Appendix "A"

Preliminary Hydrology Study Tentative Tract 38605

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Preliminary Hydrology Study

Tentative Tract Map No. 38605

JN: 10308
CLIENT: Raincross Development, LLC
DATE PREPARED
05/23/2024

adkan ENGINEERS

CIVIL ENGINEERING • SURVEYING • PLANNING

PRELIMINARY HYDROLOGY STUDY

Tentative Tract Map No. 38605

Located in the County of Riverside, CA

Prepared by:

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May 23, 2024



6.5.2024

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Exp. 06/30/2026

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Section 1 - Introduction

1. Introduction

This report provides a for an analysis of proposed storm water infrastructure, detention facilities and the development of Tentative Tract Map No. 38605. This report provides information on proposed and existing storm flows rates, storm volumes, existing facilities, recommended facilities, and the necessary basin storage and water quality sizing criteria associated with managing the projects storm water run-off while effectively treating the quality of the storm water.

Tentative Tract Map No. 38605 is located in the unincorporated area of Riverside County. The project is located on the north side of Lake Matthews, north of El Sobrante Road and East of McAllister Street. Figure 1.1 provides a location map for the project.

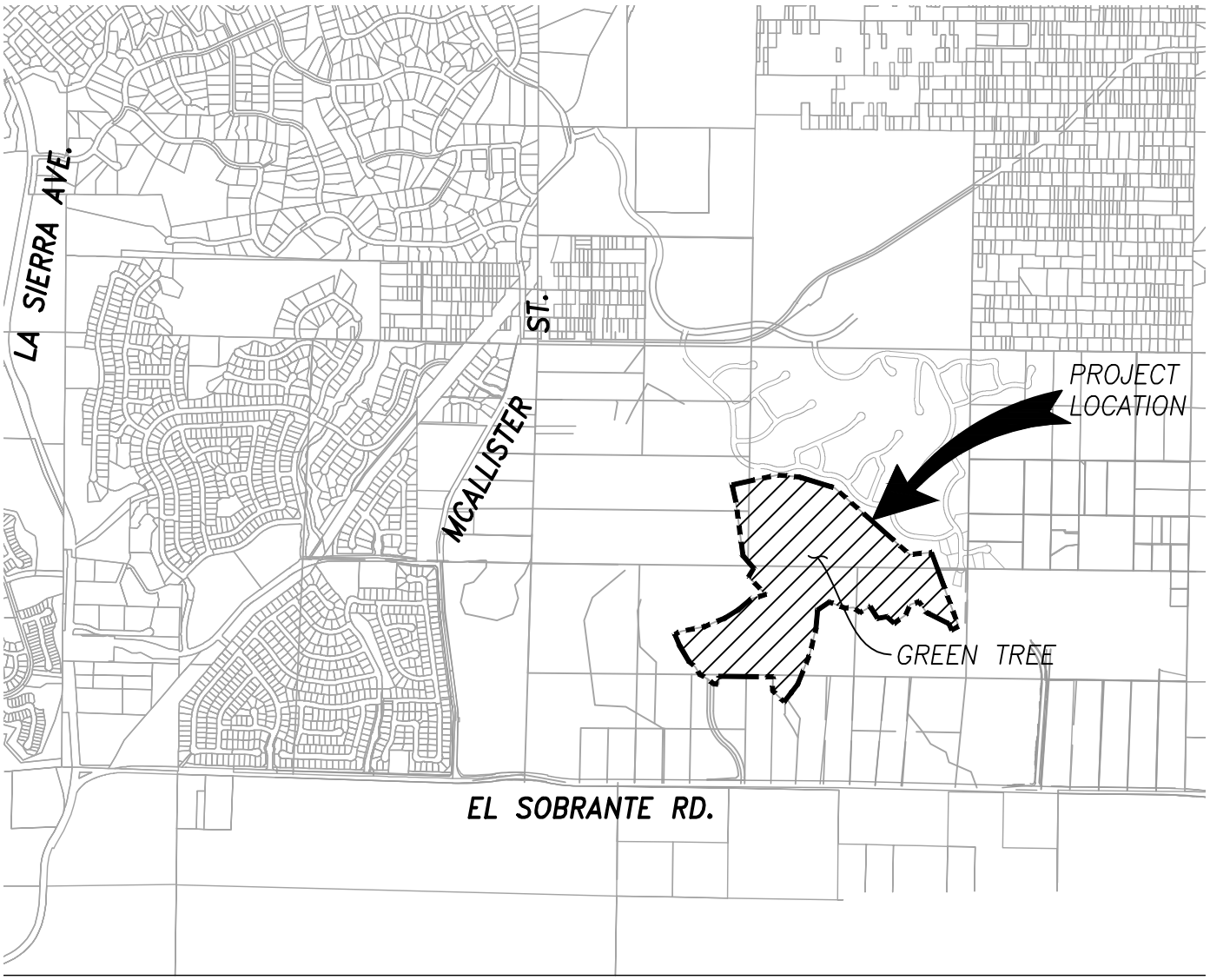
2. Land Use Plan

Tentative Tract Map No. 38605 encompasses a total of approximately 95.96 acres. Figure 1.2 provides the development plan for the project. The proposed project consists of the development of 163 detached single family dwelling units located within the unincorporated area of Riverside County known as the Lake Matthews Area. The Lake Mathew Area Plan was developed as part of the Riverside County General Plan 2025, prepared in 2003 as part of the General Plan Update. The project is located with the El Sobrante Policy Area of the Lake Matthews Area, which encourages the clustering of parcel sizes to a minimum of 10,000 square feet for the purposes of conserving open space and sensitive habitat while not exceeding the underlying housing densities identified by the general plan's designation of LDR-Low Density Residential (2 units/acre) and VLDR-Very Low Density Residentials (1 unit/acre). As part of the clustering efforts the project will be proposing a zone change to incorporate development standards that are consistent with the reduced lot sizes. It should be noted that although the project is clustering the units to a smaller overall parcel size, the total number of units is consistent with the existing land use designation.

3. Purpose of Study

The purpose of this study is to substantiate the hydrology and hydraulic design of the residential development known as Tentative Tract Map No. 38605. This study will analyze the pre-development and post-development storm water run-on and run-off values and propose storm water design recommendations to ensure the adequate size, volumes, and proper operation of drainage facilities for the proposed project while not adversely affecting downstream facilities and maintaining the conveyance of 100-year storm flows for on-site facilities. Along with the standard analysis of a typical report, this report outlines the specific analysis and back-up calculations necessary for determining the hydrology and hydraulics of the development such that the post-developed condition is equal to or improved when compared to pre-developed condition.

4. Figure 1.1 Location Map - Tentative Tract No. 38605



LAKE MATHEWS

0 2000 6000

1000 4000 8000

SCALE: 1" = 2000'

PREPARATION DATE: AUG 2023

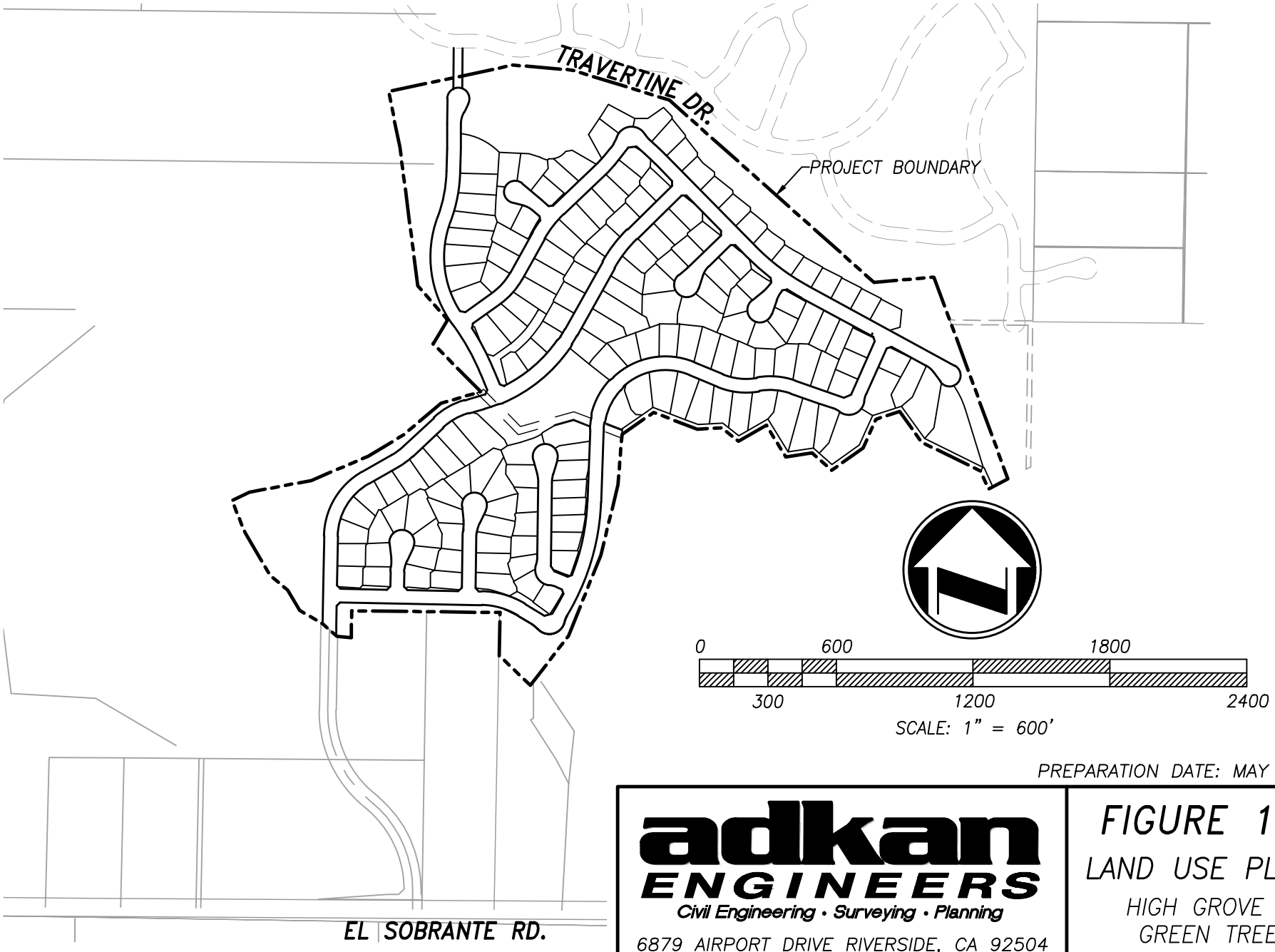
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FIGURE 1.1
VICINITY MAP

GREEN TREE
TTM 38605

U:\Projects\FOREMOST COMMUNITIES\8794\Waddell\EXHIBIT\GREEN TREE VICINITY MAP FIGURE 1.1.dwg

5. Figure 1.2 Land Use Map - Tentative Tract No. 38605



PREPARATION DATE: MAY 2024

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FIGURE 1.2
LAND USE PLAN
HIGH GROVE 3
GREEN TREE
TTM 38605

U:\Projects\FOREMOST COMMUNITIES\8794\Waddell\EXHIBIT\GREEN TREE LAND USE FIGURE 1.3.dwg

Section 2 –Rational Method Hydrology Analysis

The Rational Method is commonly used for determining park discharge from relatively small drainage areas. The rational method is based on the following equation Q = CIA, where Q is the peak discharge, C is the coefficient of runoff, I is the rainfall intensity, and A is the area of the watershed. Values of these variables necessary to calculate the park discharge are found utilizing the various plates located within the Riverside County Flood Control Hydrology Manual. The Rational Method Hydrology is calculated for the 10-year and 100-year storm events. The criteria for the protection of storm flow are determined by containing the 10-year storm event with in the tops of street curbs, and the 100-year storm event within the public right of way. Storm drains and/or channels should be considered when either condition is exceeded.

1. Existing Rational Method Hydrology

The existing site is an irregular shaped property consisting of rolling hills previously utilized for the cultivation of citrus fruit. The existing citrus trees have since been removed leaving the remanent of citrus furrows and overgrown earthen irrigation trenches. The project site is bisected by a ridgeline running from east to west close to the center of the property assemblage. The ridgeline can also be defined by an unpaved road seen within aerial imagery providing a means of maintenance access for an existing reservoir owned by Western Municipal Water District (WMWD). From the ridge line the existing flows travel north and south into two natural drainage courses that bound the north and south edges of the project site. The drainage courses have been deeply incised and defined throughout time, and in many locations exhibit exposed bedrock limiting the potential for future erosion. Each of these two natural drainage courses convey flows northwesterly to a point of confluence westerly of the project site before being conveyed through a development to the north of the project site, known as Tramonte, and finally into the Harrison Dam facility.

The Harrison Dam was constructed based on the development of the upstream tiburaties to protect the downstream properties located in the City of Riverside. The Dam was designed to detain the watershed of the proposed project, including the upstream properties, to a maximum discharge of 150 CFS. Based on the projects clustering efforts it was determined through discussion with RCFC that additional post development increased storm water runoff mitigation would be necessary beyond the normally required 2-, 5-, and 10-year storm events, and therefore detention basins are required for the project to be designed with the capacity to mitigate the 100-year storm events. This is further discussed within Section 3 of this report.

From the Harrison Dam facility existing storm flows are conveyed through the City of Riverside and ultimately into the Arizona Channel owned and maintained by RCFC. The Arizona Channel is part of a drainage system funded by Area Drainage Plan fees known at the Southwest Area Drainage Plan.

The results of the existing rational method hydrology for the north and south drainage courses are shown in Table 2-1 below. Existing Rational Method Hydrology calculations can be found in Appendix “A” of this report.

Table 2-1 Tract 38605– Existing Rational Method Flow Rates			
Drainage Area	**Node No.**	**10-Year Flow Rate**	**100-Year Flow Rate**
North	15	129.62 CFS	214.93 CFS
South	6	341.32 CFS	587.30 CFS

2. Proposed Rational Method Hydrology

The proposed project consists of 163 single family detached single family residences. The project site has been design in such a manner to respect the existing ridgeline that bisects the project from east to west. This was also done to protect the existing unpaved road seen within aerial imagery providing a means of maintenance access for an existing reservoir owned by WMWD. The storm flows for the project development north of the ridgeline are conveyed into two extended detention basins each treating approximately half of project area north of the ridgeline which is then released into the northern drainage course. The storm flows from the project development south of the ridgeline are conveyed into a single extended detention basin which is released into the southern drainage course. Preliminary storm drainage facilities and catch basins have been proposed within the proposed project to limit the spread of the 100 year on-site flows to be contained within tops of the street curbs.

As discussed within the Existing Rational Method Hydrology section, it was determined through discussion with RCFC that additional post development increased storm water runoff mitigation would be necessary beyond the 2-, 5-, and 10-year storm events, and therefore the extended detention basins are required for the project to be designed with the capacity to mitigate the 100-year storm events. These calculations were performed utilizing the Synthetic Unit Hydrograph Method and a summary of the results are included within Section 3 of this report.

There are two culvert crossings being proposed as part of the project. These culvert crossings are located in the northerly existing drainage course and the southerly existing drainage course and allow the development to provide access and utilities over the existing drainage courses. The culverts have been designed in accordance with the California Department of Fish and Wildlife (CDFW) to have a minimum size of 72” for the purposes of providing a downstream and upstream connection for habitat and wildlife within the drainage corridor. This results in culverts larger than necessary to convey the actual flow experience by a 100-year storm event. The culverts also contain the necessary headwalls, cutoff walls, and rip-rap energy dissipaters to reduce the storm flow velocities to a non-erosive level protecting the downstream drainage courses.

It should be noted the Proposed Rational Method Hydrology flow rates are utilized to size the storm drain facilities to provide a level of storm protection to adequately convey the 100-year storm flow rates. This information is utilized to analyze the hydraulics of the storm facilities for the purposes of sizing storm drain lines, inlets and outlets, spillways, street capacities and culverts for the ultimate experienced flow rates. Preliminary calculations

for the sizing of these facilities can be found within Appendix F of this report. Comparison of the proposed and existing flow rates for the purposes of the mitigation for post construction increased runoff should be evaluated utilizing the Synthetic Unit Hydrography Method as summarized in Section 3.

The results of the Proposed Rational Method Hydrology for the north and south drainage courses, and the three extended detention basins are shown in Table 2-2 below. Proposed Rational Method Hydrology calculations can be found in Appendix "B" of this report.

Table 2-1
Tract 38605– Proposed Rational Method Flow Rates

Drainage Area	Node No.	10-Year Flow Rate	100-Year Flow Rate
North Culvert	318	180.87 CFS	302.56 CFS
South Culvert	528	365.62 CFS	633.11 CFS
Extended Detention Basin "1"	27	32.83 CFS	54.19 CFS
Extended Detention Basin "2"	117	67.28 CFS	111.07 CFS
Extended Detention Basin "3"	207	11.72 CFS	19.38 CFS

Section 3 – Synthetic Unit Method Hydrology Analysis

The Synthetic Unit Method Hydrology is utilized to analyze the entire are of a proposed development that will be routed through a detention facility for mitigation of the post construction incremental increased runoff when compared to the existing condition.

Storms to be studied will include the 1-hour, 3-hour, 6-hour and 24-hour duration for the 2-year, 5-year, and 10-year return frequencies. Detention basins and outlet sizing's will ensure that none of these storm events will have up to a 10% increase in peak storm discharge of the post development condition than in the pre-development conditions. As previously discussed, peak flow storm mitigation would be necessary beyond the 2-, 5-, and 10-year storm events, however with the added level of storm protection needed for the Harrison Dam, RCFC has required the extended detention basins a to be designed with the capacity to mitigate the 100-year storm events.

The project is proposing the utilization of three extended detention basins for the mitigation of the post construction incremental increased runoff. There are two basins located tributary to the northly drainage course, Basins 1 and 2, and one basin located tributary to the southerly drainage course, Basin 3. The proposed extended basins effectively mitigate the post development flow rates ensuring none of the storm events will have up to a 10% increase in peak storm discharge of the post development condition than in the pre-development conditions.

A summary of the extended detention basins existing, proposed, and routed peak flows for all storm events and frequencies are shown in Tables 3-1, 3-2, and 3-3 below. Existing Synthetic Unit Method Hydrology calculations can be found in Appendix C of this report, Proposed Synthetic Unit Method Hydrology calculations can be found in Appendix D of this report, and Basin Routing Hydrographs along with respective Outflow Calculations can be found in Appendix E of this report.

1. Extended Detention Basin No. 1

Table 3-1
Tract 38605– Extended Detention Basin No. 1 Outflow Comparison

Storm Event	Pre-Developed		Post-Developed		Post-Developed with Basin			Pre vs. Post Percent Difference (10% Max)
	Flow (cfs)	Volume (ac.ft.)	Flow (cfs)	Volume (ac.ft.)	Routed Basin Out Flow (cfs)	Storage Volume (ac.ft.)	Depth (ft)	
2 Year - 1 Hour	24.414	0.5905	27.801	0.8252	0.256	0.813	1.09	-99.0%
2 Year - 3 Hour	12.271	0.5324	15.090	1.0911	0.390	1.056	1.38	-96.8%
2 Year - 6 Hour	10.748	0.5686	13.584	1.4087	0.542	1.333	1.72	-95.0%
2 Year - 24 Hour	0.883	0.4084	3.455	2.0108	0.665	1.556	1.99	-24.7%
5 Year - 1 Hour	36.052	0.9826	39.589	1.2294	0.474	1.208	1.57	-98.7%
5 Year - 3 Hour	18.915	0.9607	21.675	1.6091	0.664	1.553	1.99	-96.5%
5 Year - 6 Hour	17.784	1.1262	20.558	2.1615	1.113	2.030	2.52	-93.7%
5 Year - 24 Hour	3.631	0.8560	6.203	3.0093	1.345	2.274	2.80	-63.0%
10 Year - 1 Hour	48.345	1.5864	50.425	1.7037	0.770	1.669	2.12	-98.4%
10 Year - 3 Hour	27.430	2.1065	28.574	2.4556	1.410	2.343	2.87	-94.9%
10 Year - 6 Hour	26.594	2.6586	27.752	3.3486	23.440	2.639	3.19	-11.9%
10 Year - 24 Hour	8.712	3.1005	9.934	4.8202	9.515	2.523	3.07	9.2%
100 Year - 1 Hour	77.592	2.6354	80.047	2.7527	12.283	2.546	3.09	-84.2%
100 Year - 3 Hour	44.128	3.6740	45.122	4.0260	39.828	2.776	3.34	-9.7%
100 Year - 6 Hour	44.275	5.1335	45.277	5.8312	40.883	2.785	3.35	-7.7%
100 Year - 24 Hour	15.619	6.3679	16.840	8.5048	16.714	2.583	3.13	7.0%

2. Extended Detention Basin No. 2

Table 3-2
Tract 38605– Extended Detention Basin No. 2 Outflow Comparison

Storm Event	Pre-Developed		Post-Developed		Post-Developed with Basin			Pre vs. Post Percent Difference (10% Max)
	Flow (cfs)	Volume (ac.ft.)	Flow (cfs)	Volume (ac.ft.)	Routed Basin Out Flow (cfs)	Storage Volume (ac.ft.)	Depth (ft)	
2 Year - 1 Hour	49.310	1.1435	47.194	1.3402	0.815	1.305	2.73	-98.3%
2 Year - 3 Hour	22.628	1.0312	20.084	1.7706	1.146	3.360	1.67	-94.9%
2 Year - 6 Hour	18.407	1.1012	17.339	2.3931	1.470	2.161	4.17	-92.0%
2 Year - 24 Hour	1.661	0.7911	6.393	3.8846	1.728	2.705	4.99	4.0%
5 Year - 1 Hour	72.605	1.9029	68.734	1.9445	1.302	1.887	3.73	-98.2%
5 Year - 3 Hour	35.099	1.8606	32.327	2.5395	1.579	2.390	4.51	-95.5%
5 Year - 6 Hour	31.060	2.1813	29.939	3.4998	11.484	3.003	5.41	-63.0%
5 Year - 24 Hour	6.892	1.6579	9.054	5.5022	6.944	2.949	5.33	0.8%
10 Year - 1 Hour	96.988	3.0723	91.590	2.7128	1.694	2.634	4.88	-98.3%
10 Year - 3 Hour	51.290	4.0800	47.348	3.4814	14.837	3.043	5.46	-71.1%
10 Year - 6 Hour	47.388	5.1495	45.795	4.8167	43.521	3.117	5.56	-8.2%
10 Year - 24 Hour	16.731	6.0058	12.911	6.7994	12.489	3.015	5.43	-25.4%
100 Year - 1 Hour	155.539	5.1040	149.688	4.7239	125.746	3.264	5.76	-19.2%
100 Year - 3 Hour	82.628	7.1162	79.045	6.1264	79.141	3.181	5.65	-4.2%
100 Year - 6 Hour	79.183	9.9433	79.376	8.6580	76.226	3.175	5.64	-3.7%
100 Year - 24 Hour	30.032	12.3348	26.289	12.2882	26.244	3.085	5.52	-12.6%

3. Extended Detention Basin No. 3

Table 3-3
Tract 38605– Extended Detention Basin No. 3 Outflow Comparison

Storm Event	Pre-Developed		Post-Developed		Post-Developed with Basin			Pre vs. Post Percent Difference (10% Max)
	Flow (cfs)	Volume (ac.ft.)	Flow (cfs)	Volume (ac.ft.)	Routed Basin Out Flow (cfs)	Storage Volume (ac.ft.)	Depth (ft)	
2 Year - 1 Hour	7.278	0.1721	6.894	0.2016	0.059	0.199	0.65	-99.2%
2 Year - 3 Hour	3.502	0.1551	3.105	0.2663	0.076	0.258	0.85	-97.8%
2 Year - 6 Hour	3.066	0.1657	2.682	0.3599	0.119	0.340	1.10	-96.1%
2 Year - 24 Hour	0.256	0.1190	0.961	0.5842	0.207	0.453	1.39	-19.1%
5 Year - 1 Hour	10.731	0.2863	10.025	0.2926	0.085	0.288	0.95	-99.2%
5 Year - 3 Hour	5.413	0.2799	5.001	0.3820	0.141	0.369	1.17	-97.4%
5 Year - 6 Hour	5.089	0.3281	4.638	0.5264	0.240	0.494	1.50	-95.3%
5 Year - 24 Hour	1.057	0.2494	1.362	0.8275	0.341	0.623	1.84	-67.7%
10 Year - 1 Hour	14.359	0.2623	13.398	0.4082	0.166	0.401	1.26	-98.8%
10 Year - 3 Hour	7.874	0.6137	7.299	0.5237	0.248	0.504	1.53	-96.9%
10 Year - 6 Hour	7.636	0.7746	7.055	0.7245	0.384	0.678	1.99	-95.0%
10 Year - 24 Hour	2.538	0.9033	1.943	1.0226	1.176	0.692	2.02	-53.7%
100 Year - 1 Hour	23.036	0.7679	21.922	0.7108	0.917	0.690	2.02	-96.0%
100 Year - 3 Hour	12.675	1.0704	12.163	0.9216	6.777	0.761	2.19	-46.5%
100 Year - 6 Hour	12.721	1.4956	12.206	1.3023	10.360	0.806	2.29	-18.6%
100 Year - 24 Hour	4.550	1.8552	3.955	1.8482	3.864	0.726	2.10	-15.1%

Section 4 – Analytical Approach

The site hydrology was performed utilizing Riverside County Flood Control and Water Conversation District Hydrology Manual, from which pertinent soil and rainfall information was obtained. See Appendix G of this report for the referenced Plates within the Riverside County Flood Control Hydrology Manual.

Rational Method storm flow rates were analyzed by using the "RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM", Riverside County Flood Control & Water Conservation District 1978 Hydrology Manual, produced by Bondamin Engineering.

Existing and Proposed detention basin flow rates were analyzed by utilizing the "SYNTHETIC UNIT HYDROLOGY METHOD COMPUTER PROGRAM", Riverside County Flood Control & Water Conservation District 1978 Hydrology Manual, produced by Bondamin Engineering.

Detention basin routing flow rates were analyzed by utilizing the "FLOOD HYDROGRAPH ROUTING PROGRAM", produced by CIVIL CADD/CIVIL DESIGN.

Basin Outflow Curves were calculated by utilizing a Microsoft Excel Spreadsheet developed by Adkan Engineers based on fundamental fluid mechanics by determining the pressure drop across the orifice allowing for a calculation of flow rate. The fundamental formula used for flow rate in an orifice flow scenario is shown below:

$$Q=C_d \times A \times 2gH$$

"Q" denotes the flow rate
"C_d" is the discharge coefficient
"A" is the Area of the orifice
"g" is the acceleration due to gravity
"H" is the height to the orifice centroid

Hydraulic computations for catch basin sizing, street flow capacities, and sharp/broad crested weir flow rates were performed utilizing software known as "FlowMaster" produced by Haestad Methods and/or "Hydraflow Express" produced by Autodesk Civil 3D.

Section 5 – Conclusion

The hydrologic calculations provided within this report substantiate the preliminary hydrology and hydraulic design of the proposed project, Tentative Tract Map No. 38605, and indicate the following:

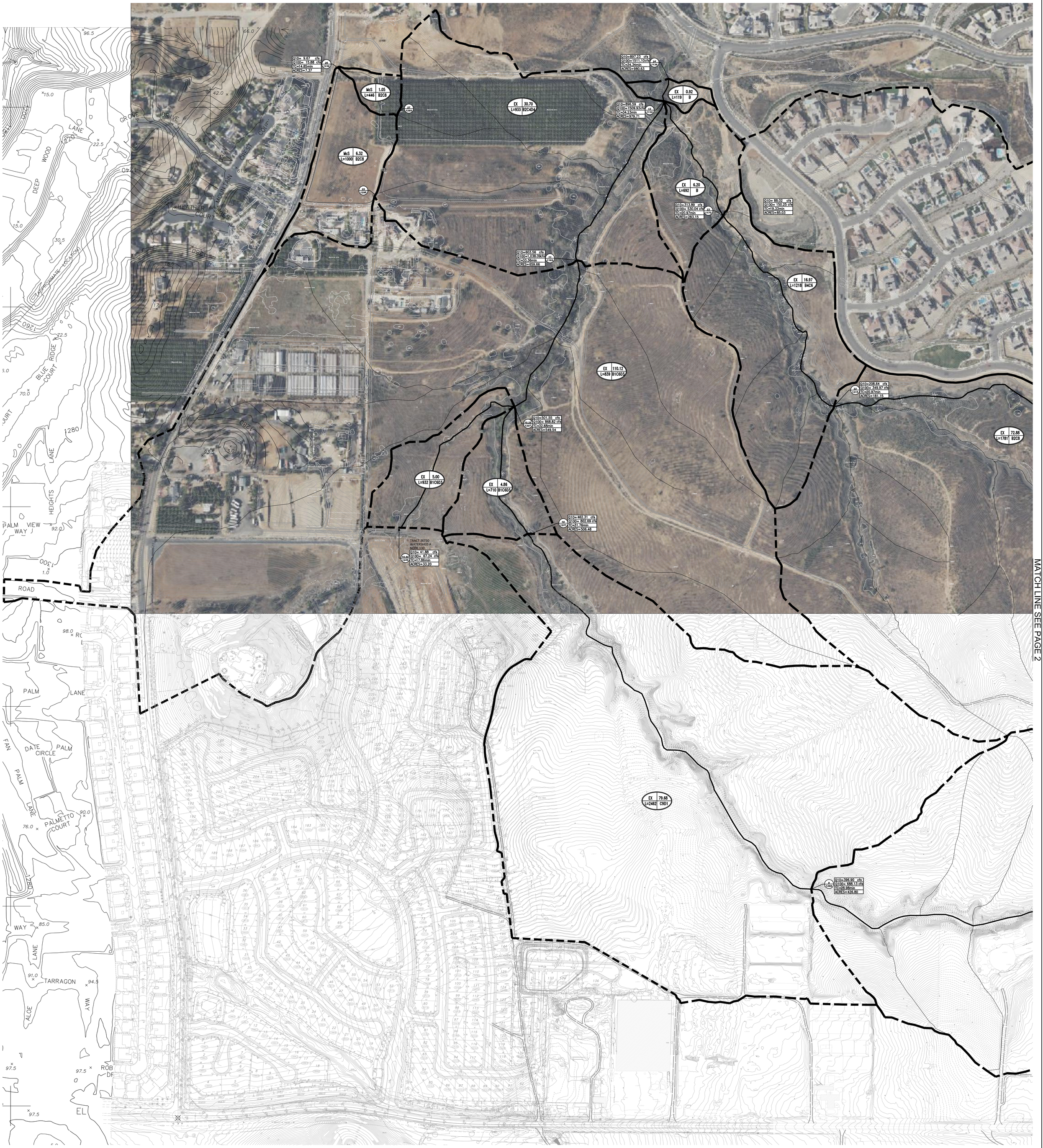
- The proposed storm drain facilities demonstrate the ability to convey the Rational Hydrology Method 10 and 100 year storm events as required by the Riverside County Flood Control Hydrology Manual.

- The proposed extended detention basins provide mitigation for post development peak storm discharge for the 1-hour, 3-hour, 6-hour and 24-hour duration for the 2-year, 5-year, 10-year, and 100-year return frequencies to the pre-development condition.

Therefore, it is our conclusion this project **does not** negatively impact the local community or watershed goals of the Santa Ana River and does not adversely affect downstream facilities while maintaining the adequate conveyance of storm flows for on-site facilities to the criteria for the protection of storm flow as determined by the Riverside County Flood Control Hydrology Manual.

Appendix A – Existing Rational Hydrology Method

EXISTING HYDROLOGY MAP



LEGEND

AREA | ACRES
LENGTH | SOIL

NODE / ELEV
Q10=_____ cfs
Q100=_____ cfs
TC=_____min
ACRES=

WATERSHED BOUNDARY

FLOW PATH

0 150 450
75 300 600
SCALE: 1" = 150'

EXISTING HYDROLOGY MAP
PREPARATION DATE : MAY 2016
REVISION DATE : MARCH 2024

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EXISTING HYDROLOGY MAP

MATCH LINE SEE PAGE 1

MATCH LINE ABOVE

MATCH LINE BELOW

EX 85.03 C

EX 1.00 L=333' C

Q10= 29.62 cfs
Q100= 214.93 cfs
TC=7.40min
ACRES= 109.27

EX 3.57 L=406' C

Q10= 49.88 CFS
Q100= 82.77CFS
TC= 17.58 MIN
ACRES= 49.39

Q10= 15.82 CFS
Q100= 34.35 CFS
TC= 17.58 MIN
ACRES= 9.85

Q10= 34.70 CFS
Q100= 57.74 CFS
TC= 15.56 MIN
ACRES= 27.07

EX 0.56 L=166' C

Q10= 24.41 CFS
Q100= 40.58 CFS
TC= 10.21 MIN
ACRES= 23.74

EX 13.72 L=1128' C

Q10= 65.95 cfs
Q100= 108.86 cfs
TC=15.40min
ACRES=54.16

EX 16.47 L=1004' C

EX 4.95 L=687' C

Q10= 18.38 cfs
Q100= 30.11 cfs
TC=13.11min
ACRES= 12.99

EX 8.04 L=583' C

EX 72.64 L=2452' B2C8

Q10= 341.32 cfs
Q100= 587.30 cfs
TC=26.36min
ACRES= 354.18

EX 66.74 L=2816' B1C8D1

EX 119.10 L=4248' C

Q10= 171.88 cfs
Q100= 291.59 cfs
TC=23.62min
ACRES= 163.35

PROOFF 8.95 L=1000' C

EX 6.82 L=930' C

EX 21.05 L=1674' B2C7D1

EX 8.56 L=972' C5D5

EX 14.56 L=1350' B2C7D1

EX 85.40 L=4065' B2C9D2

EX 9.59 L=914' B1C5

EX 57.38 L=2338' C

EX 7.53 L=952' C

EX 4.37 L=901' C

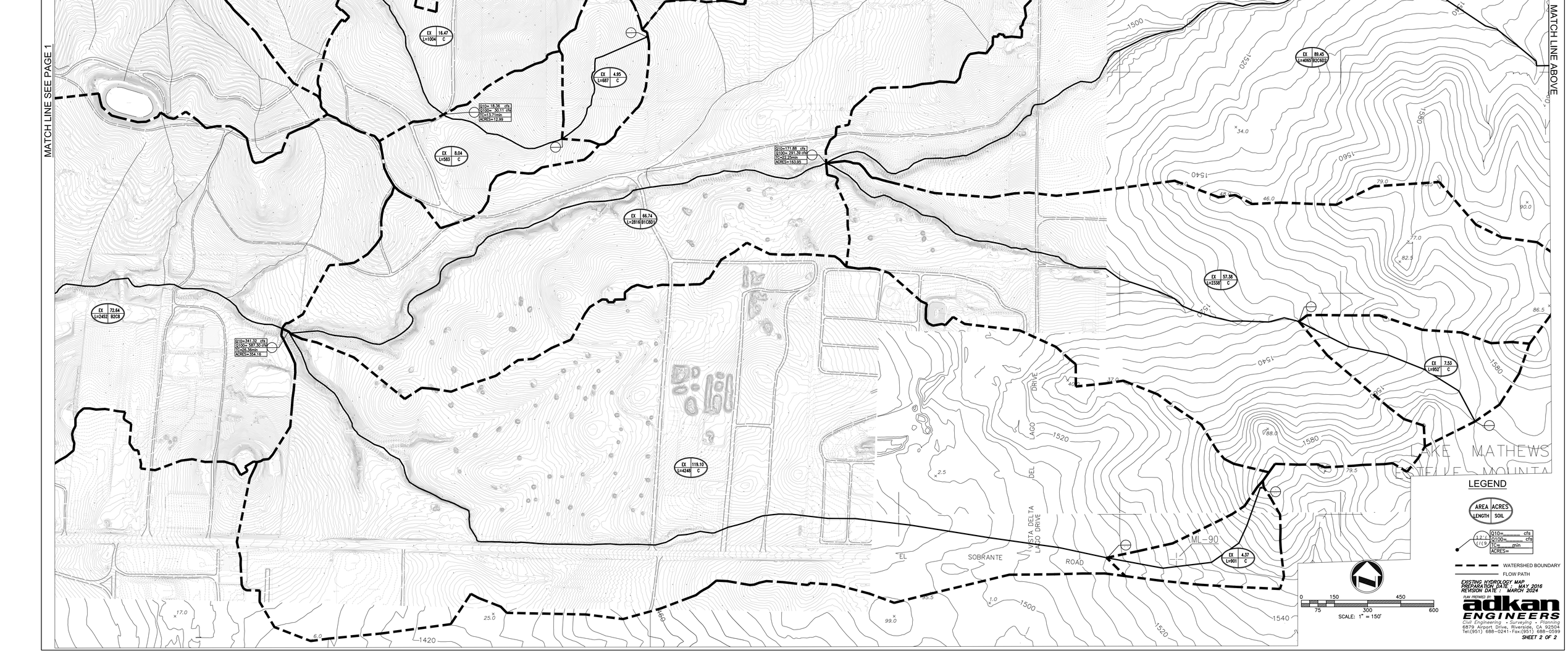
VISTA DEL LAGO DRIVE

BLACKBURN ROAD

EL SOBRANTE ROAD

ML-90

LAKE MATHEWS



EXISTING HYDROLOGY MAP
PREPARATION DATE: MAY 2016
REVISION DATE: MARCH 2024

SCALE: 1" = 150'

PLAN PREPARED BY:

adkan ENGINEERS
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 03/05/24  File:ex10.out
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 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

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Program License Serial Number 5006

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Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =   10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year =  10.0
Calculated rainfall intensity data:
1 hour intensity =  0.829(In/Hr)
Slope of intensity duration curve = 0.5000




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Process from Point/Station        1.000 to Point/Station        2.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   914.000(Ft.)
Top (of initial area) elevation =  1620.000(Ft.)
Bottom (of initial area) elevation =  1572.000(Ft.)
Difference in elevation =    48.000(Ft.)
Slope =    0.05252  s(percent)=       5.25
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.608 min.
Rainfall intensity =      1.680(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.791
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.900
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  85.20
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     12.746(CFS)
Total initial stream area =        9.590(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station        2.000 to Point/Station        3.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of natural channel elevation =   1572.000(Ft.)
End of natural channel elevation =   1444.000(Ft.)
Length of natural channel  =  4065.000(Ft.)
Estimated mean flow rate at midpoint of channel =     72.191(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.64(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0315
Corrected/adjusted channel slope =  0.0315
Travel time =    8.86 min.     TC =   23.47  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.764
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.600
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Decimal fraction soil group D = 0.200
RI index for soil(AMC 2)  =  85.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.326(In/Hr) for a    10.0 year storm
Subarea runoff =     90.636(CFS) for     89.450(Ac.)
Total runoff =    103.382(CFS)       Total area =      99.040(Ac.)


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Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     99.040(Ac.)
Runoff from this stream =    103.382(CFS)
Time of concentration =   23.47 min.
Rainfall intensity =     1.326(In/Hr)


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Process from Point/Station        4.000 to Point/Station        5.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   952.000(Ft.)
Top (of initial area) elevation =  1572.000(Ft.)
Bottom (of initial area) elevation =  1532.000(Ft.)
Difference in elevation =    40.000(Ft.)
Slope =    0.04202  s(percent)=       4.20
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   15.526 min.
Rainfall intensity =      1.630(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.794
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      9.748(CFS)
Total initial stream area =        7.530(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station        5.000 to Point/Station        3.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1532.000(Ft.)
End of natural channel elevation =   1444.000(Ft.)
Length of natural channel  =  2338.000(Ft.)
Estimated mean flow rate at midpoint of channel =     46.889(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.37(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0376
Corrected/adjusted channel slope =  0.0376
Travel time =    5.29 min.     TC =   20.81  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.780
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.408(In/Hr) for a    10.0 year storm
Subarea runoff =     62.990(CFS) for     57.380(Ac.)
Total runoff =     72.738(CFS)       Total area =      64.910(Ac.)


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Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     64.910(Ac.)
Runoff from this stream =     72.738(CFS)
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Time of concentration =   20.81 min.
Rainfall intensity =     1.408(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      103.382     23.47                 1.326
2       72.738     20.81                 1.408
Largest stream flow has longer time of concentration
Qp =    103.382 + sum of
          Qb         Ia/Ib
          72.738 *    0.942 =     68.494
Qp =    171.876

Total of 2 streams to confluence:
Flow rates before confluence point:
     103.382      72.738
Area of streams before confluence:
       99.040       64.910
Results of confluence:
Total flow rate =    171.876(CFS)
Time of concentration =    23.471 min.
Effective stream area after confluence =    163.950(Ac.)


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Process from Point/Station        3.000 to Point/Station        6.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1444.000(Ft.)
End of natural channel elevation =   1369.000(Ft.)
Length of natural channel  =  2816.000(Ft.)
Estimated mean flow rate at midpoint of channel =    206.860(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.67(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0266
Corrected/adjusted channel slope =  0.0266
Travel time =    4.85 min.     TC =   28.32  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.758
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  85.50
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.207(In/Hr) for a    10.0 year storm
Subarea runoff =     61.047(CFS) for     66.740(Ac.)
Total runoff =    232.924(CFS)       Total area =     230.690(Ac.)


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Process from Point/Station        6.000 to Point/Station        6.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    230.690(Ac.)
Runoff from this stream =    232.924(CFS)
Time of concentration =   28.32 min.
Rainfall intensity =     1.207(In/Hr)


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Process from Point/Station        7.000 to Point/Station        8.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   901.000(Ft.)
Top (of initial area) elevation =  1592.000(Ft.)
Bottom (of initial area) elevation =  1516.000(Ft.)
Difference in elevation =    76.000(Ft.)
Slope =    0.08435  s(percent)=       8.44
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.211 min.
Rainfall intensity =      1.767(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
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Runoff Coefficient = 0.802
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      6.189(CFS)
Total initial stream area =        4.370(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station        8.000 to Point/Station        6.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1516.000(Ft.)
End of natural channel elevation =   1369.000(Ft.)
Length of natural channel  =  4248.000(Ft.)
Estimated mean flow rate at midpoint of channel =     90.528(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.57(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0346
Corrected/adjusted channel slope =  0.0346
Travel time =    8.26 min.     TC =   21.47  min.


 Adding area flow to channel
UNDEVELOPED (fair cover) subarea
Runoff Coefficient = 0.717
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  79.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.386(In/Hr) for a    10.0 year storm
Subarea runoff =    118.309(CFS) for    119.100(Ac.)
Total runoff =    124.498(CFS)       Total area =     123.470(Ac.)


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Process from Point/Station        6.000 to Point/Station        6.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =    123.470(Ac.)
Runoff from this stream =    124.498(CFS)
Time of concentration =   21.47 min.
Rainfall intensity =     1.386(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      232.924     28.32                 1.207
2      124.498     21.47                 1.386
Largest stream flow has longer time of concentration
Qp =    232.924 + sum of
          Qb          Ia/Ib
         124.498 *    0.871 =    108.400
Qp =    341.324

Total of 2 streams to confluence:
Flow rates before confluence point:
     232.924     124.498
Area of streams before confluence:
      230.690      123.470
Results of confluence:
Total flow rate =    341.324(CFS)
Time of concentration =    28.323 min.
Effective stream area after confluence =    354.160(Ac.)


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Process from Point/Station        6.000 to Point/Station        9.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1369.000(Ft.)
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End of natural channel elevation =   1286.000(Ft.)
Length of natural channel  =  2452.000(Ft.)
Estimated mean flow rate at midpoint of channel =    376.328(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  13.16(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0338
Corrected/adjusted channel slope =  0.0338
Travel time =    3.11 min.     TC =   31.43  min.


 Adding area flow to channel
UNDEVELOPED (fair cover) subarea
Runoff Coefficient = 0.668
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  77.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.146(In/Hr) for a    10.0 year storm
Subarea runoff =     55.574(CFS) for     72.640(Ac.)
Total runoff =    396.898(CFS)       Total area =     426.800(Ac.)


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Process from Point/Station        9.000 to Point/Station       10.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1288.000(Ft.)
End of natural channel elevation =   1221.000(Ft.)
Length of natural channel  =  2462.000(Ft.)
Estimated mean flow rate at midpoint of channel =    433.947(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  12.35(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0272
Corrected/adjusted channel slope =  0.0272
Travel time =    3.32 min.     TC =   34.75  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.754
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.900
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  86.30
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.089(In/Hr) for a    10.0 year storm
Subarea runoff =     65.416(CFS) for     79.680(Ac.)
Total runoff =    462.314(CFS)       Total area =     506.480(Ac.)


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Process from Point/Station       10.000 to Point/Station       10.250
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1221.000(Ft.)
End of natural channel elevation =   1207.000(Ft.)
Length of natural channel  =   710.000(Ft.)
Estimated mean flow rate at midpoint of channel =    464.532(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  10.74(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0197
Corrected/adjusted channel slope =  0.0197
Travel time =    1.10 min.     TC =   35.85  min.
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 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.750
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2)  =  86.10
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.073(In/Hr) for a    10.0 year storm
Subarea runoff =      3.907(CFS) for      4.860(Ac.)
Total runoff =    466.222(CFS)       Total area =     511.340(Ac.)


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Process from Point/Station       10.250 to Point/Station       10.250
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    511.340(Ac.)
Runoff from this stream =    466.222(CFS)
Time of concentration =   35.85 min.
Rainfall intensity =     1.073(In/Hr)


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Process from Point/Station       10.500 to Point/Station       10.500
**** USER DEFINED FLOW INFORMATION AT A POINT ****
______________________________________________________________________________
Rainfall intensity =      1.520(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.773
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
User specified values are as follows:
TC =  17.86 min.  Rain intensity =       1.52(In/Hr)
Total area =        33.20(Ac.)  Total runoff =     67.24(CFS)


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Process from Point/Station       10.500 to Point/Station       10.250
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1249.000(Ft.)
End of natural channel elevation =   1207.000(Ft.)
Length of natural channel  =   932.000(Ft.)
Estimated mean flow rate at midpoint of channel =     72.303(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.15(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0451
Corrected/adjusted channel slope =  0.0451
Travel time =    1.70 min.     TC =   19.56  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.784
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2)  =  86.10
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.452(In/Hr) for a    10.0 year storm
Subarea runoff =      5.691(CFS) for      5.000(Ac.)
Total runoff =     72.931(CFS)       Total area =      38.200(Ac.)


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Process from Point/Station       10.250 to Point/Station       10.250
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     38.200(Ac.)
Runoff from this stream =     72.931(CFS)
Time of concentration =   19.56 min.
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Rainfall intensity =     1.452(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                (In/Hr)


1      466.222     35.85                 1.073
2       72.931     19.56                 1.452
Largest stream flow has longer time of concentration
Qp =    466.222 + sum of
          Qb         Ia/Ib
          72.931 *    0.739 =     53.865
Qp =    520.086

Total of 2 streams to confluence:
Flow rates before confluence point:
     466.222      72.931
Area of streams before confluence:
      511.340       38.200
Results of confluence:
Total flow rate =    520.086(CFS)
Time of concentration =    35.854 min.
Effective stream area after confluence =    549.540(Ac.)


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Process from Point/Station       10.250 to Point/Station       11.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1207.000(Ft.)
End of natural channel elevation =   1169.000(Ft.)
Length of natural channel  =   839.000(Ft.)
Estimated mean flow rate at midpoint of channel =    572.195(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  17.40(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0453
Corrected/adjusted channel slope =  0.0453
Travel time =    0.80 min.     TC =   36.66  min.


 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.873
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2)  =  75.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      1.061(In/Hr) for a    10.0 year storm
Subarea runoff =    102.024(CFS) for    110.120(Ac.)
Total runoff =    622.111(CFS)       Total area =     659.660(Ac.)


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Process from Point/Station       11.000 to Point/Station       12.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1169.000(Ft.)
End of natural channel elevation =   1139.000(Ft.)
Length of natural channel  =   933.000(Ft.)
Estimated mean flow rate at midpoint of channel =    636.587(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  15.18(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0322
Corrected/adjusted channel slope =  0.0322
Travel time =    1.02 min.     TC =   37.68  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.741
Decimal fraction soil group A = 0.000
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Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.400
Decimal fraction soil group D = 0.400
RI index for soil(AMC 2)  =  85.60
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.046(In/Hr) for a    10.0 year storm
Subarea runoff =     23.804(CFS) for     30.700(Ac.)
Total runoff =    645.915(CFS)       Total area =     690.360(Ac.)


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Process from Point/Station       12.000 to Point/Station       12.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =    690.360(Ac.)
Runoff from this stream =    645.915(CFS)
Time of concentration =   37.68 min.
Rainfall intensity =     1.046(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station       16.000 to Point/Station       17.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   972.000(Ft.)
Top (of initial area) elevation =  1518.000(Ft.)
Bottom (of initial area) elevation =  1451.000(Ft.)
Difference in elevation =    67.000(Ft.)
Slope =    0.06893  s(percent)=       6.89
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.179 min.
Rainfall intensity =      1.706(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.810
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.500
Decimal fraction soil group D = 0.500
RI index for soil(AMC 2)  =  87.50
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     11.847(CFS)
Total initial stream area =        8.580(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station       17.000 to Point/Station       17.100
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1451.000(Ft.)
End of natural channel elevation =   1371.000(Ft.)
Length of natural channel  =  1350.000(Ft.)
Estimated mean flow rate at midpoint of channel =     21.899(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.48(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0593
Corrected/adjusted channel slope =  0.0593
Travel time =    3.01 min.     TC =   17.19  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.779
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.700
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  84.70
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.549(In/Hr) for a    10.0 year storm
Subarea runoff =     17.567(CFS) for     14.560(Ac.)
Total runoff =     29.415(CFS)       Total area =      23.140(Ac.)


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Process from Point/Station       17.100 to Point/Station       17.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
```

```
Upstream point/station elevation =  1371.000(Ft.)
Downstream point/station elevation =  1360.000(Ft.)
Pipe length  =   473.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    29.415(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    29.415(CFS)
Normal flow depth in pipe =   17.04(In.)
Flow top width inside pipe =   21.78(In.)
Critical Depth =   22.24(In.)
Pipe flow velocity =     12.33(Ft/s)
Travel time through pipe =    0.64 min.
Time of concentration (TC) =    17.83 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       17.200 to Point/Station       18.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1360.000(Ft.)
End of natural channel elevation =   1347.000(Ft.)
Length of natural channel  =   166.000(Ft.)
Estimated mean flow rate at midpoint of channel =     29.771(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.35(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0783
Corrected/adjusted channel slope =  0.0783
Travel time =    0.30 min.     TC =   18.12  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.787
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.509(In/Hr) for a    10.0 year storm
Subarea runoff =      0.665(CFS) for      0.560(Ac.)
Total runoff =     30.079(CFS)       Total area =      23.700(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       18.000 to Point/Station       18.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     23.700(Ac.)
Runoff from this stream =     30.079(CFS)
Time of concentration =   18.12 min.
Rainfall intensity =     1.509(In/Hr)


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Process from Point/Station       19.000 to Point/Station       20.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   687.000(Ft.)
Top (of initial area) elevation =  1478.000(Ft.)
Bottom (of initial area) elevation =  1430.000(Ft.)
Difference in elevation =    48.000(Ft.)
Slope =    0.06987  s(percent)=       6.99
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.308 min.
Rainfall intensity =      1.831(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.805
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      7.291(CFS)
Total initial stream area =       4.950(Ac.)
Pervious area fraction = 1.000
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Process from Point/Station       20.000 to Point/Station       21.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1430.000(Ft.)
End of natural channel elevation =   1400.000(Ft.)
Length of natural channel  =   583.000(Ft.)
Estimated mean flow rate at midpoint of channel =     13.212(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.09(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0515
Corrected/adjusted channel slope =  0.0515
Travel time =    1.60 min.     TC =   13.90  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.799
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.722(In/Hr) for a    10.0 year storm
Subarea runoff =     11.068(CFS) for      8.040(Ac.)
Total runoff =     18.359(CFS)       Total area =      12.990(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       21.000 to Point/Station       18.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1400.000(Ft.)
End of natural channel elevation =   1347.000(Ft.)
Length of natural channel  =  1004.000(Ft.)
Estimated mean flow rate at midpoint of channel =     29.998(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.69(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0528
Corrected/adjusted channel slope =  0.0528
Travel time =    2.17 min.     TC =   16.08  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.793
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.602(In/Hr) for a    10.0 year storm
Subarea runoff =     20.908(CFS) for     16.470(Ac.)
Total runoff =     39.267(CFS)       Total area =      29.460(Ac.)


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Process from Point/Station       18.000 to Point/Station       18.000
**** CONFLUENCE OF MINOR STREAMS ****
----------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     29.460(Ac.)
Runoff from this stream =     39.267(CFS)
Time of concentration =   16.08 min.
Rainfall intensity =     1.602(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                (In/Hr)


1       30.079     18.12                1.509
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```
2       39.267     16.08                 1.602
Largest stream flow has longer or shorter time of concentration
Qp =     39.267 + sum of
          Qa          Tb/Ta
          30.079 *    0.887 =     26.685
Qp =     65.952

Total of 2 streams to confluence:
Flow rates before confluence point:
      30.079      39.267
Area of streams before confluence:
       23.700       29.460
Results of confluence:
Total flow rate =     65.952(CFS)
Time of concentration =    16.079 min.
Effective stream area after confluence =     53.160(Ac.)


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Process from Point/Station       18.000 to Point/Station       15.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1347.000(Ft.)
End of natural channel elevation =   1299.000(Ft.)
Length of natural channel  =  1128.000(Ft.)
Estimated mean flow rate at midpoint of channel =     74.462(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.97(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0426
Corrected/adjusted channel slope =  0.0426
Travel time =    2.10 min.     TC =   18.18  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.787
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.506(In/Hr) for a    10.0 year storm
Subarea runoff =     16.259(CFS) for     13.720(Ac.)
Total runoff =     82.211(CFS)       Total area =      66.880(Ac.)


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Process from Point/Station       15.000 to Point/Station       15.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     66.880(Ac.)
Runoff from this stream =     82.211(CFS)
Time of concentration =   18.18 min.
Rainfall intensity =     1.506(In/Hr)


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Process from Point/Station       13.000 to Point/Station       14.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   930.000(Ft.)
Top (of initial area) elevation =  1522.000(Ft.)
Bottom (of initial area) elevation =  1448.000(Ft.)
Difference in elevation =    74.000(Ft.)
Slope =    0.07957  s(percent)=       7.96
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.537 min.
Rainfall intensity =      1.746(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.800
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      9.529(CFS)
Total initial stream area =        6.820(Ac.)
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Pervious area fraction = 1.000

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Process from Point/Station       14.000 to Point/Station       14.100
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1448.000(Ft.)
End of natural channel elevation =   1363.000(Ft.)
Length of natural channel  =  1674.000(Ft.)
Estimated mean flow rate at midpoint of channel =     24.236(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.11(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0508
Corrected/adjusted channel slope =  0.0508
Travel time =    3.92 min.     TC =   17.46  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.778
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.700
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  84.70
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.537(In/Hr) for a    10.0 year storm
Subarea runoff =     25.175(CFS) for     21.050(Ac.)
Total runoff =     34.704(CFS)       Total area =      27.870(Ac.)


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Process from Point/Station       14.100 to Point/Station       14.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1363.000(Ft.)
Downstream point/station elevation =  1359.000(Ft.)
Pipe length  =    86.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    34.704(CFS)
Nearest computed pipe diameter  =     21.00(In.)
Calculated individual pipe flow  =    34.704(CFS)
Normal flow depth in pipe =   17.53(In.)
Flow top width inside pipe =   15.60(In.)
Critical depth could not be calculated.
Pipe flow velocity =     16.18(Ft/s)
Travel time through pipe =    0.09 min.
Time of concentration (TC) =    17.55 min.


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Process from Point/Station       14.300 to Point/Station       14.400
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.788
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    17.55 min.
Rainfall intensity =      1.533(In/Hr) for a    10.0 year storm
Subarea runoff =     10.818(CFS) for      8.950(Ac.)
Total runoff =     45.522(CFS)       Total area =      36.820(Ac.)


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Process from Point/Station       14.400 to Point/Station       14.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1377.000(Ft.)
Downstream point/station elevation =  1359.000(Ft.)
Pipe length  =   366.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    45.522(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    45.522(CFS)
Normal flow depth in pipe =   17.93(In.)
Flow top width inside pipe =   20.87(In.)
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Critical depth could not be calculated.
Pipe flow velocity =     18.09(Ft/s)
Travel time through pipe =    0.34 min.
Time of concentration (TC) =    17.88 min.


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Process from Point/Station       14.200 to Point/Station       14.500
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1359.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =    75.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    45.522(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    45.522(CFS)
Normal flow depth in pipe =   17.34(In.)
Flow top width inside pipe =   21.49(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.74(Ft/s)
Travel time through pipe =    0.07 min.
Time of concentration (TC) =    17.95 min.


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Process from Point/Station       14.500 to Point/Station       14.600
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1355.000(Ft.)
End of natural channel elevation =   1329.000(Ft.)
Length of natural channel  =   406.000(Ft.)
Estimated mean flow rate at midpoint of channel =     47.729(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.66(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0640
Corrected/adjusted channel slope =  0.0640
Travel time =    0.70 min.     TC =   18.65  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.785
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.487(In/Hr) for a    10.0 year storm
Subarea runoff =      4.169(CFS) for      3.570(Ac.)
Total runoff =     49.692(CFS)       Total area =      40.390(Ac.)


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Process from Point/Station       14.600 to Point/Station       14.700
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1329.000(Ft.)
Downstream point/station elevation =  1319.000(Ft.)
Pipe length  =   258.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    49.692(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    49.692(CFS)
Normal flow depth in pipe =   18.52(In.)
Flow top width inside pipe =   25.07(In.)
Critical depth could not be calculated.
Pipe flow velocity =     17.09(Ft/s)
Travel time through pipe =    0.25 min.
Time of concentration (TC) =    18.90 min.


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Process from Point/Station       14.700 to Point/Station       15.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1319.000(Ft.)
End of natural channel elevation =   1299.000(Ft.)
Length of natural channel  =   333.000(Ft.)
Estimated mean flow rate at midpoint of channel =     50.307(CFS)
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Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.50(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0601
Corrected/adjusted channel slope =  0.0601
Travel time =    0.58 min.     TC =   19.49  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.783
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.455(In/Hr) for a    10.0 year storm
Subarea runoff =      1.139(CFS) for      1.000(Ac.)
Total runoff =     50.831(CFS)       Total area =      41.390(Ac.)


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Process from Point/Station       15.000 to Point/Station       15.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     41.390(Ac.)
Runoff from this stream =     50.831(CFS)
Time of concentration =   19.49 min.
Rainfall intensity =     1.455(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       82.211     18.18                 1.506
2       50.831     19.49                 1.455
Largest stream flow has longer or shorter time of concentration
Qp =     82.211 + sum of
          Qa          Tb/Ta
          50.831 *    0.933 =     47.409
Qp =    129.620

Total of 2 streams to confluence:
Flow rates before confluence point:
      82.211      50.831
Area of streams before confluence:
       66.880       41.390
Results of confluence:
Total flow rate =    129.620(CFS)
Time of concentration =    18.175 min.
Effective stream area after confluence =    108.270(Ac.)


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Process from Point/Station       15.000 to Point/Station       22.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1299.000(Ft.)
End of natural channel elevation =   1215.000(Ft.)
Length of natural channel  =  1781.000(Ft.)
Estimated mean flow rate at midpoint of channel =    173.246(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  12.18(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0472
Corrected/adjusted channel slope =  0.0472
Travel time =    2.44 min.     TC =   20.61  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.766
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
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```
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.415(In/Hr) for a    10.0 year storm
Subarea runoff =     79.022(CFS) for     72.880(Ac.)
Total runoff =    208.642(CFS)       Total area =     181.150(Ac.)


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Process from Point/Station       22.000 to Point/Station       23.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1215.000(Ft.)
End of natural channel elevation =   1170.000(Ft.)
Length of natural channel  =  1218.000(Ft.)
Estimated mean flow rate at midpoint of channel =    218.415(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  11.59(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0369
Corrected/adjusted channel slope =  0.0369
Travel time =    1.75 min.     TC =   22.36  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.748
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.400
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  82.80
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.358(In/Hr) for a    10.0 year storm
Subarea runoff =     17.228(CFS) for     16.970(Ac.)
Total runoff =    225.870(CFS)       Total area =     198.120(Ac.)


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Process from Point/Station       23.000 to Point/Station       23.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.762
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Time of concentration =    22.36 min.
Rainfall intensity =      1.358(In/Hr) for a    10.0 year storm
Subarea runoff =     88.024(CFS) for     85.030(Ac.)
Total runoff =    313.895(CFS)       Total area =     283.150(Ac.)


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Process from Point/Station       23.000 to Point/Station       12.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1170.000(Ft.)
End of natural channel elevation =   1139.000(Ft.)
Length of natural channel  =   692.000(Ft.)
Estimated mean flow rate at midpoint of channel =    317.331(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  14.34(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0448
Corrected/adjusted channel slope =  0.0448
Travel time =    0.80 min.     TC =   23.17  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.702
```

```
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  78.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.334(In/Hr) for a    10.0 year storm
Subarea runoff =      5.808(CFS) for      6.200(Ac.)
Total runoff =    319.703(CFS)       Total area =     289.350(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       12.000 to Point/Station       12.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =    289.350(Ac.)
Runoff from this stream =    319.703(CFS)
Time of concentration =   23.17 min.
Rainfall intensity =     1.334(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)              (In/Hr)
1      645.915     37.68               1.046
2      319.703     23.17               1.334
Largest stream flow has longer time of concentration
Qp =    645.915 + sum of
          Qb         Ia/Ib
         319.703 *    0.784 =    250.679
Qp =    896.594

Total of 2 main streams to confluence:
Flow rates before confluence point:
     645.915     319.703
Area of streams before confluence:
      690.360      289.350
Results of confluence:
Total flow rate =    896.594(CFS)
Time of concentration =    37.683 min.
Effective stream area after confluence  =    979.710(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       12.000 to Point/Station       24.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1139.000(Ft.)
End of natural channel elevation =   1136.000(Ft.)
Length of natural channel  =   119.000(Ft.)
Estimated mean flow rate at midpoint of channel =    897.015(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  15.02(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0252
Corrected/adjusted channel slope =  0.0252
Travel time =    0.13 min.     TC =   37.81  min.
 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.662
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  78.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.044(In/Hr) for a    10.0 year storm
Subarea runoff =      0.636(CFS) for      0.920(Ac.)
Total runoff =    897.230(CFS)       Total area =     980.630(Ac.)
End of computations, total study area =          980.63 (Ac.)
The following figures maybe used for a unit hydrograph study of the same area.
Area averaged pervious area fraction(Ap) = 0.839
Area averaged RI index number =  80.8
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 09/22/16  File:mcs10.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

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Program License Serial Number 5006

------------------------------------------------------------------------
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =   10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year =  10.0
Calculated rainfall intensity data:
1 hour intensity =  0.829(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       25.000 to Point/Station       26.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =  1000.000(Ft.)
Top (of initial area) elevation =  1296.000(Ft.)
Bottom (of initial area) elevation =  1238.000(Ft.)
Difference in elevation =    58.000(Ft.)
Slope =    0.05800  s(percent)=       5.80
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.845 min.
Rainfall intensity =      1.667(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.784
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      8.260(CFS)
Total initial stream area =        6.320(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       26.000 to Point/Station       26.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      6.320(Ac.)
Runoff from this stream =      8.260(CFS)
Time of concentration =   14.85 min.
Rainfall intensity =     1.667(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       27.000 to Point/Station       26.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   446.000(Ft.)
Top (of initial area) elevation =  1289.000(Ft.)
Bottom (of initial area) elevation =  1238.000(Ft.)
Difference in elevation =    51.000(Ft.)
Slope =    0.11435  s(percent)=      11.43
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    9.383 min.
```

```
Rainfall intensity =      2.097(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.805
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      1.773(CFS)
Total initial stream area =        1.050(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       26.000 to Point/Station       26.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      1.050(Ac.)
Runoff from this stream =      1.773(CFS)
Time of concentration =    9.38 min.
Rainfall intensity =     2.097(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        8.260     14.85                 1.667
2        1.773      9.38                 2.097
Largest stream flow has longer time of concentration
Qp =      8.260 + sum of
         Qb         Ia/Ib
          1.773 *    0.795 =      1.410
Qp =      9.669

Total of 2 streams to confluence:
Flow rates before confluence point:
       8.260       1.773
Area of streams before confluence:
       6.320        1.050
Results of confluence:
Total flow rate =      9.669(CFS)
Time of concentration =    14.845 min.
Effective stream area after confluence =      7.370(Ac.)
End of computations, total study area =            7.37 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number =  84.4
```

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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 03/05/24  File:ex100.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

------------------------------------------------------------------------
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =  100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity =  1.300(In/Hr)
Slope of intensity duration curve = 0.5000




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Process from Point/Station        1.000 to Point/Station        2.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   914.000(Ft.)
Top (of initial area) elevation =  1620.000(Ft.)
Bottom (of initial area) elevation =  1572.000(Ft.)
Difference in elevation =    48.000(Ft.)
Slope =    0.05252  s(percent)=       5.25
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.608 min.
Rainfall intensity =      2.635(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.827
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.900
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  85.20
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     20.902(CFS)
Total initial stream area =        9.590(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station        2.000 to Point/Station        3.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of natural channel elevation =   1572.000(Ft.)
End of natural channel elevation =   1444.000(Ft.)
Length of natural channel  =  4065.000(Ft.)
Estimated mean flow rate at midpoint of channel =    118.383(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.86(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0315
Corrected/adjusted channel slope =  0.0315
Travel time =    7.64 min.     TC =   22.25  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.811
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.600
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Decimal fraction soil group D = 0.200
RI index for soil(AMC 2)  =  85.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.135(In/Hr) for a   100.0 year storm
Subarea runoff =    154.788(CFS) for     89.450(Ac.)
Total runoff =    175.690(CFS)       Total area =      99.040(Ac.)


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Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     99.040(Ac.)
Runoff from this stream =    175.690(CFS)
Time of concentration =   22.25 min.
Rainfall intensity =     2.135(In/Hr)


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Process from Point/Station        4.000 to Point/Station        5.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   952.000(Ft.)
Top (of initial area) elevation =  1572.000(Ft.)
Bottom (of initial area) elevation =  1532.000(Ft.)
Difference in elevation =    40.000(Ft.)
Slope =    0.04202  s(percent)=       4.20
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   15.526 min.
Rainfall intensity =      2.556(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.830
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     15.964(CFS)
Total initial stream area =        7.530(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        5.000 to Point/Station        3.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1532.000(Ft.)
End of natural channel elevation =   1444.000(Ft.)
Length of natural channel  =  2338.000(Ft.)
Estimated mean flow rate at midpoint of channel =     76.786(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.51(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0376
Corrected/adjusted channel slope =  0.0376
Travel time =    4.58 min.     TC =   20.10  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.821
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.246(In/Hr) for a   100.0 year storm
Subarea runoff =    105.760(CFS) for     57.380(Ac.)
Total runoff =    121.723(CFS)       Total area =      64.910(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        3.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     64.910(Ac.)
Runoff from this stream =    121.723(CFS)
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```
Time of concentration =   20.10 min.
Rainfall intensity =     2.246(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      175.690     22.25                 2.135
2      121.723     20.10                 2.246
Largest stream flow has longer time of concentration
Qp =    175.690 + sum of
          Qb         Ia/Ib
         121.723 *    0.950 =    115.695
Qp =    291.385

Total of 2 streams to confluence:
Flow rates before confluence point:
     175.690     121.723
Area of streams before confluence:
       99.040       64.910
Results of confluence:
Total flow rate =    291.385(CFS)
Time of concentration =    22.253 min.
Effective stream area after confluence =    163.950(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        6.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1444.000(Ft.)
End of natural channel elevation =   1369.000(Ft.)
Length of natural channel  =  2816.000(Ft.)
Estimated mean flow rate at midpoint of channel =    350.693(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  11.41(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0266
Corrected/adjusted channel slope =  0.0266
Travel time =    4.11 min.     TC =   26.36  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.807
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  85.50
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.961(In/Hr) for a   100.0 year storm
Subarea runoff =    105.619(CFS) for     66.740(Ac.)
Total runoff =    397.004(CFS)       Total area =     230.690(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        6.000 to Point/Station        6.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    230.690(Ac.)
Runoff from this stream =    397.004(CFS)
Time of concentration =   26.36 min.
Rainfall intensity =     1.961(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        7.000 to Point/Station        8.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   901.000(Ft.)
Top (of initial area) elevation =  1592.000(Ft.)
Bottom (of initial area) elevation =  1516.000(Ft.)
Difference in elevation =    76.000(Ft.)
Slope =    0.08435  s(percent)=       8.44
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.211 min.
Rainfall intensity =      2.770(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
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```
Runoff Coefficient = 0.835
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     10.104(CFS)
Total initial stream area =        4.370(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        8.000 to Point/Station        6.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1516.000(Ft.)
End of natural channel elevation =   1369.000(Ft.)
Length of natural channel  =  4248.000(Ft.)
Estimated mean flow rate at midpoint of channel =    147.797(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.94(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0346
Corrected/adjusted channel slope =  0.0346
Travel time =    7.12 min.     TC =   20.33  min.


 Adding area flow to channel
UNDEVELOPED (fair cover) subarea
Runoff Coefficient = 0.777
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  79.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.233(In/Hr) for a   100.0 year storm
Subarea runoff =    206.575(CFS) for    119.100(Ac.)
Total runoff =    216.680(CFS)       Total area =     123.470(Ac.)


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Process from Point/Station        6.000 to Point/Station        6.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =    123.470(Ac.)
Runoff from this stream =    216.680(CFS)
Time of concentration =   20.33 min.
Rainfall intensity =     2.233(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      397.004     26.36                 1.961
2      216.680     20.33                 2.233
Largest stream flow has longer time of concentration
Qp =    397.004 + sum of
          Qb         Ia/Ib
         216.680 *    0.878 =    190.292
Qp =    587.296

Total of 2 streams to confluence:
Flow rates before confluence point:
     397.004     216.680
Area of streams before confluence:
      230.690      123.470
Results of confluence:
Total flow rate =    587.296(CFS)
Time of concentration =    26.365 min.
Effective stream area after confluence =    354.160(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        6.000 to Point/Station        9.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1369.000(Ft.)
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End of natural channel elevation =   1286.000(Ft.)
Length of natural channel  =  2452.000(Ft.)
Estimated mean flow rate at midpoint of channel =    647.525(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  15.66(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0338
Corrected/adjusted channel slope =  0.0338
Travel time =    2.61 min.     TC =   28.98  min.


 Adding area flow to channel
UNDEVELOPED (fair cover) subarea
Runoff Coefficient = 0.742
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  77.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.871(In/Hr) for a   100.0 year storm
Subarea runoff =    100.833(CFS) for     72.640(Ac.)
Total runoff =    688.129(CFS)       Total area =     426.800(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        9.000 to Point/Station       10.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1288.000(Ft.)
End of natural channel elevation =   1221.000(Ft.)
Length of natural channel  =  2462.000(Ft.)
Estimated mean flow rate at midpoint of channel =    752.363(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  14.74(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0272
Corrected/adjusted channel slope =  0.0272
Travel time =    2.78 min.     TC =   31.76  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.805
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.900
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  86.30
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.787(In/Hr) for a   100.0 year storm
Subarea runoff =    114.566(CFS) for     79.680(Ac.)
Total runoff =    802.695(CFS)       Total area =     506.480(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       10.000 to Point/Station       10.250
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1221.000(Ft.)
End of natural channel elevation =   1207.000(Ft.)
Length of natural channel  =   710.000(Ft.)
Estimated mean flow rate at midpoint of channel =    806.546(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  12.83(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0197
Corrected/adjusted channel slope =  0.0197
Travel time =    0.92 min.     TC =   32.68  min.
```

```
 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.802
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2)  =  86.10
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.761(In/Hr) for a   100.0 year storm
Subarea runoff =      6.866(CFS) for      4.860(Ac.)
Total runoff =    809.560(CFS)       Total area =     511.340(Ac.)


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Process from Point/Station       10.250 to Point/Station       10.250
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    511.340(Ac.)
Runoff from this stream =    809.560(CFS)
Time of concentration =   32.68 min.
Rainfall intensity =     1.761(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       10.500 to Point/Station       10.500
**** USER DEFINED FLOW INFORMATION AT A POINT ****
______________________________________________________________________________
Rainfall intensity =      2.383(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.810
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
User specified values are as follows:
TC =  17.86 min.  Rain intensity =       2.38(In/Hr)
Total area =        33.20(Ac.)  Total runoff =     67.24(CFS)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       10.500 to Point/Station       10.250
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1249.000(Ft.)
End of natural channel elevation =   1207.000(Ft.)
Length of natural channel  =   932.000(Ft.)
Estimated mean flow rate at midpoint of channel =     72.303(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.15(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0451
Corrected/adjusted channel slope =  0.0451
Travel time =    1.70 min.     TC =   19.56  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.822
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2)  =  86.10
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.277(In/Hr) for a   100.0 year storm
Subarea runoff =      9.361(CFS) for      5.000(Ac.)
Total runoff =     76.601(CFS)       Total area =      38.200(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       10.250 to Point/Station       10.250
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     38.200(Ac.)
Runoff from this stream =     76.601(CFS)
Time of concentration =   19.56 min.
```

```
Rainfall intensity =     2.277(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                (In/Hr)


1      809.560     32.68                 1.761
2       76.601     19.56                 2.277
Largest stream flow has longer time of concentration
Qp =    809.560 + sum of
          Qb         Ia/Ib
          76.601 *    0.774 =     59.258
Qp =    868.818

Total of 2 streams to confluence:
Flow rates before confluence point:
     809.560      76.601
Area of streams before confluence:
      511.340       38.200
Results of confluence:
Total flow rate =    868.818(CFS)
Time of concentration =    32.682 min.
Effective stream area after confluence =    549.540(Ac.)


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Process from Point/Station       10.250 to Point/Station       11.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1207.000(Ft.)
End of natural channel elevation =   1169.000(Ft.)
Length of natural channel  =   839.000(Ft.)
Estimated mean flow rate at midpoint of channel =    955.867(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  20.55(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0453
Corrected/adjusted channel slope =  0.0453
Travel time =    0.68 min.     TC =   33.36  min.


 Adding area flow to channel
USER INPUT of soil data for subarea
Runoff Coefficient = 0.882
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.300
RI index for soil(AMC 2)  =  75.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      1.743(In/Hr) for a   100.0 year storm
Subarea runoff =    169.273(CFS) for    110.120(Ac.)
Total runoff =   1038.091(CFS)       Total area =     659.660(Ac.)


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Process from Point/Station       11.000 to Point/Station       12.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1169.000(Ft.)
End of natural channel elevation =   1139.000(Ft.)
Length of natural channel  =   933.000(Ft.)
Estimated mean flow rate at midpoint of channel =   1062.247(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  17.93(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0322
Corrected/adjusted channel slope =  0.0322
Travel time =    0.87 min.     TC =   34.23  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.796
Decimal fraction soil group A = 0.000
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```
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.400
Decimal fraction soil group D = 0.400
RI index for soil(AMC 2)  =  85.60
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.721(In/Hr) for a   100.0 year storm
Subarea runoff =     42.073(CFS) for     30.700(Ac.)
Total runoff =   1080.164(CFS)       Total area =     690.360(Ac.)


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Process from Point/Station       12.000 to Point/Station       12.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =    690.360(Ac.)
Runoff from this stream =   1080.164(CFS)
Time of concentration =   34.23 min.
Rainfall intensity =     1.721(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station       16.000 to Point/Station       17.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   972.000(Ft.)
Top (of initial area) elevation =  1518.000(Ft.)
Bottom (of initial area) elevation =  1451.000(Ft.)
Difference in elevation =    67.000(Ft.)
Slope =    0.06893  s(percent)=       6.89
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.179 min.
Rainfall intensity =      2.674(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.840
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 0.500
Decimal fraction soil group D = 0.500
RI index for soil(AMC 2)  =  87.50
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     19.277(CFS)
Total initial stream area =        8.580(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station       17.000 to Point/Station       17.100
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1451.000(Ft.)
End of natural channel elevation =   1371.000(Ft.)
Length of natural channel  =  1350.000(Ft.)
Estimated mean flow rate at midpoint of channel =     35.633(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.55(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0593
Corrected/adjusted channel slope =  0.0593
Travel time =    2.63 min.     TC =   16.81  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.820
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.700
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  84.70
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.456(In/Hr) for a   100.0 year storm
Subarea runoff =     29.310(CFS) for     14.560(Ac.)
Total runoff =     48.587(CFS)       Total area =      23.140(Ac.)


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Process from Point/Station       17.100 to Point/Station       17.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
```

```
Upstream point/station elevation =  1371.000(Ft.)
Downstream point/station elevation =  1360.000(Ft.)
Pipe length  =   473.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    48.587(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    48.587(CFS)
Normal flow depth in pipe =   22.88(In.)
Flow top width inside pipe =   19.43(In.)
Critical depth could not be calculated.
Pipe flow velocity =     13.52(Ft/s)
Travel time through pipe =    0.58 min.
Time of concentration (TC) =    17.39 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       17.200 to Point/Station       18.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1360.000(Ft.)
End of natural channel elevation =   1347.000(Ft.)
Length of natural channel  =   166.000(Ft.)
Estimated mean flow rate at midpoint of channel =     49.175(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  10.78(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0783
Corrected/adjusted channel slope =  0.0783
Travel time =    0.26 min.     TC =   17.65  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.825
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.397(In/Hr) for a   100.0 year storm
Subarea runoff =      1.108(CFS) for      0.560(Ac.)
Total runoff =     49.695(CFS)       Total area =      23.700(Ac.)


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Process from Point/Station       18.000 to Point/Station       18.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     23.700(Ac.)
Runoff from this stream =     49.695(CFS)
Time of concentration =   17.65 min.
Rainfall intensity =     2.397(In/Hr)


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Process from Point/Station       19.000 to Point/Station       20.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   687.000(Ft.)
Top (of initial area) elevation =  1478.000(Ft.)
Bottom (of initial area) elevation =  1430.000(Ft.)
Difference in elevation =    48.000(Ft.)
Slope =    0.06987  s(percent)=       6.99
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.308 min.
Rainfall intensity =      2.870(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.837
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     11.888(CFS)
Total initial stream area =        4.950(Ac.)
Pervious area fraction = 1.000
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++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       20.000 to Point/Station       21.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1430.000(Ft.)
End of natural channel elevation =   1400.000(Ft.)
Length of natural channel  =   583.000(Ft.)
Estimated mean flow rate at midpoint of channel =     21.542(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.94(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0515
Corrected/adjusted channel slope =  0.0515
Travel time =    1.40 min.     TC =   13.71  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.833
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.720(In/Hr) for a   100.0 year storm
Subarea runoff =     18.225(CFS) for      8.040(Ac.)
Total runoff =     30.113(CFS)       Total area =      12.990(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       21.000 to Point/Station       18.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1400.000(Ft.)
End of natural channel elevation =   1347.000(Ft.)
Length of natural channel  =  1004.000(Ft.)
Estimated mean flow rate at midpoint of channel =     49.202(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.85(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0528
Corrected/adjusted channel slope =  0.0528
Travel time =    1.89 min.     TC =   15.60  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.829
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.550(In/Hr) for a   100.0 year storm
Subarea runoff =     34.827(CFS) for     16.470(Ac.)
Total runoff =     64.939(CFS)       Total area =      29.460(Ac.)


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Process from Point/Station       18.000 to Point/Station       18.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     29.460(Ac.)
Runoff from this stream =     64.939(CFS)
Time of concentration =   15.60 min.
Rainfall intensity =     2.550(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                (In/Hr)


1       49.695     17.65                2.397
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2       64.939     15.60                 2.550
Largest stream flow has longer or shorter time of concentration
Qp =     64.939 + sum of
          Qa           Tb/Ta
          49.695 *    0.884 =     43.923
Qp =    108.862

Total of 2 streams to confluence:
Flow rates before confluence point:
      49.695      64.939
Area of streams before confluence:
       23.700       29.460
Results of confluence:
Total flow rate =    108.862(CFS)
Time of concentration =    15.600 min.
Effective stream area after confluence =     53.160(Ac.)


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Process from Point/Station       18.000 to Point/Station       15.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1347.000(Ft.)
End of natural channel elevation =   1299.000(Ft.)
Length of natural channel  =  1128.000(Ft.)
Estimated mean flow rate at midpoint of channel =    122.910(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  10.42(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0426
Corrected/adjusted channel slope =  0.0426
Travel time =    1.80 min.     TC =   17.40  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.826
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.414(In/Hr) for a   100.0 year storm
Subarea runoff =     27.346(CFS) for     13.720(Ac.)
Total runoff =    136.208(CFS)       Total area =      66.880(Ac.)


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Process from Point/Station       15.000 to Point/Station       15.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     66.880(Ac.)
Runoff from this stream =    136.208(CFS)
Time of concentration =   17.40 min.
Rainfall intensity =     2.414(In/Hr)


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Process from Point/Station       13.000 to Point/Station       14.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   930.000(Ft.)
Top (of initial area) elevation =  1522.000(Ft.)
Bottom (of initial area) elevation =  1448.000(Ft.)
Difference in elevation =    74.000(Ft.)
Slope =    0.07957  s(percent)=       7.96
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.537 min.
Rainfall intensity =      2.737(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.834
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     15.565(CFS)
Total initial stream area =        6.820(Ac.)
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Pervious area fraction = 1.000

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Process from Point/Station       14.000 to Point/Station       14.100
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1448.000(Ft.)
End of natural channel elevation =   1363.000(Ft.)
Length of natural channel  =  1674.000(Ft.)
Estimated mean flow rate at midpoint of channel =     39.585(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.16(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0508
Corrected/adjusted channel slope =  0.0508
Travel time =    3.42 min.     TC =   16.96  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.819
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.700
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  84.70
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.445(In/Hr) for a   100.0 year storm
Subarea runoff =     42.174(CFS) for     21.050(Ac.)
Total runoff =     57.739(CFS)       Total area =      27.870(Ac.)


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Process from Point/Station       14.100 to Point/Station       14.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1363.000(Ft.)
Downstream point/station elevation =  1359.000(Ft.)
Pipe length  =    86.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    57.739(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    57.739(CFS)
Normal flow depth in pipe =   19.38(In.)
Flow top width inside pipe =   24.30(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.91(Ft/s)
Travel time through pipe =    0.08 min.
Time of concentration (TC) =    17.03 min.


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Process from Point/Station       14.300 to Point/Station       14.400
**** SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.826
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    17.03 min.
Rainfall intensity =      2.440(In/Hr) for a   100.0 year storm
Subarea runoff =     18.048(CFS) for      8.950(Ac.)
Total runoff =     75.787(CFS)       Total area =      36.820(Ac.)


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Process from Point/Station       14.400 to Point/Station       14.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1377.000(Ft.)
Downstream point/station elevation =  1359.000(Ft.)
Pipe length  =   366.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    75.787(CFS)
Nearest computed pipe diameter  =     30.00(In.)
Calculated individual pipe flow  =    75.787(CFS)
Normal flow depth in pipe =   20.91(In.)
Flow top width inside pipe =   27.58(In.)
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Critical depth could not be calculated.
Pipe flow velocity =     20.73(Ft/s)
Travel time through pipe =    0.29 min.
Time of concentration (TC) =    17.33 min.


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Process from Point/Station       14.200 to Point/Station       14.500
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1359.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =    75.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    75.787(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    75.787(CFS)
Normal flow depth in pipe =   24.00(In.)
Flow top width inside pipe =   16.97(In.)
Critical depth could not be calculated.
Pipe flow velocity =     20.30(Ft/s)
Travel time through pipe =    0.06 min.
Time of concentration (TC) =    17.39 min.


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Process from Point/Station       14.500 to Point/Station       14.600
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1355.000(Ft.)
End of natural channel elevation =   1329.000(Ft.)
Length of natural channel  =   406.000(Ft.)
Estimated mean flow rate at midpoint of channel =     79.461(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  11.22(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0640
Corrected/adjusted channel slope =  0.0640
Travel time =    0.60 min.     TC =   17.99  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.825
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.374(In/Hr) for a   100.0 year storm
Subarea runoff =      6.989(CFS) for      3.570(Ac.)
Total runoff =     82.775(CFS)       Total area =      40.390(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.600 to Point/Station       14.700
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1329.000(Ft.)
Downstream point/station elevation =  1319.000(Ft.)
Pipe length  =   258.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    82.775(CFS)
Nearest computed pipe diameter  =     30.00(In.)
Calculated individual pipe flow  =    82.775(CFS)
Normal flow depth in pipe =   25.31(In.)
Flow top width inside pipe =   21.79(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.72(Ft/s)
Travel time through pipe =    0.23 min.
Time of concentration (TC) =    18.22 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.700 to Point/Station       15.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1319.000(Ft.)
End of natural channel elevation =   1299.000(Ft.)
Length of natural channel  =   333.000(Ft.)
Estimated mean flow rate at midpoint of channel =     83.800(CFS)
```

```
Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  11.03(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0601
Corrected/adjusted channel slope =  0.0601
Travel time =    0.50 min.     TC =   18.72  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.823
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.327(In/Hr) for a   100.0 year storm
Subarea runoff =      1.916(CFS) for      1.000(Ac.)
Total runoff =     84.691(CFS)       Total area =      41.390(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       15.000 to Point/Station       15.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     41.390(Ac.)
Runoff from this stream =     84.691(CFS)
Time of concentration =   18.72 min.
Rainfall intensity =     2.327(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      136.208     17.40                 2.414
2       84.691     18.72                 2.327
Largest stream flow has longer or shorter time of concentration
Qp =    136.208 + sum of
          Qa          Tb/Ta
          84.691 *    0.929 =     78.718
Qp =    214.927

Total of 2 streams to confluence:
Flow rates before confluence point:
     136.208      84.691
Area of streams before confluence:
       66.880       41.390
Results of confluence:
Total flow rate =    214.927(CFS)
Time of concentration =    17.404 min.
Effective stream area after confluence =    108.270(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       15.000 to Point/Station       22.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1299.000(Ft.)
End of natural channel elevation =   1215.000(Ft.)
Length of natural channel  =  1781.000(Ft.)
Estimated mean flow rate at midpoint of channel =    287.264(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  14.26(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0472
Corrected/adjusted channel slope =  0.0472
Travel time =    2.08 min.     TC =   19.49  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.812
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
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Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.281(In/Hr) for a   100.0 year storm
Subarea runoff =    135.040(CFS) for     72.880(Ac.)
Total runoff =    349.967(CFS)       Total area =     181.150(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       22.000 to Point/Station       23.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1215.000(Ft.)
End of natural channel elevation =   1170.000(Ft.)
Length of natural channel  =  1218.000(Ft.)
Estimated mean flow rate at midpoint of channel =    366.359(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  13.63(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0369
Corrected/adjusted channel slope =  0.0369
Travel time =    1.49 min.     TC =   20.97  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.799
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.400
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  82.80
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.199(In/Hr) for a   100.0 year storm
Subarea runoff =     29.824(CFS) for     16.970(Ac.)
Total runoff =    379.791(CFS)       Total area =     198.120(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       23.000 to Point/Station       23.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.804
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Time of concentration =    20.97 min.
Rainfall intensity =      2.199(In/Hr) for a   100.0 year storm
Subarea runoff =    150.248(CFS) for     85.030(Ac.)
Total runoff =    530.039(CFS)       Total area =     283.150(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       23.000 to Point/Station       12.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1170.000(Ft.)
End of natural channel elevation =   1139.000(Ft.)
Length of natural channel  =   692.000(Ft.)
Estimated mean flow rate at midpoint of channel =    535.842(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  16.95(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0448
Corrected/adjusted channel slope =  0.0448
Travel time =    0.68 min.     TC =   21.66  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.767
```

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Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  78.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.164(In/Hr) for a   100.0 year storm
Subarea runoff =     10.287(CFS) for      6.200(Ac.)
Total runoff =    540.326(CFS)       Total area =     289.350(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       12.000 to Point/Station       12.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =    289.350(Ac.)
Runoff from this stream =    540.326(CFS)
Time of concentration =   21.66 min.
Rainfall intensity =     2.164(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1     1080.164     34.23               1.721
2      540.326     21.66               2.164
Largest stream flow has longer time of concentration
Qp =   1080.164 + sum of
          Qb         Ia/Ib
         540.326 *    0.795 =    429.772
Qp =   1509.936

Total of 2 main streams to confluence:
Flow rates before confluence point:
    1080.164     540.326
Area of streams before confluence:
      690.360      289.350


Results of confluence:
Total flow rate =   1509.936(CFS)
Time of concentration =    34.229 min.
Effective stream area after confluence  =    979.710(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       12.000 to Point/Station       24.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1139.000(Ft.)
End of natural channel elevation =   1136.000(Ft.)
Length of natural channel  =   119.000(Ft.)
Estimated mean flow rate at midpoint of channel =   1510.645(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  17.82(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0252
Corrected/adjusted channel slope =  0.0252
Travel time =    0.11 min.     TC =   34.34  min.
 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.738
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 1.000
Decimal fraction soil group C = 0.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  78.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.718(In/Hr) for a   100.0 year storm
Subarea runoff =      1.167(CFS) for      0.920(Ac.)
Total runoff =   1511.103(CFS)       Total area =     980.630(Ac.)
End of computations, total study area =          980.63 (Ac.)
The following figures maybe used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.839
Area averaged RI index number =  80.8
```

```
                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 09/22/16  File:mcs100.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

------------------------------------------------------------------------
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =  100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity =  1.300(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       25.000 to Point/Station       26.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =  1000.000(Ft.)
Top (of initial area) elevation =  1296.000(Ft.)
Bottom (of initial area) elevation =  1238.000(Ft.)
Difference in elevation =    58.000(Ft.)
Slope =    0.05800  s(percent)=       5.80
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.845 min.
Rainfall intensity =      2.614(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.822
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     13.585(CFS)
Total initial stream area =        6.320(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       26.000 to Point/Station       26.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      6.320(Ac.)
Runoff from this stream =     13.585(CFS)
Time of concentration =   14.85 min.
Rainfall intensity =     2.614(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       27.000 to Point/Station       26.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   446.000(Ft.)
Top (of initial area) elevation =  1289.000(Ft.)
Bottom (of initial area) elevation =  1238.000(Ft.)
Difference in elevation =    51.000(Ft.)
Slope =    0.11435  s(percent)=      11.43
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    9.383 min.
```

```
Rainfall intensity =      3.287(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.837
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      2.890(CFS)
Total initial stream area =        1.050(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       26.000 to Point/Station       26.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      1.050(Ac.)
Runoff from this stream =      2.890(CFS)
Time of concentration =    9.38 min.
Rainfall intensity =     3.287(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)

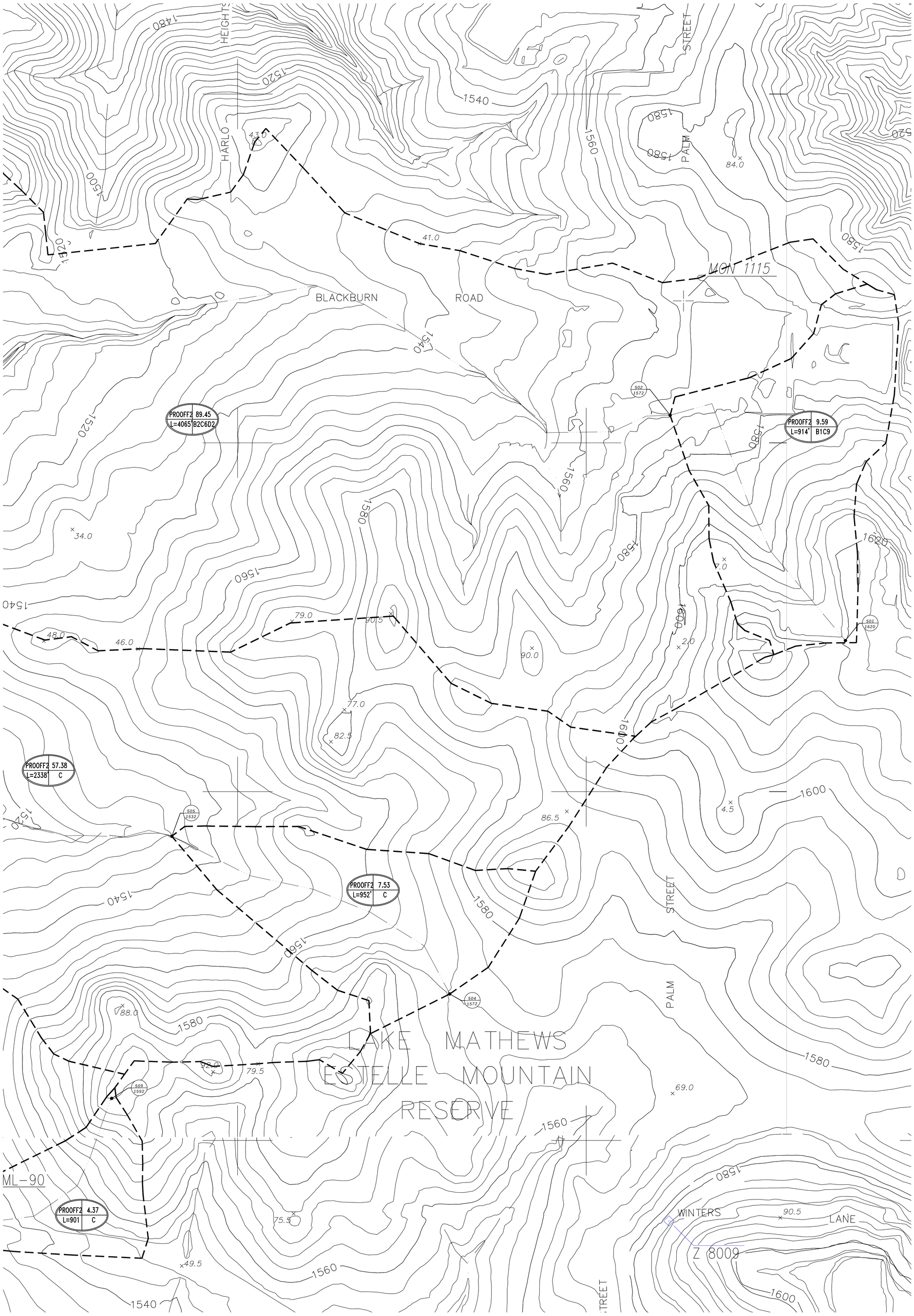

1       13.585     14.85                2.614
2        2.890      9.38                3.287
Largest stream flow has longer time of concentration
Qp =     13.585 + sum of
          Qb         Ia/Ib
           2.890 *    0.795 =      2.298
Qp =     15.882

Total of 2 streams to confluence:
Flow rates before confluence point:
      13.585       2.890
Area of streams before confluence:
        6.320        1.050
Results of confluence:
Total flow rate =     15.882(CFS)
Time of concentration =    14.845 min.
Effective stream area after confluence =      7.370(Ac.)
End of computations, total study area =            7.37 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number =  84.4
```

Appendix B – Proposed Rational Hydrology Method

PROPOSED RATIONAL HYDROLOGY MAP



LEGEND

NODE / ELEV — AREA | ACRES — LENGTH | SOIL

WATERSHED BOUNDARY

FLOW PATH

0 50 100 200 300 400

SCALE: 1" = 100'

PROPOSED RATIONAL HYDROLOGY MAP
PREPARATION DATE: DECEMBER 2022
REVISION DATE: FEBRUARY 2024

PLAN PREPARED BY:
adkan ENGINEERS
Civil Engineering • Surveying • Planning
6879 Airport Drive, Riverside, CA 92504
Tel:(951) 688-0241 Fax:(951) 688-0599

PROPOSED RATIONAL HYDROLOGY MAP

PROOFF 8.95 | L=1000 | C
PROOFF 21.06 | L=1674 | C
PROOFF 14.56 | L=1830 | C
PROOFF 4.81 | L=682 | C
PROOFF 6.82 | L=930 | C
PROOFF 8.58 | L=972 | C
PROOFF2 11.54 | L=1283 | C
PROOFF2 0.96 | L=142 | C
PROOFF2 6.34 | L=897 | C
PROOFF2 1.91 | L=777 | C
PROOFF2 9.60 | L=1990 | C
PROOFF2 23.23 | L=1860 | C
PROOFF2 37.41 | L=816 | B1C8D1
PROOFF2 15.56 | L=1024 | C
PROOFF2 7.70 | L=928 | C
PROOFF2 8.79 | L=986 | C
PROOFF2 30.37 | L=2076 | C
PROOFF2 2.41 | L=923 | C

Q10=180.62 cfs
Q100= 312.66 cfs
TC=30.03min
ACRES=201.36

Q10= 30.42 cfs
Q100= 50.27 cfs
TC=17.40min
ACRES=24.35

Q10= 10.52 cfs
Q100= 17.19 cfs
TC=14.10min
ACRES=7.70

Q10= 41.05 cfs
Q100= 68.75 cfs
TC=18.45min
ACRES=34.74

Q10= 12.66 cfs
Q100= 21.21 cfs
TC=23.23min
ACRES=12.01

L=731
L=40'
L=74'

VISTA DEL LAGO DRIVE
EL SOBRANTE ROAD

LEGEND
NODE / ELEV
AREA | ACRES
LENGTH | SOIL
WATERSHED BOUNDARY
FLOW PATH

SCALE: 1" = 100'

PROPOSED RATIONAL HYDROLOGY MAP
PREPARATION DATE: DECEMBER 2022
REVISION DATE: FEBRUARY 2024
PLAN PREPARED BY:

adkan ENGINEERS
Civil Engineering • Surveying • Planning
6879 Airport Drive, Riverside, CA 92504
Tel:(951) 688-0241 Fax:(951) 688-0599

PROPOSED RATIONAL HYDROLOGY MAP

PROOFF | 0.87 | L=225 | C
Q10= 3.72 CFS | Q100= 6.05 CFS | TC= 11.03 MIN | ACRES= 2.25 | 202 1282
Q10= 180.87 CFS | Q100= 302.56 CFS | TC= 19.94 MIN | ACRES= 155.52 | 318 1243
317 1251
Q10= 67.28 CFS | Q100= 111.07 CFS | TC= 15.49 MIN | ACRES= 51.80 | 117 1291
PRO2 | 1.41 | L=161 | C
Q10= 65.70 CFS | Q100= 108.33 CFS | TC= 15.49 MIN | ACRES= 50.39 | 116 1293
115 1315
Q10= 8.30 CFS | Q100= 13.56 CFS | TC= 13.20 MIN | ACRES= 5.95
PROOFF | 3.79 | L=1118 | C
Q10= 11.72 CFS | Q100= 19.38 CFS | TC= 10.62 MIN | ACRES= 7.79 | 207 1263
PROOFF | 2.43 | L=573 | C
PR03 | 1.25 | L=253 | C
PR03 | 1.57 | L=461 | C
112 1315
Q10= 17.49 CFS | Q100= 28.49 CFS | TC= 12.53 MIN | ACRES= 11.88
PRO2 | 2.32 | L=703 | C
309 1299
PROOFF | 1.00 | L=332 | C
308 1319
Q10= 50.45 CFS | Q100= 83.69 CFS | TC= 17.69 MIN | ACRES= 40.41 | 307 1329
PROOFF | 3.58 | L=405 | C
306 1355
303 1359
L=258'
L=75'
L=86'
L=166'
Q10= 12.49 CFS | Q100= 20.40 CFS | TC= 13.56 MIN | ACRES= 8.95 | 305 1377
319 1322
109 1309
PRO2 | 3.63 | L=800 | C
Q10= 6.78 CFS | Q100= 11.05 CFS | TC= 10.46 MIN | ACRES= 4.29 | 205 1290
203 1275
Q10= 9.93 CFS | Q100= 16.35 CFS | TC= 10.62 MIN | ACRES= 6.54 | 206 1264
201 1290
L=110'
PRO2 | 2.89 | L=675 | C
PRO2 | 3.18 | L=806 | C
Q10= 5.68 CFS | Q100= 9.36 CFS | TC= 12.22 MIN | ACRES= 3.59 | 108 1336
Q10= 35.06 CFS | Q100= 58.13 CFS | TC= 16.96 MIN | ACRES= 27.88 | 302 1363
L=473'
PR03 | 0.68 | L=936 | C
PR03 | 4.29 | L=914 | C
111 1336
103 1329
Q10= 14.60 CFS | Q100= 24.40 CFS | TC= 15.45 MIN | ACRES= 11.35 | 104 1336
PRO2 | 1.21 | L=409 | C
PROOFF | 5.22 | L=1131 | C
313 1360
Q10= 28.54 CFS | Q100= 47.31 CFS | TC= 18.34 MIN | ACRES= 23.14 | 312 1371
314 1347
PROOFF | 0.56 | L=166 | C
114 326.5
113 326.5
PRO2 | 5.81 | L=707 | C
PRO2 | 5.74 | L=411 | C
107 1357
102 1357
PRO2 | 1.73 | L=576 | C
PRO2 | 1.30 | L=493 | C
Q10= 7.11 CFS | Q100= 11.70 CFS | TC= 16.65 MIN | ACRES= 4.46 | 101.4 1362
101.2 1355
106 1363
PRO2 | 3.32 | L=980 | C
PRO2 | 0.65 | L=737 | C
PRO2 | 2.14 | L=617 | C
101.3 1370
101.1 1362
101.7 1365
Q10= 17.38 CFS | Q100= 28.59 CFS | TC= 13.73 MIN | ACRES= 12.16
PAD= 8,965 SF
LOT= 10,195 SF
PAD= 8,701 SF
PR01 | 0.47 | L=274 | C
23 360.6
110 360.6
204 1345
200 1345
24 1341
PRO2 | 5.76 | L=1000 | C
PRO2 | 4.31 | L=915 | C
PROOFF | 21.49 | L=1629 | C
PR03 | 1.75 | L=501 | C
19 1386
20 1341
5 1388
1 1388
101 1370
PRO2 | 6.40 | L=649 | C
PR01 | 0.90 | L=1079 | C
PR01 | 4.33 | L=1029 | C
105 1410
100 1423
101.6 1434
8 1358
PR01 | 5.81 | L=744 | C
PR01 | 0.83 | L=750 | C
Q10= 32.83 CFS | Q100= 54.19 CFS | TC= 12.81 MIN | ACRES= 26.74 | 27 1307
PR01 | 1.68 | L=289 | C
Q10= 2.33 CFS | Q100= 3.79 CFS | TC= 13.31 MIN | ACRES= 1.37 | 25 1327
Q10= 6.15 CFS | Q100= 10.36 CFS | TC= 23.02 MIN | ACRES= 6.08 | 21 1321
PR01 | 7.47 | L=1000 | C
Q10= 9.84 CFS | Q100= 16.02 CFS | TC= 12.02 MIN | ACRES= 6.28 | 3 1344
2 1361
PR01 | 0.47 | L=463 | C
6 1361
L=36'
L=37'
L=40'
L=140'
L=107'
L=36'
L=63'
L=30'
L=207'
L=36'
L=39'
L=36'
Q10= 30.68 CFS | Q100= 50.55 CFS | TC= 12.60 MIN | ACRES= 25.06 | 26 1308
18 1310
10 1310.5
4 1323
Q10= 10.79 CFS | Q100= 17.63 CFS | TC= 12.30 MIN | ACRES= 7.47 | 9 1326
Q10= 3.22 CFS | Q100= 5.14 CFS | TC= 13.11 MIN | ACRES= 1.87 | 7 1326
PR01 | 1.04 | L=1128 | C
Q10= 365.62 CFS | Q100= 633.11 CFS | TC= 35.68 MIN | ACRES= 420.13 | 528 1286
14 1312
Q10= 1.84 CFS | Q100= 2.92 CFS | TC= 10.00 MIN | ACRES= 0.98 | 17 1316.4
Q10= 1.89 CFS | Q100= 2.99 CFS | TC= 10.06 MIN | ACRES= 1.01 | 13 1316.4
PR01 | 0.58 | L=600 | C
PR01 | 0.59 | L=573 | C
96
PROFF2 | 58.93 | L=2132 | B2C8
527 1354
508 1369
PROOFF2 | 14.94 | L=336 | C
PROOFF2 | 3.78 | L=547 | C
12 1351.3
16 1351
PR01 | 0.42 | L=610 | C
PR01 | 0.40 | L=583 | C
15 1369
11 1369
PROOFF2 | 0.50 | L=135 | C
519 1386
523 1380
PROOFF2 | 6.90 | L=502 | C
PROOFF2 | 2.46 | L=577 | C
516 1406
526 1404
513 1412
L=75'
525 1405
Q10= 12.22 cfs
Q100= 19.94 cfs
TC=12.80min
ACRES=8.48
PROOFF2 | 8.48 | L=590 | C
524 1430
17.0
6.0
1360

LEGEND
NODE / ELEV
AREA / ACRES
LENGTH / SOIL
WATERSHED BOUNDARY
FLOW PATH

0 50 100 200 300 400
SCALE: 1" = 100'

PROPOSED RATIONAL HYDROLOGY MAP
PREPARATION DATE: DECEMBER 2022
REVISION DATE: FEBRUARY 2024
(AS PREPARED BY)

adkan ENGINEERS
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 02/06/24  File:PRO110.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

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Program License Serial Number 5006

------------------------------------------------------------------------
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =   10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year =  10.0
Calculated rainfall intensity data:
1 hour intensity =  0.829(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   744.000(Ft.)
Top (of initial area) elevation =  1388.000(Ft.)
Bottom (of initial area) elevation =  1361.000(Ft.)
Difference in elevation =    27.000(Ft.)
Slope =    0.03629  s(percent)=       3.63
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.659 min.
Rainfall intensity =      1.967(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.795
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      9.085(CFS)
Total initial stream area =        5.810(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        2.000 to Point/Station        3.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of street segment elevation =  1361.000(Ft.)
End of street segment elevation =  1344.000(Ft.)
Length of street segment  =   463.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      9.453(CFS)
Depth of flow =   0.391(Ft.), Average velocity =   5.056(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  13.202(Ft.)
Flow velocity =   5.06(Ft/s)
Travel time =    1.53 min.     TC =   12.19  min.
 Adding area flow to street
```

```
COMMERCIAL subarea type
Runoff Coefficient = 0.878
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      1.840(In/Hr) for a    10.0 year storm
Subarea runoff =      0.759(CFS) for      0.470(Ac.)
Total runoff =      9.845(CFS)       Total area =       6.280(Ac.)
Street flow at end of street =      9.845(CFS)
Half street flow at end of street =      9.845(CFS)
Depth of flow =   0.395(Ft.), Average velocity =   5.105(Ft/s)
Flow width (from curb towards crown)=  13.423(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        3.000 to Point/Station        4.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1344.000(Ft.)
Downstream point/station elevation =  1323.000(Ft.)
Pipe length  =   633.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     9.845(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     9.845(CFS)
Normal flow depth in pipe =   10.50(In.)
Flow top width inside pipe =   13.75(In.)
Critical Depth =   14.16(In.)
Pipe flow velocity =     10.74(Ft/s)
Travel time through pipe =    0.98 min.
Time of concentration (TC) =    13.17 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        4.000 to Point/Station        4.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      6.280(Ac.)
Runoff from this stream =      9.845(CFS)
Time of concentration =   13.17 min.
Rainfall intensity =     1.770(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        5.000 to Point/Station        6.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   750.000(Ft.)
Top (of initial area) elevation =  1388.000(Ft.)
Bottom (of initial area) elevation =  1361.000(Ft.)
Difference in elevation =    27.000(Ft.)
Slope =    0.03600  s(percent)=       3.60
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    8.239 min.
Rainfall intensity =      2.237(In/Hr) for a    10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.881
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      1.636(CFS)
Total initial stream area =        0.830(Ac.)
Pervious area fraction = 0.100


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        6.000 to Point/Station        7.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1361.000(Ft.)
End of street segment elevation =  1326.000(Ft.)
Length of street segment  =  1128.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
```

```
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      2.459(CFS)
Depth of flow =   0.279(Ft.), Average velocity =   3.487(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   7.606(Ft.)
Flow velocity =   3.49(Ft/s)
Travel time =    5.39 min.     TC =   13.63  min.
 Adding area flow to street
COMMERCIAL subarea type
Runoff Coefficient = 0.877
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      1.740(In/Hr) for a    10.0 year storm
Subarea runoff =      1.587(CFS) for      1.040(Ac.)
Total runoff =      3.223(CFS)       Total area =       1.870(Ac.)
Street flow at end of street =      3.223(CFS)
Half street flow at end of street =      3.223(CFS)
Depth of flow =   0.299(Ft.), Average velocity =   3.697(Ft/s)
Flow width (from curb towards crown)=   8.631(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        7.000 to Point/Station        4.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1326.000(Ft.)
Downstream point/station elevation =  1323.000(Ft.)
Pipe length  =    30.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.223(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     3.223(CFS)
Normal flow depth in pipe =    5.11(In.)
Flow top width inside pipe =    8.92(In.)
Critical depth could not be calculated.
Pipe flow velocity =     12.45(Ft/s)
Travel time through pipe =    0.04 min.
Time of concentration (TC) =    13.67 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        4.000 to Point/Station        4.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      1.870(Ac.)
Runoff from this stream =      3.223(CFS)
Time of concentration =   13.67 min.
Rainfall intensity =     1.737(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        8.000 to Point/Station        9.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =  1000.000(Ft.)
Top (of initial area) elevation =  1358.000(Ft.)
Bottom (of initial area) elevation =  1326.000(Ft.)
Difference in elevation =    32.000(Ft.)
Slope =    0.03200  s(percent)=       3.20
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.304 min.
Rainfall intensity =      1.831(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.789
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =     10.792(CFS)
Total initial stream area =        7.470(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        9.000 to Point/Station        4.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
```

```
Upstream point/station elevation =  1326.000(Ft.)
Downstream point/station elevation =  1323.000(Ft.)
Pipe length  =    36.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    10.792(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =    10.792(CFS)
Normal flow depth in pipe =    8.19(In.)
Flow top width inside pipe =   14.94(In.)
Critical depth could not be calculated.
Pipe flow velocity =     15.75(Ft/s)
Travel time through pipe =    0.04 min.
Time of concentration (TC) =    12.34 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        4.000 to Point/Station        4.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 3
Stream flow area =      7.470(Ac.)
Runoff from this stream =     10.792(CFS)
Time of concentration =   12.34 min.
Rainfall intensity =     1.828(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        9.845     13.17                1.770
2        3.223     13.67                1.737
3       10.792     12.34                1.828
Largest stream flow has longer or shorter time of concentration
Qp =     10.792 + sum of
          Qa           Tb/Ta
           9.845 *    0.937 =      9.227
          Qa           Tb/Ta
           3.223 *    0.903 =      2.909
Qp =     22.928

Total of 3 streams to confluence:
Flow rates before confluence point:
       9.845       3.223      10.792
Area of streams before confluence:
       6.280       1.870       7.470
Results of confluence:
Total flow rate =     22.928(CFS)
Time of concentration =    12.342 min.
Effective stream area after confluence =     15.620(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        4.000 to Point/Station       10.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1323.000(Ft.)
Downstream point/station elevation =  1310.500(Ft.)
Pipe length  =    38.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    22.928(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =    22.928(CFS)
Normal flow depth in pipe =    8.54(In.)
Flow top width inside pipe =   14.85(In.)
Critical depth could not be calculated.
Pipe flow velocity =     31.79(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =    12.36 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       10.000 to Point/Station       10.000
**** CONFLUENCE OF MAIN STREAMS ****
------------------------------------------------------------------------------
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     15.620(Ac.)
Runoff from this stream =     22.928(CFS)
Time of concentration =   12.36 min.
Rainfall intensity =     1.827(In/Hr)
Program is now starting with Main Stream No. 2


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       11.000 to Point/Station       12.000
**** INITIAL AREA EVALUATION ****
```

```
Initial area flow distance =   610.000(Ft.)
Top (of initial area) elevation =  1369.000(Ft.)
Bottom (of initial area) elevation =  1351.300(Ft.)
Difference in elevation =    17.700(Ft.)
Slope =    0.02902  s(percent)=       2.90
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.920 min.
Rainfall intensity =      2.282(In/Hr) for a    10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.881
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      0.845(CFS)
Total initial stream area =        0.420(Ac.)
Pervious area fraction = 0.100


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       12.000 to Point/Station       13.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of street segment elevation =  1351.300(Ft.)
End of street segment elevation =  1316.400(Ft.)
Length of street segment  =   573.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      1.402(CFS)
Depth of flow =   0.218(Ft.), Average velocity =   4.155(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   4.591(Ft.)
Flow velocity =   4.15(Ft/s)
Travel time =    2.30 min.     TC =   10.22  min.
 Adding area flow to street
COMMERCIAL subarea type
Runoff Coefficient = 0.879
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      2.009(In/Hr) for a    10.0 year storm
Subarea runoff =      1.042(CFS) for      0.590(Ac.)
Total runoff =      1.887(CFS)        Total area =       1.010(Ac.)
Street flow at end of street =      1.887(CFS)
Half street flow at end of street =      1.887(CFS)
Depth of flow =   0.238(Ft.), Average velocity =   4.347(Ft/s)
Flow width (from curb towards crown)=   5.544(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       13.000 to Point/Station       14.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1316.400(Ft.)
Downstream point/station elevation =  1312.000(Ft.)
Pipe length  =    36.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.887(CFS)
Nearest computed pipe diameter  =      6.00(In.)
Calculated individual pipe flow  =     1.887(CFS)
Normal flow depth in pipe =    4.72(In.)
Flow top width inside pipe =    4.91(In.)
Critical depth could not be calculated.
Pipe flow velocity =     11.38(Ft/s)
Travel time through pipe =    0.05 min.
Time of concentration (TC) =    10.27 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.000 to Point/Station       14.000
```

```
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      1.010(Ac.)
Runoff from this stream =      1.887(CFS)
Time of concentration =   10.27 min.
Rainfall intensity =     2.004(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       15.000 to Point/Station       16.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------
Initial area flow distance =   583.000(Ft.)
Top (of initial area) elevation =  1369.000(Ft.)
Bottom (of initial area) elevation =  1351.300(Ft.)
Difference in elevation =    17.700(Ft.)
Slope =    0.03036  s(percent)=       3.04
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.708 min.
Rainfall intensity =      2.313(In/Hr) for a    10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.881
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      0.816(CFS)
Total initial stream area =        0.400(Ac.)
Pervious area fraction = 0.100


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       16.000 to Point/Station       17.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Top of street segment elevation =  1351.300(Ft.)
End of street segment elevation =  1316.400(Ft.)
Length of street segment  =   600.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      1.368(CFS)
Depth of flow =   0.218(Ft.), Average velocity =   4.059(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   4.587(Ft.)
Flow velocity =   4.06(Ft/s)
Travel time =    2.46 min.     TC =   10.17  min.
 Adding area flow to street
COMMERCIAL subarea type
Runoff Coefficient = 0.879
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      2.014(In/Hr) for a    10.0 year storm
Subarea runoff =      1.027(CFS) for      0.580(Ac.)
Total runoff =      1.843(CFS)       Total area =       0.980(Ac.)
Street flow at end of street =      1.843(CFS)
Half street flow at end of street =      1.843(CFS)
Depth of flow =   0.238(Ft.), Average velocity =   4.248(Ft/s)
Flow width (from curb towards crown)=   5.542(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       17.000 to Point/Station       14.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =  1316.400(Ft.)
Downstream point/station elevation =  1312.000(Ft.)
Pipe length  =    39.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     1.843(CFS)
```

```
Nearest computed pipe diameter  =      6.00(In.)
Calculated individual pipe flow  =     1.843(CFS)
Normal flow depth in pipe =    4.80(In.)
Flow top width inside pipe =    4.79(In.)
Critical depth could not be calculated.
Pipe flow velocity =     10.94(Ft/s)
Travel time through pipe =    0.06 min.
Time of concentration (TC) =    10.23 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.000 to Point/Station       14.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      0.980(Ac.)
Runoff from this stream =      1.843(CFS)
Time of concentration =   10.23 min.
Rainfall intensity =     2.008(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        1.887     10.27                2.004
2        1.843     10.23                2.008
Largest stream flow has longer time of concentration
Qp =      1.887 + sum of
          Qb         Ia/Ib
           1.843 *    0.998 =      1.839
Qp =      3.726

Total of 2 streams to confluence:
Flow rates before confluence point:
       1.887       1.843
Area of streams before confluence:
       1.010        0.980
Results of confluence:
Total flow rate =      3.726(CFS)
Time of concentration =    10.271 min.
Effective stream area after confluence =      1.990(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       14.000 to Point/Station       10.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1312.000(Ft.)
Downstream point/station elevation =  1310.500(Ft.)
Pipe length  =   227.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.726(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     3.726(CFS)
Normal flow depth in pipe =    9.33(In.)
Flow top width inside pipe =   14.55(In.)
Critical Depth =    9.36(In.)
Pipe flow velocity =      4.64(Ft/s)
Travel time through pipe =    0.81 min.
Time of concentration (TC) =    11.09 min.


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Process from Point/Station       10.000 to Point/Station       10.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      1.990(Ac.)
Runoff from this stream =      3.726(CFS)
Time of concentration =   11.09 min.
Rainfall intensity =     1.929(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       22.928     12.36                1.827
2        3.726     11.09                1.929
Largest stream flow has longer time of concentration
Qp =     22.928 + sum of
          Qb         Ia/Ib
           3.726 *    0.947 =      3.529
Qp =     26.457
```

```
Total of 2 main streams to confluence:
Flow rates before confluence point:
      22.928       3.726
Area of streams before confluence:
       15.620        1.990


Results of confluence:
Total flow rate =     26.457(CFS)
Time of concentration =    12.362 min.
Effective stream area after confluence  =     17.610(Ac.)


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Process from Point/Station       10.000 to Point/Station       18.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1310.500(Ft.)
Downstream point/station elevation =  1310.000(Ft.)
Pipe length  =   107.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    26.457(CFS)
Nearest computed pipe diameter  =     30.00(In.)
Calculated individual pipe flow  =    26.457(CFS)
Normal flow depth in pipe =   23.20(In.)
Flow top width inside pipe =   25.12(In.)
Critical Depth =   21.02(In.)
Pipe flow velocity =      6.50(Ft/s)
Travel time through pipe =    0.27 min.
Time of concentration (TC) =    12.64 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       18.000 to Point/Station       18.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     17.610(Ac.)
Runoff from this stream =     26.457(CFS)
Time of concentration =   12.64 min.
Rainfall intensity =     1.807(In/Hr)
Program is now starting with Main Stream No. 2


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       19.000 to Point/Station       20.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   501.000(Ft.)
Top (of initial area) elevation =  1386.000(Ft.)
Bottom (of initial area) elevation =  1341.000(Ft.)
Difference in elevation =    45.000(Ft.)
Slope =    0.08982  s(percent)=       8.98
TC = k(0.940)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   18.297 min.
Rainfall intensity =      1.501(In/Hr) for a    10.0 year storm
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.686
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  74.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      1.802(CFS)
Total initial stream area =        1.750(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station       20.000 to Point/Station       21.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1341.000(Ft.)
End of street segment elevation =  1321.500(Ft.)
Length of street segment  =  1029.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
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 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      4.004(CFS)
Depth of flow =   0.338(Ft.), Average velocity =   3.208(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  10.589(Ft.)
Flow velocity =   3.21(Ft/s)
Travel time =    5.35 min.     TC =   23.64  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.760
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      1.321(In/Hr) for a    10.0 year storm
Subarea runoff =      4.344(CFS) for      4.330(Ac.)
Total runoff =      6.147(CFS)       Total area =       6.080(Ac.)
Street flow at end of street =      6.147(CFS)
Half street flow at end of street =      6.147(CFS)
Depth of flow =   0.380(Ft.), Average velocity =   3.547(Ft/s)
Flow width (from curb towards crown)=  12.673(Ft.)


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Process from Point/Station       21.000 to Point/Station       22.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1321.500(Ft.)
Downstream point/station elevation =  1321.000(Ft.)
Pipe length  =    37.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     6.147(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     6.147(CFS)
Normal flow depth in pipe =   10.32(In.)
Flow top width inside pipe =   13.90(In.)
Critical Depth =   12.01(In.)
Pipe flow velocity =      6.83(Ft/s)
Travel time through pipe =    0.09 min.
Time of concentration (TC) =    23.73 min.


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Process from Point/Station       22.000 to Point/Station       22.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      6.080(Ac.)
Runoff from this stream =      6.147(CFS)
Time of concentration =   23.73 min.
Rainfall intensity =     1.318(In/Hr)


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Process from Point/Station       23.000 to Point/Station       24.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   274.000(Ft.)
Top (of initial area) elevation =  1360.800(Ft.)
Bottom (of initial area) elevation =  1341.000(Ft.)
Difference in elevation =    19.800(Ft.)
Slope =    0.07226  s(percent)=       7.23
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    6.228 min.
Rainfall intensity =      2.573(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.815
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      0.986(CFS)
Total initial stream area =        0.470(Ac.)
Pervious area fraction = 0.500


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Process from Point/Station       24.000 to Point/Station       25.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1341.000(Ft.)
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End of street segment elevation =  1327.000(Ft.)
Length of street segment  =  1079.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      1.696(CFS)
Depth of flow =   0.284(Ft.), Average velocity =   2.286(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   7.843(Ft.)
Flow velocity =   2.29(Ft/s)
Travel time =    7.87 min.     TC =   14.09  min.
 Adding area flow to street
COMMERCIAL subarea type
Runoff Coefficient = 0.877
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      1.711(In/Hr) for a    10.0 year storm
Subarea runoff =      1.350(CFS) for      0.900(Ac.)
Total runoff =      2.335(CFS)       Total area =       1.370(Ac.)
Street flow at end of street =      2.335(CFS)
Half street flow at end of street =      2.335(CFS)
Depth of flow =   0.308(Ft.), Average velocity =   2.452(Ft/s)
Flow width (from curb towards crown)=   9.088(Ft.)


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Process from Point/Station       25.000 to Point/Station       22.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1327.000(Ft.)
Downstream point/station elevation =  1321.000(Ft.)
Pipe length  =    36.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.335(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     2.335(CFS)
Normal flow depth in pipe =    3.65(In.)
Flow top width inside pipe =    8.84(In.)
Critical Depth =    8.15(In.)
Pipe flow velocity =     13.89(Ft/s)
Travel time through pipe =    0.04 min.
Time of concentration (TC) =    14.14 min.


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Process from Point/Station       22.000 to Point/Station       22.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      1.370(Ac.)
Runoff from this stream =      2.335(CFS)
Time of concentration =   14.14 min.
Rainfall intensity =     1.708(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        6.147     23.73                 1.318
2        2.335     14.14                 1.708
Largest stream flow has longer time of concentration
Qp =      6.147 + sum of
          Qb         Ia/Ib
           2.335 *    0.772 =      1.803
Qp =      7.949

Total of 2 streams to confluence:
Flow rates before confluence point:
       6.147       2.335
Area of streams before confluence:
        6.080        1.370
Results of confluence:
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Total flow rate =      7.949(CFS)
Time of concentration =    23.733 min.
Effective stream area after confluence =      7.450(Ac.)


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Process from Point/Station       22.000 to Point/Station       18.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
----------------------------------------------------------------------------
Upstream point/station elevation =  1321.000(Ft.)
Downstream point/station elevation =  1310.000(Ft.)
Pipe length  =    40.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     7.949(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     7.949(CFS)
Normal flow depth in pipe =    6.77(In.)
Flow top width inside pipe =    7.77(In.)
Critical depth could not be calculated.
Pipe flow velocity =     22.27(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    23.76 min.


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Process from Point/Station       18.000 to Point/Station       18.000
**** CONFLUENCE OF MAIN STREAMS ****
----------------------------------------------------------------------------
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      7.450(Ac.)
Runoff from this stream =      7.949(CFS)
Time of concentration =   23.76 min.
Rainfall intensity =     1.317(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       26.457     12.64               1.807
2        7.949     23.76               1.317
Largest stream flow has longer or shorter time of concentration
Qp =     26.457 + sum of
          Qa          Tb/Ta
           7.949 *    0.532 =      4.227
Qp =     30.684

Total of 2 main streams to confluence:
Flow rates before confluence point:
      26.457       7.949
Area of streams before confluence:
       17.610        7.450


Results of confluence:
Total flow rate =     30.684(CFS)
Time of concentration =    12.636 min.
Effective stream area after confluence  =     25.060(Ac.)


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Process from Point/Station       18.000 to Point/Station       26.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
----------------------------------------------------------------------------
Upstream point/station elevation =  1310.000(Ft.)
Downstream point/station elevation =  1308.200(Ft.)
Pipe length  =   140.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    30.684(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    30.684(CFS)
Normal flow depth in pipe =   19.55(In.)
Flow top width inside pipe =   24.14(In.)
Critical Depth =   22.97(In.)
Pipe flow velocity =      9.96(Ft/s)
Travel time through pipe =    0.23 min.
Time of concentration (TC) =    12.87 min.


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Process from Point/Station       26.000 to Point/Station       27.000
**** SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.713
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
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Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  74.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    12.87 min.
Rainfall intensity =      1.790(In/Hr) for a    10.0 year storm
Subarea runoff =      2.145(CFS) for      1.680(Ac.)
Total runoff =     32.829(CFS)       Total area =      26.740(Ac.)
End of computations, total study area =           26.74 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.486
Area averaged RI index number =  69.6
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 02/06/24  File:PRO210.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

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Program License Serial Number 5006

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Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =   10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year =  10.0
Calculated rainfall intensity data:
1 hour intensity =  0.829(In/Hr)
Slope of intensity duration curve = 0.5000




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Process from Point/Station      100.000 to Point/Station      101.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =  1000.000(Ft.)
Top (of initial area) elevation =  1423.000(Ft.)
Bottom (of initial area) elevation =  1370.000(Ft.)
Difference in elevation =    53.000(Ft.)
Slope =    0.05300  s(percent)=       5.30
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   11.123 min.
Rainfall intensity =      1.926(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.793
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      8.799(CFS)
Total initial stream area =        5.760(Ac.)
Pervious area fraction = 0.500


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Process from Point/Station      101.000 to Point/Station      101.100
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of street segment elevation =  1370.000(Ft.)
End of street segment elevation =  1362.000(Ft.)
Length of street segment  =   649.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =     13.130(CFS)
Depth of flow =   0.498(Ft.), Average velocity =   3.674(Ft/s)
Note:  depth of flow exceeds top of street crown.
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  18.000(Ft.)
Flow velocity =   3.67(Ft/s)
Travel time =    2.94 min.     TC =   14.07  min.
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 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.783
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      1.712(In/Hr) for a    10.0 year storm
Subarea runoff =      8.585(CFS) for      6.400(Ac.)
Total runoff =     17.384(CFS)       Total area =      12.160(Ac.)
Street flow at end of street =     17.384(CFS)
Half street flow at end of street =     17.384(CFS)
Depth of flow =   0.543(Ft.), Average velocity =   3.936(Ft/s)
Warning: depth of flow exceeds top of curb
Note:  depth of flow exceeds top of street crown.
Distance that curb overflow reaches into property =    2.13(Ft.)
Flow width (from curb towards crown)=  18.000(Ft.)


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Process from Point/Station      101.100 to Point/Station      101.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1362.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =    50.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    17.384(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =    17.384(CFS)
Normal flow depth in pipe =    9.42(In.)
Flow top width inside pipe =   14.50(In.)
Critical depth could not be calculated.
Pipe flow velocity =     21.44(Ft/s)
Travel time through pipe =    0.04 min.
Time of concentration (TC) =    14.11 min.


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Process from Point/Station      101.200 to Point/Station      101.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     12.160(Ac.)
Runoff from this stream =     17.384(CFS)
Time of concentration =   14.11 min.
Rainfall intensity =     1.710(In/Hr)


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Process from Point/Station        1.000 to Point/Station      101.300
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   980.000(Ft.)
Top (of initial area) elevation =  1388.000(Ft.)
Bottom (of initial area) elevation =  1370.000(Ft.)
Difference in elevation =    18.000(Ft.)
Slope =    0.01837  s(percent)=       1.84
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.638 min.
Rainfall intensity =      1.739(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.785
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      4.531(CFS)
Total initial stream area =        3.320(Ac.)
Pervious area fraction = 0.500


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Process from Point/Station      101.300 to Point/Station      101.400
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1370.000(Ft.)
End of street segment elevation =  1362.000(Ft.)
Length of street segment  =   617.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
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Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      5.864(CFS)
Depth of flow =   0.395(Ft.), Average velocity =   3.035(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  13.436(Ft.)
Flow velocity =   3.04(Ft/s)
Travel time =    3.39 min.     TC =   17.03  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.775
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      1.556(In/Hr) for a    10.0 year storm
Subarea runoff =      2.581(CFS) for      2.140(Ac.)
Total runoff =      7.112(CFS)       Total area =       5.460(Ac.)
Street flow at end of street =      7.112(CFS)
Half street flow at end of street =      7.112(CFS)
Depth of flow =   0.417(Ft.), Average velocity =   3.179(Ft/s)
Flow width (from curb towards crown)=  14.528(Ft.)


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Process from Point/Station      101.400 to Point/Station      101.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1362.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =    34.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     7.112(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     7.112(CFS)
Normal flow depth in pipe =    6.98(In.)
Flow top width inside pipe =    7.50(In.)
Critical depth could not be calculated.
Pipe flow velocity =     19.33(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    17.05 min.


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Process from Point/Station      101.200 to Point/Station      101.200
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      5.460(Ac.)
Runoff from this stream =      7.112(CFS)
Time of concentration =   17.05 min.
Rainfall intensity =     1.555(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       17.384     14.11                 1.710
2        7.112     17.05                 1.555
Largest stream flow has longer or shorter time of concentration
Qp =     17.384 + sum of
          Qa          Tb/Ta
           7.112 *    0.827 =      5.882
Qp =     23.266

Total of 2 streams to confluence:
Flow rates before confluence point:
      17.384       7.112
Area of streams before confluence:
       12.160        5.460
Results of confluence:
Total flow rate =     23.266(CFS)
Time of concentration =    14.105 min.
Effective stream area after confluence =     17.620(Ac.)


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Process from Point/Station      101.200 to Point/Station      103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =  1355.000(Ft.)
Downstream point/station elevation =  1329.000(Ft.)
Pipe length  =   757.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    23.266(CFS)
Nearest computed pipe diameter  =     21.00(In.)
Calculated individual pipe flow  =    23.266(CFS)
Normal flow depth in pipe =   14.11(In.)
Flow top width inside pipe =   19.72(In.)
Critical Depth =   19.90(In.)
Pipe flow velocity =     13.54(Ft/s)
Travel time through pipe =    0.93 min.
Time of concentration (TC) =    15.04 min.


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Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     17.620(Ac.)
Runoff from this stream =     23.266(CFS)
Time of concentration =   15.04 min.
Rainfall intensity =     1.656(In/Hr)


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Process from Point/Station      101.600 to Point/Station      101.700
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------
Initial area flow distance =   915.000(Ft.)
Top (of initial area) elevation =  1434.400(Ft.)
Bottom (of initial area) elevation =  1365.000(Ft.)
Difference in elevation =    69.400(Ft.)
Slope =    0.07585  s(percent)=       7.58
TC = k(0.480)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.298 min.
Rainfall intensity =      1.831(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1 Acre Lot)
Runoff Coefficient = 0.723
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.800; Impervious fraction =  0.200
Initial subarea runoff =      5.703(CFS)
Total initial stream area =        4.310(Ac.)
Pervious area fraction = 0.800


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Process from Point/Station      101.700 to Point/Station      102.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Top of street segment elevation =  1365.000(Ft.)
End of street segment elevation =  1357.000(Ft.)
Length of street segment  =   493.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      6.563(CFS)
Depth of flow =   0.395(Ft.), Average velocity =   3.396(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  13.439(Ft.)
Flow velocity =   3.40(Ft/s)
Travel time =    2.42 min.     TC =   14.72  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.781
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
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RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      1.674(In/Hr) for a    10.0 year storm
Subarea runoff =      1.701(CFS) for      1.300(Ac.)
Total runoff =      7.404(CFS)       Total area =       5.610(Ac.)
Street flow at end of street =      7.404(CFS)
Half street flow at end of street =      7.404(CFS)
Depth of flow =   0.409(Ft.), Average velocity =   3.495(Ft/s)
Flow width (from curb towards crown)=  14.112(Ft.)


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Process from Point/Station      102.000 to Point/Station      104.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1357.000(Ft.)
End of street segment elevation =  1336.000(Ft.)
Length of street segment  =   411.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =     11.051(CFS)
Depth of flow =   0.390(Ft.), Average velocity =   5.951(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  13.154(Ft.)
Flow velocity =   5.95(Ft/s)
Travel time =    1.15 min.     TC =   15.87  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.778
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      1.612(In/Hr) for a    10.0 year storm
Subarea runoff =      7.201(CFS) for      5.740(Ac.)
Total runoff =     14.605(CFS)       Total area =      11.350(Ac.)
Street flow at end of street =     14.605(CFS)
Half street flow at end of street =     14.605(CFS)
Depth of flow =   0.421(Ft.), Average velocity =   6.362(Ft/s)
Flow width (from curb towards crown)=  14.727(Ft.)


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Process from Point/Station      104.000 to Point/Station      103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1336.000(Ft.)
Downstream point/station elevation =  1329.000(Ft.)
Pipe length  =    23.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    14.605(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =    14.605(CFS)
Normal flow depth in pipe =    7.70(In.)
Flow top width inside pipe =   11.51(In.)
Critical depth could not be calculated.
Pipe flow velocity =     27.41(Ft/s)
Travel time through pipe =    0.01 min.
Time of concentration (TC) =    15.88 min.


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Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     11.350(Ac.)
Runoff from this stream =     14.605(CFS)
Time of concentration =   15.88 min.
Rainfall intensity =     1.612(In/Hr)


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Process from Point/Station      105.000 to Point/Station      106.000
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**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------
Initial area flow distance =   737.000(Ft.)
Top (of initial area) elevation =  1410.000(Ft.)
Bottom (of initial area) elevation =  1363.000(Ft.)
Difference in elevation =    47.000(Ft.)
Slope =    0.06377  s(percent)=       6.38
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.298 min.
Rainfall intensity =      2.377(In/Hr) for a    10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.882
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      1.363(CFS)
Total initial stream area =        0.650(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station      106.000 to Point/Station      107.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Top of street segment elevation =  1363.000(Ft.)
End of street segment elevation =  1357.000(Ft.)
Length of street segment  =   576.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      2.699(CFS)
Depth of flow =   0.330(Ft.), Average velocity =   2.327(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  10.164(Ft.)
Flow velocity =   2.33(Ft/s)
Travel time =    4.13 min.     TC =   11.42  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.792
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      1.900(In/Hr) for a    10.0 year storm
Subarea runoff =      2.604(CFS) for      1.730(Ac.)
Total runoff =      3.967(CFS)       Total area =       2.380(Ac.)
Street flow at end of street =      3.967(CFS)
Half street flow at end of street =      3.967(CFS)
Depth of flow =   0.366(Ft.), Average velocity =   2.545(Ft/s)
Flow width (from curb towards crown)=  11.966(Ft.)


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Process from Point/Station      107.000 to Point/Station      108.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Top of street segment elevation =  1357.000(Ft.)
End of street segment elevation =  1336.000(Ft.)
Length of street segment  =   409.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
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 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      4.860(CFS)
Depth of flow =   0.312(Ft.), Average velocity =   4.927(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   9.272(Ft.)
Flow velocity =   4.93(Ft/s)
Travel time =    1.38 min.     TC =   12.81  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.787
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      1.795(In/Hr) for a    10.0 year storm
Subarea runoff =      1.710(CFS) for      1.210(Ac.)
Total runoff =      5.677(CFS)       Total area =       3.590(Ac.)
Street flow at end of street =      5.677(CFS)
Half street flow at end of street =      5.677(CFS)
Depth of flow =   0.325(Ft.), Average velocity =   5.103(Ft/s)
Flow width (from curb towards crown)=   9.928(Ft.)


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Process from Point/Station      108.000 to Point/Station      103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1336.000(Ft.)
Downstream point/station elevation =  1329.000(Ft.)
Pipe length  =    24.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     5.677(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     5.677(CFS)
Normal flow depth in pipe =    5.21(In.)
Flow top width inside pipe =    8.89(In.)
Critical depth could not be calculated.
Pipe flow velocity =     21.42(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =    12.82 min.


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Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 3
Stream flow area =      3.590(Ac.)
Runoff from this stream =      5.677(CFS)
Time of concentration =   12.82 min.
Rainfall intensity =     1.793(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                (In/Hr)


1       23.266     15.04                 1.656
2       14.605     15.88                 1.612
3        5.677     12.82                 1.793
Largest stream flow has longer or shorter time of concentration
Qp =     23.266 + sum of
          Qa          Tb/Ta
          14.605 *    0.947 =     13.828
          Qb         Ia/Ib
           5.677 *    0.924 =      5.243
Qp =     42.336

Total of 3 streams to confluence:
Flow rates before confluence point:
      23.266      14.605       5.677
Area of streams before confluence:
       17.620       11.350        3.590
Results of confluence:
Total flow rate =     42.336(CFS)
Time of concentration =    15.037 min.
Effective stream area after confluence =     32.560(Ac.)


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Process from Point/Station      103.000 to Point/Station      109.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1329.000(Ft.)
Downstream point/station elevation =  1309.000(Ft.)
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Pipe length  =   655.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    42.336(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    42.336(CFS)
Normal flow depth in pipe =   17.98(In.)
Flow top width inside pipe =   25.47(In.)
Critical Depth =   25.42(In.)
Pipe flow velocity =     15.06(Ft/s)
Travel time through pipe =    0.72 min.
Time of concentration (TC) =    15.76 min.


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Process from Point/Station      109.000 to Point/Station      109.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     32.560(Ac.)
Runoff from this stream =     42.336(CFS)
Time of concentration =   15.76 min.
Rainfall intensity =     1.618(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station      110.000 to Point/Station      111.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   707.000(Ft.)
Top (of initial area) elevation =  1360.800(Ft.)
Bottom (of initial area) elevation =  1336.000(Ft.)
Difference in elevation =    24.800(Ft.)
Slope =    0.03508  s(percent)=       3.51
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.515 min.
Rainfall intensity =      1.981(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.796
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      9.154(CFS)
Total initial stream area =        5.810(Ac.)
Pervious area fraction = 0.500


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Process from Point/Station      111.000 to Point/Station      112.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1336.000(Ft.)
End of street segment elevation =  1315.000(Ft.)
Length of street segment  =   675.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =     11.227(CFS)
Depth of flow =   0.419(Ft.), Average velocity =   4.947(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  14.638(Ft.)
Flow velocity =   4.95(Ft/s)
Travel time =    2.27 min.     TC =   12.79  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.787
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      1.796(In/Hr) for a    10.0 year storm
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Subarea runoff =      4.087(CFS) for      2.890(Ac.)
Total runoff =     13.241(CFS)        Total area =       8.700(Ac.)
Street flow at end of street =     13.241(CFS)
Half street flow at end of street =     13.241(CFS)
Depth of flow =   0.439(Ft.), Average velocity =   5.148(Ft/s)
Flow width (from curb towards crown)=  15.638(Ft.)


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Process from Point/Station      112.000 to Point/Station      112.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      8.700(Ac.)
Runoff from this stream =     13.241(CFS)
Time of concentration =   12.79 min.
Rainfall intensity =     1.796(In/Hr)


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Process from Point/Station      113.000 to Point/Station      112.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   806.000(Ft.)
Top (of initial area) elevation =  1326.500(Ft.)
Bottom (of initial area) elevation =  1315.000(Ft.)
Difference in elevation =    11.500(Ft.)
Slope =    0.01427  s(percent)=       1.43
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.266 min.
Rainfall intensity =      1.763(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.786
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      4.407(CFS)
Total initial stream area =        3.180(Ac.)
Pervious area fraction = 0.500


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Process from Point/Station      112.000 to Point/Station      112.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      3.180(Ac.)
Runoff from this stream =      4.407(CFS)
Time of concentration =   13.27 min.
Rainfall intensity =     1.763(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       13.241     12.79                 1.796
2        4.407     13.27                 1.763
Largest stream flow has longer or shorter time of concentration
Qp =     13.241 + sum of
          Qa          Tb/Ta
           4.407 *    0.964 =      4.249
Qp =     17.489

Total of 2 streams to confluence:
Flow rates before confluence point:
      13.241       4.407
Area of streams before confluence:
        8.700        3.180
Results of confluence:
Total flow rate =     17.489(CFS)
Time of concentration =    12.790 min.
Effective stream area after confluence =     11.880(Ac.)


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Process from Point/Station      112.000 to Point/Station      109.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1315.000(Ft.)
Downstream point/station elevation =  1309.000(Ft.)
Pipe length  =    30.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    17.489(CFS)
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Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =    17.489(CFS)
Normal flow depth in pipe =    8.43(In.)
Flow top width inside pipe =   14.89(In.)
Critical depth could not be calculated.
Pipe flow velocity =     24.66(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =    12.81 min.


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Process from Point/Station      109.000 to Point/Station      109.000
**** CONFLUENCE OF MAIN STREAMS ****
------------------------------------------------------------------------------
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =     11.880(Ac.)
Runoff from this stream =     17.489(CFS)
Time of concentration =   12.81 min.
Rainfall intensity =     1.794(In/Hr)
Program is now starting with Main Stream No. 3


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Process from Point/Station      108.000 to Point/Station      115.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   703.000(Ft.)
Top (of initial area) elevation =  1336.000(Ft.)
Bottom (of initial area) elevation =  1315.000(Ft.)
Difference in elevation =    21.000(Ft.)
Slope =    0.02987  s(percent)=       2.99
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.834 min.
Rainfall intensity =      1.951(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.794
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      3.596(CFS)
Total initial stream area =        2.320(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      115.000 to Point/Station      115.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 3 in normal stream number 1
Stream flow area =      2.320(Ac.)
Runoff from this stream =      3.596(CFS)
Time of concentration =   10.83 min.
Rainfall intensity =     1.951(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      114.000 to Point/Station      115.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   800.000(Ft.)
Top (of initial area) elevation =  1326.500(Ft.)
Bottom (of initial area) elevation =  1315.000(Ft.)
Difference in elevation =    11.500(Ft.)
Slope =    0.01438  s(percent)=       1.44
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.206 min.
Rainfall intensity =      1.767(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.786
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      5.043(CFS)
Total initial stream area =        3.630(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      115.000 to Point/Station      115.000
```

```
**** CONFLUENCE OF MINOR STREAMS ****
--------------------------------------------------------------------------------
Along Main Stream number: 3 in normal stream number 2
Stream flow area =      3.630(Ac.)
Runoff from this stream =      5.043(CFS)
Time of concentration =   13.21 min.
Rainfall intensity =     1.767(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        3.596     10.83                1.951
2        5.043     13.21                1.767
Largest stream flow has longer time of concentration
Qp =      5.043 + sum of
          Qb         Ia/Ib
           3.596 *    0.906 =      3.257
Qp =      8.300

Total of 2 streams to confluence:
Flow rates before confluence point:
       3.596       5.043
Area of streams before confluence:
        2.320        3.630
Results of confluence:
Total flow rate =      8.300(CFS)
Time of concentration =    13.206 min.
Effective stream area after confluence =      5.950(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      115.000 to Point/Station      109.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
--------------------------------------------------------------------------------
Upstream point/station elevation =  1315.000(Ft.)
Downstream point/station elevation =  1309.000(Ft.)
Pipe length  =    21.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     8.300(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     8.300(CFS)
Normal flow depth in pipe =    6.93(In.)
Flow top width inside pipe =    7.58(In.)
Critical depth could not be calculated.
Pipe flow velocity =     22.76(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =    13.22 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      109.000 to Point/Station      109.000
**** CONFLUENCE OF MAIN STREAMS ****
--------------------------------------------------------------------------------
The following data inside Main Stream is listed:
In Main Stream number: 3
Stream flow area =      5.950(Ac.)
Runoff from this stream =      8.300(CFS)
Time of concentration =   13.22 min.
Rainfall intensity =     1.766(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       42.336     15.76                1.618
2       17.489     12.81                1.794
3        8.300     13.22                1.766
Largest stream flow has longer time of concentration
Qp =     42.336 + sum of
          Qb         Ia/Ib
          17.489 *    0.901 =     15.767
          Qb         Ia/Ib
           8.300 *    0.916 =      7.601
Qp =     65.704

Total of 3 main streams to confluence:
Flow rates before confluence point:
      42.336      17.489       8.300
Area of streams before confluence:
       32.560       11.880        5.950


Results of confluence:
Total flow rate =     65.704(CFS)
```

```
Time of concentration =    15.762 min.
Effective stream area after confluence  =     50.390(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      109.000 to Point/Station      116.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1309.000(Ft.)
Downstream point/station elevation =  1293.000(Ft.)
Pipe length  =   317.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    65.704(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    65.704(CFS)
Normal flow depth in pipe =   20.91(In.)
Flow top width inside pipe =   22.57(In.)
Critical depth could not be calculated.
Pipe flow velocity =     19.91(Ft/s)
Travel time through pipe =    0.27 min.
Time of concentration (TC) =    16.03 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      116.000 to Point/Station      117.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.697
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  74.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    16.03 min.
Rainfall intensity =      1.604(In/Hr) for a    10.0 year storm
Subarea runoff =      1.576(CFS) for      1.410(Ac.)
Total runoff =     67.280(CFS)       Total area =      51.800(Ac.)
End of computations, total study area =           51.80 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.534
Area averaged RI index number =  69.1
```

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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 02/06/24  File:PRO310.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

------------------------------------------------------------------------
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =   10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year =  10.0
Calculated rainfall intensity data:
1 hour intensity =  0.829(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      200.000 to Point/Station      201.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   936.000(Ft.)
Top (of initial area) elevation =  1345.000(Ft.)
Bottom (of initial area) elevation =  1290.000(Ft.)
Difference in elevation =    55.000(Ft.)
Slope =    0.05876  s(percent)=       5.88
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    8.162 min.
Rainfall intensity =      2.248(In/Hr) for a    10.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.881
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      1.347(CFS)
Total initial stream area =        0.680(Ac.)
Pervious area fraction = 0.100


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      201.000 to Point/Station      202.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of street segment elevation =  1290.000(Ft.)
End of street segment elevation =  1282.000(Ft.)
Length of street segment  =   461.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [2] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      2.628(CFS)
Depth of flow =   0.255(Ft.), Average velocity =   2.436(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   6.424(Ft.)
Flow velocity =   2.44(Ft/s)
Travel time =    3.15 min.     TC =   11.32  min.
 Adding area flow to street
```

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SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.793
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      1.909(In/Hr) for a    10.0 year storm
Subarea runoff =      2.376(CFS) for      1.570(Ac.)
Total runoff =      3.722(CFS)       Total area =       2.250(Ac.)
Street flow at end of street =      3.722(CFS)
Half street flow at end of street =      1.861(CFS)
Depth of flow =   0.280(Ft.), Average velocity =   2.615(Ft/s)
Flow width (from curb towards crown)=   7.649(Ft.)


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Process from Point/Station      202.000 to Point/Station      203.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1282.000(Ft.)
Downstream point/station elevation =  1275.000(Ft.)
Pipe length  =   427.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.722(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     3.722(CFS)
Normal flow depth in pipe =    8.24(In.)
Flow top width inside pipe =   11.13(In.)
Critical Depth =    9.86(In.)
Pipe flow velocity =      6.48(Ft/s)
Travel time through pipe =    1.10 min.
Time of concentration (TC) =    12.42 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      203.000 to Point/Station      203.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      2.250(Ac.)
Runoff from this stream =      3.722(CFS)
Time of concentration =   12.42 min.
Rainfall intensity =     1.823(In/Hr)


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Process from Point/Station      204.000 to Point/Station      205.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   914.000(Ft.)
Top (of initial area) elevation =  1345.000(Ft.)
Bottom (of initial area) elevation =  1290.000(Ft.)
Difference in elevation =    55.000(Ft.)
Slope =    0.06018  s(percent)=       6.02
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.461 min.
Rainfall intensity =      1.986(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.796
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      6.778(CFS)
Total initial stream area =        4.290(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      205.000 to Point/Station      203.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1290.000(Ft.)
Downstream point/station elevation =  1275.000(Ft.)
Pipe length  =    75.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     6.778(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     6.778(CFS)
Normal flow depth in pipe =    6.77(In.)
Flow top width inside pipe =    7.77(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.99(Ft/s)
Travel time through pipe =    0.07 min.
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Time of concentration (TC) =    10.53 min.


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Process from Point/Station      203.000 to Point/Station      203.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      4.290(Ac.)
Runoff from this stream =      6.778(CFS)
Time of concentration =   10.53 min.
Rainfall intensity =     1.979(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        3.722     12.42                 1.823
2        6.778     10.53                 1.979
Largest stream flow has longer or shorter time of concentration
Qp =      6.778 + sum of
          Qa          Tb/Ta
           3.722 *    0.848 =      3.156
Qp =      9.934

Total of 2 streams to confluence:
Flow rates before confluence point:
       3.722       6.778
Area of streams before confluence:
        2.250        4.290
Results of confluence:
Total flow rate =      9.934(CFS)
Time of concentration =    10.526 min.
Effective stream area after confluence =      6.540(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      203.000 to Point/Station      206.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1275.000(Ft.)
Downstream point/station elevation =  1264.000(Ft.)
Pipe length  =   110.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     9.934(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     9.934(CFS)
Normal flow depth in pipe =    8.75(In.)
Flow top width inside pipe =   10.66(In.)
Critical depth could not be calculated.
Pipe flow velocity =     16.19(Ft/s)
Travel time through pipe =    0.11 min.
Time of concentration (TC) =    10.64 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      206.000 to Point/Station      207.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.727
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  74.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    10.64 min.
Rainfall intensity =      1.969(In/Hr) for a    10.0 year storm
Subarea runoff =      1.789(CFS) for      1.250(Ac.)
Total runoff =     11.724(CFS)       Total area =       7.790(Ac.)
End of computations, total study area =            7.79 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.545
Area averaged RI index number =  69.8
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 02/06/24  File:PROOFF10.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

------------------------------------------------------------------------
Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =   10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year =  10.0
Calculated rainfall intensity data:
1 hour intensity =  0.829(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      300.000 to Point/Station      301.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   930.000(Ft.)
Top (of initial area) elevation =  1522.000(Ft.)
Bottom (of initial area) elevation =  1448.000(Ft.)
Difference in elevation =    74.000(Ft.)
Slope =    0.07957  s(percent)=       7.96
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.537 min.
Rainfall intensity =      1.746(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.800
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      9.529(CFS)
Total initial stream area =        6.820(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      301.000 to Point/Station      302.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of natural channel elevation =   1448.000(Ft.)
End of natural channel elevation =   1363.000(Ft.)
Length of natural channel  =  1674.000(Ft.)
Estimated mean flow rate at midpoint of channel =     24.243(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.11(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0508
Corrected/adjusted channel slope =  0.0508
Travel time =    3.92 min.     TC =   17.46  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.789
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
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Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.537(In/Hr) for a    10.0 year storm
Subarea runoff =     25.529(CFS) for     21.060(Ac.)
Total runoff =     35.058(CFS)       Total area =      27.880(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      302.000 to Point/Station      303.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1363.000(Ft.)
Downstream point/station elevation =  1359.000(Ft.)
Pipe length  =    86.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    35.058(CFS)
Nearest computed pipe diameter  =     21.00(In.)
Calculated individual pipe flow  =    35.058(CFS)
Normal flow depth in pipe =   17.77(In.)
Flow top width inside pipe =   15.16(In.)
Critical depth could not be calculated.
Pipe flow velocity =     16.17(Ft/s)
Travel time through pipe =    0.09 min.
Time of concentration (TC) =    17.55 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      303.000 to Point/Station      303.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     27.880(Ac.)
Runoff from this stream =     35.058(CFS)
Time of concentration =   17.55 min.
Rainfall intensity =     1.533(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      304.000 to Point/Station      305.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =  1000.000(Ft.)
Top (of initial area) elevation =  1468.000(Ft.)
Bottom (of initial area) elevation =  1377.000(Ft.)
Difference in elevation =    91.000(Ft.)
Slope =    0.09100  s(percent)=       9.10
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.566 min.
Rainfall intensity =      1.744(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.800
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     12.490(CFS)
Total initial stream area =        8.950(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      305.000 to Point/Station      303.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1377.000(Ft.)
Downstream point/station elevation =  1359.000(Ft.)
Pipe length  =   366.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    12.490(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =    12.490(CFS)
Normal flow depth in pipe =   10.84(In.)
Flow top width inside pipe =   13.43(In.)
Critical depth could not be calculated.
Pipe flow velocity =     13.15(Ft/s)
Travel time through pipe =    0.46 min.
Time of concentration (TC) =    14.03 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      303.000 to Point/Station      303.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      8.950(Ac.)
```

```
Runoff from this stream =     12.490(CFS)
Time of concentration =   14.03 min.
Rainfall intensity =     1.715(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       35.058     17.55                  1.533
2       12.490     14.03                  1.715
Largest stream flow has longer time of concentration
Qp =     35.058 + sum of
          Qb         Ia/Ib
          12.490 *    0.894 =     11.169
Qp =     46.227

Total of 2 streams to confluence:
Flow rates before confluence point:
      35.058      12.490
Area of streams before confluence:
       27.880        8.950
Results of confluence:
Total flow rate =     46.227(CFS)
Time of concentration =    17.547 min.
Effective stream area after confluence =     36.830(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      303.000 to Point/Station      306.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1359.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =    75.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    46.227(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    46.227(CFS)
Normal flow depth in pipe =   17.55(In.)
Flow top width inside pipe =   21.27(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.78(Ft/s)
Travel time through pipe =    0.07 min.
Time of concentration (TC) =    17.61 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      306.000 to Point/Station      307.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1355.000(Ft.)
End of natural channel elevation =   1329.000(Ft.)
Length of natural channel  =   405.000(Ft.)
Estimated mean flow rate at midpoint of channel =     48.474(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.72(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0642
Corrected/adjusted channel slope =  0.0642
Travel time =    0.69 min.     TC =   18.31  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.786
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.501(In/Hr) for a    10.0 year storm
Subarea runoff =      4.225(CFS) for      3.580(Ac.)
Total runoff =     50.452(CFS)       Total area =      40.410(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      307.000 to Point/Station      308.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1329.000(Ft.)
```

```
Downstream point/station elevation =  1319.000(Ft.)
Pipe length  =   258.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    50.452(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    50.452(CFS)
Normal flow depth in pipe =   18.73(In.)
Flow top width inside pipe =   24.89(In.)
Critical depth could not be calculated.
Pipe flow velocity =     17.14(Ft/s)
Travel time through pipe =    0.25 min.
Time of concentration (TC) =    18.56 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      308.000 to Point/Station      309.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1319.000(Ft.)
End of natural channel elevation =   1299.000(Ft.)
Length of natural channel  =   332.000(Ft.)
Estimated mean flow rate at midpoint of channel =     51.076(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.56(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0602
Corrected/adjusted channel slope =  0.0602
Travel time =    0.58 min.     TC =   19.14  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.784
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.468(In/Hr) for a    10.0 year storm
Subarea runoff =      1.151(CFS) for      1.000(Ac.)
Total runoff =     51.603(CFS)       Total area =      41.410(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      309.000 to Point/Station      309.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     41.410(Ac.)
Runoff from this stream =     51.603(CFS)
Time of concentration =   19.14 min.
Rainfall intensity =     1.468(In/Hr)
Program is now starting with Main Stream No. 2


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      310.000 to Point/Station      311.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   972.000(Ft.)
Top (of initial area) elevation =  1518.000(Ft.)
Bottom (of initial area) elevation =  1451.000(Ft.)
Difference in elevation =    67.000(Ft.)
Slope =    0.06893  s(percent)=       6.89
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.179 min.
Rainfall intensity =      1.706(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.798
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     11.683(CFS)
Total initial stream area =        8.580(Ac.)
Pervious area fraction = 1.000
```

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++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      311.000 to Point/Station      312.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1451.000(Ft.)
End of natural channel elevation =   1371.000(Ft.)
Length of natural channel  =  1830.000(Ft.)
Estimated mean flow rate at midpoint of channel =     21.597(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.40(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0437
Corrected/adjusted channel slope =  0.0437
Travel time =    4.77 min.     TC =   18.95  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.785
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.475(In/Hr) for a    10.0 year storm
Subarea runoff =     16.855(CFS) for     14.560(Ac.)
Total runoff =     28.538(CFS)       Total area =      23.140(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      312.000 to Point/Station      313.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1371.000(Ft.)
Downstream point/station elevation =  1360.000(Ft.)
Pipe length  =   473.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    28.538(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    28.538(CFS)
Normal flow depth in pipe =   16.64(In.)
Flow top width inside pipe =   22.13(In.)
Critical Depth =   22.07(In.)
Pipe flow velocity =     12.27(Ft/s)
Travel time through pipe =    0.64 min.
Time of concentration (TC) =    19.59 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      313.000 to Point/Station      314.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1360.000(Ft.)
End of natural channel elevation =   1347.000(Ft.)
Length of natural channel  =   166.000(Ft.)
Estimated mean flow rate at midpoint of channel =     28.883(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.27(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0783
Corrected/adjusted channel slope =  0.0783
Travel time =    0.30 min.     TC =   19.89  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.782
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.440(In/Hr) for a    10.0 year storm
Subarea runoff =      0.631(CFS) for      0.560(Ac.)
Total runoff =     29.169(CFS)       Total area =      23.700(Ac.)
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Process from Point/Station      314.000 to Point/Station      314.000
**** CONFLUENCE OF MINOR STREAMS ****
____________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     23.700(Ac.)
Runoff from this stream =     29.169(CFS)
Time of concentration =   19.89 min.
Rainfall intensity =     1.440(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      315.000 to Point/Station      316.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   682.000(Ft.)
Top (of initial area) elevation =  1471.000(Ft.)
Bottom (of initial area) elevation =  1433.000(Ft.)
Difference in elevation =    38.000(Ft.)
Slope =    0.05572  s(percent)=       5.57
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.841 min.
Rainfall intensity =      1.792(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.803
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      6.921(CFS)
Total initial stream area =        4.810(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      316.000 to Point/Station      314.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of natural channel elevation =   1433.000(Ft.)
End of natural channel elevation =   1347.000(Ft.)
Length of natural channel  =  1629.000(Ft.)
Estimated mean flow rate at midpoint of channel =     22.380(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.10(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0528
Corrected/adjusted channel slope =  0.0528
Travel time =    3.83 min.     TC =   16.67  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.791
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.573(In/Hr) for a    10.0 year storm
Subarea runoff =     26.738(CFS) for     21.490(Ac.)
Total runoff =     33.659(CFS)       Total area =      26.300(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      314.000 to Point/Station      314.000
**** CONFLUENCE OF MINOR STREAMS ****
____________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     26.300(Ac.)
Runoff from this stream =     33.659(CFS)
Time of concentration =   16.67 min.
Rainfall intensity =     1.573(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)
```

```
1       29.169     19.89                1.440
2       33.659     16.67                1.573
Largest stream flow has longer or shorter time of concentration
Qp =     33.659 + sum of
          Qa          Tb/Ta
          29.169 *    0.838 =     24.442
Qp =     58.101

Total of 2 streams to confluence:
Flow rates before confluence point:
      29.169      33.659
Area of streams before confluence:
       23.700       26.300
Results of confluence:
Total flow rate =     58.101(CFS)
Time of concentration =    16.666 min.
Effective stream area after confluence =     50.000(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      314.000 to Point/Station      309.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1347.000(Ft.)
End of natural channel elevation =   1299.000(Ft.)
Length of natural channel  =  1131.000(Ft.)
Estimated mean flow rate at midpoint of channel =     61.134(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.45(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0424
Corrected/adjusted channel slope =  0.0424
Travel time =    2.23 min.     TC =   18.90  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.785
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.477(In/Hr) for a    10.0 year storm
Subarea runoff =      6.052(CFS) for      5.220(Ac.)
Total runoff =     64.153(CFS)        Total area =      55.220(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      309.000 to Point/Station      309.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =     55.220(Ac.)
Runoff from this stream =     64.153(CFS)
Time of concentration =   18.90 min.
Rainfall intensity =     1.477(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       51.603     19.14                1.468
2       64.153     18.90                1.477
Largest stream flow has longer or shorter time of concentration
Qp =     64.153 + sum of
          Qa          Tb/Ta
          51.603 *    0.987 =     50.950
Qp =    115.103

Total of 2 main streams to confluence:
Flow rates before confluence point:
      51.603      64.153
Area of streams before confluence:
       41.410       55.220
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Results of confluence:
Total flow rate =    115.103(CFS)
Time of concentration =    18.896 min.
Effective stream area after confluence  =     96.630(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      309.000 to Point/Station      317.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1299.000(Ft.)
End of natural channel elevation =   1251.000(Ft.)
Length of natural channel  =  1118.000(Ft.)
Estimated mean flow rate at midpoint of channel =    117.361(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  10.32(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0429
Corrected/adjusted channel slope =  0.0429
Travel time =    1.81 min.     TC =   20.70  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.780
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.412(In/Hr) for a    10.0 year storm
Subarea runoff =      4.173(CFS) for      3.790(Ac.)
Total runoff =    119.277(CFS)       Total area =     100.420(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      317.000 to Point/Station      317.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    100.420(Ac.)
Runoff from this stream =    119.277(CFS)
Time of concentration =   20.70 min.
Rainfall intensity =     1.412(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      117.000 to Point/Station      117.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****
------------------------------------------------------------------------------
Rainfall intensity =      1.632(In/Hr) for a    10.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.779
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
User specified values are as follows:
TC =  15.49 min.  Rain intensity =       1.63(In/Hr)
Total area =        51.80(Ac.)  Total runoff =     67.28(CFS)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      117.000 to Point/Station      317.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1291.000(Ft.)
Downstream point/station elevation =  1251.000(Ft.)
Pipe length  =   134.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    67.280(CFS)
Nearest computed pipe diameter  =     21.00(In.)
Calculated individual pipe flow  =    67.280(CFS)
Normal flow depth in pipe =   13.92(In.)
Flow top width inside pipe =   19.85(In.)
Critical depth could not be calculated.
Pipe flow velocity =     39.78(Ft/s)
Travel time through pipe =    0.06 min.
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Time of concentration (TC) =    15.55 min.


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Process from Point/Station      317.000 to Point/Station      317.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     51.800(Ac.)
Runoff from this stream =     67.280(CFS)
Time of concentration =   15.55 min.
Rainfall intensity =     1.629(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      119.277     20.70                 1.412
2       67.280     15.55                 1.629
Largest stream flow has longer time of concentration
Qp =    119.277 + sum of
          Qb          Ia/Ib
          67.280 *    0.867 =     58.304
Qp =    177.581

Total of 2 streams to confluence:
Flow rates before confluence point:
     119.277      67.280
Area of streams before confluence:
      100.420       51.800
Results of confluence:
Total flow rate =    177.581(CFS)
Time of concentration =    20.701 min.
Effective stream area after confluence =    152.220(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      317.000 to Point/Station      318.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1251.000(Ft.)
End of natural channel elevation =   1243.000(Ft.)
Length of natural channel  =   225.000(Ft.)
Estimated mean flow rate at midpoint of channel =    178.088(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  10.67(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0356
Corrected/adjusted channel slope =  0.0356
Travel time =    0.35 min.     TC =   21.05  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.779
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.400(In/Hr) for a    10.0 year storm
Subarea runoff =      0.949(CFS) for      0.870(Ac.)
Total runoff =    178.530(CFS)       Total area =     153.090(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      318.000 to Point/Station      318.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    153.090(Ac.)
Runoff from this stream =    178.530(CFS)
Time of concentration =   21.05 min.
Rainfall intensity =     1.400(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      319.000 to Point/Station      318.000
**** INITIAL AREA EVALUATION ****
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```
Initial area flow distance =   573.000(Ft.)
Top (of initial area) elevation =  1322.000(Ft.)
Bottom (of initial area) elevation =  1243.000(Ft.)
Difference in elevation =    79.000(Ft.)
Slope =    0.13787  s(percent)=      13.79
TC = k(0.940)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   17.721 min.
Rainfall intensity =      1.526(In/Hr) for a    10.0 year storm
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.689
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  74.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      2.553(CFS)
Total initial stream area =        2.430(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      318.000 to Point/Station      318.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      2.430(Ac.)
Runoff from this stream =      2.553(CFS)
Time of concentration =   17.72 min.
Rainfall intensity =     1.526(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      178.530     21.05                 1.400
2        2.553     17.72                 1.526
Largest stream flow has longer time of concentration
Qp =    178.530 + sum of
          Qb          Ia/Ib
           2.553 *    0.917 =      2.342
Qp =    180.872

Total of 2 streams to confluence:
Flow rates before confluence point:
     178.530       2.553
Area of streams before confluence:
      153.090        2.430
Results of confluence:
Total flow rate =    180.872(CFS)
Time of concentration =    21.053 min.
Effective stream area after confluence =    155.520(Ac.)
End of computations, total study area =          155.52 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.833
Area averaged RI index number =  80.2
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 02/06/24  File:PROOFF210.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

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Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =   10.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year =  10.0
Calculated rainfall intensity data:
1 hour intensity =  0.829(In/Hr)
Slope of intensity duration curve = 0.5000



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Process from Point/Station      501.000 to Point/Station      502.000
**** INITIAL AREA EVALUATION ****
________________________________________________________________________
Initial area flow distance =   914.000(Ft.)
Top (of initial area) elevation =  1620.000(Ft.)
Bottom (of initial area) elevation =  1572.000(Ft.)
Difference in elevation =    48.000(Ft.)
Slope =    0.05252  s(percent)=       5.25
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.608 min.
Rainfall intensity =      1.680(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.791
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.900
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  85.20
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     12.746(CFS)
Total initial stream area =        9.590(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      502.000 to Point/Station      503.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1572.000(Ft.)
End of natural channel elevation =   1444.000(Ft.)
Length of natural channel  =  4065.000(Ft.)
Estimated mean flow rate at midpoint of channel =     72.191(CFS)

Natural mountain channel type used
L.A. County flood control district formula for channel velocity:
 Velocity = 5.48(q^.33)(slope^.492)
Velocity using mean channel flow =   4.10(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0315
Corrected/adjusted channel slope =  0.0315
Travel time =   16.51 min.     TC =   31.12  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.747
Decimal fraction soil group A = 0.000
```

```
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.600
Decimal fraction soil group D = 0.200
RI index for soil(AMC 2)  =  85.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.151(In/Hr) for a    10.0 year storm
Subarea runoff =     76.958(CFS) for     89.450(Ac.)
Total runoff =     89.704(CFS)       Total area =      99.040(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      503.000 to Point/Station      503.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     99.040(Ac.)
Runoff from this stream =     89.704(CFS)
Time of concentration =   31.12 min.
Rainfall intensity =     1.151(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      504.000 to Point/Station      505.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   952.000(Ft.)
Top (of initial area) elevation =  1572.000(Ft.)
Bottom (of initial area) elevation =  1532.000(Ft.)
Difference in elevation =    40.000(Ft.)
Slope =    0.04202  s(percent)=       4.20
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   15.526 min.
Rainfall intensity =      1.630(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.794
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      9.748(CFS)
Total initial stream area =        7.530(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      505.000 to Point/Station      503.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1532.000(Ft.)
End of natural channel elevation =   1444.000(Ft.)
Length of natural channel  =  2338.000(Ft.)
Estimated mean flow rate at midpoint of channel =     46.889(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.37(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0376
Corrected/adjusted channel slope =  0.0376
Travel time =    5.29 min.     TC =   20.81  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.780
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.408(In/Hr) for a    10.0 year storm
Subarea runoff =     62.990(CFS) for     57.380(Ac.)
Total runoff =     72.738(CFS)       Total area =      64.910(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      503.000 to Point/Station      503.000
**** CONFLUENCE OF MINOR STREAMS ****
```

```
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     64.910(Ac.)
Runoff from this stream =     72.738(CFS)
Time of concentration =   20.81 min.
Rainfall intensity =     1.408(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                (In/Hr)


1       89.704     31.12                 1.151
2       72.738     20.81                 1.408
Largest stream flow has longer time of concentration
Qp =     89.704 + sum of
          Qb         Ia/Ib
          72.738 *    0.818 =     59.485
Qp =    149.190

Total of 2 streams to confluence:
Flow rates before confluence point:
      89.704      72.738
Area of streams before confluence:
       99.040       64.910
Results of confluence:
Total flow rate =    149.190(CFS)
Time of concentration =    31.118 min.
Effective stream area after confluence =    163.950(Ac.)


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Process from Point/Station      503.000 to Point/Station      506.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Top of natural channel elevation =   1444.000(Ft.)
End of natural channel elevation =   1426.000(Ft.)
Length of natural channel  =   816.000(Ft.)
Estimated mean flow rate at midpoint of channel =    166.211(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.23(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0221
Corrected/adjusted channel slope =  0.0221
Travel time =    1.65 min.     TC =   32.77  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.749
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  85.50
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.122(In/Hr) for a    10.0 year storm
Subarea runoff =     31.437(CFS) for     37.410(Ac.)
Total runoff =    180.626(CFS)       Total area =     201.360(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      506.000 to Point/Station      507.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =  1426.000(Ft.)
Downstream point/station elevation =  1414.000(Ft.)
Pipe length  =    73.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =   180.626(CFS)
Nearest computed pipe diameter  =     33.00(In.)
Calculated individual pipe flow  =   180.626(CFS)
Normal flow depth in pipe =   23.20(In.)
Flow top width inside pipe =   30.15(In.)
Critical depth could not be calculated.
Pipe flow velocity =     40.46(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    32.80 min.
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Process from Point/Station      507.000 to Point/Station      508.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1414.000(Ft.)
End of natural channel elevation =   1369.000(Ft.)
Length of natural channel  =  1860.000(Ft.)
Estimated mean flow rate at midpoint of channel =    191.046(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.99(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0242
Corrected/adjusted channel slope =  0.0242
Travel time =    3.45 min.     TC =   36.25  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.748
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.067(In/Hr) for a    10.0 year storm
Subarea runoff =     18.531(CFS) for     23.230(Ac.)
Total runoff =    199.158(CFS)       Total area =     224.590(Ac.)


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Process from Point/Station      508.000 to Point/Station      508.000
**** CONFLUENCE OF MAIN STREAMS ****
----------------------------------------------------------------------------
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =    224.590(Ac.)
Runoff from this stream =    199.158(CFS)
Time of concentration =   36.25 min.
Rainfall intensity =     1.067(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station      509.000 to Point/Station      510.000
**** INITIAL AREA EVALUATION ****
----------------------------------------------------------------------------
Initial area flow distance =   901.000(Ft.)
Top (of initial area) elevation =  1592.000(Ft.)
Bottom (of initial area) elevation =  1516.000(Ft.)
Difference in elevation =    76.000(Ft.)
Slope =    0.08435  s(percent)=       8.44
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.211 min.
Rainfall intensity =      1.767(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.802
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      6.189(CFS)
Total initial stream area =        4.370(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station      510.000 to Point/Station      511.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1516.000(Ft.)
End of natural channel elevation =   1452.000(Ft.)
Length of natural channel  =  2076.000(Ft.)
Estimated mean flow rate at midpoint of channel =     27.695(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
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 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   5.75(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0308
Corrected/adjusted channel slope =  0.0308
Travel time =    6.02 min.     TC =   19.23  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.784
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.465(In/Hr) for a    10.0 year storm
Subarea runoff =     34.866(CFS) for     30.370(Ac.)
Total runoff =     41.055(CFS)       Total area =      34.740(Ac.)


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Process from Point/Station      511.000 to Point/Station      512.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1452.000(Ft.)
Downstream point/station elevation =  1451.000(Ft.)
Pipe length  =    40.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    41.055(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    41.055(CFS)
Normal flow depth in pipe =   18.91(In.)
Flow top width inside pipe =   24.73(In.)
Critical Depth =   25.25(In.)
Pipe flow velocity =     13.79(Ft/s)
Travel time through pipe =    0.05 min.
Time of concentration (TC) =    19.28 min.


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Process from Point/Station      512.000 to Point/Station      513.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1451.000(Ft.)
End of natural channel elevation =   1412.000(Ft.)
Length of natural channel  =   777.000(Ft.)
Estimated mean flow rate at midpoint of channel =     42.183(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.26(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0502
Corrected/adjusted channel slope =  0.0502
Travel time =    1.57 min.     TC =   20.84  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.780
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.407(In/Hr) for a    10.0 year storm
Subarea runoff =      2.095(CFS) for      1.910(Ac.)
Total runoff =     43.150(CFS)       Total area =      36.650(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      513.000 to Point/Station      513.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     36.650(Ac.)
Runoff from this stream =     43.150(CFS)
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Time of concentration =   20.84 min.
Rainfall intensity =     1.407(In/Hr)


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Process from Point/Station      510.000 to Point/Station      514.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   923.000(Ft.)
Top (of initial area) elevation =  1516.000(Ft.)
Bottom (of initial area) elevation =  1493.000(Ft.)
Difference in elevation =    23.000(Ft.)
Slope =    0.02492  s(percent)=       2.49
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   17.024 min.
Rainfall intensity =      1.557(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.790
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      2.963(CFS)
Total initial stream area =        2.410(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station      514.000 to Point/Station      515.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of natural channel elevation =   1493.000(Ft.)
End of natural channel elevation =   1418.000(Ft.)
Length of natural channel  =  1990.000(Ft.)
Estimated mean flow rate at midpoint of channel =      8.865(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   4.71(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0377
Corrected/adjusted channel slope =  0.0377
Travel time =    7.05 min.     TC =   24.07  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.772
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.309(In/Hr) for a    10.0 year storm
Subarea runoff =      9.702(CFS) for      9.600(Ac.)
Total runoff =     12.665(CFS)        Total area =      12.010(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      515.000 to Point/Station      513.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1418.000(Ft.)
Downstream point/station elevation =  1412.000(Ft.)
Pipe length  =    74.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    12.665(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =    12.665(CFS)
Normal flow depth in pipe =    9.14(In.)
Flow top width inside pipe =   14.64(In.)
Critical depth could not be calculated.
Pipe flow velocity =     16.16(Ft/s)
Travel time through pipe =    0.08 min.
Time of concentration (TC) =    24.15 min.


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Process from Point/Station      513.000 to Point/Station      513.000
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**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     12.010(Ac.)
Runoff from this stream =     12.665(CFS)
Time of concentration =   24.15 min.
Rainfall intensity =     1.307(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       43.150     20.84                 1.407
2       12.665     24.15                 1.307
Largest stream flow has longer or shorter time of concentration
Qp =     43.150 + sum of
          Qa          Tb/Ta
          12.665 *    0.863 =     10.933
Qp =     54.083

Total of 2 streams to confluence:
Flow rates before confluence point:
      43.150      12.665
Area of streams before confluence:
       36.650       12.010
Results of confluence:
Total flow rate =     54.083(CFS)
Time of concentration =    20.844 min.
Effective stream area after confluence =     48.660(Ac.)


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Process from Point/Station      513.000 to Point/Station      516.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Top of natural channel elevation =   1412.000(Ft.)
End of natural channel elevation =   1406.000(Ft.)
Length of natural channel  =   142.000(Ft.)
Estimated mean flow rate at midpoint of channel =     54.616(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.16(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0423
Corrected/adjusted channel slope =  0.0423
Travel time =    0.29 min.     TC =   21.13  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.779
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.397(In/Hr) for a    10.0 year storm
Subarea runoff =      1.045(CFS) for      0.960(Ac.)
Total runoff =     55.127(CFS)       Total area =      49.620(Ac.)


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Process from Point/Station      516.000 to Point/Station      516.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     49.620(Ac.)
Runoff from this stream =     55.127(CFS)
Time of concentration =   21.13 min.
Rainfall intensity =     1.397(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      517.000 to Point/Station      518.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------
Initial area flow distance =   928.000(Ft.)
Top (of initial area) elevation =  1510.000(Ft.)
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```
Bottom (of initial area) elevation =  1450.000(Ft.)
Difference in elevation =    60.000(Ft.)
Slope =    0.06466  s(percent)=       6.47
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.099 min.
Rainfall intensity =      1.710(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.799
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     10.519(CFS)
Total initial stream area =        7.700(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station      518.000 to Point/Station      516.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1450.000(Ft.)
End of natural channel elevation =   1406.000(Ft.)
Length of natural channel  =   897.000(Ft.)
Estimated mean flow rate at midpoint of channel =     14.849(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.13(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0491
Corrected/adjusted channel slope =  0.0491
Travel time =    2.44 min.     TC =   16.54  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.791
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.579(In/Hr) for a    10.0 year storm
Subarea runoff =      7.923(CFS) for      6.340(Ac.)
Total runoff =     18.441(CFS)       Total area =      14.040(Ac.)


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Process from Point/Station      516.000 to Point/Station      516.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     14.040(Ac.)
Runoff from this stream =     18.441(CFS)
Time of concentration =   16.54 min.
Rainfall intensity =     1.579(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       55.127     21.13                 1.397
2       18.441     16.54                 1.579
Largest stream flow has longer time of concentration
Qp =     55.127 + sum of
          Qb         Ia/Ib
          18.441 *    0.885 =     16.313
Qp =     71.440

Total of 2 streams to confluence:
Flow rates before confluence point:
      55.127      18.441
Area of streams before confluence:
       49.620       14.040
Results of confluence:
Total flow rate =     71.440(CFS)
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Time of concentration =    21.134 min.
Effective stream area after confluence =     63.660(Ac.)


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Process from Point/Station      516.000 to Point/Station      519.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1406.000(Ft.)
End of natural channel elevation =   1386.000(Ft.)
Length of natural channel  =   577.000(Ft.)
Estimated mean flow rate at midpoint of channel =     72.820(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.04(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0347
Corrected/adjusted channel slope =  0.0347
Travel time =    1.20 min.     TC =   22.33  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.776
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.359(In/Hr) for a    10.0 year storm
Subarea runoff =      2.595(CFS) for      2.460(Ac.)
Total runoff =     74.035(CFS)       Total area =      66.120(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      519.000 to Point/Station      519.000
**** CONFLUENCE OF MINOR STREAMS ****
----------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     66.120(Ac.)
Runoff from this stream =     74.035(CFS)
Time of concentration =   22.33 min.
Rainfall intensity =     1.359(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      520.000 to Point/Station      521.000
**** INITIAL AREA EVALUATION ****
----------------------------------------------------------------------------
Initial area flow distance =   986.000(Ft.)
Top (of initial area) elevation =  1540.000(Ft.)
Bottom (of initial area) elevation =  1480.000(Ft.)
Difference in elevation =    60.000(Ft.)
Slope =    0.06085  s(percent)=       6.09
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.621 min.
Rainfall intensity =      1.680(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.797
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     11.767(CFS)
Total initial stream area =        8.790(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      521.000 to Point/Station      522.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1480.000(Ft.)
End of natural channel elevation =   1449.000(Ft.)
Length of natural channel  =  1024.000(Ft.)
Estimated mean flow rate at midpoint of channel =     22.182(CFS)
```

```
Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   5.36(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0303
Corrected/adjusted channel slope =  0.0303
Travel time =    3.18 min.     TC =   17.80  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.788
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.522(In/Hr) for a    10.0 year storm
Subarea runoff =     18.655(CFS) for     15.560(Ac.)
Total runoff =     30.422(CFS)       Total area =      24.350(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      522.000 to Point/Station      519.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1449.000(Ft.)
End of natural channel elevation =   1386.000(Ft.)
Length of natural channel  =  1283.000(Ft.)
Estimated mean flow rate at midpoint of channel =     37.631(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.91(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0491
Corrected/adjusted channel slope =  0.0491
Travel time =    2.70 min.     TC =   20.51  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.781
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.418(In/Hr) for a    10.0 year storm
Subarea runoff =     12.774(CFS) for     11.540(Ac.)
Total runoff =     43.196(CFS)       Total area =      35.890(Ac.)


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Process from Point/Station      519.000 to Point/Station      519.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     35.890(Ac.)
Runoff from this stream =     43.196(CFS)
Time of concentration =   20.51 min.
Rainfall intensity =     1.418(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                (In/Hr)


1       74.035     22.33                1.359
2       43.196     20.51                1.418
Largest stream flow has longer time of concentration
Qp =     74.035 + sum of
          Qb          Ia/Ib
          43.196 *    0.958 =     41.396
Qp =    115.431
```

```
Total of 2 streams to confluence:
Flow rates before confluence point:
      74.035      43.196
Area of streams before confluence:
       66.120       35.890
Results of confluence:
Total flow rate =    115.431(CFS)
Time of concentration =    22.330 min.
Effective stream area after confluence =    102.010(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      519.000 to Point/Station      523.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1386.000(Ft.)
End of natural channel elevation =   1380.000(Ft.)
Length of natural channel  =   135.000(Ft.)
Estimated mean flow rate at midpoint of channel =    115.713(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  10.46(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0444
Corrected/adjusted channel slope =  0.0444
Travel time =    0.22 min.     TC =   22.55  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.776
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.353(In/Hr) for a    10.0 year storm
Subarea runoff =      0.524(CFS) for      0.500(Ac.)
Total runoff =    115.955(CFS)       Total area =     102.510(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      523.000 to Point/Station      523.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =    102.510(Ac.)
Runoff from this stream =    115.955(CFS)
Time of concentration =   22.55 min.
Rainfall intensity =     1.353(In/Hr)


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Process from Point/Station      524.000 to Point/Station      525.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   590.000(Ft.)
Top (of initial area) elevation =  1430.000(Ft.)
Bottom (of initial area) elevation =  1405.000(Ft.)
Difference in elevation =    25.000(Ft.)
Slope =    0.04237  s(percent)=       4.24
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.800 min.
Rainfall intensity =      1.795(In/Hr) for a    10.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.803
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     12.223(CFS)
Total initial stream area =        8.480(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station      525.000 to Point/Station      526.000
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**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
_____________________________________________________________________
Upstream point/station elevation =  1405.000(Ft.)
Downstream point/station elevation =  1404.000(Ft.)
Pipe length  =    75.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    12.223(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =    12.223(CFS)
Normal flow depth in pipe =   14.88(In.)
Flow top width inside pipe =   13.62(In.)
Critical Depth =   15.88(In.)
Pipe flow velocity =      7.82(Ft/s)
Travel time through pipe =    0.16 min.
Time of concentration (TC) =    12.96 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      526.000 to Point/Station      523.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
_____________________________________________________________________
Top of natural channel elevation =   1404.000(Ft.)
End of natural channel elevation =   1380.000(Ft.)
Length of natural channel  =   502.000(Ft.)
Estimated mean flow rate at midpoint of channel =     17.195(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.29(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0478
Corrected/adjusted channel slope =  0.0478
Travel time =    1.33 min.     TC =   14.29  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.798
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.699(In/Hr) for a    10.0 year storm
Subarea runoff =       9.356(CFS) for      6.900(Ac.)
Total runoff =     21.578(CFS)        Total area =      15.380(Ac.)


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Process from Point/Station      523.000 to Point/Station      523.000
**** CONFLUENCE OF MINOR STREAMS ****
_____________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     15.380(Ac.)
Runoff from this stream =     21.578(CFS)
Time of concentration =   14.29 min.
Rainfall intensity =     1.699(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      115.955     22.55                1.353
2       21.578     14.29                1.699
Largest stream flow has longer time of concentration
Qp =    115.955 + sum of
          Qb         Ia/Ib
          21.578 *    0.796 =     17.179
Qp =    133.134

Total of 2 streams to confluence:
Flow rates before confluence point:
     115.955      21.578
Area of streams before confluence:
      102.510       15.380
Results of confluence:
Total flow rate =    133.134(CFS)
Time of concentration =    22.545 min.
Effective stream area after confluence =    117.890(Ac.)
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Process from Point/Station      523.000 to Point/Station      508.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1380.000(Ft.)
End of natural channel elevation =   1369.000(Ft.)
Length of natural channel  =   547.000(Ft.)
Estimated mean flow rate at midpoint of channel =    135.268(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.37(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0201
Corrected/adjusted channel slope =  0.0201
Travel time =    1.24 min.     TC =   23.78  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.773
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.317(In/Hr) for a    10.0 year storm
Subarea runoff =      3.846(CFS) for      3.780(Ac.)
Total runoff =    136.980(CFS)       Total area =     121.670(Ac.)


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Process from Point/Station      508.000 to Point/Station      508.000
**** CONFLUENCE OF MAIN STREAMS ****
----------------------------------------------------------------------------
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =    121.670(Ac.)
Runoff from this stream =    136.980(CFS)
Time of concentration =   23.78 min.
Rainfall intensity =     1.317(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      199.158     36.25               1.067
2      136.980     23.78               1.317
Largest stream flow has longer time of concentration
Qp =    199.158 + sum of
          Qb         Ia/Ib
         136.980 *    0.810 =    110.952
Qp =    310.110

Total of 2 main streams to confluence:
Flow rates before confluence point:
     199.158     136.980
Area of streams before confluence:
      224.590      121.670


Results of confluence:
Total flow rate =    310.110(CFS)
Time of concentration =    36.248 min.
Effective stream area after confluence  =    346.260(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      508.000 to Point/Station      527.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1369.000(Ft.)
End of natural channel elevation =   1354.000(Ft.)
Length of natural channel  =   336.000(Ft.)
Estimated mean flow rate at midpoint of channel =    316.800(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
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 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  14.31(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0446
Corrected/adjusted channel slope =  0.0446
Travel time =    0.39 min.     TC =   36.64  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.747
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.061(In/Hr) for a    10.0 year storm
Subarea runoff =     11.844(CFS) for     14.940(Ac.)
Total runoff =    321.954(CFS)       Total area =     361.200(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      527.000 to Point/Station      528.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1354.000(Ft.)
End of natural channel elevation =   1286.000(Ft.)
Length of natural channel  =  2132.000(Ft.)
Estimated mean flow rate at midpoint of channel =    348.217(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  12.46(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0319
Corrected/adjusted channel slope =  0.0319
Travel time =    2.85 min.     TC =   39.49  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.725
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.022(In/Hr) for a    10.0 year storm
Subarea runoff =     43.672(CFS) for     58.930(Ac.)
Total runoff =    365.626(CFS)       Total area =     420.130(Ac.)
End of computations, total study area =          420.13 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number =  85.5
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 02/06/24  File:PRO1.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

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Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =  100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity =  1.300(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   744.000(Ft.)
Top (of initial area) elevation =  1388.000(Ft.)
Bottom (of initial area) elevation =  1361.000(Ft.)
Difference in elevation =    27.000(Ft.)
Slope =    0.03629  s(percent)=       3.63
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.659 min.
Rainfall intensity =      3.084(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.827
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =     14.816(CFS)
Total initial stream area =        5.810(Ac.)
Pervious area fraction = 0.500


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Process from Point/Station        2.000 to Point/Station        3.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of street segment elevation =  1361.000(Ft.)
End of street segment elevation =  1344.000(Ft.)
Length of street segment  =   463.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =     15.415(CFS)
Depth of flow =   0.448(Ft.), Average velocity =   5.687(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  16.075(Ft.)
Flow velocity =   5.69(Ft/s)
Travel time =    1.36 min.     TC =   12.02  min.
 Adding area flow to street
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COMMERCIAL subarea type
Runoff Coefficient = 0.885
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      2.905(In/Hr) for a   100.0 year storm
Subarea runoff =      1.208(CFS) for      0.470(Ac.)
Total runoff =     16.024(CFS)        Total area =       6.280(Ac.)
Street flow at end of street =     16.024(CFS)
Half street flow at end of street =     16.024(CFS)
Depth of flow =   0.453(Ft.), Average velocity =   5.740(Ft/s)
Flow width (from curb towards crown)=  16.324(Ft.)


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Process from Point/Station        3.000 to Point/Station        4.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1344.000(Ft.)
Downstream point/station elevation =  1323.000(Ft.)
Pipe length  =   633.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    16.024(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =    16.024(CFS)
Normal flow depth in pipe =   12.61(In.)
Flow top width inside pipe =   16.49(In.)
Critical Depth =   17.10(In.)
Pipe flow velocity =     12.13(Ft/s)
Travel time through pipe =    0.87 min.
Time of concentration (TC) =    12.89 min.


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Process from Point/Station        4.000 to Point/Station        4.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      6.280(Ac.)
Runoff from this stream =     16.024(CFS)
Time of concentration =   12.89 min.
Rainfall intensity =     2.805(In/Hr)


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Process from Point/Station        5.000 to Point/Station        6.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   750.000(Ft.)
Top (of initial area) elevation =  1388.000(Ft.)
Bottom (of initial area) elevation =  1361.000(Ft.)
Difference in elevation =    27.000(Ft.)
Slope =    0.03600  s(percent)=       3.60
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    8.239 min.
Rainfall intensity =      3.508(In/Hr) for a   100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.887
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      2.582(CFS)
Total initial stream area =        0.830(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station        6.000 to Point/Station        7.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1361.000(Ft.)
End of street segment elevation =  1326.000(Ft.)
Length of street segment  =  1128.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
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```
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      3.904(CFS)
Depth of flow =   0.315(Ft.), Average velocity =   3.859(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   9.409(Ft.)
Flow velocity =   3.86(Ft/s)
Travel time =    4.87 min.     TC =   13.11  min.
 Adding area flow to street
COMMERCIAL subarea type
Runoff Coefficient = 0.884
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      2.781(In/Hr) for a   100.0 year storm
Subarea runoff =      2.557(CFS) for      1.040(Ac.)
Total runoff =      5.139(CFS)       Total area =       1.870(Ac.)
Street flow at end of street =      5.139(CFS)
Half street flow at end of street =      5.139(CFS)
Depth of flow =   0.339(Ft.), Average velocity =   4.108(Ft/s)
Flow width (from curb towards crown)=  10.603(Ft.)


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Process from Point/Station        7.000 to Point/Station        4.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1326.000(Ft.)
Downstream point/station elevation =  1323.000(Ft.)
Pipe length  =    30.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     5.139(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     5.139(CFS)
Normal flow depth in pipe =    7.24(In.)
Flow top width inside pipe =    7.14(In.)
Critical depth could not be calculated.
Pipe flow velocity =     13.50(Ft/s)
Travel time through pipe =    0.04 min.
Time of concentration (TC) =    13.15 min.


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Process from Point/Station        4.000 to Point/Station        4.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      1.870(Ac.)
Runoff from this stream =      5.139(CFS)
Time of concentration =   13.15 min.
Rainfall intensity =     2.777(In/Hr)


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Process from Point/Station        8.000 to Point/Station        9.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =  1000.000(Ft.)
Top (of initial area) elevation =  1358.000(Ft.)
Bottom (of initial area) elevation =  1326.000(Ft.)
Difference in elevation =    32.000(Ft.)
Slope =    0.03200  s(percent)=       3.20
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.304 min.
Rainfall intensity =      2.871(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.822
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =     17.634(CFS)
Total initial stream area =        7.470(Ac.)
Pervious area fraction = 0.500


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Process from Point/Station        9.000 to Point/Station        4.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
```

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Upstream point/station elevation =  1326.000(Ft.)
Downstream point/station elevation =  1323.000(Ft.)
Pipe length  =    36.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    17.634(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =    17.634(CFS)
Normal flow depth in pipe =   11.63(In.)
Flow top width inside pipe =   12.53(In.)
Critical depth could not be calculated.
Pipe flow velocity =     17.29(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    12.34 min.


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Process from Point/Station        4.000 to Point/Station        4.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 3
Stream flow area =      7.470(Ac.)
Runoff from this stream =     17.634(CFS)
Time of concentration =   12.34 min.
Rainfall intensity =     2.867(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       16.024     12.89                 2.805
2        5.139     13.15                 2.777
3       17.634     12.34                 2.867
Largest stream flow has longer or shorter time of concentration
Qp =     17.634 + sum of
          Qa           Tb/Ta
          16.024 *    0.957 =     15.342
          Qa           Tb/Ta
           5.139 *    0.938 =      4.823
Qp =     37.799

Total of 3 streams to confluence:
Flow rates before confluence point:
      16.024       5.139      17.634
Area of streams before confluence:
       6.280       1.870       7.470
Results of confluence:
Total flow rate =     37.799(CFS)
Time of concentration =    12.338 min.
Effective stream area after confluence =     15.620(Ac.)


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Process from Point/Station        4.000 to Point/Station       10.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1323.000(Ft.)
Downstream point/station elevation =  1310.500(Ft.)
Pipe length  =    38.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    37.799(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =    37.799(CFS)
Normal flow depth in pipe =   10.34(In.)
Flow top width inside pipe =   17.80(In.)
Critical depth could not be calculated.
Pipe flow velocity =     36.01(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =    12.36 min.


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Process from Point/Station       10.000 to Point/Station       10.000
**** CONFLUENCE OF MAIN STREAMS ****
------------------------------------------------------------------------------
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     15.620(Ac.)
Runoff from this stream =     37.799(CFS)
Time of concentration =   12.36 min.
Rainfall intensity =     2.865(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station       11.000 to Point/Station       12.000
**** INITIAL AREA EVALUATION ****
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```
Initial area flow distance =   610.000(Ft.)
Top (of initial area) elevation =  1369.000(Ft.)
Bottom (of initial area) elevation =  1351.300(Ft.)
Difference in elevation =    17.700(Ft.)
Slope =    0.02902  s(percent)=       2.90
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.920 min.
Rainfall intensity =      3.578(In/Hr) for a   100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.887
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      1.333(CFS)
Total initial stream area =        0.420(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station       12.000 to Point/Station       13.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of street segment elevation =  1351.300(Ft.)
End of street segment elevation =  1316.400(Ft.)
Length of street segment  =   573.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      2.190(CFS)
Depth of flow =   0.247(Ft.), Average velocity =   4.464(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   6.032(Ft.)
Flow velocity =   4.46(Ft/s)
Travel time =    2.14 min.     TC =   10.06  min.
 Adding area flow to street
COMMERCIAL subarea type
Runoff Coefficient = 0.886
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      3.175(In/Hr) for a   100.0 year storm
Subarea runoff =      1.659(CFS) for      0.590(Ac.)
Total runoff =      2.992(CFS)        Total area =       1.010(Ac.)
Street flow at end of street =      2.992(CFS)
Half street flow at end of street =      2.992(CFS)
Depth of flow =   0.269(Ft.), Average velocity =   4.745(Ft/s)
Flow width (from curb towards crown)=   7.099(Ft.)


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Process from Point/Station       13.000 to Point/Station       14.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1316.400(Ft.)
Downstream point/station elevation =  1312.000(Ft.)
Pipe length  =    36.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.992(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     2.992(CFS)
Normal flow depth in pipe =    4.59(In.)
Flow top width inside pipe =    9.00(In.)
Critical depth could not be calculated.
Pipe flow velocity =     13.21(Ft/s)
Travel time through pipe =    0.05 min.
Time of concentration (TC) =    10.10 min.


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Process from Point/Station       14.000 to Point/Station       14.000
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**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      1.010(Ac.)
Runoff from this stream =      2.992(CFS)
Time of concentration =   10.10 min.
Rainfall intensity =     3.168(In/Hr)


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Process from Point/Station       15.000 to Point/Station       16.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------
Initial area flow distance =   583.000(Ft.)
Top (of initial area) elevation =  1369.000(Ft.)
Bottom (of initial area) elevation =  1351.300(Ft.)
Difference in elevation =    17.700(Ft.)
Slope =    0.03036  s(percent)=       3.04
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.708 min.
Rainfall intensity =      3.627(In/Hr) for a   100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.887
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      1.287(CFS)
Total initial stream area =        0.400(Ac.)
Pervious area fraction = 0.100


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Process from Point/Station       16.000 to Point/Station       17.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Top of street segment elevation =  1351.300(Ft.)
End of street segment elevation =  1316.400(Ft.)
Length of street segment  =   600.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      2.134(CFS)
Depth of flow =   0.247(Ft.), Average velocity =   4.360(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   6.023(Ft.)
Flow velocity =   4.36(Ft/s)
Travel time =    2.29 min.     TC =   10.00  min.
 Adding area flow to street
COMMERCIAL subarea type
Runoff Coefficient = 0.886
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      3.184(In/Hr) for a   100.0 year storm
Subarea runoff =      1.636(CFS) for      0.580(Ac.)
Total runoff =      2.923(CFS)       Total area =       0.980(Ac.)
Street flow at end of street =      2.923(CFS)
Half street flow at end of street =      2.923(CFS)
Depth of flow =   0.269(Ft.), Average velocity =   4.637(Ft/s)
Flow width (from curb towards crown)=   7.098(Ft.)


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Process from Point/Station       17.000 to Point/Station       14.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------
Upstream point/station elevation =  1316.400(Ft.)
Downstream point/station elevation =  1312.000(Ft.)
Pipe length  =    39.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     2.923(CFS)
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Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     2.923(CFS)
Normal flow depth in pipe =    4.64(In.)
Flow top width inside pipe =    9.00(In.)
Critical depth could not be calculated.
Pipe flow velocity =     12.74(Ft/s)
Travel time through pipe =    0.05 min.
Time of concentration (TC) =    10.05 min.


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Process from Point/Station       14.000 to Point/Station       14.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      0.980(Ac.)
Runoff from this stream =      2.923(CFS)
Time of concentration =   10.05 min.
Rainfall intensity =     3.176(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        2.992     10.10                3.168
2        2.923     10.05                3.176
Largest stream flow has longer time of concentration
Qp =      2.992 + sum of
          Qb         Ia/Ib
           2.923 *    0.997 =      2.915
Qp =      5.908

Total of 2 streams to confluence:
Flow rates before confluence point:
      2.992       2.923
Area of streams before confluence:
       1.010        0.980
Results of confluence:
Total flow rate =      5.908(CFS)
Time of concentration =    10.105 min.
Effective stream area after confluence =      1.990(Ac.)


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Process from Point/Station       14.000 to Point/Station       10.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1312.000(Ft.)
Downstream point/station elevation =  1310.500(Ft.)
Pipe length  =   227.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     5.908(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =     5.908(CFS)
Normal flow depth in pipe =   11.02(In.)
Flow top width inside pipe =   17.54(In.)
Critical Depth =   11.26(In.)
Pipe flow velocity =      5.22(Ft/s)
Travel time through pipe =    0.73 min.
Time of concentration (TC) =    10.83 min.


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Process from Point/Station       10.000 to Point/Station       10.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      1.990(Ac.)
Runoff from this stream =      5.908(CFS)
Time of concentration =   10.83 min.
Rainfall intensity =     3.060(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       37.799     12.36                2.865
2        5.908     10.83                3.060
Largest stream flow has longer time of concentration
Qp =     37.799 + sum of
          Qb         Ia/Ib
           5.908 *    0.936 =      5.531
Qp =     43.330
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```
Total of 2 main streams to confluence:
Flow rates before confluence point:
      37.799       5.908
Area of streams before confluence:
       15.620        1.990


Results of confluence:
Total flow rate =     43.330(CFS)
Time of concentration =    12.356 min.
Effective stream area after confluence  =     17.610(Ac.)


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Process from Point/Station       10.000 to Point/Station       18.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1310.500(Ft.)
Downstream point/station elevation =  1310.000(Ft.)
Pipe length  =   107.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    43.330(CFS)
Nearest computed pipe diameter  =     36.00(In.)
Calculated individual pipe flow  =    43.330(CFS)
Normal flow depth in pipe =   28.03(In.)
Flow top width inside pipe =   29.89(In.)
Critical Depth =   25.73(In.)
Pipe flow velocity =      7.34(Ft/s)
Travel time through pipe =    0.24 min.
Time of concentration (TC) =    12.60 min.


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Process from Point/Station       18.000 to Point/Station       18.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     17.610(Ac.)
Runoff from this stream =     43.330(CFS)
Time of concentration =   12.60 min.
Rainfall intensity =     2.837(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station       19.000 to Point/Station       20.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   501.000(Ft.)
Top (of initial area) elevation =  1386.000(Ft.)
Bottom (of initial area) elevation =  1341.000(Ft.)
Difference in elevation =    45.000(Ft.)
Slope =    0.08982  s(percent)=       8.98
TC = k(0.940)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   18.297 min.
Rainfall intensity =      2.354(In/Hr) for a   100.0 year storm
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.751
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  74.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      3.092(CFS)
Total initial stream area =        1.750(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station       20.000 to Point/Station       21.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1341.000(Ft.)
End of street segment elevation =  1321.500(Ft.)
Length of street segment  =  1029.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
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 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      6.776(CFS)
Depth of flow =   0.390(Ft.), Average velocity =   3.630(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  13.190(Ft.)
Flow velocity =   3.63(Ft/s)
Travel time =    4.72 min.     TC =   23.02  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.800
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      2.099(In/Hr) for a   100.0 year storm
Subarea runoff =      7.271(CFS) for      4.330(Ac.)
Total runoff =     10.363(CFS)       Total area =       6.080(Ac.)
Street flow at end of street =     10.363(CFS)
Half street flow at end of street =     10.363(CFS)
Depth of flow =   0.440(Ft.), Average velocity =   4.020(Ft/s)
Flow width (from curb towards crown)=  15.656(Ft.)


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Process from Point/Station       21.000 to Point/Station       22.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1321.500(Ft.)
Downstream point/station elevation =  1321.000(Ft.)
Pipe length  =    37.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    10.363(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =    10.363(CFS)
Normal flow depth in pipe =   12.73(In.)
Flow top width inside pipe =   16.38(In.)
Critical Depth =   14.86(In.)
Pipe flow velocity =      7.75(Ft/s)
Travel time through pipe =    0.08 min.
Time of concentration (TC) =    23.10 min.


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Process from Point/Station       22.000 to Point/Station       22.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      6.080(Ac.)
Runoff from this stream =     10.363(CFS)
Time of concentration =   23.10 min.
Rainfall intensity =     2.095(In/Hr)


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Process from Point/Station       23.000 to Point/Station       24.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   274.000(Ft.)
Top (of initial area) elevation =  1360.800(Ft.)
Bottom (of initial area) elevation =  1341.000(Ft.)
Difference in elevation =    19.800(Ft.)
Slope =    0.07226  s(percent)=       7.23
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    6.228 min.
Rainfall intensity =      4.035(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.842
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      1.596(CFS)
Total initial stream area =        0.470(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       24.000 to Point/Station       25.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1341.000(Ft.)
```

```
End of street segment elevation =  1327.000(Ft.)
Length of street segment  =  1079.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      2.723(CFS)
Depth of flow =   0.321(Ft.), Average velocity =   2.538(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   9.727(Ft.)
Flow velocity =   2.54(Ft/s)
Travel time =    7.09 min.     TC =   13.31  min.
 Adding area flow to street
COMMERCIAL subarea type
Runoff Coefficient = 0.884
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Rainfall intensity =      2.760(In/Hr) for a   100.0 year storm
Subarea runoff =      2.196(CFS) for      0.900(Ac.)
Total runoff =      3.792(CFS)       Total area =       1.370(Ac.)
Street flow at end of street =      3.792(CFS)
Half street flow at end of street =      3.792(CFS)
Depth of flow =   0.351(Ft.), Average velocity =   2.739(Ft/s)
Flow width (from curb towards crown)=  11.214(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       25.000 to Point/Station       22.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1327.000(Ft.)
Downstream point/station elevation =  1321.000(Ft.)
Pipe length  =    36.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     3.792(CFS)
Nearest computed pipe diameter  =      9.00(In.)
Calculated individual pipe flow  =     3.792(CFS)
Normal flow depth in pipe =    4.82(In.)
Flow top width inside pipe =    8.98(In.)
Critical depth could not be calculated.
Pipe flow velocity =     15.73(Ft/s)
Travel time through pipe =    0.04 min.
Time of concentration (TC) =    13.35 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station       22.000 to Point/Station       22.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      1.370(Ac.)
Runoff from this stream =      3.792(CFS)
Time of concentration =   13.35 min.
Rainfall intensity =     2.756(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       10.363     23.10                 2.095
2        3.792     13.35                 2.756
Largest stream flow has longer time of concentration
Qp =     10.363 + sum of
          Qb         Ia/Ib
           3.792 *    0.760 =      2.883
Qp =     13.246

Total of 2 streams to confluence:
Flow rates before confluence point:
      10.363       3.792
Area of streams before confluence:
        6.080        1.370
Results of confluence:
```

```
Total flow rate =     13.246(CFS)
Time of concentration =    23.101 min.
Effective stream area after confluence =      7.450(Ac.)


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Process from Point/Station       22.000 to Point/Station       18.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
----------------------------------------------------------------------------
Upstream point/station elevation =  1321.000(Ft.)
Downstream point/station elevation =  1310.000(Ft.)
Pipe length  =    40.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    13.246(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =    13.246(CFS)
Normal flow depth in pipe =    7.46(In.)
Flow top width inside pipe =   11.64(In.)
Critical depth could not be calculated.
Pipe flow velocity =     25.81(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    23.13 min.


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Process from Point/Station       18.000 to Point/Station       18.000
**** CONFLUENCE OF MAIN STREAMS ****
----------------------------------------------------------------------------
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =      7.450(Ac.)
Runoff from this stream =     13.246(CFS)
Time of concentration =   23.13 min.
Rainfall intensity =     2.094(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       43.330     12.60               2.837
2       13.246     23.13               2.094
Largest stream flow has longer or shorter time of concentration
Qp =     43.330 + sum of
          Qa          Tb/Ta
          13.246 *    0.545 =      7.216
Qp =     50.546

Total of 2 main streams to confluence:
Flow rates before confluence point:
      43.330      13.246
Area of streams before confluence:
       17.610        7.450


Results of confluence:
Total flow rate =     50.546(CFS)
Time of concentration =    12.599 min.
Effective stream area after confluence  =     25.060(Ac.)


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Process from Point/Station       18.000 to Point/Station       26.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
----------------------------------------------------------------------------
Upstream point/station elevation =  1310.000(Ft.)
Downstream point/station elevation =  1308.200(Ft.)
Pipe length  =   140.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    50.546(CFS)
Nearest computed pipe diameter  =     33.00(In.)
Calculated individual pipe flow  =    50.546(CFS)
Normal flow depth in pipe =   23.20(In.)
Flow top width inside pipe =   30.15(In.)
Critical Depth =   28.05(In.)
Pipe flow velocity =     11.32(Ft/s)
Travel time through pipe =    0.21 min.
Time of concentration (TC) =    12.81 min.


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Process from Point/Station       26.000 to Point/Station       27.000
**** SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.772
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
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Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  74.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    12.81 min.
Rainfall intensity =      2.814(In/Hr) for a   100.0 year storm
Subarea runoff =      3.648(CFS) for      1.680(Ac.)
Total runoff =     54.194(CFS)       Total area =      26.740(Ac.)
End of computations, total study area =           26.74 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.486
Area averaged RI index number =  69.6
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 02/06/24  File:PRO2.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

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Program License Serial Number 5006

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Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =  100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity =  1.300(In/Hr)
Slope of intensity duration curve = 0.5000




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Process from Point/Station      100.000 to Point/Station      101.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =  1000.000(Ft.)
Top (of initial area) elevation =  1423.000(Ft.)
Bottom (of initial area) elevation =  1370.000(Ft.)
Difference in elevation =    53.000(Ft.)
Slope =    0.05300  s(percent)=       5.30
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   11.123 min.
Rainfall intensity =      3.019(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.826
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =     14.357(CFS)
Total initial stream area =        5.760(Ac.)
Pervious area fraction = 0.500


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Process from Point/Station      101.000 to Point/Station      101.100
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of street segment elevation =  1370.000(Ft.)
End of street segment elevation =  1362.000(Ft.)
Length of street segment  =   649.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =     21.503(CFS)
Depth of flow =   0.579(Ft.), Average velocity =   4.141(Ft/s)
Warning: depth of flow exceeds top of curb
Note:  depth of flow exceeds top of street crown.
Distance that curb overflow reaches into property =    3.97(Ft.)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  18.000(Ft.)
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Flow velocity =   4.14(Ft/s)
Travel time =    2.61 min.     TC =   13.73  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.819
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      2.717(In/Hr) for a   100.0 year storm
Subarea runoff =     14.237(CFS) for      6.400(Ac.)
Total runoff =     28.594(CFS)        Total area =      12.160(Ac.)
Street flow at end of street =     28.594(CFS)
Half street flow at end of street =     28.594(CFS)
Depth of flow =   0.633(Ft.), Average velocity =   4.436(Ft/s)
Warning: depth of flow exceeds top of curb
Note:  depth of flow exceeds top of street crown.
Distance that curb overflow reaches into property =    6.66(Ft.)
Flow width (from curb towards crown)=  18.000(Ft.)


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Process from Point/Station      101.100 to Point/Station      101.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1362.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =    50.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    28.594(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =    28.594(CFS)
Normal flow depth in pipe =   11.39(In.)
Flow top width inside pipe =   17.35(In.)
Critical depth could not be calculated.
Pipe flow velocity =     24.26(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    13.77 min.


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Process from Point/Station      101.200 to Point/Station      101.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     12.160(Ac.)
Runoff from this stream =     28.594(CFS)
Time of concentration =   13.77 min.
Rainfall intensity =     2.714(In/Hr)


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Process from Point/Station        1.000 to Point/Station      101.300
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   980.000(Ft.)
Top (of initial area) elevation =  1388.000(Ft.)
Bottom (of initial area) elevation =  1370.000(Ft.)
Difference in elevation =    18.000(Ft.)
Slope =    0.01837  s(percent)=       1.84
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.638 min.
Rainfall intensity =      2.727(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.819
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      7.414(CFS)
Total initial stream area =        3.320(Ac.)
Pervious area fraction = 0.500


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Process from Point/Station      101.300 to Point/Station      101.400
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of street segment elevation =  1370.000(Ft.)
End of street segment elevation =  1362.000(Ft.)
Length of street segment  =   617.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
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Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      9.589(CFS)
Depth of flow =   0.454(Ft.), Average velocity =   3.417(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  16.370(Ft.)
Flow velocity =   3.42(Ft/s)
Travel time =    3.01 min.     TC =   16.65  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.812
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      2.468(In/Hr) for a   100.0 year storm
Subarea runoff =      4.289(CFS) for      2.140(Ac.)
Total runoff =     11.703(CFS)       Total area =       5.460(Ac.)
Street flow at end of street =     11.703(CFS)
Half street flow at end of street =     11.703(CFS)
Depth of flow =   0.481(Ft.), Average velocity =   3.587(Ft/s)
Flow width (from curb towards crown)=  17.710(Ft.)


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Process from Point/Station      101.400 to Point/Station      101.200
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1362.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =    34.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    11.703(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =    11.703(CFS)
Normal flow depth in pipe =    7.57(In.)
Flow top width inside pipe =   11.58(In.)
Critical depth could not be calculated.
Pipe flow velocity =     22.43(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    16.67 min.


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Process from Point/Station      101.200 to Point/Station      101.200
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      5.460(Ac.)
Runoff from this stream =     11.703(CFS)
Time of concentration =   16.67 min.
Rainfall intensity =     2.466(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       28.594     13.77                 2.714
2       11.703     16.67                 2.466
Largest stream flow has longer or shorter time of concentration
Qp =     28.594 + sum of
          Qa          Tb/Ta
          11.703 *    0.826 =      9.665
Qp =     38.259

Total of 2 streams to confluence:
Flow rates before confluence point:
      28.594      11.703
Area of streams before confluence:
       12.160        5.460
Results of confluence:
Total flow rate =     38.259(CFS)
Time of concentration =    13.769 min.
Effective stream area after confluence =     17.620(Ac.)
```

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Process from Point/Station      101.200 to Point/Station      103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1355.000(Ft.)
Downstream point/station elevation =  1329.000(Ft.)
Pipe length  =   757.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    38.259(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    38.259(CFS)
Normal flow depth in pipe =   18.00(In.)
Flow top width inside pipe =   20.78(In.)
Critical depth could not be calculated.
Pipe flow velocity =     15.13(Ft/s)
Travel time through pipe =    0.83 min.
Time of concentration (TC) =    14.60 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     17.620(Ac.)
Runoff from this stream =     38.259(CFS)
Time of concentration =   14.60 min.
Rainfall intensity =     2.635(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      101.600 to Point/Station      101.700
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   915.000(Ft.)
Top (of initial area) elevation =  1434.400(Ft.)
Bottom (of initial area) elevation =  1365.000(Ft.)
Difference in elevation =    69.400(Ft.)
Slope =    0.07585  s(percent)=       7.58
TC = k(0.480)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.298 min.
Rainfall intensity =      2.871(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1 Acre Lot)
Runoff Coefficient = 0.776
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.800; Impervious fraction =  0.200
Initial subarea runoff =      9.600(CFS)
Total initial stream area =        4.310(Ac.)
Pervious area fraction = 0.800


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Process from Point/Station      101.700 to Point/Station      102.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of street segment elevation =  1365.000(Ft.)
End of street segment elevation =  1357.000(Ft.)
Length of street segment  =   493.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =     11.048(CFS)
Depth of flow =   0.458(Ft.), Average velocity =   3.850(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  16.562(Ft.)
Flow velocity =   3.85(Ft/s)
Travel time =    2.13 min.     TC =   14.43  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.817
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
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Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      2.651(In/Hr) for a   100.0 year storm
Subarea runoff =      2.815(CFS) for      1.300(Ac.)
Total runoff =     12.416(CFS)       Total area =       5.610(Ac.)
Street flow at end of street =     12.416(CFS)
Half street flow at end of street =     12.416(CFS)
Depth of flow =   0.474(Ft.), Average velocity =   3.961(Ft/s)
Flow width (from curb towards crown)=  17.344(Ft.)


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Process from Point/Station      102.000 to Point/Station      104.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of street segment elevation =  1357.000(Ft.)
End of street segment elevation =  1336.000(Ft.)
Length of street segment  =   411.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =     18.452(CFS)
Depth of flow =   0.450(Ft.), Average velocity =   6.732(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  16.169(Ft.)
Flow velocity =   6.73(Ft/s)
Travel time =    1.02 min.     TC =   15.45  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.815
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      2.562(In/Hr) for a   100.0 year storm
Subarea runoff =     11.981(CFS) for      5.740(Ac.)
Total runoff =     24.397(CFS)       Total area =      11.350(Ac.)
Street flow at end of street =     24.397(CFS)
Half street flow at end of street =     24.397(CFS)
Depth of flow =   0.488(Ft.), Average velocity =   7.214(Ft/s)
Note:  depth of flow exceeds top of street crown.
Flow width (from curb towards crown)=  18.000(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      104.000 to Point/Station      103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1336.000(Ft.)
Downstream point/station elevation =  1329.000(Ft.)
Pipe length  =    23.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    24.397(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =    24.397(CFS)
Normal flow depth in pipe =    9.12(In.)
Flow top width inside pipe =   14.65(In.)
Critical depth could not be calculated.
Pipe flow velocity =     31.28(Ft/s)
Travel time through pipe =    0.01 min.
Time of concentration (TC) =    15.46 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     11.350(Ac.)
Runoff from this stream =     24.397(CFS)
Time of concentration =   15.46 min.
Rainfall intensity =     2.561(In/Hr)
```

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++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      105.000 to Point/Station      106.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   737.000(Ft.)
Top (of initial area) elevation =  1410.000(Ft.)
Bottom (of initial area) elevation =  1363.000(Ft.)
Difference in elevation =    47.000(Ft.)
Slope =    0.06377  s(percent)=       6.38
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    7.298 min.
Rainfall intensity =      3.728(In/Hr) for a   100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.888
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      2.150(CFS)
Total initial stream area =        0.650(Ac.)
Pervious area fraction = 0.100


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      106.000 to Point/Station      107.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of street segment elevation =  1363.000(Ft.)
End of street segment elevation =  1357.000(Ft.)
Length of street segment  =   576.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      4.367(CFS)
Depth of flow =   0.376(Ft.), Average velocity =   2.603(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  12.453(Ft.)
Flow velocity =   2.60(Ft/s)
Travel time =    3.69 min.     TC =   10.99  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.826
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      3.038(In/Hr) for a   100.0 year storm
Subarea runoff =      4.341(CFS) for      1.730(Ac.)
Total runoff =      6.491(CFS)       Total area =       2.380(Ac.)
Street flow at end of street =      6.491(CFS)
Half street flow at end of street =      6.491(CFS)
Depth of flow =   0.419(Ft.), Average velocity =   2.862(Ft/s)
Flow width (from curb towards crown)=  14.634(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      107.000 to Point/Station      108.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of street segment elevation =  1357.000(Ft.)
End of street segment elevation =  1336.000(Ft.)
Length of street segment  =   409.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
```

```
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      7.952(CFS)
Depth of flow =   0.356(Ft.), Average velocity =   5.517(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  11.466(Ft.)
Flow velocity =   5.52(Ft/s)
Travel time =    1.24 min.     TC =   12.22  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.823
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      2.881(In/Hr) for a   100.0 year storm
Subarea runoff =      2.867(CFS) for      1.210(Ac.)
Total runoff =      9.358(CFS)       Total area =       3.590(Ac.)
Street flow at end of street =      9.358(CFS)
Half street flow at end of street =      9.358(CFS)
Depth of flow =   0.372(Ft.), Average velocity =   5.732(Ft/s)
Flow width (from curb towards crown)=  12.272(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      108.000 to Point/Station      103.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1336.000(Ft.)
Downstream point/station elevation =  1329.000(Ft.)
Pipe length  =    24.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     9.358(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =     9.358(CFS)
Normal flow depth in pipe =    5.91(In.)
Flow top width inside pipe =   12.00(In.)
Critical depth could not be calculated.
Pipe flow velocity =     24.33(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =    12.24 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      103.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 3
Stream flow area =      3.590(Ac.)
Runoff from this stream =      9.358(CFS)
Time of concentration =   12.24 min.
Rainfall intensity =     2.879(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       38.259     14.60                 2.635
2       24.397     15.46                 2.561
3        9.358     12.24                 2.879
Largest stream flow has longer or shorter time of concentration
Qp =     38.259 + sum of
          Qa          Tb/Ta
          24.397 *    0.944 =     23.042
          Qb         Ia/Ib
           9.358 *    0.915 =      8.567
Qp =     69.868

Total of 3 streams to confluence:
Flow rates before confluence point:
      38.259      24.397       9.358
Area of streams before confluence:
       17.620       11.350        3.590
Results of confluence:
Total flow rate =     69.868(CFS)
Time of concentration =    14.603 min.
Effective stream area after confluence =     32.560(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      103.000 to Point/Station      109.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
```

```
Upstream point/station elevation =  1329.000(Ft.)
Downstream point/station elevation =  1309.000(Ft.)
Pipe length  =   655.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    69.868(CFS)
Nearest computed pipe diameter  =     30.00(In.)
Calculated individual pipe flow  =    69.868(CFS)
Normal flow depth in pipe =   23.95(In.)
Flow top width inside pipe =   24.07(In.)
Critical depth could not be calculated.
Pipe flow velocity =     16.64(Ft/s)
Travel time through pipe =    0.66 min.
Time of concentration (TC) =    15.26 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      109.000 to Point/Station      109.000
**** CONFLUENCE OF MAIN STREAMS ****
------------------------------------------------------------------------------
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     32.560(Ac.)
Runoff from this stream =     69.868(CFS)
Time of concentration =   15.26 min.
Rainfall intensity =     2.578(In/Hr)
Program is now starting with Main Stream No. 2


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Process from Point/Station      110.000 to Point/Station      111.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   707.000(Ft.)
Top (of initial area) elevation =  1360.800(Ft.)
Bottom (of initial area) elevation =  1336.000(Ft.)
Difference in elevation =    24.800(Ft.)
Slope =    0.03508  s(percent)=       3.51
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.515 min.
Rainfall intensity =      3.105(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.827
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =     14.925(CFS)
Total initial stream area =        5.810(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      111.000 to Point/Station      112.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------------
Top of street segment elevation =  1336.000(Ft.)
End of street segment elevation =  1315.000(Ft.)
Length of street segment  =   675.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [1] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =     18.344(CFS)
Depth of flow =   0.483(Ft.), Average velocity =   5.572(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =  17.792(Ft.)
Flow velocity =   5.57(Ft/s)
Travel time =    2.02 min.     TC =   12.53  min.
 Adding area flow to street
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.822
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
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RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      2.844(In/Hr) for a   100.0 year storm
Subarea runoff =      6.754(CFS) for      2.890(Ac.)
Total runoff =     21.679(CFS)        Total area =       8.700(Ac.)
Street flow at end of street =     21.679(CFS)
Half street flow at end of street =     21.679(CFS)
Depth of flow =   0.504(Ft.), Average velocity =   5.905(Ft/s)
Warning: depth of flow exceeds top of curb
Note:  depth of flow exceeds top of street crown.
Distance that curb overflow reaches into property =    0.18(Ft.)
Flow width (from curb towards crown)=  18.000(Ft.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      112.000 to Point/Station      112.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =      8.700(Ac.)
Runoff from this stream =     21.679(CFS)
Time of concentration =   12.53 min.
Rainfall intensity =     2.844(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      113.000 to Point/Station      112.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   806.000(Ft.)
Top (of initial area) elevation =  1326.500(Ft.)
Bottom (of initial area) elevation =  1315.000(Ft.)
Difference in elevation =    11.500(Ft.)
Slope =    0.01427  s(percent)=       1.43
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.266 min.
Rainfall intensity =      2.765(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.820
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      7.208(CFS)
Total initial stream area =        3.180(Ac.)
Pervious area fraction = 0.500


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Process from Point/Station      112.000 to Point/Station      112.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =      3.180(Ac.)
Runoff from this stream =      7.208(CFS)
Time of concentration =   13.27 min.
Rainfall intensity =     2.765(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       21.679     12.53                 2.844
2        7.208     13.27                 2.765
Largest stream flow has longer or shorter time of concentration
Qp =     21.679 + sum of
          Qa          Tb/Ta
           7.208 *    0.945 =      6.811
Qp =     28.490

Total of 2 streams to confluence:
Flow rates before confluence point:
      21.679       7.208
Area of streams before confluence:
       8.700       3.180
Results of confluence:
Total flow rate =     28.490(CFS)
Time of concentration =    12.535 min.
Effective stream area after confluence =     11.880(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      112.000 to Point/Station      109.000
```

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**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
_____________________________________________________________________
Upstream point/station elevation =  1315.000(Ft.)
Downstream point/station elevation =  1309.000(Ft.)
Pipe length  =    30.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    28.490(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =    28.490(CFS)
Normal flow depth in pipe =   12.12(In.)
Flow top width inside pipe =   11.82(In.)
Critical depth could not be calculated.
Pipe flow velocity =     26.84(Ft/s)
Travel time through pipe =    0.02 min.
Time of concentration (TC) =    12.55 min.


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Process from Point/Station      109.000 to Point/Station      109.000
**** CONFLUENCE OF MAIN STREAMS ****
_____________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =     11.880(Ac.)
Runoff from this stream =     28.490(CFS)
Time of concentration =   12.55 min.
Rainfall intensity =     2.842(In/Hr)
Program is now starting with Main Stream No. 3


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Process from Point/Station      108.000 to Point/Station      115.000
**** INITIAL AREA EVALUATION ****
_____________________________________________________________________
Initial area flow distance =   703.000(Ft.)
Top (of initial area) elevation =  1336.000(Ft.)
Bottom (of initial area) elevation =  1315.000(Ft.)
Difference in elevation =    21.000(Ft.)
Slope =    0.02987  s(percent)=       2.99
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.834 min.
Rainfall intensity =      3.059(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.826
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      5.865(CFS)
Total initial stream area =        2.320(Ac.)
Pervious area fraction = 0.500


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Process from Point/Station      115.000 to Point/Station      115.000
**** CONFLUENCE OF MINOR STREAMS ****
_____________________________________________________________________
Along Main Stream number: 3 in normal stream number 1
Stream flow area =      2.320(Ac.)
Runoff from this stream =      5.865(CFS)
Time of concentration =   10.83 min.
Rainfall intensity =     3.059(In/Hr)


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Process from Point/Station      114.000 to Point/Station      115.000
**** INITIAL AREA EVALUATION ****
_____________________________________________________________________
Initial area flow distance =   800.000(Ft.)
Top (of initial area) elevation =  1326.500(Ft.)
Bottom (of initial area) elevation =  1315.000(Ft.)
Difference in elevation =    11.500(Ft.)
Slope =    0.01438  s(percent)=       1.44
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.206 min.
Rainfall intensity =      2.771(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.820
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =      8.248(CFS)
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Total initial stream area =        3.630(Ac.)
Pervious area fraction = 0.500


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Process from Point/Station      115.000 to Point/Station      115.000
**** CONFLUENCE OF MINOR STREAMS ****
----------------------------------------------------------------------------
Along Main Stream number: 3 in normal stream number 2
Stream flow area =      3.630(Ac.)
Runoff from this stream =       8.248(CFS)
Time of concentration =   13.21 min.
Rainfall intensity =     2.771(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        5.865     10.83                 3.059
2        8.248     13.21                 2.771
Largest stream flow has longer time of concentration
Qp =      8.248 + sum of
          Qb          Ia/Ib
           5.865 *    0.906 =      5.312
Qp =     13.560

Total of 2 streams to confluence:
Flow rates before confluence point:
       5.865       8.248
Area of streams before confluence:
        2.320        3.630
Results of confluence:
Total flow rate =     13.560(CFS)
Time of concentration =    13.206 min.
Effective stream area after confluence =      5.950(Ac.)


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Process from Point/Station      115.000 to Point/Station      109.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
----------------------------------------------------------------------------
Upstream point/station elevation =  1315.000(Ft.)
Downstream point/station elevation =  1309.000(Ft.)
Pipe length  =    21.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    13.560(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =    13.560(CFS)
Normal flow depth in pipe =    7.48(In.)
Flow top width inside pipe =   11.63(In.)
Critical depth could not be calculated.
Pipe flow velocity =     26.33(Ft/s)
Travel time through pipe =    0.01 min.
Time of concentration (TC) =    13.22 min.


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Process from Point/Station      109.000 to Point/Station      109.000
**** CONFLUENCE OF MAIN STREAMS ****
----------------------------------------------------------------------------
The following data inside Main Stream is listed:
In Main Stream number: 3
Stream flow area =      5.950(Ac.)
Runoff from this stream =     13.560(CFS)
Time of concentration =   13.22 min.
Rainfall intensity =     2.770(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       69.868     15.26                 2.578
2       28.490     12.55                 2.842
3       13.560     13.22                 2.770
Largest stream flow has longer time of concentration
Qp =     69.868 + sum of
          Qb          Ia/Ib
          28.490 *    0.907 =     25.841
          Qb          Ia/Ib
          13.560 *    0.931 =     12.621
Qp =    108.330

Total of 3 main streams to confluence:
Flow rates before confluence point:
      69.868      28.490      13.560
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Area of streams before confluence:
       32.560       11.880        5.950


Results of confluence:
Total flow rate =    108.330(CFS)
Time of concentration =    15.259 min.
Effective stream area after confluence  =     50.390(Ac.)


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Process from Point/Station      109.000 to Point/Station      116.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
________________________________________________________________________
Upstream point/station elevation =  1309.000(Ft.)
Downstream point/station elevation =  1293.000(Ft.)
Pipe length  =   317.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =   108.330(CFS)
Nearest computed pipe diameter  =     33.00(In.)
Calculated individual pipe flow  =   108.330(CFS)
Normal flow depth in pipe =   24.75(In.)
Flow top width inside pipe =   28.58(In.)
Critical depth could not be calculated.
Pipe flow velocity =     22.67(Ft/s)
Travel time through pipe =    0.23 min.
Time of concentration (TC) =    15.49 min.


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Process from Point/Station      116.000 to Point/Station      117.000
**** SUBAREA FLOW ADDITION ****
________________________________________________________________________
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.761
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  74.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    15.49 min.
Rainfall intensity =      2.558(In/Hr) for a   100.0 year storm
Subarea runoff =      2.744(CFS) for      1.410(Ac.)
Total runoff =    111.074(CFS)       Total area =      51.800(Ac.)
End of computations, total study area =           51.80 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.534
Area averaged RI index number =  69.1
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 02/06/24  File:PRO3.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

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Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =  100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity =  1.300(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      200.000 to Point/Station      201.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   936.000(Ft.)
Top (of initial area) elevation =  1345.000(Ft.)
Bottom (of initial area) elevation =  1290.000(Ft.)
Difference in elevation =    55.000(Ft.)
Slope =    0.05876  s(percent)=       5.88
TC = k(0.300)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =    8.162 min.
Rainfall intensity =      3.525(In/Hr) for a   100.0 year storm
COMMERCIAL subarea type
Runoff Coefficient = 0.887
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.100; Impervious fraction =  0.900
Initial subarea runoff =      2.126(CFS)
Total initial stream area =        0.680(Ac.)
Pervious area fraction = 0.100


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      201.000 to Point/Station      202.000
**** STREET FLOW TRAVEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of street segment elevation =  1290.000(Ft.)
End of street segment elevation =  1282.000(Ft.)
Length of street segment  =   461.000(Ft.)
Height of curb above gutter flowline  =    6.0(In.)
Width of half street (curb to crown)  =  18.000(Ft.)
Distance from crown to crossfall grade break  =  16.000(Ft.)
Slope from gutter to grade break (v/hz) =   0.020
Slope from grade break to crown (v/hz)  =   0.020
Street flow is on [2] side(s) of the street
Distance from curb to property line  =  10.000(Ft.)
Slope from curb to property line (v/hz) =   0.020
Gutter width =   2.000(Ft.)
Gutter hike from flowline =  2.000(In.)
 Manning's N in gutter =  0.0150
 Manning's N from gutter to grade break =  0.0150
 Manning's N from grade break to crown =  0.0150
Estimated mean flow rate at midpoint of street =      4.154(CFS)
Depth of flow =   0.288(Ft.), Average velocity =   2.677(Ft/s)
Streetflow hydraulics at midpoint of street travel:
Halfstreet flow width =   8.058(Ft.)
Flow velocity =   2.68(Ft/s)
Travel time =    2.87 min.     TC =   11.03  min.
 Adding area flow to street
```

```
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.826
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Rainfall intensity =      3.032(In/Hr) for a   100.0 year storm
Subarea runoff =      3.930(CFS) for      1.570(Ac.)
Total runoff =      6.056(CFS)       Total area =       2.250(Ac.)
Street flow at end of street =      6.056(CFS)
Half street flow at end of street =      3.028(CFS)
Depth of flow =   0.318(Ft.), Average velocity =   2.909(Ft/s)
Flow width (from curb towards crown)=   9.561(Ft.)


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Process from Point/Station      202.000 to Point/Station      203.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1282.000(Ft.)
Downstream point/station elevation =  1275.000(Ft.)
Pipe length  =   427.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =     6.056(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =     6.056(CFS)
Normal flow depth in pipe =    9.54(In.)
Flow top width inside pipe =   14.43(In.)
Critical Depth =   11.94(In.)
Pipe flow velocity =      7.36(Ft/s)
Travel time through pipe =    0.97 min.
Time of concentration (TC) =    12.00 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      203.000 to Point/Station      203.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 1
Stream flow area =      2.250(Ac.)
Runoff from this stream =      6.056(CFS)
Time of concentration =   12.00 min.
Rainfall intensity =     2.907(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      204.000 to Point/Station      205.000
**** INITIAL AREA EVALUATION ****
------------------------------------------------------------------------------
Initial area flow distance =   914.000(Ft.)
Top (of initial area) elevation =  1345.000(Ft.)
Bottom (of initial area) elevation =  1290.000(Ft.)
Difference in elevation =    55.000(Ft.)
Slope =    0.06018  s(percent)=       6.02
TC = k(0.390)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   10.461 min.
Rainfall intensity =      3.113(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.827
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
Initial subarea runoff =     11.051(CFS)
Total initial stream area =        4.290(Ac.)
Pervious area fraction = 0.500


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      205.000 to Point/Station      203.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
------------------------------------------------------------------------------
Upstream point/station elevation =  1290.000(Ft.)
Downstream point/station elevation =  1275.000(Ft.)
Pipe length  =    75.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    11.051(CFS)
Nearest computed pipe diameter  =     12.00(In.)
Calculated individual pipe flow  =    11.051(CFS)
Normal flow depth in pipe =    7.35(In.)
Flow top width inside pipe =   11.69(In.)
Critical depth could not be calculated.
Pipe flow velocity =     21.91(Ft/s)
Travel time through pipe =    0.06 min.
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```
Time of concentration (TC) =    10.52 min.


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Process from Point/Station      203.000 to Point/Station      203.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      4.290(Ac.)
Runoff from this stream =     11.051(CFS)
Time of concentration =   10.52 min.
Rainfall intensity =     3.105(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1        6.056     12.00                 2.907
2       11.051     10.52                 3.105
Largest stream flow has longer or shorter time of concentration
Qp =     11.051 + sum of
          Qa           Tb/Ta
           6.056 *    0.877 =      5.308
Qp =     16.359

Total of 2 streams to confluence:
Flow rates before confluence point:
       6.056      11.051
Area of streams before confluence:
        2.250        4.290
Results of confluence:
Total flow rate =     16.359(CFS)
Time of concentration =    10.518 min.
Effective stream area after confluence =      6.540(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      203.000 to Point/Station      206.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1275.000(Ft.)
Downstream point/station elevation =  1264.000(Ft.)
Pipe length  =   110.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    16.359(CFS)
Nearest computed pipe diameter  =     15.00(In.)
Calculated individual pipe flow  =    16.359(CFS)
Normal flow depth in pipe =   10.16(In.)
Flow top width inside pipe =   14.02(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.50(Ft/s)
Travel time through pipe =    0.10 min.
Time of concentration (TC) =    10.62 min.


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Process from Point/Station      206.000 to Point/Station      207.000
**** SUBAREA FLOW ADDITION ****
______________________________________________________________________________
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.782
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  74.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Time of concentration =    10.62 min.
Rainfall intensity =      3.090(In/Hr) for a   100.0 year storm
Subarea runoff =      3.019(CFS) for      1.250(Ac.)
Total runoff =     19.378(CFS)       Total area =       7.790(Ac.)
End of computations, total study area =            7.79 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.545
Area averaged RI index number =  69.8
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 02/06/24  File:PROOFF.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

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Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =  100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity =  1.300(In/Hr)
Slope of intensity duration curve = 0.5000




++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      300.000 to Point/Station      301.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   930.000(Ft.)
Top (of initial area) elevation =  1522.000(Ft.)
Bottom (of initial area) elevation =  1448.000(Ft.)
Difference in elevation =    74.000(Ft.)
Slope =    0.07957  s(percent)=       7.96
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.537 min.
Rainfall intensity =      2.737(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.834
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     15.565(CFS)
Total initial stream area =        6.820(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      301.000 to Point/Station      302.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of natural channel elevation =   1448.000(Ft.)
End of natural channel elevation =   1363.000(Ft.)
Length of natural channel  =  1674.000(Ft.)
Estimated mean flow rate at midpoint of channel =     39.596(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.16(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0508
Corrected/adjusted channel slope =  0.0508
Travel time =    3.42 min.     TC =   16.96  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.827
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
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Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.445(In/Hr) for a   100.0 year storm
Subarea runoff =     42.571(CFS) for     21.060(Ac.)
Total runoff =     58.136(CFS)       Total area =      27.880(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      302.000 to Point/Station      303.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1363.000(Ft.)
Downstream point/station elevation =  1359.000(Ft.)
Pipe length  =    86.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    58.136(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    58.136(CFS)
Normal flow depth in pipe =   19.48(In.)
Flow top width inside pipe =   24.21(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.92(Ft/s)
Travel time through pipe =    0.08 min.
Time of concentration (TC) =    17.03 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      303.000 to Point/Station      303.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     27.880(Ac.)
Runoff from this stream =     58.136(CFS)
Time of concentration =   17.03 min.
Rainfall intensity =     2.440(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      304.000 to Point/Station      305.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =  1000.000(Ft.)
Top (of initial area) elevation =  1468.000(Ft.)
Bottom (of initial area) elevation =  1377.000(Ft.)
Difference in elevation =    91.000(Ft.)
Slope =    0.09100  s(percent)=       9.10
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.566 min.
Rainfall intensity =      2.734(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.834
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     20.402(CFS)
Total initial stream area =        8.950(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      305.000 to Point/Station      303.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1377.000(Ft.)
Downstream point/station elevation =  1359.000(Ft.)
Pipe length  =   366.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    20.402(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =    20.402(CFS)
Normal flow depth in pipe =   13.05(In.)
Flow top width inside pipe =   16.07(In.)
Critical depth could not be calculated.
Pipe flow velocity =     14.86(Ft/s)
Travel time through pipe =    0.41 min.
Time of concentration (TC) =    13.98 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      303.000 to Point/Station      303.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      8.950(Ac.)
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Runoff from this stream =     20.402(CFS)
Time of concentration =   13.98 min.
Rainfall intensity =     2.693(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       58.136     17.03                 2.440
2       20.402     13.98                 2.693
Largest stream flow has longer time of concentration
Qp =     58.136 + sum of
          Qb         Ia/Ib
          20.402 *    0.906 =     18.482
Qp =     76.618

Total of 2 streams to confluence:
Flow rates before confluence point:
      58.136      20.402
Area of streams before confluence:
       27.880        8.950
Results of confluence:
Total flow rate =     76.618(CFS)
Time of concentration =    17.032 min.
Effective stream area after confluence =     36.830(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      303.000 to Point/Station      306.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1359.000(Ft.)
Downstream point/station elevation =  1355.000(Ft.)
Pipe length  =    75.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    76.618(CFS)
Nearest computed pipe diameter  =     30.00(In.)
Calculated individual pipe flow  =    76.618(CFS)
Normal flow depth in pipe =   20.46(In.)
Flow top width inside pipe =   27.94(In.)
Critical depth could not be calculated.
Pipe flow velocity =     21.48(Ft/s)
Travel time through pipe =    0.06 min.
Time of concentration (TC) =    17.09 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      306.000 to Point/Station      307.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1355.000(Ft.)
End of natural channel elevation =   1329.000(Ft.)
Length of natural channel  =   405.000(Ft.)
Estimated mean flow rate at midpoint of channel =     80.341(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  11.27(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0642
Corrected/adjusted channel slope =  0.0642
Travel time =    0.60 min.     TC =   17.69  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.825
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.394(In/Hr) for a   100.0 year storm
Subarea runoff =      7.073(CFS) for      3.580(Ac.)
Total runoff =     83.690(CFS)       Total area =      40.410(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      307.000 to Point/Station      308.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1329.000(Ft.)
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Downstream point/station elevation =  1319.000(Ft.)
Pipe length  =   258.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    83.690(CFS)
Nearest computed pipe diameter  =     30.00(In.)
Calculated individual pipe flow  =    83.690(CFS)
Normal flow depth in pipe =   25.69(In.)
Flow top width inside pipe =   21.05(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.70(Ft/s)
Travel time through pipe =    0.23 min.
Time of concentration (TC) =    17.92 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      308.000 to Point/Station      309.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1319.000(Ft.)
End of natural channel elevation =   1299.000(Ft.)
Length of natural channel  =   332.000(Ft.)
Estimated mean flow rate at midpoint of channel =     84.726(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  11.09(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0602
Corrected/adjusted channel slope =  0.0602
Travel time =    0.50 min.     TC =   18.42  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.824
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.346(In/Hr) for a   100.0 year storm
Subarea runoff =      1.933(CFS) for      1.000(Ac.)
Total runoff =     85.623(CFS)       Total area =      41.410(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      309.000 to Point/Station      309.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =     41.410(Ac.)
Runoff from this stream =     85.623(CFS)
Time of concentration =   18.42 min.
Rainfall intensity =     2.346(In/Hr)
Program is now starting with Main Stream No. 2


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      310.000 to Point/Station      311.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   972.000(Ft.)
Top (of initial area) elevation =  1518.000(Ft.)
Bottom (of initial area) elevation =  1451.000(Ft.)
Difference in elevation =    67.000(Ft.)
Slope =    0.06893  s(percent)=       6.89
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.179 min.
Rainfall intensity =      2.674(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.832
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     19.100(CFS)
Total initial stream area =        8.580(Ac.)
Pervious area fraction = 1.000
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++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      311.000 to Point/Station      312.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1451.000(Ft.)
End of natural channel elevation =   1371.000(Ft.)
Length of natural channel  =  1830.000(Ft.)
Estimated mean flow rate at midpoint of channel =     35.305(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.33(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0437
Corrected/adjusted channel slope =  0.0437
Travel time =    4.16 min.     TC =   18.34  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.824
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.351(In/Hr) for a   100.0 year storm
Subarea runoff =     28.207(CFS) for     14.560(Ac.)
Total runoff =     47.307(CFS)       Total area =      23.140(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      312.000 to Point/Station      313.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
----------------------------------------------------------------------------
Upstream point/station elevation =  1371.000(Ft.)
Downstream point/station elevation =  1360.000(Ft.)
Pipe length  =   473.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    47.307(CFS)
Nearest computed pipe diameter  =     27.00(In.)
Calculated individual pipe flow  =    47.307(CFS)
Normal flow depth in pipe =   22.17(In.)
Flow top width inside pipe =   20.69(In.)
Critical depth could not be calculated.
Pipe flow velocity =     13.54(Ft/s)
Travel time through pipe =    0.58 min.
Time of concentration (TC) =    18.92 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      313.000 to Point/Station      314.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1360.000(Ft.)
End of natural channel elevation =   1347.000(Ft.)
Length of natural channel  =   166.000(Ft.)
Estimated mean flow rate at midpoint of channel =     47.879(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  10.70(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0783
Corrected/adjusted channel slope =  0.0783
Travel time =    0.26 min.     TC =   19.18  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.822
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.299(In/Hr) for a   100.0 year storm
Subarea runoff =      1.059(CFS) for      0.560(Ac.)
Total runoff =     48.366(CFS)       Total area =      23.700(Ac.)
```

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Process from Point/Station      314.000 to Point/Station      314.000
**** CONFLUENCE OF MINOR STREAMS ****
____________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     23.700(Ac.)
Runoff from this stream =     48.366(CFS)
Time of concentration =   19.18 min.
Rainfall intensity =     2.299(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      315.000 to Point/Station      316.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   682.000(Ft.)
Top (of initial area) elevation =  1471.000(Ft.)
Bottom (of initial area) elevation =  1433.000(Ft.)
Difference in elevation =    38.000(Ft.)
Slope =    0.05572  s(percent)=       5.57
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.841 min.
Rainfall intensity =      2.810(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.835
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     11.293(CFS)
Total initial stream area =        4.810(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      316.000 to Point/Station      314.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of natural channel elevation =   1433.000(Ft.)
End of natural channel elevation =   1347.000(Ft.)
Length of natural channel  =  1629.000(Ft.)
Estimated mean flow rate at midpoint of channel =     36.519(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.13(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0528
Corrected/adjusted channel slope =  0.0528
Travel time =    3.34 min.     TC =   16.18  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.828
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.503(In/Hr) for a   100.0 year storm
Subarea runoff =     44.555(CFS) for     21.490(Ac.)
Total runoff =     55.848(CFS)       Total area =      26.300(Ac.)


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Process from Point/Station      314.000 to Point/Station      314.000
**** CONFLUENCE OF MINOR STREAMS ****
____________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     26.300(Ac.)
Runoff from this stream =     55.848(CFS)
Time of concentration =   16.18 min.
Rainfall intensity =     2.503(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)
```

```
1       48.366     19.18                2.299
2       55.848     16.18                2.503
Largest stream flow has longer or shorter time of concentration
Qp =     55.848 + sum of
          Qa          Tb/Ta
          48.366 *    0.843 =     40.796
Qp =     96.644

Total of 2 streams to confluence:
Flow rates before confluence point:
      48.366      55.848
Area of streams before confluence:
       23.700       26.300
Results of confluence:
Total flow rate =     96.644(CFS)
Time of concentration =    16.180 min.
Effective stream area after confluence =     50.000(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      314.000 to Point/Station      309.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
________________________________________________________________________
Top of natural channel elevation =   1347.000(Ft.)
End of natural channel elevation =   1299.000(Ft.)
Length of natural channel  =  1131.000(Ft.)
Estimated mean flow rate at midpoint of channel =    101.688(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.83(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0424
Corrected/adjusted channel slope =  0.0424
Travel time =    1.92 min.     TC =   18.10  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.824
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.367(In/Hr) for a   100.0 year storm
Subarea runoff =     10.186(CFS) for      5.220(Ac.)
Total runoff =    106.830(CFS)        Total area =      55.220(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      309.000 to Point/Station      309.000
**** CONFLUENCE OF MAIN STREAMS ****
________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =     55.220(Ac.)
Runoff from this stream =    106.830(CFS)
Time of concentration =   18.10 min.
Rainfall intensity =     2.367(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       85.623     18.42                2.346
2      106.830     18.10                2.367
Largest stream flow has longer or shorter time of concentration
Qp =    106.830 + sum of
          Qa          Tb/Ta
          85.623 *    0.983 =     84.132
Qp =    190.962

Total of 2 main streams to confluence:
Flow rates before confluence point:
      85.623     106.830
Area of streams before confluence:
       41.410       55.220
```

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Results of confluence:
Total flow rate =    190.962(CFS)
Time of concentration =    18.098 min.
Effective stream area after confluence  =     96.630(Ac.)


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Process from Point/Station      309.000 to Point/Station      317.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1299.000(Ft.)
End of natural channel elevation =   1251.000(Ft.)
Length of natural channel  =  1118.000(Ft.)
Estimated mean flow rate at midpoint of channel =    194.707(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  12.05(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0429
Corrected/adjusted channel slope =  0.0429
Travel time =    1.55 min.     TC =   19.64  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.822
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.272(In/Hr) for a   100.0 year storm
Subarea runoff =      7.074(CFS) for      3.790(Ac.)
Total runoff =    198.036(CFS)       Total area =     100.420(Ac.)


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Process from Point/Station      317.000 to Point/Station      317.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    100.420(Ac.)
Runoff from this stream =    198.036(CFS)
Time of concentration =   19.64 min.
Rainfall intensity =     2.272(In/Hr)


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Process from Point/Station      117.000 to Point/Station      117.000
**** USER DEFINED FLOW INFORMATION AT A POINT ****
______________________________________________________________________________
Rainfall intensity =      2.559(In/Hr) for a   100.0 year storm
SINGLE FAMILY (1/4 Acre Lot)
Runoff Coefficient = 0.815
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  69.00
Pervious area fraction =  0.500; Impervious fraction =  0.500
User specified values are as follows:
TC =  15.49 min.  Rain intensity =       2.56(In/Hr)
Total area =        51.80(Ac.)  Total runoff =    111.07(CFS)


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Process from Point/Station      117.000 to Point/Station      317.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1291.000(Ft.)
Downstream point/station elevation =  1251.000(Ft.)
Pipe length  =   134.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =   111.070(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =   111.070(CFS)
Normal flow depth in pipe =   17.77(In.)
Flow top width inside pipe =   21.05(In.)
Critical depth could not be calculated.
Pipe flow velocity =     44.51(Ft/s)
Travel time through pipe =    0.05 min.
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Time of concentration (TC) =    15.54 min.


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Process from Point/Station      317.000 to Point/Station      317.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     51.800(Ac.)
Runoff from this stream =    111.070(CFS)
Time of concentration =   15.54 min.
Rainfall intensity =     2.554(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      198.036     19.64                2.272
2      111.070     15.54                2.554
Largest stream flow has longer time of concentration
Qp =    198.036 + sum of
          Qb          Ia/Ib
         111.070 *    0.889 =     98.789
Qp =    296.825

Total of 2 streams to confluence:
Flow rates before confluence point:
     198.036     111.070
Area of streams before confluence:
      100.420       51.800
Results of confluence:
Total flow rate =    296.825(CFS)
Time of concentration =    19.644 min.
Effective stream area after confluence =    152.220(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      317.000 to Point/Station      318.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1251.000(Ft.)
End of natural channel elevation =   1243.000(Ft.)
Length of natural channel  =   225.000(Ft.)
Estimated mean flow rate at midpoint of channel =    297.673(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  12.52(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0356
Corrected/adjusted channel slope =  0.0356
Travel time =    0.30 min.     TC =   19.94  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.821
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.255(In/Hr) for a   100.0 year storm
Subarea runoff =      1.611(CFS) for      0.870(Ac.)
Total runoff =    298.435(CFS)       Total area =     153.090(Ac.)


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Process from Point/Station      318.000 to Point/Station      318.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =    153.090(Ac.)
Runoff from this stream =    298.435(CFS)
Time of concentration =   19.94 min.
Rainfall intensity =     2.255(In/Hr)


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Process from Point/Station      319.000 to Point/Station      318.000
**** INITIAL AREA EVALUATION ****
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Initial area flow distance =   573.000(Ft.)
Top (of initial area) elevation =  1322.000(Ft.)
Bottom (of initial area) elevation =  1243.000(Ft.)
Difference in elevation =    79.000(Ft.)
Slope =    0.13787  s(percent)=      13.79
TC = k(0.940)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   17.721 min.
Rainfall intensity =      2.392(In/Hr) for a   100.0 year storm
UNDEVELOPED (good cover) subarea
Runoff Coefficient = 0.753
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  74.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      4.375(CFS)
Total initial stream area =        2.430(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station      318.000 to Point/Station      318.000
**** CONFLUENCE OF MINOR STREAMS ****
------------------------------------------------------------------------------
Along Main Stream number: 1 in normal stream number 2
Stream flow area =      2.430(Ac.)
Runoff from this stream =      4.375(CFS)
Time of concentration =   17.72 min.
Rainfall intensity =     2.392(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      298.435     19.94                 2.255
2        4.375     17.72                 2.392
Largest stream flow has longer time of concentration
Qp =    298.435 + sum of
          Qb          Ia/Ib
           4.375 *    0.943 =      4.124
Qp =    302.559

Total of 2 streams to confluence:
Flow rates before confluence point:
     298.435       4.375
Area of streams before confluence:
      153.090        2.430
Results of confluence:
Total flow rate =    302.559(CFS)
Time of concentration =    19.944 min.
Effective stream area after confluence =    155.520(Ac.)
End of computations, total study area =          155.52 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 0.833
Area averaged RI index number =  80.2
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                Riverside County Rational Hydrology Program

CIVILCADD/CIVILDESIGN Engineering Software,(c) 1989 - 2004 Version 7.0
        Rational Hydrology Study        Date: 02/06/24  File:PROOFF2.out
------------------------------------------------------------------------
 *********   Hydrology Study Control Information **********

 English (in-lb) Units used in input data file

------------------------------------------------------------------------


Program License Serial Number 5006

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Rational Method Hydrology Program based on
Riverside County Flood Control & Water Conservation District
1978 hydrology manual

Storm event (year) =  100.00 Antecedent Moisture Condition = 2

2 year, 1 hour precipitation =  0.500(In.)
100 year, 1 hour precipitation =  1.300(In.)

Storm event year = 100.0
Calculated rainfall intensity data:
1 hour intensity =  1.300(In/Hr)
Slope of intensity duration curve = 0.5000




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Process from Point/Station      501.000 to Point/Station      502.000
**** INITIAL AREA EVALUATION ****
____________________________________________________________________________
Initial area flow distance =   914.000(Ft.)
Top (of initial area) elevation =  1620.000(Ft.)
Bottom (of initial area) elevation =  1572.000(Ft.)
Difference in elevation =    48.000(Ft.)
Slope =    0.05252  s(percent)=       5.25
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.608 min.
Rainfall intensity =      2.635(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.827
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.900
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  85.20
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     20.902(CFS)
Total initial stream area =        9.590(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      502.000 to Point/Station      503.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
____________________________________________________________________________
Top of natural channel elevation =   1572.000(Ft.)
End of natural channel elevation =   1444.000(Ft.)
Length of natural channel  =  4065.000(Ft.)
Estimated mean flow rate at midpoint of channel =    118.383(CFS)

Natural mountain channel type used
L.A. County flood control district formula for channel velocity:
 Velocity = 5.48(q^.33)(slope^.492)
Velocity using mean channel flow =   4.83(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0315
Corrected/adjusted channel slope =  0.0315
Travel time =   14.02 min.     TC =   28.63  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.800
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.600
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Decimal fraction soil group D = 0.200
RI index for soil(AMC 2)  =  85.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.882(In/Hr) for a   100.0 year storm
Subarea runoff =    134.665(CFS) for     89.450(Ac.)
Total runoff =    155.567(CFS)       Total area =      99.040(Ac.)


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Process from Point/Station      503.000 to Point/Station      503.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 1
Stream flow area =     99.040(Ac.)
Runoff from this stream =    155.567(CFS)
Time of concentration =   28.63 min.
Rainfall intensity =     1.882(In/Hr)


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Process from Point/Station      504.000 to Point/Station      505.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   952.000(Ft.)
Top (of initial area) elevation =  1572.000(Ft.)
Bottom (of initial area) elevation =  1532.000(Ft.)
Difference in elevation =    40.000(Ft.)
Slope =    0.04202  s(percent)=       4.20
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   15.526 min.
Rainfall intensity =      2.556(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.830
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     15.964(CFS)
Total initial stream area =        7.530(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station      505.000 to Point/Station      503.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1532.000(Ft.)
End of natural channel elevation =   1444.000(Ft.)
Length of natural channel  =  2338.000(Ft.)
Estimated mean flow rate at midpoint of channel =     76.786(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.51(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0376
Corrected/adjusted channel slope =  0.0376
Travel time =    4.58 min.     TC =   20.10  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.821
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.246(In/Hr) for a   100.0 year storm
Subarea runoff =    105.760(CFS) for     57.380(Ac.)
Total runoff =    121.723(CFS)       Total area =      64.910(Ac.)


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Process from Point/Station      503.000 to Point/Station      503.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 1 in normal stream number 2
Stream flow area =     64.910(Ac.)
Runoff from this stream =    121.723(CFS)
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Time of concentration =   20.10 min.
Rainfall intensity =     2.246(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      155.567     28.63                 1.882
2      121.723     20.10                 2.246
Largest stream flow has longer time of concentration
Qp =    155.567 + sum of
          Qb         Ia/Ib
         121.723 *    0.838 =    101.997
Qp =    257.564

Total of 2 streams to confluence:
Flow rates before confluence point:
     155.567     121.723
Area of streams before confluence:
       99.040       64.910
Results of confluence:
Total flow rate =    257.564(CFS)
Time of concentration =    28.632 min.
Effective stream area after confluence =    163.950(Ac.)


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Process from Point/Station      503.000 to Point/Station      506.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1444.000(Ft.)
End of natural channel elevation =   1426.000(Ft.)
Length of natural channel  =   816.000(Ft.)
Estimated mean flow rate at midpoint of channel =    286.949(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.75(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0221
Corrected/adjusted channel slope =  0.0221
Travel time =    1.39 min.     TC =   30.03  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.801
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.100
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.100
RI index for soil(AMC 2)  =  85.50
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.838(In/Hr) for a   100.0 year storm
Subarea runoff =     55.093(CFS) for     37.410(Ac.)
Total runoff =    312.657(CFS)       Total area =     201.360(Ac.)


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Process from Point/Station      506.000 to Point/Station      507.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1426.000(Ft.)
Downstream point/station elevation =  1414.000(Ft.)
Pipe length  =    73.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =   312.657(CFS)
Nearest computed pipe diameter  =     39.00(In.)
Calculated individual pipe flow  =   312.657(CFS)
Normal flow depth in pipe =   29.86(In.)
Flow top width inside pipe =   33.04(In.)
Critical depth could not be calculated.
Pipe flow velocity =     45.85(Ft/s)
Travel time through pipe =    0.03 min.
Time of concentration (TC) =    30.05 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      507.000 to Point/Station      508.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1414.000(Ft.)
End of natural channel elevation =   1369.000(Ft.)
```

```
Length of natural channel  =  1860.000(Ft.)
Estimated mean flow rate at midpoint of channel =    330.692(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  10.68(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0242
Corrected/adjusted channel slope =  0.0242
Travel time =    2.90 min.     TC =   32.96  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.801
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.754(In/Hr) for a   100.0 year storm
Subarea runoff =     32.634(CFS) for     23.230(Ac.)
Total runoff =    345.292(CFS)       Total area =     224.590(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      508.000 to Point/Station      508.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 1
Stream flow area =    224.590(Ac.)
Runoff from this stream =    345.292(CFS)
Time of concentration =   32.96 min.
Rainfall intensity =     1.754(In/Hr)
Program is now starting with Main Stream No. 2


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      509.000 to Point/Station      510.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   901.000(Ft.)
Top (of initial area) elevation =  1592.000(Ft.)
Bottom (of initial area) elevation =  1516.000(Ft.)
Difference in elevation =    76.000(Ft.)
Slope =    0.08435  s(percent)=       8.44
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   13.211 min.
Rainfall intensity =      2.770(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.835
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     10.104(CFS)
Total initial stream area =        4.370(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      510.000 to Point/Station      511.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1516.000(Ft.)
End of natural channel elevation =   1452.000(Ft.)
Length of natural channel  =  2076.000(Ft.)
Estimated mean flow rate at midpoint of channel =     45.215(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.60(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0308
Corrected/adjusted channel slope =  0.0308
Travel time =    5.24 min.     TC =   18.45  min.
```

```
 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.824
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.344(In/Hr) for a   100.0 year storm
Subarea runoff =     58.644(CFS) for     30.370(Ac.)
Total runoff =     68.749(CFS)       Total area =      34.740(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      511.000 to Point/Station      512.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1452.000(Ft.)
Downstream point/station elevation =  1451.000(Ft.)
Pipe length  =    40.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    68.749(CFS)
Nearest computed pipe diameter  =     30.00(In.)
Calculated individual pipe flow  =    68.749(CFS)
Normal flow depth in pipe =   26.72(In.)
Flow top width inside pipe =   18.73(In.)
Critical depth could not be calculated.
Pipe flow velocity =     14.90(Ft/s)
Travel time through pipe =    0.04 min.
Time of concentration (TC) =    18.50 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      512.000 to Point/Station      513.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1451.000(Ft.)
End of natural channel elevation =   1412.000(Ft.)
Length of natural channel  =   777.000(Ft.)
Estimated mean flow rate at midpoint of channel =     70.639(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.59(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0502
Corrected/adjusted channel slope =  0.0502
Travel time =    1.35 min.     TC =   19.85  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.821
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.260(In/Hr) for a   100.0 year storm
Subarea runoff =      3.545(CFS) for      1.910(Ac.)
Total runoff =     72.294(CFS)       Total area =      36.650(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      513.000 to Point/Station      513.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     36.650(Ac.)
Runoff from this stream =     72.294(CFS)
Time of concentration =   19.85 min.
Rainfall intensity =     2.260(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      510.000 to Point/Station      514.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   923.000(Ft.)
Top (of initial area) elevation =  1516.000(Ft.)
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Bottom (of initial area) elevation =  1493.000(Ft.)
Difference in elevation =    23.000(Ft.)
Slope =    0.02492  s(percent)=       2.49
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   17.024 min.
Rainfall intensity =      2.441(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.826
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =      4.861(CFS)
Total initial stream area =        2.410(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station      514.000 to Point/Station      515.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1493.000(Ft.)
End of natural channel elevation =   1418.000(Ft.)
Length of natural channel  =  1990.000(Ft.)
Estimated mean flow rate at midpoint of channel =     14.544(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   5.34(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0377
Corrected/adjusted channel slope =  0.0377
Travel time =    6.21 min.     TC =   23.23  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.815
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.089(In/Hr) for a   100.0 year storm
Subarea runoff =     16.353(CFS) for      9.600(Ac.)
Total runoff =     21.214(CFS)       Total area =      12.010(Ac.)


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Process from Point/Station      515.000 to Point/Station      513.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1418.000(Ft.)
Downstream point/station elevation =  1412.000(Ft.)
Pipe length  =    74.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    21.214(CFS)
Nearest computed pipe diameter  =     18.00(In.)
Calculated individual pipe flow  =    21.214(CFS)
Normal flow depth in pipe =   11.19(In.)
Flow top width inside pipe =   17.46(In.)
Critical depth could not be calculated.
Pipe flow velocity =     18.36(Ft/s)
Travel time through pipe =    0.07 min.
Time of concentration (TC) =    23.30 min.


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Process from Point/Station      513.000 to Point/Station      513.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     12.010(Ac.)
Runoff from this stream =     21.214(CFS)
Time of concentration =   23.30 min.
Rainfall intensity =     2.086(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)
```

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1       72.294     19.85                2.260
2       21.214     23.30                2.086
Largest stream flow has longer or shorter time of concentration
Qp =     72.294 + sum of
          Qa          Tb/Ta
          21.214 *    0.852 =     18.073
Qp =     90.366

Total of 2 streams to confluence:
Flow rates before confluence point:
      72.294      21.214
Area of streams before confluence:
       36.650       12.010
Results of confluence:
Total flow rate =     90.366(CFS)
Time of concentration =    19.847 min.
Effective stream area after confluence =     48.660(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      513.000 to Point/Station      516.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1412.000(Ft.)
End of natural channel elevation =   1406.000(Ft.)
Length of natural channel  =   142.000(Ft.)
Estimated mean flow rate at midpoint of channel =     91.258(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.49(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0423
Corrected/adjusted channel slope =  0.0423
Travel time =    0.25 min.     TC =   20.10  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.821
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.246(In/Hr) for a   100.0 year storm
Subarea runoff =      1.770(CFS) for      0.960(Ac.)
Total runoff =     92.136(CFS)       Total area =      49.620(Ac.)


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Process from Point/Station      516.000 to Point/Station      516.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     49.620(Ac.)
Runoff from this stream =     92.136(CFS)
Time of concentration =   20.10 min.
Rainfall intensity =     2.246(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      517.000 to Point/Station      518.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   928.000(Ft.)
Top (of initial area) elevation =  1510.000(Ft.)
Bottom (of initial area) elevation =  1450.000(Ft.)
Difference in elevation =    60.000(Ft.)
Slope =    0.06466  s(percent)=       6.47
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.099 min.
Rainfall intensity =      2.682(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.833
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
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Initial subarea runoff =     17.194(CFS)
Total initial stream area =        7.700(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station      518.000 to Point/Station      516.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1450.000(Ft.)
End of natural channel elevation =   1406.000(Ft.)
Length of natural channel  =   897.000(Ft.)
Estimated mean flow rate at midpoint of channel =     24.272(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.00(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0491
Corrected/adjusted channel slope =  0.0491
Travel time =    2.14 min.     TC =   16.24  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.828
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.499(In/Hr) for a   100.0 year storm
Subarea runoff =     13.120(CFS) for      6.340(Ac.)
Total runoff =     30.314(CFS)       Total area =      14.040(Ac.)


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Process from Point/Station      516.000 to Point/Station      516.000
**** CONFLUENCE OF MINOR STREAMS ****
----------------------------------------------------------------------------
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     14.040(Ac.)
Runoff from this stream =     30.314(CFS)
Time of concentration =   16.24 min.
Rainfall intensity =     2.499(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1       92.136     20.10                2.246
2       30.314     16.24                2.499
Largest stream flow has longer time of concentration
Qp =     92.136 + sum of
          Qb         Ia/Ib
          30.314 *    0.899 =     27.247
Qp =    119.383

Total of 2 streams to confluence:
Flow rates before confluence point:
      92.136      30.314
Area of streams before confluence:
       49.620       14.040
Results of confluence:
Total flow rate =    119.383(CFS)
Time of concentration =    20.096 min.
Effective stream area after confluence =     63.660(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      516.000 to Point/Station      519.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
----------------------------------------------------------------------------
Top of natural channel elevation =   1406.000(Ft.)
End of natural channel elevation =   1386.000(Ft.)
Length of natural channel  =   577.000(Ft.)
Estimated mean flow rate at midpoint of channel =    121.690(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
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Velocity using mean channel flow =   9.38(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0347
Corrected/adjusted channel slope =  0.0347
Travel time =    1.03 min.     TC =   21.12  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.819
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.191(In/Hr) for a   100.0 year storm
Subarea runoff =      4.414(CFS) for      2.460(Ac.)
Total runoff =    123.797(CFS)       Total area =      66.120(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      519.000 to Point/Station      519.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =     66.120(Ac.)
Runoff from this stream =    123.797(CFS)
Time of concentration =   21.12 min.
Rainfall intensity =     2.191(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      520.000 to Point/Station      521.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   986.000(Ft.)
Top (of initial area) elevation =  1540.000(Ft.)
Bottom (of initial area) elevation =  1480.000(Ft.)
Difference in elevation =    60.000(Ft.)
Slope =    0.06085  s(percent)=       6.09
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   14.621 min.
Rainfall intensity =      2.633(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.831
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     19.247(CFS)
Total initial stream area =        8.790(Ac.)
Pervious area fraction = 1.000


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Process from Point/Station      521.000 to Point/Station      522.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1480.000(Ft.)
End of natural channel elevation =   1449.000(Ft.)
Length of natural channel  =  1024.000(Ft.)
Estimated mean flow rate at midpoint of channel =     36.283(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   6.15(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0303
Corrected/adjusted channel slope =  0.0303
Travel time =    2.78 min.     TC =   17.40  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.826
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
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Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.414(In/Hr) for a   100.0 year storm
Subarea runoff =     31.019(CFS) for     15.560(Ac.)
Total runoff =     50.267(CFS)       Total area =      24.350(Ac.)


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Process from Point/Station      522.000 to Point/Station      519.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1449.000(Ft.)
End of natural channel elevation =   1386.000(Ft.)
Length of natural channel  =  1283.000(Ft.)
Estimated mean flow rate at midpoint of channel =     62.178(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   9.14(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0491
Corrected/adjusted channel slope =  0.0491
Travel time =    2.34 min.     TC =   19.74  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.821
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.267(In/Hr) for a   100.0 year storm
Subarea runoff =     21.483(CFS) for     11.540(Ac.)
Total runoff =     71.750(CFS)       Total area =      35.890(Ac.)


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Process from Point/Station      519.000 to Point/Station      519.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     35.890(Ac.)
Runoff from this stream =     71.750(CFS)
Time of concentration =   19.74 min.
Rainfall intensity =     2.267(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      123.797     21.12                 2.191
2       71.750     19.74                 2.267
Largest stream flow has longer time of concentration
Qp =    123.797 + sum of
          Qb          Ia/Ib
          71.750 *    0.967 =     69.359
Qp =    193.156

Total of 2 streams to confluence:
Flow rates before confluence point:
     123.797      71.750
Area of streams before confluence:
       66.120       35.890
Results of confluence:
Total flow rate =    193.156(CFS)
Time of concentration =    21.122 min.
Effective stream area after confluence =    102.010(Ac.)


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Process from Point/Station      519.000 to Point/Station      523.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1386.000(Ft.)
End of natural channel elevation =   1380.000(Ft.)
Length of natural channel  =   135.000(Ft.)
Estimated mean flow rate at midpoint of channel =    193.629(CFS)
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```
Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  12.24(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0444
Corrected/adjusted channel slope =  0.0444
Travel time =    0.18 min.     TC =   21.31  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.819
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.182(In/Hr) for a   100.0 year storm
Subarea runoff =      0.893(CFS) for      0.500(Ac.)
Total runoff =    194.049(CFS)       Total area =     102.510(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      523.000 to Point/Station      523.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 1
Stream flow area =    102.510(Ac.)
Runoff from this stream =    194.049(CFS)
Time of concentration =   21.31 min.
Rainfall intensity =     2.182(In/Hr)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      524.000 to Point/Station      525.000
**** INITIAL AREA EVALUATION ****
______________________________________________________________________________
Initial area flow distance =   590.000(Ft.)
Top (of initial area) elevation =  1430.000(Ft.)
Bottom (of initial area) elevation =  1405.000(Ft.)
Difference in elevation =    25.000(Ft.)
Slope =    0.04237  s(percent)=       4.24
TC = k(0.530)*[(length^3)/(elevation change)]^0.2
Initial area time of concentration =   12.800 min.
Rainfall intensity =      2.815(In/Hr) for a   100.0 year storm
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.836
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Initial subarea runoff =     19.943(CFS)
Total initial stream area =        8.480(Ac.)
Pervious area fraction = 1.000


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      525.000 to Point/Station      526.000
**** PIPEFLOW TRAVEL TIME (Program estimated size) ****
______________________________________________________________________________
Upstream point/station elevation =  1405.000(Ft.)
Downstream point/station elevation =  1404.000(Ft.)
Pipe length  =    75.00(Ft.)   Manning's N = 0.013
No. of pipes = 1  Required pipe flow  =    19.943(CFS)
Nearest computed pipe diameter  =     24.00(In.)
Calculated individual pipe flow  =    19.943(CFS)
Normal flow depth in pipe =   15.70(In.)
Flow top width inside pipe =   22.83(In.)
Critical Depth =   19.26(In.)
Pipe flow velocity =      9.16(Ft/s)
Travel time through pipe =    0.14 min.
Time of concentration (TC) =    12.94 min.


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      526.000 to Point/Station      523.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1404.000(Ft.)
End of natural channel elevation =   1380.000(Ft.)
```

```
Length of natural channel  =   502.000(Ft.)
Estimated mean flow rate at midpoint of channel =     28.057(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   7.19(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0478
Corrected/adjusted channel slope =  0.0478
Travel time =    1.16 min.     TC =   14.10  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.833
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.682(In/Hr) for a   100.0 year storm
Subarea runoff =     15.406(CFS) for      6.900(Ac.)
Total runoff =     35.349(CFS)       Total area =      15.380(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      523.000 to Point/Station      523.000
**** CONFLUENCE OF MINOR STREAMS ****
______________________________________________________________________________
Along Main Stream number: 2 in normal stream number 2
Stream flow area =     15.380(Ac.)
Runoff from this stream =     35.349(CFS)
Time of concentration =   14.10 min.
Rainfall intensity =     2.682(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      194.049     21.31                2.182
2       35.349     14.10                2.682
Largest stream flow has longer time of concentration
Qp =    194.049 + sum of
          Qb         Ia/Ib
          35.349 *    0.814 =     28.757
Qp =    222.806

Total of 2 streams to confluence:
Flow rates before confluence point:
     194.049      35.349
Area of streams before confluence:
      102.510       15.380
Results of confluence:
Total flow rate =    222.806(CFS)
Time of concentration =    21.306 min.
Effective stream area after confluence =    117.890(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      523.000 to Point/Station      508.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1380.000(Ft.)
End of natural channel elevation =   1369.000(Ft.)
Length of natural channel  =   547.000(Ft.)
Estimated mean flow rate at midpoint of channel =    226.378(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =   8.64(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0201
Corrected/adjusted channel slope =  0.0201
Travel time =    1.05 min.     TC =   22.36  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
```

```
Runoff Coefficient = 0.817
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      2.129(In/Hr) for a   100.0 year storm
Subarea runoff =      6.574(CFS) for      3.780(Ac.)
Total runoff =    229.381(CFS)       Total area =     121.670(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      508.000 to Point/Station      508.000
**** CONFLUENCE OF MAIN STREAMS ****
______________________________________________________________________________
The following data inside Main Stream is listed:
In Main Stream number: 2
Stream flow area =    121.670(Ac.)
Runoff from this stream =    229.381(CFS)
Time of concentration =   22.36 min.
Rainfall intensity =     2.129(In/Hr)
Summary of stream data:

Stream   Flow rate      TC            Rainfall Intensity
 No.       (CFS)       (min)                 (In/Hr)


1      345.292     32.96               1.754
2      229.381     22.36               2.129
Largest stream flow has longer time of concentration
Qp =    345.292 + sum of
          Qb         Ia/Ib
         229.381 *    0.824 =    188.943
Qp =    534.235

Total of 2 main streams to confluence:
Flow rates before confluence point:
     345.292     229.381
Area of streams before confluence:
      224.590      121.670


Results of confluence:
Total flow rate =    534.235(CFS)
Time of concentration =    32.956 min.
Effective stream area after confluence  =    346.260(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      508.000 to Point/Station      527.000
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
______________________________________________________________________________
Top of natural channel elevation =   1369.000(Ft.)
End of natural channel elevation =   1354.000(Ft.)
Length of natural channel  =   336.000(Ft.)
Estimated mean flow rate at midpoint of channel =    545.760(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  17.02(Ft/s)

Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
       Normal channel slope =  0.0446
Corrected/adjusted channel slope =  0.0446
Travel time =    0.33 min.     TC =   33.29  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.800
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.000
Decimal fraction soil group C = 1.000
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  86.00
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.745(In/Hr) for a   100.0 year storm
Subarea runoff =     20.873(CFS) for     14.940(Ac.)
Total runoff =    555.108(CFS)       Total area =     361.200(Ac.)


++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station      527.000 to Point/Station      528.000
```

```
**** NATURAL CHANNEL TIME + SUBAREA FLOW ADDITION ****
------------------------------------------------------------------------
Top of natural channel elevation =   1354.000(Ft.)
End of natural channel elevation =   1286.000(Ft.)
Length of natural channel  =  2132.000(Ft.)
Estimated mean flow rate at midpoint of channel =    600.391(CFS)

Natural valley channel type used
L.A. County flood control district formula for channel velocity:
 Velocity(ft/s) = (7 + 8(q(English Units)^.352)(slope^0.5)
Velocity using mean channel flow =  14.83(Ft/s)

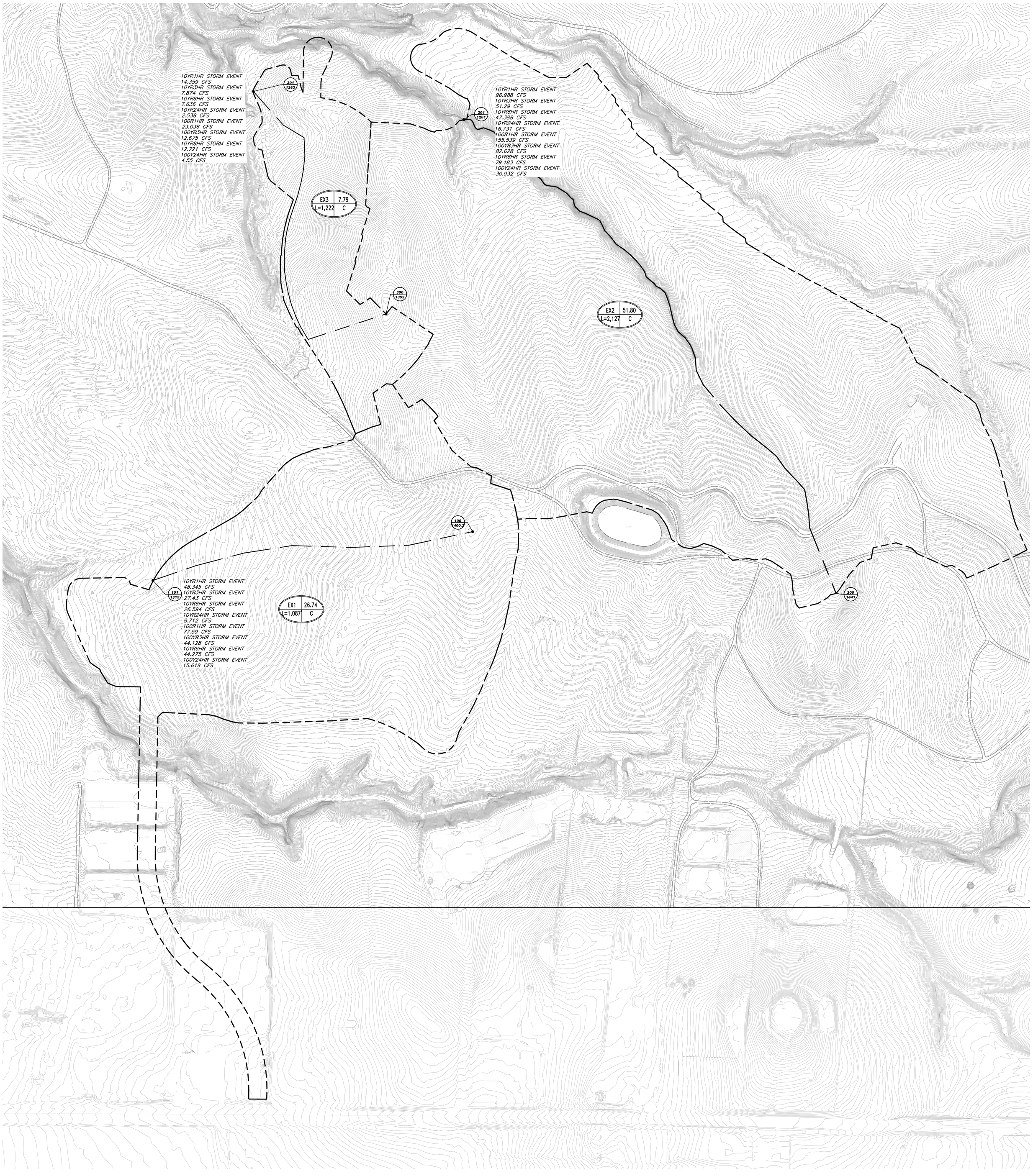
Correction to map slope used on extremely rugged channels with
drops and waterfalls (Plate D-6.2)
        Normal channel slope =  0.0319
Corrected/adjusted channel slope =  0.0319
Travel time =    2.40 min.     TC =   35.68  min.


 Adding area flow to channel
UNDEVELOPED (poor cover) subarea
Runoff Coefficient = 0.785
Decimal fraction soil group A = 0.000
Decimal fraction soil group B = 0.200
Decimal fraction soil group C = 0.800
Decimal fraction soil group D = 0.000
RI index for soil(AMC 2)  =  84.40
Pervious area fraction =  1.000; Impervious fraction =  0.000
Rainfall intensity =      1.686(In/Hr) for a   100.0 year storm
Subarea runoff =     78.005(CFS) for     58.930(Ac.)
Total runoff =    633.113(CFS)       Total area =     420.130(Ac.)
End of computations, total study area =          420.13 (Ac.)
The following figures may
be used for a unit hydrograph study of the same area.

Area averaged pervious area fraction(Ap) = 1.000
Area averaged RI index number =  85.5
```

Appendix C – Existing Synthetic Unit Hydrograph Method

EXISTING UNIT HYDROGRAPH MAP



0 100 300
50 200 400
SCALE: 1" = 100'

LEGEND

NODE ELEV

AREA | ACRES
LENGTH | SOIL

WATERSHED BOUNDARY

FLOW PATH

EXISTING UNIT HYDROGRAPH MAP
PREPARATION DATE: DECEMBER 2022
REVISION DATE: MAY 2024

PLAN PREPARED BY:
adkan ENGINEERS
Civil Engineering • Surveying • Planning
6879 Airport Drive, Riverside, CA 92504
Tel:(951) 688-0241 • Fax:(951) 688-0599

Extended Detention Basin No. 1

```
        U n i t   H y d r o g r a p h   A n a l y s i s

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                Study date  04/22/24 File: EX1212.out

++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      26.74(Ac.)  =      0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      26.74(Ac.)  =      0.042 Sq. Mi.
Length along longest watercourse =    1087.00(Ft.)
Length along longest watercourse measured to centroid =     544.00(Ft.)
Length along longest watercourse =      0.206 Mi.
Length along longest watercourse measured to centroid =      0.103 Mi.
Difference in elevation =      88.30(Ft.)
Slope along watercourse =    428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.053 Hr.
Lag time =     3.16 Min.
25% of lag time =     0.79 Min.
40% of lag time =     1.26 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           0.50                 13.37

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           1.30                 34.76

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.500(In)
Areal adjustment factor =   99.98 %
Adjusted average point rain =    0.500(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    26.740           91.00          0.000
 Total Area Entered =     26.74(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000 Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.198	(0.246) 0.178	0.020
2	0.17	4.20	0.252	(0.246) 0.227	0.025
3	0.25	4.40	0.264	(0.246) 0.238	0.026
4	0.33	4.80	0.288	0.246 (0.259)	0.042
5	0.42	5.20	0.312	0.246 (0.281)	0.066
6	0.50	6.20	0.372	0.246 (0.335)	0.126
7	0.58	6.80	0.408	0.246 (0.367)	0.162
8	0.67	8.80	0.528	0.246 (0.475)	0.282
9	0.75	13.90	0.834	0.246 (0.750)	0.587
10	0.83	31.40	1.884	0.246 (1.695)	1.637
11	0.92	7.20	0.432	0.246 (0.389)	0.186
12	1.00	3.80	0.228	(0.246) 0.205	0.023
		(Loss Rate Not Used)			
Sum =		100.0		Sum =	3.2

Flood volume = Effective rainfall 0.27(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 0.6(Ac.Ft)
Total soil loss = 0.23(In)
Total soil loss = 0.523(Ac.Ft)
Total rainfall = 0.50(In)
Flood volume = 25723.1 Cubic Feet
Total soil loss = 22798.2 Cubic Feet

Peak flow rate of this hydrograph = 24.414(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0013	0.19	Q				
0+10	0.0046	0.49	Q				
0+15	0.0089	0.62	Q				
0+20	0.0146	0.82	VQ				
0+25	0.0233	1.26	|Q				
0+30	0.0383	2.18	| Q				
0+35	0.0615	3.36	| Q				
0+40	0.0970	5.16	| Q				
0+45	0.1642	9.76	|	V Q			
0+50	0.3293	23.96	|	|	V	Q	
0+55	0.4974	24.41	|	|	|	QV	
1+ 0	0.5540	8.21	|	Q	|	|	V |
1+ 5	0.5766	3.29	| Q	|	|	|	V|
1+10	0.5864	1.43	|Q	|	|	|	V|
1+15	0.5901	0.53	Q	|	|	|	V|
1+20	0.5905	0.06	Q	|	|	|	V|
1+25	0.5905	0.01	Q	|	|	|	V

```
        U n i t   H y d r o g r a p h   A n a l y s i s

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                Study date  04/22/24 File: EX1232.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      26.74(Ac.)  =      0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      26.74(Ac.)  =      0.042 Sq. Mi.
Length along longest watercourse =    1087.00(Ft.)
Length along longest watercourse measured to centroid =     544.00(Ft.)
Length along longest watercourse =      0.206 Mi.
Length along longest watercourse measured to centroid =      0.103 Mi.
Difference in elevation =      88.30(Ft.)
Slope along watercourse =    428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.053 Hr.
Lag time =     3.16 Min.
25% of lag time =     0.79 Min.
40% of lag time =     1.26 Min.
Unit time =     5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74            0.80                 21.39

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74            2.00                 53.48

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    0.800(In)
Area Averaged 100-Year Rainfall =    2.000(In)

Point rain (area averaged) =    0.800(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    0.800(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    26.740           91.00          0.000
 Total Area Entered =     26.74(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.125	(0.246)	0.112	0.012
2	0.17	1.30	0.125	(0.246)	0.112	0.012
3	0.25	1.10	0.106	(0.246)	0.095	0.011
4	0.33	1.50	0.144	(0.246)	0.130	0.014
5	0.42	1.50	0.144	(0.246)	0.130	0.014
6	0.50	1.80	0.173	(0.246)	0.156	0.017
7	0.58	1.50	0.144	(0.246)	0.130	0.014
8	0.67	1.80	0.173	(0.246)	0.156	0.017
9	0.75	1.80	0.173	(0.246)	0.156	0.017
10	0.83	1.50	0.144	(0.246)	0.130	0.014
11	0.92	1.60	0.154	(0.246)	0.138	0.015
12	1.00	1.80	0.173	(0.246)	0.156	0.017
13	1.08	2.20	0.211	(0.246)	0.190	0.021
14	1.17	2.20	0.211	(0.246)	0.190	0.021
15	1.25	2.20	0.211	(0.246)	0.190	0.021
16	1.33	2.00	0.192	(0.246)	0.173	0.019
17	1.42	2.60	0.250	(0.246)	0.225	0.025
18	1.50	2.70	0.259	(0.246)	0.233	0.026
19	1.58	2.40	0.230	(0.246)	0.207	0.023
20	1.67	2.70	0.259	(0.246)	0.233	0.026
21	1.75	3.30	0.317	0.246	(0.285)	0.070
22	1.83	3.10	0.298	0.246	(0.268)	0.051
23	1.92	2.90	0.278	0.246	(0.251)	0.032
24	2.00	3.00	0.288	0.246	(0.259)	0.042
25	2.08	3.10	0.298	0.246	(0.268)	0.051
26	2.17	4.20	0.403	0.246	(0.363)	0.157
27	2.25	5.00	0.480	0.246	(0.432)	0.234
28	2.33	3.50	0.336	0.246	(0.302)	0.090
29	2.42	6.80	0.653	0.246	(0.587)	0.406
30	2.50	7.30	0.701	0.246	(0.631)	0.454
31	2.58	8.20	0.787	0.246	(0.708)	0.541
32	2.67	5.90	0.566	0.246	(0.510)	0.320
33	2.75	2.00	0.192	(0.246)	0.173	0.019
34	2.83	1.80	0.173	(0.246)	0.156	0.017
35	2.92	1.80	0.173	(0.246)	0.156	0.017
36	3.00	0.60	0.058	(0.246)	0.052	0.006
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	2.9

Flood volume = Effective rainfall 0.24(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 0.5(Ac.Ft)
Total soil loss = 0.56(In)
Total soil loss = 1.250(Ac.Ft)
Total rainfall = 0.80(In)
Flood volume = 23193.3 Cubic Feet
Total soil loss = 54450.6 Cubic Feet

Peak flow rate of this hydrograph = 12.271(CFS)

++

3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0008	0.12	Q	|	|	|	|
0+10	0.0027	0.27	Q	|	|	|	|
0+15	0.0047	0.29	Q	|	|	|	|
0+20	0.0069	0.32	Q	|	|	|	|
0+25	0.0095	0.37	Q	|	|	|	|
0+30	0.0123	0.41	Q	|	|	|	|
0+35	0.0152	0.42	QV	|	|	|	|
0+40	0.0181	0.42	QV	|	|	|	|
0+45	0.0212	0.46	QV	|	|	|	|
0+50	0.0242	0.43	QV	|	|	|	|
0+55	0.0271	0.41	Q V	|	|	|	|
1+ 0	0.0300	0.43	Q V	|	|	|	|
1+ 5	0.0334	0.49	Q V	|	|	|	|

```
    1+10       0.0372      0.55  |QV        |          |          |          |
    1+15       0.0410      0.56  |Q V       |          |          |          |
    1+20       0.0448      0.55  |Q V       |          |          |          |
    1+25       0.0488      0.58  |Q V       |          |          |          |
    1+30       0.0533      0.66  |Q  V      |          |          |          |
    1+35       0.0579      0.66  |Q  V      |          |          |          |
    1+40       0.0624      0.66  |Q  V      |          |          |          |
    1+45       0.0700      1.11  | Q  V     |          |          |          |
    1+50       0.0803      1.49  | Q   V    |          |          |          |
    1+55       0.0886      1.20  | Q   V    |          |          |          |
    2+ 0       0.0958      1.05  | Q    V   |          |          |          |
    2+ 5       0.1041      1.21  | Q    V   |          |          |          |
    2+10       0.1202      2.33  |   Q    V |          |          |          |
    2+15       0.1505      4.41  |       Q |V         |          |          |
    2+20       0.1803      4.32  |       Q |  V       |          |          |
    2+25       0.2208      5.88  |         |Q    V    |          |          |
    2+30       0.2900     10.04  |         |         QV          |          |
    2+35       0.3745     12.27  |         |          |   Q   V  |          |
    2+40       0.4552     11.73  |         |          |  Q       |   V      |
    2+45       0.5006      6.58  |         |  Q       |          |     V    |
    2+50       0.5169      2.38  |   Q     |          |          |       V  |
    2+55       0.5257      1.27  | Q       |          |          |         V|
    3+ 0       0.5303      0.67  |Q        |          |          |         V|
    3+ 5       0.5319      0.23  Q         |          |          |         V|
    3+10       0.5322      0.05  Q         |          |          |         V|
    3+15       0.5324      0.02  Q         |          |          |         V|
    3+20       0.5324      0.01  Q         |          |          |         V|
    3+25       0.5324      0.00  Q         |          |          |          V
-------------------------------------------------------------------------
```

```
        U n i t   H y d r o g r a p h   A n a l y s i s

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               Study date  04/22/24 File: EX1262.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      26.74(Ac.)  =      0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      26.74(Ac.)  =      0.042 Sq. Mi.
Length along longest watercourse =    1087.00(Ft.)
Length along longest watercourse measured to centroid =     544.00(Ft.)
Length along longest watercourse =      0.206 Mi.
Length along longest watercourse measured to centroid =      0.103 Mi.
Difference in elevation =      88.30(Ft.)
Slope along watercourse =    428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.053 Hr.
Lag time =     3.16 Min.
25% of lag time =     0.79 Min.
40% of lag time =     1.26 Min.
Unit time =     5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           1.10                 29.41

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           3.00                 80.22

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    1.100(In)
Area Averaged 100-Year Rainfall =    3.000(In)

Point rain (area averaged) =    1.100(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    1.100(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    26.740           91.00          0.000
 Total Area Entered =     26.74(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.066	(0.246)	0.059	0.007
2	0.17	0.60	0.079	(0.246)	0.071	0.008
3	0.25	0.60	0.079	(0.246)	0.071	0.008
4	0.33	0.60	0.079	(0.246)	0.071	0.008
5	0.42	0.60	0.079	(0.246)	0.071	0.008
6	0.50	0.70	0.092	(0.246)	0.083	0.009
7	0.58	0.70	0.092	(0.246)	0.083	0.009
8	0.67	0.70	0.092	(0.246)	0.083	0.009
9	0.75	0.70	0.092	(0.246)	0.083	0.009
10	0.83	0.70	0.092	(0.246)	0.083	0.009
11	0.92	0.70	0.092	(0.246)	0.083	0.009
12	1.00	0.80	0.106	(0.246)	0.095	0.011
13	1.08	0.80	0.106	(0.246)	0.095	0.011
14	1.17	0.80	0.106	(0.246)	0.095	0.011
15	1.25	0.80	0.106	(0.246)	0.095	0.011
16	1.33	0.80	0.106	(0.246)	0.095	0.011
17	1.42	0.80	0.106	(0.246)	0.095	0.011
18	1.50	0.80	0.106	(0.246)	0.095	0.011
19	1.58	0.80	0.106	(0.246)	0.095	0.011
20	1.67	0.80	0.106	(0.246)	0.095	0.011
21	1.75	0.80	0.106	(0.246)	0.095	0.011
22	1.83	0.80	0.106	(0.246)	0.095	0.011
23	1.92	0.80	0.106	(0.246)	0.095	0.011
24	2.00	0.90	0.119	(0.246)	0.107	0.012
25	2.08	0.80	0.106	(0.246)	0.095	0.011
26	2.17	0.90	0.119	(0.246)	0.107	0.012
27	2.25	0.90	0.119	(0.246)	0.107	0.012
28	2.33	0.90	0.119	(0.246)	0.107	0.012
29	2.42	0.90	0.119	(0.246)	0.107	0.012
30	2.50	0.90	0.119	(0.246)	0.107	0.012
31	2.58	0.90	0.119	(0.246)	0.107	0.012
32	2.67	0.90	0.119	(0.246)	0.107	0.012
33	2.75	1.00	0.132	(0.246)	0.119	0.013
34	2.83	1.00	0.132	(0.246)	0.119	0.013
35	2.92	1.00	0.132	(0.246)	0.119	0.013
36	3.00	1.00	0.132	(0.246)	0.119	0.013
37	3.08	1.00	0.132	(0.246)	0.119	0.013
38	3.17	1.10	0.145	(0.246)	0.131	0.015
39	3.25	1.10	0.145	(0.246)	0.131	0.015
40	3.33	1.10	0.145	(0.246)	0.131	0.015
41	3.42	1.20	0.158	(0.246)	0.143	0.016
42	3.50	1.30	0.172	(0.246)	0.154	0.017
43	3.58	1.40	0.185	(0.246)	0.166	0.018
44	3.67	1.40	0.185	(0.246)	0.166	0.018
45	3.75	1.50	0.198	(0.246)	0.178	0.020
46	3.83	1.50	0.198	(0.246)	0.178	0.020
47	3.92	1.60	0.211	(0.246)	0.190	0.021
48	4.00	1.60	0.211	(0.246)	0.190	0.021
49	4.08	1.70	0.224	(0.246)	0.202	0.022
50	4.17	1.80	0.238	(0.246)	0.214	0.024
51	4.25	1.90	0.251	(0.246)	0.226	0.025
52	4.33	2.00	0.264	(0.246)	0.238	0.026
53	4.42	2.10	0.277	0.246	(0.249)	0.031
54	4.50	2.10	0.277	0.246	(0.249)	0.031
55	4.58	2.20	0.290	0.246	(0.261)	0.044
56	4.67	2.30	0.304	0.246	(0.273)	0.057
57	4.75	2.40	0.317	0.246	(0.285)	0.070
58	4.83	2.40	0.317	0.246	(0.285)	0.070
59	4.92	2.50	0.330	0.246	(0.297)	0.084
60	5.00	2.60	0.343	0.246	(0.309)	0.097
61	5.08	3.10	0.409	0.246	(0.368)	0.163
62	5.17	3.60	0.475	0.246	(0.428)	0.229
63	5.25	3.90	0.515	0.246	(0.463)	0.268
64	5.33	4.20	0.554	0.246	(0.499)	0.308
65	5.42	4.70	0.620	0.246	(0.558)	0.374
66	5.50	5.60	0.739	0.246	(0.665)	0.493
67	5.58	1.90	0.251	(0.246)	0.226	0.025
68	5.67	0.90	0.119	(0.246)	0.107	0.012
69	5.75	0.60	0.079	(0.246)	0.071	0.008
70	5.83	0.50	0.066	(0.246)	0.059	0.007

```
71   5.92     0.30      0.040       (  0.246)       0.036        0.004
72   6.00     0.20      0.026       (  0.246)       0.024        0.003
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =     3.1
      Flood volume = Effective rainfall      0.26(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       0.6(Ac.Ft)
      Total soil loss =      0.84(In)
      Total soil loss =     1.882(Ac.Ft)
      Total rainfall =      1.10(In)
      Flood volume =       24767.4 Cubic Feet
      Total soil loss =       81995.6 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     10.748(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
-------------------------------------------------------------------------
  0+ 5       0.0004      0.06  Q         |         |         |         |
  0+10       0.0015      0.16  Q         |         |         |         |
  0+15       0.0028      0.19  Q         |         |         |         |
  0+20       0.0043      0.21  Q         |         |         |         |
  0+25       0.0057      0.21  Q         |         |         |         |
  0+30       0.0073      0.23  Q         |         |         |         |
  0+35       0.0089      0.24  Q         |         |         |         |
  0+40       0.0106      0.25  Q         |         |         |         |
  0+45       0.0123      0.25  Q         |         |         |         |
  0+50       0.0141      0.25  Q         |         |         |         |
  0+55       0.0158      0.25  QV        |         |         |         |
  1+ 0       0.0176      0.26  QV        |         |         |         |
  1+ 5       0.0195      0.28  QV        |         |         |         |
  1+10       0.0214      0.28  QV        |         |         |         |
  1+15       0.0234      0.28  QV        |         |         |         |
  1+20       0.0253      0.28  QV        |         |         |         |
  1+25       0.0273      0.28  QV        |         |         |         |
  1+30       0.0293      0.28  Q V       |         |         |         |
  1+35       0.0312      0.28  Q V       |         |         |         |
  1+40       0.0332      0.28  Q V       |         |         |         |
  1+45       0.0351      0.28  Q V       |         |         |         |
  1+50       0.0371      0.28  Q V       |         |         |         |
  1+55       0.0391      0.28  Q V       |         |         |         |
  2+ 0       0.0411      0.30  Q V       |         |         |         |
  2+ 5       0.0432      0.30  Q  V      |         |         |         |
  2+10       0.0453      0.30  Q  V      |         |         |         |
  2+15       0.0474      0.32  Q  V      |         |         |         |
  2+20       0.0496      0.32  Q  V      |         |         |         |
  2+25       0.0518      0.32  Q  V      |         |         |         |
  2+30       0.0540      0.32  Q  V      |         |         |         |
  2+35       0.0562      0.32  Q  V      |         |         |         |
  2+40       0.0584      0.32  Q   V     |         |         |         |
  2+45       0.0607      0.33  Q   V     |         |         |         |
  2+50       0.0631      0.35  Q   V     |         |         |         |
  2+55       0.0656      0.35  Q   V     |         |         |         |
  3+ 0       0.0680      0.35  Q   V     |         |         |         |
  3+ 5       0.0705      0.36  Q   V     |         |         |         |
  3+10       0.0730      0.37  Q    V    |         |         |         |
  3+15       0.0756      0.38  Q    V    |         |         |         |
  3+20       0.0783      0.39  Q    V    |         |         |         |
  3+25       0.0811      0.40  Q    V    |         |         |         |
  3+30       0.0841      0.43  Q    V    |         |         |         |
  3+35       0.0873      0.47  Q     V   |         |         |         |
  3+40       0.0906      0.49  Q     V   |         |         |         |
  3+45       0.0941      0.51  |Q    V   |         |         |         |
  3+50       0.0978      0.53  |Q    V   |         |         |         |
  3+55       0.1015      0.54  |Q     V  |         |         |         |
  4+ 0       0.1054      0.56  |Q     V  |         |         |         |
  4+ 5       0.1094      0.58  |Q     V  |         |         |         |
  4+10       0.1136      0.61  |Q     V  |         |         |         |
  4+15       0.1180      0.64  |Q      V |         |         |         |
  4+20       0.1227      0.68  |Q      V |         |         |         |
  4+25       0.1278      0.74  |Q      V |         |         |         |
  4+30       0.1333      0.80  |Q       V|         |         |         |
  4+35       0.1398      0.95  |Q       V|         |         |         |
  4+40       0.1484      1.24  | Q       V         |         |         |
  4+45       0.1592      1.57  |  Q      |V        |         |         |
  4+50       0.1716      1.79  |  Q      | V       |         |         |
  4+55       0.1852      1.98  |  Q      |  V      |         |         |
  5+ 0       0.2011      2.30  |   Q     |   V     |         |         |
  5+ 5       0.2227      3.14  |     Q   |    V    |         |         |
  5+10       0.2547      4.65  |       Q |      V  |         |         |
  5+15       0.2964      6.06  |         | Q       V         |         |
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    5+20       0.3461      7.22  |          |   Q      |   V      |          |
    5+25       0.4052      8.58  |          |      Q   |        V |          |
    5+30       0.4792     10.75  |          |          |Q         |  V       |
    5+35       0.5349      8.08  |          |      Q   |          |      V   |
    5+40       0.5526      2.57  |    Q     |          |          |        V |
    5+45       0.5609      1.21  | Q        |          |          |          V|
    5+50       0.5652      0.61  |Q         |          |          |          V|
    5+55       0.5672      0.29  Q          |          |          |          V|
    6+ 0       0.5680      0.12  Q          |          |          |          V|
    6+ 5       0.5684      0.06  Q          |          |          |          V|
    6+10       0.5685      0.02  Q          |          |          |          V|
    6+15       0.5686      0.01  Q          |          |          |          V|
    6+20       0.5686      0.00  Q          |          |          |          V|
    6+25       0.5686      0.00  Q          |          |          |          V|
-------------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX12242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 1087.00(Ft.)
Length along longest watercourse measured to centroid = 544.00(Ft.)
Length along longest watercourse = 0.206 Mi.
Length along longest watercourse measured to centroid = 0.103 Mi.
Difference in elevation = 88.30(Ft.)
Slope along watercourse = 428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.80	48.13

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	5.00	133.70

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 1.800(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.800(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.000

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.014	(0.437)	0.013	0.001
2	0.17	0.07	0.014	(0.435)	0.013	0.001
3	0.25	0.07	0.014	(0.433)	0.013	0.001
4	0.33	0.10	0.022	(0.432)	0.019	0.002
5	0.42	0.10	0.022	(0.430)	0.019	0.002
6	0.50	0.10	0.022	(0.428)	0.019	0.002
7	0.58	0.10	0.022	(0.427)	0.019	0.002
8	0.67	0.10	0.022	(0.425)	0.019	0.002
9	0.75	0.10	0.022	(0.423)	0.019	0.002
10	0.83	0.13	0.029	(0.422)	0.026	0.003
11	0.92	0.13	0.029	(0.420)	0.026	0.003
12	1.00	0.13	0.029	(0.418)	0.026	0.003
13	1.08	0.10	0.022	(0.417)	0.019	0.002
14	1.17	0.10	0.022	(0.415)	0.019	0.002
15	1.25	0.10	0.022	(0.413)	0.019	0.002
16	1.33	0.10	0.022	(0.412)	0.019	0.002
17	1.42	0.10	0.022	(0.410)	0.019	0.002
18	1.50	0.10	0.022	(0.408)	0.019	0.002
19	1.58	0.10	0.022	(0.407)	0.019	0.002
20	1.67	0.10	0.022	(0.405)	0.019	0.002
21	1.75	0.10	0.022	(0.404)	0.019	0.002
22	1.83	0.13	0.029	(0.402)	0.026	0.003
23	1.92	0.13	0.029	(0.400)	0.026	0.003
24	2.00	0.13	0.029	(0.399)	0.026	0.003
25	2.08	0.13	0.029	(0.397)	0.026	0.003
26	2.17	0.13	0.029	(0.395)	0.026	0.003
27	2.25	0.13	0.029	(0.394)	0.026	0.003
28	2.33	0.13	0.029	(0.392)	0.026	0.003
29	2.42	0.13	0.029	(0.391)	0.026	0.003
30	2.50	0.13	0.029	(0.389)	0.026	0.003
31	2.58	0.17	0.036	(0.387)	0.032	0.004
32	2.67	0.17	0.036	(0.386)	0.032	0.004
33	2.75	0.17	0.036	(0.384)	0.032	0.004
34	2.83	0.17	0.036	(0.383)	0.032	0.004
35	2.92	0.17	0.036	(0.381)	0.032	0.004
36	3.00	0.17	0.036	(0.380)	0.032	0.004
37	3.08	0.17	0.036	(0.378)	0.032	0.004
38	3.17	0.17	0.036	(0.376)	0.032	0.004
39	3.25	0.17	0.036	(0.375)	0.032	0.004
40	3.33	0.17	0.036	(0.373)	0.032	0.004
41	3.42	0.17	0.036	(0.372)	0.032	0.004
42	3.50	0.17	0.036	(0.370)	0.032	0.004
43	3.58	0.17	0.036	(0.369)	0.032	0.004
44	3.67	0.17	0.036	(0.367)	0.032	0.004
45	3.75	0.17	0.036	(0.366)	0.032	0.004
46	3.83	0.20	0.043	(0.364)	0.039	0.004
47	3.92	0.20	0.043	(0.362)	0.039	0.004
48	4.00	0.20	0.043	(0.361)	0.039	0.004
49	4.08	0.20	0.043	(0.359)	0.039	0.004
50	4.17	0.20	0.043	(0.358)	0.039	0.004
51	4.25	0.20	0.043	(0.356)	0.039	0.004
52	4.33	0.23	0.050	(0.355)	0.045	0.005
53	4.42	0.23	0.050	(0.353)	0.045	0.005
54	4.50	0.23	0.050	(0.352)	0.045	0.005
55	4.58	0.23	0.050	(0.350)	0.045	0.005
56	4.67	0.23	0.050	(0.349)	0.045	0.005
57	4.75	0.23	0.050	(0.347)	0.045	0.005
58	4.83	0.27	0.058	(0.346)	0.052	0.006
59	4.92	0.27	0.058	(0.344)	0.052	0.006
60	5.00	0.27	0.058	(0.343)	0.052	0.006
61	5.08	0.20	0.043	(0.341)	0.039	0.004
62	5.17	0.20	0.043	(0.340)	0.039	0.004
63	5.25	0.20	0.043	(0.338)	0.039	0.004
64	5.33	0.23	0.050	(0.337)	0.045	0.005
65	5.42	0.23	0.050	(0.335)	0.045	0.005
66	5.50	0.23	0.050	(0.334)	0.045	0.005
67	5.58	0.27	0.058	(0.332)	0.052	0.006
68	5.67	0.27	0.058	(0.331)	0.052	0.006
69	5.75	0.27	0.058	(0.330)	0.052	0.006
70	5.83	0.27	0.058	(0.328)	0.052	0.006

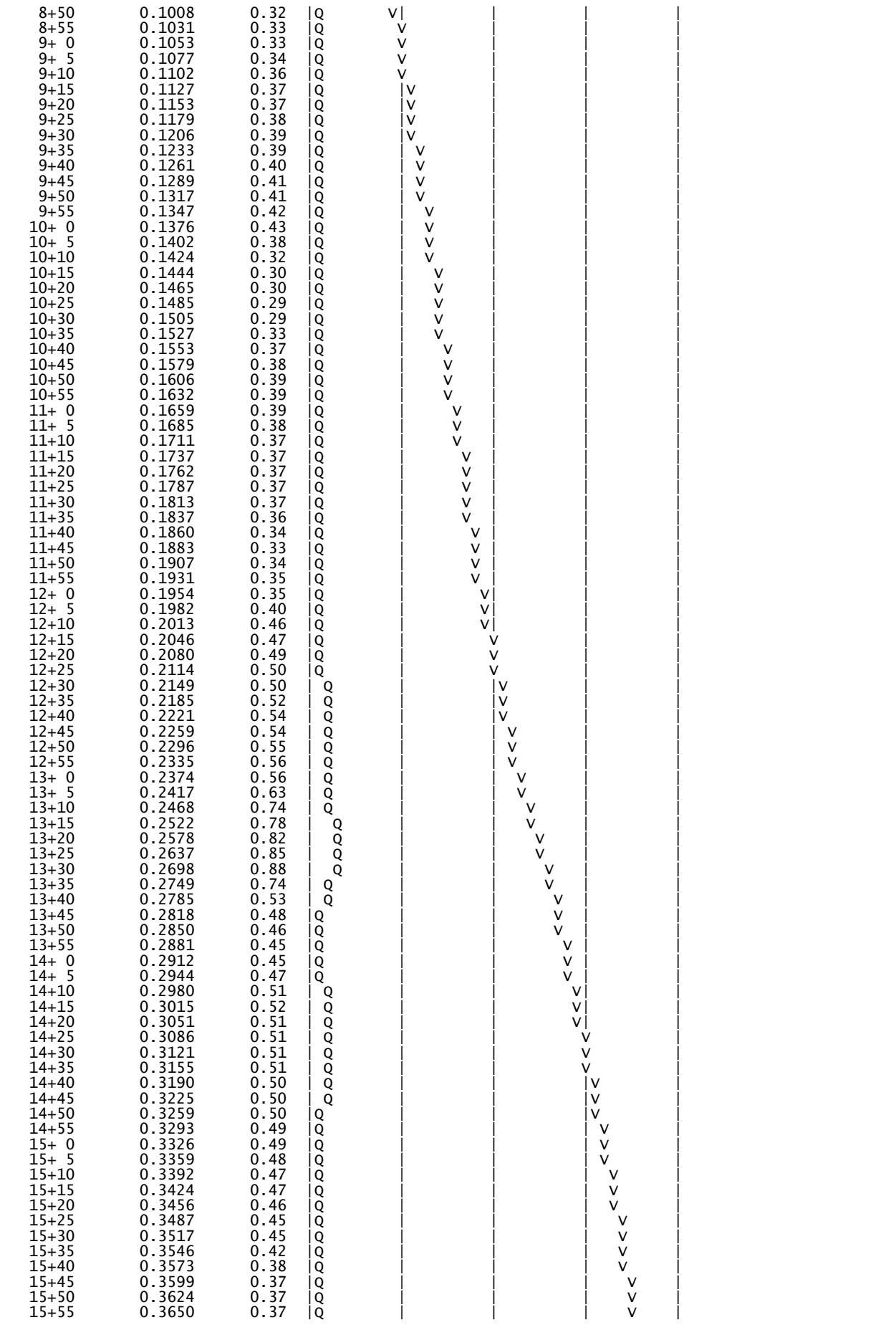
71	5.92	0.27	0.058	(0.327)	0.052	0.006
72	6.00	0.27	0.058	(0.325)	0.052	0.006
73	6.08	0.30	0.065	(0.324)	0.058	0.006
74	6.17	0.30	0.065	(0.322)	0.058	0.006
75	6.25	0.30	0.065	(0.321)	0.058	0.006
76	6.33	0.30	0.065	(0.319)	0.058	0.006
77	6.42	0.30	0.065	(0.318)	0.058	0.006
78	6.50	0.30	0.065	(0.317)	0.058	0.006
79	6.58	0.33	0.072	(0.315)	0.065	0.007
80	6.67	0.33	0.072	(0.314)	0.065	0.007
81	6.75	0.33	0.072	(0.312)	0.065	0.007
82	6.83	0.33	0.072	(0.311)	0.065	0.007
83	6.92	0.33	0.072	(0.310)	0.065	0.007
84	7.00	0.33	0.072	(0.308)	0.065	0.007
85	7.08	0.33	0.072	(0.307)	0.065	0.007
86	7.17	0.33	0.072	(0.305)	0.065	0.007
87	7.25	0.33	0.072	(0.304)	0.065	0.007
88	7.33	0.37	0.079	(0.303)	0.071	0.008
89	7.42	0.37	0.079	(0.301)	0.071	0.008
90	7.50	0.37	0.079	(0.300)	0.071	0.008
91	7.58	0.40	0.086	(0.298)	0.078	0.009
92	7.67	0.40	0.086	(0.297)	0.078	0.009
93	7.75	0.40	0.086	(0.296)	0.078	0.009
94	7.83	0.43	0.094	(0.294)	0.084	0.009
95	7.92	0.43	0.094	(0.293)	0.084	0.009
96	8.00	0.43	0.094	(0.292)	0.084	0.009
97	8.08	0.50	0.108	(0.290)	0.097	0.011
98	8.17	0.50	0.108	(0.289)	0.097	0.011
99	8.25	0.50	0.108	(0.288)	0.097	0.011
100	8.33	0.50	0.108	(0.286)	0.097	0.011
101	8.42	0.50	0.108	(0.285)	0.097	0.011
102	8.50	0.50	0.108	(0.283)	0.097	0.011
103	8.58	0.53	0.115	(0.282)	0.104	0.012
104	8.67	0.53	0.115	(0.281)	0.104	0.012
105	8.75	0.53	0.115	(0.280)	0.104	0.012
106	8.83	0.57	0.122	(0.278)	0.110	0.012
107	8.92	0.57	0.122	(0.277)	0.110	0.012
108	9.00	0.57	0.122	(0.276)	0.110	0.012
109	9.08	0.63	0.137	(0.274)	0.123	0.014
110	9.17	0.63	0.137	(0.273)	0.123	0.014
111	9.25	0.63	0.137	(0.272)	0.123	0.014
112	9.33	0.67	0.144	(0.270)	0.130	0.014
113	9.42	0.67	0.144	(0.269)	0.130	0.014
114	9.50	0.67	0.144	(0.268)	0.130	0.014
115	9.58	0.70	0.151	(0.267)	0.136	0.015
116	9.67	0.70	0.151	(0.265)	0.136	0.015
117	9.75	0.70	0.151	(0.264)	0.136	0.015
118	9.83	0.73	0.158	(0.263)	0.143	0.016
119	9.92	0.73	0.158	(0.261)	0.143	0.016
120	10.00	0.73	0.158	(0.260)	0.143	0.016
121	10.08	0.50	0.108	(0.259)	0.097	0.011
122	10.17	0.50	0.108	(0.258)	0.097	0.011
123	10.25	0.50	0.108	(0.256)	0.097	0.011
124	10.33	0.50	0.108	(0.255)	0.097	0.011
125	10.42	0.50	0.108	(0.254)	0.097	0.011
126	10.50	0.50	0.108	(0.253)	0.097	0.011
127	10.58	0.67	0.144	(0.251)	0.130	0.014
128	10.67	0.67	0.144	(0.250)	0.130	0.014
129	10.75	0.67	0.144	(0.249)	0.130	0.014
130	10.83	0.67	0.144	(0.248)	0.130	0.014
131	10.92	0.67	0.144	(0.247)	0.130	0.014
132	11.00	0.67	0.144	(0.245)	0.130	0.014
133	11.08	0.63	0.137	(0.244)	0.123	0.014
134	11.17	0.63	0.137	(0.243)	0.123	0.014
135	11.25	0.63	0.137	(0.242)	0.123	0.014
136	11.33	0.63	0.137	(0.241)	0.123	0.014
137	11.42	0.63	0.137	(0.239)	0.123	0.014
138	11.50	0.63	0.137	(0.238)	0.123	0.014
139	11.58	0.57	0.122	(0.237)	0.110	0.012
140	11.67	0.57	0.122	(0.236)	0.110	0.012
141	11.75	0.57	0.122	(0.235)	0.110	0.012
142	11.83	0.60	0.130	(0.233)	0.117	0.013
143	11.92	0.60	0.130	(0.232)	0.117	0.013
144	12.00	0.60	0.130	(0.231)	0.117	0.013
145	12.08	0.83	0.180	(0.230)	0.162	0.018
146	12.17	0.83	0.180	(0.229)	0.162	0.018
147	12.25	0.83	0.180	(0.228)	0.162	0.018
148	12.33	0.87	0.187	(0.227)	0.168	0.019
149	12.42	0.87	0.187	(0.225)	0.168	0.019
150	12.50	0.87	0.187	(0.224)	0.168	0.019
151	12.58	0.93	0.202	(0.223)	0.181	0.020
152	12.67	0.93	0.202	(0.222)	0.181	0.020
153	12.75	0.93	0.202	(0.221)	0.181	0.020
154	12.83	0.97	0.209	(0.220)	0.188	0.021
155	12.92	0.97	0.209	(0.219)	0.188	0.021
156	13.00	0.97	0.209	(0.218)	0.188	0.021

157	13.08	1.13	0.245	0.216	(0.220)	0.028
158	13.17	1.13	0.245	0.215	(0.220)	0.029
159	13.25	1.13	0.245	0.214	(0.220)	0.031
160	13.33	1.13	0.245	0.213	(0.220)	0.032
161	13.42	1.13	0.245	0.212	(0.220)	0.033
162	13.50	1.13	0.245	0.211	(0.220)	0.034
163	13.58	0.77	0.166	(0.210)	0.149	0.017
164	13.67	0.77	0.166	(0.209)	0.149	0.017
165	13.75	0.77	0.166	(0.208)	0.149	0.017
166	13.83	0.77	0.166	(0.207)	0.149	0.017
167	13.92	0.77	0.166	(0.206)	0.149	0.017
168	14.00	0.77	0.166	(0.205)	0.149	0.017
169	14.08	0.90	0.194	(0.204)	0.175	0.019
170	14.17	0.90	0.194	(0.203)	0.175	0.019
171	14.25	0.90	0.194	(0.202)	0.175	0.019
172	14.33	0.87	0.187	(0.200)	0.168	0.019
173	14.42	0.87	0.187	(0.199)	0.168	0.019
174	14.50	0.87	0.187	(0.198)	0.168	0.019
175	14.58	0.87	0.187	(0.197)	0.168	0.019
176	14.67	0.87	0.187	(0.196)	0.168	0.019
177	14.75	0.87	0.187	(0.195)	0.168	0.019
178	14.83	0.83	0.180	(0.194)	0.162	0.018
179	14.92	0.83	0.180	(0.193)	0.162	0.018
180	15.00	0.83	0.180	(0.192)	0.162	0.018
181	15.08	0.80	0.173	(0.191)	0.156	0.017
182	15.17	0.80	0.173	(0.190)	0.156	0.017
183	15.25	0.80	0.173	(0.189)	0.156	0.017
184	15.33	0.77	0.166	(0.188)	0.149	0.017
185	15.42	0.77	0.166	(0.188)	0.149	0.017
186	15.50	0.77	0.166	(0.187)	0.149	0.017
187	15.58	0.63	0.137	(0.186)	0.123	0.014
188	15.67	0.63	0.137	(0.185)	0.123	0.014
189	15.75	0.63	0.137	(0.184)	0.123	0.014
190	15.83	0.63	0.137	(0.183)	0.123	0.014
191	15.92	0.63	0.137	(0.182)	0.123	0.014
192	16.00	0.63	0.137	(0.181)	0.123	0.014
193	16.08	0.13	0.029	(0.180)	0.026	0.003
194	16.17	0.13	0.029	(0.179)	0.026	0.003
195	16.25	0.13	0.029	(0.178)	0.026	0.003
196	16.33	0.13	0.029	(0.177)	0.026	0.003
197	16.42	0.13	0.029	(0.176)	0.026	0.003
198	16.50	0.13	0.029	(0.175)	0.026	0.003
199	16.58	0.10	0.022	(0.175)	0.019	0.002
200	16.67	0.10	0.022	(0.174)	0.019	0.002
201	16.75	0.10	0.022	(0.173)	0.019	0.002
202	16.83	0.10	0.022	(0.172)	0.019	0.002
203	16.92	0.10	0.022	(0.171)	0.019	0.002
204	17.00	0.10	0.022	(0.170)	0.019	0.002
205	17.08	0.17	0.036	(0.169)	0.032	0.004
206	17.17	0.17	0.036	(0.168)	0.032	0.004
207	17.25	0.17	0.036	(0.168)	0.032	0.004
208	17.33	0.17	0.036	(0.167)	0.032	0.004
209	17.42	0.17	0.036	(0.166)	0.032	0.004
210	17.50	0.17	0.036	(0.165)	0.032	0.004
211	17.58	0.17	0.036	(0.164)	0.032	0.004
212	17.67	0.17	0.036	(0.163)	0.032	0.004
213	17.75	0.17	0.036	(0.163)	0.032	0.004
214	17.83	0.13	0.029	(0.162)	0.026	0.003
215	17.92	0.13	0.029	(0.161)	0.026	0.003
216	18.00	0.13	0.029	(0.160)	0.026	0.003
217	18.08	0.13	0.029	(0.159)	0.026	0.003
218	18.17	0.13	0.029	(0.159)	0.026	0.003
219	18.25	0.13	0.029	(0.158)	0.026	0.003
220	18.33	0.13	0.029	(0.157)	0.026	0.003
221	18.42	0.13	0.029	(0.156)	0.026	0.003
222	18.50	0.13	0.029	(0.156)	0.026	0.003
223	18.58	0.10	0.022	(0.155)	0.019	0.002
224	18.67	0.10	0.022	(0.154)	0.019	0.002
225	18.75	0.10	0.022	(0.153)	0.019	0.002
226	18.83	0.07	0.014	(0.153)	0.013	0.001
227	18.92	0.07	0.014	(0.152)	0.013	0.001
228	19.00	0.07	0.014	(0.151)	0.013	0.001
229	19.08	0.10	0.022	(0.150)	0.019	0.002
230	19.17	0.10	0.022	(0.150)	0.019	0.002
231	19.25	0.10	0.022	(0.149)	0.019	0.002
232	19.33	0.13	0.029	(0.148)	0.026	0.003
233	19.42	0.13	0.029	(0.148)	0.026	0.003
234	19.50	0.13	0.029	(0.147)	0.026	0.003
235	19.58	0.10	0.022	(0.146)	0.019	0.002
236	19.67	0.10	0.022	(0.146)	0.019	0.002
237	19.75	0.10	0.022	(0.145)	0.019	0.002
238	19.83	0.07	0.014	(0.144)	0.013	0.001
239	19.92	0.07	0.014	(0.144)	0.013	0.001
240	20.00	0.07	0.014	(0.143)	0.013	0.001
241	20.08	0.10	0.022	(0.142)	0.019	0.002
242	20.17	0.10	0.022	(0.142)	0.019	0.002

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243  20.25     0.10      0.022       (  0.141)       0.019        0.002
244  20.33     0.10      0.022       (  0.141)       0.019        0.002
245  20.42     0.10      0.022       (  0.140)       0.019        0.002
246  20.50     0.10      0.022       (  0.139)       0.019        0.002
247  20.58     0.10      0.022       (  0.139)       0.019        0.002
248  20.67     0.10      0.022       (  0.138)       0.019        0.002
249  20.75     0.10      0.022       (  0.138)       0.019        0.002
250  20.83     0.07      0.014       (  0.137)       0.013        0.001
251  20.92     0.07      0.014       (  0.137)       0.013        0.001
252  21.00     0.07      0.014       (  0.136)       0.013        0.001
253  21.08     0.10      0.022       (  0.135)       0.019        0.002
254  21.17     0.10      0.022       (  0.135)       0.019        0.002
255  21.25     0.10      0.022       (  0.134)       0.019        0.002
256  21.33     0.07      0.014       (  0.134)       0.013        0.001
257  21.42     0.07      0.014       (  0.133)       0.013        0.001
258  21.50     0.07      0.014       (  0.133)       0.013        0.001
259  21.58     0.10      0.022       (  0.132)       0.019        0.002
260  21.67     0.10      0.022       (  0.132)       0.019        0.002
261  21.75     0.10      0.022       (  0.131)       0.019        0.002
262  21.83     0.07      0.014       (  0.131)       0.013        0.001
263  21.92     0.07      0.014       (  0.131)       0.013        0.001
264  22.00     0.07      0.014       (  0.130)       0.013        0.001
265  22.08     0.10      0.022       (  0.130)       0.019        0.002
266  22.17     0.10      0.022       (  0.129)       0.019        0.002
267  22.25     0.10      0.022       (  0.129)       0.019        0.002
268  22.33     0.07      0.014       (  0.128)       0.013        0.001
269  22.42     0.07      0.014       (  0.128)       0.013        0.001
270  22.50     0.07      0.014       (  0.128)       0.013        0.001
271  22.58     0.07      0.014       (  0.127)       0.013        0.001
272  22.67     0.07      0.014       (  0.127)       0.013        0.001
273  22.75     0.07      0.014       (  0.127)       0.013        0.001
274  22.83     0.07      0.014       (  0.126)       0.013        0.001
275  22.92     0.07      0.014       (  0.126)       0.013        0.001
276  23.00     0.07      0.014       (  0.126)       0.013        0.001
277  23.08     0.07      0.014       (  0.125)       0.013        0.001
278  23.17     0.07      0.014       (  0.125)       0.013        0.001
279  23.25     0.07      0.014       (  0.125)       0.013        0.001
280  23.33     0.07      0.014       (  0.125)       0.013        0.001
281  23.42     0.07      0.014       (  0.124)       0.013        0.001
282  23.50     0.07      0.014       (  0.124)       0.013        0.001
283  23.58     0.07      0.014       (  0.124)       0.013        0.001
284  23.67     0.07      0.014       (  0.124)       0.013        0.001
285  23.75     0.07      0.014       (  0.124)       0.013        0.001
286  23.83     0.07      0.014       (  0.123)       0.013        0.001
287  23.92     0.07      0.014       (  0.123)       0.013        0.001
288  24.00     0.07      0.014       (  0.123)       0.013        0.001
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =      2.2
      Flood volume = Effective rainfall      0.18(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       0.4(Ac.Ft)
      Total soil loss =      1.62(In)
      Total soil loss =     3.602(Ac.Ft)
      Total rainfall =      1.80(In)
      Flood volume =       17790.5 Cubic Feet
      Total soil loss =      156919.5 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.883(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0001      0.01  Q          |         |         |         |
   0+10       0.0003      0.03  Q          |         |         |         |
   0+15       0.0006      0.04  Q          |         |         |         |
   0+20       0.0009      0.04  Q          |         |         |         |
   0+25       0.0012      0.05  Q          |         |         |         |
   0+30       0.0016      0.06  Q          |         |         |         |
   0+35       0.0020      0.06  Q          |         |         |         |
   0+40       0.0024      0.06  Q          |         |         |         |
   0+45       0.0028      0.06  Q          |         |         |         |
   0+50       0.0033      0.07  Q          |         |         |         |
   0+55       0.0038      0.07  Q          |         |         |         |
   1+ 0       0.0043      0.08  Q          |         |         |         |
   1+ 5       0.0048      0.07  Q          |         |         |         |
   1+10       0.0052      0.06  Q          |         |         |         |
   1+15       0.0056      0.06  Q          |         |         |         |
   1+20       0.0060      0.06  Q          |         |         |         |
   1+25       0.0064      0.06  Q          |         |         |         |
   1+30       0.0068      0.06  Q          |         |         |         |
   1+35       0.0072      0.06  Q          |         |         |         |
```

```
1+40      0.0076      0.06  Q          |          |          |          |
1+45      0.0080      0.06  Q          |          |          |          |
1+50      0.0085      0.07  Q          |          |          |          |
1+55      0.0090      0.07  Q          |          |          |          |
2+ 0      0.0095      0.08  Q          |          |          |          |
2+ 5      0.0101      0.08  Q          |          |          |          |
2+10      0.0106      0.08  QV         |          |          |          |
2+15      0.0111      0.08  QV         |          |          |          |
2+20      0.0117      0.08  QV         |          |          |          |
2+25      0.0122      0.08  QV         |          |          |          |
2+30      0.0127      0.08  QV         |          |          |          |
2+35      0.0133      0.08  QV         |          |          |          |
2+40      0.0140      0.09  QV         |          |          |          |
2+45      0.0146      0.10  QV         |          |          |          |
2+50      0.0153      0.10  QV         |          |          |          |
2+55      0.0159      0.10  QV         |          |          |          |
3+ 0      0.0166      0.10  QV         |          |          |          |
3+ 5      0.0173      0.10  QV         |          |          |          |
3+10      0.0179      0.10  QV         |          |          |          |
3+15      0.0186      0.10  QV         |          |          |          |
3+20      0.0193      0.10  QV         |          |          |          |
3+25      0.0200      0.10  QV         |          |          |          |
3+30      0.0206      0.10  Q V        |          |          |          |
3+35      0.0213      0.10  Q V        |          |          |          |
3+40      0.0220      0.10  Q V        |          |          |          |
3+45      0.0226      0.10  Q V        |          |          |          |
3+50      0.0233      0.10  Q V        |          |          |          |
3+55      0.0241      0.11  Q V        |          |          |          |
4+ 0      0.0249      0.11  Q V        |          |          |          |
4+ 5      0.0257      0.12  Q V        |          |          |          |
4+10      0.0265      0.12  Q V        |          |          |          |
4+15      0.0273      0.12  Q V        |          |          |          |
4+20      0.0282      0.12  Q V        |          |          |          |
4+25      0.0291      0.13  Q V        |          |          |          |
4+30      0.0300      0.13  Q V        |          |          |          |
4+35      0.0309      0.14  Q  V       |          |          |          |
4+40      0.0319      0.14  Q  V       |          |          |          |
4+45      0.0328      0.14  Q  V       |          |          |          |
4+50      0.0338      0.14  Q  V       |          |          |          |
4+55      0.0348      0.15  Q  V       |          |          |          |
5+ 0      0.0359      0.15  Q  V       |          |          |          |
5+ 5      0.0369      0.14  Q  V       |          |          |          |
5+10      0.0377      0.12  Q  V       |          |          |          |
5+15      0.0385      0.12  Q  V       |          |          |          |
5+20      0.0394      0.12  Q  V       |          |          |          |
5+25      0.0403      0.13  Q  V       |          |          |          |
5+30      0.0412      0.13  Q   V      |          |          |          |
5+35      0.0422      0.14  Q   V      |          |          |          |
5+40      0.0433      0.15  Q   V      |          |          |          |
5+45      0.0443      0.15  Q   V      |          |          |          |
5+50      0.0454      0.15  Q   V      |          |          |          |
5+55      0.0464      0.16  Q   V      |          |          |          |
6+ 0      0.0475      0.16  Q   V      |          |          |          |
6+ 5      0.0486      0.16  Q   V      |          |          |          |
6+10      0.0498      0.17  Q   V      |          |          |          |
6+15      0.0510      0.17  Q   V      |          |          |          |
6+20      0.0522      0.17  Q    V     |          |          |          |
6+25      0.0534      0.17  Q    V     |          |          |          |
6+30      0.0546      0.17  Q    V     |          |          |          |
6+35      0.0559      0.18  Q    V     |          |          |          |
6+40      0.0572      0.19  Q    V     |          |          |          |
6+45      0.0585      0.19  Q    V     |          |          |          |
6+50      0.0598      0.19  Q    V     |          |          |          |
6+55      0.0612      0.19  Q    V     |          |          |          |
7+ 0      0.0625      0.19  Q     V    |          |          |          |
7+ 5      0.0638      0.19  Q     V    |          |          |          |
7+10      0.0652      0.19  Q     V    |          |          |          |
7+15      0.0665      0.19  Q     V    |          |          |          |
7+20      0.0679      0.20  Q     V    |          |          |          |
7+25      0.0693      0.21  Q     V    |          |          |          |
7+30      0.0708      0.21  Q     V    |          |          |          |
7+35      0.0723      0.22  Q      V   |          |          |          |
7+40      0.0739      0.23  Q      V   |          |          |          |
7+45      0.0755      0.23  Q      V   |          |          |          |
7+50      0.0771      0.24  Q      V   |          |          |          |
7+55      0.0788      0.25  Q      V   |          |          |          |
8+ 0      0.0806      0.25  |Q     V   |          |          |          |
8+ 5      0.0824      0.27  |Q      V  |          |          |          |
8+10      0.0844      0.28  |Q      V  |          |          |          |
8+15      0.0863      0.29  |Q      V  |          |          |          |
8+20      0.0883      0.29  |Q      V  |          |          |          |
8+25      0.0903      0.29  |Q      V  |          |          |          |
8+30      0.0923      0.29  |Q       V |          |          |          |
8+35      0.0944      0.30  |Q       V |          |          |          |
8+40      0.0965      0.31  |Q       V |          |          |          |
8+45      0.0986      0.31  |Q       V |          |          |          |
```



8+50	0.1008	0.32	
8+55	0.1031	0.33	
9+ 0	0.1053	0.33	
9+ 5	0.1077	0.34	
9+10	0.1102	0.36	
9+15	0.1127	0.37	
9+20	0.1153	0.37	
9+25	0.1179	0.38	
9+30	0.1206	0.39	
9+35	0.1233	0.39	
9+40	0.1261	0.40	
9+45	0.1289	0.41	
9+50	0.1317	0.41	
9+55	0.1347	0.42	
10+ 0	0.1376	0.43	
10+ 5	0.1402	0.38	
10+10	0.1424	0.32	
10+15	0.1444	0.30	
10+20	0.1465	0.30	
10+25	0.1485	0.29	
10+30	0.1505	0.29	
10+35	0.1527	0.33	
10+40	0.1553	0.37	
10+45	0.1579	0.38	
10+50	0.1606	0.39	
10+55	0.1632	0.39	
11+ 0	0.1659	0.39	
11+ 5	0.1685	0.38	
11+10	0.1711	0.37	
11+15	0.1737	0.37	
11+20	0.1762	0.37	
11+25	0.1787	0.37	
11+30	0.1813	0.37	
11+35	0.1837	0.36	
11+40	0.1860	0.34	
11+45	0.1883	0.33	
11+50	0.1907	0.34	
11+55	0.1931	0.35	
12+ 0	0.1954	0.35	
12+ 5	0.1982	0.40	
12+10	0.2013	0.46	
12+15	0.2046	0.47	
12+20	0.2080	0.49	
12+25	0.2114	0.50	
12+30	0.2149	0.50	
12+35	0.2185	0.52	
12+40	0.2221	0.54	
12+45	0.2259	0.54	
12+50	0.2296	0.55	
12+55	0.2335	0.56	
13+ 0	0.2374	0.56	
13+ 5	0.2417	0.63	
13+10	0.2468	0.74	
13+15	0.2522	0.78	
13+20	0.2578	0.82	
13+25	0.2637	0.85	
13+30	0.2698	0.88	
13+35	0.2749	0.74	
13+40	0.2785	0.53	
13+45	0.2818	0.48	
13+50	0.2850	0.46	
13+55	0.2881	0.45	
14+ 0	0.2912	0.45	
14+ 5	0.2944	0.47	
14+10	0.2980	0.51	
14+15	0.3015	0.52	
14+20	0.3051	0.51	
14+25	0.3086	0.51	
14+30	0.3121	0.51	
14+35	0.3155	0.51	
14+40	0.3190	0.50	
14+45	0.3225	0.50	
14+50	0.3259	0.50	
14+55	0.3293	0.49	
15+ 0	0.3326	0.49	
15+ 5	0.3359	0.48	
15+10	0.3392	0.47	
15+15	0.3424	0.47	
15+20	0.3456	0.46	
15+25	0.3487	0.45	
15+30	0.3517	0.45	
15+35	0.3546	0.42	
15+40	0.3573	0.38	
15+45	0.3599	0.37	
15+50	0.3624	0.37	
15+55	0.3650	0.37	

16+ 0	0.3675	0.37	|Q	|	|	|	V |
16+ 5	0.3693	0.27	|Q	|	|	|	V |
16+10	0.3702	0.13	Q	|	|	|	V |
16+15	0.3709	0.10	Q	|	|	|	V |
16+20	0.3715	0.09	Q	|	|	|	V |
16+25	0.3721	0.08	Q	|	|	|	V |
16+30	0.3726	0.08	Q	|	|	|	V |
16+35	0.3731	0.07	Q	|	|	|	V |
16+40	0.3735	0.06	Q	|	|	|	V |
16+45	0.3739	0.06	Q	|	|	|	V |
16+50	0.3743	0.06	Q	|	|	|	V |
16+55	0.3747	0.06	Q	|	|	|	V |
17+ 0	0.3751	0.06	Q	|	|	|	V |
17+ 5	0.3756	0.07	Q	|	|	|	V |
17+10	0.3763	0.09	Q	|	|	|	V |
17+15	0.3769	0.09	Q	|	|	|	V |
17+20	0.3776	0.10	Q	|	|	|	V |
17+25	0.3782	0.10	Q	|	|	|	V |
17+30	0.3789	0.10	Q	|	|	|	V |
17+35	0.3796	0.10	Q	|	|	|	V |
17+40	0.3802	0.10	Q	|	|	|	V |
17+45	0.3809	0.10	Q	|	|	|	V |
17+50	0.3815	0.09	Q	|	|	|	V |
17+55	0.3821	0.08	Q	|	|	|	V |
18+ 0	0.3826	0.08	Q	|	|	|	V |
18+ 5	0.3832	0.08	Q	|	|	|	V |
18+10	0.3837	0.08	Q	|	|	|	V |
18+15	0.3842	0.08	Q	|	|	|	V |
18+20	0.3848	0.08	Q	|	|	|	V |
18+25	0.3853	0.08	Q	|	|	|	V |
18+30	0.3858	0.08	Q	|	|	|	V |
18+35	0.3863	0.07	Q	|	|	|	V |
18+40	0.3868	0.06	Q	|	|	|	V |
18+45	0.3872	0.06	Q	|	|	|	V |
18+50	0.3875	0.05	Q	|	|	|	V |
18+55	0.3878	0.04	Q	|	|	|	V |
19+ 0	0.3881	0.04	Q	|	|	|	V |
19+ 5	0.3884	0.05	Q	|	|	|	V |
19+10	0.3888	0.05	Q	|	|	|	V |
19+15	0.3892	0.06	Q	|	|	|	V |
19+20	0.3896	0.06	Q	|	|	|	V |
19+25	0.3901	0.07	Q	|	|	|	V |
19+30	0.3907	0.08	Q	|	|	|	V |
19+35	0.3911	0.07	Q	|	|	|	V |
19+40	0.3916	0.06	Q	|	|	|	V |
19+45	0.3920	0.06	Q	|	|	|	V |
19+50	0.3923	0.05	Q	|	|	|	V |
19+55	0.3926	0.04	Q	|	|	|	V |
20+ 0	0.3929	0.04	Q	|	|	|	V |
20+ 5	0.3932	0.05	Q	|	|	|	V |
20+10	0.3936	0.05	Q	|	|	|	V |
20+15	0.3940	0.06	Q	|	|	|	V |
20+20	0.3944	0.06	Q	|	|	|	V |
20+25	0.3948	0.06	Q	|	|	|	V |
20+30	0.3952	0.06	Q	|	|	|	V |
20+35	0.3956	0.06	Q	|	|	|	V |
20+40	0.3960	0.06	Q	|	|	|	V |
20+45	0.3964	0.06	Q	|	|	|	V |
20+50	0.3968	0.05	Q	|	|	|	V |
20+55	0.3970	0.04	Q	|	|	|	V |
21+ 0	0.3973	0.04	Q	|	|	|	V |
21+ 5	0.3976	0.05	Q	|	|	|	V |
21+10	0.3980	0.05	Q	|	|	|	V |
21+15	0.3984	0.06	Q	|	|	|	V|
21+20	0.3988	0.05	Q	|	|	|	V|
21+25	0.3991	0.04	Q	|	|	|	V|
21+30	0.3993	0.04	Q	|	|	|	V|
21+35	0.3996	0.05	Q	|	|	|	V|
21+40	0.4000	0.05	Q	|	|	|	V|
21+45	0.4004	0.06	Q	|	|	|	V|
21+50	0.4008	0.05	Q	|	|	|	V|
21+55	0.4011	0.04	Q	|	|	|	V|
22+ 0	0.4013	0.04	Q	|	|	|	V|
22+ 5	0.4017	0.05	Q	|	|	|	V|
22+10	0.4020	0.05	Q	|	|	|	V|
22+15	0.4024	0.06	Q	|	|	|	V|
22+20	0.4028	0.05	Q	|	|	|	V|
22+25	0.4031	0.04	Q	|	|	|	V|
22+30	0.4033	0.04	Q	|	|	|	V|
22+35	0.4036	0.04	Q	|	|	|	V|
22+40	0.4039	0.04	Q	|	|	|	V|
22+45	0.4041	0.04	Q	|	|	|	V|
22+50	0.4044	0.04	Q	|	|	|	V|
22+55	0.4047	0.04	Q	|	|	|	V|
23+ 0	0.4050	0.04	Q	|	|	|	V|
23+ 5	0.4052	0.04	Q	|	|	|	V|

```
   23+10       0.4055      0.04  Q          |          |          |         v|
   23+15       0.4058      0.04  Q          |          |          |         v|
   23+20       0.4060      0.04  Q          |          |          |         v|
   23+25       0.4063      0.04  Q          |          |          |         v|
   23+30       0.4066      0.04  Q          |          |          |         v|
   23+35       0.4068      0.04  Q          |          |          |         v|
   23+40       0.4071      0.04  Q          |          |          |         v|
   23+45       0.4074      0.04  Q          |          |          |         v|
   23+50       0.4076      0.04  Q          |          |          |         v|
   23+55       0.4079      0.04  Q          |          |          |         v|
   24+ 0       0.4082      0.04  Q          |          |          |         v|
   24+ 5       0.4083      0.03  Q          |          |          |         v|
   24+10       0.4084      0.01  Q          |          |          |         v|
   24+15       0.4084      0.00  Q          |          |          |         v|
   24+20       0.4084      0.00  Q          |          |          |         v|
   24+25       0.4084      0.00  Q          |          |          |          v
-------------------------------------------------------------------------------
```

```
        U n i t   H y d r o g r a p h   A n a l y s i s

        Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2008, Version 8.1
                Study date  04/22/24 File: EX1515.out

++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      26.74(Ac.)  =      0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      26.74(Ac.)  =      0.042 Sq. Mi.
Length along longest watercourse =    1087.00(Ft.)
Length along longest watercourse measured to centroid =     544.00(Ft.)
Length along longest watercourse =      0.206 Mi.
Length along longest watercourse measured to centroid =      0.103 Mi.
Difference in elevation =      88.30(Ft.)
Slope along watercourse =    428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.053 Hr.
Lag time =     3.16 Min.
25% of lag time =     0.79 Min.
40% of lag time =     1.26 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           0.50                 13.37

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           1.30                 34.76

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.687(In)
Areal adjustment factor =   99.98 %
Adjusted average point rain =    0.687(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    26.740           91.00         0.000
 Total Area Entered =     26.74(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000 Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.272	(0.246)	0.245	0.027
2	0.17	4.20	0.346	0.246	(0.312)	0.100
3	0.25	4.40	0.363	0.246	(0.327)	0.116
4	0.33	4.80	0.396	0.246	(0.356)	0.149
5	0.42	5.20	0.429	0.246	(0.386)	0.182
6	0.50	6.20	0.511	0.246	(0.460)	0.265
7	0.58	6.80	0.561	0.246	(0.505)	0.314
8	0.67	8.80	0.726	0.246	(0.653)	0.479
9	0.75	13.90	1.146	0.246	(1.032)	0.900
10	0.83	31.40	2.589	0.246	(2.330)	2.343
11	0.92	7.20	0.594	0.246	(0.534)	0.347
12	1.00	3.80	0.313	0.246	(0.282)	0.067
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.3

Flood volume = Effective rainfall 0.44(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 1.0(Ac.Ft)
Total soil loss = 0.25(In)
Total soil loss = 0.549(Ac.Ft)
Total rainfall = 0.69(In)
Flood volume = 42803.5 Cubic Feet
Total soil loss = 23901.6 Cubic Feet

Peak flow rate of this hydrograph = 36.052(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	10.0	20.0	30.0	40.0
0+ 5	0.0018	0.26	Q				
0+10	0.0106	1.29	VQ				
0+15	0.0274	2.43	VQ				
0+20	0.0494	3.20	VQ				
0+25	0.0775	4.08	VQ				
0+30	0.1149	5.44	VQ				
0+35	0.1638	7.10	VQ				
0+40	0.2298	9.58	Q				
0+45	0.3394	15.91	V Q				
0+50	0.5834	35.43	V		Q		
0+55	0.8317	36.05	V		Q		
1+ 0	0.9229	13.24	Q		V		
1+ 5	0.9603	5.43	Q		V		
1+10	0.9758	2.26	Q		V		
1+15	0.9817	0.85	Q		V		
1+20	0.9825	0.12	Q		V		
1+25	0.9826	0.02	Q		V		

```
        U n i t   H y d r o g r a p h   A n a l y s i s

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                Study date  04/22/24 File: EX1535.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      26.74(Ac.)  =      0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      26.74(Ac.)  =      0.042 Sq. Mi.
Length along longest watercourse =    1087.00(Ft.)
Length along longest watercourse measured to centroid =     544.00(Ft.)
Length along longest watercourse =      0.206 Mi.
Length along longest watercourse measured to centroid =      0.103 Mi.
Difference in elevation =      88.30(Ft.)
Slope along watercourse =    428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.053 Hr.
Lag time =     3.16 Min.
25% of lag time =     0.79 Min.
40% of lag time =     1.26 Min.
Unit time =     5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           0.80                 21.39

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           2.00                 53.48

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.800(In)
Area Averaged 100-Year Rainfall =    2.000(In)

Point rain (area averaged) =    1.081(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    1.081(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    26.740           91.00         0.000
 Total Area Entered =     26.74(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

```
      ----------------------------------------------------------------------
          1   0.083        158.322          35.130              9.467
          2   0.167        316.645          46.393             12.502
          3   0.250        474.967          10.719              2.889
          4   0.333        633.290           4.631              1.248
          5   0.417        791.612           2.248              0.606
          6   0.500        949.935           0.879              0.237
                                    Sum = 100.000    Sum=       26.949
----------------------------------------------------------------------


 The following loss rate calculations reflect use of the minimum calculated loss
 rate subtracted from the Storm Rain to produce the maximum Effective Rain value

  Unit Time   Pattern   Storm Rain     Loss rate(In./Hr)     Effective
       (Hr.)  Percent   (In/Hr)         Max   |   Low         (In/Hr)
   1   0.08     1.30      0.169       (  0.246)       0.152        0.017
   2   0.17     1.30      0.169       (  0.246)       0.152        0.017
   3   0.25     1.10      0.143       (  0.246)       0.128        0.014
   4   0.33     1.50      0.195       (  0.246)       0.175        0.019
   5   0.42     1.50      0.195       (  0.246)       0.175        0.019
   6   0.50     1.80      0.233       (  0.246)       0.210        0.023
   7   0.58     1.50      0.195       (  0.246)       0.175        0.019
   8   0.67     1.80      0.233       (  0.246)       0.210        0.023
   9   0.75     1.80      0.233       (  0.246)       0.210        0.023
  10   0.83     1.50      0.195       (  0.246)       0.175        0.019
  11   0.92     1.60      0.208       (  0.246)       0.187        0.021
  12   1.00     1.80      0.233       (  0.246)       0.210        0.023
  13   1.08     2.20      0.285          0.246    (  0.257)        0.039
  14   1.17     2.20      0.285          0.246    (  0.257)        0.039
  15   1.25     2.20      0.285          0.246    (  0.257)        0.039
  16   1.33     2.00      0.259       (  0.246)       0.233        0.026
  17   1.42     2.60      0.337          0.246    (  0.304)        0.091
  18   1.50     2.70      0.350          0.246    (  0.315)        0.104
  19   1.58     2.40      0.311          0.246    (  0.280)        0.065
  20   1.67     2.70      0.350          0.246    (  0.315)        0.104
  21   1.75     3.30      0.428          0.246    (  0.385)        0.182
  22   1.83     3.10      0.402          0.246    (  0.362)        0.156
  23   1.92     2.90      0.376          0.246    (  0.339)        0.130
  24   2.00     3.00      0.389          0.246    (  0.350)        0.143
  25   2.08     3.10      0.402          0.246    (  0.362)        0.156
  26   2.17     4.20      0.545          0.246    (  0.490)        0.298
  27   2.25     5.00      0.649          0.246    (  0.584)        0.402
  28   2.33     3.50      0.454          0.246    (  0.409)        0.208
  29   2.42     6.80      0.882          0.246    (  0.794)        0.636
  30   2.50     7.30      0.947          0.246    (  0.852)        0.701
  31   2.58     8.20      1.064          0.246    (  0.957)        0.817
  32   2.67     5.90      0.765          0.246    (  0.689)        0.519
  33   2.75     2.00      0.259       (  0.246)       0.233        0.026
  34   2.83     1.80      0.233       (  0.246)       0.210        0.023
  35   2.92     1.80      0.233       (  0.246)       0.210        0.023
  36   3.00     0.60      0.078       (  0.246)       0.070        0.008
               (Loss Rate Not Used)
     Sum =     100.0                                  Sum =     5.2
        Flood volume = Effective rainfall      0.43(In)
         times area      26.7(Ac.)/[(In)/(Ft.)] =       1.0(Ac.Ft)
        Total soil loss =      0.65(In)
        Total soil loss =     1.448(Ac.Ft)
        Total rainfall =      1.08(In)
        Flood volume =       41847.4 Cubic Feet
        Total soil loss =       63075.6 Cubic Feet
        ---------------------------------------------------------------------
         Peak flow rate of this hydrograph =     18.915(CFS)
        ---------------------------------------------------------------------
        +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                              3 - H O U R    S T O R M
                         R u n o f f      H y d r o g r a p h
        ---------------------------------------------------------------------
                    Hydrograph in   5   Minute intervals ((CFS))

        ---------------------------------------------------------------------
  Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
  ----------------------------------------------------------------------------
    0+ 5       0.0011      0.16  Q          |         |         |         |
    0+10       0.0037      0.37  Q          |         |         |         |
    0+15       0.0064      0.39  Q          |         |         |         |
    0+20       0.0094      0.43  Q          |         |         |         |
    0+25       0.0128      0.50  VQ         |         |         |         |
    0+30       0.0166      0.55  VQ         |         |         |         |
    0+35       0.0205      0.57  VQ         |         |         |         |
    0+40       0.0245      0.57  |Q         |         |         |         |
    0+45       0.0287      0.62  |Q         |         |         |         |
    0+50       0.0327      0.59  |Q         |         |         |         |
    0+55       0.0366      0.55  |Q         |         |         |         |
    1+ 0       0.0406      0.58  |Q         |         |         |         |
    1+ 5       0.0459      0.77  |Q         |         |         |         |
```

```
    1+10       0.0525      0.97  |QV        |          |          |          |
    1+15       0.0595      1.02  | Q        |          |          |          |
    1+20       0.0658      0.91  |QV        |          |          |          |
    1+25       0.0753      1.38  | QV       |          |          |          |
    1+30       0.0910      2.28  |  VQ      |          |          |          |
    1+35       0.1064      2.24  |    Q     |          |          |          |
    1+40       0.1218      2.23  |    QV    |          |          |          |
    1+45       0.1452      3.40  |      Q   |          |          |          |
    1+50       0.1742      4.21  |       VQ |          |          |          |
    1+55       0.2011      3.90  |       QV |          |          |          |
    2+ 0       0.2268      3.73  |       Q V|          |          |          |
    2+ 5       0.2541      3.97  |       Q  V          |          |          |
    2+10       0.2919      5.49  |          Q V        |          |          |
    2+15       0.3490      8.29  |          |   V Q    |          |          |
    2+20       0.4052      8.17  |          |     Q    |          |          |
    2+25       0.4761     10.28  |          |        VQ          |          |
    2+30       0.5856     15.91  |          |          |   V      |Q         |
    2+35       0.7159     18.92  |          |          |        V |     Q    |
    2+40       0.8411     18.18  |          |          |          |   VQ     |
    2+45       0.9128     10.41  |          |          Q          |       V  |
    2+50       0.9378      3.64  |       Q  |          |          |         V|
    2+55       0.9509      1.90  |  Q       |          |          |         V|
    3+ 0       0.9576      0.97  |Q         |          |          |         V|
    3+ 5       0.9599      0.33  Q          |          |          |         V|
    3+10       0.9604      0.07  Q          |          |          |         V|
    3+15       0.9606      0.03  Q          |          |          |         V|
    3+20       0.9607      0.01  Q          |          |          |         V|
    3+25       0.9607      0.00  Q          |          |          |         V|
-------------------------------------------------------------------------- |
```

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX1565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 1087.00(Ft.)
Length along longest watercourse measured to centroid = 544.00(Ft.)
Length along longest watercourse = 0.206 Mi.
Length along longest watercourse measured to centroid = 0.103 Mi.
Difference in elevation = 88.30(Ft.)
Slope along watercourse = 428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.10	29.41

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	3.00	80.22

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.545(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.545(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.000

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.093	(0.246)	0.083	0.009
2	0.17	0.60	0.111	(0.246)	0.100	0.011
3	0.25	0.60	0.111	(0.246)	0.100	0.011
4	0.33	0.60	0.111	(0.246)	0.100	0.011
5	0.42	0.60	0.111	(0.246)	0.100	0.011
6	0.50	0.70	0.130	(0.246)	0.117	0.013
7	0.58	0.70	0.130	(0.246)	0.117	0.013
8	0.67	0.70	0.130	(0.246)	0.117	0.013
9	0.75	0.70	0.130	(0.246)	0.117	0.013
10	0.83	0.70	0.130	(0.246)	0.117	0.013
11	0.92	0.70	0.130	(0.246)	0.117	0.013
12	1.00	0.80	0.148	(0.246)	0.133	0.015
13	1.08	0.80	0.148	(0.246)	0.133	0.015
14	1.17	0.80	0.148	(0.246)	0.133	0.015
15	1.25	0.80	0.148	(0.246)	0.133	0.015
16	1.33	0.80	0.148	(0.246)	0.133	0.015
17	1.42	0.80	0.148	(0.246)	0.133	0.015
18	1.50	0.80	0.148	(0.246)	0.133	0.015
19	1.58	0.80	0.148	(0.246)	0.133	0.015
20	1.67	0.80	0.148	(0.246)	0.133	0.015
21	1.75	0.80	0.148	(0.246)	0.133	0.015
22	1.83	0.80	0.148	(0.246)	0.133	0.015
23	1.92	0.80	0.148	(0.246)	0.133	0.015
24	2.00	0.90	0.167	(0.246)	0.150	0.017
25	2.08	0.80	0.148	(0.246)	0.133	0.015
26	2.17	0.90	0.167	(0.246)	0.150	0.017
27	2.25	0.90	0.167	(0.246)	0.150	0.017
28	2.33	0.90	0.167	(0.246)	0.150	0.017
29	2.42	0.90	0.167	(0.246)	0.150	0.017
30	2.50	0.90	0.167	(0.246)	0.150	0.017
31	2.58	0.90	0.167	(0.246)	0.150	0.017
32	2.67	0.90	0.167	(0.246)	0.150	0.017
33	2.75	1.00	0.185	(0.246)	0.167	0.019
34	2.83	1.00	0.185	(0.246)	0.167	0.019
35	2.92	1.00	0.185	(0.246)	0.167	0.019
36	3.00	1.00	0.185	(0.246)	0.167	0.019
37	3.08	1.00	0.185	(0.246)	0.167	0.019
38	3.17	1.10	0.204	(0.246)	0.184	0.020
39	3.25	1.10	0.204	(0.246)	0.184	0.020
40	3.33	1.10	0.204	(0.246)	0.184	0.020
41	3.42	1.20	0.222	(0.246)	0.200	0.022
42	3.50	1.30	0.241	(0.246)	0.217	0.024
43	3.58	1.40	0.260	(0.246)	0.234	0.026
44	3.67	1.40	0.260	(0.246)	0.234	0.026
45	3.75	1.50	0.278	0.246	(0.250)	0.032
46	3.83	1.50	0.278	0.246	(0.250)	0.032
47	3.92	1.60	0.297	0.246	(0.267)	0.050
48	4.00	1.60	0.297	0.246	(0.267)	0.050
49	4.08	1.70	0.315	0.246	(0.284)	0.069
50	4.17	1.80	0.334	0.246	(0.300)	0.087
51	4.25	1.90	0.352	0.246	(0.317)	0.106
52	4.33	2.00	0.371	0.246	(0.334)	0.124
53	4.42	2.10	0.389	0.246	(0.350)	0.143
54	4.50	2.10	0.389	0.246	(0.350)	0.143
55	4.58	2.20	0.408	0.246	(0.367)	0.161
56	4.67	2.30	0.426	0.246	(0.384)	0.180
57	4.75	2.40	0.445	0.246	(0.400)	0.199
58	4.83	2.40	0.445	0.246	(0.400)	0.199
59	4.92	2.50	0.463	0.246	(0.417)	0.217
60	5.00	2.60	0.482	0.246	(0.434)	0.236
61	5.08	3.10	0.575	0.246	(0.517)	0.328
62	5.17	3.60	0.667	0.246	(0.601)	0.421
63	5.25	3.90	0.723	0.246	(0.651)	0.477
64	5.33	4.20	0.779	0.246	(0.701)	0.532
65	5.42	4.70	0.871	0.246	(0.784)	0.625
66	5.50	5.60	1.038	0.246	(0.934)	0.792
67	5.58	1.90	0.352	0.246	(0.317)	0.106
68	5.67	0.90	0.167	(0.246)	0.150	0.017
69	5.75	0.60	0.111	(0.246)	0.100	0.011
70	5.83	0.50	0.093	(0.246)	0.083	0.009

```
71   5.92     0.30      0.056       (  0.246)       0.050        0.006
72   6.00     0.20      0.037       (  0.246)       0.033        0.004
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =     6.1
     Flood volume = Effective rainfall      0.51(In)
      times area      26.7(Ac.)/[(In)/(Ft.)] =       1.1(Ac.Ft)
     Total soil loss =      1.04(In)
     Total soil loss =     2.316(Ac.Ft)
     Total rainfall =      1.54(In)
     Flood volume =       49058.5 Cubic Feet
     Total soil loss =      100897.5 Cubic Feet
     ---------------------------------------------------------------------
      Peak flow rate of this hydrograph =     17.784(CFS)
     ---------------------------------------------------------------------
     +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f     H y d r o g r a p h
     ---------------------------------------------------------------------
                 Hydrograph in   5   Minute intervals ((CFS))

     ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
-------------------------------------------------------------------------
  0+ 5       0.0006      0.09  Q         |         |         |         |
  0+10       0.0021      0.22  Q         |         |         |         |
  0+15       0.0040      0.27  Q         |         |         |         |
  0+20       0.0060      0.29  Q         |         |         |         |
  0+25       0.0080      0.30  Q         |         |         |         |
  0+30       0.0102      0.32  Q         |         |         |         |
  0+35       0.0126      0.34  Q         |         |         |         |
  0+40       0.0149      0.35  Q         |         |         |         |
  0+45       0.0173      0.35  Q         |         |         |         |
  0+50       0.0197      0.35  Q         |         |         |         |
  0+55       0.0221      0.35  Q         |         |         |         |
  1+ 0       0.0247      0.37  Q         |         |         |         |
  1+ 5       0.0274      0.39  Q         |         |         |         |
  1+10       0.0301      0.40  QV        |         |         |         |
  1+15       0.0328      0.40  QV        |         |         |         |
  1+20       0.0356      0.40  QV        |         |         |         |
  1+25       0.0383      0.40  QV        |         |         |         |
  1+30       0.0411      0.40  QV        |         |         |         |
  1+35       0.0439      0.40  QV        |         |         |         |
  1+40       0.0466      0.40  QV        |         |         |         |
  1+45       0.0494      0.40  QV        |         |         |         |
  1+50       0.0521      0.40  QV        |         |         |         |
  1+55       0.0549      0.40  QV        |         |         |         |
  2+ 0       0.0577      0.42  Q V       |         |         |         |
  2+ 5       0.0607      0.42  Q V       |         |         |         |
  2+10       0.0636      0.42  Q V       |         |         |         |
  2+15       0.0666      0.44  Q V       |         |         |         |
  2+20       0.0697      0.45  Q V       |         |         |         |
  2+25       0.0728      0.45  Q V       |         |         |         |
  2+30       0.0759      0.45  Q V       |         |         |         |
  2+35       0.0790      0.45  Q V       |         |         |         |
  2+40       0.0821      0.45  Q V       |         |         |         |
  2+45       0.0853      0.47  Q  V      |         |         |         |
  2+50       0.0887      0.49  Q  V      |         |         |         |
  2+55       0.0921      0.50  Q  V      |         |         |         |
  3+ 0       0.0955      0.50  Q  V      |         |         |         |
  3+ 5       0.0990      0.50  Q  V      |         |         |         |
  3+10       0.1025      0.52  |Q V      |         |         |         |
  3+15       0.1063      0.54  |Q V      |         |         |         |
  3+20       0.1100      0.55  |Q V      |         |         |         |
  3+25       0.1139      0.57  |Q  V     |         |         |         |
  3+30       0.1181      0.61  |Q  V     |         |         |         |
  3+35       0.1226      0.65  |Q  V     |         |         |         |
  3+40       0.1273      0.69  |Q  V     |         |         |         |
  3+45       0.1325      0.75  |Q  V     |         |         |         |
  3+50       0.1382      0.82  |Q  V     |         |         |         |
  3+55       0.1452      1.02  | Q  V     |         |         |         |
  4+ 0       0.1538      1.26  | Q  V     |         |         |         |
  4+ 5       0.1641      1.49  | Q  V     |         |         |         |
  4+10       0.1773      1.92  |  Q  V    |         |         |         |
  4+15       0.1938      2.39  |   Q V    |         |         |         |
  4+20       0.2137      2.88  |    Q V   |         |         |         |
  4+25       0.2370      3.38  |     Q V  |         |         |         |
  4+30       0.2625      3.70  |      Q V |         |         |         |
  4+35       0.2898      3.97  |      Q  V|         |         |         |
  4+40       0.3202      4.42  |       Q |V         |         |         |
  4+45       0.3539      4.89  |         Q| V       |         |         |
  4+50       0.3898      5.21  |          Q  V      |         |         |
  4+55       0.4275      5.47  |          Q    V    |         |         |
  5+ 0       0.4682      5.92  |          |Q    V   |         |         |
  5+ 5       0.5171      7.10  |          |   Q   V |         |         |
  5+10       0.5806      9.21  |          |       Q V         |         |
  5+15       0.6577     11.20  |          |         | QV      |         |
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    5+20       0.7461     12.83  |          |          |    QV    |          |
    5+25       0.8475     14.74  |          |          |         QV          |
    5+30       0.9700     17.78  |          |          |          |   VQ     |
    5+35       1.0648     13.77  |          |          |       Q  |      V   |
    5+40       1.0992      4.99  |          Q          |          |          V|
    5+45       1.1137      2.11  |    Q     |          |          |          V|
    5+50       1.1209      1.04  |  Q       |          |          |          V|
    5+55       1.1241      0.47  Q          |          |          |          V|
    6+ 0       1.1254      0.18  Q          |          |          |          V|
    6+ 5       1.1259      0.08  Q          |          |          |          V|
    6+10       1.1261      0.03  Q          |          |          |          V|
    6+15       1.1262      0.01  Q          |          |          |          V|
    6+20       1.1262      0.00  Q          |          |          |          V|
    6+25       1.1262      0.00  Q          |          |          |           V
-------------------------------------------------------------------------------
```

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        U n i t   H y d r o g r a p h   A n a l y s i s

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                Study date  04/22/24 File: EX15245.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      26.74(Ac.)  =      0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      26.74(Ac.)  =      0.042 Sq. Mi.
Length along longest watercourse =    1087.00(Ft.)
Length along longest watercourse measured to centroid =     544.00(Ft.)
Length along longest watercourse =      0.206 Mi.
Length along longest watercourse measured to centroid =      0.103 Mi.
Difference in elevation =      88.30(Ft.)
Slope along watercourse =    428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.053 Hr.
Lag time =     3.16 Min.
25% of lag time =     0.79 Min.
40% of lag time =     1.26 Min.
Unit time =     5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           1.80                 48.13

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           5.00                133.70

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    1.800(In)
Area Averaged 100-Year Rainfall =    5.000(In)

Point rain (area averaged) =    2.550(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    2.549(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    26.740           91.00         0.000
 Total Area Entered =     26.74(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.020	(0.437)	0.018	0.002
2	0.17	0.07	0.020	(0.435)	0.018	0.002
3	0.25	0.07	0.020	(0.433)	0.018	0.002
4	0.33	0.10	0.031	(0.432)	0.028	0.003
5	0.42	0.10	0.031	(0.430)	0.028	0.003
6	0.50	0.10	0.031	(0.428)	0.028	0.003
7	0.58	0.10	0.031	(0.427)	0.028	0.003
8	0.67	0.10	0.031	(0.425)	0.028	0.003
9	0.75	0.10	0.031	(0.423)	0.028	0.003
10	0.83	0.13	0.041	(0.422)	0.037	0.004
11	0.92	0.13	0.041	(0.420)	0.037	0.004
12	1.00	0.13	0.041	(0.418)	0.037	0.004
13	1.08	0.10	0.031	(0.417)	0.028	0.003
14	1.17	0.10	0.031	(0.415)	0.028	0.003
15	1.25	0.10	0.031	(0.413)	0.028	0.003
16	1.33	0.10	0.031	(0.412)	0.028	0.003
17	1.42	0.10	0.031	(0.410)	0.028	0.003
18	1.50	0.10	0.031	(0.408)	0.028	0.003
19	1.58	0.10	0.031	(0.407)	0.028	0.003
20	1.67	0.10	0.031	(0.405)	0.028	0.003
21	1.75	0.10	0.031	(0.404)	0.028	0.003
22	1.83	0.13	0.041	(0.402)	0.037	0.004
23	1.92	0.13	0.041	(0.400)	0.037	0.004
24	2.00	0.13	0.041	(0.399)	0.037	0.004
25	2.08	0.13	0.041	(0.397)	0.037	0.004
26	2.17	0.13	0.041	(0.395)	0.037	0.004
27	2.25	0.13	0.041	(0.394)	0.037	0.004
28	2.33	0.13	0.041	(0.392)	0.037	0.004
29	2.42	0.13	0.041	(0.391)	0.037	0.004
30	2.50	0.13	0.041	(0.389)	0.037	0.004
31	2.58	0.17	0.051	(0.387)	0.046	0.005
32	2.67	0.17	0.051	(0.386)	0.046	0.005
33	2.75	0.17	0.051	(0.384)	0.046	0.005
34	2.83	0.17	0.051	(0.383)	0.046	0.005
35	2.92	0.17	0.051	(0.381)	0.046	0.005
36	3.00	0.17	0.051	(0.380)	0.046	0.005
37	3.08	0.17	0.051	(0.378)	0.046	0.005
38	3.17	0.17	0.051	(0.376)	0.046	0.005
39	3.25	0.17	0.051	(0.375)	0.046	0.005
40	3.33	0.17	0.051	(0.373)	0.046	0.005
41	3.42	0.17	0.051	(0.372)	0.046	0.005
42	3.50	0.17	0.051	(0.370)	0.046	0.005
43	3.58	0.17	0.051	(0.369)	0.046	0.005
44	3.67	0.17	0.051	(0.367)	0.046	0.005
45	3.75	0.17	0.051	(0.366)	0.046	0.005
46	3.83	0.20	0.061	(0.364)	0.055	0.006
47	3.92	0.20	0.061	(0.362)	0.055	0.006
48	4.00	0.20	0.061	(0.361)	0.055	0.006
49	4.08	0.20	0.061	(0.359)	0.055	0.006
50	4.17	0.20	0.061	(0.358)	0.055	0.006
51	4.25	0.20	0.061	(0.356)	0.055	0.006
52	4.33	0.23	0.071	(0.355)	0.064	0.007
53	4.42	0.23	0.071	(0.353)	0.064	0.007
54	4.50	0.23	0.071	(0.352)	0.064	0.007
55	4.58	0.23	0.071	(0.350)	0.064	0.007
56	4.67	0.23	0.071	(0.349)	0.064	0.007
57	4.75	0.23	0.071	(0.347)	0.064	0.007
58	4.83	0.27	0.082	(0.346)	0.073	0.008
59	4.92	0.27	0.082	(0.344)	0.073	0.008
60	5.00	0.27	0.082	(0.343)	0.073	0.008
61	5.08	0.20	0.061	(0.341)	0.055	0.006
62	5.17	0.20	0.061	(0.340)	0.055	0.006
63	5.25	0.20	0.061	(0.338)	0.055	0.006
64	5.33	0.23	0.071	(0.337)	0.064	0.007
65	5.42	0.23	0.071	(0.335)	0.064	0.007
66	5.50	0.23	0.071	(0.334)	0.064	0.007
67	5.58	0.27	0.082	(0.332)	0.073	0.008
68	5.67	0.27	0.082	(0.331)	0.073	0.008
69	5.75	0.27	0.082	(0.330)	0.073	0.008
70	5.83	0.27	0.082	(0.328)	0.073	0.008

71	5.92	0.27	0.082	(0.327)	0.073	0.008
72	6.00	0.27	0.082	(0.325)	0.073	0.008
73	6.08	0.30	0.092	(0.324)	0.083	0.009
74	6.17	0.30	0.092	(0.322)	0.083	0.009
75	6.25	0.30	0.092	(0.321)	0.083	0.009
76	6.33	0.30	0.092	(0.319)	0.083	0.009
77	6.42	0.30	0.092	(0.318)	0.083	0.009
78	6.50	0.30	0.092	(0.317)	0.083	0.009
79	6.58	0.33	0.102	(0.315)	0.092	0.010
80	6.67	0.33	0.102	(0.314)	0.092	0.010
81	6.75	0.33	0.102	(0.312)	0.092	0.010
82	6.83	0.33	0.102	(0.311)	0.092	0.010
83	6.92	0.33	0.102	(0.310)	0.092	0.010
84	7.00	0.33	0.102	(0.308)	0.092	0.010
85	7.08	0.33	0.102	(0.307)	0.092	0.010
86	7.17	0.33	0.102	(0.305)	0.092	0.010
87	7.25	0.33	0.102	(0.304)	0.092	0.010
88	7.33	0.37	0.112	(0.303)	0.101	0.011
89	7.42	0.37	0.112	(0.301)	0.101	0.011
90	7.50	0.37	0.112	(0.300)	0.101	0.011
91	7.58	0.40	0.122	(0.298)	0.110	0.012
92	7.67	0.40	0.122	(0.297)	0.110	0.012
93	7.75	0.40	0.122	(0.296)	0.110	0.012
94	7.83	0.43	0.133	(0.294)	0.119	0.013
95	7.92	0.43	0.133	(0.293)	0.119	0.013
96	8.00	0.43	0.133	(0.292)	0.119	0.013
97	8.08	0.50	0.153	(0.290)	0.138	0.015
98	8.17	0.50	0.153	(0.289)	0.138	0.015
99	8.25	0.50	0.153	(0.288)	0.138	0.015
100	8.33	0.50	0.153	(0.286)	0.138	0.015
101	8.42	0.50	0.153	(0.285)	0.138	0.015
102	8.50	0.50	0.153	(0.283)	0.138	0.015
103	8.58	0.53	0.163	(0.282)	0.147	0.016
104	8.67	0.53	0.163	(0.281)	0.147	0.016
105	8.75	0.53	0.163	(0.280)	0.147	0.016
106	8.83	0.57	0.173	(0.278)	0.156	0.017
107	8.92	0.57	0.173	(0.277)	0.156	0.017
108	9.00	0.57	0.173	(0.276)	0.156	0.017
109	9.08	0.63	0.194	(0.274)	0.174	0.019
110	9.17	0.63	0.194	(0.273)	0.174	0.019
111	9.25	0.63	0.194	(0.272)	0.174	0.019
112	9.33	0.67	0.204	(0.270)	0.184	0.020
113	9.42	0.67	0.204	(0.269)	0.184	0.020
114	9.50	0.67	0.204	(0.268)	0.184	0.020
115	9.58	0.70	0.214	(0.267)	0.193	0.021
116	9.67	0.70	0.214	(0.265)	0.193	0.021
117	9.75	0.70	0.214	(0.264)	0.193	0.021
118	9.83	0.73	0.224	(0.263)	0.202	0.022
119	9.92	0.73	0.224	(0.261)	0.202	0.022
120	10.00	0.73	0.224	(0.260)	0.202	0.022
121	10.08	0.50	0.153	(0.259)	0.138	0.015
122	10.17	0.50	0.153	(0.258)	0.138	0.015
123	10.25	0.50	0.153	(0.256)	0.138	0.015
124	10.33	0.50	0.153	(0.255)	0.138	0.015
125	10.42	0.50	0.153	(0.254)	0.138	0.015
126	10.50	0.50	0.153	(0.253)	0.138	0.015
127	10.58	0.67	0.204	(0.251)	0.184	0.020
128	10.67	0.67	0.204	(0.250)	0.184	0.020
129	10.75	0.67	0.204	(0.249)	0.184	0.020
130	10.83	0.67	0.204	(0.248)	0.184	0.020
131	10.92	0.67	0.204	(0.247)	0.184	0.020
132	11.00	0.67	0.204	(0.245)	0.184	0.020
133	11.08	0.63	0.194	(0.244)	0.174	0.019
134	11.17	0.63	0.194	(0.243)	0.174	0.019
135	11.25	0.63	0.194	(0.242)	0.174	0.019
136	11.33	0.63	0.194	(0.241)	0.174	0.019
137	11.42	0.63	0.194	(0.239)	0.174	0.019
138	11.50	0.63	0.194	(0.238)	0.174	0.019
139	11.58	0.57	0.173	(0.237)	0.156	0.017
140	11.67	0.57	0.173	(0.236)	0.156	0.017
141	11.75	0.57	0.173	(0.235)	0.156	0.017
142	11.83	0.60	0.184	(0.233)	0.165	0.018
143	11.92	0.60	0.184	(0.232)	0.165	0.018
144	12.00	0.60	0.184	(0.231)	0.165	0.018
145	12.08	0.83	0.255	(0.230)	0.229	0.025
146	12.17	0.83	0.255	0.229	(0.229)	0.026
147	12.25	0.83	0.255	0.228	(0.229)	0.027
148	12.33	0.87	0.265	0.227	(0.239)	0.039
149	12.42	0.87	0.265	0.225	(0.239)	0.040
150	12.50	0.87	0.265	0.224	(0.239)	0.041
151	12.58	0.93	0.286	0.223	(0.257)	0.062
152	12.67	0.93	0.286	0.222	(0.257)	0.064
153	12.75	0.93	0.286	0.221	(0.257)	0.065
154	12.83	0.97	0.296	0.220	(0.266)	0.076
155	12.92	0.97	0.296	0.219	(0.266)	0.077
156	13.00	0.97	0.296	0.218	(0.266)	0.078

157	13.08	1.13	0.347		0.216	(0.312)	0.130
158	13.17	1.13	0.347		0.215	(0.312)	0.131
159	13.25	1.13	0.347		0.214	(0.312)	0.132
160	13.33	1.13	0.347		0.213	(0.312)	0.134
161	13.42	1.13	0.347		0.212	(0.312)	0.135
162	13.50	1.13	0.347		0.211	(0.312)	0.136
163	13.58	0.77	0.235		0.210	(0.211)	0.025
164	13.67	0.77	0.235		0.209	(0.211)	0.026
165	13.75	0.77	0.235		0.208	(0.211)	0.027
166	13.83	0.77	0.235		0.207	(0.211)	0.028
167	13.92	0.77	0.235		0.206	(0.211)	0.029
168	14.00	0.77	0.235		0.205	(0.211)	0.030
169	14.08	0.90	0.275		0.204	(0.248)	0.072
170	14.17	0.90	0.275		0.203	(0.248)	0.073
171	14.25	0.90	0.275		0.202	(0.248)	0.074
172	14.33	0.87	0.265		0.200	(0.239)	0.065
173	14.42	0.87	0.265		0.199	(0.239)	0.066
174	14.50	0.87	0.265		0.198	(0.239)	0.067
175	14.58	0.87	0.265		0.197	(0.239)	0.068
176	14.67	0.87	0.265		0.196	(0.239)	0.069
177	14.75	0.87	0.265		0.195	(0.239)	0.070
178	14.83	0.83	0.255		0.194	(0.229)	0.061
179	14.92	0.83	0.255		0.193	(0.229)	0.062
180	15.00	0.83	0.255		0.192	(0.229)	0.063
181	15.08	0.80	0.245		0.191	(0.220)	0.053
182	15.17	0.80	0.245		0.190	(0.220)	0.054
183	15.25	0.80	0.245		0.189	(0.220)	0.055
184	15.33	0.77	0.235		0.188	(0.211)	0.046
185	15.42	0.77	0.235		0.188	(0.211)	0.047
186	15.50	0.77	0.235		0.187	(0.211)	0.048
187	15.58	0.63	0.194	(0.186)		0.174	0.019
188	15.67	0.63	0.194	(0.185)		0.174	0.019
189	15.75	0.63	0.194	(0.184)		0.174	0.019
190	15.83	0.63	0.194	(0.183)		0.174	0.019
191	15.92	0.63	0.194	(0.182)		0.174	0.019
192	16.00	0.63	0.194	(0.181)		0.174	0.019
193	16.08	0.13	0.041	(0.180)		0.037	0.004
194	16.17	0.13	0.041	(0.179)		0.037	0.004
195	16.25	0.13	0.041	(0.178)		0.037	0.004
196	16.33	0.13	0.041	(0.177)		0.037	0.004
197	16.42	0.13	0.041	(0.176)		0.037	0.004
198	16.50	0.13	0.041	(0.175)		0.037	0.004
199	16.58	0.10	0.031	(0.175)		0.028	0.003
200	16.67	0.10	0.031	(0.174)		0.028	0.003
201	16.75	0.10	0.031	(0.173)		0.028	0.003
202	16.83	0.10	0.031	(0.172)		0.028	0.003
203	16.92	0.10	0.031	(0.171)		0.028	0.003
204	17.00	0.10	0.031	(0.170)		0.028	0.003
205	17.08	0.17	0.051	(0.169)		0.046	0.005
206	17.17	0.17	0.051	(0.168)		0.046	0.005
207	17.25	0.17	0.051	(0.168)		0.046	0.005
208	17.33	0.17	0.051	(0.167)		0.046	0.005
209	17.42	0.17	0.051	(0.166)		0.046	0.005
210	17.50	0.17	0.051	(0.165)		0.046	0.005
211	17.58	0.17	0.051	(0.164)		0.046	0.005
212	17.67	0.17	0.051	(0.163)		0.046	0.005
213	17.75	0.17	0.051	(0.163)		0.046	0.005
214	17.83	0.13	0.041	(0.162)		0.037	0.004
215	17.92	0.13	0.041	(0.161)		0.037	0.004
216	18.00	0.13	0.041	(0.160)		0.037	0.004
217	18.08	0.13	0.041	(0.159)		0.037	0.004
218	18.17	0.13	0.041	(0.159)		0.037	0.004
219	18.25	0.13	0.041	(0.158)		0.037	0.004
220	18.33	0.13	0.041	(0.157)		0.037	0.004
221	18.42	0.13	0.041	(0.156)		0.037	0.004
222	18.50	0.13	0.041	(0.156)		0.037	0.004
223	18.58	0.10	0.031	(0.155)		0.028	0.003
224	18.67	0.10	0.031	(0.154)		0.028	0.003
225	18.75	0.10	0.031	(0.153)		0.028	0.003
226	18.83	0.07	0.020	(0.153)		0.018	0.002
227	18.92	0.07	0.020	(0.152)		0.018	0.002
228	19.00	0.07	0.020	(0.151)		0.018	0.002
229	19.08	0.10	0.031	(0.150)		0.028	0.003
230	19.17	0.10	0.031	(0.150)		0.028	0.003
231	19.25	0.10	0.031	(0.149)		0.028	0.003
232	19.33	0.13	0.041	(0.148)		0.037	0.004
233	19.42	0.13	0.041	(0.148)		0.037	0.004
234	19.50	0.13	0.041	(0.147)		0.037	0.004
235	19.58	0.10	0.031	(0.146)		0.028	0.003
236	19.67	0.10	0.031	(0.146)		0.028	0.003
237	19.75	0.10	0.031	(0.145)		0.028	0.003
238	19.83	0.07	0.020	(0.144)		0.018	0.002
239	19.92	0.07	0.020	(0.144)		0.018	0.002
240	20.00	0.07	0.020	(0.143)		0.018	0.002
241	20.08	0.10	0.031	(0.142)		0.028	0.003
242	20.17	0.10	0.031	(0.142)		0.028	0.003

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243  20.25     0.10      0.031       (  0.141)       0.028        0.003
244  20.33     0.10      0.031       (  0.141)       0.028        0.003
245  20.42     0.10      0.031       (  0.140)       0.028        0.003
246  20.50     0.10      0.031       (  0.139)       0.028        0.003
247  20.58     0.10      0.031       (  0.139)       0.028        0.003
248  20.67     0.10      0.031       (  0.138)       0.028        0.003
249  20.75     0.10      0.031       (  0.138)       0.028        0.003
250  20.83     0.07      0.020       (  0.137)       0.018        0.002
251  20.92     0.07      0.020       (  0.137)       0.018        0.002
252  21.00     0.07      0.020       (  0.136)       0.018        0.002
253  21.08     0.10      0.031       (  0.135)       0.028        0.003
254  21.17     0.10      0.031       (  0.135)       0.028        0.003
255  21.25     0.10      0.031       (  0.134)       0.028        0.003
256  21.33     0.07      0.020       (  0.134)       0.018        0.002
257  21.42     0.07      0.020       (  0.133)       0.018        0.002
258  21.50     0.07      0.020       (  0.133)       0.018        0.002
259  21.58     0.10      0.031       (  0.132)       0.028        0.003
260  21.67     0.10      0.031       (  0.132)       0.028        0.003
261  21.75     0.10      0.031       (  0.131)       0.028        0.003
262  21.83     0.07      0.020       (  0.131)       0.018        0.002
263  21.92     0.07      0.020       (  0.131)       0.018        0.002
264  22.00     0.07      0.020       (  0.130)       0.018        0.002
265  22.08     0.10      0.031       (  0.130)       0.028        0.003
266  22.17     0.10      0.031       (  0.129)       0.028        0.003
267  22.25     0.10      0.031       (  0.129)       0.028        0.003
268  22.33     0.07      0.020       (  0.128)       0.018        0.002
269  22.42     0.07      0.020       (  0.128)       0.018        0.002
270  22.50     0.07      0.020       (  0.128)       0.018        0.002
271  22.58     0.07      0.020       (  0.127)       0.018        0.002
272  22.67     0.07      0.020       (  0.127)       0.018        0.002
273  22.75     0.07      0.020       (  0.127)       0.018        0.002
274  22.83     0.07      0.020       (  0.126)       0.018        0.002
275  22.92     0.07      0.020       (  0.126)       0.018        0.002
276  23.00     0.07      0.020       (  0.126)       0.018        0.002
277  23.08     0.07      0.020       (  0.125)       0.018        0.002
278  23.17     0.07      0.020       (  0.125)       0.018        0.002
279  23.25     0.07      0.020       (  0.125)       0.018        0.002
280  23.33     0.07      0.020       (  0.125)       0.018        0.002
281  23.42     0.07      0.020       (  0.124)       0.018        0.002
282  23.50     0.07      0.020       (  0.124)       0.018        0.002
283  23.58     0.07      0.020       (  0.124)       0.018        0.002
284  23.67     0.07      0.020       (  0.124)       0.018        0.002
285  23.75     0.07      0.020       (  0.124)       0.018        0.002
286  23.83     0.07      0.020       (  0.123)       0.018        0.002
287  23.92     0.07      0.020       (  0.123)       0.018        0.002
288  24.00     0.07      0.020       (  0.123)       0.018        0.002
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =      4.6
      Flood volume = Effective rainfall      0.38(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       0.9(Ac.Ft)
      Total soil loss =      2.17(In)
      Total soil loss =     4.825(Ac.Ft)
      Total rainfall =      2.55(In)
      Flood volume =       37286.0 Cubic Feet
      Total soil loss =      210173.0 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      3.631(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0001      0.02  Q          |         |         |         |
   0+10       0.0004      0.04  Q          |         |         |         |
   0+15       0.0008      0.05  Q          |         |         |         |
   0+20       0.0012      0.06  Q          |         |         |         |
   0+25       0.0018      0.08  Q          |         |         |         |
   0+30       0.0023      0.08  Q          |         |         |         |
   0+35       0.0029      0.08  Q          |         |         |         |
   0+40       0.0034      0.08  Q          |         |         |         |
   0+45       0.0040      0.08  Q          |         |         |         |
   0+50       0.0046      0.09  Q          |         |         |         |
   0+55       0.0054      0.10  Q          |         |         |         |
   1+ 0       0.0061      0.11  Q          |         |         |         |
   1+ 5       0.0068      0.10  Q          |         |         |         |
   1+10       0.0074      0.09  Q          |         |         |         |
   1+15       0.0080      0.08  Q          |         |         |         |
   1+20       0.0085      0.08  Q          |         |         |         |
   1+25       0.0091      0.08  Q          |         |         |         |
   1+30       0.0097      0.08  Q          |         |         |         |
   1+35       0.0103      0.08  Q          |         |         |         |
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1+40	0.0108	0.08	Q	|	|	|	|
1+45	0.0114	0.08	Q	|	|	|	|
1+50	0.0120	0.09	Q	|	|	|	|
1+55	0.0127	0.10	Q	|	|	|	|
2+ 0	0.0135	0.11	Q	|	|	|	|
2+ 5	0.0142	0.11	Q	|	|	|	|
2+10	0.0150	0.11	Q	|	|	|	|
2+15	0.0158	0.11	Q	|	|	|	|
2+20	0.0165	0.11	Q	|	|	|	|
2+25	0.0173	0.11	Q	|	|	|	|
2+30	0.0180	0.11	Q	|	|	|	|
2+35	0.0189	0.12	Q	|	|	|	|
2+40	0.0198	0.13	Q	|	|	|	|
2+45	0.0207	0.14	Q	|	|	|	|
2+50	0.0216	0.14	QV	|	|	|	|
2+55	0.0226	0.14	QV	|	|	|	|
3+ 0	0.0235	0.14	QV	|	|	|	|
3+ 5	0.0245	0.14	QV	|	|	|	|
3+10	0.0254	0.14	QV	|	|	|	|
3+15	0.0264	0.14	QV	|	|	|	|
3+20	0.0273	0.14	QV	|	|	|	|
3+25	0.0283	0.14	QV	|	|	|	|
3+30	0.0292	0.14	QV	|	|	|	|
3+35	0.0302	0.14	QV	|	|	|	|
3+40	0.0311	0.14	QV	|	|	|	|
3+45	0.0320	0.14	QV	|	|	|	|
3+50	0.0331	0.15	QV	|	|	|	|
3+55	0.0342	0.16	QV	|	|	|	|
4+ 0	0.0353	0.16	QV	|	|	|	|
4+ 5	0.0364	0.16	QV	|	|	|	|
4+10	0.0375	0.16	QV	|	|	|	|
4+15	0.0387	0.16	QV	|	|	|	|
4+20	0.0399	0.17	QV	|	|	|	|
4+25	0.0412	0.19	QV	|	|	|	|
4+30	0.0425	0.19	QV	|	|	|	|
4+35	0.0438	0.19	Q V	|	|	|	|
4+40	0.0451	0.19	Q V	|	|	|	|
4+45	0.0465	0.19	Q V	|	|	|	|
4+50	0.0479	0.20	Q V	|	|	|	|
4+55	0.0493	0.21	Q V	|	|	|	|
5+ 0	0.0508	0.22	Q V	|	|	|	|
5+ 5	0.0522	0.20	Q V	|	|	|	|
5+10	0.0534	0.17	Q V	|	|	|	|
5+15	0.0546	0.17	Q V	|	|	|	|
5+20	0.0558	0.18	Q V	|	|	|	|
5+25	0.0571	0.19	Q V	|	|	|	|
5+30	0.0584	0.19	Q V	|	|	|	|
5+35	0.0598	0.20	Q V	|	|	|	|
5+40	0.0613	0.21	Q V	|	|	|	|
5+45	0.0628	0.22	Q V	|	|	|	|
5+50	0.0643	0.22	Q V	|	|	|	|
5+55	0.0658	0.22	Q V	|	|	|	|
6+ 0	0.0673	0.22	Q V	|	|	|	|
6+ 5	0.0689	0.23	Q V	|	|	|	|
6+10	0.0705	0.24	Q V	|	|	|	|
6+15	0.0722	0.25	Q V	|	|	|	|
6+20	0.0739	0.25	Q V	|	|	|	|
6+25	0.0756	0.25	Q V	|	|	|	|
6+30	0.0773	0.25	Q V	|	|	|	|
6+35	0.0791	0.26	|Q V	|	|	|	|
6+40	0.0810	0.27	|Q V	|	|	|	|
6+45	0.0829	0.27	|Q V	|	|	|	|
6+50	0.0847	0.27	|Q V	|	|	|	|
6+55	0.0866	0.27	|Q V	|	|	|	|
7+ 0	0.0885	0.27	|Q V	|	|	|	|
7+ 5	0.0904	0.27	|Q V	|	|	|	|
7+10	0.0923	0.27	|Q V	|	|	|	|
7+15	0.0942	0.27	|Q V	|	|	|	|
7+20	0.0962	0.28	|Q V	|	|	|	|
7+25	0.0982	0.30	|Q V	|	|	|	|
7+30	0.1003	0.30	|Q V	|	|	|	|
7+35	0.1024	0.31	|Q V	|	|	|	|
7+40	0.1047	0.32	|Q V	|	|	|	|
7+45	0.1069	0.33	|Q V	|	|	|	|
7+50	0.1093	0.34	|Q V	|	|	|	|
7+55	0.1117	0.35	|Q V	|	|	|	|
8+ 0	0.1141	0.36	|Q V	|	|	|	|
8+ 5	0.1167	0.38	|Q V	|	|	|	|
8+10	0.1195	0.40	|Q V	|	|	|	|
8+15	0.1223	0.41	|Q V	|	|	|	|
8+20	0.1251	0.41	|Q V	|	|	|	|
8+25	0.1280	0.41	|Q V	|	|	|	|
8+30	0.1308	0.41	|Q V	|	|	|	|
8+35	0.1337	0.42	|Q V	|	|	|	|
8+40	0.1367	0.43	|Q V	|	|	|	|
8+45	0.1397	0.44	|Q V	|	|	|	|

8+50	0.1428	0.45	
8+55	0.1460	0.46	
9+ 0	0.1492	0.47	
9+ 5	0.1525	0.49	
9+10	0.1561	0.51	
9+15	0.1596	0.52	
9+20	0.1633	0.53	
9+25	0.1670	0.54	
9+30	0.1708	0.55	
9+35	0.1747	0.56	
9+40	0.1786	0.57	
9+45	0.1826	0.58	
9+50	0.1866	0.59	
9+55	0.1907	0.60	
10+ 0	0.1949	0.60	
10+ 5	0.1986	0.54	
10+10	0.2017	0.45	
10+15	0.2046	0.43	
10+20	0.2075	0.42	
10+25	0.2103	0.41	
10+30	0.2132	0.41	
10+35	0.2163	0.46	
10+40	0.2200	0.52	
10+45	0.2237	0.54	
10+50	0.2274	0.55	
10+55	0.2312	0.55	
11+ 0	0.2350	0.55	
11+ 5	0.2387	0.54	
11+10	0.2423	0.53	
11+15	0.2460	0.52	
11+20	0.2496	0.52	
11+25	0.2532	0.52	
11+30	0.2568	0.52	
11+35	0.2602	0.50	
11+40	0.2635	0.48	
11+45	0.2668	0.47	
11+50	0.2701	0.48	
11+55	0.2734	0.49	
12+ 0	0.2768	0.49	
12+ 5	0.2807	0.56	
12+10	0.2852	0.66	
12+15	0.2900	0.70	
12+20	0.2957	0.83	
12+25	0.3026	0.99	
12+30	0.3098	1.05	
12+35	0.3187	1.29	
12+40	0.3296	1.58	
12+45	0.3411	1.67	
12+50	0.3536	1.82	
12+55	0.3674	1.99	
13+ 0	0.3815	2.06	
13+ 5	0.3993	2.58	
13+10	0.4218	3.26	
13+15	0.4454	3.44	
13+20	0.4697	3.53	
13+25	0.4945	3.59	
13+30	0.5195	3.63	
13+35	0.5374	2.60	
13+40	0.5458	1.22	
13+45	0.5522	0.93	
13+50	0.5578	0.82	
13+55	0.5632	0.78	
14+ 0	0.5685	0.78	
14+ 5	0.5768	1.19	
14+10	0.5887	1.73	
14+15	0.6016	1.88	
14+20	0.6144	1.86	
14+25	0.6267	1.79	
14+30	0.6391	1.79	
14+35	0.6515	1.81	
14+40	0.6641	1.83	
14+45	0.6769	1.85	
14+50	0.6892	1.78	
14+55	0.7008	1.68	
15+ 0	0.7124	1.68	
15+ 5	0.7234	1.60	
15+10	0.7337	1.49	
15+15	0.7439	1.49	
15+20	0.7536	1.40	
15+25	0.7625	1.30	
15+30	0.7714	1.29	
15+35	0.7784	1.02	
15+40	0.7830	0.66	
15+45	0.7870	0.58	
15+50	0.7908	0.55	
15+55	0.7944	0.53	

16+ 0	0.7980	0.52	| Q	|	|	|	V |
16+ 5	0.8006	0.38	|Q	|	|	|	V |
16+10	0.8019	0.19	Q	|	|	|	V |
16+15	0.8029	0.14	Q	|	|	|	V |
16+20	0.8037	0.12	Q	|	|	|	V |
16+25	0.8045	0.11	Q	|	|	|	V |
16+30	0.8053	0.11	Q	|	|	|	V |
16+35	0.8059	0.10	Q	|	|	|	V |
16+40	0.8066	0.09	Q	|	|	|	V |
16+45	0.8071	0.08	Q	|	|	|	V |
16+50	0.8077	0.08	Q	|	|	|	V |
16+55	0.8083	0.08	Q	|	|	|	V |
17+ 0	0.8088	0.08	Q	|	|	|	V |
17+ 5	0.8095	0.10	Q	|	|	|	V |
17+10	0.8104	0.13	Q	|	|	|	V |
17+15	0.8113	0.13	Q	|	|	|	V |
17+20	0.8123	0.14	Q	|	|	|	V |
17+25	0.8132	0.14	Q	|	|	|	V |
17+30	0.8142	0.14	Q	|	|	|	V |
17+35	0.8151	0.14	Q	|	|	|	V |
17+40	0.8161	0.14	Q	|	|	|	V |
17+45	0.8170	0.14	Q	|	|	|	V |
17+50	0.8179	0.13	Q	|	|	|	V |
17+55	0.8187	0.12	Q	|	|	|	V |
18+ 0	0.8195	0.11	Q	|	|	|	V |
18+ 5	0.8202	0.11	Q	|	|	|	V |
18+10	0.8210	0.11	Q	|	|	|	V |
18+15	0.8217	0.11	Q	|	|	|	V |
18+20	0.8225	0.11	Q	|	|	|	V |
18+25	0.8232	0.11	Q	|	|	|	V |
18+30	0.8240	0.11	Q	|	|	|	V |
18+35	0.8247	0.10	Q	|	|	|	V |
18+40	0.8253	0.09	Q	|	|	|	V |
18+45	0.8259	0.08	Q	|	|	|	V |
18+50	0.8264	0.07	Q	|	|	|	V |
18+55	0.8268	0.06	Q	|	|	|	V |
19+ 0	0.8272	0.06	Q	|	|	|	V |
19+ 5	0.8276	0.07	Q	|	|	|	V |
19+10	0.8282	0.08	Q	|	|	|	V |
19+15	0.8287	0.08	Q	|	|	|	V |
19+20	0.8294	0.09	Q	|	|	|	V |
19+25	0.8301	0.10	Q	|	|	|	V |
19+30	0.8308	0.11	Q	|	|	|	V |
19+35	0.8315	0.10	Q	|	|	|	V |
19+40	0.8321	0.09	Q	|	|	|	V |
19+45	0.8327	0.08	Q	|	|	|	V |
19+50	0.8332	0.07	Q	|	|	|	V |
19+55	0.8336	0.06	Q	|	|	|	V |
20+ 0	0.8340	0.06	Q	|	|	|	V |
20+ 5	0.8345	0.07	Q	|	|	|	V |
20+10	0.8350	0.08	Q	|	|	|	V|
20+15	0.8356	0.08	Q	|	|	|	V|
20+20	0.8361	0.08	Q	|	|	|	V|
20+25	0.8367	0.08	Q	|	|	|	V|
20+30	0.8373	0.08	Q	|	|	|	V|
20+35	0.8378	0.08	Q	|	|	|	V|
20+40	0.8384	0.08	Q	|	|	|	V|
20+45	0.8390	0.08	Q	|	|	|	V|
20+50	0.8395	0.07	Q	|	|	|	V|
20+55	0.8399	0.06	Q	|	|	|	V|
21+ 0	0.8403	0.06	Q	|	|	|	V|
21+ 5	0.8407	0.07	Q	|	|	|	V|
21+10	0.8412	0.08	Q	|	|	|	V|
21+15	0.8418	0.08	Q	|	|	|	V|
21+20	0.8423	0.07	Q	|	|	|	V|
21+25	0.8427	0.06	Q	|	|	|	V|
21+30	0.8431	0.06	Q	|	|	|	V|
21+35	0.8436	0.07	Q	|	|	|	V|
21+40	0.8441	0.08	Q	|	|	|	V|
21+45	0.8446	0.08	Q	|	|	|	V|
21+50	0.8451	0.07	Q	|	|	|	V|
21+55	0.8456	0.06	Q	|	|	|	V|
22+ 0	0.8459	0.06	Q	|	|	|	V|
22+ 5	0.8464	0.07	Q	|	|	|	V|
22+10	0.8469	0.08	Q	|	|	|	V|
22+15	0.8475	0.08	Q	|	|	|	V|
22+20	0.8480	0.07	Q	|	|	|	V|
22+25	0.8484	0.06	Q	|	|	|	V|
22+30	0.8488	0.06	Q	|	|	|	V|
22+35	0.8492	0.06	Q	|	|	|	V|
22+40	0.8495	0.06	Q	|	|	|	V|
22+45	0.8499	0.05	Q	|	|	|	V|
22+50	0.8503	0.05	Q	|	|	|	V|
22+55	0.8507	0.05	Q	|	|	|	V|
23+ 0	0.8511	0.05	Q	|	|	|	V|
23+ 5	0.8514	0.05	Q	|	|	|	V|

```
   23+10       0.8518      0.05  Q          |          |          |        v|
   23+15       0.8522      0.05  Q          |          |          |        v|
   23+20       0.8526      0.05  Q          |          |          |        v|
   23+25       0.8530      0.05  Q          |          |          |        v|
   23+30       0.8533      0.05  Q          |          |          |        v|
   23+35       0.8537      0.05  Q          |          |          |        v|
   23+40       0.8541      0.05  Q          |          |          |        v|
   23+45       0.8545      0.05  Q          |          |          |        v|
   23+50       0.8549      0.05  Q          |          |          |        v|
   23+55       0.8552      0.05  Q          |          |          |        v|
   24+ 0       0.8556      0.05  Q          |          |          |        v|
   24+ 5       0.8559      0.04  Q          |          |          |        v|
   24+10       0.8559      0.01  Q          |          |          |        v|
   24+15       0.8560      0.00  Q          |          |          |        v|
   24+20       0.8560      0.00  Q          |          |          |        v|
   24+25       0.8560      0.00  Q          |          |          |         v
---------------------------------------------------------------------------
```

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        U n i t   H y d r o g r a p h   A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      26.74(Ac.)  =      0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      26.74(Ac.)  =      0.042 Sq. Mi.
Length along longest watercourse =    1087.00(Ft.)
Length along longest watercourse measured to centroid =     544.00(Ft.)
Length along longest watercourse =      0.206 Mi.
Length along longest watercourse measured to centroid =      0.103 Mi.
Difference in elevation =      88.30(Ft.)
Slope along watercourse =    428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.053 Hr.
Lag time =     3.16 Min.
25% of lag time =     0.79 Min.
40% of lag time =     1.26 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           0.50                 13.37

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           1.30                 34.76

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.829(In)
Areal adjustment factor =   99.98 %
Adjusted average point rain =    0.829(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    26.740           91.00         0.000
 Total Area Entered =     26.74(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  91.0      0.117     0.000        0.117       1.000      0.117
                                                 Sum (F) =   0.117
Area averaged mean soil loss (F) (In/Hr) =  0.117
Minimum soil loss rate ((In/Hr)) =  0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
		Sum = 100.000	Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.328	0.117	(0.295)	0.211
2	0.17	4.20	0.418	0.117	(0.376)	0.301
3	0.25	4.40	0.438	0.117	(0.394)	0.321
4	0.33	4.80	0.477	0.117	(0.430)	0.360
5	0.42	5.20	0.517	0.117	(0.466)	0.400
6	0.50	6.20	0.617	0.117	(0.555)	0.500
7	0.58	6.80	0.676	0.117	(0.609)	0.559
8	0.67	8.80	0.875	0.117	(0.788)	0.758
9	0.75	13.90	1.383	0.117	(1.244)	1.266
10	0.83	31.40	3.123	0.117	(2.811)	3.006
11	0.92	7.20	0.716	0.117	(0.645)	0.599
12	1.00	3.80	0.378	0.117	(0.340)	0.261
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	8.5

Flood volume = Effective rainfall 0.71(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 1.6(Ac.Ft)
Total soil loss = 0.12(In)
Total soil loss = 0.261(Ac.Ft)
Total rainfall = 0.83(In)
Flood volume = 69103.9 Cubic Feet
Total soil loss = 11356.7 Cubic Feet

Peak flow rate of this hydrograph = 48.345(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	12.5	25.0	37.5	50.0
0+ 5	0.0138	2.00	VQ				
0+10	0.0516	5.49	V Q				
0+15	0.1026	7.41	V Q				
0+20	0.1616	8.56	V Q				
0+25	0.2286	9.73	V Q				
0+30	0.3072	11.41	V Q				
0+35	0.3996	13.42	Q				
0+40	0.5127	16.42	VQ				
0+45	0.6783	24.04		V Q			
0+50	1.0061	47.60			V		Q
0+55	1.3391	48.34				V	Q
1+ 0	1.4825	20.83		Q		V	
1+ 5	1.5493	9.70	Q				V
1+10	1.5743	3.62	Q				V
1+15	1.5839	1.40	Q				V
1+20	1.5860	0.30	Q				V
1+25	1.5864	0.06	Q				V

U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 1087.00(Ft.)
Length along longest watercourse measured to centroid = 544.00(Ft.)
Length along longest watercourse = 0.206 Mi.
Length along longest watercourse measured to centroid = 0.103 Mi.
Difference in elevation = 88.30(Ft.)
Slope along watercourse = 428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	0.80	21.39

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	2.00	53.48

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 1.294(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.294(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.000

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.202	0.117	(0.182)	0.085
2	0.17	1.30	0.202	0.117	(0.182)	0.085
3	0.25	1.10	0.171	0.117	(0.154)	0.054
4	0.33	1.50	0.233	0.117	(0.210)	0.116
5	0.42	1.50	0.233	0.117	(0.210)	0.116
6	0.50	1.80	0.279	0.117	(0.251)	0.162
7	0.58	1.50	0.233	0.117	(0.210)	0.116
8	0.67	1.80	0.279	0.117	(0.251)	0.162
9	0.75	1.80	0.279	0.117	(0.251)	0.162
10	0.83	1.50	0.233	0.117	(0.210)	0.116
11	0.92	1.60	0.248	0.117	(0.224)	0.131
12	1.00	1.80	0.279	0.117	(0.251)	0.162
13	1.08	2.20	0.341	0.117	(0.307)	0.224
14	1.17	2.20	0.341	0.117	(0.307)	0.224
15	1.25	2.20	0.341	0.117	(0.307)	0.224
16	1.33	2.00	0.310	0.117	(0.279)	0.193
17	1.42	2.60	0.404	0.117	(0.363)	0.287
18	1.50	2.70	0.419	0.117	(0.377)	0.302
19	1.58	2.40	0.373	0.117	(0.335)	0.256
20	1.67	2.70	0.419	0.117	(0.377)	0.302
21	1.75	3.30	0.512	0.117	(0.461)	0.395
22	1.83	3.10	0.481	0.117	(0.433)	0.364
23	1.92	2.90	0.450	0.117	(0.405)	0.333
24	2.00	3.00	0.466	0.117	(0.419)	0.349
25	2.08	3.10	0.481	0.117	(0.433)	0.364
26	2.17	4.20	0.652	0.117	(0.587)	0.535
27	2.25	5.00	0.776	0.117	(0.699)	0.659
28	2.33	3.50	0.543	0.117	(0.489)	0.426
29	2.42	6.80	1.056	0.117	(0.950)	0.939
30	2.50	7.30	1.133	0.117	(1.020)	1.016
31	2.58	8.20	1.273	0.117	(1.146)	1.156
32	2.67	5.90	0.916	0.117	(0.824)	0.799
33	2.75	2.00	0.310	0.117	(0.279)	0.193
34	2.83	1.80	0.279	0.117	(0.251)	0.162
35	2.92	1.80	0.279	0.117	(0.251)	0.162
36	3.00	0.60	0.093	(0.117)	0.084	0.009
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	11.3

Flood volume = Effective rainfall 0.95(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 2.1(Ac.Ft)
Total soil loss = 0.35(In)
Total soil loss = 0.776(Ac.Ft)
Total rainfall = 1.29(In)
Flood volume = 91757.0 Cubic Feet
Total soil loss = 33801.9 Cubic Feet

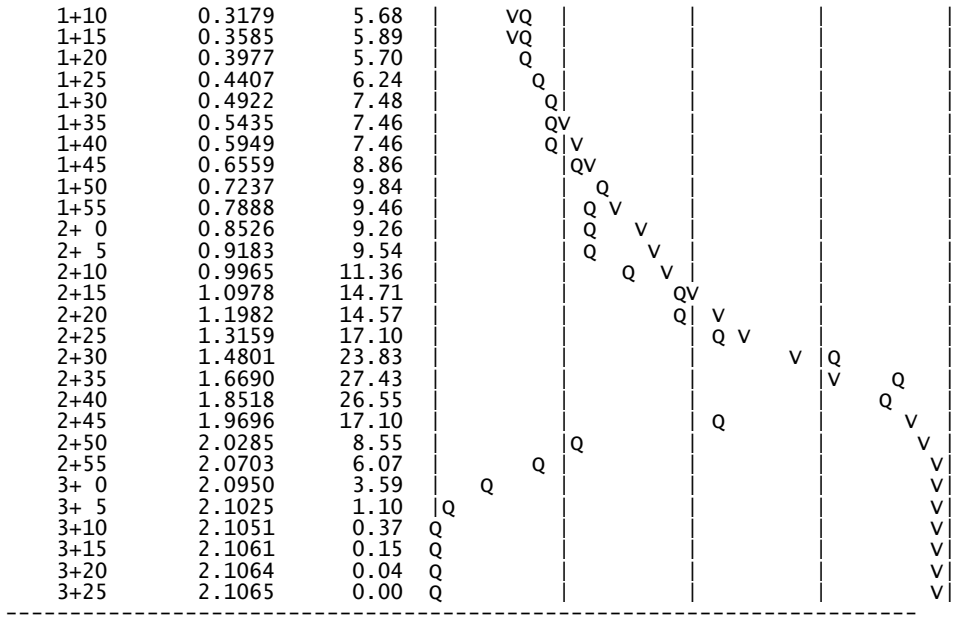
Peak flow rate of this hydrograph = 27.430(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0055	0.80	VQ				
0+10	0.0184	1.86	V Q				
0+15	0.0309	1.81	V Q				
0+20	0.0455	2.12	V Q				
0+25	0.0652	2.86	V Q				
0+30	0.0890	3.46	V Q				
0+35	0.1142	3.66	V Q				
0+40	0.1396	3.68	V Q				
0+45	0.1685	4.21	V Q				
0+50	0.1952	3.87	V Q				
0+55	0.2191	3.47	Q				
1+ 0	0.2456	3.84	VQ				
1+ 5	0.2788	4.82	VQ				



1+10	0.3179	5.68	
1+15	0.3585	5.89	
1+20	0.3977	5.70	
1+25	0.4407	6.24	
1+30	0.4922	7.48	
1+35	0.5435	7.46	
1+40	0.5949	7.46	
1+45	0.6559	8.86	
1+50	0.7237	9.84	
1+55	0.7888	9.46	
2+ 0	0.8526	9.26	
2+ 5	0.9183	9.54	
2+10	0.9965	11.36	
2+15	1.0978	14.71	
2+20	1.1982	14.57	
2+25	1.3159	17.10	
2+30	1.4801	23.83	
2+35	1.6690	27.43	
2+40	1.8518	26.55	
2+45	1.9696	17.10	
2+50	2.0285	8.55	
2+55	2.0703	6.07	
3+ 0	2.0950	3.59	
3+ 5	2.1025	1.10	
3+10	2.1051	0.37	
3+15	2.1061	0.15	
3+20	2.1064	0.04	
3+25	2.1065	0.00	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX110610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 1087.00(Ft.)
Length along longest watercourse measured to centroid = 544.00(Ft.)
Length along longest watercourse = 0.206 Mi.
Length along longest watercourse measured to centroid = 0.103 Mi.
Difference in elevation = 88.30(Ft.)
Slope along watercourse = 428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.10	29.41

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	3.00	80.22

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.882(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.882(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.000

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.113	(0.117)	0.102	0.011
2	0.17	0.60	0.135	0.117	(0.122)	0.018
3	0.25	0.60	0.135	0.117	(0.122)	0.018
4	0.33	0.60	0.135	0.117	(0.122)	0.018
5	0.42	0.60	0.135	0.117	(0.122)	0.018
6	0.50	0.70	0.158	0.117	(0.142)	0.041
7	0.58	0.70	0.158	0.117	(0.142)	0.041
8	0.67	0.70	0.158	0.117	(0.142)	0.041
9	0.75	0.70	0.158	0.117	(0.142)	0.041
10	0.83	0.70	0.158	0.117	(0.142)	0.041
11	0.92	0.70	0.158	0.117	(0.142)	0.041
12	1.00	0.80	0.181	0.117	(0.163)	0.064
13	1.08	0.80	0.181	0.117	(0.163)	0.064
14	1.17	0.80	0.181	0.117	(0.163)	0.064
15	1.25	0.80	0.181	0.117	(0.163)	0.064
16	1.33	0.80	0.181	0.117	(0.163)	0.064
17	1.42	0.80	0.181	0.117	(0.163)	0.064
18	1.50	0.80	0.181	0.117	(0.163)	0.064
19	1.58	0.80	0.181	0.117	(0.163)	0.064
20	1.67	0.80	0.181	0.117	(0.163)	0.064
21	1.75	0.80	0.181	0.117	(0.163)	0.064
22	1.83	0.80	0.181	0.117	(0.163)	0.064
23	1.92	0.80	0.181	0.117	(0.163)	0.064
24	2.00	0.90	0.203	0.117	(0.183)	0.086
25	2.08	0.80	0.181	0.117	(0.163)	0.064
26	2.17	0.90	0.203	0.117	(0.183)	0.086
27	2.25	0.90	0.203	0.117	(0.183)	0.086
28	2.33	0.90	0.203	0.117	(0.183)	0.086
29	2.42	0.90	0.203	0.117	(0.183)	0.086
30	2.50	0.90	0.203	0.117	(0.183)	0.086
31	2.58	0.90	0.203	0.117	(0.183)	0.086
32	2.67	0.90	0.203	0.117	(0.183)	0.086
33	2.75	1.00	0.226	0.117	(0.203)	0.109
34	2.83	1.00	0.226	0.117	(0.203)	0.109
35	2.92	1.00	0.226	0.117	(0.203)	0.109
36	3.00	1.00	0.226	0.117	(0.203)	0.109
37	3.08	1.00	0.226	0.117	(0.203)	0.109
38	3.17	1.10	0.248	0.117	(0.224)	0.131
39	3.25	1.10	0.248	0.117	(0.224)	0.131
40	3.33	1.10	0.248	0.117	(0.224)	0.131
41	3.42	1.20	0.271	0.117	(0.244)	0.154
42	3.50	1.30	0.294	0.117	(0.264)	0.177
43	3.58	1.40	0.316	0.117	(0.284)	0.199
44	3.67	1.40	0.316	0.117	(0.284)	0.199
45	3.75	1.50	0.339	0.117	(0.305)	0.222
46	3.83	1.50	0.339	0.117	(0.305)	0.222
47	3.92	1.60	0.361	0.117	(0.325)	0.244
48	4.00	1.60	0.361	0.117	(0.325)	0.244
49	4.08	1.70	0.384	0.117	(0.345)	0.267
50	4.17	1.80	0.406	0.117	(0.366)	0.289
51	4.25	1.90	0.429	0.117	(0.386)	0.312
52	4.33	2.00	0.452	0.117	(0.406)	0.335
53	4.42	2.10	0.474	0.117	(0.427)	0.357
54	4.50	2.10	0.474	0.117	(0.427)	0.357
55	4.58	2.20	0.497	0.117	(0.447)	0.380
56	4.67	2.30	0.519	0.117	(0.467)	0.402
57	4.75	2.40	0.542	0.117	(0.488)	0.425
58	4.83	2.40	0.542	0.117	(0.488)	0.425
59	4.92	2.50	0.564	0.117	(0.508)	0.447
60	5.00	2.60	0.587	0.117	(0.528)	0.470
61	5.08	3.10	0.700	0.117	(0.630)	0.583
62	5.17	3.60	0.813	0.117	(0.732)	0.696
63	5.25	3.90	0.881	0.117	(0.792)	0.764
64	5.33	4.20	0.948	0.117	(0.853)	0.831
65	5.42	4.70	1.061	0.117	(0.955)	0.944
66	5.50	5.60	1.264	0.117	(1.138)	1.147
67	5.58	1.90	0.429	0.117	(0.386)	0.312
68	5.67	0.90	0.203	0.117	(0.183)	0.086
69	5.75	0.60	0.135	0.117	(0.122)	0.018
70	5.83	0.50	0.113	(0.117)	0.102	0.011

```
71   5.92     0.30      0.068       (  0.117)       0.061        0.007
72   6.00     0.20      0.045       (  0.117)       0.041        0.005
               (Loss Rate Not Used)
   Sum =     100.0                                  Sum =    14.3
      Flood volume = Effective rainfall      1.19(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       2.7(Ac.Ft)
      Total soil loss =      0.69(In)
      Total soil loss =     1.534(Ac.Ft)
      Total rainfall =      1.88(In)
      Flood volume =      115809.9 Cubic Feet
      Total soil loss =       66820.4 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     26.594(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        7.5      15.0      22.5      30.0
-------------------------------------------------------------------------
  0+ 5       0.0007      0.11  Q          |          |          |          |
  0+10       0.0029      0.32  Q          |          |          |          |
  0+15       0.0059      0.44  Q          |          |          |          |
  0+20       0.0092      0.47  Q          |          |          |          |
  0+25       0.0126      0.49  Q          |          |          |          |
  0+30       0.0175      0.71  Q          |          |          |          |
  0+35       0.0243      0.99  VQ         |          |          |          |
  0+40       0.0316      1.06  VQ         |          |          |          |
  0+45       0.0391      1.09  VQ         |          |          |          |
  0+50       0.0467      1.10  VQ         |          |          |          |
  0+55       0.0543      1.11  VQ         |          |          |          |
  1+ 0       0.0634      1.32  VQ         |          |          |          |
  1+ 5       0.0744      1.60  |VQ        |          |          |          |
  1+10       0.0859      1.67  |VQ        |          |          |          |
  1+15       0.0976      1.70  |VQ        |          |          |          |
  1+20       0.1094      1.71  |VQ        |          |          |          |
  1+25       0.1212      1.72  |VQ        |          |          |          |
  1+30       0.1330      1.72  | Q        |          |          |          |
  1+35       0.1448      1.72  | Q        |          |          |          |
  1+40       0.1566      1.72  | Q        |          |          |          |
  1+45       0.1685      1.72  | Q        |          |          |          |
  1+50       0.1803      1.72  | Q        |          |          |          |
  1+55       0.1921      1.72  | Q        |          |          |          |
  2+ 0       0.2054      1.93  | QV       |          |          |          |
  2+ 5       0.2191      2.00  | QV       |          |          |          |
  2+10       0.2329      1.99  | QV       |          |          |          |
  2+15       0.2483      2.24  | QV       |          |          |          |
  2+20       0.2641      2.29  |  Q       |          |          |          |
  2+25       0.2800      2.31  |  QV      |          |          |          |
  2+30       0.2960      2.32  |  QV      |          |          |          |
  2+35       0.3120      2.32  |  QV      |          |          |          |
  2+40       0.3280      2.32  |  QV      |          |          |          |
  2+45       0.3455      2.54  |  Q V     |          |          |          |
  2+50       0.3649      2.82  |  Q V     |          |          |          |
  2+55       0.3848      2.89  |  Q V     |          |          |          |
  3+ 0       0.4048      2.91  |  Q  V    |          |          |          |
  3+ 5       0.4250      2.93  |  Q  V    |          |          |          |
  3+10       0.4467      3.15  |   Q V    |          |          |          |
  3+15       0.4703      3.43  |   Q  V   |          |          |          |
  3+20       0.4943      3.49  |   Q  V   |          |          |          |
  3+25       0.5201      3.74  |   Q  V   |          |          |          |
  3+30       0.5493      4.25  |    Q  V  |          |          |          |
  3+35       0.5825      4.81  |     Q V  |          |          |          |
  3+40       0.6182      5.19  |     Q  V|          |          |          |
  3+45       0.6562      5.51  |      Q V|          |          |          |
  3+50       0.6964      5.84  |      Q  V          |          |          |
  3+55       0.7387      6.14  |       Q |V         |          |          |
  4+ 0       0.7831      6.45  |       Q |V         |          |          |
  4+ 5       0.8296      6.75  |       Q |  V       |          |          |
  4+10       0.8797      7.28  |        Q|  V       |          |          |
  4+15       0.9338      7.85  |         Q   V      |          |          |
  4+20       0.9919      8.45  |         |Q  V      |          |          |
  4+25       1.0543      9.05  |         | Q  V     |          |          |
  4+30       1.1193      9.45  |         | Q   V    |          |          |
  4+35       1.1866      9.77  |         |  Q   V   |          |          |
  4+40       1.2577     10.32  |         |  Q    V  |          |          |
  4+45       1.3327     10.90  |         |   Q      V         |          |
  4+50       1.4104     11.28  |         |    Q     |V         |          |
  4+55       1.4902     11.60  |         |    Q     | V        |          |
  5+ 0       1.5739     12.14  |         |     Q    |  V       |          |
  5+ 5       1.6674     13.58  |         |       Q  |     V    |          |
  5+10       1.7787     16.16  |         |          |Q    V    |          |
  5+15       1.9066     18.58  |         |          |   Q   V  |          |
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    5+20       2.0482     20.55  |          |          |       Q  V          |
    5+25       2.2058     22.88  |          |          |          Q  V       |
    5+30       2.3889     26.59  |          |          |             |    Q  |
    5+35       2.5384     21.70  |          |          |          Q  |       V |
    5+40       2.6066      9.90  |          |   Q      |             |         V|
    5+45       2.6366      4.36  |     Q    |          |             |         V|
    5+50       2.6496      1.90  |  Q       |          |             |         V|
    5+55       2.6553      0.83  |Q         |          |             |         V|
    6+ 0       2.6574      0.31  Q          |          |             |         V|
    6+ 5       2.6583      0.12  Q          |          |             |         V|
    6+10       2.6585      0.03  Q          |          |             |         V|
    6+15       2.6586      0.01  Q          |          |             |         V|
    6+20       2.6586      0.00  Q          |          |             |         V|
    6+25       2.6586      0.00  Q          |          |             |         V|
-------------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX1102410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 1087.00(Ft.)
Length along longest watercourse measured to centroid = 544.00(Ft.)
Length along longest watercourse = 0.206 Mi.
Length along longest watercourse measured to centroid = 0.103 Mi.
Difference in elevation = 88.30(Ft.)
Slope along watercourse = 428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.80	48.13

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	5.00	133.70

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 3.117(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 3.116(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.000

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.025	(0.207)	0.022	0.002
2	0.17	0.07	0.025	(0.207)	0.022	0.002
3	0.25	0.07	0.025	(0.206)	0.022	0.002
4	0.33	0.10	0.037	(0.205)	0.034	0.004
5	0.42	0.10	0.037	(0.204)	0.034	0.004
6	0.50	0.10	0.037	(0.203)	0.034	0.004
7	0.58	0.10	0.037	(0.203)	0.034	0.004
8	0.67	0.10	0.037	(0.202)	0.034	0.004
9	0.75	0.10	0.037	(0.201)	0.034	0.004
10	0.83	0.13	0.050	(0.200)	0.045	0.005
11	0.92	0.13	0.050	(0.199)	0.045	0.005
12	1.00	0.13	0.050	(0.199)	0.045	0.005
13	1.08	0.10	0.037	(0.198)	0.034	0.004
14	1.17	0.10	0.037	(0.197)	0.034	0.004
15	1.25	0.10	0.037	(0.196)	0.034	0.004
16	1.33	0.10	0.037	(0.196)	0.034	0.004
17	1.42	0.10	0.037	(0.195)	0.034	0.004
18	1.50	0.10	0.037	(0.194)	0.034	0.004
19	1.58	0.10	0.037	(0.193)	0.034	0.004
20	1.67	0.10	0.037	(0.192)	0.034	0.004
21	1.75	0.10	0.037	(0.192)	0.034	0.004
22	1.83	0.13	0.050	(0.191)	0.045	0.005
23	1.92	0.13	0.050	(0.190)	0.045	0.005
24	2.00	0.13	0.050	(0.189)	0.045	0.005
25	2.08	0.13	0.050	(0.189)	0.045	0.005
26	2.17	0.13	0.050	(0.188)	0.045	0.005
27	2.25	0.13	0.050	(0.187)	0.045	0.005
28	2.33	0.13	0.050	(0.186)	0.045	0.005
29	2.42	0.13	0.050	(0.186)	0.045	0.005
30	2.50	0.13	0.050	(0.185)	0.045	0.005
31	2.58	0.17	0.062	(0.184)	0.056	0.006
32	2.67	0.17	0.062	(0.183)	0.056	0.006
33	2.75	0.17	0.062	(0.183)	0.056	0.006
34	2.83	0.17	0.062	(0.182)	0.056	0.006
35	2.92	0.17	0.062	(0.181)	0.056	0.006
36	3.00	0.17	0.062	(0.180)	0.056	0.006
37	3.08	0.17	0.062	(0.180)	0.056	0.006
38	3.17	0.17	0.062	(0.179)	0.056	0.006
39	3.25	0.17	0.062	(0.178)	0.056	0.006
40	3.33	0.17	0.062	(0.177)	0.056	0.006
41	3.42	0.17	0.062	(0.177)	0.056	0.006
42	3.50	0.17	0.062	(0.176)	0.056	0.006
43	3.58	0.17	0.062	(0.175)	0.056	0.006
44	3.67	0.17	0.062	(0.174)	0.056	0.006
45	3.75	0.17	0.062	(0.174)	0.056	0.006
46	3.83	0.20	0.075	(0.173)	0.067	0.007
47	3.92	0.20	0.075	(0.172)	0.067	0.007
48	4.00	0.20	0.075	(0.171)	0.067	0.007
49	4.08	0.20	0.075	(0.171)	0.067	0.007
50	4.17	0.20	0.075	(0.170)	0.067	0.007
51	4.25	0.20	0.075	(0.169)	0.067	0.007
52	4.33	0.23	0.087	(0.169)	0.079	0.009
53	4.42	0.23	0.087	(0.168)	0.079	0.009
54	4.50	0.23	0.087	(0.167)	0.079	0.009
55	4.58	0.23	0.087	(0.166)	0.079	0.009
56	4.67	0.23	0.087	(0.166)	0.079	0.009
57	4.75	0.23	0.087	(0.165)	0.079	0.009
58	4.83	0.27	0.100	(0.164)	0.090	0.010
59	4.92	0.27	0.100	(0.164)	0.090	0.010
60	5.00	0.27	0.100	(0.163)	0.090	0.010
61	5.08	0.20	0.075	(0.162)	0.067	0.007
62	5.17	0.20	0.075	(0.161)	0.067	0.007
63	5.25	0.20	0.075	(0.161)	0.067	0.007
64	5.33	0.23	0.087	(0.160)	0.079	0.009
65	5.42	0.23	0.087	(0.159)	0.079	0.009
66	5.50	0.23	0.087	(0.159)	0.079	0.009
67	5.58	0.27	0.100	(0.158)	0.090	0.010
68	5.67	0.27	0.100	(0.157)	0.090	0.010
69	5.75	0.27	0.100	(0.157)	0.090	0.010
70	5.83	0.27	0.100	(0.156)	0.090	0.010

