

**PRELIMINARY  
DRAINAGE STUDY**

**J@B STORAGE**

**County of Sacramento, California**

**March 29, 2024 (v.3)**



**Prepared by:**



**5220 BRADSHAW ROAD & 9680 JACKSON ROAD**

**DRAINAGE STUDY  
FOR  
5220 BRADSHAW ROAD & 9680 JACKSON ROAD  
J & B STORAGE IMPROVEMENTS**

M&P Project No. 18-0053-00

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Sacramento, California

March 29, 2024

**PREPARED BY:**



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## **PROJECT BACKGROUND**

The Jackson and Bradshaw project is located within the County of Sacramento, California. The project footprint is approximately 7.1 acres, and it is bounded by Jackson Road to the north and Bradshaw Road to the south. Improvements include 400 square foot office with associated parking, truck parking, water, sewer, and storm drain. See **Appendix-A** for Boundary and Topographic Survey.

## **OBJECTIVE**

The primary objective of this drainage study is to satisfy the County's drainage design requirements by evaluating the drainage impacts of the proposed project to the County's existing storm drain system on Bradshaw Road.

## **SITE HYDROLOGY / HYDRAULIC ANALYSIS**

### **PRE-DEVELOPMENT CONDITIONS**

The topography of the site is generally flat with the elevations varying from 63 to 66 feet in elevation. The general drainage pattern of the property is to drain from north to south into a roadside existing ditch on the East side of the property. See **Appendix-A** for Boundary and Topographic Survey.

The undeveloped shed was modeled with the SacCalc software to reflect existing conditions. The shed was modeled for a 10-year 24-hour storm event. The project location has an average existing slope of 0.67%. With SacCalc, it was determined that the existing conditions during a 10-year 24-hour storm event produces a peak discharge of 7.8 cubic feet per second. See **Appendix-B** for the Pre-Development SacCalc Watershed Map. Refer to the Pre-Development SacCalc Results in **Appendix-D**.

### **POST-DEVELOPMENT CONDITIONS**

This proposed development will primarily include truck parking with porous gravel pavement and concrete pavement for the drive aisles. The porous gravel pavement and a new bioretention basin will be constructed to provide Low Impact Development (LID) / treatment measures prior to discharge to the County's storm drain system.

The following table summarizes the bioretention basin's characteristics and storage capacities. (Refer to the Post-Development Drainage Watershed Map in **Appendix-C** for basin location).

**Table 1 – BIORETENTION BASIN NO.1 (Volume – Depth – Elevation Relationship)**

| Elevation, ft | Depth, ft | Volume, cf | Volume, ac-ft |
|---------------|-----------|------------|---------------|
| 60            | 0         | 0          | 0             |
| 61            | 1.0       | 12,502     | 0.287         |
| 62            | 2.0       | 29,969     | 0.688         |
| 63            | 3.0       | 52,403     | 1.203         |

The post-development shed, and bioretention parameters were incorporated into the SacCalc model. For a 10-year 24-hour storm event, the proposed shed produces a peak discharge of 12 cubic feet per second. An 18-inch pipe is placed at the outlet for the bioretention basin which allows the 10-year flow rate to be reduced to 6.9 cubic feet per second. This provides a storage elevation of 61.3 feet that requires a storage volume capacity of 0.40 acre-feet. Refer to the Post-Development SacCalc Results in **Appendix-D**.

### **NOLTE HGL ANALYSIS**

The design runoff (peak flows) was computed using the Nolte Chart, Figure 2-5 of the County's Hydrology Manual (Volume 2) in **Appendix-E**. For each sub-watershed area, the Nolte design flows were computed accordingly.

The starting HGL for Nolte design event is assumed to be at the top of the existing 60-inch storm drainpipe at the proposed manhole (Node MH-1) located on Bradshaw Road at the southeast corner of the project. The flowline of the 60-inch pipe is approximately 53.56 feet (NAVD 88), therefore the assumed HGL is 59.0 feet (NAVD 88). See **Appendix-F** for the Nolte Watershed Map.

Results show that the HGLs remain within the entire drain system and flows are conveyed to the point of connection to the existing storm drain system located within Bradshaw Road. Refer to **Appendix-F** for the Nolte Hydraflow Results.

## **LOW IMPACT DEVELOPMENT (LID) AND HYDROMODIFICATION**

The project will provide an integrated storm water management system that would meet the County of Sacramento's Low Impact Development (LID), storm water quality treatment, and flood control requirements. This strategy will be implemented throughout the project site to ensure storm water runoff is captured, stored, and naturally treated on-site, thereby resulting in a cleaner discharge to the receiving drainage system.

## **LOW IMPACT DEVELOPMENT (LID)**

Storm water quality design standards shall be based on the Stormwater Quality Design Manual, Integrated Design Solutions for Urban Development, (July 2018) manual. Planting new trees, providing porous gravel pavement, and constructing a bioretention basin will be used to satisfy the project's LID requirements.

Based on the County of Sacramento's Storm Water Quality Design Manual, LID measures will include the following:

- Total project shed area served = 7.10 acres
- Future commercial areas assumed to be 90% impervious
- Porous gravel pavement area: Total shed area served = 2.28 acres
- Bioretention basin
  - Bioretention area = 5,150SF total
- Proposed landscaped/open space areas = 1.35 acres

Refer to **Appendix-G** for the post-development stormwater quality watershed map.

Based on the Commercial LID calculations worksheet in the County's Storm Water Quality Design Manual (see **Appendix-G** for the LID Worksheets), the project utilized a combination of a porous gravel pavement and a new bioretention basin to achieve LID compliance.

## **TRASH CAPTURE**

Trash capture requirements will be met with the utilization of one (1) on-site bioretention basins at the discharge outlets.

## **HYDROMODIFICATION**

Per the Hydromodification Map in the Stormwater Quality Design Manual (see **Appendix-H**), Hydromodification will be required because the project is located within the applicable zone of the County of Sacramento. The SAHM model was utilized to analyze the flow rate impact based on the improvement plans and proposed LID measures. See **Appendix-I** for SAHM Project Report.

## **STORM DRAIN TIE-IN TO BRADSHAW ROAD**

The site will be served by the County's existing storm drain system on Bradshaw Road near the East side of the property. See **Appendix-J** for the grading plan.

## SUMMARY OF RESULTS

The following table summarizes the pre- and post-development 10- and 100-year 24-hour peak flow rates:

**Table 2 – Pre- and Post-Development Design Storm Flow Rates**

| Condition | Outfall                      | 10-Year 24-Hour, cfs | 100-Year 24-Hour, cfs |
|-----------|------------------------------|----------------------|-----------------------|
| Existing  | EXSHED                       | 7.8                  | 13                    |
|           | PROSHD                       | 23                   | 20                    |
| Proposed  | Outfall to Bradshaw at DE001 | 6.9                  | 12                    |

In summary:

- The proposed site will meet the County of Sacramento LID and storm water quality treatment requirements. Low Impact Development (LID) will be provided via porous pavement and a new bioretention basin. Storm water quality treatment will be provided by the on-site porous pavement and bioretention basin prior to the discharge point.
- Hydromodification is not required based on proposed LID treatments.
- Using County criteria for peak runoffs, it was determined that the Notle HGL of the on-site drainage system will be below the ground surface at all locations.
- The 10-year detention volume requirement of 0.27 acre-feet of water can be fully accommodated by the proposed bioretention basin, which will have a total holding capacity of 0.93 acre-feet of storm water.

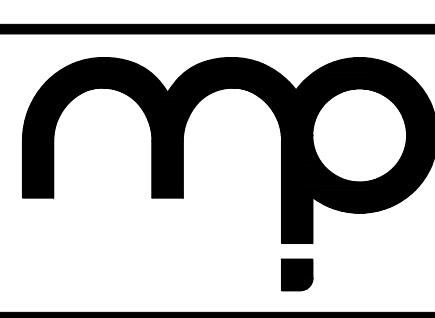
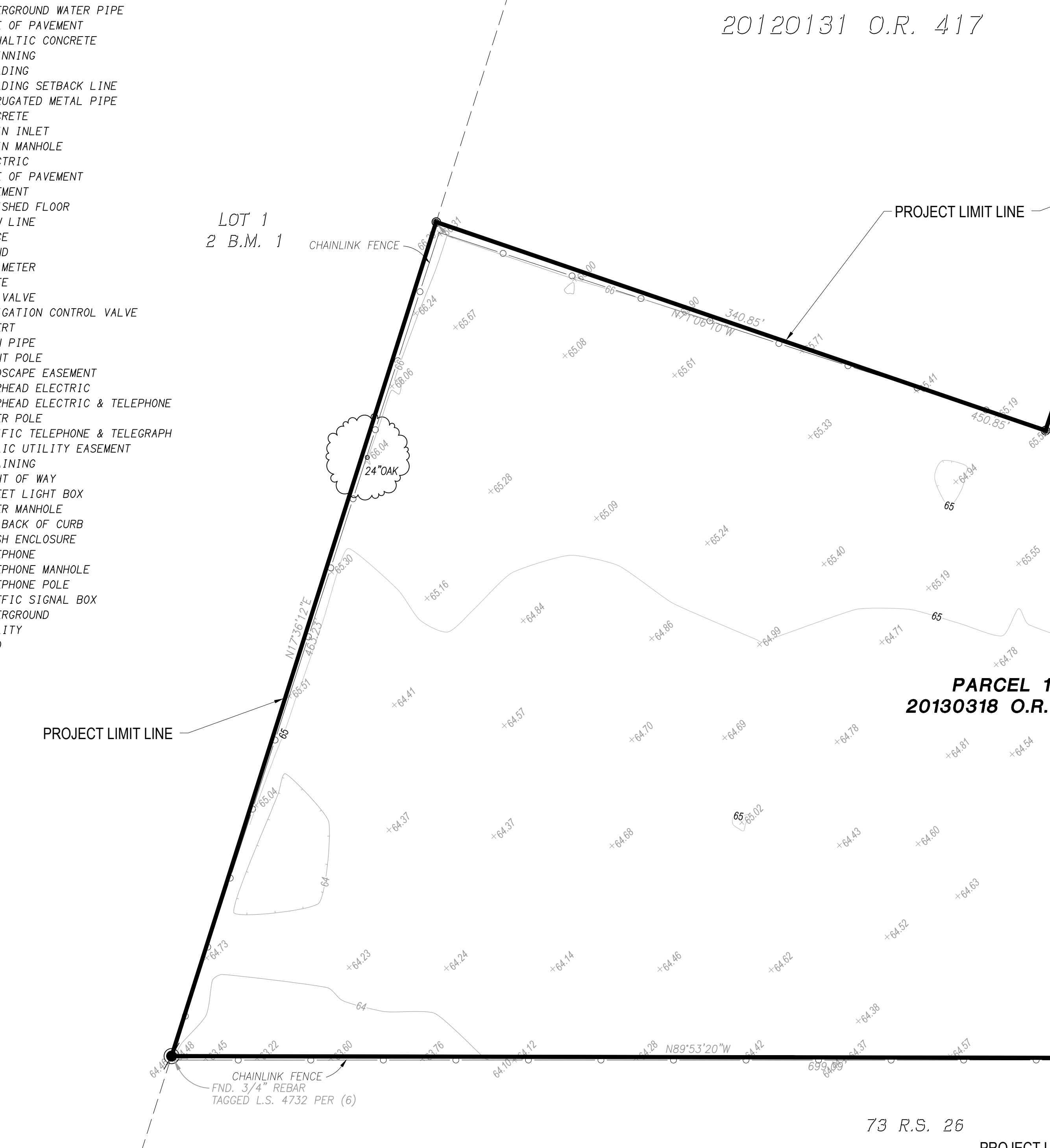
## REFERENCES

1. Volume 2 of the Sacramento City/County Drainage Manual, Hydrology Standards, County of Sacramento, December 1996.
2. Stormwater Quality Design Manual, Integrated Design Solutions for Urban Development, July 2018.

**APPENDIX A:**  
**Boundary and Topographic Survey**

**LEGEND**

- POWER OR TELEPHONE POLE W/GUY
- AREA LIGHT OR POLE LIGHT
- STREET LIGHT (ELECTROLITE)
- TRAFFIC SIGNAL
- TRANSFORMER
- MANHOLE
- CLEANOUT
- CURB INLET
- DRAIN INLET
- FIRE HYDRANT
- FIRE DEPARTMENT CONNECTION
- WATER METER
- WATER VALVE
- BACKFLOW PREVENTOR
- DOUBLE DETECTOR CHECK VALVE
- BLOW OFF VALVE
- POST INDICATOR VALVE
- POINT
- MONUMENT FOUND AS NOTED
- ROAD SIGN
- UNDERGROUND SEWER PIPE
- UNDERGROUND STORM DRAIN PIPE
- UNDERGROUND WATER PIPE
- EDGE OF PAVEMENT
- AC ASPHALTIC CONCRETE
- BEG BEGINNING
- BLDG BUILDING
- BSL BUILDING SETBACK LINE
- CMP CORROUGATED METAL PIPE
- CONC CONCRETE
- DI DRAIN INLET
- DMH DRAIN MANHOLE
- ELEC ELECTRIC
- EP EDGE OF PAVEMENT
- ESMT EASEMENT
- FF FINISHED FLOOR
- FL FLOW LINE
- FNC FENCE
- FND FOUND
- GM GAS METER
- GRT GRATE
- GV GAS VALVE
- ICV IRRIGATION CONTROL VALVE
- INV INVERT
- I.P. IRON PIPE
- JP JOINT POLE
- L.E. LANDSCAPE EASEMENT
- OHE OVERHEAD ELECTRIC
- OHT&E OVERHEAD ELECTRIC & TELEPHONE
- PP POWER POLE
- PT&T PACIFIC TELEPHONE & TELEGRAPH
- P.U.E. PUBLIC UTILITY EASEMENT
- RET RETAINING
- R/W RIGHT OF WAY
- SLB STREET LIGHT BOX
- SMH SEWER MANHOLE
- TBC TOP BACK OF CURB
- T.E. TRASH ENCLOSURE
- TELE TELEPHONE
- TMH TELEPHONE MANHOLE
- TP TELEPHONE POLE
- TSB TRAFFIC SIGNAL BOX
- UG UNDERGROUND
- UTIL UTILITY
- WD WOOD



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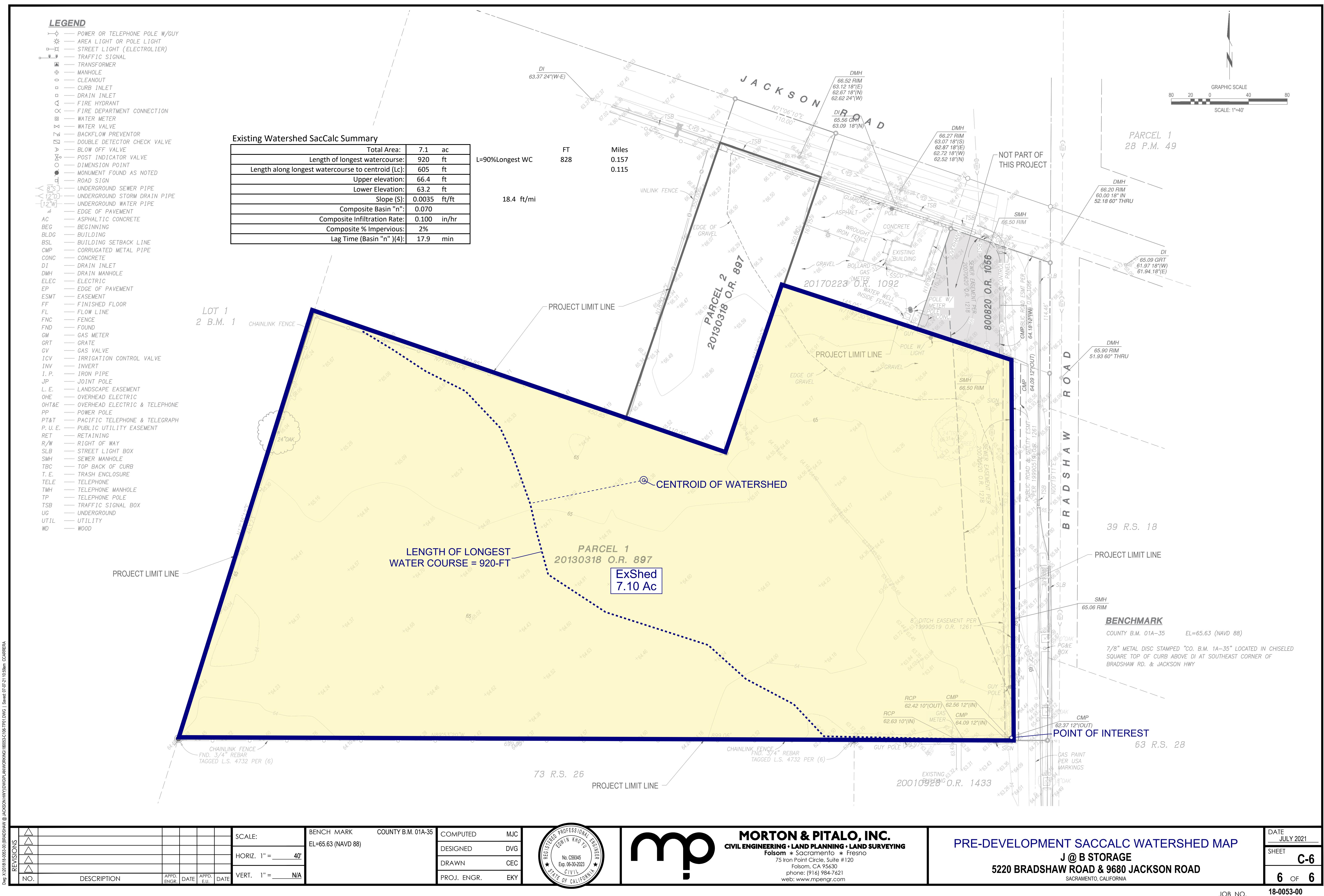
**BOUNDARY AND TOPOGRAPHIC SURVEY**  
**J @ B STORAGE**  
**5220 BRADSHAW ROAD & 9680 JACKSON ROAD**  
SACRAMENTO, CALIFORNIA

DATE  
JULY 2021  
SHEET  
C-6  
OF  
6 OF 6

| REVISIONS | DESCRIPTION | APPD. ENGR. | DATE APPD. E.U. | DATE | SCALE:                            | BENCH MARK COUNTY B.M. 01A-35 | COMPUTED MJC                                 |
|-----------|-------------|-------------|-----------------|------|-----------------------------------|-------------------------------|--|
|           |             |             |                 |      | HORIZ. 1" = 40'<br>VERT. 1" = N/A |                               | DESIGNED DVG<br>DRAWN CEC<br>PROJ. ENGR. EKY |

GRAPHIC SCALE  
80 20 0 40 80  
SCALE: 1"=40'

**APPENDIX B:**  
**Pre-Development SacCalc Watershed Map**



## **APPENDIX C:**

### **Post-Development SacCalc Watershed Map**

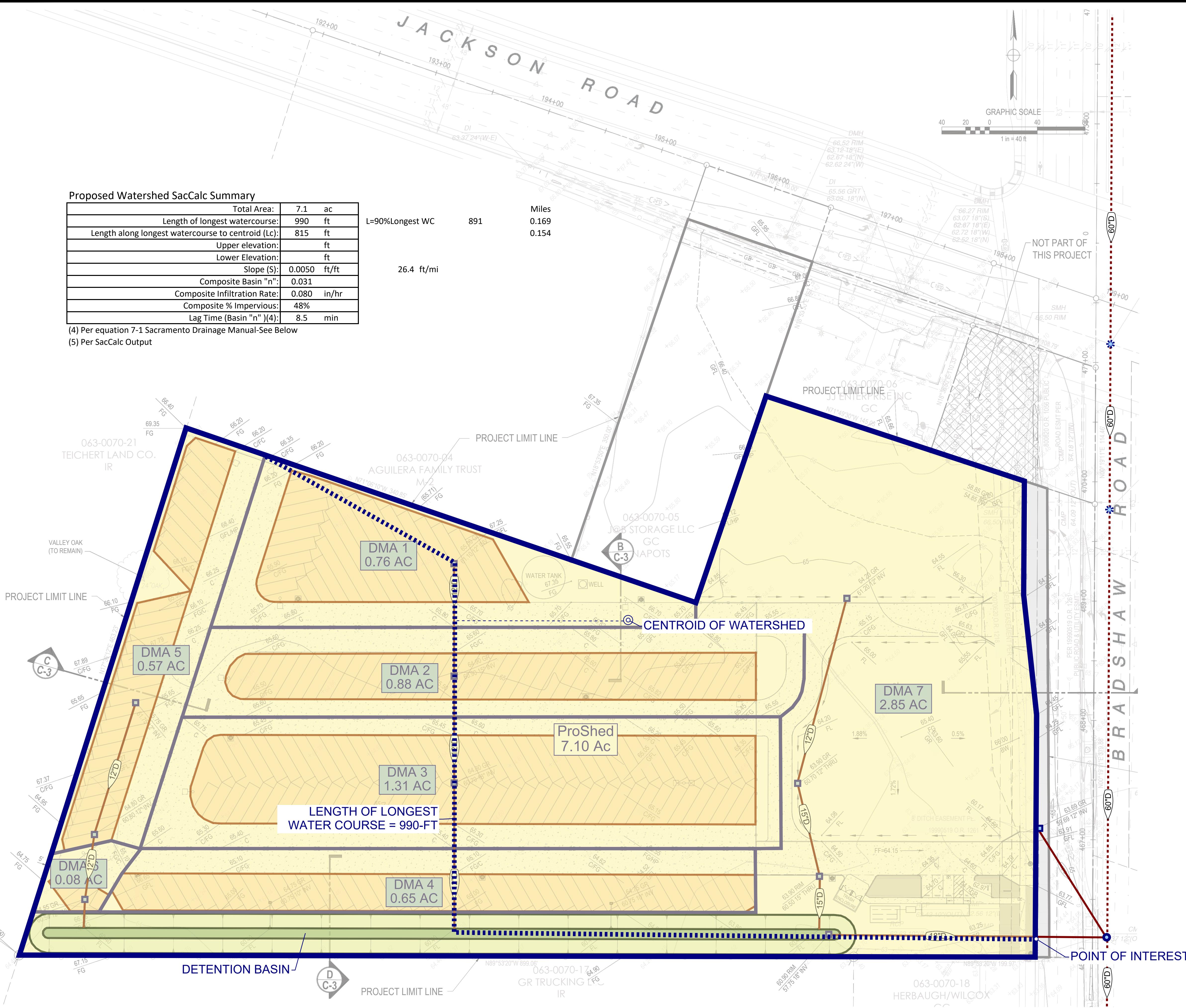
| LEGEND: |                           |
|---------|---------------------------|
|         | WATERSHED BOUNDARY        |
|         | BIORETENTION BASIN        |
|         | POROUS GRAVEL PAVEMENT    |
|         | PROPOSED DI               |
|         | PROPOSED DRAINAGE MANHOLE |
|         | EXISTING DRAINAGE MANHOLE |
|         | PROPOSED STORM DRAIN PIPE |
|         | EXISTING STORM DRAIN PIPE |

#### Proposed Watershed SacCalc Summary

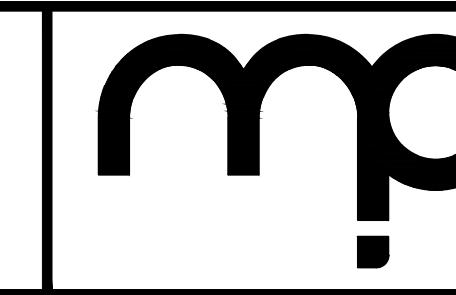
|  |              |
|--|--------------|
| Total Area:  | 7.1 ac       |
| Length of longest watercourse:                     | 990 ft       |
| Length along longest watercourse to centroid (Lc): | 815 ft       |
| Upper elevation:                                   | ft           |
| Lower Elevation:                                   | ft           |
| Slope (S):   | 0.0050 ft/ft |
| Composite Basin "n":                               | 0.031        |
| Composite Infiltration Rate:                       | 0.080 in/hr  |
| Composite % Impervious:                            | 48%          |
| Lag Time (Basin "n") <sup>(4)</sup> :              | 8.5 min      |

(4) Per equation 7-1 Sacramento Drainage Manual-See Below

(5) Per SacCalc Output



| REVISIONS |             | SCALE:      |      | BENCH MARK |      | COUNTY B.M. 01A-35 |  | COMPUTED    |     | MJC |  |
|-----------|-------------|-------------|------|------------|------|--------------------|--|-------------|-----|-----|--|
|           |             | HORIZ.      | 1" = | 40'        |      |                    |  | DESIGNED    | DVG |     |  |
|           |             | VERT.       | 1" = | N/A        |      |                    |  | DRAWN       | CEC |     |  |
| NO.       | DESCRIPTION | APPD. ENGR. | DATE | APPD. EU.  | DATE |                    |  | PROJ. ENGR. | EKY |     |  |



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**POST-DEVELOPMENT SACCALC WATERSHED MAP**  
**J @ B STORAGE**  
**5220 BRADSHAW ROAD & 9680 JACKSON ROAD**  
SACRAMENTO, CALIFORNIA

|                    |
|--------------------|
| DATE<br>MARCH 2024 |
| SHEET<br>C-2       |
| 2 OF 6             |

## **APPENDIX D:**

### **Pre- and Post-Development SacCalc Input and Results**

## SacCalc Input Summary

| Development Condition | Basic Parameters |           |           |                      |                          |                  |              |                     |                   |           |              |               |
|-----------------------|------------------|-----------|-----------|----------------------|--------------------------|------------------|--------------|---------------------|-------------------|-----------|--------------|---------------|
|                       | Shed             | Area (SF) | Area (Ac) | Land Use             | Infiltration Rate, in/hr | Initial Loss, in | % Impervious | Impervious Area, sf | Pervious Area, sf | Basin "n" | Slope, ft/ft | Lag Time, min |
| Pre-Development       | ExShed           | 309070    | 7.10      | Open Space Grassland | 0.10                     | 0.10             | 2%           | 6181                | 302889            | 0.070     | 0.0067       | 17.9          |
| Post-Development      | ProShd           | 309070    | 7.10      | Commercial           | 0.08                     | 0.10             | 48%          | 149678              | 159393            | 0.031     | 0.0050       | 8.5           |

Assumptions:

Sacramento Method Rainfall Zone 2 (Figure 2-11 Sacramento Drainage Manual)

Mean Elevation = 65-feet

Hydrologic Soils Group (HSG) C (Web Soil Survey)

Initial Loss = 0.10 in (Table 5-1 Sacramento Drainage Manual)

Infiltration Rate (Table 5-2 Sacramento Drainage Manual)

Basin "n" (Table 7-1 Sacramento Drainage Manual)

Lag Time (Equation 7-1 Sacramento Drainage Manual)

### Existing Watershed SacCalc Summary

|  |              |            |       |
|--|--------------|------------|-------|
| Total Area:  | 7.1 ac       |            |       |
| Length of longest watercourse:                     | 920 ft       | FT         | Miles |
| Length along longest watercourse to centroid (Lc): | 605 ft       | 828        | 0.157 |
| Upper elevation:                                   | 66.4 ft      |            | 0.115 |
| Lower Elevation:                                   | 63.2 ft      |            |       |
| Slope (S):   | 0.0035 ft/ft | 18.4 ft/mi |       |
| Composite Basin "n":                               | 0.070        |            |       |
| Composite Infiltration Rate:                       | 0.100 in/hr  |            |       |
| Composite % Impervious:                            | 2%           |            |       |
| Lag Time (Basin "n" )(4):                          | 17.9 min     |            |       |

(4) Per equation 7-1 Sacramento Drainage Manual-See Below

(5) Per SacCalc Output

### Proposed Watershed SacCalc Summary

|  |              |            |       |
|--|--------------|------------|-------|
| Total Area:  | 7.1 ac       |            |       |
| Length of longest watercourse:                     | 990 ft       | FT         | Miles |
| Length along longest watercourse to centroid (Lc): | 815 ft       | 891        | 0.169 |
| Upper elevation:                                   | ft           |            | 0.154 |
| Lower Elevation:                                   | ft           |            |       |
| Slope (S):   | 0.0050 ft/ft | 26.4 ft/mi |       |
| Composite Basin "n":                               | 0.031        |            |       |
| Composite Infiltration Rate:                       | 0.080 in/hr  |            |       |
| Composite % Impervious:                            | 48%          |            |       |
| Lag Time (Basin "n" )(4):                          | 8.5 min      |            |       |

(4) Per equation 7-1 Sacramento Drainage Manual-See Below

(5) Per SacCalc Output

### Lag Equation

The Basin "n" lag equation, which was originally developed by Snyder<sup>11</sup> and later revised by the U.S. Corps of Engineers and the U.S. Bureau of Reclamation,<sup>17</sup> is expressed as:

$$L_g = Cn \left[ \frac{LL_c}{S^{0.5}} \right]^{0.33} \quad (7-1)$$

where:

- C = 1560 (174)
- $L_g$  = Lag Time, min (sec)
- L = Length of longest watercourse, measured as approximately 90% of the distance from the point of interest to the headwater divide of the basin, miles (m)
- $L_c$  = Length along the longest watercourse measured upstream from the point of interest to a point close to the centroid of the basin, miles (m)
- S = Overall slope of the longest watercourse between the headwaters and concentration point, ft/mile (m/m)
- n = Basin "n" from Table 7-1.

[View HEC-1 output](#)

**Sacramento method results**  
**(Project: Bradshaw Jackson)**  
**(100-year, 1-day rainfall)**

| ID     | Peak flow (cfs) | Time of peak (hours) | Basin area (sq. mi) | Peak stage (feet) | Peak storage (ac-ft) | Diversion volume (ac-ft) |
|--------|-----------------|----------------------|---------------------|-------------------|----------------------|--------------------------|
| EXSHED | 13.             | 12:13                | .01                 |                   |                      |                          |
| PROSHD | 20.             | 12:05                | .01                 |                   |                      |                          |
| DE001  | 12.             | 12:13                | .01                 |                   | .4                   |                          |

**(10-year, 1-day rainfall)**

| ID     | Peak flow (cfs) | Time of peak (hours) | Basin area (sq. mi) | Peak stage (feet) | Peak storage (ac-ft) | Diversion volume (ac-ft) |
|--------|-----------------|----------------------|---------------------|-------------------|----------------------|--------------------------|
| EXSHED | 7.8             | 12:13                | .01                 |                   |                      |                          |
| PROSHD | 12.             | 12:05                | .01                 |                   |                      |                          |
| DE001  | 6.9             | 12:14                | .01                 |                   | .3                   |                          |

**Sacramento Hydrologic Calculator Report**

March 27, 2024 11:18

Project Title: Bradshaw Jackson

Method: Sacramento County HEC-1 method

Comments:

Date: 3/27/2024

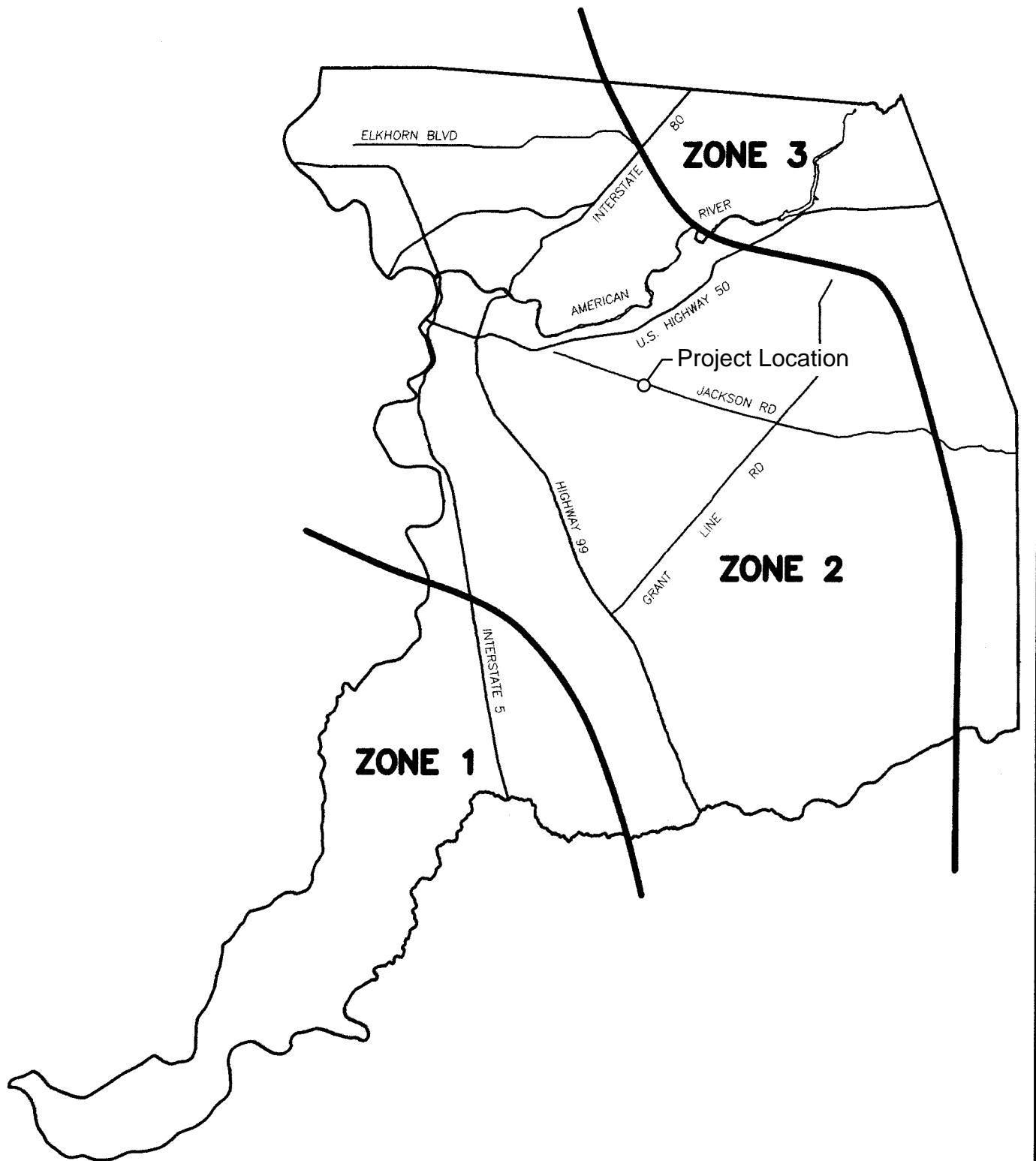
Prepared by: MDH

## Watershed Hydrologic Summary Data

| Watershed | Area<br>(acres) | Mean<br>Elevation<br>(ft) | Lag Times |                   | Basin "n" |              | Loss Rates |                      | Percent Impervious |                        |
|-----------|-----------------|---------------------------|-----------|-------------------|-----------|--------------|------------|----------------------|--------------------|------------------------|
|           |                 |                           | Method    | Lag Time<br>(min) | Method    | Basin<br>"n" | Method     | Loss Rate<br>(in/hr) | Method             | Impervious<br>Area (%) |
| EXSHED    | 7.1             | 65                        | Specified | 17.9              | -         | -            | Specified  | .1                   | Specified          | 2                      |
| PROSHD    | 7.1             | 65                        | Specified | 8.5               | -         | -            | Specified  | .08                  | Specified          | 48                     |

## Detention Basin Data

| Detention Basin | Initial Condition    | Pond Storage Relation |   |      |       |        |       |        |       |        |       |        | Outlet Data   |                 |         |          |   |
|-----------------|----------------------|-----------------------|---|------|-------|--------|-------|--------|-------|--------|-------|--------|---------------|-----------------|---------|----------|---|
|                 |                      |                       |   |      |       |        |       |        |       |        |       |        | Elev.<br>(ft) | Area<br>(sq ft) | Q Coef. | Exponent |   |
| DE001           | Volume<br>(ac-ft)    | 0                     | Volume<br>(ac-ft)                         | 0    | 0.185 | 0.237  | 0.294 | 0.356  | 0.423 | 0.495  | 0.654 | 0.833  | 0.93          | -               | -       | -        | - |
|                 |                      |                       | Discharge<br>(cfs)                        | 0.42 | 0.5   | 3.27   | 8.32  | 14.86  | 17.12 | 17.54  | 18.35 | 19.12  | 19.5          | -               | -       | -        | - |
|                 | Pump Data            |                       |   |      |       |        |       |        |       |        |       |        |               |                 |         |          |   |
|                 | Pump Hydrograph Name |                       | Pump Discharge<br>(cfs)                   |      |       | Pump 1 |       | Pump 2 |       | Pump 3 |       | Pump 4 |               | Pump 5          |         |          |   |
|                 |                      |                       | Elevation at which Pump Turns<br>On (ft)  |      |       |        |       |        |       |        |       |        |               |                 |         |          |   |
|                 |                      |                       | Elevation at which Pump Turns<br>Off (ft) |      |       |        |       |        |       |        |       |        |               |                 |         |          |   |



Note : See foldout map in the back of Hydrology Standards  
for larger scale map of Rainfall Zones.

## Sacramento City and County Rainfall Zones Sacramento Method

Date  
December  
1996

Figure

2-11

## Infiltration

### ***Initial Losses***

The initial loss depth in the infiltration calculations represents the higher infiltration capacity of the unsaturated soil at the beginning of a storm. All precipitation is assumed to infiltrate until the initial loss depth is satisfied.

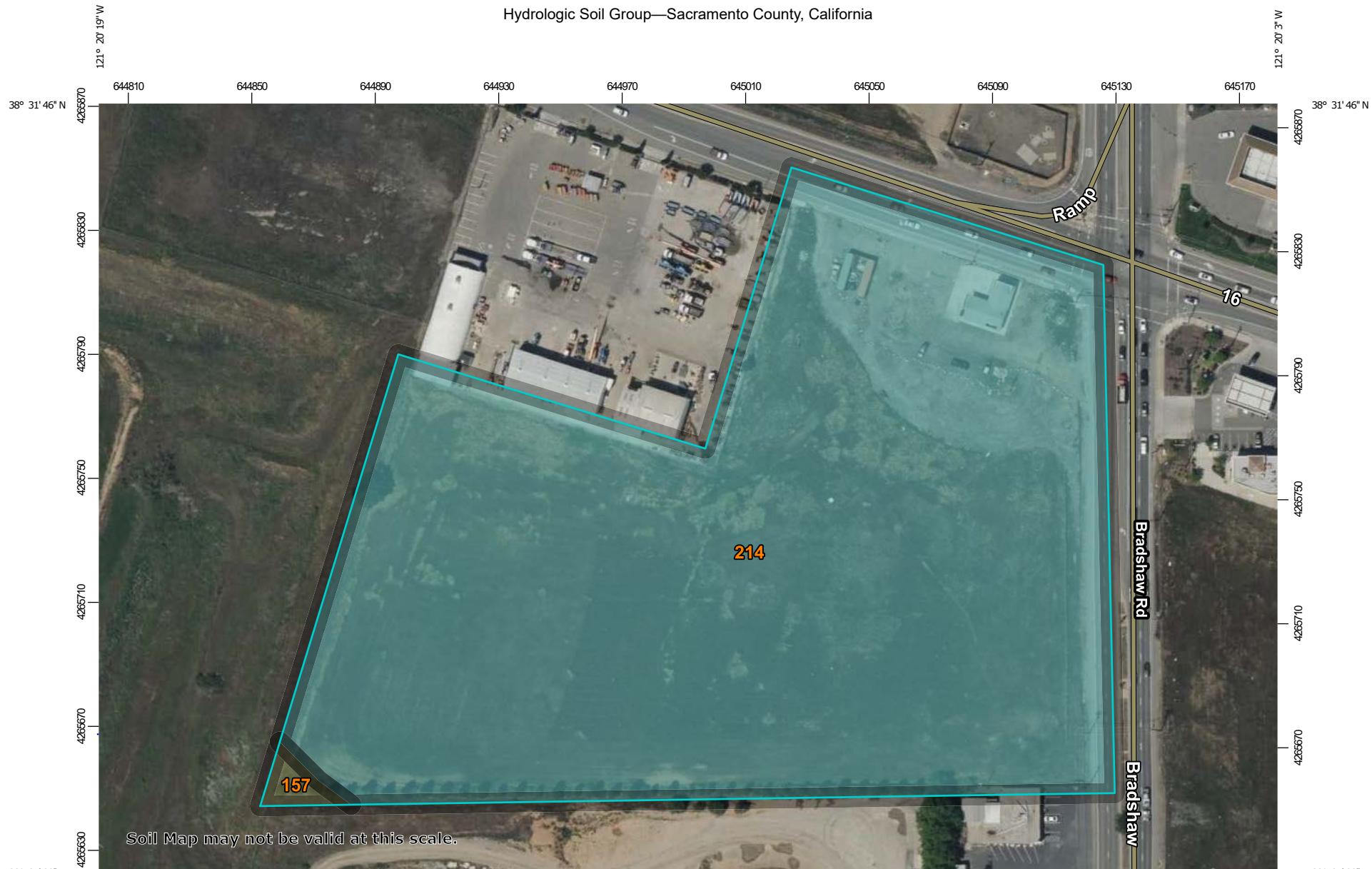
Initial losses are dependent on the soil condition. Dry soil infiltrates significantly greater amounts of precipitation than moist soil. There is also a correlation between the recurrence frequency of a storm and the initial loss. Calibration modelling with HEC-1 in the Sacramento area has shown that higher initial losses were appropriate for the more frequent events. Initial losses recommended for the City and County of Sacramento are shown in Table 5-1.

**Table 5-1. Initial Losses**

| Recurrence Interval | Loss inches (millimeters) |
|---------------------|---------------------------|
| 2                   | 0.40 (10.2)               |
| 5                   | 0.25 (6.4)                |
| 10                  | 0.20 (5.1)                |
| 25                  | 0.15 (3.8)                |
| 50                  | 0.12 (3.1)                |
| 100                 | 0.10 (2.5)                |
| 200                 | 0.08 (2.0)                |
| 500                 | 0.06 (1.5)                |

*Continued on next page...*

### Hydrologic Soil Group—Sacramento County, California



Map Scale: 1:1,750 if printed on A landscape (11" x 8.5") sheet.



Meters

Feet

Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 10N WGS84



Natural Resources  
Conservation Service

Web Soil Survey  
National Cooperative Soil Survey

3/27/2024  
Page 1 of 4

**MAP LEGEND****Area of Interest (AOI)**

Area of Interest (AOI)

C

C/D

D

Not rated or not available

**Soils****Soil Rating Polygons**

A

A/D

B

B/D

C

C/D

D

Not rated or not available

**Soil Rating Lines**

A

A/D

B

B/D

C

C/D

D

Not rated or not available

**Soil Rating Points**

A

A/D

B

B/D

**Water Features**

Streams and Canals

**Transportation**

Rails

Interstate Highways

US Routes

Major Roads

Local Roads

**Background**

Aerial Photography

**MAP INFORMATION**

The soil surveys that comprise your AOI were mapped at 1:24,000.

**Warning:** Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Sacramento County, California

Survey Area Data: Version 23, Aug 31, 2023

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Apr 23, 2022—Apr 24, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Hydrologic Soil Group

| Map unit symbol                    | Map unit name                                | Rating | Acres in AOI | Percent of AOI |
|------------------------------------|--|--------|--------------|----------------|
| 157                                | Hedge loam, 0 to 2 percent slopes            | C/D    | 0.1          | 0.7%           |
| 214                                | San Joaquin silt loam, 0 to 3 percent slopes | C      | 9.8          | 99.3%          |
| <b>Totals for Area of Interest</b> |  |        | <b>9.9</b>   | <b>100.0%</b>  |

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

### Rating Options

*Aggregation Method: Dominant Condition*



*Component Percent Cutoff: None Specified*

*Tie-break Rule: Higher*

## Infiltration (continued)

**Constant Losses**  
(Cont.)

**Table 5-2. Infiltration Rates by Hydrologic  
Soil-Cover Groups (inches/hour)**

| Cover                                 | % Imp | Soil Group |       |       |
|---------------------------------------|-------|------------|-------|-------|
|                                       |       | B          | C     | D     |
| Highways, Parking                     | 95    | 0.14       | 0.07  | 0.04  |
| Commercial, Offices                   | 90    | 0.16       | 0.08  | 0.05  |
| Intensive Industrial                  | 85    | 0.162      | 0.082 | 0.052 |
| Apartments, HDR                       | 80    | 0.165      | 0.085 | 0.055 |
| Mobil Home Park                       | 75    | 0.167      | 0.087 | 0.057 |
| Condominiums, MDR                     | 70    | 0.17       | 0.09  | 0.06  |
| Residential: 8-10 du/acre, Ext Indust | 60    | 0.18       | 0.10  | 0.07  |
| Residential: 6-8 du/acre, LDR, School | 50    | 0.18       | 0.10  | 0.07  |
| Residential: 4-6 du/acre              | 40    | 0.18       | 0.10  | 0.07  |
| Residential: 3-4 du/acre              | 30    | 0.18       | 0.10  | 0.07  |
| Residential: 2-3 du/acre              | 25    | 0.18       | 0.10  | 0.07  |
| Residential: 1-2 du/acre              | 20    | 0.18       | 0.10  | 0.07  |
| Residential: 0.5-1 du/acre            | 15    | 0.18       | 0.10  | 0.07  |
| Residential: 0.2-0.5 du/acre, Ag Res  | 10    | 0.18       | 0.10  | 0.07  |
| Residential: <0.2 du/acre, Recreation | 5     | 0.18       | 0.10  | 0.07  |
| Open Space, Grassland, Ag             | 2     | 0.18       | 0.10  | 0.07  |
| Open Space, Woodland, Natural         | 1     | 0.19       | 0.11  | 0.08  |
| Dense Oak, Shrubs, Vines              | 1     | 0.25       | 0.16  | 0.12  |

\*Sacramento County does not contain significant areas of Type "A" soils.

