

```
    1        3.51    9.98    4.163  0.40( 0.14) 0.35       1.0       1.00
    2        1.80    8.16    4.674  0.40( 0.14) 0.35       0.4       1.10

  RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
  CONFLUENCE FORMULA USED FOR  2 STREAMS.

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        5.03    8.16    4.674  0.40( 0.14) 0.35       1.2       1.10
      2        5.10    9.98    4.163  0.40( 0.14) 0.35       1.4       1.00

  COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
  PEAK FLOW RATE(CFS) =       5.10    Tc(MIN.) =     9.98
  EFFECTIVE AREA(ACRES) =       1.41   AREA-AVERAGED Fm(INCH/HR) =  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap =  0.35
  TOTAL AREA(ACRES) =        1.4
  LONGEST FLOWPATH FROM NODE      1.00 TO NODE      2.00 =     423.27 FEET.
============================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.4  TC(MIN.) =      9.98
  EFFECTIVE AREA(ACRES) =      1.41  AREA-AVERAGED Fm(INCH/HR)=  0.14
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.350
  PEAK FLOW RATE(CFS)   =       5.10

  ** PEAK FLOW RATE TABLE **
   STREAM       Q      Tc   Intensity   Fp(Fm)     Ap     Ae     HEADWATER
   NUMBER     (CFS)   (MIN.) (INCH/HR) (INCH/HR)         (ACRES)    NODE
      1        5.03    8.16    4.674  0.40( 0.14) 0.35       1.2       1.10
      2        5.10    9.98    4.163  0.40( 0.14) 0.35       1.4       1.00
============================================================================
============================================================================
  END OF RATIONAL METHOD ANALYSIS
```