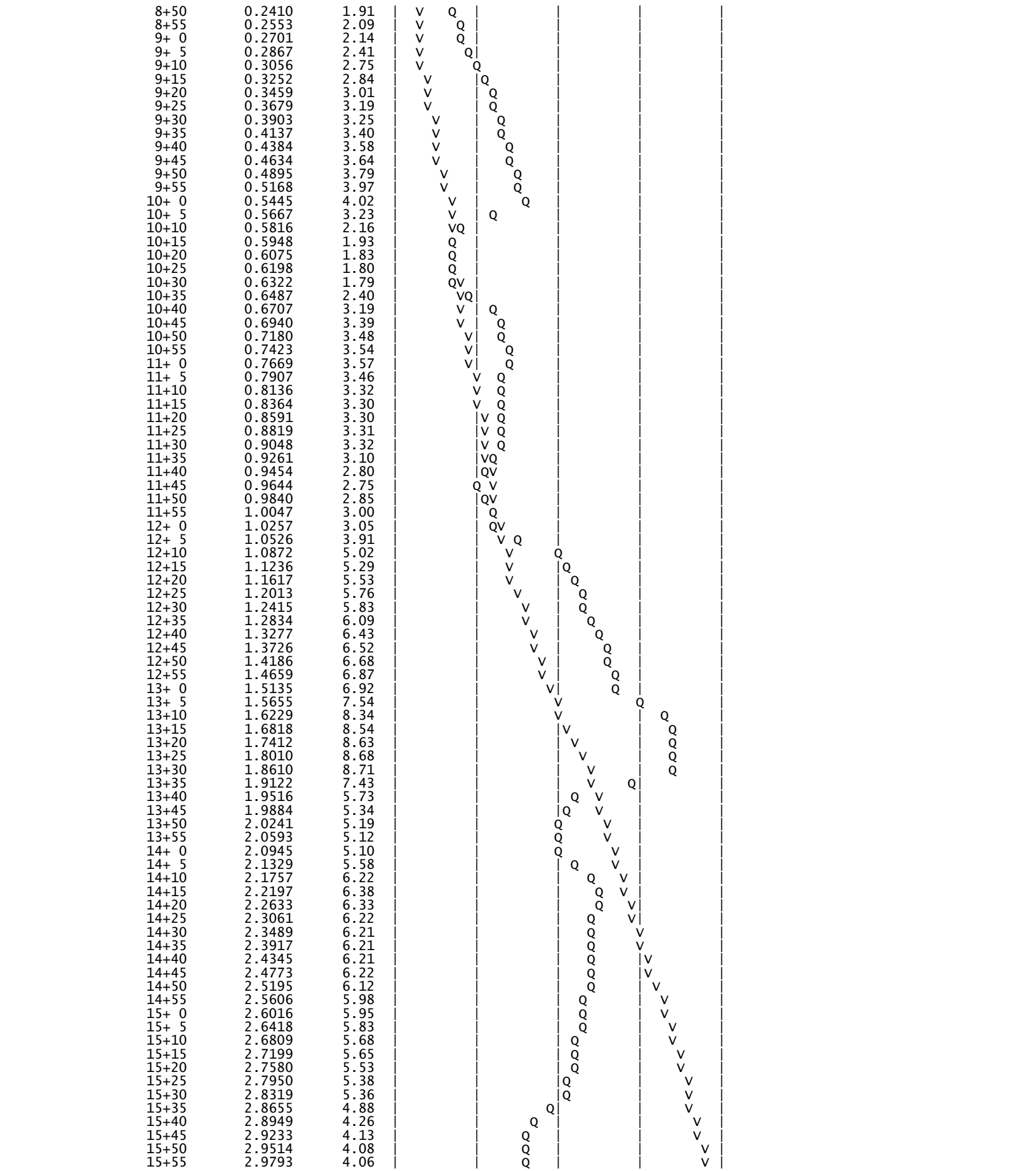
71	5.92	0.27	0.100	(	0.155)	0.090		0.010
72	6.00	0.27	0.100	(	0.154)	0.090		0.010
73	6.08	0.30	0.112	(	0.154)	0.101		0.011
74	6.17	0.30	0.112	(	0.153)	0.101		0.011
75	6.25	0.30	0.112	(	0.152)	0.101		0.011
76	6.33	0.30	0.112	(	0.152)	0.101		0.011
77	6.42	0.30	0.112	(	0.151)	0.101		0.011
78	6.50	0.30	0.112	(	0.150)	0.101		0.011
79	6.58	0.33	0.125	(	0.150)	0.112		0.012
80	6.67	0.33	0.125	(	0.149)	0.112		0.012
81	6.75	0.33	0.125	(	0.148)	0.112		0.012
82	6.83	0.33	0.125	(	0.148)	0.112		0.012
83	6.92	0.33	0.125	(	0.147)	0.112		0.012
84	7.00	0.33	0.125	(	0.146)	0.112		0.012
85	7.08	0.33	0.125	(	0.146)	0.112		0.012
86	7.17	0.33	0.125	(	0.145)	0.112		0.012
87	7.25	0.33	0.125	(	0.144)	0.112		0.012
88	7.33	0.37	0.137	(	0.144)	0.123		0.014
89	7.42	0.37	0.137	(	0.143)	0.123		0.014
90	7.50	0.37	0.137	(	0.142)	0.123		0.014
91	7.58	0.40	0.150	(	0.142)	0.135		0.015
92	7.67	0.40	0.150	(	0.141)	0.135		0.015
93	7.75	0.40	0.150	(	0.140)	0.135		0.015
94	7.83	0.43	0.162		0.140	(0.146)		0.022
95	7.92	0.43	0.162		0.139	(0.146)		0.023
96	8.00	0.43	0.162		0.138	(0.146)		0.024
97	8.08	0.50	0.187		0.138	(0.168)		0.049
98	8.17	0.50	0.187		0.137	(0.168)		0.050
99	8.25	0.50	0.187		0.137	(0.168)		0.050
100	8.33	0.50	0.187		0.136	(0.168)		0.051
101	8.42	0.50	0.187		0.135	(0.168)		0.052
102	8.50	0.50	0.187		0.135	(0.168)		0.052
103	8.58	0.53	0.199		0.134	(0.180)		0.065
104	8.67	0.53	0.199		0.133	(0.180)		0.066
105	8.75	0.53	0.199		0.133	(0.180)		0.067
106	8.83	0.57	0.212		0.132	(0.191)		0.080
107	8.92	0.57	0.212		0.131	(0.191)		0.080
108	9.00	0.57	0.212		0.131	(0.191)		0.081
109	9.08	0.63	0.237		0.130	(0.213)		0.107
110	9.17	0.63	0.237		0.130	(0.213)		0.107
111	9.25	0.63	0.237		0.129	(0.213)		0.108
112	9.33	0.67	0.249		0.128	(0.224)		0.121
113	9.42	0.67	0.249		0.128	(0.224)		0.122
114	9.50	0.67	0.249		0.127	(0.224)		0.122
115	9.58	0.70	0.262		0.127	(0.236)		0.135
116	9.67	0.70	0.262		0.126	(0.236)		0.136
117	9.75	0.70	0.262		0.125	(0.236)		0.136
118	9.83	0.73	0.274		0.125	(0.247)		0.149
119	9.92	0.73	0.274		0.124	(0.247)		0.150
120	10.00	0.73	0.274		0.124	(0.247)		0.151
121	10.08	0.50	0.187		0.123	(0.168)		0.064
122	10.17	0.50	0.187		0.122	(0.168)		0.065
123	10.25	0.50	0.187		0.122	(0.168)		0.065
124	10.33	0.50	0.187		0.121	(0.168)		0.066
125	10.42	0.50	0.187		0.121	(0.168)		0.066
126	10.50	0.50	0.187		0.120	(0.168)		0.067
127	10.58	0.67	0.249		0.119	(0.224)		0.130
128	10.67	0.67	0.249		0.119	(0.224)		0.130
129	10.75	0.67	0.249		0.118	(0.224)		0.131
130	10.83	0.67	0.249		0.118	(0.224)		0.132
131	10.92	0.67	0.249		0.117	(0.224)		0.132
132	11.00	0.67	0.249		0.117	(0.224)		0.133
133	11.08	0.63	0.237		0.116	(0.213)		0.121
134	11.17	0.63	0.237		0.115	(0.213)		0.121
135	11.25	0.63	0.237		0.115	(0.213)		0.122
136	11.33	0.63	0.237		0.114	(0.213)		0.123
137	11.42	0.63	0.237		0.114	(0.213)		0.123
138	11.50	0.63	0.237		0.113	(0.213)		0.124
139	11.58	0.57	0.212		0.113	(0.191)		0.099
140	11.67	0.57	0.212		0.112	(0.191)		0.100
141	11.75	0.57	0.212		0.111	(0.191)		0.100
142	11.83	0.60	0.224		0.111	(0.202)		0.114
143	11.92	0.60	0.224		0.110	(0.202)		0.114
144	12.00	0.60	0.224		0.110	(0.202)		0.115
145	12.08	0.83	0.312		0.109	(0.280)		0.202
146	12.17	0.83	0.312		0.109	(0.280)		0.203
147	12.25	0.83	0.312		0.108	(0.280)		0.204
148	12.33	0.87	0.324		0.108	(0.292)		0.217
149	12.42	0.87	0.324		0.107	(0.292)		0.217
150	12.50	0.87	0.324		0.107	(0.292)		0.218
151	12.58	0.93	0.349		0.106	(0.314)		0.243
152	12.67	0.93	0.349		0.105	(0.314)		0.244
153	12.75	0.93	0.349		0.105	(0.314)		0.244
154	12.83	0.97	0.361		0.104	(0.325)		0.257
155	12.92	0.97	0.361		0.104	(0.325)		0.258
156	13.00	0.97	0.361		0.103	(0.325)		0.258

157	13.08	1.13	0.424	0.103	(0.381)	0.321
158	13.17	1.13	0.424	0.102	(0.381)	0.322
159	13.25	1.13	0.424	0.102	(0.381)	0.322
160	13.33	1.13	0.424	0.101	(0.381)	0.323
161	13.42	1.13	0.424	0.101	(0.381)	0.323
162	13.50	1.13	0.424	0.100	(0.381)	0.324
163	13.58	0.77	0.287	0.100	(0.258)	0.187
164	13.67	0.77	0.287	0.099	(0.258)	0.188
165	13.75	0.77	0.287	0.099	(0.258)	0.188
166	13.83	0.77	0.287	0.098	(0.258)	0.189
167	13.92	0.77	0.287	0.098	(0.258)	0.189
168	14.00	0.77	0.287	0.097	(0.258)	0.190
169	14.08	0.90	0.337	0.097	(0.303)	0.240
170	14.17	0.90	0.337	0.096	(0.303)	0.240
171	14.25	0.90	0.337	0.096	(0.303)	0.241
172	14.33	0.87	0.324	0.095	(0.292)	0.229
173	14.42	0.87	0.324	0.095	(0.292)	0.229
174	14.50	0.87	0.324	0.094	(0.292)	0.230
175	14.58	0.87	0.324	0.094	(0.292)	0.230
176	14.67	0.87	0.324	0.093	(0.292)	0.231
177	14.75	0.87	0.324	0.093	(0.292)	0.231
178	14.83	0.83	0.312	0.092	(0.280)	0.219
179	14.92	0.83	0.312	0.092	(0.280)	0.220
180	15.00	0.83	0.312	0.091	(0.280)	0.220
181	15.08	0.80	0.299	0.091	(0.269)	0.208
182	15.17	0.80	0.299	0.090	(0.269)	0.209
183	15.25	0.80	0.299	0.090	(0.269)	0.209
184	15.33	0.77	0.287	0.090	(0.258)	0.197
185	15.42	0.77	0.287	0.089	(0.258)	0.198
186	15.50	0.77	0.287	0.089	(0.258)	0.198
187	15.58	0.63	0.237	0.088	(0.213)	0.149
188	15.67	0.63	0.237	0.088	(0.213)	0.149
189	15.75	0.63	0.237	0.087	(0.213)	0.150
190	15.83	0.63	0.237	0.087	(0.213)	0.150
191	15.92	0.63	0.237	0.086	(0.213)	0.150
192	16.00	0.63	0.237	0.086	(0.213)	0.151
193	16.08	0.13	0.050	(0.085)	0.045	0.005
194	16.17	0.13	0.050	(0.085)	0.045	0.005
195	16.25	0.13	0.050	(0.085)	0.045	0.005
196	16.33	0.13	0.050	(0.084)	0.045	0.005
197	16.42	0.13	0.050	(0.084)	0.045	0.005
198	16.50	0.13	0.050	(0.083)	0.045	0.005
199	16.58	0.10	0.037	(0.083)	0.034	0.004
200	16.67	0.10	0.037	(0.082)	0.034	0.004
201	16.75	0.10	0.037	(0.082)	0.034	0.004
202	16.83	0.10	0.037	(0.082)	0.034	0.004
203	16.92	0.10	0.037	(0.081)	0.034	0.004
204	17.00	0.10	0.037	(0.081)	0.034	0.004
205	17.08	0.17	0.062	(0.080)	0.056	0.006
206	17.17	0.17	0.062	(0.080)	0.056	0.006
207	17.25	0.17	0.062	(0.080)	0.056	0.006
208	17.33	0.17	0.062	(0.079)	0.056	0.006
209	17.42	0.17	0.062	(0.079)	0.056	0.006
210	17.50	0.17	0.062	(0.078)	0.056	0.006
211	17.58	0.17	0.062	(0.078)	0.056	0.006
212	17.67	0.17	0.062	(0.078)	0.056	0.006
213	17.75	0.17	0.062	(0.077)	0.056	0.006
214	17.83	0.13	0.050	(0.077)	0.045	0.005
215	17.92	0.13	0.050	(0.076)	0.045	0.005
216	18.00	0.13	0.050	(0.076)	0.045	0.005
217	18.08	0.13	0.050	(0.076)	0.045	0.005
218	18.17	0.13	0.050	(0.075)	0.045	0.005
219	18.25	0.13	0.050	(0.075)	0.045	0.005
220	18.33	0.13	0.050	(0.075)	0.045	0.005
221	18.42	0.13	0.050	(0.074)	0.045	0.005
222	18.50	0.13	0.050	(0.074)	0.045	0.005
223	18.58	0.10	0.037	(0.074)	0.034	0.004
224	18.67	0.10	0.037	(0.073)	0.034	0.004
225	18.75	0.10	0.037	(0.073)	0.034	0.004
226	18.83	0.07	0.025	(0.072)	0.022	0.002
227	18.92	0.07	0.025	(0.072)	0.022	0.002
228	19.00	0.07	0.025	(0.072)	0.022	0.002
229	19.08	0.10	0.037	(0.071)	0.034	0.004
230	19.17	0.10	0.037	(0.071)	0.034	0.004
231	19.25	0.10	0.037	(0.071)	0.034	0.004
232	19.33	0.13	0.050	(0.070)	0.045	0.005
233	19.42	0.13	0.050	(0.070)	0.045	0.005
234	19.50	0.13	0.050	(0.070)	0.045	0.005
235	19.58	0.10	0.037	(0.069)	0.034	0.004
236	19.67	0.10	0.037	(0.069)	0.034	0.004
237	19.75	0.10	0.037	(0.069)	0.034	0.004
238	19.83	0.07	0.025	(0.069)	0.022	0.002
239	19.92	0.07	0.025	(0.068)	0.022	0.002
240	20.00	0.07	0.025	(0.068)	0.022	0.002
241	20.08	0.10	0.037	(0.068)	0.034	0.004
242	20.17	0.10	0.037	(0.067)	0.034	0.004

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243  20.25     0.10      0.037       (  0.067)       0.034        0.004
244  20.33     0.10      0.037       (  0.067)       0.034        0.004
245  20.42     0.10      0.037       (  0.066)       0.034        0.004
246  20.50     0.10      0.037       (  0.066)       0.034        0.004
247  20.58     0.10      0.037       (  0.066)       0.034        0.004
248  20.67     0.10      0.037       (  0.066)       0.034        0.004
249  20.75     0.10      0.037       (  0.065)       0.034        0.004
250  20.83     0.07      0.025       (  0.065)       0.022        0.002
251  20.92     0.07      0.025       (  0.065)       0.022        0.002
252  21.00     0.07      0.025       (  0.065)       0.022        0.002
253  21.08     0.10      0.037       (  0.064)       0.034        0.004
254  21.17     0.10      0.037       (  0.064)       0.034        0.004
255  21.25     0.10      0.037       (  0.064)       0.034        0.004
256  21.33     0.07      0.025       (  0.064)       0.022        0.002
257  21.42     0.07      0.025       (  0.063)       0.022        0.002
258  21.50     0.07      0.025       (  0.063)       0.022        0.002
259  21.58     0.10      0.037       (  0.063)       0.034        0.004
260  21.67     0.10      0.037       (  0.063)       0.034        0.004
261  21.75     0.10      0.037       (  0.062)       0.034        0.004
262  21.83     0.07      0.025       (  0.062)       0.022        0.002
263  21.92     0.07      0.025       (  0.062)       0.022        0.002
264  22.00     0.07      0.025       (  0.062)       0.022        0.002
265  22.08     0.10      0.037       (  0.062)       0.034        0.004
266  22.17     0.10      0.037       (  0.061)       0.034        0.004
267  22.25     0.10      0.037       (  0.061)       0.034        0.004
268  22.33     0.07      0.025       (  0.061)       0.022        0.002
269  22.42     0.07      0.025       (  0.061)       0.022        0.002
270  22.50     0.07      0.025       (  0.061)       0.022        0.002
271  22.58     0.07      0.025       (  0.060)       0.022        0.002
272  22.67     0.07      0.025       (  0.060)       0.022        0.002
273  22.75     0.07      0.025       (  0.060)       0.022        0.002
274  22.83     0.07      0.025       (  0.060)       0.022        0.002
275  22.92     0.07      0.025       (  0.060)       0.022        0.002
276  23.00     0.07      0.025       (  0.060)       0.022        0.002
277  23.08     0.07      0.025       (  0.060)       0.022        0.002
278  23.17     0.07      0.025       (  0.059)       0.022        0.002
279  23.25     0.07      0.025       (  0.059)       0.022        0.002
280  23.33     0.07      0.025       (  0.059)       0.022        0.002
281  23.42     0.07      0.025       (  0.059)       0.022        0.002
282  23.50     0.07      0.025       (  0.059)       0.022        0.002
283  23.58     0.07      0.025       (  0.059)       0.022        0.002
284  23.67     0.07      0.025       (  0.059)       0.022        0.002
285  23.75     0.07      0.025       (  0.059)       0.022        0.002
286  23.83     0.07      0.025       (  0.059)       0.022        0.002
287  23.92     0.07      0.025       (  0.059)       0.022        0.002
288  24.00     0.07      0.025       (  0.059)       0.022        0.002
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    16.7
      Flood volume = Effective rainfall      1.39(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       3.1(Ac.Ft)
      Total soil loss =      1.72(In)
      Total soil loss =     3.844(Ac.Ft)
      Total rainfall =      3.12(In)
      Flood volume =      135059.7 Cubic Feet
      Total soil loss =      167431.9 Cubic Feet
      --------------------------------------------------------------------
       Peak flow rate of this hydrograph =      8.712(CFS)
      --------------------------------------------------------------------
      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      --------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      --------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0002      0.02  Q          |         |         |         |
   0+10       0.0005      0.05  Q          |         |         |         |
   0+15       0.0010      0.06  Q          |         |         |         |
   0+20       0.0015      0.08  Q          |         |         |         |
   0+25       0.0021      0.09  Q          |         |         |         |
   0+30       0.0028      0.10  Q          |         |         |         |
   0+35       0.0035      0.10  Q          |         |         |         |
   0+40       0.0042      0.10  Q          |         |         |         |
   0+45       0.0049      0.10  Q          |         |         |         |
   0+50       0.0057      0.11  Q          |         |         |         |
   0+55       0.0066      0.13  Q          |         |         |         |
   1+ 0       0.0075      0.13  Q          |         |         |         |
   1+ 5       0.0083      0.12  Q          |         |         |         |
   1+10       0.0090      0.11  Q          |         |         |         |
   1+15       0.0097      0.10  Q          |         |         |         |
   1+20       0.0104      0.10  Q          |         |         |         |
   1+25       0.0111      0.10  Q          |         |         |         |
   1+30       0.0118      0.10  Q          |         |         |         |
   1+35       0.0125      0.10  Q          |         |         |         |
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1+40	0.0132	0.10	Q	|	|	|	|
1+45	0.0139	0.10	Q	|	|	|	|
1+50	0.0147	0.11	Q	|	|	|	|
1+55	0.0156	0.13	Q	|	|	|	|
2+ 0	0.0165	0.13	Q	|	|	|	|
2+ 5	0.0174	0.13	Q	|	|	|	|
2+10	0.0183	0.13	Q	|	|	|	|
2+15	0.0193	0.13	Q	|	|	|	|
2+20	0.0202	0.13	Q	|	|	|	|
2+25	0.0211	0.13	Q	|	|	|	|
2+30	0.0220	0.13	Q	|	|	|	|
2+35	0.0230	0.15	Q	|	|	|	|
2+40	0.0242	0.16	Q	|	|	|	|
2+45	0.0253	0.17	Q	|	|	|	|
2+50	0.0264	0.17	Q	|	|	|	|
2+55	0.0276	0.17	Q	|	|	|	|
3+ 0	0.0288	0.17	Q	|	|	|	|
3+ 5	0.0299	0.17	Q	|	|	|	|
3+10	0.0311	0.17	Q	|	|	|	|
3+15	0.0322	0.17	Q	|	|	|	|
3+20	0.0334	0.17	Q	|	|	|	|
3+25	0.0345	0.17	Q	|	|	|	|
3+30	0.0357	0.17	Q	|	|	|	|
3+35	0.0369	0.17	Q	|	|	|	|
3+40	0.0380	0.17	Q	|	|	|	|
3+45	0.0392	0.17	Q	|	|	|	|
3+50	0.0404	0.18	Q	|	|	|	|
3+55	0.0418	0.20	Q	|	|	|	|
4+ 0	0.0431	0.20	Q	|	|	|	|
4+ 5	0.0445	0.20	Q	|	|	|	|
4+10	0.0459	0.20	Q	|	|	|	|
4+15	0.0473	0.20	Q	|	|	|	|
4+20	0.0488	0.21	Q	|	|	|	|
4+25	0.0503	0.23	Q	|	|	|	|
4+30	0.0519	0.23	Q	|	|	|	|
4+35	0.0536	0.23	Q	|	|	|	|
4+40	0.0552	0.23	Q	|	|	|	|
4+45	0.0568	0.24	Q	|	|	|	|
4+50	0.0585	0.25	Q	|	|	|	|
4+55	0.0603	0.26	VQ	|	|	|	|
5+ 0	0.0621	0.27	VQ	|	|	|	|
5+ 5	0.0638	0.24	Q	|	|	|	|
5+10	0.0653	0.21	Q	|	|	|	|
5+15	0.0667	0.21	Q	|	|	|	|
5+20	0.0682	0.22	Q	|	|	|	|
5+25	0.0698	0.23	Q	|	|	|	|
5+30	0.0714	0.23	Q	|	|	|	|
5+35	0.0731	0.25	Q	|	|	|	|
5+40	0.0749	0.26	VQ	|	|	|	|
5+45	0.0767	0.27	VQ	|	|	|	|
5+50	0.0786	0.27	|Q	|	|	|	|
5+55	0.0804	0.27	|Q	|	|	|	|
6+ 0	0.0823	0.27	|Q	|	|	|	|
6+ 5	0.0842	0.28	|Q	|	|	|	|
6+10	0.0862	0.30	|Q	|	|	|	|
6+15	0.0883	0.30	|Q	|	|	|	|
6+20	0.0904	0.30	|Q	|	|	|	|
6+25	0.0925	0.30	|Q	|	|	|	|
6+30	0.0945	0.30	|Q	|	|	|	|
6+35	0.0967	0.31	|Q	|	|	|	|
6+40	0.0990	0.33	|Q	|	|	|	|
6+45	0.1013	0.33	|Q	|	|	|	|
6+50	0.1036	0.34	|Q	|	|	|	|
6+55	0.1059	0.34	|Q	|	|	|	|
7+ 0	0.1082	0.34	|Q	|	|	|	|
7+ 5	0.1105	0.34	|Q	|	|	|	|
7+10	0.1128	0.34	|Q	|	|	|	|
7+15	0.1152	0.34	|Q	|	|	|	|
7+20	0.1176	0.35	|Q	|	|	|	|
7+25	0.1201	0.36	|Q	|	|	|	|
7+30	0.1226	0.37	|Q	|	|	|	|
7+35	0.1252	0.38	|Q	|	|	|	|
7+40	0.1279	0.40	|Q	|	|	|	|
7+45	0.1307	0.40	|Q	|	|	|	|
7+50	0.1339	0.47	|Q	|	|	|	|
7+55	0.1379	0.57	|VQ	|	|	|	|
8+ 0	0.1420	0.61	|VQ	|	|	|	|
8+ 5	0.1480	0.87	|V Q	|	|	|	|
8+10	0.1563	1.20	| V Q	|	|	|	|
8+15	0.1652	1.29	| V Q	|	|	|	|
8+20	0.1744	1.34	| V Q	|	|	|	|
8+25	0.1839	1.37	| V Q	|	|	|	|
8+30	0.1935	1.40	| V Q	|	|	|	|
8+35	0.2040	1.53	| V Q	|	|	|	|
8+40	0.2157	1.70	| V Q	|	|	|	|
8+45	0.2278	1.76	| V Q	|	|	|	|



8+50	0.2410	1.91	
8+55	0.2553	2.09	
9+ 0	0.2701	2.14	
9+ 5	0.2867	2.41	
9+10	0.3056	2.75	
9+15	0.3252	2.84	
9+20	0.3459	3.01	
9+25	0.3679	3.19	
9+30	0.3903	3.25	
9+35	0.4137	3.40	
9+40	0.4384	3.58	
9+45	0.4634	3.64	
9+50	0.4895	3.79	
9+55	0.5168	3.97	
10+ 0	0.5445	4.02	
10+ 5	0.5667	3.23	
10+10	0.5816	2.16	
10+15	0.5948	1.93	
10+20	0.6075	1.83	
10+25	0.6198	1.80	
10+30	0.6322	1.79	
10+35	0.6487	2.40	
10+40	0.6707	3.19	
10+45	0.6940	3.39	
10+50	0.7180	3.48	
10+55	0.7423	3.54	
11+ 0	0.7669	3.57	
11+ 5	0.7907	3.46	
11+10	0.8136	3.32	
11+15	0.8364	3.30	
11+20	0.8591	3.30	
11+25	0.8819	3.31	
11+30	0.9048	3.32	
11+35	0.9261	3.10	
11+40	0.9454	2.80	
11+45	0.9644	2.75	
11+50	0.9840	2.85	
11+55	1.0047	3.00	
12+ 0	1.0257	3.05	
12+ 5	1.0526	3.91	
12+10	1.0872	5.02	
12+15	1.1236	5.29	
12+20	1.1617	5.53	
12+25	1.2013	5.76	
12+30	1.2415	5.83	
12+35	1.2834	6.09	
12+40	1.3277	6.43	
12+45	1.3726	6.52	
12+50	1.4186	6.68	
12+55	1.4659	6.87	
13+ 0	1.5135	6.92	
13+ 5	1.5655	7.54	
13+10	1.6229	8.34	
13+15	1.6818	8.54	
13+20	1.7412	8.63	
13+25	1.8010	8.68	
13+30	1.8610	8.71	
13+35	1.9122	7.43	
13+40	1.9516	5.73	
13+45	1.9884	5.34	
13+50	2.0241	5.19	
13+55	2.0593	5.12	
14+ 0	2.0945	5.10	
14+ 5	2.1329	5.58	
14+10	2.1757	6.22	
14+15	2.2197	6.38	
14+20	2.2633	6.33	
14+25	2.3061	6.22	
14+30	2.3489	6.21	
14+35	2.3917	6.21	
14+40	2.4345	6.21	
14+45	2.4773	6.22	
14+50	2.5195	6.12	
14+55	2.5606	5.98	
15+ 0	2.6016	5.95	
15+ 5	2.6418	5.83	
15+10	2.6809	5.68	
15+15	2.7199	5.65	
15+20	2.7580	5.53	
15+25	2.7950	5.38	
15+30	2.8319	5.36	
15+35	2.8655	4.88	
15+40	2.8949	4.26	
15+45	2.9233	4.13	
15+50	2.9514	4.08	
15+55	2.9793	4.06	

16+ 0	3.0073	4.06	|	| Q	|	| V |
16+ 5	3.0257	2.68	|	Q	|	| V|
16+10	3.0317	0.86	| Q	|	|	| V|
16+15	3.0347	0.44	|Q	|	|	| V|
16+20	3.0365	0.26	|Q	|	|	| V|
16+25	3.0376	0.17	Q	|	|	| V|
16+30	3.0386	0.13	Q	|	|	| V|
16+35	3.0394	0.12	Q	|	|	| V|
16+40	3.0401	0.11	Q	|	|	| V|
16+45	3.0408	0.10	Q	|	|	| V|
16+50	3.0416	0.10	Q	|	|	| V|
16+55	3.0422	0.10	Q	|	|	| V|
17+ 0	3.0429	0.10	Q	|	|	| V|
17+ 5	3.0438	0.12	Q	|	|	| V|
17+10	3.0449	0.16	Q	|	|	| V|
17+15	3.0460	0.16	Q	|	|	| V|
17+20	3.0471	0.17	Q	|	|	| V|
17+25	3.0483	0.17	Q	|	|	| V|
17+30	3.0494	0.17	Q	|	|	| V|
17+35	3.0506	0.17	Q	|	|	| V|
17+40	3.0518	0.17	Q	|	|	| V|
17+45	3.0529	0.17	Q	|	|	| V|
17+50	3.0540	0.16	Q	|	|	| V|
17+55	3.0550	0.14	Q	|	|	| V|
18+ 0	3.0559	0.14	Q	|	|	| V|
18+ 5	3.0568	0.14	Q	|	|	| V|
18+10	3.0578	0.13	Q	|	|	| V|
18+15	3.0587	0.13	Q	|	|	| V|
18+20	3.0596	0.13	Q	|	|	| V|
18+25	3.0605	0.13	Q	|	|	| V|
18+30	3.0615	0.13	Q	|	|	| V|
18+35	3.0623	0.12	Q	|	|	| V|
18+40	3.0631	0.11	Q	|	|	| V|
18+45	3.0638	0.10	Q	|	|	| V|
18+50	3.0644	0.09	Q	|	|	| V|
18+55	3.0649	0.07	Q	|	|	| V|
19+ 0	3.0654	0.07	Q	|	|	| V|
19+ 5	3.0659	0.08	Q	|	|	| V|
19+10	3.0666	0.09	Q	|	|	| V|
19+15	3.0673	0.10	Q	|	|	| V|
19+20	3.0680	0.11	Q	|	|	| V|
19+25	3.0689	0.13	Q	|	|	| V|
19+30	3.0698	0.13	Q	|	|	| V|
19+35	3.0707	0.12	Q	|	|	| V|
19+40	3.0714	0.11	Q	|	|	| V|
19+45	3.0721	0.10	Q	|	|	| V|
19+50	3.0727	0.09	Q	|	|	| V|
19+55	3.0732	0.07	Q	|	|	| V|
20+ 0	3.0737	0.07	Q	|	|	| V|
20+ 5	3.0743	0.08	Q	|	|	| V|
20+10	3.0749	0.09	Q	|	|	| V|
20+15	3.0756	0.10	Q	|	|	| V|
20+20	3.0763	0.10	Q	|	|	| V|
20+25	3.0770	0.10	Q	|	|	| V|
20+30	3.0777	0.10	Q	|	|	| V|
20+35	3.0784	0.10	Q	|	|	| V|
20+40	3.0791	0.10	Q	|	|	| V|
20+45	3.0797	0.10	Q	|	|	| V|
20+50	3.0804	0.09	Q	|	|	| V|
20+55	3.0809	0.07	Q	|	|	| V|
21+ 0	3.0813	0.07	Q	|	|	| V|
21+ 5	3.0819	0.08	Q	|	|	| V|
21+10	3.0826	0.09	Q	|	|	| V|
21+15	3.0832	0.10	Q	|	|	| V|
21+20	3.0838	0.09	Q	|	|	| V|
21+25	3.0843	0.07	Q	|	|	| V|
21+30	3.0848	0.07	Q	|	|	| V|
21+35	3.0854	0.08	Q	|	|	| V|
21+40	3.0860	0.09	Q	|	|	| V|
21+45	3.0867	0.10	Q	|	|	| V|
21+50	3.0873	0.09	Q	|	|	| V|
21+55	3.0878	0.07	Q	|	|	| V|
22+ 0	3.0883	0.07	Q	|	|	| V|
22+ 5	3.0888	0.08	Q	|	|	| V|
22+10	3.0895	0.09	Q	|	|	| V|
22+15	3.0902	0.10	Q	|	|	| V|
22+20	3.0908	0.09	Q	|	|	| V|
22+25	3.0913	0.07	Q	|	|	| V|
22+30	3.0918	0.07	Q	|	|	| V|
22+35	3.0922	0.07	Q	|	|	| V|
22+40	3.0927	0.07	Q	|	|	| V|
22+45	3.0932	0.07	Q	|	|	| V|
22+50	3.0936	0.07	Q	|	|	| V|
22+55	3.0941	0.07	Q	|	|	| V|
23+ 0	3.0945	0.07	Q	|	|	| V|
23+ 5	3.0950	0.07	Q	|	|	| V|

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   23+10       3.0955      0.07  Q          |          |          |          v|
   23+15       3.0959      0.07  Q          |          |          |          v|
   23+20       3.0964      0.07  Q          |          |          |          v|
   23+25       3.0969      0.07  Q          |          |          |          v|
   23+30       3.0973      0.07  Q          |          |          |          v|
   23+35       3.0978      0.07  Q          |          |          |          v|
   23+40       3.0983      0.07  Q          |          |          |          v|
   23+45       3.0987      0.07  Q          |          |          |          v|
   23+50       3.0992      0.07  Q          |          |          |          v|
   23+55       3.0996      0.07  Q          |          |          |          v|
   24+ 0       3.1001      0.07  Q          |          |          |          v|
   24+ 5       3.1004      0.04  Q          |          |          |          v|
   24+10       3.1005      0.01  Q          |          |          |          v|
   24+15       3.1005      0.01  Q          |          |          |          v|
   24+20       3.1005      0.00  Q          |          |          |          v|
   24+25       3.1005      0.00  Q          |          |          |          v|
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: ex11001100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 1087.00(Ft.)
Length along longest watercourse measured to centroid = 544.00(Ft.)
Length along longest watercourse = 0.206 Mi.
Length along longest watercourse measured to centroid = 0.103 Mi.
Difference in elevation = 88.30(Ft.)
Slope along watercourse = 428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	0.50	13.37

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.30	34.76

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.300(In)

Point rain (area averaged) = 1.300(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 1.300(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.000

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

Slope of intensity-duration curve for a 1 hour storm =0.5500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000 Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.515	0.117	(0.463)	0.398
2	0.17	4.20	0.655	0.117	(0.590)	0.538
3	0.25	4.40	0.686	0.117	(0.618)	0.569
4	0.33	4.80	0.749	0.117	(0.674)	0.632
5	0.42	5.20	0.811	0.117	(0.730)	0.694
6	0.50	6.20	0.967	0.117	(0.870)	0.850
7	0.58	6.80	1.061	0.117	(0.954)	0.944
8	0.67	8.80	1.372	0.117	(1.235)	1.255
9	0.75	13.90	2.168	0.117	(1.951)	2.051
10	0.83	31.40	4.897	0.117	(4.407)	4.780
11	0.92	7.20	1.123	0.117	(1.011)	1.006
12	1.00	3.80	0.593	0.117	(0.533)	0.476
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	14.2

Flood volume = Effective rainfall 1.18(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 2.6(Ac.Ft)
Total soil loss = 0.12(In)
Total soil loss = 0.261(Ac.Ft)
Total rainfall = 1.30(In)
Flood volume = 114798.7 Cubic Feet
Total soil loss = 11356.7 Cubic Feet

Peak flow rate of this hydrograph = 77.592(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	20.0	40.0	60.0	80.0
0+ 5	0.0259	3.77	VQ				
0+10	0.0953	10.07	|V Q				
0+15	0.1867	13.27	| V Q				
0+20	0.2911	15.15	| V Q				
0+25	0.4084	17.03	| V Q				
0+30	0.5440	19.69	| VQ				
0+35	0.7012	22.84	| VQ				
0+40	0.8909	27.54	| Q				
0+45	1.1628	39.49	| V Q				
0+50	1.6891	76.42	| V			Q	
0+55	2.2235	77.59	| V			Q	
1+ 0	2.4608	34.45	| Q			V	
1+ 5	2.5735	16.37	| Q			V	
1+10	2.6149	6.01	| Q			V	
1+15	2.6310	2.34	|Q			V	
1+20	2.6346	0.53	Q			V	
1+25	2.6354	0.11	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: ex11003100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 1087.00(Ft.)
Length along longest watercourse measured to centroid = 544.00(Ft.)
Length along longest watercourse = 0.206 Mi.
Length along longest watercourse measured to centroid = 0.103 Mi.
Difference in elevation = 88.30(Ft.)
Slope along watercourse = 428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	0.80	21.39

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	2.00	53.48

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 2.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 2.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.000

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000 Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.312	0.117	(0.281)	0.195
2	0.17	1.30	0.312	0.117	(0.281)	0.195
3	0.25	1.10	0.264	0.117	(0.238)	0.147
4	0.33	1.50	0.360	0.117	(0.324)	0.243
5	0.42	1.50	0.360	0.117	(0.324)	0.243
6	0.50	1.80	0.432	0.117	(0.389)	0.315
7	0.58	1.50	0.360	0.117	(0.324)	0.243
8	0.67	1.80	0.432	0.117	(0.389)	0.315
9	0.75	1.80	0.432	0.117	(0.389)	0.315
10	0.83	1.50	0.360	0.117	(0.324)	0.243
11	0.92	1.60	0.384	0.117	(0.346)	0.267
12	1.00	1.80	0.432	0.117	(0.389)	0.315
13	1.08	2.20	0.528	0.117	(0.475)	0.411
14	1.17	2.20	0.528	0.117	(0.475)	0.411
15	1.25	2.20	0.528	0.117	(0.475)	0.411
16	1.33	2.00	0.480	0.117	(0.432)	0.363
17	1.42	2.60	0.624	0.117	(0.562)	0.507
18	1.50	2.70	0.648	0.117	(0.583)	0.531
19	1.58	2.40	0.576	0.117	(0.518)	0.459
20	1.67	2.70	0.648	0.117	(0.583)	0.531
21	1.75	3.30	0.792	0.117	(0.713)	0.675
22	1.83	3.10	0.744	0.117	(0.670)	0.627
23	1.92	2.90	0.696	0.117	(0.626)	0.579
24	2.00	3.00	0.720	0.117	(0.648)	0.603
25	2.08	3.10	0.744	0.117	(0.670)	0.627
26	2.17	4.20	1.008	0.117	(0.907)	0.891
27	2.25	5.00	1.200	0.117	(1.080)	1.083
28	2.33	3.50	0.840	0.117	(0.756)	0.723
29	2.42	6.80	1.632	0.117	(1.469)	1.515
30	2.50	7.30	1.752	0.117	(1.577)	1.635
31	2.58	8.20	1.968	0.117	(1.771)	1.851
32	2.67	5.90	1.416	0.117	(1.274)	1.299
33	2.75	2.00	0.480	0.117	(0.432)	0.363
34	2.83	1.80	0.432	0.117	(0.389)	0.315
35	2.92	1.80	0.432	0.117	(0.389)	0.315
36	3.00	0.60	0.144	0.117	(0.130)	0.027
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	19.8

Flood volume = Effective rainfall 1.65(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 3.7(Ac.Ft)
Total soil loss = 0.35(In)
Total soil loss = 0.782(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 160039.5 Cubic Feet
Total soil loss = 34070.2 Cubic Feet

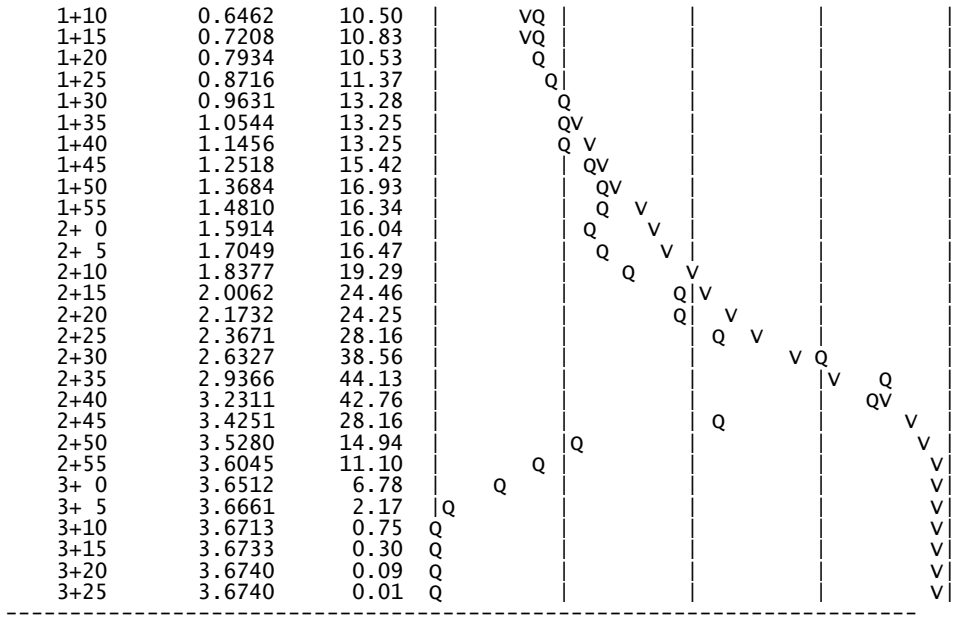
Peak flow rate of this hydrograph = 44.128(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	12.5	25.0	37.5	50.0
0+ 5	0.0127	1.85	VQ	|	|	|	|
0+10	0.0422	4.29	V Q	|	|	|	|
0+15	0.0725	4.39	V Q	|	|	|	|
0+20	0.1066	4.95	|V Q	|	|	|	|
0+25	0.1488	6.13	|V Q	|	|	|	|
0+30	0.1975	7.07	| V Q	|	|	|	|
0+35	0.2483	7.38	| V Q	|	|	|	|
0+40	0.2994	7.42	| V Q	|	|	|	|
0+45	0.3560	8.22	| V Q	|	|	|	|
0+50	0.4091	7.70	| V Q	|	|	|	|
0+55	0.4579	7.09	| VQ	|	|	|	|
1+ 0	0.5107	7.67	| VQ	|	|	|	|
1+ 5	0.5739	9.17	| VQ	|	|	|	|



1+10	0.6462	10.50	VQ
1+15	0.7208	10.83	VQ
1+20	0.7934	10.53	Q
1+25	0.8716	11.37	Q
1+30	0.9631	13.28	Q
1+35	1.0544	13.25	QV
1+40	1.1456	13.25	Q V
1+45	1.2518	15.42	QV
1+50	1.3684	16.93	QV
1+55	1.4810	16.34	Q V
2+ 0	1.5914	16.04	Q V
2+ 5	1.7049	16.47	Q V
2+10	1.8377	19.29	Q V
2+15	2.0062	24.46	Q V
2+20	2.1732	24.25	Q V
2+25	2.3671	28.16	Q V
2+30	2.6327	38.56	V Q
2+35	2.9366	44.13	V Q
2+40	3.2311	42.76	QV
2+45	3.4251	28.16	Q V
2+50	3.5280	14.94	Q V
2+55	3.6045	11.10	Q V
3+ 0	3.6512	6.78	Q V
3+ 5	3.6661	2.17	Q V
3+10	3.6713	0.75	Q V
3+15	3.6733	0.30	Q V
3+20	3.6740	0.09	Q V
3+25	3.6740	0.01	Q V

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: ex11006100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 1087.00(Ft.)
Length along longest watercourse measured to centroid = 544.00(Ft.)
Length along longest watercourse = 0.206 Mi.
Length along longest watercourse measured to centroid = 0.103 Mi.
Difference in elevation = 88.30(Ft.)
Slope along watercourse = 428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.10	29.41

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	3.00	80.22

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 3.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 3.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.000

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.180	0.117	(0.162)	0.063
2	0.17	0.60	0.216	0.117	(0.194)	0.099
3	0.25	0.60	0.216	0.117	(0.194)	0.099
4	0.33	0.60	0.216	0.117	(0.194)	0.099
5	0.42	0.60	0.216	0.117	(0.194)	0.099
6	0.50	0.70	0.252	0.117	(0.227)	0.135
7	0.58	0.70	0.252	0.117	(0.227)	0.135
8	0.67	0.70	0.252	0.117	(0.227)	0.135
9	0.75	0.70	0.252	0.117	(0.227)	0.135
10	0.83	0.70	0.252	0.117	(0.227)	0.135
11	0.92	0.70	0.252	0.117	(0.227)	0.135
12	1.00	0.80	0.288	0.117	(0.259)	0.171
13	1.08	0.80	0.288	0.117	(0.259)	0.171
14	1.17	0.80	0.288	0.117	(0.259)	0.171
15	1.25	0.80	0.288	0.117	(0.259)	0.171
16	1.33	0.80	0.288	0.117	(0.259)	0.171
17	1.42	0.80	0.288	0.117	(0.259)	0.171
18	1.50	0.80	0.288	0.117	(0.259)	0.171
19	1.58	0.80	0.288	0.117	(0.259)	0.171
20	1.67	0.80	0.288	0.117	(0.259)	0.171
21	1.75	0.80	0.288	0.117	(0.259)	0.171
22	1.83	0.80	0.288	0.117	(0.259)	0.171
23	1.92	0.80	0.288	0.117	(0.259)	0.171
24	2.00	0.90	0.324	0.117	(0.292)	0.207
25	2.08	0.80	0.288	0.117	(0.259)	0.171
26	2.17	0.90	0.324	0.117	(0.292)	0.207
27	2.25	0.90	0.324	0.117	(0.292)	0.207
28	2.33	0.90	0.324	0.117	(0.292)	0.207
29	2.42	0.90	0.324	0.117	(0.292)	0.207
30	2.50	0.90	0.324	0.117	(0.292)	0.207
31	2.58	0.90	0.324	0.117	(0.292)	0.207
32	2.67	0.90	0.324	0.117	(0.292)	0.207
33	2.75	1.00	0.360	0.117	(0.324)	0.243
34	2.83	1.00	0.360	0.117	(0.324)	0.243
35	2.92	1.00	0.360	0.117	(0.324)	0.243
36	3.00	1.00	0.360	0.117	(0.324)	0.243
37	3.08	1.00	0.360	0.117	(0.324)	0.243
38	3.17	1.10	0.396	0.117	(0.356)	0.279
39	3.25	1.10	0.396	0.117	(0.356)	0.279
40	3.33	1.10	0.396	0.117	(0.356)	0.279
41	3.42	1.20	0.432	0.117	(0.389)	0.315
42	3.50	1.30	0.468	0.117	(0.421)	0.351
43	3.58	1.40	0.504	0.117	(0.454)	0.387
44	3.67	1.40	0.504	0.117	(0.454)	0.387
45	3.75	1.50	0.540	0.117	(0.486)	0.423
46	3.83	1.50	0.540	0.117	(0.486)	0.423
47	3.92	1.60	0.576	0.117	(0.518)	0.459
48	4.00	1.60	0.576	0.117	(0.518)	0.459
49	4.08	1.70	0.612	0.117	(0.551)	0.495
50	4.17	1.80	0.648	0.117	(0.583)	0.531
51	4.25	1.90	0.684	0.117	(0.616)	0.567
52	4.33	2.00	0.720	0.117	(0.648)	0.603
53	4.42	2.10	0.756	0.117	(0.680)	0.639
54	4.50	2.10	0.756	0.117	(0.680)	0.639
55	4.58	2.20	0.792	0.117	(0.713)	0.675
56	4.67	2.30	0.828	0.117	(0.745)	0.711
57	4.75	2.40	0.864	0.117	(0.778)	0.747
58	4.83	2.40	0.864	0.117	(0.778)	0.747
59	4.92	2.50	0.900	0.117	(0.810)	0.783
60	5.00	2.60	0.936	0.117	(0.842)	0.819
61	5.08	3.10	1.116	0.117	(1.004)	0.999
62	5.17	3.60	1.296	0.117	(1.166)	1.179
63	5.25	3.90	1.404	0.117	(1.263)	1.287
64	5.33	4.20	1.512	0.117	(1.361)	1.395
65	5.42	4.70	1.692	0.117	(1.523)	1.575
66	5.50	5.60	2.016	0.117	(1.814)	1.899
67	5.58	1.90	0.684	0.117	(0.616)	0.567
68	5.67	0.90	0.324	0.117	(0.292)	0.207
69	5.75	0.60	0.216	0.117	(0.194)	0.099
70	5.83	0.50	0.180	0.117	(0.162)	0.063

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71   5.92     0.30      0.108       (  0.117)       0.097        0.011
72   6.00     0.20      0.072       (  0.117)       0.065        0.007
               (Loss Rate Not Used)
   Sum =     100.0                                  Sum =    27.6
      Flood volume = Effective rainfall      2.30(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       5.1(Ac.Ft)
      Total soil loss =      0.70(In)
      Total soil loss =     1.551(Ac.Ft)
      Total rainfall =      3.00(In)
      Flood volume =      223613.9 Cubic Feet
      Total soil loss =       67558.0 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     44.275(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        12.5       25.0       37.5       50.0
-------------------------------------------------------------------------------
  0+ 5       0.0041      0.60  Q          |          |          |          |
  0+10       0.0160      1.73  VQ         |          |          |          |
  0+15       0.0322      2.36  VQ         |          |          |          |
  0+20       0.0497      2.54  V Q        |          |          |          |
  0+25       0.0678      2.62  V Q        |          |          |          |
  0+30       0.0885      3.00  V Q        |          |          |          |
  0+35       0.1123      3.46  V Q        |          |          |          |
  0+40       0.1368      3.56  |VQ        |          |          |          |
  0+45       0.1617      3.61  |VQ        |          |          |          |
  0+50       0.1867      3.63  |VQ        |          |          |          |
  0+55       0.2118      3.64  |VQ        |          |          |          |
  1+ 0       0.2392      3.98  |V Q       |          |          |          |
  1+ 5       0.2697      4.43  | VQ       |          |          |          |
  1+10       0.3009      4.53  | VQ       |          |          |          |
  1+15       0.3325      4.58  | VQ       |          |          |          |
  1+20       0.3642      4.60  | VQ       |          |          |          |
  1+25       0.3959      4.61  |  Q       |          |          |          |
  1+30       0.4276      4.61  |  Q       |          |          |          |
  1+35       0.4594      4.61  |  Q       |          |          |          |
  1+40       0.4911      4.61  |  Q       |          |          |          |
  1+45       0.5229      4.61  |  QV      |          |          |          |
  1+50       0.5546      4.61  |  QV      |          |          |          |
  1+55       0.5864      4.61  |  QV      |          |          |          |
  2+ 0       0.6205      4.95  |  QV      |          |          |          |
  2+ 5       0.6553      5.06  |   QV     |          |          |          |
  2+10       0.6902      5.05  |   QV     |          |          |          |
  2+15       0.7277      5.45  |   QV     |          |          |          |
  2+20       0.7657      5.53  |   QV     |          |          |          |
  2+25       0.8040      5.56  |   Q V    |          |          |          |
  2+30       0.8424      5.57  |   Q V    |          |          |          |
  2+35       0.8808      5.58  |   Q V    |          |          |          |
  2+40       0.9192      5.58  |   Q  V   |          |          |          |
  2+45       0.9600      5.92  |   Q  V   |          |          |          |
  2+50       1.0039      6.37  |    Q V   |          |          |          |
  2+55       1.0485      6.48  |    Q  V  |          |          |          |
  3+ 0       1.0934      6.52  |    Q  V  |          |          |          |
  3+ 5       1.1385      6.54  |    Q  V  |          |          |          |
  3+10       1.1859      6.89  |    Q   V |          |          |          |
  3+15       1.2365      7.34  |    Q   V |          |          |          |
  3+20       1.2878      7.45  |    Q    V|          |          |          |
  3+25       1.3417      7.83  |     Q   V|          |          |          |
  3+30       1.4013      8.65  |     Q   V|          |          |          |
  3+35       1.4670      9.55  |      Q  |V          |          |          |
  3+40       1.5369     10.15  |       Q |V          |          |          |
  3+45       1.6104     10.66  |       Q | V         |          |          |
  3+50       1.6874     11.19  |       Q |  V        |          |          |
  3+55       1.7677     11.66  |        Q|  V        |          |          |
  4+ 0       1.8515     12.16  |        Q|   V       |          |          |
  4+ 5       1.9385     12.63  |         Q    V    |          |          |
  4+10       2.0313     13.48  |         Q    V    |          |          |
  4+15       2.1304     14.39  |         |Q    V    |          |          |
  4+20       2.2361     15.34  |         | Q    V   |          |          |
  4+25       2.3484     16.30  |         |  Q    V  |          |          |
  4+30       2.4650     16.93  |         |  Q     V|          |          |
  4+35       2.5852     17.45  |         |  Q      V          |          |
  4+40       2.7114     18.32  |         |   Q     |V         |          |
  4+45       2.8439     19.25  |         |    Q    | V        |          |
  4+50       2.9807     19.85  |         |    Q    |  V       |          |
  4+55       3.1209     20.37  |         |     Q   |   V      |          |
  5+ 0       3.2672     21.23  |         |     Q   |    V     |          |
  5+ 5       3.4291     23.52  |         |       Q |     V    |          |
  5+10       3.6195     27.64  |         |         | Q     V  |          |
  5+15       3.8364     31.50  |         |         |    Q   V|          |
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    5+20       4.0750     34.65  |          |          |       Q  |V         |
    5+25       4.3392     38.36  |          |          |          Q  V       |
    5+30       4.6441     44.27  |          |          |          |    QV    |
    5+35       4.8953     36.47  |          |          |         Q|       V  |
    5+40       5.0169     17.66  |          |    Q     |          |         V|
    5+45       5.0776      8.82  |          Q          |          |         V|
    5+50       5.1098      4.66  |    Q     |          |          |         V|
    5+55       5.1251      2.23  |Q         |          |          |         V|
    6+ 0       5.1304      0.77  Q          |          |          |         V|
    6+ 5       5.1325      0.31  Q          |          |          |         V|
    6+10       5.1332      0.10  Q          |          |          |         V|
    6+15       5.1334      0.03  Q          |          |          |         V|
    6+20       5.1335      0.01  Q          |          |          |         V|
    6+25       5.1335      0.00  Q          |          |          |         V|
-------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: ex110024100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 1087.00(Ft.)
Length along longest watercourse measured to centroid = 544.00(Ft.)
Length along longest watercourse = 0.206 Mi.
Length along longest watercourse measured to centroid = 0.103 Mi.
Difference in elevation = 88.30(Ft.)
Slope along watercourse = 428.9089 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.80	48.13

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	5.00	133.70

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 5.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 5.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.000

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.322	35.130	9.467
2	0.167	316.645	46.393	12.502
3	0.250	474.967	10.719	2.889
4	0.333	633.290	4.631	1.248
5	0.417	791.612	2.248	0.606
6	0.500	949.935	0.879	0.237
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.040	(0.207)	0.036	0.004
2	0.17	0.07	0.040	(0.207)	0.036	0.004
3	0.25	0.07	0.040	(0.206)	0.036	0.004
4	0.33	0.10	0.060	(0.205)	0.054	0.006
5	0.42	0.10	0.060	(0.204)	0.054	0.006
6	0.50	0.10	0.060	(0.203)	0.054	0.006
7	0.58	0.10	0.060	(0.203)	0.054	0.006
8	0.67	0.10	0.060	(0.202)	0.054	0.006
9	0.75	0.10	0.060	(0.201)	0.054	0.006
10	0.83	0.13	0.080	(0.200)	0.072	0.008
11	0.92	0.13	0.080	(0.199)	0.072	0.008
12	1.00	0.13	0.080	(0.199)	0.072	0.008
13	1.08	0.10	0.060	(0.198)	0.054	0.006
14	1.17	0.10	0.060	(0.197)	0.054	0.006
15	1.25	0.10	0.060	(0.196)	0.054	0.006
16	1.33	0.10	0.060	(0.196)	0.054	0.006
17	1.42	0.10	0.060	(0.195)	0.054	0.006
18	1.50	0.10	0.060	(0.194)	0.054	0.006
19	1.58	0.10	0.060	(0.193)	0.054	0.006
20	1.67	0.10	0.060	(0.192)	0.054	0.006
21	1.75	0.10	0.060	(0.192)	0.054	0.006
22	1.83	0.13	0.080	(0.191)	0.072	0.008
23	1.92	0.13	0.080	(0.190)	0.072	0.008
24	2.00	0.13	0.080	(0.189)	0.072	0.008
25	2.08	0.13	0.080	(0.189)	0.072	0.008
26	2.17	0.13	0.080	(0.188)	0.072	0.008
27	2.25	0.13	0.080	(0.187)	0.072	0.008
28	2.33	0.13	0.080	(0.186)	0.072	0.008
29	2.42	0.13	0.080	(0.186)	0.072	0.008
30	2.50	0.13	0.080	(0.185)	0.072	0.008
31	2.58	0.17	0.100	(0.184)	0.090	0.010
32	2.67	0.17	0.100	(0.183)	0.090	0.010
33	2.75	0.17	0.100	(0.183)	0.090	0.010
34	2.83	0.17	0.100	(0.182)	0.090	0.010
35	2.92	0.17	0.100	(0.181)	0.090	0.010
36	3.00	0.17	0.100	(0.180)	0.090	0.010
37	3.08	0.17	0.100	(0.180)	0.090	0.010
38	3.17	0.17	0.100	(0.179)	0.090	0.010
39	3.25	0.17	0.100	(0.178)	0.090	0.010
40	3.33	0.17	0.100	(0.177)	0.090	0.010
41	3.42	0.17	0.100	(0.177)	0.090	0.010
42	3.50	0.17	0.100	(0.176)	0.090	0.010
43	3.58	0.17	0.100	(0.175)	0.090	0.010
44	3.67	0.17	0.100	(0.174)	0.090	0.010
45	3.75	0.17	0.100	(0.174)	0.090	0.010
46	3.83	0.20	0.120	(0.173)	0.108	0.012
47	3.92	0.20	0.120	(0.172)	0.108	0.012
48	4.00	0.20	0.120	(0.171)	0.108	0.012
49	4.08	0.20	0.120	(0.171)	0.108	0.012
50	4.17	0.20	0.120	(0.170)	0.108	0.012
51	4.25	0.20	0.120	(0.169)	0.108	0.012
52	4.33	0.23	0.140	(0.169)	0.126	0.014
53	4.42	0.23	0.140	(0.168)	0.126	0.014
54	4.50	0.23	0.140	(0.167)	0.126	0.014
55	4.58	0.23	0.140	(0.166)	0.126	0.014
56	4.67	0.23	0.140	(0.166)	0.126	0.014
57	4.75	0.23	0.140	(0.165)	0.126	0.014
58	4.83	0.27	0.160	(0.164)	0.144	0.016
59	4.92	0.27	0.160	(0.164)	0.144	0.016
60	5.00	0.27	0.160	(0.163)	0.144	0.016
61	5.08	0.20	0.120	(0.162)	0.108	0.012
62	5.17	0.20	0.120	(0.161)	0.108	0.012
63	5.25	0.20	0.120	(0.161)	0.108	0.012
64	5.33	0.23	0.140	(0.160)	0.126	0.014
65	5.42	0.23	0.140	(0.159)	0.126	0.014
66	5.50	0.23	0.140	(0.159)	0.126	0.014
67	5.58	0.27	0.160	(0.158)	0.144	0.016
68	5.67	0.27	0.160	(0.157)	0.144	0.016
69	5.75	0.27	0.160	(0.157)	0.144	0.016
70	5.83	0.27	0.160	(0.156)	0.144	0.016

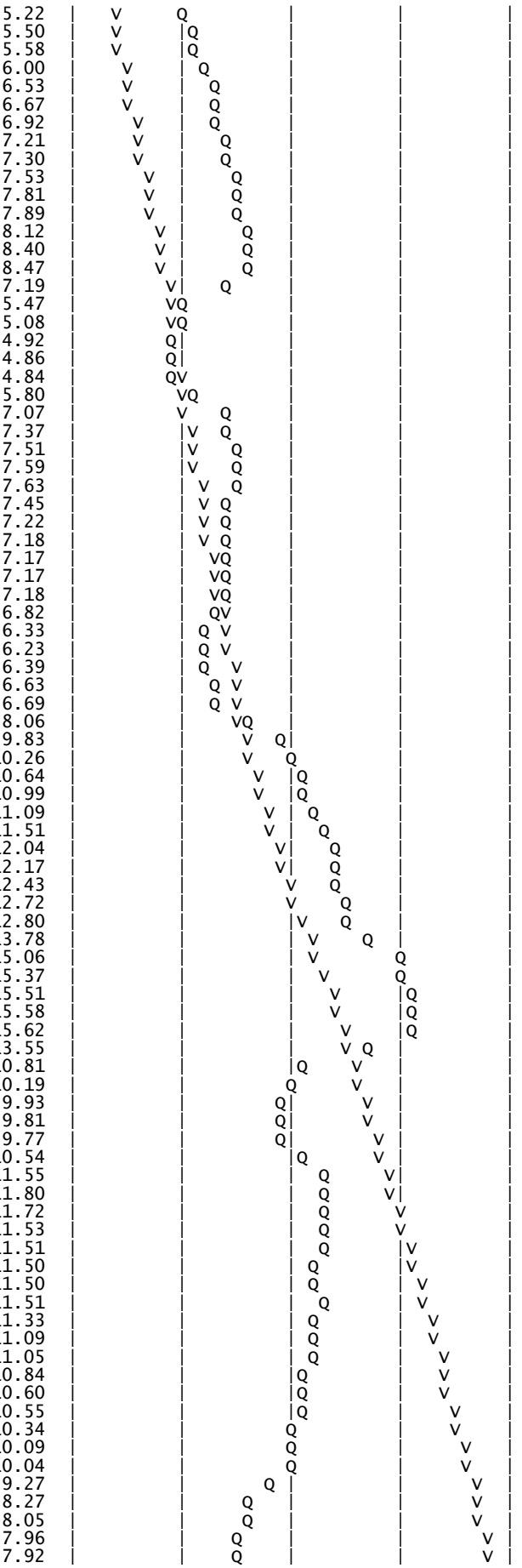
71	5.92	0.27	0.160	(	0.155)	0.144		0.016
72	6.00	0.27	0.160	(	0.154)	0.144		0.016
73	6.08	0.30	0.180		0.154	(0.162)		0.026
74	6.17	0.30	0.180		0.153	(0.162)		0.027
75	6.25	0.30	0.180		0.152	(0.162)		0.028
76	6.33	0.30	0.180		0.152	(0.162)		0.028
77	6.42	0.30	0.180		0.151	(0.162)		0.029
78	6.50	0.30	0.180		0.150	(0.162)		0.030
79	6.58	0.33	0.200		0.150	(0.180)		0.050
80	6.67	0.33	0.200		0.149	(0.180)		0.051
81	6.75	0.33	0.200		0.148	(0.180)		0.052
82	6.83	0.33	0.200		0.148	(0.180)		0.052
83	6.92	0.33	0.200		0.147	(0.180)		0.053
84	7.00	0.33	0.200		0.146	(0.180)		0.054
85	7.08	0.33	0.200		0.146	(0.180)		0.054
86	7.17	0.33	0.200		0.145	(0.180)		0.055
87	7.25	0.33	0.200		0.144	(0.180)		0.056
88	7.33	0.37	0.220		0.144	(0.198)		0.076
89	7.42	0.37	0.220		0.143	(0.198)		0.077
90	7.50	0.37	0.220		0.142	(0.198)		0.078
91	7.58	0.40	0.240		0.142	(0.216)		0.098
92	7.67	0.40	0.240		0.141	(0.216)		0.099
93	7.75	0.40	0.240		0.140	(0.216)		0.100
94	7.83	0.43	0.260		0.140	(0.234)		0.120
95	7.92	0.43	0.260		0.139	(0.234)		0.121
96	8.00	0.43	0.260		0.138	(0.234)		0.122
97	8.08	0.50	0.300		0.138	(0.270)		0.162
98	8.17	0.50	0.300		0.137	(0.270)		0.163
99	8.25	0.50	0.300		0.137	(0.270)		0.163
100	8.33	0.50	0.300		0.136	(0.270)		0.164
101	8.42	0.50	0.300		0.135	(0.270)		0.165
102	8.50	0.50	0.300		0.135	(0.270)		0.165
103	8.58	0.53	0.320		0.134	(0.288)		0.186
104	8.67	0.53	0.320		0.133	(0.288)		0.187
105	8.75	0.53	0.320		0.133	(0.288)		0.187
106	8.83	0.57	0.340		0.132	(0.306)		0.208
107	8.92	0.57	0.340		0.131	(0.306)		0.208
108	9.00	0.57	0.340		0.131	(0.306)		0.209
109	9.08	0.63	0.380		0.130	(0.342)		0.250
110	9.17	0.63	0.380		0.130	(0.342)		0.250
111	9.25	0.63	0.380		0.129	(0.342)		0.251
112	9.33	0.67	0.400		0.128	(0.360)		0.272
113	9.42	0.67	0.400		0.128	(0.360)		0.272
114	9.50	0.67	0.400		0.127	(0.360)		0.273
115	9.58	0.70	0.420		0.127	(0.378)		0.293
116	9.67	0.70	0.420		0.126	(0.378)		0.294
117	9.75	0.70	0.420		0.125	(0.378)		0.295
118	9.83	0.73	0.440		0.125	(0.396)		0.315
119	9.92	0.73	0.440		0.124	(0.396)		0.316
120	10.00	0.73	0.440		0.124	(0.396)		0.316
121	10.08	0.50	0.300		0.123	(0.270)		0.177
122	10.17	0.50	0.300		0.122	(0.270)		0.178
123	10.25	0.50	0.300		0.122	(0.270)		0.178
124	10.33	0.50	0.300		0.121	(0.270)		0.179
125	10.42	0.50	0.300		0.121	(0.270)		0.179
126	10.50	0.50	0.300		0.120	(0.270)		0.180
127	10.58	0.67	0.400		0.119	(0.360)		0.281
128	10.67	0.67	0.400		0.119	(0.360)		0.281
129	10.75	0.67	0.400		0.118	(0.360)		0.282
130	10.83	0.67	0.400		0.118	(0.360)		0.282
131	10.92	0.67	0.400		0.117	(0.360)		0.283
132	11.00	0.67	0.400		0.117	(0.360)		0.283
133	11.08	0.63	0.380		0.116	(0.342)		0.264
134	11.17	0.63	0.380		0.115	(0.342)		0.265
135	11.25	0.63	0.380		0.115	(0.342)		0.265
136	11.33	0.63	0.380		0.114	(0.342)		0.266
137	11.42	0.63	0.380		0.114	(0.342)		0.266
138	11.50	0.63	0.380		0.113	(0.342)		0.267
139	11.58	0.57	0.340		0.113	(0.306)		0.227
140	11.67	0.57	0.340		0.112	(0.306)		0.228
141	11.75	0.57	0.340		0.111	(0.306)		0.229
142	11.83	0.60	0.360		0.111	(0.324)		0.249
143	11.92	0.60	0.360		0.110	(0.324)		0.250
144	12.00	0.60	0.360		0.110	(0.324)		0.250
145	12.08	0.83	0.500		0.109	(0.450)		0.391
146	12.17	0.83	0.500		0.109	(0.450)		0.391
147	12.25	0.83	0.500		0.108	(0.450)		0.392
148	12.33	0.87	0.520		0.108	(0.468)		0.412
149	12.42	0.87	0.520		0.107	(0.468)		0.413
150	12.50	0.87	0.520		0.107	(0.468)		0.413
151	12.58	0.93	0.560		0.106	(0.504)		0.454
152	12.67	0.93	0.560		0.105	(0.504)		0.455
153	12.75	0.93	0.560		0.105	(0.504)		0.455
154	12.83	0.97	0.580		0.104	(0.522)		0.476
155	12.92	0.97	0.580		0.104	(0.522)		0.476
156	13.00	0.97	0.580		0.103	(0.522)		0.477

157	13.08	1.13	0.680	0.103	(0.612)	0.577
158	13.17	1.13	0.680	0.102	(0.612)	0.578
159	13.25	1.13	0.680	0.102	(0.612)	0.578
160	13.33	1.13	0.680	0.101	(0.612)	0.579
161	13.42	1.13	0.680	0.101	(0.612)	0.579
162	13.50	1.13	0.680	0.100	(0.612)	0.580
163	13.58	0.77	0.460	0.100	(0.414)	0.360
164	13.67	0.77	0.460	0.099	(0.414)	0.361
165	13.75	0.77	0.460	0.099	(0.414)	0.361
166	13.83	0.77	0.460	0.098	(0.414)	0.362
167	13.92	0.77	0.460	0.098	(0.414)	0.362
168	14.00	0.77	0.460	0.097	(0.414)	0.363
169	14.08	0.90	0.540	0.097	(0.486)	0.443
170	14.17	0.90	0.540	0.096	(0.486)	0.444
171	14.25	0.90	0.540	0.096	(0.486)	0.444
172	14.33	0.87	0.520	0.095	(0.468)	0.425
173	14.42	0.87	0.520	0.095	(0.468)	0.425
174	14.50	0.87	0.520	0.094	(0.468)	0.426
175	14.58	0.87	0.520	0.094	(0.468)	0.426
176	14.67	0.87	0.520	0.093	(0.468)	0.427
177	14.75	0.87	0.520	0.093	(0.468)	0.427
178	14.83	0.83	0.500	0.092	(0.450)	0.408
179	14.92	0.83	0.500	0.092	(0.450)	0.408
180	15.00	0.83	0.500	0.091	(0.450)	0.409
181	15.08	0.80	0.480	0.091	(0.432)	0.389
182	15.17	0.80	0.480	0.090	(0.432)	0.390
183	15.25	0.80	0.480	0.090	(0.432)	0.390
184	15.33	0.77	0.460	0.090	(0.414)	0.370
185	15.42	0.77	0.460	0.089	(0.414)	0.371
186	15.50	0.77	0.460	0.089	(0.414)	0.371
187	15.58	0.63	0.380	0.088	(0.342)	0.292
188	15.67	0.63	0.380	0.088	(0.342)	0.292
189	15.75	0.63	0.380	0.087	(0.342)	0.293
190	15.83	0.63	0.380	0.087	(0.342)	0.293
191	15.92	0.63	0.380	0.086	(0.342)	0.294
192	16.00	0.63	0.380	0.086	(0.342)	0.294
193	16.08	0.13	0.080	(0.085)	0.072	0.008
194	16.17	0.13	0.080	(0.085)	0.072	0.008
195	16.25	0.13	0.080	(0.085)	0.072	0.008
196	16.33	0.13	0.080	(0.084)	0.072	0.008
197	16.42	0.13	0.080	(0.084)	0.072	0.008
198	16.50	0.13	0.080	(0.083)	0.072	0.008
199	16.58	0.10	0.060	(0.083)	0.054	0.006
200	16.67	0.10	0.060	(0.082)	0.054	0.006
201	16.75	0.10	0.060	(0.082)	0.054	0.006
202	16.83	0.10	0.060	(0.082)	0.054	0.006
203	16.92	0.10	0.060	(0.081)	0.054	0.006
204	17.00	0.10	0.060	(0.081)	0.054	0.006
205	17.08	0.17	0.100	0.080	(0.090)	0.020
206	17.17	0.17	0.100	0.080	(0.090)	0.020
207	17.25	0.17	0.100	0.080	(0.090)	0.020
208	17.33	0.17	0.100	0.079	(0.090)	0.021
209	17.42	0.17	0.100	0.079	(0.090)	0.021
210	17.50	0.17	0.100	0.078	(0.090)	0.022
211	17.58	0.17	0.100	0.078	(0.090)	0.022
212	17.67	0.17	0.100	0.078	(0.090)	0.022
213	17.75	0.17	0.100	0.077	(0.090)	0.023
214	17.83	0.13	0.080	(0.077)	0.072	0.008
215	17.92	0.13	0.080	(0.076)	0.072	0.008
216	18.00	0.13	0.080	(0.076)	0.072	0.008
217	18.08	0.13	0.080	(0.076)	0.072	0.008
218	18.17	0.13	0.080	(0.075)	0.072	0.008
219	18.25	0.13	0.080	(0.075)	0.072	0.008
220	18.33	0.13	0.080	(0.075)	0.072	0.008
221	18.42	0.13	0.080	(0.074)	0.072	0.008
222	18.50	0.13	0.080	(0.074)	0.072	0.008
223	18.58	0.10	0.060	(0.074)	0.054	0.006
224	18.67	0.10	0.060	(0.073)	0.054	0.006
225	18.75	0.10	0.060	(0.073)	0.054	0.006
226	18.83	0.07	0.040	(0.072)	0.036	0.004
227	18.92	0.07	0.040	(0.072)	0.036	0.004
228	19.00	0.07	0.040	(0.072)	0.036	0.004
229	19.08	0.10	0.060	(0.071)	0.054	0.006
230	19.17	0.10	0.060	(0.071)	0.054	0.006
231	19.25	0.10	0.060	(0.071)	0.054	0.006
232	19.33	0.13	0.080	0.070	(0.072)	0.010
233	19.42	0.13	0.080	0.070	(0.072)	0.010
234	19.50	0.13	0.080	0.070	(0.072)	0.010
235	19.58	0.10	0.060	(0.069)	0.054	0.006
236	19.67	0.10	0.060	(0.069)	0.054	0.006
237	19.75	0.10	0.060	(0.069)	0.054	0.006
238	19.83	0.07	0.040	(0.069)	0.036	0.004
239	19.92	0.07	0.040	(0.068)	0.036	0.004
240	20.00	0.07	0.040	(0.068)	0.036	0.004
241	20.08	0.10	0.060	(0.068)	0.054	0.006
242	20.17	0.10	0.060	(0.067)	0.054	0.006

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243  20.25     0.10      0.060       (  0.067)       0.054        0.006
244  20.33     0.10      0.060       (  0.067)       0.054        0.006
245  20.42     0.10      0.060       (  0.066)       0.054        0.006
246  20.50     0.10      0.060       (  0.066)       0.054        0.006
247  20.58     0.10      0.060       (  0.066)       0.054        0.006
248  20.67     0.10      0.060       (  0.066)       0.054        0.006
249  20.75     0.10      0.060       (  0.065)       0.054        0.006
250  20.83     0.07      0.040       (  0.065)       0.036        0.004
251  20.92     0.07      0.040       (  0.065)       0.036        0.004
252  21.00     0.07      0.040       (  0.065)       0.036        0.004
253  21.08     0.10      0.060       (  0.064)       0.054        0.006
254  21.17     0.10      0.060       (  0.064)       0.054        0.006
255  21.25     0.10      0.060       (  0.064)       0.054        0.006
256  21.33     0.07      0.040       (  0.064)       0.036        0.004
257  21.42     0.07      0.040       (  0.063)       0.036        0.004
258  21.50     0.07      0.040       (  0.063)       0.036        0.004
259  21.58     0.10      0.060       (  0.063)       0.054        0.006
260  21.67     0.10      0.060       (  0.063)       0.054        0.006
261  21.75     0.10      0.060       (  0.062)       0.054        0.006
262  21.83     0.07      0.040       (  0.062)       0.036        0.004
263  21.92     0.07      0.040       (  0.062)       0.036        0.004
264  22.00     0.07      0.040       (  0.062)       0.036        0.004
265  22.08     0.10      0.060       (  0.062)       0.054        0.006
266  22.17     0.10      0.060       (  0.061)       0.054        0.006
267  22.25     0.10      0.060       (  0.061)       0.054        0.006
268  22.33     0.07      0.040       (  0.061)       0.036        0.004
269  22.42     0.07      0.040       (  0.061)       0.036        0.004
270  22.50     0.07      0.040       (  0.061)       0.036        0.004
271  22.58     0.07      0.040       (  0.060)       0.036        0.004
272  22.67     0.07      0.040       (  0.060)       0.036        0.004
273  22.75     0.07      0.040       (  0.060)       0.036        0.004
274  22.83     0.07      0.040       (  0.060)       0.036        0.004
275  22.92     0.07      0.040       (  0.060)       0.036        0.004
276  23.00     0.07      0.040       (  0.060)       0.036        0.004
277  23.08     0.07      0.040       (  0.060)       0.036        0.004
278  23.17     0.07      0.040       (  0.059)       0.036        0.004
279  23.25     0.07      0.040       (  0.059)       0.036        0.004
280  23.33     0.07      0.040       (  0.059)       0.036        0.004
281  23.42     0.07      0.040       (  0.059)       0.036        0.004
282  23.50     0.07      0.040       (  0.059)       0.036        0.004
283  23.58     0.07      0.040       (  0.059)       0.036        0.004
284  23.67     0.07      0.040       (  0.059)       0.036        0.004
285  23.75     0.07      0.040       (  0.059)       0.036        0.004
286  23.83     0.07      0.040       (  0.059)       0.036        0.004
287  23.92     0.07      0.040       (  0.059)       0.036        0.004
288  24.00     0.07      0.040       (  0.059)       0.036        0.004
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    34.3
      Flood volume = Effective rainfall      2.86(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       6.4(Ac.Ft)
      Total soil loss =      2.14(In)
      Total soil loss =     4.773(Ac.Ft)
      Total rainfall =      5.00(In)
      Flood volume =      277384.6 Cubic Feet
      Total soil loss =      207921.0 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     15.619(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
 ---------------------------------------------------------------------------
   0+ 5       0.0003      0.04  Q          |          |          |          |
   0+10       0.0009      0.09  Q          |          |          |          |
   0+15       0.0016      0.10  Q          |          |          |          |
   0+20       0.0024      0.12  Q          |          |          |          |
   0+25       0.0034      0.15  Q          |          |          |          |
   0+30       0.0045      0.16  Q          |          |          |          |
   0+35       0.0056      0.16  Q          |          |          |          |
   0+40       0.0067      0.16  Q          |          |          |          |
   0+45       0.0079      0.16  Q          |          |          |          |
   0+50       0.0091      0.18  Q          |          |          |          |
   0+55       0.0105      0.21  Q          |          |          |          |
   1+ 0       0.0120      0.21  Q          |          |          |          |
   1+ 5       0.0133      0.20  Q          |          |          |          |
   1+10       0.0145      0.17  Q          |          |          |          |
   1+15       0.0156      0.17  Q          |          |          |          |
   1+20       0.0168      0.16  Q          |          |          |          |
   1+25       0.0179      0.16  Q          |          |          |          |
   1+30       0.0190      0.16  Q          |          |          |          |
   1+35       0.0201      0.16  Q          |          |          |          |
```

1+40	0.0212	0.16	Q	|	|	|	|
1+45	0.0223	0.16	Q	|	|	|	|
1+50	0.0236	0.18	Q	|	|	|	|
1+55	0.0250	0.21	Q	|	|	|	|
2+ 0	0.0265	0.21	Q	|	|	|	|
2+ 5	0.0279	0.21	Q	|	|	|	|
2+10	0.0294	0.22	Q	|	|	|	|
2+15	0.0309	0.22	Q	|	|	|	|
2+20	0.0324	0.22	Q	|	|	|	|
2+25	0.0339	0.22	Q	|	|	|	|
2+30	0.0354	0.22	Q	|	|	|	|
2+35	0.0370	0.23	Q	|	|	|	|
2+40	0.0388	0.26	Q	|	|	|	|
2+45	0.0406	0.27	Q	|	|	|	|
2+50	0.0424	0.27	Q	|	|	|	|
2+55	0.0443	0.27	Q	|	|	|	|
3+ 0	0.0461	0.27	Q	|	|	|	|
3+ 5	0.0480	0.27	Q	|	|	|	|
3+10	0.0499	0.27	Q	|	|	|	|
3+15	0.0517	0.27	Q	|	|	|	|
3+20	0.0536	0.27	Q	|	|	|	|
3+25	0.0554	0.27	Q	|	|	|	|
3+30	0.0573	0.27	Q	|	|	|	|
3+35	0.0591	0.27	Q	|	|	|	|
3+40	0.0610	0.27	Q	|	|	|	|
3+45	0.0629	0.27	Q	|	|	|	|
3+50	0.0648	0.29	Q	|	|	|	|
3+55	0.0670	0.31	Q	|	|	|	|
4+ 0	0.0692	0.32	Q	|	|	|	|
4+ 5	0.0714	0.32	Q	|	|	|	|
4+10	0.0736	0.32	Q	|	|	|	|
4+15	0.0759	0.32	Q	|	|	|	|
4+20	0.0782	0.34	Q	|	|	|	|
4+25	0.0808	0.37	Q	|	|	|	|
4+30	0.0833	0.37	Q	|	|	|	|
4+35	0.0859	0.38	Q	|	|	|	|
4+40	0.0885	0.38	Q	|	|	|	|
4+45	0.0911	0.38	Q	|	|	|	|
4+50	0.0938	0.40	Q	|	|	|	|
4+55	0.0967	0.42	Q	|	|	|	|
5+ 0	0.0997	0.43	Q	|	|	|	|
5+ 5	0.1024	0.39	Q	|	|	|	|
5+10	0.1047	0.34	Q	|	|	|	|
5+15	0.1070	0.33	Q	|	|	|	|
5+20	0.1094	0.35	Q	|	|	|	|
5+25	0.1120	0.37	Q	|	|	|	|
5+30	0.1145	0.37	Q	|	|	|	|
5+35	0.1172	0.39	Q	|	|	|	|
5+40	0.1201	0.42	Q	|	|	|	|
5+45	0.1231	0.43	Q	|	|	|	|
5+50	0.1260	0.43	Q	|	|	|	|
5+55	0.1290	0.43	Q	|	|	|	|
6+ 0	0.1320	0.43	Q	|	|	|	|
6+ 5	0.1356	0.53	VQ	|	|	|	|
6+10	0.1402	0.66	VQ	|	|	|	|
6+15	0.1451	0.71	VQ	|	|	|	|
6+20	0.1501	0.74	VQ	|	|	|	|
6+25	0.1554	0.76	VQ	|	|	|	|
6+30	0.1608	0.78	|Q	|	|	|	|
6+35	0.1676	0.99	|Q	|	|	|	|
6+40	0.1762	1.26	|VQ	|	|	|	|
6+45	0.1854	1.33	|VQ	|	|	|	|
6+50	0.1949	1.38	|VQ	|	|	|	|
6+55	0.2046	1.41	|VQ	|	|	|	|
7+ 0	0.2145	1.43	|VQ	|	|	|	|
7+ 5	0.2244	1.45	|VQ	|	|	|	|
7+10	0.2345	1.47	|VQ	|	|	|	|
7+15	0.2447	1.48	|VQ	|	|	|	|
7+20	0.2564	1.69	|V Q	|	|	|	|
7+25	0.2699	1.96	|V Q	|	|	|	|
7+30	0.2839	2.03	|V Q	|	|	|	|
7+35	0.2995	2.27	|V Q	|	|	|	|
7+40	0.3170	2.55	|V Q	|	|	|	|
7+45	0.3351	2.63	| V Q	|	|	|	|
7+50	0.3548	2.86	| V Q	|	|	|	|
7+55	0.3764	3.14	| V Q	|	|	|	|
8+ 0	0.3986	3.22	| V Q	|	|	|	|
8+ 5	0.4236	3.64	| V Q	|	|	|	|
8+10	0.4524	4.17	| V Q	|	|	|	|
8+15	0.4820	4.31	| V Q	|	|	|	|
8+20	0.5121	4.37	| V Q	|	|	|	|
8+25	0.5426	4.42	| V Q	|	|	|	|
8+30	0.5731	4.44	| V Q	|	|	|	|
8+35	0.6052	4.65	| V Q|	|	|	|
8+40	0.6390	4.92	| V Q|	|	|	|
8+45	0.6734	4.99	| V Q|	|	|	|

8+50	0.7093	5.22	
8+55	0.7472	5.50	
9+ 0	0.7857	5.58	
9+ 5	0.8270	6.00	
9+10	0.8720	6.53	
9+15	0.9179	6.67	
9+20	0.9656	6.92	
9+25	1.0153	7.21	
9+30	1.0655	7.30	
9+35	1.1174	7.53	
9+40	1.1711	7.81	
9+45	1.2255	7.89	
9+50	1.2814	8.12	
9+55	1.3392	8.40	
10+ 0	1.3975	8.47	
10+ 5	1.4471	7.19	
10+10	1.4847	5.47	
10+15	1.5197	5.08	
10+20	1.5536	4.92	
10+25	1.5871	4.86	
10+30	1.6204	4.84	
10+35	1.6603	5.80	
10+40	1.7090	7.07	
10+45	1.7598	7.37	
10+50	1.8115	7.51	
10+55	1.8638	7.59	
11+ 0	1.9163	7.63	
11+ 5	1.9677	7.45	
11+10	2.0174	7.22	
11+15	2.0668	7.18	
11+20	2.1162	7.17	
11+25	2.1656	7.17	
11+30	2.2150	7.18	
11+35	2.2620	6.82	
11+40	2.3056	6.33	
11+45	2.3485	6.23	
11+50	2.3925	6.39	
11+55	2.4381	6.63	
12+ 0	2.4842	6.69	
12+ 5	2.5397	8.06	
12+10	2.6074	9.83	
12+15	2.6781	10.26	
12+20	2.7513	10.64	
12+25	2.8270	10.99	
12+30	2.9034	11.09	
12+35	2.9827	11.51	
12+40	3.0656	12.04	
12+45	3.1494	12.17	
12+50	3.2350	12.43	
12+55	3.3226	12.72	
13+ 0	3.4107	12.80	
13+ 5	3.5056	13.78	
13+10	3.6093	15.06	
13+15	3.7152	15.37	
13+20	3.8220	15.51	
13+25	3.9293	15.58	
13+30	4.0368	15.62	
13+35	4.1301	13.55	
13+40	4.2046	10.81	
13+45	4.2748	10.19	
13+50	4.3431	9.93	
13+55	4.4107	9.81	
14+ 0	4.4780	9.77	
14+ 5	4.5506	10.54	
14+10	4.6301	11.55	
14+15	4.7114	11.80	
14+20	4.7921	11.72	
14+25	4.8716	11.53	
14+30	4.9508	11.51	
14+35	5.0300	11.50	
14+40	5.1092	11.50	
14+45	5.1884	11.51	
14+50	5.2664	11.33	
14+55	5.3428	11.09	
15+ 0	5.4189	11.05	
15+ 5	5.4936	10.84	
15+10	5.5666	10.60	
15+15	5.6392	10.55	
15+20	5.7104	10.34	
15+25	5.7799	10.09	
15+30	5.8491	10.04	
15+35	5.9130	9.27	
15+40	5.9699	8.27	
15+45	6.0254	8.05	
15+50	6.0802	7.96	
15+55	6.1348	7.92	

16+ 0	6.1893	7.92	|	| Q	|	| V |
16+ 5	6.2252	5.22	|	Q |	|	| V|
16+10	6.2365	1.64	| Q	|	|	| V|
16+15	6.2421	0.81	|Q	|	|	| V|
16+20	6.2453	0.46	Q	|	|	| V|
16+25	6.2472	0.28	Q	|	|	| V|
16+30	6.2487	0.22	Q	|	|	| V|
16+35	6.2501	0.20	Q	|	|	| V|
16+40	6.2512	0.17	Q	|	|	| V|
16+45	6.2524	0.17	Q	|	|	| V|
16+50	6.2535	0.16	Q	|	|	| V|
16+55	6.2546	0.16	Q	|	|	| V|
17+ 0	6.2557	0.16	Q	|	|	| V|
17+ 5	6.2577	0.29	Q	|	|	| V|
17+10	6.2609	0.46	Q	|	|	| V|
17+15	6.2645	0.51	|Q	|	|	| V|
17+20	6.2682	0.54	|Q	|	|	| V|
17+25	6.2720	0.56	|Q	|	|	| V|
17+30	6.2760	0.57	|Q	|	|	| V|
17+35	6.2800	0.58	|Q	|	|	| V|
17+40	6.2841	0.59	|Q	|	|	| V|
17+45	6.2882	0.60	|Q	|	|	| V|
17+50	6.2914	0.47	Q	|	|	| V|
17+55	6.2934	0.29	Q	|	|	| V|
18+ 0	6.2951	0.25	Q	|	|	| V|
18+ 5	6.2967	0.23	Q	|	|	| V|
18+10	6.2982	0.22	Q	|	|	| V|
18+15	6.2997	0.22	Q	|	|	| V|
18+20	6.3012	0.22	Q	|	|	| V|
18+25	6.3027	0.22	Q	|	|	| V|
18+30	6.3041	0.22	Q	|	|	| V|
18+35	6.3055	0.20	Q	|	|	| V|
18+40	6.3067	0.17	Q	|	|	| V|
18+45	6.3078	0.17	Q	|	|	| V|
18+50	6.3088	0.14	Q	|	|	| V|
18+55	6.3096	0.12	Q	|	|	| V|
19+ 0	6.3104	0.11	Q	|	|	| V|
19+ 5	6.3113	0.13	Q	|	|	| V|
19+10	6.3123	0.15	Q	|	|	| V|
19+15	6.3134	0.16	Q	|	|	| V|
19+20	6.3148	0.19	Q	|	|	| V|
19+25	6.3164	0.24	Q	|	|	| V|
19+30	6.3182	0.26	Q	|	|	| V|
19+35	6.3198	0.23	Q	|	|	| V|
19+40	6.3210	0.18	Q	|	|	| V|
19+45	6.3222	0.17	Q	|	|	| V|
19+50	6.3232	0.15	Q	|	|	| V|
19+55	6.3240	0.12	Q	|	|	| V|
20+ 0	6.3248	0.11	Q	|	|	| V|
20+ 5	6.3257	0.13	Q	|	|	| V|
20+10	6.3268	0.15	Q	|	|	| V|
20+15	6.3278	0.16	Q	|	|	| V|
20+20	6.3289	0.16	Q	|	|	| V|
20+25	6.3300	0.16	Q	|	|	| V|
20+30	6.3312	0.16	Q	|	|	| V|
20+35	6.3323	0.16	Q	|	|	| V|
20+40	6.3334	0.16	Q	|	|	| V|
20+45	6.3345	0.16	Q	|	|	| V|
20+50	6.3355	0.14	Q	|	|	| V|
20+55	6.3363	0.12	Q	|	|	| V|
21+ 0	6.3371	0.11	Q	|	|	| V|
21+ 5	6.3380	0.13	Q	|	|	| V|
21+10	6.3390	0.15	Q	|	|	| V|
21+15	6.3401	0.16	Q	|	|	| V|
21+20	6.3411	0.14	Q	|	|	| V|
21+25	6.3419	0.12	Q	|	|	| V|
21+30	6.3426	0.11	Q	|	|	| V|
21+35	6.3435	0.13	Q	|	|	| V|
21+40	6.3446	0.15	Q	|	|	| V|
21+45	6.3457	0.16	Q	|	|	| V|
21+50	6.3466	0.14	Q	|	|	| V|
21+55	6.3474	0.12	Q	|	|	| V|
22+ 0	6.3482	0.11	Q	|	|	| V|
22+ 5	6.3491	0.13	Q	|	|	| V|
22+10	6.3501	0.15	Q	|	|	| V|
22+15	6.3512	0.16	Q	|	|	| V|
22+20	6.3522	0.14	Q	|	|	| V|
22+25	6.3530	0.12	Q	|	|	| V|
22+30	6.3538	0.11	Q	|	|	| V|
22+35	6.3545	0.11	Q	|	|	| V|
22+40	6.3553	0.11	Q	|	|	| V|
22+45	6.3560	0.11	Q	|	|	| V|
22+50	6.3568	0.11	Q	|	|	| V|
22+55	6.3575	0.11	Q	|	|	| V|
23+ 0	6.3583	0.11	Q	|	|	| V|
23+ 5	6.3590	0.11	Q	|	|	| V|

```
   23+10       6.3597      0.11  Q          |          |          |         v|
   23+15       6.3605      0.11  Q          |          |          |         v|
   23+20       6.3612      0.11  Q          |          |          |         v|
   23+25       6.3620      0.11  Q          |          |          |         v|
   23+30       6.3627      0.11  Q          |          |          |         v|
   23+35       6.3635      0.11  Q          |          |          |         v|
   23+40       6.3642      0.11  Q          |          |          |         v|
   23+45       6.3649      0.11  Q          |          |          |         v|
   23+50       6.3657      0.11  Q          |          |          |         v|
   23+55       6.3664      0.11  Q          |          |          |         v|
   24+ 0       6.3672      0.11  Q          |          |          |         v|
   24+ 5       6.3677      0.07  Q          |          |          |         v|
   24+10       6.3678      0.02  Q          |          |          |         v|
   24+15       6.3678      0.01  Q          |          |          |         v|
   24+20       6.3679      0.00  Q          |          |          |         v|
   24+25       6.3679      0.00  Q          |          |          |          v
-------------------------------------------------------------------------------
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Extended Detention Basin No. 2

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       U n i t   H y d r o g r a p h   A n a l y s i s

       Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2008, Version 8.1
              Study date  04/22/24 File: EX2212.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2127.00(Ft.)
Length along longest watercourse measured to centroid =    1064.00(Ft.)
Length along longest watercourse =      0.403 Mi.
Length along longest watercourse measured to centroid =      0.202 Mi.
Difference in elevation =     160.00(Ft.)
Slope along watercourse =    397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.089 Hr.
Lag time =     5.34 Min.
25% of lag time =     1.33 Min.
40% of lag time =     2.13 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           0.50                 25.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           1.30                 67.34

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.500(In)
Areal adjustment factor =   99.95 %
Adjusted average point rain =    0.500(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           91.00         0.000
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.198	(0.246)	0.178	0.020
2	0.17	4.20	0.252	(0.246)	0.227	0.025
3	0.25	4.40	0.264	(0.246)	0.237	0.026
4	0.33	4.80	0.288	0.246	(0.259)	0.042
5	0.42	5.20	0.312	0.246	(0.281)	0.065
6	0.50	6.20	0.372	0.246	(0.335)	0.125
7	0.58	6.80	0.408	0.246	(0.367)	0.161
8	0.67	8.80	0.528	0.246	(0.475)	0.281
9	0.75	13.90	0.834	0.246	(0.750)	0.587
10	0.83	31.40	1.883	0.246	(1.695)	1.637
11	0.92	7.20	0.432	0.246	(0.389)	0.185
12	1.00	3.80	0.228	(0.246)	0.205	0.023
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	3.2

Flood volume = Effective rainfall 0.26(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 1.1(Ac.Ft)
Total soil loss = 0.23(In)
Total soil loss = 1.014(Ac.Ft)
Total rainfall = 0.50(In)
Flood volume = 49811.8 Cubic Feet
Total soil loss = 44161.1 Cubic Feet

Peak flow rate of this hydrograph = 49.310(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	12.5	25.0	37.5	50.0
0+ 5	0.0012	0.18	Q				
0+10	0.0062	0.72	Q				
0+15	0.0133	1.04	Q				
0+20	0.0225	1.33	VQ				
0+25	0.0362	2.00	|Q				
0+30	0.0591	3.31	| Q				
0+35	0.0965	5.43	| VQ				
0+40	0.1521	8.08	| VQ				
0+45	0.2517	14.46	| V |Q				
0+50	0.4784	32.93	| | V | Q |				
0+55	0.8180	49.31	| | | V | Q|				
1+ 0	0.9723	22.41	| | Q | | V |				
1+ 5	1.0446	10.49	| Q | | | V |				
1+10	1.0846	5.81	| Q | | | V |				
1+15	1.1097	3.65	| Q | | | V |				
1+20	1.1259	2.35	|Q | | | V|				
1+25	1.1361	1.47	|Q | | | V|				
1+30	1.1427	0.96	Q | | | V|				
1+35	1.1434	0.11	Q | | | V|				
1+40	1.1435	0.01	Q | | | V|				

```
       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/22/24 File: EX2232.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2127.00(Ft.)
Length along longest watercourse measured to centroid =    1064.00(Ft.)
Length along longest watercourse =      0.403 Mi.
Length along longest watercourse measured to centroid =      0.202 Mi.
Difference in elevation =     160.00(Ft.)
Slope along watercourse =    397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.089 Hr.
Lag time =     5.34 Min.
25% of lag time =     1.33 Min.
40% of lag time =     2.13 Min.
Unit time =     5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           0.80                 41.44

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           2.00                103.60

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    0.800(In)
Area Averaged 100-Year Rainfall =    2.000(In)

Point rain (area averaged) =    0.800(In)
Areal adjustment factor =   99.98 %
Adjusted average point rain =    0.800(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           91.00         0.000
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.125	(0.246)	0.112	0.012
2	0.17	1.30	0.125	(0.246)	0.112	0.012
3	0.25	1.10	0.106	(0.246)	0.095	0.011
4	0.33	1.50	0.144	(0.246)	0.130	0.014
5	0.42	1.50	0.144	(0.246)	0.130	0.014
6	0.50	1.80	0.173	(0.246)	0.155	0.017
7	0.58	1.50	0.144	(0.246)	0.130	0.014
8	0.67	1.80	0.173	(0.246)	0.155	0.017
9	0.75	1.80	0.173	(0.246)	0.155	0.017
10	0.83	1.50	0.144	(0.246)	0.130	0.014
11	0.92	1.60	0.154	(0.246)	0.138	0.015
12	1.00	1.80	0.173	(0.246)	0.155	0.017
13	1.08	2.20	0.211	(0.246)	0.190	0.021
14	1.17	2.20	0.211	(0.246)	0.190	0.021
15	1.25	2.20	0.211	(0.246)	0.190	0.021
16	1.33	2.00	0.192	(0.246)	0.173	0.019
17	1.42	2.60	0.250	(0.246)	0.225	0.025
18	1.50	2.70	0.259	(0.246)	0.233	0.026
19	1.58	2.40	0.230	(0.246)	0.207	0.023
20	1.67	2.70	0.259	(0.246)	0.233	0.026
21	1.75	3.30	0.317	0.246	(0.285)	0.070
22	1.83	3.10	0.298	0.246	(0.268)	0.051
23	1.92	2.90	0.278	0.246	(0.251)	0.032
24	2.00	3.00	0.288	0.246	(0.259)	0.042
25	2.08	3.10	0.298	0.246	(0.268)	0.051
26	2.17	4.20	0.403	0.246	(0.363)	0.157
27	2.25	5.00	0.480	0.246	(0.432)	0.234
28	2.33	3.50	0.336	0.246	(0.302)	0.090
29	2.42	6.80	0.653	0.246	(0.587)	0.406
30	2.50	7.30	0.701	0.246	(0.631)	0.454
31	2.58	8.20	0.787	0.246	(0.708)	0.541
32	2.67	5.90	0.566	0.246	(0.510)	0.320
33	2.75	2.00	0.192	(0.246)	0.173	0.019
34	2.83	1.80	0.173	(0.246)	0.155	0.017
35	2.92	1.80	0.173	(0.246)	0.155	0.017
36	3.00	0.60	0.058	(0.246)	0.052	0.006
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	2.9

Flood volume = Effective rainfall 0.24(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 1.0(Ac.Ft)
Total soil loss = 0.56(In)
Total soil loss = 2.421(Ac.Ft)
Total rainfall = 0.80(In)
Flood volume = 44919.4 Cubic Feet
Total soil loss = 105473.7 Cubic Feet

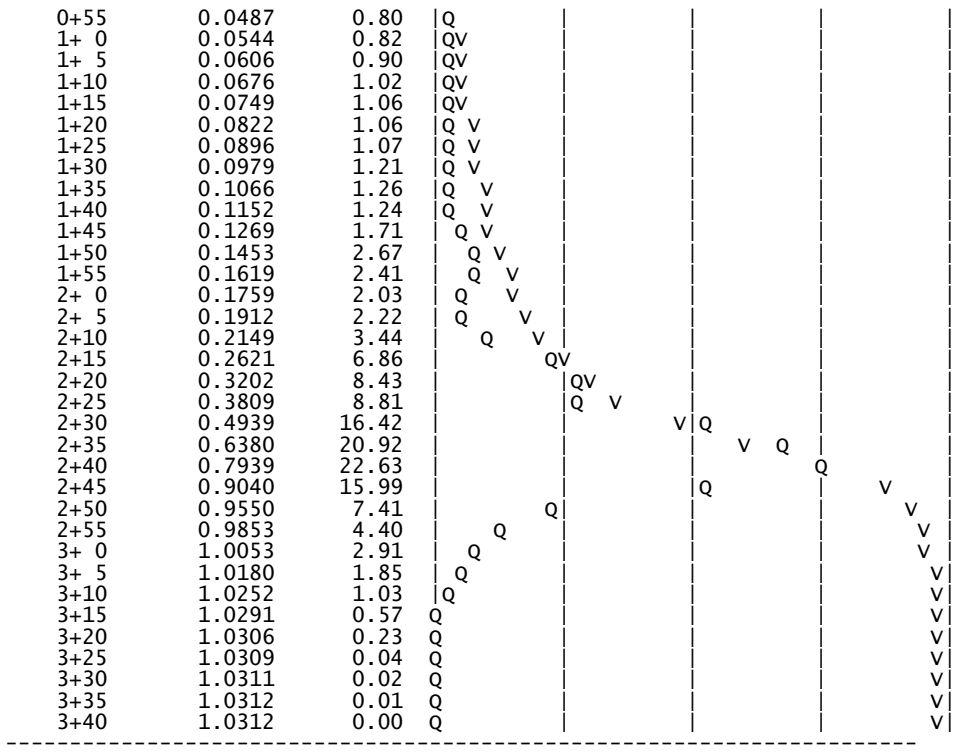
Peak flow rate of this hydrograph = 22.628(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0008	0.11	Q	|	|	|	|
0+10	0.0037	0.42	Q	|	|	|	|
0+15	0.0072	0.52	Q	|	|	|	|
0+20	0.0110	0.55	Q	|	|	|	|
0+25	0.0156	0.66	Q	|	|	|	|
0+30	0.0206	0.73	Q	|	|	|	|
0+35	0.0260	0.79	|Q	|	|	|	|
0+40	0.0315	0.79	|Q	|	|	|	|
0+45	0.0373	0.86	|Q	|	|	|	|
0+50	0.0432	0.85	|Q	|	|	|	|



0+55	0.0487	0.80	
1+ 0	0.0544	0.82	
1+ 5	0.0606	0.90	
1+10	0.0676	1.02	
1+15	0.0749	1.06	
1+20	0.0822	1.06	
1+25	0.0896	1.07	
1+30	0.0979	1.21	
1+35	0.1066	1.26	
1+40	0.1152	1.24	
1+45	0.1269	1.71	
1+50	0.1453	2.67	
1+55	0.1619	2.41	
2+ 0	0.1759	2.03	
2+ 5	0.1912	2.22	
2+10	0.2149	3.44	
2+15	0.2621	6.86	
2+20	0.3202	8.43	
2+25	0.3809	8.81	
2+30	0.4939	16.42	
2+35	0.6380	20.92	
2+40	0.7939	22.63	
2+45	0.9040	15.99	
2+50	0.9550	7.41	
2+55	0.9853	4.40	
3+ 0	1.0053	2.91	
3+ 5	1.0180	1.85	
3+10	1.0252	1.03	
3+15	1.0291	0.57	
3+20	1.0306	0.23	
3+25	1.0309	0.04	
3+30	1.0311	0.02	
3+35	1.0312	0.01	
3+40	1.0312	0.00	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX2262.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2127.00(Ft.)
Length along longest watercourse measured to centroid = 1064.00(Ft.)
Length along longest watercourse = 0.403 Mi.
Length along longest watercourse measured to centroid = 0.202 Mi.
Difference in elevation = 160.00(Ft.)
Slope along watercourse = 397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.089 Hr.
Lag time = 5.34 Min.
25% of lag time = 1.33 Min.
40% of lag time = 2.13 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	1.10	56.98

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	3.00	155.40

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.100(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 1.100(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	91.00	0.000

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000 Sum=	52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.066	(0.246)	0.059	0.007
2	0.17	0.60	0.079	(0.246)	0.071	0.008
3	0.25	0.60	0.079	(0.246)	0.071	0.008
4	0.33	0.60	0.079	(0.246)	0.071	0.008
5	0.42	0.60	0.079	(0.246)	0.071	0.008
6	0.50	0.70	0.092	(0.246)	0.083	0.009
7	0.58	0.70	0.092	(0.246)	0.083	0.009
8	0.67	0.70	0.092	(0.246)	0.083	0.009
9	0.75	0.70	0.092	(0.246)	0.083	0.009
10	0.83	0.70	0.092	(0.246)	0.083	0.009
11	0.92	0.70	0.092	(0.246)	0.083	0.009
12	1.00	0.80	0.106	(0.246)	0.095	0.011
13	1.08	0.80	0.106	(0.246)	0.095	0.011
14	1.17	0.80	0.106	(0.246)	0.095	0.011
15	1.25	0.80	0.106	(0.246)	0.095	0.011
16	1.33	0.80	0.106	(0.246)	0.095	0.011
17	1.42	0.80	0.106	(0.246)	0.095	0.011
18	1.50	0.80	0.106	(0.246)	0.095	0.011
19	1.58	0.80	0.106	(0.246)	0.095	0.011
20	1.67	0.80	0.106	(0.246)	0.095	0.011
21	1.75	0.80	0.106	(0.246)	0.095	0.011
22	1.83	0.80	0.106	(0.246)	0.095	0.011
23	1.92	0.80	0.106	(0.246)	0.095	0.011
24	2.00	0.90	0.119	(0.246)	0.107	0.012
25	2.08	0.80	0.106	(0.246)	0.095	0.011
26	2.17	0.90	0.119	(0.246)	0.107	0.012
27	2.25	0.90	0.119	(0.246)	0.107	0.012
28	2.33	0.90	0.119	(0.246)	0.107	0.012
29	2.42	0.90	0.119	(0.246)	0.107	0.012
30	2.50	0.90	0.119	(0.246)	0.107	0.012
31	2.58	0.90	0.119	(0.246)	0.107	0.012
32	2.67	0.90	0.119	(0.246)	0.107	0.012
33	2.75	1.00	0.132	(0.246)	0.119	0.013
34	2.83	1.00	0.132	(0.246)	0.119	0.013
35	2.92	1.00	0.132	(0.246)	0.119	0.013
36	3.00	1.00	0.132	(0.246)	0.119	0.013
37	3.08	1.00	0.132	(0.246)	0.119	0.013
38	3.17	1.10	0.145	(0.246)	0.131	0.015
39	3.25	1.10	0.145	(0.246)	0.131	0.015
40	3.33	1.10	0.145	(0.246)	0.131	0.015
41	3.42	1.20	0.158	(0.246)	0.143	0.016
42	3.50	1.30	0.172	(0.246)	0.154	0.017
43	3.58	1.40	0.185	(0.246)	0.166	0.018
44	3.67	1.40	0.185	(0.246)	0.166	0.018
45	3.75	1.50	0.198	(0.246)	0.178	0.020
46	3.83	1.50	0.198	(0.246)	0.178	0.020
47	3.92	1.60	0.211	(0.246)	0.190	0.021
48	4.00	1.60	0.211	(0.246)	0.190	0.021
49	4.08	1.70	0.224	(0.246)	0.202	0.022
50	4.17	1.80	0.238	(0.246)	0.214	0.024
51	4.25	1.90	0.251	(0.246)	0.226	0.025
52	4.33	2.00	0.264	(0.246)	0.238	0.026
53	4.42	2.10	0.277	0.246	(0.249)	0.031
54	4.50	2.10	0.277	0.246	(0.249)	0.031
55	4.58	2.20	0.290	0.246	(0.261)	0.044
56	4.67	2.30	0.304	0.246	(0.273)	0.057
57	4.75	2.40	0.317	0.246	(0.285)	0.070
58	4.83	2.40	0.317	0.246	(0.285)	0.070
59	4.92	2.50	0.330	0.246	(0.297)	0.084
60	5.00	2.60	0.343	0.246	(0.309)	0.097
61	5.08	3.10	0.409	0.246	(0.368)	0.163
62	5.17	3.60	0.475	0.246	(0.428)	0.229
63	5.25	3.90	0.515	0.246	(0.463)	0.268
64	5.33	4.20	0.554	0.246	(0.499)	0.308
65	5.42	4.70	0.620	0.246	(0.558)	0.374
66	5.50	5.60	0.739	0.246	(0.665)	0.493
67	5.58	1.90	0.251	(0.246)	0.226	0.025

```
68   5.67     0.90      0.119       (  0.246)       0.107        0.012
69   5.75     0.60      0.079       (  0.246)       0.071        0.008
70   5.83     0.50      0.066       (  0.246)       0.059        0.007
71   5.92     0.30      0.040       (  0.246)       0.036        0.004
72   6.00     0.20      0.026       (  0.246)       0.024        0.003
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =     3.1
      Flood volume = Effective rainfall      0.26(In)
       times area      51.8(Ac.)/[(In)/(Ft.)] =       1.1(Ac.Ft)
      Total soil loss =      0.84(In)
      Total soil loss =     3.646(Ac.Ft)
      Total rainfall =      1.10(In)
      Flood volume =       47970.0 Cubic Feet
      Total soil loss =      158830.6 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     18.407(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f     H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
-------------------------------------------------------------------------
  0+ 5       0.0004      0.06  Q          |          |          |          |
  0+10       0.0020      0.24  Q          |          |          |          |
  0+15       0.0043      0.33  Q          |          |          |          |
  0+20       0.0068      0.36  Q          |          |          |          |
  0+25       0.0094      0.38  Q          |          |          |          |
  0+30       0.0122      0.41  Q          |          |          |          |
  0+35       0.0153      0.45  Q          |          |          |          |
  0+40       0.0185      0.47  Q          |          |          |          |
  0+45       0.0218      0.47  Q          |          |          |          |
  0+50       0.0251      0.48  Q          |          |          |          |
  0+55       0.0284      0.48  QV         |          |          |          |
  1+ 0       0.0318      0.49  QV         |          |          |          |
  1+ 5       0.0354      0.53  |Q         |          |          |          |
  1+10       0.0391      0.54  |Q         |          |          |          |
  1+15       0.0429      0.54  |Q         |          |          |          |
  1+20       0.0466      0.55  |Q         |          |          |          |
  1+25       0.0504      0.55  |Q         |          |          |          |
  1+30       0.0542      0.55  |Q         |          |          |          |
  1+35       0.0580      0.55  |QV        |          |          |          |
  1+40       0.0618      0.55  |QV        |          |          |          |
  1+45       0.0656      0.55  |QV        |          |          |          |
  1+50       0.0694      0.55  |QV        |          |          |          |
  1+55       0.0732      0.55  |QV        |          |          |          |
  2+ 0       0.0771      0.56  |QV        |          |          |          |
  2+ 5       0.0811      0.58  |QV        |          |          |          |
  2+10       0.0850      0.57  |Q V       |          |          |          |
  2+15       0.0892      0.60  |Q V       |          |          |          |
  2+20       0.0934      0.61  |Q V       |          |          |          |
  2+25       0.0976      0.61  |Q V       |          |          |          |
  2+30       0.1019      0.62  |Q V       |          |          |          |
  2+35       0.1061      0.62  |Q V       |          |          |          |
  2+40       0.1104      0.62  |Q  V      |          |          |          |
  2+45       0.1148      0.63  |Q  V      |          |          |          |
  2+50       0.1193      0.67  |Q  V      |          |          |          |
  2+55       0.1240      0.68  |Q  V      |          |          |          |
  3+ 0       0.1287      0.68  |Q  V      |          |          |          |
  3+ 5       0.1334      0.68  |Q  V      |          |          |          |
  3+10       0.1382      0.70  |Q   V     |          |          |          |
  3+15       0.1433      0.73  |Q   V     |          |          |          |
  3+20       0.1484      0.74  |Q   V     |          |          |          |
  3+25       0.1536      0.76  |Q   V     |          |          |          |
  3+30       0.1592      0.81  |Q   V     |          |          |          |
  3+35       0.1652      0.87  |Q    V    |          |          |          |
  3+40       0.1715      0.92  |Q    V    |          |          |          |
  3+45       0.1781      0.95  |Q    V    |          |          |          |
  3+50       0.1850      1.00  |Q    V    |          |          |          |
  3+55       0.1920      1.02  | Q   V    |          |          |          |
  4+ 0       0.1994      1.07  | Q    V   |          |          |          |
  4+ 5       0.2069      1.10  | Q    V   |          |          |          |
  4+10       0.2148      1.15  | Q    V   |          |          |          |
  4+15       0.2231      1.21  | Q     V  |          |          |          |
  4+20       0.2319      1.27  | Q     V  |          |          |          |
  4+25       0.2413      1.37  | Q     V  |          |          |          |
  4+30       0.2517      1.50  | Q      V|          |          |          |
  4+35       0.2632      1.67  |  Q     V|          |          |          |
  4+40       0.2779      2.14  |   Q     V          |          |          |
  4+45       0.2966      2.72  |    Q    V          |          |          |
  4+50       0.3188      3.22  |     Q   |V         |          |          |
  4+55       0.3432      3.54  |      Q  | V        |          |          |
  5+ 0       0.3714      4.09  |       Q |  V       |          |          |
```

```
    5+ 5       0.4072      5.20  |          Q   V     |          |          |
    5+10       0.4598      7.64  |          |    QV   |          |          |
    5+15       0.5309     10.33  |          |       VQ          |          |
    5+20       0.6174     12.56  |          |          | V  Q    |          |
    5+25       0.7203     14.93  |          |          |    V  Q|          |
    5+30       0.8470     18.41  |          |          |        V     Q    |
    5+35       0.9719     18.13  |          |          |          |    VQ   |
    5+40       1.0264      7.91  |          |    Q     |          |      V  |
    5+45       1.0556      4.24  |        Q |          |          |        V |
    5+50       1.0738      2.65  |     Q    |          |          |         V|
    5+55       1.0859      1.75  |   Q      |          |          |         V|
    6+ 0       1.0935      1.11  | Q        |          |          |         V|
    6+ 5       1.0981      0.67  |Q         |          |          |         V|
    6+10       1.1005      0.34  Q          |          |          |         V|
    6+15       1.1008      0.06  Q          |          |          |         V|
    6+20       1.1010      0.03  Q          |          |          |         V|
    6+25       1.1011      0.02  Q          |          |          |         V|
    6+30       1.1012      0.01  Q          |          |          |         V|
    6+35       1.1012      0.00  Q          |          |          |         V|
    6+40       1.1012      0.00  Q          |          |          |         V|
-------------------------------------------------------------------------
```

```
       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/22/24 File: EX22242.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2127.00(Ft.)
Length along longest watercourse measured to centroid =    1064.00(Ft.)
Length along longest watercourse =      0.403 Mi.
Length along longest watercourse measured to centroid =      0.202 Mi.
Difference in elevation =     160.00(Ft.)
Slope along watercourse =    397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.089 Hr.
Lag time =     5.34 Min.
25% of lag time =     1.33 Min.
40% of lag time =     2.13 Min.
Unit time =     5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           1.80                 93.24

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           5.00                259.00

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    1.800(In)
Area Averaged 100-Year Rainfall =    5.000(In)

Point rain (area averaged) =    1.800(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    1.800(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           91.00         0.000
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.014	(0.437)	0.013	0.001
2	0.17	0.07	0.014	(0.435)	0.013	0.001
3	0.25	0.07	0.014	(0.433)	0.013	0.001
4	0.33	0.10	0.022	(0.432)	0.019	0.002
5	0.42	0.10	0.022	(0.430)	0.019	0.002
6	0.50	0.10	0.022	(0.428)	0.019	0.002
7	0.58	0.10	0.022	(0.427)	0.019	0.002
8	0.67	0.10	0.022	(0.425)	0.019	0.002
9	0.75	0.10	0.022	(0.423)	0.019	0.002
10	0.83	0.13	0.029	(0.422)	0.026	0.003
11	0.92	0.13	0.029	(0.420)	0.026	0.003
12	1.00	0.13	0.029	(0.418)	0.026	0.003
13	1.08	0.10	0.022	(0.417)	0.019	0.002
14	1.17	0.10	0.022	(0.415)	0.019	0.002
15	1.25	0.10	0.022	(0.413)	0.019	0.002
16	1.33	0.10	0.022	(0.412)	0.019	0.002
17	1.42	0.10	0.022	(0.410)	0.019	0.002
18	1.50	0.10	0.022	(0.408)	0.019	0.002
19	1.58	0.10	0.022	(0.407)	0.019	0.002
20	1.67	0.10	0.022	(0.405)	0.019	0.002
21	1.75	0.10	0.022	(0.404)	0.019	0.002
22	1.83	0.13	0.029	(0.402)	0.026	0.003
23	1.92	0.13	0.029	(0.400)	0.026	0.003
24	2.00	0.13	0.029	(0.399)	0.026	0.003
25	2.08	0.13	0.029	(0.397)	0.026	0.003
26	2.17	0.13	0.029	(0.395)	0.026	0.003
27	2.25	0.13	0.029	(0.394)	0.026	0.003
28	2.33	0.13	0.029	(0.392)	0.026	0.003
29	2.42	0.13	0.029	(0.391)	0.026	0.003
30	2.50	0.13	0.029	(0.389)	0.026	0.003
31	2.58	0.17	0.036	(0.387)	0.032	0.004
32	2.67	0.17	0.036	(0.386)	0.032	0.004
33	2.75	0.17	0.036	(0.384)	0.032	0.004
34	2.83	0.17	0.036	(0.383)	0.032	0.004
35	2.92	0.17	0.036	(0.381)	0.032	0.004
36	3.00	0.17	0.036	(0.380)	0.032	0.004
37	3.08	0.17	0.036	(0.378)	0.032	0.004
38	3.17	0.17	0.036	(0.376)	0.032	0.004
39	3.25	0.17	0.036	(0.375)	0.032	0.004
40	3.33	0.17	0.036	(0.373)	0.032	0.004
41	3.42	0.17	0.036	(0.372)	0.032	0.004
42	3.50	0.17	0.036	(0.370)	0.032	0.004
43	3.58	0.17	0.036	(0.369)	0.032	0.004
44	3.67	0.17	0.036	(0.367)	0.032	0.004
45	3.75	0.17	0.036	(0.366)	0.032	0.004
46	3.83	0.20	0.043	(0.364)	0.039	0.004
47	3.92	0.20	0.043	(0.362)	0.039	0.004
48	4.00	0.20	0.043	(0.361)	0.039	0.004
49	4.08	0.20	0.043	(0.359)	0.039	0.004
50	4.17	0.20	0.043	(0.358)	0.039	0.004
51	4.25	0.20	0.043	(0.356)	0.039	0.004
52	4.33	0.23	0.050	(0.355)	0.045	0.005
53	4.42	0.23	0.050	(0.353)	0.045	0.005
54	4.50	0.23	0.050	(0.352)	0.045	0.005
55	4.58	0.23	0.050	(0.350)	0.045	0.005
56	4.67	0.23	0.050	(0.349)	0.045	0.005
57	4.75	0.23	0.050	(0.347)	0.045	0.005
58	4.83	0.27	0.058	(0.346)	0.052	0.006
59	4.92	0.27	0.058	(0.344)	0.052	0.006
60	5.00	0.27	0.058	(0.343)	0.052	0.006
61	5.08	0.20	0.043	(0.341)	0.039	0.004
62	5.17	0.20	0.043	(0.340)	0.039	0.004
63	5.25	0.20	0.043	(0.338)	0.039	0.004
64	5.33	0.23	0.050	(0.337)	0.045	0.005
65	5.42	0.23	0.050	(0.335)	0.045	0.005
66	5.50	0.23	0.050	(0.334)	0.045	0.005
67	5.58	0.27	0.058	(0.332)	0.052	0.006

68	5.67	0.27	0.058	(0.331)	0.052	0.006
69	5.75	0.27	0.058	(0.330)	0.052	0.006
70	5.83	0.27	0.058	(0.328)	0.052	0.006
71	5.92	0.27	0.058	(0.327)	0.052	0.006
72	6.00	0.27	0.058	(0.325)	0.052	0.006
73	6.08	0.30	0.065	(0.324)	0.058	0.006
74	6.17	0.30	0.065	(0.322)	0.058	0.006
75	6.25	0.30	0.065	(0.321)	0.058	0.006
76	6.33	0.30	0.065	(0.319)	0.058	0.006
77	6.42	0.30	0.065	(0.318)	0.058	0.006
78	6.50	0.30	0.065	(0.317)	0.058	0.006
79	6.58	0.33	0.072	(0.315)	0.065	0.007
80	6.67	0.33	0.072	(0.314)	0.065	0.007
81	6.75	0.33	0.072	(0.312)	0.065	0.007
82	6.83	0.33	0.072	(0.311)	0.065	0.007
83	6.92	0.33	0.072	(0.310)	0.065	0.007
84	7.00	0.33	0.072	(0.308)	0.065	0.007
85	7.08	0.33	0.072	(0.307)	0.065	0.007
86	7.17	0.33	0.072	(0.305)	0.065	0.007
87	7.25	0.33	0.072	(0.304)	0.065	0.007
88	7.33	0.37	0.079	(0.303)	0.071	0.008
89	7.42	0.37	0.079	(0.301)	0.071	0.008
90	7.50	0.37	0.079	(0.300)	0.071	0.008
91	7.58	0.40	0.086	(0.298)	0.078	0.009
92	7.67	0.40	0.086	(0.297)	0.078	0.009
93	7.75	0.40	0.086	(0.296)	0.078	0.009
94	7.83	0.43	0.094	(0.294)	0.084	0.009
95	7.92	0.43	0.094	(0.293)	0.084	0.009
96	8.00	0.43	0.094	(0.292)	0.084	0.009
97	8.08	0.50	0.108	(0.290)	0.097	0.011
98	8.17	0.50	0.108	(0.289)	0.097	0.011
99	8.25	0.50	0.108	(0.288)	0.097	0.011
100	8.33	0.50	0.108	(0.286)	0.097	0.011
101	8.42	0.50	0.108	(0.285)	0.097	0.011
102	8.50	0.50	0.108	(0.283)	0.097	0.011
103	8.58	0.53	0.115	(0.282)	0.104	0.012
104	8.67	0.53	0.115	(0.281)	0.104	0.012
105	8.75	0.53	0.115	(0.280)	0.104	0.012
106	8.83	0.57	0.122	(0.278)	0.110	0.012
107	8.92	0.57	0.122	(0.277)	0.110	0.012
108	9.00	0.57	0.122	(0.276)	0.110	0.012
109	9.08	0.63	0.137	(0.274)	0.123	0.014
110	9.17	0.63	0.137	(0.273)	0.123	0.014
111	9.25	0.63	0.137	(0.272)	0.123	0.014
112	9.33	0.67	0.144	(0.270)	0.130	0.014
113	9.42	0.67	0.144	(0.269)	0.130	0.014
114	9.50	0.67	0.144	(0.268)	0.130	0.014
115	9.58	0.70	0.151	(0.267)	0.136	0.015
116	9.67	0.70	0.151	(0.265)	0.136	0.015
117	9.75	0.70	0.151	(0.264)	0.136	0.015
118	9.83	0.73	0.158	(0.263)	0.143	0.016
119	9.92	0.73	0.158	(0.261)	0.143	0.016
120	10.00	0.73	0.158	(0.260)	0.143	0.016
121	10.08	0.50	0.108	(0.259)	0.097	0.011
122	10.17	0.50	0.108	(0.258)	0.097	0.011
123	10.25	0.50	0.108	(0.256)	0.097	0.011
124	10.33	0.50	0.108	(0.255)	0.097	0.011
125	10.42	0.50	0.108	(0.254)	0.097	0.011
126	10.50	0.50	0.108	(0.253)	0.097	0.011
127	10.58	0.67	0.144	(0.251)	0.130	0.014
128	10.67	0.67	0.144	(0.250)	0.130	0.014
129	10.75	0.67	0.144	(0.249)	0.130	0.014
130	10.83	0.67	0.144	(0.248)	0.130	0.014
131	10.92	0.67	0.144	(0.247)	0.130	0.014
132	11.00	0.67	0.144	(0.245)	0.130	0.014
133	11.08	0.63	0.137	(0.244)	0.123	0.014
134	11.17	0.63	0.137	(0.243)	0.123	0.014
135	11.25	0.63	0.137	(0.242)	0.123	0.014
136	11.33	0.63	0.137	(0.241)	0.123	0.014
137	11.42	0.63	0.137	(0.239)	0.123	0.014
138	11.50	0.63	0.137	(0.238)	0.123	0.014
139	11.58	0.57	0.122	(0.237)	0.110	0.012
140	11.67	0.57	0.122	(0.236)	0.110	0.012
141	11.75	0.57	0.122	(0.235)	0.110	0.012
142	11.83	0.60	0.130	(0.233)	0.117	0.013
143	11.92	0.60	0.130	(0.232)	0.117	0.013
144	12.00	0.60	0.130	(0.231)	0.117	0.013
145	12.08	0.83	0.180	(0.230)	0.162	0.018
146	12.17	0.83	0.180	(0.229)	0.162	0.018
147	12.25	0.83	0.180	(0.228)	0.162	0.018
148	12.33	0.87	0.187	(0.227)	0.168	0.019
149	12.42	0.87	0.187	(0.225)	0.168	0.019
150	12.50	0.87	0.187	(0.224)	0.168	0.019
151	12.58	0.93	0.202	(0.223)	0.181	0.020
152	12.67	0.93	0.202	(0.222)	0.181	0.020
153	12.75	0.93	0.202	(0.221)	0.181	0.020

154	12.83	0.97	0.209	(0.220)	0.188	0.021
155	12.92	0.97	0.209	(0.219)	0.188	0.021
156	13.00	0.97	0.209	(0.218)	0.188	0.021
157	13.08	1.13	0.245	0.216	(0.220)	0.028
158	13.17	1.13	0.245	0.215	(0.220)	0.029
159	13.25	1.13	0.245	0.214	(0.220)	0.031
160	13.33	1.13	0.245	0.213	(0.220)	0.032
161	13.42	1.13	0.245	0.212	(0.220)	0.033
162	13.50	1.13	0.245	0.211	(0.220)	0.034
163	13.58	0.77	0.166	(0.210)	0.149	0.017
164	13.67	0.77	0.166	(0.209)	0.149	0.017
165	13.75	0.77	0.166	(0.208)	0.149	0.017
166	13.83	0.77	0.166	(0.207)	0.149	0.017
167	13.92	0.77	0.166	(0.206)	0.149	0.017
168	14.00	0.77	0.166	(0.205)	0.149	0.017
169	14.08	0.90	0.194	(0.204)	0.175	0.019
170	14.17	0.90	0.194	(0.203)	0.175	0.019
171	14.25	0.90	0.194	(0.202)	0.175	0.019
172	14.33	0.87	0.187	(0.200)	0.168	0.019
173	14.42	0.87	0.187	(0.199)	0.168	0.019
174	14.50	0.87	0.187	(0.198)	0.168	0.019
175	14.58	0.87	0.187	(0.197)	0.168	0.019
176	14.67	0.87	0.187	(0.196)	0.168	0.019
177	14.75	0.87	0.187	(0.195)	0.168	0.019
178	14.83	0.83	0.180	(0.194)	0.162	0.018
179	14.92	0.83	0.180	(0.193)	0.162	0.018
180	15.00	0.83	0.180	(0.192)	0.162	0.018
181	15.08	0.80	0.173	(0.191)	0.156	0.017
182	15.17	0.80	0.173	(0.190)	0.156	0.017
183	15.25	0.80	0.173	(0.189)	0.156	0.017
184	15.33	0.77	0.166	(0.188)	0.149	0.017
185	15.42	0.77	0.166	(0.188)	0.149	0.017
186	15.50	0.77	0.166	(0.187)	0.149	0.017
187	15.58	0.63	0.137	(0.186)	0.123	0.014
188	15.67	0.63	0.137	(0.185)	0.123	0.014
189	15.75	0.63	0.137	(0.184)	0.123	0.014
190	15.83	0.63	0.137	(0.183)	0.123	0.014
191	15.92	0.63	0.137	(0.182)	0.123	0.014
192	16.00	0.63	0.137	(0.181)	0.123	0.014
193	16.08	0.13	0.029	(0.180)	0.026	0.003
194	16.17	0.13	0.029	(0.179)	0.026	0.003
195	16.25	0.13	0.029	(0.178)	0.026	0.003
196	16.33	0.13	0.029	(0.177)	0.026	0.003
197	16.42	0.13	0.029	(0.176)	0.026	0.003
198	16.50	0.13	0.029	(0.175)	0.026	0.003
199	16.58	0.10	0.022	(0.175)	0.019	0.002
200	16.67	0.10	0.022	(0.174)	0.019	0.002
201	16.75	0.10	0.022	(0.173)	0.019	0.002
202	16.83	0.10	0.022	(0.172)	0.019	0.002
203	16.92	0.10	0.022	(0.171)	0.019	0.002
204	17.00	0.10	0.022	(0.170)	0.019	0.002
205	17.08	0.17	0.036	(0.169)	0.032	0.004
206	17.17	0.17	0.036	(0.168)	0.032	0.004
207	17.25	0.17	0.036	(0.168)	0.032	0.004
208	17.33	0.17	0.036	(0.167)	0.032	0.004
209	17.42	0.17	0.036	(0.166)	0.032	0.004
210	17.50	0.17	0.036	(0.165)	0.032	0.004
211	17.58	0.17	0.036	(0.164)	0.032	0.004
212	17.67	0.17	0.036	(0.163)	0.032	0.004
213	17.75	0.17	0.036	(0.163)	0.032	0.004
214	17.83	0.13	0.029	(0.162)	0.026	0.003
215	17.92	0.13	0.029	(0.161)	0.026	0.003
216	18.00	0.13	0.029	(0.160)	0.026	0.003
217	18.08	0.13	0.029	(0.159)	0.026	0.003
218	18.17	0.13	0.029	(0.159)	0.026	0.003
219	18.25	0.13	0.029	(0.158)	0.026	0.003
220	18.33	0.13	0.029	(0.157)	0.026	0.003
221	18.42	0.13	0.029	(0.156)	0.026	0.003
222	18.50	0.13	0.029	(0.156)	0.026	0.003
223	18.58	0.10	0.022	(0.155)	0.019	0.002
224	18.67	0.10	0.022	(0.154)	0.019	0.002
225	18.75	0.10	0.022	(0.153)	0.019	0.002
226	18.83	0.07	0.014	(0.153)	0.013	0.001
227	18.92	0.07	0.014	(0.152)	0.013	0.001
228	19.00	0.07	0.014	(0.151)	0.013	0.001
229	19.08	0.10	0.022	(0.150)	0.019	0.002
230	19.17	0.10	0.022	(0.150)	0.019	0.002
231	19.25	0.10	0.022	(0.149)	0.019	0.002
232	19.33	0.13	0.029	(0.148)	0.026	0.003
233	19.42	0.13	0.029	(0.148)	0.026	0.003
234	19.50	0.13	0.029	(0.147)	0.026	0.003
235	19.58	0.10	0.022	(0.146)	0.019	0.002
236	19.67	0.10	0.022	(0.146)	0.019	0.002
237	19.75	0.10	0.022	(0.145)	0.019	0.002
238	19.83	0.07	0.014	(0.144)	0.013	0.001
239	19.92	0.07	0.014	(0.144)	0.013	0.001

240	20.00	0.07	0.014	(0.143)	0.013	0.001
241	20.08	0.10	0.022	(0.142)	0.019	0.002
242	20.17	0.10	0.022	(0.142)	0.019	0.002
243	20.25	0.10	0.022	(0.141)	0.019	0.002
244	20.33	0.10	0.022	(0.141)	0.019	0.002
245	20.42	0.10	0.022	(0.140)	0.019	0.002
246	20.50	0.10	0.022	(0.139)	0.019	0.002
247	20.58	0.10	0.022	(0.139)	0.019	0.002
248	20.67	0.10	0.022	(0.138)	0.019	0.002
249	20.75	0.10	0.022	(0.138)	0.019	0.002
250	20.83	0.07	0.014	(0.137)	0.013	0.001
251	20.92	0.07	0.014	(0.137)	0.013	0.001
252	21.00	0.07	0.014	(0.136)	0.013	0.001
253	21.08	0.10	0.022	(0.135)	0.019	0.002
254	21.17	0.10	0.022	(0.135)	0.019	0.002
255	21.25	0.10	0.022	(0.134)	0.019	0.002
256	21.33	0.07	0.014	(0.134)	0.013	0.001
257	21.42	0.07	0.014	(0.133)	0.013	0.001
258	21.50	0.07	0.014	(0.133)	0.013	0.001
259	21.58	0.10	0.022	(0.132)	0.019	0.002
260	21.67	0.10	0.022	(0.132)	0.019	0.002
261	21.75	0.10	0.022	(0.131)	0.019	0.002
262	21.83	0.07	0.014	(0.131)	0.013	0.001
263	21.92	0.07	0.014	(0.131)	0.013	0.001
264	22.00	0.07	0.014	(0.130)	0.013	0.001
265	22.08	0.10	0.022	(0.130)	0.019	0.002
266	22.17	0.10	0.022	(0.129)	0.019	0.002
267	22.25	0.10	0.022	(0.129)	0.019	0.002
268	22.33	0.07	0.014	(0.128)	0.013	0.001
269	22.42	0.07	0.014	(0.128)	0.013	0.001
270	22.50	0.07	0.014	(0.128)	0.013	0.001
271	22.58	0.07	0.014	(0.127)	0.013	0.001
272	22.67	0.07	0.014	(0.127)	0.013	0.001
273	22.75	0.07	0.014	(0.127)	0.013	0.001
274	22.83	0.07	0.014	(0.126)	0.013	0.001
275	22.92	0.07	0.014	(0.126)	0.013	0.001
276	23.00	0.07	0.014	(0.126)	0.013	0.001
277	23.08	0.07	0.014	(0.125)	0.013	0.001
278	23.17	0.07	0.014	(0.125)	0.013	0.001
279	23.25	0.07	0.014	(0.125)	0.013	0.001
280	23.33	0.07	0.014	(0.125)	0.013	0.001
281	23.42	0.07	0.014	(0.124)	0.013	0.001
282	23.50	0.07	0.014	(0.124)	0.013	0.001
283	23.58	0.07	0.014	(0.124)	0.013	0.001
284	23.67	0.07	0.014	(0.124)	0.013	0.001
285	23.75	0.07	0.014	(0.124)	0.013	0.001
286	23.83	0.07	0.014	(0.123)	0.013	0.001
287	23.92	0.07	0.014	(0.123)	0.013	0.001
288	24.00	0.07	0.014	(0.123)	0.013	0.001

(Loss Rate Not Used)

Sum = 100.0 Sum = 2.2

Flood volume = Effective rainfall 0.18(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 0.8(Ac.Ft)
Total soil loss = 1.62(In)
Total soil loss = 6.978(Ac.Ft)
Total rainfall = 1.80(In)
Flood volume = 34460.7 Cubic Feet
Total soil loss = 303966.3 Cubic Feet

Peak flow rate of this hydrograph = 1.661(CFS)

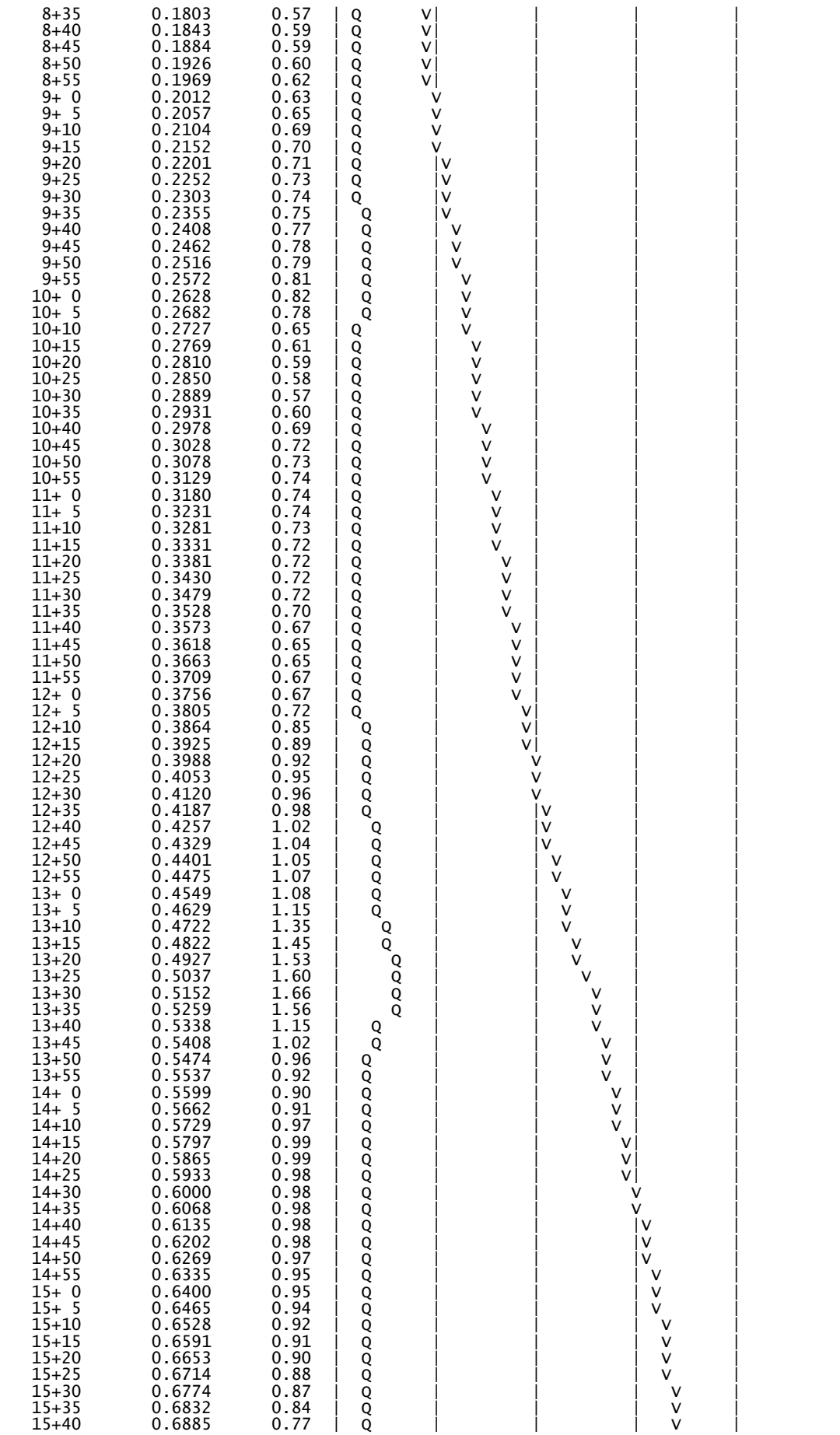
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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.01	Q	|	|	|	|
0+10	0.0004	0.05	Q	|	|	|	|
0+15	0.0008	0.06	Q	|	|	|	|
0+20	0.0014	0.07	Q	|	|	|	|
0+25	0.0020	0.09	Q	|	|	|	|
0+30	0.0027	0.10	Q	|	|	|	|
0+35	0.0035	0.11	Q	|	|	|	|
0+40	0.0042	0.11	Q	|	|	|	|
0+45	0.0050	0.11	Q	|	|	|	|
0+50	0.0058	0.12	Q	|	|	|	|
0+55	0.0067	0.14	Q	|	|	|	|
1+ 0	0.0077	0.14	Q	|	|	|	|
1+ 5	0.0087	0.14	Q	|	|	|	|
1+10	0.0095	0.12	Q	|	|	|	|
1+15	0.0104	0.12	Q	|	|	|	|
1+20	0.0112	0.12	Q	|	|	|	|

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1+25       0.0119      0.11  Q          |          |          |          |
1+30       0.0127      0.11  Q          |          |          |          |
1+35       0.0135      0.11  Q          |          |          |          |
1+40       0.0143      0.11  Q          |          |          |          |
1+45       0.0151      0.11  Q          |          |          |          |
1+50       0.0159      0.12  Q          |          |          |          |
1+55       0.0168      0.14  Q          |          |          |          |
2+ 0       0.0178      0.14  Q          |          |          |          |
2+ 5       0.0188      0.15  Q          |          |          |          |
2+10       0.0198      0.15  QV         |          |          |          |
2+15       0.0209      0.15  QV         |          |          |          |
2+20       0.0219      0.15  QV         |          |          |          |
2+25       0.0229      0.15  QV         |          |          |          |
2+30       0.0240      0.15  QV         |          |          |          |
2+35       0.0251      0.16  QV         |          |          |          |
2+40       0.0263      0.17  QV         |          |          |          |
2+45       0.0275      0.18  QV         |          |          |          |
2+50       0.0288      0.18  QV         |          |          |          |
2+55       0.0301      0.19  QV         |          |          |          |
3+ 0       0.0313      0.19  QV         |          |          |          |
3+ 5       0.0326      0.19  QV         |          |          |          |
3+10       0.0339      0.19  QV         |          |          |          |
3+15       0.0352      0.19  QV         |          |          |          |
3+20       0.0365      0.19  QV         |          |          |          |
3+25       0.0378      0.19  QV         |          |          |          |
3+30       0.0391      0.19  QV         |          |          |          |
3+35       0.0404      0.19  Q V        |          |          |          |
3+40       0.0417      0.19  Q V        |          |          |          |
3+45       0.0430      0.19  Q V        |          |          |          |
3+50       0.0443      0.19  Q V        |          |          |          |
3+55       0.0458      0.21  Q V        |          |          |          |
4+ 0       0.0473      0.22  Q V        |          |          |          |
4+ 5       0.0488      0.22  Q V        |          |          |          |
4+10       0.0504      0.22  Q V        |          |          |          |
4+15       0.0519      0.22  Q V        |          |          |          |
4+20       0.0535      0.23  Q V        |          |          |          |
4+25       0.0552      0.25  Q V        |          |          |          |
4+30       0.0570      0.26  |QV        |          |          |          |
4+35       0.0588      0.26  |QV        |          |          |          |
4+40       0.0606      0.26  |Q V       |          |          |          |
4+45       0.0624      0.26  |Q V       |          |          |          |
4+50       0.0642      0.27  |Q V       |          |          |          |
4+55       0.0662      0.29  |Q V       |          |          |          |
5+ 0       0.0682      0.29  |Q V       |          |          |          |
5+ 5       0.0702      0.28  |Q V       |          |          |          |
5+10       0.0719      0.25  Q  V       |          |          |          |
5+15       0.0735      0.24  Q  V       |          |          |          |
5+20       0.0752      0.24  Q  V       |          |          |          |
5+25       0.0769      0.25  |Q V       |          |          |          |
5+30       0.0787      0.26  |Q V       |          |          |          |
5+35       0.0806      0.27  |Q  V      |          |          |          |
5+40       0.0825      0.29  |Q  V      |          |          |          |
5+45       0.0845      0.29  |Q  V      |          |          |          |
5+50       0.0866      0.30  |Q  V      |          |          |          |
5+55       0.0886      0.30  |Q  V      |          |          |          |
6+ 0       0.0907      0.30  |Q  V      |          |          |          |
6+ 5       0.0928      0.31  |Q  V      |          |          |          |
6+10       0.0950      0.32  |Q  V      |          |          |          |
6+15       0.0973      0.33  |Q  V      |          |          |          |
6+20       0.0996      0.33  |Q   V     |          |          |          |
6+25       0.1019      0.34  |Q   V     |          |          |          |
6+30       0.1043      0.34  |Q   V     |          |          |          |
6+35       0.1066      0.34  |Q   V     |          |          |          |
6+40       0.1091      0.36  |Q   V     |          |          |          |
6+45       0.1117      0.37  |Q   V     |          |          |          |
6+50       0.1142      0.37  |Q   V     |          |          |          |
6+55       0.1168      0.37  |Q   V     |          |          |          |
7+ 0       0.1194      0.37  |Q    V    |          |          |          |
7+ 5       0.1220      0.38  |Q    V    |          |          |          |
7+10       0.1246      0.38  |Q    V    |          |          |          |
7+15       0.1271      0.38  |Q    V    |          |          |          |
7+20       0.1298      0.38  |Q    V    |          |          |          |
7+25       0.1325      0.40  |Q    V    |          |          |          |
7+30       0.1353      0.41  |Q    V    |          |          |          |
7+35       0.1382      0.42  |Q    V    |          |          |          |
7+40       0.1412      0.44  |Q     V   |          |          |          |
7+45       0.1442      0.44  |Q     V   |          |          |          |
7+50       0.1474      0.45  |Q     V   |          |          |          |
7+55       0.1506      0.47  |Q     V   |          |          |          |
8+ 0       0.1539      0.48  |Q     V   |          |          |          |
8+ 5       0.1574      0.50  |Q     V   |          |          |          |
8+10       0.1610      0.53  | Q     V  |          |          |          |
8+15       0.1648      0.55  | Q     V  |          |          |          |
8+20       0.1686      0.56  | Q     V  |          |          |          |
8+25       0.1725      0.56  | Q     V  |          |          |          |
8+30       0.1764      0.56  | Q     V  |          |          |          |
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8+35	0.1803	0.57	Q V
8+40	0.1843	0.59	Q V
8+45	0.1884	0.59	Q V
8+50	0.1926	0.60	Q V
8+55	0.1969	0.62	Q V
9+ 0	0.2012	0.63	Q V
9+ 5	0.2057	0.65	Q V
9+10	0.2104	0.69	Q V
9+15	0.2152	0.70	Q V
9+20	0.2201	0.71	Q V
9+25	0.2252	0.73	Q V
9+30	0.2303	0.74	Q V
9+35	0.2355	0.75	Q V
9+40	0.2408	0.77	Q V
9+45	0.2462	0.78	Q V
9+50	0.2516	0.79	Q V
9+55	0.2572	0.81	Q V
10+ 0	0.2628	0.82	Q V
10+ 5	0.2682	0.78	Q V
10+10	0.2727	0.65	Q V
10+15	0.2769	0.61	Q V
10+20	0.2810	0.59	Q V
10+25	0.2850	0.58	Q V
10+30	0.2889	0.57	Q V
10+35	0.2931	0.60	Q V
10+40	0.2978	0.69	Q V
10+45	0.3028	0.72	Q V
10+50	0.3078	0.73	Q V
10+55	0.3129	0.74	Q V
11+ 0	0.3180	0.74	Q V
11+ 5	0.3231	0.74	Q V
11+10	0.3281	0.73	Q V
11+15	0.3331	0.72	Q V
11+20	0.3381	0.72	Q V
11+25	0.3430	0.72	Q V
11+30	0.3479	0.72	Q V
11+35	0.3528	0.70	Q V
11+40	0.3573	0.67	Q V
11+45	0.3618	0.65	Q V
11+50	0.3663	0.65	Q V
11+55	0.3709	0.67	Q V
12+ 0	0.3756	0.67	Q V
12+ 5	0.3805	0.72	Q V
12+10	0.3864	0.85	Q V
12+15	0.3925	0.89	Q V
12+20	0.3988	0.92	Q V
12+25	0.4053	0.95	Q V
12+30	0.4120	0.96	Q V
12+35	0.4187	0.98	Q V
12+40	0.4257	1.02	Q V
12+45	0.4329	1.04	Q V
12+50	0.4401	1.05	Q V
12+55	0.4475	1.07	Q V
13+ 0	0.4549	1.08	Q V
13+ 5	0.4629	1.15	Q V
13+10	0.4722	1.35	Q V
13+15	0.4822	1.45	Q V
13+20	0.4927	1.53	Q V
13+25	0.5037	1.60	Q V
13+30	0.5152	1.66	Q V
13+35	0.5259	1.56	Q V
13+40	0.5338	1.15	Q V
13+45	0.5408	1.02	Q V
13+50	0.5474	0.96	Q V
13+55	0.5537	0.92	Q V
14+ 0	0.5599	0.90	Q V
14+ 5	0.5662	0.91	Q V
14+10	0.5729	0.97	Q V
14+15	0.5797	0.99	Q V
14+20	0.5865	0.99	Q V
14+25	0.5933	0.98	Q V
14+30	0.6000	0.98	Q V
14+35	0.6068	0.98	Q V
14+40	0.6135	0.98	Q V
14+45	0.6202	0.98	Q V
14+50	0.6269	0.97	Q V
14+55	0.6335	0.95	Q V
15+ 0	0.6400	0.95	Q V
15+ 5	0.6465	0.94	Q V
15+10	0.6528	0.92	Q V
15+15	0.6591	0.91	Q V
15+20	0.6653	0.90	Q V
15+25	0.6714	0.88	Q V
15+30	0.6774	0.87	Q V
15+35	0.6832	0.84	Q V
15+40	0.6885	0.77	Q V

```
15+45       0.6936      0.74  | Q       |         |         |    V    |
15+50       0.6986      0.73  | Q       |         |         |    V    |
15+55       0.7036      0.72  | Q       |         |         |    V    |
16+ 0       0.7086      0.72  | Q       |         |         |    V    |
16+ 5       0.7129      0.62  | Q       |         |         |     V   |
16+10       0.7153      0.35  |Q        |         |         |     V   |
16+15       0.7170      0.25  |Q        |         |         |     V   |
16+20       0.7185      0.21  Q         |         |         |     V   |
16+25       0.7198      0.19  Q         |         |         |     V   |
16+30       0.7210      0.17  Q         |         |         |     V   |
16+35       0.7220      0.16  Q         |         |         |     V   |
16+40       0.7229      0.13  Q         |         |         |     V   |
16+45       0.7238      0.12  Q         |         |         |     V   |
16+50       0.7246      0.12  Q         |         |         |     V   |
16+55       0.7254      0.12  Q         |         |         |     V   |
17+ 0       0.7261      0.11  Q         |         |         |     V   |
17+ 5       0.7270      0.13  Q         |         |         |     V   |
17+10       0.7281      0.16  Q         |         |         |     V   |
17+15       0.7293      0.17  Q         |         |         |     V   |
17+20       0.7306      0.18  Q         |         |         |     V   |
17+25       0.7318      0.18  Q         |         |         |      V  |
17+30       0.7331      0.19  Q         |         |         |      V  |
17+35       0.7344      0.19  Q         |         |         |      V  |
17+40       0.7357      0.19  Q         |         |         |      V  |
17+45       0.7370      0.19  Q         |         |         |      V  |
17+50       0.7382      0.18  Q         |         |         |      V  |
17+55       0.7394      0.16  Q         |         |         |      V  |
18+ 0       0.7404      0.16  Q         |         |         |      V  |
18+ 5       0.7415      0.15  Q         |         |         |      V  |
18+10       0.7426      0.15  Q         |         |         |      V  |
18+15       0.7436      0.15  Q         |         |         |      V  |
18+20       0.7446      0.15  Q         |         |         |      V  |
18+25       0.7457      0.15  Q         |         |         |      V  |
18+30       0.7467      0.15  Q         |         |         |      V  |
18+35       0.7477      0.14  Q         |         |         |      V  |
18+40       0.7486      0.13  Q         |         |         |      V  |
18+45       0.7494      0.12  Q         |         |         |      V  |
18+50       0.7502      0.11  Q         |         |         |      V  |
18+55       0.7508      0.09  Q         |         |         |      V  |
19+ 0       0.7514      0.08  Q         |         |         |      V  |
19+ 5       0.7520      0.09  Q         |         |         |       V |
19+10       0.7527      0.10  Q         |         |         |       V |
19+15       0.7534      0.11  Q         |         |         |       V |
19+20       0.7542      0.12  Q         |         |         |       V |
19+25       0.7551      0.14  Q         |         |         |       V |
19+30       0.7561      0.14  Q         |         |         |       V |
19+35       0.7571      0.14  Q         |         |         |       V |
19+40       0.7579      0.12  Q         |         |         |       V |
19+45       0.7587      0.12  Q         |         |         |       V |
19+50       0.7595      0.11  Q         |         |         |       V |
19+55       0.7601      0.09  Q         |         |         |       V |
20+ 0       0.7607      0.08  Q         |         |         |       V |
20+ 5       0.7613      0.09  Q         |         |         |       V |
20+10       0.7620      0.10  Q         |         |         |       V |
20+15       0.7627      0.11  Q         |         |         |       V |
20+20       0.7635      0.11  Q         |         |         |       V |
20+25       0.7642      0.11  Q         |         |         |       V |
20+30       0.7650      0.11  Q         |         |         |       V |
20+35       0.7658      0.11  Q         |         |         |       V |
20+40       0.7666      0.11  Q         |         |         |       V |
20+45       0.7673      0.11  Q         |         |         |       V |
20+50       0.7681      0.11  Q         |         |         |       V |
20+55       0.7687      0.09  Q         |         |         |       V |
21+ 0       0.7692      0.08  Q         |         |         |       V |
21+ 5       0.7698      0.09  Q         |         |         |       V |
21+10       0.7705      0.10  Q         |         |         |       V |
21+15       0.7713      0.11  Q         |         |         |       V |
21+20       0.7720      0.10  Q         |         |         |        V|
21+25       0.7726      0.09  Q         |         |         |        V|
21+30       0.7731      0.08  Q         |         |         |        V|
21+35       0.7737      0.09  Q         |         |         |        V|
21+40       0.7744      0.10  Q         |         |         |        V|
21+45       0.7752      0.11  Q         |         |         |        V|
21+50       0.7759      0.10  Q         |         |         |        V|
21+55       0.7765      0.09  Q         |         |         |        V|
22+ 0       0.7770      0.08  Q         |         |         |        V|
22+ 5       0.7776      0.09  Q         |         |         |        V|
22+10       0.7783      0.10  Q         |         |         |        V|
22+15       0.7790      0.11  Q         |         |         |        V|
22+20       0.7797      0.10  Q         |         |         |        V|
22+25       0.7803      0.09  Q         |         |         |        V|
22+30       0.7809      0.08  Q         |         |         |        V|
22+35       0.7814      0.08  Q         |         |         |        V|
22+40       0.7820      0.08  Q         |         |         |        V|
22+45       0.7825      0.08  Q         |         |         |        V|
22+50       0.7830      0.08  Q         |         |         |        V|
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   22+55       0.7835      0.08  Q          |          |          |          V|
   23+ 0       0.7841      0.08  Q          |          |          |          V|
   23+ 5       0.7846      0.08  Q          |          |          |          V|
   23+10       0.7851      0.08  Q          |          |          |          V|
   23+15       0.7856      0.08  Q          |          |          |          V|
   23+20       0.7861      0.08  Q          |          |          |          V|
   23+25       0.7867      0.08  Q          |          |          |          V|
   23+30       0.7872      0.08  Q          |          |          |          V|
   23+35       0.7877      0.08  Q          |          |          |          V|
   23+40       0.7882      0.08  Q          |          |          |          V|
   23+45       0.7887      0.08  Q          |          |          |          V|
   23+50       0.7892      0.08  Q          |          |          |          V|
   23+55       0.7898      0.08  Q          |          |          |          V|
   24+ 0       0.7903      0.08  Q          |          |          |          V|
   24+ 5       0.7907      0.06  Q          |          |          |          V|
   24+10       0.7909      0.03  Q          |          |          |          V|
   24+15       0.7910      0.01  Q          |          |          |          V|
   24+20       0.7910      0.01  Q          |          |          |          V|
   24+25       0.7911      0.01  Q          |          |          |          V|
   24+30       0.7911      0.00  Q          |          |          |          V|
   24+35       0.7911      0.00  Q          |          |          |          V|
   24+40       0.7911      0.00  Q          |          |          |          V|
-------------------------------------------------------------------------------
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```
       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/22/24 File: EX2515.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2127.00(Ft.)
Length along longest watercourse measured to centroid =    1064.00(Ft.)
Length along longest watercourse =      0.403 Mi.
Length along longest watercourse measured to centroid =      0.202 Mi.
Difference in elevation =     160.00(Ft.)
Slope along watercourse =    397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.089 Hr.
Lag time =     5.34 Min.
25% of lag time =     1.33 Min.
40% of lag time =     2.13 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           0.50                 25.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           1.30                 67.34

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.687(In)
Areal adjustment factor =   99.95 %
Adjusted average point rain =    0.687(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           91.00         0.000
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.272	(0.246)	0.245	0.027
2	0.17	4.20	0.346	0.246	(0.312)	0.100
3	0.25	4.40	0.363	0.246	(0.326)	0.116
4	0.33	4.80	0.396	0.246	(0.356)	0.149
5	0.42	5.20	0.429	0.246	(0.386)	0.182
6	0.50	6.20	0.511	0.246	(0.460)	0.265
7	0.58	6.80	0.561	0.246	(0.505)	0.314
8	0.67	8.80	0.726	0.246	(0.653)	0.479
9	0.75	13.90	1.146	0.246	(1.031)	0.900
10	0.83	31.40	2.589	0.246	(2.330)	2.342
11	0.92	7.20	0.594	0.246	(0.534)	0.347
12	1.00	3.80	0.313	0.246	(0.282)	0.067
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.3

Flood volume = Effective rainfall 0.44(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 1.9(Ac.Ft)
Total soil loss = 0.25(In)
Total soil loss = 1.063(Ac.Ft)
Total rainfall = 0.69(In)
Flood volume = 82889.4 Cubic Feet
Total soil loss = 46300.7 Cubic Feet

Peak flow rate of this hydrograph = 72.605(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	20.0	40.0	60.0	80.0
0+ 5	0.0017	0.25	Q				
0+10	0.0126	1.58	Q				
0+15	0.0386	3.78	VQ				
0+20	0.0746	5.23	VQ				
0+25	0.1216	6.83	VQ				
0+30	0.1833	8.95	VQ				
0+35	0.2661	12.03	VQ				
0+40	0.3748	15.78	Q				
0+45	0.5444	24.63	VQ				
0+50	0.8892	50.07	V	Q			
0+55	1.3893	72.61	V		Q		
1+ 0	1.6311	35.11	Q		V		
1+ 5	1.7481	17.00	Q		V		
1+10	1.8114	9.19	Q		V		
1+15	1.8505	5.68	Q		V		
1+20	1.8755	3.63	Q		V		
1+25	1.8911	2.27	Q		V		
1+30	1.9012	1.46	Q		V		
1+35	1.9026	0.22	Q		V		
1+40	1.9029	0.03	Q		V		

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX2535.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2127.00(Ft.)
Length along longest watercourse measured to centroid = 1064.00(Ft.)
Length along longest watercourse = 0.403 Mi.
Length along longest watercourse measured to centroid = 0.202 Mi.
Difference in elevation = 160.00(Ft.)
Slope along watercourse = 397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.089 Hr.
Lag time = 5.34 Min.
25% of lag time = 1.33 Min.
40% of lag time = 2.13 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	0.80	41.44

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	2.00	103.60

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 1.081(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 1.081(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	91.00	0.000

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.169	(0.246)	0.152	0.017
2	0.17	1.30	0.169	(0.246)	0.152	0.017
3	0.25	1.10	0.143	(0.246)	0.128	0.014
4	0.33	1.50	0.195	(0.246)	0.175	0.019
5	0.42	1.50	0.195	(0.246)	0.175	0.019
6	0.50	1.80	0.233	(0.246)	0.210	0.023
7	0.58	1.50	0.195	(0.246)	0.175	0.019
8	0.67	1.80	0.233	(0.246)	0.210	0.023
9	0.75	1.80	0.233	(0.246)	0.210	0.023
10	0.83	1.50	0.195	(0.246)	0.175	0.019
11	0.92	1.60	0.208	(0.246)	0.187	0.021
12	1.00	1.80	0.233	(0.246)	0.210	0.023
13	1.08	2.20	0.285	0.246	(0.257)	0.039
14	1.17	2.20	0.285	0.246	(0.257)	0.039
15	1.25	2.20	0.285	0.246	(0.257)	0.039
16	1.33	2.00	0.259	(0.246)	0.233	0.026
17	1.42	2.60	0.337	0.246	(0.303)	0.091
18	1.50	2.70	0.350	0.246	(0.315)	0.104
19	1.58	2.40	0.311	0.246	(0.280)	0.065
20	1.67	2.70	0.350	0.246	(0.315)	0.104
21	1.75	3.30	0.428	0.246	(0.385)	0.182
22	1.83	3.10	0.402	0.246	(0.362)	0.156
23	1.92	2.90	0.376	0.246	(0.339)	0.130
24	2.00	3.00	0.389	0.246	(0.350)	0.143
25	2.08	3.10	0.402	0.246	(0.362)	0.156
26	2.17	4.20	0.545	0.246	(0.490)	0.298
27	2.25	5.00	0.648	0.246	(0.584)	0.402
28	2.33	3.50	0.454	0.246	(0.409)	0.208
29	2.42	6.80	0.882	0.246	(0.794)	0.636
30	2.50	7.30	0.947	0.246	(0.852)	0.700
31	2.58	8.20	1.064	0.246	(0.957)	0.817
32	2.67	5.90	0.765	0.246	(0.689)	0.519
33	2.75	2.00	0.259	(0.246)	0.233	0.026
34	2.83	1.80	0.233	(0.246)	0.210	0.023
35	2.92	1.80	0.233	(0.246)	0.210	0.023
36	3.00	0.60	0.078	(0.246)	0.070	0.008
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.2

Flood volume = Effective rainfall 0.43(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 1.9(Ac.Ft)
Total soil loss = 0.65(In)
Total soil loss = 2.805(Ac.Ft)
Total rainfall = 1.08(In)
Flood volume = 81048.7 Cubic Feet
Total soil loss = 122183.0 Cubic Feet

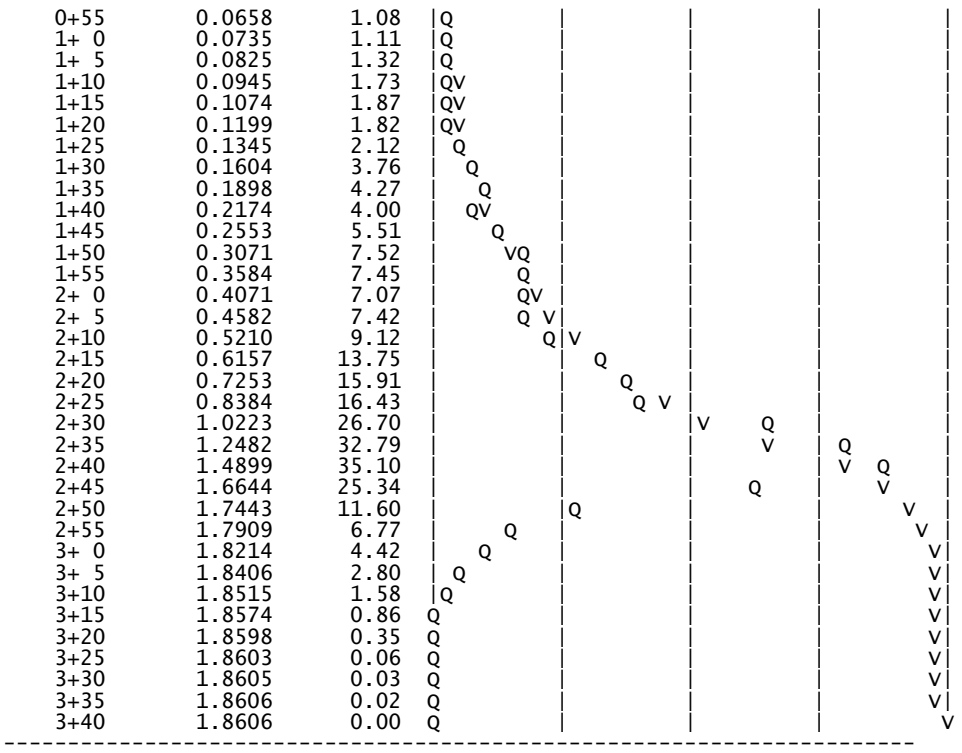
Peak flow rate of this hydrograph = 35.099(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	10.0	20.0	30.0	40.0
0+ 5	0.0010	0.15	Q	|	|	|	|
0+10	0.0050	0.57	Q	|	|	|	|
0+15	0.0098	0.70	Q	|	|	|	|
0+20	0.0149	0.74	Q	|	|	|	|
0+25	0.0210	0.89	Q	|	|	|	|
0+30	0.0278	0.98	Q	|	|	|	|
0+35	0.0352	1.07	VQ	|	|	|	|
0+40	0.0425	1.06	VQ	|	|	|	|
0+45	0.0505	1.16	|Q	|	|	|	|
0+50	0.0584	1.15	|Q	|	|	|	|



0+55	0.0658	1.08	
1+ 0	0.0735	1.11	
1+ 5	0.0825	1.32	
1+10	0.0945	1.73	
1+15	0.1074	1.87	
1+20	0.1199	1.82	
1+25	0.1345	2.12	
1+30	0.1604	3.76	
1+35	0.1898	4.27	
1+40	0.2174	4.00	
1+45	0.2553	5.51	
1+50	0.3071	7.52	
1+55	0.3584	7.45	
2+ 0	0.4071	7.07	
2+ 5	0.4582	7.42	
2+10	0.5210	9.12	
2+15	0.6157	13.75	
2+20	0.7253	15.91	
2+25	0.8384	16.43	
2+30	1.0223	26.70	
2+35	1.2482	32.79	
2+40	1.4899	35.10	
2+45	1.6644	25.34	
2+50	1.7443	11.60	
2+55	1.7909	6.77	
3+ 0	1.8214	4.42	
3+ 5	1.8406	2.80	
3+10	1.8515	1.58	
3+15	1.8574	0.86	
3+20	1.8598	0.35	
3+25	1.8603	0.06	
3+30	1.8605	0.03	
3+35	1.8606	0.02	
3+40	1.8606	0.00	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX2565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2127.00(Ft.)
Length along longest watercourse measured to centroid = 1064.00(Ft.)
Length along longest watercourse = 0.403 Mi.
Length along longest watercourse measured to centroid = 0.202 Mi.
Difference in elevation = 160.00(Ft.)
Slope along watercourse = 397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.089 Hr.
Lag time = 5.34 Min.
25% of lag time = 1.33 Min.
40% of lag time = 2.13 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	1.10	56.98

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	3.00	155.40

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.545(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 1.545(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	91.00	0.000

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

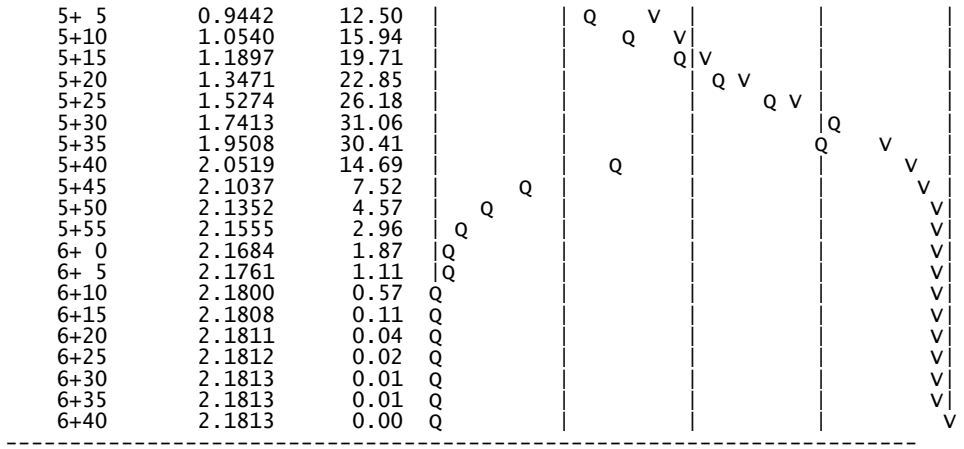
1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.093	(0.246)	0.083	0.009
2	0.17	0.60	0.111	(0.246)	0.100	0.011
3	0.25	0.60	0.111	(0.246)	0.100	0.011
4	0.33	0.60	0.111	(0.246)	0.100	0.011
5	0.42	0.60	0.111	(0.246)	0.100	0.011
6	0.50	0.70	0.130	(0.246)	0.117	0.013
7	0.58	0.70	0.130	(0.246)	0.117	0.013
8	0.67	0.70	0.130	(0.246)	0.117	0.013
9	0.75	0.70	0.130	(0.246)	0.117	0.013
10	0.83	0.70	0.130	(0.246)	0.117	0.013
11	0.92	0.70	0.130	(0.246)	0.117	0.013
12	1.00	0.80	0.148	(0.246)	0.133	0.015
13	1.08	0.80	0.148	(0.246)	0.133	0.015
14	1.17	0.80	0.148	(0.246)	0.133	0.015
15	1.25	0.80	0.148	(0.246)	0.133	0.015
16	1.33	0.80	0.148	(0.246)	0.133	0.015
17	1.42	0.80	0.148	(0.246)	0.133	0.015
18	1.50	0.80	0.148	(0.246)	0.133	0.015
19	1.58	0.80	0.148	(0.246)	0.133	0.015
20	1.67	0.80	0.148	(0.246)	0.133	0.015
21	1.75	0.80	0.148	(0.246)	0.133	0.015
22	1.83	0.80	0.148	(0.246)	0.133	0.015
23	1.92	0.80	0.148	(0.246)	0.133	0.015
24	2.00	0.90	0.167	(0.246)	0.150	0.017
25	2.08	0.80	0.148	(0.246)	0.133	0.015
26	2.17	0.90	0.167	(0.246)	0.150	0.017
27	2.25	0.90	0.167	(0.246)	0.150	0.017
28	2.33	0.90	0.167	(0.246)	0.150	0.017
29	2.42	0.90	0.167	(0.246)	0.150	0.017
30	2.50	0.90	0.167	(0.246)	0.150	0.017
31	2.58	0.90	0.167	(0.246)	0.150	0.017
32	2.67	0.90	0.167	(0.246)	0.150	0.017
33	2.75	1.00	0.185	(0.246)	0.167	0.019
34	2.83	1.00	0.185	(0.246)	0.167	0.019
35	2.92	1.00	0.185	(0.246)	0.167	0.019
36	3.00	1.00	0.185	(0.246)	0.167	0.019
37	3.08	1.00	0.185	(0.246)	0.167	0.019
38	3.17	1.10	0.204	(0.246)	0.184	0.020
39	3.25	1.10	0.204	(0.246)	0.184	0.020
40	3.33	1.10	0.204	(0.246)	0.184	0.020
41	3.42	1.20	0.222	(0.246)	0.200	0.022
42	3.50	1.30	0.241	(0.246)	0.217	0.024
43	3.58	1.40	0.260	(0.246)	0.234	0.026
44	3.67	1.40	0.260	(0.246)	0.234	0.026
45	3.75	1.50	0.278	0.246	(0.250)	0.032
46	3.83	1.50	0.278	0.246	(0.250)	0.032
47	3.92	1.60	0.297	0.246	(0.267)	0.050
48	4.00	1.60	0.297	0.246	(0.267)	0.050
49	4.08	1.70	0.315	0.246	(0.284)	0.069
50	4.17	1.80	0.334	0.246	(0.300)	0.087
51	4.25	1.90	0.352	0.246	(0.317)	0.106
52	4.33	2.00	0.371	0.246	(0.334)	0.124
53	4.42	2.10	0.389	0.246	(0.350)	0.143
54	4.50	2.10	0.389	0.246	(0.350)	0.143
55	4.58	2.20	0.408	0.246	(0.367)	0.161
56	4.67	2.30	0.426	0.246	(0.384)	0.180
57	4.75	2.40	0.445	0.246	(0.400)	0.199
58	4.83	2.40	0.445	0.246	(0.400)	0.199
59	4.92	2.50	0.463	0.246	(0.417)	0.217
60	5.00	2.60	0.482	0.246	(0.434)	0.236
61	5.08	3.10	0.575	0.246	(0.517)	0.328
62	5.17	3.60	0.667	0.246	(0.601)	0.421
63	5.25	3.90	0.723	0.246	(0.651)	0.477
64	5.33	4.20	0.779	0.246	(0.701)	0.532
65	5.42	4.70	0.871	0.246	(0.784)	0.625
66	5.50	5.60	1.038	0.246	(0.934)	0.792
67	5.58	1.90	0.352	0.246	(0.317)	0.106

```
68   5.67     0.90      0.167       (  0.246)       0.150        0.017
69   5.75     0.60      0.111       (  0.246)       0.100        0.011
70   5.83     0.50      0.093       (  0.246)       0.083        0.009
71   5.92     0.30      0.056       (  0.246)       0.050        0.006
72   6.00     0.20      0.037       (  0.246)       0.033        0.004
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =     6.1
      Flood volume = Effective rainfall      0.51(In)
       times area      51.8(Ac.)/[(In)/(Ft.)] =       2.2(Ac.Ft)
      Total soil loss =      1.04(In)
      Total soil loss =     4.487(Ac.Ft)
      Total rainfall =      1.54(In)
      Flood volume =       95018.9 Cubic Feet
      Total soil loss =      195446.8 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     31.060(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0       10.0      20.0      30.0      40.0
-------------------------------------------------------------------------
  0+ 5       0.0006      0.08  Q         |         |         |         |
  0+10       0.0029      0.33  Q         |         |         |         |
  0+15       0.0060      0.46  Q         |         |         |         |
  0+20       0.0095      0.51  Q         |         |         |         |
  0+25       0.0132      0.54  Q         |         |         |         |
  0+30       0.0172      0.57  Q         |         |         |         |
  0+35       0.0215      0.63  Q         |         |         |         |
  0+40       0.0260      0.65  Q         |         |         |         |
  0+45       0.0306      0.67  Q         |         |         |         |
  0+50       0.0352      0.67  Q         |         |         |         |
  0+55       0.0399      0.67  Q         |         |         |         |
  1+ 0       0.0446      0.69  Q         |         |         |         |
  1+ 5       0.0497      0.74  Q         |         |         |         |
  1+10       0.0549      0.76  QV        |         |         |         |
  1+15       0.0602      0.76  QV        |         |         |         |
  1+20       0.0655      0.77  QV        |         |         |         |
  1+25       0.0708      0.77  QV        |         |         |         |
  1+30       0.0761      0.77  QV        |         |         |         |
  1+35       0.0815      0.77  QV        |         |         |         |
  1+40       0.0868      0.77  QV        |         |         |         |
  1+45       0.0921      0.77  QV        |         |         |         |
  1+50       0.0975      0.77  QV        |         |         |         |
  1+55       0.1028      0.77  QV        |         |         |         |
  2+ 0       0.1082      0.79  QV        |         |         |         |
  2+ 5       0.1139      0.82  Q V       |         |         |         |
  2+10       0.1195      0.81  Q V       |         |         |         |
  2+15       0.1253      0.84  Q V       |         |         |         |
  2+20       0.1312      0.86  Q V       |         |         |         |
  2+25       0.1371      0.86  Q V       |         |         |         |
  2+30       0.1431      0.87  Q V       |         |         |         |
  2+35       0.1491      0.87  Q V       |         |         |         |
  2+40       0.1551      0.87  Q V       |         |         |         |
  2+45       0.1612      0.89  Q V       |         |         |         |
  2+50       0.1676      0.93  Q  V       |         |         |         |
  2+55       0.1742      0.95  Q  V       |         |         |         |
  3+ 0       0.1808      0.96  Q  V       |         |         |         |
  3+ 5       0.1874      0.96  Q  V       |         |         |         |
  3+10       0.1941      0.98  Q  V       |         |         |         |
  3+15       0.2012      1.03  |Q V       |         |         |         |
  3+20       0.2084      1.05  |Q V       |         |         |         |
  3+25       0.2158      1.07  |Q V       |         |         |         |
  3+30       0.2237      1.14  |Q  V      |         |         |         |
  3+35       0.2321      1.22  |Q  V      |         |         |         |
  3+40       0.2409      1.29  |Q  V      |         |         |         |
  3+45       0.2504      1.37  |Q  V      |         |         |         |
  3+50       0.2609      1.53  |Q  V      |         |         |         |
  3+55       0.2730      1.76  |Q   V     |         |         |         |
  4+ 0       0.2885      2.25  | Q  V     |         |         |         |
  4+ 5       0.3063      2.59  | Q  V     |         |         |         |
  4+10       0.3291      3.30  |  Q  V    |         |         |         |
  4+15       0.3576      4.14  |   Q V    |         |         |         |
  4+20       0.3922      5.03  |    Q V   |         |         |         |
  4+25       0.4333      5.96  |    Q V   |         |         |         |
  4+30       0.4796      6.73  |     Q V  |         |         |         |
  4+35       0.5294      7.23  |      Q V|         |         |         |
  4+40       0.5847      8.02  |       Q V         |         |         |
  4+45       0.6461      8.92  |       Q |V        |         |         |
  4+50       0.7128      9.68  |         Q|  V      |         |         |
  4+55       0.7827     10.16  |          Q   V     |         |         |
  5+ 0       0.8581     10.95  |          Q    V    |         |         |
```


5+ 5 0.9442 12.50
5+10 1.0540 15.94
5+15 1.1897 19.71
5+20 1.3471 22.85
5+25 1.5274 26.18
5+30 1.7413 31.06
5+35 1.9508 30.41
5+40 2.0519 14.69
5+45 2.1037 7.52
5+50 2.1352 4.57
5+55 2.1555 2.96
6+ 0 2.1684 1.87
6+ 5 2.1761 1.11
6+10 2.1800 0.57
6+15 2.1808 0.11
6+20 2.1811 0.04
6+25 2.1812 0.02
6+30 2.1813 0.01
6+35 2.1813 0.01
6+40 2.1813 0.00

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX25245.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2127.00(Ft.)
Length along longest watercourse measured to centroid = 1064.00(Ft.)
Length along longest watercourse = 0.403 Mi.
Length along longest watercourse measured to centroid = 0.202 Mi.
Difference in elevation = 160.00(Ft.)
Slope along watercourse = 397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.089 Hr.
Lag time = 5.34 Min.
25% of lag time = 1.33 Min.
40% of lag time = 2.13 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	1.80	93.24

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	5.00	259.00

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 2.550(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 2.549(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	91.00	0.000

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.020	(0.437)	0.018	0.002
2	0.17	0.07	0.020	(0.435)	0.018	0.002
3	0.25	0.07	0.020	(0.433)	0.018	0.002
4	0.33	0.10	0.031	(0.432)	0.028	0.003
5	0.42	0.10	0.031	(0.430)	0.028	0.003
6	0.50	0.10	0.031	(0.428)	0.028	0.003
7	0.58	0.10	0.031	(0.427)	0.028	0.003
8	0.67	0.10	0.031	(0.425)	0.028	0.003
9	0.75	0.10	0.031	(0.423)	0.028	0.003
10	0.83	0.13	0.041	(0.422)	0.037	0.004
11	0.92	0.13	0.041	(0.420)	0.037	0.004
12	1.00	0.13	0.041	(0.418)	0.037	0.004
13	1.08	0.10	0.031	(0.417)	0.028	0.003
14	1.17	0.10	0.031	(0.415)	0.028	0.003
15	1.25	0.10	0.031	(0.413)	0.028	0.003
16	1.33	0.10	0.031	(0.412)	0.028	0.003
17	1.42	0.10	0.031	(0.410)	0.028	0.003
18	1.50	0.10	0.031	(0.408)	0.028	0.003
19	1.58	0.10	0.031	(0.407)	0.028	0.003
20	1.67	0.10	0.031	(0.405)	0.028	0.003
21	1.75	0.10	0.031	(0.404)	0.028	0.003
22	1.83	0.13	0.041	(0.402)	0.037	0.004
23	1.92	0.13	0.041	(0.400)	0.037	0.004
24	2.00	0.13	0.041	(0.399)	0.037	0.004
25	2.08	0.13	0.041	(0.397)	0.037	0.004
26	2.17	0.13	0.041	(0.395)	0.037	0.004
27	2.25	0.13	0.041	(0.394)	0.037	0.004
28	2.33	0.13	0.041	(0.392)	0.037	0.004
29	2.42	0.13	0.041	(0.391)	0.037	0.004
30	2.50	0.13	0.041	(0.389)	0.037	0.004
31	2.58	0.17	0.051	(0.387)	0.046	0.005
32	2.67	0.17	0.051	(0.386)	0.046	0.005
33	2.75	0.17	0.051	(0.384)	0.046	0.005
34	2.83	0.17	0.051	(0.383)	0.046	0.005
35	2.92	0.17	0.051	(0.381)	0.046	0.005
36	3.00	0.17	0.051	(0.380)	0.046	0.005
37	3.08	0.17	0.051	(0.378)	0.046	0.005
38	3.17	0.17	0.051	(0.376)	0.046	0.005
39	3.25	0.17	0.051	(0.375)	0.046	0.005
40	3.33	0.17	0.051	(0.373)	0.046	0.005
41	3.42	0.17	0.051	(0.372)	0.046	0.005
42	3.50	0.17	0.051	(0.370)	0.046	0.005
43	3.58	0.17	0.051	(0.369)	0.046	0.005
44	3.67	0.17	0.051	(0.367)	0.046	0.005
45	3.75	0.17	0.051	(0.366)	0.046	0.005
46	3.83	0.20	0.061	(0.364)	0.055	0.006
47	3.92	0.20	0.061	(0.362)	0.055	0.006
48	4.00	0.20	0.061	(0.361)	0.055	0.006
49	4.08	0.20	0.061	(0.359)	0.055	0.006
50	4.17	0.20	0.061	(0.358)	0.055	0.006
51	4.25	0.20	0.061	(0.356)	0.055	0.006
52	4.33	0.23	0.071	(0.355)	0.064	0.007
53	4.42	0.23	0.071	(0.353)	0.064	0.007
54	4.50	0.23	0.071	(0.352)	0.064	0.007
55	4.58	0.23	0.071	(0.350)	0.064	0.007
56	4.67	0.23	0.071	(0.349)	0.064	0.007
57	4.75	0.23	0.071	(0.347)	0.064	0.007
58	4.83	0.27	0.082	(0.346)	0.073	0.008
59	4.92	0.27	0.082	(0.344)	0.073	0.008
60	5.00	0.27	0.082	(0.343)	0.073	0.008
61	5.08	0.20	0.061	(0.341)	0.055	0.006
62	5.17	0.20	0.061	(0.340)	0.055	0.006
63	5.25	0.20	0.061	(0.338)	0.055	0.006
64	5.33	0.23	0.071	(0.337)	0.064	0.007
65	5.42	0.23	0.071	(0.335)	0.064	0.007
66	5.50	0.23	0.071	(0.334)	0.064	0.007
67	5.58	0.27	0.082	(0.332)	0.073	0.008

68	5.67	0.27	0.082	(0.331)	0.073	0.008
69	5.75	0.27	0.082	(0.330)	0.073	0.008
70	5.83	0.27	0.082	(0.328)	0.073	0.008
71	5.92	0.27	0.082	(0.327)	0.073	0.008
72	6.00	0.27	0.082	(0.325)	0.073	0.008
73	6.08	0.30	0.092	(0.324)	0.083	0.009
74	6.17	0.30	0.092	(0.322)	0.083	0.009
75	6.25	0.30	0.092	(0.321)	0.083	0.009
76	6.33	0.30	0.092	(0.319)	0.083	0.009
77	6.42	0.30	0.092	(0.318)	0.083	0.009
78	6.50	0.30	0.092	(0.317)	0.083	0.009
79	6.58	0.33	0.102	(0.315)	0.092	0.010
80	6.67	0.33	0.102	(0.314)	0.092	0.010
81	6.75	0.33	0.102	(0.312)	0.092	0.010
82	6.83	0.33	0.102	(0.311)	0.092	0.010
83	6.92	0.33	0.102	(0.310)	0.092	0.010
84	7.00	0.33	0.102	(0.308)	0.092	0.010
85	7.08	0.33	0.102	(0.307)	0.092	0.010
86	7.17	0.33	0.102	(0.305)	0.092	0.010
87	7.25	0.33	0.102	(0.304)	0.092	0.010
88	7.33	0.37	0.112	(0.303)	0.101	0.011
89	7.42	0.37	0.112	(0.301)	0.101	0.011
90	7.50	0.37	0.112	(0.300)	0.101	0.011
91	7.58	0.40	0.122	(0.298)	0.110	0.012
92	7.67	0.40	0.122	(0.297)	0.110	0.012
93	7.75	0.40	0.122	(0.296)	0.110	0.012
94	7.83	0.43	0.133	(0.294)	0.119	0.013
95	7.92	0.43	0.133	(0.293)	0.119	0.013
96	8.00	0.43	0.133	(0.292)	0.119	0.013
97	8.08	0.50	0.153	(0.290)	0.138	0.015
98	8.17	0.50	0.153	(0.289)	0.138	0.015
99	8.25	0.50	0.153	(0.288)	0.138	0.015
100	8.33	0.50	0.153	(0.286)	0.138	0.015
101	8.42	0.50	0.153	(0.285)	0.138	0.015
102	8.50	0.50	0.153	(0.283)	0.138	0.015
103	8.58	0.53	0.163	(0.282)	0.147	0.016
104	8.67	0.53	0.163	(0.281)	0.147	0.016
105	8.75	0.53	0.163	(0.280)	0.147	0.016
106	8.83	0.57	0.173	(0.278)	0.156	0.017
107	8.92	0.57	0.173	(0.277)	0.156	0.017
108	9.00	0.57	0.173	(0.276)	0.156	0.017
109	9.08	0.63	0.194	(0.274)	0.174	0.019
110	9.17	0.63	0.194	(0.273)	0.174	0.019
111	9.25	0.63	0.194	(0.272)	0.174	0.019
112	9.33	0.67	0.204	(0.270)	0.184	0.020
113	9.42	0.67	0.204	(0.269)	0.184	0.020
114	9.50	0.67	0.204	(0.268)	0.184	0.020
115	9.58	0.70	0.214	(0.267)	0.193	0.021
116	9.67	0.70	0.214	(0.265)	0.193	0.021
117	9.75	0.70	0.214	(0.264)	0.193	0.021
118	9.83	0.73	0.224	(0.263)	0.202	0.022
119	9.92	0.73	0.224	(0.261)	0.202	0.022
120	10.00	0.73	0.224	(0.260)	0.202	0.022
121	10.08	0.50	0.153	(0.259)	0.138	0.015
122	10.17	0.50	0.153	(0.258)	0.138	0.015
123	10.25	0.50	0.153	(0.256)	0.138	0.015
124	10.33	0.50	0.153	(0.255)	0.138	0.015
125	10.42	0.50	0.153	(0.254)	0.138	0.015
126	10.50	0.50	0.153	(0.253)	0.138	0.015
127	10.58	0.67	0.204	(0.251)	0.184	0.020
128	10.67	0.67	0.204	(0.250)	0.184	0.020
129	10.75	0.67	0.204	(0.249)	0.184	0.020
130	10.83	0.67	0.204	(0.248)	0.184	0.020
131	10.92	0.67	0.204	(0.247)	0.184	0.020
132	11.00	0.67	0.204	(0.245)	0.184	0.020
133	11.08	0.63	0.194	(0.244)	0.174	0.019
134	11.17	0.63	0.194	(0.243)	0.174	0.019
135	11.25	0.63	0.194	(0.242)	0.174	0.019
136	11.33	0.63	0.194	(0.241)	0.174	0.019
137	11.42	0.63	0.194	(0.239)	0.174	0.019
138	11.50	0.63	0.194	(0.238)	0.174	0.019
139	11.58	0.57	0.173	(0.237)	0.156	0.017
140	11.67	0.57	0.173	(0.236)	0.156	0.017
141	11.75	0.57	0.173	(0.235)	0.156	0.017
142	11.83	0.60	0.184	(0.233)	0.165	0.018
143	11.92	0.60	0.184	(0.232)	0.165	0.018
144	12.00	0.60	0.184	(0.231)	0.165	0.018
145	12.08	0.83	0.255	(0.230)	0.229	0.025
146	12.17	0.83	0.255	0.229	(0.229)	0.026
147	12.25	0.83	0.255	0.228	(0.229)	0.027
148	12.33	0.87	0.265	0.227	(0.239)	0.039
149	12.42	0.87	0.265	0.225	(0.239)	0.040
150	12.50	0.87	0.265	0.224	(0.239)	0.041
151	12.58	0.93	0.286	0.223	(0.257)	0.062
152	12.67	0.93	0.286	0.222	(0.257)	0.064
153	12.75	0.93	0.286	0.221	(0.257)	0.065

154	12.83	0.97	0.296		0.220	(0.266)	0.076
155	12.92	0.97	0.296		0.219	(0.266)	0.077
156	13.00	0.97	0.296		0.218	(0.266)	0.078
157	13.08	1.13	0.347		0.216	(0.312)	0.130
158	13.17	1.13	0.347		0.215	(0.312)	0.131
159	13.25	1.13	0.347		0.214	(0.312)	0.132
160	13.33	1.13	0.347		0.213	(0.312)	0.134
161	13.42	1.13	0.347		0.212	(0.312)	0.135
162	13.50	1.13	0.347		0.211	(0.312)	0.136
163	13.58	0.77	0.235		0.210	(0.211)	0.025
164	13.67	0.77	0.235		0.209	(0.211)	0.026
165	13.75	0.77	0.235		0.208	(0.211)	0.027
166	13.83	0.77	0.235		0.207	(0.211)	0.028
167	13.92	0.77	0.235		0.206	(0.211)	0.029
168	14.00	0.77	0.235		0.205	(0.211)	0.030
169	14.08	0.90	0.275		0.204	(0.248)	0.072
170	14.17	0.90	0.275		0.203	(0.248)	0.073
171	14.25	0.90	0.275		0.202	(0.248)	0.074
172	14.33	0.87	0.265		0.200	(0.239)	0.065
173	14.42	0.87	0.265		0.199	(0.239)	0.066
174	14.50	0.87	0.265		0.198	(0.239)	0.067
175	14.58	0.87	0.265		0.197	(0.239)	0.068
176	14.67	0.87	0.265		0.196	(0.239)	0.069
177	14.75	0.87	0.265		0.195	(0.239)	0.070
178	14.83	0.83	0.255		0.194	(0.229)	0.061
179	14.92	0.83	0.255		0.193	(0.229)	0.062
180	15.00	0.83	0.255		0.192	(0.229)	0.063
181	15.08	0.80	0.245		0.191	(0.220)	0.053
182	15.17	0.80	0.245		0.190	(0.220)	0.054
183	15.25	0.80	0.245		0.189	(0.220)	0.055
184	15.33	0.77	0.235		0.188	(0.211)	0.046
185	15.42	0.77	0.235		0.188	(0.211)	0.047
186	15.50	0.77	0.235		0.187	(0.211)	0.048
187	15.58	0.63	0.194	(0.186)		0.174	0.019
188	15.67	0.63	0.194	(0.185)		0.174	0.019
189	15.75	0.63	0.194	(0.184)		0.174	0.019
190	15.83	0.63	0.194	(0.183)		0.174	0.019
191	15.92	0.63	0.194	(0.182)		0.174	0.019
192	16.00	0.63	0.194	(0.181)		0.174	0.019
193	16.08	0.13	0.041	(0.180)		0.037	0.004
194	16.17	0.13	0.041	(0.179)		0.037	0.004
195	16.25	0.13	0.041	(0.178)		0.037	0.004
196	16.33	0.13	0.041	(0.177)		0.037	0.004
197	16.42	0.13	0.041	(0.176)		0.037	0.004
198	16.50	0.13	0.041	(0.175)		0.037	0.004
199	16.58	0.10	0.031	(0.175)		0.028	0.003
200	16.67	0.10	0.031	(0.174)		0.028	0.003
201	16.75	0.10	0.031	(0.173)		0.028	0.003
202	16.83	0.10	0.031	(0.172)		0.028	0.003
203	16.92	0.10	0.031	(0.171)		0.028	0.003
204	17.00	0.10	0.031	(0.170)		0.028	0.003
205	17.08	0.17	0.051	(0.169)		0.046	0.005
206	17.17	0.17	0.051	(0.168)		0.046	0.005
207	17.25	0.17	0.051	(0.168)		0.046	0.005
208	17.33	0.17	0.051	(0.167)		0.046	0.005
209	17.42	0.17	0.051	(0.166)		0.046	0.005
210	17.50	0.17	0.051	(0.165)		0.046	0.005
211	17.58	0.17	0.051	(0.164)		0.046	0.005
212	17.67	0.17	0.051	(0.163)		0.046	0.005
213	17.75	0.17	0.051	(0.163)		0.046	0.005
214	17.83	0.13	0.041	(0.162)		0.037	0.004
215	17.92	0.13	0.041	(0.161)		0.037	0.004
216	18.00	0.13	0.041	(0.160)		0.037	0.004
217	18.08	0.13	0.041	(0.159)		0.037	0.004
218	18.17	0.13	0.041	(0.159)		0.037	0.004
219	18.25	0.13	0.041	(0.158)		0.037	0.004
220	18.33	0.13	0.041	(0.157)		0.037	0.004
221	18.42	0.13	0.041	(0.156)		0.037	0.004
222	18.50	0.13	0.041	(0.156)		0.037	0.004
223	18.58	0.10	0.031	(0.155)		0.028	0.003
224	18.67	0.10	0.031	(0.154)		0.028	0.003
225	18.75	0.10	0.031	(0.153)		0.028	0.003
226	18.83	0.07	0.020	(0.153)		0.018	0.002
227	18.92	0.07	0.020	(0.152)		0.018	0.002
228	19.00	0.07	0.020	(0.151)		0.018	0.002
229	19.08	0.10	0.031	(0.150)		0.028	0.003
230	19.17	0.10	0.031	(0.150)		0.028	0.003
231	19.25	0.10	0.031	(0.149)		0.028	0.003
232	19.33	0.13	0.041	(0.148)		0.037	0.004
233	19.42	0.13	0.041	(0.148)		0.037	0.004
234	19.50	0.13	0.041	(0.147)		0.037	0.004
235	19.58	0.10	0.031	(0.146)		0.028	0.003
236	19.67	0.10	0.031	(0.146)		0.028	0.003
237	19.75	0.10	0.031	(0.145)		0.028	0.003
238	19.83	0.07	0.020	(0.144)		0.018	0.002
239	19.92	0.07	0.020	(0.144)		0.018	0.002

240	20.00	0.07	0.020	(0.143)	0.018	0.002
241	20.08	0.10	0.031	(0.142)	0.028	0.003
242	20.17	0.10	0.031	(0.142)	0.028	0.003
243	20.25	0.10	0.031	(0.141)	0.028	0.003
244	20.33	0.10	0.031	(0.141)	0.028	0.003
245	20.42	0.10	0.031	(0.140)	0.028	0.003
246	20.50	0.10	0.031	(0.139)	0.028	0.003
247	20.58	0.10	0.031	(0.139)	0.028	0.003
248	20.67	0.10	0.031	(0.138)	0.028	0.003
249	20.75	0.10	0.031	(0.138)	0.028	0.003
250	20.83	0.07	0.020	(0.137)	0.018	0.002
251	20.92	0.07	0.020	(0.137)	0.018	0.002
252	21.00	0.07	0.020	(0.136)	0.018	0.002
253	21.08	0.10	0.031	(0.135)	0.028	0.003
254	21.17	0.10	0.031	(0.135)	0.028	0.003
255	21.25	0.10	0.031	(0.134)	0.028	0.003
256	21.33	0.07	0.020	(0.134)	0.018	0.002
257	21.42	0.07	0.020	(0.133)	0.018	0.002
258	21.50	0.07	0.020	(0.133)	0.018	0.002
259	21.58	0.10	0.031	(0.132)	0.028	0.003
260	21.67	0.10	0.031	(0.132)	0.028	0.003
261	21.75	0.10	0.031	(0.131)	0.028	0.003
262	21.83	0.07	0.020	(0.131)	0.018	0.002
263	21.92	0.07	0.020	(0.131)	0.018	0.002
264	22.00	0.07	0.020	(0.130)	0.018	0.002
265	22.08	0.10	0.031	(0.130)	0.028	0.003
266	22.17	0.10	0.031	(0.129)	0.028	0.003
267	22.25	0.10	0.031	(0.129)	0.028	0.003
268	22.33	0.07	0.020	(0.128)	0.018	0.002
269	22.42	0.07	0.020	(0.128)	0.018	0.002
270	22.50	0.07	0.020	(0.128)	0.018	0.002
271	22.58	0.07	0.020	(0.127)	0.018	0.002
272	22.67	0.07	0.020	(0.127)	0.018	0.002
273	22.75	0.07	0.020	(0.127)	0.018	0.002
274	22.83	0.07	0.020	(0.126)	0.018	0.002
275	22.92	0.07	0.020	(0.126)	0.018	0.002
276	23.00	0.07	0.020	(0.126)	0.018	0.002
277	23.08	0.07	0.020	(0.125)	0.018	0.002
278	23.17	0.07	0.020	(0.125)	0.018	0.002
279	23.25	0.07	0.020	(0.125)	0.018	0.002
280	23.33	0.07	0.020	(0.125)	0.018	0.002
281	23.42	0.07	0.020	(0.124)	0.018	0.002
282	23.50	0.07	0.020	(0.124)	0.018	0.002
283	23.58	0.07	0.020	(0.124)	0.018	0.002
284	23.67	0.07	0.020	(0.124)	0.018	0.002
285	23.75	0.07	0.020	(0.124)	0.018	0.002
286	23.83	0.07	0.020	(0.123)	0.018	0.002
287	23.92	0.07	0.020	(0.123)	0.018	0.002
288	24.00	0.07	0.020	(0.123)	0.018	0.002

(Loss Rate Not Used)

Sum = 100.0 Sum = 4.6

Flood volume = Effective rainfall 0.38(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 1.7(Ac.Ft)
Total soil loss = 2.17(In)
Total soil loss = 9.346(Ac.Ft)
Total rainfall = 2.55(In)
Flood volume = 72219.4 Cubic Feet
Total soil loss = 407128.1 Cubic Feet

Peak flow rate of this hydrograph = 6.892(CFS)

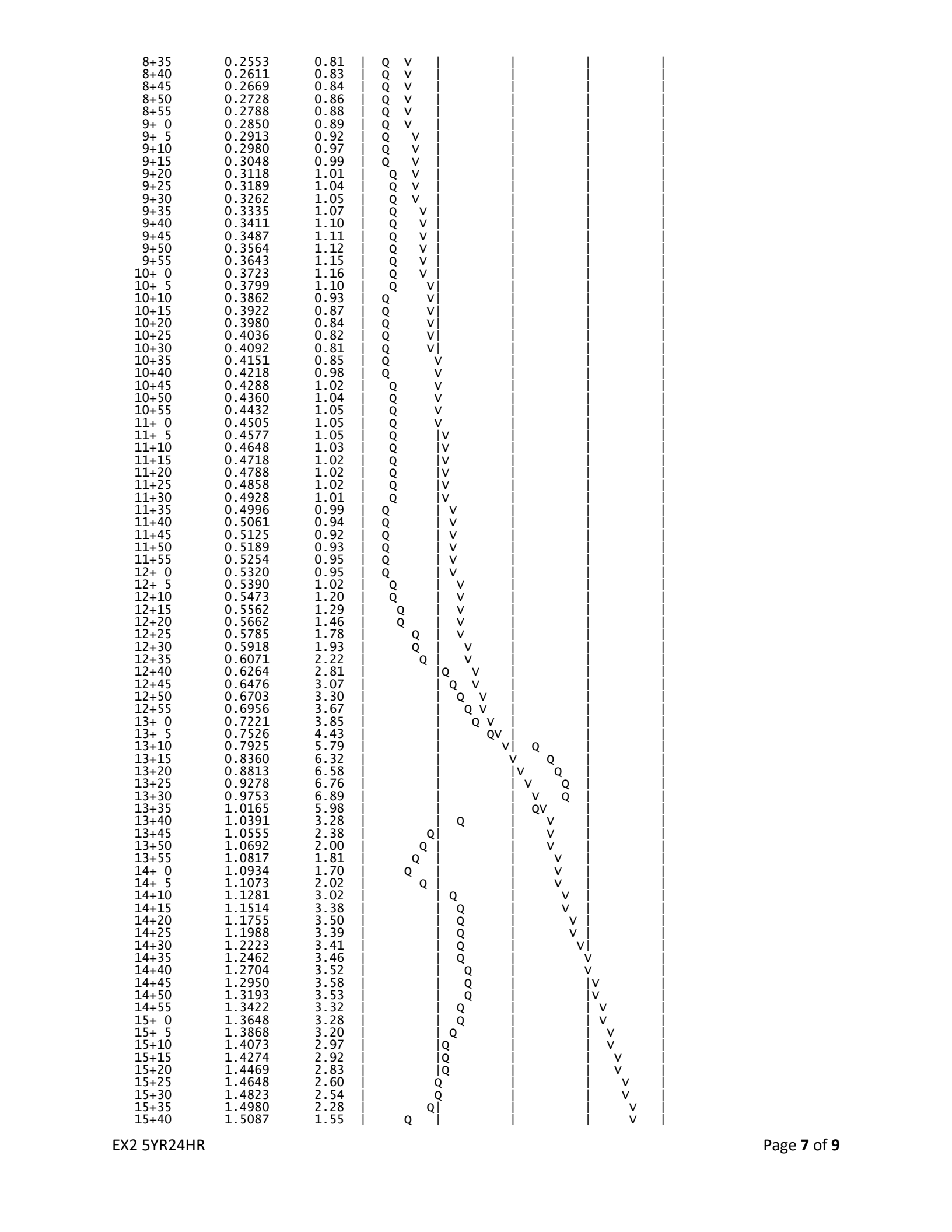
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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0001	0.02	Q	|	|	|	|
0+10	0.0006	0.07	Q	|	|	|	|
0+15	0.0012	0.09	Q	|	|	|	|
0+20	0.0019	0.10	Q	|	|	|	|
0+25	0.0028	0.13	Q	|	|	|	|
0+30	0.0038	0.15	Q	|	|	|	|
0+35	0.0049	0.15	Q	|	|	|	|
0+40	0.0060	0.16	Q	|	|	|	|
0+45	0.0070	0.16	Q	|	|	|	|
0+50	0.0082	0.17	Q	|	|	|	|
0+55	0.0095	0.19	Q	|	|	|	|
1+ 0	0.0109	0.20	Q	|	|	|	|
1+ 5	0.0123	0.20	Q	|	|	|	|
1+10	0.0135	0.17	Q	|	|	|	|
1+15	0.0147	0.17	Q	|	|	|	|
1+20	0.0158	0.16	Q	|	|	|	|

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1+25    0.0169    0.16  Q          |          |          |          |
1+30    0.0180    0.16  Q          |          |          |          |
1+35    0.0191    0.16  Q          |          |          |          |
1+40    0.0202    0.16  Q          |          |          |          |
1+45    0.0213    0.16  Q          |          |          |          |
1+50    0.0225    0.17  Q          |          |          |          |
1+55    0.0238    0.19  Q          |          |          |          |
2+ 0    0.0252    0.20  Q          |          |          |          |
2+ 5    0.0267    0.21  Q          |          |          |          |
2+10    0.0281    0.21  Q          |          |          |          |
2+15    0.0296    0.21  Q          |          |          |          |
2+20    0.0310    0.21  Q          |          |          |          |
2+25    0.0325    0.21  Q          |          |          |          |
2+30    0.0340    0.21  Q          |          |          |          |
2+35    0.0355    0.22  Q          |          |          |          |
2+40    0.0372    0.25  Q          |          |          |          |
2+45    0.0390    0.26  VQ         |          |          |          |
2+50    0.0408    0.26  VQ         |          |          |          |
2+55    0.0426    0.26  |Q         |          |          |          |
3+ 0    0.0444    0.26  |Q         |          |          |          |
3+ 5    0.0462    0.27  |Q         |          |          |          |
3+10    0.0480    0.27  |Q         |          |          |          |
3+15    0.0499    0.27  |Q         |          |          |          |
3+20    0.0517    0.27  |Q         |          |          |          |
3+25    0.0535    0.27  |Q         |          |          |          |
3+30    0.0554    0.27  |Q         |          |          |          |
3+35    0.0572    0.27  |Q         |          |          |          |
3+40    0.0590    0.27  |Q         |          |          |          |
3+45    0.0609    0.27  |Q         |          |          |          |
3+50    0.0628    0.28  |Q         |          |          |          |
3+55    0.0648    0.30  |Q         |          |          |          |
4+ 0    0.0670    0.31  |Q         |          |          |          |
4+ 5    0.0691    0.31  |Q         |          |          |          |
4+10    0.0713    0.32  |Q         |          |          |          |
4+15    0.0735    0.32  |Q         |          |          |          |
4+20    0.0758    0.33  |Q         |          |          |          |
4+25    0.0782    0.35  |Q         |          |          |          |
4+30    0.0807    0.36  |Q         |          |          |          |
4+35    0.0832    0.37  |QV        |          |          |          |
4+40    0.0858    0.37  |QV        |          |          |          |
4+45    0.0883    0.37  |QV        |          |          |          |
4+50    0.0909    0.38  |QV        |          |          |          |
4+55    0.0937    0.41  |QV        |          |          |          |
5+ 0    0.0966    0.42  |QV        |          |          |          |
5+ 5    0.0994    0.40  |QV        |          |          |          |
5+10    0.1018    0.35  |QV        |          |          |          |
5+15    0.1041    0.34  |QV        |          |          |          |
5+20    0.1065    0.34  |QV        |          |          |          |
5+25    0.1090    0.36  |QV        |          |          |          |
5+30    0.1115    0.37  |QV        |          |          |          |
5+35    0.1141    0.38  |QV        |          |          |          |
5+40    0.1169    0.40  |QV        |          |          |          |
5+45    0.1197    0.41  |QV        |          |          |          |
5+50    0.1226    0.42  |QV        |          |          |          |
5+55    0.1255    0.42  |Q V       |          |          |          |
6+ 0    0.1285    0.42  |Q V       |          |          |          |
6+ 5    0.1314    0.43  |Q V       |          |          |          |
6+10    0.1346    0.46  |Q V       |          |          |          |
6+15    0.1378    0.47  |Q V       |          |          |          |
6+20    0.1411    0.47  |Q V       |          |          |          |
6+25    0.1444    0.48  |Q V       |          |          |          |
6+30    0.1477    0.48  |Q V       |          |          |          |
6+35    0.1510    0.49  |Q V       |          |          |          |
6+40    0.1546    0.51  | QV       |          |          |          |
6+45    0.1582    0.52  | QV       |          |          |          |
6+50    0.1618    0.53  | QV       |          |          |          |
6+55    0.1654    0.53  | QV       |          |          |          |
7+ 0    0.1691    0.53  | Q V      |          |          |          |
7+ 5    0.1727    0.53  | Q V      |          |          |          |
7+10    0.1764    0.53  | Q V      |          |          |          |
7+15    0.1801    0.53  | Q V      |          |          |          |
7+20    0.1838    0.54  | Q V      |          |          |          |
7+25    0.1877    0.57  | Q V      |          |          |          |
7+30    0.1917    0.58  | Q V      |          |          |          |
7+35    0.1957    0.59  | Q V      |          |          |          |
7+40    0.2000    0.62  | Q V      |          |          |          |
7+45    0.2043    0.63  | Q V      |          |          |          |
7+50    0.2087    0.64  | Q  V     |          |          |          |
7+55    0.2133    0.67  | Q  V     |          |          |          |
8+ 0    0.2180    0.68  | Q  V     |          |          |          |
8+ 5    0.2229    0.70  | Q  V     |          |          |          |
8+10    0.2281    0.76  |  Q V     |          |          |          |
8+15    0.2335    0.78  |  Q V     |          |          |          |
8+20    0.2389    0.79  |  Q V     |          |          |          |
8+25    0.2443    0.79  |  Q V     |          |          |          |
8+30    0.2498    0.79  |  Q  V    |          |          |          |
```



8+35	0.2553	0.81	
8+40	0.2611	0.83	
8+45	0.2669	0.84	
8+50	0.2728	0.86	
8+55	0.2788	0.88	
9+ 0	0.2850	0.89	
9+ 5	0.2913	0.92	
9+10	0.2980	0.97	
9+15	0.3048	0.99	
9+20	0.3118	1.01	
9+25	0.3189	1.04	
9+30	0.3262	1.05	
9+35	0.3335	1.07	
9+40	0.3411	1.10	
9+45	0.3487	1.11	
9+50	0.3564	1.12	
9+55	0.3643	1.15	
10+ 0	0.3723	1.16	
10+ 5	0.3799	1.10	
10+10	0.3862	0.93	
10+15	0.3922	0.87	
10+20	0.3980	0.84	
10+25	0.4036	0.82	
10+30	0.4092	0.81	
10+35	0.4151	0.85	
10+40	0.4218	0.98	
10+45	0.4288	1.02	
10+50	0.4360	1.04	
10+55	0.4432	1.05	
11+ 0	0.4505	1.05	
11+ 5	0.4577	1.05	
11+10	0.4648	1.03	
11+15	0.4718	1.02	
11+20	0.4788	1.02	
11+25	0.4858	1.02	
11+30	0.4928	1.01	
11+35	0.4996	0.99	
11+40	0.5061	0.94	
11+45	0.5125	0.92	
11+50	0.5189	0.93	
11+55	0.5254	0.95	
12+ 0	0.5320	0.95	
12+ 5	0.5390	1.02	
12+10	0.5473	1.20	
12+15	0.5562	1.29	
12+20	0.5662	1.46	
12+25	0.5785	1.78	
12+30	0.5918	1.93	
12+35	0.6071	2.22	
12+40	0.6264	2.81	
12+45	0.6476	3.07	
12+50	0.6703	3.30	
12+55	0.6956	3.67	
13+ 0	0.7221	3.85	
13+ 5	0.7526	4.43	
13+10	0.7925	5.79	
13+15	0.8360	6.32	
13+20	0.8813	6.58	
13+25	0.9278	6.76	
13+30	0.9753	6.89	
13+35	1.0165	5.98	
13+40	1.0391	3.28	
13+45	1.0555	2.38	
13+50	1.0692	2.00	
13+55	1.0817	1.81	
14+ 0	1.0934	1.70	
14+ 5	1.1073	2.02	
14+10	1.1281	3.02	
14+15	1.1514	3.38	
14+20	1.1755	3.50	
14+25	1.1988	3.39	
14+30	1.2223	3.41	
14+35	1.2462	3.46	
14+40	1.2704	3.52	
14+45	1.2950	3.58	
14+50	1.3193	3.53	
14+55	1.3422	3.32	
15+ 0	1.3648	3.28	
15+ 5	1.3868	3.20	
15+10	1.4073	2.97	
15+15	1.4274	2.92	
15+20	1.4469	2.83	
15+25	1.4648	2.60	
15+30	1.4823	2.54	
15+35	1.4980	2.28	
15+40	1.5087	1.55	

```
15+45       1.5176      1.29  |     Q     |           |           |      V    |
15+50       1.5258      1.18  |    Q      |           |           |      V    |
15+55       1.5334      1.11  |    Q      |           |           |      V    |
16+ 0       1.5408      1.07  |    Q      |           |           |       V   |
16+ 5       1.5470      0.90  |   Q       |           |           |       V   |
16+10       1.5505      0.51  |  Q        |           |           |       V   |
16+15       1.5530      0.36  |Q          |           |           |       V   |
16+20       1.5551      0.30  |Q          |           |           |       V   |
16+25       1.5569      0.27  |Q          |           |           |       V   |
16+30       1.5586      0.24  Q           |           |           |       V   |
16+35       1.5601      0.22  Q           |           |           |       V   |
16+40       1.5614      0.19  Q           |           |           |       V   |
16+45       1.5625      0.17  Q           |           |           |       V   |
16+50       1.5637      0.17  Q           |           |           |       V   |
16+55       1.5648      0.16  Q           |           |           |       V   |
17+ 0       1.5659      0.16  Q           |           |           |       V   |
17+ 5       1.5672      0.18  Q           |           |           |       V   |
17+10       1.5687      0.23  Q           |           |           |       V   |
17+15       1.5704      0.25  Q           |           |           |       V   |
17+20       1.5722      0.25  |Q          |           |           |       V   |
17+25       1.5740      0.26  |Q          |           |           |       V   |
17+30       1.5758      0.26  |Q          |           |           |        V  |
17+35       1.5776      0.26  |Q          |           |           |        V  |
17+40       1.5794      0.27  |Q          |           |           |        V  |
17+45       1.5813      0.27  |Q          |           |           |        V  |
17+50       1.5830      0.26  |Q          |           |           |        V  |
17+55       1.5846      0.23  Q           |           |           |        V  |
18+ 0       1.5862      0.22  Q           |           |           |        V  |
18+ 5       1.5877      0.22  Q           |           |           |        V  |
18+10       1.5892      0.22  Q           |           |           |        V  |
18+15       1.5906      0.22  Q           |           |           |        V  |
18+20       1.5921      0.21  Q           |           |           |        V  |
18+25       1.5936      0.21  Q           |           |           |        V  |
18+30       1.5951      0.21  Q           |           |           |        V  |
18+35       1.5965      0.20  Q           |           |           |        V  |
18+40       1.5977      0.18  Q           |           |           |        V  |
18+45       1.5989      0.17  Q           |           |           |        V  |
18+50       1.5999      0.16  Q           |           |           |        V  |
18+55       1.6008      0.13  Q           |           |           |        V  |
19+ 0       1.6016      0.12  Q           |           |           |        V  |
19+ 5       1.6025      0.12  Q           |           |           |        V  |
19+10       1.6035      0.15  Q           |           |           |        V  |
19+15       1.6045      0.15  Q           |           |           |        V  |
19+20       1.6057      0.16  Q           |           |           |        V  |
19+25       1.6070      0.19  Q           |           |           |        V  |
19+30       1.6084      0.20  Q           |           |           |        V  |
19+35       1.6097      0.20  Q           |           |           |        V  |
19+40       1.6109      0.17  Q           |           |           |        V  |
19+45       1.6121      0.17  Q           |           |           |        V  |
19+50       1.6131      0.16  Q           |           |           |        V  |
19+55       1.6140      0.13  Q           |           |           |        V  |
20+ 0       1.6148      0.12  Q           |           |           |        V  |
20+ 5       1.6157      0.12  Q           |           |           |        V  |
20+10       1.6167      0.15  Q           |           |           |         V|
20+15       1.6177      0.15  Q           |           |           |         V|
20+20       1.6188      0.16  Q           |           |           |         V|
20+25       1.6199      0.16  Q           |           |           |         V|
20+30       1.6210      0.16  Q           |           |           |         V|
20+35       1.6221      0.16  Q           |           |           |         V|
20+40       1.6232      0.16  Q           |           |           |         V|
20+45       1.6243      0.16  Q           |           |           |         V|
20+50       1.6253      0.15  Q           |           |           |         V|
20+55       1.6261      0.13  Q           |           |           |         V|
21+ 0       1.6270      0.12  Q           |           |           |         V|
21+ 5       1.6278      0.12  Q           |           |           |         V|
21+10       1.6288      0.14  Q           |           |           |         V|
21+15       1.6298      0.15  Q           |           |           |         V|
21+20       1.6308      0.15  Q           |           |           |         V|
21+25       1.6317      0.12  Q           |           |           |         V|
21+30       1.6325      0.11  Q           |           |           |         V|
21+35       1.6333      0.12  Q           |           |           |         V|
21+40       1.6343      0.14  Q           |           |           |         V|
21+45       1.6353      0.15  Q           |           |           |         V|
21+50       1.6363      0.15  Q           |           |           |         V|
21+55       1.6372      0.12  Q           |           |           |         V|
22+ 0       1.6380      0.11  Q           |           |           |         V|
22+ 5       1.6388      0.12  Q           |           |           |         V|
22+10       1.6398      0.14  Q           |           |           |         V|
22+15       1.6408      0.15  Q           |           |           |         V|
22+20       1.6418      0.15  Q           |           |           |         V|
22+25       1.6427      0.12  Q           |           |           |         V|
22+30       1.6435      0.11  Q           |           |           |         V|
22+35       1.6442      0.11  Q           |           |           |         V|
22+40       1.6450      0.11  Q           |           |           |         V|
22+45       1.6457      0.11  Q           |           |           |         V|
22+50       1.6465      0.11  Q           |           |           |         V|
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   22+55       1.6472      0.11  Q          |          |          |         v|
   23+ 0       1.6479      0.11  Q          |          |          |         v|
   23+ 5       1.6487      0.11  Q          |          |          |         v|
   23+10       1.6494      0.11  Q          |          |          |         v|
   23+15       1.6501      0.11  Q          |          |          |         v|
   23+20       1.6509      0.11  Q          |          |          |         v|
   23+25       1.6516      0.11  Q          |          |          |         v|
   23+30       1.6524      0.11  Q          |          |          |         v|
   23+35       1.6531      0.11  Q          |          |          |         v|
   23+40       1.6538      0.11  Q          |          |          |         v|
   23+45       1.6546      0.11  Q          |          |          |         v|
   23+50       1.6553      0.11  Q          |          |          |         v|
   23+55       1.6560      0.11  Q          |          |          |         v|
   24+ 0       1.6568      0.11  Q          |          |          |         v|
   24+ 5       1.6574      0.09  Q          |          |          |         v|
   24+10       1.6576      0.04  Q          |          |          |         v|
   24+15       1.6578      0.02  Q          |          |          |         v|
   24+20       1.6578      0.01  Q          |          |          |         v|
   24+25       1.6579      0.01  Q          |          |          |         v|
   24+30       1.6579      0.00  Q          |          |          |         v|
   24+35       1.6579      0.00  Q          |          |          |         v|
   24+40       1.6579      0.00  Q          |          |          |          v
---------------------------------------------------------------------------
```

```
       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/22/24 File: EX210110.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2127.00(Ft.)
Length along longest watercourse measured to centroid =    1064.00(Ft.)
Length along longest watercourse =      0.403 Mi.
Length along longest watercourse measured to centroid =      0.202 Mi.
Difference in elevation =     160.00(Ft.)
Slope along watercourse =    397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.089 Hr.
Lag time =     5.34 Min.
25% of lag time =     1.33 Min.
40% of lag time =     2.13 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           0.50                 25.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           1.30                 67.34

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.829(In)
Areal adjustment factor =   99.95 %
Adjusted average point rain =    0.829(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           91.00         0.000
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  91.0      0.117     0.000        0.117       1.000      0.117
                                                 Sum (F) =   0.117
Area averaged mean soil loss (F) (In/Hr) =  0.117
Minimum soil loss rate ((In/Hr)) =  0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.328	0.117	(0.295)	0.211
2	0.17	4.20	0.418	0.117	(0.376)	0.301
3	0.25	4.40	0.438	0.117	(0.394)	0.321
4	0.33	4.80	0.477	0.117	(0.430)	0.360
5	0.42	5.20	0.517	0.117	(0.465)	0.400
6	0.50	6.20	0.617	0.117	(0.555)	0.500
7	0.58	6.80	0.676	0.117	(0.609)	0.559
8	0.67	8.80	0.875	0.117	(0.788)	0.758
9	0.75	13.90	1.382	0.117	(1.244)	1.265
10	0.83	31.40	3.123	0.117	(2.810)	3.006
11	0.92	7.20	0.716	0.117	(0.644)	0.599
12	1.00	3.80	0.378	0.117	(0.340)	0.261
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	8.5

Flood volume = Effective rainfall 0.71(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 3.1(Ac.Ft)
Total soil loss = 0.12(In)
Total soil loss = 0.505(Ac.Ft)
Total rainfall = 0.83(In)
Flood volume = 133830.8 Cubic Feet
Total soil loss = 22000.0 Cubic Feet

Peak flow rate of this hydrograph = 96.988(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	25.0	50.0	75.0	100.0
0+ 5	0.0131	1.91	Q				
0+10	0.0681	7.98	V Q				
0+15	0.1523	12.23	V Q				
0+20	0.2534	14.68	V Q				
0+25	0.3706	17.02	V Q				
0+30	0.5072	19.83	VQ				
0+35	0.6706	23.72	VQ				
0+40	0.8658	28.35	Q				
0+45	1.1352	39.12	VQ				
0+50	1.6159	69.80	V	Q			
0+55	2.2839	96.99	V			Q	
1+ 0	2.6404	51.76	Q		V		
1+ 5	2.8352	28.29	Q		V		
1+10	2.9342	14.38	Q			V	
1+15	2.9933	8.57	Q			V	
1+20	3.0305	5.40	Q			V	
1+25	3.0536	3.36	Q			V	
1+30	3.0683	2.13	Q			V	
1+35	3.0714	0.46	Q			V	
1+40	3.0723	0.13	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX210310.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2127.00(Ft.)
Length along longest watercourse measured to centroid = 1064.00(Ft.)
Length along longest watercourse = 0.403 Mi.
Length along longest watercourse measured to centroid = 0.202 Mi.
Difference in elevation = 160.00(Ft.)
Slope along watercourse = 397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.089 Hr.
Lag time = 5.34 Min.
25% of lag time = 1.33 Min.
40% of lag time = 2.13 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	0.80	41.44

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	2.00	103.60

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 1.294(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 1.293(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	91.00	0.000

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000 Sum=	52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.202	0.117	(0.182)	0.085
2	0.17	1.30	0.202	0.117	(0.182)	0.085
3	0.25	1.10	0.171	0.117	(0.154)	0.054
4	0.33	1.50	0.233	0.117	(0.210)	0.116
5	0.42	1.50	0.233	0.117	(0.210)	0.116
6	0.50	1.80	0.279	0.117	(0.251)	0.162
7	0.58	1.50	0.233	0.117	(0.210)	0.116
8	0.67	1.80	0.279	0.117	(0.251)	0.162
9	0.75	1.80	0.279	0.117	(0.251)	0.162
10	0.83	1.50	0.233	0.117	(0.210)	0.116
11	0.92	1.60	0.248	0.117	(0.223)	0.131
12	1.00	1.80	0.279	0.117	(0.251)	0.162
13	1.08	2.20	0.341	0.117	(0.307)	0.224
14	1.17	2.20	0.341	0.117	(0.307)	0.224
15	1.25	2.20	0.341	0.117	(0.307)	0.224
16	1.33	2.00	0.310	0.117	(0.279)	0.193
17	1.42	2.60	0.404	0.117	(0.363)	0.287
18	1.50	2.70	0.419	0.117	(0.377)	0.302
19	1.58	2.40	0.372	0.117	(0.335)	0.255
20	1.67	2.70	0.419	0.117	(0.377)	0.302
21	1.75	3.30	0.512	0.117	(0.461)	0.395
22	1.83	3.10	0.481	0.117	(0.433)	0.364
23	1.92	2.90	0.450	0.117	(0.405)	0.333
24	2.00	3.00	0.466	0.117	(0.419)	0.349
25	2.08	3.10	0.481	0.117	(0.433)	0.364
26	2.17	4.20	0.652	0.117	(0.587)	0.535
27	2.25	5.00	0.776	0.117	(0.698)	0.659
28	2.33	3.50	0.543	0.117	(0.489)	0.426
29	2.42	6.80	1.055	0.117	(0.950)	0.938
30	2.50	7.30	1.133	0.117	(1.020)	1.016
31	2.58	8.20	1.273	0.117	(1.145)	1.156
32	2.67	5.90	0.916	0.117	(0.824)	0.799
33	2.75	2.00	0.310	0.117	(0.279)	0.193
34	2.83	1.80	0.279	0.117	(0.251)	0.162
35	2.92	1.80	0.279	0.117	(0.251)	0.162
36	3.00	0.60	0.093	(0.117)	0.084	0.009
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	11.3

Flood volume = Effective rainfall 0.95(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 4.1(Ac.Ft)
Total soil loss = 0.35(In)
Total soil loss = 1.503(Ac.Ft)
Total rainfall = 1.29(In)
Flood volume = 177722.6 Cubic Feet
Total soil loss = 65479.9 Cubic Feet

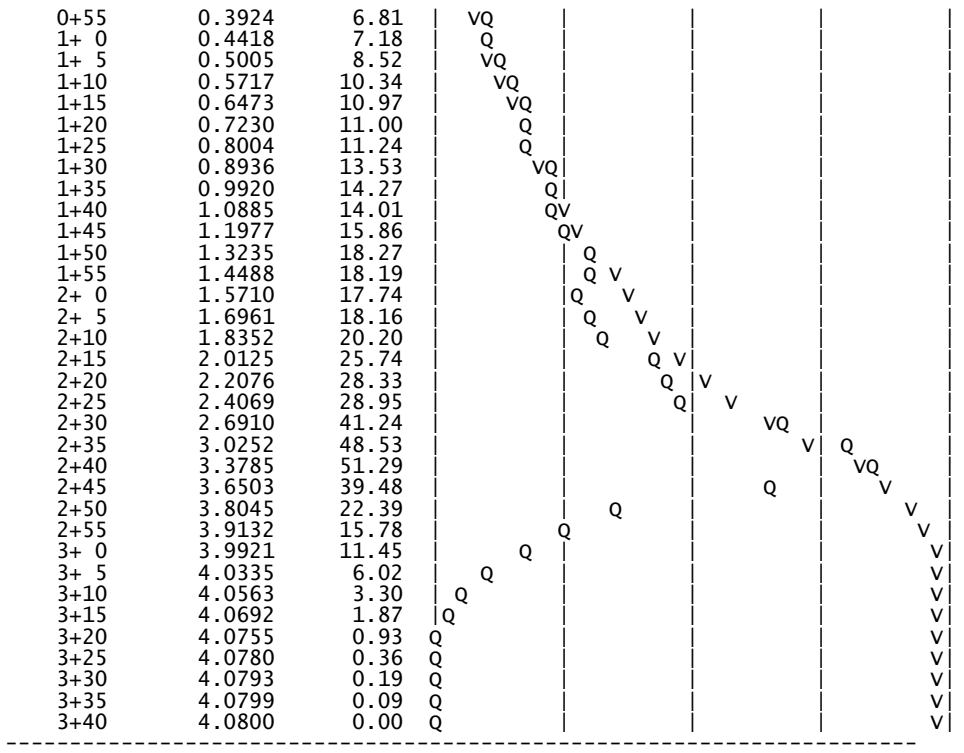
Peak flow rate of this hydrograph = 51.290(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	15.0	30.0	45.0	60.0
0+ 5	0.0053	0.77	Q	|	|	|	|
0+10	0.0251	2.88	VQ	|	|	|	|
0+15	0.0481	3.34	V Q	|	|	|	|
0+20	0.0718	3.45	V Q	|	|	|	|
0+25	0.1057	4.92	|V Q	|	|	|	|
0+30	0.1462	5.88	|V Q	|	|	|	|
0+35	0.1935	6.87	|V Q	|	|	|	|
0+40	0.2395	6.68	| V Q	|	|	|	|
0+45	0.2927	7.72	| V Q	|	|	|	|
0+50	0.3455	7.67	| V Q	|	|	|	|



0+55	0.3924	6.81	VQ				
1+ 0	0.4418	7.18	Q				
1+ 5	0.5005	8.52	VQ				
1+10	0.5717	10.34	VQ				
1+15	0.6473	10.97	VQ				
1+20	0.7230	11.00	Q				
1+25	0.8004	11.24	Q				
1+30	0.8936	13.53	VQ				
1+35	0.9920	14.27	Q				
1+40	1.0885	14.01	QV				
1+45	1.1977	15.86	QV				
1+50	1.3235	18.27	Q				
1+55	1.4488	18.19	Q V				
2+ 0	1.5710	17.74	Q V				
2+ 5	1.6961	18.16	Q V				
2+10	1.8352	20.20	Q V				
2+15	2.0125	25.74	Q V				
2+20	2.2076	28.33	Q V				
2+25	2.4069	28.95	Q V				
2+30	2.6910	41.24	VQ				
2+35	3.0252	48.53	V Q				
2+40	3.3785	51.29	VQ				
2+45	3.6503	39.48	Q V				
2+50	3.8045	22.39	Q V				
2+55	3.9132	15.78	Q V				
3+ 0	3.9921	11.45	Q V				
3+ 5	4.0335	6.02	Q V				
3+10	4.0563	3.30	Q V				
3+15	4.0692	1.87	Q V				
3+20	4.0755	0.93	Q V				
3+25	4.0780	0.36	Q V				
3+30	4.0793	0.19	Q V				
3+35	4.0799	0.09	Q V				
3+40	4.0800	0.00	Q V				

```
       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/22/24 File: EX210610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2127.00(Ft.)
Length along longest watercourse measured to centroid =    1064.00(Ft.)
Length along longest watercourse =      0.403 Mi.
Length along longest watercourse measured to centroid =      0.202 Mi.
Difference in elevation =     160.00(Ft.)
Slope along watercourse =    397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.089 Hr.
Lag time =     5.34 Min.
25% of lag time =     1.33 Min.
40% of lag time =     2.13 Min.
Unit time =     5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           1.10                 56.98

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           3.00                155.40

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    1.100(In)
Area Averaged 100-Year Rainfall =    3.000(In)

Point rain (area averaged) =    1.882(In)
Areal adjustment factor =   99.98 %
Adjusted average point rain =    1.881(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           91.00         0.000
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  91.0      0.117     0.000        0.117       1.000      0.117
                                                 Sum (F) =   0.117
Area averaged mean soil loss (F) (In/Hr) =  0.117
Minimum soil loss rate ((In/Hr)) =  0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.113	(0.117)	0.102	0.011
2	0.17	0.60	0.135	0.117	(0.122)	0.018
3	0.25	0.60	0.135	0.117	(0.122)	0.018
4	0.33	0.60	0.135	0.117	(0.122)	0.018
5	0.42	0.60	0.135	0.117	(0.122)	0.018
6	0.50	0.70	0.158	0.117	(0.142)	0.041
7	0.58	0.70	0.158	0.117	(0.142)	0.041
8	0.67	0.70	0.158	0.117	(0.142)	0.041
9	0.75	0.70	0.158	0.117	(0.142)	0.041
10	0.83	0.70	0.158	0.117	(0.142)	0.041
11	0.92	0.70	0.158	0.117	(0.142)	0.041
12	1.00	0.80	0.181	0.117	(0.163)	0.064
13	1.08	0.80	0.181	0.117	(0.163)	0.064
14	1.17	0.80	0.181	0.117	(0.163)	0.064
15	1.25	0.80	0.181	0.117	(0.163)	0.064
16	1.33	0.80	0.181	0.117	(0.163)	0.064
17	1.42	0.80	0.181	0.117	(0.163)	0.064
18	1.50	0.80	0.181	0.117	(0.163)	0.064
19	1.58	0.80	0.181	0.117	(0.163)	0.064
20	1.67	0.80	0.181	0.117	(0.163)	0.064
21	1.75	0.80	0.181	0.117	(0.163)	0.064
22	1.83	0.80	0.181	0.117	(0.163)	0.064
23	1.92	0.80	0.181	0.117	(0.163)	0.064
24	2.00	0.90	0.203	0.117	(0.183)	0.086
25	2.08	0.80	0.181	0.117	(0.163)	0.064
26	2.17	0.90	0.203	0.117	(0.183)	0.086
27	2.25	0.90	0.203	0.117	(0.183)	0.086
28	2.33	0.90	0.203	0.117	(0.183)	0.086
29	2.42	0.90	0.203	0.117	(0.183)	0.086
30	2.50	0.90	0.203	0.117	(0.183)	0.086
31	2.58	0.90	0.203	0.117	(0.183)	0.086
32	2.67	0.90	0.203	0.117	(0.183)	0.086
33	2.75	1.00	0.226	0.117	(0.203)	0.109
34	2.83	1.00	0.226	0.117	(0.203)	0.109
35	2.92	1.00	0.226	0.117	(0.203)	0.109
36	3.00	1.00	0.226	0.117	(0.203)	0.109
37	3.08	1.00	0.226	0.117	(0.203)	0.109
38	3.17	1.10	0.248	0.117	(0.224)	0.131
39	3.25	1.10	0.248	0.117	(0.224)	0.131
40	3.33	1.10	0.248	0.117	(0.224)	0.131
41	3.42	1.20	0.271	0.117	(0.244)	0.154
42	3.50	1.30	0.293	0.117	(0.264)	0.176
43	3.58	1.40	0.316	0.117	(0.284)	0.199
44	3.67	1.40	0.316	0.117	(0.284)	0.199
45	3.75	1.50	0.339	0.117	(0.305)	0.222
46	3.83	1.50	0.339	0.117	(0.305)	0.222
47	3.92	1.60	0.361	0.117	(0.325)	0.244
48	4.00	1.60	0.361	0.117	(0.325)	0.244
49	4.08	1.70	0.384	0.117	(0.345)	0.267
50	4.17	1.80	0.406	0.117	(0.366)	0.289
51	4.25	1.90	0.429	0.117	(0.386)	0.312
52	4.33	2.00	0.452	0.117	(0.406)	0.335
53	4.42	2.10	0.474	0.117	(0.427)	0.357
54	4.50	2.10	0.474	0.117	(0.427)	0.357
55	4.58	2.20	0.497	0.117	(0.447)	0.380
56	4.67	2.30	0.519	0.117	(0.467)	0.402
57	4.75	2.40	0.542	0.117	(0.488)	0.425
58	4.83	2.40	0.542	0.117	(0.488)	0.425
59	4.92	2.50	0.564	0.117	(0.508)	0.447
60	5.00	2.60	0.587	0.117	(0.528)	0.470
61	5.08	3.10	0.700	0.117	(0.630)	0.583
62	5.17	3.60	0.813	0.117	(0.731)	0.696
63	5.25	3.90	0.880	0.117	(0.792)	0.763
64	5.33	4.20	0.948	0.117	(0.853)	0.831
65	5.42	4.70	1.061	0.117	(0.955)	0.944
66	5.50	5.60	1.264	0.117	(1.138)	1.147
67	5.58	1.90	0.429	0.117	(0.386)	0.312

```
68   5.67     0.90      0.203          0.117    (  0.183)        0.086
69   5.75     0.60      0.135          0.117    (  0.122)        0.018
70   5.83     0.50      0.113       (  0.117)       0.102        0.011
71   5.92     0.30      0.068       (  0.117)       0.061        0.007
72   6.00     0.20      0.045       (  0.117)       0.041        0.005
              (Loss Rate Not Used)
   Sum =     100.0                                    Sum =    14.3
      Flood volume = Effective rainfall      1.19(In)
       times area      51.8(Ac.)/[(In)/(Ft.)] =       5.1(Ac.Ft)
      Total soil loss =      0.69(In)
      Total soil loss =     2.972(Ac.Ft)
      Total rainfall =      1.88(In)
      Flood volume =      224313.7 Cubic Feet
      Total soil loss =      129442.2 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     47.388(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0       12.5      25.0      37.5      50.0
-------------------------------------------------------------------------
  0+ 5       0.0007      0.10  Q          |         |         |         |
  0+10       0.0038      0.45  Q          |         |         |         |
  0+15       0.0088      0.72  Q          |         |         |         |
  0+20       0.0145      0.83  Q          |         |         |         |
  0+25       0.0206      0.88  Q          |         |         |         |
  0+30       0.0283      1.12  Q          |         |         |         |
  0+35       0.0400      1.70  VQ         |         |         |         |
  0+40       0.0532      1.91  VQ         |         |         |         |
  0+45       0.0671      2.01  VQ         |         |         |         |
  0+50       0.0813      2.06  VQ         |         |         |         |
  0+55       0.0957      2.10  VQ         |         |         |         |
  1+ 0       0.1117      2.32  VQ         |         |         |         |
  1+ 5       0.1317      2.90  |VQ        |         |         |         |
  1+10       0.1531      3.11  |VQ        |         |         |         |
  1+15       0.1751      3.19  |VQ        |         |         |         |
  1+20       0.1974      3.24  |VQ        |         |         |         |
  1+25       0.2200      3.28  |VQ        |         |         |         |
  1+30       0.2427      3.30  |VQ        |         |         |         |
  1+35       0.2655      3.31  | Q        |         |         |         |
  1+40       0.2884      3.32  | Q        |         |         |         |
  1+45       0.3112      3.32  | Q        |         |         |         |
  1+50       0.3341      3.32  | Q        |         |         |         |
  1+55       0.3570      3.32  | Q        |         |         |         |
  2+ 0       0.3813      3.53  | Q        |         |         |         |
  2+ 5       0.4081      3.88  |  Q       |         |         |         |
  2+10       0.4337      3.72  | QV       |         |         |         |
  2+15       0.4625      4.18  |  Q       |         |         |         |
  2+20       0.4923      4.34  |  Q       |         |         |         |
  2+25       0.5227      4.41  |  QV      |         |         |         |
  2+30       0.5533      4.44  |  QV      |         |         |         |
  2+35       0.5840      4.47  |  QV      |         |         |         |
  2+40       0.6150      4.49  |  QV      |         |         |         |
  2+45       0.6473      4.69  |  Q V     |         |         |         |
  2+50       0.6836      5.27  |   QV     |         |         |         |
  2+55       0.7212      5.46  |   QV     |         |         |         |
  3+ 0       0.7594      5.55  |   QV     |         |         |         |
  3+ 5       0.7980      5.60  |   Q V    |         |         |         |
  3+10       0.8382      5.84  |   Q V    |         |         |         |
  3+15       0.8825      6.42  |    QV    |         |         |         |
  3+20       0.9281      6.63  |    Q V   |         |         |         |
  3+25       0.9759      6.94  |    Q V   |         |         |         |
  3+30       1.0293      7.75  |     QV   |         |         |         |
  3+35       1.0895      8.75  |     Q V  |         |         |         |
  3+40       1.1557      9.62  |      QV  |         |         |         |
  3+45       1.2258     10.17  |       QV|         |         |         |
  3+50       1.3009     10.91  |       Q V        |         |         |
  3+55       1.3795     11.42  |        QV        |         |         |
  4+ 0       1.4631     12.13  |        Q|V        |         |         |
  4+ 5       1.5501     12.63  |         Q V       |         |         |
  4+10       1.6433     13.54  |         Q V       |         |         |
  4+15       1.7438     14.59  |         |Q V      |         |         |
  4+20       1.8518     15.68  |         | Q V     |         |         |
  4+25       1.9676     16.82  |         |  Q V    |         |         |
  4+30       2.0899     17.76  |         |   Q V   |         |         |
  4+35       2.2163     18.36  |         |   Q  V  |         |         |
  4+40       2.3495     19.33  |         |    Q  V |         |         |
  4+45       2.4901     20.42  |         |     Q  V|         |         |
  4+50       2.6372     21.35  |         |      Q  V        |         |
  4+55       2.7882     21.93  |         |      Q  |V       |         |
  5+ 0       2.9459     22.89  |         |       Q | V      |         |
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    5+ 5       3.1166     24.79  |          |          |          |          |          |          |
    5+10       3.3162     28.97  |          |          |          |          |          |          |
    5+15       3.5473     33.56  |          |          |          |          |          |          |
    5+20       3.8048     37.39  |          |          |          |          |          |          |
    5+25       4.0902     41.44  |          |          |          |          |          |          |
    5+30       4.4166     47.39  |          |          |          |          |          |          |
    5+35       4.7376     46.60  |          |          |          |          |          |          |
    5+40       4.9193     26.39  |          |          |          |          |          |          |
    5+45       5.0170     14.19  |          |          |          |          |          |          |
    5+50       5.0722      8.01  |          |          |          |          |          |          |
    5+55       5.1062      4.94  |          |          |          |          |          |          |
    6+ 0       5.1274      3.08  |          |          |          |          |          |          |
    6+ 5       5.1400      1.83  |          |          |          |          |          |          |
    6+10       5.1467      0.97  |          |          |          |          |          |          |
    6+15       5.1486      0.28  |          |          |          |          |          |          |
    6+20       5.1492      0.09  |          |          |          |          |          |          |
    6+25       5.1494      0.03  |          |          |          |          |          |          |
    6+30       5.1495      0.01  |          |          |          |          |          |          |
    6+35       5.1495      0.01  |          |          |          |          |          |          |
    6+40       5.1495      0.00  |          |          |          |          |          |          |
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX2102410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2127.00(Ft.)
Length along longest watercourse measured to centroid = 1064.00(Ft.)
Length along longest watercourse = 0.403 Mi.
Length along longest watercourse measured to centroid = 0.202 Mi.
Difference in elevation = 160.00(Ft.)
Slope along watercourse = 397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.089 Hr.
Lag time = 5.34 Min.
25% of lag time = 1.33 Min.
40% of lag time = 2.13 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	1.80	93.24

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	5.00	259.00

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 3.117(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 3.116(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	91.00	0.000

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.025	(0.207)	0.022	0.002
2	0.17	0.07	0.025	(0.207)	0.022	0.002
3	0.25	0.07	0.025	(0.206)	0.022	0.002
4	0.33	0.10	0.037	(0.205)	0.034	0.004
5	0.42	0.10	0.037	(0.204)	0.034	0.004
6	0.50	0.10	0.037	(0.203)	0.034	0.004
7	0.58	0.10	0.037	(0.203)	0.034	0.004
8	0.67	0.10	0.037	(0.202)	0.034	0.004
9	0.75	0.10	0.037	(0.201)	0.034	0.004
10	0.83	0.13	0.050	(0.200)	0.045	0.005
11	0.92	0.13	0.050	(0.199)	0.045	0.005
12	1.00	0.13	0.050	(0.199)	0.045	0.005
13	1.08	0.10	0.037	(0.198)	0.034	0.004
14	1.17	0.10	0.037	(0.197)	0.034	0.004
15	1.25	0.10	0.037	(0.196)	0.034	0.004
16	1.33	0.10	0.037	(0.196)	0.034	0.004
17	1.42	0.10	0.037	(0.195)	0.034	0.004
18	1.50	0.10	0.037	(0.194)	0.034	0.004
19	1.58	0.10	0.037	(0.193)	0.034	0.004
20	1.67	0.10	0.037	(0.192)	0.034	0.004
21	1.75	0.10	0.037	(0.192)	0.034	0.004
22	1.83	0.13	0.050	(0.191)	0.045	0.005
23	1.92	0.13	0.050	(0.190)	0.045	0.005
24	2.00	0.13	0.050	(0.189)	0.045	0.005
25	2.08	0.13	0.050	(0.189)	0.045	0.005
26	2.17	0.13	0.050	(0.188)	0.045	0.005
27	2.25	0.13	0.050	(0.187)	0.045	0.005
28	2.33	0.13	0.050	(0.186)	0.045	0.005
29	2.42	0.13	0.050	(0.186)	0.045	0.005
30	2.50	0.13	0.050	(0.185)	0.045	0.005
31	2.58	0.17	0.062	(0.184)	0.056	0.006
32	2.67	0.17	0.062	(0.183)	0.056	0.006
33	2.75	0.17	0.062	(0.183)	0.056	0.006
34	2.83	0.17	0.062	(0.182)	0.056	0.006
35	2.92	0.17	0.062	(0.181)	0.056	0.006
36	3.00	0.17	0.062	(0.180)	0.056	0.006
37	3.08	0.17	0.062	(0.180)	0.056	0.006
38	3.17	0.17	0.062	(0.179)	0.056	0.006
39	3.25	0.17	0.062	(0.178)	0.056	0.006
40	3.33	0.17	0.062	(0.177)	0.056	0.006
41	3.42	0.17	0.062	(0.177)	0.056	0.006
42	3.50	0.17	0.062	(0.176)	0.056	0.006
43	3.58	0.17	0.062	(0.175)	0.056	0.006
44	3.67	0.17	0.062	(0.174)	0.056	0.006
45	3.75	0.17	0.062	(0.174)	0.056	0.006
46	3.83	0.20	0.075	(0.173)	0.067	0.007
47	3.92	0.20	0.075	(0.172)	0.067	0.007
48	4.00	0.20	0.075	(0.171)	0.067	0.007
49	4.08	0.20	0.075	(0.171)	0.067	0.007
50	4.17	0.20	0.075	(0.170)	0.067	0.007
51	4.25	0.20	0.075	(0.169)	0.067	0.007
52	4.33	0.23	0.087	(0.169)	0.079	0.009
53	4.42	0.23	0.087	(0.168)	0.079	0.009
54	4.50	0.23	0.087	(0.167)	0.079	0.009
55	4.58	0.23	0.087	(0.166)	0.079	0.009
56	4.67	0.23	0.087	(0.166)	0.079	0.009
57	4.75	0.23	0.087	(0.165)	0.079	0.009
58	4.83	0.27	0.100	(0.164)	0.090	0.010
59	4.92	0.27	0.100	(0.164)	0.090	0.010
60	5.00	0.27	0.100	(0.163)	0.090	0.010
61	5.08	0.20	0.075	(0.162)	0.067	0.007
62	5.17	0.20	0.075	(0.161)	0.067	0.007
63	5.25	0.20	0.075	(0.161)	0.067	0.007
64	5.33	0.23	0.087	(0.160)	0.079	0.009
65	5.42	0.23	0.087	(0.159)	0.079	0.009
66	5.50	0.23	0.087	(0.159)	0.079	0.009
67	5.58	0.27	0.100	(0.158)	0.090	0.010

68	5.67	0.27	0.100	(0.157)	0.090	0.010
69	5.75	0.27	0.100	(0.157)	0.090	0.010
70	5.83	0.27	0.100	(0.156)	0.090	0.010
71	5.92	0.27	0.100	(0.155)	0.090	0.010
72	6.00	0.27	0.100	(0.154)	0.090	0.010
73	6.08	0.30	0.112	(0.154)	0.101	0.011
74	6.17	0.30	0.112	(0.153)	0.101	0.011
75	6.25	0.30	0.112	(0.152)	0.101	0.011
76	6.33	0.30	0.112	(0.152)	0.101	0.011
77	6.42	0.30	0.112	(0.151)	0.101	0.011
78	6.50	0.30	0.112	(0.150)	0.101	0.011
79	6.58	0.33	0.125	(0.150)	0.112	0.012
80	6.67	0.33	0.125	(0.149)	0.112	0.012
81	6.75	0.33	0.125	(0.148)	0.112	0.012
82	6.83	0.33	0.125	(0.148)	0.112	0.012
83	6.92	0.33	0.125	(0.147)	0.112	0.012
84	7.00	0.33	0.125	(0.146)	0.112	0.012
85	7.08	0.33	0.125	(0.146)	0.112	0.012
86	7.17	0.33	0.125	(0.145)	0.112	0.012
87	7.25	0.33	0.125	(0.144)	0.112	0.012
88	7.33	0.37	0.137	(0.144)	0.123	0.014
89	7.42	0.37	0.137	(0.143)	0.123	0.014
90	7.50	0.37	0.137	(0.142)	0.123	0.014
91	7.58	0.40	0.150	(0.142)	0.135	0.015
92	7.67	0.40	0.150	(0.141)	0.135	0.015
93	7.75	0.40	0.150	(0.140)	0.135	0.015
94	7.83	0.43	0.162	0.140	(0.146)	0.022
95	7.92	0.43	0.162	0.139	(0.146)	0.023
96	8.00	0.43	0.162	0.138	(0.146)	0.024
97	8.08	0.50	0.187	0.138	(0.168)	0.049
98	8.17	0.50	0.187	0.137	(0.168)	0.050
99	8.25	0.50	0.187	0.137	(0.168)	0.050
100	8.33	0.50	0.187	0.136	(0.168)	0.051
101	8.42	0.50	0.187	0.135	(0.168)	0.052
102	8.50	0.50	0.187	0.135	(0.168)	0.052
103	8.58	0.53	0.199	0.134	(0.179)	0.065
104	8.67	0.53	0.199	0.133	(0.179)	0.066
105	8.75	0.53	0.199	0.133	(0.179)	0.067
106	8.83	0.57	0.212	0.132	(0.191)	0.080
107	8.92	0.57	0.212	0.131	(0.191)	0.080
108	9.00	0.57	0.212	0.131	(0.191)	0.081
109	9.08	0.63	0.237	0.130	(0.213)	0.107
110	9.17	0.63	0.237	0.130	(0.213)	0.107
111	9.25	0.63	0.237	0.129	(0.213)	0.108
112	9.33	0.67	0.249	0.128	(0.224)	0.121
113	9.42	0.67	0.249	0.128	(0.224)	0.122
114	9.50	0.67	0.249	0.127	(0.224)	0.122
115	9.58	0.70	0.262	0.127	(0.236)	0.135
116	9.67	0.70	0.262	0.126	(0.236)	0.136
117	9.75	0.70	0.262	0.125	(0.236)	0.136
118	9.83	0.73	0.274	0.125	(0.247)	0.149
119	9.92	0.73	0.274	0.124	(0.247)	0.150
120	10.00	0.73	0.274	0.124	(0.247)	0.151
121	10.08	0.50	0.187	0.123	(0.168)	0.064
122	10.17	0.50	0.187	0.122	(0.168)	0.065
123	10.25	0.50	0.187	0.122	(0.168)	0.065
124	10.33	0.50	0.187	0.121	(0.168)	0.066
125	10.42	0.50	0.187	0.121	(0.168)	0.066
126	10.50	0.50	0.187	0.120	(0.168)	0.067
127	10.58	0.67	0.249	0.119	(0.224)	0.130
128	10.67	0.67	0.249	0.119	(0.224)	0.130
129	10.75	0.67	0.249	0.118	(0.224)	0.131
130	10.83	0.67	0.249	0.118	(0.224)	0.132
131	10.92	0.67	0.249	0.117	(0.224)	0.132
132	11.00	0.67	0.249	0.117	(0.224)	0.133
133	11.08	0.63	0.237	0.116	(0.213)	0.121
134	11.17	0.63	0.237	0.115	(0.213)	0.121
135	11.25	0.63	0.237	0.115	(0.213)	0.122
136	11.33	0.63	0.237	0.114	(0.213)	0.123
137	11.42	0.63	0.237	0.114	(0.213)	0.123
138	11.50	0.63	0.237	0.113	(0.213)	0.124
139	11.58	0.57	0.212	0.113	(0.191)	0.099
140	11.67	0.57	0.212	0.112	(0.191)	0.100
141	11.75	0.57	0.212	0.111	(0.191)	0.100
142	11.83	0.60	0.224	0.111	(0.202)	0.113
143	11.92	0.60	0.224	0.110	(0.202)	0.114
144	12.00	0.60	0.224	0.110	(0.202)	0.115
145	12.08	0.83	0.312	0.109	(0.280)	0.202
146	12.17	0.83	0.312	0.109	(0.280)	0.203
147	12.25	0.83	0.312	0.108	(0.280)	0.203
148	12.33	0.87	0.324	0.108	(0.292)	0.217
149	12.42	0.87	0.324	0.107	(0.292)	0.217
150	12.50	0.87	0.324	0.107	(0.292)	0.218
151	12.58	0.93	0.349	0.106	(0.314)	0.243
152	12.67	0.93	0.349	0.105	(0.314)	0.244
153	12.75	0.93	0.349	0.105	(0.314)	0.244

154	12.83	0.97	0.361	0.104	(0.325)	0.257
155	12.92	0.97	0.361	0.104	(0.325)	0.258
156	13.00	0.97	0.361	0.103	(0.325)	0.258
157	13.08	1.13	0.424	0.103	(0.381)	0.321
158	13.17	1.13	0.424	0.102	(0.381)	0.322
159	13.25	1.13	0.424	0.102	(0.381)	0.322
160	13.33	1.13	0.424	0.101	(0.381)	0.323
161	13.42	1.13	0.424	0.101	(0.381)	0.323
162	13.50	1.13	0.424	0.100	(0.381)	0.324
163	13.58	0.77	0.287	0.100	(0.258)	0.187
164	13.67	0.77	0.287	0.099	(0.258)	0.187
165	13.75	0.77	0.287	0.099	(0.258)	0.188
166	13.83	0.77	0.287	0.098	(0.258)	0.189
167	13.92	0.77	0.287	0.098	(0.258)	0.189
168	14.00	0.77	0.287	0.097	(0.258)	0.190
169	14.08	0.90	0.337	0.097	(0.303)	0.240
170	14.17	0.90	0.337	0.096	(0.303)	0.240
171	14.25	0.90	0.337	0.096	(0.303)	0.241
172	14.33	0.87	0.324	0.095	(0.292)	0.229
173	14.42	0.87	0.324	0.095	(0.292)	0.229
174	14.50	0.87	0.324	0.094	(0.292)	0.230
175	14.58	0.87	0.324	0.094	(0.292)	0.230
176	14.67	0.87	0.324	0.093	(0.292)	0.231
177	14.75	0.87	0.324	0.093	(0.292)	0.231
178	14.83	0.83	0.312	0.092	(0.280)	0.219
179	14.92	0.83	0.312	0.092	(0.280)	0.220
180	15.00	0.83	0.312	0.091	(0.280)	0.220
181	15.08	0.80	0.299	0.091	(0.269)	0.208
182	15.17	0.80	0.299	0.090	(0.269)	0.209
183	15.25	0.80	0.299	0.090	(0.269)	0.209
184	15.33	0.77	0.287	0.090	(0.258)	0.197
185	15.42	0.77	0.287	0.089	(0.258)	0.198
186	15.50	0.77	0.287	0.089	(0.258)	0.198
187	15.58	0.63	0.237	0.088	(0.213)	0.149
188	15.67	0.63	0.237	0.088	(0.213)	0.149
189	15.75	0.63	0.237	0.087	(0.213)	0.150
190	15.83	0.63	0.237	0.087	(0.213)	0.150
191	15.92	0.63	0.237	0.086	(0.213)	0.150
192	16.00	0.63	0.237	0.086	(0.213)	0.151
193	16.08	0.13	0.050	(0.085)	0.045	0.005
194	16.17	0.13	0.050	(0.085)	0.045	0.005
195	16.25	0.13	0.050	(0.085)	0.045	0.005
196	16.33	0.13	0.050	(0.084)	0.045	0.005
197	16.42	0.13	0.050	(0.084)	0.045	0.005
198	16.50	0.13	0.050	(0.083)	0.045	0.005
199	16.58	0.10	0.037	(0.083)	0.034	0.004
200	16.67	0.10	0.037	(0.082)	0.034	0.004
201	16.75	0.10	0.037	(0.082)	0.034	0.004
202	16.83	0.10	0.037	(0.082)	0.034	0.004
203	16.92	0.10	0.037	(0.081)	0.034	0.004
204	17.00	0.10	0.037	(0.081)	0.034	0.004
205	17.08	0.17	0.062	(0.080)	0.056	0.006
206	17.17	0.17	0.062	(0.080)	0.056	0.006
207	17.25	0.17	0.062	(0.080)	0.056	0.006
208	17.33	0.17	0.062	(0.079)	0.056	0.006
209	17.42	0.17	0.062	(0.079)	0.056	0.006
210	17.50	0.17	0.062	(0.078)	0.056	0.006
211	17.58	0.17	0.062	(0.078)	0.056	0.006
212	17.67	0.17	0.062	(0.078)	0.056	0.006
213	17.75	0.17	0.062	(0.077)	0.056	0.006
214	17.83	0.13	0.050	(0.077)	0.045	0.005
215	17.92	0.13	0.050	(0.076)	0.045	0.005
216	18.00	0.13	0.050	(0.076)	0.045	0.005
217	18.08	0.13	0.050	(0.076)	0.045	0.005
218	18.17	0.13	0.050	(0.075)	0.045	0.005
219	18.25	0.13	0.050	(0.075)	0.045	0.005
220	18.33	0.13	0.050	(0.075)	0.045	0.005
221	18.42	0.13	0.050	(0.074)	0.045	0.005
222	18.50	0.13	0.050	(0.074)	0.045	0.005
223	18.58	0.10	0.037	(0.074)	0.034	0.004
224	18.67	0.10	0.037	(0.073)	0.034	0.004
225	18.75	0.10	0.037	(0.073)	0.034	0.004
226	18.83	0.07	0.025	(0.072)	0.022	0.002
227	18.92	0.07	0.025	(0.072)	0.022	0.002
228	19.00	0.07	0.025	(0.072)	0.022	0.002
229	19.08	0.10	0.037	(0.071)	0.034	0.004
230	19.17	0.10	0.037	(0.071)	0.034	0.004
231	19.25	0.10	0.037	(0.071)	0.034	0.004
232	19.33	0.13	0.050	(0.070)	0.045	0.005
233	19.42	0.13	0.050	(0.070)	0.045	0.005
234	19.50	0.13	0.050	(0.070)	0.045	0.005
235	19.58	0.10	0.037	(0.069)	0.034	0.004
236	19.67	0.10	0.037	(0.069)	0.034	0.004
237	19.75	0.10	0.037	(0.069)	0.034	0.004
238	19.83	0.07	0.025	(0.069)	0.022	0.002
239	19.92	0.07	0.025	(0.068)	0.022	0.002

240	20.00	0.07	0.025	(0.068)	0.022	0.002
241	20.08	0.10	0.037	(0.068)	0.034	0.004
242	20.17	0.10	0.037	(0.067)	0.034	0.004
243	20.25	0.10	0.037	(0.067)	0.034	0.004
244	20.33	0.10	0.037	(0.067)	0.034	0.004
245	20.42	0.10	0.037	(0.066)	0.034	0.004
246	20.50	0.10	0.037	(0.066)	0.034	0.004
247	20.58	0.10	0.037	(0.066)	0.034	0.004
248	20.67	0.10	0.037	(0.066)	0.034	0.004
249	20.75	0.10	0.037	(0.065)	0.034	0.004
250	20.83	0.07	0.025	(0.065)	0.022	0.002
251	20.92	0.07	0.025	(0.065)	0.022	0.002
252	21.00	0.07	0.025	(0.065)	0.022	0.002
253	21.08	0.10	0.037	(0.064)	0.034	0.004
254	21.17	0.10	0.037	(0.064)	0.034	0.004
255	21.25	0.10	0.037	(0.064)	0.034	0.004
256	21.33	0.07	0.025	(0.064)	0.022	0.002
257	21.42	0.07	0.025	(0.063)	0.022	0.002
258	21.50	0.07	0.025	(0.063)	0.022	0.002
259	21.58	0.10	0.037	(0.063)	0.034	0.004
260	21.67	0.10	0.037	(0.063)	0.034	0.004
261	21.75	0.10	0.037	(0.062)	0.034	0.004
262	21.83	0.07	0.025	(0.062)	0.022	0.002
263	21.92	0.07	0.025	(0.062)	0.022	0.002
264	22.00	0.07	0.025	(0.062)	0.022	0.002
265	22.08	0.10	0.037	(0.062)	0.034	0.004
266	22.17	0.10	0.037	(0.061)	0.034	0.004
267	22.25	0.10	0.037	(0.061)	0.034	0.004
268	22.33	0.07	0.025	(0.061)	0.022	0.002
269	22.42	0.07	0.025	(0.061)	0.022	0.002
270	22.50	0.07	0.025	(0.061)	0.022	0.002
271	22.58	0.07	0.025	(0.060)	0.022	0.002
272	22.67	0.07	0.025	(0.060)	0.022	0.002
273	22.75	0.07	0.025	(0.060)	0.022	0.002
274	22.83	0.07	0.025	(0.060)	0.022	0.002
275	22.92	0.07	0.025	(0.060)	0.022	0.002
276	23.00	0.07	0.025	(0.060)	0.022	0.002
277	23.08	0.07	0.025	(0.060)	0.022	0.002
278	23.17	0.07	0.025	(0.059)	0.022	0.002
279	23.25	0.07	0.025	(0.059)	0.022	0.002
280	23.33	0.07	0.025	(0.059)	0.022	0.002
281	23.42	0.07	0.025	(0.059)	0.022	0.002
282	23.50	0.07	0.025	(0.059)	0.022	0.002
283	23.58	0.07	0.025	(0.059)	0.022	0.002
284	23.67	0.07	0.025	(0.059)	0.022	0.002
285	23.75	0.07	0.025	(0.059)	0.022	0.002
286	23.83	0.07	0.025	(0.059)	0.022	0.002
287	23.92	0.07	0.025	(0.059)	0.022	0.002
288	24.00	0.07	0.025	(0.059)	0.022	0.002

(Loss Rate Not Used)

Sum = 100.0 Sum = 16.7

Flood volume = Effective rainfall 1.39(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 6.0(Ac.Ft)
Total soil loss = 1.72(In)
Total soil loss = 7.446(Ac.Ft)
Total rainfall = 3.12(In)
Flood volume = 261612.8 Cubic Feet
Total soil loss = 324337.0 Cubic Feet

Peak flow rate of this hydrograph = 16.731(CFS)

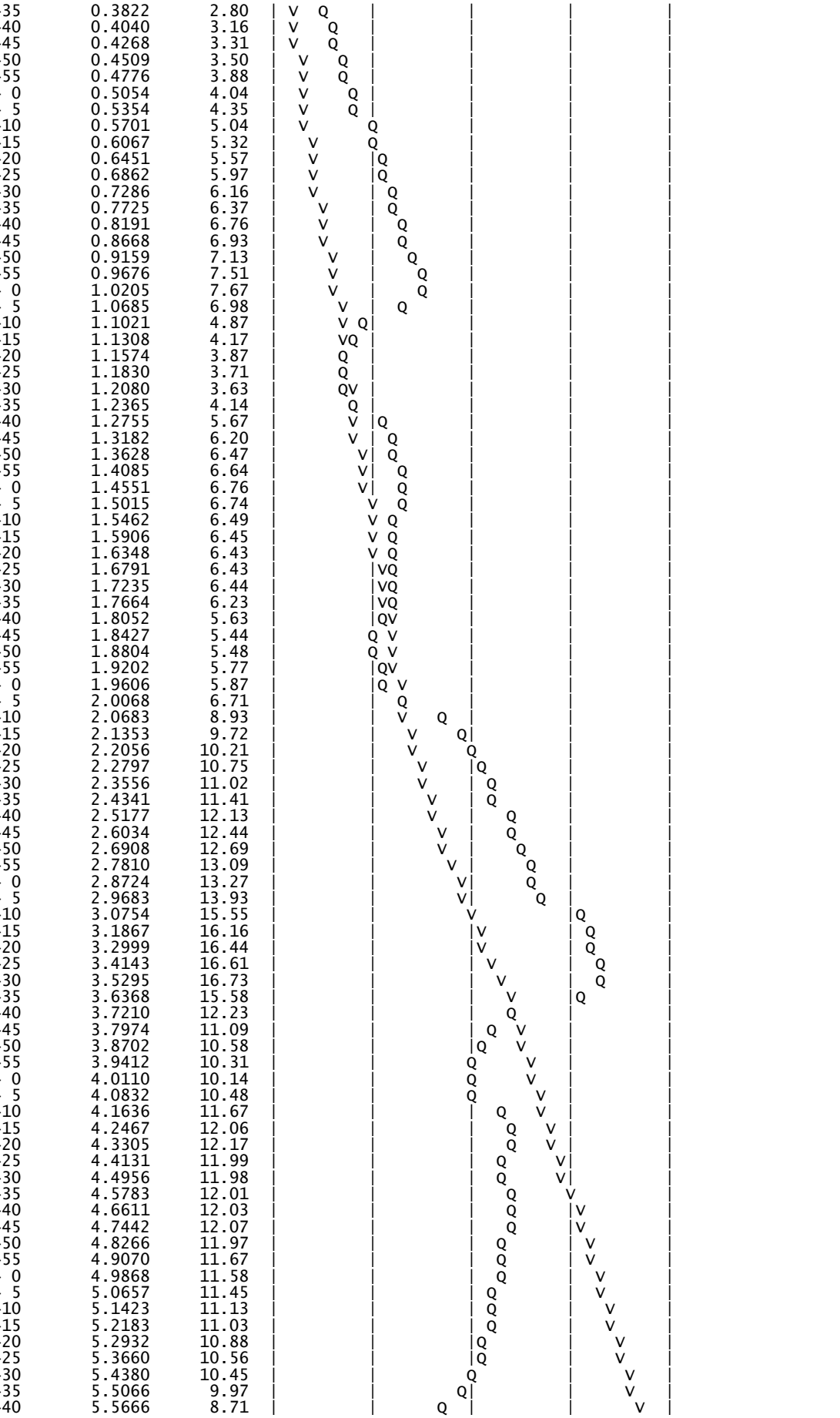
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24 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0002	0.02	Q	|	|	|	|
0+10	0.0007	0.08	Q	|	|	|	|
0+15	0.0015	0.11	Q	|	|	|	|
0+20	0.0023	0.13	Q	|	|	|	|
0+25	0.0035	0.16	Q	|	|	|	|
0+30	0.0047	0.18	Q	|	|	|	|
0+35	0.0060	0.19	Q	|	|	|	|
0+40	0.0073	0.19	Q	|	|	|	|
0+45	0.0086	0.19	Q	|	|	|	|
0+50	0.0100	0.21	Q	|	|	|	|
0+55	0.0117	0.24	Q	|	|	|	|
1+ 0	0.0134	0.25	Q	|	|	|	|
1+ 5	0.0150	0.24	Q	|	|	|	|
1+10	0.0165	0.21	Q	|	|	|	|
1+15	0.0179	0.20	Q	|	|	|	|
1+20	0.0193	0.20	Q	|	|	|	|

1+25	0.0207	0.20	Q	|	|	|	|
1+30	0.0220	0.20	Q	|	|	|	|
1+35	0.0234	0.20	Q	|	|	|	|
1+40	0.0247	0.20	Q	|	|	|	|
1+45	0.0261	0.20	Q	|	|	|	|
1+50	0.0275	0.21	Q	|	|	|	|
1+55	0.0291	0.24	Q	|	|	|	|
2+ 0	0.0309	0.25	Q	|	|	|	|
2+ 5	0.0326	0.25	Q	|	|	|	|
2+10	0.0344	0.26	Q	|	|	|	|
2+15	0.0361	0.26	Q	|	|	|	|
2+20	0.0379	0.26	Q	|	|	|	|
2+25	0.0397	0.26	Q	|	|	|	|
2+30	0.0415	0.26	Q	|	|	|	|
2+35	0.0434	0.27	Q	|	|	|	|
2+40	0.0455	0.30	Q	|	|	|	|
2+45	0.0476	0.31	Q	|	|	|	|
2+50	0.0498	0.32	Q	|	|	|	|
2+55	0.0520	0.32	Q	|	|	|	|
3+ 0	0.0543	0.32	Q	|	|	|	|
3+ 5	0.0565	0.32	Q	|	|	|	|
3+10	0.0587	0.32	Q	|	|	|	|
3+15	0.0610	0.33	Q	|	|	|	|
3+20	0.0632	0.33	Q	|	|	|	|
3+25	0.0655	0.33	Q	|	|	|	|
3+30	0.0677	0.33	Q	|	|	|	|
3+35	0.0699	0.33	Q	|	|	|	|
3+40	0.0722	0.33	Q	|	|	|	|
3+45	0.0744	0.33	Q	|	|	|	|
3+50	0.0767	0.34	Q	|	|	|	|
3+55	0.0793	0.37	Q	|	|	|	|
4+ 0	0.0819	0.38	Q	|	|	|	|
4+ 5	0.0845	0.38	Q	|	|	|	|
4+10	0.0872	0.39	Q	|	|	|	|
4+15	0.0899	0.39	Q	|	|	|	|
4+20	0.0926	0.40	Q	|	|	|	|
4+25	0.0956	0.43	Q	|	|	|	|
4+30	0.0986	0.44	Q	|	|	|	|
4+35	0.1017	0.45	Q	|	|	|	|
4+40	0.1048	0.45	Q	|	|	|	|
4+45	0.1080	0.45	Q	|	|	|	|
4+50	0.1112	0.47	Q	|	|	|	|
4+55	0.1146	0.50	Q	|	|	|	|
5+ 0	0.1181	0.51	VQ	|	|	|	|
5+ 5	0.1215	0.49	Q	|	|	|	|
5+10	0.1245	0.43	Q	|	|	|	|
5+15	0.1273	0.41	Q	|	|	|	|
5+20	0.1302	0.41	Q	|	|	|	|
5+25	0.1332	0.44	Q	|	|	|	|
5+30	0.1363	0.45	Q	|	|	|	|
5+35	0.1395	0.46	Q	|	|	|	|
5+40	0.1429	0.49	Q	|	|	|	|
5+45	0.1464	0.51	VQ	|	|	|	|
5+50	0.1499	0.51	VQ	|	|	|	|
5+55	0.1534	0.52	|Q	|	|	|	|
6+ 0	0.1570	0.52	|Q	|	|	|	|
6+ 5	0.1607	0.53	|Q	|	|	|	|
6+10	0.1645	0.56	|Q	|	|	|	|
6+15	0.1685	0.57	|Q	|	|	|	|
6+20	0.1725	0.58	|Q	|	|	|	|
6+25	0.1765	0.58	|Q	|	|	|	|
6+30	0.1805	0.58	|Q	|	|	|	|
6+35	0.1846	0.60	|Q	|	|	|	|
6+40	0.1889	0.63	|Q	|	|	|	|
6+45	0.1933	0.64	|Q	|	|	|	|
6+50	0.1978	0.64	|Q	|	|	|	|
6+55	0.2022	0.65	|Q	|	|	|	|
7+ 0	0.2067	0.65	|Q	|	|	|	|
7+ 5	0.2112	0.65	|Q	|	|	|	|
7+10	0.2156	0.65	|Q	|	|	|	|
7+15	0.2201	0.65	|Q	|	|	|	|
7+20	0.2247	0.66	|Q	|	|	|	|
7+25	0.2295	0.69	|Q	|	|	|	|
7+30	0.2343	0.70	|Q	|	|	|	|
7+35	0.2393	0.72	|Q	|	|	|	|
7+40	0.2445	0.75	|Q	|	|	|	|
7+45	0.2498	0.77	|Q	|	|	|	|
7+50	0.2555	0.84	|Q	|	|	|	|
7+55	0.2626	1.03	|VQ	|	|	|	|
8+ 0	0.2703	1.12	|VQ	|	|	|	|
8+ 5	0.2800	1.40	|VQ	|	|	|	|
8+10	0.2942	2.07	|V Q	|	|	|	|
8+15	0.3103	2.33	| V Q	|	|	|	|
8+20	0.3273	2.46	| V Q	|	|	|	|
8+25	0.3449	2.56	| V Q	|	|	|	|
8+30	0.3630	2.63	| V Q	|	|	|	|

8+35	0.3822	2.80	
8+40	0.4040	3.16	
8+45	0.4268	3.31	
8+50	0.4509	3.50	
8+55	0.4776	3.88	
9+ 0	0.5054	4.04	
9+ 5	0.5354	4.35	
9+10	0.5701	5.04	
9+15	0.6067	5.32	
9+20	0.6451	5.57	
9+25	0.6862	5.97	
9+30	0.7286	6.16	
9+35	0.7725	6.37	
9+40	0.8191	6.76	
9+45	0.8668	6.93	
9+50	0.9159	7.13	
9+55	0.9676	7.51	
10+ 0	1.0205	7.67	
10+ 5	1.0685	6.98	
10+10	1.1021	4.87	
10+15	1.1308	4.17	
10+20	1.1574	3.87	
10+25	1.1830	3.71	
10+30	1.2080	3.63	
10+35	1.2365	4.14	
10+40	1.2755	5.67	
10+45	1.3182	6.20	
10+50	1.3628	6.47	
10+55	1.4085	6.64	
11+ 0	1.4551	6.76	
11+ 5	1.5015	6.74	
11+10	1.5462	6.49	
11+15	1.5906	6.45	
11+20	1.6348	6.43	
11+25	1.6791	6.43	
11+30	1.7235	6.44	
11+35	1.7664	6.23	
11+40	1.8052	5.63	
11+45	1.8427	5.44	
11+50	1.8804	5.48	
11+55	1.9202	5.77	
12+ 0	1.9606	5.87	
12+ 5	2.0068	6.71	
12+10	2.0683	8.93	
12+15	2.1353	9.72	
12+20	2.2056	10.21	
12+25	2.2797	10.75	
12+30	2.3556	11.02	
12+35	2.4341	11.41	
12+40	2.5177	12.13	
12+45	2.6034	12.44	
12+50	2.6908	12.69	
12+55	2.7810	13.09	
13+ 0	2.8724	13.27	
13+ 5	2.9683	13.93	
13+10	3.0754	15.55	
13+15	3.1867	16.16	
13+20	3.2999	16.44	
13+25	3.4143	16.61	
13+30	3.5295	16.73	
13+35	3.6368	15.58	
13+40	3.7210	12.23	
13+45	3.7974	11.09	
13+50	3.8702	10.58	
13+55	3.9412	10.31	
14+ 0	4.0110	10.14	
14+ 5	4.0832	10.48	
14+10	4.1636	11.67	
14+15	4.2467	12.06	
14+20	4.3305	12.17	
14+25	4.4131	11.99	
14+30	4.4956	11.98	
14+35	4.5783	12.01	
14+40	4.6611	12.03	
14+45	4.7442	12.07	
14+50	4.8266	11.97	
14+55	4.9070	11.67	
15+ 0	4.9868	11.58	
15+ 5	5.0657	11.45	
15+10	5.1423	11.13	
15+15	5.2183	11.03	
15+20	5.2932	10.88	
15+25	5.3660	10.56	
15+30	5.4380	10.45	
15+35	5.5066	9.97	
15+40	5.5666	8.71	

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15+45       5.6236      8.28  |          |      Q   |          |       V   |
15+50       5.6794      8.10  |          |      Q   |          |       V   |
15+55       5.7345      8.00  |          |      Q   |          |        V  |
16+ 0       5.7892      7.95  |          |     Q    |          |        V  |
16+ 5       5.8347      6.60  |          |  Q       |          |        V  |
16+10       5.8550      2.94  |     Q    |          |          |        V  |
16+15       5.8663      1.65  |   Q      |          |          |         V |
16+20       5.8738      1.09  | Q        |          |          |         V |
16+25       5.8791      0.77  |Q         |          |          |         V |
16+30       5.8829      0.56  |Q         |          |          |         V |
16+35       5.8858      0.41  Q          |          |          |         V |
16+40       5.8878      0.29  Q          |          |          |         V |
16+45       5.8892      0.21  Q          |          |          |         V |
16+50       5.8906      0.20  Q          |          |          |         V |
16+55       5.8920      0.20  Q          |          |          |         V |
17+ 0       5.8933      0.20  Q          |          |          |         V |
17+ 5       5.8948      0.22  Q          |          |          |         V |
17+10       5.8968      0.28  Q          |          |          |         V |
17+15       5.8988      0.30  Q          |          |          |         V |
17+20       5.9010      0.31  Q          |          |          |         V |
17+25       5.9032      0.32  Q          |          |          |         V |
17+30       5.9054      0.32  Q          |          |          |         V |
17+35       5.9076      0.32  Q          |          |          |         V |
17+40       5.9098      0.32  Q          |          |          |         V |
17+45       5.9121      0.33  Q          |          |          |         V |
17+50       5.9142      0.31  Q          |          |          |         V |
17+55       5.9162      0.28  Q          |          |          |         V |
18+ 0       5.9181      0.27  Q          |          |          |         V |
18+ 5       5.9199      0.27  Q          |          |          |         V |
18+10       5.9217      0.26  Q          |          |          |         V |
18+15       5.9235      0.26  Q          |          |          |         V |
18+20       5.9253      0.26  Q          |          |          |         V |
18+25       5.9271      0.26  Q          |          |          |         V |
18+30       5.9289      0.26  Q          |          |          |         V |
18+35       5.9307      0.25  Q          |          |          |         V |
18+40       5.9322      0.22  Q          |          |          |         V |
18+45       5.9336      0.21  Q          |          |          |         V |
18+50       5.9349      0.19  Q          |          |          |         V |
18+55       5.9360      0.16  Q          |          |          |         V |
19+ 0       5.9370      0.14  Q          |          |          |         V |
19+ 5       5.9380      0.15  Q          |          |          |         V |
19+10       5.9392      0.18  Q          |          |          |         V |
19+15       5.9405      0.19  Q          |          |          |         V |
19+20       5.9419      0.20  Q          |          |          |         V |
19+25       5.9435      0.23  Q          |          |          |         V |
19+30       5.9452      0.25  Q          |          |          |         V |
19+35       5.9469      0.24  Q          |          |          |         V |
19+40       5.9483      0.21  Q          |          |          |         V |
19+45       5.9497      0.20  Q          |          |          |         V |
19+50       5.9510      0.19  Q          |          |          |         V |
19+55       5.9521      0.16  Q          |          |          |         V |
20+ 0       5.9531      0.14  Q          |          |          |         V |
20+ 5       5.9542      0.15  Q          |          |          |         V |
20+10       5.9554      0.18  Q          |          |          |         V |
20+15       5.9567      0.19  Q          |          |          |         V |
20+20       5.9580      0.19  Q          |          |          |         V |
20+25       5.9593      0.19  Q          |          |          |         V |
20+30       5.9606      0.19  Q          |          |          |         V |
20+35       5.9619      0.19  Q          |          |          |         V |
20+40       5.9633      0.19  Q          |          |          |         V |
20+45       5.9646      0.20  Q          |          |          |         V |
20+50       5.9659      0.18  Q          |          |          |         V |
20+55       5.9670      0.15  Q          |          |          |         V |
21+ 0       5.9679      0.14  Q          |          |          |         V |
21+ 5       5.9690      0.15  Q          |          |          |         V |
21+10       5.9702      0.18  Q          |          |          |         V |
21+15       5.9715      0.19  Q          |          |          |         V |
21+20       5.9727      0.18  Q          |          |          |         V |
21+25       5.9737      0.15  Q          |          |          |         V |
21+30       5.9747      0.14  Q          |          |          |         V |
21+35       5.9757      0.15  Q          |          |          |         V |
21+40       5.9769      0.18  Q          |          |          |         V |
21+45       5.9782      0.19  Q          |          |          |         V |
21+50       5.9794      0.18  Q          |          |          |         V |
21+55       5.9804      0.15  Q          |          |          |         V |
22+ 0       5.9814      0.14  Q          |          |          |         V |
22+ 5       5.9824      0.15  Q          |          |          |         V |
22+10       5.9836      0.18  Q          |          |          |         V |
22+15       5.9849      0.19  Q          |          |          |         V |
22+20       5.9861      0.18  Q          |          |          |         V |
22+25       5.9872      0.15  Q          |          |          |         V |
22+30       5.9881      0.14  Q          |          |          |         V |
22+35       5.9891      0.14  Q          |          |          |         V |
22+40       5.9900      0.13  Q          |          |          |         V |
22+45       5.9909      0.13  Q          |          |          |         V |
22+50       5.9918      0.13  Q          |          |          |         V |
```

```
   22+55       5.9927      0.13  Q          |          |          |         v|
   23+ 0       5.9936      0.13  Q          |          |          |         v|
   23+ 5       5.9945      0.13  Q          |          |          |         v|
   23+10       5.9954      0.13  Q          |          |          |         v|
   23+15       5.9963      0.13  Q          |          |          |         v|
   23+20       5.9972      0.13  Q          |          |          |         v|
   23+25       5.9981      0.13  Q          |          |          |         v|
   23+30       5.9990      0.13  Q          |          |          |         v|
   23+35       5.9999      0.13  Q          |          |          |         v|
   23+40       6.0008      0.13  Q          |          |          |         v|
   23+45       6.0017      0.13  Q          |          |          |         v|
   23+50       6.0026      0.13  Q          |          |          |         v|
   23+55       6.0035      0.13  Q          |          |          |         v|
   24+ 0       6.0044      0.13  Q          |          |          |         v|
   24+ 5       6.0051      0.11  Q          |          |          |         v|
   24+10       6.0054      0.05  Q          |          |          |         v|
   24+15       6.0056      0.02  Q          |          |          |         v|
   24+20       6.0057      0.01  Q          |          |          |         v|
   24+25       6.0057      0.01  Q          |          |          |         v|
   24+30       6.0058      0.01  Q          |          |          |         v|
   24+35       6.0058      0.00  Q          |          |          |         v|
   24+40       6.0058      0.00  Q          |          |          |          V
-------------------------------------------------------------------------
```

```
       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/18/24 File: ex21001100.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2127.00(Ft.)
Length along longest watercourse measured to centroid =    1064.00(Ft.)
Length along longest watercourse =      0.403 Mi.
Length along longest watercourse measured to centroid =      0.202 Mi.
Difference in elevation =     160.00(Ft.)
Slope along watercourse =    397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.089 Hr.
Lag time =     5.34 Min.
25% of lag time =     1.33 Min.
40% of lag time =     2.13 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           0.50                 25.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           1.30                 67.34

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    1.300(In)
Areal adjustment factor =   99.95 %
Adjusted average point rain =    1.299(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           91.00         0.000
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  91.0      0.117     0.000        0.117       1.000      0.117
                                                 Sum (F) =   0.117
Area averaged mean soil loss (F) (In/Hr) =  0.117
Minimum soil loss rate ((In/Hr)) =  0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time	(Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.515	0.117	(0.463)	0.398
2	0.17	4.20	0.655	0.117	(0.589)	0.538
3	0.25	4.40	0.686	0.117	(0.617)	0.569
4	0.33	4.80	0.748	0.117	(0.674)	0.631
5	0.42	5.20	0.811	0.117	(0.730)	0.694
6	0.50	6.20	0.967	0.117	(0.870)	0.850
7	0.58	6.80	1.060	0.117	(0.954)	0.943
8	0.67	8.80	1.372	0.117	(1.235)	1.255
9	0.75	13.90	2.167	0.117	(1.951)	2.050
10	0.83	31.40	4.896	0.117	(4.406)	4.779
11	0.92	7.20	1.123	0.117	(1.010)	1.006
12	1.00	3.80	0.593	0.117	(0.533)	0.476
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	14.2

Flood volume = Effective rainfall 1.18(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 5.1(Ac.Ft)
Total soil loss = 0.12(In)
Total soil loss = 0.505(Ac.Ft)
Total rainfall = 1.30(In)
Flood volume = 222329.5 Cubic Feet
Total soil loss = 22000.0 Cubic Feet

Peak flow rate of this hydrograph = 155.539(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	50.0	100.0	150.0	200.0
0+ 5	0.0247	3.59	Q				
0+10	0.1264	14.76	V Q				
0+15	0.2779	22.01	| V Q				
0+20	0.4578	26.11	| V Q				
0+25	0.6639	29.93	| Q				
0+30	0.9010	34.43	| QV				
0+35	1.1806	40.59	| QV				
0+40	1.5104	47.89	| Q|V				
0+45	1.9567	64.80	| Q V				
0+50	2.7343	112.91	| | VQ				
0+55	3.8055	155.54	| | | V|Q				
1+ 0	4.3884	84.63	| | Q | | V				
1+ 5	4.7136	47.22	| Q| | | V				
1+10	4.8772	23.75	| Q | | | V				
1+15	4.9742	14.08	| Q | | | V				
1+20	5.0351	8.85	|Q | | | V|				
1+25	5.0730	5.50	|Q | | | V|				
1+30	5.0969	3.47	Q | | | V|				
1+35	5.1023	0.79	Q | | | V|				
1+40	5.1040	0.24	Q | | | V				

```
        U n i t   H y d r o g r a p h   A n a l y s i s

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                Study date  04/18/24 File: ex21003100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2127.00(Ft.)
Length along longest watercourse measured to centroid =    1064.00(Ft.)
Length along longest watercourse =      0.403 Mi.
Length along longest watercourse measured to centroid =      0.202 Mi.
Difference in elevation =     160.00(Ft.)
Slope along watercourse =    397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.089 Hr.
Lag time =     5.34 Min.
25% of lag time =     1.33 Min.
40% of lag time =     2.13 Min.
Unit time =     5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           0.80                 41.44

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           2.00                103.60

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    0.800(In)
Area Averaged 100-Year Rainfall =    2.000(In)

Point rain (area averaged) =    2.000(In)
Areal adjustment factor =   99.98 %
Adjusted average point rain =    2.000(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           91.00         0.000
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  91.0      0.117     0.000        0.117       1.000      0.117
                                                 Sum (F) =   0.117
Area averaged mean soil loss (F) (In/Hr) =  0.117
Minimum soil loss rate ((In/Hr)) =  0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000 Sum=	52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.312	0.117	(0.281)	0.195
2	0.17	1.30	0.312	0.117	(0.281)	0.195
3	0.25	1.10	0.264	0.117	(0.238)	0.147
4	0.33	1.50	0.360	0.117	(0.324)	0.243
5	0.42	1.50	0.360	0.117	(0.324)	0.243
6	0.50	1.80	0.432	0.117	(0.389)	0.315
7	0.58	1.50	0.360	0.117	(0.324)	0.243
8	0.67	1.80	0.432	0.117	(0.389)	0.315
9	0.75	1.80	0.432	0.117	(0.389)	0.315
10	0.83	1.50	0.360	0.117	(0.324)	0.243
11	0.92	1.60	0.384	0.117	(0.346)	0.267
12	1.00	1.80	0.432	0.117	(0.389)	0.315
13	1.08	2.20	0.528	0.117	(0.475)	0.411
14	1.17	2.20	0.528	0.117	(0.475)	0.411
15	1.25	2.20	0.528	0.117	(0.475)	0.411
16	1.33	2.00	0.480	0.117	(0.432)	0.363
17	1.42	2.60	0.624	0.117	(0.561)	0.507
18	1.50	2.70	0.648	0.117	(0.583)	0.531
19	1.58	2.40	0.576	0.117	(0.518)	0.459
20	1.67	2.70	0.648	0.117	(0.583)	0.531
21	1.75	3.30	0.792	0.117	(0.713)	0.675
22	1.83	3.10	0.744	0.117	(0.669)	0.627
23	1.92	2.90	0.696	0.117	(0.626)	0.579
24	2.00	3.00	0.720	0.117	(0.648)	0.603
25	2.08	3.10	0.744	0.117	(0.669)	0.627
26	2.17	4.20	1.008	0.117	(0.907)	0.891
27	2.25	5.00	1.200	0.117	(1.080)	1.083
28	2.33	3.50	0.840	0.117	(0.756)	0.723
29	2.42	6.80	1.632	0.117	(1.468)	1.515
30	2.50	7.30	1.752	0.117	(1.576)	1.635
31	2.58	8.20	1.968	0.117	(1.771)	1.851
32	2.67	5.90	1.416	0.117	(1.274)	1.299
33	2.75	2.00	0.480	0.117	(0.432)	0.363
34	2.83	1.80	0.432	0.117	(0.389)	0.315
35	2.92	1.80	0.432	0.117	(0.389)	0.315
36	3.00	0.60	0.144	0.117	(0.130)	0.027
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	19.8

Flood volume = Effective rainfall 1.65(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 7.1(Ac.Ft)
Total soil loss = 0.35(In)
Total soil loss = 1.515(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 309982.8 Cubic Feet
Total soil loss = 65999.9 Cubic Feet

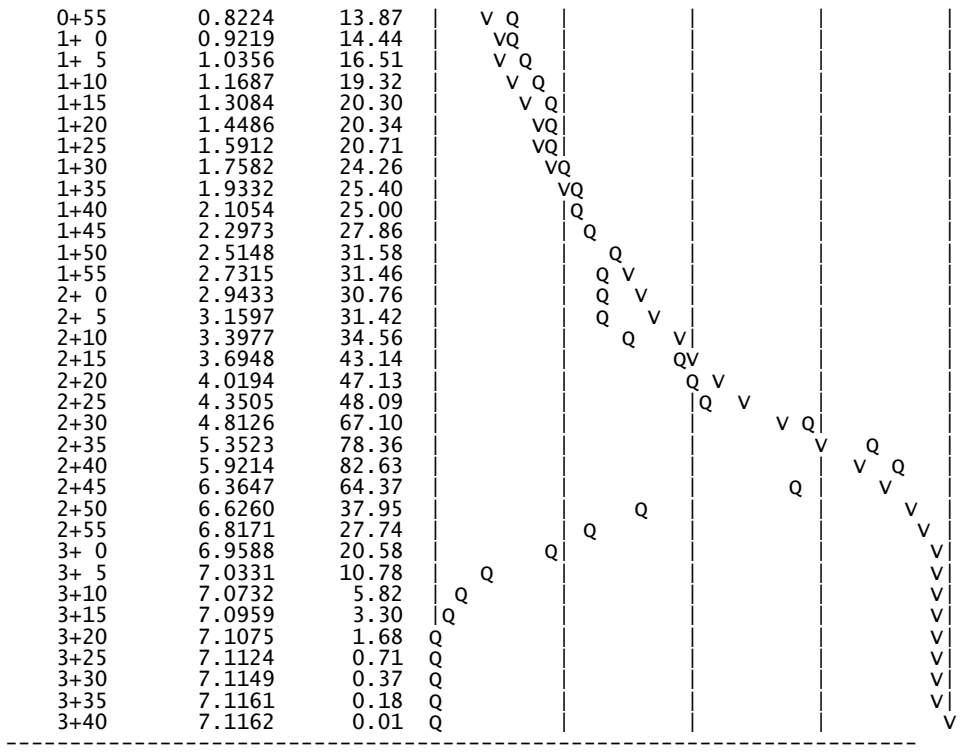
Peak flow rate of this hydrograph = 82.628(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	22.5	45.0	67.5	90.0
0+ 5	0.0121	1.76	Q	|	|	|	|
0+10	0.0577	6.62	V Q	|	|	|	|
0+15	0.1120	7.88	V Q	|	|	|	|
0+20	0.1692	8.31	V Q	|	|	|	|
0+25	0.2430	10.71	|V Q	|	|	|	|
0+30	0.3277	12.29	|V Q	|	|	|	|
0+35	0.4233	13.89	| V Q	|	|	|	|
0+40	0.5172	13.63	| V Q	|	|	|	|
0+45	0.6223	15.27	| V Q	|	|	|	|
0+50	0.7269	15.19	| V Q	|	|	|	|



0+55	0.8224	13.87	
1+ 0	0.9219	14.44	
1+ 5	1.0356	16.51	
1+10	1.1687	19.32	
1+15	1.3084	20.30	
1+20	1.4486	20.34	
1+25	1.5912	20.71	
1+30	1.7582	24.26	
1+35	1.9332	25.40	
1+40	2.1054	25.00	
1+45	2.2973	27.86	
1+50	2.5148	31.58	
1+55	2.7315	31.46	
2+ 0	2.9433	30.76	
2+ 5	3.1597	31.42	
2+10	3.3977	34.56	
2+15	3.6948	43.14	
2+20	4.0194	47.13	
2+25	4.3505	48.09	
2+30	4.8126	67.10	
2+35	5.3523	78.36	
2+40	5.9214	82.63	
2+45	6.3647	64.37	
2+50	6.6260	37.95	
2+55	6.8171	27.74	
3+ 0	6.9588	20.58	
3+ 5	7.0331	10.78	
3+10	7.0732	5.82	
3+15	7.0959	3.30	
3+20	7.1075	1.68	
3+25	7.1124	0.71	
3+30	7.1149	0.37	
3+35	7.1161	0.18	
3+40	7.1162	0.01	

```
        U n i t   H y d r o g r a p h   A n a l y s i s

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               Study date  04/18/24 File: ex21006100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2127.00(Ft.)
Length along longest watercourse measured to centroid =    1064.00(Ft.)
Length along longest watercourse =      0.403 Mi.
Length along longest watercourse measured to centroid =      0.202 Mi.
Difference in elevation =     160.00(Ft.)
Slope along watercourse =    397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.089 Hr.
Lag time =     5.34 Min.
25% of lag time =     1.33 Min.
40% of lag time =     2.13 Min.
Unit time =     5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           1.10                 56.98

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           3.00                155.40

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    1.100(In)
Area Averaged 100-Year Rainfall =    3.000(In)

Point rain (area averaged) =    3.000(In)
Areal adjustment factor =   99.98 %
Adjusted average point rain =    2.999(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           91.00         0.000
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  91.0      0.117     0.000        0.117       1.000      0.117
                                                 Sum (F) =   0.117
Area averaged mean soil loss (F) (In/Hr) =  0.117
Minimum soil loss rate ((In/Hr)) =  0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	93.693	17.279		9.021
2	0.167	187.386	47.711		24.907
3	0.250	281.078	16.693		8.714
4	0.333	374.771	7.417		3.872
5	0.417	468.464	4.247		2.217
6	0.500	562.157	2.744		1.432
7	0.583	655.849	1.804		0.942
8	0.667	749.542	1.132		0.591
9	0.750	843.235	0.973		0.508
			Sum = 100.000	Sum=	52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.180	0.117	(0.162)	0.063
2	0.17	0.60	0.216	0.117	(0.194)	0.099
3	0.25	0.60	0.216	0.117	(0.194)	0.099
4	0.33	0.60	0.216	0.117	(0.194)	0.099
5	0.42	0.60	0.216	0.117	(0.194)	0.099
6	0.50	0.70	0.252	0.117	(0.227)	0.135
7	0.58	0.70	0.252	0.117	(0.227)	0.135
8	0.67	0.70	0.252	0.117	(0.227)	0.135
9	0.75	0.70	0.252	0.117	(0.227)	0.135
10	0.83	0.70	0.252	0.117	(0.227)	0.135
11	0.92	0.70	0.252	0.117	(0.227)	0.135
12	1.00	0.80	0.288	0.117	(0.259)	0.171
13	1.08	0.80	0.288	0.117	(0.259)	0.171
14	1.17	0.80	0.288	0.117	(0.259)	0.171
15	1.25	0.80	0.288	0.117	(0.259)	0.171
16	1.33	0.80	0.288	0.117	(0.259)	0.171
17	1.42	0.80	0.288	0.117	(0.259)	0.171
18	1.50	0.80	0.288	0.117	(0.259)	0.171
19	1.58	0.80	0.288	0.117	(0.259)	0.171
20	1.67	0.80	0.288	0.117	(0.259)	0.171
21	1.75	0.80	0.288	0.117	(0.259)	0.171
22	1.83	0.80	0.288	0.117	(0.259)	0.171
23	1.92	0.80	0.288	0.117	(0.259)	0.171
24	2.00	0.90	0.324	0.117	(0.292)	0.207
25	2.08	0.80	0.288	0.117	(0.259)	0.171
26	2.17	0.90	0.324	0.117	(0.292)	0.207
27	2.25	0.90	0.324	0.117	(0.292)	0.207
28	2.33	0.90	0.324	0.117	(0.292)	0.207
29	2.42	0.90	0.324	0.117	(0.292)	0.207
30	2.50	0.90	0.324	0.117	(0.292)	0.207
31	2.58	0.90	0.324	0.117	(0.292)	0.207
32	2.67	0.90	0.324	0.117	(0.292)	0.207
33	2.75	1.00	0.360	0.117	(0.324)	0.243
34	2.83	1.00	0.360	0.117	(0.324)	0.243
35	2.92	1.00	0.360	0.117	(0.324)	0.243
36	3.00	1.00	0.360	0.117	(0.324)	0.243
37	3.08	1.00	0.360	0.117	(0.324)	0.243
38	3.17	1.10	0.396	0.117	(0.356)	0.279
39	3.25	1.10	0.396	0.117	(0.356)	0.279
40	3.33	1.10	0.396	0.117	(0.356)	0.279
41	3.42	1.20	0.432	0.117	(0.389)	0.315
42	3.50	1.30	0.468	0.117	(0.421)	0.351
43	3.58	1.40	0.504	0.117	(0.454)	0.387
44	3.67	1.40	0.504	0.117	(0.454)	0.387
45	3.75	1.50	0.540	0.117	(0.486)	0.423
46	3.83	1.50	0.540	0.117	(0.486)	0.423
47	3.92	1.60	0.576	0.117	(0.518)	0.459
48	4.00	1.60	0.576	0.117	(0.518)	0.459
49	4.08	1.70	0.612	0.117	(0.551)	0.495
50	4.17	1.80	0.648	0.117	(0.583)	0.531
51	4.25	1.90	0.684	0.117	(0.615)	0.567
52	4.33	2.00	0.720	0.117	(0.648)	0.603
53	4.42	2.10	0.756	0.117	(0.680)	0.639
54	4.50	2.10	0.756	0.117	(0.680)	0.639
55	4.58	2.20	0.792	0.117	(0.713)	0.675
56	4.67	2.30	0.828	0.117	(0.745)	0.711
57	4.75	2.40	0.864	0.117	(0.777)	0.747
58	4.83	2.40	0.864	0.117	(0.777)	0.747
59	4.92	2.50	0.900	0.117	(0.810)	0.783
60	5.00	2.60	0.936	0.117	(0.842)	0.819
61	5.08	3.10	1.116	0.117	(1.004)	0.999
62	5.17	3.60	1.296	0.117	(1.166)	1.179
63	5.25	3.90	1.404	0.117	(1.263)	1.287
64	5.33	4.20	1.512	0.117	(1.361)	1.395
65	5.42	4.70	1.692	0.117	(1.523)	1.575
66	5.50	5.60	2.016	0.117	(1.814)	1.899
67	5.58	1.90	0.684	0.117	(0.615)	0.567

68	5.67	0.90	0.324	0.117	(0.292)	0.207
69	5.75	0.60	0.216	0.117	(0.194)	0.099
70	5.83	0.50	0.180	0.117	(0.162)	0.063
71	5.92	0.30	0.108	(0.117)	0.097	0.011
72	6.00	0.20	0.072	(0.117)	0.065	0.007

(Loss Rate Not Used)

Sum = 100.0 Sum = 27.6

Flood volume = Effective rainfall 2.30(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 9.9(Ac.Ft)
Total soil loss = 0.70(In)
Total soil loss = 3.004(Ac.Ft)
Total rainfall = 3.00(In)
Flood volume = 433130.3 Cubic Feet
Total soil loss = 130871.2 Cubic Feet

Peak flow rate of this hydrograph = 79.183(CFS)

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6 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	20.0	40.0	60.0	80.0
0+ 5	0.0039	0.57	Q	|	|	|	|
0+10	0.0209	2.46	VQ	|	|	|	|
0+15	0.0478	3.91	VQ	|	|	|	|
0+20	0.0785	4.47	V Q	|	|	|	|
0+25	0.1112	4.75	V Q	|	|	|	|
0+30	0.1473	5.24	V Q	|	|	|	|
0+35	0.1903	6.25	V Q	|	|	|	|
0+40	0.2360	6.63	V Q	|	|	|	|
0+45	0.2830	6.83	|V Q	|	|	|	|
0+50	0.3307	6.92	|V Q	|	|	|	|
0+55	0.3788	6.98	|V Q	|	|	|	|
1+ 0	0.4293	7.33	|V Q	|	|	|	|
1+ 5	0.4861	8.25	|V Q	|	|	|	|
1+10	0.5452	8.58	| V Q	|	|	|	|
1+15	0.6053	8.72	| V Q	|	|	|	|
1+20	0.6659	8.80	| V Q	|	|	|	|
1+25	0.7269	8.86	| V Q	|	|	|	|
1+30	0.7882	8.89	| VQ	|	|	|	|
1+35	0.8495	8.91	| VQ	|	|	|	|
1+40	0.9110	8.93	| VQ	|	|	|	|
1+45	0.9725	8.93	| VQ	|	|	|	|
1+50	1.0340	8.93	| Q	|	|	|	|
1+55	1.0955	8.93	| Q	|	|	|	|
2+ 0	1.1592	9.25	| Q	|	|	|	|
2+ 5	1.2269	9.83	| Q	|	|	|	|
2+10	1.2928	9.57	| QV	|	|	|	|
2+15	1.3637	10.29	| Q	|	|	|	|
2+20	1.4363	10.54	| Q	|	|	|	|
2+25	1.5097	10.66	| QV	|	|	|	|
2+30	1.5835	10.72	| QV	|	|	|	|
2+35	1.6576	10.76	| QV	|	|	|	|
2+40	1.7319	10.79	| QV	|	|	|	|
2+45	1.8084	11.12	| Q V	|	|	|	|
2+50	1.8913	12.03	| QV	|	|	|	|
2+55	1.9763	12.34	| QV	|	|	|	|
3+ 0	2.0623	12.48	| Q V	|	|	|	|
3+ 5	2.1488	12.56	| Q V	|	|	|	|
3+10	2.2379	12.94	| Q V|	|	|	|	|
3+15	2.3334	13.87	| Q V|	|	|	|	|
3+20	2.4313	14.21	| Q V|	|	|	|	|
3+25	2.5325	14.69	| Q V	|	|	|	|
3+30	2.6426	15.99	| Q V	|	|	|	|
3+35	2.7636	17.58	| Q |V	|	|	|	|
3+40	2.8942	18.96	| Q|V	|	|	|	|
3+45	3.0309	19.84	| Q| V	|	|	|	|
3+50	3.1757	21.03	| Q V	|	|	|	|
3+55	3.3260	21.83	| Q V	|	|	|	|
4+ 0	3.4843	22.97	| |Q V	|	|	|	|
4+ 5	3.6480	23.77	| |Q V	|	|	|	|
4+10	3.8216	25.22	| | Q V	|	|	|	|
4+15	4.0068	26.89	| | Q V	|	|	|	|
4+20	4.2040	28.63	| | Q V	|	|	|	|
4+25	4.4137	30.44	| | Q V	|	|	|	|
4+30	4.6337	31.94	| | Q V	|	|	|	|
4+35	4.8603	32.91	| | Q V|	|	|	|	|
4+40	5.0976	34.45	| | Q V	|	|	|	|
4+45	5.3469	36.19	| | Q |V	|	|	|	|
4+50	5.6063	37.67	| | Q| V	|	|	|	|
4+55	5.8722	38.60	| | Q| V	|	|	|	|
5+ 0	6.1486	40.13	| | Q V	|	|	|	|

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    5+ 5       6.4458     43.15  |          |          |Q   V     |          |
    5+10       6.7889     49.82  |          |          |   Q  V   |          |
    5+15       7.1824     57.14  |          |          |      Q   |          |
    5+20       7.6180     63.25  |          |          |         VQ          |
    5+25       8.0981     69.70  |          |          |          | V Q      |
    5+30       8.6434     79.18  |          |          |          |   V     Q|
    5+35       9.1801     77.93  |          |          |          |     V Q  |
    5+40       9.4949     45.70  |          |          | Q        |       V  |
    5+45       9.6757     26.26  |          |  Q       |          |       V  |
    5+50       9.7871     16.18  |        Q |          |          |        V |
    5+55       9.8579     10.27  |      Q   |          |          |        V |
    6+ 0       9.8990      5.97  |  Q       |          |          |        V |
    6+ 5       9.9230      3.49  |Q         |          |          |        V |
    6+10       9.9360      1.88  Q          |          |          |        V |
    6+15       9.9404      0.65  Q          |          |          |        V |
    6+20       9.9422      0.25  Q          |          |          |        V |
    6+25       9.9429      0.11  Q          |          |          |        V |
    6+30       9.9432      0.05  Q          |          |          |        V |
    6+35       9.9433      0.01  Q          |          |          |        V |
    6+40       9.9433      0.00  Q          |          |          |        V |
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: ex210024100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2127.00(Ft.)
Length along longest watercourse measured to centroid = 1064.00(Ft.)
Length along longest watercourse = 0.403 Mi.
Length along longest watercourse measured to centroid = 0.202 Mi.
Difference in elevation = 160.00(Ft.)
Slope along watercourse = 397.1791 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.089 Hr.
Lag time = 5.34 Min.
25% of lag time = 1.33 Min.
40% of lag time = 2.13 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	1.80	93.24

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	5.00	259.00

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 5.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 4.999(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	91.00	0.000

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	93.693	17.279	9.021
2	0.167	187.386	47.711	24.907
3	0.250	281.078	16.693	8.714
4	0.333	374.771	7.417	3.872
5	0.417	468.464	4.247	2.217
6	0.500	562.157	2.744	1.432
7	0.583	655.849	1.804	0.942
8	0.667	749.542	1.132	0.591
9	0.750	843.235	0.973	0.508
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.040	(0.207)	0.036	0.004
2	0.17	0.07	0.040	(0.207)	0.036	0.004
3	0.25	0.07	0.040	(0.206)	0.036	0.004
4	0.33	0.10	0.060	(0.205)	0.054	0.006
5	0.42	0.10	0.060	(0.204)	0.054	0.006
6	0.50	0.10	0.060	(0.203)	0.054	0.006
7	0.58	0.10	0.060	(0.203)	0.054	0.006
8	0.67	0.10	0.060	(0.202)	0.054	0.006
9	0.75	0.10	0.060	(0.201)	0.054	0.006
10	0.83	0.13	0.080	(0.200)	0.072	0.008
11	0.92	0.13	0.080	(0.199)	0.072	0.008
12	1.00	0.13	0.080	(0.199)	0.072	0.008
13	1.08	0.10	0.060	(0.198)	0.054	0.006
14	1.17	0.10	0.060	(0.197)	0.054	0.006
15	1.25	0.10	0.060	(0.196)	0.054	0.006
16	1.33	0.10	0.060	(0.196)	0.054	0.006
17	1.42	0.10	0.060	(0.195)	0.054	0.006
18	1.50	0.10	0.060	(0.194)	0.054	0.006
19	1.58	0.10	0.060	(0.193)	0.054	0.006
20	1.67	0.10	0.060	(0.192)	0.054	0.006
21	1.75	0.10	0.060	(0.192)	0.054	0.006
22	1.83	0.13	0.080	(0.191)	0.072	0.008
23	1.92	0.13	0.080	(0.190)	0.072	0.008
24	2.00	0.13	0.080	(0.189)	0.072	0.008
25	2.08	0.13	0.080	(0.189)	0.072	0.008
26	2.17	0.13	0.080	(0.188)	0.072	0.008
27	2.25	0.13	0.080	(0.187)	0.072	0.008
28	2.33	0.13	0.080	(0.186)	0.072	0.008
29	2.42	0.13	0.080	(0.186)	0.072	0.008
30	2.50	0.13	0.080	(0.185)	0.072	0.008
31	2.58	0.17	0.100	(0.184)	0.090	0.010
32	2.67	0.17	0.100	(0.183)	0.090	0.010
33	2.75	0.17	0.100	(0.183)	0.090	0.010
34	2.83	0.17	0.100	(0.182)	0.090	0.010
35	2.92	0.17	0.100	(0.181)	0.090	0.010
36	3.00	0.17	0.100	(0.180)	0.090	0.010
37	3.08	0.17	0.100	(0.180)	0.090	0.010
38	3.17	0.17	0.100	(0.179)	0.090	0.010
39	3.25	0.17	0.100	(0.178)	0.090	0.010
40	3.33	0.17	0.100	(0.177)	0.090	0.010
41	3.42	0.17	0.100	(0.177)	0.090	0.010
42	3.50	0.17	0.100	(0.176)	0.090	0.010
43	3.58	0.17	0.100	(0.175)	0.090	0.010
44	3.67	0.17	0.100	(0.174)	0.090	0.010
45	3.75	0.17	0.100	(0.174)	0.090	0.010
46	3.83	0.20	0.120	(0.173)	0.108	0.012
47	3.92	0.20	0.120	(0.172)	0.108	0.012
48	4.00	0.20	0.120	(0.171)	0.108	0.012
49	4.08	0.20	0.120	(0.171)	0.108	0.012
50	4.17	0.20	0.120	(0.170)	0.108	0.012
51	4.25	0.20	0.120	(0.169)	0.108	0.012
52	4.33	0.23	0.140	(0.169)	0.126	0.014
53	4.42	0.23	0.140	(0.168)	0.126	0.014
54	4.50	0.23	0.140	(0.167)	0.126	0.014
55	4.58	0.23	0.140	(0.166)	0.126	0.014
56	4.67	0.23	0.140	(0.166)	0.126	0.014
57	4.75	0.23	0.140	(0.165)	0.126	0.014
58	4.83	0.27	0.160	(0.164)	0.144	0.016
59	4.92	0.27	0.160	(0.164)	0.144	0.016
60	5.00	0.27	0.160	(0.163)	0.144	0.016
61	5.08	0.20	0.120	(0.162)	0.108	0.012
62	5.17	0.20	0.120	(0.161)	0.108	0.012
63	5.25	0.20	0.120	(0.161)	0.108	0.012
64	5.33	0.23	0.140	(0.160)	0.126	0.014
65	5.42	0.23	0.140	(0.159)	0.126	0.014
66	5.50	0.23	0.140	(0.159)	0.126	0.014
67	5.58	0.27	0.160	(0.158)	0.144	0.016

68	5.67	0.27	0.160	(	0.157)	0.144	0.016
69	5.75	0.27	0.160	(	0.157)	0.144	0.016
70	5.83	0.27	0.160	(	0.156)	0.144	0.016
71	5.92	0.27	0.160	(	0.155)	0.144	0.016
72	6.00	0.27	0.160	(	0.154)	0.144	0.016
73	6.08	0.30	0.180		0.154	(0.162)	0.026
74	6.17	0.30	0.180		0.153	(0.162)	0.027
75	6.25	0.30	0.180		0.152	(0.162)	0.028
76	6.33	0.30	0.180		0.152	(0.162)	0.028
77	6.42	0.30	0.180		0.151	(0.162)	0.029
78	6.50	0.30	0.180		0.150	(0.162)	0.030
79	6.58	0.33	0.200		0.150	(0.180)	0.050
80	6.67	0.33	0.200		0.149	(0.180)	0.051
81	6.75	0.33	0.200		0.148	(0.180)	0.052
82	6.83	0.33	0.200		0.148	(0.180)	0.052
83	6.92	0.33	0.200		0.147	(0.180)	0.053
84	7.00	0.33	0.200		0.146	(0.180)	0.054
85	7.08	0.33	0.200		0.146	(0.180)	0.054
86	7.17	0.33	0.200		0.145	(0.180)	0.055
87	7.25	0.33	0.200		0.144	(0.180)	0.056
88	7.33	0.37	0.220		0.144	(0.198)	0.076
89	7.42	0.37	0.220		0.143	(0.198)	0.077
90	7.50	0.37	0.220		0.142	(0.198)	0.078
91	7.58	0.40	0.240		0.142	(0.216)	0.098
92	7.67	0.40	0.240		0.141	(0.216)	0.099
93	7.75	0.40	0.240		0.140	(0.216)	0.100
94	7.83	0.43	0.260		0.140	(0.234)	0.120
95	7.92	0.43	0.260		0.139	(0.234)	0.121
96	8.00	0.43	0.260		0.138	(0.234)	0.122
97	8.08	0.50	0.300		0.138	(0.270)	0.162
98	8.17	0.50	0.300		0.137	(0.270)	0.163
99	8.25	0.50	0.300		0.137	(0.270)	0.163
100	8.33	0.50	0.300		0.136	(0.270)	0.164
101	8.42	0.50	0.300		0.135	(0.270)	0.165
102	8.50	0.50	0.300		0.135	(0.270)	0.165
103	8.58	0.53	0.320		0.134	(0.288)	0.186
104	8.67	0.53	0.320		0.133	(0.288)	0.187
105	8.75	0.53	0.320		0.133	(0.288)	0.187
106	8.83	0.57	0.340		0.132	(0.306)	0.208
107	8.92	0.57	0.340		0.131	(0.306)	0.208
108	9.00	0.57	0.340		0.131	(0.306)	0.209
109	9.08	0.63	0.380		0.130	(0.342)	0.250
110	9.17	0.63	0.380		0.130	(0.342)	0.250
111	9.25	0.63	0.380		0.129	(0.342)	0.251
112	9.33	0.67	0.400		0.128	(0.360)	0.272
113	9.42	0.67	0.400		0.128	(0.360)	0.272
114	9.50	0.67	0.400		0.127	(0.360)	0.273
115	9.58	0.70	0.420		0.127	(0.378)	0.293
116	9.67	0.70	0.420		0.126	(0.378)	0.294
117	9.75	0.70	0.420		0.125	(0.378)	0.295
118	9.83	0.73	0.440		0.125	(0.396)	0.315
119	9.92	0.73	0.440		0.124	(0.396)	0.316
120	10.00	0.73	0.440		0.124	(0.396)	0.316
121	10.08	0.50	0.300		0.123	(0.270)	0.177
122	10.17	0.50	0.300		0.122	(0.270)	0.178
123	10.25	0.50	0.300		0.122	(0.270)	0.178
124	10.33	0.50	0.300		0.121	(0.270)	0.179
125	10.42	0.50	0.300		0.121	(0.270)	0.179
126	10.50	0.50	0.300		0.120	(0.270)	0.180
127	10.58	0.67	0.400		0.119	(0.360)	0.281
128	10.67	0.67	0.400		0.119	(0.360)	0.281
129	10.75	0.67	0.400		0.118	(0.360)	0.282
130	10.83	0.67	0.400		0.118	(0.360)	0.282
131	10.92	0.67	0.400		0.117	(0.360)	0.283
132	11.00	0.67	0.400		0.117	(0.360)	0.283
133	11.08	0.63	0.380		0.116	(0.342)	0.264
134	11.17	0.63	0.380		0.115	(0.342)	0.265
135	11.25	0.63	0.380		0.115	(0.342)	0.265
136	11.33	0.63	0.380		0.114	(0.342)	0.266
137	11.42	0.63	0.380		0.114	(0.342)	0.266
138	11.50	0.63	0.380		0.113	(0.342)	0.267
139	11.58	0.57	0.340		0.113	(0.306)	0.227
140	11.67	0.57	0.340		0.112	(0.306)	0.228
141	11.75	0.57	0.340		0.111	(0.306)	0.229
142	11.83	0.60	0.360		0.111	(0.324)	0.249
143	11.92	0.60	0.360		0.110	(0.324)	0.250
144	12.00	0.60	0.360		0.110	(0.324)	0.250
145	12.08	0.83	0.500		0.109	(0.450)	0.391
146	12.17	0.83	0.500		0.109	(0.450)	0.391
147	12.25	0.83	0.500		0.108	(0.450)	0.392
148	12.33	0.87	0.520		0.108	(0.468)	0.412
149	12.42	0.87	0.520		0.107	(0.468)	0.413
150	12.50	0.87	0.520		0.107	(0.468)	0.413
151	12.58	0.93	0.560		0.106	(0.504)	0.454
152	12.67	0.93	0.560		0.105	(0.504)	0.455
153	12.75	0.93	0.560		0.105	(0.504)	0.455

154	12.83	0.97	0.580	0.104	(0.522)	0.476
155	12.92	0.97	0.580	0.104	(0.522)	0.476
156	13.00	0.97	0.580	0.103	(0.522)	0.477
157	13.08	1.13	0.680	0.103	(0.612)	0.577
158	13.17	1.13	0.680	0.102	(0.612)	0.578
159	13.25	1.13	0.680	0.102	(0.612)	0.578
160	13.33	1.13	0.680	0.101	(0.612)	0.579
161	13.42	1.13	0.680	0.101	(0.612)	0.579
162	13.50	1.13	0.680	0.100	(0.612)	0.580
163	13.58	0.77	0.460	0.100	(0.414)	0.360
164	13.67	0.77	0.460	0.099	(0.414)	0.361
165	13.75	0.77	0.460	0.099	(0.414)	0.361
166	13.83	0.77	0.460	0.098	(0.414)	0.362
167	13.92	0.77	0.460	0.098	(0.414)	0.362
168	14.00	0.77	0.460	0.097	(0.414)	0.363
169	14.08	0.90	0.540	0.097	(0.486)	0.443
170	14.17	0.90	0.540	0.096	(0.486)	0.444
171	14.25	0.90	0.540	0.096	(0.486)	0.444
172	14.33	0.87	0.520	0.095	(0.468)	0.425
173	14.42	0.87	0.520	0.095	(0.468)	0.425
174	14.50	0.87	0.520	0.094	(0.468)	0.426
175	14.58	0.87	0.520	0.094	(0.468)	0.426
176	14.67	0.87	0.520	0.093	(0.468)	0.427
177	14.75	0.87	0.520	0.093	(0.468)	0.427
178	14.83	0.83	0.500	0.092	(0.450)	0.408
179	14.92	0.83	0.500	0.092	(0.450)	0.408
180	15.00	0.83	0.500	0.091	(0.450)	0.409
181	15.08	0.80	0.480	0.091	(0.432)	0.389
182	15.17	0.80	0.480	0.090	(0.432)	0.390
183	15.25	0.80	0.480	0.090	(0.432)	0.390
184	15.33	0.77	0.460	0.090	(0.414)	0.370
185	15.42	0.77	0.460	0.089	(0.414)	0.371
186	15.50	0.77	0.460	0.089	(0.414)	0.371
187	15.58	0.63	0.380	0.088	(0.342)	0.292
188	15.67	0.63	0.380	0.088	(0.342)	0.292
189	15.75	0.63	0.380	0.087	(0.342)	0.293
190	15.83	0.63	0.380	0.087	(0.342)	0.293
191	15.92	0.63	0.380	0.086	(0.342)	0.294
192	16.00	0.63	0.380	0.086	(0.342)	0.294
193	16.08	0.13	0.080	(0.085)	0.072	0.008
194	16.17	0.13	0.080	(0.085)	0.072	0.008
195	16.25	0.13	0.080	(0.085)	0.072	0.008
196	16.33	0.13	0.080	(0.084)	0.072	0.008
197	16.42	0.13	0.080	(0.084)	0.072	0.008
198	16.50	0.13	0.080	(0.083)	0.072	0.008
199	16.58	0.10	0.060	(0.083)	0.054	0.006
200	16.67	0.10	0.060	(0.082)	0.054	0.006
201	16.75	0.10	0.060	(0.082)	0.054	0.006
202	16.83	0.10	0.060	(0.082)	0.054	0.006
203	16.92	0.10	0.060	(0.081)	0.054	0.006
204	17.00	0.10	0.060	(0.081)	0.054	0.006
205	17.08	0.17	0.100	0.080	(0.090)	0.020
206	17.17	0.17	0.100	0.080	(0.090)	0.020
207	17.25	0.17	0.100	0.080	(0.090)	0.020
208	17.33	0.17	0.100	0.079	(0.090)	0.021
209	17.42	0.17	0.100	0.079	(0.090)	0.021
210	17.50	0.17	0.100	0.078	(0.090)	0.022
211	17.58	0.17	0.100	0.078	(0.090)	0.022
212	17.67	0.17	0.100	0.078	(0.090)	0.022
213	17.75	0.17	0.100	0.077	(0.090)	0.023
214	17.83	0.13	0.080	(0.077)	0.072	0.008
215	17.92	0.13	0.080	(0.076)	0.072	0.008
216	18.00	0.13	0.080	(0.076)	0.072	0.008
217	18.08	0.13	0.080	(0.076)	0.072	0.008
218	18.17	0.13	0.080	(0.075)	0.072	0.008
219	18.25	0.13	0.080	(0.075)	0.072	0.008
220	18.33	0.13	0.080	(0.075)	0.072	0.008
221	18.42	0.13	0.080	(0.074)	0.072	0.008
222	18.50	0.13	0.080	(0.074)	0.072	0.008
223	18.58	0.10	0.060	(0.074)	0.054	0.006
224	18.67	0.10	0.060	(0.073)	0.054	0.006
225	18.75	0.10	0.060	(0.073)	0.054	0.006
226	18.83	0.07	0.040	(0.072)	0.036	0.004
227	18.92	0.07	0.040	(0.072)	0.036	0.004
228	19.00	0.07	0.040	(0.072)	0.036	0.004
229	19.08	0.10	0.060	(0.071)	0.054	0.006
230	19.17	0.10	0.060	(0.071)	0.054	0.006
231	19.25	0.10	0.060	(0.071)	0.054	0.006
232	19.33	0.13	0.080	0.070	(0.072)	0.010
233	19.42	0.13	0.080	0.070	(0.072)	0.010
234	19.50	0.13	0.080	0.070	(0.072)	0.010
235	19.58	0.10	0.060	(0.069)	0.054	0.006
236	19.67	0.10	0.060	(0.069)	0.054	0.006
237	19.75	0.10	0.060	(0.069)	0.054	0.006
238	19.83	0.07	0.040	(0.069)	0.036	0.004
239	19.92	0.07	0.040	(0.068)	0.036	0.004

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240  20.00     0.07      0.040       (  0.068)       0.036        0.004
241  20.08     0.10      0.060       (  0.068)       0.054        0.006
242  20.17     0.10      0.060       (  0.067)       0.054        0.006
243  20.25     0.10      0.060       (  0.067)       0.054        0.006
244  20.33     0.10      0.060       (  0.067)       0.054        0.006
245  20.42     0.10      0.060       (  0.066)       0.054        0.006
246  20.50     0.10      0.060       (  0.066)       0.054        0.006
247  20.58     0.10      0.060       (  0.066)       0.054        0.006
248  20.67     0.10      0.060       (  0.066)       0.054        0.006
249  20.75     0.10      0.060       (  0.065)       0.054        0.006
250  20.83     0.07      0.040       (  0.065)       0.036        0.004
251  20.92     0.07      0.040       (  0.065)       0.036        0.004
252  21.00     0.07      0.040       (  0.065)       0.036        0.004
253  21.08     0.10      0.060       (  0.064)       0.054        0.006
254  21.17     0.10      0.060       (  0.064)       0.054        0.006
255  21.25     0.10      0.060       (  0.064)       0.054        0.006
256  21.33     0.07      0.040       (  0.064)       0.036        0.004
257  21.42     0.07      0.040       (  0.063)       0.036        0.004
258  21.50     0.07      0.040       (  0.063)       0.036        0.004
259  21.58     0.10      0.060       (  0.063)       0.054        0.006
260  21.67     0.10      0.060       (  0.063)       0.054        0.006
261  21.75     0.10      0.060       (  0.062)       0.054        0.006
262  21.83     0.07      0.040       (  0.062)       0.036        0.004
263  21.92     0.07      0.040       (  0.062)       0.036        0.004
264  22.00     0.07      0.040       (  0.062)       0.036        0.004
265  22.08     0.10      0.060       (  0.062)       0.054        0.006
266  22.17     0.10      0.060       (  0.061)       0.054        0.006
267  22.25     0.10      0.060       (  0.061)       0.054        0.006
268  22.33     0.07      0.040       (  0.061)       0.036        0.004
269  22.42     0.07      0.040       (  0.061)       0.036        0.004
270  22.50     0.07      0.040       (  0.061)       0.036        0.004
271  22.58     0.07      0.040       (  0.060)       0.036        0.004
272  22.67     0.07      0.040       (  0.060)       0.036        0.004
273  22.75     0.07      0.040       (  0.060)       0.036        0.004
274  22.83     0.07      0.040       (  0.060)       0.036        0.004
275  22.92     0.07      0.040       (  0.060)       0.036        0.004
276  23.00     0.07      0.040       (  0.060)       0.036        0.004
277  23.08     0.07      0.040       (  0.060)       0.036        0.004
278  23.17     0.07      0.040       (  0.059)       0.036        0.004
279  23.25     0.07      0.040       (  0.059)       0.036        0.004
280  23.33     0.07      0.040       (  0.059)       0.036        0.004
281  23.42     0.07      0.040       (  0.059)       0.036        0.004
282  23.50     0.07      0.040       (  0.059)       0.036        0.004
283  23.58     0.07      0.040       (  0.059)       0.036        0.004
284  23.67     0.07      0.040       (  0.059)       0.036        0.004
285  23.75     0.07      0.040       (  0.059)       0.036        0.004
286  23.83     0.07      0.040       (  0.059)       0.036        0.004
287  23.92     0.07      0.040       (  0.059)       0.036        0.004
288  24.00     0.07      0.040       (  0.059)       0.036        0.004
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    34.3
      Flood volume = Effective rainfall      2.86(In)
       times area      51.8(Ac.)/[(In)/(Ft.)] =      12.3(Ac.Ft)
      Total soil loss =      2.14(In)
      Total soil loss =     9.246(Ac.Ft)
      Total rainfall =      5.00(In)
      Flood volume =      537304.1 Cubic Feet
      Total soil loss =      402770.7 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     30.032(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                        24 - H O U R    S T O R M
                   R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0       10.0      20.0      30.0      40.0
 ---------------------------------------------------------------------------
   0+ 5       0.0002      0.04  Q         |         |         |         |
   0+10       0.0012      0.14  Q         |         |         |         |
   0+15       0.0024      0.17  Q         |         |         |         |
   0+20       0.0038      0.20  Q         |         |         |         |
   0+25       0.0056      0.26  Q         |         |         |         |
   0+30       0.0075      0.29  Q         |         |         |         |
   0+35       0.0096      0.30  Q         |         |         |         |
   0+40       0.0117      0.30  Q         |         |         |         |
   0+45       0.0138      0.31  Q         |         |         |         |
   0+50       0.0161      0.33  Q         |         |         |         |
   0+55       0.0187      0.38  Q         |         |         |         |
   1+ 0       0.0215      0.40  Q         |         |         |         |
   1+ 5       0.0241      0.39  Q         |         |         |         |
   1+10       0.0265      0.34  Q         |         |         |         |
   1+15       0.0288      0.33  Q         |         |         |         |
   1+20       0.0310      0.32  Q         |         |         |         |
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1+25	0.0332	0.32	Q	|	|	|	|
1+30	0.0354	0.32	Q	|	|	|	|
1+35	0.0375	0.32	Q	|	|	|	|
1+40	0.0397	0.31	Q	|	|	|	|
1+45	0.0419	0.31	Q	|	|	|	|
1+50	0.0441	0.33	Q	|	|	|	|
1+55	0.0468	0.38	Q	|	|	|	|
2+ 0	0.0495	0.40	Q	|	|	|	|
2+ 5	0.0523	0.41	Q	|	|	|	|
2+10	0.0551	0.41	Q	|	|	|	|
2+15	0.0580	0.41	Q	|	|	|	|
2+20	0.0608	0.42	Q	|	|	|	|
2+25	0.0637	0.42	Q	|	|	|	|
2+30	0.0666	0.42	Q	|	|	|	|
2+35	0.0696	0.44	Q	|	|	|	|
2+40	0.0729	0.49	Q	|	|	|	|
2+45	0.0764	0.50	Q	|	|	|	|
2+50	0.0799	0.51	Q	|	|	|	|
2+55	0.0835	0.52	Q	|	|	|	|
3+ 0	0.0870	0.52	Q	|	|	|	|
3+ 5	0.0906	0.52	Q	|	|	|	|
3+10	0.0942	0.52	Q	|	|	|	|
3+15	0.0978	0.52	Q	|	|	|	|
3+20	0.1014	0.52	Q	|	|	|	|
3+25	0.1050	0.52	Q	|	|	|	|
3+30	0.1086	0.52	Q	|	|	|	|
3+35	0.1122	0.52	Q	|	|	|	|
3+40	0.1158	0.52	Q	|	|	|	|
3+45	0.1194	0.52	Q	|	|	|	|
3+50	0.1231	0.54	Q	|	|	|	|
3+55	0.1272	0.59	Q	|	|	|	|
4+ 0	0.1314	0.61	Q	|	|	|	|
4+ 5	0.1356	0.62	Q	|	|	|	|
4+10	0.1399	0.62	Q	|	|	|	|
4+15	0.1442	0.62	Q	|	|	|	|
4+20	0.1486	0.64	Q	|	|	|	|
4+25	0.1534	0.69	Q	|	|	|	|
4+30	0.1583	0.71	Q	|	|	|	|
4+35	0.1632	0.72	Q	|	|	|	|
4+40	0.1682	0.72	Q	|	|	|	|
4+45	0.1732	0.73	Q	|	|	|	|
4+50	0.1784	0.75	Q	|	|	|	|
4+55	0.1839	0.80	Q	|	|	|	|
5+ 0	0.1895	0.82	Q	|	|	|	|
5+ 5	0.1949	0.79	Q	|	|	|	|
5+10	0.1997	0.69	Q	|	|	|	|
5+15	0.2042	0.66	Q	|	|	|	|
5+20	0.2088	0.67	Q	|	|	|	|
5+25	0.2137	0.71	Q	|	|	|	|
5+30	0.2186	0.72	Q	|	|	|	|
5+35	0.2238	0.74	Q	|	|	|	|
5+40	0.2292	0.79	Q	|	|	|	|
5+45	0.2348	0.81	Q	|	|	|	|
5+50	0.2405	0.82	Q	|	|	|	|
5+55	0.2462	0.83	Q	|	|	|	|
6+ 0	0.2519	0.83	Q	|	|	|	|
6+ 5	0.2583	0.93	Q	|	|	|	|
6+10	0.2665	1.19	VQ	|	|	|	|
6+15	0.2754	1.30	VQ	|	|	|	|
6+20	0.2849	1.37	VQ	|	|	|	|
6+25	0.2947	1.42	VQ	|	|	|	|
6+30	0.3048	1.47	VQ	|	|	|	|
6+35	0.3165	1.70	|Q	|	|	|	|
6+40	0.3319	2.24	|VQ	|	|	|	|
6+45	0.3488	2.45	|VQ	|	|	|	|
6+50	0.3664	2.56	|VQ	|	|	|	|
6+55	0.3846	2.64	|VQ	|	|	|	|
7+ 0	0.4033	2.71	|VQ	|	|	|	|
7+ 5	0.4223	2.76	|VQ	|	|	|	|
7+10	0.4416	2.81	|VQ	|	|	|	|
7+15	0.4612	2.85	|VQ	|	|	|	|
7+20	0.4823	3.07	|V Q	|	|	|	|
7+25	0.5071	3.60	|V Q	|	|	|	|
7+30	0.5333	3.81	|V Q	|	|	|	|
7+35	0.5616	4.10	|V Q	|	|	|	|
7+40	0.5938	4.68	|V Q	|	|	|	|
7+45	0.6276	4.91	| V Q	|	|	|	|
7+50	0.6636	5.22	| V Q	|	|	|	|
7+55	0.7037	5.81	| V Q	|	|	|	|
8+ 0	0.7454	6.06	| V Q	|	|	|	|
8+ 5	0.7905	6.55	| V Q	|	|	|	|
8+10	0.8431	7.64	| V Q	|	|	|	|
8+15	0.8986	8.06	| V Q	|	|	|	|
8+20	0.9555	8.27	| V Q	|	|	|	|
8+25	1.0134	8.40	| V Q	|	|	|	|
8+30	1.0719	8.50	| V Q	|	|	|	|

8+35	1.1322	8.75	
8+40	1.1963	9.31	
8+45	1.2620	9.53	
8+50	1.3296	9.83	
8+55	1.4013	10.40	
9+ 0	1.4745	10.64	
9+ 5	1.5512	11.13	
9+10	1.6353	12.21	
9+15	1.7223	12.63	
9+20	1.8119	13.02	
9+25	1.9059	13.65	
9+30	2.0018	13.92	
9+35	2.1000	14.25	
9+40	2.2022	14.85	
9+45	2.3063	15.10	
9+50	2.4124	15.41	
9+55	2.5226	16.00	
10+ 0	2.6345	16.24	
10+ 5	2.7385	15.11	
10+10	2.8191	11.71	
10+15	2.8918	10.56	
10+20	2.9612	10.06	
10+25	3.0286	9.80	
10+30	3.0950	9.64	
10+35	3.1669	10.44	
10+40	3.2556	12.88	
10+45	3.3500	13.71	
10+50	3.4473	14.13	
10+55	3.5463	14.38	
11+ 0	3.6465	14.55	
11+ 5	3.7464	14.50	
11+10	3.8434	14.09	
11+15	3.9397	13.99	
11+20	4.0358	13.95	
11+25	4.1317	13.93	
11+30	4.2277	13.93	
11+35	4.3212	13.58	
11+40	4.4080	12.60	
11+45	4.4925	12.27	
11+50	4.5774	12.33	
11+55	4.6654	12.77	
12+ 0	4.7543	12.91	
12+ 5	4.8524	14.24	
12+10	4.9749	17.78	
12+15	5.1060	19.04	
12+20	5.2424	19.81	
12+25	5.3847	20.66	
12+30	5.5298	21.07	
12+35	5.6791	21.67	
12+40	5.8362	22.82	
12+45	5.9967	23.30	
12+50	6.1598	23.68	
12+55	6.3272	24.31	
13+ 0	6.4965	24.58	
13+ 5	6.6729	25.62	
13+10	6.8672	28.21	
13+15	7.0680	29.16	
13+20	7.2718	29.59	
13+25	7.4774	29.85	
13+30	7.6843	30.03	
13+35	7.8783	28.17	
13+40	8.0351	22.77	
13+45	8.1792	20.93	
13+50	8.3177	20.11	
13+55	8.4530	19.64	
14+ 0	8.5863	19.35	
14+ 5	8.7233	19.90	
14+10	8.8734	21.79	
14+15	9.0276	22.40	
14+20	9.1829	22.55	
14+25	9.3362	22.26	
14+30	9.4893	22.22	
14+35	9.6425	22.25	
14+40	9.7959	22.27	
14+45	9.9495	22.31	
14+50	10.1020	22.14	
14+55	10.2511	21.65	
15+ 0	10.3991	21.49	
15+ 5	10.5455	21.26	
15+10	10.6884	20.74	
15+15	10.8300	20.56	
15+20	10.9698	20.31	
15+25	11.1061	19.78	
15+30	11.2410	19.59	
15+35	11.3704	18.80	
15+40	11.4859	16.77	

15+45	11.5965	16.06	|	Q	|	V	|
15+50	11.7050	15.75	|	Q	|	V	|
15+55	11.8123	15.59	|	Q	|	V	|
16+ 0	11.9190	15.48	|	Q	|	V	|
16+ 5	12.0074	12.85	|	Q	|	V	|
16+10	12.0466	5.68	|	Q	|	|	V|
16+15	12.0682	3.15	|	Q	|	|	V|
16+20	12.0823	2.04	|	Q	|	|	V|
16+25	12.0920	1.41	|Q		|	|	V|
16+30	12.0989	1.00	|Q		|	|	V|
16+35	12.1038	0.71	Q		|	|	V|
16+40	12.1072	0.50	Q		|	|	V|
16+45	12.1095	0.33	Q		|	|	V|
16+50	12.1118	0.32	Q		|	|	V|
16+55	12.1140	0.32	Q		|	|	V|
17+ 0	12.1162	0.32	Q		|	|	V|
17+ 5	12.1192	0.44	Q		|	|	V|
17+10	12.1245	0.78	Q		|	|	V|
17+15	12.1308	0.91	Q		|	|	V|
17+20	12.1376	0.98	Q		|	|	V|
17+25	12.1446	1.03	|Q		|	|	V|
17+30	12.1520	1.07	|Q		|	|	V|
17+35	12.1596	1.10	|Q		|	|	V|
17+40	12.1673	1.13	|Q		|	|	V|
17+45	12.1753	1.16	|Q		|	|	V|
17+50	12.1825	1.04	|Q		|	|	V|
17+55	12.1871	0.68	Q		|	|	V|
18+ 0	12.1910	0.55	Q		|	|	V|
18+ 5	12.1944	0.50	Q		|	|	V|
18+10	12.1976	0.47	Q		|	|	V|
18+15	12.2007	0.45	Q		|	|	V|
18+20	12.2037	0.43	Q		|	|	V|
18+25	12.2066	0.43	Q		|	|	V|
18+30	12.2095	0.42	Q		|	|	V|
18+35	12.2122	0.40	Q		|	|	V|
18+40	12.2146	0.35	Q		|	|	V|
18+45	12.2169	0.33	Q		|	|	V|
18+50	12.2190	0.31	Q		|	|	V|
18+55	12.2208	0.25	Q		|	|	V|
19+ 0	12.2224	0.23	Q		|	|	V|
19+ 5	12.2240	0.24	Q		|	|	V|
19+10	12.2260	0.28	Q		|	|	V|
19+15	12.2281	0.30	Q		|	|	V|
19+20	12.2304	0.34	Q		|	|	V|
19+25	12.2333	0.43	Q		|	|	V|
19+30	12.2366	0.47	Q		|	|	V|
19+35	12.2398	0.46	Q		|	|	V|
19+40	12.2423	0.37	Q		|	|	V|
19+45	12.2447	0.34	Q		|	|	V|
19+50	12.2469	0.31	Q		|	|	V|
19+55	12.2486	0.26	Q		|	|	V|
20+ 0	12.2503	0.24	Q		|	|	V|
20+ 5	12.2519	0.24	Q		|	|	V|
20+10	12.2539	0.29	Q		|	|	V|
20+15	12.2560	0.30	Q		|	|	V|
20+20	12.2581	0.30	Q		|	|	V|
20+25	12.2602	0.31	Q		|	|	V|
20+30	12.2623	0.31	Q		|	|	V|
20+35	12.2644	0.31	Q		|	|	V|
20+40	12.2666	0.31	Q		|	|	V|
20+45	12.2688	0.31	Q		|	|	V|
20+50	12.2708	0.30	Q		|	|	V|
20+55	12.2725	0.25	Q		|	|	V|
21+ 0	12.2740	0.23	Q		|	|	V|
21+ 5	12.2757	0.24	Q		|	|	V|
21+10	12.2776	0.28	Q		|	|	V|
21+15	12.2797	0.30	Q		|	|	V|
21+20	12.2817	0.29	Q		|	|	V|
21+25	12.2833	0.24	Q		|	|	V|
21+30	12.2849	0.22	Q		|	|	V|
21+35	12.2865	0.24	Q		|	|	V|
21+40	12.2884	0.28	Q		|	|	V|
21+45	12.2905	0.30	Q		|	|	V|
21+50	12.2925	0.29	Q		|	|	V|
21+55	12.2941	0.24	Q		|	|	V|
22+ 0	12.2957	0.22	Q		|	|	V|
22+ 5	12.2973	0.24	Q		|	|	V|
22+10	12.2992	0.28	Q		|	|	V|
22+15	12.3013	0.30	Q		|	|	V|
22+20	12.3033	0.29	Q		|	|	V|
22+25	12.3049	0.24	Q		|	|	V|
22+30	12.3064	0.22	Q		|	|	V|
22+35	12.3079	0.22	Q		|	|	V|
22+40	12.3094	0.21	Q		|	|	V|
22+45	12.3109	0.21	Q		|	|	V|
22+50	12.3123	0.21	Q		|	|	V|

```
   22+55      12.3138      0.21  Q          |          |          |          V|
   23+ 0      12.3152      0.21  Q          |          |          |          V|
   23+ 5      12.3167      0.21  Q          |          |          |          V|
   23+10      12.3181      0.21  Q          |          |          |          V|
   23+15      12.3195      0.21  Q          |          |          |          V|
   23+20      12.3210      0.21  Q          |          |          |          V|
   23+25      12.3224      0.21  Q          |          |          |          V|
   23+30      12.3239      0.21  Q          |          |          |          V|
   23+35      12.3253      0.21  Q          |          |          |          V|
   23+40      12.3267      0.21  Q          |          |          |          V|
   23+45      12.3282      0.21  Q          |          |          |          V|
   23+50      12.3296      0.21  Q          |          |          |          V|
   23+55      12.3311      0.21  Q          |          |          |          V|
   24+ 0      12.3325      0.21  Q          |          |          |          V|
   24+ 5      12.3337      0.17  Q          |          |          |          V|
   24+10      12.3342      0.07  Q          |          |          |          V|
   24+15      12.3345      0.04  Q          |          |          |          V|
   24+20      12.3346      0.02  Q          |          |          |          V|
   24+25      12.3347      0.01  Q          |          |          |          V|
   24+30      12.3348      0.01  Q          |          |          |          V|
   24+35      12.3348      0.00  Q          |          |          |          V|
   24+40      12.3348      0.00  Q          |          |          |           V
-------------------------------------------------------------------------------
```

Extended Detention Basin No. 3

```
       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/22/24 File: EX3212.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =       7.79(Ac.)  =      0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =       7.79(Ac.)  =      0.012 Sq. Mi.
Length along longest watercourse =    1222.00(Ft.)
Length along longest watercourse measured to centroid =     611.00(Ft.)
Length along longest watercourse =      0.231 Mi.
Length along longest watercourse measured to centroid =      0.116 Mi.
Difference in elevation =      89.00(Ft.)
Slope along watercourse =    384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.059 Hr.
Lag time =     3.52 Min.
25% of lag time =     0.88 Min.
40% of lag time =     1.41 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            0.50                 3.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            1.30                10.13

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.500(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    0.500(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     7.790           91.00          0.000
 Total Area Entered =      7.79(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
			Sum = 100.000 Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.198	(0.246) 0.178	0.020
2	0.17	4.20	0.252	(0.246) 0.227	0.025
3	0.25	4.40	0.264	(0.246) 0.238	0.026
4	0.33	4.80	0.288	0.246 (0.259)	0.042
5	0.42	5.20	0.312	0.246 (0.281)	0.066
6	0.50	6.20	0.372	0.246 (0.335)	0.126
7	0.58	6.80	0.408	0.246 (0.367)	0.162
8	0.67	8.80	0.528	0.246 (0.475)	0.282
9	0.75	13.90	0.834	0.246 (0.751)	0.588
10	0.83	31.40	1.884	0.246 (1.695)	1.638
11	0.92	7.20	0.432	0.246 (0.389)	0.186
12	1.00	3.80	0.228	(0.246) 0.205	0.023
		(Loss Rate Not Used)			
Sum =		100.0		Sum =	3.2

Flood volume = Effective rainfall 0.27(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 0.23(In)
Total soil loss = 0.152(Ac.Ft)
Total rainfall = 0.50(In)
Flood volume = 7495.8 Cubic Feet
Total soil loss = 6642.0 Cubic Feet

Peak flow rate of this hydrograph = 7.278(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0003	0.05	Q				
0+10	0.0013	0.14	Q				
0+15	0.0025	0.18	Q				
0+20	0.0041	0.23	Q				
0+25	0.0065	0.35	Q				
0+30	0.0107	0.61	Q				
0+35	0.0173	0.95	QV				
0+40	0.0272	1.45	QV				
0+45	0.0459	2.71	Q				
0+50	0.0911	6.56	Q		V		
0+55	0.1412	7.28	Q		V		
1+ 0	0.1589	2.57	Q		V		
1+ 5	0.1664	1.08	Q		V		
1+10	0.1700	0.52	Q		V		
1+15	0.1719	0.27	Q		V		
1+20	0.1721	0.03	Q		V		
1+25	0.1721	0.00	Q		V		

```
       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/22/24 File: EX3232.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =       7.79(Ac.)  =      0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =       7.79(Ac.)  =      0.012 Sq. Mi.
Length along longest watercourse =    1222.00(Ft.)
Length along longest watercourse measured to centroid =     611.00(Ft.)
Length along longest watercourse =      0.231 Mi.
Length along longest watercourse measured to centroid =      0.116 Mi.
Difference in elevation =      89.00(Ft.)
Slope along watercourse =    384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.059 Hr.
Lag time =     3.52 Min.
25% of lag time =     0.88 Min.
40% of lag time =     1.41 Min.
Unit time =     5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            0.80                 6.23

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            2.00                15.58

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    0.800(In)
Area Averaged 100-Year Rainfall =    2.000(In)

Point rain (area averaged) =    0.800(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    0.800(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     7.790           91.00          0.000
 Total Area Entered =      7.79(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
		Sum = 100.000	Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.125	(0.246)	0.112	0.012
2	0.17	1.30	0.125	(0.246)	0.112	0.012
3	0.25	1.10	0.106	(0.246)	0.095	0.011
4	0.33	1.50	0.144	(0.246)	0.130	0.014
5	0.42	1.50	0.144	(0.246)	0.130	0.014
6	0.50	1.80	0.173	(0.246)	0.156	0.017
7	0.58	1.50	0.144	(0.246)	0.130	0.014
8	0.67	1.80	0.173	(0.246)	0.156	0.017
9	0.75	1.80	0.173	(0.246)	0.156	0.017
10	0.83	1.50	0.144	(0.246)	0.130	0.014
11	0.92	1.60	0.154	(0.246)	0.138	0.015
12	1.00	1.80	0.173	(0.246)	0.156	0.017
13	1.08	2.20	0.211	(0.246)	0.190	0.021
14	1.17	2.20	0.211	(0.246)	0.190	0.021
15	1.25	2.20	0.211	(0.246)	0.190	0.021
16	1.33	2.00	0.192	(0.246)	0.173	0.019
17	1.42	2.60	0.250	(0.246)	0.225	0.025
18	1.50	2.70	0.259	(0.246)	0.233	0.026
19	1.58	2.40	0.230	(0.246)	0.207	0.023
20	1.67	2.70	0.259	(0.246)	0.233	0.026
21	1.75	3.30	0.317	0.246	(0.285)	0.070
22	1.83	3.10	0.298	0.246	(0.268)	0.051
23	1.92	2.90	0.278	0.246	(0.251)	0.032
24	2.00	3.00	0.288	0.246	(0.259)	0.042
25	2.08	3.10	0.298	0.246	(0.268)	0.051
26	2.17	4.20	0.403	0.246	(0.363)	0.157
27	2.25	5.00	0.480	0.246	(0.432)	0.234
28	2.33	3.50	0.336	0.246	(0.302)	0.090
29	2.42	6.80	0.653	0.246	(0.587)	0.406
30	2.50	7.30	0.701	0.246	(0.631)	0.454
31	2.58	8.20	0.787	0.246	(0.708)	0.541
32	2.67	5.90	0.566	0.246	(0.510)	0.320
33	2.75	2.00	0.192	(0.246)	0.173	0.019
34	2.83	1.80	0.173	(0.246)	0.156	0.017
35	2.92	1.80	0.173	(0.246)	0.156	0.017
36	3.00	0.60	0.058	(0.246)	0.052	0.006
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	2.9

Flood volume = Effective rainfall 0.24(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 0.56(In)
Total soil loss = 0.364(Ac.Ft)
Total rainfall = 0.80(In)
Flood volume = 6757.9 Cubic Feet
Total soil loss = 15863.5 Cubic Feet

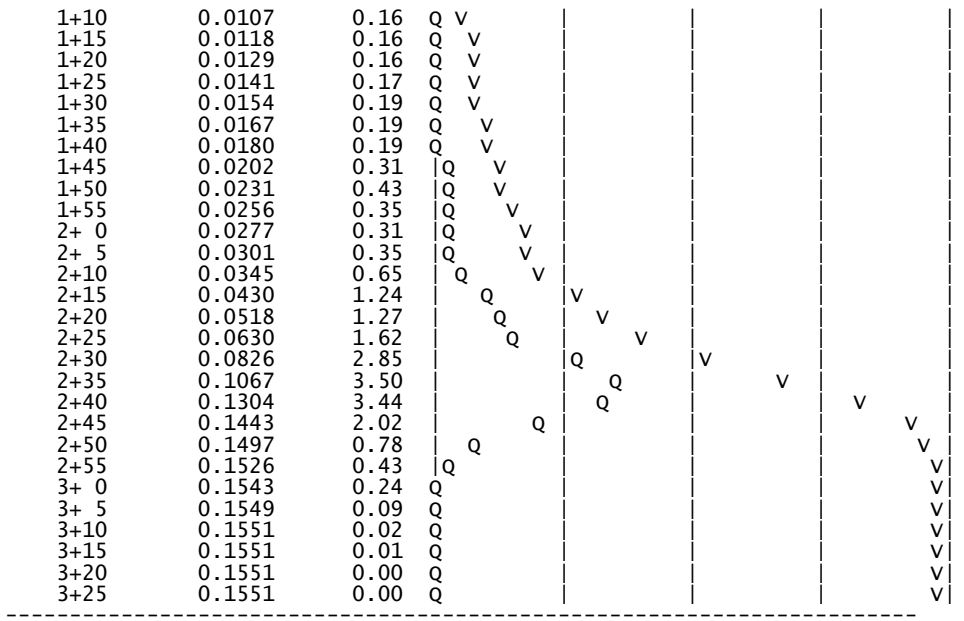
Peak flow rate of this hydrograph = 3.502(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0002	0.03	Q				
0+10	0.0007	0.08	Q				
0+15	0.0013	0.08	Q				
0+20	0.0019	0.09	Q				
0+25	0.0027	0.11	Q				
0+30	0.0035	0.12	Q				
0+35	0.0043	0.12	QV				
0+40	0.0052	0.12	QV				
0+45	0.0061	0.13	QV				
0+50	0.0070	0.13	QV				
0+55	0.0078	0.12	Q V				
1+ 0	0.0087	0.13	Q V				
1+ 5	0.0096	0.14	Q V				


1+10 0.0107 0.16
1+15 0.0118 0.16
1+20 0.0129 0.16
1+25 0.0141 0.17
1+30 0.0154 0.19
1+35 0.0167 0.19
1+40 0.0180 0.19
1+45 0.0202 0.31
1+50 0.0231 0.43
1+55 0.0256 0.35
2+ 0 0.0277 0.31
2+ 5 0.0301 0.35
2+10 0.0345 0.65
2+15 0.0430 1.24
2+20 0.0518 1.27
2+25 0.0630 1.62
2+30 0.0826 2.85
2+35 0.1067 3.50
2+40 0.1304 3.44
2+45 0.1443 2.02
2+50 0.1497 0.78
2+55 0.1526 0.43
3+ 0 0.1543 0.24
3+ 5 0.1549 0.09
3+10 0.1551 0.02
3+15 0.1551 0.01
3+20 0.1551 0.00
3+25 0.1551 0.00

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX3262.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 1222.00(Ft.)
Length along longest watercourse measured to centroid = 611.00(Ft.)
Length along longest watercourse = 0.231 Mi.
Length along longest watercourse measured to centroid = 0.116 Mi.
Difference in elevation = 89.00(Ft.)
Slope along watercourse = 384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.059 Hr.
Lag time = 3.52 Min.
25% of lag time = 0.88 Min.
40% of lag time = 1.41 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.10	8.57

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	3.00	23.37

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.100(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.100(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	91.00	0.000

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
			Sum = 100.000	Sum= 7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.066	(0.246)	0.059	0.007
2	0.17	0.60	0.079	(0.246)	0.071	0.008
3	0.25	0.60	0.079	(0.246)	0.071	0.008
4	0.33	0.60	0.079	(0.246)	0.071	0.008
5	0.42	0.60	0.079	(0.246)	0.071	0.008
6	0.50	0.70	0.092	(0.246)	0.083	0.009
7	0.58	0.70	0.092	(0.246)	0.083	0.009
8	0.67	0.70	0.092	(0.246)	0.083	0.009
9	0.75	0.70	0.092	(0.246)	0.083	0.009
10	0.83	0.70	0.092	(0.246)	0.083	0.009
11	0.92	0.70	0.092	(0.246)	0.083	0.009
12	1.00	0.80	0.106	(0.246)	0.095	0.011
13	1.08	0.80	0.106	(0.246)	0.095	0.011
14	1.17	0.80	0.106	(0.246)	0.095	0.011
15	1.25	0.80	0.106	(0.246)	0.095	0.011
16	1.33	0.80	0.106	(0.246)	0.095	0.011
17	1.42	0.80	0.106	(0.246)	0.095	0.011
18	1.50	0.80	0.106	(0.246)	0.095	0.011
19	1.58	0.80	0.106	(0.246)	0.095	0.011
20	1.67	0.80	0.106	(0.246)	0.095	0.011
21	1.75	0.80	0.106	(0.246)	0.095	0.011
22	1.83	0.80	0.106	(0.246)	0.095	0.011
23	1.92	0.80	0.106	(0.246)	0.095	0.011
24	2.00	0.90	0.119	(0.246)	0.107	0.012
25	2.08	0.80	0.106	(0.246)	0.095	0.011
26	2.17	0.90	0.119	(0.246)	0.107	0.012
27	2.25	0.90	0.119	(0.246)	0.107	0.012
28	2.33	0.90	0.119	(0.246)	0.107	0.012
29	2.42	0.90	0.119	(0.246)	0.107	0.012
30	2.50	0.90	0.119	(0.246)	0.107	0.012
31	2.58	0.90	0.119	(0.246)	0.107	0.012
32	2.67	0.90	0.119	(0.246)	0.107	0.012
33	2.75	1.00	0.132	(0.246)	0.119	0.013
34	2.83	1.00	0.132	(0.246)	0.119	0.013
35	2.92	1.00	0.132	(0.246)	0.119	0.013
36	3.00	1.00	0.132	(0.246)	0.119	0.013
37	3.08	1.00	0.132	(0.246)	0.119	0.013
38	3.17	1.10	0.145	(0.246)	0.131	0.015
39	3.25	1.10	0.145	(0.246)	0.131	0.015
40	3.33	1.10	0.145	(0.246)	0.131	0.015
41	3.42	1.20	0.158	(0.246)	0.143	0.016
42	3.50	1.30	0.172	(0.246)	0.154	0.017
43	3.58	1.40	0.185	(0.246)	0.166	0.018
44	3.67	1.40	0.185	(0.246)	0.166	0.018
45	3.75	1.50	0.198	(0.246)	0.178	0.020
46	3.83	1.50	0.198	(0.246)	0.178	0.020
47	3.92	1.60	0.211	(0.246)	0.190	0.021
48	4.00	1.60	0.211	(0.246)	0.190	0.021
49	4.08	1.70	0.224	(0.246)	0.202	0.022
50	4.17	1.80	0.238	(0.246)	0.214	0.024
51	4.25	1.90	0.251	(0.246)	0.226	0.025
52	4.33	2.00	0.264	(0.246)	0.238	0.026
53	4.42	2.10	0.277	0.246	(0.249)	0.031
54	4.50	2.10	0.277	0.246	(0.249)	0.031
55	4.58	2.20	0.290	0.246	(0.261)	0.044
56	4.67	2.30	0.304	0.246	(0.273)	0.057
57	4.75	2.40	0.317	0.246	(0.285)	0.070
58	4.83	2.40	0.317	0.246	(0.285)	0.070
59	4.92	2.50	0.330	0.246	(0.297)	0.084
60	5.00	2.60	0.343	0.246	(0.309)	0.097
61	5.08	3.10	0.409	0.246	(0.368)	0.163
62	5.17	3.60	0.475	0.246	(0.428)	0.229
63	5.25	3.90	0.515	0.246	(0.463)	0.268
64	5.33	4.20	0.554	0.246	(0.499)	0.308
65	5.42	4.70	0.620	0.246	(0.558)	0.374
66	5.50	5.60	0.739	0.246	(0.665)	0.493
67	5.58	1.90	0.251	(0.246)	0.226	0.025
68	5.67	0.90	0.119	(0.246)	0.107	0.012
69	5.75	0.60	0.079	(0.246)	0.071	0.008
70	5.83	0.50	0.066	(0.246)	0.059	0.007

```
71   5.92     0.30      0.040       (  0.246)       0.036        0.004
72   6.00     0.20      0.026       (  0.246)       0.024        0.003
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =     3.1
      Flood volume = Effective rainfall      0.26(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       0.2(Ac.Ft)
      Total soil loss =      0.84(In)
      Total soil loss =     0.548(Ac.Ft)
      Total rainfall =      1.10(In)
      Flood volume =        7216.3 Cubic Feet
      Total soil loss =       23888.3 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      3.066(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0001      0.02  Q         |         |         |         |
  0+10       0.0004      0.04  Q         |         |         |         |
  0+15       0.0008      0.06  Q         |         |         |         |
  0+20       0.0012      0.06  Q         |         |         |         |
  0+25       0.0016      0.06  Q         |         |         |         |
  0+30       0.0021      0.07  Q         |         |         |         |
  0+35       0.0026      0.07  Q         |         |         |         |
  0+40       0.0030      0.07  Q         |         |         |         |
  0+45       0.0035      0.07  Q         |         |         |         |
  0+50       0.0040      0.07  Q         |         |         |         |
  0+55       0.0045      0.07  QV        |         |         |         |
  1+ 0       0.0051      0.08  QV        |         |         |         |
  1+ 5       0.0056      0.08  QV        |         |         |         |
  1+10       0.0062      0.08  QV        |         |         |         |
  1+15       0.0068      0.08  QV        |         |         |         |
  1+20       0.0073      0.08  QV        |         |         |         |
  1+25       0.0079      0.08  QV        |         |         |         |
  1+30       0.0085      0.08  Q V       |         |         |         |
  1+35       0.0090      0.08  Q V       |         |         |         |
  1+40       0.0096      0.08  Q V       |         |         |         |
  1+45       0.0102      0.08  Q V       |         |         |         |
  1+50       0.0107      0.08  Q V       |         |         |         |
  1+55       0.0113      0.08  Q V       |         |         |         |
  2+ 0       0.0119      0.09  Q V       |         |         |         |
  2+ 5       0.0125      0.09  Q  V      |         |         |         |
  2+10       0.0131      0.09  Q  V      |         |         |         |
  2+15       0.0138      0.09  Q  V      |         |         |         |
  2+20       0.0144      0.09  Q  V      |         |         |         |
  2+25       0.0150      0.09  Q  V      |         |         |         |
  2+30       0.0157      0.09  Q  V      |         |         |         |
  2+35       0.0163      0.09  Q  V      |         |         |         |
  2+40       0.0170      0.09  Q   V     |         |         |         |
  2+45       0.0176      0.10  Q   V     |         |         |         |
  2+50       0.0183      0.10  Q   V     |         |         |         |
  2+55       0.0190      0.10  Q   V     |         |         |         |
  3+ 0       0.0197      0.10  Q   V     |         |         |         |
  3+ 5       0.0205      0.10  Q   V     |         |         |         |
  3+10       0.0212      0.11  Q    V    |         |         |         |
  3+15       0.0220      0.11  Q    V    |         |         |         |
  3+20       0.0227      0.11  Q    V    |         |         |         |
  3+25       0.0235      0.12  Q    V    |         |         |         |
  3+30       0.0244      0.13  Q    V    |         |         |         |
  3+35       0.0253      0.13  Q     V   |         |         |         |
  3+40       0.0263      0.14  Q     V   |         |         |         |
  3+45       0.0273      0.15  Q     V   |         |         |         |
  3+50       0.0284      0.15  Q     V   |         |         |         |
  3+55       0.0295      0.16  Q      V  |         |         |         |
  4+ 0       0.0306      0.16  Q      V  |         |         |         |
  4+ 5       0.0317      0.17  Q      V  |         |         |         |
  4+10       0.0330      0.18  Q      V  |         |         |         |
  4+15       0.0342      0.19  Q       V |         |         |         |
  4+20       0.0356      0.20  Q       V |         |         |         |
  4+25       0.0371      0.21  Q       V |         |         |         |
  4+30       0.0387      0.23  Q        V|         |         |         |
  4+35       0.0405      0.27  |Q       V|         |         |         |
  4+40       0.0430      0.35  |Q        V         |         |         |
  4+45       0.0461      0.45  |Q        |V        |         |         |
  4+50       0.0496      0.52  | Q       |V        |         |         |
  4+55       0.0536      0.57  | Q       | V       |         |         |
  5+ 0       0.0581      0.66  | Q       |   V     |         |         |
  5+ 5       0.0642      0.89  |  Q      |    V    |         |         |
  5+10       0.0733      1.32  |    Q    |      V  |         |         |
  5+15       0.0852      1.73  |     Q   |         V         |         |
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    5+20       0.0994      2.06  |       Q |         |   V     |         |
    5+25       0.1163      2.45  |        Q|         |       V |         |
    5+30       0.1374      3.07  |         | Q       |         |  V      |
    5+35       0.1544      2.46  |        Q|         |         |     V   |
    5+40       0.1601      0.83  |  Q      |         |         |      V  |
    5+45       0.1629      0.41  |Q        |         |         |       V|
    5+50       0.1644      0.22  Q         |         |         |       V|
    5+55       0.1652      0.12  Q         |         |         |       V|
    6+ 0       0.1655      0.04  Q         |         |         |       V|
    6+ 5       0.1656      0.02  Q         |         |         |       V|
    6+10       0.1656      0.01  Q         |         |         |       V|
    6+15       0.1657      0.00  Q         |         |         |       V|
    6+20       0.1657      0.00  Q         |         |         |       V|
    6+25       0.1657      0.00  Q         |         |         |        V
-------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX32242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 1222.00(Ft.)
Length along longest watercourse measured to centroid = 611.00(Ft.)
Length along longest watercourse = 0.231 Mi.
Length along longest watercourse measured to centroid = 0.116 Mi.
Difference in elevation = 89.00(Ft.)
Slope along watercourse = 384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.059 Hr.
Lag time = 3.52 Min.
25% of lag time = 0.88 Min.
40% of lag time = 1.41 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.80	14.02

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	5.00	38.95

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 1.800(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.800(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	91.00	0.000

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
			Sum = 100.000	Sum= 7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.014	(0.437)	0.013	0.001
2	0.17	0.07	0.014	(0.435)	0.013	0.001
3	0.25	0.07	0.014	(0.433)	0.013	0.001
4	0.33	0.10	0.022	(0.432)	0.019	0.002
5	0.42	0.10	0.022	(0.430)	0.019	0.002
6	0.50	0.10	0.022	(0.428)	0.019	0.002
7	0.58	0.10	0.022	(0.427)	0.019	0.002
8	0.67	0.10	0.022	(0.425)	0.019	0.002
9	0.75	0.10	0.022	(0.423)	0.019	0.002
10	0.83	0.13	0.029	(0.422)	0.026	0.003
11	0.92	0.13	0.029	(0.420)	0.026	0.003
12	1.00	0.13	0.029	(0.418)	0.026	0.003
13	1.08	0.10	0.022	(0.417)	0.019	0.002
14	1.17	0.10	0.022	(0.415)	0.019	0.002
15	1.25	0.10	0.022	(0.413)	0.019	0.002
16	1.33	0.10	0.022	(0.412)	0.019	0.002
17	1.42	0.10	0.022	(0.410)	0.019	0.002
18	1.50	0.10	0.022	(0.408)	0.019	0.002
19	1.58	0.10	0.022	(0.407)	0.019	0.002
20	1.67	0.10	0.022	(0.405)	0.019	0.002
21	1.75	0.10	0.022	(0.404)	0.019	0.002
22	1.83	0.13	0.029	(0.402)	0.026	0.003
23	1.92	0.13	0.029	(0.400)	0.026	0.003
24	2.00	0.13	0.029	(0.399)	0.026	0.003
25	2.08	0.13	0.029	(0.397)	0.026	0.003
26	2.17	0.13	0.029	(0.395)	0.026	0.003
27	2.25	0.13	0.029	(0.394)	0.026	0.003
28	2.33	0.13	0.029	(0.392)	0.026	0.003
29	2.42	0.13	0.029	(0.391)	0.026	0.003
30	2.50	0.13	0.029	(0.389)	0.026	0.003
31	2.58	0.17	0.036	(0.387)	0.032	0.004
32	2.67	0.17	0.036	(0.386)	0.032	0.004
33	2.75	0.17	0.036	(0.384)	0.032	0.004
34	2.83	0.17	0.036	(0.383)	0.032	0.004
35	2.92	0.17	0.036	(0.381)	0.032	0.004
36	3.00	0.17	0.036	(0.380)	0.032	0.004
37	3.08	0.17	0.036	(0.378)	0.032	0.004
38	3.17	0.17	0.036	(0.376)	0.032	0.004
39	3.25	0.17	0.036	(0.375)	0.032	0.004
40	3.33	0.17	0.036	(0.373)	0.032	0.004
41	3.42	0.17	0.036	(0.372)	0.032	0.004
42	3.50	0.17	0.036	(0.370)	0.032	0.004
43	3.58	0.17	0.036	(0.369)	0.032	0.004
44	3.67	0.17	0.036	(0.367)	0.032	0.004
45	3.75	0.17	0.036	(0.366)	0.032	0.004
46	3.83	0.20	0.043	(0.364)	0.039	0.004
47	3.92	0.20	0.043	(0.362)	0.039	0.004
48	4.00	0.20	0.043	(0.361)	0.039	0.004
49	4.08	0.20	0.043	(0.359)	0.039	0.004
50	4.17	0.20	0.043	(0.358)	0.039	0.004
51	4.25	0.20	0.043	(0.356)	0.039	0.004
52	4.33	0.23	0.050	(0.355)	0.045	0.005
53	4.42	0.23	0.050	(0.353)	0.045	0.005
54	4.50	0.23	0.050	(0.352)	0.045	0.005
55	4.58	0.23	0.050	(0.350)	0.045	0.005
56	4.67	0.23	0.050	(0.349)	0.045	0.005
57	4.75	0.23	0.050	(0.347)	0.045	0.005
58	4.83	0.27	0.058	(0.346)	0.052	0.006
59	4.92	0.27	0.058	(0.344)	0.052	0.006
60	5.00	0.27	0.058	(0.343)	0.052	0.006
61	5.08	0.20	0.043	(0.341)	0.039	0.004
62	5.17	0.20	0.043	(0.340)	0.039	0.004
63	5.25	0.20	0.043	(0.338)	0.039	0.004
64	5.33	0.23	0.050	(0.337)	0.045	0.005
65	5.42	0.23	0.050	(0.335)	0.045	0.005
66	5.50	0.23	0.050	(0.334)	0.045	0.005
67	5.58	0.27	0.058	(0.332)	0.052	0.006
68	5.67	0.27	0.058	(0.331)	0.052	0.006
69	5.75	0.27	0.058	(0.330)	0.052	0.006
70	5.83	0.27	0.058	(0.328)	0.052	0.006

71	5.92	0.27	0.058	(0.327)	0.052	0.006
72	6.00	0.27	0.058	(0.325)	0.052	0.006
73	6.08	0.30	0.065	(0.324)	0.058	0.006
74	6.17	0.30	0.065	(0.322)	0.058	0.006
75	6.25	0.30	0.065	(0.321)	0.058	0.006
76	6.33	0.30	0.065	(0.319)	0.058	0.006
77	6.42	0.30	0.065	(0.318)	0.058	0.006
78	6.50	0.30	0.065	(0.317)	0.058	0.006
79	6.58	0.33	0.072	(0.315)	0.065	0.007
80	6.67	0.33	0.072	(0.314)	0.065	0.007
81	6.75	0.33	0.072	(0.312)	0.065	0.007
82	6.83	0.33	0.072	(0.311)	0.065	0.007
83	6.92	0.33	0.072	(0.310)	0.065	0.007
84	7.00	0.33	0.072	(0.308)	0.065	0.007
85	7.08	0.33	0.072	(0.307)	0.065	0.007
86	7.17	0.33	0.072	(0.305)	0.065	0.007
87	7.25	0.33	0.072	(0.304)	0.065	0.007
88	7.33	0.37	0.079	(0.303)	0.071	0.008
89	7.42	0.37	0.079	(0.301)	0.071	0.008
90	7.50	0.37	0.079	(0.300)	0.071	0.008
91	7.58	0.40	0.086	(0.298)	0.078	0.009
92	7.67	0.40	0.086	(0.297)	0.078	0.009
93	7.75	0.40	0.086	(0.296)	0.078	0.009
94	7.83	0.43	0.094	(0.294)	0.084	0.009
95	7.92	0.43	0.094	(0.293)	0.084	0.009
96	8.00	0.43	0.094	(0.292)	0.084	0.009
97	8.08	0.50	0.108	(0.290)	0.097	0.011
98	8.17	0.50	0.108	(0.289)	0.097	0.011
99	8.25	0.50	0.108	(0.288)	0.097	0.011
100	8.33	0.50	0.108	(0.286)	0.097	0.011
101	8.42	0.50	0.108	(0.285)	0.097	0.011
102	8.50	0.50	0.108	(0.283)	0.097	0.011
103	8.58	0.53	0.115	(0.282)	0.104	0.012
104	8.67	0.53	0.115	(0.281)	0.104	0.012
105	8.75	0.53	0.115	(0.280)	0.104	0.012
106	8.83	0.57	0.122	(0.278)	0.110	0.012
107	8.92	0.57	0.122	(0.277)	0.110	0.012
108	9.00	0.57	0.122	(0.276)	0.110	0.012
109	9.08	0.63	0.137	(0.274)	0.123	0.014
110	9.17	0.63	0.137	(0.273)	0.123	0.014
111	9.25	0.63	0.137	(0.272)	0.123	0.014
112	9.33	0.67	0.144	(0.270)	0.130	0.014
113	9.42	0.67	0.144	(0.269)	0.130	0.014
114	9.50	0.67	0.144	(0.268)	0.130	0.014
115	9.58	0.70	0.151	(0.267)	0.136	0.015
116	9.67	0.70	0.151	(0.265)	0.136	0.015
117	9.75	0.70	0.151	(0.264)	0.136	0.015
118	9.83	0.73	0.158	(0.263)	0.143	0.016
119	9.92	0.73	0.158	(0.261)	0.143	0.016
120	10.00	0.73	0.158	(0.260)	0.143	0.016
121	10.08	0.50	0.108	(0.259)	0.097	0.011
122	10.17	0.50	0.108	(0.258)	0.097	0.011
123	10.25	0.50	0.108	(0.256)	0.097	0.011
124	10.33	0.50	0.108	(0.255)	0.097	0.011
125	10.42	0.50	0.108	(0.254)	0.097	0.011
126	10.50	0.50	0.108	(0.253)	0.097	0.011
127	10.58	0.67	0.144	(0.251)	0.130	0.014
128	10.67	0.67	0.144	(0.250)	0.130	0.014
129	10.75	0.67	0.144	(0.249)	0.130	0.014
130	10.83	0.67	0.144	(0.248)	0.130	0.014
131	10.92	0.67	0.144	(0.247)	0.130	0.014
132	11.00	0.67	0.144	(0.245)	0.130	0.014
133	11.08	0.63	0.137	(0.244)	0.123	0.014
134	11.17	0.63	0.137	(0.243)	0.123	0.014
135	11.25	0.63	0.137	(0.242)	0.123	0.014
136	11.33	0.63	0.137	(0.241)	0.123	0.014
137	11.42	0.63	0.137	(0.239)	0.123	0.014
138	11.50	0.63	0.137	(0.238)	0.123	0.014
139	11.58	0.57	0.122	(0.237)	0.110	0.012
140	11.67	0.57	0.122	(0.236)	0.110	0.012
141	11.75	0.57	0.122	(0.235)	0.110	0.012
142	11.83	0.60	0.130	(0.233)	0.117	0.013
143	11.92	0.60	0.130	(0.232)	0.117	0.013
144	12.00	0.60	0.130	(0.231)	0.117	0.013
145	12.08	0.83	0.180	(0.230)	0.162	0.018
146	12.17	0.83	0.180	(0.229)	0.162	0.018
147	12.25	0.83	0.180	(0.228)	0.162	0.018
148	12.33	0.87	0.187	(0.227)	0.168	0.019
149	12.42	0.87	0.187	(0.225)	0.168	0.019
150	12.50	0.87	0.187	(0.224)	0.168	0.019
151	12.58	0.93	0.202	(0.223)	0.181	0.020
152	12.67	0.93	0.202	(0.222)	0.181	0.020
153	12.75	0.93	0.202	(0.221)	0.181	0.020
154	12.83	0.97	0.209	(0.220)	0.188	0.021
155	12.92	0.97	0.209	(0.219)	0.188	0.021
156	13.00	0.97	0.209	(0.218)	0.188	0.021

157	13.08	1.13	0.245	0.216	(0.220)	0.028
158	13.17	1.13	0.245	0.215	(0.220)	0.029
159	13.25	1.13	0.245	0.214	(0.220)	0.031
160	13.33	1.13	0.245	0.213	(0.220)	0.032
161	13.42	1.13	0.245	0.212	(0.220)	0.033
162	13.50	1.13	0.245	0.211	(0.220)	0.034
163	13.58	0.77	0.166	(0.210)	0.149	0.017
164	13.67	0.77	0.166	(0.209)	0.149	0.017
165	13.75	0.77	0.166	(0.208)	0.149	0.017
166	13.83	0.77	0.166	(0.207)	0.149	0.017
167	13.92	0.77	0.166	(0.206)	0.149	0.017
168	14.00	0.77	0.166	(0.205)	0.149	0.017
169	14.08	0.90	0.194	(0.204)	0.175	0.019
170	14.17	0.90	0.194	(0.203)	0.175	0.019
171	14.25	0.90	0.194	(0.202)	0.175	0.019
172	14.33	0.87	0.187	(0.200)	0.168	0.019
173	14.42	0.87	0.187	(0.199)	0.168	0.019
174	14.50	0.87	0.187	(0.198)	0.168	0.019
175	14.58	0.87	0.187	(0.197)	0.168	0.019
176	14.67	0.87	0.187	(0.196)	0.168	0.019
177	14.75	0.87	0.187	(0.195)	0.168	0.019
178	14.83	0.83	0.180	(0.194)	0.162	0.018
179	14.92	0.83	0.180	(0.193)	0.162	0.018
180	15.00	0.83	0.180	(0.192)	0.162	0.018
181	15.08	0.80	0.173	(0.191)	0.156	0.017
182	15.17	0.80	0.173	(0.190)	0.156	0.017
183	15.25	0.80	0.173	(0.189)	0.156	0.017
184	15.33	0.77	0.166	(0.188)	0.149	0.017
185	15.42	0.77	0.166	(0.188)	0.149	0.017
186	15.50	0.77	0.166	(0.187)	0.149	0.017
187	15.58	0.63	0.137	(0.186)	0.123	0.014
188	15.67	0.63	0.137	(0.185)	0.123	0.014
189	15.75	0.63	0.137	(0.184)	0.123	0.014
190	15.83	0.63	0.137	(0.183)	0.123	0.014
191	15.92	0.63	0.137	(0.182)	0.123	0.014
192	16.00	0.63	0.137	(0.181)	0.123	0.014
193	16.08	0.13	0.029	(0.180)	0.026	0.003
194	16.17	0.13	0.029	(0.179)	0.026	0.003
195	16.25	0.13	0.029	(0.178)	0.026	0.003
196	16.33	0.13	0.029	(0.177)	0.026	0.003
197	16.42	0.13	0.029	(0.176)	0.026	0.003
198	16.50	0.13	0.029	(0.175)	0.026	0.003
199	16.58	0.10	0.022	(0.175)	0.019	0.002
200	16.67	0.10	0.022	(0.174)	0.019	0.002
201	16.75	0.10	0.022	(0.173)	0.019	0.002
202	16.83	0.10	0.022	(0.172)	0.019	0.002
203	16.92	0.10	0.022	(0.171)	0.019	0.002
204	17.00	0.10	0.022	(0.170)	0.019	0.002
205	17.08	0.17	0.036	(0.169)	0.032	0.004
206	17.17	0.17	0.036	(0.168)	0.032	0.004
207	17.25	0.17	0.036	(0.168)	0.032	0.004
208	17.33	0.17	0.036	(0.167)	0.032	0.004
209	17.42	0.17	0.036	(0.166)	0.032	0.004
210	17.50	0.17	0.036	(0.165)	0.032	0.004
211	17.58	0.17	0.036	(0.164)	0.032	0.004
212	17.67	0.17	0.036	(0.163)	0.032	0.004
213	17.75	0.17	0.036	(0.163)	0.032	0.004
214	17.83	0.13	0.029	(0.162)	0.026	0.003
215	17.92	0.13	0.029	(0.161)	0.026	0.003
216	18.00	0.13	0.029	(0.160)	0.026	0.003
217	18.08	0.13	0.029	(0.159)	0.026	0.003
218	18.17	0.13	0.029	(0.159)	0.026	0.003
219	18.25	0.13	0.029	(0.158)	0.026	0.003
220	18.33	0.13	0.029	(0.157)	0.026	0.003
221	18.42	0.13	0.029	(0.156)	0.026	0.003
222	18.50	0.13	0.029	(0.156)	0.026	0.003
223	18.58	0.10	0.022	(0.155)	0.019	0.002
224	18.67	0.10	0.022	(0.154)	0.019	0.002
225	18.75	0.10	0.022	(0.153)	0.019	0.002
226	18.83	0.07	0.014	(0.153)	0.013	0.001
227	18.92	0.07	0.014	(0.152)	0.013	0.001
228	19.00	0.07	0.014	(0.151)	0.013	0.001
229	19.08	0.10	0.022	(0.150)	0.019	0.002
230	19.17	0.10	0.022	(0.150)	0.019	0.002
231	19.25	0.10	0.022	(0.149)	0.019	0.002
232	19.33	0.13	0.029	(0.148)	0.026	0.003
233	19.42	0.13	0.029	(0.148)	0.026	0.003
234	19.50	0.13	0.029	(0.147)	0.026	0.003
235	19.58	0.10	0.022	(0.146)	0.019	0.002
236	19.67	0.10	0.022	(0.146)	0.019	0.002
237	19.75	0.10	0.022	(0.145)	0.019	0.002
238	19.83	0.07	0.014	(0.144)	0.013	0.001
239	19.92	0.07	0.014	(0.144)	0.013	0.001
240	20.00	0.07	0.014	(0.143)	0.013	0.001
241	20.08	0.10	0.022	(0.142)	0.019	0.002
242	20.17	0.10	0.022	(0.142)	0.019	0.002

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243  20.25     0.10      0.022       (  0.141)       0.019        0.002
244  20.33     0.10      0.022       (  0.141)       0.019        0.002
245  20.42     0.10      0.022       (  0.140)       0.019        0.002
246  20.50     0.10      0.022       (  0.139)       0.019        0.002
247  20.58     0.10      0.022       (  0.139)       0.019        0.002
248  20.67     0.10      0.022       (  0.138)       0.019        0.002
249  20.75     0.10      0.022       (  0.138)       0.019        0.002
250  20.83     0.07      0.014       (  0.137)       0.013        0.001
251  20.92     0.07      0.014       (  0.137)       0.013        0.001
252  21.00     0.07      0.014       (  0.136)       0.013        0.001
253  21.08     0.10      0.022       (  0.135)       0.019        0.002
254  21.17     0.10      0.022       (  0.135)       0.019        0.002
255  21.25     0.10      0.022       (  0.134)       0.019        0.002
256  21.33     0.07      0.014       (  0.134)       0.013        0.001
257  21.42     0.07      0.014       (  0.133)       0.013        0.001
258  21.50     0.07      0.014       (  0.133)       0.013        0.001
259  21.58     0.10      0.022       (  0.132)       0.019        0.002
260  21.67     0.10      0.022       (  0.132)       0.019        0.002
261  21.75     0.10      0.022       (  0.131)       0.019        0.002
262  21.83     0.07      0.014       (  0.131)       0.013        0.001
263  21.92     0.07      0.014       (  0.131)       0.013        0.001
264  22.00     0.07      0.014       (  0.130)       0.013        0.001
265  22.08     0.10      0.022       (  0.130)       0.019        0.002
266  22.17     0.10      0.022       (  0.129)       0.019        0.002
267  22.25     0.10      0.022       (  0.129)       0.019        0.002
268  22.33     0.07      0.014       (  0.128)       0.013        0.001
269  22.42     0.07      0.014       (  0.128)       0.013        0.001
270  22.50     0.07      0.014       (  0.128)       0.013        0.001
271  22.58     0.07      0.014       (  0.127)       0.013        0.001
272  22.67     0.07      0.014       (  0.127)       0.013        0.001
273  22.75     0.07      0.014       (  0.127)       0.013        0.001
274  22.83     0.07      0.014       (  0.126)       0.013        0.001
275  22.92     0.07      0.014       (  0.126)       0.013        0.001
276  23.00     0.07      0.014       (  0.126)       0.013        0.001
277  23.08     0.07      0.014       (  0.125)       0.013        0.001
278  23.17     0.07      0.014       (  0.125)       0.013        0.001
279  23.25     0.07      0.014       (  0.125)       0.013        0.001
280  23.33     0.07      0.014       (  0.125)       0.013        0.001
281  23.42     0.07      0.014       (  0.124)       0.013        0.001
282  23.50     0.07      0.014       (  0.124)       0.013        0.001
283  23.58     0.07      0.014       (  0.124)       0.013        0.001
284  23.67     0.07      0.014       (  0.124)       0.013        0.001
285  23.75     0.07      0.014       (  0.124)       0.013        0.001
286  23.83     0.07      0.014       (  0.123)       0.013        0.001
287  23.92     0.07      0.014       (  0.123)       0.013        0.001
288  24.00     0.07      0.014       (  0.123)       0.013        0.001
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =      2.2
      Flood volume = Effective rainfall      0.18(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       0.1(Ac.Ft)
      Total soil loss =      1.62(In)
      Total soil loss =     1.049(Ac.Ft)
      Total rainfall =      1.80(In)
      Flood volume =        5183.1 Cubic Feet
      Total soil loss =       45716.0 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.256(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0000      0.00  Q         |         |         |         |
   0+10       0.0001      0.01  Q         |         |         |         |
   0+15       0.0002      0.01  Q         |         |         |         |
   0+20       0.0002      0.01  Q         |         |         |         |
   0+25       0.0003      0.02  Q         |         |         |         |
   0+30       0.0005      0.02  Q         |         |         |         |
   0+35       0.0006      0.02  Q         |         |         |         |
   0+40       0.0007      0.02  Q         |         |         |         |
   0+45       0.0008      0.02  Q         |         |         |         |
   0+50       0.0009      0.02  Q         |         |         |         |
   0+55       0.0011      0.02  Q         |         |         |         |
   1+ 0       0.0012      0.02  Q         |         |         |         |
   1+ 5       0.0014      0.02  Q         |         |         |         |
   1+10       0.0015      0.02  Q         |         |         |         |
   1+15       0.0016      0.02  Q         |         |         |         |
   1+20       0.0017      0.02  Q         |         |         |         |
   1+25       0.0019      0.02  Q         |         |         |         |
   1+30       0.0020      0.02  Q         |         |         |         |
   1+35       0.0021      0.02  Q         |         |         |         |
```

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1+40       0.0022      0.02  Q          |          |          |          |
1+45       0.0023      0.02  Q          |          |          |          |
1+50       0.0025      0.02  Q          |          |          |          |
1+55       0.0026      0.02  Q          |          |          |          |
2+ 0       0.0028      0.02  Q          |          |          |          |
2+ 5       0.0029      0.02  Q          |          |          |          |
2+10       0.0031      0.02  QV         |          |          |          |
2+15       0.0032      0.02  QV         |          |          |          |
2+20       0.0034      0.02  QV         |          |          |          |
2+25       0.0035      0.02  QV         |          |          |          |
2+30       0.0037      0.02  QV         |          |          |          |
2+35       0.0039      0.02  QV         |          |          |          |
2+40       0.0040      0.03  QV         |          |          |          |
2+45       0.0042      0.03  QV         |          |          |          |
2+50       0.0044      0.03  QV         |          |          |          |
2+55       0.0046      0.03  QV         |          |          |          |
3+ 0       0.0048      0.03  QV         |          |          |          |
3+ 5       0.0050      0.03  QV         |          |          |          |
3+10       0.0052      0.03  QV         |          |          |          |
3+15       0.0054      0.03  QV         |          |          |          |
3+20       0.0056      0.03  QV         |          |          |          |
3+25       0.0058      0.03  QV         |          |          |          |
3+30       0.0060      0.03  Q V        |          |          |          |
3+35       0.0062      0.03  Q V        |          |          |          |
3+40       0.0064      0.03  Q V        |          |          |          |
3+45       0.0066      0.03  Q V        |          |          |          |
3+50       0.0068      0.03  Q V        |          |          |          |
3+55       0.0070      0.03  Q V        |          |          |          |
4+ 0       0.0072      0.03  Q V        |          |          |          |
4+ 5       0.0075      0.03  Q V        |          |          |          |
4+10       0.0077      0.03  Q V        |          |          |          |
4+15       0.0079      0.03  Q V        |          |          |          |
4+20       0.0082      0.04  Q V        |          |          |          |
4+25       0.0084      0.04  Q V        |          |          |          |
4+30       0.0087      0.04  Q V        |          |          |          |
4+35       0.0090      0.04  Q  V       |          |          |          |
4+40       0.0093      0.04  Q  V       |          |          |          |
4+45       0.0095      0.04  Q  V       |          |          |          |
4+50       0.0098      0.04  Q  V       |          |          |          |
4+55       0.0101      0.04  Q  V       |          |          |          |
5+ 0       0.0104      0.04  Q  V       |          |          |          |
5+ 5       0.0107      0.04  Q  V       |          |          |          |
5+10       0.0110      0.04  Q  V       |          |          |          |
5+15       0.0112      0.04  Q  V       |          |          |          |
5+20       0.0114      0.04  Q  V       |          |          |          |
5+25       0.0117      0.04  Q  V       |          |          |          |
5+30       0.0120      0.04  Q   V      |          |          |          |
5+35       0.0123      0.04  Q   V      |          |          |          |
5+40       0.0126      0.04  Q   V      |          |          |          |
5+45       0.0129      0.04  Q   V      |          |          |          |
5+50       0.0132      0.04  Q   V      |          |          |          |
5+55       0.0135      0.05  Q   V      |          |          |          |
6+ 0       0.0138      0.05  Q   V      |          |          |          |
6+ 5       0.0141      0.05  Q   V      |          |          |          |
6+10       0.0145      0.05  Q   V      |          |          |          |
6+15       0.0148      0.05  Q   V      |          |          |          |
6+20       0.0152      0.05  Q    V     |          |          |          |
6+25       0.0155      0.05  Q    V     |          |          |          |
6+30       0.0159      0.05  Q    V     |          |          |          |
6+35       0.0162      0.05  Q    V     |          |          |          |
6+40       0.0166      0.06  Q    V     |          |          |          |
6+45       0.0170      0.06  Q    V     |          |          |          |
6+50       0.0174      0.06  Q    V     |          |          |          |
6+55       0.0178      0.06  Q    V     |          |          |          |
7+ 0       0.0182      0.06  Q     V    |          |          |          |
7+ 5       0.0186      0.06  Q     V    |          |          |          |
7+10       0.0189      0.06  Q     V    |          |          |          |
7+15       0.0193      0.06  Q     V    |          |          |          |
7+20       0.0197      0.06  Q     V    |          |          |          |
7+25       0.0202      0.06  Q     V    |          |          |          |
7+30       0.0206      0.06  Q     V    |          |          |          |
7+35       0.0210      0.06  Q      V   |          |          |          |
7+40       0.0215      0.07  Q      V   |          |          |          |
7+45       0.0219      0.07  Q      V   |          |          |          |
7+50       0.0224      0.07  Q      V   |          |          |          |
7+55       0.0229      0.07  Q      V   |          |          |          |
8+ 0       0.0234      0.07  Q      V   |          |          |          |
8+ 5       0.0239      0.08  Q       V  |          |          |          |
8+10       0.0245      0.08  Q       V  |          |          |          |
8+15       0.0251      0.08  Q       V  |          |          |          |
8+20       0.0257      0.08  Q       V  |          |          |          |
8+25       0.0263      0.08  Q       V  |          |          |          |
8+30       0.0268      0.08  Q        V |          |          |          |
8+35       0.0274      0.09  Q        V |          |          |          |
8+40       0.0281      0.09  Q        V |          |          |          |
8+45       0.0287      0.09  Q        V |          |          |          |
```

```
 8+50       0.0293      0.09  Q        V|         |          |          |
 8+55       0.0300      0.09  Q         V         |          |          |
 9+ 0       0.0306      0.10  Q         V         |          |          |
 9+ 5       0.0313      0.10  Q         V         |          |          |
 9+10       0.0320      0.10  Q         V         |          |          |
 9+15       0.0328      0.11  Q         |V        |          |          |
 9+20       0.0335      0.11  Q         |V        |          |          |
 9+25       0.0343      0.11  Q         |V        |          |          |
 9+30       0.0351      0.11  Q         |V        |          |          |
 9+35       0.0358      0.11  Q         | V       |          |          |
 9+40       0.0366      0.12  Q         | V       |          |          |
 9+45       0.0375      0.12  Q         | V       |          |          |
 9+50       0.0383      0.12  Q         | V       |          |          |
 9+55       0.0391      0.12  Q         |  V      |          |          |
10+ 0       0.0400      0.12  Q         |  V      |          |          |
10+ 5       0.0408      0.11  Q         |  V      |          |          |
10+10       0.0414      0.09  Q         |  V      |          |          |
10+15       0.0420      0.09  Q         |   V     |          |          |
10+20       0.0426      0.09  Q         |   V     |          |          |
10+25       0.0432      0.09  Q         |   V     |          |          |
10+30       0.0438      0.08  Q         |   V     |          |          |
10+35       0.0444      0.09  Q         |   V     |          |          |
10+40       0.0452      0.11  Q         |    V    |          |          |
10+45       0.0459      0.11  Q         |    V    |          |          |
10+50       0.0467      0.11  Q         |    V    |          |          |
10+55       0.0475      0.11  Q         |    V    |          |          |
11+ 0       0.0483      0.11  Q         |     V   |          |          |
11+ 5       0.0490      0.11  Q         |     V   |          |          |
11+10       0.0498      0.11  Q         |     V   |          |          |
11+15       0.0505      0.11  Q         |     V   |          |          |
11+20       0.0513      0.11  Q         |      V  |          |          |
11+25       0.0520      0.11  Q         |      V  |          |          |
11+30       0.0527      0.11  Q         |      V  |          |          |
11+35       0.0534      0.10  Q         |      V  |          |          |
11+40       0.0541      0.10  Q         |       V |          |          |
11+45       0.0548      0.10  Q         |       V |          |          |
11+50       0.0555      0.10  Q         |       V |          |          |
11+55       0.0562      0.10  Q         |       V |          |          |
12+ 0       0.0569      0.10  Q         |        V|          |          |
12+ 5       0.0577      0.11  Q         |        V|          |          |
12+10       0.0586      0.13  Q         |        V|          |          |
12+15       0.0595      0.14  Q         |         V          |          |
12+20       0.0605      0.14  Q         |         V          |          |
12+25       0.0615      0.15  Q         |         V          |          |
12+30       0.0625      0.15  Q         |          |V        |          |
12+35       0.0635      0.15  Q         |          |V        |          |
12+40       0.0646      0.16  Q         |          |V        |          |
12+45       0.0657      0.16  Q         |          | V       |          |
12+50       0.0668      0.16  Q         |          | V       |          |
12+55       0.0679      0.16  Q         |          | V       |          |
13+ 0       0.0690      0.16  Q         |          |  V      |          |
13+ 5       0.0703      0.18  Q         |          |  V      |          |
13+10       0.0718      0.21  Q         |          |   V     |          |
13+15       0.0733      0.23  Q         |          |   V     |          |
13+20       0.0749      0.24  Q         |          |    V    |          |
13+25       0.0766      0.25  Q         |          |    V    |          |
13+30       0.0784      0.26  |Q        |          |     V   |          |
13+35       0.0799      0.22  Q         |          |     V   |          |
13+40       0.0810      0.16  Q         |          |      V  |          |
13+45       0.0820      0.14  Q         |          |      V  |          |
13+50       0.0829      0.14  Q         |          |      V  |          |
13+55       0.0838      0.13  Q         |          |       V |          |
14+ 0       0.0847      0.13  Q         |          |       V |          |
14+ 5       0.0857      0.14  Q         |          |       V |          |
14+10       0.0867      0.15  Q         |          |        V|          |
14+15       0.0877      0.15  Q         |          |        V|          |
14+20       0.0888      0.15  Q         |          |        V|          |
14+25       0.0898      0.15  Q         |          |         V          |
14+30       0.0908      0.15  Q         |          |         V          |
14+35       0.0918      0.15  Q         |          |         V          |
14+40       0.0928      0.15  Q         |          |          |V        |
14+45       0.0938      0.15  Q         |          |          |V        |
14+50       0.0948      0.15  Q         |          |          |V        |
14+55       0.0958      0.14  Q         |          |          | V       |
15+ 0       0.0968      0.14  Q         |          |          | V       |
15+ 5       0.0978      0.14  Q         |          |          | V       |
15+10       0.0987      0.14  Q         |          |          |  V      |
15+15       0.0997      0.14  Q         |          |          |  V      |
15+20       0.1006      0.13  Q         |          |          |  V      |
15+25       0.1015      0.13  Q         |          |          |   V     |
15+30       0.1024      0.13  Q         |          |          |   V     |
15+35       0.1032      0.12  Q         |          |          |   V     |
15+40       0.1040      0.11  Q         |          |          |   V     |
15+45       0.1048      0.11  Q         |          |          |    V    |
15+50       0.1055      0.11  Q         |          |          |    V    |
15+55       0.1062      0.11  Q         |          |          |    V    |
```

16+ 0	0.1070	0.11	Q	|	|	|	V |
16+ 5	0.1075	0.08	Q	|	|	|	V |
16+10	0.1078	0.04	Q	|	|	|	V |
16+15	0.1080	0.03	Q	|	|	|	V |
16+20	0.1082	0.03	Q	|	|	|	V |
16+25	0.1084	0.02	Q	|	|	|	V |
16+30	0.1085	0.02	Q	|	|	|	V |
16+35	0.1087	0.02	Q	|	|	|	V |
16+40	0.1088	0.02	Q	|	|	|	V |
16+45	0.1089	0.02	Q	|	|	|	V |
16+50	0.1090	0.02	Q	|	|	|	V |
16+55	0.1092	0.02	Q	|	|	|	V |
17+ 0	0.1093	0.02	Q	|	|	|	V |
17+ 5	0.1094	0.02	Q	|	|	|	V |
17+10	0.1096	0.03	Q	|	|	|	V |
17+15	0.1098	0.03	Q	|	|	|	V |
17+20	0.1100	0.03	Q	|	|	|	V |
17+25	0.1102	0.03	Q	|	|	|	V |
17+30	0.1104	0.03	Q	|	|	|	V |
17+35	0.1106	0.03	Q	|	|	|	V |
17+40	0.1108	0.03	Q	|	|	|	V |
17+45	0.1110	0.03	Q	|	|	|	V |
17+50	0.1111	0.03	Q	|	|	|	V |
17+55	0.1113	0.02	Q	|	|	|	V |
18+ 0	0.1115	0.02	Q	|	|	|	V |
18+ 5	0.1116	0.02	Q	|	|	|	V |
18+10	0.1118	0.02	Q	|	|	|	V |
18+15	0.1119	0.02	Q	|	|	|	V |
18+20	0.1121	0.02	Q	|	|	|	V |
18+25	0.1122	0.02	Q	|	|	|	V |
18+30	0.1124	0.02	Q	|	|	|	V |
18+35	0.1125	0.02	Q	|	|	|	V |
18+40	0.1127	0.02	Q	|	|	|	V |
18+45	0.1128	0.02	Q	|	|	|	V |
18+50	0.1129	0.02	Q	|	|	|	V |
18+55	0.1130	0.01	Q	|	|	|	V |
19+ 0	0.1131	0.01	Q	|	|	|	V |
19+ 5	0.1132	0.01	Q	|	|	|	V |
19+10	0.1133	0.02	Q	|	|	|	V |
19+15	0.1134	0.02	Q	|	|	|	V |
19+20	0.1135	0.02	Q	|	|	|	V |
19+25	0.1136	0.02	Q	|	|	|	V |
19+30	0.1138	0.02	Q	|	|	|	V |
19+35	0.1139	0.02	Q	|	|	|	V |
19+40	0.1141	0.02	Q	|	|	|	V |
19+45	0.1142	0.02	Q	|	|	|	V |
19+50	0.1143	0.02	Q	|	|	|	V |
19+55	0.1144	0.01	Q	|	|	|	V |
20+ 0	0.1145	0.01	Q	|	|	|	V |
20+ 5	0.1146	0.01	Q	|	|	|	V |
20+10	0.1147	0.02	Q	|	|	|	V |
20+15	0.1148	0.02	Q	|	|	|	V |
20+20	0.1149	0.02	Q	|	|	|	V |
20+25	0.1150	0.02	Q	|	|	|	V |
20+30	0.1151	0.02	Q	|	|	|	V |
20+35	0.1152	0.02	Q	|	|	|	V |
20+40	0.1154	0.02	Q	|	|	|	V |
20+45	0.1155	0.02	Q	|	|	|	V |
20+50	0.1156	0.02	Q	|	|	|	V |
20+55	0.1157	0.01	Q	|	|	|	V |
21+ 0	0.1157	0.01	Q	|	|	|	V |
21+ 5	0.1158	0.01	Q	|	|	|	V |
21+10	0.1159	0.02	Q	|	|	|	V |
21+15	0.1161	0.02	Q	|	|	|	V|
21+20	0.1162	0.01	Q	|	|	|	V|
21+25	0.1163	0.01	Q	|	|	|	V|
21+30	0.1163	0.01	Q	|	|	|	V|
21+35	0.1164	0.01	Q	|	|	|	V|
21+40	0.1165	0.02	Q	|	|	|	V|
21+45	0.1166	0.02	Q	|	|	|	V|
21+50	0.1167	0.01	Q	|	|	|	V|
21+55	0.1168	0.01	Q	|	|	|	V|
22+ 0	0.1169	0.01	Q	|	|	|	V|
22+ 5	0.1170	0.01	Q	|	|	|	V|
22+10	0.1171	0.02	Q	|	|	|	V|
22+15	0.1172	0.02	Q	|	|	|	V|
22+20	0.1173	0.01	Q	|	|	|	V|
22+25	0.1174	0.01	Q	|	|	|	V|
22+30	0.1175	0.01	Q	|	|	|	V|
22+35	0.1176	0.01	Q	|	|	|	V|
22+40	0.1177	0.01	Q	|	|	|	V|
22+45	0.1177	0.01	Q	|	|	|	V|
22+50	0.1178	0.01	Q	|	|	|	V|
22+55	0.1179	0.01	Q	|	|	|	V|
23+ 0	0.1180	0.01	Q	|	|	|	V|
23+ 5	0.1180	0.01	Q	|	|	|	V|

```
   23+10       0.1181      0.01  Q          |          |          |         v|
   23+15       0.1182      0.01  Q          |          |          |         v|
   23+20       0.1183      0.01  Q          |          |          |         v|
   23+25       0.1184      0.01  Q          |          |          |         v|
   23+30       0.1184      0.01  Q          |          |          |         v|
   23+35       0.1185      0.01  Q          |          |          |         v|
   23+40       0.1186      0.01  Q          |          |          |         v|
   23+45       0.1187      0.01  Q          |          |          |         v|
   23+50       0.1187      0.01  Q          |          |          |         v|
   23+55       0.1188      0.01  Q          |          |          |         v|
   24+ 0       0.1189      0.01  Q          |          |          |         v|
   24+ 5       0.1190      0.01  Q          |          |          |         v|
   24+10       0.1190      0.00  Q          |          |          |         v|
   24+15       0.1190      0.00  Q          |          |          |         v|
   24+20       0.1190      0.00  Q          |          |          |         v|
   24+25       0.1190      0.00  Q          |          |          |          v
-------------------------------------------------------------------------------
```

```
       U n i t   H y d r o g r a p h   A n a l y s i s

       Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2008, Version 8.1
              Study date  04/22/24 File: EX3515.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =       7.79(Ac.)  =      0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =       7.79(Ac.)  =      0.012 Sq. Mi.
Length along longest watercourse =    1222.00(Ft.)
Length along longest watercourse measured to centroid =     611.00(Ft.)
Length along longest watercourse =      0.231 Mi.
Length along longest watercourse measured to centroid =      0.116 Mi.
Difference in elevation =      89.00(Ft.)
Slope along watercourse =    384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.059 Hr.
Lag time =     3.52 Min.
25% of lag time =     0.88 Min.
40% of lag time =     1.41 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            0.50                 3.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            1.30                10.13

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.687(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    0.687(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     7.790           91.00          0.000
 Total Area Entered =      7.79(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
			Sum = 100.000 Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.272	(0.246)	0.245	0.027
2	0.17	4.20	0.346	0.246	(0.312)	0.100
3	0.25	4.40	0.363	0.246	(0.327)	0.117
4	0.33	4.80	0.396	0.246	(0.356)	0.150
5	0.42	5.20	0.429	0.246	(0.386)	0.183
6	0.50	6.20	0.511	0.246	(0.460)	0.265
7	0.58	6.80	0.561	0.246	(0.505)	0.315
8	0.67	8.80	0.726	0.246	(0.653)	0.479
9	0.75	13.90	1.146	0.246	(1.032)	0.900
10	0.83	31.40	2.590	0.246	(2.331)	2.344
11	0.92	7.20	0.594	0.246	(0.534)	0.347
12	1.00	3.80	0.313	0.246	(0.282)	0.067
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.3

Flood volume = Effective rainfall 0.44(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft)
Total soil loss = 0.25(In)
Total soil loss = 0.160(Ac.Ft)
Total rainfall = 0.69(In)
Flood volume = 12472.9 Cubic Feet
Total soil loss = 6963.2 Cubic Feet

Peak flow rate of this hydrograph = 10.731(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0005	0.07	Q				
0+10	0.0028	0.35	Q				
0+15	0.0076	0.68	Q				
0+20	0.0138	0.90	Q				
0+25	0.0218	1.16	QV				
0+30	0.0324	1.54	QV				
0+35	0.0463	2.03	Q V				
0+40	0.0650	2.71	Q V				
0+45	0.0957	4.45	Q V				
0+50	0.1628	9.75	Q V				
0+55	0.2367	10.73	Q V				
1+ 0	0.2651	4.12	Q V				
1+ 5	0.2773	1.77	Q V				
1+10	0.2830	0.82	Q V				
1+15	0.2859	0.42	Q V				
1+20	0.2863	0.06	Q V				
1+25	0.2863	0.01	Q V				

```
        U n i t   H y d r o g r a p h   A n a l y s i s

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                Study date  04/22/24 File: EX3535.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =       7.79(Ac.)  =      0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =       7.79(Ac.)  =      0.012 Sq. Mi.
Length along longest watercourse =    1222.00(Ft.)
Length along longest watercourse measured to centroid =     611.00(Ft.)
Length along longest watercourse =      0.231 Mi.
Length along longest watercourse measured to centroid =      0.116 Mi.
Difference in elevation =      89.00(Ft.)
Slope along watercourse =    384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.059 Hr.
Lag time =     3.52 Min.
25% of lag time =     0.88 Min.
40% of lag time =     1.41 Min.
Unit time =     5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            0.80                 6.23

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            2.00                15.58

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.800(In)
Area Averaged 100-Year Rainfall =    2.000(In)

Point rain (area averaged) =    1.081(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    1.081(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     7.790           91.00          0.000
 Total Area Entered =      7.79(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  79.8      0.246     0.000        0.246       1.000      0.246
                                                 Sum (F) =   0.246
Area averaged mean soil loss (F) (In/Hr) =  0.246
Minimum soil loss rate ((In/Hr)) =  0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
		Sum = 100.000	Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.169	(0.246)	0.152	0.017
2	0.17	1.30	0.169	(0.246)	0.152	0.017
3	0.25	1.10	0.143	(0.246)	0.128	0.014
4	0.33	1.50	0.195	(0.246)	0.175	0.019
5	0.42	1.50	0.195	(0.246)	0.175	0.019
6	0.50	1.80	0.234	(0.246)	0.210	0.023
7	0.58	1.50	0.195	(0.246)	0.175	0.019
8	0.67	1.80	0.234	(0.246)	0.210	0.023
9	0.75	1.80	0.234	(0.246)	0.210	0.023
10	0.83	1.50	0.195	(0.246)	0.175	0.019
11	0.92	1.60	0.208	(0.246)	0.187	0.021
12	1.00	1.80	0.234	(0.246)	0.210	0.023
13	1.08	2.20	0.285	0.246	(0.257)	0.039
14	1.17	2.20	0.285	0.246	(0.257)	0.039
15	1.25	2.20	0.285	0.246	(0.257)	0.039
16	1.33	2.00	0.259	(0.246)	0.234	0.026
17	1.42	2.60	0.337	0.246	(0.304)	0.091
18	1.50	2.70	0.350	0.246	(0.315)	0.104
19	1.58	2.40	0.311	0.246	(0.280)	0.065
20	1.67	2.70	0.350	0.246	(0.315)	0.104
21	1.75	3.30	0.428	0.246	(0.385)	0.182
22	1.83	3.10	0.402	0.246	(0.362)	0.156
23	1.92	2.90	0.376	0.246	(0.339)	0.130
24	2.00	3.00	0.389	0.246	(0.350)	0.143
25	2.08	3.10	0.402	0.246	(0.362)	0.156
26	2.17	4.20	0.545	0.246	(0.490)	0.298
27	2.25	5.00	0.649	0.246	(0.584)	0.402
28	2.33	3.50	0.454	0.246	(0.409)	0.208
29	2.42	6.80	0.882	0.246	(0.794)	0.636
30	2.50	7.30	0.947	0.246	(0.852)	0.701
31	2.58	8.20	1.064	0.246	(0.957)	0.817
32	2.67	5.90	0.765	0.246	(0.689)	0.519
33	2.75	2.00	0.259	(0.246)	0.234	0.026
34	2.83	1.80	0.234	(0.246)	0.210	0.023
35	2.92	1.80	0.234	(0.246)	0.210	0.023
36	3.00	0.60	0.078	(0.246)	0.070	0.008
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.2

Flood volume = Effective rainfall 0.43(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft)
Total soil loss = 0.65(In)
Total soil loss = 0.422(Ac.Ft)
Total rainfall = 1.08(In)
Flood volume = 12193.1 Cubic Feet
Total soil loss = 18376.0 Cubic Feet

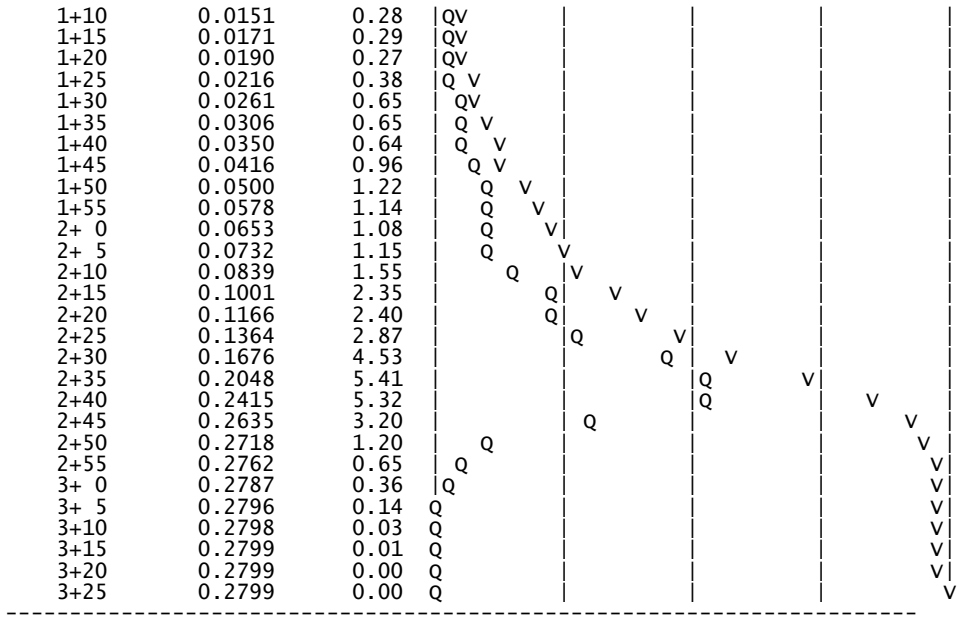
Peak flow rate of this hydrograph = 5.413(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0003	0.04	Q	|	|	|	|
0+10	0.0010	0.10	Q	|	|	|	|
0+15	0.0018	0.11	Q	|	|	|	|
0+20	0.0026	0.12	Q	|	|	|	|
0+25	0.0036	0.14	Q	|	|	|	|
0+30	0.0047	0.16	Q	|	|	|	|
0+35	0.0059	0.17	Q	|	|	|	|
0+40	0.0070	0.17	QV	|	|	|	|
0+45	0.0082	0.18	QV	|	|	|	|
0+50	0.0094	0.17	QV	|	|	|	|
0+55	0.0105	0.16	QV	|	|	|	|
1+ 0	0.0117	0.17	QV	|	|	|	|
1+ 5	0.0132	0.22	QV	|	|	|	|


1+10 0.0151 0.28
1+15 0.0171 0.29
1+20 0.0190 0.27
1+25 0.0216 0.38
1+30 0.0261 0.65
1+35 0.0306 0.65
1+40 0.0350 0.64
1+45 0.0416 0.96
1+50 0.0500 1.22
1+55 0.0578 1.14
2+ 0 0.0653 1.08
2+ 5 0.0732 1.15
2+10 0.0839 1.55
2+15 0.1001 2.35
2+20 0.1166 2.40
2+25 0.1364 2.87
2+30 0.1676 4.53
2+35 0.2048 5.41
2+40 0.2415 5.32
2+45 0.2635 3.20
2+50 0.2718 1.20
2+55 0.2762 0.65
3+ 0 0.2787 0.36
3+ 5 0.2796 0.14
3+10 0.2798 0.03
3+15 0.2799 0.01
3+20 0.2799 0.00
3+25 0.2799 0.00

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX3565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 1222.00(Ft.)
Length along longest watercourse measured to centroid = 611.00(Ft.)
Length along longest watercourse = 0.231 Mi.
Length along longest watercourse measured to centroid = 0.116 Mi.
Difference in elevation = 89.00(Ft.)
Slope along watercourse = 384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.059 Hr.
Lag time = 3.52 Min.
25% of lag time = 0.88 Min.
40% of lag time = 1.41 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.10	8.57

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	3.00	23.37

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.545(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.545(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	91.00	0.000