### Summary for Pond 3P: Basin

Inflow = 20.14 cfs @ 12.08 hrs, Volume= 1.922 af  
 Outflow = 14.86 cfs @ 12.18 hrs, Volume= 1.832 af, Atten= 26%, Lag= 5.6 min  
 Primary = 14.86 cfs @ 12.18 hrs, Volume= 1.832 af  
 Routed to nonexistent node 1P

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.01 hrs / 3  
 Peak Elev= 11.60' @ 12.18 hrs Surf.Area= 0.323 ac Storage= 0.356 af

Plug-Flow detention time= 80.7 min calculated for 1.831 af (95% of inflow)  
 Center-of-Mass det. time= 51.9 min ( 782.1 - 730.1 )

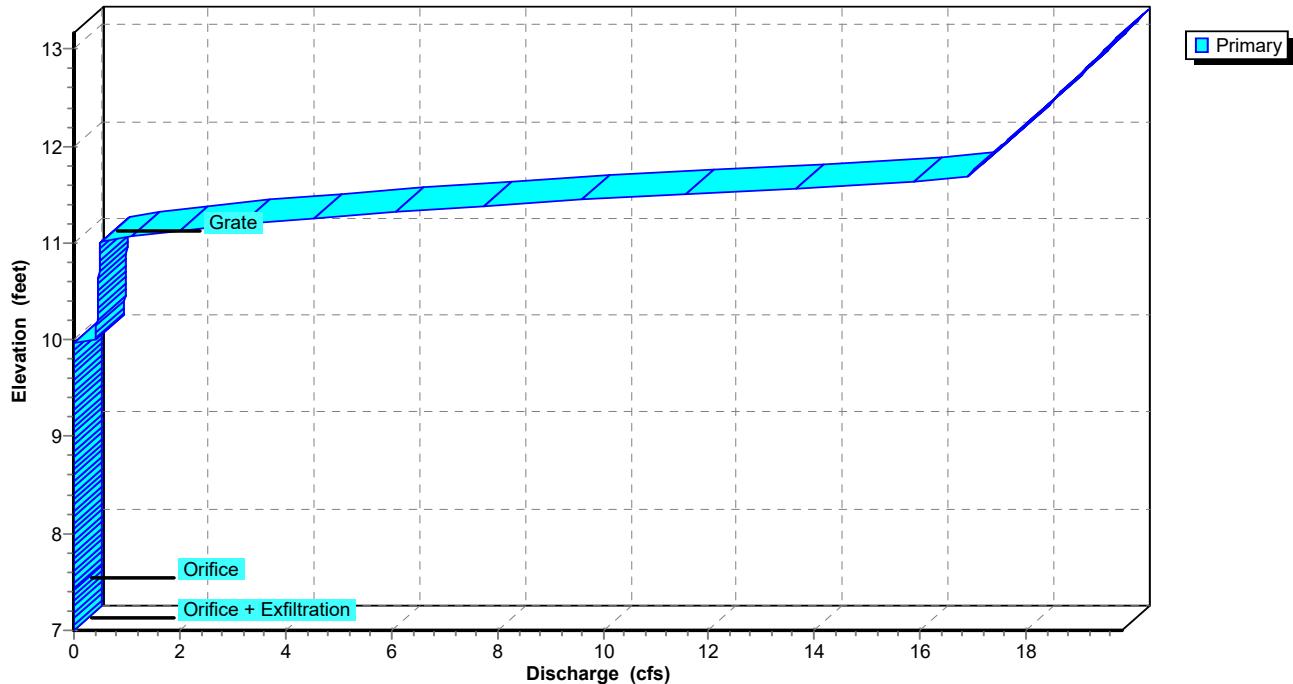
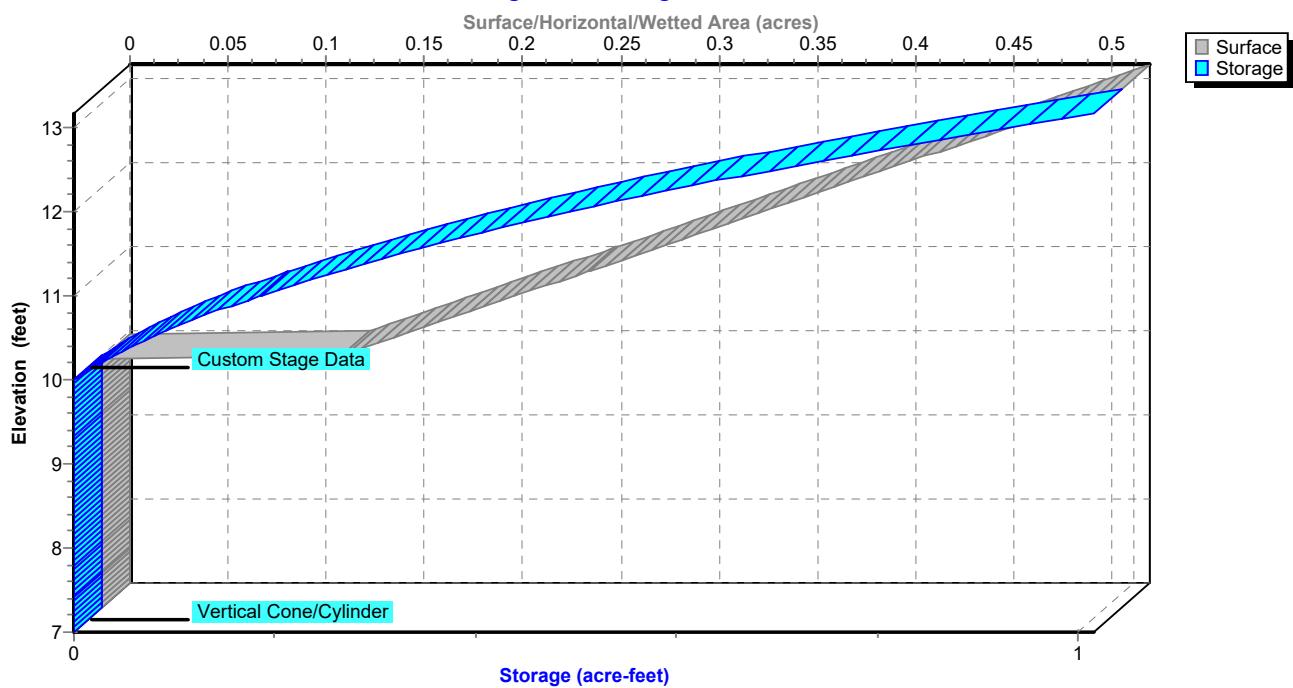
| Volume   | Invert | Avail.Storage | Storage Description                           |                         |
|----------|--------|---------------|---|-------------------------|
| #1       | 10.00' | 1.016 af      | <b>Custom Stage Data (Prismatic)</b>          | Listed below (Recalc)   |
| #2       | 7.00'  | 0.000 af      | <b>3.00'D x 3.00'H Vertical Cone/Cylinder</b> |                         |
| 1.016 af |        |               |   | Total Available Storage |

| Elevation<br>(feet) | Surf.Area<br>(acres) | Inc.Store<br>(acre-feet) | Cum.Store<br>(acre-feet) |
|---------------------|----------------------|--------------------------|--------------------------|
| 10.00               | 0.122                | 0.000                    | 0.000                    |
| 13.17               | 0.519                | 1.016                    | 1.016                    |

| Device | Routing  | Invert | Outlet Devices                                    |  |
|--------|----------|--------|---|--|
| #1     | Primary  | 7.00'  | <b>18.0" Vert. Orifice</b>                        | C= 0.600 Limited to weir flow at low heads |
| #2     | Device 1 | 11.00' | <b>36.0" Horiz. Grate</b>                         | C= 0.600 Limited to weir flow at low heads |
| #3     | Device 4 | 7.00'  | <b>5.000 in/hr Exfiltration over Surface area</b> |  |
| #4     | Device 1 | 7.42'  | <b>3.2" Vert. Orifice</b>                         | C= 0.600 Limited to weir flow at low heads |

**Primary OutFlow** Max=14.85 cfs @ 12.18 hrs HW=11.60' (Free Discharge)

- ↑ 1=Orifice (Passes 14.85 cfs of 16.69 cfs potential flow)
- └ 2=Grate (Weir Controls 14.31 cfs @ 2.53 fps)
- └ 4=Orifice (Orifice Controls 0.54 cfs @ 9.69 fps)
- └ 3=Exfiltration (Passes 0.54 cfs of 1.63 cfs potential flow)

**Pond 3P: Basin****Stage-Discharge****Pond 3P: Basin****Stage-Area-Storage**

**Stage-Discharge for Pond 3P: Basin**

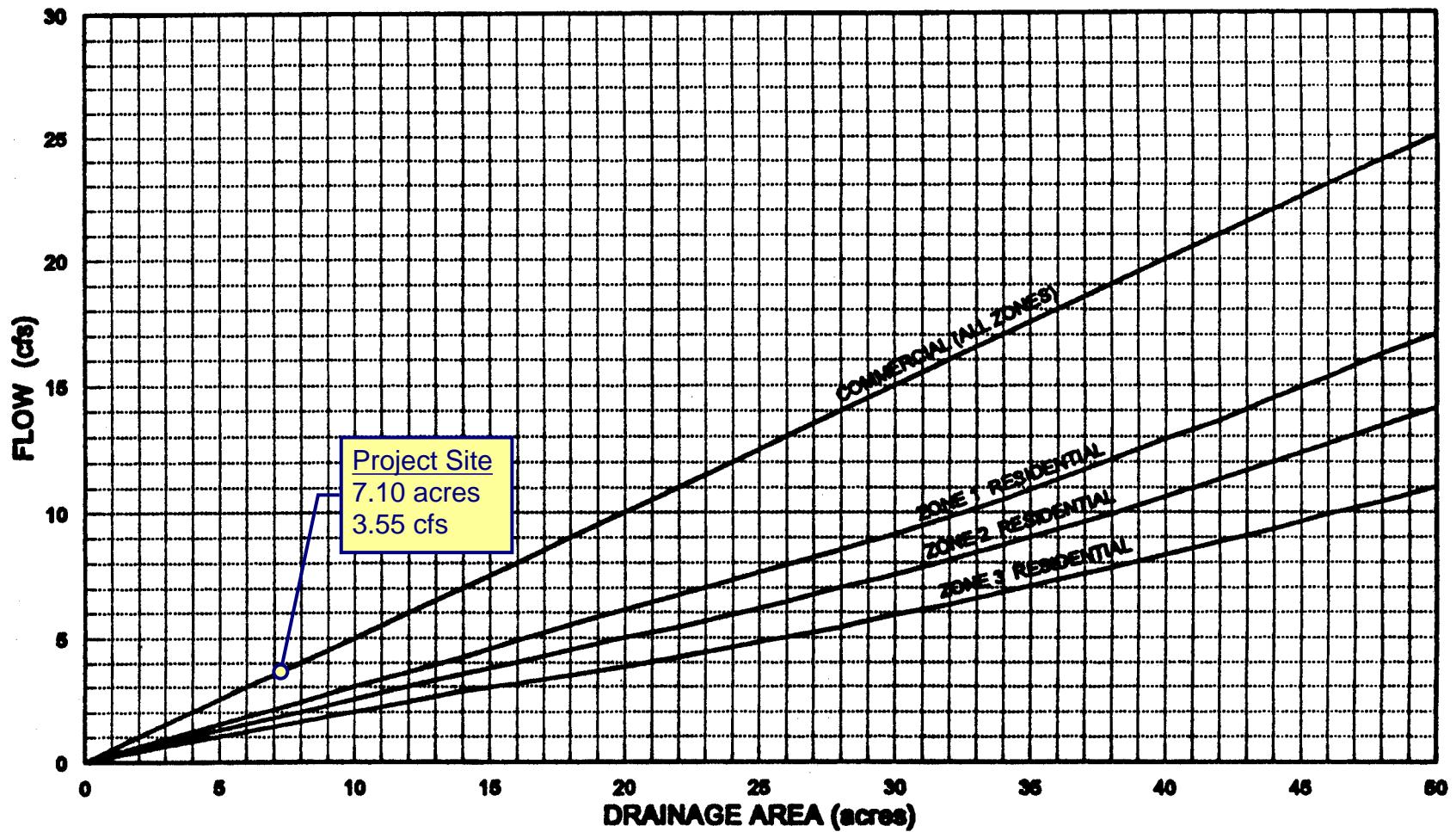
| Elevation<br>(feet) | Primary<br>(cfs) | Elevation<br>(feet) | Primary<br>(cfs) | Elevation<br>(feet) | Primary<br>(cfs) |
|---------------------|------------------|---------------------|------------------|---------------------|------------------|
| 7.00                | 0.00             | 9.60                | 0.00             | 12.20               | 17.95            |
| 7.05                | 0.00             | 9.65                | 0.00             | 12.25               | 18.05            |
| 7.10                | 0.00             | 9.70                | 0.00             | 12.30               | 18.15            |
| 7.15                | 0.00             | 9.75                | 0.00             | 12.35               | 18.25            |
| 7.20                | 0.00             | 9.80                | 0.00             | 12.40               | 18.35            |
| 7.25                | 0.00             | 9.85                | 0.00             | 12.45               | 18.45            |
| 7.30                | 0.00             | 9.90                | 0.00             | 12.50               | 18.54            |
| 7.35                | 0.00             | 9.95                | 0.00             | 12.55               | 18.64            |
| 7.40                | 0.00             | 10.00               | 0.42             | 12.60               | 18.74            |
| 7.45                | 0.00             | 10.05               | 0.42             | 12.65               | 18.83            |
| 7.50                | 0.00             | 10.10               | 0.43             | 12.70               | 18.93            |
| 7.55                | 0.00             | 10.15               | 0.43             | 12.75               | 19.03            |
| 7.60                | 0.00             | 10.20               | 0.44             | 12.80               | 19.12            |
| 7.65                | 0.00             | 10.25               | 0.44             | 12.85               | 19.22            |
| 7.70                | 0.00             | 10.30               | 0.45             | 12.90               | 19.31            |
| 7.75                | 0.00             | 10.35               | 0.45             | 12.95               | 19.40            |
| 7.80                | 0.00             | 10.40               | 0.45             | 13.00               | 19.50            |
| 7.85                | 0.00             | 10.45               | 0.46             | 13.05               | 19.59            |
| 7.90                | 0.00             | 10.50               | 0.46             | 13.10               | 19.68            |
| 7.95                | 0.00             | 10.55               | 0.47             | 13.15               | <b>19.77</b>     |
| 8.00                | 0.00             | 10.60               | 0.47             |                     |                  |
| 8.05                | 0.00             | 10.65               | 0.47             |                     |                  |
| 8.10                | 0.00             | 10.70               | 0.48             |                     |                  |
| 8.15                | 0.00             | 10.75               | 0.48             |                     |                  |
| 8.20                | 0.00             | 10.80               | 0.48             |                     |                  |
| 8.25                | 0.00             | 10.85               | 0.49             |                     |                  |
| 8.30                | 0.00             | 10.90               | 0.49             |                     |                  |
| 8.35                | 0.00             | 10.95               | 0.50             |                     |                  |
| 8.40                | 0.00             | 11.00               | 0.50             |                     |                  |
| 8.45                | 0.00             | 11.05               | 0.85             |                     |                  |
| 8.50                | 0.00             | 11.10               | 1.48             |                     |                  |
| 8.55                | 0.00             | 11.15               | 2.30             |                     |                  |
| 8.60                | 0.00             | 11.20               | 3.27             |                     |                  |
| 8.65                | 0.00             | 11.25               | 4.37             |                     |                  |
| 8.70                | 0.00             | 11.30               | 5.58             |                     |                  |
| 8.75                | 0.00             | 11.35               | 6.91             |                     |                  |
| 8.80                | 0.00             | 11.40               | 8.32             |                     |                  |
| 8.85                | 0.00             | 11.45               | 9.83             |                     |                  |
| 8.90                | 0.00             | 11.50               | 11.43            |                     |                  |
| 8.95                | 0.00             | 11.55               | 13.11            |                     |                  |
| 9.00                | 0.00             | 11.60               | 14.86            |                     |                  |
| 9.05                | 0.00             | 11.65               | 16.69            |                     |                  |
| 9.10                | 0.00             | 11.70               | 16.91            |                     |                  |
| 9.15                | 0.00             | 11.75               | 17.02            |                     |                  |
| 9.20                | 0.00             | 11.80               | 17.12            |                     |                  |
| 9.25                | 0.00             | 11.85               | 17.23            |                     |                  |
| 9.30                | 0.00             | 11.90               | 17.33            |                     |                  |
| 9.35                | 0.00             | 11.95               | 17.44            |                     |                  |
| 9.40                | 0.00             | 12.00               | 17.54            |                     |                  |
| 9.45                | 0.00             | 12.05               | 17.64            |                     |                  |
| 9.50                | 0.00             | 12.10               | 17.75            |                     |                  |
| 9.55                | 0.00             | 12.15               | 17.85            |                     |                  |

**Stage-Area-Storage for Pond 3P: Basin**

| Elevation<br>(feet) | Surface<br>(acres) | Storage<br>(acre-feet) | Elevation<br>(feet) | Surface<br>(acres) | Storage<br>(acre-feet) |
|---------------------|--------------------|------------------------|---------------------|--------------------|------------------------|
| 7.00                | 0.000              | 0.000                  | 12.20               | 0.398              | 0.572                  |
| 7.10                | 0.000              | 0.000                  | 12.30               | 0.410              | 0.612                  |
| 7.20                | 0.000              | 0.000                  | 12.40               | 0.423              | 0.654                  |
| 7.30                | 0.000              | 0.000                  | 12.50               | 0.435              | 0.697                  |
| 7.40                | 0.000              | 0.000                  | 12.60               | 0.448              | 0.741                  |
| 7.50                | 0.000              | 0.000                  | 12.70               | 0.460              | 0.786                  |
| 7.60                | 0.000              | 0.000                  | 12.80               | 0.473              | 0.833                  |
| 7.70                | 0.000              | 0.000                  | 12.90               | 0.485              | 0.881                  |
| 7.80                | 0.000              | 0.000                  | 13.00               | 0.498              | 0.930                  |
| 7.90                | 0.000              | 0.000                  | 13.10               | <b>0.510</b>       | <b>0.980</b>           |
| 8.00                | 0.000              | 0.000                  |                     |                    |                        |
| 8.10                | 0.000              | 0.000                  |                     |                    |                        |
| 8.20                | 0.000              | 0.000                  |                     |                    |                        |
| 8.30                | 0.000              | 0.000                  |                     |                    |                        |
| 8.40                | 0.000              | 0.000                  |                     |                    |                        |
| 8.50                | 0.000              | 0.000                  |                     |                    |                        |
| 8.60                | 0.000              | 0.000                  |                     |                    |                        |
| 8.70                | 0.000              | 0.000                  |                     |                    |                        |
| 8.80                | 0.000              | 0.000                  |                     |                    |                        |
| 8.90                | 0.000              | 0.000                  |                     |                    |                        |
| 9.00                | 0.000              | 0.000                  |                     |                    |                        |
| 9.10                | 0.000              | 0.000                  |                     |                    |                        |
| 9.20                | 0.000              | 0.000                  |                     |                    |                        |
| 9.30                | 0.000              | 0.000                  |                     |                    |                        |
| 9.40                | 0.000              | 0.000                  |                     |                    |                        |
| 9.50                | 0.000              | 0.000                  |                     |                    |                        |
| 9.60                | 0.000              | 0.000                  |                     |                    |                        |
| 9.70                | 0.000              | 0.000                  |                     |                    |                        |
| 9.80                | 0.000              | 0.000                  |                     |                    |                        |
| 9.90                | 0.000              | 0.000                  |                     |                    |                        |
| 10.00               | 0.122              | 0.000                  |                     |                    |                        |
| 10.10               | 0.135              | 0.013                  |                     |                    |                        |
| 10.20               | 0.147              | 0.027                  |                     |                    |                        |
| 10.30               | 0.160              | 0.043                  |                     |                    |                        |
| 10.40               | 0.172              | 0.059                  |                     |                    |                        |
| 10.50               | 0.185              | 0.077                  |                     |                    |                        |
| 10.60               | 0.197              | 0.096                  |                     |                    |                        |
| 10.70               | 0.210              | 0.117                  |                     |                    |                        |
| 10.80               | 0.222              | 0.138                  |                     |                    |                        |
| 10.90               | 0.235              | 0.161                  |                     |                    |                        |
| 11.00               | 0.247              | 0.185                  |                     |                    |                        |
| 11.10               | 0.260              | 0.210                  |                     |                    |                        |
| 11.20               | 0.272              | 0.237                  |                     |                    |                        |
| 11.30               | 0.285              | 0.265                  |                     |                    |                        |
| 11.40               | 0.297              | 0.294                  |                     |                    |                        |
| 11.50               | 0.310              | 0.324                  |                     |                    |                        |
| 11.60               | 0.323              | 0.356                  |                     |                    |                        |
| 11.70               | 0.335              | 0.389                  |                     |                    |                        |
| 11.80               | 0.348              | 0.423                  |                     |                    |                        |
| 11.90               | 0.360              | 0.458                  |                     |                    |                        |
| 12.00               | 0.373              | 0.495                  |                     |                    |                        |
| 12.10               | 0.385              | 0.533                  |                     |                    |                        |

## **APPENDIX E:**

**Figure 2-5 of the County's Hydrology Manual (Volume 2)**



**NOTE:** Design runoff for multiple family development shall be based on the following formula:

$$Q_m = Q_r + (Q_c - Q_r) (I-50)/40$$

Where:

|       |        |
|-------|--------|
| RD- 7 | I = 60 |
| RD-10 | I = 70 |
| RD-20 | I = 80 |
| RD-30 | I = 90 |

Source: County of Sacramento Master Drainage Plan,  
Part 1, County-wide Hydrology, Nolte and Assoc.

**Design Runoff  
Nolte Method  
Drainage Areas, <50 Acres**

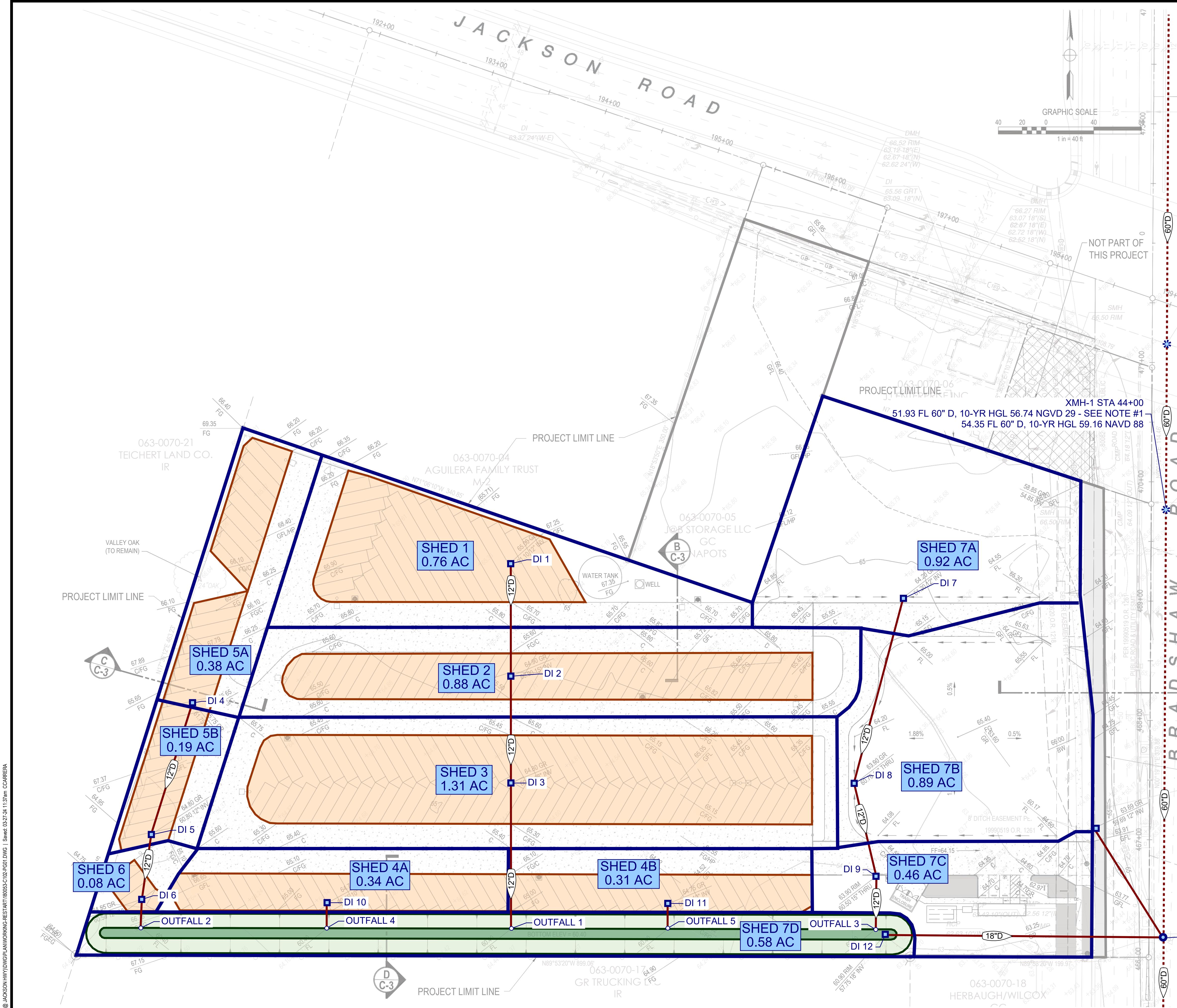
Date  
December  
1996

Figure

2-5

**APPENDIX F:**

**Nolte Watershed Map and Hydraulic Calculations**



| LEGEND:                   |  |
|---------------------------|--|
| WATERSHED BOUNDARY        |  |
| BIORETENTION BASIN        |  |
| POROUS GRAVEL PAVEMENT    |  |
| PROPOSED DI               |  |
| PROPOSED DRAINAGE MANHOLE |  |
| EXISTING DRAINAGE MANHOLE |  |
| PROPOSED STORM DRAIN PIPE |  |
| EXISTING STORM DRAIN PIPE |  |

NOTE #1 - FLOWLINE AND 10-YEAR HGL INFORMATION BASED ON RECORD DRAWINGS FOR 9750 KIEFER BLVD PREPARED BY WOOD-RODGERS, INC. 2011

#### Nolte Watershed Summary

| SHED | AREA  |      |
|------|-------|------|
|      | SF    | AC   |
| 1    | 32985 | 0.76 |
| 2    | 38171 | 0.88 |
| 3    | 57213 | 1.31 |
| 4A   | 14774 | 0.34 |
| 4B   | 13363 | 0.31 |
| 5A   | 16510 | 0.38 |
| 5B   | 8267  | 0.19 |
| 6    | 3453  | 0.08 |
| 7A   | 40250 | 0.92 |
| 7B   | 38805 | 0.89 |
| 7C   | 20052 | 0.46 |
| 7D   | 25226 | 0.58 |

#### Nolte Flow Summary

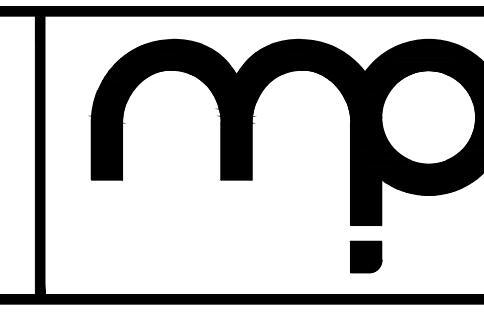
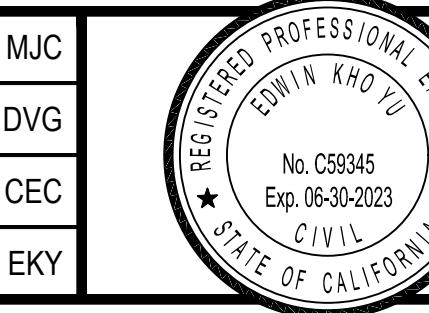
| FROM  | TO        | SHED    | AREA, AC | SUM AREA, AC | NOLTE FLOW, CFS | HYDRAFLOW PIPE NUMBER |
|-------|-----------|---------|----------|--------------|-----------------|-----------------------|
| DI 1  | DI 2      | SHED 1  | 0.76     | 0.76         | 0.38            | 3                     |
| DI 2  | DI 3      | SHED 2  | 0.88     | 1.64         | 0.82            | 2                     |
| DI 3  | OUTFALL 1 | SHED 3  | 1.31     | 2.95         | 1.48            | 1                     |
| DI 4  | DI 5      | SHED 5A | 0.38     | 0.38         | 0.19            | 6                     |
| DI 5  | DI 6      | SHED 5B | 0.19     | 0.57         | 0.29            | 5                     |
| DI 6  | OUTFALL 2 | SHED 6  | 0.08     | 0.65         | 0.33            | 4                     |
| DI 7  | DI 8      | SHED 7A | 0.92     | 0.92         | 0.46            | 9                     |
| DI 8  | DI 9      | SHED 7B | 0.89     | 1.81         | 0.91            | 8                     |
| DI 9  | OUTFALL 3 | SHED 7C | 0.46     | 2.27         | 1.14            | 7                     |
| DI 10 | OUTFALL 4 | SHED 4A | 0.34     | 0.34         | 0.17            | 10                    |
| DI 11 | OUTFALL 5 | SHED 4B | 0.31     | 0.31         | 0.16            | 11                    |
| DI 12 | MH-1      | ALL     | 7.10     | 7.10         | 3.55            | 12                    |

Nolte Flow for Commercial Land Use = 0.5 cfs/acre

MH-1  
51.26 FL 60" D, 10-YR HGL 56.68 NGVD 29  
53.68 FL 60" D, 10-YR HGL 59.10 NAVD 88

| REVISIONS |             | SCALE:      | BENCH MARK     | COUNTY B.M. 01A-35 | COMPUTED | MJC |
|-----------|-------------|-------------|----------------|--------------------|----------|-----|
|           |             | HORIZ. 1" = | 40'            |                    |          |     |
|           |             | VERT. 1" =  | N/A            |                    |          |     |
| NO.       | DESCRIPTION | APPD. ENGR. | DATE APPD. EU. | DATE               |          |     |

| NO. | DESCRIPTION | APPD. ENGR. | DATE APPD. EU. | DATE |
|-----|-------------|-------------|----------------|------|
|     |             |             |                |      |



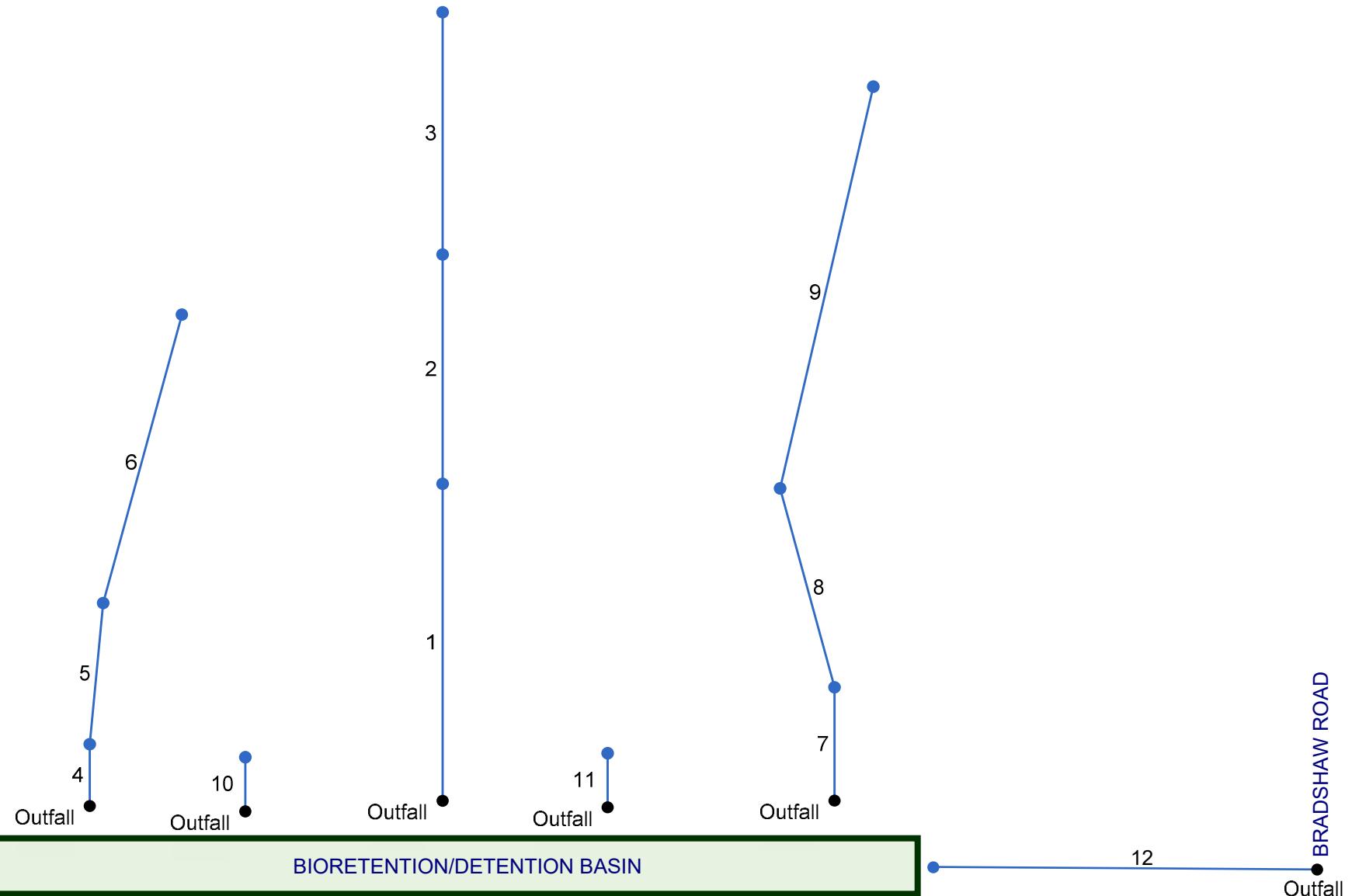
**MORTON & PITALO, INC.**  
CIVIL ENGINEERING • LAND PLANNING • LAND SURVEYING  
Folsom • Sacramento • Fresno  
75 Iron Point Circle, Suite #120  
Folsom, CA 95630

XMH-2 STA 39+00  
51.00 FL 60" D, 10-YR HGL 56.65 NGVD 29 - SEE NOTE#1  
53.42 FL 60" D, 10-YR HGL 59.07 NAVD 88

**NOLTE WATERSHED MAP**  
**J @ B STORAGE**  
**5220 BRADSHAW ROAD & 9680 JACKSON ROAD**  
SACRAMENTO, CALIFORNIA

| DATE   | MARCH 2024 |
|--------|------------|
| SHEET  | C-2        |
| 2 OF 6 |            |

# Hydraflow Storm Sewers Extension for Autodesk® Civil 3D® Plan



# Storm Sewer Summary Report

| Line No.   | Line ID   | Flow rate (cfs) | Line Size (in) | Line shape | Line length (ft) | Invert EL Dn (ft) | Invert EL Up (ft) | Line Slope (%)      | HGL Down (ft) | HGL Up (ft) | Minor loss (ft)     | HGL Junct (ft) | Dns Line No. | Junction Type |
|--|-----------|-----------------|----------------|------------|------------------|-------------------|-------------------|---------------------|---------------|-------------|---------------------|----------------|--------------|---------------|
| 1  | -90 deg   | 1.48            | 12             | Cir        | 123.000          | 60.40             | 60.70             | 0.244               | 61.70*        | 61.91*      | 0.01                | 61.92          | End          | Manhole       |
| 2  | 0 deg     | 0.82            | 12             | Cir        | 89.000           | 60.70             | 60.90             | 0.225               | 61.92*        | 61.97*      | 0.00                | 61.97          | 1            | Manhole       |
| 3  | 0 deg     | 0.38            | 12             | Cir        | 94.000           | 60.90             | 61.10             | 0.213               | 61.97         | 61.98       | 0.00                | 61.98          | 2            | Manhole       |
| 4  | -90 deg   | 0.33            | 12             | Cir        | 24.000           | 60.40             | 60.50             | 0.417               | 61.70*        | 61.70*      | 0.00                | 61.70          | End          | Manhole       |
| 5  | 5.4 deg   | 0.29            | 12             | Cir        | 55.000           | 60.50             | 60.80             | 0.545               | 61.70         | 61.71       | 0.00                | 61.71          | 4            | Manhole       |
| 6  | 9.8 deg   | 0.19            | 12             | Cir        | 116.000          | 60.80             | 61.75             | 0.819               | 61.71         | 61.93       | n/a                 | 61.93 j        | 5            | Manhole       |
| 7  | -90 deg   | 1.14            | 12             | Cir        | 44.000           | 60.40             | 60.50             | 0.227               | 61.70*        | 61.75*      | 0.01                | 61.76          | End          | Manhole       |
| 8  | -15.2 deg | 0.91            | 12             | Cir        | 80.000           | 60.50             | 60.70             | 0.250               | 61.76*        | 61.81*      | 0.01                | 61.82          | 7            | Manhole       |
| 9  | 28.2 deg  | 0.46            | 12             | Cir        | 160.000          | 60.70             | 61.20             | 0.313               | 61.82         | 61.85       | 0.01                | 61.86          | 8            | Manhole       |
| 10   | -90 deg   | 0.17            | 10             | Cir        | 21.000           | 60.40             | 60.75             | 1.667               | 61.70*        | 61.70*      | 0.00                | 61.70          | End          | Manhole       |
| 11   | -90 deg   | 0.16            | 10             | Cir        | 21.000           | 60.40             | 60.75             | 1.667               | 61.70*        | 61.70*      | 0.00                | 61.70          | End          | Manhole       |
| 12   | 180 deg   | 3.55            | 18             | Cir        | 233.000          | 57.28             | 57.75             | 0.202               | 59.10*        | 59.37*      | 0.06                | 59.43          | End          | Manhole       |
| Project File: JAB Nolte_24.0328.stm  |           |                 |                |            |                  |                   |                   | Number of lines: 12 |               |             | Run Date: 3/28/2024 |                |              |               |
| NOTES: Known Qs only ; *Surcharged (HGL above crown). ; j - Line contains hyd. jump. |           |                 |                |            |                  |                   |                   |                     |               |             |                     |                |              |               |

# Storm Sewer Tabulation

| Station   |         | Len     | Drng Area |            | Rnoff coeff | Area x C |       | Tc          |            | Rain (I) | Total flow | Cap full | Vel  | Pipe                |           | Invert Elev |         | HGL Elev            |         | Grnd / Rim Elev |         | Line ID   |
|---|---------|---------|-----------|------------|-------------|----------|-------|-------------|------------|----------|------------|----------|------|---------------------|-----------|-------------|---------|---------------------|---------|-----------------|---------|-----------|
| Line  | To Line |         | Incr (ft) | Total (ac) |             | Incr     | Total | Inlet (min) | Syst (min) |          |            |          |      | Size (in)           | Slope (%) | Dn (ft)     | Up (ft) | Dn (ft)             | Up (ft) | Dn (ft)         | Up (ft) |           |
| 1   | End     | 123.000 | 0.01      | 0.03       | 0.01        | 0.00     | 0.00  | 0.0         | 4.7        | 0.0      | 1.48       | 1.76     | 1.88 | 12                  | 0.24      | 60.40       | 60.70   | 61.70               | 61.91   | 60.40           | 64.80   | -90 deg   |
| 2   | 1       | 89.000  | 0.01      | 0.02       | 0.01        | 0.00     | 0.00  | 0.0         | 3.2        | 0.0      | 0.82       | 1.69     | 1.04 | 12                  | 0.22      | 60.70       | 60.90   | 61.92               | 61.97   | 64.80           | 64.90   | 0 deg     |
| 3   | 2       | 94.000  | 0.01      | 0.01       | 0.01        | 0.00     | 0.00  | 0.0         | 0.0        | 0.0      | 0.38       | 1.64     | 0.50 | 12                  | 0.21      | 60.90       | 61.10   | 61.97               | 61.98   | 64.90           | 65.00   | 0 deg     |
| 4   | End     | 24.000  | 0.01      | 0.03       | 0.01        | 0.00     | 0.00  | 0.0         | 10.5       | 0.0      | 0.33       | 2.30     | 0.42 | 12                  | 0.42      | 60.40       | 60.50   | 61.70               | 61.70   | 60.40           | 64.55   | -90 deg   |
| 5   | 4       | 55.000  | 0.01      | 0.02       | 0.01        | 0.00     | 0.00  | 0.0         | 8.0        | 0.0      | 0.29       | 2.63     | 0.38 | 12                  | 0.55      | 60.50       | 60.80   | 61.70               | 61.71   | 64.55           | 64.80   | 5.4 deg   |
| 6   | 5       | 116.000 | 0.01      | 0.01       | 0.01        | 0.00     | 0.00  | 0.0         | 0.0        | 0.0      | 0.19       | 3.22     | 1.13 | 12                  | 0.82      | 60.80       | 61.75   | 61.71               | 61.93   | 64.80           | 65.75   | 9.8 deg   |
| 7   | End     | 44.000  | 0.01      | 0.03       | 0.01        | 0.00     | 0.00  | 0.0         | 5.7        | 0.0      | 1.14       | 1.70     | 1.45 | 12                  | 0.23      | 60.40       | 60.50   | 61.70               | 61.75   | 60.40           | 63.90   | -90 deg   |
| 8   | 7       | 80.000  | 0.01      | 0.02       | 0.01        | 0.00     | 0.00  | 0.0         | 4.6        | 0.0      | 0.91       | 1.78     | 1.16 | 12                  | 0.25      | 60.50       | 60.70   | 61.76               | 61.81   | 63.90           | 63.90   | -15.2 deg |
| 9   | 8       | 160.000 | 0.01      | 0.01       | 0.01        | 0.00     | 0.00  | 0.0         | 0.0        | 0.0      | 0.46       | 1.99     | 0.72 | 12                  | 0.31      | 60.70       | 61.20   | 61.82               | 61.85   | 63.90           | 64.20   | 28.2 deg  |
| 10  | End     | 21.000  | 0.01      | 0.01       | 0.01        | 0.00     | 0.00  | 0.0         | 0.0        | 0.0      | 0.17       | 2.83     | 0.31 | 10                  | 1.67      | 60.40       | 60.75   | 61.70               | 61.70   | 60.40           | 64.75   | -90 deg   |
| 11  | End     | 21.000  | 0.01      | 0.01       | 0.01        | 0.00     | 0.00  | 0.0         | 0.0        | 0.0      | 0.16       | 2.83     | 0.29 | 10                  | 1.67      | 60.40       | 60.75   | 61.70               | 61.70   | 60.40           | 64.75   | -90 deg   |
| 12  | End     | 233.000 | 0.01      | 0.01       | 0.01        | 0.00     | 0.00  | 0.0         | 0.0        | 0.0      | 3.55       | 4.72     | 2.01 | 18                  | 0.20      | 57.28       | 57.75   | 59.10               | 59.37   | 64.80           | 61.40   | 180 deg   |
| Project File: JAB Nolte_24.0328.stm             |         |         |           |            |             |          |       |             |            |          |            |          |      | Number of lines: 12 |           |             |         | Run Date: 3/28/2024 |         |                 |         |           |
| NOTES:Known Qs only ; c = cir e = ellip b = box |         |         |           |            |             |          |       |             |            |          |            |          |      |                     |           |             |         |                     |         |                 |         |           |

# Hydraulic Grade Line Computations

| Line<br>(1) | Size<br>(in)<br>(2) | Q<br>(cfs)<br>(3) | Downstream                    |                            |                      |                       |                      |                            |                             | Len<br>(ft)<br>(12) | Upstream                       |                             |                       |                        |                       |                             |                             | Check             |                          | JL<br>coeff<br>(K)<br>(23)     | Minor<br>loss<br>(ft)<br>(24) |      |      |
|-------------|---------------------|-------------------|-------------------------------|----------------------------|----------------------|-----------------------|----------------------|----------------------------|-----------------------------|---------------------|--------------------------------|-----------------------------|-----------------------|------------------------|-----------------------|-----------------------------|-----------------------------|-------------------|--------------------------|--------------------------------|-------------------------------|------|------|
|             |                     |                   | Invert<br>elev<br>(ft)<br>(4) | HGL<br>elev<br>(ft)<br>(5) | Depth<br>(ft)<br>(6) | Area<br>(sqft)<br>(7) | Vel<br>(ft/s)<br>(8) | Vel<br>head<br>(ft)<br>(9) | EGL<br>elev<br>(ft)<br>(10) |                     | Invert<br>elev<br>(ft)<br>(13) | HGL<br>elev<br>(ft)<br>(14) | Depth<br>(ft)<br>(15) | Area<br>(sqft)<br>(16) | Vel<br>(ft/s)<br>(17) | Vel<br>head<br>(ft)<br>(18) | EGL<br>elev<br>(ft)<br>(19) | Sf<br>(%)<br>(20) | Ave<br>Sf<br>(%)<br>(21) | Energy<br>loss<br>(ft)<br>(22) |                               |      |      |
| 1           | 12                  | 1.48              | 60.40                         | 61.70                      | 1.00                 | 0.79                  | 1.88                 | 0.06                       | 61.76                       | 0.173               | 123.000                        | 60.70                       | 61.91                 | 1.00                   | 0.79                  | 1.88                        | 0.06                        | 61.97             | 0.173                    | 0.173                          | 0.212                         | 0.15 | 0.01 |
| 2           | 12                  | 0.82              | 60.70                         | 61.92                      | 1.00                 | 0.79                  | 1.04                 | 0.02                       | 61.94                       | 0.053               | 89.000                         | 60.90                       | 61.97                 | 1.00                   | 0.79                  | 1.04                        | 0.02                        | 61.98             | 0.053                    | 0.053                          | 0.047                         | 0.15 | 0.00 |
| 3           | 12                  | 0.38              | 60.90                         | 61.97                      | 1.00                 | 0.79                  | 0.48                 | 0.00                       | 61.97                       | 0.011               | 94.000                         | 61.10                       | 61.98                 | 0.88                   | 0.73                  | 0.52                        | 0.00                        | 61.98             | 0.010                    | 0.011                          | 0.010                         | 1.00 | 0.00 |
| 4           | 12                  | 0.33              | 60.40                         | 61.70                      | 1.00                 | 0.79                  | 0.42                 | 0.00                       | 61.70                       | 0.009               | 24.000                         | 60.50                       | 61.70                 | 1.00                   | 0.79                  | 0.42                        | 0.00                        | 61.70             | 0.009                    | 0.009                          | 0.002                         | 0.15 | 0.00 |
| 5           | 12                  | 0.29              | 60.50                         | 61.70                      | 1.00                 | 0.79                  | 0.37                 | 0.00                       | 61.70                       | 0.007               | 55.000                         | 60.80                       | 61.71                 | 0.91                   | 0.75                  | 0.39                        | 0.00                        | 61.71             | 0.006                    | 0.006                          | 0.003                         | 0.21 | 0.00 |
| 6           | 12                  | 0.19              | 60.80                         | 61.71                      | 0.91                 | 0.10                  | 0.25                 | 0.06                       | 61.77                       | 0.000               | 116.000                        | 61.75                       | 61.93 j               | 0.18**                 | 0.10                  | 2.00                        | 0.06                        | 61.99             | 0.000                    | 0.000                          | n/a                           | 1.00 | n/a  |
| 7           | 12                  | 1.14              | 60.40                         | 61.70                      | 1.00                 | 0.79                  | 1.45                 | 0.03                       | 61.73                       | 0.103               | 44.000                         | 60.50                       | 61.75                 | 1.00                   | 0.79                  | 1.45                        | 0.03                        | 61.78             | 0.102                    | 0.102                          | 0.045                         | 0.31 | 0.01 |
| 8           | 12                  | 0.91              | 60.50                         | 61.76                      | 1.00                 | 0.79                  | 1.16                 | 0.02                       | 61.78                       | 0.065               | 80.000                         | 60.70                       | 61.81                 | 1.00                   | 0.79                  | 1.16                        | 0.02                        | 61.83             | 0.065                    | 0.065                          | 0.052                         | 0.53 | 0.01 |
| 9           | 12                  | 0.46              | 60.70                         | 61.82                      | 1.00                 | 0.79                  | 0.59                 | 0.01                       | 61.82                       | 0.017               | 160.000                        | 61.20                       | 61.85                 | 0.65                   | 0.54                  | 0.85                        | 0.01                        | 61.86             | 0.029                    | 0.023                          | 0.037                         | 1.00 | 0.01 |
| 10          | 10                  | 0.17              | 60.40                         | 61.70                      | 0.83                 | 0.55                  | 0.31                 | 0.00                       | 61.70                       | 0.006               | 21.000                         | 60.75                       | 61.70                 | 0.83                   | 0.55                  | 0.31                        | 0.00                        | 61.70             | 0.006                    | 0.006                          | 0.001                         | 1.00 | 0.00 |
| 11          | 10                  | 0.16              | 60.40                         | 61.70                      | 0.83                 | 0.55                  | 0.29                 | 0.00                       | 61.70                       | 0.005               | 21.000                         | 60.75                       | 61.70                 | 0.83                   | 0.55                  | 0.29                        | 0.00                        | 61.70             | 0.005                    | 0.005                          | 0.001                         | 1.00 | 0.00 |
| 12          | 18                  | 3.55              | 57.28                         | 59.10                      | 1.50                 | 1.77                  | 2.01                 | 0.06                       | 59.16                       | 0.114               | 233.000                        | 57.75                       | 59.37                 | 1.50                   | 1.77                  | 2.01                        | 0.06                        | 59.43             | 0.114                    | 0.114                          | 0.266                         | 1.00 | 0.06 |

Project File: JAB Nolte\_24.0328.stm

Number of lines: 12

Run Date: 3/28/2024

Notes: ; \*\* Critical depth.; j-Line contains hyd. jump ; c = cir e = ellip b = box

# Hydraflow HGL Computation Procedure

---

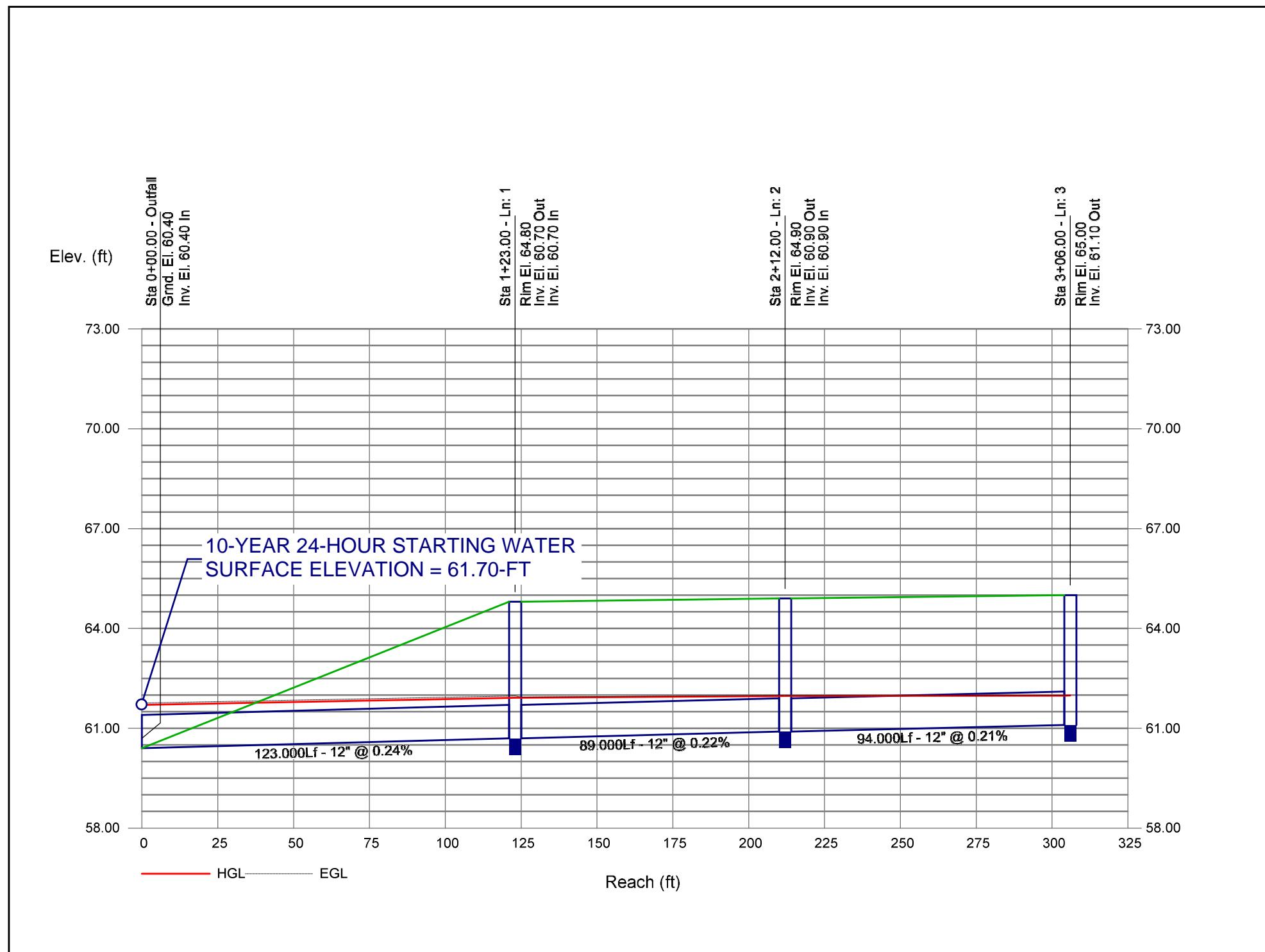
## General Procedure:

Hydraflow computes the HGL using the Bernoulli energy equation. Manning's equation is used to determine energy losses due to pipe friction. In a standard step, iterative procedure, Hydraflow assumes upstream HGLs until the energy equation balances. If the energy equation cannot balance, supercritical flow exists and critical depth is temporarily assumed at the upstream end. A supercritical flow profile is then computed using the same procedure in a downstream direction using momentum principles.

- Col. 1 The line number being computed. Calculations begin at Line 1 and proceed upstream.
- Col. 2 The line size. In the case of non-circular pipes, the line rise is printed above the span.
- Col. 3 Total flow rate in the line.
- Col. 4 The elevation of the downstream invert.
- Col. 5 Elevation of the hydraulic grade line at the downstream end. This is computed as the upstream HGL + Minor loss of this line's downstream line.
- Col. 6 The downstream depth of flow inside the pipe (HGL - Invert elevation) but not greater than the line size.
- Col. 7 Cross-sectional area of the flow at the downstream end.
- Col. 8 The velocity of the flow at the downstream end, (Col. 3 / Col. 7).
- Col. 9 Velocity head (Velocity squared / 2g).
- Col. 10 The elevation of the energy grade line at the downstream end, HGL + Velocity head, (Col. 5 + Col. 9).
- Col. 11 The friction slope at the downstream end (the S or Slope term in Manning's equation).
- Col. 12 The line length.
- Col. 13 The elevation of the upstream invert.
- Col. 14 Elevation of the hydraulic grade line at the upstream end.
- Col. 15 The upstream depth of flow inside the pipe (HGL - Invert elevation) but not greater than the line size.
- Col. 16 Cross-sectional area of the flow at the upstream end.
- Col. 17 The velocity of the flow at the upstream end, (Col. 3 / Col. 16).
- Col. 18 Velocity head (Velocity squared / 2g).
- Col. 19 The elevation of the energy grade line at the upstream end, HGL + Velocity head, (Col. 14 + Col. 18) .
- Col. 20 The friction slope at the upstream end (the S or Slope term in Manning's equation).
- Col. 21 The average of the downstream and upstream friction slopes.
- Col. 22 Energy loss. Average  $S_f/100 \times \text{Line Length}$  (Col. 21/100 x Col. 12). Equals  $(\text{EGL upstream} - \text{EGL downstream}) \pm \text{tolerance}$ .
- Col. 23 The junction loss coefficient (K).
- Col. 24 Minor loss. (Col. 23 x Col. 18). Is added to upstream HGL and used as the starting HGL for the next upstream line(s).