Phase 2B

Proposed Conditions

```
**************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2B                                                               *
* PROPOSED 2-YEAR STORM                                                  *
 ************************************************************************

  FILE NAME: YTC2BP.DAT
  TIME/DATE OF STUDY: 17:24 11/11/2024
========================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
========================================================================
                    --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =    2.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)   (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0313 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

**************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
--------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
==========================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   300.00
  ELEVATION DATA: UPSTREAM(FEET) =    131.80  DOWNSTREAM(FEET) =    128.00

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.882
  *   2 YEAR RAINFALL INTENSITY(INCH/HR) =  1.743
  SUBAREA Tc AND LOSS RATE DATA(AMC  I ):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  MOBILE HOME PARK           A        1.08      0.40     0.250    17    7.88
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.250
  SUBAREA RUNOFF(CFS) =      1.60
  TOTAL AREA(ACRES) =      1.08   PEAK FLOW RATE(CFS) =      1.60
================================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.1  TC(MIN.) =      7.88
  EFFECTIVE AREA(ACRES) =      1.08  AREA-AVERAGED Fm(INCH/HR)=  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.250
  PEAK FLOW RATE(CFS)   =       1.60
================================================================================
================================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
******************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2B                                                               *
* PROPOSED 10-YEAR STORM                                                 *
 ************************************************************************

  FILE NAME: YTC2B10P.DAT
  TIME/DATE OF STUDY: 17:30 11/11/2024
================================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
================================================================================
                     --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =   10.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)   (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0313 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

******************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
------------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
================================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   300.00
  ELEVATION DATA: UPSTREAM(FEET) =    131.80  DOWNSTREAM(FEET) =    128.00

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.882
  *  10 YEAR RAINFALL INTENSITY(INCH/HR) =  3.128
  SUBAREA Tc AND LOSS RATE DATA(AMC  II):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  MOBILE HOME PARK           A        1.08      0.40     0.250    32    7.88
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.250
  SUBAREA RUNOFF(CFS) =      2.94
  TOTAL AREA(ACRES) =      1.08   PEAK FLOW RATE(CFS) =      2.94
================================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.1  TC(MIN.) =      7.88
  EFFECTIVE AREA(ACRES) =      1.08  AREA-AVERAGED Fm(INCH/HR)=  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.250
  PEAK FLOW RATE(CFS)   =       2.94
================================================================================
================================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
******************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2B                                                               *
* PROPOSED 25-YEAR STORM                                                 *
 ************************************************************************

  FILE NAME: YTC2B25P.DAT
  TIME/DATE OF STUDY: 17:37 11/11/2024
==============================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
==============================================================================
                     --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =   25.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)   (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0312 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

******************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
------------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
==============================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   300.00
  ELEVATION DATA: UPSTREAM(FEET) =    131.80  DOWNSTREAM(FEET) =    128.00

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.882
  *  25 YEAR RAINFALL INTENSITY(INCH/HR) =  3.728
  SUBAREA Tc AND LOSS RATE DATA(AMC  II):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  MOBILE HOME PARK           A        1.08      0.40     0.250    32    7.88
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.250
  SUBAREA RUNOFF(CFS) =      3.53
  TOTAL AREA(ACRES) =      1.08   PEAK FLOW RATE(CFS) =      3.53
================================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.1  TC(MIN.) =      7.88
  EFFECTIVE AREA(ACRES) =      1.08  AREA-AVERAGED Fm(INCH/HR)=  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.250
  PEAK FLOW RATE(CFS)   =       3.53
================================================================================
================================================================================
  END OF RATIONAL METHOD ANALYSIS
```

```
******************************************************************************
            RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
           (Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
         (c) Copyright 1983-2016 Advanced Engineering Software (aes)
             Ver. 23.0  Release Date: 07/01/2016  License ID 1355

                          Analysis prepared by:

                         Fuscoe Engineering, Inc.
                          15535 Sand Canyon Ave
                                Suite 100
                             Irvine, CA 92618

 ************************* DESCRIPTION OF STUDY *************************
* ORANGE COUNTY YOUTH TRANSITION CENTER                                  *
* PHASE 2B                                                               *
* PROPOSED 100-YEAR STORM                                                *
 ************************************************************************

  FILE NAME: YT2B100P.DAT
  TIME/DATE OF STUDY: 17:44 11/11/2024
==============================================================================
  USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
==============================================================================
                    --*TIME-OF-CONCENTRATION MODEL*--

  USER SPECIFIED STORM EVENT(YEAR) =  100.00
  SPECIFIED MINIMUM PIPE SIZE(INCH) =   4.00
  SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
  *DATA BANK RAINFALL USED*
  *ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD*

  *USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL*
     HALF-  CROWN TO   STREET-CROSSFALL:   CURB  GUTTER-GEOMETRIES:  MANNING
     WIDTH  CROSSFALL  IN-  / OUT-/PARK-  HEIGHT  WIDTH  LIP   HIKE  FACTOR
NO.   (FT)     (FT)    SIDE / SIDE/ WAY    (FT)    (FT)  (FT)  (FT)    (n)
===  =====  =========  =================  ======  ===== ====== ===== =======
  1   30.0     20.0    0.018/0.018/0.020   0.67    2.00 0.0313 0.167 0.0150

  GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
    1. Relative Flow-Depth =  0.00 FEET
       as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
    2. (Depth)*(Velocity) Constraint =  6.0 (FT*FT/S)
  *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
   OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
  *USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

******************************************************************************
  FLOW PROCESS FROM NODE      1.00 TO NODE      2.00 IS CODE =  21
------------------------------------------------------------------------------
  >>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
  >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
==============================================================================
  INITIAL SUBAREA FLOW-LENGTH(FEET) =   300.00
  ELEVATION DATA: UPSTREAM(FEET) =    131.80  DOWNSTREAM(FEET) =    128.00

  Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
  SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) =    7.882
  * 100 YEAR RAINFALL INTENSITY(INCH/HR) =  4.767
  SUBAREA Tc AND LOSS RATE DATA(AMC III):
   DEVELOPMENT TYPE/      SCS SOIL   AREA      Fp         Ap      SCS   Tc
       LAND USE            GROUP   (ACRES)  (INCH/HR)  (DECIMAL)  CN  (MIN.)
```

```
  MOBILE HOME PARK           A        1.08      0.40     0.250    52    7.88
  SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) =  0.40
  SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap =  0.250
  SUBAREA RUNOFF(CFS) =      4.54
  TOTAL AREA(ACRES) =      1.08   PEAK FLOW RATE(CFS) =      4.54
================================================================================
  END OF STUDY SUMMARY:
  TOTAL AREA(ACRES)     =        1.1  TC(MIN.) =      7.88
  EFFECTIVE AREA(ACRES) =      1.08  AREA-AVERAGED Fm(INCH/HR)=  0.10
  AREA-AVERAGED Fp(INCH/HR) =  0.40  AREA-AVERAGED Ap = 0.250
  PEAK FLOW RATE(CFS)   =       4.54
================================================================================
================================================================================
  END OF RATIONAL METHOD ANALYSIS
```