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
			Sum = 100.000	Sum= 7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.093	(0.246)	0.083	0.009
2	0.17	0.60	0.111	(0.246)	0.100	0.011
3	0.25	0.60	0.111	(0.246)	0.100	0.011
4	0.33	0.60	0.111	(0.246)	0.100	0.011
5	0.42	0.60	0.111	(0.246)	0.100	0.011
6	0.50	0.70	0.130	(0.246)	0.117	0.013
7	0.58	0.70	0.130	(0.246)	0.117	0.013
8	0.67	0.70	0.130	(0.246)	0.117	0.013
9	0.75	0.70	0.130	(0.246)	0.117	0.013
10	0.83	0.70	0.130	(0.246)	0.117	0.013
11	0.92	0.70	0.130	(0.246)	0.117	0.013
12	1.00	0.80	0.148	(0.246)	0.133	0.015
13	1.08	0.80	0.148	(0.246)	0.133	0.015
14	1.17	0.80	0.148	(0.246)	0.133	0.015
15	1.25	0.80	0.148	(0.246)	0.133	0.015
16	1.33	0.80	0.148	(0.246)	0.133	0.015
17	1.42	0.80	0.148	(0.246)	0.133	0.015
18	1.50	0.80	0.148	(0.246)	0.133	0.015
19	1.58	0.80	0.148	(0.246)	0.133	0.015
20	1.67	0.80	0.148	(0.246)	0.133	0.015
21	1.75	0.80	0.148	(0.246)	0.133	0.015
22	1.83	0.80	0.148	(0.246)	0.133	0.015
23	1.92	0.80	0.148	(0.246)	0.133	0.015
24	2.00	0.90	0.167	(0.246)	0.150	0.017
25	2.08	0.80	0.148	(0.246)	0.133	0.015
26	2.17	0.90	0.167	(0.246)	0.150	0.017
27	2.25	0.90	0.167	(0.246)	0.150	0.017
28	2.33	0.90	0.167	(0.246)	0.150	0.017
29	2.42	0.90	0.167	(0.246)	0.150	0.017
30	2.50	0.90	0.167	(0.246)	0.150	0.017
31	2.58	0.90	0.167	(0.246)	0.150	0.017
32	2.67	0.90	0.167	(0.246)	0.150	0.017
33	2.75	1.00	0.185	(0.246)	0.167	0.019
34	2.83	1.00	0.185	(0.246)	0.167	0.019
35	2.92	1.00	0.185	(0.246)	0.167	0.019
36	3.00	1.00	0.185	(0.246)	0.167	0.019
37	3.08	1.00	0.185	(0.246)	0.167	0.019
38	3.17	1.10	0.204	(0.246)	0.184	0.020
39	3.25	1.10	0.204	(0.246)	0.184	0.020
40	3.33	1.10	0.204	(0.246)	0.184	0.020
41	3.42	1.20	0.222	(0.246)	0.200	0.022
42	3.50	1.30	0.241	(0.246)	0.217	0.024
43	3.58	1.40	0.260	(0.246)	0.234	0.026
44	3.67	1.40	0.260	(0.246)	0.234	0.026
45	3.75	1.50	0.278	0.246	(0.250)	0.032
46	3.83	1.50	0.278	0.246	(0.250)	0.032
47	3.92	1.60	0.297	0.246	(0.267)	0.050
48	4.00	1.60	0.297	0.246	(0.267)	0.050
49	4.08	1.70	0.315	0.246	(0.284)	0.069
50	4.17	1.80	0.334	0.246	(0.300)	0.087
51	4.25	1.90	0.352	0.246	(0.317)	0.106
52	4.33	2.00	0.371	0.246	(0.334)	0.124
53	4.42	2.10	0.389	0.246	(0.350)	0.143
54	4.50	2.10	0.389	0.246	(0.350)	0.143
55	4.58	2.20	0.408	0.246	(0.367)	0.162
56	4.67	2.30	0.426	0.246	(0.384)	0.180
57	4.75	2.40	0.445	0.246	(0.400)	0.199
58	4.83	2.40	0.445	0.246	(0.400)	0.199
59	4.92	2.50	0.463	0.246	(0.417)	0.217
60	5.00	2.60	0.482	0.246	(0.434)	0.236
61	5.08	3.10	0.575	0.246	(0.517)	0.328
62	5.17	3.60	0.667	0.246	(0.601)	0.421
63	5.25	3.90	0.723	0.246	(0.651)	0.477
64	5.33	4.20	0.779	0.246	(0.701)	0.532
65	5.42	4.70	0.871	0.246	(0.784)	0.625
66	5.50	5.60	1.038	0.246	(0.934)	0.792
67	5.58	1.90	0.352	0.246	(0.317)	0.106
68	5.67	0.90	0.167	(0.246)	0.150	0.017
69	5.75	0.60	0.111	(0.246)	0.100	0.011
70	5.83	0.50	0.093	(0.246)	0.083	0.009

```
71   5.92     0.30      0.056       (  0.246)       0.050        0.006
72   6.00     0.20      0.037       (  0.246)       0.033        0.004
               (Loss Rate Not Used)
   Sum =     100.0                                  Sum =     6.1
      Flood volume = Effective rainfall      0.51(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       0.3(Ac.Ft)
      Total soil loss =      1.04(In)
      Total soil loss =     0.675(Ac.Ft)
      Total rainfall =      1.54(In)
      Flood volume =       14293.7 Cubic Feet
      Total soil loss =       29394.9 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      5.089(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f     H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0002      0.02  Q         |         |         |         |
  0+10       0.0006      0.06  Q         |         |         |         |
  0+15       0.0011      0.08  Q         |         |         |         |
  0+20       0.0017      0.08  Q         |         |         |         |
  0+25       0.0023      0.09  Q         |         |         |         |
  0+30       0.0029      0.09  Q         |         |         |         |
  0+35       0.0036      0.10  Q         |         |         |         |
  0+40       0.0043      0.10  Q         |         |         |         |
  0+45       0.0050      0.10  Q         |         |         |         |
  0+50       0.0057      0.10  Q         |         |         |         |
  0+55       0.0064      0.10  Q         |         |         |         |
  1+ 0       0.0071      0.11  Q         |         |         |         |
  1+ 5       0.0079      0.11  Q         |         |         |         |
  1+10       0.0087      0.12  QV        |         |         |         |
  1+15       0.0095      0.12  QV        |         |         |         |
  1+20       0.0103      0.12  QV        |         |         |         |
  1+25       0.0111      0.12  QV        |         |         |         |
  1+30       0.0119      0.12  QV        |         |         |         |
  1+35       0.0127      0.12  QV        |         |         |         |
  1+40       0.0135      0.12  QV        |         |         |         |
  1+45       0.0143      0.12  QV        |         |         |         |
  1+50       0.0151      0.12  QV        |         |         |         |
  1+55       0.0159      0.12  QV        |         |         |         |
  2+ 0       0.0167      0.12  Q V       |         |         |         |
  2+ 5       0.0176      0.12  Q V       |         |         |         |
  2+10       0.0184      0.12  Q V       |         |         |         |
  2+15       0.0193      0.13  Q V       |         |         |         |
  2+20       0.0202      0.13  Q V       |         |         |         |
  2+25       0.0211      0.13  Q V       |         |         |         |
  2+30       0.0220      0.13  Q V       |         |         |         |
  2+35       0.0229      0.13  Q V       |         |         |         |
  2+40       0.0238      0.13  Q V       |         |         |         |
  2+45       0.0248      0.14  Q  V      |         |         |         |
  2+50       0.0257      0.14  Q  V      |         |         |         |
  2+55       0.0267      0.14  Q  V      |         |         |         |
  3+ 0       0.0277      0.14  Q  V      |         |         |         |
  3+ 5       0.0287      0.15  Q  V      |         |         |         |
  3+10       0.0298      0.15  Q  V      |         |         |         |
  3+15       0.0308      0.16  Q  V      |         |         |         |
  3+20       0.0319      0.16  Q  V      |         |         |         |
  3+25       0.0331      0.16  Q   V     |         |         |         |
  3+30       0.0343      0.18  Q   V     |         |         |         |
  3+35       0.0356      0.19  Q   V     |         |         |         |
  3+40       0.0370      0.20  Q   V     |         |         |         |
  3+45       0.0384      0.22  Q   V     |         |         |         |
  3+50       0.0401      0.24  Q   V     |         |         |         |
  3+55       0.0421      0.29  |Q   V     |         |         |         |
  4+ 0       0.0446      0.36  |Q   V     |         |         |         |
  4+ 5       0.0475      0.43  |Q   V     |         |         |         |
  4+10       0.0513      0.55  | Q   V    |         |         |         |
  4+15       0.0560      0.68  | Q   V    |         |         |         |
  4+20       0.0617      0.83  |  Q   V   |         |         |         |
  4+25       0.0684      0.97  |  Q    V  |         |         |         |
  4+30       0.0757      1.07  |   Q    V |         |         |         |
  4+35       0.0836      1.15  |   Q     V|         |         |         |
  4+40       0.0924      1.27  |    Q    |V        |         |         |
  4+45       0.1021      1.41  |    Q    | V       |         |         |
  4+50       0.1125      1.51  |     Q   |  V      |         |         |
  4+55       0.1234      1.58  |     Q   |    V    |         |         |
  5+ 0       0.1352      1.71  |     Q   |     V   |         |         |
  5+ 5       0.1492      2.03  |       Q |       V |         |         |
  5+10       0.1673      2.63  |         Q         V         |         |
  5+15       0.1894      3.21  |         | Q       |  V      |         |
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    5+20       0.2148      3.68  |          |   Q      |     V    |          |
    5+25       0.2439      4.23  |          |     Q    |        V |          |
    5+30       0.2789      5.09  |          |        Q |          |   V      |
    5+35       0.3076      4.17  |          |      Q   |          |      V   |
    5+40       0.3186      1.59  |     Q    |          |          |        V |
    5+45       0.3235      0.71  | Q        |          |          |          V|
    5+50       0.3261      0.38  |Q         |          |          |          V|
    5+55       0.3274      0.19  Q          |          |          |          V|
    6+ 0       0.3278      0.06  Q          |          |          |          V|
    6+ 5       0.3280      0.03  Q          |          |          |          V|
    6+10       0.3281      0.01  Q          |          |          |          V|
    6+15       0.3281      0.00  Q          |          |          |          V|
    6+20       0.3281      0.00  Q          |          |          |          V|
    6+25       0.3281      0.00  Q          |          |          |           V
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX35245.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 1222.00(Ft.)
Length along longest watercourse measured to centroid = 611.00(Ft.)
Length along longest watercourse = 0.231 Mi.
Length along longest watercourse measured to centroid = 0.116 Mi.
Difference in elevation = 89.00(Ft.)
Slope along watercourse = 384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.059 Hr.
Lag time = 3.52 Min.
25% of lag time = 0.88 Min.
40% of lag time = 1.41 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.80	14.02

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	5.00	38.95

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 2.550(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 2.549(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	91.00	0.000

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.000	0.246	1.000	0.246
					Sum (F) =	0.246

Area averaged mean soil loss (F) (In/Hr) = 0.246
Minimum soil loss rate ((In/Hr)) = 0.123
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
			Sum = 100.000	Sum= 7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.020	(0.437)	0.018	0.002
2	0.17	0.07	0.020	(0.435)	0.018	0.002
3	0.25	0.07	0.020	(0.433)	0.018	0.002
4	0.33	0.10	0.031	(0.432)	0.028	0.003
5	0.42	0.10	0.031	(0.430)	0.028	0.003
6	0.50	0.10	0.031	(0.428)	0.028	0.003
7	0.58	0.10	0.031	(0.427)	0.028	0.003
8	0.67	0.10	0.031	(0.425)	0.028	0.003
9	0.75	0.10	0.031	(0.423)	0.028	0.003
10	0.83	0.13	0.041	(0.422)	0.037	0.004
11	0.92	0.13	0.041	(0.420)	0.037	0.004
12	1.00	0.13	0.041	(0.418)	0.037	0.004
13	1.08	0.10	0.031	(0.417)	0.028	0.003
14	1.17	0.10	0.031	(0.415)	0.028	0.003
15	1.25	0.10	0.031	(0.413)	0.028	0.003
16	1.33	0.10	0.031	(0.412)	0.028	0.003
17	1.42	0.10	0.031	(0.410)	0.028	0.003
18	1.50	0.10	0.031	(0.408)	0.028	0.003
19	1.58	0.10	0.031	(0.407)	0.028	0.003
20	1.67	0.10	0.031	(0.405)	0.028	0.003
21	1.75	0.10	0.031	(0.404)	0.028	0.003
22	1.83	0.13	0.041	(0.402)	0.037	0.004
23	1.92	0.13	0.041	(0.400)	0.037	0.004
24	2.00	0.13	0.041	(0.399)	0.037	0.004
25	2.08	0.13	0.041	(0.397)	0.037	0.004
26	2.17	0.13	0.041	(0.395)	0.037	0.004
27	2.25	0.13	0.041	(0.394)	0.037	0.004
28	2.33	0.13	0.041	(0.392)	0.037	0.004
29	2.42	0.13	0.041	(0.391)	0.037	0.004
30	2.50	0.13	0.041	(0.389)	0.037	0.004
31	2.58	0.17	0.051	(0.387)	0.046	0.005
32	2.67	0.17	0.051	(0.386)	0.046	0.005
33	2.75	0.17	0.051	(0.384)	0.046	0.005
34	2.83	0.17	0.051	(0.383)	0.046	0.005
35	2.92	0.17	0.051	(0.381)	0.046	0.005
36	3.00	0.17	0.051	(0.380)	0.046	0.005
37	3.08	0.17	0.051	(0.378)	0.046	0.005
38	3.17	0.17	0.051	(0.376)	0.046	0.005
39	3.25	0.17	0.051	(0.375)	0.046	0.005
40	3.33	0.17	0.051	(0.373)	0.046	0.005
41	3.42	0.17	0.051	(0.372)	0.046	0.005
42	3.50	0.17	0.051	(0.370)	0.046	0.005
43	3.58	0.17	0.051	(0.369)	0.046	0.005
44	3.67	0.17	0.051	(0.367)	0.046	0.005
45	3.75	0.17	0.051	(0.366)	0.046	0.005
46	3.83	0.20	0.061	(0.364)	0.055	0.006
47	3.92	0.20	0.061	(0.362)	0.055	0.006
48	4.00	0.20	0.061	(0.361)	0.055	0.006
49	4.08	0.20	0.061	(0.359)	0.055	0.006
50	4.17	0.20	0.061	(0.358)	0.055	0.006
51	4.25	0.20	0.061	(0.356)	0.055	0.006
52	4.33	0.23	0.071	(0.355)	0.064	0.007
53	4.42	0.23	0.071	(0.353)	0.064	0.007
54	4.50	0.23	0.071	(0.352)	0.064	0.007
55	4.58	0.23	0.071	(0.350)	0.064	0.007
56	4.67	0.23	0.071	(0.349)	0.064	0.007
57	4.75	0.23	0.071	(0.347)	0.064	0.007
58	4.83	0.27	0.082	(0.346)	0.073	0.008
59	4.92	0.27	0.082	(0.344)	0.073	0.008
60	5.00	0.27	0.082	(0.343)	0.073	0.008
61	5.08	0.20	0.061	(0.341)	0.055	0.006
62	5.17	0.20	0.061	(0.340)	0.055	0.006
63	5.25	0.20	0.061	(0.338)	0.055	0.006
64	5.33	0.23	0.071	(0.337)	0.064	0.007
65	5.42	0.23	0.071	(0.335)	0.064	0.007
66	5.50	0.23	0.071	(0.334)	0.064	0.007
67	5.58	0.27	0.082	(0.332)	0.073	0.008
68	5.67	0.27	0.082	(0.331)	0.073	0.008
69	5.75	0.27	0.082	(0.330)	0.073	0.008
70	5.83	0.27	0.082	(0.328)	0.073	0.008

71	5.92	0.27	0.082	(0.327)	0.073	0.008
72	6.00	0.27	0.082	(0.325)	0.073	0.008
73	6.08	0.30	0.092	(0.324)	0.083	0.009
74	6.17	0.30	0.092	(0.322)	0.083	0.009
75	6.25	0.30	0.092	(0.321)	0.083	0.009
76	6.33	0.30	0.092	(0.319)	0.083	0.009
77	6.42	0.30	0.092	(0.318)	0.083	0.009
78	6.50	0.30	0.092	(0.317)	0.083	0.009
79	6.58	0.33	0.102	(0.315)	0.092	0.010
80	6.67	0.33	0.102	(0.314)	0.092	0.010
81	6.75	0.33	0.102	(0.312)	0.092	0.010
82	6.83	0.33	0.102	(0.311)	0.092	0.010
83	6.92	0.33	0.102	(0.310)	0.092	0.010
84	7.00	0.33	0.102	(0.308)	0.092	0.010
85	7.08	0.33	0.102	(0.307)	0.092	0.010
86	7.17	0.33	0.102	(0.305)	0.092	0.010
87	7.25	0.33	0.102	(0.304)	0.092	0.010
88	7.33	0.37	0.112	(0.303)	0.101	0.011
89	7.42	0.37	0.112	(0.301)	0.101	0.011
90	7.50	0.37	0.112	(0.300)	0.101	0.011
91	7.58	0.40	0.122	(0.298)	0.110	0.012
92	7.67	0.40	0.122	(0.297)	0.110	0.012
93	7.75	0.40	0.122	(0.296)	0.110	0.012
94	7.83	0.43	0.133	(0.294)	0.119	0.013
95	7.92	0.43	0.133	(0.293)	0.119	0.013
96	8.00	0.43	0.133	(0.292)	0.119	0.013
97	8.08	0.50	0.153	(0.290)	0.138	0.015
98	8.17	0.50	0.153	(0.289)	0.138	0.015
99	8.25	0.50	0.153	(0.288)	0.138	0.015
100	8.33	0.50	0.153	(0.286)	0.138	0.015
101	8.42	0.50	0.153	(0.285)	0.138	0.015
102	8.50	0.50	0.153	(0.283)	0.138	0.015
103	8.58	0.53	0.163	(0.282)	0.147	0.016
104	8.67	0.53	0.163	(0.281)	0.147	0.016
105	8.75	0.53	0.163	(0.280)	0.147	0.016
106	8.83	0.57	0.173	(0.278)	0.156	0.017
107	8.92	0.57	0.173	(0.277)	0.156	0.017
108	9.00	0.57	0.173	(0.276)	0.156	0.017
109	9.08	0.63	0.194	(0.274)	0.174	0.019
110	9.17	0.63	0.194	(0.273)	0.174	0.019
111	9.25	0.63	0.194	(0.272)	0.174	0.019
112	9.33	0.67	0.204	(0.270)	0.184	0.020
113	9.42	0.67	0.204	(0.269)	0.184	0.020
114	9.50	0.67	0.204	(0.268)	0.184	0.020
115	9.58	0.70	0.214	(0.267)	0.193	0.021
116	9.67	0.70	0.214	(0.265)	0.193	0.021
117	9.75	0.70	0.214	(0.264)	0.193	0.021
118	9.83	0.73	0.224	(0.263)	0.202	0.022
119	9.92	0.73	0.224	(0.261)	0.202	0.022
120	10.00	0.73	0.224	(0.260)	0.202	0.022
121	10.08	0.50	0.153	(0.259)	0.138	0.015
122	10.17	0.50	0.153	(0.258)	0.138	0.015
123	10.25	0.50	0.153	(0.256)	0.138	0.015
124	10.33	0.50	0.153	(0.255)	0.138	0.015
125	10.42	0.50	0.153	(0.254)	0.138	0.015
126	10.50	0.50	0.153	(0.253)	0.138	0.015
127	10.58	0.67	0.204	(0.251)	0.184	0.020
128	10.67	0.67	0.204	(0.250)	0.184	0.020
129	10.75	0.67	0.204	(0.249)	0.184	0.020
130	10.83	0.67	0.204	(0.248)	0.184	0.020
131	10.92	0.67	0.204	(0.247)	0.184	0.020
132	11.00	0.67	0.204	(0.245)	0.184	0.020
133	11.08	0.63	0.194	(0.244)	0.174	0.019
134	11.17	0.63	0.194	(0.243)	0.174	0.019
135	11.25	0.63	0.194	(0.242)	0.174	0.019
136	11.33	0.63	0.194	(0.241)	0.174	0.019
137	11.42	0.63	0.194	(0.239)	0.174	0.019
138	11.50	0.63	0.194	(0.238)	0.174	0.019
139	11.58	0.57	0.173	(0.237)	0.156	0.017
140	11.67	0.57	0.173	(0.236)	0.156	0.017
141	11.75	0.57	0.173	(0.235)	0.156	0.017
142	11.83	0.60	0.184	(0.233)	0.165	0.018
143	11.92	0.60	0.184	(0.232)	0.165	0.018
144	12.00	0.60	0.184	(0.231)	0.165	0.018
145	12.08	0.83	0.255	(0.230)	0.229	0.025
146	12.17	0.83	0.255	0.229	(0.229)	0.026
147	12.25	0.83	0.255	0.228	(0.229)	0.027
148	12.33	0.87	0.265	0.227	(0.239)	0.039
149	12.42	0.87	0.265	0.225	(0.239)	0.040
150	12.50	0.87	0.265	0.224	(0.239)	0.041
151	12.58	0.93	0.286	0.223	(0.257)	0.062
152	12.67	0.93	0.286	0.222	(0.257)	0.064
153	12.75	0.93	0.286	0.221	(0.257)	0.065
154	12.83	0.97	0.296	0.220	(0.266)	0.076
155	12.92	0.97	0.296	0.219	(0.266)	0.077
156	13.00	0.97	0.296	0.218	(0.266)	0.078

157	13.08	1.13	0.347		0.216	(	0.312)	0.130
158	13.17	1.13	0.347		0.215	(	0.312)	0.131
159	13.25	1.13	0.347		0.214	(	0.312)	0.132
160	13.33	1.13	0.347		0.213	(	0.312)	0.134
161	13.42	1.13	0.347		0.212	(	0.312)	0.135
162	13.50	1.13	0.347		0.211	(	0.312)	0.136
163	13.58	0.77	0.235		0.210	(	0.211)	0.025
164	13.67	0.77	0.235		0.209	(	0.211)	0.026
165	13.75	0.77	0.235		0.208	(	0.211)	0.027
166	13.83	0.77	0.235		0.207	(	0.211)	0.028
167	13.92	0.77	0.235		0.206	(	0.211)	0.029
168	14.00	0.77	0.235		0.205	(	0.211)	0.030
169	14.08	0.90	0.275		0.204	(	0.248)	0.072
170	14.17	0.90	0.275		0.203	(	0.248)	0.073
171	14.25	0.90	0.275		0.202	(	0.248)	0.074
172	14.33	0.87	0.265		0.200	(	0.239)	0.065
173	14.42	0.87	0.265		0.199	(	0.239)	0.066
174	14.50	0.87	0.265		0.198	(	0.239)	0.067
175	14.58	0.87	0.265		0.197	(	0.239)	0.068
176	14.67	0.87	0.265		0.196	(	0.239)	0.069
177	14.75	0.87	0.265		0.195	(	0.239)	0.070
178	14.83	0.83	0.255		0.194	(	0.229)	0.061
179	14.92	0.83	0.255		0.193	(	0.229)	0.062
180	15.00	0.83	0.255		0.192	(	0.229)	0.063
181	15.08	0.80	0.245		0.191	(	0.220)	0.053
182	15.17	0.80	0.245		0.190	(	0.220)	0.054
183	15.25	0.80	0.245		0.189	(	0.220)	0.055
184	15.33	0.77	0.235		0.188	(	0.211)	0.046
185	15.42	0.77	0.235		0.188	(	0.211)	0.047
186	15.50	0.77	0.235		0.187	(	0.211)	0.048
187	15.58	0.63	0.194	(	0.186)		0.174	0.019
188	15.67	0.63	0.194	(	0.185)		0.174	0.019
189	15.75	0.63	0.194	(	0.184)		0.174	0.019
190	15.83	0.63	0.194	(	0.183)		0.174	0.019
191	15.92	0.63	0.194	(	0.182)		0.174	0.019
192	16.00	0.63	0.194	(	0.181)		0.174	0.019
193	16.08	0.13	0.041	(	0.180)		0.037	0.004
194	16.17	0.13	0.041	(	0.179)		0.037	0.004
195	16.25	0.13	0.041	(	0.178)		0.037	0.004
196	16.33	0.13	0.041	(	0.177)		0.037	0.004
197	16.42	0.13	0.041	(	0.176)		0.037	0.004
198	16.50	0.13	0.041	(	0.175)		0.037	0.004
199	16.58	0.10	0.031	(	0.175)		0.028	0.003
200	16.67	0.10	0.031	(	0.174)		0.028	0.003
201	16.75	0.10	0.031	(	0.173)		0.028	0.003
202	16.83	0.10	0.031	(	0.172)		0.028	0.003
203	16.92	0.10	0.031	(	0.171)		0.028	0.003
204	17.00	0.10	0.031	(	0.170)		0.028	0.003
205	17.08	0.17	0.051	(	0.169)		0.046	0.005
206	17.17	0.17	0.051	(	0.168)		0.046	0.005
207	17.25	0.17	0.051	(	0.168)		0.046	0.005
208	17.33	0.17	0.051	(	0.167)		0.046	0.005
209	17.42	0.17	0.051	(	0.166)		0.046	0.005
210	17.50	0.17	0.051	(	0.165)		0.046	0.005
211	17.58	0.17	0.051	(	0.164)		0.046	0.005
212	17.67	0.17	0.051	(	0.163)		0.046	0.005
213	17.75	0.17	0.051	(	0.163)		0.046	0.005
214	17.83	0.13	0.041	(	0.162)		0.037	0.004
215	17.92	0.13	0.041	(	0.161)		0.037	0.004
216	18.00	0.13	0.041	(	0.160)		0.037	0.004
217	18.08	0.13	0.041	(	0.159)		0.037	0.004
218	18.17	0.13	0.041	(	0.159)		0.037	0.004
219	18.25	0.13	0.041	(	0.158)		0.037	0.004
220	18.33	0.13	0.041	(	0.157)		0.037	0.004
221	18.42	0.13	0.041	(	0.156)		0.037	0.004
222	18.50	0.13	0.041	(	0.156)		0.037	0.004
223	18.58	0.10	0.031	(	0.155)		0.028	0.003
224	18.67	0.10	0.031	(	0.154)		0.028	0.003
225	18.75	0.10	0.031	(	0.153)		0.028	0.003
226	18.83	0.07	0.020	(	0.153)		0.018	0.002
227	18.92	0.07	0.020	(	0.152)		0.018	0.002
228	19.00	0.07	0.020	(	0.151)		0.018	0.002
229	19.08	0.10	0.031	(	0.150)		0.028	0.003
230	19.17	0.10	0.031	(	0.150)		0.028	0.003
231	19.25	0.10	0.031	(	0.149)		0.028	0.003
232	19.33	0.13	0.041	(	0.148)		0.037	0.004
233	19.42	0.13	0.041	(	0.148)		0.037	0.004
234	19.50	0.13	0.041	(	0.147)		0.037	0.004
235	19.58	0.10	0.031	(	0.146)		0.028	0.003
236	19.67	0.10	0.031	(	0.146)		0.028	0.003
237	19.75	0.10	0.031	(	0.145)		0.028	0.003
238	19.83	0.07	0.020	(	0.144)		0.018	0.002
239	19.92	0.07	0.020	(	0.144)		0.018	0.002
240	20.00	0.07	0.020	(	0.143)		0.018	0.002
241	20.08	0.10	0.031	(	0.142)		0.028	0.003
242	20.17	0.10	0.031	(	0.142)		0.028	0.003

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243  20.25     0.10      0.031       (  0.141)       0.028        0.003
244  20.33     0.10      0.031       (  0.141)       0.028        0.003
245  20.42     0.10      0.031       (  0.140)       0.028        0.003
246  20.50     0.10      0.031       (  0.139)       0.028        0.003
247  20.58     0.10      0.031       (  0.139)       0.028        0.003
248  20.67     0.10      0.031       (  0.138)       0.028        0.003
249  20.75     0.10      0.031       (  0.138)       0.028        0.003
250  20.83     0.07      0.020       (  0.137)       0.018        0.002
251  20.92     0.07      0.020       (  0.137)       0.018        0.002
252  21.00     0.07      0.020       (  0.136)       0.018        0.002
253  21.08     0.10      0.031       (  0.135)       0.028        0.003
254  21.17     0.10      0.031       (  0.135)       0.028        0.003
255  21.25     0.10      0.031       (  0.134)       0.028        0.003
256  21.33     0.07      0.020       (  0.134)       0.018        0.002
257  21.42     0.07      0.020       (  0.133)       0.018        0.002
258  21.50     0.07      0.020       (  0.133)       0.018        0.002
259  21.58     0.10      0.031       (  0.132)       0.028        0.003
260  21.67     0.10      0.031       (  0.132)       0.028        0.003
261  21.75     0.10      0.031       (  0.131)       0.028        0.003
262  21.83     0.07      0.020       (  0.131)       0.018        0.002
263  21.92     0.07      0.020       (  0.131)       0.018        0.002
264  22.00     0.07      0.020       (  0.130)       0.018        0.002
265  22.08     0.10      0.031       (  0.130)       0.028        0.003
266  22.17     0.10      0.031       (  0.129)       0.028        0.003
267  22.25     0.10      0.031       (  0.129)       0.028        0.003
268  22.33     0.07      0.020       (  0.128)       0.018        0.002
269  22.42     0.07      0.020       (  0.128)       0.018        0.002
270  22.50     0.07      0.020       (  0.128)       0.018        0.002
271  22.58     0.07      0.020       (  0.127)       0.018        0.002
272  22.67     0.07      0.020       (  0.127)       0.018        0.002
273  22.75     0.07      0.020       (  0.127)       0.018        0.002
274  22.83     0.07      0.020       (  0.126)       0.018        0.002
275  22.92     0.07      0.020       (  0.126)       0.018        0.002
276  23.00     0.07      0.020       (  0.126)       0.018        0.002
277  23.08     0.07      0.020       (  0.125)       0.018        0.002
278  23.17     0.07      0.020       (  0.125)       0.018        0.002
279  23.25     0.07      0.020       (  0.125)       0.018        0.002
280  23.33     0.07      0.020       (  0.125)       0.018        0.002
281  23.42     0.07      0.020       (  0.124)       0.018        0.002
282  23.50     0.07      0.020       (  0.124)       0.018        0.002
283  23.58     0.07      0.020       (  0.124)       0.018        0.002
284  23.67     0.07      0.020       (  0.124)       0.018        0.002
285  23.75     0.07      0.020       (  0.124)       0.018        0.002
286  23.83     0.07      0.020       (  0.123)       0.018        0.002
287  23.92     0.07      0.020       (  0.123)       0.018        0.002
288  24.00     0.07      0.020       (  0.123)       0.018        0.002
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =      4.6
      Flood volume = Effective rainfall      0.38(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       0.2(Ac.Ft)
      Total soil loss =      2.17(In)
      Total soil loss =     1.406(Ac.Ft)
      Total rainfall =      2.55(In)
      Flood volume =       10863.5 Cubic Feet
      Total soil loss =       61229.9 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      1.057(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0000      0.00  Q          |         |         |         |
   0+10       0.0001      0.01  Q          |         |         |         |
   0+15       0.0002      0.01  Q          |         |         |         |
   0+20       0.0003      0.02  Q          |         |         |         |
   0+25       0.0005      0.02  Q          |         |         |         |
   0+30       0.0007      0.02  Q          |         |         |         |
   0+35       0.0008      0.02  Q          |         |         |         |
   0+40       0.0010      0.02  Q          |         |         |         |
   0+45       0.0011      0.02  Q          |         |         |         |
   0+50       0.0013      0.03  Q          |         |         |         |
   0+55       0.0015      0.03  Q          |         |         |         |
   1+ 0       0.0018      0.03  Q          |         |         |         |
   1+ 5       0.0020      0.03  Q          |         |         |         |
   1+10       0.0021      0.03  Q          |         |         |         |
   1+15       0.0023      0.02  Q          |         |         |         |
   1+20       0.0025      0.02  Q          |         |         |         |
   1+25       0.0026      0.02  Q          |         |         |         |
   1+30       0.0028      0.02  Q          |         |         |         |
   1+35       0.0030      0.02  Q          |         |         |         |
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1+40	0.0031	0.02	Q	|	|	|	|
1+45	0.0033	0.02	Q	|	|	|	|
1+50	0.0035	0.03	Q	|	|	|	|
1+55	0.0037	0.03	Q	|	|	|	|
2+ 0	0.0039	0.03	Q	|	|	|	|
2+ 5	0.0041	0.03	Q	|	|	|	|
2+10	0.0043	0.03	Q	|	|	|	|
2+15	0.0046	0.03	Q	|	|	|	|
2+20	0.0048	0.03	Q	|	|	|	|
2+25	0.0050	0.03	Q	|	|	|	|
2+30	0.0052	0.03	Q	|	|	|	|
2+35	0.0055	0.03	Q	|	|	|	|
2+40	0.0057	0.04	Q	|	|	|	|
2+45	0.0060	0.04	Q	|	|	|	|
2+50	0.0063	0.04	QV	|	|	|	|
2+55	0.0065	0.04	QV	|	|	|	|
3+ 0	0.0068	0.04	QV	|	|	|	|
3+ 5	0.0071	0.04	QV	|	|	|	|
3+10	0.0074	0.04	QV	|	|	|	|
3+15	0.0077	0.04	QV	|	|	|	|
3+20	0.0079	0.04	QV	|	|	|	|
3+25	0.0082	0.04	QV	|	|	|	|
3+30	0.0085	0.04	QV	|	|	|	|
3+35	0.0088	0.04	QV	|	|	|	|
3+40	0.0090	0.04	QV	|	|	|	|
3+45	0.0093	0.04	QV	|	|	|	|
3+50	0.0096	0.04	QV	|	|	|	|
3+55	0.0099	0.05	QV	|	|	|	|
4+ 0	0.0102	0.05	QV	|	|	|	|
4+ 5	0.0106	0.05	QV	|	|	|	|
4+10	0.0109	0.05	QV	|	|	|	|
4+15	0.0112	0.05	QV	|	|	|	|
4+20	0.0116	0.05	QV	|	|	|	|
4+25	0.0120	0.05	QV	|	|	|	|
4+30	0.0123	0.06	QV	|	|	|	|
4+35	0.0127	0.06	Q V	|	|	|	|
4+40	0.0131	0.06	Q V	|	|	|	|
4+45	0.0135	0.06	Q V	|	|	|	|
4+50	0.0139	0.06	Q V	|	|	|	|
4+55	0.0143	0.06	Q V	|	|	|	|
5+ 0	0.0148	0.06	Q V	|	|	|	|
5+ 5	0.0152	0.06	Q V	|	|	|	|
5+10	0.0155	0.05	Q V	|	|	|	|
5+15	0.0159	0.05	Q V	|	|	|	|
5+20	0.0162	0.05	Q V	|	|	|	|
5+25	0.0166	0.05	Q V	|	|	|	|
5+30	0.0170	0.06	Q V	|	|	|	|
5+35	0.0174	0.06	Q V	|	|	|	|
5+40	0.0178	0.06	Q V	|	|	|	|
5+45	0.0182	0.06	Q V	|	|	|	|
5+50	0.0187	0.06	Q V	|	|	|	|
5+55	0.0191	0.06	Q V	|	|	|	|
6+ 0	0.0196	0.06	Q V	|	|	|	|
6+ 5	0.0200	0.07	Q V	|	|	|	|
6+10	0.0205	0.07	Q V	|	|	|	|
6+15	0.0210	0.07	Q V	|	|	|	|
6+20	0.0215	0.07	Q V	|	|	|	|
6+25	0.0220	0.07	Q V	|	|	|	|
6+30	0.0225	0.07	Q V	|	|	|	|
6+35	0.0230	0.07	Q V	|	|	|	|
6+40	0.0235	0.08	Q V	|	|	|	|
6+45	0.0241	0.08	Q V	|	|	|	|
6+50	0.0246	0.08	Q V	|	|	|	|
6+55	0.0252	0.08	Q V	|	|	|	|
7+ 0	0.0257	0.08	Q V	|	|	|	|
7+ 5	0.0263	0.08	Q V	|	|	|	|
7+10	0.0268	0.08	Q V	|	|	|	|
7+15	0.0274	0.08	Q V	|	|	|	|
7+20	0.0280	0.08	Q V	|	|	|	|
7+25	0.0286	0.09	Q V	|	|	|	|
7+30	0.0292	0.09	Q V	|	|	|	|
7+35	0.0298	0.09	Q V	|	|	|	|
7+40	0.0304	0.09	Q V	|	|	|	|
7+45	0.0311	0.10	Q V	|	|	|	|
7+50	0.0318	0.10	Q V	|	|	|	|
7+55	0.0325	0.10	Q V	|	|	|	|
8+ 0	0.0332	0.10	Q V	|	|	|	|
8+ 5	0.0339	0.11	Q V	|	|	|	|
8+10	0.0347	0.12	Q V	|	|	|	|
8+15	0.0355	0.12	Q V	|	|	|	|
8+20	0.0364	0.12	Q V	|	|	|	|
8+25	0.0372	0.12	Q V	|	|	|	|
8+30	0.0380	0.12	Q V	|	|	|	|
8+35	0.0389	0.12	Q V	|	|	|	|
8+40	0.0397	0.13	Q V	|	|	|	|
8+45	0.0406	0.13	Q V	|	|	|	|

8+50	0.0415	0.13	
8+55	0.0424	0.13	
9+ 0	0.0434	0.14	
9+ 5	0.0443	0.14	
9+10	0.0454	0.15	
9+15	0.0464	0.15	
9+20	0.0475	0.15	
9+25	0.0485	0.16	
9+30	0.0496	0.16	
9+35	0.0508	0.16	
9+40	0.0519	0.17	
9+45	0.0531	0.17	
9+50	0.0542	0.17	
9+55	0.0554	0.17	
10+ 0	0.0566	0.18	
10+ 5	0.0577	0.16	
10+10	0.0586	0.13	
10+15	0.0595	0.13	
10+20	0.0604	0.12	
10+25	0.0612	0.12	
10+30	0.0620	0.12	
10+35	0.0629	0.13	
10+40	0.0640	0.15	
10+45	0.0651	0.16	
10+50	0.0661	0.16	
10+55	0.0672	0.16	
11+ 0	0.0683	0.16	
11+ 5	0.0694	0.16	
11+10	0.0705	0.15	
11+15	0.0715	0.15	
11+20	0.0726	0.15	
11+25	0.0736	0.15	
11+30	0.0747	0.15	
11+35	0.0757	0.15	
11+40	0.0767	0.14	
11+45	0.0776	0.14	
11+50	0.0786	0.14	
11+55	0.0796	0.14	
12+ 0	0.0805	0.14	
12+ 5	0.0817	0.16	
12+10	0.0830	0.19	
12+15	0.0844	0.20	
12+20	0.0860	0.24	
12+25	0.0879	0.29	
12+30	0.0900	0.30	
12+35	0.0926	0.37	
12+40	0.0957	0.45	
12+45	0.0990	0.48	
12+50	0.1026	0.53	
12+55	0.1066	0.58	
13+ 0	0.1107	0.60	
13+ 5	0.1158	0.73	
13+10	0.1222	0.94	
13+15	0.1291	0.99	
13+20	0.1361	1.02	
13+25	0.1433	1.04	
13+30	0.1506	1.06	
13+35	0.1560	0.79	
13+40	0.1586	0.38	
13+45	0.1606	0.29	
13+50	0.1623	0.25	
13+55	0.1639	0.23	
14+ 0	0.1655	0.23	
14+ 5	0.1678	0.33	
14+10	0.1712	0.49	
14+15	0.1749	0.54	
14+20	0.1786	0.54	
14+25	0.1822	0.52	
14+30	0.1858	0.52	
14+35	0.1894	0.53	
14+40	0.1931	0.53	
14+45	0.1968	0.54	
14+50	0.2004	0.52	
14+55	0.2038	0.49	
15+ 0	0.2072	0.49	
15+ 5	0.2104	0.47	
15+10	0.2134	0.44	
15+15	0.2164	0.43	
15+20	0.2193	0.41	
15+25	0.2219	0.38	
15+30	0.2245	0.38	
15+35	0.2266	0.31	
15+40	0.2280	0.20	
15+45	0.2292	0.17	
15+50	0.2303	0.16	
15+55	0.2313	0.16	

16+ 0	0.2324	0.15	Q	|	|	|	V |
16+ 5	0.2332	0.11	Q	|	|	|	V |
16+10	0.2336	0.06	Q	|	|	|	V |
16+15	0.2339	0.04	Q	|	|	|	V |
16+20	0.2341	0.04	Q	|	|	|	V |
16+25	0.2344	0.03	Q	|	|	|	V |
16+30	0.2346	0.03	Q	|	|	|	V |
16+35	0.2348	0.03	Q	|	|	|	V |
16+40	0.2350	0.03	Q	|	|	|	V |
16+45	0.2351	0.02	Q	|	|	|	V |
16+50	0.2353	0.02	Q	|	|	|	V |
16+55	0.2355	0.02	Q	|	|	|	V |
17+ 0	0.2356	0.02	Q	|	|	|	V |
17+ 5	0.2358	0.03	Q	|	|	|	V |
17+10	0.2361	0.04	Q	|	|	|	V |
17+15	0.2364	0.04	Q	|	|	|	V |
17+20	0.2366	0.04	Q	|	|	|	V |
17+25	0.2369	0.04	Q	|	|	|	V |
17+30	0.2372	0.04	Q	|	|	|	V |
17+35	0.2375	0.04	Q	|	|	|	V |
17+40	0.2377	0.04	Q	|	|	|	V |
17+45	0.2380	0.04	Q	|	|	|	V |
17+50	0.2383	0.04	Q	|	|	|	V |
17+55	0.2385	0.03	Q	|	|	|	V |
18+ 0	0.2387	0.03	Q	|	|	|	V |
18+ 5	0.2390	0.03	Q	|	|	|	V |
18+10	0.2392	0.03	Q	|	|	|	V |
18+15	0.2394	0.03	Q	|	|	|	V |
18+20	0.2396	0.03	Q	|	|	|	V |
18+25	0.2398	0.03	Q	|	|	|	V |
18+30	0.2401	0.03	Q	|	|	|	V |
18+35	0.2403	0.03	Q	|	|	|	V |
18+40	0.2404	0.03	Q	|	|	|	V |
18+45	0.2406	0.02	Q	|	|	|	V |
18+50	0.2408	0.02	Q	|	|	|	V |
18+55	0.2409	0.02	Q	|	|	|	V |
19+ 0	0.2410	0.02	Q	|	|	|	V |
19+ 5	0.2411	0.02	Q	|	|	|	V |
19+10	0.2413	0.02	Q	|	|	|	V |
19+15	0.2414	0.02	Q	|	|	|	V |
19+20	0.2416	0.03	Q	|	|	|	V |
19+25	0.2418	0.03	Q	|	|	|	V |
19+30	0.2420	0.03	Q	|	|	|	V |
19+35	0.2422	0.03	Q	|	|	|	V |
19+40	0.2424	0.03	Q	|	|	|	V |
19+45	0.2426	0.02	Q	|	|	|	V |
19+50	0.2427	0.02	Q	|	|	|	V |
19+55	0.2429	0.02	Q	|	|	|	V |
20+ 0	0.2430	0.02	Q	|	|	|	V |
20+ 5	0.2431	0.02	Q	|	|	|	V |
20+10	0.2433	0.02	Q	|	|	|	V|
20+15	0.2434	0.02	Q	|	|	|	V|
20+20	0.2436	0.02	Q	|	|	|	V|
20+25	0.2438	0.02	Q	|	|	|	V|
20+30	0.2439	0.02	Q	|	|	|	V|
20+35	0.2441	0.02	Q	|	|	|	V|
20+40	0.2443	0.02	Q	|	|	|	V|
20+45	0.2444	0.02	Q	|	|	|	V|
20+50	0.2446	0.02	Q	|	|	|	V|
20+55	0.2447	0.02	Q	|	|	|	V|
21+ 0	0.2448	0.02	Q	|	|	|	V|
21+ 5	0.2449	0.02	Q	|	|	|	V|
21+10	0.2451	0.02	Q	|	|	|	V|
21+15	0.2452	0.02	Q	|	|	|	V|
21+20	0.2454	0.02	Q	|	|	|	V|
21+25	0.2455	0.02	Q	|	|	|	V|
21+30	0.2456	0.02	Q	|	|	|	V|
21+35	0.2458	0.02	Q	|	|	|	V|
21+40	0.2459	0.02	Q	|	|	|	V|
21+45	0.2461	0.02	Q	|	|	|	V|
21+50	0.2462	0.02	Q	|	|	|	V|
21+55	0.2463	0.02	Q	|	|	|	V|
22+ 0	0.2465	0.02	Q	|	|	|	V|
22+ 5	0.2466	0.02	Q	|	|	|	V|
22+10	0.2467	0.02	Q	|	|	|	V|
22+15	0.2469	0.02	Q	|	|	|	V|
22+20	0.2470	0.02	Q	|	|	|	V|
22+25	0.2472	0.02	Q	|	|	|	V|
22+30	0.2473	0.02	Q	|	|	|	V|
22+35	0.2474	0.02	Q	|	|	|	V|
22+40	0.2475	0.02	Q	|	|	|	V|
22+45	0.2476	0.02	Q	|	|	|	V|
22+50	0.2477	0.02	Q	|	|	|	V|
22+55	0.2478	0.02	Q	|	|	|	V|
23+ 0	0.2479	0.02	Q	|	|	|	V|
23+ 5	0.2481	0.02	Q	|	|	|	V|

```
   23+10       0.2482      0.02  Q          |          |          |          v|
   23+15       0.2483      0.02  Q          |          |          |          v|
   23+20       0.2484      0.02  Q          |          |          |          v|
   23+25       0.2485      0.02  Q          |          |          |          v|
   23+30       0.2486      0.02  Q          |          |          |          v|
   23+35       0.2487      0.02  Q          |          |          |          v|
   23+40       0.2488      0.02  Q          |          |          |          v|
   23+45       0.2489      0.02  Q          |          |          |          v|
   23+50       0.2491      0.02  Q          |          |          |          v|
   23+55       0.2492      0.02  Q          |          |          |          v|
   24+ 0       0.2493      0.02  Q          |          |          |          v|
   24+ 5       0.2493      0.01  Q          |          |          |          v|
   24+10       0.2494      0.00  Q          |          |          |          v|
   24+15       0.2494      0.00  Q          |          |          |          v|
   24+20       0.2494      0.00  Q          |          |          |          v|
   24+25       0.2494      0.00  Q          |          |          |          v|
-------------------------------------------------------------------------------
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       U n i t   H y d r o g r a p h   A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =       7.79(Ac.)  =      0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =       7.79(Ac.)  =      0.012 Sq. Mi.
Length along longest watercourse =    1222.00(Ft.)
Length along longest watercourse measured to centroid =     611.00(Ft.)
Length along longest watercourse =      0.231 Mi.
Length along longest watercourse measured to centroid =      0.116 Mi.
Difference in elevation =      89.00(Ft.)
Slope along watercourse =    384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time =    0.059 Hr.
Lag time =     3.52 Min.
25% of lag time =     0.88 Min.
40% of lag time =     1.41 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            0.50                 3.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            1.30                10.13

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.829(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    0.829(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     7.790           91.00          0.000
 Total Area Entered =      7.79(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  91.0      0.117     0.000        0.117       1.000      0.117
                                                 Sum (F) =    0.117
Area averaged mean soil loss (F) (In/Hr) =  0.117
Minimum soil loss rate ((In/Hr)) =  0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.900
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
			Sum = 100.000 Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.328	0.117	(0.295)	0.211
2	0.17	4.20	0.418	0.117	(0.376)	0.301
3	0.25	4.40	0.438	0.117	(0.394)	0.321
4	0.33	4.80	0.478	0.117	(0.430)	0.361
5	0.42	5.20	0.517	0.117	(0.466)	0.400
6	0.50	6.20	0.617	0.117	(0.555)	0.500
7	0.58	6.80	0.677	0.117	(0.609)	0.560
8	0.67	8.80	0.875	0.117	(0.788)	0.758
9	0.75	13.90	1.383	0.117	(1.245)	1.266
10	0.83	31.40	3.124	0.117	(2.812)	3.007
11	0.92	7.20	0.716	0.117	(0.645)	0.599
12	1.00	3.80	0.378	0.117	(0.340)	0.261
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	8.5

Flood volume = Effective rainfall 0.71(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.5(Ac.Ft)
Total soil loss = 0.12(In)
Total soil loss = 0.076(Ac.Ft)
Total rainfall = 0.83(In)
Flood volume = 20135.6 Cubic Feet
Total soil loss = 3308.5 Cubic Feet

Peak flow rate of this hydrograph = 14.359(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0036	0.52	VQ				
0+10	0.0141	1.53	V Q				
0+15	0.0286	2.10	V Q				
0+20	0.0454	2.44	VQ				
0+25	0.0646	2.79	Q				
0+30	0.0871	3.27	QV				
0+35	0.1137	3.86	Q V				
0+40	0.1460	4.69	Q V				
0+45	0.1927	6.78	Q V				
0+50	0.2835	13.18	V Q				
0+55	0.3823	14.36	Q V				
1+ 0	0.4263	6.39	Q			V	
1+ 5	0.4477	3.11	Q			V	
1+10	0.4567	1.29	Q			V	
1+15	0.4611	0.64	Q			V	
1+20	0.4620	0.14	Q			V	
1+25	0.4623	0.04	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX310310.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 1222.00(Ft.)
Length along longest watercourse measured to centroid = 611.00(Ft.)
Length along longest watercourse = 0.231 Mi.
Length along longest watercourse measured to centroid = 0.116 Mi.
Difference in elevation = 89.00(Ft.)
Slope along watercourse = 384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.059 Hr.
Lag time = 3.52 Min.
25% of lag time = 0.88 Min.
40% of lag time = 1.41 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	0.80	6.23

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	2.00	15.58

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 1.294(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.294(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	91.00	0.000

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
		Sum = 100.000	Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.202	0.117	(0.182)	0.085
2	0.17	1.30	0.202	0.117	(0.182)	0.085
3	0.25	1.10	0.171	0.117	(0.154)	0.054
4	0.33	1.50	0.233	0.117	(0.210)	0.116
5	0.42	1.50	0.233	0.117	(0.210)	0.116
6	0.50	1.80	0.279	0.117	(0.251)	0.162
7	0.58	1.50	0.233	0.117	(0.210)	0.116
8	0.67	1.80	0.279	0.117	(0.251)	0.162
9	0.75	1.80	0.279	0.117	(0.251)	0.162
10	0.83	1.50	0.233	0.117	(0.210)	0.116
11	0.92	1.60	0.248	0.117	(0.224)	0.131
12	1.00	1.80	0.279	0.117	(0.251)	0.162
13	1.08	2.20	0.342	0.117	(0.307)	0.225
14	1.17	2.20	0.342	0.117	(0.307)	0.225
15	1.25	2.20	0.342	0.117	(0.307)	0.225
16	1.33	2.00	0.310	0.117	(0.279)	0.193
17	1.42	2.60	0.404	0.117	(0.363)	0.287
18	1.50	2.70	0.419	0.117	(0.377)	0.302
19	1.58	2.40	0.373	0.117	(0.335)	0.256
20	1.67	2.70	0.419	0.117	(0.377)	0.302
21	1.75	3.30	0.512	0.117	(0.461)	0.395
22	1.83	3.10	0.481	0.117	(0.433)	0.364
23	1.92	2.90	0.450	0.117	(0.405)	0.333
24	2.00	3.00	0.466	0.117	(0.419)	0.349
25	2.08	3.10	0.481	0.117	(0.433)	0.364
26	2.17	4.20	0.652	0.117	(0.587)	0.535
27	2.25	5.00	0.776	0.117	(0.699)	0.659
28	2.33	3.50	0.543	0.117	(0.489)	0.426
29	2.42	6.80	1.056	0.117	(0.950)	0.939
30	2.50	7.30	1.133	0.117	(1.020)	1.016
31	2.58	8.20	1.273	0.117	(1.146)	1.156
32	2.67	5.90	0.916	0.117	(0.824)	0.799
33	2.75	2.00	0.310	0.117	(0.279)	0.193
34	2.83	1.80	0.279	0.117	(0.251)	0.162
35	2.92	1.80	0.279	0.117	(0.251)	0.162
36	3.00	0.60	0.093	(0.117)	0.084	0.009
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	11.3

Flood volume = Effective rainfall 0.95(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.6(Ac.Ft)
Total soil loss = 0.35(In)
Total soil loss = 0.226(Ac.Ft)
Total rainfall = 1.29(In)
Flood volume = 26734.0 Cubic Feet
Total soil loss = 9847.3 Cubic Feet

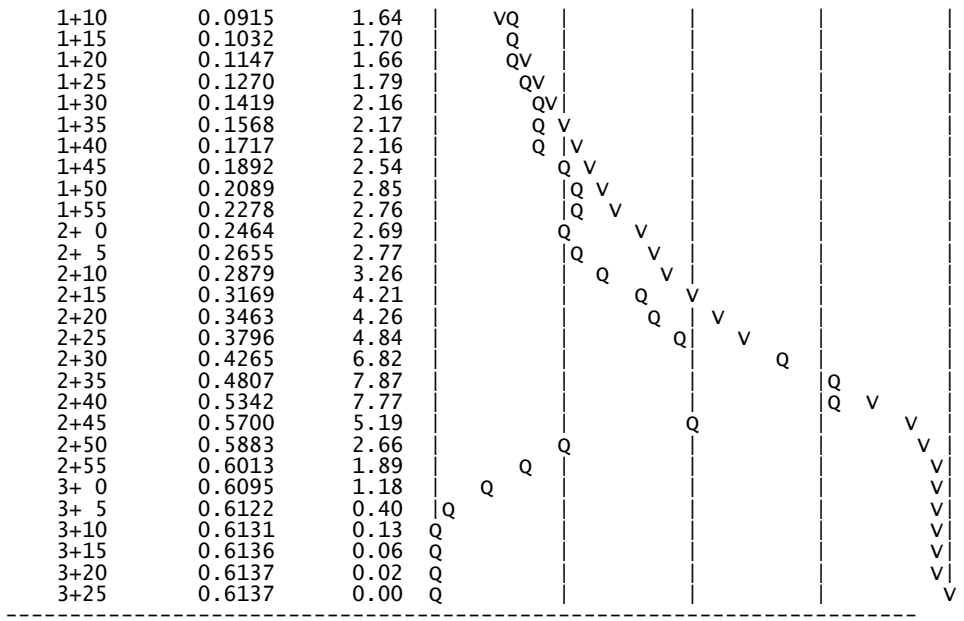
Peak flow rate of this hydrograph = 7.874(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0014	0.21	Q				
0+10	0.0050	0.52	V Q				
0+15	0.0087	0.53	V Q				
0+20	0.0128	0.60	V Q				
0+25	0.0184	0.82	V Q				
0+30	0.0252	0.99	V Q				
0+35	0.0326	1.07	V Q				
0+40	0.0399	1.06	V Q				
0+45	0.0482	1.22	VQ				
0+50	0.0561	1.14	VQ				
0+55	0.0631	1.02	Q				
1+ 0	0.0707	1.11	Q				
1+ 5	0.0802	1.38	Q				


1+10 0.0915 1.64
1+15 0.1032 1.70
1+20 0.1147 1.66
1+25 0.1270 1.79
1+30 0.1419 2.16
1+35 0.1568 2.17
1+40 0.1717 2.16
1+45 0.1892 2.54
1+50 0.2089 2.85
1+55 0.2278 2.76
2+ 0 0.2464 2.69
2+ 5 0.2655 2.77
2+10 0.2879 3.26
2+15 0.3169 4.21
2+20 0.3463 4.26
2+25 0.3796 4.84
2+30 0.4265 6.82
2+35 0.4807 7.87
2+40 0.5342 7.77
2+45 0.5700 5.19
2+50 0.5883 2.66
2+55 0.6013 1.89
3+ 0 0.6095 1.18
3+ 5 0.6122 0.40
3+10 0.6131 0.13
3+15 0.6136 0.06
3+20 0.6137 0.02
3+25 0.6137 0.00

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX310610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 1222.00(Ft.)
Length along longest watercourse measured to centroid = 611.00(Ft.)
Length along longest watercourse = 0.231 Mi.
Length along longest watercourse measured to centroid = 0.116 Mi.
Difference in elevation = 89.00(Ft.)
Slope along watercourse = 384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.059 Hr.
Lag time = 3.52 Min.
25% of lag time = 0.88 Min.
40% of lag time = 1.41 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.10	8.57

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	3.00	23.37

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.882(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.882(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	91.00	0.000

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
			Sum = 100.000	Sum= 7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.113	(0.117)	0.102	0.011
2	0.17	0.60	0.135	0.117	(0.122)	0.018
3	0.25	0.60	0.135	0.117	(0.122)	0.018
4	0.33	0.60	0.135	0.117	(0.122)	0.018
5	0.42	0.60	0.135	0.117	(0.122)	0.018
6	0.50	0.70	0.158	0.117	(0.142)	0.041
7	0.58	0.70	0.158	0.117	(0.142)	0.041
8	0.67	0.70	0.158	0.117	(0.142)	0.041
9	0.75	0.70	0.158	0.117	(0.142)	0.041
10	0.83	0.70	0.158	0.117	(0.142)	0.041
11	0.92	0.70	0.158	0.117	(0.142)	0.041
12	1.00	0.80	0.181	0.117	(0.163)	0.064
13	1.08	0.80	0.181	0.117	(0.163)	0.064
14	1.17	0.80	0.181	0.117	(0.163)	0.064
15	1.25	0.80	0.181	0.117	(0.163)	0.064
16	1.33	0.80	0.181	0.117	(0.163)	0.064
17	1.42	0.80	0.181	0.117	(0.163)	0.064
18	1.50	0.80	0.181	0.117	(0.163)	0.064
19	1.58	0.80	0.181	0.117	(0.163)	0.064
20	1.67	0.80	0.181	0.117	(0.163)	0.064
21	1.75	0.80	0.181	0.117	(0.163)	0.064
22	1.83	0.80	0.181	0.117	(0.163)	0.064
23	1.92	0.80	0.181	0.117	(0.163)	0.064
24	2.00	0.90	0.203	0.117	(0.183)	0.086
25	2.08	0.80	0.181	0.117	(0.163)	0.064
26	2.17	0.90	0.203	0.117	(0.183)	0.086
27	2.25	0.90	0.203	0.117	(0.183)	0.086
28	2.33	0.90	0.203	0.117	(0.183)	0.086
29	2.42	0.90	0.203	0.117	(0.183)	0.086
30	2.50	0.90	0.203	0.117	(0.183)	0.086
31	2.58	0.90	0.203	0.117	(0.183)	0.086
32	2.67	0.90	0.203	0.117	(0.183)	0.086
33	2.75	1.00	0.226	0.117	(0.203)	0.109
34	2.83	1.00	0.226	0.117	(0.203)	0.109
35	2.92	1.00	0.226	0.117	(0.203)	0.109
36	3.00	1.00	0.226	0.117	(0.203)	0.109
37	3.08	1.00	0.226	0.117	(0.203)	0.109
38	3.17	1.10	0.248	0.117	(0.224)	0.131
39	3.25	1.10	0.248	0.117	(0.224)	0.131
40	3.33	1.10	0.248	0.117	(0.224)	0.131
41	3.42	1.20	0.271	0.117	(0.244)	0.154
42	3.50	1.30	0.294	0.117	(0.264)	0.177
43	3.58	1.40	0.316	0.117	(0.285)	0.199
44	3.67	1.40	0.316	0.117	(0.285)	0.199
45	3.75	1.50	0.339	0.117	(0.305)	0.222
46	3.83	1.50	0.339	0.117	(0.305)	0.222
47	3.92	1.60	0.361	0.117	(0.325)	0.244
48	4.00	1.60	0.361	0.117	(0.325)	0.244
49	4.08	1.70	0.384	0.117	(0.345)	0.267
50	4.17	1.80	0.406	0.117	(0.366)	0.289
51	4.25	1.90	0.429	0.117	(0.386)	0.312
52	4.33	2.00	0.452	0.117	(0.406)	0.335
53	4.42	2.10	0.474	0.117	(0.427)	0.357
54	4.50	2.10	0.474	0.117	(0.427)	0.357
55	4.58	2.20	0.497	0.117	(0.447)	0.380
56	4.67	2.30	0.519	0.117	(0.467)	0.402
57	4.75	2.40	0.542	0.117	(0.488)	0.425
58	4.83	2.40	0.542	0.117	(0.488)	0.425
59	4.92	2.50	0.564	0.117	(0.508)	0.447
60	5.00	2.60	0.587	0.117	(0.528)	0.470
61	5.08	3.10	0.700	0.117	(0.630)	0.583
62	5.17	3.60	0.813	0.117	(0.732)	0.696
63	5.25	3.90	0.881	0.117	(0.793)	0.764
64	5.33	4.20	0.948	0.117	(0.854)	0.831
65	5.42	4.70	1.061	0.117	(0.955)	0.944
66	5.50	5.60	1.264	0.117	(1.138)	1.147
67	5.58	1.90	0.429	0.117	(0.386)	0.312
68	5.67	0.90	0.203	0.117	(0.183)	0.086
69	5.75	0.60	0.135	0.117	(0.122)	0.018
70	5.83	0.50	0.113	(0.117)	0.102	0.011

```
71   5.92     0.30      0.068       (  0.117)       0.061        0.007
72   6.00     0.20      0.045       (  0.117)       0.041        0.005
               (Loss Rate Not Used)
   Sum =     100.0                                  Sum =    14.3
      Flood volume = Effective rainfall      1.19(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       0.8(Ac.Ft)
      Total soil loss =      0.69(In)
      Total soil loss =     0.447(Ac.Ft)
      Total rainfall =      1.88(In)
      Flood volume =       33741.6 Cubic Feet
      Total soil loss =       19466.4 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      7.636(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0002      0.03  Q          |         |         |         |
  0+10       0.0008      0.09  Q          |         |         |         |
  0+15       0.0017      0.12  Q          |         |         |         |
  0+20       0.0026      0.14  Q          |         |         |         |
  0+25       0.0036      0.14  Q          |         |         |         |
  0+30       0.0049      0.20  Q          |         |         |         |
  0+35       0.0069      0.28  VQ         |         |         |         |
  0+40       0.0090      0.31  VQ         |         |         |         |
  0+45       0.0112      0.31  VQ         |         |         |         |
  0+50       0.0134      0.32  VQ         |         |         |         |
  0+55       0.0156      0.32  VQ         |         |         |         |
  1+ 0       0.0182      0.38  VQ         |         |         |         |
  1+ 5       0.0214      0.46  |Q         |         |         |         |
  1+10       0.0247      0.48  |Q         |         |         |         |
  1+15       0.0281      0.49  |Q         |         |         |         |
  1+20       0.0315      0.50  |Q         |         |         |         |
  1+25       0.0349      0.50  |Q         |         |         |         |
  1+30       0.0384      0.50  |Q         |         |         |         |
  1+35       0.0418      0.50  |QV        |         |         |         |
  1+40       0.0453      0.50  |QV        |         |         |         |
  1+45       0.0487      0.50  |QV        |         |         |         |
  1+50       0.0522      0.50  |QV        |         |         |         |
  1+55       0.0556      0.50  |QV        |         |         |         |
  2+ 0       0.0594      0.56  | QV       |         |         |         |
  2+ 5       0.0634      0.58  | QV       |         |         |         |
  2+10       0.0674      0.58  | QV       |         |         |         |
  2+15       0.0719      0.65  | QV       |         |         |         |
  2+20       0.0765      0.67  | QV       |         |         |         |
  2+25       0.0811      0.67  | Q V      |         |         |         |
  2+30       0.0857      0.67  | Q V      |         |         |         |
  2+35       0.0904      0.68  | Q V      |         |         |         |
  2+40       0.0951      0.68  | Q V      |         |         |         |
  2+45       0.1001      0.73  | Q  V     |         |         |         |
  2+50       0.1057      0.82  |  Q V     |         |         |         |
  2+55       0.1115      0.84  |  Q V     |         |         |         |
  3+ 0       0.1173      0.85  |  Q  V    |         |         |         |
  3+ 5       0.1232      0.85  |  Q  V    |         |         |         |
  3+10       0.1295      0.91  |  Q  V    |         |         |         |
  3+15       0.1363      0.99  |  Q   V   |         |         |         |
  3+20       0.1433      1.01  |   Q  V   |         |         |         |
  3+25       0.1507      1.08  |   Q  V   |         |         |         |
  3+30       0.1592      1.22  |   Q   V  |         |         |         |
  3+35       0.1687      1.39  |    Q  V  |         |         |         |
  3+40       0.1791      1.50  |     Q  V|         |         |         |
  3+45       0.1900      1.59  |     Q  V|         |         |         |
  3+50       0.2017      1.69  |     Q   V         |         |         |
  3+55       0.2139      1.78  |      Q  |V        |         |         |
  4+ 0       0.2268      1.87  |      Q  |V        |         |         |
  4+ 5       0.2403      1.95  |      Q  | V       |         |         |
  4+10       0.2548      2.11  |       Q |  V      |         |         |
  4+15       0.2704      2.27  |        Q|  V      |         |         |
  4+20       0.2872      2.44  |        Q|   V     |         |         |
  4+25       0.3053      2.62  |         Q    V    |         |         |
  4+30       0.3241      2.74  |         Q     V   |         |         |
  4+35       0.3437      2.83  |         |Q     V  |         |         |
  4+40       0.3642      2.99  |         |Q      V |         |         |
  4+45       0.3860      3.16  |         | Q      V|         |         |
  4+50       0.4085      3.28  |         |  Q       |V        |         |
  4+55       0.4317      3.36  |         |  Q       | V       |         |
  5+ 0       0.4560      3.52  |         |   Q      |  V      |         |
  5+ 5       0.4829      3.91  |         |    Q     |   V     |         |
  5+10       0.5149      4.64  |         |      Q   |    V    |         |
  5+15       0.5517      5.35  |         |          |Q      V |         |
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    5+20       0.5925      5.92  |          |          |  Q       V          |
    5+25       0.6379      6.59  |          |          |     Q    | V        |
    5+30       0.6905      7.64  |          |          |        Q     V     |
    5+35       0.7353      6.51  |          |          |     Q    |       V  |
    5+40       0.7566      3.09  |          | Q        |          |         V|
    5+45       0.7664      1.43  |     Q    |          |          |         V|
    5+50       0.7711      0.67  | Q        |          |          |         V|
    5+55       0.7734      0.33  |Q         |          |          |         V|
    6+ 0       0.7742      0.11  Q          |          |          |         V|
    6+ 5       0.7745      0.04  Q          |          |          |         V|
    6+10       0.7746      0.01  Q          |          |          |         V|
    6+15       0.7746      0.00  Q          |          |          |         V|
    6+20       0.7746      0.00  Q          |          |          |         V|
    6+25       0.7746      0.00  Q          |          |          |          V
-------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: EX3102410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 1222.00(Ft.)
Length along longest watercourse measured to centroid = 611.00(Ft.)
Length along longest watercourse = 0.231 Mi.
Length along longest watercourse measured to centroid = 0.116 Mi.
Difference in elevation = 89.00(Ft.)
Slope along watercourse = 384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.059 Hr.
Lag time = 3.52 Min.
25% of lag time = 0.88 Min.
40% of lag time = 1.41 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.80	14.02

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	5.00	38.95

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 3.117(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.116(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	91.00	0.000

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
			Sum = 100.000	Sum= 7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.025	(0.207)	0.022	0.002
2	0.17	0.07	0.025	(0.207)	0.022	0.002
3	0.25	0.07	0.025	(0.206)	0.022	0.002
4	0.33	0.10	0.037	(0.205)	0.034	0.004
5	0.42	0.10	0.037	(0.204)	0.034	0.004
6	0.50	0.10	0.037	(0.203)	0.034	0.004
7	0.58	0.10	0.037	(0.203)	0.034	0.004
8	0.67	0.10	0.037	(0.202)	0.034	0.004
9	0.75	0.10	0.037	(0.201)	0.034	0.004
10	0.83	0.13	0.050	(0.200)	0.045	0.005
11	0.92	0.13	0.050	(0.199)	0.045	0.005
12	1.00	0.13	0.050	(0.199)	0.045	0.005
13	1.08	0.10	0.037	(0.198)	0.034	0.004
14	1.17	0.10	0.037	(0.197)	0.034	0.004
15	1.25	0.10	0.037	(0.196)	0.034	0.004
16	1.33	0.10	0.037	(0.196)	0.034	0.004
17	1.42	0.10	0.037	(0.195)	0.034	0.004
18	1.50	0.10	0.037	(0.194)	0.034	0.004
19	1.58	0.10	0.037	(0.193)	0.034	0.004
20	1.67	0.10	0.037	(0.192)	0.034	0.004
21	1.75	0.10	0.037	(0.192)	0.034	0.004
22	1.83	0.13	0.050	(0.191)	0.045	0.005
23	1.92	0.13	0.050	(0.190)	0.045	0.005
24	2.00	0.13	0.050	(0.189)	0.045	0.005
25	2.08	0.13	0.050	(0.189)	0.045	0.005
26	2.17	0.13	0.050	(0.188)	0.045	0.005
27	2.25	0.13	0.050	(0.187)	0.045	0.005
28	2.33	0.13	0.050	(0.186)	0.045	0.005
29	2.42	0.13	0.050	(0.186)	0.045	0.005
30	2.50	0.13	0.050	(0.185)	0.045	0.005
31	2.58	0.17	0.062	(0.184)	0.056	0.006
32	2.67	0.17	0.062	(0.183)	0.056	0.006
33	2.75	0.17	0.062	(0.183)	0.056	0.006
34	2.83	0.17	0.062	(0.182)	0.056	0.006
35	2.92	0.17	0.062	(0.181)	0.056	0.006
36	3.00	0.17	0.062	(0.180)	0.056	0.006
37	3.08	0.17	0.062	(0.180)	0.056	0.006
38	3.17	0.17	0.062	(0.179)	0.056	0.006
39	3.25	0.17	0.062	(0.178)	0.056	0.006
40	3.33	0.17	0.062	(0.177)	0.056	0.006
41	3.42	0.17	0.062	(0.177)	0.056	0.006
42	3.50	0.17	0.062	(0.176)	0.056	0.006
43	3.58	0.17	0.062	(0.175)	0.056	0.006
44	3.67	0.17	0.062	(0.174)	0.056	0.006
45	3.75	0.17	0.062	(0.174)	0.056	0.006
46	3.83	0.20	0.075	(0.173)	0.067	0.007
47	3.92	0.20	0.075	(0.172)	0.067	0.007
48	4.00	0.20	0.075	(0.171)	0.067	0.007
49	4.08	0.20	0.075	(0.171)	0.067	0.007
50	4.17	0.20	0.075	(0.170)	0.067	0.007
51	4.25	0.20	0.075	(0.169)	0.067	0.007
52	4.33	0.23	0.087	(0.169)	0.079	0.009
53	4.42	0.23	0.087	(0.168)	0.079	0.009
54	4.50	0.23	0.087	(0.167)	0.079	0.009
55	4.58	0.23	0.087	(0.166)	0.079	0.009
56	4.67	0.23	0.087	(0.166)	0.079	0.009
57	4.75	0.23	0.087	(0.165)	0.079	0.009
58	4.83	0.27	0.100	(0.164)	0.090	0.010
59	4.92	0.27	0.100	(0.164)	0.090	0.010
60	5.00	0.27	0.100	(0.163)	0.090	0.010
61	5.08	0.20	0.075	(0.162)	0.067	0.007
62	5.17	0.20	0.075	(0.161)	0.067	0.007
63	5.25	0.20	0.075	(0.161)	0.067	0.007
64	5.33	0.23	0.087	(0.160)	0.079	0.009
65	5.42	0.23	0.087	(0.159)	0.079	0.009
66	5.50	0.23	0.087	(0.159)	0.079	0.009
67	5.58	0.27	0.100	(0.158)	0.090	0.010
68	5.67	0.27	0.100	(0.157)	0.090	0.010
69	5.75	0.27	0.100	(0.157)	0.090	0.010
70	5.83	0.27	0.100	(0.156)	0.090	0.010

71	5.92	0.27	0.100	(	0.155)	0.090		0.010
72	6.00	0.27	0.100	(	0.154)	0.090		0.010
73	6.08	0.30	0.112	(	0.154)	0.101		0.011
74	6.17	0.30	0.112	(	0.153)	0.101		0.011
75	6.25	0.30	0.112	(	0.152)	0.101		0.011
76	6.33	0.30	0.112	(	0.152)	0.101		0.011
77	6.42	0.30	0.112	(	0.151)	0.101		0.011
78	6.50	0.30	0.112	(	0.150)	0.101		0.011
79	6.58	0.33	0.125	(	0.150)	0.112		0.012
80	6.67	0.33	0.125	(	0.149)	0.112		0.012
81	6.75	0.33	0.125	(	0.148)	0.112		0.012
82	6.83	0.33	0.125	(	0.148)	0.112		0.012
83	6.92	0.33	0.125	(	0.147)	0.112		0.012
84	7.00	0.33	0.125	(	0.146)	0.112		0.012
85	7.08	0.33	0.125	(	0.146)	0.112		0.012
86	7.17	0.33	0.125	(	0.145)	0.112		0.012
87	7.25	0.33	0.125	(	0.144)	0.112		0.012
88	7.33	0.37	0.137	(	0.144)	0.123		0.014
89	7.42	0.37	0.137	(	0.143)	0.123		0.014
90	7.50	0.37	0.137	(	0.142)	0.123		0.014
91	7.58	0.40	0.150	(	0.142)	0.135		0.015
92	7.67	0.40	0.150	(	0.141)	0.135		0.015
93	7.75	0.40	0.150	(	0.140)	0.135		0.015
94	7.83	0.43	0.162		0.140	(0.146)		0.022
95	7.92	0.43	0.162		0.139	(0.146)		0.023
96	8.00	0.43	0.162		0.138	(0.146)		0.024
97	8.08	0.50	0.187		0.138	(0.168)		0.049
98	8.17	0.50	0.187		0.137	(0.168)		0.050
99	8.25	0.50	0.187		0.137	(0.168)		0.050
100	8.33	0.50	0.187		0.136	(0.168)		0.051
101	8.42	0.50	0.187		0.135	(0.168)		0.052
102	8.50	0.50	0.187		0.135	(0.168)		0.052
103	8.58	0.53	0.199		0.134	(0.180)		0.065
104	8.67	0.53	0.199		0.133	(0.180)		0.066
105	8.75	0.53	0.199		0.133	(0.180)		0.067
106	8.83	0.57	0.212		0.132	(0.191)		0.080
107	8.92	0.57	0.212		0.131	(0.191)		0.080
108	9.00	0.57	0.212		0.131	(0.191)		0.081
109	9.08	0.63	0.237		0.130	(0.213)		0.107
110	9.17	0.63	0.237		0.130	(0.213)		0.107
111	9.25	0.63	0.237		0.129	(0.213)		0.108
112	9.33	0.67	0.249		0.128	(0.224)		0.121
113	9.42	0.67	0.249		0.128	(0.224)		0.122
114	9.50	0.67	0.249		0.127	(0.224)		0.122
115	9.58	0.70	0.262		0.127	(0.236)		0.135
116	9.67	0.70	0.262		0.126	(0.236)		0.136
117	9.75	0.70	0.262		0.125	(0.236)		0.136
118	9.83	0.73	0.274		0.125	(0.247)		0.149
119	9.92	0.73	0.274		0.124	(0.247)		0.150
120	10.00	0.73	0.274		0.124	(0.247)		0.151
121	10.08	0.50	0.187		0.123	(0.168)		0.064
122	10.17	0.50	0.187		0.122	(0.168)		0.065
123	10.25	0.50	0.187		0.122	(0.168)		0.065
124	10.33	0.50	0.187		0.121	(0.168)		0.066
125	10.42	0.50	0.187		0.121	(0.168)		0.066
126	10.50	0.50	0.187		0.120	(0.168)		0.067
127	10.58	0.67	0.249		0.119	(0.224)		0.130
128	10.67	0.67	0.249		0.119	(0.224)		0.130
129	10.75	0.67	0.249		0.118	(0.224)		0.131
130	10.83	0.67	0.249		0.118	(0.224)		0.132
131	10.92	0.67	0.249		0.117	(0.224)		0.132
132	11.00	0.67	0.249		0.117	(0.224)		0.133
133	11.08	0.63	0.237		0.116	(0.213)		0.121
134	11.17	0.63	0.237		0.115	(0.213)		0.121
135	11.25	0.63	0.237		0.115	(0.213)		0.122
136	11.33	0.63	0.237		0.114	(0.213)		0.123
137	11.42	0.63	0.237		0.114	(0.213)		0.123
138	11.50	0.63	0.237		0.113	(0.213)		0.124
139	11.58	0.57	0.212		0.113	(0.191)		0.099
140	11.67	0.57	0.212		0.112	(0.191)		0.100
141	11.75	0.57	0.212		0.111	(0.191)		0.100
142	11.83	0.60	0.224		0.111	(0.202)		0.114
143	11.92	0.60	0.224		0.110	(0.202)		0.114
144	12.00	0.60	0.224		0.110	(0.202)		0.115
145	12.08	0.83	0.312		0.109	(0.280)		0.202
146	12.17	0.83	0.312		0.109	(0.280)		0.203
147	12.25	0.83	0.312		0.108	(0.280)		0.204
148	12.33	0.87	0.324		0.108	(0.292)		0.217
149	12.42	0.87	0.324		0.107	(0.292)		0.217
150	12.50	0.87	0.324		0.107	(0.292)		0.218
151	12.58	0.93	0.349		0.106	(0.314)		0.243
152	12.67	0.93	0.349		0.105	(0.314)		0.244
153	12.75	0.93	0.349		0.105	(0.314)		0.244
154	12.83	0.97	0.362		0.104	(0.325)		0.257
155	12.92	0.97	0.362		0.104	(0.325)		0.258
156	13.00	0.97	0.362		0.103	(0.325)		0.258

157	13.08	1.13	0.424	0.103	(0.381)	0.321
158	13.17	1.13	0.424	0.102	(0.381)	0.322
159	13.25	1.13	0.424	0.102	(0.381)	0.322
160	13.33	1.13	0.424	0.101	(0.381)	0.323
161	13.42	1.13	0.424	0.101	(0.381)	0.323
162	13.50	1.13	0.424	0.100	(0.381)	0.324
163	13.58	0.77	0.287	0.100	(0.258)	0.187
164	13.67	0.77	0.287	0.099	(0.258)	0.188
165	13.75	0.77	0.287	0.099	(0.258)	0.188
166	13.83	0.77	0.287	0.098	(0.258)	0.189
167	13.92	0.77	0.287	0.098	(0.258)	0.189
168	14.00	0.77	0.287	0.097	(0.258)	0.190
169	14.08	0.90	0.337	0.097	(0.303)	0.240
170	14.17	0.90	0.337	0.096	(0.303)	0.240
171	14.25	0.90	0.337	0.096	(0.303)	0.241
172	14.33	0.87	0.324	0.095	(0.292)	0.229
173	14.42	0.87	0.324	0.095	(0.292)	0.229
174	14.50	0.87	0.324	0.094	(0.292)	0.230
175	14.58	0.87	0.324	0.094	(0.292)	0.230
176	14.67	0.87	0.324	0.093	(0.292)	0.231
177	14.75	0.87	0.324	0.093	(0.292)	0.231
178	14.83	0.83	0.312	0.092	(0.280)	0.219
179	14.92	0.83	0.312	0.092	(0.280)	0.220
180	15.00	0.83	0.312	0.091	(0.280)	0.220
181	15.08	0.80	0.299	0.091	(0.269)	0.208
182	15.17	0.80	0.299	0.090	(0.269)	0.209
183	15.25	0.80	0.299	0.090	(0.269)	0.209
184	15.33	0.77	0.287	0.090	(0.258)	0.197
185	15.42	0.77	0.287	0.089	(0.258)	0.198
186	15.50	0.77	0.287	0.089	(0.258)	0.198
187	15.58	0.63	0.237	0.088	(0.213)	0.149
188	15.67	0.63	0.237	0.088	(0.213)	0.149
189	15.75	0.63	0.237	0.087	(0.213)	0.150
190	15.83	0.63	0.237	0.087	(0.213)	0.150
191	15.92	0.63	0.237	0.086	(0.213)	0.150
192	16.00	0.63	0.237	0.086	(0.213)	0.151
193	16.08	0.13	0.050	(0.085)	0.045	0.005
194	16.17	0.13	0.050	(0.085)	0.045	0.005
195	16.25	0.13	0.050	(0.085)	0.045	0.005
196	16.33	0.13	0.050	(0.084)	0.045	0.005
197	16.42	0.13	0.050	(0.084)	0.045	0.005
198	16.50	0.13	0.050	(0.083)	0.045	0.005
199	16.58	0.10	0.037	(0.083)	0.034	0.004
200	16.67	0.10	0.037	(0.082)	0.034	0.004
201	16.75	0.10	0.037	(0.082)	0.034	0.004
202	16.83	0.10	0.037	(0.082)	0.034	0.004
203	16.92	0.10	0.037	(0.081)	0.034	0.004
204	17.00	0.10	0.037	(0.081)	0.034	0.004
205	17.08	0.17	0.062	(0.080)	0.056	0.006
206	17.17	0.17	0.062	(0.080)	0.056	0.006
207	17.25	0.17	0.062	(0.080)	0.056	0.006
208	17.33	0.17	0.062	(0.079)	0.056	0.006
209	17.42	0.17	0.062	(0.079)	0.056	0.006
210	17.50	0.17	0.062	(0.078)	0.056	0.006
211	17.58	0.17	0.062	(0.078)	0.056	0.006
212	17.67	0.17	0.062	(0.078)	0.056	0.006
213	17.75	0.17	0.062	(0.077)	0.056	0.006
214	17.83	0.13	0.050	(0.077)	0.045	0.005
215	17.92	0.13	0.050	(0.076)	0.045	0.005
216	18.00	0.13	0.050	(0.076)	0.045	0.005
217	18.08	0.13	0.050	(0.076)	0.045	0.005
218	18.17	0.13	0.050	(0.075)	0.045	0.005
219	18.25	0.13	0.050	(0.075)	0.045	0.005
220	18.33	0.13	0.050	(0.075)	0.045	0.005
221	18.42	0.13	0.050	(0.074)	0.045	0.005
222	18.50	0.13	0.050	(0.074)	0.045	0.005
223	18.58	0.10	0.037	(0.074)	0.034	0.004
224	18.67	0.10	0.037	(0.073)	0.034	0.004
225	18.75	0.10	0.037	(0.073)	0.034	0.004
226	18.83	0.07	0.025	(0.072)	0.022	0.002
227	18.92	0.07	0.025	(0.072)	0.022	0.002
228	19.00	0.07	0.025	(0.072)	0.022	0.002
229	19.08	0.10	0.037	(0.071)	0.034	0.004
230	19.17	0.10	0.037	(0.071)	0.034	0.004
231	19.25	0.10	0.037	(0.071)	0.034	0.004
232	19.33	0.13	0.050	(0.070)	0.045	0.005
233	19.42	0.13	0.050	(0.070)	0.045	0.005
234	19.50	0.13	0.050	(0.070)	0.045	0.005
235	19.58	0.10	0.037	(0.069)	0.034	0.004
236	19.67	0.10	0.037	(0.069)	0.034	0.004
237	19.75	0.10	0.037	(0.069)	0.034	0.004
238	19.83	0.07	0.025	(0.069)	0.022	0.002
239	19.92	0.07	0.025	(0.068)	0.022	0.002
240	20.00	0.07	0.025	(0.068)	0.022	0.002
241	20.08	0.10	0.037	(0.068)	0.034	0.004
242	20.17	0.10	0.037	(0.067)	0.034	0.004

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243  20.25     0.10      0.037       (  0.067)       0.034        0.004
244  20.33     0.10      0.037       (  0.067)       0.034        0.004
245  20.42     0.10      0.037       (  0.066)       0.034        0.004
246  20.50     0.10      0.037       (  0.066)       0.034        0.004
247  20.58     0.10      0.037       (  0.066)       0.034        0.004
248  20.67     0.10      0.037       (  0.066)       0.034        0.004
249  20.75     0.10      0.037       (  0.065)       0.034        0.004
250  20.83     0.07      0.025       (  0.065)       0.022        0.002
251  20.92     0.07      0.025       (  0.065)       0.022        0.002
252  21.00     0.07      0.025       (  0.065)       0.022        0.002
253  21.08     0.10      0.037       (  0.064)       0.034        0.004
254  21.17     0.10      0.037       (  0.064)       0.034        0.004
255  21.25     0.10      0.037       (  0.064)       0.034        0.004
256  21.33     0.07      0.025       (  0.064)       0.022        0.002
257  21.42     0.07      0.025       (  0.063)       0.022        0.002
258  21.50     0.07      0.025       (  0.063)       0.022        0.002
259  21.58     0.10      0.037       (  0.063)       0.034        0.004
260  21.67     0.10      0.037       (  0.063)       0.034        0.004
261  21.75     0.10      0.037       (  0.062)       0.034        0.004
262  21.83     0.07      0.025       (  0.062)       0.022        0.002
263  21.92     0.07      0.025       (  0.062)       0.022        0.002
264  22.00     0.07      0.025       (  0.062)       0.022        0.002
265  22.08     0.10      0.037       (  0.062)       0.034        0.004
266  22.17     0.10      0.037       (  0.061)       0.034        0.004
267  22.25     0.10      0.037       (  0.061)       0.034        0.004
268  22.33     0.07      0.025       (  0.061)       0.022        0.002
269  22.42     0.07      0.025       (  0.061)       0.022        0.002
270  22.50     0.07      0.025       (  0.061)       0.022        0.002
271  22.58     0.07      0.025       (  0.060)       0.022        0.002
272  22.67     0.07      0.025       (  0.060)       0.022        0.002
273  22.75     0.07      0.025       (  0.060)       0.022        0.002
274  22.83     0.07      0.025       (  0.060)       0.022        0.002
275  22.92     0.07      0.025       (  0.060)       0.022        0.002
276  23.00     0.07      0.025       (  0.060)       0.022        0.002
277  23.08     0.07      0.025       (  0.060)       0.022        0.002
278  23.17     0.07      0.025       (  0.059)       0.022        0.002
279  23.25     0.07      0.025       (  0.059)       0.022        0.002
280  23.33     0.07      0.025       (  0.059)       0.022        0.002
281  23.42     0.07      0.025       (  0.059)       0.022        0.002
282  23.50     0.07      0.025       (  0.059)       0.022        0.002
283  23.58     0.07      0.025       (  0.059)       0.022        0.002
284  23.67     0.07      0.025       (  0.059)       0.022        0.002
285  23.75     0.07      0.025       (  0.059)       0.022        0.002
286  23.83     0.07      0.025       (  0.059)       0.022        0.002
287  23.92     0.07      0.025       (  0.059)       0.022        0.002
288  24.00     0.07      0.025       (  0.059)       0.022        0.002
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    16.7
      Flood volume = Effective rainfall      1.39(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       0.9(Ac.Ft)
      Total soil loss =      1.72(In)
      Total soil loss =     1.120(Ac.Ft)
      Total rainfall =      3.12(In)
      Flood volume =       39348.5 Cubic Feet
      Total soil loss =       48777.7 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      2.538(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0000      0.01  Q          |         |         |         |
   0+10       0.0001      0.02  Q          |         |         |         |
   0+15       0.0003      0.02  Q          |         |         |         |
   0+20       0.0004      0.02  Q          |         |         |         |
   0+25       0.0006      0.03  Q          |         |         |         |
   0+30       0.0008      0.03  Q          |         |         |         |
   0+35       0.0010      0.03  Q          |         |         |         |
   0+40       0.0012      0.03  Q          |         |         |         |
   0+45       0.0014      0.03  Q          |         |         |         |
   0+50       0.0016      0.03  Q          |         |         |         |
   0+55       0.0019      0.04  Q          |         |         |         |
   1+ 0       0.0021      0.04  Q          |         |         |         |
   1+ 5       0.0024      0.04  Q          |         |         |         |
   1+10       0.0026      0.03  Q          |         |         |         |
   1+15       0.0028      0.03  Q          |         |         |         |
   1+20       0.0030      0.03  Q          |         |         |         |
   1+25       0.0032      0.03  Q          |         |         |         |
   1+30       0.0034      0.03  Q          |         |         |         |
   1+35       0.0036      0.03  Q          |         |         |         |
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1+40	0.0038	0.03	Q	|	|	|	|
1+45	0.0040	0.03	Q	|	|	|	|
1+50	0.0043	0.03	Q	|	|	|	|
1+55	0.0045	0.04	Q	|	|	|	|
2+ 0	0.0048	0.04	Q	|	|	|	|
2+ 5	0.0050	0.04	Q	|	|	|	|
2+10	0.0053	0.04	Q	|	|	|	|
2+15	0.0056	0.04	Q	|	|	|	|
2+20	0.0059	0.04	Q	|	|	|	|
2+25	0.0061	0.04	Q	|	|	|	|
2+30	0.0064	0.04	Q	|	|	|	|
2+35	0.0067	0.04	Q	|	|	|	|
2+40	0.0070	0.05	Q	|	|	|	|
2+45	0.0073	0.05	Q	|	|	|	|
2+50	0.0077	0.05	Q	|	|	|	|
2+55	0.0080	0.05	Q	|	|	|	|
3+ 0	0.0083	0.05	Q	|	|	|	|
3+ 5	0.0087	0.05	Q	|	|	|	|
3+10	0.0090	0.05	Q	|	|	|	|
3+15	0.0094	0.05	Q	|	|	|	|
3+20	0.0097	0.05	Q	|	|	|	|
3+25	0.0100	0.05	Q	|	|	|	|
3+30	0.0104	0.05	Q	|	|	|	|
3+35	0.0107	0.05	Q	|	|	|	|
3+40	0.0110	0.05	Q	|	|	|	|
3+45	0.0114	0.05	Q	|	|	|	|
3+50	0.0117	0.05	Q	|	|	|	|
3+55	0.0121	0.06	Q	|	|	|	|
4+ 0	0.0125	0.06	Q	|	|	|	|
4+ 5	0.0129	0.06	Q	|	|	|	|
4+10	0.0133	0.06	Q	|	|	|	|
4+15	0.0137	0.06	Q	|	|	|	|
4+20	0.0142	0.06	Q	|	|	|	|
4+25	0.0146	0.07	Q	|	|	|	|
4+30	0.0151	0.07	Q	|	|	|	|
4+35	0.0156	0.07	Q	|	|	|	|
4+40	0.0160	0.07	Q	|	|	|	|
4+45	0.0165	0.07	Q	|	|	|	|
4+50	0.0170	0.07	Q	|	|	|	|
4+55	0.0175	0.08	Q	|	|	|	|
5+ 0	0.0180	0.08	Q	|	|	|	|
5+ 5	0.0185	0.07	Q	|	|	|	|
5+10	0.0190	0.06	Q	|	|	|	|
5+15	0.0194	0.06	Q	|	|	|	|
5+20	0.0198	0.06	Q	|	|	|	|
5+25	0.0203	0.07	Q	|	|	|	|
5+30	0.0207	0.07	Q	|	|	|	|
5+35	0.0212	0.07	Q	|	|	|	|
5+40	0.0218	0.08	Q	|	|	|	|
5+45	0.0223	0.08	Q	|	|	|	|
5+50	0.0228	0.08	QV	|	|	|	|
5+55	0.0234	0.08	QV	|	|	|	|
6+ 0	0.0239	0.08	QV	|	|	|	|
6+ 5	0.0245	0.08	QV	|	|	|	|
6+10	0.0251	0.09	QV	|	|	|	|
6+15	0.0257	0.09	QV	|	|	|	|
6+20	0.0263	0.09	QV	|	|	|	|
6+25	0.0269	0.09	QV	|	|	|	|
6+30	0.0275	0.09	QV	|	|	|	|
6+35	0.0281	0.09	QV	|	|	|	|
6+40	0.0288	0.10	QV	|	|	|	|
6+45	0.0294	0.10	QV	|	|	|	|
6+50	0.0301	0.10	QV	|	|	|	|
6+55	0.0308	0.10	QV	|	|	|	|
7+ 0	0.0315	0.10	QV	|	|	|	|
7+ 5	0.0321	0.10	QV	|	|	|	|
7+10	0.0328	0.10	QV	|	|	|	|
7+15	0.0335	0.10	QV	|	|	|	|
7+20	0.0342	0.10	QV	|	|	|	|
7+25	0.0349	0.11	QV	|	|	|	|
7+30	0.0356	0.11	QV	|	|	|	|
7+35	0.0364	0.11	QV	|	|	|	|
7+40	0.0372	0.12	QV	|	|	|	|
7+45	0.0380	0.12	QV	|	|	|	|
7+50	0.0389	0.14	QV	|	|	|	|
7+55	0.0401	0.16	QV	|	|	|	|
8+ 0	0.0413	0.18	QV	|	|	|	|
8+ 5	0.0429	0.24	QV	|	|	|	|
8+10	0.0453	0.34	|QV	|	|	|	|
8+15	0.0479	0.37	|QV	|	|	|	|
8+20	0.0505	0.39	|QV	|	|	|	|
8+25	0.0533	0.40	|QV	|	|	|	|
8+30	0.0561	0.41	|QV	|	|	|	|
8+35	0.0591	0.44	|QV	|	|	|	|
8+40	0.0625	0.49	|QV	|	|	|	|
8+45	0.0660	0.51	| Q	|	|	|	|

```
 8+50       0.0698      0.55  | QV       |          |          |          |
 8+55       0.0740      0.60  | QV       |          |          |          |
 9+ 0       0.0782      0.62  | QV       |          |          |          |
 9+ 5       0.0830      0.69  | QV       |          |          |          |
 9+10       0.0885      0.79  |  Q       |          |          |          |
 9+15       0.0942      0.82  |  QV      |          |          |          |
 9+20       0.1001      0.87  |  QV      |          |          |          |
 9+25       0.1065      0.93  |  QV      |          |          |          |
 9+30       0.1130      0.94  |  Q V     |          |          |          |
 9+35       0.1198      0.99  |  Q V     |          |          |          |
 9+40       0.1270      1.04  |   QV     |          |          |          |
 9+45       0.1342      1.06  |   QV     |          |          |          |
 9+50       0.1418      1.10  |   Q V    |          |          |          |
 9+55       0.1497      1.15  |   Q V    |          |          |          |
10+ 0       0.1578      1.17  |   Q V    |          |          |          |
10+ 5       0.1644      0.97  |  Q   V   |          |          |          |
10+10       0.1689      0.65  | Q    V   |          |          |          |
10+15       0.1728      0.57  | Q    V   |          |          |          |
10+20       0.1766      0.54  | Q    V   |          |          |          |
10+25       0.1802      0.53  | Q    V   |          |          |          |
10+30       0.1838      0.52  | Q     V  |          |          |          |
10+35       0.1885      0.68  | Q     V  |          |          |          |
10+40       0.1948      0.92  |  Q    V  |          |          |          |
10+45       0.2015      0.98  |  Q    V  |          |          |          |
10+50       0.2085      1.01  |   Q    V|          |          |          |
10+55       0.2155      1.03  |   Q    V|          |          |          |
11+ 0       0.2227      1.04  |   Q    V|          |          |          |
11+ 5       0.2296      1.01  |   Q     V          |          |          |
11+10       0.2363      0.97  | Q       V          |          |          |
11+15       0.2430      0.96  | Q       V          |          |          |
11+20       0.2496      0.96  | Q       |V         |          |          |
11+25       0.2562      0.96  | Q       |V         |          |          |
11+30       0.2629      0.97  | Q       |V         |          |          |
11+35       0.2692      0.91  | Q       |V         |          |          |
11+40       0.2748      0.82  | Q       | V        |          |          |
11+45       0.2804      0.80  | Q       | V        |          |          |
11+50       0.2861      0.83  | Q       | V        |          |          |
11+55       0.2921      0.87  | Q       | V        |          |          |
12+ 0       0.2982      0.89  | Q       |  V       |          |          |
12+ 5       0.3058      1.11  |  Q      |  V       |          |          |
12+10       0.3158      1.44  |   Q     |  V       |          |          |
12+15       0.3263      1.53  |    Q    |   V      |          |          |
12+20       0.3373      1.60  |    Q    |   V      |          |          |
12+25       0.3488      1.67  |    Q    |    V     |          |          |
12+30       0.3605      1.70  |    Q    |    V     |          |          |
12+35       0.3726      1.77  |     Q   |     V    |          |          |
12+40       0.3855      1.87  |     Q   |      V   |          |          |
12+45       0.3985      1.89  |     Q   |      V   |          |          |
12+50       0.4119      1.94  |     Q   |       V  |          |          |
12+55       0.4256      2.00  |     Q   |       V  |          |          |
13+ 0       0.4395      2.01  |      Q  |        V|          |          |
13+ 5       0.4545      2.18  |      Q  |         V          |          |
13+10       0.4711      2.42  |       Q|         V          |          |
13+15       0.4882      2.48  |       Q|          V         |          |
13+20       0.5055      2.51  |        Q         | V       |          |
13+25       0.5228      2.53  |        Q         |  V      |          |
13+30       0.5403      2.54  |        Q         |  V      |          |
13+35       0.5555      2.21  |      Q   |       |   V     |          |
13+40       0.5672      1.70  |     Q    |       |    V    |          |
13+45       0.5781      1.58  |     Q    |       |    V    |          |
13+50       0.5886      1.52  |     Q    |       |     V   |          |
13+55       0.5989      1.50  |    Q     |       |     V   |          |
14+ 0       0.6091      1.48  |    Q     |       |     V   |          |
14+ 5       0.6202      1.61  |     Q    |       |      V  |          |
14+10       0.6326      1.80  |      Q   |       |       V |          |
14+15       0.6453      1.85  |      Q   |       |       V |          |
14+20       0.6580      1.84  |      Q   |       |        V|          |
14+25       0.6705      1.81  |      Q   |       |        V|          |
14+30       0.6830      1.81  |      Q   |       |         V          |
14+35       0.6955      1.81  |      Q   |       |         V          |
14+40       0.7079      1.81  |      Q   |       |          |V         |
14+45       0.7204      1.81  |      Q   |       |          |V         |
14+50       0.7327      1.79  |      Q   |       |          | V        |
14+55       0.7447      1.74  |     Q    |       |          | V        |
15+ 0       0.7567      1.74  |     Q    |       |          |  V       |
15+ 5       0.7684      1.70  |     Q    |       |          |   V      |
15+10       0.7798      1.66  |     Q    |       |          |   V      |
15+15       0.7912      1.65  |     Q    |       |          |    V     |
15+20       0.8023      1.62  |     Q    |       |          |    V     |
15+25       0.8131      1.57  |     Q    |       |          |     V    |
15+30       0.8239      1.56  |     Q    |       |          |     V    |
15+35       0.8338      1.44  |    Q     |       |          |     V    |
15+40       0.8424      1.25  |    Q     |       |          |      V   |
15+45       0.8508      1.21  |   Q      |       |          |      V   |
15+50       0.8590      1.19  |   Q      |       |          |       V  |
15+55       0.8671      1.19  |   Q      |       |          |       V  |
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16+ 0       0.8753      1.18  |    Q      |           |           |         V |
16+ 5       0.8810      0.83  |   Q       |           |           |           V|
16+10       0.8829      0.28  |Q          |           |           |           V|
16+15       0.8839      0.15  Q           |           |           |           V|
16+20       0.8846      0.09  Q           |           |           |           V|
16+25       0.8850      0.06  Q           |           |           |           V|
16+30       0.8852      0.04  Q           |           |           |           V|
16+35       0.8855      0.04  Q           |           |           |           V|
16+40       0.8857      0.03  Q           |           |           |           V|
16+45       0.8859      0.03  Q           |           |           |           V|
16+50       0.8861      0.03  Q           |           |           |           V|
16+55       0.8863      0.03  Q           |           |           |           V|
17+ 0       0.8865      0.03  Q           |           |           |           V|
17+ 5       0.8868      0.04  Q           |           |           |           V|
17+10       0.8871      0.04  Q           |           |           |           V|
17+15       0.8874      0.05  Q           |           |           |           V|
17+20       0.8877      0.05  Q           |           |           |           V|
17+25       0.8881      0.05  Q           |           |           |           V|
17+30       0.8884      0.05  Q           |           |           |           V|
17+35       0.8887      0.05  Q           |           |           |           V|
17+40       0.8891      0.05  Q           |           |           |           V|
17+45       0.8894      0.05  Q           |           |           |           V|
17+50       0.8897      0.05  Q           |           |           |           V|
17+55       0.8900      0.04  Q           |           |           |           V|
18+ 0       0.8903      0.04  Q           |           |           |           V|
18+ 5       0.8906      0.04  Q           |           |           |           V|
18+10       0.8908      0.04  Q           |           |           |           V|
18+15       0.8911      0.04  Q           |           |           |           V|
18+20       0.8914      0.04  Q           |           |           |           V|
18+25       0.8916      0.04  Q           |           |           |           V|
18+30       0.8919      0.04  Q           |           |           |           V|
18+35       0.8922      0.04  Q           |           |           |           V|
18+40       0.8924      0.03  Q           |           |           |           V|
18+45       0.8926      0.03  Q           |           |           |           V|
18+50       0.8928      0.03  Q           |           |           |           V|
18+55       0.8929      0.02  Q           |           |           |           V|
19+ 0       0.8931      0.02  Q           |           |           |           V|
19+ 5       0.8932      0.02  Q           |           |           |           V|
19+10       0.8934      0.03  Q           |           |           |           V|
19+15       0.8936      0.03  Q           |           |           |           V|
19+20       0.8938      0.03  Q           |           |           |           V|
19+25       0.8941      0.04  Q           |           |           |           V|
19+30       0.8943      0.04  Q           |           |           |           V|
19+35       0.8946      0.04  Q           |           |           |           V|
19+40       0.8948      0.03  Q           |           |           |           V|
19+45       0.8950      0.03  Q           |           |           |           V|
19+50       0.8952      0.03  Q           |           |           |           V|
19+55       0.8953      0.02  Q           |           |           |           V|
20+ 0       0.8955      0.02  Q           |           |           |           V|
20+ 5       0.8956      0.02  Q           |           |           |           V|
20+10       0.8958      0.03  Q           |           |           |           V|
20+15       0.8960      0.03  Q           |           |           |           V|
20+20       0.8962      0.03  Q           |           |           |           V|
20+25       0.8964      0.03  Q           |           |           |           V|
20+30       0.8966      0.03  Q           |           |           |           V|
20+35       0.8968      0.03  Q           |           |           |           V|
20+40       0.8970      0.03  Q           |           |           |           V|
20+45       0.8972      0.03  Q           |           |           |           V|
20+50       0.8974      0.03  Q           |           |           |           V|
20+55       0.8976      0.02  Q           |           |           |           V|
21+ 0       0.8977      0.02  Q           |           |           |           V|
21+ 5       0.8979      0.02  Q           |           |           |           V|
21+10       0.8981      0.03  Q           |           |           |           V|
21+15       0.8983      0.03  Q           |           |           |           V|
21+20       0.8984      0.03  Q           |           |           |           V|
21+25       0.8986      0.02  Q           |           |           |           V|
21+30       0.8987      0.02  Q           |           |           |           V|
21+35       0.8989      0.02  Q           |           |           |           V|
21+40       0.8991      0.03  Q           |           |           |           V|
21+45       0.8993      0.03  Q           |           |           |           V|
21+50       0.8994      0.03  Q           |           |           |           V|
21+55       0.8996      0.02  Q           |           |           |           V|
22+ 0       0.8997      0.02  Q           |           |           |           V|
22+ 5       0.8999      0.02  Q           |           |           |           V|
22+10       0.9001      0.03  Q           |           |           |           V|
22+15       0.9003      0.03  Q           |           |           |           V|
22+20       0.9005      0.03  Q           |           |           |           V|
22+25       0.9006      0.02  Q           |           |           |           V|
22+30       0.9007      0.02  Q           |           |           |           V|
22+35       0.9009      0.02  Q           |           |           |           V|
22+40       0.9010      0.02  Q           |           |           |           V|
22+45       0.9012      0.02  Q           |           |           |           V|
22+50       0.9013      0.02  Q           |           |           |           V|
22+55       0.9014      0.02  Q           |           |           |           V|
23+ 0       0.9016      0.02  Q           |           |           |           V|
23+ 5       0.9017      0.02  Q           |           |           |           V|
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   23+10       0.9018      0.02  Q          |          |          |          v|
   23+15       0.9020      0.02  Q          |          |          |          v|
   23+20       0.9021      0.02  Q          |          |          |          v|
   23+25       0.9022      0.02  Q          |          |          |          v|
   23+30       0.9024      0.02  Q          |          |          |          v|
   23+35       0.9025      0.02  Q          |          |          |          v|
   23+40       0.9026      0.02  Q          |          |          |          v|
   23+45       0.9028      0.02  Q          |          |          |          v|
   23+50       0.9029      0.02  Q          |          |          |          v|
   23+55       0.9030      0.02  Q          |          |          |          v|
   24+ 0       0.9032      0.02  Q          |          |          |          v|
   24+ 5       0.9033      0.01  Q          |          |          |          v|
   24+10       0.9033      0.00  Q          |          |          |          v|
   24+15       0.9033      0.00  Q          |          |          |          v|
   24+20       0.9033      0.00  Q          |          |          |          v|
   24+25       0.9033      0.00  Q          |          |          |          v|
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U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 1222.00(Ft.)
Length along longest watercourse measured to centroid = 611.00(Ft.)
Length along longest watercourse = 0.231 Mi.
Length along longest watercourse measured to centroid = 0.116 Mi.
Difference in elevation = 89.00(Ft.)
Slope along watercourse = 384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.059 Hr.
Lag time = 3.52 Min.
25% of lag time = 0.88 Min.
40% of lag time = 1.41 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	0.50	3.90

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.30	10.13

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.300(In)

Point rain (area averaged) = 1.300(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.300(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	91.00	0.000

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

Slope of intensity-duration curve for a 1 hour storm =0.5500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
		Sum = 100.000	Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.515	0.117	(0.463)	0.398
2	0.17	4.20	0.655	0.117	(0.590)	0.538
3	0.25	4.40	0.686	0.117	(0.618)	0.569
4	0.33	4.80	0.749	0.117	(0.674)	0.632
5	0.42	5.20	0.811	0.117	(0.730)	0.694
6	0.50	6.20	0.967	0.117	(0.870)	0.850
7	0.58	6.80	1.061	0.117	(0.955)	0.944
8	0.67	8.80	1.373	0.117	(1.235)	1.256
9	0.75	13.90	2.168	0.117	(1.951)	2.051
10	0.83	31.40	4.898	0.117	(4.408)	4.781
11	0.92	7.20	1.123	0.117	(1.011)	1.006
12	1.00	3.80	0.593	0.117	(0.533)	0.476
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	14.2

Flood volume = Effective rainfall 1.18(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.8(Ac.Ft)
Total soil loss = 0.12(In)
Total soil loss = 0.076(Ac.Ft)
Total rainfall = 1.30(In)
Flood volume = 33449.9 Cubic Feet
Total soil loss = 3308.5 Cubic Feet

Peak flow rate of this hydrograph = 23.036(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0067	0.97	VQ				
0+10	0.0260	2.80	V Q				
0+15	0.0520	3.77	V Q				
0+20	0.0818	4.33	VQ				
0+25	0.1154	4.88	Q				
0+30	0.1544	5.65	QV				
0+35	0.1996	6.57	Q V				
0+40	0.2539	7.87	Q V				
0+45	0.3307	11.16	Q V				
0+50	0.4766	21.18	V Q				
0+55	0.6352	23.04	Q V				
1+ 0	0.7078	10.53	Q			V	
1+ 5	0.7438	5.24	Q			V	
1+10	0.7586	2.14	Q			V	
1+15	0.7658	1.05	Q			V	
1+20	0.7675	0.24	Q			V	
1+25	0.7679	0.06	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

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Length along longest watercourse measured to centroid = 0.116 Mi.
Difference in elevation = 89.00(Ft.)
Slope along watercourse = 384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.059 Hr.
Lag time = 3.52 Min.
25% of lag time = 0.88 Min.
40% of lag time = 1.41 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	0.80	6.23

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	2.00	15.58

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 2.000(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 2.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	91.00	0.000

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
		Sum = 100.000	Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.312	0.117	(0.281)	0.195
2	0.17	1.30	0.312	0.117	(0.281)	0.195
3	0.25	1.10	0.264	0.117	(0.238)	0.147
4	0.33	1.50	0.360	0.117	(0.324)	0.243
5	0.42	1.50	0.360	0.117	(0.324)	0.243
6	0.50	1.80	0.432	0.117	(0.389)	0.315
7	0.58	1.50	0.360	0.117	(0.324)	0.243
8	0.67	1.80	0.432	0.117	(0.389)	0.315
9	0.75	1.80	0.432	0.117	(0.389)	0.315
10	0.83	1.50	0.360	0.117	(0.324)	0.243
11	0.92	1.60	0.384	0.117	(0.346)	0.267
12	1.00	1.80	0.432	0.117	(0.389)	0.315
13	1.08	2.20	0.528	0.117	(0.475)	0.411
14	1.17	2.20	0.528	0.117	(0.475)	0.411
15	1.25	2.20	0.528	0.117	(0.475)	0.411
16	1.33	2.00	0.480	0.117	(0.432)	0.363
17	1.42	2.60	0.624	0.117	(0.562)	0.507
18	1.50	2.70	0.648	0.117	(0.583)	0.531
19	1.58	2.40	0.576	0.117	(0.518)	0.459
20	1.67	2.70	0.648	0.117	(0.583)	0.531
21	1.75	3.30	0.792	0.117	(0.713)	0.675
22	1.83	3.10	0.744	0.117	(0.670)	0.627
23	1.92	2.90	0.696	0.117	(0.626)	0.579
24	2.00	3.00	0.720	0.117	(0.648)	0.603
25	2.08	3.10	0.744	0.117	(0.670)	0.627
26	2.17	4.20	1.008	0.117	(0.907)	0.891
27	2.25	5.00	1.200	0.117	(1.080)	1.083
28	2.33	3.50	0.840	0.117	(0.756)	0.723
29	2.42	6.80	1.632	0.117	(1.469)	1.515
30	2.50	7.30	1.752	0.117	(1.577)	1.635
31	2.58	8.20	1.968	0.117	(1.771)	1.851
32	2.67	5.90	1.416	0.117	(1.274)	1.299
33	2.75	2.00	0.480	0.117	(0.432)	0.363
34	2.83	1.80	0.432	0.117	(0.389)	0.315
35	2.92	1.80	0.432	0.117	(0.389)	0.315
36	3.00	0.60	0.144	0.117	(0.130)	0.027
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	19.8

Flood volume = Effective rainfall 1.65(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 1.1(Ac.Ft)
Total soil loss = 0.35(In)
Total soil loss = 0.228(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 46628.0 Cubic Feet
Total soil loss = 9925.5 Cubic Feet

Peak flow rate of this hydrograph = 12.675(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0033	0.48	Q	|	|	|	|
0+10	0.0116	1.21	V Q	|	|	|	|
0+15	0.0203	1.27	V Q	|	|	|	|
0+20	0.0300	1.40	|VQ	|	|	|	|
0+25	0.0421	1.76	|V Q	|	|	|	|
0+30	0.0561	2.03	| V Q	|	|	|	|
0+35	0.0709	2.15	| V Q	|	|	|	|
0+40	0.0856	2.14	| VQ	|	|	|	|
0+45	0.1020	2.38	| VQ	|	|	|	|
0+50	0.1176	2.26	| Q	|	|	|	|
0+55	0.1318	2.07	| Q	|	|	|	|
1+ 0	0.1471	2.22	| QV	|	|	|	|
1+ 5	0.1653	2.64	| QV	|	|	|	|

```
    1+10       0.1862      3.03  |      Q   |          |          |          |
    1+15       0.2078      3.14  |      QV  |          |          |          |
    1+20       0.2289      3.07  |      Q V |          |          |          |
    1+25       0.2514      3.27  |      Q  V|          |          |          |
    1+30       0.2779      3.84  |       Q  V          |          |          |
    1+35       0.3045      3.86  |       Q  |V         |          |          |
    1+40       0.3309      3.84  |       Q  | V        |          |          |
    1+45       0.3614      4.43  |        Q |  V       |          |          |
    1+50       0.3953      4.91  |         Q|   V      |          |          |
    1+55       0.4281      4.76  |         Q|    V     |          |          |
    2+ 0       0.4602      4.66  |         Q|      V   |          |          |
    2+ 5       0.4931      4.79  |         Q|       V  |          |          |
    2+10       0.5313      5.54  |          |Q       V|          |          |
    2+15       0.5795      7.01  |          |   Q      |V         |          |
    2+20       0.6284      7.09  |          |   Q      |  V       |          |
    2+25       0.6834      7.98  |          |    Q     |    V     |          |
    2+30       0.7594     11.04  |          |          | Q     V  |          |
    2+35       0.8467     12.67  |          |          |    Q     |V         |
    2+40       0.9328     12.51  |          |          |    Q     |   V      |
    2+45       0.9915      8.52  |          |       Q  |          |      V   |
    2+50       1.0233      4.62  |         Q|          |          |       V  |
    2+55       1.0469      3.42  |     Q    |          |          |        V |
    3+ 0       1.0621      2.21  |   Q      |          |          |        V |
    3+ 5       1.0674      0.77  |Q         |          |          |        V |
    3+10       1.0692      0.27  Q          |          |          |        V |
    3+15       1.0701      0.12  Q          |          |          |        V |
    3+20       1.0704      0.05  Q          |          |          |        V |
    3+25       1.0704      0.00  Q          |          |          |         V
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: ex31006100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 1222.00(Ft.)
Length along longest watercourse measured to centroid = 611.00(Ft.)
Length along longest watercourse = 0.231 Mi.
Length along longest watercourse measured to centroid = 0.116 Mi.
Difference in elevation = 89.00(Ft.)
Slope along watercourse = 384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.059 Hr.
Lag time = 3.52 Min.
25% of lag time = 0.88 Min.
40% of lag time = 1.41 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.10	8.57

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	3.00	23.37

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 3.000(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	91.00	0.000

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
			Sum = 100.000 Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.180	0.117	(0.162)	0.063
2	0.17	0.60	0.216	0.117	(0.194)	0.099
3	0.25	0.60	0.216	0.117	(0.194)	0.099
4	0.33	0.60	0.216	0.117	(0.194)	0.099
5	0.42	0.60	0.216	0.117	(0.194)	0.099
6	0.50	0.70	0.252	0.117	(0.227)	0.135
7	0.58	0.70	0.252	0.117	(0.227)	0.135
8	0.67	0.70	0.252	0.117	(0.227)	0.135
9	0.75	0.70	0.252	0.117	(0.227)	0.135
10	0.83	0.70	0.252	0.117	(0.227)	0.135
11	0.92	0.70	0.252	0.117	(0.227)	0.135
12	1.00	0.80	0.288	0.117	(0.259)	0.171
13	1.08	0.80	0.288	0.117	(0.259)	0.171
14	1.17	0.80	0.288	0.117	(0.259)	0.171
15	1.25	0.80	0.288	0.117	(0.259)	0.171
16	1.33	0.80	0.288	0.117	(0.259)	0.171
17	1.42	0.80	0.288	0.117	(0.259)	0.171
18	1.50	0.80	0.288	0.117	(0.259)	0.171
19	1.58	0.80	0.288	0.117	(0.259)	0.171
20	1.67	0.80	0.288	0.117	(0.259)	0.171
21	1.75	0.80	0.288	0.117	(0.259)	0.171
22	1.83	0.80	0.288	0.117	(0.259)	0.171
23	1.92	0.80	0.288	0.117	(0.259)	0.171
24	2.00	0.90	0.324	0.117	(0.292)	0.207
25	2.08	0.80	0.288	0.117	(0.259)	0.171
26	2.17	0.90	0.324	0.117	(0.292)	0.207
27	2.25	0.90	0.324	0.117	(0.292)	0.207
28	2.33	0.90	0.324	0.117	(0.292)	0.207
29	2.42	0.90	0.324	0.117	(0.292)	0.207
30	2.50	0.90	0.324	0.117	(0.292)	0.207
31	2.58	0.90	0.324	0.117	(0.292)	0.207
32	2.67	0.90	0.324	0.117	(0.292)	0.207
33	2.75	1.00	0.360	0.117	(0.324)	0.243
34	2.83	1.00	0.360	0.117	(0.324)	0.243
35	2.92	1.00	0.360	0.117	(0.324)	0.243
36	3.00	1.00	0.360	0.117	(0.324)	0.243
37	3.08	1.00	0.360	0.117	(0.324)	0.243
38	3.17	1.10	0.396	0.117	(0.356)	0.279
39	3.25	1.10	0.396	0.117	(0.356)	0.279
40	3.33	1.10	0.396	0.117	(0.356)	0.279
41	3.42	1.20	0.432	0.117	(0.389)	0.315
42	3.50	1.30	0.468	0.117	(0.421)	0.351
43	3.58	1.40	0.504	0.117	(0.454)	0.387
44	3.67	1.40	0.504	0.117	(0.454)	0.387
45	3.75	1.50	0.540	0.117	(0.486)	0.423
46	3.83	1.50	0.540	0.117	(0.486)	0.423
47	3.92	1.60	0.576	0.117	(0.518)	0.459
48	4.00	1.60	0.576	0.117	(0.518)	0.459
49	4.08	1.70	0.612	0.117	(0.551)	0.495
50	4.17	1.80	0.648	0.117	(0.583)	0.531
51	4.25	1.90	0.684	0.117	(0.616)	0.567
52	4.33	2.00	0.720	0.117	(0.648)	0.603
53	4.42	2.10	0.756	0.117	(0.680)	0.639
54	4.50	2.10	0.756	0.117	(0.680)	0.639
55	4.58	2.20	0.792	0.117	(0.713)	0.675
56	4.67	2.30	0.828	0.117	(0.745)	0.711
57	4.75	2.40	0.864	0.117	(0.778)	0.747
58	4.83	2.40	0.864	0.117	(0.778)	0.747
59	4.92	2.50	0.900	0.117	(0.810)	0.783
60	5.00	2.60	0.936	0.117	(0.842)	0.819
61	5.08	3.10	1.116	0.117	(1.004)	0.999
62	5.17	3.60	1.296	0.117	(1.166)	1.179
63	5.25	3.90	1.404	0.117	(1.264)	1.287
64	5.33	4.20	1.512	0.117	(1.361)	1.395
65	5.42	4.70	1.692	0.117	(1.523)	1.575
66	5.50	5.60	2.016	0.117	(1.814)	1.899
67	5.58	1.90	0.684	0.117	(0.616)	0.567
68	5.67	0.90	0.324	0.117	(0.292)	0.207
69	5.75	0.60	0.216	0.117	(0.194)	0.099
70	5.83	0.50	0.180	0.117	(0.162)	0.063

```
71   5.92     0.30      0.108       (  0.117)       0.097        0.011
72   6.00     0.20      0.072       (  0.117)       0.065        0.007
               (Loss Rate Not Used)
   Sum =     100.0                                  Sum =    27.6
      Flood volume = Effective rainfall      2.30(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       1.5(Ac.Ft)
      Total soil loss =      0.70(In)
      Total soil loss =     0.452(Ac.Ft)
      Total rainfall =      3.00(In)
      Flood volume =       65149.6 Cubic Feet
      Total soil loss =       19681.3 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     12.721(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
-------------------------------------------------------------------------
  0+ 5       0.0011      0.15  Q         |          |          |          |
  0+10       0.0044      0.48  Q         |          |          |          |
  0+15       0.0090      0.67  VQ        |          |          |          |
  0+20       0.0140      0.73  VQ        |          |          |          |
  0+25       0.0192      0.76  VQ        |          |          |          |
  0+30       0.0251      0.86  VQ        |          |          |          |
  0+35       0.0320      1.00  V Q       |          |          |          |
  0+40       0.0391      1.03  |VQ       |          |          |          |
  0+45       0.0463      1.05  |VQ       |          |          |          |
  0+50       0.0536      1.06  |VQ       |          |          |          |
  0+55       0.0609      1.06  |VQ       |          |          |          |
  1+ 0       0.0688      1.15  |VQ       |          |          |          |
  1+ 5       0.0777      1.28  | Q       |          |          |          |
  1+10       0.0867      1.32  | Q       |          |          |          |
  1+15       0.0959      1.33  | Q       |          |          |          |
  1+20       0.1051      1.34  | Q       |          |          |          |
  1+25       0.1144      1.34  | QV      |          |          |          |
  1+30       0.1236      1.34  | QV      |          |          |          |
  1+35       0.1329      1.34  | QV      |          |          |          |
  1+40       0.1421      1.34  | QV      |          |          |          |
  1+45       0.1514      1.34  | Q V     |          |          |          |
  1+50       0.1606      1.34  | Q V     |          |          |          |
  1+55       0.1699      1.34  | Q V     |          |          |          |
  2+ 0       0.1797      1.43  | Q V     |          |          |          |
  2+ 5       0.1899      1.48  | Q  V    |          |          |          |
  2+10       0.2000      1.46  | Q  V    |          |          |          |
  2+15       0.2109      1.58  |  Q V    |          |          |          |
  2+20       0.2219      1.61  |  Q V    |          |          |          |
  2+25       0.2331      1.62  |  Q  V   |          |          |          |
  2+30       0.2442      1.62  |  Q  V   |          |          |          |
  2+35       0.2554      1.63  |  Q  V   |          |          |          |
  2+40       0.2666      1.63  |  Q   V  |          |          |          |
  2+45       0.2784      1.71  |  Q   V  |          |          |          |
  2+50       0.2912      1.85  |  Q   V  |          |          |          |
  2+55       0.3041      1.88  |  Q    V |          |          |          |
  3+ 0       0.3172      1.90  |  Q    V |          |          |          |
  3+ 5       0.3303      1.90  |  Q    V |          |          |          |
  3+10       0.3440      2.00  |  Q     V|          |          |          |
  3+15       0.3587      2.13  |   Q    V|          |          |          |
  3+20       0.3736      2.16  |   Q    V|          |          |          |
  3+25       0.3892      2.27  |   Q     V          |          |          |
  3+30       0.4064      2.50  |   Q     V          |          |          |
  3+35       0.4254      2.76  |    Q    |V         |          |          |
  3+40       0.4457      2.94  |    Q    |V         |          |          |
  3+45       0.4669      3.08  |     Q   | V        |          |          |
  3+50       0.4893      3.25  |     Q   |  V       |          |          |
  3+55       0.5125      3.38  |     Q   |  V       |          |          |
  4+ 0       0.5369      3.53  |      Q  |   V      |          |          |
  4+ 5       0.5621      3.66  |      Q  |    V     |          |          |
  4+10       0.5890      3.90  |      Q  |    V     |          |          |
  4+15       0.6177      4.17  |       Q |     V    |          |          |
  4+20       0.6483      4.44  |       Q |      V   |          |          |
  4+25       0.6808      4.72  |        Q|       V  |          |          |
  4+30       0.7146      4.91  |        Q|        V |          |          |
  4+35       0.7495      5.06  |         Q         V          |          |
  4+40       0.7861      5.31  |         Q         |V         |          |
  4+45       0.8245      5.58  |         |Q        | V        |          |
  4+50       0.8642      5.77  |         |Q        |  V       |          |
  4+55       0.9049      5.91  |         |Q        |   V      |          |
  5+ 0       0.9474      6.16  |         | Q       |    V     |          |
  5+ 5       0.9941      6.78  |         |  Q      |     V    |          |
  5+10       1.0488      7.95  |         |    Q    |      V   |          |
  5+15       1.1113      9.07  |         |      Q  |       V  |          |
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```
    5+20       1.1801      9.99  |          |         Q|          |V         |
    5+25       1.2562     11.05  |          |          | Q        |  V       |
    5+30       1.3438     12.72  |          |          |    Q     |    V     |
    5+35       1.4190     10.93  |          |          |Q         |      V   |
    5+40       1.4567      5.47  |          Q          |          |       V  |
    5+45       1.4762      2.83  |     Q    |          |          |        V|
    5+50       1.4870      1.56  |   Q      |          |          |        V|
    5+55       1.4926      0.81  |Q         |          |          |        V|
    6+ 0       1.4945      0.28  Q          |          |          |        V|
    6+ 5       1.4952      0.11  Q          |          |          |        V|
    6+10       1.4955      0.04  Q          |          |          |        V|
    6+15       1.4956      0.01  Q          |          |          |        V|
    6+20       1.4956      0.00  Q          |          |          |        V|
    6+25       1.4956      0.00  Q          |          |          |        V|
-------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: ex310024100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 1222.00(Ft.)
Length along longest watercourse measured to centroid = 611.00(Ft.)
Length along longest watercourse = 0.231 Mi.
Length along longest watercourse measured to centroid = 0.116 Mi.
Difference in elevation = 89.00(Ft.)
Slope along watercourse = 384.5499 Ft./Mi.
Average Manning's 'N' = 0.030
Lag time = 0.059 Hr.
Lag time = 3.52 Min.
25% of lag time = 0.88 Min.
40% of lag time = 1.41 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.80	14.02

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	5.00	38.95

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 5.000(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 5.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	91.00	0.000

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.000	0.117	1.000	0.117
					Sum (F) =	0.117

Area averaged mean soil loss (F) (In/Hr) = 0.117
Minimum soil loss rate ((In/Hr)) = 0.059
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.900

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	141.921	31.169	2.447
2	0.167	283.842	47.579	3.735
3	0.250	425.763	11.677	0.917
4	0.333	567.684	5.139	0.403
5	0.417	709.604	2.712	0.213
6	0.500	851.525	1.724	0.135
		Sum = 100.000	Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.040	(0.207)	0.036	0.004
2	0.17	0.07	0.040	(0.207)	0.036	0.004
3	0.25	0.07	0.040	(0.206)	0.036	0.004
4	0.33	0.10	0.060	(0.205)	0.054	0.006
5	0.42	0.10	0.060	(0.204)	0.054	0.006
6	0.50	0.10	0.060	(0.203)	0.054	0.006
7	0.58	0.10	0.060	(0.203)	0.054	0.006
8	0.67	0.10	0.060	(0.202)	0.054	0.006
9	0.75	0.10	0.060	(0.201)	0.054	0.006
10	0.83	0.13	0.080	(0.200)	0.072	0.008
11	0.92	0.13	0.080	(0.199)	0.072	0.008
12	1.00	0.13	0.080	(0.199)	0.072	0.008
13	1.08	0.10	0.060	(0.198)	0.054	0.006
14	1.17	0.10	0.060	(0.197)	0.054	0.006
15	1.25	0.10	0.060	(0.196)	0.054	0.006
16	1.33	0.10	0.060	(0.196)	0.054	0.006
17	1.42	0.10	0.060	(0.195)	0.054	0.006
18	1.50	0.10	0.060	(0.194)	0.054	0.006
19	1.58	0.10	0.060	(0.193)	0.054	0.006
20	1.67	0.10	0.060	(0.192)	0.054	0.006
21	1.75	0.10	0.060	(0.192)	0.054	0.006
22	1.83	0.13	0.080	(0.191)	0.072	0.008
23	1.92	0.13	0.080	(0.190)	0.072	0.008
24	2.00	0.13	0.080	(0.189)	0.072	0.008
25	2.08	0.13	0.080	(0.189)	0.072	0.008
26	2.17	0.13	0.080	(0.188)	0.072	0.008
27	2.25	0.13	0.080	(0.187)	0.072	0.008
28	2.33	0.13	0.080	(0.186)	0.072	0.008
29	2.42	0.13	0.080	(0.186)	0.072	0.008
30	2.50	0.13	0.080	(0.185)	0.072	0.008
31	2.58	0.17	0.100	(0.184)	0.090	0.010
32	2.67	0.17	0.100	(0.183)	0.090	0.010
33	2.75	0.17	0.100	(0.183)	0.090	0.010
34	2.83	0.17	0.100	(0.182)	0.090	0.010
35	2.92	0.17	0.100	(0.181)	0.090	0.010
36	3.00	0.17	0.100	(0.180)	0.090	0.010
37	3.08	0.17	0.100	(0.180)	0.090	0.010
38	3.17	0.17	0.100	(0.179)	0.090	0.010
39	3.25	0.17	0.100	(0.178)	0.090	0.010
40	3.33	0.17	0.100	(0.177)	0.090	0.010
41	3.42	0.17	0.100	(0.177)	0.090	0.010
42	3.50	0.17	0.100	(0.176)	0.090	0.010
43	3.58	0.17	0.100	(0.175)	0.090	0.010
44	3.67	0.17	0.100	(0.174)	0.090	0.010
45	3.75	0.17	0.100	(0.174)	0.090	0.010
46	3.83	0.20	0.120	(0.173)	0.108	0.012
47	3.92	0.20	0.120	(0.172)	0.108	0.012
48	4.00	0.20	0.120	(0.171)	0.108	0.012
49	4.08	0.20	0.120	(0.171)	0.108	0.012
50	4.17	0.20	0.120	(0.170)	0.108	0.012
51	4.25	0.20	0.120	(0.169)	0.108	0.012
52	4.33	0.23	0.140	(0.169)	0.126	0.014
53	4.42	0.23	0.140	(0.168)	0.126	0.014
54	4.50	0.23	0.140	(0.167)	0.126	0.014
55	4.58	0.23	0.140	(0.166)	0.126	0.014
56	4.67	0.23	0.140	(0.166)	0.126	0.014
57	4.75	0.23	0.140	(0.165)	0.126	0.014
58	4.83	0.27	0.160	(0.164)	0.144	0.016
59	4.92	0.27	0.160	(0.164)	0.144	0.016
60	5.00	0.27	0.160	(0.163)	0.144	0.016
61	5.08	0.20	0.120	(0.162)	0.108	0.012
62	5.17	0.20	0.120	(0.161)	0.108	0.012
63	5.25	0.20	0.120	(0.161)	0.108	0.012
64	5.33	0.23	0.140	(0.160)	0.126	0.014
65	5.42	0.23	0.140	(0.159)	0.126	0.014
66	5.50	0.23	0.140	(0.159)	0.126	0.014
67	5.58	0.27	0.160	(0.158)	0.144	0.016
68	5.67	0.27	0.160	(0.157)	0.144	0.016
69	5.75	0.27	0.160	(0.157)	0.144	0.016
70	5.83	0.27	0.160	(0.156)	0.144	0.016

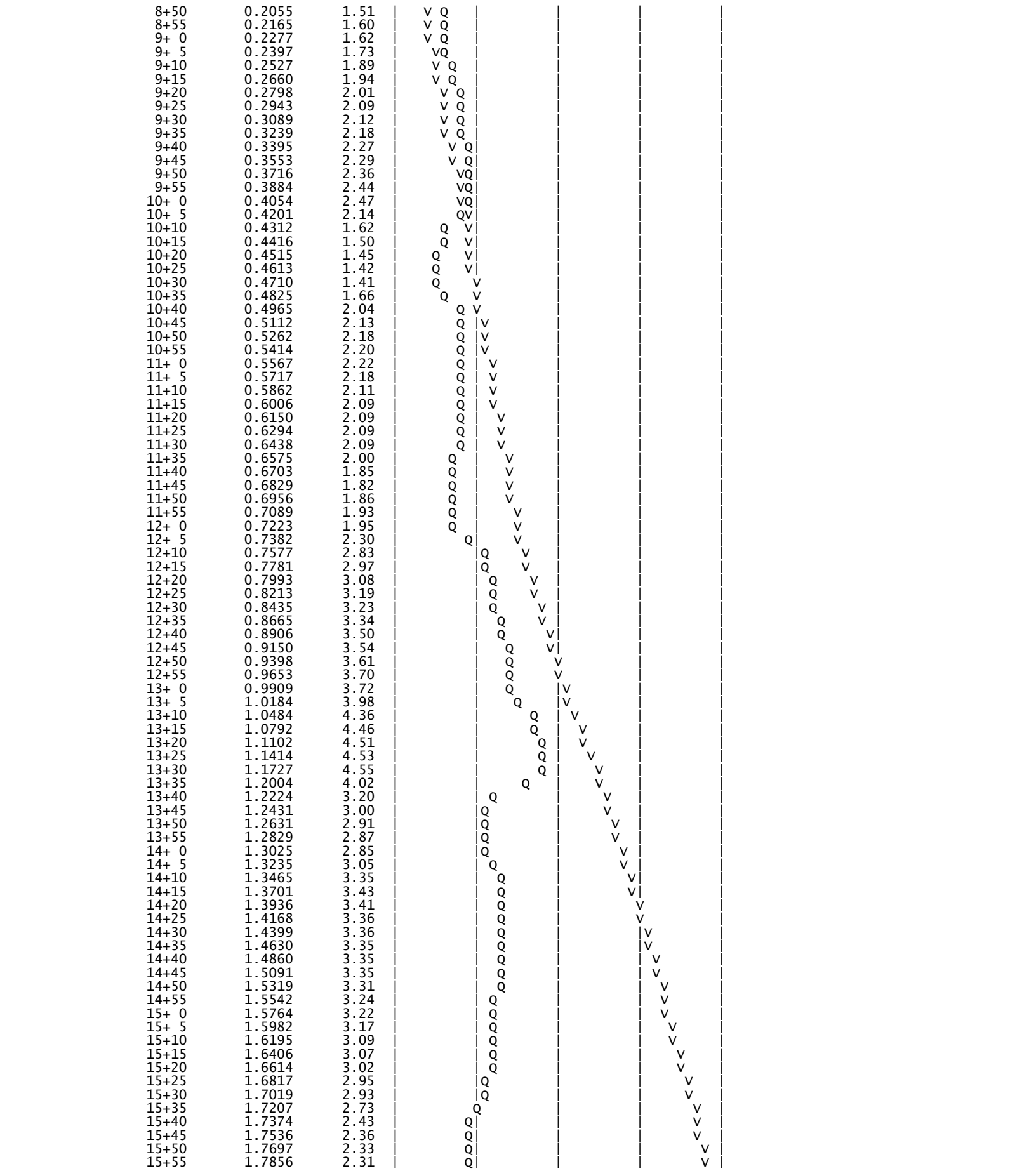
71	5.92	0.27	0.160	(	0.155)		0.144	0.016
72	6.00	0.27	0.160	(	0.154)		0.144	0.016
73	6.08	0.30	0.180		0.154	(	0.162)	0.026
74	6.17	0.30	0.180		0.153	(	0.162)	0.027
75	6.25	0.30	0.180		0.152	(	0.162)	0.028
76	6.33	0.30	0.180		0.152	(	0.162)	0.028
77	6.42	0.30	0.180		0.151	(	0.162)	0.029
78	6.50	0.30	0.180		0.150	(	0.162)	0.030
79	6.58	0.33	0.200		0.150	(	0.180)	0.050
80	6.67	0.33	0.200		0.149	(	0.180)	0.051
81	6.75	0.33	0.200		0.148	(	0.180)	0.052
82	6.83	0.33	0.200		0.148	(	0.180)	0.052
83	6.92	0.33	0.200		0.147	(	0.180)	0.053
84	7.00	0.33	0.200		0.146	(	0.180)	0.054
85	7.08	0.33	0.200		0.146	(	0.180)	0.054
86	7.17	0.33	0.200		0.145	(	0.180)	0.055
87	7.25	0.33	0.200		0.144	(	0.180)	0.056
88	7.33	0.37	0.220		0.144	(	0.198)	0.076
89	7.42	0.37	0.220		0.143	(	0.198)	0.077
90	7.50	0.37	0.220		0.142	(	0.198)	0.078
91	7.58	0.40	0.240		0.142	(	0.216)	0.098
92	7.67	0.40	0.240		0.141	(	0.216)	0.099
93	7.75	0.40	0.240		0.140	(	0.216)	0.100
94	7.83	0.43	0.260		0.140	(	0.234)	0.120
95	7.92	0.43	0.260		0.139	(	0.234)	0.121
96	8.00	0.43	0.260		0.138	(	0.234)	0.122
97	8.08	0.50	0.300		0.138	(	0.270)	0.162
98	8.17	0.50	0.300		0.137	(	0.270)	0.163
99	8.25	0.50	0.300		0.137	(	0.270)	0.163
100	8.33	0.50	0.300		0.136	(	0.270)	0.164
101	8.42	0.50	0.300		0.135	(	0.270)	0.165
102	8.50	0.50	0.300		0.135	(	0.270)	0.165
103	8.58	0.53	0.320		0.134	(	0.288)	0.186
104	8.67	0.53	0.320		0.133	(	0.288)	0.187
105	8.75	0.53	0.320		0.133	(	0.288)	0.187
106	8.83	0.57	0.340		0.132	(	0.306)	0.208
107	8.92	0.57	0.340		0.131	(	0.306)	0.209
108	9.00	0.57	0.340		0.131	(	0.306)	0.209
109	9.08	0.63	0.380		0.130	(	0.342)	0.250
110	9.17	0.63	0.380		0.130	(	0.342)	0.250
111	9.25	0.63	0.380		0.129	(	0.342)	0.251
112	9.33	0.67	0.400		0.128	(	0.360)	0.272
113	9.42	0.67	0.400		0.128	(	0.360)	0.272
114	9.50	0.67	0.400		0.127	(	0.360)	0.273
115	9.58	0.70	0.420		0.127	(	0.378)	0.293
116	9.67	0.70	0.420		0.126	(	0.378)	0.294
117	9.75	0.70	0.420		0.125	(	0.378)	0.295
118	9.83	0.73	0.440		0.125	(	0.396)	0.315
119	9.92	0.73	0.440		0.124	(	0.396)	0.316
120	10.00	0.73	0.440		0.124	(	0.396)	0.316
121	10.08	0.50	0.300		0.123	(	0.270)	0.177
122	10.17	0.50	0.300		0.122	(	0.270)	0.178
123	10.25	0.50	0.300		0.122	(	0.270)	0.178
124	10.33	0.50	0.300		0.121	(	0.270)	0.179
125	10.42	0.50	0.300		0.121	(	0.270)	0.179
126	10.50	0.50	0.300		0.120	(	0.270)	0.180
127	10.58	0.67	0.400		0.119	(	0.360)	0.281
128	10.67	0.67	0.400		0.119	(	0.360)	0.281
129	10.75	0.67	0.400		0.118	(	0.360)	0.282
130	10.83	0.67	0.400		0.118	(	0.360)	0.282
131	10.92	0.67	0.400		0.117	(	0.360)	0.283
132	11.00	0.67	0.400		0.117	(	0.360)	0.283
133	11.08	0.63	0.380		0.116	(	0.342)	0.264
134	11.17	0.63	0.380		0.115	(	0.342)	0.265
135	11.25	0.63	0.380		0.115	(	0.342)	0.265
136	11.33	0.63	0.380		0.114	(	0.342)	0.266
137	11.42	0.63	0.380		0.114	(	0.342)	0.266
138	11.50	0.63	0.380		0.113	(	0.342)	0.267
139	11.58	0.57	0.340		0.113	(	0.306)	0.227
140	11.67	0.57	0.340		0.112	(	0.306)	0.228
141	11.75	0.57	0.340		0.111	(	0.306)	0.229
142	11.83	0.60	0.360		0.111	(	0.324)	0.249
143	11.92	0.60	0.360		0.110	(	0.324)	0.250
144	12.00	0.60	0.360		0.110	(	0.324)	0.250
145	12.08	0.83	0.500		0.109	(	0.450)	0.391
146	12.17	0.83	0.500		0.109	(	0.450)	0.391
147	12.25	0.83	0.500		0.108	(	0.450)	0.392
148	12.33	0.87	0.520		0.108	(	0.468)	0.412
149	12.42	0.87	0.520		0.107	(	0.468)	0.413
150	12.50	0.87	0.520		0.107	(	0.468)	0.413
151	12.58	0.93	0.560		0.106	(	0.504)	0.454
152	12.67	0.93	0.560		0.105	(	0.504)	0.455
153	12.75	0.93	0.560		0.105	(	0.504)	0.455
154	12.83	0.97	0.580		0.104	(	0.522)	0.476
155	12.92	0.97	0.580		0.104	(	0.522)	0.476
156	13.00	0.97	0.580		0.103	(	0.522)	0.477

157	13.08	1.13	0.680	0.103	(0.612)	0.577
158	13.17	1.13	0.680	0.102	(0.612)	0.578
159	13.25	1.13	0.680	0.102	(0.612)	0.578
160	13.33	1.13	0.680	0.101	(0.612)	0.579
161	13.42	1.13	0.680	0.101	(0.612)	0.579
162	13.50	1.13	0.680	0.100	(0.612)	0.580
163	13.58	0.77	0.460	0.100	(0.414)	0.360
164	13.67	0.77	0.460	0.099	(0.414)	0.361
165	13.75	0.77	0.460	0.099	(0.414)	0.361
166	13.83	0.77	0.460	0.098	(0.414)	0.362
167	13.92	0.77	0.460	0.098	(0.414)	0.362
168	14.00	0.77	0.460	0.097	(0.414)	0.363
169	14.08	0.90	0.540	0.097	(0.486)	0.443
170	14.17	0.90	0.540	0.096	(0.486)	0.444
171	14.25	0.90	0.540	0.096	(0.486)	0.444
172	14.33	0.87	0.520	0.095	(0.468)	0.425
173	14.42	0.87	0.520	0.095	(0.468)	0.425
174	14.50	0.87	0.520	0.094	(0.468)	0.426
175	14.58	0.87	0.520	0.094	(0.468)	0.426
176	14.67	0.87	0.520	0.093	(0.468)	0.427
177	14.75	0.87	0.520	0.093	(0.468)	0.427
178	14.83	0.83	0.500	0.092	(0.450)	0.408
179	14.92	0.83	0.500	0.092	(0.450)	0.408
180	15.00	0.83	0.500	0.091	(0.450)	0.409
181	15.08	0.80	0.480	0.091	(0.432)	0.389
182	15.17	0.80	0.480	0.090	(0.432)	0.390
183	15.25	0.80	0.480	0.090	(0.432)	0.390
184	15.33	0.77	0.460	0.090	(0.414)	0.370
185	15.42	0.77	0.460	0.089	(0.414)	0.371
186	15.50	0.77	0.460	0.089	(0.414)	0.371
187	15.58	0.63	0.380	0.088	(0.342)	0.292
188	15.67	0.63	0.380	0.088	(0.342)	0.292
189	15.75	0.63	0.380	0.087	(0.342)	0.293
190	15.83	0.63	0.380	0.087	(0.342)	0.293
191	15.92	0.63	0.380	0.086	(0.342)	0.294
192	16.00	0.63	0.380	0.086	(0.342)	0.294
193	16.08	0.13	0.080	(0.085)	0.072	0.008
194	16.17	0.13	0.080	(0.085)	0.072	0.008
195	16.25	0.13	0.080	(0.085)	0.072	0.008
196	16.33	0.13	0.080	(0.084)	0.072	0.008
197	16.42	0.13	0.080	(0.084)	0.072	0.008
198	16.50	0.13	0.080	(0.083)	0.072	0.008
199	16.58	0.10	0.060	(0.083)	0.054	0.006
200	16.67	0.10	0.060	(0.082)	0.054	0.006
201	16.75	0.10	0.060	(0.082)	0.054	0.006
202	16.83	0.10	0.060	(0.082)	0.054	0.006
203	16.92	0.10	0.060	(0.081)	0.054	0.006
204	17.00	0.10	0.060	(0.081)	0.054	0.006
205	17.08	0.17	0.100	0.080	(0.090)	0.020
206	17.17	0.17	0.100	0.080	(0.090)	0.020
207	17.25	0.17	0.100	0.080	(0.090)	0.020
208	17.33	0.17	0.100	0.079	(0.090)	0.021
209	17.42	0.17	0.100	0.079	(0.090)	0.021
210	17.50	0.17	0.100	0.078	(0.090)	0.022
211	17.58	0.17	0.100	0.078	(0.090)	0.022
212	17.67	0.17	0.100	0.078	(0.090)	0.022
213	17.75	0.17	0.100	0.077	(0.090)	0.023
214	17.83	0.13	0.080	(0.077)	0.072	0.008
215	17.92	0.13	0.080	(0.076)	0.072	0.008
216	18.00	0.13	0.080	(0.076)	0.072	0.008
217	18.08	0.13	0.080	(0.076)	0.072	0.008
218	18.17	0.13	0.080	(0.075)	0.072	0.008
219	18.25	0.13	0.080	(0.075)	0.072	0.008
220	18.33	0.13	0.080	(0.075)	0.072	0.008
221	18.42	0.13	0.080	(0.074)	0.072	0.008
222	18.50	0.13	0.080	(0.074)	0.072	0.008
223	18.58	0.10	0.060	(0.074)	0.054	0.006
224	18.67	0.10	0.060	(0.073)	0.054	0.006
225	18.75	0.10	0.060	(0.073)	0.054	0.006
226	18.83	0.07	0.040	(0.072)	0.036	0.004
227	18.92	0.07	0.040	(0.072)	0.036	0.004
228	19.00	0.07	0.040	(0.072)	0.036	0.004
229	19.08	0.10	0.060	(0.071)	0.054	0.006
230	19.17	0.10	0.060	(0.071)	0.054	0.006
231	19.25	0.10	0.060	(0.071)	0.054	0.006
232	19.33	0.13	0.080	0.070	(0.072)	0.010
233	19.42	0.13	0.080	0.070	(0.072)	0.010
234	19.50	0.13	0.080	0.070	(0.072)	0.010
235	19.58	0.10	0.060	(0.069)	0.054	0.006
236	19.67	0.10	0.060	(0.069)	0.054	0.006
237	19.75	0.10	0.060	(0.069)	0.054	0.006
238	19.83	0.07	0.040	(0.069)	0.036	0.004
239	19.92	0.07	0.040	(0.068)	0.036	0.004
240	20.00	0.07	0.040	(0.068)	0.036	0.004
241	20.08	0.10	0.060	(0.068)	0.054	0.006
242	20.17	0.10	0.060	(0.067)	0.054	0.006

```
243  20.25     0.10      0.060       (  0.067)       0.054        0.006
244  20.33     0.10      0.060       (  0.067)       0.054        0.006
245  20.42     0.10      0.060       (  0.066)       0.054        0.006
246  20.50     0.10      0.060       (  0.066)       0.054        0.006
247  20.58     0.10      0.060       (  0.066)       0.054        0.006
248  20.67     0.10      0.060       (  0.066)       0.054        0.006
249  20.75     0.10      0.060       (  0.065)       0.054        0.006
250  20.83     0.07      0.040       (  0.065)       0.036        0.004
251  20.92     0.07      0.040       (  0.065)       0.036        0.004
252  21.00     0.07      0.040       (  0.065)       0.036        0.004
253  21.08     0.10      0.060       (  0.064)       0.054        0.006
254  21.17     0.10      0.060       (  0.064)       0.054        0.006
255  21.25     0.10      0.060       (  0.064)       0.054        0.006
256  21.33     0.07      0.040       (  0.064)       0.036        0.004
257  21.42     0.07      0.040       (  0.063)       0.036        0.004
258  21.50     0.07      0.040       (  0.063)       0.036        0.004
259  21.58     0.10      0.060       (  0.063)       0.054        0.006
260  21.67     0.10      0.060       (  0.063)       0.054        0.006
261  21.75     0.10      0.060       (  0.062)       0.054        0.006
262  21.83     0.07      0.040       (  0.062)       0.036        0.004
263  21.92     0.07      0.040       (  0.062)       0.036        0.004
264  22.00     0.07      0.040       (  0.062)       0.036        0.004
265  22.08     0.10      0.060       (  0.062)       0.054        0.006
266  22.17     0.10      0.060       (  0.061)       0.054        0.006
267  22.25     0.10      0.060       (  0.061)       0.054        0.006
268  22.33     0.07      0.040       (  0.061)       0.036        0.004
269  22.42     0.07      0.040       (  0.061)       0.036        0.004
270  22.50     0.07      0.040       (  0.061)       0.036        0.004
271  22.58     0.07      0.040       (  0.060)       0.036        0.004
272  22.67     0.07      0.040       (  0.060)       0.036        0.004
273  22.75     0.07      0.040       (  0.060)       0.036        0.004
274  22.83     0.07      0.040       (  0.060)       0.036        0.004
275  22.92     0.07      0.040       (  0.060)       0.036        0.004
276  23.00     0.07      0.040       (  0.060)       0.036        0.004
277  23.08     0.07      0.040       (  0.060)       0.036        0.004
278  23.17     0.07      0.040       (  0.059)       0.036        0.004
279  23.25     0.07      0.040       (  0.059)       0.036        0.004
280  23.33     0.07      0.040       (  0.059)       0.036        0.004
281  23.42     0.07      0.040       (  0.059)       0.036        0.004
282  23.50     0.07      0.040       (  0.059)       0.036        0.004
283  23.58     0.07      0.040       (  0.059)       0.036        0.004
284  23.67     0.07      0.040       (  0.059)       0.036        0.004
285  23.75     0.07      0.040       (  0.059)       0.036        0.004
286  23.83     0.07      0.040       (  0.059)       0.036        0.004
287  23.92     0.07      0.040       (  0.059)       0.036        0.004
288  24.00     0.07      0.040       (  0.059)       0.036        0.004
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    34.3
      Flood volume = Effective rainfall      2.86(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       1.9(Ac.Ft)
      Total soil loss =      2.14(In)
      Total soil loss =     1.391(Ac.Ft)
      Total rainfall =      5.00(In)
      Flood volume =       80813.1 Cubic Feet
      Total soil loss =       60573.3 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      4.550(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0001      0.01  Q          |         |         |         |
   0+10       0.0002      0.02  Q          |         |         |         |
   0+15       0.0004      0.03  Q          |         |         |         |
   0+20       0.0007      0.03  Q          |         |         |         |
   0+25       0.0010      0.04  Q          |         |         |         |
   0+30       0.0013      0.05  Q          |         |         |         |
   0+35       0.0016      0.05  Q          |         |         |         |
   0+40       0.0019      0.05  Q          |         |         |         |
   0+45       0.0023      0.05  Q          |         |         |         |
   0+50       0.0026      0.05  Q          |         |         |         |
   0+55       0.0030      0.06  Q          |         |         |         |
   1+ 0       0.0034      0.06  Q          |         |         |         |
   1+ 5       0.0038      0.06  Q          |         |         |         |
   1+10       0.0042      0.05  Q          |         |         |         |
   1+15       0.0045      0.05  Q          |         |         |         |
   1+20       0.0048      0.05  Q          |         |         |         |
   1+25       0.0052      0.05  Q          |         |         |         |
   1+30       0.0055      0.05  Q          |         |         |         |
   1+35       0.0058      0.05  Q          |         |         |         |
```

1+40	0.0061	0.05	Q				
1+45	0.0065	0.05	Q				
1+50	0.0068	0.05	Q				
1+55	0.0072	0.06	Q				
2+ 0	0.0077	0.06	Q				
2+ 5	0.0081	0.06	Q				
2+10	0.0085	0.06	Q				
2+15	0.0090	0.06	Q				
2+20	0.0094	0.06	Q				
2+25	0.0098	0.06	Q				
2+30	0.0103	0.06	Q				
2+35	0.0107	0.07	Q				
2+40	0.0112	0.08	Q				
2+45	0.0118	0.08	Q				
2+50	0.0123	0.08	Q				
2+55	0.0128	0.08	Q				
3+ 0	0.0134	0.08	Q				
3+ 5	0.0139	0.08	Q				
3+10	0.0145	0.08	Q				
3+15	0.0150	0.08	Q				
3+20	0.0155	0.08	Q				
3+25	0.0161	0.08	Q				
3+30	0.0166	0.08	Q				
3+35	0.0172	0.08	Q				
3+40	0.0177	0.08	Q				
3+45	0.0183	0.08	Q				
3+50	0.0188	0.08	Q				
3+55	0.0195	0.09	Q				
4+ 0	0.0201	0.09	Q				
4+ 5	0.0207	0.09	Q				
4+10	0.0214	0.09	Q				
4+15	0.0220	0.09	Q				
4+20	0.0227	0.10	Q				
4+25	0.0235	0.11	Q				
4+30	0.0242	0.11	Q				
4+35	0.0250	0.11	Q				
4+40	0.0257	0.11	Q				
4+45	0.0265	0.11	Q				
4+50	0.0273	0.11	Q				
4+55	0.0281	0.12	Q				
5+ 0	0.0290	0.12	Q				
5+ 5	0.0297	0.12	Q				
5+10	0.0304	0.10	Q				
5+15	0.0311	0.10	Q				
5+20	0.0318	0.10	Q				
5+25	0.0325	0.11	Q				
5+30	0.0333	0.11	Q				
5+35	0.0341	0.11	Q				
5+40	0.0349	0.12	Q				
5+45	0.0358	0.12	Q				
5+50	0.0366	0.12	Q				
5+55	0.0375	0.13	Q				
6+ 0	0.0384	0.13	Q				
6+ 5	0.0394	0.15	Q				
6+10	0.0407	0.19	Q				
6+15	0.0421	0.20	Q				
6+20	0.0436	0.21	Q				
6+25	0.0451	0.22	Q				
6+30	0.0467	0.23	QV				
6+35	0.0486	0.28	|Q				
6+40	0.0511	0.36	|Q				
6+45	0.0538	0.39	|Q				
6+50	0.0565	0.40	|Q				
6+55	0.0593	0.41	|Q				
7+ 0	0.0622	0.42	|Q				
7+ 5	0.0651	0.42	|Q				
7+10	0.0680	0.43	|Q				
7+15	0.0710	0.43	|Q				
7+20	0.0743	0.49	|Q				
7+25	0.0782	0.57	|VQ				
7+30	0.0823	0.59	|VQ				
7+35	0.0868	0.65	|VQ				
7+40	0.0918	0.74	|VQ				
7+45	0.0971	0.76	| VQ				
7+50	0.1028	0.82	| VQ				
7+55	0.1090	0.91	| VQ				
8+ 0	0.1155	0.93	| VQ				
8+ 5	0.1227	1.05	| V Q				
8+10	0.1309	1.20	| V Q				
8+15	0.1395	1.25	| VQ				
8+20	0.1483	1.27	| V Q				
8+25	0.1571	1.28	| V Q				
8+30	0.1660	1.29	| V Q				
8+35	0.1753	1.35	| V Q				
8+40	0.1851	1.43	| V Q				
8+45	0.1951	1.45	| VQ				



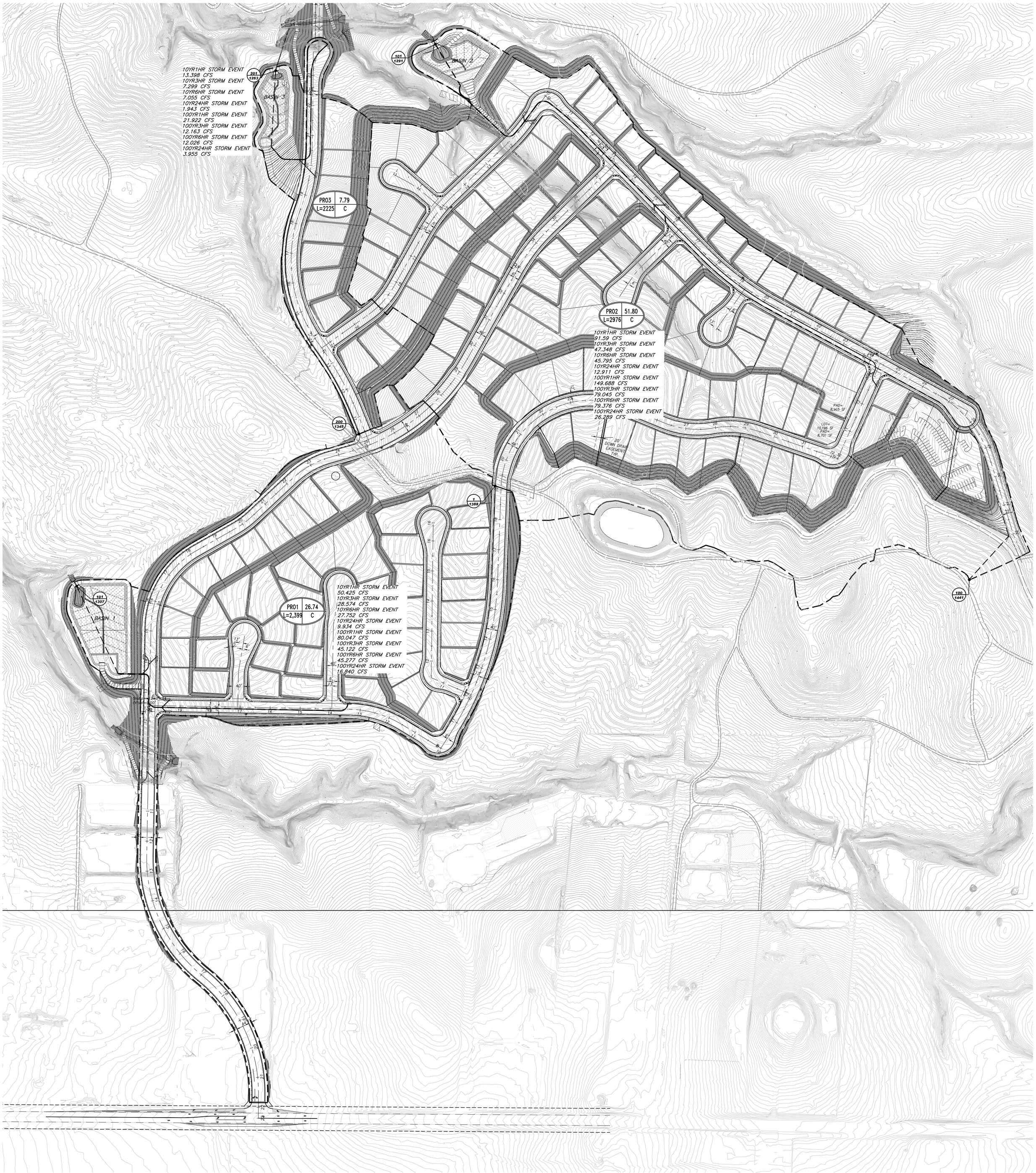
8+50	0.2055	1.51	
8+55	0.2165	1.60	
9+ 0	0.2277	1.62	
9+ 5	0.2397	1.73	
9+10	0.2527	1.89	
9+15	0.2660	1.94	
9+20	0.2798	2.01	
9+25	0.2943	2.09	
9+30	0.3089	2.12	
9+35	0.3239	2.18	
9+40	0.3395	2.27	
9+45	0.3553	2.29	
9+50	0.3716	2.36	
9+55	0.3884	2.44	
10+ 0	0.4054	2.47	
10+ 5	0.4201	2.14	
10+10	0.4312	1.62	
10+15	0.4416	1.50	
10+20	0.4515	1.45	
10+25	0.4613	1.42	
10+30	0.4710	1.41	
10+35	0.4825	1.66	
10+40	0.4965	2.04	
10+45	0.5112	2.13	
10+50	0.5262	2.18	
10+55	0.5414	2.20	
11+ 0	0.5567	2.22	
11+ 5	0.5717	2.18	
11+10	0.5862	2.11	
11+15	0.6006	2.09	
11+20	0.6150	2.09	
11+25	0.6294	2.09	
11+30	0.6438	2.09	
11+35	0.6575	2.00	
11+40	0.6703	1.85	
11+45	0.6829	1.82	
11+50	0.6956	1.86	
11+55	0.7089	1.93	
12+ 0	0.7223	1.95	
12+ 5	0.7382	2.30	
12+10	0.7577	2.83	
12+15	0.7781	2.97	
12+20	0.7993	3.08	
12+25	0.8213	3.19	
12+30	0.8435	3.23	
12+35	0.8665	3.34	
12+40	0.8906	3.50	
12+45	0.9150	3.54	
12+50	0.9398	3.61	
12+55	0.9653	3.70	
13+ 0	0.9909	3.72	
13+ 5	1.0184	3.98	
13+10	1.0484	4.36	
13+15	1.0792	4.46	
13+20	1.1102	4.51	
13+25	1.1414	4.53	
13+30	1.1727	4.55	
13+35	1.2004	4.02	
13+40	1.2224	3.20	
13+45	1.2431	3.00	
13+50	1.2631	2.91	
13+55	1.2829	2.87	
14+ 0	1.3025	2.85	
14+ 5	1.3235	3.05	
14+10	1.3465	3.35	
14+15	1.3701	3.43	
14+20	1.3936	3.41	
14+25	1.4168	3.36	
14+30	1.4399	3.36	
14+35	1.4630	3.35	
14+40	1.4860	3.35	
14+45	1.5091	3.35	
14+50	1.5319	3.31	
14+55	1.5542	3.24	
15+ 0	1.5764	3.22	
15+ 5	1.5982	3.17	
15+10	1.6195	3.09	
15+15	1.6406	3.07	
15+20	1.6614	3.02	
15+25	1.6817	2.95	
15+30	1.7019	2.93	
15+35	1.7207	2.73	
15+40	1.7374	2.43	
15+45	1.7536	2.36	
15+50	1.7697	2.33	
15+55	1.7856	2.31	

16+ 0	1.8015	2.31	| Q|	|	|	| V |
16+ 5	1.8126	1.61	| Q |	|	|	| V|
16+10	1.8163	0.54	| Q |	|	|	| V|
16+15	1.8182	0.28	|Q |	|	|	| V|
16+20	1.8193	0.16	Q |	|	|	| V|
16+25	1.8200	0.10	Q |	|	|	| V|
16+30	1.8204	0.06	Q |	|	|	| V|
16+35	1.8208	0.06	Q |	|	|	| V|
16+40	1.8212	0.05	Q |	|	|	| V|
16+45	1.8215	0.05	Q |	|	|	| V|
16+50	1.8219	0.05	Q |	|	|	| V|
16+55	1.8222	0.05	Q |	|	|	| V|
17+ 0	1.8225	0.05	Q |	|	|	| V|
17+ 5	1.8231	0.08	Q |	|	|	| V|
17+10	1.8240	0.13	Q |	|	|	| V|
17+15	1.8250	0.15	Q |	|	|	| V|
17+20	1.8261	0.16	Q |	|	|	| V|
17+25	1.8272	0.16	Q |	|	|	| V|
17+30	1.8283	0.17	Q |	|	|	| V|
17+35	1.8295	0.17	Q |	|	|	| V|
17+40	1.8307	0.17	Q |	|	|	| V|
17+45	1.8319	0.18	Q |	|	|	| V|
17+50	1.8328	0.14	Q |	|	|	| V|
17+55	1.8334	0.09	Q |	|	|	| V|
18+ 0	1.8340	0.07	Q |	|	|	| V|
18+ 5	1.8344	0.07	Q |	|	|	| V|
18+10	1.8349	0.06	Q |	|	|	| V|
18+15	1.8353	0.06	Q |	|	|	| V|
18+20	1.8357	0.06	Q |	|	|	| V|
18+25	1.8362	0.06	Q |	|	|	| V|
18+30	1.8366	0.06	Q |	|	|	| V|
18+35	1.8370	0.06	Q |	|	|	| V|
18+40	1.8373	0.05	Q |	|	|	| V|
18+45	1.8377	0.05	Q |	|	|	| V|
18+50	1.8380	0.04	Q |	|	|	| V|
18+55	1.8382	0.04	Q |	|	|	| V|
19+ 0	1.8384	0.03	Q |	|	|	| V|
19+ 5	1.8387	0.04	Q |	|	|	| V|
19+10	1.8390	0.04	Q |	|	|	| V|
19+15	1.8393	0.05	Q |	|	|	| V|
19+20	1.8397	0.06	Q |	|	|	| V|
19+25	1.8402	0.07	Q |	|	|	| V|
19+30	1.8407	0.08	Q |	|	|	| V|
19+35	1.8412	0.07	Q |	|	|	| V|
19+40	1.8415	0.05	Q |	|	|	| V|
19+45	1.8419	0.05	Q |	|	|	| V|
19+50	1.8422	0.04	Q |	|	|	| V|
19+55	1.8424	0.04	Q |	|	|	| V|
20+ 0	1.8426	0.03	Q |	|	|	| V|
20+ 5	1.8429	0.04	Q |	|	|	| V|
20+10	1.8432	0.04	Q |	|	|	| V|
20+15	1.8435	0.05	Q |	|	|	| V|
20+20	1.8438	0.05	Q |	|	|	| V|
20+25	1.8442	0.05	Q |	|	|	| V|
20+30	1.8445	0.05	Q |	|	|	| V|
20+35	1.8448	0.05	Q |	|	|	| V|
20+40	1.8451	0.05	Q |	|	|	| V|
20+45	1.8455	0.05	Q |	|	|	| V|
20+50	1.8457	0.04	Q |	|	|	| V|
20+55	1.8460	0.03	Q |	|	|	| V|
21+ 0	1.8462	0.03	Q |	|	|	| V|
21+ 5	1.8465	0.04	Q |	|	|	| V|
21+10	1.8468	0.04	Q |	|	|	| V|
21+15	1.8471	0.05	Q |	|	|	| V|
21+20	1.8474	0.04	Q |	|	|	| V|
21+25	1.8476	0.03	Q |	|	|	| V|
21+30	1.8478	0.03	Q |	|	|	| V|
21+35	1.8481	0.04	Q |	|	|	| V|
21+40	1.8484	0.04	Q |	|	|	| V|
21+45	1.8487	0.05	Q |	|	|	| V|
21+50	1.8490	0.04	Q |	|	|	| V|
21+55	1.8492	0.03	Q |	|	|	| V|
22+ 0	1.8495	0.03	Q |	|	|	| V|
22+ 5	1.8497	0.04	Q |	|	|	| V|
22+10	1.8500	0.04	Q |	|	|	| V|
22+15	1.8503	0.05	Q |	|	|	| V|
22+20	1.8506	0.04	Q |	|	|	| V|
22+25	1.8509	0.03	Q |	|	|	| V|
22+30	1.8511	0.03	Q |	|	|	| V|
22+35	1.8513	0.03	Q |	|	|	| V|
22+40	1.8515	0.03	Q |	|	|	| V|
22+45	1.8517	0.03	Q |	|	|	| V|
22+50	1.8520	0.03	Q |	|	|	| V|
22+55	1.8522	0.03	Q |	|	|	| V|
23+ 0	1.8524	0.03	Q |	|	|	| V|
23+ 5	1.8526	0.03	Q |	|	|	| V|

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   23+10       1.8528      0.03  Q          |          |          |         v|
   23+15       1.8530      0.03  Q          |          |          |         v|
   23+20       1.8533      0.03  Q          |          |          |         v|
   23+25       1.8535      0.03  Q          |          |          |         v|
   23+30       1.8537      0.03  Q          |          |          |         v|
   23+35       1.8539      0.03  Q          |          |          |         v|
   23+40       1.8541      0.03  Q          |          |          |         v|
   23+45       1.8543      0.03  Q          |          |          |         v|
   23+50       1.8546      0.03  Q          |          |          |         v|
   23+55       1.8548      0.03  Q          |          |          |         v|
   24+ 0       1.8550      0.03  Q          |          |          |         v|
   24+ 5       1.8551      0.02  Q          |          |          |         v|
   24+10       1.8552      0.01  Q          |          |          |         v|
   24+15       1.8552      0.00  Q          |          |          |         v|
   24+20       1.8552      0.00  Q          |          |          |         v|
   24+25       1.8552      0.00  Q          |          |          |          v
-------------------------------------------------------------------------------
```

Appendix D – Proposed Synthetic Unit Hydrograph Method

PROPOSED UNIT HYDROGRAPH MAP



0 100 300
50 200 400
SCALE: 1" = 100'

LEGEND

NODE / ELEV

AREA | ACRES
LENGTH | SOIL

WATERSHED BOUNDARY

FLOW PATH

PROPOSED UNIT HYDROGRAPH MAP
PREPARATION DATE: DECEMBER 2022
REVISION DATE: MAY 2024

PLAN PREPARED BY:
adkan ENGINEERS
Civil Engineering • Surveying • Planning
6879 Airport Drive, Riverside, CA 92504
Tel:(951) 688-0241 • Fax:(951) 688-0599

Extended Detention Basin No. 1

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro1212.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	0.50	13.37

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.30	34.76

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.300(In)

Point rain (area averaged) = 0.500(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 0.500(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.500	0.135	1.000	0.135
					Sum (F) =	0.135

Area averaged mean soil loss (F) (In/Hr) = 0.135
Minimum soil loss rate ((In/Hr)) = 0.068
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

Slope of intensity-duration curve for a 1 hour storm =0.5500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
		Sum = 100.000	Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.198	(0.135)	0.099	0.099
2	0.17	4.20	0.252	(0.135)	0.126	0.126
3	0.25	4.40	0.264	(0.135)	0.132	0.132
4	0.33	4.80	0.288	0.135	(0.144)	0.152
5	0.42	5.20	0.312	0.135	(0.156)	0.176
6	0.50	6.20	0.372	0.135	(0.186)	0.236
7	0.58	6.80	0.408	0.135	(0.204)	0.272
8	0.67	8.80	0.528	0.135	(0.264)	0.392
9	0.75	13.90	0.834	0.135	(0.417)	0.698
10	0.83	31.40	1.884	0.135	(0.942)	1.748
11	0.92	7.20	0.432	0.135	(0.216)	0.296
12	1.00	3.80	0.228	(0.135)	0.114	0.114
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	4.4

Flood volume = Effective rainfall 0.37(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 0.8(Ac.Ft)
Total soil loss = 0.13(In)
Total soil loss = 0.289(Ac.Ft)
Total rainfall = 0.50(In)
Flood volume = 35944.2 Cubic Feet
Total soil loss = 12577.1 Cubic Feet

Peak flow rate of this hydrograph = 27.801(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0060	0.86	VQ				
0+10	0.0222	2.36	V Q				
0+15	0.0433	3.06	V Q				
0+20	0.0676	3.53	VQ				
0+25	0.0960	4.13	VQ				
0+30	0.1310	5.08	Q				
0+35	0.1743	6.28	Q				
0+40	0.2295	8.02	QV				
0+45	0.3151	12.43		VQ			
0+50	0.4940	25.97			V	Q	
0+55	0.6854	27.80				V Q	
1+ 0	0.7642	11.44		Q		V	
1+ 5	0.8010	5.34	Q			V	
1+10	0.8164	2.23	Q			V	
1+15	0.8235	1.04	Q			V	
1+20	0.8249	0.19	Q			V	
1+25	0.8252	0.04	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	0.80	21.39

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	2.00	53.48

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 0.800(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 0.800(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.500	0.135	1.000	0.135
					Sum (F) =	0.135

Area averaged mean soil loss (F) (In/Hr) = 0.135
Minimum soil loss rate ((In/Hr)) = 0.068
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
		Sum = 100.000	Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.125	(0.135)	0.062	0.062
2	0.17	1.30	0.125	(0.135)	0.062	0.062
3	0.25	1.10	0.106	(0.135)	0.053	0.053
4	0.33	1.50	0.144	(0.135)	0.072	0.072
5	0.42	1.50	0.144	(0.135)	0.072	0.072
6	0.50	1.80	0.173	(0.135)	0.086	0.086
7	0.58	1.50	0.144	(0.135)	0.072	0.072
8	0.67	1.80	0.173	(0.135)	0.086	0.086
9	0.75	1.80	0.173	(0.135)	0.086	0.086
10	0.83	1.50	0.144	(0.135)	0.072	0.072
11	0.92	1.60	0.154	(0.135)	0.077	0.077
12	1.00	1.80	0.173	(0.135)	0.086	0.086
13	1.08	2.20	0.211	(0.135)	0.106	0.106
14	1.17	2.20	0.211	(0.135)	0.106	0.106
15	1.25	2.20	0.211	(0.135)	0.106	0.106
16	1.33	2.00	0.192	(0.135)	0.096	0.096
17	1.42	2.60	0.250	(0.135)	0.125	0.125
18	1.50	2.70	0.259	(0.135)	0.130	0.130
19	1.58	2.40	0.230	(0.135)	0.115	0.115
20	1.67	2.70	0.259	(0.135)	0.130	0.130
21	1.75	3.30	0.317	0.135	(0.158)	0.181
22	1.83	3.10	0.298	0.135	(0.149)	0.162
23	1.92	2.90	0.278	0.135	(0.139)	0.143
24	2.00	3.00	0.288	0.135	(0.144)	0.152
25	2.08	3.10	0.298	0.135	(0.149)	0.162
26	2.17	4.20	0.403	0.135	(0.202)	0.268
27	2.25	5.00	0.480	0.135	(0.240)	0.344
28	2.33	3.50	0.336	0.135	(0.168)	0.200
29	2.42	6.80	0.653	0.135	(0.326)	0.517
30	2.50	7.30	0.701	0.135	(0.350)	0.565
31	2.58	8.20	0.787	0.135	(0.394)	0.652
32	2.67	5.90	0.566	0.135	(0.283)	0.431
33	2.75	2.00	0.192	(0.135)	0.096	0.096
34	2.83	1.80	0.173	(0.135)	0.086	0.086
35	2.92	1.80	0.173	(0.135)	0.086	0.086
36	3.00	0.60	0.058	(0.135)	0.029	0.029
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.9

Flood volume = Effective rainfall 0.49(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 1.1(Ac.Ft)
Total soil loss = 0.31(In)
Total soil loss = 0.691(Ac.Ft)
Total rainfall = 0.80(In)
Flood volume = 47526.4 Cubic Feet
Total soil loss = 30117.5 Cubic Feet

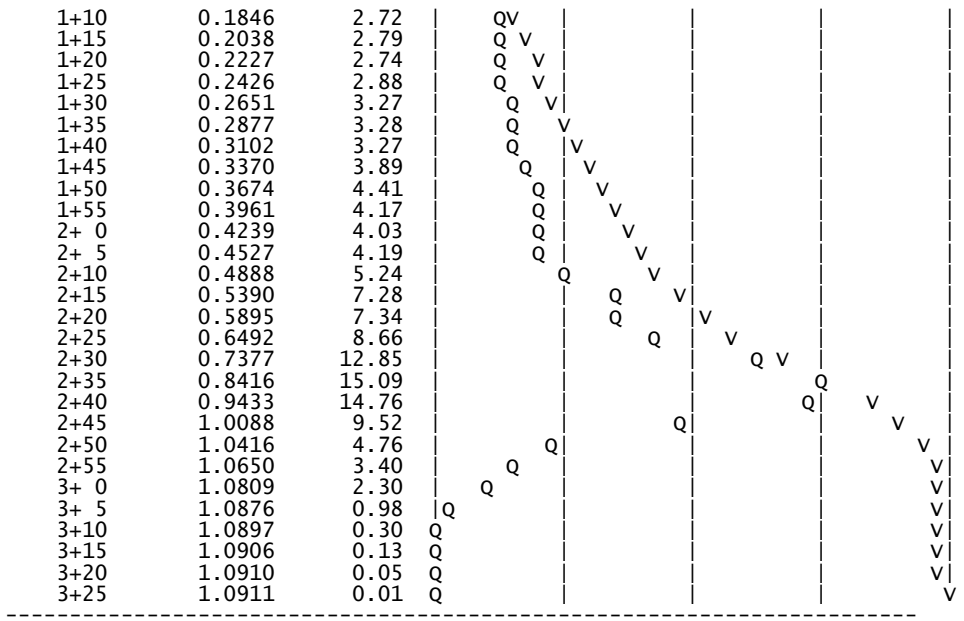
Peak flow rate of this hydrograph = 15.090(CFS)

++

3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0038	0.55	VQ				
0+10	0.0130	1.34	V Q				
0+15	0.0229	1.45	V Q				
0+20	0.0338	1.58	V Q				
0+25	0.0464	1.83	V Q				
0+30	0.0604	2.03	V Q				
0+35	0.0749	2.11	V Q				
0+40	0.0894	2.10	VQ				
0+45	0.1051	2.27	VQ				
0+50	0.1201	2.18	Q				
0+55	0.1342	2.05	Q				
1+ 0	0.1491	2.16	QV				
1+ 5	0.1659	2.45	Q V				



1+10	0.1846	2.72	
1+15	0.2038	2.79	
1+20	0.2227	2.74	
1+25	0.2426	2.88	
1+30	0.2651	3.27	
1+35	0.2877	3.28	
1+40	0.3102	3.27	
1+45	0.3370	3.89	
1+50	0.3674	4.41	
1+55	0.3961	4.17	
2+ 0	0.4239	4.03	
2+ 5	0.4527	4.19	
2+10	0.4888	5.24	
2+15	0.5390	7.28	
2+20	0.5895	7.34	
2+25	0.6492	8.66	
2+30	0.7377	12.85	
2+35	0.8416	15.09	
2+40	0.9433	14.76	
2+45	1.0088	9.52	
2+50	1.0416	4.76	
2+55	1.0650	3.40	
3+ 0	1.0809	2.30	
3+ 5	1.0876	0.98	
3+10	1.0897	0.30	
3+15	1.0906	0.13	
3+20	1.0910	0.05	
3+25	1.0911	0.01	

U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.10	29.41

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	3.00	80.22

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.100(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.100(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.500	0.135	1.000	0.135
					Sum (F) =	0.135

Area averaged mean soil loss (F) (In/Hr) = 0.135
Minimum soil loss rate ((In/Hr)) = 0.068
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

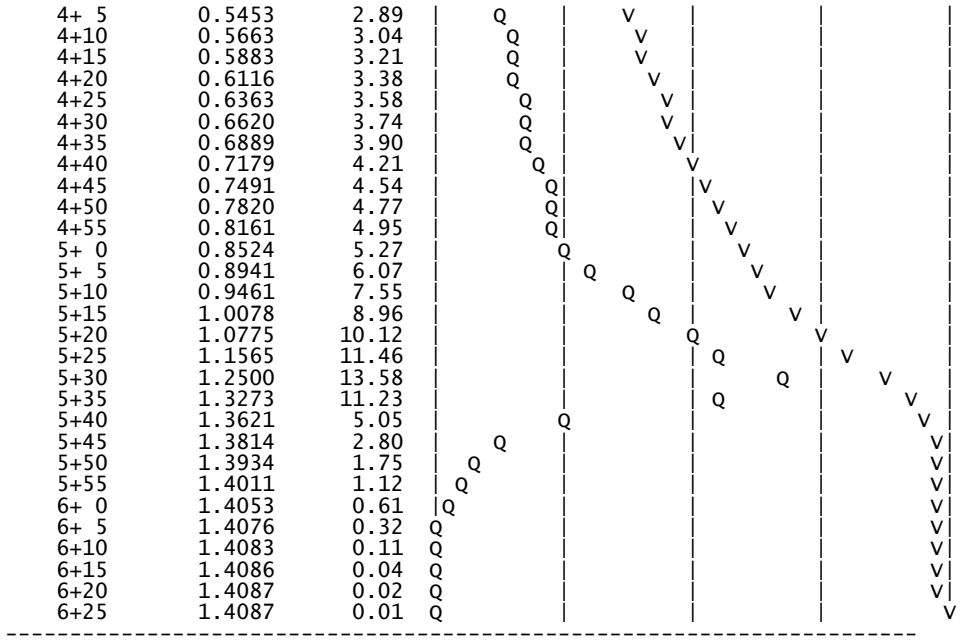
Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.066	(0.135)	0.033	0.033
2	0.17	0.60	0.079	(0.135)	0.040	0.040
3	0.25	0.60	0.079	(0.135)	0.040	0.040
4	0.33	0.60	0.079	(0.135)	0.040	0.040
5	0.42	0.60	0.079	(0.135)	0.040	0.040
6	0.50	0.70	0.092	(0.135)	0.046	0.046
7	0.58	0.70	0.092	(0.135)	0.046	0.046
8	0.67	0.70	0.092	(0.135)	0.046	0.046
9	0.75	0.70	0.092	(0.135)	0.046	0.046
10	0.83	0.70	0.092	(0.135)	0.046	0.046
11	0.92	0.70	0.092	(0.135)	0.046	0.046
12	1.00	0.80	0.106	(0.135)	0.053	0.053
13	1.08	0.80	0.106	(0.135)	0.053	0.053
14	1.17	0.80	0.106	(0.135)	0.053	0.053
15	1.25	0.80	0.106	(0.135)	0.053	0.053
16	1.33	0.80	0.106	(0.135)	0.053	0.053
17	1.42	0.80	0.106	(0.135)	0.053	0.053
18	1.50	0.80	0.106	(0.135)	0.053	0.053
19	1.58	0.80	0.106	(0.135)	0.053	0.053
20	1.67	0.80	0.106	(0.135)	0.053	0.053
21	1.75	0.80	0.106	(0.135)	0.053	0.053
22	1.83	0.80	0.106	(0.135)	0.053	0.053
23	1.92	0.80	0.106	(0.135)	0.053	0.053
24	2.00	0.90	0.119	(0.135)	0.059	0.059
25	2.08	0.80	0.106	(0.135)	0.053	0.053
26	2.17	0.90	0.119	(0.135)	0.059	0.059
27	2.25	0.90	0.119	(0.135)	0.059	0.059
28	2.33	0.90	0.119	(0.135)	0.059	0.059
29	2.42	0.90	0.119	(0.135)	0.059	0.059
30	2.50	0.90	0.119	(0.135)	0.059	0.059
31	2.58	0.90	0.119	(0.135)	0.059	0.059
32	2.67	0.90	0.119	(0.135)	0.059	0.059
33	2.75	1.00	0.132	(0.135)	0.066	0.066
34	2.83	1.00	0.132	(0.135)	0.066	0.066
35	2.92	1.00	0.132	(0.135)	0.066	0.066
36	3.00	1.00	0.132	(0.135)	0.066	0.066
37	3.08	1.00	0.132	(0.135)	0.066	0.066
38	3.17	1.10	0.145	(0.135)	0.073	0.073
39	3.25	1.10	0.145	(0.135)	0.073	0.073
40	3.33	1.10	0.145	(0.135)	0.073	0.073
41	3.42	1.20	0.158	(0.135)	0.079	0.079
42	3.50	1.30	0.172	(0.135)	0.086	0.086
43	3.58	1.40	0.185	(0.135)	0.092	0.092
44	3.67	1.40	0.185	(0.135)	0.092	0.092
45	3.75	1.50	0.198	(0.135)	0.099	0.099
46	3.83	1.50	0.198	(0.135)	0.099	0.099
47	3.92	1.60	0.211	(0.135)	0.106	0.106
48	4.00	1.60	0.211	(0.135)	0.106	0.106
49	4.08	1.70	0.224	(0.135)	0.112	0.112
50	4.17	1.80	0.238	(0.135)	0.119	0.119
51	4.25	1.90	0.251	(0.135)	0.125	0.125
52	4.33	2.00	0.264	(0.135)	0.132	0.132
53	4.42	2.10	0.277	0.135	(0.139)	0.142
54	4.50	2.10	0.277	0.135	(0.139)	0.142
55	4.58	2.20	0.290	0.135	(0.145)	0.155
56	4.67	2.30	0.304	0.135	(0.152)	0.168
57	4.75	2.40	0.317	0.135	(0.158)	0.181
58	4.83	2.40	0.317	0.135	(0.158)	0.181
59	4.92	2.50	0.330	0.135	(0.165)	0.194
60	5.00	2.60	0.343	0.135	(0.172)	0.208

```
61   5.08     3.10      0.409          0.135    (  0.205)        0.274
62   5.17     3.60      0.475          0.135    (  0.238)        0.340
63   5.25     3.90      0.515          0.135    (  0.257)        0.379
64   5.33     4.20      0.554          0.135    (  0.277)        0.419
65   5.42     4.70      0.620          0.135    (  0.310)        0.485
66   5.50     5.60      0.739          0.135    (  0.370)        0.604
67   5.58     1.90      0.251       (  0.135)       0.125        0.125
68   5.67     0.90      0.119       (  0.135)       0.059        0.059
69   5.75     0.60      0.079       (  0.135)       0.040        0.040
70   5.83     0.50      0.066       (  0.135)       0.033        0.033
71   5.92     0.30      0.040       (  0.135)       0.020        0.020
72   6.00     0.20      0.026       (  0.135)       0.013        0.013
              (Loss Rate Not Used)
   Sum =     100.0                                   Sum =     7.6
      Flood volume = Effective rainfall      0.63(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       1.4(Ac.Ft)
      Total soil loss =      0.47(In)
      Total soil loss =     1.042(Ac.Ft)
      Total rainfall =      1.10(In)
      Flood volume =       61364.9 Cubic Feet
      Total soil loss =       45398.1 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     13.584(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f     H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
-------------------------------------------------------------------------
  0+ 5       0.0020      0.29  Q         |         |         |         |
  0+10       0.0073      0.77  VQ        |         |         |         |
  0+15       0.0138      0.95  VQ        |         |         |         |
  0+20       0.0208      1.02  V Q       |         |         |         |
  0+25       0.0280      1.05  V Q       |         |         |         |
  0+30       0.0358      1.12  |VQ       |         |         |         |
  0+35       0.0441      1.21  |VQ       |         |         |         |
  0+40       0.0526      1.23  |VQ       |         |         |         |
  0+45       0.0611      1.24  |VQ       |         |         |         |
  0+50       0.0696      1.24  |VQ       |         |         |         |
  0+55       0.0782      1.25  | Q       |         |         |         |
  1+ 0       0.0872      1.30  | Q       |         |         |         |
  1+ 5       0.0968      1.39  | Q       |         |         |         |
  1+10       0.1064      1.41  | QV      |         |         |         |
  1+15       0.1162      1.42  | QV      |         |         |         |
  1+20       0.1260      1.42  | QV      |         |         |         |
  1+25       0.1358      1.42  | QV      |         |         |         |
  1+30       0.1456      1.42  | Q V     |         |         |         |
  1+35       0.1554      1.42  | Q V     |         |         |         |
  1+40       0.1652      1.42  | Q V     |         |         |         |
  1+45       0.1750      1.42  | Q V     |         |         |         |
  1+50       0.1848      1.42  | Q  V    |         |         |         |
  1+55       0.1946      1.42  | Q  V    |         |         |         |
  2+ 0       0.2048      1.48  | Q  V    |         |         |         |
  2+ 5       0.2152      1.51  |  Q  V   |         |         |         |
  2+10       0.2255      1.50  |  Q  V   |         |         |         |
  2+15       0.2364      1.57  |  Q  V   |         |         |         |
  2+20       0.2473      1.59  |  Q   V  |         |         |         |
  2+25       0.2583      1.60  |  Q   V  |         |         |         |
  2+30       0.2693      1.60  |  Q   V  |         |         |         |
  2+35       0.2804      1.60  |  Q   V  |         |         |         |
  2+40       0.2914      1.60  |  Q    V |         |         |         |
  2+45       0.3028      1.66  |  Q    V |         |         |         |
  2+50       0.3148      1.74  |  Q    V |         |         |         |
  2+55       0.3270      1.76  |  Q     V|         |         |         |
  3+ 0       0.3392      1.77  |  Q     V|         |         |         |
  3+ 5       0.3514      1.78  |  Q     V|         |         |         |
  3+10       0.3641      1.84  |  Q      V         |         |         |
  3+15       0.3773      1.92  |  Q      V         |         |         |
  3+20       0.3907      1.94  |  Q       V        |         |         |
  3+25       0.4045      2.01  |   Q      V        |         |         |
  3+30       0.4193      2.15  |   Q      V        |         |         |
  3+35       0.4353      2.32  |   Q       V       |         |         |
  3+40       0.4521      2.43  |   Q       V       |         |         |
  3+45       0.4694      2.52  |    Q      V       |         |         |
  3+50       0.4875      2.62  |    Q      V       |         |         |
  3+55       0.5061      2.71  |    Q       V      |         |         |
  4+ 0       0.5255      2.80  |    Q       V      |         |         |
```


4+ 5 0.5453 2.89
4+10 0.5663 3.04
4+15 0.5883 3.21
4+20 0.6116 3.38
4+25 0.6363 3.58
4+30 0.6620 3.74
4+35 0.6889 3.90
4+40 0.7179 4.21
4+45 0.7491 4.54
4+50 0.7820 4.77
4+55 0.8161 4.95
5+ 0 0.8524 5.27
5+ 5 0.8941 6.07
5+10 0.9461 7.55
5+15 1.0078 8.96
5+20 1.0775 10.12
5+25 1.1565 11.46
5+30 1.2500 13.58
5+35 1.3273 11.23
5+40 1.3621 5.05
5+45 1.3814 2.80
5+50 1.3934 1.75
5+55 1.4011 1.12
6+ 0 1.4053 0.61
6+ 5 1.4076 0.32
6+10 1.4083 0.11
6+15 1.4086 0.04
6+20 1.4087 0.02
6+25 1.4087 0.01

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro12242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.80	48.13

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	5.00	133.70

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 1.800(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.800(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.500	0.135	1.000	0.135
					Sum (F) =	0.135

Area averaged mean soil loss (F) (In/Hr) = 0.135
Minimum soil loss rate ((In/Hr)) = 0.068
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.014	(0.240)	0.007	0.007
2	0.17	0.07	0.014	(0.239)	0.007	0.007
3	0.25	0.07	0.014	(0.238)	0.007	0.007
4	0.33	0.10	0.022	(0.237)	0.011	0.011
5	0.42	0.10	0.022	(0.236)	0.011	0.011
6	0.50	0.10	0.022	(0.236)	0.011	0.011
7	0.58	0.10	0.022	(0.235)	0.011	0.011
8	0.67	0.10	0.022	(0.234)	0.011	0.011
9	0.75	0.10	0.022	(0.233)	0.011	0.011
10	0.83	0.13	0.029	(0.232)	0.014	0.014
11	0.92	0.13	0.029	(0.231)	0.014	0.014
12	1.00	0.13	0.029	(0.230)	0.014	0.014
13	1.08	0.10	0.022	(0.229)	0.011	0.011
14	1.17	0.10	0.022	(0.228)	0.011	0.011
15	1.25	0.10	0.022	(0.227)	0.011	0.011
16	1.33	0.10	0.022	(0.226)	0.011	0.011
17	1.42	0.10	0.022	(0.226)	0.011	0.011
18	1.50	0.10	0.022	(0.225)	0.011	0.011
19	1.58	0.10	0.022	(0.224)	0.011	0.011
20	1.67	0.10	0.022	(0.223)	0.011	0.011
21	1.75	0.10	0.022	(0.222)	0.011	0.011
22	1.83	0.13	0.029	(0.221)	0.014	0.014
23	1.92	0.13	0.029	(0.220)	0.014	0.014
24	2.00	0.13	0.029	(0.219)	0.014	0.014
25	2.08	0.13	0.029	(0.218)	0.014	0.014
26	2.17	0.13	0.029	(0.218)	0.014	0.014
27	2.25	0.13	0.029	(0.217)	0.014	0.014
28	2.33	0.13	0.029	(0.216)	0.014	0.014
29	2.42	0.13	0.029	(0.215)	0.014	0.014
30	2.50	0.13	0.029	(0.214)	0.014	0.014
31	2.58	0.17	0.036	(0.213)	0.018	0.018
32	2.67	0.17	0.036	(0.212)	0.018	0.018
33	2.75	0.17	0.036	(0.211)	0.018	0.018
34	2.83	0.17	0.036	(0.211)	0.018	0.018
35	2.92	0.17	0.036	(0.210)	0.018	0.018
36	3.00	0.17	0.036	(0.209)	0.018	0.018
37	3.08	0.17	0.036	(0.208)	0.018	0.018
38	3.17	0.17	0.036	(0.207)	0.018	0.018
39	3.25	0.17	0.036	(0.206)	0.018	0.018
40	3.33	0.17	0.036	(0.205)	0.018	0.018
41	3.42	0.17	0.036	(0.204)	0.018	0.018
42	3.50	0.17	0.036	(0.204)	0.018	0.018
43	3.58	0.17	0.036	(0.203)	0.018	0.018
44	3.67	0.17	0.036	(0.202)	0.018	0.018
45	3.75	0.17	0.036	(0.201)	0.018	0.018
46	3.83	0.20	0.043	(0.200)	0.022	0.022
47	3.92	0.20	0.043	(0.199)	0.022	0.022
48	4.00	0.20	0.043	(0.199)	0.022	0.022
49	4.08	0.20	0.043	(0.198)	0.022	0.022
50	4.17	0.20	0.043	(0.197)	0.022	0.022
51	4.25	0.20	0.043	(0.196)	0.022	0.022
52	4.33	0.23	0.050	(0.195)	0.025	0.025
53	4.42	0.23	0.050	(0.194)	0.025	0.025
54	4.50	0.23	0.050	(0.193)	0.025	0.025
55	4.58	0.23	0.050	(0.193)	0.025	0.025
56	4.67	0.23	0.050	(0.192)	0.025	0.025
57	4.75	0.23	0.050	(0.191)	0.025	0.025
58	4.83	0.27	0.058	(0.190)	0.029	0.029
59	4.92	0.27	0.058	(0.189)	0.029	0.029
60	5.00	0.27	0.058	(0.189)	0.029	0.029
61	5.08	0.20	0.043	(0.188)	0.022	0.022
62	5.17	0.20	0.043	(0.187)	0.022	0.022
63	5.25	0.20	0.043	(0.186)	0.022	0.022
64	5.33	0.23	0.050	(0.185)	0.025	0.025
65	5.42	0.23	0.050	(0.184)	0.025	0.025
66	5.50	0.23	0.050	(0.184)	0.025	0.025

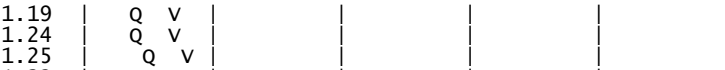
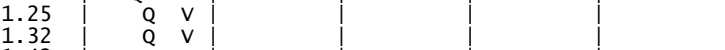
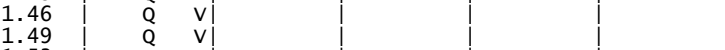
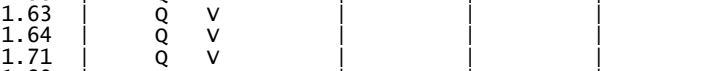
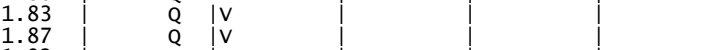
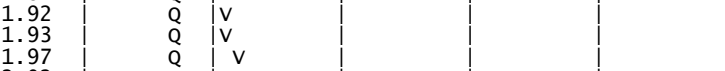
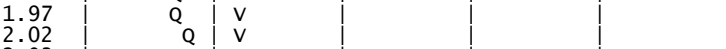
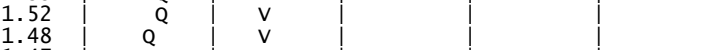
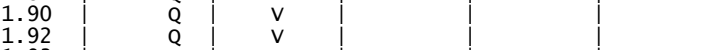
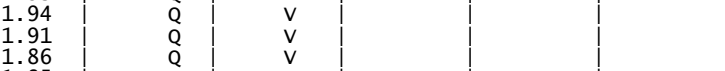
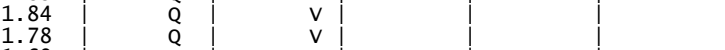
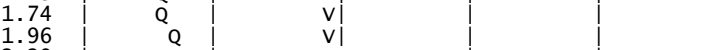
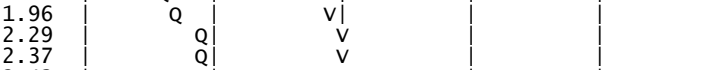
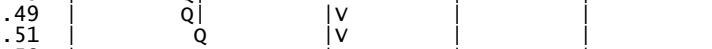
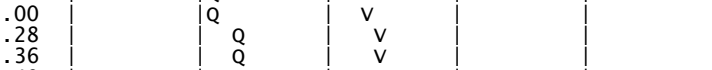
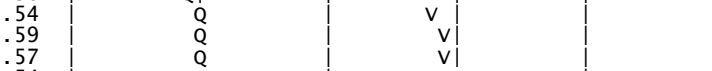
67	5.58	0.27	0.058	(0.183)	0.029	0.029
68	5.67	0.27	0.058	(0.182)	0.029	0.029
69	5.75	0.27	0.058	(0.181)	0.029	0.029
70	5.83	0.27	0.058	(0.180)	0.029	0.029
71	5.92	0.27	0.058	(0.180)	0.029	0.029
72	6.00	0.27	0.058	(0.179)	0.029	0.029
73	6.08	0.30	0.065	(0.178)	0.032	0.032
74	6.17	0.30	0.065	(0.177)	0.032	0.032
75	6.25	0.30	0.065	(0.176)	0.032	0.032
76	6.33	0.30	0.065	(0.176)	0.032	0.032
77	6.42	0.30	0.065	(0.175)	0.032	0.032
78	6.50	0.30	0.065	(0.174)	0.032	0.032
79	6.58	0.33	0.072	(0.173)	0.036	0.036
80	6.67	0.33	0.072	(0.173)	0.036	0.036
81	6.75	0.33	0.072	(0.172)	0.036	0.036
82	6.83	0.33	0.072	(0.171)	0.036	0.036
83	6.92	0.33	0.072	(0.170)	0.036	0.036
84	7.00	0.33	0.072	(0.169)	0.036	0.036
85	7.08	0.33	0.072	(0.169)	0.036	0.036
86	7.17	0.33	0.072	(0.168)	0.036	0.036
87	7.25	0.33	0.072	(0.167)	0.036	0.036
88	7.33	0.37	0.079	(0.166)	0.040	0.040
89	7.42	0.37	0.079	(0.166)	0.040	0.040
90	7.50	0.37	0.079	(0.165)	0.040	0.040
91	7.58	0.40	0.086	(0.164)	0.043	0.043
92	7.67	0.40	0.086	(0.163)	0.043	0.043
93	7.75	0.40	0.086	(0.163)	0.043	0.043
94	7.83	0.43	0.094	(0.162)	0.047	0.047
95	7.92	0.43	0.094	(0.161)	0.047	0.047
96	8.00	0.43	0.094	(0.160)	0.047	0.047
97	8.08	0.50	0.108	(0.160)	0.054	0.054
98	8.17	0.50	0.108	(0.159)	0.054	0.054
99	8.25	0.50	0.108	(0.158)	0.054	0.054
100	8.33	0.50	0.108	(0.157)	0.054	0.054
101	8.42	0.50	0.108	(0.157)	0.054	0.054
102	8.50	0.50	0.108	(0.156)	0.054	0.054
103	8.58	0.53	0.115	(0.155)	0.058	0.058
104	8.67	0.53	0.115	(0.154)	0.058	0.058
105	8.75	0.53	0.115	(0.154)	0.058	0.058
106	8.83	0.57	0.122	(0.153)	0.061	0.061
107	8.92	0.57	0.122	(0.152)	0.061	0.061
108	9.00	0.57	0.122	(0.152)	0.061	0.061
109	9.08	0.63	0.137	(0.151)	0.068	0.068
110	9.17	0.63	0.137	(0.150)	0.068	0.068
111	9.25	0.63	0.137	(0.149)	0.068	0.068
112	9.33	0.67	0.144	(0.149)	0.072	0.072
113	9.42	0.67	0.144	(0.148)	0.072	0.072
114	9.50	0.67	0.144	(0.147)	0.072	0.072
115	9.58	0.70	0.151	(0.147)	0.076	0.076
116	9.67	0.70	0.151	(0.146)	0.076	0.076
117	9.75	0.70	0.151	(0.145)	0.076	0.076
118	9.83	0.73	0.158	(0.144)	0.079	0.079
119	9.92	0.73	0.158	(0.144)	0.079	0.079
120	10.00	0.73	0.158	(0.143)	0.079	0.079
121	10.08	0.50	0.108	(0.142)	0.054	0.054
122	10.17	0.50	0.108	(0.142)	0.054	0.054
123	10.25	0.50	0.108	(0.141)	0.054	0.054
124	10.33	0.50	0.108	(0.140)	0.054	0.054
125	10.42	0.50	0.108	(0.140)	0.054	0.054
126	10.50	0.50	0.108	(0.139)	0.054	0.054
127	10.58	0.67	0.144	(0.138)	0.072	0.072
128	10.67	0.67	0.144	(0.138)	0.072	0.072
129	10.75	0.67	0.144	(0.137)	0.072	0.072
130	10.83	0.67	0.144	(0.136)	0.072	0.072
131	10.92	0.67	0.144	(0.136)	0.072	0.072
132	11.00	0.67	0.144	(0.135)	0.072	0.072
133	11.08	0.63	0.137	(0.134)	0.068	0.068
134	11.17	0.63	0.137	(0.134)	0.068	0.068
135	11.25	0.63	0.137	(0.133)	0.068	0.068
136	11.33	0.63	0.137	(0.132)	0.068	0.068
137	11.42	0.63	0.137	(0.132)	0.068	0.068
138	11.50	0.63	0.137	(0.131)	0.068	0.068
139	11.58	0.57	0.122	(0.130)	0.061	0.061
140	11.67	0.57	0.122	(0.130)	0.061	0.061
141	11.75	0.57	0.122	(0.129)	0.061	0.061
142	11.83	0.60	0.130	(0.128)	0.065	0.065
143	11.92	0.60	0.130	(0.128)	0.065	0.065
144	12.00	0.60	0.130	(0.127)	0.065	0.065
145	12.08	0.83	0.180	(0.126)	0.090	0.090
146	12.17	0.83	0.180	(0.126)	0.090	0.090
147	12.25	0.83	0.180	(0.125)	0.090	0.090
148	12.33	0.87	0.187	(0.125)	0.094	0.094
149	12.42	0.87	0.187	(0.124)	0.094	0.094
150	12.50	0.87	0.187	(0.123)	0.094	0.094

151	12.58	0.93	0.202	(0.123)	0.101	0.101
152	12.67	0.93	0.202	(0.122)	0.101	0.101
153	12.75	0.93	0.202	(0.121)	0.101	0.101
154	12.83	0.97	0.209	(0.121)	0.104	0.104
155	12.92	0.97	0.209	(0.120)	0.104	0.104
156	13.00	0.97	0.209	(0.120)	0.104	0.104
157	13.08	1.13	0.245	0.119	(0.122)	0.126
158	13.17	1.13	0.245	0.118	(0.122)	0.126
159	13.25	1.13	0.245	0.118	(0.122)	0.127
160	13.33	1.13	0.245	0.117	(0.122)	0.128
161	13.42	1.13	0.245	0.117	(0.122)	0.128
162	13.50	1.13	0.245	0.116	(0.122)	0.129
163	13.58	0.77	0.166	(0.115)	0.083	0.083
164	13.67	0.77	0.166	(0.115)	0.083	0.083
165	13.75	0.77	0.166	(0.114)	0.083	0.083
166	13.83	0.77	0.166	(0.114)	0.083	0.083
167	13.92	0.77	0.166	(0.113)	0.083	0.083
168	14.00	0.77	0.166	(0.113)	0.083	0.083
169	14.08	0.90	0.194	(0.112)	0.097	0.097
170	14.17	0.90	0.194	(0.111)	0.097	0.097
171	14.25	0.90	0.194	(0.111)	0.097	0.097
172	14.33	0.87	0.187	(0.110)	0.094	0.094
173	14.42	0.87	0.187	(0.110)	0.094	0.094
174	14.50	0.87	0.187	(0.109)	0.094	0.094
175	14.58	0.87	0.187	(0.109)	0.094	0.094
176	14.67	0.87	0.187	(0.108)	0.094	0.094
177	14.75	0.87	0.187	(0.107)	0.094	0.094
178	14.83	0.83	0.180	(0.107)	0.090	0.090
179	14.92	0.83	0.180	(0.106)	0.090	0.090
180	15.00	0.83	0.180	(0.106)	0.090	0.090
181	15.08	0.80	0.173	(0.105)	0.086	0.086
182	15.17	0.80	0.173	(0.105)	0.086	0.086
183	15.25	0.80	0.173	(0.104)	0.086	0.086
184	15.33	0.77	0.166	(0.104)	0.083	0.083
185	15.42	0.77	0.166	(0.103)	0.083	0.083
186	15.50	0.77	0.166	(0.103)	0.083	0.083
187	15.58	0.63	0.137	(0.102)	0.068	0.068
188	15.67	0.63	0.137	(0.102)	0.068	0.068
189	15.75	0.63	0.137	(0.101)	0.068	0.068
190	15.83	0.63	0.137	(0.101)	0.068	0.068
191	15.92	0.63	0.137	(0.100)	0.068	0.068
192	16.00	0.63	0.137	(0.100)	0.068	0.068
193	16.08	0.13	0.029	(0.099)	0.014	0.014
194	16.17	0.13	0.029	(0.098)	0.014	0.014
195	16.25	0.13	0.029	(0.098)	0.014	0.014
196	16.33	0.13	0.029	(0.097)	0.014	0.014
197	16.42	0.13	0.029	(0.097)	0.014	0.014
198	16.50	0.13	0.029	(0.096)	0.014	0.014
199	16.58	0.10	0.022	(0.096)	0.011	0.011
200	16.67	0.10	0.022	(0.096)	0.011	0.011
201	16.75	0.10	0.022	(0.095)	0.011	0.011
202	16.83	0.10	0.022	(0.095)	0.011	0.011
203	16.92	0.10	0.022	(0.094)	0.011	0.011
204	17.00	0.10	0.022	(0.094)	0.011	0.011
205	17.08	0.17	0.036	(0.093)	0.018	0.018
206	17.17	0.17	0.036	(0.093)	0.018	0.018
207	17.25	0.17	0.036	(0.092)	0.018	0.018
208	17.33	0.17	0.036	(0.092)	0.018	0.018
209	17.42	0.17	0.036	(0.091)	0.018	0.018
210	17.50	0.17	0.036	(0.091)	0.018	0.018
211	17.58	0.17	0.036	(0.090)	0.018	0.018
212	17.67	0.17	0.036	(0.090)	0.018	0.018
213	17.75	0.17	0.036	(0.089)	0.018	0.018
214	17.83	0.13	0.029	(0.089)	0.014	0.014
215	17.92	0.13	0.029	(0.089)	0.014	0.014
216	18.00	0.13	0.029	(0.088)	0.014	0.014
217	18.08	0.13	0.029	(0.088)	0.014	0.014
218	18.17	0.13	0.029	(0.087)	0.014	0.014
219	18.25	0.13	0.029	(0.087)	0.014	0.014
220	18.33	0.13	0.029	(0.086)	0.014	0.014
221	18.42	0.13	0.029	(0.086)	0.014	0.014
222	18.50	0.13	0.029	(0.086)	0.014	0.014
223	18.58	0.10	0.022	(0.085)	0.011	0.011
224	18.67	0.10	0.022	(0.085)	0.011	0.011
225	18.75	0.10	0.022	(0.084)	0.011	0.011
226	18.83	0.07	0.014	(0.084)	0.007	0.007
227	18.92	0.07	0.014	(0.084)	0.007	0.007
228	19.00	0.07	0.014	(0.083)	0.007	0.007
229	19.08	0.10	0.022	(0.083)	0.011	0.011
230	19.17	0.10	0.022	(0.082)	0.011	0.011
231	19.25	0.10	0.022	(0.082)	0.011	0.011
232	19.33	0.13	0.029	(0.082)	0.014	0.014
233	19.42	0.13	0.029	(0.081)	0.014	0.014
234	19.50	0.13	0.029	(0.081)	0.014	0.014

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235  19.58     0.10      0.022       (  0.080)       0.011        0.011
236  19.67     0.10      0.022       (  0.080)       0.011        0.011
237  19.75     0.10      0.022       (  0.080)       0.011        0.011
238  19.83     0.07      0.014       (  0.079)       0.007        0.007
239  19.92     0.07      0.014       (  0.079)       0.007        0.007
240  20.00     0.07      0.014       (  0.079)       0.007        0.007
241  20.08     0.10      0.022       (  0.078)       0.011        0.011
242  20.17     0.10      0.022       (  0.078)       0.011        0.011
243  20.25     0.10      0.022       (  0.078)       0.011        0.011
244  20.33     0.10      0.022       (  0.077)       0.011        0.011
245  20.42     0.10      0.022       (  0.077)       0.011        0.011
246  20.50     0.10      0.022       (  0.077)       0.011        0.011
247  20.58     0.10      0.022       (  0.076)       0.011        0.011
248  20.67     0.10      0.022       (  0.076)       0.011        0.011
249  20.75     0.10      0.022       (  0.076)       0.011        0.011
250  20.83     0.07      0.014       (  0.075)       0.007        0.007
251  20.92     0.07      0.014       (  0.075)       0.007        0.007
252  21.00     0.07      0.014       (  0.075)       0.007        0.007
253  21.08     0.10      0.022       (  0.074)       0.011        0.011
254  21.17     0.10      0.022       (  0.074)       0.011        0.011
255  21.25     0.10      0.022       (  0.074)       0.011        0.011
256  21.33     0.07      0.014       (  0.074)       0.007        0.007
257  21.42     0.07      0.014       (  0.073)       0.007        0.007
258  21.50     0.07      0.014       (  0.073)       0.007        0.007
259  21.58     0.10      0.022       (  0.073)       0.011        0.011
260  21.67     0.10      0.022       (  0.073)       0.011        0.011
261  21.75     0.10      0.022       (  0.072)       0.011        0.011
262  21.83     0.07      0.014       (  0.072)       0.007        0.007
263  21.92     0.07      0.014       (  0.072)       0.007        0.007
264  22.00     0.07      0.014       (  0.072)       0.007        0.007
265  22.08     0.10      0.022       (  0.071)       0.011        0.011
266  22.17     0.10      0.022       (  0.071)       0.011        0.011
267  22.25     0.10      0.022       (  0.071)       0.011        0.011
268  22.33     0.07      0.014       (  0.071)       0.007        0.007
269  22.42     0.07      0.014       (  0.070)       0.007        0.007
270  22.50     0.07      0.014       (  0.070)       0.007        0.007
271  22.58     0.07      0.014       (  0.070)       0.007        0.007
272  22.67     0.07      0.014       (  0.070)       0.007        0.007
273  22.75     0.07      0.014       (  0.070)       0.007        0.007
274  22.83     0.07      0.014       (  0.069)       0.007        0.007
275  22.92     0.07      0.014       (  0.069)       0.007        0.007
276  23.00     0.07      0.014       (  0.069)       0.007        0.007
277  23.08     0.07      0.014       (  0.069)       0.007        0.007
278  23.17     0.07      0.014       (  0.069)       0.007        0.007
279  23.25     0.07      0.014       (  0.069)       0.007        0.007
280  23.33     0.07      0.014       (  0.068)       0.007        0.007
281  23.42     0.07      0.014       (  0.068)       0.007        0.007
282  23.50     0.07      0.014       (  0.068)       0.007        0.007
283  23.58     0.07      0.014       (  0.068)       0.007        0.007
284  23.67     0.07      0.014       (  0.068)       0.007        0.007
285  23.75     0.07      0.014       (  0.068)       0.007        0.007
286  23.83     0.07      0.014       (  0.068)       0.007        0.007
287  23.92     0.07      0.014       (  0.068)       0.007        0.007
288  24.00     0.07      0.014       (  0.068)       0.007        0.007
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    10.8
      Flood volume = Effective rainfall      0.90(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       2.0(Ac.Ft)
      Total soil loss =      0.90(In)
      Total soil loss =     2.000(Ac.Ft)
      Total rainfall =      1.80(In)
      Flood volume =       87590.2 Cubic Feet
      Total soil loss =       87119.9 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      3.455(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0004      0.06  Q         |         |         |         |
   0+10       0.0015      0.15  Q         |         |         |         |
   0+15       0.0027      0.18  Q         |         |         |         |
   0+20       0.0042      0.22  Q         |         |         |         |
   0+25       0.0061      0.27  VQ        |         |         |         |
   0+30       0.0080      0.28  VQ        |         |         |         |
   0+35       0.0100      0.29  VQ        |         |         |         |
   0+40       0.0120      0.29  VQ        |         |         |         |
   0+45       0.0140      0.29  VQ        |         |         |         |
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0+50	0.0162	0.32	VQ	|	|	|	|
0+55	0.0187	0.37	VQ	|	|	|	|
1+ 0	0.0214	0.38	VQ	|	|	|	|
1+ 5	0.0238	0.35	VQ	|	|	|	|
1+10	0.0259	0.31	VQ	|	|	|	|
1+15	0.0280	0.30	VQ	|	|	|	|
1+20	0.0300	0.30	VQ	|	|	|	|
1+25	0.0320	0.29	VQ	|	|	|	|
1+30	0.0340	0.29	VQ	|	|	|	|
1+35	0.0360	0.29	VQ	|	|	|	|
1+40	0.0381	0.29	VQ	|	|	|	|
1+45	0.0401	0.29	VQ	|	|	|	|
1+50	0.0423	0.32	VQ	|	|	|	|
1+55	0.0448	0.37	VQ	|	|	|	|
2+ 0	0.0474	0.38	VQ	|	|	|	|
2+ 5	0.0501	0.38	VQ	|	|	|	|
2+10	0.0527	0.39	|Q	|	|	|	|
2+15	0.0554	0.39	|Q	|	|	|	|
2+20	0.0581	0.39	|Q	|	|	|	|
2+25	0.0608	0.39	|Q	|	|	|	|
2+30	0.0634	0.39	|Q	|	|	|	|
2+35	0.0663	0.42	|Q	|	|	|	|
2+40	0.0695	0.47	|Q	|	|	|	|
2+45	0.0728	0.48	|Q	|	|	|	|
2+50	0.0761	0.48	|Q	|	|	|	|
2+55	0.0795	0.48	|Q	|	|	|	|
3+ 0	0.0828	0.49	|Q	|	|	|	|
3+ 5	0.0862	0.49	|Q	|	|	|	|
3+10	0.0895	0.49	|Q	|	|	|	|
3+15	0.0928	0.49	|Q	|	|	|	|
3+20	0.0962	0.49	|Q	|	|	|	|
3+25	0.0995	0.49	|Q	|	|	|	|
3+30	0.1029	0.49	|QV	|	|	|	|
3+35	0.1062	0.49	|QV	|	|	|	|
3+40	0.1095	0.49	|QV	|	|	|	|
3+45	0.1129	0.49	|QV	|	|	|	|
3+50	0.1164	0.52	| Q	|	|	|	|
3+55	0.1203	0.56	| Q	|	|	|	|
4+ 0	0.1243	0.57	| Q	|	|	|	|
4+ 5	0.1283	0.58	| Q	|	|	|	|
4+10	0.1323	0.58	| Q	|	|	|	|
4+15	0.1363	0.58	| Q	|	|	|	|
4+20	0.1405	0.61	| Q	|	|	|	|
4+25	0.1450	0.66	| Q	|	|	|	|
4+30	0.1497	0.67	| Q	|	|	|	|
4+35	0.1543	0.68	| QV	|	|	|	|
4+40	0.1590	0.68	| QV	|	|	|	|
4+45	0.1637	0.68	| QV	|	|	|	|
4+50	0.1686	0.71	| QV	|	|	|	|
4+55	0.1738	0.76	| Q	|	|	|	|
5+ 0	0.1791	0.77	| Q	|	|	|	|
5+ 5	0.1839	0.71	| QV	|	|	|	|
5+10	0.1882	0.62	| QV	|	|	|	|
5+15	0.1923	0.60	| QV	|	|	|	|
5+20	0.1966	0.62	| QV	|	|	|	|
5+25	0.2012	0.66	| Q V	|	|	|	|
5+30	0.2058	0.67	| Q V	|	|	|	|
5+35	0.2107	0.71	| Q V	|	|	|	|
5+40	0.2159	0.76	| QV	|	|	|	|
5+45	0.2212	0.77	| QV	|	|	|	|
5+50	0.2265	0.77	| QV	|	|	|	|
5+55	0.2318	0.78	| QV	|	|	|	|
6+ 0	0.2372	0.78	| QV	|	|	|	|
6+ 5	0.2427	0.81	| QV	|	|	|	|
6+10	0.2486	0.85	| QV	|	|	|	|
6+15	0.2546	0.86	| Q V	|	|	|	|
6+20	0.2606	0.87	| Q V	|	|	|	|
6+25	0.2666	0.87	| Q V	|	|	|	|
6+30	0.2726	0.87	| Q V	|	|	|	|
6+35	0.2788	0.91	| Q V	|	|	|	|
6+40	0.2854	0.95	| Q V	|	|	|	|
6+45	0.2920	0.96	| Q V	|	|	|	|
6+50	0.2987	0.97	| Q V	|	|	|	|
6+55	0.3053	0.97	| Q V	|	|	|	|
7+ 0	0.3120	0.97	| Q V	|	|	|	|
7+ 5	0.3187	0.97	| Q V	|	|	|	|
7+10	0.3254	0.97	| Q V	|	|	|	|
7+15	0.3321	0.97	| Q V	|	|	|	|
7+20	0.3390	1.00	| Q V	|	|	|	|
7+25	0.3462	1.05	| Q V	|	|	|	|
7+30	0.3535	1.06	| Q V	|	|	|	|
7+35	0.3610	1.10	| Q V	|	|	|	|
7+40	0.3689	1.14	| Q V	|	|	|	|
7+45	0.3769	1.16	| Q V	|	|	|	|

7+50	0.3851	1.19	
7+55	0.3936	1.24	
8+ 0	0.4022	1.25	
8+ 5	0.4113	1.32	
8+10	0.4211	1.42	
8+15	0.4310	1.44	
8+20	0.4410	1.45	
8+25	0.4510	1.45	
8+30	0.4610	1.46	
8+35	0.4712	1.49	
8+40	0.4818	1.53	
8+45	0.4924	1.54	
8+50	0.5033	1.58	
8+55	0.5145	1.63	
9+ 0	0.5258	1.64	
9+ 5	0.5376	1.71	
9+10	0.5500	1.80	
9+15	0.5626	1.83	
9+20	0.5755	1.87	
9+25	0.5887	1.92	
9+30	0.6020	1.93	
9+35	0.6156	1.97	
9+40	0.6295	2.02	
9+45	0.6434	2.03	
9+50	0.6577	2.07	
9+55	0.6722	2.11	
10+ 0	0.6869	2.13	
10+ 5	0.7000	1.91	
10+10	0.7110	1.59	
10+15	0.7214	1.52	
10+20	0.7317	1.48	
10+25	0.7418	1.47	
10+30	0.7518	1.46	
10+35	0.7629	1.61	
10+40	0.7756	1.84	
10+45	0.7887	1.90	
10+50	0.8019	1.92	
10+55	0.8152	1.93	
11+ 0	0.8286	1.94	
11+ 5	0.8417	1.91	
11+10	0.8546	1.86	
11+15	0.8673	1.85	
11+20	0.8801	1.85	
11+25	0.8928	1.85	
11+30	0.9055	1.84	
11+35	0.9177	1.78	
11+40	0.9294	1.69	
11+45	0.9409	1.67	
11+50	0.9525	1.69	
11+55	0.9644	1.73	
12+ 0	0.9764	1.74	
12+ 5	0.9899	1.96	
12+10	1.0056	2.29	
12+15	1.0219	2.37	
12+20	1.0387	2.43	
12+25	1.0559	2.49	
12+30	1.0732	2.51	
12+35	1.0910	2.58	
12+40	1.1094	2.68	
12+45	1.1280	2.70	
12+50	1.1469	2.74	
12+55	1.1661	2.79	
13+ 0	1.1854	2.81	
13+ 5	1.2061	3.00	
13+10	1.2286	3.28	
13+15	1.2518	3.36	
13+20	1.2752	3.40	
13+25	1.2988	3.43	
13+30	1.3226	3.45	
13+35	1.3437	3.06	
13+40	1.3608	2.48	
13+45	1.3769	2.34	
13+50	1.3926	2.28	
13+55	1.4081	2.25	
14+ 0	1.4235	2.23	
14+ 5	1.4398	2.36	
14+10	1.4573	2.54	
14+15	1.4751	2.59	
14+20	1.4928	2.57	
14+25	1.5103	2.54	
14+30	1.5277	2.53	
14+35	1.5451	2.53	
14+40	1.5625	2.52	
14+45	1.5799	2.52	

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14+50       1.5971      2.49  |          Q|           |           |V          |
14+55       1.6139      2.45  |          Q|           |           | V         |
15+ 0       1.6307      2.44  |          Q|           |           | V         |
15+ 5       1.6472      2.40  |          Q|           |           | V         |
15+10       1.6634      2.35  |          Q|           |           |  V        |
15+15       1.6795      2.34  |          Q|           |           |  V        |
15+20       1.6953      2.30  |          Q|           |           |  V        |
15+25       1.7109      2.25  |          Q|           |           |   V       |
15+30       1.7263      2.24  |         Q |           |           |   V       |
15+35       1.7408      2.11  |         Q |           |           |   V       |
15+40       1.7541      1.92  |        Q  |           |           |   V       |
15+45       1.7670      1.88  |        Q  |           |           |    V      |
15+50       1.7798      1.86  |        Q  |           |           |    V      |
15+55       1.7926      1.85  |        Q  |           |           |    V      |
16+ 0       1.8053      1.84  |        Q  |           |           |    V      |
16+ 5       1.8147      1.37  |      Q    |           |           |     V     |
16+10       1.8194      0.68  | Q         |           |           |     V     |
16+15       1.8230      0.52  | Q         |           |           |     V     |
16+20       1.8261      0.45  |Q          |           |           |     V     |
16+25       1.8289      0.41  |Q          |           |           |     V     |
16+30       1.8316      0.39  |Q          |           |           |     V     |
16+35       1.8340      0.36  |Q          |           |           |     V     |
16+40       1.8362      0.31  |Q          |           |           |     V     |
16+45       1.8382      0.30  |Q          |           |           |     V     |
16+50       1.8403      0.30  |Q          |           |           |     V     |
16+55       1.8423      0.29  |Q          |           |           |     V     |
17+ 0       1.8443      0.29  |Q          |           |           |     V     |
17+ 5       1.8467      0.35  |Q          |           |           |     V     |
17+10       1.8498      0.45  |Q          |           |           |     V     |
17+15       1.8530      0.47  |Q          |           |           |     V     |
17+20       1.8563      0.48  |Q          |           |           |     V     |
17+25       1.8596      0.48  |Q          |           |           |     V     |
17+30       1.8630      0.49  |Q          |           |           |      V    |
17+35       1.8663      0.49  |Q          |           |           |      V    |
17+40       1.8697      0.49  |Q          |           |           |      V    |
17+45       1.8730      0.49  |Q          |           |           |      V    |
17+50       1.8761      0.45  |Q          |           |           |      V    |
17+55       1.8789      0.41  |Q          |           |           |      V    |
18+ 0       1.8817      0.40  |Q          |           |           |      V    |
18+ 5       1.8844      0.39  |Q          |           |           |      V    |
18+10       1.8871      0.39  |Q          |           |           |      V    |
18+15       1.8897      0.39  |Q          |           |           |      V    |
18+20       1.8924      0.39  |Q          |           |           |      V    |
18+25       1.8951      0.39  |Q          |           |           |      V    |
18+30       1.8978      0.39  |Q          |           |           |      V    |
18+35       1.9002      0.36  |Q          |           |           |      V    |
18+40       1.9024      0.31  |Q          |           |           |      V    |
18+45       1.9044      0.30  |Q          |           |           |      V    |
18+50       1.9062      0.26  |Q          |           |           |      V    |
18+55       1.9077      0.22  Q           |           |           |      V    |
19+ 0       1.9091      0.20  Q           |           |           |      V    |
19+ 5       1.9107      0.23  Q           |           |           |       V   |
19+10       1.9126      0.27  |Q          |           |           |       V   |
19+15       1.9145      0.28  |Q          |           |           |       V   |
19+20       1.9167      0.32  |Q          |           |           |       V   |
19+25       1.9192      0.37  |Q          |           |           |       V   |
19+30       1.9219      0.38  |Q          |           |           |       V   |
19+35       1.9243      0.35  |Q          |           |           |       V   |
19+40       1.9264      0.31  |Q          |           |           |       V   |
19+45       1.9285      0.30  |Q          |           |           |       V   |
19+50       1.9303      0.26  |Q          |           |           |       V   |
19+55       1.9318      0.22  Q           |           |           |       V   |
20+ 0       1.9332      0.20  Q           |           |           |       V   |
20+ 5       1.9348      0.23  Q           |           |           |       V   |
20+10       1.9366      0.27  |Q          |           |           |       V   |
20+15       1.9386      0.28  |Q          |           |           |       V   |
20+20       1.9406      0.29  |Q          |           |           |       V   |
20+25       1.9426      0.29  |Q          |           |           |       V   |
20+30       1.9446      0.29  |Q          |           |           |       V   |
20+35       1.9466      0.29  |Q          |           |           |       V   |
20+40       1.9486      0.29  |Q          |           |           |       V   |
20+45       1.9506      0.29  |Q          |           |           |       V   |
20+50       1.9524      0.26  |Q          |           |           |       V   |
20+55       1.9538      0.21  Q           |           |           |       V   |
21+ 0       1.9552      0.20  Q           |           |           |       V   |
21+ 5       1.9568      0.23  Q           |           |           |       V   |
21+10       1.9587      0.27  |Q          |           |           |       V   |
21+15       1.9606      0.28  |Q          |           |           |        V  |
21+20       1.9624      0.26  |Q          |           |           |        V  |
21+25       1.9639      0.21  Q           |           |           |        V  |
21+30       1.9653      0.20  Q           |           |           |        V  |
21+35       1.9668      0.23  Q           |           |           |        V  |
21+40       1.9687      0.27  |Q          |           |           |        V  |
21+45       1.9707      0.28  |Q          |           |           |        V  |
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   21+50       1.9724      0.26  |Q        |         |         |        v|
   21+55       1.9739      0.21  Q        |         |         |        v|
   22+ 0       1.9753      0.20  Q        |         |         |        v|
   22+ 5       1.9769      0.23  Q        |         |         |        v|
   22+10       1.9788      0.27  |Q        |         |         |        v|
   22+15       1.9807      0.28  |Q        |         |         |        v|
   22+20       1.9825      0.26  |Q        |         |         |        v|
   22+25       1.9839      0.21  Q        |         |         |        v|
   22+30       1.9853      0.20  Q        |         |         |        v|
   22+35       1.9867      0.20  Q        |         |         |        v|
   22+40       1.9880      0.20  Q        |         |         |        v|
   22+45       1.9894      0.19  Q        |         |         |        v|
   22+50       1.9907      0.19  Q        |         |         |        v|
   22+55       1.9920      0.19  Q        |         |         |        v|
   23+ 0       1.9934      0.19  Q        |         |         |        v|
   23+ 5       1.9947      0.19  Q        |         |         |        v|
   23+10       1.9961      0.19  Q        |         |         |        v|
   23+15       1.9974      0.19  Q        |         |         |        v|
   23+20       1.9987      0.19  Q        |         |         |        v|
   23+25       2.0001      0.19  Q        |         |         |        v|
   23+30       2.0014      0.19  Q        |         |         |        v|
   23+35       2.0027      0.19  Q        |         |         |        v|
   23+40       2.0041      0.19  Q        |         |         |        v|
   23+45       2.0054      0.19  Q        |         |         |        v|
   23+50       2.0068      0.19  Q        |         |         |        v|
   23+55       2.0081      0.19  Q        |         |         |        v|
   24+ 0       2.0094      0.19  Q        |         |         |        v|
   24+ 5       2.0103      0.13  Q        |         |         |        v|
   24+10       2.0106      0.04  Q        |         |         |        v|
   24+15       2.0107      0.02  Q        |         |         |        v|
   24+20       2.0108      0.01  Q        |         |         |        v|
   24+25       2.0108      0.00  Q        |         |         |         v
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U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	0.50	13.37

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.30	34.76

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.300(In)

Point rain (area averaged) = 0.687(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 0.687(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.500	0.135	1.000	0.135
					Sum (F) =	0.135

Area averaged mean soil loss (F) (In/Hr) = 0.135
Minimum soil loss rate ((In/Hr)) = 0.068
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

Slope of intensity-duration curve for a 1 hour storm =0.5500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
		Sum = 100.000	Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.272	0.135	(0.136)	0.137
2	0.17	4.20	0.346	0.135	(0.173)	0.211
3	0.25	4.40	0.363	0.135	(0.181)	0.227
4	0.33	4.80	0.396	0.135	(0.198)	0.260
5	0.42	5.20	0.429	0.135	(0.214)	0.293
6	0.50	6.20	0.511	0.135	(0.256)	0.376
7	0.58	6.80	0.561	0.135	(0.280)	0.425
8	0.67	8.80	0.726	0.135	(0.363)	0.590
9	0.75	13.90	1.146	0.135	(0.573)	1.011
10	0.83	31.40	2.589	0.135	(1.295)	2.454
11	0.92	7.20	0.594	0.135	(0.297)	0.458
12	1.00	3.80	0.313	0.135	(0.157)	0.178
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	6.6

Flood volume = Effective rainfall 0.55(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 1.2(Ac.Ft)
Total soil loss = 0.14(In)
Total soil loss = 0.302(Ac.Ft)
Total rainfall = 0.69(In)
Flood volume = 53552.9 Cubic Feet
Total soil loss = 13152.3 Cubic Feet

Peak flow rate of this hydrograph = 39.589(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	10.0	20.0	30.0	40.0
0+ 5	0.0082	1.19	VQ				
0+10	0.0329	3.58	V Q				
0+15	0.0680	5.09	V Q				
0+20	0.1093	6.00	V Q				
0+25	0.1572	6.95	VQ				
0+30	0.2145	8.32	V Q				
0+35	0.2833	9.99	Q				
0+40	0.3686	12.39	VQ				
0+45	0.4957	18.46		V Q			
0+50	0.7511	37.07			V	Q	
0+55	1.0237	39.59				V Q	
1+ 0	1.1397	16.84		Q		V	
1+ 5	1.1941	7.89	Q			V	
1+10	1.2164	3.25	Q			V	
1+15	1.2269	1.51	Q			V	
1+20	1.2289	0.30	Q			V	
1+25	1.2294	0.07	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro1535.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	0.80	21.39

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	2.00	53.48

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 1.081(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.081(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.500	0.135	1.000	0.135
					Sum (F) =	0.135

Area averaged mean soil loss (F) (In/Hr) = 0.135
Minimum soil loss rate ((In/Hr)) = 0.068
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064

4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.169	(0.135)	0.084	0.084
2	0.17	1.30	0.169	(0.135)	0.084	0.084
3	0.25	1.10	0.143	(0.135)	0.071	0.071
4	0.33	1.50	0.195	(0.135)	0.097	0.097
5	0.42	1.50	0.195	(0.135)	0.097	0.097
6	0.50	1.80	0.233	(0.135)	0.117	0.117
7	0.58	1.50	0.195	(0.135)	0.097	0.097
8	0.67	1.80	0.233	(0.135)	0.117	0.117
9	0.75	1.80	0.233	(0.135)	0.117	0.117
10	0.83	1.50	0.195	(0.135)	0.097	0.097
11	0.92	1.60	0.208	(0.135)	0.104	0.104
12	1.00	1.80	0.233	(0.135)	0.117	0.117
13	1.08	2.20	0.285	0.135	(0.143)	0.150
14	1.17	2.20	0.285	0.135	(0.143)	0.150
15	1.25	2.20	0.285	0.135	(0.143)	0.150
16	1.33	2.00	0.259	(0.135)	0.130	0.130
17	1.42	2.60	0.337	0.135	(0.169)	0.202
18	1.50	2.70	0.350	0.135	(0.175)	0.215
19	1.58	2.40	0.311	0.135	(0.156)	0.176
20	1.67	2.70	0.350	0.135	(0.175)	0.215
21	1.75	3.30	0.428	0.135	(0.214)	0.293
22	1.83	3.10	0.402	0.135	(0.201)	0.267
23	1.92	2.90	0.376	0.135	(0.188)	0.241
24	2.00	3.00	0.389	0.135	(0.195)	0.254
25	2.08	3.10	0.402	0.135	(0.201)	0.267
26	2.17	4.20	0.545	0.135	(0.272)	0.409
27	2.25	5.00	0.649	0.135	(0.324)	0.513
28	2.33	3.50	0.454	0.135	(0.227)	0.318
29	2.42	6.80	0.882	0.135	(0.441)	0.747
30	2.50	7.30	0.947	0.135	(0.473)	0.811
31	2.58	8.20	1.064	0.135	(0.532)	0.928
32	2.67	5.90	0.765	0.135	(0.383)	0.630
33	2.75	2.00	0.259	(0.135)	0.130	0.130
34	2.83	1.80	0.233	(0.135)	0.117	0.117
35	2.92	1.80	0.233	(0.135)	0.117	0.117
36	3.00	0.60	0.078	(0.135)	0.039	0.039
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	8.7

Flood volume = Effective rainfall 0.72(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 1.6(Ac.Ft)
Total soil loss = 0.36(In)
Total soil loss = 0.800(Ac.Ft)
Total rainfall = 1.08(In)
Flood volume = 70091.3 Cubic Feet
Total soil loss = 34831.7 Cubic Feet

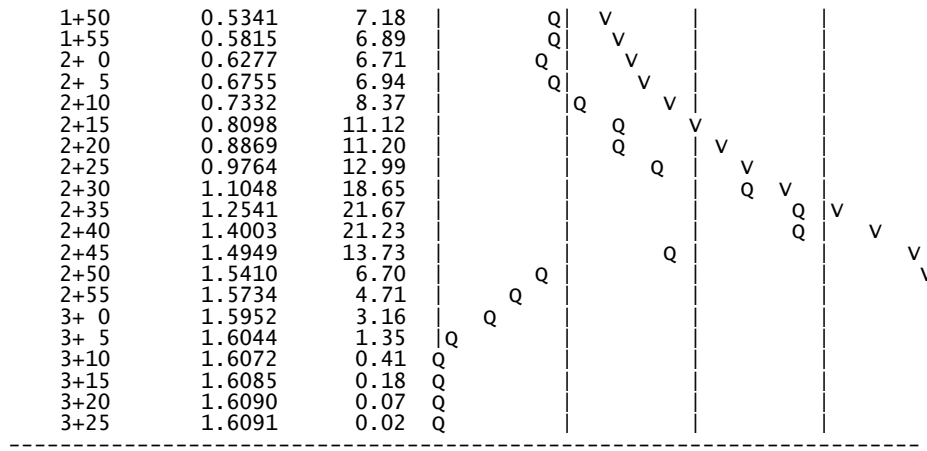
Peak flow rate of this hydrograph = 21.675(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0051	0.74	Q	|	|	|	|
0+10	0.0175	1.81	V Q	|	|	|	|
0+15	0.0310	1.96	V Q	|	|	|	|
0+20	0.0457	2.13	|VQ	|	|	|	|
0+25	0.0628	2.48	|V Q	|	|	|	|
0+30	0.0817	2.74	| VQ	|	|	|	|
0+35	0.1013	2.85	| VQ	|	|	|	|
0+40	0.1209	2.84	| Q	|	|	|	|
0+45	0.1420	3.07	| VQ	|	|	|	|
0+50	0.1622	2.94	| QV	|	|	|	|
0+55	0.1813	2.77	| QV	|	|	|	|
1+ 0	0.2014	2.92	| Q V	|	|	|	|
1+ 5	0.2246	3.37	| QV	|	|	|	|
1+10	0.2510	3.83	| QV	|	|	|	|
1+15	0.2782	3.94	| QV	|	|	|	|
1+20	0.3045	3.82	| Q V	|	|	|	|
1+25	0.3336	4.22	| Q V |	|	|	|	|
1+30	0.3695	5.21	| Q V|	|	|	|	|
1+35	0.4055	5.23	| Q V	|	|	|	|
1+40	0.4412	5.19	| Q V	|	|	|	|
1+45	0.4847	6.31	| Q | V	|	|	|	|


1+50 0.5341 7.18
1+55 0.5815 6.89
2+ 0 0.6277 6.71
2+ 5 0.6755 6.94
2+10 0.7332 8.37
2+15 0.8098 11.12
2+20 0.8869 11.20
2+25 0.9764 12.99
2+30 1.1048 18.65
2+35 1.2541 21.67
2+40 1.4003 21.23
2+45 1.4949 13.73
2+50 1.5410 6.70
2+55 1.5734 4.71
3+ 0 1.5952 3.16
3+ 5 1.6044 1.35
3+10 1.6072 0.41
3+15 1.6085 0.18
3+20 1.6090 0.07
3+25 1.6091 0.02

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro1565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.10	29.41

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	3.00	80.22

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.545(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.545(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.500	0.135	1.000	0.135
					Sum (F) =	0.135

Area averaged mean soil loss (F) (In/Hr) = 0.135
Minimum soil loss rate ((In/Hr)) = 0.068
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.093	(0.135)	0.046	0.046
2	0.17	0.60	0.111	(0.135)	0.056	0.056
3	0.25	0.60	0.111	(0.135)	0.056	0.056
4	0.33	0.60	0.111	(0.135)	0.056	0.056
5	0.42	0.60	0.111	(0.135)	0.056	0.056
6	0.50	0.70	0.130	(0.135)	0.065	0.065
7	0.58	0.70	0.130	(0.135)	0.065	0.065
8	0.67	0.70	0.130	(0.135)	0.065	0.065
9	0.75	0.70	0.130	(0.135)	0.065	0.065
10	0.83	0.70	0.130	(0.135)	0.065	0.065
11	0.92	0.70	0.130	(0.135)	0.065	0.065
12	1.00	0.80	0.148	(0.135)	0.074	0.074
13	1.08	0.80	0.148	(0.135)	0.074	0.074
14	1.17	0.80	0.148	(0.135)	0.074	0.074
15	1.25	0.80	0.148	(0.135)	0.074	0.074
16	1.33	0.80	0.148	(0.135)	0.074	0.074
17	1.42	0.80	0.148	(0.135)	0.074	0.074
18	1.50	0.80	0.148	(0.135)	0.074	0.074
19	1.58	0.80	0.148	(0.135)	0.074	0.074
20	1.67	0.80	0.148	(0.135)	0.074	0.074
21	1.75	0.80	0.148	(0.135)	0.074	0.074
22	1.83	0.80	0.148	(0.135)	0.074	0.074
23	1.92	0.80	0.148	(0.135)	0.074	0.074
24	2.00	0.90	0.167	(0.135)	0.083	0.083
25	2.08	0.80	0.148	(0.135)	0.074	0.074
26	2.17	0.90	0.167	(0.135)	0.083	0.083
27	2.25	0.90	0.167	(0.135)	0.083	0.083
28	2.33	0.90	0.167	(0.135)	0.083	0.083
29	2.42	0.90	0.167	(0.135)	0.083	0.083
30	2.50	0.90	0.167	(0.135)	0.083	0.083
31	2.58	0.90	0.167	(0.135)	0.083	0.083
32	2.67	0.90	0.167	(0.135)	0.083	0.083
33	2.75	1.00	0.185	(0.135)	0.093	0.093
34	2.83	1.00	0.185	(0.135)	0.093	0.093
35	2.92	1.00	0.185	(0.135)	0.093	0.093
36	3.00	1.00	0.185	(0.135)	0.093	0.093
37	3.08	1.00	0.185	(0.135)	0.093	0.093
38	3.17	1.10	0.204	(0.135)	0.102	0.102
39	3.25	1.10	0.204	(0.135)	0.102	0.102
40	3.33	1.10	0.204	(0.135)	0.102	0.102
41	3.42	1.20	0.222	(0.135)	0.111	0.111
42	3.50	1.30	0.241	(0.135)	0.121	0.121
43	3.58	1.40	0.260	(0.135)	0.130	0.130
44	3.67	1.40	0.260	(0.135)	0.130	0.130
45	3.75	1.50	0.278	0.135	(0.139)	0.143
46	3.83	1.50	0.278	0.135	(0.139)	0.143
47	3.92	1.60	0.297	0.135	(0.148)	0.161
48	4.00	1.60	0.297	0.135	(0.148)	0.161
49	4.08	1.70	0.315	0.135	(0.158)	0.180
50	4.17	1.80	0.334	0.135	(0.167)	0.198
51	4.25	1.90	0.352	0.135	(0.176)	0.217
52	4.33	2.00	0.371	0.135	(0.185)	0.235
53	4.42	2.10	0.389	0.135	(0.195)	0.254
54	4.50	2.10	0.389	0.135	(0.195)	0.254
55	4.58	2.20	0.408	0.135	(0.204)	0.272
56	4.67	2.30	0.426	0.135	(0.213)	0.291
57	4.75	2.40	0.445	0.135	(0.222)	0.309
58	4.83	2.40	0.445	0.135	(0.222)	0.309
59	4.92	2.50	0.463	0.135	(0.232)	0.328
60	5.00	2.60	0.482	0.135	(0.241)	0.347
61	5.08	3.10	0.575	0.135	(0.287)	0.439
62	5.17	3.60	0.667	0.135	(0.334)	0.532
63	5.25	3.90	0.723	0.135	(0.362)	0.588
64	5.33	4.20	0.779	0.135	(0.389)	0.643
65	5.42	4.70	0.871	0.135	(0.436)	0.736
66	5.50	5.60	1.038	0.135	(0.519)	0.903
67	5.58	1.90	0.352	0.135	(0.176)	0.217
68	5.67	0.90	0.167	(0.135)	0.083	0.083
69	5.75	0.60	0.111	(0.135)	0.056	0.056
70	5.83	0.50	0.093	(0.135)	0.046	0.046

```
71   5.92     0.30      0.056       (  0.135)       0.028        0.028
72   6.00     0.20      0.037       (  0.135)       0.019        0.019
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =    11.6
     Flood volume = Effective rainfall      0.97(In)
      times area      26.7(Ac.)/[(In)/(Ft.)] =       2.2(Ac.Ft)
     Total soil loss =      0.57(In)
     Total soil loss =     1.281(Ac.Ft)
     Total rainfall =      1.54(In)
     Flood volume =       94156.5 Cubic Feet
     Total soil loss =       55799.6 Cubic Feet
     ---------------------------------------------------------------------
      Peak flow rate of this hydrograph =     20.558(CFS)
     ---------------------------------------------------------------------
     +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
     ---------------------------------------------------------------------
                 Hydrograph in   5   Minute intervals ((CFS))

     ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        7.5      15.0      22.5      30.0
-------------------------------------------------------------------------
  0+ 5       0.0028      0.40  Q         |         |         |         |
  0+10       0.0102      1.08  VQ        |         |         |         |
  0+15       0.0194      1.34  VQ        |         |         |         |
  0+20       0.0292      1.43  VQ        |         |         |         |
  0+25       0.0394      1.47  VQ        |         |         |         |
  0+30       0.0502      1.58  V Q       |         |         |         |
  0+35       0.0619      1.70  |VQ       |         |         |         |
  0+40       0.0738      1.73  |VQ       |         |         |         |
  0+45       0.0858      1.74  |VQ       |         |         |         |
  0+50       0.0978      1.75  |VQ       |         |         |         |
  0+55       0.1099      1.75  | Q       |         |         |         |
  1+ 0       0.1225      1.83  | Q       |         |         |         |
  1+ 5       0.1359      1.95  | Q       |         |         |         |
  1+10       0.1495      1.98  | Q       |         |         |         |
  1+15       0.1632      1.99  | QV      |         |         |         |
  1+20       0.1770      2.00  | QV      |         |         |         |
  1+25       0.1907      2.00  | QV      |         |         |         |
  1+30       0.2045      2.00  | QV      |         |         |         |
  1+35       0.2183      2.00  | Q V     |         |         |         |
  1+40       0.2320      2.00  | Q V     |         |         |         |
  1+45       0.2458      2.00  | Q V     |         |         |         |
  1+50       0.2596      2.00  | Q V     |         |         |         |
  1+55       0.2734      2.00  | Q  V    |         |         |         |
  2+ 0       0.2877      2.08  | Q  V    |         |         |         |
  2+ 5       0.3023      2.12  | Q  V    |         |         |         |
  2+10       0.3168      2.11  | Q  V    |         |         |         |
  2+15       0.3320      2.21  | Q   V   |         |         |         |
  2+20       0.3474      2.23  | Q   V   |         |         |         |
  2+25       0.3628      2.24  | Q   V   |         |         |         |
  2+30       0.3783      2.25  | Q    V  |         |         |         |
  2+35       0.3938      2.25  | Q    V  |         |         |         |
  2+40       0.4093      2.25  | Q    V  |         |         |         |
  2+45       0.4253      2.33  |  Q   V  |         |         |         |
  2+50       0.4422      2.45  |  Q    V |         |         |         |
  2+55       0.4593      2.48  |  Q    V |         |         |         |
  3+ 0       0.4764      2.49  |  Q    V |         |         |         |
  3+ 5       0.4936      2.50  |  Q     V|         |         |         |
  3+10       0.5114      2.58  |  Q     V|         |         |         |
  3+15       0.5299      2.70  |  Q     V|         |         |         |
  3+20       0.5487      2.73  |  Q      V         |         |         |
  3+25       0.5681      2.82  |  Q      V         |         |         |
  3+30       0.5890      3.03  |   Q     V         |         |         |
  3+35       0.6114      3.26  |   Q     |V        |         |         |
  3+40       0.6349      3.42  |   Q     |V        |         |         |
  3+45       0.6596      3.57  |   Q     | V       |         |         |
  3+50       0.6855      3.76  |    Q    | V       |         |         |
  3+55       0.7128      3.97  |    Q    |  V      |         |         |
  4+ 0       0.7419      4.23  |    Q    |  V      |         |         |
  4+ 5       0.7726      4.46  |    Q    |   V     |         |         |
  4+10       0.8063      4.88  |     Q   |   V     |         |         |
  4+15       0.8431      5.35  |      Q  |    V    |         |         |
  4+20       0.8833      5.84  |      Q  |     V   |         |         |
  4+25       0.9269      6.33  |       Q |      V  |         |         |
  4+30       0.9729      6.67  |       Q |       V |         |         |
  4+35       1.0206      6.93  |        Q|       V |         |         |
  4+40       1.0714      7.38  |        Q|        V|         |         |
  4+45       1.1255      7.85  |         Q         V         |         |
  4+50       1.1818      8.18  |         Q         |V        |         |
  4+55       1.2399      8.43  |         |Q        | V       |         |
  5+ 0       1.3010      8.88  |         |Q        |   V     |         |
  5+ 5       1.3699     10.00  |         |  Q      |    V    |         |
  5+10       1.4531     12.08  |         |     Q   |     V   |         |
  5+15       1.5499     14.07  |         |       Q |       V |         |
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    5+20       1.6580     15.69  |          |          Q          V          |
    5+25       1.7790     17.57  |          |          |  Q       | V        |
    5+30       1.9206     20.56  |          |          |       Q  |    V     |
    5+35       2.0385     17.12  |          |          | Q        |      V   |
    5+40       2.0931      7.92  |          Q          |          |       V  |
    5+45       2.1219      4.18  |     Q    |          |          |        V|
    5+50       2.1396      2.57  |   Q      |          |          |        V|
    5+55       2.1507      1.62  | Q        |          |          |        V|
    6+ 0       2.1567      0.88  |Q         |          |          |        V|
    6+ 5       2.1599      0.45  Q          |          |          |        V|
    6+10       2.1609      0.15  Q          |          |          |        V|
    6+15       2.1613      0.06  Q          |          |          |        V|
    6+20       2.1615      0.02  Q          |          |          |        V|
    6+25       2.1615      0.01  Q          |          |          |         V
-------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro15245.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.80	48.13

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	5.00	133.70

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 2.550(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 2.549(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	79.8	0.246	0.500	0.135	1.000	0.135
					Sum (F) =	0.135

Area averaged mean soil loss (F) (In/Hr) = 0.135
Minimum soil loss rate ((In/Hr)) = 0.068
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.020	(0.240)	0.010	0.010
2	0.17	0.07	0.020	(0.239)	0.010	0.010
3	0.25	0.07	0.020	(0.238)	0.010	0.010
4	0.33	0.10	0.031	(0.237)	0.015	0.015
5	0.42	0.10	0.031	(0.236)	0.015	0.015
6	0.50	0.10	0.031	(0.236)	0.015	0.015
7	0.58	0.10	0.031	(0.235)	0.015	0.015
8	0.67	0.10	0.031	(0.234)	0.015	0.015
9	0.75	0.10	0.031	(0.233)	0.015	0.015
10	0.83	0.13	0.041	(0.232)	0.020	0.020
11	0.92	0.13	0.041	(0.231)	0.020	0.020
12	1.00	0.13	0.041	(0.230)	0.020	0.020
13	1.08	0.10	0.031	(0.229)	0.015	0.015
14	1.17	0.10	0.031	(0.228)	0.015	0.015
15	1.25	0.10	0.031	(0.227)	0.015	0.015
16	1.33	0.10	0.031	(0.226)	0.015	0.015
17	1.42	0.10	0.031	(0.226)	0.015	0.015
18	1.50	0.10	0.031	(0.225)	0.015	0.015
19	1.58	0.10	0.031	(0.224)	0.015	0.015
20	1.67	0.10	0.031	(0.223)	0.015	0.015
21	1.75	0.10	0.031	(0.222)	0.015	0.015
22	1.83	0.13	0.041	(0.221)	0.020	0.020
23	1.92	0.13	0.041	(0.220)	0.020	0.020
24	2.00	0.13	0.041	(0.219)	0.020	0.020
25	2.08	0.13	0.041	(0.218)	0.020	0.020
26	2.17	0.13	0.041	(0.218)	0.020	0.020
27	2.25	0.13	0.041	(0.217)	0.020	0.020
28	2.33	0.13	0.041	(0.216)	0.020	0.020
29	2.42	0.13	0.041	(0.215)	0.020	0.020
30	2.50	0.13	0.041	(0.214)	0.020	0.020
31	2.58	0.17	0.051	(0.213)	0.025	0.025
32	2.67	0.17	0.051	(0.212)	0.025	0.025
33	2.75	0.17	0.051	(0.211)	0.025	0.025
34	2.83	0.17	0.051	(0.211)	0.025	0.025
35	2.92	0.17	0.051	(0.210)	0.025	0.025
36	3.00	0.17	0.051	(0.209)	0.025	0.025
37	3.08	0.17	0.051	(0.208)	0.025	0.025
38	3.17	0.17	0.051	(0.207)	0.025	0.025
39	3.25	0.17	0.051	(0.206)	0.025	0.025
40	3.33	0.17	0.051	(0.205)	0.025	0.025
41	3.42	0.17	0.051	(0.204)	0.025	0.025
42	3.50	0.17	0.051	(0.204)	0.025	0.025
43	3.58	0.17	0.051	(0.203)	0.025	0.025
44	3.67	0.17	0.051	(0.202)	0.025	0.025
45	3.75	0.17	0.051	(0.201)	0.025	0.025
46	3.83	0.20	0.061	(0.200)	0.031	0.031
47	3.92	0.20	0.061	(0.199)	0.031	0.031
48	4.00	0.20	0.061	(0.199)	0.031	0.031
49	4.08	0.20	0.061	(0.198)	0.031	0.031
50	4.17	0.20	0.061	(0.197)	0.031	0.031
51	4.25	0.20	0.061	(0.196)	0.031	0.031
52	4.33	0.23	0.071	(0.195)	0.036	0.036
53	4.42	0.23	0.071	(0.194)	0.036	0.036
54	4.50	0.23	0.071	(0.193)	0.036	0.036
55	4.58	0.23	0.071	(0.193)	0.036	0.036
56	4.67	0.23	0.071	(0.192)	0.036	0.036
57	4.75	0.23	0.071	(0.191)	0.036	0.036
58	4.83	0.27	0.082	(0.190)	0.041	0.041
59	4.92	0.27	0.082	(0.189)	0.041	0.041
60	5.00	0.27	0.082	(0.189)	0.041	0.041
61	5.08	0.20	0.061	(0.188)	0.031	0.031
62	5.17	0.20	0.061	(0.187)	0.031	0.031
63	5.25	0.20	0.061	(0.186)	0.031	0.031
64	5.33	0.23	0.071	(0.185)	0.036	0.036
65	5.42	0.23	0.071	(0.184)	0.036	0.036
66	5.50	0.23	0.071	(0.184)	0.036	0.036
67	5.58	0.27	0.082	(0.183)	0.041	0.041
68	5.67	0.27	0.082	(0.182)	0.041	0.041
69	5.75	0.27	0.082	(0.181)	0.041	0.041
70	5.83	0.27	0.082	(0.180)	0.041	0.041

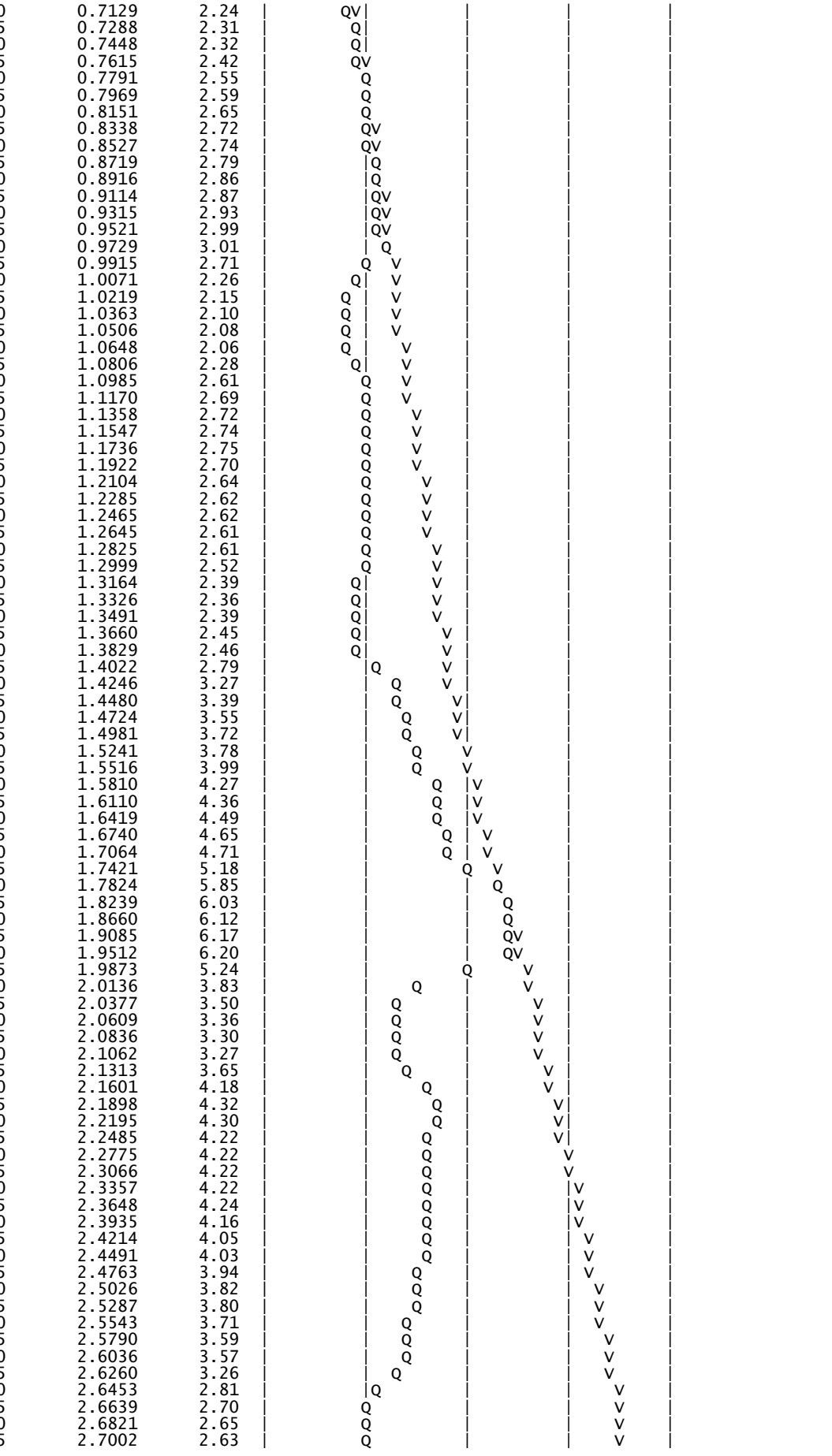
71	5.92	0.27	0.082	(	0.180)	0.041	0.041
72	6.00	0.27	0.082	(	0.179)	0.041	0.041
73	6.08	0.30	0.092	(	0.178)	0.046	0.046
74	6.17	0.30	0.092	(	0.177)	0.046	0.046
75	6.25	0.30	0.092	(	0.176)	0.046	0.046
76	6.33	0.30	0.092	(	0.176)	0.046	0.046
77	6.42	0.30	0.092	(	0.175)	0.046	0.046
78	6.50	0.30	0.092	(	0.174)	0.046	0.046
79	6.58	0.33	0.102	(	0.173)	0.051	0.051
80	6.67	0.33	0.102	(	0.173)	0.051	0.051
81	6.75	0.33	0.102	(	0.172)	0.051	0.051
82	6.83	0.33	0.102	(	0.171)	0.051	0.051
83	6.92	0.33	0.102	(	0.170)	0.051	0.051
84	7.00	0.33	0.102	(	0.169)	0.051	0.051
85	7.08	0.33	0.102	(	0.169)	0.051	0.051
86	7.17	0.33	0.102	(	0.168)	0.051	0.051
87	7.25	0.33	0.102	(	0.167)	0.051	0.051
88	7.33	0.37	0.112	(	0.166)	0.056	0.056
89	7.42	0.37	0.112	(	0.166)	0.056	0.056
90	7.50	0.37	0.112	(	0.165)	0.056	0.056
91	7.58	0.40	0.122	(	0.164)	0.061	0.061
92	7.67	0.40	0.122	(	0.163)	0.061	0.061
93	7.75	0.40	0.122	(	0.163)	0.061	0.061
94	7.83	0.43	0.133	(	0.162)	0.066	0.066
95	7.92	0.43	0.133	(	0.161)	0.066	0.066
96	8.00	0.43	0.133	(	0.160)	0.066	0.066
97	8.08	0.50	0.153	(	0.160)	0.076	0.076
98	8.17	0.50	0.153	(	0.159)	0.076	0.076
99	8.25	0.50	0.153	(	0.158)	0.076	0.076
100	8.33	0.50	0.153	(	0.157)	0.076	0.076
101	8.42	0.50	0.153	(	0.157)	0.076	0.076
102	8.50	0.50	0.153	(	0.156)	0.076	0.076
103	8.58	0.53	0.163	(	0.155)	0.082	0.082
104	8.67	0.53	0.163	(	0.154)	0.082	0.082
105	8.75	0.53	0.163	(	0.154)	0.082	0.082
106	8.83	0.57	0.173	(	0.153)	0.087	0.087
107	8.92	0.57	0.173	(	0.152)	0.087	0.087
108	9.00	0.57	0.173	(	0.152)	0.087	0.087
109	9.08	0.63	0.194	(	0.151)	0.097	0.097
110	9.17	0.63	0.194	(	0.150)	0.097	0.097
111	9.25	0.63	0.194	(	0.149)	0.097	0.097
112	9.33	0.67	0.204	(	0.149)	0.102	0.102
113	9.42	0.67	0.204	(	0.148)	0.102	0.102
114	9.50	0.67	0.204	(	0.147)	0.102	0.102
115	9.58	0.70	0.214	(	0.147)	0.107	0.107
116	9.67	0.70	0.214	(	0.146)	0.107	0.107
117	9.75	0.70	0.214	(	0.145)	0.107	0.107
118	9.83	0.73	0.224	(	0.144)	0.112	0.112
119	9.92	0.73	0.224	(	0.144)	0.112	0.112
120	10.00	0.73	0.224	(	0.143)	0.112	0.112
121	10.08	0.50	0.153	(	0.142)	0.076	0.076
122	10.17	0.50	0.153	(	0.142)	0.076	0.076
123	10.25	0.50	0.153	(	0.141)	0.076	0.076
124	10.33	0.50	0.153	(	0.140)	0.076	0.076
125	10.42	0.50	0.153	(	0.140)	0.076	0.076
126	10.50	0.50	0.153	(	0.139)	0.076	0.076
127	10.58	0.67	0.204	(	0.138)	0.102	0.102
128	10.67	0.67	0.204	(	0.138)	0.102	0.102
129	10.75	0.67	0.204	(	0.137)	0.102	0.102
130	10.83	0.67	0.204	(	0.136)	0.102	0.102
131	10.92	0.67	0.204	(	0.136)	0.102	0.102
132	11.00	0.67	0.204	(	0.135)	0.102	0.102
133	11.08	0.63	0.194	(	0.134)	0.097	0.097
134	11.17	0.63	0.194	(	0.134)	0.097	0.097
135	11.25	0.63	0.194	(	0.133)	0.097	0.097
136	11.33	0.63	0.194	(	0.132)	0.097	0.097
137	11.42	0.63	0.194	(	0.132)	0.097	0.097
138	11.50	0.63	0.194	(	0.131)	0.097	0.097
139	11.58	0.57	0.173	(	0.130)	0.087	0.087
140	11.67	0.57	0.173	(	0.130)	0.087	0.087
141	11.75	0.57	0.173	(	0.129)	0.087	0.087
142	11.83	0.60	0.184	(	0.128)	0.092	0.092
143	11.92	0.60	0.184	(	0.128)	0.092	0.092
144	12.00	0.60	0.184	(	0.127)	0.092	0.092
145	12.08	0.83	0.255		0.126	(0.127)	0.128
146	12.17	0.83	0.255		0.126	(0.127)	0.129
147	12.25	0.83	0.255		0.125	(0.127)	0.130
148	12.33	0.87	0.265		0.125	(0.133)	0.141
149	12.42	0.87	0.265		0.124	(0.133)	0.141
150	12.50	0.87	0.265		0.123	(0.133)	0.142
151	12.58	0.93	0.286		0.123	(0.143)	0.163
152	12.67	0.93	0.286		0.122	(0.143)	0.163
153	12.75	0.93	0.286		0.121	(0.143)	0.164
154	12.83	0.97	0.296		0.121	(0.148)	0.175
155	12.92	0.97	0.296		0.120	(0.148)	0.175
156	13.00	0.97	0.296		0.120	(0.148)	0.176

157	13.08	1.13	0.347	0.119	(0.173)	0.228
158	13.17	1.13	0.347	0.118	(0.173)	0.228
159	13.25	1.13	0.347	0.118	(0.173)	0.229
160	13.33	1.13	0.347	0.117	(0.173)	0.229
161	13.42	1.13	0.347	0.117	(0.173)	0.230
162	13.50	1.13	0.347	0.116	(0.173)	0.231
163	13.58	0.77	0.235	0.115	(0.117)	0.119
164	13.67	0.77	0.235	0.115	(0.117)	0.120
165	13.75	0.77	0.235	0.114	(0.117)	0.120
166	13.83	0.77	0.235	0.114	(0.117)	0.121
167	13.92	0.77	0.235	0.113	(0.117)	0.121
168	14.00	0.77	0.235	0.113	(0.117)	0.122
169	14.08	0.90	0.275	0.112	(0.138)	0.163
170	14.17	0.90	0.275	0.111	(0.138)	0.164
171	14.25	0.90	0.275	0.111	(0.138)	0.164
172	14.33	0.87	0.265	0.110	(0.133)	0.155
173	14.42	0.87	0.265	0.110	(0.133)	0.155
174	14.50	0.87	0.265	0.109	(0.133)	0.156
175	14.58	0.87	0.265	0.109	(0.133)	0.157
176	14.67	0.87	0.265	0.108	(0.133)	0.157
177	14.75	0.87	0.265	0.107	(0.133)	0.158
178	14.83	0.83	0.255	0.107	(0.127)	0.148
179	14.92	0.83	0.255	0.106	(0.127)	0.149
180	15.00	0.83	0.255	0.106	(0.127)	0.149
181	15.08	0.80	0.245	0.105	(0.122)	0.139
182	15.17	0.80	0.245	0.105	(0.122)	0.140
183	15.25	0.80	0.245	0.104	(0.122)	0.141
184	15.33	0.77	0.235	0.104	(0.117)	0.131
185	15.42	0.77	0.235	0.103	(0.117)	0.131
186	15.50	0.77	0.235	0.103	(0.117)	0.132
187	15.58	0.63	0.194	(0.102)	0.097	0.097
188	15.67	0.63	0.194	(0.102)	0.097	0.097
189	15.75	0.63	0.194	(0.101)	0.097	0.097
190	15.83	0.63	0.194	(0.101)	0.097	0.097
191	15.92	0.63	0.194	(0.100)	0.097	0.097
192	16.00	0.63	0.194	(0.100)	0.097	0.097
193	16.08	0.13	0.041	(0.099)	0.020	0.020
194	16.17	0.13	0.041	(0.098)	0.020	0.020
195	16.25	0.13	0.041	(0.098)	0.020	0.020
196	16.33	0.13	0.041	(0.097)	0.020	0.020
197	16.42	0.13	0.041	(0.097)	0.020	0.020
198	16.50	0.13	0.041	(0.096)	0.020	0.020
199	16.58	0.10	0.031	(0.096)	0.015	0.015
200	16.67	0.10	0.031	(0.096)	0.015	0.015
201	16.75	0.10	0.031	(0.095)	0.015	0.015
202	16.83	0.10	0.031	(0.095)	0.015	0.015
203	16.92	0.10	0.031	(0.094)	0.015	0.015
204	17.00	0.10	0.031	(0.094)	0.015	0.015
205	17.08	0.17	0.051	(0.093)	0.025	0.025
206	17.17	0.17	0.051	(0.093)	0.025	0.025
207	17.25	0.17	0.051	(0.092)	0.025	0.025
208	17.33	0.17	0.051	(0.092)	0.025	0.025
209	17.42	0.17	0.051	(0.091)	0.025	0.025
210	17.50	0.17	0.051	(0.091)	0.025	0.025
211	17.58	0.17	0.051	(0.090)	0.025	0.025
212	17.67	0.17	0.051	(0.090)	0.025	0.025
213	17.75	0.17	0.051	(0.089)	0.025	0.025
214	17.83	0.13	0.041	(0.089)	0.020	0.020
215	17.92	0.13	0.041	(0.089)	0.020	0.020
216	18.00	0.13	0.041	(0.088)	0.020	0.020
217	18.08	0.13	0.041	(0.088)	0.020	0.020
218	18.17	0.13	0.041	(0.087)	0.020	0.020
219	18.25	0.13	0.041	(0.087)	0.020	0.020
220	18.33	0.13	0.041	(0.086)	0.020	0.020
221	18.42	0.13	0.041	(0.086)	0.020	0.020
222	18.50	0.13	0.041	(0.086)	0.020	0.020
223	18.58	0.10	0.031	(0.085)	0.015	0.015
224	18.67	0.10	0.031	(0.085)	0.015	0.015
225	18.75	0.10	0.031	(0.084)	0.015	0.015
226	18.83	0.07	0.020	(0.084)	0.010	0.010
227	18.92	0.07	0.020	(0.084)	0.010	0.010
228	19.00	0.07	0.020	(0.083)	0.010	0.010
229	19.08	0.10	0.031	(0.083)	0.015	0.015
230	19.17	0.10	0.031	(0.082)	0.015	0.015
231	19.25	0.10	0.031	(0.082)	0.015	0.015
232	19.33	0.13	0.041	(0.082)	0.020	0.020
233	19.42	0.13	0.041	(0.081)	0.020	0.020
234	19.50	0.13	0.041	(0.081)	0.020	0.020
235	19.58	0.10	0.031	(0.080)	0.015	0.015
236	19.67	0.10	0.031	(0.080)	0.015	0.015
237	19.75	0.10	0.031	(0.080)	0.015	0.015
238	19.83	0.07	0.020	(0.079)	0.010	0.010
239	19.92	0.07	0.020	(0.079)	0.010	0.010
240	20.00	0.07	0.020	(0.079)	0.010	0.010
241	20.08	0.10	0.031	(0.078)	0.015	0.015
242	20.17	0.10	0.031	(0.078)	0.015	0.015

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243  20.25     0.10      0.031       (  0.078)       0.015        0.015
244  20.33     0.10      0.031       (  0.077)       0.015        0.015
245  20.42     0.10      0.031       (  0.077)       0.015        0.015
246  20.50     0.10      0.031       (  0.077)       0.015        0.015
247  20.58     0.10      0.031       (  0.076)       0.015        0.015
248  20.67     0.10      0.031       (  0.076)       0.015        0.015
249  20.75     0.10      0.031       (  0.076)       0.015        0.015
250  20.83     0.07      0.020       (  0.075)       0.010        0.010
251  20.92     0.07      0.020       (  0.075)       0.010        0.010
252  21.00     0.07      0.020       (  0.075)       0.010        0.010
253  21.08     0.10      0.031       (  0.074)       0.015        0.015
254  21.17     0.10      0.031       (  0.074)       0.015        0.015
255  21.25     0.10      0.031       (  0.074)       0.015        0.015
256  21.33     0.07      0.020       (  0.074)       0.010        0.010
257  21.42     0.07      0.020       (  0.073)       0.010        0.010
258  21.50     0.07      0.020       (  0.073)       0.010        0.010
259  21.58     0.10      0.031       (  0.073)       0.015        0.015
260  21.67     0.10      0.031       (  0.073)       0.015        0.015
261  21.75     0.10      0.031       (  0.072)       0.015        0.015
262  21.83     0.07      0.020       (  0.072)       0.010        0.010
263  21.92     0.07      0.020       (  0.072)       0.010        0.010
264  22.00     0.07      0.020       (  0.072)       0.010        0.010
265  22.08     0.10      0.031       (  0.071)       0.015        0.015
266  22.17     0.10      0.031       (  0.071)       0.015        0.015
267  22.25     0.10      0.031       (  0.071)       0.015        0.015
268  22.33     0.07      0.020       (  0.071)       0.010        0.010
269  22.42     0.07      0.020       (  0.070)       0.010        0.010
270  22.50     0.07      0.020       (  0.070)       0.010        0.010
271  22.58     0.07      0.020       (  0.070)       0.010        0.010
272  22.67     0.07      0.020       (  0.070)       0.010        0.010
273  22.75     0.07      0.020       (  0.070)       0.010        0.010
274  22.83     0.07      0.020       (  0.069)       0.010        0.010
275  22.92     0.07      0.020       (  0.069)       0.010        0.010
276  23.00     0.07      0.020       (  0.069)       0.010        0.010
277  23.08     0.07      0.020       (  0.069)       0.010        0.010
278  23.17     0.07      0.020       (  0.069)       0.010        0.010
279  23.25     0.07      0.020       (  0.069)       0.010        0.010
280  23.33     0.07      0.020       (  0.068)       0.010        0.010
281  23.42     0.07      0.020       (  0.068)       0.010        0.010
282  23.50     0.07      0.020       (  0.068)       0.010        0.010
283  23.58     0.07      0.020       (  0.068)       0.010        0.010
284  23.67     0.07      0.020       (  0.068)       0.010        0.010
285  23.75     0.07      0.020       (  0.068)       0.010        0.010
286  23.83     0.07      0.020       (  0.068)       0.010        0.010
287  23.92     0.07      0.020       (  0.068)       0.010        0.010
288  24.00     0.07      0.020       (  0.068)       0.010        0.010
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    16.2
      Flood volume = Effective rainfall      1.35(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       3.0(Ac.Ft)
      Total soil loss =      1.20(In)
      Total soil loss =     2.672(Ac.Ft)
      Total rainfall =      2.55(In)
      Flood volume =      131085.8 Cubic Feet
      Total soil loss =      116373.3 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      6.203(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0006      0.09  Q          |         |         |         |
   0+10       0.0021      0.22  Q          |         |         |         |
   0+15       0.0038      0.25  VQ         |         |         |         |
   0+20       0.0060      0.31  VQ         |         |         |         |
   0+25       0.0086      0.38  VQ         |         |         |         |
   0+30       0.0113      0.40  VQ         |         |         |         |
   0+35       0.0141      0.41  VQ         |         |         |         |
   0+40       0.0170      0.41  VQ         |         |         |         |
   0+45       0.0198      0.41  VQ         |         |         |         |
   0+50       0.0230      0.46  VQ         |         |         |         |
   0+55       0.0266      0.52  V Q        |         |         |         |
   1+ 0       0.0303      0.54  V Q        |         |         |         |
   1+ 5       0.0337      0.50  VQ         |         |         |         |
   1+10       0.0367      0.44  VQ         |         |         |         |
   1+15       0.0396      0.42  VQ         |         |         |         |
   1+20       0.0425      0.42  VQ         |         |         |         |
   1+25       0.0454      0.41  VQ         |         |         |         |
   1+30       0.0482      0.41  VQ         |         |         |         |
   1+35       0.0511      0.41  VQ         |         |         |         |
```

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1+40       0.0539      0.41  VQ        |         |         |         |
1+45       0.0567      0.41  VQ        |         |         |         |
1+50       0.0599      0.46  VQ        |         |         |         |
1+55       0.0635      0.52  V Q       |         |         |         |
2+ 0       0.0672      0.54  V Q       |         |         |         |
2+ 5       0.0709      0.54  V Q       |         |         |         |
2+10       0.0747      0.55  V Q       |         |         |         |
2+15       0.0785      0.55  |VQ       |         |         |         |
2+20       0.0823      0.55  |VQ       |         |         |         |
2+25       0.0861      0.55  |VQ       |         |         |         |
2+30       0.0899      0.55  |VQ       |         |         |         |
2+35       0.0940      0.59  |VQ       |         |         |         |
2+40       0.0985      0.66  |VQ       |         |         |         |
2+45       0.1031      0.68  |VQ       |         |         |         |
2+50       0.1078      0.68  |VQ       |         |         |         |
2+55       0.1126      0.69  |VQ       |         |         |         |
3+ 0       0.1173      0.69  |VQ       |         |         |         |
3+ 5       0.1220      0.69  |VQ       |         |         |         |
3+10       0.1268      0.69  |VQ       |         |         |         |
3+15       0.1315      0.69  |VQ       |         |         |         |
3+20       0.1362      0.69  |VQ       |         |         |         |
3+25       0.1410      0.69  |VQ       |         |         |         |
3+30       0.1457      0.69  |VQ       |         |         |         |
3+35       0.1504      0.69  |VQ       |         |         |         |
3+40       0.1552      0.69  | Q       |         |         |         |
3+45       0.1599      0.69  | Q       |         |         |         |
3+50       0.1649      0.73  | Q       |         |         |         |
3+55       0.1704      0.80  | VQ      |         |         |         |
4+ 0       0.1760      0.81  | VQ      |         |         |         |
4+ 5       0.1817      0.82  | VQ      |         |         |         |
4+10       0.1873      0.82  | VQ      |         |         |         |
4+15       0.1930      0.82  | VQ      |         |         |         |
4+20       0.1990      0.87  | VQ      |         |         |         |
4+25       0.2054      0.93  | VQ      |         |         |         |
4+30       0.2120      0.95  | VQ      |         |         |         |
4+35       0.2186      0.96  | VQ      |         |         |         |
4+40       0.2252      0.96  | VQ      |         |         |         |
4+45       0.2318      0.96  |  Q      |         |         |         |
4+50       0.2387      1.01  |  VQ     |         |         |         |
4+55       0.2461      1.07  |  VQ     |         |         |         |
5+ 0       0.2536      1.09  |  VQ     |         |         |         |
5+ 5       0.2605      1.01  |  VQ     |         |         |         |
5+10       0.2666      0.88  |  Q      |         |         |         |
5+15       0.2724      0.85  |  Q      |         |         |         |
5+20       0.2785      0.88  |  Q      |         |         |         |
5+25       0.2850      0.94  |  Q      |         |         |         |
5+30       0.2915      0.95  |  Q      |         |         |         |
5+35       0.2984      1.00  |  VQ     |         |         |         |
5+40       0.3058      1.07  |   Q     |         |         |         |
5+45       0.3133      1.09  |   Q     |         |         |         |
5+50       0.3208      1.09  |   Q     |         |         |         |
5+55       0.3284      1.10  |   Q     |         |         |         |
6+ 0       0.3359      1.10  |   Q     |         |         |         |
6+ 5       0.3438      1.14  |   Q     |         |         |         |
6+10       0.3521      1.21  |   Q     |         |         |         |
6+15       0.3606      1.22  |   Q     |         |         |         |
6+20       0.3691      1.23  |   Q     |         |         |         |
6+25       0.3776      1.24  |   QV    |         |         |         |
6+30       0.3861      1.24  |   QV    |         |         |         |
6+35       0.3949      1.28  |    Q    |         |         |         |
6+40       0.4042      1.35  |    Q    |         |         |         |
6+45       0.4136      1.36  |    Q    |         |         |         |
6+50       0.4230      1.37  |    Q    |         |         |         |
6+55       0.4325      1.37  |    Q    |         |         |         |
7+ 0       0.4419      1.37  |    Q    |         |         |         |
7+ 5       0.4514      1.37  |    QV   |         |         |         |
7+10       0.4609      1.37  |    QV   |         |         |         |
7+15       0.4703      1.37  |    QV   |         |         |         |
7+20       0.4801      1.42  |    QV   |         |         |         |
7+25       0.4903      1.48  |    QV   |         |         |         |
7+30       0.5007      1.50  |    QV   |         |         |         |
7+35       0.5114      1.55  |     Q   |         |         |         |
7+40       0.5225      1.62  |     Q   |         |         |         |
7+45       0.5338      1.64  |     QV  |         |         |         |
7+50       0.5454      1.69  |     QV  |         |         |         |
7+55       0.5575      1.76  |      Q  |         |         |         |
8+ 0       0.5697      1.77  |      Q  |         |         |         |
8+ 5       0.5826      1.87  |      Q  |         |         |         |
8+10       0.5964      2.00  |      VQ |         |         |         |
8+15       0.6105      2.04  |       Q |         |         |         |
8+20       0.6246      2.05  |       Q |         |         |         |
8+25       0.6388      2.06  |       Q |         |         |         |
8+30       0.6530      2.06  |       Q |         |         |         |
8+35       0.6675      2.11  |       Q |         |         |         |
8+40       0.6824      2.17  |       QV|         |         |         |
8+45       0.6975      2.19  |       QV|         |         |         |
```

8+50	0.7129	2.24	
8+55	0.7288	2.31	
9+ 0	0.7448	2.32	
9+ 5	0.7615	2.42	
9+10	0.7791	2.55	
9+15	0.7969	2.59	
9+20	0.8151	2.65	
9+25	0.8338	2.72	
9+30	0.8527	2.74	
9+35	0.8719	2.79	
9+40	0.8916	2.86	
9+45	0.9114	2.87	
9+50	0.9315	2.93	
9+55	0.9521	2.99	
10+ 0	0.9729	3.01	
10+ 5	0.9915	2.71	
10+10	1.0071	2.26	
10+15	1.0219	2.15	
10+20	1.0363	2.10	
10+25	1.0506	2.08	
10+30	1.0648	2.06	
10+35	1.0806	2.28	
10+40	1.0985	2.61	
10+45	1.1170	2.69	
10+50	1.1358	2.72	
10+55	1.1547	2.74	
11+ 0	1.1736	2.75	
11+ 5	1.1922	2.70	
11+10	1.2104	2.64	
11+15	1.2285	2.62	
11+20	1.2465	2.62	
11+25	1.2645	2.61	
11+30	1.2825	2.61	
11+35	1.2999	2.52	
11+40	1.3164	2.39	
11+45	1.3326	2.36	
11+50	1.3491	2.39	
11+55	1.3660	2.45	
12+ 0	1.3829	2.46	
12+ 5	1.4022	2.79	
12+10	1.4246	3.27	
12+15	1.4480	3.39	
12+20	1.4724	3.55	
12+25	1.4981	3.72	
12+30	1.5241	3.78	
12+35	1.5516	3.99	
12+40	1.5810	4.27	
12+45	1.6110	4.36	
12+50	1.6419	4.49	
12+55	1.6740	4.65	
13+ 0	1.7064	4.71	
13+ 5	1.7421	5.18	
13+10	1.7824	5.85	
13+15	1.8239	6.03	
13+20	1.8660	6.12	
13+25	1.9085	6.17	
13+30	1.9512	6.20	
13+35	1.9873	5.24	
13+40	2.0136	3.83	
13+45	2.0377	3.50	
13+50	2.0609	3.36	
13+55	2.0836	3.30	
14+ 0	2.1062	3.27	
14+ 5	2.1313	3.65	
14+10	2.1601	4.18	
14+15	2.1898	4.32	
14+20	2.2195	4.30	
14+25	2.2485	4.22	
14+30	2.2775	4.22	
14+35	2.3066	4.22	
14+40	2.3357	4.22	
14+45	2.3648	4.24	
14+50	2.3935	4.16	
14+55	2.4214	4.05	
15+ 0	2.4491	4.03	
15+ 5	2.4763	3.94	
15+10	2.5026	3.82	
15+15	2.5287	3.80	
15+20	2.5543	3.71	
15+25	2.5790	3.59	
15+30	2.6036	3.57	
15+35	2.6260	3.26	
15+40	2.6453	2.81	
15+45	2.6639	2.70	
15+50	2.6821	2.65	
15+55	2.7002	2.63	

16+ 0	2.7182	2.61	|	Q	|	|	V |
16+ 5	2.7316	1.94	|	Q	|	|	V |
16+10	2.7383	0.97	|	Q	|	|	V |
16+15	2.7433	0.74	| Q	|	|	|	V |
16+20	2.7477	0.63	| Q	|	|	|	V |
16+25	2.7517	0.58	| Q	|	|	|	V |
16+30	2.7555	0.55	| Q	|	|	|	V |
16+35	2.7590	0.51	| Q	|	|	|	V |
16+40	2.7620	0.44	|Q	|	|	|	V |
16+45	2.7649	0.42	|Q	|	|	|	V |
16+50	2.7678	0.42	|Q	|	|	|	V |
16+55	2.7707	0.41	|Q	|	|	|	V |
17+ 0	2.7735	0.41	|Q	|	|	|	V |
17+ 5	2.7769	0.50	| Q	|	|	|	V |
17+10	2.7813	0.63	| Q	|	|	|	V |
17+15	2.7859	0.66	| Q	|	|	|	V |
17+20	2.7905	0.68	| Q	|	|	|	V |
17+25	2.7952	0.68	| Q	|	|	|	V |
17+30	2.8000	0.69	| Q	|	|	|	V |
17+35	2.8047	0.69	| Q	|	|	|	V |
17+40	2.8094	0.69	| Q	|	|	|	V |
17+45	2.8142	0.69	| Q	|	|	|	V |
17+50	2.8186	0.64	| Q	|	|	|	V |
17+55	2.8226	0.58	| Q	|	|	|	V |
18+ 0	2.8264	0.56	| Q	|	|	|	V |
18+ 5	2.8303	0.56	| Q	|	|	|	V |
18+10	2.8341	0.55	| Q	|	|	|	V |
18+15	2.8379	0.55	| Q	|	|	|	V |
18+20	2.8416	0.55	| Q	|	|	|	V |
18+25	2.8454	0.55	| Q	|	|	|	V |
18+30	2.8492	0.55	| Q	|	|	|	V |
18+35	2.8527	0.51	| Q	|	|	|	V |
18+40	2.8557	0.44	|Q	|	|	|	V |
18+45	2.8587	0.42	|Q	|	|	|	V |
18+50	2.8612	0.37	|Q	|	|	|	V |
18+55	2.8633	0.30	|Q	|	|	|	V |
19+ 0	2.8653	0.29	|Q	|	|	|	V |
19+ 5	2.8675	0.33	|Q	|	|	|	V |
19+10	2.8702	0.39	|Q	|	|	|	V |
19+15	2.8730	0.40	|Q	|	|	|	V |
19+20	2.8761	0.45	|Q	|	|	|	V |
19+25	2.8796	0.52	| Q	|	|	|	V |
19+30	2.8834	0.54	| Q	|	|	|	V |
19+35	2.8868	0.50	|Q	|	|	|	V |
19+40	2.8898	0.44	|Q	|	|	|	V |
19+45	2.8927	0.42	|Q	|	|	|	V |
19+50	2.8953	0.37	|Q	|	|	|	V |
19+55	2.8974	0.30	|Q	|	|	|	V |
20+ 0	2.8994	0.29	|Q	|	|	|	V |
20+ 5	2.9016	0.33	|Q	|	|	|	V |
20+10	2.9043	0.39	|Q	|	|	|	V |
20+15	2.9070	0.40	|Q	|	|	|	V |
20+20	2.9098	0.41	|Q	|	|	|	V |
20+25	2.9127	0.41	|Q	|	|	|	V |
20+30	2.9155	0.41	|Q	|	|	|	V |
20+35	2.9184	0.41	|Q	|	|	|	V |
20+40	2.9212	0.41	|Q	|	|	|	V |
20+45	2.9240	0.41	|Q	|	|	|	V |
20+50	2.9266	0.37	|Q	|	|	|	V |
20+55	2.9287	0.30	|Q	|	|	|	V |
21+ 0	2.9306	0.29	|Q	|	|	|	V |
21+ 5	2.9329	0.33	|Q	|	|	|	V |
21+10	2.9355	0.39	|Q	|	|	|	V|
21+15	2.9383	0.40	|Q	|	|	|	V|
21+20	2.9408	0.36	|Q	|	|	|	V|
21+25	2.9429	0.30	|Q	|	|	|	V|
21+30	2.9448	0.29	|Q	|	|	|	V|
21+35	2.9471	0.33	|Q	|	|	|	V|
21+40	2.9497	0.39	|Q	|	|	|	V|
21+45	2.9525	0.40	|Q	|	|	|	V|
21+50	2.9550	0.36	|Q	|	|	|	V|
21+55	2.9571	0.30	|Q	|	|	|	V|
22+ 0	2.9590	0.29	|Q	|	|	|	V|
22+ 5	2.9613	0.33	|Q	|	|	|	V|
22+10	2.9639	0.39	|Q	|	|	|	V|
22+15	2.9667	0.40	|Q	|	|	|	V|
22+20	2.9692	0.36	|Q	|	|	|	V|
22+25	2.9713	0.30	|Q	|	|	|	V|
22+30	2.9732	0.29	|Q	|	|	|	V|
22+35	2.9752	0.28	|Q	|	|	|	V|
22+40	2.9771	0.28	|Q	|	|	|	V|
22+45	2.9790	0.27	|Q	|	|	|	V|
22+50	2.9809	0.27	|Q	|	|	|	V|
22+55	2.9828	0.27	|Q	|	|	|	V|
23+ 0	2.9847	0.27	|Q	|	|	|	V|
23+ 5	2.9865	0.27	|Q	|	|	|	V|

```
   23+10       2.9884      0.27  |Q        |         |         |        v|
   23+15       2.9903      0.27  |Q        |         |         |        v|
   23+20       2.9922      0.27  |Q        |         |         |        v|
   23+25       2.9941      0.27  |Q        |         |         |        v|
   23+30       2.9960      0.27  |Q        |         |         |        v|
   23+35       2.9979      0.27  |Q        |         |         |        v|
   23+40       2.9998      0.27  |Q        |         |         |        v|
   23+45       3.0017      0.27  |Q        |         |         |        v|
   23+50       3.0036      0.27  |Q        |         |         |        v|
   23+55       3.0055      0.27  |Q        |         |         |        v|
   24+ 0       3.0074      0.27  |Q        |         |         |        v|
   24+ 5       3.0087      0.19  Q         |         |         |        v|
   24+10       3.0090      0.06  Q         |         |         |        v|
   24+15       3.0092      0.02  Q         |         |         |        v|
   24+20       3.0093      0.01  Q         |         |         |        v|
   24+25       3.0093      0.00  Q         |         |         |         v
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       U n i t   H y d r o g r a p h   A n a l y s i s

       Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2008, Version 8.1
              Study date  04/22/24 File: pro110110.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      26.74(Ac.)  =      0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      26.74(Ac.)  =      0.042 Sq. Mi.
Length along longest watercourse =    2399.00(Ft.)
Length along longest watercourse measured to centroid =    1200.00(Ft.)
Length along longest watercourse =      0.454 Mi.
Length along longest watercourse measured to centroid =      0.227 Mi.
Difference in elevation =      81.00(Ft.)
Slope along watercourse =    178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.057 Hr.
Lag time =     3.40 Min.
25% of lag time =     0.85 Min.
40% of lag time =     1.36 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           0.50                 13.37

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           1.30                 34.76

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.829(In)
Areal adjustment factor =   99.98 %
Adjusted average point rain =    0.829(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    26.740           91.00         0.500
 Total Area Entered =     26.74(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  91.0      0.117     0.500        0.064       1.000      0.064
                                                 Sum (F) =   0.064
Area averaged mean soil loss (F) (In/Hr) =  0.064
Minimum soil loss rate ((In/Hr)) =  0.032
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
		Sum = 100.000	Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.328	0.064	(0.164)	0.264
2	0.17	4.20	0.418	0.064	(0.209)	0.353
3	0.25	4.40	0.438	0.064	(0.219)	0.373
4	0.33	4.80	0.477	0.064	(0.239)	0.413
5	0.42	5.20	0.517	0.064	(0.259)	0.453
6	0.50	6.20	0.617	0.064	(0.308)	0.552
7	0.58	6.80	0.676	0.064	(0.338)	0.612
8	0.67	8.80	0.875	0.064	(0.438)	0.811
9	0.75	13.90	1.383	0.064	(0.691)	1.318
10	0.83	31.40	3.123	0.064	(1.562)	3.059
11	0.92	7.20	0.716	0.064	(0.358)	0.652
12	1.00	3.80	0.378	0.064	(0.189)	0.314
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	9.2

Flood volume = Effective rainfall 0.76(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 1.7(Ac.Ft)
Total soil loss = 0.06(In)
Total soil loss = 0.143(Ac.Ft)
Total rainfall = 0.83(In)
Flood volume = 74214.4 Cubic Feet
Total soil loss = 6246.2 Cubic Feet

Peak flow rate of this hydrograph = 50.425(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	15.0	30.0	45.0	60.0
0+ 5	0.0159	2.31	VQ				
0+10	0.0603	6.45	V Q				
0+15	0.1193	8.57	V Q				
0+20	0.1868	9.80	V Q				
0+25	0.2627	11.02	VQ				
0+30	0.3503	12.71	Q				
0+35	0.4517	14.72	QV				
0+40	0.5730	17.61	Q V				
0+45	0.7447	24.94	QV				
0+50	1.0711	47.39	V			Q	
0+55	1.4184	50.42				Q	
1+ 0	1.5767	22.99	Q			V	
1+ 5	1.6547	11.33	Q			V	
1+10	1.6854	4.46	Q			V	
1+15	1.6996	2.06	Q			V	
1+20	1.7029	0.47	Q			V	
1+25	1.7037	0.12	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro110310.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	0.80	21.39

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	2.00	53.48

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 1.294(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.294(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.500	0.064	1.000	0.064
					Sum (F) =	0.064

Area averaged mean soil loss (F) (In/Hr) = 0.064
Minimum soil loss rate ((In/Hr)) = 0.032
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
		Sum = 100.000	Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.202	0.064	(0.101)	0.137
2	0.17	1.30	0.202	0.064	(0.101)	0.137
3	0.25	1.10	0.171	0.064	(0.085)	0.106
4	0.33	1.50	0.233	0.064	(0.116)	0.168
5	0.42	1.50	0.233	0.064	(0.116)	0.168
6	0.50	1.80	0.279	0.064	(0.140)	0.215
7	0.58	1.50	0.233	0.064	(0.116)	0.168
8	0.67	1.80	0.279	0.064	(0.140)	0.215
9	0.75	1.80	0.279	0.064	(0.140)	0.215
10	0.83	1.50	0.233	0.064	(0.116)	0.168
11	0.92	1.60	0.248	0.064	(0.124)	0.184
12	1.00	1.80	0.279	0.064	(0.140)	0.215
13	1.08	2.20	0.341	0.064	(0.171)	0.277
14	1.17	2.20	0.341	0.064	(0.171)	0.277
15	1.25	2.20	0.341	0.064	(0.171)	0.277
16	1.33	2.00	0.310	0.064	(0.155)	0.246
17	1.42	2.60	0.404	0.064	(0.202)	0.339
18	1.50	2.70	0.419	0.064	(0.210)	0.355
19	1.58	2.40	0.373	0.064	(0.186)	0.308
20	1.67	2.70	0.419	0.064	(0.210)	0.355
21	1.75	3.30	0.512	0.064	(0.256)	0.448
22	1.83	3.10	0.481	0.064	(0.241)	0.417
23	1.92	2.90	0.450	0.064	(0.225)	0.386
24	2.00	3.00	0.466	0.064	(0.233)	0.401
25	2.08	3.10	0.481	0.064	(0.241)	0.417
26	2.17	4.20	0.652	0.064	(0.326)	0.588
27	2.25	5.00	0.776	0.064	(0.388)	0.712
28	2.33	3.50	0.543	0.064	(0.272)	0.479
29	2.42	6.80	1.056	0.064	(0.528)	0.991
30	2.50	7.30	1.133	0.064	(0.567)	1.069
31	2.58	8.20	1.273	0.064	(0.636)	1.208
32	2.67	5.90	0.916	0.064	(0.458)	0.851
33	2.75	2.00	0.310	0.064	(0.155)	0.246
34	2.83	1.80	0.279	0.064	(0.140)	0.215
35	2.92	1.80	0.279	0.064	(0.140)	0.215
36	3.00	0.60	0.093	(0.064)	0.047	0.047
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	13.2

Flood volume = Effective rainfall 1.10(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 2.5(Ac.Ft)
Total soil loss = 0.19(In)
Total soil loss = 0.427(Ac.Ft)
Total rainfall = 1.29(In)
Flood volume = 106964.1 Cubic Feet
Total soil loss = 18594.8 Cubic Feet

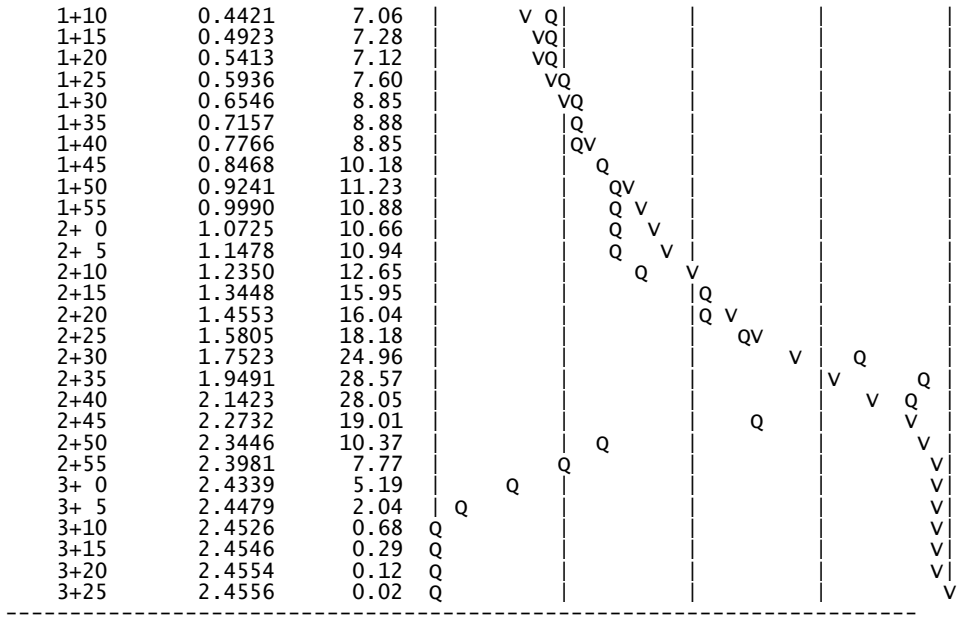
Peak flow rate of this hydrograph = 28.574(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0083	1.20	VQ				
0+10	0.0286	2.95	V Q				
0+15	0.0500	3.10	V Q				
0+20	0.0736	3.43	V Q				
0+25	0.1027	4.22	V Q				
0+30	0.1360	4.83	V Q				
0+35	0.1710	5.08	V Q				
0+40	0.2059	5.07	V Q				
0+45	0.2445	5.61	V Q				
0+50	0.2811	5.31	V Q				
0+55	0.3148	4.90	VQ				
1+ 0	0.3509	5.24	VQ				
1+ 5	0.3935	6.18	V Q				



1+10	0.4421	7.06	V Q
1+15	0.4923	7.28	VQ
1+20	0.5413	7.12	VQ
1+25	0.5936	7.60	VQ
1+30	0.6546	8.85	VQ
1+35	0.7157	8.88	Q
1+40	0.7766	8.85	QV
1+45	0.8468	10.18	Q
1+50	0.9241	11.23	QV
1+55	0.9990	10.88	Q V
2+ 0	1.0725	10.66	Q V
2+ 5	1.1478	10.94	Q V
2+10	1.2350	12.65	Q V
2+15	1.3448	15.95	Q
2+20	1.4553	16.04	Q V
2+25	1.5805	18.18	QV
2+30	1.7523	24.96	V Q
2+35	1.9491	28.57	V Q
2+40	2.1423	28.05	V Q
2+45	2.2732	19.01	Q V
2+50	2.3446	10.37	Q V
2+55	2.3981	7.77	Q V
3+ 0	2.4339	5.19	Q V
3+ 5	2.4479	2.04	Q V
3+10	2.4526	0.68	Q V
3+15	2.4546	0.29	Q V
3+20	2.4554	0.12	Q V
3+25	2.4556	0.02	Q V

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro110610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.10	29.41

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	3.00	80.22

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.882(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.882(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.500	0.064	1.000	0.064
					Sum (F) =	0.064

Area averaged mean soil loss (F) (In/Hr) = 0.064
Minimum soil loss rate ((In/Hr)) = 0.032
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.113	(0.064)	0.056	0.056
2	0.17	0.60	0.135	0.064	(0.068)	0.071
3	0.25	0.60	0.135	0.064	(0.068)	0.071
4	0.33	0.60	0.135	0.064	(0.068)	0.071
5	0.42	0.60	0.135	0.064	(0.068)	0.071
6	0.50	0.70	0.158	0.064	(0.079)	0.094
7	0.58	0.70	0.158	0.064	(0.079)	0.094
8	0.67	0.70	0.158	0.064	(0.079)	0.094
9	0.75	0.70	0.158	0.064	(0.079)	0.094
10	0.83	0.70	0.158	0.064	(0.079)	0.094
11	0.92	0.70	0.158	0.064	(0.079)	0.094
12	1.00	0.80	0.181	0.064	(0.090)	0.116
13	1.08	0.80	0.181	0.064	(0.090)	0.116
14	1.17	0.80	0.181	0.064	(0.090)	0.116
15	1.25	0.80	0.181	0.064	(0.090)	0.116
16	1.33	0.80	0.181	0.064	(0.090)	0.116
17	1.42	0.80	0.181	0.064	(0.090)	0.116
18	1.50	0.80	0.181	0.064	(0.090)	0.116
19	1.58	0.80	0.181	0.064	(0.090)	0.116
20	1.67	0.80	0.181	0.064	(0.090)	0.116
21	1.75	0.80	0.181	0.064	(0.090)	0.116
22	1.83	0.80	0.181	0.064	(0.090)	0.116
23	1.92	0.80	0.181	0.064	(0.090)	0.116
24	2.00	0.90	0.203	0.064	(0.102)	0.139
25	2.08	0.80	0.181	0.064	(0.090)	0.116
26	2.17	0.90	0.203	0.064	(0.102)	0.139
27	2.25	0.90	0.203	0.064	(0.102)	0.139
28	2.33	0.90	0.203	0.064	(0.102)	0.139
29	2.42	0.90	0.203	0.064	(0.102)	0.139
30	2.50	0.90	0.203	0.064	(0.102)	0.139
31	2.58	0.90	0.203	0.064	(0.102)	0.139
32	2.67	0.90	0.203	0.064	(0.102)	0.139
33	2.75	1.00	0.226	0.064	(0.113)	0.161
34	2.83	1.00	0.226	0.064	(0.113)	0.161
35	2.92	1.00	0.226	0.064	(0.113)	0.161
36	3.00	1.00	0.226	0.064	(0.113)	0.161
37	3.08	1.00	0.226	0.064	(0.113)	0.161
38	3.17	1.10	0.248	0.064	(0.124)	0.184
39	3.25	1.10	0.248	0.064	(0.124)	0.184
40	3.33	1.10	0.248	0.064	(0.124)	0.184
41	3.42	1.20	0.271	0.064	(0.135)	0.207
42	3.50	1.30	0.294	0.064	(0.147)	0.229
43	3.58	1.40	0.316	0.064	(0.158)	0.252
44	3.67	1.40	0.316	0.064	(0.158)	0.252
45	3.75	1.50	0.339	0.064	(0.169)	0.274
46	3.83	1.50	0.339	0.064	(0.169)	0.274
47	3.92	1.60	0.361	0.064	(0.181)	0.297
48	4.00	1.60	0.361	0.064	(0.181)	0.297
49	4.08	1.70	0.384	0.064	(0.192)	0.319
50	4.17	1.80	0.406	0.064	(0.203)	0.342
51	4.25	1.90	0.429	0.064	(0.214)	0.365
52	4.33	2.00	0.452	0.064	(0.226)	0.387
53	4.42	2.10	0.474	0.064	(0.237)	0.410
54	4.50	2.10	0.474	0.064	(0.237)	0.410
55	4.58	2.20	0.497	0.064	(0.248)	0.432
56	4.67	2.30	0.519	0.064	(0.260)	0.455
57	4.75	2.40	0.542	0.064	(0.271)	0.478
58	4.83	2.40	0.542	0.064	(0.271)	0.478
59	4.92	2.50	0.564	0.064	(0.282)	0.500
60	5.00	2.60	0.587	0.064	(0.294)	0.523
61	5.08	3.10	0.700	0.064	(0.350)	0.636
62	5.17	3.60	0.813	0.064	(0.406)	0.748
63	5.25	3.90	0.881	0.064	(0.440)	0.816
64	5.33	4.20	0.948	0.064	(0.474)	0.884
65	5.42	4.70	1.061	0.064	(0.531)	0.997
66	5.50	5.60	1.264	0.064	(0.632)	1.200
67	5.58	1.90	0.429	0.064	(0.214)	0.365
68	5.67	0.90	0.203	0.064	(0.102)	0.139
69	5.75	0.60	0.135	0.064	(0.068)	0.071
70	5.83	0.50	0.113	(0.064)	0.056	0.056

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71   5.92     0.30      0.068       (  0.064)       0.034        0.034
72   6.00     0.20      0.045       (  0.064)       0.023        0.023
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =    18.0
      Flood volume = Effective rainfall      1.50(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       3.3(Ac.Ft)
      Total soil loss =      0.38(In)
      Total soil loss =     0.844(Ac.Ft)
      Total rainfall =      1.88(In)
      Flood volume =      145865.4 Cubic Feet
      Total soil loss =       36764.9 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     27.752(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        7.5      15.0      22.5      30.0
-------------------------------------------------------------------------
  0+ 5       0.0034      0.49  Q         |          |          |          |
  0+10       0.0126      1.34  VQ        |          |          |          |
  0+15       0.0243      1.70  V Q       |          |          |          |
  0+20       0.0369      1.82  V Q       |          |          |          |
  0+25       0.0498      1.88  V Q       |          |          |          |
  0+30       0.0644      2.11  V Q       |          |          |          |
  0+35       0.0809      2.40  V  Q      |          |          |          |
  0+40       0.0979      2.47  |V Q      |          |          |          |
  0+45       0.1151      2.50  |V Q      |          |          |          |
  0+50       0.1325      2.52  |V Q      |          |          |          |
  0+55       0.1499      2.53  |V Q      |          |          |          |
  1+ 0       0.1686      2.72  | VQ      |          |          |          |
  1+ 5       0.1894      3.01  | V Q     |          |          |          |
  1+10       0.2106      3.08  | V Q     |          |          |          |
  1+15       0.2320      3.11  | V Q     |          |          |          |
  1+20       0.2536      3.13  |  VQ     |          |          |          |
  1+25       0.2751      3.14  |  VQ     |          |          |          |
  1+30       0.2967      3.14  |  VQ     |          |          |          |
  1+35       0.3183      3.14  |  VQ     |          |          |          |
  1+40       0.3399      3.14  |   Q     |          |          |          |
  1+45       0.3615      3.14  |   Q     |          |          |          |
  1+50       0.3831      3.14  |   Q     |          |          |          |
  1+55       0.4047      3.14  |   Q     |          |          |          |
  2+ 0       0.4276      3.33  |   QV    |          |          |          |
  2+ 5       0.4512      3.42  |   QV    |          |          |          |
  2+10       0.4746      3.40  |   QV    |          |          |          |
  2+15       0.4998      3.65  |   QV    |          |          |          |
  2+20       0.5253      3.70  |   Q V   |          |          |          |
  2+25       0.5510      3.73  |   Q V   |          |          |          |
  2+30       0.5767      3.74  |   Q V   |          |          |          |
  2+35       0.6025      3.74  |   Q  V  |          |          |          |
  2+40       0.6283      3.74  |   Q  V  |          |          |          |
  2+45       0.6554      3.94  |    Q V  |          |          |          |
  2+50       0.6845      4.23  |    Q  V |          |          |          |
  2+55       0.7141      4.30  |    Q  V |          |          |          |
  3+ 0       0.7439      4.33  |    Q  V |          |          |          |
  3+ 5       0.7739      4.34  |    Q   V|          |          |          |
  3+10       0.8052      4.55  |     Q  V|          |          |          |
  3+15       0.8385      4.84  |     Q   V          |          |          |
  3+20       0.8723      4.91  |     Q   V          |          |          |
  3+25       0.9077      5.13  |     Q   V          |          |          |
  3+30       0.9465      5.63  |      Q  |V         |          |          |
  3+35       0.9891      6.20  |       Q |V         |          |          |
  3+40       1.0345      6.58  |       Q | V        |          |          |
  3+45       1.0820      6.90  |        Q| V        |          |          |
  3+50       1.1319      7.24  |        Q|  V       |          |          |
  3+55       1.1837      7.53  |         Q   V      |          |          |
  4+ 0       1.2378      7.86  |         Q   V      |          |          |
  4+ 5       1.2939      8.14  |         Q    V     |          |          |
  4+10       1.3535      8.66  |         |Q    V    |          |          |
  4+15       1.4171      9.23  |         | Q   V    |          |          |
  4+20       1.4848      9.83  |         |  Q   V   |          |          |
  4+25       1.5566     10.43  |         |  Q    V  |          |          |
  4+30       1.6312     10.84  |         |   Q    V|          |          |
  4+35       1.7081     11.16  |         |   Q     V          |          |
  4+40       1.7887     11.70  |         |    Q    |V         |          |
  4+45       1.8732     12.28  |         |     Q   | V        |          |
  4+50       1.9605     12.67  |         |     Q   |  V       |          |
  4+55       2.0499     12.98  |         |      Q  |   V      |          |
  5+ 0       2.1430     13.52  |         |       Q |    V     |          |
  5+ 5       2.2456     14.89  |         |         Q|     V   |          |
  5+10       2.3656     17.42  |         |          |  Q    V |          |
  5+15       2.5023     19.85  |         |          |     Q  V|          |
```

```
    5+20       2.6526     21.82  |          |          |        Q|V         |
    5+25       2.8187     24.12  |          |          |         | QV       |
    5+30       3.0098     27.75  |          |          |         |    V Q   |
    5+35       3.1721     23.57  |          |          |         |Q     V   |
    5+40       3.2534     11.80  |          |    Q     |         |       V  |
    5+45       3.2958      6.15  |        Q |          |         |         V|
    5+50       3.3201      3.53  |    Q     |          |         |         V|
    5+55       3.3348      2.14  | Q        |          |         |         V|
    6+ 0       3.3427      1.14  |Q         |          |         |         V|
    6+ 5       3.3466      0.57  Q          |          |         |         V|
    6+10       3.3478      0.18  Q          |          |         |         V|
    6+15       3.3483      0.08  Q          |          |         |         V|
    6+20       3.3485      0.03  Q          |          |         |         V|
    6+25       3.3486      0.01  Q          |          |         |          V
-------------------------------------------------------------------------
```

```
       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/22/24 File: pro1102410.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      26.74(Ac.)  =      0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      26.74(Ac.)  =      0.042 Sq. Mi.
Length along longest watercourse =    2399.00(Ft.)
Length along longest watercourse measured to centroid =    1200.00(Ft.)
Length along longest watercourse =      0.454 Mi.
Length along longest watercourse measured to centroid =      0.227 Mi.
Difference in elevation =      81.00(Ft.)
Slope along watercourse =    178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.057 Hr.
Lag time =     3.40 Min.
25% of lag time =     0.85 Min.
40% of lag time =     1.36 Min.
Unit time =     5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           1.80                 48.13

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           5.00                133.70

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    1.800(In)
Area Averaged 100-Year Rainfall =    5.000(In)

Point rain (area averaged) =    3.117(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    3.116(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    26.740           91.00         0.500
 Total Area Entered =     26.74(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  91.0      0.117     0.500        0.064       1.000      0.064
                                                 Sum (F) =   0.064
Area averaged mean soil loss (F) (In/Hr) =  0.064
Minimum soil loss rate ((In/Hr)) =  0.032
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
			Sum = 100.000 Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.025	(0.114)	0.012	0.012
2	0.17	0.07	0.025	(0.114)	0.012	0.012
3	0.25	0.07	0.025	(0.113)	0.012	0.012
4	0.33	0.10	0.037	(0.113)	0.019	0.019
5	0.42	0.10	0.037	(0.112)	0.019	0.019
6	0.50	0.10	0.037	(0.112)	0.019	0.019
7	0.58	0.10	0.037	(0.111)	0.019	0.019
8	0.67	0.10	0.037	(0.111)	0.019	0.019
9	0.75	0.10	0.037	(0.111)	0.019	0.019
10	0.83	0.13	0.050	(0.110)	0.025	0.025
11	0.92	0.13	0.050	(0.110)	0.025	0.025
12	1.00	0.13	0.050	(0.109)	0.025	0.025
13	1.08	0.10	0.037	(0.109)	0.019	0.019
14	1.17	0.10	0.037	(0.108)	0.019	0.019
15	1.25	0.10	0.037	(0.108)	0.019	0.019
16	1.33	0.10	0.037	(0.108)	0.019	0.019
17	1.42	0.10	0.037	(0.107)	0.019	0.019
18	1.50	0.10	0.037	(0.107)	0.019	0.019
19	1.58	0.10	0.037	(0.106)	0.019	0.019
20	1.67	0.10	0.037	(0.106)	0.019	0.019
21	1.75	0.10	0.037	(0.105)	0.019	0.019
22	1.83	0.13	0.050	(0.105)	0.025	0.025
23	1.92	0.13	0.050	(0.105)	0.025	0.025
24	2.00	0.13	0.050	(0.104)	0.025	0.025
25	2.08	0.13	0.050	(0.104)	0.025	0.025
26	2.17	0.13	0.050	(0.103)	0.025	0.025
27	2.25	0.13	0.050	(0.103)	0.025	0.025
28	2.33	0.13	0.050	(0.102)	0.025	0.025
29	2.42	0.13	0.050	(0.102)	0.025	0.025
30	2.50	0.13	0.050	(0.102)	0.025	0.025
31	2.58	0.17	0.062	(0.101)	0.031	0.031
32	2.67	0.17	0.062	(0.101)	0.031	0.031
33	2.75	0.17	0.062	(0.100)	0.031	0.031
34	2.83	0.17	0.062	(0.100)	0.031	0.031
35	2.92	0.17	0.062	(0.100)	0.031	0.031
36	3.00	0.17	0.062	(0.099)	0.031	0.031
37	3.08	0.17	0.062	(0.099)	0.031	0.031
38	3.17	0.17	0.062	(0.098)	0.031	0.031
39	3.25	0.17	0.062	(0.098)	0.031	0.031
40	3.33	0.17	0.062	(0.098)	0.031	0.031
41	3.42	0.17	0.062	(0.097)	0.031	0.031
42	3.50	0.17	0.062	(0.097)	0.031	0.031
43	3.58	0.17	0.062	(0.096)	0.031	0.031
44	3.67	0.17	0.062	(0.096)	0.031	0.031
45	3.75	0.17	0.062	(0.095)	0.031	0.031
46	3.83	0.20	0.075	(0.095)	0.037	0.037
47	3.92	0.20	0.075	(0.095)	0.037	0.037
48	4.00	0.20	0.075	(0.094)	0.037	0.037
49	4.08	0.20	0.075	(0.094)	0.037	0.037
50	4.17	0.20	0.075	(0.093)	0.037	0.037
51	4.25	0.20	0.075	(0.093)	0.037	0.037
52	4.33	0.23	0.087	(0.093)	0.044	0.044
53	4.42	0.23	0.087	(0.092)	0.044	0.044
54	4.50	0.23	0.087	(0.092)	0.044	0.044
55	4.58	0.23	0.087	(0.092)	0.044	0.044
56	4.67	0.23	0.087	(0.091)	0.044	0.044
57	4.75	0.23	0.087	(0.091)	0.044	0.044
58	4.83	0.27	0.100	(0.090)	0.050	0.050
59	4.92	0.27	0.100	(0.090)	0.050	0.050
60	5.00	0.27	0.100	(0.090)	0.050	0.050
61	5.08	0.20	0.075	(0.089)	0.037	0.037
62	5.17	0.20	0.075	(0.089)	0.037	0.037
63	5.25	0.20	0.075	(0.088)	0.037	0.037
64	5.33	0.23	0.087	(0.088)	0.044	0.044
65	5.42	0.23	0.087	(0.088)	0.044	0.044
66	5.50	0.23	0.087	(0.087)	0.044	0.044
67	5.58	0.27	0.100	(0.087)	0.050	0.050
68	5.67	0.27	0.100	(0.086)	0.050	0.050
69	5.75	0.27	0.100	(0.086)	0.050	0.050
70	5.83	0.27	0.100	(0.086)	0.050	0.050

71	5.92	0.27	0.100	(	0.085)	0.050	0.050
72	6.00	0.27	0.100	(	0.085)	0.050	0.050
73	6.08	0.30	0.112	(	0.085)	0.056	0.056
74	6.17	0.30	0.112	(	0.084)	0.056	0.056
75	6.25	0.30	0.112	(	0.084)	0.056	0.056
76	6.33	0.30	0.112	(	0.083)	0.056	0.056
77	6.42	0.30	0.112	(	0.083)	0.056	0.056
78	6.50	0.30	0.112	(	0.083)	0.056	0.056
79	6.58	0.33	0.125	(	0.082)	0.062	0.062
80	6.67	0.33	0.125	(	0.082)	0.062	0.062
81	6.75	0.33	0.125	(	0.082)	0.062	0.062
82	6.83	0.33	0.125	(	0.081)	0.062	0.062
83	6.92	0.33	0.125	(	0.081)	0.062	0.062
84	7.00	0.33	0.125	(	0.080)	0.062	0.062
85	7.08	0.33	0.125	(	0.080)	0.062	0.062
86	7.17	0.33	0.125	(	0.080)	0.062	0.062
87	7.25	0.33	0.125	(	0.079)	0.062	0.062
88	7.33	0.37	0.137	(	0.079)	0.069	0.069
89	7.42	0.37	0.137	(	0.079)	0.069	0.069
90	7.50	0.37	0.137	(	0.078)	0.069	0.069
91	7.58	0.40	0.150	(	0.078)	0.075	0.075
92	7.67	0.40	0.150	(	0.078)	0.075	0.075
93	7.75	0.40	0.150	(	0.077)	0.075	0.075
94	7.83	0.43	0.162		0.077	(0.081)	0.085
95	7.92	0.43	0.162		0.077	(0.081)	0.086
96	8.00	0.43	0.162		0.076	(0.081)	0.086
97	8.08	0.50	0.187		0.076	(0.093)	0.111
98	8.17	0.50	0.187		0.075	(0.093)	0.112
99	8.25	0.50	0.187		0.075	(0.093)	0.112
100	8.33	0.50	0.187		0.075	(0.093)	0.112
101	8.42	0.50	0.187		0.074	(0.093)	0.113
102	8.50	0.50	0.187		0.074	(0.093)	0.113
103	8.58	0.53	0.199		0.074	(0.100)	0.126
104	8.67	0.53	0.199		0.073	(0.100)	0.126
105	8.75	0.53	0.199		0.073	(0.100)	0.126
106	8.83	0.57	0.212		0.073	(0.106)	0.139
107	8.92	0.57	0.212		0.072	(0.106)	0.140
108	9.00	0.57	0.212		0.072	(0.106)	0.140
109	9.08	0.63	0.237		0.072	(0.118)	0.165
110	9.17	0.63	0.237		0.071	(0.118)	0.166
111	9.25	0.63	0.237		0.071	(0.118)	0.166
112	9.33	0.67	0.249		0.071	(0.125)	0.179
113	9.42	0.67	0.249		0.070	(0.125)	0.179
114	9.50	0.67	0.249		0.070	(0.125)	0.179
115	9.58	0.70	0.262		0.070	(0.131)	0.192
116	9.67	0.70	0.262		0.069	(0.131)	0.192
117	9.75	0.70	0.262		0.069	(0.131)	0.193
118	9.83	0.73	0.274		0.069	(0.137)	0.206
119	9.92	0.73	0.274		0.068	(0.137)	0.206
120	10.00	0.73	0.274		0.068	(0.137)	0.206
121	10.08	0.50	0.187		0.068	(0.093)	0.119
122	10.17	0.50	0.187		0.067	(0.093)	0.120
123	10.25	0.50	0.187		0.067	(0.093)	0.120
124	10.33	0.50	0.187		0.067	(0.093)	0.120
125	10.42	0.50	0.187		0.066	(0.093)	0.121
126	10.50	0.50	0.187		0.066	(0.093)	0.121
127	10.58	0.67	0.249		0.066	(0.125)	0.184
128	10.67	0.67	0.249		0.065	(0.125)	0.184
129	10.75	0.67	0.249		0.065	(0.125)	0.184
130	10.83	0.67	0.249		0.065	(0.125)	0.185
131	10.92	0.67	0.249		0.064	(0.125)	0.185
132	11.00	0.67	0.249		0.064	(0.125)	0.185
133	11.08	0.63	0.237		0.064	(0.118)	0.173
134	11.17	0.63	0.237		0.063	(0.118)	0.173
135	11.25	0.63	0.237		0.063	(0.118)	0.174
136	11.33	0.63	0.237		0.063	(0.118)	0.174
137	11.42	0.63	0.237		0.063	(0.118)	0.174
138	11.50	0.63	0.237		0.062	(0.118)	0.175
139	11.58	0.57	0.212		0.062	(0.106)	0.150
140	11.67	0.57	0.212		0.062	(0.106)	0.150
141	11.75	0.57	0.212		0.061	(0.106)	0.151
142	11.83	0.60	0.224		0.061	(0.112)	0.163
143	11.92	0.60	0.224		0.061	(0.112)	0.164
144	12.00	0.60	0.224		0.060	(0.112)	0.164
145	12.08	0.83	0.312		0.060	(0.156)	0.252
146	12.17	0.83	0.312		0.060	(0.156)	0.252
147	12.25	0.83	0.312		0.059	(0.156)	0.252
148	12.33	0.87	0.324		0.059	(0.162)	0.265
149	12.42	0.87	0.324		0.059	(0.162)	0.265
150	12.50	0.87	0.324		0.059	(0.162)	0.266
151	12.58	0.93	0.349		0.058	(0.175)	0.291
152	12.67	0.93	0.349		0.058	(0.175)	0.291
153	12.75	0.93	0.349		0.058	(0.175)	0.291
154	12.83	0.97	0.361		0.057	(0.181)	0.304
155	12.92	0.97	0.361		0.057	(0.181)	0.304
156	13.00	0.97	0.361		0.057	(0.181)	0.305

157	13.08	1.13	0.424	0.057	(0.212)	0.367
158	13.17	1.13	0.424	0.056	(0.212)	0.368
159	13.25	1.13	0.424	0.056	(0.212)	0.368
160	13.33	1.13	0.424	0.056	(0.212)	0.368
161	13.42	1.13	0.424	0.055	(0.212)	0.368
162	13.50	1.13	0.424	0.055	(0.212)	0.369
163	13.58	0.77	0.287	0.055	(0.143)	0.232
164	13.67	0.77	0.287	0.055	(0.143)	0.232
165	13.75	0.77	0.287	0.054	(0.143)	0.232
166	13.83	0.77	0.287	0.054	(0.143)	0.233
167	13.92	0.77	0.287	0.054	(0.143)	0.233
168	14.00	0.77	0.287	0.053	(0.143)	0.233
169	14.08	0.90	0.337	0.053	(0.168)	0.283
170	14.17	0.90	0.337	0.053	(0.168)	0.284
171	14.25	0.90	0.337	0.053	(0.168)	0.284
172	14.33	0.87	0.324	0.052	(0.162)	0.272
173	14.42	0.87	0.324	0.052	(0.162)	0.272
174	14.50	0.87	0.324	0.052	(0.162)	0.272
175	14.58	0.87	0.324	0.052	(0.162)	0.273
176	14.67	0.87	0.324	0.051	(0.162)	0.273
177	14.75	0.87	0.324	0.051	(0.162)	0.273
178	14.83	0.83	0.312	0.051	(0.156)	0.261
179	14.92	0.83	0.312	0.051	(0.156)	0.261
180	15.00	0.83	0.312	0.050	(0.156)	0.261
181	15.08	0.80	0.299	0.050	(0.150)	0.249
182	15.17	0.80	0.299	0.050	(0.150)	0.249
183	15.25	0.80	0.299	0.049	(0.150)	0.250
184	15.33	0.77	0.287	0.049	(0.143)	0.237
185	15.42	0.77	0.287	0.049	(0.143)	0.238
186	15.50	0.77	0.287	0.049	(0.143)	0.238
187	15.58	0.63	0.237	0.048	(0.118)	0.188
188	15.67	0.63	0.237	0.048	(0.118)	0.189
189	15.75	0.63	0.237	0.048	(0.118)	0.189
190	15.83	0.63	0.237	0.048	(0.118)	0.189
191	15.92	0.63	0.237	0.047	(0.118)	0.189
192	16.00	0.63	0.237	0.047	(0.118)	0.190
193	16.08	0.13	0.050	(0.047)	0.025	0.025
194	16.17	0.13	0.050	(0.047)	0.025	0.025
195	16.25	0.13	0.050	(0.047)	0.025	0.025
196	16.33	0.13	0.050	(0.046)	0.025	0.025
197	16.42	0.13	0.050	(0.046)	0.025	0.025
198	16.50	0.13	0.050	(0.046)	0.025	0.025
199	16.58	0.10	0.037	(0.046)	0.019	0.019
200	16.67	0.10	0.037	(0.045)	0.019	0.019
201	16.75	0.10	0.037	(0.045)	0.019	0.019
202	16.83	0.10	0.037	(0.045)	0.019	0.019
203	16.92	0.10	0.037	(0.045)	0.019	0.019
204	17.00	0.10	0.037	(0.044)	0.019	0.019
205	17.08	0.17	0.062	(0.044)	0.031	0.031
206	17.17	0.17	0.062	(0.044)	0.031	0.031
207	17.25	0.17	0.062	(0.044)	0.031	0.031
208	17.33	0.17	0.062	(0.044)	0.031	0.031
209	17.42	0.17	0.062	(0.043)	0.031	0.031
210	17.50	0.17	0.062	(0.043)	0.031	0.031
211	17.58	0.17	0.062	(0.043)	0.031	0.031
212	17.67	0.17	0.062	(0.043)	0.031	0.031
213	17.75	0.17	0.062	(0.042)	0.031	0.031
214	17.83	0.13	0.050	(0.042)	0.025	0.025
215	17.92	0.13	0.050	(0.042)	0.025	0.025
216	18.00	0.13	0.050	(0.042)	0.025	0.025
217	18.08	0.13	0.050	(0.042)	0.025	0.025
218	18.17	0.13	0.050	(0.041)	0.025	0.025
219	18.25	0.13	0.050	(0.041)	0.025	0.025
220	18.33	0.13	0.050	(0.041)	0.025	0.025
221	18.42	0.13	0.050	(0.041)	0.025	0.025
222	18.50	0.13	0.050	(0.041)	0.025	0.025
223	18.58	0.10	0.037	(0.040)	0.019	0.019
224	18.67	0.10	0.037	(0.040)	0.019	0.019
225	18.75	0.10	0.037	(0.040)	0.019	0.019
226	18.83	0.07	0.025	(0.040)	0.012	0.012
227	18.92	0.07	0.025	(0.040)	0.012	0.012
228	19.00	0.07	0.025	(0.039)	0.012	0.012
229	19.08	0.10	0.037	(0.039)	0.019	0.019
230	19.17	0.10	0.037	(0.039)	0.019	0.019
231	19.25	0.10	0.037	(0.039)	0.019	0.019
232	19.33	0.13	0.050	(0.039)	0.025	0.025
233	19.42	0.13	0.050	(0.039)	0.025	0.025
234	19.50	0.13	0.050	(0.038)	0.025	0.025
235	19.58	0.10	0.037	(0.038)	0.019	0.019
236	19.67	0.10	0.037	(0.038)	0.019	0.019
237	19.75	0.10	0.037	(0.038)	0.019	0.019
238	19.83	0.07	0.025	(0.038)	0.012	0.012
239	19.92	0.07	0.025	(0.038)	0.012	0.012
240	20.00	0.07	0.025	(0.037)	0.012	0.012
241	20.08	0.10	0.037	(0.037)	0.019	0.019
242	20.17	0.10	0.037	(0.037)	0.019	0.019

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243  20.25     0.10      0.037       (  0.037)       0.019        0.019
244  20.33     0.10      0.037       (  0.037)       0.019        0.019
245  20.42     0.10      0.037       (  0.037)       0.019        0.019
246  20.50     0.10      0.037       (  0.036)       0.019        0.019
247  20.58     0.10      0.037       (  0.036)       0.019        0.019
248  20.67     0.10      0.037       (  0.036)       0.019        0.019
249  20.75     0.10      0.037       (  0.036)       0.019        0.019
250  20.83     0.07      0.025       (  0.036)       0.012        0.012
251  20.92     0.07      0.025       (  0.036)       0.012        0.012
252  21.00     0.07      0.025       (  0.036)       0.012        0.012
253  21.08     0.10      0.037       (  0.035)       0.019        0.019
254  21.17     0.10      0.037       (  0.035)       0.019        0.019
255  21.25     0.10      0.037       (  0.035)       0.019        0.019
256  21.33     0.07      0.025       (  0.035)       0.012        0.012
257  21.42     0.07      0.025       (  0.035)       0.012        0.012
258  21.50     0.07      0.025       (  0.035)       0.012        0.012
259  21.58     0.10      0.037       (  0.035)       0.019        0.019
260  21.67     0.10      0.037       (  0.034)       0.019        0.019
261  21.75     0.10      0.037       (  0.034)       0.019        0.019
262  21.83     0.07      0.025       (  0.034)       0.012        0.012
263  21.92     0.07      0.025       (  0.034)       0.012        0.012
264  22.00     0.07      0.025       (  0.034)       0.012        0.012
265  22.08     0.10      0.037       (  0.034)       0.019        0.019
266  22.17     0.10      0.037       (  0.034)       0.019        0.019
267  22.25     0.10      0.037       (  0.034)       0.019        0.019
268  22.33     0.07      0.025       (  0.034)       0.012        0.012
269  22.42     0.07      0.025       (  0.033)       0.012        0.012
270  22.50     0.07      0.025       (  0.033)       0.012        0.012
271  22.58     0.07      0.025       (  0.033)       0.012        0.012
272  22.67     0.07      0.025       (  0.033)       0.012        0.012
273  22.75     0.07      0.025       (  0.033)       0.012        0.012
274  22.83     0.07      0.025       (  0.033)       0.012        0.012
275  22.92     0.07      0.025       (  0.033)       0.012        0.012
276  23.00     0.07      0.025       (  0.033)       0.012        0.012
277  23.08     0.07      0.025       (  0.033)       0.012        0.012
278  23.17     0.07      0.025       (  0.033)       0.012        0.012
279  23.25     0.07      0.025       (  0.033)       0.012        0.012
280  23.33     0.07      0.025       (  0.033)       0.012        0.012
281  23.42     0.07      0.025       (  0.032)       0.012        0.012
282  23.50     0.07      0.025       (  0.032)       0.012        0.012
283  23.58     0.07      0.025       (  0.032)       0.012        0.012
284  23.67     0.07      0.025       (  0.032)       0.012        0.012
285  23.75     0.07      0.025       (  0.032)       0.012        0.012
286  23.83     0.07      0.025       (  0.032)       0.012        0.012
287  23.92     0.07      0.025       (  0.032)       0.012        0.012
288  24.00     0.07      0.025       (  0.032)       0.012        0.012
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    26.0
      Flood volume = Effective rainfall      2.16(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       4.8(Ac.Ft)
      Total soil loss =      0.95(In)
      Total soil loss =     2.124(Ac.Ft)
      Total rainfall =      3.12(In)
      Flood volume =      209968.5 Cubic Feet
      Total soil loss =       92523.1 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      9.934(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0008      0.11  Q          |         |         |         |
   0+10       0.0026      0.27  VQ         |         |         |         |
   0+15       0.0047      0.31  VQ         |         |         |         |
   0+20       0.0073      0.38  VQ         |         |         |         |
   0+25       0.0105      0.47  VQ         |         |         |         |
   0+30       0.0139      0.49  VQ         |         |         |         |
   0+35       0.0173      0.50  VQ         |         |         |         |
   0+40       0.0207      0.50  V Q        |         |         |         |
   0+45       0.0242      0.50  V Q        |         |         |         |
   0+50       0.0281      0.56  V Q        |         |         |         |
   0+55       0.0325      0.64  V Q        |         |         |         |
   1+ 0       0.0370      0.66  V Q        |         |         |         |
   1+ 5       0.0412      0.61  V Q        |         |         |         |
   1+10       0.0449      0.54  V Q        |         |         |         |
   1+15       0.0485      0.52  V Q        |         |         |         |
   1+20       0.0520      0.51  V Q        |         |         |         |
   1+25       0.0555      0.51  V Q        |         |         |         |
   1+30       0.0589      0.50  V Q        |         |         |         |
   1+35       0.0624      0.50  V Q        |         |         |         |
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1+40      0.0659      0.50  V Q       |         |         |         |
1+45      0.0694      0.50  V Q       |         |         |         |
1+50      0.0732      0.56  V Q       |         |         |         |
1+55      0.0776      0.64  V Q       |         |         |         |
2+ 0      0.0821      0.66  V Q       |         |         |         |
2+ 5      0.0867      0.67  V Q       |         |         |         |
2+10      0.0913      0.67  V Q       |         |         |         |
2+15      0.0960      0.67  V Q       |         |         |         |
2+20      0.1006      0.67  V Q       |         |         |         |
2+25      0.1052      0.67  V Q       |         |         |         |
2+30      0.1098      0.67  V Q       |         |         |         |
2+35      0.1148      0.73  V Q       |         |         |         |
2+40      0.1204      0.81  V  Q      |         |         |         |
2+45      0.1261      0.83  |V Q      |         |         |         |
2+50      0.1318      0.83  |V Q      |         |         |         |
2+55      0.1376      0.84  |V Q      |         |         |         |
3+ 0      0.1434      0.84  |V Q      |         |         |         |
3+ 5      0.1492      0.84  |V Q      |         |         |         |
3+10      0.1550      0.84  |V Q      |         |         |         |
3+15      0.1607      0.84  |V Q      |         |         |         |
3+20      0.1665      0.84  |V Q      |         |         |         |
3+25      0.1723      0.84  |V Q      |         |         |         |
3+30      0.1781      0.84  |V Q      |         |         |         |
3+35      0.1839      0.84  |V Q      |         |         |         |
3+40      0.1897      0.84  |V Q      |         |         |         |
3+45      0.1955      0.84  |V Q      |         |         |         |
3+50      0.2016      0.89  |V Q      |         |         |         |
3+55      0.2083      0.97  |V Q      |         |         |         |
4+ 0      0.2152      0.99  |V Q      |         |         |         |
4+ 5      0.2221      1.00  |V  Q     |         |         |         |
4+10      0.2290      1.01  |V  Q     |         |         |         |
4+15      0.2359      1.01  |V  Q     |         |         |         |
4+20      0.2433      1.06  | V Q     |         |         |         |
4+25      0.2511      1.14  | V Q     |         |         |         |
4+30      0.2591      1.16  | V Q     |         |         |         |
4+35      0.2672      1.17  | V Q     |         |         |         |
4+40      0.2753      1.17  | V Q     |         |         |         |
4+45      0.2834      1.18  | V Q     |         |         |         |
4+50      0.2918      1.23  | V Q     |         |         |         |
4+55      0.3009      1.31  | V  Q    |         |         |         |
5+ 0      0.3100      1.33  | V  Q    |         |         |         |
5+ 5      0.3185      1.23  | V Q     |         |         |         |
5+10      0.3259      1.07  | V Q     |         |         |         |
5+15      0.3330      1.04  | V Q     |         |         |         |
5+20      0.3404      1.08  | V Q     |         |         |         |
5+25      0.3483      1.15  | V Q     |         |         |         |
5+30      0.3563      1.16  | V Q     |         |         |         |
5+35      0.3648      1.22  |  VQ     |         |         |         |
5+40      0.3738      1.31  |  V Q    |         |         |         |
5+45      0.3829      1.33  |  V Q    |         |         |         |
5+50      0.3921      1.34  |  V Q    |         |         |         |
5+55      0.4014      1.34  |  V Q    |         |         |         |
6+ 0      0.4106      1.34  |  V Q    |         |         |         |
6+ 5      0.4203      1.40  |  V Q    |         |         |         |
6+10      0.4305      1.48  |  V Q    |         |         |         |
6+15      0.4408      1.50  |  V Q    |         |         |         |
6+20      0.4511      1.51  |  V  Q   |         |         |         |
6+25      0.4615      1.51  |  V  Q   |         |         |         |
6+30      0.4720      1.51  |  V  Q   |         |         |         |
6+35      0.4828      1.57  |   V Q   |         |         |         |
6+40      0.4941      1.65  |   V Q   |         |         |         |
6+45      0.5056      1.67  |   V Q   |         |         |         |
6+50      0.5171      1.67  |   V Q   |         |         |         |
6+55      0.5286      1.68  |   V Q   |         |         |         |
7+ 0      0.5402      1.68  |   V Q   |         |         |         |
7+ 5      0.5518      1.68  |   V Q   |         |         |         |
7+10      0.5634      1.68  |   V Q   |         |         |         |
7+15      0.5749      1.68  |   V Q   |         |         |         |
7+20      0.5869      1.73  |   V Q   |         |         |         |
7+25      0.5994      1.81  |   V  Q  |         |         |         |
7+30      0.6120      1.83  |    V Q  |         |         |         |
7+35      0.6251      1.90  |    V Q  |         |         |         |
7+40      0.6387      1.98  |    V Q  |         |         |         |
7+45      0.6525      2.00  |    V  Q |         |         |         |
7+50      0.6670      2.10  |    V  Q |         |         |         |
7+55      0.6824      2.24  |    V  Q |         |         |         |
8+ 0      0.6981      2.28  |    V   Q|         |         |         |
8+ 5      0.7155      2.52  |    V    Q         |         |         |
8+10      0.7352      2.86  |     V   |Q        |         |         |
8+15      0.7555      2.95  |     V   |Q        |         |         |
8+20      0.7760      2.99  |     V   |Q        |         |         |
8+25      0.7968      3.02  |     V   | Q       |         |         |
8+30      0.8177      3.04  |     V   | Q       |         |         |
8+35      0.8394      3.15  |     V   | Q       |         |         |
8+40      0.8623      3.32  |      V  |  Q      |         |         |
8+45      0.8855      3.37  |      V  |  Q      |         |         |
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 8+50       0.9097      3.50  |       V   |    Q      |           |           |
 8+55       0.9350      3.68  |       V   |    Q      |           |           |
 9+ 0       0.9607      3.73  |       V   |    Q      |           |           |
 9+ 5       0.9881      3.98  |        V  |     Q     |           |           |
 9+10       1.0178      4.31  |        V  |       Q   |           |           |
 9+15       1.0481      4.40  |        V  |        Q  |           |           |
 9+20       1.0795      4.55  |        V  |         Q |           |           |
 9+25       1.1121      4.74  |         V |         Q |           |           |
 9+30       1.1452      4.80  |         V |          Q|           |           |
 9+35       1.1791      4.93  |         V |          Q|           |           |
 9+40       1.2143      5.11  |          V|           Q           |           |
 9+45       1.2498      5.16  |          V|           Q           |           |
 9+50       1.2863      5.29  |          V|            Q          |           |
 9+55       1.3240      5.47  |          V|            Q          |           |
10+ 0       1.3620      5.52  |           V            | Q        |           |
10+ 5       1.3950      4.79  |           V|          Q|           |           |
10+10       1.4204      3.69  |           V| Q        |           |           |
10+15       1.4441      3.44  |           V Q         |           |           |
10+20       1.4670      3.33  |            VQ         |           |           |
10+25       1.4896      3.28  |            VQ         |           |           |
10+30       1.5120      3.25  |            VQ         |           |           |
10+35       1.5382      3.81  |            V  Q       |           |           |
10+40       1.5700      4.61  |             V    Q    |           |           |
10+45       1.6031      4.81  |             V     Q|  |           |           |
10+50       1.6368      4.90  |             V     Q|  |           |           |
10+55       1.6709      4.95  |             V     Q|  |           |           |
11+ 0       1.7053      4.99  |              V    Q|  |           |           |
11+ 5       1.7389      4.89  |              V    Q|  |           |           |
11+10       1.7715      4.73  |              V   Q |  |           |           |
11+15       1.8039      4.71  |              V   Q |  |           |           |
11+20       1.8363      4.70  |               V  Q |  |           |           |
11+25       1.8686      4.70  |               V  Q |  |           |           |
11+30       1.9010      4.70  |               V  Q |  |           |           |
11+35       1.9319      4.49  |                VQ  |  |           |           |
11+40       1.9607      4.18  |                Q   |  |           |           |
11+45       1.9890      4.11  |                Q   |  |           |           |
11+50       2.0179      4.20  |                Q   |  |           |           |
11+55       2.0479      4.35  |                VQ  |  |           |           |
12+ 0       2.0781      4.38  |                 Q  |  |           |           |
12+ 5       2.1137      5.17  |                 V  Q  |           |           |
12+10       2.1571      6.30  |                 V  |     Q     |           |
12+15       2.2024      6.58  |                  V |      Q    |           |
12+20       2.2493      6.81  |                  V |       Q   |           |
12+25       2.2978      7.04  |                   V|        Q  |           |
12+30       2.3468      7.12  |                   V|        Q  |           |
12+35       2.3975      7.36  |                   V|         Q |           |
12+40       2.4506      7.70  |                    V          Q|           |
12+45       2.5042      7.79  |                    V           |Q          |
12+50       2.5589      7.94  |                    |V          |Q          |
12+55       2.6148      8.12  |                    |V          | Q         |
13+ 0       2.6711      8.18  |                    | V         | Q         |
13+ 5       2.7313      8.75  |                    | V         |    Q      |
13+10       2.7971      9.56  |                    |  V        |       Q   |
13+15       2.8643      9.76  |                    |  V        |         Q |
13+20       2.9322      9.85  |                    |   V       |         Q |
13+25       3.0004      9.90  |                    |   V       |         Q |
13+30       3.0688      9.93  |                    |    V      |         Q |
13+35       3.1290      8.74  |                    |    V      |    Q      |
13+40       3.1773      7.00  |                    |     V Q   |           |
13+45       3.2226      6.59  |                    |     Q     |           |
13+50       3.2668      6.41  |                    |    Q V    |           |
13+55       3.3104      6.33  |                    |    Q V    |           |
14+ 0       3.3537      6.28  |                    |    Q V    |           |
14+ 5       3.4000      6.72  |                    |     Q V   |           |
14+10       3.4507      7.37  |                    |       VQ  |           |
14+15       3.5026      7.53  |                    |         VQ|           |
14+20       3.5542      7.49  |                    |         Q |           |
14+25       3.6050      7.38  |                    |         Q |           |
14+30       3.6557      7.36  |                    |         QV|           |
14+35       3.7063      7.35  |                    |         QV|           |
14+40       3.7570      7.35  |                    |         Q |V          |
14+45       3.8076      7.36  |                    |         Q |V          |
14+50       3.8576      7.25  |                    |         Q |  V        |
14+55       3.9065      7.10  |                    |        Q  |  V        |
15+ 0       3.9552      7.07  |                    |        Q  |  V        |
15+ 5       4.0030      6.95  |                    |       Q   |   V       |
15+10       4.0498      6.79  |                    |       Q   |   V       |
15+15       4.0963      6.76  |                    |       Q   |   V       |
15+20       4.1420      6.64  |                    |      Q    |    V      |
15+25       4.1866      6.48  |                    |    Q      |    V      |
15+30       4.2310      6.44  |                    |    Q      |     V     |
15+35       4.2723      5.99  |                    |  Q        |     V     |
15+40       4.3092      5.36  |                    |Q          |     V     |
15+45       4.3450      5.21  |                    Q           |      V    |
15+50       4.3805      5.15  |                    Q           |      V    |
15+55       4.4157      5.12  |                    Q           |      V    |
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16+ 0       4.4509      5.11  |          |          Q          |      V    |
16+ 5       4.4761      3.67  |          |     Q     |         |       V   |
16+10       4.4870      1.57  |          |        Q  |         |       V   |
16+15       4.4944      1.07  |          |     Q     |         |       V   |
16+20       4.5002      0.85  |          |   Q       |         |       V   |
16+25       4.5053      0.74  |          | Q         |         |       V   |
16+30       4.5099      0.67  |          | Q         |         |       V   |
16+35       4.5142      0.62  |          | Q         |         |       V   |
16+40       4.5179      0.54  |          | Q         |         |       V   |
16+45       4.5215      0.52  |          | Q         |         |       V   |
16+50       4.5250      0.51  |          | Q         |         |       V   |
16+55       4.5285      0.51  |          | Q         |         |       V   |
17+ 0       4.5319      0.50  |          | Q         |         |       V   |
17+ 5       4.5362      0.61  |          | Q         |         |       V   |
17+10       4.5415      0.77  |          |   Q       |         |       V   |
17+15       4.5471      0.81  |          |   Q       |         |       V   |
17+20       4.5528      0.83  |          |   Q       |         |       V   |
17+25       4.5585      0.84  |          |   Q       |         |       V   |
17+30       4.5643      0.84  |          |   Q       |         |       V   |
17+35       4.5701      0.84  |          |   Q       |         |       V   |
17+40       4.5759      0.84  |          |   Q       |         |       V   |
17+45       4.5817      0.84  |          |   Q       |         |        V  |
17+50       4.5871      0.79  |          |   Q       |         |        V  |
17+55       4.5919      0.71  |          | Q         |         |        V  |
18+ 0       4.5967      0.69  |          | Q         |         |        V  |
18+ 5       4.6013      0.68  |          | Q         |         |        V  |
18+10       4.6060      0.67  |          | Q         |         |        V  |
18+15       4.6106      0.67  |          | Q         |         |        V  |
18+20       4.6152      0.67  |          | Q         |         |        V  |
18+25       4.6199      0.67  |          | Q         |         |        V  |
18+30       4.6245      0.67  |          | Q         |         |        V  |
18+35       4.6288      0.62  |          | Q         |         |        V  |
18+40       4.6325      0.54  |          | Q         |         |        V  |
18+45       4.6360      0.52  |          | Q         |         |        V  |
18+50       4.6392      0.46  |Q         |           |         |        V  |
18+55       4.6418      0.37  |Q         |           |         |        V  |
19+ 0       4.6442      0.35  |Q         |           |         |        V  |
19+ 5       4.6469      0.40  |Q         |           |         |        V  |
19+10       4.6502      0.47  |Q         |           |         |        V  |
19+15       4.6535      0.49  |Q         |           |         |        V  |
19+20       4.6573      0.55  | Q        |           |         |        V  |
19+25       4.6617      0.64  | Q        |           |         |        V  |
19+30       4.6662      0.66  | Q        |           |         |        V  |
19+35       4.6704      0.61  | Q        |           |         |        V  |
19+40       4.6741      0.54  | Q        |           |         |        V  |
19+45       4.6777      0.52  | Q        |           |         |        V  |
19+50       4.6809      0.46  |Q         |           |         |        V  |
19+55       4.6834      0.37  |Q         |           |         |        V  |
20+ 0       4.6858      0.35  |Q         |           |         |        V  |
20+ 5       4.6886      0.40  |Q         |           |         |        V  |
20+10       4.6918      0.47  |Q         |           |         |        V  |
20+15       4.6952      0.49  |Q         |           |         |        V  |
20+20       4.6986      0.50  |Q         |           |         |        V  |
20+25       4.7021      0.50  | Q        |           |         |         V |
20+30       4.7056      0.50  | Q        |           |         |         V |
20+35       4.7090      0.50  | Q        |           |         |         V |
20+40       4.7125      0.50  | Q        |           |         |         V |
20+45       4.7160      0.50  | Q        |           |         |         V |
20+50       4.7191      0.45  |Q         |           |         |         V |
20+55       4.7216      0.37  |Q         |           |         |         V |
21+ 0       4.7240      0.35  |Q         |           |         |         V |
21+ 5       4.7268      0.40  |Q         |           |         |         V |
21+10       4.7300      0.47  |Q         |           |         |         V |
21+15       4.7334      0.49  |Q         |           |         |         V |
21+20       4.7364      0.44  |Q         |           |         |         V |
21+25       4.7390      0.37  |Q         |           |         |         V |
21+30       4.7414      0.35  |Q         |           |         |         V |
21+35       4.7441      0.40  |Q         |           |         |         V |
21+40       4.7474      0.47  |Q         |           |         |         V |
21+45       4.7508      0.49  |Q         |           |         |         V |
21+50       4.7538      0.44  |Q         |           |         |         V |
21+55       4.7563      0.37  |Q         |           |         |         V |
22+ 0       4.7588      0.35  |Q         |           |         |         V |
22+ 5       4.7615      0.40  |Q         |           |         |         V |
22+10       4.7647      0.47  |Q         |           |         |         V |
22+15       4.7681      0.49  |Q         |           |         |         V |
22+20       4.7712      0.44  |Q         |           |         |         V |
22+25       4.7737      0.37  |Q         |           |         |         V |
22+30       4.7761      0.35  |Q         |           |         |         V |
22+35       4.7785      0.34  |Q         |           |         |         V |
22+40       4.7808      0.34  |Q         |           |         |         V |
22+45       4.7831      0.34  |Q         |           |         |         V |
22+50       4.7854      0.34  |Q         |           |         |         V |
22+55       4.7878      0.34  |Q         |           |         |         V |
23+ 0       4.7901      0.34  |Q         |           |         |         V |
23+ 5       4.7924      0.34  |Q         |           |         |         V |
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   23+10       4.7947      0.34  |Q        |         |         |        v|
   23+15       4.7970      0.34  |Q        |         |         |        v|
   23+20       4.7993      0.34  |Q        |         |         |        v|
   23+25       4.8016      0.34  |Q        |         |         |        v|
   23+30       4.8040      0.34  |Q        |         |         |        v|
   23+35       4.8063      0.34  |Q        |         |         |        v|
   23+40       4.8086      0.34  |Q        |         |         |        v|
   23+45       4.8109      0.34  |Q        |         |         |        v|
   23+50       4.8132      0.34  |Q        |         |         |        v|
   23+55       4.8155      0.34  |Q        |         |         |        v|
   24+ 0       4.8178      0.34  |Q        |         |         |        v|
   24+ 5       4.8194      0.23  Q         |         |         |        v|
   24+10       4.8199      0.07  Q         |         |         |        v|
   24+15       4.8201      0.03  Q         |         |         |        v|
   24+20       4.8202      0.01  Q         |         |         |        v|
   24+25       4.8202      0.00  Q         |         |         |        v|
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       U n i t   H y d r o g r a p h   A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      26.74(Ac.)  =      0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      26.74(Ac.)  =      0.042 Sq. Mi.
Length along longest watercourse =    2399.00(Ft.)
Length along longest watercourse measured to centroid =    1200.00(Ft.)
Length along longest watercourse =      0.454 Mi.
Length along longest watercourse measured to centroid =      0.227 Mi.
Difference in elevation =      81.00(Ft.)
Slope along watercourse =    178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.057 Hr.
Lag time =     3.40 Min.
25% of lag time =     0.85 Min.
40% of lag time =     1.36 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           0.50                 13.37

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       26.74           1.30                 34.76

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    1.300(In)
Areal adjustment factor =   99.98 %
Adjusted average point rain =    1.300(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    26.740           91.00         0.500
 Total Area Entered =     26.74(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
91.0  91.0      0.117     0.500        0.064       1.000      0.064
                                                 Sum (F) =    0.064
Area averaged mean soil loss (F) (In/Hr) =  0.064
Minimum soil loss rate ((In/Hr)) =  0.032
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
			Sum = 100.000 Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.515	0.064	(0.257)	0.450
2	0.17	4.20	0.655	0.064	(0.328)	0.591
3	0.25	4.40	0.686	0.064	(0.343)	0.622
4	0.33	4.80	0.749	0.064	(0.374)	0.684
5	0.42	5.20	0.811	0.064	(0.406)	0.747
6	0.50	6.20	0.967	0.064	(0.483)	0.903
7	0.58	6.80	1.061	0.064	(0.530)	0.996
8	0.67	8.80	1.372	0.064	(0.686)	1.308
9	0.75	13.90	2.168	0.064	(1.084)	2.104
10	0.83	31.40	4.897	0.064	(2.449)	4.833
11	0.92	7.20	1.123	0.064	(0.561)	1.059
12	1.00	3.80	0.593	0.064	(0.296)	0.528
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	14.8

Flood volume = Effective rainfall 1.24(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 2.8(Ac.Ft)
Total soil loss = 0.06(In)
Total soil loss = 0.143(Ac.Ft)
Total rainfall = 1.30(In)
Flood volume = 119909.3 Cubic Feet
Total soil loss = 6246.2 Cubic Feet

Peak flow rate of this hydrograph = 80.047(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	22.5	45.0	67.5	90.0
0+ 5	0.0271	3.94	VQ				
0+10	0.1022	10.90	V Q				
0+15	0.2009	14.34	V Q				
0+20	0.3133	16.32	V Q				
0+25	0.4389	18.25	V Q				
0+30	0.5830	20.91	VQ				
0+35	0.7487	24.07	Q				
0+40	0.9457	28.60	QV				
0+45	1.2218	40.09	Q				
0+50	1.7403	75.28	V		Q		
0+55	2.2916	80.05	V		Q		
1+ 0	2.5466	37.03	Q		V		
1+ 5	2.6735	18.42	Q		V		
1+10	2.7231	7.20	Q		V		
1+15	2.7460	3.32	Q		V		
1+20	2.7513	0.78	Q		V		
1+25	2.7527	0.21	Q		V		

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: pro11003100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	0.80	21.39

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	2.00	53.48

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 2.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 2.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.500	0.064	1.000	0.064
					Sum (F) =	0.064

Area averaged mean soil loss (F) (In/Hr) = 0.064
Minimum soil loss rate ((In/Hr)) = 0.032
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
		Sum = 100.000	Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.312	0.064	(0.156)	0.248
2	0.17	1.30	0.312	0.064	(0.156)	0.248
3	0.25	1.10	0.264	0.064	(0.132)	0.200
4	0.33	1.50	0.360	0.064	(0.180)	0.296
5	0.42	1.50	0.360	0.064	(0.180)	0.296
6	0.50	1.80	0.432	0.064	(0.216)	0.368
7	0.58	1.50	0.360	0.064	(0.180)	0.296
8	0.67	1.80	0.432	0.064	(0.216)	0.368
9	0.75	1.80	0.432	0.064	(0.216)	0.368
10	0.83	1.50	0.360	0.064	(0.180)	0.296
11	0.92	1.60	0.384	0.064	(0.192)	0.320
12	1.00	1.80	0.432	0.064	(0.216)	0.368
13	1.08	2.20	0.528	0.064	(0.264)	0.464
14	1.17	2.20	0.528	0.064	(0.264)	0.464
15	1.25	2.20	0.528	0.064	(0.264)	0.464
16	1.33	2.00	0.480	0.064	(0.240)	0.416
17	1.42	2.60	0.624	0.064	(0.312)	0.560
18	1.50	2.70	0.648	0.064	(0.324)	0.584
19	1.58	2.40	0.576	0.064	(0.288)	0.512
20	1.67	2.70	0.648	0.064	(0.324)	0.584
21	1.75	3.30	0.792	0.064	(0.396)	0.728
22	1.83	3.10	0.744	0.064	(0.372)	0.680
23	1.92	2.90	0.696	0.064	(0.348)	0.632
24	2.00	3.00	0.720	0.064	(0.360)	0.656
25	2.08	3.10	0.744	0.064	(0.372)	0.680
26	2.17	4.20	1.008	0.064	(0.504)	0.944
27	2.25	5.00	1.200	0.064	(0.600)	1.136
28	2.33	3.50	0.840	0.064	(0.420)	0.776
29	2.42	6.80	1.632	0.064	(0.816)	1.567
30	2.50	7.30	1.752	0.064	(0.876)	1.687
31	2.58	8.20	1.968	0.064	(0.984)	1.903
32	2.67	5.90	1.416	0.064	(0.708)	1.351
33	2.75	2.00	0.480	0.064	(0.240)	0.416
34	2.83	1.80	0.432	0.064	(0.216)	0.368
35	2.92	1.80	0.432	0.064	(0.216)	0.368
36	3.00	0.60	0.144	0.064	(0.072)	0.080
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	21.7

Flood volume = Effective rainfall 1.81(In)
times area 26.7(Ac.)/[(In)/(Ft.)] = 4.0(Ac.Ft)
Total soil loss = 0.19(In)
Total soil loss = 0.430(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 175371.1 Cubic Feet
Total soil loss = 18738.6 Cubic Feet

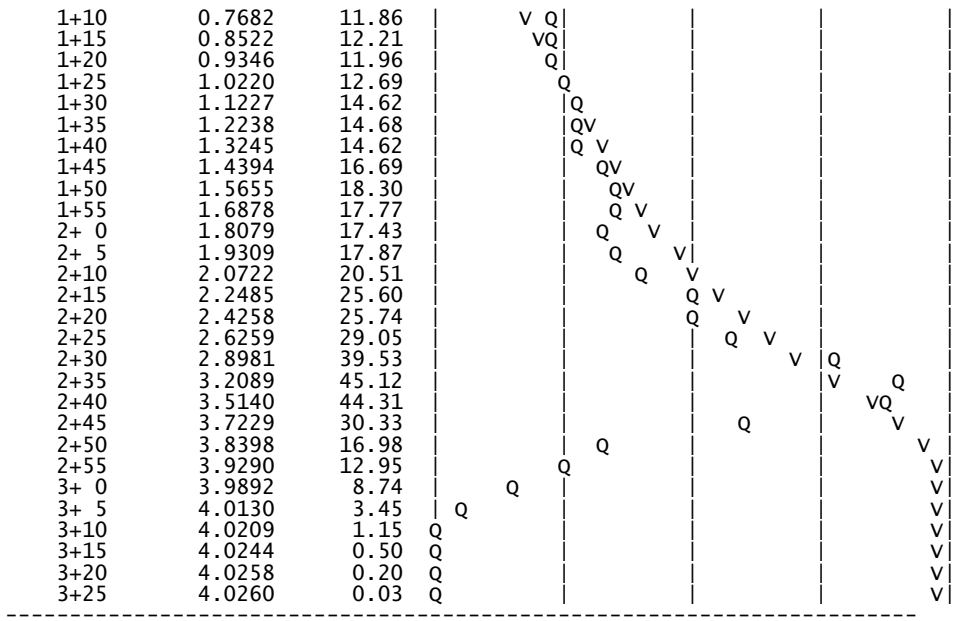
Peak flow rate of this hydrograph = 45.122(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	12.5	25.0	37.5	50.0
0+ 5	0.0149	2.16	VQ	|	|	|	|
0+10	0.0515	5.32	V Q	|	|	|	|
0+15	0.0905	5.66	V Q	|	|	|	|
0+20	0.1333	6.22	|V Q	|	|	|	|
0+25	0.1847	7.46	|V Q	|	|	|	|
0+30	0.2427	8.42	| V Q	|	|	|	|
0+35	0.3033	8.80	| V Q	|	|	|	|
0+40	0.3638	8.78	| V Q	|	|	|	|
0+45	0.4300	9.61	| V Q	|	|	|	|
0+50	0.4931	9.16	| V Q	|	|	|	|
0+55	0.5518	8.53	| VQ	|	|	|	|
1+ 0	0.6141	9.05	| VQ	|	|	|	|
1+ 5	0.6865	10.51	| V Q	|	|	|	|



1+10	0.7682	11.86	V Q
1+15	0.8522	12.21	VQ
1+20	0.9346	11.96	Q
1+25	1.0220	12.69	Q
1+30	1.1227	14.62	Q
1+35	1.2238	14.68	QV
1+40	1.3245	14.62	Q V
1+45	1.4394	16.69	QV
1+50	1.5655	18.30	QV
1+55	1.6878	17.77	Q V
2+ 0	1.8079	17.43	Q V
2+ 5	1.9309	17.87	Q V
2+10	2.0722	20.51	Q V
2+15	2.2485	25.60	Q V
2+20	2.4258	25.74	Q V
2+25	2.6259	29.05	Q V
2+30	2.8981	39.53	V Q
2+35	3.2089	45.12	V Q
2+40	3.5140	44.31	VQ
2+45	3.7229	30.33	Q V
2+50	3.8398	16.98	Q V
2+55	3.9290	12.95	Q V
3+ 0	3.9892	8.74	Q V
3+ 5	4.0130	3.45	Q V
3+10	4.0209	1.15	Q V
3+15	4.0244	0.50	Q V
3+20	4.0258	0.20	Q V
3+25	4.0260	0.03	Q V

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: pro11006100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 26.74(Ac.) = 0.042 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.10	29.41

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	3.00	80.22

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 3.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 3.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.500	0.064	1.000	0.064
					Sum (F) =	0.064

Area averaged mean soil loss (F) (In/Hr) = 0.064
Minimum soil loss rate ((In/Hr)) = 0.032
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
			Sum = 100.000 Sum=	26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.180	0.064	(0.090)	0.116
2	0.17	0.60	0.216	0.064	(0.108)	0.152
3	0.25	0.60	0.216	0.064	(0.108)	0.152
4	0.33	0.60	0.216	0.064	(0.108)	0.152
5	0.42	0.60	0.216	0.064	(0.108)	0.152
6	0.50	0.70	0.252	0.064	(0.126)	0.188
7	0.58	0.70	0.252	0.064	(0.126)	0.188
8	0.67	0.70	0.252	0.064	(0.126)	0.188
9	0.75	0.70	0.252	0.064	(0.126)	0.188
10	0.83	0.70	0.252	0.064	(0.126)	0.188
11	0.92	0.70	0.252	0.064	(0.126)	0.188
12	1.00	0.80	0.288	0.064	(0.144)	0.224
13	1.08	0.80	0.288	0.064	(0.144)	0.224
14	1.17	0.80	0.288	0.064	(0.144)	0.224
15	1.25	0.80	0.288	0.064	(0.144)	0.224
16	1.33	0.80	0.288	0.064	(0.144)	0.224
17	1.42	0.80	0.288	0.064	(0.144)	0.224
18	1.50	0.80	0.288	0.064	(0.144)	0.224
19	1.58	0.80	0.288	0.064	(0.144)	0.224
20	1.67	0.80	0.288	0.064	(0.144)	0.224
21	1.75	0.80	0.288	0.064	(0.144)	0.224
22	1.83	0.80	0.288	0.064	(0.144)	0.224
23	1.92	0.80	0.288	0.064	(0.144)	0.224
24	2.00	0.90	0.324	0.064	(0.162)	0.260
25	2.08	0.80	0.288	0.064	(0.144)	0.224
26	2.17	0.90	0.324	0.064	(0.162)	0.260
27	2.25	0.90	0.324	0.064	(0.162)	0.260
28	2.33	0.90	0.324	0.064	(0.162)	0.260
29	2.42	0.90	0.324	0.064	(0.162)	0.260
30	2.50	0.90	0.324	0.064	(0.162)	0.260
31	2.58	0.90	0.324	0.064	(0.162)	0.260
32	2.67	0.90	0.324	0.064	(0.162)	0.260
33	2.75	1.00	0.360	0.064	(0.180)	0.296
34	2.83	1.00	0.360	0.064	(0.180)	0.296
35	2.92	1.00	0.360	0.064	(0.180)	0.296
36	3.00	1.00	0.360	0.064	(0.180)	0.296
37	3.08	1.00	0.360	0.064	(0.180)	0.296
38	3.17	1.10	0.396	0.064	(0.198)	0.332
39	3.25	1.10	0.396	0.064	(0.198)	0.332
40	3.33	1.10	0.396	0.064	(0.198)	0.332
41	3.42	1.20	0.432	0.064	(0.216)	0.368
42	3.50	1.30	0.468	0.064	(0.234)	0.404
43	3.58	1.40	0.504	0.064	(0.252)	0.440
44	3.67	1.40	0.504	0.064	(0.252)	0.440
45	3.75	1.50	0.540	0.064	(0.270)	0.476
46	3.83	1.50	0.540	0.064	(0.270)	0.476
47	3.92	1.60	0.576	0.064	(0.288)	0.512
48	4.00	1.60	0.576	0.064	(0.288)	0.512
49	4.08	1.70	0.612	0.064	(0.306)	0.548
50	4.17	1.80	0.648	0.064	(0.324)	0.584
51	4.25	1.90	0.684	0.064	(0.342)	0.620
52	4.33	2.00	0.720	0.064	(0.360)	0.656
53	4.42	2.10	0.756	0.064	(0.378)	0.692
54	4.50	2.10	0.756	0.064	(0.378)	0.692
55	4.58	2.20	0.792	0.064	(0.396)	0.728
56	4.67	2.30	0.828	0.064	(0.414)	0.764
57	4.75	2.40	0.864	0.064	(0.432)	0.800
58	4.83	2.40	0.864	0.064	(0.432)	0.800
59	4.92	2.50	0.900	0.064	(0.450)	0.836
60	5.00	2.60	0.936	0.064	(0.468)	0.872
61	5.08	3.10	1.116	0.064	(0.558)	1.052
62	5.17	3.60	1.296	0.064	(0.648)	1.232
63	5.25	3.90	1.404	0.064	(0.702)	1.340
64	5.33	4.20	1.512	0.064	(0.756)	1.448
65	5.42	4.70	1.692	0.064	(0.846)	1.627
66	5.50	5.60	2.016	0.064	(1.008)	1.951
67	5.58	1.90	0.684	0.064	(0.342)	0.620
68	5.67	0.90	0.324	0.064	(0.162)	0.260
69	5.75	0.60	0.216	0.064	(0.108)	0.152
70	5.83	0.50	0.180	0.064	(0.090)	0.116

```
71   5.92     0.30      0.108       (  0.064)       0.054        0.054
72   6.00     0.20      0.072       (  0.064)       0.036        0.036
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =    31.4
     Flood volume = Effective rainfall      2.62(In)
      times area      26.7(Ac.)/[(In)/(Ft.)] =       5.8(Ac.Ft)
     Total soil loss =      0.38(In)
     Total soil loss =     0.853(Ac.Ft)
     Total rainfall =      3.00(In)
     Flood volume =      254007.7 Cubic Feet
     Total soil loss =       37164.2 Cubic Feet
     ---------------------------------------------------------------------
      Peak flow rate of this hydrograph =     45.277(CFS)
     ---------------------------------------------------------------------
     +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
     ---------------------------------------------------------------------
                 Hydrograph in   5   Minute intervals ((CFS))

     ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0       12.5      25.0      37.5      50.0
-------------------------------------------------------------------------
  0+ 5       0.0070      1.01  Q          |         |         |         |
  0+10       0.0262      2.80  V Q        |         |         |         |
  0+15       0.0511      3.61  V Q        |         |         |         |
  0+20       0.0778      3.88  V  Q       |         |         |         |
  0+25       0.1054      4.00  V  Q       |         |         |         |
  0+30       0.1356      4.39  V  Q       |         |         |         |
  0+35       0.1691      4.86  |V Q       |         |         |         |
  0+40       0.2033      4.97  |V Q       |         |         |         |
  0+45       0.2379      5.02  |V  Q      |         |         |         |
  0+50       0.2726      5.04  |V  Q      |         |         |         |
  0+55       0.3075      5.06  | V Q      |         |         |         |
  1+ 0       0.3445      5.37  | V Q      |         |         |         |
  1+ 5       0.3846      5.83  | V Q      |         |         |         |
  1+10       0.4256      5.94  | V Q      |         |         |         |
  1+15       0.4668      5.99  |  VQ      |         |         |         |
  1+20       0.5083      6.02  |  VQ      |         |         |         |
  1+25       0.5498      6.03  |  VQ      |         |         |         |
  1+30       0.5913      6.03  |   Q      |         |         |         |
  1+35       0.6328      6.03  |   Q      |         |         |         |
  1+40       0.6744      6.03  |   Q      |         |         |         |
  1+45       0.7159      6.03  |   Q      |         |         |         |
  1+50       0.7574      6.03  |   QV     |         |         |         |
  1+55       0.7989      6.03  |   QV     |         |         |         |
  2+ 0       0.8426      6.34  |    Q     |         |         |         |
  2+ 5       0.8873      6.49  |    QV    |         |         |         |
  2+10       0.9318      6.45  |    QV    |         |         |         |
  2+15       0.9789      6.85  |    QV    |         |         |         |
  2+20       1.0267      6.94  |    Q V   |         |         |         |
  2+25       1.0748      6.98  |    Q V   |         |         |         |
  2+30       1.1229      6.99  |    Q V   |         |         |         |
  2+35       1.1711      7.00  |    Q  V  |         |         |         |
  2+40       1.2193      7.00  |    Q  V  |         |         |         |
  2+45       1.2697      7.31  |    Q  V  |         |         |         |
  2+50       1.3232      7.77  |     Q  V|         |         |         |
  2+55       1.3775      7.88  |     Q  V|         |         |         |
  3+ 0       1.4321      7.93  |     Q  V|         |         |         |
  3+ 5       1.4869      7.96  |     Q   V         |         |         |
  3+10       1.5440      8.29  |     Q   V         |         |         |
  3+15       1.6042      8.74  |     Q   |V        |         |         |
  3+20       1.6652      8.85  |      Q  |V        |         |         |
  3+25       1.7287      9.22  |      Q  |V        |         |         |
  3+30       1.7976     10.01  |       Q | V       |         |         |
  3+35       1.8728     10.91  |       Q | V       |         |         |
  3+40       1.9522     11.53  |        Q|  V      |         |         |
  3+45       2.0350     12.03  |        Q|  V      |         |         |
  3+50       2.1216     12.57  |         Q   V     |         |         |
  3+55       2.2114     13.04  |         Q    V    |         |         |
  4+ 0       2.3048     13.56  |         Q    V    |         |         |
  4+ 5       2.4012     14.01  |         |Q    V   |         |         |
  4+10       2.5035     14.84  |         |Q     V  |         |         |
  4+15       2.6119     15.75  |         | Q    V  |         |         |
  4+20       2.7269     16.70  |         |  Q    V |         |         |
  4+25       2.8485     17.65  |         |   Q    V|         |         |
  4+30       2.9746     18.31  |         |   Q     V         |         |
  4+35       3.1042     18.82  |         |    Q    |V        |         |
  4+40       3.2398     19.68  |         |    Q    | V       |         |
  4+45       3.3817     20.60  |         |     Q   |  V      |         |
  4+50       3.5279     21.24  |         |     Q   |   V     |         |
  4+55       3.6776     21.73  |         |      Q  |    V    |         |
  5+ 0       3.8332     22.59  |         |       Q |     V   |         |
  5+ 5       4.0038     24.77  |         |        Q|      V  |         |
  5+10       4.2023     28.81  |         |         |  Q    V |         |
  5+15       4.4273     32.67  |         |         |     Q   V         |
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    5+20       4.6740     35.82  |          |          |       Q | V        |
    5+25       4.9459     39.48  |          |          |         |Q V      |
    5+30       5.2577     45.28  |          |          |         |     Q    |
    5+35       5.5236     38.61  |          |          |         Q       V  |
    5+40       5.6603     19.85  |          |    Q     |         |        V |
    5+45       5.7350     10.84  |          Q          |         |         V|
    5+50       5.7801      6.55  |       Q             |         |         V|
    5+55       5.8073      3.95  |    Q                |         |         V|
    6+ 0       5.8209      1.98  |Q                    |         |         V|
    6+ 5       5.8277      0.99  Q                     |         |         V|
    6+10       5.8299      0.32  Q                     |         |         V|
    6+15       5.8308      0.13  Q                     |         |         V|
    6+20       5.8311      0.05  Q                     |         |         V|
    6+25       5.8312      0.01  Q                     |         |          V
-------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: pro110024100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

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Drainage Area for Depth-Area Areal Adjustment = 26.74(Ac.) = 0.042 Sq. Mi.
Length along longest watercourse = 2399.00(Ft.)
Length along longest watercourse measured to centroid = 1200.00(Ft.)
Length along longest watercourse = 0.454 Mi.
Length along longest watercourse measured to centroid = 0.227 Mi.
Difference in elevation = 81.00(Ft.)
Slope along watercourse = 178.2743 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.057 Hr.
Lag time = 3.40 Min.
25% of lag time = 0.85 Min.
40% of lag time = 1.36 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	1.80	48.13

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
26.74	5.00	133.70

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 5.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 5.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
26.740	91.00	0.500

Total Area Entered = 26.74(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
91.0	91.0	0.117	0.500	0.064	1.000	0.064
					Sum (F) =	0.064

Area averaged mean soil loss (F) (In/Hr) = 0.064
Minimum soil loss rate ((In/Hr)) = 0.032
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	146.867	32.409	8.734
2	0.167	293.734	47.236	12.730
3	0.250	440.601	11.368	3.064
4	0.333	587.468	4.979	1.342
5	0.417	734.335	2.561	0.690
6	0.500	881.203	1.446	0.390
			Sum = 100.000	Sum= 26.949

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.040	(0.114)	0.020	0.020
2	0.17	0.07	0.040	(0.114)	0.020	0.020
3	0.25	0.07	0.040	(0.113)	0.020	0.020
4	0.33	0.10	0.060	(0.113)	0.030	0.030
5	0.42	0.10	0.060	(0.112)	0.030	0.030
6	0.50	0.10	0.060	(0.112)	0.030	0.030
7	0.58	0.10	0.060	(0.111)	0.030	0.030
8	0.67	0.10	0.060	(0.111)	0.030	0.030
9	0.75	0.10	0.060	(0.111)	0.030	0.030
10	0.83	0.13	0.080	(0.110)	0.040	0.040
11	0.92	0.13	0.080	(0.110)	0.040	0.040
12	1.00	0.13	0.080	(0.109)	0.040	0.040
13	1.08	0.10	0.060	(0.109)	0.030	0.030
14	1.17	0.10	0.060	(0.108)	0.030	0.030
15	1.25	0.10	0.060	(0.108)	0.030	0.030
16	1.33	0.10	0.060	(0.108)	0.030	0.030
17	1.42	0.10	0.060	(0.107)	0.030	0.030
18	1.50	0.10	0.060	(0.107)	0.030	0.030
19	1.58	0.10	0.060	(0.106)	0.030	0.030
20	1.67	0.10	0.060	(0.106)	0.030	0.030
21	1.75	0.10	0.060	(0.105)	0.030	0.030
22	1.83	0.13	0.080	(0.105)	0.040	0.040
23	1.92	0.13	0.080	(0.105)	0.040	0.040
24	2.00	0.13	0.080	(0.104)	0.040	0.040
25	2.08	0.13	0.080	(0.104)	0.040	0.040
26	2.17	0.13	0.080	(0.103)	0.040	0.040
27	2.25	0.13	0.080	(0.103)	0.040	0.040
28	2.33	0.13	0.080	(0.102)	0.040	0.040
29	2.42	0.13	0.080	(0.102)	0.040	0.040
30	2.50	0.13	0.080	(0.102)	0.040	0.040
31	2.58	0.17	0.100	(0.101)	0.050	0.050
32	2.67	0.17	0.100	(0.101)	0.050	0.050
33	2.75	0.17	0.100	(0.100)	0.050	0.050
34	2.83	0.17	0.100	(0.100)	0.050	0.050
35	2.92	0.17	0.100	(0.100)	0.050	0.050
36	3.00	0.17	0.100	(0.099)	0.050	0.050
37	3.08	0.17	0.100	(0.099)	0.050	0.050
38	3.17	0.17	0.100	(0.098)	0.050	0.050
39	3.25	0.17	0.100	(0.098)	0.050	0.050
40	3.33	0.17	0.100	(0.098)	0.050	0.050
41	3.42	0.17	0.100	(0.097)	0.050	0.050
42	3.50	0.17	0.100	(0.097)	0.050	0.050
43	3.58	0.17	0.100	(0.096)	0.050	0.050
44	3.67	0.17	0.100	(0.096)	0.050	0.050
45	3.75	0.17	0.100	(0.095)	0.050	0.050
46	3.83	0.20	0.120	(0.095)	0.060	0.060
47	3.92	0.20	0.120	(0.095)	0.060	0.060
48	4.00	0.20	0.120	(0.094)	0.060	0.060
49	4.08	0.20	0.120	(0.094)	0.060	0.060
50	4.17	0.20	0.120	(0.093)	0.060	0.060
51	4.25	0.20	0.120	(0.093)	0.060	0.060
52	4.33	0.23	0.140	(0.093)	0.070	0.070
53	4.42	0.23	0.140	(0.092)	0.070	0.070
54	4.50	0.23	0.140	(0.092)	0.070	0.070
55	4.58	0.23	0.140	(0.092)	0.070	0.070
56	4.67	0.23	0.140	(0.091)	0.070	0.070
57	4.75	0.23	0.140	(0.091)	0.070	0.070
58	4.83	0.27	0.160	(0.090)	0.080	0.080
59	4.92	0.27	0.160	(0.090)	0.080	0.080
60	5.00	0.27	0.160	(0.090)	0.080	0.080
61	5.08	0.20	0.120	(0.089)	0.060	0.060
62	5.17	0.20	0.120	(0.089)	0.060	0.060
63	5.25	0.20	0.120	(0.088)	0.060	0.060
64	5.33	0.23	0.140	(0.088)	0.070	0.070
65	5.42	0.23	0.140	(0.088)	0.070	0.070
66	5.50	0.23	0.140	(0.087)	0.070	0.070
67	5.58	0.27	0.160	(0.087)	0.080	0.080
68	5.67	0.27	0.160	(0.086)	0.080	0.080
69	5.75	0.27	0.160	(0.086)	0.080	0.080
70	5.83	0.27	0.160	(0.086)	0.080	0.080

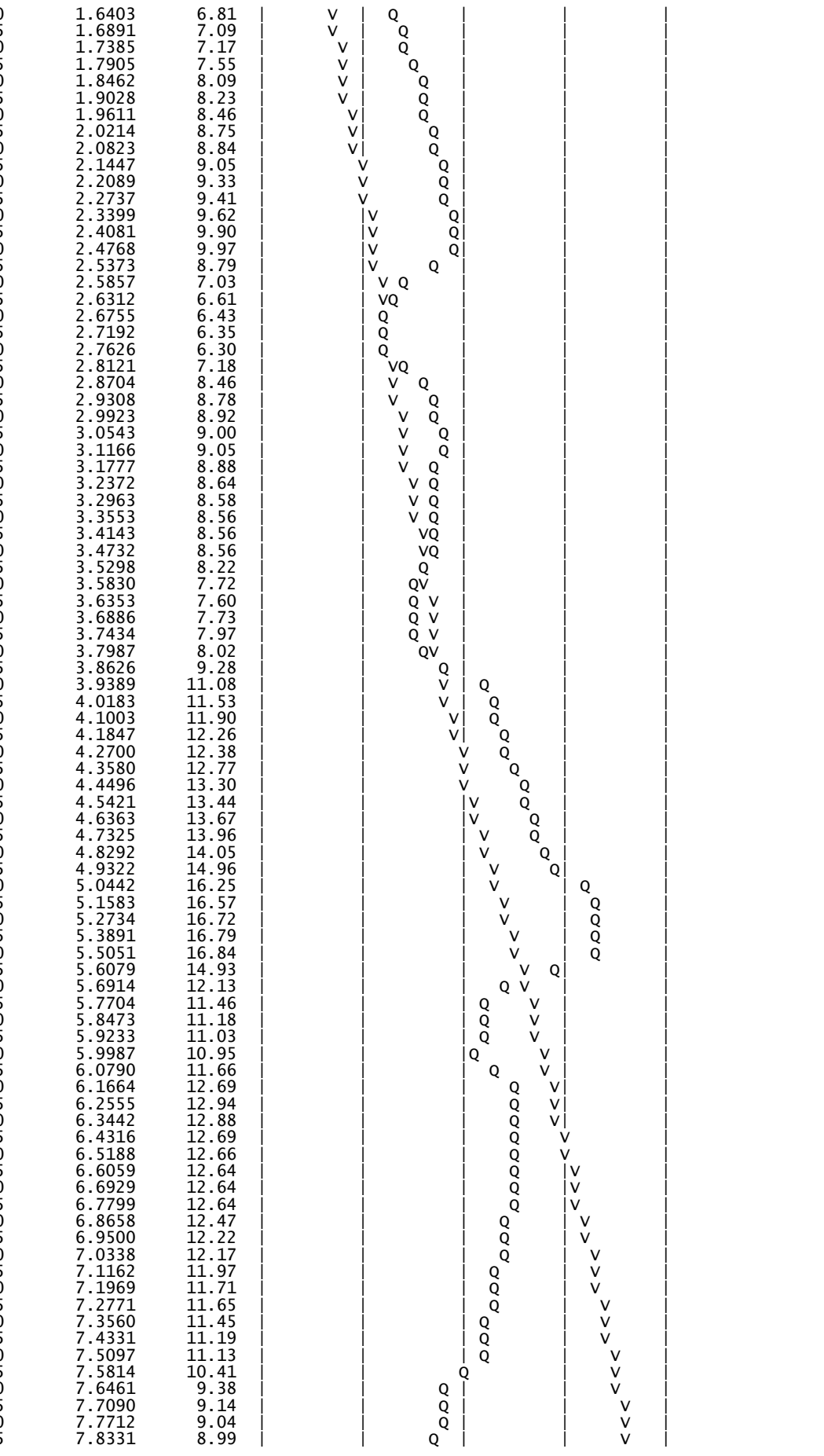
71	5.92	0.27	0.160	(0.085)	0.080	0.080
72	6.00	0.27	0.160	(0.085)	0.080	0.080
73	6.08	0.30	0.180	0.085	(0.090)	0.095
74	6.17	0.30	0.180	0.084	(0.090)	0.096
75	6.25	0.30	0.180	0.084	(0.090)	0.096
76	6.33	0.30	0.180	0.083	(0.090)	0.097
77	6.42	0.30	0.180	0.083	(0.090)	0.097
78	6.50	0.30	0.180	0.083	(0.090)	0.097
79	6.58	0.33	0.200	0.082	(0.100)	0.118
80	6.67	0.33	0.200	0.082	(0.100)	0.118
81	6.75	0.33	0.200	0.082	(0.100)	0.118
82	6.83	0.33	0.200	0.081	(0.100)	0.119
83	6.92	0.33	0.200	0.081	(0.100)	0.119
84	7.00	0.33	0.200	0.080	(0.100)	0.120
85	7.08	0.33	0.200	0.080	(0.100)	0.120
86	7.17	0.33	0.200	0.080	(0.100)	0.120
87	7.25	0.33	0.200	0.079	(0.100)	0.121
88	7.33	0.37	0.220	0.079	(0.110)	0.141
89	7.42	0.37	0.220	0.079	(0.110)	0.141
90	7.50	0.37	0.220	0.078	(0.110)	0.142
91	7.58	0.40	0.240	0.078	(0.120)	0.162
92	7.67	0.40	0.240	0.078	(0.120)	0.162
93	7.75	0.40	0.240	0.077	(0.120)	0.163
94	7.83	0.43	0.260	0.077	(0.130)	0.183
95	7.92	0.43	0.260	0.077	(0.130)	0.183
96	8.00	0.43	0.260	0.076	(0.130)	0.184
97	8.08	0.50	0.300	0.076	(0.150)	0.224
98	8.17	0.50	0.300	0.075	(0.150)	0.225
99	8.25	0.50	0.300	0.075	(0.150)	0.225
100	8.33	0.50	0.300	0.075	(0.150)	0.225
101	8.42	0.50	0.300	0.074	(0.150)	0.226
102	8.50	0.50	0.300	0.074	(0.150)	0.226
103	8.58	0.53	0.320	0.074	(0.160)	0.246
104	8.67	0.53	0.320	0.073	(0.160)	0.247
105	8.75	0.53	0.320	0.073	(0.160)	0.247
106	8.83	0.57	0.340	0.073	(0.170)	0.267
107	8.92	0.57	0.340	0.072	(0.170)	0.268
108	9.00	0.57	0.340	0.072	(0.170)	0.268
109	9.08	0.63	0.380	0.072	(0.190)	0.308
110	9.17	0.63	0.380	0.071	(0.190)	0.309
111	9.25	0.63	0.380	0.071	(0.190)	0.309
112	9.33	0.67	0.400	0.071	(0.200)	0.329
113	9.42	0.67	0.400	0.070	(0.200)	0.330
114	9.50	0.67	0.400	0.070	(0.200)	0.330
115	9.58	0.70	0.420	0.070	(0.210)	0.350
116	9.67	0.70	0.420	0.069	(0.210)	0.351
117	9.75	0.70	0.420	0.069	(0.210)	0.351
118	9.83	0.73	0.440	0.069	(0.220)	0.371
119	9.92	0.73	0.440	0.068	(0.220)	0.372
120	10.00	0.73	0.440	0.068	(0.220)	0.372
121	10.08	0.50	0.300	0.068	(0.150)	0.232
122	10.17	0.50	0.300	0.067	(0.150)	0.233
123	10.25	0.50	0.300	0.067	(0.150)	0.233
124	10.33	0.50	0.300	0.067	(0.150)	0.233
125	10.42	0.50	0.300	0.066	(0.150)	0.234
126	10.50	0.50	0.300	0.066	(0.150)	0.234
127	10.58	0.67	0.400	0.066	(0.200)	0.334
128	10.67	0.67	0.400	0.065	(0.200)	0.335
129	10.75	0.67	0.400	0.065	(0.200)	0.335
130	10.83	0.67	0.400	0.065	(0.200)	0.335
131	10.92	0.67	0.400	0.064	(0.200)	0.336
132	11.00	0.67	0.400	0.064	(0.200)	0.336
133	11.08	0.63	0.380	0.064	(0.190)	0.316
134	11.17	0.63	0.380	0.063	(0.190)	0.317
135	11.25	0.63	0.380	0.063	(0.190)	0.317
136	11.33	0.63	0.380	0.063	(0.190)	0.317
137	11.42	0.63	0.380	0.063	(0.190)	0.317
138	11.50	0.63	0.380	0.062	(0.190)	0.318
139	11.58	0.57	0.340	0.062	(0.170)	0.278
140	11.67	0.57	0.340	0.062	(0.170)	0.278
141	11.75	0.57	0.340	0.061	(0.170)	0.279
142	11.83	0.60	0.360	0.061	(0.180)	0.299
143	11.92	0.60	0.360	0.061	(0.180)	0.299
144	12.00	0.60	0.360	0.060	(0.180)	0.300
145	12.08	0.83	0.500	0.060	(0.250)	0.440
146	12.17	0.83	0.500	0.060	(0.250)	0.440
147	12.25	0.83	0.500	0.059	(0.250)	0.441
148	12.33	0.87	0.520	0.059	(0.260)	0.461
149	12.42	0.87	0.520	0.059	(0.260)	0.461
150	12.50	0.87	0.520	0.059	(0.260)	0.461
151	12.58	0.93	0.560	0.058	(0.280)	0.502
152	12.67	0.93	0.560	0.058	(0.280)	0.502
153	12.75	0.93	0.560	0.058	(0.280)	0.502
154	12.83	0.97	0.580	0.057	(0.290)	0.523
155	12.92	0.97	0.580	0.057	(0.290)	0.523
156	13.00	0.97	0.580	0.057	(0.290)	0.523

157	13.08	1.13	0.680	0.057	(0.340)	0.623
158	13.17	1.13	0.680	0.056	(0.340)	0.624
159	13.25	1.13	0.680	0.056	(0.340)	0.624
160	13.33	1.13	0.680	0.056	(0.340)	0.624
161	13.42	1.13	0.680	0.055	(0.340)	0.625
162	13.50	1.13	0.680	0.055	(0.340)	0.625
163	13.58	0.77	0.460	0.055	(0.230)	0.405
164	13.67	0.77	0.460	0.055	(0.230)	0.405
165	13.75	0.77	0.460	0.054	(0.230)	0.406
166	13.83	0.77	0.460	0.054	(0.230)	0.406
167	13.92	0.77	0.460	0.054	(0.230)	0.406
168	14.00	0.77	0.460	0.053	(0.230)	0.407
169	14.08	0.90	0.540	0.053	(0.270)	0.487
170	14.17	0.90	0.540	0.053	(0.270)	0.487
171	14.25	0.90	0.540	0.053	(0.270)	0.487
172	14.33	0.87	0.520	0.052	(0.260)	0.468
173	14.42	0.87	0.520	0.052	(0.260)	0.468
174	14.50	0.87	0.520	0.052	(0.260)	0.468
175	14.58	0.87	0.520	0.052	(0.260)	0.468
176	14.67	0.87	0.520	0.051	(0.260)	0.469
177	14.75	0.87	0.520	0.051	(0.260)	0.469
178	14.83	0.83	0.500	0.051	(0.250)	0.449
179	14.92	0.83	0.500	0.051	(0.250)	0.449
180	15.00	0.83	0.500	0.050	(0.250)	0.450
181	15.08	0.80	0.480	0.050	(0.240)	0.430
182	15.17	0.80	0.480	0.050	(0.240)	0.430
183	15.25	0.80	0.480	0.049	(0.240)	0.430
184	15.33	0.77	0.460	0.049	(0.230)	0.411
185	15.42	0.77	0.460	0.049	(0.230)	0.411
186	15.50	0.77	0.460	0.049	(0.230)	0.411
187	15.58	0.63	0.380	0.048	(0.190)	0.331
188	15.67	0.63	0.380	0.048	(0.190)	0.332
189	15.75	0.63	0.380	0.048	(0.190)	0.332
190	15.83	0.63	0.380	0.048	(0.190)	0.332
191	15.92	0.63	0.380	0.047	(0.190)	0.332
192	16.00	0.63	0.380	0.047	(0.190)	0.333
193	16.08	0.13	0.080	(0.047)	0.040	0.040
194	16.17	0.13	0.080	(0.047)	0.040	0.040
195	16.25	0.13	0.080	(0.047)	0.040	0.040
196	16.33	0.13	0.080	(0.046)	0.040	0.040
197	16.42	0.13	0.080	(0.046)	0.040	0.040
198	16.50	0.13	0.080	(0.046)	0.040	0.040
199	16.58	0.10	0.060	(0.046)	0.030	0.030
200	16.67	0.10	0.060	(0.045)	0.030	0.030
201	16.75	0.10	0.060	(0.045)	0.030	0.030
202	16.83	0.10	0.060	(0.045)	0.030	0.030
203	16.92	0.10	0.060	(0.045)	0.030	0.030
204	17.00	0.10	0.060	(0.044)	0.030	0.030
205	17.08	0.17	0.100	0.044	(0.050)	0.056
206	17.17	0.17	0.100	0.044	(0.050)	0.056
207	17.25	0.17	0.100	0.044	(0.050)	0.056
208	17.33	0.17	0.100	0.044	(0.050)	0.056
209	17.42	0.17	0.100	0.043	(0.050)	0.057
210	17.50	0.17	0.100	0.043	(0.050)	0.057
211	17.58	0.17	0.100	0.043	(0.050)	0.057
212	17.67	0.17	0.100	0.043	(0.050)	0.057
213	17.75	0.17	0.100	0.042	(0.050)	0.058
214	17.83	0.13	0.080	(0.042)	0.040	0.040
215	17.92	0.13	0.080	(0.042)	0.040	0.040
216	18.00	0.13	0.080	(0.042)	0.040	0.040
217	18.08	0.13	0.080	(0.042)	0.040	0.040
218	18.17	0.13	0.080	(0.041)	0.040	0.040
219	18.25	0.13	0.080	(0.041)	0.040	0.040
220	18.33	0.13	0.080	(0.041)	0.040	0.040
221	18.42	0.13	0.080	(0.041)	0.040	0.040
222	18.50	0.13	0.080	(0.041)	0.040	0.040
223	18.58	0.10	0.060	(0.040)	0.030	0.030
224	18.67	0.10	0.060	(0.040)	0.030	0.030
225	18.75	0.10	0.060	(0.040)	0.030	0.030
226	18.83	0.07	0.040	(0.040)	0.020	0.020
227	18.92	0.07	0.040	(0.040)	0.020	0.020
228	19.00	0.07	0.040	(0.039)	0.020	0.020
229	19.08	0.10	0.060	(0.039)	0.030	0.030
230	19.17	0.10	0.060	(0.039)	0.030	0.030
231	19.25	0.10	0.060	(0.039)	0.030	0.030
232	19.33	0.13	0.080	0.039	(0.040)	0.041
233	19.42	0.13	0.080	0.039	(0.040)	0.041
234	19.50	0.13	0.080	0.038	(0.040)	0.042
235	19.58	0.10	0.060	(0.038)	0.030	0.030
236	19.67	0.10	0.060	(0.038)	0.030	0.030
237	19.75	0.10	0.060	(0.038)	0.030	0.030
238	19.83	0.07	0.040	(0.038)	0.020	0.020
239	19.92	0.07	0.040	(0.038)	0.020	0.020
240	20.00	0.07	0.040	(0.037)	0.020	0.020
241	20.08	0.10	0.060	(0.037)	0.030	0.030
242	20.17	0.10	0.060	(0.037)	0.030	0.030

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243  20.25     0.10      0.060       (  0.037)       0.030        0.030
244  20.33     0.10      0.060       (  0.037)       0.030        0.030
245  20.42     0.10      0.060       (  0.037)       0.030        0.030
246  20.50     0.10      0.060       (  0.036)       0.030        0.030
247  20.58     0.10      0.060       (  0.036)       0.030        0.030
248  20.67     0.10      0.060       (  0.036)       0.030        0.030
249  20.75     0.10      0.060       (  0.036)       0.030        0.030
250  20.83     0.07      0.040       (  0.036)       0.020        0.020
251  20.92     0.07      0.040       (  0.036)       0.020        0.020
252  21.00     0.07      0.040       (  0.036)       0.020        0.020
253  21.08     0.10      0.060       (  0.035)       0.030        0.030
254  21.17     0.10      0.060       (  0.035)       0.030        0.030
255  21.25     0.10      0.060       (  0.035)       0.030        0.030
256  21.33     0.07      0.040       (  0.035)       0.020        0.020
257  21.42     0.07      0.040       (  0.035)       0.020        0.020
258  21.50     0.07      0.040       (  0.035)       0.020        0.020
259  21.58     0.10      0.060       (  0.035)       0.030        0.030
260  21.67     0.10      0.060       (  0.034)       0.030        0.030
261  21.75     0.10      0.060       (  0.034)       0.030        0.030
262  21.83     0.07      0.040       (  0.034)       0.020        0.020
263  21.92     0.07      0.040       (  0.034)       0.020        0.020
264  22.00     0.07      0.040       (  0.034)       0.020        0.020
265  22.08     0.10      0.060       (  0.034)       0.030        0.030
266  22.17     0.10      0.060       (  0.034)       0.030        0.030
267  22.25     0.10      0.060       (  0.034)       0.030        0.030
268  22.33     0.07      0.040       (  0.034)       0.020        0.020
269  22.42     0.07      0.040       (  0.033)       0.020        0.020
270  22.50     0.07      0.040       (  0.033)       0.020        0.020
271  22.58     0.07      0.040       (  0.033)       0.020        0.020
272  22.67     0.07      0.040       (  0.033)       0.020        0.020
273  22.75     0.07      0.040       (  0.033)       0.020        0.020
274  22.83     0.07      0.040       (  0.033)       0.020        0.020
275  22.92     0.07      0.040       (  0.033)       0.020        0.020
276  23.00     0.07      0.040       (  0.033)       0.020        0.020
277  23.08     0.07      0.040       (  0.033)       0.020        0.020
278  23.17     0.07      0.040       (  0.033)       0.020        0.020
279  23.25     0.07      0.040       (  0.033)       0.020        0.020
280  23.33     0.07      0.040       (  0.033)       0.020        0.020
281  23.42     0.07      0.040       (  0.032)       0.020        0.020
282  23.50     0.07      0.040       (  0.032)       0.020        0.020
283  23.58     0.07      0.040       (  0.032)       0.020        0.020
284  23.67     0.07      0.040       (  0.032)       0.020        0.020
285  23.75     0.07      0.040       (  0.032)       0.020        0.020
286  23.83     0.07      0.040       (  0.032)       0.020        0.020
287  23.92     0.07      0.040       (  0.032)       0.020        0.020
288  24.00     0.07      0.040       (  0.032)       0.020        0.020
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    45.8
      Flood volume = Effective rainfall      3.82(In)
       times area      26.7(Ac.)/[(In)/(Ft.)] =       8.5(Ac.Ft)
      Total soil loss =      1.18(In)
      Total soil loss =     2.636(Ac.Ft)
      Total rainfall =      5.00(In)
      Flood volume =      370468.6 Cubic Feet
      Total soil loss =      114837.0 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     16.840(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
 ------------------------------------------------------------------------
   0+ 5       0.0012      0.17  Q          |          |          |          |
   0+10       0.0042      0.43  Q          |          |          |          |
   0+15       0.0075      0.49  Q          |          |          |          |
   0+20       0.0117      0.61  VQ         |          |          |          |
   0+25       0.0168      0.75  VQ         |          |          |          |
   0+30       0.0223      0.78  VQ         |          |          |          |
   0+35       0.0277      0.80  VQ         |          |          |          |
   0+40       0.0333      0.80  VQ         |          |          |          |
   0+45       0.0389      0.81  VQ         |          |          |          |
   0+50       0.0450      0.90  VQ         |          |          |          |
   0+55       0.0521      1.02  V Q        |          |          |          |
   1+ 0       0.0593      1.05  V Q        |          |          |          |
   1+ 5       0.0661      0.98  VQ         |          |          |          |
   1+10       0.0720      0.86  VQ         |          |          |          |
   1+15       0.0778      0.83  VQ         |          |          |          |
   1+20       0.0834      0.82  VQ         |          |          |          |
   1+25       0.0890      0.81  VQ         |          |          |          |
   1+30       0.0946      0.81  VQ         |          |          |          |
   1+35       0.1001      0.81  VQ         |          |          |          |
```

```
1+40      0.1057      0.81  VQ        |         |         |         |
1+45      0.1113      0.81  VQ        |         |         |         |
1+50      0.1175      0.90  VQ        |         |         |         |
1+55      0.1245      1.02  V Q       |         |         |         |
2+ 0      0.1318      1.05  V Q       |         |         |         |
2+ 5      0.1391      1.07  V Q       |         |         |         |
2+10      0.1465      1.07  V Q       |         |         |         |
2+15      0.1539      1.08  V Q       |         |         |         |
2+20      0.1614      1.08  V Q       |         |         |         |
2+25      0.1688      1.08  V Q       |         |         |         |
2+30      0.1762      1.08  V Q       |         |         |         |
2+35      0.1843      1.17  V Q       |         |         |         |
2+40      0.1932      1.29  V Q       |         |         |         |
2+45      0.2023      1.32  V Q       |         |         |         |
2+50      0.2115      1.34  V Q       |         |         |         |
2+55      0.2207      1.34  |VQ       |         |         |         |
3+ 0      0.2300      1.35  |VQ       |         |         |         |
3+ 5      0.2393      1.35  |VQ       |         |         |         |
3+10      0.2486      1.35  |VQ       |         |         |         |
3+15      0.2579      1.35  |VQ       |         |         |         |
3+20      0.2672      1.35  |VQ       |         |         |         |
3+25      0.2764      1.35  |VQ       |         |         |         |
3+30      0.2857      1.35  |VQ       |         |         |         |
3+35      0.2950      1.35  |VQ       |         |         |         |
3+40      0.3043      1.35  |VQ       |         |         |         |
3+45      0.3136      1.35  |VQ       |         |         |         |
3+50      0.3235      1.44  |VQ       |         |         |         |
3+55      0.3342      1.56  |V Q      |         |         |         |
4+ 0      0.3452      1.59  |V Q      |         |         |         |
4+ 5      0.3563      1.61  |V Q      |         |         |         |
4+10      0.3674      1.61  |V Q      |         |         |         |
4+15      0.3785      1.62  |V Q      |         |         |         |
4+20      0.3903      1.71  |V Q      |         |         |         |
4+25      0.4029      1.83  |V Q      |         |         |         |
4+30      0.4157      1.86  |V Q      |         |         |         |
4+35      0.4286      1.88  | VQ      |         |         |         |
4+40      0.4416      1.88  | VQ      |         |         |         |
4+45      0.4546      1.89  | VQ      |         |         |         |
4+50      0.4682      1.97  | VQ      |         |         |         |
4+55      0.4827      2.10  | V Q     |         |         |         |
5+ 0      0.4974      2.13  | V Q     |         |         |         |
5+ 5      0.5110      1.97  | VQ      |         |         |         |
5+10      0.5228      1.72  | VQ      |         |         |         |
5+15      0.5343      1.67  | VQ      |         |         |         |
5+20      0.5462      1.73  | VQ      |         |         |         |
5+25      0.5589      1.84  | VQ      |         |         |         |
5+30      0.5717      1.86  | VQ      |         |         |         |
5+35      0.5852      1.96  | VQ      |         |         |         |
5+40      0.5997      2.10  | V Q     |         |         |         |
5+45      0.6144      2.13  | V Q     |         |         |         |
5+50      0.6291      2.15  | V Q     |         |         |         |
5+55      0.6440      2.15  |  VQ     |         |         |         |
6+ 0      0.6588      2.16  |  VQ     |         |         |         |
6+ 5      0.6746      2.29  |  VQ     |         |         |         |
6+10      0.6918      2.49  |  VQ     |         |         |         |
6+15      0.7093      2.55  |  V Q    |         |         |         |
6+20      0.7271      2.58  |  V Q    |         |         |         |
6+25      0.7449      2.60  |  V Q    |         |         |         |
6+30      0.7629      2.61  |  V Q    |         |         |         |
6+35      0.7822      2.80  |  V Q    |         |         |         |
6+40      0.8033      3.06  |  V  Q   |         |         |         |
6+45      0.8249      3.13  |  V  Q   |         |         |         |
6+50      0.8467      3.17  |  V  Q   |         |         |         |
6+55      0.8687      3.19  |   V Q   |         |         |         |
7+ 0      0.8908      3.21  |   V Q   |         |         |         |
7+ 5      0.9130      3.22  |   V Q   |         |         |         |
7+10      0.9353      3.23  |   V Q   |         |         |         |
7+15      0.9576      3.24  |   V Q   |         |         |         |
7+20      0.9812      3.43  |   V Q   |         |         |         |
7+25      1.0066      3.69  |   V  Q  |         |         |         |
7+30      1.0326      3.76  |   V  Q  |         |         |         |
7+35      1.0599      3.97  |   V  Q  |         |         |         |
7+40      1.0892      4.25  |    V  Q |         |         |         |
7+45      1.1190      4.33  |    V  Q |         |         |         |
7+50      1.1503      4.54  |    V   Q|         |         |         |
7+55      1.1835      4.82  |    V   Q|         |         |         |
8+ 0      1.2172      4.90  |    V   Q|         |         |         |
8+ 5      1.2536      5.28  |    V    Q         |         |         |
8+10      1.2937      5.82  |     V   |Q        |         |         |
8+15      1.3347      5.96  |     V   |Q        |         |         |
8+20      1.3762      6.02  |     V   | Q       |         |         |
8+25      1.4179      6.06  |     V   | Q       |         |         |
8+30      1.4598      6.08  |     V   | Q       |         |         |
8+35      1.5029      6.27  |      V  | Q       |         |         |
8+40      1.5479      6.53  |      V  |  Q      |         |         |
8+45      1.5934      6.60  |      V  |  Q      |         |         |
```

8+50	1.6403	6.81	
8+55	1.6891	7.09	
9+ 0	1.7385	7.17	
9+ 5	1.7905	7.55	
9+10	1.8462	8.09	
9+15	1.9028	8.23	
9+20	1.9611	8.46	
9+25	2.0214	8.75	
9+30	2.0823	8.84	
9+35	2.1447	9.05	
9+40	2.2089	9.33	
9+45	2.2737	9.41	
9+50	2.3399	9.62	
9+55	2.4081	9.90	
10+ 0	2.4768	9.97	
10+ 5	2.5373	8.79	
10+10	2.5857	7.03	
10+15	2.6312	6.61	
10+20	2.6755	6.43	
10+25	2.7192	6.35	
10+30	2.7626	6.30	
10+35	2.8121	7.18	
10+40	2.8704	8.46	
10+45	2.9308	8.78	
10+50	2.9923	8.92	
10+55	3.0543	9.00	
11+ 0	3.1166	9.05	
11+ 5	3.1777	8.88	
11+10	3.2372	8.64	
11+15	3.2963	8.58	
11+20	3.3553	8.56	
11+25	3.4143	8.56	
11+30	3.4732	8.56	
11+35	3.5298	8.22	
11+40	3.5830	7.72	
11+45	3.6353	7.60	
11+50	3.6886	7.73	
11+55	3.7434	7.97	
12+ 0	3.7987	8.02	
12+ 5	3.8626	9.28	
12+10	3.9389	11.08	
12+15	4.0183	11.53	
12+20	4.1003	11.90	
12+25	4.1847	12.26	
12+30	4.2700	12.38	
12+35	4.3580	12.77	
12+40	4.4496	13.30	
12+45	4.5421	13.44	
12+50	4.6363	13.67	
12+55	4.7325	13.96	
13+ 0	4.8292	14.05	
13+ 5	4.9322	14.96	
13+10	5.0442	16.25	
13+15	5.1583	16.57	
13+20	5.2734	16.72	
13+25	5.3891	16.79	
13+30	5.5051	16.84	
13+35	5.6079	14.93	
13+40	5.6914	12.13	
13+45	5.7704	11.46	
13+50	5.8473	11.18	
13+55	5.9233	11.03	
14+ 0	5.9987	10.95	
14+ 5	6.0790	11.66	
14+10	6.1664	12.69	
14+15	6.2555	12.94	
14+20	6.3442	12.88	
14+25	6.4316	12.69	
14+30	6.5188	12.66	
14+35	6.6059	12.64	
14+40	6.6929	12.64	
14+45	6.7799	12.64	
14+50	6.8658	12.47	
14+55	6.9500	12.22	
15+ 0	7.0338	12.17	
15+ 5	7.1162	11.97	
15+10	7.1969	11.71	
15+15	7.2771	11.65	
15+20	7.3560	11.45	
15+25	7.4331	11.19	
15+30	7.5097	11.13	
15+35	7.5814	10.41	
15+40	7.6461	9.38	
15+45	7.7090	9.14	
15+50	7.7712	9.04	
15+55	7.8331	8.99	

```
16+ 0       7.8949      8.96  |          |       Q  |          |       V  |
16+ 5       7.9390      6.41  |          |  Q       |          |       V  |
16+10       7.9575      2.68  |        Q |          |          |       V  |
16+15       7.9698      1.79  |     Q    |          |          |       V  |
16+20       7.9794      1.39  |  Q       |          |          |       V  |
16+25       7.9876      1.19  |  Q       |          |          |       V  |
16+30       7.9951      1.08  |  Q       |          |          |       V  |
16+35       8.0019      0.99  |Q         |          |          |       V  |
16+40       8.0078      0.86  |Q         |          |          |       V  |
16+45       8.0136      0.83  |Q         |          |          |       V  |
16+50       8.0192      0.82  |Q         |          |          |       V  |
16+55       8.0248      0.81  |Q         |          |          |       V  |
17+ 0       8.0304      0.81  |Q         |          |          |       V  |
17+ 5       8.0375      1.03  |  Q       |          |          |       V  |
17+10       8.0469      1.36  |  Q       |          |          |       V  |
17+15       8.0569      1.45  |  Q       |          |          |       V  |
17+20       8.0671      1.49  |  Q       |          |          |       V  |
17+25       8.0775      1.51  |    Q     |          |          |       V  |
17+30       8.0881      1.53  |    Q     |          |          |        V |
17+35       8.0986      1.53  |    Q     |          |          |        V |
17+40       8.1092      1.54  |    Q     |          |          |        V |
17+45       8.1199      1.54  |    Q     |          |          |        V |
17+50       8.1295      1.40  |  Q       |          |          |        V |
17+55       8.1376      1.17  |  Q       |          |          |        V |
18+ 0       8.1453      1.12  |  Q       |          |          |        V |
18+ 5       8.1528      1.10  |  Q       |          |          |        V |
18+10       8.1603      1.09  |  Q       |          |          |        V |
18+15       8.1677      1.08  |  Q       |          |          |        V |
18+20       8.1752      1.08  |  Q       |          |          |        V |
18+25       8.1826      1.08  |  Q       |          |          |        V |
18+30       8.1900      1.08  |  Q       |          |          |        V |
18+35       8.1968      0.99  |Q         |          |          |        V |
18+40       8.2028      0.86  |Q         |          |          |        V |
18+45       8.2085      0.83  |Q         |          |          |        V |
18+50       8.2136      0.73  |Q         |          |          |        V |
18+55       8.2177      0.60  |Q         |          |          |        V |
19+ 0       8.2216      0.56  |Q         |          |          |        V |
19+ 5       8.2260      0.64  |Q         |          |          |        V |
19+10       8.2312      0.76  |Q         |          |          |        V |
19+15       8.2366      0.78  |Q         |          |          |        V |
19+20       8.2428      0.90  |Q         |          |          |        V |
19+25       8.2500      1.05  |  Q       |          |          |        V |
19+30       8.2575      1.09  |  Q       |          |          |        V |
19+35       8.2644      1.01  |  Q       |          |          |        V |
19+40       8.2704      0.87  |Q         |          |          |        V |
19+45       8.2761      0.84  |Q         |          |          |        V |
19+50       8.2812      0.73  |Q         |          |          |        V |
19+55       8.2853      0.60  |Q         |          |          |        V |
20+ 0       8.2892      0.56  |Q         |          |          |        V |
20+ 5       8.2936      0.64  |Q         |          |          |         V|
20+10       8.2988      0.76  |Q         |          |          |         V|
20+15       8.3042      0.78  |Q         |          |          |         V|
20+20       8.3097      0.80  |Q         |          |          |         V|
20+25       8.3153      0.80  |Q         |          |          |         V|
20+30       8.3208      0.81  |Q         |          |          |         V|
20+35       8.3264      0.81  |Q         |          |          |         V|
20+40       8.3320      0.81  |Q         |          |          |         V|
20+45       8.3375      0.81  |Q         |          |          |         V|
20+50       8.3425      0.72  |Q         |          |          |         V|
20+55       8.3466      0.59  |Q         |          |          |         V|
21+ 0       8.3505      0.56  |Q         |          |          |         V|
21+ 5       8.3549      0.64  |Q         |          |          |         V|
21+10       8.3601      0.76  |Q         |          |          |         V|
21+15       8.3655      0.78  |Q         |          |          |         V|
21+20       8.3704      0.71  |Q         |          |          |         V|
21+25       8.3745      0.59  |Q         |          |          |         V|
21+30       8.3783      0.56  |Q         |          |          |         V|
21+35       8.3827      0.64  |Q         |          |          |         V|
21+40       8.3879      0.76  |Q         |          |          |         V|
21+45       8.3933      0.78  |Q         |          |          |         V|
21+50       8.3982      0.71  |Q         |          |          |         V|
21+55       8.4023      0.59  |Q         |          |          |         V|
22+ 0       8.4062      0.56  |Q         |          |          |         V|
22+ 5       8.4106      0.64  |Q         |          |          |         V|
22+10       8.4158      0.76  |Q         |          |          |         V|
22+15       8.4212      0.78  |Q         |          |          |         V|
22+20       8.4261      0.71  |Q         |          |          |         V|
22+25       8.4302      0.59  |Q         |          |          |         V|
22+30       8.4340      0.56  |Q         |          |          |         V|
22+35       8.4378      0.55  |Q         |          |          |         V|
22+40       8.4416      0.54  |Q         |          |          |         V|
22+45       8.4453      0.54  |Q         |          |          |         V|
22+50       8.4490      0.54  |Q         |          |          |         V|
22+55       8.4527      0.54  |Q         |          |          |         V|
23+ 0       8.4564      0.54  |Q         |          |          |         V|
23+ 5       8.4601      0.54  |Q         |          |          |         V|
```

```
   23+10       8.4639      0.54  |Q        |         |         |        v|
   23+15       8.4676      0.54  |Q        |         |         |        v|
   23+20       8.4713      0.54  |Q        |         |         |        v|
   23+25       8.4750      0.54  |Q        |         |         |        v|
   23+30       8.4787      0.54  |Q        |         |         |        v|
   23+35       8.4824      0.54  |Q        |         |         |        v|
   23+40       8.4861      0.54  |Q        |         |         |        v|
   23+45       8.4898      0.54  |Q        |         |         |        v|
   23+50       8.4936      0.54  |Q        |         |         |        v|
   23+55       8.4973      0.54  |Q        |         |         |        v|
   24+ 0       8.5010      0.54  |Q        |         |         |        v|
   24+ 5       8.5035      0.36  Q         |         |         |        v|
   24+10       8.5043      0.11  Q         |         |         |        v|
   24+15       8.5046      0.05  Q         |         |         |        v|
   24+20       8.5047      0.02  Q         |         |         |        v|
   24+25       8.5048      0.01  Q         |         |         |        v|
-------------------------------------------------------------------------
```

Extended Detention Basin No. 2

```
       U n i t   H y d r o g r a p h   A n a l y s i s

       Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2008, Version 8.1
              Study date  04/22/24 File: pro2212.out

++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2976.00(Ft.)
Length along longest watercourse measured to centroid =    1488.00(Ft.)
Length along longest watercourse =      0.564 Mi.
Length along longest watercourse measured to centroid =      0.282 Mi.
Difference in elevation =     150.00(Ft.)
Slope along watercourse =    266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.062 Hr.
Lag time =     3.72 Min.
25% of lag time =     0.93 Min.
40% of lag time =     1.49 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           0.50                 25.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           1.30                 67.34

STORM EVENT (YEAR) =    2.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.500(In)
Areal adjustment factor =   99.95 %
Adjusted average point rain =    0.500(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           69.00         0.500
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  49.8      0.574     0.500        0.316       1.000      0.316
                                                 Sum (F) =   0.316
Area averaged mean soil loss (F) (In/Hr) =  0.316
Minimum soil loss rate ((In/Hr)) =  0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
			Sum = 100.000 Sum=	52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.198	(0.316)	0.099	0.099
2	0.17	4.20	0.252	(0.316)	0.126	0.126
3	0.25	4.40	0.264	(0.316)	0.132	0.132
4	0.33	4.80	0.288	(0.316)	0.144	0.144
5	0.42	5.20	0.312	(0.316)	0.156	0.156
6	0.50	6.20	0.372	(0.316)	0.186	0.186
7	0.58	6.80	0.408	(0.316)	0.204	0.204
8	0.67	8.80	0.528	(0.316)	0.264	0.264
9	0.75	13.90	0.834	0.316	(0.417)	0.518
10	0.83	31.40	1.883	0.316	(0.942)	1.567
11	0.92	7.20	0.432	(0.316)	0.216	0.216
12	1.00	3.80	0.228	(0.316)	0.114	0.114
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	3.7

Flood volume = Effective rainfall 0.31(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 1.3(Ac.Ft)
Total soil loss = 0.19(In)
Total soil loss = 0.817(Ac.Ft)
Total rainfall = 0.50(In)
Flood volume = 58378.3 Cubic Feet
Total soil loss = 35594.6 Cubic Feet

Peak flow rate of this hydrograph = 47.194(CFS)

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	12.5	25.0	37.5	50.0
0+ 5	0.0104	1.51	VQ				
0+10	0.0408	4.41	V Q				
0+15	0.0807	5.81	V Q				
0+20	0.1261	6.59	V Q				
0+25	0.1767	7.34	Q				
0+30	0.2342	8.35	Q				
0+35	0.2998	9.52	QV				
0+40	0.3765	11.14	Q V				
0+45	0.4919	16.76	QV				
0+50	0.7651	39.66	V		Q		
0+55	1.0901	47.19			V Q		
1+ 0	1.2225	19.23		Q	V		
1+ 5	1.2897	9.75	Q		V		
1+10	1.3195	4.33	Q		V		
1+15	1.3364	2.45	Q		V		
1+20	1.3393	0.42	Q		V		
1+25	1.3402	0.13	Q		V		

U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2976.00(Ft.)
Length along longest watercourse measured to centroid = 1488.00(Ft.)
Length along longest watercourse = 0.564 Mi.
Length along longest watercourse measured to centroid = 0.282 Mi.
Difference in elevation = 150.00(Ft.)
Slope along watercourse = 266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.062 Hr.
Lag time = 3.72 Min.
25% of lag time = 0.93 Min.
40% of lag time = 1.49 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	0.80	41.44

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	2.00	103.60

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 0.800(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 0.800(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	69.00	0.500

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
			Sum = 100.000 Sum=	52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.125	(0.316)	0.062	0.062
2	0.17	1.30	0.125	(0.316)	0.062	0.062
3	0.25	1.10	0.106	(0.316)	0.053	0.053
4	0.33	1.50	0.144	(0.316)	0.072	0.072
5	0.42	1.50	0.144	(0.316)	0.072	0.072
6	0.50	1.80	0.173	(0.316)	0.086	0.086
7	0.58	1.50	0.144	(0.316)	0.072	0.072
8	0.67	1.80	0.173	(0.316)	0.086	0.086
9	0.75	1.80	0.173	(0.316)	0.086	0.086
10	0.83	1.50	0.144	(0.316)	0.072	0.072
11	0.92	1.60	0.154	(0.316)	0.077	0.077
12	1.00	1.80	0.173	(0.316)	0.086	0.086
13	1.08	2.20	0.211	(0.316)	0.106	0.106
14	1.17	2.20	0.211	(0.316)	0.106	0.106
15	1.25	2.20	0.211	(0.316)	0.106	0.106
16	1.33	2.00	0.192	(0.316)	0.096	0.096
17	1.42	2.60	0.250	(0.316)	0.125	0.125
18	1.50	2.70	0.259	(0.316)	0.130	0.130
19	1.58	2.40	0.230	(0.316)	0.115	0.115
20	1.67	2.70	0.259	(0.316)	0.130	0.130
21	1.75	3.30	0.317	(0.316)	0.158	0.158
22	1.83	3.10	0.298	(0.316)	0.149	0.149
23	1.92	2.90	0.278	(0.316)	0.139	0.139
24	2.00	3.00	0.288	(0.316)	0.144	0.144
25	2.08	3.10	0.298	(0.316)	0.149	0.149
26	2.17	4.20	0.403	(0.316)	0.202	0.202
27	2.25	5.00	0.480	(0.316)	0.240	0.240
28	2.33	3.50	0.336	(0.316)	0.168	0.168
29	2.42	6.80	0.653	0.316	(0.326)	0.337
30	2.50	7.30	0.701	0.316	(0.350)	0.385
31	2.58	8.20	0.787	0.316	(0.394)	0.471
32	2.67	5.90	0.566	(0.316)	0.283	0.283
33	2.75	2.00	0.192	(0.316)	0.096	0.096
34	2.83	1.80	0.173	(0.316)	0.086	0.086
35	2.92	1.80	0.173	(0.316)	0.086	0.086
36	3.00	0.60	0.058	(0.316)	0.029	0.029
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	4.9

Flood volume = Effective rainfall 0.41(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 1.8(Ac.Ft)
Total soil loss = 0.39(In)
Total soil loss = 1.682(Ac.Ft)
Total rainfall = 0.80(In)
Flood volume = 77125.8 Cubic Feet
Total soil loss = 73267.3 Cubic Feet

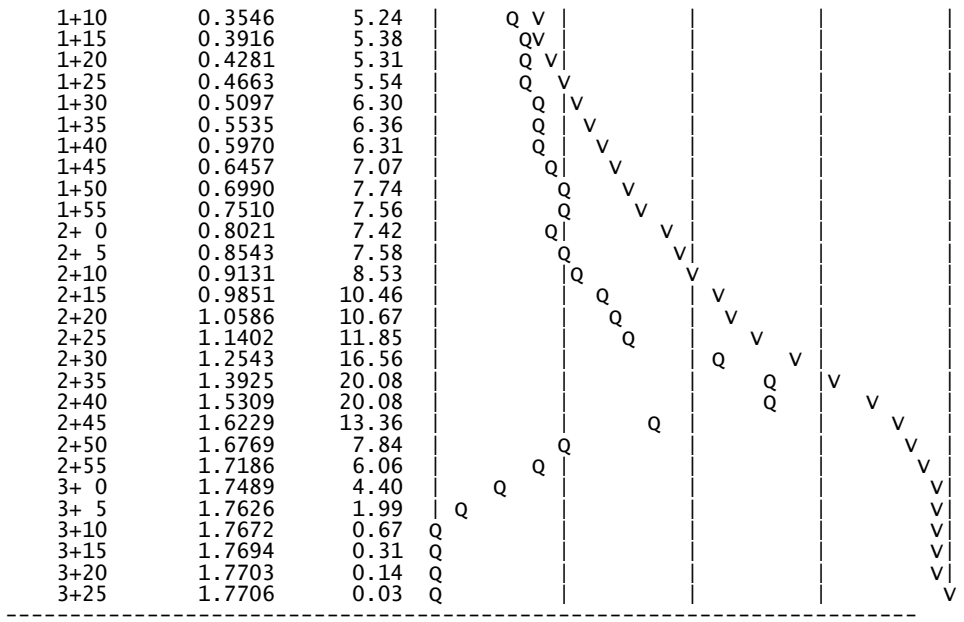
Peak flow rate of this hydrograph = 20.084(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0066	0.95	VQ				
0+10	0.0239	2.52	V Q				
0+15	0.0430	2.77	V Q				
0+20	0.0636	3.00	V Q				
0+25	0.0878	3.51	V Q				
0+30	0.1147	3.90	V Q				
0+35	0.1428	4.08	V Q				
0+40	0.1707	4.05	V Q				
0+45	0.2008	4.38	VQ				
0+50	0.2300	4.23	Q				
0+55	0.2574	3.98	Q				
1+ 0	0.2861	4.16	QV				
1+ 5	0.3185	4.70	QV				



1+10	0.3546	5.24	
1+15	0.3916	5.38	
1+20	0.4281	5.31	
1+25	0.4663	5.54	
1+30	0.5097	6.30	
1+35	0.5535	6.36	
1+40	0.5970	6.31	
1+45	0.6457	7.07	
1+50	0.6990	7.74	
1+55	0.7510	7.56	
2+ 0	0.8021	7.42	
2+ 5	0.8543	7.58	
2+10	0.9131	8.53	
2+15	0.9851	10.46	
2+20	1.0586	10.67	
2+25	1.1402	11.85	
2+30	1.2543	16.56	
2+35	1.3925	20.08	
2+40	1.5309	20.08	
2+45	1.6229	13.36	
2+50	1.6769	7.84	
2+55	1.7186	6.06	
3+ 0	1.7489	4.40	
3+ 5	1.7626	1.99	
3+10	1.7672	0.67	
3+15	1.7694	0.31	
3+20	1.7703	0.14	
3+25	1.7706	0.03	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro2262.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2976.00(Ft.)
Length along longest watercourse measured to centroid = 1488.00(Ft.)
Length along longest watercourse = 0.564 Mi.
Length along longest watercourse measured to centroid = 0.282 Mi.
Difference in elevation = 150.00(Ft.)
Slope along watercourse = 266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.062 Hr.
Lag time = 3.72 Min.
25% of lag time = 0.93 Min.
40% of lag time = 1.49 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	1.10	56.98

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	3.00	155.40

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.100(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 1.100(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	69.00	0.500

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.066	(0.316)	0.033	0.033
2	0.17	0.60	0.079	(0.316)	0.040	0.040
3	0.25	0.60	0.079	(0.316)	0.040	0.040
4	0.33	0.60	0.079	(0.316)	0.040	0.040
5	0.42	0.60	0.079	(0.316)	0.040	0.040
6	0.50	0.70	0.092	(0.316)	0.046	0.046
7	0.58	0.70	0.092	(0.316)	0.046	0.046
8	0.67	0.70	0.092	(0.316)	0.046	0.046
9	0.75	0.70	0.092	(0.316)	0.046	0.046
10	0.83	0.70	0.092	(0.316)	0.046	0.046
11	0.92	0.70	0.092	(0.316)	0.046	0.046
12	1.00	0.80	0.106	(0.316)	0.053	0.053
13	1.08	0.80	0.106	(0.316)	0.053	0.053
14	1.17	0.80	0.106	(0.316)	0.053	0.053
15	1.25	0.80	0.106	(0.316)	0.053	0.053
16	1.33	0.80	0.106	(0.316)	0.053	0.053
17	1.42	0.80	0.106	(0.316)	0.053	0.053
18	1.50	0.80	0.106	(0.316)	0.053	0.053
19	1.58	0.80	0.106	(0.316)	0.053	0.053
20	1.67	0.80	0.106	(0.316)	0.053	0.053
21	1.75	0.80	0.106	(0.316)	0.053	0.053
22	1.83	0.80	0.106	(0.316)	0.053	0.053
23	1.92	0.80	0.106	(0.316)	0.053	0.053
24	2.00	0.90	0.119	(0.316)	0.059	0.059
25	2.08	0.80	0.106	(0.316)	0.053	0.053
26	2.17	0.90	0.119	(0.316)	0.059	0.059
27	2.25	0.90	0.119	(0.316)	0.059	0.059
28	2.33	0.90	0.119	(0.316)	0.059	0.059
29	2.42	0.90	0.119	(0.316)	0.059	0.059
30	2.50	0.90	0.119	(0.316)	0.059	0.059
31	2.58	0.90	0.119	(0.316)	0.059	0.059
32	2.67	0.90	0.119	(0.316)	0.059	0.059
33	2.75	1.00	0.132	(0.316)	0.066	0.066
34	2.83	1.00	0.132	(0.316)	0.066	0.066
35	2.92	1.00	0.132	(0.316)	0.066	0.066
36	3.00	1.00	0.132	(0.316)	0.066	0.066
37	3.08	1.00	0.132	(0.316)	0.066	0.066
38	3.17	1.10	0.145	(0.316)	0.073	0.073
39	3.25	1.10	0.145	(0.316)	0.073	0.073
40	3.33	1.10	0.145	(0.316)	0.073	0.073
41	3.42	1.20	0.158	(0.316)	0.079	0.079
42	3.50	1.30	0.172	(0.316)	0.086	0.086
43	3.58	1.40	0.185	(0.316)	0.092	0.092
44	3.67	1.40	0.185	(0.316)	0.092	0.092
45	3.75	1.50	0.198	(0.316)	0.099	0.099
46	3.83	1.50	0.198	(0.316)	0.099	0.099
47	3.92	1.60	0.211	(0.316)	0.106	0.106
48	4.00	1.60	0.211	(0.316)	0.106	0.106
49	4.08	1.70	0.224	(0.316)	0.112	0.112
50	4.17	1.80	0.238	(0.316)	0.119	0.119
51	4.25	1.90	0.251	(0.316)	0.125	0.125
52	4.33	2.00	0.264	(0.316)	0.132	0.132
53	4.42	2.10	0.277	(0.316)	0.139	0.139
54	4.50	2.10	0.277	(0.316)	0.139	0.139
55	4.58	2.20	0.290	(0.316)	0.145	0.145
56	4.67	2.30	0.304	(0.316)	0.152	0.152
57	4.75	2.40	0.317	(0.316)	0.158	0.158
58	4.83	2.40	0.317	(0.316)	0.158	0.158
59	4.92	2.50	0.330	(0.316)	0.165	0.165
60	5.00	2.60	0.343	(0.316)	0.172	0.172
61	5.08	3.10	0.409	(0.316)	0.205	0.205
62	5.17	3.60	0.475	(0.316)	0.238	0.238
63	5.25	3.90	0.515	(0.316)	0.257	0.257
64	5.33	4.20	0.554	(0.316)	0.277	0.277
65	5.42	4.70	0.620	(0.316)	0.310	0.310
66	5.50	5.60	0.739	0.316	(0.370)	0.423
67	5.58	1.90	0.251	(0.316)	0.125	0.125
68	5.67	0.90	0.119	(0.316)	0.059	0.059
69	5.75	0.60	0.079	(0.316)	0.040	0.040
70	5.83	0.50	0.066	(0.316)	0.033	0.033

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71   5.92     0.30      0.040       (  0.316)       0.020        0.020
72   6.00     0.20      0.026       (  0.316)       0.013        0.013
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =     6.7
      Flood volume = Effective rainfall      0.55(In)
       times area      51.8(Ac.)/[(In)/(Ft.)] =       2.4(Ac.Ft)
      Total soil loss =      0.55(In)
      Total soil loss =     2.354(Ac.Ft)
      Total rainfall =      1.10(In)
      Flood volume =      104244.2 Cubic Feet
      Total soil loss =      102556.4 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     17.339(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
-------------------------------------------------------------------------
  0+ 5       0.0035      0.50  VQ        |         |         |         |
  0+10       0.0133      1.43  V Q       |         |         |         |
  0+15       0.0258      1.81  V  Q      |         |         |         |
  0+20       0.0392      1.94  V  Q      |         |         |         |
  0+25       0.0530      2.01  V   Q     |         |         |         |
  0+30       0.0679      2.16  |V  Q     |         |         |         |
  0+35       0.0840      2.33  |V  Q     |         |         |         |
  0+40       0.1004      2.38  |V  Q     |         |         |         |
  0+45       0.1169      2.39  |V  Q     |         |         |         |
  0+50       0.1334      2.41  | V Q     |         |         |         |
  0+55       0.1500      2.41  | V Q     |         |         |         |
  1+ 0       0.1674      2.51  | V  Q    |         |         |         |
  1+ 5       0.1858      2.68  |  V Q    |         |         |         |
  1+10       0.2045      2.72  |  V Q    |         |         |         |
  1+15       0.2234      2.74  |  V Q    |         |         |         |
  1+20       0.2423      2.75  |   VQ    |         |         |         |
  1+25       0.2613      2.76  |   VQ    |         |         |         |
  1+30       0.2803      2.76  |   VQ    |         |         |         |
  1+35       0.2993      2.76  |    Q    |         |         |         |
  1+40       0.3183      2.76  |    Q    |         |         |         |
  1+45       0.3373      2.76  |    Q    |         |         |         |
  1+50       0.3563      2.76  |    Q    |         |         |         |
  1+55       0.3753      2.76  |    QV   |         |         |         |
  2+ 0       0.3950      2.86  |    QV   |         |         |         |
  2+ 5       0.4151      2.92  |    QV   |         |         |         |
  2+10       0.4351      2.90  |    Q V  |         |         |         |
  2+15       0.4560      3.04  |     QV  |         |         |         |
  2+20       0.4772      3.08  |     QV  |         |         |         |
  2+25       0.4985      3.09  |     Q V |         |         |         |
  2+30       0.5198      3.09  |     Q V |         |         |         |
  2+35       0.5412      3.10  |     Q  V|         |         |         |
  2+40       0.5625      3.10  |     Q  V|         |         |         |
  2+45       0.5846      3.20  |     Q  V|         |         |         |
  2+50       0.6078      3.37  |     Q   V         |         |         |
  2+55       0.6313      3.41  |     Q   V         |         |         |
  3+ 0       0.6549      3.43  |     Q   V         |         |         |
  3+ 5       0.6786      3.44  |     Q   |V        |         |         |
  3+10       0.7030      3.55  |      Q  |V        |         |         |
  3+15       0.7286      3.71  |      Q  | V       |         |         |
  3+20       0.7544      3.76  |      Q  | V       |         |         |
  3+25       0.7811      3.87  |      Q  |  V      |         |         |
  3+30       0.8097      4.15  |       Q |  V      |         |         |
  3+35       0.8405      4.47  |       Q |   V     |         |         |
  3+40       0.8728      4.69  |        Q|   V     |         |         |
  3+45       0.9063      4.86  |        Q|    V    |         |         |
  3+50       0.9412      5.07  |         Q    V    |         |         |
  3+55       0.9772      5.23  |         Q     V   |         |         |
  4+ 0       1.0145      5.42  |         Q     V   |         |         |
  4+ 5       1.0529      5.57  |         |Q     V  |         |         |
  4+10       1.0933      5.86  |         |Q      V |         |         |
  4+15       1.1359      6.18  |         | Q     V |         |         |
  4+20       1.1807      6.52  |         |  Q     V|         |         |
  4+25       1.2279      6.85  |         |  Q      V         |         |
  4+30       1.2768      7.10  |         |   Q     |V        |         |
  4+35       1.3270      7.28  |         |   Q     | V       |         |
  4+40       1.3792      7.58  |         |    Q    |  V      |         |
  4+45       1.4336      7.91  |         |    Q    |  V      |         |
  4+50       1.4897      8.14  |         |     Q   |   V     |         |
  4+55       1.5469      8.31  |         |     Q   |    V    |         |
  5+ 0       1.6062      8.61  |         |      Q  |     V   |         |
  5+ 5       1.6706      9.34  |         |       Q |      V  |         |
  5+10       1.7446     10.74  |         |         |Q       V|         |
  5+15       1.8280     12.11  |         |         |  Q     V |         |
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    5+20       1.9191     13.23  |          |          |      Q   | V         |
    5+25       2.0191     14.51  |          |          |         Q|  V        |
    5+30       2.1385     17.34  |          |          |          |   QV      |
    5+35       2.2484     15.96  |          |          |          |Q      V   |
    5+40       2.3058      8.34  |          |      Q   |          |         V |
    5+45       2.3394      4.88  |          |Q         |          |          V|
    5+50       2.3617      3.23  |        Q |          |          |          V|
    5+55       2.3771      2.23  |      Q   |          |          |          V|
    6+ 0       2.3857      1.25  |  Q       |          |          |          V|
    6+ 5       2.3904      0.68  | Q        |          |          |          V|
    6+10       2.3920      0.24  |Q         |          |          |          V|
    6+15       2.3927      0.11  |Q         |          |          |          V|
    6+20       2.3930      0.04  |Q         |          |          |          V|
    6+25       2.3931      0.02  |Q         |          |          |          V|
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro22242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2976.00(Ft.)
Length along longest watercourse measured to centroid = 1488.00(Ft.)
Length along longest watercourse = 0.564 Mi.
Length along longest watercourse measured to centroid = 0.282 Mi.
Difference in elevation = 150.00(Ft.)
Slope along watercourse = 266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.062 Hr.
Lag time = 3.72 Min.
25% of lag time = 0.93 Min.
40% of lag time = 1.49 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	1.80	93.24

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	5.00	259.00

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 1.800(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 1.800(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	69.00	0.500