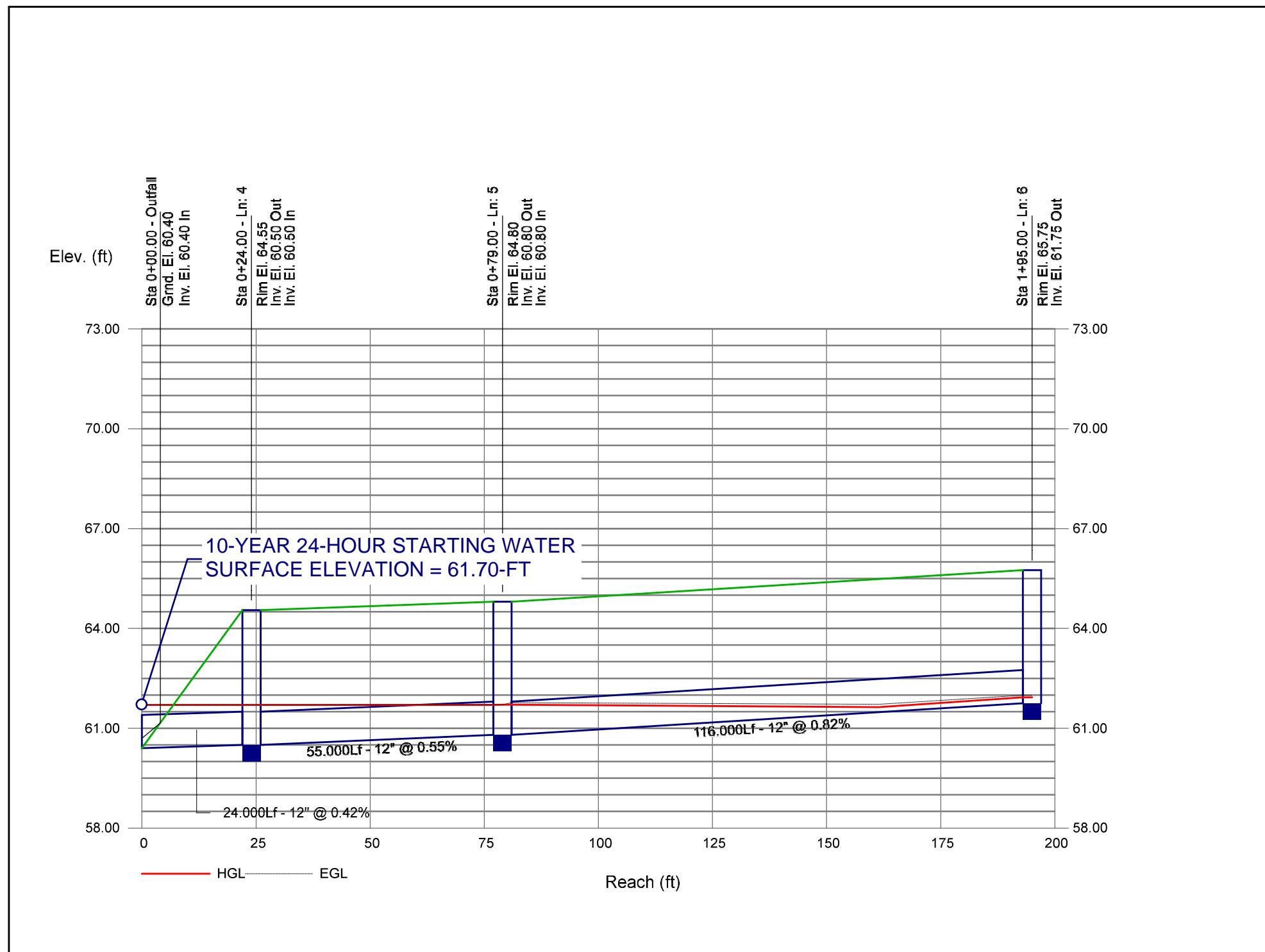
# Storm Sewer Profile

Proj. file: JAB Nolte\_24.0327.stm



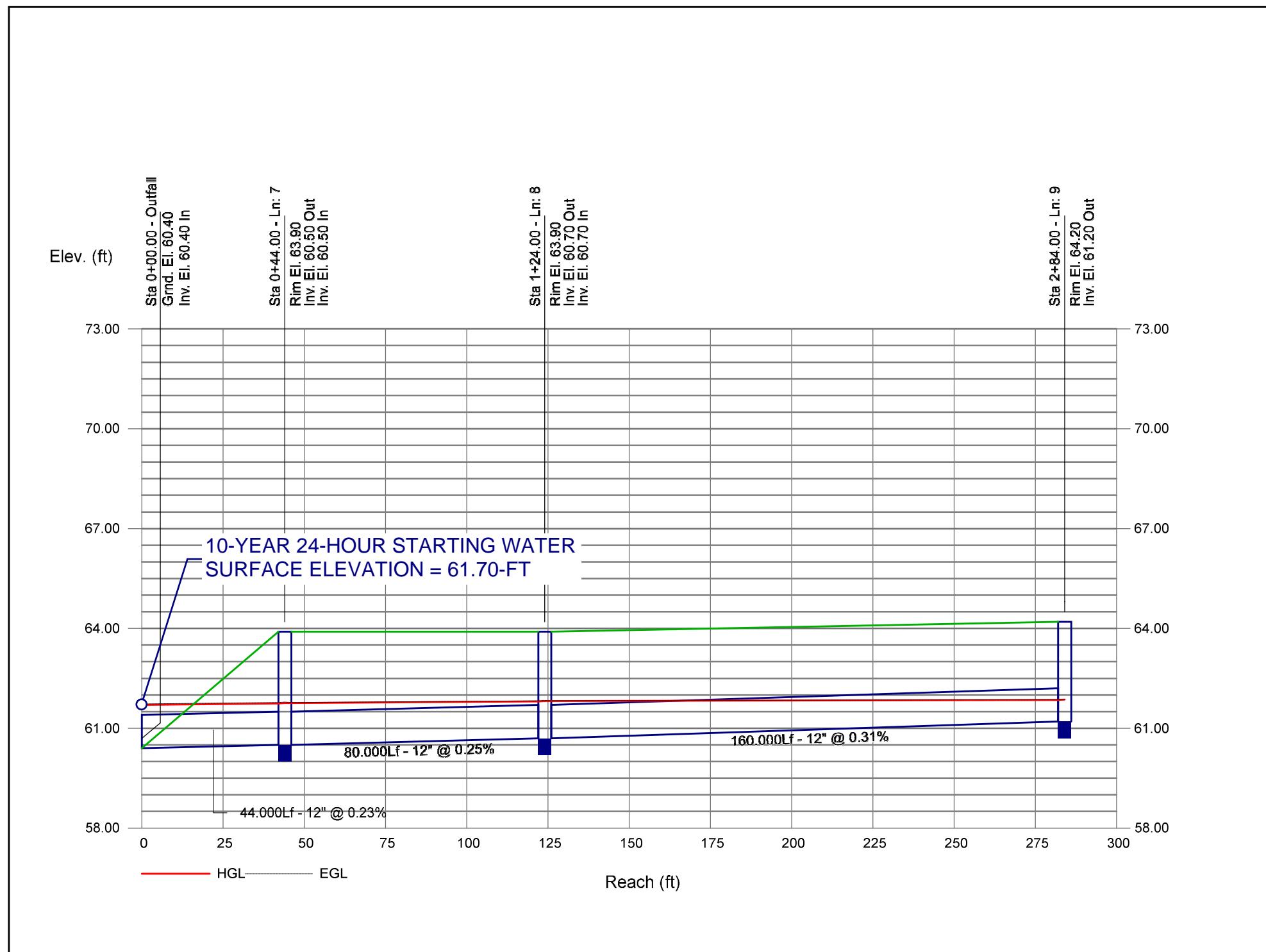
# Storm Sewer Profile

Proj. file: JAB Nolte\_24.0327.stm



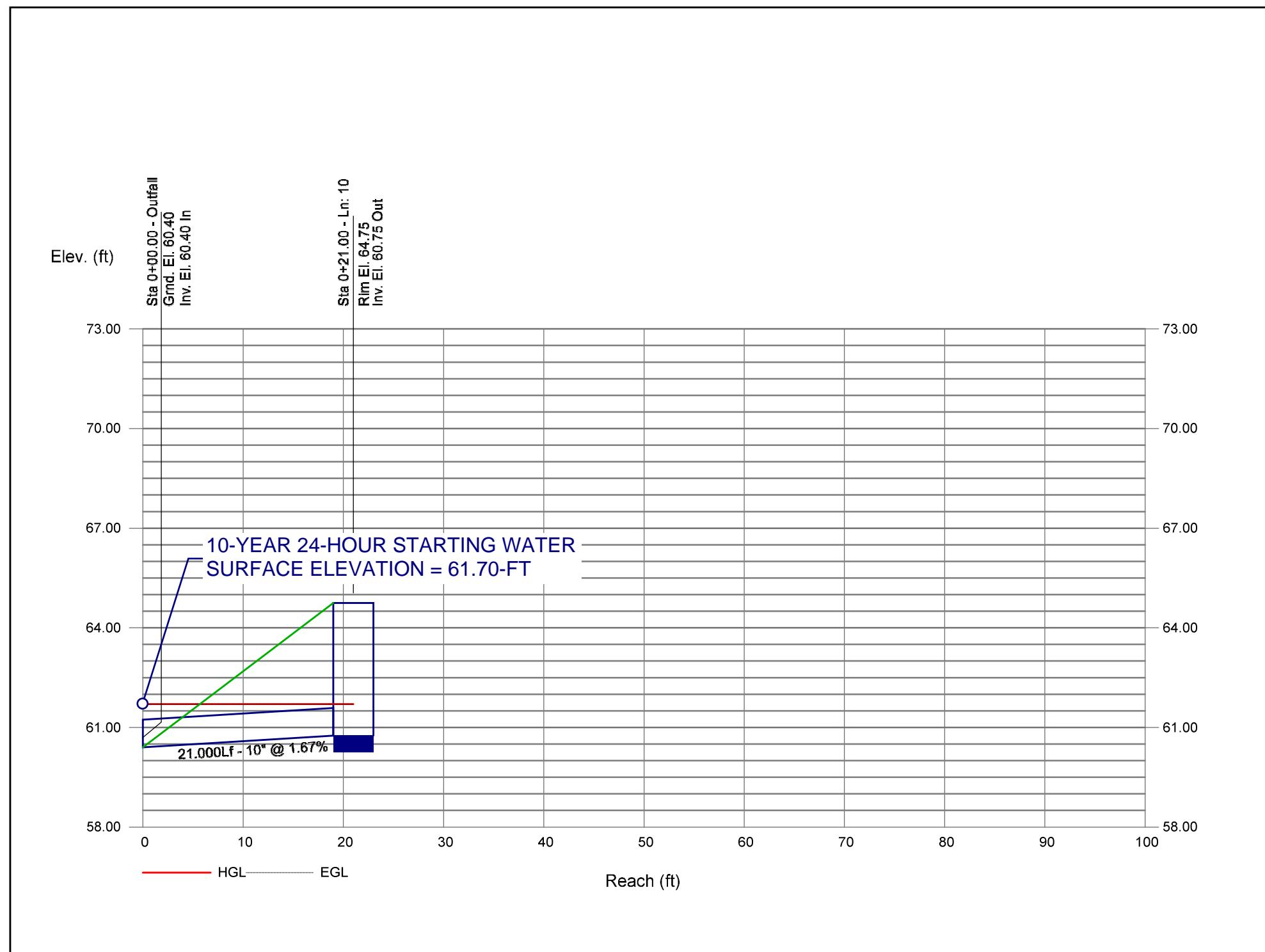
# Storm Sewer Profile

Proj. file: JAB Nolte\_24.0327.stm



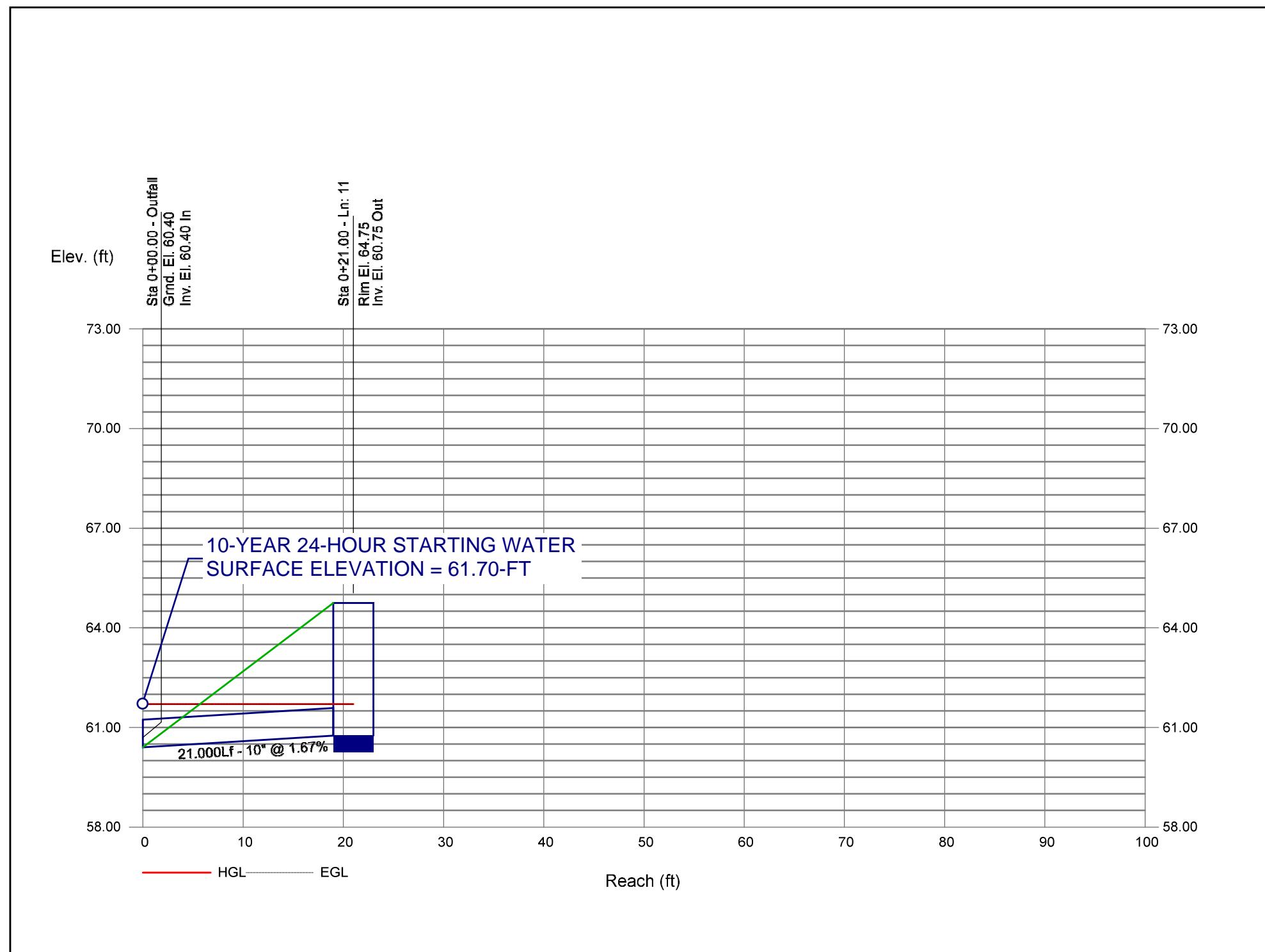
# Storm Sewer Profile

Proj. file: JAB Nolte\_24.0327.stm



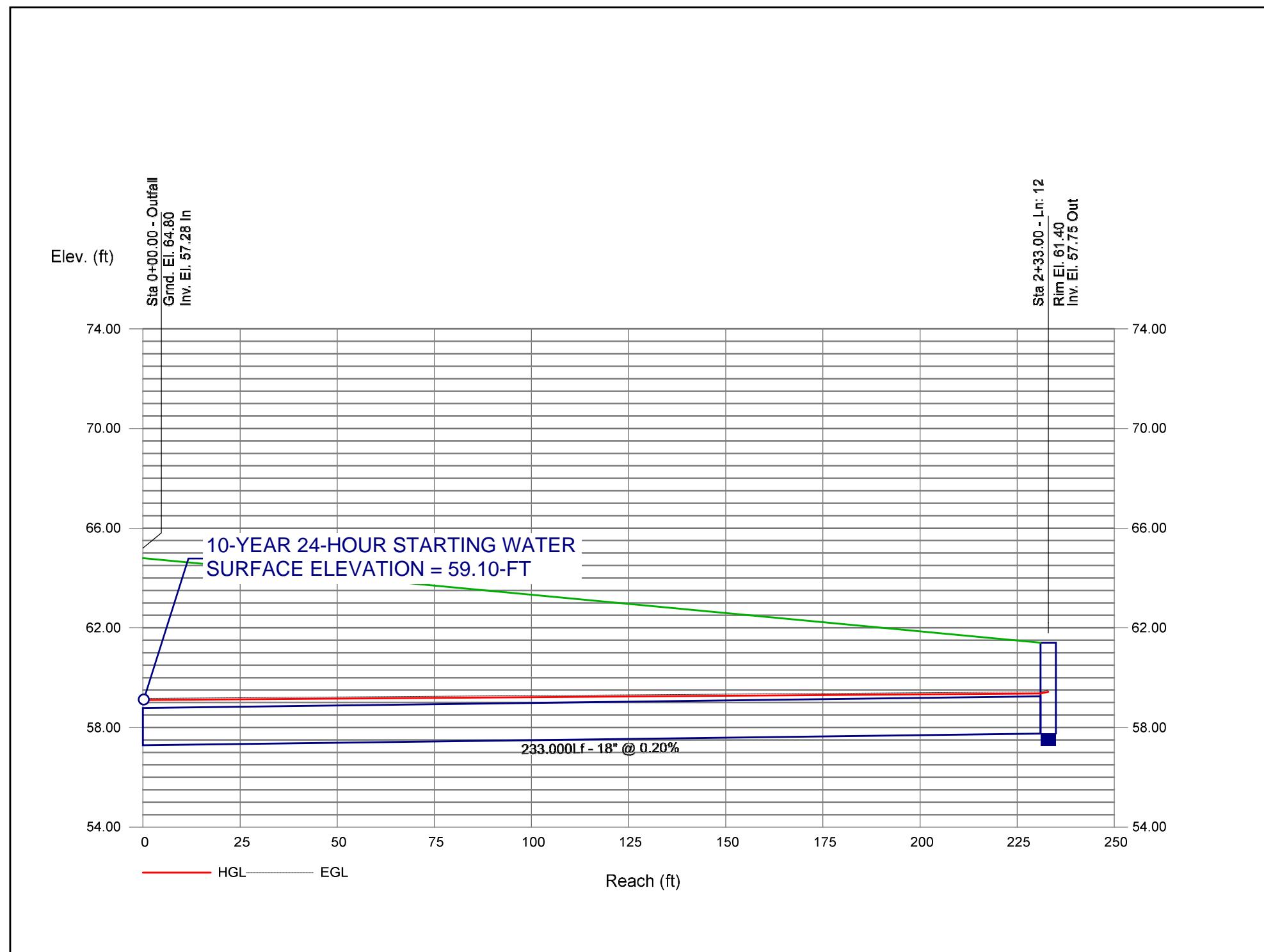
# Storm Sewer Profile

Proj. file: JAB Nolte\_24.0327.stm



# Storm Sewer Profile

Proj. file: JAB Nolte\_24.0328.stm



## **APPENDIX G:**

### **Post-Development Stormwater Watershed Map and LID Worksheets**

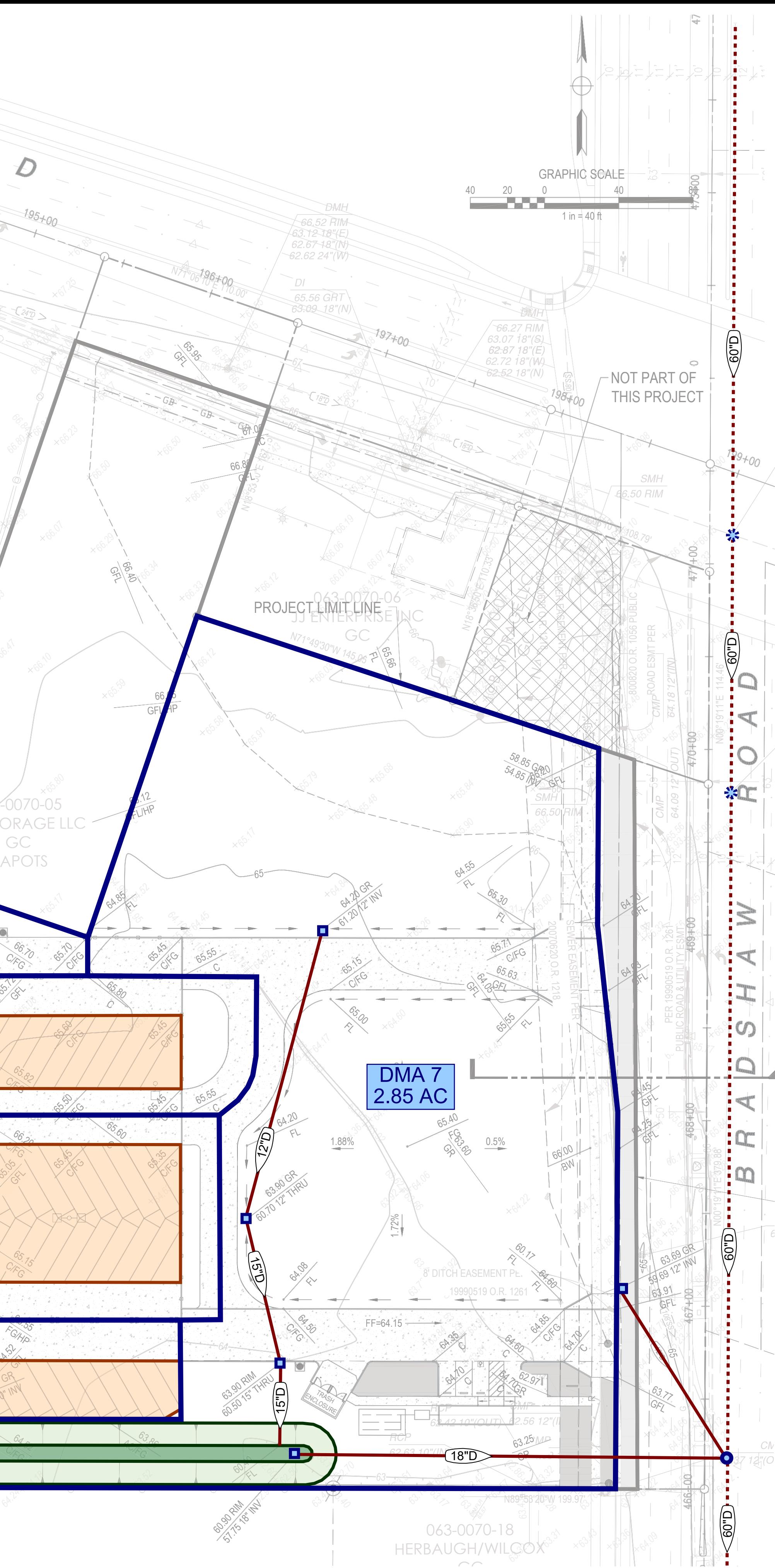
| LEGEND:  |                           |
|--|---------------------------|
| <span style="color: black;">—</span>   | WATERSHED BOUNDARY        |
| <span style="background-color: green; border: 1px solid black; display: inline-block; width: 15px; height: 10px;"></span>  | BIORETENTION BASIN        |
| <span style="background-color: orange; border: 1px solid black; display: inline-block; width: 15px; height: 10px;"></span> | POROUS GRAVEL PAVEMENT    |
| <span style="border: 1px solid black; display: inline-block; width: 10px; height: 10px;"></span>                           | PROPOSED DI               |
| <span style="color: blue; font-size: 2em; vertical-align: middle;">●</span>  | PROPOSED DRAINAGE MANHOLE |
| <span style="color: blue; font-size: 2em; vertical-align: middle;">*</span>  | EXISTING DRAINAGE MANHOLE |
| <span style="color: red; font-weight: bold;">—</span>  | PROPOSED STORM DRAIN PIPE |
| <span style="color: red; font-weight: bold;">-----</span>  | EXISTING STORM DRAIN PIPE |

#### LID Worksheet Summary

| DMA    | Area   |      | Impervious |      | Pervious (Landscape) |      | Pervious (Landscape w/o Bioretention Basin) |      |
|--------|--------|------|------------|------|----------------------|------|---|------|
|        | sf     | ac   | sf         | ac   | sf                   | ac   | sf  | ac   |
| DMA 1  | 32985  | 0.76 | 12561      | 0.29 | 4088                 | 0.09 | -   | -    |
| DMA 2  | 38171  | 0.88 | 19573      | 0.45 | 1165                 | 0.03 | -   | -    |
| DMA 3  | 57213  | 1.31 | 21604      | 0.50 | 896                  | 0.02 | -   | -    |
| DMA 4  | 28138  | 0.65 | 11003      | 0.25 | 0                    | 0.00 | -   | -    |
| DMA 5  | 24777  | 0.57 | 8540       | 0.20 | 3478                 | 0.08 | -   | -    |
| DMA 6  | 3453   | 0.08 | 1256       | 0.03 | 1041                 | 0.02 | -   | -    |
| DMA 7  | 124333 | 2.85 | 75949      | 1.74 | 48162                | 1.11 | 42802                                       | 0.98 |
| Totals | 309070 | 7.10 | 150487     | 3.45 | 58830                | 1.35 | 42802                                       | 0.98 |

| Existing Tree Canopy | Bioretention Basin |                    |               |
|----------------------|--------------------|--------------------|---------------|
|                      | sf                 | Subdrain Elevation | Ponding Depth |
| -                    | -                  | -                  | -             |
| -                    | -                  | -                  | -             |
| -                    | -                  | -                  | -             |
| -                    | -                  | -                  | -             |
| 950                  | -                  | -                  | -             |
| -                    | -                  | -                  | -             |
| -                    | 5360               | 18                 | 12            |

| Porous Gravel Pavement | Gravel Depth |      |      |      |  |
|------------------------|--------------|------|------|------|--|
|                        | sf           | in   | ft   |      |  |
| 16335                  | 0.38         | 1.00 | 0.58 | 0.35 |  |
| 17433                  | 0.40         | 1.00 | 0.58 | 0.35 |  |
| 34713                  | 0.80         | 1.00 | 0.58 | 0.35 |  |
| 17135                  | 0.39         | 1.00 | 0.58 | 0.35 |  |
| 12759                  | 0.29         | 1.00 | 0.58 | 0.35 |  |
| 1156                   | 0.03         | 1.00 | 0.58 | 0.35 |  |
| -                      | -            | -    | -    | -    |  |



NOT FOR CONSTRUCTION

| NO. | DESCRIPTION | APPD. ENGR. | DATE | APPD. EU. | DATE |
|-----|-------------|-------------|------|-----------|------|
|     |             |             |      |           |      |

SCALE:  
HORIZ. 1" = 40'  
VERT. 1" = N/A

BENCH MARK  
COUNTY B.M. 01A-35  
EL=65.63 (NAVD 88)

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**J @ B STORAGE**  
**5220 BRADSHAW ROAD & 9680 JACKSON ROAD**  
SACRAMENTO, CALIFORNIA

DATE  
MARCH 2024  
SHEET  
C-2  
2 OF 6

## LID Worksheet Summary

| DMA    | Area   |      | Impervious |      | Pervious (Landscape) |      | Pervious (Landscape w/o Bioretention Basin) |      | Existing Tree Canopy | Bioretention Basin | Subdrain Elevation | Ponding Depth | Porous Gravel Pavement |      | Gravel Depth | Sand Depth | Porosity | Design Treatment Volume |       | Required Treatment Volume (1) |       | Actual LID Credits per DMA (1) | Allowable LID Credits per DMA (2) | Percent of Site | Prorated LID Credits |                          |       |
|--------|--------|------|------------|------|----------------------|------|---|------|----------------------|--------------------|--------------------|---------------|------------------------|------|--------------|------------|----------|-------------------------|-------|-------------------------------|-------|--------------------------------|-----------------------------------|-----------------|----------------------|--------------------------|-------|
|        | sf     | ac   | sf         | ac   | sf                   | ac   | sf  | ac   |                      |                    |                    |               | sf                     | ac   | ft           | ft         | ac-ft    | ac-ft                   | ac-ft | ac-ft                         | ac-ft | ac-ft                          |                                   |                 |                      |                          |       |
| DMA 1  | 32985  | 0.76 | 12561      | 0.29 | 4088                 | 0.09 | -   | -    |                      |                    |                    |               | 16335                  | 0.38 | 1.00         | 0.58       | 0.35     | 0.208                   | 0.016 |                               |       |                                |                                   | 53.5            | 53.5                 | 10.7%                    | 5.7   |
| DMA 2  | 38171  | 0.88 | 19573      | 0.45 | 1165                 | 0.03 | -   | -    |                      |                    |                    |               | 17433                  | 0.40 | 1.00         | 0.58       | 0.35     | 0.222                   | 0.021 |                               |       |                                |                                   | 41.5            | 41.5                 | 12.4%                    | 5.1   |
| DMA 3  | 57213  | 1.31 | 21604      | 0.50 | 896                  | 0.02 | -   | -    |                      |                    |                    |               | 34713                  | 0.80 | 1.00         | 0.58       | 0.35     | 0.442                   | 0.030 |                               |       |                                |                                   | 43.9            | 43.9                 | 18.5%                    | 8.1   |
| DMA 4  | 28138  | 0.65 | 11003      | 0.25 | 0                    | 0.00 | -   | -    |                      |                    |                    |               | 17135                  | 0.39 | 1.00         | 0.58       | 0.35     | 0.218                   | 0.015 |                               |       |                                |                                   | 41.4            | 41.4                 | 9.1%                     | 3.8   |
| DMA 5  | 24777  | 0.57 | 8540       | 0.20 | 3478                 | 0.08 | -   | -    |                      |                    |                    |               | 12759                  | 0.29 | 1.00         | 0.58       | 0.35     | 0.162                   | 0.011 |                               |       |                                |                                   | 56.4            | 56.4                 | 8.0%                     | 4.5   |
| DMA 6  | 3453   | 0.08 | 1256       | 0.03 | 1041                 | 0.02 | -   | -    |                      |                    |                    |               | 1156                   | 0.03 | 1.00         | 0.58       | 0.35     | 0.015                   | 0.001 |                               |       |                                |                                   | 66.2            | 66.2                 | 1.1%                     | 0.7   |
| DMA 7  | 124333 | 2.85 | 75949      | 1.74 | 48162                | 1.11 | 42802                                       | 0.98 |                      |                    |                    |               | -                      | -    | -            | -          | -        | -                       | -     | -                             | -     |                                | 231.6                             | 200.0           | 40.2%                | 80.5                     |       |
| Totals | 309070 | 7.10 | 150487     | 3.45 | 58830                | 1.35 | 42802                                       | 0.98 |                      |                    |                    |               | 99532                  | 2.28 |              |            |          | 1.27                    | 0.094 |                               |       |                                |                                   |                 |                      | Total Project LID Points | 108.4 |

(1) Required Treatment Volume and LID Credits per Commercial LID Worksheet (excel)

(2) Maximum allowable LID points per DMA is 200

## Appendix D-2: Commercial Sites: Low Impact Development (LID) Credits and Treatment BMP Sizing Calculations

Name of Drainage Shed: DMA 1  
Location of project: Sacramento

Fill in Blue Highlighted boxes

### Step 1 - Open Space and Pervious Area Credits

Is your project within the drainage area of a common drainage plan that includes open space? If not, skip to 1 b.

1 a. Common Drainage Plan Area  acres A<sub>CDP</sub>

#### Common Drainage Plan Open Space (Off-project)

- a. Natural storage reservoirs and drainage corridors
  - b. Buffer zones for natural water bodies
  - c. Natural areas including existing trees, other vegetation, and soil
  - d. Common landscape area/park
  - e. Regional Flood Control/Drainage basins
- |                                |       |
|--------------------------------|-------|
| <input type="text" value="0"/> | acres |

A<sub>OS</sub>

see area example below

1 b. Project Drainage Shed Area (Total)  acres A

#### Project-Specific Open Space (In-project, communal\*\*)

- a. Natural storage reservoirs and drainage corridors
  - b. Buffer zones for natural water bodies
  - c. Natural areas including existing trees, other vegetation, and soil
  - d. Landscape area/park
  - e. Flood Control/Drainage basins
- |                                   |       |
|-----------------------------------|-------|
| <input type="text" value="0.09"/> | acres |
| <input type="text" value="0.00"/> | acres |
| <input type="text" value="0.00"/> | acres |
| <input type="text" value="0.00"/> | acres |
| <input type="text" value="0.09"/> | acres |
| <input type="text" value="0.00"/> | acres |

A<sub>PSOS</sub>

see area example below

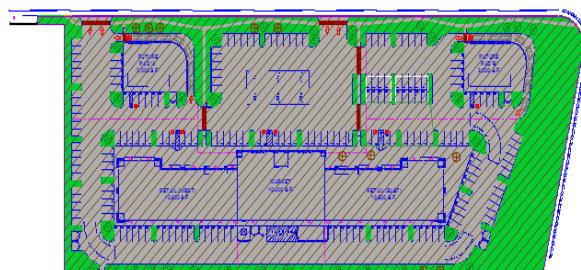
\*\* Doesn't include impervious areas within individual lots and surrounding individual units. That is accounted for below using Form D-1a in Step 2.

Area with Runoff Reduction Potential A - A<sub>PSOS</sub> =  acres A<sub>T</sub>

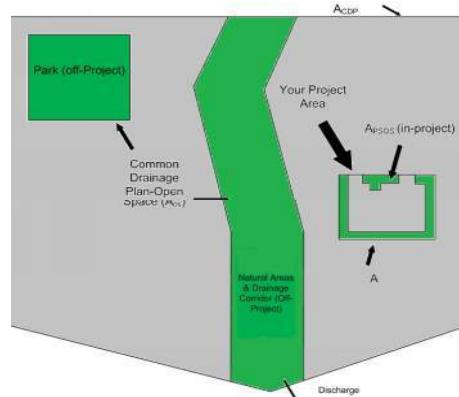
Assumed Initial Impervious Fraction A<sub>T</sub> / A =  I

#### Open Space & Pervious Area LID Credit (Step 1)

(A<sub>OS</sub>/A<sub>CDP</sub>+A<sub>PSOS</sub>/A)×100 =  pts



|  |   |
|--|---|
|  | A - Drainage Shed Area                                |
|  | A <sub>OS</sub> Open Space and Landscaping            |
|  | A <sub>T</sub> - Area with Runoff Reduction Potential |



### Step 2 - Runoff Reduction Credits

| Runoff Reduction Treatments  | Impervious Area Managed                        | Efficiency Factor  | Effective Area Managed (A <sub>C</sub> )   |
|--|--|--|--|
| <b>Porous Pavement:</b>  |  |  |  |
| Option 1: Porous Pavement<br>(see Fact Sheet, excludes porous pavement used in Option 2)       | <input type="text"/>                           | acres x <input type="text"/>   | = <input type="text" value="0.000"/> acres |
| Option 2: Disconnected Pavement<br>(see Fact Sheet, excludes porous pavement used in Option 1) | use Form D-2a for credits <input type="text"/> |  | = <input type="text" value="0.28"/> acres  |
| Landscaping used to Disconnect Pavement<br>(see Fact Sheet)                                    | 0.0000   | acres  | = <input type="text" value="0.00"/> acres  |
| Disconnected Roof Drains<br>(see Fact Sheet and/or Table D-2b for summary of requirements)     | 0  | acres  | = <input type="text" value="0.00"/> acres  |
| Ecoroof<br>(see Fact Sheet)  | 0  | acres  | = <input type="text" value="0.00"/> acres  |
| Interceptor Trees<br>(see Fact Sheet)  | use Form D-2b for credits <input type="text"/> |  | = <input type="text" value="0.00"/> acres  |
| Total Effective Area Managed by Runoff Reduction Measures                                      |  | A <sub>C</sub>   | <input type="text" value="0.28"/> acres    |
| Runoff Reduction Credit (Step 2)   |  | (A <sub>C</sub> / A <sub>T</sub> )×100 = <input type="text" value="42"/> | pts  |

**Table D-2a**

| Porous Pavement Type       | Efficiency Multiplier |
|----------------------------|-----------------------|
| Cobblestone Block Pavement | 0.40                  |
| Pervious Concrete/Asphalt  | 0.60                  |
| Modular Block Pavement &   | 0.75                  |
| Reinforced Grass Pavement  | 1.00                  |

**Table D-2b**

| Maximum roof size | Minimum travel distance |
|-------------------|-------------------------|
| ≤ 3,500 sq ft     | 21 ft                   |
| ≤ 5,000 sq ft     | 24 ft                   |
| ≤ 7,500 sq ft     | 28 ft                   |
| ≤ 10,000 sq ft    | 32 ft                   |

**Form D-2a: Disconnected Pavement Worksheet**

See Fact Sheet for more information regarding Disconnected Pavement credit guidelines

Effective Area Managed (A<sub>c</sub>)**Pavement Draining to Porous Pavement**

2. Enter area draining onto Porous Pavement

0.29

acres Box K1

3. Enter area of Receiving Porous Pavement  
(excludes area entered in Step 2 under Porous Pavement)

0.38

acres Box K2

4. Ratio of Areas (Box K1 / Box K2)

0.76

Box K3

5. Select multiplier using ratio from Box K3 and enter into Box K4

| Ratio (Box D)            | Multiplier |
|--------------------------|------------|
| Ratio is ≤ 0.5           | 1.00       |
| Ratio is > 0.5 and < 1.0 | 0.83       |
| Ratio is > 1.0 and < 1.5 | 0.71       |
| Ratio is > 1.5 and < 2.0 | 0.55       |

0.83

Box K4

6. Enter Efficiency of Porous Pavement (see table below)

0.75

Box K5

| Porous Pavement Type               | Efficiency Multiplier |
|------------------------------------|-----------------------|
| Cobblestone Block Pavement         | 0.40                  |
| Pervious Concrete Asphalt Pavement | 0.60                  |
| Modular Block Pavement             | 0.75                  |
| Porous Gravel Pavement             | 1.00                  |
| Reinforced Grass Pavement          | 1.00                  |

7. Multiply Box K2 by Box K5 and enter into Box K6

0.29

acres Box K6

8. Multiply Boxes K1,K4, and K5 and enter the result in Box K7

0.18

acres Box K7

9. Add Box K6 to Box K7 and multiply by 60%, and enter the Result in Box K8  
This is the amount of area credit to enter into the "Disconnected Pavement" Box of Form D-2

0.28 acres

**Form D-2b: Interceptor Tree Worksheet**

See Fact Sheet for more information regarding Interceptor Tree credit guidelines

**New Evergreen Trees**

1. Enter number of new evergreen trees that qualify as Interceptor Trees in Box L1.

trees

Box L1

2. Multiply Box L1 by 200 and enter result in Box L2

0 sq. ft.

Box L2

**New Deciduous Trees**

3. Enter number of new deciduous trees that qualify as Interceptor Trees in Box L3.

trees

Box L3

4. Multiply Box L3 by 100 and enter result in Box L4

0 sq. ft.

Box L4

**Existing Tree Canopy**

5. Enter square footage of existing tree canopy that qualifies as Existing Tree canopy in Box L5.

sq. ft.

Box L5

6. Multiply Box L5 by 0.5 and enter the result in Box L6

0 sq. ft.

Box L6

**Total Interceptor Tree EAM Credits**

Add Boxes L2, L4, and L6 and enter it into Box L7

0 sq. ft.

Box L7

Divide Box L7 by 43,560 and multiply by 20% to get effective area managed and enter result in Box L8

0.00 acres

Box L8

This is the amount of area credit to enter into the "Interceptor Trees" Box of Form D-2

**Step 3 - Runoff Management Credits**

**Capture and Use Credits**

**Impervious Area Managed by Rain barrels, Cisterns, and automaticallyemptied systems**  
 (see Fact Sheet) \_\_\_\_\_ enter gallons, for simple rain barrels 0.00 acres

**Automated-Control Capture and Use System**  
 (see Fact Sheet, then enter impervious area managed by the system) 0.00 acres

**Bioretention/Infiltration Credits**

**Impervious Area Managed by Bioretention BMPs**  
 (see Fact Sheet) Bioretention Area \_\_\_\_\_ sq ft  
 Subdrain Elevation \_\_\_\_\_ inches  
 Ponding Depth, inches \_\_\_\_\_ inches 0.00 acres

**Impervious Area Managed by Infiltration BMPs**  
 (see Fact Sheet) Drawdown Time, hrs \_\_\_\_\_ drawdown\_hrs\_inf  
 Soil Infiltration Rate, in/hr \_\_\_\_\_ soil\_inf\_rate

Sizing Option 1: Capture Volume, acre-ft \_\_\_\_\_ 0.00 capture\_vol\_inf 0.00 acres

Sizing Option 2: Infiltration BMP surface area, sq ft \_\_\_\_\_ 0 soil\_surface\_area 0.00 acres

Basin or trench? \_\_\_\_\_ approximate BMP depth 0.00 ft

**Impervious Area Managed by Amended Soil or Mulch Beds**  
 (see Fact Sheet) Mulched Infiltration Area, sq ft \_\_\_\_\_ mulch\_area 0.00 acres

**Total Effective Area Managed by Capture-and-Use/Bioretention/Infiltration BMPs** 0.00 A\_LIDC

**Runoff Management Credit (Step 3)** 0.0 pts

|  |   |             |
|--|---|-------------|
| <b>Total LID Credits (Step 1+2+3)</b>  | <b>Warning: More LID Is Required</b>  | <b>53.5</b> |
| Does project require hydromodification management? If yes, proceed to using SacHM. |   |             |
| Adjusted Area for Flow-Based, Non-LID Treatment                                    | $A_T - A_C - A_{LIDC} =$ <span style="border: 1px solid black; padding: 2px;">0.39</span> | $A_{AT}$    |
| Adjusted Impervious Fraction of A for Volume-Based, Non-LID Treatment              | $A_{AT} / A =$ <span style="border: 1px solid black; padding: 2px;">0.51</span>           | $I_A$       |

**Further treatment is required, see choose flow-based or volume-based sizing in Step 4**

**Step 4a Treatment - Flow-Based (Rational Method)**

Calculate treatment flow (cfs): Flow = Runoff Coefficient x Rainfall Intensity x Area

Look up value for i in Table D-2c (Rainfall Intensity) 0.18 i

Obtain  $A_{AT}$  from Step 3 0.39  $A_{AT}$

Use  $C = 0.95$  0.95 C

$Flow = 0.95 * i * A_{AT}$  0.07 cfs

|                           |                |
|---------------------------|----------------|
| <b>Table D-2c</b>         |                |
| <b>Rainfall Intensity</b> |                |
| Roseville                 | i = 0.20 in/hr |
| Sacramento                | i = 0.18 in/hr |
| Folsom                    | i = 0.20 in/hr |

**Step 4b Treatment - Volume-Based (ASCE-WEF)**

Calculate water quality volume (Acre-Feet):  $WQV = \text{Area} \times \text{Maximized Detention Volume } (P_0)$

Obtain A from Step 1 0.76 A 12 hrs Specified Draw Down time

Obtain  $P_0$ : Maximized Detention Volume from figures E-1 to E-4 in Appendix E of this manual using  $I_A$  from Step 2. 0.25  $P_0$

Calculate treatment volume (acre-ft):  $Treatment\ volume = A \times (P_0 / 12)$  0.016 Acre-Feet

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## Appendix D-2: Commercial Sites: Low Impact Development (LID) Credits and Treatment BMP Sizing Calculations

Name of Drainage Shed: DMA 2

Fill in Blue Highlighted boxes

Location of project: Sacramento

### Step 1 - Open Space and Pervious Area Credits

Is your project within the drainage area of a common drainage plan that includes open space? If not, skip to 1 b.

**1 a. Common Drainage Plan Area**

0 acres

A<sub>CDP</sub>

#### Common Drainage Plan Open Space (Off-project)

- a. Natural storage reservoirs and drainage corridors
- b. Buffer zones for natural water bodies
- c. Natural areas including existing trees, other vegetation, and soil
- d. Common landscape area/park
- e. Regional Flood Control/Drainage basins

0 acres  
0 acres  
0 acres  
0 acres  
0 acres  
0 acres

A<sub>OS</sub>

see area example below

#### 1 b. Project Drainage Shed Area (Total)

0.88 acres

A

#### Project-Specific Open Space (In-project, communal\*\*)

- a. Natural storage reservoirs and drainage corridors
- b. Buffer zones for natural water bodies
- c. Natural areas including existing trees, other vegetation, and soil
- d. Landscape area/park
- e. Flood Control/Drainage basins

0.03 acres  
0.00 acres  
0.00 acres  
0.00 acres  
0.03 acres  
0.00 acres

A<sub>PSOS</sub>

see area example below

\*\* Doesn't include impervious areas within individual lots and surrounding individual units. That is accounted for below using Form D-1a in Step 2.

#### Area with Runoff Reduction Potential

A - A<sub>PSOS</sub> =  0.85 acres

A<sub>T</sub>

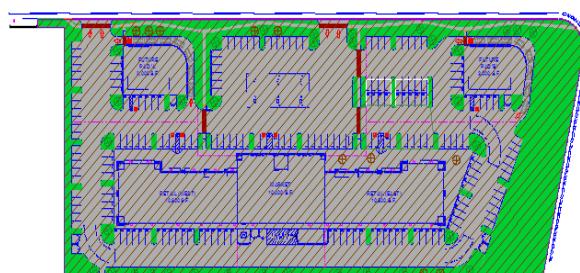
#### Assumed Initial Impervious Fraction

A<sub>T</sub> / A =  0.97

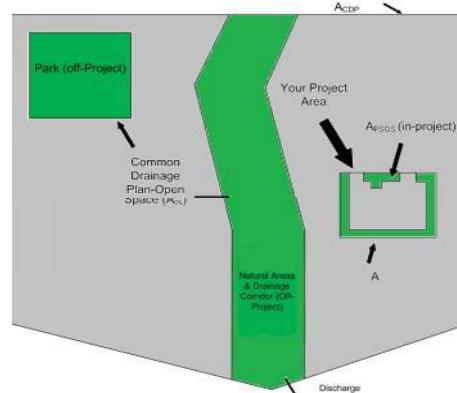
I

#### Open Space & Pervious Area LID Credit (Step 1)

(A<sub>OS</sub>/A<sub>CDP</sub>+A<sub>PSOS</sub>/A)×100 =  3 pts



|  |   |
|--|---|
|  | A - Drainage Shed Area                                |
|  | APOS Open Space and Landscaping                       |
|  | A <sub>T</sub> - Area with Runoff Reduction Potential |



### Step 2 - Runoff Reduction Credits

| Runoff Reduction Treatments   | Impervious Area Managed   | Efficiency Factor            | Effective Area Managed (A <sub>C</sub> )                             |
|---|---------------------------|------------------------------|--|
| <b>Porous Pavement:</b>   |                           |                              |  |
| <b>Option 1: Porous Pavement</b><br>(see Fact Sheet, excludes porous pavement used in Option 2)       | <input type="text"/>      | acres x <input type="text"/> | = <input type="text"/> 0.000 acres                                   |
| <b>Option 2: Disconnected Pavement</b><br>(see Fact Sheet, excludes porous pavement used in Option 1) | use Form D-2a for credits |                              | → <input type="text"/> 0.32 acres                                    |
| <b>Landscape used to Disconnect Pavement</b><br>(see Fact Sheet)                                      | 0.0000                    | acres                        | = <input type="text"/> 0.00 acres                                    |
| <b>Disconnected Roof Drains</b><br>(see Fact Sheet and/or Table D-2b for summary of requirements)     | 0                         | acres                        | = <input type="text"/> 0.00 acres                                    |
| <b>Ecoroof</b><br>(see Fact Sheet)  | 0                         | acres                        | = <input type="text"/> 0.00 acres                                    |
| <b>Interceptor Trees</b><br>(see Fact Sheet)  | use Form D-2b for credits |                              | → <input type="text"/> 0.00 acres                                    |
| <b>Total Effective Area Managed by Runoff Reduction Measures</b>                                      |                           | A <sub>C</sub>               | <input type="text"/> 0.32 acres                                      |
| <b>Runoff Reduction Credit (Step 2)</b>   |                           |                              | (A <sub>C</sub> / A <sub>T</sub> )×100 = <input type="text"/> 38 pts |

**Table D-2a**

| Porous Pavement Type       | Efficiency Multiplier |
|----------------------------|-----------------------|
| Cobblestone Block Pavement | 0.40                  |
| Pervious Concrete/Asphalt  | 0.60                  |
| Modular Block Pavement &   | 0.75                  |
| Reinforced Grass Pavement  | 1.00                  |

**Table D-2b**

| Maximum roof size | Minimum travel distance |
|-------------------|-------------------------|
| ≤ 3,500 sq ft     | 21 ft                   |
| ≤ 5,000 sq ft     | 24 ft                   |
| ≤ 7,500 sq ft     | 28 ft                   |
| ≤ 10,000 sq ft    | 32 ft                   |

**Form D-2a: Disconnected Pavement Worksheet**

See Fact Sheet for more information regarding Disconnected Pavement credit guidelines

Effective Area Managed (A<sub>c</sub>)**Pavement Draining to Porous Pavement**

2. Enter area draining onto Porous Pavement

0.45

acres Box K1

3. Enter area of Receiving Porous Pavement  
(excludes area entered in Step 2 under Porous Pavement)

0.40

acres Box K2

4. Ratio of Areas (Box K1 / Box K2)

1.13

Box K3

5. Select multiplier using ratio from Box K3 and enter into Box K4

| Ratio (Box D)            | Multiplier |
|--------------------------|------------|
| Ratio is ≤ 0.5           | 1.00       |
| Ratio is > 0.5 and < 1.0 | 0.83       |
| Ratio is > 1.0 and < 1.5 | 0.71       |
| Ratio is > 1.5 and < 2.0 | 0.55       |

0.71

Box K4

6. Enter Efficiency of Porous Pavement (see table below)

0.75

Box K5

| Porous Pavement Type               | Efficiency Multiplier |
|------------------------------------|-----------------------|
| Cobblestone Block Pavement         | 0.40                  |
| Pervious Concrete Asphalt Pavement | 0.60                  |
| Modular Block Pavement             | 0.75                  |
| Porous Gravel Pavement             | 1.00                  |
| Reinforced Grass Pavement          | 1.00                  |

7. Multiply Box K2 by Box K5 and enter into Box K6

0.30

acres Box K6

8. Multiply Boxes K1,K4, and K5 and enter the result in Box K7

0.24

acres Box K7

9. Add Box K6 to Box K7 and multiply by 60%, and enter the Result in Box K8  
This is the amount of area credit to enter into the "Disconnected Pavement" Box of Form D-2

0.32 acres

**Form D-2b: Interceptor Tree Worksheet**

See Fact Sheet for more information regarding Interceptor Tree credit guidelines

**New Evergreen Trees**

1. Enter number of new evergreen trees that qualify as Interceptor Trees in Box L1.

trees

Box L1

2. Multiply Box L1 by 200 and enter result in Box L2

0 sq. ft.