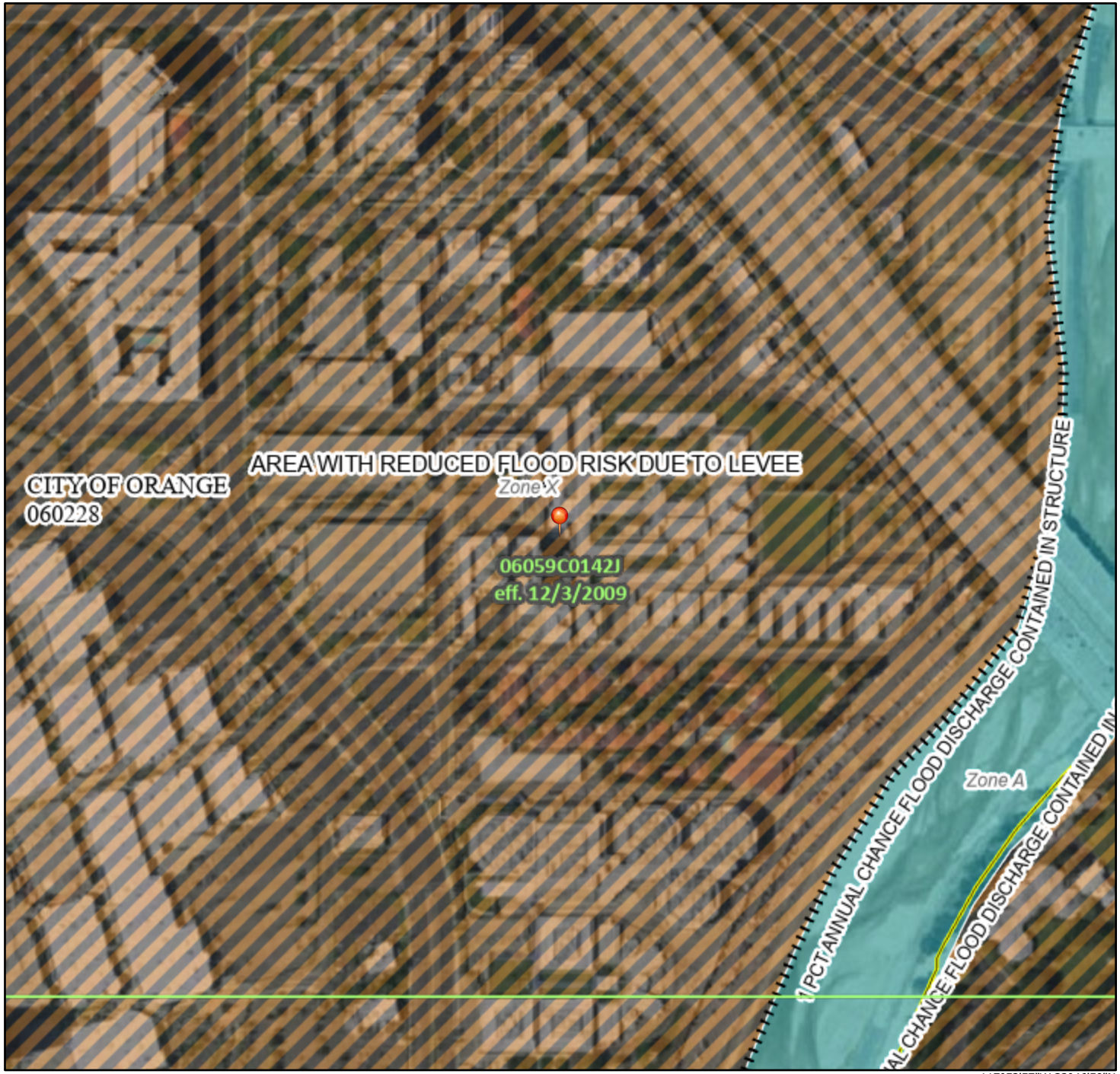
APPENDIX E

FEMA Map

National Flood Hazard Layer FIRMette

FEMA

117°53'34"W 33°47'20"N



0 250 500 1,000 1,500 2,000 Feet

1:6,000

117°52'57"W 33°46'50"N

Basemap Imagery Source: USGS National Map 2023

Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS
- Without Base Flood Elevation (BFE) *Zone A, V, A99*
- With BFE or Depth *Zone AE, AO, AH, VE, AR*
- Regulatory Floodway

OTHER AREAS OF FLOOD HAZARD
- 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile *Zone X*
- Future Conditions 1% Annual Chance Flood Hazard *Zone X*
- Area with Reduced Flood Risk due to Levee. See Notes. *Zone X*
- Area with Flood Risk due to Levee *Zone D*

OTHER AREAS
- NO SCREEN Area of Minimal Flood Hazard *Zone X*
- Effective LOMRs
- Area of Undetermined Flood Hazard *Zone D*

GENERAL STRUCTURES
- Channel, Culvert, or Storm Sewer
- Levee, Dike, or Floodwall

OTHER FEATURES
- 20.2 Cross Sections with 1% Annual Chance
- 17.5 Water Surface Elevation
- Coastal Transect
- Base Flood Elevation Line (BFE)
- Limit of Study
- Jurisdiction Boundary
- Coastal Transect Baseline
- Profile Baseline
- Hydrographic Feature

MAP PANELS
- Digital Data Available
- No Digital Data Available
- Unmapped

N

The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 11/14/2024 at 1:03 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.