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.014	(0.560)	0.007	0.007
2	0.17	0.07	0.014	(0.557)	0.007	0.007
3	0.25	0.07	0.014	(0.555)	0.007	0.007
4	0.33	0.10	0.022	(0.553)	0.011	0.011
5	0.42	0.10	0.022	(0.551)	0.011	0.011
6	0.50	0.10	0.022	(0.549)	0.011	0.011
7	0.58	0.10	0.022	(0.547)	0.011	0.011
8	0.67	0.10	0.022	(0.545)	0.011	0.011
9	0.75	0.10	0.022	(0.542)	0.011	0.011
10	0.83	0.13	0.029	(0.540)	0.014	0.014
11	0.92	0.13	0.029	(0.538)	0.014	0.014
12	1.00	0.13	0.029	(0.536)	0.014	0.014
13	1.08	0.10	0.022	(0.534)	0.011	0.011
14	1.17	0.10	0.022	(0.532)	0.011	0.011
15	1.25	0.10	0.022	(0.530)	0.011	0.011
16	1.33	0.10	0.022	(0.528)	0.011	0.011
17	1.42	0.10	0.022	(0.525)	0.011	0.011
18	1.50	0.10	0.022	(0.523)	0.011	0.011
19	1.58	0.10	0.022	(0.521)	0.011	0.011
20	1.67	0.10	0.022	(0.519)	0.011	0.011
21	1.75	0.10	0.022	(0.517)	0.011	0.011
22	1.83	0.13	0.029	(0.515)	0.014	0.014
23	1.92	0.13	0.029	(0.513)	0.014	0.014
24	2.00	0.13	0.029	(0.511)	0.014	0.014
25	2.08	0.13	0.029	(0.509)	0.014	0.014
26	2.17	0.13	0.029	(0.507)	0.014	0.014
27	2.25	0.13	0.029	(0.505)	0.014	0.014
28	2.33	0.13	0.029	(0.503)	0.014	0.014
29	2.42	0.13	0.029	(0.501)	0.014	0.014
30	2.50	0.13	0.029	(0.499)	0.014	0.014
31	2.58	0.17	0.036	(0.497)	0.018	0.018
32	2.67	0.17	0.036	(0.494)	0.018	0.018
33	2.75	0.17	0.036	(0.492)	0.018	0.018
34	2.83	0.17	0.036	(0.490)	0.018	0.018
35	2.92	0.17	0.036	(0.488)	0.018	0.018
36	3.00	0.17	0.036	(0.486)	0.018	0.018
37	3.08	0.17	0.036	(0.484)	0.018	0.018
38	3.17	0.17	0.036	(0.482)	0.018	0.018
39	3.25	0.17	0.036	(0.480)	0.018	0.018
40	3.33	0.17	0.036	(0.478)	0.018	0.018
41	3.42	0.17	0.036	(0.476)	0.018	0.018
42	3.50	0.17	0.036	(0.474)	0.018	0.018
43	3.58	0.17	0.036	(0.472)	0.018	0.018
44	3.67	0.17	0.036	(0.470)	0.018	0.018
45	3.75	0.17	0.036	(0.468)	0.018	0.018
46	3.83	0.20	0.043	(0.466)	0.022	0.022
47	3.92	0.20	0.043	(0.464)	0.022	0.022
48	4.00	0.20	0.043	(0.463)	0.022	0.022
49	4.08	0.20	0.043	(0.461)	0.022	0.022
50	4.17	0.20	0.043	(0.459)	0.022	0.022
51	4.25	0.20	0.043	(0.457)	0.022	0.022
52	4.33	0.23	0.050	(0.455)	0.025	0.025
53	4.42	0.23	0.050	(0.453)	0.025	0.025
54	4.50	0.23	0.050	(0.451)	0.025	0.025
55	4.58	0.23	0.050	(0.449)	0.025	0.025
56	4.67	0.23	0.050	(0.447)	0.025	0.025
57	4.75	0.23	0.050	(0.445)	0.025	0.025
58	4.83	0.27	0.058	(0.443)	0.029	0.029
59	4.92	0.27	0.058	(0.441)	0.029	0.029
60	5.00	0.27	0.058	(0.439)	0.029	0.029

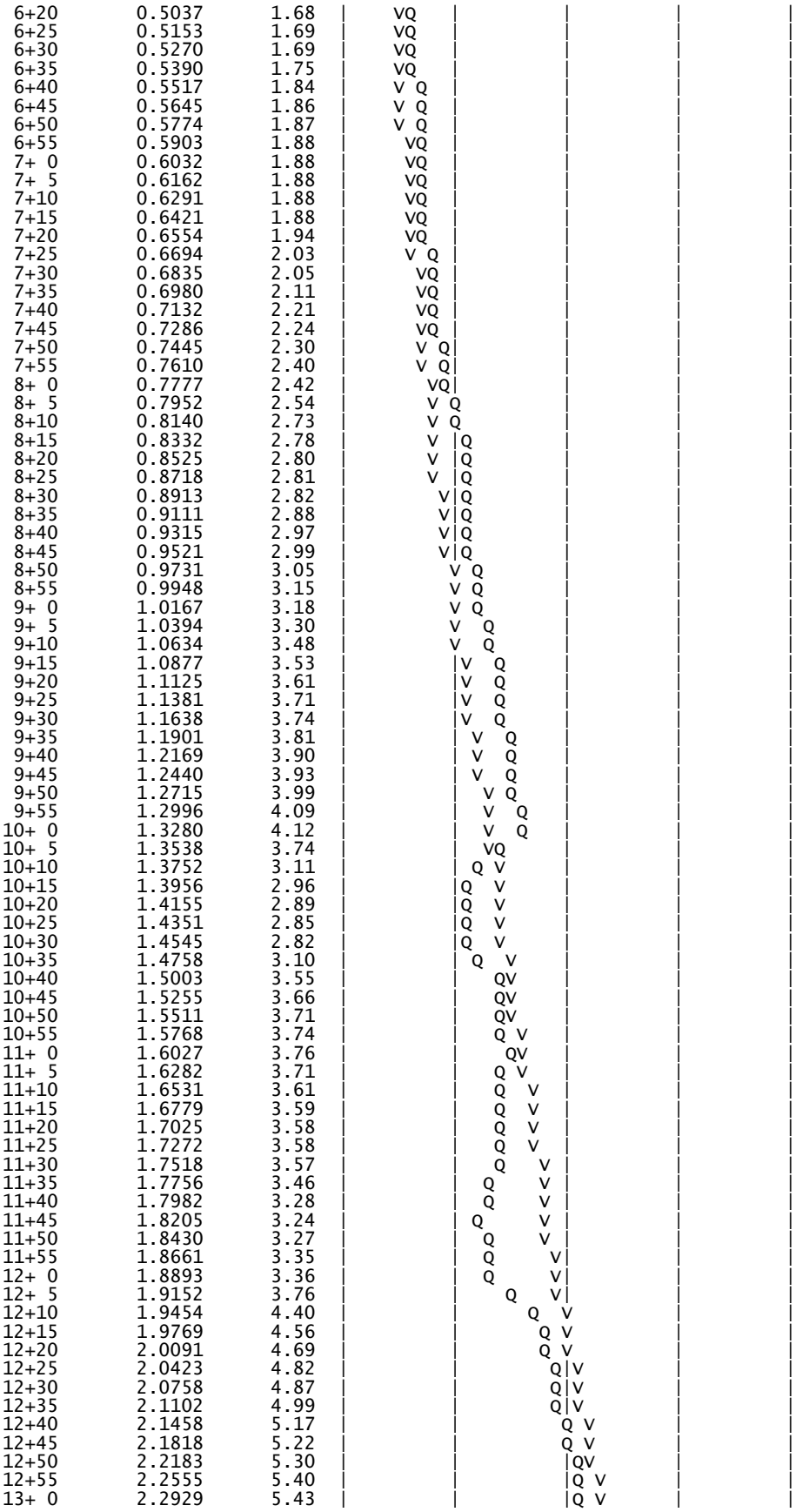
61	5.08	0.20	0.043	(0.437)	0.022	0.022
62	5.17	0.20	0.043	(0.435)	0.022	0.022
63	5.25	0.20	0.043	(0.434)	0.022	0.022
64	5.33	0.23	0.050	(0.432)	0.025	0.025
65	5.42	0.23	0.050	(0.430)	0.025	0.025
66	5.50	0.23	0.050	(0.428)	0.025	0.025
67	5.58	0.27	0.058	(0.426)	0.029	0.029
68	5.67	0.27	0.058	(0.424)	0.029	0.029
69	5.75	0.27	0.058	(0.422)	0.029	0.029
70	5.83	0.27	0.058	(0.420)	0.029	0.029
71	5.92	0.27	0.058	(0.419)	0.029	0.029
72	6.00	0.27	0.058	(0.417)	0.029	0.029
73	6.08	0.30	0.065	(0.415)	0.032	0.032
74	6.17	0.30	0.065	(0.413)	0.032	0.032
75	6.25	0.30	0.065	(0.411)	0.032	0.032
76	6.33	0.30	0.065	(0.409)	0.032	0.032
77	6.42	0.30	0.065	(0.407)	0.032	0.032
78	6.50	0.30	0.065	(0.406)	0.032	0.032
79	6.58	0.33	0.072	(0.404)	0.036	0.036
80	6.67	0.33	0.072	(0.402)	0.036	0.036
81	6.75	0.33	0.072	(0.400)	0.036	0.036
82	6.83	0.33	0.072	(0.398)	0.036	0.036
83	6.92	0.33	0.072	(0.397)	0.036	0.036
84	7.00	0.33	0.072	(0.395)	0.036	0.036
85	7.08	0.33	0.072	(0.393)	0.036	0.036
86	7.17	0.33	0.072	(0.391)	0.036	0.036
87	7.25	0.33	0.072	(0.389)	0.036	0.036
88	7.33	0.37	0.079	(0.388)	0.040	0.040
89	7.42	0.37	0.079	(0.386)	0.040	0.040
90	7.50	0.37	0.079	(0.384)	0.040	0.040
91	7.58	0.40	0.086	(0.382)	0.043	0.043
92	7.67	0.40	0.086	(0.381)	0.043	0.043
93	7.75	0.40	0.086	(0.379)	0.043	0.043
94	7.83	0.43	0.094	(0.377)	0.047	0.047
95	7.92	0.43	0.094	(0.375)	0.047	0.047
96	8.00	0.43	0.094	(0.374)	0.047	0.047
97	8.08	0.50	0.108	(0.372)	0.054	0.054
98	8.17	0.50	0.108	(0.370)	0.054	0.054
99	8.25	0.50	0.108	(0.368)	0.054	0.054
100	8.33	0.50	0.108	(0.367)	0.054	0.054
101	8.42	0.50	0.108	(0.365)	0.054	0.054
102	8.50	0.50	0.108	(0.363)	0.054	0.054
103	8.58	0.53	0.115	(0.362)	0.058	0.058
104	8.67	0.53	0.115	(0.360)	0.058	0.058
105	8.75	0.53	0.115	(0.358)	0.058	0.058
106	8.83	0.57	0.122	(0.356)	0.061	0.061
107	8.92	0.57	0.122	(0.355)	0.061	0.061
108	9.00	0.57	0.122	(0.353)	0.061	0.061
109	9.08	0.63	0.137	(0.351)	0.068	0.068
110	9.17	0.63	0.137	(0.350)	0.068	0.068
111	9.25	0.63	0.137	(0.348)	0.068	0.068
112	9.33	0.67	0.144	(0.346)	0.072	0.072
113	9.42	0.67	0.144	(0.345)	0.072	0.072
114	9.50	0.67	0.144	(0.343)	0.072	0.072
115	9.58	0.70	0.151	(0.341)	0.076	0.076
116	9.67	0.70	0.151	(0.340)	0.076	0.076
117	9.75	0.70	0.151	(0.338)	0.076	0.076
118	9.83	0.73	0.158	(0.337)	0.079	0.079
119	9.92	0.73	0.158	(0.335)	0.079	0.079
120	10.00	0.73	0.158	(0.333)	0.079	0.079
121	10.08	0.50	0.108	(0.332)	0.054	0.054
122	10.17	0.50	0.108	(0.330)	0.054	0.054
123	10.25	0.50	0.108	(0.329)	0.054	0.054
124	10.33	0.50	0.108	(0.327)	0.054	0.054
125	10.42	0.50	0.108	(0.325)	0.054	0.054
126	10.50	0.50	0.108	(0.324)	0.054	0.054
127	10.58	0.67	0.144	(0.322)	0.072	0.072
128	10.67	0.67	0.144	(0.321)	0.072	0.072
129	10.75	0.67	0.144	(0.319)	0.072	0.072
130	10.83	0.67	0.144	(0.317)	0.072	0.072
131	10.92	0.67	0.144	(0.316)	0.072	0.072
132	11.00	0.67	0.144	(0.314)	0.072	0.072
133	11.08	0.63	0.137	(0.313)	0.068	0.068
134	11.17	0.63	0.137	(0.311)	0.068	0.068
135	11.25	0.63	0.137	(0.310)	0.068	0.068
136	11.33	0.63	0.137	(0.308)	0.068	0.068
137	11.42	0.63	0.137	(0.307)	0.068	0.068
138	11.50	0.63	0.137	(0.305)	0.068	0.068
139	11.58	0.57	0.122	(0.304)	0.061	0.061
140	11.67	0.57	0.122	(0.302)	0.061	0.061
141	11.75	0.57	0.122	(0.301)	0.061	0.061

142	11.83	0.60	0.130	(0.299)	0.065	0.065
143	11.92	0.60	0.130	(0.298)	0.065	0.065
144	12.00	0.60	0.130	(0.296)	0.065	0.065
145	12.08	0.83	0.180	(0.295)	0.090	0.090
146	12.17	0.83	0.180	(0.293)	0.090	0.090
147	12.25	0.83	0.180	(0.292)	0.090	0.090
148	12.33	0.87	0.187	(0.290)	0.094	0.094
149	12.42	0.87	0.187	(0.289)	0.094	0.094
150	12.50	0.87	0.187	(0.287)	0.094	0.094
151	12.58	0.93	0.202	(0.286)	0.101	0.101
152	12.67	0.93	0.202	(0.284)	0.101	0.101
153	12.75	0.93	0.202	(0.283)	0.101	0.101
154	12.83	0.97	0.209	(0.282)	0.104	0.104
155	12.92	0.97	0.209	(0.280)	0.104	0.104
156	13.00	0.97	0.209	(0.279)	0.104	0.104
157	13.08	1.13	0.245	(0.277)	0.122	0.122
158	13.17	1.13	0.245	(0.276)	0.122	0.122
159	13.25	1.13	0.245	(0.275)	0.122	0.122
160	13.33	1.13	0.245	(0.273)	0.122	0.122
161	13.42	1.13	0.245	(0.272)	0.122	0.122
162	13.50	1.13	0.245	(0.270)	0.122	0.122
163	13.58	0.77	0.166	(0.269)	0.083	0.083
164	13.67	0.77	0.166	(0.268)	0.083	0.083
165	13.75	0.77	0.166	(0.266)	0.083	0.083
166	13.83	0.77	0.166	(0.265)	0.083	0.083
167	13.92	0.77	0.166	(0.264)	0.083	0.083
168	14.00	0.77	0.166	(0.262)	0.083	0.083
169	14.08	0.90	0.194	(0.261)	0.097	0.097
170	14.17	0.90	0.194	(0.260)	0.097	0.097
171	14.25	0.90	0.194	(0.258)	0.097	0.097
172	14.33	0.87	0.187	(0.257)	0.094	0.094
173	14.42	0.87	0.187	(0.256)	0.094	0.094
174	14.50	0.87	0.187	(0.254)	0.094	0.094
175	14.58	0.87	0.187	(0.253)	0.094	0.094
176	14.67	0.87	0.187	(0.252)	0.094	0.094
177	14.75	0.87	0.187	(0.250)	0.094	0.094
178	14.83	0.83	0.180	(0.249)	0.090	0.090
179	14.92	0.83	0.180	(0.248)	0.090	0.090
180	15.00	0.83	0.180	(0.247)	0.090	0.090
181	15.08	0.80	0.173	(0.245)	0.086	0.086
182	15.17	0.80	0.173	(0.244)	0.086	0.086
183	15.25	0.80	0.173	(0.243)	0.086	0.086
184	15.33	0.77	0.166	(0.242)	0.083	0.083
185	15.42	0.77	0.166	(0.240)	0.083	0.083
186	15.50	0.77	0.166	(0.239)	0.083	0.083
187	15.58	0.63	0.137	(0.238)	0.068	0.068
188	15.67	0.63	0.137	(0.237)	0.068	0.068
189	15.75	0.63	0.137	(0.235)	0.068	0.068
190	15.83	0.63	0.137	(0.234)	0.068	0.068
191	15.92	0.63	0.137	(0.233)	0.068	0.068
192	16.00	0.63	0.137	(0.232)	0.068	0.068
193	16.08	0.13	0.029	(0.231)	0.014	0.014
194	16.17	0.13	0.029	(0.229)	0.014	0.014
195	16.25	0.13	0.029	(0.228)	0.014	0.014
196	16.33	0.13	0.029	(0.227)	0.014	0.014
197	16.42	0.13	0.029	(0.226)	0.014	0.014
198	16.50	0.13	0.029	(0.225)	0.014	0.014
199	16.58	0.10	0.022	(0.224)	0.011	0.011
200	16.67	0.10	0.022	(0.223)	0.011	0.011
201	16.75	0.10	0.022	(0.221)	0.011	0.011
202	16.83	0.10	0.022	(0.220)	0.011	0.011
203	16.92	0.10	0.022	(0.219)	0.011	0.011
204	17.00	0.10	0.022	(0.218)	0.011	0.011
205	17.08	0.17	0.036	(0.217)	0.018	0.018
206	17.17	0.17	0.036	(0.216)	0.018	0.018
207	17.25	0.17	0.036	(0.215)	0.018	0.018
208	17.33	0.17	0.036	(0.214)	0.018	0.018
209	17.42	0.17	0.036	(0.213)	0.018	0.018
210	17.50	0.17	0.036	(0.212)	0.018	0.018
211	17.58	0.17	0.036	(0.211)	0.018	0.018
212	17.67	0.17	0.036	(0.209)	0.018	0.018
213	17.75	0.17	0.036	(0.208)	0.018	0.018
214	17.83	0.13	0.029	(0.207)	0.014	0.014
215	17.92	0.13	0.029	(0.206)	0.014	0.014
216	18.00	0.13	0.029	(0.205)	0.014	0.014
217	18.08	0.13	0.029	(0.204)	0.014	0.014
218	18.17	0.13	0.029	(0.203)	0.014	0.014
219	18.25	0.13	0.029	(0.202)	0.014	0.014
220	18.33	0.13	0.029	(0.201)	0.014	0.014
221	18.42	0.13	0.029	(0.200)	0.014	0.014
222	18.50	0.13	0.029	(0.199)	0.014	0.014

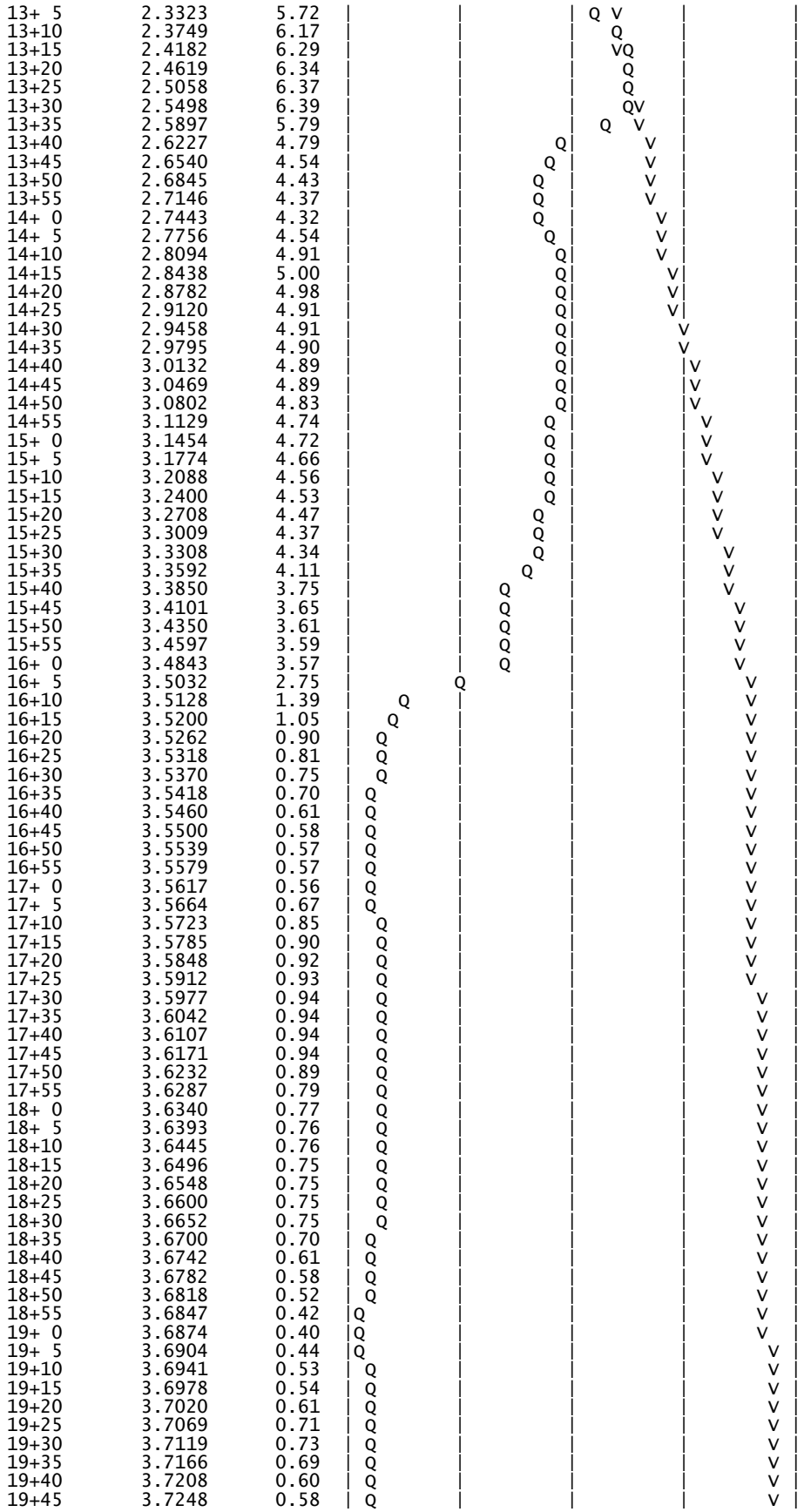
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223  18.58     0.10      0.022       (  0.198)       0.011        0.011
224  18.67     0.10      0.022       (  0.197)       0.011        0.011
225  18.75     0.10      0.022       (  0.197)       0.011        0.011
226  18.83     0.07      0.014       (  0.196)       0.007        0.007
227  18.92     0.07      0.014       (  0.195)       0.007        0.007
228  19.00     0.07      0.014       (  0.194)       0.007        0.007
229  19.08     0.10      0.022       (  0.193)       0.011        0.011
230  19.17     0.10      0.022       (  0.192)       0.011        0.011
231  19.25     0.10      0.022       (  0.191)       0.011        0.011
232  19.33     0.13      0.029       (  0.190)       0.014        0.014
233  19.42     0.13      0.029       (  0.189)       0.014        0.014
234  19.50     0.13      0.029       (  0.188)       0.014        0.014
235  19.58     0.10      0.022       (  0.187)       0.011        0.011
236  19.67     0.10      0.022       (  0.187)       0.011        0.011
237  19.75     0.10      0.022       (  0.186)       0.011        0.011
238  19.83     0.07      0.014       (  0.185)       0.007        0.007
239  19.92     0.07      0.014       (  0.184)       0.007        0.007
240  20.00     0.07      0.014       (  0.183)       0.007        0.007
241  20.08     0.10      0.022       (  0.182)       0.011        0.011
242  20.17     0.10      0.022       (  0.182)       0.011        0.011
243  20.25     0.10      0.022       (  0.181)       0.011        0.011
244  20.33     0.10      0.022       (  0.180)       0.011        0.011
245  20.42     0.10      0.022       (  0.179)       0.011        0.011
246  20.50     0.10      0.022       (  0.179)       0.011        0.011
247  20.58     0.10      0.022       (  0.178)       0.011        0.011
248  20.67     0.10      0.022       (  0.177)       0.011        0.011
249  20.75     0.10      0.022       (  0.176)       0.011        0.011
250  20.83     0.07      0.014       (  0.176)       0.007        0.007
251  20.92     0.07      0.014       (  0.175)       0.007        0.007
252  21.00     0.07      0.014       (  0.174)       0.007        0.007
253  21.08     0.10      0.022       (  0.174)       0.011        0.011
254  21.17     0.10      0.022       (  0.173)       0.011        0.011
255  21.25     0.10      0.022       (  0.172)       0.011        0.011
256  21.33     0.07      0.014       (  0.172)       0.007        0.007
257  21.42     0.07      0.014       (  0.171)       0.007        0.007
258  21.50     0.07      0.014       (  0.170)       0.007        0.007
259  21.58     0.10      0.022       (  0.170)       0.011        0.011
260  21.67     0.10      0.022       (  0.169)       0.011        0.011
261  21.75     0.10      0.022       (  0.168)       0.011        0.011
262  21.83     0.07      0.014       (  0.168)       0.007        0.007
263  21.92     0.07      0.014       (  0.167)       0.007        0.007
264  22.00     0.07      0.014       (  0.167)       0.007        0.007
265  22.08     0.10      0.022       (  0.166)       0.011        0.011
266  22.17     0.10      0.022       (  0.166)       0.011        0.011
267  22.25     0.10      0.022       (  0.165)       0.011        0.011
268  22.33     0.07      0.014       (  0.165)       0.007        0.007
269  22.42     0.07      0.014       (  0.164)       0.007        0.007
270  22.50     0.07      0.014       (  0.164)       0.007        0.007
271  22.58     0.07      0.014       (  0.163)       0.007        0.007
272  22.67     0.07      0.014       (  0.163)       0.007        0.007
273  22.75     0.07      0.014       (  0.162)       0.007        0.007
274  22.83     0.07      0.014       (  0.162)       0.007        0.007
275  22.92     0.07      0.014       (  0.161)       0.007        0.007
276  23.00     0.07      0.014       (  0.161)       0.007        0.007
277  23.08     0.07      0.014       (  0.161)       0.007        0.007
278  23.17     0.07      0.014       (  0.160)       0.007        0.007
279  23.25     0.07      0.014       (  0.160)       0.007        0.007
280  23.33     0.07      0.014       (  0.160)       0.007        0.007
281  23.42     0.07      0.014       (  0.159)       0.007        0.007
282  23.50     0.07      0.014       (  0.159)       0.007        0.007
283  23.58     0.07      0.014       (  0.159)       0.007        0.007
284  23.67     0.07      0.014       (  0.158)       0.007        0.007
285  23.75     0.07      0.014       (  0.158)       0.007        0.007
286  23.83     0.07      0.014       (  0.158)       0.007        0.007
287  23.92     0.07      0.014       (  0.158)       0.007        0.007
288  24.00     0.07      0.014       (  0.158)       0.007        0.007
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    10.8
      Flood volume = Effective rainfall      0.90(In)
       times area      51.8(Ac.)/[(In)/(Ft.)] =       3.9(Ac.Ft)
      Total soil loss =      0.90(In)
      Total soil loss =     3.885(Ac.Ft)
      Total rainfall =      1.80(In)
      Flood volume =      169213.5 Cubic Feet
      Total soil loss =      169213.5 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      6.393(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f     H y d r o g r a p h
```

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0008	0.11	Q				
0+10	0.0028	0.29	VQ				
0+15	0.0051	0.34	VQ				
0+20	0.0079	0.41	VQ				
0+25	0.0114	0.51	V Q				
0+30	0.0152	0.54	V Q				
0+35	0.0190	0.55	V Q				
0+40	0.0229	0.56	V Q				
0+45	0.0268	0.56	V Q				
0+50	0.0310	0.62	V Q				
0+55	0.0359	0.71	V Q				
1+ 0	0.0409	0.73	V Q				
1+ 5	0.0457	0.69	V Q				
1+10	0.0498	0.60	V Q				
1+15	0.0539	0.58	V Q				
1+20	0.0578	0.57	V Q				
1+25	0.0617	0.57	V Q				
1+30	0.0656	0.56	V Q				
1+35	0.0695	0.56	V Q				
1+40	0.0734	0.56	V Q				
1+45	0.0773	0.56	V Q				
1+50	0.0815	0.62	V Q				
1+55	0.0864	0.71	V Q				
2+ 0	0.0914	0.73	V Q				
2+ 5	0.0966	0.74	V Q				
2+10	0.1017	0.75	|VQ				
2+15	0.1069	0.75	|V Q				
2+20	0.1121	0.75	|V Q				
2+25	0.1172	0.75	|V Q				
2+30	0.1224	0.75	|V Q				
2+35	0.1280	0.81	|V Q				
2+40	0.1342	0.90	|V Q				
2+45	0.1405	0.92	|V Q				
2+50	0.1469	0.93	|V Q				
2+55	0.1534	0.94	|V Q				
3+ 0	0.1598	0.94	|V Q				
3+ 5	0.1663	0.94	|V Q				
3+10	0.1728	0.94	|V Q				
3+15	0.1793	0.94	|V Q				
3+20	0.1857	0.94	|V Q				
3+25	0.1922	0.94	|V Q				
3+30	0.1987	0.94	| VQ				
3+35	0.2052	0.94	| VQ				
3+40	0.2116	0.94	| VQ				
3+45	0.2181	0.94	| VQ				
3+50	0.2250	1.00	| VQ				
3+55	0.2324	1.09	| V Q				
4+ 0	0.2401	1.11	| V Q				
4+ 5	0.2478	1.12	| V Q				
4+10	0.2555	1.12	| V Q				
4+15	0.2633	1.13	| V Q				
4+20	0.2714	1.18	| V Q				
4+25	0.2802	1.27	| V Q				
4+30	0.2891	1.30	| V Q				
4+35	0.2981	1.31	| V Q				
4+40	0.3072	1.31	| V Q				
4+45	0.3162	1.32	| V Q				
4+50	0.3257	1.37	| V Q				
4+55	0.3357	1.46	| V Q				
5+ 0	0.3459	1.48	| V Q				
5+ 5	0.3555	1.38	| V Q				
5+10	0.3638	1.21	| VQ				
5+15	0.3719	1.17	| VQ				
5+20	0.3801	1.20	| VQ				
5+25	0.3890	1.28	| VQ				
5+30	0.3979	1.30	| VQ				
5+35	0.4073	1.36	| VQ				
5+40	0.4173	1.46	| VQ				
5+45	0.4275	1.48	| VQ				
5+50	0.4378	1.49	| VQ				
5+55	0.4481	1.50	| V Q				
6+ 0	0.4585	1.50	| V Q				
6+ 5	0.4692	1.56	| V Q				
6+10	0.4806	1.65	| V Q				
6+15	0.4921	1.67	| VQ				



6+20	0.5037	1.68	VQ				
6+25	0.5153	1.69	VQ				
6+30	0.5270	1.69	VQ				
6+35	0.5390	1.75	VQ				
6+40	0.5517	1.84	V Q				
6+45	0.5645	1.86	V Q				
6+50	0.5774	1.87	V Q				
6+55	0.5903	1.88	VQ				
7+ 0	0.6032	1.88	VQ				
7+ 5	0.6162	1.88	VQ				
7+10	0.6291	1.88	VQ				
7+15	0.6421	1.88	VQ				
7+20	0.6554	1.94	VQ				
7+25	0.6694	2.03	V Q				
7+30	0.6835	2.05	VQ				
7+35	0.6980	2.11	VQ				
7+40	0.7132	2.21	VQ				
7+45	0.7286	2.24	VQ				
7+50	0.7445	2.30	V Q				
7+55	0.7610	2.40	V Q				
8+ 0	0.7777	2.42	VQ				
8+ 5	0.7952	2.54	V Q				
8+10	0.8140	2.73	V Q				
8+15	0.8332	2.78	V Q				
8+20	0.8525	2.80	V Q				
8+25	0.8718	2.81	V Q				
8+30	0.8913	2.82	V Q				
8+35	0.9111	2.88	V Q				
8+40	0.9315	2.97	V Q				
8+45	0.9521	2.99	V Q				
8+50	0.9731	3.05	V Q				
8+55	0.9948	3.15	V Q				
9+ 0	1.0167	3.18	V Q				
9+ 5	1.0394	3.30	V Q				
9+10	1.0634	3.48	V Q				
9+15	1.0877	3.53	V Q				
9+20	1.1125	3.61	V Q				
9+25	1.1381	3.71	V Q				
9+30	1.1638	3.74	V Q				
9+35	1.1901	3.81	V Q				
9+40	1.2169	3.90	V Q				
9+45	1.2440	3.93	V Q				
9+50	1.2715	3.99	V Q				
9+55	1.2996	4.09	V Q				
10+ 0	1.3280	4.12	V Q				
10+ 5	1.3538	3.74	VQ				
10+10	1.3752	3.11	Q V				
10+15	1.3956	2.96	Q V				
10+20	1.4155	2.89	Q V				
10+25	1.4351	2.85	Q V				
10+30	1.4545	2.82	Q V				
10+35	1.4758	3.10	Q V				
10+40	1.5003	3.55	QV				
10+45	1.5255	3.66	QV				
10+50	1.5511	3.71	QV				
10+55	1.5768	3.74	Q V				
11+ 0	1.6027	3.76	QV				
11+ 5	1.6282	3.71	Q V				
11+10	1.6531	3.61	Q V				
11+15	1.6779	3.59	Q V				
11+20	1.7025	3.58	Q V				
11+25	1.7272	3.58	Q V				
11+30	1.7518	3.57	Q V				
11+35	1.7756	3.46	Q V				
11+40	1.7982	3.28	Q V				
11+45	1.8205	3.24	Q V				
11+50	1.8430	3.27	Q V				
11+55	1.8661	3.35	Q V				
12+ 0	1.8893	3.36	Q V				
12+ 5	1.9152	3.76	Q V				
12+10	1.9454	4.40	Q V				
12+15	1.9769	4.56	Q V				
12+20	2.0091	4.69	Q V				
12+25	2.0423	4.82	Q V				
12+30	2.0758	4.87	Q V				
12+35	2.1102	4.99	Q V				
12+40	2.1458	5.17	Q V				
12+45	2.1818	5.22	Q V				
12+50	2.2183	5.30	QV				
12+55	2.2555	5.40	Q V				
13+ 0	2.2929	5.43	Q V				



13+ 5	2.3323	5.72	
13+10	2.3749	6.17	
13+15	2.4182	6.29	
13+20	2.4619	6.34	
13+25	2.5058	6.37	
13+30	2.5498	6.39	
13+35	2.5897	5.79	
13+40	2.6227	4.79	
13+45	2.6540	4.54	
13+50	2.6845	4.43	
13+55	2.7146	4.37	
14+ 0	2.7443	4.32	
14+ 5	2.7756	4.54	
14+10	2.8094	4.91	
14+15	2.8438	5.00	
14+20	2.8782	4.98	
14+25	2.9120	4.91	
14+30	2.9458	4.91	
14+35	2.9795	4.90	
14+40	3.0132	4.89	
14+45	3.0469	4.89	
14+50	3.0802	4.83	
14+55	3.1129	4.74	
15+ 0	3.1454	4.72	
15+ 5	3.1774	4.66	
15+10	3.2088	4.56	
15+15	3.2400	4.53	
15+20	3.2708	4.47	
15+25	3.3009	4.37	
15+30	3.3308	4.34	
15+35	3.3592	4.11	
15+40	3.3850	3.75	
15+45	3.4101	3.65	
15+50	3.4350	3.61	
15+55	3.4597	3.59	
16+ 0	3.4843	3.57	
16+ 5	3.5032	2.75	
16+10	3.5128	1.39	
16+15	3.5200	1.05	
16+20	3.5262	0.90	
16+25	3.5318	0.81	
16+30	3.5370	0.75	
16+35	3.5418	0.70	
16+40	3.5460	0.61	
16+45	3.5500	0.58	
16+50	3.5539	0.57	
16+55	3.5579	0.57	
17+ 0	3.5617	0.56	
17+ 5	3.5664	0.67	
17+10	3.5723	0.85	
17+15	3.5785	0.90	
17+20	3.5848	0.92	
17+25	3.5912	0.93	
17+30	3.5977	0.94	
17+35	3.6042	0.94	
17+40	3.6107	0.94	
17+45	3.6171	0.94	
17+50	3.6232	0.89	
17+55	3.6287	0.79	
18+ 0	3.6340	0.77	
18+ 5	3.6393	0.76	
18+10	3.6445	0.76	
18+15	3.6496	0.75	
18+20	3.6548	0.75	
18+25	3.6600	0.75	
18+30	3.6652	0.75	
18+35	3.6700	0.70	
18+40	3.6742	0.61	
18+45	3.6782	0.58	
18+50	3.6818	0.52	
18+55	3.6847	0.42	
19+ 0	3.6874	0.40	
19+ 5	3.6904	0.44	
19+10	3.6941	0.53	
19+15	3.6978	0.54	
19+20	3.7020	0.61	
19+25	3.7069	0.71	
19+30	3.7119	0.73	
19+35	3.7166	0.69	
19+40	3.7208	0.60	
19+45	3.7248	0.58	

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   19+50       3.7284      0.52  | Q       |         |         |        V |
   19+55       3.7313      0.42  |Q        |         |         |        V |
   20+ 0       3.7340      0.40  |Q        |         |         |        V |
   20+ 5       3.7370      0.44  |Q        |         |         |        V |
   20+10       3.7407      0.53  | Q       |         |         |        V |
   20+15       3.7444      0.54  | Q       |         |         |        V |
   20+20       3.7482      0.55  | Q       |         |         |        V |
   20+25       3.7521      0.56  | Q       |         |         |        V |
   20+30       3.7560      0.56  | Q       |         |         |        V |
   20+35       3.7599      0.56  | Q       |         |         |        V |
   20+40       3.7637      0.56  | Q       |         |         |        V |
   20+45       3.7676      0.56  | Q       |         |         |        V |
   20+50       3.7711      0.51  | Q       |         |         |        V |
   20+55       3.7740      0.42  |Q        |         |         |        V |
   21+ 0       3.7767      0.40  |Q        |         |         |        V |
   21+ 5       3.7798      0.44  |Q        |         |         |        V |
   21+10       3.7834      0.53  | Q       |         |         |        V |
   21+15       3.7871      0.54  | Q       |         |         |        V |
   21+20       3.7906      0.50  |Q        |         |         |         V|
   21+25       3.7934      0.41  |Q        |         |         |         V|
   21+30       3.7962      0.40  |Q        |         |         |         V|
   21+35       3.7992      0.44  |Q        |         |         |         V|
   21+40       3.8028      0.53  | Q       |         |         |         V|
   21+45       3.8066      0.54  | Q       |         |         |         V|
   21+50       3.8100      0.50  |Q        |         |         |         V|
   21+55       3.8129      0.41  |Q        |         |         |         V|
   22+ 0       3.8156      0.40  |Q        |         |         |         V|
   22+ 5       3.8186      0.44  |Q        |         |         |         V|
   22+10       3.8222      0.53  | Q       |         |         |         V|
   22+15       3.8260      0.54  | Q       |         |         |         V|
   22+20       3.8294      0.50  |Q        |         |         |         V|
   22+25       3.8323      0.41  |Q        |         |         |         V|
   22+30       3.8350      0.40  |Q        |         |         |         V|
   22+35       3.8377      0.39  |Q        |         |         |         V|
   22+40       3.8403      0.38  |Q        |         |         |         V|
   22+45       3.8429      0.38  |Q        |         |         |         V|
   22+50       3.8455      0.38  |Q        |         |         |         V|
   22+55       3.8481      0.38  |Q        |         |         |         V|
   23+ 0       3.8506      0.38  |Q        |         |         |         V|
   23+ 5       3.8532      0.38  |Q        |         |         |         V|
   23+10       3.8558      0.38  |Q        |         |         |         V|
   23+15       3.8584      0.38  |Q        |         |         |         V|
   23+20       3.8610      0.38  |Q        |         |         |         V|
   23+25       3.8636      0.38  |Q        |         |         |         V|
   23+30       3.8662      0.38  |Q        |         |         |         V|
   23+35       3.8688      0.38  |Q        |         |         |         V|
   23+40       3.8714      0.38  |Q        |         |         |         V|
   23+45       3.8740      0.38  |Q        |         |         |         V|
   23+50       3.8765      0.38  |Q        |         |         |         V|
   23+55       3.8791      0.38  |Q        |         |         |         V|
   24+ 0       3.8817      0.38  |Q        |         |         |         V|
   24+ 5       3.8836      0.27  |Q        |         |         |         V|
   24+10       3.8841      0.09  Q         |         |         |         V|
   24+15       3.8844      0.04  Q         |         |         |         V|
   24+20       3.8846      0.02  Q         |         |         |         V|
   24+25       3.8846      0.01  Q         |         |         |          V
-------------------------------------------------------------------------
```

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       U n i t   H y d r o g r a p h   A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2976.00(Ft.)
Length along longest watercourse measured to centroid =    1488.00(Ft.)
Length along longest watercourse =      0.564 Mi.
Length along longest watercourse measured to centroid =      0.282 Mi.
Difference in elevation =     150.00(Ft.)
Slope along watercourse =    266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.062 Hr.
Lag time =     3.72 Min.
25% of lag time =     0.93 Min.
40% of lag time =     1.49 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           0.50                 25.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           1.30                 67.34

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.687(In)
Areal adjustment factor =   99.95 %
Adjusted average point rain =    0.687(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           69.00         0.500
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  49.8      0.574     0.500        0.316       1.000      0.316
                                                 Sum (F) =   0.316
Area averaged mean soil loss (F) (In/Hr) =  0.316
Minimum soil loss rate ((In/Hr)) =  0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
			Sum = 100.000 Sum=	52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.272	(0.316)	0.136	0.136
2	0.17	4.20	0.346	(0.316)	0.173	0.173
3	0.25	4.40	0.363	(0.316)	0.181	0.181
4	0.33	4.80	0.396	(0.316)	0.198	0.198
5	0.42	5.20	0.429	(0.316)	0.214	0.214
6	0.50	6.20	0.511	(0.316)	0.256	0.256
7	0.58	6.80	0.561	(0.316)	0.280	0.280
8	0.67	8.80	0.726	0.316	(0.363)	0.410
9	0.75	13.90	1.146	0.316	(0.573)	0.830
10	0.83	31.40	2.589	0.316	(1.294)	2.273
11	0.92	7.20	0.594	(0.316)	0.297	0.297
12	1.00	3.80	0.313	(0.316)	0.157	0.157
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.4

Flood volume = Effective rainfall 0.45(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 1.9(Ac.Ft)
Total soil loss = 0.24(In)
Total soil loss = 1.021(Ac.Ft)
Total rainfall = 0.69(In)
Flood volume = 84701.4 Cubic Feet
Total soil loss = 44488.7 Cubic Feet

Peak flow rate of this hydrograph = 68.734(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	17.5	35.0	52.5	70.0
0+ 5	0.0143	2.08	VQ				
0+10	0.0560	6.06	V Q				
0+15	0.1110	7.98	V Q				
0+20	0.1734	9.06	V Q				
0+25	0.2429	10.09	VQ				
0+30	0.3219	11.48	Q				
0+35	0.4121	13.09	QV				
0+40	0.5226	16.04	QV				
0+45	0.7018	26.03	Q				
0+50	1.1123	59.60	V			Q	
0+55	1.5857	68.73				V Q	
1+ 0	1.7757	27.59	Q			V	
1+ 5	1.8719	13.98	Q			V	
1+10	1.9152	6.28	Q			V	
1+15	1.9392	3.50	Q			V	
1+20	1.9432	0.58	Q			V	
1+25	1.9445	0.18	Q			V	

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        U n i t   H y d r o g r a p h   A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2976.00(Ft.)
Length along longest watercourse measured to centroid =    1488.00(Ft.)
Length along longest watercourse =      0.564 Mi.
Length along longest watercourse measured to centroid =      0.282 Mi.
Difference in elevation =     150.00(Ft.)
Slope along watercourse =    266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.062 Hr.
Lag time =     3.72 Min.
25% of lag time =     0.93 Min.
40% of lag time =     1.49 Min.
Unit time =     5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           0.80                 41.44

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           2.00                103.60

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.800(In)
Area Averaged 100-Year Rainfall =    2.000(In)

Point rain (area averaged) =    1.081(In)
Areal adjustment factor =   99.98 %
Adjusted average point rain =    1.081(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           69.00         0.500
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  49.8      0.574     0.500        0.316       1.000      0.316
                                                 Sum (F) =   0.316
Area averaged mean soil loss (F) (In/Hr) =  0.316
Minimum soil loss rate ((In/Hr)) =  0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
		Sum = 100.000	Sum=	52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.169	(0.316)	0.084	0.084
2	0.17	1.30	0.169	(0.316)	0.084	0.084
3	0.25	1.10	0.143	(0.316)	0.071	0.071
4	0.33	1.50	0.195	(0.316)	0.097	0.097
5	0.42	1.50	0.195	(0.316)	0.097	0.097
6	0.50	1.80	0.233	(0.316)	0.117	0.117
7	0.58	1.50	0.195	(0.316)	0.097	0.097
8	0.67	1.80	0.233	(0.316)	0.117	0.117
9	0.75	1.80	0.233	(0.316)	0.117	0.117
10	0.83	1.50	0.195	(0.316)	0.097	0.097
11	0.92	1.60	0.208	(0.316)	0.104	0.104
12	1.00	1.80	0.233	(0.316)	0.117	0.117
13	1.08	2.20	0.285	(0.316)	0.143	0.143
14	1.17	2.20	0.285	(0.316)	0.143	0.143
15	1.25	2.20	0.285	(0.316)	0.143	0.143
16	1.33	2.00	0.259	(0.316)	0.130	0.130
17	1.42	2.60	0.337	(0.316)	0.169	0.169
18	1.50	2.70	0.350	(0.316)	0.175	0.175
19	1.58	2.40	0.311	(0.316)	0.156	0.156
20	1.67	2.70	0.350	(0.316)	0.175	0.175
21	1.75	3.30	0.428	(0.316)	0.214	0.214
22	1.83	3.10	0.402	(0.316)	0.201	0.201
23	1.92	2.90	0.376	(0.316)	0.188	0.188
24	2.00	3.00	0.389	(0.316)	0.195	0.195
25	2.08	3.10	0.402	(0.316)	0.201	0.201
26	2.17	4.20	0.545	(0.316)	0.272	0.272
27	2.25	5.00	0.648	0.316	(0.324)	0.333
28	2.33	3.50	0.454	(0.316)	0.227	0.227
29	2.42	6.80	0.882	0.316	(0.441)	0.566
30	2.50	7.30	0.947	0.316	(0.473)	0.631
31	2.58	8.20	1.064	0.316	(0.532)	0.748
32	2.67	5.90	0.765	0.316	(0.383)	0.450
33	2.75	2.00	0.259	(0.316)	0.130	0.130
34	2.83	1.80	0.233	(0.316)	0.117	0.117
35	2.92	1.80	0.233	(0.316)	0.117	0.117
36	3.00	0.60	0.078	(0.316)	0.039	0.039
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	7.1

Flood volume = Effective rainfall 0.59(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 2.5(Ac.Ft)
Total soil loss = 0.49(In)
Total soil loss = 2.126(Ac.Ft)
Total rainfall = 1.08(In)
Flood volume = 110619.7 Cubic Feet
Total soil loss = 92612.0 Cubic Feet

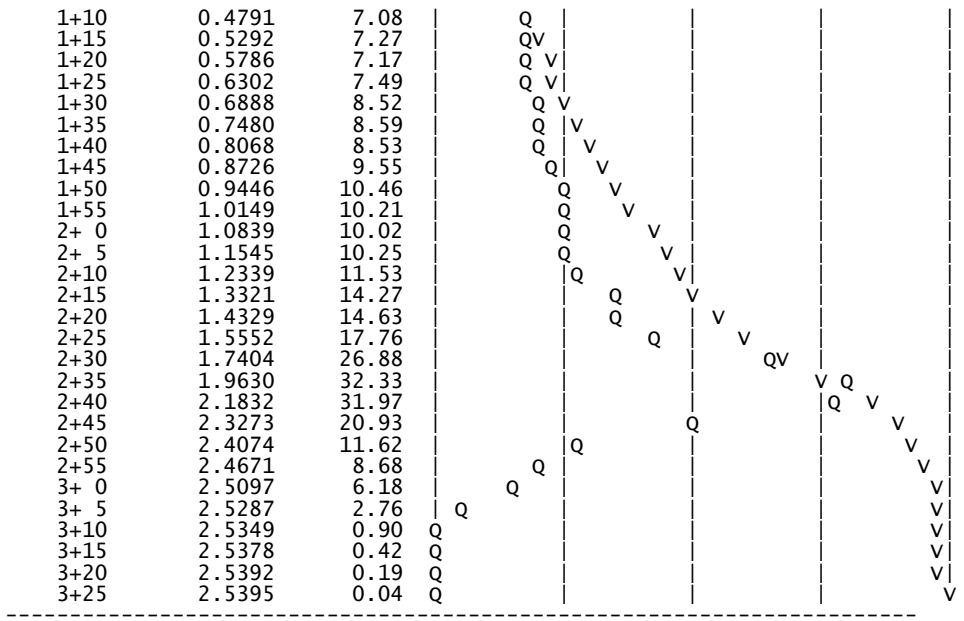
Peak flow rate of this hydrograph = 32.327(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	10.0	20.0	30.0	40.0
0+ 5	0.0089	1.29	VQ				
0+10	0.0323	3.40	V Q				
0+15	0.0581	3.74	V Q				
0+20	0.0860	4.05	V Q				
0+25	0.1187	4.75	V Q				
0+30	0.1550	5.27	V Q				
0+35	0.1929	5.51	V Q				
0+40	0.2306	5.47	V Q				
0+45	0.2714	5.92	VQ				
0+50	0.3108	5.72	VQ				
0+55	0.3479	5.38	Q				
1+ 0	0.3866	5.63	QV				
1+ 5	0.4304	6.36	Q				



1+10	0.4791	7.08	
1+15	0.5292	7.27	
1+20	0.5786	7.17	
1+25	0.6302	7.49	
1+30	0.6888	8.52	
1+35	0.7480	8.59	
1+40	0.8068	8.53	
1+45	0.8726	9.55	
1+50	0.9446	10.46	
1+55	1.0149	10.21	
2+ 0	1.0839	10.02	
2+ 5	1.1545	10.25	
2+10	1.2339	11.53	
2+15	1.3321	14.27	
2+20	1.4329	14.63	
2+25	1.5552	17.76	
2+30	1.7404	26.88	
2+35	1.9630	32.33	
2+40	2.1832	31.97	
2+45	2.3273	20.93	
2+50	2.4074	11.62	
2+55	2.4671	8.68	
3+ 0	2.5097	6.18	
3+ 5	2.5287	2.76	
3+10	2.5349	0.90	
3+15	2.5378	0.42	
3+20	2.5392	0.19	
3+25	2.5395	0.04	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro2565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2976.00(Ft.)
Length along longest watercourse measured to centroid = 1488.00(Ft.)
Length along longest watercourse = 0.564 Mi.
Length along longest watercourse measured to centroid = 0.282 Mi.
Difference in elevation = 150.00(Ft.)
Slope along watercourse = 266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.062 Hr.
Lag time = 3.72 Min.
25% of lag time = 0.93 Min.
40% of lag time = 1.49 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	1.10	56.98

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	3.00	155.40

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.545(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 1.545(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	69.00	0.500

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.093	(0.316)	0.046	0.046
2	0.17	0.60	0.111	(0.316)	0.056	0.056
3	0.25	0.60	0.111	(0.316)	0.056	0.056
4	0.33	0.60	0.111	(0.316)	0.056	0.056
5	0.42	0.60	0.111	(0.316)	0.056	0.056
6	0.50	0.70	0.130	(0.316)	0.065	0.065
7	0.58	0.70	0.130	(0.316)	0.065	0.065
8	0.67	0.70	0.130	(0.316)	0.065	0.065
9	0.75	0.70	0.130	(0.316)	0.065	0.065
10	0.83	0.70	0.130	(0.316)	0.065	0.065
11	0.92	0.70	0.130	(0.316)	0.065	0.065
12	1.00	0.80	0.148	(0.316)	0.074	0.074
13	1.08	0.80	0.148	(0.316)	0.074	0.074
14	1.17	0.80	0.148	(0.316)	0.074	0.074
15	1.25	0.80	0.148	(0.316)	0.074	0.074
16	1.33	0.80	0.148	(0.316)	0.074	0.074
17	1.42	0.80	0.148	(0.316)	0.074	0.074
18	1.50	0.80	0.148	(0.316)	0.074	0.074
19	1.58	0.80	0.148	(0.316)	0.074	0.074
20	1.67	0.80	0.148	(0.316)	0.074	0.074
21	1.75	0.80	0.148	(0.316)	0.074	0.074
22	1.83	0.80	0.148	(0.316)	0.074	0.074
23	1.92	0.80	0.148	(0.316)	0.074	0.074
24	2.00	0.90	0.167	(0.316)	0.083	0.083
25	2.08	0.80	0.148	(0.316)	0.074	0.074
26	2.17	0.90	0.167	(0.316)	0.083	0.083
27	2.25	0.90	0.167	(0.316)	0.083	0.083
28	2.33	0.90	0.167	(0.316)	0.083	0.083
29	2.42	0.90	0.167	(0.316)	0.083	0.083
30	2.50	0.90	0.167	(0.316)	0.083	0.083
31	2.58	0.90	0.167	(0.316)	0.083	0.083
32	2.67	0.90	0.167	(0.316)	0.083	0.083
33	2.75	1.00	0.185	(0.316)	0.093	0.093
34	2.83	1.00	0.185	(0.316)	0.093	0.093
35	2.92	1.00	0.185	(0.316)	0.093	0.093
36	3.00	1.00	0.185	(0.316)	0.093	0.093
37	3.08	1.00	0.185	(0.316)	0.093	0.093
38	3.17	1.10	0.204	(0.316)	0.102	0.102
39	3.25	1.10	0.204	(0.316)	0.102	0.102
40	3.33	1.10	0.204	(0.316)	0.102	0.102
41	3.42	1.20	0.222	(0.316)	0.111	0.111
42	3.50	1.30	0.241	(0.316)	0.120	0.120
43	3.58	1.40	0.260	(0.316)	0.130	0.130
44	3.67	1.40	0.260	(0.316)	0.130	0.130
45	3.75	1.50	0.278	(0.316)	0.139	0.139
46	3.83	1.50	0.278	(0.316)	0.139	0.139
47	3.92	1.60	0.297	(0.316)	0.148	0.148
48	4.00	1.60	0.297	(0.316)	0.148	0.148
49	4.08	1.70	0.315	(0.316)	0.158	0.158
50	4.17	1.80	0.334	(0.316)	0.167	0.167
51	4.25	1.90	0.352	(0.316)	0.176	0.176
52	4.33	2.00	0.371	(0.316)	0.185	0.185
53	4.42	2.10	0.389	(0.316)	0.195	0.195
54	4.50	2.10	0.389	(0.316)	0.195	0.195
55	4.58	2.20	0.408	(0.316)	0.204	0.204
56	4.67	2.30	0.426	(0.316)	0.213	0.213
57	4.75	2.40	0.445	(0.316)	0.222	0.222
58	4.83	2.40	0.445	(0.316)	0.222	0.222
59	4.92	2.50	0.463	(0.316)	0.232	0.232
60	5.00	2.60	0.482	(0.316)	0.241	0.241
61	5.08	3.10	0.575	(0.316)	0.287	0.287
62	5.17	3.60	0.667	0.316	(0.334)	0.352
63	5.25	3.90	0.723	0.316	(0.361)	0.407
64	5.33	4.20	0.779	0.316	(0.389)	0.463
65	5.42	4.70	0.871	0.316	(0.436)	0.556
66	5.50	5.60	1.038	0.316	(0.519)	0.722
67	5.58	1.90	0.352	(0.316)	0.176	0.176
68	5.67	0.90	0.167	(0.316)	0.083	0.083
69	5.75	0.60	0.111	(0.316)	0.056	0.056
70	5.83	0.50	0.093	(0.316)	0.046	0.046

```
71   5.92     0.30      0.056       (  0.316)       0.028        0.028
72   6.00     0.20      0.037       (  0.316)       0.019        0.019
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =     9.7
      Flood volume = Effective rainfall      0.81(In)
       times area      51.8(Ac.)/[(In)/(Ft.)] =       3.5(Ac.Ft)
      Total soil loss =      0.73(In)
      Total soil loss =     3.168(Ac.Ft)
      Total rainfall =      1.54(In)
      Flood volume =      152451.5 Cubic Feet
      Total soil loss =      138014.2 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     29.939(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        7.5      15.0      22.5      30.0
-------------------------------------------------------------------------
  0+ 5       0.0049      0.71  Q          |          |          |          |
  0+10       0.0187      2.01  V Q        |          |          |          |
  0+15       0.0362      2.54  V  Q       |          |          |          |
  0+20       0.0550      2.73  V  Q       |          |          |          |
  0+25       0.0745      2.83  V  Q       |          |          |          |
  0+30       0.0954      3.04  |V  Q       |          |          |          |
  0+35       0.1180      3.28  |V  Q       |          |          |          |
  0+40       0.1410      3.34  |V  Q       |          |          |          |
  0+45       0.1641      3.36  |V  Q       |          |          |          |
  0+50       0.1874      3.38  | V Q       |          |          |          |
  0+55       0.2107      3.39  | V Q       |          |          |          |
  1+ 0       0.2351      3.53  | V Q       |          |          |          |
  1+ 5       0.2610      3.76  | V  Q      |          |          |          |
  1+10       0.2873      3.82  |  V Q      |          |          |          |
  1+15       0.3138      3.85  |  V Q      |          |          |          |
  1+20       0.3404      3.86  |  V Q      |          |          |          |
  1+25       0.3671      3.87  |   VQ      |          |          |          |
  1+30       0.3937      3.87  |   VQ      |          |          |          |
  1+35       0.4204      3.87  |   VQ      |          |          |          |
  1+40       0.4471      3.87  |    Q      |          |          |          |
  1+45       0.4738      3.87  |    Q      |          |          |          |
  1+50       0.5004      3.87  |    Q      |          |          |          |
  1+55       0.5271      3.87  |    QV     |          |          |          |
  2+ 0       0.5548      4.01  |    QV     |          |          |          |
  2+ 5       0.5830      4.11  |    QV     |          |          |          |
  2+10       0.6111      4.07  |    QV     |          |          |          |
  2+15       0.6405      4.27  |    Q V    |          |          |          |
  2+20       0.6703      4.32  |    Q V    |          |          |          |
  2+25       0.7002      4.34  |    Q  V   |          |          |          |
  2+30       0.7301      4.35  |    Q  V   |          |          |          |
  2+35       0.7601      4.36  |    Q  V   |          |          |          |
  2+40       0.7901      4.36  |    Q   V  |          |          |          |
  2+45       0.8211      4.50  |    Q   V  |          |          |          |
  2+50       0.8537      4.73  |     Q  V  |          |          |          |
  2+55       0.8867      4.79  |     Q   V |          |          |          |
  3+ 0       0.9198      4.82  |     Q   V |          |          |          |
  3+ 5       0.9531      4.83  |     Q   V |          |          |          |
  3+10       0.9874      4.98  |     Q   |V          |          |          |
  3+15       1.0233      5.22  |     Q   |V          |          |          |
  3+20       1.0597      5.27  |      Q  | V         |          |          |
  3+25       1.0971      5.44  |      Q  | V         |          |          |
  3+30       1.1373      5.83  |      Q  | V         |          |          |
  3+35       1.1805      6.27  |       Q |  V        |          |          |
  3+40       1.2259      6.59  |       Q |   V       |          |          |
  3+45       1.2730      6.83  |        Q|   V       |          |          |
  3+50       1.3220      7.12  |        Q|    V      |          |          |
  3+55       1.3725      7.34  |        Q|    V      |          |          |
  4+ 0       1.4250      7.61  |         Q     V     |          |          |
  4+ 5       1.4789      7.83  |         Q     V     |          |          |
  4+10       1.5356      8.24  |         Q      V    |          |          |
  4+15       1.5954      8.68  |         |Q      V   |          |          |
  4+20       1.6584      9.15  |         | Q     V   |          |          |
  4+25       1.7247      9.63  |         | Q      V| |          |          |
  4+30       1.7934      9.97  |         |  Q      V          |          |
  4+35       1.8638     10.22  |         |  Q      |V         |          |
  4+40       1.9371     10.65  |         |   Q     | V        |          |
  4+45       2.0136     11.10  |         |   Q     |  V       |          |
  4+50       2.0923     11.43  |         |    Q    |  V       |          |
  4+55       2.1727     11.67  |         |    Q    |   V      |          |
  5+ 0       2.2561     12.10  |         |     Q   |    V     |          |
  5+ 5       2.3464     13.12  |         |      Q  |     V    |          |
  5+10       2.4523     15.36  |         |         Q       V  |          |
  5+15       2.5774     18.16  |         |         |   Q    V|          |
```

```
    5+20       2.7218     20.97  |          |          |       Q  |V         |
    5+25       2.8899     24.40  |          |          |          | QV       |
    5+30       3.0961     29.94  |          |          |          |    V   Q|
    5+35       3.2798     26.68  |          |          |          |    Q V   |
    5+40       3.3696     13.03  |          |       Q  |          |      V   |
    5+45       3.4211      7.48  |          Q|          |          |         V|
    5+50       3.4547      4.88  |        Q  |          |          |         V|
    5+55       3.4772      3.27  |     Q     |          |          |         V|
    6+ 0       3.4894      1.76  |  Q        |          |          |         V|
    6+ 5       3.4959      0.95  |Q          |          |          |         V|
    6+10       3.4982      0.33  Q           |          |          |         V|
    6+15       3.4992      0.15  Q           |          |          |         V|
    6+20       3.4997      0.06  Q           |          |          |         V|
    6+25       3.4998      0.02  Q           |          |          |          V
---------------------------------------------------------------------------
```

```
       U n i t   H y d r o g r a p h   A n a l y s i s

       Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2008, Version 8.1
              Study date  04/22/24 File: pro25245.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2976.00(Ft.)
Length along longest watercourse measured to centroid =    1488.00(Ft.)
Length along longest watercourse =      0.564 Mi.
Length along longest watercourse measured to centroid =      0.282 Mi.
Difference in elevation =     150.00(Ft.)
Slope along watercourse =    266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.062 Hr.
Lag time =     3.72 Min.
25% of lag time =     0.93 Min.
40% of lag time =     1.49 Min.
Unit time =     5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           1.80                 93.24

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           5.00                259.00

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    1.800(In)
Area Averaged 100-Year Rainfall =    5.000(In)

Point rain (area averaged) =    2.550(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    2.549(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           69.00         0.500
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  49.8      0.574     0.500        0.316       1.000      0.316
                                                 Sum (F) =   0.316
Area averaged mean soil loss (F) (In/Hr) =  0.316
Minimum soil loss rate ((In/Hr)) =  0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

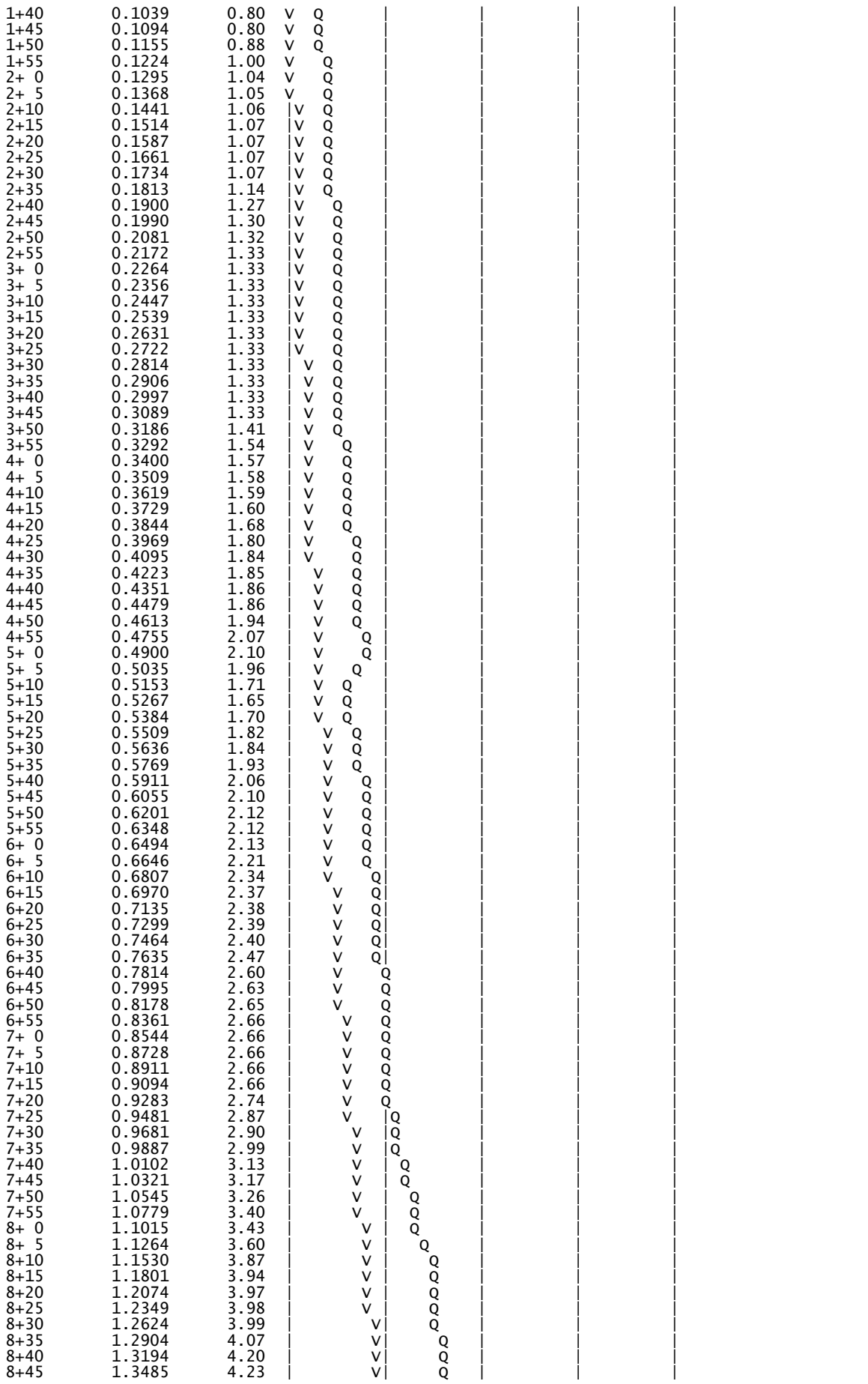
Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.020	(0.560)	0.010	0.010
2	0.17	0.07	0.020	(0.557)	0.010	0.010
3	0.25	0.07	0.020	(0.555)	0.010	0.010
4	0.33	0.10	0.031	(0.553)	0.015	0.015
5	0.42	0.10	0.031	(0.551)	0.015	0.015
6	0.50	0.10	0.031	(0.549)	0.015	0.015
7	0.58	0.10	0.031	(0.547)	0.015	0.015
8	0.67	0.10	0.031	(0.545)	0.015	0.015
9	0.75	0.10	0.031	(0.542)	0.015	0.015
10	0.83	0.13	0.041	(0.540)	0.020	0.020
11	0.92	0.13	0.041	(0.538)	0.020	0.020
12	1.00	0.13	0.041	(0.536)	0.020	0.020
13	1.08	0.10	0.031	(0.534)	0.015	0.015
14	1.17	0.10	0.031	(0.532)	0.015	0.015
15	1.25	0.10	0.031	(0.530)	0.015	0.015
16	1.33	0.10	0.031	(0.528)	0.015	0.015
17	1.42	0.10	0.031	(0.525)	0.015	0.015
18	1.50	0.10	0.031	(0.523)	0.015	0.015
19	1.58	0.10	0.031	(0.521)	0.015	0.015
20	1.67	0.10	0.031	(0.519)	0.015	0.015
21	1.75	0.10	0.031	(0.517)	0.015	0.015
22	1.83	0.13	0.041	(0.515)	0.020	0.020
23	1.92	0.13	0.041	(0.513)	0.020	0.020
24	2.00	0.13	0.041	(0.511)	0.020	0.020
25	2.08	0.13	0.041	(0.509)	0.020	0.020
26	2.17	0.13	0.041	(0.507)	0.020	0.020
27	2.25	0.13	0.041	(0.505)	0.020	0.020
28	2.33	0.13	0.041	(0.503)	0.020	0.020
29	2.42	0.13	0.041	(0.501)	0.020	0.020
30	2.50	0.13	0.041	(0.499)	0.020	0.020
31	2.58	0.17	0.051	(0.497)	0.025	0.025
32	2.67	0.17	0.051	(0.494)	0.025	0.025
33	2.75	0.17	0.051	(0.492)	0.025	0.025
34	2.83	0.17	0.051	(0.490)	0.025	0.025
35	2.92	0.17	0.051	(0.488)	0.025	0.025
36	3.00	0.17	0.051	(0.486)	0.025	0.025
37	3.08	0.17	0.051	(0.484)	0.025	0.025
38	3.17	0.17	0.051	(0.482)	0.025	0.025
39	3.25	0.17	0.051	(0.480)	0.025	0.025
40	3.33	0.17	0.051	(0.478)	0.025	0.025
41	3.42	0.17	0.051	(0.476)	0.025	0.025
42	3.50	0.17	0.051	(0.474)	0.025	0.025
43	3.58	0.17	0.051	(0.472)	0.025	0.025
44	3.67	0.17	0.051	(0.470)	0.025	0.025
45	3.75	0.17	0.051	(0.468)	0.025	0.025
46	3.83	0.20	0.061	(0.466)	0.031	0.031
47	3.92	0.20	0.061	(0.464)	0.031	0.031
48	4.00	0.20	0.061	(0.463)	0.031	0.031
49	4.08	0.20	0.061	(0.461)	0.031	0.031
50	4.17	0.20	0.061	(0.459)	0.031	0.031
51	4.25	0.20	0.061	(0.457)	0.031	0.031
52	4.33	0.23	0.071	(0.455)	0.036	0.036
53	4.42	0.23	0.071	(0.453)	0.036	0.036
54	4.50	0.23	0.071	(0.451)	0.036	0.036
55	4.58	0.23	0.071	(0.449)	0.036	0.036
56	4.67	0.23	0.071	(0.447)	0.036	0.036
57	4.75	0.23	0.071	(0.445)	0.036	0.036
58	4.83	0.27	0.082	(0.443)	0.041	0.041
59	4.92	0.27	0.082	(0.441)	0.041	0.041
60	5.00	0.27	0.082	(0.439)	0.041	0.041
61	5.08	0.20	0.061	(0.437)	0.031	0.031
62	5.17	0.20	0.061	(0.435)	0.031	0.031
63	5.25	0.20	0.061	(0.434)	0.031	0.031
64	5.33	0.23	0.071	(0.432)	0.036	0.036
65	5.42	0.23	0.071	(0.430)	0.036	0.036
66	5.50	0.23	0.071	(0.428)	0.036	0.036
67	5.58	0.27	0.082	(0.426)	0.041	0.041
68	5.67	0.27	0.082	(0.424)	0.041	0.041
69	5.75	0.27	0.082	(0.422)	0.041	0.041
70	5.83	0.27	0.082	(0.420)	0.041	0.041

71	5.92	0.27	0.082	(0.419)	0.041	0.041
72	6.00	0.27	0.082	(0.417)	0.041	0.041
73	6.08	0.30	0.092	(0.415)	0.046	0.046
74	6.17	0.30	0.092	(0.413)	0.046	0.046
75	6.25	0.30	0.092	(0.411)	0.046	0.046
76	6.33	0.30	0.092	(0.409)	0.046	0.046
77	6.42	0.30	0.092	(0.407)	0.046	0.046
78	6.50	0.30	0.092	(0.406)	0.046	0.046
79	6.58	0.33	0.102	(0.404)	0.051	0.051
80	6.67	0.33	0.102	(0.402)	0.051	0.051
81	6.75	0.33	0.102	(0.400)	0.051	0.051
82	6.83	0.33	0.102	(0.398)	0.051	0.051
83	6.92	0.33	0.102	(0.397)	0.051	0.051
84	7.00	0.33	0.102	(0.395)	0.051	0.051
85	7.08	0.33	0.102	(0.393)	0.051	0.051
86	7.17	0.33	0.102	(0.391)	0.051	0.051
87	7.25	0.33	0.102	(0.389)	0.051	0.051
88	7.33	0.37	0.112	(0.388)	0.056	0.056
89	7.42	0.37	0.112	(0.386)	0.056	0.056
90	7.50	0.37	0.112	(0.384)	0.056	0.056
91	7.58	0.40	0.122	(0.382)	0.061	0.061
92	7.67	0.40	0.122	(0.381)	0.061	0.061
93	7.75	0.40	0.122	(0.379)	0.061	0.061
94	7.83	0.43	0.133	(0.377)	0.066	0.066
95	7.92	0.43	0.133	(0.375)	0.066	0.066
96	8.00	0.43	0.133	(0.374)	0.066	0.066
97	8.08	0.50	0.153	(0.372)	0.076	0.076
98	8.17	0.50	0.153	(0.370)	0.076	0.076
99	8.25	0.50	0.153	(0.368)	0.076	0.076
100	8.33	0.50	0.153	(0.367)	0.076	0.076
101	8.42	0.50	0.153	(0.365)	0.076	0.076
102	8.50	0.50	0.153	(0.363)	0.076	0.076
103	8.58	0.53	0.163	(0.362)	0.082	0.082
104	8.67	0.53	0.163	(0.360)	0.082	0.082
105	8.75	0.53	0.163	(0.358)	0.082	0.082
106	8.83	0.57	0.173	(0.356)	0.087	0.087
107	8.92	0.57	0.173	(0.355)	0.087	0.087
108	9.00	0.57	0.173	(0.353)	0.087	0.087
109	9.08	0.63	0.194	(0.351)	0.097	0.097
110	9.17	0.63	0.194	(0.350)	0.097	0.097
111	9.25	0.63	0.194	(0.348)	0.097	0.097
112	9.33	0.67	0.204	(0.346)	0.102	0.102
113	9.42	0.67	0.204	(0.345)	0.102	0.102
114	9.50	0.67	0.204	(0.343)	0.102	0.102
115	9.58	0.70	0.214	(0.341)	0.107	0.107
116	9.67	0.70	0.214	(0.340)	0.107	0.107
117	9.75	0.70	0.214	(0.338)	0.107	0.107
118	9.83	0.73	0.224	(0.337)	0.112	0.112
119	9.92	0.73	0.224	(0.335)	0.112	0.112
120	10.00	0.73	0.224	(0.333)	0.112	0.112
121	10.08	0.50	0.153	(0.332)	0.076	0.076
122	10.17	0.50	0.153	(0.330)	0.076	0.076
123	10.25	0.50	0.153	(0.329)	0.076	0.076
124	10.33	0.50	0.153	(0.327)	0.076	0.076
125	10.42	0.50	0.153	(0.325)	0.076	0.076
126	10.50	0.50	0.153	(0.324)	0.076	0.076
127	10.58	0.67	0.204	(0.322)	0.102	0.102
128	10.67	0.67	0.204	(0.321)	0.102	0.102
129	10.75	0.67	0.204	(0.319)	0.102	0.102
130	10.83	0.67	0.204	(0.317)	0.102	0.102
131	10.92	0.67	0.204	(0.316)	0.102	0.102
132	11.00	0.67	0.204	(0.314)	0.102	0.102
133	11.08	0.63	0.194	(0.313)	0.097	0.097
134	11.17	0.63	0.194	(0.311)	0.097	0.097
135	11.25	0.63	0.194	(0.310)	0.097	0.097
136	11.33	0.63	0.194	(0.308)	0.097	0.097
137	11.42	0.63	0.194	(0.307)	0.097	0.097
138	11.50	0.63	0.194	(0.305)	0.097	0.097
139	11.58	0.57	0.173	(0.304)	0.087	0.087
140	11.67	0.57	0.173	(0.302)	0.087	0.087
141	11.75	0.57	0.173	(0.301)	0.087	0.087
142	11.83	0.60	0.184	(0.299)	0.092	0.092
143	11.92	0.60	0.184	(0.298)	0.092	0.092
144	12.00	0.60	0.184	(0.296)	0.092	0.092
145	12.08	0.83	0.255	(0.295)	0.127	0.127
146	12.17	0.83	0.255	(0.293)	0.127	0.127
147	12.25	0.83	0.255	(0.292)	0.127	0.127
148	12.33	0.87	0.265	(0.290)	0.133	0.133
149	12.42	0.87	0.265	(0.289)	0.133	0.133
150	12.50	0.87	0.265	(0.287)	0.133	0.133
151	12.58	0.93	0.286	(0.286)	0.143	0.143
152	12.67	0.93	0.286	(0.284)	0.143	0.143
153	12.75	0.93	0.286	(0.283)	0.143	0.143
154	12.83	0.97	0.296	(0.282)	0.148	0.148
155	12.92	0.97	0.296	(0.280)	0.148	0.148
156	13.00	0.97	0.296	(0.279)	0.148	0.148

157	13.08	1.13	0.347	(0.277)	0.173	0.173
158	13.17	1.13	0.347	(0.276)	0.173	0.173
159	13.25	1.13	0.347	(0.275)	0.173	0.173
160	13.33	1.13	0.347	(0.273)	0.173	0.173
161	13.42	1.13	0.347	(0.272)	0.173	0.173
162	13.50	1.13	0.347	(0.270)	0.173	0.173
163	13.58	0.77	0.235	(0.269)	0.117	0.117
164	13.67	0.77	0.235	(0.268)	0.117	0.117
165	13.75	0.77	0.235	(0.266)	0.117	0.117
166	13.83	0.77	0.235	(0.265)	0.117	0.117
167	13.92	0.77	0.235	(0.264)	0.117	0.117
168	14.00	0.77	0.235	(0.262)	0.117	0.117
169	14.08	0.90	0.275	(0.261)	0.138	0.138
170	14.17	0.90	0.275	(0.260)	0.138	0.138
171	14.25	0.90	0.275	(0.258)	0.138	0.138
172	14.33	0.87	0.265	(0.257)	0.133	0.133
173	14.42	0.87	0.265	(0.256)	0.133	0.133
174	14.50	0.87	0.265	(0.254)	0.133	0.133
175	14.58	0.87	0.265	(0.253)	0.133	0.133
176	14.67	0.87	0.265	(0.252)	0.133	0.133
177	14.75	0.87	0.265	(0.250)	0.133	0.133
178	14.83	0.83	0.255	(0.249)	0.127	0.127
179	14.92	0.83	0.255	(0.248)	0.127	0.127
180	15.00	0.83	0.255	(0.247)	0.127	0.127
181	15.08	0.80	0.245	(0.245)	0.122	0.122
182	15.17	0.80	0.245	(0.244)	0.122	0.122
183	15.25	0.80	0.245	(0.243)	0.122	0.122
184	15.33	0.77	0.235	(0.242)	0.117	0.117
185	15.42	0.77	0.235	(0.240)	0.117	0.117
186	15.50	0.77	0.235	(0.239)	0.117	0.117
187	15.58	0.63	0.194	(0.238)	0.097	0.097
188	15.67	0.63	0.194	(0.237)	0.097	0.097
189	15.75	0.63	0.194	(0.235)	0.097	0.097
190	15.83	0.63	0.194	(0.234)	0.097	0.097
191	15.92	0.63	0.194	(0.233)	0.097	0.097
192	16.00	0.63	0.194	(0.232)	0.097	0.097
193	16.08	0.13	0.041	(0.231)	0.020	0.020
194	16.17	0.13	0.041	(0.229)	0.020	0.020
195	16.25	0.13	0.041	(0.228)	0.020	0.020
196	16.33	0.13	0.041	(0.227)	0.020	0.020
197	16.42	0.13	0.041	(0.226)	0.020	0.020
198	16.50	0.13	0.041	(0.225)	0.020	0.020
199	16.58	0.10	0.031	(0.224)	0.015	0.015
200	16.67	0.10	0.031	(0.223)	0.015	0.015
201	16.75	0.10	0.031	(0.221)	0.015	0.015
202	16.83	0.10	0.031	(0.220)	0.015	0.015
203	16.92	0.10	0.031	(0.219)	0.015	0.015
204	17.00	0.10	0.031	(0.218)	0.015	0.015
205	17.08	0.17	0.051	(0.217)	0.025	0.025
206	17.17	0.17	0.051	(0.216)	0.025	0.025
207	17.25	0.17	0.051	(0.215)	0.025	0.025
208	17.33	0.17	0.051	(0.214)	0.025	0.025
209	17.42	0.17	0.051	(0.213)	0.025	0.025
210	17.50	0.17	0.051	(0.212)	0.025	0.025
211	17.58	0.17	0.051	(0.211)	0.025	0.025
212	17.67	0.17	0.051	(0.209)	0.025	0.025
213	17.75	0.17	0.051	(0.208)	0.025	0.025
214	17.83	0.13	0.041	(0.207)	0.020	0.020
215	17.92	0.13	0.041	(0.206)	0.020	0.020
216	18.00	0.13	0.041	(0.205)	0.020	0.020
217	18.08	0.13	0.041	(0.204)	0.020	0.020
218	18.17	0.13	0.041	(0.203)	0.020	0.020
219	18.25	0.13	0.041	(0.202)	0.020	0.020
220	18.33	0.13	0.041	(0.201)	0.020	0.020
221	18.42	0.13	0.041	(0.200)	0.020	0.020
222	18.50	0.13	0.041	(0.199)	0.020	0.020
223	18.58	0.10	0.031	(0.198)	0.015	0.015
224	18.67	0.10	0.031	(0.197)	0.015	0.015
225	18.75	0.10	0.031	(0.197)	0.015	0.015
226	18.83	0.07	0.020	(0.196)	0.010	0.010
227	18.92	0.07	0.020	(0.195)	0.010	0.010
228	19.00	0.07	0.020	(0.194)	0.010	0.010
229	19.08	0.10	0.031	(0.193)	0.015	0.015
230	19.17	0.10	0.031	(0.192)	0.015	0.015
231	19.25	0.10	0.031	(0.191)	0.015	0.015
232	19.33	0.13	0.041	(0.190)	0.020	0.020
233	19.42	0.13	0.041	(0.189)	0.020	0.020
234	19.50	0.13	0.041	(0.188)	0.020	0.020
235	19.58	0.10	0.031	(0.187)	0.015	0.015
236	19.67	0.10	0.031	(0.187)	0.015	0.015
237	19.75	0.10	0.031	(0.186)	0.015	0.015
238	19.83	0.07	0.020	(0.185)	0.010	0.010
239	19.92	0.07	0.020	(0.184)	0.010	0.010
240	20.00	0.07	0.020	(0.183)	0.010	0.010
241	20.08	0.10	0.031	(0.182)	0.015	0.015
242	20.17	0.10	0.031	(0.182)	0.015	0.015

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243  20.25     0.10      0.031       (  0.181)       0.015        0.015
244  20.33     0.10      0.031       (  0.180)       0.015        0.015
245  20.42     0.10      0.031       (  0.179)       0.015        0.015
246  20.50     0.10      0.031       (  0.179)       0.015        0.015
247  20.58     0.10      0.031       (  0.178)       0.015        0.015
248  20.67     0.10      0.031       (  0.177)       0.015        0.015
249  20.75     0.10      0.031       (  0.176)       0.015        0.015
250  20.83     0.07      0.020       (  0.176)       0.010        0.010
251  20.92     0.07      0.020       (  0.175)       0.010        0.010
252  21.00     0.07      0.020       (  0.174)       0.010        0.010
253  21.08     0.10      0.031       (  0.174)       0.015        0.015
254  21.17     0.10      0.031       (  0.173)       0.015        0.015
255  21.25     0.10      0.031       (  0.172)       0.015        0.015
256  21.33     0.07      0.020       (  0.172)       0.010        0.010
257  21.42     0.07      0.020       (  0.171)       0.010        0.010
258  21.50     0.07      0.020       (  0.170)       0.010        0.010
259  21.58     0.10      0.031       (  0.170)       0.015        0.015
260  21.67     0.10      0.031       (  0.169)       0.015        0.015
261  21.75     0.10      0.031       (  0.168)       0.015        0.015
262  21.83     0.07      0.020       (  0.168)       0.010        0.010
263  21.92     0.07      0.020       (  0.167)       0.010        0.010
264  22.00     0.07      0.020       (  0.167)       0.010        0.010
265  22.08     0.10      0.031       (  0.166)       0.015        0.015
266  22.17     0.10      0.031       (  0.166)       0.015        0.015
267  22.25     0.10      0.031       (  0.165)       0.015        0.015
268  22.33     0.07      0.020       (  0.165)       0.010        0.010
269  22.42     0.07      0.020       (  0.164)       0.010        0.010
270  22.50     0.07      0.020       (  0.164)       0.010        0.010
271  22.58     0.07      0.020       (  0.163)       0.010        0.010
272  22.67     0.07      0.020       (  0.163)       0.010        0.010
273  22.75     0.07      0.020       (  0.162)       0.010        0.010
274  22.83     0.07      0.020       (  0.162)       0.010        0.010
275  22.92     0.07      0.020       (  0.161)       0.010        0.010
276  23.00     0.07      0.020       (  0.161)       0.010        0.010
277  23.08     0.07      0.020       (  0.161)       0.010        0.010
278  23.17     0.07      0.020       (  0.160)       0.010        0.010
279  23.25     0.07      0.020       (  0.160)       0.010        0.010
280  23.33     0.07      0.020       (  0.160)       0.010        0.010
281  23.42     0.07      0.020       (  0.159)       0.010        0.010
282  23.50     0.07      0.020       (  0.159)       0.010        0.010
283  23.58     0.07      0.020       (  0.159)       0.010        0.010
284  23.67     0.07      0.020       (  0.158)       0.010        0.010
285  23.75     0.07      0.020       (  0.158)       0.010        0.010
286  23.83     0.07      0.020       (  0.158)       0.010        0.010
287  23.92     0.07      0.020       (  0.158)       0.010        0.010
288  24.00     0.07      0.020       (  0.158)       0.010        0.010
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    15.3
      Flood volume = Effective rainfall      1.27(In)
       times area      51.8(Ac.)/[(In)/(Ft.)] =       5.5(Ac.Ft)
      Total soil loss =      1.27(In)
      Total soil loss =     5.502(Ac.Ft)
      Total rainfall =      2.55(In)
      Flood volume =      239673.8 Cubic Feet
      Total soil loss =      239673.8 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      9.054(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0011      0.16  Q          |         |         |         |
   0+10       0.0039      0.41  VQ         |         |         |         |
   0+15       0.0072      0.48  VQ         |         |         |         |
   0+20       0.0112      0.58  V Q        |         |         |         |
   0+25       0.0162      0.73  V Q        |         |         |         |
   0+30       0.0215      0.77  V  Q       |         |         |         |
   0+35       0.0269      0.79  V  Q       |         |         |         |
   0+40       0.0324      0.79  V  Q       |         |         |         |
   0+45       0.0379      0.80  V  Q       |         |         |         |
   0+50       0.0439      0.88  V  Q       |         |         |         |
   0+55       0.0509      1.00  V   Q      |         |         |         |
   1+ 0       0.0580      1.04  V   Q      |         |         |         |
   1+ 5       0.0647      0.97  V  Q       |         |         |         |
   1+10       0.0706      0.85  V  Q       |         |         |         |
   1+15       0.0763      0.83  V  Q       |         |         |         |
   1+20       0.0819      0.81  V  Q       |         |         |         |
   1+25       0.0874      0.80  V  Q       |         |         |         |
   1+30       0.0929      0.80  V  Q       |         |         |         |
   1+35       0.0984      0.80  V  Q       |         |         |         |
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1+40 0.1039 0.80
1+45 0.1094 0.80
1+50 0.1155 0.88
1+55 0.1224 1.00
2+ 0 0.1295 1.04
2+ 5 0.1368 1.05
2+10 0.1441 1.06
2+15 0.1514 1.07
2+20 0.1587 1.07
2+25 0.1661 1.07
2+30 0.1734 1.07
2+35 0.1813 1.14
2+40 0.1900 1.27
2+45 0.1990 1.30
2+50 0.2081 1.32
2+55 0.2172 1.33
3+ 0 0.2264 1.33
3+ 5 0.2356 1.33
3+10 0.2447 1.33
3+15 0.2539 1.33
3+20 0.2631 1.33
3+25 0.2722 1.33
3+30 0.2814 1.33
3+35 0.2906 1.33
3+40 0.2997 1.33
3+45 0.3089 1.33
3+50 0.3186 1.41
3+55 0.3292 1.54
4+ 0 0.3400 1.57
4+ 5 0.3509 1.58
4+10 0.3619 1.59
4+15 0.3729 1.60
4+20 0.3844 1.68
4+25 0.3969 1.80
4+30 0.4095 1.84
4+35 0.4223 1.85
4+40 0.4351 1.86
4+45 0.4479 1.86
4+50 0.4613 1.94
4+55 0.4755 2.07
5+ 0 0.4900 2.10
5+ 5 0.5035 1.96
5+10 0.5153 1.71
5+15 0.5267 1.65
5+20 0.5384 1.70
5+25 0.5509 1.82
5+30 0.5636 1.84
5+35 0.5769 1.93
5+40 0.5911 2.06
5+45 0.6055 2.10
5+50 0.6201 2.12
5+55 0.6348 2.12
6+ 0 0.6494 2.13
6+ 5 0.6646 2.21
6+10 0.6807 2.34
6+15 0.6970 2.37
6+20 0.7135 2.38
6+25 0.7299 2.39
6+30 0.7464 2.40
6+35 0.7635 2.47
6+40 0.7814 2.60
6+45 0.7995 2.63
6+50 0.8178 2.65
6+55 0.8361 2.66
7+ 0 0.8544 2.66
7+ 5 0.8728 2.66
7+10 0.8911 2.66
7+15 0.9094 2.66
7+20 0.9283 2.74
7+25 0.9481 2.87
7+30 0.9681 2.90
7+35 0.9887 2.99
7+40 1.0102 3.13
7+45 1.0321 3.17
7+50 1.0545 3.26
7+55 1.0779 3.40
8+ 0 1.1015 3.43
8+ 5 1.1264 3.60
8+10 1.1530 3.87
8+15 1.1801 3.94
8+20 1.2074 3.97
8+25 1.2349 3.98
8+30 1.2624 3.99
8+35 1.2904 4.07
8+40 1.3194 4.20
8+45 1.3485 4.23

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 8+50       1.3783      4.33  |          V       Q  |          |          |
 8+55       1.4090      4.46  |          V       Q  |          |          |
 9+ 0       1.4400      4.50  |          V       Q  |          |          |
 9+ 5       1.4722      4.67  |          V        Q |          |          |
 9+10       1.5061      4.93  |          V         Q|          |          |
 9+15       1.5406      5.00  |          |V          Q          |          |
 9+20       1.5758      5.11  |          |V          Q          |          |
 9+25       1.6120      5.25  |          |V          |Q         |          |
 9+30       1.6485      5.30  |          |V          |Q         |          |
 9+35       1.6856      5.39  |          | V         |Q         |          |
 9+40       1.7236      5.53  |          | V         | Q        |          |
 9+45       1.7620      5.56  |          | V         | Q        |          |
 9+50       1.8009      5.66  |          |  V        | Q        |          |
 9+55       1.8408      5.79  |          |  V        |  Q       |          |
10+ 0       1.8810      5.83  |          |  V        |  Q       |          |
10+ 5       1.9175      5.30  |          |  V        |Q         |          |
10+10       1.9479      4.41  |          |   V  Q    |          |          |
10+15       1.9767      4.19  |          |   V Q     |          |          |
10+20       2.0049      4.09  |          |   V Q     |          |          |
10+25       2.0327      4.04  |          |   V Q     |          |          |
10+30       2.0602      3.99  |          |   VQ      |          |          |
10+35       2.0904      4.38  |          |    V Q    |          |          |
10+40       2.1250      5.02  |          |    V      Q          |          |
10+45       2.1607      5.19  |          |    V      Q          |          |
10+50       2.1969      5.26  |          |    V      |Q         |          |
10+55       2.2334      5.30  |          |     V     |Q         |          |
11+ 0       2.2701      5.33  |          |     V     |Q         |          |
11+ 5       2.3062      5.25  |          |     V     Q          |          |
11+10       2.3415      5.12  |          |      V    Q          |          |
11+15       2.3765      5.09  |          |      V    Q          |          |
11+20       2.4115      5.07  |          |      V    Q          |          |
11+25       2.4464      5.07  |          |      V    Q          |          |
11+30       2.4812      5.06  |          |       V Q           |          |
11+35       2.5150      4.90  |          |       VQ|           |          |
11+40       2.5470      4.65  |          |       Q |           |          |
11+45       2.5785      4.58  |          |       Q |           |          |
11+50       2.6105      4.63  |          |       Q |           |          |
11+55       2.6431      4.74  |          |       QV|           |          |
12+ 0       2.6759      4.77  |          |        Q|           |          |
12+ 5       2.7126      5.33  |          |        V|Q          |          |
12+10       2.7555      6.23  |          |         V   Q       |          |
12+15       2.8000      6.46  |          |         V    Q      |          |
12+20       2.8457      6.64  |          |         V     Q     |          |
12+25       2.8927      6.82  |          |         |V     Q    |          |
12+30       2.9402      6.90  |          |         |V     Q    |          |
12+35       2.9889      7.07  |          |         |V      Q   |          |
12+40       3.0394      7.33  |          |         | V      Q|          |
12+45       3.0903      7.40  |          |         | V      Q|          |
12+50       3.1420      7.51  |          |         | V       Q          |
12+55       3.1947      7.65  |          |         |  V      Q          |
13+ 0       3.2477      7.69  |          |         |  V      Q          |
13+ 5       3.3035      8.10  |          |         |   V      | Q       |
13+10       3.3637      8.75  |          |         |   V      |   Q     |
13+15       3.4251      8.91  |          |         |   V      |    Q    |
13+20       3.4870      8.99  |          |         |    V     |    Q    |
13+25       3.5492      9.03  |          |         |    V     |     Q   |
13+30       3.6115      9.05  |          |         |     V    |     Q   |
13+35       3.6680      8.20  |          |         |     V    | Q       |
13+40       3.7148      6.79  |          |         |      Q   |         |
13+45       3.7591      6.43  |          |         |    Q V   |         |
13+50       3.8023      6.28  |          |         |    Q V   |         |
13+55       3.8449      6.19  |          |         |   Q  V   |         |
14+ 0       3.8871      6.12  |          |         |   Q   V  |         |
14+ 5       3.9314      6.44  |          |         |    Q  V  |         |
14+10       3.9793      6.95  |          |         |      QV  |         |
14+15       4.0280      7.08  |          |         |       QV|         |
14+20       4.0766      7.06  |          |         |       QV|         |
14+25       4.1246      6.96  |          |         |      Q V|         |
14+30       4.1724      6.95  |          |         |      Q  V         |
14+35       4.2202      6.94  |          |         |      Q  V         |
14+40       4.2679      6.93  |          |         |      Q  |V        |
14+45       4.3156      6.92  |          |         |      Q  |V        |
14+50       4.3628      6.85  |          |         |      Q  |V        |
14+55       4.4090      6.72  |          |         |     Q   | V       |
15+ 0       4.4551      6.69  |          |         |     Q   | V       |
15+ 5       4.5005      6.59  |          |         |     Q   | V       |
15+10       4.5450      6.46  |          |         |    Q    |  V      |
15+15       4.5892      6.42  |          |         |    Q    |  V      |
15+20       4.6328      6.33  |          |         |    Q    |  V      |
15+25       4.6754      6.19  |          |         |   Q     |  V      |
15+30       4.7178      6.15  |          |         |   Q     |   V     |
15+35       4.7579      5.83  |          |         |  Q      |   V     |
15+40       4.7945      5.31  |          |         |Q        |   V     |
15+45       4.8301      5.17  |          |         Q         |    V    |
15+50       4.8653      5.11  |          |         Q         |    V    |
15+55       4.9003      5.08  |          |         Q         |    V    |
```

16+ 0	4.9352	5.06			Q		V
16+ 5	4.9620	3.89		Q			V
16+10	4.9755	1.97					V
16+15	4.9858	1.49	Q				V
16+20	4.9945	1.27	Q				V
16+25	5.0025	1.15	Q				V
16+30	5.0098	1.07	Q				V
16+35	5.0166	0.99	Q				V
16+40	5.0225	0.86	Q				V
16+45	5.0282	0.83	Q				V
16+50	5.0338	0.81	Q				V
16+55	5.0393	0.80	Q				V
17+ 0	5.0449	0.80	Q				V
17+ 5	5.0514	0.95	Q				V
17+10	5.0598	1.21	Q				V
17+15	5.0685	1.28	Q				V
17+20	5.0775	1.30	Q				V
17+25	5.0866	1.32	Q				V
17+30	5.0958	1.33	Q				V
17+35	5.1050	1.33	Q				V
17+40	5.1141	1.33	Q				V
17+45	5.1233	1.33	Q				V
17+50	5.1319	1.25	Q				V
17+55	5.1397	1.13	Q				V
18+ 0	5.1472	1.09	Q				V
18+ 5	5.1546	1.08	Q				V
18+10	5.1620	1.07	Q				V
18+15	5.1694	1.07	Q				V
18+20	5.1767	1.07	Q				V
18+25	5.1840	1.07	Q				V
18+30	5.1914	1.07	Q				V
18+35	5.1982	0.99	Q				V
18+40	5.2041	0.86	Q				V
18+45	5.2098	0.83	Q				V
18+50	5.2148	0.73	Q				V
18+55	5.2190	0.60	Q				V
19+ 0	5.2228	0.56	Q				V
19+ 5	5.2271	0.62	Q				V
19+10	5.2323	0.74	Q				V
19+15	5.2376	0.77	Q				V
19+20	5.2435	0.86	Q				V
19+25	5.2504	1.00	Q				V
19+30	5.2575	1.04	Q				V
19+35	5.2642	0.97	Q				V
19+40	5.2701	0.85	Q				V
19+45	5.2758	0.83	Q				V
19+50	5.2809	0.73	Q				V
19+55	5.2850	0.60	Q				V
20+ 0	5.2889	0.56	Q				V
20+ 5	5.2932	0.62	Q				V
20+10	5.2983	0.74	Q				V
20+15	5.3036	0.77	Q				V
20+20	5.3090	0.79	Q				V
20+25	5.3145	0.79	Q				V
20+30	5.3200	0.80	Q				V
20+35	5.3255	0.80	Q				V
20+40	5.3310	0.80	Q				V
20+45	5.3365	0.80	Q				V
20+50	5.3414	0.72	Q				V
20+55	5.3455	0.59	Q				V
21+ 0	5.3494	0.56	Q				V
21+ 5	5.3537	0.62	Q				V
21+10	5.3588	0.74	Q				V
21+15	5.3641	0.77	Q				V
21+20	5.3690	0.71	Q				V
21+25	5.3730	0.59	Q				V
21+30	5.3769	0.56	Q				V
21+35	5.3812	0.62	Q				V
21+40	5.3863	0.74	Q				V
21+45	5.3916	0.77	Q				V
21+50	5.3965	0.71	Q				V
21+55	5.4005	0.59	Q				V
22+ 0	5.4044	0.56	Q				V
22+ 5	5.4087	0.62	Q				V
22+10	5.4138	0.74	Q				V
22+15	5.4191	0.77	Q				V
22+20	5.4240	0.71	Q				V
22+25	5.4280	0.59	Q				V
22+30	5.4319	0.56	Q				V
22+35	5.4357	0.55	Q				V
22+40	5.4394	0.54	Q				V
22+45	5.4430	0.53	Q				V
22+50	5.4467	0.53	Q				V
22+55	5.4504	0.53	Q				V
23+ 0	5.4541	0.53	Q				V
23+ 5	5.4577	0.53	Q				V

```
   23+10       5.4614      0.53  | Q       |         |         |        v|
   23+15       5.4651      0.53  | Q       |         |         |        v|
   23+20       5.4687      0.53  | Q       |         |         |        v|
   23+25       5.4724      0.53  | Q       |         |         |        v|
   23+30       5.4761      0.53  | Q       |         |         |        v|
   23+35       5.4797      0.53  | Q       |         |         |        v|
   23+40       5.4834      0.53  | Q       |         |         |        v|
   23+45       5.4871      0.53  | Q       |         |         |        v|
   23+50       5.4907      0.53  | Q       |         |         |        v|
   23+55       5.4944      0.53  | Q       |         |         |        v|
   24+ 0       5.4981      0.53  | Q       |         |         |        v|
   24+ 5       5.5007      0.38  |Q        |         |         |        v|
   24+10       5.5015      0.12  Q         |         |         |        v|
   24+15       5.5019      0.06  Q         |         |         |        v|
   24+20       5.5021      0.03  Q         |         |         |        v|
   24+25       5.5022      0.01  Q         |         |         |         v
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       U n i t   H y d r o g r a p h   A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2976.00(Ft.)
Length along longest watercourse measured to centroid =    1488.00(Ft.)
Length along longest watercourse =      0.564 Mi.
Length along longest watercourse measured to centroid =      0.282 Mi.
Difference in elevation =     150.00(Ft.)
Slope along watercourse =    266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.062 Hr.
Lag time =     3.72 Min.
25% of lag time =     0.93 Min.
40% of lag time =     1.49 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           0.50                 25.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           1.30                 67.34

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.829(In)
Areal adjustment factor =   99.95 %
Adjusted average point rain =    0.829(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           69.00         0.500
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  69.0      0.373     0.500        0.205       1.000      0.205
                                                 Sum (F) =   0.205
Area averaged mean soil loss (F) (In/Hr) =  0.205
Minimum soil loss rate ((In/Hr)) =  0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
			Sum = 100.000 Sum=	52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.328	(0.205)	0.164	0.164
2	0.17	4.20	0.418	0.205	(0.209)	0.213
3	0.25	4.40	0.438	0.205	(0.219)	0.233
4	0.33	4.80	0.477	0.205	(0.239)	0.272
5	0.42	5.20	0.517	0.205	(0.259)	0.312
6	0.50	6.20	0.617	0.205	(0.308)	0.412
7	0.58	6.80	0.676	0.205	(0.338)	0.471
8	0.67	8.80	0.875	0.205	(0.438)	0.670
9	0.75	13.90	1.382	0.205	(0.691)	1.177
10	0.83	31.40	3.123	0.205	(1.561)	2.918
11	0.92	7.20	0.716	0.205	(0.358)	0.511
12	1.00	3.80	0.378	(0.205)	0.189	0.189
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	7.5

Flood volume = Effective rainfall 0.63(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 2.7(Ac.Ft)
Total soil loss = 0.20(In)
Total soil loss = 0.865(Ac.Ft)
Total rainfall = 0.83(In)
Flood volume = 118170.0 Cubic Feet
Total soil loss = 37660.7 Cubic Feet

Peak flow rate of this hydrograph = 91.590(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	25.0	50.0	75.0	100.0
0+ 5	0.0173	2.51	VQ				
0+10	0.0680	7.37	|VQ				
0+15	0.1364	9.93	| VQ				
0+20	0.2177	11.81	| VQ				
0+25	0.3137	13.93	| VQ				
0+30	0.4309	17.02	| Q				
0+35	0.5747	20.88	| Q				
0+40	0.7555	26.24	| QV				
0+45	1.0292	39.75	| Q				
0+50	1.5850	80.70	| V			Q	
0+55	2.2158	91.59	|			V Q	
1+ 0	2.4854	39.15	| Q			V	
1+ 5	2.6149	18.80	| Q			V	
1+10	2.6732	8.47	| Q			V	
1+15	2.7053	4.65	|Q			V	
1+20	2.7113	0.87	Q			V	
1+25	2.7128	0.22	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro210310.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2976.00(Ft.)
Length along longest watercourse measured to centroid = 1488.00(Ft.)
Length along longest watercourse = 0.564 Mi.
Length along longest watercourse measured to centroid = 0.282 Mi.
Difference in elevation = 150.00(Ft.)
Slope along watercourse = 266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.062 Hr.
Lag time = 3.72 Min.
25% of lag time = 0.93 Min.
40% of lag time = 1.49 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	0.80	41.44

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	2.00	103.60

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 1.294(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 1.293(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	69.00	0.500

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
		Sum = 100.000	Sum=	52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.202	(0.205)	0.101	0.101
2	0.17	1.30	0.202	(0.205)	0.101	0.101
3	0.25	1.10	0.171	(0.205)	0.085	0.085
4	0.33	1.50	0.233	(0.205)	0.116	0.116
5	0.42	1.50	0.233	(0.205)	0.116	0.116
6	0.50	1.80	0.279	(0.205)	0.140	0.140
7	0.58	1.50	0.233	(0.205)	0.116	0.116
8	0.67	1.80	0.279	(0.205)	0.140	0.140
9	0.75	1.80	0.279	(0.205)	0.140	0.140
10	0.83	1.50	0.233	(0.205)	0.116	0.116
11	0.92	1.60	0.248	(0.205)	0.124	0.124
12	1.00	1.80	0.279	(0.205)	0.140	0.140
13	1.08	2.20	0.341	(0.205)	0.171	0.171
14	1.17	2.20	0.341	(0.205)	0.171	0.171
15	1.25	2.20	0.341	(0.205)	0.171	0.171
16	1.33	2.00	0.310	(0.205)	0.155	0.155
17	1.42	2.60	0.404	(0.205)	0.202	0.202
18	1.50	2.70	0.419	0.205	(0.210)	0.214
19	1.58	2.40	0.372	(0.205)	0.186	0.186
20	1.67	2.70	0.419	0.205	(0.210)	0.214
21	1.75	3.30	0.512	0.205	(0.256)	0.307
22	1.83	3.10	0.481	0.205	(0.241)	0.276
23	1.92	2.90	0.450	0.205	(0.225)	0.245
24	2.00	3.00	0.466	0.205	(0.233)	0.261
25	2.08	3.10	0.481	0.205	(0.241)	0.276
26	2.17	4.20	0.652	0.205	(0.326)	0.447
27	2.25	5.00	0.776	0.205	(0.388)	0.571
28	2.33	3.50	0.543	0.205	(0.272)	0.338
29	2.42	6.80	1.055	0.205	(0.528)	0.850
30	2.50	7.30	1.133	0.205	(0.567)	0.928
31	2.58	8.20	1.273	0.205	(0.636)	1.068
32	2.67	5.90	0.916	0.205	(0.458)	0.711
33	2.75	2.00	0.310	(0.205)	0.155	0.155
34	2.83	1.80	0.279	(0.205)	0.140	0.140
35	2.92	1.80	0.279	(0.205)	0.140	0.140
36	3.00	0.60	0.093	(0.205)	0.047	0.047
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	9.7

Flood volume = Effective rainfall 0.81(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 3.5(Ac.Ft)
Total soil loss = 0.49(In)
Total soil loss = 2.102(Ac.Ft)
Total rainfall = 1.29(In)
Flood volume = 151649.0 Cubic Feet
Total soil loss = 91553.5 Cubic Feet

Peak flow rate of this hydrograph = 47.348(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	12.5	25.0	37.5	50.0
0+ 5	0.0106	1.54	VQ				
0+10	0.0387	4.07	V Q				
0+15	0.0695	4.48	V Q				
0+20	0.1029	4.85	V Q				
0+25	0.1420	5.68	V Q				
0+30	0.1854	6.31	V Q				
0+35	0.2309	6.60	V Q				
0+40	0.2760	6.55	V Q				
0+45	0.3248	7.09	V Q				
0+50	0.3720	6.85	VQ				
0+55	0.4163	6.44	VQ				
1+ 0	0.4627	6.73	Q				
1+ 5	0.5150	7.61	VQ				

```
    1+10       0.5734      8.47  |      Q    |           |           |           |
    1+15       0.6333      8.70  |      QV   |           |           |           |
    1+20       0.6924      8.58  |      QV   |           |           |           |
    1+25       0.7541      8.97  |       QV  |           |           |           |
    1+30       0.8248     10.26  |        QV |           |           |           |
    1+35       0.8963     10.39  |        Q V|           |           |           |
    1+40       0.9673     10.31  |        Q  |V          |           |           |
    1+45       1.0523     12.34  |         Q |  V        |           |           |
    1+50       1.1513     14.37  |           |Q V        |           |           |
    1+55       1.2461     13.76  |           |Q  V       |           |           |
    2+ 0       1.3376     13.29  |           Q    V      |           |           |
    2+ 5       1.4327     13.81  |           |Q    V     |           |           |
    2+10       1.5490     16.88  |           |  Q   V    |           |           |
    2+15       1.7082     23.12  |           |      QV   |           |           |
    2+20       1.8721     23.80  |           |        Q  |V          |           |
    2+25       2.0587     27.09  |           |           |Q V        |           |
    2+30       2.3361     40.28  |           |           |     V     | Q         |
    2+35       2.6622     47.35  |           |           |         V       Q   |
    2+40       2.9867     47.12  |           |           |           |   V   Q   |
    2+45       3.2023     31.31  |           |           |     Q     |     V     |
    2+50       3.3122     15.96  |           |  Q        |           |         V |
    2+55       3.3903     11.33  |         Q |           |           |         V |
    3+ 0       3.4444      7.86  |      Q    |           |           |           V|
    3+ 5       3.4685      3.50  |  Q        |           |           |           V|
    3+10       3.4759      1.08  Q           |           |           |           V|
    3+15       3.4794      0.51  Q           |           |           |           V|
    3+20       3.4810      0.23  Q           |           |           |           V|
    3+25       3.4814      0.05  Q           |           |           |           V|
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro210610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2976.00(Ft.)
Length along longest watercourse measured to centroid = 1488.00(Ft.)
Length along longest watercourse = 0.564 Mi.
Length along longest watercourse measured to centroid = 0.282 Mi.
Difference in elevation = 150.00(Ft.)
Slope along watercourse = 266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.062 Hr.
Lag time = 3.72 Min.
25% of lag time = 0.93 Min.
40% of lag time = 1.49 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	1.10	56.98

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	3.00	155.40

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.882(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 1.881(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	69.00	0.500

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.113	(0.205)	0.056	0.056
2	0.17	0.60	0.135	(0.205)	0.068	0.068
3	0.25	0.60	0.135	(0.205)	0.068	0.068
4	0.33	0.60	0.135	(0.205)	0.068	0.068
5	0.42	0.60	0.135	(0.205)	0.068	0.068
6	0.50	0.70	0.158	(0.205)	0.079	0.079
7	0.58	0.70	0.158	(0.205)	0.079	0.079
8	0.67	0.70	0.158	(0.205)	0.079	0.079
9	0.75	0.70	0.158	(0.205)	0.079	0.079
10	0.83	0.70	0.158	(0.205)	0.079	0.079
11	0.92	0.70	0.158	(0.205)	0.079	0.079
12	1.00	0.80	0.181	(0.205)	0.090	0.090
13	1.08	0.80	0.181	(0.205)	0.090	0.090
14	1.17	0.80	0.181	(0.205)	0.090	0.090
15	1.25	0.80	0.181	(0.205)	0.090	0.090
16	1.33	0.80	0.181	(0.205)	0.090	0.090
17	1.42	0.80	0.181	(0.205)	0.090	0.090
18	1.50	0.80	0.181	(0.205)	0.090	0.090
19	1.58	0.80	0.181	(0.205)	0.090	0.090
20	1.67	0.80	0.181	(0.205)	0.090	0.090
21	1.75	0.80	0.181	(0.205)	0.090	0.090
22	1.83	0.80	0.181	(0.205)	0.090	0.090
23	1.92	0.80	0.181	(0.205)	0.090	0.090
24	2.00	0.90	0.203	(0.205)	0.102	0.102
25	2.08	0.80	0.181	(0.205)	0.090	0.090
26	2.17	0.90	0.203	(0.205)	0.102	0.102
27	2.25	0.90	0.203	(0.205)	0.102	0.102
28	2.33	0.90	0.203	(0.205)	0.102	0.102
29	2.42	0.90	0.203	(0.205)	0.102	0.102
30	2.50	0.90	0.203	(0.205)	0.102	0.102
31	2.58	0.90	0.203	(0.205)	0.102	0.102
32	2.67	0.90	0.203	(0.205)	0.102	0.102
33	2.75	1.00	0.226	(0.205)	0.113	0.113
34	2.83	1.00	0.226	(0.205)	0.113	0.113
35	2.92	1.00	0.226	(0.205)	0.113	0.113
36	3.00	1.00	0.226	(0.205)	0.113	0.113
37	3.08	1.00	0.226	(0.205)	0.113	0.113
38	3.17	1.10	0.248	(0.205)	0.124	0.124
39	3.25	1.10	0.248	(0.205)	0.124	0.124
40	3.33	1.10	0.248	(0.205)	0.124	0.124
41	3.42	1.20	0.271	(0.205)	0.135	0.135
42	3.50	1.30	0.293	(0.205)	0.147	0.147
43	3.58	1.40	0.316	(0.205)	0.158	0.158
44	3.67	1.40	0.316	(0.205)	0.158	0.158
45	3.75	1.50	0.339	(0.205)	0.169	0.169
46	3.83	1.50	0.339	(0.205)	0.169	0.169
47	3.92	1.60	0.361	(0.205)	0.181	0.181
48	4.00	1.60	0.361	(0.205)	0.181	0.181
49	4.08	1.70	0.384	(0.205)	0.192	0.192
50	4.17	1.80	0.406	(0.205)	0.203	0.203
51	4.25	1.90	0.429	0.205	(0.214)	0.224
52	4.33	2.00	0.452	0.205	(0.226)	0.246
53	4.42	2.10	0.474	0.205	(0.237)	0.269
54	4.50	2.10	0.474	0.205	(0.237)	0.269
55	4.58	2.20	0.497	0.205	(0.248)	0.292
56	4.67	2.30	0.519	0.205	(0.260)	0.314
57	4.75	2.40	0.542	0.205	(0.271)	0.337
58	4.83	2.40	0.542	0.205	(0.271)	0.337
59	4.92	2.50	0.564	0.205	(0.282)	0.359
60	5.00	2.60	0.587	0.205	(0.293)	0.382
61	5.08	3.10	0.700	0.205	(0.350)	0.495
62	5.17	3.60	0.813	0.205	(0.406)	0.608
63	5.25	3.90	0.880	0.205	(0.440)	0.675
64	5.33	4.20	0.948	0.205	(0.474)	0.743
65	5.42	4.70	1.061	0.205	(0.531)	0.856
66	5.50	5.60	1.264	0.205	(0.632)	1.059
67	5.58	1.90	0.429	0.205	(0.214)	0.224
68	5.67	0.90	0.203	(0.205)	0.102	0.102
69	5.75	0.60	0.135	(0.205)	0.068	0.068
70	5.83	0.50	0.113	(0.205)	0.056	0.056

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71   5.92     0.30      0.068       (  0.205)       0.034        0.034
72   6.00     0.20      0.045       (  0.205)       0.023        0.023
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =    13.4
     Flood volume = Effective rainfall      1.12(In)
      times area      51.8(Ac.)/[(In)/(Ft.)] =       4.8(Ac.Ft)
     Total soil loss =      0.77(In)
     Total soil loss =     3.304(Ac.Ft)
     Total rainfall =      1.88(In)
     Flood volume =      209813.7 Cubic Feet
     Total soil loss =      143942.2 Cubic Feet
     ---------------------------------------------------------------------
      Peak flow rate of this hydrograph =     45.795(CFS)
     ---------------------------------------------------------------------
     +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
     ---------------------------------------------------------------------
                 Hydrograph in   5   Minute intervals ((CFS))

     ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0       12.5      25.0      37.5      50.0
-------------------------------------------------------------------------
  0+ 5       0.0059      0.86  Q         |         |         |         |
  0+10       0.0228      2.45  VQ        |         |         |         |
  0+15       0.0441      3.09  V Q       |         |         |         |
  0+20       0.0670      3.32  V Q       |         |         |         |
  0+25       0.0907      3.44  V Q       |         |         |         |
  0+30       0.1162      3.70  V Q       |         |         |         |
  0+35       0.1437      3.99  |V Q       |         |         |         |
  0+40       0.1717      4.07  |V Q       |         |         |         |
  0+45       0.1999      4.10  |V Q       |         |         |         |
  0+50       0.2282      4.11  |V Q       |         |         |         |
  0+55       0.2567      4.13  | VQ       |         |         |         |
  1+ 0       0.2863      4.30  | VQ       |         |         |         |
  1+ 5       0.3178      4.58  | VQ       |         |         |         |
  1+10       0.3499      4.65  | VQ       |         |         |         |
  1+15       0.3822      4.69  |  Q       |         |         |         |
  1+20       0.4146      4.70  |  Q       |         |         |         |
  1+25       0.4470      4.72  |  Q       |         |         |         |
  1+30       0.4795      4.72  |  Q       |         |         |         |
  1+35       0.5120      4.72  |  QV      |         |         |         |
  1+40       0.5445      4.72  |  QV      |         |         |         |
  1+45       0.5770      4.72  |  QV      |         |         |         |
  1+50       0.6095      4.72  |  Q V     |         |         |         |
  1+55       0.6420      4.72  |  Q V     |         |         |         |
  2+ 0       0.6756      4.89  |  Q V     |         |         |         |
  2+ 5       0.7101      5.00  |  Q V     |         |         |         |
  2+10       0.7442      4.96  |  Q  V    |         |         |         |
  2+15       0.7801      5.20  |   Q V    |         |         |         |
  2+20       0.8163      5.26  |   Q V    |         |         |         |
  2+25       0.8527      5.29  |   Q  V   |         |         |         |
  2+30       0.8892      5.29  |   Q  V   |         |         |         |
  2+35       0.9257      5.31  |   Q  V   |         |         |         |
  2+40       0.9623      5.31  |   Q  V   |         |         |         |
  2+45       1.0000      5.48  |   Q   V  |         |         |         |
  2+50       1.0397      5.76  |   Q   V  |         |         |         |
  2+55       1.0799      5.83  |   Q   V  |         |         |         |
  3+ 0       1.1203      5.87  |   Q    V|         |         |         |
  3+ 5       1.1608      5.88  |   Q    V|         |         |         |
  3+10       1.2026      6.07  |   Q    V|         |         |         |
  3+15       1.2463      6.35  |    Q    V         |         |         |
  3+20       1.2906      6.42  |    Q    V         |         |         |
  3+25       1.3362      6.63  |    Q    |V        |         |         |
  3+30       1.3851      7.10  |    Q    |V        |         |         |
  3+35       1.4377      7.64  |     Q   |V        |         |         |
  3+40       1.4930      8.03  |     Q   | V       |         |         |
  3+45       1.5503      8.32  |     Q   | V       |         |         |
  3+50       1.6100      8.67  |     Q   |  V      |         |         |
  3+55       1.6716      8.94  |      Q  |  V      |         |         |
  4+ 0       1.7354      9.27  |      Q  |   V     |         |         |
  4+ 5       1.8011      9.53  |      Q  |   V     |         |         |
  4+10       1.8702     10.03  |       Q |    V    |         |         |
  4+15       1.9440     10.72  |       Q |     V   |         |         |
  4+20       2.0246     11.70  |        Q|     V   |         |         |
  4+25       2.1127     12.79  |         Q      V  |         |         |
  4+30       2.2063     13.59  |         Q       V |         |         |
  4+35       2.3041     14.19  |         |Q       V|         |         |
  4+40       2.4089     15.22  |         | Q       V         |         |
  4+45       2.5214     16.34  |         |  Q      V         |         |
  4+50       2.6395     17.14  |         |  Q      |V        |         |
  4+55       2.7615     17.73  |         |   Q     | V       |         |
  5+ 0       2.8907     18.76  |         |    Q    |   V     |         |
  5+ 5       3.0371     21.26  |         |      Q  |    V    |         |
  5+10       3.2165     26.05  |         |         Q     V   |         |
  5+15       3.4282     30.73  |         |         |   Q   V |         |
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    5+20       3.6662     34.56  |          |          |       Q  V          |
    5+25       3.9343     38.93  |          |          |          |QV        |
    5+30       4.2497     45.79  |          |          |          |    VQ    |
    5+35       4.5202     39.27  |          |          |          |Q     V   |
    5+40       4.6458     18.24  |          |    Q     |          |       V  |
    5+45       4.7157     10.16  |          Q |        |          |          V|
    5+50       4.7601      6.45  |       Q    |        |          |          V|
    5+55       4.7891      4.21  |    Q       |        |          |          V|
    6+ 0       4.8040      2.16  |Q           |        |          |          V|
    6+ 5       4.8120      1.16  Q            |        |          |          V|
    6+10       4.8147      0.40  Q            |        |          |          V|
    6+15       4.8160      0.18  Q            |        |          |          V|
    6+20       4.8165      0.07  Q            |        |          |          V|
    6+25       4.8167      0.03  Q            |        |          |           V
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro2102410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2976.00(Ft.)
Length along longest watercourse measured to centroid = 1488.00(Ft.)
Length along longest watercourse = 0.564 Mi.
Length along longest watercourse measured to centroid = 0.282 Mi.
Difference in elevation = 150.00(Ft.)
Slope along watercourse = 266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.062 Hr.
Lag time = 3.72 Min.
25% of lag time = 0.93 Min.
40% of lag time = 1.49 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	1.80	93.24

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	5.00	259.00

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 3.117(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 3.116(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	69.00	0.500

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.025	(0.363)	0.012	0.012
2	0.17	0.07	0.025	(0.362)	0.012	0.012
3	0.25	0.07	0.025	(0.361)	0.012	0.012
4	0.33	0.10	0.037	(0.359)	0.019	0.019
5	0.42	0.10	0.037	(0.358)	0.019	0.019
6	0.50	0.10	0.037	(0.356)	0.019	0.019
7	0.58	0.10	0.037	(0.355)	0.019	0.019
8	0.67	0.10	0.037	(0.354)	0.019	0.019
9	0.75	0.10	0.037	(0.352)	0.019	0.019
10	0.83	0.13	0.050	(0.351)	0.025	0.025
11	0.92	0.13	0.050	(0.350)	0.025	0.025
12	1.00	0.13	0.050	(0.348)	0.025	0.025
13	1.08	0.10	0.037	(0.347)	0.019	0.019
14	1.17	0.10	0.037	(0.345)	0.019	0.019
15	1.25	0.10	0.037	(0.344)	0.019	0.019
16	1.33	0.10	0.037	(0.343)	0.019	0.019
17	1.42	0.10	0.037	(0.341)	0.019	0.019
18	1.50	0.10	0.037	(0.340)	0.019	0.019
19	1.58	0.10	0.037	(0.339)	0.019	0.019
20	1.67	0.10	0.037	(0.337)	0.019	0.019
21	1.75	0.10	0.037	(0.336)	0.019	0.019
22	1.83	0.13	0.050	(0.335)	0.025	0.025
23	1.92	0.13	0.050	(0.333)	0.025	0.025
24	2.00	0.13	0.050	(0.332)	0.025	0.025
25	2.08	0.13	0.050	(0.330)	0.025	0.025
26	2.17	0.13	0.050	(0.329)	0.025	0.025
27	2.25	0.13	0.050	(0.328)	0.025	0.025
28	2.33	0.13	0.050	(0.326)	0.025	0.025
29	2.42	0.13	0.050	(0.325)	0.025	0.025
30	2.50	0.13	0.050	(0.324)	0.025	0.025
31	2.58	0.17	0.062	(0.323)	0.031	0.031
32	2.67	0.17	0.062	(0.321)	0.031	0.031
33	2.75	0.17	0.062	(0.320)	0.031	0.031
34	2.83	0.17	0.062	(0.319)	0.031	0.031
35	2.92	0.17	0.062	(0.317)	0.031	0.031
36	3.00	0.17	0.062	(0.316)	0.031	0.031
37	3.08	0.17	0.062	(0.315)	0.031	0.031
38	3.17	0.17	0.062	(0.313)	0.031	0.031
39	3.25	0.17	0.062	(0.312)	0.031	0.031
40	3.33	0.17	0.062	(0.311)	0.031	0.031
41	3.42	0.17	0.062	(0.309)	0.031	0.031
42	3.50	0.17	0.062	(0.308)	0.031	0.031
43	3.58	0.17	0.062	(0.307)	0.031	0.031
44	3.67	0.17	0.062	(0.306)	0.031	0.031
45	3.75	0.17	0.062	(0.304)	0.031	0.031
46	3.83	0.20	0.075	(0.303)	0.037	0.037
47	3.92	0.20	0.075	(0.302)	0.037	0.037
48	4.00	0.20	0.075	(0.300)	0.037	0.037
49	4.08	0.20	0.075	(0.299)	0.037	0.037
50	4.17	0.20	0.075	(0.298)	0.037	0.037
51	4.25	0.20	0.075	(0.297)	0.037	0.037
52	4.33	0.23	0.087	(0.295)	0.044	0.044
53	4.42	0.23	0.087	(0.294)	0.044	0.044
54	4.50	0.23	0.087	(0.293)	0.044	0.044
55	4.58	0.23	0.087	(0.292)	0.044	0.044
56	4.67	0.23	0.087	(0.290)	0.044	0.044
57	4.75	0.23	0.087	(0.289)	0.044	0.044
58	4.83	0.27	0.100	(0.288)	0.050	0.050
59	4.92	0.27	0.100	(0.287)	0.050	0.050
60	5.00	0.27	0.100	(0.285)	0.050	0.050
61	5.08	0.20	0.075	(0.284)	0.037	0.037
62	5.17	0.20	0.075	(0.283)	0.037	0.037
63	5.25	0.20	0.075	(0.282)	0.037	0.037
64	5.33	0.23	0.087	(0.280)	0.044	0.044
65	5.42	0.23	0.087	(0.279)	0.044	0.044
66	5.50	0.23	0.087	(0.278)	0.044	0.044
67	5.58	0.27	0.100	(0.277)	0.050	0.050
68	5.67	0.27	0.100	(0.275)	0.050	0.050
69	5.75	0.27	0.100	(0.274)	0.050	0.050
70	5.83	0.27	0.100	(0.273)	0.050	0.050

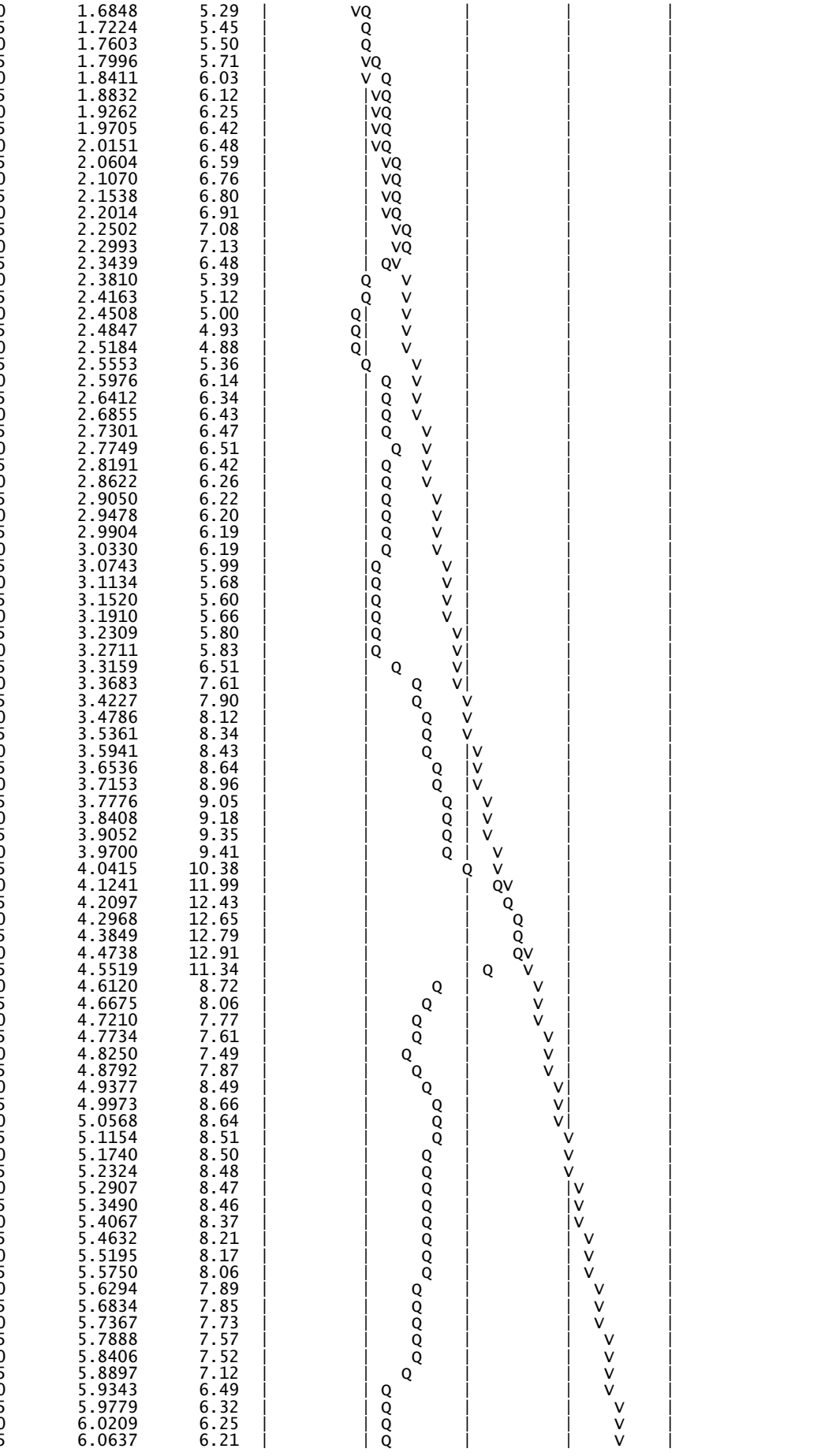
71	5.92	0.27	0.100	(0.272)	0.050	0.050
72	6.00	0.27	0.100	(0.271)	0.050	0.050
73	6.08	0.30	0.112	(0.269)	0.056	0.056
74	6.17	0.30	0.112	(0.268)	0.056	0.056
75	6.25	0.30	0.112	(0.267)	0.056	0.056
76	6.33	0.30	0.112	(0.266)	0.056	0.056
77	6.42	0.30	0.112	(0.265)	0.056	0.056
78	6.50	0.30	0.112	(0.263)	0.056	0.056
79	6.58	0.33	0.125	(0.262)	0.062	0.062
80	6.67	0.33	0.125	(0.261)	0.062	0.062
81	6.75	0.33	0.125	(0.260)	0.062	0.062
82	6.83	0.33	0.125	(0.259)	0.062	0.062
83	6.92	0.33	0.125	(0.258)	0.062	0.062
84	7.00	0.33	0.125	(0.256)	0.062	0.062
85	7.08	0.33	0.125	(0.255)	0.062	0.062
86	7.17	0.33	0.125	(0.254)	0.062	0.062
87	7.25	0.33	0.125	(0.253)	0.062	0.062
88	7.33	0.37	0.137	(0.252)	0.069	0.069
89	7.42	0.37	0.137	(0.251)	0.069	0.069
90	7.50	0.37	0.137	(0.249)	0.069	0.069
91	7.58	0.40	0.150	(0.248)	0.075	0.075
92	7.67	0.40	0.150	(0.247)	0.075	0.075
93	7.75	0.40	0.150	(0.246)	0.075	0.075
94	7.83	0.43	0.162	(0.245)	0.081	0.081
95	7.92	0.43	0.162	(0.244)	0.081	0.081
96	8.00	0.43	0.162	(0.243)	0.081	0.081
97	8.08	0.50	0.187	(0.242)	0.093	0.093
98	8.17	0.50	0.187	(0.240)	0.093	0.093
99	8.25	0.50	0.187	(0.239)	0.093	0.093
100	8.33	0.50	0.187	(0.238)	0.093	0.093
101	8.42	0.50	0.187	(0.237)	0.093	0.093
102	8.50	0.50	0.187	(0.236)	0.093	0.093
103	8.58	0.53	0.199	(0.235)	0.100	0.100
104	8.67	0.53	0.199	(0.234)	0.100	0.100
105	8.75	0.53	0.199	(0.233)	0.100	0.100
106	8.83	0.57	0.212	(0.232)	0.106	0.106
107	8.92	0.57	0.212	(0.230)	0.106	0.106
108	9.00	0.57	0.212	(0.229)	0.106	0.106
109	9.08	0.63	0.237	(0.228)	0.118	0.118
110	9.17	0.63	0.237	(0.227)	0.118	0.118
111	9.25	0.63	0.237	(0.226)	0.118	0.118
112	9.33	0.67	0.249	(0.225)	0.125	0.125
113	9.42	0.67	0.249	(0.224)	0.125	0.125
114	9.50	0.67	0.249	(0.223)	0.125	0.125
115	9.58	0.70	0.262	(0.222)	0.131	0.131
116	9.67	0.70	0.262	(0.221)	0.131	0.131
117	9.75	0.70	0.262	(0.220)	0.131	0.131
118	9.83	0.73	0.274	(0.219)	0.137	0.137
119	9.92	0.73	0.274	(0.218)	0.137	0.137
120	10.00	0.73	0.274	(0.217)	0.137	0.137
121	10.08	0.50	0.187	(0.215)	0.093	0.093
122	10.17	0.50	0.187	(0.214)	0.093	0.093
123	10.25	0.50	0.187	(0.213)	0.093	0.093
124	10.33	0.50	0.187	(0.212)	0.093	0.093
125	10.42	0.50	0.187	(0.211)	0.093	0.093
126	10.50	0.50	0.187	(0.210)	0.093	0.093
127	10.58	0.67	0.249	(0.209)	0.125	0.125
128	10.67	0.67	0.249	(0.208)	0.125	0.125
129	10.75	0.67	0.249	(0.207)	0.125	0.125
130	10.83	0.67	0.249	(0.206)	0.125	0.125
131	10.92	0.67	0.249	(0.205)	0.125	0.125
132	11.00	0.67	0.249	(0.204)	0.125	0.125
133	11.08	0.63	0.237	(0.203)	0.118	0.118
134	11.17	0.63	0.237	(0.202)	0.118	0.118
135	11.25	0.63	0.237	(0.201)	0.118	0.118
136	11.33	0.63	0.237	(0.200)	0.118	0.118
137	11.42	0.63	0.237	(0.199)	0.118	0.118
138	11.50	0.63	0.237	(0.198)	0.118	0.118
139	11.58	0.57	0.212	(0.197)	0.106	0.106
140	11.67	0.57	0.212	(0.196)	0.106	0.106
141	11.75	0.57	0.212	(0.195)	0.106	0.106
142	11.83	0.60	0.224	(0.194)	0.112	0.112
143	11.92	0.60	0.224	(0.193)	0.112	0.112
144	12.00	0.60	0.224	(0.192)	0.112	0.112
145	12.08	0.83	0.312	(0.191)	0.156	0.156
146	12.17	0.83	0.312	(0.190)	0.156	0.156
147	12.25	0.83	0.312	(0.189)	0.156	0.156
148	12.33	0.87	0.324	(0.189)	0.162	0.162
149	12.42	0.87	0.324	(0.188)	0.162	0.162
150	12.50	0.87	0.324	(0.187)	0.162	0.162
151	12.58	0.93	0.349	(0.186)	0.175	0.175
152	12.67	0.93	0.349	(0.185)	0.175	0.175
153	12.75	0.93	0.349	(0.184)	0.175	0.175
154	12.83	0.97	0.361	(0.183)	0.181	0.181
155	12.92	0.97	0.361	(0.182)	0.181	0.181
156	13.00	0.97	0.361	(0.181)	0.181	0.181

157	13.08	1.13	0.424	0.180	(0.212)	0.244
158	13.17	1.13	0.424	0.179	(0.212)	0.245
159	13.25	1.13	0.424	0.178	(0.212)	0.245
160	13.33	1.13	0.424	0.177	(0.212)	0.246
161	13.42	1.13	0.424	0.177	(0.212)	0.247
162	13.50	1.13	0.424	0.176	(0.212)	0.248
163	13.58	0.77	0.287	(0.175)	0.143	0.143
164	13.67	0.77	0.287	(0.174)	0.143	0.143
165	13.75	0.77	0.287	(0.173)	0.143	0.143
166	13.83	0.77	0.287	(0.172)	0.143	0.143
167	13.92	0.77	0.287	(0.171)	0.143	0.143
168	14.00	0.77	0.287	(0.170)	0.143	0.143
169	14.08	0.90	0.337	(0.169)	0.168	0.168
170	14.17	0.90	0.337	(0.169)	0.168	0.168
171	14.25	0.90	0.337	0.168	(0.168)	0.169
172	14.33	0.87	0.324	(0.167)	0.162	0.162
173	14.42	0.87	0.324	(0.166)	0.162	0.162
174	14.50	0.87	0.324	(0.165)	0.162	0.162
175	14.58	0.87	0.324	(0.164)	0.162	0.162
176	14.67	0.87	0.324	(0.163)	0.162	0.162
177	14.75	0.87	0.324	(0.163)	0.162	0.162
178	14.83	0.83	0.312	(0.162)	0.156	0.156
179	14.92	0.83	0.312	(0.161)	0.156	0.156
180	15.00	0.83	0.312	(0.160)	0.156	0.156
181	15.08	0.80	0.299	(0.159)	0.150	0.150
182	15.17	0.80	0.299	(0.159)	0.150	0.150
183	15.25	0.80	0.299	(0.158)	0.150	0.150
184	15.33	0.77	0.287	(0.157)	0.143	0.143
185	15.42	0.77	0.287	(0.156)	0.143	0.143
186	15.50	0.77	0.287	(0.155)	0.143	0.143
187	15.58	0.63	0.237	(0.154)	0.118	0.118
188	15.67	0.63	0.237	(0.154)	0.118	0.118
189	15.75	0.63	0.237	(0.153)	0.118	0.118
190	15.83	0.63	0.237	(0.152)	0.118	0.118
191	15.92	0.63	0.237	(0.151)	0.118	0.118
192	16.00	0.63	0.237	(0.151)	0.118	0.118
193	16.08	0.13	0.050	(0.150)	0.025	0.025
194	16.17	0.13	0.050	(0.149)	0.025	0.025
195	16.25	0.13	0.050	(0.148)	0.025	0.025
196	16.33	0.13	0.050	(0.148)	0.025	0.025
197	16.42	0.13	0.050	(0.147)	0.025	0.025
198	16.50	0.13	0.050	(0.146)	0.025	0.025
199	16.58	0.10	0.037	(0.145)	0.019	0.019
200	16.67	0.10	0.037	(0.145)	0.019	0.019
201	16.75	0.10	0.037	(0.144)	0.019	0.019
202	16.83	0.10	0.037	(0.143)	0.019	0.019
203	16.92	0.10	0.037	(0.142)	0.019	0.019
204	17.00	0.10	0.037	(0.142)	0.019	0.019
205	17.08	0.17	0.062	(0.141)	0.031	0.031
206	17.17	0.17	0.062	(0.140)	0.031	0.031
207	17.25	0.17	0.062	(0.140)	0.031	0.031
208	17.33	0.17	0.062	(0.139)	0.031	0.031
209	17.42	0.17	0.062	(0.138)	0.031	0.031
210	17.50	0.17	0.062	(0.137)	0.031	0.031
211	17.58	0.17	0.062	(0.137)	0.031	0.031
212	17.67	0.17	0.062	(0.136)	0.031	0.031
213	17.75	0.17	0.062	(0.135)	0.031	0.031
214	17.83	0.13	0.050	(0.135)	0.025	0.025
215	17.92	0.13	0.050	(0.134)	0.025	0.025
216	18.00	0.13	0.050	(0.133)	0.025	0.025
217	18.08	0.13	0.050	(0.133)	0.025	0.025
218	18.17	0.13	0.050	(0.132)	0.025	0.025
219	18.25	0.13	0.050	(0.131)	0.025	0.025
220	18.33	0.13	0.050	(0.131)	0.025	0.025
221	18.42	0.13	0.050	(0.130)	0.025	0.025
222	18.50	0.13	0.050	(0.130)	0.025	0.025
223	18.58	0.10	0.037	(0.129)	0.019	0.019
224	18.67	0.10	0.037	(0.128)	0.019	0.019
225	18.75	0.10	0.037	(0.128)	0.019	0.019
226	18.83	0.07	0.025	(0.127)	0.012	0.012
227	18.92	0.07	0.025	(0.126)	0.012	0.012
228	19.00	0.07	0.025	(0.126)	0.012	0.012
229	19.08	0.10	0.037	(0.125)	0.019	0.019
230	19.17	0.10	0.037	(0.125)	0.019	0.019
231	19.25	0.10	0.037	(0.124)	0.019	0.019
232	19.33	0.13	0.050	(0.123)	0.025	0.025
233	19.42	0.13	0.050	(0.123)	0.025	0.025
234	19.50	0.13	0.050	(0.122)	0.025	0.025
235	19.58	0.10	0.037	(0.122)	0.019	0.019
236	19.67	0.10	0.037	(0.121)	0.019	0.019
237	19.75	0.10	0.037	(0.121)	0.019	0.019
238	19.83	0.07	0.025	(0.120)	0.012	0.012
239	19.92	0.07	0.025	(0.120)	0.012	0.012
240	20.00	0.07	0.025	(0.119)	0.012	0.012
241	20.08	0.10	0.037	(0.119)	0.019	0.019
242	20.17	0.10	0.037	(0.118)	0.019	0.019

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243  20.25     0.10      0.037       (  0.118)       0.019        0.019
244  20.33     0.10      0.037       (  0.117)       0.019        0.019
245  20.42     0.10      0.037       (  0.116)       0.019        0.019
246  20.50     0.10      0.037       (  0.116)       0.019        0.019
247  20.58     0.10      0.037       (  0.116)       0.019        0.019
248  20.67     0.10      0.037       (  0.115)       0.019        0.019
249  20.75     0.10      0.037       (  0.115)       0.019        0.019
250  20.83     0.07      0.025       (  0.114)       0.012        0.012
251  20.92     0.07      0.025       (  0.114)       0.012        0.012
252  21.00     0.07      0.025       (  0.113)       0.012        0.012
253  21.08     0.10      0.037       (  0.113)       0.019        0.019
254  21.17     0.10      0.037       (  0.112)       0.019        0.019
255  21.25     0.10      0.037       (  0.112)       0.019        0.019
256  21.33     0.07      0.025       (  0.111)       0.012        0.012
257  21.42     0.07      0.025       (  0.111)       0.012        0.012
258  21.50     0.07      0.025       (  0.111)       0.012        0.012
259  21.58     0.10      0.037       (  0.110)       0.019        0.019
260  21.67     0.10      0.037       (  0.110)       0.019        0.019
261  21.75     0.10      0.037       (  0.109)       0.019        0.019
262  21.83     0.07      0.025       (  0.109)       0.012        0.012
263  21.92     0.07      0.025       (  0.109)       0.012        0.012
264  22.00     0.07      0.025       (  0.108)       0.012        0.012
265  22.08     0.10      0.037       (  0.108)       0.019        0.019
266  22.17     0.10      0.037       (  0.108)       0.019        0.019
267  22.25     0.10      0.037       (  0.107)       0.019        0.019
268  22.33     0.07      0.025       (  0.107)       0.012        0.012
269  22.42     0.07      0.025       (  0.107)       0.012        0.012
270  22.50     0.07      0.025       (  0.106)       0.012        0.012
271  22.58     0.07      0.025       (  0.106)       0.012        0.012
272  22.67     0.07      0.025       (  0.106)       0.012        0.012
273  22.75     0.07      0.025       (  0.105)       0.012        0.012
274  22.83     0.07      0.025       (  0.105)       0.012        0.012
275  22.92     0.07      0.025       (  0.105)       0.012        0.012
276  23.00     0.07      0.025       (  0.105)       0.012        0.012
277  23.08     0.07      0.025       (  0.104)       0.012        0.012
278  23.17     0.07      0.025       (  0.104)       0.012        0.012
279  23.25     0.07      0.025       (  0.104)       0.012        0.012
280  23.33     0.07      0.025       (  0.104)       0.012        0.012
281  23.42     0.07      0.025       (  0.103)       0.012        0.012
282  23.50     0.07      0.025       (  0.103)       0.012        0.012
283  23.58     0.07      0.025       (  0.103)       0.012        0.012
284  23.67     0.07      0.025       (  0.103)       0.012        0.012
285  23.75     0.07      0.025       (  0.103)       0.012        0.012
286  23.83     0.07      0.025       (  0.103)       0.012        0.012
287  23.92     0.07      0.025       (  0.103)       0.012        0.012
288  24.00     0.07      0.025       (  0.103)       0.012        0.012
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    18.9
      Flood volume = Effective rainfall      1.58(In)
       times area      51.8(Ac.)/[(In)/(Ft.)] =       6.8(Ac.Ft)
      Total soil loss =      1.54(In)
      Total soil loss =     6.652(Ac.Ft)
      Total rainfall =      3.12(In)
      Flood volume =      296182.3 Cubic Feet
      Total soil loss =      289767.5 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     12.911(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
 ------------------------------------------------------------------------
   0+ 5       0.0013      0.19  Q          |         |         |         |
   0+10       0.0048      0.50  VQ         |         |         |         |
   0+15       0.0088      0.58  VQ         |         |         |         |
   0+20       0.0137      0.71  VQ         |         |         |         |
   0+25       0.0198      0.89  VQ         |         |         |         |
   0+30       0.0263      0.94  VQ         |         |         |         |
   0+35       0.0329      0.96  VQ         |         |         |         |
   0+40       0.0396      0.97  VQ         |         |         |         |
   0+45       0.0463      0.98  VQ         |         |         |         |
   0+50       0.0537      1.07  V Q        |         |         |         |
   0+55       0.0622      1.23  V Q        |         |         |         |
   1+ 0       0.0709      1.27  V Q        |         |         |         |
   1+ 5       0.0791      1.19  V Q        |         |         |         |
   1+10       0.0863      1.04  V Q        |         |         |         |
   1+15       0.0932      1.01  V Q        |         |         |         |
   1+20       0.1001      0.99  VQ         |         |         |         |
   1+25       0.1069      0.98  VQ         |         |         |         |
   1+30       0.1136      0.98  VQ         |         |         |         |
   1+35       0.1203      0.98  VQ         |         |         |         |
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1+40       0.1270      0.98  VQ        |         |         |         |
1+45       0.1338      0.98  VQ        |         |         |         |
1+50       0.1411      1.07  V Q       |         |         |         |
1+55       0.1496      1.23  V Q       |         |         |         |
2+ 0       0.1583      1.27  V Q       |         |         |         |
2+ 5       0.1672      1.29  V Q       |         |         |         |
2+10       0.1761      1.29  |VQ       |         |         |         |
2+15       0.1851      1.30  |VQ       |         |         |         |
2+20       0.1940      1.30  |VQ       |         |         |         |
2+25       0.2030      1.30  |VQ       |         |         |         |
2+30       0.2120      1.30  |VQ       |         |         |         |
2+35       0.2216      1.40  |VQ       |         |         |         |
2+40       0.2323      1.55  |V Q      |         |         |         |
2+45       0.2433      1.59  |V Q      |         |         |         |
2+50       0.2544      1.61  |V Q      |         |         |         |
2+55       0.2655      1.62  |V Q      |         |         |         |
3+ 0       0.2767      1.63  |V Q      |         |         |         |
3+ 5       0.2879      1.63  |V Q      |         |         |         |
3+10       0.2992      1.63  |V Q      |         |         |         |
3+15       0.3104      1.63  |V Q      |         |         |         |
3+20       0.3216      1.63  |V Q      |         |         |         |
3+25       0.3328      1.63  |V Q      |         |         |         |
3+30       0.3440      1.63  | VQ      |         |         |         |
3+35       0.3552      1.63  | VQ      |         |         |         |
3+40       0.3664      1.63  | VQ      |         |         |         |
3+45       0.3776      1.63  | VQ      |         |         |         |
3+50       0.3895      1.72  | VQ      |         |         |         |
3+55       0.4024      1.88  | VQ      |         |         |         |
4+ 0       0.4156      1.92  | VQ      |         |         |         |
4+ 5       0.4290      1.94  | VQ      |         |         |         |
4+10       0.4424      1.95  | VQ      |         |         |         |
4+15       0.4558      1.95  | VQ      |         |         |         |
4+20       0.4699      2.05  | V Q     |         |         |         |
4+25       0.4851      2.20  | V Q     |         |         |         |
4+30       0.5006      2.24  | V Q     |         |         |         |
4+35       0.5162      2.26  |  VQ     |         |         |         |
4+40       0.5318      2.27  |  VQ     |         |         |         |
4+45       0.5475      2.28  |  VQ     |         |         |         |
4+50       0.5638      2.37  |  VQ     |         |         |         |
4+55       0.5813      2.53  |  V Q    |         |         |         |
5+ 0       0.5990      2.57  |  V Q    |         |         |         |
5+ 5       0.6155      2.40  |  VQ     |         |         |         |
5+10       0.6299      2.09  |  VQ     |         |         |         |
5+15       0.6438      2.02  |  VQ     |         |         |         |
5+20       0.6582      2.08  |  VQ     |         |         |         |
5+25       0.6734      2.22  |  VQ     |         |         |         |
5+30       0.6889      2.24  |   Q     |         |         |         |
5+35       0.7051      2.36  |   Q     |         |         |         |
5+40       0.7225      2.52  |   VQ    |         |         |         |
5+45       0.7402      2.57  |   VQ    |         |         |         |
5+50       0.7580      2.59  |   VQ    |         |         |         |
5+55       0.7759      2.60  |   VQ    |         |         |         |
6+ 0       0.7939      2.60  |   VQ    |         |         |         |
6+ 5       0.8124      2.70  |   VQ    |         |         |         |
6+10       0.8321      2.86  |   VQ    |         |         |         |
6+15       0.8521      2.90  |    Q    |         |         |         |
6+20       0.8721      2.91  |    Q    |         |         |         |
6+25       0.8922      2.92  |    Q    |         |         |         |
6+30       0.9124      2.93  |    Q    |         |         |         |
6+35       0.9333      3.02  |    VQ   |         |         |         |
6+40       0.9552      3.18  |    VQ   |         |         |         |
6+45       0.9774      3.22  |    VQ   |         |         |         |
6+50       0.9997      3.24  |    VQ   |         |         |         |
6+55       1.0220      3.25  |     Q   |         |         |         |
7+ 0       1.0444      3.26  |     Q   |         |         |         |
7+ 5       1.0669      3.26  |     Q   |         |         |         |
7+10       1.0893      3.26  |     Q   |         |         |         |
7+15       1.1117      3.26  |     Q   |         |         |         |
7+20       1.1348      3.35  |     Q   |         |         |         |
7+25       1.1589      3.51  |     VQ  |         |         |         |
7+30       1.1834      3.55  |     VQ  |         |         |         |
7+35       1.2086      3.66  |      Q  |         |         |         |
7+40       1.2349      3.83  |      Q  |         |         |         |
7+45       1.2616      3.87  |      Q  |         |         |         |
7+50       1.2890      3.98  |      Q  |         |         |         |
7+55       1.3176      4.15  |      VQ |         |         |         |
8+ 0       1.3465      4.20  |      VQ |         |         |         |
8+ 5       1.3768      4.41  |       Q |         |         |         |
8+10       1.4094      4.73  |       VQ|         |         |         |
8+15       1.4426      4.81  |       VQ|         |         |         |
8+20       1.4760      4.85  |       VQ|         |         |         |
8+25       1.5095      4.87  |       VQ|         |         |         |
8+30       1.5431      4.88  |        Q|         |         |         |
8+35       1.5774      4.98  |        Q|         |         |         |
8+40       1.6128      5.13  |         VQ        |         |         |
8+45       1.6484      5.17  |         VQ        |         |         |
```

8+50	1.6848	5.29	
8+55	1.7224	5.45	
9+ 0	1.7603	5.50	
9+ 5	1.7996	5.71	
9+10	1.8411	6.03	
9+15	1.8832	6.12	
9+20	1.9262	6.25	
9+25	1.9705	6.42	
9+30	2.0151	6.48	
9+35	2.0604	6.59	
9+40	2.1070	6.76	
9+45	2.1538	6.80	
9+50	2.2014	6.91	
9+55	2.2502	7.08	
10+ 0	2.2993	7.13	
10+ 5	2.3439	6.48	
10+10	2.3810	5.39	
10+15	2.4163	5.12	
10+20	2.4508	5.00	
10+25	2.4847	4.93	
10+30	2.5184	4.88	
10+35	2.5553	5.36	
10+40	2.5976	6.14	
10+45	2.6412	6.34	
10+50	2.6855	6.43	
10+55	2.7301	6.47	
11+ 0	2.7749	6.51	
11+ 5	2.8191	6.42	
11+10	2.8622	6.26	
11+15	2.9050	6.22	
11+20	2.9478	6.20	
11+25	2.9904	6.19	
11+30	3.0330	6.19	
11+35	3.0743	5.99	
11+40	3.1134	5.68	
11+45	3.1520	5.60	
11+50	3.1910	5.66	
11+55	3.2309	5.80	
12+ 0	3.2711	5.83	
12+ 5	3.3159	6.51	
12+10	3.3683	7.61	
12+15	3.4227	7.90	
12+20	3.4786	8.12	
12+25	3.5361	8.34	
12+30	3.5941	8.43	
12+35	3.6536	8.64	
12+40	3.7153	8.96	
12+45	3.7776	9.05	
12+50	3.8408	9.18	
12+55	3.9052	9.35	
13+ 0	3.9700	9.41	
13+ 5	4.0415	10.38	
13+10	4.1241	11.99	
13+15	4.2097	12.43	
13+20	4.2968	12.65	
13+25	4.3849	12.79	
13+30	4.4738	12.91	
13+35	4.5519	11.34	
13+40	4.6120	8.72	
13+45	4.6675	8.06	
13+50	4.7210	7.77	
13+55	4.7734	7.61	
14+ 0	4.8250	7.49	
14+ 5	4.8792	7.87	
14+10	4.9377	8.49	
14+15	4.9973	8.66	
14+20	5.0568	8.64	
14+25	5.1154	8.51	
14+30	5.1740	8.50	
14+35	5.2324	8.48	
14+40	5.2907	8.47	
14+45	5.3490	8.46	
14+50	5.4067	8.37	
14+55	5.4632	8.21	
15+ 0	5.5195	8.17	
15+ 5	5.5750	8.06	
15+10	5.6294	7.89	
15+15	5.6834	7.85	
15+20	5.7367	7.73	
15+25	5.7888	7.57	
15+30	5.8406	7.52	
15+35	5.8897	7.12	
15+40	5.9343	6.49	
15+45	5.9779	6.32	
15+50	6.0209	6.25	
15+55	6.0637	6.21	

```
16+ 0       6.1063      6.19  |          | Q        |          |     V    |
16+ 5       6.1391      4.76  |        Q |          |          |      V   |
16+10       6.1557      2.41  |     Q    |          |          |      V   |
16+15       6.1682      1.82  |   Q      |          |          |      V   |
16+20       6.1789      1.55  |   Q      |          |          |      V   |
16+25       6.1886      1.41  | Q        |          |          |      V   |
16+30       6.1976      1.30  | Q        |          |          |      V   |
16+35       6.2059      1.21  | Q        |          |          |      V   |
16+40       6.2131      1.05  | Q        |          |          |      V   |
16+45       6.2201      1.01  | Q        |          |          |      V   |
16+50       6.2269      0.99  |Q         |          |          |      V   |
16+55       6.2337      0.98  |Q         |          |          |      V   |
17+ 0       6.2404      0.98  |Q         |          |          |      V   |
17+ 5       6.2484      1.17  | Q        |          |          |      V   |
17+10       6.2586      1.48  | Q        |          |          |      V   |
17+15       6.2694      1.56  |   Q      |          |          |      V   |
17+20       6.2804      1.59  |   Q      |          |          |      V   |
17+25       6.2915      1.61  |   Q      |          |          |       V  |
17+30       6.3027      1.63  |   Q      |          |          |       V  |
17+35       6.3139      1.63  |   Q      |          |          |       V  |
17+40       6.3251      1.63  |   Q      |          |          |       V  |
17+45       6.3363      1.63  |   Q      |          |          |       V  |
17+50       6.3469      1.53  |   Q      |          |          |       V  |
17+55       6.3563      1.38  | Q        |          |          |       V  |
18+ 0       6.3655      1.34  | Q        |          |          |       V  |
18+ 5       6.3746      1.32  | Q        |          |          |       V  |
18+10       6.3836      1.31  | Q        |          |          |       V  |
18+15       6.3926      1.30  | Q        |          |          |       V  |
18+20       6.4016      1.30  | Q        |          |          |       V  |
18+25       6.4105      1.30  | Q        |          |          |       V  |
18+30       6.4195      1.30  | Q        |          |          |       V  |
18+35       6.4278      1.21  | Q        |          |          |       V  |
18+40       6.4351      1.05  | Q        |          |          |       V  |
18+45       6.4420      1.01  | Q        |          |          |       V  |
18+50       6.4482      0.90  |Q         |          |          |       V  |
18+55       6.4532      0.73  |Q         |          |          |       V  |
19+ 0       6.4580      0.69  |Q         |          |          |       V  |
19+ 5       6.4632      0.76  |Q         |          |          |        V |
19+10       6.4695      0.91  |Q         |          |          |        V |
19+15       6.4760      0.94  |Q         |          |          |        V |
19+20       6.4832      1.06  | Q        |          |          |        V |
19+25       6.4917      1.22  | Q        |          |          |        V |
19+30       6.5004      1.27  | Q        |          |          |        V |
19+35       6.5086      1.19  | Q        |          |          |        V |
19+40       6.5158      1.04  | Q        |          |          |        V |
19+45       6.5227      1.01  | Q        |          |          |        V |
19+50       6.5289      0.90  |Q         |          |          |        V |
19+55       6.5340      0.73  |Q         |          |          |        V |
20+ 0       6.5387      0.69  |Q         |          |          |        V |
20+ 5       6.5439      0.76  |Q         |          |          |        V |
20+10       6.5502      0.91  |Q         |          |          |        V |
20+15       6.5567      0.94  |Q         |          |          |        V |
20+20       6.5633      0.96  |Q         |          |          |        V |
20+25       6.5700      0.97  |Q         |          |          |        V |
20+30       6.5767      0.98  |Q         |          |          |        V |
20+35       6.5834      0.98  |Q         |          |          |        V |
20+40       6.5902      0.98  |Q         |          |          |        V |
20+45       6.5969      0.98  |Q         |          |          |        V |
20+50       6.6029      0.88  |Q         |          |          |        V |
20+55       6.6079      0.72  |Q         |          |          |        V |
21+ 0       6.6127      0.69  |Q         |          |          |        V |
21+ 5       6.6179      0.76  |Q         |          |          |        V |
21+10       6.6242      0.91  |Q         |          |          |        V |
21+15       6.6307      0.94  |Q         |          |          |         V|
21+20       6.6366      0.86  |Q         |          |          |         V|
21+25       6.6416      0.72  |Q         |          |          |         V|
21+30       6.6463      0.69  |Q         |          |          |         V|
21+35       6.6515      0.76  |Q         |          |          |         V|
21+40       6.6578      0.91  |Q         |          |          |         V|
21+45       6.6643      0.94  |Q         |          |          |         V|
21+50       6.6703      0.86  |Q         |          |          |         V|
21+55       6.6752      0.72  |Q         |          |          |         V|
22+ 0       6.6799      0.69  |Q         |          |          |         V|
22+ 5       6.6852      0.76  |Q         |          |          |         V|
22+10       6.6914      0.91  |Q         |          |          |         V|
22+15       6.6979      0.94  |Q         |          |          |         V|
22+20       6.7039      0.86  |Q         |          |          |         V|
22+25       6.7088      0.72  |Q         |          |          |         V|
22+30       6.7135      0.69  |Q         |          |          |         V|
22+35       6.7181      0.67  |Q         |          |          |         V|
22+40       6.7227      0.66  |Q         |          |          |         V|
22+45       6.7272      0.65  |Q         |          |          |         V|
22+50       6.7316      0.65  |Q         |          |          |         V|
22+55       6.7361      0.65  |Q         |          |          |         V|
23+ 0       6.7406      0.65  |Q         |          |          |         V|
23+ 5       6.7451      0.65  |Q         |          |          |         V|
```

```
   23+10       6.7496      0.65  |Q        |         |         |        v|
   23+15       6.7541      0.65  |Q        |         |         |        v|
   23+20       6.7585      0.65  |Q        |         |         |        v|
   23+25       6.7630      0.65  |Q        |         |         |        v|
   23+30       6.7675      0.65  |Q        |         |         |        v|
   23+35       6.7720      0.65  |Q        |         |         |        v|
   23+40       6.7765      0.65  |Q        |         |         |        v|
   23+45       6.7810      0.65  |Q        |         |         |        v|
   23+50       6.7855      0.65  |Q        |         |         |        v|
   23+55       6.7899      0.65  |Q        |         |         |        v|
   24+ 0       6.7944      0.65  |Q        |         |         |        v|
   24+ 5       6.7976      0.46  Q         |         |         |        v|
   24+10       6.7986      0.15  Q         |         |         |        v|
   24+15       6.7991      0.07  Q         |         |         |        v|
   24+20       6.7993      0.03  Q         |         |         |        v|
   24+25       6.7994      0.01  Q         |         |         |         v
-------------------------------------------------------------------------
```

```
       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/18/24 File: pro21001100.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =      51.80(Ac.)  =      0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =      51.80(Ac.)  =      0.081 Sq. Mi.
Length along longest watercourse =    2976.00(Ft.)
Length along longest watercourse measured to centroid =    1488.00(Ft.)
Length along longest watercourse =      0.564 Mi.
Length along longest watercourse measured to centroid =      0.282 Mi.
Difference in elevation =     150.00(Ft.)
Slope along watercourse =    266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.062 Hr.
Lag time =     3.72 Min.
25% of lag time =     0.93 Min.
40% of lag time =     1.49 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           0.50                 25.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
       51.80           1.30                 67.34

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    1.300(In)
Areal adjustment factor =   99.95 %
Adjusted average point rain =    1.299(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
    51.800           69.00         0.500
 Total Area Entered =     51.80(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  69.0      0.373     0.500        0.205       1.000      0.205
                                                 Sum (F) =   0.205
Area averaged mean soil loss (F) (In/Hr) =  0.205
Minimum soil loss rate ((In/Hr)) =  0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
		Sum = 100.000	Sum=	52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.515	0.205	(0.257)	0.310
2	0.17	4.20	0.655	0.205	(0.327)	0.450
3	0.25	4.40	0.686	0.205	(0.343)	0.481
4	0.33	4.80	0.748	0.205	(0.374)	0.543
5	0.42	5.20	0.811	0.205	(0.405)	0.606
6	0.50	6.20	0.967	0.205	(0.483)	0.762
7	0.58	6.80	1.060	0.205	(0.530)	0.855
8	0.67	8.80	1.372	0.205	(0.686)	1.167
9	0.75	13.90	2.167	0.205	(1.084)	1.962
10	0.83	31.40	4.896	0.205	(2.448)	4.691
11	0.92	7.20	1.123	0.205	(0.561)	0.918
12	1.00	3.80	0.593	0.205	(0.296)	0.387
		(Loss Rate Not Used)			
Sum =		100.0			Sum = 13.1

Flood volume = Effective rainfall 1.09(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 4.7(Ac.Ft)
Total soil loss = 0.21(In)
Total soil loss = 0.885(Ac.Ft)
Total rainfall = 1.30(In)
Flood volume = 205775.0 Cubic Feet
Total soil loss = 38554.5 Cubic Feet

Peak flow rate of this hydrograph = 149.688(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	50.0	100.0	150.0	200.0
0+ 5	0.0326	4.73	Q				
0+10	0.1334	14.64	VQ				
0+15	0.2753	20.61	V Q				
0+20	0.4413	24.11	VQ				
0+25	0.6321	27.69	Q				
0+30	0.8572	32.70	QV				
0+35	1.1246	38.82	Q V				
0+40	1.4499	47.23	Q V				
0+45	1.9210	68.41	Q V				
0+50	2.8343	132.61	V Q				
0+55	3.8652	149.69	Q V				
1+ 0	4.3272	67.08	Q			V	
1+ 5	4.5555	33.14	Q			V	
1+10	4.6554	14.50	Q			V	
1+15	4.7096	7.87	Q			V	
1+20	4.7209	1.64	Q			V	
1+25	4.7239	0.44	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: pro21003100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2976.00(Ft.)
Length along longest watercourse measured to centroid = 1488.00(Ft.)
Length along longest watercourse = 0.564 Mi.
Length along longest watercourse measured to centroid = 0.282 Mi.
Difference in elevation = 150.00(Ft.)
Slope along watercourse = 266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.062 Hr.
Lag time = 3.72 Min.
25% of lag time = 0.93 Min.
40% of lag time = 1.49 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	0.80	41.44

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	2.00	103.60

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 2.000(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 2.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	69.00	0.500

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
		Sum = 100.000	Sum=	52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.312	(0.205)	0.156	0.156
2	0.17	1.30	0.312	(0.205)	0.156	0.156
3	0.25	1.10	0.264	(0.205)	0.132	0.132
4	0.33	1.50	0.360	(0.205)	0.180	0.180
5	0.42	1.50	0.360	(0.205)	0.180	0.180
6	0.50	1.80	0.432	0.205	(0.216)	0.227
7	0.58	1.50	0.360	(0.205)	0.180	0.180
8	0.67	1.80	0.432	0.205	(0.216)	0.227
9	0.75	1.80	0.432	0.205	(0.216)	0.227
10	0.83	1.50	0.360	(0.205)	0.180	0.180
11	0.92	1.60	0.384	(0.205)	0.192	0.192
12	1.00	1.80	0.432	0.205	(0.216)	0.227
13	1.08	2.20	0.528	0.205	(0.264)	0.323
14	1.17	2.20	0.528	0.205	(0.264)	0.323
15	1.25	2.20	0.528	0.205	(0.264)	0.323
16	1.33	2.00	0.480	0.205	(0.240)	0.275
17	1.42	2.60	0.624	0.205	(0.312)	0.419
18	1.50	2.70	0.648	0.205	(0.324)	0.443
19	1.58	2.40	0.576	0.205	(0.288)	0.371
20	1.67	2.70	0.648	0.205	(0.324)	0.443
21	1.75	3.30	0.792	0.205	(0.396)	0.587
22	1.83	3.10	0.744	0.205	(0.372)	0.539
23	1.92	2.90	0.696	0.205	(0.348)	0.491
24	2.00	3.00	0.720	0.205	(0.360)	0.515
25	2.08	3.10	0.744	0.205	(0.372)	0.539
26	2.17	4.20	1.008	0.205	(0.504)	0.803
27	2.25	5.00	1.200	0.205	(0.600)	0.995
28	2.33	3.50	0.840	0.205	(0.420)	0.635
29	2.42	6.80	1.632	0.205	(0.816)	1.427
30	2.50	7.30	1.752	0.205	(0.876)	1.547
31	2.58	8.20	1.968	0.205	(0.984)	1.763
32	2.67	5.90	1.416	0.205	(0.708)	1.211
33	2.75	2.00	0.480	0.205	(0.240)	0.275
34	2.83	1.80	0.432	0.205	(0.216)	0.227
35	2.92	1.80	0.432	0.205	(0.216)	0.227
36	3.00	0.60	0.144	(0.205)	0.072	0.072
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	17.0

Flood volume = Effective rainfall 1.42(In)
times area 51.8(Ac.)/[(In)/(Ft.)] = 6.1(Ac.Ft)
Total soil loss = 0.58(In)
Total soil loss = 2.505(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 266864.2 Cubic Feet
Total soil loss = 109118.6 Cubic Feet

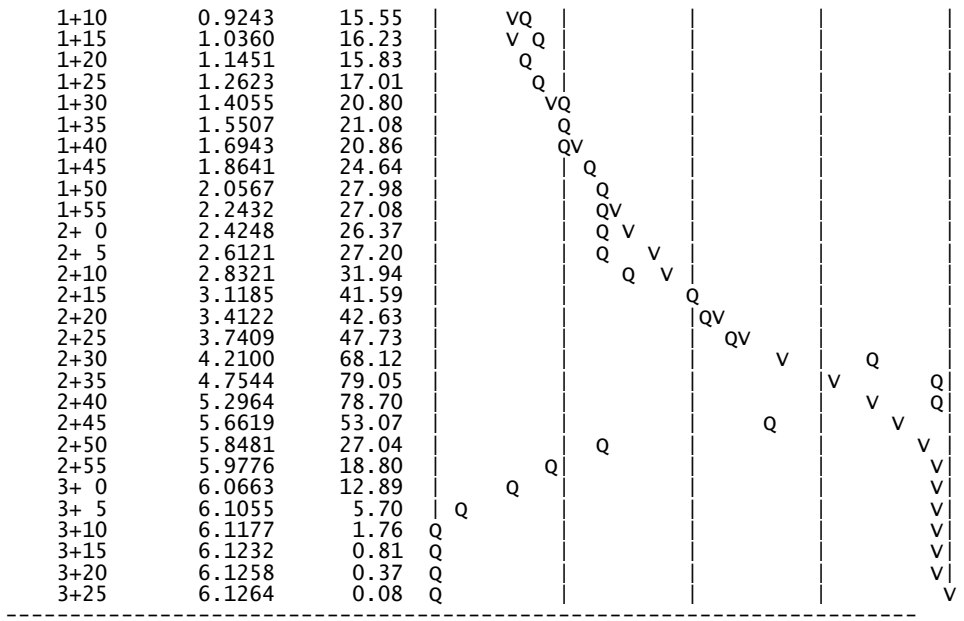
Peak flow rate of this hydrograph = 79.045(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	20.0	40.0	60.0	80.0
0+ 5	0.0164	2.38	VQ				
0+10	0.0598	6.30	V Q				
0+15	0.1074	6.92	V Q				
0+20	0.1590	7.49	V Q				
0+25	0.2195	8.78	V Q				
0+30	0.2878	9.92	V Q				
0+35	0.3600	10.48	V Q				
0+40	0.4313	10.36	V Q				
0+45	0.5100	11.43	V Q				
0+50	0.5854	10.95	V Q				
0+55	0.6547	10.07	VQ				
1+ 0	0.7279	10.62	VQ				
1+ 5	0.8172	12.96	VQ				



1+10	0.9243	15.55	VQ
1+15	1.0360	16.23	V Q
1+20	1.1451	15.83	Q
1+25	1.2623	17.01	Q
1+30	1.4055	20.80	VQ
1+35	1.5507	21.08	Q
1+40	1.6943	20.86	QV
1+45	1.8641	24.64	Q
1+50	2.0567	27.98	Q
1+55	2.2432	27.08	QV
2+ 0	2.4248	26.37	Q V
2+ 5	2.6121	27.20	Q V
2+10	2.8321	31.94	Q V
2+15	3.1185	41.59	Q
2+20	3.4122	42.63	QV
2+25	3.7409	47.73	QV
2+30	4.2100	68.12	V Q
2+35	4.7544	79.05	V Q
2+40	5.2964	78.70	V Q
2+45	5.6619	53.07	Q V
2+50	5.8481	27.04	Q V
2+55	5.9776	18.80	Q V
3+ 0	6.0663	12.89	Q V
3+ 5	6.1055	5.70	Q V
3+10	6.1177	1.76	Q V
3+15	6.1232	0.81	Q V
3+20	6.1258	0.37	Q V
3+25	6.1264	0.08	Q V

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: pro21006100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2976.00(Ft.)
Length along longest watercourse measured to centroid = 1488.00(Ft.)
Length along longest watercourse = 0.564 Mi.
Length along longest watercourse measured to centroid = 0.282 Mi.
Difference in elevation = 150.00(Ft.)
Slope along watercourse = 266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.062 Hr.
Lag time = 3.72 Min.
25% of lag time = 0.93 Min.
40% of lag time = 1.49 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	1.10	56.98

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	3.00	155.40

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 3.000(In)
Areal adjustment factor = 99.98 %
Adjusted average point rain = 2.999(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	69.00	0.500

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.180	(0.205)	0.090	0.090
2	0.17	0.60	0.216	(0.205)	0.108	0.108
3	0.25	0.60	0.216	(0.205)	0.108	0.108
4	0.33	0.60	0.216	(0.205)	0.108	0.108
5	0.42	0.60	0.216	(0.205)	0.108	0.108
6	0.50	0.70	0.252	(0.205)	0.126	0.126
7	0.58	0.70	0.252	(0.205)	0.126	0.126
8	0.67	0.70	0.252	(0.205)	0.126	0.126
9	0.75	0.70	0.252	(0.205)	0.126	0.126
10	0.83	0.70	0.252	(0.205)	0.126	0.126
11	0.92	0.70	0.252	(0.205)	0.126	0.126
12	1.00	0.80	0.288	(0.205)	0.144	0.144
13	1.08	0.80	0.288	(0.205)	0.144	0.144
14	1.17	0.80	0.288	(0.205)	0.144	0.144
15	1.25	0.80	0.288	(0.205)	0.144	0.144
16	1.33	0.80	0.288	(0.205)	0.144	0.144
17	1.42	0.80	0.288	(0.205)	0.144	0.144
18	1.50	0.80	0.288	(0.205)	0.144	0.144
19	1.58	0.80	0.288	(0.205)	0.144	0.144
20	1.67	0.80	0.288	(0.205)	0.144	0.144
21	1.75	0.80	0.288	(0.205)	0.144	0.144
22	1.83	0.80	0.288	(0.205)	0.144	0.144
23	1.92	0.80	0.288	(0.205)	0.144	0.144
24	2.00	0.90	0.324	(0.205)	0.162	0.162
25	2.08	0.80	0.288	(0.205)	0.144	0.144
26	2.17	0.90	0.324	(0.205)	0.162	0.162
27	2.25	0.90	0.324	(0.205)	0.162	0.162
28	2.33	0.90	0.324	(0.205)	0.162	0.162
29	2.42	0.90	0.324	(0.205)	0.162	0.162
30	2.50	0.90	0.324	(0.205)	0.162	0.162
31	2.58	0.90	0.324	(0.205)	0.162	0.162
32	2.67	0.90	0.324	(0.205)	0.162	0.162
33	2.75	1.00	0.360	(0.205)	0.180	0.180
34	2.83	1.00	0.360	(0.205)	0.180	0.180
35	2.92	1.00	0.360	(0.205)	0.180	0.180
36	3.00	1.00	0.360	(0.205)	0.180	0.180
37	3.08	1.00	0.360	(0.205)	0.180	0.180
38	3.17	1.10	0.396	(0.205)	0.198	0.198
39	3.25	1.10	0.396	(0.205)	0.198	0.198
40	3.33	1.10	0.396	(0.205)	0.198	0.198
41	3.42	1.20	0.432	0.205	(0.216)	0.227
42	3.50	1.30	0.468	0.205	(0.234)	0.263
43	3.58	1.40	0.504	0.205	(0.252)	0.299
44	3.67	1.40	0.504	0.205	(0.252)	0.299
45	3.75	1.50	0.540	0.205	(0.270)	0.335
46	3.83	1.50	0.540	0.205	(0.270)	0.335
47	3.92	1.60	0.576	0.205	(0.288)	0.371
48	4.00	1.60	0.576	0.205	(0.288)	0.371
49	4.08	1.70	0.612	0.205	(0.306)	0.407
50	4.17	1.80	0.648	0.205	(0.324)	0.443
51	4.25	1.90	0.684	0.205	(0.342)	0.479
52	4.33	2.00	0.720	0.205	(0.360)	0.515
53	4.42	2.10	0.756	0.205	(0.378)	0.551
54	4.50	2.10	0.756	0.205	(0.378)	0.551
55	4.58	2.20	0.792	0.205	(0.396)	0.587
56	4.67	2.30	0.828	0.205	(0.414)	0.623
57	4.75	2.40	0.864	0.205	(0.432)	0.659
58	4.83	2.40	0.864	0.205	(0.432)	0.659
59	4.92	2.50	0.900	0.205	(0.450)	0.695
60	5.00	2.60	0.936	0.205	(0.468)	0.731
61	5.08	3.10	1.116	0.205	(0.558)	0.911
62	5.17	3.60	1.296	0.205	(0.648)	1.091
63	5.25	3.90	1.404	0.205	(0.702)	1.199
64	5.33	4.20	1.512	0.205	(0.756)	1.307
65	5.42	4.70	1.692	0.205	(0.846)	1.487
66	5.50	5.60	2.016	0.205	(1.008)	1.811
67	5.58	1.90	0.684	0.205	(0.342)	0.479
68	5.67	0.90	0.324	(0.205)	0.162	0.162
69	5.75	0.60	0.216	(0.205)	0.108	0.108
70	5.83	0.50	0.180	(0.205)	0.090	0.090

```
71   5.92     0.30      0.108       (  0.205)       0.054        0.054
72   6.00     0.20      0.072       (  0.205)       0.036        0.036
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =    24.1
     Flood volume = Effective rainfall      2.01(In)
      times area      51.8(Ac.)/[(In)/(Ft.)] =       8.7(Ac.Ft)
     Total soil loss =      0.99(In)
     Total soil loss =     4.290(Ac.Ft)
     Total rainfall =      3.00(In)
     Flood volume =      377143.7 Cubic Feet
     Total soil loss =      186857.9 Cubic Feet
     ---------------------------------------------------------------------
      Peak flow rate of this hydrograph =     79.376(CFS)
     ---------------------------------------------------------------------
     +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                    R u n o f f      H y d r o g r a p h
     ---------------------------------------------------------------------
                Hydrograph in   5   Minute intervals ((CFS))

     ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0       20.0      40.0      60.0      80.0
-------------------------------------------------------------------------
  0+ 5       0.0095      1.37  Q         |         |         |         |
  0+10       0.0364      3.91  VQ        |         |         |         |
  0+15       0.0703      4.93  V Q       |         |         |         |
  0+20       0.1068      5.30  V Q       |         |         |         |
  0+25       0.1446      5.49  V Q       |         |         |         |
  0+30       0.1852      5.89  V Q       |         |         |         |
  0+35       0.2291      6.37  |V Q       |         |         |         |
  0+40       0.2737      6.48  |V Q       |         |         |         |
  0+45       0.3187      6.53  |V Q       |         |         |         |
  0+50       0.3639      6.56  |V Q       |         |         |         |
  0+55       0.4092      6.58  |V Q       |         |         |         |
  1+ 0       0.4564      6.85  | VQ       |         |         |         |
  1+ 5       0.5067      7.31  | VQ       |         |         |         |
  1+10       0.5578      7.42  | VQ       |         |         |         |
  1+15       0.6093      7.47  | VQ       |         |         |         |
  1+20       0.6609      7.50  |  Q       |         |         |         |
  1+25       0.7127      7.52  |  Q       |         |         |         |
  1+30       0.7645      7.52  |  Q       |         |         |         |
  1+35       0.8163      7.52  |  Q       |         |         |         |
  1+40       0.8681      7.52  |  QV      |         |         |         |
  1+45       0.9199      7.52  |  QV      |         |         |         |
  1+50       0.9717      7.52  |  QV      |         |         |         |
  1+55       1.0235      7.52  |  QV      |         |         |         |
  2+ 0       1.0772      7.79  |  QV      |         |         |         |
  2+ 5       1.1321      7.97  |  Q V     |         |         |         |
  2+10       1.1865      7.91  |  Q V     |         |         |         |
  2+15       1.2437      8.30  |   QV     |         |         |         |
  2+20       1.3015      8.39  |   Q V    |         |         |         |
  2+25       1.3595      8.43  |   Q V    |         |         |         |
  2+30       1.4177      8.44  |   Q V    |         |         |         |
  2+35       1.4759      8.46  |   Q V    |         |         |         |
  2+40       1.5342      8.46  |   Q  V   |         |         |         |
  2+45       1.5943      8.73  |   Q  V   |         |         |         |
  2+50       1.6576      9.19  |   Q  V   |         |         |         |
  2+55       1.7217      9.30  |   Q  V   |         |         |         |
  3+ 0       1.7861      9.35  |   Q   V  |         |         |         |
  3+ 5       1.8507      9.38  |   Q   V  |         |         |         |
  3+10       1.9173      9.67  |   Q   V  |         |         |         |
  3+15       1.9870     10.13  |    Q   V|         |         |         |
  3+20       2.0576     10.24  |    Q   V|         |         |         |
  3+25       2.1315     10.73  |    Q   V|         |         |         |
  3+30       2.2144     12.04  |     Q   V         |         |         |
  3+35       2.3087     13.69  |     Q   V         |         |         |
  3+40       2.4114     14.91  |      Q  |V        |         |         |
  3+45       2.5204     15.83  |      Q  |V        |         |         |
  3+50       2.6370     16.93  |       Q | V       |         |         |
  3+55       2.7596     17.80  |       Q | V       |         |         |
  4+ 0       2.8894     18.85  |        Q|  V      |         |         |
  4+ 5       3.0249     19.68  |        Q|  V      |         |         |
  4+10       3.1715     21.28  |         Q   V     |         |         |
  4+15       3.3300     23.01  |         |Q   V    |         |         |
  4+20       3.5011     24.84  |         | Q   V   |         |         |
  4+25       3.6848     26.68  |         |  Q   V  |         |         |
  4+30       3.8777     28.01  |         |   Q  V  |         |         |
  4+35       4.0773     28.98  |         |   Q   V |         |         |
  4+40       4.2883     30.64  |         |    Q   V|         |         |
  4+45       4.5115     32.41  |         |     Q   V         |         |
  4+50       4.7435     33.69  |         |     Q   |V        |         |
  4+55       4.9820     34.62  |         |      Q  |  V      |         |
  5+ 0       5.2318     36.28  |         |       Q |   V     |         |
  5+ 5       5.5091     40.25  |         |         Q    V    |         |
  5+10       5.8389     47.89  |         |         |  Q  V   |         |
  5+15       6.2202     55.36  |         |         |     QV  |         |
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    5+20       6.6435     61.47  |          |          |          Q          |
    5+25       7.1148     68.44  |          |          |          | V Q      |
    5+30       7.6615     79.38  |          |          |          |    V    Q|
    5+35       8.1365     68.98  |          |          |          |   Q  V   |
    5+40       8.3678     33.58  |          |     Q    |          |      V   |
    5+45       8.4893     17.65  |          Q          |          |          V|
    5+50       8.5647     10.95  |       Q             |          |          V|
    5+55       8.6131      7.03  |    Q                |          |          V|
    6+ 0       8.6378      3.58  |Q                    |          |          V|
    6+ 5       8.6505      1.85  Q                     |          |          V|
    6+10       8.6550      0.64  Q                     |          |          V|
    6+15       8.6569      0.29  Q                     |          |          V|
    6+20       8.6577      0.12  Q                     |          |          V|
    6+25       8.6580      0.04  Q                     |          |           V
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/18/24 File: pro210024100.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 51.80(Ac.) = 0.081 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 51.80(Ac.) = 0.081 Sq. Mi.
Length along longest watercourse = 2976.00(Ft.)
Length along longest watercourse measured to centroid = 1488.00(Ft.)
Length along longest watercourse = 0.564 Mi.
Length along longest watercourse measured to centroid = 0.282 Mi.
Difference in elevation = 150.00(Ft.)
Slope along watercourse = 266.1290 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.062 Hr.
Lag time = 3.72 Min.
25% of lag time = 0.93 Min.
40% of lag time = 1.49 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	1.80	93.24

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
51.80	5.00	259.00

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 5.000(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 4.999(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
51.800	69.00	0.500

Total Area Entered = 51.80(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	134.560	29.252	15.271
2	0.167	269.120	48.041	25.080
3	0.250	403.680	12.175	6.356
4	0.333	538.240	5.402	2.820
5	0.417	672.800	2.941	1.536
6	0.500	807.360	2.189	1.143
			Sum = 100.000	Sum= 52.205

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.040	(0.363)	0.020	0.020
2	0.17	0.07	0.040	(0.362)	0.020	0.020
3	0.25	0.07	0.040	(0.361)	0.020	0.020
4	0.33	0.10	0.060	(0.359)	0.030	0.030
5	0.42	0.10	0.060	(0.358)	0.030	0.030
6	0.50	0.10	0.060	(0.356)	0.030	0.030
7	0.58	0.10	0.060	(0.355)	0.030	0.030
8	0.67	0.10	0.060	(0.354)	0.030	0.030
9	0.75	0.10	0.060	(0.352)	0.030	0.030
10	0.83	0.13	0.080	(0.351)	0.040	0.040
11	0.92	0.13	0.080	(0.350)	0.040	0.040
12	1.00	0.13	0.080	(0.348)	0.040	0.040
13	1.08	0.10	0.060	(0.347)	0.030	0.030
14	1.17	0.10	0.060	(0.345)	0.030	0.030
15	1.25	0.10	0.060	(0.344)	0.030	0.030
16	1.33	0.10	0.060	(0.343)	0.030	0.030
17	1.42	0.10	0.060	(0.341)	0.030	0.030
18	1.50	0.10	0.060	(0.340)	0.030	0.030
19	1.58	0.10	0.060	(0.339)	0.030	0.030
20	1.67	0.10	0.060	(0.337)	0.030	0.030
21	1.75	0.10	0.060	(0.336)	0.030	0.030
22	1.83	0.13	0.080	(0.335)	0.040	0.040
23	1.92	0.13	0.080	(0.333)	0.040	0.040
24	2.00	0.13	0.080	(0.332)	0.040	0.040
25	2.08	0.13	0.080	(0.330)	0.040	0.040
26	2.17	0.13	0.080	(0.329)	0.040	0.040
27	2.25	0.13	0.080	(0.328)	0.040	0.040
28	2.33	0.13	0.080	(0.326)	0.040	0.040
29	2.42	0.13	0.080	(0.325)	0.040	0.040
30	2.50	0.13	0.080	(0.324)	0.040	0.040
31	2.58	0.17	0.100	(0.323)	0.050	0.050
32	2.67	0.17	0.100	(0.321)	0.050	0.050
33	2.75	0.17	0.100	(0.320)	0.050	0.050
34	2.83	0.17	0.100	(0.319)	0.050	0.050
35	2.92	0.17	0.100	(0.317)	0.050	0.050
36	3.00	0.17	0.100	(0.316)	0.050	0.050
37	3.08	0.17	0.100	(0.315)	0.050	0.050
38	3.17	0.17	0.100	(0.313)	0.050	0.050
39	3.25	0.17	0.100	(0.312)	0.050	0.050
40	3.33	0.17	0.100	(0.311)	0.050	0.050
41	3.42	0.17	0.100	(0.309)	0.050	0.050
42	3.50	0.17	0.100	(0.308)	0.050	0.050
43	3.58	0.17	0.100	(0.307)	0.050	0.050
44	3.67	0.17	0.100	(0.306)	0.050	0.050
45	3.75	0.17	0.100	(0.304)	0.050	0.050
46	3.83	0.20	0.120	(0.303)	0.060	0.060
47	3.92	0.20	0.120	(0.302)	0.060	0.060
48	4.00	0.20	0.120	(0.300)	0.060	0.060
49	4.08	0.20	0.120	(0.299)	0.060	0.060
50	4.17	0.20	0.120	(0.298)	0.060	0.060
51	4.25	0.20	0.120	(0.297)	0.060	0.060
52	4.33	0.23	0.140	(0.295)	0.070	0.070
53	4.42	0.23	0.140	(0.294)	0.070	0.070
54	4.50	0.23	0.140	(0.293)	0.070	0.070
55	4.58	0.23	0.140	(0.292)	0.070	0.070
56	4.67	0.23	0.140	(0.290)	0.070	0.070
57	4.75	0.23	0.140	(0.289)	0.070	0.070
58	4.83	0.27	0.160	(0.288)	0.080	0.080
59	4.92	0.27	0.160	(0.287)	0.080	0.080
60	5.00	0.27	0.160	(0.285)	0.080	0.080
61	5.08	0.20	0.120	(0.284)	0.060	0.060
62	5.17	0.20	0.120	(0.283)	0.060	0.060
63	5.25	0.20	0.120	(0.282)	0.060	0.060
64	5.33	0.23	0.140	(0.280)	0.070	0.070
65	5.42	0.23	0.140	(0.279)	0.070	0.070
66	5.50	0.23	0.140	(0.278)	0.070	0.070
67	5.58	0.27	0.160	(0.277)	0.080	0.080
68	5.67	0.27	0.160	(0.275)	0.080	0.080
69	5.75	0.27	0.160	(0.274)	0.080	0.080
70	5.83	0.27	0.160	(0.273)	0.080	0.080

71	5.92	0.27	0.160	(0.272)	0.080	0.080
72	6.00	0.27	0.160	(0.271)	0.080	0.080
73	6.08	0.30	0.180	(0.269)	0.090	0.090
74	6.17	0.30	0.180	(0.268)	0.090	0.090
75	6.25	0.30	0.180	(0.267)	0.090	0.090
76	6.33	0.30	0.180	(0.266)	0.090	0.090
77	6.42	0.30	0.180	(0.265)	0.090	0.090
78	6.50	0.30	0.180	(0.263)	0.090	0.090
79	6.58	0.33	0.200	(0.262)	0.100	0.100
80	6.67	0.33	0.200	(0.261)	0.100	0.100
81	6.75	0.33	0.200	(0.260)	0.100	0.100
82	6.83	0.33	0.200	(0.259)	0.100	0.100
83	6.92	0.33	0.200	(0.258)	0.100	0.100
84	7.00	0.33	0.200	(0.256)	0.100	0.100
85	7.08	0.33	0.200	(0.255)	0.100	0.100
86	7.17	0.33	0.200	(0.254)	0.100	0.100
87	7.25	0.33	0.200	(0.253)	0.100	0.100
88	7.33	0.37	0.220	(0.252)	0.110	0.110
89	7.42	0.37	0.220	(0.251)	0.110	0.110
90	7.50	0.37	0.220	(0.249)	0.110	0.110
91	7.58	0.40	0.240	(0.248)	0.120	0.120
92	7.67	0.40	0.240	(0.247)	0.120	0.120
93	7.75	0.40	0.240	(0.246)	0.120	0.120
94	7.83	0.43	0.260	(0.245)	0.130	0.130
95	7.92	0.43	0.260	(0.244)	0.130	0.130
96	8.00	0.43	0.260	(0.243)	0.130	0.130
97	8.08	0.50	0.300	(0.242)	0.150	0.150
98	8.17	0.50	0.300	(0.240)	0.150	0.150
99	8.25	0.50	0.300	(0.239)	0.150	0.150
100	8.33	0.50	0.300	(0.238)	0.150	0.150
101	8.42	0.50	0.300	(0.237)	0.150	0.150
102	8.50	0.50	0.300	(0.236)	0.150	0.150
103	8.58	0.53	0.320	(0.235)	0.160	0.160
104	8.67	0.53	0.320	(0.234)	0.160	0.160
105	8.75	0.53	0.320	(0.233)	0.160	0.160
106	8.83	0.57	0.340	(0.232)	0.170	0.170
107	8.92	0.57	0.340	(0.230)	0.170	0.170
108	9.00	0.57	0.340	(0.229)	0.170	0.170
109	9.08	0.63	0.380	(0.228)	0.190	0.190
110	9.17	0.63	0.380	(0.227)	0.190	0.190
111	9.25	0.63	0.380	(0.226)	0.190	0.190
112	9.33	0.67	0.400	(0.225)	0.200	0.200
113	9.42	0.67	0.400	(0.224)	0.200	0.200
114	9.50	0.67	0.400	(0.223)	0.200	0.200
115	9.58	0.70	0.420	(0.222)	0.210	0.210
116	9.67	0.70	0.420	(0.221)	0.210	0.210
117	9.75	0.70	0.420	(0.220)	0.210	0.210
118	9.83	0.73	0.440	0.219	(0.220)	0.221
119	9.92	0.73	0.440	0.218	(0.220)	0.222
120	10.00	0.73	0.440	0.217	(0.220)	0.223
121	10.08	0.50	0.300	(0.215)	0.150	0.150
122	10.17	0.50	0.300	(0.214)	0.150	0.150
123	10.25	0.50	0.300	(0.213)	0.150	0.150
124	10.33	0.50	0.300	(0.212)	0.150	0.150
125	10.42	0.50	0.300	(0.211)	0.150	0.150
126	10.50	0.50	0.300	(0.210)	0.150	0.150
127	10.58	0.67	0.400	(0.209)	0.200	0.200
128	10.67	0.67	0.400	(0.208)	0.200	0.200
129	10.75	0.67	0.400	(0.207)	0.200	0.200
130	10.83	0.67	0.400	(0.206)	0.200	0.200
131	10.92	0.67	0.400	(0.205)	0.200	0.200
132	11.00	0.67	0.400	(0.204)	0.200	0.200
133	11.08	0.63	0.380	(0.203)	0.190	0.190
134	11.17	0.63	0.380	(0.202)	0.190	0.190
135	11.25	0.63	0.380	(0.201)	0.190	0.190
136	11.33	0.63	0.380	(0.200)	0.190	0.190
137	11.42	0.63	0.380	(0.199)	0.190	0.190
138	11.50	0.63	0.380	(0.198)	0.190	0.190
139	11.58	0.57	0.340	(0.197)	0.170	0.170
140	11.67	0.57	0.340	(0.196)	0.170	0.170
141	11.75	0.57	0.340	(0.195)	0.170	0.170
142	11.83	0.60	0.360	(0.194)	0.180	0.180
143	11.92	0.60	0.360	(0.193)	0.180	0.180
144	12.00	0.60	0.360	(0.192)	0.180	0.180
145	12.08	0.83	0.500	0.191	(0.250)	0.309
146	12.17	0.83	0.500	0.190	(0.250)	0.310
147	12.25	0.83	0.500	0.189	(0.250)	0.310
148	12.33	0.87	0.520	0.189	(0.260)	0.331
149	12.42	0.87	0.520	0.188	(0.260)	0.332
150	12.50	0.87	0.520	0.187	(0.260)	0.333
151	12.58	0.93	0.560	0.186	(0.280)	0.374
152	12.67	0.93	0.560	0.185	(0.280)	0.375
153	12.75	0.93	0.560	0.184	(0.280)	0.376
154	12.83	0.97	0.580	0.183	(0.290)	0.397
155	12.92	0.97	0.580	0.182	(0.290)	0.398
156	13.00	0.97	0.580	0.181	(0.290)	0.399

157	13.08	1.13	0.680	0.180	(0.340)	0.500
158	13.17	1.13	0.680	0.179	(0.340)	0.501
159	13.25	1.13	0.680	0.178	(0.340)	0.502
160	13.33	1.13	0.680	0.177	(0.340)	0.503
161	13.42	1.13	0.680	0.177	(0.340)	0.503
162	13.50	1.13	0.680	0.176	(0.340)	0.504
163	13.58	0.77	0.460	0.175	(0.230)	0.285
164	13.67	0.77	0.460	0.174	(0.230)	0.286
165	13.75	0.77	0.460	0.173	(0.230)	0.287
166	13.83	0.77	0.460	0.172	(0.230)	0.288
167	13.92	0.77	0.460	0.171	(0.230)	0.289
168	14.00	0.77	0.460	0.170	(0.230)	0.290
169	14.08	0.90	0.540	0.169	(0.270)	0.370
170	14.17	0.90	0.540	0.169	(0.270)	0.371
171	14.25	0.90	0.540	0.168	(0.270)	0.372
172	14.33	0.87	0.520	0.167	(0.260)	0.353
173	14.42	0.87	0.520	0.166	(0.260)	0.354
174	14.50	0.87	0.520	0.165	(0.260)	0.355
175	14.58	0.87	0.520	0.164	(0.260)	0.356
176	14.67	0.87	0.520	0.163	(0.260)	0.356
177	14.75	0.87	0.520	0.163	(0.260)	0.357
178	14.83	0.83	0.500	0.162	(0.250)	0.338
179	14.92	0.83	0.500	0.161	(0.250)	0.339
180	15.00	0.83	0.500	0.160	(0.250)	0.340
181	15.08	0.80	0.480	0.159	(0.240)	0.321
182	15.17	0.80	0.480	0.159	(0.240)	0.321
183	15.25	0.80	0.480	0.158	(0.240)	0.322
184	15.33	0.77	0.460	0.157	(0.230)	0.303
185	15.42	0.77	0.460	0.156	(0.230)	0.304
186	15.50	0.77	0.460	0.155	(0.230)	0.305
187	15.58	0.63	0.380	0.154	(0.190)	0.225
188	15.67	0.63	0.380	0.154	(0.190)	0.226
189	15.75	0.63	0.380	0.153	(0.190)	0.227
190	15.83	0.63	0.380	0.152	(0.190)	0.228
191	15.92	0.63	0.380	0.151	(0.190)	0.229
192	16.00	0.63	0.380	0.151	(0.190)	0.229
193	16.08	0.13	0.080	(0.150)	0.040	0.040
194	16.17	0.13	0.080	(0.149)	0.040	0.040
195	16.25	0.13	0.080	(0.148)	0.040	0.040
196	16.33	0.13	0.080	(0.148)	0.040	0.040
197	16.42	0.13	0.080	(0.147)	0.040	0.040
198	16.50	0.13	0.080	(0.146)	0.040	0.040
199	16.58	0.10	0.060	(0.145)	0.030	0.030
200	16.67	0.10	0.060	(0.145)	0.030	0.030
201	16.75	0.10	0.060	(0.144)	0.030	0.030
202	16.83	0.10	0.060	(0.143)	0.030	0.030
203	16.92	0.10	0.060	(0.142)	0.030	0.030
204	17.00	0.10	0.060	(0.142)	0.030	0.030
205	17.08	0.17	0.100	(0.141)	0.050	0.050
206	17.17	0.17	0.100	(0.140)	0.050	0.050
207	17.25	0.17	0.100	(0.140)	0.050	0.050
208	17.33	0.17	0.100	(0.139)	0.050	0.050
209	17.42	0.17	0.100	(0.138)	0.050	0.050
210	17.50	0.17	0.100	(0.137)	0.050	0.050
211	17.58	0.17	0.100	(0.137)	0.050	0.050
212	17.67	0.17	0.100	(0.136)	0.050	0.050
213	17.75	0.17	0.100	(0.135)	0.050	0.050
214	17.83	0.13	0.080	(0.135)	0.040	0.040
215	17.92	0.13	0.080	(0.134)	0.040	0.040
216	18.00	0.13	0.080	(0.133)	0.040	0.040
217	18.08	0.13	0.080	(0.133)	0.040	0.040
218	18.17	0.13	0.080	(0.132)	0.040	0.040
219	18.25	0.13	0.080	(0.131)	0.040	0.040
220	18.33	0.13	0.080	(0.131)	0.040	0.040
221	18.42	0.13	0.080	(0.130)	0.040	0.040
222	18.50	0.13	0.080	(0.130)	0.040	0.040
223	18.58	0.10	0.060	(0.129)	0.030	0.030
224	18.67	0.10	0.060	(0.128)	0.030	0.030
225	18.75	0.10	0.060	(0.128)	0.030	0.030
226	18.83	0.07	0.040	(0.127)	0.020	0.020
227	18.92	0.07	0.040	(0.126)	0.020	0.020
228	19.00	0.07	0.040	(0.126)	0.020	0.020
229	19.08	0.10	0.060	(0.125)	0.030	0.030
230	19.17	0.10	0.060	(0.125)	0.030	0.030
231	19.25	0.10	0.060	(0.124)	0.030	0.030
232	19.33	0.13	0.080	(0.123)	0.040	0.040
233	19.42	0.13	0.080	(0.123)	0.040	0.040
234	19.50	0.13	0.080	(0.122)	0.040	0.040
235	19.58	0.10	0.060	(0.122)	0.030	0.030
236	19.67	0.10	0.060	(0.121)	0.030	0.030
237	19.75	0.10	0.060	(0.121)	0.030	0.030
238	19.83	0.07	0.040	(0.120)	0.020	0.020
239	19.92	0.07	0.040	(0.120)	0.020	0.020
240	20.00	0.07	0.040	(0.119)	0.020	0.020
241	20.08	0.10	0.060	(0.119)	0.030	0.030
242	20.17	0.10	0.060	(0.118)	0.030	0.030

```
243  20.25     0.10      0.060       (  0.118)       0.030        0.030
244  20.33     0.10      0.060       (  0.117)       0.030        0.030
245  20.42     0.10      0.060       (  0.116)       0.030        0.030
246  20.50     0.10      0.060       (  0.116)       0.030        0.030
247  20.58     0.10      0.060       (  0.116)       0.030        0.030
248  20.67     0.10      0.060       (  0.115)       0.030        0.030
249  20.75     0.10      0.060       (  0.115)       0.030        0.030
250  20.83     0.07      0.040       (  0.114)       0.020        0.020
251  20.92     0.07      0.040       (  0.114)       0.020        0.020
252  21.00     0.07      0.040       (  0.113)       0.020        0.020
253  21.08     0.10      0.060       (  0.113)       0.030        0.030
254  21.17     0.10      0.060       (  0.112)       0.030        0.030
255  21.25     0.10      0.060       (  0.112)       0.030        0.030
256  21.33     0.07      0.040       (  0.111)       0.020        0.020
257  21.42     0.07      0.040       (  0.111)       0.020        0.020
258  21.50     0.07      0.040       (  0.111)       0.020        0.020
259  21.58     0.10      0.060       (  0.110)       0.030        0.030
260  21.67     0.10      0.060       (  0.110)       0.030        0.030
261  21.75     0.10      0.060       (  0.109)       0.030        0.030
262  21.83     0.07      0.040       (  0.109)       0.020        0.020
263  21.92     0.07      0.040       (  0.109)       0.020        0.020
264  22.00     0.07      0.040       (  0.108)       0.020        0.020
265  22.08     0.10      0.060       (  0.108)       0.030        0.030
266  22.17     0.10      0.060       (  0.108)       0.030        0.030
267  22.25     0.10      0.060       (  0.107)       0.030        0.030
268  22.33     0.07      0.040       (  0.107)       0.020        0.020
269  22.42     0.07      0.040       (  0.107)       0.020        0.020
270  22.50     0.07      0.040       (  0.106)       0.020        0.020
271  22.58     0.07      0.040       (  0.106)       0.020        0.020
272  22.67     0.07      0.040       (  0.106)       0.020        0.020
273  22.75     0.07      0.040       (  0.105)       0.020        0.020
274  22.83     0.07      0.040       (  0.105)       0.020        0.020
275  22.92     0.07      0.040       (  0.105)       0.020        0.020
276  23.00     0.07      0.040       (  0.105)       0.020        0.020
277  23.08     0.07      0.040       (  0.104)       0.020        0.020
278  23.17     0.07      0.040       (  0.104)       0.020        0.020
279  23.25     0.07      0.040       (  0.104)       0.020        0.020
280  23.33     0.07      0.040       (  0.104)       0.020        0.020
281  23.42     0.07      0.040       (  0.103)       0.020        0.020
282  23.50     0.07      0.040       (  0.103)       0.020        0.020
283  23.58     0.07      0.040       (  0.103)       0.020        0.020
284  23.67     0.07      0.040       (  0.103)       0.020        0.020
285  23.75     0.07      0.040       (  0.103)       0.020        0.020
286  23.83     0.07      0.040       (  0.103)       0.020        0.020
287  23.92     0.07      0.040       (  0.103)       0.020        0.020
288  24.00     0.07      0.040       (  0.103)       0.020        0.020
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    34.2
      Flood volume = Effective rainfall      2.85(In)
       times area      51.8(Ac.)/[(In)/(Ft.)] =      12.3(Ac.Ft)
      Total soil loss =      2.15(In)
      Total soil loss =     9.293(Ac.Ft)
      Total rainfall =      5.00(In)
      Flood volume =      535273.3 Cubic Feet
      Total soil loss =      404801.6 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     26.289(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        7.5      15.0      22.5      30.0
 ------------------------------------------------------------------------
   0+ 5       0.0021      0.31  Q          |          |          |          |
   0+10       0.0077      0.81  VQ         |          |          |          |
   0+15       0.0141      0.93  VQ         |          |          |          |
   0+20       0.0220      1.14  VQ         |          |          |          |
   0+25       0.0318      1.43  VQ         |          |          |          |
   0+30       0.0422      1.51  V Q        |          |          |          |
   0+35       0.0528      1.54  V Q        |          |          |          |
   0+40       0.0635      1.56  V Q        |          |          |          |
   0+45       0.0743      1.57  V Q        |          |          |          |
   0+50       0.0862      1.72  V Q        |          |          |          |
   0+55       0.0997      1.97  V Q        |          |          |          |
   1+ 0       0.1137      2.03  V Q        |          |          |          |
   1+ 5       0.1269      1.91  V Q        |          |          |          |
   1+10       0.1384      1.67  V Q        |          |          |          |
   1+15       0.1496      1.62  V Q        |          |          |          |
   1+20       0.1606      1.59  V Q        |          |          |          |
   1+25       0.1714      1.58  V Q        |          |          |          |
   1+30       0.1822      1.57  V Q        |          |          |          |
   1+35       0.1930      1.57  V Q        |          |          |          |
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1+40	0.2038	1.57	V Q	|	|	|	|
1+45	0.2146	1.57	V Q	|	|	|	|
1+50	0.2264	1.72	V Q	|	|	|	|
1+55	0.2400	1.97	V Q	|	|	|	|
2+ 0	0.2540	2.03	V Q	|	|	|	|
2+ 5	0.2682	2.06	V Q	|	|	|	|
2+10	0.2825	2.08	V Q	|	|	|	|
2+15	0.2969	2.09	V Q	|	|	|	|
2+20	0.3113	2.09	|VQ	|	|	|	|
2+25	0.3257	2.09	|VQ	|	|	|	|
2+30	0.3401	2.09	|VQ	|	|	|	|
2+35	0.3555	2.24	|VQ	|	|	|	|
2+40	0.3727	2.49	|V Q	|	|	|	|
2+45	0.3903	2.56	|V Q	|	|	|	|
2+50	0.4081	2.58	|V Q	|	|	|	|
2+55	0.4260	2.60	|V Q	|	|	|	|
3+ 0	0.4440	2.61	|V Q	|	|	|	|
3+ 5	0.4620	2.61	|V Q	|	|	|	|
3+10	0.4799	2.61	|V Q	|	|	|	|
3+15	0.4979	2.61	|V Q	|	|	|	|
3+20	0.5159	2.61	|V Q	|	|	|	|
3+25	0.5339	2.61	|V Q	|	|	|	|
3+30	0.5519	2.61	|V Q	|	|	|	|
3+35	0.5699	2.61	|V Q	|	|	|	|
3+40	0.5879	2.61	|V Q	|	|	|	|
3+45	0.6058	2.61	|V Q	|	|	|	|
3+50	0.6249	2.76	| VQ	|	|	|	|
3+55	0.6456	3.01	| V Q	|	|	|	|
4+ 0	0.6668	3.08	| V Q	|	|	|	|
4+ 5	0.6882	3.11	| V Q	|	|	|	|
4+10	0.7097	3.12	| V Q	|	|	|	|
4+15	0.7313	3.13	| V Q	|	|	|	|
4+20	0.7540	3.29	| V Q	|	|	|	|
4+25	0.7783	3.54	| V Q	|	|	|	|
4+30	0.8031	3.60	| V Q	|	|	|	|
4+35	0.8281	3.63	| V Q	|	|	|	|
4+40	0.8532	3.64	| V Q	|	|	|	|
4+45	0.8784	3.66	| V Q	|	|	|	|
4+50	0.9046	3.81	| V Q	|	|	|	|
4+55	0.9326	4.06	| V Q	|	|	|	|
5+ 0	0.9610	4.12	| V Q	|	|	|	|
5+ 5	0.9875	3.85	| V Q	|	|	|	|
5+10	1.0106	3.36	| VQ	|	|	|	|
5+15	1.0329	3.24	| VQ	|	|	|	|
5+20	1.0559	3.34	| VQ	|	|	|	|
5+25	1.0804	3.56	| VQ	|	|	|	|
5+30	1.1052	3.60	| VQ	|	|	|	|
5+35	1.1313	3.78	| V Q	|	|	|	|
5+40	1.1592	4.05	| V Q	|	|	|	|
5+45	1.1876	4.12	| V Q	|	|	|	|
5+50	1.2162	4.15	| V Q	|	|	|	|
5+55	1.2449	4.17	| VQ	|	|	|	|
6+ 0	1.2736	4.18	| VQ	|	|	|	|
6+ 5	1.3035	4.33	| VQ	|	|	|	|
6+10	1.3350	4.58	| V Q	|	|	|	|
6+15	1.3670	4.65	| V Q	|	|	|	|
6+20	1.3992	4.67	| V Q	|	|	|	|
6+25	1.4315	4.69	| V Q	|	|	|	|
6+30	1.4639	4.70	| V Q	|	|	|	|
6+35	1.4973	4.85	| V Q	|	|	|	|
6+40	1.5324	5.10	| V Q	|	|	|	|
6+45	1.5680	5.17	| VQ	|	|	|	|
6+50	1.6038	5.20	| VQ	|	|	|	|
6+55	1.6397	5.21	| VQ	|	|	|	|
7+ 0	1.6757	5.22	| VQ	|	|	|	|
7+ 5	1.7116	5.22	| VQ	|	|	|	|
7+10	1.7476	5.22	| VQ	|	|	|	|
7+15	1.7836	5.22	| VQ	|	|	|	|
7+20	1.8206	5.38	| V Q	|	|	|	|
7+25	1.8593	5.63	| VQ	|	|	|	|
7+30	1.8985	5.69	| VQ	|	|	|	|
7+35	1.9390	5.87	| VQ	|	|	|	|
7+40	1.9812	6.14	| V Q	|	|	|	|
7+45	2.0240	6.21	| V Q	|	|	|	|
7+50	2.0680	6.39	| V Q	|	|	|	|
7+55	2.1139	6.66	| V Q	|	|	|	|
8+ 0	2.1603	6.73	| VQ	|	|	|	|
8+ 5	2.2090	7.07	| V Q|	|	|	|	|
8+10	2.2612	7.59	| V Q	|	|	|	|
8+15	2.3144	7.72	| V Q	|	|	|	|
8+20	2.3680	7.78	| V Q	|	|	|	|
8+25	2.4218	7.81	| V Q	|	|	|	|
8+30	2.4757	7.83	| V Q	|	|	|	|
8+35	2.5307	7.99	| V Q	|	|	|	|
8+40	2.5875	8.24	| V Q	|	|	|	|
8+45	2.6446	8.30	| V |Q	|	|	|	|

8+50	2.7031	8.48	
8+55	2.7633	8.75	
9+ 0	2.8241	8.82	
9+ 5	2.8871	9.16	
9+10	2.9538	9.67	
9+15	3.0214	9.81	
9+20	3.0904	10.02	
9+25	3.1613	10.30	
9+30	3.2329	10.39	
9+35	3.3057	10.57	
9+40	3.3803	10.84	
9+45	3.4555	10.91	
9+50	3.5320	11.11	
9+55	3.6108	11.43	
10+ 0	3.6904	11.56	
10+ 5	3.7627	10.50	
10+10	3.8225	8.68	
10+15	3.8792	8.23	
10+20	3.9345	8.03	
10+25	3.9890	7.92	
10+30	4.0430	7.83	
10+35	4.1022	8.60	
10+40	4.1700	9.85	
10+45	4.2401	10.17	
10+50	4.3111	10.31	
10+55	4.3826	10.39	
11+ 0	4.4546	10.45	
11+ 5	4.5254	10.29	
11+10	4.5946	10.04	
11+15	4.6633	9.98	
11+20	4.7318	9.95	
11+25	4.8003	9.93	
11+30	4.8686	9.92	
11+35	4.9348	9.62	
11+40	4.9976	9.12	
11+45	5.0595	8.99	
11+50	5.1221	9.08	
11+55	5.1862	9.31	
12+ 0	5.2505	9.35	
12+ 5	5.3286	11.34	
12+10	5.4291	14.59	
12+15	5.5356	15.46	
12+20	5.6470	16.17	
12+25	5.7636	16.92	
12+30	5.8823	17.24	
12+35	6.0060	17.96	
12+40	6.1372	19.04	
12+45	6.2706	19.37	
12+50	6.4072	19.84	
12+55	6.5480	20.45	
13+ 0	6.6904	20.67	
13+ 5	6.8440	22.30	
13+10	7.0154	24.89	
13+15	7.1917	25.60	
13+20	7.3703	25.93	
13+25	7.5502	26.13	
13+30	7.7312	26.29	
13+35	7.8895	22.97	
13+40	8.0100	17.50	
13+45	8.1212	16.15	
13+50	8.2285	15.57	
13+55	8.3337	15.28	
14+ 0	8.4376	15.08	
14+ 5	8.5502	16.35	
14+10	8.6769	18.40	
14+15	8.8074	18.95	
14+20	8.9377	18.92	
14+25	9.0656	18.58	
14+30	9.1937	18.59	
14+35	9.3216	18.58	
14+40	9.4497	18.59	
14+45	9.5779	18.61	
14+50	9.7043	18.35	
14+55	9.8275	17.89	
15+ 0	9.9502	17.81	
15+ 5	10.0707	17.49	
15+10	10.1878	17.00	
15+15	10.3041	16.89	
15+20	10.4183	16.58	
15+25	10.5290	16.08	
15+30	10.6391	15.98	
15+35	10.7406	14.74	
15+40	10.8284	12.74	
15+45	10.9127	12.25	
15+50	10.9959	12.07	
15+55	11.0784	11.99	

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16+ 0      11.1606     11.94 |          |    Q     |          |     V    |
16+ 5      11.2231      9.07 |          | Q        |          |     V    |
16+10      11.2529      4.33 |     Q    |          |          |     V    |
16+15      11.2745      3.13 |    Q     |          |          |     V    |
16+20      11.2923      2.60 |  Q       |          |          |     V    |
16+25      11.3082      2.31 |  Q       |          |          |     V    |
16+30      11.3226      2.09 | Q        |          |          |     V    |
16+35      11.3359      1.94 | Q        |          |          |     V    |
16+40      11.3475      1.69 | Q        |          |          |     V    |
16+45      11.3587      1.62 | Q        |          |          |     V    |
16+50      11.3697      1.59 | Q        |          |          |      V   |
16+55      11.3806      1.58 | Q        |          |          |      V   |
17+ 0      11.3913      1.57 | Q        |          |          |      V   |
17+ 5      11.4042      1.87 | Q        |          |          |      V   |
17+10      11.4206      2.37 |  Q       |          |          |      V   |
17+15      11.4378      2.50 |  Q       |          |          |      V   |
17+20      11.4554      2.56 |  Q       |          |          |      V   |
17+25      11.4733      2.59 |  Q       |          |          |      V   |
17+30      11.4912      2.61 |  Q       |          |          |      V   |
17+35      11.5092      2.61 |  Q       |          |          |      V   |
17+40      11.5272      2.61 |  Q       |          |          |      V   |
17+45      11.5452      2.61 |  Q       |          |          |      V   |
17+50      11.5621      2.46 |  Q       |          |          |      V   |
17+55      11.5773      2.21 | Q        |          |          |      V   |
18+ 0      11.5921      2.14 | Q        |          |          |      V   |
18+ 5      11.6067      2.12 | Q        |          |          |      V   |
18+10      11.6211      2.10 | Q        |          |          |      V   |
18+15      11.6355      2.09 | Q        |          |          |      V   |
18+20      11.6499      2.09 | Q        |          |          |      V   |
18+25      11.6643      2.09 | Q        |          |          |      V   |
18+30      11.6787      2.09 | Q        |          |          |       V  |
18+35      11.6920      1.94 | Q        |          |          |       V  |
18+40      11.7036      1.69 | Q        |          |          |       V  |
18+45      11.7148      1.62 | Q        |          |          |       V  |
18+50      11.7247      1.44 |Q         |          |          |       V  |
18+55      11.7328      1.17 |Q         |          |          |       V  |
19+ 0      11.7404      1.10 |Q         |          |          |       V  |
19+ 5      11.7488      1.22 |Q         |          |          |       V  |
19+10      11.7589      1.46 |Q         |          |          |       V  |
19+15      11.7693      1.51 | Q        |          |          |       V  |
19+20      11.7809      1.69 | Q        |          |          |       V  |
19+25      11.7944      1.96 | Q        |          |          |       V  |
19+30      11.8084      2.03 | Q        |          |          |       V  |
19+35      11.8216      1.91 | Q        |          |          |       V  |
19+40      11.8331      1.67 | Q        |          |          |       V  |
19+45      11.8443      1.62 | Q        |          |          |       V  |
19+50      11.8542      1.44 |Q         |          |          |       V  |
19+55      11.8623      1.17 |Q         |          |          |       V  |
20+ 0      11.8699      1.10 |Q         |          |          |       V  |
20+ 5      11.8783      1.22 |Q         |          |          |       V  |
20+10      11.8884      1.46 |Q         |          |          |       V  |
20+15      11.8988      1.51 | Q        |          |          |       V  |
20+20      11.9094      1.54 | Q        |          |          |       V  |
20+25      11.9201      1.56 | Q        |          |          |       V  |
20+30      11.9309      1.57 | Q        |          |          |       V  |
20+35      11.9417      1.57 | Q        |          |          |       V  |
20+40      11.9525      1.57 | Q        |          |          |       V  |
20+45      11.9632      1.57 | Q        |          |          |       V  |
20+50      11.9730      1.41 |Q         |          |          |       V  |
20+55      11.9810      1.16 |Q         |          |          |        V |
21+ 0      11.9886      1.10 |Q         |          |          |        V |
21+ 5      11.9970      1.22 |Q         |          |          |        V |
21+10      12.0071      1.46 |Q         |          |          |        V |
21+15      12.0175      1.51 | Q        |          |          |        V |
21+20      12.0270      1.39 |Q         |          |          |        V |
21+25      12.0349      1.15 |Q         |          |          |        V |
21+30      12.0425      1.10 |Q         |          |          |        V |
21+35      12.0510      1.22 |Q         |          |          |        V |
21+40      12.0610      1.46 |Q         |          |          |        V |
21+45      12.0714      1.51 | Q        |          |          |        V |
21+50      12.0810      1.39 |Q         |          |          |        V |
21+55      12.0889      1.15 |Q         |          |          |        V |
22+ 0      12.0965      1.10 |Q         |          |          |        V |
22+ 5      12.1049      1.22 |Q         |          |          |        V |
22+10      12.1150      1.46 |Q         |          |          |        V |
22+15      12.1254      1.51 | Q        |          |          |        V |
22+20      12.1349      1.39 |Q         |          |          |        V |
22+25      12.1429      1.15 |Q         |          |          |        V |
22+30      12.1504      1.10 |Q         |          |          |        V |
22+35      12.1578      1.07 |Q         |          |          |        V |
22+40      12.1651      1.06 |Q         |          |          |        V |
22+45      12.1723      1.04 |Q         |          |          |        V |
22+50      12.1795      1.04 |Q         |          |          |        V |
22+55      12.1867      1.04 |Q         |          |          |        V |
23+ 0      12.1939      1.04 |Q         |          |          |        V |
23+ 5      12.2010      1.04 |Q         |          |          |        V |
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   23+10      12.2082      1.04  |Q        |         |         |        v|
   23+15      12.2154      1.04  |Q        |         |         |        v|
   23+20      12.2226      1.04  |Q        |         |         |        v|
   23+25      12.2298      1.04  |Q        |         |         |        v|
   23+30      12.2370      1.04  |Q        |         |         |        v|
   23+35      12.2442      1.04  |Q        |         |         |        v|
   23+40      12.2514      1.04  |Q        |         |         |        v|
   23+45      12.2586      1.04  |Q        |         |         |        v|
   23+50      12.2658      1.04  |Q        |         |         |        v|
   23+55      12.2730      1.04  |Q        |         |         |        v|
   24+ 0      12.2802      1.04  |Q        |         |         |        v|
   24+ 5      12.2853      0.74  Q         |         |         |        v|
   24+10      12.2869      0.24  Q         |         |         |        v|
   24+15      12.2877      0.11  Q         |         |         |        v|
   24+20      12.2880      0.05  Q         |         |         |        v|
   24+25      12.2882      0.02  Q         |         |         |         v
-------------------------------------------------------------------------
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Extended Detention Basin No. 3

U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 2225.00(Ft.)
Length along longest watercourse measured to centroid = 1113.00(Ft.)
Length along longest watercourse = 0.421 Mi.
Length along longest watercourse measured to centroid = 0.211 Mi.
Difference in elevation = 82.00(Ft.)
Slope along watercourse = 194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	0.50	3.90

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.30	10.13

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.300(In)

Point rain (area averaged) = 0.500(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 0.500(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	69.00	0.500

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

Slope of intensity-duration curve for a 1 hour storm =0.5500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
		Sum = 100.000	Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.198	(0.316)	0.099	0.099
2	0.17	4.20	0.252	(0.316)	0.126	0.126
3	0.25	4.40	0.264	(0.316)	0.132	0.132
4	0.33	4.80	0.288	(0.316)	0.144	0.144
5	0.42	5.20	0.312	(0.316)	0.156	0.156
6	0.50	6.20	0.372	(0.316)	0.186	0.186
7	0.58	6.80	0.408	(0.316)	0.204	0.204
8	0.67	8.80	0.528	(0.316)	0.264	0.264
9	0.75	13.90	0.834	0.316	(0.417)	0.518
10	0.83	31.40	1.884	0.316	(0.942)	1.568
11	0.92	7.20	0.432	(0.316)	0.216	0.216
12	1.00	3.80	0.228	(0.316)	0.114	0.114
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	3.7

Flood volume = Effective rainfall 0.31(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.2(Ac.Ft)
Total soil loss = 0.19(In)
Total soil loss = 0.123(Ac.Ft)
Total rainfall = 0.50(In)
Flood volume = 8783.4 Cubic Feet
Total soil loss = 5354.5 Cubic Feet

Peak flow rate of this hydrograph = 6.894(CFS)

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0 2.5 5.0 7.5 10.0
0+ 5	0.0019	0.27	VQ
0+10	0.0068	0.71	VQ
0+15	0.0130	0.91	VQ
0+20	0.0200	1.02	VQ
0+25	0.0278	1.13	QV
0+30	0.0366	1.28	Q V
0+35	0.0466	1.46	Q V
0+40	0.0585	1.72	Q V
0+45	0.0769	2.67	Q V
0+50	0.1220	6.55	V Q
0+55	0.1695	6.89	Q V
1+ 0	0.1879	2.67	Q V
1+ 5	0.1967	1.28	Q V
1+10	0.2000	0.49	Q V
1+15	0.2013	0.19	Q V
1+20	0.2016	0.04	Q V
1+25	0.2016	0.01	Q V

U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 2225.00(Ft.)
Length along longest watercourse measured to centroid = 1113.00(Ft.)
Length along longest watercourse = 0.421 Mi.
Length along longest watercourse measured to centroid = 0.211 Mi.
Difference in elevation = 82.00(Ft.)
Slope along watercourse = 194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	0.80	6.23

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	2.00	15.58

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 0.800(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 0.800(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	69.00	0.500

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
			Sum = 100.000	Sum= 7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.125	(0.316)	0.062	0.062
2	0.17	1.30	0.125	(0.316)	0.062	0.062
3	0.25	1.10	0.106	(0.316)	0.053	0.053
4	0.33	1.50	0.144	(0.316)	0.072	0.072
5	0.42	1.50	0.144	(0.316)	0.072	0.072
6	0.50	1.80	0.173	(0.316)	0.086	0.086
7	0.58	1.50	0.144	(0.316)	0.072	0.072
8	0.67	1.80	0.173	(0.316)	0.086	0.086
9	0.75	1.80	0.173	(0.316)	0.086	0.086
10	0.83	1.50	0.144	(0.316)	0.072	0.072
11	0.92	1.60	0.154	(0.316)	0.077	0.077
12	1.00	1.80	0.173	(0.316)	0.086	0.086
13	1.08	2.20	0.211	(0.316)	0.106	0.106
14	1.17	2.20	0.211	(0.316)	0.106	0.106
15	1.25	2.20	0.211	(0.316)	0.106	0.106
16	1.33	2.00	0.192	(0.316)	0.096	0.096
17	1.42	2.60	0.250	(0.316)	0.125	0.125
18	1.50	2.70	0.259	(0.316)	0.130	0.130
19	1.58	2.40	0.230	(0.316)	0.115	0.115
20	1.67	2.70	0.259	(0.316)	0.130	0.130
21	1.75	3.30	0.317	(0.316)	0.158	0.158
22	1.83	3.10	0.298	(0.316)	0.149	0.149
23	1.92	2.90	0.278	(0.316)	0.139	0.139
24	2.00	3.00	0.288	(0.316)	0.144	0.144
25	2.08	3.10	0.298	(0.316)	0.149	0.149
26	2.17	4.20	0.403	(0.316)	0.202	0.202
27	2.25	5.00	0.480	(0.316)	0.240	0.240
28	2.33	3.50	0.336	(0.316)	0.168	0.168
29	2.42	6.80	0.653	0.316	(0.326)	0.337
30	2.50	7.30	0.701	0.316	(0.350)	0.385
31	2.58	8.20	0.787	0.316	(0.394)	0.471
32	2.67	5.90	0.566	(0.316)	0.283	0.283
33	2.75	2.00	0.192	(0.316)	0.096	0.096
34	2.83	1.80	0.173	(0.316)	0.086	0.086
35	2.92	1.80	0.173	(0.316)	0.086	0.086
36	3.00	0.60	0.058	(0.316)	0.029	0.029
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	4.9

Flood volume = Effective rainfall 0.41(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft)
Total soil loss = 0.39(In)
Total soil loss = 0.253(Ac.Ft)
Total rainfall = 0.80(In)
Flood volume = 11601.3 Cubic Feet
Total soil loss = 11020.1 Cubic Feet

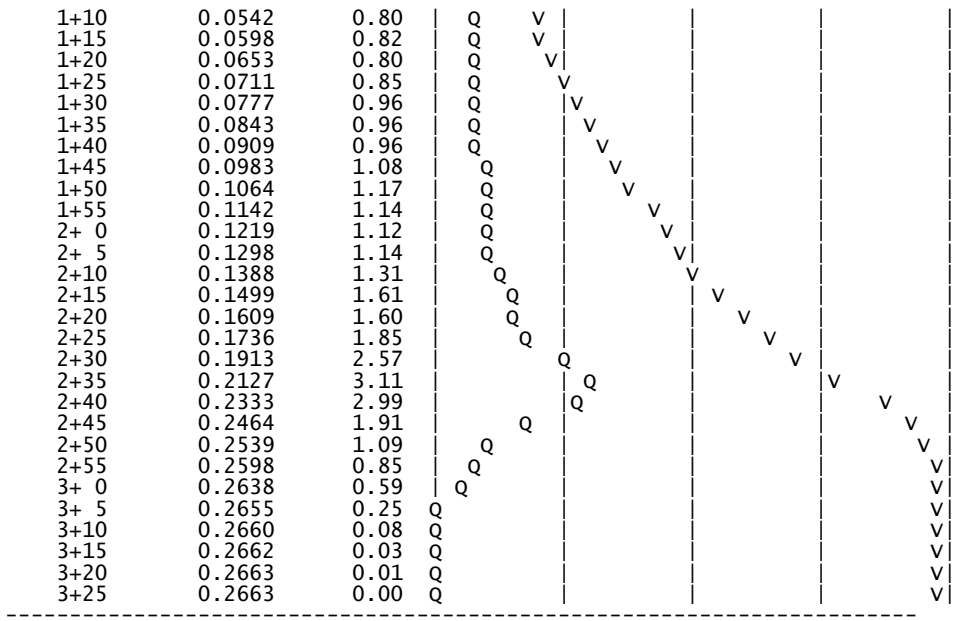
Peak flow rate of this hydrograph = 3.105(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0012	0.17	Q				
0+10	0.0039	0.40	VQ				
0+15	0.0069	0.43	|Q				
0+20	0.0101	0.47	|Q				
0+25	0.0138	0.54	| Q				
0+30	0.0179	0.60	| Q				
0+35	0.0221	0.61	| QV				
0+40	0.0264	0.62	| QV				
0+45	0.0309	0.66	| Q V				
0+50	0.0353	0.63	| Q V				
0+55	0.0394	0.60	| Q V				
1+ 0	0.0437	0.63	| Q V				
1+ 5	0.0487	0.72	| Q V				


1+10 0.0542 0.80
1+15 0.0598 0.82
1+20 0.0653 0.80
1+25 0.0711 0.85
1+30 0.0777 0.96
1+35 0.0843 0.96
1+40 0.0909 0.96
1+45 0.0983 1.08
1+50 0.1064 1.17
1+55 0.1142 1.14
2+ 0 0.1219 1.12
2+ 5 0.1298 1.14
2+10 0.1388 1.31
2+15 0.1499 1.61
2+20 0.1609 1.60
2+25 0.1736 1.85
2+30 0.1913 2.57
2+35 0.2127 3.11
2+40 0.2333 2.99
2+45 0.2464 1.91
2+50 0.2539 1.09
2+55 0.2598 0.85
3+ 0 0.2638 0.59
3+ 5 0.2655 0.25
3+10 0.2660 0.08
3+15 0.2662 0.03
3+20 0.2663 0.01
3+25 0.2663 0.00

U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 2225.00(Ft.)
Length along longest watercourse measured to centroid = 1113.00(Ft.)
Length along longest watercourse = 0.421 Mi.
Length along longest watercourse measured to centroid = 0.211 Mi.
Difference in elevation = 82.00(Ft.)
Slope along watercourse = 194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.10	8.57

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	3.00	23.37

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.100(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.100(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	69.00	0.500

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
			Sum = 100.000 Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.066	(0.316)	0.033	0.033
2	0.17	0.60	0.079	(0.316)	0.040	0.040
3	0.25	0.60	0.079	(0.316)	0.040	0.040
4	0.33	0.60	0.079	(0.316)	0.040	0.040
5	0.42	0.60	0.079	(0.316)	0.040	0.040
6	0.50	0.70	0.092	(0.316)	0.046	0.046
7	0.58	0.70	0.092	(0.316)	0.046	0.046
8	0.67	0.70	0.092	(0.316)	0.046	0.046
9	0.75	0.70	0.092	(0.316)	0.046	0.046
10	0.83	0.70	0.092	(0.316)	0.046	0.046
11	0.92	0.70	0.092	(0.316)	0.046	0.046
12	1.00	0.80	0.106	(0.316)	0.053	0.053
13	1.08	0.80	0.106	(0.316)	0.053	0.053
14	1.17	0.80	0.106	(0.316)	0.053	0.053
15	1.25	0.80	0.106	(0.316)	0.053	0.053
16	1.33	0.80	0.106	(0.316)	0.053	0.053
17	1.42	0.80	0.106	(0.316)	0.053	0.053
18	1.50	0.80	0.106	(0.316)	0.053	0.053
19	1.58	0.80	0.106	(0.316)	0.053	0.053
20	1.67	0.80	0.106	(0.316)	0.053	0.053
21	1.75	0.80	0.106	(0.316)	0.053	0.053
22	1.83	0.80	0.106	(0.316)	0.053	0.053
23	1.92	0.80	0.106	(0.316)	0.053	0.053
24	2.00	0.90	0.119	(0.316)	0.059	0.059
25	2.08	0.80	0.106	(0.316)	0.053	0.053
26	2.17	0.90	0.119	(0.316)	0.059	0.059
27	2.25	0.90	0.119	(0.316)	0.059	0.059
28	2.33	0.90	0.119	(0.316)	0.059	0.059
29	2.42	0.90	0.119	(0.316)	0.059	0.059
30	2.50	0.90	0.119	(0.316)	0.059	0.059
31	2.58	0.90	0.119	(0.316)	0.059	0.059
32	2.67	0.90	0.119	(0.316)	0.059	0.059
33	2.75	1.00	0.132	(0.316)	0.066	0.066
34	2.83	1.00	0.132	(0.316)	0.066	0.066
35	2.92	1.00	0.132	(0.316)	0.066	0.066
36	3.00	1.00	0.132	(0.316)	0.066	0.066
37	3.08	1.00	0.132	(0.316)	0.066	0.066
38	3.17	1.10	0.145	(0.316)	0.073	0.073
39	3.25	1.10	0.145	(0.316)	0.073	0.073
40	3.33	1.10	0.145	(0.316)	0.073	0.073
41	3.42	1.20	0.158	(0.316)	0.079	0.079
42	3.50	1.30	0.172	(0.316)	0.086	0.086
43	3.58	1.40	0.185	(0.316)	0.092	0.092
44	3.67	1.40	0.185	(0.316)	0.092	0.092
45	3.75	1.50	0.198	(0.316)	0.099	0.099
46	3.83	1.50	0.198	(0.316)	0.099	0.099
47	3.92	1.60	0.211	(0.316)	0.106	0.106
48	4.00	1.60	0.211	(0.316)	0.106	0.106
49	4.08	1.70	0.224	(0.316)	0.112	0.112
50	4.17	1.80	0.238	(0.316)	0.119	0.119
51	4.25	1.90	0.251	(0.316)	0.125	0.125
52	4.33	2.00	0.264	(0.316)	0.132	0.132
53	4.42	2.10	0.277	(0.316)	0.139	0.139
54	4.50	2.10	0.277	(0.316)	0.139	0.139
55	4.58	2.20	0.290	(0.316)	0.145	0.145
56	4.67	2.30	0.304	(0.316)	0.152	0.152
57	4.75	2.40	0.317	(0.316)	0.158	0.158
58	4.83	2.40	0.317	(0.316)	0.158	0.158
59	4.92	2.50	0.330	(0.316)	0.165	0.165
60	5.00	2.60	0.343	(0.316)	0.172	0.172
61	5.08	3.10	0.409	(0.316)	0.205	0.205
62	5.17	3.60	0.475	(0.316)	0.238	0.238
63	5.25	3.90	0.515	(0.316)	0.257	0.257
64	5.33	4.20	0.554	(0.316)	0.277	0.277
65	5.42	4.70	0.620	(0.316)	0.310	0.310
66	5.50	5.60	0.739	0.316	(0.370)	0.424
67	5.58	1.90	0.251	(0.316)	0.125	0.125
68	5.67	0.90	0.119	(0.316)	0.059	0.059
69	5.75	0.60	0.079	(0.316)	0.040	0.040
70	5.83	0.50	0.066	(0.316)	0.033	0.033

```
71   5.92     0.30      0.040       (  0.316)       0.020        0.020
72   6.00     0.20      0.026       (  0.316)       0.013        0.013
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =     6.7
      Flood volume = Effective rainfall      0.55(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       0.4(Ac.Ft)
      Total soil loss =      0.55(In)
      Total soil loss =     0.354(Ac.Ft)
      Total rainfall =      1.10(In)
      Flood volume =       15679.4 Cubic Feet
      Total soil loss =       15425.3 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      2.682(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f     H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0006      0.09  Q         |         |         |         |
  0+10       0.0022      0.23  Q         |         |         |         |
  0+15       0.0041      0.28  VQ        |         |         |         |
  0+20       0.0062      0.30  VQ        |         |         |         |
  0+25       0.0083      0.31  VQ        |         |         |         |
  0+30       0.0106      0.33  |Q        |         |         |         |
  0+35       0.0130      0.35  |Q        |         |         |         |
  0+40       0.0155      0.36  |Q        |         |         |         |
  0+45       0.0180      0.36  |Q        |         |         |         |
  0+50       0.0205      0.36  |QV       |         |         |         |
  0+55       0.0230      0.36  |QV       |         |         |         |
  1+ 0       0.0256      0.38  |QV       |         |         |         |
  1+ 5       0.0284      0.41  |Q V      |         |         |         |
  1+10       0.0312      0.41  |Q V      |         |         |         |
  1+15       0.0341      0.41  |Q V      |         |         |         |
  1+20       0.0369      0.41  |Q  V     |         |         |         |
  1+25       0.0398      0.41  |Q  V     |         |         |         |
  1+30       0.0426      0.41  |Q  V     |         |         |         |
  1+35       0.0455      0.41  |Q   V    |         |         |         |
  1+40       0.0483      0.41  |Q   V    |         |         |         |
  1+45       0.0512      0.41  |Q   V    |         |         |         |
  1+50       0.0540      0.41  |Q    V   |         |         |         |
  1+55       0.0569      0.41  |Q    V   |         |         |         |
  2+ 0       0.0599      0.43  |Q    V   |         |         |         |
  2+ 5       0.0629      0.44  |Q    V   |         |         |         |
  2+10       0.0659      0.44  |Q     V  |         |         |         |
  2+15       0.0691      0.46  |Q     V  |         |         |         |
  2+20       0.0723      0.46  |Q      V |         |         |         |
  2+25       0.0755      0.47  |Q      V |         |         |         |
  2+30       0.0787      0.47  |Q      V |         |         |         |
  2+35       0.0819      0.47  |Q       V|         |         |         |
  2+40       0.0851      0.47  |Q       V|         |         |         |
  2+45       0.0885      0.48  |Q       V|         |         |         |
  2+50       0.0920      0.51  | Q       V         |         |         |
  2+55       0.0955      0.51  | Q       V         |         |         |
  3+ 0       0.0991      0.52  | Q       |V        |         |         |
  3+ 5       0.1026      0.52  | Q       |V        |         |         |
  3+10       0.1063      0.54  | Q       |V        |         |         |
  3+15       0.1102      0.56  | Q       | V       |         |         |
  3+20       0.1141      0.57  | Q       | V       |         |         |
  3+25       0.1181      0.59  | Q       |  V      |         |         |
  3+30       0.1225      0.63  | Q       |  V      |         |         |
  3+35       0.1271      0.68  | Q       |   V     |         |         |
  3+40       0.1320      0.71  | Q       |   V     |         |         |
  3+45       0.1371      0.74  | Q       |    V    |         |         |
  3+50       0.1424      0.77  |  Q      |    V    |         |         |
  3+55       0.1478      0.79  |  Q      |     V   |         |         |
  4+ 0       0.1535      0.82  |  Q      |      V  |         |         |
  4+ 5       0.1593      0.84  |  Q      |      V  |         |         |
  4+10       0.1654      0.89  |  Q      |       V |         |         |
  4+15       0.1719      0.94  |  Q      |        V|         |         |
  4+20       0.1787      0.99  |  Q      |        V|         |         |
  4+25       0.1858      1.04  |   Q     |         V         |         |
  4+30       0.1932      1.07  |   Q     |         |V        |         |
  4+35       0.2008      1.10  |   Q     |         | V       |         |
  4+40       0.2087      1.15  |   Q     |         |  V      |         |
  4+45       0.2169      1.20  |   Q     |         |   V     |         |
  4+50       0.2254      1.23  |   Q     |         |    V    |         |
  4+55       0.2341      1.26  |    Q    |         |     V   |         |
  5+ 0       0.2430      1.30  |    Q    |         |      V  |         |
  5+ 5       0.2528      1.42  |    Q    |         |       V |         |
  5+10       0.2642      1.64  |     Q   |         |        V|         |
  5+15       0.2769      1.85  |      Q  |         |         V         |
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    5+20       0.2908      2.02  |       Q |         |         | V       |
    5+25       0.3061      2.22  |       Q |         |         |   V     |
    5+30       0.3245      2.68  |         Q         |         |     V   |
    5+35       0.3405      2.31  |         Q|        |         |       V |
    5+40       0.3485      1.16  |    Q     |        |         |         V|
    5+45       0.3530      0.66  |  Q       |        |         |         V|
    5+50       0.3559      0.43  |Q         |        |         |         V|
    5+55       0.3579      0.28  |Q         |        |         |         V|
    6+ 0       0.3591      0.17  Q          |        |         |         V|
    6+ 5       0.3597      0.09  Q          |        |         |         V|
    6+10       0.3598      0.03  Q          |        |         |         V|
    6+15       0.3599      0.01  Q          |        |         |         V|
    6+20       0.3599      0.00  Q          |        |         |         V|
    6+25       0.3599      0.00  Q          |        |         |          V
---------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro32242.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 2225.00(Ft.)
Length along longest watercourse measured to centroid = 1113.00(Ft.)
Length along longest watercourse = 0.421 Mi.
Length along longest watercourse measured to centroid = 0.211 Mi.
Difference in elevation = 82.00(Ft.)
Slope along watercourse = 194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.80	14.02

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	5.00	38.95

STORM EVENT (YEAR) = 2.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 1.800(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.800(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	69.00	0.500

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
			Sum = 100.000	Sum= 7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.014	(0.560)	0.007	0.007
2	0.17	0.07	0.014	(0.557)	0.007	0.007
3	0.25	0.07	0.014	(0.555)	0.007	0.007
4	0.33	0.10	0.022	(0.553)	0.011	0.011
5	0.42	0.10	0.022	(0.551)	0.011	0.011
6	0.50	0.10	0.022	(0.549)	0.011	0.011
7	0.58	0.10	0.022	(0.547)	0.011	0.011
8	0.67	0.10	0.022	(0.545)	0.011	0.011
9	0.75	0.10	0.022	(0.542)	0.011	0.011
10	0.83	0.13	0.029	(0.540)	0.014	0.014
11	0.92	0.13	0.029	(0.538)	0.014	0.014
12	1.00	0.13	0.029	(0.536)	0.014	0.014
13	1.08	0.10	0.022	(0.534)	0.011	0.011
14	1.17	0.10	0.022	(0.532)	0.011	0.011
15	1.25	0.10	0.022	(0.530)	0.011	0.011
16	1.33	0.10	0.022	(0.528)	0.011	0.011
17	1.42	0.10	0.022	(0.525)	0.011	0.011
18	1.50	0.10	0.022	(0.523)	0.011	0.011
19	1.58	0.10	0.022	(0.521)	0.011	0.011
20	1.67	0.10	0.022	(0.519)	0.011	0.011
21	1.75	0.10	0.022	(0.517)	0.011	0.011
22	1.83	0.13	0.029	(0.515)	0.014	0.014
23	1.92	0.13	0.029	(0.513)	0.014	0.014
24	2.00	0.13	0.029	(0.511)	0.014	0.014
25	2.08	0.13	0.029	(0.509)	0.014	0.014
26	2.17	0.13	0.029	(0.507)	0.014	0.014
27	2.25	0.13	0.029	(0.505)	0.014	0.014
28	2.33	0.13	0.029	(0.503)	0.014	0.014
29	2.42	0.13	0.029	(0.501)	0.014	0.014
30	2.50	0.13	0.029	(0.499)	0.014	0.014
31	2.58	0.17	0.036	(0.497)	0.018	0.018
32	2.67	0.17	0.036	(0.494)	0.018	0.018
33	2.75	0.17	0.036	(0.492)	0.018	0.018
34	2.83	0.17	0.036	(0.490)	0.018	0.018
35	2.92	0.17	0.036	(0.488)	0.018	0.018
36	3.00	0.17	0.036	(0.486)	0.018	0.018
37	3.08	0.17	0.036	(0.484)	0.018	0.018
38	3.17	0.17	0.036	(0.482)	0.018	0.018
39	3.25	0.17	0.036	(0.480)	0.018	0.018
40	3.33	0.17	0.036	(0.478)	0.018	0.018
41	3.42	0.17	0.036	(0.476)	0.018	0.018
42	3.50	0.17	0.036	(0.474)	0.018	0.018
43	3.58	0.17	0.036	(0.472)	0.018	0.018
44	3.67	0.17	0.036	(0.470)	0.018	0.018
45	3.75	0.17	0.036	(0.468)	0.018	0.018
46	3.83	0.20	0.043	(0.466)	0.022	0.022
47	3.92	0.20	0.043	(0.464)	0.022	0.022
48	4.00	0.20	0.043	(0.463)	0.022	0.022
49	4.08	0.20	0.043	(0.461)	0.022	0.022
50	4.17	0.20	0.043	(0.459)	0.022	0.022
51	4.25	0.20	0.043	(0.457)	0.022	0.022
52	4.33	0.23	0.050	(0.455)	0.025	0.025
53	4.42	0.23	0.050	(0.453)	0.025	0.025
54	4.50	0.23	0.050	(0.451)	0.025	0.025
55	4.58	0.23	0.050	(0.449)	0.025	0.025
56	4.67	0.23	0.050	(0.447)	0.025	0.025
57	4.75	0.23	0.050	(0.445)	0.025	0.025
58	4.83	0.27	0.058	(0.443)	0.029	0.029
59	4.92	0.27	0.058	(0.441)	0.029	0.029
60	5.00	0.27	0.058	(0.439)	0.029	0.029
61	5.08	0.20	0.043	(0.437)	0.022	0.022
62	5.17	0.20	0.043	(0.435)	0.022	0.022
63	5.25	0.20	0.043	(0.434)	0.022	0.022
64	5.33	0.23	0.050	(0.432)	0.025	0.025
65	5.42	0.23	0.050	(0.430)	0.025	0.025
66	5.50	0.23	0.050	(0.428)	0.025	0.025
67	5.58	0.27	0.058	(0.426)	0.029	0.029
68	5.67	0.27	0.058	(0.424)	0.029	0.029
69	5.75	0.27	0.058	(0.422)	0.029	0.029
70	5.83	0.27	0.058	(0.420)	0.029	0.029

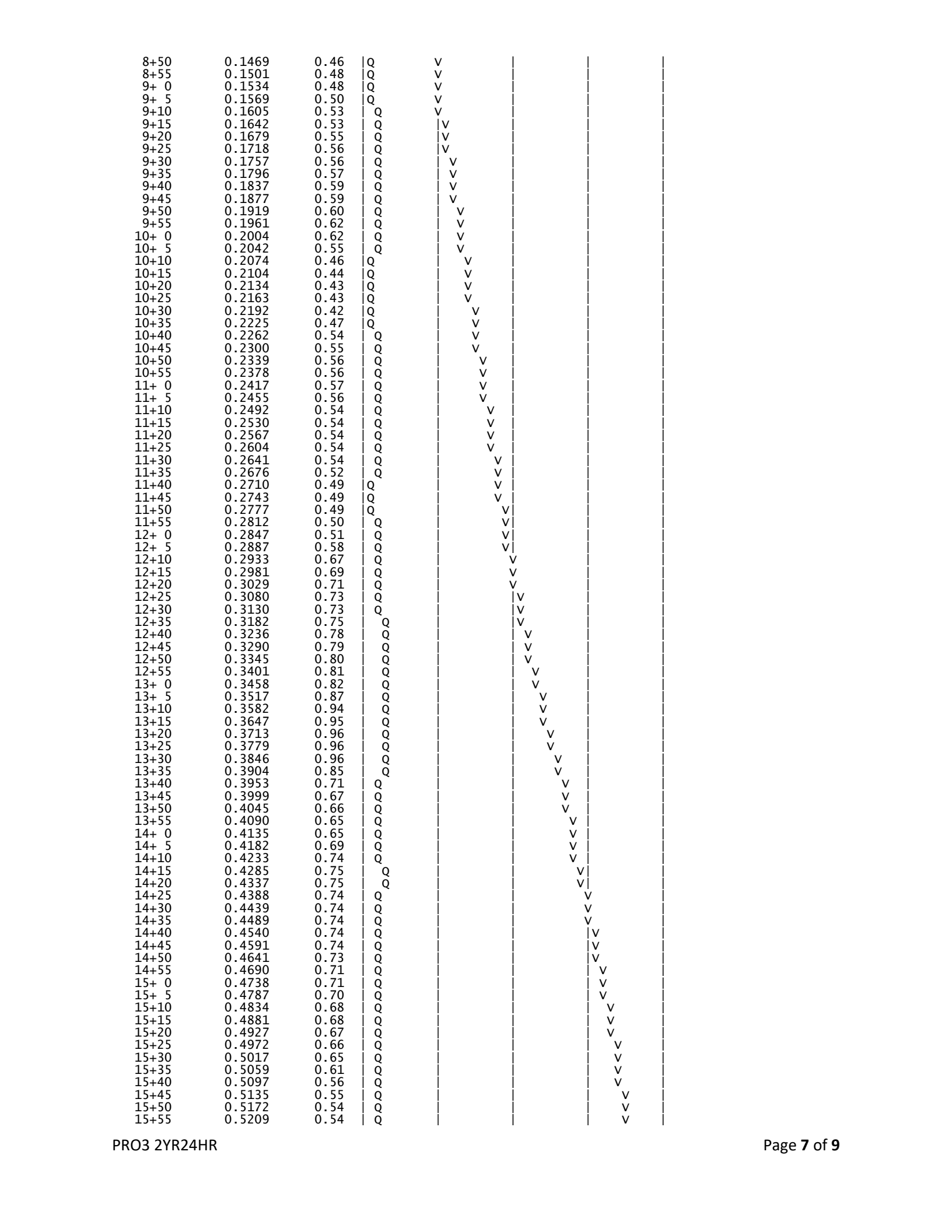
71	5.92	0.27	0.058	(0.419)	0.029	0.029
72	6.00	0.27	0.058	(0.417)	0.029	0.029
73	6.08	0.30	0.065	(0.415)	0.032	0.032
74	6.17	0.30	0.065	(0.413)	0.032	0.032
75	6.25	0.30	0.065	(0.411)	0.032	0.032
76	6.33	0.30	0.065	(0.409)	0.032	0.032
77	6.42	0.30	0.065	(0.407)	0.032	0.032
78	6.50	0.30	0.065	(0.406)	0.032	0.032
79	6.58	0.33	0.072	(0.404)	0.036	0.036
80	6.67	0.33	0.072	(0.402)	0.036	0.036
81	6.75	0.33	0.072	(0.400)	0.036	0.036
82	6.83	0.33	0.072	(0.398)	0.036	0.036
83	6.92	0.33	0.072	(0.397)	0.036	0.036
84	7.00	0.33	0.072	(0.395)	0.036	0.036
85	7.08	0.33	0.072	(0.393)	0.036	0.036
86	7.17	0.33	0.072	(0.391)	0.036	0.036
87	7.25	0.33	0.072	(0.389)	0.036	0.036
88	7.33	0.37	0.079	(0.388)	0.040	0.040
89	7.42	0.37	0.079	(0.386)	0.040	0.040
90	7.50	0.37	0.079	(0.384)	0.040	0.040
91	7.58	0.40	0.086	(0.382)	0.043	0.043
92	7.67	0.40	0.086	(0.381)	0.043	0.043
93	7.75	0.40	0.086	(0.379)	0.043	0.043
94	7.83	0.43	0.094	(0.377)	0.047	0.047
95	7.92	0.43	0.094	(0.375)	0.047	0.047
96	8.00	0.43	0.094	(0.374)	0.047	0.047
97	8.08	0.50	0.108	(0.372)	0.054	0.054
98	8.17	0.50	0.108	(0.370)	0.054	0.054
99	8.25	0.50	0.108	(0.368)	0.054	0.054
100	8.33	0.50	0.108	(0.367)	0.054	0.054
101	8.42	0.50	0.108	(0.365)	0.054	0.054
102	8.50	0.50	0.108	(0.363)	0.054	0.054
103	8.58	0.53	0.115	(0.362)	0.058	0.058
104	8.67	0.53	0.115	(0.360)	0.058	0.058
105	8.75	0.53	0.115	(0.358)	0.058	0.058
106	8.83	0.57	0.122	(0.356)	0.061	0.061
107	8.92	0.57	0.122	(0.355)	0.061	0.061
108	9.00	0.57	0.122	(0.353)	0.061	0.061
109	9.08	0.63	0.137	(0.351)	0.068	0.068
110	9.17	0.63	0.137	(0.350)	0.068	0.068
111	9.25	0.63	0.137	(0.348)	0.068	0.068
112	9.33	0.67	0.144	(0.346)	0.072	0.072
113	9.42	0.67	0.144	(0.345)	0.072	0.072
114	9.50	0.67	0.144	(0.343)	0.072	0.072
115	9.58	0.70	0.151	(0.341)	0.076	0.076
116	9.67	0.70	0.151	(0.340)	0.076	0.076
117	9.75	0.70	0.151	(0.338)	0.076	0.076
118	9.83	0.73	0.158	(0.337)	0.079	0.079
119	9.92	0.73	0.158	(0.335)	0.079	0.079
120	10.00	0.73	0.158	(0.333)	0.079	0.079
121	10.08	0.50	0.108	(0.332)	0.054	0.054
122	10.17	0.50	0.108	(0.330)	0.054	0.054
123	10.25	0.50	0.108	(0.329)	0.054	0.054
124	10.33	0.50	0.108	(0.327)	0.054	0.054
125	10.42	0.50	0.108	(0.325)	0.054	0.054
126	10.50	0.50	0.108	(0.324)	0.054	0.054
127	10.58	0.67	0.144	(0.322)	0.072	0.072
128	10.67	0.67	0.144	(0.321)	0.072	0.072
129	10.75	0.67	0.144	(0.319)	0.072	0.072
130	10.83	0.67	0.144	(0.317)	0.072	0.072
131	10.92	0.67	0.144	(0.316)	0.072	0.072
132	11.00	0.67	0.144	(0.314)	0.072	0.072
133	11.08	0.63	0.137	(0.313)	0.068	0.068
134	11.17	0.63	0.137	(0.311)	0.068	0.068
135	11.25	0.63	0.137	(0.310)	0.068	0.068
136	11.33	0.63	0.137	(0.308)	0.068	0.068
137	11.42	0.63	0.137	(0.307)	0.068	0.068
138	11.50	0.63	0.137	(0.305)	0.068	0.068
139	11.58	0.57	0.122	(0.304)	0.061	0.061
140	11.67	0.57	0.122	(0.302)	0.061	0.061
141	11.75	0.57	0.122	(0.301)	0.061	0.061
142	11.83	0.60	0.130	(0.299)	0.065	0.065
143	11.92	0.60	0.130	(0.298)	0.065	0.065
144	12.00	0.60	0.130	(0.296)	0.065	0.065
145	12.08	0.83	0.180	(0.295)	0.090	0.090
146	12.17	0.83	0.180	(0.293)	0.090	0.090
147	12.25	0.83	0.180	(0.292)	0.090	0.090
148	12.33	0.87	0.187	(0.290)	0.094	0.094
149	12.42	0.87	0.187	(0.289)	0.094	0.094
150	12.50	0.87	0.187	(0.287)	0.094	0.094
151	12.58	0.93	0.202	(0.286)	0.101	0.101
152	12.67	0.93	0.202	(0.284)	0.101	0.101
153	12.75	0.93	0.202	(0.283)	0.101	0.101
154	12.83	0.97	0.209	(0.282)	0.104	0.104
155	12.92	0.97	0.209	(0.280)	0.104	0.104
156	13.00	0.97	0.209	(0.279)	0.104	0.104

157	13.08	1.13	0.245	(0.277)	0.122	0.122
158	13.17	1.13	0.245	(0.276)	0.122	0.122
159	13.25	1.13	0.245	(0.275)	0.122	0.122
160	13.33	1.13	0.245	(0.273)	0.122	0.122
161	13.42	1.13	0.245	(0.272)	0.122	0.122
162	13.50	1.13	0.245	(0.270)	0.122	0.122
163	13.58	0.77	0.166	(0.269)	0.083	0.083
164	13.67	0.77	0.166	(0.268)	0.083	0.083
165	13.75	0.77	0.166	(0.266)	0.083	0.083
166	13.83	0.77	0.166	(0.265)	0.083	0.083
167	13.92	0.77	0.166	(0.264)	0.083	0.083
168	14.00	0.77	0.166	(0.262)	0.083	0.083
169	14.08	0.90	0.194	(0.261)	0.097	0.097
170	14.17	0.90	0.194	(0.260)	0.097	0.097
171	14.25	0.90	0.194	(0.258)	0.097	0.097
172	14.33	0.87	0.187	(0.257)	0.094	0.094
173	14.42	0.87	0.187	(0.256)	0.094	0.094
174	14.50	0.87	0.187	(0.254)	0.094	0.094
175	14.58	0.87	0.187	(0.253)	0.094	0.094
176	14.67	0.87	0.187	(0.252)	0.094	0.094
177	14.75	0.87	0.187	(0.250)	0.094	0.094
178	14.83	0.83	0.180	(0.249)	0.090	0.090
179	14.92	0.83	0.180	(0.248)	0.090	0.090
180	15.00	0.83	0.180	(0.247)	0.090	0.090
181	15.08	0.80	0.173	(0.245)	0.086	0.086
182	15.17	0.80	0.173	(0.244)	0.086	0.086
183	15.25	0.80	0.173	(0.243)	0.086	0.086
184	15.33	0.77	0.166	(0.242)	0.083	0.083
185	15.42	0.77	0.166	(0.240)	0.083	0.083
186	15.50	0.77	0.166	(0.239)	0.083	0.083
187	15.58	0.63	0.137	(0.238)	0.068	0.068
188	15.67	0.63	0.137	(0.237)	0.068	0.068
189	15.75	0.63	0.137	(0.235)	0.068	0.068
190	15.83	0.63	0.137	(0.234)	0.068	0.068
191	15.92	0.63	0.137	(0.233)	0.068	0.068
192	16.00	0.63	0.137	(0.232)	0.068	0.068
193	16.08	0.13	0.029	(0.231)	0.014	0.014
194	16.17	0.13	0.029	(0.229)	0.014	0.014
195	16.25	0.13	0.029	(0.228)	0.014	0.014
196	16.33	0.13	0.029	(0.227)	0.014	0.014
197	16.42	0.13	0.029	(0.226)	0.014	0.014
198	16.50	0.13	0.029	(0.225)	0.014	0.014
199	16.58	0.10	0.022	(0.224)	0.011	0.011
200	16.67	0.10	0.022	(0.223)	0.011	0.011
201	16.75	0.10	0.022	(0.221)	0.011	0.011
202	16.83	0.10	0.022	(0.220)	0.011	0.011
203	16.92	0.10	0.022	(0.219)	0.011	0.011
204	17.00	0.10	0.022	(0.218)	0.011	0.011
205	17.08	0.17	0.036	(0.217)	0.018	0.018
206	17.17	0.17	0.036	(0.216)	0.018	0.018
207	17.25	0.17	0.036	(0.215)	0.018	0.018
208	17.33	0.17	0.036	(0.214)	0.018	0.018
209	17.42	0.17	0.036	(0.213)	0.018	0.018
210	17.50	0.17	0.036	(0.212)	0.018	0.018
211	17.58	0.17	0.036	(0.211)	0.018	0.018
212	17.67	0.17	0.036	(0.209)	0.018	0.018
213	17.75	0.17	0.036	(0.208)	0.018	0.018
214	17.83	0.13	0.029	(0.207)	0.014	0.014
215	17.92	0.13	0.029	(0.206)	0.014	0.014
216	18.00	0.13	0.029	(0.205)	0.014	0.014
217	18.08	0.13	0.029	(0.204)	0.014	0.014
218	18.17	0.13	0.029	(0.203)	0.014	0.014
219	18.25	0.13	0.029	(0.202)	0.014	0.014
220	18.33	0.13	0.029	(0.201)	0.014	0.014
221	18.42	0.13	0.029	(0.200)	0.014	0.014
222	18.50	0.13	0.029	(0.199)	0.014	0.014
223	18.58	0.10	0.022	(0.198)	0.011	0.011
224	18.67	0.10	0.022	(0.197)	0.011	0.011
225	18.75	0.10	0.022	(0.197)	0.011	0.011
226	18.83	0.07	0.014	(0.196)	0.007	0.007
227	18.92	0.07	0.014	(0.195)	0.007	0.007
228	19.00	0.07	0.014	(0.194)	0.007	0.007
229	19.08	0.10	0.022	(0.193)	0.011	0.011
230	19.17	0.10	0.022	(0.192)	0.011	0.011
231	19.25	0.10	0.022	(0.191)	0.011	0.011
232	19.33	0.13	0.029	(0.190)	0.014	0.014
233	19.42	0.13	0.029	(0.189)	0.014	0.014
234	19.50	0.13	0.029	(0.188)	0.014	0.014
235	19.58	0.10	0.022	(0.187)	0.011	0.011
236	19.67	0.10	0.022	(0.187)	0.011	0.011
237	19.75	0.10	0.022	(0.186)	0.011	0.011
238	19.83	0.07	0.014	(0.185)	0.007	0.007
239	19.92	0.07	0.014	(0.184)	0.007	0.007
240	20.00	0.07	0.014	(0.183)	0.007	0.007
241	20.08	0.10	0.022	(0.182)	0.011	0.011
242	20.17	0.10	0.022	(0.182)	0.011	0.011

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243  20.25     0.10      0.022       (  0.181)       0.011        0.011
244  20.33     0.10      0.022       (  0.180)       0.011        0.011
245  20.42     0.10      0.022       (  0.179)       0.011        0.011
246  20.50     0.10      0.022       (  0.179)       0.011        0.011
247  20.58     0.10      0.022       (  0.178)       0.011        0.011
248  20.67     0.10      0.022       (  0.177)       0.011        0.011
249  20.75     0.10      0.022       (  0.176)       0.011        0.011
250  20.83     0.07      0.014       (  0.176)       0.007        0.007
251  20.92     0.07      0.014       (  0.175)       0.007        0.007
252  21.00     0.07      0.014       (  0.174)       0.007        0.007
253  21.08     0.10      0.022       (  0.174)       0.011        0.011
254  21.17     0.10      0.022       (  0.173)       0.011        0.011
255  21.25     0.10      0.022       (  0.172)       0.011        0.011
256  21.33     0.07      0.014       (  0.172)       0.007        0.007
257  21.42     0.07      0.014       (  0.171)       0.007        0.007
258  21.50     0.07      0.014       (  0.170)       0.007        0.007
259  21.58     0.10      0.022       (  0.170)       0.011        0.011
260  21.67     0.10      0.022       (  0.169)       0.011        0.011
261  21.75     0.10      0.022       (  0.168)       0.011        0.011
262  21.83     0.07      0.014       (  0.168)       0.007        0.007
263  21.92     0.07      0.014       (  0.167)       0.007        0.007
264  22.00     0.07      0.014       (  0.167)       0.007        0.007
265  22.08     0.10      0.022       (  0.166)       0.011        0.011
266  22.17     0.10      0.022       (  0.166)       0.011        0.011
267  22.25     0.10      0.022       (  0.165)       0.011        0.011
268  22.33     0.07      0.014       (  0.165)       0.007        0.007
269  22.42     0.07      0.014       (  0.164)       0.007        0.007
270  22.50     0.07      0.014       (  0.164)       0.007        0.007
271  22.58     0.07      0.014       (  0.163)       0.007        0.007
272  22.67     0.07      0.014       (  0.163)       0.007        0.007
273  22.75     0.07      0.014       (  0.162)       0.007        0.007
274  22.83     0.07      0.014       (  0.162)       0.007        0.007
275  22.92     0.07      0.014       (  0.161)       0.007        0.007
276  23.00     0.07      0.014       (  0.161)       0.007        0.007
277  23.08     0.07      0.014       (  0.161)       0.007        0.007
278  23.17     0.07      0.014       (  0.160)       0.007        0.007
279  23.25     0.07      0.014       (  0.160)       0.007        0.007
280  23.33     0.07      0.014       (  0.160)       0.007        0.007
281  23.42     0.07      0.014       (  0.159)       0.007        0.007
282  23.50     0.07      0.014       (  0.159)       0.007        0.007
283  23.58     0.07      0.014       (  0.159)       0.007        0.007
284  23.67     0.07      0.014       (  0.158)       0.007        0.007
285  23.75     0.07      0.014       (  0.158)       0.007        0.007
286  23.83     0.07      0.014       (  0.158)       0.007        0.007
287  23.92     0.07      0.014       (  0.158)       0.007        0.007
288  24.00     0.07      0.014       (  0.158)       0.007        0.007
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    10.8
      Flood volume = Effective rainfall      0.90(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       0.6(Ac.Ft)
      Total soil loss =      0.90(In)
      Total soil loss =     0.584(Ac.Ft)
      Total rainfall =      1.80(In)
      Flood volume =       25449.5 Cubic Feet
      Total soil loss =       25449.5 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      0.961(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0001      0.02  Q          |         |         |         |
   0+10       0.0005      0.05  Q          |         |         |         |
   0+15       0.0008      0.05  Q          |         |         |         |
   0+20       0.0013      0.06  Q          |         |         |         |
   0+25       0.0018      0.08  Q          |         |         |         |
   0+30       0.0024      0.08  Q          |         |         |         |
   0+35       0.0030      0.08  Q          |         |         |         |
   0+40       0.0035      0.08  Q          |         |         |         |
   0+45       0.0041      0.08  Q          |         |         |         |
   0+50       0.0048      0.09  Q          |         |         |         |
   0+55       0.0055      0.11  Q          |         |         |         |
   1+ 0       0.0063      0.11  Q          |         |         |         |
   1+ 5       0.0070      0.10  Q          |         |         |         |
   1+10       0.0076      0.09  Q          |         |         |         |
   1+15       0.0082      0.09  Q          |         |         |         |
   1+20       0.0088      0.09  Q          |         |         |         |
   1+25       0.0094      0.09  Q          |         |         |         |
   1+30       0.0100      0.08  Q          |         |         |         |
   1+35       0.0105      0.08  Q          |         |         |         |
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1+40      0.0111      0.08  Q          |          |          |          |
1+45      0.0117      0.08  Q          |          |          |          |
1+50      0.0124      0.09  Q          |          |          |          |
1+55      0.0131      0.11  Q          |          |          |          |
2+ 0      0.0139      0.11  Q          |          |          |          |
2+ 5      0.0146      0.11  QV         |          |          |          |
2+10      0.0154      0.11  QV         |          |          |          |
2+15      0.0162      0.11  QV         |          |          |          |
2+20      0.0170      0.11  QV         |          |          |          |
2+25      0.0178      0.11  QV         |          |          |          |
2+30      0.0185      0.11  QV         |          |          |          |
2+35      0.0194      0.12  QV         |          |          |          |
2+40      0.0203      0.14  QV         |          |          |          |
2+45      0.0213      0.14  QV         |          |          |          |
2+50      0.0222      0.14  QV         |          |          |          |
2+55      0.0232      0.14  QV         |          |          |          |
3+ 0      0.0242      0.14  QV         |          |          |          |
3+ 5      0.0252      0.14  QV         |          |          |          |
3+10      0.0261      0.14  QV         |          |          |          |
3+15      0.0271      0.14  QV         |          |          |          |
3+20      0.0281      0.14  QV         |          |          |          |
3+25      0.0291      0.14  QV         |          |          |          |
3+30      0.0300      0.14  Q V        |          |          |          |
3+35      0.0310      0.14  Q V        |          |          |          |
3+40      0.0320      0.14  Q V        |          |          |          |
3+45      0.0330      0.14  Q V        |          |          |          |
3+50      0.0340      0.15  Q V        |          |          |          |
3+55      0.0351      0.16  Q V        |          |          |          |
4+ 0      0.0363      0.17  Q V        |          |          |          |
4+ 5      0.0374      0.17  Q V        |          |          |          |
4+10      0.0386      0.17  Q V        |          |          |          |
4+15      0.0398      0.17  Q V        |          |          |          |
4+20      0.0410      0.18  Q V        |          |          |          |
4+25      0.0423      0.19  Q V        |          |          |          |
4+30      0.0437      0.20  Q V        |          |          |          |
4+35      0.0451      0.20  Q  V       |          |          |          |
4+40      0.0464      0.20  Q  V       |          |          |          |
4+45      0.0478      0.20  Q  V       |          |          |          |
4+50      0.0492      0.21  Q  V       |          |          |          |
4+55      0.0507      0.22  Q  V       |          |          |          |
5+ 0      0.0523      0.22  Q  V       |          |          |          |
5+ 5      0.0537      0.21  Q  V       |          |          |          |
5+10      0.0549      0.18  Q  V       |          |          |          |
5+15      0.0561      0.17  Q  V       |          |          |          |
5+20      0.0574      0.18  Q  V       |          |          |          |
5+25      0.0587      0.19  Q   V      |          |          |          |
5+30      0.0601      0.20  Q   V      |          |          |          |
5+35      0.0615      0.21  Q   V      |          |          |          |
5+40      0.0630      0.22  Q   V      |          |          |          |
5+45      0.0645      0.22  Q   V      |          |          |          |
5+50      0.0661      0.23  Q   V      |          |          |          |
5+55      0.0677      0.23  Q   V      |          |          |          |
6+ 0      0.0692      0.23  Q   V      |          |          |          |
6+ 5      0.0708      0.24  Q   V      |          |          |          |
6+10      0.0726      0.25  Q   V      |          |          |          |
6+15      0.0743      0.25  |Q   V      |          |          |          |
6+20      0.0760      0.25  |Q   V      |          |          |          |
6+25      0.0778      0.25  |Q   V      |          |          |          |
6+30      0.0795      0.25  |Q   V      |          |          |          |
6+35      0.0814      0.26  |Q   V      |          |          |          |
6+40      0.0833      0.28  |Q   V      |          |          |          |
6+45      0.0852      0.28  |Q   V      |          |          |          |
6+50      0.0871      0.28  |Q   V      |          |          |          |
6+55      0.0891      0.28  |Q    V     |          |          |          |
7+ 0      0.0910      0.28  |Q    V     |          |          |          |
7+ 5      0.0930      0.28  |Q    V     |          |          |          |
7+10      0.0949      0.28  |Q    V     |          |          |          |
7+15      0.0969      0.28  |Q    V     |          |          |          |
7+20      0.0989      0.29  |Q    V     |          |          |          |
7+25      0.1010      0.31  |Q    V     |          |          |          |
7+30      0.1031      0.31  |Q     V    |          |          |          |
7+35      0.1053      0.32  |Q     V    |          |          |          |
7+40      0.1076      0.33  |Q     V    |          |          |          |
7+45      0.1100      0.34  |Q     V    |          |          |          |
7+50      0.1124      0.35  |Q     V    |          |          |          |
7+55      0.1148      0.36  |Q     V    |          |          |          |
8+ 0      0.1174      0.37  |Q      V   |          |          |          |
8+ 5      0.1200      0.39  |Q      V   |          |          |          |
8+10      0.1229      0.41  |Q      V   |          |          |          |
8+15      0.1258      0.42  |Q      V   |          |          |          |
8+20      0.1287      0.42  |Q      V   |          |          |          |
8+25      0.1316      0.42  |Q       V  |          |          |          |
8+30      0.1345      0.42  |Q       V  |          |          |          |
8+35      0.1375      0.43  |Q       V  |          |          |          |
8+40      0.1406      0.45  |Q       V  |          |          |          |
8+45      0.1437      0.45  |Q       V  |          |          |          |
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8+50	0.1469	0.46	
8+55	0.1501	0.48	
9+ 0	0.1534	0.48	
9+ 5	0.1569	0.50	
9+10	0.1605	0.53	
9+15	0.1642	0.53	
9+20	0.1679	0.55	
9+25	0.1718	0.56	
9+30	0.1757	0.56	
9+35	0.1796	0.57	
9+40	0.1837	0.59	
9+45	0.1877	0.59	
9+50	0.1919	0.60	
9+55	0.1961	0.62	
10+ 0	0.2004	0.62	
10+ 5	0.2042	0.55	
10+10	0.2074	0.46	
10+15	0.2104	0.44	
10+20	0.2134	0.43	
10+25	0.2163	0.43	
10+30	0.2192	0.42	
10+35	0.2225	0.47	
10+40	0.2262	0.54	
10+45	0.2300	0.55	
10+50	0.2339	0.56	
10+55	0.2378	0.56	
11+ 0	0.2417	0.57	
11+ 5	0.2455	0.56	
11+10	0.2492	0.54	
11+15	0.2530	0.54	
11+20	0.2567	0.54	
11+25	0.2604	0.54	
11+30	0.2641	0.54	
11+35	0.2676	0.52	
11+40	0.2710	0.49	
11+45	0.2743	0.49	
11+50	0.2777	0.49	
11+55	0.2812	0.50	
12+ 0	0.2847	0.51	
12+ 5	0.2887	0.58	
12+10	0.2933	0.67	
12+15	0.2981	0.69	
12+20	0.3029	0.71	
12+25	0.3080	0.73	
12+30	0.3130	0.73	
12+35	0.3182	0.75	
12+40	0.3236	0.78	
12+45	0.3290	0.79	
12+50	0.3345	0.80	
12+55	0.3401	0.81	
13+ 0	0.3458	0.82	
13+ 5	0.3517	0.87	
13+10	0.3582	0.94	
13+15	0.3647	0.95	
13+20	0.3713	0.96	
13+25	0.3779	0.96	
13+30	0.3846	0.96	
13+35	0.3904	0.85	
13+40	0.3953	0.71	
13+45	0.3999	0.67	
13+50	0.4045	0.66	
13+55	0.4090	0.65	
14+ 0	0.4135	0.65	
14+ 5	0.4182	0.69	
14+10	0.4233	0.74	
14+15	0.4285	0.75	
14+20	0.4337	0.75	
14+25	0.4388	0.74	
14+30	0.4439	0.74	
14+35	0.4489	0.74	
14+40	0.4540	0.74	
14+45	0.4591	0.74	
14+50	0.4641	0.73	
14+55	0.4690	0.71	
15+ 0	0.4738	0.71	
15+ 5	0.4787	0.70	
15+10	0.4834	0.68	
15+15	0.4881	0.68	
15+20	0.4927	0.67	
15+25	0.4972	0.66	
15+30	0.5017	0.65	
15+35	0.5059	0.61	
15+40	0.5097	0.56	
15+45	0.5135	0.55	
15+50	0.5172	0.54	
15+55	0.5209	0.54	

```
16+ 0       0.5246      0.54  | Q       |         |         |     V     |
16+ 5       0.5273      0.39  |Q        |         |         |      V    |
16+10       0.5286      0.19  Q         |         |         |      V    |
16+15       0.5296      0.15  Q         |         |         |      V    |
16+20       0.5305      0.13  Q         |         |         |      V    |
16+25       0.5313      0.12  Q         |         |         |      V    |
16+30       0.5321      0.11  Q         |         |         |      V    |
16+35       0.5328      0.10  Q         |         |         |      V    |
16+40       0.5334      0.09  Q         |         |         |      V    |
16+45       0.5340      0.09  Q         |         |         |      V    |
16+50       0.5346      0.09  Q         |         |         |      V    |
16+55       0.5352      0.09  Q         |         |         |      V    |
17+ 0       0.5358      0.08  Q         |         |         |      V    |
17+ 5       0.5365      0.10  Q         |         |         |      V    |
17+10       0.5374      0.13  Q         |         |         |      V    |
17+15       0.5383      0.14  Q         |         |         |      V    |
17+20       0.5393      0.14  Q         |         |         |      V    |
17+25       0.5403      0.14  Q         |         |         |      V    |
17+30       0.5412      0.14  Q         |         |         |       V   |
17+35       0.5422      0.14  Q         |         |         |       V   |
17+40       0.5432      0.14  Q         |         |         |       V   |
17+45       0.5442      0.14  Q         |         |         |       V   |
17+50       0.5451      0.13  Q         |         |         |       V   |
17+55       0.5459      0.12  Q         |         |         |       V   |
18+ 0       0.5467      0.12  Q         |         |         |       V   |
18+ 5       0.5475      0.11  Q         |         |         |       V   |
18+10       0.5483      0.11  Q         |         |         |       V   |
18+15       0.5490      0.11  Q         |         |         |       V   |
18+20       0.5498      0.11  Q         |         |         |       V   |
18+25       0.5506      0.11  Q         |         |         |       V   |
18+30       0.5514      0.11  Q         |         |         |       V   |
18+35       0.5521      0.10  Q         |         |         |       V   |
18+40       0.5527      0.09  Q         |         |         |       V   |
18+45       0.5533      0.09  Q         |         |         |       V   |
18+50       0.5538      0.08  Q         |         |         |       V   |
18+55       0.5542      0.06  Q         |         |         |       V   |
19+ 0       0.5547      0.06  Q         |         |         |       V   |
19+ 5       0.5551      0.07  Q         |         |         |        V  |
19+10       0.5557      0.08  Q         |         |         |        V  |
19+15       0.5562      0.08  Q         |         |         |        V  |
19+20       0.5569      0.09  Q         |         |         |        V  |
19+25       0.5576      0.11  Q         |         |         |        V  |
19+30       0.5584      0.11  Q         |         |         |        V  |
19+35       0.5591      0.10  Q         |         |         |        V  |
19+40       0.5597      0.09  Q         |         |         |        V  |
19+45       0.5603      0.09  Q         |         |         |        V  |
19+50       0.5608      0.08  Q         |         |         |        V  |
19+55       0.5613      0.06  Q         |         |         |        V  |
20+ 0       0.5617      0.06  Q         |         |         |        V  |
20+ 5       0.5621      0.07  Q         |         |         |        V  |
20+10       0.5627      0.08  Q         |         |         |        V  |
20+15       0.5632      0.08  Q         |         |         |        V  |
20+20       0.5638      0.08  Q         |         |         |        V  |
20+25       0.5644      0.08  Q         |         |         |        V  |
20+30       0.5650      0.08  Q         |         |         |        V  |
20+35       0.5656      0.08  Q         |         |         |        V  |
20+40       0.5662      0.08  Q         |         |         |        V  |
20+45       0.5667      0.08  Q         |         |         |        V  |
20+50       0.5673      0.07  Q         |         |         |        V  |
20+55       0.5677      0.06  Q         |         |         |        V  |
21+ 0       0.5681      0.06  Q         |         |         |        V  |
21+ 5       0.5686      0.07  Q         |         |         |        V  |
21+10       0.5691      0.08  Q         |         |         |        V  |
21+15       0.5697      0.08  Q         |         |         |         V |
21+20       0.5702      0.07  Q         |         |         |         V |
21+25       0.5706      0.06  Q         |         |         |         V |
21+30       0.5710      0.06  Q         |         |         |         V |
21+35       0.5715      0.07  Q         |         |         |         V |
21+40       0.5720      0.08  Q         |         |         |         V |
21+45       0.5726      0.08  Q         |         |         |         V |
21+50       0.5731      0.07  Q         |         |         |         V |
21+55       0.5735      0.06  Q         |         |         |         V |
22+ 0       0.5739      0.06  Q         |         |         |         V |
22+ 5       0.5744      0.07  Q         |         |         |         V |
22+10       0.5749      0.08  Q         |         |         |         V |
22+15       0.5755      0.08  Q         |         |         |         V |
22+20       0.5760      0.07  Q         |         |         |         V |
22+25       0.5764      0.06  Q         |         |         |         V |
22+30       0.5769      0.06  Q         |         |         |         V |
22+35       0.5772      0.06  Q         |         |         |         V |
22+40       0.5776      0.06  Q         |         |         |         V |
22+45       0.5780      0.06  Q         |         |         |         V |
22+50       0.5784      0.06  Q         |         |         |         V |
22+55       0.5788      0.06  Q         |         |         |         V |
23+ 0       0.5792      0.06  Q         |         |         |         V |
23+ 5       0.5796      0.06  Q         |         |         |         V |
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   23+10       0.5800      0.06  Q          |          |          |         v|
   23+15       0.5804      0.06  Q          |          |          |         v|
   23+20       0.5808      0.06  Q          |          |          |         v|
   23+25       0.5811      0.06  Q          |          |          |         v|
   23+30       0.5815      0.06  Q          |          |          |         v|
   23+35       0.5819      0.06  Q          |          |          |         v|
   23+40       0.5823      0.06  Q          |          |          |         v|
   23+45       0.5827      0.06  Q          |          |          |         v|
   23+50       0.5831      0.06  Q          |          |          |         v|
   23+55       0.5835      0.06  Q          |          |          |         v|
   24+ 0       0.5839      0.06  Q          |          |          |         v|
   24+ 5       0.5841      0.04  Q          |          |          |         v|
   24+10       0.5842      0.01  Q          |          |          |         v|
   24+15       0.5842      0.00  Q          |          |          |         v|
   24+20       0.5842      0.00  Q          |          |          |         v|
   24+25       0.5842      0.00  Q          |          |          |          v
---------------------------------------------------------------------------
```

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro3515.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 2225.00(Ft.)
Length along longest watercourse measured to centroid = 1113.00(Ft.)
Length along longest watercourse = 0.421 Mi.
Length along longest watercourse measured to centroid = 0.211 Mi.
Difference in elevation = 82.00(Ft.)
Slope along watercourse = 194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	0.50	3.90

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.30	10.13

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 0.500(In)
Area Averaged 100-Year Rainfall = 1.300(In)

Point rain (area averaged) = 0.687(In)
Areal adjustment factor = 99.99 %
Adjusted average point rain = 0.687(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	69.00	0.500

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

Slope of intensity-duration curve for a 1 hour storm =0.5500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
		Sum = 100.000	Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.272	(0.316)	0.136	0.136
2	0.17	4.20	0.346	(0.316)	0.173	0.173
3	0.25	4.40	0.363	(0.316)	0.181	0.181
4	0.33	4.80	0.396	(0.316)	0.198	0.198
5	0.42	5.20	0.429	(0.316)	0.214	0.214
6	0.50	6.20	0.511	(0.316)	0.256	0.256
7	0.58	6.80	0.561	(0.316)	0.280	0.280
8	0.67	8.80	0.726	0.316	(0.363)	0.410
9	0.75	13.90	1.146	0.316	(0.573)	0.831
10	0.83	31.40	2.590	0.316	(1.295)	2.274
11	0.92	7.20	0.594	(0.316)	0.297	0.297
12	1.00	3.80	0.313	(0.316)	0.157	0.157
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	5.4

Flood volume = Effective rainfall 0.45(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.3(Ac.Ft)
Total soil loss = 0.24(In)
Total soil loss = 0.154(Ac.Ft)
Total rainfall = 0.69(In)
Flood volume = 12743.9 Cubic Feet
Total soil loss = 6692.3 Cubic Feet

Peak flow rate of this hydrograph = 10.025(CFS)

++

1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0026	0.38	Q				
0+10	0.0093	0.97	Q				
0+15	0.0179	1.25	Q				
0+20	0.0275	1.40	QV				
0+25	0.0382	1.55	Q V				
0+30	0.0503	1.76	Q V				
0+35	0.0641	2.00	Q V				
0+40	0.0813	2.49	Q	V			
0+45	0.1100	4.17	Q	V			
0+50	0.1775	9.80		Q	V		
0+55	0.2466	10.03		Q		V	
1+ 0	0.2729	3.83	Q			V	
1+ 5	0.2855	1.83	Q			V	
1+10	0.2903	0.70	Q			V	
1+15	0.2922	0.27	Q			V	
1+20	0.2925	0.05	Q			V	
1+25	0.2926	0.01	Q			V	

```
        U n i t   H y d r o g r a p h   A n a l y s i s

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                Study date  04/22/24 File: pro3535.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =       7.79(Ac.)  =      0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =       7.79(Ac.)  =      0.012 Sq. Mi.
Length along longest watercourse =    2225.00(Ft.)
Length along longest watercourse measured to centroid =    1113.00(Ft.)
Length along longest watercourse =      0.421 Mi.
Length along longest watercourse measured to centroid =      0.211 Mi.
Difference in elevation =      82.00(Ft.)
Slope along watercourse =    194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.053 Hr.
Lag time =     3.16 Min.
25% of lag time =     0.79 Min.
40% of lag time =     1.26 Min.
Unit time =     5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            0.80                 6.23

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            2.00                15.58

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    0.800(In)
Area Averaged 100-Year Rainfall =    2.000(In)

Point rain (area averaged) =    1.081(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    1.081(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     7.790           69.00          0.500
 Total Area Entered =      7.79(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  49.8      0.574     0.500        0.316       1.000      0.316
                                                 Sum (F) =   0.316
Area averaged mean soil loss (F) (In/Hr) =  0.316
Minimum soil loss rate ((In/Hr)) =  0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
			Sum = 100.000 Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.169	(0.316)	0.084	0.084
2	0.17	1.30	0.169	(0.316)	0.084	0.084
3	0.25	1.10	0.143	(0.316)	0.071	0.071
4	0.33	1.50	0.195	(0.316)	0.097	0.097
5	0.42	1.50	0.195	(0.316)	0.097	0.097
6	0.50	1.80	0.234	(0.316)	0.117	0.117
7	0.58	1.50	0.195	(0.316)	0.097	0.097
8	0.67	1.80	0.234	(0.316)	0.117	0.117
9	0.75	1.80	0.234	(0.316)	0.117	0.117
10	0.83	1.50	0.195	(0.316)	0.097	0.097
11	0.92	1.60	0.208	(0.316)	0.104	0.104
12	1.00	1.80	0.234	(0.316)	0.117	0.117
13	1.08	2.20	0.285	(0.316)	0.143	0.143
14	1.17	2.20	0.285	(0.316)	0.143	0.143
15	1.25	2.20	0.285	(0.316)	0.143	0.143
16	1.33	2.00	0.259	(0.316)	0.130	0.130
17	1.42	2.60	0.337	(0.316)	0.169	0.169
18	1.50	2.70	0.350	(0.316)	0.175	0.175
19	1.58	2.40	0.311	(0.316)	0.156	0.156
20	1.67	2.70	0.350	(0.316)	0.175	0.175
21	1.75	3.30	0.428	(0.316)	0.214	0.214
22	1.83	3.10	0.402	(0.316)	0.201	0.201
23	1.92	2.90	0.376	(0.316)	0.188	0.188
24	2.00	3.00	0.389	(0.316)	0.195	0.195
25	2.08	3.10	0.402	(0.316)	0.201	0.201
26	2.17	4.20	0.545	(0.316)	0.272	0.272
27	2.25	5.00	0.649	0.316	(0.324)	0.333
28	2.33	3.50	0.454	(0.316)	0.227	0.227
29	2.42	6.80	0.882	0.316	(0.441)	0.566
30	2.50	7.30	0.947	0.316	(0.473)	0.631
31	2.58	8.20	1.064	0.316	(0.532)	0.748
32	2.67	5.90	0.765	0.316	(0.383)	0.450
33	2.75	2.00	0.259	(0.316)	0.130	0.130
34	2.83	1.80	0.234	(0.316)	0.117	0.117
35	2.92	1.80	0.234	(0.316)	0.117	0.117
36	3.00	0.60	0.078	(0.316)	0.039	0.039
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	7.1

Flood volume = Effective rainfall 0.59(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.4(Ac.Ft)
Total soil loss = 0.49(In)
Total soil loss = 0.320(Ac.Ft)
Total rainfall = 1.08(In)
Flood volume = 16639.6 Cubic Feet
Total soil loss = 13929.5 Cubic Feet

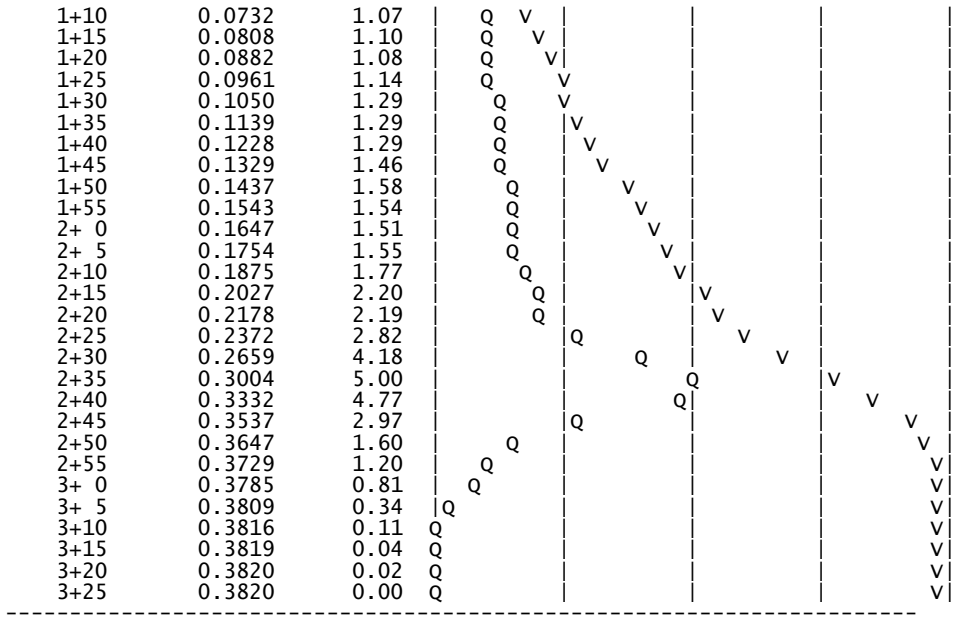
Peak flow rate of this hydrograph = 5.001(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0016	0.23	Q	|	|	|	|
0+10	0.0053	0.54	V Q	|	|	|	|
0+15	0.0093	0.58	V Q	|	|	|	|
0+20	0.0136	0.63	|VQ	|	|	|	|
0+25	0.0186	0.73	|VQ	|	|	|	|
0+30	0.0242	0.81	| VQ	|	|	|	|
0+35	0.0299	0.83	| Q	|	|	|	|
0+40	0.0356	0.83	| Q	|	|	|	|
0+45	0.0418	0.90	| QV	|	|	|	|
0+50	0.0477	0.86	| QV	|	|	|	|
0+55	0.0532	0.81	| Q V	|	|	|	|
1+ 0	0.0591	0.85	| Q V	|	|	|	|
1+ 5	0.0658	0.97	| Q V	|	|	|	|


1+10 0.0732 1.07
1+15 0.0808 1.10
1+20 0.0882 1.08
1+25 0.0961 1.14
1+30 0.1050 1.29
1+35 0.1139 1.29
1+40 0.1228 1.29
1+45 0.1329 1.46
1+50 0.1437 1.58
1+55 0.1543 1.54
2+ 0 0.1647 1.51
2+ 5 0.1754 1.55
2+10 0.1875 1.77
2+15 0.2027 2.20
2+20 0.2178 2.19
2+25 0.2372 2.82
2+30 0.2659 4.18
2+35 0.3004 5.00
2+40 0.3332 4.77
2+45 0.3537 2.97
2+50 0.3647 1.60
2+55 0.3729 1.20
3+ 0 0.3785 0.81
3+ 5 0.3809 0.34
3+10 0.3816 0.11
3+15 0.3819 0.04
3+20 0.3820 0.02
3+25 0.3820 0.00

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro3565.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 2225.00(Ft.)
Length along longest watercourse measured to centroid = 1113.00(Ft.)
Length along longest watercourse = 0.421 Mi.
Length along longest watercourse measured to centroid = 0.211 Mi.
Difference in elevation = 82.00(Ft.)
Slope along watercourse = 194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.10	8.57

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	3.00	23.37

STORM EVENT (YEAR) = 5.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.545(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.545(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	69.00	0.500

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-1	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	49.8	0.574	0.500	0.316	1.000	0.316
					Sum (F) =	0.316

Area averaged mean soil loss (F) (In/Hr) = 0.316
Minimum soil loss rate ((In/Hr)) = 0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

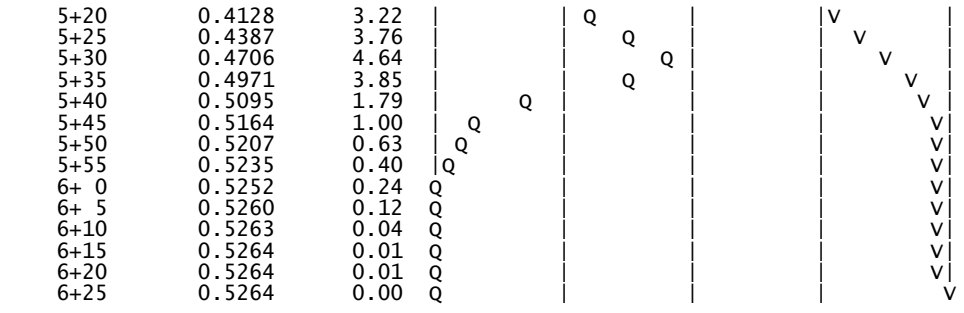
1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
			Sum = 100.000	Sum= 7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.093	(0.316)	0.046	0.046
2	0.17	0.60	0.111	(0.316)	0.056	0.056
3	0.25	0.60	0.111	(0.316)	0.056	0.056
4	0.33	0.60	0.111	(0.316)	0.056	0.056
5	0.42	0.60	0.111	(0.316)	0.056	0.056
6	0.50	0.70	0.130	(0.316)	0.065	0.065
7	0.58	0.70	0.130	(0.316)	0.065	0.065
8	0.67	0.70	0.130	(0.316)	0.065	0.065
9	0.75	0.70	0.130	(0.316)	0.065	0.065
10	0.83	0.70	0.130	(0.316)	0.065	0.065
11	0.92	0.70	0.130	(0.316)	0.065	0.065
12	1.00	0.80	0.148	(0.316)	0.074	0.074
13	1.08	0.80	0.148	(0.316)	0.074	0.074
14	1.17	0.80	0.148	(0.316)	0.074	0.074
15	1.25	0.80	0.148	(0.316)	0.074	0.074
16	1.33	0.80	0.148	(0.316)	0.074	0.074
17	1.42	0.80	0.148	(0.316)	0.074	0.074
18	1.50	0.80	0.148	(0.316)	0.074	0.074
19	1.58	0.80	0.148	(0.316)	0.074	0.074
20	1.67	0.80	0.148	(0.316)	0.074	0.074
21	1.75	0.80	0.148	(0.316)	0.074	0.074
22	1.83	0.80	0.148	(0.316)	0.074	0.074
23	1.92	0.80	0.148	(0.316)	0.074	0.074
24	2.00	0.90	0.167	(0.316)	0.083	0.083
25	2.08	0.80	0.148	(0.316)	0.074	0.074
26	2.17	0.90	0.167	(0.316)	0.083	0.083
27	2.25	0.90	0.167	(0.316)	0.083	0.083
28	2.33	0.90	0.167	(0.316)	0.083	0.083
29	2.42	0.90	0.167	(0.316)	0.083	0.083
30	2.50	0.90	0.167	(0.316)	0.083	0.083
31	2.58	0.90	0.167	(0.316)	0.083	0.083
32	2.67	0.90	0.167	(0.316)	0.083	0.083
33	2.75	1.00	0.185	(0.316)	0.093	0.093
34	2.83	1.00	0.185	(0.316)	0.093	0.093
35	2.92	1.00	0.185	(0.316)	0.093	0.093
36	3.00	1.00	0.185	(0.316)	0.093	0.093
37	3.08	1.00	0.185	(0.316)	0.093	0.093
38	3.17	1.10	0.204	(0.316)	0.102	0.102
39	3.25	1.10	0.204	(0.316)	0.102	0.102
40	3.33	1.10	0.204	(0.316)	0.102	0.102
41	3.42	1.20	0.222	(0.316)	0.111	0.111
42	3.50	1.30	0.241	(0.316)	0.121	0.121
43	3.58	1.40	0.260	(0.316)	0.130	0.130
44	3.67	1.40	0.260	(0.316)	0.130	0.130
45	3.75	1.50	0.278	(0.316)	0.139	0.139
46	3.83	1.50	0.278	(0.316)	0.139	0.139
47	3.92	1.60	0.297	(0.316)	0.148	0.148
48	4.00	1.60	0.297	(0.316)	0.148	0.148
49	4.08	1.70	0.315	(0.316)	0.158	0.158
50	4.17	1.80	0.334	(0.316)	0.167	0.167
51	4.25	1.90	0.352	(0.316)	0.176	0.176
52	4.33	2.00	0.371	(0.316)	0.185	0.185
53	4.42	2.10	0.389	(0.316)	0.195	0.195
54	4.50	2.10	0.389	(0.316)	0.195	0.195
55	4.58	2.20	0.408	(0.316)	0.204	0.204
56	4.67	2.30	0.426	(0.316)	0.213	0.213
57	4.75	2.40	0.445	(0.316)	0.222	0.222
58	4.83	2.40	0.445	(0.316)	0.222	0.222
59	4.92	2.50	0.463	(0.316)	0.232	0.232
60	5.00	2.60	0.482	(0.316)	0.241	0.241
61	5.08	3.10	0.575	(0.316)	0.287	0.287
62	5.17	3.60	0.667	0.316	(0.334)	0.352
63	5.25	3.90	0.723	0.316	(0.362)	0.407
64	5.33	4.20	0.779	0.316	(0.389)	0.463
65	5.42	4.70	0.871	0.316	(0.436)	0.556
66	5.50	5.60	1.038	0.316	(0.519)	0.723
67	5.58	1.90	0.352	(0.316)	0.176	0.176
68	5.67	0.90	0.167	(0.316)	0.083	0.083
69	5.75	0.60	0.111	(0.316)	0.056	0.056
70	5.83	0.50	0.093	(0.316)	0.046	0.046

```
71   5.92     0.30      0.056       (  0.316)       0.028        0.028
72   6.00     0.20      0.037       (  0.316)       0.019        0.019
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =     9.7
      Flood volume = Effective rainfall      0.81(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       0.5(Ac.Ft)
      Total soil loss =      0.73(In)
      Total soil loss =     0.477(Ac.Ft)
      Total rainfall =      1.54(In)
      Flood volume =       22930.6 Cubic Feet
      Total soil loss =       20758.0 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      4.638(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f     H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0009      0.13  Q         |         |         |         |
  0+10       0.0031      0.32  VQ        |         |         |         |
  0+15       0.0058      0.40  VQ        |         |         |         |
  0+20       0.0087      0.42  VQ        |         |         |         |
  0+25       0.0117      0.43  VQ        |         |         |         |
  0+30       0.0149      0.46  |Q        |         |         |         |
  0+35       0.0183      0.50  |Q        |         |         |         |
  0+40       0.0218      0.50  |VQ       |         |         |         |
  0+45       0.0252      0.51  |VQ       |         |         |         |
  0+50       0.0288      0.51  | Q       |         |         |         |
  0+55       0.0323      0.51  | Q       |         |         |         |
  1+ 0       0.0359      0.54  | Q       |         |         |         |
  1+ 5       0.0399      0.57  | QV      |         |         |         |
  1+10       0.0438      0.58  | QV      |         |         |         |
  1+15       0.0478      0.58  | QV      |         |         |         |
  1+20       0.0518      0.58  | QV      |         |         |         |
  1+25       0.0559      0.58  | Q V     |         |         |         |
  1+30       0.0599      0.58  | Q V     |         |         |         |
  1+35       0.0639      0.58  | Q V     |         |         |         |
  1+40       0.0679      0.58  | Q  V    |         |         |         |
  1+45       0.0719      0.58  | Q  V    |         |         |         |
  1+50       0.0759      0.58  | Q  V    |         |         |         |
  1+55       0.0799      0.58  | Q   V   |         |         |         |
  2+ 0       0.0841      0.61  | Q   V   |         |         |         |
  2+ 5       0.0884      0.62  | Q   V   |         |         |         |
  2+10       0.0926      0.62  | Q    V  |         |         |         |
  2+15       0.0970      0.65  | Q    V  |         |         |         |
  2+20       0.1015      0.65  | Q    V  |         |         |         |
  2+25       0.1060      0.65  | Q     V |         |         |         |
  2+30       0.1105      0.65  | Q     V |         |         |         |
  2+35       0.1151      0.66  | Q     V |         |         |         |
  2+40       0.1196      0.66  | Q      V|         |         |         |
  2+45       0.1243      0.68  | Q      V|         |         |         |
  2+50       0.1292      0.71  | Q      V|         |         |         |
  2+55       0.1342      0.72  | Q       V         |         |         |
  3+ 0       0.1392      0.73  | Q       V         |         |         |
  3+ 5       0.1442      0.73  | Q       V         |         |         |
  3+10       0.1494      0.75  |  Q      |V        |         |         |
  3+15       0.1548      0.79  |  Q      |V        |         |         |
  3+20       0.1603      0.80  |  Q      | V       |         |         |
  3+25       0.1659      0.82  |  Q      | V       |         |         |
  3+30       0.1720      0.89  |  Q      |  V      |         |         |
  3+35       0.1786      0.95  |  Q      |  V      |         |         |
  3+40       0.1855      1.00  |  Q      |   V     |         |         |
  3+45       0.1926      1.04  |   Q     |   V     |         |         |
  3+50       0.2000      1.08  |   Q     |    V    |         |         |
  3+55       0.2077      1.11  |   Q     |    V    |         |         |
  4+ 0       0.2156      1.15  |   Q     |     V   |         |         |
  4+ 5       0.2237      1.18  |   Q     |      V  |         |         |
  4+10       0.2323      1.25  |   Q     |      V  |         |         |
  4+15       0.2414      1.32  |    Q    |       V |         |         |
  4+20       0.2510      1.39  |    Q    |        V|         |         |
  4+25       0.2610      1.46  |    Q    |        V|         |         |
  4+30       0.2714      1.51  |     Q   |         V         |         |
  4+35       0.2820      1.55  |     Q   |         |V        |         |
  4+40       0.2931      1.61  |     Q   |         | V       |         |
  4+45       0.3047      1.68  |     Q   |         |  V      |         |
  4+50       0.3166      1.73  |     Q   |         |   V     |         |
  4+55       0.3287      1.76  |      Q  |         |   V     |         |
  5+ 0       0.3413      1.83  |      Q  |         |    V    |         |
  5+ 5       0.3551      2.00  |       Q |         |     V   |         |
  5+10       0.3714      2.36  |        Q|         |      V  |         |
  5+15       0.3906      2.79  |         |Q        |       V |         |
```


5+20 0.4128 3.22
5+25 0.4387 3.76
5+30 0.4706 4.64
5+35 0.4971 3.85
5+40 0.5095 1.79
5+45 0.5164 1.00
5+50 0.5207 0.63
5+55 0.5235 0.40
6+ 0 0.5252 0.24
6+ 5 0.5260 0.12
6+10 0.5263 0.04
6+15 0.5264 0.01
6+20 0.5264 0.01
6+25 0.5264 0.00

```
       U n i t   H y d r o g r a p h   A n a l y s i s

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              Study date  04/22/24 File: pro35245.out

++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =       7.79(Ac.)  =      0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =       7.79(Ac.)  =      0.012 Sq. Mi.
Length along longest watercourse =    2225.00(Ft.)
Length along longest watercourse measured to centroid =    1113.00(Ft.)
Length along longest watercourse =      0.421 Mi.
Length along longest watercourse measured to centroid =      0.211 Mi.
Difference in elevation =      82.00(Ft.)
Slope along watercourse =    194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.053 Hr.
Lag time =     3.16 Min.
25% of lag time =     0.79 Min.
40% of lag time =     1.26 Min.
Unit time =     5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            1.80                 14.02

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            5.00                 38.95

STORM EVENT (YEAR) =    5.00
Area Averaged 2-Year Rainfall =    1.800(In)
Area Averaged 100-Year Rainfall =    5.000(In)

Point rain (area averaged) =    2.550(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    2.549(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     7.790           69.00          0.500
 Total Area Entered =      7.79(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-1     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  49.8      0.574     0.500        0.316       1.000      0.316
                                                 Sum (F) =   0.316
Area averaged mean soil loss (F) (In/Hr) =  0.316
Minimum soil loss rate ((In/Hr)) =  0.158
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
			Sum = 100.000	Sum= 7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.020	(0.560)	0.010	0.010
2	0.17	0.07	0.020	(0.557)	0.010	0.010
3	0.25	0.07	0.020	(0.555)	0.010	0.010
4	0.33	0.10	0.031	(0.553)	0.015	0.015
5	0.42	0.10	0.031	(0.551)	0.015	0.015
6	0.50	0.10	0.031	(0.549)	0.015	0.015
7	0.58	0.10	0.031	(0.547)	0.015	0.015
8	0.67	0.10	0.031	(0.545)	0.015	0.015
9	0.75	0.10	0.031	(0.542)	0.015	0.015
10	0.83	0.13	0.041	(0.540)	0.020	0.020
11	0.92	0.13	0.041	(0.538)	0.020	0.020
12	1.00	0.13	0.041	(0.536)	0.020	0.020
13	1.08	0.10	0.031	(0.534)	0.015	0.015
14	1.17	0.10	0.031	(0.532)	0.015	0.015
15	1.25	0.10	0.031	(0.530)	0.015	0.015
16	1.33	0.10	0.031	(0.528)	0.015	0.015
17	1.42	0.10	0.031	(0.525)	0.015	0.015
18	1.50	0.10	0.031	(0.523)	0.015	0.015
19	1.58	0.10	0.031	(0.521)	0.015	0.015
20	1.67	0.10	0.031	(0.519)	0.015	0.015
21	1.75	0.10	0.031	(0.517)	0.015	0.015
22	1.83	0.13	0.041	(0.515)	0.020	0.020
23	1.92	0.13	0.041	(0.513)	0.020	0.020
24	2.00	0.13	0.041	(0.511)	0.020	0.020
25	2.08	0.13	0.041	(0.509)	0.020	0.020
26	2.17	0.13	0.041	(0.507)	0.020	0.020
27	2.25	0.13	0.041	(0.505)	0.020	0.020
28	2.33	0.13	0.041	(0.503)	0.020	0.020
29	2.42	0.13	0.041	(0.501)	0.020	0.020
30	2.50	0.13	0.041	(0.499)	0.020	0.020
31	2.58	0.17	0.051	(0.497)	0.025	0.025
32	2.67	0.17	0.051	(0.494)	0.025	0.025
33	2.75	0.17	0.051	(0.492)	0.025	0.025
34	2.83	0.17	0.051	(0.490)	0.025	0.025
35	2.92	0.17	0.051	(0.488)	0.025	0.025
36	3.00	0.17	0.051	(0.486)	0.025	0.025
37	3.08	0.17	0.051	(0.484)	0.025	0.025
38	3.17	0.17	0.051	(0.482)	0.025	0.025
39	3.25	0.17	0.051	(0.480)	0.025	0.025
40	3.33	0.17	0.051	(0.478)	0.025	0.025
41	3.42	0.17	0.051	(0.476)	0.025	0.025
42	3.50	0.17	0.051	(0.474)	0.025	0.025
43	3.58	0.17	0.051	(0.472)	0.025	0.025
44	3.67	0.17	0.051	(0.470)	0.025	0.025
45	3.75	0.17	0.051	(0.468)	0.025	0.025
46	3.83	0.20	0.061	(0.466)	0.031	0.031
47	3.92	0.20	0.061	(0.464)	0.031	0.031
48	4.00	0.20	0.061	(0.463)	0.031	0.031
49	4.08	0.20	0.061	(0.461)	0.031	0.031
50	4.17	0.20	0.061	(0.459)	0.031	0.031
51	4.25	0.20	0.061	(0.457)	0.031	0.031
52	4.33	0.23	0.071	(0.455)	0.036	0.036
53	4.42	0.23	0.071	(0.453)	0.036	0.036
54	4.50	0.23	0.071	(0.451)	0.036	0.036
55	4.58	0.23	0.071	(0.449)	0.036	0.036
56	4.67	0.23	0.071	(0.447)	0.036	0.036
57	4.75	0.23	0.071	(0.445)	0.036	0.036
58	4.83	0.27	0.082	(0.443)	0.041	0.041
59	4.92	0.27	0.082	(0.441)	0.041	0.041
60	5.00	0.27	0.082	(0.439)	0.041	0.041
61	5.08	0.20	0.061	(0.437)	0.031	0.031
62	5.17	0.20	0.061	(0.435)	0.031	0.031
63	5.25	0.20	0.061	(0.434)	0.031	0.031
64	5.33	0.23	0.071	(0.432)	0.036	0.036
65	5.42	0.23	0.071	(0.430)	0.036	0.036
66	5.50	0.23	0.071	(0.428)	0.036	0.036
67	5.58	0.27	0.082	(0.426)	0.041	0.041
68	5.67	0.27	0.082	(0.424)	0.041	0.041
69	5.75	0.27	0.082	(0.422)	0.041	0.041
70	5.83	0.27	0.082	(0.420)	0.041	0.041

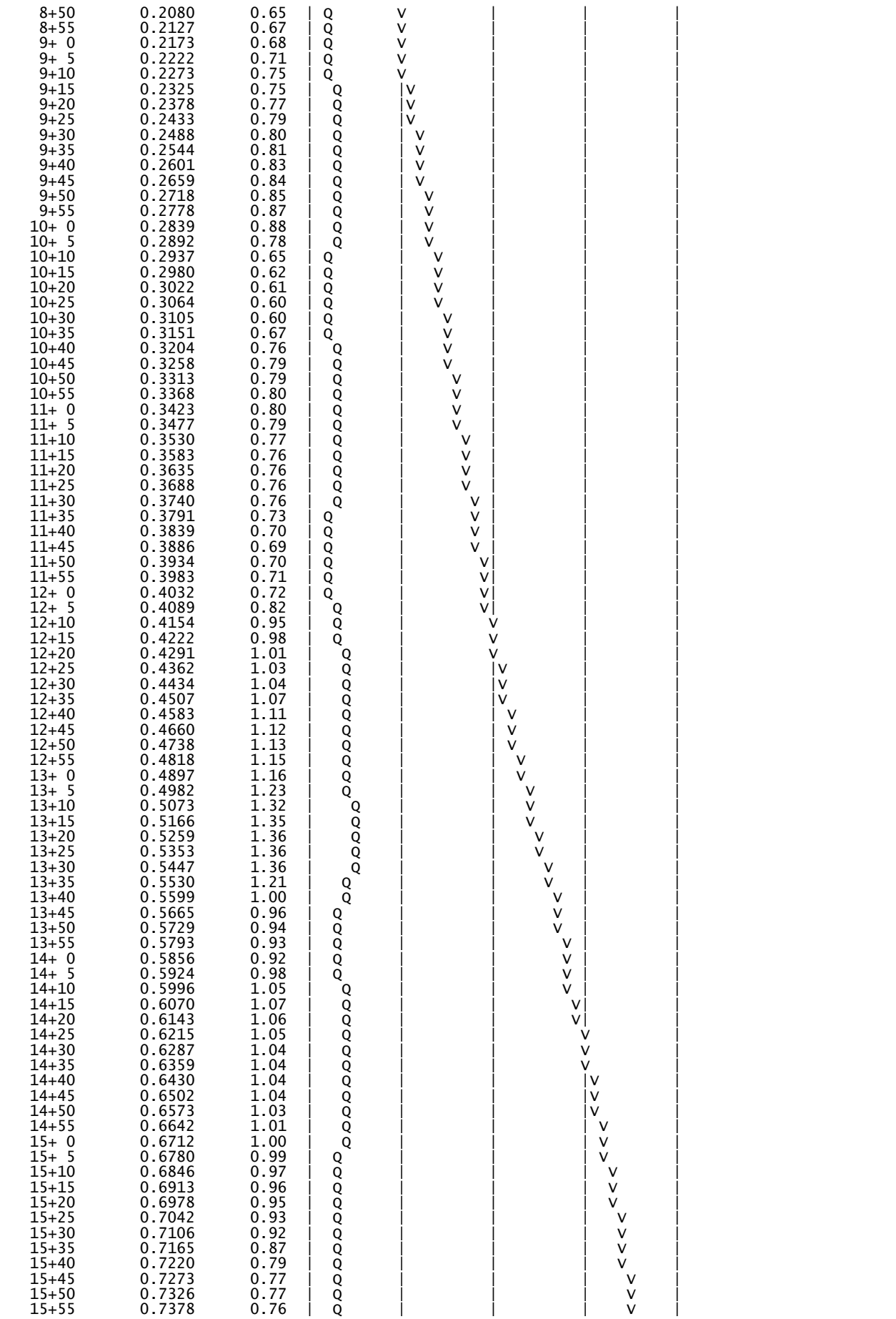
71	5.92	0.27	0.082	(0.419)	0.041	0.041
72	6.00	0.27	0.082	(0.417)	0.041	0.041
73	6.08	0.30	0.092	(0.415)	0.046	0.046
74	6.17	0.30	0.092	(0.413)	0.046	0.046
75	6.25	0.30	0.092	(0.411)	0.046	0.046
76	6.33	0.30	0.092	(0.409)	0.046	0.046
77	6.42	0.30	0.092	(0.407)	0.046	0.046
78	6.50	0.30	0.092	(0.406)	0.046	0.046
79	6.58	0.33	0.102	(0.404)	0.051	0.051
80	6.67	0.33	0.102	(0.402)	0.051	0.051
81	6.75	0.33	0.102	(0.400)	0.051	0.051
82	6.83	0.33	0.102	(0.398)	0.051	0.051
83	6.92	0.33	0.102	(0.397)	0.051	0.051
84	7.00	0.33	0.102	(0.395)	0.051	0.051
85	7.08	0.33	0.102	(0.393)	0.051	0.051
86	7.17	0.33	0.102	(0.391)	0.051	0.051
87	7.25	0.33	0.102	(0.389)	0.051	0.051
88	7.33	0.37	0.112	(0.388)	0.056	0.056
89	7.42	0.37	0.112	(0.386)	0.056	0.056
90	7.50	0.37	0.112	(0.384)	0.056	0.056
91	7.58	0.40	0.122	(0.382)	0.061	0.061
92	7.67	0.40	0.122	(0.381)	0.061	0.061
93	7.75	0.40	0.122	(0.379)	0.061	0.061
94	7.83	0.43	0.133	(0.377)	0.066	0.066
95	7.92	0.43	0.133	(0.375)	0.066	0.066
96	8.00	0.43	0.133	(0.374)	0.066	0.066
97	8.08	0.50	0.153	(0.372)	0.076	0.076
98	8.17	0.50	0.153	(0.370)	0.076	0.076
99	8.25	0.50	0.153	(0.368)	0.076	0.076
100	8.33	0.50	0.153	(0.367)	0.076	0.076
101	8.42	0.50	0.153	(0.365)	0.076	0.076
102	8.50	0.50	0.153	(0.363)	0.076	0.076
103	8.58	0.53	0.163	(0.362)	0.082	0.082
104	8.67	0.53	0.163	(0.360)	0.082	0.082
105	8.75	0.53	0.163	(0.358)	0.082	0.082
106	8.83	0.57	0.173	(0.356)	0.087	0.087
107	8.92	0.57	0.173	(0.355)	0.087	0.087
108	9.00	0.57	0.173	(0.353)	0.087	0.087
109	9.08	0.63	0.194	(0.351)	0.097	0.097
110	9.17	0.63	0.194	(0.350)	0.097	0.097
111	9.25	0.63	0.194	(0.348)	0.097	0.097
112	9.33	0.67	0.204	(0.346)	0.102	0.102
113	9.42	0.67	0.204	(0.345)	0.102	0.102
114	9.50	0.67	0.204	(0.343)	0.102	0.102
115	9.58	0.70	0.214	(0.341)	0.107	0.107
116	9.67	0.70	0.214	(0.340)	0.107	0.107
117	9.75	0.70	0.214	(0.338)	0.107	0.107
118	9.83	0.73	0.224	(0.337)	0.112	0.112
119	9.92	0.73	0.224	(0.335)	0.112	0.112
120	10.00	0.73	0.224	(0.333)	0.112	0.112
121	10.08	0.50	0.153	(0.332)	0.076	0.076
122	10.17	0.50	0.153	(0.330)	0.076	0.076
123	10.25	0.50	0.153	(0.329)	0.076	0.076
124	10.33	0.50	0.153	(0.327)	0.076	0.076
125	10.42	0.50	0.153	(0.325)	0.076	0.076
126	10.50	0.50	0.153	(0.324)	0.076	0.076
127	10.58	0.67	0.204	(0.322)	0.102	0.102
128	10.67	0.67	0.204	(0.321)	0.102	0.102
129	10.75	0.67	0.204	(0.319)	0.102	0.102
130	10.83	0.67	0.204	(0.317)	0.102	0.102
131	10.92	0.67	0.204	(0.316)	0.102	0.102
132	11.00	0.67	0.204	(0.314)	0.102	0.102
133	11.08	0.63	0.194	(0.313)	0.097	0.097
134	11.17	0.63	0.194	(0.311)	0.097	0.097
135	11.25	0.63	0.194	(0.310)	0.097	0.097
136	11.33	0.63	0.194	(0.308)	0.097	0.097
137	11.42	0.63	0.194	(0.307)	0.097	0.097
138	11.50	0.63	0.194	(0.305)	0.097	0.097
139	11.58	0.57	0.173	(0.304)	0.087	0.087
140	11.67	0.57	0.173	(0.302)	0.087	0.087
141	11.75	0.57	0.173	(0.301)	0.087	0.087
142	11.83	0.60	0.184	(0.299)	0.092	0.092
143	11.92	0.60	0.184	(0.298)	0.092	0.092
144	12.00	0.60	0.184	(0.296)	0.092	0.092
145	12.08	0.83	0.255	(0.295)	0.127	0.127
146	12.17	0.83	0.255	(0.293)	0.127	0.127
147	12.25	0.83	0.255	(0.292)	0.127	0.127
148	12.33	0.87	0.265	(0.290)	0.133	0.133
149	12.42	0.87	0.265	(0.289)	0.133	0.133
150	12.50	0.87	0.265	(0.287)	0.133	0.133
151	12.58	0.93	0.286	(0.286)	0.143	0.143
152	12.67	0.93	0.286	(0.284)	0.143	0.143
153	12.75	0.93	0.286	(0.283)	0.143	0.143
154	12.83	0.97	0.296	(0.282)	0.148	0.148
155	12.92	0.97	0.296	(0.280)	0.148	0.148
156	13.00	0.97	0.296	(0.279)	0.148	0.148

157	13.08	1.13	0.347	(0.277)	0.173	0.173
158	13.17	1.13	0.347	(0.276)	0.173	0.173
159	13.25	1.13	0.347	(0.275)	0.173	0.173
160	13.33	1.13	0.347	(0.273)	0.173	0.173
161	13.42	1.13	0.347	(0.272)	0.173	0.173
162	13.50	1.13	0.347	(0.270)	0.173	0.173
163	13.58	0.77	0.235	(0.269)	0.117	0.117
164	13.67	0.77	0.235	(0.268)	0.117	0.117
165	13.75	0.77	0.235	(0.266)	0.117	0.117
166	13.83	0.77	0.235	(0.265)	0.117	0.117
167	13.92	0.77	0.235	(0.264)	0.117	0.117
168	14.00	0.77	0.235	(0.262)	0.117	0.117
169	14.08	0.90	0.275	(0.261)	0.138	0.138
170	14.17	0.90	0.275	(0.260)	0.138	0.138
171	14.25	0.90	0.275	(0.258)	0.138	0.138
172	14.33	0.87	0.265	(0.257)	0.133	0.133
173	14.42	0.87	0.265	(0.256)	0.133	0.133
174	14.50	0.87	0.265	(0.254)	0.133	0.133
175	14.58	0.87	0.265	(0.253)	0.133	0.133
176	14.67	0.87	0.265	(0.252)	0.133	0.133
177	14.75	0.87	0.265	(0.250)	0.133	0.133
178	14.83	0.83	0.255	(0.249)	0.127	0.127
179	14.92	0.83	0.255	(0.248)	0.127	0.127
180	15.00	0.83	0.255	(0.247)	0.127	0.127
181	15.08	0.80	0.245	(0.245)	0.122	0.122
182	15.17	0.80	0.245	(0.244)	0.122	0.122
183	15.25	0.80	0.245	(0.243)	0.122	0.122
184	15.33	0.77	0.235	(0.242)	0.117	0.117
185	15.42	0.77	0.235	(0.240)	0.117	0.117
186	15.50	0.77	0.235	(0.239)	0.117	0.117
187	15.58	0.63	0.194	(0.238)	0.097	0.097
188	15.67	0.63	0.194	(0.237)	0.097	0.097
189	15.75	0.63	0.194	(0.235)	0.097	0.097
190	15.83	0.63	0.194	(0.234)	0.097	0.097
191	15.92	0.63	0.194	(0.233)	0.097	0.097
192	16.00	0.63	0.194	(0.232)	0.097	0.097
193	16.08	0.13	0.041	(0.231)	0.020	0.020
194	16.17	0.13	0.041	(0.229)	0.020	0.020
195	16.25	0.13	0.041	(0.228)	0.020	0.020
196	16.33	0.13	0.041	(0.227)	0.020	0.020
197	16.42	0.13	0.041	(0.226)	0.020	0.020
198	16.50	0.13	0.041	(0.225)	0.020	0.020
199	16.58	0.10	0.031	(0.224)	0.015	0.015
200	16.67	0.10	0.031	(0.223)	0.015	0.015
201	16.75	0.10	0.031	(0.221)	0.015	0.015
202	16.83	0.10	0.031	(0.220)	0.015	0.015
203	16.92	0.10	0.031	(0.219)	0.015	0.015
204	17.00	0.10	0.031	(0.218)	0.015	0.015
205	17.08	0.17	0.051	(0.217)	0.025	0.025
206	17.17	0.17	0.051	(0.216)	0.025	0.025
207	17.25	0.17	0.051	(0.215)	0.025	0.025
208	17.33	0.17	0.051	(0.214)	0.025	0.025
209	17.42	0.17	0.051	(0.213)	0.025	0.025
210	17.50	0.17	0.051	(0.212)	0.025	0.025
211	17.58	0.17	0.051	(0.211)	0.025	0.025
212	17.67	0.17	0.051	(0.209)	0.025	0.025
213	17.75	0.17	0.051	(0.208)	0.025	0.025
214	17.83	0.13	0.041	(0.207)	0.020	0.020
215	17.92	0.13	0.041	(0.206)	0.020	0.020
216	18.00	0.13	0.041	(0.205)	0.020	0.020
217	18.08	0.13	0.041	(0.204)	0.020	0.020
218	18.17	0.13	0.041	(0.203)	0.020	0.020
219	18.25	0.13	0.041	(0.202)	0.020	0.020
220	18.33	0.13	0.041	(0.201)	0.020	0.020
221	18.42	0.13	0.041	(0.200)	0.020	0.020
222	18.50	0.13	0.041	(0.199)	0.020	0.020
223	18.58	0.10	0.031	(0.198)	0.015	0.015
224	18.67	0.10	0.031	(0.197)	0.015	0.015
225	18.75	0.10	0.031	(0.197)	0.015	0.015
226	18.83	0.07	0.020	(0.196)	0.010	0.010
227	18.92	0.07	0.020	(0.195)	0.010	0.010
228	19.00	0.07	0.020	(0.194)	0.010	0.010
229	19.08	0.10	0.031	(0.193)	0.015	0.015
230	19.17	0.10	0.031	(0.192)	0.015	0.015
231	19.25	0.10	0.031	(0.191)	0.015	0.015
232	19.33	0.13	0.041	(0.190)	0.020	0.020
233	19.42	0.13	0.041	(0.189)	0.020	0.020
234	19.50	0.13	0.041	(0.188)	0.020	0.020
235	19.58	0.10	0.031	(0.187)	0.015	0.015
236	19.67	0.10	0.031	(0.187)	0.015	0.015
237	19.75	0.10	0.031	(0.186)	0.015	0.015
238	19.83	0.07	0.020	(0.185)	0.010	0.010
239	19.92	0.07	0.020	(0.184)	0.010	0.010
240	20.00	0.07	0.020	(0.183)	0.010	0.010
241	20.08	0.10	0.031	(0.182)	0.015	0.015
242	20.17	0.10	0.031	(0.182)	0.015	0.015

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243  20.25     0.10      0.031       (  0.181)       0.015        0.015
244  20.33     0.10      0.031       (  0.180)       0.015        0.015
245  20.42     0.10      0.031       (  0.179)       0.015        0.015
246  20.50     0.10      0.031       (  0.179)       0.015        0.015
247  20.58     0.10      0.031       (  0.178)       0.015        0.015
248  20.67     0.10      0.031       (  0.177)       0.015        0.015
249  20.75     0.10      0.031       (  0.176)       0.015        0.015
250  20.83     0.07      0.020       (  0.176)       0.010        0.010
251  20.92     0.07      0.020       (  0.175)       0.010        0.010
252  21.00     0.07      0.020       (  0.174)       0.010        0.010
253  21.08     0.10      0.031       (  0.174)       0.015        0.015
254  21.17     0.10      0.031       (  0.173)       0.015        0.015
255  21.25     0.10      0.031       (  0.172)       0.015        0.015
256  21.33     0.07      0.020       (  0.172)       0.010        0.010
257  21.42     0.07      0.020       (  0.171)       0.010        0.010
258  21.50     0.07      0.020       (  0.170)       0.010        0.010
259  21.58     0.10      0.031       (  0.170)       0.015        0.015
260  21.67     0.10      0.031       (  0.169)       0.015        0.015
261  21.75     0.10      0.031       (  0.168)       0.015        0.015
262  21.83     0.07      0.020       (  0.168)       0.010        0.010
263  21.92     0.07      0.020       (  0.167)       0.010        0.010
264  22.00     0.07      0.020       (  0.167)       0.010        0.010
265  22.08     0.10      0.031       (  0.166)       0.015        0.015
266  22.17     0.10      0.031       (  0.166)       0.015        0.015
267  22.25     0.10      0.031       (  0.165)       0.015        0.015
268  22.33     0.07      0.020       (  0.165)       0.010        0.010
269  22.42     0.07      0.020       (  0.164)       0.010        0.010
270  22.50     0.07      0.020       (  0.164)       0.010        0.010
271  22.58     0.07      0.020       (  0.163)       0.010        0.010
272  22.67     0.07      0.020       (  0.163)       0.010        0.010
273  22.75     0.07      0.020       (  0.162)       0.010        0.010
274  22.83     0.07      0.020       (  0.162)       0.010        0.010
275  22.92     0.07      0.020       (  0.161)       0.010        0.010
276  23.00     0.07      0.020       (  0.161)       0.010        0.010
277  23.08     0.07      0.020       (  0.161)       0.010        0.010
278  23.17     0.07      0.020       (  0.160)       0.010        0.010
279  23.25     0.07      0.020       (  0.160)       0.010        0.010
280  23.33     0.07      0.020       (  0.160)       0.010        0.010
281  23.42     0.07      0.020       (  0.159)       0.010        0.010
282  23.50     0.07      0.020       (  0.159)       0.010        0.010
283  23.58     0.07      0.020       (  0.159)       0.010        0.010
284  23.67     0.07      0.020       (  0.158)       0.010        0.010
285  23.75     0.07      0.020       (  0.158)       0.010        0.010
286  23.83     0.07      0.020       (  0.158)       0.010        0.010
287  23.92     0.07      0.020       (  0.158)       0.010        0.010
288  24.00     0.07      0.020       (  0.158)       0.010        0.010
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    15.3
      Flood volume = Effective rainfall      1.27(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       0.8(Ac.Ft)
      Total soil loss =      1.27(In)
      Total soil loss =     0.828(Ac.Ft)
      Total rainfall =      2.55(In)
      Flood volume =       36046.7 Cubic Feet
      Total soil loss =       36046.7 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      1.362(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0002      0.03  Q          |         |         |         |
   0+10       0.0006      0.07  Q          |         |         |         |
   0+15       0.0012      0.07  Q          |         |         |         |
   0+20       0.0018      0.09  Q          |         |         |         |
   0+25       0.0026      0.11  Q          |         |         |         |
   0+30       0.0034      0.12  Q          |         |         |         |
   0+35       0.0042      0.12  Q          |         |         |         |
   0+40       0.0050      0.12  Q          |         |         |         |
   0+45       0.0058      0.12  Q          |         |         |         |
   0+50       0.0068      0.13  Q          |         |         |         |
   0+55       0.0078      0.15  Q          |         |         |         |
   1+ 0       0.0089      0.16  Q          |         |         |         |
   1+ 5       0.0099      0.14  Q          |         |         |         |
   1+10       0.0108      0.13  Q          |         |         |         |
   1+15       0.0116      0.12  Q          |         |         |         |
   1+20       0.0124      0.12  Q          |         |         |         |
   1+25       0.0133      0.12  Q          |         |         |         |
   1+30       0.0141      0.12  Q          |         |         |         |
   1+35       0.0149      0.12  Q          |         |         |         |
```

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1+40       0.0158      0.12  Q          |          |          |          |
1+45       0.0166      0.12  Q          |          |          |          |
1+50       0.0175      0.13  Q          |          |          |          |
1+55       0.0186      0.15  Q          |          |          |          |
2+ 0       0.0196      0.16  Q          |          |          |          |
2+ 5       0.0207      0.16  QV         |          |          |          |
2+10       0.0218      0.16  QV         |          |          |          |
2+15       0.0229      0.16  QV         |          |          |          |
2+20       0.0241      0.16  QV         |          |          |          |
2+25       0.0252      0.16  QV         |          |          |          |
2+30       0.0263      0.16  QV         |          |          |          |
2+35       0.0275      0.17  QV         |          |          |          |
2+40       0.0288      0.19  QV         |          |          |          |
2+45       0.0301      0.20  QV         |          |          |          |
2+50       0.0315      0.20  QV         |          |          |          |
2+55       0.0329      0.20  QV         |          |          |          |
3+ 0       0.0343      0.20  QV         |          |          |          |
3+ 5       0.0356      0.20  QV         |          |          |          |
3+10       0.0370      0.20  QV         |          |          |          |
3+15       0.0384      0.20  QV         |          |          |          |
3+20       0.0398      0.20  QV         |          |          |          |
3+25       0.0412      0.20  QV         |          |          |          |
3+30       0.0425      0.20  Q V        |          |          |          |
3+35       0.0439      0.20  Q V        |          |          |          |
3+40       0.0453      0.20  Q V        |          |          |          |
3+45       0.0467      0.20  Q V        |          |          |          |
3+50       0.0482      0.21  Q V        |          |          |          |
3+55       0.0498      0.23  Q V        |          |          |          |
4+ 0       0.0514      0.24  Q V        |          |          |          |
4+ 5       0.0530      0.24  Q V        |          |          |          |
4+10       0.0547      0.24  Q V        |          |          |          |
4+15       0.0564      0.24  Q V        |          |          |          |
4+20       0.0581      0.25  |QV        |          |          |          |
4+25       0.0600      0.27  |QV        |          |          |          |
4+30       0.0619      0.28  |QV        |          |          |          |
4+35       0.0638      0.28  |Q V       |          |          |          |
4+40       0.0657      0.28  |Q V       |          |          |          |
4+45       0.0677      0.28  |Q V       |          |          |          |
4+50       0.0697      0.29  |Q V       |          |          |          |
4+55       0.0719      0.31  |Q V       |          |          |          |
5+ 0       0.0740      0.32  |Q V       |          |          |          |
5+ 5       0.0760      0.29  |Q V       |          |          |          |
5+10       0.0778      0.25  |Q V       |          |          |          |
5+15       0.0795      0.25  Q  V       |          |          |          |
5+20       0.0813      0.26  |Q V       |          |          |          |
5+25       0.0832      0.27  |Q  V      |          |          |          |
5+30       0.0851      0.28  |Q  V      |          |          |          |
5+35       0.0871      0.29  |Q  V      |          |          |          |
5+40       0.0892      0.31  |Q  V      |          |          |          |
5+45       0.0914      0.32  |Q  V      |          |          |          |
5+50       0.0936      0.32  |Q  V      |          |          |          |
5+55       0.0958      0.32  |Q  V      |          |          |          |
6+ 0       0.0980      0.32  |Q  V      |          |          |          |
6+ 5       0.1003      0.33  |Q  V      |          |          |          |
6+10       0.1028      0.35  |Q  V      |          |          |          |
6+15       0.1052      0.36  |Q   V     |          |          |          |
6+20       0.1077      0.36  |Q   V     |          |          |          |
6+25       0.1102      0.36  |Q   V     |          |          |          |
6+30       0.1127      0.36  |Q   V     |          |          |          |
6+35       0.1152      0.37  |Q   V     |          |          |          |
6+40       0.1179      0.39  |Q   V     |          |          |          |
6+45       0.1207      0.40  |Q   V     |          |          |          |
6+50       0.1234      0.40  |Q   V     |          |          |          |
6+55       0.1262      0.40  |Q    V    |          |          |          |
7+ 0       0.1289      0.40  |Q    V    |          |          |          |
7+ 5       0.1317      0.40  |Q    V    |          |          |          |
7+10       0.1345      0.40  |Q    V    |          |          |          |
7+15       0.1372      0.40  |Q    V    |          |          |          |
7+20       0.1401      0.41  |Q    V    |          |          |          |
7+25       0.1431      0.43  |Q    V    |          |          |          |
7+30       0.1461      0.44  |Q     V   |          |          |          |
7+35       0.1492      0.45  |Q     V   |          |          |          |
7+40       0.1525      0.47  |Q     V   |          |          |          |
7+45       0.1557      0.48  |Q     V   |          |          |          |
7+50       0.1591      0.49  |Q     V   |          |          |          |
7+55       0.1627      0.51  | Q    V   |          |          |          |
8+ 0       0.1662      0.52  | Q     V  |          |          |          |
8+ 5       0.1700      0.55  | Q     V  |          |          |          |
8+10       0.1740      0.59  | Q     V  |          |          |          |
8+15       0.1781      0.59  | Q     V  |          |          |          |
8+20       0.1823      0.60  | Q     V  |          |          |          |
8+25       0.1864      0.60  | Q      V |          |          |          |
8+30       0.1905      0.60  | Q      V |          |          |          |
8+35       0.1948      0.61  | Q      V |          |          |          |
8+40       0.1991      0.63  | Q      V |          |          |          |
8+45       0.2035      0.64  | Q      V |          |          |          |
```



8+50	0.2080	0.65	Q	V				
8+55	0.2127	0.67	Q	V				
9+ 0	0.2173	0.68	Q	V				
9+ 5	0.2222	0.71	Q	V				
9+10	0.2273	0.75	Q	V				
9+15	0.2325	0.75	Q	V				
9+20	0.2378	0.77	Q	V				
9+25	0.2433	0.79	Q	V				
9+30	0.2488	0.80	Q	V				
9+35	0.2544	0.81	Q	V				
9+40	0.2601	0.83	Q	V				
9+45	0.2659	0.84	Q	V				
9+50	0.2718	0.85	Q	V				
9+55	0.2778	0.87	Q	V				
10+ 0	0.2839	0.88	Q	V				
10+ 5	0.2892	0.78	Q	V				
10+10	0.2937	0.65	Q	V				
10+15	0.2980	0.62	Q	V				
10+20	0.3022	0.61	Q	V				
10+25	0.3064	0.60	Q	V				
10+30	0.3105	0.60	Q	V				
10+35	0.3151	0.67	Q	V				
10+40	0.3204	0.76	Q	V				
10+45	0.3258	0.79	Q	V				
10+50	0.3313	0.79	Q	V				
10+55	0.3368	0.80	Q	V				
11+ 0	0.3423	0.80	Q	V				
11+ 5	0.3477	0.79	Q	V				
11+10	0.3530	0.77	Q	V				
11+15	0.3583	0.76	Q	V				
11+20	0.3635	0.76	Q	V				
11+25	0.3688	0.76	Q	V				
11+30	0.3740	0.76	Q	V				
11+35	0.3791	0.73	Q	V				
11+40	0.3839	0.70	Q	V				
11+45	0.3886	0.69	Q	V				
11+50	0.3934	0.70	Q	V				
11+55	0.3983	0.71	Q	V				
12+ 0	0.4032	0.72	Q	V				
12+ 5	0.4089	0.82	Q	V				
12+10	0.4154	0.95	Q	V				
12+15	0.4222	0.98	Q	V				
12+20	0.4291	1.01	Q	V				
12+25	0.4362	1.03	Q	V				
12+30	0.4434	1.04	Q	V				
12+35	0.4507	1.07	Q	V				
12+40	0.4583	1.11	Q	V				
12+45	0.4660	1.12	Q	V				
12+50	0.4738	1.13	Q	V				
12+55	0.4818	1.15	Q	V				
13+ 0	0.4897	1.16	Q	V				
13+ 5	0.4982	1.23	Q	V				
13+10	0.5073	1.32	Q	V				
13+15	0.5166	1.35	Q	V				
13+20	0.5259	1.36	Q	V				
13+25	0.5353	1.36	Q	V				
13+30	0.5447	1.36	Q	V				
13+35	0.5530	1.21	Q	V				
13+40	0.5599	1.00	Q	V				
13+45	0.5665	0.96	Q	V				
13+50	0.5729	0.94	Q	V				
13+55	0.5793	0.93	Q	V				
14+ 0	0.5856	0.92	Q	V				
14+ 5	0.5924	0.98	Q	V				
14+10	0.5996	1.05	Q	V				
14+15	0.6070	1.07	Q	V				
14+20	0.6143	1.06	Q	V				
14+25	0.6215	1.05	Q	V				
14+30	0.6287	1.04	Q	V				
14+35	0.6359	1.04	Q	V				
14+40	0.6430	1.04	Q	V				
14+45	0.6502	1.04	Q	V				
14+50	0.6573	1.03	Q	V				
14+55	0.6642	1.01	Q	V				
15+ 0	0.6712	1.00	Q	V				
15+ 5	0.6780	0.99	Q	V				
15+10	0.6846	0.97	Q	V				
15+15	0.6913	0.96	Q	V				
15+20	0.6978	0.95	Q	V				
15+25	0.7042	0.93	Q	V				
15+30	0.7106	0.92	Q	V				
15+35	0.7165	0.87	Q	V				
15+40	0.7220	0.79	Q	V				
15+45	0.7273	0.77	Q	V				
15+50	0.7326	0.77	Q	V				
15+55	0.7378	0.76	Q	V				

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16+ 0       0.7431      0.76  |  Q      |         |         |     V     |
16+ 5       0.7469      0.55  | Q       |         |         |      V    |
16+10       0.7487      0.27  |Q        |         |         |      V    |
16+15       0.7502      0.21  Q         |         |         |      V    |
16+20       0.7514      0.18  Q         |         |         |      V    |
16+25       0.7525      0.17  Q         |         |         |      V    |
16+30       0.7536      0.16  Q         |         |         |      V    |
16+35       0.7547      0.15  Q         |         |         |      V    |
16+40       0.7555      0.13  Q         |         |         |      V    |
16+45       0.7564      0.12  Q         |         |         |      V    |
16+50       0.7572      0.12  Q         |         |         |      V    |
16+55       0.7580      0.12  Q         |         |         |      V    |
17+ 0       0.7589      0.12  Q         |         |         |      V    |
17+ 5       0.7599      0.15  Q         |         |         |      V    |
17+10       0.7612      0.19  Q         |         |         |      V    |
17+15       0.7625      0.19  Q         |         |         |      V    |
17+20       0.7639      0.20  Q         |         |         |      V    |
17+25       0.7652      0.20  Q         |         |         |      V    |
17+30       0.7666      0.20  Q         |         |         |       V   |
17+35       0.7680      0.20  Q         |         |         |       V   |
17+40       0.7694      0.20  Q         |         |         |       V   |
17+45       0.7708      0.20  Q         |         |         |       V   |
17+50       0.7720      0.19  Q         |         |         |       V   |
17+55       0.7732      0.17  Q         |         |         |       V   |
18+ 0       0.7743      0.16  Q         |         |         |       V   |
18+ 5       0.7754      0.16  Q         |         |         |       V   |
18+10       0.7765      0.16  Q         |         |         |       V   |
18+15       0.7776      0.16  Q         |         |         |       V   |
18+20       0.7787      0.16  Q         |         |         |       V   |
18+25       0.7799      0.16  Q         |         |         |       V   |
18+30       0.7810      0.16  Q         |         |         |       V   |
18+35       0.7820      0.15  Q         |         |         |       V   |
18+40       0.7828      0.13  Q         |         |         |       V   |
18+45       0.7837      0.12  Q         |         |         |       V   |
18+50       0.7844      0.11  Q         |         |         |       V   |
18+55       0.7850      0.09  Q         |         |         |       V   |
19+ 0       0.7856      0.08  Q         |         |         |       V   |
19+ 5       0.7863      0.10  Q         |         |         |        V  |
19+10       0.7870      0.11  Q         |         |         |        V  |
19+15       0.7878      0.12  Q         |         |         |        V  |
19+20       0.7888      0.13  Q         |         |         |        V  |
19+25       0.7898      0.15  Q         |         |         |        V  |
19+30       0.7909      0.16  Q         |         |         |        V  |
19+35       0.7919      0.14  Q         |         |         |        V  |
19+40       0.7928      0.13  Q         |         |         |        V  |
19+45       0.7936      0.12  Q         |         |         |        V  |
19+50       0.7944      0.11  Q         |         |         |        V  |
19+55       0.7950      0.09  Q         |         |         |        V  |
20+ 0       0.7955      0.08  Q         |         |         |        V  |
20+ 5       0.7962      0.10  Q         |         |         |        V  |
20+10       0.7970      0.11  Q         |         |         |        V  |
20+15       0.7978      0.12  Q         |         |         |        V  |
20+20       0.7986      0.12  Q         |         |         |        V  |
20+25       0.7994      0.12  Q         |         |         |        V  |
20+30       0.8002      0.12  Q         |         |         |        V  |
20+35       0.8011      0.12  Q         |         |         |        V  |
20+40       0.8019      0.12  Q         |         |         |        V  |
20+45       0.8027      0.12  Q         |         |         |        V  |
20+50       0.8035      0.11  Q         |         |         |        V  |
20+55       0.8041      0.09  Q         |         |         |        V  |
21+ 0       0.8046      0.08  Q         |         |         |        V  |
21+ 5       0.8053      0.10  Q         |         |         |        V  |
21+10       0.8061      0.11  Q         |         |         |        V  |
21+15       0.8069      0.12  Q         |         |         |         V |
21+20       0.8076      0.10  Q         |         |         |         V |
21+25       0.8082      0.09  Q         |         |         |         V |
21+30       0.8088      0.08  Q         |         |         |         V |
21+35       0.8094      0.10  Q         |         |         |         V |
21+40       0.8102      0.11  Q         |         |         |         V |
21+45       0.8110      0.12  Q         |         |         |         V |
21+50       0.8117      0.10  Q         |         |         |         V |
21+55       0.8123      0.09  Q         |         |         |         V |
22+ 0       0.8129      0.08  Q         |         |         |         V |
22+ 5       0.8136      0.10  Q         |         |         |         V |
22+10       0.8144      0.11  Q         |         |         |         V |
22+15       0.8152      0.12  Q         |         |         |         V |
22+20       0.8159      0.10  Q         |         |         |         V |
22+25       0.8165      0.09  Q         |         |         |         V |
22+30       0.8171      0.08  Q         |         |         |         V |
22+35       0.8176      0.08  Q         |         |         |         V |
22+40       0.8182      0.08  Q         |         |         |         V |
22+45       0.8187      0.08  Q         |         |         |         V |
22+50       0.8193      0.08  Q         |         |         |         V |
22+55       0.8198      0.08  Q         |         |         |         V |
23+ 0       0.8204      0.08  Q         |         |         |         V |
23+ 5       0.8209      0.08  Q         |         |         |         V |
```

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   23+10       0.8215      0.08  Q          |          |          |          v|
   23+15       0.8220      0.08  Q          |          |          |          v|
   23+20       0.8226      0.08  Q          |          |          |          v|
   23+25       0.8231      0.08  Q          |          |          |          v|
   23+30       0.8237      0.08  Q          |          |          |          v|
   23+35       0.8242      0.08  Q          |          |          |          v|
   23+40       0.8248      0.08  Q          |          |          |          v|
   23+45       0.8253      0.08  Q          |          |          |          v|
   23+50       0.8259      0.08  Q          |          |          |          v|
   23+55       0.8264      0.08  Q          |          |          |          v|
   24+ 0       0.8270      0.08  Q          |          |          |          v|
   24+ 5       0.8274      0.05  Q          |          |          |          v|
   24+10       0.8275      0.01  Q          |          |          |          v|
   24+15       0.8275      0.01  Q          |          |          |          v|
   24+20       0.8275      0.00  Q          |          |          |          v|
   24+25       0.8275      0.00  Q          |          |          |          v|
-------------------------------------------------------------------------------
```

```
       U n i t   H y d r o g r a p h   A n a l y s i s

       Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2008, Version 8.1
              Study date  04/22/24 File: pro310110.out

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------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =       7.79(Ac.)  =      0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =       7.79(Ac.)  =      0.012 Sq. Mi.
Length along longest watercourse =    2225.00(Ft.)
Length along longest watercourse measured to centroid =    1113.00(Ft.)
Length along longest watercourse =      0.421 Mi.
Length along longest watercourse measured to centroid =      0.211 Mi.
Difference in elevation =      82.00(Ft.)
Slope along watercourse =    194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.053 Hr.
Lag time =     3.16 Min.
25% of lag time =     0.79 Min.
40% of lag time =     1.26 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            0.50                 3.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            1.30                10.13

STORM EVENT (YEAR) =   10.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    0.829(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    0.829(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     7.790           69.00          0.500
 Total Area Entered =      7.79(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  69.0      0.373     0.500        0.205       1.000      0.205
                                                 Sum (F) =   0.205
Area averaged mean soil loss (F) (In/Hr) =  0.205
Minimum soil loss rate ((In/Hr)) =  0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
		Sum = 100.000	Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.328	(0.205)	0.164	0.164
2	0.17	4.20	0.418	0.205	(0.209)	0.213
3	0.25	4.40	0.438	0.205	(0.219)	0.233
4	0.33	4.80	0.478	0.205	(0.239)	0.273
5	0.42	5.20	0.517	0.205	(0.259)	0.312
6	0.50	6.20	0.617	0.205	(0.308)	0.412
7	0.58	6.80	0.677	0.205	(0.338)	0.471
8	0.67	8.80	0.875	0.205	(0.438)	0.670
9	0.75	13.90	1.383	0.205	(0.691)	1.178
10	0.83	31.40	3.124	0.205	(1.562)	2.919
11	0.92	7.20	0.716	0.205	(0.358)	0.511
12	1.00	3.80	0.378	(0.205)	0.189	0.189
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	7.5

Flood volume = Effective rainfall 0.63(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.4(Ac.Ft)
Total soil loss = 0.20(In)
Total soil loss = 0.130(Ac.Ft)
Total rainfall = 0.83(In)
Flood volume = 17780.2 Cubic Feet
Total soil loss = 5664.0 Cubic Feet

Peak flow rate of this hydrograph = 13.398(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0031	0.45	Q				
0+10	0.0113	1.18	VQ				
0+15	0.0220	1.56	VQ				
0+20	0.0346	1.84	Q				
0+25	0.0495	2.16	Q				
0+30	0.0677	2.64	QV				
0+35	0.0898	3.22	Q V				
0+40	0.1180	4.09	Q	V			
0+45	0.1615	6.31		Q V			
0+50	0.2522	13.17			V Q		
0+55	0.3445	13.40			Q	V	
1+ 0	0.3818	5.43		Q		V	
1+ 5	0.3986	2.44	Q			V	
1+10	0.4051	0.94	Q			V	
1+15	0.4076	0.36	Q			V	
1+20	0.4081	0.07	Q			V	
1+25	0.4082	0.01	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro310310.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 2225.00(Ft.)
Length along longest watercourse measured to centroid = 1113.00(Ft.)
Length along longest watercourse = 0.421 Mi.
Length along longest watercourse measured to centroid = 0.211 Mi.
Difference in elevation = 82.00(Ft.)
Slope along watercourse = 194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	0.80	6.23

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	2.00	15.58

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 1.294(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.294(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	69.00	0.500

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
		Sum = 100.000	Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.202	(0.205)	0.101	0.101
2	0.17	1.30	0.202	(0.205)	0.101	0.101
3	0.25	1.10	0.171	(0.205)	0.085	0.085
4	0.33	1.50	0.233	(0.205)	0.116	0.116
5	0.42	1.50	0.233	(0.205)	0.116	0.116
6	0.50	1.80	0.279	(0.205)	0.140	0.140
7	0.58	1.50	0.233	(0.205)	0.116	0.116
8	0.67	1.80	0.279	(0.205)	0.140	0.140
9	0.75	1.80	0.279	(0.205)	0.140	0.140
10	0.83	1.50	0.233	(0.205)	0.116	0.116
11	0.92	1.60	0.248	(0.205)	0.124	0.124
12	1.00	1.80	0.279	(0.205)	0.140	0.140
13	1.08	2.20	0.342	(0.205)	0.171	0.171
14	1.17	2.20	0.342	(0.205)	0.171	0.171
15	1.25	2.20	0.342	(0.205)	0.171	0.171
16	1.33	2.00	0.310	(0.205)	0.155	0.155
17	1.42	2.60	0.404	(0.205)	0.202	0.202
18	1.50	2.70	0.419	0.205	(0.210)	0.214
19	1.58	2.40	0.373	(0.205)	0.186	0.186
20	1.67	2.70	0.419	0.205	(0.210)	0.214
21	1.75	3.30	0.512	0.205	(0.256)	0.307
22	1.83	3.10	0.481	0.205	(0.241)	0.276
23	1.92	2.90	0.450	0.205	(0.225)	0.245
24	2.00	3.00	0.466	0.205	(0.233)	0.261
25	2.08	3.10	0.481	0.205	(0.241)	0.276
26	2.17	4.20	0.652	0.205	(0.326)	0.447
27	2.25	5.00	0.776	0.205	(0.388)	0.571
28	2.33	3.50	0.543	0.205	(0.272)	0.338
29	2.42	6.80	1.056	0.205	(0.528)	0.851
30	2.50	7.30	1.133	0.205	(0.567)	0.928
31	2.58	8.20	1.273	0.205	(0.636)	1.068
32	2.67	5.90	0.916	0.205	(0.458)	0.711
33	2.75	2.00	0.310	(0.205)	0.155	0.155
34	2.83	1.80	0.279	(0.205)	0.140	0.140
35	2.92	1.80	0.279	(0.205)	0.140	0.140
36	3.00	0.60	0.093	(0.205)	0.047	0.047
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	9.7

Flood volume = Effective rainfall 0.81(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.5(Ac.Ft)
Total soil loss = 0.49(In)
Total soil loss = 0.316(Ac.Ft)
Total rainfall = 1.29(In)
Flood volume = 22811.6 Cubic Feet
Total soil loss = 13769.7 Cubic Feet

Peak flow rate of this hydrograph = 7.299(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	2.5	5.0	7.5	10.0
0+ 5	0.0019	0.28	VQ				
0+10	0.0064	0.65	V Q				
0+15	0.0111	0.69	V Q				
0+20	0.0163	0.75	V Q				
0+25	0.0223	0.87	V Q				
0+30	0.0289	0.96	VQ				
0+35	0.0358	0.99	VQ				
0+40	0.0426	1.00	Q				
0+45	0.0500	1.07	VQ				
0+50	0.0571	1.02	Q				
0+55	0.0637	0.97	QV				
1+ 0	0.0707	1.02	QV				
1+ 5	0.0787	1.16	Q V				

```
    1+10       0.0876      1.29  |    QV   |         |         |         |
    1+15       0.0967      1.32  |    Q V  |         |         |         |
    1+20       0.1056      1.29  |    Q  V |         |         |         |
    1+25       0.1150      1.37  |    Q  V |         |         |         |
    1+30       0.1257      1.56  |     Q  V|         |         |         |
    1+35       0.1365      1.56  |     Q   V         |         |         |
    1+40       0.1472      1.56  |     Q   |V        |         |         |
    1+45       0.1604      1.91  |      Q  | V       |         |         |
    1+50       0.1754      2.18  |       Q |  V      |         |         |
    1+55       0.1897      2.07  |       Q |   V     |         |         |
    2+ 0       0.2035      2.01  |       Q |    V    |         |         |
    2+ 5       0.2179      2.09  |       Q |     V   |         |         |
    2+10       0.2359      2.62  |         Q       V |         |         |
    2+15       0.2606      3.59  |         |   Q     V|         |         |
    2+20       0.2851      3.55  |         |   Q      |V        |         |
    2+25       0.3147      4.29  |         |      Q   |   V     |         |
    2+30       0.3577      6.25  |         |          |    Q V  |         |
    2+35       0.4080      7.30  |         |          |       Q|V         |
    2+40       0.4565      7.04  |         |          |        Q|   V     |
    2+45       0.4870      4.43  |         |       Q  |         |     V   |
    2+50       0.5019      2.16  |       Q |          |         |      V  |
    2+55       0.5125      1.54  |     Q   |          |         |       V|
    3+ 0       0.5195      1.01  |   Q     |          |         |       V|
    3+ 5       0.5223      0.42  |Q        |          |         |       V|
    3+10       0.5232      0.13  Q         |          |         |       V|
    3+15       0.5235      0.05  Q         |          |         |       V|
    3+20       0.5237      0.02  Q         |          |         |       V|
    3+25       0.5237      0.00  Q         |          |         |        V
-------------------------------------------------------------------------
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro310610.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 2225.00(Ft.)
Length along longest watercourse measured to centroid = 1113.00(Ft.)
Length along longest watercourse = 0.421 Mi.
Length along longest watercourse measured to centroid = 0.211 Mi.
Difference in elevation = 82.00(Ft.)
Slope along watercourse = 194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.10	8.57

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	3.00	23.37

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 1.882(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 1.882(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	69.00	0.500

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
			Sum = 100.000 Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.113	(0.205)	0.056	0.056
2	0.17	0.60	0.135	(0.205)	0.068	0.068
3	0.25	0.60	0.135	(0.205)	0.068	0.068
4	0.33	0.60	0.135	(0.205)	0.068	0.068
5	0.42	0.60	0.135	(0.205)	0.068	0.068
6	0.50	0.70	0.158	(0.205)	0.079	0.079
7	0.58	0.70	0.158	(0.205)	0.079	0.079
8	0.67	0.70	0.158	(0.205)	0.079	0.079
9	0.75	0.70	0.158	(0.205)	0.079	0.079
10	0.83	0.70	0.158	(0.205)	0.079	0.079
11	0.92	0.70	0.158	(0.205)	0.079	0.079
12	1.00	0.80	0.181	(0.205)	0.090	0.090
13	1.08	0.80	0.181	(0.205)	0.090	0.090
14	1.17	0.80	0.181	(0.205)	0.090	0.090
15	1.25	0.80	0.181	(0.205)	0.090	0.090
16	1.33	0.80	0.181	(0.205)	0.090	0.090
17	1.42	0.80	0.181	(0.205)	0.090	0.090
18	1.50	0.80	0.181	(0.205)	0.090	0.090
19	1.58	0.80	0.181	(0.205)	0.090	0.090
20	1.67	0.80	0.181	(0.205)	0.090	0.090
21	1.75	0.80	0.181	(0.205)	0.090	0.090
22	1.83	0.80	0.181	(0.205)	0.090	0.090
23	1.92	0.80	0.181	(0.205)	0.090	0.090
24	2.00	0.90	0.203	(0.205)	0.102	0.102
25	2.08	0.80	0.181	(0.205)	0.090	0.090
26	2.17	0.90	0.203	(0.205)	0.102	0.102
27	2.25	0.90	0.203	(0.205)	0.102	0.102
28	2.33	0.90	0.203	(0.205)	0.102	0.102
29	2.42	0.90	0.203	(0.205)	0.102	0.102
30	2.50	0.90	0.203	(0.205)	0.102	0.102
31	2.58	0.90	0.203	(0.205)	0.102	0.102
32	2.67	0.90	0.203	(0.205)	0.102	0.102
33	2.75	1.00	0.226	(0.205)	0.113	0.113
34	2.83	1.00	0.226	(0.205)	0.113	0.113
35	2.92	1.00	0.226	(0.205)	0.113	0.113
36	3.00	1.00	0.226	(0.205)	0.113	0.113
37	3.08	1.00	0.226	(0.205)	0.113	0.113
38	3.17	1.10	0.248	(0.205)	0.124	0.124
39	3.25	1.10	0.248	(0.205)	0.124	0.124
40	3.33	1.10	0.248	(0.205)	0.124	0.124
41	3.42	1.20	0.271	(0.205)	0.135	0.135
42	3.50	1.30	0.294	(0.205)	0.147	0.147
43	3.58	1.40	0.316	(0.205)	0.158	0.158
44	3.67	1.40	0.316	(0.205)	0.158	0.158
45	3.75	1.50	0.339	(0.205)	0.169	0.169
46	3.83	1.50	0.339	(0.205)	0.169	0.169
47	3.92	1.60	0.361	(0.205)	0.181	0.181
48	4.00	1.60	0.361	(0.205)	0.181	0.181
49	4.08	1.70	0.384	(0.205)	0.192	0.192
50	4.17	1.80	0.406	(0.205)	0.203	0.203
51	4.25	1.90	0.429	0.205	(0.215)	0.224
52	4.33	2.00	0.452	0.205	(0.226)	0.247
53	4.42	2.10	0.474	0.205	(0.237)	0.269
54	4.50	2.10	0.474	0.205	(0.237)	0.269
55	4.58	2.20	0.497	0.205	(0.248)	0.292
56	4.67	2.30	0.519	0.205	(0.260)	0.314
57	4.75	2.40	0.542	0.205	(0.271)	0.337
58	4.83	2.40	0.542	0.205	(0.271)	0.337
59	4.92	2.50	0.564	0.205	(0.282)	0.359
60	5.00	2.60	0.587	0.205	(0.294)	0.382
61	5.08	3.10	0.700	0.205	(0.350)	0.495
62	5.17	3.60	0.813	0.205	(0.406)	0.608
63	5.25	3.90	0.881	0.205	(0.440)	0.676
64	5.33	4.20	0.948	0.205	(0.474)	0.743
65	5.42	4.70	1.061	0.205	(0.531)	0.856
66	5.50	5.60	1.264	0.205	(0.632)	1.059
67	5.58	1.90	0.429	0.205	(0.215)	0.224
68	5.67	0.90	0.203	(0.205)	0.102	0.102
69	5.75	0.60	0.135	(0.205)	0.068	0.068
70	5.83	0.50	0.113	(0.205)	0.056	0.056

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71   5.92     0.30      0.068       (  0.205)       0.034        0.034
72   6.00     0.20      0.045       (  0.205)       0.023        0.023
              (Loss Rate Not Used)
   Sum =     100.0                                  Sum =    13.4
      Flood volume = Effective rainfall      1.12(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       0.7(Ac.Ft)
      Total soil loss =      0.77(In)
      Total soil loss =     0.497(Ac.Ft)
      Total rainfall =      1.88(In)
      Flood volume =       31559.1 Cubic Feet
      Total soil loss =       21648.9 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      7.055(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f     H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
-------------------------------------------------------------------------
  0+ 5       0.0011      0.16  Q         |         |         |         |
  0+10       0.0038      0.39  VQ        |         |         |         |
  0+15       0.0071      0.48  VQ        |         |         |         |
  0+20       0.0106      0.51  V Q       |         |         |         |
  0+25       0.0142      0.53  V Q       |         |         |         |
  0+30       0.0181      0.56  V Q       |         |         |         |
  0+35       0.0223      0.60  |VQ       |         |         |         |
  0+40       0.0265      0.61  |VQ       |         |         |         |
  0+45       0.0307      0.62  |VQ       |         |         |         |
  0+50       0.0350      0.62  |VQ       |         |         |         |
  0+55       0.0393      0.62  | Q       |         |         |         |
  1+ 0       0.0438      0.65  | Q       |         |         |         |
  1+ 5       0.0486      0.69  | Q       |         |         |         |
  1+10       0.0534      0.70  | Q       |         |         |         |
  1+15       0.0583      0.71  | QV      |         |         |         |
  1+20       0.0631      0.71  | QV      |         |         |         |
  1+25       0.0680      0.71  | QV      |         |         |         |
  1+30       0.0729      0.71  | Q V     |         |         |         |
  1+35       0.0778      0.71  | Q V     |         |         |         |
  1+40       0.0827      0.71  | Q V     |         |         |         |
  1+45       0.0876      0.71  | Q V     |         |         |         |
  1+50       0.0925      0.71  | Q  V    |         |         |         |
  1+55       0.0973      0.71  | Q  V    |         |         |         |
  2+ 0       0.1024      0.74  | Q  V    |         |         |         |
  2+ 5       0.1076      0.75  |  Q V    |         |         |         |
  2+10       0.1128      0.75  |  Q  V   |         |         |         |
  2+15       0.1182      0.79  |  Q  V   |         |         |         |
  2+20       0.1237      0.79  |  Q  V   |         |         |         |
  2+25       0.1291      0.80  |  Q   V  |         |         |         |
  2+30       0.1346      0.80  |  Q   V  |         |         |         |
  2+35       0.1401      0.80  |  Q   V  |         |         |         |
  2+40       0.1456      0.80  |  Q    V |         |         |         |
  2+45       0.1513      0.83  |  Q    V |         |         |         |
  2+50       0.1573      0.87  |  Q    V |         |         |         |
  2+55       0.1634      0.88  |  Q     V|         |         |         |
  3+ 0       0.1695      0.88  |  Q     V|         |         |         |
  3+ 5       0.1756      0.89  |  Q     V|         |         |         |
  3+10       0.1819      0.92  |  Q      V         |         |         |
  3+15       0.1885      0.96  |  Q      V         |         |         |
  3+20       0.1952      0.97  |  Q      V         |         |         |
  3+25       0.2021      1.00  |   Q     |V        |         |         |
  3+30       0.2095      1.08  |   Q     |V        |         |         |
  3+35       0.2175      1.16  |   Q     | V       |         |         |
  3+40       0.2259      1.22  |   Q     | V       |         |         |
  3+45       0.2346      1.26  |    Q    | V       |         |         |
  3+50       0.2436      1.31  |    Q    |  V      |         |         |
  3+55       0.2529      1.35  |    Q    |  V      |         |         |
  4+ 0       0.2626      1.40  |    Q    |   V     |         |         |
  4+ 5       0.2725      1.44  |    Q    |    V    |         |         |
  4+10       0.2830      1.52  |     Q   |    V    |         |         |
  4+15       0.2942      1.63  |     Q   |     V   |         |         |
  4+20       0.3064      1.78  |      Q  |     V   |         |         |
  4+25       0.3199      1.95  |      Q  |      V  |         |         |
  4+30       0.3341      2.06  |       Q |       V |         |         |
  4+35       0.3489      2.16  |       Q |        V|         |         |
  4+40       0.3648      2.31  |        Q|         V         |         |
  4+45       0.3819      2.48  |        Q|          V        |         |
  4+50       0.3998      2.59  |         Q         | V       |         |
  4+55       0.4183      2.69  |         Q         |  V      |         |
  5+ 0       0.4379      2.85  |         |Q        |   V     |         |
  5+ 5       0.4604      3.26  |         |  Q      |    V    |         |
  5+10       0.4880      4.02  |         |    Q    |     V   |         |
  5+15       0.5206      4.72  |         |      Q  |      V  |         |
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    5+20       0.5570      5.30  |          |          |Q         V          |
    5+25       0.5982      5.97  |          |          |  Q       |  V       |
    5+30       0.6468      7.06  |          |          |        Q |    V     |
    5+35       0.6856      5.63  |          |          | Q        |      V   |
    5+40       0.7026      2.48  |        Q |          |          |       V  |
    5+45       0.7118      1.34  |     Q    |          |          |         V|
    5+50       0.7175      0.82  |   Q      |          |          |         V|
    5+55       0.7210      0.51  | Q        |          |          |         V|
    6+ 0       0.7230      0.29  |Q         |          |          |         V|
    6+ 5       0.7240      0.15  Q          |          |          |         V|
    6+10       0.7243      0.05  Q          |          |          |         V|
    6+15       0.7244      0.02  Q          |          |          |         V|
    6+20       0.7245      0.01  Q          |          |          |         V|
    6+25       0.7245      0.00  Q          |          |          |         V|
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U n i t H y d r o g r a p h A n a l y s i s

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Study date 04/22/24 File: pro3102410.out

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 2225.00(Ft.)
Length along longest watercourse measured to centroid = 1113.00(Ft.)
Length along longest watercourse = 0.421 Mi.
Length along longest watercourse measured to centroid = 0.211 Mi.
Difference in elevation = 82.00(Ft.)
Slope along watercourse = 194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.80	14.02

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	5.00	38.95

STORM EVENT (YEAR) = 10.00
Area Averaged 2-Year Rainfall = 1.800(In)
Area Averaged 100-Year Rainfall = 5.000(In)

Point rain (area averaged) = 3.117(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.116(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	69.00	0.500

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
			Sum = 100.000	Sum= 7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.025	(0.363)	0.012	0.012
2	0.17	0.07	0.025	(0.362)	0.012	0.012
3	0.25	0.07	0.025	(0.361)	0.012	0.012
4	0.33	0.10	0.037	(0.359)	0.019	0.019
5	0.42	0.10	0.037	(0.358)	0.019	0.019
6	0.50	0.10	0.037	(0.356)	0.019	0.019
7	0.58	0.10	0.037	(0.355)	0.019	0.019
8	0.67	0.10	0.037	(0.354)	0.019	0.019
9	0.75	0.10	0.037	(0.352)	0.019	0.019
10	0.83	0.13	0.050	(0.351)	0.025	0.025
11	0.92	0.13	0.050	(0.350)	0.025	0.025
12	1.00	0.13	0.050	(0.348)	0.025	0.025
13	1.08	0.10	0.037	(0.347)	0.019	0.019
14	1.17	0.10	0.037	(0.345)	0.019	0.019
15	1.25	0.10	0.037	(0.344)	0.019	0.019
16	1.33	0.10	0.037	(0.343)	0.019	0.019
17	1.42	0.10	0.037	(0.341)	0.019	0.019
18	1.50	0.10	0.037	(0.340)	0.019	0.019
19	1.58	0.10	0.037	(0.339)	0.019	0.019
20	1.67	0.10	0.037	(0.337)	0.019	0.019
21	1.75	0.10	0.037	(0.336)	0.019	0.019
22	1.83	0.13	0.050	(0.335)	0.025	0.025
23	1.92	0.13	0.050	(0.333)	0.025	0.025
24	2.00	0.13	0.050	(0.332)	0.025	0.025
25	2.08	0.13	0.050	(0.330)	0.025	0.025
26	2.17	0.13	0.050	(0.329)	0.025	0.025
27	2.25	0.13	0.050	(0.328)	0.025	0.025
28	2.33	0.13	0.050	(0.326)	0.025	0.025
29	2.42	0.13	0.050	(0.325)	0.025	0.025
30	2.50	0.13	0.050	(0.324)	0.025	0.025
31	2.58	0.17	0.062	(0.323)	0.031	0.031
32	2.67	0.17	0.062	(0.321)	0.031	0.031
33	2.75	0.17	0.062	(0.320)	0.031	0.031
34	2.83	0.17	0.062	(0.319)	0.031	0.031
35	2.92	0.17	0.062	(0.317)	0.031	0.031
36	3.00	0.17	0.062	(0.316)	0.031	0.031
37	3.08	0.17	0.062	(0.315)	0.031	0.031
38	3.17	0.17	0.062	(0.313)	0.031	0.031
39	3.25	0.17	0.062	(0.312)	0.031	0.031
40	3.33	0.17	0.062	(0.311)	0.031	0.031
41	3.42	0.17	0.062	(0.309)	0.031	0.031
42	3.50	0.17	0.062	(0.308)	0.031	0.031
43	3.58	0.17	0.062	(0.307)	0.031	0.031
44	3.67	0.17	0.062	(0.306)	0.031	0.031
45	3.75	0.17	0.062	(0.304)	0.031	0.031
46	3.83	0.20	0.075	(0.303)	0.037	0.037
47	3.92	0.20	0.075	(0.302)	0.037	0.037
48	4.00	0.20	0.075	(0.300)	0.037	0.037
49	4.08	0.20	0.075	(0.299)	0.037	0.037
50	4.17	0.20	0.075	(0.298)	0.037	0.037
51	4.25	0.20	0.075	(0.297)	0.037	0.037
52	4.33	0.23	0.087	(0.295)	0.044	0.044
53	4.42	0.23	0.087	(0.294)	0.044	0.044
54	4.50	0.23	0.087	(0.293)	0.044	0.044
55	4.58	0.23	0.087	(0.292)	0.044	0.044
56	4.67	0.23	0.087	(0.290)	0.044	0.044
57	4.75	0.23	0.087	(0.289)	0.044	0.044
58	4.83	0.27	0.100	(0.288)	0.050	0.050
59	4.92	0.27	0.100	(0.287)	0.050	0.050
60	5.00	0.27	0.100	(0.285)	0.050	0.050
61	5.08	0.20	0.075	(0.284)	0.037	0.037
62	5.17	0.20	0.075	(0.283)	0.037	0.037
63	5.25	0.20	0.075	(0.282)	0.037	0.037
64	5.33	0.23	0.087	(0.280)	0.044	0.044
65	5.42	0.23	0.087	(0.279)	0.044	0.044
66	5.50	0.23	0.087	(0.278)	0.044	0.044
67	5.58	0.27	0.100	(0.277)	0.050	0.050
68	5.67	0.27	0.100	(0.275)	0.050	0.050
69	5.75	0.27	0.100	(0.274)	0.050	0.050
70	5.83	0.27	0.100	(0.273)	0.050	0.050

71	5.92	0.27	0.100	(0.272)	0.050	0.050
72	6.00	0.27	0.100	(0.271)	0.050	0.050
73	6.08	0.30	0.112	(0.269)	0.056	0.056
74	6.17	0.30	0.112	(0.268)	0.056	0.056
75	6.25	0.30	0.112	(0.267)	0.056	0.056
76	6.33	0.30	0.112	(0.266)	0.056	0.056
77	6.42	0.30	0.112	(0.265)	0.056	0.056
78	6.50	0.30	0.112	(0.263)	0.056	0.056
79	6.58	0.33	0.125	(0.262)	0.062	0.062
80	6.67	0.33	0.125	(0.261)	0.062	0.062
81	6.75	0.33	0.125	(0.260)	0.062	0.062
82	6.83	0.33	0.125	(0.259)	0.062	0.062
83	6.92	0.33	0.125	(0.258)	0.062	0.062
84	7.00	0.33	0.125	(0.256)	0.062	0.062
85	7.08	0.33	0.125	(0.255)	0.062	0.062
86	7.17	0.33	0.125	(0.254)	0.062	0.062
87	7.25	0.33	0.125	(0.253)	0.062	0.062
88	7.33	0.37	0.137	(0.252)	0.069	0.069
89	7.42	0.37	0.137	(0.251)	0.069	0.069
90	7.50	0.37	0.137	(0.249)	0.069	0.069
91	7.58	0.40	0.150	(0.248)	0.075	0.075
92	7.67	0.40	0.150	(0.247)	0.075	0.075
93	7.75	0.40	0.150	(0.246)	0.075	0.075
94	7.83	0.43	0.162	(0.245)	0.081	0.081
95	7.92	0.43	0.162	(0.244)	0.081	0.081
96	8.00	0.43	0.162	(0.243)	0.081	0.081
97	8.08	0.50	0.187	(0.242)	0.093	0.093
98	8.17	0.50	0.187	(0.240)	0.093	0.093
99	8.25	0.50	0.187	(0.239)	0.093	0.093
100	8.33	0.50	0.187	(0.238)	0.093	0.093
101	8.42	0.50	0.187	(0.237)	0.093	0.093
102	8.50	0.50	0.187	(0.236)	0.093	0.093
103	8.58	0.53	0.199	(0.235)	0.100	0.100
104	8.67	0.53	0.199	(0.234)	0.100	0.100
105	8.75	0.53	0.199	(0.233)	0.100	0.100
106	8.83	0.57	0.212	(0.232)	0.106	0.106
107	8.92	0.57	0.212	(0.230)	0.106	0.106
108	9.00	0.57	0.212	(0.229)	0.106	0.106
109	9.08	0.63	0.237	(0.228)	0.118	0.118
110	9.17	0.63	0.237	(0.227)	0.118	0.118
111	9.25	0.63	0.237	(0.226)	0.118	0.118
112	9.33	0.67	0.249	(0.225)	0.125	0.125
113	9.42	0.67	0.249	(0.224)	0.125	0.125
114	9.50	0.67	0.249	(0.223)	0.125	0.125
115	9.58	0.70	0.262	(0.222)	0.131	0.131
116	9.67	0.70	0.262	(0.221)	0.131	0.131
117	9.75	0.70	0.262	(0.220)	0.131	0.131
118	9.83	0.73	0.274	(0.219)	0.137	0.137
119	9.92	0.73	0.274	(0.218)	0.137	0.137
120	10.00	0.73	0.274	(0.217)	0.137	0.137
121	10.08	0.50	0.187	(0.215)	0.093	0.093
122	10.17	0.50	0.187	(0.214)	0.093	0.093
123	10.25	0.50	0.187	(0.213)	0.093	0.093
124	10.33	0.50	0.187	(0.212)	0.093	0.093
125	10.42	0.50	0.187	(0.211)	0.093	0.093
126	10.50	0.50	0.187	(0.210)	0.093	0.093
127	10.58	0.67	0.249	(0.209)	0.125	0.125
128	10.67	0.67	0.249	(0.208)	0.125	0.125
129	10.75	0.67	0.249	(0.207)	0.125	0.125
130	10.83	0.67	0.249	(0.206)	0.125	0.125
131	10.92	0.67	0.249	(0.205)	0.125	0.125
132	11.00	0.67	0.249	(0.204)	0.125	0.125
133	11.08	0.63	0.237	(0.203)	0.118	0.118
134	11.17	0.63	0.237	(0.202)	0.118	0.118
135	11.25	0.63	0.237	(0.201)	0.118	0.118
136	11.33	0.63	0.237	(0.200)	0.118	0.118
137	11.42	0.63	0.237	(0.199)	0.118	0.118
138	11.50	0.63	0.237	(0.198)	0.118	0.118
139	11.58	0.57	0.212	(0.197)	0.106	0.106
140	11.67	0.57	0.212	(0.196)	0.106	0.106
141	11.75	0.57	0.212	(0.195)	0.106	0.106
142	11.83	0.60	0.224	(0.194)	0.112	0.112
143	11.92	0.60	0.224	(0.193)	0.112	0.112
144	12.00	0.60	0.224	(0.192)	0.112	0.112
145	12.08	0.83	0.312	(0.191)	0.156	0.156
146	12.17	0.83	0.312	(0.190)	0.156	0.156
147	12.25	0.83	0.312	(0.189)	0.156	0.156
148	12.33	0.87	0.324	(0.189)	0.162	0.162
149	12.42	0.87	0.324	(0.188)	0.162	0.162
150	12.50	0.87	0.324	(0.187)	0.162	0.162
151	12.58	0.93	0.349	(0.186)	0.175	0.175
152	12.67	0.93	0.349	(0.185)	0.175	0.175
153	12.75	0.93	0.349	(0.184)	0.175	0.175
154	12.83	0.97	0.362	(0.183)	0.181	0.181
155	12.92	0.97	0.362	(0.182)	0.181	0.181
156	13.00	0.97	0.362	(0.181)	0.181	0.181

157	13.08	1.13	0.424	0.180	(0.212)	0.244
158	13.17	1.13	0.424	0.179	(0.212)	0.245
159	13.25	1.13	0.424	0.178	(0.212)	0.246
160	13.33	1.13	0.424	0.177	(0.212)	0.246
161	13.42	1.13	0.424	0.177	(0.212)	0.247
162	13.50	1.13	0.424	0.176	(0.212)	0.248
163	13.58	0.77	0.287	(0.175)	0.143	0.143
164	13.67	0.77	0.287	(0.174)	0.143	0.143
165	13.75	0.77	0.287	(0.173)	0.143	0.143
166	13.83	0.77	0.287	(0.172)	0.143	0.143
167	13.92	0.77	0.287	(0.171)	0.143	0.143
168	14.00	0.77	0.287	(0.170)	0.143	0.143
169	14.08	0.90	0.337	(0.169)	0.168	0.168
170	14.17	0.90	0.337	(0.169)	0.168	0.168
171	14.25	0.90	0.337	0.168	(0.168)	0.169
172	14.33	0.87	0.324	(0.167)	0.162	0.162
173	14.42	0.87	0.324	(0.166)	0.162	0.162
174	14.50	0.87	0.324	(0.165)	0.162	0.162
175	14.58	0.87	0.324	(0.164)	0.162	0.162
176	14.67	0.87	0.324	(0.163)	0.162	0.162
177	14.75	0.87	0.324	(0.163)	0.162	0.162
178	14.83	0.83	0.312	(0.162)	0.156	0.156
179	14.92	0.83	0.312	(0.161)	0.156	0.156
180	15.00	0.83	0.312	(0.160)	0.156	0.156
181	15.08	0.80	0.299	(0.159)	0.150	0.150
182	15.17	0.80	0.299	(0.159)	0.150	0.150
183	15.25	0.80	0.299	(0.158)	0.150	0.150
184	15.33	0.77	0.287	(0.157)	0.143	0.143
185	15.42	0.77	0.287	(0.156)	0.143	0.143
186	15.50	0.77	0.287	(0.155)	0.143	0.143
187	15.58	0.63	0.237	(0.154)	0.118	0.118
188	15.67	0.63	0.237	(0.154)	0.118	0.118
189	15.75	0.63	0.237	(0.153)	0.118	0.118
190	15.83	0.63	0.237	(0.152)	0.118	0.118
191	15.92	0.63	0.237	(0.151)	0.118	0.118
192	16.00	0.63	0.237	(0.151)	0.118	0.118
193	16.08	0.13	0.050	(0.150)	0.025	0.025
194	16.17	0.13	0.050	(0.149)	0.025	0.025
195	16.25	0.13	0.050	(0.148)	0.025	0.025
196	16.33	0.13	0.050	(0.148)	0.025	0.025
197	16.42	0.13	0.050	(0.147)	0.025	0.025
198	16.50	0.13	0.050	(0.146)	0.025	0.025
199	16.58	0.10	0.037	(0.145)	0.019	0.019
200	16.67	0.10	0.037	(0.145)	0.019	0.019
201	16.75	0.10	0.037	(0.144)	0.019	0.019
202	16.83	0.10	0.037	(0.143)	0.019	0.019
203	16.92	0.10	0.037	(0.142)	0.019	0.019
204	17.00	0.10	0.037	(0.142)	0.019	0.019
205	17.08	0.17	0.062	(0.141)	0.031	0.031
206	17.17	0.17	0.062	(0.140)	0.031	0.031
207	17.25	0.17	0.062	(0.140)	0.031	0.031
208	17.33	0.17	0.062	(0.139)	0.031	0.031
209	17.42	0.17	0.062	(0.138)	0.031	0.031
210	17.50	0.17	0.062	(0.137)	0.031	0.031
211	17.58	0.17	0.062	(0.137)	0.031	0.031
212	17.67	0.17	0.062	(0.136)	0.031	0.031
213	17.75	0.17	0.062	(0.135)	0.031	0.031
214	17.83	0.13	0.050	(0.135)	0.025	0.025
215	17.92	0.13	0.050	(0.134)	0.025	0.025
216	18.00	0.13	0.050	(0.133)	0.025	0.025
217	18.08	0.13	0.050	(0.133)	0.025	0.025
218	18.17	0.13	0.050	(0.132)	0.025	0.025
219	18.25	0.13	0.050	(0.131)	0.025	0.025
220	18.33	0.13	0.050	(0.131)	0.025	0.025
221	18.42	0.13	0.050	(0.130)	0.025	0.025
222	18.50	0.13	0.050	(0.130)	0.025	0.025
223	18.58	0.10	0.037	(0.129)	0.019	0.019
224	18.67	0.10	0.037	(0.128)	0.019	0.019
225	18.75	0.10	0.037	(0.128)	0.019	0.019
226	18.83	0.07	0.025	(0.127)	0.012	0.012
227	18.92	0.07	0.025	(0.126)	0.012	0.012
228	19.00	0.07	0.025	(0.126)	0.012	0.012
229	19.08	0.10	0.037	(0.125)	0.019	0.019
230	19.17	0.10	0.037	(0.125)	0.019	0.019
231	19.25	0.10	0.037	(0.124)	0.019	0.019
232	19.33	0.13	0.050	(0.123)	0.025	0.025
233	19.42	0.13	0.050	(0.123)	0.025	0.025
234	19.50	0.13	0.050	(0.122)	0.025	0.025
235	19.58	0.10	0.037	(0.122)	0.019	0.019
236	19.67	0.10	0.037	(0.121)	0.019	0.019
237	19.75	0.10	0.037	(0.121)	0.019	0.019
238	19.83	0.07	0.025	(0.120)	0.012	0.012
239	19.92	0.07	0.025	(0.120)	0.012	0.012
240	20.00	0.07	0.025	(0.119)	0.012	0.012
241	20.08	0.10	0.037	(0.119)	0.019	0.019
242	20.17	0.10	0.037	(0.118)	0.019	0.019

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243  20.25     0.10      0.037       (  0.118)       0.019        0.019
244  20.33     0.10      0.037       (  0.117)       0.019        0.019
245  20.42     0.10      0.037       (  0.116)       0.019        0.019
246  20.50     0.10      0.037       (  0.116)       0.019        0.019
247  20.58     0.10      0.037       (  0.116)       0.019        0.019
248  20.67     0.10      0.037       (  0.115)       0.019        0.019
249  20.75     0.10      0.037       (  0.115)       0.019        0.019
250  20.83     0.07      0.025       (  0.114)       0.012        0.012
251  20.92     0.07      0.025       (  0.114)       0.012        0.012
252  21.00     0.07      0.025       (  0.113)       0.012        0.012
253  21.08     0.10      0.037       (  0.113)       0.019        0.019
254  21.17     0.10      0.037       (  0.112)       0.019        0.019
255  21.25     0.10      0.037       (  0.112)       0.019        0.019
256  21.33     0.07      0.025       (  0.111)       0.012        0.012
257  21.42     0.07      0.025       (  0.111)       0.012        0.012
258  21.50     0.07      0.025       (  0.111)       0.012        0.012
259  21.58     0.10      0.037       (  0.110)       0.019        0.019
260  21.67     0.10      0.037       (  0.110)       0.019        0.019
261  21.75     0.10      0.037       (  0.109)       0.019        0.019
262  21.83     0.07      0.025       (  0.109)       0.012        0.012
263  21.92     0.07      0.025       (  0.109)       0.012        0.012
264  22.00     0.07      0.025       (  0.108)       0.012        0.012
265  22.08     0.10      0.037       (  0.108)       0.019        0.019
266  22.17     0.10      0.037       (  0.108)       0.019        0.019
267  22.25     0.10      0.037       (  0.107)       0.019        0.019
268  22.33     0.07      0.025       (  0.107)       0.012        0.012
269  22.42     0.07      0.025       (  0.107)       0.012        0.012
270  22.50     0.07      0.025       (  0.106)       0.012        0.012
271  22.58     0.07      0.025       (  0.106)       0.012        0.012
272  22.67     0.07      0.025       (  0.106)       0.012        0.012
273  22.75     0.07      0.025       (  0.105)       0.012        0.012
274  22.83     0.07      0.025       (  0.105)       0.012        0.012
275  22.92     0.07      0.025       (  0.105)       0.012        0.012
276  23.00     0.07      0.025       (  0.105)       0.012        0.012
277  23.08     0.07      0.025       (  0.104)       0.012        0.012
278  23.17     0.07      0.025       (  0.104)       0.012        0.012
279  23.25     0.07      0.025       (  0.104)       0.012        0.012
280  23.33     0.07      0.025       (  0.104)       0.012        0.012
281  23.42     0.07      0.025       (  0.103)       0.012        0.012
282  23.50     0.07      0.025       (  0.103)       0.012        0.012
283  23.58     0.07      0.025       (  0.103)       0.012        0.012
284  23.67     0.07      0.025       (  0.103)       0.012        0.012
285  23.75     0.07      0.025       (  0.103)       0.012        0.012
286  23.83     0.07      0.025       (  0.103)       0.012        0.012
287  23.92     0.07      0.025       (  0.103)       0.012        0.012
288  24.00     0.07      0.025       (  0.103)       0.012        0.012
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    18.9
      Flood volume = Effective rainfall      1.58(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       1.0(Ac.Ft)
      Total soil loss =      1.54(In)
      Total soil loss =     1.000(Ac.Ft)
      Total rainfall =      3.12(In)
      Flood volume =       44545.8 Cubic Feet
      Total soil loss =       43580.5 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      1.943(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0002      0.03  Q          |         |         |         |
   0+10       0.0008      0.08  Q          |         |         |         |
   0+15       0.0014      0.09  Q          |         |         |         |
   0+20       0.0022      0.11  Q          |         |         |         |
   0+25       0.0031      0.14  Q          |         |         |         |
   0+30       0.0041      0.14  Q          |         |         |         |
   0+35       0.0051      0.15  Q          |         |         |         |
   0+40       0.0061      0.15  Q          |         |         |         |
   0+45       0.0071      0.15  Q          |         |         |         |
   0+50       0.0083      0.16  Q          |         |         |         |
   0+55       0.0095      0.19  Q          |         |         |         |
   1+ 0       0.0109      0.19  Q          |         |         |         |
   1+ 5       0.0121      0.18  Q          |         |         |         |
   1+10       0.0132      0.16  Q          |         |         |         |
   1+15       0.0142      0.15  Q          |         |         |         |
   1+20       0.0152      0.15  Q          |         |         |         |
   1+25       0.0162      0.15  Q          |         |         |         |
   1+30       0.0172      0.15  Q          |         |         |         |
   1+35       0.0183      0.15  Q          |         |         |         |
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1+40      0.0193      0.15  Q          |          |          |          |
1+45      0.0203      0.15  Q          |          |          |          |
1+50      0.0214      0.16  Q          |          |          |          |
1+55      0.0227      0.19  Q          |          |          |          |
2+ 0      0.0240      0.19  Q          |          |          |          |
2+ 5      0.0254      0.19  Q          |          |          |          |
2+10      0.0267      0.20  QV         |          |          |          |
2+15      0.0281      0.20  QV         |          |          |          |
2+20      0.0294      0.20  QV         |          |          |          |
2+25      0.0307      0.20  QV         |          |          |          |
2+30      0.0321      0.20  QV         |          |          |          |
2+35      0.0336      0.21  QV         |          |          |          |
2+40      0.0352      0.24  QV         |          |          |          |
2+45      0.0368      0.24  QV         |          |          |          |
2+50      0.0385      0.24  QV         |          |          |          |
2+55      0.0402      0.24  QV         |          |          |          |
3+ 0      0.0419      0.24  QV         |          |          |          |
3+ 5      0.0436      0.24  QV         |          |          |          |
3+10      0.0453      0.24  QV         |          |          |          |
3+15      0.0469      0.24  QV         |          |          |          |
3+20      0.0486      0.24  QV         |          |          |          |
3+25      0.0503      0.24  QV         |          |          |          |
3+30      0.0520      0.24  Q V        |          |          |          |
3+35      0.0537      0.24  Q V        |          |          |          |
3+40      0.0554      0.24  Q V        |          |          |          |
3+45      0.0571      0.24  Q V        |          |          |          |
3+50      0.0589      0.26  |QV        |          |          |          |
3+55      0.0608      0.28  |QV        |          |          |          |
4+ 0      0.0628      0.29  |QV        |          |          |          |
4+ 5      0.0648      0.29  |QV        |          |          |          |
4+10      0.0669      0.29  |QV        |          |          |          |
4+15      0.0689      0.29  |QV        |          |          |          |
4+20      0.0710      0.31  |QV        |          |          |          |
4+25      0.0733      0.33  |QV        |          |          |          |
4+30      0.0757      0.34  |QV        |          |          |          |
4+35      0.0780      0.34  |Q V       |          |          |          |
4+40      0.0804      0.34  |Q V       |          |          |          |
4+45      0.0827      0.34  |Q V       |          |          |          |
4+50      0.0852      0.36  |Q V       |          |          |          |
4+55      0.0878      0.38  |Q V       |          |          |          |
5+ 0      0.0905      0.39  |Q V       |          |          |          |
5+ 5      0.0930      0.36  |Q V       |          |          |          |
5+10      0.0951      0.31  |Q V       |          |          |          |
5+15      0.0972      0.30  |Q V       |          |          |          |
5+20      0.0993      0.31  |Q V       |          |          |          |
5+25      0.1016      0.33  |Q V       |          |          |          |
5+30      0.1040      0.34  |Q  V      |          |          |          |
5+35      0.1064      0.36  |Q  V      |          |          |          |
5+40      0.1091      0.38  |Q  V      |          |          |          |
5+45      0.1117      0.39  |Q  V      |          |          |          |
5+50      0.1144      0.39  |Q  V      |          |          |          |
5+55      0.1171      0.39  |Q  V      |          |          |          |
6+ 0      0.1198      0.39  |Q  V      |          |          |          |
6+ 5      0.1226      0.41  |Q  V      |          |          |          |
6+10      0.1256      0.43  |Q  V      |          |          |          |
6+15      0.1286      0.44  |Q   V     |          |          |          |
6+20      0.1316      0.44  |Q   V     |          |          |          |
6+25      0.1347      0.44  |Q   V     |          |          |          |
6+30      0.1377      0.44  |Q   V     |          |          |          |
6+35      0.1409      0.46  |Q   V     |          |          |          |
6+40      0.1442      0.48  |Q   V     |          |          |          |
6+45      0.1475      0.49  |Q   V     |          |          |          |
6+50      0.1509      0.49  |Q   V     |          |          |          |
6+55      0.1543      0.49  |Q    V    |          |          |          |
7+ 0      0.1576      0.49  |Q    V    |          |          |          |
7+ 5      0.1610      0.49  |Q    V    |          |          |          |
7+10      0.1644      0.49  |Q    V    |          |          |          |
7+15      0.1677      0.49  |Q    V    |          |          |          |
7+20      0.1712      0.51  | Q   V    |          |          |          |
7+25      0.1749      0.53  | Q   V    |          |          |          |
7+30      0.1786      0.53  | Q   V    |          |          |          |
7+35      0.1824      0.55  | Q    V   |          |          |          |
7+40      0.1864      0.58  | Q    V   |          |          |          |
7+45      0.1904      0.58  | Q    V   |          |          |          |
7+50      0.1945      0.60  | Q    V   |          |          |          |
7+55      0.1988      0.63  | Q    V   |          |          |          |
8+ 0      0.2032      0.63  | Q    V   |          |          |          |
8+ 5      0.2078      0.67  | Q     V  |          |          |          |
8+10      0.2127      0.72  | Q     V  |          |          |          |
8+15      0.2178      0.73  | Q     V  |          |          |          |
8+20      0.2228      0.73  | Q     V  |          |          |          |
8+25      0.2278      0.73  | Q     V  |          |          |          |
8+30      0.2329      0.73  | Q      V |          |          |          |
8+35      0.2381      0.75  |  Q     V |          |          |          |
8+40      0.2434      0.77  |  Q     V |          |          |          |
8+45      0.2488      0.78  |  Q     V |          |          |          |
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 8+50       0.2543      0.80  |  Q     V|          |          |          |
 8+55       0.2599      0.82  |  Q      V          |          |          |
 9+ 0       0.2657      0.83  |  Q      V          |          |          |
 9+ 5       0.2716      0.87  |  Q      V          |          |          |
 9+10       0.2779      0.91  |  Q      V          |          |          |
 9+15       0.2842      0.92  |  Q      |V         |          |          |
 9+20       0.2907      0.94  |  Q      |V         |          |          |
 9+25       0.2974      0.97  |  Q      |V         |          |          |
 9+30       0.3041      0.98  |  Q      |V         |          |          |
 9+35       0.3110      0.99  |  Q      | V        |          |          |
 9+40       0.3180      1.02  |    Q    | V        |          |          |
 9+45       0.3251      1.02  |    Q    | V        |          |          |
 9+50       0.3322      1.04  |    Q    | V        |          |          |
 9+55       0.3396      1.07  |    Q    |  V       |          |          |
10+ 0       0.3470      1.07  |    Q    |  V       |          |          |
10+ 5       0.3536      0.96  |  Q      |  V       |          |          |
10+10       0.3591      0.80  |  Q      |   V      |          |          |
10+15       0.3643      0.76  |  Q      |   V      |          |          |
10+20       0.3694      0.75  |Q        |   V      |          |          |
10+25       0.3745      0.74  |Q        |   V      |          |          |
10+30       0.3796      0.73  |Q        |   V      |          |          |
10+35       0.3852      0.82  |  Q      |    V     |          |          |
10+40       0.3917      0.93  |  Q      |    V     |          |          |
10+45       0.3983      0.96  |  Q      |    V     |          |          |
10+50       0.4050      0.97  |  Q      |    V     |          |          |
10+55       0.4117      0.98  |  Q      |     V    |          |          |
11+ 0       0.4184      0.98  |  Q      |     V    |          |          |
11+ 5       0.4251      0.96  |  Q      |     V    |          |          |
11+10       0.4315      0.94  |  Q      |     V    |          |          |
11+15       0.4380      0.93  |  Q      |      V   |          |          |
11+20       0.4444      0.93  |  Q      |      V   |          |          |
11+25       0.4508      0.93  |  Q      |      V   |          |          |
11+30       0.4572      0.93  |  Q      |      V   |          |          |
11+35       0.4634      0.90  |  Q      |       V  |          |          |
11+40       0.4692      0.85  |  Q      |       V  |          |          |
11+45       0.4750      0.84  |  Q      |       V  |          |          |
11+50       0.4809      0.85  |  Q      |       V  |          |          |
11+55       0.4869      0.87  |  Q      |        V|          |          |
12+ 0       0.4929      0.88  |  Q      |        V|          |          |
12+ 5       0.4998      1.00  |  Q      |        V|          |          |
12+10       0.5078      1.16  |    Q    |        V|          |          |
12+15       0.5161      1.20  |    Q    |         V          |          |
12+20       0.5245      1.23  |    Q    |         V          |          |
12+25       0.5332      1.26  |      Q  |         V          |          |
12+30       0.5419      1.27  |      Q  |         |V         |          |
12+35       0.5509      1.31  |      Q  |         |V         |          |
12+40       0.5603      1.35  |      Q  |         |V         |          |
12+45       0.5696      1.36  |      Q  |         | V        |          |
12+50       0.5792      1.38  |      Q  |         | V        |          |
12+55       0.5889      1.41  |      Q  |         |  V       |          |
13+ 0       0.5986      1.42  |      Q  |         |  V       |          |
13+ 5       0.6096      1.59  |       Q |         |  V       |          |
13+10       0.6222      1.82  |        Q|         |   V      |          |
13+15       0.6351      1.88  |        Q|         |   V      |          |
13+20       0.6483      1.91  |        Q|         |    V     |          |
13+25       0.6616      1.93  |        Q|         |    V     |          |
13+30       0.6750      1.94  |        Q|         |     V    |          |
13+35       0.6864      1.66  |       Q |         |     V    |          |
13+40       0.6952      1.28  |      Q  |         |      V   |          |
13+45       0.7034      1.19  |    Q    |         |      V   |          |
13+50       0.7114      1.15  |    Q    |         |      V   |          |
13+55       0.7192      1.13  |    Q    |         |       V  |          |
14+ 0       0.7269      1.13  |    Q    |         |       V  |          |
14+ 5       0.7352      1.19  |    Q    |         |       V  |          |
14+10       0.7440      1.29  |      Q  |         |        V|          |
14+15       0.7530      1.31  |      Q  |         |        V|          |
14+20       0.7620      1.30  |      Q  |         |        V|          |
14+25       0.7708      1.28  |      Q  |         |         V          |
14+30       0.7796      1.28  |      Q  |         |         V          |
14+35       0.7884      1.27  |      Q  |         |         V          |
14+40       0.7971      1.27  |      Q  |         |         |V         |
14+45       0.8059      1.27  |      Q  |         |         |V         |
14+50       0.8146      1.26  |      Q  |         |         |V         |
14+55       0.8230      1.23  |    Q    |         |         | V        |
15+ 0       0.8315      1.23  |    Q    |         |         | V        |
15+ 5       0.8398      1.21  |    Q    |         |         | V        |
15+10       0.8480      1.18  |    Q    |         |         |  V       |
15+15       0.8561      1.18  |    Q    |         |         |  V       |
15+20       0.8641      1.16  |    Q    |         |         |  V       |
15+25       0.8719      1.14  |    Q    |         |         |   V      |
15+30       0.8797      1.13  |    Q    |         |         |   V      |
15+35       0.8870      1.06  |    Q    |         |         |   V      |
15+40       0.8936      0.97  |  Q      |         |         |   V      |
15+45       0.9001      0.95  |  Q      |         |         |    V     |
15+50       0.9066      0.94  |  Q      |         |         |    V     |
15+55       0.9130      0.93  |  Q      |         |         |    V     |
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16+ 0       0.9194      0.93  |  Q      |         |         |    V    |
16+ 5       0.9241      0.67  | Q       |         |         |     V   |
16+10       0.9263      0.33  |Q        |         |         |     V   |
16+15       0.9281      0.25  |Q        |         |         |     V   |
16+20       0.9296      0.22  Q         |         |         |     V   |
16+25       0.9310      0.20  Q         |         |         |     V   |
16+30       0.9323      0.20  Q         |         |         |     V   |
16+35       0.9336      0.18  Q         |         |         |     V   |
16+40       0.9346      0.16  Q         |         |         |     V   |
16+45       0.9357      0.15  Q         |         |         |     V   |
16+50       0.9367      0.15  Q         |         |         |     V   |
16+55       0.9377      0.15  Q         |         |         |     V   |
17+ 0       0.9387      0.15  Q         |         |         |     V   |
17+ 5       0.9400      0.18  Q         |         |         |     V   |
17+10       0.9415      0.23  Q         |         |         |     V   |
17+15       0.9432      0.24  Q         |         |         |     V   |
17+20       0.9448      0.24  Q         |         |         |     V   |
17+25       0.9465      0.24  Q         |         |         |      V  |
17+30       0.9482      0.24  Q         |         |         |      V  |
17+35       0.9499      0.24  Q         |         |         |      V  |
17+40       0.9516      0.24  Q         |         |         |      V  |
17+45       0.9533      0.24  Q         |         |         |      V  |
17+50       0.9548      0.23  Q         |         |         |      V  |
17+55       0.9562      0.20  Q         |         |         |      V  |
18+ 0       0.9576      0.20  Q         |         |         |      V  |
18+ 5       0.9590      0.20  Q         |         |         |      V  |
18+10       0.9603      0.20  Q         |         |         |      V  |
18+15       0.9617      0.20  Q         |         |         |      V  |
18+20       0.9630      0.20  Q         |         |         |      V  |
18+25       0.9644      0.20  Q         |         |         |      V  |
18+30       0.9657      0.20  Q         |         |         |      V  |
18+35       0.9669      0.18  Q         |         |         |      V  |
18+40       0.9680      0.16  Q         |         |         |      V  |
18+45       0.9691      0.15  Q         |         |         |      V  |
18+50       0.9700      0.13  Q         |         |         |      V  |
18+55       0.9707      0.11  Q         |         |         |      V  |
19+ 0       0.9714      0.10  Q         |         |         |      V  |
19+ 5       0.9722      0.12  Q         |         |         |       V |
19+10       0.9732      0.14  Q         |         |         |       V |
19+15       0.9741      0.14  Q         |         |         |       V |
19+20       0.9753      0.16  Q         |         |         |       V |
19+25       0.9765      0.19  Q         |         |         |       V |
19+30       0.9779      0.19  Q         |         |         |       V |
19+35       0.9791      0.18  Q         |         |         |       V |
19+40       0.9802      0.16  Q         |         |         |       V |
19+45       0.9812      0.15  Q         |         |         |       V |
19+50       0.9821      0.13  Q         |         |         |       V |
19+55       0.9828      0.11  Q         |         |         |       V |
20+ 0       0.9835      0.10  Q         |         |         |       V |
20+ 5       0.9843      0.12  Q         |         |         |       V |
20+10       0.9853      0.14  Q         |         |         |       V |
20+15       0.9863      0.14  Q         |         |         |       V |
20+20       0.9873      0.15  Q         |         |         |       V |
20+25       0.9883      0.15  Q         |         |         |       V |
20+30       0.9893      0.15  Q         |         |         |       V |
20+35       0.9903      0.15  Q         |         |         |       V |
20+40       0.9913      0.15  Q         |         |         |       V |
20+45       0.9923      0.15  Q         |         |         |       V |
20+50       0.9932      0.13  Q         |         |         |       V |
20+55       0.9940      0.11  Q         |         |         |       V |
21+ 0       0.9947      0.10  Q         |         |         |       V |
21+ 5       0.9955      0.12  Q         |         |         |       V |
21+10       0.9964      0.14  Q         |         |         |       V |
21+15       0.9974      0.14  Q         |         |         |        V|
21+20       0.9983      0.13  Q         |         |         |        V|
21+25       0.9990      0.11  Q         |         |         |        V|
21+30       0.9997      0.10  Q         |         |         |        V|
21+35       1.0005      0.12  Q         |         |         |        V|
21+40       1.0015      0.14  Q         |         |         |        V|
21+45       1.0025      0.14  Q         |         |         |        V|
21+50       1.0033      0.13  Q         |         |         |        V|
21+55       1.0041      0.11  Q         |         |         |        V|
22+ 0       1.0048      0.10  Q         |         |         |        V|
22+ 5       1.0056      0.12  Q         |         |         |        V|
22+10       1.0065      0.14  Q         |         |         |        V|
22+15       1.0075      0.14  Q         |         |         |        V|
22+20       1.0084      0.13  Q         |         |         |        V|
22+25       1.0091      0.11  Q         |         |         |        V|
22+30       1.0098      0.10  Q         |         |         |        V|
22+35       1.0105      0.10  Q         |         |         |        V|
22+40       1.0112      0.10  Q         |         |         |        V|
22+45       1.0119      0.10  Q         |         |         |        V|
22+50       1.0125      0.10  Q         |         |         |        V|
22+55       1.0132      0.10  Q         |         |         |        V|
23+ 0       1.0139      0.10  Q         |         |         |        V|
23+ 5       1.0146      0.10  Q         |         |         |        V|
```

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   23+10       1.0152      0.10  Q          |          |          |          v|
   23+15       1.0159      0.10  Q          |          |          |          v|
   23+20       1.0166      0.10  Q          |          |          |          v|
   23+25       1.0173      0.10  Q          |          |          |          v|
   23+30       1.0179      0.10  Q          |          |          |          v|
   23+35       1.0186      0.10  Q          |          |          |          v|
   23+40       1.0193      0.10  Q          |          |          |          v|
   23+45       1.0200      0.10  Q          |          |          |          v|
   23+50       1.0206      0.10  Q          |          |          |          v|
   23+55       1.0213      0.10  Q          |          |          |          v|
   24+ 0       1.0220      0.10  Q          |          |          |          v|
   24+ 5       1.0224      0.06  Q          |          |          |          v|
   24+10       1.0226      0.02  Q          |          |          |          v|
   24+15       1.0226      0.01  Q          |          |          |          v|
   24+20       1.0226      0.00  Q          |          |          |          v|
   24+25       1.0226      0.00  Q          |          |          |          v|
-------------------------------------------------------------------------------
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        U n i t   H y d r o g r a p h   A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =       7.79(Ac.)  =      0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =       7.79(Ac.)  =      0.012 Sq. Mi.
Length along longest watercourse =    2225.00(Ft.)
Length along longest watercourse measured to centroid =    1113.00(Ft.)
Length along longest watercourse =      0.421 Mi.
Length along longest watercourse measured to centroid =      0.211 Mi.
Difference in elevation =      82.00(Ft.)
Slope along watercourse =    194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.053 Hr.
Lag time =     3.16 Min.
25% of lag time =     0.79 Min.
40% of lag time =     1.26 Min.
Unit time =     5.00 Min.
Duration of storm = 1 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            0.50                 3.90

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            1.30                10.13

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    0.500(In)
Area Averaged 100-Year Rainfall =    1.300(In)

Point rain (area averaged) =    1.300(In)
Areal adjustment factor =   99.99 %
Adjusted average point rain =    1.300(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     7.790           69.00          0.500
 Total Area Entered =      7.79(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  69.0      0.373     0.500        0.205       1.000      0.205
                                                 Sum (F) =    0.205
Area averaged mean soil loss (F) (In/Hr) =  0.205
Minimum soil loss rate ((In/Hr)) =  0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------
Slope of intensity-duration curve for a 1 hour storm =0.5500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
---------------------------------------------------------------
               Unit Hydrograph Data
---------------------------------------------------------------
```

Unit time period (hrs)		Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)
1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
		Sum = 100.000	Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	3.30	0.515	0.205	(0.257)	0.310
2	0.17	4.20	0.655	0.205	(0.328)	0.450
3	0.25	4.40	0.686	0.205	(0.343)	0.481
4	0.33	4.80	0.749	0.205	(0.374)	0.544
5	0.42	5.20	0.811	0.205	(0.406)	0.606
6	0.50	6.20	0.967	0.205	(0.484)	0.762
7	0.58	6.80	1.061	0.205	(0.530)	0.856
8	0.67	8.80	1.373	0.205	(0.686)	1.168
9	0.75	13.90	2.168	0.205	(1.084)	1.963
10	0.83	31.40	4.898	0.205	(2.449)	4.693
11	0.92	7.20	1.123	0.205	(0.562)	0.918
12	1.00	3.80	0.593	0.205	(0.296)	0.388
		(Loss Rate Not Used)			
Sum =		100.0			Sum = 13.1

Flood volume = Effective rainfall 1.09(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.7(Ac.Ft)
Total soil loss = 0.21(In)
Total soil loss = 0.133(Ac.Ft)
Total rainfall = 1.30(In)
Flood volume = 30960.4 Cubic Feet
Total soil loss = 5798.1 Cubic Feet

Peak flow rate of this hydrograph = 21.922(CFS)

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1 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	7.5	15.0	22.5	30.0
0+ 5	0.0059	0.85	VQ				
0+10	0.0222	2.37	V Q				
0+15	0.0444	3.23	V Q				
0+20	0.0702	3.75	VQ				
0+25	0.0997	4.28	Q				
0+30	0.1344	5.04	QV				
0+35	0.1755	5.96	Q V				
0+40	0.2260	7.33	Q V				
0+45	0.3004	10.81	Q V				
0+50	0.4489	21.56	V Q				
0+55	0.5999	21.92	Q V				
1+ 0	0.6643	9.35	Q			V	
1+ 5	0.6941	4.33	Q			V	
1+10	0.7053	1.63	Q			V	
1+15	0.7097	0.63	Q			V	
1+20	0.7106	0.13	Q			V	
1+25	0.7108	0.03	Q			V	

U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 2225.00(Ft.)
Length along longest watercourse measured to centroid = 1113.00(Ft.)
Length along longest watercourse = 0.421 Mi.
Length along longest watercourse measured to centroid = 0.211 Mi.
Difference in elevation = 82.00(Ft.)
Slope along watercourse = 194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 3 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	0.80	6.23

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	2.00	15.58

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 0.800(In)
Area Averaged 100-Year Rainfall = 2.000(In)

Point rain (area averaged) = 2.000(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 2.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	69.00	0.500

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
			Sum = 100.000 Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	1.30	0.312	(0.205)	0.156	0.156
2	0.17	1.30	0.312	(0.205)	0.156	0.156
3	0.25	1.10	0.264	(0.205)	0.132	0.132
4	0.33	1.50	0.360	(0.205)	0.180	0.180
5	0.42	1.50	0.360	(0.205)	0.180	0.180
6	0.50	1.80	0.432	0.205	(0.216)	0.227
7	0.58	1.50	0.360	(0.205)	0.180	0.180
8	0.67	1.80	0.432	0.205	(0.216)	0.227
9	0.75	1.80	0.432	0.205	(0.216)	0.227
10	0.83	1.50	0.360	(0.205)	0.180	0.180
11	0.92	1.60	0.384	(0.205)	0.192	0.192
12	1.00	1.80	0.432	0.205	(0.216)	0.227
13	1.08	2.20	0.528	0.205	(0.264)	0.323
14	1.17	2.20	0.528	0.205	(0.264)	0.323
15	1.25	2.20	0.528	0.205	(0.264)	0.323
16	1.33	2.00	0.480	0.205	(0.240)	0.275
17	1.42	2.60	0.624	0.205	(0.312)	0.419
18	1.50	2.70	0.648	0.205	(0.324)	0.443
19	1.58	2.40	0.576	0.205	(0.288)	0.371
20	1.67	2.70	0.648	0.205	(0.324)	0.443
21	1.75	3.30	0.792	0.205	(0.396)	0.587
22	1.83	3.10	0.744	0.205	(0.372)	0.539
23	1.92	2.90	0.696	0.205	(0.348)	0.491
24	2.00	3.00	0.720	0.205	(0.360)	0.515
25	2.08	3.10	0.744	0.205	(0.372)	0.539
26	2.17	4.20	1.008	0.205	(0.504)	0.803
27	2.25	5.00	1.200	0.205	(0.600)	0.995
28	2.33	3.50	0.840	0.205	(0.420)	0.635
29	2.42	6.80	1.632	0.205	(0.816)	1.427
30	2.50	7.30	1.752	0.205	(0.876)	1.547
31	2.58	8.20	1.968	0.205	(0.984)	1.763
32	2.67	5.90	1.416	0.205	(0.708)	1.211
33	2.75	2.00	0.480	0.205	(0.240)	0.275
34	2.83	1.80	0.432	0.205	(0.216)	0.227
35	2.92	1.80	0.432	0.205	(0.216)	0.227
36	3.00	0.60	0.144	(0.205)	0.072	0.072
		(Loss Rate Not Used)				
Sum =		100.0			Sum =	17.0

Flood volume = Effective rainfall 1.42(In)
times area 7.8(Ac.)/[(In)/(Ft.)] = 0.9(Ac.Ft)
Total soil loss = 0.58(In)
Total soil loss = 0.377(Ac.Ft)
Total rainfall = 2.00(In)
Flood volume = 40142.9 Cubic Feet
Total soil loss = 16410.6 Cubic Feet

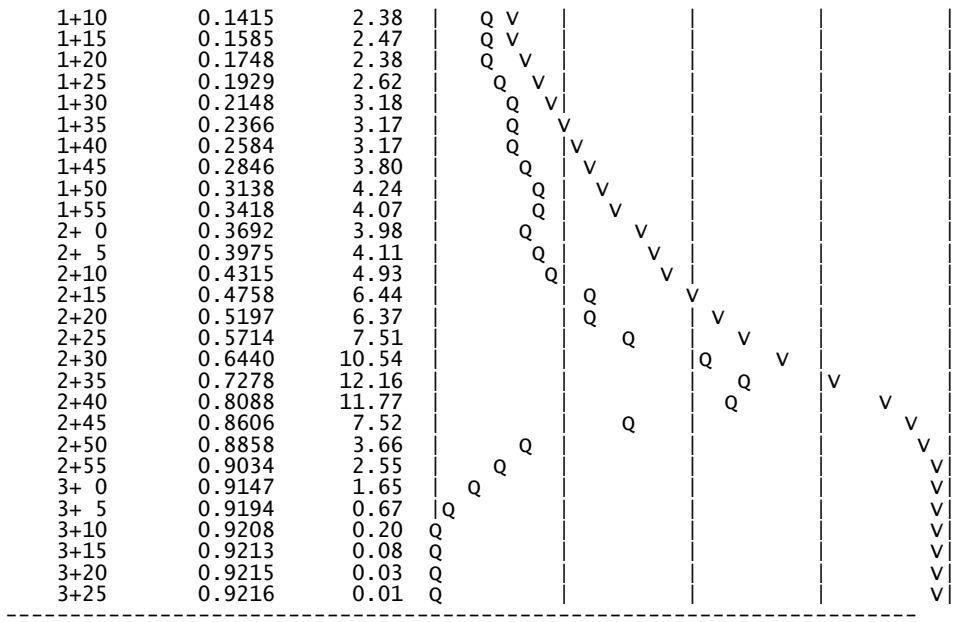
Peak flow rate of this hydrograph = 12.163(CFS)

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3 - H O U R S T O R M
R u n o f f H y d r o g r a p h

Hydrograph in 5 Minute intervals ((CFS))

Time(h+m)	Volume Ac.Ft	Q(CFS)	0	5.0	10.0	15.0	20.0
0+ 5	0.0030	0.43	Q				
0+10	0.0098	1.00	VQ				
0+15	0.0172	1.06	V Q				
0+20	0.0252	1.17	|VQ				
0+25	0.0345	1.35	|VQ				
0+30	0.0449	1.52	|V Q				
0+35	0.0558	1.57	| VQ				
0+40	0.0667	1.58	| VQ				
0+45	0.0786	1.73	| Q				
0+50	0.0898	1.63	| Q				
0+55	0.1002	1.51	| QV				
1+ 0	0.1113	1.61	| QV				
1+ 5	0.1251	2.00	| QV				



1+10	0.1415	2.38	Q V				
1+15	0.1585	2.47	Q V				
1+20	0.1748	2.38	Q V				
1+25	0.1929	2.62	Q V				
1+30	0.2148	3.18	Q V				
1+35	0.2366	3.17	Q V				
1+40	0.2584	3.17	Q V				
1+45	0.2846	3.80	Q V				
1+50	0.3138	4.24	Q V				
1+55	0.3418	4.07	Q V				
2+ 0	0.3692	3.98	Q V				
2+ 5	0.3975	4.11	Q V				
2+10	0.4315	4.93	Q V				
2+15	0.4758	6.44	Q V				
2+20	0.5197	6.37	Q V				
2+25	0.5714	7.51	Q V				
2+30	0.6440	10.54	Q V				
2+35	0.7278	12.16	Q V				
2+40	0.8088	11.77	Q V				
2+45	0.8606	7.52	Q V				
2+50	0.8858	3.66	Q V				
2+55	0.9034	2.55	Q V				
3+ 0	0.9147	1.65	Q V				
3+ 5	0.9194	0.67	Q V				
3+10	0.9208	0.20	Q V				
3+15	0.9213	0.08	Q V				
3+20	0.9215	0.03	Q V				
3+25	0.9216	0.01	Q V				

U n i t H y d r o g r a p h A n a l y s i s

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Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978

Program License Serial Number 5006

English (in-lb) Input Units Used
English Rainfall Data (Inches) Input Values Used

English Units used in output format

Drainage Area = 7.79(Ac.) = 0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment = 7.79(Ac.) = 0.012 Sq. Mi.
Length along longest watercourse = 2225.00(Ft.)
Length along longest watercourse measured to centroid = 1113.00(Ft.)
Length along longest watercourse = 0.421 Mi.
Length along longest watercourse measured to centroid = 0.211 Mi.
Difference in elevation = 82.00(Ft.)
Slope along watercourse = 194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time = 0.053 Hr.
Lag time = 3.16 Min.
25% of lag time = 0.79 Min.
40% of lag time = 1.26 Min.
Unit time = 5.00 Min.
Duration of storm = 6 Hour(s)
User Entered Base Flow = 0.00(CFS)

2 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	1.10	8.57

100 YEAR Area rainfall data:

Area(Ac.)[1]	Rainfall(In)[2]	Weighting[1*2]
7.79	3.00	23.37

STORM EVENT (YEAR) = 100.00
Area Averaged 2-Year Rainfall = 1.100(In)
Area Averaged 100-Year Rainfall = 3.000(In)

Point rain (area averaged) = 3.000(In)
Areal adjustment factor = 100.00 %
Adjusted average point rain = 3.000(In)

Sub-Area Data:

Area(Ac.)	Runoff Index	Impervious %
7.790	69.00	0.500

Total Area Entered = 7.79(Ac.)

RI AMC2	RI AMC-2	Infil. Rate (In/Hr)	Impervious (Dec.%)	Adj. Infil. Rate (In/Hr)	Area% (Dec.)	F (In/Hr)
69.0	69.0	0.373	0.500	0.205	1.000	0.205
					Sum (F) =	0.205

Area averaged mean soil loss (F) (In/Hr) = 0.205
Minimum soil loss rate ((In/Hr)) = 0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) = 0.500

U n i t H y d r o g r a p h
VALLEY S-Curve

Unit Hydrograph Data

Unit time period (hrs)	Time % of lag	Distribution Graph %	Unit Hydrograph (CFS)

1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
			Sum = 100.000 Sum=	7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.50	0.180	(0.205)	0.090	0.090
2	0.17	0.60	0.216	(0.205)	0.108	0.108
3	0.25	0.60	0.216	(0.205)	0.108	0.108
4	0.33	0.60	0.216	(0.205)	0.108	0.108
5	0.42	0.60	0.216	(0.205)	0.108	0.108
6	0.50	0.70	0.252	(0.205)	0.126	0.126
7	0.58	0.70	0.252	(0.205)	0.126	0.126
8	0.67	0.70	0.252	(0.205)	0.126	0.126
9	0.75	0.70	0.252	(0.205)	0.126	0.126
10	0.83	0.70	0.252	(0.205)	0.126	0.126
11	0.92	0.70	0.252	(0.205)	0.126	0.126
12	1.00	0.80	0.288	(0.205)	0.144	0.144
13	1.08	0.80	0.288	(0.205)	0.144	0.144
14	1.17	0.80	0.288	(0.205)	0.144	0.144
15	1.25	0.80	0.288	(0.205)	0.144	0.144
16	1.33	0.80	0.288	(0.205)	0.144	0.144
17	1.42	0.80	0.288	(0.205)	0.144	0.144
18	1.50	0.80	0.288	(0.205)	0.144	0.144
19	1.58	0.80	0.288	(0.205)	0.144	0.144
20	1.67	0.80	0.288	(0.205)	0.144	0.144
21	1.75	0.80	0.288	(0.205)	0.144	0.144
22	1.83	0.80	0.288	(0.205)	0.144	0.144
23	1.92	0.80	0.288	(0.205)	0.144	0.144
24	2.00	0.90	0.324	(0.205)	0.162	0.162
25	2.08	0.80	0.288	(0.205)	0.144	0.144
26	2.17	0.90	0.324	(0.205)	0.162	0.162
27	2.25	0.90	0.324	(0.205)	0.162	0.162
28	2.33	0.90	0.324	(0.205)	0.162	0.162
29	2.42	0.90	0.324	(0.205)	0.162	0.162
30	2.50	0.90	0.324	(0.205)	0.162	0.162
31	2.58	0.90	0.324	(0.205)	0.162	0.162
32	2.67	0.90	0.324	(0.205)	0.162	0.162
33	2.75	1.00	0.360	(0.205)	0.180	0.180
34	2.83	1.00	0.360	(0.205)	0.180	0.180
35	2.92	1.00	0.360	(0.205)	0.180	0.180
36	3.00	1.00	0.360	(0.205)	0.180	0.180
37	3.08	1.00	0.360	(0.205)	0.180	0.180
38	3.17	1.10	0.396	(0.205)	0.198	0.198
39	3.25	1.10	0.396	(0.205)	0.198	0.198
40	3.33	1.10	0.396	(0.205)	0.198	0.198
41	3.42	1.20	0.432	0.205	(0.216)	0.227
42	3.50	1.30	0.468	0.205	(0.234)	0.263
43	3.58	1.40	0.504	0.205	(0.252)	0.299
44	3.67	1.40	0.504	0.205	(0.252)	0.299
45	3.75	1.50	0.540	0.205	(0.270)	0.335
46	3.83	1.50	0.540	0.205	(0.270)	0.335
47	3.92	1.60	0.576	0.205	(0.288)	0.371
48	4.00	1.60	0.576	0.205	(0.288)	0.371
49	4.08	1.70	0.612	0.205	(0.306)	0.407
50	4.17	1.80	0.648	0.205	(0.324)	0.443
51	4.25	1.90	0.684	0.205	(0.342)	0.479
52	4.33	2.00	0.720	0.205	(0.360)	0.515
53	4.42	2.10	0.756	0.205	(0.378)	0.551
54	4.50	2.10	0.756	0.205	(0.378)	0.551
55	4.58	2.20	0.792	0.205	(0.396)	0.587
56	4.67	2.30	0.828	0.205	(0.414)	0.623
57	4.75	2.40	0.864	0.205	(0.432)	0.659
58	4.83	2.40	0.864	0.205	(0.432)	0.659
59	4.92	2.50	0.900	0.205	(0.450)	0.695
60	5.00	2.60	0.936	0.205	(0.468)	0.731
61	5.08	3.10	1.116	0.205	(0.558)	0.911
62	5.17	3.60	1.296	0.205	(0.648)	1.091
63	5.25	3.90	1.404	0.205	(0.702)	1.199
64	5.33	4.20	1.512	0.205	(0.756)	1.307
65	5.42	4.70	1.692	0.205	(0.846)	1.487
66	5.50	5.60	2.016	0.205	(1.008)	1.811
67	5.58	1.90	0.684	0.205	(0.342)	0.479
68	5.67	0.90	0.324	(0.205)	0.162	0.162
69	5.75	0.60	0.216	(0.205)	0.108	0.108
70	5.83	0.50	0.180	(0.205)	0.090	0.090

```
71   5.92     0.30      0.108       (  0.205)       0.054        0.054
72   6.00     0.20      0.072       (  0.205)       0.036        0.036
               (Loss Rate Not Used)
   Sum =     100.0                                  Sum =    24.1
      Flood volume = Effective rainfall      2.01(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       1.3(Ac.Ft)
      Total soil loss =      0.99(In)
      Total soil loss =     0.645(Ac.Ft)
      Total rainfall =      3.00(In)
      Flood volume =       56727.7 Cubic Feet
      Total soil loss =       28103.1 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =     12.206(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          6 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
Time(h+m) Volume Ac.Ft   Q(CFS)  0        5.0      10.0      15.0      20.0
-------------------------------------------------------------------------
  0+ 5       0.0017      0.25  Q         |         |         |         |
  0+10       0.0060      0.63  VQ        |         |         |         |
  0+15       0.0113      0.77  VQ        |         |         |         |
  0+20       0.0169      0.82  VQ        |         |         |         |
  0+25       0.0227      0.84  VQ        |         |         |         |
  0+30       0.0289      0.90  VQ        |         |         |         |
  0+35       0.0355      0.96  |Q        |         |         |         |
  0+40       0.0422      0.98  |Q        |         |         |         |
  0+45       0.0490      0.99  |Q        |         |         |         |
  0+50       0.0558      0.99  |Q        |         |         |         |
  0+55       0.0626      0.99  |Q        |         |         |         |
  1+ 0       0.0698      1.04  | Q       |         |         |         |
  1+ 5       0.0774      1.10  | Q       |         |         |         |
  1+10       0.0851      1.12  | Q       |         |         |         |
  1+15       0.0929      1.13  | Q       |         |         |         |
  1+20       0.1007      1.13  | QV      |         |         |         |
  1+25       0.1085      1.13  | QV      |         |         |         |
  1+30       0.1162      1.13  | QV      |         |         |         |
  1+35       0.1240      1.13  | QV      |         |         |         |
  1+40       0.1318      1.13  | Q V     |         |         |         |
  1+45       0.1396      1.13  | Q V     |         |         |         |
  1+50       0.1474      1.13  | Q V     |         |         |         |
  1+55       0.1552      1.13  | Q V     |         |         |         |
  2+ 0       0.1633      1.18  | Q  V    |         |         |         |
  2+ 5       0.1716      1.20  | Q  V    |         |         |         |
  2+10       0.1798      1.20  | Q  V    |         |         |         |
  2+15       0.1884      1.25  | Q  V    |         |         |         |
  2+20       0.1971      1.26  | Q   V   |         |         |         |
  2+25       0.2059      1.27  | Q   V   |         |         |         |
  2+30       0.2146      1.27  | Q   V   |         |         |         |
  2+35       0.2234      1.27  | Q   V   |         |         |         |
  2+40       0.2322      1.27  | Q    V  |         |         |         |
  2+45       0.2413      1.32  | Q    V  |         |         |         |
  2+50       0.2508      1.39  | Q    V  |         |         |         |
  2+55       0.2605      1.40  | Q     V |         |         |         |
  3+ 0       0.2702      1.41  | Q     V |         |         |         |
  3+ 5       0.2799      1.41  | Q     V |         |         |         |
  3+10       0.2900      1.46  | Q     V |         |         |         |
  3+15       0.3005      1.53  |  Q     V|         |         |         |
  3+20       0.3112      1.54  |  Q     V|         |         |         |
  3+25       0.3224      1.63  |  Q     V|         |         |         |
  3+30       0.3351      1.84  |  Q      V         |         |         |
  3+35       0.3495      2.09  |   Q     V         |         |         |
  3+40       0.3651      2.27  |   Q     |V        |         |         |
  3+45       0.3817      2.41  |   Q     |V        |         |         |
  3+50       0.3994      2.57  |    Q    | V       |         |         |
  3+55       0.4180      2.71  |    Q    | V       |         |         |
  4+ 0       0.4377      2.85  |    Q    |  V      |         |         |
  4+ 5       0.4583      2.99  |    Q    |   V     |         |         |
  4+10       0.4805      3.23  |     Q   |   V     |         |         |
  4+15       0.5047      3.50  |      Q  |    V    |         |         |
  4+20       0.5307      3.78  |      Q  |     V   |         |         |
  4+25       0.5586      4.06  |       Q |      V  |         |         |
  4+30       0.5878      4.24  |       Q |       V |         |         |
  4+35       0.6181      4.39  |       Q |       V |         |         |
  4+40       0.6501      4.65  |        Q|        V|         |         |
  4+45       0.6840      4.92  |        Q|         |V        |         |
  4+50       0.7190      5.09  |         Q         | V       |         |
  4+55       0.7551      5.24  |         Q         |  V      |         |
  5+ 0       0.7930      5.49  |         Q         |   V     |         |
  5+ 5       0.8354      6.16  |         | Q       |    V    |         |
  5+10       0.8861      7.36  |         |   Q     |     V   |         |
  5+15       0.9445      8.48  |         |     Q   |      V  |         |
```

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    5+20       1.0092      9.40  |          |        Q |          V          |
    5+25       1.0814     10.48  |          |          Q          |  V       |
    5+30       1.1655     12.21  |          |            |   Q    |    V     |
    5+35       1.2339      9.94  |          |          Q |        |      V   |
    5+40       1.2655      4.58  |        Q |            |        |       V  |
    5+45       1.2813      2.31  |   Q      |            |        |         V|
    5+50       1.2908      1.38  |  Q       |            |        |         V|
    5+55       1.2966      0.84  |Q         |            |        |         V|
    6+ 0       1.2998      0.47  Q          |            |        |         V|
    6+ 5       1.3015      0.24  Q          |            |        |         V|
    6+10       1.3020      0.07  Q          |            |        |         V|
    6+15       1.3022      0.03  Q          |            |        |         V|
    6+20       1.3023      0.01  Q          |            |        |         V|
    6+25       1.3023      0.00  Q          |            |        |          V
-------------------------------------------------------------------------------
```

```
       U n i t   H y d r o g r a p h   A n a l y s i s

       Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2008, Version 8.1
              Study date  04/18/24 File: pro310024100.out

++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
------------------------------------------------------------------------------

Riverside County Synthetic Unit Hydrology Method
RCFC & WCD Manual date - April 1978


Program License Serial Number 5006

------------------------------------------------------------------------
 English (in-lb) Input Units Used
 English Rainfall Data (Inches) Input Values Used

 English Units used in output format



------------------------------------------------------------------------
------------------------------------------------------------------------
Drainage Area =       7.79(Ac.)  =      0.012 Sq. Mi.
Drainage Area for Depth-Area Areal Adjustment =       7.79(Ac.)  =      0.012 Sq. Mi.
Length along longest watercourse =    2225.00(Ft.)
Length along longest watercourse measured to centroid =    1113.00(Ft.)
Length along longest watercourse =      0.421 Mi.
Length along longest watercourse measured to centroid =      0.211 Mi.
Difference in elevation =      82.00(Ft.)
Slope along watercourse =    194.5888 Ft./Mi.
Average Manning's 'N' = 0.015
Lag time =    0.053 Hr.
Lag time =     3.16 Min.
25% of lag time =     0.79 Min.
40% of lag time =     1.26 Min.
Unit time =     5.00 Min.
Duration of storm = 24 Hour(s)
User Entered Base Flow =     0.00(CFS)

2 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            1.80                 14.02

100 YEAR Area rainfall data:


Area(Ac.)[1]       Rainfall(In)[2]      Weighting[1*2]
        7.79            5.00                 38.95

STORM EVENT (YEAR) =  100.00
Area Averaged 2-Year Rainfall =    1.800(In)
Area Averaged 100-Year Rainfall =    5.000(In)

Point rain (area averaged) =    5.000(In)
Areal adjustment factor =  100.00 %
Adjusted average point rain =    5.000(In)

Sub-Area Data:
Area(Ac.)         Runoff Index   Impervious %
     7.790           69.00          0.500
 Total Area Entered =      7.79(Ac.)


RI    RI   Infil. Rate Impervious   Adj. Infil. Rate  Area%     F
AMC2 AMC-2     (In/Hr)    (Dec.%)     (In/Hr)      (Dec.)    (In/Hr)
69.0  69.0      0.373     0.500        0.205       1.000      0.205
                                                 Sum (F) =   0.205
Area averaged mean soil loss (F) (In/Hr) =  0.205
Minimum soil loss rate ((In/Hr)) =  0.103
(for 24 hour storm duration)
Soil low loss rate (decimal) =   0.500
------------------------------------------------------------------------

               U n i t  H y d r o g r a p h
                      VALLEY S-Curve
------------------------------------------------------------------------
               Unit Hydrograph Data
------------------------------------------------------------------------
Unit time period   Time % of lag   Distribution   Unit Hydrograph
    (hrs)                          Graph %           (CFS)
```

1	0.083	158.124	35.084	2.754
2	0.167	316.247	46.408	3.643
3	0.250	474.371	10.730	0.842
4	0.333	632.495	4.637	0.364
5	0.417	790.618	2.252	0.177
6	0.500	948.742	0.888	0.070
			Sum = 100.000	Sum= 7.851

The following loss rate calculations reflect use of the minimum calculated loss rate subtracted from the Storm Rain to produce the maximum Effective Rain value

Unit	Time (Hr.)	Pattern Percent	Storm Rain (In/Hr)	Loss rate(In./Hr) Max	Low	Effective (In/Hr)
1	0.08	0.07	0.040	(0.363)	0.020	0.020
2	0.17	0.07	0.040	(0.362)	0.020	0.020
3	0.25	0.07	0.040	(0.361)	0.020	0.020
4	0.33	0.10	0.060	(0.359)	0.030	0.030
5	0.42	0.10	0.060	(0.358)	0.030	0.030
6	0.50	0.10	0.060	(0.356)	0.030	0.030
7	0.58	0.10	0.060	(0.355)	0.030	0.030
8	0.67	0.10	0.060	(0.354)	0.030	0.030
9	0.75	0.10	0.060	(0.352)	0.030	0.030
10	0.83	0.13	0.080	(0.351)	0.040	0.040
11	0.92	0.13	0.080	(0.350)	0.040	0.040
12	1.00	0.13	0.080	(0.348)	0.040	0.040
13	1.08	0.10	0.060	(0.347)	0.030	0.030
14	1.17	0.10	0.060	(0.345)	0.030	0.030
15	1.25	0.10	0.060	(0.344)	0.030	0.030
16	1.33	0.10	0.060	(0.343)	0.030	0.030
17	1.42	0.10	0.060	(0.341)	0.030	0.030
18	1.50	0.10	0.060	(0.340)	0.030	0.030
19	1.58	0.10	0.060	(0.339)	0.030	0.030
20	1.67	0.10	0.060	(0.337)	0.030	0.030
21	1.75	0.10	0.060	(0.336)	0.030	0.030
22	1.83	0.13	0.080	(0.335)	0.040	0.040
23	1.92	0.13	0.080	(0.333)	0.040	0.040
24	2.00	0.13	0.080	(0.332)	0.040	0.040
25	2.08	0.13	0.080	(0.330)	0.040	0.040
26	2.17	0.13	0.080	(0.329)	0.040	0.040
27	2.25	0.13	0.080	(0.328)	0.040	0.040
28	2.33	0.13	0.080	(0.326)	0.040	0.040
29	2.42	0.13	0.080	(0.325)	0.040	0.040
30	2.50	0.13	0.080	(0.324)	0.040	0.040
31	2.58	0.17	0.100	(0.323)	0.050	0.050
32	2.67	0.17	0.100	(0.321)	0.050	0.050
33	2.75	0.17	0.100	(0.320)	0.050	0.050
34	2.83	0.17	0.100	(0.319)	0.050	0.050
35	2.92	0.17	0.100	(0.317)	0.050	0.050
36	3.00	0.17	0.100	(0.316)	0.050	0.050
37	3.08	0.17	0.100	(0.315)	0.050	0.050
38	3.17	0.17	0.100	(0.313)	0.050	0.050
39	3.25	0.17	0.100	(0.312)	0.050	0.050
40	3.33	0.17	0.100	(0.311)	0.050	0.050
41	3.42	0.17	0.100	(0.309)	0.050	0.050
42	3.50	0.17	0.100	(0.308)	0.050	0.050
43	3.58	0.17	0.100	(0.307)	0.050	0.050
44	3.67	0.17	0.100	(0.306)	0.050	0.050
45	3.75	0.17	0.100	(0.304)	0.050	0.050
46	3.83	0.20	0.120	(0.303)	0.060	0.060
47	3.92	0.20	0.120	(0.302)	0.060	0.060
48	4.00	0.20	0.120	(0.300)	0.060	0.060
49	4.08	0.20	0.120	(0.299)	0.060	0.060
50	4.17	0.20	0.120	(0.298)	0.060	0.060
51	4.25	0.20	0.120	(0.297)	0.060	0.060
52	4.33	0.23	0.140	(0.295)	0.070	0.070
53	4.42	0.23	0.140	(0.294)	0.070	0.070
54	4.50	0.23	0.140	(0.293)	0.070	0.070
55	4.58	0.23	0.140	(0.292)	0.070	0.070
56	4.67	0.23	0.140	(0.290)	0.070	0.070
57	4.75	0.23	0.140	(0.289)	0.070	0.070
58	4.83	0.27	0.160	(0.288)	0.080	0.080
59	4.92	0.27	0.160	(0.287)	0.080	0.080
60	5.00	0.27	0.160	(0.285)	0.080	0.080
61	5.08	0.20	0.120	(0.284)	0.060	0.060
62	5.17	0.20	0.120	(0.283)	0.060	0.060
63	5.25	0.20	0.120	(0.282)	0.060	0.060
64	5.33	0.23	0.140	(0.280)	0.070	0.070
65	5.42	0.23	0.140	(0.279)	0.070	0.070
66	5.50	0.23	0.140	(0.278)	0.070	0.070
67	5.58	0.27	0.160	(0.277)	0.080	0.080
68	5.67	0.27	0.160	(0.275)	0.080	0.080
69	5.75	0.27	0.160	(0.274)	0.080	0.080
70	5.83	0.27	0.160	(0.273)	0.080	0.080

71	5.92	0.27	0.160	(0.272)	0.080	0.080
72	6.00	0.27	0.160	(0.271)	0.080	0.080
73	6.08	0.30	0.180	(0.269)	0.090	0.090
74	6.17	0.30	0.180	(0.268)	0.090	0.090
75	6.25	0.30	0.180	(0.267)	0.090	0.090
76	6.33	0.30	0.180	(0.266)	0.090	0.090
77	6.42	0.30	0.180	(0.265)	0.090	0.090
78	6.50	0.30	0.180	(0.263)	0.090	0.090
79	6.58	0.33	0.200	(0.262)	0.100	0.100
80	6.67	0.33	0.200	(0.261)	0.100	0.100
81	6.75	0.33	0.200	(0.260)	0.100	0.100
82	6.83	0.33	0.200	(0.259)	0.100	0.100
83	6.92	0.33	0.200	(0.258)	0.100	0.100
84	7.00	0.33	0.200	(0.256)	0.100	0.100
85	7.08	0.33	0.200	(0.255)	0.100	0.100
86	7.17	0.33	0.200	(0.254)	0.100	0.100
87	7.25	0.33	0.200	(0.253)	0.100	0.100
88	7.33	0.37	0.220	(0.252)	0.110	0.110
89	7.42	0.37	0.220	(0.251)	0.110	0.110
90	7.50	0.37	0.220	(0.249)	0.110	0.110
91	7.58	0.40	0.240	(0.248)	0.120	0.120
92	7.67	0.40	0.240	(0.247)	0.120	0.120
93	7.75	0.40	0.240	(0.246)	0.120	0.120
94	7.83	0.43	0.260	(0.245)	0.130	0.130
95	7.92	0.43	0.260	(0.244)	0.130	0.130
96	8.00	0.43	0.260	(0.243)	0.130	0.130
97	8.08	0.50	0.300	(0.242)	0.150	0.150
98	8.17	0.50	0.300	(0.240)	0.150	0.150
99	8.25	0.50	0.300	(0.239)	0.150	0.150
100	8.33	0.50	0.300	(0.238)	0.150	0.150
101	8.42	0.50	0.300	(0.237)	0.150	0.150
102	8.50	0.50	0.300	(0.236)	0.150	0.150
103	8.58	0.53	0.320	(0.235)	0.160	0.160
104	8.67	0.53	0.320	(0.234)	0.160	0.160
105	8.75	0.53	0.320	(0.233)	0.160	0.160
106	8.83	0.57	0.340	(0.232)	0.170	0.170
107	8.92	0.57	0.340	(0.230)	0.170	0.170
108	9.00	0.57	0.340	(0.229)	0.170	0.170
109	9.08	0.63	0.380	(0.228)	0.190	0.190
110	9.17	0.63	0.380	(0.227)	0.190	0.190
111	9.25	0.63	0.380	(0.226)	0.190	0.190
112	9.33	0.67	0.400	(0.225)	0.200	0.200
113	9.42	0.67	0.400	(0.224)	0.200	0.200
114	9.50	0.67	0.400	(0.223)	0.200	0.200
115	9.58	0.70	0.420	(0.222)	0.210	0.210
116	9.67	0.70	0.420	(0.221)	0.210	0.210
117	9.75	0.70	0.420	(0.220)	0.210	0.210
118	9.83	0.73	0.440	0.219	(0.220)	0.221
119	9.92	0.73	0.440	0.218	(0.220)	0.222
120	10.00	0.73	0.440	0.217	(0.220)	0.223
121	10.08	0.50	0.300	(0.215)	0.150	0.150
122	10.17	0.50	0.300	(0.214)	0.150	0.150
123	10.25	0.50	0.300	(0.213)	0.150	0.150
124	10.33	0.50	0.300	(0.212)	0.150	0.150
125	10.42	0.50	0.300	(0.211)	0.150	0.150
126	10.50	0.50	0.300	(0.210)	0.150	0.150
127	10.58	0.67	0.400	(0.209)	0.200	0.200
128	10.67	0.67	0.400	(0.208)	0.200	0.200
129	10.75	0.67	0.400	(0.207)	0.200	0.200
130	10.83	0.67	0.400	(0.206)	0.200	0.200
131	10.92	0.67	0.400	(0.205)	0.200	0.200
132	11.00	0.67	0.400	(0.204)	0.200	0.200
133	11.08	0.63	0.380	(0.203)	0.190	0.190
134	11.17	0.63	0.380	(0.202)	0.190	0.190
135	11.25	0.63	0.380	(0.201)	0.190	0.190
136	11.33	0.63	0.380	(0.200)	0.190	0.190
137	11.42	0.63	0.380	(0.199)	0.190	0.190
138	11.50	0.63	0.380	(0.198)	0.190	0.190
139	11.58	0.57	0.340	(0.197)	0.170	0.170
140	11.67	0.57	0.340	(0.196)	0.170	0.170
141	11.75	0.57	0.340	(0.195)	0.170	0.170
142	11.83	0.60	0.360	(0.194)	0.180	0.180
143	11.92	0.60	0.360	(0.193)	0.180	0.180
144	12.00	0.60	0.360	(0.192)	0.180	0.180
145	12.08	0.83	0.500	0.191	(0.250)	0.309
146	12.17	0.83	0.500	0.190	(0.250)	0.310
147	12.25	0.83	0.500	0.189	(0.250)	0.311
148	12.33	0.87	0.520	0.189	(0.260)	0.331
149	12.42	0.87	0.520	0.188	(0.260)	0.332
150	12.50	0.87	0.520	0.187	(0.260)	0.333
151	12.58	0.93	0.560	0.186	(0.280)	0.374
152	12.67	0.93	0.560	0.185	(0.280)	0.375
153	12.75	0.93	0.560	0.184	(0.280)	0.376
154	12.83	0.97	0.580	0.183	(0.290)	0.397
155	12.92	0.97	0.580	0.182	(0.290)	0.398
156	13.00	0.97	0.580	0.181	(0.290)	0.399

157	13.08	1.13	0.680	0.180	(0.340)	0.500
158	13.17	1.13	0.680	0.179	(0.340)	0.501
159	13.25	1.13	0.680	0.178	(0.340)	0.502
160	13.33	1.13	0.680	0.177	(0.340)	0.503
161	13.42	1.13	0.680	0.177	(0.340)	0.503
162	13.50	1.13	0.680	0.176	(0.340)	0.504
163	13.58	0.77	0.460	0.175	(0.230)	0.285
164	13.67	0.77	0.460	0.174	(0.230)	0.286
165	13.75	0.77	0.460	0.173	(0.230)	0.287
166	13.83	0.77	0.460	0.172	(0.230)	0.288
167	13.92	0.77	0.460	0.171	(0.230)	0.289
168	14.00	0.77	0.460	0.170	(0.230)	0.290
169	14.08	0.90	0.540	0.169	(0.270)	0.371
170	14.17	0.90	0.540	0.169	(0.270)	0.371
171	14.25	0.90	0.540	0.168	(0.270)	0.372
172	14.33	0.87	0.520	0.167	(0.260)	0.353
173	14.42	0.87	0.520	0.166	(0.260)	0.354
174	14.50	0.87	0.520	0.165	(0.260)	0.355
175	14.58	0.87	0.520	0.164	(0.260)	0.356
176	14.67	0.87	0.520	0.163	(0.260)	0.357
177	14.75	0.87	0.520	0.163	(0.260)	0.357
178	14.83	0.83	0.500	0.162	(0.250)	0.338
179	14.92	0.83	0.500	0.161	(0.250)	0.339
180	15.00	0.83	0.500	0.160	(0.250)	0.340
181	15.08	0.80	0.480	0.159	(0.240)	0.321
182	15.17	0.80	0.480	0.159	(0.240)	0.321
183	15.25	0.80	0.480	0.158	(0.240)	0.322
184	15.33	0.77	0.460	0.157	(0.230)	0.303
185	15.42	0.77	0.460	0.156	(0.230)	0.304
186	15.50	0.77	0.460	0.155	(0.230)	0.305
187	15.58	0.63	0.380	0.154	(0.190)	0.226
188	15.67	0.63	0.380	0.154	(0.190)	0.226
189	15.75	0.63	0.380	0.153	(0.190)	0.227
190	15.83	0.63	0.380	0.152	(0.190)	0.228
191	15.92	0.63	0.380	0.151	(0.190)	0.229
192	16.00	0.63	0.380	0.151	(0.190)	0.229
193	16.08	0.13	0.080	(0.150)	0.040	0.040
194	16.17	0.13	0.080	(0.149)	0.040	0.040
195	16.25	0.13	0.080	(0.148)	0.040	0.040
196	16.33	0.13	0.080	(0.148)	0.040	0.040
197	16.42	0.13	0.080	(0.147)	0.040	0.040
198	16.50	0.13	0.080	(0.146)	0.040	0.040
199	16.58	0.10	0.060	(0.145)	0.030	0.030
200	16.67	0.10	0.060	(0.145)	0.030	0.030
201	16.75	0.10	0.060	(0.144)	0.030	0.030
202	16.83	0.10	0.060	(0.143)	0.030	0.030
203	16.92	0.10	0.060	(0.142)	0.030	0.030
204	17.00	0.10	0.060	(0.142)	0.030	0.030
205	17.08	0.17	0.100	(0.141)	0.050	0.050
206	17.17	0.17	0.100	(0.140)	0.050	0.050
207	17.25	0.17	0.100	(0.140)	0.050	0.050
208	17.33	0.17	0.100	(0.139)	0.050	0.050
209	17.42	0.17	0.100	(0.138)	0.050	0.050
210	17.50	0.17	0.100	(0.137)	0.050	0.050
211	17.58	0.17	0.100	(0.137)	0.050	0.050
212	17.67	0.17	0.100	(0.136)	0.050	0.050
213	17.75	0.17	0.100	(0.135)	0.050	0.050
214	17.83	0.13	0.080	(0.135)	0.040	0.040
215	17.92	0.13	0.080	(0.134)	0.040	0.040
216	18.00	0.13	0.080	(0.133)	0.040	0.040
217	18.08	0.13	0.080	(0.133)	0.040	0.040
218	18.17	0.13	0.080	(0.132)	0.040	0.040
219	18.25	0.13	0.080	(0.131)	0.040	0.040
220	18.33	0.13	0.080	(0.131)	0.040	0.040
221	18.42	0.13	0.080	(0.130)	0.040	0.040
222	18.50	0.13	0.080	(0.130)	0.040	0.040
223	18.58	0.10	0.060	(0.129)	0.030	0.030
224	18.67	0.10	0.060	(0.128)	0.030	0.030
225	18.75	0.10	0.060	(0.128)	0.030	0.030
226	18.83	0.07	0.040	(0.127)	0.020	0.020
227	18.92	0.07	0.040	(0.126)	0.020	0.020
228	19.00	0.07	0.040	(0.126)	0.020	0.020
229	19.08	0.10	0.060	(0.125)	0.030	0.030
230	19.17	0.10	0.060	(0.125)	0.030	0.030
231	19.25	0.10	0.060	(0.124)	0.030	0.030
232	19.33	0.13	0.080	(0.123)	0.040	0.040
233	19.42	0.13	0.080	(0.123)	0.040	0.040
234	19.50	0.13	0.080	(0.122)	0.040	0.040
235	19.58	0.10	0.060	(0.122)	0.030	0.030
236	19.67	0.10	0.060	(0.121)	0.030	0.030
237	19.75	0.10	0.060	(0.121)	0.030	0.030
238	19.83	0.07	0.040	(0.120)	0.020	0.020
239	19.92	0.07	0.040	(0.120)	0.020	0.020
240	20.00	0.07	0.040	(0.119)	0.020	0.020
241	20.08	0.10	0.060	(0.119)	0.030	0.030
242	20.17	0.10	0.060	(0.118)	0.030	0.030

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243  20.25     0.10      0.060       (  0.118)       0.030        0.030
244  20.33     0.10      0.060       (  0.117)       0.030        0.030
245  20.42     0.10      0.060       (  0.116)       0.030        0.030
246  20.50     0.10      0.060       (  0.116)       0.030        0.030
247  20.58     0.10      0.060       (  0.116)       0.030        0.030
248  20.67     0.10      0.060       (  0.115)       0.030        0.030
249  20.75     0.10      0.060       (  0.115)       0.030        0.030
250  20.83     0.07      0.040       (  0.114)       0.020        0.020
251  20.92     0.07      0.040       (  0.114)       0.020        0.020
252  21.00     0.07      0.040       (  0.113)       0.020        0.020
253  21.08     0.10      0.060       (  0.113)       0.030        0.030
254  21.17     0.10      0.060       (  0.112)       0.030        0.030
255  21.25     0.10      0.060       (  0.112)       0.030        0.030
256  21.33     0.07      0.040       (  0.111)       0.020        0.020
257  21.42     0.07      0.040       (  0.111)       0.020        0.020
258  21.50     0.07      0.040       (  0.111)       0.020        0.020
259  21.58     0.10      0.060       (  0.110)       0.030        0.030
260  21.67     0.10      0.060       (  0.110)       0.030        0.030
261  21.75     0.10      0.060       (  0.109)       0.030        0.030
262  21.83     0.07      0.040       (  0.109)       0.020        0.020
263  21.92     0.07      0.040       (  0.109)       0.020        0.020
264  22.00     0.07      0.040       (  0.108)       0.020        0.020
265  22.08     0.10      0.060       (  0.108)       0.030        0.030
266  22.17     0.10      0.060       (  0.108)       0.030        0.030
267  22.25     0.10      0.060       (  0.107)       0.030        0.030
268  22.33     0.07      0.040       (  0.107)       0.020        0.020
269  22.42     0.07      0.040       (  0.107)       0.020        0.020
270  22.50     0.07      0.040       (  0.106)       0.020        0.020
271  22.58     0.07      0.040       (  0.106)       0.020        0.020
272  22.67     0.07      0.040       (  0.106)       0.020        0.020
273  22.75     0.07      0.040       (  0.105)       0.020        0.020
274  22.83     0.07      0.040       (  0.105)       0.020        0.020
275  22.92     0.07      0.040       (  0.105)       0.020        0.020
276  23.00     0.07      0.040       (  0.105)       0.020        0.020
277  23.08     0.07      0.040       (  0.104)       0.020        0.020
278  23.17     0.07      0.040       (  0.104)       0.020        0.020
279  23.25     0.07      0.040       (  0.104)       0.020        0.020
280  23.33     0.07      0.040       (  0.104)       0.020        0.020
281  23.42     0.07      0.040       (  0.103)       0.020        0.020
282  23.50     0.07      0.040       (  0.103)       0.020        0.020
283  23.58     0.07      0.040       (  0.103)       0.020        0.020
284  23.67     0.07      0.040       (  0.103)       0.020        0.020
285  23.75     0.07      0.040       (  0.103)       0.020        0.020
286  23.83     0.07      0.040       (  0.103)       0.020        0.020
287  23.92     0.07      0.040       (  0.103)       0.020        0.020
288  24.00     0.07      0.040       (  0.103)       0.020        0.020
               (Loss Rate Not Used)
    Sum =     100.0                                  Sum =    34.2
      Flood volume = Effective rainfall      2.85(In)
       times area       7.8(Ac.)/[(In)/(Ft.)] =       1.8(Ac.Ft)
      Total soil loss =      2.15(In)
      Total soil loss =     1.398(Ac.Ft)
      Total rainfall =      5.00(In)
      Flood volume =       80506.4 Cubic Feet
      Total soil loss =       60880.0 Cubic Feet
      ---------------------------------------------------------------------
       Peak flow rate of this hydrograph =      3.955(CFS)
      ---------------------------------------------------------------------
      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
                          24 - H O U R    S T O R M
                     R u n o f f      H y d r o g r a p h
      ---------------------------------------------------------------------
                  Hydrograph in   5   Minute intervals ((CFS))

      ---------------------------------------------------------------------
 Time(h+m) Volume Ac.Ft   Q(CFS)  0        2.5       5.0       7.5      10.0
 ------------------------------------------------------------------------
   0+ 5       0.0004      0.06  Q          |         |         |         |
   0+10       0.0013      0.13  Q          |         |         |         |
   0+15       0.0023      0.14  Q          |         |         |         |
   0+20       0.0035      0.18  Q          |         |         |         |
   0+25       0.0050      0.22  Q          |         |         |         |
   0+30       0.0066      0.23  Q          |         |         |         |
   0+35       0.0082      0.23  Q          |         |         |         |
   0+40       0.0098      0.23  Q          |         |         |         |
   0+45       0.0114      0.24  Q          |         |         |         |
   0+50       0.0133      0.26  VQ         |         |         |         |
   0+55       0.0153      0.30  VQ         |         |         |         |
   1+ 0       0.0174      0.31  VQ         |         |         |         |
   1+ 5       0.0194      0.28  VQ         |         |         |         |
   1+10       0.0211      0.25  Q          |         |         |         |
   1+15       0.0228      0.24  Q          |         |         |         |
   1+20       0.0244      0.24  Q          |         |         |         |
   1+25       0.0260      0.24  Q          |         |         |         |
   1+30       0.0277      0.24  Q          |         |         |         |
   1+35       0.0293      0.24  Q          |         |         |         |
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1+40	0.0309	0.24	Q	|	|	|	|
1+45	0.0325	0.24	Q	|	|	|	|
1+50	0.0343	0.26	VQ	|	|	|	|
1+55	0.0364	0.30	VQ	|	|	|	|
2+ 0	0.0385	0.31	VQ	|	|	|	|
2+ 5	0.0407	0.31	VQ	|	|	|	|
2+10	0.0428	0.31	VQ	|	|	|	|
2+15	0.0450	0.31	VQ	|	|	|	|
2+20	0.0472	0.31	|Q	|	|	|	|
2+25	0.0493	0.31	|Q	|	|	|	|
2+30	0.0515	0.31	|Q	|	|	|	|
2+35	0.0538	0.34	|Q	|	|	|	|
2+40	0.0565	0.38	|Q	|	|	|	|
2+45	0.0591	0.39	|Q	|	|	|	|
2+50	0.0618	0.39	|Q	|	|	|	|
2+55	0.0645	0.39	|Q	|	|	|	|
3+ 0	0.0672	0.39	|Q	|	|	|	|
3+ 5	0.0699	0.39	|Q	|	|	|	|
3+10	0.0726	0.39	|Q	|	|	|	|
3+15	0.0753	0.39	|Q	|	|	|	|
3+20	0.0780	0.39	|Q	|	|	|	|
3+25	0.0807	0.39	|Q	|	|	|	|
3+30	0.0834	0.39	|Q	|	|	|	|
3+35	0.0861	0.39	|Q	|	|	|	|
3+40	0.0888	0.39	|Q	|	|	|	|
3+45	0.0916	0.39	|Q	|	|	|	|
3+50	0.0944	0.42	|QV	|	|	|	|
3+55	0.0976	0.46	|QV	|	|	|	|
4+ 0	0.1008	0.47	|QV	|	|	|	|
4+ 5	0.1040	0.47	|QV	|	|	|	|
4+10	0.1073	0.47	|QV	|	|	|	|
4+15	0.1105	0.47	|QV	|	|	|	|
4+20	0.1139	0.50	|QV	|	|	|	|
4+25	0.1176	0.54	| Q	|	|	|	|
4+30	0.1214	0.54	| Q	|	|	|	|
4+35	0.1251	0.55	| Q	|	|	|	|
4+40	0.1289	0.55	| Q	|	|	|	|
4+45	0.1327	0.55	| Q	|	|	|	|
4+50	0.1367	0.58	| Q	|	|	|	|
4+55	0.1409	0.61	| QV	|	|	|	|
5+ 0	0.1452	0.62	| QV	|	|	|	|
5+ 5	0.1491	0.57	| QV	|	|	|	|
5+10	0.1526	0.50	|Q V	|	|	|	|
5+15	0.1559	0.48	|Q V	|	|	|	|
5+20	0.1594	0.50	| QV	|	|	|	|
5+25	0.1631	0.54	| QV	|	|	|	|
5+30	0.1668	0.54	| QV	|	|	|	|
5+35	0.1708	0.57	| QV	|	|	|	|
5+40	0.1750	0.61	| QV	|	|	|	|
5+45	0.1793	0.62	| QV	|	|	|	|
5+50	0.1836	0.63	| QV	|	|	|	|
5+55	0.1879	0.63	| Q V	|	|	|	|
6+ 0	0.1922	0.63	| Q V	|	|	|	|
6+ 5	0.1968	0.66	| Q V	|	|	|	|
6+10	0.2015	0.69	| Q V	|	|	|	|
6+15	0.2064	0.70	| Q V	|	|	|	|
6+20	0.2112	0.70	| Q V	|	|	|	|
6+25	0.2161	0.71	| Q V	|	|	|	|
6+30	0.2209	0.71	| Q V	|	|	|	|
6+35	0.2260	0.73	| Q V	|	|	|	|
6+40	0.2313	0.77	| Q V	|	|	|	|
6+45	0.2367	0.78	| Q V	|	|	|	|
6+50	0.2421	0.78	| Q V	|	|	|	|
6+55	0.2475	0.78	| Q V	|	|	|	|
7+ 0	0.2529	0.79	| Q V	|	|	|	|
7+ 5	0.2583	0.79	| Q V	|	|	|	|
7+10	0.2637	0.79	| Q V	|	|	|	|
7+15	0.2691	0.79	| Q V	|	|	|	|
7+20	0.2747	0.81	| Q V	|	|	|	|
7+25	0.2806	0.85	| Q V	|	|	|	|
7+30	0.2865	0.86	| Q V	|	|	|	|
7+35	0.2926	0.89	| Q V	|	|	|	|
7+40	0.2990	0.93	| Q V	|	|	|	|
7+45	0.3054	0.94	| Q V	|	|	|	|
7+50	0.3121	0.97	| Q V	|	|	|	|
7+55	0.3190	1.01	| Q V	|	|	|	|
8+ 0	0.3260	1.02	| Q V	|	|	|	|
8+ 5	0.3334	1.07	| Q V	|	|	|	|
8+10	0.3413	1.15	| Q V	|	|	|	|
8+15	0.3494	1.17	| Q V	|	|	|	|
8+20	0.3574	1.17	| Q V	|	|	|	|
8+25	0.3655	1.18	| Q V	|	|	|	|
8+30	0.3737	1.18	| Q V	|	|	|	|
8+35	0.3820	1.21	| Q V	|	|	|	|
8+40	0.3905	1.24	| Q V	|	|	|	|
8+45	0.3991	1.25	| Q V	|	|	|	|

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 8+50       0.4080      1.28  |     Q  V |          |          |          |
 8+55       0.4170      1.32  |     Q   V|          |          |          |
 9+ 0       0.4262      1.33  |     Q   V|          |          |          |
 9+ 5       0.4358      1.39  |     Q   V|          |          |          |
 9+10       0.4458      1.46  |     Q   V|          |          |          |
 9+15       0.4560      1.48  |     Q   V|          |          |          |
 9+20       0.4665      1.52  |      Q   V          |          |          |
 9+25       0.4772      1.56  |      Q   V          |          |          |
 9+30       0.4879      1.56  |      Q   V          |          |          |
 9+35       0.4989      1.60  |      Q   V          |          |          |
 9+40       0.5102      1.63  |      Q   |V         |          |          |
 9+45       0.5215      1.64  |      Q   |V         |          |          |
 9+50       0.5331      1.68  |      Q   |V         |          |          |
 9+55       0.5449      1.72  |      Q   |V         |          |          |
10+ 0       0.5569      1.74  |      Q   | V        |          |          |
10+ 5       0.5676      1.55  |      Q   | V        |          |          |
10+10       0.5764      1.28  |     Q    | V        |          |          |
10+15       0.5849      1.22  |    Q     | V        |          |          |
10+20       0.5931      1.20  |    Q     | V        |          |          |
10+25       0.6013      1.18  |    Q     |  V       |          |          |
10+30       0.6094      1.18  |    Q     |  V       |          |          |
10+35       0.6184      1.32  |     Q    |  V       |          |          |
10+40       0.6287      1.50  |     Q    |  V       |          |          |
10+45       0.6394      1.54  |      Q   |  V       |          |          |
10+50       0.6501      1.56  |      Q   |   V      |          |          |
10+55       0.6609      1.57  |      Q   |   V      |          |          |
11+ 0       0.6717      1.57  |      Q   |   V      |          |          |
11+ 5       0.6823      1.54  |      Q   |   V      |          |          |
11+10       0.6927      1.51  |      Q   |   V      |          |          |
11+15       0.7030      1.50  |     Q    |    V     |          |          |
11+20       0.7133      1.49  |     Q    |    V     |          |          |
11+25       0.7236      1.49  |     Q    |    V     |          |          |
11+30       0.7339      1.49  |     Q    |    V     |          |          |
11+35       0.7438      1.44  |     Q    |     V    |          |          |
11+40       0.7532      1.36  |     Q    |     V    |          |          |
11+45       0.7625      1.35  |     Q    |     V    |          |          |
11+50       0.7719      1.37  |     Q    |     V    |          |          |
11+55       0.7815      1.40  |     Q    |     V    |          |          |
12+ 0       0.7912      1.41  |     Q    |      V   |          |          |
12+ 5       0.8034      1.77  |       Q  |      V   |          |          |
12+10       0.8188      2.24  |        Q |      V   |          |          |
12+15       0.8350      2.35  |         Q|       V  |          |          |
12+20       0.8520      2.46  |         Q|       V  |          |          |
12+25       0.8697      2.57  |          Q       V  |          |          |
12+30       0.8876      2.60  |          Q        V|          |          |
12+35       0.9063      2.72  |          Q        V|          |          |
12+40       0.9262      2.88  |          |Q        V          |          |
12+45       0.9463      2.92  |          |Q        V          |          |
12+50       0.9670      3.00  |          | Q       V          |          |
12+55       0.9882      3.09  |          | Q       |V         |          |
13+ 0       1.0097      3.11  |          | Q       |V         |          |
13+ 5       1.0331      3.40  |          |  Q      | V        |          |
13+10       1.0591      3.78  |          |    Q    | V        |          |
13+15       1.0858      3.87  |          |    Q    |  V       |          |
13+20       1.1128      3.92  |          |    Q    |   V      |          |
13+25       1.1399      3.94  |          |    Q    |   V      |          |
13+30       1.1672      3.96  |          |    Q    |    V     |          |
13+35       1.1903      3.36  |          |  Q      |    V     |          |
13+40       1.2079      2.56  |          Q         |     V    |          |
13+45       1.2243      2.38  |         Q|         |     V    |          |
13+50       1.2402      2.31  |         Q|         |     V    |          |
13+55       1.2559      2.28  |         Q|         |      V   |          |
14+ 0       1.2715      2.27  |         Q|         |      V   |          |
14+ 5       1.2887      2.50  |         Q|         |      V   |          |
14+10       1.3080      2.79  |          |Q        |       V  |          |
14+15       1.3277      2.87  |          |Q        |       V  |          |
14+20       1.3474      2.85  |          |Q        |        V|          |
14+25       1.3666      2.80  |          |Q        |        V|          |
14+30       1.3859      2.79  |          |Q        |        V|          |
14+35       1.4051      2.79  |          |Q        |         V          |
14+40       1.4243      2.80  |          |Q        |         V          |
14+45       1.4436      2.80  |          |Q        |          |V         |
14+50       1.4626      2.75  |          |Q        |          |V         |
14+55       1.4811      2.69  |          Q         |          | V        |
15+ 0       1.4995      2.68  |          Q         |          | V        |
15+ 5       1.5176      2.62  |          Q         |          | V        |
15+10       1.5351      2.55  |          Q         |          |  V       |
15+15       1.5526      2.54  |          Q         |          |  V       |
15+20       1.5697      2.48  |         Q|         |          |  V       |
15+25       1.5863      2.41  |         Q|         |          |   V      |
15+30       1.6028      2.40  |         Q|         |          |   V      |
15+35       1.6178      2.18  |        Q |         |          |    V     |
15+40       1.6308      1.89  |       Q  |         |          |    V     |
15+45       1.6434      1.83  |       Q  |         |          |    V     |
15+50       1.6558      1.80  |       Q  |         |          |    V     |
15+55       1.6682      1.80  |       Q  |         |          |     V    |
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16+ 0       1.6806      1.80  |       Q  |          |          |      V    |
16+ 5       1.6894      1.28  |     Q    |          |          |      V    |
16+10       1.6934      0.59  |  Q       |          |          |      V    |
16+15       1.6964      0.43  |Q         |          |          |      V    |
16+20       1.6989      0.36  |Q         |          |          |      V    |
16+25       1.7011      0.33  |Q         |          |          |      V    |
16+30       1.7033      0.31  |Q         |          |          |      V    |
16+35       1.7053      0.29  |Q         |          |          |      V    |
16+40       1.7070      0.25  |Q         |          |          |      V    |
16+45       1.7087      0.24  Q          |          |          |      V    |
16+50       1.7103      0.24  Q          |          |          |       V   |
16+55       1.7119      0.24  Q          |          |          |       V   |
17+ 0       1.7135      0.24  Q          |          |          |       V   |
17+ 5       1.7156      0.29  |Q         |          |          |       V   |
17+10       1.7181      0.36  |Q         |          |          |       V   |
17+15       1.7207      0.38  |Q         |          |          |       V   |
17+20       1.7233      0.39  |Q         |          |          |       V   |
17+25       1.7260      0.39  |Q         |          |          |       V   |
17+30       1.7287      0.39  |Q         |          |          |       V   |
17+35       1.7315      0.39  |Q         |          |          |       V   |
17+40       1.7342      0.39  |Q         |          |          |       V   |
17+45       1.7369      0.39  |Q         |          |          |       V   |
17+50       1.7394      0.37  |Q         |          |          |       V   |
17+55       1.7416      0.33  |Q         |          |          |       V   |
18+ 0       1.7438      0.32  |Q         |          |          |       V   |
18+ 5       1.7460      0.32  |Q         |          |          |       V   |
18+10       1.7482      0.31  |Q         |          |          |       V   |
18+15       1.7504      0.31  |Q         |          |          |       V   |
18+20       1.7525      0.31  |Q         |          |          |       V   |
18+25       1.7547      0.31  |Q         |          |          |       V   |
18+30       1.7569      0.31  |Q         |          |          |        V  |
18+35       1.7588      0.29  |Q         |          |          |        V  |
18+40       1.7605      0.25  |Q         |          |          |        V  |
18+45       1.7622      0.24  Q          |          |          |        V  |
18+50       1.7637      0.21  Q          |          |          |        V  |
18+55       1.7649      0.17  Q          |          |          |        V  |
19+ 0       1.7660      0.16  Q          |          |          |        V  |
19+ 5       1.7673      0.19  Q          |          |          |        V  |
19+10       1.7688      0.22  Q          |          |          |        V  |
19+15       1.7704      0.23  Q          |          |          |        V  |
19+20       1.7722      0.26  |Q         |          |          |        V  |
19+25       1.7742      0.30  |Q         |          |          |        V  |
19+30       1.7763      0.31  |Q         |          |          |        V  |
19+35       1.7783      0.28  |Q         |          |          |        V  |
19+40       1.7800      0.25  Q          |          |          |        V  |
19+45       1.7817      0.24  Q          |          |          |        V  |
19+50       1.7831      0.21  Q          |          |          |        V  |
19+55       1.7843      0.17  Q          |          |          |        V  |
20+ 0       1.7854      0.16  Q          |          |          |        V  |
20+ 5       1.7867      0.19  Q          |          |          |        V  |
20+10       1.7883      0.22  Q          |          |          |        V  |
20+15       1.7898      0.23  Q          |          |          |        V  |
20+20       1.7915      0.23  Q          |          |          |        V  |
20+25       1.7931      0.23  Q          |          |          |        V  |
20+30       1.7947      0.24  Q          |          |          |        V  |
20+35       1.7963      0.24  Q          |          |          |        V  |
20+40       1.7979      0.24  Q          |          |          |        V  |
20+45       1.7996      0.24  Q          |          |          |        V  |
20+50       1.8010      0.21  Q          |          |          |        V  |
20+55       1.8022      0.17  Q          |          |          |         V |
21+ 0       1.8033      0.16  Q          |          |          |         V |
21+ 5       1.8046      0.19  Q          |          |          |         V |
21+10       1.8061      0.22  Q          |          |          |         V |
21+15       1.8077      0.23  Q          |          |          |         V |
21+20       1.8091      0.21  Q          |          |          |         V |
21+25       1.8103      0.17  Q          |          |          |         V |
21+30       1.8114      0.16  Q          |          |          |         V |
21+35       1.8127      0.19  Q          |          |          |         V |
21+40       1.8142      0.22  Q          |          |          |         V |
21+45       1.8158      0.23  Q          |          |          |         V |
21+50       1.8172      0.21  Q          |          |          |         V |
21+55       1.8184      0.17  Q          |          |          |         V |
22+ 0       1.8195      0.16  Q          |          |          |         V |
22+ 5       1.8208      0.19  Q          |          |          |         V |
22+10       1.8223      0.22  Q          |          |          |         V |
22+15       1.8239      0.23  Q          |          |          |         V |
22+20       1.8253      0.21  Q          |          |          |         V |
22+25       1.8265      0.17  Q          |          |          |         V |
22+30       1.8276      0.16  Q          |          |          |         V |
22+35       1.8287      0.16  Q          |          |          |         V |
22+40       1.8298      0.16  Q          |          |          |         V |
22+45       1.8309      0.16  Q          |          |          |         V |
22+50       1.8320      0.16  Q          |          |          |         V |
22+55       1.8331      0.16  Q          |          |          |         V |
23+ 0       1.8342      0.16  Q          |          |          |         V |
23+ 5       1.8352      0.16  Q          |          |          |         V |
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   23+10       1.8363      0.16  Q          |          |          |          v|
   23+15       1.8374      0.16  Q          |          |          |          v|
   23+20       1.8385      0.16  Q          |          |          |          v|
   23+25       1.8396      0.16  Q          |          |          |          v|
   23+30       1.8407      0.16  Q          |          |          |          v|
   23+35       1.8417      0.16  Q          |          |          |          v|
   23+40       1.8428      0.16  Q          |          |          |          v|
   23+45       1.8439      0.16  Q          |          |          |          v|
   23+50       1.8450      0.16  Q          |          |          |          v|
   23+55       1.8461      0.16  Q          |          |          |          v|
   24+ 0       1.8471      0.16  Q          |          |          |          v|
   24+ 5       1.8478      0.10  Q          |          |          |          v|
   24+10       1.8480      0.03  Q          |          |          |          v|
   24+15       1.8481      0.01  Q          |          |          |          v|
   24+20       1.8482      0.00  Q          |          |          |          v|
   24+25       1.8482      0.00  Q          |          |          |          v|
-------------------------------------------------------------------------------
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Appendix E – Basin Routing and Outflow Calculations

Extended Detention Basin No. 1

Drainage Areas	Storm Event	Existing Condition		Developed		Routed Basin			Ex (cfs) +10% Difference Max
		Flow (cfs)	Volume (ac.ft.)	Flow (cfs)	Volume (ac.ft.)	Routed Basin Out Flow (cfs)	Storage Volume (ac.ft.)	Depth (ft)	
BASIN 1	2 Year - 1 Hour	24.414	0.5905	27.801	0.8252	0.256	0.813	1.09	-0.990
	2 Year - 3 Hour	12.271	0.5324	15.090	1.0911	0.390	1.056	1.38	-0.968
	2 Year - 6 Hour	10.748	0.5686	13.584	1.4087	0.542	1.333	1.72	-0.950
	2 Year - 24 Hour	0.883	0.4084	3.455	2.0108	0.665	1.556	1.99	-0.247
	5 Year - 1 Hour	36.052	0.9826	39.589	1.2294	0.474	1.208	1.57	-0.987
	5 Year - 3 Hour	18.915	0.9607	21.675	1.6091	0.664	1.553	1.99	-0.965
	5 Year - 6 Hour	17.784	1.1262	20.558	2.1615	1.113	2.030	2.52	-0.937
	5 Year - 24 Hour	3.631	0.8560	6.203	3.0093	1.345	2.274	2.80	-0.630
	10 Year - 1 Hour	48.345	1.5864	50.425	1.7037	0.770	1.669	2.12	-0.984
	10 Year - 3 Hour	27.430	2.1065	28.574	2.4556	1.410	2.343	2.87	-0.949
	10 Year - 6 Hour	26.594	2.6586	27.752	3.3486	23.440	2.639	3.19	-0.119
	10 Year - 24 Hour	8.712	3.1005	9.934	4.8202	9.515	2.523	3.07	0.092
	100 Year - 1 Hour	77.592	2.6354	80.047	2.7527	12.283	2.546	3.09	-0.842
	100 Year - 3 Hour	44.128	3.6740	45.122	4.0260	39.828	2.776	3.34	-0.097
	100 Year - 6 Hour	44.275	5.1335	45.277	5.8312	40.883	2.785	3.35	-0.077
	100 Year - 24 Hour	15.619	6.3679	16.840	8.5048	16.714	2.583	3.13	0.070

Basin 1 Size and Flow Calculations

BASIN 1

Horiz. : Vert.