Box L2

**New Deciduous Trees**

3. Enter number of new deciduous trees that qualify as Interceptor Trees in Box L3.

trees

Box L3

4. Multiply Box L3 by 100 and enter result in Box L4

0 sq. ft.

Box L4

**Existing Tree Canopy**

5. Enter square footage of existing tree canopy that qualifies as Existing Tree canopy in Box L5.

sq. ft.

Box L5

6. Multiply Box L5 by 0.5 and enter the result in Box L6

0 sq. ft.

Box L6

**Total Interceptor Tree EAM Credits**

Add Boxes L2, L4, and L6 and enter it into Box L7

0 sq. ft.

Box L7

Divide Box L7 by 43,560 and multiply by 20% to get effective area managed and enter result in Box L8

0.00

acres

This is the amount of area credit to enter into the "Interceptor Trees" Box of Form D-2

### Step 3 - Runoff Management Credits

#### Capture and Use Credits

##### Impervious Area Managed by Rain barrels, Cisterns, and automaticallyemptied systems

(see Fact Sheet) \_\_\_\_\_ enter gallons, for simple rain barrels

acres

##### Automated-Control Capture and Use System

(see Fact Sheet, then enter impervious area managed by the system)

acres

#### Bioretention/Infiltration Credits

##### Impervious Area Managed by Bioretention BMPs

(see Fact Sheet)

Bioretention Area \_\_\_\_\_ sq ft

Subdrain Elevation \_\_\_\_\_ inches

Ponding Depth, inches \_\_\_\_\_ inches

acres

##### Impervious Area Managed by Infiltration BMPs

(see Fact Sheet)

Drawdown Time, hrs \_\_\_\_\_ drawdown\_hrs\_inf

Soil Infiltration Rate, in/hr \_\_\_\_\_ soil\_inf\_rate

Sizing Option 1: Capture Volume, acre-ft \_\_\_\_\_ 0.00 capture\_vol\_inf

acres

Sizing Option 2: Infiltration BMP surface area, sq ft \_\_\_\_\_ 0 soil\_surface\_area

acres

Basin or trench? \_\_\_\_\_ approximate BMP depth  ft

##### Impervious Area Managed by Amended Soil or Mulch Beds

(see Fact Sheet)

Mulched Infiltration Area, sq ft \_\_\_\_\_ mulch\_area

acres

#### Total Effective Area Managed by Capture-and-Use/Bioretention/Infiltration BMPs

A\_LIDC

#### Runoff Management Credit (Step 3)

A\_LIDC/A\_T \* 200 =  pts

### Total LID Credits (Step 1+2+3)

Warning: More LID Is Required 41.5

Does project require hydromodification management? If yes, proceed to using SacHM.

Adjusted Area for Flow-Based, Non-LID Treatment

A\_T - A\_C - A\_LIDC =  A\_AT

Adjusted Impervious Fraction of A for Volume-Based, Non-LID Treatment

A\_AT / A =  I\_A

**Further treatment is required, see choose flow-based or volume-based sizing in Step 4**

### Step 4a Treatment - Flow-Based (Rational Method)

Calculate treatment flow (cfs):

Flow = Runoff Coefficient x Rainfall Intensity x Area

Look up value for i in Table D-2c (Rainfall Intensity)

i

Table D-2c

| Rainfall Intensity |     |            |
|--------------------|-----|------------|
| Roseville          | i = | 0.20 in/hr |
| Sacramento         | i = | 0.18 in/hr |
| Folsom             | i = | 0.20 in/hr |

Obtain A\_AT from Step 3

A\_AT

Use C = 0.95

C

Flow = 0.95 \* i \* A\_AT

cfs

### Step 4b Treatment - Volume-Based (ASCE-WEF)

Calculate water quality volume (Acre-Feet):

WQV = Area x Maximized Detention Volume ( $P_0$ )

Obtain A from Step 1

A

hrs

Specified Draw Down time

Obtain  $P_0$ : Maximized Detention Volume from figures E-1 to E-4 in Appendix E of this manual using  $I_A$  from Step 2.

$P_0$

Calculate treatment volume (acre-ft):

Treatment volume = A x ( $P_0$  / 12)

Acre-Feet

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## Appendix D-2: Commercial Sites: Low Impact Development (LID) Credits and Treatment BMP Sizing Calculations

Name of Drainage Shed: DMA 3  
Location of project: Sacramento

Fill in Blue Highlighted boxes

### Step 1 - Open Space and Pervious Area Credits

Is your project within the drainage area of a common drainage plan that includes open space? If not, skip to 1 b.

**1 a. Common Drainage Plan Area**

#### Common Drainage Plan Open Space (Off-project)

- a. Natural storage reservoirs and drainage corridors
- b. Buffer zones for natural water bodies
- c. Natural areas including existing trees, other vegetation, and soil
- d. Common landscape area/park
- e. Regional Flood Control/Drainage basins

|   |       |
|---|-------|
| 0 | acres |

A<sub>CDP</sub>

see area example below

**1 b. Project Drainage Shed Area (Total)**

|      |       |
|------|-------|
| 1.31 | acres |
| 0.02 | acres |
| 0.00 | acres |
| 0.00 | acres |
| 0.00 | acres |
| 0.02 | acres |
| 0.00 | acres |

A

#### Project-Specific Open Space (In-project, communal\*\*)

- a. Natural storage reservoirs and drainage corridors
- b. Buffer zones for natural water bodies
- c. Natural areas including existing trees, other vegetation, and soil
- d. Landscape area/park
- e. Flood Control/Drainage basins

|      |       |
|------|-------|
| 0.02 | acres |
| 0.00 | acres |
| 0.00 | acres |
| 0.00 | acres |
| 0.02 | acres |
| 0.00 | acres |

A<sub>PSOS</sub>

see area example below

\*\* Doesn't include impervious areas within individual lots and surrounding individual units. That is accounted for below using Form D-1a in Step 2.

**Area with Runoff Reduction Potential**

A - A<sub>PSOS</sub> = 1.29 acres

A<sub>T</sub>

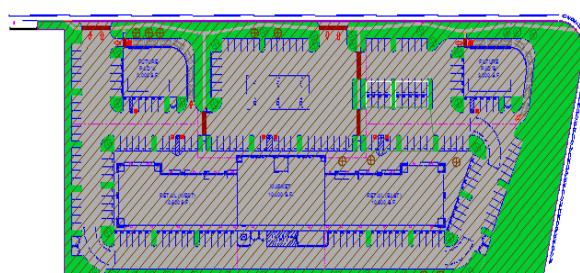
**Assumed Initial Impervious Fraction**

A<sub>T</sub> / A = 0.98

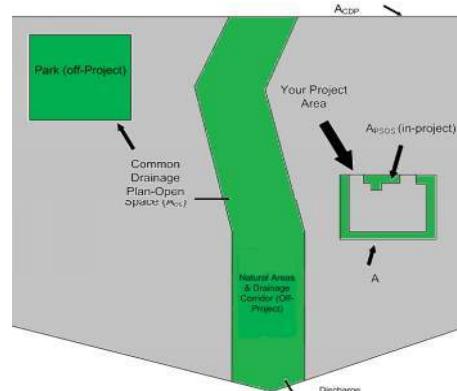
I

#### Open Space & Pervious Area LID Credit (Step 1)

(A<sub>OS</sub>/A<sub>CDP</sub>+A<sub>PSOS</sub>/A)×100 = 2 pts



|   |
|---|
| A - Drainage Shed Area                                |
| A <sub>PSOS</sub> Open Space and Landscaping          |
| A <sub>T</sub> - Area with Runoff Reduction Potential |



### Step 2 - Runoff Reduction Credits

| Runoff Reduction Treatments   | Impervious Area Managed   | Efficiency Factor                        | Effective Area Managed (A <sub>C</sub> ) |
|---|---------------------------|--|--|
| <b>Porous Pavement:</b>   |                           |  |  |
| <b>Option 1: Porous Pavement</b><br>(see Fact Sheet, excludes porous pavement used in Option 2)       |                           | acres                                    | x      =      0.000      acres           |
| <b>Option 2: Disconnected Pavement</b><br>(see Fact Sheet, excludes porous pavement used in Option 1) | use Form D-2a for credits |  | →      0.55      acres                   |
| <b>Landscape used to Disconnect Pavement</b><br>(see Fact Sheet)                                      | 0.0000                    | acres                                    | =      0.00      acres                   |
| <b>Disconnected Roof Drains</b><br>(see Fact Sheet and/or Table D-2b for summary of requirements)     | 0                         | acres                                    | =      0.00      acres                   |
| <b>Ecoroof</b><br>(see Fact Sheet)  | 0                         | acres                                    | =      0.00      acres                   |
| <b>Interceptor Trees</b><br>(see Fact Sheet)  | use Form D-2b for credits |  | →      0.00      acres                   |
| <b>Total Effective Area Managed by Runoff Reduction Measures</b>                                      |                           | A <sub>C</sub>                           | 0.55      acres                          |
| <b>Runoff Reduction Credit (Step 2)</b>   |                           | (A <sub>C</sub> / A <sub>T</sub> )×100 = | 42      pts                              |

**Table D-2a**

| Porous Pavement Type       | Efficiency Multiplier |
|----------------------------|-----------------------|
| Cobblestone Block Pavement | 0.40                  |
| Pervious Concrete/Asphalt  | 0.60                  |
| Modular Block Pavement &   | 0.75                  |
| Reinforced Grass Pavement  | 1.00                  |

**Table D-2b**

| Maximum roof size | Minimum travel distance |
|-------------------|-------------------------|
| ≤ 3,500 sq ft     | 21 ft                   |
| ≤ 5,000 sq ft     | 24 ft                   |
| ≤ 7,500 sq ft     | 28 ft                   |
| ≤ 10,000 sq ft    | 32 ft                   |

**Form D-2a: Disconnected Pavement Worksheet**

See Fact Sheet for more information regarding Disconnected Pavement credit guidelines

Effective Area Managed (A<sub>c</sub>)**Pavement Draining to Porous Pavement**

2. Enter area draining onto Porous Pavement

0.50

acres Box K1

3. Enter area of Receiving Porous Pavement  
(excludes area entered in Step 2 under Porous Pavement)

0.80

acres Box K2

4. Ratio of Areas (Box K1 / Box K2)

0.63

Box K3

5. Select multiplier using ratio from Box K3 and enter into Box K4

| Ratio (Box D)            | Multiplier |
|--------------------------|------------|
| Ratio is ≤ 0.5           | 1.00       |
| Ratio is > 0.5 and < 1.0 | 0.83       |
| Ratio is > 1.0 and < 1.5 | 0.71       |
| Ratio is > 1.5 and < 2.0 | 0.55       |

0.83

Box K4

6. Enter Efficiency of Porous Pavement (see table below)

0.75

Box K5

| Porous Pavement Type               | Efficiency Multiplier |
|------------------------------------|-----------------------|
| Cobblestone Block Pavement         | 0.40                  |
| Pervious Concrete Asphalt Pavement | 0.60                  |
| Modular Block Pavement             | 0.75                  |
| Porous Gravel Pavement             | 1.00                  |
| Reinforced Grass Pavement          | 1.00                  |

7. Multiply Box K2 by Box K5 and enter into Box K6

0.60

acres Box K6

8. Multiply Boxes K1,K4, and K5 and enter the result in Box K7

0.31

acres Box K7

9. Add Box K6 to Box K7 and multiply by 60%, and enter the Result in Box K8  
This is the amount of area credit to enter into the "Disconnected Pavement" Box of Form D-2

0.55 acres

**Form D-2b: Interceptor Tree Worksheet**

See Fact Sheet for more information regarding Interceptor Tree credit guidelines

**New Evergreen Trees**

1. Enter number of new evergreen trees that qualify as Interceptor Trees in Box L1.

trees

Box L1

2. Multiply Box L1 by 200 and enter result in Box L2

0 sq. ft.

Box L2

**New Deciduous Trees**

3. Enter number of new deciduous trees that qualify as Interceptor Trees in Box L3.

trees

Box L3

4. Multiply Box L3 by 100 and enter result in Box L4

0 sq. ft.

Box L4

**Existing Tree Canopy**

5. Enter square footage of existing tree canopy that qualifies as Existing Tree canopy in Box L5.

sq. ft.

Box L5

6. Multiply Box L5 by 0.5 and enter the result in Box L6

0 sq. ft.

Box L6

**Total Interceptor Tree EAM Credits**

Add Boxes L2, L4, and L6 and enter it into Box L7

0 sq. ft.

Box L7

Divide Box L7 by 43,560 and multiply by 20% to get effective area managed and enter result in Box L8

0.00 acres

Box L8

This is the amount of area credit to enter into the "Interceptor Trees" Box of Form D-2

### Step 3 - Runoff Management Credits

#### Capture and Use Credits

##### Impervious Area Managed by Rain barrels, Cisterns, and automaticallyemptied systems

(see Fact Sheet) \_\_\_\_\_ enter gallons, for simple rain barrels

acres

##### Automated-Control Capture and Use System

(see Fact Sheet, then enter impervious area managed by the system)

acres

#### Bioretention/Infiltration Credits

##### Impervious Area Managed by Bioretention BMPs

(see Fact Sheet)

Bioretention Area \_\_\_\_\_ sq ft

Subdrain Elevation \_\_\_\_\_ inches

Ponding Depth, inches \_\_\_\_\_ inches

acres

##### Impervious Area Managed by Infiltration BMPs

(see Fact Sheet)

Drawdown Time, hrs \_\_\_\_\_ drawdown\_hrs\_inf

Soil Infiltration Rate, in/hr \_\_\_\_\_ soil\_inf\_rate

Sizing Option 1: Capture Volume, acre-ft \_\_\_\_\_ 0.00 capture\_vol\_inf

acres

Sizing Option 2: Infiltration BMP surface area, sq ft \_\_\_\_\_ 0 soil\_surface\_area

acres

Basin or trench? \_\_\_\_\_ approximate BMP depth  ft

##### Impervious Area Managed by Amended Soil or Mulch Beds

(see Fact Sheet)

Mulched Infiltration Area, sq ft \_\_\_\_\_ mulch\_area

acres

#### Total Effective Area Managed by Capture-and-Use/Bioretention/Infiltration BMPs

A\_LIDC

#### Runoff Management Credit (Step 3)

A\_LIDC/A\_T \* 200 =  pts

### Total LID Credits (Step 1+2+3)

Warning: More LID Is Required 43.9

Does project require hydromodification management? If yes, proceed to using SacHM.

Adjusted Area for Flow-Based, Non-LID Treatment

A\_T - A\_C - A\_LIDC =  A\_AT

Adjusted Impervious Fraction of A for Volume-Based, Non-LID Treatment

A\_AT / A =  I\_A

**Further treatment is required, see choose flow-based or volume-based sizing in Step 4**

### Step 4a Treatment - Flow-Based (Rational Method)

Calculate treatment flow (cfs):

Flow = Runoff Coefficient x Rainfall Intensity x Area

Look up value for i in Table D-2c (Rainfall Intensity)

i

Table D-2c

| Rainfall Intensity |     |            |
|--------------------|-----|------------|
| Roseville          | i = | 0.20 in/hr |
| Sacramento         | i = | 0.18 in/hr |
| Folsom             | i = | 0.20 in/hr |

Obtain A\_AT from Step 3

A\_AT

Use C = 0.95

C

Flow = 0.95 \* i \* A\_AT

cfs

### Step 4b Treatment - Volume-Based (ASCE-WEF)

Calculate water quality volume (Acre-Feet):

WQV = Area x Maximized Detention Volume ( $P_0$ )

Obtain A from Step 1

A

hrs

Specified Draw Down time

Obtain  $P_0$ : Maximized Detention Volume from figures E-1 to E-4 in Appendix E of this manual using  $I_A$  from Step 2.

$P_0$

Calculate treatment volume (acre-ft):

Treatment volume = A x ( $P_0$  / 12)

Acre-Feet

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## Appendix D-2: Commercial Sites: Low Impact Development (LID) Credits and Treatment BMP Sizing Calculations

Name of Drainage Shed: DMA 4  
Location of project: Sacramento

Fill in Blue Highlighted boxes

### Step 1 - Open Space and Pervious Area Credits

Is your project within the drainage area of a common drainage plan that includes open space? If not, skip to 1 b.

**1 a. Common Drainage Plan Area**

#### Common Drainage Plan Open Space (Off-project)

- a. Natural storage reservoirs and drainage corridors
- b. Buffer zones for natural water bodies
- c. Natural areas including existing trees, other vegetation, and soil
- d. Common landscape area/park
- e. Regional Flood Control/Drainage basins

|   |       |
|---|-------|
| 0 | acres |

A<sub>CDP</sub>

see area example below

**1 b. Project Drainage Shed Area (Total)**

|      |       |
|------|-------|
| 0.65 | acres |
|------|-------|

A

#### Project-Specific Open Space (In-project, communal\*\*)

- a. Natural storage reservoirs and drainage corridors
- b. Buffer zones for natural water bodies
- c. Natural areas including existing trees, other vegetation, and soil
- d. Landscape area/park
- e. Flood Control/Drainage basins

|      |       |
|------|-------|
| 0.00 | acres |

A<sub>PSOS</sub>

see area example below

\*\* Doesn't include impervious areas within individual lots and surrounding individual units. That is accounted for below using Form D-1a in Step 2.

**Area with Runoff Reduction Potential**

A - A<sub>PSOS</sub> = 

|      |       |
|------|-------|
| 0.65 | acres |
|------|-------|

A<sub>T</sub>

**Assumed Initial Impervious Fraction**

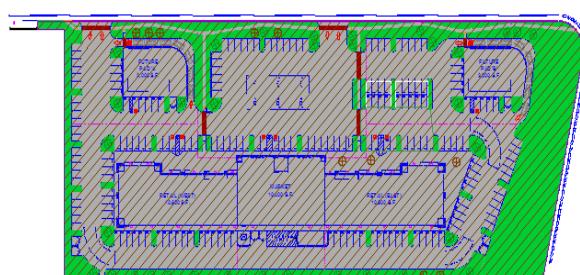
A<sub>T</sub> / A = 

|      |
|------|
| 1.00 |
|------|

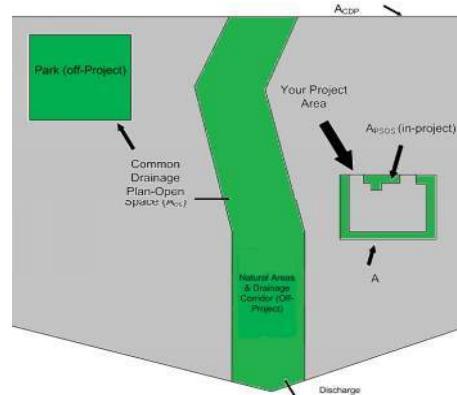
I

**Open Space & Pervious Area LID Credit (Step 1)**

$$(A_{OS}/A_{CDP}+A_{PSOS}/A)\times 100 = \boxed{0} \text{ pts}$$



**A – Drainage Shed Area**  
**A<sub>POS</sub> Open Space and Landscaping**  
**A<sub>T</sub> – Area with Runoff Reduction Potential**



### Step 2 - Runoff Reduction Credits

| Runoff Reduction Treatments   | Impervious Area Managed                                  | Efficiency Factor | Effective Area Managed (A <sub>C</sub> )               |  |   |       |
|---|--|-------------------|--|--|---|-------|
| <b>Porous Pavement:</b>   |  |                   |  |  |   |       |
| <b>Option 1: Porous Pavement</b><br>(see Fact Sheet, excludes porous pavement used in Option 2)       | <table border="1"><tr><td></td></tr></table> acres       |                   | x <table border="1"><tr><td></td></tr></table>         |  | = <table border="1"><tr><td>0.000</td></tr></table> acres | 0.000 |
|   |  |                   |  |  |   |       |
|   |  |                   |  |  |   |       |
| 0.000   |  |                   |  |  |   |       |
| <b>Option 2: Disconnected Pavement</b><br>(see Fact Sheet, excludes porous pavement used in Option 1) | <table border="1"><tr><td></td></tr></table> acres       |                   | use Form D-2a for credits →                            | <table border="1"><tr><td>0.27</td></tr></table> acres | 0.27  |       |
|   |  |                   |  |  |   |       |
| 0.27  |  |                   |  |  |   |       |
| <b>Landscaping used to Disconnect Pavement</b><br>(see Fact Sheet)                                    | <table border="1"><tr><td>0.0000</td></tr></table> acres | 0.0000            | =  | <table border="1"><tr><td>0.00</td></tr></table> acres | 0.00  |       |
| 0.0000  |  |                   |  |  |   |       |
| 0.00  |  |                   |  |  |   |       |
| <b>Disconnected Roof Drains</b><br>(see Fact Sheet and/or Table D-2b for summary of requirements)     | <table border="1"><tr><td>0</td></tr></table> acres      | 0                 | =  | <table border="1"><tr><td>0.00</td></tr></table> acres | 0.00  |       |
| 0   |  |                   |  |  |   |       |
| 0.00  |  |                   |  |  |   |       |
| <b>Ecoroof</b><br>(see Fact Sheet)  | <table border="1"><tr><td>0</td></tr></table> acres      | 0                 | =  | <table border="1"><tr><td>0.00</td></tr></table> acres | 0.00  |       |
| 0   |  |                   |  |  |   |       |
| 0.00  |  |                   |  |  |   |       |
| <b>Interceptor Trees</b><br>(see Fact Sheet)  | <table border="1"><tr><td></td></tr></table> acres       |                   | use Form D-2b for credits →                            | <table border="1"><tr><td>0.00</td></tr></table> acres | 0.00  |       |
|   |  |                   |  |  |   |       |
| 0.00  |  |                   |  |  |   |       |
| <b>Total Effective Area Managed by Runoff Reduction Measures</b>                                      |  | A <sub>C</sub>    | <table border="1"><tr><td>0.27</td></tr></table> acres | 0.27   |   |       |
| 0.27  |  |                   |  |  |   |       |
| <b>Runoff Reduction Credit (Step 2)</b>   |  |                   | $(A_C / A_T) \times 100 = \boxed{41}$ pts              |  |   |       |

**Table D-2a**

| Porous Pavement Type       | Efficiency Multiplier |
|----------------------------|-----------------------|
| Cobblestone Block Pavement | 0.40                  |
| Pervious Concrete/Asphalt  | 0.60                  |
| Modular Block Pavement &   | 0.75                  |
| Reinforced Grass Pavement  | 1.00                  |

**Table D-2b**

| Maximum roof size | Minimum travel distance |
|-------------------|-------------------------|
| ≤ 3,500 sq ft     | 21 ft                   |
| ≤ 5,000 sq ft     | 24 ft                   |
| ≤ 7,500 sq ft     | 28 ft                   |
| ≤ 10,000 sq ft    | 32 ft                   |

**Form D-2a: Disconnected Pavement Worksheet**

See Fact Sheet for more information regarding Disconnected Pavement credit guidelines

Effective Area Managed (A<sub>c</sub>)**Pavement Draining to Porous Pavement**

2. Enter area draining onto Porous Pavement

0.25

acres Box K1

3. Enter area of Receiving Porous Pavement  
(excludes area entered in Step 2 under Porous Pavement)

0.39

acres Box K2

4. Ratio of Areas (Box K1 / Box K2)

0.64

Box K3

5. Select multiplier using ratio from Box K3 and enter into Box K4

| Ratio (Box D)            | Multiplier |
|--------------------------|------------|
| Ratio is ≤ 0.5           | 1.00       |
| Ratio is > 0.5 and < 1.0 | 0.83       |
| Ratio is > 1.0 and < 1.5 | 0.71       |
| Ratio is > 1.5 and < 2.0 | 0.55       |

0.83

Box K4

6. Enter Efficiency of Porous Pavement (see table below)

0.75

Box K5

| Porous Pavement Type               | Efficiency Multiplier |
|------------------------------------|-----------------------|
| Cobblestone Block Pavement         | 0.40                  |
| Pervious Concrete Asphalt Pavement | 0.60                  |
| Modular Block Pavement             | 0.75                  |
| Porous Gravel Pavement             | 1.00                  |
| Reinforced Grass Pavement          | 1.00                  |

7. Multiply Box K2 by Box K5 and enter into Box K6

0.29

acres Box K6

8. Multiply Boxes K1,K4, and K5 and enter the result in Box K7

0.16

acres Box K7

9. Add Box K6 to Box K7 and multiply by 60%, and enter the Result in Box K8  
This is the amount of area credit to enter into the "Disconnected Pavement" Box of Form D-2

0.27 acres

**Form D-2b: Interceptor Tree Worksheet**

See Fact Sheet for more information regarding Interceptor Tree credit guidelines

**New Evergreen Trees**

1. Enter number of new evergreen trees that qualify as Interceptor Trees in Box L1.

trees

Box L1

2. Multiply Box L1 by 200 and enter result in Box L2

0 sq. ft.

Box L2

**New Deciduous Trees**

3. Enter number of new deciduous trees that qualify as Interceptor Trees in Box L3.

trees

Box L3

4. Multiply Box L3 by 100 and enter result in Box L4

0 sq. ft.

Box L4

**Existing Tree Canopy**

5. Enter square footage of existing tree canopy that qualifies as Existing Tree canopy in Box L5.

sq. ft.

Box L5

6. Multiply Box L5 by 0.5 and enter the result in Box L6

0 sq. ft.

Box L6

**Total Interceptor Tree EAM Credits**

Add Boxes L2, L4, and L6 and enter it into Box L7

0 sq. ft.

Box L7

Divide Box L7 by 43,560 and multiply by 20% to get effective area managed and enter result in Box L8

0.00 acres

Box L8

This is the amount of area credit to enter into the "Interceptor Trees" Box of Form D-2

### Step 3 - Runoff Management Credits

#### Capture and Use Credits

##### Impervious Area Managed by Rain barrels, Cisterns, and automaticallyemptied systems

(see Fact Sheet) \_\_\_\_\_ enter gallons, for simple rain barrels

acres

##### Automated-Control Capture and Use System

(see Fact Sheet, then enter impervious area managed by the system)

acres

#### Bioretention/Infiltration Credits

##### Impervious Area Managed by Bioretention BMPs

(see Fact Sheet)

Bioretention Area \_\_\_\_\_ sq ft

Subdrain Elevation \_\_\_\_\_ inches

Ponding Depth, inches \_\_\_\_\_ inches

acres

##### Impervious Area Managed by Infiltration BMPs

(see Fact Sheet)

Drawdown Time, hrs \_\_\_\_\_ drawdown\_hrs\_inf

Soil Infiltration Rate, in/hr \_\_\_\_\_ soil\_inf\_rate

Sizing Option 1: Capture Volume, acre-ft \_\_\_\_\_ 0.00 capture\_vol\_inf

acres

Sizing Option 2: Infiltration BMP surface area, sq ft \_\_\_\_\_ 0 soil\_surface\_area

acres

Basin or trench? \_\_\_\_\_ approximate BMP depth  ft

##### Impervious Area Managed by Amended Soil or Mulch Beds

(see Fact Sheet)

Mulched Infiltration Area, sq ft \_\_\_\_\_ mulch\_area

acres

#### Total Effective Area Managed by Capture-and-Use/Bioretention/Infiltration BMPs

A\_LIDC

#### Runoff Management Credit (Step 3)

A\_LIDC/A\_T \* 200 =  pts

### Total LID Credits (Step 1+2+3)

Warning: More LID Is Required 41.4

Does project require hydromodification management? If yes, proceed to using SacHM.

Adjusted Area for Flow-Based, Non-LID Treatment

A\_T - A\_C - A\_LIDC =  A\_AT

Adjusted Impervious Fraction of A for Volume-Based, Non-LID Treatment

A\_AT / A =  I\_A

**Further treatment is required, see choose flow-based or volume-based sizing in Step 4**

### Step 4a Treatment - Flow-Based (Rational Method)

Calculate treatment flow (cfs):

Flow = Runoff Coefficient x Rainfall Intensity x Area

Look up value for i in Table D-2c (Rainfall Intensity)

i

Table D-2c

| Rainfall Intensity |     |            |
|--------------------|-----|------------|
| Roseville          | i = | 0.20 in/hr |
| Sacramento         | i = | 0.18 in/hr |
| Folsom             | i = | 0.20 in/hr |

Obtain A\_AT from Step 3

A\_AT

Use C = 0.95

C

Flow = 0.95 \* i \* A\_AT

cfs

### Step 4b Treatment - Volume-Based (ASCE-WEF)

Calculate water quality volume (Acre-Feet):

WQV = Area x Maximized Detention Volume ( $P_0$ )

Obtain A from Step 1

A

hrs

Specified Draw Down time

Obtain  $P_0$ : Maximized Detention Volume from figures E-1 to E-4 in Appendix E of this manual using  $I_A$  from Step 2.

$P_0$

Calculate treatment volume (acre-ft):

Treatment volume = A x ( $P_0$  / 12)

Acre-Feet

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## Appendix D-2: Commercial Sites: Low Impact Development (LID) Credits and Treatment BMP Sizing Calculations

Name of Drainage Shed: DMA 5  
Location of project: Sacramento

Fill in Blue Highlighted boxes

### Step 1 - Open Space and Pervious Area Credits

Is your project within the drainage area of a common drainage plan that includes open space? If not, skip to 1 b.

1 a. Common Drainage Plan Area  acres A<sub>CDP</sub>

#### Common Drainage Plan Open Space (Off-project)

- a. Natural storage reservoirs and drainage corridors
  - b. Buffer zones for natural water bodies
  - c. Natural areas including existing trees, other vegetation, and soil
  - d. Common landscape area/park
  - e. Regional Flood Control/Drainage basins
- |                                      |                 |
|--------------------------------------|-----------------|
| <input type="text" value="0"/> acres | A <sub>OS</sub> |
| <input type="text" value="0"/> acres |                 |

see area example below

1 b. Project Drainage Shed Area (Total)  acres A

#### Project-Specific Open Space (In-project, communal\*\*)

- a. Natural storage reservoirs and drainage corridors
  - b. Buffer zones for natural water bodies
  - c. Natural areas including existing trees, other vegetation, and soil
  - d. Landscape area/park
  - e. Flood Control/Drainage basins
- |   |                   |
|---|-------------------|
| <input type="text" value="0.08"/> acres | A <sub>PSOS</sub> |
| <input type="text" value="0.00"/> acres |                   |
| <input type="text" value="0.00"/> acres |                   |
| <input type="text" value="0.00"/> acres |                   |
| <input type="text" value="0.08"/> acres |                   |
| <input type="text" value="0.00"/> acres |                   |

see area example below

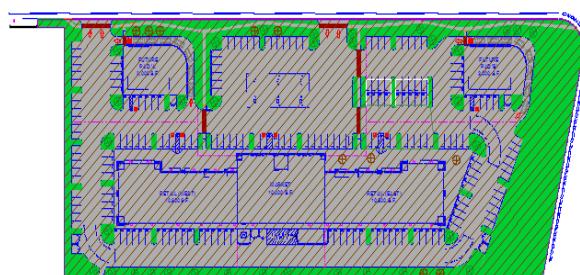
\*\* Doesn't include impervious areas within individual lots and surrounding individual units. That is accounted for below using Form D-1a in Step 2.

Area with Runoff Reduction Potential A - A<sub>PSOS</sub> =  acres A<sub>T</sub>

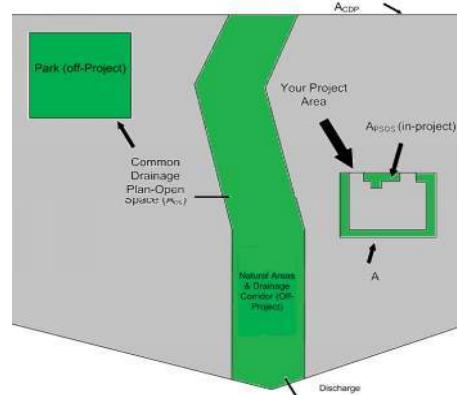
Assumed Initial Impervious Fraction A<sub>T</sub> / A =  I

#### Open Space & Pervious Area LID Credit (Step 1)

(A<sub>OS</sub>/A<sub>CDP</sub>+A<sub>PSOS</sub>/A)×100 =  pts



A - Drainage Shed Area  
 A<sub>PSOS</sub> Open Space and Landscaping  
 A<sub>T</sub> - Area with Runoff Reduction Potential



### Step 2 - Runoff Reduction Credits

| Runoff Reduction Treatments  | Impervious Area Managed             | Efficiency Factor                        | Effective Area Managed (A <sub>C</sub> )   |
|--|-------------------------------------|--|--|
| <b>Porous Pavement:</b>  |                                     |  |  |
| Option 1: Porous Pavement<br>(see Fact Sheet, excludes porous pavement used in Option 2)       | <input type="text"/>                | x <input type="text"/>                   | = <input type="text" value="0.000"/> acres |
| Option 2: Disconnected Pavement<br>(see Fact Sheet, excludes porous pavement used in Option 1) | <input type="text" value="0.0000"/> | use Form D-2a for credits →              | <input type="text" value="0.21"/> acres    |
| Landscaping used to Disconnect Pavement<br>(see Fact Sheet)                                    | <input type="text" value="0.0000"/> | =  | <input type="text" value="0.00"/> acres    |
| Disconnected Roof Drains<br>(see Fact Sheet and/or Table D-2b for summary of requirements)     | <input type="text" value="0"/>      | =  | <input type="text" value="0.00"/> acres    |
| Ecoroof<br>(see Fact Sheet)  | <input type="text" value="0"/>      | =  | <input type="text" value="0.00"/> acres    |
| Interceptor Trees<br>(see Fact Sheet)  | <input type="text"/>                | use Form D-2b for credits →              | <input type="text" value="0.00"/> acres    |
| Total Effective Area Managed by Runoff Reduction Measures                                      |                                     | A <sub>C</sub>                           | <input type="text" value="0.21"/> acres    |
| Runoff Reduction Credit (Step 2)   |                                     | (A <sub>C</sub> / A <sub>T</sub> )×100 = | <input type="text" value="42"/> pts        |

**Table D-2a**

| Porous Pavement Type       | Efficiency Multiplier |
|----------------------------|-----------------------|
| Cobblestone Block Pavement | 0.40                  |
| Pervious Concrete/Asphalt  | 0.60                  |
| Modular Block Pavement &   | 0.75                  |
| Reinforced Grass Pavement  | 1.00                  |

**Table D-2b**

| Maximum roof size | Minimum travel distance |
|-------------------|-------------------------|
| ≤ 3,500 sq ft     | 21 ft                   |
| ≤ 5,000 sq ft     | 24 ft                   |
| ≤ 7,500 sq ft     | 28 ft                   |
| ≤ 10,000 sq ft    | 32 ft                   |

**Form D-2a: Disconnected Pavement Worksheet**

See Fact Sheet for more information regarding Disconnected Pavement credit guidelines

Effective Area Managed (A<sub>c</sub>)**Pavement Draining to Porous Pavement**

2. Enter area draining onto Porous Pavement

0.20

acres Box K1

3. Enter area of Receiving Porous Pavement  
(excludes area entered in Step 2 under Porous Pavement)

0.29

acres Box K2

4. Ratio of Areas (Box K1 / Box K2)

0.69

Box K3

5. Select multiplier using ratio from Box K3 and enter into Box K4

| Ratio (Box D)            | Multiplier |
|--------------------------|------------|
| Ratio is ≤ 0.5           | 1.00       |
| Ratio is > 0.5 and < 1.0 | 0.83       |
| Ratio is > 1.0 and < 1.5 | 0.71       |
| Ratio is > 1.5 and < 2.0 | 0.55       |

0.83

Box K4

6. Enter Efficiency of Porous Pavement (see table below)

0.75

Box K5

| Porous Pavement Type               | Efficiency Multiplier |
|------------------------------------|-----------------------|
| Cobblestone Block Pavement         | 0.40                  |
| Pervious Concrete Asphalt Pavement | 0.60                  |
| Modular Block Pavement             | 0.75                  |
| Porous Gravel Pavement             | 1.00                  |
| Reinforced Grass Pavement          | 1.00                  |

7. Multiply Box K2 by Box K5 and enter into Box K6

0.22

acres Box K6

8. Multiply Boxes K1,K4, and K5 and enter the result in Box K7

0.12

acres Box K7

9. Add Box K6 to Box K7 and multiply by 60%, and enter the Result in Box K8  
This is the amount of area credit to enter into the "Disconnected Pavement" Box of Form D-2

0.21 acres

**Form D-2b: Interceptor Tree Worksheet**

See Fact Sheet for more information regarding Interceptor Tree credit guidelines

**New Evergreen Trees**

1. Enter number of new evergreen trees that qualify as Interceptor Trees in Box L1.

trees

Box L1

2. Multiply Box L1 by 200 and enter result in Box L2

0 sq. ft.

Box L2

**New Deciduous Trees**

3. Enter number of new deciduous trees that qualify as Interceptor Trees in Box L3.

trees

Box L3

4. Multiply Box L3 by 100 and enter result in Box L4

0 sq. ft.

Box L4

**Existing Tree Canopy**

5. Enter square footage of existing tree canopy that qualifies as Existing Tree canopy in Box L5.

950 sq. ft.

Box L5

6. Multiply Box L5 by 0.5 and enter the result in Box L6

475 sq. ft.

Box L6

**Total Interceptor Tree EAM Credits**

Add Boxes L2, L4, and L6 and enter it into Box L7

475 sq. ft.

Box L7

Divide Box L7 by 43,560 and multiply by 20% to get effective area managed and enter result in Box L8

0.00 acres

Box L8

This is the amount of area credit to enter into the "Interceptor Trees" Box of Form D-2

### Step 3 - Runoff Management Credits

#### Capture and Use Credits

##### Impervious Area Managed by Rain barrels, Cisterns, and automaticallyemptied systems

(see Fact Sheet) \_\_\_\_\_ enter gallons, for simple rain barrels

acres

##### Automated-Control Capture and Use System

(see Fact Sheet, then enter impervious area managed by the system)

acres

#### Bioretention/Infiltration Credits

##### Impervious Area Managed by Bioretention BMPs

(see Fact Sheet)

Bioretention Area \_\_\_\_\_ sq ft

Subdrain Elevation \_\_\_\_\_ inches

Ponding Depth, inches \_\_\_\_\_ inches

acres

##### Impervious Area Managed by Infiltration BMPs

(see Fact Sheet)

Drawdown Time, hrs \_\_\_\_\_ drawdown\_hrs\_inf

Soil Infiltration Rate, in/hr \_\_\_\_\_ soil\_inf\_rate

Sizing Option 1: Capture Volume, acre-ft \_\_\_\_\_ 0.00 capture\_vol\_inf

acres

Sizing Option 2: Infiltration BMP surface area, sq ft \_\_\_\_\_ 0 soil\_surface\_area

acres

Basin or trench? \_\_\_\_\_ approximate BMP depth  ft

##### Impervious Area Managed by Amended Soil or Mulch Beds

(see Fact Sheet)

Mulched Infiltration Area, sq ft \_\_\_\_\_ mulch\_area

acres

#### Total Effective Area Managed by Capture-and-Use/Bioretention/Infiltration BMPs

A\_LIDC

#### Runoff Management Credit (Step 3)

A\_LIDC/A\_T \* 200 =  pts

### Total LID Credits (Step 1+2+3)

Warning: More LID Is Required 56.4

Does project require hydromodification management? If yes, proceed to using SacHM.

Adjusted Area for Flow-Based, Non-LID Treatment

A\_T - A\_C - A\_LIDC =  A\_AT

Adjusted Impervious Fraction of A for Volume-Based, Non-LID Treatment

A\_AT / A =  I\_A

**Further treatment is required, see choose flow-based or volume-based sizing in Step 4**

### Step 4a Treatment - Flow-Based (Rational Method)

Calculate treatment flow (cfs):

Flow = Runoff Coefficient x Rainfall Intensity x Area

Look up value for i in Table D-2c (Rainfall Intensity)

i

Table D-2c

| Rainfall Intensity |     |            |
|--------------------|-----|------------|
| Roseville          | i = | 0.20 in/hr |
| Sacramento         | i = | 0.18 in/hr |
| Folsom             | i = | 0.20 in/hr |

Obtain A\_AT from Step 3

A\_AT

Use C = 0.95

C

Flow = 0.95 \* i \* A\_AT

cfs

### Step 4b Treatment - Volume-Based (ASCE-WEF)

Calculate water quality volume (Acre-Feet):

WQV = Area x Maximized Detention Volume ( $P_0$ )

Obtain A from Step 1

A

hrs

Specified Draw Down time

Obtain  $P_0$ : Maximized Detention Volume from figures E-1 to E-4 in Appendix E of this manual using  $I_A$  from Step 2.

$P_0$

Calculate treatment volume (acre-ft):

Treatment volume = A x ( $P_0$  / 12)

Acre-Feet

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## Appendix D-2: Commercial Sites: Low Impact Development (LID) Credits and Treatment BMP Sizing Calculations

Name of Drainage Shed: DMA 6  
Location of project: Sacramento

Fill in Blue Highlighted boxes

### Step 1 - Open Space and Pervious Area Credits

Is your project within the drainage area of a common drainage plan that includes open space? If not, skip to 1 b.

**1 a. Common Drainage Plan Area**

#### Common Drainage Plan Open Space (Off-project)

- a. Natural storage reservoirs and drainage corridors
- b. Buffer zones for natural water bodies
- c. Natural areas including existing trees, other vegetation, and soil
- d. Common landscape area/park
- e. Regional Flood Control/Drainage basins

|   |       |
|---|-------|
| 0 | acres |

A<sub>CDP</sub>

see area example below

**1 b. Project Drainage Shed Area (Total)**

|      |       |
|------|-------|
| 0.08 | acres |
|------|-------|

A

#### Project-Specific Open Space (In-project, communal\*\*)

- a. Natural storage reservoirs and drainage corridors
- b. Buffer zones for natural water bodies
- c. Natural areas including existing trees, other vegetation, and soil
- d. Landscape area/park
- e. Flood Control/Drainage basins

|      |       |
|------|-------|
| 0.02 | acres |
| 0.00 | acres |
| 0.00 | acres |
| 0.00 | acres |
| 0.02 | acres |
| 0.00 | acres |

A<sub>PSOS</sub>

see area example below

\*\* Doesn't include impervious areas within individual lots and surrounding individual units. That is accounted for below using Form D-1a in Step 2.

**Area with Runoff Reduction Potential**

A - A<sub>PSOS</sub> = 

|      |       |
|------|-------|
| 0.06 | acres |
|------|-------|

A<sub>T</sub>

**Assumed Initial Impervious Fraction**

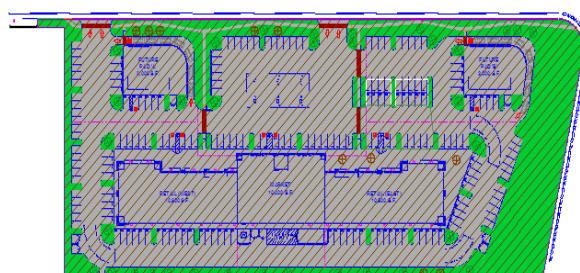
A<sub>T</sub> / A = 

|      |
|------|
| 0.75 |
|------|

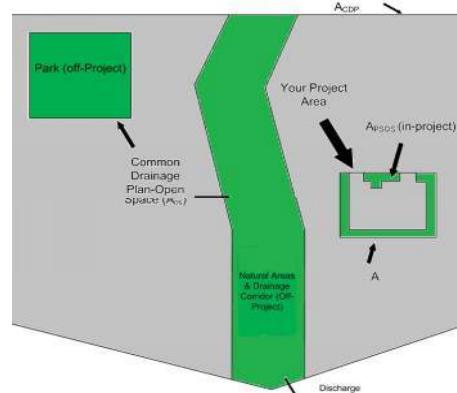
I

#### Open Space & Pervious Area LID Credit (Step 1)

$$(A_{OS}/A_{CDP}+A_{PSOS}/A)\times 100 = \boxed{25 \text{ pts}}$$



**A – Drainage Shed Area**  
**A<sub>POS</sub> Open Space and Landscaping**  
**A<sub>T</sub> – Area with Runoff Reduction Potential**



### Step 2 - Runoff Reduction Credits

| Runoff Reduction Treatments   | Impervious Area Managed                                  | Efficiency Factor | Effective Area Managed (A <sub>C</sub> )               |  |   |       |
|---|--|-------------------|--|--|---|-------|
| <b>Porous Pavement:</b>   |  |                   |  |  |   |       |
| <b>Option 1: Porous Pavement</b><br>(see Fact Sheet, excludes porous pavement used in Option 2)       | <table border="1"><tr><td></td></tr></table> acres       |                   | x <table border="1"><tr><td></td></tr></table>         |  | = <table border="1"><tr><td>0.000</td></tr></table> acres | 0.000 |
|   |  |                   |  |  |   |       |
|   |  |                   |  |  |   |       |
| 0.000   |  |                   |  |  |   |       |
| <b>Option 2: Disconnected Pavement</b><br>(see Fact Sheet, excludes porous pavement used in Option 1) | <table border="1"><tr><td></td></tr></table> acres       |                   | use Form D-2a for credits →                            | <table border="1"><tr><td>0.02</td></tr></table> acres | 0.02  |       |
|   |  |                   |  |  |   |       |
| 0.02  |  |                   |  |  |   |       |
| <b>Landscaping used to Disconnect Pavement</b><br>(see Fact Sheet)                                    | <table border="1"><tr><td>0.0000</td></tr></table> acres | 0.0000            | =  | <table border="1"><tr><td>0.00</td></tr></table> acres | 0.00  |       |
| 0.0000  |  |                   |  |  |   |       |
| 0.00  |  |                   |  |  |   |       |
| <b>Disconnected Roof Drains</b><br>(see Fact Sheet and/or Table D-2b for summary of requirements)     | <table border="1"><tr><td>0</td></tr></table> acres      | 0                 | =  | <table border="1"><tr><td>0.00</td></tr></table> acres | 0.00  |       |
| 0   |  |                   |  |  |   |       |
| 0.00  |  |                   |  |  |   |       |
| <b>Ecoroof</b><br>(see Fact Sheet)  | <table border="1"><tr><td>0</td></tr></table> acres      | 0                 | =  | <table border="1"><tr><td>0.00</td></tr></table> acres | 0.00  |       |
| 0   |  |                   |  |  |   |       |
| 0.00  |  |                   |  |  |   |       |
| <b>Interceptor Trees</b><br>(see Fact Sheet)  | <table border="1"><tr><td></td></tr></table> acres       |                   | use Form D-2b for credits →                            | <table border="1"><tr><td>0.00</td></tr></table> acres | 0.00  |       |
|   |  |                   |  |  |   |       |
| 0.00  |  |                   |  |  |   |       |
| <b>Total Effective Area Managed by Runoff Reduction Measures</b>                                      |  | A <sub>C</sub>    | <table border="1"><tr><td>0.02</td></tr></table> acres | 0.02   |   |       |
| 0.02  |  |                   |  |  |   |       |
| <b>Runoff Reduction Credit (Step 2)</b>   |  |                   | $(A_C / A_T) \times 100 = \boxed{41 \text{ pts}}$      |  |   |       |

**Table D-2a**

| Porous Pavement Type       | Efficiency Multiplier |
|----------------------------|-----------------------|
| Cobblestone Block Pavement | 0.40                  |
| Pervious Concrete/Asphalt  | 0.60                  |
| Modular Block Pavement &   | 0.75                  |
| Reinforced Grass Pavement  | 1.00                  |

**Table D-2b**

| Maximum roof size | Minimum travel distance |
|-------------------|-------------------------|
| ≤ 3,500 sq ft     | 21 ft                   |
| ≤ 5,000 sq ft     | 24 ft                   |
| ≤ 7,500 sq ft     | 28 ft                   |
| ≤ 10,000 sq ft    | 32 ft                   |

**Form D-2a: Disconnected Pavement Worksheet**

See Fact Sheet for more information regarding Disconnected Pavement credit guidelines

Effective Area Managed (A<sub>c</sub>)**Pavement Draining to Porous Pavement**

2. Enter area draining onto Porous Pavement

0.03

acres Box K1

3. Enter area of Receiving Porous Pavement  
(excludes area entered in Step 2 under Porous Pavement)

0.03

acres Box K2

4. Ratio of Areas (Box K1 / Box K2)

1.00

Box K3

5. Select multiplier using ratio from Box K3 and enter into Box K4

| Ratio (Box D)            | Multiplier |
|--------------------------|------------|
| Ratio is ≤ 0.5           | 1.00       |
| Ratio is > 0.5 and < 1.0 | 0.83       |
| Ratio is > 1.0 and < 1.5 | 0.71       |
| Ratio is > 1.5 and < 2.0 | 0.55       |

0.83

Box K4

6. Enter Efficiency of Porous Pavement (see table below)

0.75

Box K5

| Porous Pavement Type               | Efficiency Multiplier |
|------------------------------------|-----------------------|
| Cobblestone Block Pavement         | 0.40                  |
| Pervious Concrete Asphalt Pavement | 0.60                  |
| Modular Block Pavement             | 0.75                  |
| Porous Gravel Pavement             | 1.00                  |
| Reinforced Grass Pavement          | 1.00                  |

7. Multiply Box K2 by Box K5 and enter into Box K6

0.02

acres Box K6

8. Multiply Boxes K1,K4, and K5 and enter the result in Box K7

0.02

acres Box K7

9. Add Box K6 to Box K7 and multiply by 60%, and enter the Result in Box K8  
This is the amount of area credit to enter into the "Disconnected Pavement" Box of Form D-2

0.02 acres

**Form D-2b: Interceptor Tree Worksheet**

See Fact Sheet for more information regarding Interceptor Tree credit guidelines

**New Evergreen Trees**

1. Enter number of new evergreen trees that qualify as Interceptor Trees in Box L1.

trees

Box L1

2. Multiply Box L1 by 200 and enter result in Box L2

0 sq. ft.