4 : 1 = Basin Side Slope

	BASIN PARAMETERS					OUTLET								
Basin Elevation	Depth	Area S.F.	Volume C.F.	Volume AC-FT	Effective Volume AC-FT	Q1 Orifice Plate (cfs)	Q2 Orifice Plate (cfs)	Q3 Orifice Plate (cfs)	Q4 Orifice Plate (cfs)	Q5Orifice Plate (cfs)	Q6 Orifice Plate (cfs)	Q7Orifice Plate (cfs)	Q Weir 1 (cfs)	Q Total (cfs)
1305.00	0.00	30,759.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1306.00	1.00	33,957.00	32,358.00	0.743	0.743	0.218	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.218
1307.00	2.00	37,229.00	67,988.00	1.561	1.561	0.339	0.329	0.000	0.000	0.000	0.000	0.000	0.000	0.668
1308.00	3.00	40,552.00	106,966.50	2.456	2.456	0.427	1.091	0.000	0.000	0.000	0.000	0.000	0.000	1.518
1308.50	3.50	42,193.00	127,666.00	2.931	2.931	0.465	1.315	0.000	0.000	0.000	0.000	0.000	56.569	58.349
1309.00	4.00	43,834.00	149,186.00	3.425	3.425	0.500	1.507	0.000	0.000	0.000	0.000	0.000	160.000	162.007

SUPPORTING DESIGN PARAMETERS

Orifice Coefficient	0.66	Dia of Orifice	3.00	6.00						
Gravimetric Constant	32.2 ft/s^2	Eff Dia of Orifice	0.2500	0.5000	0.0000	0.0000	0.0000	0.0000	0.0000	
Number of Rows		Area of Orifice	0.0491	0.1963	0.0000	0.0000	0.0000	0.0000	0.0000	
Minimum Orifice Plate Height		Number of Orifeces	1	1	1	1	1	1	1	
Minimum Orifice Plate Width		Elev	1305.3	1306.9						

Weir	Sharp Crest Weir Coefficient	4	
	Length of Weir	40.00	
	Elev. at Crest of Weir	1308	

Q100 Elevation Weir Calc		
Basin 1 Weir Calc		
Crest Wier Elev.	1308.00	
Q100	55.22	cfs
Weir Length	40	
Weir Coeff.	4	
H Weir	0.49202	
Q100 Elevation	**1308.49**	

```
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                            Study date: 05/09/24

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      Program License Serial Number 5006

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      ********************* HYDROGRAPH INFORMATION **********************

                  From study/file name: pro1212.rte
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =    17
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =       27.801 (CFS)
                  Total volume =       0.825 (Ac.Ft)
             Status of hydrographs being held in storage
                       Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
             Peak (CFS)      0.000     0.000     0.000     0.000     0.000
             Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      *************************************************************************



      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
      Process from Point/Station        1.000 to Point/Station        2.000
      **** RETARDING BASIN ROUTING ****
      _________________________________________________________________________

      User entry of depth-outflow-storage data
      ---------------------------------------------------------------------
      Total number of inflow hydrograph intervals = 17
      Hydrograph time unit =  5.000 (Min.)
      Initial depth in storage basin =   0.00(Ft.)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Initial basin depth =   0.00 (Ft.)
      Initial basin storage =      0.00 (Ac.Ft)
      Initial basin outflow =   0.00 (CFS)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Depth vs. Storage and Depth vs. Discharge data:
       Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
            (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
      ---------------------------------------------------------------------
         0.000      0.000      0.000      0.000        0.000
         1.000      0.743      0.218      0.742        0.744
         2.000      1.561      0.668      1.559        1.563
         3.000      2.456      1.518      2.451        2.461
         3.500      2.931     58.349      2.730        3.132
         4.000      3.425    162.007      2.867        3.983
      ---------------------------------------------------------------------
                       Hydrograph Detention Basin Routing
      ---------------------------------------------------------------------

      Graph values: 'I'= unit inflow; 'O'=outflow at time shown
      ---------------------------------------------------------------------
       Time   Inflow  Outflow    Storage                                    Depth
      (Hours)  (CFS)   (CFS)     (Ac.Ft) .0       7.0   13.90   20.85   27.80 (Ft.)
       0.083    0.86    0.00      0.003  O       |       |       |       |     0.00
       0.167    2.36    0.00      0.014  O I     |       |       |       |     0.02
       0.250    3.06    0.01      0.033  O  I    |       |       |       |     0.04
       0.333    3.53    0.02      0.055  O   I   |       |       |       |     0.07
       0.417    4.13    0.02      0.082  O   I   |       |       |       |     0.11
       0.500    5.08    0.03      0.113  O    I  |       |       |       |     0.15
       0.583    6.28    0.04      0.152  O      I|       |       |       |     0.20
       0.667    8.02    0.06      0.201  O       I       |       |       |     0.27
       0.750   12.43    0.08      0.271  O       |     I |       |       |     0.36
       0.833   25.97    0.12      0.402  O       |       |       |    I  |     0.54
       0.917   27.80    0.17      0.586  O       |       |       |       I     0.79
       1.000   11.44    0.21      0.720  O       |    I  |       |       |     0.97
       1.083    5.34    0.24      0.777  O     I |       |       |       |     1.04
       1.167    2.23    0.25      0.801  O I     |       |       |       |     1.07
       1.250    1.04    0.26      0.810  OI      |       |       |       |     1.08
       1.333    0.19    0.26      0.813  O       |       |       |       |     1.09
       1.417    0.04    0.26      0.812  O       |       |       |       |     1.08
       1.500    0.00    0.26      0.810  O       |       |       |       |     1.08
       1.583    0.00    0.25      0.809  O       |       |       |       |     1.08
       1.667    0.00    0.25      0.807  O       |       |       |       |     1.08
       1.750    0.00    0.25      0.805  O       |       |       |       |     1.08
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1.833	0.00	0.25	0.803	o	|	|	|	1.07
1.917	0.00	0.25	0.802	o	|	|	|	1.07
2.000	0.00	0.25	0.800	o	|	|	|	1.07
2.083	0.00	0.25	0.798	o	|	|	|	1.07
2.167	0.00	0.25	0.796	o	|	|	|	1.07
2.250	0.00	0.25	0.795	o	|	|	|	1.06
2.333	0.00	0.25	0.793	o	|	|	|	1.06
2.417	0.00	0.24	0.791	o	|	|	|	1.06
2.500	0.00	0.24	0.790	o	|	|	|	1.06
2.583	0.00	0.24	0.788	o	|	|	|	1.06
2.667	0.00	0.24	0.786	o	|	|	|	1.05
2.750	0.00	0.24	0.785	o	|	|	|	1.05
2.833	0.00	0.24	0.783	o	|	|	|	1.05
2.917	0.00	0.24	0.781	o	|	|	|	1.05
3.000	0.00	0.24	0.780	o	|	|	|	1.04
3.083	0.00	0.24	0.778	o	|	|	|	1.04
3.167	0.00	0.24	0.777	o	|	|	|	1.04
3.250	0.00	0.24	0.775	o	|	|	|	1.04
3.333	0.00	0.23	0.773	o	|	|	|	1.04
3.417	0.00	0.23	0.772	o	|	|	|	1.04
3.500	0.00	0.23	0.770	o	|	|	|	1.03
3.583	0.00	0.23	0.768	o	|	|	|	1.03
3.667	0.00	0.23	0.767	o	|	|	|	1.03
3.750	0.00	0.23	0.765	o	|	|	|	1.03
3.833	0.00	0.23	0.764	o	|	|	|	1.03
3.917	0.00	0.23	0.762	o	|	|	|	1.02
4.000	0.00	0.23	0.761	o	|	|	|	1.02
4.083	0.00	0.23	0.759	o	|	|	|	1.02
4.167	0.00	0.23	0.757	o	|	|	|	1.02
4.250	0.00	0.23	0.756	o	|	|	|	1.02
4.333	0.00	0.22	0.754	o	|	|	|	1.01
4.417	0.00	0.22	0.753	o	|	|	|	1.01
4.500	0.00	0.22	0.751	o	|	|	|	1.01
4.583	0.00	0.22	0.750	o	|	|	|	1.01
4.667	0.00	0.22	0.748	o	|	|	|	1.01
4.750	0.00	0.22	0.747	o	|	|	|	1.00
4.833	0.00	0.22	0.745	o	|	|	|	1.00
4.917	0.00	0.22	0.744	o	|	|	|	1.00
5.000	0.00	0.22	0.742	o	|	|	|	1.00
5.083	0.00	0.22	0.741	o	|	|	|	1.00
5.167	0.00	0.22	0.739	o	|	|	|	0.99
5.250	0.00	0.22	0.738	o	|	|	|	0.99
5.333	0.00	0.22	0.736	o	|	|	|	0.99
5.417	0.00	0.22	0.735	o	|	|	|	0.99
5.500	0.00	0.22	0.733	o	|	|	|	0.99
5.583	0.00	0.21	0.732	o	|	|	|	0.98
5.667	0.00	0.21	0.730	o	|	|	|	0.98
5.750	0.00	0.21	0.729	o	|	|	|	0.98
5.833	0.00	0.21	0.727	o	|	|	|	0.98
5.917	0.00	0.21	0.726	o	|	|	|	0.98
6.000	0.00	0.21	0.724	o	|	|	|	0.97
6.083	0.00	0.21	0.723	o	|	|	|	0.97
6.167	0.00	0.21	0.721	o	|	|	|	0.97
6.250	0.00	0.21	0.720	o	|	|	|	0.97
6.333	0.00	0.21	0.719	o	|	|	|	0.97
6.417	0.00	0.21	0.717	o	|	|	|	0.97
6.500	0.00	0.21	0.716	o	|	|	|	0.96
6.583	0.00	0.21	0.714	o	|	|	|	0.96
6.667	0.00	0.21	0.713	o	|	|	|	0.96
6.750	0.00	0.21	0.711	o	|	|	|	0.96
6.833	0.00	0.21	0.710	o	|	|	|	0.96
6.917	0.00	0.21	0.708	o	|	|	|	0.95
7.000	0.00	0.21	0.707	o	|	|	|	0.95
7.083	0.00	0.21	0.706	o	|	|	|	0.95
7.167	0.00	0.21	0.704	o	|	|	|	0.95
7.250	0.00	0.21	0.703	o	|	|	|	0.95
7.333	0.00	0.21	0.701	o	|	|	|	0.94
7.417	0.00	0.21	0.700	o	|	|	|	0.94
7.500	0.00	0.20	0.698	o	|	|	|	0.94
7.583	0.00	0.20	0.697	o	|	|	|	0.94
7.667	0.00	0.20	0.696	o	|	|	|	0.94
7.750	0.00	0.20	0.694	o	|	|	|	0.93
7.833	0.00	0.20	0.693	o	|	|	|	0.93
7.917	0.00	0.20	0.691	o	|	|	|	0.93
8.000	0.00	0.20	0.690	o	|	|	|	0.93
8.083	0.00	0.20	0.689	o	|	|	|	0.93
8.167	0.00	0.20	0.687	o	|	|	|	0.93
8.250	0.00	0.20	0.686	o	|	|	|	0.92
8.333	0.00	0.20	0.685	o	|	|	|	0.92
8.417	0.00	0.20	0.683	o	|	|	|	0.92
8.500	0.00	0.20	0.682	o	|	|	|	0.92
8.583	0.00	0.20	0.680	o	|	|	|	0.92
8.667	0.00	0.20	0.679	o	|	|	|	0.91
8.750	0.00	0.20	0.678	o	|	|	|	0.91
8.833	0.00	0.20	0.676	o	|	|	|	0.91
8.917	0.00	0.20	0.675	o	|	|	|	0.91

9.000	0.00	0.20	0.674	o	|	|	|	|	0.91
9.083	0.00	0.20	0.672	o	|	|	|	|	0.90
9.167	0.00	0.20	0.671	o	|	|	|	|	0.90
9.250	0.00	0.20	0.669	o	|	|	|	|	0.90
9.333	0.00	0.20	0.668	o	|	|	|	|	0.90
9.417	0.00	0.20	0.667	o	|	|	|	|	0.90
9.500	0.00	0.20	0.665	o	|	|	|	|	0.90
9.583	0.00	0.19	0.664	o	|	|	|	|	0.89
9.667	0.00	0.19	0.663	o	|	|	|	|	0.89
9.750	0.00	0.19	0.661	o	|	|	|	|	0.89
9.833	0.00	0.19	0.660	o	|	|	|	|	0.89
9.917	0.00	0.19	0.659	o	|	|	|	|	0.89
10.000	0.00	0.19	0.657	o	|	|	|	|	0.88
10.083	0.00	0.19	0.656	o	|	|	|	|	0.88
10.167	0.00	0.19	0.655	o	|	|	|	|	0.88
10.250	0.00	0.19	0.653	o	|	|	|	|	0.88
10.333	0.00	0.19	0.652	o	|	|	|	|	0.88
10.417	0.00	0.19	0.651	o	|	|	|	|	0.88
10.500	0.00	0.19	0.649	o	|	|	|	|	0.87
10.583	0.00	0.19	0.648	o	|	|	|	|	0.87
10.667	0.00	0.19	0.647	o	|	|	|	|	0.87
10.750	0.00	0.19	0.646	o	|	|	|	|	0.87
10.833	0.00	0.19	0.644	o	|	|	|	|	0.87
10.917	0.00	0.19	0.643	o	|	|	|	|	0.87
11.000	0.00	0.19	0.642	o	|	|	|	|	0.86
11.083	0.00	0.19	0.640	o	|	|	|	|	0.86
11.167	0.00	0.19	0.639	o	|	|	|	|	0.86
11.250	0.00	0.19	0.638	o	|	|	|	|	0.86
11.333	0.00	0.19	0.636	o	|	|	|	|	0.86
11.417	0.00	0.19	0.635	o	|	|	|	|	0.85
11.500	0.00	0.19	0.634	o	|	|	|	|	0.85
11.583	0.00	0.19	0.633	o	|	|	|	|	0.85
11.667	0.00	0.19	0.631	o	|	|	|	|	0.85
11.750	0.00	0.18	0.630	o	|	|	|	|	0.85
11.833	0.00	0.18	0.629	o	|	|	|	|	0.85
11.917	0.00	0.18	0.628	o	|	|	|	|	0.84
12.000	0.00	0.18	0.626	o	|	|	|	|	0.84
12.083	0.00	0.18	0.625	o	|	|	|	|	0.84
12.167	0.00	0.18	0.624	o	|	|	|	|	0.84
12.250	0.00	0.18	0.622	o	|	|	|	|	0.84
12.333	0.00	0.18	0.621	o	|	|	|	|	0.84
12.417	0.00	0.18	0.620	o	|	|	|	|	0.83
12.500	0.00	0.18	0.619	o	|	|	|	|	0.83
12.583	0.00	0.18	0.617	o	|	|	|	|	0.83
12.667	0.00	0.18	0.616	o	|	|	|	|	0.83
12.750	0.00	0.18	0.615	o	|	|	|	|	0.83
12.833	0.00	0.18	0.614	o	|	|	|	|	0.83
12.917	0.00	0.18	0.613	o	|	|	|	|	0.82
13.000	0.00	0.18	0.611	o	|	|	|	|	0.82
13.083	0.00	0.18	0.610	o	|	|	|	|	0.82
13.167	0.00	0.18	0.609	o	|	|	|	|	0.82
13.250	0.00	0.18	0.608	o	|	|	|	|	0.82
13.333	0.00	0.18	0.606	o	|	|	|	|	0.82
13.417	0.00	0.18	0.605	o	|	|	|	|	0.81
13.500	0.00	0.18	0.604	o	|	|	|	|	0.81
13.583	0.00	0.18	0.603	o	|	|	|	|	0.81
13.667	0.00	0.18	0.601	o	|	|	|	|	0.81
13.750	0.00	0.18	0.600	o	|	|	|	|	0.81
13.833	0.00	0.18	0.599	o	|	|	|	|	0.81
13.917	0.00	0.18	0.598	o	|	|	|	|	0.80
14.000	0.00	0.18	0.597	o	|	|	|	|	0.80
14.083	0.00	0.17	0.595	o	|	|	|	|	0.80
14.167	0.00	0.17	0.594	o	|	|	|	|	0.80
14.250	0.00	0.17	0.593	o	|	|	|	|	0.80
14.333	0.00	0.17	0.592	o	|	|	|	|	0.80
14.417	0.00	0.17	0.591	o	|	|	|	|	0.79
14.500	0.00	0.17	0.589	o	|	|	|	|	0.79
14.583	0.00	0.17	0.588	o	|	|	|	|	0.79
14.667	0.00	0.17	0.587	o	|	|	|	|	0.79
14.750	0.00	0.17	0.586	o	|	|	|	|	0.79
14.833	0.00	0.17	0.585	o	|	|	|	|	0.79
14.917	0.00	0.17	0.584	o	|	|	|	|	0.79
15.000	0.00	0.17	0.582	o	|	|	|	|	0.78
15.083	0.00	0.17	0.581	o	|	|	|	|	0.78
15.167	0.00	0.17	0.580	o	|	|	|	|	0.78
15.250	0.00	0.17	0.579	o	|	|	|	|	0.78
15.333	0.00	0.17	0.578	o	|	|	|	|	0.78
15.417	0.00	0.17	0.576	o	|	|	|	|	0.78
15.500	0.00	0.17	0.575	o	|	|	|	|	0.77
15.583	0.00	0.17	0.574	o	|	|	|	|	0.77
15.667	0.00	0.17	0.573	o	|	|	|	|	0.77
15.750	0.00	0.17	0.572	o	|	|	|	|	0.77
15.833	0.00	0.17	0.571	o	|	|	|	|	0.77
15.917	0.00	0.17	0.570	o	|	|	|	|	0.77
16.000	0.00	0.17	0.568	o	|	|	|	|	0.76
16.083	0.00	0.17	0.567	o	|	|	|	|	0.76

16.167	0.00	0.17	0.566	o	|	|	|	|	0.76
16.250	0.00	0.17	0.565	o	|	|	|	|	0.76
16.333	0.00	0.17	0.564	o	|	|	|	|	0.76
16.417	0.00	0.17	0.563	o	|	|	|	|	0.76
16.500	0.00	0.16	0.562	o	|	|	|	|	0.76
16.583	0.00	0.16	0.560	o	|	|	|	|	0.75
16.667	0.00	0.16	0.559	o	|	|	|	|	0.75
16.750	0.00	0.16	0.558	o	|	|	|	|	0.75
16.833	0.00	0.16	0.557	o	|	|	|	|	0.75
16.917	0.00	0.16	0.556	o	|	|	|	|	0.75
17.000	0.00	0.16	0.555	o	|	|	|	|	0.75
17.083	0.00	0.16	0.554	o	|	|	|	|	0.75
17.167	0.00	0.16	0.553	o	|	|	|	|	0.74
17.250	0.00	0.16	0.551	o	|	|	|	|	0.74
17.333	0.00	0.16	0.550	o	|	|	|	|	0.74
17.417	0.00	0.16	0.549	o	|	|	|	|	0.74
17.500	0.00	0.16	0.548	o	|	|	|	|	0.74
17.583	0.00	0.16	0.547	o	|	|	|	|	0.74
17.667	0.00	0.16	0.546	o	|	|	|	|	0.73
17.750	0.00	0.16	0.545	o	|	|	|	|	0.73
17.833	0.00	0.16	0.544	o	|	|	|	|	0.73
17.917	0.00	0.16	0.543	o	|	|	|	|	0.73
18.000	0.00	0.16	0.541	o	|	|	|	|	0.73
18.083	0.00	0.16	0.540	o	|	|	|	|	0.73
18.167	0.00	0.16	0.539	o	|	|	|	|	0.73
18.250	0.00	0.16	0.538	o	|	|	|	|	0.72
18.333	0.00	0.16	0.537	o	|	|	|	|	0.72
18.417	0.00	0.16	0.536	o	|	|	|	|	0.72
18.500	0.00	0.16	0.535	o	|	|	|	|	0.72
18.583	0.00	0.16	0.534	o	|	|	|	|	0.72
18.667	0.00	0.16	0.533	o	|	|	|	|	0.72
18.750	0.00	0.16	0.532	o	|	|	|	|	0.72
18.833	0.00	0.16	0.531	o	|	|	|	|	0.71
18.917	0.00	0.16	0.530	o	|	|	|	|	0.71
19.000	0.00	0.16	0.529	o	|	|	|	|	0.71
19.083	0.00	0.15	0.527	o	|	|	|	|	0.71
19.167	0.00	0.15	0.526	o	|	|	|	|	0.71
19.250	0.00	0.15	0.525	o	|	|	|	|	0.71
19.333	0.00	0.15	0.524	o	|	|	|	|	0.71
19.417	0.00	0.15	0.523	o	|	|	|	|	0.70
19.500	0.00	0.15	0.522	o	|	|	|	|	0.70
19.583	0.00	0.15	0.521	o	|	|	|	|	0.70
19.667	0.00	0.15	0.520	o	|	|	|	|	0.70
19.750	0.00	0.15	0.519	o	|	|	|	|	0.70
19.833	0.00	0.15	0.518	o	|	|	|	|	0.70
19.917	0.00	0.15	0.517	o	|	|	|	|	0.70
20.000	0.00	0.15	0.516	o	|	|	|	|	0.69
20.083	0.00	0.15	0.515	o	|	|	|	|	0.69
20.167	0.00	0.15	0.514	o	|	|	|	|	0.69
20.250	0.00	0.15	0.513	o	|	|	|	|	0.69
20.333	0.00	0.15	0.512	o	|	|	|	|	0.69
20.417	0.00	0.15	0.511	o	|	|	|	|	0.69
20.500	0.00	0.15	0.510	o	|	|	|	|	0.69
20.583	0.00	0.15	0.509	o	|	|	|	|	0.68
20.667	0.00	0.15	0.508	o	|	|	|	|	0.68
20.750	0.00	0.15	0.507	o	|	|	|	|	0.68
20.833	0.00	0.15	0.506	o	|	|	|	|	0.68
20.917	0.00	0.15	0.505	o	|	|	|	|	0.68
21.000	0.00	0.15	0.503	o	|	|	|	|	0.68
21.083	0.00	0.15	0.502	o	|	|	|	|	0.68
21.167	0.00	0.15	0.501	o	|	|	|	|	0.67
21.250	0.00	0.15	0.500	o	|	|	|	|	0.67
21.333	0.00	0.15	0.499	o	|	|	|	|	0.67
21.417	0.00	0.15	0.498	o	|	|	|	|	0.67
21.500	0.00	0.15	0.497	o	|	|	|	|	0.67
21.583	0.00	0.15	0.496	o	|	|	|	|	0.67
21.667	0.00	0.15	0.495	o	|	|	|	|	0.67
21.750	0.00	0.15	0.494	o	|	|	|	|	0.67
21.833	0.00	0.14	0.493	o	|	|	|	|	0.66
21.917	0.00	0.14	0.492	o	|	|	|	|	0.66
22.000	0.00	0.14	0.491	o	|	|	|	|	0.66
22.083	0.00	0.14	0.490	o	|	|	|	|	0.66
22.167	0.00	0.14	0.489	o	|	|	|	|	0.66
22.250	0.00	0.14	0.488	o	|	|	|	|	0.66
22.333	0.00	0.14	0.487	o	|	|	|	|	0.66
22.417	0.00	0.14	0.486	o	|	|	|	|	0.65
22.500	0.00	0.14	0.486	o	|	|	|	|	0.65
22.583	0.00	0.14	0.485	o	|	|	|	|	0.65
22.667	0.00	0.14	0.484	o	|	|	|	|	0.65
22.750	0.00	0.14	0.483	o	|	|	|	|	0.65
22.833	0.00	0.14	0.482	o	|	|	|	|	0.65
22.917	0.00	0.14	0.481	o	|	|	|	|	0.65
23.000	0.00	0.14	0.480	o	|	|	|	|	0.65
23.083	0.00	0.14	0.479	o	|	|	|	|	0.64
23.167	0.00	0.14	0.478	o	|	|	|	|	0.64
23.250	0.00	0.14	0.477	o	|	|	|	|	0.64

23.333	0.00	0.14	0.476	o	|	|	|	|	0.64
23.417	0.00	0.14	0.475	o	|	|	|	|	0.64
23.500	0.00	0.14	0.474	o	|	|	|	|	0.64
23.583	0.00	0.14	0.473	o	|	|	|	|	0.64
23.667	0.00	0.14	0.472	o	|	|	|	|	0.64
23.750	0.00	0.14	0.471	o	|	|	|	|	0.63
23.833	0.00	0.14	0.470	o	|	|	|	|	0.63
23.917	0.00	0.14	0.469	o	|	|	|	|	0.63
24.000	0.00	0.14	0.468	o	|	|	|	|	0.63
24.083	0.00	0.14	0.467	o	|	|	|	|	0.63
24.167	0.00	0.14	0.466	o	|	|	|	|	0.63
24.250	0.00	0.14	0.465	o	|	|	|	|	0.63
24.333	0.00	0.14	0.464	o	|	|	|	|	0.63
24.417	0.00	0.14	0.463	o	|	|	|	|	0.62
24.500	0.00	0.14	0.463	o	|	|	|	|	0.62
24.583	0.00	0.14	0.462	o	|	|	|	|	0.62
24.667	0.00	0.14	0.461	o	|	|	|	|	0.62
24.750	0.00	0.13	0.460	o	|	|	|	|	0.62
24.833	0.00	0.13	0.459	o	|	|	|	|	0.62
24.917	0.00	0.13	0.458	o	|	|	|	|	0.62
25.000	0.00	0.13	0.457	o	|	|	|	|	0.61
25.083	0.00	0.13	0.456	o	|	|	|	|	0.61
25.167	0.00	0.13	0.455	o	|	|	|	|	0.61
25.250	0.00	0.13	0.454	o	|	|	|	|	0.61
25.333	0.00	0.13	0.453	o	|	|	|	|	0.61
25.417	0.00	0.13	0.452	o	|	|	|	|	0.61
25.500	0.00	0.13	0.451	o	|	|	|	|	0.61
25.583	0.00	0.13	0.451	o	|	|	|	|	0.61
25.667	0.00	0.13	0.450	o	|	|	|	|	0.61
25.750	0.00	0.13	0.449	o	|	|	|	|	0.60
25.833	0.00	0.13	0.448	o	|	|	|	|	0.60
25.917	0.00	0.13	0.447	o	|	|	|	|	0.60
26.000	0.00	0.13	0.446	o	|	|	|	|	0.60
26.083	0.00	0.13	0.445	o	|	|	|	|	0.60
26.167	0.00	0.13	0.444	o	|	|	|	|	0.60
26.250	0.00	0.13	0.443	o	|	|	|	|	0.60
26.333	0.00	0.13	0.442	o	|	|	|	|	0.60
26.417	0.00	0.13	0.442	o	|	|	|	|	0.59
26.500	0.00	0.13	0.441	o	|	|	|	|	0.59
26.583	0.00	0.13	0.440	o	|	|	|	|	0.59
26.667	0.00	0.13	0.439	o	|	|	|	|	0.59
26.750	0.00	0.13	0.438	o	|	|	|	|	0.59
26.833	0.00	0.13	0.437	o	|	|	|	|	0.59
26.917	0.00	0.13	0.436	o	|	|	|	|	0.59
27.000	0.00	0.13	0.435	o	|	|	|	|	0.59
27.083	0.00	0.13	0.434	o	|	|	|	|	0.58
27.167	0.00	0.13	0.434	o	|	|	|	|	0.58
27.250	0.00	0.13	0.433	o	|	|	|	|	0.58
27.333	0.00	0.13	0.432	o	|	|	|	|	0.58
27.417	0.00	0.13	0.431	o	|	|	|	|	0.58
27.500	0.00	0.13	0.430	o	|	|	|	|	0.58
27.583	0.00	0.13	0.429	o	|	|	|	|	0.58
27.667	0.00	0.13	0.428	o	|	|	|	|	0.58
27.750	0.00	0.13	0.427	o	|	|	|	|	0.58
27.833	0.00	0.13	0.427	o	|	|	|	|	0.57
27.917	0.00	0.12	0.426	o	|	|	|	|	0.57
28.000	0.00	0.12	0.425	o	|	|	|	|	0.57
28.083	0.00	0.12	0.424	o	|	|	|	|	0.57
28.167	0.00	0.12	0.423	o	|	|	|	|	0.57
28.250	0.00	0.12	0.422	o	|	|	|	|	0.57
28.333	0.00	0.12	0.421	o	|	|	|	|	0.57
28.417	0.00	0.12	0.421	o	|	|	|	|	0.57
28.500	0.00	0.12	0.420	o	|	|	|	|	0.56
28.583	0.00	0.12	0.419	o	|	|	|	|	0.56
28.667	0.00	0.12	0.418	o	|	|	|	|	0.56
28.750	0.00	0.12	0.417	o	|	|	|	|	0.56
28.833	0.00	0.12	0.416	o	|	|	|	|	0.56
28.917	0.00	0.12	0.416	o	|	|	|	|	0.56
29.000	0.00	0.12	0.415	o	|	|	|	|	0.56
29.083	0.00	0.12	0.414	o	|	|	|	|	0.56
29.167	0.00	0.12	0.413	o	|	|	|	|	0.56
29.250	0.00	0.12	0.412	o	|	|	|	|	0.55
29.333	0.00	0.12	0.411	o	|	|	|	|	0.55
29.417	0.00	0.12	0.411	o	|	|	|	|	0.55
29.500	0.00	0.12	0.410	o	|	|	|	|	0.55
29.583	0.00	0.12	0.409	o	|	|	|	|	0.55
29.667	0.00	0.12	0.408	o	|	|	|	|	0.55
29.750	0.00	0.12	0.407	o	|	|	|	|	0.55
29.833	0.00	0.12	0.406	o	|	|	|	|	0.55
29.917	0.00	0.12	0.406	o	|	|	|	|	0.55
30.000	0.00	0.12	0.405	o	|	|	|	|	0.54
30.083	0.00	0.12	0.404	o	|	|	|	|	0.54
30.167	0.00	0.12	0.403	o	|	|	|	|	0.54
30.250	0.00	0.12	0.402	o	|	|	|	|	0.54
30.333	0.00	0.12	0.402	o	|	|	|	|	0.54
30.417	0.00	0.12	0.401	o	|	|	|	|	0.54

30.500	0.00	0.12	0.400	o	|	|	|	0.54
30.583	0.00	0.12	0.399	o	|	|	|	0.54
30.667	0.00	0.12	0.398	o	|	|	|	0.54
30.750	0.00	0.12	0.397	o	|	|	|	0.53
30.833	0.00	0.12	0.397	o	|	|	|	0.53
30.917	0.00	0.12	0.396	o	|	|	|	0.53
31.000	0.00	0.12	0.395	o	|	|	|	0.53
31.083	0.00	0.12	0.394	o	|	|	|	0.53
31.167	0.00	0.12	0.393	o	|	|	|	0.53
31.250	0.00	0.12	0.393	o	|	|	|	0.53
31.333	0.00	0.11	0.392	o	|	|	|	0.53
31.417	0.00	0.11	0.391	o	|	|	|	0.53
31.500	0.00	0.11	0.390	o	|	|	|	0.53
31.583	0.00	0.11	0.390	o	|	|	|	0.52
31.667	0.00	0.11	0.389	o	|	|	|	0.52
31.750	0.00	0.11	0.388	o	|	|	|	0.52
31.833	0.00	0.11	0.387	o	|	|	|	0.52
31.917	0.00	0.11	0.386	o	|	|	|	0.52
32.000	0.00	0.11	0.386	o	|	|	|	0.52
32.083	0.00	0.11	0.385	o	|	|	|	0.52
32.167	0.00	0.11	0.384	o	|	|	|	0.52
32.250	0.00	0.11	0.383	o	|	|	|	0.52
32.333	0.00	0.11	0.383	o	|	|	|	0.51
32.417	0.00	0.11	0.382	o	|	|	|	0.51
32.500	0.00	0.11	0.381	o	|	|	|	0.51
32.583	0.00	0.11	0.380	o	|	|	|	0.51
32.667	0.00	0.11	0.379	o	|	|	|	0.51
32.750	0.00	0.11	0.379	o	|	|	|	0.51
32.833	0.00	0.11	0.378	o	|	|	|	0.51
32.917	0.00	0.11	0.377	o	|	|	|	0.51
33.000	0.00	0.11	0.376	o	|	|	|	0.51
33.083	0.00	0.11	0.376	o	|	|	|	0.51
33.167	0.00	0.11	0.375	o	|	|	|	0.50
33.250	0.00	0.11	0.374	o	|	|	|	0.50
33.333	0.00	0.11	0.373	o	|	|	|	0.50
33.417	0.00	0.11	0.373	o	|	|	|	0.50
33.500	0.00	0.11	0.372	o	|	|	|	0.50
33.583	0.00	0.11	0.371	o	|	|	|	0.50
33.667	0.00	0.11	0.370	o	|	|	|	0.50
33.750	0.00	0.11	0.370	o	|	|	|	0.50
33.833	0.00	0.11	0.369	o	|	|	|	0.50
33.917	0.00	0.11	0.368	o	|	|	|	0.50
34.000	0.00	0.11	0.367	o	|	|	|	0.49
34.083	0.00	0.11	0.367	o	|	|	|	0.49
34.167	0.00	0.11	0.366	o	|	|	|	0.49
34.250	0.00	0.11	0.365	o	|	|	|	0.49
34.333	0.00	0.11	0.364	o	|	|	|	0.49
34.417	0.00	0.11	0.364	o	|	|	|	0.49
34.500	0.00	0.11	0.363	o	|	|	|	0.49
34.583	0.00	0.11	0.362	o	|	|	|	0.49
34.667	0.00	0.11	0.361	o	|	|	|	0.49
34.750	0.00	0.11	0.361	o	|	|	|	0.49
34.833	0.00	0.11	0.360	o	|	|	|	0.48
34.917	0.00	0.11	0.359	o	|	|	|	0.48
35.000	0.00	0.11	0.359	o	|	|	|	0.48
35.083	0.00	0.10	0.358	o	|	|	|	0.48
35.167	0.00	0.10	0.357	o	|	|	|	0.48
35.250	0.00	0.10	0.356	o	|	|	|	0.48
35.333	0.00	0.10	0.356	o	|	|	|	0.48
35.417	0.00	0.10	0.355	o	|	|	|	0.48
35.500	0.00	0.10	0.354	o	|	|	|	0.48
35.583	0.00	0.10	0.354	o	|	|	|	0.48
35.667	0.00	0.10	0.353	o	|	|	|	0.47
35.750	0.00	0.10	0.352	o	|	|	|	0.47
35.833	0.00	0.10	0.351	o	|	|	|	0.47
35.917	0.00	0.10	0.351	o	|	|	|	0.47
36.000	0.00	0.10	0.350	o	|	|	|	0.47
36.083	0.00	0.10	0.349	o	|	|	|	0.47
36.167	0.00	0.10	0.349	o	|	|	|	0.47
36.250	0.00	0.10	0.348	o	|	|	|	0.47
36.333	0.00	0.10	0.347	o	|	|	|	0.47
36.417	0.00	0.10	0.346	o	|	|	|	0.47
36.500	0.00	0.10	0.346	o	|	|	|	0.47
36.583	0.00	0.10	0.345	o	|	|	|	0.46
36.667	0.00	0.10	0.344	o	|	|	|	0.46
36.750	0.00	0.10	0.344	o	|	|	|	0.46
36.833	0.00	0.10	0.343	o	|	|	|	0.46
36.917	0.00	0.10	0.342	o	|	|	|	0.46
37.000	0.00	0.10	0.342	o	|	|	|	0.46
37.083	0.00	0.10	0.341	o	|	|	|	0.46
37.167	0.00	0.10	0.340	o	|	|	|	0.46

Remaining water in basin = 0.34 (Ac.Ft)

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**************************HYDROGRAPH DATA**************************
               Number of intervals =   446
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =        0.256 (CFS)
               Total volume =       0.485 (Ac.Ft)
        Status of hydrographs being held in storage
                    Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
        Peak (CFS)      0.000     0.000     0.000     0.000     0.000
        Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
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FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro1232.rte
**********HYDROGRAPH DATA**********
Number of intervals = 41
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 15.090 (CFS)
Total volume = 1.091 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 41
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 3.8 7.54 11.32 15.09	Depth (Ft.)
0.083	0.55	0.00	0.002	OI	0.00
0.167	1.34	0.00	0.008	O I	0.01
0.250	1.45	0.01	0.018	O I	0.02
0.333	1.58	0.01	0.028	O I	0.04
0.417	1.83	0.01	0.040	O I	0.05
0.500	2.03	0.02	0.053	O I	0.07
0.583	2.11	0.02	0.067	O I	0.09
0.667	2.10	0.02	0.082	O I	0.11
0.750	2.27	0.03	0.097	O I	0.13
0.833	2.18	0.03	0.112	O I	0.15
0.917	2.05	0.04	0.126	O I	0.17
1.000	2.16	0.04	0.140	O I	0.19
1.083	2.45	0.05	0.156	O I	0.21
1.167	2.72	0.05	0.173	O I	0.23
1.250	2.79	0.06	0.192	O I	0.26
1.333	2.74	0.06	0.210	O I	0.28
1.417	2.88	0.07	0.229	O I	0.31
1.500	3.27	0.07	0.250	O I	0.34
1.583	3.28	0.08	0.272	O I	0.37
1.667	3.27	0.09	0.294	O I	0.40
1.750	3.89	0.09	0.318	O I	0.43

1.833	4.41	0.10	0.346	o	|I	|	|	|	|	0.47
1.917	4.17	0.11	0.375	o	I	|	|	|	|	0.50
2.000	4.03	0.12	0.402	o	I	|	|	|	|	0.54
2.083	4.19	0.13	0.430	o	I	|	|	|	|	0.58
2.167	5.24	0.14	0.461	o	| I	|	|	|	|	0.62
2.250	7.28	0.15	0.504	o	| I|	|	|	|	|	0.68
2.333	7.34	0.16	0.553	o	| I|	|	|	|	|	0.74
2.417	8.66	0.18	0.607	o	| I	|	|	|	|	0.82
2.500	12.85	0.20	0.680	o	|	|	| I	|	|	0.91
2.583	15.09	0.24	0.774	o	|	|	|	| I	|	1.04
2.667	14.76	0.29	0.875	o	|	|	|	| I|	|	1.16
2.750	9.52	0.34	0.957	o	|	| I	|	|	|	1.26
2.833	4.76	0.36	1.003	o	| I	|	|	|	|	1.32
2.917	3.40	0.38	1.029	o	I|	|	|	|	|	1.35
3.000	2.30	0.38	1.046	o	I |	|	|	|	|	1.37
3.083	0.98	0.39	1.055	o	I |	|	|	|	|	1.38
3.167	0.30	0.39	1.056	o	|	|	|	|	|	1.38
3.250	0.13	0.39	1.055	o	|	|	|	|	|	1.38
3.333	0.05	0.39	1.053	o	|	|	|	|	|	1.38
3.417	0.01	0.39	1.051	o	|	|	|	|	|	1.38
3.500	0.00	0.39	1.048	o	|	|	|	|	|	1.37
3.583	0.00	0.38	1.045	o	|	|	|	|	|	1.37
3.667	0.00	0.38	1.043	o	|	|	|	|	|	1.37
3.750	0.00	0.38	1.040	o	|	|	|	|	|	1.36
3.833	0.00	0.38	1.038	o	|	|	|	|	|	1.36
3.917	0.00	0.38	1.035	o	|	|	|	|	|	1.36
4.000	0.00	0.38	1.032	o	|	|	|	|	|	1.35
4.083	0.00	0.38	1.030	o	|	|	|	|	|	1.35
4.167	0.00	0.37	1.027	o	|	|	|	|	|	1.35
4.250	0.00	0.37	1.025	o	|	|	|	|	|	1.34
4.333	0.00	0.37	1.022	o	|	|	|	|	|	1.34
4.417	0.00	0.37	1.019	o	|	|	|	|	|	1.34
4.500	0.00	0.37	1.017	o	|	|	|	|	|	1.33
4.583	0.00	0.37	1.014	o	|	|	|	|	|	1.33
4.667	0.00	0.37	1.012	o	|	|	|	|	|	1.33
4.750	0.00	0.36	1.009	o	|	|	|	|	|	1.33
4.833	0.00	0.36	1.007	o	|	|	|	|	|	1.32
4.917	0.00	0.36	1.004	o	|	|	|	|	|	1.32
5.000	0.00	0.36	1.002	o	|	|	|	|	|	1.32
5.083	0.00	0.36	0.999	o	|	|	|	|	|	1.31
5.167	0.00	0.36	0.997	o	|	|	|	|	|	1.31
5.250	0.00	0.36	0.994	o	|	|	|	|	|	1.31
5.333	0.00	0.35	0.992	o	|	|	|	|	|	1.30
5.417	0.00	0.35	0.990	o	|	|	|	|	|	1.30
5.500	0.00	0.35	0.987	o	|	|	|	|	|	1.30
5.583	0.00	0.35	0.985	o	|	|	|	|	|	1.30
5.667	0.00	0.35	0.982	o	|	|	|	|	|	1.29
5.750	0.00	0.35	0.980	o	|	|	|	|	|	1.29
5.833	0.00	0.35	0.977	o	|	|	|	|	|	1.29
5.917	0.00	0.35	0.975	o	|	|	|	|	|	1.28
6.000	0.00	0.34	0.973	o	|	|	|	|	|	1.28
6.083	0.00	0.34	0.970	o	|	|	|	|	|	1.28
6.167	0.00	0.34	0.968	o	|	|	|	|	|	1.28
6.250	0.00	0.34	0.966	o	|	|	|	|	|	1.27
6.333	0.00	0.34	0.963	o	|	|	|	|	|	1.27
6.417	0.00	0.34	0.961	o	|	|	|	|	|	1.27
6.500	0.00	0.34	0.959	o	|	|	|	|	|	1.26
6.583	0.00	0.34	0.956	o	|	|	|	|	|	1.26
6.667	0.00	0.33	0.954	o	|	|	|	|	|	1.26
6.750	0.00	0.33	0.952	o	|	|	|	|	|	1.26
6.833	0.00	0.33	0.949	o	|	|	|	|	|	1.25
6.917	0.00	0.33	0.947	o	|	|	|	|	|	1.25
7.000	0.00	0.33	0.945	o	|	|	|	|	|	1.25
7.083	0.00	0.33	0.943	o	|	|	|	|	|	1.24
7.167	0.00	0.33	0.940	o	|	|	|	|	|	1.24
7.250	0.00	0.33	0.938	o	|	|	|	|	|	1.24
7.333	0.00	0.32	0.936	o	|	|	|	|	|	1.24
7.417	0.00	0.32	0.934	o	|	|	|	|	|	1.23
7.500	0.00	0.32	0.931	o	|	|	|	|	|	1.23
7.583	0.00	0.32	0.929	o	|	|	|	|	|	1.23
7.667	0.00	0.32	0.927	o	|	|	|	|	|	1.22
7.750	0.00	0.32	0.925	o	|	|	|	|	|	1.22
7.833	0.00	0.32	0.923	o	|	|	|	|	|	1.22
7.917	0.00	0.32	0.920	o	|	|	|	|	|	1.22
8.000	0.00	0.31	0.918	o	|	|	|	|	|	1.21
8.083	0.00	0.31	0.916	o	|	|	|	|	|	1.21
8.167	0.00	0.31	0.914	o	|	|	|	|	|	1.21
8.250	0.00	0.31	0.912	o	|	|	|	|	|	1.21
8.333	0.00	0.31	0.910	o	|	|	|	|	|	1.20
8.417	0.00	0.31	0.908	o	|	|	|	|	|	1.20
8.500	0.00	0.31	0.905	o	|	|	|	|	|	1.20
8.583	0.00	0.31	0.903	o	|	|	|	|	|	1.20
8.667	0.00	0.31	0.901	o	|	|	|	|	|	1.19
8.750	0.00	0.30	0.899	o	|	|	|	|	|	1.19
8.833	0.00	0.30	0.897	o	|	|	|	|	|	1.19
8.917	0.00	0.30	0.895	o	|	|	|	|	|	1.19

9.000	0.00	0.30	0.893	o	|	|	|	|	1.18
9.083	0.00	0.30	0.891	o	|	|	|	|	1.18
9.167	0.00	0.30	0.889	o	|	|	|	|	1.18
9.250	0.00	0.30	0.887	o	|	|	|	|	1.18
9.333	0.00	0.30	0.885	o	|	|	|	|	1.17
9.417	0.00	0.29	0.883	o	|	|	|	|	1.17
9.500	0.00	0.29	0.881	o	|	|	|	|	1.17
9.583	0.00	0.29	0.879	o	|	|	|	|	1.17
9.667	0.00	0.29	0.877	o	|	|	|	|	1.16
9.750	0.00	0.29	0.875	o	|	|	|	|	1.16
9.833	0.00	0.29	0.873	o	|	|	|	|	1.16
9.917	0.00	0.29	0.871	o	|	|	|	|	1.16
10.000	0.00	0.29	0.869	o	|	|	|	|	1.15
10.083	0.00	0.29	0.867	o	|	|	|	|	1.15
10.167	0.00	0.28	0.865	o	|	|	|	|	1.15
10.250	0.00	0.28	0.863	o	|	|	|	|	1.15
10.333	0.00	0.28	0.861	o	|	|	|	|	1.14
10.417	0.00	0.28	0.859	o	|	|	|	|	1.14
10.500	0.00	0.28	0.857	o	|	|	|	|	1.14
10.583	0.00	0.28	0.855	o	|	|	|	|	1.14
10.667	0.00	0.28	0.853	o	|	|	|	|	1.13
10.750	0.00	0.28	0.851	o	|	|	|	|	1.13
10.833	0.00	0.28	0.849	o	|	|	|	|	1.13
10.917	0.00	0.28	0.847	o	|	|	|	|	1.13
11.000	0.00	0.27	0.845	o	|	|	|	|	1.13
11.083	0.00	0.27	0.844	o	|	|	|	|	1.12
11.167	0.00	0.27	0.842	o	|	|	|	|	1.12
11.250	0.00	0.27	0.840	o	|	|	|	|	1.12
11.333	0.00	0.27	0.838	o	|	|	|	|	1.12
11.417	0.00	0.27	0.836	o	|	|	|	|	1.11
11.500	0.00	0.27	0.834	o	|	|	|	|	1.11
11.583	0.00	0.27	0.832	o	|	|	|	|	1.11
11.667	0.00	0.27	0.831	o	|	|	|	|	1.11
11.750	0.00	0.27	0.829	o	|	|	|	|	1.10
11.833	0.00	0.26	0.827	o	|	|	|	|	1.10
11.917	0.00	0.26	0.825	o	|	|	|	|	1.10
12.000	0.00	0.26	0.823	o	|	|	|	|	1.10
12.083	0.00	0.26	0.821	o	|	|	|	|	1.10
12.167	0.00	0.26	0.820	o	|	|	|	|	1.09
12.250	0.00	0.26	0.818	o	|	|	|	|	1.09
12.333	0.00	0.26	0.816	o	|	|	|	|	1.09
12.417	0.00	0.26	0.814	o	|	|	|	|	1.09
12.500	0.00	0.26	0.813	o	|	|	|	|	1.09
12.583	0.00	0.26	0.811	o	|	|	|	|	1.08
12.667	0.00	0.25	0.809	o	|	|	|	|	1.08
12.750	0.00	0.25	0.807	o	|	|	|	|	1.08
12.833	0.00	0.25	0.806	o	|	|	|	|	1.08
12.917	0.00	0.25	0.804	o	|	|	|	|	1.07
13.000	0.00	0.25	0.802	o	|	|	|	|	1.07
13.083	0.00	0.25	0.800	o	|	|	|	|	1.07
13.167	0.00	0.25	0.799	o	|	|	|	|	1.07
13.250	0.00	0.25	0.797	o	|	|	|	|	1.07
13.333	0.00	0.25	0.795	o	|	|	|	|	1.06
13.417	0.00	0.25	0.794	o	|	|	|	|	1.06
13.500	0.00	0.24	0.792	o	|	|	|	|	1.06
13.583	0.00	0.24	0.790	o	|	|	|	|	1.06
13.667	0.00	0.24	0.788	o	|	|	|	|	1.06
13.750	0.00	0.24	0.787	o	|	|	|	|	1.05
13.833	0.00	0.24	0.785	o	|	|	|	|	1.05
13.917	0.00	0.24	0.783	o	|	|	|	|	1.05
14.000	0.00	0.24	0.782	o	|	|	|	|	1.05
14.083	0.00	0.24	0.780	o	|	|	|	|	1.05
14.167	0.00	0.24	0.779	o	|	|	|	|	1.04
14.250	0.00	0.24	0.777	o	|	|	|	|	1.04
14.333	0.00	0.24	0.775	o	|	|	|	|	1.04
14.417	0.00	0.23	0.774	o	|	|	|	|	1.04
14.500	0.00	0.23	0.772	o	|	|	|	|	1.04
14.583	0.00	0.23	0.770	o	|	|	|	|	1.03
14.667	0.00	0.23	0.769	o	|	|	|	|	1.03
14.750	0.00	0.23	0.767	o	|	|	|	|	1.03
14.833	0.00	0.23	0.766	o	|	|	|	|	1.03
14.917	0.00	0.23	0.764	o	|	|	|	|	1.03
15.000	0.00	0.23	0.763	o	|	|	|	|	1.02
15.083	0.00	0.23	0.761	o	|	|	|	|	1.02
15.167	0.00	0.23	0.759	o	|	|	|	|	1.02
15.250	0.00	0.23	0.758	o	|	|	|	|	1.02
15.333	0.00	0.23	0.756	o	|	|	|	|	1.02
15.417	0.00	0.22	0.755	o	|	|	|	|	1.01
15.500	0.00	0.22	0.753	o	|	|	|	|	1.01
15.583	0.00	0.22	0.752	o	|	|	|	|	1.01
15.667	0.00	0.22	0.750	o	|	|	|	|	1.01
15.750	0.00	0.22	0.749	o	|	|	|	|	1.01
15.833	0.00	0.22	0.747	o	|	|	|	|	1.00
15.917	0.00	0.22	0.746	o	|	|	|	|	1.00
16.000	0.00	0.22	0.744	o	|	|	|	|	1.00
16.083	0.00	0.22	0.743	o	|	|	|	|	1.00

16.167	0.00	0.22	0.741	o	|	|	|	1.00
16.250	0.00	0.22	0.740	o	|	|	|	1.00
16.333	0.00	0.22	0.738	o	|	|	|	0.99
16.417	0.00	0.22	0.737	o	|	|	|	0.99
16.500	0.00	0.22	0.735	o	|	|	|	0.99
16.583	0.00	0.22	0.734	o	|	|	|	0.99
16.667	0.00	0.21	0.732	o	|	|	|	0.99
16.750	0.00	0.21	0.731	o	|	|	|	0.98
16.833	0.00	0.21	0.729	o	|	|	|	0.98
16.917	0.00	0.21	0.728	o	|	|	|	0.98
17.000	0.00	0.21	0.726	o	|	|	|	0.98
17.083	0.00	0.21	0.725	o	|	|	|	0.98
17.167	0.00	0.21	0.723	o	|	|	|	0.97
17.250	0.00	0.21	0.722	o	|	|	|	0.97
17.333	0.00	0.21	0.720	o	|	|	|	0.97
17.417	0.00	0.21	0.719	o	|	|	|	0.97
17.500	0.00	0.21	0.717	o	|	|	|	0.97
17.583	0.00	0.21	0.716	o	|	|	|	0.96
17.667	0.00	0.21	0.715	o	|	|	|	0.96
17.750	0.00	0.21	0.713	o	|	|	|	0.96
17.833	0.00	0.21	0.712	o	|	|	|	0.96
17.917	0.00	0.21	0.710	o	|	|	|	0.96
18.000	0.00	0.21	0.709	o	|	|	|	0.95
18.083	0.00	0.21	0.707	o	|	|	|	0.95
18.167	0.00	0.21	0.706	o	|	|	|	0.95
18.250	0.00	0.21	0.705	o	|	|	|	0.95
18.333	0.00	0.21	0.703	o	|	|	|	0.95
18.417	0.00	0.21	0.702	o	|	|	|	0.94
18.500	0.00	0.21	0.700	o	|	|	|	0.94
18.583	0.00	0.21	0.699	o	|	|	|	0.94
18.667	0.00	0.20	0.697	o	|	|	|	0.94
18.750	0.00	0.20	0.696	o	|	|	|	0.94
18.833	0.00	0.20	0.695	o	|	|	|	0.93
18.917	0.00	0.20	0.693	o	|	|	|	0.93
19.000	0.00	0.20	0.692	o	|	|	|	0.93
19.083	0.00	0.20	0.690	o	|	|	|	0.93
19.167	0.00	0.20	0.689	o	|	|	|	0.93
19.250	0.00	0.20	0.688	o	|	|	|	0.93
19.333	0.00	0.20	0.686	o	|	|	|	0.92
19.417	0.00	0.20	0.685	o	|	|	|	0.92
19.500	0.00	0.20	0.683	o	|	|	|	0.92
19.583	0.00	0.20	0.682	o	|	|	|	0.92
19.667	0.00	0.20	0.681	o	|	|	|	0.92
19.750	0.00	0.20	0.679	o	|	|	|	0.91
19.833	0.00	0.20	0.678	o	|	|	|	0.91
19.917	0.00	0.20	0.677	o	|	|	|	0.91
20.000	0.00	0.20	0.675	o	|	|	|	0.91
20.083	0.00	0.20	0.674	o	|	|	|	0.91
20.167	0.00	0.20	0.673	o	|	|	|	0.91
20.250	0.00	0.20	0.671	o	|	|	|	0.90
20.333	0.00	0.20	0.670	o	|	|	|	0.90
20.417	0.00	0.20	0.668	o	|	|	|	0.90
20.500	0.00	0.20	0.667	o	|	|	|	0.90
20.583	0.00	0.20	0.666	o	|	|	|	0.90
20.667	0.00	0.19	0.664	o	|	|	|	0.89
20.750	0.00	0.19	0.663	o	|	|	|	0.89
20.833	0.00	0.19	0.662	o	|	|	|	0.89
20.917	0.00	0.19	0.660	o	|	|	|	0.89
21.000	0.00	0.19	0.659	o	|	|	|	0.89
21.083	0.00	0.19	0.658	o	|	|	|	0.89
21.167	0.00	0.19	0.656	o	|	|	|	0.88
21.250	0.00	0.19	0.655	o	|	|	|	0.88
21.333	0.00	0.19	0.654	o	|	|	|	0.88
21.417	0.00	0.19	0.652	o	|	|	|	0.88
21.500	0.00	0.19	0.651	o	|	|	|	0.88
21.583	0.00	0.19	0.650	o	|	|	|	0.87
21.667	0.00	0.19	0.649	o	|	|	|	0.87
21.750	0.00	0.19	0.647	o	|	|	|	0.87
21.833	0.00	0.19	0.646	o	|	|	|	0.87
21.917	0.00	0.19	0.645	o	|	|	|	0.87
22.000	0.00	0.19	0.643	o	|	|	|	0.87
22.083	0.00	0.19	0.642	o	|	|	|	0.86
22.167	0.00	0.19	0.641	o	|	|	|	0.86
22.250	0.00	0.19	0.639	o	|	|	|	0.86
22.333	0.00	0.19	0.638	o	|	|	|	0.86
22.417	0.00	0.19	0.637	o	|	|	|	0.86
22.500	0.00	0.19	0.636	o	|	|	|	0.86
22.583	0.00	0.19	0.634	o	|	|	|	0.85
22.667	0.00	0.19	0.633	o	|	|	|	0.85
22.750	0.00	0.19	0.632	o	|	|	|	0.85
22.833	0.00	0.18	0.630	o	|	|	|	0.85
22.917	0.00	0.18	0.629	o	|	|	|	0.85
23.000	0.00	0.18	0.628	o	|	|	|	0.85
23.083	0.00	0.18	0.627	o	|	|	|	0.84
23.167	0.00	0.18	0.625	o	|	|	|	0.84
23.250	0.00	0.18	0.624	o	|	|	|	0.84

23.333	0.00	0.18	0.623	o	|	|	|	|	0.84
23.417	0.00	0.18	0.622	o	|	|	|	|	0.84
23.500	0.00	0.18	0.620	o	|	|	|	|	0.83
23.583	0.00	0.18	0.619	o	|	|	|	|	0.83
23.667	0.00	0.18	0.618	o	|	|	|	|	0.83
23.750	0.00	0.18	0.617	o	|	|	|	|	0.83
23.833	0.00	0.18	0.615	o	|	|	|	|	0.83
23.917	0.00	0.18	0.614	o	|	|	|	|	0.83
24.000	0.00	0.18	0.613	o	|	|	|	|	0.82
24.083	0.00	0.18	0.612	o	|	|	|	|	0.82
24.167	0.00	0.18	0.610	o	|	|	|	|	0.82
24.250	0.00	0.18	0.609	o	|	|	|	|	0.82
24.333	0.00	0.18	0.608	o	|	|	|	|	0.82
24.417	0.00	0.18	0.607	o	|	|	|	|	0.82
24.500	0.00	0.18	0.605	o	|	|	|	|	0.81
24.583	0.00	0.18	0.604	o	|	|	|	|	0.81
24.667	0.00	0.18	0.603	o	|	|	|	|	0.81
24.750	0.00	0.18	0.602	o	|	|	|	|	0.81
24.833	0.00	0.18	0.601	o	|	|	|	|	0.81
24.917	0.00	0.18	0.599	o	|	|	|	|	0.81
25.000	0.00	0.18	0.598	o	|	|	|	|	0.81
25.083	0.00	0.18	0.597	o	|	|	|	|	0.80
25.167	0.00	0.17	0.596	o	|	|	|	|	0.80
25.250	0.00	0.17	0.595	o	|	|	|	|	0.80
25.333	0.00	0.17	0.593	o	|	|	|	|	0.80
25.417	0.00	0.17	0.592	o	|	|	|	|	0.80
25.500	0.00	0.17	0.591	o	|	|	|	|	0.80
25.583	0.00	0.17	0.590	o	|	|	|	|	0.79
25.667	0.00	0.17	0.589	o	|	|	|	|	0.79
25.750	0.00	0.17	0.587	o	|	|	|	|	0.79
25.833	0.00	0.17	0.586	o	|	|	|	|	0.79
25.917	0.00	0.17	0.585	o	|	|	|	|	0.79
26.000	0.00	0.17	0.584	o	|	|	|	|	0.79
26.083	0.00	0.17	0.583	o	|	|	|	|	0.78
26.167	0.00	0.17	0.581	o	|	|	|	|	0.78
26.250	0.00	0.17	0.580	o	|	|	|	|	0.78
26.333	0.00	0.17	0.579	o	|	|	|	|	0.78
26.417	0.00	0.17	0.578	o	|	|	|	|	0.78
26.500	0.00	0.17	0.577	o	|	|	|	|	0.78
26.583	0.00	0.17	0.576	o	|	|	|	|	0.77
26.667	0.00	0.17	0.574	o	|	|	|	|	0.77
26.750	0.00	0.17	0.573	o	|	|	|	|	0.77
26.833	0.00	0.17	0.572	o	|	|	|	|	0.77
26.917	0.00	0.17	0.571	o	|	|	|	|	0.77
27.000	0.00	0.17	0.570	o	|	|	|	|	0.77
27.083	0.00	0.17	0.569	o	|	|	|	|	0.77
27.167	0.00	0.17	0.568	o	|	|	|	|	0.76
27.250	0.00	0.17	0.566	o	|	|	|	|	0.76
27.333	0.00	0.17	0.565	o	|	|	|	|	0.76
27.417	0.00	0.17	0.564	o	|	|	|	|	0.76
27.500	0.00	0.17	0.563	o	|	|	|	|	0.76
27.583	0.00	0.16	0.562	o	|	|	|	|	0.76
27.667	0.00	0.16	0.561	o	|	|	|	|	0.75
27.750	0.00	0.16	0.560	o	|	|	|	|	0.75
27.833	0.00	0.16	0.558	o	|	|	|	|	0.75
27.917	0.00	0.16	0.557	o	|	|	|	|	0.75
28.000	0.00	0.16	0.556	o	|	|	|	|	0.75
28.083	0.00	0.16	0.555	o	|	|	|	|	0.75
28.167	0.00	0.16	0.554	o	|	|	|	|	0.75
28.250	0.00	0.16	0.553	o	|	|	|	|	0.74
28.333	0.00	0.16	0.552	o	|	|	|	|	0.74
28.417	0.00	0.16	0.551	o	|	|	|	|	0.74
28.500	0.00	0.16	0.549	o	|	|	|	|	0.74
28.583	0.00	0.16	0.548	o	|	|	|	|	0.74
28.667	0.00	0.16	0.547	o	|	|	|	|	0.74
28.750	0.00	0.16	0.546	o	|	|	|	|	0.74
28.833	0.00	0.16	0.545	o	|	|	|	|	0.73
28.917	0.00	0.16	0.544	o	|	|	|	|	0.73
29.000	0.00	0.16	0.543	o	|	|	|	|	0.73
29.083	0.00	0.16	0.542	o	|	|	|	|	0.73
29.167	0.00	0.16	0.541	o	|	|	|	|	0.73
29.250	0.00	0.16	0.540	o	|	|	|	|	0.73
29.333	0.00	0.16	0.538	o	|	|	|	|	0.72
29.417	0.00	0.16	0.537	o	|	|	|	|	0.72
29.500	0.00	0.16	0.536	o	|	|	|	|	0.72
29.583	0.00	0.16	0.535	o	|	|	|	|	0.72
29.667	0.00	0.16	0.534	o	|	|	|	|	0.72
29.750	0.00	0.16	0.533	o	|	|	|	|	0.72
29.833	0.00	0.16	0.532	o	|	|	|	|	0.72
29.917	0.00	0.16	0.531	o	|	|	|	|	0.71
30.000	0.00	0.16	0.530	o	|	|	|	|	0.71
30.083	0.00	0.16	0.529	o	|	|	|	|	0.71
30.167	0.00	0.15	0.528	o	|	|	|	|	0.71
30.250	0.00	0.15	0.527	o	|	|	|	|	0.71
30.333	0.00	0.15	0.526	o	|	|	|	|	0.71
30.417	0.00	0.15	0.525	o	|	|	|	|	0.71

30.500	0.00	0.15	0.523	o	|	|	|	|	0.70
30.583	0.00	0.15	0.522	o	|	|	|	|	0.70
30.667	0.00	0.15	0.521	o	|	|	|	|	0.70
30.750	0.00	0.15	0.520	o	|	|	|	|	0.70
30.833	0.00	0.15	0.519	o	|	|	|	|	0.70
30.917	0.00	0.15	0.518	o	|	|	|	|	0.70
31.000	0.00	0.15	0.517	o	|	|	|	|	0.70
31.083	0.00	0.15	0.516	o	|	|	|	|	0.69
31.167	0.00	0.15	0.515	o	|	|	|	|	0.69
31.250	0.00	0.15	0.514	o	|	|	|	|	0.69
31.333	0.00	0.15	0.513	o	|	|	|	|	0.69
31.417	0.00	0.15	0.512	o	|	|	|	|	0.69
31.500	0.00	0.15	0.511	o	|	|	|	|	0.69
31.583	0.00	0.15	0.510	o	|	|	|	|	0.69
31.667	0.00	0.15	0.509	o	|	|	|	|	0.68
31.750	0.00	0.15	0.508	o	|	|	|	|	0.68
31.833	0.00	0.15	0.507	o	|	|	|	|	0.68
31.917	0.00	0.15	0.506	o	|	|	|	|	0.68
32.000	0.00	0.15	0.505	o	|	|	|	|	0.68
32.083	0.00	0.15	0.504	o	|	|	|	|	0.68
32.167	0.00	0.15	0.503	o	|	|	|	|	0.68
32.250	0.00	0.15	0.502	o	|	|	|	|	0.68
32.333	0.00	0.15	0.501	o	|	|	|	|	0.67
32.417	0.00	0.15	0.500	o	|	|	|	|	0.67
32.500	0.00	0.15	0.499	o	|	|	|	|	0.67
32.583	0.00	0.15	0.498	o	|	|	|	|	0.67
32.667	0.00	0.15	0.497	o	|	|	|	|	0.67
32.750	0.00	0.15	0.496	o	|	|	|	|	0.67
32.833	0.00	0.15	0.495	o	|	|	|	|	0.67
32.917	0.00	0.14	0.494	o	|	|	|	|	0.66
33.000	0.00	0.14	0.493	o	|	|	|	|	0.66
33.083	0.00	0.14	0.492	o	|	|	|	|	0.66
33.167	0.00	0.14	0.491	o	|	|	|	|	0.66
33.250	0.00	0.14	0.490	o	|	|	|	|	0.66
33.333	0.00	0.14	0.489	o	|	|	|	|	0.66
33.417	0.00	0.14	0.488	o	|	|	|	|	0.66
33.500	0.00	0.14	0.487	o	|	|	|	|	0.66
33.583	0.00	0.14	0.486	o	|	|	|	|	0.65
33.667	0.00	0.14	0.485	o	|	|	|	|	0.65
33.750	0.00	0.14	0.484	o	|	|	|	|	0.65
33.833	0.00	0.14	0.483	o	|	|	|	|	0.65
33.917	0.00	0.14	0.482	o	|	|	|	|	0.65
34.000	0.00	0.14	0.481	o	|	|	|	|	0.65
34.083	0.00	0.14	0.480	o	|	|	|	|	0.65
34.167	0.00	0.14	0.479	o	|	|	|	|	0.64
34.250	0.00	0.14	0.478	o	|	|	|	|	0.64
34.333	0.00	0.14	0.477	o	|	|	|	|	0.64
34.417	0.00	0.14	0.476	o	|	|	|	|	0.64
34.500	0.00	0.14	0.475	o	|	|	|	|	0.64
34.583	0.00	0.14	0.474	o	|	|	|	|	0.64
34.667	0.00	0.14	0.473	o	|	|	|	|	0.64
34.750	0.00	0.14	0.472	o	|	|	|	|	0.64
34.833	0.00	0.14	0.471	o	|	|	|	|	0.63
34.917	0.00	0.14	0.470	o	|	|	|	|	0.63
35.000	0.00	0.14	0.469	o	|	|	|	|	0.63
35.083	0.00	0.14	0.468	o	|	|	|	|	0.63
35.167	0.00	0.14	0.467	o	|	|	|	|	0.63
35.250	0.00	0.14	0.467	o	|	|	|	|	0.63
35.333	0.00	0.14	0.466	o	|	|	|	|	0.63
35.417	0.00	0.14	0.465	o	|	|	|	|	0.63
35.500	0.00	0.14	0.464	o	|	|	|	|	0.62
35.583	0.00	0.14	0.463	o	|	|	|	|	0.62
35.667	0.00	0.14	0.462	o	|	|	|	|	0.62
35.750	0.00	0.14	0.461	o	|	|	|	|	0.62
35.833	0.00	0.13	0.460	o	|	|	|	|	0.62
35.917	0.00	0.13	0.459	o	|	|	|	|	0.62
36.000	0.00	0.13	0.458	o	|	|	|	|	0.62
36.083	0.00	0.13	0.457	o	|	|	|	|	0.62
36.167	0.00	0.13	0.456	o	|	|	|	|	0.61
36.250	0.00	0.13	0.455	o	|	|	|	|	0.61
36.333	0.00	0.13	0.454	o	|	|	|	|	0.61
36.417	0.00	0.13	0.454	o	|	|	|	|	0.61
36.500	0.00	0.13	0.453	o	|	|	|	|	0.61
36.583	0.00	0.13	0.452	o	|	|	|	|	0.61
36.667	0.00	0.13	0.451	o	|	|	|	|	0.61
36.750	0.00	0.13	0.450	o	|	|	|	|	0.61
36.833	0.00	0.13	0.449	o	|	|	|	|	0.60
36.917	0.00	0.13	0.448	o	|	|	|	|	0.60
37.000	0.00	0.13	0.447	o	|	|	|	|	0.60
37.083	0.00	0.13	0.446	o	|	|	|	|	0.60
37.167	0.00	0.13	0.445	o	|	|	|	|	0.60
37.250	0.00	0.13	0.444	o	|	|	|	|	0.60
37.333	0.00	0.13	0.444	o	|	|	|	|	0.60
37.417	0.00	0.13	0.443	o	|	|	|	|	0.60
37.500	0.00	0.13	0.442	o	|	|	|	|	0.59
37.583	0.00	0.13	0.441	o	|	|	|	|	0.59

37.667	0.00	0.13	0.440	o	|	|	|	|	0.59
37.750	0.00	0.13	0.439	o	|	|	|	|	0.59
37.833	0.00	0.13	0.438	o	|	|	|	|	0.59
37.917	0.00	0.13	0.437	o	|	|	|	|	0.59
38.000	0.00	0.13	0.436	o	|	|	|	|	0.59
38.083	0.00	0.13	0.436	o	|	|	|	|	0.59
38.167	0.00	0.13	0.435	o	|	|	|	|	0.59
38.250	0.00	0.13	0.434	o	|	|	|	|	0.58
38.333	0.00	0.13	0.433	o	|	|	|	|	0.58
38.417	0.00	0.13	0.432	o	|	|	|	|	0.58
38.500	0.00	0.13	0.431	o	|	|	|	|	0.58
38.583	0.00	0.13	0.430	o	|	|	|	|	0.58
38.667	0.00	0.13	0.429	o	|	|	|	|	0.58
38.750	0.00	0.13	0.429	o	|	|	|	|	0.58
38.833	0.00	0.13	0.428	o	|	|	|	|	0.58
38.917	0.00	0.13	0.427	o	|	|	|	|	0.57
39.000	0.00	0.12	0.426	o	|	|	|	|	0.57
39.083	0.00	0.12	0.425	o	|	|	|	|	0.57
39.167	0.00	0.12	0.424	o	|	|	|	|	0.57
39.250	0.00	0.12	0.423	o	|	|	|	|	0.57
39.333	0.00	0.12	0.423	o	|	|	|	|	0.57
39.417	0.00	0.12	0.422	o	|	|	|	|	0.57
39.500	0.00	0.12	0.421	o	|	|	|	|	0.57
39.583	0.00	0.12	0.420	o	|	|	|	|	0.57
39.667	0.00	0.12	0.419	o	|	|	|	|	0.56
39.750	0.00	0.12	0.418	o	|	|	|	|	0.56
39.833	0.00	0.12	0.417	o	|	|	|	|	0.56
39.917	0.00	0.12	0.417	o	|	|	|	|	0.56
40.000	0.00	0.12	0.416	o	|	|	|	|	0.56
40.083	0.00	0.12	0.415	o	|	|	|	|	0.56
40.167	0.00	0.12	0.414	o	|	|	|	|	0.56
40.250	0.00	0.12	0.413	o	|	|	|	|	0.56
40.333	0.00	0.12	0.412	o	|	|	|	|	0.56
40.417	0.00	0.12	0.412	o	|	|	|	|	0.55
40.500	0.00	0.12	0.411	o	|	|	|	|	0.55
40.583	0.00	0.12	0.410	o	|	|	|	|	0.55
40.667	0.00	0.12	0.409	o	|	|	|	|	0.55
40.750	0.00	0.12	0.408	o	|	|	|	|	0.55
40.833	0.00	0.12	0.407	o	|	|	|	|	0.55
40.917	0.00	0.12	0.407	o	|	|	|	|	0.55
41.000	0.00	0.12	0.406	o	|	|	|	|	0.55
41.083	0.00	0.12	0.405	o	|	|	|	|	0.55
41.167	0.00	0.12	0.404	o	|	|	|	|	0.54
41.250	0.00	0.12	0.403	o	|	|	|	|	0.54
41.333	0.00	0.12	0.403	o	|	|	|	|	0.54
41.417	0.00	0.12	0.402	o	|	|	|	|	0.54
41.500	0.00	0.12	0.401	o	|	|	|	|	0.54
41.583	0.00	0.12	0.400	o	|	|	|	|	0.54
41.667	0.00	0.12	0.399	o	|	|	|	|	0.54
41.750	0.00	0.12	0.398	o	|	|	|	|	0.54
41.833	0.00	0.12	0.398	o	|	|	|	|	0.54
41.917	0.00	0.12	0.397	o	|	|	|	|	0.53
42.000	0.00	0.12	0.396	o	|	|	|	|	0.53
42.083	0.00	0.12	0.395	o	|	|	|	|	0.53
42.167	0.00	0.12	0.394	o	|	|	|	|	0.53
42.250	0.00	0.12	0.394	o	|	|	|	|	0.53
42.333	0.00	0.12	0.393	o	|	|	|	|	0.53
42.417	0.00	0.12	0.392	o	|	|	|	|	0.53
42.500	0.00	0.11	0.391	o	|	|	|	|	0.53
42.583	0.00	0.11	0.391	o	|	|	|	|	0.53
42.667	0.00	0.11	0.390	o	|	|	|	|	0.52
42.750	0.00	0.11	0.389	o	|	|	|	|	0.52
42.833	0.00	0.11	0.388	o	|	|	|	|	0.52
42.917	0.00	0.11	0.387	o	|	|	|	|	0.52
43.000	0.00	0.11	0.387	o	|	|	|	|	0.52
43.083	0.00	0.11	0.386	o	|	|	|	|	0.52
43.167	0.00	0.11	0.385	o	|	|	|	|	0.52
43.250	0.00	0.11	0.384	o	|	|	|	|	0.52
43.333	0.00	0.11	0.383	o	|	|	|	|	0.52
43.417	0.00	0.11	0.383	o	|	|	|	|	0.52
43.500	0.00	0.11	0.382	o	|	|	|	|	0.51
43.583	0.00	0.11	0.381	o	|	|	|	|	0.51
43.667	0.00	0.11	0.380	o	|	|	|	|	0.51
43.750	0.00	0.11	0.380	o	|	|	|	|	0.51
43.833	0.00	0.11	0.379	o	|	|	|	|	0.51
43.917	0.00	0.11	0.378	o	|	|	|	|	0.51
44.000	0.00	0.11	0.377	o	|	|	|	|	0.51
44.083	0.00	0.11	0.377	o	|	|	|	|	0.51
44.167	0.00	0.11	0.376	o	|	|	|	|	0.51
44.250	0.00	0.11	0.375	o	|	|	|	|	0.50
44.333	0.00	0.11	0.374	o	|	|	|	|	0.50
44.417	0.00	0.11	0.374	o	|	|	|	|	0.50
44.500	0.00	0.11	0.373	o	|	|	|	|	0.50
44.583	0.00	0.11	0.372	o	|	|	|	|	0.50
44.667	0.00	0.11	0.371	o	|	|	|	|	0.50
44.750	0.00	0.11	0.371	o	|	|	|	|	0.50

44.833	0.00	0.11	0.370	o	|	|	|	|	0.50
44.917	0.00	0.11	0.369	o	|	|	|	|	0.50
45.000	0.00	0.11	0.368	o	|	|	|	|	0.50
45.083	0.00	0.11	0.368	o	|	|	|	|	0.49
45.167	0.00	0.11	0.367	o	|	|	|	|	0.49
45.250	0.00	0.11	0.366	o	|	|	|	|	0.49
45.333	0.00	0.11	0.365	o	|	|	|	|	0.49
45.417	0.00	0.11	0.365	o	|	|	|	|	0.49
45.500	0.00	0.11	0.364	o	|	|	|	|	0.49
45.583	0.00	0.11	0.363	o	|	|	|	|	0.49
45.667	0.00	0.11	0.362	o	|	|	|	|	0.49
45.750	0.00	0.11	0.362	o	|	|	|	|	0.49
45.833	0.00	0.11	0.361	o	|	|	|	|	0.49
45.917	0.00	0.11	0.360	o	|	|	|	|	0.48
46.000	0.00	0.11	0.359	o	|	|	|	|	0.48
46.083	0.00	0.11	0.359	o	|	|	|	|	0.48
46.167	0.00	0.11	0.358	o	|	|	|	|	0.48
46.250	0.00	0.10	0.357	o	|	|	|	|	0.48
46.333	0.00	0.10	0.357	o	|	|	|	|	0.48
46.417	0.00	0.10	0.356	o	|	|	|	|	0.48
46.500	0.00	0.10	0.355	o	|	|	|	|	0.48
46.583	0.00	0.10	0.354	o	|	|	|	|	0.48
46.667	0.00	0.10	0.354	o	|	|	|	|	0.48
46.750	0.00	0.10	0.353	o	|	|	|	|	0.48
46.833	0.00	0.10	0.352	o	|	|	|	|	0.47
46.917	0.00	0.10	0.352	o	|	|	|	|	0.47
47.000	0.00	0.10	0.351	o	|	|	|	|	0.47
47.083	0.00	0.10	0.350	o	|	|	|	|	0.47
47.167	0.00	0.10	0.349	o	|	|	|	|	0.47
47.250	0.00	0.10	0.349	o	|	|	|	|	0.47
47.333	0.00	0.10	0.348	o	|	|	|	|	0.47
47.417	0.00	0.10	0.347	o	|	|	|	|	0.47
47.500	0.00	0.10	0.347	o	|	|	|	|	0.47
47.583	0.00	0.10	0.346	o	|	|	|	|	0.47
47.667	0.00	0.10	0.345	o	|	|	|	|	0.46
47.750	0.00	0.10	0.345	o	|	|	|	|	0.46
47.833	0.00	0.10	0.344	o	|	|	|	|	0.46
47.917	0.00	0.10	0.343	o	|	|	|	|	0.46
48.000	0.00	0.10	0.342	o	|	|	|	|	0.46
48.083	0.00	0.10	0.342	o	|	|	|	|	0.46
48.167	0.00	0.10	0.341	o	|	|	|	|	0.46
48.250	0.00	0.10	0.340	o	|	|	|	|	0.46

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 579
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.390 (CFS)
Total volume = 0.751 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro1262.rte
**********HYDROGRAPH DATA**********
Number of intervals = 77
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 13.584 (CFS)
Total volume = 1.409 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 77
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 3.4 6.79 10.19 13.58	Depth (Ft.)
0.083	0.29	0.00	0.001	O	0.00
0.167	0.77	0.00	0.005	OI	0.01
0.250	0.95	0.00	0.011	O I	0.01
0.333	1.02	0.01	0.017	O I	0.02
0.417	1.05	0.01	0.024	O I	0.03
0.500	1.12	0.01	0.032	O I	0.04
0.583	1.21	0.01	0.040	O I	0.05
0.667	1.23	0.01	0.048	O I	0.06
0.750	1.24	0.02	0.056	O I	0.08
0.833	1.24	0.02	0.065	O I	0.09
0.917	1.25	0.02	0.073	O I	0.10
1.000	1.30	0.02	0.082	O I	0.11
1.083	1.39	0.03	0.091	O I	0.12
1.167	1.41	0.03	0.100	O I	0.14
1.250	1.42	0.03	0.110	O I	0.15
1.333	1.42	0.04	0.119	O I	0.16
1.417	1.42	0.04	0.129	O I	0.17
1.500	1.42	0.04	0.139	O I	0.19
1.583	1.42	0.04	0.148	O I	0.20
1.667	1.42	0.05	0.158	O I	0.21
1.750	1.42	0.05	0.167	O I	0.22
1.833	1.42	0.05	0.176	O I	0.24
1.917	1.42	0.05	0.186	O I	0.25
2.000	1.48	0.06	0.196	O I	0.26
2.083	1.51	0.06	0.205	O I	0.28
2.167	1.50	0.06	0.215	O I	0.29
2.250	1.57	0.07	0.225	O I	0.30
2.333	1.59	0.07	0.236	O I	0.32
2.417	1.60	0.07	0.246	O I	0.33

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2.500    1.60    0.08      0.257  O  I    |        |        |        |     0.35
2.583    1.60    0.08      0.267  O  I    |        |        |        |     0.36
2.667    1.60    0.08      0.278  O  I    |        |        |        |     0.37
2.750    1.66    0.08      0.289  O  I    |        |        |        |     0.39
2.833    1.74    0.09      0.300  O   I   |        |        |        |     0.40
2.917    1.76    0.09      0.311  O   I   |        |        |        |     0.42
3.000    1.77    0.09      0.323  O   I   |        |        |        |     0.43
3.083    1.78    0.10      0.334  O   I   |        |        |        |     0.45
3.167    1.84    0.10      0.346  O   I   |        |        |        |     0.47
3.250    1.92    0.11      0.358  O   I   |        |        |        |     0.48
3.333    1.94    0.11      0.371  O   I   |        |        |        |     0.50
3.417    2.01    0.11      0.384  O   I   |        |        |        |     0.52
3.500    2.15    0.12      0.397  O    I  |        |        |        |     0.53
3.583    2.32    0.12      0.412  O    I  |        |        |        |     0.55
3.667    2.43    0.13      0.427  O    I  |        |        |        |     0.58
3.750    2.52    0.13      0.443  O    I  |        |        |        |     0.60
3.833    2.62    0.14      0.460  O     I |        |        |        |     0.62
3.917    2.71    0.14      0.478  O     I |        |        |        |     0.64
4.000    2.80    0.15      0.496  O     I |        |        |        |     0.67
4.083    2.89    0.15      0.514  O     I |        |        |        |     0.69
4.167    3.04    0.16      0.534  O      I|        |        |        |     0.72
4.250    3.21    0.16      0.554  O      I|        |        |        |     0.75
4.333    3.38    0.17      0.575  O      I|        |        |        |     0.77
4.417    3.58    0.18      0.598  O       I        |        |        |     0.81
4.500    3.74    0.18      0.622  O       I        |        |        |     0.84
4.583    3.90    0.19      0.647  O       |I       |        |        |     0.87
4.667    4.21    0.20      0.674  O       |I       |        |        |     0.91
4.750    4.54    0.21      0.703  O       | I      |        |        |     0.95
4.833    4.77    0.22      0.733  O       |  I     |        |        |     0.99
4.917    4.95    0.23      0.765  O       |  I     |        |        |     1.03
5.000    5.27    0.25      0.799  O       |   I    |        |        |     1.07
5.083    6.07    0.27      0.836  O       |     I  |        |        |     1.11
5.167    7.55    0.29      0.881  O       |        |I       |        |     1.17
5.250    8.96    0.32      0.936  O       |        |    I   |        |     1.24
5.333   10.12    0.36      0.999  O       |        |      I |        |     1.31
5.417   11.46    0.40      1.071  O       |        |        |  I     |     1.40
5.500   13.58    0.44      1.154  |O      |        |        |      I |     1.50
5.583   11.23    0.49      1.236  |O      |        |        |  I     |     1.60
5.667    5.05    0.52      1.289  |O      |  I     |        |        |     1.67
5.750    2.80    0.53      1.312  |O   I  |        |        |        |     1.70
5.833    1.75    0.54      1.324  |O  I   |        |        |        |     1.71
5.917    1.12    0.54      1.330  |OI     |        |        |        |     1.72
6.000    0.61    0.54      1.333  |O      |        |        |        |     1.72
6.083    0.32    0.54      1.332  IO      |        |        |        |     1.72
6.167    0.11    0.54      1.330  IO      |        |        |        |     1.72
6.250    0.04    0.54      1.327  IO      |        |        |        |     1.71
6.333    0.02    0.54      1.323  IO      |        |        |        |     1.71
6.417    0.01    0.54      1.319  IO      |        |        |        |     1.70
6.500    0.00    0.53      1.316  IO      |        |        |        |     1.70
6.583    0.00    0.53      1.312  IO      |        |        |        |     1.70
6.667    0.00    0.53      1.308  IO      |        |        |        |     1.69
6.750    0.00    0.53      1.305  IO      |        |        |        |     1.69
6.833    0.00    0.53      1.301  IO      |        |        |        |     1.68
6.917    0.00    0.52      1.298  IO      |        |        |        |     1.68
7.000    0.00    0.52      1.294  IO      |        |        |        |     1.67
7.083    0.00    0.52      1.290  IO      |        |        |        |     1.67
7.167    0.00    0.52      1.287  IO      |        |        |        |     1.66
7.250    0.00    0.52      1.283  IO      |        |        |        |     1.66
7.333    0.00    0.51      1.280  IO      |        |        |        |     1.66
7.417    0.00    0.51      1.276  IO      |        |        |        |     1.65
7.500    0.00    0.51      1.273  IO      |        |        |        |     1.65
7.583    0.00    0.51      1.269  IO      |        |        |        |     1.64
7.667    0.00    0.51      1.266  IO      |        |        |        |     1.64
7.750    0.00    0.50      1.262  IO      |        |        |        |     1.63
7.833    0.00    0.50      1.259  IO      |        |        |        |     1.63
7.917    0.00    0.50      1.255  IO      |        |        |        |     1.63
8.000    0.00    0.50      1.252  IO      |        |        |        |     1.62
8.083    0.00    0.50      1.248  IO      |        |        |        |     1.62
8.167    0.00    0.49      1.245  IO      |        |        |        |     1.61
8.250    0.00    0.49      1.242  IO      |        |        |        |     1.61
8.333    0.00    0.49      1.238  IO      |        |        |        |     1.61
8.417    0.00    0.49      1.235  IO      |        |        |        |     1.60
8.500    0.00    0.49      1.232  IO      |        |        |        |     1.60
8.583    0.00    0.48      1.228  IO      |        |        |        |     1.59
8.667    0.00    0.48      1.225  IO      |        |        |        |     1.59
8.750    0.00    0.48      1.222  IO      |        |        |        |     1.59
8.833    0.00    0.48      1.218  IO      |        |        |        |     1.58
8.917    0.00    0.48      1.215  IO      |        |        |        |     1.58
9.000    0.00    0.48      1.212  IO      |        |        |        |     1.57
9.083    0.00    0.47      1.208  IO      |        |        |        |     1.57
9.167    0.00    0.47      1.205  IO      |        |        |        |     1.56
9.250    0.00    0.47      1.202  IO      |        |        |        |     1.56
9.333    0.00    0.47      1.199  IO      |        |        |        |     1.56
9.417    0.00    0.47      1.195  IO      |        |        |        |     1.55
9.500    0.00    0.47      1.192  IO      |        |        |        |     1.55
9.583    0.00    0.46      1.189  IO      |        |        |        |     1.55
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9.667	0.00	0.46	1.186	IO				1.54
9.750	0.00	0.46	1.183	IO				1.54
9.833	0.00	0.46	1.180	IO				1.53
9.917	0.00	0.46	1.176	IO				1.53
10.000	0.00	0.45	1.173	IO				1.53
10.083	0.00	0.45	1.170	IO				1.52
10.167	0.00	0.45	1.167	IO				1.52
10.250	0.00	0.45	1.164	IO				1.51
10.333	0.00	0.45	1.161	IO				1.51
10.417	0.00	0.45	1.158	IO				1.51
10.500	0.00	0.44	1.155	IO				1.50
10.583	0.00	0.44	1.152	IO				1.50
10.667	0.00	0.44	1.149	IO				1.50
10.750	0.00	0.44	1.146	IO				1.49
10.833	0.00	0.44	1.143	IO				1.49
10.917	0.00	0.44	1.140	IO				1.48
11.000	0.00	0.43	1.137	IO				1.48
11.083	0.00	0.43	1.134	IO				1.48
11.167	0.00	0.43	1.131	IO				1.47
11.250	0.00	0.43	1.128	IO				1.47
11.333	0.00	0.43	1.125	IO				1.47
11.417	0.00	0.43	1.122	IO				1.46
11.500	0.00	0.42	1.119	IO				1.46
11.583	0.00	0.42	1.116	O				1.46
11.667	0.00	0.42	1.113	O				1.45
11.750	0.00	0.42	1.110	O				1.45
11.833	0.00	0.42	1.107	O				1.45
11.917	0.00	0.42	1.104	O				1.44
12.000	0.00	0.42	1.101	O				1.44
12.083	0.00	0.41	1.099	O				1.43
12.167	0.00	0.41	1.096	O				1.43
12.250	0.00	0.41	1.093	O				1.43
12.333	0.00	0.41	1.090	O				1.42
12.417	0.00	0.41	1.087	O				1.42
12.500	0.00	0.41	1.084	O				1.42
12.583	0.00	0.40	1.082	O				1.41
12.667	0.00	0.40	1.079	O				1.41
12.750	0.00	0.40	1.076	O				1.41
12.833	0.00	0.40	1.073	O				1.40
12.917	0.00	0.40	1.071	O				1.40
13.000	0.00	0.40	1.068	O				1.40
13.083	0.00	0.40	1.065	O				1.39
13.167	0.00	0.39	1.062	O				1.39
13.250	0.00	0.39	1.060	O				1.39
13.333	0.00	0.39	1.057	O				1.38
13.417	0.00	0.39	1.054	O				1.38
13.500	0.00	0.39	1.052	O				1.38
13.583	0.00	0.39	1.049	O				1.37
13.667	0.00	0.38	1.046	O				1.37
13.750	0.00	0.38	1.044	O				1.37
13.833	0.00	0.38	1.041	O				1.36
13.917	0.00	0.38	1.038	O				1.36
14.000	0.00	0.38	1.036	O				1.36
14.083	0.00	0.38	1.033	O				1.35
14.167	0.00	0.38	1.031	O				1.35
14.250	0.00	0.37	1.028	O				1.35
14.333	0.00	0.37	1.025	O				1.35
14.417	0.00	0.37	1.023	O				1.34
14.500	0.00	0.37	1.020	O				1.34
14.583	0.00	0.37	1.018	O				1.34
14.667	0.00	0.37	1.015	O				1.33
14.750	0.00	0.37	1.013	O				1.33
14.833	0.00	0.36	1.010	O				1.33
14.917	0.00	0.36	1.008	O				1.32
15.000	0.00	0.36	1.005	O				1.32
15.083	0.00	0.36	1.003	O				1.32
15.167	0.00	0.36	1.000	O				1.31
15.250	0.00	0.36	0.998	O				1.31
15.333	0.00	0.36	0.995	O				1.31
15.417	0.00	0.36	0.993	O				1.31
15.500	0.00	0.35	0.990	O				1.30
15.583	0.00	0.35	0.988	O				1.30
15.667	0.00	0.35	0.986	O				1.30
15.750	0.00	0.35	0.983	O				1.29
15.833	0.00	0.35	0.981	O				1.29
15.917	0.00	0.35	0.978	O				1.29
16.000	0.00	0.35	0.976	O				1.28
16.083	0.00	0.34	0.974	O				1.28
16.167	0.00	0.34	0.971	O				1.28
16.250	0.00	0.34	0.969	O				1.28
16.333	0.00	0.34	0.966	O				1.27
16.417	0.00	0.34	0.964	O				1.27
16.500	0.00	0.34	0.962	O				1.27
16.583	0.00	0.34	0.959	O				1.26
16.667	0.00	0.34	0.957	O				1.26
16.750	0.00	0.33	0.955	O				1.26

16.833	0.00	0.33	0.953	o	|	|	|	|	1.26
16.917	0.00	0.33	0.950	o	|	|	|	|	1.25
17.000	0.00	0.33	0.948	o	|	|	|	|	1.25
17.083	0.00	0.33	0.946	o	|	|	|	|	1.25
17.167	0.00	0.33	0.943	o	|	|	|	|	1.24
17.250	0.00	0.33	0.941	o	|	|	|	|	1.24
17.333	0.00	0.33	0.939	o	|	|	|	|	1.24
17.417	0.00	0.32	0.937	o	|	|	|	|	1.24
17.500	0.00	0.32	0.934	o	|	|	|	|	1.23
17.583	0.00	0.32	0.932	o	|	|	|	|	1.23
17.667	0.00	0.32	0.930	o	|	|	|	|	1.23
17.750	0.00	0.32	0.928	o	|	|	|	|	1.23
17.833	0.00	0.32	0.926	o	|	|	|	|	1.22
17.917	0.00	0.32	0.923	o	|	|	|	|	1.22
18.000	0.00	0.32	0.921	o	|	|	|	|	1.22
18.083	0.00	0.31	0.919	o	|	|	|	|	1.22
18.167	0.00	0.31	0.917	o	|	|	|	|	1.21
18.250	0.00	0.31	0.915	o	|	|	|	|	1.21
18.333	0.00	0.31	0.913	o	|	|	|	|	1.21
18.417	0.00	0.31	0.910	o	|	|	|	|	1.20
18.500	0.00	0.31	0.908	o	|	|	|	|	1.20
18.583	0.00	0.31	0.906	o	|	|	|	|	1.20
18.667	0.00	0.31	0.904	o	|	|	|	|	1.20
18.750	0.00	0.31	0.902	o	|	|	|	|	1.19
18.833	0.00	0.30	0.900	o	|	|	|	|	1.19
18.917	0.00	0.30	0.898	o	|	|	|	|	1.19
19.000	0.00	0.30	0.896	o	|	|	|	|	1.19
19.083	0.00	0.30	0.894	o	|	|	|	|	1.18
19.167	0.00	0.30	0.892	o	|	|	|	|	1.18
19.250	0.00	0.30	0.889	o	|	|	|	|	1.18
19.333	0.00	0.30	0.887	o	|	|	|	|	1.18
19.417	0.00	0.30	0.885	o	|	|	|	|	1.17
19.500	0.00	0.30	0.883	o	|	|	|	|	1.17
19.583	0.00	0.29	0.881	o	|	|	|	|	1.17
19.667	0.00	0.29	0.879	o	|	|	|	|	1.17
19.750	0.00	0.29	0.877	o	|	|	|	|	1.16
19.833	0.00	0.29	0.875	o	|	|	|	|	1.16
19.917	0.00	0.29	0.873	o	|	|	|	|	1.16
20.000	0.00	0.29	0.871	o	|	|	|	|	1.16
20.083	0.00	0.29	0.869	o	|	|	|	|	1.15
20.167	0.00	0.29	0.867	o	|	|	|	|	1.15
20.250	0.00	0.29	0.865	o	|	|	|	|	1.15
20.333	0.00	0.28	0.863	o	|	|	|	|	1.15
20.417	0.00	0.28	0.861	o	|	|	|	|	1.14
20.500	0.00	0.28	0.860	o	|	|	|	|	1.14
20.583	0.00	0.28	0.858	o	|	|	|	|	1.14
20.667	0.00	0.28	0.856	o	|	|	|	|	1.14
20.750	0.00	0.28	0.854	o	|	|	|	|	1.14
20.833	0.00	0.28	0.852	o	|	|	|	|	1.13
20.917	0.00	0.28	0.850	o	|	|	|	|	1.13
21.000	0.00	0.28	0.848	o	|	|	|	|	1.13
21.083	0.00	0.27	0.846	o	|	|	|	|	1.13
21.167	0.00	0.27	0.844	o	|	|	|	|	1.12
21.250	0.00	0.27	0.842	o	|	|	|	|	1.12
21.333	0.00	0.27	0.840	o	|	|	|	|	1.12
21.417	0.00	0.27	0.839	o	|	|	|	|	1.12
21.500	0.00	0.27	0.837	o	|	|	|	|	1.11
21.583	0.00	0.27	0.835	o	|	|	|	|	1.11
21.667	0.00	0.27	0.833	o	|	|	|	|	1.11
21.750	0.00	0.27	0.831	o	|	|	|	|	1.11
21.833	0.00	0.27	0.829	o	|	|	|	|	1.11
21.917	0.00	0.26	0.828	o	|	|	|	|	1.10
22.000	0.00	0.26	0.826	o	|	|	|	|	1.10
22.083	0.00	0.26	0.824	o	|	|	|	|	1.10
22.167	0.00	0.26	0.822	o	|	|	|	|	1.10
22.250	0.00	0.26	0.820	o	|	|	|	|	1.09
22.333	0.00	0.26	0.818	o	|	|	|	|	1.09
22.417	0.00	0.26	0.817	o	|	|	|	|	1.09
22.500	0.00	0.26	0.815	o	|	|	|	|	1.09
22.583	0.00	0.26	0.813	o	|	|	|	|	1.09
22.667	0.00	0.26	0.811	o	|	|	|	|	1.08
22.750	0.00	0.25	0.810	o	|	|	|	|	1.08
22.833	0.00	0.25	0.808	o	|	|	|	|	1.08
22.917	0.00	0.25	0.806	o	|	|	|	|	1.08
23.000	0.00	0.25	0.804	o	|	|	|	|	1.08
23.083	0.00	0.25	0.803	o	|	|	|	|	1.07
23.167	0.00	0.25	0.801	o	|	|	|	|	1.07
23.250	0.00	0.25	0.799	o	|	|	|	|	1.07
23.333	0.00	0.25	0.798	o	|	|	|	|	1.07
23.417	0.00	0.25	0.796	o	|	|	|	|	1.06
23.500	0.00	0.25	0.794	o	|	|	|	|	1.06
23.583	0.00	0.25	0.792	o	|	|	|	|	1.06
23.667	0.00	0.24	0.791	o	|	|	|	|	1.06
23.750	0.00	0.24	0.789	o	|	|	|	|	1.06
23.833	0.00	0.24	0.787	o	|	|	|	|	1.05
23.917	0.00	0.24	0.786	o	|	|	|	|	1.05

24.000	0.00	0.24	0.784	o	|	|	|	|	1.05
24.083	0.00	0.24	0.782	o	|	|	|	|	1.05
24.167	0.00	0.24	0.781	o	|	|	|	|	1.05
24.250	0.00	0.24	0.779	o	|	|	|	|	1.04
24.333	0.00	0.24	0.777	o	|	|	|	|	1.04
24.417	0.00	0.24	0.776	o	|	|	|	|	1.04
24.500	0.00	0.24	0.774	o	|	|	|	|	1.04
24.583	0.00	0.23	0.773	o	|	|	|	|	1.04
24.667	0.00	0.23	0.771	o	|	|	|	|	1.03
24.750	0.00	0.23	0.769	o	|	|	|	|	1.03
24.833	0.00	0.23	0.768	o	|	|	|	|	1.03
24.917	0.00	0.23	0.766	o	|	|	|	|	1.03
25.000	0.00	0.23	0.765	o	|	|	|	|	1.03
25.083	0.00	0.23	0.763	o	|	|	|	|	1.02
25.167	0.00	0.23	0.761	o	|	|	|	|	1.02
25.250	0.00	0.23	0.760	o	|	|	|	|	1.02
25.333	0.00	0.23	0.758	o	|	|	|	|	1.02
25.417	0.00	0.23	0.757	o	|	|	|	|	1.02
25.500	0.00	0.22	0.755	o	|	|	|	|	1.01
25.583	0.00	0.22	0.754	o	|	|	|	|	1.01
25.667	0.00	0.22	0.752	o	|	|	|	|	1.01
25.750	0.00	0.22	0.751	o	|	|	|	|	1.01
25.833	0.00	0.22	0.749	o	|	|	|	|	1.01
25.917	0.00	0.22	0.748	o	|	|	|	|	1.01
26.000	0.00	0.22	0.746	o	|	|	|	|	1.00
26.083	0.00	0.22	0.745	o	|	|	|	|	1.00
26.167	0.00	0.22	0.743	o	|	|	|	|	1.00
26.250	0.00	0.22	0.742	o	|	|	|	|	1.00
26.333	0.00	0.22	0.740	o	|	|	|	|	1.00
26.417	0.00	0.22	0.739	o	|	|	|	|	0.99
26.500	0.00	0.22	0.737	o	|	|	|	|	0.99
26.583	0.00	0.22	0.736	o	|	|	|	|	0.99
26.667	0.00	0.22	0.734	o	|	|	|	|	0.99
26.750	0.00	0.21	0.733	o	|	|	|	|	0.99
26.833	0.00	0.21	0.731	o	|	|	|	|	0.98
26.917	0.00	0.21	0.730	o	|	|	|	|	0.98
27.000	0.00	0.21	0.728	o	|	|	|	|	0.98
27.083	0.00	0.21	0.727	o	|	|	|	|	0.98
27.167	0.00	0.21	0.725	o	|	|	|	|	0.98
27.250	0.00	0.21	0.724	o	|	|	|	|	0.97
27.333	0.00	0.21	0.722	o	|	|	|	|	0.97
27.417	0.00	0.21	0.721	o	|	|	|	|	0.97
27.500	0.00	0.21	0.719	o	|	|	|	|	0.97
27.583	0.00	0.21	0.718	o	|	|	|	|	0.97
27.667	0.00	0.21	0.716	o	|	|	|	|	0.96
27.750	0.00	0.21	0.715	o	|	|	|	|	0.96
27.833	0.00	0.21	0.714	o	|	|	|	|	0.96
27.917	0.00	0.21	0.712	o	|	|	|	|	0.96
28.000	0.00	0.21	0.711	o	|	|	|	|	0.96
28.083	0.00	0.21	0.709	o	|	|	|	|	0.95
28.167	0.00	0.21	0.708	o	|	|	|	|	0.95
28.250	0.00	0.21	0.706	o	|	|	|	|	0.95
28.333	0.00	0.21	0.705	o	|	|	|	|	0.95
28.417	0.00	0.21	0.704	o	|	|	|	|	0.95
28.500	0.00	0.21	0.702	o	|	|	|	|	0.95
28.583	0.00	0.21	0.701	o	|	|	|	|	0.94
28.667	0.00	0.21	0.699	o	|	|	|	|	0.94
28.750	0.00	0.20	0.698	o	|	|	|	|	0.94
28.833	0.00	0.20	0.697	o	|	|	|	|	0.94
28.917	0.00	0.20	0.695	o	|	|	|	|	0.94
29.000	0.00	0.20	0.694	o	|	|	|	|	0.93
29.083	0.00	0.20	0.692	o	|	|	|	|	0.93
29.167	0.00	0.20	0.691	o	|	|	|	|	0.93
29.250	0.00	0.20	0.690	o	|	|	|	|	0.93
29.333	0.00	0.20	0.688	o	|	|	|	|	0.93
29.417	0.00	0.20	0.687	o	|	|	|	|	0.92
29.500	0.00	0.20	0.685	o	|	|	|	|	0.92
29.583	0.00	0.20	0.684	o	|	|	|	|	0.92
29.667	0.00	0.20	0.683	o	|	|	|	|	0.92
29.750	0.00	0.20	0.681	o	|	|	|	|	0.92
29.833	0.00	0.20	0.680	o	|	|	|	|	0.91
29.917	0.00	0.20	0.678	o	|	|	|	|	0.91
30.000	0.00	0.20	0.677	o	|	|	|	|	0.91
30.083	0.00	0.20	0.676	o	|	|	|	|	0.91
30.167	0.00	0.20	0.674	o	|	|	|	|	0.91
30.250	0.00	0.20	0.673	o	|	|	|	|	0.91
30.333	0.00	0.20	0.672	o	|	|	|	|	0.90
30.417	0.00	0.20	0.670	o	|	|	|	|	0.90
30.500	0.00	0.20	0.669	o	|	|	|	|	0.90
30.583	0.00	0.20	0.668	o	|	|	|	|	0.90
30.667	0.00	0.20	0.666	o	|	|	|	|	0.90
30.750	0.00	0.20	0.665	o	|	|	|	|	0.89
30.833	0.00	0.19	0.664	o	|	|	|	|	0.89
30.917	0.00	0.19	0.662	o	|	|	|	|	0.89
31.000	0.00	0.19	0.661	o	|	|	|	|	0.89
31.083	0.00	0.19	0.660	o	|	|	|	|	0.89

31.167	0.00	0.19	0.658	o	|	|	|	|	0.89
31.250	0.00	0.19	0.657	o	|	|	|	|	0.88
31.333	0.00	0.19	0.656	o	|	|	|	|	0.88
31.417	0.00	0.19	0.654	o	|	|	|	|	0.88
31.500	0.00	0.19	0.653	o	|	|	|	|	0.88
31.583	0.00	0.19	0.652	o	|	|	|	|	0.88
31.667	0.00	0.19	0.650	o	|	|	|	|	0.88
31.750	0.00	0.19	0.649	o	|	|	|	|	0.87
31.833	0.00	0.19	0.648	o	|	|	|	|	0.87
31.917	0.00	0.19	0.646	o	|	|	|	|	0.87
32.000	0.00	0.19	0.645	o	|	|	|	|	0.87
32.083	0.00	0.19	0.644	o	|	|	|	|	0.87
32.167	0.00	0.19	0.642	o	|	|	|	|	0.86
32.250	0.00	0.19	0.641	o	|	|	|	|	0.86
32.333	0.00	0.19	0.640	o	|	|	|	|	0.86
32.417	0.00	0.19	0.639	o	|	|	|	|	0.86
32.500	0.00	0.19	0.637	o	|	|	|	|	0.86
32.583	0.00	0.19	0.636	o	|	|	|	|	0.86
32.667	0.00	0.19	0.635	o	|	|	|	|	0.85
32.750	0.00	0.19	0.633	o	|	|	|	|	0.85
32.833	0.00	0.19	0.632	o	|	|	|	|	0.85
32.917	0.00	0.19	0.631	o	|	|	|	|	0.85
33.000	0.00	0.18	0.630	o	|	|	|	|	0.85
33.083	0.00	0.18	0.628	o	|	|	|	|	0.85
33.167	0.00	0.18	0.627	o	|	|	|	|	0.84
33.250	0.00	0.18	0.626	o	|	|	|	|	0.84
33.333	0.00	0.18	0.625	o	|	|	|	|	0.84
33.417	0.00	0.18	0.623	o	|	|	|	|	0.84
33.500	0.00	0.18	0.622	o	|	|	|	|	0.84
33.583	0.00	0.18	0.621	o	|	|	|	|	0.84
33.667	0.00	0.18	0.619	o	|	|	|	|	0.83
33.750	0.00	0.18	0.618	o	|	|	|	|	0.83
33.833	0.00	0.18	0.617	o	|	|	|	|	0.83
33.917	0.00	0.18	0.616	o	|	|	|	|	0.83
34.000	0.00	0.18	0.614	o	|	|	|	|	0.83
34.083	0.00	0.18	0.613	o	|	|	|	|	0.83
34.167	0.00	0.18	0.612	o	|	|	|	|	0.82
34.250	0.00	0.18	0.611	o	|	|	|	|	0.82
34.333	0.00	0.18	0.610	o	|	|	|	|	0.82
34.417	0.00	0.18	0.608	o	|	|	|	|	0.82
34.500	0.00	0.18	0.607	o	|	|	|	|	0.82
34.583	0.00	0.18	0.606	o	|	|	|	|	0.82
34.667	0.00	0.18	0.605	o	|	|	|	|	0.81
34.750	0.00	0.18	0.603	o	|	|	|	|	0.81
34.833	0.00	0.18	0.602	o	|	|	|	|	0.81
34.917	0.00	0.18	0.601	o	|	|	|	|	0.81
35.000	0.00	0.18	0.600	o	|	|	|	|	0.81
35.083	0.00	0.18	0.599	o	|	|	|	|	0.81
35.167	0.00	0.18	0.597	o	|	|	|	|	0.80
35.250	0.00	0.17	0.596	o	|	|	|	|	0.80
35.333	0.00	0.17	0.595	o	|	|	|	|	0.80
35.417	0.00	0.17	0.594	o	|	|	|	|	0.80
35.500	0.00	0.17	0.593	o	|	|	|	|	0.80
35.583	0.00	0.17	0.591	o	|	|	|	|	0.80
35.667	0.00	0.17	0.590	o	|	|	|	|	0.79
35.750	0.00	0.17	0.589	o	|	|	|	|	0.79
35.833	0.00	0.17	0.588	o	|	|	|	|	0.79
35.917	0.00	0.17	0.587	o	|	|	|	|	0.79
36.000	0.00	0.17	0.585	o	|	|	|	|	0.79
36.083	0.00	0.17	0.584	o	|	|	|	|	0.79
36.167	0.00	0.17	0.583	o	|	|	|	|	0.78
36.250	0.00	0.17	0.582	o	|	|	|	|	0.78
36.333	0.00	0.17	0.581	o	|	|	|	|	0.78
36.417	0.00	0.17	0.580	o	|	|	|	|	0.78
36.500	0.00	0.17	0.578	o	|	|	|	|	0.78
36.583	0.00	0.17	0.577	o	|	|	|	|	0.78
36.667	0.00	0.17	0.576	o	|	|	|	|	0.78
36.750	0.00	0.17	0.575	o	|	|	|	|	0.77
36.833	0.00	0.17	0.574	o	|	|	|	|	0.77
36.917	0.00	0.17	0.573	o	|	|	|	|	0.77
37.000	0.00	0.17	0.571	o	|	|	|	|	0.77
37.083	0.00	0.17	0.570	o	|	|	|	|	0.77
37.167	0.00	0.17	0.569	o	|	|	|	|	0.77
37.250	0.00	0.17	0.568	o	|	|	|	|	0.76
37.333	0.00	0.17	0.567	o	|	|	|	|	0.76
37.417	0.00	0.17	0.566	o	|	|	|	|	0.76
37.500	0.00	0.17	0.564	o	|	|	|	|	0.76
37.583	0.00	0.17	0.563	o	|	|	|	|	0.76
37.667	0.00	0.16	0.562	o	|	|	|	|	0.76
37.750	0.00	0.16	0.561	o	|	|	|	|	0.76
37.833	0.00	0.16	0.560	o	|	|	|	|	0.75
37.917	0.00	0.16	0.559	o	|	|	|	|	0.75
38.000	0.00	0.16	0.558	o	|	|	|	|	0.75
38.083	0.00	0.16	0.557	o	|	|	|	|	0.75
38.167	0.00	0.16	0.555	o	|	|	|	|	0.75
38.250	0.00	0.16	0.554	o	|	|	|	|	0.75

38.333	0.00	0.16	0.553	o	|	|	|	|	0.74
38.417	0.00	0.16	0.552	o	|	|	|	|	0.74
38.500	0.00	0.16	0.551	o	|	|	|	|	0.74
38.583	0.00	0.16	0.550	o	|	|	|	|	0.74
38.667	0.00	0.16	0.549	o	|	|	|	|	0.74
38.750	0.00	0.16	0.548	o	|	|	|	|	0.74
38.833	0.00	0.16	0.547	o	|	|	|	|	0.74
38.917	0.00	0.16	0.545	o	|	|	|	|	0.73
39.000	0.00	0.16	0.544	o	|	|	|	|	0.73
39.083	0.00	0.16	0.543	o	|	|	|	|	0.73
39.167	0.00	0.16	0.542	o	|	|	|	|	0.73
39.250	0.00	0.16	0.541	o	|	|	|	|	0.73
39.333	0.00	0.16	0.540	o	|	|	|	|	0.73
39.417	0.00	0.16	0.539	o	|	|	|	|	0.73
39.500	0.00	0.16	0.538	o	|	|	|	|	0.72
39.583	0.00	0.16	0.537	o	|	|	|	|	0.72
39.667	0.00	0.16	0.536	o	|	|	|	|	0.72
39.750	0.00	0.16	0.535	o	|	|	|	|	0.72
39.833	0.00	0.16	0.533	o	|	|	|	|	0.72
39.917	0.00	0.16	0.532	o	|	|	|	|	0.72
40.000	0.00	0.16	0.531	o	|	|	|	|	0.72
40.083	0.00	0.16	0.530	o	|	|	|	|	0.71
40.167	0.00	0.16	0.529	o	|	|	|	|	0.71
40.250	0.00	0.15	0.528	o	|	|	|	|	0.71
40.333	0.00	0.15	0.527	o	|	|	|	|	0.71
40.417	0.00	0.15	0.526	o	|	|	|	|	0.71
40.500	0.00	0.15	0.525	o	|	|	|	|	0.71
40.583	0.00	0.15	0.524	o	|	|	|	|	0.71
40.667	0.00	0.15	0.523	o	|	|	|	|	0.70
40.750	0.00	0.15	0.522	o	|	|	|	|	0.70
40.833	0.00	0.15	0.521	o	|	|	|	|	0.70
40.917	0.00	0.15	0.520	o	|	|	|	|	0.70
41.000	0.00	0.15	0.519	o	|	|	|	|	0.70
41.083	0.00	0.15	0.518	o	|	|	|	|	0.70
41.167	0.00	0.15	0.516	o	|	|	|	|	0.70
41.250	0.00	0.15	0.515	o	|	|	|	|	0.69
41.333	0.00	0.15	0.514	o	|	|	|	|	0.69
41.417	0.00	0.15	0.513	o	|	|	|	|	0.69
41.500	0.00	0.15	0.512	o	|	|	|	|	0.69
41.583	0.00	0.15	0.511	o	|	|	|	|	0.69
41.667	0.00	0.15	0.510	o	|	|	|	|	0.69
41.750	0.00	0.15	0.509	o	|	|	|	|	0.69
41.833	0.00	0.15	0.508	o	|	|	|	|	0.68
41.917	0.00	0.15	0.507	o	|	|	|	|	0.68
42.000	0.00	0.15	0.506	o	|	|	|	|	0.68
42.083	0.00	0.15	0.505	o	|	|	|	|	0.68
42.167	0.00	0.15	0.504	o	|	|	|	|	0.68
42.250	0.00	0.15	0.503	o	|	|	|	|	0.68
42.333	0.00	0.15	0.502	o	|	|	|	|	0.68
42.417	0.00	0.15	0.501	o	|	|	|	|	0.67
42.500	0.00	0.15	0.500	o	|	|	|	|	0.67
42.583	0.00	0.15	0.499	o	|	|	|	|	0.67
42.667	0.00	0.15	0.498	o	|	|	|	|	0.67
42.750	0.00	0.15	0.497	o	|	|	|	|	0.67
42.833	0.00	0.15	0.496	o	|	|	|	|	0.67
42.917	0.00	0.15	0.495	o	|	|	|	|	0.67
43.000	0.00	0.14	0.494	o	|	|	|	|	0.66
43.083	0.00	0.14	0.493	o	|	|	|	|	0.66
43.167	0.00	0.14	0.492	o	|	|	|	|	0.66
43.250	0.00	0.14	0.491	o	|	|	|	|	0.66
43.333	0.00	0.14	0.490	o	|	|	|	|	0.66
43.417	0.00	0.14	0.489	o	|	|	|	|	0.66
43.500	0.00	0.14	0.488	o	|	|	|	|	0.66
43.583	0.00	0.14	0.487	o	|	|	|	|	0.66
43.667	0.00	0.14	0.486	o	|	|	|	|	0.65
43.750	0.00	0.14	0.485	o	|	|	|	|	0.65
43.833	0.00	0.14	0.484	o	|	|	|	|	0.65
43.917	0.00	0.14	0.483	o	|	|	|	|	0.65
44.000	0.00	0.14	0.482	o	|	|	|	|	0.65
44.083	0.00	0.14	0.481	o	|	|	|	|	0.65
44.167	0.00	0.14	0.480	o	|	|	|	|	0.65
44.250	0.00	0.14	0.479	o	|	|	|	|	0.65
44.333	0.00	0.14	0.478	o	|	|	|	|	0.64
44.417	0.00	0.14	0.477	o	|	|	|	|	0.64
44.500	0.00	0.14	0.476	o	|	|	|	|	0.64
44.583	0.00	0.14	0.475	o	|	|	|	|	0.64
44.667	0.00	0.14	0.474	o	|	|	|	|	0.64
44.750	0.00	0.14	0.473	o	|	|	|	|	0.64
44.833	0.00	0.14	0.473	o	|	|	|	|	0.64
44.917	0.00	0.14	0.472	o	|	|	|	|	0.63
45.000	0.00	0.14	0.471	o	|	|	|	|	0.63
45.083	0.00	0.14	0.470	o	|	|	|	|	0.63
45.167	0.00	0.14	0.469	o	|	|	|	|	0.63
45.250	0.00	0.14	0.468	o	|	|	|	|	0.63
45.333	0.00	0.14	0.467	o	|	|	|	|	0.63
45.417	0.00	0.14	0.466	o	|	|	|	|	0.63

45.500	0.00	0.14	0.465	o	|	|	|	|	0.63
45.583	0.00	0.14	0.464	o	|	|	|	|	0.62
45.667	0.00	0.14	0.463	o	|	|	|	|	0.62
45.750	0.00	0.14	0.462	o	|	|	|	|	0.62
45.833	0.00	0.14	0.461	o	|	|	|	|	0.62
45.917	0.00	0.14	0.460	o	|	|	|	|	0.62
46.000	0.00	0.13	0.459	o	|	|	|	|	0.62
46.083	0.00	0.13	0.458	o	|	|	|	|	0.62
46.167	0.00	0.13	0.458	o	|	|	|	|	0.62
46.250	0.00	0.13	0.457	o	|	|	|	|	0.61
46.333	0.00	0.13	0.456	o	|	|	|	|	0.61
46.417	0.00	0.13	0.455	o	|	|	|	|	0.61
46.500	0.00	0.13	0.454	o	|	|	|	|	0.61
46.583	0.00	0.13	0.453	o	|	|	|	|	0.61
46.667	0.00	0.13	0.452	o	|	|	|	|	0.61
46.750	0.00	0.13	0.451	o	|	|	|	|	0.61
46.833	0.00	0.13	0.450	o	|	|	|	|	0.61
46.917	0.00	0.13	0.449	o	|	|	|	|	0.60
47.000	0.00	0.13	0.448	o	|	|	|	|	0.60
47.083	0.00	0.13	0.447	o	|	|	|	|	0.60
47.167	0.00	0.13	0.447	o	|	|	|	|	0.60
47.250	0.00	0.13	0.446	o	|	|	|	|	0.60
47.333	0.00	0.13	0.445	o	|	|	|	|	0.60
47.417	0.00	0.13	0.444	o	|	|	|	|	0.60
47.500	0.00	0.13	0.443	o	|	|	|	|	0.60
47.583	0.00	0.13	0.442	o	|	|	|	|	0.59
47.667	0.00	0.13	0.441	o	|	|	|	|	0.59
47.750	0.00	0.13	0.440	o	|	|	|	|	0.59
47.833	0.00	0.13	0.439	o	|	|	|	|	0.59
47.917	0.00	0.13	0.438	o	|	|	|	|	0.59
48.000	0.00	0.13	0.438	o	|	|	|	|	0.59
48.083	0.00	0.13	0.437	o	|	|	|	|	0.59
48.167	0.00	0.13	0.436	o	|	|	|	|	0.59
48.250	0.00	0.13	0.435	o	|	|	|	|	0.59
48.333	0.00	0.13	0.434	o	|	|	|	|	0.58
48.417	0.00	0.13	0.433	o	|	|	|	|	0.58
48.500	0.00	0.13	0.432	o	|	|	|	|	0.58
48.583	0.00	0.13	0.431	o	|	|	|	|	0.58
48.667	0.00	0.13	0.431	o	|	|	|	|	0.58
48.750	0.00	0.13	0.430	o	|	|	|	|	0.58
48.833	0.00	0.13	0.429	o	|	|	|	|	0.58
48.917	0.00	0.13	0.428	o	|	|	|	|	0.58
49.000	0.00	0.13	0.427	o	|	|	|	|	0.57
49.083	0.00	0.13	0.426	o	|	|	|	|	0.57
49.167	0.00	0.12	0.425	o	|	|	|	|	0.57
49.250	0.00	0.12	0.425	o	|	|	|	|	0.57
49.333	0.00	0.12	0.424	o	|	|	|	|	0.57
49.417	0.00	0.12	0.423	o	|	|	|	|	0.57
49.500	0.00	0.12	0.422	o	|	|	|	|	0.57
49.583	0.00	0.12	0.421	o	|	|	|	|	0.57
49.667	0.00	0.12	0.420	o	|	|	|	|	0.57
49.750	0.00	0.12	0.419	o	|	|	|	|	0.56
49.833	0.00	0.12	0.419	o	|	|	|	|	0.56
49.917	0.00	0.12	0.418	o	|	|	|	|	0.56
50.000	0.00	0.12	0.417	o	|	|	|	|	0.56
50.083	0.00	0.12	0.416	o	|	|	|	|	0.56
50.167	0.00	0.12	0.415	o	|	|	|	|	0.56
50.250	0.00	0.12	0.414	o	|	|	|	|	0.56
50.333	0.00	0.12	0.414	o	|	|	|	|	0.56
50.417	0.00	0.12	0.413	o	|	|	|	|	0.56
50.500	0.00	0.12	0.412	o	|	|	|	|	0.55
50.583	0.00	0.12	0.411	o	|	|	|	|	0.55
50.667	0.00	0.12	0.410	o	|	|	|	|	0.55
50.750	0.00	0.12	0.409	o	|	|	|	|	0.55
50.833	0.00	0.12	0.409	o	|	|	|	|	0.55
50.917	0.00	0.12	0.408	o	|	|	|	|	0.55
51.000	0.00	0.12	0.407	o	|	|	|	|	0.55
51.083	0.00	0.12	0.406	o	|	|	|	|	0.55
51.167	0.00	0.12	0.405	o	|	|	|	|	0.55
51.250	0.00	0.12	0.404	o	|	|	|	|	0.54
51.333	0.00	0.12	0.404	o	|	|	|	|	0.54
51.417	0.00	0.12	0.403	o	|	|	|	|	0.54
51.500	0.00	0.12	0.402	o	|	|	|	|	0.54
51.583	0.00	0.12	0.401	o	|	|	|	|	0.54
51.667	0.00	0.12	0.400	o	|	|	|	|	0.54
51.750	0.00	0.12	0.400	o	|	|	|	|	0.54
51.833	0.00	0.12	0.399	o	|	|	|	|	0.54
51.917	0.00	0.12	0.398	o	|	|	|	|	0.54
52.000	0.00	0.12	0.397	o	|	|	|	|	0.53
52.083	0.00	0.12	0.396	o	|	|	|	|	0.53
52.167	0.00	0.12	0.396	o	|	|	|	|	0.53
52.250	0.00	0.12	0.395	o	|	|	|	|	0.53
52.333	0.00	0.12	0.394	o	|	|	|	|	0.53
52.417	0.00	0.12	0.393	o	|	|	|	|	0.53
52.500	0.00	0.12	0.392	o	|	|	|	|	0.53
52.583	0.00	0.11	0.392	o	|	|	|	|	0.53

52.667	0.00	0.11	0.391	o	|	|	|	|	0.53
52.750	0.00	0.11	0.390	o	|	|	|	|	0.52
52.833	0.00	0.11	0.389	o	|	|	|	|	0.52
52.917	0.00	0.11	0.388	o	|	|	|	|	0.52
53.000	0.00	0.11	0.388	o	|	|	|	|	0.52
53.083	0.00	0.11	0.387	o	|	|	|	|	0.52
53.167	0.00	0.11	0.386	o	|	|	|	|	0.52
53.250	0.00	0.11	0.385	o	|	|	|	|	0.52
53.333	0.00	0.11	0.385	o	|	|	|	|	0.52
53.417	0.00	0.11	0.384	o	|	|	|	|	0.52
53.500	0.00	0.11	0.383	o	|	|	|	|	0.52
53.583	0.00	0.11	0.382	o	|	|	|	|	0.51
53.667	0.00	0.11	0.381	o	|	|	|	|	0.51
53.750	0.00	0.11	0.381	o	|	|	|	|	0.51
53.833	0.00	0.11	0.380	o	|	|	|	|	0.51
53.917	0.00	0.11	0.379	o	|	|	|	|	0.51
54.000	0.00	0.11	0.378	o	|	|	|	|	0.51
54.083	0.00	0.11	0.378	o	|	|	|	|	0.51
54.167	0.00	0.11	0.377	o	|	|	|	|	0.51
54.250	0.00	0.11	0.376	o	|	|	|	|	0.51
54.333	0.00	0.11	0.375	o	|	|	|	|	0.51
54.417	0.00	0.11	0.375	o	|	|	|	|	0.50
54.500	0.00	0.11	0.374	o	|	|	|	|	0.50
54.583	0.00	0.11	0.373	o	|	|	|	|	0.50
54.667	0.00	0.11	0.372	o	|	|	|	|	0.50
54.750	0.00	0.11	0.372	o	|	|	|	|	0.50
54.833	0.00	0.11	0.371	o	|	|	|	|	0.50
54.917	0.00	0.11	0.370	o	|	|	|	|	0.50
55.000	0.00	0.11	0.369	o	|	|	|	|	0.50
55.083	0.00	0.11	0.369	o	|	|	|	|	0.50
55.167	0.00	0.11	0.368	o	|	|	|	|	0.50
55.250	0.00	0.11	0.367	o	|	|	|	|	0.49
55.333	0.00	0.11	0.366	o	|	|	|	|	0.49
55.417	0.00	0.11	0.366	o	|	|	|	|	0.49
55.500	0.00	0.11	0.365	o	|	|	|	|	0.49
55.583	0.00	0.11	0.364	o	|	|	|	|	0.49
55.667	0.00	0.11	0.363	o	|	|	|	|	0.49
55.750	0.00	0.11	0.363	o	|	|	|	|	0.49
55.833	0.00	0.11	0.362	o	|	|	|	|	0.49
55.917	0.00	0.11	0.361	o	|	|	|	|	0.49
56.000	0.00	0.11	0.360	o	|	|	|	|	0.49
56.083	0.00	0.11	0.360	o	|	|	|	|	0.48
56.167	0.00	0.11	0.359	o	|	|	|	|	0.48
56.250	0.00	0.11	0.358	o	|	|	|	|	0.48
56.333	0.00	0.10	0.358	o	|	|	|	|	0.48
56.417	0.00	0.10	0.357	o	|	|	|	|	0.48
56.500	0.00	0.10	0.356	o	|	|	|	|	0.48
56.583	0.00	0.10	0.355	o	|	|	|	|	0.48
56.667	0.00	0.10	0.355	o	|	|	|	|	0.48
56.750	0.00	0.10	0.354	o	|	|	|	|	0.48
56.833	0.00	0.10	0.353	o	|	|	|	|	0.48
56.917	0.00	0.10	0.353	o	|	|	|	|	0.47
57.000	0.00	0.10	0.352	o	|	|	|	|	0.47
57.083	0.00	0.10	0.351	o	|	|	|	|	0.47
57.167	0.00	0.10	0.350	o	|	|	|	|	0.47
57.250	0.00	0.10	0.350	o	|	|	|	|	0.47
57.333	0.00	0.10	0.349	o	|	|	|	|	0.47
57.417	0.00	0.10	0.348	o	|	|	|	|	0.47
57.500	0.00	0.10	0.348	o	|	|	|	|	0.47
57.583	0.00	0.10	0.347	o	|	|	|	|	0.47
57.667	0.00	0.10	0.346	o	|	|	|	|	0.47
57.750	0.00	0.10	0.345	o	|	|	|	|	0.46
57.833	0.00	0.10	0.345	o	|	|	|	|	0.46
57.917	0.00	0.10	0.344	o	|	|	|	|	0.46
58.000	0.00	0.10	0.343	o	|	|	|	|	0.46
58.083	0.00	0.10	0.343	o	|	|	|	|	0.46
58.167	0.00	0.10	0.342	o	|	|	|	|	0.46
58.250	0.00	0.10	0.341	o	|	|	|	|	0.46
58.333	0.00	0.10	0.341	o	|	|	|	|	0.46

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 700
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.542 (CFS)
Total volume = 1.068 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro12242.rte
**********HYDROGRAPH DATA**********
Number of intervals = 293
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 3.455 (CFS)
Total volume = 2.011 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 293
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.9	1.73	2.59	3.45 (Ft.)	Depth
0.083	0.06	0.00	0.000	O	|	|	|	|	0.00
0.167	0.15	0.00	0.001	OI	|	|	|	|	0.00
0.250	0.18	0.00	0.002	OI	|	|	|	|	0.00
0.333	0.22	0.00	0.003	O I	|	|	|	|	0.00
0.417	0.27	0.00	0.005	O I	|	|	|	|	0.01
0.500	0.28	0.00	0.007	O I	|	|	|	|	0.01
0.583	0.29	0.00	0.009	O I	|	|	|	|	0.01
0.667	0.29	0.00	0.011	O I	|	|	|	|	0.01
0.750	0.29	0.00	0.013	O I	|	|	|	|	0.02
0.833	0.32	0.00	0.015	O I	|	|	|	|	0.02
0.917	0.37	0.01	0.017	O I	|	|	|	|	0.02
1.000	0.38	0.01	0.020	O I	|	|	|	|	0.03
1.083	0.35	0.01	0.022	O I	|	|	|	|	0.03
1.167	0.31	0.01	0.025	O I	|	|	|	|	0.03
1.250	0.30	0.01	0.027	O I	|	|	|	|	0.04
1.333	0.30	0.01	0.029	O I	|	|	|	|	0.04
1.417	0.29	0.01	0.031	O I	|	|	|	|	0.04
1.500	0.29	0.01	0.033	O I	|	|	|	|	0.04
1.583	0.29	0.01	0.034	O I	|	|	|	|	0.05
1.667	0.29	0.01	0.036	O I	|	|	|	|	0.05
1.750	0.29	0.01	0.038	O I	|	|	|	|	0.05

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1.833   0.32   0.01    0.040  o I     |       |       |       |     0.05
1.917   0.37   0.01    0.043  o  I    |       |       |       |     0.06
2.000   0.38   0.01    0.045  o  I    |       |       |       |     0.06
2.083   0.38   0.01    0.048  o  I    |       |       |       |     0.06
2.167   0.39   0.01    0.050  o  I    |       |       |       |     0.07
2.250   0.39   0.02    0.053  o  I    |       |       |       |     0.07
2.333   0.39   0.02    0.055  o  I    |       |       |       |     0.07
2.417   0.39   0.02    0.058  o  I    |       |       |       |     0.08
2.500   0.39   0.02    0.060  o  I    |       |       |       |     0.08
2.583   0.42   0.02    0.063  o  I    |       |       |       |     0.08
2.667   0.47   0.02    0.066  o   I   |       |       |       |     0.09
2.750   0.48   0.02    0.069  o   I   |       |       |       |     0.09
2.833   0.48   0.02    0.072  o   I   |       |       |       |     0.10
2.917   0.48   0.02    0.075  o   I   |       |       |       |     0.10
3.000   0.49   0.02    0.079  o   I   |       |       |       |     0.11
3.083   0.49   0.02    0.082  o   I   |       |       |       |     0.11
3.167   0.49   0.02    0.085  o   I   |       |       |       |     0.11
3.250   0.49   0.03    0.088  o   I   |       |       |       |     0.12
3.333   0.49   0.03    0.091  o   I   |       |       |       |     0.12
3.417   0.49   0.03    0.095  o   I   |       |       |       |     0.13
3.500   0.49   0.03    0.098  o   I   |       |       |       |     0.13
3.583   0.49   0.03    0.101  o   I   |       |       |       |     0.14
3.667   0.49   0.03    0.104  o   I   |       |       |       |     0.14
3.750   0.49   0.03    0.107  o   I   |       |       |       |     0.14
3.833   0.52   0.03    0.110  o   I   |       |       |       |     0.15
3.917   0.56   0.03    0.114  o    I  |       |       |       |     0.15
4.000   0.57   0.03    0.117  o    I  |       |       |       |     0.16
4.083   0.58   0.04    0.121  o    I  |       |       |       |     0.16
4.167   0.58   0.04    0.125  o    I  |       |       |       |     0.17
4.250   0.58   0.04    0.129  o    I  |       |       |       |     0.17
4.333   0.61   0.04    0.133  o    I  |       |       |       |     0.18
4.417   0.66   0.04    0.137  o     I |       |       |       |     0.18
4.500   0.67   0.04    0.141  o     I |       |       |       |     0.19
4.583   0.68   0.04    0.145  o     I |       |       |       |     0.20
4.667   0.68   0.04    0.150  o     I |       |       |       |     0.20
4.750   0.68   0.05    0.154  o     I |       |       |       |     0.21
4.833   0.71   0.05    0.159  o     I |       |       |       |     0.21
4.917   0.76   0.05    0.163  o      I|       |       |       |     0.22
5.000   0.77   0.05    0.168  o      I|       |       |       |     0.23
5.083   0.71   0.05    0.173  o     I |       |       |       |     0.23
5.167   0.62   0.05    0.177  o    I  |       |       |       |     0.24
5.250   0.60   0.05    0.181  o    I  |       |       |       |     0.24
5.333   0.62   0.05    0.185  o    I  |       |       |       |     0.25
5.417   0.66   0.06    0.189  o     I |       |       |       |     0.25
5.500   0.67   0.06    0.193  o     I |       |       |       |     0.26
5.583   0.71   0.06    0.197  o     I |       |       |       |     0.27
5.667   0.76   0.06    0.202  o     I |       |       |       |     0.27
5.750   0.77   0.06    0.207  o      I|       |       |       |     0.28
5.833   0.77   0.06    0.212  o      I|       |       |       |     0.28
5.917   0.78   0.06    0.217  o      I|       |       |       |     0.29
6.000   0.78   0.07    0.222  o      I|       |       |       |     0.30
6.083   0.81   0.07    0.227  o      I|       |       |       |     0.30
6.167   0.85   0.07    0.232  o      I|       |       |       |     0.31
6.250   0.86   0.07    0.237  o       I       |       |       |     0.32
6.333   0.87   0.07    0.243  o       I       |       |       |     0.33
6.417   0.87   0.07    0.248  o       I       |       |       |     0.33
6.500   0.87   0.07    0.254  o       I       |       |       |     0.34
6.583   0.91   0.08    0.259  o       I       |       |       |     0.35
6.667   0.95   0.08    0.265  o       I       |       |       |     0.36
6.750   0.96   0.08    0.271  o       I       |       |       |     0.37
6.833   0.97   0.08    0.277  o       I       |       |       |     0.37
6.917   0.97   0.08    0.283  o       I       |       |       |     0.38
7.000   0.97   0.08    0.290  o       I       |       |       |     0.39
7.083   0.97   0.09    0.296  o       I       |       |       |     0.40
7.167   0.97   0.09    0.302  o       I       |       |       |     0.41
7.250   0.97   0.09    0.308  o       I       |       |       |     0.41
7.333   1.00   0.09    0.314  o       |I      |       |       |     0.42
7.417   1.05   0.09    0.320  o       |I      |       |       |     0.43
7.500   1.06   0.10    0.327  o       |I      |       |       |     0.44
7.583   1.10   0.10    0.334  o       | I     |       |       |     0.45
7.667   1.14   0.10    0.341  o       | I     |       |       |     0.46
7.750   1.16   0.10    0.348  o       | I     |       |       |     0.47
7.833   1.19   0.10    0.355  o       |  I    |       |       |     0.48
7.917   1.24   0.11    0.363  o       |  I    |       |       |     0.49
8.000   1.25   0.11    0.371  |o      |  I    |       |       |     0.50
8.083   1.32   0.11    0.379  |o      |   I   |       |       |     0.51
8.167   1.42   0.11    0.388  |o      |    I  |       |       |     0.52
8.250   1.44   0.12    0.397  |o      |    I  |       |       |     0.53
8.333   1.45   0.12    0.406  |o      |    I  |       |       |     0.55
8.417   1.45   0.12    0.415  |o      |    I  |       |       |     0.56
8.500   1.46   0.12    0.424  |o      |    I  |       |       |     0.57
8.583   1.49   0.13    0.433  |o      |    I  |       |       |     0.58
8.667   1.53   0.13    0.443  |o      |     I |       |       |     0.60
8.750   1.54   0.13    0.453  |o      |     I |       |       |     0.61
8.833   1.58   0.14    0.462  |o      |     I |       |       |     0.62
8.917   1.63   0.14    0.473  |o      |      I|       |       |     0.64
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 9.000    1.64    0.14      0.483  |O       |       I|        |        |     0.65
 9.083    1.71    0.14      0.493  |O       |       I|        |        |     0.66
 9.167    1.80    0.15      0.504  |O       |        I        |        |     0.68
 9.250    1.83    0.15      0.516  |O       |        I        |        |     0.69
 9.333    1.87    0.15      0.528  |O       |        |I       |        |     0.71
 9.417    1.92    0.16      0.540  |O       |        |I       |        |     0.73
 9.500    1.93    0.16      0.552  |O       |        |I       |        |     0.74
 9.583    1.97    0.17      0.564  |O       |        | I      |        |     0.76
 9.667    2.02    0.17      0.577  |O       |        | I      |        |     0.78
 9.750    2.03    0.17      0.589  |O       |        | I      |        |     0.79
 9.833    2.07    0.18      0.602  |O       |        |  I     |        |     0.81
 9.917    2.11    0.18      0.615  |O       |        |  I     |        |     0.83
10.000    2.13    0.18      0.629  |O       |        |  I     |        |     0.85
10.083    1.91    0.19      0.641  |O       |        |I       |        |     0.86
10.167    1.59    0.19      0.652  |O       |      I |        |        |     0.88
10.250    1.52    0.19      0.662  |O       |      I |        |        |     0.89
10.333    1.48    0.20      0.670  |O       |     I  |        |        |     0.90
10.417    1.47    0.20      0.679  |O       |     I  |        |        |     0.91
10.500    1.46    0.20      0.688  |O       |     I  |        |        |     0.93
10.583    1.61    0.20      0.697  |O       |      I |        |        |     0.94
10.667    1.84    0.21      0.708  |O       |        |I       |        |     0.95
10.750    1.90    0.21      0.719  |O       |        |I       |        |     0.97
10.833    1.92    0.21      0.731  |O       |        |I       |        |     0.98
10.917    1.93    0.22      0.743  | O      |        |I       |        |     1.00
11.000    1.94    0.22      0.754  | O      |        |I       |        |     1.01
11.083    1.91    0.23      0.766  | O      |        |I       |        |     1.03
11.167    1.86    0.24      0.777  | O      |        |I       |        |     1.04
11.250    1.85    0.24      0.789  | O      |        |I       |        |     1.06
11.333    1.85    0.25      0.800  | O      |        |I       |        |     1.07
11.417    1.85    0.26      0.811  | O      |        |I       |        |     1.08
11.500    1.84    0.26      0.822  | O      |        |I       |        |     1.10
11.583    1.78    0.27      0.832  | O      |        I        |        |     1.11
11.667    1.69    0.27      0.842  | O      |       I|        |        |     1.12
11.750    1.67    0.28      0.852  | O      |       I|        |        |     1.13
11.833    1.69    0.28      0.862  | O      |       I|        |        |     1.14
11.917    1.73    0.29      0.871  | O      |        I        |        |     1.16
12.000    1.74    0.29      0.881  | O      |        I        |        |     1.17
12.083    1.96    0.30      0.892  | O      |        | I      |        |     1.18
12.167    2.29    0.31      0.905  | O      |        |    I   |        |     1.20
12.250    2.37    0.31      0.918  | O      |        |    I   |        |     1.21
12.333    2.43    0.32      0.933  | O      |        |     I  |        |     1.23
12.417    2.49    0.33      0.947  |  O     |        |      I|        |     1.25
12.500    2.51    0.34      0.962  |  O     |        |      I|        |     1.27
12.583    2.58    0.35      0.978  |  O     |        |      I|        |     1.29
12.667    2.68    0.36      0.993  |  O     |        |       I        |     1.31
12.750    2.70    0.36      1.009  |  O     |        |       |I       |     1.33
12.833    2.74    0.37      1.026  |  O     |        |       |I       |     1.35
12.917    2.79    0.38      1.042  |  O     |        |       |I       |     1.37
13.000    2.81    0.39      1.059  |  O     |        |       |I       |     1.39
13.083    3.00    0.40      1.076  |  O     |        |       |  I     |     1.41
13.167    3.28    0.41      1.095  |  O     |        |       |    I   |     1.43
13.250    3.36    0.42      1.115  |  O     |        |       |     I  |     1.45
13.333    3.40    0.43      1.135  |   O    |        |       |     I  |     1.48
13.417    3.43    0.44      1.155  |   O    |        |       |     I  |     1.50
13.500    3.45    0.46      1.176  |   O    |        |       |      I |     1.53
13.583    3.06    0.47      1.195  |   O    |        |       |   I    |     1.55
13.667    2.48    0.48      1.211  |   O    |        |     I  |       |     1.57
13.750    2.34    0.48      1.225  |   O    |        |    I   |       |     1.59
13.833    2.28    0.49      1.237  |   O    |        |    I   |       |     1.60
13.917    2.25    0.50      1.249  |   O    |        |   I    |       |     1.62
14.000    2.23    0.50      1.261  |   O    |        |   I    |       |     1.63
14.083    2.36    0.51      1.274  |   O    |        |    I   |       |     1.65
14.167    2.54    0.52      1.287  |   O    |        |      I|       |     1.66
14.250    2.59    0.52      1.301  |   O    |        |      I|       |     1.68
14.333    2.57    0.53      1.315  |   O    |        |      I|       |     1.70
14.417    2.54    0.54      1.329  |    O   |        |      I|       |     1.72
14.500    2.53    0.55      1.343  |    O   |        |      I|       |     1.73
14.583    2.53    0.56      1.356  |    O   |        |      I|       |     1.75
14.667    2.52    0.56      1.370  |    O   |        |      I|       |     1.77
14.750    2.52    0.57      1.383  |    O   |        |      I|       |     1.78
14.833    2.49    0.58      1.397  |    O   |        |      I|       |     1.80
14.917    2.45    0.58      1.410  |    O   |        |     I |       |     1.82
15.000    2.44    0.59      1.422  |    O   |        |     I |       |     1.83
15.083    2.40    0.60      1.435  |    O   |        |     I |       |     1.85
15.167    2.35    0.61      1.447  |    O   |        |    I  |       |     1.86
15.250    2.34    0.61      1.459  |    O   |        |    I  |       |     1.88
15.333    2.30    0.62      1.471  |    O   |        |    I  |       |     1.89
15.417    2.25    0.62      1.482  |    O   |        |   I   |       |     1.90
15.500    2.24    0.63      1.493  |    O   |        |   I   |       |     1.92
15.583    2.11    0.64      1.504  |    O   |        |  I    |       |     1.93
15.667    1.92    0.64      1.514  |    O   |        |I      |       |     1.94
15.750    1.88    0.65      1.522  |    O   |        |I      |       |     1.95
15.833    1.86    0.65      1.531  |     O  |        |I      |       |     1.96
15.917    1.85    0.66      1.539  |     O  |        |I      |       |     1.97
16.000    1.84    0.66      1.547  |     O  |        |I      |       |     1.98
16.083    1.37    0.66      1.554  |     O  |   I    |       |       |     1.99
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16.167	0.68	0.67	1.556	| O |	|	|	|	1.99
16.250	0.52	0.67	1.556	| I O |	|	|	|	1.99
16.333	0.45	0.66	1.554	| I O |	|	|	|	1.99
16.417	0.41	0.66	1.553	| I O |	|	|	|	1.99
16.500	0.39	0.66	1.551	| I O |	|	|	|	1.99
16.583	0.36	0.66	1.549	| I O |	|	|	|	1.99
16.667	0.31	0.66	1.547	| I O |	|	|	|	1.98
16.750	0.30	0.66	1.544	| I O |	|	|	|	1.98
16.833	0.30	0.66	1.542	| I O |	|	|	|	1.98
16.917	0.29	0.66	1.539	| I O |	|	|	|	1.97
17.000	0.29	0.65	1.537	| I O |	|	|	|	1.97
17.083	0.35	0.65	1.535	| I O |	|	|	|	1.97
17.167	0.45	0.65	1.533	| I O |	|	|	|	1.97
17.250	0.47	0.65	1.531	| I O |	|	|	|	1.96
17.333	0.48	0.65	1.530	| I O |	|	|	|	1.96
17.417	0.48	0.65	1.529	| I O |	|	|	|	1.96
17.500	0.49	0.65	1.528	| I O |	|	|	|	1.96
17.583	0.49	0.65	1.527	| I O |	|	|	|	1.96
17.667	0.49	0.65	1.526	| I O |	|	|	|	1.96
17.750	0.49	0.65	1.525	| I O |	|	|	|	1.96
17.833	0.45	0.65	1.523	| IO |	|	|	|	1.95
17.917	0.41	0.65	1.522	| I O |	|	|	|	1.95
18.000	0.40	0.65	1.520	| I O |	|	|	|	1.95
18.083	0.39	0.64	1.518	| I O |	|	|	|	1.95
18.167	0.39	0.64	1.517	| I O |	|	|	|	1.95
18.250	0.39	0.64	1.515	| I O |	|	|	|	1.94
18.333	0.39	0.64	1.513	| I O |	|	|	|	1.94
18.417	0.39	0.64	1.511	| I O |	|	|	|	1.94
18.500	0.39	0.64	1.510	| I O |	|	|	|	1.94
18.583	0.36	0.64	1.508	| I O |	|	|	|	1.94
18.667	0.31	0.64	1.506	| I O |	|	|	|	1.93
18.750	0.30	0.64	1.503	| I O |	|	|	|	1.93
18.833	0.26	0.64	1.501	| I O |	|	|	|	1.93
18.917	0.22	0.63	1.498	| I O |	|	|	|	1.92
19.000	0.20	0.63	1.495	| I O |	|	|	|	1.92
19.083	0.23	0.63	1.493	| I O |	|	|	|	1.92
19.167	0.27	0.63	1.490	| I O |	|	|	|	1.91
19.250	0.28	0.63	1.488	| I O |	|	|	|	1.91
19.333	0.32	0.63	1.485	| I O |	|	|	|	1.91
19.417	0.37	0.63	1.483	| I O |	|	|	|	1.91
19.500	0.38	0.62	1.482	| I O |	|	|	|	1.90
19.583	0.35	0.62	1.480	| I O |	|	|	|	1.90
19.667	0.31	0.62	1.478	| I O |	|	|	|	1.90
19.750	0.30	0.62	1.476	| I O |	|	|	|	1.90
19.833	0.26	0.62	1.473	| I O |	|	|	|	1.89
19.917	0.22	0.62	1.471	| I O |	|	|	|	1.89
20.000	0.20	0.62	1.468	| I O |	|	|	|	1.89
20.083	0.23	0.62	1.465	| I O |	|	|	|	1.88
20.167	0.27	0.61	1.463	| I O |	|	|	|	1.88
20.250	0.28	0.61	1.460	| I O |	|	|	|	1.88
20.333	0.29	0.61	1.458	| I O |	|	|	|	1.87
20.417	0.29	0.61	1.456	| I O |	|	|	|	1.87
20.500	0.29	0.61	1.454	| I O |	|	|	|	1.87
20.583	0.29	0.61	1.451	| I O |	|	|	|	1.87
20.667	0.29	0.61	1.449	| I O |	|	|	|	1.86
20.750	0.29	0.61	1.447	| I O |	|	|	|	1.86
20.833	0.26	0.60	1.445	| I O |	|	|	|	1.86
20.917	0.21	0.60	1.442	| I O |	|	|	|	1.85
21.000	0.20	0.60	1.440	| I O |	|	|	|	1.85
21.083	0.23	0.60	1.437	| I O |	|	|	|	1.85
21.167	0.27	0.60	1.435	| I O |	|	|	|	1.85
21.250	0.28	0.60	1.432	| I O |	|	|	|	1.84
21.333	0.26	0.60	1.430	| I O |	|	|	|	1.84
21.417	0.21	0.59	1.428	| I O |	|	|	|	1.84
21.500	0.20	0.59	1.425	| I O |	|	|	|	1.83
21.583	0.23	0.59	1.422	| I O |	|	|	|	1.83
21.667	0.27	0.59	1.420	| I O |	|	|	|	1.83
21.750	0.28	0.59	1.418	| I O |	|	|	|	1.83
21.833	0.26	0.59	1.416	| I O |	|	|	|	1.82
21.917	0.21	0.59	1.413	| I O |	|	|	|	1.82
22.000	0.20	0.59	1.411	| I O |	|	|	|	1.82
22.083	0.23	0.58	1.408	| I O |	|	|	|	1.81
22.167	0.27	0.58	1.406	| I O |	|	|	|	1.81
22.250	0.28	0.58	1.404	| I O |	|	|	|	1.81
22.333	0.26	0.58	1.402	| I O |	|	|	|	1.81
22.417	0.21	0.58	1.399	| I O |	|	|	|	1.80
22.500	0.20	0.58	1.397	| I O |	|	|	|	1.80
22.583	0.20	0.58	1.394	| I O |	|	|	|	1.80
22.667	0.20	0.57	1.391	| I O |	|	|	|	1.79
22.750	0.19	0.57	1.389	| I O |	|	|	|	1.79
22.833	0.19	0.57	1.386	| I O |	|	|	|	1.79
22.917	0.19	0.57	1.384	| I O |	|	|	|	1.78
23.000	0.19	0.57	1.381	| I O |	|	|	|	1.78
23.083	0.19	0.57	1.378	| I O |	|	|	|	1.78
23.167	0.19	0.57	1.376	| I O |	|	|	|	1.77
23.250	0.19	0.56	1.373	| I O |	|	|	|	1.77

23.333	0.19	0.56	1.371	|I o	|	|	|	1.77
23.417	0.19	0.56	1.368	|I o	|	|	|	1.76
23.500	0.19	0.56	1.366	|I o	|	|	|	1.76
23.583	0.19	0.56	1.363	|I o	|	|	|	1.76
23.667	0.19	0.56	1.361	|I o	|	|	|	1.76
23.750	0.19	0.56	1.358	|I o	|	|	|	1.75
23.833	0.19	0.56	1.356	|I o	|	|	|	1.75
23.917	0.19	0.55	1.353	|I o	|	|	|	1.75
24.000	0.19	0.55	1.351	|I o	|	|	|	1.74
24.083	0.13	0.55	1.348	|I o	|	|	|	1.74
24.167	0.04	0.55	1.345	I o	|	|	|	1.74
24.250	0.02	0.55	1.341	I o	|	|	|	1.73
24.333	0.01	0.55	1.338	I o	|	|	|	1.73
24.417	0.00	0.54	1.334	I o	|	|	|	1.72
24.500	0.00	0.54	1.330	I o	|	|	|	1.72
24.583	0.00	0.54	1.326	I o	|	|	|	1.71
24.667	0.00	0.54	1.323	I o	|	|	|	1.71
24.750	0.00	0.53	1.319	I o	|	|	|	1.70
24.833	0.00	0.53	1.315	I o	|	|	|	1.70
24.917	0.00	0.53	1.312	I o	|	|	|	1.70
25.000	0.00	0.53	1.308	I o	|	|	|	1.69
25.083	0.00	0.53	1.304	I o	|	|	|	1.69
25.167	0.00	0.52	1.301	I o	|	|	|	1.68
25.250	0.00	0.52	1.297	I o	|	|	|	1.68
25.333	0.00	0.52	1.294	I o	|	|	|	1.67
25.417	0.00	0.52	1.290	I o	|	|	|	1.67
25.500	0.00	0.52	1.286	I o	|	|	|	1.66
25.583	0.00	0.52	1.283	I o	|	|	|	1.66
25.667	0.00	0.51	1.279	I o	|	|	|	1.66
25.750	0.00	0.51	1.276	I o	|	|	|	1.65
25.833	0.00	0.51	1.272	I o	|	|	|	1.65
25.917	0.00	0.51	1.269	I o	|	|	|	1.64
26.000	0.00	0.51	1.265	I o	|	|	|	1.64
26.083	0.00	0.50	1.262	I o	|	|	|	1.63
26.167	0.00	0.50	1.258	I o	|	|	|	1.63
26.250	0.00	0.50	1.255	I o	|	|	|	1.63
26.333	0.00	0.50	1.252	I o	|	|	|	1.62
26.417	0.00	0.50	1.248	I o	|	|	|	1.62
26.500	0.00	0.49	1.245	I o	|	|	|	1.61
26.583	0.00	0.49	1.241	I o	|	|	|	1.61
26.667	0.00	0.49	1.238	I o	|	|	|	1.61
26.750	0.00	0.49	1.235	I o	|	|	|	1.60
26.833	0.00	0.49	1.231	I o	|	|	|	1.60
26.917	0.00	0.48	1.228	I o	|	|	|	1.59
27.000	0.00	0.48	1.225	I o	|	|	|	1.59
27.083	0.00	0.48	1.221	I o	|	|	|	1.58
27.167	0.00	0.48	1.218	I o	|	|	|	1.58
27.250	0.00	0.48	1.215	I o	|	|	|	1.58
27.333	0.00	0.48	1.211	I o	|	|	|	1.57
27.417	0.00	0.47	1.208	I o	|	|	|	1.57
27.500	0.00	0.47	1.205	I o	|	|	|	1.56
27.583	0.00	0.47	1.202	I o	|	|	|	1.56
27.667	0.00	0.47	1.198	I o	|	|	|	1.56
27.750	0.00	0.47	1.195	I o	|	|	|	1.55
27.833	0.00	0.46	1.192	I o	|	|	|	1.55
27.917	0.00	0.46	1.189	I o	|	|	|	1.54
28.000	0.00	0.46	1.186	I o	|	|	|	1.54
28.083	0.00	0.46	1.182	I o	|	|	|	1.54
28.167	0.00	0.46	1.179	I o	|	|	|	1.53
28.250	0.00	0.46	1.176	I o	|	|	|	1.53
28.333	0.00	0.45	1.173	I o	|	|	|	1.53
28.417	0.00	0.45	1.170	I o	|	|	|	1.52
28.500	0.00	0.45	1.167	I o	|	|	|	1.52
28.583	0.00	0.45	1.164	I o	|	|	|	1.51
28.667	0.00	0.45	1.160	I o	|	|	|	1.51
28.750	0.00	0.45	1.157	I o	|	|	|	1.51
28.833	0.00	0.44	1.154	I o	|	|	|	1.50
28.917	0.00	0.44	1.151	I o	|	|	|	1.50
29.000	0.00	0.44	1.148	I o	|	|	|	1.50
29.083	0.00	0.44	1.145	I o	|	|	|	1.49
29.167	0.00	0.44	1.142	I o	|	|	|	1.49
29.250	0.00	0.44	1.139	I o	|	|	|	1.48
29.333	0.00	0.43	1.136	I o	|	|	|	1.48
29.417	0.00	0.43	1.133	I o	|	|	|	1.48
29.500	0.00	0.43	1.130	I o	|	|	|	1.47
29.583	0.00	0.43	1.127	I o	|	|	|	1.47
29.667	0.00	0.43	1.124	I o	|	|	|	1.47
29.750	0.00	0.43	1.121	I o	|	|	|	1.46
29.833	0.00	0.42	1.118	I o	|	|	|	1.46
29.917	0.00	0.42	1.116	I o	|	|	|	1.46
30.000	0.00	0.42	1.113	I o	|	|	|	1.45
30.083	0.00	0.42	1.110	I o	|	|	|	1.45
30.167	0.00	0.42	1.107	I o	|	|	|	1.44
30.250	0.00	0.42	1.104	I o	|	|	|	1.44
30.333	0.00	0.41	1.101	I o	|	|	|	1.44
30.417	0.00	0.41	1.098	I o	|	|	|	1.43

30.500	0.00	0.41	1.095	I o	|	|	|	1.43
30.583	0.00	0.41	1.093	I o	|	|	|	1.43
30.667	0.00	0.41	1.090	I o	|	|	|	1.42
30.750	0.00	0.41	1.087	I o	|	|	|	1.42
30.833	0.00	0.41	1.084	I o	|	|	|	1.42
30.917	0.00	0.40	1.081	I o	|	|	|	1.41
31.000	0.00	0.40	1.079	I o	|	|	|	1.41
31.083	0.00	0.40	1.076	I o	|	|	|	1.41
31.167	0.00	0.40	1.073	I o	|	|	|	1.40
31.250	0.00	0.40	1.070	I o	|	|	|	1.40
31.333	0.00	0.40	1.068	I o	|	|	|	1.40
31.417	0.00	0.40	1.065	I o	|	|	|	1.39
31.500	0.00	0.39	1.062	I o	|	|	|	1.39
31.583	0.00	0.39	1.059	I o	|	|	|	1.39
31.667	0.00	0.39	1.057	I o	|	|	|	1.38
31.750	0.00	0.39	1.054	I o	|	|	|	1.38
31.833	0.00	0.39	1.051	I o	|	|	|	1.38
31.917	0.00	0.39	1.049	I o	|	|	|	1.37
32.000	0.00	0.38	1.046	I o	|	|	|	1.37
32.083	0.00	0.38	1.043	I o	|	|	|	1.37
32.167	0.00	0.38	1.041	I o	|	|	|	1.36
32.250	0.00	0.38	1.038	I o	|	|	|	1.36
32.333	0.00	0.38	1.036	I o	|	|	|	1.36
32.417	0.00	0.38	1.033	I o	|	|	|	1.35
32.500	0.00	0.38	1.030	I o	|	|	|	1.35
32.583	0.00	0.37	1.028	I o	|	|	|	1.35
32.667	0.00	0.37	1.025	I o	|	|	|	1.34
32.750	0.00	0.37	1.023	I o	|	|	|	1.34
32.833	0.00	0.37	1.020	I o	|	|	|	1.34
32.917	0.00	0.37	1.017	I o	|	|	|	1.34
33.000	0.00	0.37	1.015	I o	|	|	|	1.33
33.083	0.00	0.37	1.012	I o	|	|	|	1.33
33.167	0.00	0.36	1.010	I o	|	|	|	1.33
33.250	0.00	0.36	1.007	I o	|	|	|	1.32
33.333	0.00	0.36	1.005	I o	|	|	|	1.32
33.417	0.00	0.36	1.002	I o	|	|	|	1.32
33.500	0.00	0.36	1.000	I o	|	|	|	1.31
33.583	0.00	0.36	0.997	I o	|	|	|	1.31
33.667	0.00	0.36	0.995	I o	|	|	|	1.31
33.750	0.00	0.36	0.993	I o	|	|	|	1.31
33.833	0.00	0.35	0.990	I o	|	|	|	1.30
33.917	0.00	0.35	0.988	I o	|	|	|	1.30
34.000	0.00	0.35	0.985	I o	|	|	|	1.30
34.083	0.00	0.35	0.983	I o	|	|	|	1.29
34.167	0.00	0.35	0.980	I o	|	|	|	1.29
34.250	0.00	0.35	0.978	I o	|	|	|	1.29
34.333	0.00	0.35	0.976	I o	|	|	|	1.28
34.417	0.00	0.34	0.973	I o	|	|	|	1.28
34.500	0.00	0.34	0.971	I o	|	|	|	1.28
34.583	0.00	0.34	0.969	I o	|	|	|	1.28
34.667	0.00	0.34	0.966	I o	|	|	|	1.27
34.750	0.00	0.34	0.964	I o	|	|	|	1.27
34.833	0.00	0.34	0.962	I o	|	|	|	1.27
34.917	0.00	0.34	0.959	I o	|	|	|	1.26
35.000	0.00	0.34	0.957	I o	|	|	|	1.26
35.083	0.00	0.33	0.955	I o	|	|	|	1.26
35.167	0.00	0.33	0.952	I o	|	|	|	1.26
35.250	0.00	0.33	0.950	I o	|	|	|	1.25
35.333	0.00	0.33	0.948	I o	|	|	|	1.25
35.417	0.00	0.33	0.945	I o	|	|	|	1.25
35.500	0.00	0.33	0.943	I o	|	|	|	1.24
35.583	0.00	0.33	0.941	I o	|	|	|	1.24
35.667	0.00	0.33	0.939	I o	|	|	|	1.24
35.750	0.00	0.32	0.936	I o	|	|	|	1.24
35.833	0.00	0.32	0.934	I o	|	|	|	1.23
35.917	0.00	0.32	0.932	I o	|	|	|	1.23
36.000	0.00	0.32	0.930	I o	|	|	|	1.23
36.083	0.00	0.32	0.928	I o	|	|	|	1.23
36.167	0.00	0.32	0.925	I o	|	|	|	1.22
36.250	0.00	0.32	0.923	I o	|	|	|	1.22
36.333	0.00	0.32	0.921	I o	|	|	|	1.22
36.417	0.00	0.31	0.919	I o	|	|	|	1.21
36.500	0.00	0.31	0.917	I o	|	|	|	1.21
36.583	0.00	0.31	0.914	I o	|	|	|	1.21
36.667	0.00	0.31	0.912	I o	|	|	|	1.21
36.750	0.00	0.31	0.910	I o	|	|	|	1.20
36.833	0.00	0.31	0.908	I o	|	|	|	1.20
36.917	0.00	0.31	0.906	I o	|	|	|	1.20
37.000	0.00	0.31	0.904	I o	|	|	|	1.20
37.083	0.00	0.31	0.902	I o	|	|	|	1.19
37.167	0.00	0.30	0.900	I o	|	|	|	1.19
37.250	0.00	0.30	0.898	I o	|	|	|	1.19
37.333	0.00	0.30	0.895	I o	|	|	|	1.19
37.417	0.00	0.30	0.893	I o	|	|	|	1.18
37.500	0.00	0.30	0.891	I o	|	|	|	1.18
37.583	0.00	0.30	0.889	I o	|	|	|	1.18

37.667	0.00	0.30	0.887	I o	|	|	|	1.18
37.750	0.00	0.30	0.885	I o	|	|	|	1.17
37.833	0.00	0.30	0.883	I o	|	|	|	1.17
37.917	0.00	0.29	0.881	I o	|	|	|	1.17
38.000	0.00	0.29	0.879	I o	|	|	|	1.17
38.083	0.00	0.29	0.877	I o	|	|	|	1.16
38.167	0.00	0.29	0.875	I o	|	|	|	1.16
38.250	0.00	0.29	0.873	I o	|	|	|	1.16
38.333	0.00	0.29	0.871	I o	|	|	|	1.16
38.417	0.00	0.29	0.869	I o	|	|	|	1.15
38.500	0.00	0.29	0.867	I o	|	|	|	1.15
38.583	0.00	0.29	0.865	I o	|	|	|	1.15
38.667	0.00	0.28	0.863	I o	|	|	|	1.15
38.750	0.00	0.28	0.861	I o	|	|	|	1.14
38.833	0.00	0.28	0.859	I o	|	|	|	1.14
38.917	0.00	0.28	0.857	I o	|	|	|	1.14
39.000	0.00	0.28	0.855	I o	|	|	|	1.14
39.083	0.00	0.28	0.853	I o	|	|	|	1.14
39.167	0.00	0.28	0.852	I o	|	|	|	1.13
39.250	0.00	0.28	0.850	I o	|	|	|	1.13
39.333	0.00	0.28	0.848	I o	|	|	|	1.13
39.417	0.00	0.27	0.846	I o	|	|	|	1.13
39.500	0.00	0.27	0.844	I o	|	|	|	1.12
39.583	0.00	0.27	0.842	I o	|	|	|	1.12
39.667	0.00	0.27	0.840	I o	|	|	|	1.12
39.750	0.00	0.27	0.838	I o	|	|	|	1.12
39.833	0.00	0.27	0.837	I o	|	|	|	1.11
39.917	0.00	0.27	0.835	I o	|	|	|	1.11
40.000	0.00	0.27	0.833	I o	|	|	|	1.11
40.083	0.00	0.27	0.831	I o	|	|	|	1.11
40.167	0.00	0.27	0.829	I o	|	|	|	1.11
40.250	0.00	0.26	0.827	I o	|	|	|	1.10
40.333	0.00	0.26	0.825	I o	|	|	|	1.10
40.417	0.00	0.26	0.824	I o	|	|	|	1.10
40.500	0.00	0.26	0.822	I o	|	|	|	1.10
40.583	0.00	0.26	0.820	I o	|	|	|	1.09
40.667	0.00	0.26	0.818	I o	|	|	|	1.09
40.750	0.00	0.26	0.817	I o	|	|	|	1.09
40.833	0.00	0.26	0.815	I o	|	|	|	1.09
40.917	0.00	0.26	0.813	I o	|	|	|	1.09
41.000	0.00	0.26	0.811	I o	|	|	|	1.08
41.083	0.00	0.25	0.809	I o	|	|	|	1.08
41.167	0.00	0.25	0.808	I o	|	|	|	1.08
41.250	0.00	0.25	0.806	I o	|	|	|	1.08
41.333	0.00	0.25	0.804	I o	|	|	|	1.07
41.417	0.00	0.25	0.802	I o	|	|	|	1.07
41.500	0.00	0.25	0.801	I o	|	|	|	1.07
41.583	0.00	0.25	0.799	I o	|	|	|	1.07
41.667	0.00	0.25	0.797	I o	|	|	|	1.07
41.750	0.00	0.25	0.796	I o	|	|	|	1.06
41.833	0.00	0.25	0.794	I o	|	|	|	1.06
41.917	0.00	0.25	0.792	I o	|	|	|	1.06
42.000	0.00	0.24	0.791	I o	|	|	|	1.06
42.083	0.00	0.24	0.789	I o	|	|	|	1.06
42.167	0.00	0.24	0.787	I o	|	|	|	1.05
42.250	0.00	0.24	0.786	I o	|	|	|	1.05
42.333	0.00	0.24	0.784	I o	|	|	|	1.05
42.417	0.00	0.24	0.782	I o	|	|	|	1.05
42.500	0.00	0.24	0.781	I o	|	|	|	1.05
42.583	0.00	0.24	0.779	I o	|	|	|	1.04
42.667	0.00	0.24	0.777	I o	|	|	|	1.04
42.750	0.00	0.24	0.776	I o	|	|	|	1.04
42.833	0.00	0.24	0.774	I o	|	|	|	1.04
42.917	0.00	0.23	0.772	I o	|	|	|	1.04
43.000	0.00	0.23	0.771	I o	|	|	|	1.03
43.083	0.00	0.23	0.769	I o	|	|	|	1.03
43.167	0.00	0.23	0.768	I o	|	|	|	1.03
43.250	0.00	0.23	0.766	I o	|	|	|	1.03
43.333	0.00	0.23	0.764	I o	|	|	|	1.03
43.417	0.00	0.23	0.763	I o	|	|	|	1.02
43.500	0.00	0.23	0.761	I o	|	|	|	1.02
43.583	0.00	0.23	0.760	I o	|	|	|	1.02
43.667	0.00	0.23	0.758	I o	|	|	|	1.02
43.750	0.00	0.23	0.757	I o	|	|	|	1.02
43.833	0.00	0.22	0.755	I o	|	|	|	1.01
43.917	0.00	0.22	0.754	I o	|	|	|	1.01
44.000	0.00	0.22	0.752	I o	|	|	|	1.01
44.083	0.00	0.22	0.750	I o	|	|	|	1.01
44.167	0.00	0.22	0.749	I o	|	|	|	1.01
44.250	0.00	0.22	0.747	I o	|	|	|	1.01
44.333	0.00	0.22	0.746	I o	|	|	|	1.00
44.417	0.00	0.22	0.744	I o	|	|	|	1.00
44.500	0.00	0.22	0.743	I o	|	|	|	1.00
44.583	0.00	0.22	0.741	I o	|	|	|	1.00
44.667	0.00	0.22	0.740	I o	|	|	|	1.00
44.750	0.00	0.22	0.738	I o	|	|	|	0.99

44.833	0.00	0.22	0.737	I O	|	|	|	0.99
44.917	0.00	0.22	0.735	IO	|	|	|	0.99
45.000	0.00	0.22	0.734	IO	|	|	|	0.99
45.083	0.00	0.21	0.732	IO	|	|	|	0.99
45.167	0.00	0.21	0.731	IO	|	|	|	0.98
45.250	0.00	0.21	0.729	IO	|	|	|	0.98
45.333	0.00	0.21	0.728	IO	|	|	|	0.98
45.417	0.00	0.21	0.727	IO	|	|	|	0.98
45.500	0.00	0.21	0.725	IO	|	|	|	0.98
45.583	0.00	0.21	0.724	IO	|	|	|	0.97
45.667	0.00	0.21	0.722	IO	|	|	|	0.97
45.750	0.00	0.21	0.721	IO	|	|	|	0.97
45.833	0.00	0.21	0.719	IO	|	|	|	0.97
45.917	0.00	0.21	0.718	IO	|	|	|	0.97
46.000	0.00	0.21	0.716	IO	|	|	|	0.96
46.083	0.00	0.21	0.715	IO	|	|	|	0.96
46.167	0.00	0.21	0.713	IO	|	|	|	0.96
46.250	0.00	0.21	0.712	IO	|	|	|	0.96
46.333	0.00	0.21	0.711	IO	|	|	|	0.96
46.417	0.00	0.21	0.709	IO	|	|	|	0.95
46.500	0.00	0.21	0.708	IO	|	|	|	0.95
46.583	0.00	0.21	0.706	IO	|	|	|	0.95
46.667	0.00	0.21	0.705	IO	|	|	|	0.95
46.750	0.00	0.21	0.703	IO	|	|	|	0.95
46.833	0.00	0.21	0.702	IO	|	|	|	0.94
46.917	0.00	0.21	0.701	IO	|	|	|	0.94
47.000	0.00	0.21	0.699	IO	|	|	|	0.94
47.083	0.00	0.20	0.698	IO	|	|	|	0.94
47.167	0.00	0.20	0.696	IO	|	|	|	0.94
47.250	0.00	0.20	0.695	IO	|	|	|	0.94
47.333	0.00	0.20	0.694	IO	|	|	|	0.93
47.417	0.00	0.20	0.692	IO	|	|	|	0.93
47.500	0.00	0.20	0.691	IO	|	|	|	0.93
47.583	0.00	0.20	0.689	IO	|	|	|	0.93
47.667	0.00	0.20	0.688	IO	|	|	|	0.93
47.750	0.00	0.20	0.687	IO	|	|	|	0.92
47.833	0.00	0.20	0.685	IO	|	|	|	0.92
47.917	0.00	0.20	0.684	IO	|	|	|	0.92
48.000	0.00	0.20	0.682	IO	|	|	|	0.92
48.083	0.00	0.20	0.681	IO	|	|	|	0.92
48.167	0.00	0.20	0.680	IO	|	|	|	0.91
48.250	0.00	0.20	0.678	IO	|	|	|	0.91
48.333	0.00	0.20	0.677	IO	|	|	|	0.91
48.417	0.00	0.20	0.676	IO	|	|	|	0.91
48.500	0.00	0.20	0.674	IO	|	|	|	0.91
48.583	0.00	0.20	0.673	IO	|	|	|	0.91
48.667	0.00	0.20	0.671	IO	|	|	|	0.90
48.750	0.00	0.20	0.670	IO	|	|	|	0.90
48.833	0.00	0.20	0.669	IO	|	|	|	0.90
48.917	0.00	0.20	0.667	IO	|	|	|	0.90
49.000	0.00	0.20	0.666	IO	|	|	|	0.90
49.083	0.00	0.20	0.665	IO	|	|	|	0.89
49.167	0.00	0.19	0.663	IO	|	|	|	0.89
49.250	0.00	0.19	0.662	IO	|	|	|	0.89
49.333	0.00	0.19	0.661	IO	|	|	|	0.89
49.417	0.00	0.19	0.659	IO	|	|	|	0.89
49.500	0.00	0.19	0.658	IO	|	|	|	0.89
49.583	0.00	0.19	0.657	IO	|	|	|	0.88
49.667	0.00	0.19	0.655	IO	|	|	|	0.88
49.750	0.00	0.19	0.654	IO	|	|	|	0.88
49.833	0.00	0.19	0.653	IO	|	|	|	0.88
49.917	0.00	0.19	0.651	IO	|	|	|	0.88
50.000	0.00	0.19	0.650	IO	|	|	|	0.87
50.083	0.00	0.19	0.649	IO	|	|	|	0.87
50.167	0.00	0.19	0.647	IO	|	|	|	0.87
50.250	0.00	0.19	0.646	IO	|	|	|	0.87
50.333	0.00	0.19	0.645	IO	|	|	|	0.87
50.417	0.00	0.19	0.644	IO	|	|	|	0.87
50.500	0.00	0.19	0.642	IO	|	|	|	0.86
50.583	0.00	0.19	0.641	IO	|	|	|	0.86
50.667	0.00	0.19	0.640	IO	|	|	|	0.86
50.750	0.00	0.19	0.638	IO	|	|	|	0.86
50.833	0.00	0.19	0.637	IO	|	|	|	0.86
50.917	0.00	0.19	0.636	IO	|	|	|	0.86
51.000	0.00	0.19	0.635	IO	|	|	|	0.85
51.083	0.00	0.19	0.633	IO	|	|	|	0.85
51.167	0.00	0.19	0.632	IO	|	|	|	0.85
51.250	0.00	0.19	0.631	IO	|	|	|	0.85
51.333	0.00	0.18	0.629	IO	|	|	|	0.85
51.417	0.00	0.18	0.628	IO	|	|	|	0.85
51.500	0.00	0.18	0.627	IO	|	|	|	0.84
51.583	0.00	0.18	0.626	IO	|	|	|	0.84
51.667	0.00	0.18	0.624	IO	|	|	|	0.84
51.750	0.00	0.18	0.623	IO	|	|	|	0.84
51.833	0.00	0.18	0.622	IO	|	|	|	0.84
51.917	0.00	0.18	0.621	IO	|	|	|	0.84

52.000	0.00	0.18	0.619	IO				0.83
52.083	0.00	0.18	0.618	IO				0.83
52.167	0.00	0.18	0.617	IO				0.83
52.250	0.00	0.18	0.616	IO				0.83
52.333	0.00	0.18	0.614	IO				0.83
52.417	0.00	0.18	0.613	IO				0.83
52.500	0.00	0.18	0.612	IO				0.82
52.583	0.00	0.18	0.611	IO				0.82
52.667	0.00	0.18	0.609	IO				0.82
52.750	0.00	0.18	0.608	IO				0.82
52.833	0.00	0.18	0.607	IO				0.82
52.917	0.00	0.18	0.606	IO				0.82
53.000	0.00	0.18	0.605	IO				0.81
53.083	0.00	0.18	0.603	IO				0.81
53.167	0.00	0.18	0.602	IO				0.81
53.250	0.00	0.18	0.601	IO				0.81
53.333	0.00	0.18	0.600	IO				0.81
53.417	0.00	0.18	0.598	IO				0.81
53.500	0.00	0.18	0.597	IO				0.80
53.583	0.00	0.17	0.596	IO				0.80
53.667	0.00	0.17	0.595	IO				0.80
53.750	0.00	0.17	0.594	IO				0.80
53.833	0.00	0.17	0.592	IO				0.80
53.917	0.00	0.17	0.591	IO				0.80
54.000	0.00	0.17	0.590	IO				0.79
54.083	0.00	0.17	0.589	IO				0.79
54.167	0.00	0.17	0.588	IO				0.79
54.250	0.00	0.17	0.586	IO				0.79
54.333	0.00	0.17	0.585	IO				0.79
54.417	0.00	0.17	0.584	IO				0.79
54.500	0.00	0.17	0.583	IO				0.78
54.583	0.00	0.17	0.582	IO				0.78
54.667	0.00	0.17	0.581	IO				0.78
54.750	0.00	0.17	0.579	IO				0.78
54.833	0.00	0.17	0.578	IO				0.78
54.917	0.00	0.17	0.577	IO				0.78
55.000	0.00	0.17	0.576	IO				0.78
55.083	0.00	0.17	0.575	IO				0.77
55.167	0.00	0.17	0.574	IO				0.77
55.250	0.00	0.17	0.572	IO				0.77
55.333	0.00	0.17	0.571	IO				0.77
55.417	0.00	0.17	0.570	IO				0.77
55.500	0.00	0.17	0.569	IO				0.77
55.583	0.00	0.17	0.568	IO				0.76
55.667	0.00	0.17	0.567	IO				0.76
55.750	0.00	0.17	0.566	IO				0.76
55.833	0.00	0.17	0.564	IO				0.76
55.917	0.00	0.17	0.563	IO				0.76
56.000	0.00	0.16	0.562	IO				0.76
56.083	0.00	0.16	0.561	IO				0.75
56.167	0.00	0.16	0.560	IO				0.75
56.250	0.00	0.16	0.559	IO				0.75
56.333	0.00	0.16	0.558	IO				0.75
56.417	0.00	0.16	0.556	IO				0.75
56.500	0.00	0.16	0.555	IO				0.75
56.583	0.00	0.16	0.554	IO				0.75
56.667	0.00	0.16	0.553	IO				0.74
56.750	0.00	0.16	0.552	IO				0.74
56.833	0.00	0.16	0.551	IO				0.74
56.917	0.00	0.16	0.550	IO				0.74
57.000	0.00	0.16	0.549	IO				0.74
57.083	0.00	0.16	0.548	IO				0.74
57.167	0.00	0.16	0.546	IO				0.74
57.250	0.00	0.16	0.545	IO				0.73
57.333	0.00	0.16	0.544	IO				0.73
57.417	0.00	0.16	0.543	IO				0.73
57.500	0.00	0.16	0.542	IO				0.73
57.583	0.00	0.16	0.541	IO				0.73
57.667	0.00	0.16	0.540	IO				0.73
57.750	0.00	0.16	0.539	IO				0.73
57.833	0.00	0.16	0.538	IO				0.72
57.917	0.00	0.16	0.537	IO				0.72
58.000	0.00	0.16	0.535	IO				0.72
58.083	0.00	0.16	0.534	IO				0.72
58.167	0.00	0.16	0.533	IO				0.72
58.250	0.00	0.16	0.532	IO				0.72
58.333	0.00	0.16	0.531	IO				0.71
58.417	0.00	0.16	0.530	IO				0.71
58.500	0.00	0.16	0.529	IO				0.71
58.583	0.00	0.15	0.528	IO				0.71
58.667	0.00	0.15	0.527	IO				0.71
58.750	0.00	0.15	0.526	IO				0.71
58.833	0.00	0.15	0.525	IO				0.71
58.917	0.00	0.15	0.524	IO				0.70
59.000	0.00	0.15	0.523	IO				0.70
59.083	0.00	0.15	0.522	IO				0.70

59.167	0.00	0.15	0.521	IO				0.70
59.250	0.00	0.15	0.519	IO				0.70
59.333	0.00	0.15	0.518	IO				0.70
59.417	0.00	0.15	0.517	IO				0.70
59.500	0.00	0.15	0.516	IO				0.69
59.583	0.00	0.15	0.515	IO				0.69
59.667	0.00	0.15	0.514	IO				0.69
59.750	0.00	0.15	0.513	IO				0.69
59.833	0.00	0.15	0.512	IO				0.69
59.917	0.00	0.15	0.511	IO				0.69
60.000	0.00	0.15	0.510	IO				0.69
60.083	0.00	0.15	0.509	IO				0.69
60.167	0.00	0.15	0.508	IO				0.68
60.250	0.00	0.15	0.507	IO				0.68
60.333	0.00	0.15	0.506	IO				0.68
60.417	0.00	0.15	0.505	IO				0.68
60.500	0.00	0.15	0.504	IO				0.68
60.583	0.00	0.15	0.503	IO				0.68
60.667	0.00	0.15	0.502	IO				0.68
60.750	0.00	0.15	0.501	IO				0.67
60.833	0.00	0.15	0.500	IO				0.67
60.917	0.00	0.15	0.499	IO				0.67
61.000	0.00	0.15	0.498	IO				0.67
61.083	0.00	0.15	0.497	IO				0.67
61.167	0.00	0.15	0.496	IO				0.67
61.250	0.00	0.15	0.495	IO				0.67
61.333	0.00	0.14	0.494	IO				0.66
61.417	0.00	0.14	0.493	IO				0.66
61.500	0.00	0.14	0.492	IO				0.66
61.583	0.00	0.14	0.491	IO				0.66
61.667	0.00	0.14	0.490	IO				0.66
61.750	0.00	0.14	0.489	IO				0.66
61.833	0.00	0.14	0.488	IO				0.66
61.917	0.00	0.14	0.487	IO				0.66
62.000	0.00	0.14	0.486	IO				0.65
62.083	0.00	0.14	0.485	IO				0.65
62.167	0.00	0.14	0.484	IO				0.65
62.250	0.00	0.14	0.483	IO				0.65
62.333	0.00	0.14	0.482	IO				0.65
62.417	0.00	0.14	0.481	IO				0.65
62.500	0.00	0.14	0.480	IO				0.65
62.583	0.00	0.14	0.479	IO				0.64
62.667	0.00	0.14	0.478	IO				0.64
62.750	0.00	0.14	0.477	IO				0.64
62.833	0.00	0.14	0.476	IO				0.64
62.917	0.00	0.14	0.475	IO				0.64
63.000	0.00	0.14	0.474	IO				0.64
63.083	0.00	0.14	0.473	IO				0.64
63.167	0.00	0.14	0.472	IO				0.64
63.250	0.00	0.14	0.471	IO				0.63
63.333	0.00	0.14	0.471	IO				0.63
63.417	0.00	0.14	0.470	IO				0.63
63.500	0.00	0.14	0.469	IO				0.63
63.583	0.00	0.14	0.468	IO				0.63
63.667	0.00	0.14	0.467	IO				0.63
63.750	0.00	0.14	0.466	IO				0.63
63.833	0.00	0.14	0.465	IO				0.63
63.917	0.00	0.14	0.464	IO				0.62
64.000	0.00	0.14	0.463	IO				0.62
64.083	0.00	0.14	0.462	IO				0.62
64.167	0.00	0.14	0.461	IO				0.62
64.250	0.00	0.14	0.460	IO				0.62
64.333	0.00	0.13	0.459	IO				0.62
64.417	0.00	0.13	0.458	IO				0.62
64.500	0.00	0.13	0.457	IO				0.62
64.583	0.00	0.13	0.456	IO				0.61
64.667	0.00	0.13	0.456	IO				0.61
64.750	0.00	0.13	0.455	IO				0.61
64.833	0.00	0.13	0.454	IO				0.61
64.917	0.00	0.13	0.453	IO				0.61
65.000	0.00	0.13	0.452	IO				0.61
65.083	0.00	0.13	0.451	IO				0.61
65.167	0.00	0.13	0.450	IO				0.61
65.250	0.00	0.13	0.449	IO				0.60
65.333	0.00	0.13	0.448	IO				0.60
65.417	0.00	0.13	0.447	IO				0.60
65.500	0.00	0.13	0.446	IO				0.60
65.583	0.00	0.13	0.446	IO				0.60
65.667	0.00	0.13	0.445	IO				0.60
65.750	0.00	0.13	0.444	IO				0.60
65.833	0.00	0.13	0.443	IO				0.60
65.917	0.00	0.13	0.442	IO				0.59
66.000	0.00	0.13	0.441	IO				0.59
66.083	0.00	0.13	0.440	IO				0.59
66.167	0.00	0.13	0.439	IO				0.59
66.250	0.00	0.13	0.438	IO				0.59

66.333	0.00	0.13	0.438	IO				0.59
66.417	0.00	0.13	0.437	IO				0.59
66.500	0.00	0.13	0.436	IO				0.59
66.583	0.00	0.13	0.435	IO				0.59
66.667	0.00	0.13	0.434	IO				0.58
66.750	0.00	0.13	0.433	IO				0.58
66.833	0.00	0.13	0.432	IO				0.58
66.917	0.00	0.13	0.431	IO				0.58
67.000	0.00	0.13	0.430	IO				0.58
67.083	0.00	0.13	0.430	IO				0.58
67.167	0.00	0.13	0.429	IO				0.58
67.250	0.00	0.13	0.428	IO				0.58
67.333	0.00	0.13	0.427	IO				0.57
67.417	0.00	0.13	0.426	IO				0.57
67.500	0.00	0.12	0.425	IO				0.57
67.583	0.00	0.12	0.424	IO				0.57
67.667	0.00	0.12	0.424	IO				0.57
67.750	0.00	0.12	0.423	IO				0.57
67.833	0.00	0.12	0.422	IO				0.57
67.917	0.00	0.12	0.421	IO				0.57
68.000	0.00	0.12	0.420	IO				0.57
68.083	0.00	0.12	0.419	IO				0.56
68.167	0.00	0.12	0.418	IO				0.56
68.250	0.00	0.12	0.418	IO				0.56
68.333	0.00	0.12	0.417	IO				0.56
68.417	0.00	0.12	0.416	IO				0.56
68.500	0.00	0.12	0.415	IO				0.56
68.583	0.00	0.12	0.414	IO				0.56
68.667	0.00	0.12	0.413	IO				0.56
68.750	0.00	0.12	0.413	IO				0.56
68.833	0.00	0.12	0.412	IO				0.55
68.917	0.00	0.12	0.411	IO				0.55
69.000	0.00	0.12	0.410	IO				0.55
69.083	0.00	0.12	0.409	IO				0.55
69.167	0.00	0.12	0.408	IO				0.55
69.250	0.00	0.12	0.408	IO				0.55
69.333	0.00	0.12	0.407	IO				0.55
69.417	0.00	0.12	0.406	IO				0.55
69.500	0.00	0.12	0.405	IO				0.55
69.583	0.00	0.12	0.404	IO				0.54
69.667	0.00	0.12	0.404	IO				0.54
69.750	0.00	0.12	0.403	IO				0.54
69.833	0.00	0.12	0.402	IO				0.54
69.917	0.00	0.12	0.401	IO				0.54
70.000	0.00	0.12	0.400	IO				0.54
70.083	0.00	0.12	0.399	IO				0.54
70.167	0.00	0.12	0.399	IO				0.54
70.250	0.00	0.12	0.398	IO				0.54
70.333	0.00	0.12	0.397	IO				0.53
70.417	0.00	0.12	0.396	IO				0.53
70.500	0.00	0.12	0.395	IO				0.53
70.583	0.00	0.12	0.395	IO				0.53
70.667	0.00	0.12	0.394	IO				0.53
70.750	0.00	0.12	0.393	IO				0.53
70.833	0.00	0.12	0.392	IO				0.53
70.917	0.00	0.11	0.391	IO				0.53
71.000	0.00	0.11	0.391	IO				0.53
71.083	0.00	0.11	0.390	IO				0.52
71.167	0.00	0.11	0.389	IO				0.52
71.250	0.00	0.11	0.388	IO				0.52
71.333	0.00	0.11	0.388	IO				0.52
71.417	0.00	0.11	0.387	IO				0.52
71.500	0.00	0.11	0.386	IO				0.52
71.583	0.00	0.11	0.385	IO				0.52
71.667	0.00	0.11	0.384	IO				0.52
71.750	0.00	0.11	0.384	IO				0.52
71.833	0.00	0.11	0.383	IO				0.52
71.917	0.00	0.11	0.382	IO				0.51
72.000	0.00	0.11	0.381	IO				0.51
72.083	0.00	0.11	0.381	IO				0.51
72.167	0.00	0.11	0.380	IO				0.51
72.250	0.00	0.11	0.379	IO				0.51
72.333	0.00	0.11	0.378	IO				0.51
72.417	0.00	0.11	0.378	IO				0.51
72.500	0.00	0.11	0.377	IO				0.51
72.583	0.00	0.11	0.376	IO				0.51
72.667	0.00	0.11	0.375	IO				0.51
72.750	0.00	0.11	0.374	IO				0.50
72.833	0.00	0.11	0.374	IO				0.50
72.917	0.00	0.11	0.373	IO				0.50
73.000	0.00	0.11	0.372	IO				0.50
73.083	0.00	0.11	0.371	IO				0.50
73.167	0.00	0.11	0.371	IO				0.50
73.250	0.00	0.11	0.370	IO				0.50
73.333	0.00	0.11	0.369	IO				0.50
73.417	0.00	0.11	0.368	IO				0.50

73.500	0.00	0.11	0.368	o	|	|	|	0.49
73.583	0.00	0.11	0.367	o	|	|	|	0.49
73.667	0.00	0.11	0.366	o	|	|	|	0.49
73.750	0.00	0.11	0.365	o	|	|	|	0.49
73.833	0.00	0.11	0.365	o	|	|	|	0.49
73.917	0.00	0.11	0.364	o	|	|	|	0.49
74.000	0.00	0.11	0.363	o	|	|	|	0.49
74.083	0.00	0.11	0.363	o	|	|	|	0.49
74.167	0.00	0.11	0.362	o	|	|	|	0.49
74.250	0.00	0.11	0.361	o	|	|	|	0.49
74.333	0.00	0.11	0.360	o	|	|	|	0.49
74.417	0.00	0.11	0.360	o	|	|	|	0.48
74.500	0.00	0.11	0.359	o	|	|	|	0.48
74.583	0.00	0.11	0.358	o	|	|	|	0.48
74.667	0.00	0.10	0.357	o	|	|	|	0.48
74.750	0.00	0.10	0.357	o	|	|	|	0.48
74.833	0.00	0.10	0.356	o	|	|	|	0.48
74.917	0.00	0.10	0.355	o	|	|	|	0.48
75.000	0.00	0.10	0.355	o	|	|	|	0.48
75.083	0.00	0.10	0.354	o	|	|	|	0.48
75.167	0.00	0.10	0.353	o	|	|	|	0.48
75.250	0.00	0.10	0.352	o	|	|	|	0.47
75.333	0.00	0.10	0.352	o	|	|	|	0.47
75.417	0.00	0.10	0.351	o	|	|	|	0.47
75.500	0.00	0.10	0.350	o	|	|	|	0.47
75.583	0.00	0.10	0.350	o	|	|	|	0.47
75.667	0.00	0.10	0.349	o	|	|	|	0.47
75.750	0.00	0.10	0.348	o	|	|	|	0.47
75.833	0.00	0.10	0.347	o	|	|	|	0.47
75.917	0.00	0.10	0.347	o	|	|	|	0.47
76.000	0.00	0.10	0.346	o	|	|	|	0.47
76.083	0.00	0.10	0.345	o	|	|	|	0.46
76.167	0.00	0.10	0.345	o	|	|	|	0.46
76.250	0.00	0.10	0.344	o	|	|	|	0.46
76.333	0.00	0.10	0.343	o	|	|	|	0.46
76.417	0.00	0.10	0.343	o	|	|	|	0.46
76.500	0.00	0.10	0.342	o	|	|	|	0.46
76.583	0.00	0.10	0.341	o	|	|	|	0.46
76.667	0.00	0.10	0.341	o	|	|	|	0.46

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 920
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.665 (CFS)
Total volume = 1.671 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro1515.rte
**********HYDROGRAPH DATA**********
Number of intervals = 17
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 39.589 (CFS)
Total volume = 1.229 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 17
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	9.9	19.79	29.69	39.59	Depth (Ft.)
0.083	1.19	0.00	0.004	O	|	|	|	|	0.01
0.167	3.58	0.01	0.021	O I	|	|	|	|	0.03
0.250	5.09	0.01	0.050	O I	|	|	|	|	0.07
0.333	6.00	0.03	0.088	O I	|	|	|	|	0.12
0.417	6.95	0.04	0.133	O I	|	|	|	|	0.18
0.500	8.32	0.05	0.185	O I	|	|	|	|	0.25
0.583	9.99	0.07	0.248	O I	|	|	|	|	0.33
0.667	12.39	0.10	0.324	O I	|	|	|	|	0.44
0.750	18.46	0.13	0.430	O I	|	|	|	|	0.58
0.833	37.07	0.18	0.620	O	I |	|	|	|	0.83
0.917	39.59	0.29	0.882	O	|	|	|	I |	1.17
1.000	16.84	0.40	1.074	O	| I	|	|	|	1.40
1.083	7.89	0.45	1.156	O I	|	|	|	|	1.51
1.167	3.25	0.46	1.192	O I	|	|	|	|	1.55
1.250	1.51	0.47	1.205	OI	|	|	|	|	1.56
1.333	0.30	0.47	1.208	O	|	|	|	|	1.57
1.417	0.07	0.47	1.206	O	|	|	|	|	1.57
1.500	0.00	0.47	1.203	O	|	|	|	|	1.56
1.583	0.00	0.47	1.199	O	|	|	|	|	1.56
1.667	0.00	0.47	1.196	O	|	|	|	|	1.55
1.750	0.00	0.47	1.193	O	|	|	|	|	1.55

1.833	0.00	0.46	1.190	o	|	|	|	|	1.55
1.917	0.00	0.46	1.187	o	|	|	|	|	1.54
2.000	0.00	0.46	1.183	o	|	|	|	|	1.54
2.083	0.00	0.46	1.180	o	|	|	|	|	1.53
2.167	0.00	0.46	1.177	o	|	|	|	|	1.53
2.250	0.00	0.46	1.174	o	|	|	|	|	1.53
2.333	0.00	0.45	1.171	o	|	|	|	|	1.52
2.417	0.00	0.45	1.168	o	|	|	|	|	1.52
2.500	0.00	0.45	1.165	o	|	|	|	|	1.52
2.583	0.00	0.45	1.162	o	|	|	|	|	1.51
2.667	0.00	0.45	1.158	o	|	|	|	|	1.51
2.750	0.00	0.44	1.155	o	|	|	|	|	1.50
2.833	0.00	0.44	1.152	o	|	|	|	|	1.50
2.917	0.00	0.44	1.149	o	|	|	|	|	1.50
3.000	0.00	0.44	1.146	o	|	|	|	|	1.49
3.083	0.00	0.44	1.143	o	|	|	|	|	1.49
3.167	0.00	0.44	1.140	o	|	|	|	|	1.49
3.250	0.00	0.43	1.137	o	|	|	|	|	1.48
3.333	0.00	0.43	1.134	o	|	|	|	|	1.48
3.417	0.00	0.43	1.131	o	|	|	|	|	1.47
3.500	0.00	0.43	1.128	o	|	|	|	|	1.47
3.583	0.00	0.43	1.125	o	|	|	|	|	1.47
3.667	0.00	0.43	1.122	o	|	|	|	|	1.46
3.750	0.00	0.43	1.119	o	|	|	|	|	1.46
3.833	0.00	0.42	1.117	o	|	|	|	|	1.46
3.917	0.00	0.42	1.114	o	|	|	|	|	1.45
4.000	0.00	0.42	1.111	o	|	|	|	|	1.45
4.083	0.00	0.42	1.108	o	|	|	|	|	1.45
4.167	0.00	0.42	1.105	o	|	|	|	|	1.44
4.250	0.00	0.42	1.102	o	|	|	|	|	1.44
4.333	0.00	0.41	1.099	o	|	|	|	|	1.44
4.417	0.00	0.41	1.096	o	|	|	|	|	1.43
4.500	0.00	0.41	1.094	o	|	|	|	|	1.43
4.583	0.00	0.41	1.091	o	|	|	|	|	1.43
4.667	0.00	0.41	1.088	o	|	|	|	|	1.42
4.750	0.00	0.41	1.085	o	|	|	|	|	1.42
4.833	0.00	0.40	1.082	o	|	|	|	|	1.41
4.917	0.00	0.40	1.080	o	|	|	|	|	1.41
5.000	0.00	0.40	1.077	o	|	|	|	|	1.41
5.083	0.00	0.40	1.074	o	|	|	|	|	1.40
5.167	0.00	0.40	1.071	o	|	|	|	|	1.40
5.250	0.00	0.40	1.069	o	|	|	|	|	1.40
5.333	0.00	0.40	1.066	o	|	|	|	|	1.39
5.417	0.00	0.39	1.063	o	|	|	|	|	1.39
5.500	0.00	0.39	1.060	o	|	|	|	|	1.39
5.583	0.00	0.39	1.058	o	|	|	|	|	1.38
5.667	0.00	0.39	1.055	o	|	|	|	|	1.38
5.750	0.00	0.39	1.052	o	|	|	|	|	1.38
5.833	0.00	0.39	1.050	o	|	|	|	|	1.37
5.917	0.00	0.39	1.047	o	|	|	|	|	1.37
6.000	0.00	0.38	1.044	o	|	|	|	|	1.37
6.083	0.00	0.38	1.042	o	|	|	|	|	1.37
6.167	0.00	0.38	1.039	o	|	|	|	|	1.36
6.250	0.00	0.38	1.036	o	|	|	|	|	1.36
6.333	0.00	0.38	1.034	o	|	|	|	|	1.36
6.417	0.00	0.38	1.031	o	|	|	|	|	1.35
6.500	0.00	0.38	1.029	o	|	|	|	|	1.35
6.583	0.00	0.37	1.026	o	|	|	|	|	1.35
6.667	0.00	0.37	1.024	o	|	|	|	|	1.34
6.750	0.00	0.37	1.021	o	|	|	|	|	1.34
6.833	0.00	0.37	1.018	o	|	|	|	|	1.34
6.917	0.00	0.37	1.016	o	|	|	|	|	1.33
7.000	0.00	0.37	1.013	o	|	|	|	|	1.33
7.083	0.00	0.37	1.011	o	|	|	|	|	1.33
7.167	0.00	0.36	1.008	o	|	|	|	|	1.32
7.250	0.00	0.36	1.006	o	|	|	|	|	1.32
7.333	0.00	0.36	1.003	o	|	|	|	|	1.32
7.417	0.00	0.36	1.001	o	|	|	|	|	1.32
7.500	0.00	0.36	0.998	o	|	|	|	|	1.31
7.583	0.00	0.36	0.996	o	|	|	|	|	1.31
7.667	0.00	0.36	0.993	o	|	|	|	|	1.31
7.750	0.00	0.35	0.991	o	|	|	|	|	1.30
7.833	0.00	0.35	0.989	o	|	|	|	|	1.30
7.917	0.00	0.35	0.986	o	|	|	|	|	1.30
8.000	0.00	0.35	0.984	o	|	|	|	|	1.29
8.083	0.00	0.35	0.981	o	|	|	|	|	1.29
8.167	0.00	0.35	0.979	o	|	|	|	|	1.29
8.250	0.00	0.35	0.977	o	|	|	|	|	1.29
8.333	0.00	0.35	0.974	o	|	|	|	|	1.28
8.417	0.00	0.34	0.972	o	|	|	|	|	1.28
8.500	0.00	0.34	0.969	o	|	|	|	|	1.28
8.583	0.00	0.34	0.967	o	|	|	|	|	1.27
8.667	0.00	0.34	0.965	o	|	|	|	|	1.27
8.750	0.00	0.34	0.962	o	|	|	|	|	1.27
8.833	0.00	0.34	0.960	o	|	|	|	|	1.27
8.917	0.00	0.34	0.958	o	|	|	|	|	1.26

9.000	0.00	0.33	0.955	o	|	|	|	|	1.26
9.083	0.00	0.33	0.953	o	|	|	|	|	1.26
9.167	0.00	0.33	0.951	o	|	|	|	|	1.25
9.250	0.00	0.33	0.949	o	|	|	|	|	1.25
9.333	0.00	0.33	0.946	o	|	|	|	|	1.25
9.417	0.00	0.33	0.944	o	|	|	|	|	1.25
9.500	0.00	0.33	0.942	o	|	|	|	|	1.24
9.583	0.00	0.33	0.939	o	|	|	|	|	1.24
9.667	0.00	0.32	0.937	o	|	|	|	|	1.24
9.750	0.00	0.32	0.935	o	|	|	|	|	1.23
9.833	0.00	0.32	0.933	o	|	|	|	|	1.23
9.917	0.00	0.32	0.931	o	|	|	|	|	1.23
10.000	0.00	0.32	0.928	o	|	|	|	|	1.23
10.083	0.00	0.32	0.926	o	|	|	|	|	1.22
10.167	0.00	0.32	0.924	o	|	|	|	|	1.22
10.250	0.00	0.32	0.922	o	|	|	|	|	1.22
10.333	0.00	0.32	0.920	o	|	|	|	|	1.22
10.417	0.00	0.31	0.917	o	|	|	|	|	1.21
10.500	0.00	0.31	0.915	o	|	|	|	|	1.21
10.583	0.00	0.31	0.913	o	|	|	|	|	1.21
10.667	0.00	0.31	0.911	o	|	|	|	|	1.21
10.750	0.00	0.31	0.909	o	|	|	|	|	1.20
10.833	0.00	0.31	0.907	o	|	|	|	|	1.20
10.917	0.00	0.31	0.905	o	|	|	|	|	1.20
11.000	0.00	0.31	0.902	o	|	|	|	|	1.19
11.083	0.00	0.30	0.900	o	|	|	|	|	1.19
11.167	0.00	0.30	0.898	o	|	|	|	|	1.19
11.250	0.00	0.30	0.896	o	|	|	|	|	1.19
11.333	0.00	0.30	0.894	o	|	|	|	|	1.18
11.417	0.00	0.30	0.892	o	|	|	|	|	1.18
11.500	0.00	0.30	0.890	o	|	|	|	|	1.18
11.583	0.00	0.30	0.888	o	|	|	|	|	1.18
11.667	0.00	0.30	0.886	o	|	|	|	|	1.17
11.750	0.00	0.30	0.884	o	|	|	|	|	1.17
11.833	0.00	0.29	0.882	o	|	|	|	|	1.17
11.917	0.00	0.29	0.880	o	|	|	|	|	1.17
12.000	0.00	0.29	0.878	o	|	|	|	|	1.16
12.083	0.00	0.29	0.876	o	|	|	|	|	1.16
12.167	0.00	0.29	0.874	o	|	|	|	|	1.16
12.250	0.00	0.29	0.872	o	|	|	|	|	1.16
12.333	0.00	0.29	0.870	o	|	|	|	|	1.16
12.417	0.00	0.29	0.868	o	|	|	|	|	1.15
12.500	0.00	0.29	0.866	o	|	|	|	|	1.15
12.583	0.00	0.28	0.864	o	|	|	|	|	1.15
12.667	0.00	0.28	0.862	o	|	|	|	|	1.15
12.750	0.00	0.28	0.860	o	|	|	|	|	1.14
12.833	0.00	0.28	0.858	o	|	|	|	|	1.14
12.917	0.00	0.28	0.856	o	|	|	|	|	1.14
13.000	0.00	0.28	0.854	o	|	|	|	|	1.14
13.083	0.00	0.28	0.852	o	|	|	|	|	1.13
13.167	0.00	0.28	0.850	o	|	|	|	|	1.13
13.250	0.00	0.28	0.848	o	|	|	|	|	1.13
13.333	0.00	0.27	0.847	o	|	|	|	|	1.13
13.417	0.00	0.27	0.845	o	|	|	|	|	1.12
13.500	0.00	0.27	0.843	o	|	|	|	|	1.12
13.583	0.00	0.27	0.841	o	|	|	|	|	1.12
13.667	0.00	0.27	0.839	o	|	|	|	|	1.12
13.750	0.00	0.27	0.837	o	|	|	|	|	1.12
13.833	0.00	0.27	0.835	o	|	|	|	|	1.11
13.917	0.00	0.27	0.833	o	|	|	|	|	1.11
14.000	0.00	0.27	0.832	o	|	|	|	|	1.11
14.083	0.00	0.27	0.830	o	|	|	|	|	1.11
14.167	0.00	0.26	0.828	o	|	|	|	|	1.10
14.250	0.00	0.26	0.826	o	|	|	|	|	1.10
14.333	0.00	0.26	0.824	o	|	|	|	|	1.10
14.417	0.00	0.26	0.823	o	|	|	|	|	1.10
14.500	0.00	0.26	0.821	o	|	|	|	|	1.10
14.583	0.00	0.26	0.819	o	|	|	|	|	1.09
14.667	0.00	0.26	0.817	o	|	|	|	|	1.09
14.750	0.00	0.26	0.815	o	|	|	|	|	1.09
14.833	0.00	0.26	0.814	o	|	|	|	|	1.09
14.917	0.00	0.26	0.812	o	|	|	|	|	1.08
15.000	0.00	0.25	0.810	o	|	|	|	|	1.08
15.083	0.00	0.25	0.808	o	|	|	|	|	1.08
15.167	0.00	0.25	0.807	o	|	|	|	|	1.08
15.250	0.00	0.25	0.805	o	|	|	|	|	1.08
15.333	0.00	0.25	0.803	o	|	|	|	|	1.07
15.417	0.00	0.25	0.801	o	|	|	|	|	1.07
15.500	0.00	0.25	0.800	o	|	|	|	|	1.07
15.583	0.00	0.25	0.798	o	|	|	|	|	1.07
15.667	0.00	0.25	0.796	o	|	|	|	|	1.07
15.750	0.00	0.25	0.795	o	|	|	|	|	1.06
15.833	0.00	0.25	0.793	o	|	|	|	|	1.06
15.917	0.00	0.24	0.791	o	|	|	|	|	1.06
16.000	0.00	0.24	0.789	o	|	|	|	|	1.06
16.083	0.00	0.24	0.788	o	|	|	|	|	1.05

16.167	0.00	0.24	0.786	o	|	|	|	|	1.05
16.250	0.00	0.24	0.784	o	|	|	|	|	1.05
16.333	0.00	0.24	0.783	o	|	|	|	|	1.05
16.417	0.00	0.24	0.781	o	|	|	|	|	1.05
16.500	0.00	0.24	0.780	o	|	|	|	|	1.04
16.583	0.00	0.24	0.778	o	|	|	|	|	1.04
16.667	0.00	0.24	0.776	o	|	|	|	|	1.04
16.750	0.00	0.24	0.775	o	|	|	|	|	1.04
16.833	0.00	0.23	0.773	o	|	|	|	|	1.04
16.917	0.00	0.23	0.771	o	|	|	|	|	1.03
17.000	0.00	0.23	0.770	o	|	|	|	|	1.03
17.083	0.00	0.23	0.768	o	|	|	|	|	1.03
17.167	0.00	0.23	0.767	o	|	|	|	|	1.03
17.250	0.00	0.23	0.765	o	|	|	|	|	1.03
17.333	0.00	0.23	0.763	o	|	|	|	|	1.02
17.417	0.00	0.23	0.762	o	|	|	|	|	1.02
17.500	0.00	0.23	0.760	o	|	|	|	|	1.02
17.583	0.00	0.23	0.759	o	|	|	|	|	1.02
17.667	0.00	0.23	0.757	o	|	|	|	|	1.02
17.750	0.00	0.22	0.756	o	|	|	|	|	1.02
17.833	0.00	0.22	0.754	o	|	|	|	|	1.01
17.917	0.00	0.22	0.753	o	|	|	|	|	1.01
18.000	0.00	0.22	0.751	o	|	|	|	|	1.01
18.083	0.00	0.22	0.749	o	|	|	|	|	1.01
18.167	0.00	0.22	0.748	o	|	|	|	|	1.01
18.250	0.00	0.22	0.746	o	|	|	|	|	1.00
18.333	0.00	0.22	0.745	o	|	|	|	|	1.00
18.417	0.00	0.22	0.743	o	|	|	|	|	1.00
18.500	0.00	0.22	0.742	o	|	|	|	|	1.00
18.583	0.00	0.22	0.740	o	|	|	|	|	1.00
18.667	0.00	0.22	0.739	o	|	|	|	|	0.99
18.750	0.00	0.22	0.737	o	|	|	|	|	0.99
18.833	0.00	0.22	0.736	o	|	|	|	|	0.99
18.917	0.00	0.22	0.734	o	|	|	|	|	0.99
19.000	0.00	0.22	0.733	o	|	|	|	|	0.99
19.083	0.00	0.21	0.731	o	|	|	|	|	0.98
19.167	0.00	0.21	0.730	o	|	|	|	|	0.98
19.250	0.00	0.21	0.729	o	|	|	|	|	0.98
19.333	0.00	0.21	0.727	o	|	|	|	|	0.98
19.417	0.00	0.21	0.726	o	|	|	|	|	0.98
19.500	0.00	0.21	0.724	o	|	|	|	|	0.97
19.583	0.00	0.21	0.723	o	|	|	|	|	0.97
19.667	0.00	0.21	0.721	o	|	|	|	|	0.97
19.750	0.00	0.21	0.720	o	|	|	|	|	0.97
19.833	0.00	0.21	0.718	o	|	|	|	|	0.97
19.917	0.00	0.21	0.717	o	|	|	|	|	0.96
20.000	0.00	0.21	0.715	o	|	|	|	|	0.96
20.083	0.00	0.21	0.714	o	|	|	|	|	0.96
20.167	0.00	0.21	0.713	o	|	|	|	|	0.96
20.250	0.00	0.21	0.711	o	|	|	|	|	0.96
20.333	0.00	0.21	0.710	o	|	|	|	|	0.96
20.417	0.00	0.21	0.708	o	|	|	|	|	0.95
20.500	0.00	0.21	0.707	o	|	|	|	|	0.95
20.583	0.00	0.21	0.705	o	|	|	|	|	0.95
20.667	0.00	0.21	0.704	o	|	|	|	|	0.95
20.750	0.00	0.21	0.703	o	|	|	|	|	0.95
20.833	0.00	0.21	0.701	o	|	|	|	|	0.94
20.917	0.00	0.21	0.700	o	|	|	|	|	0.94
21.000	0.00	0.20	0.698	o	|	|	|	|	0.94
21.083	0.00	0.20	0.697	o	|	|	|	|	0.94
21.167	0.00	0.20	0.695	o	|	|	|	|	0.94
21.250	0.00	0.20	0.694	o	|	|	|	|	0.93
21.333	0.00	0.20	0.693	o	|	|	|	|	0.93
21.417	0.00	0.20	0.691	o	|	|	|	|	0.93
21.500	0.00	0.20	0.690	o	|	|	|	|	0.93
21.583	0.00	0.20	0.688	o	|	|	|	|	0.93
21.667	0.00	0.20	0.687	o	|	|	|	|	0.92
21.750	0.00	0.20	0.686	o	|	|	|	|	0.92
21.833	0.00	0.20	0.684	o	|	|	|	|	0.92
21.917	0.00	0.20	0.683	o	|	|	|	|	0.92
22.000	0.00	0.20	0.682	o	|	|	|	|	0.92
22.083	0.00	0.20	0.680	o	|	|	|	|	0.92
22.167	0.00	0.20	0.679	o	|	|	|	|	0.91
22.250	0.00	0.20	0.677	o	|	|	|	|	0.91
22.333	0.00	0.20	0.676	o	|	|	|	|	0.91
22.417	0.00	0.20	0.675	o	|	|	|	|	0.91
22.500	0.00	0.20	0.673	o	|	|	|	|	0.91
22.583	0.00	0.20	0.672	o	|	|	|	|	0.90
22.667	0.00	0.20	0.671	o	|	|	|	|	0.90
22.750	0.00	0.20	0.669	o	|	|	|	|	0.90
22.833	0.00	0.20	0.668	o	|	|	|	|	0.90
22.917	0.00	0.20	0.667	o	|	|	|	|	0.90
23.000	0.00	0.20	0.665	o	|	|	|	|	0.90
23.083	0.00	0.19	0.664	o	|	|	|	|	0.89
23.167	0.00	0.19	0.663	o	|	|	|	|	0.89
23.250	0.00	0.19	0.661	o	|	|	|	|	0.89

23.333	0.00	0.19	0.660	o	|	|	|	|	0.89
23.417	0.00	0.19	0.659	o	|	|	|	|	0.89
23.500	0.00	0.19	0.657	o	|	|	|	|	0.88
23.583	0.00	0.19	0.656	o	|	|	|	|	0.88
23.667	0.00	0.19	0.655	o	|	|	|	|	0.88
23.750	0.00	0.19	0.653	o	|	|	|	|	0.88
23.833	0.00	0.19	0.652	o	|	|	|	|	0.88
23.917	0.00	0.19	0.651	o	|	|	|	|	0.88
24.000	0.00	0.19	0.649	o	|	|	|	|	0.87
24.083	0.00	0.19	0.648	o	|	|	|	|	0.87
24.167	0.00	0.19	0.647	o	|	|	|	|	0.87
24.250	0.00	0.19	0.645	o	|	|	|	|	0.87
24.333	0.00	0.19	0.644	o	|	|	|	|	0.87
24.417	0.00	0.19	0.643	o	|	|	|	|	0.87
24.500	0.00	0.19	0.641	o	|	|	|	|	0.86
24.583	0.00	0.19	0.640	o	|	|	|	|	0.86
24.667	0.00	0.19	0.639	o	|	|	|	|	0.86
24.750	0.00	0.19	0.638	o	|	|	|	|	0.86
24.833	0.00	0.19	0.636	o	|	|	|	|	0.86
24.917	0.00	0.19	0.635	o	|	|	|	|	0.85
25.000	0.00	0.19	0.634	o	|	|	|	|	0.85
25.083	0.00	0.19	0.632	o	|	|	|	|	0.85
25.167	0.00	0.19	0.631	o	|	|	|	|	0.85
25.250	0.00	0.18	0.630	o	|	|	|	|	0.85
25.333	0.00	0.18	0.629	o	|	|	|	|	0.85
25.417	0.00	0.18	0.627	o	|	|	|	|	0.84
25.500	0.00	0.18	0.626	o	|	|	|	|	0.84
25.583	0.00	0.18	0.625	o	|	|	|	|	0.84
25.667	0.00	0.18	0.624	o	|	|	|	|	0.84
25.750	0.00	0.18	0.622	o	|	|	|	|	0.84
25.833	0.00	0.18	0.621	o	|	|	|	|	0.84
25.917	0.00	0.18	0.620	o	|	|	|	|	0.83
26.000	0.00	0.18	0.619	o	|	|	|	|	0.83
26.083	0.00	0.18	0.617	o	|	|	|	|	0.83
26.167	0.00	0.18	0.616	o	|	|	|	|	0.83
26.250	0.00	0.18	0.615	o	|	|	|	|	0.83
26.333	0.00	0.18	0.614	o	|	|	|	|	0.83
26.417	0.00	0.18	0.612	o	|	|	|	|	0.82
26.500	0.00	0.18	0.611	o	|	|	|	|	0.82
26.583	0.00	0.18	0.610	o	|	|	|	|	0.82
26.667	0.00	0.18	0.609	o	|	|	|	|	0.82
26.750	0.00	0.18	0.607	o	|	|	|	|	0.82
26.833	0.00	0.18	0.606	o	|	|	|	|	0.82
26.917	0.00	0.18	0.605	o	|	|	|	|	0.81
27.000	0.00	0.18	0.604	o	|	|	|	|	0.81
27.083	0.00	0.18	0.603	o	|	|	|	|	0.81
27.167	0.00	0.18	0.601	o	|	|	|	|	0.81
27.250	0.00	0.18	0.600	o	|	|	|	|	0.81
27.333	0.00	0.18	0.599	o	|	|	|	|	0.81
27.417	0.00	0.18	0.598	o	|	|	|	|	0.80
27.500	0.00	0.18	0.596	o	|	|	|	|	0.80
27.583	0.00	0.17	0.595	o	|	|	|	|	0.80
27.667	0.00	0.17	0.594	o	|	|	|	|	0.80
27.750	0.00	0.17	0.593	o	|	|	|	|	0.80
27.833	0.00	0.17	0.592	o	|	|	|	|	0.80
27.917	0.00	0.17	0.590	o	|	|	|	|	0.79
28.000	0.00	0.17	0.589	o	|	|	|	|	0.79
28.083	0.00	0.17	0.588	o	|	|	|	|	0.79
28.167	0.00	0.17	0.587	o	|	|	|	|	0.79
28.250	0.00	0.17	0.586	o	|	|	|	|	0.79
28.333	0.00	0.17	0.585	o	|	|	|	|	0.79
28.417	0.00	0.17	0.583	o	|	|	|	|	0.79
28.500	0.00	0.17	0.582	o	|	|	|	|	0.78
28.583	0.00	0.17	0.581	o	|	|	|	|	0.78
28.667	0.00	0.17	0.580	o	|	|	|	|	0.78
28.750	0.00	0.17	0.579	o	|	|	|	|	0.78
28.833	0.00	0.17	0.577	o	|	|	|	|	0.78
28.917	0.00	0.17	0.576	o	|	|	|	|	0.78
29.000	0.00	0.17	0.575	o	|	|	|	|	0.77
29.083	0.00	0.17	0.574	o	|	|	|	|	0.77
29.167	0.00	0.17	0.573	o	|	|	|	|	0.77
29.250	0.00	0.17	0.572	o	|	|	|	|	0.77
29.333	0.00	0.17	0.571	o	|	|	|	|	0.77
29.417	0.00	0.17	0.569	o	|	|	|	|	0.77
29.500	0.00	0.17	0.568	o	|	|	|	|	0.76
29.583	0.00	0.17	0.567	o	|	|	|	|	0.76
29.667	0.00	0.17	0.566	o	|	|	|	|	0.76
29.750	0.00	0.17	0.565	o	|	|	|	|	0.76
29.833	0.00	0.17	0.564	o	|	|	|	|	0.76
29.917	0.00	0.17	0.563	o	|	|	|	|	0.76
30.000	0.00	0.16	0.561	o	|	|	|	|	0.76
30.083	0.00	0.16	0.560	o	|	|	|	|	0.75
30.167	0.00	0.16	0.559	o	|	|	|	|	0.75
30.250	0.00	0.16	0.558	o	|	|	|	|	0.75
30.333	0.00	0.16	0.557	o	|	|	|	|	0.75
30.417	0.00	0.16	0.556	o	|	|	|	|	0.75

30.500	0.00	0.16	0.555	o	|	|	|	|	0.75
30.583	0.00	0.16	0.553	o	|	|	|	|	0.74
30.667	0.00	0.16	0.552	o	|	|	|	|	0.74
30.750	0.00	0.16	0.551	o	|	|	|	|	0.74
30.833	0.00	0.16	0.550	o	|	|	|	|	0.74
30.917	0.00	0.16	0.549	o	|	|	|	|	0.74
31.000	0.00	0.16	0.548	o	|	|	|	|	0.74
31.083	0.00	0.16	0.547	o	|	|	|	|	0.74
31.167	0.00	0.16	0.546	o	|	|	|	|	0.73
31.250	0.00	0.16	0.545	o	|	|	|	|	0.73
31.333	0.00	0.16	0.544	o	|	|	|	|	0.73
31.417	0.00	0.16	0.542	o	|	|	|	|	0.73
31.500	0.00	0.16	0.541	o	|	|	|	|	0.73
31.583	0.00	0.16	0.540	o	|	|	|	|	0.73
31.667	0.00	0.16	0.539	o	|	|	|	|	0.73
31.750	0.00	0.16	0.538	o	|	|	|	|	0.72
31.833	0.00	0.16	0.537	o	|	|	|	|	0.72
31.917	0.00	0.16	0.536	o	|	|	|	|	0.72
32.000	0.00	0.16	0.535	o	|	|	|	|	0.72
32.083	0.00	0.16	0.534	o	|	|	|	|	0.72
32.167	0.00	0.16	0.533	o	|	|	|	|	0.72
32.250	0.00	0.16	0.532	o	|	|	|	|	0.72
32.333	0.00	0.16	0.530	o	|	|	|	|	0.71
32.417	0.00	0.16	0.529	o	|	|	|	|	0.71
32.500	0.00	0.16	0.528	o	|	|	|	|	0.71
32.583	0.00	0.15	0.527	o	|	|	|	|	0.71
32.667	0.00	0.15	0.526	o	|	|	|	|	0.71
32.750	0.00	0.15	0.525	o	|	|	|	|	0.71
32.833	0.00	0.15	0.524	o	|	|	|	|	0.71
32.917	0.00	0.15	0.523	o	|	|	|	|	0.70
33.000	0.00	0.15	0.522	o	|	|	|	|	0.70
33.083	0.00	0.15	0.521	o	|	|	|	|	0.70
33.167	0.00	0.15	0.520	o	|	|	|	|	0.70
33.250	0.00	0.15	0.519	o	|	|	|	|	0.70
33.333	0.00	0.15	0.518	o	|	|	|	|	0.70
33.417	0.00	0.15	0.517	o	|	|	|	|	0.70
33.500	0.00	0.15	0.516	o	|	|	|	|	0.69
33.583	0.00	0.15	0.515	o	|	|	|	|	0.69
33.667	0.00	0.15	0.514	o	|	|	|	|	0.69
33.750	0.00	0.15	0.513	o	|	|	|	|	0.69
33.833	0.00	0.15	0.512	o	|	|	|	|	0.69
33.917	0.00	0.15	0.511	o	|	|	|	|	0.69
34.000	0.00	0.15	0.509	o	|	|	|	|	0.69
34.083	0.00	0.15	0.508	o	|	|	|	|	0.68
34.167	0.00	0.15	0.507	o	|	|	|	|	0.68
34.250	0.00	0.15	0.506	o	|	|	|	|	0.68
34.333	0.00	0.15	0.505	o	|	|	|	|	0.68
34.417	0.00	0.15	0.504	o	|	|	|	|	0.68
34.500	0.00	0.15	0.503	o	|	|	|	|	0.68
34.583	0.00	0.15	0.502	o	|	|	|	|	0.68
34.667	0.00	0.15	0.501	o	|	|	|	|	0.67
34.750	0.00	0.15	0.500	o	|	|	|	|	0.67
34.833	0.00	0.15	0.499	o	|	|	|	|	0.67
34.917	0.00	0.15	0.498	o	|	|	|	|	0.67
35.000	0.00	0.15	0.497	o	|	|	|	|	0.67
35.083	0.00	0.15	0.496	o	|	|	|	|	0.67
35.167	0.00	0.15	0.495	o	|	|	|	|	0.67
35.250	0.00	0.15	0.494	o	|	|	|	|	0.67
35.333	0.00	0.14	0.493	o	|	|	|	|	0.66
35.417	0.00	0.14	0.492	o	|	|	|	|	0.66
35.500	0.00	0.14	0.491	o	|	|	|	|	0.66
35.583	0.00	0.14	0.490	o	|	|	|	|	0.66
35.667	0.00	0.14	0.489	o	|	|	|	|	0.66
35.750	0.00	0.14	0.488	o	|	|	|	|	0.66
35.833	0.00	0.14	0.487	o	|	|	|	|	0.66
35.917	0.00	0.14	0.486	o	|	|	|	|	0.65
36.000	0.00	0.14	0.485	o	|	|	|	|	0.65
36.083	0.00	0.14	0.484	o	|	|	|	|	0.65
36.167	0.00	0.14	0.483	o	|	|	|	|	0.65
36.250	0.00	0.14	0.482	o	|	|	|	|	0.65
36.333	0.00	0.14	0.481	o	|	|	|	|	0.65
36.417	0.00	0.14	0.480	o	|	|	|	|	0.65
36.500	0.00	0.14	0.480	o	|	|	|	|	0.65
36.583	0.00	0.14	0.479	o	|	|	|	|	0.64
36.667	0.00	0.14	0.478	o	|	|	|	|	0.64
36.750	0.00	0.14	0.477	o	|	|	|	|	0.64
36.833	0.00	0.14	0.476	o	|	|	|	|	0.64
36.917	0.00	0.14	0.475	o	|	|	|	|	0.64
37.000	0.00	0.14	0.474	o	|	|	|	|	0.64
37.083	0.00	0.14	0.473	o	|	|	|	|	0.64
37.167	0.00	0.14	0.472	o	|	|	|	|	0.64
37.250	0.00	0.14	0.471	o	|	|	|	|	0.63
37.333	0.00	0.14	0.470	o	|	|	|	|	0.63
37.417	0.00	0.14	0.469	o	|	|	|	|	0.63
37.500	0.00	0.14	0.468	o	|	|	|	|	0.63
37.583	0.00	0.14	0.467	o	|	|	|	|	0.63

37.667	0.00	0.14	0.466	o	|	|	|	|	0.63
37.750	0.00	0.14	0.465	o	|	|	|	|	0.63
37.833	0.00	0.14	0.464	o	|	|	|	|	0.62
37.917	0.00	0.14	0.463	o	|	|	|	|	0.62
38.000	0.00	0.14	0.462	o	|	|	|	|	0.62
38.083	0.00	0.14	0.461	o	|	|	|	|	0.62
38.167	0.00	0.14	0.461	o	|	|	|	|	0.62
38.250	0.00	0.13	0.460	o	|	|	|	|	0.62
38.333	0.00	0.13	0.459	o	|	|	|	|	0.62
38.417	0.00	0.13	0.458	o	|	|	|	|	0.62
38.500	0.00	0.13	0.457	o	|	|	|	|	0.61
38.583	0.00	0.13	0.456	o	|	|	|	|	0.61
38.667	0.00	0.13	0.455	o	|	|	|	|	0.61
38.750	0.00	0.13	0.454	o	|	|	|	|	0.61
38.833	0.00	0.13	0.453	o	|	|	|	|	0.61
38.917	0.00	0.13	0.452	o	|	|	|	|	0.61
39.000	0.00	0.13	0.451	o	|	|	|	|	0.61
39.083	0.00	0.13	0.450	o	|	|	|	|	0.61
39.167	0.00	0.13	0.449	o	|	|	|	|	0.60
39.250	0.00	0.13	0.449	o	|	|	|	|	0.60
39.333	0.00	0.13	0.448	o	|	|	|	|	0.60
39.417	0.00	0.13	0.447	o	|	|	|	|	0.60
39.500	0.00	0.13	0.446	o	|	|	|	|	0.60
39.583	0.00	0.13	0.445	o	|	|	|	|	0.60
39.667	0.00	0.13	0.444	o	|	|	|	|	0.60
39.750	0.00	0.13	0.443	o	|	|	|	|	0.60
39.833	0.00	0.13	0.442	o	|	|	|	|	0.60
39.917	0.00	0.13	0.441	o	|	|	|	|	0.59
40.000	0.00	0.13	0.440	o	|	|	|	|	0.59
40.083	0.00	0.13	0.440	o	|	|	|	|	0.59
40.167	0.00	0.13	0.439	o	|	|	|	|	0.59
40.250	0.00	0.13	0.438	o	|	|	|	|	0.59
40.333	0.00	0.13	0.437	o	|	|	|	|	0.59
40.417	0.00	0.13	0.436	o	|	|	|	|	0.59
40.500	0.00	0.13	0.435	o	|	|	|	|	0.59
40.583	0.00	0.13	0.434	o	|	|	|	|	0.58
40.667	0.00	0.13	0.433	o	|	|	|	|	0.58
40.750	0.00	0.13	0.433	o	|	|	|	|	0.58
40.833	0.00	0.13	0.432	o	|	|	|	|	0.58
40.917	0.00	0.13	0.431	o	|	|	|	|	0.58
41.000	0.00	0.13	0.430	o	|	|	|	|	0.58
41.083	0.00	0.13	0.429	o	|	|	|	|	0.58
41.167	0.00	0.13	0.428	o	|	|	|	|	0.58
41.250	0.00	0.13	0.427	o	|	|	|	|	0.58
41.333	0.00	0.13	0.426	o	|	|	|	|	0.57
41.417	0.00	0.12	0.426	o	|	|	|	|	0.57
41.500	0.00	0.12	0.425	o	|	|	|	|	0.57
41.583	0.00	0.12	0.424	o	|	|	|	|	0.57
41.667	0.00	0.12	0.423	o	|	|	|	|	0.57
41.750	0.00	0.12	0.422	o	|	|	|	|	0.57
41.833	0.00	0.12	0.421	o	|	|	|	|	0.57
41.917	0.00	0.12	0.420	o	|	|	|	|	0.57
42.000	0.00	0.12	0.420	o	|	|	|	|	0.56
42.083	0.00	0.12	0.419	o	|	|	|	|	0.56
42.167	0.00	0.12	0.418	o	|	|	|	|	0.56
42.250	0.00	0.12	0.417	o	|	|	|	|	0.56
42.333	0.00	0.12	0.416	o	|	|	|	|	0.56
42.417	0.00	0.12	0.415	o	|	|	|	|	0.56
42.500	0.00	0.12	0.415	o	|	|	|	|	0.56
42.583	0.00	0.12	0.414	o	|	|	|	|	0.56
42.667	0.00	0.12	0.413	o	|	|	|	|	0.56
42.750	0.00	0.12	0.412	o	|	|	|	|	0.55
42.833	0.00	0.12	0.411	o	|	|	|	|	0.55
42.917	0.00	0.12	0.410	o	|	|	|	|	0.55
43.000	0.00	0.12	0.410	o	|	|	|	|	0.55
43.083	0.00	0.12	0.409	o	|	|	|	|	0.55
43.167	0.00	0.12	0.408	o	|	|	|	|	0.55
43.250	0.00	0.12	0.407	o	|	|	|	|	0.55
43.333	0.00	0.12	0.406	o	|	|	|	|	0.55
43.417	0.00	0.12	0.405	o	|	|	|	|	0.55
43.500	0.00	0.12	0.405	o	|	|	|	|	0.54
43.583	0.00	0.12	0.404	o	|	|	|	|	0.54
43.667	0.00	0.12	0.403	o	|	|	|	|	0.54
43.750	0.00	0.12	0.402	o	|	|	|	|	0.54
43.833	0.00	0.12	0.401	o	|	|	|	|	0.54
43.917	0.00	0.12	0.401	o	|	|	|	|	0.54
44.000	0.00	0.12	0.400	o	|	|	|	|	0.54
44.083	0.00	0.12	0.399	o	|	|	|	|	0.54
44.167	0.00	0.12	0.398	o	|	|	|	|	0.54
44.250	0.00	0.12	0.397	o	|	|	|	|	0.53
44.333	0.00	0.12	0.397	o	|	|	|	|	0.53
44.417	0.00	0.12	0.396	o	|	|	|	|	0.53
44.500	0.00	0.12	0.395	o	|	|	|	|	0.53
44.583	0.00	0.12	0.394	o	|	|	|	|	0.53
44.667	0.00	0.12	0.393	o	|	|	|	|	0.53
44.750	0.00	0.12	0.393	o	|	|	|	|	0.53

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44.833    0.00    0.11      0.392  o       |       |       |       |     0.53
44.917    0.00    0.11      0.391  o       |       |       |       |     0.53
45.000    0.00    0.11      0.390  o       |       |       |       |     0.53
45.083    0.00    0.11      0.389  o       |       |       |       |     0.52
45.167    0.00    0.11      0.389  o       |       |       |       |     0.52
45.250    0.00    0.11      0.388  o       |       |       |       |     0.52
45.333    0.00    0.11      0.387  o       |       |       |       |     0.52
45.417    0.00    0.11      0.386  o       |       |       |       |     0.52
45.500    0.00    0.11      0.385  o       |       |       |       |     0.52
45.583    0.00    0.11      0.385  o       |       |       |       |     0.52
45.667    0.00    0.11      0.384  o       |       |       |       |     0.52
45.750    0.00    0.11      0.383  o       |       |       |       |     0.52
45.833    0.00    0.11      0.382  o       |       |       |       |     0.51
45.917    0.00    0.11      0.382  o       |       |       |       |     0.51
46.000    0.00    0.11      0.381  o       |       |       |       |     0.51
46.083    0.00    0.11      0.380  o       |       |       |       |     0.51
46.167    0.00    0.11      0.379  o       |       |       |       |     0.51
46.250    0.00    0.11      0.379  o       |       |       |       |     0.51
46.333    0.00    0.11      0.378  o       |       |       |       |     0.51
46.417    0.00    0.11      0.377  o       |       |       |       |     0.51
46.500    0.00    0.11      0.376  o       |       |       |       |     0.51
46.583    0.00    0.11      0.375  o       |       |       |       |     0.51
46.667    0.00    0.11      0.375  o       |       |       |       |     0.50
46.750    0.00    0.11      0.374  o       |       |       |       |     0.50
46.833    0.00    0.11      0.373  o       |       |       |       |     0.50
46.917    0.00    0.11      0.372  o       |       |       |       |     0.50
47.000    0.00    0.11      0.372  o       |       |       |       |     0.50
47.083    0.00    0.11      0.371  o       |       |       |       |     0.50
47.167    0.00    0.11      0.370  o       |       |       |       |     0.50
47.250    0.00    0.11      0.369  o       |       |       |       |     0.50
47.333    0.00    0.11      0.369  o       |       |       |       |     0.50
47.417    0.00    0.11      0.368  o       |       |       |       |     0.50
47.500    0.00    0.11      0.367  o       |       |       |       |     0.49
47.583    0.00    0.11      0.367  o       |       |       |       |     0.49
47.667    0.00    0.11      0.366  o       |       |       |       |     0.49
47.750    0.00    0.11      0.365  o       |       |       |       |     0.49
47.833    0.00    0.11      0.364  o       |       |       |       |     0.49
47.917    0.00    0.11      0.364  o       |       |       |       |     0.49
48.000    0.00    0.11      0.363  o       |       |       |       |     0.49
48.083    0.00    0.11      0.362  o       |       |       |       |     0.49
48.167    0.00    0.11      0.361  o       |       |       |       |     0.49
48.250    0.00    0.11      0.361  o       |       |       |       |     0.49
48.333    0.00    0.11      0.360  o       |       |       |       |     0.48
48.417    0.00    0.11      0.359  o       |       |       |       |     0.48
48.500    0.00    0.11      0.358  o       |       |       |       |     0.48
48.583    0.00    0.10      0.358  o       |       |       |       |     0.48
48.667    0.00    0.10      0.357  o       |       |       |       |     0.48
48.750    0.00    0.10      0.356  o       |       |       |       |     0.48
48.833    0.00    0.10      0.356  o       |       |       |       |     0.48
48.917    0.00    0.10      0.355  o       |       |       |       |     0.48
49.000    0.00    0.10      0.354  o       |       |       |       |     0.48
49.083    0.00    0.10      0.353  o       |       |       |       |     0.48
49.167    0.00    0.10      0.353  o       |       |       |       |     0.47
49.250    0.00    0.10      0.352  o       |       |       |       |     0.47
49.333    0.00    0.10      0.351  o       |       |       |       |     0.47
49.417    0.00    0.10      0.351  o       |       |       |       |     0.47
49.500    0.00    0.10      0.350  o       |       |       |       |     0.47
49.583    0.00    0.10      0.349  o       |       |       |       |     0.47
49.667    0.00    0.10      0.348  o       |       |       |       |     0.47
49.750    0.00    0.10      0.348  o       |       |       |       |     0.47
49.833    0.00    0.10      0.347  o       |       |       |       |     0.47
49.917    0.00    0.10      0.346  o       |       |       |       |     0.47
50.000    0.00    0.10      0.346  o       |       |       |       |     0.47
50.083    0.00    0.10      0.345  o       |       |       |       |     0.46
50.167    0.00    0.10      0.344  o       |       |       |       |     0.46
50.250    0.00    0.10      0.344  o       |       |       |       |     0.46
50.333    0.00    0.10      0.343  o       |       |       |       |     0.46
50.417    0.00    0.10      0.342  o       |       |       |       |     0.46
50.500    0.00    0.10      0.341  o       |       |       |       |     0.46
50.583    0.00    0.10      0.341  o       |       |       |       |     0.46
      Remaining water in basin =    0.34 (Ac.Ft)
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =   607
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =        0.474 (CFS)
                  Total volume =       0.889 (Ac.Ft)
            Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
      ************************************************************************
      ------------------------------------------------------------------
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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro1535.rte
**********HYDROGRAPH DATA**********
Number of intervals = 41
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 21.675 (CFS)
Total volume = 1.609 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 41
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 5.4 10.84 16.26 21.67	Depth (Ft.)
0.083	0.74	0.00	0.003	OI	0.00
0.167	1.81	0.00	0.011	O I	0.02
0.250	1.96	0.01	0.024	O I	0.03
0.333	2.13	0.01	0.038	O I	0.05
0.417	2.48	0.02	0.054	O I	0.07
0.500	2.74	0.02	0.072	O I	0.10
0.583	2.85	0.03	0.091	O I	0.12
0.667	2.84	0.03	0.110	O I	0.15
0.750	3.07	0.04	0.130	O I	0.18
0.833	2.94	0.04	0.151	O I	0.20
0.917	2.77	0.05	0.170	O I	0.23
1.000	2.92	0.06	0.189	O I	0.26
1.083	3.37	0.06	0.211	O I	0.28
1.167	3.83	0.07	0.235	O I	0.32
1.250	3.94	0.08	0.261	O I	0.35
1.333	3.82	0.08	0.288	O I	0.39
1.417	4.22	0.09	0.315	O I	0.42
1.500	5.21	0.10	0.346	O I	0.47
1.583	5.23	0.11	0.382	O I	0.51
1.667	5.19	0.12	0.417	O I	0.56
1.750	6.31	0.13	0.455	O I	0.61

1.833	7.18	0.15	0.501	O	| I	|	|	|	|	0.67
1.917	6.89	0.16	0.548	O	| I	|	|	|	|	0.74
2.000	6.71	0.17	0.594	O	|I	|	|	|	|	0.80
2.083	6.94	0.19	0.640	O	| I	|	|	|	|	0.86
2.167	8.37	0.20	0.691	O	| I	|	|	|	|	0.93
2.250	11.12	0.23	0.757	O	| I	|	|	|	|	1.02
2.333	11.20	0.27	0.832	O	| I	|	|	|	|	1.11
2.417	12.99	0.31	0.913	O	| I	|	|	|	|	1.21
2.500	18.65	0.37	1.020	O	| I	|	|	|	|	1.34
2.583	21.67	0.45	1.156	O	| I	|	|	|	|	1.50
2.667	21.23	0.52	1.300	O	| I	|	|	|	|	1.68
2.750	13.73	0.59	1.417	O	| I	|	|	|	|	1.82
2.833	6.70	0.63	1.483	O	|I	|	|	|	|	1.90
2.917	4.71	0.64	1.518	O	I |	|	|	|	|	1.95
3.000	3.16	0.66	1.540	O	I |	|	|	|	|	1.97
3.083	1.35	0.66	1.551	OI	|	|	|	|	|	1.99
3.167	0.41	0.66	1.553	O	|	|	|	|	|	1.99
3.250	0.18	0.66	1.550	O	|	|	|	|	|	1.99
3.333	0.07	0.66	1.547	O	|	|	|	|	|	1.98
3.417	0.02	0.66	1.542	O	|	|	|	|	|	1.98
3.500	0.00	0.66	1.538	O	|	|	|	|	|	1.97
3.583	0.00	0.65	1.533	O	|	|	|	|	|	1.97
3.667	0.00	0.65	1.529	O	|	|	|	|	|	1.96
3.750	0.00	0.65	1.525	O	|	|	|	|	|	1.96
3.833	0.00	0.65	1.520	O	|	|	|	|	|	1.95
3.917	0.00	0.64	1.516	O	|	|	|	|	|	1.94
4.000	0.00	0.64	1.511	O	|	|	|	|	|	1.94
4.083	0.00	0.64	1.507	O	|	|	|	|	|	1.93
4.167	0.00	0.64	1.502	O	|	|	|	|	|	1.93
4.250	0.00	0.63	1.498	O	|	|	|	|	|	1.92
4.333	0.00	0.63	1.494	O	|	|	|	|	|	1.92
4.417	0.00	0.63	1.489	O	|	|	|	|	|	1.91
4.500	0.00	0.63	1.485	O	|	|	|	|	|	1.91
4.583	0.00	0.62	1.481	O	|	|	|	|	|	1.90
4.667	0.00	0.62	1.476	O	|	|	|	|	|	1.90
4.750	0.00	0.62	1.472	O	|	|	|	|	|	1.89
4.833	0.00	0.62	1.468	O	|	|	|	|	|	1.89
4.917	0.00	0.61	1.464	O	|	|	|	|	|	1.88
5.000	0.00	0.61	1.459	O	|	|	|	|	|	1.88
5.083	0.00	0.61	1.455	O	|	|	|	|	|	1.87
5.167	0.00	0.61	1.451	O	|	|	|	|	|	1.87
5.250	0.00	0.61	1.447	O	|	|	|	|	|	1.86
5.333	0.00	0.60	1.443	O	|	|	|	|	|	1.86
5.417	0.00	0.60	1.439	O	|	|	|	|	|	1.85
5.500	0.00	0.60	1.434	O	|	|	|	|	|	1.85
5.583	0.00	0.60	1.430	O	|	|	|	|	|	1.84
5.667	0.00	0.59	1.426	O	|	|	|	|	|	1.84
5.750	0.00	0.59	1.422	O	|	|	|	|	|	1.83
5.833	0.00	0.59	1.418	O	|	|	|	|	|	1.83
5.917	0.00	0.59	1.414	O	|	|	|	|	|	1.82
6.000	0.00	0.58	1.410	O	|	|	|	|	|	1.82
6.083	0.00	0.58	1.406	O	|	|	|	|	|	1.81
6.167	0.00	0.58	1.402	O	|	|	|	|	|	1.81
6.250	0.00	0.58	1.398	O	|	|	|	|	|	1.80
6.333	0.00	0.58	1.394	O	|	|	|	|	|	1.80
6.417	0.00	0.57	1.390	O	|	|	|	|	|	1.79
6.500	0.00	0.57	1.386	O	|	|	|	|	|	1.79
6.583	0.00	0.57	1.382	O	|	|	|	|	|	1.78
6.667	0.00	0.57	1.378	O	|	|	|	|	|	1.78
6.750	0.00	0.57	1.374	O	|	|	|	|	|	1.77
6.833	0.00	0.56	1.370	O	|	|	|	|	|	1.77
6.917	0.00	0.56	1.367	O	|	|	|	|	|	1.76
7.000	0.00	0.56	1.363	O	|	|	|	|	|	1.76
7.083	0.00	0.56	1.359	O	|	|	|	|	|	1.75
7.167	0.00	0.55	1.355	O	|	|	|	|	|	1.75
7.250	0.00	0.55	1.351	O	|	|	|	|	|	1.74
7.333	0.00	0.55	1.347	O	|	|	|	|	|	1.74
7.417	0.00	0.55	1.344	O	|	|	|	|	|	1.73
7.500	0.00	0.55	1.340	O	|	|	|	|	|	1.73
7.583	0.00	0.54	1.336	O	|	|	|	|	|	1.73
7.667	0.00	0.54	1.332	O	|	|	|	|	|	1.72
7.750	0.00	0.54	1.329	O	|	|	|	|	|	1.72
7.833	0.00	0.54	1.325	O	|	|	|	|	|	1.71
7.917	0.00	0.54	1.321	O	|	|	|	|	|	1.71
8.000	0.00	0.53	1.318	O	|	|	|	|	|	1.70
8.083	0.00	0.53	1.314	O	|	|	|	|	|	1.70
8.167	0.00	0.53	1.310	O	|	|	|	|	|	1.69
8.250	0.00	0.53	1.307	O	|	|	|	|	|	1.69
8.333	0.00	0.53	1.303	O	|	|	|	|	|	1.68
8.417	0.00	0.52	1.299	O	|	|	|	|	|	1.68
8.500	0.00	0.52	1.296	O	|	|	|	|	|	1.68
8.583	0.00	0.52	1.292	O	|	|	|	|	|	1.67
8.667	0.00	0.52	1.289	O	|	|	|	|	|	1.67
8.750	0.00	0.52	1.285	O	|	|	|	|	|	1.66
8.833	0.00	0.51	1.281	O	|	|	|	|	|	1.66
8.917	0.00	0.51	1.278	O	|	|	|	|	|	1.65

9.000	0.00	0.51	1.274	o	|	|	|	|	1.65
9.083	0.00	0.51	1.271	o	|	|	|	|	1.65
9.167	0.00	0.51	1.267	o	|	|	|	|	1.64
9.250	0.00	0.50	1.264	o	|	|	|	|	1.64
9.333	0.00	0.50	1.260	o	|	|	|	|	1.63
9.417	0.00	0.50	1.257	o	|	|	|	|	1.63
9.500	0.00	0.50	1.254	o	|	|	|	|	1.62
9.583	0.00	0.50	1.250	o	|	|	|	|	1.62
9.667	0.00	0.50	1.247	o	|	|	|	|	1.62
9.750	0.00	0.49	1.243	o	|	|	|	|	1.61
9.833	0.00	0.49	1.240	o	|	|	|	|	1.61
9.917	0.00	0.49	1.237	o	|	|	|	|	1.60
10.000	0.00	0.49	1.233	o	|	|	|	|	1.60
10.083	0.00	0.49	1.230	o	|	|	|	|	1.60
10.167	0.00	0.48	1.226	o	|	|	|	|	1.59
10.250	0.00	0.48	1.223	o	|	|	|	|	1.59
10.333	0.00	0.48	1.220	o	|	|	|	|	1.58
10.417	0.00	0.48	1.217	o	|	|	|	|	1.58
10.500	0.00	0.48	1.213	o	|	|	|	|	1.57
10.583	0.00	0.47	1.210	o	|	|	|	|	1.57
10.667	0.00	0.47	1.207	o	|	|	|	|	1.57
10.750	0.00	0.47	1.203	o	|	|	|	|	1.56
10.833	0.00	0.47	1.200	o	|	|	|	|	1.56
10.917	0.00	0.47	1.197	o	|	|	|	|	1.56
11.000	0.00	0.47	1.194	o	|	|	|	|	1.55
11.083	0.00	0.46	1.191	o	|	|	|	|	1.55
11.167	0.00	0.46	1.187	o	|	|	|	|	1.54
11.250	0.00	0.46	1.184	o	|	|	|	|	1.54
11.333	0.00	0.46	1.181	o	|	|	|	|	1.54
11.417	0.00	0.46	1.178	o	|	|	|	|	1.53
11.500	0.00	0.46	1.175	o	|	|	|	|	1.53
11.583	0.00	0.45	1.172	o	|	|	|	|	1.52
11.667	0.00	0.45	1.168	o	|	|	|	|	1.52
11.750	0.00	0.45	1.165	o	|	|	|	|	1.52
11.833	0.00	0.45	1.162	o	|	|	|	|	1.51
11.917	0.00	0.45	1.159	o	|	|	|	|	1.51
12.000	0.00	0.45	1.156	o	|	|	|	|	1.51
12.083	0.00	0.44	1.153	o	|	|	|	|	1.50
12.167	0.00	0.44	1.150	o	|	|	|	|	1.50
12.250	0.00	0.44	1.147	o	|	|	|	|	1.49
12.333	0.00	0.44	1.144	o	|	|	|	|	1.49
12.417	0.00	0.44	1.141	o	|	|	|	|	1.49
12.500	0.00	0.44	1.138	o	|	|	|	|	1.48
12.583	0.00	0.43	1.135	o	|	|	|	|	1.48
12.667	0.00	0.43	1.132	o	|	|	|	|	1.48
12.750	0.00	0.43	1.129	o	|	|	|	|	1.47
12.833	0.00	0.43	1.126	o	|	|	|	|	1.47
12.917	0.00	0.43	1.123	o	|	|	|	|	1.46
13.000	0.00	0.43	1.120	o	|	|	|	|	1.46
13.083	0.00	0.42	1.117	o	|	|	|	|	1.46
13.167	0.00	0.42	1.114	o	|	|	|	|	1.45
13.250	0.00	0.42	1.111	o	|	|	|	|	1.45
13.333	0.00	0.42	1.109	o	|	|	|	|	1.45
13.417	0.00	0.42	1.106	o	|	|	|	|	1.44
13.500	0.00	0.42	1.103	o	|	|	|	|	1.44
13.583	0.00	0.41	1.100	o	|	|	|	|	1.44
13.667	0.00	0.41	1.097	o	|	|	|	|	1.43
13.750	0.00	0.41	1.094	o	|	|	|	|	1.43
13.833	0.00	0.41	1.091	o	|	|	|	|	1.43
13.917	0.00	0.41	1.089	o	|	|	|	|	1.42
14.000	0.00	0.41	1.086	o	|	|	|	|	1.42
14.083	0.00	0.41	1.083	o	|	|	|	|	1.42
14.167	0.00	0.40	1.080	o	|	|	|	|	1.41
14.250	0.00	0.40	1.077	o	|	|	|	|	1.41
14.333	0.00	0.40	1.075	o	|	|	|	|	1.41
14.417	0.00	0.40	1.072	o	|	|	|	|	1.40
14.500	0.00	0.40	1.069	o	|	|	|	|	1.40
14.583	0.00	0.40	1.066	o	|	|	|	|	1.40
14.667	0.00	0.39	1.064	o	|	|	|	|	1.39
14.750	0.00	0.39	1.061	o	|	|	|	|	1.39
14.833	0.00	0.39	1.058	o	|	|	|	|	1.39
14.917	0.00	0.39	1.056	o	|	|	|	|	1.38
15.000	0.00	0.39	1.053	o	|	|	|	|	1.38
15.083	0.00	0.39	1.050	o	|	|	|	|	1.38
15.167	0.00	0.39	1.048	o	|	|	|	|	1.37
15.250	0.00	0.38	1.045	o	|	|	|	|	1.37
15.333	0.00	0.38	1.042	o	|	|	|	|	1.37
15.417	0.00	0.38	1.040	o	|	|	|	|	1.36
15.500	0.00	0.38	1.037	o	|	|	|	|	1.36
15.583	0.00	0.38	1.034	o	|	|	|	|	1.36
15.667	0.00	0.38	1.032	o	|	|	|	|	1.35
15.750	0.00	0.38	1.029	o	|	|	|	|	1.35
15.833	0.00	0.37	1.027	o	|	|	|	|	1.35
15.917	0.00	0.37	1.024	o	|	|	|	|	1.34
16.000	0.00	0.37	1.022	o	|	|	|	|	1.34
16.083	0.00	0.37	1.019	o	|	|	|	|	1.34

16.167	0.00	0.37	1.016	o	|	|	|	|	1.33
16.250	0.00	0.37	1.014	o	|	|	|	|	1.33
16.333	0.00	0.37	1.011	o	|	|	|	|	1.33
16.417	0.00	0.36	1.009	o	|	|	|	|	1.33
16.500	0.00	0.36	1.006	o	|	|	|	|	1.32
16.583	0.00	0.36	1.004	o	|	|	|	|	1.32
16.667	0.00	0.36	1.001	o	|	|	|	|	1.32
16.750	0.00	0.36	0.999	o	|	|	|	|	1.31
16.833	0.00	0.36	0.996	o	|	|	|	|	1.31
16.917	0.00	0.36	0.994	o	|	|	|	|	1.31
17.000	0.00	0.35	0.992	o	|	|	|	|	1.30
17.083	0.00	0.35	0.989	o	|	|	|	|	1.30
17.167	0.00	0.35	0.987	o	|	|	|	|	1.30
17.250	0.00	0.35	0.984	o	|	|	|	|	1.29
17.333	0.00	0.35	0.982	o	|	|	|	|	1.29
17.417	0.00	0.35	0.979	o	|	|	|	|	1.29
17.500	0.00	0.35	0.977	o	|	|	|	|	1.29
17.583	0.00	0.35	0.975	o	|	|	|	|	1.28
17.667	0.00	0.34	0.972	o	|	|	|	|	1.28
17.750	0.00	0.34	0.970	o	|	|	|	|	1.28
17.833	0.00	0.34	0.968	o	|	|	|	|	1.27
17.917	0.00	0.34	0.965	o	|	|	|	|	1.27
18.000	0.00	0.34	0.963	o	|	|	|	|	1.27
18.083	0.00	0.34	0.961	o	|	|	|	|	1.27
18.167	0.00	0.34	0.958	o	|	|	|	|	1.26
18.250	0.00	0.34	0.956	o	|	|	|	|	1.26
18.333	0.00	0.33	0.954	o	|	|	|	|	1.26
18.417	0.00	0.33	0.951	o	|	|	|	|	1.25
18.500	0.00	0.33	0.949	o	|	|	|	|	1.25
18.583	0.00	0.33	0.947	o	|	|	|	|	1.25
18.667	0.00	0.33	0.944	o	|	|	|	|	1.25
18.750	0.00	0.33	0.942	o	|	|	|	|	1.24
18.833	0.00	0.33	0.940	o	|	|	|	|	1.24
18.917	0.00	0.33	0.938	o	|	|	|	|	1.24
19.000	0.00	0.32	0.936	o	|	|	|	|	1.24
19.083	0.00	0.32	0.933	o	|	|	|	|	1.23
19.167	0.00	0.32	0.931	o	|	|	|	|	1.23
19.250	0.00	0.32	0.929	o	|	|	|	|	1.23
19.333	0.00	0.32	0.927	o	|	|	|	|	1.22
19.417	0.00	0.32	0.924	o	|	|	|	|	1.22
19.500	0.00	0.32	0.922	o	|	|	|	|	1.22
19.583	0.00	0.32	0.920	o	|	|	|	|	1.22
19.667	0.00	0.31	0.918	o	|	|	|	|	1.21
19.750	0.00	0.31	0.916	o	|	|	|	|	1.21
19.833	0.00	0.31	0.914	o	|	|	|	|	1.21
19.917	0.00	0.31	0.911	o	|	|	|	|	1.21
20.000	0.00	0.31	0.909	o	|	|	|	|	1.20
20.083	0.00	0.31	0.907	o	|	|	|	|	1.20
20.167	0.00	0.31	0.905	o	|	|	|	|	1.20
20.250	0.00	0.31	0.903	o	|	|	|	|	1.20
20.333	0.00	0.30	0.901	o	|	|	|	|	1.19
20.417	0.00	0.30	0.899	o	|	|	|	|	1.19
20.500	0.00	0.30	0.897	o	|	|	|	|	1.19
20.583	0.00	0.30	0.895	o	|	|	|	|	1.19
20.667	0.00	0.30	0.893	o	|	|	|	|	1.18
20.750	0.00	0.30	0.890	o	|	|	|	|	1.18
20.833	0.00	0.30	0.888	o	|	|	|	|	1.18
20.917	0.00	0.30	0.886	o	|	|	|	|	1.18
21.000	0.00	0.30	0.884	o	|	|	|	|	1.17
21.083	0.00	0.29	0.882	o	|	|	|	|	1.17
21.167	0.00	0.29	0.880	o	|	|	|	|	1.17
21.250	0.00	0.29	0.878	o	|	|	|	|	1.17
21.333	0.00	0.29	0.876	o	|	|	|	|	1.16
21.417	0.00	0.29	0.874	o	|	|	|	|	1.16
21.500	0.00	0.29	0.872	o	|	|	|	|	1.16
21.583	0.00	0.29	0.870	o	|	|	|	|	1.16
21.667	0.00	0.29	0.868	o	|	|	|	|	1.15
21.750	0.00	0.29	0.866	o	|	|	|	|	1.15
21.833	0.00	0.28	0.864	o	|	|	|	|	1.15
21.917	0.00	0.28	0.862	o	|	|	|	|	1.15
22.000	0.00	0.28	0.860	o	|	|	|	|	1.14
22.083	0.00	0.28	0.858	o	|	|	|	|	1.14
22.167	0.00	0.28	0.857	o	|	|	|	|	1.14
22.250	0.00	0.28	0.855	o	|	|	|	|	1.14
22.333	0.00	0.28	0.853	o	|	|	|	|	1.13
22.417	0.00	0.28	0.851	o	|	|	|	|	1.13
22.500	0.00	0.28	0.849	o	|	|	|	|	1.13
22.583	0.00	0.28	0.847	o	|	|	|	|	1.13
22.667	0.00	0.27	0.845	o	|	|	|	|	1.12
22.750	0.00	0.27	0.843	o	|	|	|	|	1.12
22.833	0.00	0.27	0.841	o	|	|	|	|	1.12
22.917	0.00	0.27	0.839	o	|	|	|	|	1.12
23.000	0.00	0.27	0.838	o	|	|	|	|	1.12
23.083	0.00	0.27	0.836	o	|	|	|	|	1.11
23.167	0.00	0.27	0.834	o	|	|	|	|	1.11
23.250	0.00	0.27	0.832	o	|	|	|	|	1.11

23.333	0.00	0.27	0.830	o	|	|	|	|	1.11
23.417	0.00	0.26	0.828	o	|	|	|	|	1.10
23.500	0.00	0.26	0.827	o	|	|	|	|	1.10
23.583	0.00	0.26	0.825	o	|	|	|	|	1.10
23.667	0.00	0.26	0.823	o	|	|	|	|	1.10
23.750	0.00	0.26	0.821	o	|	|	|	|	1.10
23.833	0.00	0.26	0.819	o	|	|	|	|	1.09
23.917	0.00	0.26	0.818	o	|	|	|	|	1.09
24.000	0.00	0.26	0.816	o	|	|	|	|	1.09
24.083	0.00	0.26	0.814	o	|	|	|	|	1.09
24.167	0.00	0.26	0.812	o	|	|	|	|	1.08
24.250	0.00	0.26	0.810	o	|	|	|	|	1.08
24.333	0.00	0.25	0.809	o	|	|	|	|	1.08
24.417	0.00	0.25	0.807	o	|	|	|	|	1.08
24.500	0.00	0.25	0.805	o	|	|	|	|	1.08
24.583	0.00	0.25	0.804	o	|	|	|	|	1.07
24.667	0.00	0.25	0.802	o	|	|	|	|	1.07
24.750	0.00	0.25	0.800	o	|	|	|	|	1.07
24.833	0.00	0.25	0.798	o	|	|	|	|	1.07
24.917	0.00	0.25	0.797	o	|	|	|	|	1.07
25.000	0.00	0.25	0.795	o	|	|	|	|	1.06
25.083	0.00	0.25	0.793	o	|	|	|	|	1.06
25.167	0.00	0.24	0.792	o	|	|	|	|	1.06
25.250	0.00	0.24	0.790	o	|	|	|	|	1.06
25.333	0.00	0.24	0.788	o	|	|	|	|	1.06
25.417	0.00	0.24	0.787	o	|	|	|	|	1.05
25.500	0.00	0.24	0.785	o	|	|	|	|	1.05
25.583	0.00	0.24	0.783	o	|	|	|	|	1.05
25.667	0.00	0.24	0.782	o	|	|	|	|	1.05
25.750	0.00	0.24	0.780	o	|	|	|	|	1.05
25.833	0.00	0.24	0.778	o	|	|	|	|	1.04
25.917	0.00	0.24	0.777	o	|	|	|	|	1.04
26.000	0.00	0.24	0.775	o	|	|	|	|	1.04
26.083	0.00	0.23	0.773	o	|	|	|	|	1.04
26.167	0.00	0.23	0.772	o	|	|	|	|	1.04
26.250	0.00	0.23	0.770	o	|	|	|	|	1.03
26.333	0.00	0.23	0.769	o	|	|	|	|	1.03
26.417	0.00	0.23	0.767	o	|	|	|	|	1.03
26.500	0.00	0.23	0.765	o	|	|	|	|	1.03
26.583	0.00	0.23	0.764	o	|	|	|	|	1.03
26.667	0.00	0.23	0.762	o	|	|	|	|	1.02
26.750	0.00	0.23	0.761	o	|	|	|	|	1.02
26.833	0.00	0.23	0.759	o	|	|	|	|	1.02
26.917	0.00	0.23	0.758	o	|	|	|	|	1.02
27.000	0.00	0.23	0.756	o	|	|	|	|	1.02
27.083	0.00	0.22	0.754	o	|	|	|	|	1.01
27.167	0.00	0.22	0.753	o	|	|	|	|	1.01
27.250	0.00	0.22	0.751	o	|	|	|	|	1.01
27.333	0.00	0.22	0.750	o	|	|	|	|	1.01
27.417	0.00	0.22	0.748	o	|	|	|	|	1.01
27.500	0.00	0.22	0.747	o	|	|	|	|	1.00
27.583	0.00	0.22	0.745	o	|	|	|	|	1.00
27.667	0.00	0.22	0.744	o	|	|	|	|	1.00
27.750	0.00	0.22	0.742	o	|	|	|	|	1.00
27.833	0.00	0.22	0.741	o	|	|	|	|	1.00
27.917	0.00	0.22	0.739	o	|	|	|	|	0.99
28.000	0.00	0.22	0.738	o	|	|	|	|	0.99
28.083	0.00	0.22	0.736	o	|	|	|	|	0.99
28.167	0.00	0.22	0.735	o	|	|	|	|	0.99
28.250	0.00	0.22	0.733	o	|	|	|	|	0.99
28.333	0.00	0.21	0.732	o	|	|	|	|	0.98
28.417	0.00	0.21	0.730	o	|	|	|	|	0.98
28.500	0.00	0.21	0.729	o	|	|	|	|	0.98
28.583	0.00	0.21	0.727	o	|	|	|	|	0.98
28.667	0.00	0.21	0.726	o	|	|	|	|	0.98
28.750	0.00	0.21	0.724	o	|	|	|	|	0.98
28.833	0.00	0.21	0.723	o	|	|	|	|	0.97
28.917	0.00	0.21	0.722	o	|	|	|	|	0.97
29.000	0.00	0.21	0.720	o	|	|	|	|	0.97
29.083	0.00	0.21	0.719	o	|	|	|	|	0.97
29.167	0.00	0.21	0.717	o	|	|	|	|	0.97
29.250	0.00	0.21	0.716	o	|	|	|	|	0.96
29.333	0.00	0.21	0.714	o	|	|	|	|	0.96
29.417	0.00	0.21	0.713	o	|	|	|	|	0.96
29.500	0.00	0.21	0.711	o	|	|	|	|	0.96
29.583	0.00	0.21	0.710	o	|	|	|	|	0.96
29.667	0.00	0.21	0.709	o	|	|	|	|	0.95
29.750	0.00	0.21	0.707	o	|	|	|	|	0.95
29.833	0.00	0.21	0.706	o	|	|	|	|	0.95
29.917	0.00	0.21	0.704	o	|	|	|	|	0.95
30.000	0.00	0.21	0.703	o	|	|	|	|	0.95
30.083	0.00	0.21	0.701	o	|	|	|	|	0.94
30.167	0.00	0.21	0.700	o	|	|	|	|	0.94
30.250	0.00	0.20	0.699	o	|	|	|	|	0.94
30.333	0.00	0.20	0.697	o	|	|	|	|	0.94
30.417	0.00	0.20	0.696	o	|	|	|	|	0.94

30.500	0.00	0.20	0.694	o	|	|	|	|	0.93
30.583	0.00	0.20	0.693	o	|	|	|	|	0.93
30.667	0.00	0.20	0.692	o	|	|	|	|	0.93
30.750	0.00	0.20	0.690	o	|	|	|	|	0.93
30.833	0.00	0.20	0.689	o	|	|	|	|	0.93
30.917	0.00	0.20	0.687	o	|	|	|	|	0.93
31.000	0.00	0.20	0.686	o	|	|	|	|	0.92
31.083	0.00	0.20	0.685	o	|	|	|	|	0.92
31.167	0.00	0.20	0.683	o	|	|	|	|	0.92
31.250	0.00	0.20	0.682	o	|	|	|	|	0.92
31.333	0.00	0.20	0.680	o	|	|	|	|	0.92
31.417	0.00	0.20	0.679	o	|	|	|	|	0.91
31.500	0.00	0.20	0.678	o	|	|	|	|	0.91
31.583	0.00	0.20	0.676	o	|	|	|	|	0.91
31.667	0.00	0.20	0.675	o	|	|	|	|	0.91
31.750	0.00	0.20	0.674	o	|	|	|	|	0.91
31.833	0.00	0.20	0.672	o	|	|	|	|	0.90
31.917	0.00	0.20	0.671	o	|	|	|	|	0.90
32.000	0.00	0.20	0.670	o	|	|	|	|	0.90
32.083	0.00	0.20	0.668	o	|	|	|	|	0.90
32.167	0.00	0.20	0.667	o	|	|	|	|	0.90
32.250	0.00	0.20	0.666	o	|	|	|	|	0.90
32.333	0.00	0.19	0.664	o	|	|	|	|	0.89
32.417	0.00	0.19	0.663	o	|	|	|	|	0.89
32.500	0.00	0.19	0.662	o	|	|	|	|	0.89
32.583	0.00	0.19	0.660	o	|	|	|	|	0.89
32.667	0.00	0.19	0.659	o	|	|	|	|	0.89
32.750	0.00	0.19	0.658	o	|	|	|	|	0.88
32.833	0.00	0.19	0.656	o	|	|	|	|	0.88
32.917	0.00	0.19	0.655	o	|	|	|	|	0.88
33.000	0.00	0.19	0.654	o	|	|	|	|	0.88
33.083	0.00	0.19	0.652	o	|	|	|	|	0.88
33.167	0.00	0.19	0.651	o	|	|	|	|	0.88
33.250	0.00	0.19	0.650	o	|	|	|	|	0.87
33.333	0.00	0.19	0.648	o	|	|	|	|	0.87
33.417	0.00	0.19	0.647	o	|	|	|	|	0.87
33.500	0.00	0.19	0.646	o	|	|	|	|	0.87
33.583	0.00	0.19	0.644	o	|	|	|	|	0.87
33.667	0.00	0.19	0.643	o	|	|	|	|	0.87
33.750	0.00	0.19	0.642	o	|	|	|	|	0.86
33.833	0.00	0.19	0.640	o	|	|	|	|	0.86
33.917	0.00	0.19	0.639	o	|	|	|	|	0.86
34.000	0.00	0.19	0.638	o	|	|	|	|	0.86
34.083	0.00	0.19	0.637	o	|	|	|	|	0.86
34.167	0.00	0.19	0.635	o	|	|	|	|	0.86
34.250	0.00	0.19	0.634	o	|	|	|	|	0.85
34.333	0.00	0.19	0.633	o	|	|	|	|	0.85
34.417	0.00	0.19	0.631	o	|	|	|	|	0.85
34.500	0.00	0.18	0.630	o	|	|	|	|	0.85
34.583	0.00	0.18	0.629	o	|	|	|	|	0.85
34.667	0.00	0.18	0.628	o	|	|	|	|	0.84
34.750	0.00	0.18	0.626	o	|	|	|	|	0.84
34.833	0.00	0.18	0.625	o	|	|	|	|	0.84
34.917	0.00	0.18	0.624	o	|	|	|	|	0.84
35.000	0.00	0.18	0.623	o	|	|	|	|	0.84
35.083	0.00	0.18	0.621	o	|	|	|	|	0.84
35.167	0.00	0.18	0.620	o	|	|	|	|	0.83
35.250	0.00	0.18	0.619	o	|	|	|	|	0.83
35.333	0.00	0.18	0.618	o	|	|	|	|	0.83
35.417	0.00	0.18	0.616	o	|	|	|	|	0.83
35.500	0.00	0.18	0.615	o	|	|	|	|	0.83
35.583	0.00	0.18	0.614	o	|	|	|	|	0.83
35.667	0.00	0.18	0.613	o	|	|	|	|	0.82
35.750	0.00	0.18	0.611	o	|	|	|	|	0.82
35.833	0.00	0.18	0.610	o	|	|	|	|	0.82
35.917	0.00	0.18	0.609	o	|	|	|	|	0.82
36.000	0.00	0.18	0.608	o	|	|	|	|	0.82
36.083	0.00	0.18	0.606	o	|	|	|	|	0.82
36.167	0.00	0.18	0.605	o	|	|	|	|	0.81
36.250	0.00	0.18	0.604	o	|	|	|	|	0.81
36.333	0.00	0.18	0.603	o	|	|	|	|	0.81
36.417	0.00	0.18	0.602	o	|	|	|	|	0.81
36.500	0.00	0.18	0.600	o	|	|	|	|	0.81
36.583	0.00	0.18	0.599	o	|	|	|	|	0.81
36.667	0.00	0.18	0.598	o	|	|	|	|	0.80
36.750	0.00	0.18	0.597	o	|	|	|	|	0.80
36.833	0.00	0.17	0.596	o	|	|	|	|	0.80
36.917	0.00	0.17	0.594	o	|	|	|	|	0.80
37.000	0.00	0.17	0.593	o	|	|	|	|	0.80
37.083	0.00	0.17	0.592	o	|	|	|	|	0.80
37.167	0.00	0.17	0.591	o	|	|	|	|	0.80
37.250	0.00	0.17	0.590	o	|	|	|	|	0.79
37.333	0.00	0.17	0.588	o	|	|	|	|	0.79
37.417	0.00	0.17	0.587	o	|	|	|	|	0.79
37.500	0.00	0.17	0.586	o	|	|	|	|	0.79
37.583	0.00	0.17	0.585	o	|	|	|	|	0.79

37.667	0.00	0.17	0.584	o	|	|	|	|	0.79
37.750	0.00	0.17	0.582	o	|	|	|	|	0.78
37.833	0.00	0.17	0.581	o	|	|	|	|	0.78
37.917	0.00	0.17	0.580	o	|	|	|	|	0.78
38.000	0.00	0.17	0.579	o	|	|	|	|	0.78
38.083	0.00	0.17	0.578	o	|	|	|	|	0.78
38.167	0.00	0.17	0.577	o	|	|	|	|	0.78
38.250	0.00	0.17	0.575	o	|	|	|	|	0.77
38.333	0.00	0.17	0.574	o	|	|	|	|	0.77
38.417	0.00	0.17	0.573	o	|	|	|	|	0.77
38.500	0.00	0.17	0.572	o	|	|	|	|	0.77
38.583	0.00	0.17	0.571	o	|	|	|	|	0.77
38.667	0.00	0.17	0.570	o	|	|	|	|	0.77
38.750	0.00	0.17	0.568	o	|	|	|	|	0.77
38.833	0.00	0.17	0.567	o	|	|	|	|	0.76
38.917	0.00	0.17	0.566	o	|	|	|	|	0.76
39.000	0.00	0.17	0.565	o	|	|	|	|	0.76
39.083	0.00	0.17	0.564	o	|	|	|	|	0.76
39.167	0.00	0.17	0.563	o	|	|	|	|	0.76
39.250	0.00	0.16	0.562	o	|	|	|	|	0.76
39.333	0.00	0.16	0.560	o	|	|	|	|	0.75
39.417	0.00	0.16	0.559	o	|	|	|	|	0.75
39.500	0.00	0.16	0.558	o	|	|	|	|	0.75
39.583	0.00	0.16	0.557	o	|	|	|	|	0.75
39.667	0.00	0.16	0.556	o	|	|	|	|	0.75
39.750	0.00	0.16	0.555	o	|	|	|	|	0.75
39.833	0.00	0.16	0.554	o	|	|	|	|	0.75
39.917	0.00	0.16	0.553	o	|	|	|	|	0.74
40.000	0.00	0.16	0.552	o	|	|	|	|	0.74
40.083	0.00	0.16	0.550	o	|	|	|	|	0.74
40.167	0.00	0.16	0.549	o	|	|	|	|	0.74
40.250	0.00	0.16	0.548	o	|	|	|	|	0.74
40.333	0.00	0.16	0.547	o	|	|	|	|	0.74
40.417	0.00	0.16	0.546	o	|	|	|	|	0.73
40.500	0.00	0.16	0.545	o	|	|	|	|	0.73
40.583	0.00	0.16	0.544	o	|	|	|	|	0.73
40.667	0.00	0.16	0.543	o	|	|	|	|	0.73
40.750	0.00	0.16	0.542	o	|	|	|	|	0.73
40.833	0.00	0.16	0.540	o	|	|	|	|	0.73
40.917	0.00	0.16	0.539	o	|	|	|	|	0.73
41.000	0.00	0.16	0.538	o	|	|	|	|	0.72
41.083	0.00	0.16	0.537	o	|	|	|	|	0.72
41.167	0.00	0.16	0.536	o	|	|	|	|	0.72
41.250	0.00	0.16	0.535	o	|	|	|	|	0.72
41.333	0.00	0.16	0.534	o	|	|	|	|	0.72
41.417	0.00	0.16	0.533	o	|	|	|	|	0.72
41.500	0.00	0.16	0.532	o	|	|	|	|	0.72
41.583	0.00	0.16	0.531	o	|	|	|	|	0.71
41.667	0.00	0.16	0.530	o	|	|	|	|	0.71
41.750	0.00	0.16	0.529	o	|	|	|	|	0.71
41.833	0.00	0.15	0.528	o	|	|	|	|	0.71
41.917	0.00	0.15	0.526	o	|	|	|	|	0.71
42.000	0.00	0.15	0.525	o	|	|	|	|	0.71
42.083	0.00	0.15	0.524	o	|	|	|	|	0.71
42.167	0.00	0.15	0.523	o	|	|	|	|	0.70
42.250	0.00	0.15	0.522	o	|	|	|	|	0.70
42.333	0.00	0.15	0.521	o	|	|	|	|	0.70
42.417	0.00	0.15	0.520	o	|	|	|	|	0.70
42.500	0.00	0.15	0.519	o	|	|	|	|	0.70
42.583	0.00	0.15	0.518	o	|	|	|	|	0.70
42.667	0.00	0.15	0.517	o	|	|	|	|	0.70
42.750	0.00	0.15	0.516	o	|	|	|	|	0.69
42.833	0.00	0.15	0.515	o	|	|	|	|	0.69
42.917	0.00	0.15	0.514	o	|	|	|	|	0.69
43.000	0.00	0.15	0.513	o	|	|	|	|	0.69
43.083	0.00	0.15	0.512	o	|	|	|	|	0.69
43.167	0.00	0.15	0.511	o	|	|	|	|	0.69
43.250	0.00	0.15	0.510	o	|	|	|	|	0.69
43.333	0.00	0.15	0.509	o	|	|	|	|	0.68
43.417	0.00	0.15	0.508	o	|	|	|	|	0.68
43.500	0.00	0.15	0.507	o	|	|	|	|	0.68
43.583	0.00	0.15	0.506	o	|	|	|	|	0.68
43.667	0.00	0.15	0.505	o	|	|	|	|	0.68
43.750	0.00	0.15	0.504	o	|	|	|	|	0.68
43.833	0.00	0.15	0.503	o	|	|	|	|	0.68
43.917	0.00	0.15	0.502	o	|	|	|	|	0.68
44.000	0.00	0.15	0.501	o	|	|	|	|	0.67
44.083	0.00	0.15	0.500	o	|	|	|	|	0.67
44.167	0.00	0.15	0.499	o	|	|	|	|	0.67
44.250	0.00	0.15	0.497	o	|	|	|	|	0.67
44.333	0.00	0.15	0.496	o	|	|	|	|	0.67
44.417	0.00	0.15	0.495	o	|	|	|	|	0.67
44.500	0.00	0.15	0.494	o	|	|	|	|	0.67
44.583	0.00	0.14	0.493	o	|	|	|	|	0.66
44.667	0.00	0.14	0.492	o	|	|	|	|	0.66
44.750	0.00	0.14	0.492	o	|	|	|	|	0.66

44.833	0.00	0.14	0.491	o	|	|	|	|	0.66
44.917	0.00	0.14	0.490	o	|	|	|	|	0.66
45.000	0.00	0.14	0.489	o	|	|	|	|	0.66
45.083	0.00	0.14	0.488	o	|	|	|	|	0.66
45.167	0.00	0.14	0.487	o	|	|	|	|	0.65
45.250	0.00	0.14	0.486	o	|	|	|	|	0.65
45.333	0.00	0.14	0.485	o	|	|	|	|	0.65
45.417	0.00	0.14	0.484	o	|	|	|	|	0.65
45.500	0.00	0.14	0.483	o	|	|	|	|	0.65
45.583	0.00	0.14	0.482	o	|	|	|	|	0.65
45.667	0.00	0.14	0.481	o	|	|	|	|	0.65
45.750	0.00	0.14	0.480	o	|	|	|	|	0.65
45.833	0.00	0.14	0.479	o	|	|	|	|	0.64
45.917	0.00	0.14	0.478	o	|	|	|	|	0.64
46.000	0.00	0.14	0.477	o	|	|	|	|	0.64
46.083	0.00	0.14	0.476	o	|	|	|	|	0.64
46.167	0.00	0.14	0.475	o	|	|	|	|	0.64
46.250	0.00	0.14	0.474	o	|	|	|	|	0.64
46.333	0.00	0.14	0.473	o	|	|	|	|	0.64
46.417	0.00	0.14	0.472	o	|	|	|	|	0.64
46.500	0.00	0.14	0.471	o	|	|	|	|	0.63
46.583	0.00	0.14	0.470	o	|	|	|	|	0.63
46.667	0.00	0.14	0.469	o	|	|	|	|	0.63
46.750	0.00	0.14	0.468	o	|	|	|	|	0.63
46.833	0.00	0.14	0.467	o	|	|	|	|	0.63
46.917	0.00	0.14	0.466	o	|	|	|	|	0.63
47.000	0.00	0.14	0.465	o	|	|	|	|	0.63
47.083	0.00	0.14	0.464	o	|	|	|	|	0.63
47.167	0.00	0.14	0.464	o	|	|	|	|	0.62
47.250	0.00	0.14	0.463	o	|	|	|	|	0.62
47.333	0.00	0.14	0.462	o	|	|	|	|	0.62
47.417	0.00	0.14	0.461	o	|	|	|	|	0.62
47.500	0.00	0.13	0.460	o	|	|	|	|	0.62
47.583	0.00	0.13	0.459	o	|	|	|	|	0.62
47.667	0.00	0.13	0.458	o	|	|	|	|	0.62
47.750	0.00	0.13	0.457	o	|	|	|	|	0.62
47.833	0.00	0.13	0.456	o	|	|	|	|	0.61
47.917	0.00	0.13	0.455	o	|	|	|	|	0.61
48.000	0.00	0.13	0.454	o	|	|	|	|	0.61
48.083	0.00	0.13	0.453	o	|	|	|	|	0.61
48.167	0.00	0.13	0.452	o	|	|	|	|	0.61
48.250	0.00	0.13	0.452	o	|	|	|	|	0.61
48.333	0.00	0.13	0.451	o	|	|	|	|	0.61
48.417	0.00	0.13	0.450	o	|	|	|	|	0.61
48.500	0.00	0.13	0.449	o	|	|	|	|	0.60
48.583	0.00	0.13	0.448	o	|	|	|	|	0.60
48.667	0.00	0.13	0.447	o	|	|	|	|	0.60
48.750	0.00	0.13	0.446	o	|	|	|	|	0.60
48.833	0.00	0.13	0.445	o	|	|	|	|	0.60
48.917	0.00	0.13	0.444	o	|	|	|	|	0.60
49.000	0.00	0.13	0.443	o	|	|	|	|	0.60
49.083	0.00	0.13	0.442	o	|	|	|	|	0.60
49.167	0.00	0.13	0.442	o	|	|	|	|	0.59
49.250	0.00	0.13	0.441	o	|	|	|	|	0.59
49.333	0.00	0.13	0.440	o	|	|	|	|	0.59
49.417	0.00	0.13	0.439	o	|	|	|	|	0.59
49.500	0.00	0.13	0.438	o	|	|	|	|	0.59
49.583	0.00	0.13	0.437	o	|	|	|	|	0.59
49.667	0.00	0.13	0.436	o	|	|	|	|	0.59
49.750	0.00	0.13	0.435	o	|	|	|	|	0.59
49.833	0.00	0.13	0.435	o	|	|	|	|	0.58
49.917	0.00	0.13	0.434	o	|	|	|	|	0.58
50.000	0.00	0.13	0.433	o	|	|	|	|	0.58
50.083	0.00	0.13	0.432	o	|	|	|	|	0.58
50.167	0.00	0.13	0.431	o	|	|	|	|	0.58
50.250	0.00	0.13	0.430	o	|	|	|	|	0.58
50.333	0.00	0.13	0.429	o	|	|	|	|	0.58
50.417	0.00	0.13	0.428	o	|	|	|	|	0.58
50.500	0.00	0.13	0.428	o	|	|	|	|	0.58
50.583	0.00	0.13	0.427	o	|	|	|	|	0.57
50.667	0.00	0.12	0.426	o	|	|	|	|	0.57
50.750	0.00	0.12	0.425	o	|	|	|	|	0.57
50.833	0.00	0.12	0.424	o	|	|	|	|	0.57
50.917	0.00	0.12	0.423	o	|	|	|	|	0.57
51.000	0.00	0.12	0.422	o	|	|	|	|	0.57
51.083	0.00	0.12	0.422	o	|	|	|	|	0.57
51.167	0.00	0.12	0.421	o	|	|	|	|	0.57
51.250	0.00	0.12	0.420	o	|	|	|	|	0.57
51.333	0.00	0.12	0.419	o	|	|	|	|	0.56
51.417	0.00	0.12	0.418	o	|	|	|	|	0.56
51.500	0.00	0.12	0.417	o	|	|	|	|	0.56
51.583	0.00	0.12	0.416	o	|	|	|	|	0.56
51.667	0.00	0.12	0.416	o	|	|	|	|	0.56
51.750	0.00	0.12	0.415	o	|	|	|	|	0.56
51.833	0.00	0.12	0.414	o	|	|	|	|	0.56
51.917	0.00	0.12	0.413	o	|	|	|	|	0.56

52.000	0.00	0.12	0.412	o	|	|	|	|	0.55
52.083	0.00	0.12	0.411	o	|	|	|	|	0.55
52.167	0.00	0.12	0.411	o	|	|	|	|	0.55
52.250	0.00	0.12	0.410	o	|	|	|	|	0.55
52.333	0.00	0.12	0.409	o	|	|	|	|	0.55
52.417	0.00	0.12	0.408	o	|	|	|	|	0.55
52.500	0.00	0.12	0.407	o	|	|	|	|	0.55
52.583	0.00	0.12	0.406	o	|	|	|	|	0.55
52.667	0.00	0.12	0.406	o	|	|	|	|	0.55
52.750	0.00	0.12	0.405	o	|	|	|	|	0.54
52.833	0.00	0.12	0.404	o	|	|	|	|	0.54
52.917	0.00	0.12	0.403	o	|	|	|	|	0.54
53.000	0.00	0.12	0.402	o	|	|	|	|	0.54
53.083	0.00	0.12	0.402	o	|	|	|	|	0.54
53.167	0.00	0.12	0.401	o	|	|	|	|	0.54
53.250	0.00	0.12	0.400	o	|	|	|	|	0.54
53.333	0.00	0.12	0.399	o	|	|	|	|	0.54
53.417	0.00	0.12	0.398	o	|	|	|	|	0.54
53.500	0.00	0.12	0.398	o	|	|	|	|	0.54
53.583	0.00	0.12	0.397	o	|	|	|	|	0.53
53.667	0.00	0.12	0.396	o	|	|	|	|	0.53
53.750	0.00	0.12	0.395	o	|	|	|	|	0.53
53.833	0.00	0.12	0.394	o	|	|	|	|	0.53
53.917	0.00	0.12	0.394	o	|	|	|	|	0.53
54.000	0.00	0.12	0.393	o	|	|	|	|	0.53
54.083	0.00	0.12	0.392	o	|	|	|	|	0.53
54.167	0.00	0.11	0.391	o	|	|	|	|	0.53
54.250	0.00	0.11	0.390	o	|	|	|	|	0.53
54.333	0.00	0.11	0.390	o	|	|	|	|	0.52
54.417	0.00	0.11	0.389	o	|	|	|	|	0.52
54.500	0.00	0.11	0.388	o	|	|	|	|	0.52
54.583	0.00	0.11	0.387	o	|	|	|	|	0.52
54.667	0.00	0.11	0.386	o	|	|	|	|	0.52
54.750	0.00	0.11	0.386	o	|	|	|	|	0.52
54.833	0.00	0.11	0.385	o	|	|	|	|	0.52
54.917	0.00	0.11	0.384	o	|	|	|	|	0.52
55.000	0.00	0.11	0.383	o	|	|	|	|	0.52
55.083	0.00	0.11	0.383	o	|	|	|	|	0.51
55.167	0.00	0.11	0.382	o	|	|	|	|	0.51
55.250	0.00	0.11	0.381	o	|	|	|	|	0.51
55.333	0.00	0.11	0.380	o	|	|	|	|	0.51
55.417	0.00	0.11	0.379	o	|	|	|	|	0.51
55.500	0.00	0.11	0.379	o	|	|	|	|	0.51
55.583	0.00	0.11	0.378	o	|	|	|	|	0.51
55.667	0.00	0.11	0.377	o	|	|	|	|	0.51
55.750	0.00	0.11	0.376	o	|	|	|	|	0.51
55.833	0.00	0.11	0.376	o	|	|	|	|	0.51
55.917	0.00	0.11	0.375	o	|	|	|	|	0.50
56.000	0.00	0.11	0.374	o	|	|	|	|	0.50
56.083	0.00	0.11	0.373	o	|	|	|	|	0.50
56.167	0.00	0.11	0.373	o	|	|	|	|	0.50
56.250	0.00	0.11	0.372	o	|	|	|	|	0.50
56.333	0.00	0.11	0.371	o	|	|	|	|	0.50
56.417	0.00	0.11	0.370	o	|	|	|	|	0.50
56.500	0.00	0.11	0.370	o	|	|	|	|	0.50
56.583	0.00	0.11	0.369	o	|	|	|	|	0.50
56.667	0.00	0.11	0.368	o	|	|	|	|	0.50
56.750	0.00	0.11	0.367	o	|	|	|	|	0.49
56.833	0.00	0.11	0.367	o	|	|	|	|	0.49
56.917	0.00	0.11	0.366	o	|	|	|	|	0.49
57.000	0.00	0.11	0.365	o	|	|	|	|	0.49
57.083	0.00	0.11	0.364	o	|	|	|	|	0.49
57.167	0.00	0.11	0.364	o	|	|	|	|	0.49
57.250	0.00	0.11	0.363	o	|	|	|	|	0.49
57.333	0.00	0.11	0.362	o	|	|	|	|	0.49
57.417	0.00	0.11	0.362	o	|	|	|	|	0.49
57.500	0.00	0.11	0.361	o	|	|	|	|	0.49
57.583	0.00	0.11	0.360	o	|	|	|	|	0.48
57.667	0.00	0.11	0.359	o	|	|	|	|	0.48
57.750	0.00	0.11	0.359	o	|	|	|	|	0.48
57.833	0.00	0.11	0.358	o	|	|	|	|	0.48
57.917	0.00	0.10	0.357	o	|	|	|	|	0.48
58.000	0.00	0.10	0.356	o	|	|	|	|	0.48
58.083	0.00	0.10	0.356	o	|	|	|	|	0.48
58.167	0.00	0.10	0.355	o	|	|	|	|	0.48
58.250	0.00	0.10	0.354	o	|	|	|	|	0.48
58.333	0.00	0.10	0.354	o	|	|	|	|	0.48
58.417	0.00	0.10	0.353	o	|	|	|	|	0.47
58.500	0.00	0.10	0.352	o	|	|	|	|	0.47
58.583	0.00	0.10	0.351	o	|	|	|	|	0.47
58.667	0.00	0.10	0.351	o	|	|	|	|	0.47
58.750	0.00	0.10	0.350	o	|	|	|	|	0.47
58.833	0.00	0.10	0.349	o	|	|	|	|	0.47
58.917	0.00	0.10	0.349	o	|	|	|	|	0.47
59.000	0.00	0.10	0.348	o	|	|	|	|	0.47
59.083	0.00	0.10	0.347	o	|	|	|	|	0.47

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59.167    0.00    0.10      0.347  o       |       |       |       |     0.47
59.250    0.00    0.10      0.346  o       |       |       |       |     0.47
59.333    0.00    0.10      0.345  o       |       |       |       |     0.46
59.417    0.00    0.10      0.344  o       |       |       |       |     0.46
59.500    0.00    0.10      0.344  o       |       |       |       |     0.46
59.583    0.00    0.10      0.343  o       |       |       |       |     0.46
59.667    0.00    0.10      0.342  o       |       |       |       |     0.46
59.750    0.00    0.10      0.342  o       |       |       |       |     0.46
59.833    0.00    0.10      0.341  o       |       |       |       |     0.46
59.917    0.00    0.10      0.340  o       |       |       |       |     0.46

       Remaining water in basin =    0.34 (Ac.Ft)


       ****************************HYDROGRAPH DATA****************************
                     Number of intervals =   719
                     Time interval =    5.0 (Min.)
                     Maximum/Peak flow rate =         0.664 (CFS)
                     Total volume =       1.269 (Ac.Ft)
              Status of hydrographs being held in storage
                         Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
       ***********************************************************************

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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro1565.rte
**********HYDROGRAPH DATA**********
Number of intervals = 77
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 20.558 (CFS)
Total volume = 2.162 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 77
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 5.1 10.28 15.42 20.56	Depth (Ft.)
0.083	0.40	0.00	0.001	O	0.00
0.167	1.08	0.00	0.006	OI	0.01
0.250	1.34	0.00	0.015	O I	0.02
0.333	1.43	0.01	0.024	O I	0.03
0.417	1.47	0.01	0.034	O I	0.05
0.500	1.58	0.01	0.045	O I	0.06
0.583	1.70	0.02	0.056	O I	0.08
0.667	1.73	0.02	0.067	O I	0.09
0.750	1.74	0.02	0.079	O I	0.11
0.833	1.75	0.03	0.091	O I	0.12
0.917	1.75	0.03	0.103	O I	0.14
1.000	1.83	0.03	0.115	O I	0.15
1.083	1.95	0.04	0.128	O I	0.17
1.167	1.98	0.04	0.141	O I	0.19
1.250	1.99	0.05	0.154	O I	0.21
1.333	2.00	0.05	0.168	O I	0.23
1.417	2.00	0.05	0.181	O I	0.24
1.500	2.00	0.06	0.195	O I	0.26
1.583	2.00	0.06	0.208	O I	0.28
1.667	2.00	0.06	0.221	O I	0.30
1.750	2.00	0.07	0.235	O I	0.32

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1.833    2.00    0.07      0.248  O  I    |        |        |        |     0.33
1.917    2.00    0.08      0.261  O  I    |        |        |        |     0.35
2.000    2.08    0.08      0.275  O  I    |        |        |        |     0.37
2.083    2.12    0.08      0.289  O  I    |        |        |        |     0.39
2.167    2.11    0.09      0.302  O  I    |        |        |        |     0.41
2.250    2.21    0.09      0.317  O  I    |        |        |        |     0.43
2.333    2.23    0.10      0.331  O  I    |        |        |        |     0.45
2.417    2.24    0.10      0.346  O  I    |        |        |        |     0.47
2.500    2.25    0.11      0.361  O  I    |        |        |        |     0.49
2.583    2.25    0.11      0.376  O  I    |        |        |        |     0.51
2.667    2.25    0.11      0.390  O  I    |        |        |        |     0.53
2.750    2.33    0.12      0.405  O  I    |        |        |        |     0.55
2.833    2.45    0.12      0.421  O  I    |        |        |        |     0.57
2.917    2.48    0.13      0.437  O  I    |        |        |        |     0.59
3.000    2.49    0.13      0.453  O  I    |        |        |        |     0.61
3.083    2.50    0.14      0.469  O  I    |        |        |        |     0.63
3.167    2.58    0.14      0.486  O   I   |        |        |        |     0.65
3.250    2.70    0.15      0.503  O   I   |        |        |        |     0.68
3.333    2.73    0.15      0.521  O   I   |        |        |        |     0.70
3.417    2.82    0.16      0.539  O   I   |        |        |        |     0.73
3.500    3.03    0.16      0.558  O   I   |        |        |        |     0.75
3.583    3.26    0.17      0.578  O    I  |        |        |        |     0.78
3.667    3.42    0.18      0.600  O    I  |        |        |        |     0.81
3.750    3.57    0.18      0.623  O    I  |        |        |        |     0.84
3.833    3.76    0.19      0.647  O    I  |        |        |        |     0.87
3.917    3.97    0.20      0.672  O     I |        |        |        |     0.90
4.000    4.23    0.21      0.699  O     I |        |        |        |     0.94
4.083    4.46    0.21      0.727  O     I |        |        |        |     0.98
4.167    4.88    0.23      0.758  O      I|        |        |        |     1.02
4.250    5.35    0.24      0.792  O       I        |        |        |     1.06
4.333    5.84    0.27      0.829  O       |I       |        |        |     1.10
4.417    6.33    0.29      0.869  O       |I       |        |        |     1.15
4.500    6.67    0.31      0.911  O        | I     |        |        |     1.21
4.583    6.93    0.34      0.956  O        | I     |        |        |     1.26
4.667    7.38    0.36      1.003  O        |  I    |        |        |     1.32
4.750    7.85    0.39      1.053  O        |   I   |        |        |     1.38
4.833    8.18    0.42      1.105  O        |   I   |        |        |     1.44
4.917    8.43    0.45      1.159  O        |    I  |        |        |     1.51
5.000    8.88    0.48      1.216  O        |    I  |        |        |     1.58
5.083   10.00    0.51      1.277  O        |      I|        |        |     1.65
5.167   12.08    0.55      1.350  O        |       | I      |        |     1.74
5.250   14.07    0.60      1.436  O        |       |    I   |        |     1.85
5.333   15.69    0.65      1.534  |O       |       |      I |        |     1.97
5.417   17.57    0.75      1.644  |O       |       |        |  I     |     2.09
5.500   20.56    0.87      1.769  |O       |       |        |       I|     2.23
5.583   17.12    0.98      1.893  |O       |       |        | I      |     2.37
5.667    7.92    1.06      1.972  |O       |   I   |        |        |     2.46
5.750    4.18    1.09      2.006  |O    I  |       |        |        |     2.50
5.833    2.57    1.11      2.022  |O  I    |       |        |        |     2.51
5.917    1.62    1.11      2.029  |OI      |       |        |        |     2.52
6.000    0.88    1.11      2.030  |O       |       |        |        |     2.52
6.083    0.45    1.11      2.027  IO       |       |        |        |     2.52
6.167    0.15    1.10      2.021  IO       |       |        |        |     2.51
6.250    0.06    1.10      2.014  IO       |       |        |        |     2.51
6.333    0.02    1.09      2.007  IO       |       |        |        |     2.50
6.417    0.01    1.08      1.999  IO       |       |        |        |     2.49
6.500    0.00    1.08      1.992  IO       |       |        |        |     2.48
6.583    0.00    1.07      1.985  IO       |       |        |        |     2.47
6.667    0.00    1.06      1.977  IO       |       |        |        |     2.47
6.750    0.00    1.06      1.970  IO       |       |        |        |     2.46
6.833    0.00    1.05      1.963  IO       |       |        |        |     2.45
6.917    0.00    1.04      1.956  IO       |       |        |        |     2.44
7.000    0.00    1.04      1.948  IO       |       |        |        |     2.43
7.083    0.00    1.03      1.941  IO       |       |        |        |     2.42
7.167    0.00    1.02      1.934  IO       |       |        |        |     2.42
7.250    0.00    1.02      1.927  IO       |       |        |        |     2.41
7.333    0.00    1.01      1.920  IO       |       |        |        |     2.40
7.417    0.00    1.00      1.913  IO       |       |        |        |     2.39
7.500    0.00    1.00      1.906  IO       |       |        |        |     2.39
7.583    0.00    0.99      1.900  IO       |       |        |        |     2.38
7.667    0.00    0.98      1.893  IO       |       |        |        |     2.37
7.750    0.00    0.98      1.886  IO       |       |        |        |     2.36
7.833    0.00    0.97      1.879  IO       |       |        |        |     2.36
7.917    0.00    0.96      1.873  IO       |       |        |        |     2.35
8.000    0.00    0.96      1.866  IO       |       |        |        |     2.34
8.083    0.00    0.95      1.859  IO       |       |        |        |     2.33
8.167    0.00    0.95      1.853  IO       |       |        |        |     2.33
8.250    0.00    0.94      1.846  IO       |       |        |        |     2.32
8.333    0.00    0.93      1.840  IO       |       |        |        |     2.31
8.417    0.00    0.93      1.834  IO       |       |        |        |     2.30
8.500    0.00    0.92      1.827  IO       |       |        |        |     2.30
8.583    0.00    0.91      1.821  IO       |       |        |        |     2.29
8.667    0.00    0.91      1.815  IO       |       |        |        |     2.28
8.750    0.00    0.90      1.808  IO       |       |        |        |     2.28
8.833    0.00    0.90      1.802  IO       |       |        |        |     2.27
8.917    0.00    0.89      1.796  IO       |       |        |        |     2.26
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9.000	0.00	0.89	1.790	IO				2.26
9.083	0.00	0.88	1.784	IO				2.25
9.167	0.00	0.87	1.778	IO				2.24
9.250	0.00	0.87	1.772	IO				2.24
9.333	0.00	0.86	1.766	IO				2.23
9.417	0.00	0.86	1.760	IO				2.22
9.500	0.00	0.85	1.754	IO				2.22
9.583	0.00	0.85	1.748	IO				2.21
9.667	0.00	0.84	1.742	IO				2.20
9.750	0.00	0.83	1.737	IO				2.20
9.833	0.00	0.83	1.731	IO				2.19
9.917	0.00	0.82	1.725	IO				2.18
10.000	0.00	0.82	1.720	IO				2.18
10.083	0.00	0.81	1.714	IO				2.17
10.167	0.00	0.81	1.708	IO				2.16
10.250	0.00	0.80	1.703	IO				2.16
10.333	0.00	0.80	1.697	IO				2.15
10.417	0.00	0.79	1.692	IO				2.15
10.500	0.00	0.79	1.686	IO				2.14
10.583	0.00	0.78	1.681	IO				2.13
10.667	0.00	0.78	1.676	IO				2.13
10.750	0.00	0.77	1.670	IO				2.12
10.833	0.00	0.77	1.665	IO				2.12
10.917	0.00	0.76	1.660	IO				2.11
11.000	0.00	0.76	1.654	IO				2.10
11.083	0.00	0.75	1.649	IO				2.10
11.167	0.00	0.75	1.644	IO				2.09
11.250	0.00	0.74	1.639	IO				2.09
11.333	0.00	0.74	1.634	IO				2.08
11.417	0.00	0.73	1.629	IO				2.08
11.500	0.00	0.73	1.624	IO				2.07
11.583	0.00	0.72	1.619	IO				2.06
11.667	0.00	0.72	1.614	IO				2.06
11.750	0.00	0.71	1.609	IO				2.05
11.833	0.00	0.71	1.604	IO				2.05
11.917	0.00	0.70	1.599	IO				2.04
12.000	0.00	0.70	1.594	IO				2.04
12.083	0.00	0.70	1.590	IO				2.03
12.167	0.00	0.69	1.585	IO				2.03
12.250	0.00	0.69	1.580	IO				2.02
12.333	0.00	0.68	1.575	IO				2.02
12.417	0.00	0.68	1.571	IO				2.01
12.500	0.00	0.67	1.566	IO				2.01
12.583	0.00	0.67	1.561	IO				2.00
12.667	0.00	0.67	1.557	IO				1.99
12.750	0.00	0.66	1.552	IO				1.99
12.833	0.00	0.66	1.548	IO				1.98
12.917	0.00	0.66	1.543	IO				1.98
13.000	0.00	0.66	1.539	IO				1.97
13.083	0.00	0.65	1.534	IO				1.97
13.167	0.00	0.65	1.530	IO				1.96
13.250	0.00	0.65	1.525	IO				1.96
13.333	0.00	0.65	1.521	IO				1.95
13.417	0.00	0.64	1.516	IO				1.95
13.500	0.00	0.64	1.512	O				1.94
13.583	0.00	0.64	1.507	O				1.93
13.667	0.00	0.64	1.503	O				1.93
13.750	0.00	0.63	1.499	O				1.92
13.833	0.00	0.63	1.494	O				1.92
13.917	0.00	0.63	1.490	O				1.91
14.000	0.00	0.63	1.486	O				1.91
14.083	0.00	0.62	1.481	O				1.90
14.167	0.00	0.62	1.477	O				1.90
14.250	0.00	0.62	1.473	O				1.89
14.333	0.00	0.62	1.468	O				1.89
14.417	0.00	0.61	1.464	O				1.88
14.500	0.00	0.61	1.460	O				1.88
14.583	0.00	0.61	1.456	O				1.87
14.667	0.00	0.61	1.452	O				1.87
14.750	0.00	0.61	1.447	O				1.86
14.833	0.00	0.60	1.443	O				1.86
14.917	0.00	0.60	1.439	O				1.85
15.000	0.00	0.60	1.435	O				1.85
15.083	0.00	0.60	1.431	O				1.84
15.167	0.00	0.59	1.427	O				1.84
15.250	0.00	0.59	1.423	O				1.83
15.333	0.00	0.59	1.419	O				1.83
15.417	0.00	0.59	1.415	O				1.82
15.500	0.00	0.59	1.411	O				1.82
15.583	0.00	0.58	1.406	O				1.81
15.667	0.00	0.58	1.402	O				1.81
15.750	0.00	0.58	1.398	O				1.80
15.833	0.00	0.58	1.395	O				1.80
15.917	0.00	0.57	1.391	O				1.79
16.000	0.00	0.57	1.387	O				1.79
16.083	0.00	0.57	1.383	O				1.78

16.167	0.00	0.57	1.379	o	|	|	|	|	1.78
16.250	0.00	0.57	1.375	o	|	|	|	|	1.77
16.333	0.00	0.56	1.371	o	|	|	|	|	1.77
16.417	0.00	0.56	1.367	o	|	|	|	|	1.76
16.500	0.00	0.56	1.363	o	|	|	|	|	1.76
16.583	0.00	0.56	1.359	o	|	|	|	|	1.75
16.667	0.00	0.55	1.356	o	|	|	|	|	1.75
16.750	0.00	0.55	1.352	o	|	|	|	|	1.74
16.833	0.00	0.55	1.348	o	|	|	|	|	1.74
16.917	0.00	0.55	1.344	o	|	|	|	|	1.73
17.000	0.00	0.55	1.340	o	|	|	|	|	1.73
17.083	0.00	0.54	1.337	o	|	|	|	|	1.73
17.167	0.00	0.54	1.333	o	|	|	|	|	1.72
17.250	0.00	0.54	1.329	o	|	|	|	|	1.72
17.333	0.00	0.54	1.325	o	|	|	|	|	1.71
17.417	0.00	0.54	1.322	o	|	|	|	|	1.71
17.500	0.00	0.53	1.318	o	|	|	|	|	1.70
17.583	0.00	0.53	1.314	o	|	|	|	|	1.70
17.667	0.00	0.53	1.311	o	|	|	|	|	1.69
17.750	0.00	0.53	1.307	o	|	|	|	|	1.69
17.833	0.00	0.53	1.303	o	|	|	|	|	1.69
17.917	0.00	0.52	1.300	o	|	|	|	|	1.68
18.000	0.00	0.52	1.296	o	|	|	|	|	1.68
18.083	0.00	0.52	1.293	o	|	|	|	|	1.67
18.167	0.00	0.52	1.289	o	|	|	|	|	1.67
18.250	0.00	0.52	1.285	o	|	|	|	|	1.66
18.333	0.00	0.51	1.282	o	|	|	|	|	1.66
18.417	0.00	0.51	1.278	o	|	|	|	|	1.65
18.500	0.00	0.51	1.275	o	|	|	|	|	1.65
18.583	0.00	0.51	1.271	o	|	|	|	|	1.65
18.667	0.00	0.51	1.268	o	|	|	|	|	1.64
18.750	0.00	0.50	1.264	o	|	|	|	|	1.64
18.833	0.00	0.50	1.261	o	|	|	|	|	1.63
18.917	0.00	0.50	1.257	o	|	|	|	|	1.63
19.000	0.00	0.50	1.254	o	|	|	|	|	1.62
19.083	0.00	0.50	1.251	o	|	|	|	|	1.62
19.167	0.00	0.50	1.247	o	|	|	|	|	1.62
19.250	0.00	0.49	1.244	o	|	|	|	|	1.61
19.333	0.00	0.49	1.240	o	|	|	|	|	1.61
19.417	0.00	0.49	1.237	o	|	|	|	|	1.60
19.500	0.00	0.49	1.234	o	|	|	|	|	1.60
19.583	0.00	0.49	1.230	o	|	|	|	|	1.60
19.667	0.00	0.48	1.227	o	|	|	|	|	1.59
19.750	0.00	0.48	1.224	o	|	|	|	|	1.59
19.833	0.00	0.48	1.220	o	|	|	|	|	1.58
19.917	0.00	0.48	1.217	o	|	|	|	|	1.58
20.000	0.00	0.48	1.214	o	|	|	|	|	1.58
20.083	0.00	0.48	1.210	o	|	|	|	|	1.57
20.167	0.00	0.47	1.207	o	|	|	|	|	1.57
20.250	0.00	0.47	1.204	o	|	|	|	|	1.56
20.333	0.00	0.47	1.201	o	|	|	|	|	1.56
20.417	0.00	0.47	1.197	o	|	|	|	|	1.56
20.500	0.00	0.47	1.194	o	|	|	|	|	1.55
20.583	0.00	0.46	1.191	o	|	|	|	|	1.55
20.667	0.00	0.46	1.188	o	|	|	|	|	1.54
20.750	0.00	0.46	1.185	o	|	|	|	|	1.54
20.833	0.00	0.46	1.181	o	|	|	|	|	1.54
20.917	0.00	0.46	1.178	o	|	|	|	|	1.53
21.000	0.00	0.46	1.175	o	|	|	|	|	1.53
21.083	0.00	0.45	1.172	o	|	|	|	|	1.52
21.167	0.00	0.45	1.169	o	|	|	|	|	1.52
21.250	0.00	0.45	1.166	o	|	|	|	|	1.52
21.333	0.00	0.45	1.163	o	|	|	|	|	1.51
21.417	0.00	0.45	1.160	o	|	|	|	|	1.51
21.500	0.00	0.45	1.157	o	|	|	|	|	1.51
21.583	0.00	0.44	1.153	o	|	|	|	|	1.50
21.667	0.00	0.44	1.150	o	|	|	|	|	1.50
21.750	0.00	0.44	1.147	o	|	|	|	|	1.49
21.833	0.00	0.44	1.144	o	|	|	|	|	1.49
21.917	0.00	0.44	1.141	o	|	|	|	|	1.49
22.000	0.00	0.44	1.138	o	|	|	|	|	1.48
22.083	0.00	0.43	1.135	o	|	|	|	|	1.48
22.167	0.00	0.43	1.132	o	|	|	|	|	1.48
22.250	0.00	0.43	1.129	o	|	|	|	|	1.47
22.333	0.00	0.43	1.126	o	|	|	|	|	1.47
22.417	0.00	0.43	1.123	o	|	|	|	|	1.47
22.500	0.00	0.43	1.121	o	|	|	|	|	1.46
22.583	0.00	0.42	1.118	o	|	|	|	|	1.46
22.667	0.00	0.42	1.115	o	|	|	|	|	1.45
22.750	0.00	0.42	1.112	o	|	|	|	|	1.45
22.833	0.00	0.42	1.109	o	|	|	|	|	1.45
22.917	0.00	0.42	1.106	o	|	|	|	|	1.44
23.000	0.00	0.42	1.103	o	|	|	|	|	1.44
23.083	0.00	0.41	1.100	o	|	|	|	|	1.44
23.167	0.00	0.41	1.097	o	|	|	|	|	1.43
23.250	0.00	0.41	1.095	o	|	|	|	|	1.43

23.333	0.00	0.41	1.092	o	|	|	|	|	1.43
23.417	0.00	0.41	1.089	o	|	|	|	|	1.42
23.500	0.00	0.41	1.086	o	|	|	|	|	1.42
23.583	0.00	0.41	1.083	o	|	|	|	|	1.42
23.667	0.00	0.40	1.081	o	|	|	|	|	1.41
23.750	0.00	0.40	1.078	o	|	|	|	|	1.41
23.833	0.00	0.40	1.075	o	|	|	|	|	1.41
23.917	0.00	0.40	1.072	o	|	|	|	|	1.40
24.000	0.00	0.40	1.070	o	|	|	|	|	1.40
24.083	0.00	0.40	1.067	o	|	|	|	|	1.40
24.167	0.00	0.39	1.064	o	|	|	|	|	1.39
24.250	0.00	0.39	1.061	o	|	|	|	|	1.39
24.333	0.00	0.39	1.059	o	|	|	|	|	1.39
24.417	0.00	0.39	1.056	o	|	|	|	|	1.38
24.500	0.00	0.39	1.053	o	|	|	|	|	1.38
24.583	0.00	0.39	1.051	o	|	|	|	|	1.38
24.667	0.00	0.39	1.048	o	|	|	|	|	1.37
24.750	0.00	0.38	1.045	o	|	|	|	|	1.37
24.833	0.00	0.38	1.043	o	|	|	|	|	1.37
24.917	0.00	0.38	1.040	o	|	|	|	|	1.36
25.000	0.00	0.38	1.037	o	|	|	|	|	1.36
25.083	0.00	0.38	1.035	o	|	|	|	|	1.36
25.167	0.00	0.38	1.032	o	|	|	|	|	1.35
25.250	0.00	0.38	1.030	o	|	|	|	|	1.35
25.333	0.00	0.37	1.027	o	|	|	|	|	1.35
25.417	0.00	0.37	1.024	o	|	|	|	|	1.34
25.500	0.00	0.37	1.022	o	|	|	|	|	1.34
25.583	0.00	0.37	1.019	o	|	|	|	|	1.34
25.667	0.00	0.37	1.017	o	|	|	|	|	1.33
25.750	0.00	0.37	1.014	o	|	|	|	|	1.33
25.833	0.00	0.37	1.012	o	|	|	|	|	1.33
25.917	0.00	0.36	1.009	o	|	|	|	|	1.33
26.000	0.00	0.36	1.007	o	|	|	|	|	1.32
26.083	0.00	0.36	1.004	o	|	|	|	|	1.32
26.167	0.00	0.36	1.002	o	|	|	|	|	1.32
26.250	0.00	0.36	0.999	o	|	|	|	|	1.31
26.333	0.00	0.36	0.997	o	|	|	|	|	1.31
26.417	0.00	0.36	0.994	o	|	|	|	|	1.31
26.500	0.00	0.35	0.992	o	|	|	|	|	1.30
26.583	0.00	0.35	0.989	o	|	|	|	|	1.30
26.667	0.00	0.35	0.987	o	|	|	|	|	1.30
26.750	0.00	0.35	0.985	o	|	|	|	|	1.30
26.833	0.00	0.35	0.982	o	|	|	|	|	1.29
26.917	0.00	0.35	0.980	o	|	|	|	|	1.29
27.000	0.00	0.35	0.977	o	|	|	|	|	1.29
27.083	0.00	0.35	0.975	o	|	|	|	|	1.28
27.167	0.00	0.34	0.973	o	|	|	|	|	1.28
27.250	0.00	0.34	0.970	o	|	|	|	|	1.28
27.333	0.00	0.34	0.968	o	|	|	|	|	1.27
27.417	0.00	0.34	0.966	o	|	|	|	|	1.27
27.500	0.00	0.34	0.963	o	|	|	|	|	1.27
27.583	0.00	0.34	0.961	o	|	|	|	|	1.27
27.667	0.00	0.34	0.959	o	|	|	|	|	1.26
27.750	0.00	0.34	0.956	o	|	|	|	|	1.26
27.833	0.00	0.33	0.954	o	|	|	|	|	1.26
27.917	0.00	0.33	0.952	o	|	|	|	|	1.26
28.000	0.00	0.33	0.949	o	|	|	|	|	1.25
28.083	0.00	0.33	0.947	o	|	|	|	|	1.25
28.167	0.00	0.33	0.945	o	|	|	|	|	1.25
28.250	0.00	0.33	0.943	o	|	|	|	|	1.24
28.333	0.00	0.33	0.940	o	|	|	|	|	1.24
28.417	0.00	0.33	0.938	o	|	|	|	|	1.24
28.500	0.00	0.32	0.936	o	|	|	|	|	1.24
28.583	0.00	0.32	0.934	o	|	|	|	|	1.23
28.667	0.00	0.32	0.931	o	|	|	|	|	1.23
28.750	0.00	0.32	0.929	o	|	|	|	|	1.23
28.833	0.00	0.32	0.927	o	|	|	|	|	1.22
28.917	0.00	0.32	0.925	o	|	|	|	|	1.22
29.000	0.00	0.32	0.923	o	|	|	|	|	1.22
29.083	0.00	0.32	0.920	o	|	|	|	|	1.22
29.167	0.00	0.31	0.918	o	|	|	|	|	1.21
29.250	0.00	0.31	0.916	o	|	|	|	|	1.21
29.333	0.00	0.31	0.914	o	|	|	|	|	1.21
29.417	0.00	0.31	0.912	o	|	|	|	|	1.21
29.500	0.00	0.31	0.910	o	|	|	|	|	1.20
29.583	0.00	0.31	0.907	o	|	|	|	|	1.20
29.667	0.00	0.31	0.905	o	|	|	|	|	1.20
29.750	0.00	0.31	0.903	o	|	|	|	|	1.20
29.833	0.00	0.31	0.901	o	|	|	|	|	1.19
29.917	0.00	0.30	0.899	o	|	|	|	|	1.19
30.000	0.00	0.30	0.897	o	|	|	|	|	1.19
30.083	0.00	0.30	0.895	o	|	|	|	|	1.19
30.167	0.00	0.30	0.893	o	|	|	|	|	1.18
30.250	0.00	0.30	0.891	o	|	|	|	|	1.18
30.333	0.00	0.30	0.889	o	|	|	|	|	1.18
30.417	0.00	0.30	0.887	o	|	|	|	|	1.18

30.500	0.00	0.30	0.885	o	|	|	|	|	1.17
30.583	0.00	0.29	0.883	o	|	|	|	|	1.17
30.667	0.00	0.29	0.881	o	|	|	|	|	1.17
30.750	0.00	0.29	0.879	o	|	|	|	|	1.17
30.833	0.00	0.29	0.877	o	|	|	|	|	1.16
30.917	0.00	0.29	0.875	o	|	|	|	|	1.16
31.000	0.00	0.29	0.873	o	|	|	|	|	1.16
31.083	0.00	0.29	0.871	o	|	|	|	|	1.16
31.167	0.00	0.29	0.869	o	|	|	|	|	1.15
31.250	0.00	0.29	0.867	o	|	|	|	|	1.15
31.333	0.00	0.28	0.865	o	|	|	|	|	1.15
31.417	0.00	0.28	0.863	o	|	|	|	|	1.15
31.500	0.00	0.28	0.861	o	|	|	|	|	1.14
31.583	0.00	0.28	0.859	o	|	|	|	|	1.14
31.667	0.00	0.28	0.857	o	|	|	|	|	1.14
31.750	0.00	0.28	0.855	o	|	|	|	|	1.14
31.833	0.00	0.28	0.853	o	|	|	|	|	1.13
31.917	0.00	0.28	0.851	o	|	|	|	|	1.13
32.000	0.00	0.28	0.849	o	|	|	|	|	1.13
32.083	0.00	0.28	0.847	o	|	|	|	|	1.13
32.167	0.00	0.27	0.845	o	|	|	|	|	1.13
32.250	0.00	0.27	0.843	o	|	|	|	|	1.12
32.333	0.00	0.27	0.842	o	|	|	|	|	1.12
32.417	0.00	0.27	0.840	o	|	|	|	|	1.12
32.500	0.00	0.27	0.838	o	|	|	|	|	1.12
32.583	0.00	0.27	0.836	o	|	|	|	|	1.11
32.667	0.00	0.27	0.834	o	|	|	|	|	1.11
32.750	0.00	0.27	0.832	o	|	|	|	|	1.11
32.833	0.00	0.27	0.830	o	|	|	|	|	1.11
32.917	0.00	0.27	0.829	o	|	|	|	|	1.10
33.000	0.00	0.26	0.827	o	|	|	|	|	1.10
33.083	0.00	0.26	0.825	o	|	|	|	|	1.10
33.167	0.00	0.26	0.823	o	|	|	|	|	1.10
33.250	0.00	0.26	0.821	o	|	|	|	|	1.10
33.333	0.00	0.26	0.820	o	|	|	|	|	1.09
33.417	0.00	0.26	0.818	o	|	|	|	|	1.09
33.500	0.00	0.26	0.816	o	|	|	|	|	1.09
33.583	0.00	0.26	0.814	o	|	|	|	|	1.09
33.667	0.00	0.26	0.812	o	|	|	|	|	1.08
33.750	0.00	0.26	0.811	o	|	|	|	|	1.08
33.833	0.00	0.25	0.809	o	|	|	|	|	1.08
33.917	0.00	0.25	0.807	o	|	|	|	|	1.08
34.000	0.00	0.25	0.805	o	|	|	|	|	1.08
34.083	0.00	0.25	0.804	o	|	|	|	|	1.07
34.167	0.00	0.25	0.802	o	|	|	|	|	1.07
34.250	0.00	0.25	0.800	o	|	|	|	|	1.07
34.333	0.00	0.25	0.799	o	|	|	|	|	1.07
34.417	0.00	0.25	0.797	o	|	|	|	|	1.07
34.500	0.00	0.25	0.795	o	|	|	|	|	1.06
34.583	0.00	0.25	0.793	o	|	|	|	|	1.06
34.667	0.00	0.24	0.792	o	|	|	|	|	1.06
34.750	0.00	0.24	0.790	o	|	|	|	|	1.06
34.833	0.00	0.24	0.788	o	|	|	|	|	1.06
34.917	0.00	0.24	0.787	o	|	|	|	|	1.05
35.000	0.00	0.24	0.785	o	|	|	|	|	1.05
35.083	0.00	0.24	0.783	o	|	|	|	|	1.05
35.167	0.00	0.24	0.782	o	|	|	|	|	1.05
35.250	0.00	0.24	0.780	o	|	|	|	|	1.05
35.333	0.00	0.24	0.778	o	|	|	|	|	1.04
35.417	0.00	0.24	0.777	o	|	|	|	|	1.04
35.500	0.00	0.24	0.775	o	|	|	|	|	1.04
35.583	0.00	0.23	0.774	o	|	|	|	|	1.04
35.667	0.00	0.23	0.772	o	|	|	|	|	1.04
35.750	0.00	0.23	0.770	o	|	|	|	|	1.03
35.833	0.00	0.23	0.769	o	|	|	|	|	1.03
35.917	0.00	0.23	0.767	o	|	|	|	|	1.03
36.000	0.00	0.23	0.766	o	|	|	|	|	1.03
36.083	0.00	0.23	0.764	o	|	|	|	|	1.03
36.167	0.00	0.23	0.762	o	|	|	|	|	1.02
36.250	0.00	0.23	0.761	o	|	|	|	|	1.02
36.333	0.00	0.23	0.759	o	|	|	|	|	1.02
36.417	0.00	0.23	0.758	o	|	|	|	|	1.02
36.500	0.00	0.23	0.756	o	|	|	|	|	1.02
36.583	0.00	0.22	0.755	o	|	|	|	|	1.01
36.667	0.00	0.22	0.753	o	|	|	|	|	1.01
36.750	0.00	0.22	0.752	o	|	|	|	|	1.01
36.833	0.00	0.22	0.750	o	|	|	|	|	1.01
36.917	0.00	0.22	0.748	o	|	|	|	|	1.01
37.000	0.00	0.22	0.747	o	|	|	|	|	1.00
37.083	0.00	0.22	0.745	o	|	|	|	|	1.00
37.167	0.00	0.22	0.744	o	|	|	|	|	1.00
37.250	0.00	0.22	0.742	o	|	|	|	|	1.00
37.333	0.00	0.22	0.741	o	|	|	|	|	1.00
37.417	0.00	0.22	0.739	o	|	|	|	|	1.00
37.500	0.00	0.22	0.738	o	|	|	|	|	0.99
37.583	0.00	0.22	0.736	o	|	|	|	|	0.99

37.667	0.00	0.22	0.735	o	|	|	|	|	0.99
37.750	0.00	0.22	0.734	o	|	|	|	|	0.99
37.833	0.00	0.21	0.732	o	|	|	|	|	0.99
37.917	0.00	0.21	0.731	o	|	|	|	|	0.98
38.000	0.00	0.21	0.729	o	|	|	|	|	0.98
38.083	0.00	0.21	0.728	o	|	|	|	|	0.98
38.167	0.00	0.21	0.726	o	|	|	|	|	0.98
38.250	0.00	0.21	0.725	o	|	|	|	|	0.98
38.333	0.00	0.21	0.723	o	|	|	|	|	0.97
38.417	0.00	0.21	0.722	o	|	|	|	|	0.97
38.500	0.00	0.21	0.720	o	|	|	|	|	0.97
38.583	0.00	0.21	0.719	o	|	|	|	|	0.97
38.667	0.00	0.21	0.717	o	|	|	|	|	0.97
38.750	0.00	0.21	0.716	o	|	|	|	|	0.96
38.833	0.00	0.21	0.714	o	|	|	|	|	0.96
38.917	0.00	0.21	0.713	o	|	|	|	|	0.96
39.000	0.00	0.21	0.712	o	|	|	|	|	0.96
39.083	0.00	0.21	0.710	o	|	|	|	|	0.96
39.167	0.00	0.21	0.709	o	|	|	|	|	0.95
39.250	0.00	0.21	0.707	o	|	|	|	|	0.95
39.333	0.00	0.21	0.706	o	|	|	|	|	0.95
39.417	0.00	0.21	0.704	o	|	|	|	|	0.95
39.500	0.00	0.21	0.703	o	|	|	|	|	0.95
39.583	0.00	0.21	0.702	o	|	|	|	|	0.94
39.667	0.00	0.21	0.700	o	|	|	|	|	0.94
39.750	0.00	0.21	0.699	o	|	|	|	|	0.94
39.833	0.00	0.20	0.697	o	|	|	|	|	0.94
39.917	0.00	0.20	0.696	o	|	|	|	|	0.94
40.000	0.00	0.20	0.695	o	|	|	|	|	0.93
40.083	0.00	0.20	0.693	o	|	|	|	|	0.93
40.167	0.00	0.20	0.692	o	|	|	|	|	0.93
40.250	0.00	0.20	0.690	o	|	|	|	|	0.93
40.333	0.00	0.20	0.689	o	|	|	|	|	0.93
40.417	0.00	0.20	0.688	o	|	|	|	|	0.93
40.500	0.00	0.20	0.686	o	|	|	|	|	0.92
40.583	0.00	0.20	0.685	o	|	|	|	|	0.92
40.667	0.00	0.20	0.683	o	|	|	|	|	0.92
40.750	0.00	0.20	0.682	o	|	|	|	|	0.92
40.833	0.00	0.20	0.681	o	|	|	|	|	0.92
40.917	0.00	0.20	0.679	o	|	|	|	|	0.91
41.000	0.00	0.20	0.678	o	|	|	|	|	0.91
41.083	0.00	0.20	0.677	o	|	|	|	|	0.91
41.167	0.00	0.20	0.675	o	|	|	|	|	0.91
41.250	0.00	0.20	0.674	o	|	|	|	|	0.91
41.333	0.00	0.20	0.672	o	|	|	|	|	0.91
41.417	0.00	0.20	0.671	o	|	|	|	|	0.90
41.500	0.00	0.20	0.670	o	|	|	|	|	0.90
41.583	0.00	0.20	0.668	o	|	|	|	|	0.90
41.667	0.00	0.20	0.667	o	|	|	|	|	0.90
41.750	0.00	0.20	0.666	o	|	|	|	|	0.90
41.833	0.00	0.19	0.664	o	|	|	|	|	0.89
41.917	0.00	0.19	0.663	o	|	|	|	|	0.89
42.000	0.00	0.19	0.662	o	|	|	|	|	0.89
42.083	0.00	0.19	0.660	o	|	|	|	|	0.89
42.167	0.00	0.19	0.659	o	|	|	|	|	0.89
42.250	0.00	0.19	0.658	o	|	|	|	|	0.89
42.333	0.00	0.19	0.656	o	|	|	|	|	0.88
42.417	0.00	0.19	0.655	o	|	|	|	|	0.88
42.500	0.00	0.19	0.654	o	|	|	|	|	0.88
42.583	0.00	0.19	0.652	o	|	|	|	|	0.88
42.667	0.00	0.19	0.651	o	|	|	|	|	0.88
42.750	0.00	0.19	0.650	o	|	|	|	|	0.87
42.833	0.00	0.19	0.648	o	|	|	|	|	0.87
42.917	0.00	0.19	0.647	o	|	|	|	|	0.87
43.000	0.00	0.19	0.646	o	|	|	|	|	0.87
43.083	0.00	0.19	0.645	o	|	|	|	|	0.87
43.167	0.00	0.19	0.643	o	|	|	|	|	0.87
43.250	0.00	0.19	0.642	o	|	|	|	|	0.86
43.333	0.00	0.19	0.641	o	|	|	|	|	0.86
43.417	0.00	0.19	0.639	o	|	|	|	|	0.86
43.500	0.00	0.19	0.638	o	|	|	|	|	0.86
43.583	0.00	0.19	0.637	o	|	|	|	|	0.86
43.667	0.00	0.19	0.635	o	|	|	|	|	0.86
43.750	0.00	0.19	0.634	o	|	|	|	|	0.85
43.833	0.00	0.19	0.633	o	|	|	|	|	0.85
43.917	0.00	0.19	0.632	o	|	|	|	|	0.85
44.000	0.00	0.18	0.630	o	|	|	|	|	0.85
44.083	0.00	0.18	0.629	o	|	|	|	|	0.85
44.167	0.00	0.18	0.628	o	|	|	|	|	0.84
44.250	0.00	0.18	0.627	o	|	|	|	|	0.84
44.333	0.00	0.18	0.625	o	|	|	|	|	0.84
44.417	0.00	0.18	0.624	o	|	|	|	|	0.84
44.500	0.00	0.18	0.623	o	|	|	|	|	0.84
44.583	0.00	0.18	0.622	o	|	|	|	|	0.84
44.667	0.00	0.18	0.620	o	|	|	|	|	0.83
44.750	0.00	0.18	0.619	o	|	|	|	|	0.83

44.833	0.00	0.18	0.618	o	|	|	|	|	0.83
44.917	0.00	0.18	0.617	o	|	|	|	|	0.83
45.000	0.00	0.18	0.615	o	|	|	|	|	0.83
45.083	0.00	0.18	0.614	o	|	|	|	|	0.83
45.167	0.00	0.18	0.613	o	|	|	|	|	0.82
45.250	0.00	0.18	0.612	o	|	|	|	|	0.82
45.333	0.00	0.18	0.610	o	|	|	|	|	0.82
45.417	0.00	0.18	0.609	o	|	|	|	|	0.82
45.500	0.00	0.18	0.608	o	|	|	|	|	0.82
45.583	0.00	0.18	0.607	o	|	|	|	|	0.82
45.667	0.00	0.18	0.605	o	|	|	|	|	0.81
45.750	0.00	0.18	0.604	o	|	|	|	|	0.81
45.833	0.00	0.18	0.603	o	|	|	|	|	0.81
45.917	0.00	0.18	0.602	o	|	|	|	|	0.81
46.000	0.00	0.18	0.601	o	|	|	|	|	0.81
46.083	0.00	0.18	0.599	o	|	|	|	|	0.81
46.167	0.00	0.18	0.598	o	|	|	|	|	0.80
46.250	0.00	0.18	0.597	o	|	|	|	|	0.80
46.333	0.00	0.17	0.596	o	|	|	|	|	0.80
46.417	0.00	0.17	0.594	o	|	|	|	|	0.80
46.500	0.00	0.17	0.593	o	|	|	|	|	0.80
46.583	0.00	0.17	0.592	o	|	|	|	|	0.80
46.667	0.00	0.17	0.591	o	|	|	|	|	0.80
46.750	0.00	0.17	0.590	o	|	|	|	|	0.79
46.833	0.00	0.17	0.589	o	|	|	|	|	0.79
46.917	0.00	0.17	0.587	o	|	|	|	|	0.79
47.000	0.00	0.17	0.586	o	|	|	|	|	0.79
47.083	0.00	0.17	0.585	o	|	|	|	|	0.79
47.167	0.00	0.17	0.584	o	|	|	|	|	0.79
47.250	0.00	0.17	0.583	o	|	|	|	|	0.78
47.333	0.00	0.17	0.581	o	|	|	|	|	0.78
47.417	0.00	0.17	0.580	o	|	|	|	|	0.78
47.500	0.00	0.17	0.579	o	|	|	|	|	0.78
47.583	0.00	0.17	0.578	o	|	|	|	|	0.78
47.667	0.00	0.17	0.577	o	|	|	|	|	0.78
47.750	0.00	0.17	0.576	o	|	|	|	|	0.77
47.833	0.00	0.17	0.574	o	|	|	|	|	0.77
47.917	0.00	0.17	0.573	o	|	|	|	|	0.77
48.000	0.00	0.17	0.572	o	|	|	|	|	0.77
48.083	0.00	0.17	0.571	o	|	|	|	|	0.77
48.167	0.00	0.17	0.570	o	|	|	|	|	0.77
48.250	0.00	0.17	0.569	o	|	|	|	|	0.77
48.333	0.00	0.17	0.567	o	|	|	|	|	0.76
48.417	0.00	0.17	0.566	o	|	|	|	|	0.76
48.500	0.00	0.17	0.565	o	|	|	|	|	0.76
48.583	0.00	0.17	0.564	o	|	|	|	|	0.76
48.667	0.00	0.17	0.563	o	|	|	|	|	0.76
48.750	0.00	0.16	0.562	o	|	|	|	|	0.76
48.833	0.00	0.16	0.561	o	|	|	|	|	0.75
48.917	0.00	0.16	0.560	o	|	|	|	|	0.75
49.000	0.00	0.16	0.558	o	|	|	|	|	0.75
49.083	0.00	0.16	0.557	o	|	|	|	|	0.75
49.167	0.00	0.16	0.556	o	|	|	|	|	0.75
49.250	0.00	0.16	0.555	o	|	|	|	|	0.75
49.333	0.00	0.16	0.554	o	|	|	|	|	0.75
49.417	0.00	0.16	0.553	o	|	|	|	|	0.74
49.500	0.00	0.16	0.552	o	|	|	|	|	0.74
49.583	0.00	0.16	0.551	o	|	|	|	|	0.74
49.667	0.00	0.16	0.549	o	|	|	|	|	0.74
49.750	0.00	0.16	0.548	o	|	|	|	|	0.74
49.833	0.00	0.16	0.547	o	|	|	|	|	0.74
49.917	0.00	0.16	0.546	o	|	|	|	|	0.74
50.000	0.00	0.16	0.545	o	|	|	|	|	0.73
50.083	0.00	0.16	0.544	o	|	|	|	|	0.73
50.167	0.00	0.16	0.543	o	|	|	|	|	0.73
50.250	0.00	0.16	0.542	o	|	|	|	|	0.73
50.333	0.00	0.16	0.541	o	|	|	|	|	0.73
50.417	0.00	0.16	0.540	o	|	|	|	|	0.73
50.500	0.00	0.16	0.538	o	|	|	|	|	0.72
50.583	0.00	0.16	0.537	o	|	|	|	|	0.72
50.667	0.00	0.16	0.536	o	|	|	|	|	0.72
50.750	0.00	0.16	0.535	o	|	|	|	|	0.72
50.833	0.00	0.16	0.534	o	|	|	|	|	0.72
50.917	0.00	0.16	0.533	o	|	|	|	|	0.72
51.000	0.00	0.16	0.532	o	|	|	|	|	0.72
51.083	0.00	0.16	0.531	o	|	|	|	|	0.71
51.167	0.00	0.16	0.530	o	|	|	|	|	0.71
51.250	0.00	0.16	0.529	o	|	|	|	|	0.71
51.333	0.00	0.15	0.528	o	|	|	|	|	0.71
51.417	0.00	0.15	0.527	o	|	|	|	|	0.71
51.500	0.00	0.15	0.526	o	|	|	|	|	0.71
51.583	0.00	0.15	0.524	o	|	|	|	|	0.71
51.667	0.00	0.15	0.523	o	|	|	|	|	0.70
51.750	0.00	0.15	0.522	o	|	|	|	|	0.70
51.833	0.00	0.15	0.521	o	|	|	|	|	0.70
51.917	0.00	0.15	0.520	o	|	|	|	|	0.70

52.000	0.00	0.15	0.519	o	|	|	|	|	0.70
52.083	0.00	0.15	0.518	o	|	|	|	|	0.70
52.167	0.00	0.15	0.517	o	|	|	|	|	0.70
52.250	0.00	0.15	0.516	o	|	|	|	|	0.69
52.333	0.00	0.15	0.515	o	|	|	|	|	0.69
52.417	0.00	0.15	0.514	o	|	|	|	|	0.69
52.500	0.00	0.15	0.513	o	|	|	|	|	0.69
52.583	0.00	0.15	0.512	o	|	|	|	|	0.69
52.667	0.00	0.15	0.511	o	|	|	|	|	0.69
52.750	0.00	0.15	0.510	o	|	|	|	|	0.69
52.833	0.00	0.15	0.509	o	|	|	|	|	0.68
52.917	0.00	0.15	0.508	o	|	|	|	|	0.68
53.000	0.00	0.15	0.507	o	|	|	|	|	0.68
53.083	0.00	0.15	0.506	o	|	|	|	|	0.68
53.167	0.00	0.15	0.505	o	|	|	|	|	0.68
53.250	0.00	0.15	0.504	o	|	|	|	|	0.68
53.333	0.00	0.15	0.503	o	|	|	|	|	0.68
53.417	0.00	0.15	0.502	o	|	|	|	|	0.68
53.500	0.00	0.15	0.501	o	|	|	|	|	0.67
53.583	0.00	0.15	0.500	o	|	|	|	|	0.67
53.667	0.00	0.15	0.499	o	|	|	|	|	0.67
53.750	0.00	0.15	0.498	o	|	|	|	|	0.67
53.833	0.00	0.15	0.497	o	|	|	|	|	0.67
53.917	0.00	0.15	0.496	o	|	|	|	|	0.67
54.000	0.00	0.15	0.495	o	|	|	|	|	0.67
54.083	0.00	0.14	0.494	o	|	|	|	|	0.66
54.167	0.00	0.14	0.493	o	|	|	|	|	0.66
54.250	0.00	0.14	0.492	o	|	|	|	|	0.66
54.333	0.00	0.14	0.491	o	|	|	|	|	0.66
54.417	0.00	0.14	0.490	o	|	|	|	|	0.66
54.500	0.00	0.14	0.489	o	|	|	|	|	0.66
54.583	0.00	0.14	0.488	o	|	|	|	|	0.66
54.667	0.00	0.14	0.487	o	|	|	|	|	0.66
54.750	0.00	0.14	0.486	o	|	|	|	|	0.65
54.833	0.00	0.14	0.485	o	|	|	|	|	0.65
54.917	0.00	0.14	0.484	o	|	|	|	|	0.65
55.000	0.00	0.14	0.483	o	|	|	|	|	0.65
55.083	0.00	0.14	0.482	o	|	|	|	|	0.65
55.167	0.00	0.14	0.481	o	|	|	|	|	0.65
55.250	0.00	0.14	0.480	o	|	|	|	|	0.65
55.333	0.00	0.14	0.479	o	|	|	|	|	0.64
55.417	0.00	0.14	0.478	o	|	|	|	|	0.64
55.500	0.00	0.14	0.477	o	|	|	|	|	0.64
55.583	0.00	0.14	0.476	o	|	|	|	|	0.64
55.667	0.00	0.14	0.475	o	|	|	|	|	0.64
55.750	0.00	0.14	0.474	o	|	|	|	|	0.64
55.833	0.00	0.14	0.473	o	|	|	|	|	0.64
55.917	0.00	0.14	0.472	o	|	|	|	|	0.64
56.000	0.00	0.14	0.471	o	|	|	|	|	0.63
56.083	0.00	0.14	0.470	o	|	|	|	|	0.63
56.167	0.00	0.14	0.469	o	|	|	|	|	0.63
56.250	0.00	0.14	0.468	o	|	|	|	|	0.63
56.333	0.00	0.14	0.467	o	|	|	|	|	0.63
56.417	0.00	0.14	0.466	o	|	|	|	|	0.63
56.500	0.00	0.14	0.466	o	|	|	|	|	0.63
56.583	0.00	0.14	0.465	o	|	|	|	|	0.63
56.667	0.00	0.14	0.464	o	|	|	|	|	0.62
56.750	0.00	0.14	0.463	o	|	|	|	|	0.62
56.833	0.00	0.14	0.462	o	|	|	|	|	0.62
56.917	0.00	0.14	0.461	o	|	|	|	|	0.62
57.000	0.00	0.13	0.460	o	|	|	|	|	0.62
57.083	0.00	0.13	0.459	o	|	|	|	|	0.62
57.167	0.00	0.13	0.458	o	|	|	|	|	0.62
57.250	0.00	0.13	0.457	o	|	|	|	|	0.62
57.333	0.00	0.13	0.456	o	|	|	|	|	0.61
57.417	0.00	0.13	0.455	o	|	|	|	|	0.61
57.500	0.00	0.13	0.454	o	|	|	|	|	0.61
57.583	0.00	0.13	0.453	o	|	|	|	|	0.61
57.667	0.00	0.13	0.453	o	|	|	|	|	0.61
57.750	0.00	0.13	0.452	o	|	|	|	|	0.61
57.833	0.00	0.13	0.451	o	|	|	|	|	0.61
57.917	0.00	0.13	0.450	o	|	|	|	|	0.61
58.000	0.00	0.13	0.449	o	|	|	|	|	0.60
58.083	0.00	0.13	0.448	o	|	|	|	|	0.60
58.167	0.00	0.13	0.447	o	|	|	|	|	0.60
58.250	0.00	0.13	0.446	o	|	|	|	|	0.60
58.333	0.00	0.13	0.445	o	|	|	|	|	0.60
58.417	0.00	0.13	0.444	o	|	|	|	|	0.60
58.500	0.00	0.13	0.443	o	|	|	|	|	0.60
58.583	0.00	0.13	0.443	o	|	|	|	|	0.60
58.667	0.00	0.13	0.442	o	|	|	|	|	0.59
58.750	0.00	0.13	0.441	o	|	|	|	|	0.59
58.833	0.00	0.13	0.440	o	|	|	|	|	0.59
58.917	0.00	0.13	0.439	o	|	|	|	|	0.59
59.000	0.00	0.13	0.438	o	|	|	|	|	0.59
59.083	0.00	0.13	0.437	o	|	|	|	|	0.59

59.167	0.00	0.13	0.436	o	|	|	|	|	0.59
59.250	0.00	0.13	0.436	o	|	|	|	|	0.59
59.333	0.00	0.13	0.435	o	|	|	|	|	0.58
59.417	0.00	0.13	0.434	o	|	|	|	|	0.58
59.500	0.00	0.13	0.433	o	|	|	|	|	0.58
59.583	0.00	0.13	0.432	o	|	|	|	|	0.58
59.667	0.00	0.13	0.431	o	|	|	|	|	0.58
59.750	0.00	0.13	0.430	o	|	|	|	|	0.58
59.833	0.00	0.13	0.429	o	|	|	|	|	0.58
59.917	0.00	0.13	0.429	o	|	|	|	|	0.58
60.000	0.00	0.13	0.428	o	|	|	|	|	0.58
60.083	0.00	0.13	0.427	o	|	|	|	|	0.57
60.167	0.00	0.12	0.426	o	|	|	|	|	0.57
60.250	0.00	0.12	0.425	o	|	|	|	|	0.57
60.333	0.00	0.12	0.424	o	|	|	|	|	0.57
60.417	0.00	0.12	0.423	o	|	|	|	|	0.57
60.500	0.00	0.12	0.422	o	|	|	|	|	0.57
60.583	0.00	0.12	0.422	o	|	|	|	|	0.57
60.667	0.00	0.12	0.421	o	|	|	|	|	0.57
60.750	0.00	0.12	0.420	o	|	|	|	|	0.57
60.833	0.00	0.12	0.419	o	|	|	|	|	0.56
60.917	0.00	0.12	0.418	o	|	|	|	|	0.56
61.000	0.00	0.12	0.417	o	|	|	|	|	0.56
61.083	0.00	0.12	0.417	o	|	|	|	|	0.56
61.167	0.00	0.12	0.416	o	|	|	|	|	0.56
61.250	0.00	0.12	0.415	o	|	|	|	|	0.56
61.333	0.00	0.12	0.414	o	|	|	|	|	0.56
61.417	0.00	0.12	0.413	o	|	|	|	|	0.56
61.500	0.00	0.12	0.412	o	|	|	|	|	0.56
61.583	0.00	0.12	0.412	o	|	|	|	|	0.55
61.667	0.00	0.12	0.411	o	|	|	|	|	0.55
61.750	0.00	0.12	0.410	o	|	|	|	|	0.55
61.833	0.00	0.12	0.409	o	|	|	|	|	0.55
61.917	0.00	0.12	0.408	o	|	|	|	|	0.55
62.000	0.00	0.12	0.407	o	|	|	|	|	0.55
62.083	0.00	0.12	0.407	o	|	|	|	|	0.55
62.167	0.00	0.12	0.406	o	|	|	|	|	0.55
62.250	0.00	0.12	0.405	o	|	|	|	|	0.55
62.333	0.00	0.12	0.404	o	|	|	|	|	0.54
62.417	0.00	0.12	0.403	o	|	|	|	|	0.54
62.500	0.00	0.12	0.402	o	|	|	|	|	0.54
62.583	0.00	0.12	0.402	o	|	|	|	|	0.54
62.667	0.00	0.12	0.401	o	|	|	|	|	0.54
62.750	0.00	0.12	0.400	o	|	|	|	|	0.54
62.833	0.00	0.12	0.399	o	|	|	|	|	0.54
62.917	0.00	0.12	0.398	o	|	|	|	|	0.54
63.000	0.00	0.12	0.398	o	|	|	|	|	0.54
63.083	0.00	0.12	0.397	o	|	|	|	|	0.53
63.167	0.00	0.12	0.396	o	|	|	|	|	0.53
63.250	0.00	0.12	0.395	o	|	|	|	|	0.53
63.333	0.00	0.12	0.394	o	|	|	|	|	0.53
63.417	0.00	0.12	0.394	o	|	|	|	|	0.53
63.500	0.00	0.12	0.393	o	|	|	|	|	0.53
63.583	0.00	0.12	0.392	o	|	|	|	|	0.53
63.667	0.00	0.11	0.391	o	|	|	|	|	0.53
63.750	0.00	0.11	0.390	o	|	|	|	|	0.53
63.833	0.00	0.11	0.390	o	|	|	|	|	0.52
63.917	0.00	0.11	0.389	o	|	|	|	|	0.52
64.000	0.00	0.11	0.388	o	|	|	|	|	0.52
64.083	0.00	0.11	0.387	o	|	|	|	|	0.52
64.167	0.00	0.11	0.387	o	|	|	|	|	0.52
64.250	0.00	0.11	0.386	o	|	|	|	|	0.52
64.333	0.00	0.11	0.385	o	|	|	|	|	0.52
64.417	0.00	0.11	0.384	o	|	|	|	|	0.52
64.500	0.00	0.11	0.383	o	|	|	|	|	0.52
64.583	0.00	0.11	0.383	o	|	|	|	|	0.52
64.667	0.00	0.11	0.382	o	|	|	|	|	0.51
64.750	0.00	0.11	0.381	o	|	|	|	|	0.51
64.833	0.00	0.11	0.380	o	|	|	|	|	0.51
64.917	0.00	0.11	0.380	o	|	|	|	|	0.51
65.000	0.00	0.11	0.379	o	|	|	|	|	0.51
65.083	0.00	0.11	0.378	o	|	|	|	|	0.51
65.167	0.00	0.11	0.377	o	|	|	|	|	0.51
65.250	0.00	0.11	0.377	o	|	|	|	|	0.51
65.333	0.00	0.11	0.376	o	|	|	|	|	0.51
65.417	0.00	0.11	0.375	o	|	|	|	|	0.50
65.500	0.00	0.11	0.374	o	|	|	|	|	0.50
65.583	0.00	0.11	0.374	o	|	|	|	|	0.50
65.667	0.00	0.11	0.373	o	|	|	|	|	0.50
65.750	0.00	0.11	0.372	o	|	|	|	|	0.50
65.833	0.00	0.11	0.371	o	|	|	|	|	0.50
65.917	0.00	0.11	0.370	o	|	|	|	|	0.50
66.000	0.00	0.11	0.370	o	|	|	|	|	0.50
66.083	0.00	0.11	0.369	o	|	|	|	|	0.50
66.167	0.00	0.11	0.368	o	|	|	|	|	0.50
66.250	0.00	0.11	0.368	o	|	|	|	|	0.49

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66.333    0.00    0.11      0.367  o       |       |       |       |     0.49
66.417    0.00    0.11      0.366  o       |       |       |       |     0.49
66.500    0.00    0.11      0.365  o       |       |       |       |     0.49
66.583    0.00    0.11      0.365  o       |       |       |       |     0.49
66.667    0.00    0.11      0.364  o       |       |       |       |     0.49
66.750    0.00    0.11      0.363  o       |       |       |       |     0.49
66.833    0.00    0.11      0.362  o       |       |       |       |     0.49
66.917    0.00    0.11      0.362  o       |       |       |       |     0.49
67.000    0.00    0.11      0.361  o       |       |       |       |     0.49
67.083    0.00    0.11      0.360  o       |       |       |       |     0.48
67.167    0.00    0.11      0.359  o       |       |       |       |     0.48
67.250    0.00    0.11      0.359  o       |       |       |       |     0.48
67.333    0.00    0.11      0.358  o       |       |       |       |     0.48
67.417    0.00    0.10      0.357  o       |       |       |       |     0.48
67.500    0.00    0.10      0.357  o       |       |       |       |     0.48
67.583    0.00    0.10      0.356  o       |       |       |       |     0.48
67.667    0.00    0.10      0.355  o       |       |       |       |     0.48
67.750    0.00    0.10      0.354  o       |       |       |       |     0.48
67.833    0.00    0.10      0.354  o       |       |       |       |     0.48
67.917    0.00    0.10      0.353  o       |       |       |       |     0.48
68.000    0.00    0.10      0.352  o       |       |       |       |     0.47
68.083    0.00    0.10      0.352  o       |       |       |       |     0.47
68.167    0.00    0.10      0.351  o       |       |       |       |     0.47
68.250    0.00    0.10      0.350  o       |       |       |       |     0.47
68.333    0.00    0.10      0.349  o       |       |       |       |     0.47
68.417    0.00    0.10      0.349  o       |       |       |       |     0.47
68.500    0.00    0.10      0.348  o       |       |       |       |     0.47
68.583    0.00    0.10      0.347  o       |       |       |       |     0.47
68.667    0.00    0.10      0.347  o       |       |       |       |     0.47
68.750    0.00    0.10      0.346  o       |       |       |       |     0.47
68.833    0.00    0.10      0.345  o       |       |       |       |     0.46
68.917    0.00    0.10      0.345  o       |       |       |       |     0.46
69.000    0.00    0.10      0.344  o       |       |       |       |     0.46
69.083    0.00    0.10      0.343  o       |       |       |       |     0.46
69.167    0.00    0.10      0.342  o       |       |       |       |     0.46
69.250    0.00    0.10      0.342  o       |       |       |       |     0.46
69.333    0.00    0.10      0.341  o       |       |       |       |     0.46
69.417    0.00    0.10      0.340  o       |       |       |       |     0.46

Remaining water in basin =    0.34 (Ac.Ft)

****************************HYDROGRAPH DATA****************************
               Number of intervals =   833
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =        1.113 (CFS)
               Total volume =       1.822 (Ac.Ft)
       Status of hydrographs being held in storage
                  Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro15245.rte
**********HYDROGRAPH DATA**********
Number of intervals = 293
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 6.203 (CFS)
Total volume = 3.009 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

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Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 293
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	1.6	3.10	4.65	6.20 (Ft.)	Depth
0.083	0.09	0.00	0.000	O	|	|	|	|	0.00
0.167	0.22	0.00	0.001	OI	|	|	|	|	0.00
0.250	0.25	0.00	0.003	OI	|	|	|	|	0.00
0.333	0.31	0.00	0.005	OI	|	|	|	|	0.01
0.417	0.38	0.00	0.007	OI	|	|	|	|	0.01
0.500	0.40	0.00	0.010	O I	|	|	|	|	0.01
0.583	0.41	0.00	0.013	O I	|	|	|	|	0.02
0.667	0.41	0.00	0.015	O I	|	|	|	|	0.02
0.750	0.41	0.01	0.018	O I	|	|	|	|	0.02
0.833	0.46	0.01	0.021	O I	|	|	|	|	0.03
0.917	0.52	0.01	0.025	O I	|	|	|	|	0.03
1.000	0.54	0.01	0.028	O I	|	|	|	|	0.04
1.083	0.50	0.01	0.032	O I	|	|	|	|	0.04
1.167	0.44	0.01	0.035	O I	|	|	|	|	0.05
1.250	0.42	0.01	0.038	O I	|	|	|	|	0.05
1.333	0.42	0.01	0.041	O I	|	|	|	|	0.05
1.417	0.41	0.01	0.043	O I	|	|	|	|	0.06
1.500	0.41	0.01	0.046	O I	|	|	|	|	0.06
1.583	0.41	0.01	0.049	O I	|	|	|	|	0.07
1.667	0.41	0.02	0.052	O I	|	|	|	|	0.07
1.750	0.41	0.02	0.054	O I	|	|	|	|	0.07

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1.833    0.46    0.02      0.057  o I     |       |       |       |     0.08
1.917    0.52    0.02      0.060  o I     |       |       |       |     0.08
2.000    0.54    0.02      0.064  o I     |       |       |       |     0.09
2.083    0.54    0.02      0.068  o I     |       |       |       |     0.09
2.167    0.55    0.02      0.071  o I     |       |       |       |     0.10
2.250    0.55    0.02      0.075  o I     |       |       |       |     0.10
2.333    0.55    0.02      0.078  o I     |       |       |       |     0.11
2.417    0.55    0.02      0.082  o I     |       |       |       |     0.11
2.500    0.55    0.03      0.086  o I     |       |       |       |     0.12
2.583    0.59    0.03      0.089  o  I    |       |       |       |     0.12
2.667    0.66    0.03      0.094  o  I    |       |       |       |     0.13
2.750    0.68    0.03      0.098  o  I    |       |       |       |     0.13
2.833    0.68    0.03      0.102  o  I    |       |       |       |     0.14
2.917    0.69    0.03      0.107  o  I    |       |       |       |     0.14
3.000    0.69    0.03      0.111  o  I    |       |       |       |     0.15
3.083    0.69    0.03      0.116  o  I    |       |       |       |     0.16
3.167    0.69    0.04      0.120  o  I    |       |       |       |     0.16
3.250    0.69    0.04      0.125  o  I    |       |       |       |     0.17
3.333    0.69    0.04      0.129  o  I    |       |       |       |     0.17
3.417    0.69    0.04      0.134  o  I    |       |       |       |     0.18
3.500    0.69    0.04      0.138  o  I    |       |       |       |     0.19
3.583    0.69    0.04      0.143  o  I    |       |       |       |     0.19
3.667    0.69    0.04      0.147  o  I    |       |       |       |     0.20
3.750    0.69    0.04      0.152  o  I    |       |       |       |     0.20
3.833    0.73    0.05      0.156  o  I    |       |       |       |     0.21
3.917    0.80    0.05      0.161  o   I   |       |       |       |     0.22
4.000    0.81    0.05      0.166  o   I   |       |       |       |     0.22
4.083    0.82    0.05      0.172  o   I   |       |       |       |     0.23
4.167    0.82    0.05      0.177  o   I   |       |       |       |     0.24
4.250    0.82    0.05      0.182  o   I   |       |       |       |     0.25
4.333    0.87    0.06      0.188  o   I   |       |       |       |     0.25
4.417    0.93    0.06      0.194  o   I   |       |       |       |     0.26
4.500    0.95    0.06      0.200  o   I   |       |       |       |     0.27
4.583    0.96    0.06      0.206  o   I   |       |       |       |     0.28
4.667    0.96    0.06      0.212  o   I   |       |       |       |     0.29
4.750    0.96    0.06      0.218  o   I   |       |       |       |     0.29
4.833    1.01    0.07      0.225  o    I  |       |       |       |     0.30
4.917    1.07    0.07      0.231  o    I  |       |       |       |     0.31
5.000    1.09    0.07      0.238  o    I  |       |       |       |     0.32
5.083    1.01    0.07      0.245  o    I  |       |       |       |     0.33
5.167    0.88    0.07      0.251  o   I   |       |       |       |     0.34
5.250    0.85    0.08      0.256  o   I   |       |       |       |     0.34
5.333    0.88    0.08      0.262  o   I   |       |       |       |     0.35
5.417    0.94    0.08      0.267  o   I   |       |       |       |     0.36
5.500    0.95    0.08      0.273  o   I   |       |       |       |     0.37
5.583    1.00    0.08      0.280  o    I  |       |       |       |     0.38
5.667    1.07    0.08      0.286  o    I  |       |       |       |     0.39
5.750    1.09    0.09      0.293  o    I  |       |       |       |     0.39
5.833    1.09    0.09      0.300  o    I  |       |       |       |     0.40
5.917    1.10    0.09      0.307  o    I  |       |       |       |     0.41
6.000    1.10    0.09      0.314  o    I  |       |       |       |     0.42
6.083    1.14    0.09      0.321  o    I  |       |       |       |     0.43
6.167    1.21    0.10      0.328  o     I |       |       |       |     0.44
6.250    1.22    0.10      0.336  o     I |       |       |       |     0.45
6.333    1.23    0.10      0.344  o     I |       |       |       |     0.46
6.417    1.24    0.10      0.352  o     I |       |       |       |     0.47
6.500    1.24    0.11      0.359  o     I |       |       |       |     0.48
6.583    1.28    0.11      0.367  o     I |       |       |       |     0.49
6.667    1.35    0.11      0.376  o     I |       |       |       |     0.51
6.750    1.36    0.11      0.384  o      I|       |       |       |     0.52
6.833    1.37    0.12      0.393  o      I|       |       |       |     0.53
6.917    1.37    0.12      0.401  o      I|       |       |       |     0.54
7.000    1.37    0.12      0.410  o      I|       |       |       |     0.55
7.083    1.37    0.12      0.419  o      I|       |       |       |     0.56
7.167    1.37    0.13      0.427  o      I|       |       |       |     0.58
7.250    1.37    0.13      0.436  o      I|       |       |       |     0.59
7.333    1.42    0.13      0.445  o      I|       |       |       |     0.60
7.417    1.48    0.13      0.454  o      I|       |       |       |     0.61
7.500    1.50    0.14      0.463  o      I|       |       |       |     0.62
7.583    1.55    0.14      0.473  o       I       |       |       |     0.64
7.667    1.62    0.14      0.483  o       I       |       |       |     0.65
7.750    1.64    0.14      0.493  o       I       |       |       |     0.66
7.833    1.69    0.15      0.503  o       I       |       |       |     0.68
7.917    1.76    0.15      0.514  o       |I      |       |       |     0.69
8.000    1.77    0.15      0.525  o       |I      |       |       |     0.71
8.083    1.87    0.16      0.537  o       |I      |       |       |     0.72
8.167    2.00    0.16      0.549  o       | I     |       |       |     0.74
8.250    2.04    0.16      0.562  o       | I     |       |       |     0.76
8.333    2.05    0.17      0.575  o       | I     |       |       |     0.77
8.417    2.06    0.17      0.588  o       | I     |       |       |     0.79
8.500    2.06    0.18      0.601  o       | I     |       |       |     0.81
8.583    2.11    0.18      0.614  o       | I     |       |       |     0.83
8.667    2.17    0.18      0.627  o       |  I    |       |       |     0.84
8.750    2.19    0.19      0.641  o       |  I    |       |       |     0.86
8.833    2.24    0.19      0.655  o       |  I    |       |       |     0.88
8.917    2.31    0.20      0.669  |o      |  I    |       |       |     0.90
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 9.000    2.32    0.20      0.684  |o       |  I     |        |        |     0.92
 9.083    2.42    0.21      0.699  |o       |   I    |        |        |     0.94
 9.167    2.55    0.21      0.714  |o       |    I   |        |        |     0.96
 9.250    2.59    0.21      0.731  |o       |    I   |        |        |     0.98
 9.333    2.65    0.22      0.747  |o       |    I   |        |        |     1.01
 9.417    2.72    0.23      0.764  |o       |     I  |        |        |     1.03
 9.500    2.74    0.24      0.781  |o       |     I  |        |        |     1.05
 9.583    2.79    0.25      0.799  |o       |     I  |        |        |     1.07
 9.667    2.86    0.26      0.816  |o       |     I  |        |        |     1.09
 9.750    2.87    0.27      0.834  |o       |     I  |        |        |     1.11
 9.833    2.93    0.28      0.852  |o       |      I |        |        |     1.13
 9.917    2.99    0.29      0.871  |o       |      I |        |        |     1.16
10.000    3.01    0.30      0.890  |o       |      I |        |        |     1.18
10.083    2.71    0.31      0.907  |o       |    I   |        |        |     1.20
10.167    2.26    0.32      0.922  |o       |  I     |        |        |     1.22
10.250    2.15    0.32      0.935  |o       |  I     |        |        |     1.23
10.333    2.10    0.33      0.947  |o       | I      |        |        |     1.25
10.417    2.08    0.34      0.959  |o       | I      |        |        |     1.26
10.500    2.06    0.34      0.971  |o       | I      |        |        |     1.28
10.583    2.28    0.35      0.984  |o       |  I     |        |        |     1.29
10.667    2.61    0.36      0.998  |o       |    I   |        |        |     1.31
10.750    2.69    0.37      1.014  |o       |    I   |        |        |     1.33
10.833    2.72    0.38      1.030  |o       |     I  |        |        |     1.35
10.917    2.74    0.38      1.046  |o       |     I  |        |        |     1.37
11.000    2.75    0.39      1.063  | o      |     I  |        |        |     1.39
11.083    2.70    0.40      1.079  | o      |    I   |        |        |     1.41
11.167    2.64    0.41      1.094  | o      |    I   |        |        |     1.43
11.250    2.62    0.42      1.110  | o      |    I   |        |        |     1.45
11.333    2.62    0.43      1.125  | o      |    I   |        |        |     1.47
11.417    2.61    0.44      1.140  | o      |    I   |        |        |     1.48
11.500    2.61    0.44      1.155  | o      |    I   |        |        |     1.50
11.583    2.52    0.45      1.169  | o      |    I   |        |        |     1.52
11.667    2.39    0.46      1.183  | o      |   I    |        |        |     1.54
11.750    2.36    0.47      1.196  | o      |   I    |        |        |     1.55
11.833    2.39    0.47      1.209  | o      |   I    |        |        |     1.57
11.917    2.45    0.48      1.223  | o      |   I    |        |        |     1.59
12.000    2.46    0.49      1.236  | o      |   I    |        |        |     1.60
12.083    2.79    0.50      1.251  | o      |     I  |        |        |     1.62
12.167    3.27    0.51      1.268  | o      |       I|        |        |     1.64
12.250    3.39    0.52      1.288  | o      |        I       |        |     1.67
12.333    3.55    0.53      1.308  | o      |        | I     |        |     1.69
12.417    3.72    0.54      1.329  | o      |        |  I    |        |     1.72
12.500    3.78    0.55      1.351  | o      |        |  I    |        |     1.74
12.583    3.99    0.57      1.374  | o      |        |   I   |        |     1.77
12.667    4.27    0.58      1.399  | o      |        |     I |        |     1.80
12.750    4.36    0.59      1.425  |  o     |        |     I |        |     1.83
12.833    4.49    0.61      1.451  |  o     |        |      I|        |     1.87
12.917    4.65    0.62      1.478  |  o     |        |      I|        |     1.90
13.000    4.71    0.64      1.506  |  o     |        |       I        |     1.93
13.083    5.18    0.65      1.536  |  o     |        |        | I     |     1.97
13.167    5.85    0.68      1.569  |  o     |        |        |    I  |     2.01
13.250    6.03    0.71      1.605  |  o     |        |        |     I|     2.05
13.333    6.12    0.74      1.642  |  o     |        |        |     I|     2.09
13.417    6.17    0.78      1.679  |   o    |        |        |     I|     2.13
13.500    6.20    0.82      1.716  |   o    |        |        |      I     2.17
13.583    5.24    0.85      1.750  |   o    |        |        | I    |     2.21
13.667    3.83    0.87      1.775  |   o    |        |  I     |      |     2.24
13.750    3.50    0.89      1.794  |   o    |        | I      |      |     2.26
13.833    3.36    0.91      1.812  |   o    |        |I       |      |     2.28
13.917    3.30    0.92      1.828  |   o    |        |I       |      |     2.30
14.000    3.27    0.94      1.845  |   o    |        I        |      |     2.32
14.083    3.65    0.95      1.862  |   o    |        | I      |      |     2.34
14.167    4.18    0.97      1.882  |    o   |        |    I   |      |     2.36
14.250    4.32    0.99      1.905  |    o   |        |     I  |      |     2.38
14.333    4.30    1.02      1.928  |    o   |        |     I  |      |     2.41
14.417    4.22    1.04      1.950  |    o   |        |    I   |      |     2.43
14.500    4.22    1.06      1.972  |    o   |        |    I   |      |     2.46
14.583    4.22    1.08      1.993  |    o   |        |    I   |      |     2.48
14.667    4.22    1.10      2.015  |    o   |        |    I   |      |     2.51
14.750    4.24    1.12      2.036  |    o   |        |    I   |      |     2.53
14.833    4.16    1.14      2.057  |    o   |        |    I   |      |     2.55
14.917    4.05    1.16      2.078  |    o   |        |   I    |      |     2.58
15.000    4.03    1.18      2.098  |     o  |        |   I    |      |     2.60
15.083    3.94    1.20      2.117  |     o  |        |   I    |      |     2.62
15.167    3.82    1.21      2.135  |     o  |        |  I     |      |     2.64
15.250    3.80    1.23      2.153  |     o  |        |  I     |      |     2.66
15.333    3.71    1.25      2.170  |     o  |        |  I     |      |     2.68
15.417    3.59    1.26      2.187  |     o  |        | I      |      |     2.70
15.500    3.57    1.28      2.203  |     o  |        | I      |      |     2.72
15.583    3.26    1.29      2.217  |     o  |       I        |      |     2.73
15.667    2.81    1.30      2.229  |     o  |     I  |       |      |     2.75
15.750    2.70    1.31      2.239  |     o  |    I   |       |      |     2.76
15.833    2.65    1.32      2.249  |     o  |    I   |       |      |     2.77
15.917    2.63    1.33      2.258  |     o  |    I   |       |      |     2.78
16.000    2.61    1.34      2.267  |     o  |    I   |       |      |     2.79
16.083    1.94    1.34      2.273  |     o  | I      |       |      |     2.80
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16.167	0.97	1.34	2.274	IO				2.80
16.250	0.74	1.34	2.270	I O				2.79
16.333	0.63	1.34	2.266	I O				2.79
16.417	0.58	1.33	2.261	I O				2.78
16.500	0.55	1.33	2.256	I O				2.78
16.583	0.51	1.32	2.250	I O				2.77
16.667	0.44	1.32	2.244	I O				2.76
16.750	0.42	1.31	2.238	I O				2.76
16.833	0.42	1.31	2.232	I O				2.75
16.917	0.41	1.30	2.226	I O				2.74
17.000	0.41	1.29	2.220	I O				2.74
17.083	0.50	1.29	2.214	I O				2.73
17.167	0.63	1.28	2.209	I O				2.72
17.250	0.66	1.28	2.205	I O				2.72
17.333	0.68	1.28	2.201	I O				2.71
17.417	0.68	1.27	2.197	I O				2.71
17.500	0.69	1.27	2.193	I O				2.71
17.583	0.69	1.26	2.189	I O				2.70
17.667	0.69	1.26	2.185	I O				2.70
17.750	0.69	1.26	2.181	I O				2.69
17.833	0.64	1.25	2.177	I O				2.69
17.917	0.58	1.25	2.172	I O				2.68
18.000	0.56	1.24	2.168	I O				2.68
18.083	0.56	1.24	2.163	I O				2.67
18.167	0.55	1.24	2.158	I O				2.67
18.250	0.55	1.23	2.153	I O				2.66
18.333	0.55	1.23	2.149	I O				2.66
18.417	0.55	1.22	2.144	I O				2.65
18.500	0.55	1.22	2.140	I O				2.65
18.583	0.51	1.21	2.135	I O				2.64
18.667	0.44	1.21	2.130	I O				2.64
18.750	0.42	1.20	2.124	I O				2.63
18.833	0.37	1.20	2.119	I O				2.62
18.917	0.30	1.19	2.113	I O				2.62
19.000	0.29	1.19	2.107	I O				2.61
19.083	0.33	1.18	2.101	I O				2.60
19.167	0.39	1.18	2.095	I O				2.60
19.250	0.40	1.17	2.090	I O				2.59
19.333	0.45	1.17	2.085	I O				2.59
19.417	0.52	1.16	2.080	I O				2.58
19.500	0.54	1.16	2.076	I O				2.58
19.583	0.50	1.15	2.071	I O				2.57
19.667	0.44	1.15	2.067	I O				2.56
19.750	0.42	1.14	2.062	I O				2.56
19.833	0.37	1.14	2.057	I O				2.55
19.917	0.30	1.13	2.051	I O				2.55
20.000	0.29	1.13	2.045	I O				2.54
20.083	0.33	1.12	2.040	I O				2.53
20.167	0.39	1.12	2.034	I O				2.53
20.250	0.40	1.11	2.029	I O				2.52
20.333	0.41	1.11	2.025	I O				2.52
20.417	0.41	1.10	2.020	I O				2.51
20.500	0.41	1.10	2.015	I O				2.51
20.583	0.41	1.09	2.010	I O				2.50
20.667	0.41	1.09	2.006	I O				2.50
20.750	0.41	1.09	2.001	I O				2.49
20.833	0.37	1.08	1.996	I O				2.49
20.917	0.30	1.08	1.991	I O				2.48
21.000	0.29	1.07	1.986	I O				2.47
21.083	0.33	1.07	1.980	I O				2.47
21.167	0.39	1.06	1.976	I O				2.46
21.250	0.40	1.06	1.971	I O				2.46
21.333	0.36	1.05	1.966	I O				2.45
21.417	0.30	1.05	1.961	I O				2.45
21.500	0.29	1.04	1.956	I O				2.44
21.583	0.33	1.04	1.951	I O				2.44
21.667	0.39	1.03	1.946	I O				2.43
21.750	0.40	1.03	1.942	I O				2.43
21.833	0.36	1.03	1.938	I O				2.42
21.917	0.30	1.02	1.933	I O				2.42
22.000	0.29	1.02	1.928	I O				2.41
22.083	0.33	1.01	1.923	I O				2.40
22.167	0.39	1.01	1.918	I O				2.40
22.250	0.40	1.00	1.914	I O				2.39
22.333	0.36	1.00	1.910	I O				2.39
22.417	0.30	1.00	1.905	I O				2.38
22.500	0.29	0.99	1.901	I O				2.38
22.583	0.28	0.99	1.896	I O				2.37
22.667	0.28	0.98	1.891	I O				2.37
22.750	0.27	0.98	1.886	I O				2.36
22.833	0.27	0.97	1.881	I O				2.36
22.917	0.27	0.97	1.876	I O				2.35
23.000	0.27	0.96	1.872	I O				2.35
23.083	0.27	0.96	1.867	I O				2.34
23.167	0.27	0.95	1.862	I O				2.34
23.250	0.27	0.95	1.858	I O				2.33

23.333	0.27	0.95	1.853	|I o	|	|	|	2.33
23.417	0.27	0.94	1.848	|I o	|	|	|	2.32
23.500	0.27	0.94	1.844	|I o	|	|	|	2.32
23.583	0.27	0.93	1.839	|I o	|	|	|	2.31
23.667	0.27	0.93	1.835	|I o	|	|	|	2.31
23.750	0.27	0.92	1.830	|I o	|	|	|	2.30
23.833	0.27	0.92	1.826	|I o	|	|	|	2.30
23.917	0.27	0.92	1.821	|I o	|	|	|	2.29
24.000	0.27	0.91	1.817	|I o	|	|	|	2.29
24.083	0.19	0.91	1.812	I o	|	|	|	2.28
24.167	0.06	0.90	1.807	I o	|	|	|	2.27
24.250	0.02	0.90	1.801	I o	|	|	|	2.27
24.333	0.01	0.89	1.795	I o	|	|	|	2.26
24.417	0.00	0.88	1.789	I o	|	|	|	2.25
24.500	0.00	0.88	1.783	I o	|	|	|	2.25
24.583	0.00	0.87	1.777	I o	|	|	|	2.24
24.667	0.00	0.87	1.771	I o	|	|	|	2.23
24.750	0.00	0.86	1.765	I o	|	|	|	2.23
24.833	0.00	0.86	1.759	I o	|	|	|	2.22
24.917	0.00	0.85	1.753	I o	|	|	|	2.21
25.000	0.00	0.84	1.747	I o	|	|	|	2.21
25.083	0.00	0.84	1.741	I o	|	|	|	2.20
25.167	0.00	0.83	1.736	I o	|	|	|	2.20
25.250	0.00	0.83	1.730	I o	|	|	|	2.19
25.333	0.00	0.82	1.724	I o	|	|	|	2.18
25.417	0.00	0.82	1.719	I o	|	|	|	2.18
25.500	0.00	0.81	1.713	I o	|	|	|	2.17
25.583	0.00	0.81	1.707	I o	|	|	|	2.16
25.667	0.00	0.80	1.702	I o	|	|	|	2.16
25.750	0.00	0.80	1.696	I o	|	|	|	2.15
25.833	0.00	0.79	1.691	I o	|	|	|	2.15
25.917	0.00	0.79	1.685	I o	|	|	|	2.14
26.000	0.00	0.78	1.680	I o	|	|	|	2.13
26.083	0.00	0.78	1.675	I o	|	|	|	2.13
26.167	0.00	0.77	1.669	I o	|	|	|	2.12
26.250	0.00	0.77	1.664	I o	|	|	|	2.12
26.333	0.00	0.76	1.659	I o	|	|	|	2.11
26.417	0.00	0.76	1.654	I o	|	|	|	2.10
26.500	0.00	0.75	1.648	I o	|	|	|	2.10
26.583	0.00	0.75	1.643	I o	|	|	|	2.09
26.667	0.00	0.74	1.638	I o	|	|	|	2.09
26.750	0.00	0.74	1.633	I o	|	|	|	2.08
26.833	0.00	0.73	1.628	I o	|	|	|	2.07
26.917	0.00	0.73	1.623	I o	|	|	|	2.07
27.000	0.00	0.72	1.618	I o	|	|	|	2.06
27.083	0.00	0.72	1.613	I o	|	|	|	2.06
27.167	0.00	0.71	1.608	I o	|	|	|	2.05
27.250	0.00	0.71	1.603	I o	|	|	|	2.05
27.333	0.00	0.70	1.598	I o	|	|	|	2.04
27.417	0.00	0.70	1.594	I o	|	|	|	2.04
27.500	0.00	0.69	1.589	I o	|	|	|	2.03
27.583	0.00	0.69	1.584	I o	|	|	|	2.03
27.667	0.00	0.69	1.579	I o	|	|	|	2.02
27.750	0.00	0.68	1.575	I o	|	|	|	2.02
27.833	0.00	0.68	1.570	I o	|	|	|	2.01
27.917	0.00	0.67	1.565	I o	|	|	|	2.00
28.000	0.00	0.67	1.561	I o	|	|	|	2.00
28.083	0.00	0.67	1.556	I o	|	|	|	1.99
28.167	0.00	0.66	1.551	I o	|	|	|	1.99
28.250	0.00	0.66	1.547	I o	|	|	|	1.98
28.333	0.00	0.66	1.542	I o	|	|	|	1.98
28.417	0.00	0.66	1.538	I o	|	|	|	1.97
28.500	0.00	0.65	1.533	I o	|	|	|	1.97
28.583	0.00	0.65	1.529	I o	|	|	|	1.96
28.667	0.00	0.65	1.524	I o	|	|	|	1.96
28.750	0.00	0.65	1.520	I o	|	|	|	1.95
28.833	0.00	0.64	1.515	I o	|	|	|	1.94
28.917	0.00	0.64	1.511	I o	|	|	|	1.94
29.000	0.00	0.64	1.507	I o	|	|	|	1.93
29.083	0.00	0.64	1.502	I o	|	|	|	1.93
29.167	0.00	0.63	1.498	I o	|	|	|	1.92
29.250	0.00	0.63	1.494	I o	|	|	|	1.92
29.333	0.00	0.63	1.489	I o	|	|	|	1.91
29.417	0.00	0.63	1.485	I o	|	|	|	1.91
29.500	0.00	0.62	1.481	I o	|	|	|	1.90
29.583	0.00	0.62	1.476	I o	|	|	|	1.90
29.667	0.00	0.62	1.472	I o	|	|	|	1.89
29.750	0.00	0.62	1.468	I o	|	|	|	1.89
29.833	0.00	0.61	1.464	I o	|	|	|	1.88
29.917	0.00	0.61	1.459	I o	|	|	|	1.88
30.000	0.00	0.61	1.455	I o	|	|	|	1.87
30.083	0.00	0.61	1.451	I o	|	|	|	1.87
30.167	0.00	0.61	1.447	I o	|	|	|	1.86
30.250	0.00	0.60	1.443	I o	|	|	|	1.86
30.333	0.00	0.60	1.438	I o	|	|	|	1.85
30.417	0.00	0.60	1.434	I o	|	|	|	1.85

30.500	0.00	0.60	1.430	I o	|	|	|	1.84
30.583	0.00	0.59	1.426	I o	|	|	|	1.84
30.667	0.00	0.59	1.422	I o	|	|	|	1.83
30.750	0.00	0.59	1.418	I o	|	|	|	1.83
30.833	0.00	0.59	1.414	I o	|	|	|	1.82
30.917	0.00	0.58	1.410	I o	|	|	|	1.82
31.000	0.00	0.58	1.406	I o	|	|	|	1.81
31.083	0.00	0.58	1.402	I o	|	|	|	1.81
31.167	0.00	0.58	1.398	I o	|	|	|	1.80
31.250	0.00	0.58	1.394	I o	|	|	|	1.80
31.333	0.00	0.57	1.390	I o	|	|	|	1.79
31.417	0.00	0.57	1.386	I o	|	|	|	1.79
31.500	0.00	0.57	1.382	I o	|	|	|	1.78
31.583	0.00	0.57	1.378	I o	|	|	|	1.78
31.667	0.00	0.57	1.374	I o	|	|	|	1.77
31.750	0.00	0.56	1.370	I o	|	|	|	1.77
31.833	0.00	0.56	1.366	I o	|	|	|	1.76
31.917	0.00	0.56	1.363	I o	|	|	|	1.76
32.000	0.00	0.56	1.359	I o	|	|	|	1.75
32.083	0.00	0.55	1.355	I o	|	|	|	1.75
32.167	0.00	0.55	1.351	I o	|	|	|	1.74
32.250	0.00	0.55	1.347	I o	|	|	|	1.74
32.333	0.00	0.55	1.344	I o	|	|	|	1.73
32.417	0.00	0.55	1.340	I o	|	|	|	1.73
32.500	0.00	0.54	1.336	I o	|	|	|	1.72
32.583	0.00	0.54	1.332	I o	|	|	|	1.72
32.667	0.00	0.54	1.329	I o	|	|	|	1.72
32.750	0.00	0.54	1.325	I o	|	|	|	1.71
32.833	0.00	0.54	1.321	I o	|	|	|	1.71
32.917	0.00	0.53	1.317	I o	|	|	|	1.70
33.000	0.00	0.53	1.314	I o	|	|	|	1.70
33.083	0.00	0.53	1.310	I o	|	|	|	1.69
33.167	0.00	0.53	1.306	I o	|	|	|	1.69
33.250	0.00	0.53	1.303	I o	|	|	|	1.68
33.333	0.00	0.52	1.299	I o	|	|	|	1.68
33.417	0.00	0.52	1.296	I o	|	|	|	1.68
33.500	0.00	0.52	1.292	I o	|	|	|	1.67
33.583	0.00	0.52	1.288	I o	|	|	|	1.67
33.667	0.00	0.52	1.285	I o	|	|	|	1.66
33.750	0.00	0.51	1.281	I o	|	|	|	1.66
33.833	0.00	0.51	1.278	I o	|	|	|	1.65
33.917	0.00	0.51	1.274	I o	|	|	|	1.65
34.000	0.00	0.51	1.271	I o	|	|	|	1.65
34.083	0.00	0.51	1.267	I o	|	|	|	1.64
34.167	0.00	0.50	1.264	I o	|	|	|	1.64
34.250	0.00	0.50	1.260	I o	|	|	|	1.63
34.333	0.00	0.50	1.257	I o	|	|	|	1.63
34.417	0.00	0.50	1.253	I o	|	|	|	1.62
34.500	0.00	0.50	1.250	I o	|	|	|	1.62
34.583	0.00	0.50	1.247	I o	|	|	|	1.62
34.667	0.00	0.49	1.243	I o	|	|	|	1.61
34.750	0.00	0.49	1.240	I o	|	|	|	1.61
34.833	0.00	0.49	1.236	I o	|	|	|	1.60
34.917	0.00	0.49	1.233	I o	|	|	|	1.60
35.000	0.00	0.49	1.230	I o	|	|	|	1.60
35.083	0.00	0.48	1.226	I o	|	|	|	1.59
35.167	0.00	0.48	1.223	I o	|	|	|	1.59
35.250	0.00	0.48	1.220	I o	|	|	|	1.58
35.333	0.00	0.48	1.216	I o	|	|	|	1.58
35.417	0.00	0.48	1.213	I o	|	|	|	1.57
35.500	0.00	0.47	1.210	I o	|	|	|	1.57
35.583	0.00	0.47	1.207	I o	|	|	|	1.57
35.667	0.00	0.47	1.203	I o	|	|	|	1.56
35.750	0.00	0.47	1.200	I o	|	|	|	1.56
35.833	0.00	0.47	1.197	I o	|	|	|	1.55
35.917	0.00	0.47	1.194	I o	|	|	|	1.55
36.000	0.00	0.46	1.190	I o	|	|	|	1.55
36.083	0.00	0.46	1.187	I o	|	|	|	1.54
36.167	0.00	0.46	1.184	I o	|	|	|	1.54
36.250	0.00	0.46	1.181	I o	|	|	|	1.54
36.333	0.00	0.46	1.178	I o	|	|	|	1.53
36.417	0.00	0.46	1.175	I o	|	|	|	1.53
36.500	0.00	0.45	1.172	I o	|	|	|	1.52
36.583	0.00	0.45	1.168	I o	|	|	|	1.52
36.667	0.00	0.45	1.165	I o	|	|	|	1.52
36.750	0.00	0.45	1.162	I o	|	|	|	1.51
36.833	0.00	0.45	1.159	I o	|	|	|	1.51
36.917	0.00	0.45	1.156	I o	|	|	|	1.50
37.000	0.00	0.44	1.153	I o	|	|	|	1.50
37.083	0.00	0.44	1.150	I o	|	|	|	1.50
37.167	0.00	0.44	1.147	I o	|	|	|	1.49
37.250	0.00	0.44	1.144	I o	|	|	|	1.49
37.333	0.00	0.44	1.141	I o	|	|	|	1.49
37.417	0.00	0.44	1.138	I o	|	|	|	1.48
37.500	0.00	0.43	1.135	I o	|	|	|	1.48
37.583	0.00	0.43	1.132	I o	|	|	|	1.48

37.667	0.00	0.43	1.129	I O	|	|	|	1.47
37.750	0.00	0.43	1.126	I O	|	|	|	1.47
37.833	0.00	0.43	1.123	I O	|	|	|	1.46
37.917	0.00	0.43	1.120	I O	|	|	|	1.46
38.000	0.00	0.42	1.117	I O	|	|	|	1.46
38.083	0.00	0.42	1.114	I O	|	|	|	1.45
38.167	0.00	0.42	1.111	I O	|	|	|	1.45
38.250	0.00	0.42	1.108	I O	|	|	|	1.45
38.333	0.00	0.42	1.106	I O	|	|	|	1.44
38.417	0.00	0.42	1.103	I O	|	|	|	1.44
38.500	0.00	0.41	1.100	I O	|	|	|	1.44
38.583	0.00	0.41	1.097	I O	|	|	|	1.43
38.667	0.00	0.41	1.094	I O	|	|	|	1.43
38.750	0.00	0.41	1.091	I O	|	|	|	1.43
38.833	0.00	0.41	1.089	I O	|	|	|	1.42
38.917	0.00	0.41	1.086	I O	|	|	|	1.42
39.000	0.00	0.40	1.083	I O	|	|	|	1.42
39.083	0.00	0.40	1.080	I O	|	|	|	1.41
39.167	0.00	0.40	1.077	I O	|	|	|	1.41
39.250	0.00	0.40	1.075	I O	|	|	|	1.41
39.333	0.00	0.40	1.072	I O	|	|	|	1.40
39.417	0.00	0.40	1.069	I O	|	|	|	1.40
39.500	0.00	0.40	1.066	I O	|	|	|	1.40
39.583	0.00	0.39	1.064	I O	|	|	|	1.39
39.667	0.00	0.39	1.061	I O	|	|	|	1.39
39.750	0.00	0.39	1.058	I O	|	|	|	1.39
39.833	0.00	0.39	1.056	I O	|	|	|	1.38
39.917	0.00	0.39	1.053	I O	|	|	|	1.38
40.000	0.00	0.39	1.050	IO	|	|	|	1.38
40.083	0.00	0.39	1.048	IO	|	|	|	1.37
40.167	0.00	0.38	1.045	IO	|	|	|	1.37
40.250	0.00	0.38	1.042	IO	|	|	|	1.37
40.333	0.00	0.38	1.040	IO	|	|	|	1.36
40.417	0.00	0.38	1.037	IO	|	|	|	1.36
40.500	0.00	0.38	1.034	IO	|	|	|	1.36
40.583	0.00	0.38	1.032	IO	|	|	|	1.35
40.667	0.00	0.38	1.029	IO	|	|	|	1.35
40.750	0.00	0.37	1.027	IO	|	|	|	1.35
40.833	0.00	0.37	1.024	IO	|	|	|	1.34
40.917	0.00	0.37	1.021	IO	|	|	|	1.34
41.000	0.00	0.37	1.019	IO	|	|	|	1.34
41.083	0.00	0.37	1.016	IO	|	|	|	1.33
41.167	0.00	0.37	1.014	IO	|	|	|	1.33
41.250	0.00	0.37	1.011	IO	|	|	|	1.33
41.333	0.00	0.36	1.009	IO	|	|	|	1.32
41.417	0.00	0.36	1.006	IO	|	|	|	1.32
41.500	0.00	0.36	1.004	IO	|	|	|	1.32
41.583	0.00	0.36	1.001	IO	|	|	|	1.32
41.667	0.00	0.36	0.999	IO	|	|	|	1.31
41.750	0.00	0.36	0.996	IO	|	|	|	1.31
41.833	0.00	0.36	0.994	IO	|	|	|	1.31
41.917	0.00	0.35	0.991	IO	|	|	|	1.30
42.000	0.00	0.35	0.989	IO	|	|	|	1.30
42.083	0.00	0.35	0.987	IO	|	|	|	1.30
42.167	0.00	0.35	0.984	IO	|	|	|	1.29
42.250	0.00	0.35	0.982	IO	|	|	|	1.29
42.333	0.00	0.35	0.979	IO	|	|	|	1.29
42.417	0.00	0.35	0.977	IO	|	|	|	1.29
42.500	0.00	0.35	0.975	IO	|	|	|	1.28
42.583	0.00	0.34	0.972	IO	|	|	|	1.28
42.667	0.00	0.34	0.970	IO	|	|	|	1.28
42.750	0.00	0.34	0.968	IO	|	|	|	1.27
42.833	0.00	0.34	0.965	IO	|	|	|	1.27
42.917	0.00	0.34	0.963	IO	|	|	|	1.27
43.000	0.00	0.34	0.960	IO	|	|	|	1.27
43.083	0.00	0.34	0.958	IO	|	|	|	1.26
43.167	0.00	0.34	0.956	IO	|	|	|	1.26
43.250	0.00	0.33	0.954	IO	|	|	|	1.26
43.333	0.00	0.33	0.951	IO	|	|	|	1.25
43.417	0.00	0.33	0.949	IO	|	|	|	1.25
43.500	0.00	0.33	0.947	IO	|	|	|	1.25
43.583	0.00	0.33	0.944	IO	|	|	|	1.25
43.667	0.00	0.33	0.942	IO	|	|	|	1.24
43.750	0.00	0.33	0.940	IO	|	|	|	1.24
43.833	0.00	0.33	0.938	IO	|	|	|	1.24
43.917	0.00	0.32	0.935	IO	|	|	|	1.24
44.000	0.00	0.32	0.933	IO	|	|	|	1.23
44.083	0.00	0.32	0.931	IO	|	|	|	1.23
44.167	0.00	0.32	0.929	IO	|	|	|	1.23
44.250	0.00	0.32	0.927	IO	|	|	|	1.22
44.333	0.00	0.32	0.924	IO	|	|	|	1.22
44.417	0.00	0.32	0.922	IO	|	|	|	1.22
44.500	0.00	0.32	0.920	IO	|	|	|	1.22
44.583	0.00	0.31	0.918	IO	|	|	|	1.21
44.667	0.00	0.31	0.916	IO	|	|	|	1.21
44.750	0.00	0.31	0.914	IO	|	|	|	1.21

44.833	0.00	0.31	0.911	IO					1.21
44.917	0.00	0.31	0.909	IO					1.20
45.000	0.00	0.31	0.907	IO					1.20
45.083	0.00	0.31	0.905	IO					1.20
45.167	0.00	0.31	0.903	IO					1.20
45.250	0.00	0.30	0.901	IO					1.19
45.333	0.00	0.30	0.899	IO					1.19
45.417	0.00	0.30	0.897	IO					1.19
45.500	0.00	0.30	0.895	IO					1.19
45.583	0.00	0.30	0.892	IO					1.18
45.667	0.00	0.30	0.890	IO					1.18
45.750	0.00	0.30	0.888	IO					1.18
45.833	0.00	0.30	0.886	IO					1.18
45.917	0.00	0.30	0.884	IO					1.17
46.000	0.00	0.29	0.882	IO					1.17
46.083	0.00	0.29	0.880	IO					1.17
46.167	0.00	0.29	0.878	IO					1.17
46.250	0.00	0.29	0.876	IO					1.16
46.333	0.00	0.29	0.874	IO					1.16
46.417	0.00	0.29	0.872	IO					1.16
46.500	0.00	0.29	0.870	IO					1.16
46.583	0.00	0.29	0.868	IO					1.15
46.667	0.00	0.29	0.866	IO					1.15
46.750	0.00	0.28	0.864	IO					1.15
46.833	0.00	0.28	0.862	IO					1.15
46.917	0.00	0.28	0.860	IO					1.14
47.000	0.00	0.28	0.858	IO					1.14
47.083	0.00	0.28	0.856	IO					1.14
47.167	0.00	0.28	0.855	IO					1.14
47.250	0.00	0.28	0.853	IO					1.13
47.333	0.00	0.28	0.851	IO					1.13
47.417	0.00	0.28	0.849	IO					1.13
47.500	0.00	0.28	0.847	IO					1.13
47.583	0.00	0.27	0.845	IO					1.12
47.667	0.00	0.27	0.843	IO					1.12
47.750	0.00	0.27	0.841	IO					1.12
47.833	0.00	0.27	0.839	IO					1.12
47.917	0.00	0.27	0.838	IO					1.12
48.000	0.00	0.27	0.836	IO					1.11
48.083	0.00	0.27	0.834	IO					1.11
48.167	0.00	0.27	0.832	IO					1.11
48.250	0.00	0.27	0.830	IO					1.11
48.333	0.00	0.26	0.828	IO					1.10
48.417	0.00	0.26	0.827	IO					1.10
48.500	0.00	0.26	0.825	IO					1.10
48.583	0.00	0.26	0.823	IO					1.10
48.667	0.00	0.26	0.821	IO					1.10
48.750	0.00	0.26	0.819	IO					1.09
48.833	0.00	0.26	0.818	IO					1.09
48.917	0.00	0.26	0.816	IO					1.09
49.000	0.00	0.26	0.814	IO					1.09
49.083	0.00	0.26	0.812	IO					1.08
49.167	0.00	0.26	0.810	IO					1.08
49.250	0.00	0.25	0.809	IO					1.08
49.333	0.00	0.25	0.807	IO					1.08
49.417	0.00	0.25	0.805	IO					1.08
49.500	0.00	0.25	0.803	IO					1.07
49.583	0.00	0.25	0.802	IO					1.07
49.667	0.00	0.25	0.800	IO					1.07
49.750	0.00	0.25	0.798	IO					1.07
49.833	0.00	0.25	0.797	IO					1.07
49.917	0.00	0.25	0.795	IO					1.06
50.000	0.00	0.25	0.793	IO					1.06
50.083	0.00	0.24	0.792	IO					1.06
50.167	0.00	0.24	0.790	IO					1.06
50.250	0.00	0.24	0.788	IO					1.06
50.333	0.00	0.24	0.786	IO					1.05
50.417	0.00	0.24	0.785	IO					1.05
50.500	0.00	0.24	0.783	IO					1.05
50.583	0.00	0.24	0.782	IO					1.05
50.667	0.00	0.24	0.780	IO					1.05
50.750	0.00	0.24	0.778	IO					1.04
50.833	0.00	0.24	0.777	IO					1.04
50.917	0.00	0.24	0.775	IO					1.04
51.000	0.00	0.23	0.773	IO					1.04
51.083	0.00	0.23	0.772	IO					1.04
51.167	0.00	0.23	0.770	IO					1.03
51.250	0.00	0.23	0.769	IO					1.03
51.333	0.00	0.23	0.767	IO					1.03
51.417	0.00	0.23	0.765	IO					1.03
51.500	0.00	0.23	0.764	IO					1.03
51.583	0.00	0.23	0.762	IO					1.02
51.667	0.00	0.23	0.761	IO					1.02
51.750	0.00	0.23	0.759	IO					1.02
51.833	0.00	0.23	0.757	IO					1.02
51.917	0.00	0.23	0.756	IO					1.02

52.000	0.00	0.22	0.754	IO				1.01
52.083	0.00	0.22	0.753	IO				1.01
52.167	0.00	0.22	0.751	IO				1.01
52.250	0.00	0.22	0.750	IO				1.01
52.333	0.00	0.22	0.748	IO				1.01
52.417	0.00	0.22	0.747	IO				1.00
52.500	0.00	0.22	0.745	IO				1.00
52.583	0.00	0.22	0.744	IO				1.00
52.667	0.00	0.22	0.742	IO				1.00
52.750	0.00	0.22	0.741	IO				1.00
52.833	0.00	0.22	0.739	IO				0.99
52.917	0.00	0.22	0.738	IO				0.99
53.000	0.00	0.22	0.736	IO				0.99
53.083	0.00	0.22	0.735	IO				0.99
53.167	0.00	0.22	0.733	IO				0.99
53.250	0.00	0.21	0.732	IO				0.98
53.333	0.00	0.21	0.730	IO				0.98
53.417	0.00	0.21	0.729	IO				0.98
53.500	0.00	0.21	0.727	IO				0.98
53.583	0.00	0.21	0.726	IO				0.98
53.667	0.00	0.21	0.724	IO				0.98
53.750	0.00	0.21	0.723	IO				0.97
53.833	0.00	0.21	0.722	IO				0.97
53.917	0.00	0.21	0.720	IO				0.97
54.000	0.00	0.21	0.719	IO				0.97
54.083	0.00	0.21	0.717	IO				0.97
54.167	0.00	0.21	0.716	IO				0.96
54.250	0.00	0.21	0.714	IO				0.96
54.333	0.00	0.21	0.713	IO				0.96
54.417	0.00	0.21	0.711	IO				0.96
54.500	0.00	0.21	0.710	IO				0.96
54.583	0.00	0.21	0.709	IO				0.95
54.667	0.00	0.21	0.707	IO				0.95
54.750	0.00	0.21	0.706	IO				0.95
54.833	0.00	0.21	0.704	IO				0.95
54.917	0.00	0.21	0.703	IO				0.95
55.000	0.00	0.21	0.701	IO				0.94
55.083	0.00	0.21	0.700	IO				0.94
55.167	0.00	0.20	0.699	IO				0.94
55.250	0.00	0.20	0.697	IO				0.94
55.333	0.00	0.20	0.696	IO				0.94
55.417	0.00	0.20	0.694	IO				0.93
55.500	0.00	0.20	0.693	IO				0.93
55.583	0.00	0.20	0.692	IO				0.93
55.667	0.00	0.20	0.690	IO				0.93
55.750	0.00	0.20	0.689	IO				0.93
55.833	0.00	0.20	0.687	IO				0.93
55.917	0.00	0.20	0.686	IO				0.92
56.000	0.00	0.20	0.685	IO				0.92
56.083	0.00	0.20	0.683	IO				0.92
56.167	0.00	0.20	0.682	IO				0.92
56.250	0.00	0.20	0.680	IO				0.92
56.333	0.00	0.20	0.679	IO				0.91
56.417	0.00	0.20	0.678	IO				0.91
56.500	0.00	0.20	0.676	IO				0.91
56.583	0.00	0.20	0.675	IO				0.91
56.667	0.00	0.20	0.674	IO				0.91
56.750	0.00	0.20	0.672	IO				0.90
56.833	0.00	0.20	0.671	IO				0.90
56.917	0.00	0.20	0.670	IO				0.90
57.000	0.00	0.20	0.668	IO				0.90
57.083	0.00	0.20	0.667	IO				0.90
57.167	0.00	0.20	0.665	IO				0.90
57.250	0.00	0.19	0.664	IO				0.89
57.333	0.00	0.19	0.663	IO				0.89
57.417	0.00	0.19	0.661	IO				0.89
57.500	0.00	0.19	0.660	O				0.89
57.583	0.00	0.19	0.659	O				0.89
57.667	0.00	0.19	0.657	O				0.88
57.750	0.00	0.19	0.656	O				0.88
57.833	0.00	0.19	0.655	O				0.88
57.917	0.00	0.19	0.653	O				0.88
58.000	0.00	0.19	0.652	O				0.88
58.083	0.00	0.19	0.651	O				0.88
58.167	0.00	0.19	0.650	O				0.87
58.250	0.00	0.19	0.648	O				0.87
58.333	0.00	0.19	0.647	O				0.87
58.417	0.00	0.19	0.646	O				0.87
58.500	0.00	0.19	0.644	O				0.87
58.583	0.00	0.19	0.643	O				0.87
58.667	0.00	0.19	0.642	O				0.86
58.750	0.00	0.19	0.640	O				0.86
58.833	0.00	0.19	0.639	O				0.86
58.917	0.00	0.19	0.638	O				0.86
59.000	0.00	0.19	0.637	O				0.86
59.083	0.00	0.19	0.635	O				0.86

59.167	0.00	0.19	0.634	o	|	|	|	0.85
59.250	0.00	0.19	0.633	o	|	|	|	0.85
59.333	0.00	0.19	0.631	o	|	|	|	0.85
59.417	0.00	0.18	0.630	o	|	|	|	0.85
59.500	0.00	0.18	0.629	o	|	|	|	0.85
59.583	0.00	0.18	0.628	o	|	|	|	0.84
59.667	0.00	0.18	0.626	o	|	|	|	0.84
59.750	0.00	0.18	0.625	o	|	|	|	0.84
59.833	0.00	0.18	0.624	o	|	|	|	0.84
59.917	0.00	0.18	0.623	o	|	|	|	0.84
60.000	0.00	0.18	0.621	o	|	|	|	0.84
60.083	0.00	0.18	0.620	o	|	|	|	0.83
60.167	0.00	0.18	0.619	o	|	|	|	0.83
60.250	0.00	0.18	0.618	o	|	|	|	0.83
60.333	0.00	0.18	0.616	o	|	|	|	0.83
60.417	0.00	0.18	0.615	o	|	|	|	0.83
60.500	0.00	0.18	0.614	o	|	|	|	0.83
60.583	0.00	0.18	0.613	o	|	|	|	0.82
60.667	0.00	0.18	0.611	o	|	|	|	0.82
60.750	0.00	0.18	0.610	o	|	|	|	0.82
60.833	0.00	0.18	0.609	o	|	|	|	0.82
60.917	0.00	0.18	0.608	o	|	|	|	0.82
61.000	0.00	0.18	0.606	o	|	|	|	0.82
61.083	0.00	0.18	0.605	o	|	|	|	0.81
61.167	0.00	0.18	0.604	o	|	|	|	0.81
61.250	0.00	0.18	0.603	o	|	|	|	0.81
61.333	0.00	0.18	0.602	o	|	|	|	0.81
61.417	0.00	0.18	0.600	o	|	|	|	0.81
61.500	0.00	0.18	0.599	o	|	|	|	0.81
61.583	0.00	0.18	0.598	o	|	|	|	0.80
61.667	0.00	0.18	0.597	o	|	|	|	0.80
61.750	0.00	0.17	0.595	o	|	|	|	0.80
61.833	0.00	0.17	0.594	o	|	|	|	0.80
61.917	0.00	0.17	0.593	o	|	|	|	0.80
62.000	0.00	0.17	0.592	o	|	|	|	0.80
62.083	0.00	0.17	0.591	o	|	|	|	0.80
62.167	0.00	0.17	0.590	o	|	|	|	0.79
62.250	0.00	0.17	0.588	o	|	|	|	0.79
62.333	0.00	0.17	0.587	o	|	|	|	0.79
62.417	0.00	0.17	0.586	o	|	|	|	0.79
62.500	0.00	0.17	0.585	o	|	|	|	0.79
62.583	0.00	0.17	0.584	o	|	|	|	0.79
62.667	0.00	0.17	0.582	o	|	|	|	0.78
62.750	0.00	0.17	0.581	o	|	|	|	0.78
62.833	0.00	0.17	0.580	o	|	|	|	0.78
62.917	0.00	0.17	0.579	o	|	|	|	0.78
63.000	0.00	0.17	0.578	o	|	|	|	0.78
63.083	0.00	0.17	0.577	o	|	|	|	0.78
63.167	0.00	0.17	0.575	o	|	|	|	0.77
63.250	0.00	0.17	0.574	o	|	|	|	0.77
63.333	0.00	0.17	0.573	o	|	|	|	0.77
63.417	0.00	0.17	0.572	o	|	|	|	0.77
63.500	0.00	0.17	0.571	o	|	|	|	0.77
63.583	0.00	0.17	0.570	o	|	|	|	0.77
63.667	0.00	0.17	0.568	o	|	|	|	0.77
63.750	0.00	0.17	0.567	o	|	|	|	0.76
63.833	0.00	0.17	0.566	o	|	|	|	0.76
63.917	0.00	0.17	0.565	o	|	|	|	0.76
64.000	0.00	0.17	0.564	o	|	|	|	0.76
64.083	0.00	0.17	0.563	o	|	|	|	0.76
64.167	0.00	0.16	0.562	o	|	|	|	0.76
64.250	0.00	0.16	0.560	o	|	|	|	0.75
64.333	0.00	0.16	0.559	o	|	|	|	0.75
64.417	0.00	0.16	0.558	o	|	|	|	0.75
64.500	0.00	0.16	0.557	o	|	|	|	0.75
64.583	0.00	0.16	0.556	o	|	|	|	0.75
64.667	0.00	0.16	0.555	o	|	|	|	0.75
64.750	0.00	0.16	0.554	o	|	|	|	0.75
64.833	0.00	0.16	0.553	o	|	|	|	0.74
64.917	0.00	0.16	0.551	o	|	|	|	0.74
65.000	0.00	0.16	0.550	o	|	|	|	0.74
65.083	0.00	0.16	0.549	o	|	|	|	0.74
65.167	0.00	0.16	0.548	o	|	|	|	0.74
65.250	0.00	0.16	0.547	o	|	|	|	0.74
65.333	0.00	0.16	0.546	o	|	|	|	0.73
65.417	0.00	0.16	0.545	o	|	|	|	0.73
65.500	0.00	0.16	0.544	o	|	|	|	0.73
65.583	0.00	0.16	0.543	o	|	|	|	0.73
65.667	0.00	0.16	0.542	o	|	|	|	0.73
65.750	0.00	0.16	0.540	o	|	|	|	0.73
65.833	0.00	0.16	0.539	o	|	|	|	0.73
65.917	0.00	0.16	0.538	o	|	|	|	0.72
66.000	0.00	0.16	0.537	o	|	|	|	0.72
66.083	0.00	0.16	0.536	o	|	|	|	0.72
66.167	0.00	0.16	0.535	o	|	|	|	0.72
66.250	0.00	0.16	0.534	o	|	|	|	0.72

66.333	0.00	0.16	0.533	o	|	|	|	|	0.72
66.417	0.00	0.16	0.532	o	|	|	|	|	0.72
66.500	0.00	0.16	0.531	o	|	|	|	|	0.71
66.583	0.00	0.16	0.530	o	|	|	|	|	0.71
66.667	0.00	0.16	0.529	o	|	|	|	|	0.71
66.750	0.00	0.15	0.527	o	|	|	|	|	0.71
66.833	0.00	0.15	0.526	o	|	|	|	|	0.71
66.917	0.00	0.15	0.525	o	|	|	|	|	0.71
67.000	0.00	0.15	0.524	o	|	|	|	|	0.71
67.083	0.00	0.15	0.523	o	|	|	|	|	0.70
67.167	0.00	0.15	0.522	o	|	|	|	|	0.70
67.250	0.00	0.15	0.521	o	|	|	|	|	0.70
67.333	0.00	0.15	0.520	o	|	|	|	|	0.70
67.417	0.00	0.15	0.519	o	|	|	|	|	0.70
67.500	0.00	0.15	0.518	o	|	|	|	|	0.70
67.583	0.00	0.15	0.517	o	|	|	|	|	0.70
67.667	0.00	0.15	0.516	o	|	|	|	|	0.69
67.750	0.00	0.15	0.515	o	|	|	|	|	0.69
67.833	0.00	0.15	0.514	o	|	|	|	|	0.69
67.917	0.00	0.15	0.513	o	|	|	|	|	0.69
68.000	0.00	0.15	0.512	o	|	|	|	|	0.69
68.083	0.00	0.15	0.511	o	|	|	|	|	0.69
68.167	0.00	0.15	0.510	o	|	|	|	|	0.69
68.250	0.00	0.15	0.509	o	|	|	|	|	0.68
68.333	0.00	0.15	0.508	o	|	|	|	|	0.68
68.417	0.00	0.15	0.507	o	|	|	|	|	0.68
68.500	0.00	0.15	0.506	o	|	|	|	|	0.68
68.583	0.00	0.15	0.505	o	|	|	|	|	0.68
68.667	0.00	0.15	0.504	o	|	|	|	|	0.68
68.750	0.00	0.15	0.503	o	|	|	|	|	0.68
68.833	0.00	0.15	0.502	o	|	|	|	|	0.67
68.917	0.00	0.15	0.500	o	|	|	|	|	0.67
69.000	0.00	0.15	0.499	o	|	|	|	|	0.67
69.083	0.00	0.15	0.498	o	|	|	|	|	0.67
69.167	0.00	0.15	0.497	o	|	|	|	|	0.67
69.250	0.00	0.15	0.496	o	|	|	|	|	0.67
69.333	0.00	0.15	0.495	o	|	|	|	|	0.67
69.417	0.00	0.15	0.494	o	|	|	|	|	0.67
69.500	0.00	0.14	0.493	o	|	|	|	|	0.66
69.583	0.00	0.14	0.492	o	|	|	|	|	0.66
69.667	0.00	0.14	0.491	o	|	|	|	|	0.66
69.750	0.00	0.14	0.490	o	|	|	|	|	0.66
69.833	0.00	0.14	0.489	o	|	|	|	|	0.66
69.917	0.00	0.14	0.489	o	|	|	|	|	0.66
70.000	0.00	0.14	0.488	o	|	|	|	|	0.66
70.083	0.00	0.14	0.487	o	|	|	|	|	0.65
70.167	0.00	0.14	0.486	o	|	|	|	|	0.65
70.250	0.00	0.14	0.485	o	|	|	|	|	0.65
70.333	0.00	0.14	0.484	o	|	|	|	|	0.65
70.417	0.00	0.14	0.483	o	|	|	|	|	0.65
70.500	0.00	0.14	0.482	o	|	|	|	|	0.65
70.583	0.00	0.14	0.481	o	|	|	|	|	0.65
70.667	0.00	0.14	0.480	o	|	|	|	|	0.65
70.750	0.00	0.14	0.479	o	|	|	|	|	0.64
70.833	0.00	0.14	0.478	o	|	|	|	|	0.64
70.917	0.00	0.14	0.477	o	|	|	|	|	0.64
71.000	0.00	0.14	0.476	o	|	|	|	|	0.64
71.083	0.00	0.14	0.475	o	|	|	|	|	0.64
71.167	0.00	0.14	0.474	o	|	|	|	|	0.64
71.250	0.00	0.14	0.473	o	|	|	|	|	0.64
71.333	0.00	0.14	0.472	o	|	|	|	|	0.64
71.417	0.00	0.14	0.471	o	|	|	|	|	0.63
71.500	0.00	0.14	0.470	o	|	|	|	|	0.63
71.583	0.00	0.14	0.469	o	|	|	|	|	0.63
71.667	0.00	0.14	0.468	o	|	|	|	|	0.63
71.750	0.00	0.14	0.467	o	|	|	|	|	0.63
71.833	0.00	0.14	0.466	o	|	|	|	|	0.63
71.917	0.00	0.14	0.465	o	|	|	|	|	0.63
72.000	0.00	0.14	0.464	o	|	|	|	|	0.63
72.083	0.00	0.14	0.464	o	|	|	|	|	0.62
72.167	0.00	0.14	0.463	o	|	|	|	|	0.62
72.250	0.00	0.14	0.462	o	|	|	|	|	0.62
72.333	0.00	0.14	0.461	o	|	|	|	|	0.62
72.417	0.00	0.13	0.460	o	|	|	|	|	0.62
72.500	0.00	0.13	0.459	o	|	|	|	|	0.62
72.583	0.00	0.13	0.458	o	|	|	|	|	0.62
72.667	0.00	0.13	0.457	o	|	|	|	|	0.62
72.750	0.00	0.13	0.456	o	|	|	|	|	0.61
72.833	0.00	0.13	0.455	o	|	|	|	|	0.61
72.917	0.00	0.13	0.454	o	|	|	|	|	0.61
73.000	0.00	0.13	0.453	o	|	|	|	|	0.61
73.083	0.00	0.13	0.452	o	|	|	|	|	0.61
73.167	0.00	0.13	0.451	o	|	|	|	|	0.61
73.250	0.00	0.13	0.451	o	|	|	|	|	0.61
73.333	0.00	0.13	0.450	o	|	|	|	|	0.61
73.417	0.00	0.13	0.449	o	|	|	|	|	0.60

73.500	0.00	0.13	0.448	o	|	|	|	0.60
73.583	0.00	0.13	0.447	o	|	|	|	0.60
73.667	0.00	0.13	0.446	o	|	|	|	0.60
73.750	0.00	0.13	0.445	o	|	|	|	0.60
73.833	0.00	0.13	0.444	o	|	|	|	0.60
73.917	0.00	0.13	0.443	o	|	|	|	0.60
74.000	0.00	0.13	0.442	o	|	|	|	0.60
74.083	0.00	0.13	0.442	o	|	|	|	0.59
74.167	0.00	0.13	0.441	o	|	|	|	0.59
74.250	0.00	0.13	0.440	o	|	|	|	0.59
74.333	0.00	0.13	0.439	o	|	|	|	0.59
74.417	0.00	0.13	0.438	o	|	|	|	0.59
74.500	0.00	0.13	0.437	o	|	|	|	0.59
74.583	0.00	0.13	0.436	o	|	|	|	0.59
74.667	0.00	0.13	0.435	o	|	|	|	0.59
74.750	0.00	0.13	0.434	o	|	|	|	0.58
74.833	0.00	0.13	0.434	o	|	|	|	0.58
74.917	0.00	0.13	0.433	o	|	|	|	0.58
75.000	0.00	0.13	0.432	o	|	|	|	0.58
75.083	0.00	0.13	0.431	o	|	|	|	0.58
75.167	0.00	0.13	0.430	o	|	|	|	0.58
75.250	0.00	0.13	0.429	o	|	|	|	0.58
75.333	0.00	0.13	0.428	o	|	|	|	0.58
75.417	0.00	0.13	0.428	o	|	|	|	0.58
75.500	0.00	0.13	0.427	o	|	|	|	0.57
75.583	0.00	0.12	0.426	o	|	|	|	0.57
75.667	0.00	0.12	0.425	o	|	|	|	0.57
75.750	0.00	0.12	0.424	o	|	|	|	0.57
75.833	0.00	0.12	0.423	o	|	|	|	0.57
75.917	0.00	0.12	0.422	o	|	|	|	0.57
76.000	0.00	0.12	0.422	o	|	|	|	0.57
76.083	0.00	0.12	0.421	o	|	|	|	0.57
76.167	0.00	0.12	0.420	o	|	|	|	0.57
76.250	0.00	0.12	0.419	o	|	|	|	0.56
76.333	0.00	0.12	0.418	o	|	|	|	0.56
76.417	0.00	0.12	0.417	o	|	|	|	0.56
76.500	0.00	0.12	0.416	o	|	|	|	0.56
76.583	0.00	0.12	0.416	o	|	|	|	0.56
76.667	0.00	0.12	0.415	o	|	|	|	0.56
76.750	0.00	0.12	0.414	o	|	|	|	0.56
76.833	0.00	0.12	0.413	o	|	|	|	0.56
76.917	0.00	0.12	0.412	o	|	|	|	0.55
77.000	0.00	0.12	0.411	o	|	|	|	0.55
77.083	0.00	0.12	0.411	o	|	|	|	0.55
77.167	0.00	0.12	0.410	o	|	|	|	0.55
77.250	0.00	0.12	0.409	o	|	|	|	0.55
77.333	0.00	0.12	0.408	o	|	|	|	0.55
77.417	0.00	0.12	0.407	o	|	|	|	0.55
77.500	0.00	0.12	0.406	o	|	|	|	0.55
77.583	0.00	0.12	0.406	o	|	|	|	0.55
77.667	0.00	0.12	0.405	o	|	|	|	0.54
77.750	0.00	0.12	0.404	o	|	|	|	0.54
77.833	0.00	0.12	0.403	o	|	|	|	0.54
77.917	0.00	0.12	0.402	o	|	|	|	0.54
78.000	0.00	0.12	0.402	o	|	|	|	0.54
78.083	0.00	0.12	0.401	o	|	|	|	0.54
78.167	0.00	0.12	0.400	o	|	|	|	0.54
78.250	0.00	0.12	0.399	o	|	|	|	0.54
78.333	0.00	0.12	0.398	o	|	|	|	0.54
78.417	0.00	0.12	0.398	o	|	|	|	0.54
78.500	0.00	0.12	0.397	o	|	|	|	0.53
78.583	0.00	0.12	0.396	o	|	|	|	0.53
78.667	0.00	0.12	0.395	o	|	|	|	0.53
78.750	0.00	0.12	0.394	o	|	|	|	0.53
78.833	0.00	0.12	0.394	o	|	|	|	0.53
78.917	0.00	0.12	0.393	o	|	|	|	0.53
79.000	0.00	0.11	0.392	o	|	|	|	0.53
79.083	0.00	0.11	0.391	o	|	|	|	0.53
79.167	0.00	0.11	0.390	o	|	|	|	0.53
79.250	0.00	0.11	0.390	o	|	|	|	0.52
79.333	0.00	0.11	0.389	o	|	|	|	0.52
79.417	0.00	0.11	0.388	o	|	|	|	0.52
79.500	0.00	0.11	0.387	o	|	|	|	0.52
79.583	0.00	0.11	0.386	o	|	|	|	0.52
79.667	0.00	0.11	0.386	o	|	|	|	0.52
79.750	0.00	0.11	0.385	o	|	|	|	0.52
79.833	0.00	0.11	0.384	o	|	|	|	0.52
79.917	0.00	0.11	0.383	o	|	|	|	0.52
80.000	0.00	0.11	0.383	o	|	|	|	0.51
80.083	0.00	0.11	0.382	o	|	|	|	0.51
80.167	0.00	0.11	0.381	o	|	|	|	0.51
80.250	0.00	0.11	0.380	o	|	|	|	0.51
80.333	0.00	0.11	0.379	o	|	|	|	0.51
80.417	0.00	0.11	0.379	o	|	|	|	0.51
80.500	0.00	0.11	0.378	o	|	|	|	0.51
80.583	0.00	0.11	0.377	o	|	|	|	0.51

80.667	0.00	0.11	0.376	o	|	|	|	|	0.51
80.750	0.00	0.11	0.376	o	|	|	|	|	0.51
80.833	0.00	0.11	0.375	o	|	|	|	|	0.50
80.917	0.00	0.11	0.374	o	|	|	|	|	0.50
81.000	0.00	0.11	0.373	o	|	|	|	|	0.50
81.083	0.00	0.11	0.373	o	|	|	|	|	0.50
81.167	0.00	0.11	0.372	o	|	|	|	|	0.50
81.250	0.00	0.11	0.371	o	|	|	|	|	0.50
81.333	0.00	0.11	0.370	o	|	|	|	|	0.50
81.417	0.00	0.11	0.370	o	|	|	|	|	0.50
81.500	0.00	0.11	0.369	o	|	|	|	|	0.50
81.583	0.00	0.11	0.368	o	|	|	|	|	0.50
81.667	0.00	0.11	0.367	o	|	|	|	|	0.49
81.750	0.00	0.11	0.367	o	|	|	|	|	0.49
81.833	0.00	0.11	0.366	o	|	|	|	|	0.49
81.917	0.00	0.11	0.365	o	|	|	|	|	0.49
82.000	0.00	0.11	0.364	o	|	|	|	|	0.49
82.083	0.00	0.11	0.364	o	|	|	|	|	0.49
82.167	0.00	0.11	0.363	o	|	|	|	|	0.49
82.250	0.00	0.11	0.362	o	|	|	|	|	0.49
82.333	0.00	0.11	0.362	o	|	|	|	|	0.49
82.417	0.00	0.11	0.361	o	|	|	|	|	0.49
82.500	0.00	0.11	0.360	o	|	|	|	|	0.48
82.583	0.00	0.11	0.359	o	|	|	|	|	0.48
82.667	0.00	0.11	0.359	o	|	|	|	|	0.48
82.750	0.00	0.11	0.358	o	|	|	|	|	0.48
82.833	0.00	0.10	0.357	o	|	|	|	|	0.48
82.917	0.00	0.10	0.356	o	|	|	|	|	0.48
83.000	0.00	0.10	0.356	o	|	|	|	|	0.48
83.083	0.00	0.10	0.355	o	|	|	|	|	0.48
83.167	0.00	0.10	0.354	o	|	|	|	|	0.48
83.250	0.00	0.10	0.354	o	|	|	|	|	0.48
83.333	0.00	0.10	0.353	o	|	|	|	|	0.47
83.417	0.00	0.10	0.352	o	|	|	|	|	0.47
83.500	0.00	0.10	0.351	o	|	|	|	|	0.47
83.583	0.00	0.10	0.351	o	|	|	|	|	0.47
83.667	0.00	0.10	0.350	o	|	|	|	|	0.47
83.750	0.00	0.10	0.349	o	|	|	|	|	0.47
83.833	0.00	0.10	0.349	o	|	|	|	|	0.47
83.917	0.00	0.10	0.348	o	|	|	|	|	0.47
84.000	0.00	0.10	0.347	o	|	|	|	|	0.47
84.083	0.00	0.10	0.346	o	|	|	|	|	0.47
84.167	0.00	0.10	0.346	o	|	|	|	|	0.47
84.250	0.00	0.10	0.345	o	|	|	|	|	0.46
84.333	0.00	0.10	0.344	o	|	|	|	|	0.46
84.417	0.00	0.10	0.344	o	|	|	|	|	0.46
84.500	0.00	0.10	0.343	o	|	|	|	|	0.46
84.583	0.00	0.10	0.342	o	|	|	|	|	0.46
84.667	0.00	0.10	0.342	o	|	|	|	|	0.46
84.750	0.00	0.10	0.341	o	|	|	|	|	0.46
84.833	0.00	0.10	0.340	o	|	|	|	|	0.46

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 1018
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.345 (CFS)
Total volume = 2.669 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 05/09/24

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: pro110110.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    17
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       50.425 (CFS)
               Total volume =       1.704 (Ac.Ft)
       Status of hydrographs being held in storage
                  Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
*************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
___________________________________________________________________________

User entry of depth-outflow-storage data
---------------------------------------------------------------------
Total number of inflow hydrograph intervals = 17
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
---------------------------------------------------------------------
---------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
---------------------------------------------------------------------
---------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
---------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.743      0.218      0.742        0.744
   2.000      1.561      0.668      1.559        1.563
   3.000      2.456      1.518      2.451        2.461
   3.500      2.931     58.349      2.730        3.132
   4.000      3.425    162.007      2.867        3.983
---------------------------------------------------------------------
               Hydrograph Detention Basin Routing
---------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
---------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                    Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0      12.6   25.21   37.82   50.42 (Ft.)
 0.083    2.31    0.00      0.008  OI      |       |       |       |     0.01
 0.167    6.45    0.01      0.038  O   I   |       |       |       |     0.05
 0.250    8.57    0.03      0.090  O    I  |       |       |       |     0.12
 0.333    9.80    0.04      0.153  O     I |       |       |       |     0.21
 0.417   11.02    0.07      0.224  O     I |       |       |       |     0.30
 0.500   12.71    0.09      0.305  O       I       |       |       |     0.41
 0.583   14.72    0.12      0.399  O       |I      |       |       |     0.54
 0.667   17.61    0.15      0.509  O       |  I    |       |       |     0.69
 0.750   24.94    0.19      0.655  O       |      I|       |       |     0.88
 0.833   47.39    0.31      0.902  O       |       |       |     I |     1.19
 0.917   50.42    0.49      1.236  O       |       |       |       I     1.60
 1.000   22.99    0.63      1.485  O       |     I |       |       |     1.91
 1.083   11.33    0.70      1.599  O      I|       |       |       |     2.04
 1.167    4.46    0.75      1.648  O I     |       |       |       |     2.10
 1.250    2.06    0.77      1.665  OI      |       |       |       |     2.12
 1.333    0.47    0.77      1.669  O       |       |       |       |     2.12
 1.417    0.12    0.77      1.665  O       |       |       |       |     2.12
 1.500    0.00    0.76      1.661  O       |       |       |       |     2.11
 1.583    0.00    0.76      1.655  O       |       |       |       |     2.11
 1.667    0.00    0.75      1.650  O       |       |       |       |     2.10
 1.750    0.00    0.75      1.645  O       |       |       |       |     2.09
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1.833	0.00	0.74	1.640	o	|	|	|	|	2.09
1.917	0.00	0.74	1.635	o	|	|	|	|	2.08
2.000	0.00	0.73	1.630	o	|	|	|	|	2.08
2.083	0.00	0.73	1.625	o	|	|	|	|	2.07
2.167	0.00	0.72	1.620	o	|	|	|	|	2.07
2.250	0.00	0.72	1.615	o	|	|	|	|	2.06
2.333	0.00	0.71	1.610	o	|	|	|	|	2.05
2.417	0.00	0.71	1.605	o	|	|	|	|	2.05
2.500	0.00	0.71	1.600	o	|	|	|	|	2.04
2.583	0.00	0.70	1.595	o	|	|	|	|	2.04
2.667	0.00	0.70	1.590	o	|	|	|	|	2.03
2.750	0.00	0.69	1.586	o	|	|	|	|	2.03
2.833	0.00	0.69	1.581	o	|	|	|	|	2.02
2.917	0.00	0.68	1.576	o	|	|	|	|	2.02
3.000	0.00	0.68	1.571	o	|	|	|	|	2.01
3.083	0.00	0.67	1.567	o	|	|	|	|	2.01
3.167	0.00	0.67	1.562	o	|	|	|	|	2.00
3.250	0.00	0.67	1.558	o	|	|	|	|	2.00
3.333	0.00	0.66	1.553	o	|	|	|	|	1.99
3.417	0.00	0.66	1.548	o	|	|	|	|	1.98
3.500	0.00	0.66	1.544	o	|	|	|	|	1.98
3.583	0.00	0.66	1.539	o	|	|	|	|	1.97
3.667	0.00	0.65	1.535	o	|	|	|	|	1.97
3.750	0.00	0.65	1.530	o	|	|	|	|	1.96
3.833	0.00	0.65	1.526	o	|	|	|	|	1.96
3.917	0.00	0.65	1.521	o	|	|	|	|	1.95
4.000	0.00	0.64	1.517	o	|	|	|	|	1.95
4.083	0.00	0.64	1.513	o	|	|	|	|	1.94
4.167	0.00	0.64	1.508	o	|	|	|	|	1.94
4.250	0.00	0.64	1.504	o	|	|	|	|	1.93
4.333	0.00	0.63	1.499	o	|	|	|	|	1.92
4.417	0.00	0.63	1.495	o	|	|	|	|	1.92
4.500	0.00	0.63	1.491	o	|	|	|	|	1.91
4.583	0.00	0.63	1.486	o	|	|	|	|	1.91
4.667	0.00	0.62	1.482	o	|	|	|	|	1.90
4.750	0.00	0.62	1.478	o	|	|	|	|	1.90
4.833	0.00	0.62	1.473	o	|	|	|	|	1.89
4.917	0.00	0.62	1.469	o	|	|	|	|	1.89
5.000	0.00	0.62	1.465	o	|	|	|	|	1.88
5.083	0.00	0.61	1.461	o	|	|	|	|	1.88
5.167	0.00	0.61	1.457	o	|	|	|	|	1.87
5.250	0.00	0.61	1.452	o	|	|	|	|	1.87
5.333	0.00	0.61	1.448	o	|	|	|	|	1.86
5.417	0.00	0.60	1.444	o	|	|	|	|	1.86
5.500	0.00	0.60	1.440	o	|	|	|	|	1.85
5.583	0.00	0.60	1.436	o	|	|	|	|	1.85
5.667	0.00	0.60	1.432	o	|	|	|	|	1.84
5.750	0.00	0.59	1.427	o	|	|	|	|	1.84
5.833	0.00	0.59	1.423	o	|	|	|	|	1.83
5.917	0.00	0.59	1.419	o	|	|	|	|	1.83
6.000	0.00	0.59	1.415	o	|	|	|	|	1.82
6.083	0.00	0.59	1.411	o	|	|	|	|	1.82
6.167	0.00	0.58	1.407	o	|	|	|	|	1.81
6.250	0.00	0.58	1.403	o	|	|	|	|	1.81
6.333	0.00	0.58	1.399	o	|	|	|	|	1.80
6.417	0.00	0.58	1.395	o	|	|	|	|	1.80
6.500	0.00	0.57	1.391	o	|	|	|	|	1.79
6.583	0.00	0.57	1.387	o	|	|	|	|	1.79
6.667	0.00	0.57	1.383	o	|	|	|	|	1.78
6.750	0.00	0.57	1.379	o	|	|	|	|	1.78
6.833	0.00	0.57	1.376	o	|	|	|	|	1.77
6.917	0.00	0.56	1.372	o	|	|	|	|	1.77
7.000	0.00	0.56	1.368	o	|	|	|	|	1.76
7.083	0.00	0.56	1.364	o	|	|	|	|	1.76
7.167	0.00	0.56	1.360	o	|	|	|	|	1.75
7.250	0.00	0.56	1.356	o	|	|	|	|	1.75
7.333	0.00	0.55	1.352	o	|	|	|	|	1.74
7.417	0.00	0.55	1.349	o	|	|	|	|	1.74
7.500	0.00	0.55	1.345	o	|	|	|	|	1.74
7.583	0.00	0.55	1.341	o	|	|	|	|	1.73
7.667	0.00	0.54	1.337	o	|	|	|	|	1.73
7.750	0.00	0.54	1.334	o	|	|	|	|	1.72
7.833	0.00	0.54	1.330	o	|	|	|	|	1.72
7.917	0.00	0.54	1.326	o	|	|	|	|	1.71
8.000	0.00	0.54	1.322	o	|	|	|	|	1.71
8.083	0.00	0.53	1.319	o	|	|	|	|	1.70
8.167	0.00	0.53	1.315	o	|	|	|	|	1.70
8.250	0.00	0.53	1.311	o	|	|	|	|	1.69
8.333	0.00	0.53	1.308	o	|	|	|	|	1.69
8.417	0.00	0.53	1.304	o	|	|	|	|	1.69
8.500	0.00	0.52	1.300	o	|	|	|	|	1.68
8.583	0.00	0.52	1.297	o	|	|	|	|	1.68
8.667	0.00	0.52	1.293	o	|	|	|	|	1.67
8.750	0.00	0.52	1.290	o	|	|	|	|	1.67
8.833	0.00	0.52	1.286	o	|	|	|	|	1.66
8.917	0.00	0.51	1.283	o	|	|	|	|	1.66

9.000	0.00	0.51	1.279	o	|	|	|	|	1.66
9.083	0.00	0.51	1.275	o	|	|	|	|	1.65
9.167	0.00	0.51	1.272	o	|	|	|	|	1.65
9.250	0.00	0.51	1.268	o	|	|	|	|	1.64
9.333	0.00	0.51	1.265	o	|	|	|	|	1.64
9.417	0.00	0.50	1.262	o	|	|	|	|	1.63
9.500	0.00	0.50	1.258	o	|	|	|	|	1.63
9.583	0.00	0.50	1.255	o	|	|	|	|	1.63
9.667	0.00	0.50	1.251	o	|	|	|	|	1.62
9.750	0.00	0.50	1.248	o	|	|	|	|	1.62
9.833	0.00	0.49	1.244	o	|	|	|	|	1.61
9.917	0.00	0.49	1.241	o	|	|	|	|	1.61
10.000	0.00	0.49	1.238	o	|	|	|	|	1.60
10.083	0.00	0.49	1.234	o	|	|	|	|	1.60
10.167	0.00	0.49	1.231	o	|	|	|	|	1.60
10.250	0.00	0.48	1.228	o	|	|	|	|	1.59
10.333	0.00	0.48	1.224	o	|	|	|	|	1.59
10.417	0.00	0.48	1.221	o	|	|	|	|	1.58
10.500	0.00	0.48	1.218	o	|	|	|	|	1.58
10.583	0.00	0.48	1.214	o	|	|	|	|	1.58
10.667	0.00	0.48	1.211	o	|	|	|	|	1.57
10.750	0.00	0.47	1.208	o	|	|	|	|	1.57
10.833	0.00	0.47	1.204	o	|	|	|	|	1.56
10.917	0.00	0.47	1.201	o	|	|	|	|	1.56
11.000	0.00	0.47	1.198	o	|	|	|	|	1.56
11.083	0.00	0.47	1.195	o	|	|	|	|	1.55
11.167	0.00	0.46	1.192	o	|	|	|	|	1.55
11.250	0.00	0.46	1.188	o	|	|	|	|	1.54
11.333	0.00	0.46	1.185	o	|	|	|	|	1.54
11.417	0.00	0.46	1.182	o	|	|	|	|	1.54
11.500	0.00	0.46	1.179	o	|	|	|	|	1.53
11.583	0.00	0.46	1.176	o	|	|	|	|	1.53
11.667	0.00	0.45	1.173	o	|	|	|	|	1.53
11.750	0.00	0.45	1.169	o	|	|	|	|	1.52
11.833	0.00	0.45	1.166	o	|	|	|	|	1.52
11.917	0.00	0.45	1.163	o	|	|	|	|	1.51
12.000	0.00	0.45	1.160	o	|	|	|	|	1.51
12.083	0.00	0.45	1.157	o	|	|	|	|	1.51
12.167	0.00	0.44	1.154	o	|	|	|	|	1.50
12.250	0.00	0.44	1.151	o	|	|	|	|	1.50
12.333	0.00	0.44	1.148	o	|	|	|	|	1.50
12.417	0.00	0.44	1.145	o	|	|	|	|	1.49
12.500	0.00	0.44	1.142	o	|	|	|	|	1.49
12.583	0.00	0.44	1.139	o	|	|	|	|	1.48
12.667	0.00	0.43	1.136	o	|	|	|	|	1.48
12.750	0.00	0.43	1.133	o	|	|	|	|	1.48
12.833	0.00	0.43	1.130	o	|	|	|	|	1.47
12.917	0.00	0.43	1.127	o	|	|	|	|	1.47
13.000	0.00	0.43	1.124	o	|	|	|	|	1.47
13.083	0.00	0.43	1.121	o	|	|	|	|	1.46
13.167	0.00	0.42	1.118	o	|	|	|	|	1.46
13.250	0.00	0.42	1.115	o	|	|	|	|	1.46
13.333	0.00	0.42	1.112	o	|	|	|	|	1.45
13.417	0.00	0.42	1.109	o	|	|	|	|	1.45
13.500	0.00	0.42	1.107	o	|	|	|	|	1.44
13.583	0.00	0.42	1.104	o	|	|	|	|	1.44
13.667	0.00	0.41	1.101	o	|	|	|	|	1.44
13.750	0.00	0.41	1.098	o	|	|	|	|	1.43
13.833	0.00	0.41	1.095	o	|	|	|	|	1.43
13.917	0.00	0.41	1.092	o	|	|	|	|	1.43
14.000	0.00	0.41	1.089	o	|	|	|	|	1.42
14.083	0.00	0.41	1.087	o	|	|	|	|	1.42
14.167	0.00	0.41	1.084	o	|	|	|	|	1.42
14.250	0.00	0.40	1.081	o	|	|	|	|	1.41
14.333	0.00	0.40	1.078	o	|	|	|	|	1.41
14.417	0.00	0.40	1.076	o	|	|	|	|	1.41
14.500	0.00	0.40	1.073	o	|	|	|	|	1.40
14.583	0.00	0.40	1.070	o	|	|	|	|	1.40
14.667	0.00	0.40	1.067	o	|	|	|	|	1.40
14.750	0.00	0.39	1.065	o	|	|	|	|	1.39
14.833	0.00	0.39	1.062	o	|	|	|	|	1.39
14.917	0.00	0.39	1.059	o	|	|	|	|	1.39
15.000	0.00	0.39	1.056	o	|	|	|	|	1.38
15.083	0.00	0.39	1.054	o	|	|	|	|	1.38
15.167	0.00	0.39	1.051	o	|	|	|	|	1.38
15.250	0.00	0.39	1.048	o	|	|	|	|	1.37
15.333	0.00	0.38	1.046	o	|	|	|	|	1.37
15.417	0.00	0.38	1.043	o	|	|	|	|	1.37
15.500	0.00	0.38	1.040	o	|	|	|	|	1.36
15.583	0.00	0.38	1.038	o	|	|	|	|	1.36
15.667	0.00	0.38	1.035	o	|	|	|	|	1.36
15.750	0.00	0.38	1.033	o	|	|	|	|	1.35
15.833	0.00	0.38	1.030	o	|	|	|	|	1.35
15.917	0.00	0.37	1.027	o	|	|	|	|	1.35
16.000	0.00	0.37	1.025	o	|	|	|	|	1.34
16.083	0.00	0.37	1.022	o	|	|	|	|	1.34

16.167	0.00	0.37	1.020	o	|	|	|	|	1.34
16.250	0.00	0.37	1.017	o	|	|	|	|	1.34
16.333	0.00	0.37	1.015	o	|	|	|	|	1.33
16.417	0.00	0.37	1.012	o	|	|	|	|	1.33
16.500	0.00	0.36	1.010	o	|	|	|	|	1.33
16.583	0.00	0.36	1.007	o	|	|	|	|	1.32
16.667	0.00	0.36	1.005	o	|	|	|	|	1.32
16.750	0.00	0.36	1.002	o	|	|	|	|	1.32
16.833	0.00	0.36	1.000	o	|	|	|	|	1.31
16.917	0.00	0.36	0.997	o	|	|	|	|	1.31
17.000	0.00	0.36	0.995	o	|	|	|	|	1.31
17.083	0.00	0.36	0.992	o	|	|	|	|	1.30
17.167	0.00	0.35	0.990	o	|	|	|	|	1.30
17.250	0.00	0.35	0.987	o	|	|	|	|	1.30
17.333	0.00	0.35	0.985	o	|	|	|	|	1.30
17.417	0.00	0.35	0.983	o	|	|	|	|	1.29
17.500	0.00	0.35	0.980	o	|	|	|	|	1.29
17.583	0.00	0.35	0.978	o	|	|	|	|	1.29
17.667	0.00	0.35	0.975	o	|	|	|	|	1.28
17.750	0.00	0.34	0.973	o	|	|	|	|	1.28
17.833	0.00	0.34	0.971	o	|	|	|	|	1.28
17.917	0.00	0.34	0.968	o	|	|	|	|	1.28
18.000	0.00	0.34	0.966	o	|	|	|	|	1.27
18.083	0.00	0.34	0.964	o	|	|	|	|	1.27
18.167	0.00	0.34	0.961	o	|	|	|	|	1.27
18.250	0.00	0.34	0.959	o	|	|	|	|	1.26
18.333	0.00	0.34	0.957	o	|	|	|	|	1.26
18.417	0.00	0.33	0.954	o	|	|	|	|	1.26
18.500	0.00	0.33	0.952	o	|	|	|	|	1.26
18.583	0.00	0.33	0.950	o	|	|	|	|	1.25
18.667	0.00	0.33	0.947	o	|	|	|	|	1.25
18.750	0.00	0.33	0.945	o	|	|	|	|	1.25
18.833	0.00	0.33	0.943	o	|	|	|	|	1.24
18.917	0.00	0.33	0.941	o	|	|	|	|	1.24
19.000	0.00	0.33	0.938	o	|	|	|	|	1.24
19.083	0.00	0.32	0.936	o	|	|	|	|	1.24
19.167	0.00	0.32	0.934	o	|	|	|	|	1.23
19.250	0.00	0.32	0.932	o	|	|	|	|	1.23
19.333	0.00	0.32	0.930	o	|	|	|	|	1.23
19.417	0.00	0.32	0.927	o	|	|	|	|	1.23
19.500	0.00	0.32	0.925	o	|	|	|	|	1.22
19.583	0.00	0.32	0.923	o	|	|	|	|	1.22
19.667	0.00	0.32	0.921	o	|	|	|	|	1.22
19.750	0.00	0.31	0.919	o	|	|	|	|	1.21
19.833	0.00	0.31	0.916	o	|	|	|	|	1.21
19.917	0.00	0.31	0.914	o	|	|	|	|	1.21
20.000	0.00	0.31	0.912	o	|	|	|	|	1.21
20.083	0.00	0.31	0.910	o	|	|	|	|	1.20
20.167	0.00	0.31	0.908	o	|	|	|	|	1.20
20.250	0.00	0.31	0.906	o	|	|	|	|	1.20
20.333	0.00	0.31	0.904	o	|	|	|	|	1.20
20.417	0.00	0.31	0.902	o	|	|	|	|	1.19
20.500	0.00	0.30	0.899	o	|	|	|	|	1.19
20.583	0.00	0.30	0.897	o	|	|	|	|	1.19
20.667	0.00	0.30	0.895	o	|	|	|	|	1.19
20.750	0.00	0.30	0.893	o	|	|	|	|	1.18
20.833	0.00	0.30	0.891	o	|	|	|	|	1.18
20.917	0.00	0.30	0.889	o	|	|	|	|	1.18
21.000	0.00	0.30	0.887	o	|	|	|	|	1.18
21.083	0.00	0.30	0.885	o	|	|	|	|	1.17
21.167	0.00	0.29	0.883	o	|	|	|	|	1.17
21.250	0.00	0.29	0.881	o	|	|	|	|	1.17
21.333	0.00	0.29	0.879	o	|	|	|	|	1.17
21.417	0.00	0.29	0.877	o	|	|	|	|	1.16
21.500	0.00	0.29	0.875	o	|	|	|	|	1.16
21.583	0.00	0.29	0.873	o	|	|	|	|	1.16
21.667	0.00	0.29	0.871	o	|	|	|	|	1.16
21.750	0.00	0.29	0.869	o	|	|	|	|	1.15
21.833	0.00	0.29	0.867	o	|	|	|	|	1.15
21.917	0.00	0.29	0.865	o	|	|	|	|	1.15
22.000	0.00	0.28	0.863	o	|	|	|	|	1.15
22.083	0.00	0.28	0.861	o	|	|	|	|	1.14
22.167	0.00	0.28	0.859	o	|	|	|	|	1.14
22.250	0.00	0.28	0.857	o	|	|	|	|	1.14
22.333	0.00	0.28	0.855	o	|	|	|	|	1.14
22.417	0.00	0.28	0.853	o	|	|	|	|	1.13
22.500	0.00	0.28	0.851	o	|	|	|	|	1.13
22.583	0.00	0.28	0.849	o	|	|	|	|	1.13
22.667	0.00	0.28	0.848	o	|	|	|	|	1.13
22.750	0.00	0.27	0.846	o	|	|	|	|	1.13
22.833	0.00	0.27	0.844	o	|	|	|	|	1.12
22.917	0.00	0.27	0.842	o	|	|	|	|	1.12
23.000	0.00	0.27	0.840	o	|	|	|	|	1.12
23.083	0.00	0.27	0.838	o	|	|	|	|	1.12
23.167	0.00	0.27	0.836	o	|	|	|	|	1.11
23.250	0.00	0.27	0.834	o	|	|	|	|	1.11

23.333	0.00	0.27	0.833	o	|	|	|	|	1.11
23.417	0.00	0.27	0.831	o	|	|	|	|	1.11
23.500	0.00	0.27	0.829	o	|	|	|	|	1.11
23.583	0.00	0.26	0.827	o	|	|	|	|	1.10
23.667	0.00	0.26	0.825	o	|	|	|	|	1.10
23.750	0.00	0.26	0.823	o	|	|	|	|	1.10
23.833	0.00	0.26	0.822	o	|	|	|	|	1.10
23.917	0.00	0.26	0.820	o	|	|	|	|	1.09
24.000	0.00	0.26	0.818	o	|	|	|	|	1.09
24.083	0.00	0.26	0.816	o	|	|	|	|	1.09
24.167	0.00	0.26	0.815	o	|	|	|	|	1.09
24.250	0.00	0.26	0.813	o	|	|	|	|	1.09
24.333	0.00	0.26	0.811	o	|	|	|	|	1.08
24.417	0.00	0.25	0.809	o	|	|	|	|	1.08
24.500	0.00	0.25	0.808	o	|	|	|	|	1.08
24.583	0.00	0.25	0.806	o	|	|	|	|	1.08
24.667	0.00	0.25	0.804	o	|	|	|	|	1.07
24.750	0.00	0.25	0.802	o	|	|	|	|	1.07
24.833	0.00	0.25	0.801	o	|	|	|	|	1.07
24.917	0.00	0.25	0.799	o	|	|	|	|	1.07
25.000	0.00	0.25	0.797	o	|	|	|	|	1.07
25.083	0.00	0.25	0.795	o	|	|	|	|	1.06
25.167	0.00	0.25	0.794	o	|	|	|	|	1.06
25.250	0.00	0.24	0.792	o	|	|	|	|	1.06
25.333	0.00	0.24	0.790	o	|	|	|	|	1.06
25.417	0.00	0.24	0.789	o	|	|	|	|	1.06
25.500	0.00	0.24	0.787	o	|	|	|	|	1.05
25.583	0.00	0.24	0.785	o	|	|	|	|	1.05
25.667	0.00	0.24	0.784	o	|	|	|	|	1.05
25.750	0.00	0.24	0.782	o	|	|	|	|	1.05
25.833	0.00	0.24	0.780	o	|	|	|	|	1.05
25.917	0.00	0.24	0.779	o	|	|	|	|	1.04
26.000	0.00	0.24	0.777	o	|	|	|	|	1.04
26.083	0.00	0.24	0.776	o	|	|	|	|	1.04
26.167	0.00	0.23	0.774	o	|	|	|	|	1.04
26.250	0.00	0.23	0.772	o	|	|	|	|	1.04
26.333	0.00	0.23	0.771	o	|	|	|	|	1.03
26.417	0.00	0.23	0.769	o	|	|	|	|	1.03
26.500	0.00	0.23	0.767	o	|	|	|	|	1.03
26.583	0.00	0.23	0.766	o	|	|	|	|	1.03
26.667	0.00	0.23	0.764	o	|	|	|	|	1.03
26.750	0.00	0.23	0.763	o	|	|	|	|	1.02
26.833	0.00	0.23	0.761	o	|	|	|	|	1.02
26.917	0.00	0.23	0.760	o	|	|	|	|	1.02
27.000	0.00	0.23	0.758	o	|	|	|	|	1.02
27.083	0.00	0.23	0.756	o	|	|	|	|	1.02
27.167	0.00	0.22	0.755	o	|	|	|	|	1.01
27.250	0.00	0.22	0.753	o	|	|	|	|	1.01
27.333	0.00	0.22	0.752	o	|	|	|	|	1.01
27.417	0.00	0.22	0.750	o	|	|	|	|	1.01
27.500	0.00	0.22	0.749	o	|	|	|	|	1.01
27.583	0.00	0.22	0.747	o	|	|	|	|	1.01
27.667	0.00	0.22	0.746	o	|	|	|	|	1.00
27.750	0.00	0.22	0.744	o	|	|	|	|	1.00
27.833	0.00	0.22	0.743	o	|	|	|	|	1.00
27.917	0.00	0.22	0.741	o	|	|	|	|	1.00
28.000	0.00	0.22	0.740	o	|	|	|	|	1.00
28.083	0.00	0.22	0.738	o	|	|	|	|	0.99
28.167	0.00	0.22	0.737	o	|	|	|	|	0.99
28.250	0.00	0.22	0.735	o	|	|	|	|	0.99
28.333	0.00	0.22	0.734	o	|	|	|	|	0.99
28.417	0.00	0.21	0.732	o	|	|	|	|	0.99
28.500	0.00	0.21	0.731	o	|	|	|	|	0.98
28.583	0.00	0.21	0.729	o	|	|	|	|	0.98
28.667	0.00	0.21	0.728	o	|	|	|	|	0.98
28.750	0.00	0.21	0.726	o	|	|	|	|	0.98
28.833	0.00	0.21	0.725	o	|	|	|	|	0.98
28.917	0.00	0.21	0.723	o	|	|	|	|	0.97
29.000	0.00	0.21	0.722	o	|	|	|	|	0.97
29.083	0.00	0.21	0.721	o	|	|	|	|	0.97
29.167	0.00	0.21	0.719	o	|	|	|	|	0.97
29.250	0.00	0.21	0.718	o	|	|	|	|	0.97
29.333	0.00	0.21	0.716	o	|	|	|	|	0.96
29.417	0.00	0.21	0.715	o	|	|	|	|	0.96
29.500	0.00	0.21	0.713	o	|	|	|	|	0.96
29.583	0.00	0.21	0.712	o	|	|	|	|	0.96
29.667	0.00	0.21	0.710	o	|	|	|	|	0.96
29.750	0.00	0.21	0.709	o	|	|	|	|	0.95
29.833	0.00	0.21	0.708	o	|	|	|	|	0.95
29.917	0.00	0.21	0.706	o	|	|	|	|	0.95
30.000	0.00	0.21	0.705	o	|	|	|	|	0.95
30.083	0.00	0.21	0.703	o	|	|	|	|	0.95
30.167	0.00	0.21	0.702	o	|	|	|	|	0.94
30.250	0.00	0.21	0.700	o	|	|	|	|	0.94
30.333	0.00	0.21	0.699	o	|	|	|	|	0.94
30.417	0.00	0.20	0.698	o	|	|	|	|	0.94

30.500	0.00	0.20	0.696	o	|	|	|	|	0.94
30.583	0.00	0.20	0.695	o	|	|	|	|	0.94
30.667	0.00	0.20	0.693	o	|	|	|	|	0.93
30.750	0.00	0.20	0.692	o	|	|	|	|	0.93
30.833	0.00	0.20	0.691	o	|	|	|	|	0.93
30.917	0.00	0.20	0.689	o	|	|	|	|	0.93
31.000	0.00	0.20	0.688	o	|	|	|	|	0.93
31.083	0.00	0.20	0.686	o	|	|	|	|	0.92
31.167	0.00	0.20	0.685	o	|	|	|	|	0.92
31.250	0.00	0.20	0.684	o	|	|	|	|	0.92
31.333	0.00	0.20	0.682	o	|	|	|	|	0.92
31.417	0.00	0.20	0.681	o	|	|	|	|	0.92
31.500	0.00	0.20	0.680	o	|	|	|	|	0.91
31.583	0.00	0.20	0.678	o	|	|	|	|	0.91
31.667	0.00	0.20	0.677	o	|	|	|	|	0.91
31.750	0.00	0.20	0.675	o	|	|	|	|	0.91
31.833	0.00	0.20	0.674	o	|	|	|	|	0.91
31.917	0.00	0.20	0.673	o	|	|	|	|	0.91
32.000	0.00	0.20	0.671	o	|	|	|	|	0.90
32.083	0.00	0.20	0.670	o	|	|	|	|	0.90
32.167	0.00	0.20	0.669	o	|	|	|	|	0.90
32.250	0.00	0.20	0.667	o	|	|	|	|	0.90
32.333	0.00	0.20	0.666	o	|	|	|	|	0.90
32.417	0.00	0.19	0.665	o	|	|	|	|	0.89
32.500	0.00	0.19	0.663	o	|	|	|	|	0.89
32.583	0.00	0.19	0.662	o	|	|	|	|	0.89
32.667	0.00	0.19	0.661	o	|	|	|	|	0.89
32.750	0.00	0.19	0.659	o	|	|	|	|	0.89
32.833	0.00	0.19	0.658	o	|	|	|	|	0.89
32.917	0.00	0.19	0.657	o	|	|	|	|	0.88
33.000	0.00	0.19	0.655	o	|	|	|	|	0.88
33.083	0.00	0.19	0.654	o	|	|	|	|	0.88
33.167	0.00	0.19	0.653	o	|	|	|	|	0.88
33.250	0.00	0.19	0.651	o	|	|	|	|	0.88
33.333	0.00	0.19	0.650	o	|	|	|	|	0.87
33.417	0.00	0.19	0.649	o	|	|	|	|	0.87
33.500	0.00	0.19	0.647	o	|	|	|	|	0.87
33.583	0.00	0.19	0.646	o	|	|	|	|	0.87
33.667	0.00	0.19	0.645	o	|	|	|	|	0.87
33.750	0.00	0.19	0.643	o	|	|	|	|	0.87
33.833	0.00	0.19	0.642	o	|	|	|	|	0.86
33.917	0.00	0.19	0.641	o	|	|	|	|	0.86
34.000	0.00	0.19	0.640	o	|	|	|	|	0.86
34.083	0.00	0.19	0.638	o	|	|	|	|	0.86
34.167	0.00	0.19	0.637	o	|	|	|	|	0.86
34.250	0.00	0.19	0.636	o	|	|	|	|	0.86
34.333	0.00	0.19	0.634	o	|	|	|	|	0.85
34.417	0.00	0.19	0.633	o	|	|	|	|	0.85
34.500	0.00	0.19	0.632	o	|	|	|	|	0.85
34.583	0.00	0.19	0.631	o	|	|	|	|	0.85
34.667	0.00	0.18	0.629	o	|	|	|	|	0.85
34.750	0.00	0.18	0.628	o	|	|	|	|	0.85
34.833	0.00	0.18	0.627	o	|	|	|	|	0.84
34.917	0.00	0.18	0.626	o	|	|	|	|	0.84
35.000	0.00	0.18	0.624	o	|	|	|	|	0.84
35.083	0.00	0.18	0.623	o	|	|	|	|	0.84
35.167	0.00	0.18	0.622	o	|	|	|	|	0.84
35.250	0.00	0.18	0.620	o	|	|	|	|	0.84
35.333	0.00	0.18	0.619	o	|	|	|	|	0.83
35.417	0.00	0.18	0.618	o	|	|	|	|	0.83
35.500	0.00	0.18	0.617	o	|	|	|	|	0.83
35.583	0.00	0.18	0.615	o	|	|	|	|	0.83
35.667	0.00	0.18	0.614	o	|	|	|	|	0.83
35.750	0.00	0.18	0.613	o	|	|	|	|	0.83
35.833	0.00	0.18	0.612	o	|	|	|	|	0.82
35.917	0.00	0.18	0.611	o	|	|	|	|	0.82
36.000	0.00	0.18	0.609	o	|	|	|	|	0.82
36.083	0.00	0.18	0.608	o	|	|	|	|	0.82
36.167	0.00	0.18	0.607	o	|	|	|	|	0.82
36.250	0.00	0.18	0.606	o	|	|	|	|	0.82
36.333	0.00	0.18	0.604	o	|	|	|	|	0.81
36.417	0.00	0.18	0.603	o	|	|	|	|	0.81
36.500	0.00	0.18	0.602	o	|	|	|	|	0.81
36.583	0.00	0.18	0.601	o	|	|	|	|	0.81
36.667	0.00	0.18	0.600	o	|	|	|	|	0.81
36.750	0.00	0.18	0.598	o	|	|	|	|	0.81
36.833	0.00	0.18	0.597	o	|	|	|	|	0.80
36.917	0.00	0.17	0.596	o	|	|	|	|	0.80
37.000	0.00	0.17	0.595	o	|	|	|	|	0.80
37.083	0.00	0.17	0.593	o	|	|	|	|	0.80
37.167	0.00	0.17	0.592	o	|	|	|	|	0.80
37.250	0.00	0.17	0.591	o	|	|	|	|	0.80
37.333	0.00	0.17	0.590	o	|	|	|	|	0.79
37.417	0.00	0.17	0.589	o	|	|	|	|	0.79
37.500	0.00	0.17	0.588	o	|	|	|	|	0.79
37.583	0.00	0.17	0.586	o	|	|	|	|	0.79

37.667	0.00	0.17	0.585	o	|	|	|	|	0.79
37.750	0.00	0.17	0.584	o	|	|	|	|	0.79
37.833	0.00	0.17	0.583	o	|	|	|	|	0.78
37.917	0.00	0.17	0.582	o	|	|	|	|	0.78
38.000	0.00	0.17	0.580	o	|	|	|	|	0.78
38.083	0.00	0.17	0.579	o	|	|	|	|	0.78
38.167	0.00	0.17	0.578	o	|	|	|	|	0.78
38.250	0.00	0.17	0.577	o	|	|	|	|	0.78
38.333	0.00	0.17	0.576	o	|	|	|	|	0.77
38.417	0.00	0.17	0.575	o	|	|	|	|	0.77
38.500	0.00	0.17	0.573	o	|	|	|	|	0.77
38.583	0.00	0.17	0.572	o	|	|	|	|	0.77
38.667	0.00	0.17	0.571	o	|	|	|	|	0.77
38.750	0.00	0.17	0.570	o	|	|	|	|	0.77
38.833	0.00	0.17	0.569	o	|	|	|	|	0.77
38.917	0.00	0.17	0.568	o	|	|	|	|	0.76
39.000	0.00	0.17	0.567	o	|	|	|	|	0.76
39.083	0.00	0.17	0.565	o	|	|	|	|	0.76
39.167	0.00	0.17	0.564	o	|	|	|	|	0.76
39.250	0.00	0.17	0.563	o	|	|	|	|	0.76
39.333	0.00	0.16	0.562	o	|	|	|	|	0.76
39.417	0.00	0.16	0.561	o	|	|	|	|	0.75
39.500	0.00	0.16	0.560	o	|	|	|	|	0.75
39.583	0.00	0.16	0.559	o	|	|	|	|	0.75
39.667	0.00	0.16	0.557	o	|	|	|	|	0.75
39.750	0.00	0.16	0.556	o	|	|	|	|	0.75
39.833	0.00	0.16	0.555	o	|	|	|	|	0.75
39.917	0.00	0.16	0.554	o	|	|	|	|	0.75
40.000	0.00	0.16	0.553	o	|	|	|	|	0.74
40.083	0.00	0.16	0.552	o	|	|	|	|	0.74
40.167	0.00	0.16	0.551	o	|	|	|	|	0.74
40.250	0.00	0.16	0.550	o	|	|	|	|	0.74
40.333	0.00	0.16	0.549	o	|	|	|	|	0.74
40.417	0.00	0.16	0.547	o	|	|	|	|	0.74
40.500	0.00	0.16	0.546	o	|	|	|	|	0.74
40.583	0.00	0.16	0.545	o	|	|	|	|	0.73
40.667	0.00	0.16	0.544	o	|	|	|	|	0.73
40.750	0.00	0.16	0.543	o	|	|	|	|	0.73
40.833	0.00	0.16	0.542	o	|	|	|	|	0.73
40.917	0.00	0.16	0.541	o	|	|	|	|	0.73
41.000	0.00	0.16	0.540	o	|	|	|	|	0.73
41.083	0.00	0.16	0.539	o	|	|	|	|	0.72
41.167	0.00	0.16	0.538	o	|	|	|	|	0.72
41.250	0.00	0.16	0.536	o	|	|	|	|	0.72
41.333	0.00	0.16	0.535	o	|	|	|	|	0.72
41.417	0.00	0.16	0.534	o	|	|	|	|	0.72
41.500	0.00	0.16	0.533	o	|	|	|	|	0.72
41.583	0.00	0.16	0.532	o	|	|	|	|	0.72
41.667	0.00	0.16	0.531	o	|	|	|	|	0.71
41.750	0.00	0.16	0.530	o	|	|	|	|	0.71
41.833	0.00	0.16	0.529	o	|	|	|	|	0.71
41.917	0.00	0.15	0.528	o	|	|	|	|	0.71
42.000	0.00	0.15	0.527	o	|	|	|	|	0.71
42.083	0.00	0.15	0.526	o	|	|	|	|	0.71
42.167	0.00	0.15	0.525	o	|	|	|	|	0.71
42.250	0.00	0.15	0.524	o	|	|	|	|	0.70
42.333	0.00	0.15	0.523	o	|	|	|	|	0.70
42.417	0.00	0.15	0.521	o	|	|	|	|	0.70
42.500	0.00	0.15	0.520	o	|	|	|	|	0.70
42.583	0.00	0.15	0.519	o	|	|	|	|	0.70
42.667	0.00	0.15	0.518	o	|	|	|	|	0.70
42.750	0.00	0.15	0.517	o	|	|	|	|	0.70
42.833	0.00	0.15	0.516	o	|	|	|	|	0.69
42.917	0.00	0.15	0.515	o	|	|	|	|	0.69
43.000	0.00	0.15	0.514	o	|	|	|	|	0.69
43.083	0.00	0.15	0.513	o	|	|	|	|	0.69
43.167	0.00	0.15	0.512	o	|	|	|	|	0.69
43.250	0.00	0.15	0.511	o	|	|	|	|	0.69
43.333	0.00	0.15	0.510	o	|	|	|	|	0.69
43.417	0.00	0.15	0.509	o	|	|	|	|	0.69
43.500	0.00	0.15	0.508	o	|	|	|	|	0.68
43.583	0.00	0.15	0.507	o	|	|	|	|	0.68
43.667	0.00	0.15	0.506	o	|	|	|	|	0.68
43.750	0.00	0.15	0.505	o	|	|	|	|	0.68
43.833	0.00	0.15	0.504	o	|	|	|	|	0.68
43.917	0.00	0.15	0.503	o	|	|	|	|	0.68
44.000	0.00	0.15	0.502	o	|	|	|	|	0.68
44.083	0.00	0.15	0.501	o	|	|	|	|	0.67
44.167	0.00	0.15	0.500	o	|	|	|	|	0.67
44.250	0.00	0.15	0.499	o	|	|	|	|	0.67
44.333	0.00	0.15	0.498	o	|	|	|	|	0.67
44.417	0.00	0.15	0.497	o	|	|	|	|	0.67
44.500	0.00	0.15	0.496	o	|	|	|	|	0.67
44.583	0.00	0.15	0.495	o	|	|	|	|	0.67
44.667	0.00	0.14	0.494	o	|	|	|	|	0.66
44.750	0.00	0.14	0.493	o	|	|	|	|	0.66

44.833	0.00	0.14	0.492	o	|	|	|	|	0.66
44.917	0.00	0.14	0.491	o	|	|	|	|	0.66
45.000	0.00	0.14	0.490	o	|	|	|	|	0.66
45.083	0.00	0.14	0.489	o	|	|	|	|	0.66
45.167	0.00	0.14	0.488	o	|	|	|	|	0.66
45.250	0.00	0.14	0.487	o	|	|	|	|	0.66
45.333	0.00	0.14	0.486	o	|	|	|	|	0.65
45.417	0.00	0.14	0.485	o	|	|	|	|	0.65
45.500	0.00	0.14	0.484	o	|	|	|	|	0.65
45.583	0.00	0.14	0.483	o	|	|	|	|	0.65
45.667	0.00	0.14	0.482	o	|	|	|	|	0.65
45.750	0.00	0.14	0.481	o	|	|	|	|	0.65
45.833	0.00	0.14	0.480	o	|	|	|	|	0.65
45.917	0.00	0.14	0.479	o	|	|	|	|	0.64
46.000	0.00	0.14	0.478	o	|	|	|	|	0.64
46.083	0.00	0.14	0.477	o	|	|	|	|	0.64
46.167	0.00	0.14	0.476	o	|	|	|	|	0.64
46.250	0.00	0.14	0.475	o	|	|	|	|	0.64
46.333	0.00	0.14	0.474	o	|	|	|	|	0.64
46.417	0.00	0.14	0.473	o	|	|	|	|	0.64
46.500	0.00	0.14	0.472	o	|	|	|	|	0.64
46.583	0.00	0.14	0.471	o	|	|	|	|	0.63
46.667	0.00	0.14	0.470	o	|	|	|	|	0.63
46.750	0.00	0.14	0.469	o	|	|	|	|	0.63
46.833	0.00	0.14	0.469	o	|	|	|	|	0.63
46.917	0.00	0.14	0.468	o	|	|	|	|	0.63
47.000	0.00	0.14	0.467	o	|	|	|	|	0.63
47.083	0.00	0.14	0.466	o	|	|	|	|	0.63
47.167	0.00	0.14	0.465	o	|	|	|	|	0.63
47.250	0.00	0.14	0.464	o	|	|	|	|	0.62
47.333	0.00	0.14	0.463	o	|	|	|	|	0.62
47.417	0.00	0.14	0.462	o	|	|	|	|	0.62
47.500	0.00	0.14	0.461	o	|	|	|	|	0.62
47.583	0.00	0.13	0.460	o	|	|	|	|	0.62
47.667	0.00	0.13	0.459	o	|	|	|	|	0.62
47.750	0.00	0.13	0.458	o	|	|	|	|	0.62
47.833	0.00	0.13	0.457	o	|	|	|	|	0.62
47.917	0.00	0.13	0.456	o	|	|	|	|	0.61
48.000	0.00	0.13	0.455	o	|	|	|	|	0.61
48.083	0.00	0.13	0.455	o	|	|	|	|	0.61
48.167	0.00	0.13	0.454	o	|	|	|	|	0.61
48.250	0.00	0.13	0.453	o	|	|	|	|	0.61
48.333	0.00	0.13	0.452	o	|	|	|	|	0.61
48.417	0.00	0.13	0.451	o	|	|	|	|	0.61
48.500	0.00	0.13	0.450	o	|	|	|	|	0.61
48.583	0.00	0.13	0.449	o	|	|	|	|	0.60
48.667	0.00	0.13	0.448	o	|	|	|	|	0.60
48.750	0.00	0.13	0.447	o	|	|	|	|	0.60
48.833	0.00	0.13	0.446	o	|	|	|	|	0.60
48.917	0.00	0.13	0.445	o	|	|	|	|	0.60
49.000	0.00	0.13	0.445	o	|	|	|	|	0.60
49.083	0.00	0.13	0.444	o	|	|	|	|	0.60
49.167	0.00	0.13	0.443	o	|	|	|	|	0.60
49.250	0.00	0.13	0.442	o	|	|	|	|	0.59
49.333	0.00	0.13	0.441	o	|	|	|	|	0.59
49.417	0.00	0.13	0.440	o	|	|	|	|	0.59
49.500	0.00	0.13	0.439	o	|	|	|	|	0.59
49.583	0.00	0.13	0.438	o	|	|	|	|	0.59
49.667	0.00	0.13	0.437	o	|	|	|	|	0.59
49.750	0.00	0.13	0.437	o	|	|	|	|	0.59
49.833	0.00	0.13	0.436	o	|	|	|	|	0.59
49.917	0.00	0.13	0.435	o	|	|	|	|	0.59
50.000	0.00	0.13	0.434	o	|	|	|	|	0.58
50.083	0.00	0.13	0.433	o	|	|	|	|	0.58
50.167	0.00	0.13	0.432	o	|	|	|	|	0.58
50.250	0.00	0.13	0.431	o	|	|	|	|	0.58
50.333	0.00	0.13	0.430	o	|	|	|	|	0.58
50.417	0.00	0.13	0.430	o	|	|	|	|	0.58
50.500	0.00	0.13	0.429	o	|	|	|	|	0.58
50.583	0.00	0.13	0.428	o	|	|	|	|	0.58
50.667	0.00	0.13	0.427	o	|	|	|	|	0.57
50.750	0.00	0.13	0.426	o	|	|	|	|	0.57
50.833	0.00	0.12	0.425	o	|	|	|	|	0.57
50.917	0.00	0.12	0.424	o	|	|	|	|	0.57
51.000	0.00	0.12	0.424	o	|	|	|	|	0.57
51.083	0.00	0.12	0.423	o	|	|	|	|	0.57
51.167	0.00	0.12	0.422	o	|	|	|	|	0.57
51.250	0.00	0.12	0.421	o	|	|	|	|	0.57
51.333	0.00	0.12	0.420	o	|	|	|	|	0.57
51.417	0.00	0.12	0.419	o	|	|	|	|	0.56
51.500	0.00	0.12	0.418	o	|	|	|	|	0.56
51.583	0.00	0.12	0.418	o	|	|	|	|	0.56
51.667	0.00	0.12	0.417	o	|	|	|	|	0.56
51.750	0.00	0.12	0.416	o	|	|	|	|	0.56
51.833	0.00	0.12	0.415	o	|	|	|	|	0.56
51.917	0.00	0.12	0.414	o	|	|	|	|	0.56

52.000	0.00	0.12	0.413	o	|	|	|	|	0.56
52.083	0.00	0.12	0.413	o	|	|	|	|	0.56
52.167	0.00	0.12	0.412	o	|	|	|	|	0.55
52.250	0.00	0.12	0.411	o	|	|	|	|	0.55
52.333	0.00	0.12	0.410	o	|	|	|	|	0.55
52.417	0.00	0.12	0.409	o	|	|	|	|	0.55
52.500	0.00	0.12	0.408	o	|	|	|	|	0.55
52.583	0.00	0.12	0.408	o	|	|	|	|	0.55
52.667	0.00	0.12	0.407	o	|	|	|	|	0.55
52.750	0.00	0.12	0.406	o	|	|	|	|	0.55
52.833	0.00	0.12	0.405	o	|	|	|	|	0.55
52.917	0.00	0.12	0.404	o	|	|	|	|	0.54
53.000	0.00	0.12	0.403	o	|	|	|	|	0.54
53.083	0.00	0.12	0.403	o	|	|	|	|	0.54
53.167	0.00	0.12	0.402	o	|	|	|	|	0.54
53.250	0.00	0.12	0.401	o	|	|	|	|	0.54
53.333	0.00	0.12	0.400	o	|	|	|	|	0.54
53.417	0.00	0.12	0.399	o	|	|	|	|	0.54
53.500	0.00	0.12	0.399	o	|	|	|	|	0.54
53.583	0.00	0.12	0.398	o	|	|	|	|	0.54
53.667	0.00	0.12	0.397	o	|	|	|	|	0.53
53.750	0.00	0.12	0.396	o	|	|	|	|	0.53
53.833	0.00	0.12	0.395	o	|	|	|	|	0.53
53.917	0.00	0.12	0.395	o	|	|	|	|	0.53
54.000	0.00	0.12	0.394	o	|	|	|	|	0.53
54.083	0.00	0.12	0.393	o	|	|	|	|	0.53
54.167	0.00	0.12	0.392	o	|	|	|	|	0.53
54.250	0.00	0.11	0.391	o	|	|	|	|	0.53
54.333	0.00	0.11	0.391	o	|	|	|	|	0.53
54.417	0.00	0.11	0.390	o	|	|	|	|	0.52
54.500	0.00	0.11	0.389	o	|	|	|	|	0.52
54.583	0.00	0.11	0.388	o	|	|	|	|	0.52
54.667	0.00	0.11	0.387	o	|	|	|	|	0.52
54.750	0.00	0.11	0.387	o	|	|	|	|	0.52
54.833	0.00	0.11	0.386	o	|	|	|	|	0.52
54.917	0.00	0.11	0.385	o	|	|	|	|	0.52
55.000	0.00	0.11	0.384	o	|	|	|	|	0.52
55.083	0.00	0.11	0.384	o	|	|	|	|	0.52
55.167	0.00	0.11	0.383	o	|	|	|	|	0.52
55.250	0.00	0.11	0.382	o	|	|	|	|	0.51
55.333	0.00	0.11	0.381	o	|	|	|	|	0.51
55.417	0.00	0.11	0.380	o	|	|	|	|	0.51
55.500	0.00	0.11	0.380	o	|	|	|	|	0.51
55.583	0.00	0.11	0.379	o	|	|	|	|	0.51
55.667	0.00	0.11	0.378	o	|	|	|	|	0.51
55.750	0.00	0.11	0.377	o	|	|	|	|	0.51
55.833	0.00	0.11	0.377	o	|	|	|	|	0.51
55.917	0.00	0.11	0.376	o	|	|	|	|	0.51
56.000	0.00	0.11	0.375	o	|	|	|	|	0.50
56.083	0.00	0.11	0.374	o	|	|	|	|	0.50
56.167	0.00	0.11	0.374	o	|	|	|	|	0.50
56.250	0.00	0.11	0.373	o	|	|	|	|	0.50
56.333	0.00	0.11	0.372	o	|	|	|	|	0.50
56.417	0.00	0.11	0.371	o	|	|	|	|	0.50
56.500	0.00	0.11	0.371	o	|	|	|	|	0.50
56.583	0.00	0.11	0.370	o	|	|	|	|	0.50
56.667	0.00	0.11	0.369	o	|	|	|	|	0.50
56.750	0.00	0.11	0.368	o	|	|	|	|	0.50
56.833	0.00	0.11	0.368	o	|	|	|	|	0.49
56.917	0.00	0.11	0.367	o	|	|	|	|	0.49
57.000	0.00	0.11	0.366	o	|	|	|	|	0.49
57.083	0.00	0.11	0.365	o	|	|	|	|	0.49
57.167	0.00	0.11	0.365	o	|	|	|	|	0.49
57.250	0.00	0.11	0.364	o	|	|	|	|	0.49
57.333	0.00	0.11	0.363	o	|	|	|	|	0.49
57.417	0.00	0.11	0.362	o	|	|	|	|	0.49
57.500	0.00	0.11	0.362	o	|	|	|	|	0.49
57.583	0.00	0.11	0.361	o	|	|	|	|	0.49
57.667	0.00	0.11	0.360	o	|	|	|	|	0.48
57.750	0.00	0.11	0.360	o	|	|	|	|	0.48
57.833	0.00	0.11	0.359	o	|	|	|	|	0.48
57.917	0.00	0.11	0.358	o	|	|	|	|	0.48
58.000	0.00	0.10	0.357	o	|	|	|	|	0.48
58.083	0.00	0.10	0.357	o	|	|	|	|	0.48
58.167	0.00	0.10	0.356	o	|	|	|	|	0.48
58.250	0.00	0.10	0.355	o	|	|	|	|	0.48
58.333	0.00	0.10	0.355	o	|	|	|	|	0.48
58.417	0.00	0.10	0.354	o	|	|	|	|	0.48
58.500	0.00	0.10	0.353	o	|	|	|	|	0.48
58.583	0.00	0.10	0.352	o	|	|	|	|	0.47
58.667	0.00	0.10	0.352	o	|	|	|	|	0.47
58.750	0.00	0.10	0.351	o	|	|	|	|	0.47
58.833	0.00	0.10	0.350	o	|	|	|	|	0.47
58.917	0.00	0.10	0.350	o	|	|	|	|	0.47
59.000	0.00	0.10	0.349	o	|	|	|	|	0.47
59.083	0.00	0.10	0.348	o	|	|	|	|	0.47

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59.167    0.00    0.10      0.347  o       |       |       |       |     0.47
59.250    0.00    0.10      0.347  o       |       |       |       |     0.47
59.333    0.00    0.10      0.346  o       |       |       |       |     0.47
59.417    0.00    0.10      0.345  o       |       |       |       |     0.46
59.500    0.00    0.10      0.345  o       |       |       |       |     0.46
59.583    0.00    0.10      0.344  o       |       |       |       |     0.46
59.667    0.00    0.10      0.343  o       |       |       |       |     0.46
59.750    0.00    0.10      0.343  o       |       |       |       |     0.46
59.833    0.00    0.10      0.342  o       |       |       |       |     0.46
59.917    0.00    0.10      0.341  o       |       |       |       |     0.46
60.000    0.00    0.10      0.340  o       |       |       |       |     0.46

       Remaining water in basin =    0.34 (Ac.Ft)

       ****************************HYDROGRAPH DATA****************************
                     Number of intervals =   720
                     Time interval =    5.0 (Min.)
                     Maximum/Peak flow rate =        0.770 (CFS)
                     Total volume =       1.364 (Ac.Ft)
              Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
       ***********************************************************************

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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro110310.rte
**********HYDROGRAPH DATA**********
Number of intervals = 41
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 28.574 (CFS)
Total volume = 2.456 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 41
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 7.1 14.29 21.43 28.57	Depth (Ft.)
0.083	1.20	0.00	0.004	OI	0.01
0.167	2.95	0.01	0.018	O I	0.02
0.250	3.10	0.01	0.039	O I	0.05
0.333	3.43	0.02	0.062	O I	0.08
0.417	4.22	0.03	0.088	O I	0.12
0.500	4.83	0.03	0.119	O I	0.16
0.583	5.08	0.04	0.153	O I	0.21
0.667	5.07	0.05	0.187	O I	0.25
0.750	5.61	0.07	0.224	O I	0.30
0.833	5.31	0.08	0.261	O I	0.35
0.917	4.90	0.09	0.295	O I	0.40
1.000	5.24	0.10	0.330	O I	0.44
1.083	6.18	0.11	0.368	O I	0.50
1.167	7.06	0.12	0.413	O I	0.56
1.250	7.28	0.14	0.462	O I	0.62
1.333	7.12	0.15	0.510	O I	0.69
1.417	7.60	0.16	0.560	O I	0.75
1.500	8.85	0.18	0.615	O I	0.83
1.583	8.88	0.20	0.675	O I	0.91
1.667	8.85	0.22	0.735	O I	0.99
1.750	10.18	0.25	0.798	O I	1.07

1.833	11.23	0.29	0.870	O	| I |	|	|	|	1.16
1.917	10.88	0.33	0.944	O	| I |	|	|	|	1.25
2.000	10.66	0.37	1.016	O	| I |	|	|	|	1.33
2.083	10.94	0.41	1.088	O	| I |	|	|	|	1.42
2.167	12.65	0.45	1.166	O	| I |	|	|	|	1.52
2.250	15.95	0.50	1.261	O	| |I |	|	|	1.63
2.333	16.04	0.56	1.368	O	| |I |	|	|	1.76
2.417	18.18	0.62	1.482	O	| | I |	|	|	1.90
2.500	24.96	0.73	1.625	O	| | | I |	|	2.07
2.583	28.57	0.90	1.804	|O	| | | | I	2.27
2.667	28.05	1.08	1.992	|O	| | | I|	2.48
2.750	19.01	1.22	2.146	|O	| | I | |	2.65
2.833	10.37	1.31	2.239	|O	| I | | |	2.76
2.917	7.77	1.36	2.292	|O	I | | | |	2.82
3.000	5.19	1.40	2.327	|O I | | | |	2.86
3.083	2.04	1.41	2.343	|OI | | | |	2.87
3.167	0.68	1.41	2.342	IO | | | |	2.87
3.250	0.29	1.40	2.336	IO | | | |	2.87
3.333	0.12	1.40	2.328	IO | | | |	2.86
3.417	0.02	1.39	2.319	IO | | | |	2.85
3.500	0.00	1.38	2.309	IO | | | |	2.84
3.583	0.00	1.37	2.300	IO | | | |	2.83
3.667	0.00	1.36	2.290	IO | | | |	2.81
3.750	0.00	1.35	2.281	IO | | | |	2.80
3.833	0.00	1.34	2.272	IO | | | |	2.79
3.917	0.00	1.33	2.262	IO | | | |	2.78
4.000	0.00	1.33	2.253	IO | | | |	2.77
4.083	0.00	1.32	2.244	IO | | | |	2.76
4.167	0.00	1.31	2.235	IO | | | |	2.75
4.250	0.00	1.30	2.226	IO | | | |	2.74
4.333	0.00	1.29	2.217	IO | | | |	2.73
4.417	0.00	1.28	2.208	IO | | | |	2.72
4.500	0.00	1.27	2.199	IO | | | |	2.71
4.583	0.00	1.27	2.191	IO | | | |	2.70
4.667	0.00	1.26	2.182	IO | | | |	2.69
4.750	0.00	1.25	2.173	IO | | | |	2.68
4.833	0.00	1.24	2.165	IO | | | |	2.67
4.917	0.00	1.23	2.156	IO | | | |	2.67
5.000	0.00	1.23	2.148	IO | | | |	2.66
5.083	0.00	1.22	2.139	IO | | | |	2.65
5.167	0.00	1.21	2.131	IO | | | |	2.64
5.250	0.00	1.20	2.123	IO | | | |	2.63
5.333	0.00	1.19	2.115	IO | | | |	2.62
5.417	0.00	1.19	2.106	IO | | | |	2.61
5.500	0.00	1.18	2.098	IO | | | |	2.60
5.583	0.00	1.17	2.090	IO | | | |	2.59
5.667	0.00	1.16	2.082	IO | | | |	2.58
5.750	0.00	1.16	2.074	IO | | | |	2.57
5.833	0.00	1.15	2.066	IO | | | |	2.56
5.917	0.00	1.14	2.058	IO | | | |	2.56
6.000	0.00	1.13	2.050	IO | | | |	2.55
6.083	0.00	1.13	2.043	IO | | | |	2.54
6.167	0.00	1.12	2.035	IO | | | |	2.53
6.250	0.00	1.11	2.027	IO | | | |	2.52
6.333	0.00	1.10	2.020	IO | | | |	2.51
6.417	0.00	1.10	2.012	IO | | | |	2.50
6.500	0.00	1.09	2.005	IO | | | |	2.50
6.583	0.00	1.08	1.997	IO | | | |	2.49
6.667	0.00	1.08	1.990	IO | | | |	2.48
6.750	0.00	1.07	1.982	IO | | | |	2.47
6.833	0.00	1.06	1.975	IO | | | |	2.46
6.917	0.00	1.05	1.968	IO | | | |	2.45
7.000	0.00	1.05	1.960	IO | | | |	2.45
7.083	0.00	1.04	1.953	IO | | | |	2.44
7.167	0.00	1.03	1.946	IO | | | |	2.43
7.250	0.00	1.03	1.939	IO | | | |	2.42
7.333	0.00	1.02	1.932	IO | | | |	2.41
7.417	0.00	1.01	1.925	IO | | | |	2.41
7.500	0.00	1.01	1.918	IO | | | |	2.40
7.583	0.00	1.00	1.911	IO | | | |	2.39
7.667	0.00	0.99	1.904	IO | | | |	2.38
7.750	0.00	0.99	1.897	IO | | | |	2.38
7.833	0.00	0.98	1.891	IO | | | |	2.37
7.917	0.00	0.97	1.884	IO | | | |	2.36
8.000	0.00	0.97	1.877	IO | | | |	2.35
8.083	0.00	0.96	1.871	IO | | | |	2.35
8.167	0.00	0.96	1.864	IO | | | |	2.34
8.250	0.00	0.95	1.857	IO | | | |	2.33
8.333	0.00	0.94	1.851	IO | | | |	2.32
8.417	0.00	0.94	1.844	IO | | | |	2.32
8.500	0.00	0.93	1.838	IO | | | |	2.31
8.583	0.00	0.92	1.832	IO | | | |	2.30
8.667	0.00	0.92	1.825	IO | | | |	2.30
8.750	0.00	0.91	1.819	IO | | | |	2.29
8.833	0.00	0.91	1.813	IO | | | |	2.28
8.917	0.00	0.90	1.806	IO | | | |	2.27

9.000	0.00	0.90	1.800	IO	|	|	|	2.27
9.083	0.00	0.89	1.794	O	|	|	|	2.26
9.167	0.00	0.88	1.788	O	|	|	|	2.25
9.250	0.00	0.88	1.782	O	|	|	|	2.25
9.333	0.00	0.87	1.776	O	|	|	|	2.24
9.417	0.00	0.87	1.770	O	|	|	|	2.23
9.500	0.00	0.86	1.764	O	|	|	|	2.23
9.583	0.00	0.86	1.758	O	|	|	|	2.22
9.667	0.00	0.85	1.752	O	|	|	|	2.21
9.750	0.00	0.84	1.746	O	|	|	|	2.21
9.833	0.00	0.84	1.741	O	|	|	|	2.20
9.917	0.00	0.83	1.735	O	|	|	|	2.19
10.000	0.00	0.83	1.729	O	|	|	|	2.19
10.083	0.00	0.82	1.723	O	|	|	|	2.18
10.167	0.00	0.82	1.718	O	|	|	|	2.18
10.250	0.00	0.81	1.712	O	|	|	|	2.17
10.333	0.00	0.81	1.707	O	|	|	|	2.16
10.417	0.00	0.80	1.701	O	|	|	|	2.16
10.500	0.00	0.80	1.696	O	|	|	|	2.15
10.583	0.00	0.79	1.690	O	|	|	|	2.14
10.667	0.00	0.79	1.685	O	|	|	|	2.14
10.750	0.00	0.78	1.679	O	|	|	|	2.13
10.833	0.00	0.78	1.674	O	|	|	|	2.13
10.917	0.00	0.77	1.669	O	|	|	|	2.12
11.000	0.00	0.77	1.663	O	|	|	|	2.11
11.083	0.00	0.76	1.658	O	|	|	|	2.11
11.167	0.00	0.76	1.653	O	|	|	|	2.10
11.250	0.00	0.75	1.648	O	|	|	|	2.10
11.333	0.00	0.75	1.642	O	|	|	|	2.09
11.417	0.00	0.74	1.637	O	|	|	|	2.09
11.500	0.00	0.74	1.632	O	|	|	|	2.08
11.583	0.00	0.73	1.627	O	|	|	|	2.07
11.667	0.00	0.73	1.622	O	|	|	|	2.07
11.750	0.00	0.72	1.617	O	|	|	|	2.06
11.833	0.00	0.72	1.612	O	|	|	|	2.06
11.917	0.00	0.71	1.607	O	|	|	|	2.05
12.000	0.00	0.71	1.602	O	|	|	|	2.05
12.083	0.00	0.70	1.598	O	|	|	|	2.04
12.167	0.00	0.70	1.593	O	|	|	|	2.04
12.250	0.00	0.69	1.588	O	|	|	|	2.03
12.333	0.00	0.69	1.583	O	|	|	|	2.02
12.417	0.00	0.68	1.578	O	|	|	|	2.02
12.500	0.00	0.68	1.574	O	|	|	|	2.01
12.583	0.00	0.68	1.569	O	|	|	|	2.01
12.667	0.00	0.67	1.564	O	|	|	|	2.00
12.750	0.00	0.67	1.560	O	|	|	|	2.00
12.833	0.00	0.66	1.555	O	|	|	|	1.99
12.917	0.00	0.66	1.551	O	|	|	|	1.99
13.000	0.00	0.66	1.546	O	|	|	|	1.98
13.083	0.00	0.66	1.542	O	|	|	|	1.98
13.167	0.00	0.65	1.537	O	|	|	|	1.97
13.250	0.00	0.65	1.533	O	|	|	|	1.97
13.333	0.00	0.65	1.528	O	|	|	|	1.96
13.417	0.00	0.65	1.524	O	|	|	|	1.95
13.500	0.00	0.65	1.519	O	|	|	|	1.95
13.583	0.00	0.64	1.515	O	|	|	|	1.94
13.667	0.00	0.64	1.510	O	|	|	|	1.94
13.750	0.00	0.64	1.506	O	|	|	|	1.93
13.833	0.00	0.64	1.502	O	|	|	|	1.93
13.917	0.00	0.63	1.497	O	|	|	|	1.92
14.000	0.00	0.63	1.493	O	|	|	|	1.92
14.083	0.00	0.63	1.489	O	|	|	|	1.91
14.167	0.00	0.63	1.484	O	|	|	|	1.91
14.250	0.00	0.62	1.480	O	|	|	|	1.90
14.333	0.00	0.62	1.476	O	|	|	|	1.90
14.417	0.00	0.62	1.471	O	|	|	|	1.89
14.500	0.00	0.62	1.467	O	|	|	|	1.89
14.583	0.00	0.61	1.463	O	|	|	|	1.88
14.667	0.00	0.61	1.459	O	|	|	|	1.87
14.750	0.00	0.61	1.454	O	|	|	|	1.87
14.833	0.00	0.61	1.450	O	|	|	|	1.86
14.917	0.00	0.60	1.446	O	|	|	|	1.86
15.000	0.00	0.60	1.442	O	|	|	|	1.85
15.083	0.00	0.60	1.438	O	|	|	|	1.85
15.167	0.00	0.60	1.434	O	|	|	|	1.84
15.250	0.00	0.60	1.430	O	|	|	|	1.84
15.333	0.00	0.59	1.425	O	|	|	|	1.83
15.417	0.00	0.59	1.421	O	|	|	|	1.83
15.500	0.00	0.59	1.417	O	|	|	|	1.82
15.583	0.00	0.59	1.413	O	|	|	|	1.82
15.667	0.00	0.58	1.409	O	|	|	|	1.81
15.750	0.00	0.58	1.405	O	|	|	|	1.81
15.833	0.00	0.58	1.401	O	|	|	|	1.80
15.917	0.00	0.58	1.397	O	|	|	|	1.80
16.000	0.00	0.58	1.393	O	|	|	|	1.79
16.083	0.00	0.57	1.389	O	|	|	|	1.79

16.167	0.00	0.57	1.385	o	|	|	|	|	1.79
16.250	0.00	0.57	1.381	o	|	|	|	|	1.78
16.333	0.00	0.57	1.377	o	|	|	|	|	1.78
16.417	0.00	0.56	1.374	o	|	|	|	|	1.77
16.500	0.00	0.56	1.370	o	|	|	|	|	1.77
16.583	0.00	0.56	1.366	o	|	|	|	|	1.76
16.667	0.00	0.56	1.362	o	|	|	|	|	1.76
16.750	0.00	0.56	1.358	o	|	|	|	|	1.75
16.833	0.00	0.55	1.354	o	|	|	|	|	1.75
16.917	0.00	0.55	1.351	o	|	|	|	|	1.74
17.000	0.00	0.55	1.347	o	|	|	|	|	1.74
17.083	0.00	0.55	1.343	o	|	|	|	|	1.73
17.167	0.00	0.55	1.339	o	|	|	|	|	1.73
17.250	0.00	0.54	1.335	o	|	|	|	|	1.72
17.333	0.00	0.54	1.332	o	|	|	|	|	1.72
17.417	0.00	0.54	1.328	o	|	|	|	|	1.72
17.500	0.00	0.54	1.324	o	|	|	|	|	1.71
17.583	0.00	0.54	1.321	o	|	|	|	|	1.71
17.667	0.00	0.53	1.317	o	|	|	|	|	1.70
17.750	0.00	0.53	1.313	o	|	|	|	|	1.70
17.833	0.00	0.53	1.310	o	|	|	|	|	1.69
17.917	0.00	0.53	1.306	o	|	|	|	|	1.69
18.000	0.00	0.53	1.302	o	|	|	|	|	1.68
18.083	0.00	0.52	1.299	o	|	|	|	|	1.68
18.167	0.00	0.52	1.295	o	|	|	|	|	1.67
18.250	0.00	0.52	1.291	o	|	|	|	|	1.67
18.333	0.00	0.52	1.288	o	|	|	|	|	1.67
18.417	0.00	0.52	1.284	o	|	|	|	|	1.66
18.500	0.00	0.51	1.281	o	|	|	|	|	1.66
18.583	0.00	0.51	1.277	o	|	|	|	|	1.65
18.667	0.00	0.51	1.274	o	|	|	|	|	1.65
18.750	0.00	0.51	1.270	o	|	|	|	|	1.64
18.833	0.00	0.51	1.267	o	|	|	|	|	1.64
18.917	0.00	0.50	1.263	o	|	|	|	|	1.64
19.000	0.00	0.50	1.260	o	|	|	|	|	1.63
19.083	0.00	0.50	1.256	o	|	|	|	|	1.63
19.167	0.00	0.50	1.253	o	|	|	|	|	1.62
19.250	0.00	0.50	1.249	o	|	|	|	|	1.62
19.333	0.00	0.49	1.246	o	|	|	|	|	1.61
19.417	0.00	0.49	1.243	o	|	|	|	|	1.61
19.500	0.00	0.49	1.239	o	|	|	|	|	1.61
19.583	0.00	0.49	1.236	o	|	|	|	|	1.60
19.667	0.00	0.49	1.233	o	|	|	|	|	1.60
19.750	0.00	0.49	1.229	o	|	|	|	|	1.59
19.833	0.00	0.48	1.226	o	|	|	|	|	1.59
19.917	0.00	0.48	1.223	o	|	|	|	|	1.59
20.000	0.00	0.48	1.219	o	|	|	|	|	1.58
20.083	0.00	0.48	1.216	o	|	|	|	|	1.58
20.167	0.00	0.48	1.213	o	|	|	|	|	1.57
20.250	0.00	0.47	1.209	o	|	|	|	|	1.57
20.333	0.00	0.47	1.206	o	|	|	|	|	1.57
20.417	0.00	0.47	1.203	o	|	|	|	|	1.56
20.500	0.00	0.47	1.200	o	|	|	|	|	1.56
20.583	0.00	0.47	1.196	o	|	|	|	|	1.55
20.667	0.00	0.47	1.193	o	|	|	|	|	1.55
20.750	0.00	0.46	1.190	o	|	|	|	|	1.55
20.833	0.00	0.46	1.187	o	|	|	|	|	1.54
20.917	0.00	0.46	1.184	o	|	|	|	|	1.54
21.000	0.00	0.46	1.180	o	|	|	|	|	1.53
21.083	0.00	0.46	1.177	o	|	|	|	|	1.53
21.167	0.00	0.46	1.174	o	|	|	|	|	1.53
21.250	0.00	0.45	1.171	o	|	|	|	|	1.52
21.333	0.00	0.45	1.168	o	|	|	|	|	1.52
21.417	0.00	0.45	1.165	o	|	|	|	|	1.52
21.500	0.00	0.45	1.162	o	|	|	|	|	1.51
21.583	0.00	0.45	1.159	o	|	|	|	|	1.51
21.667	0.00	0.44	1.156	o	|	|	|	|	1.50
21.750	0.00	0.44	1.152	o	|	|	|	|	1.50
21.833	0.00	0.44	1.149	o	|	|	|	|	1.50
21.917	0.00	0.44	1.146	o	|	|	|	|	1.49
22.000	0.00	0.44	1.143	o	|	|	|	|	1.49
22.083	0.00	0.44	1.140	o	|	|	|	|	1.49
22.167	0.00	0.43	1.137	o	|	|	|	|	1.48
22.250	0.00	0.43	1.134	o	|	|	|	|	1.48
22.333	0.00	0.43	1.131	o	|	|	|	|	1.47
22.417	0.00	0.43	1.128	o	|	|	|	|	1.47
22.500	0.00	0.43	1.125	o	|	|	|	|	1.47
22.583	0.00	0.43	1.123	o	|	|	|	|	1.46
22.667	0.00	0.43	1.120	o	|	|	|	|	1.46
22.750	0.00	0.42	1.117	o	|	|	|	|	1.46
22.833	0.00	0.42	1.114	o	|	|	|	|	1.45
22.917	0.00	0.42	1.111	o	|	|	|	|	1.45
23.000	0.00	0.42	1.108	o	|	|	|	|	1.45
23.083	0.00	0.42	1.105	o	|	|	|	|	1.44
23.167	0.00	0.42	1.102	o	|	|	|	|	1.44
23.250	0.00	0.41	1.099	o	|	|	|	|	1.44

23.333	0.00	0.41	1.097	o	|	|	|	|	1.43
23.417	0.00	0.41	1.094	o	|	|	|	|	1.43
23.500	0.00	0.41	1.091	o	|	|	|	|	1.43
23.583	0.00	0.41	1.088	o	|	|	|	|	1.42
23.667	0.00	0.41	1.085	o	|	|	|	|	1.42
23.750	0.00	0.40	1.082	o	|	|	|	|	1.41
23.833	0.00	0.40	1.080	o	|	|	|	|	1.41
23.917	0.00	0.40	1.077	o	|	|	|	|	1.41
24.000	0.00	0.40	1.074	o	|	|	|	|	1.40
24.083	0.00	0.40	1.071	o	|	|	|	|	1.40
24.167	0.00	0.40	1.069	o	|	|	|	|	1.40
24.250	0.00	0.40	1.066	o	|	|	|	|	1.39
24.333	0.00	0.39	1.063	o	|	|	|	|	1.39
24.417	0.00	0.39	1.060	o	|	|	|	|	1.39
24.500	0.00	0.39	1.058	o	|	|	|	|	1.38
24.583	0.00	0.39	1.055	o	|	|	|	|	1.38
24.667	0.00	0.39	1.052	o	|	|	|	|	1.38
24.750	0.00	0.39	1.050	o	|	|	|	|	1.37
24.833	0.00	0.39	1.047	o	|	|	|	|	1.37
24.917	0.00	0.38	1.044	o	|	|	|	|	1.37
25.000	0.00	0.38	1.042	o	|	|	|	|	1.37
25.083	0.00	0.38	1.039	o	|	|	|	|	1.36
25.167	0.00	0.38	1.037	o	|	|	|	|	1.36
25.250	0.00	0.38	1.034	o	|	|	|	|	1.36
25.333	0.00	0.38	1.031	o	|	|	|	|	1.35
25.417	0.00	0.38	1.029	o	|	|	|	|	1.35
25.500	0.00	0.37	1.026	o	|	|	|	|	1.35
25.583	0.00	0.37	1.024	o	|	|	|	|	1.34
25.667	0.00	0.37	1.021	o	|	|	|	|	1.34
25.750	0.00	0.37	1.019	o	|	|	|	|	1.34
25.833	0.00	0.37	1.016	o	|	|	|	|	1.33
25.917	0.00	0.37	1.013	o	|	|	|	|	1.33
26.000	0.00	0.37	1.011	o	|	|	|	|	1.33
26.083	0.00	0.36	1.008	o	|	|	|	|	1.32
26.167	0.00	0.36	1.006	o	|	|	|	|	1.32
26.250	0.00	0.36	1.003	o	|	|	|	|	1.32
26.333	0.00	0.36	1.001	o	|	|	|	|	1.32
26.417	0.00	0.36	0.998	o	|	|	|	|	1.31
26.500	0.00	0.36	0.996	o	|	|	|	|	1.31
26.583	0.00	0.36	0.994	o	|	|	|	|	1.31
26.667	0.00	0.35	0.991	o	|	|	|	|	1.30
26.750	0.00	0.35	0.989	o	|	|	|	|	1.30
26.833	0.00	0.35	0.986	o	|	|	|	|	1.30
26.917	0.00	0.35	0.984	o	|	|	|	|	1.29
27.000	0.00	0.35	0.981	o	|	|	|	|	1.29
27.083	0.00	0.35	0.979	o	|	|	|	|	1.29
27.167	0.00	0.35	0.977	o	|	|	|	|	1.29
27.250	0.00	0.35	0.974	o	|	|	|	|	1.28
27.333	0.00	0.34	0.972	o	|	|	|	|	1.28
27.417	0.00	0.34	0.969	o	|	|	|	|	1.28
27.500	0.00	0.34	0.967	o	|	|	|	|	1.27
27.583	0.00	0.34	0.965	o	|	|	|	|	1.27
27.667	0.00	0.34	0.962	o	|	|	|	|	1.27
27.750	0.00	0.34	0.960	o	|	|	|	|	1.27
27.833	0.00	0.34	0.958	o	|	|	|	|	1.26
27.917	0.00	0.33	0.955	o	|	|	|	|	1.26
28.000	0.00	0.33	0.953	o	|	|	|	|	1.26
28.083	0.00	0.33	0.951	o	|	|	|	|	1.25
28.167	0.00	0.33	0.949	o	|	|	|	|	1.25
28.250	0.00	0.33	0.946	o	|	|	|	|	1.25
28.333	0.00	0.33	0.944	o	|	|	|	|	1.25
28.417	0.00	0.33	0.942	o	|	|	|	|	1.24
28.500	0.00	0.33	0.940	o	|	|	|	|	1.24
28.583	0.00	0.32	0.937	o	|	|	|	|	1.24
28.667	0.00	0.32	0.935	o	|	|	|	|	1.23
28.750	0.00	0.32	0.933	o	|	|	|	|	1.23
28.833	0.00	0.32	0.931	o	|	|	|	|	1.23
28.917	0.00	0.32	0.928	o	|	|	|	|	1.23
29.000	0.00	0.32	0.926	o	|	|	|	|	1.22
29.083	0.00	0.32	0.924	o	|	|	|	|	1.22
29.167	0.00	0.32	0.922	o	|	|	|	|	1.22
29.250	0.00	0.32	0.920	o	|	|	|	|	1.22
29.333	0.00	0.31	0.918	o	|	|	|	|	1.21
29.417	0.00	0.31	0.915	o	|	|	|	|	1.21
29.500	0.00	0.31	0.913	o	|	|	|	|	1.21
29.583	0.00	0.31	0.911	o	|	|	|	|	1.21
29.667	0.00	0.31	0.909	o	|	|	|	|	1.20
29.750	0.00	0.31	0.907	o	|	|	|	|	1.20
29.833	0.00	0.31	0.905	o	|	|	|	|	1.20
29.917	0.00	0.31	0.903	o	|	|	|	|	1.20
30.000	0.00	0.30	0.900	o	|	|	|	|	1.19
30.083	0.00	0.30	0.898	o	|	|	|	|	1.19
30.167	0.00	0.30	0.896	o	|	|	|	|	1.19
30.250	0.00	0.30	0.894	o	|	|	|	|	1.18
30.333	0.00	0.30	0.892	o	|	|	|	|	1.18
30.417	0.00	0.30	0.890	o	|	|	|	|	1.18

30.500	0.00	0.30	0.888	o	|	|	|	|	1.18
30.583	0.00	0.30	0.886	o	|	|	|	|	1.17
30.667	0.00	0.30	0.884	o	|	|	|	|	1.17
30.750	0.00	0.29	0.882	o	|	|	|	|	1.17
30.833	0.00	0.29	0.880	o	|	|	|	|	1.17
30.917	0.00	0.29	0.878	o	|	|	|	|	1.16
31.000	0.00	0.29	0.876	o	|	|	|	|	1.16
31.083	0.00	0.29	0.874	o	|	|	|	|	1.16
31.167	0.00	0.29	0.872	o	|	|	|	|	1.16
31.250	0.00	0.29	0.870	o	|	|	|	|	1.16
31.333	0.00	0.29	0.868	o	|	|	|	|	1.15
31.417	0.00	0.29	0.866	o	|	|	|	|	1.15
31.500	0.00	0.28	0.864	o	|	|	|	|	1.15
31.583	0.00	0.28	0.862	o	|	|	|	|	1.15
31.667	0.00	0.28	0.860	o	|	|	|	|	1.14
31.750	0.00	0.28	0.858	o	|	|	|	|	1.14
31.833	0.00	0.28	0.856	o	|	|	|	|	1.14
31.917	0.00	0.28	0.854	o	|	|	|	|	1.14
32.000	0.00	0.28	0.852	o	|	|	|	|	1.13
32.083	0.00	0.28	0.850	o	|	|	|	|	1.13
32.167	0.00	0.28	0.849	o	|	|	|	|	1.13
32.250	0.00	0.28	0.847	o	|	|	|	|	1.13
32.333	0.00	0.27	0.845	o	|	|	|	|	1.12
32.417	0.00	0.27	0.843	o	|	|	|	|	1.12
32.500	0.00	0.27	0.841	o	|	|	|	|	1.12
32.583	0.00	0.27	0.839	o	|	|	|	|	1.12
32.667	0.00	0.27	0.837	o	|	|	|	|	1.12
32.750	0.00	0.27	0.835	o	|	|	|	|	1.11
32.833	0.00	0.27	0.834	o	|	|	|	|	1.11
32.917	0.00	0.27	0.832	o	|	|	|	|	1.11
33.000	0.00	0.27	0.830	o	|	|	|	|	1.11
33.083	0.00	0.26	0.828	o	|	|	|	|	1.10
33.167	0.00	0.26	0.826	o	|	|	|	|	1.10
33.250	0.00	0.26	0.824	o	|	|	|	|	1.10
33.333	0.00	0.26	0.823	o	|	|	|	|	1.10
33.417	0.00	0.26	0.821	o	|	|	|	|	1.10
33.500	0.00	0.26	0.819	o	|	|	|	|	1.09
33.583	0.00	0.26	0.817	o	|	|	|	|	1.09
33.667	0.00	0.26	0.815	o	|	|	|	|	1.09
33.750	0.00	0.26	0.814	o	|	|	|	|	1.09
33.833	0.00	0.26	0.812	o	|	|	|	|	1.08
33.917	0.00	0.25	0.810	o	|	|	|	|	1.08
34.000	0.00	0.25	0.808	o	|	|	|	|	1.08
34.083	0.00	0.25	0.807	o	|	|	|	|	1.08
34.167	0.00	0.25	0.805	o	|	|	|	|	1.08
34.250	0.00	0.25	0.803	o	|	|	|	|	1.07
34.333	0.00	0.25	0.801	o	|	|	|	|	1.07
34.417	0.00	0.25	0.800	o	|	|	|	|	1.07
34.500	0.00	0.25	0.798	o	|	|	|	|	1.07
34.583	0.00	0.25	0.796	o	|	|	|	|	1.07
34.667	0.00	0.25	0.795	o	|	|	|	|	1.06
34.750	0.00	0.25	0.793	o	|	|	|	|	1.06
34.833	0.00	0.24	0.791	o	|	|	|	|	1.06
34.917	0.00	0.24	0.790	o	|	|	|	|	1.06
35.000	0.00	0.24	0.788	o	|	|	|	|	1.05
35.083	0.00	0.24	0.786	o	|	|	|	|	1.05
35.167	0.00	0.24	0.785	o	|	|	|	|	1.05
35.250	0.00	0.24	0.783	o	|	|	|	|	1.05
35.333	0.00	0.24	0.781	o	|	|	|	|	1.05
35.417	0.00	0.24	0.780	o	|	|	|	|	1.04
35.500	0.00	0.24	0.778	o	|	|	|	|	1.04
35.583	0.00	0.24	0.776	o	|	|	|	|	1.04
35.667	0.00	0.24	0.775	o	|	|	|	|	1.04
35.750	0.00	0.23	0.773	o	|	|	|	|	1.04
35.833	0.00	0.23	0.771	o	|	|	|	|	1.03
35.917	0.00	0.23	0.770	o	|	|	|	|	1.03
36.000	0.00	0.23	0.768	o	|	|	|	|	1.03
36.083	0.00	0.23	0.767	o	|	|	|	|	1.03
36.167	0.00	0.23	0.765	o	|	|	|	|	1.03
36.250	0.00	0.23	0.764	o	|	|	|	|	1.03
36.333	0.00	0.23	0.762	o	|	|	|	|	1.02
36.417	0.00	0.23	0.760	o	|	|	|	|	1.02
36.500	0.00	0.23	0.759	o	|	|	|	|	1.02
36.583	0.00	0.23	0.757	o	|	|	|	|	1.02
36.667	0.00	0.22	0.756	o	|	|	|	|	1.02
36.750	0.00	0.22	0.754	o	|	|	|	|	1.01
36.833	0.00	0.22	0.753	o	|	|	|	|	1.01
36.917	0.00	0.22	0.751	o	|	|	|	|	1.01
37.000	0.00	0.22	0.750	o	|	|	|	|	1.01
37.083	0.00	0.22	0.748	o	|	|	|	|	1.01
37.167	0.00	0.22	0.746	o	|	|	|	|	1.00
37.250	0.00	0.22	0.745	o	|	|	|	|	1.00
37.333	0.00	0.22	0.743	o	|	|	|	|	1.00
37.417	0.00	0.22	0.742	o	|	|	|	|	1.00
37.500	0.00	0.22	0.740	o	|	|	|	|	1.00
37.583	0.00	0.22	0.739	o	|	|	|	|	0.99

37.667	0.00	0.22	0.737	o	|	|	|	0.99
37.750	0.00	0.22	0.736	o	|	|	|	0.99
37.833	0.00	0.22	0.735	o	|	|	|	0.99
37.917	0.00	0.22	0.733	o	|	|	|	0.99
38.000	0.00	0.21	0.732	o	|	|	|	0.98
38.083	0.00	0.21	0.730	o	|	|	|	0.98
38.167	0.00	0.21	0.729	o	|	|	|	0.98
38.250	0.00	0.21	0.727	o	|	|	|	0.98
38.333	0.00	0.21	0.726	o	|	|	|	0.98
38.417	0.00	0.21	0.724	o	|	|	|	0.97
38.500	0.00	0.21	0.723	o	|	|	|	0.97
38.583	0.00	0.21	0.721	o	|	|	|	0.97
38.667	0.00	0.21	0.720	o	|	|	|	0.97
38.750	0.00	0.21	0.718	o	|	|	|	0.97
38.833	0.00	0.21	0.717	o	|	|	|	0.96
38.917	0.00	0.21	0.715	o	|	|	|	0.96
39.000	0.00	0.21	0.714	o	|	|	|	0.96
39.083	0.00	0.21	0.713	o	|	|	|	0.96
39.167	0.00	0.21	0.711	o	|	|	|	0.96
39.250	0.00	0.21	0.710	o	|	|	|	0.96
39.333	0.00	0.21	0.708	o	|	|	|	0.95
39.417	0.00	0.21	0.707	o	|	|	|	0.95
39.500	0.00	0.21	0.705	o	|	|	|	0.95
39.583	0.00	0.21	0.704	o	|	|	|	0.95
39.667	0.00	0.21	0.703	o	|	|	|	0.95
39.750	0.00	0.21	0.701	o	|	|	|	0.94
39.833	0.00	0.21	0.700	o	|	|	|	0.94
39.917	0.00	0.20	0.698	o	|	|	|	0.94
40.000	0.00	0.20	0.697	o	|	|	|	0.94
40.083	0.00	0.20	0.696	o	|	|	|	0.94
40.167	0.00	0.20	0.694	o	|	|	|	0.93
40.250	0.00	0.20	0.693	o	|	|	|	0.93
40.333	0.00	0.20	0.691	o	|	|	|	0.93
40.417	0.00	0.20	0.690	o	|	|	|	0.93
40.500	0.00	0.20	0.689	o	|	|	|	0.93
40.583	0.00	0.20	0.687	o	|	|	|	0.92
40.667	0.00	0.20	0.686	o	|	|	|	0.92
40.750	0.00	0.20	0.684	o	|	|	|	0.92
40.833	0.00	0.20	0.683	o	|	|	|	0.92
40.917	0.00	0.20	0.682	o	|	|	|	0.92
41.000	0.00	0.20	0.680	o	|	|	|	0.92
41.083	0.00	0.20	0.679	o	|	|	|	0.91
41.167	0.00	0.20	0.677	o	|	|	|	0.91
41.250	0.00	0.20	0.676	o	|	|	|	0.91
41.333	0.00	0.20	0.675	o	|	|	|	0.91
41.417	0.00	0.20	0.673	o	|	|	|	0.91
41.500	0.00	0.20	0.672	o	|	|	|	0.90
41.583	0.00	0.20	0.671	o	|	|	|	0.90
41.667	0.00	0.20	0.669	o	|	|	|	0.90
41.750	0.00	0.20	0.668	o	|	|	|	0.90
41.833	0.00	0.20	0.667	o	|	|	|	0.90
41.917	0.00	0.20	0.665	o	|	|	|	0.90
42.000	0.00	0.19	0.664	o	|	|	|	0.89
42.083	0.00	0.19	0.663	o	|	|	|	0.89
42.167	0.00	0.19	0.661	o	|	|	|	0.89
42.250	0.00	0.19	0.660	o	|	|	|	0.89
42.333	0.00	0.19	0.659	o	|	|	|	0.89
42.417	0.00	0.19	0.657	o	|	|	|	0.88
42.500	0.00	0.19	0.656	o	|	|	|	0.88
42.583	0.00	0.19	0.655	o	|	|	|	0.88
42.667	0.00	0.19	0.653	o	|	|	|	0.88
42.750	0.00	0.19	0.652	o	|	|	|	0.88
42.833	0.00	0.19	0.651	o	|	|	|	0.88
42.917	0.00	0.19	0.649	o	|	|	|	0.87
43.000	0.00	0.19	0.648	o	|	|	|	0.87
43.083	0.00	0.19	0.647	o	|	|	|	0.87
43.167	0.00	0.19	0.645	o	|	|	|	0.87
43.250	0.00	0.19	0.644	o	|	|	|	0.87
43.333	0.00	0.19	0.643	o	|	|	|	0.87
43.417	0.00	0.19	0.642	o	|	|	|	0.86
43.500	0.00	0.19	0.640	o	|	|	|	0.86
43.583	0.00	0.19	0.639	o	|	|	|	0.86
43.667	0.00	0.19	0.638	o	|	|	|	0.86
43.750	0.00	0.19	0.636	o	|	|	|	0.86
43.833	0.00	0.19	0.635	o	|	|	|	0.85
43.917	0.00	0.19	0.634	o	|	|	|	0.85
44.000	0.00	0.19	0.632	o	|	|	|	0.85
44.083	0.00	0.19	0.631	o	|	|	|	0.85
44.167	0.00	0.18	0.630	o	|	|	|	0.85
44.250	0.00	0.18	0.629	o	|	|	|	0.85
44.333	0.00	0.18	0.627	o	|	|	|	0.84
44.417	0.00	0.18	0.626	o	|	|	|	0.84
44.500	0.00	0.18	0.625	o	|	|	|	0.84
44.583	0.00	0.18	0.624	o	|	|	|	0.84
44.667	0.00	0.18	0.622	o	|	|	|	0.84
44.750	0.00	0.18	0.621	o	|	|	|	0.84

44.833	0.00	0.18	0.620	o	|	|	|	0.83
44.917	0.00	0.18	0.619	o	|	|	|	0.83
45.000	0.00	0.18	0.617	o	|	|	|	0.83
45.083	0.00	0.18	0.616	o	|	|	|	0.83
45.167	0.00	0.18	0.615	o	|	|	|	0.83
45.250	0.00	0.18	0.614	o	|	|	|	0.83
45.333	0.00	0.18	0.612	o	|	|	|	0.82
45.417	0.00	0.18	0.611	o	|	|	|	0.82
45.500	0.00	0.18	0.610	o	|	|	|	0.82
45.583	0.00	0.18	0.609	o	|	|	|	0.82
45.667	0.00	0.18	0.607	o	|	|	|	0.82
45.750	0.00	0.18	0.606	o	|	|	|	0.82
45.833	0.00	0.18	0.605	o	|	|	|	0.81
45.917	0.00	0.18	0.604	o	|	|	|	0.81
46.000	0.00	0.18	0.603	o	|	|	|	0.81
46.083	0.00	0.18	0.601	o	|	|	|	0.81
46.167	0.00	0.18	0.600	o	|	|	|	0.81
46.250	0.00	0.18	0.599	o	|	|	|	0.81
46.333	0.00	0.18	0.598	o	|	|	|	0.80
46.417	0.00	0.18	0.596	o	|	|	|	0.80
46.500	0.00	0.17	0.595	o	|	|	|	0.80
46.583	0.00	0.17	0.594	o	|	|	|	0.80
46.667	0.00	0.17	0.593	o	|	|	|	0.80
46.750	0.00	0.17	0.592	o	|	|	|	0.80
46.833	0.00	0.17	0.590	o	|	|	|	0.79
46.917	0.00	0.17	0.589	o	|	|	|	0.79
47.000	0.00	0.17	0.588	o	|	|	|	0.79
47.083	0.00	0.17	0.587	o	|	|	|	0.79
47.167	0.00	0.17	0.586	o	|	|	|	0.79
47.250	0.00	0.17	0.585	o	|	|	|	0.79
47.333	0.00	0.17	0.583	o	|	|	|	0.79
47.417	0.00	0.17	0.582	o	|	|	|	0.78
47.500	0.00	0.17	0.581	o	|	|	|	0.78
47.583	0.00	0.17	0.580	o	|	|	|	0.78
47.667	0.00	0.17	0.579	o	|	|	|	0.78
47.750	0.00	0.17	0.578	o	|	|	|	0.78
47.833	0.00	0.17	0.576	o	|	|	|	0.78
47.917	0.00	0.17	0.575	o	|	|	|	0.77
48.000	0.00	0.17	0.574	o	|	|	|	0.77
48.083	0.00	0.17	0.573	o	|	|	|	0.77
48.167	0.00	0.17	0.572	o	|	|	|	0.77
48.250	0.00	0.17	0.571	o	|	|	|	0.77
48.333	0.00	0.17	0.569	o	|	|	|	0.77
48.417	0.00	0.17	0.568	o	|	|	|	0.76
48.500	0.00	0.17	0.567	o	|	|	|	0.76
48.583	0.00	0.17	0.566	o	|	|	|	0.76
48.667	0.00	0.17	0.565	o	|	|	|	0.76
48.750	0.00	0.17	0.564	o	|	|	|	0.76
48.833	0.00	0.17	0.563	o	|	|	|	0.76
48.917	0.00	0.16	0.561	o	|	|	|	0.76
49.000	0.00	0.16	0.560	o	|	|	|	0.75
49.083	0.00	0.16	0.559	o	|	|	|	0.75
49.167	0.00	0.16	0.558	o	|	|	|	0.75
49.250	0.00	0.16	0.557	o	|	|	|	0.75
49.333	0.00	0.16	0.556	o	|	|	|	0.75
49.417	0.00	0.16	0.555	o	|	|	|	0.75
49.500	0.00	0.16	0.554	o	|	|	|	0.74
49.583	0.00	0.16	0.552	o	|	|	|	0.74
49.667	0.00	0.16	0.551	o	|	|	|	0.74
49.750	0.00	0.16	0.550	o	|	|	|	0.74
49.833	0.00	0.16	0.549	o	|	|	|	0.74
49.917	0.00	0.16	0.548	o	|	|	|	0.74
50.000	0.00	0.16	0.547	o	|	|	|	0.74
50.083	0.00	0.16	0.546	o	|	|	|	0.73
50.167	0.00	0.16	0.545	o	|	|	|	0.73
50.250	0.00	0.16	0.544	o	|	|	|	0.73
50.333	0.00	0.16	0.542	o	|	|	|	0.73
50.417	0.00	0.16	0.541	o	|	|	|	0.73
50.500	0.00	0.16	0.540	o	|	|	|	0.73
50.583	0.00	0.16	0.539	o	|	|	|	0.73
50.667	0.00	0.16	0.538	o	|	|	|	0.72
50.750	0.00	0.16	0.537	o	|	|	|	0.72
50.833	0.00	0.16	0.536	o	|	|	|	0.72
50.917	0.00	0.16	0.535	o	|	|	|	0.72
51.000	0.00	0.16	0.534	o	|	|	|	0.72
51.083	0.00	0.16	0.533	o	|	|	|	0.72
51.167	0.00	0.16	0.532	o	|	|	|	0.72
51.250	0.00	0.16	0.531	o	|	|	|	0.71
51.333	0.00	0.16	0.529	o	|	|	|	0.71
51.417	0.00	0.16	0.528	o	|	|	|	0.71
51.500	0.00	0.15	0.527	o	|	|	|	0.71
51.583	0.00	0.15	0.526	o	|	|	|	0.71
51.667	0.00	0.15	0.525	o	|	|	|	0.71
51.750	0.00	0.15	0.524	o	|	|	|	0.71
51.833	0.00	0.15	0.523	o	|	|	|	0.70
51.917	0.00	0.15	0.522	o	|	|	|	0.70

52.000	0.00	0.15	0.521	o	|	|	|	|	0.70
52.083	0.00	0.15	0.520	o	|	|	|	|	0.70
52.167	0.00	0.15	0.519	o	|	|	|	|	0.70
52.250	0.00	0.15	0.518	o	|	|	|	|	0.70
52.333	0.00	0.15	0.517	o	|	|	|	|	0.70
52.417	0.00	0.15	0.516	o	|	|	|	|	0.69
52.500	0.00	0.15	0.515	o	|	|	|	|	0.69
52.583	0.00	0.15	0.514	o	|	|	|	|	0.69
52.667	0.00	0.15	0.513	o	|	|	|	|	0.69
52.750	0.00	0.15	0.512	o	|	|	|	|	0.69
52.833	0.00	0.15	0.511	o	|	|	|	|	0.69
52.917	0.00	0.15	0.510	o	|	|	|	|	0.69
53.000	0.00	0.15	0.508	o	|	|	|	|	0.68
53.083	0.00	0.15	0.507	o	|	|	|	|	0.68
53.167	0.00	0.15	0.506	o	|	|	|	|	0.68
53.250	0.00	0.15	0.505	o	|	|	|	|	0.68
53.333	0.00	0.15	0.504	o	|	|	|	|	0.68
53.417	0.00	0.15	0.503	o	|	|	|	|	0.68
53.500	0.00	0.15	0.502	o	|	|	|	|	0.68
53.583	0.00	0.15	0.501	o	|	|	|	|	0.67
53.667	0.00	0.15	0.500	o	|	|	|	|	0.67
53.750	0.00	0.15	0.499	o	|	|	|	|	0.67
53.833	0.00	0.15	0.498	o	|	|	|	|	0.67
53.917	0.00	0.15	0.497	o	|	|	|	|	0.67
54.000	0.00	0.15	0.496	o	|	|	|	|	0.67
54.083	0.00	0.15	0.495	o	|	|	|	|	0.67
54.167	0.00	0.15	0.494	o	|	|	|	|	0.67
54.250	0.00	0.14	0.493	o	|	|	|	|	0.66
54.333	0.00	0.14	0.492	o	|	|	|	|	0.66
54.417	0.00	0.14	0.491	o	|	|	|	|	0.66
54.500	0.00	0.14	0.490	o	|	|	|	|	0.66
54.583	0.00	0.14	0.489	o	|	|	|	|	0.66
54.667	0.00	0.14	0.488	o	|	|	|	|	0.66
54.750	0.00	0.14	0.487	o	|	|	|	|	0.66
54.833	0.00	0.14	0.486	o	|	|	|	|	0.65
54.917	0.00	0.14	0.485	o	|	|	|	|	0.65
55.000	0.00	0.14	0.484	o	|	|	|	|	0.65
55.083	0.00	0.14	0.483	o	|	|	|	|	0.65
55.167	0.00	0.14	0.482	o	|	|	|	|	0.65
55.250	0.00	0.14	0.481	o	|	|	|	|	0.65
55.333	0.00	0.14	0.481	o	|	|	|	|	0.65
55.417	0.00	0.14	0.480	o	|	|	|	|	0.65
55.500	0.00	0.14	0.479	o	|	|	|	|	0.64
55.583	0.00	0.14	0.478	o	|	|	|	|	0.64
55.667	0.00	0.14	0.477	o	|	|	|	|	0.64
55.750	0.00	0.14	0.476	o	|	|	|	|	0.64
55.833	0.00	0.14	0.475	o	|	|	|	|	0.64
55.917	0.00	0.14	0.474	o	|	|	|	|	0.64
56.000	0.00	0.14	0.473	o	|	|	|	|	0.64
56.083	0.00	0.14	0.472	o	|	|	|	|	0.64
56.167	0.00	0.14	0.471	o	|	|	|	|	0.63
56.250	0.00	0.14	0.470	o	|	|	|	|	0.63
56.333	0.00	0.14	0.469	o	|	|	|	|	0.63
56.417	0.00	0.14	0.468	o	|	|	|	|	0.63
56.500	0.00	0.14	0.467	o	|	|	|	|	0.63
56.583	0.00	0.14	0.466	o	|	|	|	|	0.63
56.667	0.00	0.14	0.465	o	|	|	|	|	0.63
56.750	0.00	0.14	0.464	o	|	|	|	|	0.62
56.833	0.00	0.14	0.463	o	|	|	|	|	0.62
56.917	0.00	0.14	0.462	o	|	|	|	|	0.62
57.000	0.00	0.14	0.461	o	|	|	|	|	0.62
57.083	0.00	0.14	0.461	o	|	|	|	|	0.62
57.167	0.00	0.13	0.460	o	|	|	|	|	0.62
57.250	0.00	0.13	0.459	o	|	|	|	|	0.62
57.333	0.00	0.13	0.458	o	|	|	|	|	0.62
57.417	0.00	0.13	0.457	o	|	|	|	|	0.61
57.500	0.00	0.13	0.456	o	|	|	|	|	0.61
57.583	0.00	0.13	0.455	o	|	|	|	|	0.61
57.667	0.00	0.13	0.454	o	|	|	|	|	0.61
57.750	0.00	0.13	0.453	o	|	|	|	|	0.61
57.833	0.00	0.13	0.452	o	|	|	|	|	0.61
57.917	0.00	0.13	0.451	o	|	|	|	|	0.61
58.000	0.00	0.13	0.450	o	|	|	|	|	0.61
58.083	0.00	0.13	0.450	o	|	|	|	|	0.61
58.167	0.00	0.13	0.449	o	|	|	|	|	0.60
58.250	0.00	0.13	0.448	o	|	|	|	|	0.60
58.333	0.00	0.13	0.447	o	|	|	|	|	0.60
58.417	0.00	0.13	0.446	o	|	|	|	|	0.60
58.500	0.00	0.13	0.445	o	|	|	|	|	0.60
58.583	0.00	0.13	0.444	o	|	|	|	|	0.60
58.667	0.00	0.13	0.443	o	|	|	|	|	0.60
58.750	0.00	0.13	0.442	o	|	|	|	|	0.60
58.833	0.00	0.13	0.441	o	|	|	|	|	0.59
58.917	0.00	0.13	0.441	o	|	|	|	|	0.59
59.000	0.00	0.13	0.440	o	|	|	|	|	0.59
59.083	0.00	0.13	0.439	o	|	|	|	|	0.59

59.167	0.00	0.13	0.438	o	|	|	|	0.59
59.250	0.00	0.13	0.437	o	|	|	|	0.59
59.333	0.00	0.13	0.436	o	|	|	|	0.59
59.417	0.00	0.13	0.435	o	|	|	|	0.59
59.500	0.00	0.13	0.434	o	|	|	|	0.58
59.583	0.00	0.13	0.433	o	|	|	|	0.58
59.667	0.00	0.13	0.433	o	|	|	|	0.58
59.750	0.00	0.13	0.432	o	|	|	|	0.58
59.833	0.00	0.13	0.431	o	|	|	|	0.58
59.917	0.00	0.13	0.430	o	|	|	|	0.58
60.000	0.00	0.13	0.429	o	|	|	|	0.58
60.083	0.00	0.13	0.428	o	|	|	|	0.58
60.167	0.00	0.13	0.427	o	|	|	|	0.58
60.250	0.00	0.13	0.427	o	|	|	|	0.57
60.333	0.00	0.12	0.426	o	|	|	|	0.57
60.417	0.00	0.12	0.425	o	|	|	|	0.57
60.500	0.00	0.12	0.424	o	|	|	|	0.57
60.583	0.00	0.12	0.423	o	|	|	|	0.57
60.667	0.00	0.12	0.422	o	|	|	|	0.57
60.750	0.00	0.12	0.421	o	|	|	|	0.57
60.833	0.00	0.12	0.421	o	|	|	|	0.57
60.917	0.00	0.12	0.420	o	|	|	|	0.56
61.000	0.00	0.12	0.419	o	|	|	|	0.56
61.083	0.00	0.12	0.418	o	|	|	|	0.56
61.167	0.00	0.12	0.417	o	|	|	|	0.56
61.250	0.00	0.12	0.416	o	|	|	|	0.56
61.333	0.00	0.12	0.415	o	|	|	|	0.56
61.417	0.00	0.12	0.415	o	|	|	|	0.56
61.500	0.00	0.12	0.414	o	|	|	|	0.56
61.583	0.00	0.12	0.413	o	|	|	|	0.56
61.667	0.00	0.12	0.412	o	|	|	|	0.55
61.750	0.00	0.12	0.411	o	|	|	|	0.55
61.833	0.00	0.12	0.410	o	|	|	|	0.55
61.917	0.00	0.12	0.410	o	|	|	|	0.55
62.000	0.00	0.12	0.409	o	|	|	|	0.55
62.083	0.00	0.12	0.408	o	|	|	|	0.55
62.167	0.00	0.12	0.407	o	|	|	|	0.55
62.250	0.00	0.12	0.406	o	|	|	|	0.55
62.333	0.00	0.12	0.405	o	|	|	|	0.55
62.417	0.00	0.12	0.405	o	|	|	|	0.54
62.500	0.00	0.12	0.404	o	|	|	|	0.54
62.583	0.00	0.12	0.403	o	|	|	|	0.54
62.667	0.00	0.12	0.402	o	|	|	|	0.54
62.750	0.00	0.12	0.401	o	|	|	|	0.54
62.833	0.00	0.12	0.401	o	|	|	|	0.54
62.917	0.00	0.12	0.400	o	|	|	|	0.54
63.000	0.00	0.12	0.399	o	|	|	|	0.54
63.083	0.00	0.12	0.398	o	|	|	|	0.54
63.167	0.00	0.12	0.397	o	|	|	|	0.53
63.250	0.00	0.12	0.397	o	|	|	|	0.53
63.333	0.00	0.12	0.396	o	|	|	|	0.53
63.417	0.00	0.12	0.395	o	|	|	|	0.53
63.500	0.00	0.12	0.394	o	|	|	|	0.53
63.583	0.00	0.12	0.393	o	|	|	|	0.53
63.667	0.00	0.12	0.393	o	|	|	|	0.53
63.750	0.00	0.11	0.392	o	|	|	|	0.53
63.833	0.00	0.11	0.391	o	|	|	|	0.53
63.917	0.00	0.11	0.390	o	|	|	|	0.53
64.000	0.00	0.11	0.389	o	|	|	|	0.52
64.083	0.00	0.11	0.389	o	|	|	|	0.52
64.167	0.00	0.11	0.388	o	|	|	|	0.52
64.250	0.00	0.11	0.387	o	|	|	|	0.52
64.333	0.00	0.11	0.386	o	|	|	|	0.52
64.417	0.00	0.11	0.386	o	|	|	|	0.52
64.500	0.00	0.11	0.385	o	|	|	|	0.52
64.583	0.00	0.11	0.384	o	|	|	|	0.52
64.667	0.00	0.11	0.383	o	|	|	|	0.52
64.750	0.00	0.11	0.382	o	|	|	|	0.51
64.833	0.00	0.11	0.382	o	|	|	|	0.51
64.917	0.00	0.11	0.381	o	|	|	|	0.51
65.000	0.00	0.11	0.380	o	|	|	|	0.51
65.083	0.00	0.11	0.379	o	|	|	|	0.51
65.167	0.00	0.11	0.379	o	|	|	|	0.51
65.250	0.00	0.11	0.378	o	|	|	|	0.51
65.333	0.00	0.11	0.377	o	|	|	|	0.51
65.417	0.00	0.11	0.376	o	|	|	|	0.51
65.500	0.00	0.11	0.376	o	|	|	|	0.51
65.583	0.00	0.11	0.375	o	|	|	|	0.50
65.667	0.00	0.11	0.374	o	|	|	|	0.50
65.750	0.00	0.11	0.373	o	|	|	|	0.50
65.833	0.00	0.11	0.373	o	|	|	|	0.50
65.917	0.00	0.11	0.372	o	|	|	|	0.50
66.000	0.00	0.11	0.371	o	|	|	|	0.50
66.083	0.00	0.11	0.370	o	|	|	|	0.50
66.167	0.00	0.11	0.370	o	|	|	|	0.50
66.250	0.00	0.11	0.369	o	|	|	|	0.50

66.333	0.00	0.11	0.368	o	|	|	|	0.50
66.417	0.00	0.11	0.367	o	|	|	|	0.49
66.500	0.00	0.11	0.367	o	|	|	|	0.49
66.583	0.00	0.11	0.366	o	|	|	|	0.49
66.667	0.00	0.11	0.365	o	|	|	|	0.49
66.750	0.00	0.11	0.364	o	|	|	|	0.49
66.833	0.00	0.11	0.364	o	|	|	|	0.49
66.917	0.00	0.11	0.363	o	|	|	|	0.49
67.000	0.00	0.11	0.362	o	|	|	|	0.49
67.083	0.00	0.11	0.361	o	|	|	|	0.49
67.167	0.00	0.11	0.361	o	|	|	|	0.49
67.250	0.00	0.11	0.360	o	|	|	|	0.48
67.333	0.00	0.11	0.359	o	|	|	|	0.48
67.417	0.00	0.11	0.358	o	|	|	|	0.48
67.500	0.00	0.10	0.358	o	|	|	|	0.48
67.583	0.00	0.10	0.357	o	|	|	|	0.48
67.667	0.00	0.10	0.356	o	|	|	|	0.48
67.750	0.00	0.10	0.356	o	|	|	|	0.48
67.833	0.00	0.10	0.355	o	|	|	|	0.48
67.917	0.00	0.10	0.354	o	|	|	|	0.48
68.000	0.00	0.10	0.353	o	|	|	|	0.48
68.083	0.00	0.10	0.353	o	|	|	|	0.47
68.167	0.00	0.10	0.352	o	|	|	|	0.47
68.250	0.00	0.10	0.351	o	|	|	|	0.47
68.333	0.00	0.10	0.351	o	|	|	|	0.47
68.417	0.00	0.10	0.350	o	|	|	|	0.47
68.500	0.00	0.10	0.349	o	|	|	|	0.47
68.583	0.00	0.10	0.348	o	|	|	|	0.47
68.667	0.00	0.10	0.348	o	|	|	|	0.47
68.750	0.00	0.10	0.347	o	|	|	|	0.47
68.833	0.00	0.10	0.346	o	|	|	|	0.47
68.917	0.00	0.10	0.346	o	|	|	|	0.47
69.000	0.00	0.10	0.345	o	|	|	|	0.46
69.083	0.00	0.10	0.344	o	|	|	|	0.46
69.167	0.00	0.10	0.344	o	|	|	|	0.46
69.250	0.00	0.10	0.343	o	|	|	|	0.46
69.333	0.00	0.10	0.342	o	|	|	|	0.46
69.417	0.00	0.10	0.342	o	|	|	|	0.46
69.500	0.00	0.10	0.341	o	|	|	|	0.46

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 834
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.410 (CFS)
Total volume = 2.115 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro110610.rte
**********HYDROGRAPH DATA**********
Number of intervals = 77
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 27.752 (CFS)
Total volume = 3.349 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 77
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	6.9	13.88	20.81	27.75	Depth (Ft.)
0.083	0.49	0.00	0.002	O	|	|	|	|	0.00
0.167	1.34	0.00	0.008	OI	|	|	|	|	0.01
0.250	1.70	0.01	0.018	OI	|	|	|	|	0.02
0.333	1.82	0.01	0.031	O I	|	|	|	|	0.04
0.417	1.88	0.01	0.043	O I	|	|	|	|	0.06
0.500	2.11	0.02	0.057	O I	|	|	|	|	0.08
0.583	2.40	0.02	0.072	O I	|	|	|	|	0.10
0.667	2.47	0.03	0.089	O I	|	|	|	|	0.12
0.750	2.50	0.03	0.106	O I	|	|	|	|	0.14
0.833	2.52	0.04	0.123	O I	|	|	|	|	0.17
0.917	2.53	0.04	0.140	O I	|	|	|	|	0.19
1.000	2.72	0.05	0.158	O I	|	|	|	|	0.21
1.083	3.01	0.05	0.177	O I	|	|	|	|	0.24
1.167	3.08	0.06	0.198	O I	|	|	|	|	0.27
1.250	3.11	0.06	0.219	O I	|	|	|	|	0.29
1.333	3.13	0.07	0.240	O I	|	|	|	|	0.32
1.417	3.14	0.08	0.261	O I	|	|	|	|	0.35
1.500	3.14	0.08	0.282	O I	|	|	|	|	0.38
1.583	3.14	0.09	0.303	O I	|	|	|	|	0.41
1.667	3.14	0.09	0.324	O I	|	|	|	|	0.44
1.750	3.14	0.10	0.345	O I	|	|	|	|	0.46

1.833	3.14	0.11	0.365	O	I	|	|	|	0.49
1.917	3.14	0.11	0.386	O	I	|	|	|	0.52
2.000	3.33	0.12	0.408	O	I	|	|	|	0.55
2.083	3.42	0.13	0.430	O	I	|	|	|	0.58
2.167	3.40	0.13	0.453	O	I	|	|	|	0.61
2.250	3.65	0.14	0.476	O	I	|	|	|	0.64
2.333	3.70	0.15	0.500	O	I	|	|	|	0.67
2.417	3.73	0.15	0.525	O	I	|	|	|	0.71
2.500	3.74	0.16	0.550	O	I	|	|	|	0.74
2.583	3.74	0.17	0.574	O	I	|	|	|	0.77
2.667	3.74	0.18	0.599	O	I	|	|	|	0.81
2.750	3.94	0.18	0.624	O	I	|	|	|	0.84
2.833	4.23	0.19	0.651	O	I	|	|	|	0.88
2.917	4.30	0.20	0.679	O	I	|	|	|	0.91
3.000	4.33	0.21	0.707	O	I	|	|	|	0.95
3.083	4.34	0.22	0.736	O	I	|	|	|	0.99
3.167	4.55	0.23	0.765	O	I	|	|	|	1.03
3.250	4.84	0.25	0.795	O	I	|	|	|	1.06
3.333	4.91	0.26	0.827	O	I	|	|	|	1.10
3.417	5.13	0.28	0.860	O	I	|	|	|	1.14
3.500	5.63	0.30	0.895	O	I	|	|	|	1.19
3.583	6.20	0.32	0.934	O	I	|	|	|	1.23
3.667	6.58	0.35	0.975	O	I	|	|	|	1.28
3.750	6.90	0.37	1.019	O	I	|	|	|	1.34
3.833	7.24	0.40	1.065	O	I	|	|	|	1.39
3.917	7.53	0.42	1.113	O	I	|	|	|	1.45
4.000	7.86	0.45	1.163	O	I	|	|	|	1.51
4.083	8.14	0.48	1.215	O	I	|	|	|	1.58
4.167	8.66	0.51	1.270	O	I	|	|	|	1.64
4.250	9.23	0.54	1.328	O	I	|	|	|	1.71
4.333	9.83	0.57	1.390	O	I	|	|	|	1.79
4.417	10.43	0.61	1.455	O	I	|	|	|	1.87
4.500	10.84	0.65	1.524	O	I	|	|	|	1.95
4.583	11.16	0.70	1.595	O	I	|	|	|	2.04
4.667	11.70	0.77	1.669	O	I	|	|	|	2.12
4.750	12.28	0.84	1.746	O	I	|	|	|	2.21
4.833	12.67	0.92	1.826	O	I	|	|	|	2.30
4.917	12.98	1.00	1.907	O	I	|	|	|	2.39
5.000	13.52	1.08	1.992	O	I	|	|	|	2.48
5.083	14.89	1.16	2.082	O	I	|	|	|	2.58
5.167	17.42	1.26	2.185	O	I	|	|	|	2.70
5.250	19.85	1.37	2.304	O	I	|	|	|	2.83
5.333	21.82	1.50	2.437	O	I	|	|	|	2.98
5.417	24.12	12.47	2.548	|	|	O	|	I	3.10
5.500	27.75	20.33	2.613	|	|	|	O	I	3.17
5.583	23.57	23.44	2.639	|	|	|	O	|	3.19
5.667	11.80	20.08	2.611	|	|	I	O	|	3.16
5.750	6.15	13.60	2.557	|	I	O	|	|	3.11
5.833	3.53	8.49	2.514	|	I	O	|	|	3.06
5.917	2.14	5.19	2.487	|	I	O	|	|	3.03
6.000	1.14	3.12	2.469	|	I	O	|	|	3.01
6.083	0.57	1.80	2.458	I	O	|	|	|	3.00
6.167	0.18	1.51	2.450	I	O	|	|	|	2.99
6.250	0.08	1.50	2.440	I	O	|	|	|	2.98
6.333	0.03	1.49	2.430	I	O	|	|	|	2.97
6.417	0.01	1.48	2.420	I	O	|	|	|	2.96
6.500	0.00	1.47	2.410	I	O	|	|	|	2.95
6.583	0.00	1.46	2.400	I	O	|	|	|	2.94
6.667	0.00	1.45	2.390	I	O	|	|	|	2.93
6.750	0.00	1.45	2.380	I	O	|	|	|	2.91
6.833	0.00	1.44	2.370	I	O	|	|	|	2.90
6.917	0.00	1.43	2.360	I	O	|	|	|	2.89
7.000	0.00	1.42	2.350	I	O	|	|	|	2.88
7.083	0.00	1.41	2.340	I	O	|	|	|	2.87
7.167	0.00	1.40	2.331	I	O	|	|	|	2.86
7.250	0.00	1.39	2.321	I	O	|	|	|	2.85
7.333	0.00	1.38	2.312	I	O	|	|	|	2.84
7.417	0.00	1.37	2.302	I	O	|	|	|	2.83
7.500	0.00	1.36	2.293	I	O	|	|	|	2.82
7.583	0.00	1.35	2.283	I	O	|	|	|	2.81
7.667	0.00	1.35	2.274	I	O	|	|	|	2.80
7.750	0.00	1.34	2.265	I	O	|	|	|	2.79
7.833	0.00	1.33	2.256	I	O	|	|	|	2.78
7.917	0.00	1.32	2.246	I	O	|	|	|	2.77
8.000	0.00	1.31	2.237	I	O	|	|	|	2.76
8.083	0.00	1.30	2.228	I	O	|	|	|	2.75
8.167	0.00	1.29	2.219	I	O	|	|	|	2.74
8.250	0.00	1.28	2.211	I	O	|	|	|	2.73
8.333	0.00	1.28	2.202	I	O	|	|	|	2.72
8.417	0.00	1.27	2.193	I	O	|	|	|	2.71
8.500	0.00	1.26	2.184	I	O	|	|	|	2.70
8.583	0.00	1.25	2.176	I	O	|	|	|	2.69
8.667	0.00	1.24	2.167	I	O	|	|	|	2.68
8.750	0.00	1.24	2.159	I	O	|	|	|	2.67
8.833	0.00	1.23	2.150	I	O	|	|	|	2.66
8.917	0.00	1.22	2.142	I	O	|	|	|	2.65

9.000	0.00	1.21	2.133	IO					2.64
9.083	0.00	1.20	2.125	IO					2.63
9.167	0.00	1.20	2.117	IO					2.62
9.250	0.00	1.19	2.108	IO					2.61
9.333	0.00	1.18	2.100	IO					2.60
9.417	0.00	1.17	2.092	IO					2.59
9.500	0.00	1.16	2.084	IO					2.58
9.583	0.00	1.16	2.076	IO					2.58
9.667	0.00	1.15	2.068	IO					2.57
9.750	0.00	1.14	2.060	IO					2.56
9.833	0.00	1.13	2.052	IO					2.55
9.917	0.00	1.13	2.045	IO					2.54
10.000	0.00	1.12	2.037	IO					2.53
10.083	0.00	1.11	2.029	IO					2.52
10.167	0.00	1.11	2.022	IO					2.51
10.250	0.00	1.10	2.014	IO					2.51
10.333	0.00	1.09	2.006	IO					2.50
10.417	0.00	1.08	1.999	IO					2.49
10.500	0.00	1.08	1.992	IO					2.48
10.583	0.00	1.07	1.984	IO					2.47
10.667	0.00	1.06	1.977	IO					2.46
10.750	0.00	1.06	1.970	IO					2.46
10.833	0.00	1.05	1.962	IO					2.45
10.917	0.00	1.04	1.955	IO					2.44
11.000	0.00	1.04	1.948	IO					2.43
11.083	0.00	1.03	1.941	IO					2.42
11.167	0.00	1.02	1.934	IO					2.42
11.250	0.00	1.02	1.927	IO					2.41
11.333	0.00	1.01	1.920	IO					2.40
11.417	0.00	1.00	1.913	IO					2.39
11.500	0.00	1.00	1.906	IO					2.39
11.583	0.00	0.99	1.899	IO					2.38
11.667	0.00	0.98	1.892	IO					2.37
11.750	0.00	0.98	1.886	IO					2.36
11.833	0.00	0.97	1.879	IO					2.36
11.917	0.00	0.96	1.872	IO					2.35
12.000	0.00	0.96	1.866	IO					2.34
12.083	0.00	0.95	1.859	IO					2.33
12.167	0.00	0.94	1.853	IO					2.33
12.250	0.00	0.94	1.846	IO					2.32
12.333	0.00	0.93	1.840	IO					2.31
12.417	0.00	0.93	1.833	IO					2.30
12.500	0.00	0.92	1.827	IO					2.30
12.583	0.00	0.91	1.821	IO					2.29
12.667	0.00	0.91	1.814	IO					2.28
12.750	0.00	0.90	1.808	IO					2.28
12.833	0.00	0.90	1.802	IO					2.27
12.917	0.00	0.89	1.796	IO					2.26
13.000	0.00	0.89	1.790	IO					2.26
13.083	0.00	0.88	1.783	IO					2.25
13.167	0.00	0.87	1.777	IO					2.24
13.250	0.00	0.87	1.771	IO					2.24
13.333	0.00	0.86	1.765	O					2.23
13.417	0.00	0.86	1.760	O					2.22
13.500	0.00	0.85	1.754	O					2.22
13.583	0.00	0.85	1.748	O					2.21
13.667	0.00	0.84	1.742	O					2.20
13.750	0.00	0.83	1.736	O					2.20
13.833	0.00	0.83	1.731	O					2.19
13.917	0.00	0.82	1.725	O					2.18
14.000	0.00	0.82	1.719	O					2.18
14.083	0.00	0.81	1.714	O					2.17
14.167	0.00	0.81	1.708	O					2.16
14.250	0.00	0.80	1.702	O					2.16
14.333	0.00	0.80	1.697	O					2.15
14.417	0.00	0.79	1.691	O					2.15
14.500	0.00	0.79	1.686	O					2.14
14.583	0.00	0.78	1.681	O					2.13
14.667	0.00	0.78	1.675	O					2.13
14.750	0.00	0.77	1.670	O					2.12
14.833	0.00	0.77	1.665	O					2.12
14.917	0.00	0.76	1.659	O					2.11
15.000	0.00	0.76	1.654	O					2.10
15.083	0.00	0.75	1.649	O					2.10
15.167	0.00	0.75	1.644	O					2.09
15.250	0.00	0.74	1.639	O					2.09
15.333	0.00	0.74	1.634	O					2.08
15.417	0.00	0.73	1.629	O					2.08
15.500	0.00	0.73	1.623	O					2.07
15.583	0.00	0.72	1.618	O					2.06
15.667	0.00	0.72	1.614	O					2.06
15.750	0.00	0.71	1.609	O					2.05
15.833	0.00	0.71	1.604	O					2.05
15.917	0.00	0.70	1.599	O					2.04
16.000	0.00	0.70	1.594	O					2.04
16.083	0.00	0.69	1.589	O					2.03

16.167	0.00	0.69	1.584	o	|	|	|	|	2.03
16.250	0.00	0.69	1.580	o	|	|	|	|	2.02
16.333	0.00	0.68	1.575	o	|	|	|	|	2.02
16.417	0.00	0.68	1.570	o	|	|	|	|	2.01
16.500	0.00	0.67	1.566	o	|	|	|	|	2.01
16.583	0.00	0.67	1.561	o	|	|	|	|	2.00
16.667	0.00	0.67	1.556	o	|	|	|	|	1.99
16.750	0.00	0.66	1.552	o	|	|	|	|	1.99
16.833	0.00	0.66	1.547	o	|	|	|	|	1.98
16.917	0.00	0.66	1.543	o	|	|	|	|	1.98
17.000	0.00	0.66	1.538	o	|	|	|	|	1.97
17.083	0.00	0.65	1.534	o	|	|	|	|	1.97
17.167	0.00	0.65	1.529	o	|	|	|	|	1.96
17.250	0.00	0.65	1.525	o	|	|	|	|	1.96
17.333	0.00	0.65	1.520	o	|	|	|	|	1.95
17.417	0.00	0.64	1.516	o	|	|	|	|	1.94
17.500	0.00	0.64	1.511	o	|	|	|	|	1.94
17.583	0.00	0.64	1.507	o	|	|	|	|	1.93
17.667	0.00	0.64	1.503	o	|	|	|	|	1.93
17.750	0.00	0.63	1.498	o	|	|	|	|	1.92
17.833	0.00	0.63	1.494	o	|	|	|	|	1.92
17.917	0.00	0.63	1.490	o	|	|	|	|	1.91
18.000	0.00	0.63	1.485	o	|	|	|	|	1.91
18.083	0.00	0.62	1.481	o	|	|	|	|	1.90
18.167	0.00	0.62	1.477	o	|	|	|	|	1.90
18.250	0.00	0.62	1.472	o	|	|	|	|	1.89
18.333	0.00	0.62	1.468	o	|	|	|	|	1.89
18.417	0.00	0.61	1.464	o	|	|	|	|	1.88
18.500	0.00	0.61	1.460	o	|	|	|	|	1.88
18.583	0.00	0.61	1.456	o	|	|	|	|	1.87
18.667	0.00	0.61	1.451	o	|	|	|	|	1.87
18.750	0.00	0.61	1.447	o	|	|	|	|	1.86
18.833	0.00	0.60	1.443	o	|	|	|	|	1.86
18.917	0.00	0.60	1.439	o	|	|	|	|	1.85
19.000	0.00	0.60	1.435	o	|	|	|	|	1.85
19.083	0.00	0.60	1.431	o	|	|	|	|	1.84
19.167	0.00	0.59	1.426	o	|	|	|	|	1.84
19.250	0.00	0.59	1.422	o	|	|	|	|	1.83
19.333	0.00	0.59	1.418	o	|	|	|	|	1.83
19.417	0.00	0.59	1.414	o	|	|	|	|	1.82
19.500	0.00	0.59	1.410	o	|	|	|	|	1.82
19.583	0.00	0.58	1.406	o	|	|	|	|	1.81
19.667	0.00	0.58	1.402	o	|	|	|	|	1.81
19.750	0.00	0.58	1.398	o	|	|	|	|	1.80
19.833	0.00	0.58	1.394	o	|	|	|	|	1.80
19.917	0.00	0.57	1.390	o	|	|	|	|	1.79
20.000	0.00	0.57	1.386	o	|	|	|	|	1.79
20.083	0.00	0.57	1.382	o	|	|	|	|	1.78
20.167	0.00	0.57	1.379	o	|	|	|	|	1.78
20.250	0.00	0.57	1.375	o	|	|	|	|	1.77
20.333	0.00	0.56	1.371	o	|	|	|	|	1.77
20.417	0.00	0.56	1.367	o	|	|	|	|	1.76
20.500	0.00	0.56	1.363	o	|	|	|	|	1.76
20.583	0.00	0.56	1.359	o	|	|	|	|	1.75
20.667	0.00	0.55	1.355	o	|	|	|	|	1.75
20.750	0.00	0.55	1.351	o	|	|	|	|	1.74
20.833	0.00	0.55	1.348	o	|	|	|	|	1.74
20.917	0.00	0.55	1.344	o	|	|	|	|	1.73
21.000	0.00	0.55	1.340	o	|	|	|	|	1.73
21.083	0.00	0.54	1.336	o	|	|	|	|	1.73
21.167	0.00	0.54	1.333	o	|	|	|	|	1.72
21.250	0.00	0.54	1.329	o	|	|	|	|	1.72
21.333	0.00	0.54	1.325	o	|	|	|	|	1.71
21.417	0.00	0.54	1.321	o	|	|	|	|	1.71
21.500	0.00	0.53	1.318	o	|	|	|	|	1.70
21.583	0.00	0.53	1.314	o	|	|	|	|	1.70
21.667	0.00	0.53	1.310	o	|	|	|	|	1.69
21.750	0.00	0.53	1.307	o	|	|	|	|	1.69
21.833	0.00	0.53	1.303	o	|	|	|	|	1.68
21.917	0.00	0.52	1.300	o	|	|	|	|	1.68
22.000	0.00	0.52	1.296	o	|	|	|	|	1.68
22.083	0.00	0.52	1.292	o	|	|	|	|	1.67
22.167	0.00	0.52	1.289	o	|	|	|	|	1.67
22.250	0.00	0.52	1.285	o	|	|	|	|	1.66
22.333	0.00	0.51	1.282	o	|	|	|	|	1.66
22.417	0.00	0.51	1.278	o	|	|	|	|	1.65
22.500	0.00	0.51	1.275	o	|	|	|	|	1.65
22.583	0.00	0.51	1.271	o	|	|	|	|	1.65
22.667	0.00	0.51	1.268	o	|	|	|	|	1.64
22.750	0.00	0.50	1.264	o	|	|	|	|	1.64
22.833	0.00	0.50	1.261	o	|	|	|	|	1.63
22.917	0.00	0.50	1.257	o	|	|	|	|	1.63
23.000	0.00	0.50	1.254	o	|	|	|	|	1.62
23.083	0.00	0.50	1.250	o	|	|	|	|	1.62
23.167	0.00	0.50	1.247	o	|	|	|	|	1.62
23.250	0.00	0.49	1.244	o	|	|	|	|	1.61

23.333	0.00	0.49	1.240	o	|	|	|	|	1.61
23.417	0.00	0.49	1.237	o	|	|	|	|	1.60
23.500	0.00	0.49	1.233	o	|	|	|	|	1.60
23.583	0.00	0.49	1.230	o	|	|	|	|	1.60
23.667	0.00	0.48	1.227	o	|	|	|	|	1.59
23.750	0.00	0.48	1.223	o	|	|	|	|	1.59
23.833	0.00	0.48	1.220	o	|	|	|	|	1.58
23.917	0.00	0.48	1.217	o	|	|	|	|	1.58
24.000	0.00	0.48	1.213	o	|	|	|	|	1.58
24.083	0.00	0.48	1.210	o	|	|	|	|	1.57
24.167	0.00	0.47	1.207	o	|	|	|	|	1.57
24.250	0.00	0.47	1.204	o	|	|	|	|	1.56
24.333	0.00	0.47	1.200	o	|	|	|	|	1.56
24.417	0.00	0.47	1.197	o	|	|	|	|	1.56
24.500	0.00	0.47	1.194	o	|	|	|	|	1.55
24.583	0.00	0.46	1.191	o	|	|	|	|	1.55
24.667	0.00	0.46	1.188	o	|	|	|	|	1.54
24.750	0.00	0.46	1.184	o	|	|	|	|	1.54
24.833	0.00	0.46	1.181	o	|	|	|	|	1.54
24.917	0.00	0.46	1.178	o	|	|	|	|	1.53
25.000	0.00	0.46	1.175	o	|	|	|	|	1.53
25.083	0.00	0.45	1.172	o	|	|	|	|	1.52
25.167	0.00	0.45	1.169	o	|	|	|	|	1.52
25.250	0.00	0.45	1.166	o	|	|	|	|	1.52
25.333	0.00	0.45	1.162	o	|	|	|	|	1.51
25.417	0.00	0.45	1.159	o	|	|	|	|	1.51
25.500	0.00	0.45	1.156	o	|	|	|	|	1.51
25.583	0.00	0.44	1.153	o	|	|	|	|	1.50
25.667	0.00	0.44	1.150	o	|	|	|	|	1.50
25.750	0.00	0.44	1.147	o	|	|	|	|	1.49
25.833	0.00	0.44	1.144	o	|	|	|	|	1.49
25.917	0.00	0.44	1.141	o	|	|	|	|	1.49
26.000	0.00	0.44	1.138	o	|	|	|	|	1.48
26.083	0.00	0.43	1.135	o	|	|	|	|	1.48
26.167	0.00	0.43	1.132	o	|	|	|	|	1.48
26.250	0.00	0.43	1.129	o	|	|	|	|	1.47
26.333	0.00	0.43	1.126	o	|	|	|	|	1.47
26.417	0.00	0.43	1.123	o	|	|	|	|	1.46
26.500	0.00	0.43	1.120	o	|	|	|	|	1.46
26.583	0.00	0.42	1.117	o	|	|	|	|	1.46
26.667	0.00	0.42	1.115	o	|	|	|	|	1.45
26.750	0.00	0.42	1.112	o	|	|	|	|	1.45
26.833	0.00	0.42	1.109	o	|	|	|	|	1.45
26.917	0.00	0.42	1.106	o	|	|	|	|	1.44
27.000	0.00	0.42	1.103	o	|	|	|	|	1.44
27.083	0.00	0.41	1.100	o	|	|	|	|	1.44
27.167	0.00	0.41	1.097	o	|	|	|	|	1.43
27.250	0.00	0.41	1.094	o	|	|	|	|	1.43
27.333	0.00	0.41	1.092	o	|	|	|	|	1.43
27.417	0.00	0.41	1.089	o	|	|	|	|	1.42
27.500	0.00	0.41	1.086	o	|	|	|	|	1.42
27.583	0.00	0.41	1.083	o	|	|	|	|	1.42
27.667	0.00	0.40	1.080	o	|	|	|	|	1.41
27.750	0.00	0.40	1.078	o	|	|	|	|	1.41
27.833	0.00	0.40	1.075	o	|	|	|	|	1.41
27.917	0.00	0.40	1.072	o	|	|	|	|	1.40
28.000	0.00	0.40	1.069	o	|	|	|	|	1.40
28.083	0.00	0.40	1.067	o	|	|	|	|	1.40
28.167	0.00	0.39	1.064	o	|	|	|	|	1.39
28.250	0.00	0.39	1.061	o	|	|	|	|	1.39
28.333	0.00	0.39	1.058	o	|	|	|	|	1.39
28.417	0.00	0.39	1.056	o	|	|	|	|	1.38
28.500	0.00	0.39	1.053	o	|	|	|	|	1.38
28.583	0.00	0.39	1.050	o	|	|	|	|	1.38
28.667	0.00	0.39	1.048	o	|	|	|	|	1.37
28.750	0.00	0.38	1.045	o	|	|	|	|	1.37
28.833	0.00	0.38	1.042	o	|	|	|	|	1.37
28.917	0.00	0.38	1.040	o	|	|	|	|	1.36
29.000	0.00	0.38	1.037	o	|	|	|	|	1.36
29.083	0.00	0.38	1.035	o	|	|	|	|	1.36
29.167	0.00	0.38	1.032	o	|	|	|	|	1.35
29.250	0.00	0.38	1.029	o	|	|	|	|	1.35
29.333	0.00	0.37	1.027	o	|	|	|	|	1.35
29.417	0.00	0.37	1.024	o	|	|	|	|	1.34
29.500	0.00	0.37	1.022	o	|	|	|	|	1.34
29.583	0.00	0.37	1.019	o	|	|	|	|	1.34
29.667	0.00	0.37	1.017	o	|	|	|	|	1.33
29.750	0.00	0.37	1.014	o	|	|	|	|	1.33
29.833	0.00	0.37	1.012	o	|	|	|	|	1.33
29.917	0.00	0.36	1.009	o	|	|	|	|	1.33
30.000	0.00	0.36	1.007	o	|	|	|	|	1.32
30.083	0.00	0.36	1.004	o	|	|	|	|	1.32
30.167	0.00	0.36	1.002	o	|	|	|	|	1.32
30.250	0.00	0.36	0.999	o	|	|	|	|	1.31
30.333	0.00	0.36	0.997	o	|	|	|	|	1.31
30.417	0.00	0.36	0.994	o	|	|	|	|	1.31

30.500	0.00	0.35	0.992	o	|	|	|	|	1.30
30.583	0.00	0.35	0.989	o	|	|	|	|	1.30
30.667	0.00	0.35	0.987	o	|	|	|	|	1.30
30.750	0.00	0.35	0.984	o	|	|	|	|	1.30
30.833	0.00	0.35	0.982	o	|	|	|	|	1.29
30.917	0.00	0.35	0.980	o	|	|	|	|	1.29
31.000	0.00	0.35	0.977	o	|	|	|	|	1.29
31.083	0.00	0.35	0.975	o	|	|	|	|	1.28
31.167	0.00	0.34	0.972	o	|	|	|	|	1.28
31.250	0.00	0.34	0.970	o	|	|	|	|	1.28
31.333	0.00	0.34	0.968	o	|	|	|	|	1.27
31.417	0.00	0.34	0.965	o	|	|	|	|	1.27
31.500	0.00	0.34	0.963	o	|	|	|	|	1.27
31.583	0.00	0.34	0.961	o	|	|	|	|	1.27
31.667	0.00	0.34	0.958	o	|	|	|	|	1.26
31.750	0.00	0.34	0.956	o	|	|	|	|	1.26
31.833	0.00	0.33	0.954	o	|	|	|	|	1.26
31.917	0.00	0.33	0.951	o	|	|	|	|	1.25
32.000	0.00	0.33	0.949	o	|	|	|	|	1.25
32.083	0.00	0.33	0.947	o	|	|	|	|	1.25
32.167	0.00	0.33	0.945	o	|	|	|	|	1.25
32.250	0.00	0.33	0.942	o	|	|	|	|	1.24
32.333	0.00	0.33	0.940	o	|	|	|	|	1.24
32.417	0.00	0.33	0.938	o	|	|	|	|	1.24
32.500	0.00	0.32	0.936	o	|	|	|	|	1.24
32.583	0.00	0.32	0.933	o	|	|	|	|	1.23
32.667	0.00	0.32	0.931	o	|	|	|	|	1.23
32.750	0.00	0.32	0.929	o	|	|	|	|	1.23
32.833	0.00	0.32	0.927	o	|	|	|	|	1.22
32.917	0.00	0.32	0.925	o	|	|	|	|	1.22
33.000	0.00	0.32	0.922	o	|	|	|	|	1.22
33.083	0.00	0.32	0.920	o	|	|	|	|	1.22
33.167	0.00	0.31	0.918	o	|	|	|	|	1.21
33.250	0.00	0.31	0.916	o	|	|	|	|	1.21
33.333	0.00	0.31	0.914	o	|	|	|	|	1.21
33.417	0.00	0.31	0.912	o	|	|	|	|	1.21
33.500	0.00	0.31	0.909	o	|	|	|	|	1.20
33.583	0.00	0.31	0.907	o	|	|	|	|	1.20
33.667	0.00	0.31	0.905	o	|	|	|	|	1.20
33.750	0.00	0.31	0.903	o	|	|	|	|	1.20
33.833	0.00	0.30	0.901	o	|	|	|	|	1.19
33.917	0.00	0.30	0.899	o	|	|	|	|	1.19
34.000	0.00	0.30	0.897	o	|	|	|	|	1.19
34.083	0.00	0.30	0.895	o	|	|	|	|	1.19
34.167	0.00	0.30	0.893	o	|	|	|	|	1.18
34.250	0.00	0.30	0.891	o	|	|	|	|	1.18
34.333	0.00	0.30	0.889	o	|	|	|	|	1.18
34.417	0.00	0.30	0.887	o	|	|	|	|	1.18
34.500	0.00	0.30	0.884	o	|	|	|	|	1.17
34.583	0.00	0.29	0.882	o	|	|	|	|	1.17
34.667	0.00	0.29	0.880	o	|	|	|	|	1.17
34.750	0.00	0.29	0.878	o	|	|	|	|	1.17
34.833	0.00	0.29	0.876	o	|	|	|	|	1.16
34.917	0.00	0.29	0.874	o	|	|	|	|	1.16
35.000	0.00	0.29	0.872	o	|	|	|	|	1.16
35.083	0.00	0.29	0.870	o	|	|	|	|	1.16
35.167	0.00	0.29	0.868	o	|	|	|	|	1.15
35.250	0.00	0.29	0.866	o	|	|	|	|	1.15
35.333	0.00	0.28	0.864	o	|	|	|	|	1.15
35.417	0.00	0.28	0.863	o	|	|	|	|	1.15
35.500	0.00	0.28	0.861	o	|	|	|	|	1.14
35.583	0.00	0.28	0.859	o	|	|	|	|	1.14
35.667	0.00	0.28	0.857	o	|	|	|	|	1.14
35.750	0.00	0.28	0.855	o	|	|	|	|	1.14
35.833	0.00	0.28	0.853	o	|	|	|	|	1.13
35.917	0.00	0.28	0.851	o	|	|	|	|	1.13
36.000	0.00	0.28	0.849	o	|	|	|	|	1.13
36.083	0.00	0.28	0.847	o	|	|	|	|	1.13
36.167	0.00	0.27	0.845	o	|	|	|	|	1.12
36.250	0.00	0.27	0.843	o	|	|	|	|	1.12
36.333	0.00	0.27	0.841	o	|	|	|	|	1.12
36.417	0.00	0.27	0.840	o	|	|	|	|	1.12
36.500	0.00	0.27	0.838	o	|	|	|	|	1.12
36.583	0.00	0.27	0.836	o	|	|	|	|	1.11
36.667	0.00	0.27	0.834	o	|	|	|	|	1.11
36.750	0.00	0.27	0.832	o	|	|	|	|	1.11
36.833	0.00	0.27	0.830	o	|	|	|	|	1.11
36.917	0.00	0.27	0.829	o	|	|	|	|	1.10
37.000	0.00	0.26	0.827	o	|	|	|	|	1.10
37.083	0.00	0.26	0.825	o	|	|	|	|	1.10
37.167	0.00	0.26	0.823	o	|	|	|	|	1.10
37.250	0.00	0.26	0.821	o	|	|	|	|	1.10
37.333	0.00	0.26	0.819	o	|	|	|	|	1.09
37.417	0.00	0.26	0.818	o	|	|	|	|	1.09
37.500	0.00	0.26	0.816	o	|	|	|	|	1.09
37.583	0.00	0.26	0.814	o	|	|	|	|	1.09

37.667	0.00	0.26	0.812	o	|	|	|	|	1.08
37.750	0.00	0.26	0.811	o	|	|	|	|	1.08
37.833	0.00	0.25	0.809	o	|	|	|	|	1.08
37.917	0.00	0.25	0.807	o	|	|	|	|	1.08
38.000	0.00	0.25	0.805	o	|	|	|	|	1.08
38.083	0.00	0.25	0.804	o	|	|	|	|	1.07
38.167	0.00	0.25	0.802	o	|	|	|	|	1.07
38.250	0.00	0.25	0.800	o	|	|	|	|	1.07
38.333	0.00	0.25	0.798	o	|	|	|	|	1.07
38.417	0.00	0.25	0.797	o	|	|	|	|	1.07
38.500	0.00	0.25	0.795	o	|	|	|	|	1.06
38.583	0.00	0.25	0.793	o	|	|	|	|	1.06
38.667	0.00	0.24	0.792	o	|	|	|	|	1.06
38.750	0.00	0.24	0.790	o	|	|	|	|	1.06
38.833	0.00	0.24	0.788	o	|	|	|	|	1.06
38.917	0.00	0.24	0.787	o	|	|	|	|	1.05
39.000	0.00	0.24	0.785	o	|	|	|	|	1.05
39.083	0.00	0.24	0.783	o	|	|	|	|	1.05
39.167	0.00	0.24	0.782	o	|	|	|	|	1.05
39.250	0.00	0.24	0.780	o	|	|	|	|	1.05
39.333	0.00	0.24	0.778	o	|	|	|	|	1.04
39.417	0.00	0.24	0.777	o	|	|	|	|	1.04
39.500	0.00	0.24	0.775	o	|	|	|	|	1.04
39.583	0.00	0.23	0.774	o	|	|	|	|	1.04
39.667	0.00	0.23	0.772	o	|	|	|	|	1.04
39.750	0.00	0.23	0.770	o	|	|	|	|	1.03
39.833	0.00	0.23	0.769	o	|	|	|	|	1.03
39.917	0.00	0.23	0.767	o	|	|	|	|	1.03
40.000	0.00	0.23	0.765	o	|	|	|	|	1.03
40.083	0.00	0.23	0.764	o	|	|	|	|	1.03
40.167	0.00	0.23	0.762	o	|	|	|	|	1.02
40.250	0.00	0.23	0.761	o	|	|	|	|	1.02
40.333	0.00	0.23	0.759	o	|	|	|	|	1.02
40.417	0.00	0.23	0.758	o	|	|	|	|	1.02
40.500	0.00	0.23	0.756	o	|	|	|	|	1.02
40.583	0.00	0.22	0.755	o	|	|	|	|	1.01
40.667	0.00	0.22	0.753	o	|	|	|	|	1.01
40.750	0.00	0.22	0.751	o	|	|	|	|	1.01
40.833	0.00	0.22	0.750	o	|	|	|	|	1.01
40.917	0.00	0.22	0.748	o	|	|	|	|	1.01
41.000	0.00	0.22	0.747	o	|	|	|	|	1.00
41.083	0.00	0.22	0.745	o	|	|	|	|	1.00
41.167	0.00	0.22	0.744	o	|	|	|	|	1.00
41.250	0.00	0.22	0.742	o	|	|	|	|	1.00
41.333	0.00	0.22	0.741	o	|	|	|	|	1.00
41.417	0.00	0.22	0.739	o	|	|	|	|	1.00
41.500	0.00	0.22	0.738	o	|	|	|	|	0.99
41.583	0.00	0.22	0.736	o	|	|	|	|	0.99
41.667	0.00	0.22	0.735	o	|	|	|	|	0.99
41.750	0.00	0.22	0.733	o	|	|	|	|	0.99
41.833	0.00	0.21	0.732	o	|	|	|	|	0.99
41.917	0.00	0.21	0.730	o	|	|	|	|	0.98
42.000	0.00	0.21	0.729	o	|	|	|	|	0.98
42.083	0.00	0.21	0.728	o	|	|	|	|	0.98
42.167	0.00	0.21	0.726	o	|	|	|	|	0.98
42.250	0.00	0.21	0.725	o	|	|	|	|	0.98
42.333	0.00	0.21	0.723	o	|	|	|	|	0.97
42.417	0.00	0.21	0.722	o	|	|	|	|	0.97
42.500	0.00	0.21	0.720	o	|	|	|	|	0.97
42.583	0.00	0.21	0.719	o	|	|	|	|	0.97
42.667	0.00	0.21	0.717	o	|	|	|	|	0.97
42.750	0.00	0.21	0.716	o	|	|	|	|	0.96
42.833	0.00	0.21	0.714	o	|	|	|	|	0.96
42.917	0.00	0.21	0.713	o	|	|	|	|	0.96
43.000	0.00	0.21	0.712	o	|	|	|	|	0.96
43.083	0.00	0.21	0.710	o	|	|	|	|	0.96
43.167	0.00	0.21	0.709	o	|	|	|	|	0.95
43.250	0.00	0.21	0.707	o	|	|	|	|	0.95
43.333	0.00	0.21	0.706	o	|	|	|	|	0.95
43.417	0.00	0.21	0.704	o	|	|	|	|	0.95
43.500	0.00	0.21	0.703	o	|	|	|	|	0.95
43.583	0.00	0.21	0.702	o	|	|	|	|	0.94
43.667	0.00	0.21	0.700	o	|	|	|	|	0.94
43.750	0.00	0.20	0.699	o	|	|	|	|	0.94
43.833	0.00	0.20	0.697	o	|	|	|	|	0.94
43.917	0.00	0.20	0.696	o	|	|	|	|	0.94
44.000	0.00	0.20	0.694	o	|	|	|	|	0.93
44.083	0.00	0.20	0.693	o	|	|	|	|	0.93
44.167	0.00	0.20	0.692	o	|	|	|	|	0.93
44.250	0.00	0.20	0.690	o	|	|	|	|	0.93
44.333	0.00	0.20	0.689	o	|	|	|	|	0.93
44.417	0.00	0.20	0.687	o	|	|	|	|	0.93
44.500	0.00	0.20	0.686	o	|	|	|	|	0.92
44.583	0.00	0.20	0.685	o	|	|	|	|	0.92
44.667	0.00	0.20	0.683	o	|	|	|	|	0.92
44.750	0.00	0.20	0.682	o	|	|	|	|	0.92

44.833	0.00	0.20	0.681	o	|	|	|	|	0.92
44.917	0.00	0.20	0.679	o	|	|	|	|	0.91
45.000	0.00	0.20	0.678	o	|	|	|	|	0.91
45.083	0.00	0.20	0.676	o	|	|	|	|	0.91
45.167	0.00	0.20	0.675	o	|	|	|	|	0.91
45.250	0.00	0.20	0.674	o	|	|	|	|	0.91
45.333	0.00	0.20	0.672	o	|	|	|	|	0.90
45.417	0.00	0.20	0.671	o	|	|	|	|	0.90
45.500	0.00	0.20	0.670	o	|	|	|	|	0.90
45.583	0.00	0.20	0.668	o	|	|	|	|	0.90
45.667	0.00	0.20	0.667	o	|	|	|	|	0.90
45.750	0.00	0.20	0.666	o	|	|	|	|	0.90
45.833	0.00	0.19	0.664	o	|	|	|	|	0.89
45.917	0.00	0.19	0.663	o	|	|	|	|	0.89
46.000	0.00	0.19	0.662	o	|	|	|	|	0.89
46.083	0.00	0.19	0.660	o	|	|	|	|	0.89
46.167	0.00	0.19	0.659	o	|	|	|	|	0.89
46.250	0.00	0.19	0.658	o	|	|	|	|	0.89
46.333	0.00	0.19	0.656	o	|	|	|	|	0.88
46.417	0.00	0.19	0.655	o	|	|	|	|	0.88
46.500	0.00	0.19	0.654	o	|	|	|	|	0.88
46.583	0.00	0.19	0.652	o	|	|	|	|	0.88
46.667	0.00	0.19	0.651	o	|	|	|	|	0.88
46.750	0.00	0.19	0.650	o	|	|	|	|	0.87
46.833	0.00	0.19	0.648	o	|	|	|	|	0.87
46.917	0.00	0.19	0.647	o	|	|	|	|	0.87
47.000	0.00	0.19	0.646	o	|	|	|	|	0.87
47.083	0.00	0.19	0.644	o	|	|	|	|	0.87
47.167	0.00	0.19	0.643	o	|	|	|	|	0.87
47.250	0.00	0.19	0.642	o	|	|	|	|	0.86
47.333	0.00	0.19	0.641	o	|	|	|	|	0.86
47.417	0.00	0.19	0.639	o	|	|	|	|	0.86
47.500	0.00	0.19	0.638	o	|	|	|	|	0.86
47.583	0.00	0.19	0.637	o	|	|	|	|	0.86
47.667	0.00	0.19	0.635	o	|	|	|	|	0.86
47.750	0.00	0.19	0.634	o	|	|	|	|	0.85
47.833	0.00	0.19	0.633	o	|	|	|	|	0.85
47.917	0.00	0.19	0.632	o	|	|	|	|	0.85
48.000	0.00	0.18	0.630	o	|	|	|	|	0.85
48.083	0.00	0.18	0.629	o	|	|	|	|	0.85
48.167	0.00	0.18	0.628	o	|	|	|	|	0.84
48.250	0.00	0.18	0.626	o	|	|	|	|	0.84
48.333	0.00	0.18	0.625	o	|	|	|	|	0.84
48.417	0.00	0.18	0.624	o	|	|	|	|	0.84
48.500	0.00	0.18	0.623	o	|	|	|	|	0.84
48.583	0.00	0.18	0.621	o	|	|	|	|	0.84
48.667	0.00	0.18	0.620	o	|	|	|	|	0.83
48.750	0.00	0.18	0.619	o	|	|	|	|	0.83
48.833	0.00	0.18	0.618	o	|	|	|	|	0.83
48.917	0.00	0.18	0.616	o	|	|	|	|	0.83
49.000	0.00	0.18	0.615	o	|	|	|	|	0.83
49.083	0.00	0.18	0.614	o	|	|	|	|	0.83
49.167	0.00	0.18	0.613	o	|	|	|	|	0.82
49.250	0.00	0.18	0.611	o	|	|	|	|	0.82
49.333	0.00	0.18	0.610	o	|	|	|	|	0.82
49.417	0.00	0.18	0.609	o	|	|	|	|	0.82
49.500	0.00	0.18	0.608	o	|	|	|	|	0.82
49.583	0.00	0.18	0.607	o	|	|	|	|	0.82
49.667	0.00	0.18	0.605	o	|	|	|	|	0.81
49.750	0.00	0.18	0.604	o	|	|	|	|	0.81
49.833	0.00	0.18	0.603	o	|	|	|	|	0.81
49.917	0.00	0.18	0.602	o	|	|	|	|	0.81
50.000	0.00	0.18	0.600	o	|	|	|	|	0.81
50.083	0.00	0.18	0.599	o	|	|	|	|	0.81
50.167	0.00	0.18	0.598	o	|	|	|	|	0.80
50.250	0.00	0.18	0.597	o	|	|	|	|	0.80
50.333	0.00	0.17	0.596	o	|	|	|	|	0.80
50.417	0.00	0.17	0.594	o	|	|	|	|	0.80
50.500	0.00	0.17	0.593	o	|	|	|	|	0.80
50.583	0.00	0.17	0.592	o	|	|	|	|	0.80
50.667	0.00	0.17	0.591	o	|	|	|	|	0.80
50.750	0.00	0.17	0.590	o	|	|	|	|	0.79
50.833	0.00	0.17	0.588	o	|	|	|	|	0.79
50.917	0.00	0.17	0.587	o	|	|	|	|	0.79
51.000	0.00	0.17	0.586	o	|	|	|	|	0.79
51.083	0.00	0.17	0.585	o	|	|	|	|	0.79
51.167	0.00	0.17	0.584	o	|	|	|	|	0.79
51.250	0.00	0.17	0.583	o	|	|	|	|	0.78
51.333	0.00	0.17	0.581	o	|	|	|	|	0.78
51.417	0.00	0.17	0.580	o	|	|	|	|	0.78
51.500	0.00	0.17	0.579	o	|	|	|	|	0.78
51.583	0.00	0.17	0.578	o	|	|	|	|	0.78
51.667	0.00	0.17	0.577	o	|	|	|	|	0.78
51.750	0.00	0.17	0.575	o	|	|	|	|	0.77
51.833	0.00	0.17	0.574	o	|	|	|	|	0.77
51.917	0.00	0.17	0.573	o	|	|	|	|	0.77

52.000	0.00	0.17	0.572	o	|	|	|	|	0.77
52.083	0.00	0.17	0.571	o	|	|	|	|	0.77
52.167	0.00	0.17	0.570	o	|	|	|	|	0.77
52.250	0.00	0.17	0.569	o	|	|	|	|	0.77
52.333	0.00	0.17	0.567	o	|	|	|	|	0.76
52.417	0.00	0.17	0.566	o	|	|	|	|	0.76
52.500	0.00	0.17	0.565	o	|	|	|	|	0.76
52.583	0.00	0.17	0.564	o	|	|	|	|	0.76
52.667	0.00	0.17	0.563	o	|	|	|	|	0.76
52.750	0.00	0.16	0.562	o	|	|	|	|	0.76
52.833	0.00	0.16	0.561	o	|	|	|	|	0.75
52.917	0.00	0.16	0.559	o	|	|	|	|	0.75
53.000	0.00	0.16	0.558	o	|	|	|	|	0.75
53.083	0.00	0.16	0.557	o	|	|	|	|	0.75
53.167	0.00	0.16	0.556	o	|	|	|	|	0.75
53.250	0.00	0.16	0.555	o	|	|	|	|	0.75
53.333	0.00	0.16	0.554	o	|	|	|	|	0.75
53.417	0.00	0.16	0.553	o	|	|	|	|	0.74
53.500	0.00	0.16	0.552	o	|	|	|	|	0.74
53.583	0.00	0.16	0.550	o	|	|	|	|	0.74
53.667	0.00	0.16	0.549	o	|	|	|	|	0.74
53.750	0.00	0.16	0.548	o	|	|	|	|	0.74
53.833	0.00	0.16	0.547	o	|	|	|	|	0.74
53.917	0.00	0.16	0.546	o	|	|	|	|	0.73
54.000	0.00	0.16	0.545	o	|	|	|	|	0.73
54.083	0.00	0.16	0.544	o	|	|	|	|	0.73
54.167	0.00	0.16	0.543	o	|	|	|	|	0.73
54.250	0.00	0.16	0.542	o	|	|	|	|	0.73
54.333	0.00	0.16	0.541	o	|	|	|	|	0.73
54.417	0.00	0.16	0.539	o	|	|	|	|	0.73
54.500	0.00	0.16	0.538	o	|	|	|	|	0.72
54.583	0.00	0.16	0.537	o	|	|	|	|	0.72
54.667	0.00	0.16	0.536	o	|	|	|	|	0.72
54.750	0.00	0.16	0.535	o	|	|	|	|	0.72
54.833	0.00	0.16	0.534	o	|	|	|	|	0.72
54.917	0.00	0.16	0.533	o	|	|	|	|	0.72
55.000	0.00	0.16	0.532	o	|	|	|	|	0.72
55.083	0.00	0.16	0.531	o	|	|	|	|	0.71
55.167	0.00	0.16	0.530	o	|	|	|	|	0.71
55.250	0.00	0.16	0.529	o	|	|	|	|	0.71
55.333	0.00	0.15	0.528	o	|	|	|	|	0.71
55.417	0.00	0.15	0.527	o	|	|	|	|	0.71
55.500	0.00	0.15	0.525	o	|	|	|	|	0.71
55.583	0.00	0.15	0.524	o	|	|	|	|	0.71
55.667	0.00	0.15	0.523	o	|	|	|	|	0.70
55.750	0.00	0.15	0.522	o	|	|	|	|	0.70
55.833	0.00	0.15	0.521	o	|	|	|	|	0.70
55.917	0.00	0.15	0.520	o	|	|	|	|	0.70
56.000	0.00	0.15	0.519	o	|	|	|	|	0.70
56.083	0.00	0.15	0.518	o	|	|	|	|	0.70
56.167	0.00	0.15	0.517	o	|	|	|	|	0.70
56.250	0.00	0.15	0.516	o	|	|	|	|	0.69
56.333	0.00	0.15	0.515	o	|	|	|	|	0.69
56.417	0.00	0.15	0.514	o	|	|	|	|	0.69
56.500	0.00	0.15	0.513	o	|	|	|	|	0.69
56.583	0.00	0.15	0.512	o	|	|	|	|	0.69
56.667	0.00	0.15	0.511	o	|	|	|	|	0.69
56.750	0.00	0.15	0.510	o	|	|	|	|	0.69
56.833	0.00	0.15	0.509	o	|	|	|	|	0.68
56.917	0.00	0.15	0.508	o	|	|	|	|	0.68
57.000	0.00	0.15	0.507	o	|	|	|	|	0.68
57.083	0.00	0.15	0.506	o	|	|	|	|	0.68
57.167	0.00	0.15	0.505	o	|	|	|	|	0.68
57.250	0.00	0.15	0.504	o	|	|	|	|	0.68
57.333	0.00	0.15	0.503	o	|	|	|	|	0.68
57.417	0.00	0.15	0.502	o	|	|	|	|	0.68
57.500	0.00	0.15	0.501	o	|	|	|	|	0.67
57.583	0.00	0.15	0.500	o	|	|	|	|	0.67
57.667	0.00	0.15	0.499	o	|	|	|	|	0.67
57.750	0.00	0.15	0.498	o	|	|	|	|	0.67
57.833	0.00	0.15	0.497	o	|	|	|	|	0.67
57.917	0.00	0.15	0.496	o	|	|	|	|	0.67
58.000	0.00	0.15	0.495	o	|	|	|	|	0.67
58.083	0.00	0.14	0.494	o	|	|	|	|	0.66
58.167	0.00	0.14	0.493	o	|	|	|	|	0.66
58.250	0.00	0.14	0.492	o	|	|	|	|	0.66
58.333	0.00	0.14	0.491	o	|	|	|	|	0.66
58.417	0.00	0.14	0.490	o	|	|	|	|	0.66
58.500	0.00	0.14	0.489	o	|	|	|	|	0.66
58.583	0.00	0.14	0.488	o	|	|	|	|	0.66
58.667	0.00	0.14	0.487	o	|	|	|	|	0.65
58.750	0.00	0.14	0.486	o	|	|	|	|	0.65
58.833	0.00	0.14	0.485	o	|	|	|	|	0.65
58.917	0.00	0.14	0.484	o	|	|	|	|	0.65
59.000	0.00	0.14	0.483	o	|	|	|	|	0.65
59.083	0.00	0.14	0.482	o	|	|	|	|	0.65

59.167	0.00	0.14	0.481	o	|	|	|	0.65
59.250	0.00	0.14	0.480	o	|	|	|	0.65
59.333	0.00	0.14	0.479	o	|	|	|	0.64
59.417	0.00	0.14	0.478	o	|	|	|	0.64
59.500	0.00	0.14	0.477	o	|	|	|	0.64
59.583	0.00	0.14	0.476	o	|	|	|	0.64
59.667	0.00	0.14	0.475	o	|	|	|	0.64
59.750	0.00	0.14	0.474	o	|	|	|	0.64
59.833	0.00	0.14	0.473	o	|	|	|	0.64
59.917	0.00	0.14	0.472	o	|	|	|	0.64
60.000	0.00	0.14	0.471	o	|	|	|	0.63
60.083	0.00	0.14	0.470	o	|	|	|	0.63
60.167	0.00	0.14	0.469	o	|	|	|	0.63
60.250	0.00	0.14	0.468	o	|	|	|	0.63
60.333	0.00	0.14	0.467	o	|	|	|	0.63
60.417	0.00	0.14	0.466	o	|	|	|	0.63
60.500	0.00	0.14	0.465	o	|	|	|	0.63
60.583	0.00	0.14	0.465	o	|	|	|	0.63
60.667	0.00	0.14	0.464	o	|	|	|	0.62
60.750	0.00	0.14	0.463	o	|	|	|	0.62
60.833	0.00	0.14	0.462	o	|	|	|	0.62
60.917	0.00	0.14	0.461	o	|	|	|	0.62
61.000	0.00	0.13	0.460	o	|	|	|	0.62
61.083	0.00	0.13	0.459	o	|	|	|	0.62
61.167	0.00	0.13	0.458	o	|	|	|	0.62
61.250	0.00	0.13	0.457	o	|	|	|	0.62
61.333	0.00	0.13	0.456	o	|	|	|	0.61
61.417	0.00	0.13	0.455	o	|	|	|	0.61
61.500	0.00	0.13	0.454	o	|	|	|	0.61
61.583	0.00	0.13	0.453	o	|	|	|	0.61
61.667	0.00	0.13	0.452	o	|	|	|	0.61
61.750	0.00	0.13	0.452	o	|	|	|	0.61
61.833	0.00	0.13	0.451	o	|	|	|	0.61
61.917	0.00	0.13	0.450	o	|	|	|	0.61
62.000	0.00	0.13	0.449	o	|	|	|	0.60
62.083	0.00	0.13	0.448	o	|	|	|	0.60
62.167	0.00	0.13	0.447	o	|	|	|	0.60
62.250	0.00	0.13	0.446	o	|	|	|	0.60
62.333	0.00	0.13	0.445	o	|	|	|	0.60
62.417	0.00	0.13	0.444	o	|	|	|	0.60
62.500	0.00	0.13	0.443	o	|	|	|	0.60
62.583	0.00	0.13	0.443	o	|	|	|	0.60
62.667	0.00	0.13	0.442	o	|	|	|	0.59
62.750	0.00	0.13	0.441	o	|	|	|	0.59
62.833	0.00	0.13	0.440	o	|	|	|	0.59
62.917	0.00	0.13	0.439	o	|	|	|	0.59
63.000	0.00	0.13	0.438	o	|	|	|	0.59
63.083	0.00	0.13	0.437	o	|	|	|	0.59
63.167	0.00	0.13	0.436	o	|	|	|	0.59
63.250	0.00	0.13	0.435	o	|	|	|	0.59
63.333	0.00	0.13	0.435	o	|	|	|	0.58
63.417	0.00	0.13	0.434	o	|	|	|	0.58
63.500	0.00	0.13	0.433	o	|	|	|	0.58
63.583	0.00	0.13	0.432	o	|	|	|	0.58
63.667	0.00	0.13	0.431	o	|	|	|	0.58
63.750	0.00	0.13	0.430	o	|	|	|	0.58
63.833	0.00	0.13	0.429	o	|	|	|	0.58
63.917	0.00	0.13	0.428	o	|	|	|	0.58
64.000	0.00	0.13	0.428	o	|	|	|	0.58
64.083	0.00	0.13	0.427	o	|	|	|	0.57
64.167	0.00	0.12	0.426	o	|	|	|	0.57
64.250	0.00	0.12	0.425	o	|	|	|	0.57
64.333	0.00	0.12	0.424	o	|	|	|	0.57
64.417	0.00	0.12	0.423	o	|	|	|	0.57
64.500	0.00	0.12	0.422	o	|	|	|	0.57
64.583	0.00	0.12	0.422	o	|	|	|	0.57
64.667	0.00	0.12	0.421	o	|	|	|	0.57
64.750	0.00	0.12	0.420	o	|	|	|	0.57
64.833	0.00	0.12	0.419	o	|	|	|	0.56
64.917	0.00	0.12	0.418	o	|	|	|	0.56
65.000	0.00	0.12	0.417	o	|	|	|	0.56
65.083	0.00	0.12	0.417	o	|	|	|	0.56
65.167	0.00	0.12	0.416	o	|	|	|	0.56
65.250	0.00	0.12	0.415	o	|	|	|	0.56
65.333	0.00	0.12	0.414	o	|	|	|	0.56
65.417	0.00	0.12	0.413	o	|	|	|	0.56
65.500	0.00	0.12	0.412	o	|	|	|	0.55
65.583	0.00	0.12	0.411	o	|	|	|	0.55
65.667	0.00	0.12	0.411	o	|	|	|	0.55
65.750	0.00	0.12	0.410	o	|	|	|	0.55
65.833	0.00	0.12	0.409	o	|	|	|	0.55
65.917	0.00	0.12	0.408	o	|	|	|	0.55
66.000	0.00	0.12	0.407	o	|	|	|	0.55
66.083	0.00	0.12	0.407	o	|	|	|	0.55
66.167	0.00	0.12	0.406	o	|	|	|	0.55
66.250	0.00	0.12	0.405	o	|	|	|	0.54

66.333	0.00	0.12	0.404	o	|	|	|	|	0.54
66.417	0.00	0.12	0.403	o	|	|	|	|	0.54
66.500	0.00	0.12	0.402	o	|	|	|	|	0.54
66.583	0.00	0.12	0.402	o	|	|	|	|	0.54
66.667	0.00	0.12	0.401	o	|	|	|	|	0.54
66.750	0.00	0.12	0.400	o	|	|	|	|	0.54
66.833	0.00	0.12	0.399	o	|	|	|	|	0.54
66.917	0.00	0.12	0.398	o	|	|	|	|	0.54
67.000	0.00	0.12	0.398	o	|	|	|	|	0.54
67.083	0.00	0.12	0.397	o	|	|	|	|	0.53
67.167	0.00	0.12	0.396	o	|	|	|	|	0.53
67.250	0.00	0.12	0.395	o	|	|	|	|	0.53
67.333	0.00	0.12	0.394	o	|	|	|	|	0.53
67.417	0.00	0.12	0.394	o	|	|	|	|	0.53
67.500	0.00	0.12	0.393	o	|	|	|	|	0.53
67.583	0.00	0.12	0.392	o	|	|	|	|	0.53
67.667	0.00	0.11	0.391	o	|	|	|	|	0.53
67.750	0.00	0.11	0.390	o	|	|	|	|	0.53
67.833	0.00	0.11	0.390	o	|	|	|	|	0.52
67.917	0.00	0.11	0.389	o	|	|	|	|	0.52
68.000	0.00	0.11	0.388	o	|	|	|	|	0.52
68.083	0.00	0.11	0.387	o	|	|	|	|	0.52
68.167	0.00	0.11	0.387	o	|	|	|	|	0.52
68.250	0.00	0.11	0.386	o	|	|	|	|	0.52
68.333	0.00	0.11	0.385	o	|	|	|	|	0.52
68.417	0.00	0.11	0.384	o	|	|	|	|	0.52
68.500	0.00	0.11	0.383	o	|	|	|	|	0.52
68.583	0.00	0.11	0.383	o	|	|	|	|	0.51
68.667	0.00	0.11	0.382	o	|	|	|	|	0.51
68.750	0.00	0.11	0.381	o	|	|	|	|	0.51
68.833	0.00	0.11	0.380	o	|	|	|	|	0.51
68.917	0.00	0.11	0.380	o	|	|	|	|	0.51
69.000	0.00	0.11	0.379	o	|	|	|	|	0.51
69.083	0.00	0.11	0.378	o	|	|	|	|	0.51
69.167	0.00	0.11	0.377	o	|	|	|	|	0.51
69.250	0.00	0.11	0.376	o	|	|	|	|	0.51
69.333	0.00	0.11	0.376	o	|	|	|	|	0.51
69.417	0.00	0.11	0.375	o	|	|	|	|	0.50
69.500	0.00	0.11	0.374	o	|	|	|	|	0.50
69.583	0.00	0.11	0.373	o	|	|	|	|	0.50
69.667	0.00	0.11	0.373	o	|	|	|	|	0.50
69.750	0.00	0.11	0.372	o	|	|	|	|	0.50
69.833	0.00	0.11	0.371	o	|	|	|	|	0.50
69.917	0.00	0.11	0.370	o	|	|	|	|	0.50
70.000	0.00	0.11	0.370	o	|	|	|	|	0.50
70.083	0.00	0.11	0.369	o	|	|	|	|	0.50
70.167	0.00	0.11	0.368	o	|	|	|	|	0.50
70.250	0.00	0.11	0.367	o	|	|	|	|	0.49
70.333	0.00	0.11	0.367	o	|	|	|	|	0.49
70.417	0.00	0.11	0.366	o	|	|	|	|	0.49
70.500	0.00	0.11	0.365	o	|	|	|	|	0.49
70.583	0.00	0.11	0.365	o	|	|	|	|	0.49
70.667	0.00	0.11	0.364	o	|	|	|	|	0.49
70.750	0.00	0.11	0.363	o	|	|	|	|	0.49
70.833	0.00	0.11	0.362	o	|	|	|	|	0.49
70.917	0.00	0.11	0.362	o	|	|	|	|	0.49
71.000	0.00	0.11	0.361	o	|	|	|	|	0.49
71.083	0.00	0.11	0.360	o	|	|	|	|	0.48
71.167	0.00	0.11	0.359	o	|	|	|	|	0.48
71.250	0.00	0.11	0.359	o	|	|	|	|	0.48
71.333	0.00	0.11	0.358	o	|	|	|	|	0.48
71.417	0.00	0.10	0.357	o	|	|	|	|	0.48
71.500	0.00	0.10	0.356	o	|	|	|	|	0.48
71.583	0.00	0.10	0.356	o	|	|	|	|	0.48
71.667	0.00	0.10	0.355	o	|	|	|	|	0.48
71.750	0.00	0.10	0.354	o	|	|	|	|	0.48
71.833	0.00	0.10	0.354	o	|	|	|	|	0.48
71.917	0.00	0.10	0.353	o	|	|	|	|	0.47
72.000	0.00	0.10	0.352	o	|	|	|	|	0.47
72.083	0.00	0.10	0.351	o	|	|	|	|	0.47
72.167	0.00	0.10	0.351	o	|	|	|	|	0.47
72.250	0.00	0.10	0.350	o	|	|	|	|	0.47
72.333	0.00	0.10	0.349	o	|	|	|	|	0.47
72.417	0.00	0.10	0.349	o	|	|	|	|	0.47
72.500	0.00	0.10	0.348	o	|	|	|	|	0.47
72.583	0.00	0.10	0.347	o	|	|	|	|	0.47
72.667	0.00	0.10	0.347	o	|	|	|	|	0.47
72.750	0.00	0.10	0.346	o	|	|	|	|	0.47
72.833	0.00	0.10	0.345	o	|	|	|	|	0.46
72.917	0.00	0.10	0.344	o	|	|	|	|	0.46
73.000	0.00	0.10	0.344	o	|	|	|	|	0.46
73.083	0.00	0.10	0.343	o	|	|	|	|	0.46
73.167	0.00	0.10	0.342	o	|	|	|	|	0.46
73.250	0.00	0.10	0.342	o	|	|	|	|	0.46
73.333	0.00	0.10	0.341	o	|	|	|	|	0.46
73.417	0.00	0.10	0.340	o	|	|	|	|	0.46

```
Remaining water in basin =    0.34 (Ac.Ft)

**************************HYDROGRAPH DATA**************************
               Number of intervals =   881
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       23.440 (CFS)
               Total volume =       3.009 (Ac.Ft)
       Status of hydrographs being held in storage
                  Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
*******************************************************************************

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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro1102410.rte
**********HYDROGRAPH DATA**********
Number of intervals = 293
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 9.934 (CFS)
Total volume = 4.820 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 293
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	2.5	4.97	7.45	9.93 (Ft.) Depth
0.083	0.11	0.00	0.000	O	|	|	|	| 0.00
0.167	0.27	0.00	0.002	O	|	|	|	| 0.00
0.250	0.31	0.00	0.004	O	|	|	|	| 0.00
0.333	0.38	0.00	0.006	OI	|	|	|	| 0.01
0.417	0.47	0.00	0.009	OI	|	|	|	| 0.01
0.500	0.49	0.00	0.012	OI	|	|	|	| 0.02
0.583	0.50	0.00	0.016	OI	|	|	|	| 0.02
0.667	0.50	0.01	0.019	OI	|	|	|	| 0.03
0.750	0.50	0.01	0.022	OI	|	|	|	| 0.03
0.833	0.56	0.01	0.026	OI	|	|	|	| 0.03
0.917	0.64	0.01	0.030	O I	|	|	|	| 0.04
1.000	0.66	0.01	0.034	O I	|	|	|	| 0.05
1.083	0.61	0.01	0.039	OI	|	|	|	| 0.05
1.167	0.54	0.01	0.043	OI	|	|	|	| 0.06
1.250	0.52	0.01	0.046	OI	|	|	|	| 0.06
1.333	0.51	0.01	0.050	OI	|	|	|	| 0.07
1.417	0.51	0.02	0.053	OI	|	|	|	| 0.07
1.500	0.50	0.02	0.056	OI	|	|	|	| 0.08
1.583	0.50	0.02	0.060	OI	|	|	|	| 0.08
1.667	0.50	0.02	0.063	OI	|	|	|	| 0.08
1.750	0.50	0.02	0.066	OI	|	|	|	| 0.09

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1.833   0.56   0.02    0.070  oI      |       |       |       |     0.09
1.917   0.64   0.02    0.074  o I     |       |       |       |     0.10
2.000   0.66   0.02    0.078  o I     |       |       |       |     0.11
2.083   0.67   0.02    0.083  o I     |       |       |       |     0.11
2.167   0.67   0.03    0.087  o I     |       |       |       |     0.12
2.250   0.67   0.03    0.091  o I     |       |       |       |     0.12
2.333   0.67   0.03    0.096  o I     |       |       |       |     0.13
2.417   0.67   0.03    0.100  o I     |       |       |       |     0.13
2.500   0.67   0.03    0.105  o I     |       |       |       |     0.14
2.583   0.73   0.03    0.109  o I     |       |       |       |     0.15
2.667   0.81   0.03    0.114  o I     |       |       |       |     0.15
2.750   0.83   0.04    0.120  o I     |       |       |       |     0.16
2.833   0.83   0.04    0.125  o I     |       |       |       |     0.17
2.917   0.84   0.04    0.131  o I     |       |       |       |     0.18
3.000   0.84   0.04    0.136  o I     |       |       |       |     0.18
3.083   0.84   0.04    0.142  o I     |       |       |       |     0.19
3.167   0.84   0.04    0.147  o I     |       |       |       |     0.20
3.250   0.84   0.04    0.153  o I     |       |       |       |     0.21
3.333   0.84   0.05    0.158  o I     |       |       |       |     0.21
3.417   0.84   0.05    0.164  o I     |       |       |       |     0.22
3.500   0.84   0.05    0.169  o I     |       |       |       |     0.23
3.583   0.84   0.05    0.175  o I     |       |       |       |     0.23
3.667   0.84   0.05    0.180  o I     |       |       |       |     0.24
3.750   0.84   0.05    0.185  o I     |       |       |       |     0.25
3.833   0.89   0.06    0.191  o I     |       |       |       |     0.26
3.917   0.97   0.06    0.197  o  I    |       |       |       |     0.27
4.000   0.99   0.06    0.203  o  I    |       |       |       |     0.27
4.083   1.00   0.06    0.210  o  I    |       |       |       |     0.28
4.167   1.01   0.06    0.216  o  I    |       |       |       |     0.29
4.250   1.01   0.07    0.223  o  I    |       |       |       |     0.30
4.333   1.06   0.07    0.229  o  I    |       |       |       |     0.31
4.417   1.14   0.07    0.237  o  I    |       |       |       |     0.32
4.500   1.16   0.07    0.244  o  I    |       |       |       |     0.33
4.583   1.17   0.07    0.252  o  I    |       |       |       |     0.34
4.667   1.17   0.08    0.259  o  I    |       |       |       |     0.35
4.750   1.18   0.08    0.267  o  I    |       |       |       |     0.36
4.833   1.23   0.08    0.274  o  I    |       |       |       |     0.37
4.917   1.31   0.08    0.283  o   I   |       |       |       |     0.38
5.000   1.33   0.09    0.291  o   I   |       |       |       |     0.39
5.083   1.23   0.09    0.299  o  I    |       |       |       |     0.40
5.167   1.07   0.09    0.307  o  I    |       |       |       |     0.41
5.250   1.04   0.09    0.313  o  I    |       |       |       |     0.42
5.333   1.08   0.09    0.320  o  I    |       |       |       |     0.43
5.417   1.15   0.10    0.327  o  I    |       |       |       |     0.44
5.500   1.16   0.10    0.334  o  I    |       |       |       |     0.45
5.583   1.22   0.10    0.342  o  I    |       |       |       |     0.46
5.667   1.31   0.10    0.350  o   I   |       |       |       |     0.47
5.750   1.33   0.11    0.358  o   I   |       |       |       |     0.48
5.833   1.34   0.11    0.367  o   I   |       |       |       |     0.49
5.917   1.34   0.11    0.375  o   I   |       |       |       |     0.50
6.000   1.34   0.11    0.384  o   I   |       |       |       |     0.52
6.083   1.40   0.12    0.392  o   I   |       |       |       |     0.53
6.167   1.48   0.12    0.401  o   I   |       |       |       |     0.54
6.250   1.50   0.12    0.411  o   I   |       |       |       |     0.55
6.333   1.51   0.12    0.420  o   I   |       |       |       |     0.57
6.417   1.51   0.13    0.430  o   I   |       |       |       |     0.58
6.500   1.51   0.13    0.439  o   I   |       |       |       |     0.59
6.583   1.57   0.13    0.449  o    I  |       |       |       |     0.60
6.667   1.65   0.13    0.459  o    I  |       |       |       |     0.62
6.750   1.67   0.14    0.470  o    I  |       |       |       |     0.63
6.833   1.67   0.14    0.480  o    I  |       |       |       |     0.65
6.917   1.68   0.14    0.491  o    I  |       |       |       |     0.66
7.000   1.68   0.15    0.501  o    I  |       |       |       |     0.67
7.083   1.68   0.15    0.512  o    I  |       |       |       |     0.69
7.167   1.68   0.15    0.522  o    I  |       |       |       |     0.70
7.250   1.68   0.16    0.533  o    I  |       |       |       |     0.72
7.333   1.73   0.16    0.544  o    I  |       |       |       |     0.73
7.417   1.81   0.16    0.555  o    I  |       |       |       |     0.75
7.500   1.83   0.17    0.566  o    I  |       |       |       |     0.76
7.583   1.90   0.17    0.578  o     I |       |       |       |     0.78
7.667   1.98   0.17    0.590  o     I |       |       |       |     0.79
7.750   2.00   0.18    0.602  o     I |       |       |       |     0.81
7.833   2.10   0.18    0.615  o     I |       |       |       |     0.83
7.917   2.24   0.18    0.629  o      I|       |       |       |     0.85
8.000   2.28   0.19    0.643  o      I|       |       |       |     0.87
8.083   2.52   0.19    0.659  o       I       |       |       |     0.89
8.167   2.86   0.20    0.676  o       |I      |       |       |     0.91
8.250   2.95   0.20    0.694  o       |I      |       |       |     0.93
8.333   2.99   0.21    0.713  o       |I      |       |       |     0.96
8.417   3.02   0.21    0.733  o       |I      |       |       |     0.99
8.500   3.04   0.22    0.752  o       |I      |       |       |     1.01
8.583   3.15   0.23    0.772  o       | I     |       |       |     1.04
8.667   3.32   0.25    0.792  o       | I     |       |       |     1.06
8.750   3.37   0.26    0.814  o       | I     |       |       |     1.09
8.833   3.50   0.27    0.835  o       |  I    |       |       |     1.11
8.917   3.68   0.28    0.858  o       |  I    |       |       |     1.14
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 9.000    3.73    0.29      0.882  O       |   I   |       |       |     1.17
 9.083    3.98    0.31      0.906  O       |   I   |       |       |     1.20
 9.167    4.31    0.32      0.933  |O      |    I  |       |       |     1.23
 9.250    4.40    0.34      0.960  |O      |     I |       |       |     1.27
 9.333    4.55    0.35      0.989  |O      |     I |       |       |     1.30
 9.417    4.74    0.37      1.018  |O      |      I|       |       |     1.34
 9.500    4.80    0.39      1.049  |O      |      I|       |       |     1.37
 9.583    4.93    0.40      1.079  |O      |      I|       |       |     1.41
 9.667    5.11    0.42      1.111  |O      |       I       |       |     1.45
 9.750    5.16    0.44      1.144  |O      |       I       |       |     1.49
 9.833    5.29    0.46      1.177  |O      |        |I      |       |     1.53
 9.917    5.47    0.48      1.210  |O      |        |I      |       |     1.57
10.000    5.52    0.49      1.245  |O      |        |I      |       |     1.61
10.083    4.79    0.51      1.277  |O      |      I|       |       |     1.65
10.167    3.69    0.53      1.303  |O      |  I    |       |       |     1.68
10.250    3.44    0.54      1.323  |O      |  I    |       |       |     1.71
10.333    3.33    0.55      1.343  |O      | I     |       |       |     1.73
10.417    3.28    0.56      1.362  |O      | I     |       |       |     1.76
10.500    3.25    0.57      1.381  |O      | I     |       |       |     1.78
10.583    3.81    0.58      1.401  |O      |   I   |       |       |     1.80
10.667    4.61    0.59      1.426  |O      |    I  |       |       |     1.83
10.750    4.81    0.61      1.454  |O      |     I|       |       |     1.87
10.833    4.90    0.63      1.483  | O     |      I|       |       |     1.91
10.917    4.95    0.64      1.513  | O     |      I|       |       |     1.94
11.000    4.99    0.66      1.543  | O     |       I       |       |     1.98
11.083    4.89    0.68      1.572  | O     |      I|       |       |     2.01
11.167    4.73    0.71      1.600  | O     |      I|       |       |     2.04
11.250    4.71    0.73      1.628  | O     |      I|       |       |     2.07
11.333    4.70    0.76      1.655  | O     |      I|       |       |     2.11
11.417    4.70    0.78      1.682  | O     |      I|       |       |     2.14
11.500    4.70    0.81      1.709  | O     |      I|       |       |     2.17
11.583    4.49    0.83      1.735  | O     |     I |       |       |     2.19
11.667    4.18    0.86      1.759  | O     |    I  |       |       |     2.22
11.750    4.11    0.88      1.782  | O     |    I  |       |       |     2.25
11.833    4.20    0.90      1.804  | O     |    I  |       |       |     2.27
11.917    4.35    0.92      1.827  | O     |     I |       |       |     2.30
12.000    4.38    0.94      1.851  |  O    |     I |       |       |     2.32
12.083    5.17    0.97      1.877  |  O    |       I       |       |     2.35
12.167    6.30    1.00      1.910  |  O    |       |   I   |       |     2.39
12.250    6.58    1.03      1.947  |  O    |       |    I  |       |     2.43
12.333    6.81    1.07      1.986  |  O    |       |    I  |       |     2.48
12.417    7.04    1.11      2.026  |  O    |       |     I |       |     2.52
12.500    7.12    1.15      2.067  |  O    |       |     I |       |     2.57
12.583    7.36    1.19      2.109  |  O    |       |      I|       |     2.61
12.667    7.70    1.23      2.153  |  O    |       |       I       |     2.66
12.750    7.79    1.27      2.198  |   O   |       |       |I      |     2.71
12.833    7.94    1.32      2.243  |   O   |       |       |I      |     2.76
12.917    8.12    1.36      2.289  |   O   |       |       | I     |     2.81
13.000    8.18    1.40      2.335  |   O   |       |       | I     |     2.87
13.083    8.75    1.45      2.384  |   O   |       |       |   I   |     2.92
13.167    9.56    1.50      2.437  |   O   |       |       |     I |     2.98
13.250    9.76    4.64      2.482  |       |     O |       |      I|     3.03
13.333    9.85    7.66      2.507  |       |       |      O      I|     3.05
13.417    9.90    8.95      2.518  |       |       |       |   O  I|     3.07
13.500    9.93    9.52      2.523  |       |       |       |     O I     3.07
13.583    8.74    9.41      2.522  |       |       |       |    I O |    3.07
13.667    7.00    8.51      2.514  |       |       |     I |  O     |    3.06
13.750    6.59    7.51      2.506  |       |       |    I  O       |    3.05
13.833    6.41    6.92      2.501  |       |       |   I O |       |    3.05
13.917    6.33    6.60      2.498  |       |       |   IO  |       |    3.04
14.000    6.28    6.43      2.497  |       |       |   O   |       |    3.04
14.083    6.72    6.47      2.497  |       |       |   OI  |       |    3.04
14.167    7.37    6.81      2.500  |       |       |    O I|       |    3.05
14.250    7.53    7.18      2.503  |       |       |      OI       |    3.05
14.333    7.49    7.37      2.505  |       |       |      OI       |    3.05
14.417    7.38    7.41      2.505  |       |       |      O|       |    3.05
14.500    7.36    7.39      2.505  |       |       |      O|       |    3.05
14.583    7.35    7.37      2.505  |       |       |      O|       |    3.05
14.667    7.35    7.36      2.505  |       |       |      O|       |    3.05
14.750    7.36    7.36      2.505  |       |       |      O|       |    3.05
14.833    7.25    7.33      2.505  |       |       |      O|       |    3.05
14.917    7.10    7.24      2.504  |       |       |     IO|       |    3.05
15.000    7.07    7.15      2.503  |       |       |     IO|       |    3.05
15.083    6.95    7.07      2.502  |       |       |     O |       |    3.05
15.167    6.79    6.95      2.501  |       |       |    IO |       |    3.05
15.250    6.76    6.85      2.501  |       |       |    IO |       |    3.05
15.333    6.64    6.76      2.500  |       |       |    O  |       |    3.05
15.417    6.48    6.64      2.499  |       |       |   IO  |       |    3.05
15.500    6.44    6.53      2.498  |       |       |   IO  |       |    3.04
15.583    5.99    6.35      2.496  |       |       |  IO   |       |    3.04
15.667    5.36    5.96      2.493  |       |       |I O    |       |    3.04
15.750    5.21    5.56      2.490  |       |       IO      |       |    3.04
15.833    5.15    5.34      2.488  |       |       IO      |       |    3.03
15.917    5.12    5.22      2.487  |       |       O       |       |    3.03
16.000    5.11    5.16      2.486  |       |       O       |       |    3.03
16.083    3.67    4.71      2.483  |       |  I   O|       |       |    3.03
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16.167	1.57	3.49	2.472	I	O			3.02
16.250	1.07	2.23	2.462	I	O			3.01
16.333	0.85	1.52	2.456	I O				3.00
16.417	0.74	1.51	2.451	I O				2.99
16.500	0.67	1.51	2.445	I O				2.99
16.583	0.62	1.50	2.439	I O				2.98
16.667	0.54	1.50	2.433	I O				2.97
16.750	0.52	1.49	2.426	I O				2.97
16.833	0.51	1.48	2.420	I O				2.96
16.917	0.51	1.48	2.413	I O				2.95
17.000	0.50	1.47	2.406	I O				2.94
17.083	0.61	1.46	2.400	I O				2.94
17.167	0.77	1.46	2.395	I O				2.93
17.250	0.81	1.46	2.390	I O				2.93
17.333	0.83	1.45	2.386	I O				2.92
17.417	0.84	1.45	2.381	I O				2.92
17.500	0.84	1.44	2.377	I O				2.91
17.583	0.84	1.44	2.373	I O				2.91
17.667	0.84	1.44	2.369	I O				2.90
17.750	0.84	1.43	2.365	I O				2.90
17.833	0.79	1.43	2.361	I O				2.89
17.917	0.71	1.42	2.356	I O				2.89
18.000	0.69	1.42	2.351	I O				2.88
18.083	0.68	1.41	2.346	I O				2.88
18.167	0.67	1.41	2.341	I O				2.87
18.250	0.67	1.40	2.336	I O				2.87
18.333	0.67	1.40	2.331	I O				2.86
18.417	0.67	1.39	2.326	I O				2.85
18.500	0.67	1.39	2.321	I O				2.85
18.583	0.62	1.38	2.316	I O				2.84
18.667	0.54	1.38	2.310	I O				2.84
18.750	0.52	1.37	2.304	I O				2.83
18.833	0.46	1.37	2.298	I O				2.82
18.917	0.37	1.36	2.292	I O				2.82
19.000	0.35	1.36	2.285	I O				2.81
19.083	0.40	1.35	2.278	I O				2.80
19.167	0.47	1.34	2.272	I O				2.79
19.250	0.49	1.34	2.266	I O				2.79
19.333	0.55	1.33	2.260	I O				2.78
19.417	0.64	1.33	2.255	I O				2.78
19.500	0.66	1.32	2.251	I O				2.77
19.583	0.61	1.32	2.246	I O				2.77
19.667	0.54	1.31	2.241	I O				2.76
19.750	0.52	1.31	2.235	I O				2.75
19.833	0.46	1.30	2.230	I O				2.75
19.917	0.37	1.30	2.224	I O				2.74
20.000	0.35	1.29	2.217	I O				2.73
20.083	0.40	1.29	2.211	I O				2.73
20.167	0.47	1.28	2.205	I O				2.72
20.250	0.49	1.27	2.200	I O				2.71
20.333	0.50	1.27	2.194	I O				2.71
20.417	0.50	1.26	2.189	I O				2.70
20.500	0.50	1.26	2.184	I O				2.70
20.583	0.50	1.25	2.179	I O				2.69
20.667	0.50	1.25	2.173	I O				2.68
20.750	0.50	1.24	2.168	I O				2.68
20.833	0.45	1.24	2.163	I O				2.67
20.917	0.37	1.23	2.157	I O				2.67
21.000	0.35	1.23	2.151	I O				2.66
21.083	0.40	1.22	2.145	I O				2.65
21.167	0.47	1.22	2.140	I O				2.65
21.250	0.49	1.21	2.135	I O				2.64
21.333	0.44	1.21	2.130	I O				2.64
21.417	0.37	1.20	2.124	I O				2.63
21.500	0.35	1.20	2.119	I O				2.62
21.583	0.40	1.19	2.113	I O				2.62
21.667	0.47	1.19	2.108	I O				2.61
21.750	0.49	1.18	2.103	I O				2.61
21.833	0.44	1.18	2.098	I O				2.60
21.917	0.37	1.17	2.093	I O				2.59
22.000	0.35	1.17	2.087	I O				2.59
22.083	0.40	1.16	2.082	I O				2.58
22.167	0.47	1.16	2.077	I O				2.58
22.250	0.49	1.15	2.072	I O				2.57
22.333	0.44	1.15	2.067	I O				2.57
22.417	0.37	1.14	2.062	I O				2.56
22.500	0.35	1.14	2.057	I O				2.55
22.583	0.34	1.13	2.051	I O				2.55
22.667	0.34	1.13	2.046	I O				2.54
22.750	0.34	1.12	2.040	I O				2.54
22.833	0.34	1.12	2.035	I O				2.53
22.917	0.34	1.11	2.030	I O				2.52
23.000	0.34	1.11	2.024	I O				2.52
23.083	0.34	1.10	2.019	I O				2.51
23.167	0.34	1.10	2.014	I O				2.51
23.250	0.34	1.09	2.009	I O				2.50

23.333	0.34	1.09	2.003	I o				2.49
23.417	0.34	1.08	1.998	I o				2.49
23.500	0.34	1.08	1.993	I o				2.48
23.583	0.34	1.07	1.988	I o				2.48
23.667	0.34	1.07	1.983	I o				2.47
23.750	0.34	1.06	1.978	I o				2.47
23.833	0.34	1.06	1.973	I o				2.46
23.917	0.34	1.05	1.968	I o				2.45
24.000	0.34	1.05	1.963	I o				2.45
24.083	0.23	1.04	1.958	I o				2.44
24.167	0.07	1.04	1.952	I o				2.44
24.250	0.03	1.03	1.945	I o				2.43
24.333	0.01	1.03	1.938	I o				2.42
24.417	0.00	1.02	1.931	I o				2.41
24.500	0.00	1.01	1.924	I o				2.41
24.583	0.00	1.01	1.917	I o				2.40
24.667	0.00	1.00	1.910	I o				2.39
24.750	0.00	0.99	1.903	I o				2.38
24.833	0.00	0.99	1.896	I o				2.37
24.917	0.00	0.98	1.890	I o				2.37
25.000	0.00	0.97	1.883	I o				2.36
25.083	0.00	0.97	1.876	I o				2.35
25.167	0.00	0.96	1.869	I o				2.34
25.250	0.00	0.95	1.863	I o				2.34
25.333	0.00	0.95	1.856	I o				2.33
25.417	0.00	0.94	1.850	I o				2.32
25.500	0.00	0.94	1.843	I o				2.32
25.583	0.00	0.93	1.837	I o				2.31
25.667	0.00	0.92	1.831	I o				2.30
25.750	0.00	0.92	1.824	I o				2.29
25.833	0.00	0.91	1.818	I o				2.29
25.917	0.00	0.91	1.812	I o				2.28
26.000	0.00	0.90	1.805	I o				2.27
26.083	0.00	0.89	1.799	I o				2.27
26.167	0.00	0.89	1.793	I o				2.26
26.250	0.00	0.88	1.787	I o				2.25
26.333	0.00	0.88	1.781	I o				2.25
26.417	0.00	0.87	1.775	I o				2.24
26.500	0.00	0.87	1.769	I o				2.23
26.583	0.00	0.86	1.763	I o				2.23
26.667	0.00	0.85	1.757	I o				2.22
26.750	0.00	0.85	1.751	I o				2.21
26.833	0.00	0.84	1.745	I o				2.21
26.917	0.00	0.84	1.740	I o				2.20
27.000	0.00	0.83	1.734	I o				2.19
27.083	0.00	0.83	1.728	I o				2.19
27.167	0.00	0.82	1.722	I o				2.18
27.250	0.00	0.82	1.717	I o				2.17
27.333	0.00	0.81	1.711	I o				2.17
27.417	0.00	0.81	1.706	I o				2.16
27.500	0.00	0.80	1.700	I o				2.16
27.583	0.00	0.79	1.695	I o				2.15
27.667	0.00	0.79	1.689	I o				2.14
27.750	0.00	0.78	1.684	I o				2.14
27.833	0.00	0.78	1.678	I o				2.13
27.917	0.00	0.77	1.673	I o				2.13
28.000	0.00	0.77	1.668	I o				2.12
28.083	0.00	0.76	1.662	I o				2.11
28.167	0.00	0.76	1.657	I o				2.11
28.250	0.00	0.75	1.652	I o				2.10
28.333	0.00	0.75	1.647	I o				2.10
28.417	0.00	0.74	1.642	I o				2.09
28.500	0.00	0.74	1.637	I o				2.08
28.583	0.00	0.73	1.631	I o				2.08
28.667	0.00	0.73	1.626	I o				2.07
28.750	0.00	0.73	1.621	I o				2.07
28.833	0.00	0.72	1.616	I o				2.06
28.917	0.00	0.72	1.611	I o				2.06
29.000	0.00	0.71	1.607	I o				2.05
29.083	0.00	0.71	1.602	I o				2.05
29.167	0.00	0.70	1.597	I o				2.04
29.250	0.00	0.70	1.592	I o				2.03
29.333	0.00	0.69	1.587	I o				2.03
29.417	0.00	0.69	1.582	I o				2.02
29.500	0.00	0.68	1.578	I o				2.02
29.583	0.00	0.68	1.573	I o				2.01
29.667	0.00	0.68	1.568	I o				2.01
29.750	0.00	0.67	1.564	I o				2.00
29.833	0.00	0.67	1.559	I o				2.00
29.917	0.00	0.66	1.555	I o				1.99
30.000	0.00	0.66	1.550	I o				1.99
30.083	0.00	0.66	1.545	I o				1.98
30.167	0.00	0.66	1.541	I o				1.98
30.250	0.00	0.65	1.536	I o				1.97
30.333	0.00	0.65	1.532	I o				1.96
30.417	0.00	0.65	1.527	I o				1.96

30.500	0.00	0.65	1.523	I O	|	|	|	1.95
30.583	0.00	0.64	1.518	I O	|	|	|	1.95
30.667	0.00	0.64	1.514	I O	|	|	|	1.94
30.750	0.00	0.64	1.510	I O	|	|	|	1.94
30.833	0.00	0.64	1.505	I O	|	|	|	1.93
30.917	0.00	0.63	1.501	I O	|	|	|	1.93
31.000	0.00	0.63	1.497	I O	|	|	|	1.92
31.083	0.00	0.63	1.492	I O	|	|	|	1.92
31.167	0.00	0.63	1.488	I O	|	|	|	1.91
31.250	0.00	0.63	1.484	I O	|	|	|	1.91
31.333	0.00	0.62	1.479	I O	|	|	|	1.90
31.417	0.00	0.62	1.475	IO	|	|	|	1.89
31.500	0.00	0.62	1.471	IO	|	|	|	1.89
31.583	0.00	0.62	1.466	IO	|	|	|	1.88
31.667	0.00	0.61	1.462	IO	|	|	|	1.88
31.750	0.00	0.61	1.458	IO	|	|	|	1.87
31.833	0.00	0.61	1.454	IO	|	|	|	1.87
31.917	0.00	0.61	1.450	IO	|	|	|	1.86
32.000	0.00	0.60	1.445	IO	|	|	|	1.86
32.083	0.00	0.60	1.441	IO	|	|	|	1.85
32.167	0.00	0.60	1.437	IO	|	|	|	1.85
32.250	0.00	0.60	1.433	IO	|	|	|	1.84
32.333	0.00	0.60	1.429	IO	|	|	|	1.84
32.417	0.00	0.59	1.425	IO	|	|	|	1.83
32.500	0.00	0.59	1.421	IO	|	|	|	1.83
32.583	0.00	0.59	1.417	IO	|	|	|	1.82
32.667	0.00	0.59	1.413	IO	|	|	|	1.82
32.750	0.00	0.58	1.409	IO	|	|	|	1.81
32.833	0.00	0.58	1.405	IO	|	|	|	1.81
32.917	0.00	0.58	1.401	IO	|	|	|	1.80
33.000	0.00	0.58	1.397	IO	|	|	|	1.80
33.083	0.00	0.58	1.393	IO	|	|	|	1.79
33.167	0.00	0.57	1.389	IO	|	|	|	1.79
33.250	0.00	0.57	1.385	IO	|	|	|	1.78
33.333	0.00	0.57	1.381	IO	|	|	|	1.78
33.417	0.00	0.57	1.377	IO	|	|	|	1.77
33.500	0.00	0.56	1.373	IO	|	|	|	1.77
33.583	0.00	0.56	1.369	IO	|	|	|	1.77
33.667	0.00	0.56	1.365	IO	|	|	|	1.76
33.750	0.00	0.56	1.361	IO	|	|	|	1.76
33.833	0.00	0.56	1.358	IO	|	|	|	1.75
33.917	0.00	0.55	1.354	IO	|	|	|	1.75
34.000	0.00	0.55	1.350	IO	|	|	|	1.74
34.083	0.00	0.55	1.346	IO	|	|	|	1.74
34.167	0.00	0.55	1.342	IO	|	|	|	1.73
34.250	0.00	0.55	1.339	IO	|	|	|	1.73
34.333	0.00	0.54	1.335	IO	|	|	|	1.72
34.417	0.00	0.54	1.331	IO	|	|	|	1.72
34.500	0.00	0.54	1.327	IO	|	|	|	1.71
34.583	0.00	0.54	1.324	IO	|	|	|	1.71
34.667	0.00	0.54	1.320	IO	|	|	|	1.71
34.750	0.00	0.53	1.316	IO	|	|	|	1.70
34.833	0.00	0.53	1.313	IO	|	|	|	1.70
34.917	0.00	0.53	1.309	IO	|	|	|	1.69
35.000	0.00	0.53	1.305	IO	|	|	|	1.69
35.083	0.00	0.53	1.302	IO	|	|	|	1.68
35.167	0.00	0.52	1.298	IO	|	|	|	1.68
35.250	0.00	0.52	1.294	IO	|	|	|	1.67
35.333	0.00	0.52	1.291	IO	|	|	|	1.67
35.417	0.00	0.52	1.287	IO	|	|	|	1.67
35.500	0.00	0.52	1.284	IO	|	|	|	1.66
35.583	0.00	0.51	1.280	IO	|	|	|	1.66
35.667	0.00	0.51	1.277	IO	|	|	|	1.65
35.750	0.00	0.51	1.273	IO	|	|	|	1.65
35.833	0.00	0.51	1.270	IO	|	|	|	1.64
35.917	0.00	0.51	1.266	IO	|	|	|	1.64
36.000	0.00	0.50	1.263	IO	|	|	|	1.64
36.083	0.00	0.50	1.259	IO	|	|	|	1.63
36.167	0.00	0.50	1.256	IO	|	|	|	1.63
36.250	0.00	0.50	1.252	IO	|	|	|	1.62
36.333	0.00	0.50	1.249	IO	|	|	|	1.62
36.417	0.00	0.49	1.246	IO	|	|	|	1.61
36.500	0.00	0.49	1.242	IO	|	|	|	1.61
36.583	0.00	0.49	1.239	IO	|	|	|	1.61
36.667	0.00	0.49	1.235	IO	|	|	|	1.60
36.750	0.00	0.49	1.232	IO	|	|	|	1.60
36.833	0.00	0.49	1.229	IO	|	|	|	1.59
36.917	0.00	0.48	1.225	IO	|	|	|	1.59
37.000	0.00	0.48	1.222	IO	|	|	|	1.59
37.083	0.00	0.48	1.219	IO	|	|	|	1.58
37.167	0.00	0.48	1.215	IO	|	|	|	1.58
37.250	0.00	0.48	1.212	IO	|	|	|	1.57
37.333	0.00	0.47	1.209	IO	|	|	|	1.57
37.417	0.00	0.47	1.206	IO	|	|	|	1.57
37.500	0.00	0.47	1.202	IO	|	|	|	1.56
37.583	0.00	0.47	1.199	IO	|	|	|	1.56

37.667	0.00	0.47	1.196	IO					1.55
37.750	0.00	0.47	1.193	IO					1.55
37.833	0.00	0.46	1.189	IO					1.55
37.917	0.00	0.46	1.186	IO					1.54
38.000	0.00	0.46	1.183	IO					1.54
38.083	0.00	0.46	1.180	IO					1.53
38.167	0.00	0.46	1.177	IO					1.53
38.250	0.00	0.45	1.174	IO					1.53
38.333	0.00	0.45	1.171	IO					1.52
38.417	0.00	0.45	1.167	IO					1.52
38.500	0.00	0.45	1.164	IO					1.52
38.583	0.00	0.45	1.161	IO					1.51
38.667	0.00	0.45	1.158	IO					1.51
38.750	0.00	0.44	1.155	IO					1.50
38.833	0.00	0.44	1.152	IO					1.50
38.917	0.00	0.44	1.149	IO					1.50
39.000	0.00	0.44	1.146	IO					1.49
39.083	0.00	0.44	1.143	IO					1.49
39.167	0.00	0.44	1.140	IO					1.49
39.250	0.00	0.43	1.137	IO					1.48
39.333	0.00	0.43	1.134	IO					1.48
39.417	0.00	0.43	1.131	IO					1.47
39.500	0.00	0.43	1.128	IO					1.47
39.583	0.00	0.43	1.125	IO					1.47
39.667	0.00	0.43	1.122	IO					1.46
39.750	0.00	0.42	1.119	IO					1.46
39.833	0.00	0.42	1.116	IO					1.46
39.917	0.00	0.42	1.113	IO					1.45
40.000	0.00	0.42	1.110	IO					1.45
40.083	0.00	0.42	1.108	IO					1.45
40.167	0.00	0.42	1.105	IO					1.44
40.250	0.00	0.42	1.102	IO					1.44
40.333	0.00	0.41	1.099	IO					1.44
40.417	0.00	0.41	1.096	IO					1.43
40.500	0.00	0.41	1.093	IO					1.43
40.583	0.00	0.41	1.090	IO					1.42
40.667	0.00	0.41	1.088	IO					1.42
40.750	0.00	0.41	1.085	IO					1.42
40.833	0.00	0.40	1.082	IO					1.41
40.917	0.00	0.40	1.079	IO					1.41
41.000	0.00	0.40	1.076	IO					1.41
41.083	0.00	0.40	1.074	IO					1.40
41.167	0.00	0.40	1.071	IO					1.40
41.250	0.00	0.40	1.068	IO					1.40
41.333	0.00	0.40	1.065	IO					1.39
41.417	0.00	0.39	1.063	IO					1.39
41.500	0.00	0.39	1.060	IO					1.39
41.583	0.00	0.39	1.057	IO					1.38
41.667	0.00	0.39	1.055	IO					1.38
41.750	0.00	0.39	1.052	IO					1.38
41.833	0.00	0.39	1.049	IO					1.37
41.917	0.00	0.39	1.047	IO					1.37
42.000	0.00	0.38	1.044	IO					1.37
42.083	0.00	0.38	1.041	IO					1.36
42.167	0.00	0.38	1.039	IO					1.36
42.250	0.00	0.38	1.036	IO					1.36
42.333	0.00	0.38	1.034	IO					1.36
42.417	0.00	0.38	1.031	IO					1.35
42.500	0.00	0.37	1.028	IO					1.35
42.583	0.00	0.37	1.026	IO					1.35
42.667	0.00	0.37	1.023	IO					1.34
42.750	0.00	0.37	1.021	IO					1.34
42.833	0.00	0.37	1.018	IO					1.34
42.917	0.00	0.37	1.016	IO					1.33
43.000	0.00	0.37	1.013	IO					1.33
43.083	0.00	0.37	1.011	IO					1.33
43.167	0.00	0.36	1.008	IO					1.32
43.250	0.00	0.36	1.006	IO					1.32
43.333	0.00	0.36	1.003	IO					1.32
43.417	0.00	0.36	1.001	IO					1.31
43.500	0.00	0.36	0.998	IO					1.31
43.583	0.00	0.36	0.996	IO					1.31
43.667	0.00	0.36	0.993	IO					1.31
43.750	0.00	0.35	0.991	IO					1.30
43.833	0.00	0.35	0.988	IO					1.30
43.917	0.00	0.35	0.986	IO					1.30
44.000	0.00	0.35	0.983	IO					1.29
44.083	0.00	0.35	0.981	IO					1.29
44.167	0.00	0.35	0.979	IO					1.29
44.250	0.00	0.35	0.976	IO					1.29
44.333	0.00	0.34	0.974	IO					1.28
44.417	0.00	0.34	0.971	IO					1.28
44.500	0.00	0.34	0.969	IO					1.28
44.583	0.00	0.34	0.967	IO					1.27
44.667	0.00	0.34	0.964	IO					1.27
44.750	0.00	0.34	0.962	IO					1.27

44.833	0.00	0.34	0.960	IO				1.26
44.917	0.00	0.34	0.957	IO				1.26
45.000	0.00	0.33	0.955	IO				1.26
45.083	0.00	0.33	0.953	IO				1.26
45.167	0.00	0.33	0.951	IO				1.25
45.250	0.00	0.33	0.948	IO				1.25
45.333	0.00	0.33	0.946	IO				1.25
45.417	0.00	0.33	0.944	IO				1.25
45.500	0.00	0.33	0.941	IO				1.24
45.583	0.00	0.33	0.939	IO				1.24
45.667	0.00	0.32	0.937	IO				1.24
45.750	0.00	0.32	0.935	IO				1.23
45.833	0.00	0.32	0.933	IO				1.23
45.917	0.00	0.32	0.930	IO				1.23
46.000	0.00	0.32	0.928	IO				1.23
46.083	0.00	0.32	0.926	IO				1.22
46.167	0.00	0.32	0.924	IO				1.22
46.250	0.00	0.32	0.922	IO				1.22
46.333	0.00	0.32	0.919	IO				1.22
46.417	0.00	0.31	0.917	IO				1.21
46.500	0.00	0.31	0.915	IO				1.21
46.583	0.00	0.31	0.913	IO				1.21
46.667	0.00	0.31	0.911	O				1.21
46.750	0.00	0.31	0.909	O				1.20
46.833	0.00	0.31	0.906	O				1.20
46.917	0.00	0.31	0.904	O				1.20
47.000	0.00	0.31	0.902	O				1.19
47.083	0.00	0.30	0.900	O				1.19
47.167	0.00	0.30	0.898	O				1.19
47.250	0.00	0.30	0.896	O				1.19
47.333	0.00	0.30	0.894	O				1.18
47.417	0.00	0.30	0.892	O				1.18
47.500	0.00	0.30	0.890	O				1.18
47.583	0.00	0.30	0.888	O				1.18
47.667	0.00	0.30	0.886	O				1.17
47.750	0.00	0.30	0.884	O				1.17
47.833	0.00	0.29	0.882	O				1.17
47.917	0.00	0.29	0.880	O				1.17
48.000	0.00	0.29	0.878	O				1.16
48.083	0.00	0.29	0.876	O				1.16
48.167	0.00	0.29	0.874	O				1.16
48.250	0.00	0.29	0.872	O				1.16
48.333	0.00	0.29	0.870	O				1.15
48.417	0.00	0.29	0.868	O				1.15
48.500	0.00	0.29	0.866	O				1.15
48.583	0.00	0.28	0.864	O				1.15
48.667	0.00	0.28	0.862	O				1.15
48.750	0.00	0.28	0.860	O				1.14
48.833	0.00	0.28	0.858	O				1.14
48.917	0.00	0.28	0.856	O				1.14
49.000	0.00	0.28	0.854	O				1.14
49.083	0.00	0.28	0.852	O				1.13
49.167	0.00	0.28	0.850	O				1.13
49.250	0.00	0.28	0.848	O				1.13
49.333	0.00	0.27	0.846	O				1.13
49.417	0.00	0.27	0.844	O				1.12
49.500	0.00	0.27	0.843	O				1.12
49.583	0.00	0.27	0.841	O				1.12
49.667	0.00	0.27	0.839	O				1.12
49.750	0.00	0.27	0.837	O				1.11
49.833	0.00	0.27	0.835	O				1.11
49.917	0.00	0.27	0.833	O				1.11
50.000	0.00	0.27	0.831	O				1.11
50.083	0.00	0.27	0.830	O				1.11
50.167	0.00	0.26	0.828	O				1.10
50.250	0.00	0.26	0.826	O				1.10
50.333	0.00	0.26	0.824	O				1.10
50.417	0.00	0.26	0.822	O				1.10
50.500	0.00	0.26	0.821	O				1.09
50.583	0.00	0.26	0.819	O				1.09
50.667	0.00	0.26	0.817	O				1.09
50.750	0.00	0.26	0.815	O				1.09
50.833	0.00	0.26	0.813	O				1.09
50.917	0.00	0.26	0.812	O				1.08
51.000	0.00	0.25	0.810	O				1.08
51.083	0.00	0.25	0.808	O				1.08
51.167	0.00	0.25	0.806	O				1.08
51.250	0.00	0.25	0.805	O				1.08
51.333	0.00	0.25	0.803	O				1.07
51.417	0.00	0.25	0.801	O				1.07
51.500	0.00	0.25	0.799	O				1.07
51.583	0.00	0.25	0.798	O				1.07
51.667	0.00	0.25	0.796	O				1.06
51.750	0.00	0.25	0.794	O				1.06
51.833	0.00	0.25	0.793	O				1.06
51.917	0.00	0.24	0.791	O				1.06

52.000	0.00	0.24	0.789	o	|	|	|	|	1.06
52.083	0.00	0.24	0.788	o	|	|	|	|	1.05
52.167	0.00	0.24	0.786	o	|	|	|	|	1.05
52.250	0.00	0.24	0.784	o	|	|	|	|	1.05
52.333	0.00	0.24	0.783	o	|	|	|	|	1.05
52.417	0.00	0.24	0.781	o	|	|	|	|	1.05
52.500	0.00	0.24	0.779	o	|	|	|	|	1.04
52.583	0.00	0.24	0.778	o	|	|	|	|	1.04
52.667	0.00	0.24	0.776	o	|	|	|	|	1.04
52.750	0.00	0.24	0.774	o	|	|	|	|	1.04
52.833	0.00	0.23	0.773	o	|	|	|	|	1.04
52.917	0.00	0.23	0.771	o	|	|	|	|	1.03
53.000	0.00	0.23	0.770	o	|	|	|	|	1.03
53.083	0.00	0.23	0.768	o	|	|	|	|	1.03
53.167	0.00	0.23	0.766	o	|	|	|	|	1.03
53.250	0.00	0.23	0.765	o	|	|	|	|	1.03
53.333	0.00	0.23	0.763	o	|	|	|	|	1.02
53.417	0.00	0.23	0.762	o	|	|	|	|	1.02
53.500	0.00	0.23	0.760	o	|	|	|	|	1.02
53.583	0.00	0.23	0.759	o	|	|	|	|	1.02
53.667	0.00	0.23	0.757	o	|	|	|	|	1.02
53.750	0.00	0.22	0.755	o	|	|	|	|	1.02
53.833	0.00	0.22	0.754	o	|	|	|	|	1.01
53.917	0.00	0.22	0.752	o	|	|	|	|	1.01
54.000	0.00	0.22	0.751	o	|	|	|	|	1.01
54.083	0.00	0.22	0.749	o	|	|	|	|	1.01
54.167	0.00	0.22	0.748	o	|	|	|	|	1.01
54.250	0.00	0.22	0.746	o	|	|	|	|	1.00
54.333	0.00	0.22	0.745	o	|	|	|	|	1.00
54.417	0.00	0.22	0.743	o	|	|	|	|	1.00
54.500	0.00	0.22	0.742	o	|	|	|	|	1.00
54.583	0.00	0.22	0.740	o	|	|	|	|	1.00
54.667	0.00	0.22	0.739	o	|	|	|	|	0.99
54.750	0.00	0.22	0.737	o	|	|	|	|	0.99
54.833	0.00	0.22	0.736	o	|	|	|	|	0.99
54.917	0.00	0.22	0.734	o	|	|	|	|	0.99
55.000	0.00	0.22	0.733	o	|	|	|	|	0.99
55.083	0.00	0.21	0.731	o	|	|	|	|	0.98
55.167	0.00	0.21	0.730	o	|	|	|	|	0.98
55.250	0.00	0.21	0.728	o	|	|	|	|	0.98
55.333	0.00	0.21	0.727	o	|	|	|	|	0.98
55.417	0.00	0.21	0.725	o	|	|	|	|	0.98
55.500	0.00	0.21	0.724	o	|	|	|	|	0.97
55.583	0.00	0.21	0.723	o	|	|	|	|	0.97
55.667	0.00	0.21	0.721	o	|	|	|	|	0.97
55.750	0.00	0.21	0.720	o	|	|	|	|	0.97
55.833	0.00	0.21	0.718	o	|	|	|	|	0.97
55.917	0.00	0.21	0.717	o	|	|	|	|	0.96
56.000	0.00	0.21	0.715	o	|	|	|	|	0.96
56.083	0.00	0.21	0.714	o	|	|	|	|	0.96
56.167	0.00	0.21	0.712	o	|	|	|	|	0.96
56.250	0.00	0.21	0.711	o	|	|	|	|	0.96
56.333	0.00	0.21	0.709	o	|	|	|	|	0.95
56.417	0.00	0.21	0.708	o	|	|	|	|	0.95
56.500	0.00	0.21	0.707	o	|	|	|	|	0.95
56.583	0.00	0.21	0.705	o	|	|	|	|	0.95
56.667	0.00	0.21	0.704	o	|	|	|	|	0.95
56.750	0.00	0.21	0.702	o	|	|	|	|	0.95
56.833	0.00	0.21	0.701	o	|	|	|	|	0.94
56.917	0.00	0.21	0.700	o	|	|	|	|	0.94
57.000	0.00	0.20	0.698	o	|	|	|	|	0.94
57.083	0.00	0.20	0.697	o	|	|	|	|	0.94
57.167	0.00	0.20	0.695	o	|	|	|	|	0.94
57.250	0.00	0.20	0.694	o	|	|	|	|	0.93
57.333	0.00	0.20	0.692	o	|	|	|	|	0.93
57.417	0.00	0.20	0.691	o	|	|	|	|	0.93
57.500	0.00	0.20	0.690	o	|	|	|	|	0.93
57.583	0.00	0.20	0.688	o	|	|	|	|	0.93
57.667	0.00	0.20	0.687	o	|	|	|	|	0.92
57.750	0.00	0.20	0.686	o	|	|	|	|	0.92
57.833	0.00	0.20	0.684	o	|	|	|	|	0.92
57.917	0.00	0.20	0.683	o	|	|	|	|	0.92
58.000	0.00	0.20	0.681	o	|	|	|	|	0.92
58.083	0.00	0.20	0.680	o	|	|	|	|	0.92
58.167	0.00	0.20	0.679	o	|	|	|	|	0.91
58.250	0.00	0.20	0.677	o	|	|	|	|	0.91
58.333	0.00	0.20	0.676	o	|	|	|	|	0.91
58.417	0.00	0.20	0.675	o	|	|	|	|	0.91
58.500	0.00	0.20	0.673	o	|	|	|	|	0.91
58.583	0.00	0.20	0.672	o	|	|	|	|	0.90
58.667	0.00	0.20	0.670	o	|	|	|	|	0.90
58.750	0.00	0.20	0.669	o	|	|	|	|	0.90
58.833	0.00	0.20	0.668	o	|	|	|	|	0.90
58.917	0.00	0.20	0.666	o	|	|	|	|	0.90
59.000	0.00	0.20	0.665	o	|	|	|	|	0.90
59.083	0.00	0.19	0.664	o	|	|	|	|	0.89

59.167	0.00	0.19	0.662	o	|	|	|	0.89
59.250	0.00	0.19	0.661	o	|	|	|	0.89
59.333	0.00	0.19	0.660	o	|	|	|	0.89
59.417	0.00	0.19	0.658	o	|	|	|	0.89
59.500	0.00	0.19	0.657	o	|	|	|	0.88
59.583	0.00	0.19	0.656	o	|	|	|	0.88
59.667	0.00	0.19	0.654	o	|	|	|	0.88
59.750	0.00	0.19	0.653	o	|	|	|	0.88
59.833	0.00	0.19	0.652	o	|	|	|	0.88
59.917	0.00	0.19	0.650	o	|	|	|	0.88
60.000	0.00	0.19	0.649	o	|	|	|	0.87
60.083	0.00	0.19	0.648	o	|	|	|	0.87
60.167	0.00	0.19	0.647	o	|	|	|	0.87
60.250	0.00	0.19	0.645	o	|	|	|	0.87
60.333	0.00	0.19	0.644	o	|	|	|	0.87
60.417	0.00	0.19	0.643	o	|	|	|	0.86
60.500	0.00	0.19	0.641	o	|	|	|	0.86
60.583	0.00	0.19	0.640	o	|	|	|	0.86
60.667	0.00	0.19	0.639	o	|	|	|	0.86
60.750	0.00	0.19	0.637	o	|	|	|	0.86
60.833	0.00	0.19	0.636	o	|	|	|	0.86
60.917	0.00	0.19	0.635	o	|	|	|	0.85
61.000	0.00	0.19	0.634	o	|	|	|	0.85
61.083	0.00	0.19	0.632	o	|	|	|	0.85
61.167	0.00	0.19	0.631	o	|	|	|	0.85
61.250	0.00	0.18	0.630	o	|	|	|	0.85
61.333	0.00	0.18	0.628	o	|	|	|	0.85
61.417	0.00	0.18	0.627	o	|	|	|	0.84
61.500	0.00	0.18	0.626	o	|	|	|	0.84
61.583	0.00	0.18	0.625	o	|	|	|	0.84
61.667	0.00	0.18	0.623	o	|	|	|	0.84
61.750	0.00	0.18	0.622	o	|	|	|	0.84
61.833	0.00	0.18	0.621	o	|	|	|	0.84
61.917	0.00	0.18	0.620	o	|	|	|	0.83
62.000	0.00	0.18	0.618	o	|	|	|	0.83
62.083	0.00	0.18	0.617	o	|	|	|	0.83
62.167	0.00	0.18	0.616	o	|	|	|	0.83
62.250	0.00	0.18	0.615	o	|	|	|	0.83
62.333	0.00	0.18	0.613	o	|	|	|	0.83
62.417	0.00	0.18	0.612	o	|	|	|	0.82
62.500	0.00	0.18	0.611	o	|	|	|	0.82
62.583	0.00	0.18	0.610	o	|	|	|	0.82
62.667	0.00	0.18	0.608	o	|	|	|	0.82
62.750	0.00	0.18	0.607	o	|	|	|	0.82
62.833	0.00	0.18	0.606	o	|	|	|	0.82
62.917	0.00	0.18	0.605	o	|	|	|	0.81
63.000	0.00	0.18	0.604	o	|	|	|	0.81
63.083	0.00	0.18	0.602	o	|	|	|	0.81
63.167	0.00	0.18	0.601	o	|	|	|	0.81
63.250	0.00	0.18	0.600	o	|	|	|	0.81
63.333	0.00	0.18	0.599	o	|	|	|	0.81
63.417	0.00	0.18	0.598	o	|	|	|	0.80
63.500	0.00	0.17	0.596	o	|	|	|	0.80
63.583	0.00	0.17	0.595	o	|	|	|	0.80
63.667	0.00	0.17	0.594	o	|	|	|	0.80
63.750	0.00	0.17	0.593	o	|	|	|	0.80
63.833	0.00	0.17	0.592	o	|	|	|	0.80
63.917	0.00	0.17	0.590	o	|	|	|	0.79
64.000	0.00	0.17	0.589	o	|	|	|	0.79
64.083	0.00	0.17	0.588	o	|	|	|	0.79
64.167	0.00	0.17	0.587	o	|	|	|	0.79
64.250	0.00	0.17	0.586	o	|	|	|	0.79
64.333	0.00	0.17	0.584	o	|	|	|	0.79
64.417	0.00	0.17	0.583	o	|	|	|	0.78
64.500	0.00	0.17	0.582	o	|	|	|	0.78
64.583	0.00	0.17	0.581	o	|	|	|	0.78
64.667	0.00	0.17	0.580	o	|	|	|	0.78
64.750	0.00	0.17	0.579	o	|	|	|	0.78
64.833	0.00	0.17	0.577	o	|	|	|	0.78
64.917	0.00	0.17	0.576	o	|	|	|	0.78
65.000	0.00	0.17	0.575	o	|	|	|	0.77
65.083	0.00	0.17	0.574	o	|	|	|	0.77
65.167	0.00	0.17	0.573	o	|	|	|	0.77
65.250	0.00	0.17	0.572	o	|	|	|	0.77
65.333	0.00	0.17	0.570	o	|	|	|	0.77
65.417	0.00	0.17	0.569	o	|	|	|	0.77
65.500	0.00	0.17	0.568	o	|	|	|	0.76
65.583	0.00	0.17	0.567	o	|	|	|	0.76
65.667	0.00	0.17	0.566	o	|	|	|	0.76
65.750	0.00	0.17	0.565	o	|	|	|	0.76
65.833	0.00	0.17	0.564	o	|	|	|	0.76
65.917	0.00	0.17	0.562	o	|	|	|	0.76
66.000	0.00	0.16	0.561	o	|	|	|	0.76
66.083	0.00	0.16	0.560	o	|	|	|	0.75
66.167	0.00	0.16	0.559	o	|	|	|	0.75
66.250	0.00	0.16	0.558	o	|	|	|	0.75

66.333	0.00	0.16	0.557	o	|	|	|	|	0.75
66.417	0.00	0.16	0.556	o	|	|	|	|	0.75
66.500	0.00	0.16	0.554	o	|	|	|	|	0.75
66.583	0.00	0.16	0.553	o	|	|	|	|	0.74
66.667	0.00	0.16	0.552	o	|	|	|	|	0.74
66.750	0.00	0.16	0.551	o	|	|	|	|	0.74
66.833	0.00	0.16	0.550	o	|	|	|	|	0.74
66.917	0.00	0.16	0.549	o	|	|	|	|	0.74
67.000	0.00	0.16	0.548	o	|	|	|	|	0.74
67.083	0.00	0.16	0.547	o	|	|	|	|	0.74
67.167	0.00	0.16	0.546	o	|	|	|	|	0.73
67.250	0.00	0.16	0.544	o	|	|	|	|	0.73
67.333	0.00	0.16	0.543	o	|	|	|	|	0.73
67.417	0.00	0.16	0.542	o	|	|	|	|	0.73
67.500	0.00	0.16	0.541	o	|	|	|	|	0.73
67.583	0.00	0.16	0.540	o	|	|	|	|	0.73
67.667	0.00	0.16	0.539	o	|	|	|	|	0.73
67.750	0.00	0.16	0.538	o	|	|	|	|	0.72
67.833	0.00	0.16	0.537	o	|	|	|	|	0.72
67.917	0.00	0.16	0.536	o	|	|	|	|	0.72
68.000	0.00	0.16	0.535	o	|	|	|	|	0.72
68.083	0.00	0.16	0.534	o	|	|	|	|	0.72
68.167	0.00	0.16	0.533	o	|	|	|	|	0.72
68.250	0.00	0.16	0.531	o	|	|	|	|	0.72
68.333	0.00	0.16	0.530	o	|	|	|	|	0.71
68.417	0.00	0.16	0.529	o	|	|	|	|	0.71
68.500	0.00	0.15	0.528	o	|	|	|	|	0.71
68.583	0.00	0.15	0.527	o	|	|	|	|	0.71
68.667	0.00	0.15	0.526	o	|	|	|	|	0.71
68.750	0.00	0.15	0.525	o	|	|	|	|	0.71
68.833	0.00	0.15	0.524	o	|	|	|	|	0.71
68.917	0.00	0.15	0.523	o	|	|	|	|	0.70
69.000	0.00	0.15	0.522	o	|	|	|	|	0.70
69.083	0.00	0.15	0.521	o	|	|	|	|	0.70
69.167	0.00	0.15	0.520	o	|	|	|	|	0.70
69.250	0.00	0.15	0.519	o	|	|	|	|	0.70
69.333	0.00	0.15	0.518	o	|	|	|	|	0.70
69.417	0.00	0.15	0.517	o	|	|	|	|	0.70
69.500	0.00	0.15	0.516	o	|	|	|	|	0.69
69.583	0.00	0.15	0.515	o	|	|	|	|	0.69
69.667	0.00	0.15	0.513	o	|	|	|	|	0.69
69.750	0.00	0.15	0.512	o	|	|	|	|	0.69
69.833	0.00	0.15	0.511	o	|	|	|	|	0.69
69.917	0.00	0.15	0.510	o	|	|	|	|	0.69
70.000	0.00	0.15	0.509	o	|	|	|	|	0.69
70.083	0.00	0.15	0.508	o	|	|	|	|	0.68
70.167	0.00	0.15	0.507	o	|	|	|	|	0.68
70.250	0.00	0.15	0.506	o	|	|	|	|	0.68
70.333	0.00	0.15	0.505	o	|	|	|	|	0.68
70.417	0.00	0.15	0.504	o	|	|	|	|	0.68
70.500	0.00	0.15	0.503	o	|	|	|	|	0.68
70.583	0.00	0.15	0.502	o	|	|	|	|	0.68
70.667	0.00	0.15	0.501	o	|	|	|	|	0.67
70.750	0.00	0.15	0.500	o	|	|	|	|	0.67
70.833	0.00	0.15	0.499	o	|	|	|	|	0.67
70.917	0.00	0.15	0.498	o	|	|	|	|	0.67
71.000	0.00	0.15	0.497	o	|	|	|	|	0.67
71.083	0.00	0.15	0.496	o	|	|	|	|	0.67
71.167	0.00	0.15	0.495	o	|	|	|	|	0.67
71.250	0.00	0.14	0.494	o	|	|	|	|	0.67
71.333	0.00	0.14	0.493	o	|	|	|	|	0.66
71.417	0.00	0.14	0.492	o	|	|	|	|	0.66
71.500	0.00	0.14	0.491	o	|	|	|	|	0.66
71.583	0.00	0.14	0.490	o	|	|	|	|	0.66
71.667	0.00	0.14	0.489	o	|	|	|	|	0.66
71.750	0.00	0.14	0.488	o	|	|	|	|	0.66
71.833	0.00	0.14	0.487	o	|	|	|	|	0.66
71.917	0.00	0.14	0.486	o	|	|	|	|	0.65
72.000	0.00	0.14	0.485	o	|	|	|	|	0.65
72.083	0.00	0.14	0.484	o	|	|	|	|	0.65
72.167	0.00	0.14	0.483	o	|	|	|	|	0.65
72.250	0.00	0.14	0.482	o	|	|	|	|	0.65
72.333	0.00	0.14	0.481	o	|	|	|	|	0.65
72.417	0.00	0.14	0.480	o	|	|	|	|	0.65
72.500	0.00	0.14	0.479	o	|	|	|	|	0.65
72.583	0.00	0.14	0.478	o	|	|	|	|	0.64
72.667	0.00	0.14	0.477	o	|	|	|	|	0.64
72.750	0.00	0.14	0.476	o	|	|	|	|	0.64
72.833	0.00	0.14	0.476	o	|	|	|	|	0.64
72.917	0.00	0.14	0.475	o	|	|	|	|	0.64
73.000	0.00	0.14	0.474	o	|	|	|	|	0.64
73.083	0.00	0.14	0.473	o	|	|	|	|	0.64
73.167	0.00	0.14	0.472	o	|	|	|	|	0.63
73.250	0.00	0.14	0.471	o	|	|	|	|	0.63
73.333	0.00	0.14	0.470	o	|	|	|	|	0.63
73.417	0.00	0.14	0.469	o	|	|	|	|	0.63

73.500	0.00	0.14	0.468	o	|	|	|	|	0.63
73.583	0.00	0.14	0.467	o	|	|	|	|	0.63
73.667	0.00	0.14	0.466	o	|	|	|	|	0.63
73.750	0.00	0.14	0.465	o	|	|	|	|	0.63
73.833	0.00	0.14	0.464	o	|	|	|	|	0.62
73.917	0.00	0.14	0.463	o	|	|	|	|	0.62
74.000	0.00	0.14	0.462	o	|	|	|	|	0.62
74.083	0.00	0.14	0.461	o	|	|	|	|	0.62
74.167	0.00	0.14	0.460	o	|	|	|	|	0.62
74.250	0.00	0.13	0.459	o	|	|	|	|	0.62
74.333	0.00	0.13	0.459	o	|	|	|	|	0.62
74.417	0.00	0.13	0.458	o	|	|	|	|	0.62
74.500	0.00	0.13	0.457	o	|	|	|	|	0.61
74.583	0.00	0.13	0.456	o	|	|	|	|	0.61
74.667	0.00	0.13	0.455	o	|	|	|	|	0.61
74.750	0.00	0.13	0.454	o	|	|	|	|	0.61
74.833	0.00	0.13	0.453	o	|	|	|	|	0.61
74.917	0.00	0.13	0.452	o	|	|	|	|	0.61
75.000	0.00	0.13	0.451	o	|	|	|	|	0.61
75.083	0.00	0.13	0.450	o	|	|	|	|	0.61
75.167	0.00	0.13	0.449	o	|	|	|	|	0.60
75.250	0.00	0.13	0.448	o	|	|	|	|	0.60
75.333	0.00	0.13	0.448	o	|	|	|	|	0.60
75.417	0.00	0.13	0.447	o	|	|	|	|	0.60
75.500	0.00	0.13	0.446	o	|	|	|	|	0.60
75.583	0.00	0.13	0.445	o	|	|	|	|	0.60
75.667	0.00	0.13	0.444	o	|	|	|	|	0.60
75.750	0.00	0.13	0.443	o	|	|	|	|	0.60
75.833	0.00	0.13	0.442	o	|	|	|	|	0.60
75.917	0.00	0.13	0.441	o	|	|	|	|	0.59
76.000	0.00	0.13	0.440	o	|	|	|	|	0.59
76.083	0.00	0.13	0.439	o	|	|	|	|	0.59
76.167	0.00	0.13	0.439	o	|	|	|	|	0.59
76.250	0.00	0.13	0.438	o	|	|	|	|	0.59
76.333	0.00	0.13	0.437	o	|	|	|	|	0.59
76.417	0.00	0.13	0.436	o	|	|	|	|	0.59
76.500	0.00	0.13	0.435	o	|	|	|	|	0.59
76.583	0.00	0.13	0.434	o	|	|	|	|	0.58
76.667	0.00	0.13	0.433	o	|	|	|	|	0.58
76.750	0.00	0.13	0.432	o	|	|	|	|	0.58
76.833	0.00	0.13	0.432	o	|	|	|	|	0.58
76.917	0.00	0.13	0.431	o	|	|	|	|	0.58
77.000	0.00	0.13	0.430	o	|	|	|	|	0.58
77.083	0.00	0.13	0.429	o	|	|	|	|	0.58
77.167	0.00	0.13	0.428	o	|	|	|	|	0.58
77.250	0.00	0.13	0.427	o	|	|	|	|	0.58
77.333	0.00	0.13	0.426	o	|	|	|	|	0.57
77.417	0.00	0.12	0.426	o	|	|	|	|	0.57
77.500	0.00	0.12	0.425	o	|	|	|	|	0.57
77.583	0.00	0.12	0.424	o	|	|	|	|	0.57
77.667	0.00	0.12	0.423	o	|	|	|	|	0.57
77.750	0.00	0.12	0.422	o	|	|	|	|	0.57
77.833	0.00	0.12	0.421	o	|	|	|	|	0.57
77.917	0.00	0.12	0.420	o	|	|	|	|	0.57
78.000	0.00	0.12	0.420	o	|	|	|	|	0.56
78.083	0.00	0.12	0.419	o	|	|	|	|	0.56
78.167	0.00	0.12	0.418	o	|	|	|	|	0.56
78.250	0.00	0.12	0.417	o	|	|	|	|	0.56
78.333	0.00	0.12	0.416	o	|	|	|	|	0.56
78.417	0.00	0.12	0.415	o	|	|	|	|	0.56
78.500	0.00	0.12	0.414	o	|	|	|	|	0.56
78.583	0.00	0.12	0.414	o	|	|	|	|	0.56
78.667	0.00	0.12	0.413	o	|	|	|	|	0.56
78.750	0.00	0.12	0.412	o	|	|	|	|	0.55
78.833	0.00	0.12	0.411	o	|	|	|	|	0.55
78.917	0.00	0.12	0.410	o	|	|	|	|	0.55
79.000	0.00	0.12	0.409	o	|	|	|	|	0.55
79.083	0.00	0.12	0.409	o	|	|	|	|	0.55
79.167	0.00	0.12	0.408	o	|	|	|	|	0.55
79.250	0.00	0.12	0.407	o	|	|	|	|	0.55
79.333	0.00	0.12	0.406	o	|	|	|	|	0.55
79.417	0.00	0.12	0.405	o	|	|	|	|	0.55
79.500	0.00	0.12	0.405	o	|	|	|	|	0.54
79.583	0.00	0.12	0.404	o	|	|	|	|	0.54
79.667	0.00	0.12	0.403	o	|	|	|	|	0.54
79.750	0.00	0.12	0.402	o	|	|	|	|	0.54
79.833	0.00	0.12	0.401	o	|	|	|	|	0.54
79.917	0.00	0.12	0.400	o	|	|	|	|	0.54
80.000	0.00	0.12	0.400	o	|	|	|	|	0.54
80.083	0.00	0.12	0.399	o	|	|	|	|	0.54
80.167	0.00	0.12	0.398	o	|	|	|	|	0.54
80.250	0.00	0.12	0.397	o	|	|	|	|	0.53
80.333	0.00	0.12	0.396	o	|	|	|	|	0.53
80.417	0.00	0.12	0.396	o	|	|	|	|	0.53
80.500	0.00	0.12	0.395	o	|	|	|	|	0.53
80.583	0.00	0.12	0.394	o	|	|	|	|	0.53

80.667	0.00	0.12	0.393	o					0.53
80.750	0.00	0.12	0.392	o					0.53
80.833	0.00	0.11	0.392	o					0.53
80.917	0.00	0.11	0.391	o					0.53
81.000	0.00	0.11	0.390	o					0.53
81.083	0.00	0.11	0.389	o					0.52
81.167	0.00	0.11	0.389	o					0.52
81.250	0.00	0.11	0.388	o					0.52
81.333	0.00	0.11	0.387	o					0.52
81.417	0.00	0.11	0.386	o					0.52
81.500	0.00	0.11	0.385	o					0.52
81.583	0.00	0.11	0.385	o					0.52
81.667	0.00	0.11	0.384	o					0.52
81.750	0.00	0.11	0.383	o					0.52
81.833	0.00	0.11	0.382	o					0.51
81.917	0.00	0.11	0.382	o					0.51
82.000	0.00	0.11	0.381	o					0.51
82.083	0.00	0.11	0.380	o					0.51
82.167	0.00	0.11	0.379	o					0.51
82.250	0.00	0.11	0.378	o					0.51
82.333	0.00	0.11	0.378	o					0.51
82.417	0.00	0.11	0.377	o					0.51
82.500	0.00	0.11	0.376	o					0.51
82.583	0.00	0.11	0.375	o					0.51
82.667	0.00	0.11	0.375	o					0.50
82.750	0.00	0.11	0.374	o					0.50
82.833	0.00	0.11	0.373	o					0.50
82.917	0.00	0.11	0.372	o					0.50
83.000	0.00	0.11	0.372	o					0.50
83.083	0.00	0.11	0.371	o					0.50
83.167	0.00	0.11	0.370	o					0.50
83.250	0.00	0.11	0.369	o					0.50
83.333	0.00	0.11	0.369	o					0.50
83.417	0.00	0.11	0.368	o					0.50
83.500	0.00	0.11	0.367	o					0.49
83.583	0.00	0.11	0.366	o					0.49
83.667	0.00	0.11	0.366	o					0.49
83.750	0.00	0.11	0.365	o					0.49
83.833	0.00	0.11	0.364	o					0.49
83.917	0.00	0.11	0.363	o					0.49
84.000	0.00	0.11	0.363	o					0.49
84.083	0.00	0.11	0.362	o					0.49
84.167	0.00	0.11	0.361	o					0.49
84.250	0.00	0.11	0.361	o					0.49
84.333	0.00	0.11	0.360	o					0.48
84.417	0.00	0.11	0.359	o					0.48
84.500	0.00	0.11	0.358	o					0.48
84.583	0.00	0.10	0.358	o					0.48
84.667	0.00	0.10	0.357	o					0.48
84.750	0.00	0.10	0.356	o					0.48
84.833	0.00	0.10	0.355	o					0.48
84.917	0.00	0.10	0.355	o					0.48
85.000	0.00	0.10	0.354	o					0.48
85.083	0.00	0.10	0.353	o					0.48
85.167	0.00	0.10	0.353	o					0.47
85.250	0.00	0.10	0.352	o					0.47
85.333	0.00	0.10	0.351	o					0.47
85.417	0.00	0.10	0.350	o					0.47
85.500	0.00	0.10	0.350	o					0.47
85.583	0.00	0.10	0.349	o					0.47
85.667	0.00	0.10	0.348	o					0.47
85.750	0.00	0.10	0.348	o					0.47
85.833	0.00	0.10	0.347	o					0.47
85.917	0.00	0.10	0.346	o					0.47
86.000	0.00	0.10	0.346	o					0.47
86.083	0.00	0.10	0.345	o					0.46
86.167	0.00	0.10	0.344	o					0.46
86.250	0.00	0.10	0.343	o					0.46
86.333	0.00	0.10	0.343	o					0.46
86.417	0.00	0.10	0.342	o					0.46
86.500	0.00	0.10	0.341	o					0.46
86.583	0.00	0.10	0.341	o					0.4

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 1039
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 9.515 (CFS)
Total volume = 4.480 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro11001100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 17
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 80.047 (CFS)
Total volume = 2.753 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 17
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 20.0 40.02 60.04 80.05	Depth (Ft.)
0.083	3.94	0.00	0.014	OI	0.02
0.167	10.90	0.02	0.065	O I	0.09
0.250	14.34	0.04	0.151	O I	0.20
0.333	16.32	0.08	0.256	O I	0.35
0.417	18.25	0.11	0.375	O I	0.50
0.500	20.91	0.15	0.509	O I	0.68
0.583	24.07	0.19	0.662	O I	0.89
0.667	28.60	0.27	0.842	O I	1.12
0.750	40.09	0.40	1.076	O I	1.41
0.833	75.28	0.62	1.470	O I	1.89
0.917	80.05	1.08	1.999	O I	2.49
1.000	37.03	1.46	2.394	O I	2.93
1.083	18.42	11.54	2.540	O I	3.09
1.167	7.20	12.28	2.546	I O	3.09
1.250	3.32	8.19	2.512	I O	3.06
1.333	0.78	4.61	2.482	IO	3.03
1.417	0.21	2.20	2.462	O	3.01
1.500	0.00	1.51	2.450	O	2.99
1.583	0.00	1.50	2.439	O	2.98
1.667	0.00	1.49	2.429	O	2.97
1.750	0.00	1.48	2.419	O	2.96

1.833	0.00	1.47	2.409	o	|	|	|	|	2.95
1.917	0.00	1.46	2.398	o	|	|	|	|	2.94
2.000	0.00	1.45	2.388	o	|	|	|	|	2.92
2.083	0.00	1.44	2.378	o	|	|	|	|	2.91
2.167	0.00	1.43	2.368	o	|	|	|	|	2.90
2.250	0.00	1.43	2.359	o	|	|	|	|	2.89
2.333	0.00	1.42	2.349	o	|	|	|	|	2.88
2.417	0.00	1.41	2.339	o	|	|	|	|	2.87
2.500	0.00	1.40	2.329	o	|	|	|	|	2.86
2.583	0.00	1.39	2.320	o	|	|	|	|	2.85
2.667	0.00	1.38	2.310	o	|	|	|	|	2.84
2.750	0.00	1.37	2.301	o	|	|	|	|	2.83
2.833	0.00	1.36	2.291	o	|	|	|	|	2.82
2.917	0.00	1.35	2.282	o	|	|	|	|	2.81
3.000	0.00	1.34	2.273	o	|	|	|	|	2.80
3.083	0.00	1.34	2.264	o	|	|	|	|	2.79
3.167	0.00	1.33	2.254	o	|	|	|	|	2.77
3.250	0.00	1.32	2.245	o	|	|	|	|	2.76
3.333	0.00	1.31	2.236	o	|	|	|	|	2.75
3.417	0.00	1.30	2.227	o	|	|	|	|	2.74
3.500	0.00	1.29	2.218	o	|	|	|	|	2.73
3.583	0.00	1.28	2.209	o	|	|	|	|	2.72
3.667	0.00	1.28	2.201	o	|	|	|	|	2.71
3.750	0.00	1.27	2.192	o	|	|	|	|	2.70
3.833	0.00	1.26	2.183	o	|	|	|	|	2.70
3.917	0.00	1.25	2.175	o	|	|	|	|	2.69
4.000	0.00	1.24	2.166	o	|	|	|	|	2.68
4.083	0.00	1.23	2.157	o	|	|	|	|	2.67
4.167	0.00	1.23	2.149	o	|	|	|	|	2.66
4.250	0.00	1.22	2.141	o	|	|	|	|	2.65
4.333	0.00	1.21	2.132	o	|	|	|	|	2.64
4.417	0.00	1.20	2.124	o	|	|	|	|	2.63
4.500	0.00	1.19	2.116	o	|	|	|	|	2.62
4.583	0.00	1.19	2.107	o	|	|	|	|	2.61
4.667	0.00	1.18	2.099	o	|	|	|	|	2.60
4.750	0.00	1.17	2.091	o	|	|	|	|	2.59
4.833	0.00	1.16	2.083	o	|	|	|	|	2.58
4.917	0.00	1.16	2.075	o	|	|	|	|	2.57
5.000	0.00	1.15	2.067	o	|	|	|	|	2.57
5.083	0.00	1.14	2.059	o	|	|	|	|	2.56
5.167	0.00	1.13	2.052	o	|	|	|	|	2.55
5.250	0.00	1.13	2.044	o	|	|	|	|	2.54
5.333	0.00	1.12	2.036	o	|	|	|	|	2.53
5.417	0.00	1.11	2.028	o	|	|	|	|	2.52
5.500	0.00	1.10	2.021	o	|	|	|	|	2.51
5.583	0.00	1.10	2.013	o	|	|	|	|	2.51
5.667	0.00	1.09	2.006	o	|	|	|	|	2.50
5.750	0.00	1.08	1.998	o	|	|	|	|	2.49
5.833	0.00	1.08	1.991	o	|	|	|	|	2.48
5.917	0.00	1.07	1.983	o	|	|	|	|	2.47
6.000	0.00	1.06	1.976	o	|	|	|	|	2.46
6.083	0.00	1.06	1.969	o	|	|	|	|	2.46
6.167	0.00	1.05	1.961	o	|	|	|	|	2.45
6.250	0.00	1.04	1.954	o	|	|	|	|	2.44
6.333	0.00	1.03	1.947	o	|	|	|	|	2.43
6.417	0.00	1.03	1.940	o	|	|	|	|	2.42
6.500	0.00	1.02	1.933	o	|	|	|	|	2.42
6.583	0.00	1.01	1.926	o	|	|	|	|	2.41
6.667	0.00	1.01	1.919	o	|	|	|	|	2.40
6.750	0.00	1.00	1.912	o	|	|	|	|	2.39
6.833	0.00	0.99	1.905	o	|	|	|	|	2.38
6.917	0.00	0.99	1.898	o	|	|	|	|	2.38
7.000	0.00	0.98	1.892	o	|	|	|	|	2.37
7.083	0.00	0.98	1.885	o	|	|	|	|	2.36
7.167	0.00	0.97	1.878	o	|	|	|	|	2.35
7.250	0.00	0.96	1.871	o	|	|	|	|	2.35
7.333	0.00	0.96	1.865	o	|	|	|	|	2.34
7.417	0.00	0.95	1.858	o	|	|	|	|	2.33
7.500	0.00	0.94	1.852	o	|	|	|	|	2.32
7.583	0.00	0.94	1.845	o	|	|	|	|	2.32
7.667	0.00	0.93	1.839	o	|	|	|	|	2.31
7.750	0.00	0.93	1.832	o	|	|	|	|	2.30
7.833	0.00	0.92	1.826	o	|	|	|	|	2.30
7.917	0.00	0.91	1.820	o	|	|	|	|	2.29
8.000	0.00	0.91	1.813	o	|	|	|	|	2.28
8.083	0.00	0.90	1.807	o	|	|	|	|	2.28
8.167	0.00	0.90	1.801	o	|	|	|	|	2.27
8.250	0.00	0.89	1.795	o	|	|	|	|	2.26
8.333	0.00	0.88	1.789	o	|	|	|	|	2.25
8.417	0.00	0.88	1.783	o	|	|	|	|	2.25
8.500	0.00	0.87	1.777	o	|	|	|	|	2.24
8.583	0.00	0.87	1.771	o	|	|	|	|	2.23
8.667	0.00	0.86	1.765	o	|	|	|	|	2.23
8.750	0.00	0.86	1.759	o	|	|	|	|	2.22
8.833	0.00	0.85	1.753	o	|	|	|	|	2.21
8.917	0.00	0.84	1.747	o	|	|	|	|	2.21

9.000	0.00	0.84	1.741	o	|	|	|	|	2.20
9.083	0.00	0.83	1.736	o	|	|	|	|	2.20
9.167	0.00	0.83	1.730	o	|	|	|	|	2.19
9.250	0.00	0.82	1.724	o	|	|	|	|	2.18
9.333	0.00	0.82	1.718	o	|	|	|	|	2.18
9.417	0.00	0.81	1.713	o	|	|	|	|	2.17
9.500	0.00	0.81	1.707	o	|	|	|	|	2.16
9.583	0.00	0.80	1.702	o	|	|	|	|	2.16
9.667	0.00	0.80	1.696	o	|	|	|	|	2.15
9.750	0.00	0.79	1.691	o	|	|	|	|	2.15
9.833	0.00	0.79	1.685	o	|	|	|	|	2.14
9.917	0.00	0.78	1.680	o	|	|	|	|	2.13
10.000	0.00	0.78	1.675	o	|	|	|	|	2.13
10.083	0.00	0.77	1.669	o	|	|	|	|	2.12
10.167	0.00	0.77	1.664	o	|	|	|	|	2.12
10.250	0.00	0.76	1.659	o	|	|	|	|	2.11
10.333	0.00	0.76	1.654	o	|	|	|	|	2.10
10.417	0.00	0.75	1.648	o	|	|	|	|	2.10
10.500	0.00	0.75	1.643	o	|	|	|	|	2.09
10.583	0.00	0.74	1.638	o	|	|	|	|	2.09
10.667	0.00	0.74	1.633	o	|	|	|	|	2.08
10.750	0.00	0.73	1.628	o	|	|	|	|	2.07
10.833	0.00	0.73	1.623	o	|	|	|	|	2.07
10.917	0.00	0.72	1.618	o	|	|	|	|	2.06
11.000	0.00	0.72	1.613	o	|	|	|	|	2.06
11.083	0.00	0.71	1.608	o	|	|	|	|	2.05
11.167	0.00	0.71	1.603	o	|	|	|	|	2.05
11.250	0.00	0.70	1.598	o	|	|	|	|	2.04
11.333	0.00	0.70	1.593	o	|	|	|	|	2.04
11.417	0.00	0.69	1.589	o	|	|	|	|	2.03
11.500	0.00	0.69	1.584	o	|	|	|	|	2.03
11.583	0.00	0.69	1.579	o	|	|	|	|	2.02
11.667	0.00	0.68	1.574	o	|	|	|	|	2.01
11.750	0.00	0.68	1.570	o	|	|	|	|	2.01
11.833	0.00	0.67	1.565	o	|	|	|	|	2.00
11.917	0.00	0.67	1.560	o	|	|	|	|	2.00
12.000	0.00	0.67	1.556	o	|	|	|	|	1.99
12.083	0.00	0.66	1.551	o	|	|	|	|	1.99
12.167	0.00	0.66	1.547	o	|	|	|	|	1.98
12.250	0.00	0.66	1.542	o	|	|	|	|	1.98
12.333	0.00	0.66	1.538	o	|	|	|	|	1.97
12.417	0.00	0.65	1.533	o	|	|	|	|	1.97
12.500	0.00	0.65	1.529	o	|	|	|	|	1.96
12.583	0.00	0.65	1.524	o	|	|	|	|	1.96
12.667	0.00	0.65	1.520	o	|	|	|	|	1.95
12.750	0.00	0.64	1.515	o	|	|	|	|	1.94
12.833	0.00	0.64	1.511	o	|	|	|	|	1.94
12.917	0.00	0.64	1.507	o	|	|	|	|	1.93
13.000	0.00	0.64	1.502	o	|	|	|	|	1.93
13.083	0.00	0.63	1.498	o	|	|	|	|	1.92
13.167	0.00	0.63	1.493	o	|	|	|	|	1.92
13.250	0.00	0.63	1.489	o	|	|	|	|	1.91
13.333	0.00	0.63	1.485	o	|	|	|	|	1.91
13.417	0.00	0.62	1.480	o	|	|	|	|	1.90
13.500	0.00	0.62	1.476	o	|	|	|	|	1.90
13.583	0.00	0.62	1.472	o	|	|	|	|	1.89
13.667	0.00	0.62	1.468	o	|	|	|	|	1.89
13.750	0.00	0.61	1.463	o	|	|	|	|	1.88
13.833	0.00	0.61	1.459	o	|	|	|	|	1.88
13.917	0.00	0.61	1.455	o	|	|	|	|	1.87
14.000	0.00	0.61	1.451	o	|	|	|	|	1.87
14.083	0.00	0.61	1.447	o	|	|	|	|	1.86
14.167	0.00	0.60	1.442	o	|	|	|	|	1.86
14.250	0.00	0.60	1.438	o	|	|	|	|	1.85
14.333	0.00	0.60	1.434	o	|	|	|	|	1.84
14.417	0.00	0.60	1.430	o	|	|	|	|	1.84
14.500	0.00	0.59	1.426	o	|	|	|	|	1.83
14.583	0.00	0.59	1.422	o	|	|	|	|	1.83
14.667	0.00	0.59	1.418	o	|	|	|	|	1.82
14.750	0.00	0.59	1.414	o	|	|	|	|	1.82
14.833	0.00	0.58	1.410	o	|	|	|	|	1.82
14.917	0.00	0.58	1.406	o	|	|	|	|	1.81
15.000	0.00	0.58	1.402	o	|	|	|	|	1.81
15.083	0.00	0.58	1.398	o	|	|	|	|	1.80
15.167	0.00	0.58	1.394	o	|	|	|	|	1.80
15.250	0.00	0.57	1.390	o	|	|	|	|	1.79
15.333	0.00	0.57	1.386	o	|	|	|	|	1.79
15.417	0.00	0.57	1.382	o	|	|	|	|	1.78
15.500	0.00	0.57	1.378	o	|	|	|	|	1.78
15.583	0.00	0.57	1.374	o	|	|	|	|	1.77
15.667	0.00	0.56	1.370	o	|	|	|	|	1.77
15.750	0.00	0.56	1.366	o	|	|	|	|	1.76
15.833	0.00	0.56	1.363	o	|	|	|	|	1.76
15.917	0.00	0.56	1.359	o	|	|	|	|	1.75
16.000	0.00	0.55	1.355	o	|	|	|	|	1.75
16.083	0.00	0.55	1.351	o	|	|	|	|	1.74

16.167	0.00	0.55	1.347	o	|	|	|	|	1.74
16.250	0.00	0.55	1.343	o	|	|	|	|	1.73
16.333	0.00	0.55	1.340	o	|	|	|	|	1.73
16.417	0.00	0.54	1.336	o	|	|	|	|	1.72
16.500	0.00	0.54	1.332	o	|	|	|	|	1.72
16.583	0.00	0.54	1.328	o	|	|	|	|	1.72
16.667	0.00	0.54	1.325	o	|	|	|	|	1.71
16.750	0.00	0.54	1.321	o	|	|	|	|	1.71
16.833	0.00	0.53	1.317	o	|	|	|	|	1.70
16.917	0.00	0.53	1.314	o	|	|	|	|	1.70
17.000	0.00	0.53	1.310	o	|	|	|	|	1.69
17.083	0.00	0.53	1.306	o	|	|	|	|	1.69
17.167	0.00	0.53	1.303	o	|	|	|	|	1.68
17.250	0.00	0.52	1.299	o	|	|	|	|	1.68
17.333	0.00	0.52	1.296	o	|	|	|	|	1.68
17.417	0.00	0.52	1.292	o	|	|	|	|	1.67
17.500	0.00	0.52	1.288	o	|	|	|	|	1.67
17.583	0.00	0.52	1.285	o	|	|	|	|	1.66
17.667	0.00	0.51	1.281	o	|	|	|	|	1.66
17.750	0.00	0.51	1.278	o	|	|	|	|	1.65
17.833	0.00	0.51	1.274	o	|	|	|	|	1.65
17.917	0.00	0.51	1.271	o	|	|	|	|	1.65
18.000	0.00	0.51	1.267	o	|	|	|	|	1.64
18.083	0.00	0.50	1.264	o	|	|	|	|	1.64
18.167	0.00	0.50	1.260	o	|	|	|	|	1.63
18.250	0.00	0.50	1.257	o	|	|	|	|	1.63
18.333	0.00	0.50	1.253	o	|	|	|	|	1.62
18.417	0.00	0.50	1.250	o	|	|	|	|	1.62
18.500	0.00	0.50	1.247	o	|	|	|	|	1.62
18.583	0.00	0.49	1.243	o	|	|	|	|	1.61
18.667	0.00	0.49	1.240	o	|	|	|	|	1.61
18.750	0.00	0.49	1.236	o	|	|	|	|	1.60
18.833	0.00	0.49	1.233	o	|	|	|	|	1.60
18.917	0.00	0.49	1.230	o	|	|	|	|	1.59
19.000	0.00	0.48	1.226	o	|	|	|	|	1.59
19.083	0.00	0.48	1.223	o	|	|	|	|	1.59
19.167	0.00	0.48	1.220	o	|	|	|	|	1.58
19.250	0.00	0.48	1.216	o	|	|	|	|	1.58
19.333	0.00	0.48	1.213	o	|	|	|	|	1.57
19.417	0.00	0.47	1.210	o	|	|	|	|	1.57
19.500	0.00	0.47	1.207	o	|	|	|	|	1.57
19.583	0.00	0.47	1.203	o	|	|	|	|	1.56
19.667	0.00	0.47	1.200	o	|	|	|	|	1.56
19.750	0.00	0.47	1.197	o	|	|	|	|	1.55
19.833	0.00	0.47	1.194	o	|	|	|	|	1.55
19.917	0.00	0.46	1.190	o	|	|	|	|	1.55
20.000	0.00	0.46	1.187	o	|	|	|	|	1.54
20.083	0.00	0.46	1.184	o	|	|	|	|	1.54
20.167	0.00	0.46	1.181	o	|	|	|	|	1.54
20.250	0.00	0.46	1.178	o	|	|	|	|	1.53
20.333	0.00	0.46	1.175	o	|	|	|	|	1.53
20.417	0.00	0.45	1.171	o	|	|	|	|	1.52
20.500	0.00	0.45	1.168	o	|	|	|	|	1.52
20.583	0.00	0.45	1.165	o	|	|	|	|	1.52
20.667	0.00	0.45	1.162	o	|	|	|	|	1.51
20.750	0.00	0.45	1.159	o	|	|	|	|	1.51
20.833	0.00	0.45	1.156	o	|	|	|	|	1.50
20.917	0.00	0.44	1.153	o	|	|	|	|	1.50
21.000	0.00	0.44	1.150	o	|	|	|	|	1.50
21.083	0.00	0.44	1.147	o	|	|	|	|	1.49
21.167	0.00	0.44	1.144	o	|	|	|	|	1.49
21.250	0.00	0.44	1.141	o	|	|	|	|	1.49
21.333	0.00	0.44	1.138	o	|	|	|	|	1.48
21.417	0.00	0.43	1.135	o	|	|	|	|	1.48
21.500	0.00	0.43	1.132	o	|	|	|	|	1.48
21.583	0.00	0.43	1.129	o	|	|	|	|	1.47
21.667	0.00	0.43	1.126	o	|	|	|	|	1.47
21.750	0.00	0.43	1.123	o	|	|	|	|	1.46
21.833	0.00	0.43	1.120	o	|	|	|	|	1.46
21.917	0.00	0.42	1.117	o	|	|	|	|	1.46
22.000	0.00	0.42	1.114	o	|	|	|	|	1.45
22.083	0.00	0.42	1.111	o	|	|	|	|	1.45
22.167	0.00	0.42	1.108	o	|	|	|	|	1.45
22.250	0.00	0.42	1.105	o	|	|	|	|	1.44
22.333	0.00	0.42	1.103	o	|	|	|	|	1.44
22.417	0.00	0.41	1.100	o	|	|	|	|	1.44
22.500	0.00	0.41	1.097	o	|	|	|	|	1.43
22.583	0.00	0.41	1.094	o	|	|	|	|	1.43
22.667	0.00	0.41	1.091	o	|	|	|	|	1.43
22.750	0.00	0.41	1.088	o	|	|	|	|	1.42
22.833	0.00	0.41	1.086	o	|	|	|	|	1.42
22.917	0.00	0.40	1.083	o	|	|	|	|	1.42
23.000	0.00	0.40	1.080	o	|	|	|	|	1.41
23.083	0.00	0.40	1.077	o	|	|	|	|	1.41
23.167	0.00	0.40	1.075	o	|	|	|	|	1.41
23.250	0.00	0.40	1.072	o	|	|	|	|	1.40

23.333	0.00	0.40	1.069	o	|	|	|	|	1.40
23.417	0.00	0.40	1.066	o	|	|	|	|	1.40
23.500	0.00	0.39	1.064	o	|	|	|	|	1.39
23.583	0.00	0.39	1.061	o	|	|	|	|	1.39
23.667	0.00	0.39	1.058	o	|	|	|	|	1.39
23.750	0.00	0.39	1.055	o	|	|	|	|	1.38
23.833	0.00	0.39	1.053	o	|	|	|	|	1.38
23.917	0.00	0.39	1.050	o	|	|	|	|	1.38
24.000	0.00	0.39	1.047	o	|	|	|	|	1.37
24.083	0.00	0.38	1.045	o	|	|	|	|	1.37
24.167	0.00	0.38	1.042	o	|	|	|	|	1.37
24.250	0.00	0.38	1.040	o	|	|	|	|	1.36
24.333	0.00	0.38	1.037	o	|	|	|	|	1.36
24.417	0.00	0.38	1.034	o	|	|	|	|	1.36
24.500	0.00	0.38	1.032	o	|	|	|	|	1.35
24.583	0.00	0.38	1.029	o	|	|	|	|	1.35
24.667	0.00	0.37	1.027	o	|	|	|	|	1.35
24.750	0.00	0.37	1.024	o	|	|	|	|	1.34
24.833	0.00	0.37	1.021	o	|	|	|	|	1.34
24.917	0.00	0.37	1.019	o	|	|	|	|	1.34
25.000	0.00	0.37	1.016	o	|	|	|	|	1.33
25.083	0.00	0.37	1.014	o	|	|	|	|	1.33
25.167	0.00	0.37	1.011	o	|	|	|	|	1.33
25.250	0.00	0.36	1.009	o	|	|	|	|	1.32
25.333	0.00	0.36	1.006	o	|	|	|	|	1.32
25.417	0.00	0.36	1.004	o	|	|	|	|	1.32
25.500	0.00	0.36	1.001	o	|	|	|	|	1.32
25.583	0.00	0.36	0.999	o	|	|	|	|	1.31
25.667	0.00	0.36	0.996	o	|	|	|	|	1.31
25.750	0.00	0.36	0.994	o	|	|	|	|	1.31
25.833	0.00	0.35	0.991	o	|	|	|	|	1.30
25.917	0.00	0.35	0.989	o	|	|	|	|	1.30
26.000	0.00	0.35	0.987	o	|	|	|	|	1.30
26.083	0.00	0.35	0.984	o	|	|	|	|	1.29
26.167	0.00	0.35	0.982	o	|	|	|	|	1.29
26.250	0.00	0.35	0.979	o	|	|	|	|	1.29
26.333	0.00	0.35	0.977	o	|	|	|	|	1.29
26.417	0.00	0.35	0.975	o	|	|	|	|	1.28
26.500	0.00	0.34	0.972	o	|	|	|	|	1.28
26.583	0.00	0.34	0.970	o	|	|	|	|	1.28
26.667	0.00	0.34	0.967	o	|	|	|	|	1.27
26.750	0.00	0.34	0.965	o	|	|	|	|	1.27
26.833	0.00	0.34	0.963	o	|	|	|	|	1.27
26.917	0.00	0.34	0.960	o	|	|	|	|	1.27
27.000	0.00	0.34	0.958	o	|	|	|	|	1.26
27.083	0.00	0.34	0.956	o	|	|	|	|	1.26
27.167	0.00	0.33	0.953	o	|	|	|	|	1.26
27.250	0.00	0.33	0.951	o	|	|	|	|	1.25
27.333	0.00	0.33	0.949	o	|	|	|	|	1.25
27.417	0.00	0.33	0.947	o	|	|	|	|	1.25
27.500	0.00	0.33	0.944	o	|	|	|	|	1.25
27.583	0.00	0.33	0.942	o	|	|	|	|	1.24
27.667	0.00	0.33	0.940	o	|	|	|	|	1.24
27.750	0.00	0.33	0.938	o	|	|	|	|	1.24
27.833	0.00	0.32	0.935	o	|	|	|	|	1.24
27.917	0.00	0.32	0.933	o	|	|	|	|	1.23
28.000	0.00	0.32	0.931	o	|	|	|	|	1.23
28.083	0.00	0.32	0.929	o	|	|	|	|	1.23
28.167	0.00	0.32	0.927	o	|	|	|	|	1.22
28.250	0.00	0.32	0.924	o	|	|	|	|	1.22
28.333	0.00	0.32	0.922	o	|	|	|	|	1.22
28.417	0.00	0.32	0.920	o	|	|	|	|	1.22
28.500	0.00	0.31	0.918	o	|	|	|	|	1.21
28.583	0.00	0.31	0.916	o	|	|	|	|	1.21
28.667	0.00	0.31	0.913	o	|	|	|	|	1.21
28.750	0.00	0.31	0.911	o	|	|	|	|	1.21
28.833	0.00	0.31	0.909	o	|	|	|	|	1.20
28.917	0.00	0.31	0.907	o	|	|	|	|	1.20
29.000	0.00	0.31	0.905	o	|	|	|	|	1.20
29.083	0.00	0.31	0.903	o	|	|	|	|	1.20
29.167	0.00	0.30	0.901	o	|	|	|	|	1.19
29.250	0.00	0.30	0.899	o	|	|	|	|	1.19
29.333	0.00	0.30	0.897	o	|	|	|	|	1.19
29.417	0.00	0.30	0.894	o	|	|	|	|	1.19
29.500	0.00	0.30	0.892	o	|	|	|	|	1.18
29.583	0.00	0.30	0.890	o	|	|	|	|	1.18
29.667	0.00	0.30	0.888	o	|	|	|	|	1.18
29.750	0.00	0.30	0.886	o	|	|	|	|	1.18
29.833	0.00	0.30	0.884	o	|	|	|	|	1.17
29.917	0.00	0.29	0.882	o	|	|	|	|	1.17
30.000	0.00	0.29	0.880	o	|	|	|	|	1.17
30.083	0.00	0.29	0.878	o	|	|	|	|	1.17
30.167	0.00	0.29	0.876	o	|	|	|	|	1.16
30.250	0.00	0.29	0.874	o	|	|	|	|	1.16
30.333	0.00	0.29	0.872	o	|	|	|	|	1.16
30.417	0.00	0.29	0.870	o	|	|	|	|	1.16

30.500	0.00	0.29	0.868	o	|	|	|	|	1.15
30.583	0.00	0.29	0.866	o	|	|	|	|	1.15
30.667	0.00	0.28	0.864	o	|	|	|	|	1.15
30.750	0.00	0.28	0.862	o	|	|	|	|	1.15
30.833	0.00	0.28	0.860	o	|	|	|	|	1.14
30.917	0.00	0.28	0.858	o	|	|	|	|	1.14
31.000	0.00	0.28	0.856	o	|	|	|	|	1.14
31.083	0.00	0.28	0.855	o	|	|	|	|	1.14
31.167	0.00	0.28	0.853	o	|	|	|	|	1.13
31.250	0.00	0.28	0.851	o	|	|	|	|	1.13
31.333	0.00	0.28	0.849	o	|	|	|	|	1.13
31.417	0.00	0.28	0.847	o	|	|	|	|	1.13
31.500	0.00	0.27	0.845	o	|	|	|	|	1.12
31.583	0.00	0.27	0.843	o	|	|	|	|	1.12
31.667	0.00	0.27	0.841	o	|	|	|	|	1.12
31.750	0.00	0.27	0.839	o	|	|	|	|	1.12
31.833	0.00	0.27	0.837	o	|	|	|	|	1.12
31.917	0.00	0.27	0.836	o	|	|	|	|	1.11
32.000	0.00	0.27	0.834	o	|	|	|	|	1.11
32.083	0.00	0.27	0.832	o	|	|	|	|	1.11
32.167	0.00	0.27	0.830	o	|	|	|	|	1.11
32.250	0.00	0.26	0.828	o	|	|	|	|	1.10
32.333	0.00	0.26	0.826	o	|	|	|	|	1.10
32.417	0.00	0.26	0.825	o	|	|	|	|	1.10
32.500	0.00	0.26	0.823	o	|	|	|	|	1.10
32.583	0.00	0.26	0.821	o	|	|	|	|	1.10
32.667	0.00	0.26	0.819	o	|	|	|	|	1.09
32.750	0.00	0.26	0.817	o	|	|	|	|	1.09
32.833	0.00	0.26	0.816	o	|	|	|	|	1.09
32.917	0.00	0.26	0.814	o	|	|	|	|	1.09
33.000	0.00	0.26	0.812	o	|	|	|	|	1.08
33.083	0.00	0.26	0.810	o	|	|	|	|	1.08
33.167	0.00	0.25	0.809	o	|	|	|	|	1.08
33.250	0.00	0.25	0.807	o	|	|	|	|	1.08
33.333	0.00	0.25	0.805	o	|	|	|	|	1.08
33.417	0.00	0.25	0.803	o	|	|	|	|	1.07
33.500	0.00	0.25	0.802	o	|	|	|	|	1.07
33.583	0.00	0.25	0.800	o	|	|	|	|	1.07
33.667	0.00	0.25	0.798	o	|	|	|	|	1.07
33.750	0.00	0.25	0.797	o	|	|	|	|	1.07
33.833	0.00	0.25	0.795	o	|	|	|	|	1.06
33.917	0.00	0.25	0.793	o	|	|	|	|	1.06
34.000	0.00	0.24	0.791	o	|	|	|	|	1.06
34.083	0.00	0.24	0.790	o	|	|	|	|	1.06
34.167	0.00	0.24	0.788	o	|	|	|	|	1.06
34.250	0.00	0.24	0.786	o	|	|	|	|	1.05
34.333	0.00	0.24	0.785	o	|	|	|	|	1.05
34.417	0.00	0.24	0.783	o	|	|	|	|	1.05
34.500	0.00	0.24	0.781	o	|	|	|	|	1.05
34.583	0.00	0.24	0.780	o	|	|	|	|	1.05
34.667	0.00	0.24	0.778	o	|	|	|	|	1.04
34.750	0.00	0.24	0.777	o	|	|	|	|	1.04
34.833	0.00	0.24	0.775	o	|	|	|	|	1.04
34.917	0.00	0.23	0.773	o	|	|	|	|	1.04
35.000	0.00	0.23	0.772	o	|	|	|	|	1.04
35.083	0.00	0.23	0.770	o	|	|	|	|	1.03
35.167	0.00	0.23	0.768	o	|	|	|	|	1.03
35.250	0.00	0.23	0.767	o	|	|	|	|	1.03
35.333	0.00	0.23	0.765	o	|	|	|	|	1.03
35.417	0.00	0.23	0.764	o	|	|	|	|	1.03
35.500	0.00	0.23	0.762	o	|	|	|	|	1.02
35.583	0.00	0.23	0.761	o	|	|	|	|	1.02
35.667	0.00	0.23	0.759	o	|	|	|	|	1.02
35.750	0.00	0.23	0.757	o	|	|	|	|	1.02
35.833	0.00	0.23	0.756	o	|	|	|	|	1.02
35.917	0.00	0.22	0.754	o	|	|	|	|	1.01
36.000	0.00	0.22	0.753	o	|	|	|	|	1.01
36.083	0.00	0.22	0.751	o	|	|	|	|	1.01
36.167	0.00	0.22	0.750	o	|	|	|	|	1.01
36.250	0.00	0.22	0.748	o	|	|	|	|	1.01
36.333	0.00	0.22	0.747	o	|	|	|	|	1.00
36.417	0.00	0.22	0.745	o	|	|	|	|	1.00
36.500	0.00	0.22	0.744	o	|	|	|	|	1.00
36.583	0.00	0.22	0.742	o	|	|	|	|	1.00
36.667	0.00	0.22	0.741	o	|	|	|	|	1.00
36.750	0.00	0.22	0.739	o	|	|	|	|	0.99
36.833	0.00	0.22	0.738	o	|	|	|	|	0.99
36.917	0.00	0.22	0.736	o	|	|	|	|	0.99
37.000	0.00	0.22	0.735	o	|	|	|	|	0.99
37.083	0.00	0.22	0.733	o	|	|	|	|	0.99
37.167	0.00	0.21	0.732	o	|	|	|	|	0.98
37.250	0.00	0.21	0.730	o	|	|	|	|	0.98
37.333	0.00	0.21	0.729	o	|	|	|	|	0.98
37.417	0.00	0.21	0.727	o	|	|	|	|	0.98
37.500	0.00	0.21	0.726	o	|	|	|	|	0.98
37.583	0.00	0.21	0.724	o	|	|	|	|	0.97

37.667	0.00	0.21	0.723	o	|	|	|	|	0.97
37.750	0.00	0.21	0.721	o	|	|	|	|	0.97
37.833	0.00	0.21	0.720	o	|	|	|	|	0.97
37.917	0.00	0.21	0.719	o	|	|	|	|	0.97
38.000	0.00	0.21	0.717	o	|	|	|	|	0.97
38.083	0.00	0.21	0.716	o	|	|	|	|	0.96
38.167	0.00	0.21	0.714	o	|	|	|	|	0.96
38.250	0.00	0.21	0.713	o	|	|	|	|	0.96
38.333	0.00	0.21	0.711	o	|	|	|	|	0.96
38.417	0.00	0.21	0.710	o	|	|	|	|	0.96
38.500	0.00	0.21	0.708	o	|	|	|	|	0.95
38.583	0.00	0.21	0.707	o	|	|	|	|	0.95
38.667	0.00	0.21	0.706	o	|	|	|	|	0.95
38.750	0.00	0.21	0.704	o	|	|	|	|	0.95
38.833	0.00	0.21	0.703	o	|	|	|	|	0.95
38.917	0.00	0.21	0.701	o	|	|	|	|	0.94
39.000	0.00	0.21	0.700	o	|	|	|	|	0.94
39.083	0.00	0.20	0.699	o	|	|	|	|	0.94
39.167	0.00	0.20	0.697	o	|	|	|	|	0.94
39.250	0.00	0.20	0.696	o	|	|	|	|	0.94
39.333	0.00	0.20	0.694	o	|	|	|	|	0.93
39.417	0.00	0.20	0.693	o	|	|	|	|	0.93
39.500	0.00	0.20	0.691	o	|	|	|	|	0.93
39.583	0.00	0.20	0.690	o	|	|	|	|	0.93
39.667	0.00	0.20	0.689	o	|	|	|	|	0.93
39.750	0.00	0.20	0.687	o	|	|	|	|	0.93
39.833	0.00	0.20	0.686	o	|	|	|	|	0.92
39.917	0.00	0.20	0.685	o	|	|	|	|	0.92
40.000	0.00	0.20	0.683	o	|	|	|	|	0.92
40.083	0.00	0.20	0.682	o	|	|	|	|	0.92
40.167	0.00	0.20	0.680	o	|	|	|	|	0.92
40.250	0.00	0.20	0.679	o	|	|	|	|	0.91
40.333	0.00	0.20	0.678	o	|	|	|	|	0.91
40.417	0.00	0.20	0.676	o	|	|	|	|	0.91
40.500	0.00	0.20	0.675	o	|	|	|	|	0.91
40.583	0.00	0.20	0.674	o	|	|	|	|	0.91
40.667	0.00	0.20	0.672	o	|	|	|	|	0.90
40.750	0.00	0.20	0.671	o	|	|	|	|	0.90
40.833	0.00	0.20	0.669	o	|	|	|	|	0.90
40.917	0.00	0.20	0.668	o	|	|	|	|	0.90
41.000	0.00	0.20	0.667	o	|	|	|	|	0.90
41.083	0.00	0.20	0.665	o	|	|	|	|	0.90
41.167	0.00	0.19	0.664	o	|	|	|	|	0.89
41.250	0.00	0.19	0.663	o	|	|	|	|	0.89
41.333	0.00	0.19	0.661	o	|	|	|	|	0.89
41.417	0.00	0.19	0.660	o	|	|	|	|	0.89
41.500	0.00	0.19	0.659	o	|	|	|	|	0.89
41.583	0.00	0.19	0.657	o	|	|	|	|	0.88
41.667	0.00	0.19	0.656	o	|	|	|	|	0.88
41.750	0.00	0.19	0.655	o	|	|	|	|	0.88
41.833	0.00	0.19	0.653	o	|	|	|	|	0.88
41.917	0.00	0.19	0.652	o	|	|	|	|	0.88
42.000	0.00	0.19	0.651	o	|	|	|	|	0.88
42.083	0.00	0.19	0.650	o	|	|	|	|	0.87
42.167	0.00	0.19	0.648	o	|	|	|	|	0.87
42.250	0.00	0.19	0.647	o	|	|	|	|	0.87
42.333	0.00	0.19	0.646	o	|	|	|	|	0.87
42.417	0.00	0.19	0.644	o	|	|	|	|	0.87
42.500	0.00	0.19	0.643	o	|	|	|	|	0.87
42.583	0.00	0.19	0.642	o	|	|	|	|	0.86
42.667	0.00	0.19	0.640	o	|	|	|	|	0.86
42.750	0.00	0.19	0.639	o	|	|	|	|	0.86
42.833	0.00	0.19	0.638	o	|	|	|	|	0.86
42.917	0.00	0.19	0.637	o	|	|	|	|	0.86
43.000	0.00	0.19	0.635	o	|	|	|	|	0.85
43.083	0.00	0.19	0.634	o	|	|	|	|	0.85
43.167	0.00	0.19	0.633	o	|	|	|	|	0.85
43.250	0.00	0.19	0.631	o	|	|	|	|	0.85
43.333	0.00	0.18	0.630	o	|	|	|	|	0.85
43.417	0.00	0.18	0.629	o	|	|	|	|	0.85
43.500	0.00	0.18	0.628	o	|	|	|	|	0.84
43.583	0.00	0.18	0.626	o	|	|	|	|	0.84
43.667	0.00	0.18	0.625	o	|	|	|	|	0.84
43.750	0.00	0.18	0.624	o	|	|	|	|	0.84
43.833	0.00	0.18	0.623	o	|	|	|	|	0.84
43.917	0.00	0.18	0.621	o	|	|	|	|	0.84
44.000	0.00	0.18	0.620	o	|	|	|	|	0.83
44.083	0.00	0.18	0.619	o	|	|	|	|	0.83
44.167	0.00	0.18	0.618	o	|	|	|	|	0.83
44.250	0.00	0.18	0.616	o	|	|	|	|	0.83
44.333	0.00	0.18	0.615	o	|	|	|	|	0.83
44.417	0.00	0.18	0.614	o	|	|	|	|	0.83
44.500	0.00	0.18	0.613	o	|	|	|	|	0.82
44.583	0.00	0.18	0.611	o	|	|	|	|	0.82
44.667	0.00	0.18	0.610	o	|	|	|	|	0.82
44.750	0.00	0.18	0.609	o	|	|	|	|	0.82

44.833	0.00	0.18	0.608	o	|	|	|	|	0.82
44.917	0.00	0.18	0.606	o	|	|	|	|	0.82
45.000	0.00	0.18	0.605	o	|	|	|	|	0.81
45.083	0.00	0.18	0.604	o	|	|	|	|	0.81
45.167	0.00	0.18	0.603	o	|	|	|	|	0.81
45.250	0.00	0.18	0.602	o	|	|	|	|	0.81
45.333	0.00	0.18	0.600	o	|	|	|	|	0.81
45.417	0.00	0.18	0.599	o	|	|	|	|	0.81
45.500	0.00	0.18	0.598	o	|	|	|	|	0.80
45.583	0.00	0.18	0.597	o	|	|	|	|	0.80
45.667	0.00	0.17	0.595	o	|	|	|	|	0.80
45.750	0.00	0.17	0.594	o	|	|	|	|	0.80
45.833	0.00	0.17	0.593	o	|	|	|	|	0.80
45.917	0.00	0.17	0.592	o	|	|	|	|	0.80
46.000	0.00	0.17	0.591	o	|	|	|	|	0.79
46.083	0.00	0.17	0.589	o	|	|	|	|	0.79
46.167	0.00	0.17	0.588	o	|	|	|	|	0.79
46.250	0.00	0.17	0.587	o	|	|	|	|	0.79
46.333	0.00	0.17	0.586	o	|	|	|	|	0.79
46.417	0.00	0.17	0.585	o	|	|	|	|	0.79
46.500	0.00	0.17	0.584	o	|	|	|	|	0.79
46.583	0.00	0.17	0.582	o	|	|	|	|	0.78
46.667	0.00	0.17	0.581	o	|	|	|	|	0.78
46.750	0.00	0.17	0.580	o	|	|	|	|	0.78
46.833	0.00	0.17	0.579	o	|	|	|	|	0.78
46.917	0.00	0.17	0.578	o	|	|	|	|	0.78
47.000	0.00	0.17	0.577	o	|	|	|	|	0.78
47.083	0.00	0.17	0.575	o	|	|	|	|	0.77
47.167	0.00	0.17	0.574	o	|	|	|	|	0.77
47.250	0.00	0.17	0.573	o	|	|	|	|	0.77
47.333	0.00	0.17	0.572	o	|	|	|	|	0.77
47.417	0.00	0.17	0.571	o	|	|	|	|	0.77
47.500	0.00	0.17	0.570	o	|	|	|	|	0.77
47.583	0.00	0.17	0.568	o	|	|	|	|	0.77
47.667	0.00	0.17	0.567	o	|	|	|	|	0.76
47.750	0.00	0.17	0.566	o	|	|	|	|	0.76
47.833	0.00	0.17	0.565	o	|	|	|	|	0.76
47.917	0.00	0.17	0.564	o	|	|	|	|	0.76
48.000	0.00	0.17	0.563	o	|	|	|	|	0.76
48.083	0.00	0.16	0.562	o	|	|	|	|	0.76
48.167	0.00	0.16	0.560	o	|	|	|	|	0.75
48.250	0.00	0.16	0.559	o	|	|	|	|	0.75
48.333	0.00	0.16	0.558	o	|	|	|	|	0.75
48.417	0.00	0.16	0.557	o	|	|	|	|	0.75
48.500	0.00	0.16	0.556	o	|	|	|	|	0.75
48.583	0.00	0.16	0.555	o	|	|	|	|	0.75
48.667	0.00	0.16	0.554	o	|	|	|	|	0.75
48.750	0.00	0.16	0.553	o	|	|	|	|	0.74
48.833	0.00	0.16	0.551	o	|	|	|	|	0.74
48.917	0.00	0.16	0.550	o	|	|	|	|	0.74
49.000	0.00	0.16	0.549	o	|	|	|	|	0.74
49.083	0.00	0.16	0.548	o	|	|	|	|	0.74
49.167	0.00	0.16	0.547	o	|	|	|	|	0.74
49.250	0.00	0.16	0.546	o	|	|	|	|	0.73
49.333	0.00	0.16	0.545	o	|	|	|	|	0.73
49.417	0.00	0.16	0.544	o	|	|	|	|	0.73
49.500	0.00	0.16	0.543	o	|	|	|	|	0.73
49.583	0.00	0.16	0.542	o	|	|	|	|	0.73
49.667	0.00	0.16	0.540	o	|	|	|	|	0.73
49.750	0.00	0.16	0.539	o	|	|	|	|	0.73
49.833	0.00	0.16	0.538	o	|	|	|	|	0.72
49.917	0.00	0.16	0.537	o	|	|	|	|	0.72
50.000	0.00	0.16	0.536	o	|	|	|	|	0.72
50.083	0.00	0.16	0.535	o	|	|	|	|	0.72
50.167	0.00	0.16	0.534	o	|	|	|	|	0.72
50.250	0.00	0.16	0.533	o	|	|	|	|	0.72
50.333	0.00	0.16	0.532	o	|	|	|	|	0.72
50.417	0.00	0.16	0.531	o	|	|	|	|	0.71
50.500	0.00	0.16	0.530	o	|	|	|	|	0.71
50.583	0.00	0.16	0.529	o	|	|	|	|	0.71
50.667	0.00	0.15	0.527	o	|	|	|	|	0.71
50.750	0.00	0.15	0.526	o	|	|	|	|	0.71
50.833	0.00	0.15	0.525	o	|	|	|	|	0.71
50.917	0.00	0.15	0.524	o	|	|	|	|	0.71
51.000	0.00	0.15	0.523	o	|	|	|	|	0.70
51.083	0.00	0.15	0.522	o	|	|	|	|	0.70
51.167	0.00	0.15	0.521	o	|	|	|	|	0.70
51.250	0.00	0.15	0.520	o	|	|	|	|	0.70
51.333	0.00	0.15	0.519	o	|	|	|	|	0.70
51.417	0.00	0.15	0.518	o	|	|	|	|	0.70
51.500	0.00	0.15	0.517	o	|	|	|	|	0.70
51.583	0.00	0.15	0.516	o	|	|	|	|	0.69
51.667	0.00	0.15	0.515	o	|	|	|	|	0.69
51.750	0.00	0.15	0.514	o	|	|	|	|	0.69
51.833	0.00	0.15	0.513	o	|	|	|	|	0.69
51.917	0.00	0.15	0.512	o	|	|	|	|	0.69

52.000	0.00	0.15	0.511	o	|	|	|	0.69
52.083	0.00	0.15	0.510	o	|	|	|	0.69
52.167	0.00	0.15	0.509	o	|	|	|	0.68
52.250	0.00	0.15	0.508	o	|	|	|	0.68
52.333	0.00	0.15	0.507	o	|	|	|	0.68
52.417	0.00	0.15	0.506	o	|	|	|	0.68
52.500	0.00	0.15	0.505	o	|	|	|	0.68
52.583	0.00	0.15	0.504	o	|	|	|	0.68
52.667	0.00	0.15	0.502	o	|	|	|	0.68
52.750	0.00	0.15	0.501	o	|	|	|	0.67
52.833	0.00	0.15	0.500	o	|	|	|	0.67
52.917	0.00	0.15	0.499	o	|	|	|	0.67
53.000	0.00	0.15	0.498	o	|	|	|	0.67
53.083	0.00	0.15	0.497	o	|	|	|	0.67
53.167	0.00	0.15	0.496	o	|	|	|	0.67
53.250	0.00	0.15	0.495	o	|	|	|	0.67
53.333	0.00	0.15	0.494	o	|	|	|	0.67
53.417	0.00	0.14	0.493	o	|	|	|	0.66
53.500	0.00	0.14	0.492	o	|	|	|	0.66
53.583	0.00	0.14	0.491	o	|	|	|	0.66
53.667	0.00	0.14	0.490	o	|	|	|	0.66
53.750	0.00	0.14	0.489	o	|	|	|	0.66
53.833	0.00	0.14	0.488	o	|	|	|	0.66
53.917	0.00	0.14	0.487	o	|	|	|	0.66
54.000	0.00	0.14	0.487	o	|	|	|	0.65
54.083	0.00	0.14	0.486	o	|	|	|	0.65
54.167	0.00	0.14	0.485	o	|	|	|	0.65
54.250	0.00	0.14	0.484	o	|	|	|	0.65
54.333	0.00	0.14	0.483	o	|	|	|	0.65
54.417	0.00	0.14	0.482	o	|	|	|	0.65
54.500	0.00	0.14	0.481	o	|	|	|	0.65
54.583	0.00	0.14	0.480	o	|	|	|	0.65
54.667	0.00	0.14	0.479	o	|	|	|	0.64
54.750	0.00	0.14	0.478	o	|	|	|	0.64
54.833	0.00	0.14	0.477	o	|	|	|	0.64
54.917	0.00	0.14	0.476	o	|	|	|	0.64
55.000	0.00	0.14	0.475	o	|	|	|	0.64
55.083	0.00	0.14	0.474	o	|	|	|	0.64
55.167	0.00	0.14	0.473	o	|	|	|	0.64
55.250	0.00	0.14	0.472	o	|	|	|	0.64
55.333	0.00	0.14	0.471	o	|	|	|	0.63
55.417	0.00	0.14	0.470	o	|	|	|	0.63
55.500	0.00	0.14	0.469	o	|	|	|	0.63
55.583	0.00	0.14	0.468	o	|	|	|	0.63
55.667	0.00	0.14	0.467	o	|	|	|	0.63
55.750	0.00	0.14	0.466	o	|	|	|	0.63
55.833	0.00	0.14	0.465	o	|	|	|	0.63
55.917	0.00	0.14	0.464	o	|	|	|	0.63
56.000	0.00	0.14	0.463	o	|	|	|	0.62
56.083	0.00	0.14	0.463	o	|	|	|	0.62
56.167	0.00	0.14	0.462	o	|	|	|	0.62
56.250	0.00	0.14	0.461	o	|	|	|	0.62
56.333	0.00	0.13	0.460	o	|	|	|	0.62
56.417	0.00	0.13	0.459	o	|	|	|	0.62
56.500	0.00	0.13	0.458	o	|	|	|	0.62
56.583	0.00	0.13	0.457	o	|	|	|	0.62
56.667	0.00	0.13	0.456	o	|	|	|	0.61
56.750	0.00	0.13	0.455	o	|	|	|	0.61
56.833	0.00	0.13	0.454	o	|	|	|	0.61
56.917	0.00	0.13	0.453	o	|	|	|	0.61
57.000	0.00	0.13	0.452	o	|	|	|	0.61
57.083	0.00	0.13	0.451	o	|	|	|	0.61
57.167	0.00	0.13	0.451	o	|	|	|	0.61
57.250	0.00	0.13	0.450	o	|	|	|	0.61
57.333	0.00	0.13	0.449	o	|	|	|	0.60
57.417	0.00	0.13	0.448	o	|	|	|	0.60
57.500	0.00	0.13	0.447	o	|	|	|	0.60
57.583	0.00	0.13	0.446	o	|	|	|	0.60
57.667	0.00	0.13	0.445	o	|	|	|	0.60
57.750	0.00	0.13	0.444	o	|	|	|	0.60
57.833	0.00	0.13	0.443	o	|	|	|	0.60
57.917	0.00	0.13	0.442	o	|	|	|	0.60
58.000	0.00	0.13	0.442	o	|	|	|	0.59
58.083	0.00	0.13	0.441	o	|	|	|	0.59
58.167	0.00	0.13	0.440	o	|	|	|	0.59
58.250	0.00	0.13	0.439	o	|	|	|	0.59
58.333	0.00	0.13	0.438	o	|	|	|	0.59
58.417	0.00	0.13	0.437	o	|	|	|	0.59
58.500	0.00	0.13	0.436	o	|	|	|	0.59
58.583	0.00	0.13	0.435	o	|	|	|	0.59
58.667	0.00	0.13	0.434	o	|	|	|	0.58
58.750	0.00	0.13	0.434	o	|	|	|	0.58
58.833	0.00	0.13	0.433	o	|	|	|	0.58
58.917	0.00	0.13	0.432	o	|	|	|	0.58
59.000	0.00	0.13	0.431	o	|	|	|	0.58
59.083	0.00	0.13	0.430	o	|	|	|	0.58

59.167	0.00	0.13	0.429	o	|	|	|	|	0.58
59.250	0.00	0.13	0.428	o	|	|	|	|	0.58
59.333	0.00	0.13	0.427	o	|	|	|	|	0.58
59.417	0.00	0.13	0.427	o	|	|	|	|	0.57
59.500	0.00	0.12	0.426	o	|	|	|	|	0.57
59.583	0.00	0.12	0.425	o	|	|	|	|	0.57
59.667	0.00	0.12	0.424	o	|	|	|	|	0.57
59.750	0.00	0.12	0.423	o	|	|	|	|	0.57
59.833	0.00	0.12	0.422	o	|	|	|	|	0.57
59.917	0.00	0.12	0.421	o	|	|	|	|	0.57
60.000	0.00	0.12	0.421	o	|	|	|	|	0.57
60.083	0.00	0.12	0.420	o	|	|	|	|	0.56
60.167	0.00	0.12	0.419	o	|	|	|	|	0.56
60.250	0.00	0.12	0.418	o	|	|	|	|	0.56
60.333	0.00	0.12	0.417	o	|	|	|	|	0.56
60.417	0.00	0.12	0.416	o	|	|	|	|	0.56
60.500	0.00	0.12	0.416	o	|	|	|	|	0.56
60.583	0.00	0.12	0.415	o	|	|	|	|	0.56
60.667	0.00	0.12	0.414	o	|	|	|	|	0.56
60.750	0.00	0.12	0.413	o	|	|	|	|	0.56
60.833	0.00	0.12	0.412	o	|	|	|	|	0.55
60.917	0.00	0.12	0.411	o	|	|	|	|	0.55
61.000	0.00	0.12	0.411	o	|	|	|	|	0.55
61.083	0.00	0.12	0.410	o	|	|	|	|	0.55
61.167	0.00	0.12	0.409	o	|	|	|	|	0.55
61.250	0.00	0.12	0.408	o	|	|	|	|	0.55
61.333	0.00	0.12	0.407	o	|	|	|	|	0.55
61.417	0.00	0.12	0.406	o	|	|	|	|	0.55
61.500	0.00	0.12	0.406	o	|	|	|	|	0.55
61.583	0.00	0.12	0.405	o	|	|	|	|	0.54
61.667	0.00	0.12	0.404	o	|	|	|	|	0.54
61.750	0.00	0.12	0.403	o	|	|	|	|	0.54
61.833	0.00	0.12	0.402	o	|	|	|	|	0.54
61.917	0.00	0.12	0.402	o	|	|	|	|	0.54
62.000	0.00	0.12	0.401	o	|	|	|	|	0.54
62.083	0.00	0.12	0.400	o	|	|	|	|	0.54
62.167	0.00	0.12	0.399	o	|	|	|	|	0.54
62.250	0.00	0.12	0.398	o	|	|	|	|	0.54
62.333	0.00	0.12	0.397	o	|	|	|	|	0.53
62.417	0.00	0.12	0.397	o	|	|	|	|	0.53
62.500	0.00	0.12	0.396	o	|	|	|	|	0.53
62.583	0.00	0.12	0.395	o	|	|	|	|	0.53
62.667	0.00	0.12	0.394	o	|	|	|	|	0.53
62.750	0.00	0.12	0.394	o	|	|	|	|	0.53
62.833	0.00	0.12	0.393	o	|	|	|	|	0.53
62.917	0.00	0.11	0.392	o	|	|	|	|	0.53
63.000	0.00	0.11	0.391	o	|	|	|	|	0.53
63.083	0.00	0.11	0.390	o	|	|	|	|	0.53
63.167	0.00	0.11	0.390	o	|	|	|	|	0.52
63.250	0.00	0.11	0.389	o	|	|	|	|	0.52
63.333	0.00	0.11	0.388	o	|	|	|	|	0.52
63.417	0.00	0.11	0.387	o	|	|	|	|	0.52
63.500	0.00	0.11	0.386	o	|	|	|	|	0.52
63.583	0.00	0.11	0.386	o	|	|	|	|	0.52
63.667	0.00	0.11	0.385	o	|	|	|	|	0.52
63.750	0.00	0.11	0.384	o	|	|	|	|	0.52
63.833	0.00	0.11	0.383	o	|	|	|	|	0.52
63.917	0.00	0.11	0.383	o	|	|	|	|	0.51
64.000	0.00	0.11	0.382	o	|	|	|	|	0.51
64.083	0.00	0.11	0.381	o	|	|	|	|	0.51
64.167	0.00	0.11	0.380	o	|	|	|	|	0.51
64.250	0.00	0.11	0.379	o	|	|	|	|	0.51
64.333	0.00	0.11	0.379	o	|	|	|	|	0.51
64.417	0.00	0.11	0.378	o	|	|	|	|	0.51
64.500	0.00	0.11	0.377	o	|	|	|	|	0.51
64.583	0.00	0.11	0.376	o	|	|	|	|	0.51
64.667	0.00	0.11	0.376	o	|	|	|	|	0.51
64.750	0.00	0.11	0.375	o	|	|	|	|	0.50
64.833	0.00	0.11	0.374	o	|	|	|	|	0.50
64.917	0.00	0.11	0.373	o	|	|	|	|	0.50
65.000	0.00	0.11	0.373	o	|	|	|	|	0.50
65.083	0.00	0.11	0.372	o	|	|	|	|	0.50
65.167	0.00	0.11	0.371	o	|	|	|	|	0.50
65.250	0.00	0.11	0.370	o	|	|	|	|	0.50
65.333	0.00	0.11	0.370	o	|	|	|	|	0.50
65.417	0.00	0.11	0.369	o	|	|	|	|	0.50
65.500	0.00	0.11	0.368	o	|	|	|	|	0.50
65.583	0.00	0.11	0.367	o	|	|	|	|	0.49
65.667	0.00	0.11	0.367	o	|	|	|	|	0.49
65.750	0.00	0.11	0.366	o	|	|	|	|	0.49
65.833	0.00	0.11	0.365	o	|	|	|	|	0.49
65.917	0.00	0.11	0.364	o	|	|	|	|	0.49
66.000	0.00	0.11	0.364	o	|	|	|	|	0.49
66.083	0.00	0.11	0.363	o	|	|	|	|	0.49
66.167	0.00	0.11	0.362	o	|	|	|	|	0.49
66.250	0.00	0.11	0.361	o	|	|	|	|	0.49

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66.333    0.00    0.11      0.361  o       |       |       |       |     0.49
66.417    0.00    0.11      0.360  o       |       |       |       |     0.48
66.500    0.00    0.11      0.359  o       |       |       |       |     0.48
66.583    0.00    0.11      0.359  o       |       |       |       |     0.48
66.667    0.00    0.10      0.358  o       |       |       |       |     0.48
66.750    0.00    0.10      0.357  o       |       |       |       |     0.48
66.833    0.00    0.10      0.356  o       |       |       |       |     0.48
66.917    0.00    0.10      0.356  o       |       |       |       |     0.48
67.000    0.00    0.10      0.355  o       |       |       |       |     0.48
67.083    0.00    0.10      0.354  o       |       |       |       |     0.48
67.167    0.00    0.10      0.354  o       |       |       |       |     0.48
67.250    0.00    0.10      0.353  o       |       |       |       |     0.47
67.333    0.00    0.10      0.352  o       |       |       |       |     0.47
67.417    0.00    0.10      0.351  o       |       |       |       |     0.47
67.500    0.00    0.10      0.351  o       |       |       |       |     0.47
67.583    0.00    0.10      0.350  o       |       |       |       |     0.47
67.667    0.00    0.10      0.349  o       |       |       |       |     0.47
67.750    0.00    0.10      0.349  o       |       |       |       |     0.47
67.833    0.00    0.10      0.348  o       |       |       |       |     0.47
67.917    0.00    0.10      0.347  o       |       |       |       |     0.47
68.000    0.00    0.10      0.346  o       |       |       |       |     0.47
68.083    0.00    0.10      0.346  o       |       |       |       |     0.47
68.167    0.00    0.10      0.345  o       |       |       |       |     0.46
68.250    0.00    0.10      0.344  o       |       |       |       |     0.46
68.333    0.00    0.10      0.344  o       |       |       |       |     0.46
68.417    0.00    0.10      0.343  o       |       |       |       |     0.46
68.500    0.00    0.10      0.342  o       |       |       |       |     0.46
68.583    0.00    0.10      0.342  o       |       |       |       |     0.46
68.667    0.00    0.10      0.341  o       |       |       |       |     0.46
68.750    0.00    0.10      0.340  o       |       |       |       |     0.46

Remaining water in basin =    0.34 (Ac.Ft)


****************************HYDROGRAPH DATA****************************
               Number of intervals =   825
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       12.283 (CFS)
               Total volume =       2.413 (Ac.Ft)
       Status of hydrographs being held in storage
                  Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro11003100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 41
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 45.122 (CFS)
Total volume = 4.026 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 41
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	11.3	22.56	33.84	45.12	Depth (Ft.)
0.083	2.16	0.00	0.007	OI					0.01
0.167	5.32	0.01	0.033	O I					0.04
0.250	5.66	0.02	0.071	O I					0.10
0.333	6.22	0.03	0.112	O I					0.15
0.417	7.46	0.05	0.158	O I					0.21
0.500	8.42	0.06	0.213	O I					0.29
0.583	8.80	0.08	0.272	O I					0.37
0.667	8.78	0.10	0.331	O I					0.45
0.750	9.61	0.12	0.394	O I					0.53
0.833	9.16	0.13	0.458	O I					0.62
0.917	8.53	0.15	0.518	O I					0.70
1.000	9.05	0.17	0.577	O I					0.78
1.083	10.51	0.19	0.643	O I					0.87
1.167	11.86	0.21	0.719	O I					0.97
1.250	12.21	0.25	0.800	O I					1.07
1.333	11.96	0.29	0.882	O I					1.17
1.417	12.69	0.34	0.964	O I					1.27
1.500	14.62	0.39	1.056	O	I				1.38
1.583	14.68	0.44	1.154	O	I				1.50
1.667	14.62	0.50	1.251	O	I				1.62
1.750	16.69	0.56	1.356	O	I				1.75

1.833	18.30	0.62	1.472	O	|	I	|	|	1.89
1.917	17.77	0.70	1.592	O	|	I	|	|	2.03
2.000	17.43	0.81	1.708	O	|	I	|	|	2.16
2.083	17.87	0.92	1.823	O	|	I	|	|	2.29
2.167	20.51	1.04	1.949	O	|	I	|	|	2.43
2.250	25.60	1.18	2.100	O	|	| I	|	|	2.60
2.333	25.74	1.34	2.268	O	|	| I	|	|	2.79
2.417	29.05	1.51	2.447	|O	|	| I	|	|	2.99
2.500	39.53	19.88	2.610	|	|	O |	| I	|	3.16
2.583	45.12	32.98	2.719	|	|	| O	|	I 3.28
2.667	44.31	39.83	2.776	|	|	|	| O	I| 3.34
2.750	30.33	38.36	2.764	|	|	| I	| O	|	3.32
2.833	16.98	29.78	2.692	|	| I	|	O |	|	3.25
2.917	12.95	21.14	2.620	|	I|	O |	|	|	3.17
3.000	8.74	15.13	2.570	|	I |	O |	|	|	3.12
3.083	3.45	9.86	2.526	| I	O |	|	|	|	3.07
3.167	1.15	5.45	2.489	I O	|	|	|	|	3.03
3.250	0.50	2.75	2.466	IO	|	|	|	|	3.01
3.333	0.20	1.52	2.454	IO	|	|	|	|	3.00
3.417	0.03	1.51	2.444	IO	|	|	|	|	2.99
3.500	0.00	1.50	2.434	IO	|	|	|	|	2.98
3.583	0.00	1.49	2.424	IO	|	|	|	|	2.96
3.667	0.00	1.48	2.414	IO	|	|	|	|	2.95
3.750	0.00	1.47	2.404	IO	|	|	|	|	2.94
3.833	0.00	1.46	2.393	IO	|	|	|	|	2.93
3.917	0.00	1.45	2.383	IO	|	|	|	|	2.92
4.000	0.00	1.44	2.374	IO	|	|	|	|	2.91
4.083	0.00	1.43	2.364	IO	|	|	|	|	2.90
4.167	0.00	1.42	2.354	IO	|	|	|	|	2.89
4.250	0.00	1.41	2.344	IO	|	|	|	|	2.87
4.333	0.00	1.40	2.334	O	|	|	|	|	2.86
4.417	0.00	1.39	2.325	O	|	|	|	|	2.85
4.500	0.00	1.38	2.315	O	|	|	|	|	2.84
4.583	0.00	1.38	2.306	O	|	|	|	|	2.83
4.667	0.00	1.37	2.296	O	|	|	|	|	2.82
4.750	0.00	1.36	2.287	O	|	|	|	|	2.81
4.833	0.00	1.35	2.278	O	|	|	|	|	2.80
4.917	0.00	1.34	2.268	O	|	|	|	|	2.79
5.000	0.00	1.33	2.259	O	|	|	|	|	2.78
5.083	0.00	1.32	2.250	O	|	|	|	|	2.77
5.167	0.00	1.31	2.241	O	|	|	|	|	2.76
5.250	0.00	1.31	2.232	O	|	|	|	|	2.75
5.333	0.00	1.30	2.223	O	|	|	|	|	2.74
5.417	0.00	1.29	2.214	O	|	|	|	|	2.73
5.500	0.00	1.28	2.205	O	|	|	|	|	2.72
5.583	0.00	1.27	2.196	O	|	|	|	|	2.71
5.667	0.00	1.26	2.188	O	|	|	|	|	2.70
5.750	0.00	1.25	2.179	O	|	|	|	|	2.69
5.833	0.00	1.25	2.170	O	|	|	|	|	2.68
5.917	0.00	1.24	2.162	O	|	|	|	|	2.67
6.000	0.00	1.23	2.153	O	|	|	|	|	2.66
6.083	0.00	1.22	2.145	O	|	|	|	|	2.65
6.167	0.00	1.21	2.136	O	|	|	|	|	2.64
6.250	0.00	1.21	2.128	O	|	|	|	|	2.63
6.333	0.00	1.20	2.120	O	|	|	|	|	2.62
6.417	0.00	1.19	2.112	O	|	|	|	|	2.62
6.500	0.00	1.18	2.103	O	|	|	|	|	2.61
6.583	0.00	1.18	2.095	O	|	|	|	|	2.60
6.667	0.00	1.17	2.087	O	|	|	|	|	2.59
6.750	0.00	1.16	2.079	O	|	|	|	|	2.58
6.833	0.00	1.15	2.071	O	|	|	|	|	2.57
6.917	0.00	1.15	2.063	O	|	|	|	|	2.56
7.000	0.00	1.14	2.055	O	|	|	|	|	2.55
7.083	0.00	1.13	2.048	O	|	|	|	|	2.54
7.167	0.00	1.12	2.040	O	|	|	|	|	2.54
7.250	0.00	1.12	2.032	O	|	|	|	|	2.53
7.333	0.00	1.11	2.025	O	|	|	|	|	2.52
7.417	0.00	1.10	2.017	O	|	|	|	|	2.51
7.500	0.00	1.09	2.009	O	|	|	|	|	2.50
7.583	0.00	1.09	2.002	O	|	|	|	|	2.49
7.667	0.00	1.08	1.994	O	|	|	|	|	2.48
7.750	0.00	1.07	1.987	O	|	|	|	|	2.48
7.833	0.00	1.07	1.980	O	|	|	|	|	2.47
7.917	0.00	1.06	1.972	O	|	|	|	|	2.46
8.000	0.00	1.05	1.965	O	|	|	|	|	2.45
8.083	0.00	1.04	1.958	O	|	|	|	|	2.44
8.167	0.00	1.04	1.951	O	|	|	|	|	2.44
8.250	0.00	1.03	1.944	O	|	|	|	|	2.43
8.333	0.00	1.02	1.936	O	|	|	|	|	2.42
8.417	0.00	1.02	1.929	O	|	|	|	|	2.41
8.500	0.00	1.01	1.922	O	|	|	|	|	2.40
8.583	0.00	1.00	1.915	O	|	|	|	|	2.40
8.667	0.00	1.00	1.909	O	|	|	|	|	2.39
8.750	0.00	0.99	1.902	O	|	|	|	|	2.38
8.833	0.00	0.99	1.895	O	|	|	|	|	2.37
8.917	0.00	0.98	1.888	O	|	|	|	|	2.37

9.000	0.00	0.97	1.881	o	|	|	|	2.36
9.083	0.00	0.97	1.875	o	|	|	|	2.35
9.167	0.00	0.96	1.868	o	|	|	|	2.34
9.250	0.00	0.95	1.862	o	|	|	|	2.34
9.333	0.00	0.95	1.855	o	|	|	|	2.33
9.417	0.00	0.94	1.849	o	|	|	|	2.32
9.500	0.00	0.93	1.842	o	|	|	|	2.31
9.583	0.00	0.93	1.836	o	|	|	|	2.31
9.667	0.00	0.92	1.829	o	|	|	|	2.30
9.750	0.00	0.92	1.823	o	|	|	|	2.29
9.833	0.00	0.91	1.817	o	|	|	|	2.29
9.917	0.00	0.90	1.810	o	|	|	|	2.28
10.000	0.00	0.90	1.804	o	|	|	|	2.27
10.083	0.00	0.89	1.798	o	|	|	|	2.26
10.167	0.00	0.89	1.792	o	|	|	|	2.26
10.250	0.00	0.88	1.786	o	|	|	|	2.25
10.333	0.00	0.88	1.780	o	|	|	|	2.24
10.417	0.00	0.87	1.774	o	|	|	|	2.24
10.500	0.00	0.86	1.768	o	|	|	|	2.23
10.583	0.00	0.86	1.762	o	|	|	|	2.22
10.667	0.00	0.85	1.756	o	|	|	|	2.22
10.750	0.00	0.85	1.750	o	|	|	|	2.21
10.833	0.00	0.84	1.744	o	|	|	|	2.20
10.917	0.00	0.84	1.738	o	|	|	|	2.20
11.000	0.00	0.83	1.733	o	|	|	|	2.19
11.083	0.00	0.83	1.727	o	|	|	|	2.19
11.167	0.00	0.82	1.721	o	|	|	|	2.18
11.250	0.00	0.81	1.716	o	|	|	|	2.17
11.333	0.00	0.81	1.710	o	|	|	|	2.17
11.417	0.00	0.80	1.705	o	|	|	|	2.16
11.500	0.00	0.80	1.699	o	|	|	|	2.15
11.583	0.00	0.79	1.694	o	|	|	|	2.15
11.667	0.00	0.79	1.688	o	|	|	|	2.14
11.750	0.00	0.78	1.683	o	|	|	|	2.14
11.833	0.00	0.78	1.677	o	|	|	|	2.13
11.917	0.00	0.77	1.672	o	|	|	|	2.12
12.000	0.00	0.77	1.667	o	|	|	|	2.12
12.083	0.00	0.76	1.661	o	|	|	|	2.11
12.167	0.00	0.76	1.656	o	|	|	|	2.11
12.250	0.00	0.75	1.651	o	|	|	|	2.10
12.333	0.00	0.75	1.646	o	|	|	|	2.09
12.417	0.00	0.74	1.641	o	|	|	|	2.09
12.500	0.00	0.74	1.636	o	|	|	|	2.08
12.583	0.00	0.73	1.630	o	|	|	|	2.08
12.667	0.00	0.73	1.625	o	|	|	|	2.07
12.750	0.00	0.72	1.620	o	|	|	|	2.07
12.833	0.00	0.72	1.615	o	|	|	|	2.06
12.917	0.00	0.72	1.610	o	|	|	|	2.06
13.000	0.00	0.71	1.606	o	|	|	|	2.05
13.083	0.00	0.71	1.601	o	|	|	|	2.04
13.167	0.00	0.70	1.596	o	|	|	|	2.04
13.250	0.00	0.70	1.591	o	|	|	|	2.03
13.333	0.00	0.69	1.586	o	|	|	|	2.03
13.417	0.00	0.69	1.582	o	|	|	|	2.02
13.500	0.00	0.68	1.577	o	|	|	|	2.02
13.583	0.00	0.68	1.572	o	|	|	|	2.01
13.667	0.00	0.67	1.567	o	|	|	|	2.01
13.750	0.00	0.67	1.563	o	|	|	|	2.00
13.833	0.00	0.67	1.558	o	|	|	|	2.00
13.917	0.00	0.66	1.554	o	|	|	|	1.99
14.000	0.00	0.66	1.549	o	|	|	|	1.99
14.083	0.00	0.66	1.545	o	|	|	|	1.98
14.167	0.00	0.66	1.540	o	|	|	|	1.97
14.250	0.00	0.65	1.535	o	|	|	|	1.97
14.333	0.00	0.65	1.531	o	|	|	|	1.96
14.417	0.00	0.65	1.527	o	|	|	|	1.96
14.500	0.00	0.65	1.522	o	|	|	|	1.95
14.583	0.00	0.64	1.518	o	|	|	|	1.95
14.667	0.00	0.64	1.513	o	|	|	|	1.94
14.750	0.00	0.64	1.509	o	|	|	|	1.94
14.833	0.00	0.64	1.504	o	|	|	|	1.93
14.917	0.00	0.63	1.500	o	|	|	|	1.93
15.000	0.00	0.63	1.496	o	|	|	|	1.92
15.083	0.00	0.63	1.491	o	|	|	|	1.91
15.167	0.00	0.63	1.487	o	|	|	|	1.91
15.250	0.00	0.62	1.483	o	|	|	|	1.90
15.333	0.00	0.62	1.478	o	|	|	|	1.90
15.417	0.00	0.62	1.474	o	|	|	|	1.89
15.500	0.00	0.62	1.470	o	|	|	|	1.89
15.583	0.00	0.62	1.466	o	|	|	|	1.88
15.667	0.00	0.61	1.461	o	|	|	|	1.88
15.750	0.00	0.61	1.457	o	|	|	|	1.87
15.833	0.00	0.61	1.453	o	|	|	|	1.87
15.917	0.00	0.61	1.449	o	|	|	|	1.86
16.000	0.00	0.60	1.445	o	|	|	|	1.86
16.083	0.00	0.60	1.440	o	|	|	|	1.85

16.167	0.00	0.60	1.436	o	|	|	|	|	1.85
16.250	0.00	0.60	1.432	o	|	|	|	|	1.84
16.333	0.00	0.59	1.428	o	|	|	|	|	1.84
16.417	0.00	0.59	1.424	o	|	|	|	|	1.83
16.500	0.00	0.59	1.420	o	|	|	|	|	1.83
16.583	0.00	0.59	1.416	o	|	|	|	|	1.82
16.667	0.00	0.59	1.412	o	|	|	|	|	1.82
16.750	0.00	0.58	1.408	o	|	|	|	|	1.81
16.833	0.00	0.58	1.404	o	|	|	|	|	1.81
16.917	0.00	0.58	1.400	o	|	|	|	|	1.80
17.000	0.00	0.58	1.396	o	|	|	|	|	1.80
17.083	0.00	0.57	1.392	o	|	|	|	|	1.79
17.167	0.00	0.57	1.388	o	|	|	|	|	1.79
17.250	0.00	0.57	1.384	o	|	|	|	|	1.78
17.333	0.00	0.57	1.380	o	|	|	|	|	1.78
17.417	0.00	0.57	1.376	o	|	|	|	|	1.77
17.500	0.00	0.56	1.372	o	|	|	|	|	1.77
17.583	0.00	0.56	1.368	o	|	|	|	|	1.76
17.667	0.00	0.56	1.364	o	|	|	|	|	1.76
17.750	0.00	0.56	1.361	o	|	|	|	|	1.76
17.833	0.00	0.56	1.357	o	|	|	|	|	1.75
17.917	0.00	0.55	1.353	o	|	|	|	|	1.75
18.000	0.00	0.55	1.349	o	|	|	|	|	1.74
18.083	0.00	0.55	1.345	o	|	|	|	|	1.74
18.167	0.00	0.55	1.342	o	|	|	|	|	1.73
18.250	0.00	0.55	1.338	o	|	|	|	|	1.73
18.333	0.00	0.54	1.334	o	|	|	|	|	1.72
18.417	0.00	0.54	1.330	o	|	|	|	|	1.72
18.500	0.00	0.54	1.327	o	|	|	|	|	1.71
18.583	0.00	0.54	1.323	o	|	|	|	|	1.71
18.667	0.00	0.53	1.319	o	|	|	|	|	1.70
18.750	0.00	0.53	1.316	o	|	|	|	|	1.70
18.833	0.00	0.53	1.312	o	|	|	|	|	1.70
18.917	0.00	0.53	1.308	o	|	|	|	|	1.69
19.000	0.00	0.53	1.305	o	|	|	|	|	1.69
19.083	0.00	0.52	1.301	o	|	|	|	|	1.68
19.167	0.00	0.52	1.297	o	|	|	|	|	1.68
19.250	0.00	0.52	1.294	o	|	|	|	|	1.67
19.333	0.00	0.52	1.290	o	|	|	|	|	1.67
19.417	0.00	0.52	1.287	o	|	|	|	|	1.66
19.500	0.00	0.52	1.283	o	|	|	|	|	1.66
19.583	0.00	0.51	1.280	o	|	|	|	|	1.66
19.667	0.00	0.51	1.276	o	|	|	|	|	1.65
19.750	0.00	0.51	1.272	o	|	|	|	|	1.65
19.833	0.00	0.51	1.269	o	|	|	|	|	1.64
19.917	0.00	0.51	1.265	o	|	|	|	|	1.64
20.000	0.00	0.50	1.262	o	|	|	|	|	1.63
20.083	0.00	0.50	1.259	o	|	|	|	|	1.63
20.167	0.00	0.50	1.255	o	|	|	|	|	1.63
20.250	0.00	0.50	1.252	o	|	|	|	|	1.62
20.333	0.00	0.50	1.248	o	|	|	|	|	1.62
20.417	0.00	0.49	1.245	o	|	|	|	|	1.61
20.500	0.00	0.49	1.241	o	|	|	|	|	1.61
20.583	0.00	0.49	1.238	o	|	|	|	|	1.61
20.667	0.00	0.49	1.235	o	|	|	|	|	1.60
20.750	0.00	0.49	1.231	o	|	|	|	|	1.60
20.833	0.00	0.48	1.228	o	|	|	|	|	1.59
20.917	0.00	0.48	1.225	o	|	|	|	|	1.59
21.000	0.00	0.48	1.221	o	|	|	|	|	1.58
21.083	0.00	0.48	1.218	o	|	|	|	|	1.58
21.167	0.00	0.48	1.215	o	|	|	|	|	1.58
21.250	0.00	0.48	1.211	o	|	|	|	|	1.57
21.333	0.00	0.47	1.208	o	|	|	|	|	1.57
21.417	0.00	0.47	1.205	o	|	|	|	|	1.56
21.500	0.00	0.47	1.202	o	|	|	|	|	1.56
21.583	0.00	0.47	1.198	o	|	|	|	|	1.56
21.667	0.00	0.47	1.195	o	|	|	|	|	1.55
21.750	0.00	0.47	1.192	o	|	|	|	|	1.55
21.833	0.00	0.46	1.189	o	|	|	|	|	1.55
21.917	0.00	0.46	1.186	o	|	|	|	|	1.54
22.000	0.00	0.46	1.182	o	|	|	|	|	1.54
22.083	0.00	0.46	1.179	o	|	|	|	|	1.53
22.167	0.00	0.46	1.176	o	|	|	|	|	1.53
22.250	0.00	0.45	1.173	o	|	|	|	|	1.53
22.333	0.00	0.45	1.170	o	|	|	|	|	1.52
22.417	0.00	0.45	1.167	o	|	|	|	|	1.52
22.500	0.00	0.45	1.164	o	|	|	|	|	1.51
22.583	0.00	0.45	1.161	o	|	|	|	|	1.51
22.667	0.00	0.45	1.158	o	|	|	|	|	1.51
22.750	0.00	0.44	1.154	o	|	|	|	|	1.50
22.833	0.00	0.44	1.151	o	|	|	|	|	1.50
22.917	0.00	0.44	1.148	o	|	|	|	|	1.50
23.000	0.00	0.44	1.145	o	|	|	|	|	1.49
23.083	0.00	0.44	1.142	o	|	|	|	|	1.49
23.167	0.00	0.44	1.139	o	|	|	|	|	1.48
23.250	0.00	0.43	1.136	o	|	|	|	|	1.48

23.333	0.00	0.43	1.133	o	|	|	|	|	1.48
23.417	0.00	0.43	1.130	o	|	|	|	|	1.47
23.500	0.00	0.43	1.127	o	|	|	|	|	1.47
23.583	0.00	0.43	1.124	o	|	|	|	|	1.47
23.667	0.00	0.43	1.121	o	|	|	|	|	1.46
23.750	0.00	0.42	1.119	o	|	|	|	|	1.46
23.833	0.00	0.42	1.116	o	|	|	|	|	1.46
23.917	0.00	0.42	1.113	o	|	|	|	|	1.45
24.000	0.00	0.42	1.110	o	|	|	|	|	1.45
24.083	0.00	0.42	1.107	o	|	|	|	|	1.44
24.167	0.00	0.42	1.104	o	|	|	|	|	1.44
24.250	0.00	0.42	1.101	o	|	|	|	|	1.44
24.333	0.00	0.41	1.098	o	|	|	|	|	1.43
24.417	0.00	0.41	1.096	o	|	|	|	|	1.43
24.500	0.00	0.41	1.093	o	|	|	|	|	1.43
24.583	0.00	0.41	1.090	o	|	|	|	|	1.42
24.667	0.00	0.41	1.087	o	|	|	|	|	1.42
24.750	0.00	0.41	1.084	o	|	|	|	|	1.42
24.833	0.00	0.40	1.081	o	|	|	|	|	1.41
24.917	0.00	0.40	1.079	o	|	|	|	|	1.41
25.000	0.00	0.40	1.076	o	|	|	|	|	1.41
25.083	0.00	0.40	1.073	o	|	|	|	|	1.40
25.167	0.00	0.40	1.070	o	|	|	|	|	1.40
25.250	0.00	0.40	1.068	o	|	|	|	|	1.40
25.333	0.00	0.40	1.065	o	|	|	|	|	1.39
25.417	0.00	0.39	1.062	o	|	|	|	|	1.39
25.500	0.00	0.39	1.060	o	|	|	|	|	1.39
25.583	0.00	0.39	1.057	o	|	|	|	|	1.38
25.667	0.00	0.39	1.054	o	|	|	|	|	1.38
25.750	0.00	0.39	1.051	o	|	|	|	|	1.38
25.833	0.00	0.39	1.049	o	|	|	|	|	1.37
25.917	0.00	0.38	1.046	o	|	|	|	|	1.37
26.000	0.00	0.38	1.043	o	|	|	|	|	1.37
26.083	0.00	0.38	1.041	o	|	|	|	|	1.36
26.167	0.00	0.38	1.038	o	|	|	|	|	1.36
26.250	0.00	0.38	1.036	o	|	|	|	|	1.36
26.333	0.00	0.38	1.033	o	|	|	|	|	1.35
26.417	0.00	0.38	1.030	o	|	|	|	|	1.35
26.500	0.00	0.37	1.028	o	|	|	|	|	1.35
26.583	0.00	0.37	1.025	o	|	|	|	|	1.35
26.667	0.00	0.37	1.023	o	|	|	|	|	1.34
26.750	0.00	0.37	1.020	o	|	|	|	|	1.34
26.833	0.00	0.37	1.018	o	|	|	|	|	1.34
26.917	0.00	0.37	1.015	o	|	|	|	|	1.33
27.000	0.00	0.37	1.013	o	|	|	|	|	1.33
27.083	0.00	0.36	1.010	o	|	|	|	|	1.33
27.167	0.00	0.36	1.008	o	|	|	|	|	1.32
27.250	0.00	0.36	1.005	o	|	|	|	|	1.32
27.333	0.00	0.36	1.003	o	|	|	|	|	1.32
27.417	0.00	0.36	1.000	o	|	|	|	|	1.31
27.500	0.00	0.36	0.998	o	|	|	|	|	1.31
27.583	0.00	0.36	0.995	o	|	|	|	|	1.31
27.667	0.00	0.36	0.993	o	|	|	|	|	1.31
27.750	0.00	0.35	0.990	o	|	|	|	|	1.30
27.833	0.00	0.35	0.988	o	|	|	|	|	1.30
27.917	0.00	0.35	0.985	o	|	|	|	|	1.30
28.000	0.00	0.35	0.983	o	|	|	|	|	1.29
28.083	0.00	0.35	0.981	o	|	|	|	|	1.29
28.167	0.00	0.35	0.978	o	|	|	|	|	1.29
28.250	0.00	0.35	0.976	o	|	|	|	|	1.28
28.333	0.00	0.34	0.973	o	|	|	|	|	1.28
28.417	0.00	0.34	0.971	o	|	|	|	|	1.28
28.500	0.00	0.34	0.969	o	|	|	|	|	1.28
28.583	0.00	0.34	0.966	o	|	|	|	|	1.27
28.667	0.00	0.34	0.964	o	|	|	|	|	1.27
28.750	0.00	0.34	0.962	o	|	|	|	|	1.27
28.833	0.00	0.34	0.959	o	|	|	|	|	1.26
28.917	0.00	0.34	0.957	o	|	|	|	|	1.26
29.000	0.00	0.33	0.955	o	|	|	|	|	1.26
29.083	0.00	0.33	0.952	o	|	|	|	|	1.26
29.167	0.00	0.33	0.950	o	|	|	|	|	1.25
29.250	0.00	0.33	0.948	o	|	|	|	|	1.25
29.333	0.00	0.33	0.946	o	|	|	|	|	1.25
29.417	0.00	0.33	0.943	o	|	|	|	|	1.24
29.500	0.00	0.33	0.941	o	|	|	|	|	1.24
29.583	0.00	0.33	0.939	o	|	|	|	|	1.24
29.667	0.00	0.32	0.937	o	|	|	|	|	1.24
29.750	0.00	0.32	0.934	o	|	|	|	|	1.23
29.833	0.00	0.32	0.932	o	|	|	|	|	1.23
29.917	0.00	0.32	0.930	o	|	|	|	|	1.23
30.000	0.00	0.32	0.928	o	|	|	|	|	1.23
30.083	0.00	0.32	0.925	o	|	|	|	|	1.22
30.167	0.00	0.32	0.923	o	|	|	|	|	1.22
30.250	0.00	0.32	0.921	o	|	|	|	|	1.22
30.333	0.00	0.31	0.919	o	|	|	|	|	1.22
30.417	0.00	0.31	0.917	o	|	|	|	|	1.21

30.500	0.00	0.31	0.915	o	|	|	|	|	1.21
30.583	0.00	0.31	0.912	o	|	|	|	|	1.21
30.667	0.00	0.31	0.910	o	|	|	|	|	1.20
30.750	0.00	0.31	0.908	o	|	|	|	|	1.20
30.833	0.00	0.31	0.906	o	|	|	|	|	1.20
30.917	0.00	0.31	0.904	o	|	|	|	|	1.20
31.000	0.00	0.31	0.902	o	|	|	|	|	1.19
31.083	0.00	0.30	0.900	o	|	|	|	|	1.19
31.167	0.00	0.30	0.898	o	|	|	|	|	1.19
31.250	0.00	0.30	0.896	o	|	|	|	|	1.19
31.333	0.00	0.30	0.893	o	|	|	|	|	1.18
31.417	0.00	0.30	0.891	o	|	|	|	|	1.18
31.500	0.00	0.30	0.889	o	|	|	|	|	1.18
31.583	0.00	0.30	0.887	o	|	|	|	|	1.18
31.667	0.00	0.30	0.885	o	|	|	|	|	1.17
31.750	0.00	0.30	0.883	o	|	|	|	|	1.17
31.833	0.00	0.29	0.881	o	|	|	|	|	1.17
31.917	0.00	0.29	0.879	o	|	|	|	|	1.17
32.000	0.00	0.29	0.877	o	|	|	|	|	1.16
32.083	0.00	0.29	0.875	o	|	|	|	|	1.16
32.167	0.00	0.29	0.873	o	|	|	|	|	1.16
32.250	0.00	0.29	0.871	o	|	|	|	|	1.16
32.333	0.00	0.29	0.869	o	|	|	|	|	1.15
32.417	0.00	0.29	0.867	o	|	|	|	|	1.15
32.500	0.00	0.29	0.865	o	|	|	|	|	1.15
32.583	0.00	0.28	0.863	o	|	|	|	|	1.15
32.667	0.00	0.28	0.861	o	|	|	|	|	1.14
32.750	0.00	0.28	0.859	o	|	|	|	|	1.14
32.833	0.00	0.28	0.857	o	|	|	|	|	1.14
32.917	0.00	0.28	0.855	o	|	|	|	|	1.14
33.000	0.00	0.28	0.854	o	|	|	|	|	1.14
33.083	0.00	0.28	0.852	o	|	|	|	|	1.13
33.167	0.00	0.28	0.850	o	|	|	|	|	1.13
33.250	0.00	0.28	0.848	o	|	|	|	|	1.13
33.333	0.00	0.27	0.846	o	|	|	|	|	1.13
33.417	0.00	0.27	0.844	o	|	|	|	|	1.12
33.500	0.00	0.27	0.842	o	|	|	|	|	1.12
33.583	0.00	0.27	0.840	o	|	|	|	|	1.12
33.667	0.00	0.27	0.838	o	|	|	|	|	1.12
33.750	0.00	0.27	0.837	o	|	|	|	|	1.11
33.833	0.00	0.27	0.835	o	|	|	|	|	1.11
33.917	0.00	0.27	0.833	o	|	|	|	|	1.11
34.000	0.00	0.27	0.831	o	|	|	|	|	1.11
34.083	0.00	0.27	0.829	o	|	|	|	|	1.11
34.167	0.00	0.26	0.827	o	|	|	|	|	1.10
34.250	0.00	0.26	0.826	o	|	|	|	|	1.10
34.333	0.00	0.26	0.824	o	|	|	|	|	1.10
34.417	0.00	0.26	0.822	o	|	|	|	|	1.10
34.500	0.00	0.26	0.820	o	|	|	|	|	1.09
34.583	0.00	0.26	0.818	o	|	|	|	|	1.09
34.667	0.00	0.26	0.817	o	|	|	|	|	1.09
34.750	0.00	0.26	0.815	o	|	|	|	|	1.09
34.833	0.00	0.26	0.813	o	|	|	|	|	1.09
34.917	0.00	0.26	0.811	o	|	|	|	|	1.08
35.000	0.00	0.25	0.810	o	|	|	|	|	1.08
35.083	0.00	0.25	0.808	o	|	|	|	|	1.08
35.167	0.00	0.25	0.806	o	|	|	|	|	1.08
35.250	0.00	0.25	0.804	o	|	|	|	|	1.07
35.333	0.00	0.25	0.803	o	|	|	|	|	1.07
35.417	0.00	0.25	0.801	o	|	|	|	|	1.07
35.500	0.00	0.25	0.799	o	|	|	|	|	1.07
35.583	0.00	0.25	0.797	o	|	|	|	|	1.07
35.667	0.00	0.25	0.796	o	|	|	|	|	1.06
35.750	0.00	0.25	0.794	o	|	|	|	|	1.06
35.833	0.00	0.25	0.792	o	|	|	|	|	1.06
35.917	0.00	0.24	0.791	o	|	|	|	|	1.06
36.000	0.00	0.24	0.789	o	|	|	|	|	1.06
36.083	0.00	0.24	0.787	o	|	|	|	|	1.05
36.167	0.00	0.24	0.786	o	|	|	|	|	1.05
36.250	0.00	0.24	0.784	o	|	|	|	|	1.05
36.333	0.00	0.24	0.782	o	|	|	|	|	1.05
36.417	0.00	0.24	0.781	o	|	|	|	|	1.05
36.500	0.00	0.24	0.779	o	|	|	|	|	1.04
36.583	0.00	0.24	0.777	o	|	|	|	|	1.04
36.667	0.00	0.24	0.776	o	|	|	|	|	1.04
36.750	0.00	0.24	0.774	o	|	|	|	|	1.04
36.833	0.00	0.23	0.773	o	|	|	|	|	1.04
36.917	0.00	0.23	0.771	o	|	|	|	|	1.03
37.000	0.00	0.23	0.769	o	|	|	|	|	1.03
37.083	0.00	0.23	0.768	o	|	|	|	|	1.03
37.167	0.00	0.23	0.766	o	|	|	|	|	1.03
37.250	0.00	0.23	0.765	o	|	|	|	|	1.03
37.333	0.00	0.23	0.763	o	|	|	|	|	1.02
37.417	0.00	0.23	0.761	o	|	|	|	|	1.02
37.500	0.00	0.23	0.760	o	|	|	|	|	1.02
37.583	0.00	0.23	0.758	o	|	|	|	|	1.02

37.667	0.00	0.23	0.757	o	|	|	|	|	1.02
37.750	0.00	0.22	0.755	o	|	|	|	|	1.01
37.833	0.00	0.22	0.754	o	|	|	|	|	1.01
37.917	0.00	0.22	0.752	o	|	|	|	|	1.01
38.000	0.00	0.22	0.751	o	|	|	|	|	1.01
38.083	0.00	0.22	0.749	o	|	|	|	|	1.01
38.167	0.00	0.22	0.747	o	|	|	|	|	1.01
38.250	0.00	0.22	0.746	o	|	|	|	|	1.00
38.333	0.00	0.22	0.744	o	|	|	|	|	1.00
38.417	0.00	0.22	0.743	o	|	|	|	|	1.00
38.500	0.00	0.22	0.741	o	|	|	|	|	1.00
38.583	0.00	0.22	0.740	o	|	|	|	|	1.00
38.667	0.00	0.22	0.738	o	|	|	|	|	0.99
38.750	0.00	0.22	0.737	o	|	|	|	|	0.99
38.833	0.00	0.22	0.735	o	|	|	|	|	0.99
38.917	0.00	0.22	0.734	o	|	|	|	|	0.99
39.000	0.00	0.21	0.732	o	|	|	|	|	0.99
39.083	0.00	0.21	0.731	o	|	|	|	|	0.98
39.167	0.00	0.21	0.730	o	|	|	|	|	0.98
39.250	0.00	0.21	0.728	o	|	|	|	|	0.98
39.333	0.00	0.21	0.727	o	|	|	|	|	0.98
39.417	0.00	0.21	0.725	o	|	|	|	|	0.98
39.500	0.00	0.21	0.724	o	|	|	|	|	0.97
39.583	0.00	0.21	0.722	o	|	|	|	|	0.97
39.667	0.00	0.21	0.721	o	|	|	|	|	0.97
39.750	0.00	0.21	0.719	o	|	|	|	|	0.97
39.833	0.00	0.21	0.718	o	|	|	|	|	0.97
39.917	0.00	0.21	0.716	o	|	|	|	|	0.96
40.000	0.00	0.21	0.715	o	|	|	|	|	0.96
40.083	0.00	0.21	0.714	o	|	|	|	|	0.96
40.167	0.00	0.21	0.712	o	|	|	|	|	0.96
40.250	0.00	0.21	0.711	o	|	|	|	|	0.96
40.333	0.00	0.21	0.709	o	|	|	|	|	0.95
40.417	0.00	0.21	0.708	o	|	|	|	|	0.95
40.500	0.00	0.21	0.706	o	|	|	|	|	0.95
40.583	0.00	0.21	0.705	o	|	|	|	|	0.95
40.667	0.00	0.21	0.703	o	|	|	|	|	0.95
40.750	0.00	0.21	0.702	o	|	|	|	|	0.94
40.833	0.00	0.21	0.701	o	|	|	|	|	0.94
40.917	0.00	0.21	0.699	o	|	|	|	|	0.94
41.000	0.00	0.20	0.698	o	|	|	|	|	0.94
41.083	0.00	0.20	0.696	o	|	|	|	|	0.94
41.167	0.00	0.20	0.695	o	|	|	|	|	0.94
41.250	0.00	0.20	0.694	o	|	|	|	|	0.93
41.333	0.00	0.20	0.692	o	|	|	|	|	0.93
41.417	0.00	0.20	0.691	o	|	|	|	|	0.93
41.500	0.00	0.20	0.689	o	|	|	|	|	0.93
41.583	0.00	0.20	0.688	o	|	|	|	|	0.93
41.667	0.00	0.20	0.687	o	|	|	|	|	0.92
41.750	0.00	0.20	0.685	o	|	|	|	|	0.92
41.833	0.00	0.20	0.684	o	|	|	|	|	0.92
41.917	0.00	0.20	0.682	o	|	|	|	|	0.92
42.000	0.00	0.20	0.681	o	|	|	|	|	0.92
42.083	0.00	0.20	0.680	o	|	|	|	|	0.91
42.167	0.00	0.20	0.678	o	|	|	|	|	0.91
42.250	0.00	0.20	0.677	o	|	|	|	|	0.91
42.333	0.00	0.20	0.676	o	|	|	|	|	0.91
42.417	0.00	0.20	0.674	o	|	|	|	|	0.91
42.500	0.00	0.20	0.673	o	|	|	|	|	0.91
42.583	0.00	0.20	0.672	o	|	|	|	|	0.90
42.667	0.00	0.20	0.670	o	|	|	|	|	0.90
42.750	0.00	0.20	0.669	o	|	|	|	|	0.90
42.833	0.00	0.20	0.667	o	|	|	|	|	0.90
42.917	0.00	0.20	0.666	o	|	|	|	|	0.90
43.000	0.00	0.20	0.665	o	|	|	|	|	0.89
43.083	0.00	0.19	0.663	o	|	|	|	|	0.89
43.167	0.00	0.19	0.662	o	|	|	|	|	0.89
43.250	0.00	0.19	0.661	o	|	|	|	|	0.89
43.333	0.00	0.19	0.659	o	|	|	|	|	0.89
43.417	0.00	0.19	0.658	o	|	|	|	|	0.89
43.500	0.00	0.19	0.657	o	|	|	|	|	0.88
43.583	0.00	0.19	0.655	o	|	|	|	|	0.88
43.667	0.00	0.19	0.654	o	|	|	|	|	0.88
43.750	0.00	0.19	0.653	o	|	|	|	|	0.88
43.833	0.00	0.19	0.651	o	|	|	|	|	0.88
43.917	0.00	0.19	0.650	o	|	|	|	|	0.88
44.000	0.00	0.19	0.649	o	|	|	|	|	0.87
44.083	0.00	0.19	0.648	o	|	|	|	|	0.87
44.167	0.00	0.19	0.646	o	|	|	|	|	0.87
44.250	0.00	0.19	0.645	o	|	|	|	|	0.87
44.333	0.00	0.19	0.644	o	|	|	|	|	0.87
44.417	0.00	0.19	0.642	o	|	|	|	|	0.86
44.500	0.00	0.19	0.641	o	|	|	|	|	0.86
44.583	0.00	0.19	0.640	o	|	|	|	|	0.86
44.667	0.00	0.19	0.638	o	|	|	|	|	0.86
44.750	0.00	0.19	0.637	o	|	|	|	|	0.86

44.833	0.00	0.19	0.636	o	|	|	|	|	0.86
44.917	0.00	0.19	0.635	o	|	|	|	|	0.85
45.000	0.00	0.19	0.633	o	|	|	|	|	0.85
45.083	0.00	0.19	0.632	o	|	|	|	|	0.85
45.167	0.00	0.19	0.631	o	|	|	|	|	0.85
45.250	0.00	0.18	0.629	o	|	|	|	|	0.85
45.333	0.00	0.18	0.628	o	|	|	|	|	0.85
45.417	0.00	0.18	0.627	o	|	|	|	|	0.84
45.500	0.00	0.18	0.626	o	|	|	|	|	0.84
45.583	0.00	0.18	0.624	o	|	|	|	|	0.84
45.667	0.00	0.18	0.623	o	|	|	|	|	0.84
45.750	0.00	0.18	0.622	o	|	|	|	|	0.84
45.833	0.00	0.18	0.621	o	|	|	|	|	0.84
45.917	0.00	0.18	0.619	o	|	|	|	|	0.83
46.000	0.00	0.18	0.618	o	|	|	|	|	0.83
46.083	0.00	0.18	0.617	o	|	|	|	|	0.83
46.167	0.00	0.18	0.616	o	|	|	|	|	0.83
46.250	0.00	0.18	0.614	o	|	|	|	|	0.83
46.333	0.00	0.18	0.613	o	|	|	|	|	0.83
46.417	0.00	0.18	0.612	o	|	|	|	|	0.82
46.500	0.00	0.18	0.611	o	|	|	|	|	0.82
46.583	0.00	0.18	0.609	o	|	|	|	|	0.82
46.667	0.00	0.18	0.608	o	|	|	|	|	0.82
46.750	0.00	0.18	0.607	o	|	|	|	|	0.82
46.833	0.00	0.18	0.606	o	|	|	|	|	0.82
46.917	0.00	0.18	0.605	o	|	|	|	|	0.81
47.000	0.00	0.18	0.603	o	|	|	|	|	0.81
47.083	0.00	0.18	0.602	o	|	|	|	|	0.81
47.167	0.00	0.18	0.601	o	|	|	|	|	0.81
47.250	0.00	0.18	0.600	o	|	|	|	|	0.81
47.333	0.00	0.18	0.598	o	|	|	|	|	0.81
47.417	0.00	0.18	0.597	o	|	|	|	|	0.80
47.500	0.00	0.17	0.596	o	|	|	|	|	0.80
47.583	0.00	0.17	0.595	o	|	|	|	|	0.80
47.667	0.00	0.17	0.594	o	|	|	|	|	0.80
47.750	0.00	0.17	0.592	o	|	|	|	|	0.80
47.833	0.00	0.17	0.591	o	|	|	|	|	0.80
47.917	0.00	0.17	0.590	o	|	|	|	|	0.79
48.000	0.00	0.17	0.589	o	|	|	|	|	0.79
48.083	0.00	0.17	0.588	o	|	|	|	|	0.79
48.167	0.00	0.17	0.587	o	|	|	|	|	0.79
48.250	0.00	0.17	0.585	o	|	|	|	|	0.79
48.333	0.00	0.17	0.584	o	|	|	|	|	0.79
48.417	0.00	0.17	0.583	o	|	|	|	|	0.78
48.500	0.00	0.17	0.582	o	|	|	|	|	0.78
48.583	0.00	0.17	0.581	o	|	|	|	|	0.78
48.667	0.00	0.17	0.579	o	|	|	|	|	0.78
48.750	0.00	0.17	0.578	o	|	|	|	|	0.78
48.833	0.00	0.17	0.577	o	|	|	|	|	0.78
48.917	0.00	0.17	0.576	o	|	|	|	|	0.78
49.000	0.00	0.17	0.575	o	|	|	|	|	0.77
49.083	0.00	0.17	0.574	o	|	|	|	|	0.77
49.167	0.00	0.17	0.572	o	|	|	|	|	0.77
49.250	0.00	0.17	0.571	o	|	|	|	|	0.77
49.333	0.00	0.17	0.570	o	|	|	|	|	0.77
49.417	0.00	0.17	0.569	o	|	|	|	|	0.77
49.500	0.00	0.17	0.568	o	|	|	|	|	0.76
49.583	0.00	0.17	0.567	o	|	|	|	|	0.76
49.667	0.00	0.17	0.566	o	|	|	|	|	0.76
49.750	0.00	0.17	0.564	o	|	|	|	|	0.76
49.833	0.00	0.17	0.563	o	|	|	|	|	0.76
49.917	0.00	0.16	0.562	o	|	|	|	|	0.76
50.000	0.00	0.16	0.561	o	|	|	|	|	0.76
50.083	0.00	0.16	0.560	o	|	|	|	|	0.75
50.167	0.00	0.16	0.559	o	|	|	|	|	0.75
50.250	0.00	0.16	0.558	o	|	|	|	|	0.75
50.333	0.00	0.16	0.556	o	|	|	|	|	0.75
50.417	0.00	0.16	0.555	o	|	|	|	|	0.75
50.500	0.00	0.16	0.554	o	|	|	|	|	0.75
50.583	0.00	0.16	0.553	o	|	|	|	|	0.74
50.667	0.00	0.16	0.552	o	|	|	|	|	0.74
50.750	0.00	0.16	0.551	o	|	|	|	|	0.74
50.833	0.00	0.16	0.550	o	|	|	|	|	0.74
50.917	0.00	0.16	0.549	o	|	|	|	|	0.74
51.000	0.00	0.16	0.548	o	|	|	|	|	0.74
51.083	0.00	0.16	0.546	o	|	|	|	|	0.74
51.167	0.00	0.16	0.545	o	|	|	|	|	0.73
51.250	0.00	0.16	0.544	o	|	|	|	|	0.73
51.333	0.00	0.16	0.543	o	|	|	|	|	0.73
51.417	0.00	0.16	0.542	o	|	|	|	|	0.73
51.500	0.00	0.16	0.541	o	|	|	|	|	0.73
51.583	0.00	0.16	0.540	o	|	|	|	|	0.73
51.667	0.00	0.16	0.539	o	|	|	|	|	0.73
51.750	0.00	0.16	0.538	o	|	|	|	|	0.72
51.833	0.00	0.16	0.537	o	|	|	|	|	0.72
51.917	0.00	0.16	0.536	o	|	|	|	|	0.72

52.000	0.00	0.16	0.534	o	|	|	|	|	0.72
52.083	0.00	0.16	0.533	o	|	|	|	|	0.72
52.167	0.00	0.16	0.532	o	|	|	|	|	0.72
52.250	0.00	0.16	0.531	o	|	|	|	|	0.71
52.333	0.00	0.16	0.530	o	|	|	|	|	0.71
52.417	0.00	0.16	0.529	o	|	|	|	|	0.71
52.500	0.00	0.15	0.528	o	|	|	|	|	0.71
52.583	0.00	0.15	0.527	o	|	|	|	|	0.71
52.667	0.00	0.15	0.526	o	|	|	|	|	0.71
52.750	0.00	0.15	0.525	o	|	|	|	|	0.71
52.833	0.00	0.15	0.524	o	|	|	|	|	0.70
52.917	0.00	0.15	0.523	o	|	|	|	|	0.70
53.000	0.00	0.15	0.522	o	|	|	|	|	0.70
53.083	0.00	0.15	0.521	o	|	|	|	|	0.70
53.167	0.00	0.15	0.520	o	|	|	|	|	0.70
53.250	0.00	0.15	0.518	o	|	|	|	|	0.70
53.333	0.00	0.15	0.517	o	|	|	|	|	0.70
53.417	0.00	0.15	0.516	o	|	|	|	|	0.70
53.500	0.00	0.15	0.515	o	|	|	|	|	0.69
53.583	0.00	0.15	0.514	o	|	|	|	|	0.69
53.667	0.00	0.15	0.513	o	|	|	|	|	0.69
53.750	0.00	0.15	0.512	o	|	|	|	|	0.69
53.833	0.00	0.15	0.511	o	|	|	|	|	0.69
53.917	0.00	0.15	0.510	o	|	|	|	|	0.69
54.000	0.00	0.15	0.509	o	|	|	|	|	0.69
54.083	0.00	0.15	0.508	o	|	|	|	|	0.68
54.167	0.00	0.15	0.507	o	|	|	|	|	0.68
54.250	0.00	0.15	0.506	o	|	|	|	|	0.68
54.333	0.00	0.15	0.505	o	|	|	|	|	0.68
54.417	0.00	0.15	0.504	o	|	|	|	|	0.68
54.500	0.00	0.15	0.503	o	|	|	|	|	0.68
54.583	0.00	0.15	0.502	o	|	|	|	|	0.68
54.667	0.00	0.15	0.501	o	|	|	|	|	0.67
54.750	0.00	0.15	0.500	o	|	|	|	|	0.67
54.833	0.00	0.15	0.499	o	|	|	|	|	0.67
54.917	0.00	0.15	0.498	o	|	|	|	|	0.67
55.000	0.00	0.15	0.497	o	|	|	|	|	0.67
55.083	0.00	0.15	0.496	o	|	|	|	|	0.67
55.167	0.00	0.15	0.495	o	|	|	|	|	0.67
55.250	0.00	0.14	0.494	o	|	|	|	|	0.66
55.333	0.00	0.14	0.493	o	|	|	|	|	0.66
55.417	0.00	0.14	0.492	o	|	|	|	|	0.66
55.500	0.00	0.14	0.491	o	|	|	|	|	0.66
55.583	0.00	0.14	0.490	o	|	|	|	|	0.66
55.667	0.00	0.14	0.489	o	|	|	|	|	0.66
55.750	0.00	0.14	0.488	o	|	|	|	|	0.66
55.833	0.00	0.14	0.487	o	|	|	|	|	0.66
55.917	0.00	0.14	0.486	o	|	|	|	|	0.65
56.000	0.00	0.14	0.485	o	|	|	|	|	0.65
56.083	0.00	0.14	0.484	o	|	|	|	|	0.65
56.167	0.00	0.14	0.483	o	|	|	|	|	0.65
56.250	0.00	0.14	0.482	o	|	|	|	|	0.65
56.333	0.00	0.14	0.481	o	|	|	|	|	0.65
56.417	0.00	0.14	0.480	o	|	|	|	|	0.65
56.500	0.00	0.14	0.479	o	|	|	|	|	0.64
56.583	0.00	0.14	0.478	o	|	|	|	|	0.64
56.667	0.00	0.14	0.477	o	|	|	|	|	0.64
56.750	0.00	0.14	0.476	o	|	|	|	|	0.64
56.833	0.00	0.14	0.475	o	|	|	|	|	0.64
56.917	0.00	0.14	0.474	o	|	|	|	|	0.64
57.000	0.00	0.14	0.473	o	|	|	|	|	0.64
57.083	0.00	0.14	0.472	o	|	|	|	|	0.64
57.167	0.00	0.14	0.472	o	|	|	|	|	0.63
57.250	0.00	0.14	0.471	o	|	|	|	|	0.63
57.333	0.00	0.14	0.470	o	|	|	|	|	0.63
57.417	0.00	0.14	0.469	o	|	|	|	|	0.63
57.500	0.00	0.14	0.468	o	|	|	|	|	0.63
57.583	0.00	0.14	0.467	o	|	|	|	|	0.63
57.667	0.00	0.14	0.466	o	|	|	|	|	0.63
57.750	0.00	0.14	0.465	o	|	|	|	|	0.63
57.833	0.00	0.14	0.464	o	|	|	|	|	0.62
57.917	0.00	0.14	0.463	o	|	|	|	|	0.62
58.000	0.00	0.14	0.462	o	|	|	|	|	0.62
58.083	0.00	0.14	0.461	o	|	|	|	|	0.62
58.167	0.00	0.14	0.460	o	|	|	|	|	0.62
58.250	0.00	0.13	0.459	o	|	|	|	|	0.62
58.333	0.00	0.13	0.458	o	|	|	|	|	0.62
58.417	0.00	0.13	0.457	o	|	|	|	|	0.62
58.500	0.00	0.13	0.457	o	|	|	|	|	0.61
58.583	0.00	0.13	0.456	o	|	|	|	|	0.61
58.667	0.00	0.13	0.455	o	|	|	|	|	0.61
58.750	0.00	0.13	0.454	o	|	|	|	|	0.61
58.833	0.00	0.13	0.453	o	|	|	|	|	0.61
58.917	0.00	0.13	0.452	o	|	|	|	|	0.61
59.000	0.00	0.13	0.451	o	|	|	|	|	0.61
59.083	0.00	0.13	0.450	o	|	|	|	|	0.61

59.167	0.00	0.13	0.449	o	|	|	|	0.60
59.250	0.00	0.13	0.448	o	|	|	|	0.60
59.333	0.00	0.13	0.447	o	|	|	|	0.60
59.417	0.00	0.13	0.446	o	|	|	|	0.60
59.500	0.00	0.13	0.446	o	|	|	|	0.60
59.583	0.00	0.13	0.445	o	|	|	|	0.60
59.667	0.00	0.13	0.444	o	|	|	|	0.60
59.750	0.00	0.13	0.443	o	|	|	|	0.60
59.833	0.00	0.13	0.442	o	|	|	|	0.59
59.917	0.00	0.13	0.441	o	|	|	|	0.59
60.000	0.00	0.13	0.440	o	|	|	|	0.59
60.083	0.00	0.13	0.439	o	|	|	|	0.59
60.167	0.00	0.13	0.438	o	|	|	|	0.59
60.250	0.00	0.13	0.438	o	|	|	|	0.59
60.333	0.00	0.13	0.437	o	|	|	|	0.59
60.417	0.00	0.13	0.436	o	|	|	|	0.59
60.500	0.00	0.13	0.435	o	|	|	|	0.59
60.583	0.00	0.13	0.434	o	|	|	|	0.58
60.667	0.00	0.13	0.433	o	|	|	|	0.58
60.750	0.00	0.13	0.432	o	|	|	|	0.58
60.833	0.00	0.13	0.431	o	|	|	|	0.58
60.917	0.00	0.13	0.431	o	|	|	|	0.58
61.000	0.00	0.13	0.430	o	|	|	|	0.58
61.083	0.00	0.13	0.429	o	|	|	|	0.58
61.167	0.00	0.13	0.428	o	|	|	|	0.58
61.250	0.00	0.13	0.427	o	|	|	|	0.57
61.333	0.00	0.13	0.426	o	|	|	|	0.57
61.417	0.00	0.12	0.425	o	|	|	|	0.57
61.500	0.00	0.12	0.424	o	|	|	|	0.57
61.583	0.00	0.12	0.424	o	|	|	|	0.57
61.667	0.00	0.12	0.423	o	|	|	|	0.57
61.750	0.00	0.12	0.422	o	|	|	|	0.57
61.833	0.00	0.12	0.421	o	|	|	|	0.57
61.917	0.00	0.12	0.420	o	|	|	|	0.57
62.000	0.00	0.12	0.419	o	|	|	|	0.56
62.083	0.00	0.12	0.419	o	|	|	|	0.56
62.167	0.00	0.12	0.418	o	|	|	|	0.56
62.250	0.00	0.12	0.417	o	|	|	|	0.56
62.333	0.00	0.12	0.416	o	|	|	|	0.56
62.417	0.00	0.12	0.415	o	|	|	|	0.56
62.500	0.00	0.12	0.414	o	|	|	|	0.56
62.583	0.00	0.12	0.413	o	|	|	|	0.56
62.667	0.00	0.12	0.413	o	|	|	|	0.56
62.750	0.00	0.12	0.412	o	|	|	|	0.55
62.833	0.00	0.12	0.411	o	|	|	|	0.55
62.917	0.00	0.12	0.410	o	|	|	|	0.55
63.000	0.00	0.12	0.409	o	|	|	|	0.55
63.083	0.00	0.12	0.408	o	|	|	|	0.55
63.167	0.00	0.12	0.408	o	|	|	|	0.55
63.250	0.00	0.12	0.407	o	|	|	|	0.55
63.333	0.00	0.12	0.406	o	|	|	|	0.55
63.417	0.00	0.12	0.405	o	|	|	|	0.55
63.500	0.00	0.12	0.404	o	|	|	|	0.54
63.583	0.00	0.12	0.404	o	|	|	|	0.54
63.667	0.00	0.12	0.403	o	|	|	|	0.54
63.750	0.00	0.12	0.402	o	|	|	|	0.54
63.833	0.00	0.12	0.401	o	|	|	|	0.54
63.917	0.00	0.12	0.400	o	|	|	|	0.54
64.000	0.00	0.12	0.400	o	|	|	|	0.54
64.083	0.00	0.12	0.399	o	|	|	|	0.54
64.167	0.00	0.12	0.398	o	|	|	|	0.54
64.250	0.00	0.12	0.397	o	|	|	|	0.53
64.333	0.00	0.12	0.396	o	|	|	|	0.53
64.417	0.00	0.12	0.395	o	|	|	|	0.53
64.500	0.00	0.12	0.395	o	|	|	|	0.53
64.583	0.00	0.12	0.394	o	|	|	|	0.53
64.667	0.00	0.12	0.393	o	|	|	|	0.53
64.750	0.00	0.12	0.392	o	|	|	|	0.53
64.833	0.00	0.11	0.392	o	|	|	|	0.53
64.917	0.00	0.11	0.391	o	|	|	|	0.53
65.000	0.00	0.11	0.390	o	|	|	|	0.52
65.083	0.00	0.11	0.389	o	|	|	|	0.52
65.167	0.00	0.11	0.388	o	|	|	|	0.52
65.250	0.00	0.11	0.388	o	|	|	|	0.52
65.333	0.00	0.11	0.387	o	|	|	|	0.52
65.417	0.00	0.11	0.386	o	|	|	|	0.52
65.500	0.00	0.11	0.385	o	|	|	|	0.52
65.583	0.00	0.11	0.384	o	|	|	|	0.52
65.667	0.00	0.11	0.384	o	|	|	|	0.52
65.750	0.00	0.11	0.383	o	|	|	|	0.52
65.833	0.00	0.11	0.382	o	|	|	|	0.51
65.917	0.00	0.11	0.381	o	|	|	|	0.51
66.000	0.00	0.11	0.381	o	|	|	|	0.51
66.083	0.00	0.11	0.380	o	|	|	|	0.51
66.167	0.00	0.11	0.379	o	|	|	|	0.51
66.250	0.00	0.11	0.378	o	|	|	|	0.51

66.333	0.00	0.11	0.378	o	|	|	|	|	0.51
66.417	0.00	0.11	0.377	o	|	|	|	|	0.51
66.500	0.00	0.11	0.376	o	|	|	|	|	0.51
66.583	0.00	0.11	0.375	o	|	|	|	|	0.51
66.667	0.00	0.11	0.374	o	|	|	|	|	0.50
66.750	0.00	0.11	0.374	o	|	|	|	|	0.50
66.833	0.00	0.11	0.373	o	|	|	|	|	0.50
66.917	0.00	0.11	0.372	o	|	|	|	|	0.50
67.000	0.00	0.11	0.371	o	|	|	|	|	0.50
67.083	0.00	0.11	0.371	o	|	|	|	|	0.50
67.167	0.00	0.11	0.370	o	|	|	|	|	0.50
67.250	0.00	0.11	0.369	o	|	|	|	|	0.50
67.333	0.00	0.11	0.368	o	|	|	|	|	0.50
67.417	0.00	0.11	0.368	o	|	|	|	|	0.49
67.500	0.00	0.11	0.367	o	|	|	|	|	0.49
67.583	0.00	0.11	0.366	o	|	|	|	|	0.49
67.667	0.00	0.11	0.366	o	|	|	|	|	0.49
67.750	0.00	0.11	0.365	o	|	|	|	|	0.49
67.833	0.00	0.11	0.364	o	|	|	|	|	0.49
67.917	0.00	0.11	0.363	o	|	|	|	|	0.49
68.000	0.00	0.11	0.363	o	|	|	|	|	0.49
68.083	0.00	0.11	0.362	o	|	|	|	|	0.49
68.167	0.00	0.11	0.361	o	|	|	|	|	0.49
68.250	0.00	0.11	0.360	o	|	|	|	|	0.49
68.333	0.00	0.11	0.360	o	|	|	|	|	0.48
68.417	0.00	0.11	0.359	o	|	|	|	|	0.48
68.500	0.00	0.11	0.358	o	|	|	|	|	0.48
68.583	0.00	0.10	0.357	o	|	|	|	|	0.48
68.667	0.00	0.10	0.357	o	|	|	|	|	0.48
68.750	0.00	0.10	0.356	o	|	|	|	|	0.48
68.833	0.00	0.10	0.355	o	|	|	|	|	0.48
68.917	0.00	0.10	0.355	o	|	|	|	|	0.48
69.000	0.00	0.10	0.354	o	|	|	|	|	0.48
69.083	0.00	0.10	0.353	o	|	|	|	|	0.48
69.167	0.00	0.10	0.352	o	|	|	|	|	0.47
69.250	0.00	0.10	0.352	o	|	|	|	|	0.47
69.333	0.00	0.10	0.351	o	|	|	|	|	0.47
69.417	0.00	0.10	0.350	o	|	|	|	|	0.47
69.500	0.00	0.10	0.350	o	|	|	|	|	0.47
69.583	0.00	0.10	0.349	o	|	|	|	|	0.47
69.667	0.00	0.10	0.348	o	|	|	|	|	0.47
69.750	0.00	0.10	0.348	o	|	|	|	|	0.47
69.833	0.00	0.10	0.347	o	|	|	|	|	0.47
69.917	0.00	0.10	0.346	o	|	|	|	|	0.47
70.000	0.00	0.10	0.345	o	|	|	|	|	0.46
70.083	0.00	0.10	0.345	o	|	|	|	|	0.46
70.167	0.00	0.10	0.344	o	|	|	|	|	0.46
70.250	0.00	0.10	0.343	o	|	|	|	|	0.46
70.333	0.00	0.10	0.343	o	|	|	|	|	0.46
70.417	0.00	0.10	0.342	o	|	|	|	|	0.46
70.500	0.00	0.10	0.341	o	|	|	|	|	0.46
70.583	0.00	0.10	0.341	o	|	|	|	|	0.46

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 847
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 39.828 (CFS)
Total volume = 3.686 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro11006100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 77
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 45.277 (CFS)
Total volume = 5.831 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 77
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	11.3	22.64	33.96	45.28	Depth (Ft.)
0.083	1.01	0.00	0.003	O					0.00
0.167	2.80	0.00	0.017	OI					0.02
0.250	3.61	0.01	0.039	O I					0.05
0.333	3.88	0.02	0.064	O I					0.09
0.417	4.00	0.03	0.091	O I					0.12
0.500	4.39	0.04	0.120	O I					0.16
0.583	4.86	0.04	0.152	O I					0.20
0.667	4.97	0.05	0.185	O I					0.25
0.750	5.02	0.06	0.219	O I					0.29
0.833	5.04	0.07	0.253	O I					0.34
0.917	5.06	0.08	0.287	O I					0.39
1.000	5.37	0.09	0.323	O I					0.43
1.083	5.83	0.11	0.361	O I					0.49
1.167	5.94	0.12	0.400	O I					0.54
1.250	5.99	0.13	0.441	O I					0.59
1.333	6.02	0.14	0.481	O I					0.65
1.417	6.03	0.15	0.522	O I					0.70
1.500	6.03	0.16	0.562	O I					0.76
1.583	6.03	0.18	0.602	O I					0.81
1.667	6.03	0.19	0.643	O I					0.86
1.750	6.03	0.20	0.683	O I					0.92

1.833	6.03	0.21	0.723	O	I	|	|	|	0.97
1.917	6.03	0.23	0.763	O	I	|	|	|	1.02
2.000	6.34	0.25	0.804	O	I	|	|	|	1.07
2.083	6.49	0.27	0.846	O	I	|	|	|	1.13
2.167	6.45	0.30	0.889	O	I	|	|	|	1.18
2.250	6.85	0.32	0.933	O	I	|	|	|	1.23
2.333	6.94	0.35	0.978	O	I	|	|	|	1.29
2.417	6.98	0.37	1.023	O	I	|	|	|	1.34
2.500	6.99	0.40	1.069	O	I	|	|	|	1.40
2.583	7.00	0.42	1.114	O	I	|	|	|	1.45
2.667	7.00	0.45	1.159	O	I	|	|	|	1.51
2.750	7.31	0.47	1.205	O	I	|	|	|	1.57
2.833	7.77	0.50	1.254	O	I	|	|	|	1.62
2.917	7.88	0.53	1.304	O	I	|	|	|	1.69
3.000	7.93	0.55	1.355	O	I	|	|	|	1.75
3.083	7.96	0.58	1.406	O	I	|	|	|	1.81
3.167	8.29	0.61	1.458	O	I	|	|	|	1.87
3.250	8.74	0.64	1.512	O	I	|	|	|	1.94
3.333	8.85	0.67	1.568	O	I	|	|	|	2.01
3.417	9.22	0.73	1.625	O	I	|	|	|	2.07
3.500	10.01	0.79	1.686	O	I	|	|	|	2.14
3.583	10.91	0.85	1.753	O	I	|	|	|	2.21
3.667	11.53	0.92	1.824	O	I	|	|	|	2.29
3.750	12.03	0.99	1.899	O	I	|	|	|	2.38
3.833	12.57	1.06	1.976	O	I	|	|	|	2.46
3.917	13.04	1.14	2.057	O	I	|	|	|	2.55
4.000	13.56	1.22	2.140	O	I	|	|	|	2.65
4.083	14.01	1.30	2.227	O	I	|	|	|	2.74
4.167	14.84	1.39	2.317	O	I	|	|	|	2.84
4.250	15.75	1.48	2.412	O	I	|	|	|	2.95
4.333	16.70	6.39	2.497	O	I	|	|	|	3.04
4.417	17.65	12.68	2.549	O	I	|	|	|	3.10
4.500	18.31	15.78	2.575	O	I	|	|	|	3.13
4.583	18.82	17.40	2.589	O	I	|	|	|	3.14
4.667	19.68	18.48	2.598	O	I	|	|	|	3.15
4.750	20.60	19.45	2.606	O	I	|	|	|	3.16
4.833	21.24	20.31	2.613	O	I	|	|	|	3.17
4.917	21.73	20.99	2.619	O	I	|	|	|	3.17
5.000	22.59	21.68	2.624	O	I	|	|	|	3.18
5.083	24.77	22.85	2.634	O	I	|	|	|	3.19
5.167	28.81	25.15	2.654	O	I	|	|	|	3.21
5.250	32.67	28.41	2.681	O	I	|	|	|	3.24
5.333	35.82	31.82	2.709	O	I	|	|	|	3.27
5.417	39.48	35.22	2.738	O	I	|	|	|	3.30
5.500	45.28	39.40	2.773	O	I	|	|	|	3.33
5.583	38.61	40.88	2.785	O	I	|	|	|	3.35
5.667	19.85	34.08	2.728	O	I	|	|	|	3.29
5.750	10.84	23.15	2.637	O	I	|	|	|	3.19
5.833	6.55	14.71	2.566	O	I	|	|	|	3.12
5.917	3.95	9.19	2.520	O	I	|	|	|	3.07
6.000	1.98	5.56	2.490	O	I	|	|	|	3.04
6.083	0.99	3.18	2.470	O	I	|	|	|	3.01
6.167	0.32	1.71	2.458	O	I	|	|	|	3.00
6.250	0.13	1.51	2.448	O	I	|	|	|	2.99
6.333	0.05	1.50	2.438	O	I	|	|	|	2.98
6.417	0.01	1.49	2.428	O	I	|	|	|	2.97
6.500	0.00	1.48	2.418	O	I	|	|	|	2.96
6.583	0.00	1.47	2.408	O	I	|	|	|	2.95
6.667	0.00	1.46	2.398	O	I	|	|	|	2.93
6.750	0.00	1.45	2.388	O	I	|	|	|	2.92
6.833	0.00	1.44	2.378	O	I	|	|	|	2.91
6.917	0.00	1.43	2.368	O	I	|	|	|	2.90
7.000	0.00	1.42	2.358	O	I	|	|	|	2.89
7.083	0.00	1.42	2.348	O	I	|	|	|	2.88
7.167	0.00	1.41	2.338	O	|	|	|	|	2.87
7.250	0.00	1.40	2.329	O	|	|	|	|	2.86
7.333	0.00	1.39	2.319	O	|	|	|	|	2.85
7.417	0.00	1.38	2.310	O	|	|	|	|	2.84
7.500	0.00	1.37	2.300	O	|	|	|	|	2.83
7.583	0.00	1.36	2.291	O	|	|	|	|	2.82
7.667	0.00	1.35	2.281	O	|	|	|	|	2.80
7.750	0.00	1.34	2.272	O	|	|	|	|	2.79
7.833	0.00	1.33	2.263	O	|	|	|	|	2.78
7.917	0.00	1.33	2.254	O	|	|	|	|	2.77
8.000	0.00	1.32	2.245	O	|	|	|	|	2.76
8.083	0.00	1.31	2.236	O	|	|	|	|	2.75
8.167	0.00	1.30	2.227	O	|	|	|	|	2.74
8.250	0.00	1.29	2.218	O	|	|	|	|	2.73
8.333	0.00	1.28	2.209	O	|	|	|	|	2.72
8.417	0.00	1.27	2.200	O	|	|	|	|	2.71
8.500	0.00	1.27	2.191	O	|	|	|	|	2.70
8.583	0.00	1.26	2.183	O	|	|	|	|	2.69
8.667	0.00	1.25	2.174	O	|	|	|	|	2.68
8.750	0.00	1.24	2.165	O	|	|	|	|	2.68
8.833	0.00	1.23	2.157	O	|	|	|	|	2.67
8.917	0.00	1.23	2.148	O	|	|	|	|	2.66

9.000	0.00	1.22	2.140	o	|	|	|	|	2.65
9.083	0.00	1.21	2.132	o	|	|	|	|	2.64
9.167	0.00	1.20	2.123	o	|	|	|	|	2.63
9.250	0.00	1.19	2.115	o	|	|	|	|	2.62
9.333	0.00	1.19	2.107	o	|	|	|	|	2.61
9.417	0.00	1.18	2.099	o	|	|	|	|	2.60
9.500	0.00	1.17	2.091	o	|	|	|	|	2.59
9.583	0.00	1.16	2.083	o	|	|	|	|	2.58
9.667	0.00	1.16	2.075	o	|	|	|	|	2.57
9.750	0.00	1.15	2.067	o	|	|	|	|	2.57
9.833	0.00	1.14	2.059	o	|	|	|	|	2.56
9.917	0.00	1.13	2.051	o	|	|	|	|	2.55
10.000	0.00	1.13	2.043	o	|	|	|	|	2.54
10.083	0.00	1.12	2.035	o	|	|	|	|	2.53
10.167	0.00	1.11	2.028	o	|	|	|	|	2.52
10.250	0.00	1.10	2.020	o	|	|	|	|	2.51
10.333	0.00	1.10	2.013	o	|	|	|	|	2.50
10.417	0.00	1.09	2.005	o	|	|	|	|	2.50
10.500	0.00	1.08	1.998	o	|	|	|	|	2.49
10.583	0.00	1.08	1.990	o	|	|	|	|	2.48
10.667	0.00	1.07	1.983	o	|	|	|	|	2.47
10.750	0.00	1.06	1.975	o	|	|	|	|	2.46
10.833	0.00	1.05	1.968	o	|	|	|	|	2.45
10.917	0.00	1.05	1.961	o	|	|	|	|	2.45
11.000	0.00	1.04	1.954	o	|	|	|	|	2.44
11.083	0.00	1.03	1.947	o	|	|	|	|	2.43
11.167	0.00	1.03	1.939	o	|	|	|	|	2.42
11.250	0.00	1.02	1.932	o	|	|	|	|	2.41
11.333	0.00	1.01	1.925	o	|	|	|	|	2.41
11.417	0.00	1.01	1.918	o	|	|	|	|	2.40
11.500	0.00	1.00	1.912	o	|	|	|	|	2.39
11.583	0.00	0.99	1.905	o	|	|	|	|	2.38
11.667	0.00	0.99	1.898	o	|	|	|	|	2.38
11.750	0.00	0.98	1.891	o	|	|	|	|	2.37
11.833	0.00	0.98	1.884	o	|	|	|	|	2.36
11.917	0.00	0.97	1.878	o	|	|	|	|	2.35
12.000	0.00	0.96	1.871	o	|	|	|	|	2.35
12.083	0.00	0.96	1.864	o	|	|	|	|	2.34
12.167	0.00	0.95	1.858	o	|	|	|	|	2.33
12.250	0.00	0.94	1.851	o	|	|	|	|	2.32
12.333	0.00	0.94	1.845	o	|	|	|	|	2.32
12.417	0.00	0.93	1.838	o	|	|	|	|	2.31
12.500	0.00	0.93	1.832	o	|	|	|	|	2.30
12.583	0.00	0.92	1.826	o	|	|	|	|	2.30
12.667	0.00	0.91	1.819	o	|	|	|	|	2.29
12.750	0.00	0.91	1.813	o	|	|	|	|	2.28
12.833	0.00	0.90	1.807	o	|	|	|	|	2.27
12.917	0.00	0.90	1.801	o	|	|	|	|	2.27
13.000	0.00	0.89	1.794	o	|	|	|	|	2.26
13.083	0.00	0.88	1.788	o	|	|	|	|	2.25
13.167	0.00	0.88	1.782	o	|	|	|	|	2.25
13.250	0.00	0.87	1.776	o	|	|	|	|	2.24
13.333	0.00	0.87	1.770	o	|	|	|	|	2.23
13.417	0.00	0.86	1.764	o	|	|	|	|	2.23
13.500	0.00	0.86	1.758	o	|	|	|	|	2.22
13.583	0.00	0.85	1.753	o	|	|	|	|	2.21
13.667	0.00	0.84	1.747	o	|	|	|	|	2.21
13.750	0.00	0.84	1.741	o	|	|	|	|	2.20
13.833	0.00	0.83	1.735	o	|	|	|	|	2.19
13.917	0.00	0.83	1.729	o	|	|	|	|	2.19
14.000	0.00	0.82	1.724	o	|	|	|	|	2.18
14.083	0.00	0.82	1.718	o	|	|	|	|	2.18
14.167	0.00	0.81	1.712	o	|	|	|	|	2.17
14.250	0.00	0.81	1.707	o	|	|	|	|	2.16
14.333	0.00	0.80	1.701	o	|	|	|	|	2.16
14.417	0.00	0.80	1.696	o	|	|	|	|	2.15
14.500	0.00	0.79	1.690	o	|	|	|	|	2.14
14.583	0.00	0.79	1.685	o	|	|	|	|	2.14
14.667	0.00	0.78	1.680	o	|	|	|	|	2.13
14.750	0.00	0.78	1.674	o	|	|	|	|	2.13
14.833	0.00	0.77	1.669	o	|	|	|	|	2.12
14.917	0.00	0.77	1.664	o	|	|	|	|	2.11
15.000	0.00	0.76	1.658	o	|	|	|	|	2.11
15.083	0.00	0.76	1.653	o	|	|	|	|	2.10
15.167	0.00	0.75	1.648	o	|	|	|	|	2.10
15.250	0.00	0.75	1.643	o	|	|	|	|	2.09
15.333	0.00	0.74	1.638	o	|	|	|	|	2.09
15.417	0.00	0.74	1.633	o	|	|	|	|	2.08
15.500	0.00	0.73	1.628	o	|	|	|	|	2.07
15.583	0.00	0.73	1.623	o	|	|	|	|	2.07
15.667	0.00	0.72	1.618	o	|	|	|	|	2.06
15.750	0.00	0.72	1.613	o	|	|	|	|	2.06
15.833	0.00	0.71	1.608	o	|	|	|	|	2.05
15.917	0.00	0.71	1.603	o	|	|	|	|	2.05
16.000	0.00	0.70	1.598	o	|	|	|	|	2.04
16.083	0.00	0.70	1.593	o	|	|	|	|	2.04

16.167	0.00	0.69	1.588	o	|	|	|	|	2.03
16.250	0.00	0.69	1.584	o	|	|	|	|	2.03
16.333	0.00	0.68	1.579	o	|	|	|	|	2.02
16.417	0.00	0.68	1.574	o	|	|	|	|	2.01
16.500	0.00	0.68	1.569	o	|	|	|	|	2.01
16.583	0.00	0.67	1.565	o	|	|	|	|	2.00
16.667	0.00	0.67	1.560	o	|	|	|	|	2.00
16.750	0.00	0.67	1.556	o	|	|	|	|	1.99
16.833	0.00	0.66	1.551	o	|	|	|	|	1.99
16.917	0.00	0.66	1.546	o	|	|	|	|	1.98
17.000	0.00	0.66	1.542	o	|	|	|	|	1.98
17.083	0.00	0.66	1.537	o	|	|	|	|	1.97
17.167	0.00	0.65	1.533	o	|	|	|	|	1.97
17.250	0.00	0.65	1.528	o	|	|	|	|	1.96
17.333	0.00	0.65	1.524	o	|	|	|	|	1.95
17.417	0.00	0.65	1.519	o	|	|	|	|	1.95
17.500	0.00	0.64	1.515	o	|	|	|	|	1.94
17.583	0.00	0.64	1.511	o	|	|	|	|	1.94
17.667	0.00	0.64	1.506	o	|	|	|	|	1.93
17.750	0.00	0.64	1.502	o	|	|	|	|	1.93
17.833	0.00	0.63	1.497	o	|	|	|	|	1.92
17.917	0.00	0.63	1.493	o	|	|	|	|	1.92
18.000	0.00	0.63	1.489	o	|	|	|	|	1.91
18.083	0.00	0.63	1.484	o	|	|	|	|	1.91
18.167	0.00	0.62	1.480	o	|	|	|	|	1.90
18.250	0.00	0.62	1.476	o	|	|	|	|	1.90
18.333	0.00	0.62	1.472	o	|	|	|	|	1.89
18.417	0.00	0.62	1.467	o	|	|	|	|	1.89
18.500	0.00	0.61	1.463	o	|	|	|	|	1.88
18.583	0.00	0.61	1.459	o	|	|	|	|	1.88
18.667	0.00	0.61	1.455	o	|	|	|	|	1.87
18.750	0.00	0.61	1.451	o	|	|	|	|	1.86
18.833	0.00	0.60	1.446	o	|	|	|	|	1.86
18.917	0.00	0.60	1.442	o	|	|	|	|	1.85
19.000	0.00	0.60	1.438	o	|	|	|	|	1.85
19.083	0.00	0.60	1.434	o	|	|	|	|	1.84
19.167	0.00	0.60	1.430	o	|	|	|	|	1.84
19.250	0.00	0.59	1.426	o	|	|	|	|	1.83
19.333	0.00	0.59	1.422	o	|	|	|	|	1.83
19.417	0.00	0.59	1.418	o	|	|	|	|	1.82
19.500	0.00	0.59	1.414	o	|	|	|	|	1.82
19.583	0.00	0.58	1.409	o	|	|	|	|	1.81
19.667	0.00	0.58	1.405	o	|	|	|	|	1.81
19.750	0.00	0.58	1.401	o	|	|	|	|	1.80
19.833	0.00	0.58	1.397	o	|	|	|	|	1.80
19.917	0.00	0.58	1.393	o	|	|	|	|	1.80
20.000	0.00	0.57	1.390	o	|	|	|	|	1.79
20.083	0.00	0.57	1.386	o	|	|	|	|	1.79
20.167	0.00	0.57	1.382	o	|	|	|	|	1.78
20.250	0.00	0.57	1.378	o	|	|	|	|	1.78
20.333	0.00	0.57	1.374	o	|	|	|	|	1.77
20.417	0.00	0.56	1.370	o	|	|	|	|	1.77
20.500	0.00	0.56	1.366	o	|	|	|	|	1.76
20.583	0.00	0.56	1.362	o	|	|	|	|	1.76
20.667	0.00	0.56	1.358	o	|	|	|	|	1.75
20.750	0.00	0.55	1.355	o	|	|	|	|	1.75
20.833	0.00	0.55	1.351	o	|	|	|	|	1.74
20.917	0.00	0.55	1.347	o	|	|	|	|	1.74
21.000	0.00	0.55	1.343	o	|	|	|	|	1.73
21.083	0.00	0.55	1.339	o	|	|	|	|	1.73
21.167	0.00	0.54	1.336	o	|	|	|	|	1.72
21.250	0.00	0.54	1.332	o	|	|	|	|	1.72
21.333	0.00	0.54	1.328	o	|	|	|	|	1.72
21.417	0.00	0.54	1.324	o	|	|	|	|	1.71
21.500	0.00	0.54	1.321	o	|	|	|	|	1.71
21.583	0.00	0.53	1.317	o	|	|	|	|	1.70
21.667	0.00	0.53	1.313	o	|	|	|	|	1.70
21.750	0.00	0.53	1.310	o	|	|	|	|	1.69
21.833	0.00	0.53	1.306	o	|	|	|	|	1.69
21.917	0.00	0.53	1.303	o	|	|	|	|	1.68
22.000	0.00	0.52	1.299	o	|	|	|	|	1.68
22.083	0.00	0.52	1.295	o	|	|	|	|	1.68
22.167	0.00	0.52	1.292	o	|	|	|	|	1.67
22.250	0.00	0.52	1.288	o	|	|	|	|	1.67
22.333	0.00	0.52	1.285	o	|	|	|	|	1.66
22.417	0.00	0.51	1.281	o	|	|	|	|	1.66
22.500	0.00	0.51	1.277	o	|	|	|	|	1.65
22.583	0.00	0.51	1.274	o	|	|	|	|	1.65
22.667	0.00	0.51	1.270	o	|	|	|	|	1.64
22.750	0.00	0.51	1.267	o	|	|	|	|	1.64
22.833	0.00	0.50	1.263	o	|	|	|	|	1.64
22.917	0.00	0.50	1.260	o	|	|	|	|	1.63
23.000	0.00	0.50	1.257	o	|	|	|	|	1.63
23.083	0.00	0.50	1.253	o	|	|	|	|	1.62
23.167	0.00	0.50	1.250	o	|	|	|	|	1.62
23.250	0.00	0.49	1.246	o	|	|	|	|	1.62