Box L2

**New Deciduous Trees**

3. Enter number of new deciduous trees that qualify as Interceptor Trees in Box L3.

trees

Box L3

4. Multiply Box L3 by 100 and enter result in Box L4

0 sq. ft.

Box L4

**Existing Tree Canopy**

5. Enter square footage of existing tree canopy that qualifies as Existing Tree canopy in Box L5.

sq. ft.

Box L5

6. Multiply Box L5 by 0.5 and enter the result in Box L6

0 sq. ft.

Box L6

**Total Interceptor Tree EAM Credits**

Add Boxes L2, L4, and L6 and enter it into Box L7

0 sq. ft.

Box L7

Divide Box L7 by 43,560 and multiply by 20% to get effective area managed and enter result in Box L8

0.00 acres

Box L8

This is the amount of area credit to enter into the "Interceptor Trees" Box of Form D-2

### Step 3 - Runoff Management Credits

#### Capture and Use Credits

##### Impervious Area Managed by Rain barrels, Cisterns, and automaticallyemptied systems

(see Fact Sheet) \_\_\_\_\_ enter gallons, for simple rain barrels

acres

##### Automated-Control Capture and Use System

(see Fact Sheet, then enter impervious area managed by the system)

acres

#### Bioretention/Infiltration Credits

##### Impervious Area Managed by Bioretention BMPs

(see Fact Sheet)

Bioretention Area \_\_\_\_\_ sq ft

Subdrain Elevation \_\_\_\_\_ inches

Ponding Depth, inches \_\_\_\_\_ inches

acres

##### Impervious Area Managed by Infiltration BMPs

(see Fact Sheet)

Drawdown Time, hrs \_\_\_\_\_ drawdown\_hrs\_inf

Soil Infiltration Rate, in/hr \_\_\_\_\_ soil\_inf\_rate

Sizing Option 1: Capture Volume, acre-ft \_\_\_\_\_ 0.00 capture\_vol\_inf

acres

Sizing Option 2: Infiltration BMP surface area, sq ft \_\_\_\_\_ 0 soil\_surface\_area

acres

Basin or trench? \_\_\_\_\_ approximate BMP depth  ft

##### Impervious Area Managed by Amended Soil or Mulch Beds

(see Fact Sheet)

Mulched Infiltration Area, sq ft \_\_\_\_\_ mulch\_area

acres

#### Total Effective Area Managed by Capture-and-Use/Bioretention/Infiltration BMPs

A\_LIDC

#### Runoff Management Credit (Step 3)

A\_LIDC/A\_T \* 200 =  pts

### Total LID Credits (Step 1+2+3)

Warning: More LID Is Required 66.2

Does project require hydromodification management? If yes, proceed to using SacHM.

Adjusted Area for Flow-Based, Non-LID Treatment

A\_T - A\_C - A\_LIDC =  A\_AT

Adjusted Impervious Fraction of A for Volume-Based, Non-LID Treatment

A\_AT / A =  I\_A

**Further treatment is required, see choose flow-based or volume-based sizing in Step 4**

### Step 4a Treatment - Flow-Based (Rational Method)

Calculate treatment flow (cfs):

Flow = Runoff Coefficient x Rainfall Intensity x Area

Look up value for i in Table D-2c (Rainfall Intensity)

i

Table D-2c

| Rainfall Intensity |     |            |
|--------------------|-----|------------|
| Roseville          | i = | 0.20 in/hr |
| Sacramento         | i = | 0.18 in/hr |
| Folsom             | i = | 0.20 in/hr |

Obtain A\_AT from Step 3

A\_AT

Use C = 0.95

C

Flow = 0.95 \* i \* A\_AT

cfs

### Step 4b Treatment - Volume-Based (ASCE-WEF)

Calculate water quality volume (Acre-Feet):

WQV = Area x Maximized Detention Volume ( $P_0$ )

Obtain A from Step 1

A

hrs

Specified Draw Down time

Obtain  $P_0$ : Maximized Detention Volume from figures E-1 to E-4 in Appendix E of this manual using  $I_A$  from Step 2.

$P_0$

Calculate treatment volume (acre-ft):

Treatment volume = A x ( $P_0$  / 12)

Acre-Feet

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## Appendix D-2: Commercial Sites: Low Impact Development (LID) Credits and Treatment BMP Sizing Calculations

Name of Drainage Shed: DMA 7  
Location of project: Sacramento

Fill in Blue Highlighted boxes

### Step 1 - Open Space and Pervious Area Credits

Is your project within the drainage area of a common drainage plan that includes open space? If not, skip to 1 b.

**1 a. Common Drainage Plan Area**

#### Common Drainage Plan Open Space (Off-project)

- a. Natural storage reservoirs and drainage corridors
- b. Buffer zones for natural water bodies
- c. Natural areas including existing trees, other vegetation, and soil
- d. Common landscape area/park
- e. Regional Flood Control/Drainage basins

|   |       |
|---|-------|
| 0 | acres |

A<sub>CDP</sub>

see area example below

**1 b. Project Drainage Shed Area (Total)**

|      |       |
|------|-------|
| 2.85 | acres |
| 0.99 | acres |
| 0.00 | acres |
| 0.00 | acres |
| 0.00 | acres |
| 0.99 | acres |
| 0.00 | acres |

A

#### Project-Specific Open Space (In-project, communal\*\*)

- a. Natural storage reservoirs and drainage corridors
- b. Buffer zones for natural water bodies
- c. Natural areas including existing trees, other vegetation, and soil
- d. Landscape area/park
- e. Flood Control/Drainage basins

|      |       |
|------|-------|
| 0.99 | acres |
| 0.00 | acres |
| 0.00 | acres |
| 0.00 | acres |
| 0.99 | acres |
| 0.00 | acres |

A<sub>PSOS</sub>

see area example below

\*\* Doesn't include impervious areas within individual lots and surrounding individual units. That is accounted for below using Form D-1a in Step 2.

**Area with Runoff Reduction Potential**

A - A<sub>PSOS</sub> = 1.86 acres

A<sub>T</sub>

**Assumed Initial Impervious Fraction**

A<sub>T</sub> / A = 0.65

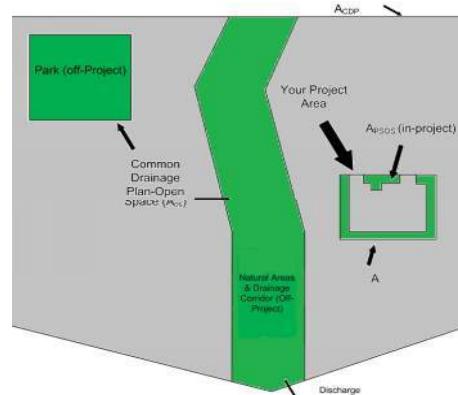
I

#### Open Space & Pervious Area LID Credit (Step 1)

(A<sub>OS</sub>/A<sub>CDP</sub>+A<sub>PSOS</sub>/A)×100 = 35 pts



|   |
|---|
| A - Drainage Shed Area                                |
| A <sub>PSOS</sub> Open Space and Landscaping          |
| A <sub>T</sub> - Area with Runoff Reduction Potential |



### Step 2 - Runoff Reduction Credits

| Runoff Reduction Treatments   | Impervious Area Managed   | Efficiency Factor | Effective Area Managed (A <sub>C</sub> )            |
|---|---------------------------|-------------------|---|
| <b>Porous Pavement:</b>   |                           |                   |   |
| <b>Option 1: Porous Pavement</b><br>(see Fact Sheet, excludes porous pavement used in Option 2)       |                           | acres             | x      =      0.000      acres                      |
| <b>Option 2: Disconnected Pavement</b><br>(see Fact Sheet, excludes porous pavement used in Option 1) | use Form D-2a for credits |                   | →      0.00      acres                              |
| <b>Landscaping used to Disconnect Pavement</b><br>(see Fact Sheet)                                    | 0.0000                    | acres             | =      0.00      acres                              |
| <b>Disconnected Roof Drains</b><br>(see Fact Sheet and/or Table D-2b for summary of requirements)     | 0                         | acres             | =      0.00      acres                              |
| <b>Ecoroof</b><br>(see Fact Sheet)  | 0                         | acres             | =      0.00      acres                              |
| <b>Interceptor Trees</b><br>(see Fact Sheet)  | use Form D-2b for credits |                   | →      0.00      acres                              |
| <b>Total Effective Area Managed by Runoff Reduction Measures</b>                                      |                           | A <sub>C</sub>    | 0.00      acres                                     |
| <b>Runoff Reduction Credit (Step 2)</b>   |                           |                   | (A <sub>C</sub> / A <sub>T</sub> )×100 = 0      pts |

**Table D-2a**

| Porous Pavement Type       | Efficiency Multiplier |
|----------------------------|-----------------------|
| Cobblestone Block Pavement | 0.40                  |
| Pervious Concrete/Asphalt  | 0.60                  |
| Modular Block Pavement &   | 0.75                  |
| Reinforced Grass Pavement  | 1.00                  |

**Table D-2b**

| Maximum roof size | Minimum travel distance |
|-------------------|-------------------------|
| ≤ 3,500 sq ft     | 21 ft                   |
| ≤ 5,000 sq ft     | 24 ft                   |
| ≤ 7,500 sq ft     | 28 ft                   |
| ≤ 10,000 sq ft    | 32 ft                   |

**Form D-2a: Disconnected Pavement Worksheet**

See Fact Sheet for more information regarding Disconnected Pavement credit guidelines

Effective Area Managed (A<sub>c</sub>)**Pavement Draining to Porous Pavement**

2. Enter area draining onto Porous Pavement

acres Box K1

3. Enter area of Receiving Porous Pavement  
(excludes area entered in Step 2 under Porous Pavement)

acres Box K2

4. Ratio of Areas (Box K1 / Box K2)

0.00

Box K3

5. Select multiplier using ratio from Box K3 and enter into Box K4

| Ratio (Box D)            | Multiplier |
|--------------------------|------------|
| Ratio is ≤ 0.5           | 1.00       |
| Ratio is > 0.5 and < 1.0 | 0.83       |
| Ratio is > 1.0 and < 1.5 | 0.71       |
| Ratio is > 1.5 and < 2.0 | 0.55       |

1

Box K4

6. Enter Efficiency of Porous Pavement (see table below)

| Porous Pavement Type               | Efficiency Multiplier |
|------------------------------------|-----------------------|
| Cobblestone Block Pavement         | 0.40                  |
| Pervious Concrete Asphalt Pavement | 0.60                  |
| Modular Block Pavement             | 0.75                  |
| Porous Gravel Pavement             | 1.00                  |
| Reinforced Grass Pavement          | 1.00                  |

Box K5

7. Multiply Box K2 by Box K5 and enter into Box K6

0.00

acres Box K6

8. Multiply Boxes K1,K4, and K5 and enter the result in Box K7

0.00

acres Box K7

9. Add Box K6 to Box K7 and multiply by 60%, and enter the Result in Box K8  
This is the amount of area credit to enter into the "Disconnected Pavement" Box of Form D-20.00 acres**Form D-2b: Interceptor Tree Worksheet**

See Fact Sheet for more information regarding Interceptor Tree credit guidelines

**New Evergreen Trees**

1. Enter number of new evergreen trees that qualify as Interceptor Trees in Box L1.

trees Box L1

2. Multiply Box L1 by 200 and enter result in Box L2

0

sq. ft. Box L2

**New Deciduous Trees**

3. Enter number of new deciduous trees that qualify as Interceptor Trees in Box L3.

trees Box L3

4. Multiply Box L3 by 100 and enter result in Box L4

0

sq. ft. Box L4

**Existing Tree Canopy**

5. Enter square footage of existing tree canopy that qualifies as Existing Tree canopy in Box L5.

sq. ft. Box L5

6. Multiply Box L5 by 0.5 and enter the result in Box L6

0

sq. ft. Box L6

**Total Interceptor Tree EAM Credits**

Add Boxes L2, L4, and L6 and enter it into Box L7

0

sq. ft. Box L7

Divide Box L7 by 43,560 and multiply by 20% to get effective area managed and enter result in Box L8

0.00

acres Box L8

This is the amount of area credit to enter into the "Interceptor Trees" Box of Form D-2

### Step 3 - Runoff Management Credits

#### Capture and Use Credits

##### Impervious Area Managed by Rain barrels, Cisterns, and automaticallyemptied systems

(see Fact Sheet) \_\_\_\_\_ enter gallons, for simple rain barrels

acres

##### Automated-Control Capture and Use System

(see Fact Sheet, then enter impervious area managed by the system)

acres

#### Bioretention/Infiltration Credits

##### Impervious Area Managed by Bioretention BMPs

(see Fact Sheet)

Bioretention Area  sq ft

Subdrain Elevation  inches

Ponding Depth, inches  inches

acres

##### Impervious Area Managed by Infiltration BMPs

(see Fact Sheet)

Drawdown Time, hrs

Soil Infiltration Rate, in/hr

Sizing Option 1: Capture Volume, acre-ft  capture\_vol\_inf

acres

Sizing Option 2: Infiltration BMP surface area, sq ft  soil\_surface\_area

acres

Basin or trench?  approximate BMP depth  ft

##### Impervious Area Managed by Amended Soil or Mulch Beds

(see Fact Sheet)

Mulched Infiltration Area, sq ft

acres

#### Total Effective Area Managed by Capture-and-Use/Bioretention/Infiltration BMPs

A<sub>LIDc</sub>

#### Runoff Management Credit (Step 3)

A<sub>LIDc</sub>/A<sub>T</sub>\*200 =  pts

### Total LID Credits (Step 1+2+3)

LID compliant, check for treatment sizing in Step 4

231.6

Does project require hydromodification management? If yes, proceed to using SacHM.

Adjusted Area for Flow-Based, Non-LID Treatment

A<sub>T</sub> - A<sub>C</sub> - A<sub>LIDc</sub> =  A<sub>AT</sub>

Adjusted Impervious Fraction of A for Volume-Based, Non-LID Treatment

A<sub>AT</sub> / A =  I<sub>A</sub>

### STOP: No additional treatment needed

#### Step 4a Treatment - Flow-Based (Rational Method)

Calculate treatment flow (cfs):

Flow = Runoff Coefficient x Rainfall Intensity x Area

Look up value for i in Table D-2c (Rainfall Intensity)

i

Table D-2c

| Rainfall Intensity |     |            |
|--------------------|-----|------------|
| Roseville          | i = | 0.20 in/hr |
| Sacramento         | i = | 0.18 in/hr |
| Folsom             | i = | 0.20 in/hr |

Obtain A<sub>AT</sub> from Step 3

A<sub>AT</sub>

Use C = 0.95

C

Flow = 0.95 \* i \* A<sub>AT</sub>

cfs

#### Step 4b Treatment - Volume-Based (ASCE-WEF)

Calculate water quality volume (Acre-Feet):

WQV = Area x Maximized Detention Volume (P<sub>0</sub>)

Obtain A from Step 1

A

hrs

Specified Draw Down time

Obtain P<sub>0</sub>: Maximized Detention Volume from figures E-1 to E-4 in Appendix E of this manual using I<sub>A</sub> from Step 2.

P<sub>0</sub>

Calculate treatment volume (acre-ft):

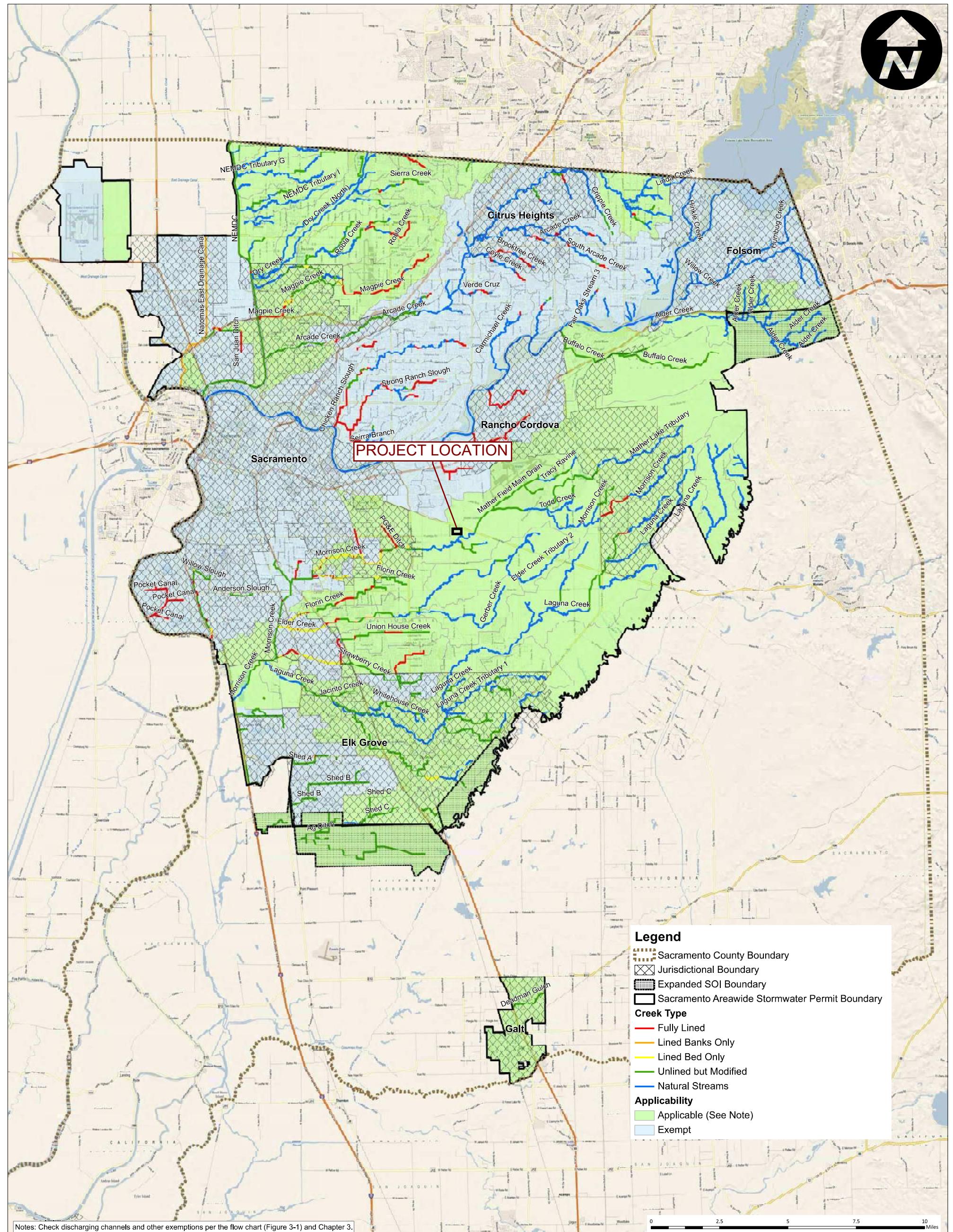
Treatment volume = A x (P<sub>0</sub> / 12)

Acre-Feet

v06232012

## **APPENDIX H:**

### **Hydromodification Map**

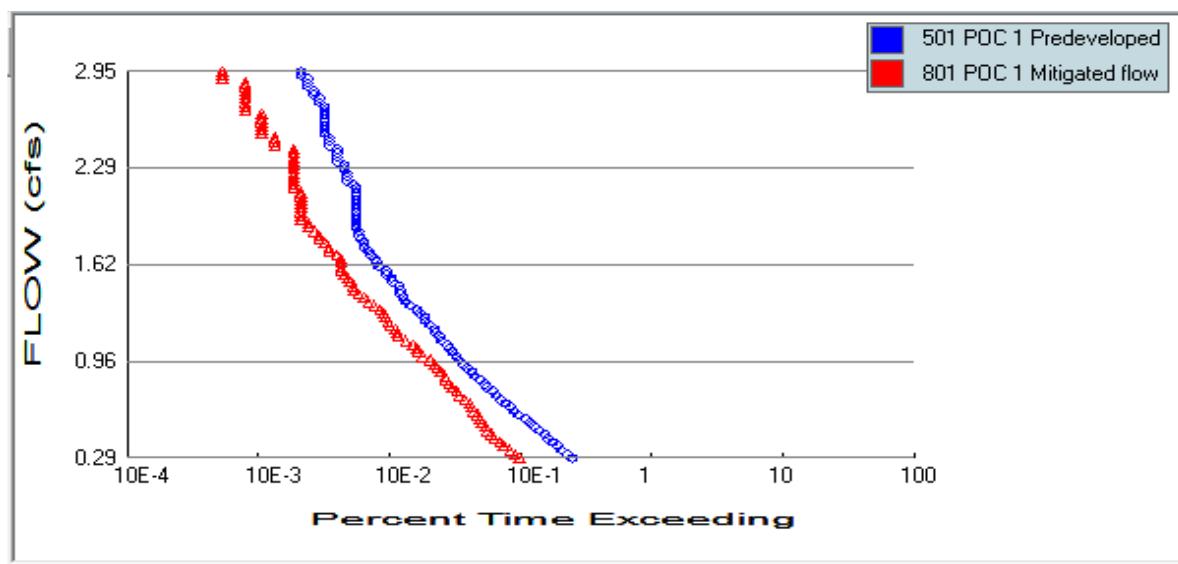


## **APPENDIX I:**

### **SAHM Project Report**

## SAHM Summary

| Development Condition | Shed   | Area (Ac) | Porous Gravel                                |   |                             | Bioretention Basin |            |           |                     |                  |                |                 |                  |                 |                         |                                 |                               |                    |                  |                            |
|-----------------------|--------|-----------|--|---|-----------------------------|--------------------|------------|-----------|---------------------|------------------|----------------|-----------------|------------------|-----------------|-------------------------|---------------------------------|-------------------------------|--------------------|------------------|----------------------------|
|                       |        |           | Pervious Area (HSG C, Grass Flat (0-1%)), ac | Pervious Area (HSG C, Grass Mod (1-2%)), ac | Impervious, Flat (0-1%), ac | Area, sf           | Length, ft | Width, ft | Bottom Slope, ft/ft | Gravel Depth, ft | Sand Depth, ft | Basin Width, ft | Basin Length, ft | Bottom Area, sf | Underdrain Diameter, ft | Underdrain Orifice Diameter, in | Underdrain Orifice Offset, in | Riser Diameter, in | Riser Height, ft | Riser Orifice Diameter, in |
| Pre-Project           | ExShed | 7.10      | 6.96   | -   | 0.14                        | -                  | -          | -         | -                   | -                | -              | -               | -                | -               | -                       | -                               | -                             | -                  | -                | -                          |
| Mitigated             | DMA 1  | 0.76      | -  | 0.09  | 0.29                        | 16335              | 180.00     | 90.75     | 0.01                | 1.00             | 0.58           | -               | -                | -               | -                       | -                               | -                             | -                  | -                | -                          |
|                       | DMA 2  | 0.88      | -  | 0.03  | 0.45                        | 17433              | 440.24     | 39.60     | 0.01                | 1.00             | 0.58           | -               | -                | -               | -                       | -                               | -                             | -                  | -                | -                          |
|                       | DMA 3  | 1.31      | -  | 0.02  | 0.50                        | 34713              | 467.33     | 74.28     | 0.01                | 1.00             | 0.58           | -               | -                | -               | -                       | -                               | -                             | -                  | -                | -                          |
|                       | DMA 4  | 0.65      | -  | 0.00  | 0.25                        | 17135              | 540.53     | 31.70     | 0.01                | 1.00             | 0.58           | -               | -                | -               | -                       | -                               | -                             | -                  | -                | -                          |
|                       | DMA 5  | 0.57      | -  | 0.08  | 0.20                        | 12759              | 321.87     | 39.64     | 0.01                | 1.00             | 0.58           | -               | -                | -               | -                       | -                               | -                             | -                  | -                | -                          |
|                       | DMA 6  | 0.08      | -  | 0.02  | 0.03                        | 1156               | 38.37      | 30.14     | 0.01                | 1.00             | 0.58           | -               | -                | -               | -                       | -                               | -                             | -                  | -                | -                          |
|                       | DMA 7  | 2.85      | -  | 1.11  | 1.74                        | -                  | -          | -         | -                   | -                | -              | 8.00            | 660              | 5324            | 0.33                    | 3.25                            | 5.0                           | 36.0               | 1.00             | 6.0                        |



**SAHM**

**PROJECT REPORT**

## *General Model Information*

Project Name: Bradshaw & Jackson

Site Name:

Site Address:

City:

Report Date: 3/27/2024

Gage: RANCHO C

Data Start: 1961/10/01

Data End: 2004/09/30

Timestep: Hourly

Precip Scale: 0.944

Version Date: 2021/03/09

## *POC Thresholds*

---

Low Flow Threshold for POC1: 25 Percent of the 2 Year

High Flow Threshold for POC1: 10 Year

---

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## *Landuse Basin Data*

### *Pre-Project Land Use*

#### **Basin 1**

|  |              |
|--|--------------|
| Bypass:                                  | No           |
| GroundWater:                             | No           |
| Pervious Land Use<br>D,Grass,Flat(0-1%)  | acre<br>6.96 |
| Pervious Total                           | 6.96         |
| Impervious Land Use<br>Imperv,Flat(0-1%) | acre<br>0.14 |
| Impervious Total                         | 0.14         |
| Basin Total                              | 7.1          |

Element Flows To:  
Surface

Interflow

Groundwater

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## *Mitigated Land Use*

### DMA 7 Basin

|  |              |
|--|--------------|
| Bypass:                                  | No           |
| GroundWater:                             | No           |
| Pervious Land Use<br>C,Grass,Mod (1-2%)  | acre<br>1.66 |
| Pervious Total                           | 1.66         |
| Impervious Land Use<br>Imperv,Flat(0-1%) | acre<br>1.19 |
| Impervious Total                         | 1.19         |
| Basin Total                              | 2.85         |

### Element Flows To:

|                      |                      |             |
|----------------------|----------------------|-------------|
| Surface              | Interflow            | Groundwater |
| Surface Bioretention | Surface Bioretention |             |

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## DMA 1 Lateral Basin

Bypass: No

GroundWater: No

Pervious Land Use acre  
C, Grass, Mod (1-2%) .09

Element Flows To:

| Surface               | Interflow             | Groundwater |
|-----------------------|-----------------------|-------------|
| DMA 1 Porous Pavement | DMA 1 Porous Pavement |             |

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## DMA 1 Lateral I Basin

Bypass: No  
Impervious Land Use acre  
Imperv,Flat(0-1%) 0.29  
Element Flows To:  
Outlet 1 Outlet 2  
DMA 1 Porous Pavement

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## DMA 2 Lateral I Basin

Bypass: No  
Impervious Land Use acre  
Imperv,Flat(0-1%) 0.45  
Element Flows To:  
Outlet 1                  Outlet 2  
DMA 2 Porous Pavement

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## DMA 2 Lateral Basin

Bypass: No

GroundWater: No

Pervious Land Use acre  
C, Grass, Mod (1-2%) .03

Element Flows To:

| Surface               | Interflow             | Groundwater |
|-----------------------|-----------------------|-------------|
| DMA 2 Porous Pavement | DMA 2 Porous Pavement |             |

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## DMA 3 Lateral I Basin

Bypass: No  
Impervious Land Use acre  
Imperv,Flat(0-1%) 0.5  
Element Flows To:  
Outlet 1                  Outlet 2  
DMA 3 Porous Pavement

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## DMA 3 Lateral Basin

Bypass: No

GroundWater: No

Pervious Land Use acre  
C,Grass,Mod (1-2%) .02

Element Flows To:

| Surface               | Interflow             | Groundwater |
|-----------------------|-----------------------|-------------|
| DMA 3 Porous Pavement | DMA 3 Porous Pavement |             |

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## DMA 4 Lateral I Basin

Bypass: No  
Impervious Land Use acre  
Imperv,Flat(0-1%) 0.25  
Element Flows To:  
Outlet 1                  Outlet 2  
DMA 4 Porous Pavement

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## DMA 5 Lateral I Basin

Bypass: No  
Impervious Land Use acre  
Imperv,Flat(0-1%) 0.2  
Element Flows To:  
Outlet 1 Outlet 2  
DMA 5 Porous Pavement

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## DMA 5 Lateral Basin

Bypass: No

GroundWater: No

Pervious Land Use acre  
C, Grass, Mod (1-2%) .08

Element Flows To:

| Surface               | Interflow             | Groundwater |
|-----------------------|-----------------------|-------------|
| DMA 5 Porous Pavement | DMA 5 Porous Pavement |             |

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## DMA 6 Lateral I Basin

Bypass: No  
Impervious Land Use acre  
Imperv,Flat(0-1%) 0.03  
Element Flows To:  
Outlet 1 Outlet 2  
DMA 6 Porous Pavement

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## DMA 6 Lateral Basin

Bypass: No

GroundWater: No

Pervious Land Use acre  
C, Grass, Mod (1-2%) .02

Element Flows To:

| Surface               | Interflow             | Groundwater |
|-----------------------|-----------------------|-------------|
| DMA 6 Porous Pavement | DMA 6 Porous Pavement |             |

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# *Routing Elements*

## *Pre-Project Routing*

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## Mitigated Routing

### Bioretention Bioretention

|                                     |                 |
|-------------------------------------|-----------------|
| Bottom Length:                      | 660.00 ft.      |
| Bottom Width:                       | 8.00 ft.        |
| Material thickness of first layer:  | 0.5             |
| Material type for first layer:      | Sandy loam      |
| Material thickness of second layer: | 1.5             |
| Material type for second layer:     | Amended 5 in/hr |
| Material thickness of third layer:  | 0.75            |
| Material type for third layer:      | GRAVEL          |
| Underdrain used                     |                 |
| Underdrain Diameter (feet):         | 0.33            |
| Orifice Diameter (in.):             | 3.25            |
| Offset (in.):                       | 5               |
| Flow Through Underdrain (ac-ft.):   | 292.7           |
| Total Outflow (ac-ft.):             | 305.802         |
| Percent Through Underdrain:         | 95.72           |

### Discharge Structure

|                 |        |
|-----------------|--------|
| Riser Height:   | 1 ft.  |
| Riser Diameter: | 36 in. |

### Element Flows To:

Outlet 1                          Outlet 2

Landscape Swale Hydraulic Table

| Stage(feet) | Area(ac.) | Volume(ac-ft.) | Discharge(cfs) | Infilt(cfs) |
|-------------|-----------|----------------|----------------|-------------|
| 0.0000      | 0.3712    | 0.0000         | 0.0000         | 0.0000      |
| 0.0467      | 0.3675    | 0.0023         | 0.0000         | 0.0000      |
| 0.0934      | 0.3632    | 0.0047         | 0.0000         | 0.0000      |
| 0.1401      | 0.3590    | 0.0072         | 0.0000         | 0.0000      |
| 0.1868      | 0.3547    | 0.0097         | 0.0000         | 0.0000      |
| 0.2335      | 0.3505    | 0.0124         | 0.0000         | 0.0000      |
| 0.2802      | 0.3462    | 0.0151         | 0.0000         | 0.0000      |
| 0.3269      | 0.3420    | 0.0179         | 0.0000         | 0.0000      |
| 0.3736      | 0.3377    | 0.0208         | 0.0000         | 0.0000      |
| 0.4203      | 0.3335    | 0.0237         | 0.0000         | 0.0000      |
| 0.4670      | 0.3293    | 0.0267         | 0.0000         | 0.0000      |
| 0.5137      | 0.3250    | 0.0300         | 0.0000         | 0.0000      |
| 0.5604      | 0.3208    | 0.0333         | 0.0000         | 0.0000      |
| 0.6071      | 0.3165    | 0.0367         | 0.0000         | 0.0000      |
| 0.6538      | 0.3123    | 0.0403         | 0.0000         | 0.0000      |
| 0.7005      | 0.3080    | 0.0438         | 0.0000         | 0.0000      |
| 0.7473      | 0.3038    | 0.0475         | 0.0000         | 0.0000      |
| 0.7940      | 0.2995    | 0.0513         | 0.0000         | 0.0000      |
| 0.8407      | 0.2953    | 0.0551         | 0.0000         | 0.0000      |
| 0.8874      | 0.2910    | 0.0590         | 0.0000         | 0.0000      |
| 0.9341      | 0.2868    | 0.0630         | 0.0000         | 0.0000      |
| 0.9808      | 0.2826    | 0.0671         | 0.0000         | 0.0000      |
| 1.0275      | 0.2783    | 0.0713         | 0.0000         | 0.0000      |
| 1.0742      | 0.2741    | 0.0755         | 0.0000         | 0.0000      |
| 1.1209      | 0.2698    | 0.0799         | 0.0000         | 0.0000      |
| 1.1676      | 0.2656    | 0.0843         | 0.0000         | 0.0000      |
| 1.2143      | 0.2613    | 0.0888         | 0.0000         | 0.0000      |
| 1.2610      | 0.2571    | 0.0934         | 0.0000         | 0.0000      |
| 1.3077      | 0.2528    | 0.0980         | 0.0000         | 0.0000      |

|        |        |        |        |        |
|--------|--------|--------|--------|--------|
| 1.3544 | 0.2486 | 0.1028 | 0.0000 | 0.0000 |
| 1.4011 | 0.2443 | 0.1076 | 0.0000 | 0.0000 |
| 1.4478 | 0.2401 | 0.1125 | 0.0000 | 0.0000 |
| 1.4945 | 0.2358 | 0.1175 | 0.0000 | 0.0000 |
| 1.5412 | 0.2316 | 0.1226 | 0.0000 | 0.0000 |
| 1.5879 | 0.2274 | 0.1278 | 0.0000 | 0.0000 |
| 1.6346 | 0.2231 | 0.1330 | 0.0000 | 0.0000 |
| 1.6813 | 0.2189 | 0.1384 | 0.0000 | 0.0000 |
| 1.7280 | 0.2146 | 0.1438 | 0.0000 | 0.0000 |
| 1.7747 | 0.2104 | 0.1493 | 0.0000 | 0.0000 |
| 1.8214 | 0.2061 | 0.1549 | 0.0000 | 0.0000 |
| 1.8681 | 0.2019 | 0.1605 | 0.0000 | 0.0000 |
| 1.9148 | 0.1976 | 0.1663 | 0.0000 | 0.0000 |
| 1.9615 | 0.1934 | 0.1721 | 0.0000 | 0.0000 |
| 2.0082 | 0.1891 | 0.1780 | 0.0000 | 0.0000 |
| 2.0549 | 0.1849 | 0.1839 | 0.0000 | 0.0000 |
| 2.1016 | 0.1807 | 0.1899 | 0.0000 | 0.0000 |
| 2.1484 | 0.1764 | 0.1960 | 0.0136 | 0.0000 |
| 2.1951 | 0.1722 | 0.2022 | 0.0203 | 0.0000 |
| 2.2418 | 0.1679 | 0.2084 | 0.0361 | 0.0000 |
| 2.2885 | 0.1637 | 0.2148 | 0.0440 | 0.0000 |
| 2.3352 | 0.1594 | 0.2212 | 0.0561 | 0.0000 |
| 2.3819 | 0.1552 | 0.2277 | 0.0621 | 0.0000 |
| 2.4286 | 0.1509 | 0.2343 | 0.0651 | 0.0000 |
| 2.4753 | 0.1467 | 0.2410 | 0.0666 | 0.0000 |
| 2.5220 | 0.1424 | 0.2477 | 0.0725 | 0.0000 |
| 2.5687 | 0.1382 | 0.2545 | 0.0864 | 0.0000 |
| 2.6154 | 0.1339 | 0.2615 | 0.1023 | 0.0000 |
| 2.6621 | 0.1297 | 0.2685 | 0.1181 | 0.0000 |
| 2.7088 | 0.1255 | 0.2755 | 0.1331 | 0.0000 |
| 2.7500 | 0.1212 | 0.2819 | 0.4362 | 0.0000 |

Landscape Swale Hydraulic Table

| Stage(feet) | Area(ac.) | Volume(ac-ft.) | Discharge(cfs) | To Amended(cfs) | Infilt(cfs) |
|-------------|-----------|----------------|----------------|-----------------|-------------|
| 2.7500      | 0.3712    | 0.2819         | 0.0000         | 0.2878          | 0.0000      |
| 2.7967      | 0.3755    | 0.2993         | 0.0000         | 0.2878          | 0.0000      |
| 2.8434      | 0.3797    | 0.3169         | 0.0000         | 0.3415          | 0.0000      |
| 2.8901      | 0.3839    | 0.3348         | 0.0000         | 0.3684          | 0.0000      |
| 2.9368      | 0.3882    | 0.3528         | 0.0000         | 0.3953          | 0.0000      |
| 2.9835      | 0.3924    | 0.3710         | 0.0000         | 0.4221          | 0.0000      |
| 3.0302      | 0.3967    | 0.3894         | 0.0000         | 0.4490          | 0.0000      |
| 3.0769      | 0.4009    | 0.4081         | 0.0000         | 0.4759          | 0.0000      |
| 3.1236      | 0.4052    | 0.4269         | 0.0000         | 0.5028          | 0.0000      |
| 3.1703      | 0.4094    | 0.4459         | 0.0000         | 0.5297          | 0.0000      |
| 3.2170      | 0.4137    | 0.4651         | 0.0000         | 0.5565          | 0.0000      |
| 3.2637      | 0.4179    | 0.4846         | 0.0000         | 0.5834          | 0.0000      |
| 3.3104      | 0.4222    | 0.5042         | 0.0000         | 0.6103          | 0.0000      |
| 3.3571      | 0.4264    | 0.5240         | 0.0000         | 0.6372          | 0.0000      |
| 3.4038      | 0.4307    | 0.5440         | 0.0000         | 0.6640          | 0.0000      |
| 3.4505      | 0.4349    | 0.5642         | 0.0000         | 0.6909          | 0.0000      |
| 3.4973      | 0.4391    | 0.5846         | 0.0000         | 0.7178          | 0.0000      |
| 3.5440      | 0.4434    | 0.6052         | 0.0000         | 0.7447          | 0.0000      |
| 3.5907      | 0.4476    | 0.6260         | 0.0000         | 0.7716          | 0.0000      |
| 3.6374      | 0.4519    | 0.6470         | 0.0000         | 0.7984          | 0.0000      |
| 3.6841      | 0.4561    | 0.6683         | 0.0000         | 0.8253          | 0.0000      |
| 3.7308      | 0.4604    | 0.6897         | 0.0000         | 0.8522          | 0.0000      |
| 3.7775      | 0.4646    | 0.7113         | 0.1450         | 0.8791          | 0.0000      |
| 3.8242      | 0.4689    | 0.7331         | 0.6429         | 0.9059          | 0.0000      |

|        |        |        |        |        |        |
|--------|--------|--------|--------|--------|--------|
| 3.8709 | 0.4731 | 0.7550 | 1.3367 | 0.9328 | 0.0000 |
| 3.9176 | 0.4774 | 0.7772 | 2.1804 | 0.9597 | 0.0000 |
| 3.9643 | 0.4816 | 0.7996 | 3.1493 | 0.9866 | 0.0000 |
| 4.0110 | 0.4858 | 0.8222 | 4.2264 | 1.0135 | 0.0000 |
| 4.0577 | 0.4901 | 0.8450 | 5.3980 | 1.0403 | 0.0000 |
| 4.1044 | 0.4943 | 0.8680 | 6.6519 | 1.0672 | 0.0000 |
| 4.1511 | 0.4986 | 0.8912 | 7.9768 | 1.0941 | 0.0000 |
| 4.1978 | 0.5028 | 0.9146 | 9.3612 | 1.1210 | 0.0000 |
| 4.2445 | 0.5071 | 0.9382 | 10.794 | 1.1478 | 0.0000 |
| 4.2500 | 0.5076 | 0.9409 | 12.264 | 1.1510 | 0.0000 |

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## Surface Bioretention

Element Flows To:

Outlet 1

Outlet 2

Bioretention Bioretention

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## DMA 1 Porous Pavement

Pavement Area:0.3750 acre.Pavement Length:180.00 ft.

Pavement Width: 90.75 ft.

Pavement slope 1:0.01 To 1

Pavement thickness: 1

Pour Space of Pavement: 0.35

Material thickness of second layer: 0.58

Pour Space of material for second layer: 0.35

Material thickness of third layer: 0

Pour Space of material for third layer: 0

Element Flows To:

Outlet 1                          Outlet 2

Surface Bioretention

Porous Pavement Hydraulic Table

| <b>Stage(feet)</b> | <b>Area(ac.)</b> | <b>Volume(ac-ft.)</b> | <b>Discharge(cfs)</b> | <b>Infilt(cfs)</b> |
|--------------------|------------------|-----------------------|-----------------------|--------------------|
| 0.0000             | 0.375            | 0.000                 | 0.000                 | 0.000              |
| 0.0203             | 0.375            | 0.002                 | 0.061                 | 0.000              |
| 0.0407             | 0.375            | 0.005                 | 0.087                 | 0.000              |
| 0.0610             | 0.375            | 0.008                 | 0.107                 | 0.000              |
| 0.0813             | 0.375            | 0.010                 | 0.123                 | 0.000              |
| 0.1017             | 0.375            | 0.013                 | 0.138                 | 0.000              |
| 0.1220             | 0.375            | 0.016                 | 0.151                 | 0.000              |
| 0.1423             | 0.375            | 0.018                 | 0.163                 | 0.000              |
| 0.1627             | 0.375            | 0.021                 | 0.175                 | 0.000              |
| 0.1830             | 0.375            | 0.024                 | 0.185                 | 0.000              |
| 0.2033             | 0.375            | 0.026                 | 0.195                 | 0.000              |
| 0.2237             | 0.375            | 0.029                 | 0.205                 | 0.000              |
| 0.2440             | 0.375            | 0.032                 | 0.214                 | 0.000              |
| 0.2643             | 0.375            | 0.034                 | 0.223                 | 0.000              |
| 0.2847             | 0.375            | 0.037                 | 0.231                 | 0.000              |
| 0.3050             | 0.375            | 0.040                 | 0.239                 | 0.000              |
| 0.3253             | 0.375            | 0.042                 | 0.247                 | 0.000              |
| 0.3457             | 0.375            | 0.045                 | 0.255                 | 0.000              |
| 0.3660             | 0.375            | 0.048                 | 0.262                 | 0.000              |
| 0.3863             | 0.375            | 0.050                 | 0.269                 | 0.000              |
| 0.4067             | 0.375            | 0.053                 | 0.276                 | 0.000              |
| 0.4270             | 0.375            | 0.056                 | 0.283                 | 0.000              |
| 0.4473             | 0.375            | 0.058                 | 0.290                 | 0.000              |
| 0.4677             | 0.375            | 0.061                 | 0.296                 | 0.000              |
| 0.4880             | 0.375            | 0.064                 | 0.303                 | 0.000              |
| 0.5083             | 0.375            | 0.066                 | 0.309                 | 0.000              |
| 0.5287             | 0.375            | 0.069                 | 0.315                 | 0.000              |
| 0.5490             | 0.375            | 0.072                 | 0.321                 | 0.000              |
| 0.5693             | 0.375            | 0.074                 | 0.327                 | 0.000              |
| 0.5897             | 0.375            | 0.077                 | 0.333                 | 0.000              |
| 0.6100             | 0.375            | 0.080                 | 0.339                 | 0.000              |
| 0.6303             | 0.375            | 0.082                 | 0.344                 | 0.000              |
| 0.6507             | 0.375            | 0.085                 | 0.350                 | 0.000              |
| 0.6710             | 0.375            | 0.088                 | 0.355                 | 0.000              |
| 0.6913             | 0.375            | 0.090                 | 0.361                 | 0.000              |
| 0.7117             | 0.375            | 0.093                 | 0.366                 | 0.000              |
| 0.7320             | 0.375            | 0.096                 | 0.371                 | 0.000              |
| 0.7523             | 0.375            | 0.098                 | 0.376                 | 0.000              |
| 0.7727             | 0.375            | 0.101                 | 0.381                 | 0.000              |
| 0.7930             | 0.375            | 0.104                 | 0.386                 | 0.000              |

|        |       |       |       |       |
|--------|-------|-------|-------|-------|
| 0.8133 | 0.375 | 0.106 | 0.391 | 0.000 |
| 0.8337 | 0.375 | 0.109 | 0.396 | 0.000 |
| 0.8540 | 0.375 | 0.112 | 0.401 | 0.000 |
| 0.8743 | 0.375 | 0.114 | 0.406 | 0.000 |
| 0.8947 | 0.375 | 0.117 | 0.410 | 0.000 |
| 0.9150 | 0.375 | 0.120 | 0.415 | 0.000 |
| 0.9353 | 0.375 | 0.122 | 0.419 | 0.000 |
| 0.9557 | 0.375 | 0.125 | 0.424 | 0.000 |
| 0.9760 | 0.375 | 0.128 | 0.428 | 0.000 |
| 0.9963 | 0.375 | 0.130 | 0.433 | 0.000 |
| 1.0167 | 0.375 | 0.133 | 0.437 | 0.000 |
| 1.0370 | 0.375 | 0.136 | 0.442 | 0.000 |
| 1.0573 | 0.375 | 0.138 | 0.446 | 0.000 |
| 1.0777 | 0.375 | 0.141 | 0.450 | 0.000 |
| 1.0980 | 0.375 | 0.144 | 0.455 | 0.000 |
| 1.1183 | 0.375 | 0.146 | 0.459 | 0.000 |
| 1.1387 | 0.375 | 0.149 | 0.463 | 0.000 |
| 1.1590 | 0.375 | 0.152 | 0.467 | 0.000 |
| 1.1793 | 0.375 | 0.154 | 0.471 | 0.000 |
| 1.1997 | 0.375 | 0.157 | 0.475 | 0.000 |
| 1.2200 | 0.375 | 0.160 | 0.479 | 0.000 |
| 1.2403 | 0.375 | 0.162 | 0.483 | 0.000 |
| 1.2607 | 0.375 | 0.165 | 0.487 | 0.000 |
| 1.2810 | 0.375 | 0.168 | 0.491 | 0.000 |
| 1.3013 | 0.375 | 0.170 | 0.495 | 0.000 |
| 1.3217 | 0.375 | 0.173 | 0.499 | 0.000 |
| 1.3420 | 0.375 | 0.176 | 0.503 | 0.000 |
| 1.3623 | 0.375 | 0.178 | 0.506 | 0.000 |
| 1.3827 | 0.375 | 0.181 | 0.510 | 0.000 |
| 1.4030 | 0.375 | 0.184 | 0.514 | 0.000 |
| 1.4233 | 0.375 | 0.186 | 0.518 | 0.000 |
| 1.4437 | 0.375 | 0.189 | 0.521 | 0.000 |
| 1.4640 | 0.375 | 0.192 | 0.525 | 0.000 |
| 1.4843 | 0.375 | 0.194 | 0.529 | 0.000 |
| 1.5047 | 0.375 | 0.197 | 0.532 | 0.000 |
| 1.5250 | 0.375 | 0.200 | 0.536 | 0.000 |
| 1.5453 | 0.375 | 0.202 | 0.539 | 0.000 |
| 1.5657 | 0.375 | 0.205 | 0.543 | 0.000 |
| 1.5860 | 0.375 | 0.213 | 0.546 | 0.000 |
| 1.6063 | 0.375 | 0.220 | 0.550 | 0.000 |
| 1.6267 | 0.375 | 0.228 | 0.553 | 0.000 |
| 1.6470 | 0.375 | 0.236 | 0.557 | 0.000 |
| 1.6673 | 0.375 | 0.243 | 0.560 | 0.000 |
| 1.6877 | 0.375 | 0.251 | 0.564 | 0.000 |
| 1.7080 | 0.375 | 0.258 | 0.567 | 0.000 |
| 1.7283 | 0.375 | 0.266 | 0.570 | 0.000 |
| 1.7487 | 0.375 | 0.274 | 0.574 | 0.000 |
| 1.7690 | 0.375 | 0.281 | 0.577 | 0.000 |
| 1.7893 | 0.375 | 0.289 | 0.580 | 0.000 |
| 1.8097 | 0.375 | 0.297 | 0.584 | 0.000 |
| 1.8300 | 0.375 | 0.304 | 0.587 | 0.000 |

## DMA 2 Porous Pavement

Pavement Area: 0.4002 acre. Pavement Length: 440.24 ft.

Pavement Width: 39.60 ft.