23.333	0.00	0.49	1.243	o	|	|	|	|	1.61
23.417	0.00	0.49	1.239	o	|	|	|	|	1.61
23.500	0.00	0.49	1.236	o	|	|	|	|	1.60
23.583	0.00	0.49	1.233	o	|	|	|	|	1.60
23.667	0.00	0.49	1.229	o	|	|	|	|	1.59
23.750	0.00	0.48	1.226	o	|	|	|	|	1.59
23.833	0.00	0.48	1.223	o	|	|	|	|	1.59
23.917	0.00	0.48	1.219	o	|	|	|	|	1.58
24.000	0.00	0.48	1.216	o	|	|	|	|	1.58
24.083	0.00	0.48	1.213	o	|	|	|	|	1.57
24.167	0.00	0.47	1.210	o	|	|	|	|	1.57
24.250	0.00	0.47	1.206	o	|	|	|	|	1.57
24.333	0.00	0.47	1.203	o	|	|	|	|	1.56
24.417	0.00	0.47	1.200	o	|	|	|	|	1.56
24.500	0.00	0.47	1.197	o	|	|	|	|	1.55
24.583	0.00	0.47	1.193	o	|	|	|	|	1.55
24.667	0.00	0.46	1.190	o	|	|	|	|	1.55
24.750	0.00	0.46	1.187	o	|	|	|	|	1.54
24.833	0.00	0.46	1.184	o	|	|	|	|	1.54
24.917	0.00	0.46	1.181	o	|	|	|	|	1.54
25.000	0.00	0.46	1.177	o	|	|	|	|	1.53
25.083	0.00	0.46	1.174	o	|	|	|	|	1.53
25.167	0.00	0.45	1.171	o	|	|	|	|	1.52
25.250	0.00	0.45	1.168	o	|	|	|	|	1.52
25.333	0.00	0.45	1.165	o	|	|	|	|	1.52
25.417	0.00	0.45	1.162	o	|	|	|	|	1.51
25.500	0.00	0.45	1.159	o	|	|	|	|	1.51
25.583	0.00	0.45	1.156	o	|	|	|	|	1.50
25.667	0.00	0.44	1.153	o	|	|	|	|	1.50
25.750	0.00	0.44	1.150	o	|	|	|	|	1.50
25.833	0.00	0.44	1.147	o	|	|	|	|	1.49
25.917	0.00	0.44	1.144	o	|	|	|	|	1.49
26.000	0.00	0.44	1.141	o	|	|	|	|	1.49
26.083	0.00	0.44	1.138	o	|	|	|	|	1.48
26.167	0.00	0.43	1.135	o	|	|	|	|	1.48
26.250	0.00	0.43	1.132	o	|	|	|	|	1.48
26.333	0.00	0.43	1.129	o	|	|	|	|	1.47
26.417	0.00	0.43	1.126	o	|	|	|	|	1.47
26.500	0.00	0.43	1.123	o	|	|	|	|	1.46
26.583	0.00	0.43	1.120	o	|	|	|	|	1.46
26.667	0.00	0.42	1.117	o	|	|	|	|	1.46
26.750	0.00	0.42	1.114	o	|	|	|	|	1.45
26.833	0.00	0.42	1.111	o	|	|	|	|	1.45
26.917	0.00	0.42	1.108	o	|	|	|	|	1.45
27.000	0.00	0.42	1.105	o	|	|	|	|	1.44
27.083	0.00	0.42	1.102	o	|	|	|	|	1.44
27.167	0.00	0.41	1.100	o	|	|	|	|	1.44
27.250	0.00	0.41	1.097	o	|	|	|	|	1.43
27.333	0.00	0.41	1.094	o	|	|	|	|	1.43
27.417	0.00	0.41	1.091	o	|	|	|	|	1.43
27.500	0.00	0.41	1.088	o	|	|	|	|	1.42
27.583	0.00	0.41	1.085	o	|	|	|	|	1.42
27.667	0.00	0.40	1.083	o	|	|	|	|	1.42
27.750	0.00	0.40	1.080	o	|	|	|	|	1.41
27.833	0.00	0.40	1.077	o	|	|	|	|	1.41
27.917	0.00	0.40	1.074	o	|	|	|	|	1.41
28.000	0.00	0.40	1.072	o	|	|	|	|	1.40
28.083	0.00	0.40	1.069	o	|	|	|	|	1.40
28.167	0.00	0.40	1.066	o	|	|	|	|	1.39
28.250	0.00	0.39	1.063	o	|	|	|	|	1.39
28.333	0.00	0.39	1.061	o	|	|	|	|	1.39
28.417	0.00	0.39	1.058	o	|	|	|	|	1.39
28.500	0.00	0.39	1.055	o	|	|	|	|	1.38
28.583	0.00	0.39	1.053	o	|	|	|	|	1.38
28.667	0.00	0.39	1.050	o	|	|	|	|	1.38
28.750	0.00	0.39	1.047	o	|	|	|	|	1.37
28.833	0.00	0.38	1.045	o	|	|	|	|	1.37
28.917	0.00	0.38	1.042	o	|	|	|	|	1.37
29.000	0.00	0.38	1.039	o	|	|	|	|	1.36
29.083	0.00	0.38	1.037	o	|	|	|	|	1.36
29.167	0.00	0.38	1.034	o	|	|	|	|	1.36
29.250	0.00	0.38	1.032	o	|	|	|	|	1.35
29.333	0.00	0.38	1.029	o	|	|	|	|	1.35
29.417	0.00	0.37	1.026	o	|	|	|	|	1.35
29.500	0.00	0.37	1.024	o	|	|	|	|	1.34
29.583	0.00	0.37	1.021	o	|	|	|	|	1.34
29.667	0.00	0.37	1.019	o	|	|	|	|	1.34
29.750	0.00	0.37	1.016	o	|	|	|	|	1.33
29.833	0.00	0.37	1.014	o	|	|	|	|	1.33
29.917	0.00	0.37	1.011	o	|	|	|	|	1.33
30.000	0.00	0.36	1.009	o	|	|	|	|	1.32
30.083	0.00	0.36	1.006	o	|	|	|	|	1.32
30.167	0.00	0.36	1.004	o	|	|	|	|	1.32
30.250	0.00	0.36	1.001	o	|	|	|	|	1.32
30.333	0.00	0.36	0.999	o	|	|	|	|	1.31
30.417	0.00	0.36	0.996	o	|	|	|	|	1.31

30.500	0.00	0.36	0.994	o	|	|	|	|	1.31
30.583	0.00	0.35	0.991	o	|	|	|	|	1.30
30.667	0.00	0.35	0.989	o	|	|	|	|	1.30
30.750	0.00	0.35	0.986	o	|	|	|	|	1.30
30.833	0.00	0.35	0.984	o	|	|	|	|	1.29
30.917	0.00	0.35	0.982	o	|	|	|	|	1.29
31.000	0.00	0.35	0.979	o	|	|	|	|	1.29
31.083	0.00	0.35	0.977	o	|	|	|	|	1.29
31.167	0.00	0.35	0.974	o	|	|	|	|	1.28
31.250	0.00	0.34	0.972	o	|	|	|	|	1.28
31.333	0.00	0.34	0.970	o	|	|	|	|	1.28
31.417	0.00	0.34	0.967	o	|	|	|	|	1.27
31.500	0.00	0.34	0.965	o	|	|	|	|	1.27
31.583	0.00	0.34	0.963	o	|	|	|	|	1.27
31.667	0.00	0.34	0.960	o	|	|	|	|	1.27
31.750	0.00	0.34	0.958	o	|	|	|	|	1.26
31.833	0.00	0.33	0.956	o	|	|	|	|	1.26
31.917	0.00	0.33	0.953	o	|	|	|	|	1.26
32.000	0.00	0.33	0.951	o	|	|	|	|	1.25
32.083	0.00	0.33	0.949	o	|	|	|	|	1.25
32.167	0.00	0.33	0.946	o	|	|	|	|	1.25
32.250	0.00	0.33	0.944	o	|	|	|	|	1.25
32.333	0.00	0.33	0.942	o	|	|	|	|	1.24
32.417	0.00	0.33	0.940	o	|	|	|	|	1.24
32.500	0.00	0.32	0.937	o	|	|	|	|	1.24
32.583	0.00	0.32	0.935	o	|	|	|	|	1.23
32.667	0.00	0.32	0.933	o	|	|	|	|	1.23
32.750	0.00	0.32	0.931	o	|	|	|	|	1.23
32.833	0.00	0.32	0.929	o	|	|	|	|	1.23
32.917	0.00	0.32	0.926	o	|	|	|	|	1.22
33.000	0.00	0.32	0.924	o	|	|	|	|	1.22
33.083	0.00	0.32	0.922	o	|	|	|	|	1.22
33.167	0.00	0.32	0.920	o	|	|	|	|	1.22
33.250	0.00	0.31	0.918	o	|	|	|	|	1.21
33.333	0.00	0.31	0.915	o	|	|	|	|	1.21
33.417	0.00	0.31	0.913	o	|	|	|	|	1.21
33.500	0.00	0.31	0.911	o	|	|	|	|	1.21
33.583	0.00	0.31	0.909	o	|	|	|	|	1.20
33.667	0.00	0.31	0.907	o	|	|	|	|	1.20
33.750	0.00	0.31	0.905	o	|	|	|	|	1.20
33.833	0.00	0.31	0.903	o	|	|	|	|	1.20
33.917	0.00	0.30	0.901	o	|	|	|	|	1.19
34.000	0.00	0.30	0.899	o	|	|	|	|	1.19
34.083	0.00	0.30	0.896	o	|	|	|	|	1.19
34.167	0.00	0.30	0.894	o	|	|	|	|	1.19
34.250	0.00	0.30	0.892	o	|	|	|	|	1.18
34.333	0.00	0.30	0.890	o	|	|	|	|	1.18
34.417	0.00	0.30	0.888	o	|	|	|	|	1.18
34.500	0.00	0.30	0.886	o	|	|	|	|	1.17
34.583	0.00	0.30	0.884	o	|	|	|	|	1.17
34.667	0.00	0.29	0.882	o	|	|	|	|	1.17
34.750	0.00	0.29	0.880	o	|	|	|	|	1.17
34.833	0.00	0.29	0.878	o	|	|	|	|	1.17
34.917	0.00	0.29	0.876	o	|	|	|	|	1.16
35.000	0.00	0.29	0.874	o	|	|	|	|	1.16
35.083	0.00	0.29	0.872	o	|	|	|	|	1.16
35.167	0.00	0.29	0.870	o	|	|	|	|	1.16
35.250	0.00	0.29	0.868	o	|	|	|	|	1.15
35.333	0.00	0.29	0.866	o	|	|	|	|	1.15
35.417	0.00	0.28	0.864	o	|	|	|	|	1.15
35.500	0.00	0.28	0.862	o	|	|	|	|	1.15
35.583	0.00	0.28	0.860	o	|	|	|	|	1.14
35.667	0.00	0.28	0.858	o	|	|	|	|	1.14
35.750	0.00	0.28	0.856	o	|	|	|	|	1.14
35.833	0.00	0.28	0.854	o	|	|	|	|	1.14
35.917	0.00	0.28	0.852	o	|	|	|	|	1.13
36.000	0.00	0.28	0.851	o	|	|	|	|	1.13
36.083	0.00	0.28	0.849	o	|	|	|	|	1.13
36.167	0.00	0.28	0.847	o	|	|	|	|	1.13
36.250	0.00	0.27	0.845	o	|	|	|	|	1.12
36.333	0.00	0.27	0.843	o	|	|	|	|	1.12
36.417	0.00	0.27	0.841	o	|	|	|	|	1.12
36.500	0.00	0.27	0.839	o	|	|	|	|	1.12
36.583	0.00	0.27	0.837	o	|	|	|	|	1.12
36.667	0.00	0.27	0.836	o	|	|	|	|	1.11
36.750	0.00	0.27	0.834	o	|	|	|	|	1.11
36.833	0.00	0.27	0.832	o	|	|	|	|	1.11
36.917	0.00	0.27	0.830	o	|	|	|	|	1.11
37.000	0.00	0.26	0.828	o	|	|	|	|	1.10
37.083	0.00	0.26	0.826	o	|	|	|	|	1.10
37.167	0.00	0.26	0.825	o	|	|	|	|	1.10
37.250	0.00	0.26	0.823	o	|	|	|	|	1.10
37.333	0.00	0.26	0.821	o	|	|	|	|	1.10
37.417	0.00	0.26	0.819	o	|	|	|	|	1.09
37.500	0.00	0.26	0.817	o	|	|	|	|	1.09
37.583	0.00	0.26	0.816	o	|	|	|	|	1.09

37.667	0.00	0.26	0.814	o	|	|	|	|	1.09
37.750	0.00	0.26	0.812	o	|	|	|	|	1.08
37.833	0.00	0.26	0.810	o	|	|	|	|	1.08
37.917	0.00	0.25	0.809	o	|	|	|	|	1.08
38.000	0.00	0.25	0.807	o	|	|	|	|	1.08
38.083	0.00	0.25	0.805	o	|	|	|	|	1.08
38.167	0.00	0.25	0.803	o	|	|	|	|	1.07
38.250	0.00	0.25	0.802	o	|	|	|	|	1.07
38.333	0.00	0.25	0.800	o	|	|	|	|	1.07
38.417	0.00	0.25	0.798	o	|	|	|	|	1.07
38.500	0.00	0.25	0.796	o	|	|	|	|	1.07
38.583	0.00	0.25	0.795	o	|	|	|	|	1.06
38.667	0.00	0.25	0.793	o	|	|	|	|	1.06
38.750	0.00	0.24	0.791	o	|	|	|	|	1.06
38.833	0.00	0.24	0.790	o	|	|	|	|	1.06
38.917	0.00	0.24	0.788	o	|	|	|	|	1.05
39.000	0.00	0.24	0.786	o	|	|	|	|	1.05
39.083	0.00	0.24	0.785	o	|	|	|	|	1.05
39.167	0.00	0.24	0.783	o	|	|	|	|	1.05
39.250	0.00	0.24	0.781	o	|	|	|	|	1.05
39.333	0.00	0.24	0.780	o	|	|	|	|	1.04
39.417	0.00	0.24	0.778	o	|	|	|	|	1.04
39.500	0.00	0.24	0.776	o	|	|	|	|	1.04
39.583	0.00	0.24	0.775	o	|	|	|	|	1.04
39.667	0.00	0.23	0.773	o	|	|	|	|	1.04
39.750	0.00	0.23	0.772	o	|	|	|	|	1.03
39.833	0.00	0.23	0.770	o	|	|	|	|	1.03
39.917	0.00	0.23	0.768	o	|	|	|	|	1.03
40.000	0.00	0.23	0.767	o	|	|	|	|	1.03
40.083	0.00	0.23	0.765	o	|	|	|	|	1.03
40.167	0.00	0.23	0.764	o	|	|	|	|	1.03
40.250	0.00	0.23	0.762	o	|	|	|	|	1.02
40.333	0.00	0.23	0.760	o	|	|	|	|	1.02
40.417	0.00	0.23	0.759	o	|	|	|	|	1.02
40.500	0.00	0.23	0.757	o	|	|	|	|	1.02
40.583	0.00	0.23	0.756	o	|	|	|	|	1.02
40.667	0.00	0.22	0.754	o	|	|	|	|	1.01
40.750	0.00	0.22	0.753	o	|	|	|	|	1.01
40.833	0.00	0.22	0.751	o	|	|	|	|	1.01
40.917	0.00	0.22	0.750	o	|	|	|	|	1.01
41.000	0.00	0.22	0.748	o	|	|	|	|	1.01
41.083	0.00	0.22	0.747	o	|	|	|	|	1.00
41.167	0.00	0.22	0.745	o	|	|	|	|	1.00
41.250	0.00	0.22	0.744	o	|	|	|	|	1.00
41.333	0.00	0.22	0.742	o	|	|	|	|	1.00
41.417	0.00	0.22	0.741	o	|	|	|	|	1.00
41.500	0.00	0.22	0.739	o	|	|	|	|	0.99
41.583	0.00	0.22	0.738	o	|	|	|	|	0.99
41.667	0.00	0.22	0.736	o	|	|	|	|	0.99
41.750	0.00	0.22	0.735	o	|	|	|	|	0.99
41.833	0.00	0.22	0.733	o	|	|	|	|	0.99
41.917	0.00	0.21	0.732	o	|	|	|	|	0.98
42.000	0.00	0.21	0.730	o	|	|	|	|	0.98
42.083	0.00	0.21	0.729	o	|	|	|	|	0.98
42.167	0.00	0.21	0.727	o	|	|	|	|	0.98
42.250	0.00	0.21	0.726	o	|	|	|	|	0.98
42.333	0.00	0.21	0.724	o	|	|	|	|	0.97
42.417	0.00	0.21	0.723	o	|	|	|	|	0.97
42.500	0.00	0.21	0.721	o	|	|	|	|	0.97
42.583	0.00	0.21	0.720	o	|	|	|	|	0.97
42.667	0.00	0.21	0.718	o	|	|	|	|	0.97
42.750	0.00	0.21	0.717	o	|	|	|	|	0.97
42.833	0.00	0.21	0.716	o	|	|	|	|	0.96
42.917	0.00	0.21	0.714	o	|	|	|	|	0.96
43.000	0.00	0.21	0.713	o	|	|	|	|	0.96
43.083	0.00	0.21	0.711	o	|	|	|	|	0.96
43.167	0.00	0.21	0.710	o	|	|	|	|	0.96
43.250	0.00	0.21	0.708	o	|	|	|	|	0.95
43.333	0.00	0.21	0.707	o	|	|	|	|	0.95
43.417	0.00	0.21	0.706	o	|	|	|	|	0.95
43.500	0.00	0.21	0.704	o	|	|	|	|	0.95
43.583	0.00	0.21	0.703	o	|	|	|	|	0.95
43.667	0.00	0.21	0.701	o	|	|	|	|	0.94
43.750	0.00	0.21	0.700	o	|	|	|	|	0.94
43.833	0.00	0.20	0.698	o	|	|	|	|	0.94
43.917	0.00	0.20	0.697	o	|	|	|	|	0.94
44.000	0.00	0.20	0.696	o	|	|	|	|	0.94
44.083	0.00	0.20	0.694	o	|	|	|	|	0.93
44.167	0.00	0.20	0.693	o	|	|	|	|	0.93
44.250	0.00	0.20	0.691	o	|	|	|	|	0.93
44.333	0.00	0.20	0.690	o	|	|	|	|	0.93
44.417	0.00	0.20	0.689	o	|	|	|	|	0.93
44.500	0.00	0.20	0.687	o	|	|	|	|	0.92
44.583	0.00	0.20	0.686	o	|	|	|	|	0.92
44.667	0.00	0.20	0.684	o	|	|	|	|	0.92
44.750	0.00	0.20	0.683	o	|	|	|	|	0.92

44.833	0.00	0.20	0.682	o	|	|	|	0.92
44.917	0.00	0.20	0.680	o	|	|	|	0.92
45.000	0.00	0.20	0.679	o	|	|	|	0.91
45.083	0.00	0.20	0.678	o	|	|	|	0.91
45.167	0.00	0.20	0.676	o	|	|	|	0.91
45.250	0.00	0.20	0.675	o	|	|	|	0.91
45.333	0.00	0.20	0.673	o	|	|	|	0.91
45.417	0.00	0.20	0.672	o	|	|	|	0.90
45.500	0.00	0.20	0.671	o	|	|	|	0.90
45.583	0.00	0.20	0.669	o	|	|	|	0.90
45.667	0.00	0.20	0.668	o	|	|	|	0.90
45.750	0.00	0.20	0.667	o	|	|	|	0.90
45.833	0.00	0.20	0.665	o	|	|	|	0.90
45.917	0.00	0.19	0.664	o	|	|	|	0.89
46.000	0.00	0.19	0.663	o	|	|	|	0.89
46.083	0.00	0.19	0.661	o	|	|	|	0.89
46.167	0.00	0.19	0.660	o	|	|	|	0.89
46.250	0.00	0.19	0.659	o	|	|	|	0.89
46.333	0.00	0.19	0.657	o	|	|	|	0.88
46.417	0.00	0.19	0.656	o	|	|	|	0.88
46.500	0.00	0.19	0.655	o	|	|	|	0.88
46.583	0.00	0.19	0.653	o	|	|	|	0.88
46.667	0.00	0.19	0.652	o	|	|	|	0.88
46.750	0.00	0.19	0.651	o	|	|	|	0.88
46.833	0.00	0.19	0.649	o	|	|	|	0.87
46.917	0.00	0.19	0.648	o	|	|	|	0.87
47.000	0.00	0.19	0.647	o	|	|	|	0.87
47.083	0.00	0.19	0.645	o	|	|	|	0.87
47.167	0.00	0.19	0.644	o	|	|	|	0.87
47.250	0.00	0.19	0.643	o	|	|	|	0.87
47.333	0.00	0.19	0.642	o	|	|	|	0.86
47.417	0.00	0.19	0.640	o	|	|	|	0.86
47.500	0.00	0.19	0.639	o	|	|	|	0.86
47.583	0.00	0.19	0.638	o	|	|	|	0.86
47.667	0.00	0.19	0.636	o	|	|	|	0.86
47.750	0.00	0.19	0.635	o	|	|	|	0.85
47.833	0.00	0.19	0.634	o	|	|	|	0.85
47.917	0.00	0.19	0.633	o	|	|	|	0.85
48.000	0.00	0.19	0.631	o	|	|	|	0.85
48.083	0.00	0.18	0.630	o	|	|	|	0.85
48.167	0.00	0.18	0.629	o	|	|	|	0.85
48.250	0.00	0.18	0.627	o	|	|	|	0.84
48.333	0.00	0.18	0.626	o	|	|	|	0.84
48.417	0.00	0.18	0.625	o	|	|	|	0.84
48.500	0.00	0.18	0.624	o	|	|	|	0.84
48.583	0.00	0.18	0.622	o	|	|	|	0.84
48.667	0.00	0.18	0.621	o	|	|	|	0.84
48.750	0.00	0.18	0.620	o	|	|	|	0.83
48.833	0.00	0.18	0.619	o	|	|	|	0.83
48.917	0.00	0.18	0.617	o	|	|	|	0.83
49.000	0.00	0.18	0.616	o	|	|	|	0.83
49.083	0.00	0.18	0.615	o	|	|	|	0.83
49.167	0.00	0.18	0.614	o	|	|	|	0.83
49.250	0.00	0.18	0.612	o	|	|	|	0.82
49.333	0.00	0.18	0.611	o	|	|	|	0.82
49.417	0.00	0.18	0.610	o	|	|	|	0.82
49.500	0.00	0.18	0.609	o	|	|	|	0.82
49.583	0.00	0.18	0.608	o	|	|	|	0.82
49.667	0.00	0.18	0.606	o	|	|	|	0.82
49.750	0.00	0.18	0.605	o	|	|	|	0.81
49.833	0.00	0.18	0.604	o	|	|	|	0.81
49.917	0.00	0.18	0.603	o	|	|	|	0.81
50.000	0.00	0.18	0.601	o	|	|	|	0.81
50.083	0.00	0.18	0.600	o	|	|	|	0.81
50.167	0.00	0.18	0.599	o	|	|	|	0.81
50.250	0.00	0.18	0.598	o	|	|	|	0.80
50.333	0.00	0.18	0.597	o	|	|	|	0.80
50.417	0.00	0.17	0.595	o	|	|	|	0.80
50.500	0.00	0.17	0.594	o	|	|	|	0.80
50.583	0.00	0.17	0.593	o	|	|	|	0.80
50.667	0.00	0.17	0.592	o	|	|	|	0.80
50.750	0.00	0.17	0.591	o	|	|	|	0.79
50.833	0.00	0.17	0.589	o	|	|	|	0.79
50.917	0.00	0.17	0.588	o	|	|	|	0.79
51.000	0.00	0.17	0.587	o	|	|	|	0.79
51.083	0.00	0.17	0.586	o	|	|	|	0.79
51.167	0.00	0.17	0.585	o	|	|	|	0.79
51.250	0.00	0.17	0.583	o	|	|	|	0.79
51.333	0.00	0.17	0.582	o	|	|	|	0.78
51.417	0.00	0.17	0.581	o	|	|	|	0.78
51.500	0.00	0.17	0.580	o	|	|	|	0.78
51.583	0.00	0.17	0.579	o	|	|	|	0.78
51.667	0.00	0.17	0.578	o	|	|	|	0.78
51.750	0.00	0.17	0.576	o	|	|	|	0.78
51.833	0.00	0.17	0.575	o	|	|	|	0.77
51.917	0.00	0.17	0.574	o	|	|	|	0.77

52.000	0.00	0.17	0.573	o	|	|	|	|	0.77
52.083	0.00	0.17	0.572	o	|	|	|	|	0.77
52.167	0.00	0.17	0.571	o	|	|	|	|	0.77
52.250	0.00	0.17	0.569	o	|	|	|	|	0.77
52.333	0.00	0.17	0.568	o	|	|	|	|	0.76
52.417	0.00	0.17	0.567	o	|	|	|	|	0.76
52.500	0.00	0.17	0.566	o	|	|	|	|	0.76
52.583	0.00	0.17	0.565	o	|	|	|	|	0.76
52.667	0.00	0.17	0.564	o	|	|	|	|	0.76
52.750	0.00	0.17	0.563	o	|	|	|	|	0.76
52.833	0.00	0.16	0.561	o	|	|	|	|	0.76
52.917	0.00	0.16	0.560	o	|	|	|	|	0.75
53.000	0.00	0.16	0.559	o	|	|	|	|	0.75
53.083	0.00	0.16	0.558	o	|	|	|	|	0.75
53.167	0.00	0.16	0.557	o	|	|	|	|	0.75
53.250	0.00	0.16	0.556	o	|	|	|	|	0.75
53.333	0.00	0.16	0.555	o	|	|	|	|	0.75
53.417	0.00	0.16	0.554	o	|	|	|	|	0.75
53.500	0.00	0.16	0.552	o	|	|	|	|	0.74
53.583	0.00	0.16	0.551	o	|	|	|	|	0.74
53.667	0.00	0.16	0.550	o	|	|	|	|	0.74
53.750	0.00	0.16	0.549	o	|	|	|	|	0.74
53.833	0.00	0.16	0.548	o	|	|	|	|	0.74
53.917	0.00	0.16	0.547	o	|	|	|	|	0.74
54.000	0.00	0.16	0.546	o	|	|	|	|	0.73
54.083	0.00	0.16	0.545	o	|	|	|	|	0.73
54.167	0.00	0.16	0.544	o	|	|	|	|	0.73
54.250	0.00	0.16	0.543	o	|	|	|	|	0.73
54.333	0.00	0.16	0.541	o	|	|	|	|	0.73
54.417	0.00	0.16	0.540	o	|	|	|	|	0.73
54.500	0.00	0.16	0.539	o	|	|	|	|	0.73
54.583	0.00	0.16	0.538	o	|	|	|	|	0.72
54.667	0.00	0.16	0.537	o	|	|	|	|	0.72
54.750	0.00	0.16	0.536	o	|	|	|	|	0.72
54.833	0.00	0.16	0.535	o	|	|	|	|	0.72
54.917	0.00	0.16	0.534	o	|	|	|	|	0.72
55.000	0.00	0.16	0.533	o	|	|	|	|	0.72
55.083	0.00	0.16	0.532	o	|	|	|	|	0.72
55.167	0.00	0.16	0.531	o	|	|	|	|	0.71
55.250	0.00	0.16	0.530	o	|	|	|	|	0.71
55.333	0.00	0.16	0.528	o	|	|	|	|	0.71
55.417	0.00	0.15	0.527	o	|	|	|	|	0.71
55.500	0.00	0.15	0.526	o	|	|	|	|	0.71
55.583	0.00	0.15	0.525	o	|	|	|	|	0.71
55.667	0.00	0.15	0.524	o	|	|	|	|	0.71
55.750	0.00	0.15	0.523	o	|	|	|	|	0.70
55.833	0.00	0.15	0.522	o	|	|	|	|	0.70
55.917	0.00	0.15	0.521	o	|	|	|	|	0.70
56.000	0.00	0.15	0.520	o	|	|	|	|	0.70
56.083	0.00	0.15	0.519	o	|	|	|	|	0.70
56.167	0.00	0.15	0.518	o	|	|	|	|	0.70
56.250	0.00	0.15	0.517	o	|	|	|	|	0.70
56.333	0.00	0.15	0.516	o	|	|	|	|	0.69
56.417	0.00	0.15	0.515	o	|	|	|	|	0.69
56.500	0.00	0.15	0.514	o	|	|	|	|	0.69
56.583	0.00	0.15	0.513	o	|	|	|	|	0.69
56.667	0.00	0.15	0.512	o	|	|	|	|	0.69
56.750	0.00	0.15	0.511	o	|	|	|	|	0.69
56.833	0.00	0.15	0.510	o	|	|	|	|	0.69
56.917	0.00	0.15	0.509	o	|	|	|	|	0.68
57.000	0.00	0.15	0.508	o	|	|	|	|	0.68
57.083	0.00	0.15	0.507	o	|	|	|	|	0.68
57.167	0.00	0.15	0.505	o	|	|	|	|	0.68
57.250	0.00	0.15	0.504	o	|	|	|	|	0.68
57.333	0.00	0.15	0.503	o	|	|	|	|	0.68
57.417	0.00	0.15	0.502	o	|	|	|	|	0.68
57.500	0.00	0.15	0.501	o	|	|	|	|	0.67
57.583	0.00	0.15	0.500	o	|	|	|	|	0.67
57.667	0.00	0.15	0.499	o	|	|	|	|	0.67
57.750	0.00	0.15	0.498	o	|	|	|	|	0.67
57.833	0.00	0.15	0.497	o	|	|	|	|	0.67
57.917	0.00	0.15	0.496	o	|	|	|	|	0.67
58.000	0.00	0.15	0.495	o	|	|	|	|	0.67
58.083	0.00	0.15	0.494	o	|	|	|	|	0.67
58.167	0.00	0.14	0.493	o	|	|	|	|	0.66
58.250	0.00	0.14	0.492	o	|	|	|	|	0.66
58.333	0.00	0.14	0.491	o	|	|	|	|	0.66
58.417	0.00	0.14	0.490	o	|	|	|	|	0.66
58.500	0.00	0.14	0.489	o	|	|	|	|	0.66
58.583	0.00	0.14	0.488	o	|	|	|	|	0.66
58.667	0.00	0.14	0.487	o	|	|	|	|	0.66
58.750	0.00	0.14	0.486	o	|	|	|	|	0.65
58.833	0.00	0.14	0.485	o	|	|	|	|	0.65
58.917	0.00	0.14	0.484	o	|	|	|	|	0.65
59.000	0.00	0.14	0.484	o	|	|	|	|	0.65
59.083	0.00	0.14	0.483	o	|	|	|	|	0.65

59.167	0.00	0.14	0.482	o	|	|	|	|	0.65
59.250	0.00	0.14	0.481	o	|	|	|	|	0.65
59.333	0.00	0.14	0.480	o	|	|	|	|	0.65
59.417	0.00	0.14	0.479	o	|	|	|	|	0.64
59.500	0.00	0.14	0.478	o	|	|	|	|	0.64
59.583	0.00	0.14	0.477	o	|	|	|	|	0.64
59.667	0.00	0.14	0.476	o	|	|	|	|	0.64
59.750	0.00	0.14	0.475	o	|	|	|	|	0.64
59.833	0.00	0.14	0.474	o	|	|	|	|	0.64
59.917	0.00	0.14	0.473	o	|	|	|	|	0.64
60.000	0.00	0.14	0.472	o	|	|	|	|	0.64
60.083	0.00	0.14	0.471	o	|	|	|	|	0.63
60.167	0.00	0.14	0.470	o	|	|	|	|	0.63
60.250	0.00	0.14	0.469	o	|	|	|	|	0.63
60.333	0.00	0.14	0.468	o	|	|	|	|	0.63
60.417	0.00	0.14	0.467	o	|	|	|	|	0.63
60.500	0.00	0.14	0.466	o	|	|	|	|	0.63
60.583	0.00	0.14	0.465	o	|	|	|	|	0.63
60.667	0.00	0.14	0.464	o	|	|	|	|	0.62
60.750	0.00	0.14	0.463	o	|	|	|	|	0.62
60.833	0.00	0.14	0.462	o	|	|	|	|	0.62
60.917	0.00	0.14	0.462	o	|	|	|	|	0.62
61.000	0.00	0.14	0.461	o	|	|	|	|	0.62
61.083	0.00	0.13	0.460	o	|	|	|	|	0.62
61.167	0.00	0.13	0.459	o	|	|	|	|	0.62
61.250	0.00	0.13	0.458	o	|	|	|	|	0.62
61.333	0.00	0.13	0.457	o	|	|	|	|	0.61
61.417	0.00	0.13	0.456	o	|	|	|	|	0.61
61.500	0.00	0.13	0.455	o	|	|	|	|	0.61
61.583	0.00	0.13	0.454	o	|	|	|	|	0.61
61.667	0.00	0.13	0.453	o	|	|	|	|	0.61
61.750	0.00	0.13	0.452	o	|	|	|	|	0.61
61.833	0.00	0.13	0.451	o	|	|	|	|	0.61
61.917	0.00	0.13	0.450	o	|	|	|	|	0.61
62.000	0.00	0.13	0.450	o	|	|	|	|	0.61
62.083	0.00	0.13	0.449	o	|	|	|	|	0.60
62.167	0.00	0.13	0.448	o	|	|	|	|	0.60
62.250	0.00	0.13	0.447	o	|	|	|	|	0.60
62.333	0.00	0.13	0.446	o	|	|	|	|	0.60
62.417	0.00	0.13	0.445	o	|	|	|	|	0.60
62.500	0.00	0.13	0.444	o	|	|	|	|	0.60
62.583	0.00	0.13	0.443	o	|	|	|	|	0.60
62.667	0.00	0.13	0.442	o	|	|	|	|	0.60
62.750	0.00	0.13	0.441	o	|	|	|	|	0.59
62.833	0.00	0.13	0.441	o	|	|	|	|	0.59
62.917	0.00	0.13	0.440	o	|	|	|	|	0.59
63.000	0.00	0.13	0.439	o	|	|	|	|	0.59
63.083	0.00	0.13	0.438	o	|	|	|	|	0.59
63.167	0.00	0.13	0.437	o	|	|	|	|	0.59
63.250	0.00	0.13	0.436	o	|	|	|	|	0.59
63.333	0.00	0.13	0.435	o	|	|	|	|	0.59
63.417	0.00	0.13	0.434	o	|	|	|	|	0.58
63.500	0.00	0.13	0.434	o	|	|	|	|	0.58
63.583	0.00	0.13	0.433	o	|	|	|	|	0.58
63.667	0.00	0.13	0.432	o	|	|	|	|	0.58
63.750	0.00	0.13	0.431	o	|	|	|	|	0.58
63.833	0.00	0.13	0.430	o	|	|	|	|	0.58
63.917	0.00	0.13	0.429	o	|	|	|	|	0.58
64.000	0.00	0.13	0.428	o	|	|	|	|	0.58
64.083	0.00	0.13	0.427	o	|	|	|	|	0.58
64.167	0.00	0.13	0.427	o	|	|	|	|	0.57
64.250	0.00	0.12	0.426	o	|	|	|	|	0.57
64.333	0.00	0.12	0.425	o	|	|	|	|	0.57
64.417	0.00	0.12	0.424	o	|	|	|	|	0.57
64.500	0.00	0.12	0.423	o	|	|	|	|	0.57
64.583	0.00	0.12	0.422	o	|	|	|	|	0.57
64.667	0.00	0.12	0.421	o	|	|	|	|	0.57
64.750	0.00	0.12	0.421	o	|	|	|	|	0.57
64.833	0.00	0.12	0.420	o	|	|	|	|	0.56
64.917	0.00	0.12	0.419	o	|	|	|	|	0.56
65.000	0.00	0.12	0.418	o	|	|	|	|	0.56
65.083	0.00	0.12	0.417	o	|	|	|	|	0.56
65.167	0.00	0.12	0.416	o	|	|	|	|	0.56
65.250	0.00	0.12	0.416	o	|	|	|	|	0.56
65.333	0.00	0.12	0.415	o	|	|	|	|	0.56
65.417	0.00	0.12	0.414	o	|	|	|	|	0.56
65.500	0.00	0.12	0.413	o	|	|	|	|	0.56
65.583	0.00	0.12	0.412	o	|	|	|	|	0.55
65.667	0.00	0.12	0.411	o	|	|	|	|	0.55
65.750	0.00	0.12	0.411	o	|	|	|	|	0.55
65.833	0.00	0.12	0.410	o	|	|	|	|	0.55
65.917	0.00	0.12	0.409	o	|	|	|	|	0.55
66.000	0.00	0.12	0.408	o	|	|	|	|	0.55
66.083	0.00	0.12	0.407	o	|	|	|	|	0.55
66.167	0.00	0.12	0.406	o	|	|	|	|	0.55
66.250	0.00	0.12	0.406	o	|	|	|	|	0.55

66.333	0.00	0.12	0.405	o	|	|	|	0.54
66.417	0.00	0.12	0.404	o	|	|	|	0.54
66.500	0.00	0.12	0.403	o	|	|	|	0.54
66.583	0.00	0.12	0.402	o	|	|	|	0.54
66.667	0.00	0.12	0.401	o	|	|	|	0.54
66.750	0.00	0.12	0.401	o	|	|	|	0.54
66.833	0.00	0.12	0.400	o	|	|	|	0.54
66.917	0.00	0.12	0.399	o	|	|	|	0.54
67.000	0.00	0.12	0.398	o	|	|	|	0.54
67.083	0.00	0.12	0.397	o	|	|	|	0.53
67.167	0.00	0.12	0.397	o	|	|	|	0.53
67.250	0.00	0.12	0.396	o	|	|	|	0.53
67.333	0.00	0.12	0.395	o	|	|	|	0.53
67.417	0.00	0.12	0.394	o	|	|	|	0.53
67.500	0.00	0.12	0.393	o	|	|	|	0.53
67.583	0.00	0.12	0.393	o	|	|	|	0.53
67.667	0.00	0.11	0.392	o	|	|	|	0.53
67.750	0.00	0.11	0.391	o	|	|	|	0.53
67.833	0.00	0.11	0.390	o	|	|	|	0.53
67.917	0.00	0.11	0.389	o	|	|	|	0.52
68.000	0.00	0.11	0.389	o	|	|	|	0.52
68.083	0.00	0.11	0.388	o	|	|	|	0.52
68.167	0.00	0.11	0.387	o	|	|	|	0.52
68.250	0.00	0.11	0.386	o	|	|	|	0.52
68.333	0.00	0.11	0.386	o	|	|	|	0.52
68.417	0.00	0.11	0.385	o	|	|	|	0.52
68.500	0.00	0.11	0.384	o	|	|	|	0.52
68.583	0.00	0.11	0.383	o	|	|	|	0.52
68.667	0.00	0.11	0.382	o	|	|	|	0.51
68.750	0.00	0.11	0.382	o	|	|	|	0.51
68.833	0.00	0.11	0.381	o	|	|	|	0.51
68.917	0.00	0.11	0.380	o	|	|	|	0.51
69.000	0.00	0.11	0.379	o	|	|	|	0.51
69.083	0.00	0.11	0.379	o	|	|	|	0.51
69.167	0.00	0.11	0.378	o	|	|	|	0.51
69.250	0.00	0.11	0.377	o	|	|	|	0.51
69.333	0.00	0.11	0.376	o	|	|	|	0.51
69.417	0.00	0.11	0.376	o	|	|	|	0.51
69.500	0.00	0.11	0.375	o	|	|	|	0.50
69.583	0.00	0.11	0.374	o	|	|	|	0.50
69.667	0.00	0.11	0.373	o	|	|	|	0.50
69.750	0.00	0.11	0.373	o	|	|	|	0.50
69.833	0.00	0.11	0.372	o	|	|	|	0.50
69.917	0.00	0.11	0.371	o	|	|	|	0.50
70.000	0.00	0.11	0.370	o	|	|	|	0.50
70.083	0.00	0.11	0.370	o	|	|	|	0.50
70.167	0.00	0.11	0.369	o	|	|	|	0.50
70.250	0.00	0.11	0.368	o	|	|	|	0.50
70.333	0.00	0.11	0.367	o	|	|	|	0.49
70.417	0.00	0.11	0.367	o	|	|	|	0.49
70.500	0.00	0.11	0.366	o	|	|	|	0.49
70.583	0.00	0.11	0.365	o	|	|	|	0.49
70.667	0.00	0.11	0.364	o	|	|	|	0.49
70.750	0.00	0.11	0.364	o	|	|	|	0.49
70.833	0.00	0.11	0.363	o	|	|	|	0.49
70.917	0.00	0.11	0.362	o	|	|	|	0.49
71.000	0.00	0.11	0.361	o	|	|	|	0.49
71.083	0.00	0.11	0.361	o	|	|	|	0.49
71.167	0.00	0.11	0.360	o	|	|	|	0.48
71.250	0.00	0.11	0.359	o	|	|	|	0.48
71.333	0.00	0.11	0.359	o	|	|	|	0.48
71.417	0.00	0.10	0.358	o	|	|	|	0.48
71.500	0.00	0.10	0.357	o	|	|	|	0.48
71.583	0.00	0.10	0.356	o	|	|	|	0.48
71.667	0.00	0.10	0.356	o	|	|	|	0.48
71.750	0.00	0.10	0.355	o	|	|	|	0.48
71.833	0.00	0.10	0.354	o	|	|	|	0.48
71.917	0.00	0.10	0.353	o	|	|	|	0.48
72.000	0.00	0.10	0.353	o	|	|	|	0.47
72.083	0.00	0.10	0.352	o	|	|	|	0.47
72.167	0.00	0.10	0.351	o	|	|	|	0.47
72.250	0.00	0.10	0.351	o	|	|	|	0.47
72.333	0.00	0.10	0.350	o	|	|	|	0.47
72.417	0.00	0.10	0.349	o	|	|	|	0.47
72.500	0.00	0.10	0.349	o	|	|	|	0.47
72.583	0.00	0.10	0.348	o	|	|	|	0.47
72.667	0.00	0.10	0.347	o	|	|	|	0.47
72.750	0.00	0.10	0.346	o	|	|	|	0.47
72.833	0.00	0.10	0.346	o	|	|	|	0.47
72.917	0.00	0.10	0.345	o	|	|	|	0.46
73.000	0.00	0.10	0.344	o	|	|	|	0.46
73.083	0.00	0.10	0.344	o	|	|	|	0.46
73.167	0.00	0.10	0.343	o	|	|	|	0.46
73.250	0.00	0.10	0.342	o	|	|	|	0.46
73.333	0.00	0.10	0.342	o	|	|	|	0.46
73.417	0.00	0.10	0.341	o	|	|	|	0.46

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73.500    0.00    0.10      0.340  o       |       |       |       |     0.46

       Remaining water in basin =    0.34 (Ac.Ft)


       ****************************HYDROGRAPH DATA****************************
                     Number of intervals =   882
                     Time interval =    5.0 (Min.)
                     Maximum/Peak flow rate =       40.883 (CFS)
                     Total volume =       5.491 (Ac.Ft)
              Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
       ***********************************************************************

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FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
Study date: 05/09/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro110024100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 293
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 16.840 (CFS)
Total volume = 8.505 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 293
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.743	0.218	0.742	0.744
2.000	1.561	0.668	1.559	1.563
3.000	2.456	1.518	2.451	2.461
3.500	2.931	58.349	2.730	3.132
4.000	3.425	162.007	2.867	3.983

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	4.2	8.42	12.63	16.84	Depth (Ft.)
0.083	0.17	0.00	0.001	O	|	|	|	|	0.00
0.167	0.43	0.00	0.003	O	|	|	|	|	0.00
0.250	0.49	0.00	0.006	O	|	|	|	|	0.01
0.333	0.61	0.00	0.010	OI	|	|	|	|	0.01
0.417	0.75	0.00	0.014	OI	|	|	|	|	0.02
0.500	0.78	0.01	0.019	OI	|	|	|	|	0.03
0.583	0.80	0.01	0.025	OI	|	|	|	|	0.03
0.667	0.80	0.01	0.030	OI	|	|	|	|	0.04
0.750	0.81	0.01	0.036	OI	|	|	|	|	0.05
0.833	0.90	0.01	0.042	OI	|	|	|	|	0.06
0.917	1.02	0.01	0.048	OI	|	|	|	|	0.06
1.000	1.05	0.02	0.055	O I	|	|	|	|	0.07
1.083	0.98	0.02	0.062	OI	|	|	|	|	0.08
1.167	0.86	0.02	0.068	OI	|	|	|	|	0.09
1.250	0.83	0.02	0.074	OI	|	|	|	|	0.10
1.333	0.82	0.02	0.080	OI	|	|	|	|	0.11
1.417	0.81	0.02	0.085	OI	|	|	|	|	0.11
1.500	0.81	0.03	0.090	OI	|	|	|	|	0.12
1.583	0.81	0.03	0.096	OI	|	|	|	|	0.13
1.667	0.81	0.03	0.101	OI	|	|	|	|	0.14
1.750	0.81	0.03	0.106	OI	|	|	|	|	0.14

1.833	0.90	0.03	0.112	oI	|	|	|	|	0.15
1.917	1.02	0.03	0.119	oI	|	|	|	|	0.16
2.000	1.05	0.04	0.125	o I	|	|	|	|	0.17
2.083	1.07	0.04	0.132	o I	|	|	|	|	0.18
2.167	1.07	0.04	0.140	o I	|	|	|	|	0.19
2.250	1.08	0.04	0.147	o I	|	|	|	|	0.20
2.333	1.08	0.05	0.154	o I	|	|	|	|	0.21
2.417	1.08	0.05	0.161	o I	|	|	|	|	0.22
2.500	1.08	0.05	0.168	o I	|	|	|	|	0.23
2.583	1.17	0.05	0.175	o I	|	|	|	|	0.24
2.667	1.29	0.05	0.184	o I	|	|	|	|	0.25
2.750	1.32	0.06	0.192	o I	|	|	|	|	0.26
2.833	1.34	0.06	0.201	o I	|	|	|	|	0.27
2.917	1.34	0.06	0.210	o I	|	|	|	|	0.28
3.000	1.35	0.06	0.219	o I	|	|	|	|	0.29
3.083	1.35	0.07	0.227	o I	|	|	|	|	0.31
3.167	1.35	0.07	0.236	o I	|	|	|	|	0.32
3.250	1.35	0.07	0.245	o I	|	|	|	|	0.33
3.333	1.35	0.07	0.254	o I	|	|	|	|	0.34
3.417	1.35	0.08	0.263	o I	|	|	|	|	0.35
3.500	1.35	0.08	0.271	o I	|	|	|	|	0.37
3.583	1.35	0.08	0.280	o I	|	|	|	|	0.38
3.667	1.35	0.08	0.289	o I	|	|	|	|	0.39
3.750	1.35	0.09	0.297	o I	|	|	|	|	0.40
3.833	1.44	0.09	0.306	o I	|	|	|	|	0.41
3.917	1.56	0.09	0.316	o I	|	|	|	|	0.43
4.000	1.59	0.10	0.326	o I	|	|	|	|	0.44
4.083	1.61	0.10	0.337	o I	|	|	|	|	0.45
4.167	1.61	0.10	0.347	o I	|	|	|	|	0.47
4.250	1.62	0.10	0.357	o I	|	|	|	|	0.48
4.333	1.71	0.11	0.368	o I	|	|	|	|	0.50
4.417	1.83	0.11	0.380	o I	|	|	|	|	0.51
4.500	1.86	0.11	0.392	o I	|	|	|	|	0.53
4.583	1.88	0.12	0.404	o I	|	|	|	|	0.54
4.667	1.88	0.12	0.416	o I	|	|	|	|	0.56
4.750	1.89	0.13	0.428	o I	|	|	|	|	0.58
4.833	1.97	0.13	0.440	o I	|	|	|	|	0.59
4.917	2.10	0.13	0.453	o I	|	|	|	|	0.61
5.000	2.13	0.14	0.467	o I	|	|	|	|	0.63
5.083	1.97	0.14	0.480	o I	|	|	|	|	0.65
5.167	1.72	0.14	0.492	o I	|	|	|	|	0.66
5.250	1.67	0.15	0.503	o I	|	|	|	|	0.68
5.333	1.73	0.15	0.513	o I	|	|	|	|	0.69
5.417	1.84	0.15	0.525	o I	|	|	|	|	0.71
5.500	1.86	0.16	0.536	o I	|	|	|	|	0.72
5.583	1.96	0.16	0.548	o I	|	|	|	|	0.74
5.667	2.10	0.16	0.561	o I	|	|	|	|	0.76
5.750	2.13	0.17	0.575	o I	|	|	|	|	0.77
5.833	2.15	0.17	0.588	o I	|	|	|	|	0.79
5.917	2.15	0.18	0.602	o I	|	|	|	|	0.81
6.000	2.16	0.18	0.615	o I	|	|	|	|	0.83
6.083	2.29	0.18	0.629	o I	|	|	|	|	0.85
6.167	2.49	0.19	0.645	o I	|	|	|	|	0.87
6.250	2.55	0.19	0.661	o I	|	|	|	|	0.89
6.333	2.58	0.20	0.677	o I	|	|	|	|	0.91
6.417	2.60	0.20	0.693	o I	|	|	|	|	0.93
6.500	2.61	0.21	0.710	o I	|	|	|	|	0.96
6.583	2.80	0.21	0.727	o I	|	|	|	|	0.98
6.667	3.06	0.22	0.746	o I	|	|	|	|	1.00
6.750	3.13	0.23	0.766	o I	|	|	|	|	1.03
6.833	3.17	0.24	0.786	o I	|	|	|	|	1.05
6.917	3.19	0.25	0.806	o I	|	|	|	|	1.08
7.000	3.21	0.26	0.826	o I	|	|	|	|	1.10
7.083	3.22	0.27	0.846	o I	|	|	|	|	1.13
7.167	3.23	0.29	0.867	o I	|	|	|	|	1.15
7.250	3.24	0.30	0.887	o I	|	|	|	|	1.18
7.333	3.43	0.31	0.908	o I	|	|	|	|	1.20
7.417	3.69	0.32	0.930	o I	|	|	|	|	1.23
7.500	3.76	0.33	0.954	o I	|	|	|	|	1.26
7.583	3.97	0.35	0.978	o I	|	|	|	|	1.29
7.667	4.25	0.36	1.004	o I	|	|	|	|	1.32
7.750	4.33	0.38	1.031	o I	|	|	|	|	1.35
7.833	4.54	0.39	1.059	o I	|	|	|	|	1.39
7.917	4.82	0.41	1.088	o I	|	|	|	|	1.42
8.000	4.90	0.42	1.119	o I	|	|	|	|	1.46
8.083	5.28	0.44	1.151	o I	|	|	|	|	1.50
8.167	5.82	0.46	1.186	o I	|	|	|	|	1.54
8.250	5.96	0.48	1.223	o I	|	|	|	|	1.59
8.333	6.02	0.50	1.261	o I	|	|	|	|	1.63
8.417	6.06	0.52	1.299	o I	|	|	|	|	1.68
8.500	6.08	0.54	1.337	|o I	|	|	|	|	1.73
8.583	6.27	0.57	1.376	|o I	|	|	|	|	1.77
8.667	6.53	0.59	1.416	|o I	|	|	|	|	1.82
8.750	6.60	0.61	1.457	|o I	|	|	|	|	1.87
8.833	6.81	0.63	1.499	|o I	|	|	|	|	1.92
8.917	7.09	0.66	1.543	|o I	|	|	|	|	1.98

9.000	7.17	0.69	1.587	O	I			2.03
9.083	7.55	0.74	1.633	O	I			2.08
9.167	8.09	0.78	1.681	O	I			2.13
9.250	8.23	0.83	1.732	O	I			2.19
9.333	8.46	0.88	1.784	O	I			2.25
9.417	8.75	0.93	1.837	O	I			2.31
9.500	8.84	0.98	1.891	O	I			2.37
9.583	9.05	1.03	1.945	O	I			2.43
9.667	9.33	1.09	2.001	O	I			2.49
9.750	9.41	1.14	2.058	O	I			2.56
9.833	9.62	1.19	2.116	O	I			2.62
9.917	9.90	1.25	2.174	O	I			2.69
10.000	9.97	1.31	2.234	O	I			2.75
10.083	8.79	1.36	2.289	O	I			2.81
10.167	7.03	1.40	2.334	O	I			2.86
10.250	6.61	1.44	2.372	O	I			2.91
10.333	6.43	1.47	2.406	O	I			2.94
10.417	6.35	1.50	2.440	O	I			2.98
10.500	6.30	2.99	2.468	O	I			3.01
10.583	7.18	5.18	2.487	O	I			3.03
10.667	8.46	6.72	2.500	O	I			3.05
10.750	8.78	7.83	2.509	O	I			3.06
10.833	8.92	8.43	2.514	O				3.06
10.917	9.00	8.74	2.516	OI				3.06
11.000	9.05	8.91	2.518	OI				3.06
11.083	8.88	8.94	2.518	O				3.07
11.167	8.64	8.83	2.517	O				3.06
11.250	8.58	8.70	2.516	O				3.06
11.333	8.56	8.63	2.515	O				3.06
11.417	8.56	8.59	2.515	O				3.06
11.500	8.56	8.57	2.515	O				3.06
11.583	8.22	8.47	2.514	IO				3.06
11.667	7.72	8.17	2.512	IO				3.06
11.750	7.60	7.87	2.509	O				3.06
11.833	7.73	7.75	2.508	O				3.05
11.917	7.97	7.81	2.509	OI				3.06
12.000	8.02	7.92	2.509	O				3.06
12.083	9.28	8.35	2.513	O	I			3.06
12.167	11.08	9.42	2.522	O	I			3.07
12.250	11.53	10.52	2.531	O	I			3.08
12.333	11.90	11.22	2.537	OI				3.09
12.417	12.26	11.72	2.541	OI				3.09
12.500	12.38	12.07	2.544	OI				3.09
12.583	12.77	12.37	2.547	OI				3.10
12.667	13.30	12.76	2.550	OI				3.10
12.750	13.44	13.11	2.553	OI				3.10
12.833	13.67	13.37	2.555	O				3.10
12.917	13.96	13.63	2.557	OI				3.11
13.000	14.05	13.85	2.559	O				3.11
13.083	14.96	14.23	2.562	OI				3.11
13.167	16.25	15.03	2.569	O	I			3.12
13.250	16.57	15.84	2.576	OI				3.13
13.333	16.72	16.31	2.580	OI				3.13
13.417	16.79	16.57	2.582	O				3.13
13.500	16.84	16.71	2.583	O				3.13
13.583	14.93	16.23	2.579	I	O			3.13
13.667	12.13	14.65	2.566	I	O			3.12
13.750	11.46	12.99	2.552	I	O			3.10
13.833	11.18	12.01	2.544	IO				3.09
13.917	11.03	11.48	2.539	IO				3.09
14.000	10.95	11.20	2.537	IO				3.09
14.083	11.66	11.26	2.537	OI				3.09
14.167	12.69	11.79	2.542	O	I			3.09
14.250	12.94	12.39	2.547	OI				3.10
14.333	12.88	12.69	2.549	O				3.10
14.417	12.69	12.74	2.550	O				3.10
14.500	12.66	12.70	2.549	O				3.10
14.583	12.64	12.67	2.549	O				3.10
14.667	12.64	12.65	2.549	O				3.10
14.750	12.64	12.64	2.549	O				3.10
14.833	12.47	12.59	2.549	O				3.10
14.917	12.22	12.45	2.547	O				3.10
15.000	12.17	12.30	2.546	O				3.09
15.083	11.97	12.17	2.545	IO				3.09
15.167	11.71	11.98	2.543	O				3.09
15.250	11.65	11.80	2.542	O				3.09
15.333	11.45	11.66	2.541	IO				3.09
15.417	11.19	11.46	2.539	O				3.09
15.500	11.13	11.29	2.538	O				3.09
15.583	10.41	10.99	2.535	IO				3.08
15.667	9.38	10.35	2.530	I	O			3.08
15.750	9.14	9.72	2.525	IO				3.07
15.833	9.04	9.35	2.521	O				3.07
15.917	8.99	9.15	2.520	O				3.07
16.000	8.96	9.05	2.519	O				3.07
16.083	6.41	8.26	2.512	I	O			3.06

16.167	2.68	6.09	2.494	I	O			3.04
16.250	1.79	3.84	2.475	I O				3.02
16.333	1.39	2.53	2.464	I O				3.01
16.417	1.19	1.81	2.458	IO				3.00
16.500	1.08	1.52	2.455	O				3.00
16.583	0.99	1.51	2.451	IO				2.99
16.667	0.86	1.51	2.447	IO				2.99
16.750	0.83	1.51	2.443	IO				2.99
16.833	0.82	1.50	2.438	IO				2.98
16.917	0.81	1.50	2.434	IO				2.97
17.000	0.81	1.49	2.429	IO				2.97
17.083	1.03	1.49	2.425	IO				2.97
17.167	1.36	1.49	2.423	O				2.96
17.250	1.45	1.49	2.422	O				2.96
17.333	1.49	1.49	2.422	O				2.96
17.417	1.51	1.49	2.422	O				2.96
17.500	1.53	1.49	2.423	O				2.96
17.583	1.53	1.49	2.423	O				2.96
17.667	1.54	1.49	2.423	O				2.96
17.750	1.54	1.49	2.424	O				2.96
17.833	1.40	1.49	2.423	O				2.96
17.917	1.17	1.49	2.422	O				2.96
18.000	1.12	1.48	2.420	O				2.96
18.083	1.10	1.48	2.417	O				2.96
18.167	1.09	1.48	2.415	O				2.95
18.250	1.08	1.48	2.412	O				2.95
18.333	1.08	1.47	2.409	O				2.95
18.417	1.08	1.47	2.406	O				2.94
18.500	1.08	1.47	2.404	O				2.94
18.583	0.99	1.47	2.401	IO				2.94
18.667	0.86	1.46	2.397	IO				2.93
18.750	0.83	1.46	2.393	IO				2.93
18.833	0.73	1.45	2.388	IO				2.92
18.917	0.60	1.45	2.383	IO				2.92
19.000	0.56	1.44	2.377	IO				2.91
19.083	0.64	1.44	2.371	IO				2.91
19.167	0.76	1.43	2.366	IO				2.90
19.250	0.78	1.43	2.361	IO				2.89
19.333	0.90	1.42	2.357	IO				2.89
19.417	1.05	1.42	2.354	IO				2.89
19.500	1.09	1.42	2.352	O				2.88
19.583	1.01	1.42	2.349	IO				2.88
19.667	0.87	1.41	2.346	IO				2.88
19.750	0.84	1.41	2.342	IO				2.87
19.833	0.73	1.41	2.338	IO				2.87
19.917	0.60	1.40	2.333	IO				2.86
20.000	0.56	1.40	2.327	IO				2.86
20.083	0.64	1.39	2.322	IO				2.85
20.167	0.76	1.39	2.317	IO				2.84
20.250	0.78	1.38	2.313	IO				2.84
20.333	0.80	1.38	2.309	IO				2.84
20.417	0.80	1.37	2.305	IO				2.83
20.500	0.81	1.37	2.301	IO				2.83
20.583	0.81	1.37	2.297	IO				2.82
20.667	0.81	1.36	2.293	IO				2.82
20.750	0.81	1.36	2.289	IO				2.81
20.833	0.72	1.36	2.285	IO				2.81
20.917	0.59	1.35	2.280	IO				2.80
21.000	0.56	1.35	2.275	IO				2.80
21.083	0.64	1.34	2.270	IO				2.79
21.167	0.76	1.34	2.266	IO				2.79
21.250	0.78	1.33	2.262	IO				2.78
21.333	0.71	1.33	2.258	IO				2.78
21.417	0.59	1.33	2.253	IO				2.77
21.500	0.56	1.32	2.248	IO				2.77
21.583	0.64	1.32	2.243	IO				2.76
21.667	0.76	1.31	2.239	IO				2.76
21.750	0.78	1.31	2.235	IO				2.75
21.833	0.71	1.30	2.231	IO				2.75
21.917	0.59	1.30	2.227	IO				2.74
22.000	0.56	1.30	2.222	IO				2.74
22.083	0.64	1.29	2.217	IO				2.73
22.167	0.76	1.29	2.213	IO				2.73
22.250	0.78	1.28	2.209	IO				2.72
22.333	0.71	1.28	2.206	IO				2.72
22.417	0.59	1.28	2.201	IO				2.72
22.500	0.56	1.27	2.197	IO				2.71
22.583	0.55	1.27	2.192	IO				2.70
22.667	0.54	1.26	2.187	IO				2.70
22.750	0.54	1.26	2.182	IO				2.69
22.833	0.54	1.25	2.177	IO				2.69
22.917	0.54	1.25	2.172	IO				2.68
23.000	0.54	1.24	2.167	IO				2.68
23.083	0.54	1.24	2.162	IO				2.67
23.167	0.54	1.23	2.157	IO				2.67
23.250	0.54	1.23	2.153	IO				2.66

23.333	0.54	1.23	2.148	|IO	|	|	|	2.66
23.417	0.54	1.22	2.143	|IO	|	|	|	2.65
23.500	0.54	1.22	2.138	|IO	|	|	|	2.65
23.583	0.54	1.21	2.134	|IO	|	|	|	2.64
23.667	0.54	1.21	2.129	|IO	|	|	|	2.63
23.750	0.54	1.20	2.125	|IO	|	|	|	2.63
23.833	0.54	1.20	2.120	|IO	|	|	|	2.62
23.917	0.54	1.19	2.116	|IO	|	|	|	2.62
24.000	0.54	1.19	2.111	|IO	|	|	|	2.61
24.083	0.36	1.19	2.106	I O	|	|	|	2.61
24.167	0.11	1.18	2.099	I O	|	|	|	2.60
24.250	0.05	1.17	2.092	I O	|	|	|	2.59
24.333	0.02	1.16	2.084	I O	|	|	|	2.58
24.417	0.01	1.16	2.076	I O	|	|	|	2.58
24.500	0.00	1.15	2.068	I O	|	|	|	2.57
24.583	0.00	1.14	2.060	I O	|	|	|	2.56
24.667	0.00	1.13	2.053	I O	|	|	|	2.55
24.750	0.00	1.13	2.045	I O	|	|	|	2.54
24.833	0.00	1.12	2.037	I O	|	|	|	2.53
24.917	0.00	1.11	2.029	I O	|	|	|	2.52
25.000	0.00	1.11	2.022	I O	|	|	|	2.51
25.083	0.00	1.10	2.014	I O	|	|	|	2.51
25.167	0.00	1.09	2.007	I O	|	|	|	2.50
25.250	0.00	1.08	1.999	I O	|	|	|	2.49
25.333	0.00	1.08	1.992	I O	|	|	|	2.48
25.417	0.00	1.07	1.984	I O	|	|	|	2.47
25.500	0.00	1.06	1.977	I O	|	|	|	2.46
25.583	0.00	1.06	1.970	I O	|	|	|	2.46
25.667	0.00	1.05	1.962	IO	|	|	|	2.45
25.750	0.00	1.04	1.955	IO	|	|	|	2.44
25.833	0.00	1.04	1.948	IO	|	|	|	2.43
25.917	0.00	1.03	1.941	IO	|	|	|	2.42
26.000	0.00	1.02	1.934	IO	|	|	|	2.42
26.083	0.00	1.02	1.927	IO	|	|	|	2.41
26.167	0.00	1.01	1.920	IO	|	|	|	2.40
26.250	0.00	1.00	1.913	IO	|	|	|	2.39
26.333	0.00	1.00	1.906	IO	|	|	|	2.39
26.417	0.00	0.99	1.899	IO	|	|	|	2.38
26.500	0.00	0.98	1.892	IO	|	|	|	2.37
26.583	0.00	0.98	1.886	IO	|	|	|	2.36
26.667	0.00	0.97	1.879	IO	|	|	|	2.36
26.750	0.00	0.96	1.872	IO	|	|	|	2.35
26.833	0.00	0.96	1.866	IO	|	|	|	2.34
26.917	0.00	0.95	1.859	IO	|	|	|	2.33
27.000	0.00	0.94	1.853	IO	|	|	|	2.33
27.083	0.00	0.94	1.846	IO	|	|	|	2.32
27.167	0.00	0.93	1.840	IO	|	|	|	2.31
27.250	0.00	0.93	1.833	IO	|	|	|	2.30
27.333	0.00	0.92	1.827	IO	|	|	|	2.30
27.417	0.00	0.91	1.821	IO	|	|	|	2.29
27.500	0.00	0.91	1.814	IO	|	|	|	2.28
27.583	0.00	0.90	1.808	IO	|	|	|	2.28
27.667	0.00	0.90	1.802	IO	|	|	|	2.27
27.750	0.00	0.89	1.796	IO	|	|	|	2.26
27.833	0.00	0.89	1.790	IO	|	|	|	2.26
27.917	0.00	0.88	1.784	IO	|	|	|	2.25
28.000	0.00	0.87	1.777	IO	|	|	|	2.24
28.083	0.00	0.87	1.771	IO	|	|	|	2.24
28.167	0.00	0.86	1.766	IO	|	|	|	2.23
28.250	0.00	0.86	1.760	IO	|	|	|	2.22
28.333	0.00	0.85	1.754	IO	|	|	|	2.22
28.417	0.00	0.85	1.748	IO	|	|	|	2.21
28.500	0.00	0.84	1.742	IO	|	|	|	2.20
28.583	0.00	0.83	1.736	IO	|	|	|	2.20
28.667	0.00	0.83	1.731	IO	|	|	|	2.19
28.750	0.00	0.82	1.725	IO	|	|	|	2.18
28.833	0.00	0.82	1.719	IO	|	|	|	2.18
28.917	0.00	0.81	1.714	IO	|	|	|	2.17
29.000	0.00	0.81	1.708	IO	|	|	|	2.16
29.083	0.00	0.80	1.702	IO	|	|	|	2.16
29.167	0.00	0.80	1.697	IO	|	|	|	2.15
29.250	0.00	0.79	1.692	IO	|	|	|	2.15
29.333	0.00	0.79	1.686	IO	|	|	|	2.14
29.417	0.00	0.78	1.681	IO	|	|	|	2.13
29.500	0.00	0.78	1.675	IO	|	|	|	2.13
29.583	0.00	0.77	1.670	IO	|	|	|	2.12
29.667	0.00	0.77	1.665	IO	|	|	|	2.12
29.750	0.00	0.76	1.659	IO	|	|	|	2.11
29.833	0.00	0.76	1.654	IO	|	|	|	2.10
29.917	0.00	0.75	1.649	IO	|	|	|	2.10
30.000	0.00	0.75	1.644	IO	|	|	|	2.09
30.083	0.00	0.74	1.639	IO	|	|	|	2.09
30.167	0.00	0.74	1.634	IO	|	|	|	2.08
30.250	0.00	0.73	1.629	IO	|	|	|	2.08
30.333	0.00	0.73	1.624	IO	|	|	|	2.07
30.417	0.00	0.72	1.619	IO	|	|	|	2.06

30.500	0.00	0.72	1.614	IO				2.06
30.583	0.00	0.71	1.609	IO				2.05
30.667	0.00	0.71	1.604	IO				2.05
30.750	0.00	0.70	1.599	IO				2.04
30.833	0.00	0.70	1.594	IO				2.04
30.917	0.00	0.69	1.589	IO				2.03
31.000	0.00	0.69	1.584	IO				2.03
31.083	0.00	0.69	1.580	IO				2.02
31.167	0.00	0.68	1.575	IO				2.02
31.250	0.00	0.68	1.570	IO				2.01
31.333	0.00	0.67	1.566	IO				2.01
31.417	0.00	0.67	1.561	IO				2.00
31.500	0.00	0.67	1.557	IO				1.99
31.583	0.00	0.66	1.552	IO				1.99
31.667	0.00	0.66	1.547	IO				1.98
31.750	0.00	0.66	1.543	IO				1.98
31.833	0.00	0.66	1.538	IO				1.97
31.917	0.00	0.65	1.534	IO				1.97
32.000	0.00	0.65	1.529	IO				1.96
32.083	0.00	0.65	1.525	IO				1.96
32.167	0.00	0.65	1.520	IO				1.95
32.250	0.00	0.64	1.516	IO				1.94
32.333	0.00	0.64	1.512	IO				1.94
32.417	0.00	0.64	1.507	IO				1.93
32.500	0.00	0.64	1.503	IO				1.93
32.583	0.00	0.63	1.498	IO				1.92
32.667	0.00	0.63	1.494	IO				1.92
32.750	0.00	0.63	1.490	IO				1.91
32.833	0.00	0.63	1.485	IO				1.91
32.917	0.00	0.62	1.481	IO				1.90
33.000	0.00	0.62	1.477	IO				1.90
33.083	0.00	0.62	1.472	IO				1.89
33.167	0.00	0.62	1.468	IO				1.89
33.250	0.00	0.61	1.464	IO				1.88
33.333	0.00	0.61	1.460	IO				1.88
33.417	0.00	0.61	1.456	IO				1.87
33.500	0.00	0.61	1.451	IO				1.87
33.583	0.00	0.61	1.447	IO				1.86
33.667	0.00	0.60	1.443	IO				1.86
33.750	0.00	0.60	1.439	IO				1.85
33.833	0.00	0.60	1.435	IO				1.85
33.917	0.00	0.60	1.431	IO				1.84
34.000	0.00	0.59	1.427	IO				1.84
34.083	0.00	0.59	1.422	IO				1.83
34.167	0.00	0.59	1.418	IO				1.83
34.250	0.00	0.59	1.414	IO				1.82
34.333	0.00	0.59	1.410	IO				1.82
34.417	0.00	0.58	1.406	IO				1.81
34.500	0.00	0.58	1.402	IO				1.81
34.583	0.00	0.58	1.398	IO				1.80
34.667	0.00	0.58	1.394	IO				1.80
34.750	0.00	0.57	1.390	IO				1.79
34.833	0.00	0.57	1.386	IO				1.79
34.917	0.00	0.57	1.382	IO				1.78
35.000	0.00	0.57	1.379	IO				1.78
35.083	0.00	0.57	1.375	IO				1.77
35.167	0.00	0.56	1.371	IO				1.77
35.250	0.00	0.56	1.367	IO				1.76
35.333	0.00	0.56	1.363	IO				1.76
35.417	0.00	0.56	1.359	IO				1.75
35.500	0.00	0.55	1.355	IO				1.75
35.583	0.00	0.55	1.352	IO				1.74
35.667	0.00	0.55	1.348	IO				1.74
35.750	0.00	0.55	1.344	IO				1.73
35.833	0.00	0.55	1.340	IO				1.73
35.917	0.00	0.54	1.336	IO				1.73
36.000	0.00	0.54	1.333	IO				1.72
36.083	0.00	0.54	1.329	IO				1.72
36.167	0.00	0.54	1.325	IO				1.71
36.250	0.00	0.54	1.322	IO				1.71
36.333	0.00	0.53	1.318	IO				1.70
36.417	0.00	0.53	1.314	IO				1.70
36.500	0.00	0.53	1.311	IO				1.69
36.583	0.00	0.53	1.307	IO				1.69
36.667	0.00	0.53	1.303	O				1.68
36.750	0.00	0.52	1.300	O				1.68
36.833	0.00	0.52	1.296	O				1.68
36.917	0.00	0.52	1.292	O				1.67
37.000	0.00	0.52	1.289	O				1.67
37.083	0.00	0.52	1.285	O				1.66
37.167	0.00	0.51	1.282	O				1.66
37.250	0.00	0.51	1.278	O				1.65
37.333	0.00	0.51	1.275	O				1.65
37.417	0.00	0.51	1.271	O				1.65
37.500	0.00	0.51	1.268	O				1.64
37.583	0.00	0.50	1.264	O				1.64

37.667	0.00	0.50	1.261	o	|	|	|	|	1.63
37.750	0.00	0.50	1.257	o	|	|	|	|	1.63
37.833	0.00	0.50	1.254	o	|	|	|	|	1.62
37.917	0.00	0.50	1.250	o	|	|	|	|	1.62
38.000	0.00	0.50	1.247	o	|	|	|	|	1.62
38.083	0.00	0.49	1.244	o	|	|	|	|	1.61
38.167	0.00	0.49	1.240	o	|	|	|	|	1.61
38.250	0.00	0.49	1.237	o	|	|	|	|	1.60
38.333	0.00	0.49	1.233	o	|	|	|	|	1.60
38.417	0.00	0.49	1.230	o	|	|	|	|	1.60
38.500	0.00	0.48	1.227	o	|	|	|	|	1.59
38.583	0.00	0.48	1.223	o	|	|	|	|	1.59
38.667	0.00	0.48	1.220	o	|	|	|	|	1.58
38.750	0.00	0.48	1.217	o	|	|	|	|	1.58
38.833	0.00	0.48	1.214	o	|	|	|	|	1.58
38.917	0.00	0.48	1.210	o	|	|	|	|	1.57
39.000	0.00	0.47	1.207	o	|	|	|	|	1.57
39.083	0.00	0.47	1.204	o	|	|	|	|	1.56
39.167	0.00	0.47	1.200	o	|	|	|	|	1.56
39.250	0.00	0.47	1.197	o	|	|	|	|	1.56
39.333	0.00	0.47	1.194	o	|	|	|	|	1.55
39.417	0.00	0.46	1.191	o	|	|	|	|	1.55
39.500	0.00	0.46	1.188	o	|	|	|	|	1.54
39.583	0.00	0.46	1.184	o	|	|	|	|	1.54
39.667	0.00	0.46	1.181	o	|	|	|	|	1.54
39.750	0.00	0.46	1.178	o	|	|	|	|	1.53
39.833	0.00	0.46	1.175	o	|	|	|	|	1.53
39.917	0.00	0.45	1.172	o	|	|	|	|	1.52
40.000	0.00	0.45	1.169	o	|	|	|	|	1.52
40.083	0.00	0.45	1.166	o	|	|	|	|	1.52
40.167	0.00	0.45	1.163	o	|	|	|	|	1.51
40.250	0.00	0.45	1.159	o	|	|	|	|	1.51
40.333	0.00	0.45	1.156	o	|	|	|	|	1.51
40.417	0.00	0.44	1.153	o	|	|	|	|	1.50
40.500	0.00	0.44	1.150	o	|	|	|	|	1.50
40.583	0.00	0.44	1.147	o	|	|	|	|	1.49
40.667	0.00	0.44	1.144	o	|	|	|	|	1.49
40.750	0.00	0.44	1.141	o	|	|	|	|	1.49
40.833	0.00	0.44	1.138	o	|	|	|	|	1.48
40.917	0.00	0.43	1.135	o	|	|	|	|	1.48
41.000	0.00	0.43	1.132	o	|	|	|	|	1.48
41.083	0.00	0.43	1.129	o	|	|	|	|	1.47
41.167	0.00	0.43	1.126	o	|	|	|	|	1.47
41.250	0.00	0.43	1.123	o	|	|	|	|	1.46
41.333	0.00	0.43	1.120	o	|	|	|	|	1.46
41.417	0.00	0.42	1.117	o	|	|	|	|	1.46
41.500	0.00	0.42	1.115	o	|	|	|	|	1.45
41.583	0.00	0.42	1.112	o	|	|	|	|	1.45
41.667	0.00	0.42	1.109	o	|	|	|	|	1.45
41.750	0.00	0.42	1.106	o	|	|	|	|	1.44
41.833	0.00	0.42	1.103	o	|	|	|	|	1.44
41.917	0.00	0.41	1.100	o	|	|	|	|	1.44
42.000	0.00	0.41	1.097	o	|	|	|	|	1.43
42.083	0.00	0.41	1.094	o	|	|	|	|	1.43
42.167	0.00	0.41	1.092	o	|	|	|	|	1.43
42.250	0.00	0.41	1.089	o	|	|	|	|	1.42
42.333	0.00	0.41	1.086	o	|	|	|	|	1.42
42.417	0.00	0.41	1.083	o	|	|	|	|	1.42
42.500	0.00	0.40	1.080	o	|	|	|	|	1.41
42.583	0.00	0.40	1.078	o	|	|	|	|	1.41
42.667	0.00	0.40	1.075	o	|	|	|	|	1.41
42.750	0.00	0.40	1.072	o	|	|	|	|	1.40
42.833	0.00	0.40	1.069	o	|	|	|	|	1.40
42.917	0.00	0.40	1.067	o	|	|	|	|	1.40
43.000	0.00	0.39	1.064	o	|	|	|	|	1.39
43.083	0.00	0.39	1.061	o	|	|	|	|	1.39
43.167	0.00	0.39	1.059	o	|	|	|	|	1.39
43.250	0.00	0.39	1.056	o	|	|	|	|	1.38
43.333	0.00	0.39	1.053	o	|	|	|	|	1.38
43.417	0.00	0.39	1.050	o	|	|	|	|	1.38
43.500	0.00	0.39	1.048	o	|	|	|	|	1.37
43.583	0.00	0.38	1.045	o	|	|	|	|	1.37
43.667	0.00	0.38	1.043	o	|	|	|	|	1.37
43.750	0.00	0.38	1.040	o	|	|	|	|	1.36
43.833	0.00	0.38	1.037	o	|	|	|	|	1.36
43.917	0.00	0.38	1.035	o	|	|	|	|	1.36
44.000	0.00	0.38	1.032	o	|	|	|	|	1.35
44.083	0.00	0.38	1.029	o	|	|	|	|	1.35
44.167	0.00	0.37	1.027	o	|	|	|	|	1.35
44.250	0.00	0.37	1.024	o	|	|	|	|	1.34
44.333	0.00	0.37	1.022	o	|	|	|	|	1.34
44.417	0.00	0.37	1.019	o	|	|	|	|	1.34
44.500	0.00	0.37	1.017	o	|	|	|	|	1.33
44.583	0.00	0.37	1.014	o	|	|	|	|	1.33
44.667	0.00	0.37	1.012	o	|	|	|	|	1.33
44.750	0.00	0.36	1.009	o	|	|	|	|	1.33

44.833	0.00	0.36	1.007	o	|	|	|	|	1.32
44.917	0.00	0.36	1.004	o	|	|	|	|	1.32
45.000	0.00	0.36	1.002	o	|	|	|	|	1.32
45.083	0.00	0.36	0.999	o	|	|	|	|	1.31
45.167	0.00	0.36	0.997	o	|	|	|	|	1.31
45.250	0.00	0.36	0.994	o	|	|	|	|	1.31
45.333	0.00	0.35	0.992	o	|	|	|	|	1.30
45.417	0.00	0.35	0.989	o	|	|	|	|	1.30
45.500	0.00	0.35	0.987	o	|	|	|	|	1.30
45.583	0.00	0.35	0.984	o	|	|	|	|	1.30
45.667	0.00	0.35	0.982	o	|	|	|	|	1.29
45.750	0.00	0.35	0.980	o	|	|	|	|	1.29
45.833	0.00	0.35	0.977	o	|	|	|	|	1.29
45.917	0.00	0.35	0.975	o	|	|	|	|	1.28
46.000	0.00	0.34	0.972	o	|	|	|	|	1.28
46.083	0.00	0.34	0.970	o	|	|	|	|	1.28
46.167	0.00	0.34	0.968	o	|	|	|	|	1.27
46.250	0.00	0.34	0.965	o	|	|	|	|	1.27
46.333	0.00	0.34	0.963	o	|	|	|	|	1.27
46.417	0.00	0.34	0.961	o	|	|	|	|	1.27
46.500	0.00	0.34	0.958	o	|	|	|	|	1.26
46.583	0.00	0.34	0.956	o	|	|	|	|	1.26
46.667	0.00	0.33	0.954	o	|	|	|	|	1.26
46.750	0.00	0.33	0.952	o	|	|	|	|	1.25
46.833	0.00	0.33	0.949	o	|	|	|	|	1.25
46.917	0.00	0.33	0.947	o	|	|	|	|	1.25
47.000	0.00	0.33	0.945	o	|	|	|	|	1.25
47.083	0.00	0.33	0.942	o	|	|	|	|	1.24
47.167	0.00	0.33	0.940	o	|	|	|	|	1.24
47.250	0.00	0.33	0.938	o	|	|	|	|	1.24
47.333	0.00	0.32	0.936	o	|	|	|	|	1.24
47.417	0.00	0.32	0.933	o	|	|	|	|	1.23
47.500	0.00	0.32	0.931	o	|	|	|	|	1.23
47.583	0.00	0.32	0.929	o	|	|	|	|	1.23
47.667	0.00	0.32	0.927	o	|	|	|	|	1.22
47.750	0.00	0.32	0.925	o	|	|	|	|	1.22
47.833	0.00	0.32	0.922	o	|	|	|	|	1.22
47.917	0.00	0.32	0.920	o	|	|	|	|	1.22
48.000	0.00	0.31	0.918	o	|	|	|	|	1.21
48.083	0.00	0.31	0.916	o	|	|	|	|	1.21
48.167	0.00	0.31	0.914	o	|	|	|	|	1.21
48.250	0.00	0.31	0.912	o	|	|	|	|	1.21
48.333	0.00	0.31	0.909	o	|	|	|	|	1.20
48.417	0.00	0.31	0.907	o	|	|	|	|	1.20
48.500	0.00	0.31	0.905	o	|	|	|	|	1.20
48.583	0.00	0.31	0.903	o	|	|	|	|	1.20
48.667	0.00	0.30	0.901	o	|	|	|	|	1.19
48.750	0.00	0.30	0.899	o	|	|	|	|	1.19
48.833	0.00	0.30	0.897	o	|	|	|	|	1.19
48.917	0.00	0.30	0.895	o	|	|	|	|	1.19
49.000	0.00	0.30	0.893	o	|	|	|	|	1.18
49.083	0.00	0.30	0.891	o	|	|	|	|	1.18
49.167	0.00	0.30	0.889	o	|	|	|	|	1.18
49.250	0.00	0.30	0.887	o	|	|	|	|	1.18
49.333	0.00	0.30	0.884	o	|	|	|	|	1.17
49.417	0.00	0.29	0.882	o	|	|	|	|	1.17
49.500	0.00	0.29	0.880	o	|	|	|	|	1.17
49.583	0.00	0.29	0.878	o	|	|	|	|	1.17
49.667	0.00	0.29	0.876	o	|	|	|	|	1.16
49.750	0.00	0.29	0.874	o	|	|	|	|	1.16
49.833	0.00	0.29	0.872	o	|	|	|	|	1.16
49.917	0.00	0.29	0.870	o	|	|	|	|	1.16
50.000	0.00	0.29	0.868	o	|	|	|	|	1.15
50.083	0.00	0.29	0.866	o	|	|	|	|	1.15
50.167	0.00	0.28	0.864	o	|	|	|	|	1.15
50.250	0.00	0.28	0.863	o	|	|	|	|	1.15
50.333	0.00	0.28	0.861	o	|	|	|	|	1.14
50.417	0.00	0.28	0.859	o	|	|	|	|	1.14
50.500	0.00	0.28	0.857	o	|	|	|	|	1.14
50.583	0.00	0.28	0.855	o	|	|	|	|	1.14
50.667	0.00	0.28	0.853	o	|	|	|	|	1.13
50.750	0.00	0.28	0.851	o	|	|	|	|	1.13
50.833	0.00	0.28	0.849	o	|	|	|	|	1.13
50.917	0.00	0.28	0.847	o	|	|	|	|	1.13
51.000	0.00	0.27	0.845	o	|	|	|	|	1.12
51.083	0.00	0.27	0.843	o	|	|	|	|	1.12
51.167	0.00	0.27	0.841	o	|	|	|	|	1.12
51.250	0.00	0.27	0.840	o	|	|	|	|	1.12
51.333	0.00	0.27	0.838	o	|	|	|	|	1.12
51.417	0.00	0.27	0.836	o	|	|	|	|	1.11
51.500	0.00	0.27	0.834	o	|	|	|	|	1.11
51.583	0.00	0.27	0.832	o	|	|	|	|	1.11
51.667	0.00	0.27	0.830	o	|	|	|	|	1.11
51.750	0.00	0.27	0.829	o	|	|	|	|	1.10
51.833	0.00	0.26	0.827	o	|	|	|	|	1.10
51.917	0.00	0.26	0.825	o	|	|	|	|	1.10

52.000	0.00	0.26	0.823	o	|	|	|	|	1.10
52.083	0.00	0.26	0.821	o	|	|	|	|	1.10
52.167	0.00	0.26	0.819	o	|	|	|	|	1.09
52.250	0.00	0.26	0.818	o	|	|	|	|	1.09
52.333	0.00	0.26	0.816	o	|	|	|	|	1.09
52.417	0.00	0.26	0.814	o	|	|	|	|	1.09
52.500	0.00	0.26	0.812	o	|	|	|	|	1.08
52.583	0.00	0.26	0.811	o	|	|	|	|	1.08
52.667	0.00	0.25	0.809	o	|	|	|	|	1.08
52.750	0.00	0.25	0.807	o	|	|	|	|	1.08
52.833	0.00	0.25	0.805	o	|	|	|	|	1.08
52.917	0.00	0.25	0.804	o	|	|	|	|	1.07
53.000	0.00	0.25	0.802	o	|	|	|	|	1.07
53.083	0.00	0.25	0.800	o	|	|	|	|	1.07
53.167	0.00	0.25	0.798	o	|	|	|	|	1.07
53.250	0.00	0.25	0.797	o	|	|	|	|	1.07
53.333	0.00	0.25	0.795	o	|	|	|	|	1.06
53.417	0.00	0.25	0.793	o	|	|	|	|	1.06
53.500	0.00	0.24	0.792	o	|	|	|	|	1.06
53.583	0.00	0.24	0.790	o	|	|	|	|	1.06
53.667	0.00	0.24	0.788	o	|	|	|	|	1.06
53.750	0.00	0.24	0.787	o	|	|	|	|	1.05
53.833	0.00	0.24	0.785	o	|	|	|	|	1.05
53.917	0.00	0.24	0.783	o	|	|	|	|	1.05
54.000	0.00	0.24	0.782	o	|	|	|	|	1.05
54.083	0.00	0.24	0.780	o	|	|	|	|	1.05
54.167	0.00	0.24	0.778	o	|	|	|	|	1.04
54.250	0.00	0.24	0.777	o	|	|	|	|	1.04
54.333	0.00	0.24	0.775	o	|	|	|	|	1.04
54.417	0.00	0.23	0.774	o	|	|	|	|	1.04
54.500	0.00	0.23	0.772	o	|	|	|	|	1.04
54.583	0.00	0.23	0.770	o	|	|	|	|	1.03
54.667	0.00	0.23	0.769	o	|	|	|	|	1.03
54.750	0.00	0.23	0.767	o	|	|	|	|	1.03
54.833	0.00	0.23	0.766	o	|	|	|	|	1.03
54.917	0.00	0.23	0.764	o	|	|	|	|	1.03
55.000	0.00	0.23	0.762	o	|	|	|	|	1.02
55.083	0.00	0.23	0.761	o	|	|	|	|	1.02
55.167	0.00	0.23	0.759	o	|	|	|	|	1.02
55.250	0.00	0.23	0.758	o	|	|	|	|	1.02
55.333	0.00	0.23	0.756	o	|	|	|	|	1.02
55.417	0.00	0.22	0.755	o	|	|	|	|	1.01
55.500	0.00	0.22	0.753	o	|	|	|	|	1.01
55.583	0.00	0.22	0.751	o	|	|	|	|	1.01
55.667	0.00	0.22	0.750	o	|	|	|	|	1.01
55.750	0.00	0.22	0.748	o	|	|	|	|	1.01
55.833	0.00	0.22	0.747	o	|	|	|	|	1.00
55.917	0.00	0.22	0.745	o	|	|	|	|	1.00
56.000	0.00	0.22	0.744	o	|	|	|	|	1.00
56.083	0.00	0.22	0.742	o	|	|	|	|	1.00
56.167	0.00	0.22	0.741	o	|	|	|	|	1.00
56.250	0.00	0.22	0.739	o	|	|	|	|	1.00
56.333	0.00	0.22	0.738	o	|	|	|	|	0.99
56.417	0.00	0.22	0.736	o	|	|	|	|	0.99
56.500	0.00	0.22	0.735	o	|	|	|	|	0.99
56.583	0.00	0.22	0.733	o	|	|	|	|	0.99
56.667	0.00	0.21	0.732	o	|	|	|	|	0.99
56.750	0.00	0.21	0.730	o	|	|	|	|	0.98
56.833	0.00	0.21	0.729	o	|	|	|	|	0.98
56.917	0.00	0.21	0.728	o	|	|	|	|	0.98
57.000	0.00	0.21	0.726	o	|	|	|	|	0.98
57.083	0.00	0.21	0.725	o	|	|	|	|	0.98
57.167	0.00	0.21	0.723	o	|	|	|	|	0.97
57.250	0.00	0.21	0.722	o	|	|	|	|	0.97
57.333	0.00	0.21	0.720	o	|	|	|	|	0.97
57.417	0.00	0.21	0.719	o	|	|	|	|	0.97
57.500	0.00	0.21	0.717	o	|	|	|	|	0.97
57.583	0.00	0.21	0.716	o	|	|	|	|	0.96
57.667	0.00	0.21	0.714	o	|	|	|	|	0.96
57.750	0.00	0.21	0.713	o	|	|	|	|	0.96
57.833	0.00	0.21	0.712	o	|	|	|	|	0.96
57.917	0.00	0.21	0.710	o	|	|	|	|	0.96
58.000	0.00	0.21	0.709	o	|	|	|	|	0.95
58.083	0.00	0.21	0.707	o	|	|	|	|	0.95
58.167	0.00	0.21	0.706	o	|	|	|	|	0.95
58.250	0.00	0.21	0.704	o	|	|	|	|	0.95
58.333	0.00	0.21	0.703	o	|	|	|	|	0.95
58.417	0.00	0.21	0.702	o	|	|	|	|	0.94
58.500	0.00	0.21	0.700	o	|	|	|	|	0.94
58.583	0.00	0.21	0.699	o	|	|	|	|	0.94
58.667	0.00	0.20	0.697	o	|	|	|	|	0.94
58.750	0.00	0.20	0.696	o	|	|	|	|	0.94
58.833	0.00	0.20	0.694	o	|	|	|	|	0.93
58.917	0.00	0.20	0.693	o	|	|	|	|	0.93
59.000	0.00	0.20	0.692	o	|	|	|	|	0.93
59.083	0.00	0.20	0.690	o	|	|	|	|	0.93

59.167	0.00	0.20	0.689	o	|	|	|	0.93
59.250	0.00	0.20	0.688	o	|	|	|	0.93
59.333	0.00	0.20	0.686	o	|	|	|	0.92
59.417	0.00	0.20	0.685	o	|	|	|	0.92
59.500	0.00	0.20	0.683	o	|	|	|	0.92
59.583	0.00	0.20	0.682	o	|	|	|	0.92
59.667	0.00	0.20	0.681	o	|	|	|	0.92
59.750	0.00	0.20	0.679	o	|	|	|	0.91
59.833	0.00	0.20	0.678	o	|	|	|	0.91
59.917	0.00	0.20	0.676	o	|	|	|	0.91
60.000	0.00	0.20	0.675	o	|	|	|	0.91
60.083	0.00	0.20	0.674	o	|	|	|	0.91
60.167	0.00	0.20	0.672	o	|	|	|	0.90
60.250	0.00	0.20	0.671	o	|	|	|	0.90
60.333	0.00	0.20	0.670	o	|	|	|	0.90
60.417	0.00	0.20	0.668	o	|	|	|	0.90
60.500	0.00	0.20	0.667	o	|	|	|	0.90
60.583	0.00	0.20	0.666	o	|	|	|	0.90
60.667	0.00	0.19	0.664	o	|	|	|	0.89
60.750	0.00	0.19	0.663	o	|	|	|	0.89
60.833	0.00	0.19	0.662	o	|	|	|	0.89
60.917	0.00	0.19	0.660	o	|	|	|	0.89
61.000	0.00	0.19	0.659	o	|	|	|	0.89
61.083	0.00	0.19	0.658	o	|	|	|	0.89
61.167	0.00	0.19	0.656	o	|	|	|	0.88
61.250	0.00	0.19	0.655	o	|	|	|	0.88
61.333	0.00	0.19	0.654	o	|	|	|	0.88
61.417	0.00	0.19	0.652	o	|	|	|	0.88
61.500	0.00	0.19	0.651	o	|	|	|	0.88
61.583	0.00	0.19	0.650	o	|	|	|	0.87
61.667	0.00	0.19	0.648	o	|	|	|	0.87
61.750	0.00	0.19	0.647	o	|	|	|	0.87
61.833	0.00	0.19	0.646	o	|	|	|	0.87
61.917	0.00	0.19	0.644	o	|	|	|	0.87
62.000	0.00	0.19	0.643	o	|	|	|	0.87
62.083	0.00	0.19	0.642	o	|	|	|	0.86
62.167	0.00	0.19	0.641	o	|	|	|	0.86
62.250	0.00	0.19	0.639	o	|	|	|	0.86
62.333	0.00	0.19	0.638	o	|	|	|	0.86
62.417	0.00	0.19	0.637	o	|	|	|	0.86
62.500	0.00	0.19	0.635	o	|	|	|	0.86
62.583	0.00	0.19	0.634	o	|	|	|	0.85
62.667	0.00	0.19	0.633	o	|	|	|	0.85
62.750	0.00	0.19	0.632	o	|	|	|	0.85
62.833	0.00	0.18	0.630	o	|	|	|	0.85
62.917	0.00	0.18	0.629	o	|	|	|	0.85
63.000	0.00	0.18	0.628	o	|	|	|	0.84
63.083	0.00	0.18	0.626	o	|	|	|	0.84
63.167	0.00	0.18	0.625	o	|	|	|	0.84
63.250	0.00	0.18	0.624	o	|	|	|	0.84
63.333	0.00	0.18	0.623	o	|	|	|	0.84
63.417	0.00	0.18	0.621	o	|	|	|	0.84
63.500	0.00	0.18	0.620	o	|	|	|	0.83
63.583	0.00	0.18	0.619	o	|	|	|	0.83
63.667	0.00	0.18	0.618	o	|	|	|	0.83
63.750	0.00	0.18	0.616	o	|	|	|	0.83
63.833	0.00	0.18	0.615	o	|	|	|	0.83
63.917	0.00	0.18	0.614	o	|	|	|	0.83
64.000	0.00	0.18	0.613	o	|	|	|	0.82
64.083	0.00	0.18	0.611	o	|	|	|	0.82
64.167	0.00	0.18	0.610	o	|	|	|	0.82
64.250	0.00	0.18	0.609	o	|	|	|	0.82
64.333	0.00	0.18	0.608	o	|	|	|	0.82
64.417	0.00	0.18	0.607	o	|	|	|	0.82
64.500	0.00	0.18	0.605	o	|	|	|	0.81
64.583	0.00	0.18	0.604	o	|	|	|	0.81
64.667	0.00	0.18	0.603	o	|	|	|	0.81
64.750	0.00	0.18	0.602	o	|	|	|	0.81
64.833	0.00	0.18	0.600	o	|	|	|	0.81
64.917	0.00	0.18	0.599	o	|	|	|	0.81
65.000	0.00	0.18	0.598	o	|	|	|	0.80
65.083	0.00	0.18	0.597	o	|	|	|	0.80
65.167	0.00	0.17	0.596	o	|	|	|	0.80
65.250	0.00	0.17	0.594	o	|	|	|	0.80
65.333	0.00	0.17	0.593	o	|	|	|	0.80
65.417	0.00	0.17	0.592	o	|	|	|	0.80
65.500	0.00	0.17	0.591	o	|	|	|	0.80
65.583	0.00	0.17	0.590	o	|	|	|	0.79
65.667	0.00	0.17	0.588	o	|	|	|	0.79
65.750	0.00	0.17	0.587	o	|	|	|	0.79
65.833	0.00	0.17	0.586	o	|	|	|	0.79
65.917	0.00	0.17	0.585	o	|	|	|	0.79
66.000	0.00	0.17	0.584	o	|	|	|	0.79
66.083	0.00	0.17	0.583	o	|	|	|	0.78
66.167	0.00	0.17	0.581	o	|	|	|	0.78
66.250	0.00	0.17	0.580	o	|	|	|	0.78

66.333	0.00	0.17	0.579	o	|	|	|	|	0.78
66.417	0.00	0.17	0.578	o	|	|	|	|	0.78
66.500	0.00	0.17	0.577	o	|	|	|	|	0.78
66.583	0.00	0.17	0.576	o	|	|	|	|	0.77
66.667	0.00	0.17	0.574	o	|	|	|	|	0.77
66.750	0.00	0.17	0.573	o	|	|	|	|	0.77
66.833	0.00	0.17	0.572	o	|	|	|	|	0.77
66.917	0.00	0.17	0.571	o	|	|	|	|	0.77
67.000	0.00	0.17	0.570	o	|	|	|	|	0.77
67.083	0.00	0.17	0.569	o	|	|	|	|	0.77
67.167	0.00	0.17	0.567	o	|	|	|	|	0.76
67.250	0.00	0.17	0.566	o	|	|	|	|	0.76
67.333	0.00	0.17	0.565	o	|	|	|	|	0.76
67.417	0.00	0.17	0.564	o	|	|	|	|	0.76
67.500	0.00	0.17	0.563	o	|	|	|	|	0.76
67.583	0.00	0.16	0.562	o	|	|	|	|	0.76
67.667	0.00	0.16	0.561	o	|	|	|	|	0.75
67.750	0.00	0.16	0.559	o	|	|	|	|	0.75
67.833	0.00	0.16	0.558	o	|	|	|	|	0.75
67.917	0.00	0.16	0.557	o	|	|	|	|	0.75
68.000	0.00	0.16	0.556	o	|	|	|	|	0.75
68.083	0.00	0.16	0.555	o	|	|	|	|	0.75
68.167	0.00	0.16	0.554	o	|	|	|	|	0.75
68.250	0.00	0.16	0.553	o	|	|	|	|	0.74
68.333	0.00	0.16	0.552	o	|	|	|	|	0.74
68.417	0.00	0.16	0.550	o	|	|	|	|	0.74
68.500	0.00	0.16	0.549	o	|	|	|	|	0.74
68.583	0.00	0.16	0.548	o	|	|	|	|	0.74
68.667	0.00	0.16	0.547	o	|	|	|	|	0.74
68.750	0.00	0.16	0.546	o	|	|	|	|	0.73
68.833	0.00	0.16	0.545	o	|	|	|	|	0.73
68.917	0.00	0.16	0.544	o	|	|	|	|	0.73
69.000	0.00	0.16	0.543	o	|	|	|	|	0.73
69.083	0.00	0.16	0.542	o	|	|	|	|	0.73
69.167	0.00	0.16	0.541	o	|	|	|	|	0.73
69.250	0.00	0.16	0.539	o	|	|	|	|	0.73
69.333	0.00	0.16	0.538	o	|	|	|	|	0.72
69.417	0.00	0.16	0.537	o	|	|	|	|	0.72
69.500	0.00	0.16	0.536	o	|	|	|	|	0.72
69.583	0.00	0.16	0.535	o	|	|	|	|	0.72
69.667	0.00	0.16	0.534	o	|	|	|	|	0.72
69.750	0.00	0.16	0.533	o	|	|	|	|	0.72
69.833	0.00	0.16	0.532	o	|	|	|	|	0.72
69.917	0.00	0.16	0.531	o	|	|	|	|	0.71
70.000	0.00	0.16	0.530	o	|	|	|	|	0.71
70.083	0.00	0.16	0.529	o	|	|	|	|	0.71
70.167	0.00	0.15	0.528	o	|	|	|	|	0.71
70.250	0.00	0.15	0.527	o	|	|	|	|	0.71
70.333	0.00	0.15	0.525	o	|	|	|	|	0.71
70.417	0.00	0.15	0.524	o	|	|	|	|	0.71
70.500	0.00	0.15	0.523	o	|	|	|	|	0.70
70.583	0.00	0.15	0.522	o	|	|	|	|	0.70
70.667	0.00	0.15	0.521	o	|	|	|	|	0.70
70.750	0.00	0.15	0.520	o	|	|	|	|	0.70
70.833	0.00	0.15	0.519	o	|	|	|	|	0.70
70.917	0.00	0.15	0.518	o	|	|	|	|	0.70
71.000	0.00	0.15	0.517	o	|	|	|	|	0.70
71.083	0.00	0.15	0.516	o	|	|	|	|	0.69
71.167	0.00	0.15	0.515	o	|	|	|	|	0.69
71.250	0.00	0.15	0.514	o	|	|	|	|	0.69
71.333	0.00	0.15	0.513	o	|	|	|	|	0.69
71.417	0.00	0.15	0.512	o	|	|	|	|	0.69
71.500	0.00	0.15	0.511	o	|	|	|	|	0.69
71.583	0.00	0.15	0.510	o	|	|	|	|	0.69
71.667	0.00	0.15	0.509	o	|	|	|	|	0.68
71.750	0.00	0.15	0.508	o	|	|	|	|	0.68
71.833	0.00	0.15	0.507	o	|	|	|	|	0.68
71.917	0.00	0.15	0.506	o	|	|	|	|	0.68
72.000	0.00	0.15	0.505	o	|	|	|	|	0.68
72.083	0.00	0.15	0.504	o	|	|	|	|	0.68
72.167	0.00	0.15	0.503	o	|	|	|	|	0.68
72.250	0.00	0.15	0.502	o	|	|	|	|	0.68
72.333	0.00	0.15	0.501	o	|	|	|	|	0.67
72.417	0.00	0.15	0.500	o	|	|	|	|	0.67
72.500	0.00	0.15	0.499	o	|	|	|	|	0.67
72.583	0.00	0.15	0.498	o	|	|	|	|	0.67
72.667	0.00	0.15	0.497	o	|	|	|	|	0.67
72.750	0.00	0.15	0.496	o	|	|	|	|	0.67
72.833	0.00	0.15	0.495	o	|	|	|	|	0.67
72.917	0.00	0.14	0.494	o	|	|	|	|	0.66
73.000	0.00	0.14	0.493	o	|	|	|	|	0.66
73.083	0.00	0.14	0.492	o	|	|	|	|	0.66
73.167	0.00	0.14	0.491	o	|	|	|	|	0.66
73.250	0.00	0.14	0.490	o	|	|	|	|	0.66
73.333	0.00	0.14	0.489	o	|	|	|	|	0.66
73.417	0.00	0.14	0.488	o	|	|	|	|	0.66

73.500	0.00	0.14	0.487	o	|	|	|	0.65
73.583	0.00	0.14	0.486	o	|	|	|	0.65
73.667	0.00	0.14	0.485	o	|	|	|	0.65
73.750	0.00	0.14	0.484	o	|	|	|	0.65
73.833	0.00	0.14	0.483	o	|	|	|	0.65
73.917	0.00	0.14	0.482	o	|	|	|	0.65
74.000	0.00	0.14	0.481	o	|	|	|	0.65
74.083	0.00	0.14	0.480	o	|	|	|	0.65
74.167	0.00	0.14	0.479	o	|	|	|	0.64
74.250	0.00	0.14	0.478	o	|	|	|	0.64
74.333	0.00	0.14	0.477	o	|	|	|	0.64
74.417	0.00	0.14	0.476	o	|	|	|	0.64
74.500	0.00	0.14	0.475	o	|	|	|	0.64
74.583	0.00	0.14	0.474	o	|	|	|	0.64
74.667	0.00	0.14	0.473	o	|	|	|	0.64
74.750	0.00	0.14	0.472	o	|	|	|	0.64
74.833	0.00	0.14	0.471	o	|	|	|	0.63
74.917	0.00	0.14	0.470	o	|	|	|	0.63
75.000	0.00	0.14	0.469	o	|	|	|	0.63
75.083	0.00	0.14	0.468	o	|	|	|	0.63
75.167	0.00	0.14	0.467	o	|	|	|	0.63
75.250	0.00	0.14	0.466	o	|	|	|	0.63
75.333	0.00	0.14	0.465	o	|	|	|	0.63
75.417	0.00	0.14	0.465	o	|	|	|	0.63
75.500	0.00	0.14	0.464	o	|	|	|	0.62
75.583	0.00	0.14	0.463	o	|	|	|	0.62
75.667	0.00	0.14	0.462	o	|	|	|	0.62
75.750	0.00	0.14	0.461	o	|	|	|	0.62
75.833	0.00	0.13	0.460	o	|	|	|	0.62
75.917	0.00	0.13	0.459	o	|	|	|	0.62
76.000	0.00	0.13	0.458	o	|	|	|	0.62
76.083	0.00	0.13	0.457	o	|	|	|	0.62
76.167	0.00	0.13	0.456	o	|	|	|	0.61
76.250	0.00	0.13	0.455	o	|	|	|	0.61
76.333	0.00	0.13	0.454	o	|	|	|	0.61
76.417	0.00	0.13	0.453	o	|	|	|	0.61
76.500	0.00	0.13	0.452	o	|	|	|	0.61
76.583	0.00	0.13	0.452	o	|	|	|	0.61
76.667	0.00	0.13	0.451	o	|	|	|	0.61
76.750	0.00	0.13	0.450	o	|	|	|	0.61
76.833	0.00	0.13	0.449	o	|	|	|	0.60
76.917	0.00	0.13	0.448	o	|	|	|	0.60
77.000	0.00	0.13	0.447	o	|	|	|	0.60
77.083	0.00	0.13	0.446	o	|	|	|	0.60
77.167	0.00	0.13	0.445	o	|	|	|	0.60
77.250	0.00	0.13	0.444	o	|	|	|	0.60
77.333	0.00	0.13	0.443	o	|	|	|	0.60
77.417	0.00	0.13	0.443	o	|	|	|	0.60
77.500	0.00	0.13	0.442	o	|	|	|	0.59
77.583	0.00	0.13	0.441	o	|	|	|	0.59
77.667	0.00	0.13	0.440	o	|	|	|	0.59
77.750	0.00	0.13	0.439	o	|	|	|	0.59
77.833	0.00	0.13	0.438	o	|	|	|	0.59
77.917	0.00	0.13	0.437	o	|	|	|	0.59
78.000	0.00	0.13	0.436	o	|	|	|	0.59
78.083	0.00	0.13	0.435	o	|	|	|	0.59
78.167	0.00	0.13	0.435	o	|	|	|	0.58
78.250	0.00	0.13	0.434	o	|	|	|	0.58
78.333	0.00	0.13	0.433	o	|	|	|	0.58
78.417	0.00	0.13	0.432	o	|	|	|	0.58
78.500	0.00	0.13	0.431	o	|	|	|	0.58
78.583	0.00	0.13	0.430	o	|	|	|	0.58
78.667	0.00	0.13	0.429	o	|	|	|	0.58
78.750	0.00	0.13	0.428	o	|	|	|	0.58
78.833	0.00	0.13	0.428	o	|	|	|	0.58
78.917	0.00	0.13	0.427	o	|	|	|	0.57
79.000	0.00	0.12	0.426	o	|	|	|	0.57
79.083	0.00	0.12	0.425	o	|	|	|	0.57
79.167	0.00	0.12	0.424	o	|	|	|	0.57
79.250	0.00	0.12	0.423	o	|	|	|	0.57
79.333	0.00	0.12	0.422	o	|	|	|	0.57
79.417	0.00	0.12	0.422	o	|	|	|	0.57
79.500	0.00	0.12	0.421	o	|	|	|	0.57
79.583	0.00	0.12	0.420	o	|	|	|	0.57
79.667	0.00	0.12	0.419	o	|	|	|	0.56
79.750	0.00	0.12	0.418	o	|	|	|	0.56
79.833	0.00	0.12	0.417	o	|	|	|	0.56
79.917	0.00	0.12	0.417	o	|	|	|	0.56
80.000	0.00	0.12	0.416	o	|	|	|	0.56
80.083	0.00	0.12	0.415	o	|	|	|	0.56
80.167	0.00	0.12	0.414	o	|	|	|	0.56
80.250	0.00	0.12	0.413	o	|	|	|	0.56
80.333	0.00	0.12	0.412	o	|	|	|	0.55
80.417	0.00	0.12	0.411	o	|	|	|	0.55
80.500	0.00	0.12	0.411	o	|	|	|	0.55
80.583	0.00	0.12	0.410	o	|	|	|	0.55

80.667	0.00	0.12	0.409	o	|	|	|	|	0.55
80.750	0.00	0.12	0.408	o	|	|	|	|	0.55
80.833	0.00	0.12	0.407	o	|	|	|	|	0.55
80.917	0.00	0.12	0.407	o	|	|	|	|	0.55
81.000	0.00	0.12	0.406	o	|	|	|	|	0.55
81.083	0.00	0.12	0.405	o	|	|	|	|	0.54
81.167	0.00	0.12	0.404	o	|	|	|	|	0.54
81.250	0.00	0.12	0.403	o	|	|	|	|	0.54
81.333	0.00	0.12	0.402	o	|	|	|	|	0.54
81.417	0.00	0.12	0.402	o	|	|	|	|	0.54
81.500	0.00	0.12	0.401	o	|	|	|	|	0.54
81.583	0.00	0.12	0.400	o	|	|	|	|	0.54
81.667	0.00	0.12	0.399	o	|	|	|	|	0.54
81.750	0.00	0.12	0.398	o	|	|	|	|	0.54
81.833	0.00	0.12	0.398	o	|	|	|	|	0.54
81.917	0.00	0.12	0.397	o	|	|	|	|	0.53
82.000	0.00	0.12	0.396	o	|	|	|	|	0.53
82.083	0.00	0.12	0.395	o	|	|	|	|	0.53
82.167	0.00	0.12	0.394	o	|	|	|	|	0.53
82.250	0.00	0.12	0.394	o	|	|	|	|	0.53
82.333	0.00	0.12	0.393	o	|	|	|	|	0.53
82.417	0.00	0.12	0.392	o	|	|	|	|	0.53
82.500	0.00	0.11	0.391	o	|	|	|	|	0.53
82.583	0.00	0.11	0.390	o	|	|	|	|	0.53
82.667	0.00	0.11	0.390	o	|	|	|	|	0.52
82.750	0.00	0.11	0.389	o	|	|	|	|	0.52
82.833	0.00	0.11	0.388	o	|	|	|	|	0.52
82.917	0.00	0.11	0.387	o	|	|	|	|	0.52
83.000	0.00	0.11	0.387	o	|	|	|	|	0.52
83.083	0.00	0.11	0.386	o	|	|	|	|	0.52
83.167	0.00	0.11	0.385	o	|	|	|	|	0.52
83.250	0.00	0.11	0.384	o	|	|	|	|	0.52
83.333	0.00	0.11	0.383	o	|	|	|	|	0.52
83.417	0.00	0.11	0.383	o	|	|	|	|	0.51
83.500	0.00	0.11	0.382	o	|	|	|	|	0.51
83.583	0.00	0.11	0.381	o	|	|	|	|	0.51
83.667	0.00	0.11	0.380	o	|	|	|	|	0.51
83.750	0.00	0.11	0.380	o	|	|	|	|	0.51
83.833	0.00	0.11	0.379	o	|	|	|	|	0.51
83.917	0.00	0.11	0.378	o	|	|	|	|	0.51
84.000	0.00	0.11	0.377	o	|	|	|	|	0.51
84.083	0.00	0.11	0.376	o	|	|	|	|	0.51
84.167	0.00	0.11	0.376	o	|	|	|	|	0.51
84.250	0.00	0.11	0.375	o	|	|	|	|	0.50
84.333	0.00	0.11	0.374	o	|	|	|	|	0.50
84.417	0.00	0.11	0.373	o	|	|	|	|	0.50
84.500	0.00	0.11	0.373	o	|	|	|	|	0.50
84.583	0.00	0.11	0.372	o	|	|	|	|	0.50
84.667	0.00	0.11	0.371	o	|	|	|	|	0.50
84.750	0.00	0.11	0.370	o	|	|	|	|	0.50
84.833	0.00	0.11	0.370	o	|	|	|	|	0.50
84.917	0.00	0.11	0.369	o	|	|	|	|	0.50
85.000	0.00	0.11	0.368	o	|	|	|	|	0.50
85.083	0.00	0.11	0.367	o	|	|	|	|	0.49
85.167	0.00	0.11	0.367	o	|	|	|	|	0.49
85.250	0.00	0.11	0.366	o	|	|	|	|	0.49
85.333	0.00	0.11	0.365	o	|	|	|	|	0.49
85.417	0.00	0.11	0.365	o	|	|	|	|	0.49
85.500	0.00	0.11	0.364	o	|	|	|	|	0.49
85.583	0.00	0.11	0.363	o	|	|	|	|	0.49
85.667	0.00	0.11	0.362	o	|	|	|	|	0.49
85.750	0.00	0.11	0.362	o	|	|	|	|	0.49
85.833	0.00	0.11	0.361	o	|	|	|	|	0.49
85.917	0.00	0.11	0.360	o	|	|	|	|	0.48
86.000	0.00	0.11	0.359	o	|	|	|	|	0.48
86.083	0.00	0.11	0.359	o	|	|	|	|	0.48
86.167	0.00	0.11	0.358	o	|	|	|	|	0.48
86.250	0.00	0.10	0.357	o	|	|	|	|	0.48
86.333	0.00	0.10	0.357	o	|	|	|	|	0.48
86.417	0.00	0.10	0.356	o	|	|	|	|	0.48
86.500	0.00	0.10	0.355	o	|	|	|	|	0.48
86.583	0.00	0.10	0.354	o	|	|	|	|	0.48
86.667	0.00	0.10	0.354	o	|	|	|	|	0.48
86.750	0.00	0.10	0.353	o	|	|	|	|	0.47
86.833	0.00	0.10	0.352	o	|	|	|	|	0.47
86.917	0.00	0.10	0.351	o	|	|	|	|	0.47
87.000	0.00	0.10	0.351	o	|	|	|	|	0.47
87.083	0.00	0.10	0.350	o	|	|	|	|	0.47
87.167	0.00	0.10	0.349	o	|	|	|	|	0.47
87.250	0.00	0.10	0.349	o	|	|	|	|	0.47
87.333	0.00	0.10	0.348	o	|	|	|	|	0.47
87.417	0.00	0.10	0.347	o	|	|	|	|	0.47
87.500	0.00	0.10	0.347	o	|	|	|	|	0.47
87.583	0.00	0.10	0.346	o	|	|	|	|	0.47
87.667	0.00	0.10	0.345	o	|	|	|	|	0.46
87.750	0.00	0.10	0.344	o	|	|	|	|	0.46

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87.833    0.00    0.10      0.344  o       |       |       |       |     0.46
87.917    0.00    0.10      0.343  o       |       |       |       |     0.46
88.000    0.00    0.10      0.342  o       |       |       |       |     0.46
88.083    0.00    0.10      0.342  o       |       |       |       |     0.46
88.167    0.00    0.10      0.341  o       |       |       |       |     0.46
88.250    0.00    0.10      0.340  o       |       |       |       |     0.46

Remaining water in basin =    0.34 (Ac.Ft)

****************************HYDROGRAPH DATA****************************
               Number of intervals =  1059
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       16.714 (CFS)
               Total volume =       8.165 (Ac.Ft)
       Status of hydrographs being held in storage
                  Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
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Extended Detention Basin No. 2

Drainage Areas	Storm Event	Existing Condition		Developed		Routed Basin			Ex (cfs) +10% Difference Max
		Flow (cfs)	Volume (ac.ft.)	Flow (cfs)	Volume (ac.ft.)	Routed Basin Out Flow (cfs)	Storage Volume (ac.ft.)	Depth (ft)	
BASIN 2	2 Year - 1 Hour	49.310	1.1435	47.194	1.3402	0.815	1.305	2.73	-0.983
	2 Year - 3 Hour	22.628	1.0312	20.084	1.7706	1.146	3.360	1.67	-0.949
	2 Year - 6 Hour	18.407	1.1012	17.339	2.3931	1.470	2.161	4.17	-0.920
	2 Year - 24 Hour	1.661	0.7911	6.393	3.8846	1.728	2.705	4.99	0.040
	5 Year - 1 Hour	72.605	1.9029	68.734	1.9445	1.302	1.887	3.73	-0.982
	5 Year - 3 Hour	35.099	1.8606	32.327	2.5395	1.579	2.390	4.51	-0.955
	5 Year - 6 Hour	31.060	2.1813	29.939	3.4998	11.484	3.003	5.41	-0.630
	5 Year - 24 Hour	6.892	1.6579	9.054	5.5022	6.944	2.949	5.33	0.008
	10 Year - 1 Hour	96.988	3.0723	91.590	2.7128	1.694	2.634	4.88	-0.983
	10 Year - 3 Hour	51.290	4.0800	47.348	3.4814	14.837	3.043	5.46	-0.711
	10 Year - 6 Hour	47.388	5.1495	45.795	4.8167	43.521	3.117	5.56	-0.082
	10 Year - 24 Hour	16.731	6.0058	12.911	6.7994	12.489	3.015	5.43	-0.254
	100 Year - 1 Hour	155.539	5.1040	149.688	4.7239	125.746	3.264	5.76	-0.192
	100 Year - 3 Hour	82.628	7.1162	79.045	6.1264	79.141	3.181	5.65	-0.042
	100 Year - 6 Hour	79.183	9.9433	79.376	8.6580	76.226	3.175	5.64	-0.037
	100 Year - 24 Hour	30.032	12.3348	26.289	12.2882	26.244	3.085	5.52	-0.126

Basin 2 Size and Flow Calculations

BASIN 2

Horiz. : Vert.

4 : 1 = Basin Side Slope

	BASIN PARAMETERS					OUTLET								
Basin Elevation	Depth	Area S.F.	Volume C.F.	Volume AC-FT	Effective Volume AC-FT	Q1 Orifice Plate (cfs)	Q2 Orifice Plate (cfs)	Q3 Orifice Plate (cfs)	Q4 Orifice Plate (cfs)	Q5Orifice Plate (cfs)	Q6 Orifice Plate (cfs)	Q7Orifice Plate (cfs)	Q Weir 1 (cfs)	Q Total (cfs)
1289.00	0.00	17,745.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1290.00	1.00	19,839.00	18,792.00	0.431	0.431	0.225	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.225
1291.00	2.00	22,060.00	39,805.00	0.914	0.914	0.344	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.344
1292.00	3.00	24,708.00	63,189.00	1.451	1.451	0.431	0.559	0.000	0.000	0.000	0.000	0.000	0.000	0.991
1293.00	4.00	27,403.00	89,244.50	2.049	2.049	0.503	0.914	0.000	0.000	0.000	0.000	0.000	0.000	1.417
1294.00	5.00	30,344.00	118,118.00	2.712	2.712	0.567	1.165	0.000	0.000	0.000	0.000	0.000	0.000	1.731
1294.25	5.25	31,098.25	125,798.28	2.888	2.888	0.581	1.219	0.000	0.000	0.000	0.000	0.000	0.000	1.801
1294.50	5.50	31,852.50	133,667.13	3.069	3.069	0.596	1.272	0.000	0.000	0.000	0.000	0.000	15.179	17.046
1295.00	6.00	33,361.00	149,970.50	3.443	3.443	0.623	1.370	0.000	0.000	0.000	0.000	0.000	223.084	225.078

SUPPORTING DESIGN PARAMETERS

Orifice Coefficient	0.66		Dia of Orifice	3.00	5.00						
Gravimetric Constant	32.2	ft/s^2	Eff Dia of Orifice	0.2500	0.4167	0.0000	0.0000	0.0000	0.0000	0.0000	
Number of Rows			Area of Orifice	0.0491	0.1364	0.0000	0.0000	0.0000	0.0000	0.0000	
Minimum Orifice Plate Height			Number of Orifeces	1	1	1	1	1	1	1	
Minimum Orifice Plate Width			Elev	1289.25	1291.4	1293	1293.7				

Weir	Sharp Crest Weir Coefficient	4
	Length of Weir	120.00
	Elev. at Crest of Weir	1294.4

Q100 Elevation Weir Calc		
Basin 2 Weir Calc		
Crest Wier Elev.	1294.40	
Q100	115.36	cfs
Weir Length	120	
Weir Coeff.	4	
H Weir	0.38655	
Q100 Elevation	**1294.79**	

FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro2212.rte
**********HYDROGRAPH DATA**********
Number of intervals = 17
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 47.194 (CFS)
Total volume = 1.340 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

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Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 17
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.431	0.225	0.430	0.432
2.000	0.914	0.344	0.913	0.915
3.000	1.451	0.991	1.448	1.454
4.000	2.049	1.417	2.044	2.054
5.000	2.712	1.731	2.706	2.718
5.250	2.888	1.801	2.882	2.894
5.500	3.069	17.046	3.010	3.128
6.000	3.443	225.078	2.668	4.218

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 11.8 23.60 35.40 47.19	Depth (Ft.)
0.083	1.51	0.00	0.005	OI	0.01
0.167	4.41	0.01	0.026	O I	0.06
0.250	5.81	0.03	0.061	O I	0.14
0.333	6.59	0.05	0.103	O I	0.24
0.417	7.34	0.08	0.150	O I	0.35
0.500	8.35	0.11	0.204	O I	0.47
0.583	9.52	0.14	0.265	O I	0.61
0.667	11.14	0.17	0.335	O I	0.78
0.750	16.76	0.22	0.429	O I	1.00
0.833	39.66	0.27	0.622	O I	1.40
0.917	47.19	0.35	0.919	O I	2.01
1.000	19.23	0.62	1.144	O I	2.43
1.083	9.75	0.74	1.239	O I	2.61
1.167	4.33	0.79	1.283	O I	2.69
1.250	2.45	0.81	1.300	OI	2.72
1.333	0.42	0.81	1.305	O	2.73
1.417	0.13	0.81	1.301	O	2.72
1.500	0.00	0.80	1.296	O	2.71

1.583	0.00	0.80	1.290	o	|	|	|	|	2.70
1.667	0.00	0.79	1.285	o	|	|	|	|	2.69
1.750	0.00	0.78	1.280	o	|	|	|	|	2.68
1.833	0.00	0.78	1.274	o	|	|	|	|	2.67
1.917	0.00	0.77	1.269	o	|	|	|	|	2.66
2.000	0.00	0.77	1.263	o	|	|	|	|	2.65
2.083	0.00	0.76	1.258	o	|	|	|	|	2.64
2.167	0.00	0.75	1.253	o	|	|	|	|	2.63
2.250	0.00	0.75	1.248	o	|	|	|	|	2.62
2.333	0.00	0.74	1.243	o	|	|	|	|	2.61
2.417	0.00	0.73	1.238	o	|	|	|	|	2.60
2.500	0.00	0.73	1.233	o	|	|	|	|	2.59
2.583	0.00	0.72	1.228	o	|	|	|	|	2.58
2.667	0.00	0.72	1.223	o	|	|	|	|	2.57
2.750	0.00	0.71	1.218	o	|	|	|	|	2.57
2.833	0.00	0.70	1.213	o	|	|	|	|	2.56
2.917	0.00	0.70	1.208	o	|	|	|	|	2.55
3.000	0.00	0.69	1.203	o	|	|	|	|	2.54
3.083	0.00	0.69	1.199	o	|	|	|	|	2.53
3.167	0.00	0.68	1.194	o	|	|	|	|	2.52
3.250	0.00	0.68	1.189	o	|	|	|	|	2.51
3.333	0.00	0.67	1.185	o	|	|	|	|	2.50
3.417	0.00	0.66	1.180	o	|	|	|	|	2.50
3.500	0.00	0.66	1.175	o	|	|	|	|	2.49
3.583	0.00	0.65	1.171	o	|	|	|	|	2.48
3.667	0.00	0.65	1.166	o	|	|	|	|	2.47
3.750	0.00	0.64	1.162	o	|	|	|	|	2.46
3.833	0.00	0.64	1.158	o	|	|	|	|	2.45
3.917	0.00	0.63	1.153	o	|	|	|	|	2.45
4.000	0.00	0.63	1.149	o	|	|	|	|	2.44
4.083	0.00	0.62	1.145	o	|	|	|	|	2.43
4.167	0.00	0.62	1.140	o	|	|	|	|	2.42
4.250	0.00	0.61	1.136	o	|	|	|	|	2.41
4.333	0.00	0.61	1.132	o	|	|	|	|	2.41
4.417	0.00	0.60	1.128	o	|	|	|	|	2.40
4.500	0.00	0.60	1.124	o	|	|	|	|	2.39
4.583	0.00	0.59	1.119	o	|	|	|	|	2.38
4.667	0.00	0.59	1.115	o	|	|	|	|	2.38
4.750	0.00	0.58	1.111	o	|	|	|	|	2.37
4.833	0.00	0.58	1.107	o	|	|	|	|	2.36
4.917	0.00	0.57	1.103	o	|	|	|	|	2.35
5.000	0.00	0.57	1.100	o	|	|	|	|	2.35
5.083	0.00	0.56	1.096	o	|	|	|	|	2.34
5.167	0.00	0.56	1.092	o	|	|	|	|	2.33
5.250	0.00	0.55	1.088	o	|	|	|	|	2.32
5.333	0.00	0.55	1.084	o	|	|	|	|	2.32
5.417	0.00	0.54	1.080	o	|	|	|	|	2.31
5.500	0.00	0.54	1.077	o	|	|	|	|	2.30
5.583	0.00	0.54	1.073	o	|	|	|	|	2.30
5.667	0.00	0.53	1.069	o	|	|	|	|	2.29
5.750	0.00	0.53	1.066	o	|	|	|	|	2.28
5.833	0.00	0.52	1.062	o	|	|	|	|	2.28
5.917	0.00	0.52	1.058	o	|	|	|	|	2.27
6.000	0.00	0.51	1.055	o	|	|	|	|	2.26
6.083	0.00	0.51	1.051	o	|	|	|	|	2.26
6.167	0.00	0.51	1.048	o	|	|	|	|	2.25
6.250	0.00	0.50	1.044	o	|	|	|	|	2.24
6.333	0.00	0.50	1.041	o	|	|	|	|	2.24
6.417	0.00	0.49	1.038	o	|	|	|	|	2.23
6.500	0.00	0.49	1.034	o	|	|	|	|	2.22
6.583	0.00	0.48	1.031	o	|	|	|	|	2.22
6.667	0.00	0.48	1.027	o	|	|	|	|	2.21
6.750	0.00	0.48	1.024	o	|	|	|	|	2.21
6.833	0.00	0.47	1.021	o	|	|	|	|	2.20
6.917	0.00	0.47	1.018	o	|	|	|	|	2.19
7.000	0.00	0.47	1.014	o	|	|	|	|	2.19
7.083	0.00	0.46	1.011	o	|	|	|	|	2.18
7.167	0.00	0.46	1.008	o	|	|	|	|	2.18
7.250	0.00	0.45	1.005	o	|	|	|	|	2.17
7.333	0.00	0.45	1.002	o	|	|	|	|	2.16
7.417	0.00	0.45	0.999	o	|	|	|	|	2.16
7.500	0.00	0.44	0.996	o	|	|	|	|	2.15
7.583	0.00	0.44	0.993	o	|	|	|	|	2.15
7.667	0.00	0.44	0.990	o	|	|	|	|	2.14
7.750	0.00	0.43	0.987	o	|	|	|	|	2.14
7.833	0.00	0.43	0.984	o	|	|	|	|	2.13
7.917	0.00	0.42	0.981	o	|	|	|	|	2.12
8.000	0.00	0.42	0.978	o	|	|	|	|	2.12
8.083	0.00	0.42	0.975	o	|	|	|	|	2.11
8.167	0.00	0.41	0.972	o	|	|	|	|	2.11
8.250	0.00	0.41	0.969	o	|	|	|	|	2.10
8.333	0.00	0.41	0.966	o	|	|	|	|	2.10
8.417	0.00	0.40	0.964	o	|	|	|	|	2.09
8.500	0.00	0.40	0.961	o	|	|	|	|	2.09
8.583	0.00	0.40	0.958	o	|	|	|	|	2.08
8.667	0.00	0.39	0.955	o	|	|	|	|	2.08

8.750	0.00	0.39	0.953	o	|	|	|	|	2.07
8.833	0.00	0.39	0.950	o	|	|	|	|	2.07
8.917	0.00	0.38	0.947	o	|	|	|	|	2.06
9.000	0.00	0.38	0.945	o	|	|	|	|	2.06
9.083	0.00	0.38	0.942	o	|	|	|	|	2.05
9.167	0.00	0.37	0.940	o	|	|	|	|	2.05
9.250	0.00	0.37	0.937	o	|	|	|	|	2.04
9.333	0.00	0.37	0.934	o	|	|	|	|	2.04
9.417	0.00	0.37	0.932	o	|	|	|	|	2.03
9.500	0.00	0.36	0.929	o	|	|	|	|	2.03
9.583	0.00	0.36	0.927	o	|	|	|	|	2.02
9.667	0.00	0.36	0.924	o	|	|	|	|	2.02
9.750	0.00	0.35	0.922	o	|	|	|	|	2.01
9.833	0.00	0.35	0.920	o	|	|	|	|	2.01
9.917	0.00	0.35	0.917	o	|	|	|	|	2.01
10.000	0.00	0.34	0.915	o	|	|	|	|	2.00
10.083	0.00	0.34	0.912	o	|	|	|	|	2.00
10.167	0.00	0.34	0.910	o	|	|	|	|	1.99
10.250	0.00	0.34	0.908	o	|	|	|	|	1.99
10.333	0.00	0.34	0.905	o	|	|	|	|	1.98
10.417	0.00	0.34	0.903	o	|	|	|	|	1.98
10.500	0.00	0.34	0.901	o	|	|	|	|	1.97
10.583	0.00	0.34	0.898	o	|	|	|	|	1.97
10.667	0.00	0.34	0.896	o	|	|	|	|	1.96
10.750	0.00	0.34	0.894	o	|	|	|	|	1.96
10.833	0.00	0.34	0.891	o	|	|	|	|	1.95
10.917	0.00	0.34	0.889	o	|	|	|	|	1.95
11.000	0.00	0.34	0.887	o	|	|	|	|	1.94
11.083	0.00	0.34	0.884	o	|	|	|	|	1.94
11.167	0.00	0.34	0.882	o	|	|	|	|	1.93
11.250	0.00	0.34	0.880	o	|	|	|	|	1.93
11.333	0.00	0.33	0.877	o	|	|	|	|	1.92
11.417	0.00	0.33	0.875	o	|	|	|	|	1.92
11.500	0.00	0.33	0.873	o	|	|	|	|	1.91
11.583	0.00	0.33	0.870	o	|	|	|	|	1.91
11.667	0.00	0.33	0.868	o	|	|	|	|	1.91
11.750	0.00	0.33	0.866	o	|	|	|	|	1.90
11.833	0.00	0.33	0.864	o	|	|	|	|	1.90
11.917	0.00	0.33	0.861	o	|	|	|	|	1.89
12.000	0.00	0.33	0.859	o	|	|	|	|	1.89
12.083	0.00	0.33	0.857	o	|	|	|	|	1.88
12.167	0.00	0.33	0.854	o	|	|	|	|	1.88
12.250	0.00	0.33	0.852	o	|	|	|	|	1.87
12.333	0.00	0.33	0.850	o	|	|	|	|	1.87
12.417	0.00	0.33	0.848	o	|	|	|	|	1.86
12.500	0.00	0.33	0.845	o	|	|	|	|	1.86
12.583	0.00	0.33	0.843	o	|	|	|	|	1.85
12.667	0.00	0.33	0.841	o	|	|	|	|	1.85
12.750	0.00	0.33	0.839	o	|	|	|	|	1.84
12.833	0.00	0.32	0.836	o	|	|	|	|	1.84
12.917	0.00	0.32	0.834	o	|	|	|	|	1.83
13.000	0.00	0.32	0.832	o	|	|	|	|	1.83
13.083	0.00	0.32	0.830	o	|	|	|	|	1.83
13.167	0.00	0.32	0.828	o	|	|	|	|	1.82
13.250	0.00	0.32	0.825	o	|	|	|	|	1.82
13.333	0.00	0.32	0.823	o	|	|	|	|	1.81
13.417	0.00	0.32	0.821	o	|	|	|	|	1.81
13.500	0.00	0.32	0.819	o	|	|	|	|	1.80
13.583	0.00	0.32	0.816	o	|	|	|	|	1.80
13.667	0.00	0.32	0.814	o	|	|	|	|	1.79
13.750	0.00	0.32	0.812	o	|	|	|	|	1.79
13.833	0.00	0.32	0.810	o	|	|	|	|	1.78
13.917	0.00	0.32	0.808	o	|	|	|	|	1.78
14.000	0.00	0.32	0.806	o	|	|	|	|	1.78
14.083	0.00	0.32	0.803	o	|	|	|	|	1.77
14.167	0.00	0.32	0.801	o	|	|	|	|	1.77
14.250	0.00	0.32	0.799	o	|	|	|	|	1.76
14.333	0.00	0.32	0.797	o	|	|	|	|	1.76
14.417	0.00	0.31	0.795	o	|	|	|	|	1.75
14.500	0.00	0.31	0.792	o	|	|	|	|	1.75
14.583	0.00	0.31	0.790	o	|	|	|	|	1.74
14.667	0.00	0.31	0.788	o	|	|	|	|	1.74
14.750	0.00	0.31	0.786	o	|	|	|	|	1.73
14.833	0.00	0.31	0.784	o	|	|	|	|	1.73
14.917	0.00	0.31	0.782	o	|	|	|	|	1.73
15.000	0.00	0.31	0.780	o	|	|	|	|	1.72
15.083	0.00	0.31	0.777	o	|	|	|	|	1.72
15.167	0.00	0.31	0.775	o	|	|	|	|	1.71
15.250	0.00	0.31	0.773	o	|	|	|	|	1.71
15.333	0.00	0.31	0.771	o	|	|	|	|	1.70
15.417	0.00	0.31	0.769	o	|	|	|	|	1.70
15.500	0.00	0.31	0.767	o	|	|	|	|	1.70
15.583	0.00	0.31	0.765	o	|	|	|	|	1.69
15.667	0.00	0.31	0.763	o	|	|	|	|	1.69
15.750	0.00	0.31	0.760	o	|	|	|	|	1.68
15.833	0.00	0.31	0.758	o	|	|	|	|	1.68

15.917	0.00	0.31	0.756	o	|	|	|	|	1.67
16.000	0.00	0.30	0.754	o	|	|	|	|	1.67
16.083	0.00	0.30	0.752	o	|	|	|	|	1.66
16.167	0.00	0.30	0.750	o	|	|	|	|	1.66
16.250	0.00	0.30	0.748	o	|	|	|	|	1.66
16.333	0.00	0.30	0.746	o	|	|	|	|	1.65
16.417	0.00	0.30	0.744	o	|	|	|	|	1.65
16.500	0.00	0.30	0.742	o	|	|	|	|	1.64
16.583	0.00	0.30	0.740	o	|	|	|	|	1.64
16.667	0.00	0.30	0.737	o	|	|	|	|	1.63
16.750	0.00	0.30	0.735	o	|	|	|	|	1.63
16.833	0.00	0.30	0.733	o	|	|	|	|	1.63
16.917	0.00	0.30	0.731	o	|	|	|	|	1.62
17.000	0.00	0.30	0.729	o	|	|	|	|	1.62
17.083	0.00	0.30	0.727	o	|	|	|	|	1.61
17.167	0.00	0.30	0.725	o	|	|	|	|	1.61
17.250	0.00	0.30	0.723	o	|	|	|	|	1.60
17.333	0.00	0.30	0.721	o	|	|	|	|	1.60
17.417	0.00	0.30	0.719	o	|	|	|	|	1.60
17.500	0.00	0.30	0.717	o	|	|	|	|	1.59
17.583	0.00	0.29	0.715	o	|	|	|	|	1.59
17.667	0.00	0.29	0.713	o	|	|	|	|	1.58
17.750	0.00	0.29	0.711	o	|	|	|	|	1.58
17.833	0.00	0.29	0.709	o	|	|	|	|	1.58
17.917	0.00	0.29	0.707	o	|	|	|	|	1.57
18.000	0.00	0.29	0.705	o	|	|	|	|	1.57
18.083	0.00	0.29	0.703	o	|	|	|	|	1.56
18.167	0.00	0.29	0.701	o	|	|	|	|	1.56
18.250	0.00	0.29	0.699	o	|	|	|	|	1.55
18.333	0.00	0.29	0.697	o	|	|	|	|	1.55
18.417	0.00	0.29	0.695	o	|	|	|	|	1.55
18.500	0.00	0.29	0.693	o	|	|	|	|	1.54
18.583	0.00	0.29	0.691	o	|	|	|	|	1.54
18.667	0.00	0.29	0.689	o	|	|	|	|	1.53
18.750	0.00	0.29	0.687	o	|	|	|	|	1.53
18.833	0.00	0.29	0.685	o	|	|	|	|	1.53
18.917	0.00	0.29	0.683	o	|	|	|	|	1.52
19.000	0.00	0.29	0.681	o	|	|	|	|	1.52
19.083	0.00	0.29	0.679	o	|	|	|	|	1.51
19.167	0.00	0.29	0.677	o	|	|	|	|	1.51
19.250	0.00	0.29	0.675	o	|	|	|	|	1.51
19.333	0.00	0.28	0.673	o	|	|	|	|	1.50
19.417	0.00	0.28	0.671	o	|	|	|	|	1.50
19.500	0.00	0.28	0.669	o	|	|	|	|	1.49
19.583	0.00	0.28	0.667	o	|	|	|	|	1.49
19.667	0.00	0.28	0.665	o	|	|	|	|	1.48
19.750	0.00	0.28	0.663	o	|	|	|	|	1.48
19.833	0.00	0.28	0.661	o	|	|	|	|	1.48
19.917	0.00	0.28	0.659	o	|	|	|	|	1.47
20.000	0.00	0.28	0.657	o	|	|	|	|	1.47
20.083	0.00	0.28	0.655	o	|	|	|	|	1.46
20.167	0.00	0.28	0.654	o	|	|	|	|	1.46
20.250	0.00	0.28	0.652	o	|	|	|	|	1.46
20.333	0.00	0.28	0.650	o	|	|	|	|	1.45
20.417	0.00	0.28	0.648	o	|	|	|	|	1.45
20.500	0.00	0.28	0.646	o	|	|	|	|	1.44
20.583	0.00	0.28	0.644	o	|	|	|	|	1.44
20.667	0.00	0.28	0.642	o	|	|	|	|	1.44
20.750	0.00	0.28	0.640	o	|	|	|	|	1.43
20.833	0.00	0.28	0.638	o	|	|	|	|	1.43
20.917	0.00	0.28	0.636	o	|	|	|	|	1.43
21.000	0.00	0.28	0.634	o	|	|	|	|	1.42
21.083	0.00	0.27	0.633	o	|	|	|	|	1.42
21.167	0.00	0.27	0.631	o	|	|	|	|	1.41
21.250	0.00	0.27	0.629	o	|	|	|	|	1.41
21.333	0.00	0.27	0.627	o	|	|	|	|	1.41
21.417	0.00	0.27	0.625	o	|	|	|	|	1.40
21.500	0.00	0.27	0.623	o	|	|	|	|	1.40
21.583	0.00	0.27	0.621	o	|	|	|	|	1.39
21.667	0.00	0.27	0.619	o	|	|	|	|	1.39
21.750	0.00	0.27	0.618	o	|	|	|	|	1.39
21.833	0.00	0.27	0.616	o	|	|	|	|	1.38
21.917	0.00	0.27	0.614	o	|	|	|	|	1.38
22.000	0.00	0.27	0.612	o	|	|	|	|	1.37
22.083	0.00	0.27	0.610	o	|	|	|	|	1.37
22.167	0.00	0.27	0.608	o	|	|	|	|	1.37
22.250	0.00	0.27	0.606	o	|	|	|	|	1.36
22.333	0.00	0.27	0.605	o	|	|	|	|	1.36
22.417	0.00	0.27	0.603	o	|	|	|	|	1.36
22.500	0.00	0.27	0.601	o	|	|	|	|	1.35
22.583	0.00	0.27	0.599	o	|	|	|	|	1.35
22.667	0.00	0.27	0.597	o	|	|	|	|	1.34
22.750	0.00	0.27	0.595	o	|	|	|	|	1.34
22.833	0.00	0.27	0.594	o	|	|	|	|	1.34
22.917	0.00	0.26	0.592	o	|	|	|	|	1.33
23.000	0.00	0.26	0.590	o	|	|	|	|	1.33

23.083	0.00	0.26	0.588	o	|	|	|	|	1.33
23.167	0.00	0.26	0.586	o	|	|	|	|	1.32
23.250	0.00	0.26	0.584	o	|	|	|	|	1.32
23.333	0.00	0.26	0.583	o	|	|	|	|	1.31
23.417	0.00	0.26	0.581	o	|	|	|	|	1.31
23.500	0.00	0.26	0.579	o	|	|	|	|	1.31
23.583	0.00	0.26	0.577	o	|	|	|	|	1.30
23.667	0.00	0.26	0.575	o	|	|	|	|	1.30
23.750	0.00	0.26	0.574	o	|	|	|	|	1.30
23.833	0.00	0.26	0.572	o	|	|	|	|	1.29
23.917	0.00	0.26	0.570	o	|	|	|	|	1.29
24.000	0.00	0.26	0.568	o	|	|	|	|	1.28
24.083	0.00	0.26	0.566	o	|	|	|	|	1.28
24.167	0.00	0.26	0.565	o	|	|	|	|	1.28
24.250	0.00	0.26	0.563	o	|	|	|	|	1.27
24.333	0.00	0.26	0.561	o	|	|	|	|	1.27
24.417	0.00	0.26	0.559	o	|	|	|	|	1.27
24.500	0.00	0.26	0.558	o	|	|	|	|	1.26
24.583	0.00	0.26	0.556	o	|	|	|	|	1.26
24.667	0.00	0.26	0.554	o	|	|	|	|	1.25
24.750	0.00	0.25	0.552	o	|	|	|	|	1.25
24.833	0.00	0.25	0.551	o	|	|	|	|	1.25
24.917	0.00	0.25	0.549	o	|	|	|	|	1.24
25.000	0.00	0.25	0.547	o	|	|	|	|	1.24
25.083	0.00	0.25	0.545	o	|	|	|	|	1.24
25.167	0.00	0.25	0.544	o	|	|	|	|	1.23
25.250	0.00	0.25	0.542	o	|	|	|	|	1.23
25.333	0.00	0.25	0.540	o	|	|	|	|	1.23
25.417	0.00	0.25	0.538	o	|	|	|	|	1.22
25.500	0.00	0.25	0.537	o	|	|	|	|	1.22
25.583	0.00	0.25	0.535	o	|	|	|	|	1.22
25.667	0.00	0.25	0.533	o	|	|	|	|	1.21
25.750	0.00	0.25	0.532	o	|	|	|	|	1.21
25.833	0.00	0.25	0.530	o	|	|	|	|	1.20
25.917	0.00	0.25	0.528	o	|	|	|	|	1.20
26.000	0.00	0.25	0.526	o	|	|	|	|	1.20
26.083	0.00	0.25	0.525	o	|	|	|	|	1.19
26.167	0.00	0.25	0.523	o	|	|	|	|	1.19
26.250	0.00	0.25	0.521	o	|	|	|	|	1.19
26.333	0.00	0.25	0.520	o	|	|	|	|	1.18
26.417	0.00	0.25	0.518	o	|	|	|	|	1.18
26.500	0.00	0.25	0.516	o	|	|	|	|	1.18
26.583	0.00	0.25	0.514	o	|	|	|	|	1.17
26.667	0.00	0.25	0.513	o	|	|	|	|	1.17
26.750	0.00	0.24	0.511	o	|	|	|	|	1.17
26.833	0.00	0.24	0.509	o	|	|	|	|	1.16
26.917	0.00	0.24	0.508	o	|	|	|	|	1.16
27.000	0.00	0.24	0.506	o	|	|	|	|	1.16
27.083	0.00	0.24	0.504	o	|	|	|	|	1.15
27.167	0.00	0.24	0.503	o	|	|	|	|	1.15
27.250	0.00	0.24	0.501	o	|	|	|	|	1.14
27.333	0.00	0.24	0.499	o	|	|	|	|	1.14
27.417	0.00	0.24	0.498	o	|	|	|	|	1.14
27.500	0.00	0.24	0.496	o	|	|	|	|	1.13
27.583	0.00	0.24	0.494	o	|	|	|	|	1.13
27.667	0.00	0.24	0.493	o	|	|	|	|	1.13
27.750	0.00	0.24	0.491	o	|	|	|	|	1.12
27.833	0.00	0.24	0.489	o	|	|	|	|	1.12
27.917	0.00	0.24	0.488	o	|	|	|	|	1.12
28.000	0.00	0.24	0.486	o	|	|	|	|	1.11
28.083	0.00	0.24	0.484	o	|	|	|	|	1.11
28.167	0.00	0.24	0.483	o	|	|	|	|	1.11
28.250	0.00	0.24	0.481	o	|	|	|	|	1.10
28.333	0.00	0.24	0.480	o	|	|	|	|	1.10
28.417	0.00	0.24	0.478	o	|	|	|	|	1.10
28.500	0.00	0.24	0.476	o	|	|	|	|	1.09
28.583	0.00	0.24	0.475	o	|	|	|	|	1.09
28.667	0.00	0.24	0.473	o	|	|	|	|	1.09
28.750	0.00	0.23	0.471	o	|	|	|	|	1.08
28.833	0.00	0.23	0.470	o	|	|	|	|	1.08
28.917	0.00	0.23	0.468	o	|	|	|	|	1.08
29.000	0.00	0.23	0.467	o	|	|	|	|	1.07
29.083	0.00	0.23	0.465	o	|	|	|	|	1.07
29.167	0.00	0.23	0.463	o	|	|	|	|	1.07
29.250	0.00	0.23	0.462	o	|	|	|	|	1.06
29.333	0.00	0.23	0.460	o	|	|	|	|	1.06
29.417	0.00	0.23	0.459	o	|	|	|	|	1.06
29.500	0.00	0.23	0.457	o	|	|	|	|	1.05
29.583	0.00	0.23	0.455	o	|	|	|	|	1.05
29.667	0.00	0.23	0.454	o	|	|	|	|	1.05
29.750	0.00	0.23	0.452	o	|	|	|	|	1.04
29.833	0.00	0.23	0.451	o	|	|	|	|	1.04
29.917	0.00	0.23	0.449	o	|	|	|	|	1.04
30.000	0.00	0.23	0.447	o	|	|	|	|	1.03
30.083	0.00	0.23	0.446	o	|	|	|	|	1.03
30.167	0.00	0.23	0.444	o	|	|	|	|	1.03

30.250	0.00	0.23	0.443	o	|	|	|	|	1.02
30.333	0.00	0.23	0.441	o	|	|	|	|	1.02
30.417	0.00	0.23	0.440	o	|	|	|	|	1.02
30.500	0.00	0.23	0.438	o	|	|	|	|	1.01
30.583	0.00	0.23	0.436	o	|	|	|	|	1.01
30.667	0.00	0.23	0.435	o	|	|	|	|	1.01
30.750	0.00	0.23	0.433	o	|	|	|	|	1.00
30.833	0.00	0.23	0.432	o	|	|	|	|	1.00
30.917	0.00	0.22	0.430	o	|	|	|	|	1.00
31.000	0.00	0.22	0.429	o	|	|	|	|	0.99
31.083	0.00	0.22	0.427	o	|	|	|	|	0.99
31.167	0.00	0.22	0.426	o	|	|	|	|	0.99
31.250	0.00	0.22	0.424	o	|	|	|	|	0.98
31.333	0.00	0.22	0.423	o	|	|	|	|	0.98
31.417	0.00	0.22	0.421	o	|	|	|	|	0.98
31.500	0.00	0.22	0.420	o	|	|	|	|	0.97
31.583	0.00	0.22	0.418	o	|	|	|	|	0.97
31.667	0.00	0.22	0.417	o	|	|	|	|	0.97
31.750	0.00	0.22	0.415	o	|	|	|	|	0.96
31.833	0.00	0.22	0.414	o	|	|	|	|	0.96
31.917	0.00	0.22	0.412	o	|	|	|	|	0.96
32.000	0.00	0.21	0.411	o	|	|	|	|	0.95
32.083	0.00	0.21	0.409	o	|	|	|	|	0.95
32.167	0.00	0.21	0.408	o	|	|	|	|	0.95
32.250	0.00	0.21	0.406	o	|	|	|	|	0.94
32.333	0.00	0.21	0.405	o	|	|	|	|	0.94
32.417	0.00	0.21	0.403	o	|	|	|	|	0.94
32.500	0.00	0.21	0.402	o	|	|	|	|	0.93
32.583	0.00	0.21	0.400	o	|	|	|	|	0.93
32.667	0.00	0.21	0.399	o	|	|	|	|	0.93
32.750	0.00	0.21	0.398	o	|	|	|	|	0.92
32.833	0.00	0.21	0.396	o	|	|	|	|	0.92
32.917	0.00	0.21	0.395	o	|	|	|	|	0.92
33.000	0.00	0.21	0.393	o	|	|	|	|	0.91
33.083	0.00	0.20	0.392	o	|	|	|	|	0.91
33.167	0.00	0.20	0.390	o	|	|	|	|	0.91
33.250	0.00	0.20	0.389	o	|	|	|	|	0.90
33.333	0.00	0.20	0.388	o	|	|	|	|	0.90
33.417	0.00	0.20	0.386	o	|	|	|	|	0.90
33.500	0.00	0.20	0.385	o	|	|	|	|	0.89
33.583	0.00	0.20	0.384	o	|	|	|	|	0.89
33.667	0.00	0.20	0.382	o	|	|	|	|	0.89
33.750	0.00	0.20	0.381	o	|	|	|	|	0.88
33.833	0.00	0.20	0.379	o	|	|	|	|	0.88
33.917	0.00	0.20	0.378	o	|	|	|	|	0.88
34.000	0.00	0.20	0.377	o	|	|	|	|	0.87
34.083	0.00	0.20	0.375	o	|	|	|	|	0.87
34.167	0.00	0.20	0.374	o	|	|	|	|	0.87
34.250	0.00	0.19	0.373	o	|	|	|	|	0.86
34.333	0.00	0.19	0.371	o	|	|	|	|	0.86
34.417	0.00	0.19	0.370	o	|	|	|	|	0.86
34.500	0.00	0.19	0.369	o	|	|	|	|	0.86
34.583	0.00	0.19	0.367	o	|	|	|	|	0.85
34.667	0.00	0.19	0.366	o	|	|	|	|	0.85
34.750	0.00	0.19	0.365	o	|	|	|	|	0.85
34.833	0.00	0.19	0.363	o	|	|	|	|	0.84
34.917	0.00	0.19	0.362	o	|	|	|	|	0.84
35.000	0.00	0.19	0.361	o	|	|	|	|	0.84
35.083	0.00	0.19	0.359	o	|	|	|	|	0.83
35.167	0.00	0.19	0.358	o	|	|	|	|	0.83
35.250	0.00	0.19	0.357	o	|	|	|	|	0.83
35.333	0.00	0.19	0.356	o	|	|	|	|	0.83
35.417	0.00	0.18	0.354	o	|	|	|	|	0.82
35.500	0.00	0.18	0.353	o	|	|	|	|	0.82
35.583	0.00	0.18	0.352	o	|	|	|	|	0.82
35.667	0.00	0.18	0.351	o	|	|	|	|	0.81
35.750	0.00	0.18	0.349	o	|	|	|	|	0.81
35.833	0.00	0.18	0.348	o	|	|	|	|	0.81
35.917	0.00	0.18	0.347	o	|	|	|	|	0.80
36.000	0.00	0.18	0.346	o	|	|	|	|	0.80
36.083	0.00	0.18	0.344	o	|	|	|	|	0.80
36.167	0.00	0.18	0.343	o	|	|	|	|	0.80
36.250	0.00	0.18	0.342	o	|	|	|	|	0.79
36.333	0.00	0.18	0.341	o	|	|	|	|	0.79
36.417	0.00	0.18	0.339	o	|	|	|	|	0.79
36.500	0.00	0.18	0.338	o	|	|	|	|	0.78
36.583	0.00	0.18	0.337	o	|	|	|	|	0.78
36.667	0.00	0.18	0.336	o	|	|	|	|	0.78
36.750	0.00	0.17	0.335	o	|	|	|	|	0.78
36.833	0.00	0.17	0.333	o	|	|	|	|	0.77
36.917	0.00	0.17	0.332	o	|	|	|	|	0.77
37.000	0.00	0.17	0.331	o	|	|	|	|	0.77
37.083	0.00	0.17	0.330	o	|	|	|	|	0.77
37.167	0.00	0.17	0.329	o	|	|	|	|	0.76
37.250	0.00	0.17	0.327	o	|	|	|	|	0.76
37.333	0.00	0.17	0.326	o	|	|	|	|	0.76

37.417	0.00	0.17	0.325	o	|	|	|	0.75
37.500	0.00	0.17	0.324	o	|	|	|	0.75
37.583	0.00	0.17	0.323	o	|	|	|	0.75
37.667	0.00	0.17	0.322	o	|	|	|	0.75
37.750	0.00	0.17	0.320	o	|	|	|	0.74
37.833	0.00	0.17	0.319	o	|	|	|	0.74
37.917	0.00	0.17	0.318	o	|	|	|	0.74
38.000	0.00	0.17	0.317	o	|	|	|	0.74
38.083	0.00	0.16	0.316	o	|	|	|	0.73
38.167	0.00	0.16	0.315	o	|	|	|	0.73
38.250	0.00	0.16	0.314	o	|	|	|	0.73
38.333	0.00	0.16	0.312	o	|	|	|	0.72
38.417	0.00	0.16	0.311	o	|	|	|	0.72
38.500	0.00	0.16	0.310	o	|	|	|	0.72
38.583	0.00	0.16	0.309	o	|	|	|	0.72
38.667	0.00	0.16	0.308	o	|	|	|	0.71
38.750	0.00	0.16	0.307	o	|	|	|	0.71
38.833	0.00	0.16	0.306	o	|	|	|	0.71
38.917	0.00	0.16	0.305	o	|	|	|	0.71
39.000	0.00	0.16	0.304	o	|	|	|	0.70
39.083	0.00	0.16	0.303	o	|	|	|	0.70
39.167	0.00	0.16	0.301	o	|	|	|	0.70
39.250	0.00	0.16	0.300	o	|	|	|	0.70
39.333	0.00	0.16	0.299	o	|	|	|	0.69
39.417	0.00	0.16	0.298	o	|	|	|	0.69
39.500	0.00	0.16	0.297	o	|	|	|	0.69
39.583	0.00	0.15	0.296	o	|	|	|	0.69
39.667	0.00	0.15	0.295	o	|	|	|	0.68
39.750	0.00	0.15	0.294	o	|	|	|	0.68
39.833	0.00	0.15	0.293	o	|	|	|	0.68
39.917	0.00	0.15	0.292	o	|	|	|	0.68
40.000	0.00	0.15	0.291	o	|	|	|	0.67
40.083	0.00	0.15	0.290	o	|	|	|	0.67
40.167	0.00	0.15	0.289	o	|	|	|	0.67
40.250	0.00	0.15	0.288	o	|	|	|	0.67
40.333	0.00	0.15	0.287	o	|	|	|	0.67
40.417	0.00	0.15	0.286	o	|	|	|	0.66
40.500	0.00	0.15	0.285	o	|	|	|	0.66
40.583	0.00	0.15	0.284	o	|	|	|	0.66
40.667	0.00	0.15	0.283	o	|	|	|	0.66
40.750	0.00	0.15	0.282	o	|	|	|	0.65
40.833	0.00	0.15	0.281	o	|	|	|	0.65
40.917	0.00	0.15	0.279	o	|	|	|	0.65
41.000	0.00	0.15	0.278	o	|	|	|	0.65
41.083	0.00	0.14	0.277	o	|	|	|	0.64
41.167	0.00	0.14	0.276	o	|	|	|	0.64
41.250	0.00	0.14	0.276	o	|	|	|	0.64
41.333	0.00	0.14	0.275	o	|	|	|	0.64
41.417	0.00	0.14	0.274	o	|	|	|	0.63
41.500	0.00	0.14	0.273	o	|	|	|	0.63
41.583	0.00	0.14	0.272	o	|	|	|	0.63
41.667	0.00	0.14	0.271	o	|	|	|	0.63
41.750	0.00	0.14	0.270	o	|	|	|	0.63
41.833	0.00	0.14	0.269	o	|	|	|	0.62
41.917	0.00	0.14	0.268	o	|	|	|	0.62
42.000	0.00	0.14	0.267	o	|	|	|	0.62
42.083	0.00	0.14	0.266	o	|	|	|	0.62
42.167	0.00	0.14	0.265	o	|	|	|	0.61
42.250	0.00	0.14	0.264	o	|	|	|	0.61
42.333	0.00	0.14	0.263	o	|	|	|	0.61
42.417	0.00	0.14	0.262	o	|	|	|	0.61
42.500	0.00	0.14	0.261	o	|	|	|	0.61
42.583	0.00	0.14	0.260	o	|	|	|	0.60
42.667	0.00	0.14	0.259	o	|	|	|	0.60
42.750	0.00	0.13	0.258	o	|	|	|	0.60
42.833	0.00	0.13	0.257	o	|	|	|	0.60
42.917	0.00	0.13	0.256	o	|	|	|	0.59
43.000	0.00	0.13	0.255	o	|	|	|	0.59
43.083	0.00	0.13	0.255	o	|	|	|	0.59
43.167	0.00	0.13	0.254	o	|	|	|	0.59
43.250	0.00	0.13	0.253	o	|	|	|	0.59
43.333	0.00	0.13	0.252	o	|	|	|	0.58
43.417	0.00	0.13	0.251	o	|	|	|	0.58
43.500	0.00	0.13	0.250	o	|	|	|	0.58
43.583	0.00	0.13	0.249	o	|	|	|	0.58
43.667	0.00	0.13	0.248	o	|	|	|	0.58
43.750	0.00	0.13	0.247	o	|	|	|	0.57
43.833	0.00	0.13	0.246	o	|	|	|	0.57
43.917	0.00	0.13	0.246	o	|	|	|	0.57
44.000	0.00	0.13	0.245	o	|	|	|	0.57
44.083	0.00	0.13	0.244	o	|	|	|	0.57
44.167	0.00	0.13	0.243	o	|	|	|	0.56
44.250	0.00	0.13	0.242	o	|	|	|	0.56
44.333	0.00	0.13	0.241	o	|	|	|	0.56
44.417	0.00	0.13	0.240	o	|	|	|	0.56
44.500	0.00	0.13	0.239	o	|	|	|	0.56

44.583	0.00	0.12	0.239	o	|	|	|	|	0.55
44.667	0.00	0.12	0.238	o	|	|	|	|	0.55
44.750	0.00	0.12	0.237	o	|	|	|	|	0.55
44.833	0.00	0.12	0.236	o	|	|	|	|	0.55
44.917	0.00	0.12	0.235	o	|	|	|	|	0.55
45.000	0.00	0.12	0.234	o	|	|	|	|	0.54
45.083	0.00	0.12	0.234	o	|	|	|	|	0.54
45.167	0.00	0.12	0.233	o	|	|	|	|	0.54
45.250	0.00	0.12	0.232	o	|	|	|	|	0.54
45.333	0.00	0.12	0.231	o	|	|	|	|	0.54
45.417	0.00	0.12	0.230	o	|	|	|	|	0.53
45.500	0.00	0.12	0.229	o	|	|	|	|	0.53
45.583	0.00	0.12	0.229	o	|	|	|	|	0.53
45.667	0.00	0.12	0.228	o	|	|	|	|	0.53
45.750	0.00	0.12	0.227	o	|	|	|	|	0.53
45.833	0.00	0.12	0.226	o	|	|	|	|	0.52
45.917	0.00	0.12	0.225	o	|	|	|	|	0.52
46.000	0.00	0.12	0.224	o	|	|	|	|	0.52
46.083	0.00	0.12	0.224	o	|	|	|	|	0.52
46.167	0.00	0.12	0.223	o	|	|	|	|	0.52
46.250	0.00	0.12	0.222	o	|	|	|	|	0.52
46.333	0.00	0.12	0.221	o	|	|	|	|	0.51
46.417	0.00	0.12	0.220	o	|	|	|	|	0.51
46.500	0.00	0.11	0.220	o	|	|	|	|	0.51
46.583	0.00	0.11	0.219	o	|	|	|	|	0.51
46.667	0.00	0.11	0.218	o	|	|	|	|	0.51
46.750	0.00	0.11	0.217	o	|	|	|	|	0.50
46.833	0.00	0.11	0.217	o	|	|	|	|	0.50
46.917	0.00	0.11	0.216	o	|	|	|	|	0.50
47.000	0.00	0.11	0.215	o	|	|	|	|	0.50
47.083	0.00	0.11	0.214	o	|	|	|	|	0.50
47.167	0.00	0.11	0.213	o	|	|	|	|	0.50
47.250	0.00	0.11	0.213	o	|	|	|	|	0.49
47.333	0.00	0.11	0.212	o	|	|	|	|	0.49
47.417	0.00	0.11	0.211	o	|	|	|	|	0.49
47.500	0.00	0.11	0.210	o	|	|	|	|	0.49
47.583	0.00	0.11	0.210	o	|	|	|	|	0.49
47.667	0.00	0.11	0.209	o	|	|	|	|	0.48
47.750	0.00	0.11	0.208	o	|	|	|	|	0.48
47.833	0.00	0.11	0.207	o	|	|	|	|	0.48
47.917	0.00	0.11	0.207	o	|	|	|	|	0.48
48.000	0.00	0.11	0.206	o	|	|	|	|	0.48
48.083	0.00	0.11	0.205	o	|	|	|	|	0.48
48.167	0.00	0.11	0.204	o	|	|	|	|	0.47
48.250	0.00	0.11	0.204	o	|	|	|	|	0.47
48.333	0.00	0.11	0.203	o	|	|	|	|	0.47
48.417	0.00	0.11	0.202	o	|	|	|	|	0.47
48.500	0.00	0.11	0.202	o	|	|	|	|	0.47
48.583	0.00	0.10	0.201	o	|	|	|	|	0.47
48.667	0.00	0.10	0.200	o	|	|	|	|	0.46
48.750	0.00	0.10	0.199	o	|	|	|	|	0.46
48.833	0.00	0.10	0.199	o	|	|	|	|	0.46
48.917	0.00	0.10	0.198	o	|	|	|	|	0.46
49.000	0.00	0.10	0.197	o	|	|	|	|	0.46
49.083	0.00	0.10	0.196	o	|	|	|	|	0.46
49.167	0.00	0.10	0.196	o	|	|	|	|	0.45
49.250	0.00	0.10	0.195	o	|	|	|	|	0.45
49.333	0.00	0.10	0.194	o	|	|	|	|	0.45
49.417	0.00	0.10	0.194	o	|	|	|	|	0.45
49.500	0.00	0.10	0.193	o	|	|	|	|	0.45
49.583	0.00	0.10	0.192	o	|	|	|	|	0.45
49.667	0.00	0.10	0.192	o	|	|	|	|	0.44
49.750	0.00	0.10	0.191	o	|	|	|	|	0.44

Remaining water in basin = 0.19 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 597
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.815 (CFS)
Total volume = 1.150 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro2232.rte
**********HYDROGRAPH DATA**********
Number of intervals = 41
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 20.084 (CFS)
Total volume = 1.771 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 41
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.431	0.225	0.430	0.432
2.000	0.914	0.344	0.913	0.915
3.000	1.451	0.991	1.448	1.454
4.000	2.049	1.417	2.044	2.054
5.000	2.712	1.731	2.706	2.718
5.250	2.888	1.801	2.882	2.894
5.500	3.069	17.046	3.010	3.128
6.000	3.443	225.078	2.668	4.218

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 5.0 10.04 15.06 20.08	Depth (Ft.)
0.083	0.95	0.00	0.003	OI	0.01
0.167	2.52	0.01	0.015	O I	0.04
0.250	2.77	0.02	0.033	O I	0.08
0.333	3.00	0.03	0.053	O I	0.12
0.417	3.51	0.04	0.075	O I	0.17
0.500	3.90	0.05	0.100	O I	0.23
0.583	4.08	0.07	0.127	O I	0.30
0.667	4.05	0.08	0.155	O I	0.36
0.750	4.38	0.10	0.183	O I	0.43
0.833	4.23	0.11	0.212	O I	0.49
0.917	3.98	0.13	0.240	O I	0.56
1.000	4.16	0.14	0.267	O I	0.62
1.083	4.70	0.15	0.296	O I	0.69
1.167	5.24	0.17	0.330	O I	0.76
1.250	5.38	0.19	0.365	O I	0.85
1.333	5.31	0.21	0.400	O I	0.93
1.417	5.54	0.23	0.436	O I	1.01
1.500	6.30	0.24	0.475	O I	1.09

1.583	6.36	0.25	0.517	O	| I	|	|	|	|	1.18
1.667	6.31	0.26	0.559	O	| I	|	|	|	|	1.27
1.750	7.07	0.27	0.604	O	| I	|	|	|	|	1.36
1.833	7.74	0.28	0.653	O	| I	|	|	|	|	1.46
1.917	7.56	0.29	0.703	O	| I	|	|	|	|	1.56
2.000	7.42	0.30	0.753	O	| I	|	|	|	|	1.67
2.083	7.58	0.32	0.802	O	| I	|	|	|	|	1.77
2.167	8.53	0.33	0.856	O	| I	|	|	|	|	1.88
2.250	10.46	0.35	0.919	O	| I	|	|	|	|	2.01
2.333	10.67	0.43	0.989	O	| I	|	|	|	|	2.14
2.417	11.85	0.52	1.063	O	| I	|	|	|	|	2.28
2.500	16.56	0.64	1.157	|O	|	|	|	I |	|	2.45
2.583	20.08	0.78	1.278	|O	|	|	|	| I	|	2.68
2.667	20.08	0.94	1.410	|O	|	|	|	| I	|	2.92
2.750	13.36	1.04	1.519	|O	|	|	I |	|	|	3.11
2.833	7.84	1.09	1.584	|O	| I	|	|	|	|	3.22
2.917	6.06	1.11	1.625	|O	I |	|	|	|	|	3.29
3.000	4.40	1.13	1.653	|O	I |	|	|	|	|	3.34
3.083	1.99	1.14	1.667	|O I	|	|	|	|	|	3.36
3.167	0.67	1.15	1.668	|O	|	|	|	|	|	3.36
3.250	0.31	1.14	1.664	IO	|	|	|	|	|	3.36
3.333	0.14	1.14	1.658	IO	|	|	|	|	|	3.35
3.417	0.03	1.13	1.650	IO	|	|	|	|	|	3.33
3.500	0.00	1.13	1.643	IO	|	|	|	|	|	3.32
3.583	0.00	1.12	1.635	IO	|	|	|	|	|	3.31
3.667	0.00	1.12	1.627	IO	|	|	|	|	|	3.29
3.750	0.00	1.11	1.620	IO	|	|	|	|	|	3.28
3.833	0.00	1.11	1.612	IO	|	|	|	|	|	3.27
3.917	0.00	1.10	1.604	IO	|	|	|	|	|	3.26
4.000	0.00	1.09	1.597	IO	|	|	|	|	|	3.24
4.083	0.00	1.09	1.589	IO	|	|	|	|	|	3.23
4.167	0.00	1.08	1.582	IO	|	|	|	|	|	3.22
4.250	0.00	1.08	1.574	IO	|	|	|	|	|	3.21
4.333	0.00	1.07	1.567	IO	|	|	|	|	|	3.19
4.417	0.00	1.07	1.560	IO	|	|	|	|	|	3.18
4.500	0.00	1.06	1.552	IO	|	|	|	|	|	3.17
4.583	0.00	1.06	1.545	IO	|	|	|	|	|	3.16
4.667	0.00	1.05	1.538	IO	|	|	|	|	|	3.14
4.750	0.00	1.05	1.530	IO	|	|	|	|	|	3.13
4.833	0.00	1.04	1.523	IO	|	|	|	|	|	3.12
4.917	0.00	1.04	1.516	IO	|	|	|	|	|	3.11
5.000	0.00	1.03	1.509	IO	|	|	|	|	|	3.10
5.083	0.00	1.03	1.502	IO	|	|	|	|	|	3.09
5.167	0.00	1.02	1.495	IO	|	|	|	|	|	3.07
5.250	0.00	1.02	1.488	IO	|	|	|	|	|	3.06
5.333	0.00	1.01	1.481	IO	|	|	|	|	|	3.05
5.417	0.00	1.01	1.474	IO	|	|	|	|	|	3.04
5.500	0.00	1.00	1.467	IO	|	|	|	|	|	3.03
5.583	0.00	1.00	1.460	IO	|	|	|	|	|	3.02
5.667	0.00	0.99	1.453	IO	|	|	|	|	|	3.00
5.750	0.00	0.99	1.446	IO	|	|	|	|	|	2.99
5.833	0.00	0.98	1.440	IO	|	|	|	|	|	2.98
5.917	0.00	0.97	1.433	IO	|	|	|	|	|	2.97
6.000	0.00	0.96	1.426	IO	|	|	|	|	|	2.95
6.083	0.00	0.95	1.420	IO	|	|	|	|	|	2.94
6.167	0.00	0.95	1.413	IO	|	|	|	|	|	2.93
6.250	0.00	0.94	1.407	IO	|	|	|	|	|	2.92
6.333	0.00	0.93	1.400	IO	|	|	|	|	|	2.91
6.417	0.00	0.92	1.394	IO	|	|	|	|	|	2.89
6.500	0.00	0.91	1.388	IO	|	|	|	|	|	2.88
6.583	0.00	0.91	1.381	IO	|	|	|	|	|	2.87
6.667	0.00	0.90	1.375	IO	|	|	|	|	|	2.86
6.750	0.00	0.89	1.369	IO	|	|	|	|	|	2.85
6.833	0.00	0.88	1.363	IO	|	|	|	|	|	2.84
6.917	0.00	0.88	1.357	IO	|	|	|	|	|	2.82
7.000	0.00	0.87	1.351	IO	|	|	|	|	|	2.81
7.083	0.00	0.86	1.345	IO	|	|	|	|	|	2.80
7.167	0.00	0.86	1.339	IO	|	|	|	|	|	2.79
7.250	0.00	0.85	1.333	IO	|	|	|	|	|	2.78
7.333	0.00	0.84	1.327	IO	|	|	|	|	|	2.77
7.417	0.00	0.83	1.321	IO	|	|	|	|	|	2.76
7.500	0.00	0.83	1.316	IO	|	|	|	|	|	2.75
7.583	0.00	0.82	1.310	IO	|	|	|	|	|	2.74
7.667	0.00	0.81	1.304	IO	|	|	|	|	|	2.73
7.750	0.00	0.81	1.299	IO	|	|	|	|	|	2.72
7.833	0.00	0.80	1.293	IO	|	|	|	|	|	2.71
7.917	0.00	0.79	1.288	IO	|	|	|	|	|	2.70
8.000	0.00	0.79	1.282	IO	|	|	|	|	|	2.69
8.083	0.00	0.78	1.277	IO	|	|	|	|	|	2.68
8.167	0.00	0.77	1.271	IO	|	|	|	|	|	2.67
8.250	0.00	0.77	1.266	IO	|	|	|	|	|	2.66
8.333	0.00	0.76	1.261	IO	|	|	|	|	|	2.65
8.417	0.00	0.76	1.256	IO	|	|	|	|	|	2.64
8.500	0.00	0.75	1.250	IO	|	|	|	|	|	2.63
8.583	0.00	0.74	1.245	IO	|	|	|	|	|	2.62
8.667	0.00	0.74	1.240	IO	|	|	|	|	|	2.61

8.750	0.00	0.73	1.235	IO					2.60
8.833	0.00	0.72	1.230	IO					2.59
8.917	0.00	0.72	1.225	IO					2.58
9.000	0.00	0.71	1.220	IO					2.57
9.083	0.00	0.71	1.215	IO					2.56
9.167	0.00	0.70	1.211	IO					2.55
9.250	0.00	0.70	1.206	IO					2.54
9.333	0.00	0.69	1.201	IO					2.53
9.417	0.00	0.68	1.196	IO					2.53
9.500	0.00	0.68	1.192	IO					2.52
9.583	0.00	0.67	1.187	IO					2.51
9.667	0.00	0.67	1.182	IO					2.50
9.750	0.00	0.66	1.178	IO					2.49
9.833	0.00	0.66	1.173	IO					2.48
9.917	0.00	0.65	1.169	IO					2.47
10.000	0.00	0.65	1.164	IO					2.47
10.083	0.00	0.64	1.160	IO					2.46
10.167	0.00	0.63	1.155	IO					2.45
10.250	0.00	0.63	1.151	IO					2.44
10.333	0.00	0.62	1.147	O					2.43
10.417	0.00	0.62	1.142	O					2.43
10.500	0.00	0.61	1.138	O					2.42
10.583	0.00	0.61	1.134	O					2.41
10.667	0.00	0.60	1.130	O					2.40
10.750	0.00	0.60	1.126	O					2.39
10.833	0.00	0.59	1.122	O					2.39
10.917	0.00	0.59	1.117	O					2.38
11.000	0.00	0.58	1.113	O					2.37
11.083	0.00	0.58	1.109	O					2.36
11.167	0.00	0.57	1.105	O					2.36
11.250	0.00	0.57	1.101	O					2.35
11.333	0.00	0.57	1.098	O					2.34
11.417	0.00	0.56	1.094	O					2.33
11.500	0.00	0.56	1.090	O					2.33
11.583	0.00	0.55	1.086	O					2.32
11.667	0.00	0.55	1.082	O					2.31
11.750	0.00	0.54	1.079	O					2.31
11.833	0.00	0.54	1.075	O					2.30
11.917	0.00	0.53	1.071	O					2.29
12.000	0.00	0.53	1.067	O					2.29
12.083	0.00	0.52	1.064	O					2.28
12.167	0.00	0.52	1.060	O					2.27
12.250	0.00	0.52	1.057	O					2.27
12.333	0.00	0.51	1.053	O					2.26
12.417	0.00	0.51	1.050	O					2.25
12.500	0.00	0.50	1.046	O					2.25
12.583	0.00	0.50	1.043	O					2.24
12.667	0.00	0.49	1.039	O					2.23
12.750	0.00	0.49	1.036	O					2.23
12.833	0.00	0.49	1.032	O					2.22
12.917	0.00	0.48	1.029	O					2.21
13.000	0.00	0.48	1.026	O					2.21
13.083	0.00	0.47	1.023	O					2.20
13.167	0.00	0.47	1.019	O					2.20
13.250	0.00	0.47	1.016	O					2.19
13.333	0.00	0.46	1.013	O					2.18
13.417	0.00	0.46	1.010	O					2.18
13.500	0.00	0.46	1.007	O					2.17
13.583	0.00	0.45	1.003	O					2.17
13.667	0.00	0.45	1.000	O					2.16
13.750	0.00	0.44	0.997	O					2.16
13.833	0.00	0.44	0.994	O					2.15
13.917	0.00	0.44	0.991	O					2.14
14.000	0.00	0.43	0.988	O					2.14
14.083	0.00	0.43	0.985	O					2.13
14.167	0.00	0.43	0.982	O					2.13
14.250	0.00	0.42	0.979	O					2.12
14.333	0.00	0.42	0.976	O					2.12
14.417	0.00	0.42	0.974	O					2.11
14.500	0.00	0.41	0.971	O					2.11
14.583	0.00	0.41	0.968	O					2.10
14.667	0.00	0.41	0.965	O					2.10
14.750	0.00	0.40	0.962	O					2.09
14.833	0.00	0.40	0.960	O					2.08
14.917	0.00	0.40	0.957	O					2.08
15.000	0.00	0.39	0.954	O					2.07
15.083	0.00	0.39	0.951	O					2.07
15.167	0.00	0.39	0.949	O					2.06
15.250	0.00	0.38	0.946	O					2.06
15.333	0.00	0.38	0.943	O					2.05
15.417	0.00	0.38	0.941	O					2.05
15.500	0.00	0.37	0.938	O					2.05
15.583	0.00	0.37	0.936	O					2.04
15.667	0.00	0.37	0.933	O					2.04
15.750	0.00	0.36	0.931	O					2.03
15.833	0.00	0.36	0.928	O					2.03

15.917	0.00	0.36	0.926	o	|	|	|	|	2.02
16.000	0.00	0.36	0.923	o	|	|	|	|	2.02
16.083	0.00	0.35	0.921	o	|	|	|	|	2.01
16.167	0.00	0.35	0.918	o	|	|	|	|	2.01
16.250	0.00	0.35	0.916	o	|	|	|	|	2.00
16.333	0.00	0.34	0.914	o	|	|	|	|	2.00
16.417	0.00	0.34	0.911	o	|	|	|	|	1.99
16.500	0.00	0.34	0.909	o	|	|	|	|	1.99
16.583	0.00	0.34	0.907	o	|	|	|	|	1.98
16.667	0.00	0.34	0.904	o	|	|	|	|	1.98
16.750	0.00	0.34	0.902	o	|	|	|	|	1.97
16.833	0.00	0.34	0.899	o	|	|	|	|	1.97
16.917	0.00	0.34	0.897	o	|	|	|	|	1.97
17.000	0.00	0.34	0.895	o	|	|	|	|	1.96
17.083	0.00	0.34	0.892	o	|	|	|	|	1.96
17.167	0.00	0.34	0.890	o	|	|	|	|	1.95
17.250	0.00	0.34	0.888	o	|	|	|	|	1.95
17.333	0.00	0.34	0.885	o	|	|	|	|	1.94
17.417	0.00	0.34	0.883	o	|	|	|	|	1.94
17.500	0.00	0.34	0.881	o	|	|	|	|	1.93
17.583	0.00	0.34	0.879	o	|	|	|	|	1.93
17.667	0.00	0.33	0.876	o	|	|	|	|	1.92
17.750	0.00	0.33	0.874	o	|	|	|	|	1.92
17.833	0.00	0.33	0.872	o	|	|	|	|	1.91
17.917	0.00	0.33	0.869	o	|	|	|	|	1.91
18.000	0.00	0.33	0.867	o	|	|	|	|	1.90
18.083	0.00	0.33	0.865	o	|	|	|	|	1.90
18.167	0.00	0.33	0.862	o	|	|	|	|	1.89
18.250	0.00	0.33	0.860	o	|	|	|	|	1.89
18.333	0.00	0.33	0.858	o	|	|	|	|	1.88
18.417	0.00	0.33	0.856	o	|	|	|	|	1.88
18.500	0.00	0.33	0.853	o	|	|	|	|	1.87
18.583	0.00	0.33	0.851	o	|	|	|	|	1.87
18.667	0.00	0.33	0.849	o	|	|	|	|	1.87
18.750	0.00	0.33	0.847	o	|	|	|	|	1.86
18.833	0.00	0.33	0.844	o	|	|	|	|	1.86
18.917	0.00	0.33	0.842	o	|	|	|	|	1.85
19.000	0.00	0.33	0.840	o	|	|	|	|	1.85
19.083	0.00	0.33	0.838	o	|	|	|	|	1.84
19.167	0.00	0.32	0.835	o	|	|	|	|	1.84
19.250	0.00	0.32	0.833	o	|	|	|	|	1.83
19.333	0.00	0.32	0.831	o	|	|	|	|	1.83
19.417	0.00	0.32	0.829	o	|	|	|	|	1.82
19.500	0.00	0.32	0.826	o	|	|	|	|	1.82
19.583	0.00	0.32	0.824	o	|	|	|	|	1.81
19.667	0.00	0.32	0.822	o	|	|	|	|	1.81
19.750	0.00	0.32	0.820	o	|	|	|	|	1.80
19.833	0.00	0.32	0.818	o	|	|	|	|	1.80
19.917	0.00	0.32	0.815	o	|	|	|	|	1.80
20.000	0.00	0.32	0.813	o	|	|	|	|	1.79
20.083	0.00	0.32	0.811	o	|	|	|	|	1.79
20.167	0.00	0.32	0.809	o	|	|	|	|	1.78
20.250	0.00	0.32	0.807	o	|	|	|	|	1.78
20.333	0.00	0.32	0.804	o	|	|	|	|	1.77
20.417	0.00	0.32	0.802	o	|	|	|	|	1.77
20.500	0.00	0.32	0.800	o	|	|	|	|	1.76
20.583	0.00	0.32	0.798	o	|	|	|	|	1.76
20.667	0.00	0.31	0.796	o	|	|	|	|	1.76
20.750	0.00	0.31	0.794	o	|	|	|	|	1.75
20.833	0.00	0.31	0.791	o	|	|	|	|	1.75
20.917	0.00	0.31	0.789	o	|	|	|	|	1.74
21.000	0.00	0.31	0.787	o	|	|	|	|	1.74
21.083	0.00	0.31	0.785	o	|	|	|	|	1.73
21.167	0.00	0.31	0.783	o	|	|	|	|	1.73
21.250	0.00	0.31	0.781	o	|	|	|	|	1.72
21.333	0.00	0.31	0.778	o	|	|	|	|	1.72
21.417	0.00	0.31	0.776	o	|	|	|	|	1.72
21.500	0.00	0.31	0.774	o	|	|	|	|	1.71
21.583	0.00	0.31	0.772	o	|	|	|	|	1.71
21.667	0.00	0.31	0.770	o	|	|	|	|	1.70
21.750	0.00	0.31	0.768	o	|	|	|	|	1.70
21.833	0.00	0.31	0.766	o	|	|	|	|	1.69
21.917	0.00	0.31	0.764	o	|	|	|	|	1.69
22.000	0.00	0.31	0.761	o	|	|	|	|	1.68
22.083	0.00	0.31	0.759	o	|	|	|	|	1.68
22.167	0.00	0.31	0.757	o	|	|	|	|	1.68
22.250	0.00	0.30	0.755	o	|	|	|	|	1.67
22.333	0.00	0.30	0.753	o	|	|	|	|	1.67
22.417	0.00	0.30	0.751	o	|	|	|	|	1.66
22.500	0.00	0.30	0.749	o	|	|	|	|	1.66
22.583	0.00	0.30	0.747	o	|	|	|	|	1.65
22.667	0.00	0.30	0.745	o	|	|	|	|	1.65
22.750	0.00	0.30	0.743	o	|	|	|	|	1.65
22.833	0.00	0.30	0.741	o	|	|	|	|	1.64
22.917	0.00	0.30	0.738	o	|	|	|	|	1.64
23.000	0.00	0.30	0.736	o	|	|	|	|	1.63

23.083	0.00	0.30	0.734	o	|	|	|	|	1.63
23.167	0.00	0.30	0.732	o	|	|	|	|	1.62
23.250	0.00	0.30	0.730	o	|	|	|	|	1.62
23.333	0.00	0.30	0.728	o	|	|	|	|	1.62
23.417	0.00	0.30	0.726	o	|	|	|	|	1.61
23.500	0.00	0.30	0.724	o	|	|	|	|	1.61
23.583	0.00	0.30	0.722	o	|	|	|	|	1.60
23.667	0.00	0.30	0.720	o	|	|	|	|	1.60
23.750	0.00	0.30	0.718	o	|	|	|	|	1.59
23.833	0.00	0.30	0.716	o	|	|	|	|	1.59
23.917	0.00	0.29	0.714	o	|	|	|	|	1.59
24.000	0.00	0.29	0.712	o	|	|	|	|	1.58
24.083	0.00	0.29	0.710	o	|	|	|	|	1.58
24.167	0.00	0.29	0.708	o	|	|	|	|	1.57
24.250	0.00	0.29	0.706	o	|	|	|	|	1.57
24.333	0.00	0.29	0.704	o	|	|	|	|	1.56
24.417	0.00	0.29	0.702	o	|	|	|	|	1.56
24.500	0.00	0.29	0.700	o	|	|	|	|	1.56
24.583	0.00	0.29	0.698	o	|	|	|	|	1.55
24.667	0.00	0.29	0.696	o	|	|	|	|	1.55
24.750	0.00	0.29	0.694	o	|	|	|	|	1.54
24.833	0.00	0.29	0.692	o	|	|	|	|	1.54
24.917	0.00	0.29	0.690	o	|	|	|	|	1.54
25.000	0.00	0.29	0.688	o	|	|	|	|	1.53
25.083	0.00	0.29	0.686	o	|	|	|	|	1.53
25.167	0.00	0.29	0.684	o	|	|	|	|	1.52
25.250	0.00	0.29	0.682	o	|	|	|	|	1.52
25.333	0.00	0.29	0.680	o	|	|	|	|	1.52
25.417	0.00	0.29	0.678	o	|	|	|	|	1.51
25.500	0.00	0.29	0.676	o	|	|	|	|	1.51
25.583	0.00	0.28	0.674	o	|	|	|	|	1.50
25.667	0.00	0.28	0.672	o	|	|	|	|	1.50
25.750	0.00	0.28	0.670	o	|	|	|	|	1.49
25.833	0.00	0.28	0.668	o	|	|	|	|	1.49
25.917	0.00	0.28	0.666	o	|	|	|	|	1.49
26.000	0.00	0.28	0.664	o	|	|	|	|	1.48
26.083	0.00	0.28	0.662	o	|	|	|	|	1.48
26.167	0.00	0.28	0.660	o	|	|	|	|	1.47
26.250	0.00	0.28	0.658	o	|	|	|	|	1.47
26.333	0.00	0.28	0.656	o	|	|	|	|	1.47
26.417	0.00	0.28	0.655	o	|	|	|	|	1.46
26.500	0.00	0.28	0.653	o	|	|	|	|	1.46
26.583	0.00	0.28	0.651	o	|	|	|	|	1.45
26.667	0.00	0.28	0.649	o	|	|	|	|	1.45
26.750	0.00	0.28	0.647	o	|	|	|	|	1.45
26.833	0.00	0.28	0.645	o	|	|	|	|	1.44
26.917	0.00	0.28	0.643	o	|	|	|	|	1.44
27.000	0.00	0.28	0.641	o	|	|	|	|	1.43
27.083	0.00	0.28	0.639	o	|	|	|	|	1.43
27.167	0.00	0.28	0.637	o	|	|	|	|	1.43
27.250	0.00	0.28	0.635	o	|	|	|	|	1.42
27.333	0.00	0.27	0.634	o	|	|	|	|	1.42
27.417	0.00	0.27	0.632	o	|	|	|	|	1.42
27.500	0.00	0.27	0.630	o	|	|	|	|	1.41
27.583	0.00	0.27	0.628	o	|	|	|	|	1.41
27.667	0.00	0.27	0.626	o	|	|	|	|	1.40
27.750	0.00	0.27	0.624	o	|	|	|	|	1.40
27.833	0.00	0.27	0.622	o	|	|	|	|	1.40
27.917	0.00	0.27	0.620	o	|	|	|	|	1.39
28.000	0.00	0.27	0.618	o	|	|	|	|	1.39
28.083	0.00	0.27	0.617	o	|	|	|	|	1.38
28.167	0.00	0.27	0.615	o	|	|	|	|	1.38
28.250	0.00	0.27	0.613	o	|	|	|	|	1.38
28.333	0.00	0.27	0.611	o	|	|	|	|	1.37
28.417	0.00	0.27	0.609	o	|	|	|	|	1.37
28.500	0.00	0.27	0.607	o	|	|	|	|	1.37
28.583	0.00	0.27	0.605	o	|	|	|	|	1.36
28.667	0.00	0.27	0.604	o	|	|	|	|	1.36
28.750	0.00	0.27	0.602	o	|	|	|	|	1.35
28.833	0.00	0.27	0.600	o	|	|	|	|	1.35
28.917	0.00	0.27	0.598	o	|	|	|	|	1.35
29.000	0.00	0.27	0.596	o	|	|	|	|	1.34
29.083	0.00	0.27	0.594	o	|	|	|	|	1.34
29.167	0.00	0.26	0.593	o	|	|	|	|	1.33
29.250	0.00	0.26	0.591	o	|	|	|	|	1.33
29.333	0.00	0.26	0.589	o	|	|	|	|	1.33
29.417	0.00	0.26	0.587	o	|	|	|	|	1.32
29.500	0.00	0.26	0.585	o	|	|	|	|	1.32
29.583	0.00	0.26	0.584	o	|	|	|	|	1.32
29.667	0.00	0.26	0.582	o	|	|	|	|	1.31
29.750	0.00	0.26	0.580	o	|	|	|	|	1.31
29.833	0.00	0.26	0.578	o	|	|	|	|	1.30
29.917	0.00	0.26	0.576	o	|	|	|	|	1.30
30.000	0.00	0.26	0.575	o	|	|	|	|	1.30
30.083	0.00	0.26	0.573	o	|	|	|	|	1.29
30.167	0.00	0.26	0.571	o	|	|	|	|	1.29

30.250	0.00	0.26	0.569	o	|	|	|	|	1.29
30.333	0.00	0.26	0.567	o	|	|	|	|	1.28
30.417	0.00	0.26	0.566	o	|	|	|	|	1.28
30.500	0.00	0.26	0.564	o	|	|	|	|	1.28
30.583	0.00	0.26	0.562	o	|	|	|	|	1.27
30.667	0.00	0.26	0.560	o	|	|	|	|	1.27
30.750	0.00	0.26	0.559	o	|	|	|	|	1.26
30.833	0.00	0.26	0.557	o	|	|	|	|	1.26
30.917	0.00	0.26	0.555	o	|	|	|	|	1.26
31.000	0.00	0.26	0.553	o	|	|	|	|	1.25
31.083	0.00	0.25	0.551	o	|	|	|	|	1.25
31.167	0.00	0.25	0.550	o	|	|	|	|	1.25
31.250	0.00	0.25	0.548	o	|	|	|	|	1.24
31.333	0.00	0.25	0.546	o	|	|	|	|	1.24
31.417	0.00	0.25	0.544	o	|	|	|	|	1.23
31.500	0.00	0.25	0.543	o	|	|	|	|	1.23
31.583	0.00	0.25	0.541	o	|	|	|	|	1.23
31.667	0.00	0.25	0.539	o	|	|	|	|	1.22
31.750	0.00	0.25	0.538	o	|	|	|	|	1.22
31.833	0.00	0.25	0.536	o	|	|	|	|	1.22
31.917	0.00	0.25	0.534	o	|	|	|	|	1.21
32.000	0.00	0.25	0.532	o	|	|	|	|	1.21
32.083	0.00	0.25	0.531	o	|	|	|	|	1.21
32.167	0.00	0.25	0.529	o	|	|	|	|	1.20
32.250	0.00	0.25	0.527	o	|	|	|	|	1.20
32.333	0.00	0.25	0.526	o	|	|	|	|	1.20
32.417	0.00	0.25	0.524	o	|	|	|	|	1.19
32.500	0.00	0.25	0.522	o	|	|	|	|	1.19
32.583	0.00	0.25	0.520	o	|	|	|	|	1.19
32.667	0.00	0.25	0.519	o	|	|	|	|	1.18
32.750	0.00	0.25	0.517	o	|	|	|	|	1.18
32.833	0.00	0.25	0.515	o	|	|	|	|	1.17
32.917	0.00	0.25	0.514	o	|	|	|	|	1.17
33.000	0.00	0.24	0.512	o	|	|	|	|	1.17
33.083	0.00	0.24	0.510	o	|	|	|	|	1.16
33.167	0.00	0.24	0.509	o	|	|	|	|	1.16
33.250	0.00	0.24	0.507	o	|	|	|	|	1.16
33.333	0.00	0.24	0.505	o	|	|	|	|	1.15
33.417	0.00	0.24	0.504	o	|	|	|	|	1.15
33.500	0.00	0.24	0.502	o	|	|	|	|	1.15
33.583	0.00	0.24	0.500	o	|	|	|	|	1.14
33.667	0.00	0.24	0.499	o	|	|	|	|	1.14
33.750	0.00	0.24	0.497	o	|	|	|	|	1.14
33.833	0.00	0.24	0.495	o	|	|	|	|	1.13
33.917	0.00	0.24	0.494	o	|	|	|	|	1.13
34.000	0.00	0.24	0.492	o	|	|	|	|	1.13
34.083	0.00	0.24	0.490	o	|	|	|	|	1.12
34.167	0.00	0.24	0.489	o	|	|	|	|	1.12
34.250	0.00	0.24	0.487	o	|	|	|	|	1.12
34.333	0.00	0.24	0.485	o	|	|	|	|	1.11
34.417	0.00	0.24	0.484	o	|	|	|	|	1.11
34.500	0.00	0.24	0.482	o	|	|	|	|	1.11
34.583	0.00	0.24	0.480	o	|	|	|	|	1.10
34.667	0.00	0.24	0.479	o	|	|	|	|	1.10
34.750	0.00	0.24	0.477	o	|	|	|	|	1.10
34.833	0.00	0.24	0.475	o	|	|	|	|	1.09
34.917	0.00	0.24	0.474	o	|	|	|	|	1.09
35.000	0.00	0.24	0.472	o	|	|	|	|	1.09
35.083	0.00	0.23	0.471	o	|	|	|	|	1.08
35.167	0.00	0.23	0.469	o	|	|	|	|	1.08
35.250	0.00	0.23	0.467	o	|	|	|	|	1.08
35.333	0.00	0.23	0.466	o	|	|	|	|	1.07
35.417	0.00	0.23	0.464	o	|	|	|	|	1.07
35.500	0.00	0.23	0.463	o	|	|	|	|	1.07
35.583	0.00	0.23	0.461	o	|	|	|	|	1.06
35.667	0.00	0.23	0.459	o	|	|	|	|	1.06
35.750	0.00	0.23	0.458	o	|	|	|	|	1.06
35.833	0.00	0.23	0.456	o	|	|	|	|	1.05
35.917	0.00	0.23	0.455	o	|	|	|	|	1.05
36.000	0.00	0.23	0.453	o	|	|	|	|	1.05
36.083	0.00	0.23	0.451	o	|	|	|	|	1.04
36.167	0.00	0.23	0.450	o	|	|	|	|	1.04
36.250	0.00	0.23	0.448	o	|	|	|	|	1.04
36.333	0.00	0.23	0.447	o	|	|	|	|	1.03
36.417	0.00	0.23	0.445	o	|	|	|	|	1.03
36.500	0.00	0.23	0.444	o	|	|	|	|	1.03
36.583	0.00	0.23	0.442	o	|	|	|	|	1.02
36.667	0.00	0.23	0.440	o	|	|	|	|	1.02
36.750	0.00	0.23	0.439	o	|	|	|	|	1.02
36.833	0.00	0.23	0.437	o	|	|	|	|	1.01
36.917	0.00	0.23	0.436	o	|	|	|	|	1.01
37.000	0.00	0.23	0.434	o	|	|	|	|	1.01
37.083	0.00	0.23	0.433	o	|	|	|	|	1.00
37.167	0.00	0.23	0.431	o	|	|	|	|	1.00
37.250	0.00	0.22	0.430	o	|	|	|	|	1.00
37.333	0.00	0.22	0.428	o	|	|	|	|	0.99

37.417	0.00	0.22	0.426	o	|	|	|	|	0.99
37.500	0.00	0.22	0.425	o	|	|	|	|	0.99
37.583	0.00	0.22	0.423	o	|	|	|	|	0.98
37.667	0.00	0.22	0.422	o	|	|	|	|	0.98
37.750	0.00	0.22	0.420	o	|	|	|	|	0.98
37.833	0.00	0.22	0.419	o	|	|	|	|	0.97
37.917	0.00	0.22	0.417	o	|	|	|	|	0.97
38.000	0.00	0.22	0.416	o	|	|	|	|	0.96
38.083	0.00	0.22	0.414	o	|	|	|	|	0.96
38.167	0.00	0.22	0.413	o	|	|	|	|	0.96
38.250	0.00	0.21	0.411	o	|	|	|	|	0.95
38.333	0.00	0.21	0.410	o	|	|	|	|	0.95
38.417	0.00	0.21	0.408	o	|	|	|	|	0.95
38.500	0.00	0.21	0.407	o	|	|	|	|	0.94
38.583	0.00	0.21	0.405	o	|	|	|	|	0.94
38.667	0.00	0.21	0.404	o	|	|	|	|	0.94
38.750	0.00	0.21	0.403	o	|	|	|	|	0.93
38.833	0.00	0.21	0.401	o	|	|	|	|	0.93
38.917	0.00	0.21	0.400	o	|	|	|	|	0.93
39.000	0.00	0.21	0.398	o	|	|	|	|	0.92
39.083	0.00	0.21	0.397	o	|	|	|	|	0.92
39.167	0.00	0.21	0.395	o	|	|	|	|	0.92
39.250	0.00	0.21	0.394	o	|	|	|	|	0.91
39.333	0.00	0.20	0.393	o	|	|	|	|	0.91
39.417	0.00	0.20	0.391	o	|	|	|	|	0.91
39.500	0.00	0.20	0.390	o	|	|	|	|	0.90
39.583	0.00	0.20	0.388	o	|	|	|	|	0.90
39.667	0.00	0.20	0.387	o	|	|	|	|	0.90
39.750	0.00	0.20	0.386	o	|	|	|	|	0.89
39.833	0.00	0.20	0.384	o	|	|	|	|	0.89
39.917	0.00	0.20	0.383	o	|	|	|	|	0.89
40.000	0.00	0.20	0.381	o	|	|	|	|	0.89
40.083	0.00	0.20	0.380	o	|	|	|	|	0.88
40.167	0.00	0.20	0.379	o	|	|	|	|	0.88
40.250	0.00	0.20	0.377	o	|	|	|	|	0.88
40.333	0.00	0.20	0.376	o	|	|	|	|	0.87
40.417	0.00	0.20	0.375	o	|	|	|	|	0.87
40.500	0.00	0.19	0.373	o	|	|	|	|	0.87
40.583	0.00	0.19	0.372	o	|	|	|	|	0.86
40.667	0.00	0.19	0.371	o	|	|	|	|	0.86
40.750	0.00	0.19	0.369	o	|	|	|	|	0.86
40.833	0.00	0.19	0.368	o	|	|	|	|	0.85
40.917	0.00	0.19	0.367	o	|	|	|	|	0.85
41.000	0.00	0.19	0.365	o	|	|	|	|	0.85
41.083	0.00	0.19	0.364	o	|	|	|	|	0.84
41.167	0.00	0.19	0.363	o	|	|	|	|	0.84
41.250	0.00	0.19	0.361	o	|	|	|	|	0.84
41.333	0.00	0.19	0.360	o	|	|	|	|	0.84
41.417	0.00	0.19	0.359	o	|	|	|	|	0.83
41.500	0.00	0.19	0.358	o	|	|	|	|	0.83
41.583	0.00	0.19	0.356	o	|	|	|	|	0.83
41.667	0.00	0.19	0.355	o	|	|	|	|	0.82
41.750	0.00	0.18	0.354	o	|	|	|	|	0.82
41.833	0.00	0.18	0.352	o	|	|	|	|	0.82
41.917	0.00	0.18	0.351	o	|	|	|	|	0.81
42.000	0.00	0.18	0.350	o	|	|	|	|	0.81
42.083	0.00	0.18	0.349	o	|	|	|	|	0.81
42.167	0.00	0.18	0.347	o	|	|	|	|	0.81
42.250	0.00	0.18	0.346	o	|	|	|	|	0.80
42.333	0.00	0.18	0.345	o	|	|	|	|	0.80
42.417	0.00	0.18	0.344	o	|	|	|	|	0.80
42.500	0.00	0.18	0.342	o	|	|	|	|	0.79
42.583	0.00	0.18	0.341	o	|	|	|	|	0.79
42.667	0.00	0.18	0.340	o	|	|	|	|	0.79
42.750	0.00	0.18	0.339	o	|	|	|	|	0.79
42.833	0.00	0.18	0.338	o	|	|	|	|	0.78
42.917	0.00	0.18	0.336	o	|	|	|	|	0.78
43.000	0.00	0.17	0.335	o	|	|	|	|	0.78
43.083	0.00	0.17	0.334	o	|	|	|	|	0.77
43.167	0.00	0.17	0.333	o	|	|	|	|	0.77
43.250	0.00	0.17	0.332	o	|	|	|	|	0.77
43.333	0.00	0.17	0.330	o	|	|	|	|	0.77
43.417	0.00	0.17	0.329	o	|	|	|	|	0.76
43.500	0.00	0.17	0.328	o	|	|	|	|	0.76
43.583	0.00	0.17	0.327	o	|	|	|	|	0.76
43.667	0.00	0.17	0.326	o	|	|	|	|	0.76
43.750	0.00	0.17	0.324	o	|	|	|	|	0.75
43.833	0.00	0.17	0.323	o	|	|	|	|	0.75
43.917	0.00	0.17	0.322	o	|	|	|	|	0.75
44.000	0.00	0.17	0.321	o	|	|	|	|	0.74
44.083	0.00	0.17	0.320	o	|	|	|	|	0.74
44.167	0.00	0.17	0.319	o	|	|	|	|	0.74
44.250	0.00	0.17	0.318	o	|	|	|	|	0.74
44.333	0.00	0.17	0.316	o	|	|	|	|	0.73
44.417	0.00	0.16	0.315	o	|	|	|	|	0.73
44.500	0.00	0.16	0.314	o	|	|	|	|	0.73

44.583	0.00	0.16	0.313	o	|	|	|	|	0.73
44.667	0.00	0.16	0.312	o	|	|	|	|	0.72
44.750	0.00	0.16	0.311	o	|	|	|	|	0.72
44.833	0.00	0.16	0.310	o	|	|	|	|	0.72
44.917	0.00	0.16	0.309	o	|	|	|	|	0.72
45.000	0.00	0.16	0.307	o	|	|	|	|	0.71
45.083	0.00	0.16	0.306	o	|	|	|	|	0.71
45.167	0.00	0.16	0.305	o	|	|	|	|	0.71
45.250	0.00	0.16	0.304	o	|	|	|	|	0.71
45.333	0.00	0.16	0.303	o	|	|	|	|	0.70
45.417	0.00	0.16	0.302	o	|	|	|	|	0.70
45.500	0.00	0.16	0.301	o	|	|	|	|	0.70
45.583	0.00	0.16	0.300	o	|	|	|	|	0.70
45.667	0.00	0.16	0.299	o	|	|	|	|	0.69
45.750	0.00	0.16	0.298	o	|	|	|	|	0.69
45.833	0.00	0.15	0.297	o	|	|	|	|	0.69
45.917	0.00	0.15	0.296	o	|	|	|	|	0.69
46.000	0.00	0.15	0.294	o	|	|	|	|	0.68
46.083	0.00	0.15	0.293	o	|	|	|	|	0.68
46.167	0.00	0.15	0.292	o	|	|	|	|	0.68
46.250	0.00	0.15	0.291	o	|	|	|	|	0.68
46.333	0.00	0.15	0.290	o	|	|	|	|	0.67
46.417	0.00	0.15	0.289	o	|	|	|	|	0.67
46.500	0.00	0.15	0.288	o	|	|	|	|	0.67
46.583	0.00	0.15	0.287	o	|	|	|	|	0.67
46.667	0.00	0.15	0.286	o	|	|	|	|	0.66
46.750	0.00	0.15	0.285	o	|	|	|	|	0.66
46.833	0.00	0.15	0.284	o	|	|	|	|	0.66
46.917	0.00	0.15	0.283	o	|	|	|	|	0.66
47.000	0.00	0.15	0.282	o	|	|	|	|	0.65
47.083	0.00	0.15	0.281	o	|	|	|	|	0.65
47.167	0.00	0.15	0.280	o	|	|	|	|	0.65
47.250	0.00	0.15	0.279	o	|	|	|	|	0.65
47.333	0.00	0.15	0.278	o	|	|	|	|	0.64
47.417	0.00	0.14	0.277	o	|	|	|	|	0.64
47.500	0.00	0.14	0.276	o	|	|	|	|	0.64
47.583	0.00	0.14	0.275	o	|	|	|	|	0.64
47.667	0.00	0.14	0.274	o	|	|	|	|	0.64
47.750	0.00	0.14	0.273	o	|	|	|	|	0.63
47.833	0.00	0.14	0.272	o	|	|	|	|	0.63
47.917	0.00	0.14	0.271	o	|	|	|	|	0.63
48.000	0.00	0.14	0.270	o	|	|	|	|	0.63
48.083	0.00	0.14	0.269	o	|	|	|	|	0.62
48.167	0.00	0.14	0.268	o	|	|	|	|	0.62
48.250	0.00	0.14	0.267	o	|	|	|	|	0.62
48.333	0.00	0.14	0.266	o	|	|	|	|	0.62
48.417	0.00	0.14	0.265	o	|	|	|	|	0.62
48.500	0.00	0.14	0.264	o	|	|	|	|	0.61
48.583	0.00	0.14	0.263	o	|	|	|	|	0.61
48.667	0.00	0.14	0.262	o	|	|	|	|	0.61
48.750	0.00	0.14	0.262	o	|	|	|	|	0.61
48.833	0.00	0.14	0.261	o	|	|	|	|	0.60
48.917	0.00	0.14	0.260	o	|	|	|	|	0.60
49.000	0.00	0.14	0.259	o	|	|	|	|	0.60
49.083	0.00	0.13	0.258	o	|	|	|	|	0.60
49.167	0.00	0.13	0.257	o	|	|	|	|	0.60
49.250	0.00	0.13	0.256	o	|	|	|	|	0.59
49.333	0.00	0.13	0.255	o	|	|	|	|	0.59
49.417	0.00	0.13	0.254	o	|	|	|	|	0.59
49.500	0.00	0.13	0.253	o	|	|	|	|	0.59
49.583	0.00	0.13	0.252	o	|	|	|	|	0.59
49.667	0.00	0.13	0.251	o	|	|	|	|	0.58
49.750	0.00	0.13	0.250	o	|	|	|	|	0.58
49.833	0.00	0.13	0.250	o	|	|	|	|	0.58
49.917	0.00	0.13	0.249	o	|	|	|	|	0.58
50.000	0.00	0.13	0.248	o	|	|	|	|	0.57
50.083	0.00	0.13	0.247	o	|	|	|	|	0.57
50.167	0.00	0.13	0.246	o	|	|	|	|	0.57
50.250	0.00	0.13	0.245	o	|	|	|	|	0.57
50.333	0.00	0.13	0.244	o	|	|	|	|	0.57
50.417	0.00	0.13	0.243	o	|	|	|	|	0.56
50.500	0.00	0.13	0.242	o	|	|	|	|	0.56
50.583	0.00	0.13	0.242	o	|	|	|	|	0.56
50.667	0.00	0.13	0.241	o	|	|	|	|	0.56
50.750	0.00	0.13	0.240	o	|	|	|	|	0.56
50.833	0.00	0.12	0.239	o	|	|	|	|	0.55
50.917	0.00	0.12	0.238	o	|	|	|	|	0.55
51.000	0.00	0.12	0.237	o	|	|	|	|	0.55
51.083	0.00	0.12	0.236	o	|	|	|	|	0.55
51.167	0.00	0.12	0.236	o	|	|	|	|	0.55
51.250	0.00	0.12	0.235	o	|	|	|	|	0.54
51.333	0.00	0.12	0.234	o	|	|	|	|	0.54
51.417	0.00	0.12	0.233	o	|	|	|	|	0.54
51.500	0.00	0.12	0.232	o	|	|	|	|	0.54
51.583	0.00	0.12	0.231	o	|	|	|	|	0.54
51.667	0.00	0.12	0.231	o	|	|	|	|	0.54

51.750	0.00	0.12	0.230	o	|	|	|	|	0.53
51.833	0.00	0.12	0.229	o	|	|	|	|	0.53
51.917	0.00	0.12	0.228	o	|	|	|	|	0.53
52.000	0.00	0.12	0.227	o	|	|	|	|	0.53
52.083	0.00	0.12	0.226	o	|	|	|	|	0.53
52.167	0.00	0.12	0.226	o	|	|	|	|	0.52
52.250	0.00	0.12	0.225	o	|	|	|	|	0.52
52.333	0.00	0.12	0.224	o	|	|	|	|	0.52
52.417	0.00	0.12	0.223	o	|	|	|	|	0.52
52.500	0.00	0.12	0.222	o	|	|	|	|	0.52
52.583	0.00	0.12	0.222	o	|	|	|	|	0.51
52.667	0.00	0.12	0.221	o	|	|	|	|	0.51
52.750	0.00	0.11	0.220	o	|	|	|	|	0.51
52.833	0.00	0.11	0.219	o	|	|	|	|	0.51
52.917	0.00	0.11	0.218	o	|	|	|	|	0.51
53.000	0.00	0.11	0.218	o	|	|	|	|	0.51
53.083	0.00	0.11	0.217	o	|	|	|	|	0.50
53.167	0.00	0.11	0.216	o	|	|	|	|	0.50
53.250	0.00	0.11	0.215	o	|	|	|	|	0.50
53.333	0.00	0.11	0.215	o	|	|	|	|	0.50
53.417	0.00	0.11	0.214	o	|	|	|	|	0.50
53.500	0.00	0.11	0.213	o	|	|	|	|	0.49
53.583	0.00	0.11	0.212	o	|	|	|	|	0.49
53.667	0.00	0.11	0.212	o	|	|	|	|	0.49
53.750	0.00	0.11	0.211	o	|	|	|	|	0.49
53.833	0.00	0.11	0.210	o	|	|	|	|	0.49
53.917	0.00	0.11	0.209	o	|	|	|	|	0.49
54.000	0.00	0.11	0.209	o	|	|	|	|	0.48
54.083	0.00	0.11	0.208	o	|	|	|	|	0.48
54.167	0.00	0.11	0.207	o	|	|	|	|	0.48
54.250	0.00	0.11	0.206	o	|	|	|	|	0.48
54.333	0.00	0.11	0.206	o	|	|	|	|	0.48
54.417	0.00	0.11	0.205	o	|	|	|	|	0.48
54.500	0.00	0.11	0.204	o	|	|	|	|	0.47
54.583	0.00	0.11	0.203	o	|	|	|	|	0.47
54.667	0.00	0.11	0.203	o	|	|	|	|	0.47
54.750	0.00	0.11	0.202	o	|	|	|	|	0.47
54.833	0.00	0.11	0.201	o	|	|	|	|	0.47
54.917	0.00	0.10	0.200	o	|	|	|	|	0.47
55.000	0.00	0.10	0.200	o	|	|	|	|	0.46
55.083	0.00	0.10	0.199	o	|	|	|	|	0.46
55.167	0.00	0.10	0.198	o	|	|	|	|	0.46
55.250	0.00	0.10	0.198	o	|	|	|	|	0.46
55.333	0.00	0.10	0.197	o	|	|	|	|	0.46
55.417	0.00	0.10	0.196	o	|	|	|	|	0.46
55.500	0.00	0.10	0.195	o	|	|	|	|	0.45
55.583	0.00	0.10	0.195	o	|	|	|	|	0.45
55.667	0.00	0.10	0.194	o	|	|	|	|	0.45
55.750	0.00	0.10	0.193	o	|	|	|	|	0.45
55.833	0.00	0.10	0.193	o	|	|	|	|	0.45
55.917	0.00	0.10	0.192	o	|	|	|	|	0.45
56.000	0.00	0.10	0.191	o	|	|	|	|	0.44

Remaining water in basin = 0.19 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 672
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.146 (CFS)
Total volume = 1.580 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro2262.rte
**********HYDROGRAPH DATA**********
Number of intervals = 77
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 17.339 (CFS)
Total volume = 2.393 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 77
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.431	0.225	0.430	0.432
2.000	0.914	0.344	0.913	0.915
3.000	1.451	0.991	1.448	1.454
4.000	2.049	1.417	2.044	2.054
5.000	2.712	1.731	2.706	2.718
5.250	2.888	1.801	2.882	2.894
5.500	3.069	17.046	3.010	3.128
6.000	3.443	225.078	2.668	4.218

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 4.3 8.67 13.00 17.34	Depth (Ft.)
0.083	0.50	0.00	0.002	O | | | |	0.00
0.167	1.43	0.00	0.008	O I | | | |	0.02
0.250	1.81	0.01	0.019	O I | | | |	0.05
0.333	1.94	0.02	0.032	O I | | | |	0.07
0.417	2.01	0.02	0.046	O I | | | |	0.11
0.500	2.16	0.03	0.060	O I | | | |	0.14
0.583	2.33	0.04	0.075	O I | | | |	0.17
0.667	2.38	0.05	0.091	O I | | | |	0.21
0.750	2.39	0.06	0.107	O I | | | |	0.25
0.833	2.41	0.06	0.123	O I | | | |	0.29
0.917	2.41	0.07	0.139	O I | | | |	0.32
1.000	2.51	0.08	0.156	O I | | | |	0.36
1.083	2.68	0.09	0.173	O I | | | |	0.40
1.167	2.72	0.10	0.191	O I | | | |	0.44
1.250	2.74	0.11	0.209	O I | | | |	0.49
1.333	2.75	0.12	0.227	O I | | | |	0.53
1.417	2.76	0.13	0.245	O I | | | |	0.57
1.500	2.76	0.14	0.264	O I | | | |	0.61

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1.583    2.76    0.15      0.282  o    I  |        |        |        |     0.65
1.667    2.76    0.16      0.299  o    I  |        |        |        |     0.69
1.750    2.76    0.17      0.317  o    I  |        |        |        |     0.74
1.833    2.76    0.17      0.335  o    I  |        |        |        |     0.78
1.917    2.76    0.18      0.353  o    I  |        |        |        |     0.82
2.000    2.86    0.19      0.371  o    I  |        |        |        |     0.86
2.083    2.92    0.20      0.389  o    I  |        |        |        |     0.90
2.167    2.90    0.21      0.408  o    I  |        |        |        |     0.95
2.250    3.04    0.22      0.427  o    I  |        |        |        |     0.99
2.333    3.08    0.23      0.447  o    I  |        |        |        |     1.03
2.417    3.09    0.23      0.466  o    I  |        |        |        |     1.07
2.500    3.09    0.24      0.486  o    I  |        |        |        |     1.11
2.583    3.10    0.24      0.506  o    I  |        |        |        |     1.15
2.667    3.10    0.25      0.525  o    I  |        |        |        |     1.20
2.750    3.20    0.25      0.545  o    I  |        |        |        |     1.24
2.833    3.37    0.26      0.566  o     I |        |        |        |     1.28
2.917    3.41    0.26      0.588  o     I |        |        |        |     1.32
3.000    3.43    0.27      0.609  o     I |        |        |        |     1.37
3.083    3.44    0.27      0.631  o     I |        |        |        |     1.41
3.167    3.55    0.28      0.653  o     I |        |        |        |     1.46
3.250    3.71    0.29      0.676  o     I |        |        |        |     1.51
3.333    3.76    0.29      0.700  o     I |        |        |        |     1.56
3.417    3.87    0.30      0.724  o      I|        |        |        |     1.61
3.500    4.15    0.30      0.750  o      I|        |        |        |     1.66
3.583    4.47    0.31      0.777  o       I        |        |        |     1.72
3.667    4.69    0.32      0.807  o       I        |        |        |     1.78
3.750    4.86    0.33      0.838  o       I        |        |        |     1.84
3.833    5.07    0.33      0.869  o       |I       |        |        |     1.91
3.917    5.23    0.34      0.903  o       |I       |        |        |     1.98
4.000    5.42    0.37      0.937  o       | I      |        |        |     2.04
4.083    5.57    0.41      0.972  o       | I      |        |        |     2.11
4.167    5.86    0.46      1.008  o       | I      |        |        |     2.18
4.250    6.18    0.50      1.046  o       |  I     |        |        |     2.25
4.333    6.52    0.55      1.087  |o       |   I    |        |        |     2.32
4.417    6.85    0.60      1.129  |o       |   I    |        |        |     2.40
4.500    7.10    0.66      1.172  |o       |    I   |        |        |     2.48
4.583    7.28    0.71      1.217  |o       |    I   |        |        |     2.56
4.667    7.58    0.76      1.263  |o       |    I   |        |        |     2.65
4.750    7.91    0.82      1.311  |o       |     I  |        |        |     2.74
4.833    8.14    0.88      1.361  |o       |      I|        |        |     2.83
4.917    8.31    0.94      1.411  |o       |      I|        |        |     2.93
5.000    8.61    1.00      1.462  |o       |      I|        |        |     3.02
5.083    9.34    1.04      1.517  |o       |       |I       |        |     3.11
5.167   10.74    1.08      1.579  |o       |       |  I     |        |     3.21
5.250   12.11    1.13      1.650  | o      |       |    I   |        |     3.33
5.333   13.23    1.19      1.730  | o      |       |      I |        |     3.47
5.417   14.51    1.25      1.817  | o      |       |        | I      |     3.61
5.500   17.34    1.32      1.917  | o      |       |        |      I |     3.78
5.583   15.96    1.40      2.023  | o      |       |        |   I    |     3.96
5.667    8.34    1.44      2.097  | o      |       |      I|        |     4.07
5.750    4.88    1.46      2.132  | o      |I      |        |        |     4.13
5.833    3.23    1.46      2.150  | o  I   |       |        |        |     4.15
5.917    2.23    1.47      2.159  | o I    |       |        |        |     4.17
6.000    1.25    1.47      2.161  | o      |       |        |        |     4.17
6.083    0.68    1.47      2.157  |Io      |       |        |        |     4.16
6.167    0.24    1.46      2.150  I o      |       |        |        |     4.15
6.250    0.11    1.46      2.141  I o      |       |        |        |     4.14
6.333    0.04    1.46      2.132  I o      |       |        |        |     4.12
6.417    0.02    1.45      2.122  I o      |       |        |        |     4.11
6.500    0.00    1.45      2.112  I o      |       |        |        |     4.10
6.583    0.00    1.44      2.102  I o      |       |        |        |     4.08
6.667    0.00    1.44      2.092  I o      |       |        |        |     4.07
6.750    0.00    1.43      2.082  I o      |       |        |        |     4.05
6.833    0.00    1.43      2.072  I o      |       |        |        |     4.04
6.917    0.00    1.42      2.063  I o      |       |        |        |     4.02
7.000    0.00    1.42      2.053  I o      |       |        |        |     4.01
7.083    0.00    1.41      2.043  I o      |       |        |        |     3.99
7.167    0.00    1.41      2.033  I o      |       |        |        |     3.97
7.250    0.00    1.40      2.024  I o      |       |        |        |     3.96
7.333    0.00    1.39      2.014  I o      |       |        |        |     3.94
7.417    0.00    1.39      2.005  I o      |       |        |        |     3.93
7.500    0.00    1.38      1.995  I o      |       |        |        |     3.91
7.583    0.00    1.37      1.986  I o      |       |        |        |     3.89
7.667    0.00    1.37      1.976  I o      |       |        |        |     3.88
7.750    0.00    1.36      1.967  I o      |       |        |        |     3.86
7.833    0.00    1.35      1.957  I o      |       |        |        |     3.85
7.917    0.00    1.35      1.948  I o      |       |        |        |     3.83
8.000    0.00    1.34      1.939  I o      |       |        |        |     3.82
8.083    0.00    1.33      1.930  I o      |       |        |        |     3.80
8.167    0.00    1.33      1.921  I o      |       |        |        |     3.79
8.250    0.00    1.32      1.911  I o      |       |        |        |     3.77
8.333    0.00    1.31      1.902  I o      |       |        |        |     3.75
8.417    0.00    1.31      1.893  I o      |       |        |        |     3.74
8.500    0.00    1.30      1.884  I o      |       |        |        |     3.72
8.583    0.00    1.29      1.875  I o      |       |        |        |     3.71
8.667    0.00    1.29      1.867  I o      |       |        |        |     3.69
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8.750	0.00	1.28	1.858	I O				3.68
8.833	0.00	1.27	1.849	I O				3.67
8.917	0.00	1.27	1.840	I O				3.65
9.000	0.00	1.26	1.831	I O				3.64
9.083	0.00	1.26	1.823	I O				3.62
9.167	0.00	1.25	1.814	I O				3.61
9.250	0.00	1.24	1.806	I O				3.59
9.333	0.00	1.24	1.797	I O				3.58
9.417	0.00	1.23	1.789	I O				3.56
9.500	0.00	1.23	1.780	I O				3.55
9.583	0.00	1.22	1.772	I O				3.54
9.667	0.00	1.21	1.763	I O				3.52
9.750	0.00	1.21	1.755	I O				3.51
9.833	0.00	1.20	1.747	I O				3.49
9.917	0.00	1.20	1.738	I O				3.48
10.000	0.00	1.19	1.730	I O				3.47
10.083	0.00	1.18	1.722	I O				3.45
10.167	0.00	1.18	1.714	I O				3.44
10.250	0.00	1.17	1.706	I O				3.43
10.333	0.00	1.17	1.698	I O				3.41
10.417	0.00	1.16	1.690	I O				3.40
10.500	0.00	1.16	1.682	I O				3.39
10.583	0.00	1.15	1.674	I O				3.37
10.667	0.00	1.14	1.666	I O				3.36
10.750	0.00	1.14	1.658	I O				3.35
10.833	0.00	1.13	1.650	I O				3.33
10.917	0.00	1.13	1.642	I O				3.32
11.000	0.00	1.12	1.635	I O				3.31
11.083	0.00	1.12	1.627	I O				3.29
11.167	0.00	1.11	1.619	I O				3.28
11.250	0.00	1.11	1.612	I O				3.27
11.333	0.00	1.10	1.604	I O				3.26
11.417	0.00	1.09	1.597	I O				3.24
11.500	0.00	1.09	1.589	I O				3.23
11.583	0.00	1.08	1.582	I O				3.22
11.667	0.00	1.08	1.574	IO				3.21
11.750	0.00	1.07	1.567	IO				3.19
11.833	0.00	1.07	1.559	IO				3.18
11.917	0.00	1.06	1.552	IO				3.17
12.000	0.00	1.06	1.545	IO				3.16
12.083	0.00	1.05	1.537	IO				3.14
12.167	0.00	1.05	1.530	IO				3.13
12.250	0.00	1.04	1.523	IO				3.12
12.333	0.00	1.04	1.516	IO				3.11
12.417	0.00	1.03	1.509	IO				3.10
12.500	0.00	1.03	1.502	IO				3.08
12.583	0.00	1.02	1.495	IO				3.07
12.667	0.00	1.02	1.488	IO				3.06
12.750	0.00	1.01	1.481	IO				3.05
12.833	0.00	1.01	1.474	IO				3.04
12.917	0.00	1.00	1.467	IO				3.03
13.000	0.00	1.00	1.460	IO				3.01
13.083	0.00	0.99	1.453	IO				3.00
13.167	0.00	0.99	1.446	IO				2.99
13.250	0.00	0.98	1.439	IO				2.98
13.333	0.00	0.97	1.433	IO				2.97
13.417	0.00	0.96	1.426	IO				2.95
13.500	0.00	0.95	1.419	IO				2.94
13.583	0.00	0.95	1.413	IO				2.93
13.667	0.00	0.94	1.406	IO				2.92
13.750	0.00	0.93	1.400	IO				2.90
13.833	0.00	0.92	1.394	IO				2.89
13.917	0.00	0.91	1.387	IO				2.88
14.000	0.00	0.91	1.381	IO				2.87
14.083	0.00	0.90	1.375	IO				2.86
14.167	0.00	0.89	1.369	IO				2.85
14.250	0.00	0.88	1.362	IO				2.84
14.333	0.00	0.88	1.356	IO				2.82
14.417	0.00	0.87	1.350	IO				2.81
14.500	0.00	0.86	1.344	IO				2.80
14.583	0.00	0.86	1.339	IO				2.79
14.667	0.00	0.85	1.333	IO				2.78
14.750	0.00	0.84	1.327	IO				2.77
14.833	0.00	0.83	1.321	IO				2.76
14.917	0.00	0.83	1.315	IO				2.75
15.000	0.00	0.82	1.310	IO				2.74
15.083	0.00	0.81	1.304	IO				2.73
15.167	0.00	0.81	1.298	IO				2.72
15.250	0.00	0.80	1.293	IO				2.71
15.333	0.00	0.79	1.287	IO				2.70
15.417	0.00	0.79	1.282	IO				2.69
15.500	0.00	0.78	1.277	IO				2.68
15.583	0.00	0.77	1.271	IO				2.67
15.667	0.00	0.77	1.266	IO				2.66
15.750	0.00	0.76	1.261	IO				2.65
15.833	0.00	0.76	1.255	IO				2.64

15.917	0.00	0.75	1.250	IO					2.63
16.000	0.00	0.74	1.245	IO					2.62
16.083	0.00	0.74	1.240	IO					2.61
16.167	0.00	0.73	1.235	IO					2.60
16.250	0.00	0.72	1.230	IO					2.59
16.333	0.00	0.72	1.225	IO					2.58
16.417	0.00	0.71	1.220	IO					2.57
16.500	0.00	0.71	1.215	IO					2.56
16.583	0.00	0.70	1.210	IO					2.55
16.667	0.00	0.70	1.206	IO					2.54
16.750	0.00	0.69	1.201	IO					2.53
16.833	0.00	0.68	1.196	IO					2.53
16.917	0.00	0.68	1.191	IO					2.52
17.000	0.00	0.67	1.187	IO					2.51
17.083	0.00	0.67	1.182	IO					2.50
17.167	0.00	0.66	1.177	IO					2.49
17.250	0.00	0.66	1.173	IO					2.48
17.333	0.00	0.65	1.168	IO					2.47
17.417	0.00	0.65	1.164	IO					2.47
17.500	0.00	0.64	1.160	IO					2.46
17.583	0.00	0.63	1.155	IO					2.45
17.667	0.00	0.63	1.151	IO					2.44
17.750	0.00	0.62	1.147	IO					2.43
17.833	0.00	0.62	1.142	IO					2.43
17.917	0.00	0.61	1.138	IO					2.42
18.000	0.00	0.61	1.134	IO					2.41
18.083	0.00	0.60	1.130	IO					2.40
18.167	0.00	0.60	1.125	IO					2.39
18.250	0.00	0.59	1.121	IO					2.39
18.333	0.00	0.59	1.117	IO					2.38
18.417	0.00	0.58	1.113	IO					2.37
18.500	0.00	0.58	1.109	IO					2.36
18.583	0.00	0.57	1.105	IO					2.36
18.667	0.00	0.57	1.101	IO					2.35
18.750	0.00	0.56	1.097	IO					2.34
18.833	0.00	0.56	1.094	IO					2.33
18.917	0.00	0.56	1.090	IO					2.33
19.000	0.00	0.55	1.086	IO					2.32
19.083	0.00	0.55	1.082	IO					2.31
19.167	0.00	0.54	1.078	IO					2.31
19.250	0.00	0.54	1.075	O					2.30
19.333	0.00	0.53	1.071	O					2.29
19.417	0.00	0.53	1.067	O					2.29
19.500	0.00	0.52	1.064	O					2.28
19.583	0.00	0.52	1.060	O					2.27
19.667	0.00	0.52	1.057	O					2.27
19.750	0.00	0.51	1.053	O					2.26
19.833	0.00	0.51	1.049	O					2.25
19.917	0.00	0.50	1.046	O					2.25
20.000	0.00	0.50	1.043	O					2.24
20.083	0.00	0.49	1.039	O					2.23
20.167	0.00	0.49	1.036	O					2.23
20.250	0.00	0.49	1.032	O					2.22
20.333	0.00	0.48	1.029	O					2.21
20.417	0.00	0.48	1.026	O					2.21
20.500	0.00	0.47	1.022	O					2.20
20.583	0.00	0.47	1.019	O					2.20
20.667	0.00	0.47	1.016	O					2.19
20.750	0.00	0.46	1.013	O					2.18
20.833	0.00	0.46	1.010	O					2.18
20.917	0.00	0.46	1.006	O					2.17
21.000	0.00	0.45	1.003	O					2.17
21.083	0.00	0.45	1.000	O					2.16
21.167	0.00	0.44	0.997	O					2.15
21.250	0.00	0.44	0.994	O					2.15
21.333	0.00	0.44	0.991	O					2.14
21.417	0.00	0.43	0.988	O					2.14
21.500	0.00	0.43	0.985	O					2.13
21.583	0.00	0.43	0.982	O					2.13
21.667	0.00	0.42	0.979	O					2.12
21.750	0.00	0.42	0.976	O					2.12
21.833	0.00	0.42	0.973	O					2.11
21.917	0.00	0.41	0.971	O					2.11
22.000	0.00	0.41	0.968	O					2.10
22.083	0.00	0.41	0.965	O					2.09
22.167	0.00	0.40	0.962	O					2.09
22.250	0.00	0.40	0.959	O					2.08
22.333	0.00	0.40	0.957	O					2.08
22.417	0.00	0.39	0.954	O					2.07
22.500	0.00	0.39	0.951	O					2.07
22.583	0.00	0.39	0.949	O					2.06
22.667	0.00	0.38	0.946	O					2.06
22.750	0.00	0.38	0.943	O					2.05
22.833	0.00	0.38	0.941	O					2.05
22.917	0.00	0.37	0.938	O					2.05
23.000	0.00	0.37	0.936	O					2.04

23.083	0.00	0.37	0.933	o	|	|	|	|	2.04
23.167	0.00	0.36	0.931	o	|	|	|	|	2.03
23.250	0.00	0.36	0.928	o	|	|	|	|	2.03
23.333	0.00	0.36	0.926	o	|	|	|	|	2.02
23.417	0.00	0.35	0.923	o	|	|	|	|	2.02
23.500	0.00	0.35	0.921	o	|	|	|	|	2.01
23.583	0.00	0.35	0.918	o	|	|	|	|	2.01
23.667	0.00	0.35	0.916	o	|	|	|	|	2.00
23.750	0.00	0.34	0.914	o	|	|	|	|	2.00
23.833	0.00	0.34	0.911	o	|	|	|	|	1.99
23.917	0.00	0.34	0.909	o	|	|	|	|	1.99
24.000	0.00	0.34	0.906	o	|	|	|	|	1.98
24.083	0.00	0.34	0.904	o	|	|	|	|	1.98
24.167	0.00	0.34	0.902	o	|	|	|	|	1.97
24.250	0.00	0.34	0.899	o	|	|	|	|	1.97
24.333	0.00	0.34	0.897	o	|	|	|	|	1.96
24.417	0.00	0.34	0.895	o	|	|	|	|	1.96
24.500	0.00	0.34	0.892	o	|	|	|	|	1.96
24.583	0.00	0.34	0.890	o	|	|	|	|	1.95
24.667	0.00	0.34	0.888	o	|	|	|	|	1.95
24.750	0.00	0.34	0.885	o	|	|	|	|	1.94
24.833	0.00	0.34	0.883	o	|	|	|	|	1.94
24.917	0.00	0.34	0.881	o	|	|	|	|	1.93
25.000	0.00	0.34	0.878	o	|	|	|	|	1.93
25.083	0.00	0.33	0.876	o	|	|	|	|	1.92
25.167	0.00	0.33	0.874	o	|	|	|	|	1.92
25.250	0.00	0.33	0.872	o	|	|	|	|	1.91
25.333	0.00	0.33	0.869	o	|	|	|	|	1.91
25.417	0.00	0.33	0.867	o	|	|	|	|	1.90
25.500	0.00	0.33	0.865	o	|	|	|	|	1.90
25.583	0.00	0.33	0.862	o	|	|	|	|	1.89
25.667	0.00	0.33	0.860	o	|	|	|	|	1.89
25.750	0.00	0.33	0.858	o	|	|	|	|	1.88
25.833	0.00	0.33	0.856	o	|	|	|	|	1.88
25.917	0.00	0.33	0.853	o	|	|	|	|	1.87
26.000	0.00	0.33	0.851	o	|	|	|	|	1.87
26.083	0.00	0.33	0.849	o	|	|	|	|	1.86
26.167	0.00	0.33	0.846	o	|	|	|	|	1.86
26.250	0.00	0.33	0.844	o	|	|	|	|	1.86
26.333	0.00	0.33	0.842	o	|	|	|	|	1.85
26.417	0.00	0.33	0.840	o	|	|	|	|	1.85
26.500	0.00	0.33	0.838	o	|	|	|	|	1.84
26.583	0.00	0.32	0.835	o	|	|	|	|	1.84
26.667	0.00	0.32	0.833	o	|	|	|	|	1.83
26.750	0.00	0.32	0.831	o	|	|	|	|	1.83
26.833	0.00	0.32	0.829	o	|	|	|	|	1.82
26.917	0.00	0.32	0.826	o	|	|	|	|	1.82
27.000	0.00	0.32	0.824	o	|	|	|	|	1.81
27.083	0.00	0.32	0.822	o	|	|	|	|	1.81
27.167	0.00	0.32	0.820	o	|	|	|	|	1.80
27.250	0.00	0.32	0.818	o	|	|	|	|	1.80
27.333	0.00	0.32	0.815	o	|	|	|	|	1.80
27.417	0.00	0.32	0.813	o	|	|	|	|	1.79
27.500	0.00	0.32	0.811	o	|	|	|	|	1.79
27.583	0.00	0.32	0.809	o	|	|	|	|	1.78
27.667	0.00	0.32	0.807	o	|	|	|	|	1.78
27.750	0.00	0.32	0.804	o	|	|	|	|	1.77
27.833	0.00	0.32	0.802	o	|	|	|	|	1.77
27.917	0.00	0.32	0.800	o	|	|	|	|	1.76
28.000	0.00	0.32	0.798	o	|	|	|	|	1.76
28.083	0.00	0.31	0.796	o	|	|	|	|	1.75
28.167	0.00	0.31	0.793	o	|	|	|	|	1.75
28.250	0.00	0.31	0.791	o	|	|	|	|	1.75
28.333	0.00	0.31	0.789	o	|	|	|	|	1.74
28.417	0.00	0.31	0.787	o	|	|	|	|	1.74
28.500	0.00	0.31	0.785	o	|	|	|	|	1.73
28.583	0.00	0.31	0.783	o	|	|	|	|	1.73
28.667	0.00	0.31	0.781	o	|	|	|	|	1.72
28.750	0.00	0.31	0.778	o	|	|	|	|	1.72
28.833	0.00	0.31	0.776	o	|	|	|	|	1.71
28.917	0.00	0.31	0.774	o	|	|	|	|	1.71
29.000	0.00	0.31	0.772	o	|	|	|	|	1.71
29.083	0.00	0.31	0.770	o	|	|	|	|	1.70
29.167	0.00	0.31	0.768	o	|	|	|	|	1.70
29.250	0.00	0.31	0.766	o	|	|	|	|	1.69
29.333	0.00	0.31	0.764	o	|	|	|	|	1.69
29.417	0.00	0.31	0.761	o	|	|	|	|	1.68
29.500	0.00	0.31	0.759	o	|	|	|	|	1.68
29.583	0.00	0.31	0.757	o	|	|	|	|	1.68
29.667	0.00	0.30	0.755	o	|	|	|	|	1.67
29.750	0.00	0.30	0.753	o	|	|	|	|	1.67
29.833	0.00	0.30	0.751	o	|	|	|	|	1.66
29.917	0.00	0.30	0.749	o	|	|	|	|	1.66
30.000	0.00	0.30	0.747	o	|	|	|	|	1.65
30.083	0.00	0.30	0.745	o	|	|	|	|	1.65
30.167	0.00	0.30	0.743	o	|	|	|	|	1.65

30.250	0.00	0.30	0.740	o	|	|	|	|	1.64
30.333	0.00	0.30	0.738	o	|	|	|	|	1.64
30.417	0.00	0.30	0.736	o	|	|	|	|	1.63
30.500	0.00	0.30	0.734	o	|	|	|	|	1.63
30.583	0.00	0.30	0.732	o	|	|	|	|	1.62
30.667	0.00	0.30	0.730	o	|	|	|	|	1.62
30.750	0.00	0.30	0.728	o	|	|	|	|	1.62
30.833	0.00	0.30	0.726	o	|	|	|	|	1.61
30.917	0.00	0.30	0.724	o	|	|	|	|	1.61
31.000	0.00	0.30	0.722	o	|	|	|	|	1.60
31.083	0.00	0.30	0.720	o	|	|	|	|	1.60
31.167	0.00	0.30	0.718	o	|	|	|	|	1.59
31.250	0.00	0.30	0.716	o	|	|	|	|	1.59
31.333	0.00	0.29	0.714	o	|	|	|	|	1.59
31.417	0.00	0.29	0.712	o	|	|	|	|	1.58
31.500	0.00	0.29	0.710	o	|	|	|	|	1.58
31.583	0.00	0.29	0.708	o	|	|	|	|	1.57
31.667	0.00	0.29	0.706	o	|	|	|	|	1.57
31.750	0.00	0.29	0.704	o	|	|	|	|	1.56
31.833	0.00	0.29	0.702	o	|	|	|	|	1.56
31.917	0.00	0.29	0.700	o	|	|	|	|	1.56
32.000	0.00	0.29	0.698	o	|	|	|	|	1.55
32.083	0.00	0.29	0.696	o	|	|	|	|	1.55
32.167	0.00	0.29	0.694	o	|	|	|	|	1.54
32.250	0.00	0.29	0.692	o	|	|	|	|	1.54
32.333	0.00	0.29	0.690	o	|	|	|	|	1.54
32.417	0.00	0.29	0.688	o	|	|	|	|	1.53
32.500	0.00	0.29	0.686	o	|	|	|	|	1.53
32.583	0.00	0.29	0.684	o	|	|	|	|	1.52
32.667	0.00	0.29	0.682	o	|	|	|	|	1.52
32.750	0.00	0.29	0.680	o	|	|	|	|	1.52
32.833	0.00	0.29	0.678	o	|	|	|	|	1.51
32.917	0.00	0.29	0.676	o	|	|	|	|	1.51
33.000	0.00	0.28	0.674	o	|	|	|	|	1.50
33.083	0.00	0.28	0.672	o	|	|	|	|	1.50
33.167	0.00	0.28	0.670	o	|	|	|	|	1.49
33.250	0.00	0.28	0.668	o	|	|	|	|	1.49
33.333	0.00	0.28	0.666	o	|	|	|	|	1.49
33.417	0.00	0.28	0.664	o	|	|	|	|	1.48
33.500	0.00	0.28	0.662	o	|	|	|	|	1.48
33.583	0.00	0.28	0.660	o	|	|	|	|	1.47
33.667	0.00	0.28	0.658	o	|	|	|	|	1.47
33.750	0.00	0.28	0.656	o	|	|	|	|	1.47
33.833	0.00	0.28	0.654	o	|	|	|	|	1.46
33.917	0.00	0.28	0.653	o	|	|	|	|	1.46
34.000	0.00	0.28	0.651	o	|	|	|	|	1.45
34.083	0.00	0.28	0.649	o	|	|	|	|	1.45
34.167	0.00	0.28	0.647	o	|	|	|	|	1.45
34.250	0.00	0.28	0.645	o	|	|	|	|	1.44
34.333	0.00	0.28	0.643	o	|	|	|	|	1.44
34.417	0.00	0.28	0.641	o	|	|	|	|	1.43
34.500	0.00	0.28	0.639	o	|	|	|	|	1.43
34.583	0.00	0.28	0.637	o	|	|	|	|	1.43
34.667	0.00	0.28	0.635	o	|	|	|	|	1.42
34.750	0.00	0.27	0.633	o	|	|	|	|	1.42
34.833	0.00	0.27	0.632	o	|	|	|	|	1.42
34.917	0.00	0.27	0.630	o	|	|	|	|	1.41
35.000	0.00	0.27	0.628	o	|	|	|	|	1.41
35.083	0.00	0.27	0.626	o	|	|	|	|	1.40
35.167	0.00	0.27	0.624	o	|	|	|	|	1.40
35.250	0.00	0.27	0.622	o	|	|	|	|	1.40
35.333	0.00	0.27	0.620	o	|	|	|	|	1.39
35.417	0.00	0.27	0.618	o	|	|	|	|	1.39
35.500	0.00	0.27	0.617	o	|	|	|	|	1.38
35.583	0.00	0.27	0.615	o	|	|	|	|	1.38
35.667	0.00	0.27	0.613	o	|	|	|	|	1.38
35.750	0.00	0.27	0.611	o	|	|	|	|	1.37
35.833	0.00	0.27	0.609	o	|	|	|	|	1.37
35.917	0.00	0.27	0.607	o	|	|	|	|	1.36
36.000	0.00	0.27	0.605	o	|	|	|	|	1.36
36.083	0.00	0.27	0.604	o	|	|	|	|	1.36
36.167	0.00	0.27	0.602	o	|	|	|	|	1.35
36.250	0.00	0.27	0.600	o	|	|	|	|	1.35
36.333	0.00	0.27	0.598	o	|	|	|	|	1.35
36.417	0.00	0.27	0.596	o	|	|	|	|	1.34
36.500	0.00	0.27	0.594	o	|	|	|	|	1.34
36.583	0.00	0.26	0.593	o	|	|	|	|	1.33
36.667	0.00	0.26	0.591	o	|	|	|	|	1.33
36.750	0.00	0.26	0.589	o	|	|	|	|	1.33
36.833	0.00	0.26	0.587	o	|	|	|	|	1.32
36.917	0.00	0.26	0.585	o	|	|	|	|	1.32
37.000	0.00	0.26	0.583	o	|	|	|	|	1.32
37.083	0.00	0.26	0.582	o	|	|	|	|	1.31
37.167	0.00	0.26	0.580	o	|	|	|	|	1.31
37.250	0.00	0.26	0.578	o	|	|	|	|	1.30
37.333	0.00	0.26	0.576	o	|	|	|	|	1.30

37.417	0.00	0.26	0.574	o	|	|	|	|	1.30
37.500	0.00	0.26	0.573	o	|	|	|	|	1.29
37.583	0.00	0.26	0.571	o	|	|	|	|	1.29
37.667	0.00	0.26	0.569	o	|	|	|	|	1.29
37.750	0.00	0.26	0.567	o	|	|	|	|	1.28
37.833	0.00	0.26	0.566	o	|	|	|	|	1.28
37.917	0.00	0.26	0.564	o	|	|	|	|	1.27
38.000	0.00	0.26	0.562	o	|	|	|	|	1.27
38.083	0.00	0.26	0.560	o	|	|	|	|	1.27
38.167	0.00	0.26	0.558	o	|	|	|	|	1.26
38.250	0.00	0.26	0.557	o	|	|	|	|	1.26
38.333	0.00	0.26	0.555	o	|	|	|	|	1.26
38.417	0.00	0.26	0.553	o	|	|	|	|	1.25
38.500	0.00	0.25	0.551	o	|	|	|	|	1.25
38.583	0.00	0.25	0.550	o	|	|	|	|	1.25
38.667	0.00	0.25	0.548	o	|	|	|	|	1.24
38.750	0.00	0.25	0.546	o	|	|	|	|	1.24
38.833	0.00	0.25	0.544	o	|	|	|	|	1.23
38.917	0.00	0.25	0.543	o	|	|	|	|	1.23
39.000	0.00	0.25	0.541	o	|	|	|	|	1.23
39.083	0.00	0.25	0.539	o	|	|	|	|	1.22
39.167	0.00	0.25	0.537	o	|	|	|	|	1.22
39.250	0.00	0.25	0.536	o	|	|	|	|	1.22
39.333	0.00	0.25	0.534	o	|	|	|	|	1.21
39.417	0.00	0.25	0.532	o	|	|	|	|	1.21
39.500	0.00	0.25	0.531	o	|	|	|	|	1.21
39.583	0.00	0.25	0.529	o	|	|	|	|	1.20
39.667	0.00	0.25	0.527	o	|	|	|	|	1.20
39.750	0.00	0.25	0.525	o	|	|	|	|	1.20
39.833	0.00	0.25	0.524	o	|	|	|	|	1.19
39.917	0.00	0.25	0.522	o	|	|	|	|	1.19
40.000	0.00	0.25	0.520	o	|	|	|	|	1.18
40.083	0.00	0.25	0.519	o	|	|	|	|	1.18
40.167	0.00	0.25	0.517	o	|	|	|	|	1.18
40.250	0.00	0.25	0.515	o	|	|	|	|	1.17
40.333	0.00	0.25	0.514	o	|	|	|	|	1.17
40.417	0.00	0.24	0.512	o	|	|	|	|	1.17
40.500	0.00	0.24	0.510	o	|	|	|	|	1.16
40.583	0.00	0.24	0.508	o	|	|	|	|	1.16
40.667	0.00	0.24	0.507	o	|	|	|	|	1.16
40.750	0.00	0.24	0.505	o	|	|	|	|	1.15
40.833	0.00	0.24	0.503	o	|	|	|	|	1.15
40.917	0.00	0.24	0.502	o	|	|	|	|	1.15
41.000	0.00	0.24	0.500	o	|	|	|	|	1.14
41.083	0.00	0.24	0.498	o	|	|	|	|	1.14
41.167	0.00	0.24	0.497	o	|	|	|	|	1.14
41.250	0.00	0.24	0.495	o	|	|	|	|	1.13
41.333	0.00	0.24	0.493	o	|	|	|	|	1.13
41.417	0.00	0.24	0.492	o	|	|	|	|	1.13
41.500	0.00	0.24	0.490	o	|	|	|	|	1.12
41.583	0.00	0.24	0.489	o	|	|	|	|	1.12
41.667	0.00	0.24	0.487	o	|	|	|	|	1.12
41.750	0.00	0.24	0.485	o	|	|	|	|	1.11
41.833	0.00	0.24	0.484	o	|	|	|	|	1.11
41.917	0.00	0.24	0.482	o	|	|	|	|	1.11
42.000	0.00	0.24	0.480	o	|	|	|	|	1.10
42.083	0.00	0.24	0.479	o	|	|	|	|	1.10
42.167	0.00	0.24	0.477	o	|	|	|	|	1.10
42.250	0.00	0.24	0.475	o	|	|	|	|	1.09
42.333	0.00	0.24	0.474	o	|	|	|	|	1.09
42.417	0.00	0.24	0.472	o	|	|	|	|	1.09
42.500	0.00	0.23	0.471	o	|	|	|	|	1.08
42.583	0.00	0.23	0.469	o	|	|	|	|	1.08
42.667	0.00	0.23	0.467	o	|	|	|	|	1.08
42.750	0.00	0.23	0.466	o	|	|	|	|	1.07
42.833	0.00	0.23	0.464	o	|	|	|	|	1.07
42.917	0.00	0.23	0.463	o	|	|	|	|	1.07
43.000	0.00	0.23	0.461	o	|	|	|	|	1.06
43.083	0.00	0.23	0.459	o	|	|	|	|	1.06
43.167	0.00	0.23	0.458	o	|	|	|	|	1.06
43.250	0.00	0.23	0.456	o	|	|	|	|	1.05
43.333	0.00	0.23	0.455	o	|	|	|	|	1.05
43.417	0.00	0.23	0.453	o	|	|	|	|	1.05
43.500	0.00	0.23	0.451	o	|	|	|	|	1.04
43.583	0.00	0.23	0.450	o	|	|	|	|	1.04
43.667	0.00	0.23	0.448	o	|	|	|	|	1.04
43.750	0.00	0.23	0.447	o	|	|	|	|	1.03
43.833	0.00	0.23	0.445	o	|	|	|	|	1.03
43.917	0.00	0.23	0.443	o	|	|	|	|	1.03
44.000	0.00	0.23	0.442	o	|	|	|	|	1.02
44.083	0.00	0.23	0.440	o	|	|	|	|	1.02
44.167	0.00	0.23	0.439	o	|	|	|	|	1.02
44.250	0.00	0.23	0.437	o	|	|	|	|	1.01
44.333	0.00	0.23	0.436	o	|	|	|	|	1.01
44.417	0.00	0.23	0.434	o	|	|	|	|	1.01
44.500	0.00	0.23	0.433	o	|	|	|	|	1.00

44.583	0.00	0.22	0.431	o	|	|	|	|	1.00
44.667	0.00	0.22	0.429	o	|	|	|	|	1.00
44.750	0.00	0.22	0.428	o	|	|	|	|	0.99
44.833	0.00	0.22	0.426	o	|	|	|	|	0.99
44.917	0.00	0.22	0.425	o	|	|	|	|	0.99
45.000	0.00	0.22	0.423	o	|	|	|	|	0.98
45.083	0.00	0.22	0.422	o	|	|	|	|	0.98
45.167	0.00	0.22	0.420	o	|	|	|	|	0.98
45.250	0.00	0.22	0.419	o	|	|	|	|	0.97
45.333	0.00	0.22	0.417	o	|	|	|	|	0.97
45.417	0.00	0.22	0.416	o	|	|	|	|	0.96
45.500	0.00	0.22	0.414	o	|	|	|	|	0.96
45.583	0.00	0.22	0.413	o	|	|	|	|	0.96
45.667	0.00	0.21	0.411	o	|	|	|	|	0.95
45.750	0.00	0.21	0.410	o	|	|	|	|	0.95
45.833	0.00	0.21	0.408	o	|	|	|	|	0.95
45.917	0.00	0.21	0.407	o	|	|	|	|	0.94
46.000	0.00	0.21	0.405	o	|	|	|	|	0.94
46.083	0.00	0.21	0.404	o	|	|	|	|	0.94
46.167	0.00	0.21	0.403	o	|	|	|	|	0.93
46.250	0.00	0.21	0.401	o	|	|	|	|	0.93
46.333	0.00	0.21	0.400	o	|	|	|	|	0.93
46.417	0.00	0.21	0.398	o	|	|	|	|	0.92
46.500	0.00	0.21	0.397	o	|	|	|	|	0.92
46.583	0.00	0.21	0.395	o	|	|	|	|	0.92
46.667	0.00	0.21	0.394	o	|	|	|	|	0.91
46.750	0.00	0.20	0.393	o	|	|	|	|	0.91
46.833	0.00	0.20	0.391	o	|	|	|	|	0.91
46.917	0.00	0.20	0.390	o	|	|	|	|	0.90
47.000	0.00	0.20	0.388	o	|	|	|	|	0.90
47.083	0.00	0.20	0.387	o	|	|	|	|	0.90
47.167	0.00	0.20	0.386	o	|	|	|	|	0.89
47.250	0.00	0.20	0.384	o	|	|	|	|	0.89
47.333	0.00	0.20	0.383	o	|	|	|	|	0.89
47.417	0.00	0.20	0.381	o	|	|	|	|	0.88
47.500	0.00	0.20	0.380	o	|	|	|	|	0.88
47.583	0.00	0.20	0.379	o	|	|	|	|	0.88
47.667	0.00	0.20	0.377	o	|	|	|	|	0.88
47.750	0.00	0.20	0.376	o	|	|	|	|	0.87
47.833	0.00	0.20	0.375	o	|	|	|	|	0.87
47.917	0.00	0.19	0.373	o	|	|	|	|	0.87
48.000	0.00	0.19	0.372	o	|	|	|	|	0.86
48.083	0.00	0.19	0.371	o	|	|	|	|	0.86
48.167	0.00	0.19	0.369	o	|	|	|	|	0.86
48.250	0.00	0.19	0.368	o	|	|	|	|	0.85
48.333	0.00	0.19	0.367	o	|	|	|	|	0.85
48.417	0.00	0.19	0.365	o	|	|	|	|	0.85
48.500	0.00	0.19	0.364	o	|	|	|	|	0.84
48.583	0.00	0.19	0.363	o	|	|	|	|	0.84
48.667	0.00	0.19	0.361	o	|	|	|	|	0.84
48.750	0.00	0.19	0.360	o	|	|	|	|	0.84
48.833	0.00	0.19	0.359	o	|	|	|	|	0.83
48.917	0.00	0.19	0.357	o	|	|	|	|	0.83
49.000	0.00	0.19	0.356	o	|	|	|	|	0.83
49.083	0.00	0.19	0.355	o	|	|	|	|	0.82
49.167	0.00	0.18	0.354	o	|	|	|	|	0.82
49.250	0.00	0.18	0.352	o	|	|	|	|	0.82
49.333	0.00	0.18	0.351	o	|	|	|	|	0.81
49.417	0.00	0.18	0.350	o	|	|	|	|	0.81
49.500	0.00	0.18	0.349	o	|	|	|	|	0.81
49.583	0.00	0.18	0.347	o	|	|	|	|	0.81
49.667	0.00	0.18	0.346	o	|	|	|	|	0.80
49.750	0.00	0.18	0.345	o	|	|	|	|	0.80
49.833	0.00	0.18	0.344	o	|	|	|	|	0.80
49.917	0.00	0.18	0.342	o	|	|	|	|	0.79
50.000	0.00	0.18	0.341	o	|	|	|	|	0.79
50.083	0.00	0.18	0.340	o	|	|	|	|	0.79
50.167	0.00	0.18	0.339	o	|	|	|	|	0.79
50.250	0.00	0.18	0.338	o	|	|	|	|	0.78
50.333	0.00	0.18	0.336	o	|	|	|	|	0.78
50.417	0.00	0.17	0.335	o	|	|	|	|	0.78
50.500	0.00	0.17	0.334	o	|	|	|	|	0.77
50.583	0.00	0.17	0.333	o	|	|	|	|	0.77
50.667	0.00	0.17	0.331	o	|	|	|	|	0.77
50.750	0.00	0.17	0.330	o	|	|	|	|	0.77
50.833	0.00	0.17	0.329	o	|	|	|	|	0.76
50.917	0.00	0.17	0.328	o	|	|	|	|	0.76
51.000	0.00	0.17	0.327	o	|	|	|	|	0.76
51.083	0.00	0.17	0.326	o	|	|	|	|	0.76
51.167	0.00	0.17	0.324	o	|	|	|	|	0.75
51.250	0.00	0.17	0.323	o	|	|	|	|	0.75
51.333	0.00	0.17	0.322	o	|	|	|	|	0.75
51.417	0.00	0.17	0.321	o	|	|	|	|	0.74
51.500	0.00	0.17	0.320	o	|	|	|	|	0.74
51.583	0.00	0.17	0.319	o	|	|	|	|	0.74
51.667	0.00	0.17	0.317	o	|	|	|	|	0.74

51.750	0.00	0.17	0.316	o	|	|	|	|	0.73
51.833	0.00	0.16	0.315	o	|	|	|	|	0.73
51.917	0.00	0.16	0.314	o	|	|	|	|	0.73
52.000	0.00	0.16	0.313	o	|	|	|	|	0.73
52.083	0.00	0.16	0.312	o	|	|	|	|	0.72
52.167	0.00	0.16	0.311	o	|	|	|	|	0.72
52.250	0.00	0.16	0.310	o	|	|	|	|	0.72
52.333	0.00	0.16	0.308	o	|	|	|	|	0.72
52.417	0.00	0.16	0.307	o	|	|	|	|	0.71
52.500	0.00	0.16	0.306	o	|	|	|	|	0.71
52.583	0.00	0.16	0.305	o	|	|	|	|	0.71
52.667	0.00	0.16	0.304	o	|	|	|	|	0.71
52.750	0.00	0.16	0.303	o	|	|	|	|	0.70
52.833	0.00	0.16	0.302	o	|	|	|	|	0.70
52.917	0.00	0.16	0.301	o	|	|	|	|	0.70
53.000	0.00	0.16	0.300	o	|	|	|	|	0.70
53.083	0.00	0.16	0.299	o	|	|	|	|	0.69
53.167	0.00	0.16	0.298	o	|	|	|	|	0.69
53.250	0.00	0.15	0.297	o	|	|	|	|	0.69
53.333	0.00	0.15	0.295	o	|	|	|	|	0.69
53.417	0.00	0.15	0.294	o	|	|	|	|	0.68
53.500	0.00	0.15	0.293	o	|	|	|	|	0.68
53.583	0.00	0.15	0.292	o	|	|	|	|	0.68
53.667	0.00	0.15	0.291	o	|	|	|	|	0.68
53.750	0.00	0.15	0.290	o	|	|	|	|	0.67
53.833	0.00	0.15	0.289	o	|	|	|	|	0.67
53.917	0.00	0.15	0.288	o	|	|	|	|	0.67
54.000	0.00	0.15	0.287	o	|	|	|	|	0.67
54.083	0.00	0.15	0.286	o	|	|	|	|	0.66
54.167	0.00	0.15	0.285	o	|	|	|	|	0.66
54.250	0.00	0.15	0.284	o	|	|	|	|	0.66
54.333	0.00	0.15	0.283	o	|	|	|	|	0.66
54.417	0.00	0.15	0.282	o	|	|	|	|	0.65
54.500	0.00	0.15	0.281	o	|	|	|	|	0.65
54.583	0.00	0.15	0.280	o	|	|	|	|	0.65
54.667	0.00	0.15	0.279	o	|	|	|	|	0.65
54.750	0.00	0.15	0.278	o	|	|	|	|	0.64
54.833	0.00	0.14	0.277	o	|	|	|	|	0.64
54.917	0.00	0.14	0.276	o	|	|	|	|	0.64
55.000	0.00	0.14	0.275	o	|	|	|	|	0.64
55.083	0.00	0.14	0.274	o	|	|	|	|	0.64
55.167	0.00	0.14	0.273	o	|	|	|	|	0.63
55.250	0.00	0.14	0.272	o	|	|	|	|	0.63
55.333	0.00	0.14	0.271	o	|	|	|	|	0.63
55.417	0.00	0.14	0.270	o	|	|	|	|	0.63
55.500	0.00	0.14	0.269	o	|	|	|	|	0.62
55.583	0.00	0.14	0.268	o	|	|	|	|	0.62
55.667	0.00	0.14	0.267	o	|	|	|	|	0.62
55.750	0.00	0.14	0.266	o	|	|	|	|	0.62
55.833	0.00	0.14	0.265	o	|	|	|	|	0.62
55.917	0.00	0.14	0.264	o	|	|	|	|	0.61
56.000	0.00	0.14	0.263	o	|	|	|	|	0.61
56.083	0.00	0.14	0.262	o	|	|	|	|	0.61
56.167	0.00	0.14	0.261	o	|	|	|	|	0.61
56.250	0.00	0.14	0.261	o	|	|	|	|	0.60
56.333	0.00	0.14	0.260	o	|	|	|	|	0.60
56.417	0.00	0.14	0.259	o	|	|	|	|	0.60
56.500	0.00	0.13	0.258	o	|	|	|	|	0.60
56.583	0.00	0.13	0.257	o	|	|	|	|	0.60
56.667	0.00	0.13	0.256	o	|	|	|	|	0.59
56.750	0.00	0.13	0.255	o	|	|	|	|	0.59
56.833	0.00	0.13	0.254	o	|	|	|	|	0.59
56.917	0.00	0.13	0.253	o	|	|	|	|	0.59
57.000	0.00	0.13	0.252	o	|	|	|	|	0.59
57.083	0.00	0.13	0.251	o	|	|	|	|	0.58
57.167	0.00	0.13	0.250	o	|	|	|	|	0.58
57.250	0.00	0.13	0.250	o	|	|	|	|	0.58
57.333	0.00	0.13	0.249	o	|	|	|	|	0.58
57.417	0.00	0.13	0.248	o	|	|	|	|	0.57
57.500	0.00	0.13	0.247	o	|	|	|	|	0.57
57.583	0.00	0.13	0.246	o	|	|	|	|	0.57
57.667	0.00	0.13	0.245	o	|	|	|	|	0.57
57.750	0.00	0.13	0.244	o	|	|	|	|	0.57
57.833	0.00	0.13	0.243	o	|	|	|	|	0.56
57.917	0.00	0.13	0.242	o	|	|	|	|	0.56
58.000	0.00	0.13	0.242	o	|	|	|	|	0.56
58.083	0.00	0.13	0.241	o	|	|	|	|	0.56
58.167	0.00	0.13	0.240	o	|	|	|	|	0.56
58.250	0.00	0.12	0.239	o	|	|	|	|	0.55
58.333	0.00	0.12	0.238	o	|	|	|	|	0.55
58.417	0.00	0.12	0.237	o	|	|	|	|	0.55
58.500	0.00	0.12	0.236	o	|	|	|	|	0.55
58.583	0.00	0.12	0.236	o	|	|	|	|	0.55
58.667	0.00	0.12	0.235	o	|	|	|	|	0.54
58.750	0.00	0.12	0.234	o	|	|	|	|	0.54
58.833	0.00	0.12	0.233	o	|	|	|	|	0.54

58.917	0.00	0.12	0.232	o	|	|	|	|	0.54
59.000	0.00	0.12	0.231	o	|	|	|	|	0.54
59.083	0.00	0.12	0.231	o	|	|	|	|	0.53
59.167	0.00	0.12	0.230	o	|	|	|	|	0.53
59.250	0.00	0.12	0.229	o	|	|	|	|	0.53
59.333	0.00	0.12	0.228	o	|	|	|	|	0.53
59.417	0.00	0.12	0.227	o	|	|	|	|	0.53
59.500	0.00	0.12	0.226	o	|	|	|	|	0.53
59.583	0.00	0.12	0.226	o	|	|	|	|	0.52
59.667	0.00	0.12	0.225	o	|	|	|	|	0.52
59.750	0.00	0.12	0.224	o	|	|	|	|	0.52
59.833	0.00	0.12	0.223	o	|	|	|	|	0.52
59.917	0.00	0.12	0.222	o	|	|	|	|	0.52
60.000	0.00	0.12	0.222	o	|	|	|	|	0.51
60.083	0.00	0.12	0.221	o	|	|	|	|	0.51
60.167	0.00	0.11	0.220	o	|	|	|	|	0.51
60.250	0.00	0.11	0.219	o	|	|	|	|	0.51
60.333	0.00	0.11	0.218	o	|	|	|	|	0.51
60.417	0.00	0.11	0.218	o	|	|	|	|	0.51
60.500	0.00	0.11	0.217	o	|	|	|	|	0.50
60.583	0.00	0.11	0.216	o	|	|	|	|	0.50
60.667	0.00	0.11	0.215	o	|	|	|	|	0.50
60.750	0.00	0.11	0.215	o	|	|	|	|	0.50
60.833	0.00	0.11	0.214	o	|	|	|	|	0.50
60.917	0.00	0.11	0.213	o	|	|	|	|	0.49
61.000	0.00	0.11	0.212	o	|	|	|	|	0.49
61.083	0.00	0.11	0.211	o	|	|	|	|	0.49
61.167	0.00	0.11	0.211	o	|	|	|	|	0.49
61.250	0.00	0.11	0.210	o	|	|	|	|	0.49
61.333	0.00	0.11	0.209	o	|	|	|	|	0.49
61.417	0.00	0.11	0.208	o	|	|	|	|	0.48
61.500	0.00	0.11	0.208	o	|	|	|	|	0.48
61.583	0.00	0.11	0.207	o	|	|	|	|	0.48
61.667	0.00	0.11	0.206	o	|	|	|	|	0.48
61.750	0.00	0.11	0.205	o	|	|	|	|	0.48
61.833	0.00	0.11	0.205	o	|	|	|	|	0.48
61.917	0.00	0.11	0.204	o	|	|	|	|	0.47
62.000	0.00	0.11	0.203	o	|	|	|	|	0.47
62.083	0.00	0.11	0.203	o	|	|	|	|	0.47
62.167	0.00	0.11	0.202	o	|	|	|	|	0.47
62.250	0.00	0.10	0.201	o	|	|	|	|	0.47
62.333	0.00	0.10	0.200	o	|	|	|	|	0.46
62.417	0.00	0.10	0.200	o	|	|	|	|	0.46
62.500	0.00	0.10	0.199	o	|	|	|	|	0.46
62.583	0.00	0.10	0.198	o	|	|	|	|	0.46
62.667	0.00	0.10	0.198	o	|	|	|	|	0.46
62.750	0.00	0.10	0.197	o	|	|	|	|	0.46
62.833	0.00	0.10	0.196	o	|	|	|	|	0.46
62.917	0.00	0.10	0.195	o	|	|	|	|	0.45
63.000	0.00	0.10	0.195	o	|	|	|	|	0.45
63.083	0.00	0.10	0.194	o	|	|	|	|	0.45
63.167	0.00	0.10	0.193	o	|	|	|	|	0.45
63.250	0.00	0.10	0.193	o	|	|	|	|	0.45
63.333	0.00	0.10	0.192	o	|	|	|	|	0.45
63.417	0.00	0.10	0.191	o	|	|	|	|	0.44

Remaining water in basin = 0.19 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 761
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.470 (CFS)
Total volume = 2.202 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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                FLOOD HYDROGRAPH ROUTING PROGRAM
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                      Study date: 06/03/24

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: pro22242.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =   293
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =        6.393 (CFS)
               Total volume =       3.885 (Ac.Ft)
       Status of hydrographs being held in storage
                  Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
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Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
___________________________________________________________________________

User entry of depth-outflow-storage data
---------------------------------------------------------------------
Total number of inflow hydrograph intervals = 293
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
---------------------------------------------------------------------
---------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
---------------------------------------------------------------------
---------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
---------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.431      0.225      0.430        0.432
   2.000      0.914      0.344      0.913        0.915
   3.000      1.451      0.991      1.448        1.454
   4.000      2.049      1.417      2.044        2.054
   5.000      2.712      1.731      2.706        2.718
   5.250      2.888      1.801      2.882        2.894
   5.500      3.069     17.046      3.010        3.128
   6.000      3.443    225.078      2.668        4.218
---------------------------------------------------------------------
               Hydrograph Detention Basin Routing
---------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
---------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                  Depth
(Hours) (CFS)   (CFS)     (Ac.Ft) .0       1.6    3.20    4.79    6.39 (Ft.)
 0.083    0.11    0.00      0.000  O       |       |       |       |     0.00
 0.167    0.29    0.00      0.002  OI      |       |       |       |     0.00
 0.250    0.34    0.00      0.004  OI      |       |       |       |     0.01
 0.333    0.41    0.00      0.006  O I     |       |       |       |     0.01
 0.417    0.51    0.01      0.010  O I     |       |       |       |     0.02
 0.500    0.54    0.01      0.013  O I     |       |       |       |     0.03
 0.583    0.55    0.01      0.017  O I     |       |       |       |     0.04
 0.667    0.56    0.01      0.021  O I     |       |       |       |     0.05
 0.750    0.56    0.01      0.025  O I     |       |       |       |     0.06
 0.833    0.62    0.01      0.028  O  I    |       |       |       |     0.07
 0.917    0.71    0.02      0.033  O  I    |       |       |       |     0.08
 1.000    0.73    0.02      0.038  O  I    |       |       |       |     0.09
 1.083    0.69    0.02      0.043  O  I    |       |       |       |     0.10
 1.167    0.60    0.02      0.047  O  I    |       |       |       |     0.11
 1.250    0.58    0.03      0.051  O I     |       |       |       |     0.12
 1.333    0.57    0.03      0.055  O I     |       |       |       |     0.13
 1.417    0.57    0.03      0.058  O I     |       |       |       |     0.14
 1.500    0.56    0.03      0.062  O I     |       |       |       |     0.14
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1.583    0.56    0.03      0.066  o I     |       |       |       |      0.15
1.667    0.56    0.04      0.069  o I     |       |       |       |      0.16
1.750    0.56    0.04      0.073  o I     |       |       |       |      0.17
1.833    0.62    0.04      0.077  o  I    |       |       |       |      0.18
1.917    0.71    0.04      0.081  o  I    |       |       |       |      0.19
2.000    0.73    0.04      0.086  o  I    |       |       |       |      0.20
2.083    0.74    0.05      0.090  o  I    |       |       |       |      0.21
2.167    0.75    0.05      0.095  o  I    |       |       |       |      0.22
2.250    0.75    0.05      0.100  o  I    |       |       |       |      0.23
2.333    0.75    0.05      0.105  o  I    |       |       |       |      0.24
2.417    0.75    0.06      0.110  o  I    |       |       |       |      0.25
2.500    0.75    0.06      0.114  o  I    |       |       |       |      0.27
2.583    0.81    0.06      0.119  o   I   |       |       |       |      0.28
2.667    0.90    0.07      0.125  o   I   |       |       |       |      0.29
2.750    0.92    0.07      0.131  o   I   |       |       |       |      0.30
2.833    0.93    0.07      0.136  o   I   |       |       |       |      0.32
2.917    0.94    0.07      0.142  o   I   |       |       |       |      0.33
3.000    0.94    0.08      0.148  o   I   |       |       |       |      0.34
3.083    0.94    0.08      0.154  o   I   |       |       |       |      0.36
3.167    0.94    0.08      0.160  o   I   |       |       |       |      0.37
3.250    0.94    0.09      0.166  o   I   |       |       |       |      0.39
3.333    0.94    0.09      0.172  o   I   |       |       |       |      0.40
3.417    0.94    0.09      0.178  o   I   |       |       |       |      0.41
3.500    0.94    0.10      0.184  o   I   |       |       |       |      0.43
3.583    0.94    0.10      0.189  o   I   |       |       |       |      0.44
3.667    0.94    0.10      0.195  o   I   |       |       |       |      0.45
3.750    0.94    0.10      0.201  o   I   |       |       |       |      0.47
3.833    1.00    0.11      0.207  o   I   |       |       |       |      0.48
3.917    1.09    0.11      0.213  o    I  |       |       |       |      0.49
4.000    1.11    0.11      0.220  o    I  |       |       |       |      0.51
4.083    1.12    0.12      0.227  o    I  |       |       |       |      0.53
4.167    1.12    0.12      0.234  o    I  |       |       |       |      0.54
4.250    1.13    0.13      0.241  o    I  |       |       |       |      0.56
4.333    1.18    0.13      0.248  o    I  |       |       |       |      0.57
4.417    1.27    0.13      0.255  o     I |       |       |       |      0.59
4.500    1.30    0.14      0.263  o     I |       |       |       |      0.61
4.583    1.31    0.14      0.271  o     I |       |       |       |      0.63
4.667    1.31    0.15      0.279  o     I |       |       |       |      0.65
4.750    1.32    0.15      0.287  o     I |       |       |       |      0.67
4.833    1.37    0.15      0.296  o     I |       |       |       |      0.69
4.917    1.46    0.16      0.304  o      I|       |       |       |      0.71
5.000    1.48    0.16      0.313  o      I|       |       |       |      0.73
5.083    1.38    0.17      0.322  o     I |       |       |       |      0.75
5.167    1.21    0.17      0.330  o     I |       |       |       |      0.77
5.250    1.17    0.18      0.337  o    I  |       |       |       |      0.78
5.333    1.20    0.18      0.344  o     I |       |       |       |      0.80
5.417    1.28    0.18      0.351  o     I |       |       |       |      0.81
5.500    1.30    0.19      0.359  o     I |       |       |       |      0.83
5.583    1.36    0.19      0.366  o     I |       |       |       |      0.85
5.667    1.46    0.20      0.375  o      I|       |       |       |      0.87
5.750    1.48    0.20      0.384  |o     I|       |       |       |      0.89
5.833    1.49    0.20      0.392  |o     I|       |       |       |      0.91
5.917    1.50    0.21      0.401  |o     I|       |       |       |      0.93
6.000    1.50    0.21      0.410  |o     I|       |       |       |      0.95
6.083    1.56    0.22      0.419  |o     I|       |       |       |      0.97
6.167    1.65    0.22      0.429  |o      I       |       |       |      0.99
6.250    1.67    0.23      0.439  |o      I       |       |       |      1.02
6.333    1.68    0.23      0.449  |o      I       |       |       |      1.04
6.417    1.69    0.23      0.459  |o      I       |       |       |      1.06
6.500    1.69    0.23      0.469  |o      I       |       |       |      1.08
6.583    1.75    0.24      0.479  |o      I       |       |       |      1.10
6.667    1.84    0.24      0.490  |o      |I      |       |       |      1.12
6.750    1.86    0.24      0.501  |o      |I      |       |       |      1.14
6.833    1.87    0.24      0.512  |o      |I      |       |       |      1.17
6.917    1.88    0.25      0.523  |o      |I      |       |       |      1.19
7.000    1.88    0.25      0.534  |o      |I      |       |       |      1.21
7.083    1.88    0.25      0.545  |o      |I      |       |       |      1.24
7.167    1.88    0.26      0.557  |o      |I      |       |       |      1.26
7.250    1.88    0.26      0.568  |o      |I      |       |       |      1.28
7.333    1.94    0.26      0.579  |o      |I      |       |       |      1.31
7.417    2.03    0.26      0.591  |o      | I     |       |       |      1.33
7.500    2.05    0.27      0.603  |o      | I     |       |       |      1.36
7.583    2.11    0.27      0.616  |o      | I     |       |       |      1.38
7.667    2.21    0.27      0.629  |o      |  I    |       |       |      1.41
7.750    2.24    0.28      0.642  |o      |  I    |       |       |      1.44
7.833    2.30    0.28      0.656  |o      |  I    |       |       |      1.47
7.917    2.40    0.28      0.670  |o      |   I   |       |       |      1.49
8.000    2.42    0.29      0.685  |o      |   I   |       |       |      1.53
8.083    2.54    0.29      0.700  |o      |   I   |       |       |      1.56
8.167    2.73    0.30      0.716  |o      |    I  |       |       |      1.59
8.250    2.78    0.30      0.733  |o      |    I  |       |       |      1.63
8.333    2.80    0.30      0.750  |o      |     I |       |       |      1.66
8.417    2.81    0.31      0.767  |o      |     I |       |       |      1.70
8.500    2.82    0.31      0.785  |o      |     I |       |       |      1.73
8.583    2.88    0.32      0.802  |o      |     I |       |       |      1.77
8.667    2.97    0.32      0.820  |o      |     I |       |       |      1.81
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 8.750    2.99    0.33      0.838  |O       |     I |        |        |     1.84
 8.833    3.05    0.33      0.857  |O       |      I|        |        |     1.88
 8.917    3.15    0.33      0.876  |O       |      I|        |        |     1.92
 9.000    3.18    0.34      0.895  |O       |      I|        |        |     1.96
 9.083    3.30    0.35      0.915  |O       |       I        |        |     2.00
 9.167    3.48    0.37      0.936  |O       |        |I      |        |     2.04
 9.250    3.53    0.40      0.958  |O       |        |I      |        |     2.08
 9.333    3.61    0.42      0.979  | O      |        | I     |        |     2.12
 9.417    3.71    0.45      1.002  | O      |        | I     |        |     2.16
 9.500    3.74    0.48      1.024  | O      |        | I     |        |     2.20
 9.583    3.81    0.50      1.047  | O      |        |  I    |        |     2.25
 9.667    3.90    0.53      1.070  | O      |        |  I    |        |     2.29
 9.750    3.93    0.56      1.093  | O      |        |  I    |        |     2.33
 9.833    3.99    0.59      1.116  | O      |        |  I    |        |     2.38
 9.917    4.09    0.62      1.140  |  O     |        |   I   |        |     2.42
10.000    4.12    0.64      1.164  |  O     |        |   I   |        |     2.47
10.083    3.74    0.67      1.186  |  O     |        | I     |        |     2.51
10.167    3.11    0.69      1.205  |  O     |       I|       |        |     2.54
10.250    2.96    0.71      1.221  |  O     |     I  |       |        |     2.57
10.333    2.89    0.73      1.236  |  O     |     I  |       |        |     2.60
10.417    2.85    0.75      1.251  |  O     |     I  |       |        |     2.63
10.500    2.82    0.77      1.265  |  O     |     I  |       |        |     2.65
10.583    3.10    0.79      1.280  |  O     |      I|       |        |     2.68
10.667    3.55    0.81      1.298  |   O    |       I       |        |     2.71
10.750    3.66    0.83      1.317  |   O    |        I      |        |     2.75
10.833    3.71    0.85      1.337  |   O    |        I      |        |     2.79
10.917    3.74    0.88      1.356  |   O    |        I      |        |     2.82
11.000    3.76    0.90      1.376  |   O    |        I      |        |     2.86
11.083    3.71    0.92      1.395  |   O    |        I      |        |     2.90
11.167    3.61    0.95      1.414  |   O    |        I      |        |     2.93
11.250    3.59    0.97      1.432  |   O    |       I       |        |     2.97
11.333    3.58    0.99      1.450  |   O    |       I       |        |     3.00
11.417    3.58    1.00      1.468  |    O   |       I       |        |     3.03
11.500    3.57    1.02      1.486  |    O   |       I       |        |     3.06
11.583    3.46    1.03      1.503  |    O   |       I       |        |     3.09
11.667    3.28    1.04      1.519  |    O   |      I        |        |     3.11
11.750    3.24    1.05      1.534  |    O   |      I        |        |     3.14
11.833    3.27    1.06      1.549  |    O   |      I        |        |     3.16
11.917    3.35    1.07      1.565  |    O   |      I        |        |     3.19
12.000    3.36    1.08      1.581  |    O   |      I        |        |     3.22
12.083    3.76    1.10      1.598  |    O   |       I       |        |     3.25
12.167    4.40    1.11      1.618  |    O   |           I   |        |     3.28
12.250    4.56    1.13      1.641  |    O   |           I   |        |     3.32
12.333    4.69    1.14      1.665  |    O   |            I  |        |     3.36
12.417    4.82    1.16      1.690  |    O   |             I |        |     3.40
12.500    4.87    1.18      1.715  |    O   |             I |        |     3.44
12.583    4.99    1.20      1.741  |    O   |             I |        |     3.49
12.667    5.17    1.22      1.768  |     O  |              I|        |     3.53
12.750    5.22    1.24      1.795  |     O  |               I        |     3.58
12.833    5.30    1.26      1.823  |     O  |               I        |     3.62
12.917    5.40    1.28      1.851  |     O  |                I       |     3.67
13.000    5.43    1.30      1.879  |     O  |                I       |     3.72
13.083    5.72    1.32      1.909  |     O  |                 I      |     3.77
13.167    6.17    1.34      1.941  |     O  |                    I   |     3.82
13.250    6.29    1.36      1.974  |     O  |                     I  |     3.88
13.333    6.34    1.39      2.008  |     O  |                     I  |     3.93
13.417    6.37    1.41      2.042  |      O |                     I  |     3.99
13.500    6.39    1.43      2.077  |      O |                      I |     4.04
13.583    5.79    1.45      2.109  |      O |                 I     |     4.09
13.667    4.79    1.46      2.135  |      O |              I|       |     4.13
13.750    4.54    1.47      2.157  |      O |            I  |       |     4.16
13.833    4.43    1.48      2.178  |      O |            I  |       |     4.19
13.917    4.37    1.49      2.198  |      O |           I   |       |     4.22
14.000    4.32    1.50      2.218  |      O |           I   |       |     4.25
14.083    4.54    1.51      2.238  |      O |            I  |       |     4.28
14.167    4.91    1.52      2.260  |      O |              I        |     4.32
14.250    5.00    1.53      2.284  |      O |               I       |     4.35
14.333    4.98    1.54      2.307  |      O |              I        |     4.39
14.417    4.91    1.55      2.331  |      O |              I        |     4.43
14.500    4.91    1.56      2.354  |      O |              I        |     4.46
14.583    4.90    1.57      2.377  |      O |              I        |     4.49
14.667    4.89    1.58      2.400  |      O |              I        |     4.53
14.750    4.89    1.59      2.423  |      O |              I        |     4.56
14.833    4.83    1.60      2.445  |       O|              I        |     4.60
14.917    4.74    1.61      2.467  |       O|             I|        |     4.63
15.000    4.72    1.63      2.488  |       O|             I|        |     4.66
15.083    4.66    1.64      2.509  |       O|             I|        |     4.69
15.167    4.56    1.64      2.530  |       O|           I  |        |     4.73
15.250    4.53    1.65      2.550  |       O|           I  |        |     4.76
15.333    4.47    1.66      2.569  |       O|           I  |        |     4.78
15.417    4.37    1.67      2.588  |       O|          I   |        |     4.81
15.500    4.34    1.68      2.607  |       O|          I   |        |     4.84
15.583    4.11    1.69      2.624  |       O|         I    |        |     4.87
15.667    3.75    1.70      2.640  |       O|       I      |        |     4.89
15.750    3.65    1.70      2.653  |       O|       I      |        |     4.91
15.833    3.61    1.71      2.667  |       O|       I      |        |     4.93
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15.917	3.59	1.72	2.680	| O |I | | |				4.95
16.000	3.57	1.72	2.693	| O |I | | |				4.97
16.083	2.75	1.73	2.702	| O I | | |				4.99
16.167	1.39	1.73	2.705	| I O | | |				4.99
16.250	1.05	1.73	2.701	| I O | | |				4.98
16.333	0.90	1.72	2.696	| I O | | |				4.98
16.417	0.81	1.72	2.690	| I O | | |				4.97
16.500	0.75	1.72	2.684	| I O | | |				4.96
16.583	0.70	1.71	2.677	| I O | | |				4.95
16.667	0.61	1.71	2.670	| I O | | |				4.94
16.750	0.58	1.71	2.662	| I O | | |				4.92
16.833	0.57	1.70	2.654	| I O | | |				4.91
16.917	0.57	1.70	2.646	| I O | | |				4.90
17.000	0.56	1.70	2.639	| I O | | |				4.89
17.083	0.67	1.69	2.631	| I O | | |				4.88
17.167	0.85	1.69	2.625	| I O | | |				4.87
17.250	0.90	1.69	2.619	| I O | | |				4.86
17.333	0.92	1.68	2.614	| I O | | |				4.85
17.417	0.93	1.68	2.609	| I O | | |				4.84
17.500	0.94	1.68	2.603	| I O | | |				4.84
17.583	0.94	1.68	2.598	| I O | | |				4.83
17.667	0.94	1.67	2.593	| I O | | |				4.82
17.750	0.94	1.67	2.588	| I O | | |				4.81
17.833	0.89	1.67	2.583	| I O | | |				4.81
17.917	0.79	1.67	2.577	| I O | | |				4.80
18.000	0.77	1.66	2.571	| I O | | |				4.79
18.083	0.76	1.66	2.565	| I O | | |				4.78
18.167	0.76	1.66	2.559	| I O | | |				4.77
18.250	0.75	1.66	2.553	| I O | | |				4.76
18.333	0.75	1.65	2.546	| I O | | |				4.75
18.417	0.75	1.65	2.540	| I O | | |				4.74
18.500	0.75	1.65	2.534	| I O | | |				4.73
18.583	0.70	1.64	2.528	| I O | | |				4.72
18.667	0.61	1.64	2.521	| I O | | |				4.71
18.750	0.58	1.64	2.514	| I O | | |				4.70
18.833	0.52	1.63	2.506	| I O | | |				4.69
18.917	0.42	1.63	2.498	| I O | | |				4.68
19.000	0.40	1.63	2.490	|I O | | |				4.66
19.083	0.44	1.62	2.482	| I O | | |				4.65
19.167	0.53	1.62	2.474	| I O | | |				4.64
19.250	0.54	1.61	2.466	| I O | | |				4.63
19.333	0.61	1.61	2.459	| I O | | |				4.62
19.417	0.71	1.61	2.453	| I O | | |				4.61
19.500	0.73	1.61	2.447	| I O | | |				4.60
19.583	0.69	1.60	2.440	| I O | | |				4.59
19.667	0.60	1.60	2.434	| I O | | |				4.58
19.750	0.58	1.60	2.427	| I O| | |				4.57
19.833	0.52	1.59	2.420	| I O| | |				4.56
19.917	0.42	1.59	2.412	| I O| | |				4.55
20.000	0.40	1.59	2.404	|I O| | |				4.54
20.083	0.44	1.58	2.396	| I O| | |				4.52
20.167	0.53	1.58	2.388	| I O| | |				4.51
20.250	0.54	1.57	2.381	| I O| | |				4.50
20.333	0.55	1.57	2.374	| I O| | |				4.49
20.417	0.56	1.57	2.367	| I O| | |				4.48
20.500	0.56	1.56	2.360	| I O| | |				4.47
20.583	0.56	1.56	2.353	| I O| | |				4.46
20.667	0.56	1.56	2.346	| I O| | |				4.45
20.750	0.56	1.55	2.340	| I O| | |				4.44
20.833	0.51	1.55	2.333	| I O| | |				4.43
20.917	0.42	1.55	2.325	| I O| | |				4.42
21.000	0.40	1.54	2.317	|I O| | |				4.40
21.083	0.44	1.54	2.310	| I O| | |				4.39
21.167	0.53	1.54	2.302	| I O| | |				4.38
21.250	0.54	1.53	2.295	| I O| | |				4.37
21.333	0.50	1.53	2.288	| I O| | |				4.36
21.417	0.41	1.53	2.281	| I O| | |				4.35
21.500	0.40	1.52	2.273	|I O| | |				4.34
21.583	0.44	1.52	2.266	| I O| | |				4.33
21.667	0.53	1.52	2.259	| I O| | |				4.32
21.750	0.54	1.51	2.252	| I O| | |				4.31
21.833	0.50	1.51	2.245	| I O| | |				4.30
21.917	0.41	1.51	2.238	| I O| | |				4.28
22.000	0.40	1.50	2.230	|I O| | |				4.27
22.083	0.44	1.50	2.223	| I O| | |				4.26
22.167	0.53	1.50	2.216	| I O| | |				4.25
22.250	0.54	1.49	2.209	| I O| | |				4.24
22.333	0.50	1.49	2.202	| I O| | |				4.23
22.417	0.41	1.49	2.195	| I O| | |				4.22
22.500	0.40	1.48	2.188	|I O| | |				4.21
22.583	0.39	1.48	2.180	|I O| | |				4.20
22.667	0.38	1.48	2.173	|I O| | |				4.19
22.750	0.38	1.47	2.165	|I O| | |				4.18
22.833	0.38	1.47	2.158	|I O| | |				4.16
22.917	0.38	1.46	2.150	|I O| | |				4.15
23.000	0.38	1.46	2.143	|I O| | |				4.14

23.083	0.38	1.46	2.135	I o				4.13
23.167	0.38	1.45	2.128	I o				4.12
23.250	0.38	1.45	2.121	I o				4.11
23.333	0.38	1.45	2.113	I o				4.10
23.417	0.38	1.44	2.106	I o				4.09
23.500	0.38	1.44	2.098	I o				4.07
23.583	0.38	1.44	2.091	I o				4.06
23.667	0.38	1.43	2.084	I o				4.05
23.750	0.38	1.43	2.077	I o				4.04
23.833	0.38	1.43	2.069	I o				4.03
23.917	0.38	1.42	2.062	I o				4.02
24.000	0.38	1.42	2.055	I o				4.01
24.083	0.27	1.42	2.047	I o				4.00
24.167	0.09	1.41	2.039	I o				3.98
24.250	0.04	1.40	2.030	I o				3.97
24.333	0.02	1.40	2.020	I o				3.95
24.417	0.01	1.39	2.011	I o				3.94
24.500	0.00	1.38	2.001	I o				3.92
24.583	0.00	1.38	1.992	I o				3.90
24.667	0.00	1.37	1.982	I o				3.89
24.750	0.00	1.36	1.973	I o				3.87
24.833	0.00	1.36	1.963	I o				3.86
24.917	0.00	1.35	1.954	I o				3.84
25.000	0.00	1.34	1.945	I o				3.83
25.083	0.00	1.34	1.936	I o				3.81
25.167	0.00	1.33	1.926	I o				3.79
25.250	0.00	1.32	1.917	I o				3.78
25.333	0.00	1.32	1.908	I o				3.76
25.417	0.00	1.31	1.899	I o				3.75
25.500	0.00	1.30	1.890	I o				3.73
25.583	0.00	1.30	1.881	I o				3.72
25.667	0.00	1.29	1.872	I o				3.70
25.750	0.00	1.28	1.863	I o				3.69
25.833	0.00	1.28	1.855	I o				3.67
25.917	0.00	1.27	1.846	I o				3.66
26.000	0.00	1.27	1.837	I o				3.65
26.083	0.00	1.26	1.828	I o				3.63
26.167	0.00	1.25	1.820	I o				3.62
26.250	0.00	1.25	1.811	I o				3.60
26.333	0.00	1.24	1.802	I o				3.59
26.417	0.00	1.24	1.794	I o				3.57
26.500	0.00	1.23	1.785	I o				3.56
26.583	0.00	1.22	1.777	I o				3.55
26.667	0.00	1.22	1.769	I o				3.53
26.750	0.00	1.21	1.760	I o				3.52
26.833	0.00	1.21	1.752	I o				3.50
26.917	0.00	1.20	1.744	I o				3.49
27.000	0.00	1.19	1.735	I o				3.48
27.083	0.00	1.19	1.727	I o				3.46
27.167	0.00	1.18	1.719	I o				3.45
27.250	0.00	1.18	1.711	I o				3.43
27.333	0.00	1.17	1.703	I o				3.42
27.417	0.00	1.16	1.695	I o				3.41
27.500	0.00	1.16	1.687	I o				3.39
27.583	0.00	1.15	1.679	I o				3.38
27.667	0.00	1.15	1.671	I o				3.37
27.750	0.00	1.14	1.663	I o				3.35
27.833	0.00	1.14	1.655	I o				3.34
27.917	0.00	1.13	1.647	I o				3.33
28.000	0.00	1.13	1.640	I o				3.32
28.083	0.00	1.12	1.632	I o				3.30
28.167	0.00	1.11	1.624	I o				3.29
28.250	0.00	1.11	1.617	I o				3.28
28.333	0.00	1.10	1.609	I o				3.26
28.417	0.00	1.10	1.601	I o				3.25
28.500	0.00	1.09	1.594	I o				3.24
28.583	0.00	1.09	1.586	I o				3.23
28.667	0.00	1.08	1.579	I o				3.21
28.750	0.00	1.08	1.571	I o				3.20
28.833	0.00	1.07	1.564	I o				3.19
28.917	0.00	1.07	1.557	I o				3.18
29.000	0.00	1.06	1.549	I o				3.16
29.083	0.00	1.06	1.542	I o				3.15
29.167	0.00	1.05	1.535	I o				3.14
29.250	0.00	1.05	1.528	I o				3.13
29.333	0.00	1.04	1.520	I o				3.12
29.417	0.00	1.04	1.513	I o				3.10
29.500	0.00	1.03	1.506	I o				3.09
29.583	0.00	1.03	1.499	I o				3.08
29.667	0.00	1.02	1.492	I o				3.07
29.750	0.00	1.02	1.485	I o				3.06
29.833	0.00	1.01	1.478	I o				3.05
29.917	0.00	1.01	1.471	I o				3.03
30.000	0.00	1.00	1.464	I o				3.02
30.083	0.00	1.00	1.457	I o				3.01
30.167	0.00	0.99	1.450	I o				3.00

30.250	0.00	0.98	1.444	I	o	|	|	|	2.99
30.333	0.00	0.97	1.437	I	o	|	|	|	2.97
30.417	0.00	0.97	1.430	I	o	|	|	|	2.96
30.500	0.00	0.96	1.424	I	o	|	|	|	2.95
30.583	0.00	0.95	1.417	I	o	|	|	|	2.94
30.667	0.00	0.94	1.410	I	o	|	|	|	2.92
30.750	0.00	0.93	1.404	I	o	|	|	|	2.91
30.833	0.00	0.93	1.398	I	o	|	|	|	2.90
30.917	0.00	0.92	1.391	I	o	|	|	|	2.89
31.000	0.00	0.91	1.385	I	o	|	|	|	2.88
31.083	0.00	0.90	1.379	I	o	|	|	|	2.87
31.167	0.00	0.90	1.373	I	o	|	|	|	2.85
31.250	0.00	0.89	1.366	I	o	|	|	|	2.84
31.333	0.00	0.88	1.360	I	o	|	|	|	2.83
31.417	0.00	0.87	1.354	I	o	|	|	|	2.82
31.500	0.00	0.87	1.348	I	o	|	|	|	2.81
31.583	0.00	0.86	1.342	I	o	|	|	|	2.80
31.667	0.00	0.85	1.336	I	o	|	|	|	2.79
31.750	0.00	0.85	1.331	I	o	|	|	|	2.78
31.833	0.00	0.84	1.325	I	o	|	|	|	2.76
31.917	0.00	0.83	1.319	I	o	|	|	|	2.75
32.000	0.00	0.83	1.313	I	o	|	|	|	2.74
32.083	0.00	0.82	1.308	I	o	|	|	|	2.73
32.167	0.00	0.81	1.302	I	o	|	|	|	2.72
32.250	0.00	0.80	1.296	I	o	|	|	|	2.71
32.333	0.00	0.80	1.291	I	o	|	|	|	2.70
32.417	0.00	0.79	1.285	I	o	|	|	|	2.69
32.500	0.00	0.78	1.280	I	o	|	|	|	2.68
32.583	0.00	0.78	1.275	I	o	|	|	|	2.67
32.667	0.00	0.77	1.269	I	o	|	|	|	2.66
32.750	0.00	0.77	1.264	I	o	|	|	|	2.65
32.833	0.00	0.76	1.259	I	o	|	|	|	2.64
32.917	0.00	0.75	1.254	I	o	|	|	|	2.63
33.000	0.00	0.75	1.248	I	o	|	|	|	2.62
33.083	0.00	0.74	1.243	I	o	|	|	|	2.61
33.167	0.00	0.73	1.238	I	o	|	|	|	2.60
33.250	0.00	0.73	1.233	I	o	|	|	|	2.59
33.333	0.00	0.72	1.228	I	o	|	|	|	2.58
33.417	0.00	0.72	1.223	I	o	|	|	|	2.58
33.500	0.00	0.71	1.218	I	o	|	|	|	2.57
33.583	0.00	0.70	1.213	I	o	|	|	|	2.56
33.667	0.00	0.70	1.209	I	o	|	|	|	2.55
33.750	0.00	0.69	1.204	I	o	|	|	|	2.54
33.833	0.00	0.69	1.199	I	o	|	|	|	2.53
33.917	0.00	0.68	1.194	I	o	|	|	|	2.52
34.000	0.00	0.68	1.190	I	o	|	|	|	2.51
34.083	0.00	0.67	1.185	I	o	|	|	|	2.50
34.167	0.00	0.66	1.180	I	o	|	|	|	2.50
34.250	0.00	0.66	1.176	I	o	|	|	|	2.49
34.333	0.00	0.65	1.171	I	o	|	|	|	2.48
34.417	0.00	0.65	1.167	I	o	|	|	|	2.47
34.500	0.00	0.64	1.162	I	o	|	|	|	2.46
34.583	0.00	0.64	1.158	I	o	|	|	|	2.45
34.667	0.00	0.63	1.154	I	o	|	|	|	2.45
34.750	0.00	0.63	1.149	I	o	|	|	|	2.44
34.833	0.00	0.62	1.145	I	o	|	|	|	2.43
34.917	0.00	0.62	1.141	I	o	|	|	|	2.42
35.000	0.00	0.61	1.136	I	o	|	|	|	2.41
35.083	0.00	0.61	1.132	I	o	|	|	|	2.41
35.167	0.00	0.60	1.128	I	o	|	|	|	2.40
35.250	0.00	0.60	1.124	I	o	|	|	|	2.39
35.333	0.00	0.59	1.120	I	o	|	|	|	2.38
35.417	0.00	0.59	1.116	I	o	|	|	|	2.38
35.500	0.00	0.58	1.112	I	o	|	|	|	2.37
35.583	0.00	0.58	1.108	I	o	|	|	|	2.36
35.667	0.00	0.57	1.104	I	o	|	|	|	2.35
35.750	0.00	0.57	1.100	I	o	|	|	|	2.35
35.833	0.00	0.56	1.096	I	o	|	|	|	2.34
35.917	0.00	0.56	1.092	I	o	|	|	|	2.33
36.000	0.00	0.55	1.088	I	o	|	|	|	2.32
36.083	0.00	0.55	1.084	I	o	|	|	|	2.32
36.167	0.00	0.54	1.081	I	o	|	|	|	2.31
36.250	0.00	0.54	1.077	I	o	|	|	|	2.30
36.333	0.00	0.54	1.073	I	o	|	|	|	2.30
36.417	0.00	0.53	1.070	I	o	|	|	|	2.29
36.500	0.00	0.53	1.066	I	o	|	|	|	2.28
36.583	0.00	0.52	1.062	I	o	|	|	|	2.28
36.667	0.00	0.52	1.059	I	o	|	|	|	2.27
36.750	0.00	0.51	1.055	I	o	|	|	|	2.26
36.833	0.00	0.51	1.052	I	o	|	|	|	2.26
36.917	0.00	0.51	1.048	I	o	|	|	|	2.25
37.000	0.00	0.50	1.045	I	o	|	|	|	2.24
37.083	0.00	0.50	1.041	I	o	|	|	|	2.24
37.167	0.00	0.49	1.038	I	o	|	|	|	2.23
37.250	0.00	0.49	1.034	I	o	|	|	|	2.22
37.333	0.00	0.49	1.031	I	o	|	|	|	2.22

37.417	0.00	0.48	1.028	I O	|	|	|	2.21
37.500	0.00	0.48	1.024	I O	|	|	|	2.21
37.583	0.00	0.47	1.021	I O	|	|	|	2.20
37.667	0.00	0.47	1.018	I O	|	|	|	2.19
37.750	0.00	0.47	1.015	I O	|	|	|	2.19
37.833	0.00	0.46	1.012	I O	|	|	|	2.18
37.917	0.00	0.46	1.008	I O	|	|	|	2.18
38.000	0.00	0.45	1.005	I O	|	|	|	2.17
38.083	0.00	0.45	1.002	I O	|	|	|	2.16
38.167	0.00	0.45	0.999	I O	|	|	|	2.16
38.250	0.00	0.44	0.996	I O	|	|	|	2.15
38.333	0.00	0.44	0.993	I O	|	|	|	2.15
38.417	0.00	0.44	0.990	I O	|	|	|	2.14
38.500	0.00	0.43	0.987	I O	|	|	|	2.14
38.583	0.00	0.43	0.984	I O	|	|	|	2.13
38.667	0.00	0.42	0.981	I O	|	|	|	2.12
38.750	0.00	0.42	0.978	I O	|	|	|	2.12
38.833	0.00	0.42	0.975	I O	|	|	|	2.11
38.917	0.00	0.41	0.972	I O	|	|	|	2.11
39.000	0.00	0.41	0.970	I O	|	|	|	2.10
39.083	0.00	0.41	0.967	I O	|	|	|	2.10
39.167	0.00	0.40	0.964	I O	|	|	|	2.09
39.250	0.00	0.40	0.961	I O	|	|	|	2.09
39.333	0.00	0.40	0.958	IO	|	|	|	2.08
39.417	0.00	0.39	0.956	IO	|	|	|	2.08
39.500	0.00	0.39	0.953	IO	|	|	|	2.07
39.583	0.00	0.39	0.950	IO	|	|	|	2.07
39.667	0.00	0.38	0.948	IO	|	|	|	2.06
39.750	0.00	0.38	0.945	IO	|	|	|	2.06
39.833	0.00	0.38	0.942	IO	|	|	|	2.05
39.917	0.00	0.38	0.940	IO	|	|	|	2.05
40.000	0.00	0.37	0.937	IO	|	|	|	2.04
40.083	0.00	0.37	0.935	IO	|	|	|	2.04
40.167	0.00	0.37	0.932	IO	|	|	|	2.03
40.250	0.00	0.36	0.930	IO	|	|	|	2.03
40.333	0.00	0.36	0.927	IO	|	|	|	2.02
40.417	0.00	0.36	0.925	IO	|	|	|	2.02
40.500	0.00	0.35	0.922	IO	|	|	|	2.02
40.583	0.00	0.35	0.920	IO	|	|	|	2.01
40.667	0.00	0.35	0.917	IO	|	|	|	2.01
40.750	0.00	0.35	0.915	IO	|	|	|	2.00
40.833	0.00	0.34	0.913	IO	|	|	|	2.00
40.917	0.00	0.34	0.910	IO	|	|	|	1.99
41.000	0.00	0.34	0.908	IO	|	|	|	1.99
41.083	0.00	0.34	0.906	IO	|	|	|	1.98
41.167	0.00	0.34	0.903	IO	|	|	|	1.98
41.250	0.00	0.34	0.901	IO	|	|	|	1.97
41.333	0.00	0.34	0.899	IO	|	|	|	1.97
41.417	0.00	0.34	0.896	IO	|	|	|	1.96
41.500	0.00	0.34	0.894	IO	|	|	|	1.96
41.583	0.00	0.34	0.891	IO	|	|	|	1.95
41.667	0.00	0.34	0.889	IO	|	|	|	1.95
41.750	0.00	0.34	0.887	IO	|	|	|	1.94
41.833	0.00	0.34	0.885	IO	|	|	|	1.94
41.917	0.00	0.34	0.882	IO	|	|	|	1.93
42.000	0.00	0.34	0.880	IO	|	|	|	1.93
42.083	0.00	0.34	0.878	IO	|	|	|	1.92
42.167	0.00	0.33	0.875	IO	|	|	|	1.92
42.250	0.00	0.33	0.873	IO	|	|	|	1.92
42.333	0.00	0.33	0.871	IO	|	|	|	1.91
42.417	0.00	0.33	0.868	IO	|	|	|	1.91
42.500	0.00	0.33	0.866	IO	|	|	|	1.90
42.583	0.00	0.33	0.864	IO	|	|	|	1.90
42.667	0.00	0.33	0.862	IO	|	|	|	1.89
42.750	0.00	0.33	0.859	IO	|	|	|	1.89
42.833	0.00	0.33	0.857	IO	|	|	|	1.88
42.917	0.00	0.33	0.855	IO	|	|	|	1.88
43.000	0.00	0.33	0.852	IO	|	|	|	1.87
43.083	0.00	0.33	0.850	IO	|	|	|	1.87
43.167	0.00	0.33	0.848	IO	|	|	|	1.86
43.250	0.00	0.33	0.846	IO	|	|	|	1.86
43.333	0.00	0.33	0.843	IO	|	|	|	1.85
43.417	0.00	0.33	0.841	IO	|	|	|	1.85
43.500	0.00	0.33	0.839	IO	|	|	|	1.84
43.583	0.00	0.32	0.837	IO	|	|	|	1.84
43.667	0.00	0.32	0.834	IO	|	|	|	1.84
43.750	0.00	0.32	0.832	IO	|	|	|	1.83
43.833	0.00	0.32	0.830	IO	|	|	|	1.83
43.917	0.00	0.32	0.828	IO	|	|	|	1.82
44.000	0.00	0.32	0.826	IO	|	|	|	1.82
44.083	0.00	0.32	0.823	IO	|	|	|	1.81
44.167	0.00	0.32	0.821	IO	|	|	|	1.81
44.250	0.00	0.32	0.819	IO	|	|	|	1.80
44.333	0.00	0.32	0.817	IO	|	|	|	1.80
44.417	0.00	0.32	0.814	IO	|	|	|	1.79
44.500	0.00	0.32	0.812	IO	|	|	|	1.79

44.583	0.00	0.32	0.810	IO					1.78
44.667	0.00	0.32	0.808	IO					1.78
44.750	0.00	0.32	0.806	IO					1.78
44.833	0.00	0.32	0.804	IO					1.77
44.917	0.00	0.32	0.801	IO					1.77
45.000	0.00	0.32	0.799	IO					1.76
45.083	0.00	0.32	0.797	IO					1.76
45.167	0.00	0.31	0.795	IO					1.75
45.250	0.00	0.31	0.793	IO					1.75
45.333	0.00	0.31	0.791	IO					1.74
45.417	0.00	0.31	0.788	IO					1.74
45.500	0.00	0.31	0.786	IO					1.74
45.583	0.00	0.31	0.784	IO					1.73
45.667	0.00	0.31	0.782	IO					1.73
45.750	0.00	0.31	0.780	IO					1.72
45.833	0.00	0.31	0.778	IO					1.72
45.917	0.00	0.31	0.775	IO					1.71
46.000	0.00	0.31	0.773	IO					1.71
46.083	0.00	0.31	0.771	IO					1.70
46.167	0.00	0.31	0.769	IO					1.70
46.250	0.00	0.31	0.767	IO					1.70
46.333	0.00	0.31	0.765	IO					1.69
46.417	0.00	0.31	0.763	IO					1.69
46.500	0.00	0.31	0.761	IO					1.68
46.583	0.00	0.31	0.759	IO					1.68
46.667	0.00	0.31	0.756	IO					1.67
46.750	0.00	0.30	0.754	IO					1.67
46.833	0.00	0.30	0.752	IO					1.67
46.917	0.00	0.30	0.750	IO					1.66
47.000	0.00	0.30	0.748	IO					1.66
47.083	0.00	0.30	0.746	IO					1.65
47.167	0.00	0.30	0.744	IO					1.65
47.250	0.00	0.30	0.742	IO					1.64
47.333	0.00	0.30	0.740	IO					1.64
47.417	0.00	0.30	0.738	IO					1.63
47.500	0.00	0.30	0.736	IO					1.63
47.583	0.00	0.30	0.734	IO					1.63
47.667	0.00	0.30	0.731	IO					1.62
47.750	0.00	0.30	0.729	IO					1.62
47.833	0.00	0.30	0.727	IO					1.61
47.917	0.00	0.30	0.725	IO					1.61
48.000	0.00	0.30	0.723	IO					1.61
48.083	0.00	0.30	0.721	IO					1.60
48.167	0.00	0.30	0.719	IO					1.60
48.250	0.00	0.30	0.717	IO					1.59
48.333	0.00	0.29	0.715	IO					1.59
48.417	0.00	0.29	0.713	IO					1.58
48.500	0.00	0.29	0.711	IO					1.58
48.583	0.00	0.29	0.709	IO					1.58
48.667	0.00	0.29	0.707	IO					1.57
48.750	0.00	0.29	0.705	IO					1.57
48.833	0.00	0.29	0.703	IO					1.56
48.917	0.00	0.29	0.701	IO					1.56
49.000	0.00	0.29	0.699	IO					1.55
49.083	0.00	0.29	0.697	IO					1.55
49.167	0.00	0.29	0.695	IO					1.55
49.250	0.00	0.29	0.693	IO					1.54
49.333	0.00	0.29	0.691	IO					1.54
49.417	0.00	0.29	0.689	IO					1.53
49.500	0.00	0.29	0.687	IO					1.53
49.583	0.00	0.29	0.685	IO					1.53
49.667	0.00	0.29	0.683	IO					1.52
49.750	0.00	0.29	0.681	IO					1.52
49.833	0.00	0.29	0.679	IO					1.51
49.917	0.00	0.29	0.677	IO					1.51
50.000	0.00	0.29	0.675	IO					1.51
50.083	0.00	0.28	0.673	IO					1.50
50.167	0.00	0.28	0.671	IO					1.50
50.250	0.00	0.28	0.669	IO					1.49
50.333	0.00	0.28	0.667	IO					1.49
50.417	0.00	0.28	0.665	IO					1.49
50.500	0.00	0.28	0.663	IO					1.48
50.583	0.00	0.28	0.661	IO					1.48
50.667	0.00	0.28	0.660	IO					1.47
50.750	0.00	0.28	0.658	IO					1.47
50.833	0.00	0.28	0.656	IO					1.47
50.917	0.00	0.28	0.654	IO					1.46
51.000	0.00	0.28	0.652	IO					1.46
51.083	0.00	0.28	0.650	IO					1.45
51.167	0.00	0.28	0.648	IO					1.45
51.250	0.00	0.28	0.646	IO					1.45
51.333	0.00	0.28	0.644	IO					1.44
51.417	0.00	0.28	0.642	IO					1.44
51.500	0.00	0.28	0.640	IO					1.43
51.583	0.00	0.28	0.638	IO					1.43
51.667	0.00	0.28	0.637	IO					1.43

51.750	0.00	0.28	0.635	IO					1.42
51.833	0.00	0.27	0.633	IO					1.42
51.917	0.00	0.27	0.631	IO					1.41
52.000	0.00	0.27	0.629	IO					1.41
52.083	0.00	0.27	0.627	IO					1.41
52.167	0.00	0.27	0.625	IO					1.40
52.250	0.00	0.27	0.623	IO					1.40
52.333	0.00	0.27	0.621	IO					1.39
52.417	0.00	0.27	0.620	IO					1.39
52.500	0.00	0.27	0.618	IO					1.39
52.583	0.00	0.27	0.616	IO					1.38
52.667	0.00	0.27	0.614	IO					1.38
52.750	0.00	0.27	0.612	IO					1.37
52.833	0.00	0.27	0.610	IO					1.37
52.917	0.00	0.27	0.608	IO					1.37
53.000	0.00	0.27	0.607	IO					1.36
53.083	0.00	0.27	0.605	IO					1.36
53.167	0.00	0.27	0.603	IO					1.36
53.250	0.00	0.27	0.601	IO					1.35
53.333	0.00	0.27	0.599	IO					1.35
53.417	0.00	0.27	0.597	IO					1.34
53.500	0.00	0.27	0.596	IO					1.34
53.583	0.00	0.27	0.594	IO					1.34
53.667	0.00	0.26	0.592	IO					1.33
53.750	0.00	0.26	0.590	IO					1.33
53.833	0.00	0.26	0.588	IO					1.33
53.917	0.00	0.26	0.586	IO					1.32
54.000	0.00	0.26	0.585	IO					1.32
54.083	0.00	0.26	0.583	IO					1.31
54.167	0.00	0.26	0.581	IO					1.31
54.250	0.00	0.26	0.579	IO					1.31
54.333	0.00	0.26	0.577	IO					1.30
54.417	0.00	0.26	0.576	IO					1.30
54.500	0.00	0.26	0.574	IO					1.30
54.583	0.00	0.26	0.572	IO					1.29
54.667	0.00	0.26	0.570	IO					1.29
54.750	0.00	0.26	0.568	IO					1.28
54.833	0.00	0.26	0.567	IO					1.28
54.917	0.00	0.26	0.565	IO					1.28
55.000	0.00	0.26	0.563	IO					1.27
55.083	0.00	0.26	0.561	IO					1.27
55.167	0.00	0.26	0.560	IO					1.27
55.250	0.00	0.26	0.558	IO					1.26
55.333	0.00	0.26	0.556	IO					1.26
55.417	0.00	0.26	0.554	IO					1.26
55.500	0.00	0.25	0.553	IO					1.25
55.583	0.00	0.25	0.551	IO					1.25
55.667	0.00	0.25	0.549	IO					1.24
55.750	0.00	0.25	0.547	IO					1.24
55.833	0.00	0.25	0.546	IO					1.24
55.917	0.00	0.25	0.544	IO					1.23
56.000	0.00	0.25	0.542	IO					1.23
56.083	0.00	0.25	0.540	IO					1.23
56.167	0.00	0.25	0.539	IO					1.22
56.250	0.00	0.25	0.537	IO					1.22
56.333	0.00	0.25	0.535	IO					1.22
56.417	0.00	0.25	0.533	IO					1.21
56.500	0.00	0.25	0.532	IO					1.21
56.583	0.00	0.25	0.530	IO					1.20
56.667	0.00	0.25	0.528	IO					1.20
56.750	0.00	0.25	0.527	IO					1.20
56.833	0.00	0.25	0.525	IO					1.19
56.917	0.00	0.25	0.523	IO					1.19
57.000	0.00	0.25	0.521	IO					1.19
57.083	0.00	0.25	0.520	IO					1.18
57.167	0.00	0.25	0.518	IO					1.18
57.250	0.00	0.25	0.516	IO					1.18
57.333	0.00	0.25	0.515	IO					1.17
57.417	0.00	0.25	0.513	IO					1.17
57.500	0.00	0.24	0.511	IO					1.17
57.583	0.00	0.24	0.510	IO					1.16
57.667	0.00	0.24	0.508	IO					1.16
57.750	0.00	0.24	0.506	IO					1.16
57.833	0.00	0.24	0.505	IO					1.15
57.917	0.00	0.24	0.503	IO					1.15
58.000	0.00	0.24	0.501	IO					1.15
58.083	0.00	0.24	0.499	IO					1.14
58.167	0.00	0.24	0.498	IO					1.14
58.250	0.00	0.24	0.496	IO					1.13
58.333	0.00	0.24	0.495	IO					1.13
58.417	0.00	0.24	0.493	IO					1.13
58.500	0.00	0.24	0.491	IO					1.12
58.583	0.00	0.24	0.490	IO					1.12
58.667	0.00	0.24	0.488	IO					1.12
58.750	0.00	0.24	0.486	IO					1.11
58.833	0.00	0.24	0.485	IO					1.11

58.917	0.00	0.24	0.483	IO				1.11
59.000	0.00	0.24	0.481	IO				1.10
59.083	0.00	0.24	0.480	IO				1.10
59.167	0.00	0.24	0.478	IO				1.10
59.250	0.00	0.24	0.476	IO				1.09
59.333	0.00	0.24	0.475	IO				1.09
59.417	0.00	0.24	0.473	IO				1.09
59.500	0.00	0.23	0.472	IO				1.08
59.583	0.00	0.23	0.470	IO				1.08
59.667	0.00	0.23	0.468	IO				1.08
59.750	0.00	0.23	0.467	IO				1.07
59.833	0.00	0.23	0.465	IO				1.07
59.917	0.00	0.23	0.464	IO				1.07
60.000	0.00	0.23	0.462	IO				1.06
60.083	0.00	0.23	0.460	IO				1.06
60.167	0.00	0.23	0.459	IO				1.06
60.250	0.00	0.23	0.457	IO				1.05
60.333	0.00	0.23	0.456	IO				1.05
60.417	0.00	0.23	0.454	IO				1.05
60.500	0.00	0.23	0.452	IO				1.04
60.583	0.00	0.23	0.451	IO				1.04
60.667	0.00	0.23	0.449	IO				1.04
60.750	0.00	0.23	0.448	IO				1.03
60.833	0.00	0.23	0.446	IO				1.03
60.917	0.00	0.23	0.444	IO				1.03
61.000	0.00	0.23	0.443	IO				1.02
61.083	0.00	0.23	0.441	IO				1.02
61.167	0.00	0.23	0.440	IO				1.02
61.250	0.00	0.23	0.438	IO				1.01
61.333	0.00	0.23	0.437	IO				1.01
61.417	0.00	0.23	0.435	IO				1.01
61.500	0.00	0.23	0.434	IO				1.01
61.583	0.00	0.23	0.432	IO				1.00
61.667	0.00	0.22	0.430	IO				1.00
61.750	0.00	0.22	0.429	IO				1.00
61.833	0.00	0.22	0.427	IO				0.99
61.917	0.00	0.22	0.426	IO				0.99
62.000	0.00	0.22	0.424	IO				0.98
62.083	0.00	0.22	0.423	IO				0.98
62.167	0.00	0.22	0.421	IO				0.98
62.250	0.00	0.22	0.420	IO				0.97
62.333	0.00	0.22	0.418	IO				0.97
62.417	0.00	0.22	0.417	IO				0.97
62.500	0.00	0.22	0.415	IO				0.96
62.583	0.00	0.22	0.414	IO				0.96
62.667	0.00	0.22	0.412	IO				0.96
62.750	0.00	0.21	0.411	IO				0.95
62.833	0.00	0.21	0.409	IO				0.95
62.917	0.00	0.21	0.408	IO				0.95
63.000	0.00	0.21	0.406	IO				0.94
63.083	0.00	0.21	0.405	IO				0.94
63.167	0.00	0.21	0.403	IO				0.94
63.250	0.00	0.21	0.402	IO				0.93
63.333	0.00	0.21	0.401	IO				0.93
63.417	0.00	0.21	0.399	IO				0.93
63.500	0.00	0.21	0.398	IO				0.92
63.583	0.00	0.21	0.396	IO				0.92
63.667	0.00	0.21	0.395	IO				0.92
63.750	0.00	0.21	0.393	IO				0.91
63.833	0.00	0.20	0.392	IO				0.91
63.917	0.00	0.20	0.391	IO				0.91
64.000	0.00	0.20	0.389	IO				0.90
64.083	0.00	0.20	0.388	IO				0.90
64.167	0.00	0.20	0.386	IO				0.90
64.250	0.00	0.20	0.385	IO				0.89
64.333	0.00	0.20	0.384	IO				0.89
64.417	0.00	0.20	0.382	O				0.89
64.500	0.00	0.20	0.381	O				0.88
64.583	0.00	0.20	0.380	O				0.88
64.667	0.00	0.20	0.378	O				0.88
64.750	0.00	0.20	0.377	O				0.87
64.833	0.00	0.20	0.375	O				0.87
64.917	0.00	0.20	0.374	O				0.87
65.000	0.00	0.19	0.373	O				0.86
65.083	0.00	0.19	0.371	O				0.86
65.167	0.00	0.19	0.370	O				0.86
65.250	0.00	0.19	0.369	O				0.86
65.333	0.00	0.19	0.367	O				0.85
65.417	0.00	0.19	0.366	O				0.85
65.500	0.00	0.19	0.365	O				0.85
65.583	0.00	0.19	0.363	O				0.84
65.667	0.00	0.19	0.362	O				0.84
65.750	0.00	0.19	0.361	O				0.84
65.833	0.00	0.19	0.360	O				0.83
65.917	0.00	0.19	0.358	O				0.83
66.000	0.00	0.19	0.357	O				0.83

66.083	0.00	0.19	0.356	o	|	|	|	0.83
66.167	0.00	0.19	0.354	o	|	|	|	0.82
66.250	0.00	0.18	0.353	o	|	|	|	0.82
66.333	0.00	0.18	0.352	o	|	|	|	0.82
66.417	0.00	0.18	0.351	o	|	|	|	0.81
66.500	0.00	0.18	0.349	o	|	|	|	0.81
66.583	0.00	0.18	0.348	o	|	|	|	0.81
66.667	0.00	0.18	0.347	o	|	|	|	0.80
66.750	0.00	0.18	0.346	o	|	|	|	0.80
66.833	0.00	0.18	0.344	o	|	|	|	0.80
66.917	0.00	0.18	0.343	o	|	|	|	0.80
67.000	0.00	0.18	0.342	o	|	|	|	0.79
67.083	0.00	0.18	0.341	o	|	|	|	0.79
67.167	0.00	0.18	0.339	o	|	|	|	0.79
67.250	0.00	0.18	0.338	o	|	|	|	0.78
67.333	0.00	0.18	0.337	o	|	|	|	0.78
67.417	0.00	0.18	0.336	o	|	|	|	0.78
67.500	0.00	0.17	0.335	o	|	|	|	0.78
67.583	0.00	0.17	0.333	o	|	|	|	0.77
67.667	0.00	0.17	0.332	o	|	|	|	0.77
67.750	0.00	0.17	0.331	o	|	|	|	0.77
67.833	0.00	0.17	0.330	o	|	|	|	0.77
67.917	0.00	0.17	0.329	o	|	|	|	0.76
68.000	0.00	0.17	0.328	o	|	|	|	0.76
68.083	0.00	0.17	0.326	o	|	|	|	0.76
68.167	0.00	0.17	0.325	o	|	|	|	0.75
68.250	0.00	0.17	0.324	o	|	|	|	0.75
68.333	0.00	0.17	0.323	o	|	|	|	0.75
68.417	0.00	0.17	0.322	o	|	|	|	0.75
68.500	0.00	0.17	0.321	o	|	|	|	0.74
68.583	0.00	0.17	0.319	o	|	|	|	0.74
68.667	0.00	0.17	0.318	o	|	|	|	0.74
68.750	0.00	0.17	0.317	o	|	|	|	0.74
68.833	0.00	0.16	0.316	o	|	|	|	0.73
68.917	0.00	0.16	0.315	o	|	|	|	0.73
69.000	0.00	0.16	0.314	o	|	|	|	0.73
69.083	0.00	0.16	0.313	o	|	|	|	0.73
69.167	0.00	0.16	0.311	o	|	|	|	0.72
69.250	0.00	0.16	0.310	o	|	|	|	0.72
69.333	0.00	0.16	0.309	o	|	|	|	0.72
69.417	0.00	0.16	0.308	o	|	|	|	0.71
69.500	0.00	0.16	0.307	o	|	|	|	0.71
69.583	0.00	0.16	0.306	o	|	|	|	0.71
69.667	0.00	0.16	0.305	o	|	|	|	0.71
69.750	0.00	0.16	0.304	o	|	|	|	0.70
69.833	0.00	0.16	0.303	o	|	|	|	0.70
69.917	0.00	0.16	0.302	o	|	|	|	0.70
70.000	0.00	0.16	0.300	o	|	|	|	0.70
70.083	0.00	0.16	0.299	o	|	|	|	0.69
70.167	0.00	0.16	0.298	o	|	|	|	0.69
70.250	0.00	0.16	0.297	o	|	|	|	0.69
70.333	0.00	0.15	0.296	o	|	|	|	0.69
70.417	0.00	0.15	0.295	o	|	|	|	0.68
70.500	0.00	0.15	0.294	o	|	|	|	0.68
70.583	0.00	0.15	0.293	o	|	|	|	0.68
70.667	0.00	0.15	0.292	o	|	|	|	0.68
70.750	0.00	0.15	0.291	o	|	|	|	0.67
70.833	0.00	0.15	0.290	o	|	|	|	0.67
70.917	0.00	0.15	0.289	o	|	|	|	0.67
71.000	0.00	0.15	0.288	o	|	|	|	0.67
71.083	0.00	0.15	0.287	o	|	|	|	0.67
71.167	0.00	0.15	0.286	o	|	|	|	0.66
71.250	0.00	0.15	0.285	o	|	|	|	0.66
71.333	0.00	0.15	0.284	o	|	|	|	0.66
71.417	0.00	0.15	0.283	o	|	|	|	0.66
71.500	0.00	0.15	0.282	o	|	|	|	0.65
71.583	0.00	0.15	0.281	o	|	|	|	0.65
71.667	0.00	0.15	0.280	o	|	|	|	0.65
71.750	0.00	0.15	0.279	o	|	|	|	0.65
71.833	0.00	0.14	0.278	o	|	|	|	0.64
71.917	0.00	0.14	0.277	o	|	|	|	0.64
72.000	0.00	0.14	0.276	o	|	|	|	0.64
72.083	0.00	0.14	0.275	o	|	|	|	0.64
72.167	0.00	0.14	0.274	o	|	|	|	0.63
72.250	0.00	0.14	0.273	o	|	|	|	0.63
72.333	0.00	0.14	0.272	o	|	|	|	0.63
72.417	0.00	0.14	0.271	o	|	|	|	0.63
72.500	0.00	0.14	0.270	o	|	|	|	0.63
72.583	0.00	0.14	0.269	o	|	|	|	0.62
72.667	0.00	0.14	0.268	o	|	|	|	0.62
72.750	0.00	0.14	0.267	o	|	|	|	0.62
72.833	0.00	0.14	0.266	o	|	|	|	0.62
72.917	0.00	0.14	0.265	o	|	|	|	0.61
73.000	0.00	0.14	0.264	o	|	|	|	0.61
73.083	0.00	0.14	0.263	o	|	|	|	0.61
73.167	0.00	0.14	0.262	o	|	|	|	0.61