Pavement slope 1:0.01 To 1

Pavement thickness: 1

Pour Space of Pavement: 0.35

Material thickness of second layer: 0.58

Pour Space of material for second layer: 0.35

Material thickness of third layer: 0

Pour Space of material for third layer: 0

Element Flows To:

Outlet 1                          Outlet 2

Surface Bioretention

Porous Pavement Hydraulic Table

| <b>Stage(feet)</b> | <b>Area(ac.)</b> | <b>Volume(ac-ft.)</b> | <b>Discharge(cfs)</b> | <b>Infilt(cfs)</b> |
|--------------------|------------------|-----------------------|-----------------------|--------------------|
| 0.0000             | 0.400            | 0.000                 | 0.000                 | 0.000              |
| 0.0203             | 0.400            | 0.002                 | 0.061                 | 0.000              |
| 0.0407             | 0.400            | 0.005                 | 0.087                 | 0.000              |
| 0.0610             | 0.400            | 0.008                 | 0.107                 | 0.000              |
| 0.0813             | 0.400            | 0.011                 | 0.123                 | 0.000              |
| 0.1017             | 0.400            | 0.014                 | 0.138                 | 0.000              |
| 0.1220             | 0.400            | 0.017                 | 0.151                 | 0.000              |
| 0.1423             | 0.400            | 0.019                 | 0.163                 | 0.000              |
| 0.1627             | 0.400            | 0.022                 | 0.175                 | 0.000              |
| 0.1830             | 0.400            | 0.025                 | 0.185                 | 0.000              |
| 0.2033             | 0.400            | 0.028                 | 0.195                 | 0.000              |
| 0.2237             | 0.400            | 0.031                 | 0.205                 | 0.000              |
| 0.2440             | 0.400            | 0.034                 | 0.214                 | 0.000              |
| 0.2643             | 0.400            | 0.037                 | 0.223                 | 0.000              |
| 0.2847             | 0.400            | 0.039                 | 0.231                 | 0.000              |
| 0.3050             | 0.400            | 0.042                 | 0.239                 | 0.000              |
| 0.3253             | 0.400            | 0.045                 | 0.247                 | 0.000              |
| 0.3457             | 0.400            | 0.048                 | 0.255                 | 0.000              |
| 0.3660             | 0.400            | 0.051                 | 0.262                 | 0.000              |
| 0.3863             | 0.400            | 0.054                 | 0.269                 | 0.000              |
| 0.4067             | 0.400            | 0.057                 | 0.276                 | 0.000              |
| 0.4270             | 0.400            | 0.059                 | 0.283                 | 0.000              |
| 0.4473             | 0.400            | 0.062                 | 0.290                 | 0.000              |
| 0.4677             | 0.400            | 0.065                 | 0.296                 | 0.000              |
| 0.4880             | 0.400            | 0.068                 | 0.303                 | 0.000              |
| 0.5083             | 0.400            | 0.071                 | 0.309                 | 0.000              |
| 0.5287             | 0.400            | 0.074                 | 0.315                 | 0.000              |
| 0.5490             | 0.400            | 0.076                 | 0.321                 | 0.000              |
| 0.5693             | 0.400            | 0.079                 | 0.327                 | 0.000              |
| 0.5897             | 0.400            | 0.082                 | 0.333                 | 0.000              |
| 0.6100             | 0.400            | 0.085                 | 0.339                 | 0.000              |
| 0.6303             | 0.400            | 0.088                 | 0.344                 | 0.000              |
| 0.6507             | 0.400            | 0.091                 | 0.350                 | 0.000              |
| 0.6710             | 0.400            | 0.094                 | 0.355                 | 0.000              |
| 0.6913             | 0.400            | 0.096                 | 0.361                 | 0.000              |
| 0.7117             | 0.400            | 0.099                 | 0.366                 | 0.000              |
| 0.7320             | 0.400            | 0.102                 | 0.371                 | 0.000              |
| 0.7523             | 0.400            | 0.105                 | 0.376                 | 0.000              |
| 0.7727             | 0.400            | 0.108                 | 0.381                 | 0.000              |
| 0.7930             | 0.400            | 0.111                 | 0.386                 | 0.000              |

|        |       |       |       |       |
|--------|-------|-------|-------|-------|
| 0.8133 | 0.400 | 0.113 | 0.391 | 0.000 |
| 0.8337 | 0.400 | 0.116 | 0.396 | 0.000 |
| 0.8540 | 0.400 | 0.119 | 0.401 | 0.000 |
| 0.8743 | 0.400 | 0.122 | 0.406 | 0.000 |
| 0.8947 | 0.400 | 0.125 | 0.410 | 0.000 |
| 0.9150 | 0.400 | 0.128 | 0.415 | 0.000 |
| 0.9353 | 0.400 | 0.131 | 0.419 | 0.000 |
| 0.9557 | 0.400 | 0.133 | 0.424 | 0.000 |
| 0.9760 | 0.400 | 0.136 | 0.428 | 0.000 |
| 0.9963 | 0.400 | 0.139 | 0.433 | 0.000 |
| 1.0167 | 0.400 | 0.142 | 0.437 | 0.000 |
| 1.0370 | 0.400 | 0.145 | 0.442 | 0.000 |
| 1.0573 | 0.400 | 0.148 | 0.446 | 0.000 |
| 1.0777 | 0.400 | 0.151 | 0.450 | 0.000 |
| 1.0980 | 0.400 | 0.153 | 0.455 | 0.000 |
| 1.1183 | 0.400 | 0.156 | 0.459 | 0.000 |
| 1.1387 | 0.400 | 0.159 | 0.463 | 0.000 |
| 1.1590 | 0.400 | 0.162 | 0.467 | 0.000 |
| 1.1793 | 0.400 | 0.165 | 0.471 | 0.000 |
| 1.1997 | 0.400 | 0.168 | 0.475 | 0.000 |
| 1.2200 | 0.400 | 0.170 | 0.479 | 0.000 |
| 1.2403 | 0.400 | 0.173 | 0.483 | 0.000 |
| 1.2607 | 0.400 | 0.176 | 0.487 | 0.000 |
| 1.2810 | 0.400 | 0.179 | 0.491 | 0.000 |
| 1.3013 | 0.400 | 0.182 | 0.495 | 0.000 |
| 1.3217 | 0.400 | 0.185 | 0.499 | 0.000 |
| 1.3420 | 0.400 | 0.188 | 0.503 | 0.000 |
| 1.3623 | 0.400 | 0.190 | 0.506 | 0.000 |
| 1.3827 | 0.400 | 0.193 | 0.510 | 0.000 |
| 1.4030 | 0.400 | 0.196 | 0.514 | 0.000 |
| 1.4233 | 0.400 | 0.199 | 0.518 | 0.000 |
| 1.4437 | 0.400 | 0.202 | 0.521 | 0.000 |
| 1.4640 | 0.400 | 0.205 | 0.525 | 0.000 |
| 1.4843 | 0.400 | 0.207 | 0.529 | 0.000 |
| 1.5047 | 0.400 | 0.210 | 0.532 | 0.000 |
| 1.5250 | 0.400 | 0.213 | 0.536 | 0.000 |
| 1.5453 | 0.400 | 0.216 | 0.539 | 0.000 |
| 1.5657 | 0.400 | 0.219 | 0.543 | 0.000 |
| 1.5860 | 0.400 | 0.227 | 0.546 | 0.000 |
| 1.6063 | 0.400 | 0.235 | 0.550 | 0.000 |
| 1.6267 | 0.400 | 0.243 | 0.553 | 0.000 |
| 1.6470 | 0.400 | 0.251 | 0.557 | 0.000 |
| 1.6673 | 0.400 | 0.260 | 0.560 | 0.000 |
| 1.6877 | 0.400 | 0.268 | 0.564 | 0.000 |
| 1.7080 | 0.400 | 0.276 | 0.567 | 0.000 |
| 1.7283 | 0.400 | 0.284 | 0.570 | 0.000 |
| 1.7487 | 0.400 | 0.292 | 0.574 | 0.000 |
| 1.7690 | 0.400 | 0.300 | 0.577 | 0.000 |
| 1.7893 | 0.400 | 0.308 | 0.580 | 0.000 |
| 1.8097 | 0.400 | 0.317 | 0.584 | 0.000 |
| 1.8300 | 0.400 | 0.325 | 0.587 | 0.000 |

## DMA 3 Porous Pavement

Pavement Area:0.7969 acre.Pavement Length:467.33 ft.

Pavement Width: 74.28 ft.

Pavement slope 1:0.01 To 1

Pavement thickness: 1

Pour Space of Pavement: 0.35

Material thickness of second layer: 0.58

Pour Space of material for second layer: 0.35

Material thickness of third layer: 0

Pour Space of material for third layer: 0

Element Flows To:

Outlet 1                          Outlet 2

Surface Bioretention

Porous Pavement Hydraulic Table

| <b>Stage(feet)</b> | <b>Area(ac.)</b> | <b>Volume(ac-ft.)</b> | <b>Discharge(cfs)</b> | <b>Infilt(cfs)</b> |
|--------------------|------------------|-----------------------|-----------------------|--------------------|
| 0.0000             | 0.796            | 0.000                 | 0.000                 | 0.000              |
| 0.0203             | 0.796            | 0.005                 | 0.061                 | 0.000              |
| 0.0407             | 0.796            | 0.011                 | 0.087                 | 0.000              |
| 0.0610             | 0.796            | 0.017                 | 0.107                 | 0.000              |
| 0.0813             | 0.796            | 0.022                 | 0.123                 | 0.000              |
| 0.1017             | 0.796            | 0.028                 | 0.138                 | 0.000              |
| 0.1220             | 0.796            | 0.034                 | 0.151                 | 0.000              |
| 0.1423             | 0.796            | 0.039                 | 0.163                 | 0.000              |
| 0.1627             | 0.796            | 0.045                 | 0.175                 | 0.000              |
| 0.1830             | 0.796            | 0.051                 | 0.185                 | 0.000              |
| 0.2033             | 0.796            | 0.056                 | 0.195                 | 0.000              |
| 0.2237             | 0.796            | 0.062                 | 0.205                 | 0.000              |
| 0.2440             | 0.796            | 0.068                 | 0.214                 | 0.000              |
| 0.2643             | 0.796            | 0.073                 | 0.223                 | 0.000              |
| 0.2847             | 0.796            | 0.079                 | 0.231                 | 0.000              |
| 0.3050             | 0.796            | 0.085                 | 0.239                 | 0.000              |
| 0.3253             | 0.796            | 0.090                 | 0.247                 | 0.000              |
| 0.3457             | 0.796            | 0.096                 | 0.255                 | 0.000              |
| 0.3660             | 0.796            | 0.102                 | 0.262                 | 0.000              |
| 0.3863             | 0.796            | 0.107                 | 0.269                 | 0.000              |
| 0.4067             | 0.796            | 0.113                 | 0.276                 | 0.000              |
| 0.4270             | 0.796            | 0.119                 | 0.283                 | 0.000              |
| 0.4473             | 0.796            | 0.124                 | 0.290                 | 0.000              |
| 0.4677             | 0.796            | 0.130                 | 0.296                 | 0.000              |
| 0.4880             | 0.796            | 0.136                 | 0.303                 | 0.000              |
| 0.5083             | 0.796            | 0.141                 | 0.309                 | 0.000              |
| 0.5287             | 0.796            | 0.147                 | 0.315                 | 0.000              |
| 0.5490             | 0.796            | 0.153                 | 0.321                 | 0.000              |
| 0.5693             | 0.796            | 0.158                 | 0.327                 | 0.000              |
| 0.5897             | 0.796            | 0.164                 | 0.333                 | 0.000              |
| 0.6100             | 0.796            | 0.170                 | 0.339                 | 0.000              |
| 0.6303             | 0.796            | 0.175                 | 0.344                 | 0.000              |
| 0.6507             | 0.796            | 0.181                 | 0.350                 | 0.000              |
| 0.6710             | 0.796            | 0.187                 | 0.355                 | 0.000              |
| 0.6913             | 0.796            | 0.192                 | 0.361                 | 0.000              |
| 0.7117             | 0.796            | 0.198                 | 0.366                 | 0.000              |
| 0.7320             | 0.796            | 0.204                 | 0.371                 | 0.000              |
| 0.7523             | 0.796            | 0.209                 | 0.376                 | 0.000              |
| 0.7727             | 0.796            | 0.215                 | 0.381                 | 0.000              |
| 0.7930             | 0.796            | 0.221                 | 0.386                 | 0.000              |

|        |       |       |       |       |
|--------|-------|-------|-------|-------|
| 0.8133 | 0.796 | 0.226 | 0.391 | 0.000 |
| 0.8337 | 0.796 | 0.232 | 0.396 | 0.000 |
| 0.8540 | 0.796 | 0.238 | 0.401 | 0.000 |
| 0.8743 | 0.796 | 0.243 | 0.406 | 0.000 |
| 0.8947 | 0.796 | 0.249 | 0.410 | 0.000 |
| 0.9150 | 0.796 | 0.255 | 0.415 | 0.000 |
| 0.9353 | 0.796 | 0.260 | 0.419 | 0.000 |
| 0.9557 | 0.796 | 0.266 | 0.424 | 0.000 |
| 0.9760 | 0.796 | 0.272 | 0.428 | 0.000 |
| 0.9963 | 0.796 | 0.277 | 0.433 | 0.000 |
| 1.0167 | 0.796 | 0.283 | 0.437 | 0.000 |
| 1.0370 | 0.796 | 0.289 | 0.442 | 0.000 |
| 1.0573 | 0.796 | 0.294 | 0.446 | 0.000 |
| 1.0777 | 0.796 | 0.300 | 0.450 | 0.000 |
| 1.0980 | 0.796 | 0.306 | 0.455 | 0.000 |
| 1.1183 | 0.796 | 0.311 | 0.459 | 0.000 |
| 1.1387 | 0.796 | 0.317 | 0.463 | 0.000 |
| 1.1590 | 0.796 | 0.323 | 0.467 | 0.000 |
| 1.1793 | 0.796 | 0.328 | 0.471 | 0.000 |
| 1.1997 | 0.796 | 0.334 | 0.475 | 0.000 |
| 1.2200 | 0.796 | 0.340 | 0.479 | 0.000 |
| 1.2403 | 0.796 | 0.346 | 0.483 | 0.000 |
| 1.2607 | 0.797 | 0.351 | 0.487 | 0.000 |
| 1.2810 | 0.797 | 0.357 | 0.491 | 0.000 |
| 1.3013 | 0.797 | 0.363 | 0.495 | 0.000 |
| 1.3217 | 0.797 | 0.368 | 0.499 | 0.000 |
| 1.3420 | 0.797 | 0.374 | 0.503 | 0.000 |
| 1.3623 | 0.797 | 0.380 | 0.506 | 0.000 |
| 1.3827 | 0.797 | 0.385 | 0.510 | 0.000 |
| 1.4030 | 0.797 | 0.391 | 0.514 | 0.000 |
| 1.4233 | 0.797 | 0.397 | 0.518 | 0.000 |
| 1.4437 | 0.797 | 0.402 | 0.521 | 0.000 |
| 1.4640 | 0.797 | 0.408 | 0.525 | 0.000 |
| 1.4843 | 0.797 | 0.414 | 0.529 | 0.000 |
| 1.5047 | 0.797 | 0.419 | 0.532 | 0.000 |
| 1.5250 | 0.797 | 0.425 | 0.536 | 0.000 |
| 1.5453 | 0.797 | 0.431 | 0.539 | 0.000 |
| 1.5657 | 0.797 | 0.436 | 0.543 | 0.000 |
| 1.5860 | 0.797 | 0.452 | 0.546 | 0.000 |
| 1.6063 | 0.797 | 0.469 | 0.550 | 0.000 |
| 1.6267 | 0.797 | 0.485 | 0.553 | 0.000 |
| 1.6470 | 0.797 | 0.501 | 0.557 | 0.000 |
| 1.6673 | 0.797 | 0.517 | 0.560 | 0.000 |
| 1.6877 | 0.797 | 0.533 | 0.564 | 0.000 |
| 1.7080 | 0.797 | 0.550 | 0.567 | 0.000 |
| 1.7283 | 0.797 | 0.566 | 0.570 | 0.000 |
| 1.7487 | 0.797 | 0.582 | 0.574 | 0.000 |
| 1.7690 | 0.797 | 0.598 | 0.577 | 0.000 |
| 1.7893 | 0.797 | 0.615 | 0.580 | 0.000 |
| 1.8097 | 0.797 | 0.631 | 0.584 | 0.000 |
| 1.8300 | 0.797 | 0.647 | 0.587 | 0.000 |

## DMA 4 Porous Pavement

Pavement Area:0.3934 acre.Pavement Length:540.53 ft.

Pavement Width: 31.70 ft.

Pavement slope 1:0.01 To 1

Pavement thickness: 1

Pour Space of Pavement: 0.35

Material thickness of second layer: 0.58

Pour Space of material for second layer: 0.35

Material thickness of third layer: 0

Pour Space of material for third layer: 0

Element Flows To:

Outlet 1                          Outlet 2

Surface Bioretention

Porous Pavement Hydraulic Table

| <b>Stage(feet)</b> | <b>Area(ac.)</b> | <b>Volume(ac-ft.)</b> | <b>Discharge(cfs)</b> | <b>Infilt(cfs)</b> |
|--------------------|------------------|-----------------------|-----------------------|--------------------|
| 0.0000             | 0.393            | 0.000                 | 0.000                 | 0.000              |
| 0.0203             | 0.393            | 0.002                 | 0.061                 | 0.000              |
| 0.0407             | 0.393            | 0.005                 | 0.087                 | 0.000              |
| 0.0610             | 0.393            | 0.008                 | 0.107                 | 0.000              |
| 0.0813             | 0.393            | 0.011                 | 0.123                 | 0.000              |
| 0.1017             | 0.393            | 0.014                 | 0.138                 | 0.000              |
| 0.1220             | 0.393            | 0.016                 | 0.151                 | 0.000              |
| 0.1423             | 0.393            | 0.019                 | 0.163                 | 0.000              |
| 0.1627             | 0.393            | 0.022                 | 0.175                 | 0.000              |
| 0.1830             | 0.393            | 0.025                 | 0.185                 | 0.000              |
| 0.2033             | 0.393            | 0.028                 | 0.195                 | 0.000              |
| 0.2237             | 0.393            | 0.030                 | 0.205                 | 0.000              |
| 0.2440             | 0.393            | 0.033                 | 0.214                 | 0.000              |
| 0.2643             | 0.393            | 0.036                 | 0.223                 | 0.000              |
| 0.2847             | 0.393            | 0.039                 | 0.231                 | 0.000              |
| 0.3050             | 0.393            | 0.042                 | 0.239                 | 0.000              |
| 0.3253             | 0.393            | 0.044                 | 0.247                 | 0.000              |
| 0.3457             | 0.393            | 0.047                 | 0.255                 | 0.000              |
| 0.3660             | 0.393            | 0.050                 | 0.262                 | 0.000              |
| 0.3863             | 0.393            | 0.053                 | 0.269                 | 0.000              |
| 0.4067             | 0.393            | 0.056                 | 0.276                 | 0.000              |
| 0.4270             | 0.393            | 0.058                 | 0.283                 | 0.000              |
| 0.4473             | 0.393            | 0.061                 | 0.290                 | 0.000              |
| 0.4677             | 0.393            | 0.064                 | 0.296                 | 0.000              |
| 0.4880             | 0.393            | 0.067                 | 0.303                 | 0.000              |
| 0.5083             | 0.393            | 0.070                 | 0.309                 | 0.000              |
| 0.5287             | 0.393            | 0.072                 | 0.315                 | 0.000              |
| 0.5490             | 0.393            | 0.075                 | 0.321                 | 0.000              |
| 0.5693             | 0.393            | 0.078                 | 0.327                 | 0.000              |
| 0.5897             | 0.393            | 0.081                 | 0.333                 | 0.000              |
| 0.6100             | 0.393            | 0.084                 | 0.339                 | 0.000              |
| 0.6303             | 0.393            | 0.086                 | 0.344                 | 0.000              |
| 0.6507             | 0.393            | 0.089                 | 0.350                 | 0.000              |
| 0.6710             | 0.393            | 0.092                 | 0.355                 | 0.000              |
| 0.6913             | 0.393            | 0.095                 | 0.361                 | 0.000              |
| 0.7117             | 0.393            | 0.098                 | 0.366                 | 0.000              |
| 0.7320             | 0.393            | 0.100                 | 0.371                 | 0.000              |
| 0.7523             | 0.393            | 0.103                 | 0.376                 | 0.000              |
| 0.7727             | 0.393            | 0.106                 | 0.381                 | 0.000              |
| 0.7930             | 0.393            | 0.109                 | 0.386                 | 0.000              |

|        |       |       |       |       |
|--------|-------|-------|-------|-------|
| 0.8133 | 0.393 | 0.112 | 0.391 | 0.000 |
| 0.8337 | 0.393 | 0.114 | 0.396 | 0.000 |
| 0.8540 | 0.393 | 0.117 | 0.401 | 0.000 |
| 0.8743 | 0.393 | 0.120 | 0.406 | 0.000 |
| 0.8947 | 0.393 | 0.123 | 0.410 | 0.000 |
| 0.9150 | 0.393 | 0.126 | 0.415 | 0.000 |
| 0.9353 | 0.393 | 0.128 | 0.419 | 0.000 |
| 0.9557 | 0.393 | 0.131 | 0.424 | 0.000 |
| 0.9760 | 0.393 | 0.134 | 0.428 | 0.000 |
| 0.9963 | 0.393 | 0.137 | 0.433 | 0.000 |
| 1.0167 | 0.393 | 0.140 | 0.437 | 0.000 |
| 1.0370 | 0.393 | 0.142 | 0.442 | 0.000 |
| 1.0573 | 0.393 | 0.145 | 0.446 | 0.000 |
| 1.0777 | 0.393 | 0.148 | 0.450 | 0.000 |
| 1.0980 | 0.393 | 0.151 | 0.455 | 0.000 |
| 1.1183 | 0.393 | 0.154 | 0.459 | 0.000 |
| 1.1387 | 0.393 | 0.156 | 0.463 | 0.000 |
| 1.1590 | 0.393 | 0.159 | 0.467 | 0.000 |
| 1.1793 | 0.393 | 0.162 | 0.471 | 0.000 |
| 1.1997 | 0.393 | 0.165 | 0.475 | 0.000 |
| 1.2200 | 0.393 | 0.168 | 0.479 | 0.000 |
| 1.2403 | 0.393 | 0.170 | 0.483 | 0.000 |
| 1.2607 | 0.393 | 0.173 | 0.487 | 0.000 |
| 1.2810 | 0.393 | 0.176 | 0.491 | 0.000 |
| 1.3013 | 0.393 | 0.179 | 0.495 | 0.000 |
| 1.3217 | 0.393 | 0.182 | 0.499 | 0.000 |
| 1.3420 | 0.393 | 0.184 | 0.503 | 0.000 |
| 1.3623 | 0.393 | 0.187 | 0.506 | 0.000 |
| 1.3827 | 0.393 | 0.190 | 0.510 | 0.000 |
| 1.4030 | 0.393 | 0.193 | 0.514 | 0.000 |
| 1.4233 | 0.393 | 0.196 | 0.518 | 0.000 |
| 1.4437 | 0.393 | 0.198 | 0.521 | 0.000 |
| 1.4640 | 0.393 | 0.201 | 0.525 | 0.000 |
| 1.4843 | 0.393 | 0.204 | 0.529 | 0.000 |
| 1.5047 | 0.393 | 0.207 | 0.532 | 0.000 |
| 1.5250 | 0.393 | 0.210 | 0.536 | 0.000 |
| 1.5453 | 0.393 | 0.212 | 0.539 | 0.000 |
| 1.5657 | 0.393 | 0.215 | 0.543 | 0.000 |
| 1.5860 | 0.393 | 0.223 | 0.546 | 0.000 |
| 1.6063 | 0.393 | 0.231 | 0.550 | 0.000 |
| 1.6267 | 0.393 | 0.239 | 0.553 | 0.000 |
| 1.6470 | 0.393 | 0.247 | 0.557 | 0.000 |
| 1.6673 | 0.393 | 0.255 | 0.560 | 0.000 |
| 1.6877 | 0.393 | 0.263 | 0.564 | 0.000 |
| 1.7080 | 0.393 | 0.271 | 0.567 | 0.000 |
| 1.7283 | 0.393 | 0.279 | 0.570 | 0.000 |
| 1.7487 | 0.393 | 0.287 | 0.574 | 0.000 |
| 1.7690 | 0.393 | 0.295 | 0.577 | 0.000 |
| 1.7893 | 0.393 | 0.303 | 0.580 | 0.000 |
| 1.8097 | 0.393 | 0.311 | 0.584 | 0.000 |
| 1.8300 | 0.393 | 0.319 | 0.587 | 0.000 |

## DMA 5 Porous Pavement

Pavement Area: 0.2929 acre. Pavement Length: 321.87 ft.

Pavement Width: 39.64 ft.

Pavement slope 1:0.01 To 1

Pavement thickness: 1

Pour Space of Pavement: 0.35

Material thickness of second layer: 0.58

Pour Space of material for second layer: 0.35

Material thickness of third layer: 0

Pour Space of material for third layer: 0

Element Flows To:

Outlet 1                          Outlet 2

Surface Bioretention

Porous Pavement Hydraulic Table

| <b>Stage(feet)</b> | <b>Area(ac.)</b> | <b>Volume(ac-ft.)</b> | <b>Discharge(cfs)</b> | <b>Infilt(cfs)</b> |
|--------------------|------------------|-----------------------|-----------------------|--------------------|
| 0.0000             | 0.292            | 0.000                 | 0.000                 | 0.000              |
| 0.0203             | 0.292            | 0.002                 | 0.061                 | 0.000              |
| 0.0407             | 0.292            | 0.004                 | 0.087                 | 0.000              |
| 0.0610             | 0.292            | 0.006                 | 0.107                 | 0.000              |
| 0.0813             | 0.292            | 0.008                 | 0.123                 | 0.000              |
| 0.1017             | 0.292            | 0.010                 | 0.138                 | 0.000              |
| 0.1220             | 0.292            | 0.012                 | 0.151                 | 0.000              |
| 0.1423             | 0.292            | 0.014                 | 0.163                 | 0.000              |
| 0.1627             | 0.292            | 0.016                 | 0.175                 | 0.000              |
| 0.1830             | 0.292            | 0.018                 | 0.185                 | 0.000              |
| 0.2033             | 0.292            | 0.020                 | 0.195                 | 0.000              |
| 0.2237             | 0.292            | 0.022                 | 0.205                 | 0.000              |
| 0.2440             | 0.292            | 0.025                 | 0.214                 | 0.000              |
| 0.2643             | 0.292            | 0.027                 | 0.223                 | 0.000              |
| 0.2847             | 0.292            | 0.029                 | 0.231                 | 0.000              |
| 0.3050             | 0.292            | 0.031                 | 0.239                 | 0.000              |
| 0.3253             | 0.292            | 0.033                 | 0.247                 | 0.000              |
| 0.3457             | 0.292            | 0.035                 | 0.255                 | 0.000              |
| 0.3660             | 0.292            | 0.037                 | 0.262                 | 0.000              |
| 0.3863             | 0.292            | 0.039                 | 0.269                 | 0.000              |
| 0.4067             | 0.292            | 0.041                 | 0.276                 | 0.000              |
| 0.4270             | 0.292            | 0.043                 | 0.283                 | 0.000              |
| 0.4473             | 0.292            | 0.045                 | 0.290                 | 0.000              |
| 0.4677             | 0.292            | 0.047                 | 0.296                 | 0.000              |
| 0.4880             | 0.292            | 0.050                 | 0.303                 | 0.000              |
| 0.5083             | 0.292            | 0.052                 | 0.309                 | 0.000              |
| 0.5287             | 0.292            | 0.054                 | 0.315                 | 0.000              |
| 0.5490             | 0.292            | 0.056                 | 0.321                 | 0.000              |
| 0.5693             | 0.292            | 0.058                 | 0.327                 | 0.000              |
| 0.5897             | 0.292            | 0.060                 | 0.333                 | 0.000              |
| 0.6100             | 0.292            | 0.062                 | 0.339                 | 0.000              |
| 0.6303             | 0.292            | 0.064                 | 0.344                 | 0.000              |
| 0.6507             | 0.292            | 0.066                 | 0.350                 | 0.000              |
| 0.6710             | 0.292            | 0.068                 | 0.355                 | 0.000              |
| 0.6913             | 0.292            | 0.070                 | 0.361                 | 0.000              |
| 0.7117             | 0.292            | 0.073                 | 0.366                 | 0.000              |
| 0.7320             | 0.292            | 0.075                 | 0.371                 | 0.000              |
| 0.7523             | 0.292            | 0.077                 | 0.376                 | 0.000              |
| 0.7727             | 0.292            | 0.079                 | 0.381                 | 0.000              |
| 0.7930             | 0.292            | 0.081                 | 0.386                 | 0.000              |

|        |       |       |       |       |
|--------|-------|-------|-------|-------|
| 0.8133 | 0.292 | 0.083 | 0.391 | 0.000 |
| 0.8337 | 0.292 | 0.085 | 0.396 | 0.000 |
| 0.8540 | 0.292 | 0.087 | 0.401 | 0.000 |
| 0.8743 | 0.292 | 0.089 | 0.406 | 0.000 |
| 0.8947 | 0.292 | 0.091 | 0.410 | 0.000 |
| 0.9150 | 0.292 | 0.093 | 0.415 | 0.000 |
| 0.9353 | 0.292 | 0.095 | 0.419 | 0.000 |
| 0.9557 | 0.292 | 0.098 | 0.424 | 0.000 |
| 0.9760 | 0.292 | 0.100 | 0.428 | 0.000 |
| 0.9963 | 0.292 | 0.102 | 0.433 | 0.000 |
| 1.0167 | 0.292 | 0.104 | 0.437 | 0.000 |
| 1.0370 | 0.292 | 0.106 | 0.442 | 0.000 |
| 1.0573 | 0.292 | 0.108 | 0.446 | 0.000 |
| 1.0777 | 0.292 | 0.110 | 0.450 | 0.000 |
| 1.0980 | 0.292 | 0.112 | 0.455 | 0.000 |
| 1.1183 | 0.292 | 0.114 | 0.459 | 0.000 |
| 1.1387 | 0.292 | 0.116 | 0.463 | 0.000 |
| 1.1590 | 0.292 | 0.118 | 0.467 | 0.000 |
| 1.1793 | 0.292 | 0.120 | 0.471 | 0.000 |
| 1.1997 | 0.292 | 0.123 | 0.475 | 0.000 |
| 1.2200 | 0.292 | 0.125 | 0.479 | 0.000 |
| 1.2403 | 0.292 | 0.127 | 0.483 | 0.000 |
| 1.2607 | 0.292 | 0.129 | 0.487 | 0.000 |
| 1.2810 | 0.292 | 0.131 | 0.491 | 0.000 |
| 1.3013 | 0.292 | 0.133 | 0.495 | 0.000 |
| 1.3217 | 0.292 | 0.135 | 0.499 | 0.000 |
| 1.3420 | 0.292 | 0.137 | 0.503 | 0.000 |
| 1.3623 | 0.292 | 0.139 | 0.506 | 0.000 |
| 1.3827 | 0.292 | 0.141 | 0.510 | 0.000 |
| 1.4030 | 0.292 | 0.143 | 0.514 | 0.000 |
| 1.4233 | 0.292 | 0.145 | 0.518 | 0.000 |
| 1.4437 | 0.292 | 0.148 | 0.521 | 0.000 |
| 1.4640 | 0.292 | 0.150 | 0.525 | 0.000 |
| 1.4843 | 0.292 | 0.152 | 0.529 | 0.000 |
| 1.5047 | 0.292 | 0.154 | 0.532 | 0.000 |
| 1.5250 | 0.292 | 0.156 | 0.536 | 0.000 |
| 1.5453 | 0.292 | 0.158 | 0.539 | 0.000 |
| 1.5657 | 0.292 | 0.160 | 0.543 | 0.000 |
| 1.5860 | 0.292 | 0.166 | 0.546 | 0.000 |
| 1.6063 | 0.292 | 0.172 | 0.550 | 0.000 |
| 1.6267 | 0.292 | 0.178 | 0.553 | 0.000 |
| 1.6470 | 0.292 | 0.184 | 0.557 | 0.000 |
| 1.6673 | 0.292 | 0.190 | 0.560 | 0.000 |
| 1.6877 | 0.292 | 0.196 | 0.564 | 0.000 |
| 1.7080 | 0.292 | 0.202 | 0.567 | 0.000 |
| 1.7283 | 0.292 | 0.208 | 0.570 | 0.000 |
| 1.7487 | 0.292 | 0.214 | 0.574 | 0.000 |
| 1.7690 | 0.292 | 0.220 | 0.577 | 0.000 |
| 1.7893 | 0.292 | 0.226 | 0.580 | 0.000 |
| 1.8097 | 0.292 | 0.232 | 0.584 | 0.000 |
| 1.8300 | 0.292 | 0.237 | 0.587 | 0.000 |

## DMA 6 Porous Pavement

Pavement Area: 0.0265 acre. Pavement Length: 38.37 ft.

Pavement Width: 30.14 ft.

Pavement slope 1:0.01 To 1

Pavement thickness: 1

Pour Space of Pavement: 0.35

Material thickness of second layer: 0.58

Pour Space of material for second layer: 0.35

Material thickness of third layer: 0

Pour Space of material for third layer: 0

Element Flows To:

Outlet 1                          Outlet 2

Surface Bioretention

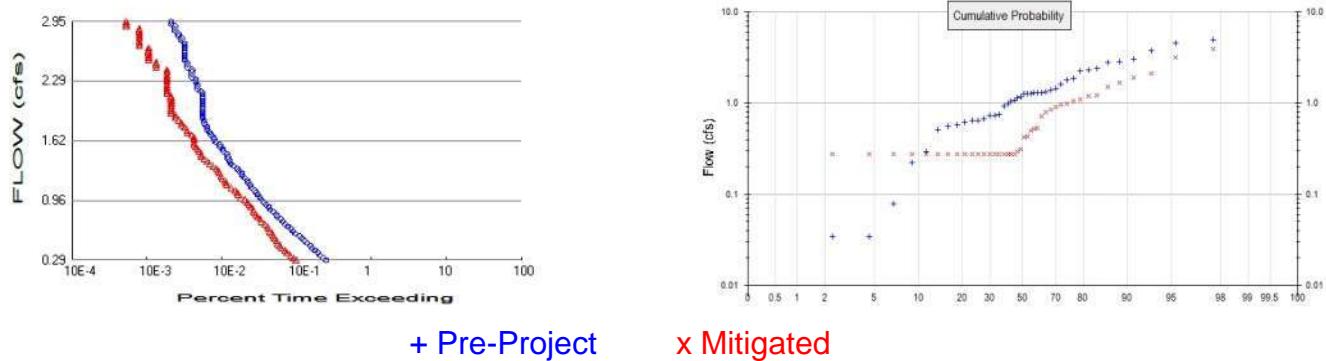
Porous Pavement Hydraulic Table

| <b>Stage(feet)</b> | <b>Area(ac.)</b> | <b>Volume(ac-ft.)</b> | <b>Discharge(cfs)</b> | <b>Infilt(cfs)</b> |
|--------------------|------------------|-----------------------|-----------------------|--------------------|
| 0.0000             | 0.026            | 0.000                 | 0.000                 | 0.000              |
| 0.0203             | 0.026            | 0.000                 | 0.061                 | 0.000              |
| 0.0407             | 0.026            | 0.000                 | 0.087                 | 0.000              |
| 0.0610             | 0.026            | 0.000                 | 0.107                 | 0.000              |
| 0.0813             | 0.026            | 0.000                 | 0.123                 | 0.000              |
| 0.1017             | 0.026            | 0.000                 | 0.138                 | 0.000              |
| 0.1220             | 0.026            | 0.001                 | 0.151                 | 0.000              |
| 0.1423             | 0.026            | 0.001                 | 0.163                 | 0.000              |
| 0.1627             | 0.026            | 0.001                 | 0.175                 | 0.000              |
| 0.1830             | 0.026            | 0.001                 | 0.185                 | 0.000              |
| 0.2033             | 0.026            | 0.001                 | 0.195                 | 0.000              |
| 0.2237             | 0.026            | 0.002                 | 0.205                 | 0.000              |
| 0.2440             | 0.026            | 0.002                 | 0.214                 | 0.000              |
| 0.2643             | 0.026            | 0.002                 | 0.223                 | 0.000              |
| 0.2847             | 0.026            | 0.002                 | 0.231                 | 0.000              |
| 0.3050             | 0.026            | 0.002                 | 0.239                 | 0.000              |
| 0.3253             | 0.026            | 0.003                 | 0.247                 | 0.000              |
| 0.3457             | 0.026            | 0.003                 | 0.255                 | 0.000              |
| 0.3660             | 0.026            | 0.003                 | 0.262                 | 0.000              |
| 0.3863             | 0.026            | 0.003                 | 0.269                 | 0.000              |
| 0.4067             | 0.026            | 0.003                 | 0.276                 | 0.000              |
| 0.4270             | 0.026            | 0.004                 | 0.283                 | 0.000              |
| 0.4473             | 0.026            | 0.004                 | 0.290                 | 0.000              |
| 0.4677             | 0.026            | 0.004                 | 0.296                 | 0.000              |
| 0.4880             | 0.026            | 0.004                 | 0.303                 | 0.000              |
| 0.5083             | 0.026            | 0.004                 | 0.309                 | 0.000              |
| 0.5287             | 0.026            | 0.004                 | 0.315                 | 0.000              |
| 0.5490             | 0.026            | 0.005                 | 0.321                 | 0.000              |
| 0.5693             | 0.026            | 0.005                 | 0.327                 | 0.000              |
| 0.5897             | 0.026            | 0.005                 | 0.333                 | 0.000              |
| 0.6100             | 0.026            | 0.005                 | 0.339                 | 0.000              |
| 0.6303             | 0.026            | 0.005                 | 0.344                 | 0.000              |
| 0.6507             | 0.026            | 0.006                 | 0.350                 | 0.000              |
| 0.6710             | 0.026            | 0.006                 | 0.355                 | 0.000              |
| 0.6913             | 0.026            | 0.006                 | 0.361                 | 0.000              |
| 0.7117             | 0.026            | 0.006                 | 0.366                 | 0.000              |
| 0.7320             | 0.026            | 0.006                 | 0.371                 | 0.000              |
| 0.7523             | 0.026            | 0.007                 | 0.376                 | 0.000              |
| 0.7727             | 0.026            | 0.007                 | 0.381                 | 0.000              |
| 0.7930             | 0.026            | 0.007                 | 0.386                 | 0.000              |

|        |       |       |       |       |
|--------|-------|-------|-------|-------|
| 0.8133 | 0.026 | 0.007 | 0.391 | 0.000 |
| 0.8337 | 0.026 | 0.007 | 0.396 | 0.000 |
| 0.8540 | 0.026 | 0.007 | 0.401 | 0.000 |
| 0.8743 | 0.026 | 0.008 | 0.406 | 0.000 |
| 0.8947 | 0.026 | 0.008 | 0.410 | 0.000 |
| 0.9150 | 0.026 | 0.008 | 0.415 | 0.000 |
| 0.9353 | 0.026 | 0.008 | 0.419 | 0.000 |
| 0.9557 | 0.026 | 0.008 | 0.424 | 0.000 |
| 0.9760 | 0.026 | 0.009 | 0.428 | 0.000 |
| 0.9963 | 0.026 | 0.009 | 0.433 | 0.000 |
| 1.0167 | 0.026 | 0.009 | 0.437 | 0.000 |
| 1.0370 | 0.026 | 0.009 | 0.442 | 0.000 |
| 1.0573 | 0.026 | 0.009 | 0.446 | 0.000 |
| 1.0777 | 0.026 | 0.010 | 0.450 | 0.000 |
| 1.0980 | 0.026 | 0.010 | 0.455 | 0.000 |
| 1.1183 | 0.026 | 0.010 | 0.459 | 0.000 |
| 1.1387 | 0.026 | 0.010 | 0.463 | 0.000 |
| 1.1590 | 0.026 | 0.010 | 0.467 | 0.000 |
| 1.1793 | 0.026 | 0.011 | 0.471 | 0.000 |
| 1.1997 | 0.026 | 0.011 | 0.475 | 0.000 |
| 1.2200 | 0.026 | 0.011 | 0.479 | 0.000 |
| 1.2403 | 0.026 | 0.011 | 0.483 | 0.000 |
| 1.2607 | 0.026 | 0.011 | 0.487 | 0.000 |
| 1.2810 | 0.026 | 0.011 | 0.491 | 0.000 |
| 1.3013 | 0.026 | 0.012 | 0.495 | 0.000 |
| 1.3217 | 0.026 | 0.012 | 0.499 | 0.000 |
| 1.3420 | 0.026 | 0.012 | 0.503 | 0.000 |
| 1.3623 | 0.026 | 0.012 | 0.506 | 0.000 |
| 1.3827 | 0.026 | 0.012 | 0.510 | 0.000 |
| 1.4030 | 0.026 | 0.013 | 0.514 | 0.000 |
| 1.4233 | 0.026 | 0.013 | 0.518 | 0.000 |
| 1.4437 | 0.026 | 0.013 | 0.521 | 0.000 |
| 1.4640 | 0.026 | 0.013 | 0.525 | 0.000 |
| 1.4843 | 0.026 | 0.013 | 0.529 | 0.000 |
| 1.5047 | 0.026 | 0.014 | 0.532 | 0.000 |
| 1.5250 | 0.026 | 0.014 | 0.536 | 0.000 |
| 1.5453 | 0.026 | 0.014 | 0.539 | 0.000 |
| 1.5657 | 0.026 | 0.014 | 0.543 | 0.000 |
| 1.5860 | 0.026 | 0.015 | 0.546 | 0.000 |
| 1.6063 | 0.026 | 0.015 | 0.550 | 0.000 |
| 1.6267 | 0.026 | 0.016 | 0.553 | 0.000 |
| 1.6470 | 0.026 | 0.016 | 0.557 | 0.000 |
| 1.6673 | 0.026 | 0.017 | 0.560 | 0.000 |
| 1.6877 | 0.026 | 0.017 | 0.564 | 0.000 |
| 1.7080 | 0.026 | 0.018 | 0.567 | 0.000 |
| 1.7283 | 0.026 | 0.018 | 0.570 | 0.000 |
| 1.7487 | 0.026 | 0.019 | 0.574 | 0.000 |
| 1.7690 | 0.026 | 0.020 | 0.577 | 0.000 |
| 1.7893 | 0.026 | 0.020 | 0.580 | 0.000 |
| 1.8097 | 0.026 | 0.021 | 0.584 | 0.000 |
| 1.8300 | 0.026 | 0.021 | 0.587 | 0.000 |

## Analysis Results

### POC 1



#### Pre-Project Landuse Totals for POC #1

Total Pervious Area: 6.96  
Total Impervious Area: 0.14

#### Mitigated Landuse Totals for POC #1

Total Pervious Area: 1.9  
Total Impervious Area: 5.19494

Flow Frequency Method: Log Pearson Type III 17B

#### Flow Frequency Return Periods for Pre-Project. POC #1

| Return Period | Flow(cfs) |
|---------------|-----------|
| 2 year        | 1.16484   |
| 5 year        | 2.285182  |
| 10 year       | 2.95431   |
| 25 year       | 4.663007  |

#### Flow Frequency Return Periods for Mitigated. POC #1

| Return Period | Flow(cfs) |
|---------------|-----------|
| 2 year        | 0.316607  |
| 5 year        | 1.109459  |
| 10 year       | 1.802665  |
| 25 year       | 3.29896   |

#### Annual Peaks

#### Annual Peaks for Pre-Project and Mitigated. POC #1

| Year | Pre-Project | Mitigated |
|------|-------------|-----------|
| 1962 | 1.311       | 0.994     |
| 1963 | 0.674       | 0.274     |
| 1964 | 0.223       | 0.274     |
| 1965 | 1.267       | 0.317     |
| 1966 | 0.079       | 0.274     |
| 1967 | 1.273       | 1.214     |
| 1968 | 0.515       | 0.274     |
| 1969 | 1.150       | 0.435     |
| 1970 | 0.935       | 0.421     |
| 1971 | 1.387       | 1.059     |
| 1972 | 0.034       | 0.274     |
| 1973 | 2.782       | 0.538     |
| 1974 | 0.992       | 0.274     |
| 1975 | 1.311       | 0.274     |

|      |       |       |
|------|-------|-------|
| 1976 | 0.029 | 0.274 |
| 1977 | 0.034 | 0.193 |
| 1978 | 1.459 | 0.504 |
| 1979 | 0.560 | 0.274 |
| 1980 | 2.330 | 0.295 |
| 1981 | 0.293 | 0.274 |
| 1982 | 2.275 | 1.525 |
| 1983 | 2.833 | 2.145 |
| 1984 | 1.165 | 0.843 |
| 1985 | 0.736 | 0.791 |
| 1986 | 4.619 | 3.199 |
| 1987 | 0.648 | 0.274 |
| 1988 | 1.045 | 0.274 |
| 1989 | 1.601 | 0.274 |
| 1990 | 1.308 | 0.274 |
| 1991 | 1.086 | 0.715 |
| 1992 | 1.789 | 0.976 |
| 1993 | 1.279 | 0.520 |
| 1994 | 0.625 | 0.274 |
| 1995 | 4.941 | 3.933 |
| 1996 | 3.055 | 1.088 |
| 1997 | 3.741 | 1.667 |
| 1998 | 2.434 | 1.916 |
| 1999 | 0.756 | 0.274 |
| 2000 | 1.868 | 1.204 |
| 2001 | 0.644 | 0.274 |
| 2002 | 0.579 | 0.274 |
| 2003 | 0.730 | 0.274 |
| 2004 | 1.341 | 0.910 |

## Ranked Annual Peaks

Ranked Annual Peaks for Pre-Project and Mitigated. POC #1

| Rank | Pre-Project | Mitigated |
|------|-------------|-----------|
| 1    | 4.9408      | 3.9327    |
| 2    | 4.6191      | 3.1989    |
| 3    | 3.7415      | 2.1449    |
| 4    | 3.0553      | 1.9158    |
| 5    | 2.8332      | 1.6669    |
| 6    | 2.7823      | 1.5249    |
| 7    | 2.4339      | 1.2138    |
| 8    | 2.3300      | 1.2039    |
| 9    | 2.2752      | 1.0885    |
| 10   | 1.8678      | 1.0593    |
| 11   | 1.7886      | 0.9937    |
| 12   | 1.6015      | 0.9759    |
| 13   | 1.4585      | 0.9101    |
| 14   | 1.3866      | 0.8431    |
| 15   | 1.3407      | 0.7911    |
| 16   | 1.3112      | 0.7151    |
| 17   | 1.3106      | 0.5376    |
| 18   | 1.3076      | 0.5204    |
| 19   | 1.2787      | 0.5043    |
| 20   | 1.2726      | 0.4349    |
| 21   | 1.2668      | 0.4209    |
| 22   | 1.1648      | 0.3166    |
| 23   | 1.1499      | 0.2946    |
| 24   | 1.0861      | 0.2742    |
| 25   | 1.0452      | 0.2742    |

|    |        |        |
|----|--------|--------|
| 26 | 0.9920 | 0.2742 |
| 27 | 0.9347 | 0.2742 |
| 28 | 0.7563 | 0.2742 |
| 29 | 0.7364 | 0.2742 |
| 30 | 0.7301 | 0.2742 |
| 31 | 0.6744 | 0.2742 |
| 32 | 0.6476 | 0.2742 |
| 33 | 0.6435 | 0.2742 |
| 34 | 0.6252 | 0.2742 |
| 35 | 0.5786 | 0.2742 |
| 36 | 0.5600 | 0.2742 |
| 37 | 0.5151 | 0.2742 |
| 38 | 0.2928 | 0.2742 |
| 39 | 0.2234 | 0.2742 |
| 40 | 0.0789 | 0.2742 |
| 41 | 0.0344 | 0.2741 |
| 42 | 0.0339 | 0.2741 |
| 43 | 0.0291 | 0.1929 |

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## Duration Flows

The Facility PASSED

| Flow(cfs) | Predev | Mit | Percentage | Pass/Fail |
|-----------|--------|-----|------------|-----------|
| 0.2912    | 941    | 368 | 39         | Pass      |
| 0.3181    | 864    | 338 | 39         | Pass      |
| 0.3450    | 780    | 312 | 40         | Pass      |
| 0.3719    | 722    | 279 | 38         | Pass      |
| 0.3988    | 660    | 264 | 40         | Pass      |
| 0.4257    | 614    | 239 | 38         | Pass      |
| 0.4526    | 574    | 228 | 39         | Pass      |
| 0.4795    | 529    | 212 | 40         | Pass      |
| 0.5064    | 475    | 202 | 42         | Pass      |
| 0.5333    | 443    | 189 | 42         | Pass      |
| 0.5602    | 411    | 183 | 44         | Pass      |
| 0.5871    | 365    | 178 | 48         | Pass      |
| 0.6140    | 339    | 167 | 49         | Pass      |
| 0.6409    | 314    | 159 | 50         | Pass      |
| 0.6678    | 290    | 153 | 52         | Pass      |
| 0.6947    | 268    | 142 | 52         | Pass      |
| 0.7216    | 246    | 128 | 52         | Pass      |
| 0.7485    | 230    | 123 | 53         | Pass      |
| 0.7754    | 210    | 112 | 53         | Pass      |
| 0.8023    | 199    | 108 | 54         | Pass      |
| 0.8292    | 184    | 103 | 55         | Pass      |
| 0.8561    | 171    | 100 | 58         | Pass      |
| 0.8830    | 160    | 93  | 58         | Pass      |
| 0.9099    | 148    | 87  | 58         | Pass      |
| 0.9368    | 138    | 82  | 59         | Pass      |
| 0.9637    | 127    | 77  | 60         | Pass      |
| 0.9906    | 122    | 68  | 55         | Pass      |
| 1.0175    | 114    | 62  | 54         | Pass      |
| 1.0444    | 108    | 61  | 56         | Pass      |
| 1.0713    | 105    | 57  | 54         | Pass      |
| 1.0982    | 95     | 50  | 52         | Pass      |
| 1.1251    | 90     | 44  | 48         | Pass      |
| 1.1520    | 85     | 43  | 50         | Pass      |
| 1.1789    | 83     | 42  | 50         | Pass      |
| 1.2058    | 77     | 38  | 49         | Pass      |
| 1.2327    | 72     | 37  | 51         | Pass      |
| 1.2596    | 70     | 35  | 50         | Pass      |
| 1.2865    | 64     | 34  | 53         | Pass      |
| 1.3134    | 61     | 32  | 52         | Pass      |
| 1.3403    | 54     | 29  | 53         | Pass      |
| 1.3672    | 50     | 26  | 52         | Pass      |
| 1.3941    | 48     | 24  | 50         | Pass      |
| 1.4210    | 46     | 22  | 47         | Pass      |
| 1.4479    | 46     | 20  | 43         | Pass      |
| 1.4748    | 45     | 20  | 44         | Pass      |
| 1.5017    | 40     | 19  | 47         | Pass      |
| 1.5286    | 39     | 18  | 46         | Pass      |
| 1.5555    | 36     | 17  | 47         | Pass      |
| 1.5824    | 36     | 16  | 44         | Pass      |
| 1.6093    | 31     | 16  | 51         | Pass      |
| 1.6362    | 30     | 16  | 53         | Pass      |
| 1.6631    | 29     | 16  | 55         | Pass      |
| 1.6900    | 27     | 15  | 55         | Pass      |

|        |    |    |    |      |
|--------|----|----|----|------|
| 1.7169 | 26 | 13 | 50 | Pass |
| 1.7438 | 24 | 13 | 54 | Pass |
| 1.7707 | 24 | 12 | 50 | Pass |
| 1.7976 | 23 | 11 | 47 | Pass |
| 1.8245 | 22 | 11 | 50 | Pass |
| 1.8514 | 22 | 10 | 45 | Pass |
| 1.8783 | 21 | 9  | 42 | Pass |
| 1.9052 | 21 | 9  | 42 | Pass |
| 1.9321 | 21 | 8  | 38 | Pass |
| 1.9590 | 21 | 8  | 38 | Pass |
| 1.9859 | 21 | 8  | 38 | Pass |
| 2.0128 | 21 | 8  | 38 | Pass |
| 2.0397 | 21 | 8  | 38 | Pass |
| 2.0666 | 21 | 8  | 38 | Pass |
| 2.0935 | 21 | 8  | 38 | Pass |
| 2.1204 | 21 | 8  | 38 | Pass |
| 2.1473 | 21 | 7  | 33 | Pass |
| 2.1742 | 20 | 7  | 35 | Pass |
| 2.2011 | 18 | 7  | 38 | Pass |
| 2.2280 | 18 | 7  | 38 | Pass |
| 2.2549 | 18 | 7  | 38 | Pass |
| 2.2818 | 17 | 7  | 41 | Pass |
| 2.3087 | 17 | 7  | 41 | Pass |
| 2.3356 | 15 | 7  | 46 | Pass |
| 2.3625 | 15 | 7  | 46 | Pass |
| 2.3894 | 15 | 7  | 46 | Pass |
| 2.4163 | 15 | 7  | 46 | Pass |
| 2.4432 | 13 | 5  | 38 | Pass |
| 2.4701 | 13 | 5  | 38 | Pass |
| 2.4970 | 13 | 5  | 38 | Pass |
| 2.5239 | 12 | 4  | 33 | Pass |
| 2.5508 | 12 | 4  | 33 | Pass |
| 2.5777 | 12 | 4  | 33 | Pass |
| 2.6046 | 12 | 4  | 33 | Pass |
| 2.6315 | 12 | 4  | 33 | Pass |
| 2.6584 | 12 | 4  | 33 | Pass |
| 2.6853 | 12 | 3  | 25 | Pass |
| 2.7122 | 12 | 3  | 25 | Pass |
| 2.7391 | 11 | 3  | 27 | Pass |
| 2.7660 | 11 | 3  | 27 | Pass |
| 2.7929 | 10 | 3  | 30 | Pass |
| 2.8198 | 10 | 3  | 30 | Pass |
| 2.8467 | 9  | 3  | 33 | Pass |
| 2.8736 | 9  | 3  | 33 | Pass |
| 2.9005 | 9  | 2  | 22 | Pass |
| 2.9274 | 8  | 2  | 25 | Pass |
| 2.9543 | 8  | 2  | 25 | Pass |

## Water Quality

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## *Model Default Modifications*

Total of 0 changes have been made.

### *PERLND Changes*

No PERLND changes have been made.

### *IMPLND Changes*

No IMPLND changes have been made.

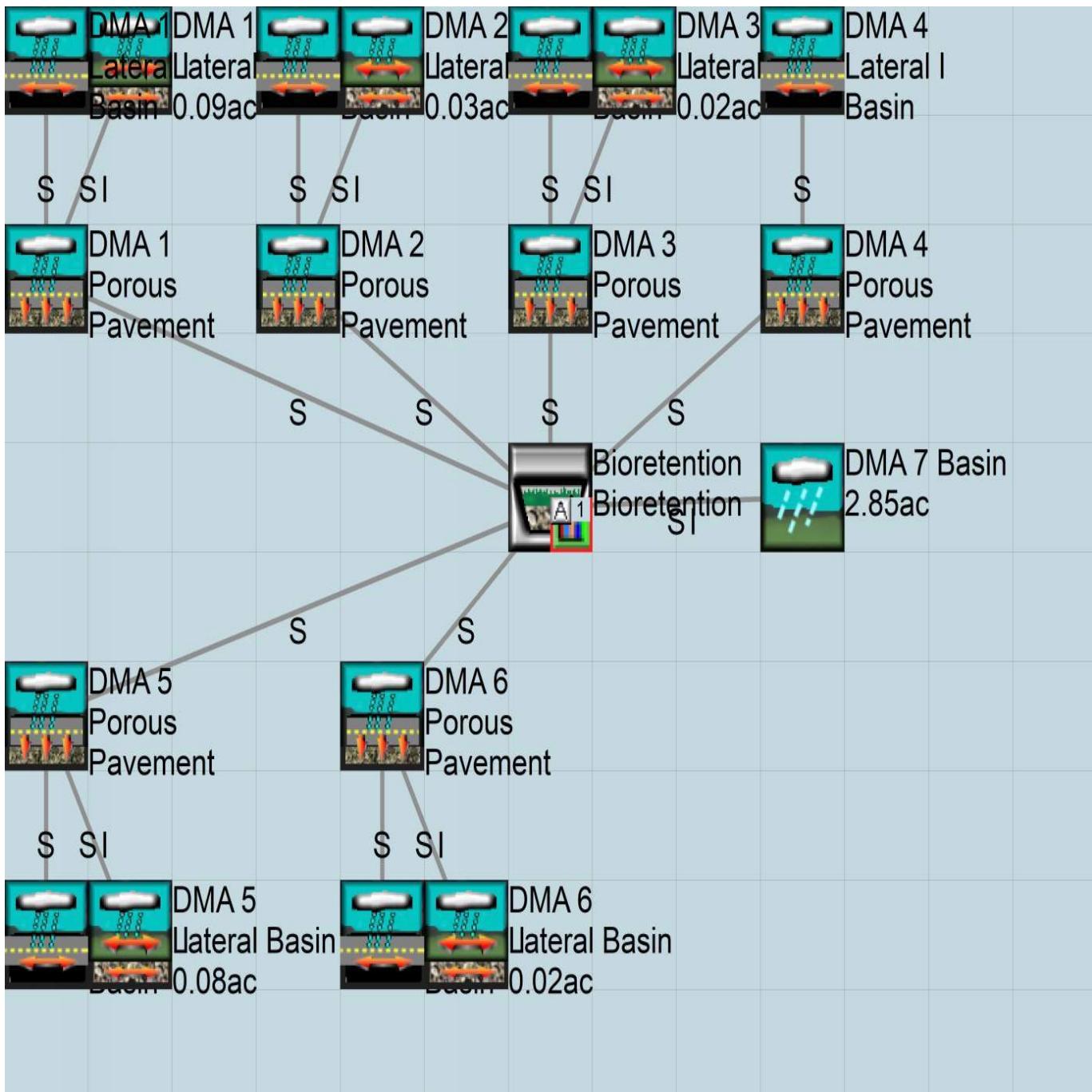
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## *Appendix*

### *Pre-Project Schematic*



## Mitigated Schematic



## Pre-Project UCI File

RUN

GLOBAL

WWHM4 model simulation  
START 1961 10 01 END 2004 09 30  
RUN INTERP OUTPUT LEVEL 3 0  
RESUME 0 RUN 1  
UNIT SYSTEM 1  
END GLOBAL

FILES

<File> <Un#> <-----File Name----->\*\*\*  
<-ID->  
WDM 26 Bradshaw & Jackson.wdm  
MESSU 25 PreBradshaw & Jackson.MES  
27 PreBradshaw & Jackson.L61  
28 PreBradshaw & Jackson.L62  
30 POCBradshaw & Jackson1.dat

END FILES

OPN SEQUENCE

INGRP INDELT 00:60  
PERLND 49  
IMPLND 1  
COPY 501  
DISPLAY 1

END INGRP

END OPN SEQUENCE

DISPLAY

DISPLAY-INFO1  
# - # <-----Title----->\*\*\*TRAN PIVL DIG1 FIL1 PYR DIG2 FIL2 YRND  
1 Basin 1 MAX 1 2 30 9

END DISPLAY-INFO1

END DISPLAY

COPY

TIMESERIES  
# - # NPT NMN \*\*\*  
1 1 1  
501 1 1

END TIMESERIES

END COPY

GENER

OPCODE  
# # OPCD \*\*\*

END OPCODE

PARM

# # K \*\*\*

END PARM

END GENER

PERLND

GEN-INFO  
<PLS ><-----Name----->NBLKS Unit-systems Printer \*\*\*  
# - # User t-series Engl Metr \*\*\*  
in out \*\*\*  
49 D,Grass,Flat(0-1%) 1 1 1 27 0

END GEN-INFO

\*\*\* Section PWATER\*\*\*

ACTIVITY

<PLS > \*\*\*\*\* Active Sections \*\*\*\*\*  
# - # ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC \*\*\*  
49 0 0 1 0 0 0 0 0 0 0 0 0 0

END ACTIVITY

PRINT-INFO

<PLS > \*\*\*\*\* Print-flags \*\*\*\*\* PIVL PYR  
# - # ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC \*\*\*\*\*  
49 0 0 4 0 0 0 0 0 0 0 0 0 1 9

END PRINT-INFO

```

PWAT-PARM1
<PLS > PWATER variable monthly parameter value flags ***
# - # CSNO RTOP UZFG VCS VUZ VNN VIFW VIRG VLE INFC HWT ***
49 0 0 0 1 0 0 0 0 1 0 0
END PWAT-PARM1

PWAT-PARM2
<PLS > PWATER input info: Part 2 ***
# - # ***FOREST LZSN INFILT LSUR SLSUR KVARY AGWRC
49 0 4.4 0.03 400 0.01 3 0.92
END PWAT-PARM2

PWAT-PARM3
<PLS > PWATER input info: Part 3 ***
# - # ***PETMAX PETMIN INFEXP INFILD DEEPFR BASETP AGWETP
49 40 35 2 2 0 0 0.05
END PWAT-PARM3
PWAT-PARM4
<PLS > PWATER input info: Part 4 ***
# - # CEPSC UZSN NSUR INTFW IRC LZETP ***
49 0 0.3 0.25 0.7 0.5 0
END PWAT-PARM4
MON-LZETPARM
<PLS > PWATER input info: Part 3 ***
# - # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC ***
49 0.4 0.4 0.4 0.45 0.5 0.55 0.55 0.55 0.55 0.55 0.45 0.4
END MON-LZETPARM
MON-INTERCEP
<PLS > PWATER input info: Part 3 ***
# - # JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC ***
49 0.12 0.12 0.12 0.11 0.1 0.1 0.1 0.1 0.1 0.1 0.11 0.12
END MON-INTERCEP

PWAT-STATE1
<PLS > *** Initial conditions at start of simulation
ran from 1990 to end of 1992 (pat 1-11-95) RUN 21 ***
# - # *** CEPS SURS UZS IFWS Lzs AGWS GWVS
49 0 0 0.15 0 4 0.05 0
END PWAT-STATE1

END PERLND

IMPLND
GEN-INFO
<PLS ><-----Name-----> Unit-systems Printer ***
# - # User t-series Engl Metr ***
in out ***
1 Imperv,Flat(0-1%) 1 1 1 27 0
END GEN-INFO
*** Section IWATER***

ACTIVITY
<PLS > ***** Active Sections *****
# - # ATMP SNOW IWAT SLD IWG IQAL ***
1 0 0 1 0 0 0
END ACTIVITY

PRINT-INFO
<PLS > ***** Print-flags ***** PIVL PYR
# - # ATMP SNOW IWAT SLD IWG IQAL *****
1 0 0 4 0 0 0 1 9
END PRINT-INFO

IWAT-PARM1
<PLS > IWATER variable monthly parameter value flags ***
# - # CSNO RTOP VRS VNN RTL1 ***
1 0 0 0 0
END IWAT-PARM1

```

```

IWAT-PARM2
<PLS >           IWATER input info: Part 2          ***
# - # *** LSUR      SLSUR      NSUR      RETSC
1             100        0.01      0.05      0.1
END IWAT-PARM2

IWAT-PARM3
<PLS >           IWATER input info: Part 3          ***
# - # *** PETMAX    PETMIN
1             0         0
END IWAT-PARM3

IWAT-STATE1
<PLS > *** Initial conditions at start of simulation
# - # *** RETS      SURS
1             0         0
END IWAT-STATE1

END IMPLND

SCHEMATIC
<-Source->          <-Area-->          <-Target->          MBLK      ***
<Name>   #          <-factor->          <Name>   #          Tbl#      ***
Basin 1***          PERLND   49          6.96      COPY      501      12
PERLND   49          PERLND   49          6.96      COPY      501      13
IMPLND   1           IMPLND   1           0.14      COPY      501      15

*****Routing*****
END SCHEMATIC

NETWORK
<-Volume-> <-Grp> <-Member-><-Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>   #          <Name>   # <-factor->strg <Name>   #   #          <Name>   # #      ***
COPY     501 OUTPUT MEAN 1 1 12.1          DISPLAY 1           INPUT   TIMSER 1

<-Volume-> <-Grp> <-Member-><-Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>   #          <Name>   # <-factor->strg <Name>   #   #          <Name>   # #      ***
END NETWORK

RCHRES
GEN-INFO
  RCHRES      Name       Nexists   Unit Systems   Printer      ***
  # - #-----><----> User T-series   Engl Metr LKFG      ***
                           in       out      ***
END GEN-INFO
*** Section RCHRES***

ACTIVITY
<PLS > **** Active Sections ****
# - # HYFG ADFG CNFG HTFG SDFG GQFG OXFG NUFG PKFG PHFG ***
END ACTIVITY

PRINT-INFO
<PLS > **** Print-flags **** PIVL  PYR
# - # HYDR ADCA CONS HEAT  SED  GQL OXRX NUTR PLNK PHCB PIVL  PYR  ****
END PRINT-INFO

HYDR-PARM1
  RCHRES  Flags for each HYDR Section      ***
  # - # VC A1 A2 A3 ODFVFG for each *** ODGTFG for each      FUNCT for each
      FG FG FG FG possible exit *** possible exit      possible exit      ***
      * * * * * * * * * * * * * * * * * * * * * * * * * * * *
END HYDR-PARM1

HYDR-PARM2
# - # FTABNO      LEN      DELTH      STCOR      KS      DB50      ***
<----><----><----><----><----><----><----><---->

```

```

END HYDR-PARM2
HYDR-INIT
  RCHRES Initial conditions for each HYDR section      ***
  # - # *** VOL    Initial value of COLIND      Initial value of OUTDGT
    *** ac-ft     for each possible exit      for each possible exit
<----><-----> <---><---><---><---> *** <---><---><---><---><--->
END HYDR-INIT
END RCHRES

SPEC-ACTIONS
END SPEC-ACTIONS
FTABLES
END FTABLES

EXT SOURCES
<-Volume-> <Member> SsysSgap<--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name> # <Name> # tem strg<-factor->strg <Name> # # <Name> # # ***
WDM      2 PREC      ENGL      0.944      PERLND      1 999 EXTNL      PREC
WDM      2 PREC      ENGL      0.944      IMPLND      1 999 EXTNL      PREC
WDM      1 EVAP      ENGL      0.85       PERLND      1 999 EXTNL      PETINP
WDM      1 EVAP      ENGL      0.85       IMPLND      1 999 EXTNL      PETINP

END EXT SOURCES

EXT TARGETS
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Volume-> <Member> Tsys Tgap Amd ***
<Name> # <Name> # #<-factor->strg <Name> # <Name> tem strg strg ***
COPY 501 OUTPUT MEAN 1 1 12.1 WDM 501 FLOW ENGL REPL
END EXT TARGETS

MASS-LINK
<Volume> <-Grp> <-Member-><--Mult--> <Target> <-Grp> <-Member->***
<Name> <Name> # #<-factor-> <Name> <Name> # # ***
  MASS-LINK 12
PERLND PWATER SURO 0.083333 COPY INPUT MEAN
  END MASS-LINK 12

  MASS-LINK 13
PERLND PWATER IFWO 0.083333 COPY INPUT MEAN
  END MASS-LINK 13

  MASS-LINK 15
IMPLND IWATER SURO 0.083333 COPY INPUT MEAN
  END MASS-LINK 15

END MASS-LINK

END RUN

```

## Mitigated UCI File

RUN

GLOBAL  
WWHM4 model simulation  
START 1961 10 01 END 2004 09 30  
RUN INTERP OUTPUT LEVEL 3 0  
RESUME 0 RUN 1  
UNIT SYSTEM 1  
END GLOBAL

FILES  
<File> <Un#> <-----File Name----->\*\*\*  
<-ID->  
WDM 26 Bradshaw & Jackson.wdm  
MESSU 25 MitBradshaw & Jackson.MES  
27 MitBradshaw & Jackson.L61  
28 MitBradshaw & Jackson.L62  
30 POCBradshaw & Jackson1.dat  
END FILES

OPN SEQUENCE  
INGRP INDELT 00:60  
PERLND 34  
IMPLND 1  
PERLND 66  
IMPLND 8  
IMPLND 9  
PERLND 67  
IMPLND 11  
PERLND 68  
IMPLND 13  
IMPLND 15  
PERLND 70  
IMPLND 17  
PERLND 71  
IMPLND 14  
RCHRES 1  
IMPLND 7  
RCHRES 2  
IMPLND 10  
RCHRES 3  
IMPLND 12  
RCHRES 4  
IMPLND 16  
RCHRES 5  
IMPLND 18  
RCHRES 6  
GENER 8  
RCHRES 7  
RCHRES 8  
COPY 1  
COPY 501  
DISPLAY 1  
END INGRP  
END OPN SEQUENCE  
DISPLAY  
DISPLAY-INFO1  
# - #-----Title----->\*\*\*TRAN PIVL DIG1 FIL1 PYR DIG2 FIL2 YRND  
1 Surface Bioretention MAX 1 2 30 9  
END DISPLAY-INFO1  
END DISPLAY  
COPY  
TIMESERIES  
# - # NPT NMN \*\*\*  
1 1 1  
501 1 1  
END TIMESERIES  
END COPY  
GENER

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```

OPCODE
#      # OPCODE ***
8          24
END OPCODE
PARM
#      #      K ***
8          0.
END PARM
END GENER
PERLND
GEN-INFO
<PLS ><-----Name----->NBLKS   Unit-systems   Printer ***
# - #
                   User   t-series Engl Metr ***
                   in     out   ***

34    C,Grass,Mod (1-2%)    1      1      1      27      0
66    C,Grass,Mod (1-2%)    1      1      1      27      0
67    C,Grass,Mod (1-2%)    1      1      1      27      0
68    C,Grass,Mod (1-2%)    1      1      1      27      0
70    C,Grass,Mod (1-2%)    1      1      1      27      0
71    C,Grass,Mod (1-2%)    1      1      1      27      0
END GEN-INFO
*** Section PWATER***

ACTIVITY
<PLS > ***** Active Sections *****
# - # ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC ***
34    0      0      1      0      0      0      0      0      0      0      0      0      0
66    0      0      1      0      0      0      0      0      0      0      0      0      0
67    0      0      1      0      0      0      0      0      0      0      0      0      0
68    0      0      1      0      0      0      0      0      0      0      0      0      0
70    0      0      1      0      0      0      0      0      0      0      0      0      0
71    0      0      1      0      0      0      0      0      0      0      0      0      0
END ACTIVITY
PRINT-INFO
<PLS > ***** Print-flags *****
# - # ATMP SNOW PWAT SED PST PWG PQAL MSTL PEST NITR PHOS TRAC PIVL PYR *****
34    0      0      4      0      0      0      0      0      0      0      0      0      0      1      9
66    0      0      4      0      0      0      0      0      0      0      0      0      0      1      9
67    0      0      4      0      0      0      0      0      0      0      0      0      0      1      9
68    0      0      4      0      0      0      0      0      0      0      0      0      0      1      9
70    0      0      4      0      0      0      0      0      0      0      0      0      0      1      9
71    0      0      4      0      0      0      0      0      0      0      0      0      0      1      9
END PRINT-INFO
PWAT-PARM1
<PLS > PWATER variable monthly parameter value flags ***
# - # CSNO RTOP UZFG VCS VUZ VNN VIFW VIRG VLE INF C HWT ***
34    0      0      0      1      0      0      0      0      1      0      0
66    0      0      0      1      0      0      0      0      1      0      0
67    0      0      0      1      0      0      0      0      1      0      0
68    0      0      0      1      0      0      0      0      1      0      0
70    0      0      0      1      0      0      0      0      1      0      0
71    0      0      0      1      0      0      0      0      1      0      0
END PWAT-PARM1
PWAT-PARM2
<PLS >      PWATER input info: Part 2      ***
# - # ***FOREST      LZSN      INFILT      LSUR      SLSUR      KVARY      AGWR C
34      0      4.45      0.043      400      0.02      3      0.92
66      0      4.45      0.043      400      0.02      3      0.92
67      0      4.45      0.043      400      0.02      3      0.92
68      0      4.45      0.043      400      0.02      3      0.92
70      0      4.45      0.043      400      0.02      3      0.92
71      0      4.45      0.043      400      0.02      3      0.92
END PWAT-PARM2
PWAT-PARM3
<PLS >      PWATER input info: Part 3      ***
# - # ***PETMAX      PETMIN      INFEXP      INFILD      DEEPFR      BASETP      AGWETP
```

```

34          40      35      2      2      0      0      0.05
66          40      35      2      2      0      0      0.05
67          40      35      2      2      0      0      0.05
68          40      35      2      2      0      0      0.05
70          40      35      2      2      0      0      0.05
71          40      35      2      2      0      0      0.05
END PWAT-PARM3
PWAT-PARM4
<PLS >    PWATER input info: Part 4
# - #     CEPSC     UZSN     NSUR     INTFW     IRC     LZETP ***
34          0       0.28    0.25    0.65    0.48    0
66          0       0.28    0.25    0.65    0.48    0
67          0       0.28    0.25    0.65    0.48    0
68          0       0.28    0.25    0.65    0.48    0
70          0       0.28    0.25    0.65    0.48    0
71          0       0.28    0.25    0.65    0.48    0
END PWAT-PARM4
MON-LZETPARM
<PLS >    PWATER input info: Part 3
# - #     JAN     FEB     MAR     APR     MAY     JUN     JUL     AUG     SEP     OCT     NOV     DEC ***
34          0.4    0.4    0.4    0.45   0.5    0.55   0.55   0.55   0.55   0.55   0.45   0.4
66          0.4    0.4    0.4    0.45   0.5    0.55   0.55   0.55   0.55   0.55   0.45   0.4
67          0.4    0.4    0.4    0.45   0.5    0.55   0.55   0.55   0.55   0.55   0.45   0.4
68          0.4    0.4    0.4    0.45   0.5    0.55   0.55   0.55   0.55   0.55   0.45   0.4
70          0.4    0.4    0.4    0.45   0.5    0.55   0.55   0.55   0.55   0.55   0.45   0.4
71          0.4    0.4    0.4    0.45   0.5    0.55   0.55   0.55   0.55   0.55   0.45   0.4
END MON-LZETPARM
MON-INTERCEP
<PLS >    PWATER input info: Part 3
# - #     JAN     FEB     MAR     APR     MAY     JUN     JUL     AUG     SEP     OCT     NOV     DEC ***
34          0.12   0.12   0.12   0.11   0.1    0.1    0.1    0.1    0.1    0.1    0.11   0.12
66          0.12   0.12   0.12   0.11   0.1    0.1    0.1    0.1    0.1    0.1    0.11   0.12
67          0.12   0.12   0.12   0.11   0.1    0.1    0.1    0.1    0.1    0.1    0.11   0.12
68          0.12   0.12   0.12   0.11   0.1    0.1    0.1    0.1    0.1    0.1    0.11   0.12
70          0.12   0.12   0.12   0.11   0.1    0.1    0.1    0.1    0.1    0.1    0.11   0.12
71          0.12   0.12   0.12   0.11   0.1    0.1    0.1    0.1    0.1    0.1    0.11   0.12
END MON-INTERCEP
PWAT-STATE1
<PLS > *** Initial conditions at start of simulation
           ran from 1990 to end of 1992 (pat 1-11-95) RUN 21 ***
# - # *** CEPS     SURS     UZS     IFWS     Lzs     AGWS     GWVS
34          0       0       0.15    0       4       0.05    0
66          0       0       0.15    0       4       0.05    0
67          0       0       0.15    0       4       0.05    0
68          0       0       0.15    0       4       0.05    0
70          0       0       0.15    0       4       0.05    0
71          0       0       0.15    0       4       0.05    0
END PWAT-STATE1
END PERLND
IMPLND
GEN-INFO
<PLS ><-----Name-----> Unit-systems  Printer ***
# - #             User   t-series   Engl   Metr   ***
                           in     out     ***

1  Imperv,Flat(0-1%)   1     1     1     27     0
8  Imperv,Flat(0-1%)   1     1     1     27     0
9  Imperv,Flat(0-1%)   1     1     1     27     0
11 Imperv,Flat(0-1%)   1     1     1     27     0
13 Imperv,Flat(0-1%)   1     1     1     27     0
15 Imperv,Flat(0-1%)   1     1     1     27     0
17 Imperv,Flat(0-1%)   1     1     1     27     0
14 Porous Pavement     1     1     1     27     0
7  Porous Pavement     1     1     1     27     0
10 Porous Pavement     1     1     1     27     0
12 Porous Pavement     1     1     1     27     0
16 Porous Pavement     1     1     1     27     0
18 Porous Pavement     1     1     1     27     0

```

END GEN-INFO

\*\*\* Section IWATER\*\*\*

ACTIVITY

<PLS > \*\*\*\*\* Active Sections \*\*\*\*\*

| # - # | ATMP | SNOW | IWAT | SLD | IWG | IQAL | *** |
|-------|------|------|------|-----|-----|------|-----|
| 1     | 0    | 0    | 1    | 0   | 0   | 0    |     |
| 8     | 0    | 0    | 1    | 0   | 0   | 0    |     |
| 9     | 0    | 0    | 1    | 0   | 0   | 0    |     |
| 11    | 0    | 0    | 1    | 0   | 0   | 0    |     |
| 13    | 0    | 0    | 1    | 0   | 0   | 0    |     |
| 15    | 0    | 0    | 1    | 0   | 0   | 0    |     |
| 17    | 0    | 0    | 1    | 0   | 0   | 0    |     |
| 14    | 0    | 0    | 1    | 0   | 0   | 0    |     |
| 7     | 0    | 0    | 1    | 0   | 0   | 0    |     |
| 10    | 0    | 0    | 1    | 0   | 0   | 0    |     |
| 12    | 0    | 0    | 1    | 0   | 0   | 0    |     |
| 16    | 0    | 0    | 1    | 0   | 0   | 0    |     |
| 18    | 0    | 0    | 1    | 0   | 0   | 0    |     |

END ACTIVITY

PRINT-INFO

<ILS > \*\*\*\*\* Print-flags \*\*\*\*\* PIVL PYR

| # - # | ATMP | SNOW | IWAT | SLD | IWG | IQAL | ***** | PIVL | PYR |
|-------|------|------|------|-----|-----|------|-------|------|-----|
| 1     | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |
| 8     | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |
| 9     | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |
| 11    | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |
| 13    | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |
| 15    | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |
| 17    | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |
| 14    | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |
| 7     | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |
| 10    | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |
| 12    | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |
| 16    | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |
| 18    | 0    | 0    | 4    | 0   | 0   | 0    |       | 1    | 9   |

END PRINT-INFO

IWAT-PARM1

<PLS > IWATER variable monthly parameter value flags \*\*\*

| # - # | CSNO | RTOP | VRS | VNN | RTL1 | *** |
|-------|------|------|-----|-----|------|-----|
| 1     | 0    | 0    | 0   | 0   | 0    |     |
| 8     | 0    | 0    | 0   | 0   | 0    |     |
| 9     | 0    | 0    | 0   | 0   | 0    |     |
| 11    | 0    | 0    | 0   | 0   | 0    |     |
| 13    | 0    | 0    | 0   | 0   | 0    |     |
| 15    | 0    | 0    | 0   | 0   | 0    |     |
| 17    | 0    | 0    | 0   | 0   | 0    |     |
| 14    | 0    | 0    | 0   | 0   | 0    |     |
| 7     | 0    | 0    | 0   | 0   | 0    |     |
| 10    | 0    | 0    | 0   | 0   | 0    |     |
| 12    | 0    | 0    | 0   | 0   | 0    |     |
| 16    | 0    | 0    | 0   | 0   | 0    |     |
| 18    | 0    | 0    | 0   | 0   | 0    |     |

END IWAT-PARM1

IWAT-PARM2

<PLS > IWATER input info: Part 2 \*\*\*

| # - # | *** | LSUR | SLSUR | NSUR | RETSC |
|-------|-----|------|-------|------|-------|
| 1     |     | 100  | 0.01  | 0.05 | 0.1   |
| 8     |     | 100  | 0.01  | 0.05 | 0.1   |
| 9     |     | 100  | 0.01  | 0.05 | 0.1   |
| 11    |     | 100  | 0.01  | 0.05 | 0.1   |
| 13    |     | 100  | 0.01  | 0.05 | 0.1   |
| 15    |     | 100  | 0.01  | 0.05 | 0.1   |
| 17    |     | 100  | 0.01  | 0.05 | 0.1   |
| 14    |     | 100  | 0.01  | 0.05 | 0.1   |
| 7     |     | 100  | 0.01  | 0.05 | 0.1   |
| 10    |     | 100  | 0.01  | 0.05 | 0.1   |

```

12          100      0.01      0.05      0.1
16          100      0.01      0.05      0.1
18          100      0.01      0.05      0.1
END IWAT-PARM2

```

```

IWAT-PARM3
<PLS >      IWATER input info: Part 3      ***
# - # ***PETMAX      PETMIN
1          0      0
8          0      0
9          0      0
11         0      0
13         0      0
15         0      0
17         0      0
14         0      0
7          0      0
10         0      0
12         0      0
16         0      0
18         0      0
END IWAT-PARM3

```

```

IWAT-STATE1
<PLS > *** Initial conditions at start of simulation
# - # *** RETS      SURS
1          0      0
8          0      0
9          0      0
11         0      0
13         0      0
15         0      0
17         0      0
14         0      0
7          0      0
10         0      0
12         0      0
16         0      0
18         0      0
END IWAT-STATE1

```

**DRAFT**

```
END IMPLND
```

| <-Source->               |    | <-Area-->  | <-Target-> | MBLK | ***  |     |
|--------------------------|----|------------|------------|------|------|-----|
| <Name>                   | #  | <-factor-> | <Name>     | #    | Tbl# | *** |
| DMA 7 Basin***           |    |            |            |      |      |     |
| PERLND                   | 34 | 1.66       | RCHRES     | 7    | 2    |     |
| PERLND                   | 34 | 1.66       | RCHRES     | 7    | 3    |     |
| IMPLND                   | 1  | 1.19       | RCHRES     | 7    | 5    |     |
| IMPLND                   | 7  | 0.375      | RCHRES     | 2    | 5    |     |
| DMA 1 Lateral Basin***   |    |            |            |      |      |     |
| PERLND                   | 66 | 0.24       | IMPLND     | 7    | 54   |     |
| PERLND                   | 66 | 0.24       | IMPLND     | 7    | 55   |     |
| DMA 1 Lateral I Basin*** |    |            |            |      |      |     |
| IMPLND                   | 8  | 0.7733     | IMPLND     | 7    | 53   |     |
| DMA 2 Lateral I Basin*** |    |            |            |      |      |     |
| IMPLND                   | 9  | 1.1244     | IMPLND     | 10   | 53   |     |
| DMA 2 Lateral Basin***   |    |            |            |      |      |     |
| PERLND                   | 67 | 0.075      | IMPLND     | 10   | 54   |     |
| PERLND                   | 67 | 0.075      | IMPLND     | 10   | 55   |     |
| IMPLND                   | 10 | 0.4002     | RCHRES     | 3    | 5    |     |
| DMA 3 Lateral I Basin*** |    |            |            |      |      |     |
| IMPLND                   | 11 | 0.6274     | IMPLND     | 12   | 53   |     |
| DMA 3 Lateral Basin***   |    |            |            |      |      |     |
| PERLND                   | 68 | 0.0251     | IMPLND     | 12   | 54   |     |
| PERLND                   | 68 | 0.0251     | IMPLND     | 12   | 55   |     |
| IMPLND                   | 12 | 0.7969     | RCHRES     | 4    | 5    |     |
| DMA 4 Lateral I Basin*** |    |            |            |      |      |     |
| IMPLND                   | 13 | 0.6355     | IMPLND     | 14   | 53   |     |

|                          |    |        |        |    |    |
|--------------------------|----|--------|--------|----|----|
| IMPLND                   | 14 | 0.3934 | RCHRES | 1  | 5  |
| DMA 5 Lateral Basin***   |    |        |        |    |    |
| PERLND                   | 70 | 0.2731 | IMPLND | 16 | 54 |
| PERLND                   | 70 | 0.2731 | IMPLND | 16 | 55 |
| DMA 5 Lateral I Basin*** |    |        |        |    |    |
| IMPLND                   | 15 | 0.6828 | IMPLND | 16 | 53 |
| IMPLND                   | 16 | 0.2929 | RCHRES | 5  | 5  |
| DMA 6 Lateral Basin***   |    |        |        |    |    |
| PERLND                   | 71 | 0.7533 | IMPLND | 18 | 54 |
| PERLND                   | 71 | 0.7533 | IMPLND | 18 | 55 |
| DMA 6 Lateral I Basin*** |    |        |        |    |    |
| IMPLND                   | 17 | 1.13   | IMPLND | 18 | 53 |
| IMPLND                   | 18 | 0.0265 | RCHRES | 6  | 5  |

\*\*\*\*\*Routing\*\*\*\*\*

|        |    |      |        |     |    |
|--------|----|------|--------|-----|----|
| PERLND | 34 | 1.66 | COPY   | 1   | 12 |
| IMPLND | 1  | 1.19 | COPY   | 1   | 15 |
| PERLND | 34 | 1.66 | COPY   | 1   | 13 |
| RCHRES | 7  | 1    | RCHRES | 8   | 8  |
| RCHRES | 2  | 1    | RCHRES | 7   | 6  |
| RCHRES | 2  |      | COPY   | 1   | 16 |
| RCHRES | 3  | 1    | RCHRES | 7   | 6  |
| RCHRES | 3  |      | COPY   | 1   | 16 |
| RCHRES | 4  | 1    | RCHRES | 7   | 6  |
| RCHRES | 4  |      | COPY   | 1   | 16 |
| RCHRES | 1  | 1    | RCHRES | 7   | 6  |
| RCHRES | 1  |      | COPY   | 1   | 16 |
| RCHRES | 5  | 1    | RCHRES | 7   | 6  |
| RCHRES | 5  |      | COPY   | 1   | 16 |
| RCHRES | 6  | 1    | RCHRES | 7   | 6  |
| RCHRES | 6  |      | COPY   | 1   | 16 |
| RCHRES | 8  | 1    | COPY   | 501 | 16 |
| RCHRES | 7  | 1    | COPY   | 501 | 17 |

END SCHEMATIC

NETWORK

|            |        |            |            |                |                |         |            |                |
|------------|--------|------------|------------|----------------|----------------|---------|------------|----------------|
| <-Volume-> | <-Grp> | <-Member-> | <--Mult--> | Tran           | <-Target vols> | <-Grp>  | <-Member-> | ***            |
| <Name>     | #      | <Name>     | #          | <-factor->strg | <Name>         | #       | #          | <Name> # # *** |
| COPY       | 501    | OUTPUT     | MEAN       | 1 1            | 12.1           | DISPLAY | 1          | INPUT TIMSER 1 |
| GENER      | 8      | OUTPUT     | TIMSER     | .0002778       |                | RCHRES  | 7          | EXTNL OUTDGT 1 |

|            |        |            |            |                |                |        |            |                |
|------------|--------|------------|------------|----------------|----------------|--------|------------|----------------|
| <-Volume-> | <-Grp> | <-Member-> | <--Mult--> | Tran           | <-Target vols> | <-Grp> | <-Member-> | ***            |
| <Name>     | #      | <Name>     | #          | <-factor->strg | <Name>         | #      | #          | <Name> # # *** |

END NETWORK

RCHRES

| GEN-INFO |              |                  |         |         |         |          |      |      |     |
|----------|--------------|------------------|---------|---------|---------|----------|------|------|-----|
| RCHRES   | Name         | Nexits           | Unit    | Systems | Printer | Engl     | Metr | LKFG | *** |
| #        | -            | #                | <-----> | <---->  | User    | T-series | in   | out  | *** |
| 1        | DMA 4        | Porous           | Pav-019 | 1       | 1       | 1        | 28   | 0    | 1   |
| 2        | DMA 1        | Porous           | Pav-008 | 1       | 1       | 1        | 28   | 0    | 1   |
| 3        | DMA 2        | Porous           | Pav-013 | 1       | 1       | 1        | 28   | 0    | 1   |
| 4        | DMA 3        | Porous           | Pav-016 | 1       | 1       | 1        | 28   | 0    | 1   |
| 5        | DMA 5        | Porous           | Pav-022 | 1       | 1       | 1        | 28   | 0    | 1   |
| 6        | DMA 6        | Porous           | Pav-025 | 1       | 1       | 1        | 28   | 0    | 1   |
| 7        | Surface      | Bioretention-006 |         | 2       | 1       | 1        | 28   | 0    | 1   |
| 8        | Bioretention | Bi-005           |         | 1       | 1       | 1        | 28   | 0    | 1   |

END GEN-INFO

\*\*\* Section RCHRES\*\*\*

ACTIVITY

| <PLS > ***** Active Sections ***** |   |   |      |      |      |      |      |      |      |      |      |      |     |
|------------------------------------|---|---|------|------|------|------|------|------|------|------|------|------|-----|
| #                                  | - | # | HYFG | ADFG | CNFG | HTFG | SDFG | GQFG | OXFG | NUFG | PKFG | PHFG | *** |
| 1                                  |   |   | 1    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |     |
| 2                                  |   |   | 1    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |     |
| 3                                  |   |   | 1    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |     |
| 4                                  |   |   | 1    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |     |

```

5      1   0   0   0   0   0   0   0   0   0
6      1   0   0   0   0   0   0   0   0   0
7      1   0   0   0   0   0   0   0   0   0
8      1   0   0   0   0   0   0   0   0   0
END ACTIVITY

PRINT-INFO
<PLS > **** Print-flags **** PIVL PYR ****
# - # HYDR ADCA CONS HEAT SED GQL OXRX NUTR PLNK PHCB PIVL PYR ****
1     4   0   0   0   0   0   0   0   0   0   0   1   9
2     4   0   0   0   0   0   0   0   0   0   0   1   9
3     4   0   0   0   0   0   0   0   0   0   0   1   9
4     4   0   0   0   0   0   0   0   0   0   0   1   9
5     4   0   0   0   0   0   0   0   0   0   0   1   9
6     4   0   0   0   0   0   0   0   0   0   0   1   9
7     4   0   0   0   0   0   0   0   0   0   0   1   9
8     4   0   0   0   0   0   0   0   0   0   0   1   9
END PRINT-INFO

HYDR-PARM1
RCHRES Flags for each HYDR Section
# - # VC A1 A2 A3 ODFVFG for each *** ODGTFG for each ***
          FG FG FG FG possible exit *** possible exit *** FUNCT for each
          * * * * * * * * * * * * * * * * possible exit ***
1     0 1 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 2 2 2 2 2
2     0 1 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 2 2 2 2 2
3     0 1 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 2 2 2 2 2
4     0 1 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 2 2 2 2 2
5     0 1 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 2 2 2 2 2
6     0 1 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 2 2 2 2 2
7     0 1 0 0 4 5 0 0 0 0 0 0 0 1 0 0 0 0 0 0 2 1 2 2 2
8     0 1 0 0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 2 2 2 2 2
END HYDR-PARM1

HYDR-PARM2
# - # FTABNO LEN DELTH STCOR KS DB50 ***
<----><----><----><----><----><----><----><----> ****
1     1    0.1   0.0   0.0   0.5   0.0
2     2    0.03   0.0   0.0   0.5   0.0
3     3    0.08   0.0   0.0   0.5   0.0
4     4    0.09   0.0   0.0   0.5   0.0
5     5    0.06   0.0   0.0   0.5   0.0
6     6    0.01   0.0   0.0   0.5   0.0
7     7    0.01   0.0   0.0   0.0   0.0
8     8    0.13   0.0   0.0   0.0   0.0
END HYDR-PARM2

HYDR-INIT
RCHRES Initial conditions for each HYDR section
# - # *** VOL Initial value of COLIND Initial value of OUTDGT
      *** ac-ft for each possible exit for each possible exit
<----><----> <----><----><----><----> *** <----><----><----><---->
1     0     4.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
2     0     4.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
3     0     4.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
4     0     4.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
5     0     4.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
6     0     4.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
7     0     4.0   5.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
8     0     4.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0   0.0
END HYDR-INIT
END RCHRES

SPEC-ACTIONS
*** User-Defined Variable Quantity Lines
***           addr
***           <---->
*** kwd varnam optyp opn vari s1 s2 s3 tp multiply lc ls ac as agfn ***
<****> <----> <----> <-> <----><-><-><-><----> <><-> <><-> <-> ***
UVQUAN vol8    RCHRES    8 VOL        4
UVQUAN v2m8    GLOBAL    WORKSP    7      3

```

```

UVQUAN vpo8    GLOBAL      WORKSP  8      3
UVQUAN v2d8    GENER     8 K      1      3
*** User-Defined Target Variable Names
***           addr or           addr or
***           <----->           <----->
*** kwd   varnam ct  vari  s1 s2 s3  frac oper
<****> <----><-> <----><-><-><-> <---> <->
UVNAME v2m8     1 WORKSP  7      1.0 QUAN
UVNAME vpo8     1 WORKSP  8      1.0 QUAN
UVNAME v2d8     1 K      1      1.0 QUAN
*** opt foplop dcdts yr mo dy hr mn d t  vnam  s1 s2 s3 ac quantity  tc  ts rp
<****><-><-><-><-> <> <> <><><> <----><-><-><-><-><-> <> <-><->
GENER 8          vpo8           =  v2m8
GENER 8          vpo8           =  vol8
*** Compute remaining available pore space
GENER 8          vpo8           =  v2m8
GENER 8          vpo8           =  vol8
*** Check to see if VPORA goes negative; if so set VPORA = 0.0
IF (vpo8 < 0.0) THEN
  GENER 8          vpo8           =  0.0
END IF
*** Infiltration volume
GENER 8          v2d8           =  vpo8
END SPEC-ACTIONS
FTABLES
FTABLE     8
 60 4
  Depth      Area      Volume  Outflow1 Velocity  Travel Time***  

  (ft)      (acres) (acre-ft) (cfs)   (ft/sec)   (Minutes)***  

0.000000  0.371212  0.000000  0.000000  

0.046703  0.367466  0.002316  0.000000  

0.093407  0.363220  0.004711  0.000000  

0.140110  0.358974  0.007186  0.000000  

0.186813  0.354729  0.009741  0.000000  

0.233516  0.350483  0.012375  0.000000  

0.280220  0.346237  0.015089  0.000000  

0.326923  0.341991  0.017883  0.000000  

0.373626  0.337746  0.020757  0.000000  

0.420330  0.333500  0.023710  0.000000  

0.467033  0.329254  0.026743  0.000000  

0.513736  0.325008  0.029995  0.000000  

0.560440  0.320763  0.033330  0.000000  

0.607143  0.316517  0.036749  0.000000  

0.653846  0.312271  0.040251  0.000000  

0.700549  0.308025  0.043836  0.000000  

0.747253  0.303780  0.047505  0.000000  

0.793956  0.299534  0.051256  0.000000  

0.840659  0.295288  0.055091  0.000000  

0.887363  0.291042  0.059010  0.000000  

0.934066  0.286797  0.063011  0.000000  

0.980769  0.282551  0.067096  0.000000  

1.027473  0.278305  0.071265  0.000000  

1.074176  0.274059  0.075516  0.000000  

1.120879  0.269814  0.079851  0.000000  

1.167582  0.265568  0.084269  0.000000  

1.214286  0.261322  0.088770  0.000000  

1.260989  0.257076  0.093355  0.000000  

1.307692  0.252831  0.098023  0.000000  

1.354396  0.248585  0.102774  0.000000  

1.401099  0.244339  0.107608  0.000000  

1.447802  0.240093  0.112526  0.000000  

1.494505  0.235847  0.117527  0.000000  

1.541209  0.231602  0.122611  0.000000  

1.587912  0.227356  0.127779  0.000000  

1.634615  0.223110  0.133030  0.000000  

1.681319  0.218864  0.138364  0.000000  

1.728022  0.214619  0.143781  0.000000  

1.774725  0.210373  0.149282  0.000000  

1.821429  0.206127  0.154866  0.000000  

1.868132  0.201881  0.160533  0.000000  

1.914835  0.197636  0.166284  0.000000

```

|          |          |          |          |
|----------|----------|----------|----------|
| 1.961538 | 0.193390 | 0.172118 | 0.000000 |
| 2.008242 | 0.189144 | 0.177964 | 0.000000 |
| 2.054945 | 0.184898 | 0.183893 | 0.000000 |
| 2.101648 | 0.180653 | 0.189904 | 0.000000 |
| 2.148352 | 0.176407 | 0.195998 | 0.013558 |
| 2.195055 | 0.172161 | 0.202174 | 0.020337 |
| 2.241758 | 0.167915 | 0.208432 | 0.036097 |
| 2.288462 | 0.163670 | 0.214772 | 0.043977 |
| 2.335165 | 0.159424 | 0.221195 | 0.056061 |
| 2.381868 | 0.155178 | 0.227700 | 0.062103 |
| 2.428571 | 0.150932 | 0.234287 | 0.065124 |
| 2.475275 | 0.146687 | 0.240957 | 0.066635 |
| 2.521978 | 0.142441 | 0.247709 | 0.072494 |
| 2.568681 | 0.138195 | 0.254543 | 0.086386 |
| 2.615385 | 0.133949 | 0.261459 | 0.102319 |
| 2.662088 | 0.129704 | 0.268458 | 0.118122 |
| 2.708791 | 0.125458 | 0.275539 | 0.133139 |
| 2.750000 | 0.121212 | 0.317906 | 0.436211 |

END FTABLE 8  
FTABLE 7

34 5

| Depth<br>(ft) | Area<br>(acres) | Volume<br>(acre-ft) | Outflow1<br>(cfs) | Outflow2<br>(cfs) | Velocity<br>(ft/sec) | Travel Time***<br>(Minutes)*** |
|---------------|-----------------|---------------------|-------------------|-------------------|----------------------|--------------------------------|
| 0.000000      | 0.121212        | 0.000000            | 0.000000          | 0.000000          |                      |                                |
| 0.046703      | 0.375458        | 0.017436            | 0.000000          | 0.287752          |                      |                                |
| 0.093407      | 0.379704        | 0.035070            | 0.000000          | 0.341508          |                      |                                |
| 0.140110      | 0.383949        | 0.052903            | 0.000000          | 0.368385          |                      |                                |
| 0.186813      | 0.388195        | 0.070934            | 0.000000          | 0.395263          |                      |                                |
| 0.233516      | 0.392441        | 0.089163            | 0.000000          | 0.422141          |                      |                                |
| 0.280220      | 0.396687        | 0.107590            | 0.000000          | 0.449019          |                      |                                |
| 0.326923      | 0.400932        | 0.126216            | 0.000000          | 0.475897          |                      |                                |
| 0.373626      | 0.405178        | 0.145040            | 0.000000          | 0.502775          |                      |                                |
| 0.420330      | 0.409424        | 0.164062            | 0.000000          | 0.529653          |                      |                                |
| 0.467033      | 0.413670        | 0.183283            | 0.000000          | 0.556531          |                      |                                |
| 0.513736      | 0.417915        | 0.202702            | 0.000000          | 0.583409          |                      |                                |
| 0.560440      | 0.422161        | 0.222319            | 0.000000          | 0.610287          |                      |                                |
| 0.607143      | 0.426407        | 0.242134            | 0.000000          | 0.637165          |                      |                                |
| 0.653846      | 0.430653        | 0.262148            | 0.000000          | 0.664043          |                      |                                |
| 0.700549      | 0.434898        | 0.282360            | 0.000000          | 0.690920          |                      |                                |
| 0.747253      | 0.439144        | 0.302770            | 0.000000          | 0.717798          |                      |                                |
| 0.793956      | 0.443390        | 0.323379            | 0.000000          | 0.744676          |                      |                                |
| 0.840659      | 0.447636        | 0.344186            | 0.000000          | 0.771554          |                      |                                |
| 0.887363      | 0.451881        | 0.365191            | 0.000000          | 0.798432          |                      |                                |
| 0.934066      | 0.456127        | 0.386395            | 0.000000          | 0.825310          |                      |                                |
| 0.980769      | 0.460373        | 0.407797            | 0.000000          | 0.852188          |                      |                                |
| 1.027473      | 0.464619        | 0.429397            | 0.145022          | 0.879066          |                      |                                |
| 1.074176      | 0.468864        | 0.451195            | 0.642943          | 0.905944          |                      |                                |
| 1.120879      | 0.473110        | 0.473192            | 1.336713          | 0.932822          |                      |                                |
| 1.167582      | 0.477356        | 0.495387            | 2.180380          | 0.959700          |                      |                                |
| 1.214286      | 0.481602        | 0.517780            | 3.149312          | 0.986577          |                      |                                |
| 1.260989      | 0.485847        | 0.540371            | 4.226429          | 1.013455          |                      |                                |
| 1.307692      | 0.490093        | 0.563161            | 5.398013          | 1.040333          |                      |                                |
| 1.354396      | 0.494339        | 0.586149            | 6.651932          | 1.067211          |                      |                                |
| 1.401099      | 0.498585        | 0.609336            | 7.976750          | 1.094089          |                      |                                |
| 1.447802      | 0.502831        | 0.632720            | 9.361249          | 1.120967          |                      |                                |
| 1.494505      | 0.507076        | 0.656303            | 10.79418          | 1.147845          |                      |                                |
| 1.500000      | 0.507576        | 0.659091            | 12.26414          | 1.151007          |                      |                                |

END FTABLE 7  
FTABLE 2

91 4

| Depth<br>(ft) | Area<br>(acres) | Volume<br>(acre-ft) | Outflow1<br>(cfs) | Velocity<br>(ft/sec) | Travel Time***<br>(Minutes)*** |
|---------------|-----------------|---------------------|-------------------|----------------------|--------------------------------|
| 0.000000      | 0.375000        | 0.000000            | 0.000000          |                      |                                |
| 0.020333      | 0.375000        | 0.002669            | 0.061913          |                      |                                |
| 0.040667      | 0.375000        | 0.005338            | 0.087558          |                      |                                |
| 0.061000      | 0.375000        | 0.008006            | 0.107237          |                      |                                |
| 0.081333      | 0.375000        | 0.010675            | 0.123826          |                      |                                |
| 0.101667      | 0.375000        | 0.013344            | 0.138442          |                      |                                |
| 0.122000      | 0.375000        | 0.016013            | 0.151656          |                      |                                |
| 0.142333      | 0.375000        | 0.018681            | 0.163807          |                      |                                |

|          |          |          |          |
|----------|----------|----------|----------|
| 0.162667 | 0.375000 | 0.021350 | 0.175117 |
| 0.183000 | 0.375000 | 0.024019 | 0.185739 |
| 0.203333 | 0.375000 | 0.026688 | 0.195787 |
| 0.223667 | 0.375000 | 0.029356 | 0.205343 |
| 0.244000 | 0.375000 | 0.032025 | 0.214473 |
| 0.264333 | 0.375000 | 0.034694 | 0.223231 |
| 0.284667 | 0.375000 | 0.037363 | 0.231658 |
| 0.305000 | 0.375000 | 0.040031 | 0.239789 |
| 0.325333 | 0.375000 | 0.042700 | 0.247653 |
| 0.345667 | 0.375000 | 0.045369 | 0.255275 |
| 0.366000 | 0.375000 | 0.048038 | 0.262675 |
| 0.386333 | 0.375000 | 0.050706 | 0.269873 |
| 0.406667 | 0.375000 | 0.053375 | 0.276884 |
| 0.427000 | 0.375000 | 0.056044 | 0.283722 |
| 0.447333 | 0.375000 | 0.058713 | 0.290398 |
| 0.467667 | 0.375000 | 0.061381 | 0.296925 |
| 0.488000 | 0.375000 | 0.064050 | 0.303311 |
| 0.508333 | 0.375000 | 0.066719 | 0.309566 |
| 0.528667 | 0.375000 | 0.069388 | 0.315696 |
| 0.549000 | 0.375000 | 0.072056 | 0.321710 |
| 0.569333 | 0.375000 | 0.074725 | 0.327614 |
| 0.589667 | 0.375000 | 0.077394 | 0.333413 |
| 0.610000 | 0.375000 | 0.080063 | 0.339112 |
| 0.630333 | 0.375000 | 0.082731 | 0.344718 |
| 0.650667 | 0.375000 | 0.085400 | 0.350234 |
| 0.671000 | 0.375000 | 0.088069 | 0.355664 |
| 0.691333 | 0.375000 | 0.090738 | 0.361013 |
| 0.711667 | 0.375000 | 0.093406 | 0.366283 |
| 0.732000 | 0.375000 | 0.096075 | 0.371479 |
| 0.752333 | 0.375000 | 0.098744 | 0.376603 |
| 0.772667 | 0.375000 | 0.101413 | 0.381658 |
| 0.793000 | 0.375000 | 0.104081 | 0.386648 |
| 0.813333 | 0.375000 | 0.106750 | 0.391573 |
| 0.833667 | 0.375000 | 0.109419 | 0.396438 |
| 0.854000 | 0.375000 | 0.112088 | 0.401243 |
| 0.874333 | 0.375000 | 0.114756 | 0.405992 |
| 0.894667 | 0.375000 | 0.117425 | 0.410685 |
| 0.915000 | 0.375000 | 0.120094 | 0.415326 |
| 0.935333 | 0.375000 | 0.122763 | 0.419916 |
| 0.955667 | 0.375000 | 0.125431 | 0.424455 |
| 0.976000 | 0.375000 | 0.128100 | 0.428947 |
| 0.996333 | 0.375000 | 0.130769 | 0.433392 |
| 1.016667 | 0.375000 | 0.133438 | 0.437792 |
| 1.037000 | 0.375000 | 0.136106 | 0.442148 |
| 1.057333 | 0.375000 | 0.138775 | 0.446462 |
| 1.077667 | 0.375000 | 0.141444 | 0.450735 |
| 1.098000 | 0.375000 | 0.144113 | 0.454967 |
| 1.118333 | 0.375000 | 0.146781 | 0.459160 |
| 1.138667 | 0.375000 | 0.149450 | 0.463316 |
| 1.159000 | 0.375000 | 0.152119 | 0.467434 |
| 1.179333 | 0.375000 | 0.154788 | 0.471517 |
| 1.199667 | 0.375000 | 0.157456 | 0.475564 |
| 1.220000 | 0.375000 | 0.160125 | 0.479577 |
| 1.240333 | 0.375000 | 0.162794 | 0.483557 |
| 1.260667 | 0.375000 | 0.165463 | 0.487505 |
| 1.281000 | 0.375000 | 0.168131 | 0.491421 |
| 1.301333 | 0.375000 | 0.170800 | 0.495305 |
| 1.321667 | 0.375000 | 0.173469 | 0.499160 |
| 1.342000 | 0.375000 | 0.176138 | 0.502985 |
| 1.362333 | 0.375000 | 0.178806 | 0.506781 |
| 1.382667 | 0.375000 | 0.181475 | 0.510549 |
| 1.403000 | 0.375000 | 0.184144 | 0.514289 |
| 1.423333 | 0.375000 | 0.186813 | 0.518003 |
| 1.443667 | 0.375000 | 0.189481 | 0.521690 |
| 1.464000 | 0.375000 | 0.192150 | 0.525351 |
| 1.484333 | 0.375000 | 0.194819 | 0.528986 |
| 1.504667 | 0.375000 | 0.197488 | 0.532597 |
| 1.525000 | 0.375000 | 0.200156 | 0.536184 |
| 1.545333 | 0.375000 | 0.202825 | 0.539746 |
| 1.565667 | 0.375000 | 0.205494 | 0.543286 |

| 1.586000      | 0.375000        | 0.213119            | 0.546802          |                      |                                |
|---------------|-----------------|---------------------|-------------------|----------------------|--------------------------------|
| 1.606333      | 0.375000        | 0.220744            | 0.550296          |                      |                                |
| 1.626667      | 0.375000        | 0.228369            | 0.553768          |                      |                                |
| 1.647000      | 0.375000        | 0.235994            | 0.557218          |                      |                                |
| 1.667333      | 0.375000        | 0.243619            | 0.560648          |                      |                                |
| 1.687667      | 0.375000        | 0.251244            | 0.564056          |                      |                                |
| 1.708000      | 0.375000        | 0.258869            | 0.567444          |                      |                                |
| 1.728333      | 0.375000        | 0.266494            | 0.570811          |                      |                                |
| 1.748667      | 0.375000        | 0.274119            | 0.574159          |                      |                                |
| 1.769000      | 0.375000        | 0.281744            | 0.577488          |                      |                                |
| 1.789333      | 0.375000        | 0.289369            | 0.580797          |                      |                                |
| 1.809667      | 0.375000        | 0.296994            | 0.584088          |                      |                                |
| 1.830000      | 0.375000        | 0.304619            | 0.587360          |                      |                                |
| END FTABLE    | 2               |                     |                   |                      |                                |
| FTABLE        | 3               |                     |                   |                      |                                |
| 91            | 4               |                     |                   |                      |                                |
| Depth<br>(ft) | Area<br>(acres) | Volume<br>(acre-ft) | Outflow1<br>(cfs) | Velocity<br>(ft/sec) | Travel Time***<br>(Minutes)*** |
| 0.000000      | 0.400218        | 0.000000            | 0.000000          |                      |                                |
| 0.020333      | 0.400218        | 0.002848            | 0.061913          |                      |                                |
| 0.040667      | 0.400218        | 0.005696            | 0.087558          |                      |                                |
| 0.061000      | 0.400218        | 0.008545            | 0.107237          |                      |                                |
| 0.081333      | 0.400218        | 0.011393            | 0.123826          |                      |                                |
| 0.101667      | 0.400218        | 0.014241            | 0.138442          |                      |                                |
| 0.122000      | 0.400218        | 0.017089            | 0.151656          |                      |                                |
| 0.142333      | 0.400218        | 0.019938            | 0.163807          |                      |                                |
| 0.162667      | 0.400218        | 0.022786            | 0.175117          |                      |                                |
| 0.183000      | 0.400218        | 0.025634            | 0.185739          |                      |                                |
| 0.203333      | 0.400218        | 0.028482            | 0.195787          |                      |                                |
| 0.223667      | 0.400218        | 0.031330            | 0.205343          |                      |                                |
| 0.244000      | 0.400218        | 0.034179            | 0.214473          |                      |                                |
| 0.264333      | 0.400218        | 0.037027            | 0.223231          |                      |                                |
| 0.284667      | 0.400218        | 0.039875            | 0.231658          |                      |                                |
| 0.305000      | 0.400218        | 0.042723            | 0.239789          |                      |                                |
| 0.325333      | 0.400218        | 0.045572            | 0.247653          |                      |                                |
| 0.345667      | 0.400218        | 0.048420            | 0.255275          |                      |                                |
| 0.366000      | 0.400218        | 0.051268            | 0.262675          |                      |                                |
| 0.386333      | 0.400218        | 0.054116            | 0.269873          |                      |                                |
| 0.406667      | 0.400218        | 0.056964            | 0.276884          |                      |                                |
| 0.427000      | 0.400218        | 0.059813            | 0.283722          |                      |                                |
| 0.447333      | 0.400218        | 0.062661            | 0.290398          |                      |                                |
| 0.467667      | 0.400218        | 0.065509            | 0.296925          |                      |                                |
| 0.488000      | 0.400218        | 0.068357            | 0.303311          |                      |                                |
| 0.508333      | 0.400218        | 0.071205            | 0.309566          |                      |                                |
| 0.528667      | 0.400218        | 0.074054            | 0.315696          |                      |                                |
| 0.549000      | 0.400218        | 0.076902            | 0.321710          |                      |                                |
| 0.569333      | 0.400218        | 0.079750            | 0.327614          |                      |                                |
| 0.589667      | 0.400218        | 0.082598            | 0.333413          |                      |                                |
| 0.610000      | 0.400218        | 0.085447            | 0.339112          |                      |                                |
| 0.630333      | 0.400218        | 0.088295            | 0.344718          |                      |                                |
| 0.650667      | 0.400218        | 0.091143            | 0.350234          |                      |                                |
| 0.671000      | 0.400218        | 0.093991            | 0.355664          |                      |                                |
| 0.691333      | 0.400218        | 0.096839            | 0.361013          |                      |                                |
| 0.711667      | 0.400218        | 0.099688            | 0.366283          |                      |                                |
| 0.732000      | 0.400218        | 0.102536            | 0.371479          |                      |                                |
| 0.752333      | 0.400218        | 0.105384            | 0.376603          |                      |                                |
| 0.772667      | 0.400218        | 0.108232            | 0.381658          |                      |                                |
| 0.793000      | 0.400218        | 0.111081            | 0.386648          |                      |                                |
| 0.813333      | 0.400218        | 0.113929            | 0.391573          |                      |                                |
| 0.833667      | 0.400218        | 0.116777            | 0.396438          |                      |                                |
| 0.854000      | 0.400218        | 0.119625            | 0.401243          |                      |                                |
| 0.874333      | 0.400218        | 0.122473            | 0.405992          |                      |                                |
| 0.894667      | 0.400218        | 0.125322            | 0.410685          |                      |                                |
| 0.915000      | 0.400218        | 0.128170            | 0.415326          |                      |                                |
| 0.935333      | 0.400218        | 0.131018            | 0.419916          |                      |                                |
| 0.955667      | 0.400218        | 0.133866            | 0.424455          |                      |                                |
| 0.976000      | 0.400218        | 0.136715            | 0.428947          |                      |                                |
| 0.996333      | 0.400218        | 0.139563            | 0.433392          |                      |                                |
| 1.016667      | 0.400218        | 0.142411            | 0.437792          |                      |                                |
| 1.037000      | 0.400218        | 0.145259            | 0.442148          |                      |                                |

|          |          |          |          |
|----------|----------|----------|----------|
| 1.057333 | 0.400218 | 0.148107 | 0.446462 |
| 1.077667 | 0.400218 | 0.150956 | 0.450735 |
| 1.098000 | 0.400218 | 0.153804 | 0.454967 |
| 1.118333 | 0.400218 | 0.156652 | 0.459160 |
| 1.138667 | 0.400218 | 0.159500 | 0.463316 |
| 1.159000 | 0.400218 | 0.162349 | 0.467434 |
| 1.179333 | 0.400218 | 0.165197 | 0.471517 |
| 1.199667 | 0.400218 | 0.168045 | 0.475564 |
| 1.220000 | 0.400218 | 0.170893 | 0.479577 |
| 1.240333 | 0.400218 | 0.173741 | 0.483557 |
| 1.260667 | 0.400218 | 0.176590 | 0.487505 |
| 1.281000 | 0.400218 | 0.179438 | 0.491421 |
| 1.301333 | 0.400218 | 0.182286 | 0.495305 |
| 1.321667 | 0.400218 | 0.185134 | 0.499160 |
| 1.342000 | 0.400218 | 0.187982 | 0.502985 |
| 1.362333 | 0.400218 | 0.190831 | 0.506781 |
| 1.382667 | 0.400218 | 0.193679 | 0.510549 |
| 1.403000 | 0.400218 | 0.196527 | 0.514289 |
| 1.423333 | 0.400218 | 0.199375 | 0.518003 |
| 1.443667 | 0.400218 | 0.202224 | 0.521690 |
| 1.464000 | 0.400218 | 0.205072 | 0.525351 |
| 1.484333 | 0.400218 | 0.207920 | 0.528986 |
| 1.504667 | 0.400218 | 0.210768 | 0.532597 |
| 1.525000 | 0.400218 | 0.213616 | 0.536184 |
| 1.545333 | 0.400218 | 0.216465 | 0.539746 |
| 1.565667 | 0.400218 | 0.219313 | 0.543286 |
| 1.586000 | 0.400218 | 0.227451 | 0.546802 |
| 1.606333 | 0.400218 | 0.235588 | 0.550296 |
| 1.626667 | 0.400218 | 0.243726 | 0.553768 |
| 1.647000 | 0.400218 | 0.251864 | 0.557218 |
| 1.667333 | 0.400218 | 0.260002 | 0.560648 |
| 1.687667 | 0.400218 | 0.268140 | 0.564056 |
| 1.708000 | 0.400218 | 0.276277 | 0.567444 |
| 1.728333 | 0.400218 | 0.284415 | 0.570811 |
| 1.748667 | 0.400218 | 0.292553 | 0.574159 |
| 1.769000 | 0.400218 | 0.300691 | 0.577488 |
| 1.789333 | 0.400218 | 0.308828 | 0.580797 |
| 1.809667 | 0.400218 | 0.316966 | 0.584088 |
| 1.830000 | 0.400218 | 0.325104 | 0.587360 |

END FTABLE 3  
FTABLE 4

| 91       | 4        | Depth    | Area     | Volume    | Outflow1 | Velocity | Travel Time*** |
|----------|----------|----------|----------|-----------|----------|----------|----------------|
|          |          | (ft)     | (acres)  | (acre-ft) | (cfs)    | (ft/sec) | (Minutes)***   |
| 0.000000 | 0.796907 | 0.000000 | 0.000000 |           |          |          |                |
| 0.020333 | 0.796907 | 0.005671 | 0.061913 |           |          |          |                |
| 0.040667 | 0.796907 | 0.011343 | 0.087558 |           |          |          |                |
| 0.061000 | 0.796907 | 0.017014 | 0.107237 |           |          |          |                |
| 0.081333 | 0.796907 | 0.022685 | 0.123826 |           |          |          |                |
| 0.101667 | 0.796907 | 0.028357 | 0.138442 |           |          |          |                |
| 0.122000 | 0.796907 | 0.034028 | 0.151656 |           |          |          |                |
| 0.142333 | 0.796907 | 0.039699 | 0.163807 |           |          |          |                |
| 0.162667 | 0.796907 | 0.045371 | 0.175117 |           |          |          |                |
| 0.183000 | 0.796907 | 0.051042 | 0.185739 |           |          |          |                |
| 0.203333 | 0.796907 | 0.056713 | 0.195787 |           |          |          |                |
| 0.223667 | 0.796907 | 0.062385 | 0.205343 |           |          |          |                |
| 0.244000 | 0.796907 | 0.068056 | 0.214473 |           |          |          |                |
| 0.264333 | 0.796907 | 0.073727 | 0.223231 |           |          |          |                |
| 0.284667 | 0.796907 | 0.079399 | 0.231658 |           |          |          |                |
| 0.305000 | 0.796907 | 0.085070 | 0.239789 |           |          |          |                |
| 0.325333 | 0.796907 | 0.090741 | 0.247653 |           |          |          |                |
| 0.345667 | 0.796907 | 0.096412 | 0.255275 |           |          |          |                |
| 0.366000 | 0.796907 | 0.102084 | 0.262675 |           |          |          |                |
| 0.386333 | 0.796907 | 0.107755 | 0.269873 |           |          |          |                |
| 0.406667 | 0.796907 | 0.113426 | 0.276884 |           |          |          |                |
| 0.427000 | 0.796907 | 0.119098 | 0.283722 |           |          |          |                |
| 0.447333 | 0.796907 | 0.124769 | 0.290398 |           |          |          |                |
| 0.467667 | 0.796907 | 0.130440 | 0.296925 |           |          |          |                |
| 0.488000 | 0.796907 | 0.136112 | 0.303311 |           |          |          |                |
| 0.508333 | 0.796907 | 0.141783 | 0.309566 |           |          |          |                |

| Depth<br>(ft) | Area<br>(acres) | Volume<br>(acre-ft) | Outflow1<br>(cfs) | Velocity<br>(ft/sec) | Travel Time***<br>(Minutes)*** |
|---------------|-----------------|---------------------|-------------------|----------------------|--------------------------------|
| 0.528667      | 0.796907        | 0.147454            | 0.315696          |                      |                                |
| 0.549000      | 0.796907        | 0.153126            | 0.321710          |                      |                                |
| 0.569333      | 0.796907        | 0.158797            | 0.327614          |                      |                                |
| 0.589667      | 0.796907        | 0.164468            | 0.333413          |                      |                                |
| 0.610000      | 0.796907        | 0.170140            | 0.339112          |                      |                                |
| 0.630333      | 0.796907        | 0.175811            | 0.344718          |                      |                                |
| 0.650667      | 0.796907        | 0.181482            | 0.350234          |                      |                                |
| 0.671000      | 0.796907        | 0.187154            | 0.355664          |                      |                                |
| 0.691333      | 0.796907        | 0.192825            | 0.361013          |                      |                                |
| 0.711667      | 0.796907        | 0.198496            | 0.366283          |                      |                                |
| 0.732000      | 0.796907        | 0.204168            | 0.371479          |                      |                                |
| 0.752333      | 0.796907        | 0.209839            | 0.376603          |                      |                                |
| 0.772667      | 0.796907        | 0.215510            | 0.381658          |                      |                                |
| 0.793000      | 0.796907        | 0.221182            | 0.386648          |                      |                                |
| 0.813333      | 0.796907        | 0.226853            | 0.391573          |                      |                                |
| 0.833667      | 0.796907        | 0.232524            | 0.396438          |                      |                                |
| 0.854000      | 0.796907        | 0.238196            | 0.401243          |                      |                                |
| 0.874333      | 0.796907        | 0.243867            | 0.405992          |                      |                                |
| 0.894667      | 0.796907        | 0.249538            | 0.410685          |                      |                                |
| 0.915000      | 0.796907        | 0.255209            | 0.415326          |                      |                                |
| 0.935333      | 0.796907        | 0.260881            | 0.419916          |                      |                                |
| 0.955667      | 0.796907        | 0.266552            | 0.424455          |                      |                                |
| 0.976000      | 0.796907        | 0.272223            | 0.428947          |                      |                                |
| 0.996333      | 0.796907        | 0.277895            | 0.433392          |                      |                                |
| 1.016667      | 0.796907        | 0.283566            | 0.437792          |                      |                                |
| 1.037000      | 0.796907        | 0.289237            | 0.442148          |                      |                                |
| 1.057333      | 0.796907        | 0.294909            | 0.446462          |                      |                                |
| 1.077667      | 0.796907        | 0.300580            | 0.450735          |                      |                                |
| 1.098000      | 0.796907        | 0.306251            | 0.454967          |                      |                                |
| 1.118333      | 0.796907        | 0.311923            | 0.459160          |                      |                                |
| 1.138667      | 0.796907        | 0.317594            | 0.463316          |                      |                                |
| 1.159000      | 0.796907        | 0.323265            | 0.467434          |                      |                                |
| 1.179333      | 0.796907        | 0.328937            | 0.471517          |                      |                                |
| 1.199667      | 0.796907        | 0.334608            | 0.475564          |                      |                                |
| 1.220000      | 0.796907        | 0.340279            | 0.479577          |                      |                                |
| 1.240333      | 0.796907        | 0.345951            | 0.483557          |                      |                                |
| 1.260667      | 0.796907        | 0.351622            | 0.487505          |                      |                                |
| 1.281000      | 0.796907        | 0.357293            | 0.491421          |                      |                                |
| 1.301333      | 0.796907        | 0.362965            | 0.495305          |                      |                                |
| 1.321667      | 0.796907        | 0.368636            | 0.499160          |                      |                                |
| 1.342000      | 0.796907        | 0.374307            | 0.502985          |                      |                                |
| 1.362333      | 0.796907        | 0.379979            | 0.506781          |                      |                                |
| 1.382667      | 0.796907        | 0.385650            | 0.510549          |                      |                                |
| 1.403000      | 0.796907        | 0.391321            | 0.514289          |                      |                                |
| 1.423333      | 0.796907        | 0.396993            | 0.518003          |                      |                                |
| 1.443667      | 0.796907        | 0.402664            | 0.521690          |                      |                                |
| 1.464000      | 0.796907        | 0.408335            | 0.525351          |                      |                                |
| 1.484333      | 0.796907        | 0.414007            | 0.528986          |                      |                                |
| 1.504667      | 0.796907        | 0.419678            | 0.532597          |                      |                                |
| 1.525000      | 0.796907        | 0.425349            | 0.536184          |                      |                                |
| 1.545333      | 0.796907        | 0.431020            | 0.539746          |                      |                                |
| 1.565667      | 0.796907        | 0.436692            | 0.543286          |                      |                                |
| 1.586000      | 0.796907        | 0.452896            | 0.546802          |                      |                                |
| 1.606333      | 0.796907        | 0.469099            | 0.550296          |                      |                                |
| 1.626667      | 0.796907        | 0.485303            | 0.553768          |                      |                                |
| 1.647000      | 0.796907        | 0.501507            | 0.557218          |                      |                                |
| 1.667333      | 0.796907        | 0.517711            | 0.560648          |                      |                                |
| 1.687667      | 0.796907        | 0.533914            | 0.564056          |                      |                                |
| 1.708000      | 0.796907        | 0.550118            | 0.567444          |                      |                                |
| 1.728333      | 0.796907        | 0.566322            | 0.570811          |                      |                                |
| 1.748667      | 0.796907        | 0.582526            | 0.574159          |                      |                                |
| 1.769000      | 0.796907        | 0.598730            | 0.577488          |                      |                                |
| 1.789333      | 0.796907        | 0.614933            | 0.580797          |                      |                                |
| 1.809667      | 0.796907        | 0.631137            | 0.584088          |                      |                                |
| 1.830000      | 0.796907        | 0.647341            | 0.587360          |                      |                                |
| END FTABLE    | 4               |                     |                   |                      |                                |
| FTABLE        | 1               |                     |                   |                      |                                |
| 91            | 4               |                     |                   |                      |                                |
| Depth<br>(ft) | Area<br>(acres) | Volume<br>(acre-ft) | Outflow1<br>(cfs) | Velocity<br>(ft/sec) | Travel Time***<br>(Minutes)*** |

|          |          |          |          |
|----------|----------|----------|----------|
| 0.000000 | 0.393361 | 0.000000 | 0.000000 |
| 0.020333 | 0.393361 | 0.002799 | 0.061913 |
| 0.040667 | 0.393361 | 0.005599 | 0.087558 |
| 0.061000 | 0.393361 | 0.008398 | 0.107237 |
| 0.081333 | 0.393361 | 0.011198 | 0.123826 |
| 0.101667 | 0.393361 | 0.013997 | 0.138442 |
| 0.122000 | 0.393361 | 0.016797 | 0.151656 |
| 0.142333 | 0.393361 | 0.019596 | 0.163807 |
| 0.162667 | 0.393361 | 0.022395 | 0.175117 |
| 0.183000 | 0.393361 | 0.025195 | 0.185739 |
| 0.203333 | 0.393361 | 0.027994 | 0.195787 |
| 0.223667 | 0.393361 | 0.030794 | 0.205343 |
| 0.244000 | 0.393361 | 0.033593 | 0.214473 |
| 0.264333 | 0.393361 | 0.036392 | 0.223231 |
| 0.284667 | 0.393361 | 0.039192 | 0.231658 |
| 0.305000 | 0.393361 | 0.041991 | 0.239789 |
| 0.325333 | 0.393361 | 0.044791 | 0.247653 |
| 0.345667 | 0.393361 | 0.047590 | 0.255275 |
| 0.366000 | 0.393361 | 0.050390 | 0.262675 |
| 0.386333 | 0.393361 | 0.053189 | 0.269873 |
| 0.406667 | 0.393361 | 0.055988 | 0.276884 |
| 0.427000 | 0.393361 | 0.058788 | 0.283722 |
| 0.447333 | 0.393361 | 0.061587 | 0.290398 |
| 0.467667 | 0.393361 | 0.064387 | 0.296925 |
| 0.488000 | 0.393361 | 0.067186 | 0.303311 |
| 0.508333 | 0.393361 | 0.069985 | 0.309566 |
| 0.528667 | 0.393361 | 0.072785 | 0.315696 |
| 0.549000 | 0.393361 | 0.075584 | 0.321710 |
| 0.569333 | 0.393361 | 0.078384 | 0.327614 |
| 0.589667 | 0.393361 | 0.081183 | 0.333413 |
| 0.610000 | 0.393361 | 0.083983 | 0.339112 |
| 0.630333 | 0.393361 | 0.086782 | 0.344718 |
| 0.650667 | 0.393361 | 0.089581 | 0.350234 |
| 0.671000 | 0.393361 | 0.092381 | 0.355664 |
| 0.691333 | 0.393361 | 0.095180 | 0.361013 |
| 0.711667 | 0.393361 | 0.097980 | 0.366283 |
| 0.732000 | 0.393361 | 0.100779 | 0.371479 |
| 0.752333 | 0.393361 | 0.103578 | 0.376603 |
| 0.772667 | 0.393361 | 0.106378 | 0.381658 |
| 0.793000 | 0.393361 | 0.109177 | 0.386648 |
| 0.813333 | 0.393361 | 0.111977 | 0.391573 |
| 0.833667 | 0.393361 | 0.114776 | 0.396438 |
| 0.854000 | 0.393361 | 0.117576 | 0.401243 |
| 0.874333 | 0.393361 | 0.120375 | 0.405992 |
| 0.894667 | 0.393361 | 0.123174 | 0.410685 |
| 0.915000 | 0.393361 | 0.125974 | 0.415326 |
| 0.935333 | 0.393361 | 0.128773 | 0.419916 |
| 0.955667 | 0.393361 | 0.131573 | 0.424455 |
| 0.976000 | 0.393361 | 0.134372 | 0.428947 |
| 0.996333 | 0.393361 | 0.137172 | 0.433392 |
| 1.016667 | 0.393361 | 0.139971 | 0.437792 |
| 1.037000 | 0.393361 | 0.142770 | 0.442148 |
| 1.057333 | 0.393361 | 0.145570 | 0.446462 |
| 1.077667 | 0.393361 | 0.148369 | 0.450735 |
| 1.098000 | 0.393361 | 0.151169 | 0.454967 |
| 1.118333 | 0.393361 | 0.153968 | 0.459160 |
| 1.138667 | 0.393361 | 0.156767 | 0.463316 |
| 1.159000 | 0.393361 | 0.159567 | 0.467434 |
| 1.179333 | 0.393361 | 0.162366 | 0.471517 |
| 1.199667 | 0.393361 | 0.165166 | 0.475564 |
| 1.220000 | 0.393361 | 0.167965 | 0.479577 |
| 1.240333 | 0.393361 | 0.170765 | 0.483557 |
| 1.260667 | 0.393361 | 0.173564 | 0.487505 |
| 1.281000 | 0.393361 | 0.176363 | 0.491421 |
| 1.301333 | 0.393361 | 0.179163 | 0.495305 |
| 1.321667 | 0.393361 | 0.181962 | 0.499160 |
| 1.342000 | 0.393361 | 0.184762 | 0.502985 |
| 1.362333 | 0.393361 | 0.187561 | 0.506781 |
| 1.382667 | 0.393361 | 0.190360 | 0.510549 |
| 1.403000 | 0.393361 | 0.193160 | 0.514289 |

|          |          |          |          |
|----------|----------|----------|----------|
| 1.423333 | 0.393361 | 0.195959 | 0.518003 |
| 1.443667 | 0.393361 | 0.198759 | 0.521690 |
| 1.464000 | 0.393361 | 0.201558 | 0.525351 |
| 1.484333 | 0.393361 | 0.204358 | 0.528986 |
| 1.504667 | 0.393361 | 0.207157 | 0.532597 |
| 1.525000 | 0.393361 | 0.209956 | 0.536184 |
| 1.545333 | 0.393361 | 0.212756 | 0.539746 |
| 1.565667 | 0.393361 | 0.215555 | 0.543286 |
| 1.586000 | 0.393361 | 0.223554 | 0.546802 |
| 1.606333 | 0.393361 | 0.231552 | 0.550296 |
| 1.626667 | 0.393361 | 0.239550 | 0.553768 |
| 1.647000 | 0.393361 | 0.247549 | 0.557218 |
| 1.667333 | 0.393361 | 0.255547 | 0.560648 |
| 1.687667 | 0.393361 | 0.263545 | 0.564056 |
| 1.708000 | 0.393361 | 0.271544 | 0.567444 |
| 1.728333 | 0.393361 | 0.279542 | 0.570811 |
| 1.748667 | 0.393361 | 0.287540 | 0.574159 |
| 1.769000 | 0.393361 | 0.295539 | 0.577488 |
| 1.789333 | 0.393361 | 0.303537 | 0.580797 |
| 1.809667 | 0.393361 | 0.311535 | 0.584088 |
| 1.830000 | 0.393361 | 0.319534 | 0.587360 |

END FTABLE 1  
FTABLE 5

| 91       | 4        | Depth<br>(ft) | Area<br>(acres) | Volume<br>(acre-ft) | Outflow1<br>(cfs) | Velocity<br>(ft/sec) | Travel Time***<br>(Minutes)*** |
|----------|----------|---------------|-----------------|---------------------|-------------------|----------------------|--------------------------------|
| 0.000000 | 0.292905 | 0.000000      | 0.000000        |                     |                   |                      |                                |
| 0.020333 | 0.292905 | 0.002085      | 0.061913        |                     |                   |                      |                                |
| 0.040667 | 0.292905 | 0.004169      | 0.087558        |                     |                   |                      |                                |
| 0.061000 | 0.292905 | 0.006254      | 0.107237        |                     |                   |                      |                                |
| 0.081333 | 0.292905 | 0.008338      | 0.123826        |                     |                   |                      |                                |
| 0.101667 | 0.292905 | 0.010423      | 0.138442        |                     |                   |                      |                                |
| 0.122000 | 0.292905 | 0.012507      | 0.151656        |                     |                   |                      |                                |
| 0.142333 | 0.292905 | 0.014592      | 0.163807        |                     |                   |                      |                                |
| 0.162667 | 0.292905 | 0.016676      | 0.175117        |                     |                   |                      |                                |
| 0.183000 | 0.292905 | 0.018761      | 0.185739        |                     |                   |                      |                                |
| 0.203333 | 0.292905 | 0.020845      | 0.195787        |                     |                   |                      |                                |
| 0.223667 | 0.292905 | 0.022930      | 0.205343        |                     |                   |                      |                                |
| 0.244000 | 0.292905 | 0.025014      | 0.214473        |                     |                   |                      |                                |
| 0.264333 | 0.292905 | 0.027099      | 0.223231        |                     |                   |                      |                                |
| 0.284667 | 0.292905 | 0.029183      | 0.231658        |                     |                   |                      |                                |
| 0.305000 | 0.292905 | 0.031268      | 0.239789        |                     |                   |                      |                                |
| 0.325333 | 0.292905 | 0.033352      | 0.247653        |                     |                   |                      |                                |
| 0.345667 | 0.292905 | 0.035437      | 0.255275        |                     |                   |                      |                                |
| 0.366000 | 0.292905 | 0.037521      | 0.262675        |                     |                   |                      |                                |
| 0.386333 | 0.292905 | 0.039606      | 0.269873        |                     |                   |                      |                                |
| 0.406667 | 0.292905 | 0.041690      | 0.276884        |                     |                   |                      |                                |
| 0.427000 | 0.292905 | 0.043775      | 0.283722        |                     |                   |                      |                                |
| 0.447333 | 0.292905 | 0.045859      | 0.290398        |                     |                   |                      |                                |
| 0.467667 | 0.292905 | 0.047944      | 0.296925        |                     |                   |                      |                                |
| 0.488000 | 0.292905 | 0.050028      | 0.303311        |                     |                   |                      |                                |
| 0.508333 | 0.292905 | 0.052113      | 0.309566        |                     |                   |                      |                                |
| 0.528667 | 0.292905 | 0.054197      | 0.315696        |                     |                   |                      |                                |
| 0.549000 | 0.292905 | 0.056282      | 0.321710        |                     |                   |                      |                                |
| 0.569333 | 0.292905 | 0.058366      | 0.327614        |                     |                   |                      |                                |
| 0.589667 | 0.292905 | 0.060451      | 0.333413        |                     |                   |                      |                                |
| 0.610000 | 0.292905 | 0.062535      | 0.339112        |                     |                   |                      |                                |
| 0.630333 | 0.292905 | 0.064620      | 0.344718        |                     |                   |                      |                                |
| 0.650667 | 0.292905 | 0.066704      | 0.350234        |                     |                   |                      |                                |
| 0.671000 | 0.292905 | 0.068789      | 0.355664        |                     |                   |                      |                                |
| 0.691333 | 0.292905 | 0.070873      | 0.361013        |                     |                   |                      |                                |
| 0.711667 | 0.292905 | 0.072958      | 0.366283        |                     |                   |                      |                                |
| 0.732000 | 0.292905 | 0.075042      | 0.371479        |                     |                   |                      |                                |
| 0.752333 | 0.292905 | 0.077127      | 0.376603        |                     |                   |                      |                                |
| 0.772667 | 0.292905 | 0.079211      | 0.381658        |                     |                   |                      |                                |
| 0.793000 | 0.292905 | 0.081296      | 0.386648        |                     |                   |                      |                                |
| 0.813333 | 0.292905 | 0.083380      | 0.391573        |                     |                   |                      |                                |
| 0.833667 | 0.292905 | 0.085465      | 0.396438        |                     |                   |                      |                                |
| 0.854000 | 0.292905 | 0.087549      | 0.401243        |                     |                   |                      |                                |
| 0.874333 | 0.292905 | 0.089634      | 0.405992        |                     |                   |                      |                                |

|          |          |          |          |
|----------|----------|----------|----------|
| 0.894667 | 0.292905 | 0.091718 | 0.410685 |
| 0.915000 | 0.292905 | 0.093803 | 0.415326 |
| 0.935333 | 0.292905 | 0.095887 | 0.419916 |
| 0.955667 | 0.292905 | 0.097972 | 0.424455 |
| 0.976000 | 0.292905 | 0.100056 | 0.428947 |
| 0.996333 | 0.292905 | 0.102141 | 0.433392 |
| 1.016667 | 0.292905 | 0.104225 | 0.437792 |
| 1.037000 | 0.292905 | 0.106310 | 0.442148 |
| 1.057333 | 0.292905 | 0.108394 | 0.446462 |
| 1.077667 | 0.292905 | 0.110479 | 0.450735 |
| 1.098000 | 0.292905 | 0.112563 | 0.454967 |
| 1.118333 | 0.292905 | 0.114648 | 0.459160 |
| 1.138667 | 0.292905 | 0.116732 | 0.463316 |
| 1.159000 | 0.292905 | 0.118817 | 0.467434 |
| 1.179333 | 0.292905 | 0.120901 | 0.471517 |
| 1.199667 | 0.292905 | 0.122986 | 0.475564 |
| 1.220000 | 0.292905 | 0.125070 | 0.479577 |
| 1.240333 | 0.292905 | 0.127155 | 0.483557 |
| 1.260667 | 0.292905 | 0.129239 | 0.487505 |
| 1.281000 | 0.292905 | 0.131324 | 0.491421 |
| 1.301333 | 0.292905 | 0.133408 | 0.495305 |
| 1.321667 | 0.292905 | 0.135493 | 0.499160 |
| 1.342000 | 0.292905 | 0.137577 | 0.502985 |
| 1.362333 | 0.292905 | 0.139662 | 0.506781 |
| 1.382667 | 0.292905 | 0.141746 | 0.510549 |
| 1.403000 | 0.292905 | 0.143831 | 0.514289 |
| 1.423333 | 0.292905 | 0.145915 | 0.518003 |
| 1.443667 | 0.292905 | 0.148000 | 0.521690 |
| 1.464000 | 0.292905 | 0.150084 | 0.525351 |
| 1.484333 | 0.292905 | 0.152169 | 0.528986 |
| 1.504667 | 0.292905 | 0.154253 | 0.532597 |
| 1.525000 | 0.292905 | 0.156338 | 0.536184 |
| 1.545333 | 0.292905 | 0.158422 | 0.539746 |
| 1.565667 | 0.292905 | 0.160507 | 0.543286 |
| 1.586000 | 0.292905 | 0.166463 | 0.546802 |
| 1.606333 | 0.292905 | 0.172418 | 0.550296 |
| 1.626667 | 0.292905 | 0.178374 | 0.553768 |
| 1.647000 | 0.292905 | 0.184330 | 0.557218 |
| 1.667333 | 0.292905 | 0.190286 | 0.560648 |
| 1.687667 | 0.292905 | 0.196241 | 0.564056 |
| 1.708000 | 0.292905 | 0.202197 | 0.567444 |
| 1.728333 | 0.292905 | 0.208153 | 0.570811 |
| 1.748667 | 0.292905 | 0.214108 | 0.574159 |
| 1.769000 | 0.292905 | 0.220064 | 0.577488 |
| 1.789333 | 0.292905 | 0.226020 | 0.580797 |
| 1.809667 | 0.292905 | 0.231976 | 0.584088 |
| 1.830000 | 0.292905 | 0.237931 | 0.587360 |

END FTABLE 5  
FTABLE 6

| 91       | 4        | Depth<br>(ft) | Area<br>(acres) | Volume<br>(acre-ft) | Outflow1<br>(cfs) | Velocity<br>(ft/sec) | Travel Time***<br>(Minutes)*** |
|----------|----------|---------------|-----------------|---------------------|-------------------|----------------------|--------------------------------|
| 0.000000 | 0.026549 | 0.000000      | 0.000000        | 0.000000            | 0.061913          | 0.087558             | 0.107237                       |
| 0.020333 | 0.026549 | 0.000189      | 0.000378        | 0.000567            | 0.123826          | 0.138442             | 0.151656                       |
| 0.040667 | 0.026549 | 0.000945      | 0.001134        | 0.001323            | 0.163807          | 0.175117             | 0.185739                       |
| 0.061000 | 0.026549 | 0.001700      | 0.001889        | 0.002078            | 0.214473          | 0.223231             | 0.231658                       |
| 0.081333 | 0.026549 | 0.002456      | 0.002645        | 0.002834            | 0.239789          | 0.247653             | 0.255275                       |
| 0.101667 | 0.026549 | 0.003023      | 0.003212        |                     |                   |                      |                                |

|          |          |          |          |
|----------|----------|----------|----------|
| 0.366000 | 0.026549 | 0.003401 | 0.262675 |
| 0.386333 | 0.026549 | 0.003590 | 0.269873 |
| 0.406667 | 0.026549 | 0.003779 | 0.276884 |
| 0.427000 | 0.026549 | 0.003968 | 0.283722 |
| 0.447333 | 0.026549 | 0.004157 | 0.290398 |
| 0.467667 | 0.026549 | 0.004346 | 0.296925 |
| 0.488000 | 0.026549 | 0.004535 | 0.303311 |
| 0.508333 | 0.026549 | 0.004723 | 0.309566 |
| 0.528667 | 0.026549 | 0.004912 | 0.315696 |
| 0.549000 | 0.026549 | 0.005101 | 0.321710 |
| 0.569333 | 0.026549 | 0.005290 | 0.327614 |
| 0.589667 | 0.026549 | 0.005479 | 0.333413 |
| 0.610000 | 0.026549 | 0.005668 | 0.339112 |
| 0.630333 | 0.026549 | 0.005857 | 0.344718 |
| 0.650667 | 0.026549 | 0.006046 | 0.350234 |
| 0.671000 | 0.026549 | 0.006235 | 0.355664 |
| 0.691333 | 0.026549 | 0.006424 | 0.361013 |
| 0.711667 | 0.026549 | 0.006613 | 0.366283 |
| 0.732000 | 0.026549 | 0.006802 | 0.371479 |
| 0.752333 | 0.026549 | 0.006991 | 0.376603 |
| 0.772667 | 0.026549 | 0.007180 | 0.381658 |
| 0.793000 | 0.026549 | 0.007369 | 0.386648 |
| 0.813333 | 0.026549 | 0.007558 | 0.391573 |
| 0.833667 | 0.026549 | 0.007747 | 0.396438 |
| 0.854000 | 0.026549 | 0.007935 | 0.401243 |
| 0.874333 | 0.026549 | 0.008124 | 0.405992 |
| 0.894667 | 0.026549 | 0.008313 | 0.410685 |
| 0.915000 | 0.026549 | 0.008502 | 0.415326 |
| 0.935333 | 0.026549 | 0.008691 | 0.419916 |
| 0.955667 | 0.026549 | 0.008880 | 0.424455 |
| 0.976000 | 0.026549 | 0.009069 | 0.428947 |
| 0.996333 | 0.026549 | 0.009258 | 0.433392 |
| 1.016667 | 0.026549 | 0.009447 | 0.437792 |
| 1.037000 | 0.026549 | 0.009636 | 0.442148 |
| 1.057333 | 0.026549 | 0.009825 | 0.446462 |
| 1.077667 | 0.026549 | 0.010014 | 0.450735 |
| 1.098000 | 0.026549 | 0.010203 | 0.454967 |
| 1.118333 | 0.026549 | 0.010392 | 0.459160 |
| 1.138667 | 0.026549 | 0.010581 | 0.463316 |
| 1.159000 | 0.026549 | 0.010770 | 0.467434 |
| 1.179333 | 0.026549 | 0.010959 | 0.471517 |
| 1.199667 | 0.026549 | 0.011147 | 0.475564 |
| 1.220000 | 0.026549 | 0.011336 | 0.479577 |
| 1.240333 | 0.026549 | 0.011525 | 0.483557 |
| 1.260667 | 0.026549 | 0.011714 | 0.487505 |
| 1.281000 | 0.026549 | 0.011903 | 0.491421 |
| 1.301333 | 0.026549 | 0.012092 | 0.495305 |
| 1.321667 | 0.026549 | 0.012281 | 0.499160 |
| 1.342000 | 0.026549 | 0.012470 | 0.502985 |
| 1.362333 | 0.026549 | 0.012659 | 0.506781 |
| 1.382667 | 0.026549 | 0.012848 | 0.510549 |
| 1.403000 | 0.026549 | 0.013037 | 0.514289 |
| 1.423333 | 0.026549 | 0.013226 | 0.518003 |
| 1.443667 | 0.026549 | 0.013415 | 0.521690 |
| 1.464000 | 0.026549 | 0.013604 | 0.525351 |
| 1.484333 | 0.026549 | 0.013793 | 0.528986 |
| 1.504667 | 0.026549 | 0.013982 | 0.532597 |
| 1.525000 | 0.026549 | 0.014170 | 0.536184 |
| 1.545333 | 0.026549 | 0.014359 | 0.539746 |
| 1.565667 | 0.026549 | 0.014548 | 0.543286 |
| 1.586000 | 0.026549 | 0.015088 | 0.546802 |
| 1.606333 | 0.026549 | 0.015628 | 0.550296 |
| 1.626667 | 0.026549 | 0.016168 | 0.553768 |
| 1.647000 | 0.026549 | 0.016708 | 0.557218 |
| 1.667333 | 0.026549 | 0.017248 | 0.560648 |
| 1.687667 | 0.026549 | 0.017787 | 0.564056 |
| 1.708000 | 0.026549 | 0.018327 | 0.567444 |
| 1.728333 | 0.026549 | 0.018867 | 0.570811 |
| 1.748667 | 0.026549 | 0.019407 | 0.574159 |
| 1.769000 | 0.026549 | 0.019947 | 0.577488 |

```

1.789333 0.026549 0.020486 0.580797
1.809667 0.026549 0.021026 0.584088
1.830000 0.026549 0.021566 0.587360
END FTABLE 6
END FTABLES

```

#### EXT SOURCES

| <-Volume-> <Member> SsysSgap<--Mult-->Tran |   | <-Target vols> |      | <-Grp> <-Member-> *** |                           |
|--|---|----------------|------|-----------------------|---------------------------|
| <Name>                                     | # | <Name>         | #    | <Name>                | # # ***                   |
| WDM  | 2 | PREC           | ENGL | 0.944                 | PERLND 1 999 EXTNL PREC   |
| WDM  | 2 | PREC           | ENGL | 0.944                 | IMPLND 1 999 EXTNL PREC   |
| WDM  | 1 | EVAP           | ENGL | 0.85                  | PERLND 1 999 EXTNL PETINP |
| WDM  | 1 | EVAP           | ENGL | 0.85                  | IMPLND 1 999 EXTNL PETINP |
| WDM  | 2 | PREC           | ENGL | 0.944                 | RCHRES 7 EXTNL PREC       |
| WDM  | 1 | EVAP           | ENGL | 0.85                  | RCHRES 1 EXTNL POTEV      |
| WDM  | 1 | EVAP           | ENGL | 0.85                  | RCHRES 2 EXTNL POTEV      |
| WDM  | 1 | EVAP           | ENGL | 0.85                  | RCHRES 3 EXTNL POTEV      |
| WDM  | 1 | EVAP           | ENGL | 0.85                  | RCHRES 4 EXTNL POTEV      |
| WDM  | 1 | EVAP           | ENGL | 0.85                  | RCHRES 5 EXTNL POTEV      |
| WDM  | 1 | EVAP           | ENGL | 0.85                  | RCHRES 6 EXTNL POTEV      |
| WDM  | 1 | EVAP           | ENGL | 0.5                   | RCHRES 7 EXTNL POTEV      |
| WDM  | 1 | EVAP           | ENGL | 0.595                 | RCHRES 8 EXTNL POTEV      |

```
END EXT SOURCES
```

#### EXT TARGETS

| <-Volume-> <-Grp> <-Member-><--Mult-->Tran |     | <-Volume-> <Member> Tsys Tgap Amd *** |     |                         |
|--|-----|---------------------------------------|-----|-------------------------|
| <Name>                                     | #   | <Name>                                | #   | tem strg strg***        |
| RCHRES                                     | 8   | HYDR RO                               | 1 1 | WDM 1000 FLOW ENGL REPL |
| RCHRES                                     | 8   | HYDR STAGE                            | 1 1 | WDM 1001 STAG ENGL REPL |
| RCHRES                                     | 7   | HYDR STAGE                            | 1 1 | WDM 1002 STAG ENGL REPL |
| RCHRES                                     | 7   | HYDR O                                | 1 1 | WDM 1003 FLOW ENGL REPL |
| COPY                                       | 1   | OUTPUT MEAN                           | 1 1 | WDM 701 FLOW ENGL REPL  |
| COPY                                       | 501 | OUTPUT MEAN                           | 1 1 | WDM 801 FLOW ENGL REPL  |

```
END EXT TARGETS
```

#### MASS-LINK

| <Volume> <-Grp> <-Member-><--Mult--> |          | <Target> |          | <-Grp> <-Member->*** |                |
|--------------------------------------|----------|----------|----------|----------------------|----------------|
| <Name>                               | <Name> # | <Name>   | <Name>   | <Name>               | <Name> # # *** |
| PERLND                               | PWATER   | SURO     | 0.083333 | RCHRES               | INFLOW IVOL    |
| END MASS-LINK                        | 2        |          |          |                      |                |
| PERLND                               | PWATER   | IFWO     | 0.083333 | RCHRES               | INFLOW IVOL    |
| END MASS-LINK                        | 3        |          |          |                      |                |
| IMPLND                               | IWATER   | SURO     | 0.083333 | RCHRES               | INFLOW IVOL    |
| END MASS-LINK                        | 5        |          |          |                      |                |
| RCHRES                               | ROFLOW   |          |          | RCHRES               | INFLOW         |
| END MASS-LINK                        | 6        |          |          |                      |                |
| RCHRES                               | OFLOW    | OVOL     | 2        | RCHRES               | INFLOW IVOL    |
| END MASS-LINK                        | 8        |          |          |                      |                |
| PERLND                               | PWATER   | SURO     | 0.083333 | COPY                 | INPUT MEAN     |
| END MASS-LINK                        | 12       |          |          |                      |                |
| PERLND                               | PWATER   | IFWO     | 0.083333 | COPY                 | INPUT MEAN     |
| END MASS-LINK                        | 13       |          |          |                      |                |
| IMPLND                               | IWATER   | SURO     | 0.083333 | COPY                 | INPUT MEAN     |
| END MASS-LINK                        | 15       |          |          |                      |                |

```
MASS-LINK      16
RCHRES      ROFLOW
END MASS-LINK    16
                           COPY           INPUT   MEAN

MASS-LINK      17
RCHRES      OFLOW   OVOL    1
END MASS-LINK    17
                           COPY           INPUT   MEAN

MASS-LINK      53
IMPLND      IWATER  SURO
END MASS-LINK    53
                           IMPLND        EXTNL   SURLI

MASS-LINK      54
PERLND      PWATER  SURO
END MASS-LINK    54
                           IMPLND        EXTNL   SURLI

MASS-LINK      55
PERLND      PWATER  IFWO
END MASS-LINK    55
                           IMPLND        EXTNL   SURLI

END MASS-LINK
END RUN
```

DRAFT

*Pre-Project HSPF Message File*

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*Mitigated HSPF Message File*

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## **APPENDIX J:**

### **Grading Plan**



|     |             | SCALE:      | BENCH MARK  | COUNTY B.M. 1A-35 | COMPUTED    | MJC |
|-----|-------------|-------------|---|-------------------|-------------|-----|
|     |             | HORIZ. 1" = | EL=55.63 (NAVD 88)  | DESIGNED          | DVG         |     |
|     |             | VERT. 1" =  | 7/8" METAL DISC STAMPED "CO. B.M. 1A-35" LOCATED IN CHISELED SQUARE TOP OF CURB ABOVE DI AT SOUTH-EAST CORNER OF BRADSHAW RD. & JACKSON HWY. (NGVD ELEV. = 63.29) | DRAWN             | CEC         |     |
| NO. | DESCRIPTION | APPD. ENGR. | DATE APPD. E.U.   | DATE              | PROJ. ENGR. | EKY |



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web: www.mpengr.com

## PRELIMINARY GRADING AND DRAINAGE PLAN

**J @ B STORAGE**  
**5220 BRADSHAW ROAD & 9680 JACKSON ROAD**  
SACRAMENTO COUNTY, CALIFORNIA

| DATE   | APRIL 2024 |
|--------|------------|
| SHEET  | C-2        |
| 2 OF 6 |            |