73.250	0.00	0.14	0.261	o	|	|	|	|	0.61
73.333	0.00	0.14	0.260	o	|	|	|	|	0.60
73.417	0.00	0.14	0.259	o	|	|	|	|	0.60
73.500	0.00	0.13	0.258	o	|	|	|	|	0.60
73.583	0.00	0.13	0.257	o	|	|	|	|	0.60
73.667	0.00	0.13	0.256	o	|	|	|	|	0.60
73.750	0.00	0.13	0.256	o	|	|	|	|	0.59
73.833	0.00	0.13	0.255	o	|	|	|	|	0.59
73.917	0.00	0.13	0.254	o	|	|	|	|	0.59
74.000	0.00	0.13	0.253	o	|	|	|	|	0.59
74.083	0.00	0.13	0.252	o	|	|	|	|	0.58
74.167	0.00	0.13	0.251	o	|	|	|	|	0.58
74.250	0.00	0.13	0.250	o	|	|	|	|	0.58
74.333	0.00	0.13	0.249	o	|	|	|	|	0.58
74.417	0.00	0.13	0.248	o	|	|	|	|	0.58
74.500	0.00	0.13	0.247	o	|	|	|	|	0.57
74.583	0.00	0.13	0.247	o	|	|	|	|	0.57
74.667	0.00	0.13	0.246	o	|	|	|	|	0.57
74.750	0.00	0.13	0.245	o	|	|	|	|	0.57
74.833	0.00	0.13	0.244	o	|	|	|	|	0.57
74.917	0.00	0.13	0.243	o	|	|	|	|	0.56
75.000	0.00	0.13	0.242	o	|	|	|	|	0.56
75.083	0.00	0.13	0.241	o	|	|	|	|	0.56
75.167	0.00	0.13	0.240	o	|	|	|	|	0.56
75.250	0.00	0.13	0.240	o	|	|	|	|	0.56
75.333	0.00	0.12	0.239	o	|	|	|	|	0.55
75.417	0.00	0.12	0.238	o	|	|	|	|	0.55
75.500	0.00	0.12	0.237	o	|	|	|	|	0.55
75.583	0.00	0.12	0.236	o	|	|	|	|	0.55
75.667	0.00	0.12	0.235	o	|	|	|	|	0.55
75.750	0.00	0.12	0.234	o	|	|	|	|	0.54
75.833	0.00	0.12	0.234	o	|	|	|	|	0.54
75.917	0.00	0.12	0.233	o	|	|	|	|	0.54
76.000	0.00	0.12	0.232	o	|	|	|	|	0.54
76.083	0.00	0.12	0.231	o	|	|	|	|	0.54
76.167	0.00	0.12	0.230	o	|	|	|	|	0.53
76.250	0.00	0.12	0.229	o	|	|	|	|	0.53
76.333	0.00	0.12	0.229	o	|	|	|	|	0.53
76.417	0.00	0.12	0.228	o	|	|	|	|	0.53
76.500	0.00	0.12	0.227	o	|	|	|	|	0.53
76.583	0.00	0.12	0.226	o	|	|	|	|	0.52
76.667	0.00	0.12	0.225	o	|	|	|	|	0.52
76.750	0.00	0.12	0.225	o	|	|	|	|	0.52
76.833	0.00	0.12	0.224	o	|	|	|	|	0.52
76.917	0.00	0.12	0.223	o	|	|	|	|	0.52
77.000	0.00	0.12	0.222	o	|	|	|	|	0.52
77.083	0.00	0.12	0.221	o	|	|	|	|	0.51
77.167	0.00	0.12	0.221	o	|	|	|	|	0.51
77.250	0.00	0.11	0.220	o	|	|	|	|	0.51
77.333	0.00	0.11	0.219	o	|	|	|	|	0.51
77.417	0.00	0.11	0.218	o	|	|	|	|	0.51
77.500	0.00	0.11	0.217	o	|	|	|	|	0.50
77.583	0.00	0.11	0.217	o	|	|	|	|	0.50
77.667	0.00	0.11	0.216	o	|	|	|	|	0.50
77.750	0.00	0.11	0.215	o	|	|	|	|	0.50
77.833	0.00	0.11	0.214	o	|	|	|	|	0.50
77.917	0.00	0.11	0.214	o	|	|	|	|	0.50
78.000	0.00	0.11	0.213	o	|	|	|	|	0.49
78.083	0.00	0.11	0.212	o	|	|	|	|	0.49
78.167	0.00	0.11	0.211	o	|	|	|	|	0.49
78.250	0.00	0.11	0.210	o	|	|	|	|	0.49
78.333	0.00	0.11	0.210	o	|	|	|	|	0.49
78.417	0.00	0.11	0.209	o	|	|	|	|	0.48
78.500	0.00	0.11	0.208	o	|	|	|	|	0.48
78.583	0.00	0.11	0.207	o	|	|	|	|	0.48
78.667	0.00	0.11	0.207	o	|	|	|	|	0.48
78.750	0.00	0.11	0.206	o	|	|	|	|	0.48
78.833	0.00	0.11	0.205	o	|	|	|	|	0.48
78.917	0.00	0.11	0.204	o	|	|	|	|	0.47
79.000	0.00	0.11	0.204	o	|	|	|	|	0.47
79.083	0.00	0.11	0.203	o	|	|	|	|	0.47
79.167	0.00	0.11	0.202	o	|	|	|	|	0.47
79.250	0.00	0.11	0.202	o	|	|	|	|	0.47
79.333	0.00	0.10	0.201	o	|	|	|	|	0.47
79.417	0.00	0.10	0.200	o	|	|	|	|	0.46
79.500	0.00	0.10	0.199	o	|	|	|	|	0.46
79.583	0.00	0.10	0.199	o	|	|	|	|	0.46
79.667	0.00	0.10	0.198	o	|	|	|	|	0.46
79.750	0.00	0.10	0.197	o	|	|	|	|	0.46
79.833	0.00	0.10	0.197	o	|	|	|	|	0.46
79.917	0.00	0.10	0.196	o	|	|	|	|	0.45
80.000	0.00	0.10	0.195	o	|	|	|	|	0.45
80.083	0.00	0.10	0.194	o	|	|	|	|	0.45
80.167	0.00	0.10	0.194	o	|	|	|	|	0.45
80.250	0.00	0.10	0.193	o	|	|	|	|	0.45
80.333	0.00	0.10	0.192	o	|	|	|	|	0.45

```
80.417    0.00    0.10      0.192  O       |       |       |       |     0.44
80.500    0.00    0.10      0.191  O       |       |       |       |     0.44

       Remaining water in basin =    0.19 (Ac.Ft)


       ****************************HYDROGRAPH DATA****************************
                     Number of intervals =   966
                     Time interval =    5.0 (Min.)
                     Maximum/Peak flow rate =        1.728 (CFS)
                     Total volume =       3.694 (Ac.Ft)
              Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
       ***********************************************************************

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FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro2515.rte
**********HYDROGRAPH DATA**********
Number of intervals = 17
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 68.734 (CFS)
Total volume = 1.944 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 17
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.431	0.225	0.430	0.432
2.000	0.914	0.344	0.913	0.915
3.000	1.451	0.991	1.448	1.454
4.000	2.049	1.417	2.044	2.054
5.000	2.712	1.731	2.706	2.718
5.250	2.888	1.801	2.882	2.894
5.500	3.069	17.046	3.010	3.128
6.000	3.443	225.078	2.668	4.218

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 17.2 34.37 51.55 68.73	Depth (Ft.)
0.083	2.08	0.00	0.007	O | | | |	0.02
0.167	6.06	0.02	0.035	O I | | | |	0.08
0.250	7.98	0.04	0.083	O I | | | |	0.19
0.333	9.06	0.07	0.141	O I | | | |	0.33
0.417	10.09	0.11	0.207	O I | | | |	0.48
0.500	11.48	0.15	0.280	O I | | | |	0.65
0.583	13.09	0.19	0.364	O I | | | |	0.84
0.667	16.04	0.23	0.463	O I | | | |	1.07
0.750	26.03	0.27	0.606	O | I | | |	1.36
0.833	59.60	0.34	0.898	O | | | I |	1.97
0.917	68.73	0.85	1.336	O | | | I	2.79
1.000	27.59	1.14	1.661	O | I | | |	3.35
1.083	13.98	1.24	1.796	O I | | | |	3.58
1.167	6.28	1.28	1.857	O I | | | |	3.68
1.250	3.50	1.30	1.882	OI | | | |	3.72
1.333	0.58	1.30	1.887	O | | | |	3.73
1.417	0.18	1.30	1.881	O | | | |	3.72
1.500	0.00	1.29	1.872	O | | | |	3.70

1.583	0.00	1.28	1.863	o	|	|	|	3.69
1.667	0.00	1.28	1.855	o	|	|	|	3.67
1.750	0.00	1.27	1.846	o	|	|	|	3.66
1.833	0.00	1.27	1.837	o	|	|	|	3.65
1.917	0.00	1.26	1.828	o	|	|	|	3.63
2.000	0.00	1.25	1.820	o	|	|	|	3.62
2.083	0.00	1.25	1.811	o	|	|	|	3.60
2.167	0.00	1.24	1.803	o	|	|	|	3.59
2.250	0.00	1.24	1.794	o	|	|	|	3.57
2.333	0.00	1.23	1.786	o	|	|	|	3.56
2.417	0.00	1.22	1.777	o	|	|	|	3.55
2.500	0.00	1.22	1.769	o	|	|	|	3.53
2.583	0.00	1.21	1.760	o	|	|	|	3.52
2.667	0.00	1.21	1.752	o	|	|	|	3.50
2.750	0.00	1.20	1.744	o	|	|	|	3.49
2.833	0.00	1.19	1.735	o	|	|	|	3.48
2.917	0.00	1.19	1.727	o	|	|	|	3.46
3.000	0.00	1.18	1.719	o	|	|	|	3.45
3.083	0.00	1.18	1.711	o	|	|	|	3.43
3.167	0.00	1.17	1.703	o	|	|	|	3.42
3.250	0.00	1.16	1.695	o	|	|	|	3.41
3.333	0.00	1.16	1.687	o	|	|	|	3.39
3.417	0.00	1.15	1.679	o	|	|	|	3.38
3.500	0.00	1.15	1.671	o	|	|	|	3.37
3.583	0.00	1.14	1.663	o	|	|	|	3.35
3.667	0.00	1.14	1.655	o	|	|	|	3.34
3.750	0.00	1.13	1.647	o	|	|	|	3.33
3.833	0.00	1.13	1.640	o	|	|	|	3.32
3.917	0.00	1.12	1.632	o	|	|	|	3.30
4.000	0.00	1.11	1.624	o	|	|	|	3.29
4.083	0.00	1.11	1.617	o	|	|	|	3.28
4.167	0.00	1.10	1.609	o	|	|	|	3.26
4.250	0.00	1.10	1.601	o	|	|	|	3.25
4.333	0.00	1.09	1.594	o	|	|	|	3.24
4.417	0.00	1.09	1.586	o	|	|	|	3.23
4.500	0.00	1.08	1.579	o	|	|	|	3.21
4.583	0.00	1.08	1.571	o	|	|	|	3.20
4.667	0.00	1.07	1.564	o	|	|	|	3.19
4.750	0.00	1.07	1.557	o	|	|	|	3.18
4.833	0.00	1.06	1.549	o	|	|	|	3.16
4.917	0.00	1.06	1.542	o	|	|	|	3.15
5.000	0.00	1.05	1.535	o	|	|	|	3.14
5.083	0.00	1.05	1.528	o	|	|	|	3.13
5.167	0.00	1.04	1.520	o	|	|	|	3.12
5.250	0.00	1.04	1.513	o	|	|	|	3.10
5.333	0.00	1.03	1.506	o	|	|	|	3.09
5.417	0.00	1.03	1.499	o	|	|	|	3.08
5.500	0.00	1.02	1.492	o	|	|	|	3.07
5.583	0.00	1.02	1.485	o	|	|	|	3.06
5.667	0.00	1.01	1.478	o	|	|	|	3.05
5.750	0.00	1.01	1.471	o	|	|	|	3.03
5.833	0.00	1.00	1.464	o	|	|	|	3.02
5.917	0.00	1.00	1.457	o	|	|	|	3.01
6.000	0.00	0.99	1.450	o	|	|	|	3.00
6.083	0.00	0.98	1.444	o	|	|	|	2.99
6.167	0.00	0.97	1.437	o	|	|	|	2.97
6.250	0.00	0.97	1.430	o	|	|	|	2.96
6.333	0.00	0.96	1.424	o	|	|	|	2.95
6.417	0.00	0.95	1.417	o	|	|	|	2.94
6.500	0.00	0.94	1.411	o	|	|	|	2.92
6.583	0.00	0.93	1.404	o	|	|	|	2.91
6.667	0.00	0.93	1.398	o	|	|	|	2.90
6.750	0.00	0.92	1.391	o	|	|	|	2.89
6.833	0.00	0.91	1.385	o	|	|	|	2.88
6.917	0.00	0.90	1.379	o	|	|	|	2.87
7.000	0.00	0.90	1.373	o	|	|	|	2.85
7.083	0.00	0.89	1.366	o	|	|	|	2.84
7.167	0.00	0.88	1.360	o	|	|	|	2.83
7.250	0.00	0.87	1.354	o	|	|	|	2.82
7.333	0.00	0.87	1.348	o	|	|	|	2.81
7.417	0.00	0.86	1.342	o	|	|	|	2.80
7.500	0.00	0.85	1.336	o	|	|	|	2.79
7.583	0.00	0.85	1.331	o	|	|	|	2.78
7.667	0.00	0.84	1.325	o	|	|	|	2.76
7.750	0.00	0.83	1.319	o	|	|	|	2.75
7.833	0.00	0.83	1.313	o	|	|	|	2.74
7.917	0.00	0.82	1.308	o	|	|	|	2.73
8.000	0.00	0.81	1.302	o	|	|	|	2.72
8.083	0.00	0.80	1.296	o	|	|	|	2.71
8.167	0.00	0.80	1.291	o	|	|	|	2.70
8.250	0.00	0.79	1.285	o	|	|	|	2.69
8.333	0.00	0.79	1.280	o	|	|	|	2.68
8.417	0.00	0.78	1.275	o	|	|	|	2.67
8.500	0.00	0.77	1.269	o	|	|	|	2.66
8.583	0.00	0.77	1.264	o	|	|	|	2.65
8.667	0.00	0.76	1.259	o	|	|	|	2.64

8.750	0.00	0.75	1.254	o	|	|	|	|	2.63
8.833	0.00	0.75	1.248	o	|	|	|	|	2.62
8.917	0.00	0.74	1.243	o	|	|	|	|	2.61
9.000	0.00	0.73	1.238	o	|	|	|	|	2.60
9.083	0.00	0.73	1.233	o	|	|	|	|	2.59
9.167	0.00	0.72	1.228	o	|	|	|	|	2.59
9.250	0.00	0.72	1.223	o	|	|	|	|	2.58
9.333	0.00	0.71	1.218	o	|	|	|	|	2.57
9.417	0.00	0.70	1.213	o	|	|	|	|	2.56
9.500	0.00	0.70	1.209	o	|	|	|	|	2.55
9.583	0.00	0.69	1.204	o	|	|	|	|	2.54
9.667	0.00	0.69	1.199	o	|	|	|	|	2.53
9.750	0.00	0.68	1.194	o	|	|	|	|	2.52
9.833	0.00	0.68	1.190	o	|	|	|	|	2.51
9.917	0.00	0.67	1.185	o	|	|	|	|	2.50
10.000	0.00	0.67	1.180	o	|	|	|	|	2.50
10.083	0.00	0.66	1.176	o	|	|	|	|	2.49
10.167	0.00	0.65	1.171	o	|	|	|	|	2.48
10.250	0.00	0.65	1.167	o	|	|	|	|	2.47
10.333	0.00	0.64	1.162	o	|	|	|	|	2.46
10.417	0.00	0.64	1.158	o	|	|	|	|	2.45
10.500	0.00	0.63	1.154	o	|	|	|	|	2.45
10.583	0.00	0.63	1.149	o	|	|	|	|	2.44
10.667	0.00	0.62	1.145	o	|	|	|	|	2.43
10.750	0.00	0.62	1.141	o	|	|	|	|	2.42
10.833	0.00	0.61	1.136	o	|	|	|	|	2.41
10.917	0.00	0.61	1.132	o	|	|	|	|	2.41
11.000	0.00	0.60	1.128	o	|	|	|	|	2.40
11.083	0.00	0.60	1.124	o	|	|	|	|	2.39
11.167	0.00	0.59	1.120	o	|	|	|	|	2.38
11.250	0.00	0.59	1.116	o	|	|	|	|	2.38
11.333	0.00	0.58	1.112	o	|	|	|	|	2.37
11.417	0.00	0.58	1.108	o	|	|	|	|	2.36
11.500	0.00	0.57	1.104	o	|	|	|	|	2.35
11.583	0.00	0.57	1.100	o	|	|	|	|	2.35
11.667	0.00	0.56	1.096	o	|	|	|	|	2.34
11.750	0.00	0.56	1.092	o	|	|	|	|	2.33
11.833	0.00	0.55	1.088	o	|	|	|	|	2.32
11.917	0.00	0.55	1.085	o	|	|	|	|	2.32
12.000	0.00	0.54	1.081	o	|	|	|	|	2.31
12.083	0.00	0.54	1.077	o	|	|	|	|	2.30
12.167	0.00	0.54	1.073	o	|	|	|	|	2.30
12.250	0.00	0.53	1.070	o	|	|	|	|	2.29
12.333	0.00	0.53	1.066	o	|	|	|	|	2.28
12.417	0.00	0.52	1.062	o	|	|	|	|	2.28
12.500	0.00	0.52	1.059	o	|	|	|	|	2.27
12.583	0.00	0.51	1.055	o	|	|	|	|	2.26
12.667	0.00	0.51	1.052	o	|	|	|	|	2.26
12.750	0.00	0.51	1.048	o	|	|	|	|	2.25
12.833	0.00	0.50	1.045	o	|	|	|	|	2.24
12.917	0.00	0.50	1.041	o	|	|	|	|	2.24
13.000	0.00	0.49	1.038	o	|	|	|	|	2.23
13.083	0.00	0.49	1.035	o	|	|	|	|	2.22
13.167	0.00	0.49	1.031	o	|	|	|	|	2.22
13.250	0.00	0.48	1.028	o	|	|	|	|	2.21
13.333	0.00	0.48	1.025	o	|	|	|	|	2.21
13.417	0.00	0.47	1.021	o	|	|	|	|	2.20
13.500	0.00	0.47	1.018	o	|	|	|	|	2.19
13.583	0.00	0.47	1.015	o	|	|	|	|	2.19
13.667	0.00	0.46	1.012	o	|	|	|	|	2.18
13.750	0.00	0.46	1.008	o	|	|	|	|	2.18
13.833	0.00	0.45	1.005	o	|	|	|	|	2.17
13.917	0.00	0.45	1.002	o	|	|	|	|	2.16
14.000	0.00	0.45	0.999	o	|	|	|	|	2.16
14.083	0.00	0.44	0.996	o	|	|	|	|	2.15
14.167	0.00	0.44	0.993	o	|	|	|	|	2.15
14.250	0.00	0.44	0.990	o	|	|	|	|	2.14
14.333	0.00	0.43	0.987	o	|	|	|	|	2.14
14.417	0.00	0.43	0.984	o	|	|	|	|	2.13
14.500	0.00	0.42	0.981	o	|	|	|	|	2.12
14.583	0.00	0.42	0.978	o	|	|	|	|	2.12
14.667	0.00	0.42	0.975	o	|	|	|	|	2.11
14.750	0.00	0.41	0.972	o	|	|	|	|	2.11
14.833	0.00	0.41	0.970	o	|	|	|	|	2.10
14.917	0.00	0.41	0.967	o	|	|	|	|	2.10
15.000	0.00	0.40	0.964	o	|	|	|	|	2.09
15.083	0.00	0.40	0.961	o	|	|	|	|	2.09
15.167	0.00	0.40	0.958	o	|	|	|	|	2.08
15.250	0.00	0.39	0.956	o	|	|	|	|	2.08
15.333	0.00	0.39	0.953	o	|	|	|	|	2.07
15.417	0.00	0.39	0.950	o	|	|	|	|	2.07
15.500	0.00	0.38	0.948	o	|	|	|	|	2.06
15.583	0.00	0.38	0.945	o	|	|	|	|	2.06
15.667	0.00	0.38	0.942	o	|	|	|	|	2.05
15.750	0.00	0.38	0.940	o	|	|	|	|	2.05
15.833	0.00	0.37	0.937	o	|	|	|	|	2.04

15.917	0.00	0.37	0.935	o	|	|	|	|	2.04
16.000	0.00	0.37	0.932	o	|	|	|	|	2.03
16.083	0.00	0.36	0.930	o	|	|	|	|	2.03
16.167	0.00	0.36	0.927	o	|	|	|	|	2.02
16.250	0.00	0.36	0.925	o	|	|	|	|	2.02
16.333	0.00	0.35	0.922	o	|	|	|	|	2.02
16.417	0.00	0.35	0.920	o	|	|	|	|	2.01
16.500	0.00	0.35	0.917	o	|	|	|	|	2.01
16.583	0.00	0.35	0.915	o	|	|	|	|	2.00
16.667	0.00	0.34	0.913	o	|	|	|	|	2.00
16.750	0.00	0.34	0.910	o	|	|	|	|	1.99
16.833	0.00	0.34	0.908	o	|	|	|	|	1.99
16.917	0.00	0.34	0.906	o	|	|	|	|	1.98
17.000	0.00	0.34	0.903	o	|	|	|	|	1.98
17.083	0.00	0.34	0.901	o	|	|	|	|	1.97
17.167	0.00	0.34	0.899	o	|	|	|	|	1.97
17.250	0.00	0.34	0.896	o	|	|	|	|	1.96
17.333	0.00	0.34	0.894	o	|	|	|	|	1.96
17.417	0.00	0.34	0.892	o	|	|	|	|	1.95
17.500	0.00	0.34	0.889	o	|	|	|	|	1.95
17.583	0.00	0.34	0.887	o	|	|	|	|	1.94
17.667	0.00	0.34	0.885	o	|	|	|	|	1.94
17.750	0.00	0.34	0.882	o	|	|	|	|	1.93
17.833	0.00	0.34	0.880	o	|	|	|	|	1.93
17.917	0.00	0.34	0.878	o	|	|	|	|	1.92
18.000	0.00	0.33	0.875	o	|	|	|	|	1.92
18.083	0.00	0.33	0.873	o	|	|	|	|	1.92
18.167	0.00	0.33	0.871	o	|	|	|	|	1.91
18.250	0.00	0.33	0.868	o	|	|	|	|	1.91
18.333	0.00	0.33	0.866	o	|	|	|	|	1.90
18.417	0.00	0.33	0.864	o	|	|	|	|	1.90
18.500	0.00	0.33	0.862	o	|	|	|	|	1.89
18.583	0.00	0.33	0.859	o	|	|	|	|	1.89
18.667	0.00	0.33	0.857	o	|	|	|	|	1.88
18.750	0.00	0.33	0.855	o	|	|	|	|	1.88
18.833	0.00	0.33	0.852	o	|	|	|	|	1.87
18.917	0.00	0.33	0.850	o	|	|	|	|	1.87
19.000	0.00	0.33	0.848	o	|	|	|	|	1.86
19.083	0.00	0.33	0.846	o	|	|	|	|	1.86
19.167	0.00	0.33	0.843	o	|	|	|	|	1.85
19.250	0.00	0.33	0.841	o	|	|	|	|	1.85
19.333	0.00	0.33	0.839	o	|	|	|	|	1.84
19.417	0.00	0.32	0.837	o	|	|	|	|	1.84
19.500	0.00	0.32	0.834	o	|	|	|	|	1.84
19.583	0.00	0.32	0.832	o	|	|	|	|	1.83
19.667	0.00	0.32	0.830	o	|	|	|	|	1.83
19.750	0.00	0.32	0.828	o	|	|	|	|	1.82
19.833	0.00	0.32	0.826	o	|	|	|	|	1.82
19.917	0.00	0.32	0.823	o	|	|	|	|	1.81
20.000	0.00	0.32	0.821	o	|	|	|	|	1.81
20.083	0.00	0.32	0.819	o	|	|	|	|	1.80
20.167	0.00	0.32	0.817	o	|	|	|	|	1.80
20.250	0.00	0.32	0.815	o	|	|	|	|	1.79
20.333	0.00	0.32	0.812	o	|	|	|	|	1.79
20.417	0.00	0.32	0.810	o	|	|	|	|	1.78
20.500	0.00	0.32	0.808	o	|	|	|	|	1.78
20.583	0.00	0.32	0.806	o	|	|	|	|	1.78
20.667	0.00	0.32	0.804	o	|	|	|	|	1.77
20.750	0.00	0.32	0.801	o	|	|	|	|	1.77
20.833	0.00	0.32	0.799	o	|	|	|	|	1.76
20.917	0.00	0.32	0.797	o	|	|	|	|	1.76
21.000	0.00	0.31	0.795	o	|	|	|	|	1.75
21.083	0.00	0.31	0.793	o	|	|	|	|	1.75
21.167	0.00	0.31	0.791	o	|	|	|	|	1.74
21.250	0.00	0.31	0.788	o	|	|	|	|	1.74
21.333	0.00	0.31	0.786	o	|	|	|	|	1.74
21.417	0.00	0.31	0.784	o	|	|	|	|	1.73
21.500	0.00	0.31	0.782	o	|	|	|	|	1.73
21.583	0.00	0.31	0.780	o	|	|	|	|	1.72
21.667	0.00	0.31	0.778	o	|	|	|	|	1.72
21.750	0.00	0.31	0.776	o	|	|	|	|	1.71
21.833	0.00	0.31	0.773	o	|	|	|	|	1.71
21.917	0.00	0.31	0.771	o	|	|	|	|	1.70
22.000	0.00	0.31	0.769	o	|	|	|	|	1.70
22.083	0.00	0.31	0.767	o	|	|	|	|	1.70
22.167	0.00	0.31	0.765	o	|	|	|	|	1.69
22.250	0.00	0.31	0.763	o	|	|	|	|	1.69
22.333	0.00	0.31	0.761	o	|	|	|	|	1.68
22.417	0.00	0.31	0.759	o	|	|	|	|	1.68
22.500	0.00	0.31	0.756	o	|	|	|	|	1.67
22.583	0.00	0.30	0.754	o	|	|	|	|	1.67
22.667	0.00	0.30	0.752	o	|	|	|	|	1.67
22.750	0.00	0.30	0.750	o	|	|	|	|	1.66
22.833	0.00	0.30	0.748	o	|	|	|	|	1.66
22.917	0.00	0.30	0.746	o	|	|	|	|	1.65
23.000	0.00	0.30	0.744	o	|	|	|	|	1.65

23.083	0.00	0.30	0.742	o	|	|	|	|	1.64
23.167	0.00	0.30	0.740	o	|	|	|	|	1.64
23.250	0.00	0.30	0.738	o	|	|	|	|	1.63
23.333	0.00	0.30	0.736	o	|	|	|	|	1.63
23.417	0.00	0.30	0.734	o	|	|	|	|	1.63
23.500	0.00	0.30	0.731	o	|	|	|	|	1.62
23.583	0.00	0.30	0.729	o	|	|	|	|	1.62
23.667	0.00	0.30	0.727	o	|	|	|	|	1.61
23.750	0.00	0.30	0.725	o	|	|	|	|	1.61
23.833	0.00	0.30	0.723	o	|	|	|	|	1.61
23.917	0.00	0.30	0.721	o	|	|	|	|	1.60
24.000	0.00	0.30	0.719	o	|	|	|	|	1.60
24.083	0.00	0.30	0.717	o	|	|	|	|	1.59
24.167	0.00	0.29	0.715	o	|	|	|	|	1.59
24.250	0.00	0.29	0.713	o	|	|	|	|	1.58
24.333	0.00	0.29	0.711	o	|	|	|	|	1.58
24.417	0.00	0.29	0.709	o	|	|	|	|	1.58
24.500	0.00	0.29	0.707	o	|	|	|	|	1.57
24.583	0.00	0.29	0.705	o	|	|	|	|	1.57
24.667	0.00	0.29	0.703	o	|	|	|	|	1.56
24.750	0.00	0.29	0.701	o	|	|	|	|	1.56
24.833	0.00	0.29	0.699	o	|	|	|	|	1.55
24.917	0.00	0.29	0.697	o	|	|	|	|	1.55
25.000	0.00	0.29	0.695	o	|	|	|	|	1.55
25.083	0.00	0.29	0.693	o	|	|	|	|	1.54
25.167	0.00	0.29	0.691	o	|	|	|	|	1.54
25.250	0.00	0.29	0.689	o	|	|	|	|	1.53
25.333	0.00	0.29	0.687	o	|	|	|	|	1.53
25.417	0.00	0.29	0.685	o	|	|	|	|	1.53
25.500	0.00	0.29	0.683	o	|	|	|	|	1.52
25.583	0.00	0.29	0.681	o	|	|	|	|	1.52
25.667	0.00	0.29	0.679	o	|	|	|	|	1.51
25.750	0.00	0.29	0.677	o	|	|	|	|	1.51
25.833	0.00	0.29	0.675	o	|	|	|	|	1.51
25.917	0.00	0.28	0.673	o	|	|	|	|	1.50
26.000	0.00	0.28	0.671	o	|	|	|	|	1.50
26.083	0.00	0.28	0.669	o	|	|	|	|	1.49
26.167	0.00	0.28	0.667	o	|	|	|	|	1.49
26.250	0.00	0.28	0.665	o	|	|	|	|	1.49
26.333	0.00	0.28	0.663	o	|	|	|	|	1.48
26.417	0.00	0.28	0.661	o	|	|	|	|	1.48
26.500	0.00	0.28	0.660	o	|	|	|	|	1.47
26.583	0.00	0.28	0.658	o	|	|	|	|	1.47
26.667	0.00	0.28	0.656	o	|	|	|	|	1.47
26.750	0.00	0.28	0.654	o	|	|	|	|	1.46
26.833	0.00	0.28	0.652	o	|	|	|	|	1.46
26.917	0.00	0.28	0.650	o	|	|	|	|	1.45
27.000	0.00	0.28	0.648	o	|	|	|	|	1.45
27.083	0.00	0.28	0.646	o	|	|	|	|	1.45
27.167	0.00	0.28	0.644	o	|	|	|	|	1.44
27.250	0.00	0.28	0.642	o	|	|	|	|	1.44
27.333	0.00	0.28	0.640	o	|	|	|	|	1.43
27.417	0.00	0.28	0.638	o	|	|	|	|	1.43
27.500	0.00	0.28	0.637	o	|	|	|	|	1.43
27.583	0.00	0.28	0.635	o	|	|	|	|	1.42
27.667	0.00	0.27	0.633	o	|	|	|	|	1.42
27.750	0.00	0.27	0.631	o	|	|	|	|	1.41
27.833	0.00	0.27	0.629	o	|	|	|	|	1.41
27.917	0.00	0.27	0.627	o	|	|	|	|	1.41
28.000	0.00	0.27	0.625	o	|	|	|	|	1.40
28.083	0.00	0.27	0.623	o	|	|	|	|	1.40
28.167	0.00	0.27	0.621	o	|	|	|	|	1.39
28.250	0.00	0.27	0.620	o	|	|	|	|	1.39
28.333	0.00	0.27	0.618	o	|	|	|	|	1.39
28.417	0.00	0.27	0.616	o	|	|	|	|	1.38
28.500	0.00	0.27	0.614	o	|	|	|	|	1.38
28.583	0.00	0.27	0.612	o	|	|	|	|	1.38
28.667	0.00	0.27	0.610	o	|	|	|	|	1.37
28.750	0.00	0.27	0.608	o	|	|	|	|	1.37
28.833	0.00	0.27	0.607	o	|	|	|	|	1.36
28.917	0.00	0.27	0.605	o	|	|	|	|	1.36
29.000	0.00	0.27	0.603	o	|	|	|	|	1.36
29.083	0.00	0.27	0.601	o	|	|	|	|	1.35
29.167	0.00	0.27	0.599	o	|	|	|	|	1.35
29.250	0.00	0.27	0.597	o	|	|	|	|	1.34
29.333	0.00	0.27	0.596	o	|	|	|	|	1.34
29.417	0.00	0.27	0.594	o	|	|	|	|	1.34
29.500	0.00	0.26	0.592	o	|	|	|	|	1.33
29.583	0.00	0.26	0.590	o	|	|	|	|	1.33
29.667	0.00	0.26	0.588	o	|	|	|	|	1.33
29.750	0.00	0.26	0.586	o	|	|	|	|	1.32
29.833	0.00	0.26	0.585	o	|	|	|	|	1.32
29.917	0.00	0.26	0.583	o	|	|	|	|	1.31
30.000	0.00	0.26	0.581	o	|	|	|	|	1.31
30.083	0.00	0.26	0.579	o	|	|	|	|	1.31
30.167	0.00	0.26	0.577	o	|	|	|	|	1.30

30.250	0.00	0.26	0.576	o	|	|	|	|	1.30
30.333	0.00	0.26	0.574	o	|	|	|	|	1.30
30.417	0.00	0.26	0.572	o	|	|	|	|	1.29
30.500	0.00	0.26	0.570	o	|	|	|	|	1.29
30.583	0.00	0.26	0.568	o	|	|	|	|	1.28
30.667	0.00	0.26	0.567	o	|	|	|	|	1.28
30.750	0.00	0.26	0.565	o	|	|	|	|	1.28
30.833	0.00	0.26	0.563	o	|	|	|	|	1.27
30.917	0.00	0.26	0.561	o	|	|	|	|	1.27
31.000	0.00	0.26	0.560	o	|	|	|	|	1.27
31.083	0.00	0.26	0.558	o	|	|	|	|	1.26
31.167	0.00	0.26	0.556	o	|	|	|	|	1.26
31.250	0.00	0.26	0.554	o	|	|	|	|	1.26
31.333	0.00	0.25	0.553	o	|	|	|	|	1.25
31.417	0.00	0.25	0.551	o	|	|	|	|	1.25
31.500	0.00	0.25	0.549	o	|	|	|	|	1.24
31.583	0.00	0.25	0.547	o	|	|	|	|	1.24
31.667	0.00	0.25	0.546	o	|	|	|	|	1.24
31.750	0.00	0.25	0.544	o	|	|	|	|	1.23
31.833	0.00	0.25	0.542	o	|	|	|	|	1.23
31.917	0.00	0.25	0.540	o	|	|	|	|	1.23
32.000	0.00	0.25	0.539	o	|	|	|	|	1.22
32.083	0.00	0.25	0.537	o	|	|	|	|	1.22
32.167	0.00	0.25	0.535	o	|	|	|	|	1.22
32.250	0.00	0.25	0.533	o	|	|	|	|	1.21
32.333	0.00	0.25	0.532	o	|	|	|	|	1.21
32.417	0.00	0.25	0.530	o	|	|	|	|	1.20
32.500	0.00	0.25	0.528	o	|	|	|	|	1.20
32.583	0.00	0.25	0.527	o	|	|	|	|	1.20
32.667	0.00	0.25	0.525	o	|	|	|	|	1.19
32.750	0.00	0.25	0.523	o	|	|	|	|	1.19
32.833	0.00	0.25	0.521	o	|	|	|	|	1.19
32.917	0.00	0.25	0.520	o	|	|	|	|	1.18
33.000	0.00	0.25	0.518	o	|	|	|	|	1.18
33.083	0.00	0.25	0.516	o	|	|	|	|	1.18
33.167	0.00	0.25	0.515	o	|	|	|	|	1.17
33.250	0.00	0.25	0.513	o	|	|	|	|	1.17
33.333	0.00	0.24	0.511	o	|	|	|	|	1.17
33.417	0.00	0.24	0.510	o	|	|	|	|	1.16
33.500	0.00	0.24	0.508	o	|	|	|	|	1.16
33.583	0.00	0.24	0.506	o	|	|	|	|	1.16
33.667	0.00	0.24	0.505	o	|	|	|	|	1.15
33.750	0.00	0.24	0.503	o	|	|	|	|	1.15
33.833	0.00	0.24	0.501	o	|	|	|	|	1.15
33.917	0.00	0.24	0.500	o	|	|	|	|	1.14
34.000	0.00	0.24	0.498	o	|	|	|	|	1.14
34.083	0.00	0.24	0.496	o	|	|	|	|	1.13
34.167	0.00	0.24	0.495	o	|	|	|	|	1.13
34.250	0.00	0.24	0.493	o	|	|	|	|	1.13
34.333	0.00	0.24	0.491	o	|	|	|	|	1.12
34.417	0.00	0.24	0.490	o	|	|	|	|	1.12
34.500	0.00	0.24	0.488	o	|	|	|	|	1.12
34.583	0.00	0.24	0.486	o	|	|	|	|	1.11
34.667	0.00	0.24	0.485	o	|	|	|	|	1.11
34.750	0.00	0.24	0.483	o	|	|	|	|	1.11
34.833	0.00	0.24	0.481	o	|	|	|	|	1.10
34.917	0.00	0.24	0.480	o	|	|	|	|	1.10
35.000	0.00	0.24	0.478	o	|	|	|	|	1.10
35.083	0.00	0.24	0.476	o	|	|	|	|	1.09
35.167	0.00	0.24	0.475	o	|	|	|	|	1.09
35.250	0.00	0.24	0.473	o	|	|	|	|	1.09
35.333	0.00	0.24	0.472	o	|	|	|	|	1.08
35.417	0.00	0.23	0.470	o	|	|	|	|	1.08
35.500	0.00	0.23	0.468	o	|	|	|	|	1.08
35.583	0.00	0.23	0.467	o	|	|	|	|	1.07
35.667	0.00	0.23	0.465	o	|	|	|	|	1.07
35.750	0.00	0.23	0.464	o	|	|	|	|	1.07
35.833	0.00	0.23	0.462	o	|	|	|	|	1.06
35.917	0.00	0.23	0.460	o	|	|	|	|	1.06
36.000	0.00	0.23	0.459	o	|	|	|	|	1.06
36.083	0.00	0.23	0.457	o	|	|	|	|	1.05
36.167	0.00	0.23	0.456	o	|	|	|	|	1.05
36.250	0.00	0.23	0.454	o	|	|	|	|	1.05
36.333	0.00	0.23	0.452	o	|	|	|	|	1.04
36.417	0.00	0.23	0.451	o	|	|	|	|	1.04
36.500	0.00	0.23	0.449	o	|	|	|	|	1.04
36.583	0.00	0.23	0.448	o	|	|	|	|	1.03
36.667	0.00	0.23	0.446	o	|	|	|	|	1.03
36.750	0.00	0.23	0.444	o	|	|	|	|	1.03
36.833	0.00	0.23	0.443	o	|	|	|	|	1.02
36.917	0.00	0.23	0.441	o	|	|	|	|	1.02
37.000	0.00	0.23	0.440	o	|	|	|	|	1.02
37.083	0.00	0.23	0.438	o	|	|	|	|	1.01
37.167	0.00	0.23	0.437	o	|	|	|	|	1.01
37.250	0.00	0.23	0.435	o	|	|	|	|	1.01
37.333	0.00	0.23	0.434	o	|	|	|	|	1.01

37.417	0.00	0.23	0.432	o	|	|	|	1.00
37.500	0.00	0.22	0.430	o	|	|	|	1.00
37.583	0.00	0.22	0.429	o	|	|	|	1.00
37.667	0.00	0.22	0.427	o	|	|	|	0.99
37.750	0.00	0.22	0.426	o	|	|	|	0.99
37.833	0.00	0.22	0.424	o	|	|	|	0.98
37.917	0.00	0.22	0.423	o	|	|	|	0.98
38.000	0.00	0.22	0.421	o	|	|	|	0.98
38.083	0.00	0.22	0.420	o	|	|	|	0.97
38.167	0.00	0.22	0.418	o	|	|	|	0.97
38.250	0.00	0.22	0.417	o	|	|	|	0.97
38.333	0.00	0.22	0.415	o	|	|	|	0.96
38.417	0.00	0.22	0.414	o	|	|	|	0.96
38.500	0.00	0.22	0.412	o	|	|	|	0.96
38.583	0.00	0.21	0.411	o	|	|	|	0.95
38.667	0.00	0.21	0.409	o	|	|	|	0.95
38.750	0.00	0.21	0.408	o	|	|	|	0.95
38.833	0.00	0.21	0.406	o	|	|	|	0.94
38.917	0.00	0.21	0.405	o	|	|	|	0.94
39.000	0.00	0.21	0.403	o	|	|	|	0.94
39.083	0.00	0.21	0.402	o	|	|	|	0.93
39.167	0.00	0.21	0.401	o	|	|	|	0.93
39.250	0.00	0.21	0.399	o	|	|	|	0.93
39.333	0.00	0.21	0.398	o	|	|	|	0.92
39.417	0.00	0.21	0.396	o	|	|	|	0.92
39.500	0.00	0.21	0.395	o	|	|	|	0.92
39.583	0.00	0.21	0.393	o	|	|	|	0.91
39.667	0.00	0.20	0.392	o	|	|	|	0.91
39.750	0.00	0.20	0.391	o	|	|	|	0.91
39.833	0.00	0.20	0.389	o	|	|	|	0.90
39.917	0.00	0.20	0.388	o	|	|	|	0.90
40.000	0.00	0.20	0.386	o	|	|	|	0.90
40.083	0.00	0.20	0.385	o	|	|	|	0.89
40.167	0.00	0.20	0.384	o	|	|	|	0.89
40.250	0.00	0.20	0.382	o	|	|	|	0.89
40.333	0.00	0.20	0.381	o	|	|	|	0.88
40.417	0.00	0.20	0.380	o	|	|	|	0.88
40.500	0.00	0.20	0.378	o	|	|	|	0.88
40.583	0.00	0.20	0.377	o	|	|	|	0.87
40.667	0.00	0.20	0.375	o	|	|	|	0.87
40.750	0.00	0.20	0.374	o	|	|	|	0.87
40.833	0.00	0.19	0.373	o	|	|	|	0.86
40.917	0.00	0.19	0.371	o	|	|	|	0.86
41.000	0.00	0.19	0.370	o	|	|	|	0.86
41.083	0.00	0.19	0.369	o	|	|	|	0.86
41.167	0.00	0.19	0.367	o	|	|	|	0.85
41.250	0.00	0.19	0.366	o	|	|	|	0.85
41.333	0.00	0.19	0.365	o	|	|	|	0.85
41.417	0.00	0.19	0.364	o	|	|	|	0.84
41.500	0.00	0.19	0.362	o	|	|	|	0.84
41.583	0.00	0.19	0.361	o	|	|	|	0.84
41.667	0.00	0.19	0.360	o	|	|	|	0.83
41.750	0.00	0.19	0.358	o	|	|	|	0.83
41.833	0.00	0.19	0.357	o	|	|	|	0.83
41.917	0.00	0.19	0.356	o	|	|	|	0.83
42.000	0.00	0.19	0.354	o	|	|	|	0.82
42.083	0.00	0.18	0.353	o	|	|	|	0.82
42.167	0.00	0.18	0.352	o	|	|	|	0.82
42.250	0.00	0.18	0.351	o	|	|	|	0.81
42.333	0.00	0.18	0.349	o	|	|	|	0.81
42.417	0.00	0.18	0.348	o	|	|	|	0.81
42.500	0.00	0.18	0.347	o	|	|	|	0.80
42.583	0.00	0.18	0.346	o	|	|	|	0.80
42.667	0.00	0.18	0.344	o	|	|	|	0.80
42.750	0.00	0.18	0.343	o	|	|	|	0.80
42.833	0.00	0.18	0.342	o	|	|	|	0.79
42.917	0.00	0.18	0.341	o	|	|	|	0.79
43.000	0.00	0.18	0.340	o	|	|	|	0.79
43.083	0.00	0.18	0.338	o	|	|	|	0.78
43.167	0.00	0.18	0.337	o	|	|	|	0.78
43.250	0.00	0.18	0.336	o	|	|	|	0.78
43.333	0.00	0.17	0.335	o	|	|	|	0.78
43.417	0.00	0.17	0.333	o	|	|	|	0.77
43.500	0.00	0.17	0.332	o	|	|	|	0.77
43.583	0.00	0.17	0.331	o	|	|	|	0.77
43.667	0.00	0.17	0.330	o	|	|	|	0.77
43.750	0.00	0.17	0.329	o	|	|	|	0.76
43.833	0.00	0.17	0.328	o	|	|	|	0.76
43.917	0.00	0.17	0.326	o	|	|	|	0.76
44.000	0.00	0.17	0.325	o	|	|	|	0.75
44.083	0.00	0.17	0.324	o	|	|	|	0.75
44.167	0.00	0.17	0.323	o	|	|	|	0.75
44.250	0.00	0.17	0.322	o	|	|	|	0.75
44.333	0.00	0.17	0.321	o	|	|	|	0.74
44.417	0.00	0.17	0.319	o	|	|	|	0.74
44.500	0.00	0.17	0.318	o	|	|	|	0.74

44.583	0.00	0.17	0.317	o	|	|	|	|	0.74
44.667	0.00	0.16	0.316	o	|	|	|	|	0.73
44.750	0.00	0.16	0.315	o	|	|	|	|	0.73
44.833	0.00	0.16	0.314	o	|	|	|	|	0.73
44.917	0.00	0.16	0.313	o	|	|	|	|	0.73
45.000	0.00	0.16	0.311	o	|	|	|	|	0.72
45.083	0.00	0.16	0.310	o	|	|	|	|	0.72
45.167	0.00	0.16	0.309	o	|	|	|	|	0.72
45.250	0.00	0.16	0.308	o	|	|	|	|	0.71
45.333	0.00	0.16	0.307	o	|	|	|	|	0.71
45.417	0.00	0.16	0.306	o	|	|	|	|	0.71
45.500	0.00	0.16	0.305	o	|	|	|	|	0.71
45.583	0.00	0.16	0.304	o	|	|	|	|	0.70
45.667	0.00	0.16	0.303	o	|	|	|	|	0.70
45.750	0.00	0.16	0.302	o	|	|	|	|	0.70
45.833	0.00	0.16	0.300	o	|	|	|	|	0.70
45.917	0.00	0.16	0.299	o	|	|	|	|	0.69
46.000	0.00	0.16	0.298	o	|	|	|	|	0.69
46.083	0.00	0.16	0.297	o	|	|	|	|	0.69
46.167	0.00	0.15	0.296	o	|	|	|	|	0.69
46.250	0.00	0.15	0.295	o	|	|	|	|	0.68
46.333	0.00	0.15	0.294	o	|	|	|	|	0.68
46.417	0.00	0.15	0.293	o	|	|	|	|	0.68
46.500	0.00	0.15	0.292	o	|	|	|	|	0.68
46.583	0.00	0.15	0.291	o	|	|	|	|	0.67
46.667	0.00	0.15	0.290	o	|	|	|	|	0.67
46.750	0.00	0.15	0.289	o	|	|	|	|	0.67
46.833	0.00	0.15	0.288	o	|	|	|	|	0.67
46.917	0.00	0.15	0.287	o	|	|	|	|	0.67
47.000	0.00	0.15	0.286	o	|	|	|	|	0.66
47.083	0.00	0.15	0.285	o	|	|	|	|	0.66
47.167	0.00	0.15	0.284	o	|	|	|	|	0.66
47.250	0.00	0.15	0.283	o	|	|	|	|	0.66
47.333	0.00	0.15	0.282	o	|	|	|	|	0.65
47.417	0.00	0.15	0.281	o	|	|	|	|	0.65
47.500	0.00	0.15	0.280	o	|	|	|	|	0.65
47.583	0.00	0.15	0.279	o	|	|	|	|	0.65
47.667	0.00	0.14	0.278	o	|	|	|	|	0.64
47.750	0.00	0.14	0.277	o	|	|	|	|	0.64
47.833	0.00	0.14	0.276	o	|	|	|	|	0.64
47.917	0.00	0.14	0.275	o	|	|	|	|	0.64
48.000	0.00	0.14	0.274	o	|	|	|	|	0.63
48.083	0.00	0.14	0.273	o	|	|	|	|	0.63
48.167	0.00	0.14	0.272	o	|	|	|	|	0.63
48.250	0.00	0.14	0.271	o	|	|	|	|	0.63
48.333	0.00	0.14	0.270	o	|	|	|	|	0.63
48.417	0.00	0.14	0.269	o	|	|	|	|	0.62
48.500	0.00	0.14	0.268	o	|	|	|	|	0.62
48.583	0.00	0.14	0.267	o	|	|	|	|	0.62
48.667	0.00	0.14	0.266	o	|	|	|	|	0.62
48.750	0.00	0.14	0.265	o	|	|	|	|	0.61
48.833	0.00	0.14	0.264	o	|	|	|	|	0.61
48.917	0.00	0.14	0.263	o	|	|	|	|	0.61
49.000	0.00	0.14	0.262	o	|	|	|	|	0.61
49.083	0.00	0.14	0.261	o	|	|	|	|	0.61
49.167	0.00	0.14	0.260	o	|	|	|	|	0.60
49.250	0.00	0.14	0.259	o	|	|	|	|	0.60
49.333	0.00	0.13	0.258	o	|	|	|	|	0.60
49.417	0.00	0.13	0.257	o	|	|	|	|	0.60
49.500	0.00	0.13	0.256	o	|	|	|	|	0.60
49.583	0.00	0.13	0.256	o	|	|	|	|	0.59
49.667	0.00	0.13	0.255	o	|	|	|	|	0.59
49.750	0.00	0.13	0.254	o	|	|	|	|	0.59
49.833	0.00	0.13	0.253	o	|	|	|	|	0.59
49.917	0.00	0.13	0.252	o	|	|	|	|	0.58
50.000	0.00	0.13	0.251	o	|	|	|	|	0.58
50.083	0.00	0.13	0.250	o	|	|	|	|	0.58
50.167	0.00	0.13	0.249	o	|	|	|	|	0.58
50.250	0.00	0.13	0.248	o	|	|	|	|	0.58
50.333	0.00	0.13	0.247	o	|	|	|	|	0.57
50.417	0.00	0.13	0.247	o	|	|	|	|	0.57
50.500	0.00	0.13	0.246	o	|	|	|	|	0.57
50.583	0.00	0.13	0.245	o	|	|	|	|	0.57
50.667	0.00	0.13	0.244	o	|	|	|	|	0.57
50.750	0.00	0.13	0.243	o	|	|	|	|	0.56
50.833	0.00	0.13	0.242	o	|	|	|	|	0.56
50.917	0.00	0.13	0.241	o	|	|	|	|	0.56
51.000	0.00	0.13	0.240	o	|	|	|	|	0.56
51.083	0.00	0.13	0.240	o	|	|	|	|	0.56
51.167	0.00	0.12	0.239	o	|	|	|	|	0.55
51.250	0.00	0.12	0.238	o	|	|	|	|	0.55
51.333	0.00	0.12	0.237	o	|	|	|	|	0.55
51.417	0.00	0.12	0.236	o	|	|	|	|	0.55
51.500	0.00	0.12	0.235	o	|	|	|	|	0.55
51.583	0.00	0.12	0.234	o	|	|	|	|	0.54
51.667	0.00	0.12	0.234	o	|	|	|	|	0.54

51.750	0.00	0.12	0.233	o					0.54
51.833	0.00	0.12	0.232	o					0.54
51.917	0.00	0.12	0.231	o					0.54
52.000	0.00	0.12	0.230	o					0.53
52.083	0.00	0.12	0.229	o					0.53
52.167	0.00	0.12	0.229	o					0.53
52.250	0.00	0.12	0.228	o					0.53
52.333	0.00	0.12	0.227	o					0.53
52.417	0.00	0.12	0.226	o					0.52
52.500	0.00	0.12	0.225	o					0.52
52.583	0.00	0.12	0.225	o					0.52
52.667	0.00	0.12	0.224	o					0.52
52.750	0.00	0.12	0.223	o					0.52
52.833	0.00	0.12	0.222	o					0.52
52.917	0.00	0.12	0.221	o					0.51
53.000	0.00	0.12	0.221	o					0.51
53.083	0.00	0.11	0.220	o					0.51
53.167	0.00	0.11	0.219	o					0.51
53.250	0.00	0.11	0.218	o					0.51
53.333	0.00	0.11	0.217	o					0.50
53.417	0.00	0.11	0.217	o					0.50
53.500	0.00	0.11	0.216	o					0.50
53.583	0.00	0.11	0.215	o					0.50
53.667	0.00	0.11	0.214	o					0.50
53.750	0.00	0.11	0.214	o					0.50
53.833	0.00	0.11	0.213	o					0.49
53.917	0.00	0.11	0.212	o					0.49
54.000	0.00	0.11	0.211	o					0.49
54.083	0.00	0.11	0.210	o					0.49
54.167	0.00	0.11	0.210	o					0.49
54.250	0.00	0.11	0.209	o					0.48
54.333	0.00	0.11	0.208	o					0.48
54.417	0.00	0.11	0.207	o					0.48
54.500	0.00	0.11	0.207	o					0.48
54.583	0.00	0.11	0.206	o					0.48
54.667	0.00	0.11	0.205	o					0.48
54.750	0.00	0.11	0.204	o					0.47
54.833	0.00	0.11	0.204	o					0.47
54.917	0.00	0.11	0.203	o					0.47
55.000	0.00	0.11	0.202	o					0.47
55.083	0.00	0.11	0.202	o					0.47
55.167	0.00	0.10	0.201	o					0.47
55.250	0.00	0.10	0.200	o					0.46
55.333	0.00	0.10	0.199	o					0.46
55.417	0.00	0.10	0.199	o					0.46
55.500	0.00	0.10	0.198	o					0.46
55.583	0.00	0.10	0.197	o					0.46
55.667	0.00	0.10	0.197	o					0.46
55.750	0.00	0.10	0.196	o					0.45
55.833	0.00	0.10	0.195	o					0.45
55.917	0.00	0.10	0.194	o					0.45
56.000	0.00	0.10	0.194	o					0.45
56.083	0.00	0.10	0.193	o					0.45
56.167	0.00	0.10	0.192	o					0.45
56.250	0.00	0.10	0.192	o					0.44
56.333	0.00	0.10	0.191	o					0.44

Remaining water in basin = 0.19 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 676
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.302 (CFS)
Total volume = 1.754 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro2535.rte
**********HYDROGRAPH DATA**********
Number of intervals = 41
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 32.327 (CFS)
Total volume = 2.539 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 41
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.431	0.225	0.430	0.432
2.000	0.914	0.344	0.913	0.915
3.000	1.451	0.991	1.448	1.454
4.000	2.049	1.417	2.044	2.054
5.000	2.712	1.731	2.706	2.718
5.250	2.888	1.801	2.882	2.894
5.500	3.069	17.046	3.010	3.128
6.000	3.443	225.078	2.668	4.218

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 8.1 16.16 24.25 32.33	Depth (Ft.)
0.083	1.29	0.00	0.004	OI | | | |	0.01
0.167	3.40	0.01	0.021	O I | | | |	0.05
0.250	3.74	0.02	0.045	O I | | | |	0.10
0.333	4.05	0.04	0.072	O I | | | |	0.17
0.417	4.75	0.05	0.102	O I | | | |	0.24
0.500	5.27	0.07	0.136	O I | | | |	0.31
0.583	5.51	0.09	0.172	O I | | | |	0.40
0.667	5.47	0.11	0.209	O I | | | |	0.49
0.750	5.92	0.13	0.248	O I | | | |	0.58
0.833	5.72	0.15	0.287	O I | | | |	0.67
0.917	5.38	0.17	0.324	O I | | | |	0.75
1.000	5.63	0.19	0.361	O I | | | |	0.84
1.083	6.36	0.21	0.401	O I | | | |	0.93
1.167	7.08	0.23	0.445	O I | | | |	1.03
1.250	7.27	0.24	0.493	O I | | | |	1.13
1.333	7.17	0.25	0.541	O I | | | |	1.23
1.417	7.49	0.26	0.590	O I | | | |	1.33
1.500	8.52	0.28	0.643	O I | | | |	1.44

1.583	8.59	0.29	0.700	O	I	|	|	|	|	1.56
1.667	8.53	0.31	0.757	O	I	|	|	|	|	1.68
1.750	9.55	0.32	0.817	O	|I	|	|	|	|	1.80
1.833	10.46	0.34	0.884	O	| I	|	|	|	|	1.94
1.917	10.21	0.39	0.952	O	| I	|	|	|	|	2.07
2.000	10.02	0.47	1.019	O	|I	|	|	|	|	2.20
2.083	10.25	0.55	1.085	O	| I	|	|	|	|	2.32
2.167	11.53	0.64	1.156	O	| I	|	|	|	|	2.45
2.250	14.27	0.74	1.240	O	| |	I |	|	|	|	2.61
2.333	14.63	0.85	1.334	O	| |	I |	|	|	|	2.78
2.417	17.76	0.98	1.440	O	| |	|	I |	|	|	2.98
2.500	26.88	1.09	1.586	|O	| |	|	|	I |	|	3.23
2.583	32.33	1.23	1.782	|O	| |	|	|	|	I |	3.55
2.667	31.97	1.38	1.995	|O	| |	|	|	|	I |	3.91
2.750	20.93	1.47	2.167	|O	| |	|	I |	|	|	4.18
2.833	11.62	1.52	2.269	|O	| I |	|	|	|	|	4.33
2.917	8.68	1.55	2.328	|O	I |	|	|	|	|	4.42
3.000	6.18	1.57	2.369	|O	I |	|	|	|	|	4.48
3.083	2.76	1.58	2.389	|OI	|	|	|	|	|	4.51
3.167	0.90	1.58	2.390	IO	|	|	|	|	|	4.51
3.250	0.42	1.58	2.384	IO	|	|	|	|	|	4.51
3.333	0.19	1.57	2.375	IO	|	|	|	|	|	4.49
3.417	0.04	1.57	2.365	IO	|	|	|	|	|	4.48
3.500	0.00	1.56	2.355	IO	|	|	|	|	|	4.46
3.583	0.00	1.56	2.344	IO	|	|	|	|	|	4.44
3.667	0.00	1.55	2.333	IO	|	|	|	|	|	4.43
3.750	0.00	1.55	2.323	IO	|	|	|	|	|	4.41
3.833	0.00	1.54	2.312	IO	|	|	|	|	|	4.40
3.917	0.00	1.54	2.301	IO	|	|	|	|	|	4.38
4.000	0.00	1.53	2.291	IO	|	|	|	|	|	4.36
4.083	0.00	1.53	2.280	IO	|	|	|	|	|	4.35
4.167	0.00	1.52	2.270	IO	|	|	|	|	|	4.33
4.250	0.00	1.52	2.259	IO	|	|	|	|	|	4.32
4.333	0.00	1.51	2.249	IO	|	|	|	|	|	4.30
4.417	0.00	1.51	2.238	IO	|	|	|	|	|	4.29
4.500	0.00	1.50	2.228	IO	|	|	|	|	|	4.27
4.583	0.00	1.50	2.218	IO	|	|	|	|	|	4.25
4.667	0.00	1.49	2.208	IO	|	|	|	|	|	4.24
4.750	0.00	1.49	2.197	IO	|	|	|	|	|	4.22
4.833	0.00	1.48	2.187	IO	|	|	|	|	|	4.21
4.917	0.00	1.48	2.177	IO	|	|	|	|	|	4.19
5.000	0.00	1.47	2.167	IO	|	|	|	|	|	4.18
5.083	0.00	1.47	2.157	IO	|	|	|	|	|	4.16
5.167	0.00	1.46	2.146	IO	|	|	|	|	|	4.15
5.250	0.00	1.46	2.136	IO	|	|	|	|	|	4.13
5.333	0.00	1.45	2.126	IO	|	|	|	|	|	4.12
5.417	0.00	1.45	2.116	IO	|	|	|	|	|	4.10
5.500	0.00	1.44	2.106	IO	|	|	|	|	|	4.09
5.583	0.00	1.44	2.096	IO	|	|	|	|	|	4.07
5.667	0.00	1.43	2.087	IO	|	|	|	|	|	4.06
5.750	0.00	1.43	2.077	IO	|	|	|	|	|	4.04
5.833	0.00	1.43	2.067	IO	|	|	|	|	|	4.03
5.917	0.00	1.42	2.057	IO	|	|	|	|	|	4.01
6.000	0.00	1.42	2.047	IO	|	|	|	|	|	4.00
6.083	0.00	1.41	2.038	IO	|	|	|	|	|	3.98
6.167	0.00	1.40	2.028	IO	|	|	|	|	|	3.96
6.250	0.00	1.40	2.018	IO	|	|	|	|	|	3.95
6.333	0.00	1.39	2.009	IO	|	|	|	|	|	3.93
6.417	0.00	1.38	1.999	IO	|	|	|	|	|	3.92
6.500	0.00	1.37	1.990	IO	|	|	|	|	|	3.90
6.583	0.00	1.37	1.980	IO	|	|	|	|	|	3.88
6.667	0.00	1.36	1.971	IO	|	|	|	|	|	3.87
6.750	0.00	1.35	1.961	IO	|	|	|	|	|	3.85
6.833	0.00	1.35	1.952	IO	|	|	|	|	|	3.84
6.917	0.00	1.34	1.943	IO	|	|	|	|	|	3.82
7.000	0.00	1.33	1.934	IO	|	|	|	|	|	3.81
7.083	0.00	1.33	1.925	IO	|	|	|	|	|	3.79
7.167	0.00	1.32	1.915	IO	|	|	|	|	|	3.78
7.250	0.00	1.32	1.906	IO	|	|	|	|	|	3.76
7.333	0.00	1.31	1.897	IO	|	|	|	|	|	3.75
7.417	0.00	1.30	1.888	IO	|	|	|	|	|	3.73
7.500	0.00	1.30	1.879	IO	|	|	|	|	|	3.72
7.583	0.00	1.29	1.870	IO	|	|	|	|	|	3.70
7.667	0.00	1.28	1.862	IO	|	|	|	|	|	3.69
7.750	0.00	1.28	1.853	IO	|	|	|	|	|	3.67
7.833	0.00	1.27	1.844	IO	|	|	|	|	|	3.66
7.917	0.00	1.26	1.835	IO	|	|	|	|	|	3.64
8.000	0.00	1.26	1.827	IO	|	|	|	|	|	3.63
8.083	0.00	1.25	1.818	IO	|	|	|	|	|	3.61
8.167	0.00	1.25	1.809	IO	|	|	|	|	|	3.60
8.250	0.00	1.24	1.801	IO	|	|	|	|	|	3.58
8.333	0.00	1.23	1.792	IO	|	|	|	|	|	3.57
8.417	0.00	1.23	1.784	IO	|	|	|	|	|	3.56
8.500	0.00	1.22	1.775	IO	|	|	|	|	|	3.54
8.583	0.00	1.22	1.767	IO	|	|	|	|	|	3.53
8.667	0.00	1.21	1.759	IO	|	|	|	|	|	3.51

8.750	0.00	1.20	1.750	IO					3.50
8.833	0.00	1.20	1.742	IO					3.49
8.917	0.00	1.19	1.734	IO					3.47
9.000	0.00	1.19	1.726	IO					3.46
9.083	0.00	1.18	1.717	IO					3.45
9.167	0.00	1.17	1.709	IO					3.43
9.250	0.00	1.17	1.701	IO					3.42
9.333	0.00	1.16	1.693	IO					3.40
9.417	0.00	1.16	1.685	IO					3.39
9.500	0.00	1.15	1.677	IO					3.38
9.583	0.00	1.15	1.669	IO					3.37
9.667	0.00	1.14	1.661	IO					3.35
9.750	0.00	1.14	1.654	IO					3.34
9.833	0.00	1.13	1.646	IO					3.33
9.917	0.00	1.12	1.638	IO					3.31
10.000	0.00	1.12	1.630	IO					3.30
10.083	0.00	1.11	1.623	IO					3.29
10.167	0.00	1.11	1.615	IO					3.27
10.250	0.00	1.10	1.607	IO					3.26
10.333	0.00	1.10	1.600	IO					3.25
10.417	0.00	1.09	1.592	IO					3.24
10.500	0.00	1.09	1.585	IO					3.22
10.583	0.00	1.08	1.577	IO					3.21
10.667	0.00	1.08	1.570	IO					3.20
10.750	0.00	1.07	1.562	IO					3.19
10.833	0.00	1.07	1.555	IO					3.17
10.917	0.00	1.06	1.548	IO					3.16
11.000	0.00	1.05	1.541	IO					3.15
11.083	0.00	1.05	1.533	IO					3.14
11.167	0.00	1.04	1.526	IO					3.13
11.250	0.00	1.04	1.519	IO					3.11
11.333	0.00	1.03	1.512	IO					3.10
11.417	0.00	1.03	1.505	IO					3.09
11.500	0.00	1.02	1.498	IO					3.08
11.583	0.00	1.02	1.491	IO					3.07
11.667	0.00	1.01	1.484	IO					3.05
11.750	0.00	1.01	1.477	O					3.04
11.833	0.00	1.00	1.470	O					3.03
11.917	0.00	1.00	1.463	O					3.02
12.000	0.00	0.99	1.456	O					3.01
12.083	0.00	0.99	1.449	O					3.00
12.167	0.00	0.98	1.442	O					2.98
12.250	0.00	0.97	1.436	O					2.97
12.333	0.00	0.96	1.429	O					2.96
12.417	0.00	0.96	1.422	O					2.95
12.500	0.00	0.95	1.416	O					2.93
12.583	0.00	0.94	1.409	O					2.92
12.667	0.00	0.93	1.403	O					2.91
12.750	0.00	0.93	1.396	O					2.90
12.833	0.00	0.92	1.390	O					2.89
12.917	0.00	0.91	1.384	O					2.87
13.000	0.00	0.90	1.377	O					2.86
13.083	0.00	0.89	1.371	O					2.85
13.167	0.00	0.89	1.365	O					2.84
13.250	0.00	0.88	1.359	O					2.83
13.333	0.00	0.87	1.353	O					2.82
13.417	0.00	0.87	1.347	O					2.81
13.500	0.00	0.86	1.341	O					2.80
13.583	0.00	0.85	1.335	O					2.78
13.667	0.00	0.84	1.329	O					2.77
13.750	0.00	0.84	1.324	O					2.76
13.833	0.00	0.83	1.318	O					2.75
13.917	0.00	0.82	1.312	O					2.74
14.000	0.00	0.82	1.306	O					2.73
14.083	0.00	0.81	1.301	O					2.72
14.167	0.00	0.80	1.295	O					2.71
14.250	0.00	0.80	1.290	O					2.70
14.333	0.00	0.79	1.284	O					2.69
14.417	0.00	0.78	1.279	O					2.68
14.500	0.00	0.78	1.274	O					2.67
14.583	0.00	0.77	1.268	O					2.66
14.667	0.00	0.76	1.263	O					2.65
14.750	0.00	0.76	1.258	O					2.64
14.833	0.00	0.75	1.252	O					2.63
14.917	0.00	0.75	1.247	O					2.62
15.000	0.00	0.74	1.242	O					2.61
15.083	0.00	0.73	1.237	O					2.60
15.167	0.00	0.73	1.232	O					2.59
15.250	0.00	0.72	1.227	O					2.58
15.333	0.00	0.72	1.222	O					2.57
15.417	0.00	0.71	1.217	O					2.56
15.500	0.00	0.70	1.212	O					2.56
15.583	0.00	0.70	1.208	O					2.55
15.667	0.00	0.69	1.203	O					2.54
15.750	0.00	0.69	1.198	O					2.53
15.833	0.00	0.68	1.193	O					2.52

15.917	0.00	0.67	1.189	o	|	|	|	2.51
16.000	0.00	0.67	1.184	o	|	|	|	2.50
16.083	0.00	0.66	1.179	o	|	|	|	2.49
16.167	0.00	0.66	1.175	o	|	|	|	2.49
16.250	0.00	0.65	1.170	o	|	|	|	2.48
16.333	0.00	0.65	1.166	o	|	|	|	2.47
16.417	0.00	0.64	1.161	o	|	|	|	2.46
16.500	0.00	0.64	1.157	o	|	|	|	2.45
16.583	0.00	0.63	1.153	o	|	|	|	2.44
16.667	0.00	0.63	1.148	o	|	|	|	2.44
16.750	0.00	0.62	1.144	o	|	|	|	2.43
16.833	0.00	0.62	1.140	o	|	|	|	2.42
16.917	0.00	0.61	1.136	o	|	|	|	2.41
17.000	0.00	0.61	1.131	o	|	|	|	2.40
17.083	0.00	0.60	1.127	o	|	|	|	2.40
17.167	0.00	0.60	1.123	o	|	|	|	2.39
17.250	0.00	0.59	1.119	o	|	|	|	2.38
17.333	0.00	0.59	1.115	o	|	|	|	2.37
17.417	0.00	0.58	1.111	o	|	|	|	2.37
17.500	0.00	0.58	1.107	o	|	|	|	2.36
17.583	0.00	0.57	1.103	o	|	|	|	2.35
17.667	0.00	0.57	1.099	o	|	|	|	2.34
17.750	0.00	0.56	1.095	o	|	|	|	2.34
17.833	0.00	0.56	1.091	o	|	|	|	2.33
17.917	0.00	0.55	1.088	o	|	|	|	2.32
18.000	0.00	0.55	1.084	o	|	|	|	2.32
18.083	0.00	0.54	1.080	o	|	|	|	2.31
18.167	0.00	0.54	1.076	o	|	|	|	2.30
18.250	0.00	0.54	1.073	o	|	|	|	2.30
18.333	0.00	0.53	1.069	o	|	|	|	2.29
18.417	0.00	0.53	1.065	o	|	|	|	2.28
18.500	0.00	0.52	1.062	o	|	|	|	2.27
18.583	0.00	0.52	1.058	o	|	|	|	2.27
18.667	0.00	0.51	1.054	o	|	|	|	2.26
18.750	0.00	0.51	1.051	o	|	|	|	2.26
18.833	0.00	0.50	1.047	o	|	|	|	2.25
18.917	0.00	0.50	1.044	o	|	|	|	2.24
19.000	0.00	0.50	1.041	o	|	|	|	2.24
19.083	0.00	0.49	1.037	o	|	|	|	2.23
19.167	0.00	0.49	1.034	o	|	|	|	2.22
19.250	0.00	0.48	1.030	o	|	|	|	2.22
19.333	0.00	0.48	1.027	o	|	|	|	2.21
19.417	0.00	0.48	1.024	o	|	|	|	2.20
19.500	0.00	0.47	1.021	o	|	|	|	2.20
19.583	0.00	0.47	1.017	o	|	|	|	2.19
19.667	0.00	0.46	1.014	o	|	|	|	2.19
19.750	0.00	0.46	1.011	o	|	|	|	2.18
19.833	0.00	0.46	1.008	o	|	|	|	2.17
19.917	0.00	0.45	1.005	o	|	|	|	2.17
20.000	0.00	0.45	1.002	o	|	|	|	2.16
20.083	0.00	0.45	0.998	o	|	|	|	2.16
20.167	0.00	0.44	0.995	o	|	|	|	2.15
20.250	0.00	0.44	0.992	o	|	|	|	2.15
20.333	0.00	0.43	0.989	o	|	|	|	2.14
20.417	0.00	0.43	0.986	o	|	|	|	2.13
20.500	0.00	0.43	0.983	o	|	|	|	2.13
20.583	0.00	0.42	0.980	o	|	|	|	2.12
20.667	0.00	0.42	0.978	o	|	|	|	2.12
20.750	0.00	0.42	0.975	o	|	|	|	2.11
20.833	0.00	0.41	0.972	o	|	|	|	2.11
20.917	0.00	0.41	0.969	o	|	|	|	2.10
21.000	0.00	0.41	0.966	o	|	|	|	2.10
21.083	0.00	0.40	0.963	o	|	|	|	2.09
21.167	0.00	0.40	0.961	o	|	|	|	2.09
21.250	0.00	0.40	0.958	o	|	|	|	2.08
21.333	0.00	0.39	0.955	o	|	|	|	2.08
21.417	0.00	0.39	0.952	o	|	|	|	2.07
21.500	0.00	0.39	0.950	o	|	|	|	2.07
21.583	0.00	0.38	0.947	o	|	|	|	2.06
21.667	0.00	0.38	0.944	o	|	|	|	2.06
21.750	0.00	0.38	0.942	o	|	|	|	2.05
21.833	0.00	0.37	0.939	o	|	|	|	2.05
21.917	0.00	0.37	0.937	o	|	|	|	2.04
22.000	0.00	0.37	0.934	o	|	|	|	2.04
22.083	0.00	0.37	0.932	o	|	|	|	2.03
22.167	0.00	0.36	0.929	o	|	|	|	2.03
22.250	0.00	0.36	0.927	o	|	|	|	2.02
22.333	0.00	0.36	0.924	o	|	|	|	2.02
22.417	0.00	0.35	0.922	o	|	|	|	2.01
22.500	0.00	0.35	0.919	o	|	|	|	2.01
22.583	0.00	0.35	0.917	o	|	|	|	2.01
22.667	0.00	0.34	0.915	o	|	|	|	2.00
22.750	0.00	0.34	0.912	o	|	|	|	2.00
22.833	0.00	0.34	0.910	o	|	|	|	1.99
22.917	0.00	0.34	0.907	o	|	|	|	1.99
23.000	0.00	0.34	0.905	o	|	|	|	1.98

23.083	0.00	0.34	0.903	o	|	|	|	|	1.98
23.167	0.00	0.34	0.900	o	|	|	|	|	1.97
23.250	0.00	0.34	0.898	o	|	|	|	|	1.97
23.333	0.00	0.34	0.896	o	|	|	|	|	1.96
23.417	0.00	0.34	0.893	o	|	|	|	|	1.96
23.500	0.00	0.34	0.891	o	|	|	|	|	1.95
23.583	0.00	0.34	0.889	o	|	|	|	|	1.95
23.667	0.00	0.34	0.886	o	|	|	|	|	1.94
23.750	0.00	0.34	0.884	o	|	|	|	|	1.94
23.833	0.00	0.34	0.882	o	|	|	|	|	1.93
23.917	0.00	0.34	0.879	o	|	|	|	|	1.93
24.000	0.00	0.33	0.877	o	|	|	|	|	1.92
24.083	0.00	0.33	0.875	o	|	|	|	|	1.92
24.167	0.00	0.33	0.873	o	|	|	|	|	1.91
24.250	0.00	0.33	0.870	o	|	|	|	|	1.91
24.333	0.00	0.33	0.868	o	|	|	|	|	1.90
24.417	0.00	0.33	0.866	o	|	|	|	|	1.90
24.500	0.00	0.33	0.863	o	|	|	|	|	1.90
24.583	0.00	0.33	0.861	o	|	|	|	|	1.89
24.667	0.00	0.33	0.859	o	|	|	|	|	1.89
24.750	0.00	0.33	0.857	o	|	|	|	|	1.88
24.833	0.00	0.33	0.854	o	|	|	|	|	1.88
24.917	0.00	0.33	0.852	o	|	|	|	|	1.87
25.000	0.00	0.33	0.850	o	|	|	|	|	1.87
25.083	0.00	0.33	0.847	o	|	|	|	|	1.86
25.167	0.00	0.33	0.845	o	|	|	|	|	1.86
25.250	0.00	0.33	0.843	o	|	|	|	|	1.85
25.333	0.00	0.33	0.841	o	|	|	|	|	1.85
25.417	0.00	0.33	0.838	o	|	|	|	|	1.84
25.500	0.00	0.32	0.836	o	|	|	|	|	1.84
25.583	0.00	0.32	0.834	o	|	|	|	|	1.83
25.667	0.00	0.32	0.832	o	|	|	|	|	1.83
25.750	0.00	0.32	0.830	o	|	|	|	|	1.83
25.833	0.00	0.32	0.827	o	|	|	|	|	1.82
25.917	0.00	0.32	0.825	o	|	|	|	|	1.82
26.000	0.00	0.32	0.823	o	|	|	|	|	1.81
26.083	0.00	0.32	0.821	o	|	|	|	|	1.81
26.167	0.00	0.32	0.818	o	|	|	|	|	1.80
26.250	0.00	0.32	0.816	o	|	|	|	|	1.80
26.333	0.00	0.32	0.814	o	|	|	|	|	1.79
26.417	0.00	0.32	0.812	o	|	|	|	|	1.79
26.500	0.00	0.32	0.810	o	|	|	|	|	1.78
26.583	0.00	0.32	0.807	o	|	|	|	|	1.78
26.667	0.00	0.32	0.805	o	|	|	|	|	1.77
26.750	0.00	0.32	0.803	o	|	|	|	|	1.77
26.833	0.00	0.32	0.801	o	|	|	|	|	1.77
26.917	0.00	0.32	0.799	o	|	|	|	|	1.76
27.000	0.00	0.32	0.797	o	|	|	|	|	1.76
27.083	0.00	0.31	0.794	o	|	|	|	|	1.75
27.167	0.00	0.31	0.792	o	|	|	|	|	1.75
27.250	0.00	0.31	0.790	o	|	|	|	|	1.74
27.333	0.00	0.31	0.788	o	|	|	|	|	1.74
27.417	0.00	0.31	0.786	o	|	|	|	|	1.73
27.500	0.00	0.31	0.784	o	|	|	|	|	1.73
27.583	0.00	0.31	0.781	o	|	|	|	|	1.73
27.667	0.00	0.31	0.779	o	|	|	|	|	1.72
27.750	0.00	0.31	0.777	o	|	|	|	|	1.72
27.833	0.00	0.31	0.775	o	|	|	|	|	1.71
27.917	0.00	0.31	0.773	o	|	|	|	|	1.71
28.000	0.00	0.31	0.771	o	|	|	|	|	1.70
28.083	0.00	0.31	0.769	o	|	|	|	|	1.70
28.167	0.00	0.31	0.767	o	|	|	|	|	1.69
28.250	0.00	0.31	0.764	o	|	|	|	|	1.69
28.333	0.00	0.31	0.762	o	|	|	|	|	1.69
28.417	0.00	0.31	0.760	o	|	|	|	|	1.68
28.500	0.00	0.31	0.758	o	|	|	|	|	1.68
28.583	0.00	0.31	0.756	o	|	|	|	|	1.67
28.667	0.00	0.30	0.754	o	|	|	|	|	1.67
28.750	0.00	0.30	0.752	o	|	|	|	|	1.66
28.833	0.00	0.30	0.750	o	|	|	|	|	1.66
28.917	0.00	0.30	0.748	o	|	|	|	|	1.66
29.000	0.00	0.30	0.746	o	|	|	|	|	1.65
29.083	0.00	0.30	0.743	o	|	|	|	|	1.65
29.167	0.00	0.30	0.741	o	|	|	|	|	1.64
29.250	0.00	0.30	0.739	o	|	|	|	|	1.64
29.333	0.00	0.30	0.737	o	|	|	|	|	1.63
29.417	0.00	0.30	0.735	o	|	|	|	|	1.63
29.500	0.00	0.30	0.733	o	|	|	|	|	1.63
29.583	0.00	0.30	0.731	o	|	|	|	|	1.62
29.667	0.00	0.30	0.729	o	|	|	|	|	1.62
29.750	0.00	0.30	0.727	o	|	|	|	|	1.61
29.833	0.00	0.30	0.725	o	|	|	|	|	1.61
29.917	0.00	0.30	0.723	o	|	|	|	|	1.60
30.000	0.00	0.30	0.721	o	|	|	|	|	1.60
30.083	0.00	0.30	0.719	o	|	|	|	|	1.60
30.167	0.00	0.30	0.717	o	|	|	|	|	1.59

30.250	0.00	0.29	0.715	o	|	|	|	|	1.59
30.333	0.00	0.29	0.713	o	|	|	|	|	1.58
30.417	0.00	0.29	0.711	o	|	|	|	|	1.58
30.500	0.00	0.29	0.709	o	|	|	|	|	1.57
30.583	0.00	0.29	0.707	o	|	|	|	|	1.57
30.667	0.00	0.29	0.705	o	|	|	|	|	1.57
30.750	0.00	0.29	0.703	o	|	|	|	|	1.56
30.833	0.00	0.29	0.701	o	|	|	|	|	1.56
30.917	0.00	0.29	0.699	o	|	|	|	|	1.55
31.000	0.00	0.29	0.697	o	|	|	|	|	1.55
31.083	0.00	0.29	0.695	o	|	|	|	|	1.55
31.167	0.00	0.29	0.693	o	|	|	|	|	1.54
31.250	0.00	0.29	0.691	o	|	|	|	|	1.54
31.333	0.00	0.29	0.689	o	|	|	|	|	1.53
31.417	0.00	0.29	0.687	o	|	|	|	|	1.53
31.500	0.00	0.29	0.685	o	|	|	|	|	1.53
31.583	0.00	0.29	0.683	o	|	|	|	|	1.52
31.667	0.00	0.29	0.681	o	|	|	|	|	1.52
31.750	0.00	0.29	0.679	o	|	|	|	|	1.51
31.833	0.00	0.29	0.677	o	|	|	|	|	1.51
31.917	0.00	0.29	0.675	o	|	|	|	|	1.50
32.000	0.00	0.28	0.673	o	|	|	|	|	1.50
32.083	0.00	0.28	0.671	o	|	|	|	|	1.50
32.167	0.00	0.28	0.669	o	|	|	|	|	1.49
32.250	0.00	0.28	0.667	o	|	|	|	|	1.49
32.333	0.00	0.28	0.665	o	|	|	|	|	1.48
32.417	0.00	0.28	0.663	o	|	|	|	|	1.48
32.500	0.00	0.28	0.661	o	|	|	|	|	1.48
32.583	0.00	0.28	0.659	o	|	|	|	|	1.47
32.667	0.00	0.28	0.657	o	|	|	|	|	1.47
32.750	0.00	0.28	0.655	o	|	|	|	|	1.46
32.833	0.00	0.28	0.653	o	|	|	|	|	1.46
32.917	0.00	0.28	0.651	o	|	|	|	|	1.46
33.000	0.00	0.28	0.650	o	|	|	|	|	1.45
33.083	0.00	0.28	0.648	o	|	|	|	|	1.45
33.167	0.00	0.28	0.646	o	|	|	|	|	1.44
33.250	0.00	0.28	0.644	o	|	|	|	|	1.44
33.333	0.00	0.28	0.642	o	|	|	|	|	1.44
33.417	0.00	0.28	0.640	o	|	|	|	|	1.43
33.500	0.00	0.28	0.638	o	|	|	|	|	1.43
33.583	0.00	0.28	0.636	o	|	|	|	|	1.42
33.667	0.00	0.28	0.634	o	|	|	|	|	1.42
33.750	0.00	0.27	0.632	o	|	|	|	|	1.42
33.833	0.00	0.27	0.630	o	|	|	|	|	1.41
33.917	0.00	0.27	0.629	o	|	|	|	|	1.41
34.000	0.00	0.27	0.627	o	|	|	|	|	1.41
34.083	0.00	0.27	0.625	o	|	|	|	|	1.40
34.167	0.00	0.27	0.623	o	|	|	|	|	1.40
34.250	0.00	0.27	0.621	o	|	|	|	|	1.39
34.333	0.00	0.27	0.619	o	|	|	|	|	1.39
34.417	0.00	0.27	0.617	o	|	|	|	|	1.39
34.500	0.00	0.27	0.615	o	|	|	|	|	1.38
34.583	0.00	0.27	0.614	o	|	|	|	|	1.38
34.667	0.00	0.27	0.612	o	|	|	|	|	1.37
34.750	0.00	0.27	0.610	o	|	|	|	|	1.37
34.833	0.00	0.27	0.608	o	|	|	|	|	1.37
34.917	0.00	0.27	0.606	o	|	|	|	|	1.36
35.000	0.00	0.27	0.604	o	|	|	|	|	1.36
35.083	0.00	0.27	0.602	o	|	|	|	|	1.36
35.167	0.00	0.27	0.601	o	|	|	|	|	1.35
35.250	0.00	0.27	0.599	o	|	|	|	|	1.35
35.333	0.00	0.27	0.597	o	|	|	|	|	1.34
35.417	0.00	0.27	0.595	o	|	|	|	|	1.34
35.500	0.00	0.26	0.593	o	|	|	|	|	1.34
35.583	0.00	0.26	0.592	o	|	|	|	|	1.33
35.667	0.00	0.26	0.590	o	|	|	|	|	1.33
35.750	0.00	0.26	0.588	o	|	|	|	|	1.32
35.833	0.00	0.26	0.586	o	|	|	|	|	1.32
35.917	0.00	0.26	0.584	o	|	|	|	|	1.32
36.000	0.00	0.26	0.582	o	|	|	|	|	1.31
36.083	0.00	0.26	0.581	o	|	|	|	|	1.31
36.167	0.00	0.26	0.579	o	|	|	|	|	1.31
36.250	0.00	0.26	0.577	o	|	|	|	|	1.30
36.333	0.00	0.26	0.575	o	|	|	|	|	1.30
36.417	0.00	0.26	0.573	o	|	|	|	|	1.29
36.500	0.00	0.26	0.572	o	|	|	|	|	1.29
36.583	0.00	0.26	0.570	o	|	|	|	|	1.29
36.667	0.00	0.26	0.568	o	|	|	|	|	1.28
36.750	0.00	0.26	0.566	o	|	|	|	|	1.28
36.833	0.00	0.26	0.565	o	|	|	|	|	1.28
36.917	0.00	0.26	0.563	o	|	|	|	|	1.27
37.000	0.00	0.26	0.561	o	|	|	|	|	1.27
37.083	0.00	0.26	0.559	o	|	|	|	|	1.27
37.167	0.00	0.26	0.557	o	|	|	|	|	1.26
37.250	0.00	0.26	0.556	o	|	|	|	|	1.26
37.333	0.00	0.26	0.554	o	|	|	|	|	1.25

37.417	0.00	0.25	0.552	o	|	|	|	|	1.25
37.500	0.00	0.25	0.550	o	|	|	|	|	1.25
37.583	0.00	0.25	0.549	o	|	|	|	|	1.24
37.667	0.00	0.25	0.547	o	|	|	|	|	1.24
37.750	0.00	0.25	0.545	o	|	|	|	|	1.24
37.833	0.00	0.25	0.543	o	|	|	|	|	1.23
37.917	0.00	0.25	0.542	o	|	|	|	|	1.23
38.000	0.00	0.25	0.540	o	|	|	|	|	1.23
38.083	0.00	0.25	0.538	o	|	|	|	|	1.22
38.167	0.00	0.25	0.536	o	|	|	|	|	1.22
38.250	0.00	0.25	0.535	o	|	|	|	|	1.21
38.333	0.00	0.25	0.533	o	|	|	|	|	1.21
38.417	0.00	0.25	0.531	o	|	|	|	|	1.21
38.500	0.00	0.25	0.530	o	|	|	|	|	1.20
38.583	0.00	0.25	0.528	o	|	|	|	|	1.20
38.667	0.00	0.25	0.526	o	|	|	|	|	1.20
38.750	0.00	0.25	0.524	o	|	|	|	|	1.19
38.833	0.00	0.25	0.523	o	|	|	|	|	1.19
38.917	0.00	0.25	0.521	o	|	|	|	|	1.19
39.000	0.00	0.25	0.519	o	|	|	|	|	1.18
39.083	0.00	0.25	0.518	o	|	|	|	|	1.18
39.167	0.00	0.25	0.516	o	|	|	|	|	1.18
39.250	0.00	0.25	0.514	o	|	|	|	|	1.17
39.333	0.00	0.25	0.513	o	|	|	|	|	1.17
39.417	0.00	0.24	0.511	o	|	|	|	|	1.17
39.500	0.00	0.24	0.509	o	|	|	|	|	1.16
39.583	0.00	0.24	0.508	o	|	|	|	|	1.16
39.667	0.00	0.24	0.506	o	|	|	|	|	1.15
39.750	0.00	0.24	0.504	o	|	|	|	|	1.15
39.833	0.00	0.24	0.502	o	|	|	|	|	1.15
39.917	0.00	0.24	0.501	o	|	|	|	|	1.14
40.000	0.00	0.24	0.499	o	|	|	|	|	1.14
40.083	0.00	0.24	0.497	o	|	|	|	|	1.14
40.167	0.00	0.24	0.496	o	|	|	|	|	1.13
40.250	0.00	0.24	0.494	o	|	|	|	|	1.13
40.333	0.00	0.24	0.493	o	|	|	|	|	1.13
40.417	0.00	0.24	0.491	o	|	|	|	|	1.12
40.500	0.00	0.24	0.489	o	|	|	|	|	1.12
40.583	0.00	0.24	0.488	o	|	|	|	|	1.12
40.667	0.00	0.24	0.486	o	|	|	|	|	1.11
40.750	0.00	0.24	0.484	o	|	|	|	|	1.11
40.833	0.00	0.24	0.483	o	|	|	|	|	1.11
40.917	0.00	0.24	0.481	o	|	|	|	|	1.10
41.000	0.00	0.24	0.479	o	|	|	|	|	1.10
41.083	0.00	0.24	0.478	o	|	|	|	|	1.10
41.167	0.00	0.24	0.476	o	|	|	|	|	1.09
41.250	0.00	0.24	0.474	o	|	|	|	|	1.09
41.333	0.00	0.24	0.473	o	|	|	|	|	1.09
41.417	0.00	0.23	0.471	o	|	|	|	|	1.08
41.500	0.00	0.23	0.470	o	|	|	|	|	1.08
41.583	0.00	0.23	0.468	o	|	|	|	|	1.08
41.667	0.00	0.23	0.466	o	|	|	|	|	1.07
41.750	0.00	0.23	0.465	o	|	|	|	|	1.07
41.833	0.00	0.23	0.463	o	|	|	|	|	1.07
41.917	0.00	0.23	0.462	o	|	|	|	|	1.06
42.000	0.00	0.23	0.460	o	|	|	|	|	1.06
42.083	0.00	0.23	0.458	o	|	|	|	|	1.06
42.167	0.00	0.23	0.457	o	|	|	|	|	1.05
42.250	0.00	0.23	0.455	o	|	|	|	|	1.05
42.333	0.00	0.23	0.454	o	|	|	|	|	1.05
42.417	0.00	0.23	0.452	o	|	|	|	|	1.04
42.500	0.00	0.23	0.450	o	|	|	|	|	1.04
42.583	0.00	0.23	0.449	o	|	|	|	|	1.04
42.667	0.00	0.23	0.447	o	|	|	|	|	1.03
42.750	0.00	0.23	0.446	o	|	|	|	|	1.03
42.833	0.00	0.23	0.444	o	|	|	|	|	1.03
42.917	0.00	0.23	0.443	o	|	|	|	|	1.02
43.000	0.00	0.23	0.441	o	|	|	|	|	1.02
43.083	0.00	0.23	0.439	o	|	|	|	|	1.02
43.167	0.00	0.23	0.438	o	|	|	|	|	1.01
43.250	0.00	0.23	0.436	o	|	|	|	|	1.01
43.333	0.00	0.23	0.435	o	|	|	|	|	1.01
43.417	0.00	0.23	0.433	o	|	|	|	|	1.00
43.500	0.00	0.23	0.432	o	|	|	|	|	1.00
43.583	0.00	0.22	0.430	o	|	|	|	|	1.00
43.667	0.00	0.22	0.429	o	|	|	|	|	0.99
43.750	0.00	0.22	0.427	o	|	|	|	|	0.99
43.833	0.00	0.22	0.425	o	|	|	|	|	0.99
43.917	0.00	0.22	0.424	o	|	|	|	|	0.98
44.000	0.00	0.22	0.422	o	|	|	|	|	0.98
44.083	0.00	0.22	0.421	o	|	|	|	|	0.98
44.167	0.00	0.22	0.419	o	|	|	|	|	0.97
44.250	0.00	0.22	0.418	o	|	|	|	|	0.97
44.333	0.00	0.22	0.416	o	|	|	|	|	0.97
44.417	0.00	0.22	0.415	o	|	|	|	|	0.96
44.500	0.00	0.22	0.413	o	|	|	|	|	0.96

44.583	0.00	0.22	0.412	o	|	|	|	|	0.96
44.667	0.00	0.21	0.410	o	|	|	|	|	0.95
44.750	0.00	0.21	0.409	o	|	|	|	|	0.95
44.833	0.00	0.21	0.408	o	|	|	|	|	0.95
44.917	0.00	0.21	0.406	o	|	|	|	|	0.94
45.000	0.00	0.21	0.405	o	|	|	|	|	0.94
45.083	0.00	0.21	0.403	o	|	|	|	|	0.94
45.167	0.00	0.21	0.402	o	|	|	|	|	0.93
45.250	0.00	0.21	0.400	o	|	|	|	|	0.93
45.333	0.00	0.21	0.399	o	|	|	|	|	0.93
45.417	0.00	0.21	0.397	o	|	|	|	|	0.92
45.500	0.00	0.21	0.396	o	|	|	|	|	0.92
45.583	0.00	0.21	0.395	o	|	|	|	|	0.92
45.667	0.00	0.21	0.393	o	|	|	|	|	0.91
45.750	0.00	0.20	0.392	o	|	|	|	|	0.91
45.833	0.00	0.20	0.390	o	|	|	|	|	0.91
45.917	0.00	0.20	0.389	o	|	|	|	|	0.90
46.000	0.00	0.20	0.388	o	|	|	|	|	0.90
46.083	0.00	0.20	0.386	o	|	|	|	|	0.90
46.167	0.00	0.20	0.385	o	|	|	|	|	0.89
46.250	0.00	0.20	0.383	o	|	|	|	|	0.89
46.333	0.00	0.20	0.382	o	|	|	|	|	0.89
46.417	0.00	0.20	0.381	o	|	|	|	|	0.88
46.500	0.00	0.20	0.379	o	|	|	|	|	0.88
46.583	0.00	0.20	0.378	o	|	|	|	|	0.88
46.667	0.00	0.20	0.377	o	|	|	|	|	0.87
46.750	0.00	0.20	0.375	o	|	|	|	|	0.87
46.833	0.00	0.20	0.374	o	|	|	|	|	0.87
46.917	0.00	0.19	0.372	o	|	|	|	|	0.86
47.000	0.00	0.19	0.371	o	|	|	|	|	0.86
47.083	0.00	0.19	0.370	o	|	|	|	|	0.86
47.167	0.00	0.19	0.368	o	|	|	|	|	0.85
47.250	0.00	0.19	0.367	o	|	|	|	|	0.85
47.333	0.00	0.19	0.366	o	|	|	|	|	0.85
47.417	0.00	0.19	0.365	o	|	|	|	|	0.85
47.500	0.00	0.19	0.363	o	|	|	|	|	0.84
47.583	0.00	0.19	0.362	o	|	|	|	|	0.84
47.667	0.00	0.19	0.361	o	|	|	|	|	0.84
47.750	0.00	0.19	0.359	o	|	|	|	|	0.83
47.833	0.00	0.19	0.358	o	|	|	|	|	0.83
47.917	0.00	0.19	0.357	o	|	|	|	|	0.83
48.000	0.00	0.19	0.355	o	|	|	|	|	0.82
48.083	0.00	0.18	0.354	o	|	|	|	|	0.82
48.167	0.00	0.18	0.353	o	|	|	|	|	0.82
48.250	0.00	0.18	0.352	o	|	|	|	|	0.82
48.333	0.00	0.18	0.350	o	|	|	|	|	0.81
48.417	0.00	0.18	0.349	o	|	|	|	|	0.81
48.500	0.00	0.18	0.348	o	|	|	|	|	0.81
48.583	0.00	0.18	0.347	o	|	|	|	|	0.80
48.667	0.00	0.18	0.345	o	|	|	|	|	0.80
48.750	0.00	0.18	0.344	o	|	|	|	|	0.80
48.833	0.00	0.18	0.343	o	|	|	|	|	0.80
48.917	0.00	0.18	0.342	o	|	|	|	|	0.79
49.000	0.00	0.18	0.340	o	|	|	|	|	0.79
49.083	0.00	0.18	0.339	o	|	|	|	|	0.79
49.167	0.00	0.18	0.338	o	|	|	|	|	0.78
49.250	0.00	0.18	0.337	o	|	|	|	|	0.78
49.333	0.00	0.18	0.336	o	|	|	|	|	0.78
49.417	0.00	0.17	0.334	o	|	|	|	|	0.78
49.500	0.00	0.17	0.333	o	|	|	|	|	0.77
49.583	0.00	0.17	0.332	o	|	|	|	|	0.77
49.667	0.00	0.17	0.331	o	|	|	|	|	0.77
49.750	0.00	0.17	0.330	o	|	|	|	|	0.76
49.833	0.00	0.17	0.328	o	|	|	|	|	0.76
49.917	0.00	0.17	0.327	o	|	|	|	|	0.76
50.000	0.00	0.17	0.326	o	|	|	|	|	0.76
50.083	0.00	0.17	0.325	o	|	|	|	|	0.75
50.167	0.00	0.17	0.324	o	|	|	|	|	0.75
50.250	0.00	0.17	0.323	o	|	|	|	|	0.75
50.333	0.00	0.17	0.321	o	|	|	|	|	0.75
50.417	0.00	0.17	0.320	o	|	|	|	|	0.74
50.500	0.00	0.17	0.319	o	|	|	|	|	0.74
50.583	0.00	0.17	0.318	o	|	|	|	|	0.74
50.667	0.00	0.17	0.317	o	|	|	|	|	0.74
50.750	0.00	0.16	0.316	o	|	|	|	|	0.73
50.833	0.00	0.16	0.315	o	|	|	|	|	0.73
50.917	0.00	0.16	0.313	o	|	|	|	|	0.73
51.000	0.00	0.16	0.312	o	|	|	|	|	0.72
51.083	0.00	0.16	0.311	o	|	|	|	|	0.72
51.167	0.00	0.16	0.310	o	|	|	|	|	0.72
51.250	0.00	0.16	0.309	o	|	|	|	|	0.72
51.333	0.00	0.16	0.308	o	|	|	|	|	0.71
51.417	0.00	0.16	0.307	o	|	|	|	|	0.71
51.500	0.00	0.16	0.306	o	|	|	|	|	0.71
51.583	0.00	0.16	0.305	o	|	|	|	|	0.71
51.667	0.00	0.16	0.303	o	|	|	|	|	0.70

51.750	0.00	0.16	0.302	o	|	|	|	0.70
51.833	0.00	0.16	0.301	o	|	|	|	0.70
51.917	0.00	0.16	0.300	o	|	|	|	0.70
52.000	0.00	0.16	0.299	o	|	|	|	0.69
52.083	0.00	0.16	0.298	o	|	|	|	0.69
52.167	0.00	0.16	0.297	o	|	|	|	0.69
52.250	0.00	0.15	0.296	o	|	|	|	0.69
52.333	0.00	0.15	0.295	o	|	|	|	0.68
52.417	0.00	0.15	0.294	o	|	|	|	0.68
52.500	0.00	0.15	0.293	o	|	|	|	0.68
52.583	0.00	0.15	0.292	o	|	|	|	0.68
52.667	0.00	0.15	0.291	o	|	|	|	0.67
52.750	0.00	0.15	0.290	o	|	|	|	0.67
52.833	0.00	0.15	0.289	o	|	|	|	0.67
52.917	0.00	0.15	0.288	o	|	|	|	0.67
53.000	0.00	0.15	0.287	o	|	|	|	0.66
53.083	0.00	0.15	0.285	o	|	|	|	0.66
53.167	0.00	0.15	0.284	o	|	|	|	0.66
53.250	0.00	0.15	0.283	o	|	|	|	0.66
53.333	0.00	0.15	0.282	o	|	|	|	0.66
53.417	0.00	0.15	0.281	o	|	|	|	0.65
53.500	0.00	0.15	0.280	o	|	|	|	0.65
53.583	0.00	0.15	0.279	o	|	|	|	0.65
53.667	0.00	0.15	0.278	o	|	|	|	0.65
53.750	0.00	0.14	0.277	o	|	|	|	0.64
53.833	0.00	0.14	0.276	o	|	|	|	0.64
53.917	0.00	0.14	0.275	o	|	|	|	0.64
54.000	0.00	0.14	0.274	o	|	|	|	0.64
54.083	0.00	0.14	0.273	o	|	|	|	0.63
54.167	0.00	0.14	0.272	o	|	|	|	0.63
54.250	0.00	0.14	0.271	o	|	|	|	0.63
54.333	0.00	0.14	0.270	o	|	|	|	0.63
54.417	0.00	0.14	0.270	o	|	|	|	0.63
54.500	0.00	0.14	0.269	o	|	|	|	0.62
54.583	0.00	0.14	0.268	o	|	|	|	0.62
54.667	0.00	0.14	0.267	o	|	|	|	0.62
54.750	0.00	0.14	0.266	o	|	|	|	0.62
54.833	0.00	0.14	0.265	o	|	|	|	0.61
54.917	0.00	0.14	0.264	o	|	|	|	0.61
55.000	0.00	0.14	0.263	o	|	|	|	0.61
55.083	0.00	0.14	0.262	o	|	|	|	0.61
55.167	0.00	0.14	0.261	o	|	|	|	0.61
55.250	0.00	0.14	0.260	o	|	|	|	0.60
55.333	0.00	0.14	0.259	o	|	|	|	0.60
55.417	0.00	0.13	0.258	o	|	|	|	0.60
55.500	0.00	0.13	0.257	o	|	|	|	0.60
55.583	0.00	0.13	0.256	o	|	|	|	0.59
55.667	0.00	0.13	0.255	o	|	|	|	0.59
55.750	0.00	0.13	0.254	o	|	|	|	0.59
55.833	0.00	0.13	0.254	o	|	|	|	0.59
55.917	0.00	0.13	0.253	o	|	|	|	0.59
56.000	0.00	0.13	0.252	o	|	|	|	0.58
56.083	0.00	0.13	0.251	o	|	|	|	0.58
56.167	0.00	0.13	0.250	o	|	|	|	0.58
56.250	0.00	0.13	0.249	o	|	|	|	0.58
56.333	0.00	0.13	0.248	o	|	|	|	0.58
56.417	0.00	0.13	0.247	o	|	|	|	0.57
56.500	0.00	0.13	0.246	o	|	|	|	0.57
56.583	0.00	0.13	0.245	o	|	|	|	0.57
56.667	0.00	0.13	0.245	o	|	|	|	0.57
56.750	0.00	0.13	0.244	o	|	|	|	0.57
56.833	0.00	0.13	0.243	o	|	|	|	0.56
56.917	0.00	0.13	0.242	o	|	|	|	0.56
57.000	0.00	0.13	0.241	o	|	|	|	0.56
57.083	0.00	0.13	0.240	o	|	|	|	0.56
57.167	0.00	0.12	0.239	o	|	|	|	0.56
57.250	0.00	0.12	0.239	o	|	|	|	0.55
57.333	0.00	0.12	0.238	o	|	|	|	0.55
57.417	0.00	0.12	0.237	o	|	|	|	0.55
57.500	0.00	0.12	0.236	o	|	|	|	0.55
57.583	0.00	0.12	0.235	o	|	|	|	0.55
57.667	0.00	0.12	0.234	o	|	|	|	0.54
57.750	0.00	0.12	0.233	o	|	|	|	0.54
57.833	0.00	0.12	0.233	o	|	|	|	0.54
57.917	0.00	0.12	0.232	o	|	|	|	0.54
58.000	0.00	0.12	0.231	o	|	|	|	0.54
58.083	0.00	0.12	0.230	o	|	|	|	0.53
58.167	0.00	0.12	0.229	o	|	|	|	0.53
58.250	0.00	0.12	0.228	o	|	|	|	0.53
58.333	0.00	0.12	0.228	o	|	|	|	0.53
58.417	0.00	0.12	0.227	o	|	|	|	0.53
58.500	0.00	0.12	0.226	o	|	|	|	0.52
58.583	0.00	0.12	0.225	o	|	|	|	0.52
58.667	0.00	0.12	0.224	o	|	|	|	0.52
58.750	0.00	0.12	0.224	o	|	|	|	0.52
58.833	0.00	0.12	0.223	o	|	|	|	0.52

58.917	0.00	0.12	0.222	o	|	|	|	|	0.51
59.000	0.00	0.12	0.221	o	|	|	|	|	0.51
59.083	0.00	0.12	0.220	o	|	|	|	|	0.51
59.167	0.00	0.11	0.220	o	|	|	|	|	0.51
59.250	0.00	0.11	0.219	o	|	|	|	|	0.51
59.333	0.00	0.11	0.218	o	|	|	|	|	0.51
59.417	0.00	0.11	0.217	o	|	|	|	|	0.50
59.500	0.00	0.11	0.216	o	|	|	|	|	0.50
59.583	0.00	0.11	0.216	o	|	|	|	|	0.50
59.667	0.00	0.11	0.215	o	|	|	|	|	0.50
59.750	0.00	0.11	0.214	o	|	|	|	|	0.50
59.833	0.00	0.11	0.213	o	|	|	|	|	0.50
59.917	0.00	0.11	0.213	o	|	|	|	|	0.49
60.000	0.00	0.11	0.212	o	|	|	|	|	0.49
60.083	0.00	0.11	0.211	o	|	|	|	|	0.49
60.167	0.00	0.11	0.210	o	|	|	|	|	0.49
60.250	0.00	0.11	0.210	o	|	|	|	|	0.49
60.333	0.00	0.11	0.209	o	|	|	|	|	0.48
60.417	0.00	0.11	0.208	o	|	|	|	|	0.48
60.500	0.00	0.11	0.207	o	|	|	|	|	0.48
60.583	0.00	0.11	0.207	o	|	|	|	|	0.48
60.667	0.00	0.11	0.206	o	|	|	|	|	0.48
60.750	0.00	0.11	0.205	o	|	|	|	|	0.48
60.833	0.00	0.11	0.204	o	|	|	|	|	0.47
60.917	0.00	0.11	0.204	o	|	|	|	|	0.47
61.000	0.00	0.11	0.203	o	|	|	|	|	0.47
61.083	0.00	0.11	0.202	o	|	|	|	|	0.47
61.167	0.00	0.11	0.201	o	|	|	|	|	0.47
61.250	0.00	0.10	0.201	o	|	|	|	|	0.47
61.333	0.00	0.10	0.200	o	|	|	|	|	0.46
61.417	0.00	0.10	0.199	o	|	|	|	|	0.46
61.500	0.00	0.10	0.199	o	|	|	|	|	0.46
61.583	0.00	0.10	0.198	o	|	|	|	|	0.46
61.667	0.00	0.10	0.197	o	|	|	|	|	0.46
61.750	0.00	0.10	0.196	o	|	|	|	|	0.46
61.833	0.00	0.10	0.196	o	|	|	|	|	0.45
61.917	0.00	0.10	0.195	o	|	|	|	|	0.45
62.000	0.00	0.10	0.194	o	|	|	|	|	0.45
62.083	0.00	0.10	0.194	o	|	|	|	|	0.45
62.167	0.00	0.10	0.193	o	|	|	|	|	0.45
62.250	0.00	0.10	0.192	o	|	|	|	|	0.45
62.333	0.00	0.10	0.192	o	|	|	|	|	0.44

Remaining water in basin = 0.19 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 748
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.579 (CFS)
Total volume = 2.348 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro2565.rte
**********HYDROGRAPH DATA**********
Number of intervals = 77
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 29.939 (CFS)
Total volume = 3.500 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 77
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.431	0.225	0.430	0.432
2.000	0.914	0.344	0.913	0.915
3.000	1.451	0.991	1.448	1.454
4.000	2.049	1.417	2.044	2.054
5.000	2.712	1.731	2.706	2.718
5.250	2.888	1.801	2.882	2.894
5.500	3.069	17.046	3.010	3.128
6.000	3.443	225.078	2.668	4.218

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 7.5 14.97 22.45 29.94	Depth (Ft.)
0.083	0.71	0.00	0.002	O | | | |	0.01
0.167	2.01	0.01	0.012	O I | | | |	0.03
0.250	2.54	0.01	0.027	O I | | | |	0.06
0.333	2.73	0.02	0.045	O I | | | |	0.11
0.417	2.83	0.03	0.064	O I | | | |	0.15
0.500	3.04	0.04	0.084	O I | | | |	0.20
0.583	3.28	0.06	0.106	O I | | | |	0.25
0.667	3.34	0.07	0.128	O I | | | |	0.30
0.750	3.36	0.08	0.151	O I | | | |	0.35
0.833	3.38	0.09	0.173	O I | | | |	0.40
0.917	3.39	0.10	0.196	O I | | | |	0.45
1.000	3.53	0.11	0.219	O I | | | |	0.51
1.083	3.76	0.13	0.243	O I | | | |	0.56
1.167	3.82	0.14	0.268	O I | | | |	0.62
1.250	3.85	0.15	0.294	O I | | | |	0.68
1.333	3.86	0.17	0.319	O I | | | |	0.74
1.417	3.87	0.18	0.345	O I | | | |	0.80
1.500	3.87	0.19	0.370	O I | | | |	0.86

1.583	3.87	0.21	0.395	O	I	|	|	|	|	0.92
1.667	3.87	0.22	0.421	O	I	|	|	|	|	0.98
1.750	3.87	0.23	0.446	O	I	|	|	|	|	1.03
1.833	3.87	0.23	0.471	O	I	|	|	|	|	1.08
1.917	3.87	0.24	0.496	O	I	|	|	|	|	1.13
2.000	4.01	0.25	0.521	O	I	|	|	|	|	1.19
2.083	4.11	0.25	0.548	O	I	|	|	|	|	1.24
2.167	4.07	0.26	0.574	O	I	|	|	|	|	1.30
2.250	4.27	0.27	0.601	O	I	|	|	|	|	1.35
2.333	4.32	0.27	0.629	O	I	|	|	|	|	1.41
2.417	4.34	0.28	0.657	O	I	|	|	|	|	1.47
2.500	4.35	0.29	0.685	O	I	|	|	|	|	1.52
2.583	4.36	0.29	0.712	O	I	|	|	|	|	1.58
2.667	4.36	0.30	0.740	O	I	|	|	|	|	1.64
2.750	4.50	0.31	0.769	O	I	|	|	|	|	1.70
2.833	4.73	0.32	0.798	O	I	|	|	|	|	1.76
2.917	4.79	0.32	0.829	O	I	|	|	|	|	1.82
3.000	4.82	0.33	0.860	O	I	|	|	|	|	1.89
3.083	4.83	0.34	0.891	O	I	|	|	|	|	1.95
3.167	4.98	0.35	0.922	O	I	|	|	|	|	2.02
3.250	5.22	0.39	0.955	O	I	|	|	|	|	2.08
3.333	5.27	0.43	0.988	O	I	|	|	|	|	2.14
3.417	5.44	0.47	1.022	O	I	|	|	|	|	2.20
3.500	5.83	0.52	1.057	O	I	|	|	|	|	2.27
3.583	6.27	0.56	1.095	O	I	|	|	|	|	2.34
3.667	6.59	0.61	1.135	O	I	|	|	|	|	2.41
3.750	6.83	0.66	1.177	O	I	|	|	|	|	2.49
3.833	7.12	0.71	1.221	O	I	|	|	|	|	2.57
3.917	7.34	0.77	1.265	O	I	|	|	|	|	2.65
4.000	7.61	0.82	1.311	O	I	|	|	|	|	2.74
4.083	7.83	0.88	1.359	O	I	|	|	|	|	2.83
4.167	8.24	0.94	1.408	O	I	|	|	|	|	2.92
4.250	8.68	1.00	1.459	O	I	|	|	|	|	3.01
4.333	9.15	1.04	1.514	O	I	|	|	|	|	3.10
4.417	9.63	1.08	1.571	O	I	|	|	|	|	3.20
4.500	9.97	1.12	1.631	O	I	|	|	|	|	3.30
4.583	10.22	1.16	1.693	O	I	|	|	|	|	3.40
4.667	10.65	1.21	1.756	O	I	|	|	|	|	3.51
4.750	11.10	1.26	1.823	O	I	|	|	|	|	3.62
4.833	11.43	1.30	1.892	O	I	|	|	|	|	3.74
4.917	11.67	1.35	1.962	O	I	|	|	|	|	3.85
5.000	12.10	1.41	2.034	O	I	|	|	|	|	3.98
5.083	13.12	1.45	2.111	O	I	|	|	|	|	4.09
5.167	15.36	1.49	2.199	O	I	|	|	|	|	4.23
5.250	18.16	1.54	2.304	O	I	|	|	|	|	4.39
5.333	20.97	1.60	2.428	O	I	|	|	|	|	4.57
5.417	24.40	1.67	2.573	O	I	|	|	|	|	4.79
5.500	29.94	1.75	2.749	O	I	|	|	|	|	5.05
5.583	26.68	4.64	2.922	O	I	|	|	|	|	5.30
5.667	13.03	11.48	3.003	O	I	|	|	|	|	5.41
5.750	7.48	10.93	2.996	O	I	|	|	|	|	5.40
5.833	4.88	8.80	2.971	O	I	|	|	|	|	5.36
5.917	3.27	6.67	2.946	O	I	|	|	|	|	5.33
6.000	1.76	4.80	2.924	O	I	|	|	|	|	5.30
6.083	0.95	3.25	2.905	O	I	|	|	|	|	5.27
6.167	0.33	2.08	2.891	O	I	|	|	|	|	5.25
6.250	0.15	1.80	2.880	O	I	|	|	|	|	5.24
6.333	0.06	1.79	2.868	O	I	|	|	|	|	5.22
6.417	0.02	1.79	2.856	O	I	|	|	|	|	5.20
6.500	0.00	1.78	2.844	O	I	|	|	|	|	5.19
6.583	0.00	1.78	2.831	O	I	|	|	|	|	5.17
6.667	0.00	1.77	2.819	O	I	|	|	|	|	5.15
6.750	0.00	1.77	2.807	O	I	|	|	|	|	5.13
6.833	0.00	1.76	2.795	O	I	|	|	|	|	5.12
6.917	0.00	1.76	2.783	O	I	|	|	|	|	5.10
7.000	0.00	1.75	2.771	O	I	|	|	|	|	5.08
7.083	0.00	1.75	2.759	O	I	|	|	|	|	5.07
7.167	0.00	1.74	2.746	O	I	|	|	|	|	5.05
7.250	0.00	1.74	2.734	O	I	|	|	|	|	5.03
7.333	0.00	1.74	2.723	O	I	|	|	|	|	5.01
7.417	0.00	1.73	2.711	O	I	|	|	|	|	5.00
7.500	0.00	1.72	2.699	O	I	|	|	|	|	4.98
7.583	0.00	1.72	2.687	O	I	|	|	|	|	4.96
7.667	0.00	1.71	2.675	O	I	|	|	|	|	4.94
7.750	0.00	1.71	2.663	O	I	|	|	|	|	4.93
7.833	0.00	1.70	2.651	O	I	|	|	|	|	4.91
7.917	0.00	1.70	2.640	O	I	|	|	|	|	4.89
8.000	0.00	1.69	2.628	O	I	|	|	|	|	4.87
8.083	0.00	1.69	2.616	O	I	|	|	|	|	4.86
8.167	0.00	1.68	2.605	O	I	|	|	|	|	4.84
8.250	0.00	1.67	2.593	O	I	|	|	|	|	4.82
8.333	0.00	1.67	2.582	O	I	|	|	|	|	4.80
8.417	0.00	1.66	2.570	O	I	|	|	|	|	4.79
8.500	0.00	1.66	2.559	O	I	|	|	|	|	4.77
8.583	0.00	1.65	2.548	O	I	|	|	|	|	4.75
8.667	0.00	1.65	2.536	O	I	|	|	|	|	4.73

8.750	0.00	1.64	2.525	IO				4.72
8.833	0.00	1.64	2.514	IO				4.70
8.917	0.00	1.63	2.502	IO				4.68
9.000	0.00	1.63	2.491	IO				4.67
9.083	0.00	1.62	2.480	IO				4.65
9.167	0.00	1.62	2.469	IO				4.63
9.250	0.00	1.61	2.458	IO				4.62
9.333	0.00	1.61	2.447	IO				4.60
9.417	0.00	1.60	2.435	IO				4.58
9.500	0.00	1.59	2.424	IO				4.57
9.583	0.00	1.59	2.414	IO				4.55
9.667	0.00	1.58	2.403	IO				4.53
9.750	0.00	1.58	2.392	IO				4.52
9.833	0.00	1.57	2.381	IO				4.50
9.917	0.00	1.57	2.370	IO				4.48
10.000	0.00	1.56	2.359	IO				4.47
10.083	0.00	1.56	2.348	IO				4.45
10.167	0.00	1.55	2.338	IO				4.44
10.250	0.00	1.55	2.327	IO				4.42
10.333	0.00	1.54	2.316	IO				4.40
10.417	0.00	1.54	2.306	IO				4.39
10.500	0.00	1.53	2.295	IO				4.37
10.583	0.00	1.53	2.285	IO				4.36
10.667	0.00	1.52	2.274	IO				4.34
10.750	0.00	1.52	2.264	IO				4.32
10.833	0.00	1.51	2.253	IO				4.31
10.917	0.00	1.51	2.243	IO				4.29
11.000	0.00	1.50	2.232	IO				4.28
11.083	0.00	1.50	2.222	IO				4.26
11.167	0.00	1.49	2.212	IO				4.25
11.250	0.00	1.49	2.202	IO				4.23
11.333	0.00	1.48	2.191	IO				4.21
11.417	0.00	1.48	2.181	IO				4.20
11.500	0.00	1.47	2.171	IO				4.18
11.583	0.00	1.47	2.161	IO				4.17
11.667	0.00	1.47	2.151	IO				4.15
11.750	0.00	1.46	2.141	IO				4.14
11.833	0.00	1.46	2.131	IO				4.12
11.917	0.00	1.45	2.121	IO				4.11
12.000	0.00	1.45	2.111	IO				4.09
12.083	0.00	1.44	2.101	IO				4.08
12.167	0.00	1.44	2.091	IO				4.06
12.250	0.00	1.43	2.081	IO				4.05
12.333	0.00	1.43	2.071	IO				4.03
12.417	0.00	1.42	2.061	IO				4.02
12.500	0.00	1.42	2.051	IO				4.00
12.583	0.00	1.41	2.042	IO				3.99
12.667	0.00	1.40	2.032	IO				3.97
12.750	0.00	1.40	2.022	IO				3.96
12.833	0.00	1.39	2.013	IO				3.94
12.917	0.00	1.38	2.003	IO				3.92
13.000	0.00	1.38	1.994	IO				3.91
13.083	0.00	1.37	1.984	IO				3.89
13.167	0.00	1.36	1.975	IO				3.88
13.250	0.00	1.36	1.965	IO				3.86
13.333	0.00	1.35	1.956	IO				3.84
13.417	0.00	1.34	1.947	IO				3.83
13.500	0.00	1.34	1.938	IO				3.81
13.583	0.00	1.33	1.928	IO				3.80
13.667	0.00	1.32	1.919	IO				3.78
13.750	0.00	1.32	1.910	IO				3.77
13.833	0.00	1.31	1.901	IO				3.75
13.917	0.00	1.31	1.892	IO				3.74
14.000	0.00	1.30	1.883	IO				3.72
14.083	0.00	1.29	1.874	IO				3.71
14.167	0.00	1.29	1.865	IO				3.69
14.250	0.00	1.28	1.856	IO				3.68
14.333	0.00	1.27	1.848	IO				3.66
14.417	0.00	1.27	1.839	IO				3.65
14.500	0.00	1.26	1.830	IO				3.63
14.583	0.00	1.25	1.822	IO				3.62
14.667	0.00	1.25	1.813	IO				3.61
14.750	0.00	1.24	1.804	IO				3.59
14.833	0.00	1.24	1.796	IO				3.58
14.917	0.00	1.23	1.787	IO				3.56
15.000	0.00	1.22	1.779	IO				3.55
15.083	0.00	1.22	1.770	IO				3.53
15.167	0.00	1.21	1.762	IO				3.52
15.250	0.00	1.21	1.754	IO				3.51
15.333	0.00	1.20	1.745	IO				3.49
15.417	0.00	1.19	1.737	IO				3.48
15.500	0.00	1.19	1.729	IO				3.46
15.583	0.00	1.18	1.721	IO				3.45
15.667	0.00	1.18	1.713	IO				3.44
15.750	0.00	1.17	1.705	IO				3.42
15.833	0.00	1.17	1.697	IO				3.41

15.917	0.00	1.16	1.689	IO	|	|	|	3.40
16.000	0.00	1.15	1.681	IO	|	|	|	3.38
16.083	0.00	1.15	1.673	IO	|	|	|	3.37
16.167	0.00	1.14	1.665	IO	|	|	|	3.36
16.250	0.00	1.14	1.657	IO	|	|	|	3.34
16.333	0.00	1.13	1.649	IO	|	|	|	3.33
16.417	0.00	1.13	1.641	IO	|	|	|	3.32
16.500	0.00	1.12	1.634	IO	|	|	|	3.31
16.583	0.00	1.12	1.626	IO	|	|	|	3.29
16.667	0.00	1.11	1.618	IO	|	|	|	3.28
16.750	0.00	1.10	1.611	IO	|	|	|	3.27
16.833	0.00	1.10	1.603	IO	|	|	|	3.25
16.917	0.00	1.09	1.595	IO	|	|	|	3.24
17.000	0.00	1.09	1.588	IO	|	|	|	3.23
17.083	0.00	1.08	1.580	IO	|	|	|	3.22
17.167	0.00	1.08	1.573	IO	|	|	|	3.20
17.250	0.00	1.07	1.566	IO	|	|	|	3.19
17.333	0.00	1.07	1.558	IO	|	|	|	3.18
17.417	0.00	1.06	1.551	IO	|	|	|	3.17
17.500	0.00	1.06	1.544	IO	|	|	|	3.15
17.583	0.00	1.05	1.536	IO	|	|	|	3.14
17.667	0.00	1.05	1.529	IO	|	|	|	3.13
17.750	0.00	1.04	1.522	IO	|	|	|	3.12
17.833	0.00	1.04	1.515	IO	|	|	|	3.11
17.917	0.00	1.03	1.508	IO	|	|	|	3.09
18.000	0.00	1.03	1.501	IO	|	|	|	3.08
18.083	0.00	1.02	1.493	IO	|	|	|	3.07
18.167	0.00	1.02	1.486	IO	|	|	|	3.06
18.250	0.00	1.01	1.479	IO	|	|	|	3.05
18.333	0.00	1.01	1.473	IO	|	|	|	3.04
18.417	0.00	1.00	1.466	IO	|	|	|	3.02
18.500	0.00	1.00	1.459	IO	|	|	|	3.01
18.583	0.00	0.99	1.452	IO	|	|	|	3.00
18.667	0.00	0.98	1.445	IO	|	|	|	2.99
18.750	0.00	0.98	1.438	IO	|	|	|	2.98
18.833	0.00	0.97	1.432	IO	|	|	|	2.96
18.917	0.00	0.96	1.425	IO	|	|	|	2.95
19.000	0.00	0.95	1.418	IO	|	|	|	2.94
19.083	0.00	0.94	1.412	IO	|	|	|	2.93
19.167	0.00	0.94	1.405	IO	|	|	|	2.92
19.250	0.00	0.93	1.399	O	|	|	|	2.90
19.333	0.00	0.92	1.393	O	|	|	|	2.89
19.417	0.00	0.91	1.386	O	|	|	|	2.88
19.500	0.00	0.91	1.380	O	|	|	|	2.87
19.583	0.00	0.90	1.374	O	|	|	|	2.86
19.667	0.00	0.89	1.368	O	|	|	|	2.84
19.750	0.00	0.88	1.362	O	|	|	|	2.83
19.833	0.00	0.88	1.356	O	|	|	|	2.82
19.917	0.00	0.87	1.350	O	|	|	|	2.81
20.000	0.00	0.86	1.344	O	|	|	|	2.80
20.083	0.00	0.85	1.338	O	|	|	|	2.79
20.167	0.00	0.85	1.332	O	|	|	|	2.78
20.250	0.00	0.84	1.326	O	|	|	|	2.77
20.333	0.00	0.83	1.320	O	|	|	|	2.76
20.417	0.00	0.83	1.315	O	|	|	|	2.75
20.500	0.00	0.82	1.309	O	|	|	|	2.74
20.583	0.00	0.81	1.303	O	|	|	|	2.72
20.667	0.00	0.81	1.298	O	|	|	|	2.71
20.750	0.00	0.80	1.292	O	|	|	|	2.70
20.833	0.00	0.79	1.287	O	|	|	|	2.69
20.917	0.00	0.79	1.281	O	|	|	|	2.68
21.000	0.00	0.78	1.276	O	|	|	|	2.67
21.083	0.00	0.77	1.270	O	|	|	|	2.66
21.167	0.00	0.77	1.265	O	|	|	|	2.65
21.250	0.00	0.76	1.260	O	|	|	|	2.64
21.333	0.00	0.75	1.255	O	|	|	|	2.63
21.417	0.00	0.75	1.249	O	|	|	|	2.62
21.500	0.00	0.74	1.244	O	|	|	|	2.62
21.583	0.00	0.74	1.239	O	|	|	|	2.61
21.667	0.00	0.73	1.234	O	|	|	|	2.60
21.750	0.00	0.72	1.229	O	|	|	|	2.59
21.833	0.00	0.72	1.224	O	|	|	|	2.58
21.917	0.00	0.71	1.219	O	|	|	|	2.57
22.000	0.00	0.71	1.214	O	|	|	|	2.56
22.083	0.00	0.70	1.210	O	|	|	|	2.55
22.167	0.00	0.69	1.205	O	|	|	|	2.54
22.250	0.00	0.69	1.200	O	|	|	|	2.53
22.333	0.00	0.68	1.195	O	|	|	|	2.52
22.417	0.00	0.68	1.191	O	|	|	|	2.52
22.500	0.00	0.67	1.186	O	|	|	|	2.51
22.583	0.00	0.67	1.181	O	|	|	|	2.50
22.667	0.00	0.66	1.177	O	|	|	|	2.49
22.750	0.00	0.66	1.172	O	|	|	|	2.48
22.833	0.00	0.65	1.168	O	|	|	|	2.47
22.917	0.00	0.64	1.163	O	|	|	|	2.46
23.000	0.00	0.64	1.159	O	|	|	|	2.46

23.083	0.00	0.63	1.155	o	|	|	|	|	2.45
23.167	0.00	0.63	1.150	o	|	|	|	|	2.44
23.250	0.00	0.62	1.146	o	|	|	|	|	2.43
23.333	0.00	0.62	1.142	o	|	|	|	|	2.42
23.417	0.00	0.61	1.137	o	|	|	|	|	2.42
23.500	0.00	0.61	1.133	o	|	|	|	|	2.41
23.583	0.00	0.60	1.129	o	|	|	|	|	2.40
23.667	0.00	0.60	1.125	o	|	|	|	|	2.39
23.750	0.00	0.59	1.121	o	|	|	|	|	2.38
23.833	0.00	0.59	1.117	o	|	|	|	|	2.38
23.917	0.00	0.58	1.113	o	|	|	|	|	2.37
24.000	0.00	0.58	1.109	o	|	|	|	|	2.36
24.083	0.00	0.57	1.105	o	|	|	|	|	2.36
24.167	0.00	0.57	1.101	o	|	|	|	|	2.35
24.250	0.00	0.56	1.097	o	|	|	|	|	2.34
24.333	0.00	0.56	1.093	o	|	|	|	|	2.33
24.417	0.00	0.55	1.089	o	|	|	|	|	2.33
24.500	0.00	0.55	1.085	o	|	|	|	|	2.32
24.583	0.00	0.55	1.082	o	|	|	|	|	2.31
24.667	0.00	0.54	1.078	o	|	|	|	|	2.31
24.750	0.00	0.54	1.074	o	|	|	|	|	2.30
24.833	0.00	0.53	1.070	o	|	|	|	|	2.29
24.917	0.00	0.53	1.067	o	|	|	|	|	2.28
25.000	0.00	0.52	1.063	o	|	|	|	|	2.28
25.083	0.00	0.52	1.060	o	|	|	|	|	2.27
25.167	0.00	0.52	1.056	o	|	|	|	|	2.26
25.250	0.00	0.51	1.052	o	|	|	|	|	2.26
25.333	0.00	0.51	1.049	o	|	|	|	|	2.25
25.417	0.00	0.50	1.045	o	|	|	|	|	2.24
25.500	0.00	0.50	1.042	o	|	|	|	|	2.24
25.583	0.00	0.49	1.039	o	|	|	|	|	2.23
25.667	0.00	0.49	1.035	o	|	|	|	|	2.23
25.750	0.00	0.49	1.032	o	|	|	|	|	2.22
25.833	0.00	0.48	1.029	o	|	|	|	|	2.21
25.917	0.00	0.48	1.025	o	|	|	|	|	2.21
26.000	0.00	0.47	1.022	o	|	|	|	|	2.20
26.083	0.00	0.47	1.019	o	|	|	|	|	2.19
26.167	0.00	0.47	1.015	o	|	|	|	|	2.19
26.250	0.00	0.46	1.012	o	|	|	|	|	2.18
26.333	0.00	0.46	1.009	o	|	|	|	|	2.18
26.417	0.00	0.45	1.006	o	|	|	|	|	2.17
26.500	0.00	0.45	1.003	o	|	|	|	|	2.17
26.583	0.00	0.45	1.000	o	|	|	|	|	2.16
26.667	0.00	0.44	0.997	o	|	|	|	|	2.15
26.750	0.00	0.44	0.994	o	|	|	|	|	2.15
26.833	0.00	0.44	0.991	o	|	|	|	|	2.14
26.917	0.00	0.43	0.988	o	|	|	|	|	2.14
27.000	0.00	0.43	0.985	o	|	|	|	|	2.13
27.083	0.00	0.43	0.982	o	|	|	|	|	2.13
27.167	0.00	0.42	0.979	o	|	|	|	|	2.12
27.250	0.00	0.42	0.976	o	|	|	|	|	2.12
27.333	0.00	0.42	0.973	o	|	|	|	|	2.11
27.417	0.00	0.41	0.970	o	|	|	|	|	2.10
27.500	0.00	0.41	0.967	o	|	|	|	|	2.10
27.583	0.00	0.40	0.965	o	|	|	|	|	2.09
27.667	0.00	0.40	0.962	o	|	|	|	|	2.09
27.750	0.00	0.40	0.959	o	|	|	|	|	2.08
27.833	0.00	0.39	0.956	o	|	|	|	|	2.08
27.917	0.00	0.39	0.954	o	|	|	|	|	2.07
28.000	0.00	0.39	0.951	o	|	|	|	|	2.07
28.083	0.00	0.39	0.948	o	|	|	|	|	2.06
28.167	0.00	0.38	0.946	o	|	|	|	|	2.06
28.250	0.00	0.38	0.943	o	|	|	|	|	2.05
28.333	0.00	0.38	0.940	o	|	|	|	|	2.05
28.417	0.00	0.37	0.938	o	|	|	|	|	2.04
28.500	0.00	0.37	0.935	o	|	|	|	|	2.04
28.583	0.00	0.37	0.933	o	|	|	|	|	2.03
28.667	0.00	0.36	0.930	o	|	|	|	|	2.03
28.750	0.00	0.36	0.928	o	|	|	|	|	2.03
28.833	0.00	0.36	0.925	o	|	|	|	|	2.02
28.917	0.00	0.35	0.923	o	|	|	|	|	2.02
29.000	0.00	0.35	0.920	o	|	|	|	|	2.01
29.083	0.00	0.35	0.918	o	|	|	|	|	2.01
29.167	0.00	0.35	0.916	o	|	|	|	|	2.00
29.250	0.00	0.34	0.913	o	|	|	|	|	2.00
29.333	0.00	0.34	0.911	o	|	|	|	|	1.99
29.417	0.00	0.34	0.908	o	|	|	|	|	1.99
29.500	0.00	0.34	0.906	o	|	|	|	|	1.98
29.583	0.00	0.34	0.904	o	|	|	|	|	1.98
29.667	0.00	0.34	0.901	o	|	|	|	|	1.97
29.750	0.00	0.34	0.899	o	|	|	|	|	1.97
29.833	0.00	0.34	0.897	o	|	|	|	|	1.96
29.917	0.00	0.34	0.894	o	|	|	|	|	1.96
30.000	0.00	0.34	0.892	o	|	|	|	|	1.95
30.083	0.00	0.34	0.890	o	|	|	|	|	1.95
30.167	0.00	0.34	0.887	o	|	|	|	|	1.94

30.250	0.00	0.34	0.885	o	|	|	|	|	1.94
30.333	0.00	0.34	0.883	o	|	|	|	|	1.94
30.417	0.00	0.34	0.880	o	|	|	|	|	1.93
30.500	0.00	0.34	0.878	o	|	|	|	|	1.93
30.583	0.00	0.33	0.876	o	|	|	|	|	1.92
30.667	0.00	0.33	0.873	o	|	|	|	|	1.92
30.750	0.00	0.33	0.871	o	|	|	|	|	1.91
30.833	0.00	0.33	0.869	o	|	|	|	|	1.91
30.917	0.00	0.33	0.867	o	|	|	|	|	1.90
31.000	0.00	0.33	0.864	o	|	|	|	|	1.90
31.083	0.00	0.33	0.862	o	|	|	|	|	1.89
31.167	0.00	0.33	0.860	o	|	|	|	|	1.89
31.250	0.00	0.33	0.857	o	|	|	|	|	1.88
31.333	0.00	0.33	0.855	o	|	|	|	|	1.88
31.417	0.00	0.33	0.853	o	|	|	|	|	1.87
31.500	0.00	0.33	0.851	o	|	|	|	|	1.87
31.583	0.00	0.33	0.848	o	|	|	|	|	1.86
31.667	0.00	0.33	0.846	o	|	|	|	|	1.86
31.750	0.00	0.33	0.844	o	|	|	|	|	1.85
31.833	0.00	0.33	0.842	o	|	|	|	|	1.85
31.917	0.00	0.33	0.839	o	|	|	|	|	1.85
32.000	0.00	0.33	0.837	o	|	|	|	|	1.84
32.083	0.00	0.32	0.835	o	|	|	|	|	1.84
32.167	0.00	0.32	0.833	o	|	|	|	|	1.83
32.250	0.00	0.32	0.830	o	|	|	|	|	1.83
32.333	0.00	0.32	0.828	o	|	|	|	|	1.82
32.417	0.00	0.32	0.826	o	|	|	|	|	1.82
32.500	0.00	0.32	0.824	o	|	|	|	|	1.81
32.583	0.00	0.32	0.822	o	|	|	|	|	1.81
32.667	0.00	0.32	0.819	o	|	|	|	|	1.80
32.750	0.00	0.32	0.817	o	|	|	|	|	1.80
32.833	0.00	0.32	0.815	o	|	|	|	|	1.79
32.917	0.00	0.32	0.813	o	|	|	|	|	1.79
33.000	0.00	0.32	0.811	o	|	|	|	|	1.79
33.083	0.00	0.32	0.808	o	|	|	|	|	1.78
33.167	0.00	0.32	0.806	o	|	|	|	|	1.78
33.250	0.00	0.32	0.804	o	|	|	|	|	1.77
33.333	0.00	0.32	0.802	o	|	|	|	|	1.77
33.417	0.00	0.32	0.800	o	|	|	|	|	1.76
33.500	0.00	0.32	0.797	o	|	|	|	|	1.76
33.583	0.00	0.31	0.795	o	|	|	|	|	1.75
33.667	0.00	0.31	0.793	o	|	|	|	|	1.75
33.750	0.00	0.31	0.791	o	|	|	|	|	1.75
33.833	0.00	0.31	0.789	o	|	|	|	|	1.74
33.917	0.00	0.31	0.787	o	|	|	|	|	1.74
34.000	0.00	0.31	0.785	o	|	|	|	|	1.73
34.083	0.00	0.31	0.782	o	|	|	|	|	1.73
34.167	0.00	0.31	0.780	o	|	|	|	|	1.72
34.250	0.00	0.31	0.778	o	|	|	|	|	1.72
34.333	0.00	0.31	0.776	o	|	|	|	|	1.71
34.417	0.00	0.31	0.774	o	|	|	|	|	1.71
34.500	0.00	0.31	0.772	o	|	|	|	|	1.71
34.583	0.00	0.31	0.770	o	|	|	|	|	1.70
34.667	0.00	0.31	0.767	o	|	|	|	|	1.70
34.750	0.00	0.31	0.765	o	|	|	|	|	1.69
34.833	0.00	0.31	0.763	o	|	|	|	|	1.69
34.917	0.00	0.31	0.761	o	|	|	|	|	1.68
35.000	0.00	0.31	0.759	o	|	|	|	|	1.68
35.083	0.00	0.31	0.757	o	|	|	|	|	1.67
35.167	0.00	0.30	0.755	o	|	|	|	|	1.67
35.250	0.00	0.30	0.753	o	|	|	|	|	1.67
35.333	0.00	0.30	0.751	o	|	|	|	|	1.66
35.417	0.00	0.30	0.748	o	|	|	|	|	1.66
35.500	0.00	0.30	0.746	o	|	|	|	|	1.65
35.583	0.00	0.30	0.744	o	|	|	|	|	1.65
35.667	0.00	0.30	0.742	o	|	|	|	|	1.64
35.750	0.00	0.30	0.740	o	|	|	|	|	1.64
35.833	0.00	0.30	0.738	o	|	|	|	|	1.64
35.917	0.00	0.30	0.736	o	|	|	|	|	1.63
36.000	0.00	0.30	0.734	o	|	|	|	|	1.63
36.083	0.00	0.30	0.732	o	|	|	|	|	1.62
36.167	0.00	0.30	0.730	o	|	|	|	|	1.62
36.250	0.00	0.30	0.728	o	|	|	|	|	1.61
36.333	0.00	0.30	0.726	o	|	|	|	|	1.61
36.417	0.00	0.30	0.724	o	|	|	|	|	1.61
36.500	0.00	0.30	0.722	o	|	|	|	|	1.60
36.583	0.00	0.30	0.720	o	|	|	|	|	1.60
36.667	0.00	0.30	0.718	o	|	|	|	|	1.59
36.750	0.00	0.30	0.716	o	|	|	|	|	1.59
36.833	0.00	0.29	0.714	o	|	|	|	|	1.58
36.917	0.00	0.29	0.711	o	|	|	|	|	1.58
37.000	0.00	0.29	0.709	o	|	|	|	|	1.58
37.083	0.00	0.29	0.707	o	|	|	|	|	1.57
37.167	0.00	0.29	0.705	o	|	|	|	|	1.57
37.250	0.00	0.29	0.703	o	|	|	|	|	1.56
37.333	0.00	0.29	0.701	o	|	|	|	|	1.56

37.417	0.00	0.29	0.699	o	|	|	|	|	1.56
37.500	0.00	0.29	0.697	o	|	|	|	|	1.55
37.583	0.00	0.29	0.695	o	|	|	|	|	1.55
37.667	0.00	0.29	0.693	o	|	|	|	|	1.54
37.750	0.00	0.29	0.691	o	|	|	|	|	1.54
37.833	0.00	0.29	0.689	o	|	|	|	|	1.53
37.917	0.00	0.29	0.687	o	|	|	|	|	1.53
38.000	0.00	0.29	0.685	o	|	|	|	|	1.53
38.083	0.00	0.29	0.683	o	|	|	|	|	1.52
38.167	0.00	0.29	0.681	o	|	|	|	|	1.52
38.250	0.00	0.29	0.680	o	|	|	|	|	1.51
38.333	0.00	0.29	0.678	o	|	|	|	|	1.51
38.417	0.00	0.29	0.676	o	|	|	|	|	1.51
38.500	0.00	0.28	0.674	o	|	|	|	|	1.50
38.583	0.00	0.28	0.672	o	|	|	|	|	1.50
38.667	0.00	0.28	0.670	o	|	|	|	|	1.49
38.750	0.00	0.28	0.668	o	|	|	|	|	1.49
38.833	0.00	0.28	0.666	o	|	|	|	|	1.49
38.917	0.00	0.28	0.664	o	|	|	|	|	1.48
39.000	0.00	0.28	0.662	o	|	|	|	|	1.48
39.083	0.00	0.28	0.660	o	|	|	|	|	1.47
39.167	0.00	0.28	0.658	o	|	|	|	|	1.47
39.250	0.00	0.28	0.656	o	|	|	|	|	1.47
39.333	0.00	0.28	0.654	o	|	|	|	|	1.46
39.417	0.00	0.28	0.652	o	|	|	|	|	1.46
39.500	0.00	0.28	0.650	o	|	|	|	|	1.45
39.583	0.00	0.28	0.648	o	|	|	|	|	1.45
39.667	0.00	0.28	0.646	o	|	|	|	|	1.45
39.750	0.00	0.28	0.645	o	|	|	|	|	1.44
39.833	0.00	0.28	0.643	o	|	|	|	|	1.44
39.917	0.00	0.28	0.641	o	|	|	|	|	1.43
40.000	0.00	0.28	0.639	o	|	|	|	|	1.43
40.083	0.00	0.28	0.637	o	|	|	|	|	1.43
40.167	0.00	0.28	0.635	o	|	|	|	|	1.42
40.250	0.00	0.27	0.633	o	|	|	|	|	1.42
40.333	0.00	0.27	0.631	o	|	|	|	|	1.41
40.417	0.00	0.27	0.629	o	|	|	|	|	1.41
40.500	0.00	0.27	0.627	o	|	|	|	|	1.41
40.583	0.00	0.27	0.626	o	|	|	|	|	1.40
40.667	0.00	0.27	0.624	o	|	|	|	|	1.40
40.750	0.00	0.27	0.622	o	|	|	|	|	1.40
40.833	0.00	0.27	0.620	o	|	|	|	|	1.39
40.917	0.00	0.27	0.618	o	|	|	|	|	1.39
41.000	0.00	0.27	0.616	o	|	|	|	|	1.38
41.083	0.00	0.27	0.614	o	|	|	|	|	1.38
41.167	0.00	0.27	0.613	o	|	|	|	|	1.38
41.250	0.00	0.27	0.611	o	|	|	|	|	1.37
41.333	0.00	0.27	0.609	o	|	|	|	|	1.37
41.417	0.00	0.27	0.607	o	|	|	|	|	1.36
41.500	0.00	0.27	0.605	o	|	|	|	|	1.36
41.583	0.00	0.27	0.603	o	|	|	|	|	1.36
41.667	0.00	0.27	0.601	o	|	|	|	|	1.35
41.750	0.00	0.27	0.600	o	|	|	|	|	1.35
41.833	0.00	0.27	0.598	o	|	|	|	|	1.35
41.917	0.00	0.27	0.596	o	|	|	|	|	1.34
42.000	0.00	0.27	0.594	o	|	|	|	|	1.34
42.083	0.00	0.26	0.592	o	|	|	|	|	1.33
42.167	0.00	0.26	0.590	o	|	|	|	|	1.33
42.250	0.00	0.26	0.589	o	|	|	|	|	1.33
42.333	0.00	0.26	0.587	o	|	|	|	|	1.32
42.417	0.00	0.26	0.585	o	|	|	|	|	1.32
42.500	0.00	0.26	0.583	o	|	|	|	|	1.32
42.583	0.00	0.26	0.581	o	|	|	|	|	1.31
42.667	0.00	0.26	0.580	o	|	|	|	|	1.31
42.750	0.00	0.26	0.578	o	|	|	|	|	1.30
42.833	0.00	0.26	0.576	o	|	|	|	|	1.30
42.917	0.00	0.26	0.574	o	|	|	|	|	1.30
43.000	0.00	0.26	0.572	o	|	|	|	|	1.29
43.083	0.00	0.26	0.571	o	|	|	|	|	1.29
43.167	0.00	0.26	0.569	o	|	|	|	|	1.29
43.250	0.00	0.26	0.567	o	|	|	|	|	1.28
43.333	0.00	0.26	0.565	o	|	|	|	|	1.28
43.417	0.00	0.26	0.563	o	|	|	|	|	1.27
43.500	0.00	0.26	0.562	o	|	|	|	|	1.27
43.583	0.00	0.26	0.560	o	|	|	|	|	1.27
43.667	0.00	0.26	0.558	o	|	|	|	|	1.26
43.750	0.00	0.26	0.556	o	|	|	|	|	1.26
43.833	0.00	0.26	0.555	o	|	|	|	|	1.26
43.917	0.00	0.26	0.553	o	|	|	|	|	1.25
44.000	0.00	0.25	0.551	o	|	|	|	|	1.25
44.083	0.00	0.25	0.549	o	|	|	|	|	1.25
44.167	0.00	0.25	0.548	o	|	|	|	|	1.24
44.250	0.00	0.25	0.546	o	|	|	|	|	1.24
44.333	0.00	0.25	0.544	o	|	|	|	|	1.23
44.417	0.00	0.25	0.542	o	|	|	|	|	1.23
44.500	0.00	0.25	0.541	o	|	|	|	|	1.23

44.583	0.00	0.25	0.539	o	|	|	|	|	1.22
44.667	0.00	0.25	0.537	o	|	|	|	|	1.22
44.750	0.00	0.25	0.535	o	|	|	|	|	1.22
44.833	0.00	0.25	0.534	o	|	|	|	|	1.21
44.917	0.00	0.25	0.532	o	|	|	|	|	1.21
45.000	0.00	0.25	0.530	o	|	|	|	|	1.21
45.083	0.00	0.25	0.529	o	|	|	|	|	1.20
45.167	0.00	0.25	0.527	o	|	|	|	|	1.20
45.250	0.00	0.25	0.525	o	|	|	|	|	1.19
45.333	0.00	0.25	0.523	o	|	|	|	|	1.19
45.417	0.00	0.25	0.522	o	|	|	|	|	1.19
45.500	0.00	0.25	0.520	o	|	|	|	|	1.18
45.583	0.00	0.25	0.518	o	|	|	|	|	1.18
45.667	0.00	0.25	0.517	o	|	|	|	|	1.18
45.750	0.00	0.25	0.515	o	|	|	|	|	1.17
45.833	0.00	0.25	0.513	o	|	|	|	|	1.17
45.917	0.00	0.24	0.512	o	|	|	|	|	1.17
46.000	0.00	0.24	0.510	o	|	|	|	|	1.16
46.083	0.00	0.24	0.508	o	|	|	|	|	1.16
46.167	0.00	0.24	0.507	o	|	|	|	|	1.16
46.250	0.00	0.24	0.505	o	|	|	|	|	1.15
46.333	0.00	0.24	0.503	o	|	|	|	|	1.15
46.417	0.00	0.24	0.502	o	|	|	|	|	1.15
46.500	0.00	0.24	0.500	o	|	|	|	|	1.14
46.583	0.00	0.24	0.498	o	|	|	|	|	1.14
46.667	0.00	0.24	0.497	o	|	|	|	|	1.14
46.750	0.00	0.24	0.495	o	|	|	|	|	1.13
46.833	0.00	0.24	0.493	o	|	|	|	|	1.13
46.917	0.00	0.24	0.492	o	|	|	|	|	1.13
47.000	0.00	0.24	0.490	o	|	|	|	|	1.12
47.083	0.00	0.24	0.488	o	|	|	|	|	1.12
47.167	0.00	0.24	0.487	o	|	|	|	|	1.12
47.250	0.00	0.24	0.485	o	|	|	|	|	1.11
47.333	0.00	0.24	0.483	o	|	|	|	|	1.11
47.417	0.00	0.24	0.482	o	|	|	|	|	1.10
47.500	0.00	0.24	0.480	o	|	|	|	|	1.10
47.583	0.00	0.24	0.478	o	|	|	|	|	1.10
47.667	0.00	0.24	0.477	o	|	|	|	|	1.09
47.750	0.00	0.24	0.475	o	|	|	|	|	1.09
47.833	0.00	0.24	0.474	o	|	|	|	|	1.09
47.917	0.00	0.24	0.472	o	|	|	|	|	1.08
48.000	0.00	0.23	0.470	o	|	|	|	|	1.08
48.083	0.00	0.23	0.469	o	|	|	|	|	1.08
48.167	0.00	0.23	0.467	o	|	|	|	|	1.07
48.250	0.00	0.23	0.465	o	|	|	|	|	1.07
48.333	0.00	0.23	0.464	o	|	|	|	|	1.07
48.417	0.00	0.23	0.462	o	|	|	|	|	1.06
48.500	0.00	0.23	0.461	o	|	|	|	|	1.06
48.583	0.00	0.23	0.459	o	|	|	|	|	1.06
48.667	0.00	0.23	0.457	o	|	|	|	|	1.05
48.750	0.00	0.23	0.456	o	|	|	|	|	1.05
48.833	0.00	0.23	0.454	o	|	|	|	|	1.05
48.917	0.00	0.23	0.453	o	|	|	|	|	1.04
49.000	0.00	0.23	0.451	o	|	|	|	|	1.04
49.083	0.00	0.23	0.450	o	|	|	|	|	1.04
49.167	0.00	0.23	0.448	o	|	|	|	|	1.04
49.250	0.00	0.23	0.446	o	|	|	|	|	1.03
49.333	0.00	0.23	0.445	o	|	|	|	|	1.03
49.417	0.00	0.23	0.443	o	|	|	|	|	1.03
49.500	0.00	0.23	0.442	o	|	|	|	|	1.02
49.583	0.00	0.23	0.440	o	|	|	|	|	1.02
49.667	0.00	0.23	0.439	o	|	|	|	|	1.02
49.750	0.00	0.23	0.437	o	|	|	|	|	1.01
49.833	0.00	0.23	0.435	o	|	|	|	|	1.01
49.917	0.00	0.23	0.434	o	|	|	|	|	1.01
50.000	0.00	0.23	0.432	o	|	|	|	|	1.00
50.083	0.00	0.22	0.431	o	|	|	|	|	1.00
50.167	0.00	0.22	0.429	o	|	|	|	|	1.00
50.250	0.00	0.22	0.428	o	|	|	|	|	0.99
50.333	0.00	0.22	0.426	o	|	|	|	|	0.99
50.417	0.00	0.22	0.425	o	|	|	|	|	0.99
50.500	0.00	0.22	0.423	o	|	|	|	|	0.98
50.583	0.00	0.22	0.422	o	|	|	|	|	0.98
50.667	0.00	0.22	0.420	o	|	|	|	|	0.97
50.750	0.00	0.22	0.419	o	|	|	|	|	0.97
50.833	0.00	0.22	0.417	o	|	|	|	|	0.97
50.917	0.00	0.22	0.416	o	|	|	|	|	0.96
51.000	0.00	0.22	0.414	o	|	|	|	|	0.96
51.083	0.00	0.22	0.413	o	|	|	|	|	0.96
51.167	0.00	0.21	0.411	o	|	|	|	|	0.95
51.250	0.00	0.21	0.410	o	|	|	|	|	0.95
51.333	0.00	0.21	0.408	o	|	|	|	|	0.95
51.417	0.00	0.21	0.407	o	|	|	|	|	0.94
51.500	0.00	0.21	0.405	o	|	|	|	|	0.94
51.583	0.00	0.21	0.404	o	|	|	|	|	0.94
51.667	0.00	0.21	0.402	o	|	|	|	|	0.93

51.750	0.00	0.21	0.401	o	|	|	|	0.93
51.833	0.00	0.21	0.399	o	|	|	|	0.93
51.917	0.00	0.21	0.398	o	|	|	|	0.92
52.000	0.00	0.21	0.397	o	|	|	|	0.92
52.083	0.00	0.21	0.395	o	|	|	|	0.92
52.167	0.00	0.21	0.394	o	|	|	|	0.91
52.250	0.00	0.20	0.392	o	|	|	|	0.91
52.333	0.00	0.20	0.391	o	|	|	|	0.91
52.417	0.00	0.20	0.390	o	|	|	|	0.90
52.500	0.00	0.20	0.388	o	|	|	|	0.90
52.583	0.00	0.20	0.387	o	|	|	|	0.90
52.667	0.00	0.20	0.385	o	|	|	|	0.89
52.750	0.00	0.20	0.384	o	|	|	|	0.89
52.833	0.00	0.20	0.383	o	|	|	|	0.89
52.917	0.00	0.20	0.381	o	|	|	|	0.88
53.000	0.00	0.20	0.380	o	|	|	|	0.88
53.083	0.00	0.20	0.378	o	|	|	|	0.88
53.167	0.00	0.20	0.377	o	|	|	|	0.87
53.250	0.00	0.20	0.376	o	|	|	|	0.87
53.333	0.00	0.20	0.374	o	|	|	|	0.87
53.417	0.00	0.19	0.373	o	|	|	|	0.87
53.500	0.00	0.19	0.372	o	|	|	|	0.86
53.583	0.00	0.19	0.370	o	|	|	|	0.86
53.667	0.00	0.19	0.369	o	|	|	|	0.86
53.750	0.00	0.19	0.368	o	|	|	|	0.85
53.833	0.00	0.19	0.366	o	|	|	|	0.85
53.917	0.00	0.19	0.365	o	|	|	|	0.85
54.000	0.00	0.19	0.364	o	|	|	|	0.84
54.083	0.00	0.19	0.362	o	|	|	|	0.84
54.167	0.00	0.19	0.361	o	|	|	|	0.84
54.250	0.00	0.19	0.360	o	|	|	|	0.83
54.333	0.00	0.19	0.359	o	|	|	|	0.83
54.417	0.00	0.19	0.357	o	|	|	|	0.83
54.500	0.00	0.19	0.356	o	|	|	|	0.83
54.583	0.00	0.19	0.355	o	|	|	|	0.82
54.667	0.00	0.18	0.353	o	|	|	|	0.82
54.750	0.00	0.18	0.352	o	|	|	|	0.82
54.833	0.00	0.18	0.351	o	|	|	|	0.81
54.917	0.00	0.18	0.350	o	|	|	|	0.81
55.000	0.00	0.18	0.348	o	|	|	|	0.81
55.083	0.00	0.18	0.347	o	|	|	|	0.81
55.167	0.00	0.18	0.346	o	|	|	|	0.80
55.250	0.00	0.18	0.345	o	|	|	|	0.80
55.333	0.00	0.18	0.343	o	|	|	|	0.80
55.417	0.00	0.18	0.342	o	|	|	|	0.79
55.500	0.00	0.18	0.341	o	|	|	|	0.79
55.583	0.00	0.18	0.340	o	|	|	|	0.79
55.667	0.00	0.18	0.339	o	|	|	|	0.79
55.750	0.00	0.18	0.337	o	|	|	|	0.78
55.833	0.00	0.18	0.336	o	|	|	|	0.78
55.917	0.00	0.17	0.335	o	|	|	|	0.78
56.000	0.00	0.17	0.334	o	|	|	|	0.77
56.083	0.00	0.17	0.333	o	|	|	|	0.77
56.167	0.00	0.17	0.331	o	|	|	|	0.77
56.250	0.00	0.17	0.330	o	|	|	|	0.77
56.333	0.00	0.17	0.329	o	|	|	|	0.76
56.417	0.00	0.17	0.328	o	|	|	|	0.76
56.500	0.00	0.17	0.327	o	|	|	|	0.76
56.583	0.00	0.17	0.325	o	|	|	|	0.76
56.667	0.00	0.17	0.324	o	|	|	|	0.75
56.750	0.00	0.17	0.323	o	|	|	|	0.75
56.833	0.00	0.17	0.322	o	|	|	|	0.75
56.917	0.00	0.17	0.321	o	|	|	|	0.74
57.000	0.00	0.17	0.320	o	|	|	|	0.74
57.083	0.00	0.17	0.318	o	|	|	|	0.74
57.167	0.00	0.17	0.317	o	|	|	|	0.74
57.250	0.00	0.17	0.316	o	|	|	|	0.73
57.333	0.00	0.16	0.315	o	|	|	|	0.73
57.417	0.00	0.16	0.314	o	|	|	|	0.73
57.500	0.00	0.16	0.313	o	|	|	|	0.73
57.583	0.00	0.16	0.312	o	|	|	|	0.72
57.667	0.00	0.16	0.311	o	|	|	|	0.72
57.750	0.00	0.16	0.309	o	|	|	|	0.72
57.833	0.00	0.16	0.308	o	|	|	|	0.72
57.917	0.00	0.16	0.307	o	|	|	|	0.71
58.000	0.00	0.16	0.306	o	|	|	|	0.71
58.083	0.00	0.16	0.305	o	|	|	|	0.71
58.167	0.00	0.16	0.304	o	|	|	|	0.71
58.250	0.00	0.16	0.303	o	|	|	|	0.70
58.333	0.00	0.16	0.302	o	|	|	|	0.70
58.417	0.00	0.16	0.301	o	|	|	|	0.70
58.500	0.00	0.16	0.300	o	|	|	|	0.70
58.583	0.00	0.16	0.299	o	|	|	|	0.69
58.667	0.00	0.16	0.297	o	|	|	|	0.69
58.750	0.00	0.15	0.296	o	|	|	|	0.69
58.833	0.00	0.15	0.295	o	|	|	|	0.69

58.917	0.00	0.15	0.294	o	|	|	|	0.68
59.000	0.00	0.15	0.293	o	|	|	|	0.68
59.083	0.00	0.15	0.292	o	|	|	|	0.68
59.167	0.00	0.15	0.291	o	|	|	|	0.68
59.250	0.00	0.15	0.290	o	|	|	|	0.67
59.333	0.00	0.15	0.289	o	|	|	|	0.67
59.417	0.00	0.15	0.288	o	|	|	|	0.67
59.500	0.00	0.15	0.287	o	|	|	|	0.67
59.583	0.00	0.15	0.286	o	|	|	|	0.66
59.667	0.00	0.15	0.285	o	|	|	|	0.66
59.750	0.00	0.15	0.284	o	|	|	|	0.66
59.833	0.00	0.15	0.283	o	|	|	|	0.66
59.917	0.00	0.15	0.282	o	|	|	|	0.65
60.000	0.00	0.15	0.281	o	|	|	|	0.65
60.083	0.00	0.15	0.280	o	|	|	|	0.65
60.167	0.00	0.15	0.279	o	|	|	|	0.65
60.250	0.00	0.15	0.278	o	|	|	|	0.64
60.333	0.00	0.14	0.277	o	|	|	|	0.64
60.417	0.00	0.14	0.276	o	|	|	|	0.64
60.500	0.00	0.14	0.275	o	|	|	|	0.64
60.583	0.00	0.14	0.274	o	|	|	|	0.64
60.667	0.00	0.14	0.273	o	|	|	|	0.63
60.750	0.00	0.14	0.272	o	|	|	|	0.63
60.833	0.00	0.14	0.271	o	|	|	|	0.63
60.917	0.00	0.14	0.270	o	|	|	|	0.63
61.000	0.00	0.14	0.269	o	|	|	|	0.62
61.083	0.00	0.14	0.268	o	|	|	|	0.62
61.167	0.00	0.14	0.267	o	|	|	|	0.62
61.250	0.00	0.14	0.266	o	|	|	|	0.62
61.333	0.00	0.14	0.265	o	|	|	|	0.62
61.417	0.00	0.14	0.264	o	|	|	|	0.61
61.500	0.00	0.14	0.263	o	|	|	|	0.61
61.583	0.00	0.14	0.262	o	|	|	|	0.61
61.667	0.00	0.14	0.261	o	|	|	|	0.61
61.750	0.00	0.14	0.260	o	|	|	|	0.60
61.833	0.00	0.14	0.259	o	|	|	|	0.60
61.917	0.00	0.13	0.259	o	|	|	|	0.60
62.000	0.00	0.13	0.258	o	|	|	|	0.60
62.083	0.00	0.13	0.257	o	|	|	|	0.60
62.167	0.00	0.13	0.256	o	|	|	|	0.59
62.250	0.00	0.13	0.255	o	|	|	|	0.59
62.333	0.00	0.13	0.254	o	|	|	|	0.59
62.417	0.00	0.13	0.253	o	|	|	|	0.59
62.500	0.00	0.13	0.252	o	|	|	|	0.58
62.583	0.00	0.13	0.251	o	|	|	|	0.58
62.667	0.00	0.13	0.250	o	|	|	|	0.58
62.750	0.00	0.13	0.249	o	|	|	|	0.58
62.833	0.00	0.13	0.249	o	|	|	|	0.58
62.917	0.00	0.13	0.248	o	|	|	|	0.57
63.000	0.00	0.13	0.247	o	|	|	|	0.57
63.083	0.00	0.13	0.246	o	|	|	|	0.57
63.167	0.00	0.13	0.245	o	|	|	|	0.57
63.250	0.00	0.13	0.244	o	|	|	|	0.57
63.333	0.00	0.13	0.243	o	|	|	|	0.56
63.417	0.00	0.13	0.242	o	|	|	|	0.56
63.500	0.00	0.13	0.241	o	|	|	|	0.56
63.583	0.00	0.13	0.241	o	|	|	|	0.56
63.667	0.00	0.13	0.240	o	|	|	|	0.56
63.750	0.00	0.12	0.239	o	|	|	|	0.55
63.833	0.00	0.12	0.238	o	|	|	|	0.55
63.917	0.00	0.12	0.237	o	|	|	|	0.55
64.000	0.00	0.12	0.236	o	|	|	|	0.55
64.083	0.00	0.12	0.235	o	|	|	|	0.55
64.167	0.00	0.12	0.235	o	|	|	|	0.54
64.250	0.00	0.12	0.234	o	|	|	|	0.54
64.333	0.00	0.12	0.233	o	|	|	|	0.54
64.417	0.00	0.12	0.232	o	|	|	|	0.54
64.500	0.00	0.12	0.231	o	|	|	|	0.54
64.583	0.00	0.12	0.230	o	|	|	|	0.53
64.667	0.00	0.12	0.230	o	|	|	|	0.53
64.750	0.00	0.12	0.229	o	|	|	|	0.53
64.833	0.00	0.12	0.228	o	|	|	|	0.53
64.917	0.00	0.12	0.227	o	|	|	|	0.53
65.000	0.00	0.12	0.226	o	|	|	|	0.53
65.083	0.00	0.12	0.226	o	|	|	|	0.52
65.167	0.00	0.12	0.225	o	|	|	|	0.52
65.250	0.00	0.12	0.224	o	|	|	|	0.52
65.333	0.00	0.12	0.223	o	|	|	|	0.52
65.417	0.00	0.12	0.222	o	|	|	|	0.52
65.500	0.00	0.12	0.221	o	|	|	|	0.51
65.583	0.00	0.12	0.221	o	|	|	|	0.51
65.667	0.00	0.11	0.220	o	|	|	|	0.51
65.750	0.00	0.11	0.219	o	|	|	|	0.51
65.833	0.00	0.11	0.218	o	|	|	|	0.51
65.917	0.00	0.11	0.218	o	|	|	|	0.50
66.000	0.00	0.11	0.217	o	|	|	|	0.50

66.083	0.00	0.11	0.216	o	|	|	|	|	0.50
66.167	0.00	0.11	0.215	o	|	|	|	|	0.50
66.250	0.00	0.11	0.214	o	|	|	|	|	0.50
66.333	0.00	0.11	0.214	o	|	|	|	|	0.50
66.417	0.00	0.11	0.213	o	|	|	|	|	0.49
66.500	0.00	0.11	0.212	o	|	|	|	|	0.49
66.583	0.00	0.11	0.211	o	|	|	|	|	0.49
66.667	0.00	0.11	0.211	o	|	|	|	|	0.49
66.750	0.00	0.11	0.210	o	|	|	|	|	0.49
66.833	0.00	0.11	0.209	o	|	|	|	|	0.49
66.917	0.00	0.11	0.208	o	|	|	|	|	0.48
67.000	0.00	0.11	0.208	o	|	|	|	|	0.48
67.083	0.00	0.11	0.207	o	|	|	|	|	0.48
67.167	0.00	0.11	0.206	o	|	|	|	|	0.48
67.250	0.00	0.11	0.205	o	|	|	|	|	0.48
67.333	0.00	0.11	0.205	o	|	|	|	|	0.47
67.417	0.00	0.11	0.204	o	|	|	|	|	0.47
67.500	0.00	0.11	0.203	o	|	|	|	|	0.47
67.583	0.00	0.11	0.202	o	|	|	|	|	0.47
67.667	0.00	0.11	0.202	o	|	|	|	|	0.47
67.750	0.00	0.10	0.201	o	|	|	|	|	0.47
67.833	0.00	0.10	0.200	o	|	|	|	|	0.46
67.917	0.00	0.10	0.200	o	|	|	|	|	0.46
68.000	0.00	0.10	0.199	o	|	|	|	|	0.46
68.083	0.00	0.10	0.198	o	|	|	|	|	0.46
68.167	0.00	0.10	0.197	o	|	|	|	|	0.46
68.250	0.00	0.10	0.197	o	|	|	|	|	0.46
68.333	0.00	0.10	0.196	o	|	|	|	|	0.45
68.417	0.00	0.10	0.195	o	|	|	|	|	0.45
68.500	0.00	0.10	0.195	o	|	|	|	|	0.45
68.583	0.00	0.10	0.194	o	|	|	|	|	0.45
68.667	0.00	0.10	0.193	o	|	|	|	|	0.45
68.750	0.00	0.10	0.193	o	|	|	|	|	0.45
68.833	0.00	0.10	0.192	o	|	|	|	|	0.45
68.917	0.00	0.10	0.191	o	|	|	|	|	0.44

Remaining water in basin = 0.19 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 827
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 11.484 (CFS)
Total volume = 3.309 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro25245.rte
**********HYDROGRAPH DATA**********
Number of intervals = 293
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 9.054 (CFS)
Total volume = 5.502 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
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Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 293
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.431	0.225	0.430	0.432
2.000	0.914	0.344	0.913	0.915
3.000	1.451	0.991	1.448	1.454
4.000	2.049	1.417	2.044	2.054
5.000	2.712	1.731	2.706	2.718
5.250	2.888	1.801	2.882	2.894
5.500	3.069	17.046	3.010	3.128
6.000	3.443	225.078	2.668	4.218

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 2.3 4.53 6.79 9.05	Depth (Ft.)
0.083	0.16	0.00	0.001	O | | | |	0.00
0.167	0.41	0.00	0.002	OI | | | |	0.01
0.250	0.48	0.00	0.006	OI | | | |	0.01
0.333	0.58	0.00	0.009	O I | | | |	0.02
0.417	0.73	0.01	0.014	O I | | | |	0.03
0.500	0.77	0.01	0.019	O I | | | |	0.04
0.583	0.79	0.01	0.024	O I | | | |	0.06
0.667	0.79	0.02	0.029	O I | | | |	0.07
0.750	0.80	0.02	0.035	O I | | | |	0.08
0.833	0.88	0.02	0.040	O I | | | |	0.09
0.917	1.00	0.02	0.047	O I | | | |	0.11
1.000	1.04	0.03	0.054	O I | | | |	0.12
1.083	0.97	0.03	0.060	O I | | | |	0.14
1.167	0.85	0.03	0.066	O I | | | |	0.15
1.250	0.83	0.04	0.072	O I | | | |	0.17
1.333	0.81	0.04	0.077	O I | | | |	0.18
1.417	0.80	0.04	0.083	O I | | | |	0.19
1.500	0.80	0.05	0.088	O I | | | |	0.20

1.583	0.80	0.05	0.093	o I	|	|	|	|	0.22
1.667	0.80	0.05	0.098	o I	|	|	|	|	0.23
1.750	0.80	0.05	0.103	o I	|	|	|	|	0.24
1.833	0.88	0.06	0.109	o I	|	|	|	|	0.25
1.917	1.00	0.06	0.115	o I	|	|	|	|	0.27
2.000	1.04	0.06	0.121	o I	|	|	|	|	0.28
2.083	1.05	0.07	0.128	o I	|	|	|	|	0.30
2.167	1.06	0.07	0.135	o I	|	|	|	|	0.31
2.250	1.07	0.07	0.142	o I	|	|	|	|	0.33
2.333	1.07	0.08	0.148	o I	|	|	|	|	0.34
2.417	1.07	0.08	0.155	o I	|	|	|	|	0.36
2.500	1.07	0.08	0.162	o I	|	|	|	|	0.38
2.583	1.14	0.09	0.169	o I	|	|	|	|	0.39
2.667	1.27	0.09	0.177	o I	|	|	|	|	0.41
2.750	1.30	0.10	0.185	o I	|	|	|	|	0.43
2.833	1.32	0.10	0.193	o I	|	|	|	|	0.45
2.917	1.33	0.11	0.202	o I	|	|	|	|	0.47
3.000	1.33	0.11	0.210	o I	|	|	|	|	0.49
3.083	1.33	0.11	0.218	o I	|	|	|	|	0.51
3.167	1.33	0.12	0.227	o I	|	|	|	|	0.53
3.250	1.33	0.12	0.235	o I	|	|	|	|	0.55
3.333	1.33	0.13	0.243	o I	|	|	|	|	0.56
3.417	1.33	0.13	0.252	o I	|	|	|	|	0.58
3.500	1.33	0.14	0.260	o I	|	|	|	|	0.60
3.583	1.33	0.14	0.268	o I	|	|	|	|	0.62
3.667	1.33	0.14	0.276	o I	|	|	|	|	0.64
3.750	1.33	0.15	0.285	o I	|	|	|	|	0.66
3.833	1.41	0.15	0.293	o I	|	|	|	|	0.68
3.917	1.54	0.16	0.302	o I	|	|	|	|	0.70
4.000	1.57	0.16	0.312	o I	|	|	|	|	0.72
4.083	1.58	0.17	0.321	o I	|	|	|	|	0.75
4.167	1.59	0.17	0.331	o I	|	|	|	|	0.77
4.250	1.60	0.18	0.341	o I	|	|	|	|	0.79
4.333	1.68	0.18	0.351	o I	|	|	|	|	0.81
4.417	1.80	0.19	0.362	o I	|	|	|	|	0.84
4.500	1.84	0.19	0.373	o I	|	|	|	|	0.87
4.583	1.85	0.20	0.384	o I	|	|	|	|	0.89
4.667	1.86	0.21	0.396	o I	|	|	|	|	0.92
4.750	1.86	0.21	0.407	o I	|	|	|	|	0.94
4.833	1.94	0.22	0.419	o I	|	|	|	|	0.97
4.917	2.07	0.22	0.431	o I	|	|	|	|	1.00
5.000	2.10	0.23	0.444	o I	|	|	|	|	1.03
5.083	1.96	0.23	0.456	o I	|	|	|	|	1.05
5.167	1.71	0.23	0.467	o I	|	|	|	|	1.07
5.250	1.65	0.24	0.477	o I	|	|	|	|	1.10
5.333	1.70	0.24	0.487	o I	|	|	|	|	1.12
5.417	1.82	0.24	0.497	o I	|	|	|	|	1.14
5.500	1.84	0.24	0.508	o I	|	|	|	|	1.16
5.583	1.93	0.25	0.520	o I	|	|	|	|	1.18
5.667	2.06	0.25	0.532	o I	|	|	|	|	1.21
5.750	2.10	0.25	0.544	o I	|	|	|	|	1.23
5.833	2.12	0.26	0.557	o I	|	|	|	|	1.26
5.917	2.12	0.26	0.570	o I	|	|	|	|	1.29
6.000	2.13	0.26	0.583	o I	|	|	|	|	1.31
6.083	2.21	0.27	0.596	o I	|	|	|	|	1.34
6.167	2.34	0.27	0.610	o I	|	|	|	|	1.37
6.250	2.37	0.27	0.624	o I	|	|	|	|	1.40
6.333	2.38	0.28	0.639	o I	|	|	|	|	1.43
6.417	2.39	0.28	0.653	o I	|	|	|	|	1.46
6.500	2.40	0.28	0.668	| o I	|	|	|	|	1.49
6.583	2.47	0.29	0.682	| o I	|	|	|	|	1.52
6.667	2.60	0.29	0.698	| o I	|	|	|	|	1.55
6.750	2.63	0.29	0.714	| o I	|	|	|	|	1.59
6.833	2.65	0.30	0.730	| o I	|	|	|	|	1.62
6.917	2.66	0.30	0.746	| o I	|	|	|	|	1.65
7.000	2.66	0.31	0.762	| o I	|	|	|	|	1.69
7.083	2.66	0.31	0.779	| o I	|	|	|	|	1.72
7.167	2.66	0.31	0.795	| o I	|	|	|	|	1.75
7.250	2.66	0.32	0.811	| o I	|	|	|	|	1.79
7.333	2.74	0.32	0.827	| o I	|	|	|	|	1.82
7.417	2.87	0.33	0.845	| o I	|	|	|	|	1.86
7.500	2.90	0.33	0.862	| o I	|	|	|	|	1.89
7.583	2.99	0.34	0.880	| o I	|	|	|	|	1.93
7.667	3.13	0.34	0.899	| o I	|	|	|	|	1.97
7.750	3.17	0.35	0.918	| o I	|	|	|	|	2.01
7.833	3.26	0.37	0.938	| o I	|	|	|	|	2.04
7.917	3.40	0.40	0.958	| o I	|	|	|	|	2.08
8.000	3.43	0.42	0.979	| o I	|	|	|	|	2.12
8.083	3.60	0.45	1.000	| o I	|	|	|	|	2.16
8.167	3.87	0.47	1.023	| o I	|	|	|	|	2.20
8.250	3.94	0.50	1.046	| o I	|	|	|	|	2.25
8.333	3.97	0.53	1.070	| o I	|	|	|	|	2.29
8.417	3.98	0.56	1.093	| o I	|	|	|	|	2.33
8.500	3.99	0.59	1.117	| o I	|	|	|	|	2.38
8.583	4.07	0.62	1.141	| o I	|	|	|	|	2.42
8.667	4.20	0.65	1.165	| o I	|	|	|	|	2.47

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 8.750    4.23    0.68      1.189  | O      |      I |        |        |      2.51
 8.833    4.33    0.71      1.214  | O      |       I|        |        |      2.56
 8.917    4.46    0.74      1.239  | O      |       I|        |        |      2.61
 9.000    4.50    0.77      1.265  | O      |       I|        |        |      2.65
 9.083    4.67    0.80      1.291  | O      |        I        |        |      2.70
 9.167    4.93    0.83      1.318  | O      |        |I       |        |      2.75
 9.250    5.00    0.87      1.347  |  O     |        |I       |        |      2.81
 9.333    5.11    0.90      1.376  |  O     |        | I      |        |      2.86
 9.417    5.25    0.94      1.405  |  O     |        | I      |        |      2.91
 9.500    5.30    0.97      1.435  |  O     |        | I      |        |      2.97
 9.583    5.39    1.00      1.465  |  O     |        |  I     |        |      3.02
 9.667    5.53    1.02      1.495  |  O     |        |  I     |        |      3.07
 9.750    5.56    1.04      1.526  |  O     |        |  I     |        |      3.13
 9.833    5.66    1.07      1.558  |  O     |        |  I     |        |      3.18
 9.917    5.79    1.09      1.590  |  O     |        |   I    |        |      3.23
10.000    5.83    1.11      1.622  |  O     |        |   I    |        |      3.29
10.083    5.30    1.13      1.653  |   O    |        | I      |        |      3.34
10.167    4.41    1.15      1.678  |   O    |       I|        |        |      3.38
10.250    4.19    1.17      1.700  |   O    |      I |        |        |      3.42
10.333    4.09    1.18      1.720  |   O    |      I |        |        |      3.45
10.417    4.04    1.20      1.740  |   O    |      I |        |        |      3.48
10.500    3.99    1.21      1.760  |   O    |      I |        |        |      3.52
10.583    4.38    1.23      1.780  |   O    |       I|        |        |      3.55
10.667    5.02    1.24      1.804  |   O    |        |I       |        |      3.59
10.750    5.19    1.26      1.831  |   O    |        | I      |        |      3.63
10.833    5.26    1.28      1.858  |   O    |        | I      |        |      3.68
10.917    5.30    1.30      1.885  |   O    |        | I      |        |      3.73
11.000    5.33    1.32      1.913  |   O    |        | I      |        |      3.77
11.083    5.25    1.34      1.940  |   O    |        | I      |        |      3.82
11.167    5.12    1.36      1.966  |   O    |        | I      |        |      3.86
11.250    5.09    1.38      1.992  |   O    |        |I       |        |      3.90
11.333    5.07    1.39      2.018  |   O    |        |I       |        |      3.95
11.417    5.07    1.41      2.043  |   O    |        |I       |        |      3.99
11.500    5.06    1.43      2.068  |    O   |        |I       |        |      4.03
11.583    4.90    1.44      2.092  |    O   |        |I       |        |      4.07
11.667    4.65    1.45      2.115  |    O   |        I        |        |      4.10
11.750    4.58    1.46      2.137  |    O   |        I        |        |      4.13
11.833    4.63    1.47      2.159  |    O   |        I        |        |      4.17
11.917    4.74    1.48      2.181  |    O   |        I        |        |      4.20
12.000    4.77    1.49      2.203  |    O   |        I        |        |      4.23
12.083    5.33    1.50      2.228  |    O   |        | I      |        |      4.27
12.167    6.23    1.52      2.257  |    O   |        |     I  |        |      4.31
12.250    6.46    1.53      2.290  |    O   |        |     I  |        |      4.36
12.333    6.64    1.55      2.325  |    O   |        |      I|        |      4.42
12.417    6.82    1.56      2.361  |    O   |        |       I        |      4.47
12.500    6.90    1.58      2.397  |    O   |        |       I        |      4.52
12.583    7.07    1.60      2.434  |    O   |        |       I        |      4.58
12.667    7.33    1.62      2.473  |    O   |        |        |I      |      4.64
12.750    7.40    1.64      2.512  |    O   |        |        | I     |      4.70
12.833    7.51    1.66      2.552  |    O   |        |        | I     |      4.76
12.917    7.65    1.67      2.593  |    O   |        |        |  I    |      4.82
13.000    7.69    1.69      2.634  |    O   |        |        |  I    |      4.88
13.083    8.10    1.71      2.677  |     O  |        |        |   I   |      4.95
13.167    8.75    1.74      2.723  |     O  |        |        |     I |      5.02
13.250    8.91    1.75      2.772  |     O  |        |        |      I|      5.08
13.333    8.99    1.77      2.821  |     O  |        |        |      I|      5.16
13.417    9.03    1.79      2.871  |     O  |        |        |      I|      5.23
13.500    9.05    3.94      2.913  |        |    O   |        |       I      5.29
13.583    8.20    6.05      2.938  |        |        |    O   |   I    |     5.32
13.667    6.79    6.70      2.946  |        |        |     O  |        |     5.33
13.750    6.43    6.66      2.946  |        |        |     IO |        |     5.33
13.833    6.28    6.52      2.944  |        |        |     IO |        |     5.33
13.917    6.19    6.39      2.943  |        |        |    IO  |        |     5.33
14.000    6.12    6.29      2.941  |        |        |    IO  |        |     5.32
14.083    6.44    6.28      2.941  |        |        |     O  |        |     5.32
14.167    6.95    6.47      2.943  |        |        |     O I        |     5.33
14.250    7.08    6.71      2.946  |        |        |      O|I       |     5.33
14.333    7.06    6.87      2.948  |        |        |       O        |     5.33
14.417    6.96    6.93      2.949  |        |        |       O        |     5.33
14.500    6.95    6.94      2.949  |        |        |       O        |     5.33
14.583    6.94    6.94      2.949  |        |        |       O        |     5.33
14.667    6.93    6.94      2.949  |        |        |       O        |     5.33
14.750    6.92    6.93      2.949  |        |        |       O        |     5.33
14.833    6.85    6.91      2.949  |        |        |       O        |     5.33
14.917    6.72    6.85      2.948  |        |        |      IO        |     5.33
15.000    6.69    6.79      2.947  |        |        |      O|        |     5.33
15.083    6.59    6.72      2.946  |        |        |      O|        |     5.33
15.167    6.46    6.63      2.945  |        |        |     IO|        |     5.33
15.250    6.42    6.55      2.944  |        |        |     IO|        |     5.33
15.333    6.33    6.47      2.943  |        |        |     O |        |     5.33
15.417    6.19    6.37      2.942  |        |        |    IO |        |     5.32
15.500    6.15    6.28      2.941  |        |        |    IO |        |     5.32
15.583    5.83    6.15      2.940  |        |        |   IO  |        |     5.32
15.667    5.31    5.89      2.937  |        |        | I O   |        |     5.32
15.750    5.17    5.60      2.933  |        |        | IO    |        |     5.31
15.833    5.11    5.39      2.931  |        |        | IO    |        |     5.31
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15.917	5.08	5.26	2.929			IO			5.31
16.000	5.06	5.18	2.928			IO			5.31
16.083	3.89	4.86	2.924		I	O			5.30
16.167	1.97	3.99	2.914	I	O				5.29
16.250	1.49	2.98	2.902	I	O				5.27
16.333	1.27	2.26	2.893	I O					5.26
16.417	1.15	1.80	2.888	I O					5.25
16.500	1.07	1.80	2.883	I O					5.24
16.583	0.99	1.80	2.878	I O					5.24
16.667	0.86	1.79	2.872	I O					5.23
16.750	0.83	1.79	2.865	I O					5.22
16.833	0.81	1.79	2.858	I O					5.21
16.917	0.80	1.79	2.852	I O					5.20
17.000	0.80	1.78	2.845	I O					5.19
17.083	0.95	1.78	2.839	I O					5.18
17.167	1.21	1.78	2.834	I O					5.17
17.250	1.28	1.78	2.830	I O					5.17
17.333	1.30	1.78	2.827	I O					5.16
17.417	1.32	1.78	2.824	I O					5.16
17.500	1.33	1.77	2.821	I O					5.15
17.583	1.33	1.77	2.818	I O					5.15
17.667	1.33	1.77	2.814	I O					5.15
17.750	1.33	1.77	2.811	I O					5.14
17.833	1.25	1.77	2.808	I O					5.14
17.917	1.13	1.77	2.804	I O					5.13
18.000	1.09	1.77	2.800	I O					5.12
18.083	1.08	1.76	2.795	I O					5.12
18.167	1.07	1.76	2.790	I O					5.11
18.250	1.07	1.76	2.785	I O					5.10
18.333	1.07	1.76	2.781	I O					5.10
18.417	1.07	1.76	2.776	I O					5.09
18.500	1.07	1.75	2.771	I O					5.08
18.583	0.99	1.75	2.766	I O					5.08
18.667	0.86	1.75	2.760	I O					5.07
18.750	0.83	1.75	2.754	I O					5.06
18.833	0.73	1.75	2.748	I O					5.05
18.917	0.60	1.74	2.740	I O					5.04
19.000	0.56	1.74	2.732	I O					5.03
19.083	0.62	1.74	2.724	I O					5.02
19.167	0.74	1.73	2.717	I O					5.01
19.250	0.77	1.73	2.710	I O					5.00
19.333	0.86	1.73	2.704	I O					4.99
19.417	1.00	1.72	2.699	I O					4.98
19.500	1.04	1.72	2.694	I O					4.97
19.583	0.97	1.72	2.689	I O					4.97
19.667	0.85	1.72	2.683	I O					4.96
19.750	0.83	1.71	2.677	I O					4.95
19.833	0.73	1.71	2.671	I O					4.94
19.917	0.60	1.71	2.664	I O					4.93
20.000	0.56	1.70	2.656	I O					4.92
20.083	0.62	1.70	2.648	I O					4.90
20.167	0.74	1.70	2.641	I O					4.89
20.250	0.77	1.69	2.635	I O					4.88
20.333	0.79	1.69	2.628	I O					4.87
20.417	0.79	1.69	2.622	I O					4.86
20.500	0.80	1.69	2.616	I O					4.86
20.583	0.80	1.68	2.610	I O					4.85
20.667	0.80	1.68	2.604	I O					4.84
20.750	0.80	1.68	2.598	I O					4.83
20.833	0.72	1.67	2.592	I O					4.82
20.917	0.59	1.67	2.585	I O					4.81
21.000	0.56	1.67	2.577	I O					4.80
21.083	0.62	1.66	2.570	I O					4.79
21.167	0.74	1.66	2.563	I O					4.78
21.250	0.77	1.66	2.557	I O					4.77
21.333	0.71	1.65	2.550	I O					4.76
21.417	0.59	1.65	2.544	I O					4.75
21.500	0.56	1.65	2.536	I O					4.73
21.583	0.62	1.64	2.529	I O					4.72
21.667	0.74	1.64	2.522	I O					4.71
21.750	0.77	1.64	2.516	I O					4.70
21.833	0.71	1.64	2.510	I O					4.70
21.917	0.59	1.63	2.503	I O					4.69
22.000	0.56	1.63	2.496	I O					4.67
22.083	0.62	1.63	2.489	I O					4.66
22.167	0.74	1.62	2.482	I O					4.65
22.250	0.77	1.62	2.476	I O					4.64
22.333	0.71	1.62	2.470	I O					4.64
22.417	0.59	1.61	2.464	I O					4.63
22.500	0.56	1.61	2.457	I O					4.61
22.583	0.55	1.61	2.449	I O					4.60
22.667	0.54	1.60	2.442	I O					4.59
22.750	0.53	1.60	2.435	I O					4.58
22.833	0.53	1.60	2.427	I O					4.57
22.917	0.53	1.59	2.420	I O					4.56
23.000	0.53	1.59	2.413	I O					4.55

23.083	0.53	1.59	2.405	I O				4.54
23.167	0.53	1.58	2.398	I O				4.53
23.250	0.53	1.58	2.391	I O				4.52
23.333	0.53	1.58	2.384	I O				4.50
23.417	0.53	1.57	2.377	I O				4.49
23.500	0.53	1.57	2.369	I O				4.48
23.583	0.53	1.57	2.362	I O				4.47
23.667	0.53	1.56	2.355	I O				4.46
23.750	0.53	1.56	2.348	I O				4.45
23.833	0.53	1.56	2.341	I O				4.44
23.917	0.53	1.55	2.334	I O				4.43
24.000	0.53	1.55	2.327	I O				4.42
24.083	0.38	1.55	2.319	I O				4.41
24.167	0.12	1.54	2.311	I O				4.39
24.250	0.06	1.54	2.301	I O				4.38
24.333	0.03	1.53	2.290	I O				4.36
24.417	0.01	1.53	2.280	I O				4.35
24.500	0.00	1.52	2.269	I O				4.33
24.583	0.00	1.52	2.259	I O				4.32
24.667	0.00	1.51	2.249	I O				4.30
24.750	0.00	1.51	2.238	I O				4.29
24.833	0.00	1.50	2.228	I O				4.27
24.917	0.00	1.50	2.217	I O				4.25
25.000	0.00	1.49	2.207	I O				4.24
25.083	0.00	1.49	2.197	I O				4.22
25.167	0.00	1.48	2.187	I O				4.21
25.250	0.00	1.48	2.177	I O				4.19
25.333	0.00	1.47	2.166	I O				4.18
25.417	0.00	1.47	2.156	I O				4.16
25.500	0.00	1.46	2.146	I O				4.15
25.583	0.00	1.46	2.136	I O				4.13
25.667	0.00	1.45	2.126	I O				4.12
25.750	0.00	1.45	2.116	I O				4.10
25.833	0.00	1.44	2.106	I O				4.09
25.917	0.00	1.44	2.096	I O				4.07
26.000	0.00	1.43	2.086	I O				4.06
26.083	0.00	1.43	2.076	I O				4.04
26.167	0.00	1.43	2.067	I O				4.03
26.250	0.00	1.42	2.057	I O				4.01
26.333	0.00	1.42	2.047	I O				4.00
26.417	0.00	1.41	2.037	I O				3.98
26.500	0.00	1.40	2.028	I O				3.96
26.583	0.00	1.39	2.018	I O				3.95
26.667	0.00	1.39	2.008	I O				3.93
26.750	0.00	1.38	1.999	I O				3.92
26.833	0.00	1.37	1.989	I O				3.90
26.917	0.00	1.37	1.980	I O				3.88
27.000	0.00	1.36	1.971	I O				3.87
27.083	0.00	1.35	1.961	I O				3.85
27.167	0.00	1.35	1.952	I O				3.84
27.250	0.00	1.34	1.943	I O				3.82
27.333	0.00	1.33	1.933	I O				3.81
27.417	0.00	1.33	1.924	I O				3.79
27.500	0.00	1.32	1.915	I O				3.78
27.583	0.00	1.32	1.906	I O				3.76
27.667	0.00	1.31	1.897	I O				3.75
27.750	0.00	1.30	1.888	I O				3.73
27.833	0.00	1.30	1.879	I O				3.72
27.917	0.00	1.29	1.870	I O				3.70
28.000	0.00	1.28	1.861	I O				3.69
28.083	0.00	1.28	1.852	I O				3.67
28.167	0.00	1.27	1.844	I O				3.66
28.250	0.00	1.26	1.835	I O				3.64
28.333	0.00	1.26	1.826	I O				3.63
28.417	0.00	1.25	1.818	I O				3.61
28.500	0.00	1.25	1.809	I O				3.60
28.583	0.00	1.24	1.800	I O				3.58
28.667	0.00	1.23	1.792	I O				3.57
28.750	0.00	1.23	1.783	I O				3.56
28.833	0.00	1.22	1.775	I O				3.54
28.917	0.00	1.22	1.767	I O				3.53
29.000	0.00	1.21	1.758	I O				3.51
29.083	0.00	1.20	1.750	I O				3.50
29.167	0.00	1.20	1.742	I O				3.49
29.250	0.00	1.19	1.733	I O				3.47
29.333	0.00	1.19	1.725	I O				3.46
29.417	0.00	1.18	1.717	I O				3.45
29.500	0.00	1.17	1.709	I O				3.43
29.583	0.00	1.17	1.701	I O				3.42
29.667	0.00	1.16	1.693	I O				3.40
29.750	0.00	1.16	1.685	I O				3.39
29.833	0.00	1.15	1.677	I O				3.38
29.917	0.00	1.15	1.669	I O				3.36
30.000	0.00	1.14	1.661	I O				3.35
30.083	0.00	1.14	1.653	I O				3.34
30.167	0.00	1.13	1.646	I O				3.33

30.250	0.00	1.12	1.638	I o	|	|	|	3.31
30.333	0.00	1.12	1.630	I o	|	|	|	3.30
30.417	0.00	1.11	1.622	I o	|	|	|	3.29
30.500	0.00	1.11	1.615	I o	|	|	|	3.27
30.583	0.00	1.10	1.607	I o	|	|	|	3.26
30.667	0.00	1.10	1.600	I o	|	|	|	3.25
30.750	0.00	1.09	1.592	I o	|	|	|	3.24
30.833	0.00	1.09	1.585	I o	|	|	|	3.22
30.917	0.00	1.08	1.577	I o	|	|	|	3.21
31.000	0.00	1.08	1.570	I o	|	|	|	3.20
31.083	0.00	1.07	1.562	I o	|	|	|	3.19
31.167	0.00	1.07	1.555	I o	|	|	|	3.17
31.250	0.00	1.06	1.548	I o	|	|	|	3.16
31.333	0.00	1.05	1.540	I o	|	|	|	3.15
31.417	0.00	1.05	1.533	I o	|	|	|	3.14
31.500	0.00	1.04	1.526	I o	|	|	|	3.13
31.583	0.00	1.04	1.519	I o	|	|	|	3.11
31.667	0.00	1.03	1.512	I o	|	|	|	3.10
31.750	0.00	1.03	1.504	I o	|	|	|	3.09
31.833	0.00	1.02	1.497	I o	|	|	|	3.08
31.917	0.00	1.02	1.490	I o	|	|	|	3.07
32.000	0.00	1.01	1.483	I o	|	|	|	3.05
32.083	0.00	1.01	1.476	I o	|	|	|	3.04
32.167	0.00	1.00	1.469	I o	|	|	|	3.03
32.250	0.00	1.00	1.463	I o	|	|	|	3.02
32.333	0.00	0.99	1.456	I o	|	|	|	3.01
32.417	0.00	0.99	1.449	I o	|	|	|	3.00
32.500	0.00	0.98	1.442	I o	|	|	|	2.98
32.583	0.00	0.97	1.435	I o	|	|	|	2.97
32.667	0.00	0.96	1.429	I o	|	|	|	2.96
32.750	0.00	0.96	1.422	I o	|	|	|	2.95
32.833	0.00	0.95	1.415	I o	|	|	|	2.93
32.917	0.00	0.94	1.409	I o	|	|	|	2.92
33.000	0.00	0.93	1.403	I o	|	|	|	2.91
33.083	0.00	0.92	1.396	I o	|	|	|	2.90
33.167	0.00	0.92	1.390	I o	|	|	|	2.89
33.250	0.00	0.91	1.384	I o	|	|	|	2.87
33.333	0.00	0.90	1.377	I o	|	|	|	2.86
33.417	0.00	0.89	1.371	I o	|	|	|	2.85
33.500	0.00	0.89	1.365	I o	|	|	|	2.84
33.583	0.00	0.88	1.359	I o	|	|	|	2.83
33.667	0.00	0.87	1.353	I o	|	|	|	2.82
33.750	0.00	0.87	1.347	I o	|	|	|	2.81
33.833	0.00	0.86	1.341	I o	|	|	|	2.79
33.917	0.00	0.85	1.335	I o	|	|	|	2.78
34.000	0.00	0.84	1.329	I o	|	|	|	2.77
34.083	0.00	0.84	1.323	I o	|	|	|	2.76
34.167	0.00	0.83	1.318	I o	|	|	|	2.75
34.250	0.00	0.82	1.312	I o	|	|	|	2.74
34.333	0.00	0.82	1.306	I o	|	|	|	2.73
34.417	0.00	0.81	1.301	I o	|	|	|	2.72
34.500	0.00	0.80	1.295	I o	|	|	|	2.71
34.583	0.00	0.80	1.290	I o	|	|	|	2.70
34.667	0.00	0.79	1.284	I o	|	|	|	2.69
34.750	0.00	0.78	1.279	I o	|	|	|	2.68
34.833	0.00	0.78	1.273	I o	|	|	|	2.67
34.917	0.00	0.77	1.268	I o	|	|	|	2.66
35.000	0.00	0.76	1.263	I o	|	|	|	2.65
35.083	0.00	0.76	1.258	I o	|	|	|	2.64
35.167	0.00	0.75	1.252	I o	|	|	|	2.63
35.250	0.00	0.75	1.247	I o	|	|	|	2.62
35.333	0.00	0.74	1.242	I o	|	|	|	2.61
35.417	0.00	0.73	1.237	I o	|	|	|	2.60
35.500	0.00	0.73	1.232	I o	|	|	|	2.59
35.583	0.00	0.72	1.227	I o	|	|	|	2.58
35.667	0.00	0.72	1.222	I o	|	|	|	2.57
35.750	0.00	0.71	1.217	I o	|	|	|	2.56
35.833	0.00	0.70	1.212	I o	|	|	|	2.56
35.917	0.00	0.70	1.207	I o	|	|	|	2.55
36.000	0.00	0.69	1.203	I o	|	|	|	2.54
36.083	0.00	0.69	1.198	I o	|	|	|	2.53
36.167	0.00	0.68	1.193	I o	|	|	|	2.52
36.250	0.00	0.67	1.189	I o	|	|	|	2.51
36.333	0.00	0.67	1.184	I o	|	|	|	2.50
36.417	0.00	0.66	1.179	I o	|	|	|	2.49
36.500	0.00	0.66	1.175	I o	|	|	|	2.49
36.583	0.00	0.65	1.170	I o	|	|	|	2.48
36.667	0.00	0.65	1.166	I o	|	|	|	2.47
36.750	0.00	0.64	1.161	I o	|	|	|	2.46
36.833	0.00	0.64	1.157	I o	|	|	|	2.45
36.917	0.00	0.63	1.153	I o	|	|	|	2.44
37.000	0.00	0.63	1.148	I o	|	|	|	2.44
37.083	0.00	0.62	1.144	I o	|	|	|	2.43
37.167	0.00	0.62	1.140	I o	|	|	|	2.42
37.250	0.00	0.61	1.135	I o	|	|	|	2.41
37.333	0.00	0.61	1.131	I o	|	|	|	2.40

37.417	0.00	0.60	1.127	I O	|	|	|	2.40
37.500	0.00	0.60	1.123	I O	|	|	|	2.39
37.583	0.00	0.59	1.119	I O	|	|	|	2.38
37.667	0.00	0.59	1.115	I O	|	|	|	2.37
37.750	0.00	0.58	1.111	I O	|	|	|	2.37
37.833	0.00	0.58	1.107	I O	|	|	|	2.36
37.917	0.00	0.57	1.103	I O	|	|	|	2.35
38.000	0.00	0.57	1.099	I O	|	|	|	2.34
38.083	0.00	0.56	1.095	IO	|	|	|	2.34
38.167	0.00	0.56	1.091	IO	|	|	|	2.33
38.250	0.00	0.55	1.087	IO	|	|	|	2.32
38.333	0.00	0.55	1.084	IO	|	|	|	2.32
38.417	0.00	0.54	1.080	IO	|	|	|	2.31
38.500	0.00	0.54	1.076	IO	|	|	|	2.30
38.583	0.00	0.53	1.072	IO	|	|	|	2.30
38.667	0.00	0.53	1.069	IO	|	|	|	2.29
38.750	0.00	0.53	1.065	IO	|	|	|	2.28
38.833	0.00	0.52	1.062	IO	|	|	|	2.27
38.917	0.00	0.52	1.058	IO	|	|	|	2.27
39.000	0.00	0.51	1.054	IO	|	|	|	2.26
39.083	0.00	0.51	1.051	IO	|	|	|	2.25
39.167	0.00	0.50	1.047	IO	|	|	|	2.25
39.250	0.00	0.50	1.044	IO	|	|	|	2.24
39.333	0.00	0.50	1.040	IO	|	|	|	2.24
39.417	0.00	0.49	1.037	IO	|	|	|	2.23
39.500	0.00	0.49	1.034	IO	|	|	|	2.22
39.583	0.00	0.48	1.030	IO	|	|	|	2.22
39.667	0.00	0.48	1.027	IO	|	|	|	2.21
39.750	0.00	0.48	1.024	IO	|	|	|	2.20
39.833	0.00	0.47	1.020	IO	|	|	|	2.20
39.917	0.00	0.47	1.017	IO	|	|	|	2.19
40.000	0.00	0.46	1.014	IO	|	|	|	2.19
40.083	0.00	0.46	1.011	IO	|	|	|	2.18
40.167	0.00	0.46	1.008	IO	|	|	|	2.17
40.250	0.00	0.45	1.005	IO	|	|	|	2.17
40.333	0.00	0.45	1.001	IO	|	|	|	2.16
40.417	0.00	0.45	0.998	IO	|	|	|	2.16
40.500	0.00	0.44	0.995	IO	|	|	|	2.15
40.583	0.00	0.44	0.992	IO	|	|	|	2.15
40.667	0.00	0.43	0.989	IO	|	|	|	2.14
40.750	0.00	0.43	0.986	IO	|	|	|	2.13
40.833	0.00	0.43	0.983	IO	|	|	|	2.13
40.917	0.00	0.42	0.980	IO	|	|	|	2.12
41.000	0.00	0.42	0.977	IO	|	|	|	2.12
41.083	0.00	0.42	0.975	IO	|	|	|	2.11
41.167	0.00	0.41	0.972	IO	|	|	|	2.11
41.250	0.00	0.41	0.969	IO	|	|	|	2.10
41.333	0.00	0.41	0.966	IO	|	|	|	2.10
41.417	0.00	0.40	0.963	IO	|	|	|	2.09
41.500	0.00	0.40	0.961	IO	|	|	|	2.09
41.583	0.00	0.40	0.958	IO	|	|	|	2.08
41.667	0.00	0.39	0.955	IO	|	|	|	2.08
41.750	0.00	0.39	0.952	IO	|	|	|	2.07
41.833	0.00	0.39	0.950	IO	|	|	|	2.07
41.917	0.00	0.38	0.947	IO	|	|	|	2.06
42.000	0.00	0.38	0.944	IO	|	|	|	2.06
42.083	0.00	0.38	0.942	IO	|	|	|	2.05
42.167	0.00	0.37	0.939	IO	|	|	|	2.05
42.250	0.00	0.37	0.937	IO	|	|	|	2.04
42.333	0.00	0.37	0.934	IO	|	|	|	2.04
42.417	0.00	0.37	0.932	IO	|	|	|	2.03
42.500	0.00	0.36	0.929	IO	|	|	|	2.03
42.583	0.00	0.36	0.927	IO	|	|	|	2.02
42.667	0.00	0.36	0.924	IO	|	|	|	2.02
42.750	0.00	0.35	0.922	IO	|	|	|	2.01
42.833	0.00	0.35	0.919	IO	|	|	|	2.01
42.917	0.00	0.35	0.917	IO	|	|	|	2.01
43.000	0.00	0.34	0.914	IO	|	|	|	2.00
43.083	0.00	0.34	0.912	IO	|	|	|	2.00
43.167	0.00	0.34	0.910	IO	|	|	|	1.99
43.250	0.00	0.34	0.907	IO	|	|	|	1.99
43.333	0.00	0.34	0.905	IO	|	|	|	1.98
43.417	0.00	0.34	0.903	IO	|	|	|	1.98
43.500	0.00	0.34	0.900	IO	|	|	|	1.97
43.583	0.00	0.34	0.898	IO	|	|	|	1.97
43.667	0.00	0.34	0.896	IO	|	|	|	1.96
43.750	0.00	0.34	0.893	IO	|	|	|	1.96
43.833	0.00	0.34	0.891	IO	|	|	|	1.95
43.917	0.00	0.34	0.889	IO	|	|	|	1.95
44.000	0.00	0.34	0.886	IO	|	|	|	1.94
44.083	0.00	0.34	0.884	IO	|	|	|	1.94
44.167	0.00	0.34	0.882	IO	|	|	|	1.93
44.250	0.00	0.34	0.879	IO	|	|	|	1.93
44.333	0.00	0.33	0.877	IO	|	|	|	1.92
44.417	0.00	0.33	0.875	IO	|	|	|	1.92
44.500	0.00	0.33	0.872	IO	|	|	|	1.91

44.583	0.00	0.33	0.870	IO					1.91
44.667	0.00	0.33	0.868	IO					1.90
44.750	0.00	0.33	0.866	IO					1.90
44.833	0.00	0.33	0.863	IO					1.89
44.917	0.00	0.33	0.861	IO					1.89
45.000	0.00	0.33	0.859	IO					1.89
45.083	0.00	0.33	0.856	IO					1.88
45.167	0.00	0.33	0.854	IO					1.88
45.250	0.00	0.33	0.852	IO					1.87
45.333	0.00	0.33	0.850	IO					1.87
45.417	0.00	0.33	0.847	IO					1.86
45.500	0.00	0.33	0.845	IO					1.86
45.583	0.00	0.33	0.843	IO					1.85
45.667	0.00	0.33	0.841	IO					1.85
45.750	0.00	0.33	0.838	IO					1.84
45.833	0.00	0.32	0.836	IO					1.84
45.917	0.00	0.32	0.834	IO					1.83
46.000	0.00	0.32	0.832	IO					1.83
46.083	0.00	0.32	0.829	IO					1.82
46.167	0.00	0.32	0.827	IO					1.82
46.250	0.00	0.32	0.825	IO					1.82
46.333	0.00	0.32	0.823	IO					1.81
46.417	0.00	0.32	0.821	IO					1.81
46.500	0.00	0.32	0.818	IO					1.80
46.583	0.00	0.32	0.816	IO					1.80
46.667	0.00	0.32	0.814	IO					1.79
46.750	0.00	0.32	0.812	IO					1.79
46.833	0.00	0.32	0.810	IO					1.78
46.917	0.00	0.32	0.807	IO					1.78
47.000	0.00	0.32	0.805	IO					1.77
47.083	0.00	0.32	0.803	IO					1.77
47.167	0.00	0.32	0.801	IO					1.77
47.250	0.00	0.32	0.799	IO					1.76
47.333	0.00	0.32	0.797	IO					1.76
47.417	0.00	0.31	0.794	IO					1.75
47.500	0.00	0.31	0.792	IO					1.75
47.583	0.00	0.31	0.790	IO					1.74
47.667	0.00	0.31	0.788	IO					1.74
47.750	0.00	0.31	0.786	IO					1.73
47.833	0.00	0.31	0.784	IO					1.73
47.917	0.00	0.31	0.781	IO					1.73
48.000	0.00	0.31	0.779	IO					1.72
48.083	0.00	0.31	0.777	IO					1.72
48.167	0.00	0.31	0.775	IO					1.71
48.250	0.00	0.31	0.773	IO					1.71
48.333	0.00	0.31	0.771	IO					1.70
48.417	0.00	0.31	0.769	IO					1.70
48.500	0.00	0.31	0.766	IO					1.69
48.583	0.00	0.31	0.764	IO					1.69
48.667	0.00	0.31	0.762	IO					1.69
48.750	0.00	0.31	0.760	IO					1.68
48.833	0.00	0.31	0.758	IO					1.68
48.917	0.00	0.31	0.756	IO					1.67
49.000	0.00	0.30	0.754	IO					1.67
49.083	0.00	0.30	0.752	IO					1.66
49.167	0.00	0.30	0.750	IO					1.66
49.250	0.00	0.30	0.748	IO					1.66
49.333	0.00	0.30	0.745	IO					1.65
49.417	0.00	0.30	0.743	IO					1.65
49.500	0.00	0.30	0.741	IO					1.64
49.583	0.00	0.30	0.739	IO					1.64
49.667	0.00	0.30	0.737	IO					1.63
49.750	0.00	0.30	0.735	IO					1.63
49.833	0.00	0.30	0.733	IO					1.63
49.917	0.00	0.30	0.731	IO					1.62
50.000	0.00	0.30	0.729	IO					1.62
50.083	0.00	0.30	0.727	IO					1.61
50.167	0.00	0.30	0.725	IO					1.61
50.250	0.00	0.30	0.723	IO					1.60
50.333	0.00	0.30	0.721	IO					1.60
50.417	0.00	0.30	0.719	IO					1.60
50.500	0.00	0.30	0.717	IO					1.59
50.583	0.00	0.29	0.715	IO					1.59
50.667	0.00	0.29	0.713	IO					1.58
50.750	0.00	0.29	0.711	IO					1.58
50.833	0.00	0.29	0.709	IO					1.57
50.917	0.00	0.29	0.707	IO					1.57
51.000	0.00	0.29	0.705	IO					1.57
51.083	0.00	0.29	0.702	IO					1.56
51.167	0.00	0.29	0.700	IO					1.56
51.250	0.00	0.29	0.698	IO					1.55
51.333	0.00	0.29	0.696	IO					1.55
51.417	0.00	0.29	0.694	IO					1.55
51.500	0.00	0.29	0.692	IO					1.54
51.583	0.00	0.29	0.690	IO					1.54
51.667	0.00	0.29	0.689	IO					1.53

51.750	0.00	0.29	0.687	IO					1.53
51.833	0.00	0.29	0.685	IO					1.52
51.917	0.00	0.29	0.683	IO					1.52
52.000	0.00	0.29	0.681	IO					1.52
52.083	0.00	0.29	0.679	IO					1.51
52.167	0.00	0.29	0.677	IO					1.51
52.250	0.00	0.29	0.675	IO					1.50
52.333	0.00	0.28	0.673	IO					1.50
52.417	0.00	0.28	0.671	IO					1.50
52.500	0.00	0.28	0.669	IO					1.49
52.583	0.00	0.28	0.667	IO					1.49
52.667	0.00	0.28	0.665	O					1.48
52.750	0.00	0.28	0.663	O					1.48
52.833	0.00	0.28	0.661	O					1.48
52.917	0.00	0.28	0.659	O					1.47
53.000	0.00	0.28	0.657	O					1.47
53.083	0.00	0.28	0.655	O					1.46
53.167	0.00	0.28	0.653	O					1.46
53.250	0.00	0.28	0.651	O					1.46
53.333	0.00	0.28	0.649	O					1.45
53.417	0.00	0.28	0.648	O					1.45
53.500	0.00	0.28	0.646	O					1.44
53.583	0.00	0.28	0.644	O					1.44
53.667	0.00	0.28	0.642	O					1.44
53.750	0.00	0.28	0.640	O					1.43
53.833	0.00	0.28	0.638	O					1.43
53.917	0.00	0.28	0.636	O					1.42
54.000	0.00	0.28	0.634	O					1.42
54.083	0.00	0.27	0.632	O					1.42
54.167	0.00	0.27	0.630	O					1.41
54.250	0.00	0.27	0.629	O					1.41
54.333	0.00	0.27	0.627	O					1.41
54.417	0.00	0.27	0.625	O					1.40
54.500	0.00	0.27	0.623	O					1.40
54.583	0.00	0.27	0.621	O					1.39
54.667	0.00	0.27	0.619	O					1.39
54.750	0.00	0.27	0.617	O					1.39
54.833	0.00	0.27	0.615	O					1.38
54.917	0.00	0.27	0.614	O					1.38
55.000	0.00	0.27	0.612	O					1.37
55.083	0.00	0.27	0.610	O					1.37
55.167	0.00	0.27	0.608	O					1.37
55.250	0.00	0.27	0.606	O					1.36
55.333	0.00	0.27	0.604	O					1.36
55.417	0.00	0.27	0.602	O					1.35
55.500	0.00	0.27	0.601	O					1.35
55.583	0.00	0.27	0.599	O					1.35
55.667	0.00	0.27	0.597	O					1.34
55.750	0.00	0.27	0.595	O					1.34
55.833	0.00	0.26	0.593	O					1.34
55.917	0.00	0.26	0.591	O					1.33
56.000	0.00	0.26	0.590	O					1.33
56.083	0.00	0.26	0.588	O					1.32
56.167	0.00	0.26	0.586	O					1.32
56.250	0.00	0.26	0.584	O					1.32
56.333	0.00	0.26	0.582	O					1.31
56.417	0.00	0.26	0.581	O					1.31
56.500	0.00	0.26	0.579	O					1.31
56.583	0.00	0.26	0.577	O					1.30
56.667	0.00	0.26	0.575	O					1.30
56.750	0.00	0.26	0.573	O					1.29
56.833	0.00	0.26	0.572	O					1.29
56.917	0.00	0.26	0.570	O					1.29
57.000	0.00	0.26	0.568	O					1.28
57.083	0.00	0.26	0.566	O					1.28
57.167	0.00	0.26	0.564	O					1.28
57.250	0.00	0.26	0.563	O					1.27
57.333	0.00	0.26	0.561	O					1.27
57.417	0.00	0.26	0.559	O					1.27
57.500	0.00	0.26	0.557	O					1.26
57.583	0.00	0.26	0.556	O					1.26
57.667	0.00	0.26	0.554	O					1.25
57.750	0.00	0.25	0.552	O					1.25
57.833	0.00	0.25	0.550	O					1.25
57.917	0.00	0.25	0.549	O					1.24
58.000	0.00	0.25	0.547	O					1.24
58.083	0.00	0.25	0.545	O					1.24
58.167	0.00	0.25	0.543	O					1.23
58.250	0.00	0.25	0.542	O					1.23
58.333	0.00	0.25	0.540	O					1.23
58.417	0.00	0.25	0.538	O					1.22
58.500	0.00	0.25	0.536	O					1.22
58.583	0.00	0.25	0.535	O					1.21
58.667	0.00	0.25	0.533	O					1.21
58.750	0.00	0.25	0.531	O					1.21
58.833	0.00	0.25	0.530	O					1.20

58.917	0.00	0.25	0.528	o	|	|	|	|	1.20
59.000	0.00	0.25	0.526	o	|	|	|	|	1.20
59.083	0.00	0.25	0.524	o	|	|	|	|	1.19
59.167	0.00	0.25	0.523	o	|	|	|	|	1.19
59.250	0.00	0.25	0.521	o	|	|	|	|	1.19
59.333	0.00	0.25	0.519	o	|	|	|	|	1.18
59.417	0.00	0.25	0.518	o	|	|	|	|	1.18
59.500	0.00	0.25	0.516	o	|	|	|	|	1.18
59.583	0.00	0.25	0.514	o	|	|	|	|	1.17
59.667	0.00	0.25	0.513	o	|	|	|	|	1.17
59.750	0.00	0.24	0.511	o	|	|	|	|	1.17
59.833	0.00	0.24	0.509	o	|	|	|	|	1.16
59.917	0.00	0.24	0.507	o	|	|	|	|	1.16
60.000	0.00	0.24	0.506	o	|	|	|	|	1.15
60.083	0.00	0.24	0.504	o	|	|	|	|	1.15
60.167	0.00	0.24	0.502	o	|	|	|	|	1.15
60.250	0.00	0.24	0.501	o	|	|	|	|	1.14
60.333	0.00	0.24	0.499	o	|	|	|	|	1.14
60.417	0.00	0.24	0.497	o	|	|	|	|	1.14
60.500	0.00	0.24	0.496	o	|	|	|	|	1.13
60.583	0.00	0.24	0.494	o	|	|	|	|	1.13
60.667	0.00	0.24	0.492	o	|	|	|	|	1.13
60.750	0.00	0.24	0.491	o	|	|	|	|	1.12
60.833	0.00	0.24	0.489	o	|	|	|	|	1.12
60.917	0.00	0.24	0.488	o	|	|	|	|	1.12
61.000	0.00	0.24	0.486	o	|	|	|	|	1.11
61.083	0.00	0.24	0.484	o	|	|	|	|	1.11
61.167	0.00	0.24	0.483	o	|	|	|	|	1.11
61.250	0.00	0.24	0.481	o	|	|	|	|	1.10
61.333	0.00	0.24	0.479	o	|	|	|	|	1.10
61.417	0.00	0.24	0.478	o	|	|	|	|	1.10
61.500	0.00	0.24	0.476	o	|	|	|	|	1.09
61.583	0.00	0.24	0.474	o	|	|	|	|	1.09
61.667	0.00	0.24	0.473	o	|	|	|	|	1.09
61.750	0.00	0.23	0.471	o	|	|	|	|	1.08
61.833	0.00	0.23	0.470	o	|	|	|	|	1.08
61.917	0.00	0.23	0.468	o	|	|	|	|	1.08
62.000	0.00	0.23	0.466	o	|	|	|	|	1.07
62.083	0.00	0.23	0.465	o	|	|	|	|	1.07
62.167	0.00	0.23	0.463	o	|	|	|	|	1.07
62.250	0.00	0.23	0.462	o	|	|	|	|	1.06
62.333	0.00	0.23	0.460	o	|	|	|	|	1.06
62.417	0.00	0.23	0.458	o	|	|	|	|	1.06
62.500	0.00	0.23	0.457	o	|	|	|	|	1.05
62.583	0.00	0.23	0.455	o	|	|	|	|	1.05
62.667	0.00	0.23	0.454	o	|	|	|	|	1.05
62.750	0.00	0.23	0.452	o	|	|	|	|	1.04
62.833	0.00	0.23	0.450	o	|	|	|	|	1.04
62.917	0.00	0.23	0.449	o	|	|	|	|	1.04
63.000	0.00	0.23	0.447	o	|	|	|	|	1.03
63.083	0.00	0.23	0.446	o	|	|	|	|	1.03
63.167	0.00	0.23	0.444	o	|	|	|	|	1.03
63.250	0.00	0.23	0.443	o	|	|	|	|	1.02
63.333	0.00	0.23	0.441	o	|	|	|	|	1.02
63.417	0.00	0.23	0.439	o	|	|	|	|	1.02
63.500	0.00	0.23	0.438	o	|	|	|	|	1.01
63.583	0.00	0.23	0.436	o	|	|	|	|	1.01
63.667	0.00	0.23	0.435	o	|	|	|	|	1.01
63.750	0.00	0.23	0.433	o	|	|	|	|	1.00
63.833	0.00	0.23	0.432	o	|	|	|	|	1.00
63.917	0.00	0.22	0.430	o	|	|	|	|	1.00
64.000	0.00	0.22	0.429	o	|	|	|	|	0.99
64.083	0.00	0.22	0.427	o	|	|	|	|	0.99
64.167	0.00	0.22	0.425	o	|	|	|	|	0.99
64.250	0.00	0.22	0.424	o	|	|	|	|	0.98
64.333	0.00	0.22	0.422	o	|	|	|	|	0.98
64.417	0.00	0.22	0.421	o	|	|	|	|	0.98
64.500	0.00	0.22	0.419	o	|	|	|	|	0.97
64.583	0.00	0.22	0.418	o	|	|	|	|	0.97
64.667	0.00	0.22	0.416	o	|	|	|	|	0.97
64.750	0.00	0.22	0.415	o	|	|	|	|	0.96
64.833	0.00	0.22	0.413	o	|	|	|	|	0.96
64.917	0.00	0.22	0.412	o	|	|	|	|	0.96
65.000	0.00	0.21	0.410	o	|	|	|	|	0.95
65.083	0.00	0.21	0.409	o	|	|	|	|	0.95
65.167	0.00	0.21	0.407	o	|	|	|	|	0.95
65.250	0.00	0.21	0.406	o	|	|	|	|	0.94
65.333	0.00	0.21	0.405	o	|	|	|	|	0.94
65.417	0.00	0.21	0.403	o	|	|	|	|	0.94
65.500	0.00	0.21	0.402	o	|	|	|	|	0.93
65.583	0.00	0.21	0.400	o	|	|	|	|	0.93
65.667	0.00	0.21	0.399	o	|	|	|	|	0.93
65.750	0.00	0.21	0.397	o	|	|	|	|	0.92
65.833	0.00	0.21	0.396	o	|	|	|	|	0.92
65.917	0.00	0.21	0.395	o	|	|	|	|	0.92
66.000	0.00	0.21	0.393	o	|	|	|	|	0.91

66.083	0.00	0.20	0.392	o	|	|	|	0.91
66.167	0.00	0.20	0.390	o	|	|	|	0.91
66.250	0.00	0.20	0.389	o	|	|	|	0.90
66.333	0.00	0.20	0.387	o	|	|	|	0.90
66.417	0.00	0.20	0.386	o	|	|	|	0.90
66.500	0.00	0.20	0.385	o	|	|	|	0.89
66.583	0.00	0.20	0.383	o	|	|	|	0.89
66.667	0.00	0.20	0.382	o	|	|	|	0.89
66.750	0.00	0.20	0.381	o	|	|	|	0.88
66.833	0.00	0.20	0.379	o	|	|	|	0.88
66.917	0.00	0.20	0.378	o	|	|	|	0.88
67.000	0.00	0.20	0.376	o	|	|	|	0.87
67.083	0.00	0.20	0.375	o	|	|	|	0.87
67.167	0.00	0.20	0.374	o	|	|	|	0.87
67.250	0.00	0.19	0.372	o	|	|	|	0.86
67.333	0.00	0.19	0.371	o	|	|	|	0.86
67.417	0.00	0.19	0.370	o	|	|	|	0.86
67.500	0.00	0.19	0.368	o	|	|	|	0.85
67.583	0.00	0.19	0.367	o	|	|	|	0.85
67.667	0.00	0.19	0.366	o	|	|	|	0.85
67.750	0.00	0.19	0.365	o	|	|	|	0.85
67.833	0.00	0.19	0.363	o	|	|	|	0.84
67.917	0.00	0.19	0.362	o	|	|	|	0.84
68.000	0.00	0.19	0.361	o	|	|	|	0.84
68.083	0.00	0.19	0.359	o	|	|	|	0.83
68.167	0.00	0.19	0.358	o	|	|	|	0.83
68.250	0.00	0.19	0.357	o	|	|	|	0.83
68.333	0.00	0.19	0.355	o	|	|	|	0.82
68.417	0.00	0.18	0.354	o	|	|	|	0.82
68.500	0.00	0.18	0.353	o	|	|	|	0.82
68.583	0.00	0.18	0.352	o	|	|	|	0.82
68.667	0.00	0.18	0.350	o	|	|	|	0.81
68.750	0.00	0.18	0.349	o	|	|	|	0.81
68.833	0.00	0.18	0.348	o	|	|	|	0.81
68.917	0.00	0.18	0.347	o	|	|	|	0.80
69.000	0.00	0.18	0.345	o	|	|	|	0.80
69.083	0.00	0.18	0.344	o	|	|	|	0.80
69.167	0.00	0.18	0.343	o	|	|	|	0.80
69.250	0.00	0.18	0.342	o	|	|	|	0.79
69.333	0.00	0.18	0.340	o	|	|	|	0.79
69.417	0.00	0.18	0.339	o	|	|	|	0.79
69.500	0.00	0.18	0.338	o	|	|	|	0.78
69.583	0.00	0.18	0.337	o	|	|	|	0.78
69.667	0.00	0.18	0.336	o	|	|	|	0.78
69.750	0.00	0.17	0.334	o	|	|	|	0.78
69.833	0.00	0.17	0.333	o	|	|	|	0.77
69.917	0.00	0.17	0.332	o	|	|	|	0.77
70.000	0.00	0.17	0.331	o	|	|	|	0.77
70.083	0.00	0.17	0.330	o	|	|	|	0.76
70.167	0.00	0.17	0.328	o	|	|	|	0.76
70.250	0.00	0.17	0.327	o	|	|	|	0.76
70.333	0.00	0.17	0.326	o	|	|	|	0.76
70.417	0.00	0.17	0.325	o	|	|	|	0.75
70.500	0.00	0.17	0.324	o	|	|	|	0.75
70.583	0.00	0.17	0.323	o	|	|	|	0.75
70.667	0.00	0.17	0.321	o	|	|	|	0.75
70.750	0.00	0.17	0.320	o	|	|	|	0.74
70.833	0.00	0.17	0.319	o	|	|	|	0.74
70.917	0.00	0.17	0.318	o	|	|	|	0.74
71.000	0.00	0.17	0.317	o	|	|	|	0.74
71.083	0.00	0.16	0.316	o	|	|	|	0.73
71.167	0.00	0.16	0.315	o	|	|	|	0.73
71.250	0.00	0.16	0.313	o	|	|	|	0.73
71.333	0.00	0.16	0.312	o	|	|	|	0.72
71.417	0.00	0.16	0.311	o	|	|	|	0.72
71.500	0.00	0.16	0.310	o	|	|	|	0.72
71.583	0.00	0.16	0.309	o	|	|	|	0.72
71.667	0.00	0.16	0.308	o	|	|	|	0.71
71.750	0.00	0.16	0.307	o	|	|	|	0.71
71.833	0.00	0.16	0.306	o	|	|	|	0.71
71.917	0.00	0.16	0.305	o	|	|	|	0.71
72.000	0.00	0.16	0.303	o	|	|	|	0.70
72.083	0.00	0.16	0.302	o	|	|	|	0.70
72.167	0.00	0.16	0.301	o	|	|	|	0.70
72.250	0.00	0.16	0.300	o	|	|	|	0.70
72.333	0.00	0.16	0.299	o	|	|	|	0.69
72.417	0.00	0.16	0.298	o	|	|	|	0.69
72.500	0.00	0.16	0.297	o	|	|	|	0.69
72.583	0.00	0.15	0.296	o	|	|	|	0.69
72.667	0.00	0.15	0.295	o	|	|	|	0.68
72.750	0.00	0.15	0.294	o	|	|	|	0.68
72.833	0.00	0.15	0.293	o	|	|	|	0.68
72.917	0.00	0.15	0.292	o	|	|	|	0.68
73.000	0.00	0.15	0.291	o	|	|	|	0.67
73.083	0.00	0.15	0.290	o	|	|	|	0.67
73.167	0.00	0.15	0.289	o	|	|	|	0.67

73.250	0.00	0.15	0.288	o	|	|	|	0.67
73.333	0.00	0.15	0.286	o	|	|	|	0.66
73.417	0.00	0.15	0.285	o	|	|	|	0.66
73.500	0.00	0.15	0.284	o	|	|	|	0.66
73.583	0.00	0.15	0.283	o	|	|	|	0.66
73.667	0.00	0.15	0.282	o	|	|	|	0.66
73.750	0.00	0.15	0.281	o	|	|	|	0.65
73.833	0.00	0.15	0.280	o	|	|	|	0.65
73.917	0.00	0.15	0.279	o	|	|	|	0.65
74.000	0.00	0.15	0.278	o	|	|	|	0.65
74.083	0.00	0.14	0.277	o	|	|	|	0.64
74.167	0.00	0.14	0.276	o	|	|	|	0.64
74.250	0.00	0.14	0.275	o	|	|	|	0.64
74.333	0.00	0.14	0.274	o	|	|	|	0.64
74.417	0.00	0.14	0.273	o	|	|	|	0.63
74.500	0.00	0.14	0.272	o	|	|	|	0.63
74.583	0.00	0.14	0.271	o	|	|	|	0.63
74.667	0.00	0.14	0.270	o	|	|	|	0.63
74.750	0.00	0.14	0.269	o	|	|	|	0.63
74.833	0.00	0.14	0.269	o	|	|	|	0.62
74.917	0.00	0.14	0.268	o	|	|	|	0.62
75.000	0.00	0.14	0.267	o	|	|	|	0.62
75.083	0.00	0.14	0.266	o	|	|	|	0.62
75.167	0.00	0.14	0.265	o	|	|	|	0.61
75.250	0.00	0.14	0.264	o	|	|	|	0.61
75.333	0.00	0.14	0.263	o	|	|	|	0.61
75.417	0.00	0.14	0.262	o	|	|	|	0.61
75.500	0.00	0.14	0.261	o	|	|	|	0.61
75.583	0.00	0.14	0.260	o	|	|	|	0.60
75.667	0.00	0.14	0.259	o	|	|	|	0.60
75.750	0.00	0.13	0.258	o	|	|	|	0.60
75.833	0.00	0.13	0.257	o	|	|	|	0.60
75.917	0.00	0.13	0.256	o	|	|	|	0.59
76.000	0.00	0.13	0.255	o	|	|	|	0.59
76.083	0.00	0.13	0.254	o	|	|	|	0.59
76.167	0.00	0.13	0.254	o	|	|	|	0.59
76.250	0.00	0.13	0.253	o	|	|	|	0.59
76.333	0.00	0.13	0.252	o	|	|	|	0.58
76.417	0.00	0.13	0.251	o	|	|	|	0.58
76.500	0.00	0.13	0.250	o	|	|	|	0.58
76.583	0.00	0.13	0.249	o	|	|	|	0.58
76.667	0.00	0.13	0.248	o	|	|	|	0.58
76.750	0.00	0.13	0.247	o	|	|	|	0.57
76.833	0.00	0.13	0.246	o	|	|	|	0.57
76.917	0.00	0.13	0.245	o	|	|	|	0.57
77.000	0.00	0.13	0.245	o	|	|	|	0.57
77.083	0.00	0.13	0.244	o	|	|	|	0.57
77.167	0.00	0.13	0.243	o	|	|	|	0.56
77.250	0.00	0.13	0.242	o	|	|	|	0.56
77.333	0.00	0.13	0.241	o	|	|	|	0.56
77.417	0.00	0.13	0.240	o	|	|	|	0.56
77.500	0.00	0.12	0.239	o	|	|	|	0.56
77.583	0.00	0.12	0.238	o	|	|	|	0.55
77.667	0.00	0.12	0.238	o	|	|	|	0.55
77.750	0.00	0.12	0.237	o	|	|	|	0.55
77.833	0.00	0.12	0.236	o	|	|	|	0.55
77.917	0.00	0.12	0.235	o	|	|	|	0.55
78.000	0.00	0.12	0.234	o	|	|	|	0.54
78.083	0.00	0.12	0.233	o	|	|	|	0.54
78.167	0.00	0.12	0.233	o	|	|	|	0.54
78.250	0.00	0.12	0.232	o	|	|	|	0.54
78.333	0.00	0.12	0.231	o	|	|	|	0.54
78.417	0.00	0.12	0.230	o	|	|	|	0.53
78.500	0.00	0.12	0.229	o	|	|	|	0.53
78.583	0.00	0.12	0.228	o	|	|	|	0.53
78.667	0.00	0.12	0.228	o	|	|	|	0.53
78.750	0.00	0.12	0.227	o	|	|	|	0.53
78.833	0.00	0.12	0.226	o	|	|	|	0.52
78.917	0.00	0.12	0.225	o	|	|	|	0.52
79.000	0.00	0.12	0.224	o	|	|	|	0.52
79.083	0.00	0.12	0.224	o	|	|	|	0.52
79.167	0.00	0.12	0.223	o	|	|	|	0.52
79.250	0.00	0.12	0.222	o	|	|	|	0.51
79.333	0.00	0.12	0.221	o	|	|	|	0.51
79.417	0.00	0.12	0.220	o	|	|	|	0.51
79.500	0.00	0.11	0.220	o	|	|	|	0.51
79.583	0.00	0.11	0.219	o	|	|	|	0.51
79.667	0.00	0.11	0.218	o	|	|	|	0.51
79.750	0.00	0.11	0.217	o	|	|	|	0.50
79.833	0.00	0.11	0.216	o	|	|	|	0.50
79.917	0.00	0.11	0.216	o	|	|	|	0.50
80.000	0.00	0.11	0.215	o	|	|	|	0.50
80.083	0.00	0.11	0.214	o	|	|	|	0.50
80.167	0.00	0.11	0.213	o	|	|	|	0.49
80.250	0.00	0.11	0.213	o	|	|	|	0.49
80.333	0.00	0.11	0.212	o	|	|	|	0.49

80.417	0.00	0.11	0.211	o	|	|	|	0.49
80.500	0.00	0.11	0.210	o	|	|	|	0.49
80.583	0.00	0.11	0.210	o	|	|	|	0.49
80.667	0.00	0.11	0.209	o	|	|	|	0.48
80.750	0.00	0.11	0.208	o	|	|	|	0.48
80.833	0.00	0.11	0.207	o	|	|	|	0.48
80.917	0.00	0.11	0.207	o	|	|	|	0.48
81.000	0.00	0.11	0.206	o	|	|	|	0.48
81.083	0.00	0.11	0.205	o	|	|	|	0.48
81.167	0.00	0.11	0.204	o	|	|	|	0.47
81.250	0.00	0.11	0.204	o	|	|	|	0.47
81.333	0.00	0.11	0.203	o	|	|	|	0.47
81.417	0.00	0.11	0.202	o	|	|	|	0.47
81.500	0.00	0.11	0.201	o	|	|	|	0.47
81.583	0.00	0.10	0.201	o	|	|	|	0.47
81.667	0.00	0.10	0.200	o	|	|	|	0.46
81.750	0.00	0.10	0.199	o	|	|	|	0.46
81.833	0.00	0.10	0.199	o	|	|	|	0.46
81.917	0.00	0.10	0.198	o	|	|	|	0.46
82.000	0.00	0.10	0.197	o	|	|	|	0.46
82.083	0.00	0.10	0.196	o	|	|	|	0.46
82.167	0.00	0.10	0.196	o	|	|	|	0.45
82.250	0.00	0.10	0.195	o	|	|	|	0.45
82.333	0.00	0.10	0.194	o	|	|	|	0.45
82.417	0.00	0.10	0.194	o	|	|	|	0.45
82.500	0.00	0.10	0.193	o	|	|	|	0.45
82.583	0.00	0.10	0.192	o	|	|	|	0.45
82.667	0.00	0.10	0.192	o	|	|	|	0.44

Remaining water in basin = 0.19 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 992
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 6.944 (CFS)
Total volume = 5.311 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 06/03/24

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: pro210110.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    17
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       91.590 (CFS)
               Total volume =       2.713 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
*************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
_________________________________________________________________________

User entry of depth-outflow-storage data
-------------------------------------------------------------------
Total number of inflow hydrograph intervals = 17
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
-------------------------------------------------------------------
-------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
-------------------------------------------------------------------
-------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
-------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.431      0.225      0.430        0.432
   2.000      0.914      0.344      0.913        0.915
   3.000      1.451      0.991      1.448        1.454
   4.000      2.049      1.417      2.044        2.054
   5.000      2.712      1.731      2.706        2.718
   5.250      2.888      1.801      2.882        2.894
   5.500      3.069     17.046      3.010        3.128
   6.000      3.443    225.078      2.668        4.218
-------------------------------------------------------------------
               Hydrograph Detention Basin Routing
-------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
-------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                  Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0      22.9   45.80   68.69   91.59 (Ft.)
 0.083    2.51    0.00      0.009  O       |       |       |       |     0.02
 0.167    7.37    0.02      0.043  O I     |       |       |       |     0.10
 0.250    9.93    0.05      0.102  O  I    |       |       |       |     0.24
 0.333   11.81    0.09      0.176  O   I   |       |       |       |     0.41
 0.417   13.93    0.14      0.264  O   I   |       |       |       |     0.61
 0.500   17.02    0.19      0.370  O    I  |       |       |       |     0.86
 0.583   20.88    0.24      0.499  O      I|       |       |       |     1.14
 0.667   26.24    0.28      0.659  O       I       |       |       |     1.47
 0.750   39.75    0.34      0.884  O       |    I  |       |       |     1.94
 0.833   80.70    0.80      1.295  O       |       |       |   I   |     2.71
 0.917   91.59    1.30      1.881  O       |       |       |      I|     3.72
 1.000   39.15    1.55      2.321  O       |    I  |       |       |     4.41
 1.083   18.80    1.64      2.510  O     I |       |       |       |     4.70
 1.167    8.47    1.67      2.593  O I     |       |       |       |     4.82
 1.250    4.65    1.69      2.626  OI      |       |       |       |     4.87
 1.333    0.87    1.69      2.634  O       |       |       |       |     4.88
 1.417    0.22    1.69      2.626  O       |       |       |       |     4.87
 1.500    0.00    1.68      2.615  O       |       |       |       |     4.85
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1.583	0.00	1.68	2.603	o	|	|	|	4.84
1.667	0.00	1.67	2.592	o	|	|	|	4.82
1.750	0.00	1.67	2.580	o	|	|	|	4.80
1.833	0.00	1.66	2.569	o	|	|	|	4.78
1.917	0.00	1.66	2.557	o	|	|	|	4.77
2.000	0.00	1.65	2.546	o	|	|	|	4.75
2.083	0.00	1.65	2.534	o	|	|	|	4.73
2.167	0.00	1.64	2.523	o	|	|	|	4.72
2.250	0.00	1.64	2.512	o	|	|	|	4.70
2.333	0.00	1.63	2.501	o	|	|	|	4.68
2.417	0.00	1.63	2.489	o	|	|	|	4.66
2.500	0.00	1.62	2.478	o	|	|	|	4.65
2.583	0.00	1.62	2.467	o	|	|	|	4.63
2.667	0.00	1.61	2.456	o	|	|	|	4.61
2.750	0.00	1.60	2.445	o	|	|	|	4.60
2.833	0.00	1.60	2.434	o	|	|	|	4.58
2.917	0.00	1.59	2.423	o	|	|	|	4.56
3.000	0.00	1.59	2.412	o	|	|	|	4.55
3.083	0.00	1.58	2.401	o	|	|	|	4.53
3.167	0.00	1.58	2.390	o	|	|	|	4.51
3.250	0.00	1.57	2.379	o	|	|	|	4.50
3.333	0.00	1.57	2.368	o	|	|	|	4.48
3.417	0.00	1.56	2.358	o	|	|	|	4.47
3.500	0.00	1.56	2.347	o	|	|	|	4.45
3.583	0.00	1.55	2.336	o	|	|	|	4.43
3.667	0.00	1.55	2.325	o	|	|	|	4.42
3.750	0.00	1.54	2.315	o	|	|	|	4.40
3.833	0.00	1.54	2.304	o	|	|	|	4.38
3.917	0.00	1.53	2.294	o	|	|	|	4.37
4.000	0.00	1.53	2.283	o	|	|	|	4.35
4.083	0.00	1.52	2.273	o	|	|	|	4.34
4.167	0.00	1.52	2.262	o	|	|	|	4.32
4.250	0.00	1.51	2.252	o	|	|	|	4.31
4.333	0.00	1.51	2.241	o	|	|	|	4.29
4.417	0.00	1.50	2.231	o	|	|	|	4.27
4.500	0.00	1.50	2.221	o	|	|	|	4.26
4.583	0.00	1.49	2.210	o	|	|	|	4.24
4.667	0.00	1.49	2.200	o	|	|	|	4.23
4.750	0.00	1.48	2.190	o	|	|	|	4.21
4.833	0.00	1.48	2.180	o	|	|	|	4.20
4.917	0.00	1.47	2.169	o	|	|	|	4.18
5.000	0.00	1.47	2.159	o	|	|	|	4.17
5.083	0.00	1.46	2.149	o	|	|	|	4.15
5.167	0.00	1.46	2.139	o	|	|	|	4.14
5.250	0.00	1.45	2.129	o	|	|	|	4.12
5.333	0.00	1.45	2.119	o	|	|	|	4.11
5.417	0.00	1.45	2.109	o	|	|	|	4.09
5.500	0.00	1.44	2.099	o	|	|	|	4.08
5.583	0.00	1.44	2.089	o	|	|	|	4.06
5.667	0.00	1.43	2.079	o	|	|	|	4.05
5.750	0.00	1.43	2.070	o	|	|	|	4.03
5.833	0.00	1.42	2.060	o	|	|	|	4.02
5.917	0.00	1.42	2.050	o	|	|	|	4.00
6.000	0.00	1.41	2.040	o	|	|	|	3.99
6.083	0.00	1.40	2.031	o	|	|	|	3.97
6.167	0.00	1.40	2.021	o	|	|	|	3.95
6.250	0.00	1.39	2.011	o	|	|	|	3.94
6.333	0.00	1.38	2.002	o	|	|	|	3.92
6.417	0.00	1.38	1.992	o	|	|	|	3.91
6.500	0.00	1.37	1.983	o	|	|	|	3.89
6.583	0.00	1.36	1.973	o	|	|	|	3.87
6.667	0.00	1.36	1.964	o	|	|	|	3.86
6.750	0.00	1.35	1.955	o	|	|	|	3.84
6.833	0.00	1.34	1.945	o	|	|	|	3.83
6.917	0.00	1.34	1.936	o	|	|	|	3.81
7.000	0.00	1.33	1.927	o	|	|	|	3.80
7.083	0.00	1.32	1.918	o	|	|	|	3.78
7.167	0.00	1.32	1.909	o	|	|	|	3.77
7.250	0.00	1.31	1.900	o	|	|	|	3.75
7.333	0.00	1.30	1.891	o	|	|	|	3.74
7.417	0.00	1.30	1.882	o	|	|	|	3.72
7.500	0.00	1.29	1.873	o	|	|	|	3.71
7.583	0.00	1.29	1.864	o	|	|	|	3.69
7.667	0.00	1.28	1.855	o	|	|	|	3.68
7.750	0.00	1.27	1.846	o	|	|	|	3.66
7.833	0.00	1.27	1.838	o	|	|	|	3.65
7.917	0.00	1.26	1.829	o	|	|	|	3.63
8.000	0.00	1.25	1.820	o	|	|	|	3.62
8.083	0.00	1.25	1.812	o	|	|	|	3.60
8.167	0.00	1.24	1.803	o	|	|	|	3.59
8.250	0.00	1.24	1.795	o	|	|	|	3.57
8.333	0.00	1.23	1.786	o	|	|	|	3.56
8.417	0.00	1.22	1.778	o	|	|	|	3.55
8.500	0.00	1.22	1.769	o	|	|	|	3.53
8.583	0.00	1.21	1.761	o	|	|	|	3.52
8.667	0.00	1.21	1.752	o	|	|	|	3.50

8.750	0.00	1.20	1.744	o	|	|	|	|	3.49
8.833	0.00	1.19	1.736	o	|	|	|	|	3.48
8.917	0.00	1.19	1.728	o	|	|	|	|	3.46
9.000	0.00	1.18	1.720	o	|	|	|	|	3.45
9.083	0.00	1.18	1.711	o	|	|	|	|	3.44
9.167	0.00	1.17	1.703	o	|	|	|	|	3.42
9.250	0.00	1.17	1.695	o	|	|	|	|	3.41
9.333	0.00	1.16	1.687	o	|	|	|	|	3.40
9.417	0.00	1.15	1.679	o	|	|	|	|	3.38
9.500	0.00	1.15	1.671	o	|	|	|	|	3.37
9.583	0.00	1.14	1.664	o	|	|	|	|	3.36
9.667	0.00	1.14	1.656	o	|	|	|	|	3.34
9.750	0.00	1.13	1.648	o	|	|	|	|	3.33
9.833	0.00	1.13	1.640	o	|	|	|	|	3.32
9.917	0.00	1.12	1.632	o	|	|	|	|	3.30
10.000	0.00	1.11	1.625	o	|	|	|	|	3.29
10.083	0.00	1.11	1.617	o	|	|	|	|	3.28
10.167	0.00	1.10	1.609	o	|	|	|	|	3.26
10.250	0.00	1.10	1.602	o	|	|	|	|	3.25
10.333	0.00	1.09	1.594	o	|	|	|	|	3.24
10.417	0.00	1.09	1.587	o	|	|	|	|	3.23
10.500	0.00	1.08	1.579	o	|	|	|	|	3.21
10.583	0.00	1.08	1.572	o	|	|	|	|	3.20
10.667	0.00	1.07	1.564	o	|	|	|	|	3.19
10.750	0.00	1.07	1.557	o	|	|	|	|	3.18
10.833	0.00	1.06	1.550	o	|	|	|	|	3.17
10.917	0.00	1.06	1.542	o	|	|	|	|	3.15
11.000	0.00	1.05	1.535	o	|	|	|	|	3.14
11.083	0.00	1.05	1.528	o	|	|	|	|	3.13
11.167	0.00	1.04	1.521	o	|	|	|	|	3.12
11.250	0.00	1.04	1.514	o	|	|	|	|	3.10
11.333	0.00	1.03	1.507	o	|	|	|	|	3.09
11.417	0.00	1.03	1.499	o	|	|	|	|	3.08
11.500	0.00	1.02	1.492	o	|	|	|	|	3.07
11.583	0.00	1.02	1.485	o	|	|	|	|	3.06
11.667	0.00	1.01	1.478	o	|	|	|	|	3.05
11.750	0.00	1.01	1.472	o	|	|	|	|	3.03
11.833	0.00	1.00	1.465	o	|	|	|	|	3.02
11.917	0.00	1.00	1.458	o	|	|	|	|	3.01
12.000	0.00	0.99	1.451	o	|	|	|	|	3.00
12.083	0.00	0.98	1.444	o	|	|	|	|	2.99
12.167	0.00	0.97	1.437	o	|	|	|	|	2.97
12.250	0.00	0.97	1.431	o	|	|	|	|	2.96
12.333	0.00	0.96	1.424	o	|	|	|	|	2.95
12.417	0.00	0.95	1.417	o	|	|	|	|	2.94
12.500	0.00	0.94	1.411	o	|	|	|	|	2.93
12.583	0.00	0.93	1.404	o	|	|	|	|	2.91
12.667	0.00	0.93	1.398	o	|	|	|	|	2.90
12.750	0.00	0.92	1.392	o	|	|	|	|	2.89
12.833	0.00	0.91	1.385	o	|	|	|	|	2.88
12.917	0.00	0.90	1.379	o	|	|	|	|	2.87
13.000	0.00	0.90	1.373	o	|	|	|	|	2.85
13.083	0.00	0.89	1.367	o	|	|	|	|	2.84
13.167	0.00	0.88	1.361	o	|	|	|	|	2.83
13.250	0.00	0.87	1.355	o	|	|	|	|	2.82
13.333	0.00	0.87	1.349	o	|	|	|	|	2.81
13.417	0.00	0.86	1.343	o	|	|	|	|	2.80
13.500	0.00	0.85	1.337	o	|	|	|	|	2.79
13.583	0.00	0.85	1.331	o	|	|	|	|	2.78
13.667	0.00	0.84	1.325	o	|	|	|	|	2.77
13.750	0.00	0.83	1.319	o	|	|	|	|	2.75
13.833	0.00	0.83	1.314	o	|	|	|	|	2.74
13.917	0.00	0.82	1.308	o	|	|	|	|	2.73
14.000	0.00	0.81	1.302	o	|	|	|	|	2.72
14.083	0.00	0.81	1.297	o	|	|	|	|	2.71
14.167	0.00	0.80	1.291	o	|	|	|	|	2.70
14.250	0.00	0.79	1.286	o	|	|	|	|	2.69
14.333	0.00	0.79	1.280	o	|	|	|	|	2.68
14.417	0.00	0.78	1.275	o	|	|	|	|	2.67
14.500	0.00	0.77	1.270	o	|	|	|	|	2.66
14.583	0.00	0.77	1.264	o	|	|	|	|	2.65
14.667	0.00	0.76	1.259	o	|	|	|	|	2.64
14.750	0.00	0.75	1.254	o	|	|	|	|	2.63
14.833	0.00	0.75	1.249	o	|	|	|	|	2.62
14.917	0.00	0.74	1.244	o	|	|	|	|	2.61
15.000	0.00	0.73	1.239	o	|	|	|	|	2.60
15.083	0.00	0.73	1.233	o	|	|	|	|	2.59
15.167	0.00	0.72	1.228	o	|	|	|	|	2.59
15.250	0.00	0.72	1.224	o	|	|	|	|	2.58
15.333	0.00	0.71	1.219	o	|	|	|	|	2.57
15.417	0.00	0.71	1.214	o	|	|	|	|	2.56
15.500	0.00	0.70	1.209	o	|	|	|	|	2.55
15.583	0.00	0.69	1.204	o	|	|	|	|	2.54
15.667	0.00	0.69	1.199	o	|	|	|	|	2.53
15.750	0.00	0.68	1.195	o	|	|	|	|	2.52
15.833	0.00	0.68	1.190	o	|	|	|	|	2.51

15.917	0.00	0.67	1.185	o	|	|	|	|	2.51
16.000	0.00	0.67	1.181	o	|	|	|	|	2.50
16.083	0.00	0.66	1.176	o	|	|	|	|	2.49
16.167	0.00	0.65	1.172	o	|	|	|	|	2.48
16.250	0.00	0.65	1.167	o	|	|	|	|	2.47
16.333	0.00	0.64	1.163	o	|	|	|	|	2.46
16.417	0.00	0.64	1.158	o	|	|	|	|	2.45
16.500	0.00	0.63	1.154	o	|	|	|	|	2.45
16.583	0.00	0.63	1.150	o	|	|	|	|	2.44
16.667	0.00	0.62	1.145	o	|	|	|	|	2.43
16.750	0.00	0.62	1.141	o	|	|	|	|	2.42
16.833	0.00	0.61	1.137	o	|	|	|	|	2.41
16.917	0.00	0.61	1.133	o	|	|	|	|	2.41
17.000	0.00	0.60	1.128	o	|	|	|	|	2.40
17.083	0.00	0.60	1.124	o	|	|	|	|	2.39
17.167	0.00	0.59	1.120	o	|	|	|	|	2.38
17.250	0.00	0.59	1.116	o	|	|	|	|	2.38
17.333	0.00	0.58	1.112	o	|	|	|	|	2.37
17.417	0.00	0.58	1.108	o	|	|	|	|	2.36
17.500	0.00	0.57	1.104	o	|	|	|	|	2.35
17.583	0.00	0.57	1.100	o	|	|	|	|	2.35
17.667	0.00	0.56	1.096	o	|	|	|	|	2.34
17.750	0.00	0.56	1.092	o	|	|	|	|	2.33
17.833	0.00	0.55	1.089	o	|	|	|	|	2.33
17.917	0.00	0.55	1.085	o	|	|	|	|	2.32
18.000	0.00	0.55	1.081	o	|	|	|	|	2.31
18.083	0.00	0.54	1.077	o	|	|	|	|	2.30
18.167	0.00	0.54	1.074	o	|	|	|	|	2.30
18.250	0.00	0.53	1.070	o	|	|	|	|	2.29
18.333	0.00	0.53	1.066	o	|	|	|	|	2.28
18.417	0.00	0.52	1.063	o	|	|	|	|	2.28
18.500	0.00	0.52	1.059	o	|	|	|	|	2.27
18.583	0.00	0.51	1.055	o	|	|	|	|	2.26
18.667	0.00	0.51	1.052	o	|	|	|	|	2.26
18.750	0.00	0.51	1.048	o	|	|	|	|	2.25
18.833	0.00	0.50	1.045	o	|	|	|	|	2.24
18.917	0.00	0.50	1.042	o	|	|	|	|	2.24
19.000	0.00	0.49	1.038	o	|	|	|	|	2.23
19.083	0.00	0.49	1.035	o	|	|	|	|	2.22
19.167	0.00	0.49	1.031	o	|	|	|	|	2.22
19.250	0.00	0.48	1.028	o	|	|	|	|	2.21
19.333	0.00	0.48	1.025	o	|	|	|	|	2.21
19.417	0.00	0.47	1.021	o	|	|	|	|	2.20
19.500	0.00	0.47	1.018	o	|	|	|	|	2.19
19.583	0.00	0.47	1.015	o	|	|	|	|	2.19
19.667	0.00	0.46	1.012	o	|	|	|	|	2.18
19.750	0.00	0.46	1.009	o	|	|	|	|	2.18
19.833	0.00	0.45	1.005	o	|	|	|	|	2.17
19.917	0.00	0.45	1.002	o	|	|	|	|	2.16
20.000	0.00	0.45	0.999	o	|	|	|	|	2.16
20.083	0.00	0.44	0.996	o	|	|	|	|	2.15
20.167	0.00	0.44	0.993	o	|	|	|	|	2.15
20.250	0.00	0.44	0.990	o	|	|	|	|	2.14
20.333	0.00	0.43	0.987	o	|	|	|	|	2.14
20.417	0.00	0.43	0.984	o	|	|	|	|	2.13
20.500	0.00	0.43	0.981	o	|	|	|	|	2.13
20.583	0.00	0.42	0.978	o	|	|	|	|	2.12
20.667	0.00	0.42	0.975	o	|	|	|	|	2.11
20.750	0.00	0.41	0.973	o	|	|	|	|	2.11
20.833	0.00	0.41	0.970	o	|	|	|	|	2.10
20.917	0.00	0.41	0.967	o	|	|	|	|	2.10
21.000	0.00	0.40	0.964	o	|	|	|	|	2.09
21.083	0.00	0.40	0.961	o	|	|	|	|	2.09
21.167	0.00	0.40	0.959	o	|	|	|	|	2.08
21.250	0.00	0.39	0.956	o	|	|	|	|	2.08
21.333	0.00	0.39	0.953	o	|	|	|	|	2.07
21.417	0.00	0.39	0.950	o	|	|	|	|	2.07
21.500	0.00	0.38	0.948	o	|	|	|	|	2.06
21.583	0.00	0.38	0.945	o	|	|	|	|	2.06
21.667	0.00	0.38	0.943	o	|	|	|	|	2.05
21.750	0.00	0.38	0.940	o	|	|	|	|	2.05
21.833	0.00	0.37	0.937	o	|	|	|	|	2.04
21.917	0.00	0.37	0.935	o	|	|	|	|	2.04
22.000	0.00	0.37	0.932	o	|	|	|	|	2.03
22.083	0.00	0.36	0.930	o	|	|	|	|	2.03
22.167	0.00	0.36	0.927	o	|	|	|	|	2.02
22.250	0.00	0.36	0.925	o	|	|	|	|	2.02
22.333	0.00	0.35	0.922	o	|	|	|	|	2.02
22.417	0.00	0.35	0.920	o	|	|	|	|	2.01
22.500	0.00	0.35	0.918	o	|	|	|	|	2.01
22.583	0.00	0.35	0.915	o	|	|	|	|	2.00
22.667	0.00	0.34	0.913	o	|	|	|	|	2.00
22.750	0.00	0.34	0.910	o	|	|	|	|	1.99
22.833	0.00	0.34	0.908	o	|	|	|	|	1.99
22.917	0.00	0.34	0.906	o	|	|	|	|	1.98
23.000	0.00	0.34	0.903	o	|	|	|	|	1.98

23.083	0.00	0.34	0.901	o	|	|	|	|	1.97
23.167	0.00	0.34	0.899	o	|	|	|	|	1.97
23.250	0.00	0.34	0.896	o	|	|	|	|	1.96
23.333	0.00	0.34	0.894	o	|	|	|	|	1.96
23.417	0.00	0.34	0.892	o	|	|	|	|	1.95
23.500	0.00	0.34	0.889	o	|	|	|	|	1.95
23.583	0.00	0.34	0.887	o	|	|	|	|	1.94
23.667	0.00	0.34	0.885	o	|	|	|	|	1.94
23.750	0.00	0.34	0.882	o	|	|	|	|	1.93
23.833	0.00	0.34	0.880	o	|	|	|	|	1.93
23.917	0.00	0.34	0.878	o	|	|	|	|	1.92
24.000	0.00	0.33	0.875	o	|	|	|	|	1.92
24.083	0.00	0.33	0.873	o	|	|	|	|	1.92
24.167	0.00	0.33	0.871	o	|	|	|	|	1.91
24.250	0.00	0.33	0.869	o	|	|	|	|	1.91
24.333	0.00	0.33	0.866	o	|	|	|	|	1.90
24.417	0.00	0.33	0.864	o	|	|	|	|	1.90
24.500	0.00	0.33	0.862	o	|	|	|	|	1.89
24.583	0.00	0.33	0.859	o	|	|	|	|	1.89
24.667	0.00	0.33	0.857	o	|	|	|	|	1.88
24.750	0.00	0.33	0.855	o	|	|	|	|	1.88
24.833	0.00	0.33	0.853	o	|	|	|	|	1.87
24.917	0.00	0.33	0.850	o	|	|	|	|	1.87
25.000	0.00	0.33	0.848	o	|	|	|	|	1.86
25.083	0.00	0.33	0.846	o	|	|	|	|	1.86
25.167	0.00	0.33	0.844	o	|	|	|	|	1.85
25.250	0.00	0.33	0.841	o	|	|	|	|	1.85
25.333	0.00	0.33	0.839	o	|	|	|	|	1.84
25.417	0.00	0.32	0.837	o	|	|	|	|	1.84
25.500	0.00	0.32	0.835	o	|	|	|	|	1.84
25.583	0.00	0.32	0.832	o	|	|	|	|	1.83
25.667	0.00	0.32	0.830	o	|	|	|	|	1.83
25.750	0.00	0.32	0.828	o	|	|	|	|	1.82
25.833	0.00	0.32	0.826	o	|	|	|	|	1.82
25.917	0.00	0.32	0.823	o	|	|	|	|	1.81
26.000	0.00	0.32	0.821	o	|	|	|	|	1.81
26.083	0.00	0.32	0.819	o	|	|	|	|	1.80
26.167	0.00	0.32	0.817	o	|	|	|	|	1.80
26.250	0.00	0.32	0.815	o	|	|	|	|	1.79
26.333	0.00	0.32	0.812	o	|	|	|	|	1.79
26.417	0.00	0.32	0.810	o	|	|	|	|	1.79
26.500	0.00	0.32	0.808	o	|	|	|	|	1.78
26.583	0.00	0.32	0.806	o	|	|	|	|	1.78
26.667	0.00	0.32	0.804	o	|	|	|	|	1.77
26.750	0.00	0.32	0.802	o	|	|	|	|	1.77
26.833	0.00	0.32	0.799	o	|	|	|	|	1.76
26.917	0.00	0.32	0.797	o	|	|	|	|	1.76
27.000	0.00	0.31	0.795	o	|	|	|	|	1.75
27.083	0.00	0.31	0.793	o	|	|	|	|	1.75
27.167	0.00	0.31	0.791	o	|	|	|	|	1.74
27.250	0.00	0.31	0.789	o	|	|	|	|	1.74
27.333	0.00	0.31	0.786	o	|	|	|	|	1.74
27.417	0.00	0.31	0.784	o	|	|	|	|	1.73
27.500	0.00	0.31	0.782	o	|	|	|	|	1.73
27.583	0.00	0.31	0.780	o	|	|	|	|	1.72
27.667	0.00	0.31	0.778	o	|	|	|	|	1.72
27.750	0.00	0.31	0.776	o	|	|	|	|	1.71
27.833	0.00	0.31	0.773	o	|	|	|	|	1.71
27.917	0.00	0.31	0.771	o	|	|	|	|	1.70
28.000	0.00	0.31	0.769	o	|	|	|	|	1.70
28.083	0.00	0.31	0.767	o	|	|	|	|	1.70
28.167	0.00	0.31	0.765	o	|	|	|	|	1.69
28.250	0.00	0.31	0.763	o	|	|	|	|	1.69
28.333	0.00	0.31	0.761	o	|	|	|	|	1.68
28.417	0.00	0.31	0.759	o	|	|	|	|	1.68
28.500	0.00	0.31	0.757	o	|	|	|	|	1.67
28.583	0.00	0.30	0.754	o	|	|	|	|	1.67
28.667	0.00	0.30	0.752	o	|	|	|	|	1.67
28.750	0.00	0.30	0.750	o	|	|	|	|	1.66
28.833	0.00	0.30	0.748	o	|	|	|	|	1.66
28.917	0.00	0.30	0.746	o	|	|	|	|	1.65
29.000	0.00	0.30	0.744	o	|	|	|	|	1.65
29.083	0.00	0.30	0.742	o	|	|	|	|	1.64
29.167	0.00	0.30	0.740	o	|	|	|	|	1.64
29.250	0.00	0.30	0.738	o	|	|	|	|	1.64
29.333	0.00	0.30	0.736	o	|	|	|	|	1.63
29.417	0.00	0.30	0.734	o	|	|	|	|	1.63
29.500	0.00	0.30	0.732	o	|	|	|	|	1.62
29.583	0.00	0.30	0.730	o	|	|	|	|	1.62
29.667	0.00	0.30	0.727	o	|	|	|	|	1.61
29.750	0.00	0.30	0.725	o	|	|	|	|	1.61
29.833	0.00	0.30	0.723	o	|	|	|	|	1.61
29.917	0.00	0.30	0.721	o	|	|	|	|	1.60
30.000	0.00	0.30	0.719	o	|	|	|	|	1.60
30.083	0.00	0.30	0.717	o	|	|	|	|	1.59
30.167	0.00	0.30	0.715	o	|	|	|	|	1.59

30.250	0.00	0.29	0.713	o	|	|	|	|	1.58
30.333	0.00	0.29	0.711	o	|	|	|	|	1.58
30.417	0.00	0.29	0.709	o	|	|	|	|	1.58
30.500	0.00	0.29	0.707	o	|	|	|	|	1.57
30.583	0.00	0.29	0.705	o	|	|	|	|	1.57
30.667	0.00	0.29	0.703	o	|	|	|	|	1.56
30.750	0.00	0.29	0.701	o	|	|	|	|	1.56
30.833	0.00	0.29	0.699	o	|	|	|	|	1.56
30.917	0.00	0.29	0.697	o	|	|	|	|	1.55
31.000	0.00	0.29	0.695	o	|	|	|	|	1.55
31.083	0.00	0.29	0.693	o	|	|	|	|	1.54
31.167	0.00	0.29	0.691	o	|	|	|	|	1.54
31.250	0.00	0.29	0.689	o	|	|	|	|	1.53
31.333	0.00	0.29	0.687	o	|	|	|	|	1.53
31.417	0.00	0.29	0.685	o	|	|	|	|	1.53
31.500	0.00	0.29	0.683	o	|	|	|	|	1.52
31.583	0.00	0.29	0.681	o	|	|	|	|	1.52
31.667	0.00	0.29	0.679	o	|	|	|	|	1.51
31.750	0.00	0.29	0.677	o	|	|	|	|	1.51
31.833	0.00	0.29	0.675	o	|	|	|	|	1.51
31.917	0.00	0.28	0.673	o	|	|	|	|	1.50
32.000	0.00	0.28	0.671	o	|	|	|	|	1.50
32.083	0.00	0.28	0.669	o	|	|	|	|	1.49
32.167	0.00	0.28	0.667	o	|	|	|	|	1.49
32.250	0.00	0.28	0.665	o	|	|	|	|	1.49
32.333	0.00	0.28	0.664	o	|	|	|	|	1.48
32.417	0.00	0.28	0.662	o	|	|	|	|	1.48
32.500	0.00	0.28	0.660	o	|	|	|	|	1.47
32.583	0.00	0.28	0.658	o	|	|	|	|	1.47
32.667	0.00	0.28	0.656	o	|	|	|	|	1.47
32.750	0.00	0.28	0.654	o	|	|	|	|	1.46
32.833	0.00	0.28	0.652	o	|	|	|	|	1.46
32.917	0.00	0.28	0.650	o	|	|	|	|	1.45
33.000	0.00	0.28	0.648	o	|	|	|	|	1.45
33.083	0.00	0.28	0.646	o	|	|	|	|	1.45
33.167	0.00	0.28	0.644	o	|	|	|	|	1.44
33.250	0.00	0.28	0.642	o	|	|	|	|	1.44
33.333	0.00	0.28	0.640	o	|	|	|	|	1.43
33.417	0.00	0.28	0.639	o	|	|	|	|	1.43
33.500	0.00	0.28	0.637	o	|	|	|	|	1.43
33.583	0.00	0.28	0.635	o	|	|	|	|	1.42
33.667	0.00	0.27	0.633	o	|	|	|	|	1.42
33.750	0.00	0.27	0.631	o	|	|	|	|	1.41
33.833	0.00	0.27	0.629	o	|	|	|	|	1.41
33.917	0.00	0.27	0.627	o	|	|	|	|	1.41
34.000	0.00	0.27	0.625	o	|	|	|	|	1.40
34.083	0.00	0.27	0.623	o	|	|	|	|	1.40
34.167	0.00	0.27	0.622	o	|	|	|	|	1.39
34.250	0.00	0.27	0.620	o	|	|	|	|	1.39
34.333	0.00	0.27	0.618	o	|	|	|	|	1.39
34.417	0.00	0.27	0.616	o	|	|	|	|	1.38
34.500	0.00	0.27	0.614	o	|	|	|	|	1.38
34.583	0.00	0.27	0.612	o	|	|	|	|	1.38
34.667	0.00	0.27	0.610	o	|	|	|	|	1.37
34.750	0.00	0.27	0.609	o	|	|	|	|	1.37
34.833	0.00	0.27	0.607	o	|	|	|	|	1.36
34.917	0.00	0.27	0.605	o	|	|	|	|	1.36
35.000	0.00	0.27	0.603	o	|	|	|	|	1.36
35.083	0.00	0.27	0.601	o	|	|	|	|	1.35
35.167	0.00	0.27	0.599	o	|	|	|	|	1.35
35.250	0.00	0.27	0.597	o	|	|	|	|	1.34
35.333	0.00	0.27	0.596	o	|	|	|	|	1.34
35.417	0.00	0.27	0.594	o	|	|	|	|	1.34
35.500	0.00	0.26	0.592	o	|	|	|	|	1.33
35.583	0.00	0.26	0.590	o	|	|	|	|	1.33
35.667	0.00	0.26	0.588	o	|	|	|	|	1.33
35.750	0.00	0.26	0.587	o	|	|	|	|	1.32
35.833	0.00	0.26	0.585	o	|	|	|	|	1.32
35.917	0.00	0.26	0.583	o	|	|	|	|	1.31
36.000	0.00	0.26	0.581	o	|	|	|	|	1.31
36.083	0.00	0.26	0.579	o	|	|	|	|	1.31
36.167	0.00	0.26	0.578	o	|	|	|	|	1.30
36.250	0.00	0.26	0.576	o	|	|	|	|	1.30
36.333	0.00	0.26	0.574	o	|	|	|	|	1.30
36.417	0.00	0.26	0.572	o	|	|	|	|	1.29
36.500	0.00	0.26	0.570	o	|	|	|	|	1.29
36.583	0.00	0.26	0.569	o	|	|	|	|	1.28
36.667	0.00	0.26	0.567	o	|	|	|	|	1.28
36.750	0.00	0.26	0.565	o	|	|	|	|	1.28
36.833	0.00	0.26	0.563	o	|	|	|	|	1.27
36.917	0.00	0.26	0.561	o	|	|	|	|	1.27
37.000	0.00	0.26	0.560	o	|	|	|	|	1.27
37.083	0.00	0.26	0.558	o	|	|	|	|	1.26
37.167	0.00	0.26	0.556	o	|	|	|	|	1.26
37.250	0.00	0.26	0.554	o	|	|	|	|	1.26
37.333	0.00	0.25	0.553	o	|	|	|	|	1.25

37.417	0.00	0.25	0.551	o	|	|	|	|	1.25
37.500	0.00	0.25	0.549	o	|	|	|	|	1.24
37.583	0.00	0.25	0.547	o	|	|	|	|	1.24
37.667	0.00	0.25	0.546	o	|	|	|	|	1.24
37.750	0.00	0.25	0.544	o	|	|	|	|	1.23
37.833	0.00	0.25	0.542	o	|	|	|	|	1.23
37.917	0.00	0.25	0.540	o	|	|	|	|	1.23
38.000	0.00	0.25	0.539	o	|	|	|	|	1.22
38.083	0.00	0.25	0.537	o	|	|	|	|	1.22
38.167	0.00	0.25	0.535	o	|	|	|	|	1.22
38.250	0.00	0.25	0.534	o	|	|	|	|	1.21
38.333	0.00	0.25	0.532	o	|	|	|	|	1.21
38.417	0.00	0.25	0.530	o	|	|	|	|	1.21
38.500	0.00	0.25	0.528	o	|	|	|	|	1.20
38.583	0.00	0.25	0.527	o	|	|	|	|	1.20
38.667	0.00	0.25	0.525	o	|	|	|	|	1.19
38.750	0.00	0.25	0.523	o	|	|	|	|	1.19
38.833	0.00	0.25	0.522	o	|	|	|	|	1.19
38.917	0.00	0.25	0.520	o	|	|	|	|	1.18
39.000	0.00	0.25	0.518	o	|	|	|	|	1.18
39.083	0.00	0.25	0.516	o	|	|	|	|	1.18
39.167	0.00	0.25	0.515	o	|	|	|	|	1.17
39.250	0.00	0.25	0.513	o	|	|	|	|	1.17
39.333	0.00	0.24	0.511	o	|	|	|	|	1.17
39.417	0.00	0.24	0.510	o	|	|	|	|	1.16
39.500	0.00	0.24	0.508	o	|	|	|	|	1.16
39.583	0.00	0.24	0.506	o	|	|	|	|	1.16
39.667	0.00	0.24	0.505	o	|	|	|	|	1.15
39.750	0.00	0.24	0.503	o	|	|	|	|	1.15
39.833	0.00	0.24	0.501	o	|	|	|	|	1.15
39.917	0.00	0.24	0.500	o	|	|	|	|	1.14
40.000	0.00	0.24	0.498	o	|	|	|	|	1.14
40.083	0.00	0.24	0.496	o	|	|	|	|	1.14
40.167	0.00	0.24	0.495	o	|	|	|	|	1.13
40.250	0.00	0.24	0.493	o	|	|	|	|	1.13
40.333	0.00	0.24	0.491	o	|	|	|	|	1.12
40.417	0.00	0.24	0.490	o	|	|	|	|	1.12
40.500	0.00	0.24	0.488	o	|	|	|	|	1.12
40.583	0.00	0.24	0.486	o	|	|	|	|	1.11
40.667	0.00	0.24	0.485	o	|	|	|	|	1.11
40.750	0.00	0.24	0.483	o	|	|	|	|	1.11
40.833	0.00	0.24	0.481	o	|	|	|	|	1.10
40.917	0.00	0.24	0.480	o	|	|	|	|	1.10
41.000	0.00	0.24	0.478	o	|	|	|	|	1.10
41.083	0.00	0.24	0.477	o	|	|	|	|	1.09
41.167	0.00	0.24	0.475	o	|	|	|	|	1.09
41.250	0.00	0.24	0.473	o	|	|	|	|	1.09
41.333	0.00	0.24	0.472	o	|	|	|	|	1.08
41.417	0.00	0.23	0.470	o	|	|	|	|	1.08
41.500	0.00	0.23	0.468	o	|	|	|	|	1.08
41.583	0.00	0.23	0.467	o	|	|	|	|	1.07
41.667	0.00	0.23	0.465	o	|	|	|	|	1.07
41.750	0.00	0.23	0.464	o	|	|	|	|	1.07
41.833	0.00	0.23	0.462	o	|	|	|	|	1.06
41.917	0.00	0.23	0.460	o	|	|	|	|	1.06
42.000	0.00	0.23	0.459	o	|	|	|	|	1.06
42.083	0.00	0.23	0.457	o	|	|	|	|	1.05
42.167	0.00	0.23	0.456	o	|	|	|	|	1.05
42.250	0.00	0.23	0.454	o	|	|	|	|	1.05
42.333	0.00	0.23	0.452	o	|	|	|	|	1.04
42.417	0.00	0.23	0.451	o	|	|	|	|	1.04
42.500	0.00	0.23	0.449	o	|	|	|	|	1.04
42.583	0.00	0.23	0.448	o	|	|	|	|	1.03
42.667	0.00	0.23	0.446	o	|	|	|	|	1.03
42.750	0.00	0.23	0.445	o	|	|	|	|	1.03
42.833	0.00	0.23	0.443	o	|	|	|	|	1.02
42.917	0.00	0.23	0.441	o	|	|	|	|	1.02
43.000	0.00	0.23	0.440	o	|	|	|	|	1.02
43.083	0.00	0.23	0.438	o	|	|	|	|	1.02
43.167	0.00	0.23	0.437	o	|	|	|	|	1.01
43.250	0.00	0.23	0.435	o	|	|	|	|	1.01
43.333	0.00	0.23	0.434	o	|	|	|	|	1.01
43.417	0.00	0.23	0.432	o	|	|	|	|	1.00
43.500	0.00	0.22	0.431	o	|	|	|	|	1.00
43.583	0.00	0.22	0.429	o	|	|	|	|	1.00
43.667	0.00	0.22	0.427	o	|	|	|	|	0.99
43.750	0.00	0.22	0.426	o	|	|	|	|	0.99
43.833	0.00	0.22	0.424	o	|	|	|	|	0.98
43.917	0.00	0.22	0.423	o	|	|	|	|	0.98
44.000	0.00	0.22	0.421	o	|	|	|	|	0.98
44.083	0.00	0.22	0.420	o	|	|	|	|	0.97
44.167	0.00	0.22	0.418	o	|	|	|	|	0.97
44.250	0.00	0.22	0.417	o	|	|	|	|	0.97
44.333	0.00	0.22	0.415	o	|	|	|	|	0.96
44.417	0.00	0.22	0.414	o	|	|	|	|	0.96
44.500	0.00	0.22	0.412	o	|	|	|	|	0.96

44.583	0.00	0.21	0.411	o	|	|	|	0.95
44.667	0.00	0.21	0.409	o	|	|	|	0.95
44.750	0.00	0.21	0.408	o	|	|	|	0.95
44.833	0.00	0.21	0.406	o	|	|	|	0.94
44.917	0.00	0.21	0.405	o	|	|	|	0.94
45.000	0.00	0.21	0.404	o	|	|	|	0.94
45.083	0.00	0.21	0.402	o	|	|	|	0.93
45.167	0.00	0.21	0.401	o	|	|	|	0.93
45.250	0.00	0.21	0.399	o	|	|	|	0.93
45.333	0.00	0.21	0.398	o	|	|	|	0.92
45.417	0.00	0.21	0.396	o	|	|	|	0.92
45.500	0.00	0.21	0.395	o	|	|	|	0.92
45.583	0.00	0.21	0.394	o	|	|	|	0.91
45.667	0.00	0.20	0.392	o	|	|	|	0.91
45.750	0.00	0.20	0.391	o	|	|	|	0.91
45.833	0.00	0.20	0.389	o	|	|	|	0.90
45.917	0.00	0.20	0.388	o	|	|	|	0.90
46.000	0.00	0.20	0.387	o	|	|	|	0.90
46.083	0.00	0.20	0.385	o	|	|	|	0.89
46.167	0.00	0.20	0.384	o	|	|	|	0.89
46.250	0.00	0.20	0.382	o	|	|	|	0.89
46.333	0.00	0.20	0.381	o	|	|	|	0.88
46.417	0.00	0.20	0.380	o	|	|	|	0.88
46.500	0.00	0.20	0.378	o	|	|	|	0.88
46.583	0.00	0.20	0.377	o	|	|	|	0.87
46.667	0.00	0.20	0.376	o	|	|	|	0.87
46.750	0.00	0.20	0.374	o	|	|	|	0.87
46.833	0.00	0.19	0.373	o	|	|	|	0.87
46.917	0.00	0.19	0.372	o	|	|	|	0.86
47.000	0.00	0.19	0.370	o	|	|	|	0.86
47.083	0.00	0.19	0.369	o	|	|	|	0.86
47.167	0.00	0.19	0.368	o	|	|	|	0.85
47.250	0.00	0.19	0.366	o	|	|	|	0.85
47.333	0.00	0.19	0.365	o	|	|	|	0.85
47.417	0.00	0.19	0.364	o	|	|	|	0.84
47.500	0.00	0.19	0.362	o	|	|	|	0.84
47.583	0.00	0.19	0.361	o	|	|	|	0.84
47.667	0.00	0.19	0.360	o	|	|	|	0.83
47.750	0.00	0.19	0.358	o	|	|	|	0.83
47.833	0.00	0.19	0.357	o	|	|	|	0.83
47.917	0.00	0.19	0.356	o	|	|	|	0.83
48.000	0.00	0.19	0.355	o	|	|	|	0.82
48.083	0.00	0.18	0.353	o	|	|	|	0.82
48.167	0.00	0.18	0.352	o	|	|	|	0.82
48.250	0.00	0.18	0.351	o	|	|	|	0.81
48.333	0.00	0.18	0.349	o	|	|	|	0.81
48.417	0.00	0.18	0.348	o	|	|	|	0.81
48.500	0.00	0.18	0.347	o	|	|	|	0.81
48.583	0.00	0.18	0.346	o	|	|	|	0.80
48.667	0.00	0.18	0.345	o	|	|	|	0.80
48.750	0.00	0.18	0.343	o	|	|	|	0.80
48.833	0.00	0.18	0.342	o	|	|	|	0.79
48.917	0.00	0.18	0.341	o	|	|	|	0.79
49.000	0.00	0.18	0.340	o	|	|	|	0.79
49.083	0.00	0.18	0.338	o	|	|	|	0.79
49.167	0.00	0.18	0.337	o	|	|	|	0.78
49.250	0.00	0.18	0.336	o	|	|	|	0.78
49.333	0.00	0.17	0.335	o	|	|	|	0.78
49.417	0.00	0.17	0.334	o	|	|	|	0.77
49.500	0.00	0.17	0.332	o	|	|	|	0.77
49.583	0.00	0.17	0.331	o	|	|	|	0.77
49.667	0.00	0.17	0.330	o	|	|	|	0.77
49.750	0.00	0.17	0.329	o	|	|	|	0.76
49.833	0.00	0.17	0.328	o	|	|	|	0.76
49.917	0.00	0.17	0.326	o	|	|	|	0.76
50.000	0.00	0.17	0.325	o	|	|	|	0.75
50.083	0.00	0.17	0.324	o	|	|	|	0.75
50.167	0.00	0.17	0.323	o	|	|	|	0.75
50.250	0.00	0.17	0.322	o	|	|	|	0.75
50.333	0.00	0.17	0.321	o	|	|	|	0.74
50.417	0.00	0.17	0.319	o	|	|	|	0.74
50.500	0.00	0.17	0.318	o	|	|	|	0.74
50.583	0.00	0.17	0.317	o	|	|	|	0.74
50.667	0.00	0.16	0.316	o	|	|	|	0.73
50.750	0.00	0.16	0.315	o	|	|	|	0.73
50.833	0.00	0.16	0.314	o	|	|	|	0.73
50.917	0.00	0.16	0.313	o	|	|	|	0.73
51.000	0.00	0.16	0.312	o	|	|	|	0.72
51.083	0.00	0.16	0.310	o	|	|	|	0.72
51.167	0.00	0.16	0.309	o	|	|	|	0.72
51.250	0.00	0.16	0.308	o	|	|	|	0.72
51.333	0.00	0.16	0.307	o	|	|	|	0.71
51.417	0.00	0.16	0.306	o	|	|	|	0.71
51.500	0.00	0.16	0.305	o	|	|	|	0.71
51.583	0.00	0.16	0.304	o	|	|	|	0.70
51.667	0.00	0.16	0.303	o	|	|	|	0.70

51.750	0.00	0.16	0.302	o	|	|	|	0.70
51.833	0.00	0.16	0.301	o	|	|	|	0.70
51.917	0.00	0.16	0.299	o	|	|	|	0.69
52.000	0.00	0.16	0.298	o	|	|	|	0.69
52.083	0.00	0.16	0.297	o	|	|	|	0.69
52.167	0.00	0.15	0.296	o	|	|	|	0.69
52.250	0.00	0.15	0.295	o	|	|	|	0.68
52.333	0.00	0.15	0.294	o	|	|	|	0.68
52.417	0.00	0.15	0.293	o	|	|	|	0.68
52.500	0.00	0.15	0.292	o	|	|	|	0.68
52.583	0.00	0.15	0.291	o	|	|	|	0.68
52.667	0.00	0.15	0.290	o	|	|	|	0.67
52.750	0.00	0.15	0.289	o	|	|	|	0.67
52.833	0.00	0.15	0.288	o	|	|	|	0.67
52.917	0.00	0.15	0.287	o	|	|	|	0.67
53.000	0.00	0.15	0.286	o	|	|	|	0.66
53.083	0.00	0.15	0.285	o	|	|	|	0.66
53.167	0.00	0.15	0.284	o	|	|	|	0.66
53.250	0.00	0.15	0.283	o	|	|	|	0.66
53.333	0.00	0.15	0.282	o	|	|	|	0.65
53.417	0.00	0.15	0.281	o	|	|	|	0.65
53.500	0.00	0.15	0.280	o	|	|	|	0.65
53.583	0.00	0.15	0.279	o	|	|	|	0.65
53.667	0.00	0.14	0.278	o	|	|	|	0.64
53.750	0.00	0.14	0.277	o	|	|	|	0.64
53.833	0.00	0.14	0.276	o	|	|	|	0.64
53.917	0.00	0.14	0.275	o	|	|	|	0.64
54.000	0.00	0.14	0.274	o	|	|	|	0.64
54.083	0.00	0.14	0.273	o	|	|	|	0.63
54.167	0.00	0.14	0.272	o	|	|	|	0.63
54.250	0.00	0.14	0.271	o	|	|	|	0.63
54.333	0.00	0.14	0.270	o	|	|	|	0.63
54.417	0.00	0.14	0.269	o	|	|	|	0.62
54.500	0.00	0.14	0.268	o	|	|	|	0.62
54.583	0.00	0.14	0.267	o	|	|	|	0.62
54.667	0.00	0.14	0.266	o	|	|	|	0.62
54.750	0.00	0.14	0.265	o	|	|	|	0.61
54.833	0.00	0.14	0.264	o	|	|	|	0.61
54.917	0.00	0.14	0.263	o	|	|	|	0.61
55.000	0.00	0.14	0.262	o	|	|	|	0.61
55.083	0.00	0.14	0.261	o	|	|	|	0.61
55.167	0.00	0.14	0.260	o	|	|	|	0.60
55.250	0.00	0.14	0.259	o	|	|	|	0.60
55.333	0.00	0.13	0.258	o	|	|	|	0.60
55.417	0.00	0.13	0.257	o	|	|	|	0.60
55.500	0.00	0.13	0.257	o	|	|	|	0.60
55.583	0.00	0.13	0.256	o	|	|	|	0.59
55.667	0.00	0.13	0.255	o	|	|	|	0.59
55.750	0.00	0.13	0.254	o	|	|	|	0.59
55.833	0.00	0.13	0.253	o	|	|	|	0.59
55.917	0.00	0.13	0.252	o	|	|	|	0.58
56.000	0.00	0.13	0.251	o	|	|	|	0.58
56.083	0.00	0.13	0.250	o	|	|	|	0.58
56.167	0.00	0.13	0.249	o	|	|	|	0.58
56.250	0.00	0.13	0.248	o	|	|	|	0.58
56.333	0.00	0.13	0.247	o	|	|	|	0.57
56.417	0.00	0.13	0.247	o	|	|	|	0.57
56.500	0.00	0.13	0.246	o	|	|	|	0.57
56.583	0.00	0.13	0.245	o	|	|	|	0.57
56.667	0.00	0.13	0.244	o	|	|	|	0.57
56.750	0.00	0.13	0.243	o	|	|	|	0.56
56.833	0.00	0.13	0.242	o	|	|	|	0.56
56.917	0.00	0.13	0.241	o	|	|	|	0.56
57.000	0.00	0.13	0.240	o	|	|	|	0.56
57.083	0.00	0.13	0.240	o	|	|	|	0.56
57.167	0.00	0.12	0.239	o	|	|	|	0.55
57.250	0.00	0.12	0.238	o	|	|	|	0.55
57.333	0.00	0.12	0.237	o	|	|	|	0.55
57.417	0.00	0.12	0.236	o	|	|	|	0.55
57.500	0.00	0.12	0.235	o	|	|	|	0.55
57.583	0.00	0.12	0.234	o	|	|	|	0.54
57.667	0.00	0.12	0.234	o	|	|	|	0.54
57.750	0.00	0.12	0.233	o	|	|	|	0.54
57.833	0.00	0.12	0.232	o	|	|	|	0.54
57.917	0.00	0.12	0.231	o	|	|	|	0.54
58.000	0.00	0.12	0.230	o	|	|	|	0.53
58.083	0.00	0.12	0.229	o	|	|	|	0.53
58.167	0.00	0.12	0.229	o	|	|	|	0.53
58.250	0.00	0.12	0.228	o	|	|	|	0.53
58.333	0.00	0.12	0.227	o	|	|	|	0.53
58.417	0.00	0.12	0.226	o	|	|	|	0.52
58.500	0.00	0.12	0.225	o	|	|	|	0.52
58.583	0.00	0.12	0.225	o	|	|	|	0.52
58.667	0.00	0.12	0.224	o	|	|	|	0.52
58.750	0.00	0.12	0.223	o	|	|	|	0.52
58.833	0.00	0.12	0.222	o	|	|	|	0.52

58.917	0.00	0.12	0.221	o	|	|	|	|	0.51
59.000	0.00	0.12	0.221	o	|	|	|	|	0.51
59.083	0.00	0.11	0.220	o	|	|	|	|	0.51
59.167	0.00	0.11	0.219	o	|	|	|	|	0.51
59.250	0.00	0.11	0.218	o	|	|	|	|	0.51
59.333	0.00	0.11	0.217	o	|	|	|	|	0.50
59.417	0.00	0.11	0.217	o	|	|	|	|	0.50
59.500	0.00	0.11	0.216	o	|	|	|	|	0.50
59.583	0.00	0.11	0.215	o	|	|	|	|	0.50
59.667	0.00	0.11	0.214	o	|	|	|	|	0.50
59.750	0.00	0.11	0.214	o	|	|	|	|	0.50
59.833	0.00	0.11	0.213	o	|	|	|	|	0.49
59.917	0.00	0.11	0.212	o	|	|	|	|	0.49
60.000	0.00	0.11	0.211	o	|	|	|	|	0.49
60.083	0.00	0.11	0.211	o	|	|	|	|	0.49
60.167	0.00	0.11	0.210	o	|	|	|	|	0.49
60.250	0.00	0.11	0.209	o	|	|	|	|	0.48
60.333	0.00	0.11	0.208	o	|	|	|	|	0.48
60.417	0.00	0.11	0.208	o	|	|	|	|	0.48
60.500	0.00	0.11	0.207	o	|	|	|	|	0.48
60.583	0.00	0.11	0.206	o	|	|	|	|	0.48
60.667	0.00	0.11	0.205	o	|	|	|	|	0.48
60.750	0.00	0.11	0.205	o	|	|	|	|	0.47
60.833	0.00	0.11	0.204	o	|	|	|	|	0.47
60.917	0.00	0.11	0.203	o	|	|	|	|	0.47
61.000	0.00	0.11	0.202	o	|	|	|	|	0.47
61.083	0.00	0.11	0.202	o	|	|	|	|	0.47
61.167	0.00	0.10	0.201	o	|	|	|	|	0.47
61.250	0.00	0.10	0.200	o	|	|	|	|	0.46
61.333	0.00	0.10	0.199	o	|	|	|	|	0.46
61.417	0.00	0.10	0.199	o	|	|	|	|	0.46
61.500	0.00	0.10	0.198	o	|	|	|	|	0.46
61.583	0.00	0.10	0.197	o	|	|	|	|	0.46
61.667	0.00	0.10	0.197	o	|	|	|	|	0.46
61.750	0.00	0.10	0.196	o	|	|	|	|	0.45
61.833	0.00	0.10	0.195	o	|	|	|	|	0.45
61.917	0.00	0.10	0.195	o	|	|	|	|	0.45
62.000	0.00	0.10	0.194	o	|	|	|	|	0.45
62.083	0.00	0.10	0.193	o	|	|	|	|	0.45
62.167	0.00	0.10	0.192	o	|	|	|	|	0.45
62.250	0.00	0.10	0.192	o	|	|	|	|	0.44
62.333	0.00	0.10	0.191	o	|	|	|	|	0.44

Remaining water in basin = 0.19 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 748
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.694 (CFS)
Total volume = 2.522 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro210310.rte
**********HYDROGRAPH DATA**********
Number of intervals = 41
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 47.348 (CFS)
Total volume = 3.481 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 41
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.431	0.225	0.430	0.432
2.000	0.914	0.344	0.913	0.915
3.000	1.451	0.991	1.448	1.454
4.000	2.049	1.417	2.044	2.054
5.000	2.712	1.731	2.706	2.718
5.250	2.888	1.801	2.882	2.894
5.500	3.069	17.046	3.010	3.128
6.000	3.443	225.078	2.668	4.218

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	11.8	23.67	35.51	47.35	Depth (Ft.)
0.083	1.54	0.00	0.005	OI	|	|	|	|	0.01
0.167	4.07	0.01	0.025	O I	|	|	|	|	0.06
0.250	4.48	0.03	0.054	O I	|	|	|	|	0.13
0.333	4.85	0.04	0.086	O I	|	|	|	|	0.20
0.417	5.68	0.06	0.122	O I	|	|	|	|	0.28
0.500	6.31	0.08	0.162	O I	|	|	|	|	0.38
0.583	6.60	0.11	0.206	O I	|	|	|	|	0.48
0.667	6.55	0.13	0.251	O I	|	|	|	|	0.58
0.750	7.09	0.15	0.297	O I	|	|	|	|	0.69
0.833	6.85	0.18	0.343	O I	|	|	|	|	0.80
0.917	6.44	0.20	0.388	O I	|	|	|	|	0.90
1.000	6.73	0.23	0.432	O I	|	|	|	|	1.00
1.083	7.61	0.24	0.480	O I	|	|	|	|	1.10
1.167	8.47	0.25	0.533	O I	|	|	|	|	1.21
1.250	8.70	0.26	0.591	O I	|	|	|	|	1.33
1.333	8.58	0.28	0.648	O I	|	|	|	|	1.45
1.417	8.97	0.29	0.707	O I	|	|	|	|	1.57
1.500	10.26	0.31	0.771	O I	|	|	|	|	1.70

1.583	10.39	0.33	0.840	O	I|	|	|	|	1.85
1.667	10.31	0.34	0.909	O	I |	|	|	|	1.99
1.750	12.34	0.43	0.984	O	I	|	|	|	2.13
1.833	14.37	0.54	1.073	O	|I	|	|	|	2.30
1.917	13.76	0.65	1.165	O	|I	|	|	|	2.47
2.000	13.29	0.75	1.254	O	I	|	|	|	2.63
2.083	13.81	0.86	1.342	O	|I	|	|	|	2.80
2.167	16.88	0.98	1.441	O	| I	|	|	|	2.98
2.250	23.12	1.08	1.572	O	| I|	|	|	|	3.20
2.333	23.80	1.19	1.725	O	| I	|	|	|	3.46
2.417	27.09	1.31	1.892	O	| | I	|	|	|	3.74
2.500	40.28	1.45	2.115	O	| |	I |	|	|	4.10
2.583	47.35	1.59	2.406	|O	| |	|	|	I	4.54
2.667	47.12	1.73	2.720	|O	| |	|	|	I|	5.01
2.750	31.31	7.65	2.957	| O	| |	| I	|	|	5.35
2.833	15.96	14.84	3.043	| | O	| |	|	|	|	5.46
2.917	11.33	14.30	3.036	| I|O	| |	|	|	|	5.45
3.000	7.86	12.18	3.011	| I O	| |	|	|	|	5.42
3.083	3.50	9.26	2.977	| I O |	| |	|	|	|	5.37
3.167	1.08	6.13	2.939	I O	| |	|	|	|	5.32
3.250	0.51	3.73	2.911	I O	| |	|	|	|	5.28
3.333	0.23	2.22	2.893	IO	| |	|	|	|	5.26
3.417	0.05	1.80	2.880	IO	| |	|	|	|	5.24
3.500	0.00	1.79	2.868	IO	| |	|	|	|	5.22
3.583	0.00	1.79	2.856	IO	| |	|	|	|	5.20
3.667	0.00	1.78	2.843	IO	| |	|	|	|	5.19
3.750	0.00	1.78	2.831	IO	| |	|	|	|	5.17
3.833	0.00	1.77	2.819	IO	| |	|	|	|	5.15
3.917	0.00	1.77	2.807	IO	| |	|	|	|	5.13
4.000	0.00	1.76	2.794	IO	| |	|	|	|	5.12
4.083	0.00	1.76	2.782	IO	| |	|	|	|	5.10
4.167	0.00	1.75	2.770	IO	| |	|	|	|	5.08
4.250	0.00	1.75	2.758	IO	| |	|	|	|	5.07
4.333	0.00	1.74	2.746	IO	| |	|	|	|	5.05
4.417	0.00	1.74	2.734	IO	| |	|	|	|	5.03
4.500	0.00	1.74	2.722	IO	| |	|	|	|	5.01
4.583	0.00	1.73	2.710	IO	| |	|	|	|	5.00
4.667	0.00	1.72	2.698	IO	| |	|	|	|	4.98
4.750	0.00	1.72	2.686	IO	| |	|	|	|	4.96
4.833	0.00	1.71	2.675	IO	| |	|	|	|	4.94
4.917	0.00	1.71	2.663	IO	| |	|	|	|	4.93
5.000	0.00	1.70	2.651	IO	| |	|	|	|	4.91
5.083	0.00	1.70	2.639	IO	| |	|	|	|	4.89
5.167	0.00	1.69	2.628	IO	| |	|	|	|	4.87
5.250	0.00	1.69	2.616	IO	| |	|	|	|	4.86
5.333	0.00	1.68	2.605	IO	| |	|	|	|	4.84
5.417	0.00	1.67	2.593	IO	| |	|	|	|	4.82
5.500	0.00	1.67	2.581	IO	| |	|	|	|	4.80
5.583	0.00	1.66	2.570	IO	| |	|	|	|	4.79
5.667	0.00	1.66	2.559	IO	| |	|	|	|	4.77
5.750	0.00	1.65	2.547	IO	| |	|	|	|	4.75
5.833	0.00	1.65	2.536	IO	| |	|	|	|	4.73
5.917	0.00	1.64	2.524	IO	| |	|	|	|	4.72
6.000	0.00	1.64	2.513	IO	| |	|	|	|	4.70
6.083	0.00	1.63	2.502	IO	| |	|	|	|	4.68
6.167	0.00	1.63	2.491	IO	| |	|	|	|	4.67
6.250	0.00	1.62	2.480	IO	| |	|	|	|	4.65
6.333	0.00	1.62	2.468	IO	| |	|	|	|	4.63
6.417	0.00	1.61	2.457	IO	| |	|	|	|	4.62
6.500	0.00	1.61	2.446	IO	| |	|	|	|	4.60
6.583	0.00	1.60	2.435	IO	| |	|	|	|	4.58
6.667	0.00	1.59	2.424	IO	| |	|	|	|	4.57
6.750	0.00	1.59	2.413	IO	| |	|	|	|	4.55
6.833	0.00	1.58	2.402	IO	| |	|	|	|	4.53
6.917	0.00	1.58	2.391	IO	| |	|	|	|	4.52
7.000	0.00	1.57	2.380	IO	| |	|	|	|	4.50
7.083	0.00	1.57	2.370	IO	| |	|	|	|	4.48
7.167	0.00	1.56	2.359	IO	| |	|	|	|	4.47
7.250	0.00	1.56	2.348	IO	| |	|	|	|	4.45
7.333	0.00	1.55	2.337	IO	| |	|	|	|	4.44
7.417	0.00	1.55	2.327	IO	| |	|	|	|	4.42
7.500	0.00	1.54	2.316	IO	| |	|	|	|	4.40
7.583	0.00	1.54	2.305	IO	| |	|	|	|	4.39
7.667	0.00	1.53	2.295	IO	| |	|	|	|	4.37
7.750	0.00	1.53	2.284	IO	| |	|	|	|	4.35
7.833	0.00	1.52	2.274	IO	| |	|	|	|	4.34
7.917	0.00	1.52	2.263	IO	| |	|	|	|	4.32
8.000	0.00	1.51	2.253	IO	| |	|	|	|	4.31
8.083	0.00	1.51	2.243	IO	| |	|	|	|	4.29
8.167	0.00	1.50	2.232	IO	| |	|	|	|	4.28
8.250	0.00	1.50	2.222	IO	| |	|	|	|	4.26
8.333	0.00	1.49	2.212	IO	| |	|	|	|	4.25
8.417	0.00	1.49	2.201	IO	| |	|	|	|	4.23
8.500	0.00	1.48	2.191	IO	| |	|	|	|	4.21
8.583	0.00	1.48	2.181	O	| |	|	|	|	4.20
8.667	0.00	1.47	2.171	O	| |	|	|	|	4.18

8.750	0.00	1.47	2.160	o					4.17
8.833	0.00	1.47	2.150	o					4.15
8.917	0.00	1.46	2.140	o					4.14
9.000	0.00	1.46	2.130	o					4.12
9.083	0.00	1.45	2.120	o					4.11
9.167	0.00	1.45	2.110	o					4.09
9.250	0.00	1.44	2.100	o					4.08
9.333	0.00	1.44	2.090	o					4.06
9.417	0.00	1.43	2.081	o					4.05
9.500	0.00	1.43	2.071	o					4.03
9.583	0.00	1.42	2.061	o					4.02
9.667	0.00	1.42	2.051	o					4.00
9.750	0.00	1.41	2.041	o					3.99
9.833	0.00	1.40	2.032	o					3.97
9.917	0.00	1.40	2.022	o					3.95
10.000	0.00	1.39	2.012	o					3.94
10.083	0.00	1.38	2.003	o					3.92
10.167	0.00	1.38	1.993	o					3.91
10.250	0.00	1.37	1.984	o					3.89
10.333	0.00	1.36	1.974	o					3.88
10.417	0.00	1.36	1.965	o					3.86
10.500	0.00	1.35	1.956	o					3.84
10.583	0.00	1.34	1.946	o					3.83
10.667	0.00	1.34	1.937	o					3.81
10.750	0.00	1.33	1.928	o					3.80
10.833	0.00	1.32	1.919	o					3.78
10.917	0.00	1.32	1.910	o					3.77
11.000	0.00	1.31	1.901	o					3.75
11.083	0.00	1.30	1.892	o					3.74
11.167	0.00	1.30	1.883	o					3.72
11.250	0.00	1.29	1.874	o					3.71
11.333	0.00	1.29	1.865	o					3.69
11.417	0.00	1.28	1.856	o					3.68
11.500	0.00	1.27	1.847	o					3.66
11.583	0.00	1.27	1.839	o					3.65
11.667	0.00	1.26	1.830	o					3.63
11.750	0.00	1.25	1.821	o					3.62
11.833	0.00	1.25	1.813	o					3.60
11.917	0.00	1.24	1.804	o					3.59
12.000	0.00	1.24	1.796	o					3.58
12.083	0.00	1.23	1.787	o					3.56
12.167	0.00	1.22	1.779	o					3.55
12.250	0.00	1.22	1.770	o					3.53
12.333	0.00	1.21	1.762	o					3.52
12.417	0.00	1.21	1.753	o					3.51
12.500	0.00	1.20	1.745	o					3.49
12.583	0.00	1.19	1.737	o					3.48
12.667	0.00	1.19	1.729	o					3.46
12.750	0.00	1.18	1.721	o					3.45
12.833	0.00	1.18	1.712	o					3.44
12.917	0.00	1.17	1.704	o					3.42
13.000	0.00	1.17	1.696	o					3.41
13.083	0.00	1.16	1.688	o					3.40
13.167	0.00	1.15	1.680	o					3.38
13.250	0.00	1.15	1.672	o					3.37
13.333	0.00	1.14	1.664	o					3.36
13.417	0.00	1.14	1.657	o					3.34
13.500	0.00	1.13	1.649	o					3.33
13.583	0.00	1.13	1.641	o					3.32
13.667	0.00	1.12	1.633	o					3.30
13.750	0.00	1.12	1.626	o					3.29
13.833	0.00	1.11	1.618	o					3.28
13.917	0.00	1.10	1.610	o					3.27
14.000	0.00	1.10	1.603	o					3.25
14.083	0.00	1.09	1.595	o					3.24
14.167	0.00	1.09	1.588	o					3.23
14.250	0.00	1.08	1.580	o					3.22
14.333	0.00	1.08	1.573	o					3.20
14.417	0.00	1.07	1.565	o					3.19
14.500	0.00	1.07	1.558	o					3.18
14.583	0.00	1.06	1.551	o					3.17
14.667	0.00	1.06	1.543	o					3.15
14.750	0.00	1.05	1.536	o					3.14
14.833	0.00	1.05	1.529	o					3.13
14.917	0.00	1.04	1.522	o					3.12
15.000	0.00	1.04	1.515	o					3.11
15.083	0.00	1.03	1.507	o					3.09
15.167	0.00	1.03	1.500	o					3.08
15.250	0.00	1.02	1.493	o					3.07
15.333	0.00	1.02	1.486	o					3.06
15.417	0.00	1.01	1.479	o					3.05
15.500	0.00	1.01	1.472	o					3.04
15.583	0.00	1.00	1.465	o					3.02
15.667	0.00	1.00	1.459	o					3.01
15.750	0.00	0.99	1.452	o					3.00
15.833	0.00	0.98	1.445	o					2.99

15.917	0.00	0.98	1.438	o	|	|	|	|	2.98
16.000	0.00	0.97	1.431	o	|	|	|	|	2.96
16.083	0.00	0.96	1.425	o	|	|	|	|	2.95
16.167	0.00	0.95	1.418	o	|	|	|	|	2.94
16.250	0.00	0.94	1.412	o	|	|	|	|	2.93
16.333	0.00	0.94	1.405	o	|	|	|	|	2.91
16.417	0.00	0.93	1.399	o	|	|	|	|	2.90
16.500	0.00	0.92	1.392	o	|	|	|	|	2.89
16.583	0.00	0.91	1.386	o	|	|	|	|	2.88
16.667	0.00	0.91	1.380	o	|	|	|	|	2.87
16.750	0.00	0.90	1.374	o	|	|	|	|	2.86
16.833	0.00	0.89	1.368	o	|	|	|	|	2.84
16.917	0.00	0.88	1.361	o	|	|	|	|	2.83
17.000	0.00	0.88	1.355	o	|	|	|	|	2.82
17.083	0.00	0.87	1.349	o	|	|	|	|	2.81
17.167	0.00	0.86	1.343	o	|	|	|	|	2.80
17.250	0.00	0.85	1.337	o	|	|	|	|	2.79
17.333	0.00	0.85	1.332	o	|	|	|	|	2.78
17.417	0.00	0.84	1.326	o	|	|	|	|	2.77
17.500	0.00	0.83	1.320	o	|	|	|	|	2.76
17.583	0.00	0.83	1.314	o	|	|	|	|	2.75
17.667	0.00	0.82	1.309	o	|	|	|	|	2.73
17.750	0.00	0.81	1.303	o	|	|	|	|	2.72
17.833	0.00	0.81	1.297	o	|	|	|	|	2.71
17.917	0.00	0.80	1.292	o	|	|	|	|	2.70
18.000	0.00	0.79	1.286	o	|	|	|	|	2.69
18.083	0.00	0.79	1.281	o	|	|	|	|	2.68
18.167	0.00	0.78	1.276	o	|	|	|	|	2.67
18.250	0.00	0.77	1.270	o	|	|	|	|	2.66
18.333	0.00	0.77	1.265	o	|	|	|	|	2.65
18.417	0.00	0.76	1.260	o	|	|	|	|	2.64
18.500	0.00	0.75	1.254	o	|	|	|	|	2.63
18.583	0.00	0.75	1.249	o	|	|	|	|	2.62
18.667	0.00	0.74	1.244	o	|	|	|	|	2.61
18.750	0.00	0.74	1.239	o	|	|	|	|	2.61
18.833	0.00	0.73	1.234	o	|	|	|	|	2.60
18.917	0.00	0.72	1.229	o	|	|	|	|	2.59
19.000	0.00	0.72	1.224	o	|	|	|	|	2.58
19.083	0.00	0.71	1.219	o	|	|	|	|	2.57
19.167	0.00	0.71	1.214	o	|	|	|	|	2.56
19.250	0.00	0.70	1.209	o	|	|	|	|	2.55
19.333	0.00	0.69	1.205	o	|	|	|	|	2.54
19.417	0.00	0.69	1.200	o	|	|	|	|	2.53
19.500	0.00	0.68	1.195	o	|	|	|	|	2.52
19.583	0.00	0.68	1.190	o	|	|	|	|	2.51
19.667	0.00	0.67	1.186	o	|	|	|	|	2.51
19.750	0.00	0.67	1.181	o	|	|	|	|	2.50
19.833	0.00	0.66	1.177	o	|	|	|	|	2.49
19.917	0.00	0.66	1.172	o	|	|	|	|	2.48
20.000	0.00	0.65	1.168	o	|	|	|	|	2.47
20.083	0.00	0.64	1.163	o	|	|	|	|	2.46
20.167	0.00	0.64	1.159	o	|	|	|	|	2.46
20.250	0.00	0.63	1.154	o	|	|	|	|	2.45
20.333	0.00	0.63	1.150	o	|	|	|	|	2.44
20.417	0.00	0.62	1.146	o	|	|	|	|	2.43
20.500	0.00	0.62	1.141	o	|	|	|	|	2.42
20.583	0.00	0.61	1.137	o	|	|	|	|	2.42
20.667	0.00	0.61	1.133	o	|	|	|	|	2.41
20.750	0.00	0.60	1.129	o	|	|	|	|	2.40
20.833	0.00	0.60	1.125	o	|	|	|	|	2.39
20.917	0.00	0.59	1.121	o	|	|	|	|	2.38
21.000	0.00	0.59	1.117	o	|	|	|	|	2.38
21.083	0.00	0.58	1.113	o	|	|	|	|	2.37
21.167	0.00	0.58	1.109	o	|	|	|	|	2.36
21.250	0.00	0.57	1.105	o	|	|	|	|	2.35
21.333	0.00	0.57	1.101	o	|	|	|	|	2.35
21.417	0.00	0.56	1.097	o	|	|	|	|	2.34
21.500	0.00	0.56	1.093	o	|	|	|	|	2.33
21.583	0.00	0.55	1.089	o	|	|	|	|	2.33
21.667	0.00	0.55	1.085	o	|	|	|	|	2.32
21.750	0.00	0.55	1.081	o	|	|	|	|	2.31
21.833	0.00	0.54	1.078	o	|	|	|	|	2.30
21.917	0.00	0.54	1.074	o	|	|	|	|	2.30
22.000	0.00	0.53	1.070	o	|	|	|	|	2.29
22.083	0.00	0.53	1.067	o	|	|	|	|	2.28
22.167	0.00	0.52	1.063	o	|	|	|	|	2.28
22.250	0.00	0.52	1.059	o	|	|	|	|	2.27
22.333	0.00	0.51	1.056	o	|	|	|	|	2.26
22.417	0.00	0.51	1.052	o	|	|	|	|	2.26
22.500	0.00	0.51	1.049	o	|	|	|	|	2.25
22.583	0.00	0.50	1.045	o	|	|	|	|	2.24
22.667	0.00	0.50	1.042	o	|	|	|	|	2.24
22.750	0.00	0.49	1.038	o	|	|	|	|	2.23
22.833	0.00	0.49	1.035	o	|	|	|	|	2.23
22.917	0.00	0.49	1.032	o	|	|	|	|	2.22
23.000	0.00	0.48	1.028	o	|	|	|	|	2.21

23.083	0.00	0.48	1.025	o	|	|	|	|	2.21
23.167	0.00	0.47	1.022	o	|	|	|	|	2.20
23.250	0.00	0.47	1.019	o	|	|	|	|	2.19
23.333	0.00	0.47	1.015	o	|	|	|	|	2.19
23.417	0.00	0.46	1.012	o	|	|	|	|	2.18
23.500	0.00	0.46	1.009	o	|	|	|	|	2.18
23.583	0.00	0.45	1.006	o	|	|	|	|	2.17
23.667	0.00	0.45	1.003	o	|	|	|	|	2.17
23.750	0.00	0.45	1.000	o	|	|	|	|	2.16
23.833	0.00	0.44	0.997	o	|	|	|	|	2.15
23.917	0.00	0.44	0.994	o	|	|	|	|	2.15
24.000	0.00	0.44	0.991	o	|	|	|	|	2.14
24.083	0.00	0.43	0.988	o	|	|	|	|	2.14
24.167	0.00	0.43	0.985	o	|	|	|	|	2.13
24.250	0.00	0.43	0.982	o	|	|	|	|	2.13
24.333	0.00	0.42	0.979	o	|	|	|	|	2.12
24.417	0.00	0.42	0.976	o	|	|	|	|	2.12
24.500	0.00	0.41	0.973	o	|	|	|	|	2.11
24.583	0.00	0.41	0.970	o	|	|	|	|	2.10
24.667	0.00	0.41	0.967	o	|	|	|	|	2.10
24.750	0.00	0.40	0.964	o	|	|	|	|	2.09
24.833	0.00	0.40	0.962	o	|	|	|	|	2.09
24.917	0.00	0.40	0.959	o	|	|	|	|	2.08
25.000	0.00	0.39	0.956	o	|	|	|	|	2.08
25.083	0.00	0.39	0.953	o	|	|	|	|	2.07
25.167	0.00	0.39	0.951	o	|	|	|	|	2.07
25.250	0.00	0.39	0.948	o	|	|	|	|	2.06
25.333	0.00	0.38	0.945	o	|	|	|	|	2.06
25.417	0.00	0.38	0.943	o	|	|	|	|	2.05
25.500	0.00	0.38	0.940	o	|	|	|	|	2.05
25.583	0.00	0.37	0.938	o	|	|	|	|	2.04
25.667	0.00	0.37	0.935	o	|	|	|	|	2.04
25.750	0.00	0.37	0.933	o	|	|	|	|	2.03
25.833	0.00	0.36	0.930	o	|	|	|	|	2.03
25.917	0.00	0.36	0.928	o	|	|	|	|	2.03
26.000	0.00	0.36	0.925	o	|	|	|	|	2.02
26.083	0.00	0.35	0.923	o	|	|	|	|	2.02
26.167	0.00	0.35	0.920	o	|	|	|	|	2.01
26.250	0.00	0.35	0.918	o	|	|	|	|	2.01
26.333	0.00	0.35	0.915	o	|	|	|	|	2.00
26.417	0.00	0.34	0.913	o	|	|	|	|	2.00
26.500	0.00	0.34	0.911	o	|	|	|	|	1.99
26.583	0.00	0.34	0.908	o	|	|	|	|	1.99
26.667	0.00	0.34	0.906	o	|	|	|	|	1.98
26.750	0.00	0.34	0.904	o	|	|	|	|	1.98
26.833	0.00	0.34	0.901	o	|	|	|	|	1.97
26.917	0.00	0.34	0.899	o	|	|	|	|	1.97
27.000	0.00	0.34	0.897	o	|	|	|	|	1.96
27.083	0.00	0.34	0.894	o	|	|	|	|	1.96
27.167	0.00	0.34	0.892	o	|	|	|	|	1.95
27.250	0.00	0.34	0.890	o	|	|	|	|	1.95
27.333	0.00	0.34	0.887	o	|	|	|	|	1.94
27.417	0.00	0.34	0.885	o	|	|	|	|	1.94
27.500	0.00	0.34	0.883	o	|	|	|	|	1.94
27.583	0.00	0.34	0.880	o	|	|	|	|	1.93
27.667	0.00	0.34	0.878	o	|	|	|	|	1.93
27.750	0.00	0.33	0.876	o	|	|	|	|	1.92
27.833	0.00	0.33	0.873	o	|	|	|	|	1.92
27.917	0.00	0.33	0.871	o	|	|	|	|	1.91
28.000	0.00	0.33	0.869	o	|	|	|	|	1.91
28.083	0.00	0.33	0.867	o	|	|	|	|	1.90
28.167	0.00	0.33	0.864	o	|	|	|	|	1.90
28.250	0.00	0.33	0.862	o	|	|	|	|	1.89
28.333	0.00	0.33	0.860	o	|	|	|	|	1.89
28.417	0.00	0.33	0.857	o	|	|	|	|	1.88
28.500	0.00	0.33	0.855	o	|	|	|	|	1.88
28.583	0.00	0.33	0.853	o	|	|	|	|	1.87
28.667	0.00	0.33	0.851	o	|	|	|	|	1.87
28.750	0.00	0.33	0.848	o	|	|	|	|	1.86
28.833	0.00	0.33	0.846	o	|	|	|	|	1.86
28.917	0.00	0.33	0.844	o	|	|	|	|	1.85
29.000	0.00	0.33	0.842	o	|	|	|	|	1.85
29.083	0.00	0.33	0.839	o	|	|	|	|	1.85
29.167	0.00	0.33	0.837	o	|	|	|	|	1.84
29.250	0.00	0.32	0.835	o	|	|	|	|	1.84
29.333	0.00	0.32	0.833	o	|	|	|	|	1.83
29.417	0.00	0.32	0.830	o	|	|	|	|	1.83
29.500	0.00	0.32	0.828	o	|	|	|	|	1.82
29.583	0.00	0.32	0.826	o	|	|	|	|	1.82
29.667	0.00	0.32	0.824	o	|	|	|	|	1.81
29.750	0.00	0.32	0.822	o	|	|	|	|	1.81
29.833	0.00	0.32	0.819	o	|	|	|	|	1.80
29.917	0.00	0.32	0.817	o	|	|	|	|	1.80
30.000	0.00	0.32	0.815	o	|	|	|	|	1.79
30.083	0.00	0.32	0.813	o	|	|	|	|	1.79
30.167	0.00	0.32	0.811	o	|	|	|	|	1.79

30.250	0.00	0.32	0.808	o	|	|	|	|	1.78
30.333	0.00	0.32	0.806	o	|	|	|	|	1.78
30.417	0.00	0.32	0.804	o	|	|	|	|	1.77
30.500	0.00	0.32	0.802	o	|	|	|	|	1.77
30.583	0.00	0.32	0.800	o	|	|	|	|	1.76
30.667	0.00	0.32	0.797	o	|	|	|	|	1.76
30.750	0.00	0.31	0.795	o	|	|	|	|	1.75
30.833	0.00	0.31	0.793	o	|	|	|	|	1.75
30.917	0.00	0.31	0.791	o	|	|	|	|	1.75
31.000	0.00	0.31	0.789	o	|	|	|	|	1.74
31.083	0.00	0.31	0.787	o	|	|	|	|	1.74
31.167	0.00	0.31	0.784	o	|	|	|	|	1.73
31.250	0.00	0.31	0.782	o	|	|	|	|	1.73
31.333	0.00	0.31	0.780	o	|	|	|	|	1.72
31.417	0.00	0.31	0.778	o	|	|	|	|	1.72
31.500	0.00	0.31	0.776	o	|	|	|	|	1.71
31.583	0.00	0.31	0.774	o	|	|	|	|	1.71
31.667	0.00	0.31	0.772	o	|	|	|	|	1.71
31.750	0.00	0.31	0.769	o	|	|	|	|	1.70
31.833	0.00	0.31	0.767	o	|	|	|	|	1.70
31.917	0.00	0.31	0.765	o	|	|	|	|	1.69
32.000	0.00	0.31	0.763	o	|	|	|	|	1.69
32.083	0.00	0.31	0.761	o	|	|	|	|	1.68
32.167	0.00	0.31	0.759	o	|	|	|	|	1.68
32.250	0.00	0.31	0.757	o	|	|	|	|	1.67
32.333	0.00	0.30	0.755	o	|	|	|	|	1.67
32.417	0.00	0.30	0.753	o	|	|	|	|	1.67
32.500	0.00	0.30	0.751	o	|	|	|	|	1.66
32.583	0.00	0.30	0.748	o	|	|	|	|	1.66
32.667	0.00	0.30	0.746	o	|	|	|	|	1.65
32.750	0.00	0.30	0.744	o	|	|	|	|	1.65
32.833	0.00	0.30	0.742	o	|	|	|	|	1.64
32.917	0.00	0.30	0.740	o	|	|	|	|	1.64
33.000	0.00	0.30	0.738	o	|	|	|	|	1.64
33.083	0.00	0.30	0.736	o	|	|	|	|	1.63
33.167	0.00	0.30	0.734	o	|	|	|	|	1.63
33.250	0.00	0.30	0.732	o	|	|	|	|	1.62
33.333	0.00	0.30	0.730	o	|	|	|	|	1.62
33.417	0.00	0.30	0.728	o	|	|	|	|	1.61
33.500	0.00	0.30	0.726	o	|	|	|	|	1.61
33.583	0.00	0.30	0.724	o	|	|	|	|	1.61
33.667	0.00	0.30	0.722	o	|	|	|	|	1.60
33.750	0.00	0.30	0.720	o	|	|	|	|	1.60
33.833	0.00	0.30	0.718	o	|	|	|	|	1.59
33.917	0.00	0.30	0.715	o	|	|	|	|	1.59
34.000	0.00	0.29	0.713	o	|	|	|	|	1.58
34.083	0.00	0.29	0.711	o	|	|	|	|	1.58
34.167	0.00	0.29	0.709	o	|	|	|	|	1.58
34.250	0.00	0.29	0.707	o	|	|	|	|	1.57
34.333	0.00	0.29	0.705	o	|	|	|	|	1.57
34.417	0.00	0.29	0.703	o	|	|	|	|	1.56
34.500	0.00	0.29	0.701	o	|	|	|	|	1.56
34.583	0.00	0.29	0.699	o	|	|	|	|	1.56
34.667	0.00	0.29	0.697	o	|	|	|	|	1.55
34.750	0.00	0.29	0.695	o	|	|	|	|	1.55
34.833	0.00	0.29	0.693	o	|	|	|	|	1.54
34.917	0.00	0.29	0.691	o	|	|	|	|	1.54
35.000	0.00	0.29	0.689	o	|	|	|	|	1.53
35.083	0.00	0.29	0.687	o	|	|	|	|	1.53
35.167	0.00	0.29	0.685	o	|	|	|	|	1.53
35.250	0.00	0.29	0.683	o	|	|	|	|	1.52
35.333	0.00	0.29	0.681	o	|	|	|	|	1.52
35.417	0.00	0.29	0.679	o	|	|	|	|	1.51
35.500	0.00	0.29	0.677	o	|	|	|	|	1.51
35.583	0.00	0.29	0.676	o	|	|	|	|	1.51
35.667	0.00	0.28	0.674	o	|	|	|	|	1.50
35.750	0.00	0.28	0.672	o	|	|	|	|	1.50
35.833	0.00	0.28	0.670	o	|	|	|	|	1.49
35.917	0.00	0.28	0.668	o	|	|	|	|	1.49
36.000	0.00	0.28	0.666	o	|	|	|	|	1.49
36.083	0.00	0.28	0.664	o	|	|	|	|	1.48
36.167	0.00	0.28	0.662	o	|	|	|	|	1.48
36.250	0.00	0.28	0.660	o	|	|	|	|	1.47
36.333	0.00	0.28	0.658	o	|	|	|	|	1.47
36.417	0.00	0.28	0.656	o	|	|	|	|	1.47
36.500	0.00	0.28	0.654	o	|	|	|	|	1.46
36.583	0.00	0.28	0.652	o	|	|	|	|	1.46
36.667	0.00	0.28	0.650	o	|	|	|	|	1.45
36.750	0.00	0.28	0.648	o	|	|	|	|	1.45
36.833	0.00	0.28	0.646	o	|	|	|	|	1.45
36.917	0.00	0.28	0.644	o	|	|	|	|	1.44
37.000	0.00	0.28	0.643	o	|	|	|	|	1.44
37.083	0.00	0.28	0.641	o	|	|	|	|	1.43
37.167	0.00	0.28	0.639	o	|	|	|	|	1.43
37.250	0.00	0.28	0.637	o	|	|	|	|	1.43
37.333	0.00	0.28	0.635	o	|	|	|	|	1.42

37.417	0.00	0.27	0.633	o	|	|	|	|	1.42
37.500	0.00	0.27	0.631	o	|	|	|	|	1.41
37.583	0.00	0.27	0.629	o	|	|	|	|	1.41
37.667	0.00	0.27	0.627	o	|	|	|	|	1.41
37.750	0.00	0.27	0.626	o	|	|	|	|	1.40
37.833	0.00	0.27	0.624	o	|	|	|	|	1.40
37.917	0.00	0.27	0.622	o	|	|	|	|	1.40
38.000	0.00	0.27	0.620	o	|	|	|	|	1.39
38.083	0.00	0.27	0.618	o	|	|	|	|	1.39
38.167	0.00	0.27	0.616	o	|	|	|	|	1.38
38.250	0.00	0.27	0.614	o	|	|	|	|	1.38
38.333	0.00	0.27	0.612	o	|	|	|	|	1.38
38.417	0.00	0.27	0.611	o	|	|	|	|	1.37
38.500	0.00	0.27	0.609	o	|	|	|	|	1.37
38.583	0.00	0.27	0.607	o	|	|	|	|	1.36
38.667	0.00	0.27	0.605	o	|	|	|	|	1.36
38.750	0.00	0.27	0.603	o	|	|	|	|	1.36
38.833	0.00	0.27	0.601	o	|	|	|	|	1.35
38.917	0.00	0.27	0.600	o	|	|	|	|	1.35
39.000	0.00	0.27	0.598	o	|	|	|	|	1.35
39.083	0.00	0.27	0.596	o	|	|	|	|	1.34
39.167	0.00	0.27	0.594	o	|	|	|	|	1.34
39.250	0.00	0.26	0.592	o	|	|	|	|	1.33
39.333	0.00	0.26	0.590	o	|	|	|	|	1.33
39.417	0.00	0.26	0.589	o	|	|	|	|	1.33
39.500	0.00	0.26	0.587	o	|	|	|	|	1.32
39.583	0.00	0.26	0.585	o	|	|	|	|	1.32
39.667	0.00	0.26	0.583	o	|	|	|	|	1.31
39.750	0.00	0.26	0.581	o	|	|	|	|	1.31
39.833	0.00	0.26	0.580	o	|	|	|	|	1.31
39.917	0.00	0.26	0.578	o	|	|	|	|	1.30
40.000	0.00	0.26	0.576	o	|	|	|	|	1.30
40.083	0.00	0.26	0.574	o	|	|	|	|	1.30
40.167	0.00	0.26	0.572	o	|	|	|	|	1.29
40.250	0.00	0.26	0.571	o	|	|	|	|	1.29
40.333	0.00	0.26	0.569	o	|	|	|	|	1.29
40.417	0.00	0.26	0.567	o	|	|	|	|	1.28
40.500	0.00	0.26	0.565	o	|	|	|	|	1.28
40.583	0.00	0.26	0.563	o	|	|	|	|	1.27
40.667	0.00	0.26	0.562	o	|	|	|	|	1.27
40.750	0.00	0.26	0.560	o	|	|	|	|	1.27
40.833	0.00	0.26	0.558	o	|	|	|	|	1.26
40.917	0.00	0.26	0.556	o	|	|	|	|	1.26
41.000	0.00	0.26	0.555	o	|	|	|	|	1.26
41.083	0.00	0.26	0.553	o	|	|	|	|	1.25
41.167	0.00	0.25	0.551	o	|	|	|	|	1.25
41.250	0.00	0.25	0.549	o	|	|	|	|	1.25
41.333	0.00	0.25	0.548	o	|	|	|	|	1.24
41.417	0.00	0.25	0.546	o	|	|	|	|	1.24
41.500	0.00	0.25	0.544	o	|	|	|	|	1.23
41.583	0.00	0.25	0.542	o	|	|	|	|	1.23
41.667	0.00	0.25	0.541	o	|	|	|	|	1.23
41.750	0.00	0.25	0.539	o	|	|	|	|	1.22
41.833	0.00	0.25	0.537	o	|	|	|	|	1.22
41.917	0.00	0.25	0.535	o	|	|	|	|	1.22
42.000	0.00	0.25	0.534	o	|	|	|	|	1.21
42.083	0.00	0.25	0.532	o	|	|	|	|	1.21
42.167	0.00	0.25	0.530	o	|	|	|	|	1.21
42.250	0.00	0.25	0.529	o	|	|	|	|	1.20
42.333	0.00	0.25	0.527	o	|	|	|	|	1.20
42.417	0.00	0.25	0.525	o	|	|	|	|	1.19
42.500	0.00	0.25	0.523	o	|	|	|	|	1.19
42.583	0.00	0.25	0.522	o	|	|	|	|	1.19
42.667	0.00	0.25	0.520	o	|	|	|	|	1.18
42.750	0.00	0.25	0.518	o	|	|	|	|	1.18
42.833	0.00	0.25	0.517	o	|	|	|	|	1.18
42.917	0.00	0.25	0.515	o	|	|	|	|	1.17
43.000	0.00	0.25	0.513	o	|	|	|	|	1.17
43.083	0.00	0.24	0.512	o	|	|	|	|	1.17
43.167	0.00	0.24	0.510	o	|	|	|	|	1.16
43.250	0.00	0.24	0.508	o	|	|	|	|	1.16
43.333	0.00	0.24	0.506	o	|	|	|	|	1.16
43.417	0.00	0.24	0.505	o	|	|	|	|	1.15
43.500	0.00	0.24	0.503	o	|	|	|	|	1.15
43.583	0.00	0.24	0.501	o	|	|	|	|	1.15
43.667	0.00	0.24	0.500	o	|	|	|	|	1.14
43.750	0.00	0.24	0.498	o	|	|	|	|	1.14
43.833	0.00	0.24	0.496	o	|	|	|	|	1.14
43.917	0.00	0.24	0.495	o	|	|	|	|	1.13
44.000	0.00	0.24	0.493	o	|	|	|	|	1.13
44.083	0.00	0.24	0.492	o	|	|	|	|	1.13
44.167	0.00	0.24	0.490	o	|	|	|	|	1.12
44.250	0.00	0.24	0.488	o	|	|	|	|	1.12
44.333	0.00	0.24	0.487	o	|	|	|	|	1.12
44.417	0.00	0.24	0.485	o	|	|	|	|	1.11
44.500	0.00	0.24	0.483	o	|	|	|	|	1.11

44.583	0.00	0.24	0.482	o	|	|	|	|	1.10
44.667	0.00	0.24	0.480	o	|	|	|	|	1.10
44.750	0.00	0.24	0.478	o	|	|	|	|	1.10
44.833	0.00	0.24	0.477	o	|	|	|	|	1.09
44.917	0.00	0.24	0.475	o	|	|	|	|	1.09
45.000	0.00	0.24	0.474	o	|	|	|	|	1.09
45.083	0.00	0.24	0.472	o	|	|	|	|	1.08
45.167	0.00	0.23	0.470	o	|	|	|	|	1.08
45.250	0.00	0.23	0.469	o	|	|	|	|	1.08
45.333	0.00	0.23	0.467	o	|	|	|	|	1.07
45.417	0.00	0.23	0.465	o	|	|	|	|	1.07
45.500	0.00	0.23	0.464	o	|	|	|	|	1.07
45.583	0.00	0.23	0.462	o	|	|	|	|	1.06
45.667	0.00	0.23	0.461	o	|	|	|	|	1.06
45.750	0.00	0.23	0.459	o	|	|	|	|	1.06
45.833	0.00	0.23	0.457	o	|	|	|	|	1.05
45.917	0.00	0.23	0.456	o	|	|	|	|	1.05
46.000	0.00	0.23	0.454	o	|	|	|	|	1.05
46.083	0.00	0.23	0.453	o	|	|	|	|	1.04
46.167	0.00	0.23	0.451	o	|	|	|	|	1.04
46.250	0.00	0.23	0.449	o	|	|	|	|	1.04
46.333	0.00	0.23	0.448	o	|	|	|	|	1.04
46.417	0.00	0.23	0.446	o	|	|	|	|	1.03
46.500	0.00	0.23	0.445	o	|	|	|	|	1.03
46.583	0.00	0.23	0.443	o	|	|	|	|	1.03
46.667	0.00	0.23	0.442	o	|	|	|	|	1.02
46.750	0.00	0.23	0.440	o	|	|	|	|	1.02
46.833	0.00	0.23	0.438	o	|	|	|	|	1.02
46.917	0.00	0.23	0.437	o	|	|	|	|	1.01
47.000	0.00	0.23	0.435	o	|	|	|	|	1.01
47.083	0.00	0.23	0.434	o	|	|	|	|	1.01
47.167	0.00	0.23	0.432	o	|	|	|	|	1.00
47.250	0.00	0.22	0.431	o	|	|	|	|	1.00
47.333	0.00	0.22	0.429	o	|	|	|	|	1.00
47.417	0.00	0.22	0.428	o	|	|	|	|	0.99
47.500	0.00	0.22	0.426	o	|	|	|	|	0.99
47.583	0.00	0.22	0.425	o	|	|	|	|	0.99
47.667	0.00	0.22	0.423	o	|	|	|	|	0.98
47.750	0.00	0.22	0.422	o	|	|	|	|	0.98
47.833	0.00	0.22	0.420	o	|	|	|	|	0.97
47.917	0.00	0.22	0.418	o	|	|	|	|	0.97
48.000	0.00	0.22	0.417	o	|	|	|	|	0.97
48.083	0.00	0.22	0.415	o	|	|	|	|	0.96
48.167	0.00	0.22	0.414	o	|	|	|	|	0.96
48.250	0.00	0.22	0.413	o	|	|	|	|	0.96
48.333	0.00	0.21	0.411	o	|	|	|	|	0.95
48.417	0.00	0.21	0.410	o	|	|	|	|	0.95
48.500	0.00	0.21	0.408	o	|	|	|	|	0.95
48.583	0.00	0.21	0.407	o	|	|	|	|	0.94
48.667	0.00	0.21	0.405	o	|	|	|	|	0.94
48.750	0.00	0.21	0.404	o	|	|	|	|	0.94
48.833	0.00	0.21	0.402	o	|	|	|	|	0.93
48.917	0.00	0.21	0.401	o	|	|	|	|	0.93
49.000	0.00	0.21	0.399	o	|	|	|	|	0.93
49.083	0.00	0.21	0.398	o	|	|	|	|	0.92
49.167	0.00	0.21	0.397	o	|	|	|	|	0.92
49.250	0.00	0.21	0.395	o	|	|	|	|	0.92
49.333	0.00	0.21	0.394	o	|	|	|	|	0.91
49.417	0.00	0.20	0.392	o	|	|	|	|	0.91
49.500	0.00	0.20	0.391	o	|	|	|	|	0.91
49.583	0.00	0.20	0.389	o	|	|	|	|	0.90
49.667	0.00	0.20	0.388	o	|	|	|	|	0.90
49.750	0.00	0.20	0.387	o	|	|	|	|	0.90
49.833	0.00	0.20	0.385	o	|	|	|	|	0.89
49.917	0.00	0.20	0.384	o	|	|	|	|	0.89
50.000	0.00	0.20	0.383	o	|	|	|	|	0.89
50.083	0.00	0.20	0.381	o	|	|	|	|	0.88
50.167	0.00	0.20	0.380	o	|	|	|	|	0.88
50.250	0.00	0.20	0.378	o	|	|	|	|	0.88
50.333	0.00	0.20	0.377	o	|	|	|	|	0.87
50.417	0.00	0.20	0.376	o	|	|	|	|	0.87
50.500	0.00	0.20	0.374	o	|	|	|	|	0.87
50.583	0.00	0.19	0.373	o	|	|	|	|	0.87
50.667	0.00	0.19	0.372	o	|	|	|	|	0.86
50.750	0.00	0.19	0.370	o	|	|	|	|	0.86
50.833	0.00	0.19	0.369	o	|	|	|	|	0.86
50.917	0.00	0.19	0.368	o	|	|	|	|	0.85
51.000	0.00	0.19	0.366	o	|	|	|	|	0.85
51.083	0.00	0.19	0.365	o	|	|	|	|	0.85
51.167	0.00	0.19	0.364	o	|	|	|	|	0.84
51.250	0.00	0.19	0.362	o	|	|	|	|	0.84
51.333	0.00	0.19	0.361	o	|	|	|	|	0.84
51.417	0.00	0.19	0.360	o	|	|	|	|	0.83
51.500	0.00	0.19	0.359	o	|	|	|	|	0.83
51.583	0.00	0.19	0.357	o	|	|	|	|	0.83
51.667	0.00	0.19	0.356	o	|	|	|	|	0.83

51.750	0.00	0.19	0.355	o	|	|	|	0.82
51.833	0.00	0.18	0.353	o	|	|	|	0.82
51.917	0.00	0.18	0.352	o	|	|	|	0.82
52.000	0.00	0.18	0.351	o	|	|	|	0.81
52.083	0.00	0.18	0.350	o	|	|	|	0.81
52.167	0.00	0.18	0.348	o	|	|	|	0.81
52.250	0.00	0.18	0.347	o	|	|	|	0.81
52.333	0.00	0.18	0.346	o	|	|	|	0.80
52.417	0.00	0.18	0.345	o	|	|	|	0.80
52.500	0.00	0.18	0.343	o	|	|	|	0.80
52.583	0.00	0.18	0.342	o	|	|	|	0.79
52.667	0.00	0.18	0.341	o	|	|	|	0.79
52.750	0.00	0.18	0.340	o	|	|	|	0.79
52.833	0.00	0.18	0.339	o	|	|	|	0.79
52.917	0.00	0.18	0.337	o	|	|	|	0.78
53.000	0.00	0.18	0.336	o	|	|	|	0.78
53.083	0.00	0.17	0.335	o	|	|	|	0.78
53.167	0.00	0.17	0.334	o	|	|	|	0.77
53.250	0.00	0.17	0.332	o	|	|	|	0.77
53.333	0.00	0.17	0.331	o	|	|	|	0.77
53.417	0.00	0.17	0.330	o	|	|	|	0.77
53.500	0.00	0.17	0.329	o	|	|	|	0.76
53.583	0.00	0.17	0.328	o	|	|	|	0.76
53.667	0.00	0.17	0.327	o	|	|	|	0.76
53.750	0.00	0.17	0.325	o	|	|	|	0.75
53.833	0.00	0.17	0.324	o	|	|	|	0.75
53.917	0.00	0.17	0.323	o	|	|	|	0.75
54.000	0.00	0.17	0.322	o	|	|	|	0.75
54.083	0.00	0.17	0.321	o	|	|	|	0.74
54.167	0.00	0.17	0.320	o	|	|	|	0.74
54.250	0.00	0.17	0.318	o	|	|	|	0.74
54.333	0.00	0.17	0.317	o	|	|	|	0.74
54.417	0.00	0.17	0.316	o	|	|	|	0.73
54.500	0.00	0.16	0.315	o	|	|	|	0.73
54.583	0.00	0.16	0.314	o	|	|	|	0.73
54.667	0.00	0.16	0.313	o	|	|	|	0.73
54.750	0.00	0.16	0.312	o	|	|	|	0.72
54.833	0.00	0.16	0.311	o	|	|	|	0.72
54.917	0.00	0.16	0.309	o	|	|	|	0.72
55.000	0.00	0.16	0.308	o	|	|	|	0.72
55.083	0.00	0.16	0.307	o	|	|	|	0.71
55.167	0.00	0.16	0.306	o	|	|	|	0.71
55.250	0.00	0.16	0.305	o	|	|	|	0.71
55.333	0.00	0.16	0.304	o	|	|	|	0.71
55.417	0.00	0.16	0.303	o	|	|	|	0.70
55.500	0.00	0.16	0.302	o	|	|	|	0.70
55.583	0.00	0.16	0.301	o	|	|	|	0.70
55.667	0.00	0.16	0.300	o	|	|	|	0.70
55.750	0.00	0.16	0.298	o	|	|	|	0.69
55.833	0.00	0.16	0.297	o	|	|	|	0.69
55.917	0.00	0.15	0.296	o	|	|	|	0.69
56.000	0.00	0.15	0.295	o	|	|	|	0.69
56.083	0.00	0.15	0.294	o	|	|	|	0.68
56.167	0.00	0.15	0.293	o	|	|	|	0.68
56.250	0.00	0.15	0.292	o	|	|	|	0.68
56.333	0.00	0.15	0.291	o	|	|	|	0.68
56.417	0.00	0.15	0.290	o	|	|	|	0.67
56.500	0.00	0.15	0.289	o	|	|	|	0.67
56.583	0.00	0.15	0.288	o	|	|	|	0.67
56.667	0.00	0.15	0.287	o	|	|	|	0.67
56.750	0.00	0.15	0.286	o	|	|	|	0.66
56.833	0.00	0.15	0.285	o	|	|	|	0.66
56.917	0.00	0.15	0.284	o	|	|	|	0.66
57.000	0.00	0.15	0.283	o	|	|	|	0.66
57.083	0.00	0.15	0.282	o	|	|	|	0.65
57.167	0.00	0.15	0.281	o	|	|	|	0.65
57.250	0.00	0.15	0.280	o	|	|	|	0.65
57.333	0.00	0.15	0.279	o	|	|	|	0.65
57.417	0.00	0.15	0.278	o	|	|	|	0.64
57.500	0.00	0.14	0.277	o	|	|	|	0.64
57.583	0.00	0.14	0.276	o	|	|	|	0.64
57.667	0.00	0.14	0.275	o	|	|	|	0.64
57.750	0.00	0.14	0.274	o	|	|	|	0.64
57.833	0.00	0.14	0.273	o	|	|	|	0.63
57.917	0.00	0.14	0.272	o	|	|	|	0.63
58.000	0.00	0.14	0.271	o	|	|	|	0.63
58.083	0.00	0.14	0.270	o	|	|	|	0.63
58.167	0.00	0.14	0.269	o	|	|	|	0.62
58.250	0.00	0.14	0.268	o	|	|	|	0.62
58.333	0.00	0.14	0.267	o	|	|	|	0.62
58.417	0.00	0.14	0.266	o	|	|	|	0.62
58.500	0.00	0.14	0.265	o	|	|	|	0.62
58.583	0.00	0.14	0.264	o	|	|	|	0.61
58.667	0.00	0.14	0.263	o	|	|	|	0.61
58.750	0.00	0.14	0.262	o	|	|	|	0.61
58.833	0.00	0.14	0.261	o	|	|	|	0.61

58.917	0.00	0.14	0.260	o	|	|	|	0.60
59.000	0.00	0.14	0.259	o	|	|	|	0.60
59.083	0.00	0.13	0.258	o	|	|	|	0.60
59.167	0.00	0.13	0.258	o	|	|	|	0.60
59.250	0.00	0.13	0.257	o	|	|	|	0.60
59.333	0.00	0.13	0.256	o	|	|	|	0.59
59.417	0.00	0.13	0.255	o	|	|	|	0.59
59.500	0.00	0.13	0.254	o	|	|	|	0.59
59.583	0.00	0.13	0.253	o	|	|	|	0.59
59.667	0.00	0.13	0.252	o	|	|	|	0.58
59.750	0.00	0.13	0.251	o	|	|	|	0.58
59.833	0.00	0.13	0.250	o	|	|	|	0.58
59.917	0.00	0.13	0.249	o	|	|	|	0.58
60.000	0.00	0.13	0.248	o	|	|	|	0.58
60.083	0.00	0.13	0.248	o	|	|	|	0.57
60.167	0.00	0.13	0.247	o	|	|	|	0.57
60.250	0.00	0.13	0.246	o	|	|	|	0.57
60.333	0.00	0.13	0.245	o	|	|	|	0.57
60.417	0.00	0.13	0.244	o	|	|	|	0.57
60.500	0.00	0.13	0.243	o	|	|	|	0.56
60.583	0.00	0.13	0.242	o	|	|	|	0.56
60.667	0.00	0.13	0.241	o	|	|	|	0.56
60.750	0.00	0.13	0.241	o	|	|	|	0.56
60.833	0.00	0.13	0.240	o	|	|	|	0.56
60.917	0.00	0.12	0.239	o	|	|	|	0.55
61.000	0.00	0.12	0.238	o	|	|	|	0.55
61.083	0.00	0.12	0.237	o	|	|	|	0.55
61.167	0.00	0.12	0.236	o	|	|	|	0.55
61.250	0.00	0.12	0.235	o	|	|	|	0.55
61.333	0.00	0.12	0.235	o	|	|	|	0.54
61.417	0.00	0.12	0.234	o	|	|	|	0.54
61.500	0.00	0.12	0.233	o	|	|	|	0.54
61.583	0.00	0.12	0.232	o	|	|	|	0.54
61.667	0.00	0.12	0.231	o	|	|	|	0.54
61.750	0.00	0.12	0.230	o	|	|	|	0.53
61.833	0.00	0.12	0.230	o	|	|	|	0.53
61.917	0.00	0.12	0.229	o	|	|	|	0.53
62.000	0.00	0.12	0.228	o	|	|	|	0.53
62.083	0.00	0.12	0.227	o	|	|	|	0.53
62.167	0.00	0.12	0.226	o	|	|	|	0.53
62.250	0.00	0.12	0.225	o	|	|	|	0.52
62.333	0.00	0.12	0.225	o	|	|	|	0.52
62.417	0.00	0.12	0.224	o	|	|	|	0.52
62.500	0.00	0.12	0.223	o	|	|	|	0.52
62.583	0.00	0.12	0.222	o	|	|	|	0.52
62.667	0.00	0.12	0.221	o	|	|	|	0.51
62.750	0.00	0.12	0.221	o	|	|	|	0.51
62.833	0.00	0.11	0.220	o	|	|	|	0.51
62.917	0.00	0.11	0.219	o	|	|	|	0.51
63.000	0.00	0.11	0.218	o	|	|	|	0.51
63.083	0.00	0.11	0.218	o	|	|	|	0.50
63.167	0.00	0.11	0.217	o	|	|	|	0.50
63.250	0.00	0.11	0.216	o	|	|	|	0.50
63.333	0.00	0.11	0.215	o	|	|	|	0.50
63.417	0.00	0.11	0.214	o	|	|	|	0.50
63.500	0.00	0.11	0.214	o	|	|	|	0.50
63.583	0.00	0.11	0.213	o	|	|	|	0.49
63.667	0.00	0.11	0.212	o	|	|	|	0.49
63.750	0.00	0.11	0.211	o	|	|	|	0.49
63.833	0.00	0.11	0.211	o	|	|	|	0.49
63.917	0.00	0.11	0.210	o	|	|	|	0.49
64.000	0.00	0.11	0.209	o	|	|	|	0.49
64.083	0.00	0.11	0.208	o	|	|	|	0.48
64.167	0.00	0.11	0.208	o	|	|	|	0.48
64.250	0.00	0.11	0.207	o	|	|	|	0.48
64.333	0.00	0.11	0.206	o	|	|	|	0.48
64.417	0.00	0.11	0.205	o	|	|	|	0.48
64.500	0.00	0.11	0.205	o	|	|	|	0.47
64.583	0.00	0.11	0.204	o	|	|	|	0.47
64.667	0.00	0.11	0.203	o	|	|	|	0.47
64.750	0.00	0.11	0.202	o	|	|	|	0.47
64.833	0.00	0.11	0.202	o	|	|	|	0.47
64.917	0.00	0.10	0.201	o	|	|	|	0.47
65.000	0.00	0.10	0.200	o	|	|	|	0.46
65.083	0.00	0.10	0.200	o	|	|	|	0.46
65.167	0.00	0.10	0.199	o	|	|	|	0.46
65.250	0.00	0.10	0.198	o	|	|	|	0.46
65.333	0.00	0.10	0.197	o	|	|	|	0.46
65.417	0.00	0.10	0.197	o	|	|	|	0.46
65.500	0.00	0.10	0.196	o	|	|	|	0.45
65.583	0.00	0.10	0.195	o	|	|	|	0.45
65.667	0.00	0.10	0.195	o	|	|	|	0.45
65.750	0.00	0.10	0.194	o	|	|	|	0.45
65.833	0.00	0.10	0.193	o	|	|	|	0.45
65.917	0.00	0.10	0.192	o	|	|	|	0.45
66.000	0.00	0.10	0.192	o	|	|	|	0.45

```
66.083    0.00    0.10      0.191  o       |       |       |       |     0.44

       Remaining water in basin =    0.19 (Ac.Ft)


       ****************************HYDROGRAPH DATA****************************
                     Number of intervals =   793
                     Time interval =    5.0 (Min.)
                     Maximum/Peak flow rate =       14.837 (CFS)
                     Total volume =       3.291 (Ac.Ft)
              Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
       ***********************************************************************

       ----------------------------------------------------------------------
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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 06/03/24

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: pro210610.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    77
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       45.795 (CFS)
               Total volume =       4.817 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
____________________________________________________________________________

User entry of depth-outflow-storage data
------------------------------------------------------------------------
Total number of inflow hydrograph intervals = 77
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
------------------------------------------------------------------------
------------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
------------------------------------------------------------------------
------------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
------------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.431      0.225      0.430        0.432
   2.000      0.914      0.344      0.913        0.915
   3.000      1.451      0.991      1.448        1.454
   4.000      2.049      1.417      2.044        2.054
   5.000      2.712      1.731      2.706        2.718
   5.250      2.888      1.801      2.882        2.894
   5.500      3.069     17.046      3.010        3.128
   6.000      3.443    225.078      2.668        4.218
------------------------------------------------------------------
               Hydrograph Detention Basin Routing
------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                  Depth
(Hours) (CFS)   (CFS)     (Ac.Ft) .0      11.4   22.90   34.35   45.79 (Ft.)
 0.083    0.86    0.00      0.003  O       |       |       |       |     0.01
 0.167    2.45    0.01      0.014  OI      |       |       |       |     0.03
 0.250    3.09    0.02      0.033  O I     |       |       |       |     0.08
 0.333    3.32    0.03      0.055  O I     |       |       |       |     0.13
 0.417    3.44    0.04      0.078  O I     |       |       |       |     0.18
 0.500    3.70    0.05      0.103  O I     |       |       |       |     0.24
 0.583    3.99    0.07      0.129  O I     |       |       |       |     0.30
 0.667    4.07    0.08      0.156  O I     |       |       |       |     0.36
 0.750    4.10    0.10      0.183  O I     |       |       |       |     0.43
 0.833    4.11    0.11      0.211  O I     |       |       |       |     0.49
 0.917    4.13    0.12      0.239  O I     |       |       |       |     0.55
 1.000    4.30    0.14      0.267  O  I    |       |       |       |     0.62
 1.083    4.58    0.15      0.296  O  I    |       |       |       |     0.69
 1.167    4.65    0.17      0.327  O  I    |       |       |       |     0.76
 1.250    4.69    0.19      0.358  O  I    |       |       |       |     0.83
 1.333    4.70    0.20      0.389  O  I    |       |       |       |     0.90
 1.417    4.72    0.22      0.420  O  I    |       |       |       |     0.97
 1.500    4.72    0.23      0.451  O  I    |       |       |       |     1.04
```

1.583	4.72	0.24	0.482	O I	|	|	|	|	1.10
1.667	4.72	0.25	0.512	O I	|	|	|	|	1.17
1.750	4.72	0.25	0.543	O I	|	|	|	|	1.23
1.833	4.72	0.26	0.574	O I	|	|	|	|	1.30
1.917	4.72	0.27	0.605	O I	|	|	|	|	1.36
2.000	4.89	0.28	0.636	O I	|	|	|	|	1.42
2.083	5.00	0.28	0.668	O I	|	|	|	|	1.49
2.167	4.96	0.29	0.700	O I	|	|	|	|	1.56
2.250	5.20	0.30	0.733	O I	|	|	|	|	1.63
2.333	5.26	0.31	0.767	O I	|	|	|	|	1.70
2.417	5.29	0.32	0.801	O I	|	|	|	|	1.77
2.500	5.29	0.32	0.836	O I	|	|	|	|	1.84
2.583	5.31	0.33	0.870	O I	|	|	|	|	1.91
2.667	5.31	0.34	0.904	O I	|	|	|	|	1.98
2.750	5.48	0.37	0.939	O I	|	|	|	|	2.05
2.833	5.76	0.42	0.975	O I	|	|	|	|	2.11
2.917	5.83	0.46	1.012	O I	|	|	|	|	2.18
3.000	5.87	0.51	1.049	O I	|	|	|	|	2.25
3.083	5.88	0.55	1.085	O I	|	|	|	|	2.32
3.167	6.07	0.60	1.123	O I	|	|	|	|	2.39
3.250	6.35	0.64	1.161	O I	|	|	|	|	2.46
3.333	6.42	0.69	1.201	O I	|	|	|	|	2.53
3.417	6.63	0.74	1.241	O I	|	|	|	|	2.61
3.500	7.10	0.79	1.283	O I	|	|	|	|	2.69
3.583	7.64	0.84	1.328	O I	|	|	|	|	2.77
3.667	8.03	0.90	1.376	O I	|	|	|	|	2.86
3.750	8.32	0.96	1.426	O I	|	|	|	|	2.95
3.833	8.67	1.01	1.477	O I	|	|	|	|	3.04
3.917	8.94	1.05	1.531	O I	|	|	|	|	3.13
4.000	9.27	1.09	1.586	O I	|	|	|	|	3.23
4.083	9.53	1.13	1.643	O I	|	|	|	|	3.32
4.167	10.03	1.17	1.703	O I	|	|	|	|	3.42
4.250	10.72	1.22	1.766	O I	|	|	|	|	3.53
4.333	11.70	1.26	1.835	O I	|	|	|	|	3.64
4.417	12.79	1.32	1.910	O I	|	|	|	|	3.77
4.500	13.59	1.38	1.992	O I	|	|	|	|	3.90
4.583	14.19	1.43	2.078	O I	|	|	|	|	4.04
4.667	15.22	1.47	2.169	|O I	|	|	|	|	4.18
4.750	16.34	1.52	2.267	|O I	|	|	|	|	4.33
4.833	17.14	1.57	2.372	|O I	|	|	|	|	4.49
4.917	17.73	1.62	2.481	|O I	|	|	|	|	4.65
5.000	18.76	1.68	2.595	|O I	|	|	|	|	4.82
5.083	21.26	1.73	2.721	|O I	|	|	|	|	5.01
5.167	26.05	1.79	2.872	|O I	|	|	|	|	5.23
5.250	30.73	12.72	3.018	| O	|	|	|	|	5.43
5.333	34.56	30.59	3.093	| O	|	|	|	|	5.53
5.417	38.93	38.68	3.108	| O	|	|	|	|	5.55
5.500	45.79	43.52	3.117	| O	|	|	|	|	5.56
5.583	39.27	42.22	3.114	| O	|	|	|	|	5.56
5.667	18.24	24.52	3.082	| O	|	|	|	|	5.52
5.750	10.16	14.96	3.044	| O	|	|	|	|	5.47
5.833	6.45	11.97	3.009	| O	|	|	|	|	5.42
5.917	4.21	8.98	2.973	| O	|	|	|	|	5.37
6.000	2.16	6.37	2.942	| O	|	|	|	|	5.32
6.083	1.16	4.25	2.917	O	|	|	|	|	5.29
6.167	0.40	2.69	2.899	O	|	|	|	|	5.26
6.250	0.18	1.80	2.885	O	|	|	|	|	5.25
6.333	0.07	1.80	2.874	O	|	|	|	|	5.23
6.417	0.03	1.79	2.862	O	|	|	|	|	5.21
6.500	0.00	1.79	2.849	O	|	|	|	|	5.20
6.583	0.00	1.78	2.837	O	|	|	|	|	5.18
6.667	0.00	1.78	2.825	O	|	|	|	|	5.16
6.750	0.00	1.77	2.813	O	|	|	|	|	5.14
6.833	0.00	1.77	2.800	O	|	|	|	|	5.13
6.917	0.00	1.76	2.788	O	|	|	|	|	5.11
7.000	0.00	1.76	2.776	O	|	|	|	|	5.09
7.083	0.00	1.75	2.764	O	|	|	|	|	5.07
7.167	0.00	1.75	2.752	O	|	|	|	|	5.06
7.250	0.00	1.74	2.740	O	|	|	|	|	5.04
7.333	0.00	1.74	2.728	O	|	|	|	|	5.02
7.417	0.00	1.73	2.716	O	|	|	|	|	5.01
7.500	0.00	1.73	2.704	O	|	|	|	|	4.99
7.583	0.00	1.72	2.692	O	|	|	|	|	4.97
7.667	0.00	1.72	2.681	O	|	|	|	|	4.95
7.750	0.00	1.71	2.669	O	|	|	|	|	4.93
7.833	0.00	1.70	2.657	O	|	|	|	|	4.92
7.917	0.00	1.70	2.645	O	|	|	|	|	4.90
8.000	0.00	1.69	2.634	O	|	|	|	|	4.88
8.083	0.00	1.69	2.622	O	|	|	|	|	4.86
8.167	0.00	1.68	2.610	O	|	|	|	|	4.85
8.250	0.00	1.68	2.599	O	|	|	|	|	4.83
8.333	0.00	1.67	2.587	O	|	|	|	|	4.81
8.417	0.00	1.67	2.576	O	|	|	|	|	4.79
8.500	0.00	1.66	2.564	O	|	|	|	|	4.78
8.583	0.00	1.66	2.553	O	|	|	|	|	4.76
8.667	0.00	1.65	2.541	O	|	|	|	|	4.74

8.750	0.00	1.64	2.530	IO				4.73
8.833	0.00	1.64	2.519	IO				4.71
8.917	0.00	1.63	2.507	IO				4.69
9.000	0.00	1.63	2.496	IO				4.67
9.083	0.00	1.62	2.485	IO				4.66
9.167	0.00	1.62	2.474	IO				4.64
9.250	0.00	1.61	2.463	IO				4.62
9.333	0.00	1.61	2.452	IO				4.61
9.417	0.00	1.60	2.441	IO				4.59
9.500	0.00	1.60	2.430	IO				4.57
9.583	0.00	1.59	2.419	IO				4.56
9.667	0.00	1.59	2.408	IO				4.54
9.750	0.00	1.58	2.397	IO				4.52
9.833	0.00	1.58	2.386	IO				4.51
9.917	0.00	1.57	2.375	IO				4.49
10.000	0.00	1.57	2.364	IO				4.48
10.083	0.00	1.56	2.353	IO				4.46
10.167	0.00	1.56	2.343	IO				4.44
10.250	0.00	1.55	2.332	IO				4.43
10.333	0.00	1.55	2.321	IO				4.41
10.417	0.00	1.54	2.311	IO				4.39
10.500	0.00	1.54	2.300	IO				4.38
10.583	0.00	1.53	2.290	IO				4.36
10.667	0.00	1.53	2.279	IO				4.35
10.750	0.00	1.52	2.269	IO				4.33
10.833	0.00	1.52	2.258	IO				4.32
10.917	0.00	1.51	2.248	IO				4.30
11.000	0.00	1.51	2.237	IO				4.28
11.083	0.00	1.50	2.227	IO				4.27
11.167	0.00	1.50	2.217	IO				4.25
11.250	0.00	1.49	2.206	IO				4.24
11.333	0.00	1.49	2.196	IO				4.22
11.417	0.00	1.48	2.186	IO				4.21
11.500	0.00	1.48	2.176	IO				4.19
11.583	0.00	1.47	2.166	IO				4.18
11.667	0.00	1.47	2.155	IO				4.16
11.750	0.00	1.46	2.145	IO				4.15
11.833	0.00	1.46	2.135	IO				4.13
11.917	0.00	1.45	2.125	IO				4.11
12.000	0.00	1.45	2.115	IO				4.10
12.083	0.00	1.44	2.105	IO				4.08
12.167	0.00	1.44	2.095	IO				4.07
12.250	0.00	1.43	2.085	IO				4.05
12.333	0.00	1.43	2.076	O				4.04
12.417	0.00	1.42	2.066	O				4.03
12.500	0.00	1.42	2.056	O				4.01
12.583	0.00	1.41	2.046	O				4.00
12.667	0.00	1.41	2.036	O				3.98
12.750	0.00	1.40	2.027	O				3.96
12.833	0.00	1.39	2.017	O				3.95
12.917	0.00	1.39	2.008	O				3.93
13.000	0.00	1.38	1.998	O				3.91
13.083	0.00	1.37	1.989	O				3.90
13.167	0.00	1.37	1.979	O				3.88
13.250	0.00	1.36	1.970	O				3.87
13.333	0.00	1.35	1.960	O				3.85
13.417	0.00	1.35	1.951	O				3.84
13.500	0.00	1.34	1.942	O				3.82
13.583	0.00	1.33	1.933	O				3.81
13.667	0.00	1.33	1.923	O				3.79
13.750	0.00	1.32	1.914	O				3.77
13.833	0.00	1.31	1.905	O				3.76
13.917	0.00	1.31	1.896	O				3.74
14.000	0.00	1.30	1.887	O				3.73
14.083	0.00	1.30	1.878	O				3.71
14.167	0.00	1.29	1.869	O				3.70
14.250	0.00	1.28	1.861	O				3.68
14.333	0.00	1.28	1.852	O				3.67
14.417	0.00	1.27	1.843	O				3.66
14.500	0.00	1.26	1.834	O				3.64
14.583	0.00	1.26	1.826	O				3.63
14.667	0.00	1.25	1.817	O				3.61
14.750	0.00	1.25	1.808	O				3.60
14.833	0.00	1.24	1.800	O				3.58
14.917	0.00	1.23	1.791	O				3.57
15.000	0.00	1.23	1.783	O				3.55
15.083	0.00	1.22	1.774	O				3.54
15.167	0.00	1.22	1.766	O				3.53
15.250	0.00	1.21	1.758	O				3.51
15.333	0.00	1.20	1.749	O				3.50
15.417	0.00	1.20	1.741	O				3.48
15.500	0.00	1.19	1.733	O				3.47
15.583	0.00	1.19	1.725	O				3.46
15.667	0.00	1.18	1.716	O				3.44
15.750	0.00	1.17	1.708	O				3.43
15.833	0.00	1.17	1.700	O				3.42

15.917	0.00	1.16	1.692	o	|	|	|	|	3.40
16.000	0.00	1.16	1.684	o	|	|	|	|	3.39
16.083	0.00	1.15	1.676	o	|	|	|	|	3.38
16.167	0.00	1.15	1.668	o	|	|	|	|	3.36
16.250	0.00	1.14	1.661	o	|	|	|	|	3.35
16.333	0.00	1.13	1.653	o	|	|	|	|	3.34
16.417	0.00	1.13	1.645	o	|	|	|	|	3.32
16.500	0.00	1.12	1.637	o	|	|	|	|	3.31
16.583	0.00	1.12	1.629	o	|	|	|	|	3.30
16.667	0.00	1.11	1.622	o	|	|	|	|	3.29
16.750	0.00	1.11	1.614	o	|	|	|	|	3.27
16.833	0.00	1.10	1.606	o	|	|	|	|	3.26
16.917	0.00	1.10	1.599	o	|	|	|	|	3.25
17.000	0.00	1.09	1.591	o	|	|	|	|	3.23
17.083	0.00	1.09	1.584	o	|	|	|	|	3.22
17.167	0.00	1.08	1.576	o	|	|	|	|	3.21
17.250	0.00	1.08	1.569	o	|	|	|	|	3.20
17.333	0.00	1.07	1.562	o	|	|	|	|	3.18
17.417	0.00	1.06	1.554	o	|	|	|	|	3.17
17.500	0.00	1.06	1.547	o	|	|	|	|	3.16
17.583	0.00	1.05	1.540	o	|	|	|	|	3.15
17.667	0.00	1.05	1.532	o	|	|	|	|	3.14
17.750	0.00	1.04	1.525	o	|	|	|	|	3.12
17.833	0.00	1.04	1.518	o	|	|	|	|	3.11
17.917	0.00	1.03	1.511	o	|	|	|	|	3.10
18.000	0.00	1.03	1.504	o	|	|	|	|	3.09
18.083	0.00	1.02	1.497	o	|	|	|	|	3.08
18.167	0.00	1.02	1.490	o	|	|	|	|	3.06
18.250	0.00	1.01	1.483	o	|	|	|	|	3.05
18.333	0.00	1.01	1.476	o	|	|	|	|	3.04
18.417	0.00	1.00	1.469	o	|	|	|	|	3.03
18.500	0.00	1.00	1.462	o	|	|	|	|	3.02
18.583	0.00	0.99	1.455	o	|	|	|	|	3.01
18.667	0.00	0.99	1.448	o	|	|	|	|	2.99
18.750	0.00	0.98	1.441	o	|	|	|	|	2.98
18.833	0.00	0.97	1.435	o	|	|	|	|	2.97
18.917	0.00	0.96	1.428	o	|	|	|	|	2.96
19.000	0.00	0.96	1.421	o	|	|	|	|	2.95
19.083	0.00	0.95	1.415	o	|	|	|	|	2.93
19.167	0.00	0.94	1.408	o	|	|	|	|	2.92
19.250	0.00	0.93	1.402	o	|	|	|	|	2.91
19.333	0.00	0.92	1.396	o	|	|	|	|	2.90
19.417	0.00	0.92	1.389	o	|	|	|	|	2.89
19.500	0.00	0.91	1.383	o	|	|	|	|	2.87
19.583	0.00	0.90	1.377	o	|	|	|	|	2.86
19.667	0.00	0.89	1.371	o	|	|	|	|	2.85
19.750	0.00	0.89	1.364	o	|	|	|	|	2.84
19.833	0.00	0.88	1.358	o	|	|	|	|	2.83
19.917	0.00	0.87	1.352	o	|	|	|	|	2.82
20.000	0.00	0.86	1.346	o	|	|	|	|	2.81
20.083	0.00	0.86	1.340	o	|	|	|	|	2.79
20.167	0.00	0.85	1.335	o	|	|	|	|	2.78
20.250	0.00	0.84	1.329	o	|	|	|	|	2.77
20.333	0.00	0.84	1.323	o	|	|	|	|	2.76
20.417	0.00	0.83	1.317	o	|	|	|	|	2.75
20.500	0.00	0.82	1.311	o	|	|	|	|	2.74
20.583	0.00	0.82	1.306	o	|	|	|	|	2.73
20.667	0.00	0.81	1.300	o	|	|	|	|	2.72
20.750	0.00	0.80	1.295	o	|	|	|	|	2.71
20.833	0.00	0.80	1.289	o	|	|	|	|	2.70
20.917	0.00	0.79	1.284	o	|	|	|	|	2.69
21.000	0.00	0.78	1.278	o	|	|	|	|	2.68
21.083	0.00	0.78	1.273	o	|	|	|	|	2.67
21.167	0.00	0.77	1.268	o	|	|	|	|	2.66
21.250	0.00	0.76	1.262	o	|	|	|	|	2.65
21.333	0.00	0.76	1.257	o	|	|	|	|	2.64
21.417	0.00	0.75	1.252	o	|	|	|	|	2.63
21.500	0.00	0.74	1.247	o	|	|	|	|	2.62
21.583	0.00	0.74	1.242	o	|	|	|	|	2.61
21.667	0.00	0.73	1.237	o	|	|	|	|	2.60
21.750	0.00	0.73	1.232	o	|	|	|	|	2.59
21.833	0.00	0.72	1.227	o	|	|	|	|	2.58
21.917	0.00	0.71	1.222	o	|	|	|	|	2.57
22.000	0.00	0.71	1.217	o	|	|	|	|	2.56
22.083	0.00	0.70	1.212	o	|	|	|	|	2.55
22.167	0.00	0.70	1.207	o	|	|	|	|	2.55
22.250	0.00	0.69	1.202	o	|	|	|	|	2.54
22.333	0.00	0.69	1.198	o	|	|	|	|	2.53
22.417	0.00	0.68	1.193	o	|	|	|	|	2.52
22.500	0.00	0.67	1.188	o	|	|	|	|	2.51
22.583	0.00	0.67	1.184	o	|	|	|	|	2.50
22.667	0.00	0.66	1.179	o	|	|	|	|	2.49
22.750	0.00	0.66	1.174	o	|	|	|	|	2.48
22.833	0.00	0.65	1.170	o	|	|	|	|	2.48
22.917	0.00	0.65	1.165	o	|	|	|	|	2.47
23.000	0.00	0.64	1.161	o	|	|	|	|	2.46

23.083	0.00	0.64	1.157	o	|	|	|	|	2.45
23.167	0.00	0.63	1.152	o	|	|	|	|	2.44
23.250	0.00	0.63	1.148	o	|	|	|	|	2.44
23.333	0.00	0.62	1.144	o	|	|	|	|	2.43
23.417	0.00	0.62	1.139	o	|	|	|	|	2.42
23.500	0.00	0.61	1.135	o	|	|	|	|	2.41
23.583	0.00	0.61	1.131	o	|	|	|	|	2.40
23.667	0.00	0.60	1.127	o	|	|	|	|	2.40
23.750	0.00	0.60	1.123	o	|	|	|	|	2.39
23.833	0.00	0.59	1.119	o	|	|	|	|	2.38
23.917	0.00	0.59	1.115	o	|	|	|	|	2.37
24.000	0.00	0.58	1.110	o	|	|	|	|	2.37
24.083	0.00	0.58	1.107	o	|	|	|	|	2.36
24.167	0.00	0.57	1.103	o	|	|	|	|	2.35
24.250	0.00	0.57	1.099	o	|	|	|	|	2.34
24.333	0.00	0.56	1.095	o	|	|	|	|	2.34
24.417	0.00	0.56	1.091	o	|	|	|	|	2.33
24.500	0.00	0.55	1.087	o	|	|	|	|	2.32
24.583	0.00	0.55	1.083	o	|	|	|	|	2.32
24.667	0.00	0.54	1.080	o	|	|	|	|	2.31
24.750	0.00	0.54	1.076	o	|	|	|	|	2.30
24.833	0.00	0.53	1.072	o	|	|	|	|	2.29
24.917	0.00	0.53	1.068	o	|	|	|	|	2.29
25.000	0.00	0.53	1.065	o	|	|	|	|	2.28
25.083	0.00	0.52	1.061	o	|	|	|	|	2.27
25.167	0.00	0.52	1.058	o	|	|	|	|	2.27
25.250	0.00	0.51	1.054	o	|	|	|	|	2.26
25.333	0.00	0.51	1.051	o	|	|	|	|	2.25
25.417	0.00	0.50	1.047	o	|	|	|	|	2.25
25.500	0.00	0.50	1.044	o	|	|	|	|	2.24
25.583	0.00	0.50	1.040	o	|	|	|	|	2.23
25.667	0.00	0.49	1.037	o	|	|	|	|	2.23
25.750	0.00	0.49	1.033	o	|	|	|	|	2.22
25.833	0.00	0.48	1.030	o	|	|	|	|	2.22
25.917	0.00	0.48	1.027	o	|	|	|	|	2.21
26.000	0.00	0.48	1.023	o	|	|	|	|	2.20
26.083	0.00	0.47	1.020	o	|	|	|	|	2.20
26.167	0.00	0.47	1.017	o	|	|	|	|	2.19
26.250	0.00	0.46	1.014	o	|	|	|	|	2.19
26.333	0.00	0.46	1.011	o	|	|	|	|	2.18
26.417	0.00	0.46	1.007	o	|	|	|	|	2.17
26.500	0.00	0.45	1.004	o	|	|	|	|	2.17
26.583	0.00	0.45	1.001	o	|	|	|	|	2.16
26.667	0.00	0.45	0.998	o	|	|	|	|	2.16
26.750	0.00	0.44	0.995	o	|	|	|	|	2.15
26.833	0.00	0.44	0.992	o	|	|	|	|	2.15
26.917	0.00	0.43	0.989	o	|	|	|	|	2.14
27.000	0.00	0.43	0.986	o	|	|	|	|	2.13
27.083	0.00	0.43	0.983	o	|	|	|	|	2.13
27.167	0.00	0.42	0.980	o	|	|	|	|	2.12
27.250	0.00	0.42	0.977	o	|	|	|	|	2.12
27.333	0.00	0.42	0.974	o	|	|	|	|	2.11
27.417	0.00	0.41	0.971	o	|	|	|	|	2.11
27.500	0.00	0.41	0.969	o	|	|	|	|	2.10
27.583	0.00	0.41	0.966	o	|	|	|	|	2.10
27.667	0.00	0.40	0.963	o	|	|	|	|	2.09
27.750	0.00	0.40	0.960	o	|	|	|	|	2.09
27.833	0.00	0.40	0.958	o	|	|	|	|	2.08
27.917	0.00	0.39	0.955	o	|	|	|	|	2.08
28.000	0.00	0.39	0.952	o	|	|	|	|	2.07
28.083	0.00	0.39	0.949	o	|	|	|	|	2.07
28.167	0.00	0.38	0.947	o	|	|	|	|	2.06
28.250	0.00	0.38	0.944	o	|	|	|	|	2.06
28.333	0.00	0.38	0.942	o	|	|	|	|	2.05
28.417	0.00	0.37	0.939	o	|	|	|	|	2.05
28.500	0.00	0.37	0.936	o	|	|	|	|	2.04
28.583	0.00	0.37	0.934	o	|	|	|	|	2.04
28.667	0.00	0.36	0.931	o	|	|	|	|	2.03
28.750	0.00	0.36	0.929	o	|	|	|	|	2.03
28.833	0.00	0.36	0.926	o	|	|	|	|	2.02
28.917	0.00	0.36	0.924	o	|	|	|	|	2.02
29.000	0.00	0.35	0.921	o	|	|	|	|	2.01
29.083	0.00	0.35	0.919	o	|	|	|	|	2.01
29.167	0.00	0.35	0.917	o	|	|	|	|	2.00
29.250	0.00	0.34	0.914	o	|	|	|	|	2.00
29.333	0.00	0.34	0.912	o	|	|	|	|	2.00
29.417	0.00	0.34	0.910	o	|	|	|	|	1.99
29.500	0.00	0.34	0.907	o	|	|	|	|	1.99
29.583	0.00	0.34	0.905	o	|	|	|	|	1.98
29.667	0.00	0.34	0.902	o	|	|	|	|	1.98
29.750	0.00	0.34	0.900	o	|	|	|	|	1.97
29.833	0.00	0.34	0.898	o	|	|	|	|	1.97
29.917	0.00	0.34	0.895	o	|	|	|	|	1.96
30.000	0.00	0.34	0.893	o	|	|	|	|	1.96
30.083	0.00	0.34	0.891	o	|	|	|	|	1.95
30.167	0.00	0.34	0.888	o	|	|	|	|	1.95

30.250	0.00	0.34	0.886	o	|	|	|	|	1.94
30.333	0.00	0.34	0.884	o	|	|	|	|	1.94
30.417	0.00	0.34	0.881	o	|	|	|	|	1.93
30.500	0.00	0.34	0.879	o	|	|	|	|	1.93
30.583	0.00	0.33	0.877	o	|	|	|	|	1.92
30.667	0.00	0.33	0.875	o	|	|	|	|	1.92
30.750	0.00	0.33	0.872	o	|	|	|	|	1.91
30.833	0.00	0.33	0.870	o	|	|	|	|	1.91
30.917	0.00	0.33	0.868	o	|	|	|	|	1.90
31.000	0.00	0.33	0.865	o	|	|	|	|	1.90
31.083	0.00	0.33	0.863	o	|	|	|	|	1.89
31.167	0.00	0.33	0.861	o	|	|	|	|	1.89
31.250	0.00	0.33	0.859	o	|	|	|	|	1.89
31.333	0.00	0.33	0.856	o	|	|	|	|	1.88
31.417	0.00	0.33	0.854	o	|	|	|	|	1.88
31.500	0.00	0.33	0.852	o	|	|	|	|	1.87
31.583	0.00	0.33	0.849	o	|	|	|	|	1.87
31.667	0.00	0.33	0.847	o	|	|	|	|	1.86
31.750	0.00	0.33	0.845	o	|	|	|	|	1.86
31.833	0.00	0.33	0.843	o	|	|	|	|	1.85
31.917	0.00	0.33	0.840	o	|	|	|	|	1.85
32.000	0.00	0.33	0.838	o	|	|	|	|	1.84
32.083	0.00	0.32	0.836	o	|	|	|	|	1.84
32.167	0.00	0.32	0.834	o	|	|	|	|	1.83
32.250	0.00	0.32	0.832	o	|	|	|	|	1.83
32.333	0.00	0.32	0.829	o	|	|	|	|	1.82
32.417	0.00	0.32	0.827	o	|	|	|	|	1.82
32.500	0.00	0.32	0.825	o	|	|	|	|	1.82
32.583	0.00	0.32	0.823	o	|	|	|	|	1.81
32.667	0.00	0.32	0.820	o	|	|	|	|	1.81
32.750	0.00	0.32	0.818	o	|	|	|	|	1.80
32.833	0.00	0.32	0.816	o	|	|	|	|	1.80
32.917	0.00	0.32	0.814	o	|	|	|	|	1.79
33.000	0.00	0.32	0.812	o	|	|	|	|	1.79
33.083	0.00	0.32	0.809	o	|	|	|	|	1.78
33.167	0.00	0.32	0.807	o	|	|	|	|	1.78
33.250	0.00	0.32	0.805	o	|	|	|	|	1.77
33.333	0.00	0.32	0.803	o	|	|	|	|	1.77
33.417	0.00	0.32	0.801	o	|	|	|	|	1.77
33.500	0.00	0.32	0.798	o	|	|	|	|	1.76
33.583	0.00	0.32	0.796	o	|	|	|	|	1.76
33.667	0.00	0.31	0.794	o	|	|	|	|	1.75
33.750	0.00	0.31	0.792	o	|	|	|	|	1.75
33.833	0.00	0.31	0.790	o	|	|	|	|	1.74
33.917	0.00	0.31	0.788	o	|	|	|	|	1.74
34.000	0.00	0.31	0.786	o	|	|	|	|	1.73
34.083	0.00	0.31	0.783	o	|	|	|	|	1.73
34.167	0.00	0.31	0.781	o	|	|	|	|	1.73
34.250	0.00	0.31	0.779	o	|	|	|	|	1.72
34.333	0.00	0.31	0.777	o	|	|	|	|	1.72
34.417	0.00	0.31	0.775	o	|	|	|	|	1.71
34.500	0.00	0.31	0.773	o	|	|	|	|	1.71
34.583	0.00	0.31	0.771	o	|	|	|	|	1.70
34.667	0.00	0.31	0.768	o	|	|	|	|	1.70
34.750	0.00	0.31	0.766	o	|	|	|	|	1.69
34.833	0.00	0.31	0.764	o	|	|	|	|	1.69
34.917	0.00	0.31	0.762	o	|	|	|	|	1.69
35.000	0.00	0.31	0.760	o	|	|	|	|	1.68
35.083	0.00	0.31	0.758	o	|	|	|	|	1.68
35.167	0.00	0.31	0.756	o	|	|	|	|	1.67
35.250	0.00	0.30	0.754	o	|	|	|	|	1.67
35.333	0.00	0.30	0.752	o	|	|	|	|	1.66
35.417	0.00	0.30	0.749	o	|	|	|	|	1.66
35.500	0.00	0.30	0.747	o	|	|	|	|	1.66
35.583	0.00	0.30	0.745	o	|	|	|	|	1.65
35.667	0.00	0.30	0.743	o	|	|	|	|	1.65
35.750	0.00	0.30	0.741	o	|	|	|	|	1.64
35.833	0.00	0.30	0.739	o	|	|	|	|	1.64
35.917	0.00	0.30	0.737	o	|	|	|	|	1.63
36.000	0.00	0.30	0.735	o	|	|	|	|	1.63
36.083	0.00	0.30	0.733	o	|	|	|	|	1.62
36.167	0.00	0.30	0.731	o	|	|	|	|	1.62
36.250	0.00	0.30	0.729	o	|	|	|	|	1.62
36.333	0.00	0.30	0.727	o	|	|	|	|	1.61
36.417	0.00	0.30	0.725	o	|	|	|	|	1.61
36.500	0.00	0.30	0.723	o	|	|	|	|	1.60
36.583	0.00	0.30	0.721	o	|	|	|	|	1.60
36.667	0.00	0.30	0.719	o	|	|	|	|	1.60
36.750	0.00	0.30	0.716	o	|	|	|	|	1.59
36.833	0.00	0.29	0.714	o	|	|	|	|	1.59
36.917	0.00	0.29	0.712	o	|	|	|	|	1.58
37.000	0.00	0.29	0.710	o	|	|	|	|	1.58
37.083	0.00	0.29	0.708	o	|	|	|	|	1.57
37.167	0.00	0.29	0.706	o	|	|	|	|	1.57
37.250	0.00	0.29	0.704	o	|	|	|	|	1.57
37.333	0.00	0.29	0.702	o	|	|	|	|	1.56

37.417	0.00	0.29	0.700	o	|	|	|	|	1.56
37.500	0.00	0.29	0.698	o	|	|	|	|	1.55
37.583	0.00	0.29	0.696	o	|	|	|	|	1.55
37.667	0.00	0.29	0.694	o	|	|	|	|	1.55
37.750	0.00	0.29	0.692	o	|	|	|	|	1.54
37.833	0.00	0.29	0.690	o	|	|	|	|	1.54
37.917	0.00	0.29	0.688	o	|	|	|	|	1.53
38.000	0.00	0.29	0.686	o	|	|	|	|	1.53
38.083	0.00	0.29	0.684	o	|	|	|	|	1.52
38.167	0.00	0.29	0.682	o	|	|	|	|	1.52
38.250	0.00	0.29	0.680	o	|	|	|	|	1.52
38.333	0.00	0.29	0.678	o	|	|	|	|	1.51
38.417	0.00	0.29	0.676	o	|	|	|	|	1.51
38.500	0.00	0.28	0.675	o	|	|	|	|	1.50
38.583	0.00	0.28	0.673	o	|	|	|	|	1.50
38.667	0.00	0.28	0.671	o	|	|	|	|	1.50
38.750	0.00	0.28	0.669	o	|	|	|	|	1.49
38.833	0.00	0.28	0.667	o	|	|	|	|	1.49
38.917	0.00	0.28	0.665	o	|	|	|	|	1.48
39.000	0.00	0.28	0.663	o	|	|	|	|	1.48
39.083	0.00	0.28	0.661	o	|	|	|	|	1.48
39.167	0.00	0.28	0.659	o	|	|	|	|	1.47
39.250	0.00	0.28	0.657	o	|	|	|	|	1.47
39.333	0.00	0.28	0.655	o	|	|	|	|	1.46
39.417	0.00	0.28	0.653	o	|	|	|	|	1.46
39.500	0.00	0.28	0.651	o	|	|	|	|	1.46
39.583	0.00	0.28	0.649	o	|	|	|	|	1.45
39.667	0.00	0.28	0.647	o	|	|	|	|	1.45
39.750	0.00	0.28	0.645	o	|	|	|	|	1.44
39.833	0.00	0.28	0.644	o	|	|	|	|	1.44
39.917	0.00	0.28	0.642	o	|	|	|	|	1.44
40.000	0.00	0.28	0.640	o	|	|	|	|	1.43
40.083	0.00	0.28	0.638	o	|	|	|	|	1.43
40.167	0.00	0.28	0.636	o	|	|	|	|	1.42
40.250	0.00	0.28	0.634	o	|	|	|	|	1.42
40.333	0.00	0.27	0.632	o	|	|	|	|	1.42
40.417	0.00	0.27	0.630	o	|	|	|	|	1.41
40.500	0.00	0.27	0.628	o	|	|	|	|	1.41
40.583	0.00	0.27	0.626	o	|	|	|	|	1.40
40.667	0.00	0.27	0.625	o	|	|	|	|	1.40
40.750	0.00	0.27	0.623	o	|	|	|	|	1.40
40.833	0.00	0.27	0.621	o	|	|	|	|	1.39
40.917	0.00	0.27	0.619	o	|	|	|	|	1.39
41.000	0.00	0.27	0.617	o	|	|	|	|	1.39
41.083	0.00	0.27	0.615	o	|	|	|	|	1.38
41.167	0.00	0.27	0.613	o	|	|	|	|	1.38
41.250	0.00	0.27	0.612	o	|	|	|	|	1.37
41.333	0.00	0.27	0.610	o	|	|	|	|	1.37
41.417	0.00	0.27	0.608	o	|	|	|	|	1.37
41.500	0.00	0.27	0.606	o	|	|	|	|	1.36
41.583	0.00	0.27	0.604	o	|	|	|	|	1.36
41.667	0.00	0.27	0.602	o	|	|	|	|	1.35
41.750	0.00	0.27	0.600	o	|	|	|	|	1.35
41.833	0.00	0.27	0.599	o	|	|	|	|	1.35
41.917	0.00	0.27	0.597	o	|	|	|	|	1.34
42.000	0.00	0.27	0.595	o	|	|	|	|	1.34
42.083	0.00	0.26	0.593	o	|	|	|	|	1.34
42.167	0.00	0.26	0.591	o	|	|	|	|	1.33
42.250	0.00	0.26	0.589	o	|	|	|	|	1.33
42.333	0.00	0.26	0.588	o	|	|	|	|	1.32
42.417	0.00	0.26	0.586	o	|	|	|	|	1.32
42.500	0.00	0.26	0.584	o	|	|	|	|	1.32
42.583	0.00	0.26	0.582	o	|	|	|	|	1.31
42.667	0.00	0.26	0.580	o	|	|	|	|	1.31
42.750	0.00	0.26	0.579	o	|	|	|	|	1.31
42.833	0.00	0.26	0.577	o	|	|	|	|	1.30
42.917	0.00	0.26	0.575	o	|	|	|	|	1.30
43.000	0.00	0.26	0.573	o	|	|	|	|	1.29
43.083	0.00	0.26	0.571	o	|	|	|	|	1.29
43.167	0.00	0.26	0.570	o	|	|	|	|	1.29
43.250	0.00	0.26	0.568	o	|	|	|	|	1.28
43.333	0.00	0.26	0.566	o	|	|	|	|	1.28
43.417	0.00	0.26	0.564	o	|	|	|	|	1.28
43.500	0.00	0.26	0.563	o	|	|	|	|	1.27
43.583	0.00	0.26	0.561	o	|	|	|	|	1.27
43.667	0.00	0.26	0.559	o	|	|	|	|	1.27
43.750	0.00	0.26	0.557	o	|	|	|	|	1.26
43.833	0.00	0.26	0.555	o	|	|	|	|	1.26
43.917	0.00	0.26	0.554	o	|	|	|	|	1.25
44.000	0.00	0.25	0.552	o	|	|	|	|	1.25
44.083	0.00	0.25	0.550	o	|	|	|	|	1.25
44.167	0.00	0.25	0.548	o	|	|	|	|	1.24
44.250	0.00	0.25	0.547	o	|	|	|	|	1.24
44.333	0.00	0.25	0.545	o	|	|	|	|	1.24
44.417	0.00	0.25	0.543	o	|	|	|	|	1.23
44.500	0.00	0.25	0.541	o	|	|	|	|	1.23

44.583	0.00	0.25	0.540	o	|	|	|	|	1.23
44.667	0.00	0.25	0.538	o	|	|	|	|	1.22
44.750	0.00	0.25	0.536	o	|	|	|	|	1.22
44.833	0.00	0.25	0.535	o	|	|	|	|	1.21
44.917	0.00	0.25	0.533	o	|	|	|	|	1.21
45.000	0.00	0.25	0.531	o	|	|	|	|	1.21
45.083	0.00	0.25	0.529	o	|	|	|	|	1.20
45.167	0.00	0.25	0.528	o	|	|	|	|	1.20
45.250	0.00	0.25	0.526	o	|	|	|	|	1.20
45.333	0.00	0.25	0.524	o	|	|	|	|	1.19
45.417	0.00	0.25	0.523	o	|	|	|	|	1.19
45.500	0.00	0.25	0.521	o	|	|	|	|	1.19
45.583	0.00	0.25	0.519	o	|	|	|	|	1.18
45.667	0.00	0.25	0.517	o	|	|	|	|	1.18
45.750	0.00	0.25	0.516	o	|	|	|	|	1.18
45.833	0.00	0.25	0.514	o	|	|	|	|	1.17
45.917	0.00	0.25	0.512	o	|	|	|	|	1.17
46.000	0.00	0.24	0.511	o	|	|	|	|	1.16
46.083	0.00	0.24	0.509	o	|	|	|	|	1.16
46.167	0.00	0.24	0.507	o	|	|	|	|	1.16
46.250	0.00	0.24	0.506	o	|	|	|	|	1.15
46.333	0.00	0.24	0.504	o	|	|	|	|	1.15
46.417	0.00	0.24	0.502	o	|	|	|	|	1.15
46.500	0.00	0.24	0.501	o	|	|	|	|	1.14
46.583	0.00	0.24	0.499	o	|	|	|	|	1.14
46.667	0.00	0.24	0.497	o	|	|	|	|	1.14
46.750	0.00	0.24	0.496	o	|	|	|	|	1.13
46.833	0.00	0.24	0.494	o	|	|	|	|	1.13
46.917	0.00	0.24	0.492	o	|	|	|	|	1.13
47.000	0.00	0.24	0.491	o	|	|	|	|	1.12
47.083	0.00	0.24	0.489	o	|	|	|	|	1.12
47.167	0.00	0.24	0.487	o	|	|	|	|	1.12
47.250	0.00	0.24	0.486	o	|	|	|	|	1.11
47.333	0.00	0.24	0.484	o	|	|	|	|	1.11
47.417	0.00	0.24	0.482	o	|	|	|	|	1.11
47.500	0.00	0.24	0.481	o	|	|	|	|	1.10
47.583	0.00	0.24	0.479	o	|	|	|	|	1.10
47.667	0.00	0.24	0.478	o	|	|	|	|	1.10
47.750	0.00	0.24	0.476	o	|	|	|	|	1.09
47.833	0.00	0.24	0.474	o	|	|	|	|	1.09
47.917	0.00	0.24	0.473	o	|	|	|	|	1.09
48.000	0.00	0.23	0.471	o	|	|	|	|	1.08
48.083	0.00	0.23	0.469	o	|	|	|	|	1.08
48.167	0.00	0.23	0.468	o	|	|	|	|	1.08
48.250	0.00	0.23	0.466	o	|	|	|	|	1.07
48.333	0.00	0.23	0.465	o	|	|	|	|	1.07
48.417	0.00	0.23	0.463	o	|	|	|	|	1.07
48.500	0.00	0.23	0.461	o	|	|	|	|	1.06
48.583	0.00	0.23	0.460	o	|	|	|	|	1.06
48.667	0.00	0.23	0.458	o	|	|	|	|	1.06
48.750	0.00	0.23	0.457	o	|	|	|	|	1.05
48.833	0.00	0.23	0.455	o	|	|	|	|	1.05
48.917	0.00	0.23	0.453	o	|	|	|	|	1.05
49.000	0.00	0.23	0.452	o	|	|	|	|	1.04
49.083	0.00	0.23	0.450	o	|	|	|	|	1.04
49.167	0.00	0.23	0.449	o	|	|	|	|	1.04
49.250	0.00	0.23	0.447	o	|	|	|	|	1.03
49.333	0.00	0.23	0.446	o	|	|	|	|	1.03
49.417	0.00	0.23	0.444	o	|	|	|	|	1.03
49.500	0.00	0.23	0.442	o	|	|	|	|	1.02
49.583	0.00	0.23	0.441	o	|	|	|	|	1.02
49.667	0.00	0.23	0.439	o	|	|	|	|	1.02
49.750	0.00	0.23	0.438	o	|	|	|	|	1.01
49.833	0.00	0.23	0.436	o	|	|	|	|	1.01
49.917	0.00	0.23	0.435	o	|	|	|	|	1.01
50.000	0.00	0.23	0.433	o	|	|	|	|	1.00
50.083	0.00	0.23	0.431	o	|	|	|	|	1.00
50.167	0.00	0.22	0.430	o	|	|	|	|	1.00
50.250	0.00	0.22	0.428	o	|	|	|	|	0.99
50.333	0.00	0.22	0.427	o	|	|	|	|	0.99
50.417	0.00	0.22	0.425	o	|	|	|	|	0.99
50.500	0.00	0.22	0.424	o	|	|	|	|	0.98
50.583	0.00	0.22	0.422	o	|	|	|	|	0.98
50.667	0.00	0.22	0.421	o	|	|	|	|	0.98
50.750	0.00	0.22	0.419	o	|	|	|	|	0.97
50.833	0.00	0.22	0.418	o	|	|	|	|	0.97
50.917	0.00	0.22	0.416	o	|	|	|	|	0.97
51.000	0.00	0.22	0.415	o	|	|	|	|	0.96
51.083	0.00	0.22	0.413	o	|	|	|	|	0.96
51.167	0.00	0.21	0.412	o	|	|	|	|	0.96
51.250	0.00	0.21	0.410	o	|	|	|	|	0.95
51.333	0.00	0.21	0.409	o	|	|	|	|	0.95
51.417	0.00	0.21	0.407	o	|	|	|	|	0.95
51.500	0.00	0.21	0.406	o	|	|	|	|	0.94
51.583	0.00	0.21	0.404	o	|	|	|	|	0.94
51.667	0.00	0.21	0.403	o	|	|	|	|	0.94

51.750	0.00	0.21	0.402	o	|	|	|	0.93
51.833	0.00	0.21	0.400	o	|	|	|	0.93
51.917	0.00	0.21	0.399	o	|	|	|	0.92
52.000	0.00	0.21	0.397	o	|	|	|	0.92
52.083	0.00	0.21	0.396	o	|	|	|	0.92
52.167	0.00	0.21	0.394	o	|	|	|	0.92
52.250	0.00	0.21	0.393	o	|	|	|	0.91
52.333	0.00	0.20	0.392	o	|	|	|	0.91
52.417	0.00	0.20	0.390	o	|	|	|	0.91
52.500	0.00	0.20	0.389	o	|	|	|	0.90
52.583	0.00	0.20	0.387	o	|	|	|	0.90
52.667	0.00	0.20	0.386	o	|	|	|	0.90
52.750	0.00	0.20	0.385	o	|	|	|	0.89
52.833	0.00	0.20	0.383	o	|	|	|	0.89
52.917	0.00	0.20	0.382	o	|	|	|	0.89
53.000	0.00	0.20	0.380	o	|	|	|	0.88
53.083	0.00	0.20	0.379	o	|	|	|	0.88
53.167	0.00	0.20	0.378	o	|	|	|	0.88
53.250	0.00	0.20	0.376	o	|	|	|	0.87
53.333	0.00	0.20	0.375	o	|	|	|	0.87
53.417	0.00	0.20	0.374	o	|	|	|	0.87
53.500	0.00	0.19	0.372	o	|	|	|	0.86
53.583	0.00	0.19	0.371	o	|	|	|	0.86
53.667	0.00	0.19	0.370	o	|	|	|	0.86
53.750	0.00	0.19	0.368	o	|	|	|	0.85
53.833	0.00	0.19	0.367	o	|	|	|	0.85
53.917	0.00	0.19	0.366	o	|	|	|	0.85
54.000	0.00	0.19	0.364	o	|	|	|	0.85
54.083	0.00	0.19	0.363	o	|	|	|	0.84
54.167	0.00	0.19	0.362	o	|	|	|	0.84
54.250	0.00	0.19	0.360	o	|	|	|	0.84
54.333	0.00	0.19	0.359	o	|	|	|	0.83
54.417	0.00	0.19	0.358	o	|	|	|	0.83
54.500	0.00	0.19	0.357	o	|	|	|	0.83
54.583	0.00	0.19	0.355	o	|	|	|	0.82
54.667	0.00	0.18	0.354	o	|	|	|	0.82
54.750	0.00	0.18	0.353	o	|	|	|	0.82
54.833	0.00	0.18	0.352	o	|	|	|	0.82
54.917	0.00	0.18	0.350	o	|	|	|	0.81
55.000	0.00	0.18	0.349	o	|	|	|	0.81
55.083	0.00	0.18	0.348	o	|	|	|	0.81
55.167	0.00	0.18	0.347	o	|	|	|	0.80
55.250	0.00	0.18	0.345	o	|	|	|	0.80
55.333	0.00	0.18	0.344	o	|	|	|	0.80
55.417	0.00	0.18	0.343	o	|	|	|	0.80
55.500	0.00	0.18	0.342	o	|	|	|	0.79
55.583	0.00	0.18	0.340	o	|	|	|	0.79
55.667	0.00	0.18	0.339	o	|	|	|	0.79
55.750	0.00	0.18	0.338	o	|	|	|	0.78
55.833	0.00	0.18	0.337	o	|	|	|	0.78
55.917	0.00	0.18	0.335	o	|	|	|	0.78
56.000	0.00	0.17	0.334	o	|	|	|	0.78
56.083	0.00	0.17	0.333	o	|	|	|	0.77
56.167	0.00	0.17	0.332	o	|	|	|	0.77
56.250	0.00	0.17	0.331	o	|	|	|	0.77
56.333	0.00	0.17	0.329	o	|	|	|	0.76
56.417	0.00	0.17	0.328	o	|	|	|	0.76
56.500	0.00	0.17	0.327	o	|	|	|	0.76
56.583	0.00	0.17	0.326	o	|	|	|	0.76
56.667	0.00	0.17	0.325	o	|	|	|	0.75
56.750	0.00	0.17	0.324	o	|	|	|	0.75
56.833	0.00	0.17	0.322	o	|	|	|	0.75
56.917	0.00	0.17	0.321	o	|	|	|	0.75
57.000	0.00	0.17	0.320	o	|	|	|	0.74
57.083	0.00	0.17	0.319	o	|	|	|	0.74
57.167	0.00	0.17	0.318	o	|	|	|	0.74
57.250	0.00	0.17	0.317	o	|	|	|	0.73
57.333	0.00	0.16	0.316	o	|	|	|	0.73
57.417	0.00	0.16	0.314	o	|	|	|	0.73
57.500	0.00	0.16	0.313	o	|	|	|	0.73
57.583	0.00	0.16	0.312	o	|	|	|	0.72
57.667	0.00	0.16	0.311	o	|	|	|	0.72
57.750	0.00	0.16	0.310	o	|	|	|	0.72
57.833	0.00	0.16	0.309	o	|	|	|	0.72
57.917	0.00	0.16	0.308	o	|	|	|	0.71
58.000	0.00	0.16	0.307	o	|	|	|	0.71
58.083	0.00	0.16	0.306	o	|	|	|	0.71
58.167	0.00	0.16	0.304	o	|	|	|	0.71
58.250	0.00	0.16	0.303	o	|	|	|	0.70
58.333	0.00	0.16	0.302	o	|	|	|	0.70
58.417	0.00	0.16	0.301	o	|	|	|	0.70
58.500	0.00	0.16	0.300	o	|	|	|	0.70
58.583	0.00	0.16	0.299	o	|	|	|	0.69
58.667	0.00	0.16	0.298	o	|	|	|	0.69
58.750	0.00	0.15	0.297	o	|	|	|	0.69
58.833	0.00	0.15	0.296	o	|	|	|	0.69

58.917	0.00	0.15	0.295	o	|	|	|	0.68
59.000	0.00	0.15	0.294	o	|	|	|	0.68
59.083	0.00	0.15	0.293	o	|	|	|	0.68
59.167	0.00	0.15	0.292	o	|	|	|	0.68
59.250	0.00	0.15	0.291	o	|	|	|	0.67
59.333	0.00	0.15	0.289	o	|	|	|	0.67
59.417	0.00	0.15	0.288	o	|	|	|	0.67
59.500	0.00	0.15	0.287	o	|	|	|	0.67
59.583	0.00	0.15	0.286	o	|	|	|	0.66
59.667	0.00	0.15	0.285	o	|	|	|	0.66
59.750	0.00	0.15	0.284	o	|	|	|	0.66
59.833	0.00	0.15	0.283	o	|	|	|	0.66
59.917	0.00	0.15	0.282	o	|	|	|	0.65
60.000	0.00	0.15	0.281	o	|	|	|	0.65
60.083	0.00	0.15	0.280	o	|	|	|	0.65
60.167	0.00	0.15	0.279	o	|	|	|	0.65
60.250	0.00	0.15	0.278	o	|	|	|	0.65
60.333	0.00	0.14	0.277	o	|	|	|	0.64
60.417	0.00	0.14	0.276	o	|	|	|	0.64
60.500	0.00	0.14	0.275	o	|	|	|	0.64
60.583	0.00	0.14	0.274	o	|	|	|	0.64
60.667	0.00	0.14	0.273	o	|	|	|	0.63
60.750	0.00	0.14	0.272	o	|	|	|	0.63
60.833	0.00	0.14	0.271	o	|	|	|	0.63
60.917	0.00	0.14	0.270	o	|	|	|	0.63
61.000	0.00	0.14	0.269	o	|	|	|	0.63
61.083	0.00	0.14	0.268	o	|	|	|	0.62
61.167	0.00	0.14	0.267	o	|	|	|	0.62
61.250	0.00	0.14	0.267	o	|	|	|	0.62
61.333	0.00	0.14	0.266	o	|	|	|	0.62
61.417	0.00	0.14	0.265	o	|	|	|	0.61
61.500	0.00	0.14	0.264	o	|	|	|	0.61
61.583	0.00	0.14	0.263	o	|	|	|	0.61
61.667	0.00	0.14	0.262	o	|	|	|	0.61
61.750	0.00	0.14	0.261	o	|	|	|	0.61
61.833	0.00	0.14	0.260	o	|	|	|	0.60
61.917	0.00	0.14	0.259	o	|	|	|	0.60
62.000	0.00	0.13	0.258	o	|	|	|	0.60
62.083	0.00	0.13	0.257	o	|	|	|	0.60
62.167	0.00	0.13	0.256	o	|	|	|	0.59
62.250	0.00	0.13	0.255	o	|	|	|	0.59
62.333	0.00	0.13	0.254	o	|	|	|	0.59
62.417	0.00	0.13	0.253	o	|	|	|	0.59
62.500	0.00	0.13	0.253	o	|	|	|	0.59
62.583	0.00	0.13	0.252	o	|	|	|	0.58
62.667	0.00	0.13	0.251	o	|	|	|	0.58
62.750	0.00	0.13	0.250	o	|	|	|	0.58
62.833	0.00	0.13	0.249	o	|	|	|	0.58
62.917	0.00	0.13	0.248	o	|	|	|	0.58
63.000	0.00	0.13	0.247	o	|	|	|	0.57
63.083	0.00	0.13	0.246	o	|	|	|	0.57
63.167	0.00	0.13	0.245	o	|	|	|	0.57
63.250	0.00	0.13	0.244	o	|	|	|	0.57
63.333	0.00	0.13	0.244	o	|	|	|	0.57
63.417	0.00	0.13	0.243	o	|	|	|	0.56
63.500	0.00	0.13	0.242	o	|	|	|	0.56
63.583	0.00	0.13	0.241	o	|	|	|	0.56
63.667	0.00	0.13	0.240	o	|	|	|	0.56
63.750	0.00	0.12	0.239	o	|	|	|	0.56
63.833	0.00	0.12	0.238	o	|	|	|	0.55
63.917	0.00	0.12	0.238	o	|	|	|	0.55
64.000	0.00	0.12	0.237	o	|	|	|	0.55
64.083	0.00	0.12	0.236	o	|	|	|	0.55
64.167	0.00	0.12	0.235	o	|	|	|	0.55
64.250	0.00	0.12	0.234	o	|	|	|	0.54
64.333	0.00	0.12	0.233	o	|	|	|	0.54
64.417	0.00	0.12	0.232	o	|	|	|	0.54
64.500	0.00	0.12	0.232	o	|	|	|	0.54
64.583	0.00	0.12	0.231	o	|	|	|	0.54
64.667	0.00	0.12	0.230	o	|	|	|	0.53
64.750	0.00	0.12	0.229	o	|	|	|	0.53
64.833	0.00	0.12	0.228	o	|	|	|	0.53
64.917	0.00	0.12	0.228	o	|	|	|	0.53
65.000	0.00	0.12	0.227	o	|	|	|	0.53
65.083	0.00	0.12	0.226	o	|	|	|	0.52
65.167	0.00	0.12	0.225	o	|	|	|	0.52
65.250	0.00	0.12	0.224	o	|	|	|	0.52
65.333	0.00	0.12	0.223	o	|	|	|	0.52
65.417	0.00	0.12	0.223	o	|	|	|	0.52
65.500	0.00	0.12	0.222	o	|	|	|	0.51
65.583	0.00	0.12	0.221	o	|	|	|	0.51
65.667	0.00	0.11	0.220	o	|	|	|	0.51
65.750	0.00	0.11	0.219	o	|	|	|	0.51
65.833	0.00	0.11	0.219	o	|	|	|	0.51
65.917	0.00	0.11	0.218	o	|	|	|	0.51
66.000	0.00	0.11	0.217	o	|	|	|	0.50

66.083	0.00	0.11	0.216	o	|	|	|	|	0.50
66.167	0.00	0.11	0.216	o	|	|	|	|	0.50
66.250	0.00	0.11	0.215	o	|	|	|	|	0.50
66.333	0.00	0.11	0.214	o	|	|	|	|	0.50
66.417	0.00	0.11	0.213	o	|	|	|	|	0.49
66.500	0.00	0.11	0.212	o	|	|	|	|	0.49
66.583	0.00	0.11	0.212	o	|	|	|	|	0.49
66.667	0.00	0.11	0.211	o	|	|	|	|	0.49
66.750	0.00	0.11	0.210	o	|	|	|	|	0.49
66.833	0.00	0.11	0.209	o	|	|	|	|	0.49
66.917	0.00	0.11	0.209	o	|	|	|	|	0.48
67.000	0.00	0.11	0.208	o	|	|	|	|	0.48
67.083	0.00	0.11	0.207	o	|	|	|	|	0.48
67.167	0.00	0.11	0.206	o	|	|	|	|	0.48
67.250	0.00	0.11	0.206	o	|	|	|	|	0.48
67.333	0.00	0.11	0.205	o	|	|	|	|	0.48
67.417	0.00	0.11	0.204	o	|	|	|	|	0.47
67.500	0.00	0.11	0.204	o	|	|	|	|	0.47
67.583	0.00	0.11	0.203	o	|	|	|	|	0.47
67.667	0.00	0.11	0.202	o	|	|	|	|	0.47
67.750	0.00	0.11	0.201	o	|	|	|	|	0.47
67.833	0.00	0.10	0.201	o	|	|	|	|	0.47
67.917	0.00	0.10	0.200	o	|	|	|	|	0.46
68.000	0.00	0.10	0.199	o	|	|	|	|	0.46
68.083	0.00	0.10	0.198	o	|	|	|	|	0.46
68.167	0.00	0.10	0.198	o	|	|	|	|	0.46
68.250	0.00	0.10	0.197	o	|	|	|	|	0.46
68.333	0.00	0.10	0.196	o	|	|	|	|	0.46
68.417	0.00	0.10	0.196	o	|	|	|	|	0.45
68.500	0.00	0.10	0.195	o	|	|	|	|	0.45
68.583	0.00	0.10	0.194	o	|	|	|	|	0.45
68.667	0.00	0.10	0.194	o	|	|	|	|	0.45
68.750	0.00	0.10	0.193	o	|	|	|	|	0.45
68.833	0.00	0.10	0.192	o	|	|	|	|	0.45
68.917	0.00	0.10	0.191	o	|	|	|	|	0.44

Remaining water in basin = 0.19 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 827
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 43.521 (CFS)
Total volume = 4.626 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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                FLOOD HYDROGRAPH ROUTING PROGRAM
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                      Study date: 06/03/24

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: pro2102410.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =   293
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       12.911 (CFS)
               Total volume =       6.799 (Ac.Ft)
       Status of hydrographs being held in storage
                  Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
____________________________________________________________________________

User entry of depth-outflow-storage data
---------------------------------------------------------------------
Total number of inflow hydrograph intervals = 293
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
---------------------------------------------------------------------
---------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
---------------------------------------------------------------------
---------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
---------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.431      0.225      0.430        0.432
   2.000      0.914      0.344      0.913        0.915
   3.000      1.451      0.991      1.448        1.454
   4.000      2.049      1.417      2.044        2.054
   5.000      2.712      1.731      2.706        2.718
   5.250      2.888      1.801      2.882        2.894
   5.500      3.069     17.046      3.010        3.128
   6.000      3.443    225.078      2.668        4.218
---------------------------------------------------------------------
               Hydrograph Detention Basin Routing
---------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
---------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                  Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0       3.2    6.46    9.68   12.91 (Ft.)
 0.083    0.19    0.00      0.001  O       |       |       |       |     0.00
 0.167    0.50    0.00      0.003  OI      |       |       |       |     0.01
 0.250    0.58    0.00      0.007  OI      |       |       |       |     0.02
 0.333    0.71    0.01      0.011  OI      |       |       |       |     0.03
 0.417    0.89    0.01      0.017  O I     |       |       |       |     0.04
 0.500    0.94    0.01      0.023  O I     |       |       |       |     0.05
 0.583    0.96    0.02      0.029  O I     |       |       |       |     0.07
 0.667    0.97    0.02      0.036  O I     |       |       |       |     0.08
 0.750    0.98    0.02      0.042  O I     |       |       |       |     0.10
 0.833    1.07    0.03      0.049  O I     |       |       |       |     0.11
 0.917    1.23    0.03      0.057  O  I    |       |       |       |     0.13
 1.000    1.27    0.03      0.065  O  I    |       |       |       |     0.15
 1.083    1.19    0.04      0.074  O I     |       |       |       |     0.17
 1.167    1.04    0.04      0.081  O I     |       |       |       |     0.19
 1.250    1.01    0.05      0.088  O I     |       |       |       |     0.20
 1.333    0.99    0.05      0.094  O I     |       |       |       |     0.22
 1.417    0.98    0.05      0.101  O I     |       |       |       |     0.23
 1.500    0.98    0.06      0.107  O I     |       |       |       |     0.25
 1.583    0.98    0.06      0.114  O I     |       |       |       |     0.26
 1.667    0.98    0.06      0.120  O I     |       |       |       |     0.28
```

1.750	0.98	0.07	0.126	o I	|	|	|	|	0.29
1.833	1.07	0.07	0.133	o I	|	|	|	|	0.31
1.917	1.23	0.07	0.140	o I	|	|	|	|	0.33
2.000	1.27	0.08	0.148	o I	|	|	|	|	0.34
2.083	1.29	0.08	0.156	o I	|	|	|	|	0.36
2.167	1.29	0.09	0.165	o I	|	|	|	|	0.38
2.250	1.30	0.09	0.173	o I	|	|	|	|	0.40
2.333	1.30	0.09	0.181	o I	|	|	|	|	0.42
2.417	1.30	0.10	0.190	o I	|	|	|	|	0.44
2.500	1.30	0.10	0.198	o I	|	|	|	|	0.46
2.583	1.40	0.11	0.207	o I	|	|	|	|	0.48
2.667	1.55	0.11	0.216	o I	|	|	|	|	0.50
2.750	1.59	0.12	0.226	o I	|	|	|	|	0.52
2.833	1.61	0.12	0.236	o I	|	|	|	|	0.55
2.917	1.62	0.13	0.247	o I	|	|	|	|	0.57
3.000	1.63	0.13	0.257	o I	|	|	|	|	0.60
3.083	1.63	0.14	0.267	o I	|	|	|	|	0.62
3.167	1.63	0.14	0.277	o I	|	|	|	|	0.64
3.250	1.63	0.15	0.287	o I	|	|	|	|	0.67
3.333	1.63	0.16	0.298	o I	|	|	|	|	0.69
3.417	1.63	0.16	0.308	o I	|	|	|	|	0.71
3.500	1.63	0.17	0.318	o I	|	|	|	|	0.74
3.583	1.63	0.17	0.328	o I	|	|	|	|	0.76
3.667	1.63	0.18	0.338	o I	|	|	|	|	0.78
3.750	1.63	0.18	0.348	o I	|	|	|	|	0.81
3.833	1.72	0.19	0.358	o I	|	|	|	|	0.83
3.917	1.88	0.19	0.369	o I	|	|	|	|	0.86
4.000	1.92	0.20	0.381	o I	|	|	|	|	0.88
4.083	1.94	0.21	0.393	o I	|	|	|	|	0.91
4.167	1.95	0.21	0.405	o I	|	|	|	|	0.94
4.250	1.95	0.22	0.417	o I	|	|	|	|	0.97
4.333	2.05	0.22	0.429	o I	|	|	|	|	1.00
4.417	2.20	0.23	0.442	o I	|	|	|	|	1.02
4.500	2.24	0.23	0.456	o I	|	|	|	|	1.05
4.583	2.26	0.23	0.470	o I	|	|	|	|	1.08
4.667	2.27	0.24	0.484	o I	|	|	|	|	1.11
4.750	2.28	0.24	0.498	o I	|	|	|	|	1.14
4.833	2.37	0.24	0.512	o I	|	|	|	|	1.17
4.917	2.53	0.25	0.527	o I	|	|	|	|	1.20
5.000	2.57	0.25	0.543	o I	|	|	|	|	1.23
5.083	2.40	0.26	0.558	o I	|	|	|	|	1.26
5.167	2.09	0.26	0.572	o I	|	|	|	|	1.29
5.250	2.02	0.26	0.585	o I	|	|	|	|	1.32
5.333	2.08	0.27	0.597	o I	|	|	|	|	1.34
5.417	2.22	0.27	0.610	o I	|	|	|	|	1.37
5.500	2.24	0.27	0.623	o I	|	|	|	|	1.40
5.583	2.36	0.28	0.637	o I	|	|	|	|	1.43
5.667	2.52	0.28	0.652	o I	|	|	|	|	1.46
5.750	2.57	0.28	0.668	o I	|	|	|	|	1.49
5.833	2.59	0.29	0.684	o I	|	|	|	|	1.52
5.917	2.60	0.29	0.699	o I	|	|	|	|	1.56
6.000	2.60	0.30	0.715	o I	|	|	|	|	1.59
6.083	2.70	0.30	0.732	o I	|	|	|	|	1.62
6.167	2.86	0.30	0.749	o I	|	|	|	|	1.66
6.250	2.90	0.31	0.766	o I	|	|	|	|	1.69
6.333	2.91	0.31	0.784	o I	|	|	|	|	1.73
6.417	2.92	0.32	0.802	o I	|	|	|	|	1.77
6.500	2.93	0.32	0.820	o I	|	|	|	|	1.81
6.583	3.02	0.33	0.838	o I	|	|	|	|	1.84
6.667	3.18	0.33	0.857	o I	|	|	|	|	1.88
6.750	3.22	0.33	0.877	o I	|	|	|	|	1.92
6.833	3.24	0.34	0.897	o I	|	|	|	|	1.97
6.917	3.25	0.35	0.917	o I	|	|	|	|	2.01
7.000	3.26	0.37	0.937	o I	|	|	|	|	2.04
7.083	3.26	0.40	0.957	o I	|	|	|	|	2.08
7.167	3.26	0.42	0.976	|o I	|	|	|	|	2.12
7.250	3.26	0.44	0.996	|o I	|	|	|	|	2.15
7.333	3.35	0.47	1.015	|o I	|	|	|	|	2.19
7.417	3.51	0.49	1.036	|o I	|	|	|	|	2.23
7.500	3.55	0.52	1.057	|o I	|	|	|	|	2.27
7.583	3.66	0.54	1.078	|o |I	|	|	|	|	2.30
7.667	3.83	0.57	1.100	|o |I	|	|	|	|	2.35
7.750	3.87	0.59	1.122	|o |I	|	|	|	|	2.39
7.833	3.98	0.62	1.145	|o |I	|	|	|	|	2.43
7.917	4.15	0.65	1.169	|o | I	|	|	|	|	2.47
8.000	4.20	0.68	1.193	|o | I	|	|	|	|	2.52
8.083	4.41	0.71	1.218	|o | I	|	|	|	|	2.57
8.167	4.73	0.74	1.244	|o | I	|	|	|	|	2.61
8.250	4.81	0.78	1.272	|o | I	|	|	|	|	2.67
8.333	4.85	0.81	1.300	| o | I	|	|	|	|	2.72
8.417	4.87	0.84	1.327	| o | I	|	|	|	|	2.77
8.500	4.88	0.88	1.355	| o | I	|	|	|	|	2.82
8.583	4.98	0.91	1.383	| o | I	|	|	|	|	2.87
8.667	5.13	0.94	1.411	| o | I	|	|	|	|	2.93
8.750	5.17	0.98	1.440	| o | I	|	|	|	|	2.98
8.833	5.29	1.00	1.469	| o | I	|	|	|	|	3.03
8.917	5.45	1.03	1.499	| o | I	|	|	|	|	3.08
9.000	5.50	1.05	1.530	| o | I	|	|	|	|	3.13

9.083	5.71	1.07	1.561	O	I			3.18
9.167	6.03	1.09	1.594	O	I			3.24
9.250	6.12	1.12	1.628	O	I			3.30
9.333	6.25	1.14	1.663	O	I			3.35
9.417	6.42	1.17	1.699	O	I			3.41
9.500	6.48	1.19	1.735	O	I			3.48
9.583	6.59	1.22	1.772	O	I			3.54
9.667	6.76	1.25	1.809	O	I			3.60
9.750	6.80	1.27	1.847	O	I			3.66
9.833	6.91	1.30	1.886	O	I			3.73
9.917	7.08	1.33	1.925	O	I			3.79
10.000	7.13	1.36	1.965	O	I			3.86
10.083	6.48	1.38	2.002	O	I			3.92
10.167	5.39	1.41	2.033	O	I			3.97
10.250	5.12	1.42	2.060	O	I			4.02
10.333	5.00	1.43	2.085	O	I			4.05
10.417	4.93	1.45	2.109	O	I			4.09
10.500	4.88	1.46	2.133	O	I			4.13
10.583	5.36	1.47	2.158	O	I			4.16
10.667	6.14	1.48	2.187	O	I			4.21
10.750	6.34	1.50	2.220	O	I			4.26
10.833	6.43	1.51	2.254	O	I			4.31
10.917	6.47	1.53	2.288	O	I			4.36
11.000	6.51	1.55	2.322	O	I			4.41
11.083	6.42	1.56	2.356	O	I			4.46
11.167	6.26	1.58	2.388	O	I			4.51
11.250	6.22	1.59	2.421	O	I			4.56
11.333	6.20	1.61	2.452	O	I			4.61
11.417	6.19	1.62	2.484	O	I			4.66
11.500	6.19	1.64	2.515	O	I			4.70
11.583	5.99	1.65	2.546	O	I			4.75
11.667	5.68	1.67	2.575	O	I			4.79
11.750	5.60	1.68	2.602	O	I			4.83
11.833	5.66	1.69	2.629	O	I			4.88
11.917	5.80	1.70	2.657	O	I			4.92
12.000	5.83	1.72	2.685	O	I			4.96
12.083	6.51	1.73	2.716	O	I			5.01
12.167	7.61	1.75	2.752	O	I			5.06
12.250	7.90	1.76	2.794	O	I			5.12
12.333	8.12	1.78	2.837	O	I			5.18
12.417	8.34	1.80	2.881	O	I			5.24
12.500	8.43	4.31	2.918	O	I			5.29
12.583	8.64	6.21	2.940	O	I			5.32
12.667	8.96	7.37	2.954	O	I			5.34
12.750	9.05	8.11	2.963	O	I			5.35
12.833	9.18	8.56	2.968	O	I			5.36
12.917	9.35	8.88	2.972	O	I			5.37
13.000	9.41	9.10	2.975	O	I			5.37
13.083	10.38	9.46	2.979	O	I			5.38
13.167	11.99	10.24	2.988	O	I			5.39
13.250	12.43	11.12	2.999	O	I			5.40
13.333	12.65	11.76	3.006	O	I			5.41
13.417	12.79	12.19	3.011	O	I			5.42
13.500	12.91	12.49	3.015	O	I			5.43
13.583	11.34	12.33	3.013	O	I			5.42
13.667	8.72	11.29	3.001	O	I			5.41
13.750	8.06	9.99	2.985	O	I			5.38
13.833	7.77	9.06	2.974	O	I			5.37
13.917	7.61	8.44	2.967	O	I			5.36
14.000	7.49	8.04	2.962	O	I			5.35
14.083	7.87	7.88	2.960	O	I			5.35
14.167	8.49	8.01	2.962	O	I			5.35
14.250	8.66	8.27	2.965	O	I			5.36
14.333	8.64	8.44	2.967	O	I			5.36
14.417	8.51	8.50	2.968	O	I			5.36
14.500	8.50	8.50	2.968	O	I			5.36
14.583	8.48	8.50	2.968	O	I			5.36
14.667	8.47	8.49	2.967	O	I			5.36
14.750	8.46	8.48	2.967	O	I			5.36
14.833	8.37	8.45	2.967	O	I			5.36
14.917	8.21	8.38	2.966	O	I			5.36
15.000	8.17	8.29	2.965	O	I			5.36
15.083	8.06	8.21	2.964	O	I			5.36
15.167	7.89	8.11	2.963	O	I			5.35
15.250	7.85	8.00	2.962	O	I			5.35
15.333	7.73	7.91	2.960	O	I			5.35
15.417	7.57	7.79	2.959	O	I			5.35
15.500	7.52	7.68	2.958	O	I			5.35
15.583	7.12	7.52	2.956	O	I			5.34
15.667	6.49	7.20	2.952	O	I			5.34
15.750	6.32	6.84	2.948	O	I			5.33
15.833	6.25	6.59	2.945	O	I			5.33
15.917	6.21	6.43	2.943	O	I			5.33
16.000	6.19	6.33	2.942	O	I			5.32
16.083	4.76	5.94	2.937	O	I			5.32
16.167	2.41	4.88	2.925	O	I			5.30
16.250	1.82	3.64	2.910	O	I			5.28
16.333	1.55	2.76	2.899	O	I			5.27

16.417	1.41	2.18	2.893	I O				5.26
16.500	1.30	1.81	2.888	IO				5.25
16.583	1.21	1.80	2.884	I O				5.24
16.667	1.05	1.80	2.880	I O				5.24
16.750	1.01	1.80	2.874	I O				5.23
16.833	0.99	1.79	2.869	I O				5.22
16.917	0.98	1.79	2.863	I O				5.22
17.000	0.98	1.79	2.858	I O				5.21
17.083	1.17	1.79	2.853	I O				5.20
17.167	1.48	1.79	2.850	IO				5.20
17.250	1.56	1.79	2.848	IO				5.19
17.333	1.59	1.78	2.846	IO				5.19
17.417	1.61	1.78	2.845	IO				5.19
17.500	1.63	1.78	2.844	O				5.19
17.583	1.63	1.78	2.843	O				5.19
17.667	1.63	1.78	2.842	O				5.18
17.750	1.63	1.78	2.841	O				5.18
17.833	1.53	1.78	2.840	IO				5.18
17.917	1.38	1.78	2.837	IO				5.18
18.000	1.34	1.78	2.834	IO				5.17
18.083	1.32	1.78	2.831	IO				5.17
18.167	1.31	1.78	2.828	IO				5.16
18.250	1.30	1.78	2.825	IO				5.16
18.333	1.30	1.77	2.822	IO				5.16
18.417	1.30	1.77	2.818	IO				5.15
18.500	1.30	1.77	2.815	IO				5.15
18.583	1.21	1.77	2.811	I O				5.14
18.667	1.05	1.77	2.807	I O				5.14
18.750	1.01	1.77	2.802	I O				5.13
18.833	0.90	1.76	2.796	I O				5.12
18.917	0.73	1.76	2.790	I O				5.11
19.000	0.69	1.76	2.783	I O				5.10
19.083	0.76	1.76	2.776	I O				5.09
19.167	0.91	1.75	2.769	I O				5.08
19.250	0.94	1.75	2.764	I O				5.07
19.333	1.06	1.75	2.758	I O				5.07
19.417	1.22	1.75	2.754	IO				5.06
19.500	1.27	1.75	2.751	IO				5.05
19.583	1.19	1.74	2.747	I O				5.05
19.667	1.04	1.74	2.743	I O				5.04
19.750	1.01	1.74	2.738	I O				5.04
19.833	0.90	1.74	2.732	I O				5.03
19.917	0.73	1.74	2.726	I O				5.02
20.000	0.69	1.73	2.719	I O				5.01
20.083	0.76	1.73	2.712	I O				5.00
20.167	0.91	1.73	2.706	I O				4.99
20.250	0.94	1.73	2.700	I O				4.98
20.333	0.96	1.72	2.695	I O				4.97
20.417	0.97	1.72	2.690	I O				4.97
20.500	0.98	1.72	2.685	I O				4.96
20.583	0.98	1.72	2.680	I O				4.95
20.667	0.98	1.71	2.675	I O				4.94
20.750	0.98	1.71	2.669	I O				4.94
20.833	0.88	1.71	2.664	I O				4.93
20.917	0.72	1.71	2.658	I O				4.92
21.000	0.69	1.70	2.651	I O				4.91
21.083	0.76	1.70	2.644	I O				4.90
21.167	0.91	1.70	2.638	I O				4.89
21.250	0.94	1.69	2.633	I O				4.88
21.333	0.86	1.69	2.628	I O				4.87
21.417	0.72	1.69	2.621	I O				4.86
21.500	0.69	1.68	2.615	I O				4.85
21.583	0.76	1.68	2.608	I O				4.84
21.667	0.91	1.68	2.602	I O				4.83
21.750	0.94	1.68	2.597	I O				4.83
21.833	0.86	1.67	2.592	I O				4.82
21.917	0.72	1.67	2.586	I O				4.81
22.000	0.69	1.67	2.579	I O				4.80
22.083	0.76	1.66	2.573	I O				4.79
22.167	0.91	1.66	2.567	I O				4.78
22.250	0.94	1.66	2.562	I O				4.77
22.333	0.86	1.66	2.557	I O				4.77
22.417	0.72	1.65	2.551	I O				4.76
22.500	0.69	1.65	2.544	I O				4.75
22.583	0.67	1.65	2.537	I O				4.74
22.667	0.66	1.65	2.531	I O				4.73
22.750	0.65	1.64	2.524	I O				4.72
22.833	0.65	1.64	2.517	I O				4.71
22.917	0.65	1.64	2.510	I O				4.70
23.000	0.65	1.63	2.503	I O				4.69
23.083	0.65	1.63	2.497	I O				4.68
23.167	0.65	1.63	2.490	I O				4.67
23.250	0.65	1.62	2.483	I O				4.65
23.333	0.65	1.62	2.477	I O				4.64
23.417	0.65	1.62	2.470	I O				4.63
23.500	0.65	1.61	2.463	I O				4.62
23.583	0.65	1.61	2.457	I O				4.61
23.667	0.65	1.61	2.450	I O				4.60

23.750	0.65	1.60	2.443	|I O	|	|	|	4.59
23.833	0.65	1.60	2.437	|I O	|	|	|	4.59
23.917	0.65	1.60	2.430	|I O	|	|	|	4.58
24.000	0.65	1.59	2.424	|I O	|	|	|	4.57
24.083	0.46	1.59	2.417	|I O	|	|	|	4.55
24.167	0.15	1.59	2.408	I O	|	|	|	4.54
24.250	0.07	1.58	2.398	I O	|	|	|	4.53
24.333	0.03	1.58	2.387	I O	|	|	|	4.51
24.417	0.01	1.57	2.377	I O	|	|	|	4.49
24.500	0.00	1.57	2.366	I O	|	|	|	4.48
24.583	0.00	1.56	2.355	I O	|	|	|	4.46
24.667	0.00	1.56	2.344	I O	|	|	|	4.45
24.750	0.00	1.55	2.334	I O	|	|	|	4.43
24.833	0.00	1.55	2.323	I O	|	|	|	4.41
24.917	0.00	1.54	2.312	I O	|	|	|	4.40
25.000	0.00	1.54	2.302	I O	|	|	|	4.38
25.083	0.00	1.53	2.291	I O	|	|	|	4.37
25.167	0.00	1.53	2.281	I O	|	|	|	4.35
25.250	0.00	1.52	2.270	I O	|	|	|	4.33
25.333	0.00	1.52	2.260	I O	|	|	|	4.32
25.417	0.00	1.51	2.249	I O	|	|	|	4.30
25.500	0.00	1.51	2.239	I O	|	|	|	4.29
25.583	0.00	1.50	2.228	I O	|	|	|	4.27
25.667	0.00	1.50	2.218	I O	|	|	|	4.25
25.750	0.00	1.49	2.208	I O	|	|	|	4.24
25.833	0.00	1.49	2.197	I O	|	|	|	4.22
25.917	0.00	1.48	2.187	I O	|	|	|	4.21
26.000	0.00	1.48	2.177	I O	|	|	|	4.19
26.083	0.00	1.47	2.167	I O	|	|	|	4.18
26.167	0.00	1.47	2.157	I O	|	|	|	4.16
26.250	0.00	1.46	2.147	I O	|	|	|	4.15
26.333	0.00	1.46	2.137	I O	|	|	|	4.13
26.417	0.00	1.45	2.127	I O	|	|	|	4.12
26.500	0.00	1.45	2.117	I O	|	|	|	4.10
26.583	0.00	1.44	2.107	I O	|	|	|	4.09
26.667	0.00	1.44	2.097	I O	|	|	|	4.07
26.750	0.00	1.43	2.087	I O	|	|	|	4.06
26.833	0.00	1.43	2.077	I O	|	|	|	4.04
26.917	0.00	1.43	2.067	I O	|	|	|	4.03
27.000	0.00	1.42	2.057	I O	|	|	|	4.01
27.083	0.00	1.42	2.048	I O	|	|	|	4.00
27.167	0.00	1.41	2.038	I O	|	|	|	3.98
27.250	0.00	1.40	2.028	I O	|	|	|	3.97
27.333	0.00	1.40	2.019	I O	|	|	|	3.95
27.417	0.00	1.39	2.009	I O	|	|	|	3.93
27.500	0.00	1.38	1.999	I O	|	|	|	3.92
27.583	0.00	1.37	1.990	I O	|	|	|	3.90
27.667	0.00	1.37	1.980	I O	|	|	|	3.89
27.750	0.00	1.36	1.971	I O	|	|	|	3.87
27.833	0.00	1.35	1.962	I O	|	|	|	3.85
27.917	0.00	1.35	1.952	I O	|	|	|	3.84
28.000	0.00	1.34	1.943	I O	|	|	|	3.82
28.083	0.00	1.34	1.934	I O	|	|	|	3.81
28.167	0.00	1.33	1.925	I O	|	|	|	3.79
28.250	0.00	1.32	1.916	I O	|	|	|	3.78
28.333	0.00	1.32	1.907	I O	|	|	|	3.76
28.417	0.00	1.31	1.897	I O	|	|	|	3.75
28.500	0.00	1.30	1.888	I O	|	|	|	3.73
28.583	0.00	1.30	1.880	I O	|	|	|	3.72
28.667	0.00	1.29	1.871	I O	|	|	|	3.70
28.750	0.00	1.28	1.862	I O	|	|	|	3.69
28.833	0.00	1.28	1.853	I O	|	|	|	3.67
28.917	0.00	1.27	1.844	I O	|	|	|	3.66
29.000	0.00	1.26	1.835	I O	|	|	|	3.64
29.083	0.00	1.26	1.827	I O	|	|	|	3.63
29.167	0.00	1.25	1.818	I O	|	|	|	3.61
29.250	0.00	1.25	1.810	I O	|	|	|	3.60
29.333	0.00	1.24	1.801	I O	|	|	|	3.59
29.417	0.00	1.23	1.792	I O	|	|	|	3.57
29.500	0.00	1.23	1.784	I O	|	|	|	3.56
29.583	0.00	1.22	1.776	I O	|	|	|	3.54
29.667	0.00	1.22	1.767	I O	|	|	|	3.53
29.750	0.00	1.21	1.759	I O	|	|	|	3.51
29.833	0.00	1.20	1.750	I O	|	|	|	3.50
29.917	0.00	1.20	1.742	I O	|	|	|	3.49
30.000	0.00	1.19	1.734	I O	|	|	|	3.47
30.083	0.00	1.19	1.726	I O	|	|	|	3.46
30.167	0.00	1.18	1.718	I O	|	|	|	3.45
30.250	0.00	1.18	1.709	I O	|	|	|	3.43
30.333	0.00	1.17	1.701	I O	|	|	|	3.42
30.417	0.00	1.16	1.693	I O	|	|	|	3.41
30.500	0.00	1.16	1.685	I O	|	|	|	3.39
30.583	0.00	1.15	1.677	I O	|	|	|	3.38
30.667	0.00	1.15	1.669	I O	|	|	|	3.37
30.750	0.00	1.14	1.662	I O	|	|	|	3.35
30.833	0.00	1.14	1.654	I O	|	|	|	3.34
30.917	0.00	1.13	1.646	I O	|	|	|	3.33
31.000	0.00	1.12	1.638	I O	|	|	|	3.31

31.083	0.00	1.12	1.630	I O	|	|	|	3.30
31.167	0.00	1.11	1.623	I O	|	|	|	3.29
31.250	0.00	1.11	1.615	I O	|	|	|	3.27
31.333	0.00	1.10	1.608	I O	|	|	|	3.26
31.417	0.00	1.10	1.600	I O	|	|	|	3.25
31.500	0.00	1.09	1.592	I O	|	|	|	3.24
31.583	0.00	1.09	1.585	I O	|	|	|	3.22
31.667	0.00	1.08	1.577	I O	|	|	|	3.21
31.750	0.00	1.08	1.570	I O	|	|	|	3.20
31.833	0.00	1.07	1.563	I O	|	|	|	3.19
31.917	0.00	1.07	1.555	I O	|	|	|	3.17
32.000	0.00	1.06	1.548	I O	|	|	|	3.16
32.083	0.00	1.05	1.541	I O	|	|	|	3.15
32.167	0.00	1.05	1.533	I O	|	|	|	3.14
32.250	0.00	1.04	1.526	I O	|	|	|	3.13
32.333	0.00	1.04	1.519	I O	|	|	|	3.11
32.417	0.00	1.03	1.512	I O	|	|	|	3.10
32.500	0.00	1.03	1.505	I O	|	|	|	3.09
32.583	0.00	1.02	1.498	I O	|	|	|	3.08
32.667	0.00	1.02	1.491	I O	|	|	|	3.07
32.750	0.00	1.01	1.484	I O	|	|	|	3.05
32.833	0.00	1.01	1.477	I O	|	|	|	3.04
32.917	0.00	1.00	1.470	I O	|	|	|	3.03
33.000	0.00	1.00	1.463	I O	|	|	|	3.02
33.083	0.00	0.99	1.456	I O	|	|	|	3.01
33.167	0.00	0.99	1.449	I O	|	|	|	3.00
33.250	0.00	0.98	1.442	I O	|	|	|	2.98
33.333	0.00	0.97	1.436	I O	|	|	|	2.97
33.417	0.00	0.96	1.429	I O	|	|	|	2.96
33.500	0.00	0.96	1.422	I O	|	|	|	2.95
33.583	0.00	0.95	1.416	I O	|	|	|	2.93
33.667	0.00	0.94	1.409	I O	|	|	|	2.92
33.750	0.00	0.93	1.403	I O	|	|	|	2.91
33.833	0.00	0.93	1.396	I O	|	|	|	2.90
33.917	0.00	0.92	1.390	I O	|	|	|	2.89
34.000	0.00	0.91	1.384	I O	|	|	|	2.87
34.083	0.00	0.90	1.378	I O	|	|	|	2.86
34.167	0.00	0.90	1.371	I O	|	|	|	2.85
34.250	0.00	0.89	1.365	I O	|	|	|	2.84
34.333	0.00	0.88	1.359	I O	|	|	|	2.83
34.417	0.00	0.87	1.353	I O	|	|	|	2.82
34.500	0.00	0.87	1.347	I O	|	|	|	2.81
34.583	0.00	0.86	1.341	I O	|	|	|	2.80
34.667	0.00	0.85	1.335	I O	|	|	|	2.78
34.750	0.00	0.84	1.329	I O	|	|	|	2.77
34.833	0.00	0.84	1.324	I O	|	|	|	2.76
34.917	0.00	0.83	1.318	I O	|	|	|	2.75
35.000	0.00	0.82	1.312	I O	|	|	|	2.74
35.083	0.00	0.82	1.307	I O	|	|	|	2.73
35.167	0.00	0.81	1.301	I O	|	|	|	2.72
35.250	0.00	0.80	1.295	IO	|	|	|	2.71
35.333	0.00	0.80	1.290	IO	|	|	|	2.70
35.417	0.00	0.79	1.284	IO	|	|	|	2.69
35.500	0.00	0.78	1.279	IO	|	|	|	2.68
35.583	0.00	0.78	1.274	IO	|	|	|	2.67
35.667	0.00	0.77	1.268	IO	|	|	|	2.66
35.750	0.00	0.76	1.263	IO	|	|	|	2.65
35.833	0.00	0.76	1.258	IO	|	|	|	2.64
35.917	0.00	0.75	1.253	IO	|	|	|	2.63
36.000	0.00	0.75	1.247	IO	|	|	|	2.62
36.083	0.00	0.74	1.242	IO	|	|	|	2.61
36.167	0.00	0.73	1.237	IO	|	|	|	2.60
36.250	0.00	0.73	1.232	IO	|	|	|	2.59
36.333	0.00	0.72	1.227	IO	|	|	|	2.58
36.417	0.00	0.72	1.222	IO	|	|	|	2.57
36.500	0.00	0.71	1.217	IO	|	|	|	2.56
36.583	0.00	0.70	1.213	IO	|	|	|	2.56
36.667	0.00	0.70	1.208	IO	|	|	|	2.55
36.750	0.00	0.69	1.203	IO	|	|	|	2.54
36.833	0.00	0.69	1.198	IO	|	|	|	2.53
36.917	0.00	0.68	1.193	IO	|	|	|	2.52
37.000	0.00	0.68	1.189	IO	|	|	|	2.51
37.083	0.00	0.67	1.184	IO	|	|	|	2.50
37.167	0.00	0.66	1.180	IO	|	|	|	2.49
37.250	0.00	0.66	1.175	IO	|	|	|	2.49
37.333	0.00	0.65	1.170	IO	|	|	|	2.48
37.417	0.00	0.65	1.166	IO	|	|	|	2.47
37.500	0.00	0.64	1.162	IO	|	|	|	2.46
37.583	0.00	0.64	1.157	IO	|	|	|	2.45
37.667	0.00	0.63	1.153	IO	|	|	|	2.44
37.750	0.00	0.63	1.148	IO	|	|	|	2.44
37.833	0.00	0.62	1.144	IO	|	|	|	2.43
37.917	0.00	0.62	1.140	IO	|	|	|	2.42
38.000	0.00	0.61	1.136	IO	|	|	|	2.41
38.083	0.00	0.61	1.131	IO	|	|	|	2.41
38.167	0.00	0.60	1.127	IO	|	|	|	2.40
38.250	0.00	0.60	1.123	IO	|	|	|	2.39
38.333	0.00	0.59	1.119	IO	|	|	|	2.38

38.417	0.00	0.59	1.115	IO	|	|	|	2.37
38.500	0.00	0.58	1.111	IO	|	|	|	2.37
38.583	0.00	0.58	1.107	IO	|	|	|	2.36
38.667	0.00	0.57	1.103	IO	|	|	|	2.35
38.750	0.00	0.57	1.099	IO	|	|	|	2.34
38.833	0.00	0.56	1.095	IO	|	|	|	2.34
38.917	0.00	0.56	1.091	IO	|	|	|	2.33
39.000	0.00	0.55	1.088	IO	|	|	|	2.32
39.083	0.00	0.55	1.084	IO	|	|	|	2.32
39.167	0.00	0.54	1.080	IO	|	|	|	2.31
39.250	0.00	0.54	1.076	IO	|	|	|	2.30
39.333	0.00	0.54	1.073	IO	|	|	|	2.30
39.417	0.00	0.53	1.069	IO	|	|	|	2.29
39.500	0.00	0.53	1.065	IO	|	|	|	2.28
39.583	0.00	0.52	1.062	IO	|	|	|	2.28
39.667	0.00	0.52	1.058	IO	|	|	|	2.27
39.750	0.00	0.51	1.055	IO	|	|	|	2.26
39.833	0.00	0.51	1.051	IO	|	|	|	2.26
39.917	0.00	0.50	1.048	IO	|	|	|	2.25
40.000	0.00	0.50	1.044	IO	|	|	|	2.24
40.083	0.00	0.50	1.041	IO	|	|	|	2.24
40.167	0.00	0.49	1.037	IO	|	|	|	2.23
40.250	0.00	0.49	1.034	IO	|	|	|	2.22
40.333	0.00	0.48	1.031	IO	|	|	|	2.22
40.417	0.00	0.48	1.027	IO	|	|	|	2.21
40.500	0.00	0.48	1.024	IO	|	|	|	2.20
40.583	0.00	0.47	1.021	IO	|	|	|	2.20
40.667	0.00	0.47	1.017	IO	|	|	|	2.19
40.750	0.00	0.46	1.014	IO	|	|	|	2.19
40.833	0.00	0.46	1.011	IO	|	|	|	2.18
40.917	0.00	0.46	1.008	IO	|	|	|	2.17
41.000	0.00	0.45	1.005	IO	|	|	|	2.17
41.083	0.00	0.45	1.002	IO	|	|	|	2.16
41.167	0.00	0.45	0.999	IO	|	|	|	2.16
41.250	0.00	0.44	0.995	IO	|	|	|	2.15
41.333	0.00	0.44	0.992	IO	|	|	|	2.15
41.417	0.00	0.43	0.989	IO	|	|	|	2.14
41.500	0.00	0.43	0.986	IO	|	|	|	2.13
41.583	0.00	0.43	0.983	IO	|	|	|	2.13
41.667	0.00	0.42	0.981	IO	|	|	|	2.12
41.750	0.00	0.42	0.978	IO	|	|	|	2.12
41.833	0.00	0.42	0.975	IO	|	|	|	2.11
41.917	0.00	0.41	0.972	IO	|	|	|	2.11
42.000	0.00	0.41	0.969	IO	|	|	|	2.10
42.083	0.00	0.41	0.966	IO	|	|	|	2.10
42.167	0.00	0.40	0.963	IO	|	|	|	2.09
42.250	0.00	0.40	0.961	O	|	|	|	2.09
42.333	0.00	0.40	0.958	O	|	|	|	2.08
42.417	0.00	0.39	0.955	O	|	|	|	2.08
42.500	0.00	0.39	0.953	O	|	|	|	2.07
42.583	0.00	0.39	0.950	O	|	|	|	2.07
42.667	0.00	0.38	0.947	O	|	|	|	2.06
42.750	0.00	0.38	0.945	O	|	|	|	2.06
42.833	0.00	0.38	0.942	O	|	|	|	2.05
42.917	0.00	0.37	0.939	O	|	|	|	2.05
43.000	0.00	0.37	0.937	O	|	|	|	2.04
43.083	0.00	0.37	0.934	O	|	|	|	2.04
43.167	0.00	0.37	0.932	O	|	|	|	2.03
43.250	0.00	0.36	0.929	O	|	|	|	2.03
43.333	0.00	0.36	0.927	O	|	|	|	2.02
43.417	0.00	0.36	0.924	O	|	|	|	2.02
43.500	0.00	0.35	0.922	O	|	|	|	2.01
43.583	0.00	0.35	0.919	O	|	|	|	2.01
43.667	0.00	0.35	0.917	O	|	|	|	2.01
43.750	0.00	0.34	0.915	O	|	|	|	2.00
43.833	0.00	0.34	0.912	O	|	|	|	2.00
43.917	0.00	0.34	0.910	O	|	|	|	1.99
44.000	0.00	0.34	0.907	O	|	|	|	1.99
44.083	0.00	0.34	0.905	O	|	|	|	1.98
44.167	0.00	0.34	0.903	O	|	|	|	1.98
44.250	0.00	0.34	0.900	O	|	|	|	1.97
44.333	0.00	0.34	0.898	O	|	|	|	1.97
44.417	0.00	0.34	0.896	O	|	|	|	1.96
44.500	0.00	0.34	0.893	O	|	|	|	1.96
44.583	0.00	0.34	0.891	O	|	|	|	1.95
44.667	0.00	0.34	0.889	O	|	|	|	1.95
44.750	0.00	0.34	0.886	O	|	|	|	1.94
44.833	0.00	0.34	0.884	O	|	|	|	1.94
44.917	0.00	0.34	0.882	O	|	|	|	1.93
45.000	0.00	0.34	0.879	O	|	|	|	1.93
45.083	0.00	0.33	0.877	O	|	|	|	1.92
45.167	0.00	0.33	0.875	O	|	|	|	1.92
45.250	0.00	0.33	0.873	O	|	|	|	1.91
45.333	0.00	0.33	0.870	O	|	|	|	1.91
45.417	0.00	0.33	0.868	O	|	|	|	1.90
45.500	0.00	0.33	0.866	O	|	|	|	1.90
45.583	0.00	0.33	0.863	O	|	|	|	1.90
45.667	0.00	0.33	0.861	O	|	|	|	1.89

45.750	0.00	0.33	0.859	o	|	|	|	|	1.89
45.833	0.00	0.33	0.857	o	|	|	|	|	1.88
45.917	0.00	0.33	0.854	o	|	|	|	|	1.88
46.000	0.00	0.33	0.852	o	|	|	|	|	1.87
46.083	0.00	0.33	0.850	o	|	|	|	|	1.87
46.167	0.00	0.33	0.848	o	|	|	|	|	1.86
46.250	0.00	0.33	0.845	o	|	|	|	|	1.86
46.333	0.00	0.33	0.843	o	|	|	|	|	1.85
46.417	0.00	0.33	0.841	o	|	|	|	|	1.85
46.500	0.00	0.33	0.839	o	|	|	|	|	1.84
46.583	0.00	0.32	0.836	o	|	|	|	|	1.84
46.667	0.00	0.32	0.834	o	|	|	|	|	1.83
46.750	0.00	0.32	0.832	o	|	|	|	|	1.83
46.833	0.00	0.32	0.830	o	|	|	|	|	1.83
46.917	0.00	0.32	0.827	o	|	|	|	|	1.82
47.000	0.00	0.32	0.825	o	|	|	|	|	1.82
47.083	0.00	0.32	0.823	o	|	|	|	|	1.81
47.167	0.00	0.32	0.821	o	|	|	|	|	1.81
47.250	0.00	0.32	0.819	o	|	|	|	|	1.80
47.333	0.00	0.32	0.816	o	|	|	|	|	1.80
47.417	0.00	0.32	0.814	o	|	|	|	|	1.79
47.500	0.00	0.32	0.812	o	|	|	|	|	1.79
47.583	0.00	0.32	0.810	o	|	|	|	|	1.78
47.667	0.00	0.32	0.808	o	|	|	|	|	1.78
47.750	0.00	0.32	0.805	o	|	|	|	|	1.78
47.833	0.00	0.32	0.803	o	|	|	|	|	1.77
47.917	0.00	0.32	0.801	o	|	|	|	|	1.77
48.000	0.00	0.32	0.799	o	|	|	|	|	1.76
48.083	0.00	0.32	0.797	o	|	|	|	|	1.76
48.167	0.00	0.31	0.794	o	|	|	|	|	1.75
48.250	0.00	0.31	0.792	o	|	|	|	|	1.75
48.333	0.00	0.31	0.790	o	|	|	|	|	1.74
48.417	0.00	0.31	0.788	o	|	|	|	|	1.74
48.500	0.00	0.31	0.786	o	|	|	|	|	1.73
48.583	0.00	0.31	0.784	o	|	|	|	|	1.73
48.667	0.00	0.31	0.782	o	|	|	|	|	1.73
48.750	0.00	0.31	0.779	o	|	|	|	|	1.72
48.833	0.00	0.31	0.777	o	|	|	|	|	1.72
48.917	0.00	0.31	0.775	o	|	|	|	|	1.71
49.000	0.00	0.31	0.773	o	|	|	|	|	1.71
49.083	0.00	0.31	0.771	o	|	|	|	|	1.70
49.167	0.00	0.31	0.769	o	|	|	|	|	1.70
49.250	0.00	0.31	0.767	o	|	|	|	|	1.69
49.333	0.00	0.31	0.764	o	|	|	|	|	1.69
49.417	0.00	0.31	0.762	o	|	|	|	|	1.69
49.500	0.00	0.31	0.760	o	|	|	|	|	1.68
49.583	0.00	0.31	0.758	o	|	|	|	|	1.68
49.667	0.00	0.31	0.756	o	|	|	|	|	1.67
49.750	0.00	0.30	0.754	o	|	|	|	|	1.67
49.833	0.00	0.30	0.752	o	|	|	|	|	1.66
49.917	0.00	0.30	0.750	o	|	|	|	|	1.66
50.000	0.00	0.30	0.748	o	|	|	|	|	1.66
50.083	0.00	0.30	0.746	o	|	|	|	|	1.65
50.167	0.00	0.30	0.744	o	|	|	|	|	1.65
50.250	0.00	0.30	0.741	o	|	|	|	|	1.64
50.333	0.00	0.30	0.739	o	|	|	|	|	1.64
50.417	0.00	0.30	0.737	o	|	|	|	|	1.63
50.500	0.00	0.30	0.735	o	|	|	|	|	1.63
50.583	0.00	0.30	0.733	o	|	|	|	|	1.63
50.667	0.00	0.30	0.731	o	|	|	|	|	1.62
50.750	0.00	0.30	0.729	o	|	|	|	|	1.62
50.833	0.00	0.30	0.727	o	|	|	|	|	1.61
50.917	0.00	0.30	0.725	o	|	|	|	|	1.61
51.000	0.00	0.30	0.723	o	|	|	|	|	1.60
51.083	0.00	0.30	0.721	o	|	|	|	|	1.60
51.167	0.00	0.30	0.719	o	|	|	|	|	1.60
51.250	0.00	0.30	0.717	o	|	|	|	|	1.59
51.333	0.00	0.29	0.715	o	|	|	|	|	1.59
51.417	0.00	0.29	0.713	o	|	|	|	|	1.58
51.500	0.00	0.29	0.711	o	|	|	|	|	1.58
51.583	0.00	0.29	0.709	o	|	|	|	|	1.57
51.667	0.00	0.29	0.707	o	|	|	|	|	1.57
51.750	0.00	0.29	0.705	o	|	|	|	|	1.57
51.833	0.00	0.29	0.703	o	|	|	|	|	1.56
51.917	0.00	0.29	0.701	o	|	|	|	|	1.56
52.000	0.00	0.29	0.699	o	|	|	|	|	1.55
52.083	0.00	0.29	0.697	o	|	|	|	|	1.55
52.167	0.00	0.29	0.695	o	|	|	|	|	1.55
52.250	0.00	0.29	0.693	o	|	|	|	|	1.54
52.333	0.00	0.29	0.691	o	|	|	|	|	1.54
52.417	0.00	0.29	0.689	o	|	|	|	|	1.53
52.500	0.00	0.29	0.687	o	|	|	|	|	1.53
52.583	0.00	0.29	0.685	o	|	|	|	|	1.53
52.667	0.00	0.29	0.683	o	|	|	|	|	1.52
52.750	0.00	0.29	0.681	o	|	|	|	|	1.52
52.833	0.00	0.29	0.679	o	|	|	|	|	1.51
52.917	0.00	0.29	0.677	o	|	|	|	|	1.51
53.000	0.00	0.29	0.675	o	|	|	|	|	1.50

53.083	0.00	0.28	0.673	o	|	|	|	|	1.50
53.167	0.00	0.28	0.671	o	|	|	|	|	1.50
53.250	0.00	0.28	0.669	o	|	|	|	|	1.49
53.333	0.00	0.28	0.667	o	|	|	|	|	1.49
53.417	0.00	0.28	0.665	o	|	|	|	|	1.48
53.500	0.00	0.28	0.663	o	|	|	|	|	1.48
53.583	0.00	0.28	0.661	o	|	|	|	|	1.48
53.667	0.00	0.28	0.659	o	|	|	|	|	1.47
53.750	0.00	0.28	0.657	o	|	|	|	|	1.47
53.833	0.00	0.28	0.655	o	|	|	|	|	1.46
53.917	0.00	0.28	0.653	o	|	|	|	|	1.46
54.000	0.00	0.28	0.651	o	|	|	|	|	1.46
54.083	0.00	0.28	0.650	o	|	|	|	|	1.45
54.167	0.00	0.28	0.648	o	|	|	|	|	1.45
54.250	0.00	0.28	0.646	o	|	|	|	|	1.44
54.333	0.00	0.28	0.644	o	|	|	|	|	1.44
54.417	0.00	0.28	0.642	o	|	|	|	|	1.44
54.500	0.00	0.28	0.640	o	|	|	|	|	1.43
54.583	0.00	0.28	0.638	o	|	|	|	|	1.43
54.667	0.00	0.28	0.636	o	|	|	|	|	1.42
54.750	0.00	0.28	0.634	o	|	|	|	|	1.42
54.833	0.00	0.27	0.632	o	|	|	|	|	1.42
54.917	0.00	0.27	0.631	o	|	|	|	|	1.41
55.000	0.00	0.27	0.629	o	|	|	|	|	1.41
55.083	0.00	0.27	0.627	o	|	|	|	|	1.41
55.167	0.00	0.27	0.625	o	|	|	|	|	1.40
55.250	0.00	0.27	0.623	o	|	|	|	|	1.40
55.333	0.00	0.27	0.621	o	|	|	|	|	1.39
55.417	0.00	0.27	0.619	o	|	|	|	|	1.39
55.500	0.00	0.27	0.617	o	|	|	|	|	1.39
55.583	0.00	0.27	0.616	o	|	|	|	|	1.38
55.667	0.00	0.27	0.614	o	|	|	|	|	1.38
55.750	0.00	0.27	0.612	o	|	|	|	|	1.37
55.833	0.00	0.27	0.610	o	|	|	|	|	1.37
55.917	0.00	0.27	0.608	o	|	|	|	|	1.37
56.000	0.00	0.27	0.606	o	|	|	|	|	1.36
56.083	0.00	0.27	0.604	o	|	|	|	|	1.36
56.167	0.00	0.27	0.603	o	|	|	|	|	1.36
56.250	0.00	0.27	0.601	o	|	|	|	|	1.35
56.333	0.00	0.27	0.599	o	|	|	|	|	1.35
56.417	0.00	0.27	0.597	o	|	|	|	|	1.34
56.500	0.00	0.27	0.595	o	|	|	|	|	1.34
56.583	0.00	0.27	0.593	o	|	|	|	|	1.34
56.667	0.00	0.26	0.592	o	|	|	|	|	1.33
56.750	0.00	0.26	0.590	o	|	|	|	|	1.33
56.833	0.00	0.26	0.588	o	|	|	|	|	1.32
56.917	0.00	0.26	0.586	o	|	|	|	|	1.32
57.000	0.00	0.26	0.584	o	|	|	|	|	1.32
57.083	0.00	0.26	0.582	o	|	|	|	|	1.31
57.167	0.00	0.26	0.581	o	|	|	|	|	1.31
57.250	0.00	0.26	0.579	o	|	|	|	|	1.31
57.333	0.00	0.26	0.577	o	|	|	|	|	1.30
57.417	0.00	0.26	0.575	o	|	|	|	|	1.30
57.500	0.00	0.26	0.573	o	|	|	|	|	1.30
57.583	0.00	0.26	0.572	o	|	|	|	|	1.29
57.667	0.00	0.26	0.570	o	|	|	|	|	1.29
57.750	0.00	0.26	0.568	o	|	|	|	|	1.28
57.833	0.00	0.26	0.566	o	|	|	|	|	1.28
57.917	0.00	0.26	0.565	o	|	|	|	|	1.28
58.000	0.00	0.26	0.563	o	|	|	|	|	1.27
58.083	0.00	0.26	0.561	o	|	|	|	|	1.27
58.167	0.00	0.26	0.559	o	|	|	|	|	1.27
58.250	0.00	0.26	0.557	o	|	|	|	|	1.26
58.333	0.00	0.26	0.556	o	|	|	|	|	1.26
58.417	0.00	0.26	0.554	o	|	|	|	|	1.25
58.500	0.00	0.25	0.552	o	|	|	|	|	1.25
58.583	0.00	0.25	0.550	o	|	|	|	|	1.25
58.667	0.00	0.25	0.549	o	|	|	|	|	1.24
58.750	0.00	0.25	0.547	o	|	|	|	|	1.24
58.833	0.00	0.25	0.545	o	|	|	|	|	1.24
58.917	0.00	0.25	0.543	o	|	|	|	|	1.23
59.000	0.00	0.25	0.542	o	|	|	|	|	1.23
59.083	0.00	0.25	0.540	o	|	|	|	|	1.23
59.167	0.00	0.25	0.538	o	|	|	|	|	1.22
59.250	0.00	0.25	0.537	o	|	|	|	|	1.22
59.333	0.00	0.25	0.535	o	|	|	|	|	1.21
59.417	0.00	0.25	0.533	o	|	|	|	|	1.21
59.500	0.00	0.25	0.531	o	|	|	|	|	1.21
59.583	0.00	0.25	0.530	o	|	|	|	|	1.20
59.667	0.00	0.25	0.528	o	|	|	|	|	1.20
59.750	0.00	0.25	0.526	o	|	|	|	|	1.20
59.833	0.00	0.25	0.525	o	|	|	|	|	1.19
59.917	0.00	0.25	0.523	o	|	|	|	|	1.19
60.000	0.00	0.25	0.521	o	|	|	|	|	1.19
60.083	0.00	0.25	0.519	o	|	|	|	|	1.18
60.167	0.00	0.25	0.518	o	|	|	|	|	1.18
60.250	0.00	0.25	0.516	o	|	|	|	|	1.18
60.333	0.00	0.25	0.514	o	|	|	|	|	1.17

60.417	0.00	0.25	0.513	o	|	|	|	1.17
60.500	0.00	0.24	0.511	o	|	|	|	1.17
60.583	0.00	0.24	0.509	o	|	|	|	1.16
60.667	0.00	0.24	0.508	o	|	|	|	1.16
60.750	0.00	0.24	0.506	o	|	|	|	1.16
60.833	0.00	0.24	0.504	o	|	|	|	1.15
60.917	0.00	0.24	0.503	o	|	|	|	1.15
61.000	0.00	0.24	0.501	o	|	|	|	1.14
61.083	0.00	0.24	0.499	o	|	|	|	1.14
61.167	0.00	0.24	0.498	o	|	|	|	1.14
61.250	0.00	0.24	0.496	o	|	|	|	1.13
61.333	0.00	0.24	0.494	o	|	|	|	1.13
61.417	0.00	0.24	0.493	o	|	|	|	1.13
61.500	0.00	0.24	0.491	o	|	|	|	1.12
61.583	0.00	0.24	0.489	o	|	|	|	1.12
61.667	0.00	0.24	0.488	o	|	|	|	1.12
61.750	0.00	0.24	0.486	o	|	|	|	1.11
61.833	0.00	0.24	0.484	o	|	|	|	1.11
61.917	0.00	0.24	0.483	o	|	|	|	1.11
62.000	0.00	0.24	0.481	o	|	|	|	1.10
62.083	0.00	0.24	0.479	o	|	|	|	1.10
62.167	0.00	0.24	0.478	o	|	|	|	1.10
62.250	0.00	0.24	0.476	o	|	|	|	1.09
62.333	0.00	0.24	0.475	o	|	|	|	1.09
62.417	0.00	0.24	0.473	o	|	|	|	1.09
62.500	0.00	0.23	0.471	o	|	|	|	1.08
62.583	0.00	0.23	0.470	o	|	|	|	1.08
62.667	0.00	0.23	0.468	o	|	|	|	1.08
62.750	0.00	0.23	0.466	o	|	|	|	1.07
62.833	0.00	0.23	0.465	o	|	|	|	1.07
62.917	0.00	0.23	0.463	o	|	|	|	1.07
63.000	0.00	0.23	0.462	o	|	|	|	1.06
63.083	0.00	0.23	0.460	o	|	|	|	1.06
63.167	0.00	0.23	0.458	o	|	|	|	1.06
63.250	0.00	0.23	0.457	o	|	|	|	1.05
63.333	0.00	0.23	0.455	o	|	|	|	1.05
63.417	0.00	0.23	0.454	o	|	|	|	1.05
63.500	0.00	0.23	0.452	o	|	|	|	1.04
63.583	0.00	0.23	0.450	o	|	|	|	1.04
63.667	0.00	0.23	0.449	o	|	|	|	1.04
63.750	0.00	0.23	0.447	o	|	|	|	1.03
63.833	0.00	0.23	0.446	o	|	|	|	1.03
63.917	0.00	0.23	0.444	o	|	|	|	1.03
64.000	0.00	0.23	0.443	o	|	|	|	1.02
64.083	0.00	0.23	0.441	o	|	|	|	1.02
64.167	0.00	0.23	0.439	o	|	|	|	1.02
64.250	0.00	0.23	0.438	o	|	|	|	1.01
64.333	0.00	0.23	0.436	o	|	|	|	1.01
64.417	0.00	0.23	0.435	o	|	|	|	1.01
64.500	0.00	0.23	0.433	o	|	|	|	1.00
64.583	0.00	0.23	0.432	o	|	|	|	1.00
64.667	0.00	0.22	0.430	o	|	|	|	1.00
64.750	0.00	0.22	0.429	o	|	|	|	0.99
64.833	0.00	0.22	0.427	o	|	|	|	0.99
64.917	0.00	0.22	0.426	o	|	|	|	0.99
65.000	0.00	0.22	0.424	o	|	|	|	0.98
65.083	0.00	0.22	0.422	o	|	|	|	0.98
65.167	0.00	0.22	0.421	o	|	|	|	0.98
65.250	0.00	0.22	0.419	o	|	|	|	0.97
65.333	0.00	0.22	0.418	o	|	|	|	0.97
65.417	0.00	0.22	0.416	o	|	|	|	0.97
65.500	0.00	0.22	0.415	o	|	|	|	0.96
65.583	0.00	0.22	0.413	o	|	|	|	0.96
65.667	0.00	0.22	0.412	o	|	|	|	0.96
65.750	0.00	0.21	0.411	o	|	|	|	0.95
65.833	0.00	0.21	0.409	o	|	|	|	0.95
65.917	0.00	0.21	0.408	o	|	|	|	0.95
66.000	0.00	0.21	0.406	o	|	|	|	0.94
66.083	0.00	0.21	0.405	o	|	|	|	0.94
66.167	0.00	0.21	0.403	o	|	|	|	0.94
66.250	0.00	0.21	0.402	o	|	|	|	0.93
66.333	0.00	0.21	0.400	o	|	|	|	0.93
66.417	0.00	0.21	0.399	o	|	|	|	0.93
66.500	0.00	0.21	0.397	o	|	|	|	0.92
66.583	0.00	0.21	0.396	o	|	|	|	0.92
66.667	0.00	0.21	0.395	o	|	|	|	0.92
66.750	0.00	0.21	0.393	o	|	|	|	0.91
66.833	0.00	0.20	0.392	o	|	|	|	0.91
66.917	0.00	0.20	0.390	o	|	|	|	0.91
67.000	0.00	0.20	0.389	o	|	|	|	0.90
67.083	0.00	0.20	0.388	o	|	|	|	0.90
67.167	0.00	0.20	0.386	o	|	|	|	0.90
67.250	0.00	0.20	0.385	o	|	|	|	0.89
67.333	0.00	0.20	0.383	o	|	|	|	0.89
67.417	0.00	0.20	0.382	o	|	|	|	0.89
67.500	0.00	0.20	0.381	o	|	|	|	0.88
67.583	0.00	0.20	0.379	o	|	|	|	0.88
67.667	0.00	0.20	0.378	o	|	|	|	0.88

67.750	0.00	0.20	0.377	o	|	|	|	0.87
67.833	0.00	0.20	0.375	o	|	|	|	0.87
67.917	0.00	0.20	0.374	o	|	|	|	0.87
68.000	0.00	0.19	0.373	o	|	|	|	0.86
68.083	0.00	0.19	0.371	o	|	|	|	0.86
68.167	0.00	0.19	0.370	o	|	|	|	0.86
68.250	0.00	0.19	0.369	o	|	|	|	0.86
68.333	0.00	0.19	0.367	o	|	|	|	0.85
68.417	0.00	0.19	0.366	o	|	|	|	0.85
68.500	0.00	0.19	0.365	o	|	|	|	0.85
68.583	0.00	0.19	0.363	o	|	|	|	0.84
68.667	0.00	0.19	0.362	o	|	|	|	0.84
68.750	0.00	0.19	0.361	o	|	|	|	0.84
68.833	0.00	0.19	0.359	o	|	|	|	0.83
68.917	0.00	0.19	0.358	o	|	|	|	0.83
69.000	0.00	0.19	0.357	o	|	|	|	0.83
69.083	0.00	0.19	0.356	o	|	|	|	0.82
69.167	0.00	0.18	0.354	o	|	|	|	0.82
69.250	0.00	0.18	0.353	o	|	|	|	0.82
69.333	0.00	0.18	0.352	o	|	|	|	0.82
69.417	0.00	0.18	0.350	o	|	|	|	0.81
69.500	0.00	0.18	0.349	o	|	|	|	0.81
69.583	0.00	0.18	0.348	o	|	|	|	0.81
69.667	0.00	0.18	0.347	o	|	|	|	0.80
69.750	0.00	0.18	0.345	o	|	|	|	0.80
69.833	0.00	0.18	0.344	o	|	|	|	0.80
69.917	0.00	0.18	0.343	o	|	|	|	0.80
70.000	0.00	0.18	0.342	o	|	|	|	0.79
70.083	0.00	0.18	0.341	o	|	|	|	0.79
70.167	0.00	0.18	0.339	o	|	|	|	0.79
70.250	0.00	0.18	0.338	o	|	|	|	0.78
70.333	0.00	0.18	0.337	o	|	|	|	0.78
70.417	0.00	0.18	0.336	o	|	|	|	0.78
70.500	0.00	0.17	0.334	o	|	|	|	0.78
70.583	0.00	0.17	0.333	o	|	|	|	0.77
70.667	0.00	0.17	0.332	o	|	|	|	0.77
70.750	0.00	0.17	0.331	o	|	|	|	0.77
70.833	0.00	0.17	0.330	o	|	|	|	0.76
70.917	0.00	0.17	0.328	o	|	|	|	0.76
71.000	0.00	0.17	0.327	o	|	|	|	0.76
71.083	0.00	0.17	0.326	o	|	|	|	0.76
71.167	0.00	0.17	0.325	o	|	|	|	0.75
71.250	0.00	0.17	0.324	o	|	|	|	0.75
71.333	0.00	0.17	0.323	o	|	|	|	0.75
71.417	0.00	0.17	0.321	o	|	|	|	0.75
71.500	0.00	0.17	0.320	o	|	|	|	0.74
71.583	0.00	0.17	0.319	o	|	|	|	0.74
71.667	0.00	0.17	0.318	o	|	|	|	0.74
71.750	0.00	0.17	0.317	o	|	|	|	0.74
71.833	0.00	0.16	0.316	o	|	|	|	0.73
71.917	0.00	0.16	0.315	o	|	|	|	0.73
72.000	0.00	0.16	0.313	o	|	|	|	0.73
72.083	0.00	0.16	0.312	o	|	|	|	0.72
72.167	0.00	0.16	0.311	o	|	|	|	0.72
72.250	0.00	0.16	0.310	o	|	|	|	0.72
72.333	0.00	0.16	0.309	o	|	|	|	0.72
72.417	0.00	0.16	0.308	o	|	|	|	0.71
72.500	0.00	0.16	0.307	o	|	|	|	0.71
72.583	0.00	0.16	0.306	o	|	|	|	0.71
72.667	0.00	0.16	0.305	o	|	|	|	0.71
72.750	0.00	0.16	0.303	o	|	|	|	0.70
72.833	0.00	0.16	0.302	o	|	|	|	0.70
72.917	0.00	0.16	0.301	o	|	|	|	0.70
73.000	0.00	0.16	0.300	o	|	|	|	0.70
73.083	0.00	0.16	0.299	o	|	|	|	0.69
73.167	0.00	0.16	0.298	o	|	|	|	0.69
73.250	0.00	0.16	0.297	o	|	|	|	0.69
73.333	0.00	0.15	0.296	o	|	|	|	0.69
73.417	0.00	0.15	0.295	o	|	|	|	0.68
73.500	0.00	0.15	0.294	o	|	|	|	0.68
73.583	0.00	0.15	0.293	o	|	|	|	0.68
73.667	0.00	0.15	0.292	o	|	|	|	0.68
73.750	0.00	0.15	0.291	o	|	|	|	0.67
73.833	0.00	0.15	0.290	o	|	|	|	0.67
73.917	0.00	0.15	0.289	o	|	|	|	0.67
74.000	0.00	0.15	0.288	o	|	|	|	0.67
74.083	0.00	0.15	0.287	o	|	|	|	0.66
74.167	0.00	0.15	0.286	o	|	|	|	0.66
74.250	0.00	0.15	0.284	o	|	|	|	0.66
74.333	0.00	0.15	0.283	o	|	|	|	0.66
74.417	0.00	0.15	0.282	o	|	|	|	0.66
74.500	0.00	0.15	0.281	o	|	|	|	0.65
74.583	0.00	0.15	0.280	o	|	|	|	0.65
74.667	0.00	0.15	0.279	o	|	|	|	0.65
74.750	0.00	0.15	0.278	o	|	|	|	0.65
74.833	0.00	0.14	0.277	o	|	|	|	0.64
74.917	0.00	0.14	0.276	o	|	|	|	0.64
75.000	0.00	0.14	0.275	o	|	|	|	0.64

75.083	0.00	0.14	0.274	o	|	|	|	0.64
75.167	0.00	0.14	0.273	o	|	|	|	0.63
75.250	0.00	0.14	0.272	o	|	|	|	0.63
75.333	0.00	0.14	0.271	o	|	|	|	0.63
75.417	0.00	0.14	0.271	o	|	|	|	0.63
75.500	0.00	0.14	0.270	o	|	|	|	0.63
75.583	0.00	0.14	0.269	o	|	|	|	0.62
75.667	0.00	0.14	0.268	o	|	|	|	0.62
75.750	0.00	0.14	0.267	o	|	|	|	0.62
75.833	0.00	0.14	0.266	o	|	|	|	0.62
75.917	0.00	0.14	0.265	o	|	|	|	0.61
76.000	0.00	0.14	0.264	o	|	|	|	0.61
76.083	0.00	0.14	0.263	o	|	|	|	0.61
76.167	0.00	0.14	0.262	o	|	|	|	0.61
76.250	0.00	0.14	0.261	o	|	|	|	0.61
76.333	0.00	0.14	0.260	o	|	|	|	0.60
76.417	0.00	0.14	0.259	o	|	|	|	0.60
76.500	0.00	0.13	0.258	o	|	|	|	0.60
76.583	0.00	0.13	0.257	o	|	|	|	0.60
76.667	0.00	0.13	0.256	o	|	|	|	0.59
76.750	0.00	0.13	0.255	o	|	|	|	0.59
76.833	0.00	0.13	0.254	o	|	|	|	0.59
76.917	0.00	0.13	0.254	o	|	|	|	0.59
77.000	0.00	0.13	0.253	o	|	|	|	0.59
77.083	0.00	0.13	0.252	o	|	|	|	0.58
77.167	0.00	0.13	0.251	o	|	|	|	0.58
77.250	0.00	0.13	0.250	o	|	|	|	0.58
77.333	0.00	0.13	0.249	o	|	|	|	0.58
77.417	0.00	0.13	0.248	o	|	|	|	0.58
77.500	0.00	0.13	0.247	o	|	|	|	0.57
77.583	0.00	0.13	0.246	o	|	|	|	0.57
77.667	0.00	0.13	0.245	o	|	|	|	0.57
77.750	0.00	0.13	0.245	o	|	|	|	0.57
77.833	0.00	0.13	0.244	o	|	|	|	0.57
77.917	0.00	0.13	0.243	o	|	|	|	0.56
78.000	0.00	0.13	0.242	o	|	|	|	0.56
78.083	0.00	0.13	0.241	o	|	|	|	0.56
78.167	0.00	0.13	0.240	o	|	|	|	0.56
78.250	0.00	0.12	0.239	o	|	|	|	0.56
78.333	0.00	0.12	0.239	o	|	|	|	0.55
78.417	0.00	0.12	0.238	o	|	|	|	0.55
78.500	0.00	0.12	0.237	o	|	|	|	0.55
78.583	0.00	0.12	0.236	o	|	|	|	0.55
78.667	0.00	0.12	0.235	o	|	|	|	0.55
78.750	0.00	0.12	0.234	o	|	|	|	0.54
78.833	0.00	0.12	0.233	o	|	|	|	0.54
78.917	0.00	0.12	0.233	o	|	|	|	0.54
79.000	0.00	0.12	0.232	o	|	|	|	0.54
79.083	0.00	0.12	0.231	o	|	|	|	0.54
79.167	0.00	0.12	0.230	o	|	|	|	0.53
79.250	0.00	0.12	0.229	o	|	|	|	0.53
79.333	0.00	0.12	0.228	o	|	|	|	0.53
79.417	0.00	0.12	0.228	o	|	|	|	0.53
79.500	0.00	0.12	0.227	o	|	|	|	0.53
79.583	0.00	0.12	0.226	o	|	|	|	0.52
79.667	0.00	0.12	0.225	o	|	|	|	0.52
79.750	0.00	0.12	0.224	o	|	|	|	0.52
79.833	0.00	0.12	0.224	o	|	|	|	0.52
79.917	0.00	0.12	0.223	o	|	|	|	0.52
80.000	0.00	0.12	0.222	o	|	|	|	0.52
80.083	0.00	0.12	0.221	o	|	|	|	0.51
80.167	0.00	0.12	0.220	o	|	|	|	0.51
80.250	0.00	0.11	0.220	o	|	|	|	0.51
80.333	0.00	0.11	0.219	o	|	|	|	0.51
80.417	0.00	0.11	0.218	o	|	|	|	0.51
80.500	0.00	0.11	0.217	o	|	|	|	0.50
80.583	0.00	0.11	0.216	o	|	|	|	0.50
80.667	0.00	0.11	0.216	o	|	|	|	0.50
80.750	0.00	0.11	0.215	o	|	|	|	0.50
80.833	0.00	0.11	0.214	o	|	|	|	0.50
80.917	0.00	0.11	0.213	o	|	|	|	0.50
81.000	0.00	0.11	0.213	o	|	|	|	0.49
81.083	0.00	0.11	0.212	o	|	|	|	0.49
81.167	0.00	0.11	0.211	o	|	|	|	0.49
81.250	0.00	0.11	0.210	o	|	|	|	0.49
81.333	0.00	0.11	0.210	o	|	|	|	0.49
81.417	0.00	0.11	0.209	o	|	|	|	0.48
81.500	0.00	0.11	0.208	o	|	|	|	0.48
81.583	0.00	0.11	0.207	o	|	|	|	0.48
81.667	0.00	0.11	0.207	o	|	|	|	0.48
81.750	0.00	0.11	0.206	o	|	|	|	0.48
81.833	0.00	0.11	0.205	o	|	|	|	0.48
81.917	0.00	0.11	0.204	o	|	|	|	0.47
82.000	0.00	0.11	0.204	o	|	|	|	0.47
82.083	0.00	0.11	0.203	o	|	|	|	0.47
82.167	0.00	0.11	0.202	o	|	|	|	0.47
82.250	0.00	0.11	0.201	o	|	|	|	0.47
82.333	0.00	0.10	0.201	o	|	|	|	0.47

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82.417    0.00    0.10      0.200  o       |       |       |       |     0.46
82.500    0.00    0.10      0.199  o       |       |       |       |     0.46
82.583    0.00    0.10      0.199  o       |       |       |       |     0.46
82.667    0.00    0.10      0.198  o       |       |       |       |     0.46
82.750    0.00    0.10      0.197  o       |       |       |       |     0.46
82.833    0.00    0.10      0.196  o       |       |       |       |     0.46
82.917    0.00    0.10      0.196  o       |       |       |       |     0.45
83.000    0.00    0.10      0.195  o       |       |       |       |     0.45
83.083    0.00    0.10      0.194  o       |       |       |       |     0.45
83.167    0.00    0.10      0.194  o       |       |       |       |     0.45
83.250    0.00    0.10      0.193  o       |       |       |       |     0.45
83.333    0.00    0.10      0.192  o       |       |       |       |     0.45
83.417    0.00    0.10      0.192  o       |       |       |       |     0.44

      Remaining water in basin =    0.19 (Ac.Ft)


      ****************************HYDROGRAPH DATA****************************
                    Number of intervals =  1001
                    Time interval =    5.0 (Min.)
                    Maximum/Peak flow rate =       12.489 (CFS)
                    Total volume =       6.608 (Ac.Ft)
              Status of hydrographs being held in storage
                         Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      ***********************************************************************

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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 06/03/24

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: pro21001100.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    17
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =      149.688 (CFS)
               Total volume =       4.724 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
*************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
___________________________________________________________________________

User entry of depth-outflow-storage data
---------------------------------------------------------------------
Total number of inflow hydrograph intervals = 17
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
---------------------------------------------------------------------
---------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
---------------------------------------------------------------------
---------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
---------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.431      0.225      0.430        0.432
   2.000      0.914      0.344      0.913        0.915
   3.000      1.451      0.991      1.448        1.454
   4.000      2.049      1.417      2.044        2.054
   5.000      2.712      1.731      2.706        2.718
   5.250      2.888      1.801      2.882        2.894
   5.500      3.069     17.046      3.010        3.128
   6.000      3.443    225.078      2.668        4.218
---------------------------------------------------------------------
               Hydrograph Detention Basin Routing
---------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
---------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                  Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0      37.4   74.84  112.27  149.69 (Ft.)
 0.083    4.73    0.01      0.016  OI      |       |       |       |     0.04
 0.167   14.64    0.04      0.083  O  I    |       |       |       |     0.19
 0.250   20.61    0.11      0.204  O   I   |       |       |       |     0.47
 0.333   24.11    0.19      0.357  O    I  |       |       |       |     0.83
 0.417   27.69    0.25      0.533  O    I  |       |       |       |     1.21
 0.500   32.70    0.30      0.740  O     I |       |       |       |     1.64
 0.583   38.82    0.43      0.983  O       I       |       |       |     2.13
 0.667   47.23    0.78      1.275  O       | I     |       |       |     2.67
 0.750   68.41    1.14      1.667  O       |     I |       |       |     3.36
 0.833  132.61    1.56      2.350  O       |       |       |   I   |     4.45
 0.917  149.69   53.10      3.134  |       |  O    |       |      I|     5.59
 1.000   67.08  125.75      3.264  |       |     I |       | O     |     5.76
 1.083   33.14   26.37      3.086  |    O I|       |       |       |     5.52
 1.167   14.50   23.03      3.080  |  IO   |       |       |       |     5.51
 1.250    7.87   13.77      3.030  |IO     |       |       |       |     5.45
 1.333    1.64    9.72      2.982  I O    |       |       |       |     5.38
 1.417    0.44    5.82      2.936  IO     |       |       |       |     5.32
 1.500    0.00    3.30      2.906  O      |       |       |       |     5.27
```

1.583	0.00	1.82	2.888	o	|	|	|	|	5.25
1.667	0.00	1.80	2.876	o	|	|	|	|	5.23
1.750	0.00	1.79	2.863	o	|	|	|	|	5.22
1.833	0.00	1.79	2.851	o	|	|	|	|	5.20
1.917	0.00	1.78	2.839	o	|	|	|	|	5.18
2.000	0.00	1.78	2.827	o	|	|	|	|	5.16
2.083	0.00	1.77	2.814	o	|	|	|	|	5.15
2.167	0.00	1.77	2.802	o	|	|	|	|	5.13
2.250	0.00	1.76	2.790	o	|	|	|	|	5.11
2.333	0.00	1.76	2.778	o	|	|	|	|	5.09
2.417	0.00	1.75	2.766	o	|	|	|	|	5.08
2.500	0.00	1.75	2.754	o	|	|	|	|	5.06
2.583	0.00	1.74	2.742	o	|	|	|	|	5.04
2.667	0.00	1.74	2.730	o	|	|	|	|	5.03
2.750	0.00	1.73	2.718	o	|	|	|	|	5.01
2.833	0.00	1.73	2.706	o	|	|	|	|	4.99
2.917	0.00	1.72	2.694	o	|	|	|	|	4.97
3.000	0.00	1.72	2.682	o	|	|	|	|	4.95
3.083	0.00	1.71	2.670	o	|	|	|	|	4.94
3.167	0.00	1.71	2.659	o	|	|	|	|	4.92
3.250	0.00	1.70	2.647	o	|	|	|	|	4.90
3.333	0.00	1.69	2.635	o	|	|	|	|	4.88
3.417	0.00	1.69	2.623	o	|	|	|	|	4.87
3.500	0.00	1.68	2.612	o	|	|	|	|	4.85
3.583	0.00	1.68	2.600	o	|	|	|	|	4.83
3.667	0.00	1.67	2.589	o	|	|	|	|	4.81
3.750	0.00	1.67	2.577	o	|	|	|	|	4.80
3.833	0.00	1.66	2.566	o	|	|	|	|	4.78
3.917	0.00	1.66	2.554	o	|	|	|	|	4.76
4.000	0.00	1.65	2.543	o	|	|	|	|	4.75
4.083	0.00	1.65	2.532	o	|	|	|	|	4.73
4.167	0.00	1.64	2.520	o	|	|	|	|	4.71
4.250	0.00	1.63	2.509	o	|	|	|	|	4.69
4.333	0.00	1.63	2.498	o	|	|	|	|	4.68
4.417	0.00	1.62	2.487	o	|	|	|	|	4.66
4.500	0.00	1.62	2.475	o	|	|	|	|	4.64
4.583	0.00	1.61	2.464	o	|	|	|	|	4.63
4.667	0.00	1.61	2.453	o	|	|	|	|	4.61
4.750	0.00	1.60	2.442	o	|	|	|	|	4.59
4.833	0.00	1.60	2.431	o	|	|	|	|	4.58
4.917	0.00	1.59	2.420	o	|	|	|	|	4.56
5.000	0.00	1.59	2.409	o	|	|	|	|	4.54
5.083	0.00	1.58	2.398	o	|	|	|	|	4.53
5.167	0.00	1.58	2.387	o	|	|	|	|	4.51
5.250	0.00	1.57	2.377	o	|	|	|	|	4.49
5.333	0.00	1.57	2.366	o	|	|	|	|	4.48
5.417	0.00	1.56	2.355	o	|	|	|	|	4.46
5.500	0.00	1.56	2.344	o	|	|	|	|	4.45
5.583	0.00	1.55	2.333	o	|	|	|	|	4.43
5.667	0.00	1.55	2.323	o	|	|	|	|	4.41
5.750	0.00	1.54	2.312	o	|	|	|	|	4.40
5.833	0.00	1.54	2.302	o	|	|	|	|	4.38
5.917	0.00	1.53	2.291	o	|	|	|	|	4.37
6.000	0.00	1.53	2.280	o	|	|	|	|	4.35
6.083	0.00	1.52	2.270	o	|	|	|	|	4.33
6.167	0.00	1.52	2.260	o	|	|	|	|	4.32
6.250	0.00	1.51	2.249	o	|	|	|	|	4.30
6.333	0.00	1.51	2.239	o	|	|	|	|	4.29
6.417	0.00	1.50	2.228	o	|	|	|	|	4.27
6.500	0.00	1.50	2.218	o	|	|	|	|	4.25
6.583	0.00	1.49	2.208	o	|	|	|	|	4.24
6.667	0.00	1.49	2.197	o	|	|	|	|	4.22
6.750	0.00	1.48	2.187	o	|	|	|	|	4.21
6.833	0.00	1.48	2.177	o	|	|	|	|	4.19
6.917	0.00	1.47	2.167	o	|	|	|	|	4.18
7.000	0.00	1.47	2.157	o	|	|	|	|	4.16
7.083	0.00	1.46	2.147	o	|	|	|	|	4.15
7.167	0.00	1.46	2.137	o	|	|	|	|	4.13
7.250	0.00	1.45	2.127	o	|	|	|	|	4.12
7.333	0.00	1.45	2.117	o	|	|	|	|	4.10
7.417	0.00	1.44	2.107	o	|	|	|	|	4.09
7.500	0.00	1.44	2.097	o	|	|	|	|	4.07
7.583	0.00	1.43	2.087	o	|	|	|	|	4.06
7.667	0.00	1.43	2.077	o	|	|	|	|	4.04
7.750	0.00	1.43	2.067	o	|	|	|	|	4.03
7.833	0.00	1.42	2.057	o	|	|	|	|	4.01
7.917	0.00	1.42	2.048	o	|	|	|	|	4.00
8.000	0.00	1.41	2.038	o	|	|	|	|	3.98
8.083	0.00	1.40	2.028	o	|	|	|	|	3.97
8.167	0.00	1.40	2.018	o	|	|	|	|	3.95
8.250	0.00	1.39	2.009	o	|	|	|	|	3.93
8.333	0.00	1.38	1.999	o	|	|	|	|	3.92
8.417	0.00	1.37	1.990	o	|	|	|	|	3.90
8.500	0.00	1.37	1.980	o	|	|	|	|	3.89
8.583	0.00	1.36	1.971	o	|	|	|	|	3.87
8.667	0.00	1.35	1.962	o	|	|	|	|	3.85

8.750	0.00	1.35	1.952	o	|	|	|	|	3.84
8.833	0.00	1.34	1.943	o	|	|	|	|	3.82
8.917	0.00	1.33	1.934	o	|	|	|	|	3.81
9.000	0.00	1.33	1.925	o	|	|	|	|	3.79
9.083	0.00	1.32	1.916	o	|	|	|	|	3.78
9.167	0.00	1.32	1.906	o	|	|	|	|	3.76
9.250	0.00	1.31	1.897	o	|	|	|	|	3.75
9.333	0.00	1.30	1.888	o	|	|	|	|	3.73
9.417	0.00	1.30	1.880	o	|	|	|	|	3.72
9.500	0.00	1.29	1.871	o	|	|	|	|	3.70
9.583	0.00	1.28	1.862	o	|	|	|	|	3.69
9.667	0.00	1.28	1.853	o	|	|	|	|	3.67
9.750	0.00	1.27	1.844	o	|	|	|	|	3.66
9.833	0.00	1.26	1.835	o	|	|	|	|	3.64
9.917	0.00	1.26	1.827	o	|	|	|	|	3.63
10.000	0.00	1.25	1.818	o	|	|	|	|	3.61
10.083	0.00	1.25	1.809	o	|	|	|	|	3.60
10.167	0.00	1.24	1.801	o	|	|	|	|	3.59
10.250	0.00	1.23	1.792	o	|	|	|	|	3.57
10.333	0.00	1.23	1.784	o	|	|	|	|	3.56
10.417	0.00	1.22	1.775	o	|	|	|	|	3.54
10.500	0.00	1.22	1.767	o	|	|	|	|	3.53
10.583	0.00	1.21	1.759	o	|	|	|	|	3.51
10.667	0.00	1.20	1.750	o	|	|	|	|	3.50
10.750	0.00	1.20	1.742	o	|	|	|	|	3.49
10.833	0.00	1.19	1.734	o	|	|	|	|	3.47
10.917	0.00	1.19	1.726	o	|	|	|	|	3.46
11.000	0.00	1.18	1.718	o	|	|	|	|	3.45
11.083	0.00	1.18	1.709	o	|	|	|	|	3.43
11.167	0.00	1.17	1.701	o	|	|	|	|	3.42
11.250	0.00	1.16	1.693	o	|	|	|	|	3.41
11.333	0.00	1.16	1.685	o	|	|	|	|	3.39
11.417	0.00	1.15	1.677	o	|	|	|	|	3.38
11.500	0.00	1.15	1.669	o	|	|	|	|	3.37
11.583	0.00	1.14	1.662	o	|	|	|	|	3.35
11.667	0.00	1.14	1.654	o	|	|	|	|	3.34
11.750	0.00	1.13	1.646	o	|	|	|	|	3.33
11.833	0.00	1.12	1.638	o	|	|	|	|	3.31
11.917	0.00	1.12	1.630	o	|	|	|	|	3.30
12.000	0.00	1.11	1.623	o	|	|	|	|	3.29
12.083	0.00	1.11	1.615	o	|	|	|	|	3.27
12.167	0.00	1.10	1.608	o	|	|	|	|	3.26
12.250	0.00	1.10	1.600	o	|	|	|	|	3.25
12.333	0.00	1.09	1.592	o	|	|	|	|	3.24
12.417	0.00	1.09	1.585	o	|	|	|	|	3.22
12.500	0.00	1.08	1.577	o	|	|	|	|	3.21
12.583	0.00	1.08	1.570	o	|	|	|	|	3.20
12.667	0.00	1.07	1.563	o	|	|	|	|	3.19
12.750	0.00	1.07	1.555	o	|	|	|	|	3.17
12.833	0.00	1.06	1.548	o	|	|	|	|	3.16
12.917	0.00	1.05	1.541	o	|	|	|	|	3.15
13.000	0.00	1.05	1.533	o	|	|	|	|	3.14
13.083	0.00	1.04	1.526	o	|	|	|	|	3.13
13.167	0.00	1.04	1.519	o	|	|	|	|	3.11
13.250	0.00	1.03	1.512	o	|	|	|	|	3.10
13.333	0.00	1.03	1.505	o	|	|	|	|	3.09
13.417	0.00	1.02	1.498	o	|	|	|	|	3.08
13.500	0.00	1.02	1.491	o	|	|	|	|	3.07
13.583	0.00	1.01	1.484	o	|	|	|	|	3.05
13.667	0.00	1.01	1.477	o	|	|	|	|	3.04
13.750	0.00	1.00	1.470	o	|	|	|	|	3.03
13.833	0.00	1.00	1.463	o	|	|	|	|	3.02
13.917	0.00	0.99	1.456	o	|	|	|	|	3.01
14.000	0.00	0.99	1.449	o	|	|	|	|	3.00
14.083	0.00	0.98	1.442	o	|	|	|	|	2.98
14.167	0.00	0.97	1.436	o	|	|	|	|	2.97
14.250	0.00	0.96	1.429	o	|	|	|	|	2.96
14.333	0.00	0.96	1.422	o	|	|	|	|	2.95
14.417	0.00	0.95	1.416	o	|	|	|	|	2.93
14.500	0.00	0.94	1.409	o	|	|	|	|	2.92
14.583	0.00	0.93	1.403	o	|	|	|	|	2.91
14.667	0.00	0.93	1.396	o	|	|	|	|	2.90
14.750	0.00	0.92	1.390	o	|	|	|	|	2.89
14.833	0.00	0.91	1.384	o	|	|	|	|	2.87
14.917	0.00	0.90	1.378	o	|	|	|	|	2.86
15.000	0.00	0.90	1.371	o	|	|	|	|	2.85
15.083	0.00	0.89	1.365	o	|	|	|	|	2.84
15.167	0.00	0.88	1.359	o	|	|	|	|	2.83
15.250	0.00	0.87	1.353	o	|	|	|	|	2.82
15.333	0.00	0.87	1.347	o	|	|	|	|	2.81
15.417	0.00	0.86	1.341	o	|	|	|	|	2.80
15.500	0.00	0.85	1.335	o	|	|	|	|	2.78
15.583	0.00	0.84	1.329	o	|	|	|	|	2.77
15.667	0.00	0.84	1.324	o	|	|	|	|	2.76
15.750	0.00	0.83	1.318	o	|	|	|	|	2.75
15.833	0.00	0.82	1.312	o	|	|	|	|	2.74

15.917	0.00	0.82	1.307	o	|	|	|	|	2.73
16.000	0.00	0.81	1.301	o	|	|	|	|	2.72
16.083	0.00	0.80	1.295	o	|	|	|	|	2.71
16.167	0.00	0.80	1.290	o	|	|	|	|	2.70
16.250	0.00	0.79	1.284	o	|	|	|	|	2.69
16.333	0.00	0.78	1.279	o	|	|	|	|	2.68
16.417	0.00	0.78	1.274	o	|	|	|	|	2.67
16.500	0.00	0.77	1.268	o	|	|	|	|	2.66
16.583	0.00	0.76	1.263	o	|	|	|	|	2.65
16.667	0.00	0.76	1.258	o	|	|	|	|	2.64
16.750	0.00	0.75	1.253	o	|	|	|	|	2.63
16.833	0.00	0.75	1.247	o	|	|	|	|	2.62
16.917	0.00	0.74	1.242	o	|	|	|	|	2.61
17.000	0.00	0.73	1.237	o	|	|	|	|	2.60
17.083	0.00	0.73	1.232	o	|	|	|	|	2.59
17.167	0.00	0.72	1.227	o	|	|	|	|	2.58
17.250	0.00	0.72	1.222	o	|	|	|	|	2.57
17.333	0.00	0.71	1.217	o	|	|	|	|	2.56
17.417	0.00	0.70	1.213	o	|	|	|	|	2.56
17.500	0.00	0.70	1.208	o	|	|	|	|	2.55
17.583	0.00	0.69	1.203	o	|	|	|	|	2.54
17.667	0.00	0.69	1.198	o	|	|	|	|	2.53
17.750	0.00	0.68	1.193	o	|	|	|	|	2.52
17.833	0.00	0.68	1.189	o	|	|	|	|	2.51
17.917	0.00	0.67	1.184	o	|	|	|	|	2.50
18.000	0.00	0.66	1.180	o	|	|	|	|	2.49
18.083	0.00	0.66	1.175	o	|	|	|	|	2.49
18.167	0.00	0.65	1.170	o	|	|	|	|	2.48
18.250	0.00	0.65	1.166	o	|	|	|	|	2.47
18.333	0.00	0.64	1.162	o	|	|	|	|	2.46
18.417	0.00	0.64	1.157	o	|	|	|	|	2.45
18.500	0.00	0.63	1.153	o	|	|	|	|	2.44
18.583	0.00	0.63	1.148	o	|	|	|	|	2.44
18.667	0.00	0.62	1.144	o	|	|	|	|	2.43
18.750	0.00	0.62	1.140	o	|	|	|	|	2.42
18.833	0.00	0.61	1.136	o	|	|	|	|	2.41
18.917	0.00	0.61	1.131	o	|	|	|	|	2.40
19.000	0.00	0.60	1.127	o	|	|	|	|	2.40
19.083	0.00	0.60	1.123	o	|	|	|	|	2.39
19.167	0.00	0.59	1.119	o	|	|	|	|	2.38
19.250	0.00	0.59	1.115	o	|	|	|	|	2.37
19.333	0.00	0.58	1.111	o	|	|	|	|	2.37
19.417	0.00	0.58	1.107	o	|	|	|	|	2.36
19.500	0.00	0.57	1.103	o	|	|	|	|	2.35
19.583	0.00	0.57	1.099	o	|	|	|	|	2.34
19.667	0.00	0.56	1.095	o	|	|	|	|	2.34
19.750	0.00	0.56	1.091	o	|	|	|	|	2.33
19.833	0.00	0.55	1.088	o	|	|	|	|	2.32
19.917	0.00	0.55	1.084	o	|	|	|	|	2.32
20.000	0.00	0.54	1.080	o	|	|	|	|	2.31
20.083	0.00	0.54	1.076	o	|	|	|	|	2.30
20.167	0.00	0.54	1.073	o	|	|	|	|	2.30
20.250	0.00	0.53	1.069	o	|	|	|	|	2.29
20.333	0.00	0.53	1.065	o	|	|	|	|	2.28
20.417	0.00	0.52	1.062	o	|	|	|	|	2.28
20.500	0.00	0.52	1.058	o	|	|	|	|	2.27
20.583	0.00	0.51	1.055	o	|	|	|	|	2.26
20.667	0.00	0.51	1.051	o	|	|	|	|	2.26
20.750	0.00	0.50	1.048	o	|	|	|	|	2.25
20.833	0.00	0.50	1.044	o	|	|	|	|	2.24
20.917	0.00	0.50	1.041	o	|	|	|	|	2.24
21.000	0.00	0.49	1.037	o	|	|	|	|	2.23
21.083	0.00	0.49	1.034	o	|	|	|	|	2.22
21.167	0.00	0.48	1.031	o	|	|	|	|	2.22
21.250	0.00	0.48	1.027	o	|	|	|	|	2.21
21.333	0.00	0.48	1.024	o	|	|	|	|	2.20
21.417	0.00	0.47	1.021	o	|	|	|	|	2.20
21.500	0.00	0.47	1.017	o	|	|	|	|	2.19
21.583	0.00	0.46	1.014	o	|	|	|	|	2.19
21.667	0.00	0.46	1.011	o	|	|	|	|	2.18
21.750	0.00	0.46	1.008	o	|	|	|	|	2.17
21.833	0.00	0.45	1.005	o	|	|	|	|	2.17
21.917	0.00	0.45	1.002	o	|	|	|	|	2.16
22.000	0.00	0.45	0.999	o	|	|	|	|	2.16
22.083	0.00	0.44	0.995	o	|	|	|	|	2.15
22.167	0.00	0.44	0.992	o	|	|	|	|	2.15
22.250	0.00	0.43	0.989	o	|	|	|	|	2.14
22.333	0.00	0.43	0.986	o	|	|	|	|	2.13
22.417	0.00	0.43	0.983	o	|	|	|	|	2.13
22.500	0.00	0.42	0.981	o	|	|	|	|	2.12
22.583	0.00	0.42	0.978	o	|	|	|	|	2.12
22.667	0.00	0.42	0.975	o	|	|	|	|	2.11
22.750	0.00	0.41	0.972	o	|	|	|	|	2.11
22.833	0.00	0.41	0.969	o	|	|	|	|	2.10
22.917	0.00	0.41	0.966	o	|	|	|	|	2.10
23.000	0.00	0.40	0.963	o	|	|	|	|	2.09

23.083	0.00	0.40	0.961	o	|	|	|	|	2.09
23.167	0.00	0.40	0.958	o	|	|	|	|	2.08
23.250	0.00	0.39	0.955	o	|	|	|	|	2.08
23.333	0.00	0.39	0.953	o	|	|	|	|	2.07
23.417	0.00	0.39	0.950	o	|	|	|	|	2.07
23.500	0.00	0.38	0.947	o	|	|	|	|	2.06
23.583	0.00	0.38	0.945	o	|	|	|	|	2.06
23.667	0.00	0.38	0.942	o	|	|	|	|	2.05
23.750	0.00	0.37	0.939	o	|	|	|	|	2.05
23.833	0.00	0.37	0.937	o	|	|	|	|	2.04
23.917	0.00	0.37	0.934	o	|	|	|	|	2.04
24.000	0.00	0.37	0.932	o	|	|	|	|	2.03
24.083	0.00	0.36	0.929	o	|	|	|	|	2.03
24.167	0.00	0.36	0.927	o	|	|	|	|	2.02
24.250	0.00	0.36	0.924	o	|	|	|	|	2.02
24.333	0.00	0.35	0.922	o	|	|	|	|	2.01
24.417	0.00	0.35	0.919	o	|	|	|	|	2.01
24.500	0.00	0.35	0.917	o	|	|	|	|	2.01
24.583	0.00	0.34	0.915	o	|	|	|	|	2.00
24.667	0.00	0.34	0.912	o	|	|	|	|	2.00
24.750	0.00	0.34	0.910	o	|	|	|	|	1.99
24.833	0.00	0.34	0.907	o	|	|	|	|	1.99
24.917	0.00	0.34	0.905	o	|	|	|	|	1.98
25.000	0.00	0.34	0.903	o	|	|	|	|	1.98
25.083	0.00	0.34	0.900	o	|	|	|	|	1.97
25.167	0.00	0.34	0.898	o	|	|	|	|	1.97
25.250	0.00	0.34	0.896	o	|	|	|	|	1.96
25.333	0.00	0.34	0.893	o	|	|	|	|	1.96
25.417	0.00	0.34	0.891	o	|	|	|	|	1.95
25.500	0.00	0.34	0.889	o	|	|	|	|	1.95
25.583	0.00	0.34	0.886	o	|	|	|	|	1.94
25.667	0.00	0.34	0.884	o	|	|	|	|	1.94
25.750	0.00	0.34	0.882	o	|	|	|	|	1.93
25.833	0.00	0.34	0.879	o	|	|	|	|	1.93
25.917	0.00	0.33	0.877	o	|	|	|	|	1.92
26.000	0.00	0.33	0.875	o	|	|	|	|	1.92
26.083	0.00	0.33	0.873	o	|	|	|	|	1.91
26.167	0.00	0.33	0.870	o	|	|	|	|	1.91
26.250	0.00	0.33	0.868	o	|	|	|	|	1.90
26.333	0.00	0.33	0.866	o	|	|	|	|	1.90
26.417	0.00	0.33	0.863	o	|	|	|	|	1.90
26.500	0.00	0.33	0.861	o	|	|	|	|	1.89
26.583	0.00	0.33	0.859	o	|	|	|	|	1.89
26.667	0.00	0.33	0.857	o	|	|	|	|	1.88
26.750	0.00	0.33	0.854	o	|	|	|	|	1.88
26.833	0.00	0.33	0.852	o	|	|	|	|	1.87
26.917	0.00	0.33	0.850	o	|	|	|	|	1.87
27.000	0.00	0.33	0.848	o	|	|	|	|	1.86
27.083	0.00	0.33	0.845	o	|	|	|	|	1.86
27.167	0.00	0.33	0.843	o	|	|	|	|	1.85
27.250	0.00	0.33	0.841	o	|	|	|	|	1.85
27.333	0.00	0.33	0.839	o	|	|	|	|	1.84
27.417	0.00	0.32	0.836	o	|	|	|	|	1.84
27.500	0.00	0.32	0.834	o	|	|	|	|	1.83
27.583	0.00	0.32	0.832	o	|	|	|	|	1.83
27.667	0.00	0.32	0.830	o	|	|	|	|	1.83
27.750	0.00	0.32	0.827	o	|	|	|	|	1.82
27.833	0.00	0.32	0.825	o	|	|	|	|	1.82
27.917	0.00	0.32	0.823	o	|	|	|	|	1.81
28.000	0.00	0.32	0.821	o	|	|	|	|	1.81
28.083	0.00	0.32	0.818	o	|	|	|	|	1.80
28.167	0.00	0.32	0.816	o	|	|	|	|	1.80
28.250	0.00	0.32	0.814	o	|	|	|	|	1.79
28.333	0.00	0.32	0.812	o	|	|	|	|	1.79
28.417	0.00	0.32	0.810	o	|	|	|	|	1.78
28.500	0.00	0.32	0.808	o	|	|	|	|	1.78
28.583	0.00	0.32	0.805	o	|	|	|	|	1.77
28.667	0.00	0.32	0.803	o	|	|	|	|	1.77
28.750	0.00	0.32	0.801	o	|	|	|	|	1.77
28.833	0.00	0.32	0.799	o	|	|	|	|	1.76
28.917	0.00	0.32	0.797	o	|	|	|	|	1.76
29.000	0.00	0.31	0.794	o	|	|	|	|	1.75
29.083	0.00	0.31	0.792	o	|	|	|	|	1.75
29.167	0.00	0.31	0.790	o	|	|	|	|	1.74
29.250	0.00	0.31	0.788	o	|	|	|	|	1.74
29.333	0.00	0.31	0.786	o	|	|	|	|	1.73
29.417	0.00	0.31	0.784	o	|	|	|	|	1.73
29.500	0.00	0.31	0.782	o	|	|	|	|	1.73
29.583	0.00	0.31	0.779	o	|	|	|	|	1.72
29.667	0.00	0.31	0.777	o	|	|	|	|	1.72
29.750	0.00	0.31	0.775	o	|	|	|	|	1.71
29.833	0.00	0.31	0.773	o	|	|	|	|	1.71
29.917	0.00	0.31	0.771	o	|	|	|	|	1.70
30.000	0.00	0.31	0.769	o	|	|	|	|	1.70
30.083	0.00	0.31	0.767	o	|	|	|	|	1.69
30.167	0.00	0.31	0.764	o	|	|	|	|	1.69

30.250	0.00	0.31	0.762	o	|	|	|	|	1.69
30.333	0.00	0.31	0.760	o	|	|	|	|	1.68
30.417	0.00	0.31	0.758	o	|	|	|	|	1.68
30.500	0.00	0.31	0.756	o	|	|	|	|	1.67
30.583	0.00	0.30	0.754	o	|	|	|	|	1.67
30.667	0.00	0.30	0.752	o	|	|	|	|	1.66
30.750	0.00	0.30	0.750	o	|	|	|	|	1.66
30.833	0.00	0.30	0.748	o	|	|	|	|	1.66
30.917	0.00	0.30	0.746	o	|	|	|	|	1.65
31.000	0.00	0.30	0.743	o	|	|	|	|	1.65
31.083	0.00	0.30	0.741	o	|	|	|	|	1.64
31.167	0.00	0.30	0.739	o	|	|	|	|	1.64
31.250	0.00	0.30	0.737	o	|	|	|	|	1.63
31.333	0.00	0.30	0.735	o	|	|	|	|	1.63
31.417	0.00	0.30	0.733	o	|	|	|	|	1.63
31.500	0.00	0.30	0.731	o	|	|	|	|	1.62
31.583	0.00	0.30	0.729	o	|	|	|	|	1.62
31.667	0.00	0.30	0.727	o	|	|	|	|	1.61
31.750	0.00	0.30	0.725	o	|	|	|	|	1.61
31.833	0.00	0.30	0.723	o	|	|	|	|	1.60
31.917	0.00	0.30	0.721	o	|	|	|	|	1.60
32.000	0.00	0.30	0.719	o	|	|	|	|	1.60
32.083	0.00	0.30	0.717	o	|	|	|	|	1.59
32.167	0.00	0.29	0.715	o	|	|	|	|	1.59
32.250	0.00	0.29	0.713	o	|	|	|	|	1.58
32.333	0.00	0.29	0.711	o	|	|	|	|	1.58
32.417	0.00	0.29	0.709	o	|	|	|	|	1.57
32.500	0.00	0.29	0.707	o	|	|	|	|	1.57
32.583	0.00	0.29	0.705	o	|	|	|	|	1.57
32.667	0.00	0.29	0.703	o	|	|	|	|	1.56
32.750	0.00	0.29	0.701	o	|	|	|	|	1.56
32.833	0.00	0.29	0.699	o	|	|	|	|	1.55
32.917	0.00	0.29	0.697	o	|	|	|	|	1.55
33.000	0.00	0.29	0.695	o	|	|	|	|	1.55
33.083	0.00	0.29	0.693	o	|	|	|	|	1.54
33.167	0.00	0.29	0.691	o	|	|	|	|	1.54
33.250	0.00	0.29	0.689	o	|	|	|	|	1.53
33.333	0.00	0.29	0.687	o	|	|	|	|	1.53
33.417	0.00	0.29	0.685	o	|	|	|	|	1.53
33.500	0.00	0.29	0.683	o	|	|	|	|	1.52
33.583	0.00	0.29	0.681	o	|	|	|	|	1.52
33.667	0.00	0.29	0.679	o	|	|	|	|	1.51
33.750	0.00	0.29	0.677	o	|	|	|	|	1.51
33.833	0.00	0.29	0.675	o	|	|	|	|	1.50
33.917	0.00	0.28	0.673	o	|	|	|	|	1.50
34.000	0.00	0.28	0.671	o	|	|	|	|	1.50
34.083	0.00	0.28	0.669	o	|	|	|	|	1.49
34.167	0.00	0.28	0.667	o	|	|	|	|	1.49
34.250	0.00	0.28	0.665	o	|	|	|	|	1.48
34.333	0.00	0.28	0.663	o	|	|	|	|	1.48
34.417	0.00	0.28	0.661	o	|	|	|	|	1.48
34.500	0.00	0.28	0.659	o	|	|	|	|	1.47
34.583	0.00	0.28	0.657	o	|	|	|	|	1.47
34.667	0.00	0.28	0.655	o	|	|	|	|	1.46
34.750	0.00	0.28	0.653	o	|	|	|	|	1.46
34.833	0.00	0.28	0.651	o	|	|	|	|	1.46
34.917	0.00	0.28	0.650	o	|	|	|	|	1.45
35.000	0.00	0.28	0.648	o	|	|	|	|	1.45
35.083	0.00	0.28	0.646	o	|	|	|	|	1.44
35.167	0.00	0.28	0.644	o	|	|	|	|	1.44
35.250	0.00	0.28	0.642	o	|	|	|	|	1.44
35.333	0.00	0.28	0.640	o	|	|	|	|	1.43
35.417	0.00	0.28	0.638	o	|	|	|	|	1.43
35.500	0.00	0.28	0.636	o	|	|	|	|	1.42
35.583	0.00	0.28	0.634	o	|	|	|	|	1.42
35.667	0.00	0.27	0.632	o	|	|	|	|	1.42
35.750	0.00	0.27	0.630	o	|	|	|	|	1.41
35.833	0.00	0.27	0.629	o	|	|	|	|	1.41
35.917	0.00	0.27	0.627	o	|	|	|	|	1.41
36.000	0.00	0.27	0.625	o	|	|	|	|	1.40
36.083	0.00	0.27	0.623	o	|	|	|	|	1.40
36.167	0.00	0.27	0.621	o	|	|	|	|	1.39
36.250	0.00	0.27	0.619	o	|	|	|	|	1.39
36.333	0.00	0.27	0.617	o	|	|	|	|	1.39
36.417	0.00	0.27	0.615	o	|	|	|	|	1.38
36.500	0.00	0.27	0.614	o	|	|	|	|	1.38
36.583	0.00	0.27	0.612	o	|	|	|	|	1.37
36.667	0.00	0.27	0.610	o	|	|	|	|	1.37
36.750	0.00	0.27	0.608	o	|	|	|	|	1.37
36.833	0.00	0.27	0.606	o	|	|	|	|	1.36
36.917	0.00	0.27	0.604	o	|	|	|	|	1.36
37.000	0.00	0.27	0.603	o	|	|	|	|	1.36
37.083	0.00	0.27	0.601	o	|	|	|	|	1.35
37.167	0.00	0.27	0.599	o	|	|	|	|	1.35
37.250	0.00	0.27	0.597	o	|	|	|	|	1.34
37.333	0.00	0.27	0.595	o	|	|	|	|	1.34

37.417	0.00	0.27	0.593	o	|	|	|	|	1.34
37.500	0.00	0.26	0.592	o	|	|	|	|	1.33
37.583	0.00	0.26	0.590	o	|	|	|	|	1.33
37.667	0.00	0.26	0.588	o	|	|	|	|	1.32
37.750	0.00	0.26	0.586	o	|	|	|	|	1.32
37.833	0.00	0.26	0.584	o	|	|	|	|	1.32
37.917	0.00	0.26	0.582	o	|	|	|	|	1.31
38.000	0.00	0.26	0.581	o	|	|	|	|	1.31
38.083	0.00	0.26	0.579	o	|	|	|	|	1.31
38.167	0.00	0.26	0.577	o	|	|	|	|	1.30
38.250	0.00	0.26	0.575	o	|	|	|	|	1.30
38.333	0.00	0.26	0.573	o	|	|	|	|	1.29
38.417	0.00	0.26	0.572	o	|	|	|	|	1.29
38.500	0.00	0.26	0.570	o	|	|	|	|	1.29
38.583	0.00	0.26	0.568	o	|	|	|	|	1.28
38.667	0.00	0.26	0.566	o	|	|	|	|	1.28
38.750	0.00	0.26	0.565	o	|	|	|	|	1.28
38.833	0.00	0.26	0.563	o	|	|	|	|	1.27
38.917	0.00	0.26	0.561	o	|	|	|	|	1.27
39.000	0.00	0.26	0.559	o	|	|	|	|	1.27
39.083	0.00	0.26	0.557	o	|	|	|	|	1.26
39.167	0.00	0.26	0.556	o	|	|	|	|	1.26
39.250	0.00	0.26	0.554	o	|	|	|	|	1.25
39.333	0.00	0.25	0.552	o	|	|	|	|	1.25
39.417	0.00	0.25	0.550	o	|	|	|	|	1.25
39.500	0.00	0.25	0.549	o	|	|	|	|	1.24
39.583	0.00	0.25	0.547	o	|	|	|	|	1.24
39.667	0.00	0.25	0.545	o	|	|	|	|	1.24
39.750	0.00	0.25	0.543	o	|	|	|	|	1.23
39.833	0.00	0.25	0.542	o	|	|	|	|	1.23
39.917	0.00	0.25	0.540	o	|	|	|	|	1.23
40.000	0.00	0.25	0.538	o	|	|	|	|	1.22
40.083	0.00	0.25	0.537	o	|	|	|	|	1.22
40.167	0.00	0.25	0.535	o	|	|	|	|	1.21
40.250	0.00	0.25	0.533	o	|	|	|	|	1.21
40.333	0.00	0.25	0.531	o	|	|	|	|	1.21
40.417	0.00	0.25	0.530	o	|	|	|	|	1.20
40.500	0.00	0.25	0.528	o	|	|	|	|	1.20
40.583	0.00	0.25	0.526	o	|	|	|	|	1.20
40.667	0.00	0.25	0.524	o	|	|	|	|	1.19
40.750	0.00	0.25	0.523	o	|	|	|	|	1.19
40.833	0.00	0.25	0.521	o	|	|	|	|	1.19
40.917	0.00	0.25	0.519	o	|	|	|	|	1.18
41.000	0.00	0.25	0.518	o	|	|	|	|	1.18
41.083	0.00	0.25	0.516	o	|	|	|	|	1.18
41.167	0.00	0.25	0.514	o	|	|	|	|	1.17
41.250	0.00	0.25	0.513	o	|	|	|	|	1.17
41.333	0.00	0.24	0.511	o	|	|	|	|	1.17
41.417	0.00	0.24	0.509	o	|	|	|	|	1.16
41.500	0.00	0.24	0.508	o	|	|	|	|	1.16
41.583	0.00	0.24	0.506	o	|	|	|	|	1.16
41.667	0.00	0.24	0.504	o	|	|	|	|	1.15
41.750	0.00	0.24	0.503	o	|	|	|	|	1.15
41.833	0.00	0.24	0.501	o	|	|	|	|	1.14
41.917	0.00	0.24	0.499	o	|	|	|	|	1.14
42.000	0.00	0.24	0.498	o	|	|	|	|	1.14
42.083	0.00	0.24	0.496	o	|	|	|	|	1.13
42.167	0.00	0.24	0.494	o	|	|	|	|	1.13
42.250	0.00	0.24	0.493	o	|	|	|	|	1.13
42.333	0.00	0.24	0.491	o	|	|	|	|	1.12
42.417	0.00	0.24	0.489	o	|	|	|	|	1.12
42.500	0.00	0.24	0.488	o	|	|	|	|	1.12
42.583	0.00	0.24	0.486	o	|	|	|	|	1.11
42.667	0.00	0.24	0.484	o	|	|	|	|	1.11
42.750	0.00	0.24	0.483	o	|	|	|	|	1.11
42.833	0.00	0.24	0.481	o	|	|	|	|	1.10
42.917	0.00	0.24	0.479	o	|	|	|	|	1.10
43.000	0.00	0.24	0.478	o	|	|	|	|	1.10
43.083	0.00	0.24	0.476	o	|	|	|	|	1.09
43.167	0.00	0.24	0.475	o	|	|	|	|	1.09
43.250	0.00	0.24	0.473	o	|	|	|	|	1.09
43.333	0.00	0.23	0.471	o	|	|	|	|	1.08
43.417	0.00	0.23	0.470	o	|	|	|	|	1.08
43.500	0.00	0.23	0.468	o	|	|	|	|	1.08
43.583	0.00	0.23	0.466	o	|	|	|	|	1.07
43.667	0.00	0.23	0.465	o	|	|	|	|	1.07
43.750	0.00	0.23	0.463	o	|	|	|	|	1.07
43.833	0.00	0.23	0.462	o	|	|	|	|	1.06
43.917	0.00	0.23	0.460	o	|	|	|	|	1.06
44.000	0.00	0.23	0.458	o	|	|	|	|	1.06
44.083	0.00	0.23	0.457	o	|	|	|	|	1.05
44.167	0.00	0.23	0.455	o	|	|	|	|	1.05
44.250	0.00	0.23	0.454	o	|	|	|	|	1.05
44.333	0.00	0.23	0.452	o	|	|	|	|	1.04
44.417	0.00	0.23	0.450	o	|	|	|	|	1.04
44.500	0.00	0.23	0.449	o	|	|	|	|	1.04

44.583	0.00	0.23	0.447	o	|	|	|	1.03
44.667	0.00	0.23	0.446	o	|	|	|	1.03
44.750	0.00	0.23	0.444	o	|	|	|	1.03
44.833	0.00	0.23	0.443	o	|	|	|	1.02
44.917	0.00	0.23	0.441	o	|	|	|	1.02
45.000	0.00	0.23	0.439	o	|	|	|	1.02
45.083	0.00	0.23	0.438	o	|	|	|	1.01
45.167	0.00	0.23	0.436	o	|	|	|	1.01
45.250	0.00	0.23	0.435	o	|	|	|	1.01
45.333	0.00	0.23	0.433	o	|	|	|	1.00
45.417	0.00	0.23	0.432	o	|	|	|	1.00
45.500	0.00	0.22	0.430	o	|	|	|	1.00
45.583	0.00	0.22	0.429	o	|	|	|	0.99
45.667	0.00	0.22	0.427	o	|	|	|	0.99
45.750	0.00	0.22	0.426	o	|	|	|	0.99
45.833	0.00	0.22	0.424	o	|	|	|	0.98
45.917	0.00	0.22	0.422	o	|	|	|	0.98
46.000	0.00	0.22	0.421	o	|	|	|	0.98
46.083	0.00	0.22	0.419	o	|	|	|	0.97
46.167	0.00	0.22	0.418	o	|	|	|	0.97
46.250	0.00	0.22	0.416	o	|	|	|	0.97
46.333	0.00	0.22	0.415	o	|	|	|	0.96
46.417	0.00	0.22	0.413	o	|	|	|	0.96
46.500	0.00	0.22	0.412	o	|	|	|	0.96
46.583	0.00	0.21	0.410	o	|	|	|	0.95
46.667	0.00	0.21	0.409	o	|	|	|	0.95
46.750	0.00	0.21	0.408	o	|	|	|	0.95
46.833	0.00	0.21	0.406	o	|	|	|	0.94
46.917	0.00	0.21	0.405	o	|	|	|	0.94
47.000	0.00	0.21	0.403	o	|	|	|	0.94
47.083	0.00	0.21	0.402	o	|	|	|	0.93
47.167	0.00	0.21	0.400	o	|	|	|	0.93
47.250	0.00	0.21	0.399	o	|	|	|	0.93
47.333	0.00	0.21	0.397	o	|	|	|	0.92
47.417	0.00	0.21	0.396	o	|	|	|	0.92
47.500	0.00	0.21	0.395	o	|	|	|	0.92
47.583	0.00	0.21	0.393	o	|	|	|	0.91
47.667	0.00	0.20	0.392	o	|	|	|	0.91
47.750	0.00	0.20	0.390	o	|	|	|	0.91
47.833	0.00	0.20	0.389	o	|	|	|	0.90
47.917	0.00	0.20	0.388	o	|	|	|	0.90
48.000	0.00	0.20	0.386	o	|	|	|	0.90
48.083	0.00	0.20	0.385	o	|	|	|	0.89
48.167	0.00	0.20	0.383	o	|	|	|	0.89
48.250	0.00	0.20	0.382	o	|	|	|	0.89
48.333	0.00	0.20	0.381	o	|	|	|	0.88
48.417	0.00	0.20	0.379	o	|	|	|	0.88
48.500	0.00	0.20	0.378	o	|	|	|	0.88
48.583	0.00	0.20	0.377	o	|	|	|	0.87
48.667	0.00	0.20	0.375	o	|	|	|	0.87
48.750	0.00	0.20	0.374	o	|	|	|	0.87
48.833	0.00	0.19	0.373	o	|	|	|	0.86
48.917	0.00	0.19	0.371	o	|	|	|	0.86
49.000	0.00	0.19	0.370	o	|	|	|	0.86
49.083	0.00	0.19	0.369	o	|	|	|	0.86
49.167	0.00	0.19	0.367	o	|	|	|	0.85
49.250	0.00	0.19	0.366	o	|	|	|	0.85
49.333	0.00	0.19	0.365	o	|	|	|	0.85
49.417	0.00	0.19	0.363	o	|	|	|	0.84
49.500	0.00	0.19	0.362	o	|	|	|	0.84
49.583	0.00	0.19	0.361	o	|	|	|	0.84
49.667	0.00	0.19	0.359	o	|	|	|	0.83
49.750	0.00	0.19	0.358	o	|	|	|	0.83
49.833	0.00	0.19	0.357	o	|	|	|	0.83
49.917	0.00	0.19	0.356	o	|	|	|	0.82
50.000	0.00	0.18	0.354	o	|	|	|	0.82
50.083	0.00	0.18	0.353	o	|	|	|	0.82
50.167	0.00	0.18	0.352	o	|	|	|	0.82
50.250	0.00	0.18	0.350	o	|	|	|	0.81
50.333	0.00	0.18	0.349	o	|	|	|	0.81
50.417	0.00	0.18	0.348	o	|	|	|	0.81
50.500	0.00	0.18	0.347	o	|	|	|	0.80
50.583	0.00	0.18	0.345	o	|	|	|	0.80
50.667	0.00	0.18	0.344	o	|	|	|	0.80
50.750	0.00	0.18	0.343	o	|	|	|	0.80
50.833	0.00	0.18	0.342	o	|	|	|	0.79
50.917	0.00	0.18	0.340	o	|	|	|	0.79
51.000	0.00	0.18	0.339	o	|	|	|	0.79
51.083	0.00	0.18	0.338	o	|	|	|	0.78
51.167	0.00	0.18	0.337	o	|	|	|	0.78
51.250	0.00	0.18	0.336	o	|	|	|	0.78
51.333	0.00	0.17	0.334	o	|	|	|	0.78
51.417	0.00	0.17	0.333	o	|	|	|	0.77
51.500	0.00	0.17	0.332	o	|	|	|	0.77
51.583	0.00	0.17	0.331	o	|	|	|	0.77
51.667	0.00	0.17	0.330	o	|	|	|	0.76

51.750	0.00	0.17	0.328	o	|	|	|	|	0.76
51.833	0.00	0.17	0.327	o	|	|	|	|	0.76
51.917	0.00	0.17	0.326	o	|	|	|	|	0.76
52.000	0.00	0.17	0.325	o	|	|	|	|	0.75
52.083	0.00	0.17	0.324	o	|	|	|	|	0.75
52.167	0.00	0.17	0.323	o	|	|	|	|	0.75
52.250	0.00	0.17	0.321	o	|	|	|	|	0.75
52.333	0.00	0.17	0.320	o	|	|	|	|	0.74
52.417	0.00	0.17	0.319	o	|	|	|	|	0.74
52.500	0.00	0.17	0.318	o	|	|	|	|	0.74
52.583	0.00	0.17	0.317	o	|	|	|	|	0.74
52.667	0.00	0.16	0.316	o	|	|	|	|	0.73
52.750	0.00	0.16	0.315	o	|	|	|	|	0.73
52.833	0.00	0.16	0.313	o	|	|	|	|	0.73
52.917	0.00	0.16	0.312	o	|	|	|	|	0.72
53.000	0.00	0.16	0.311	o	|	|	|	|	0.72
53.083	0.00	0.16	0.310	o	|	|	|	|	0.72
53.167	0.00	0.16	0.309	o	|	|	|	|	0.72
53.250	0.00	0.16	0.308	o	|	|	|	|	0.71
53.333	0.00	0.16	0.307	o	|	|	|	|	0.71
53.417	0.00	0.16	0.306	o	|	|	|	|	0.71
53.500	0.00	0.16	0.305	o	|	|	|	|	0.71
53.583	0.00	0.16	0.303	o	|	|	|	|	0.70
53.667	0.00	0.16	0.302	o	|	|	|	|	0.70
53.750	0.00	0.16	0.301	o	|	|	|	|	0.70
53.833	0.00	0.16	0.300	o	|	|	|	|	0.70
53.917	0.00	0.16	0.299	o	|	|	|	|	0.69
54.000	0.00	0.16	0.298	o	|	|	|	|	0.69
54.083	0.00	0.16	0.297	o	|	|	|	|	0.69
54.167	0.00	0.15	0.296	o	|	|	|	|	0.69
54.250	0.00	0.15	0.295	o	|	|	|	|	0.68
54.333	0.00	0.15	0.294	o	|	|	|	|	0.68
54.417	0.00	0.15	0.293	o	|	|	|	|	0.68
54.500	0.00	0.15	0.292	o	|	|	|	|	0.68
54.583	0.00	0.15	0.291	o	|	|	|	|	0.67
54.667	0.00	0.15	0.290	o	|	|	|	|	0.67
54.750	0.00	0.15	0.289	o	|	|	|	|	0.67
54.833	0.00	0.15	0.288	o	|	|	|	|	0.67
54.917	0.00	0.15	0.287	o	|	|	|	|	0.66
55.000	0.00	0.15	0.285	o	|	|	|	|	0.66
55.083	0.00	0.15	0.284	o	|	|	|	|	0.66
55.167	0.00	0.15	0.283	o	|	|	|	|	0.66
55.250	0.00	0.15	0.282	o	|	|	|	|	0.66
55.333	0.00	0.15	0.281	o	|	|	|	|	0.65
55.417	0.00	0.15	0.280	o	|	|	|	|	0.65
55.500	0.00	0.15	0.279	o	|	|	|	|	0.65
55.583	0.00	0.15	0.278	o	|	|	|	|	0.65
55.667	0.00	0.14	0.277	o	|	|	|	|	0.64
55.750	0.00	0.14	0.276	o	|	|	|	|	0.64
55.833	0.00	0.14	0.275	o	|	|	|	|	0.64
55.917	0.00	0.14	0.274	o	|	|	|	|	0.64
56.000	0.00	0.14	0.273	o	|	|	|	|	0.63
56.083	0.00	0.14	0.272	o	|	|	|	|	0.63
56.167	0.00	0.14	0.271	o	|	|	|	|	0.63
56.250	0.00	0.14	0.271	o	|	|	|	|	0.63
56.333	0.00	0.14	0.270	o	|	|	|	|	0.63
56.417	0.00	0.14	0.269	o	|	|	|	|	0.62
56.500	0.00	0.14	0.268	o	|	|	|	|	0.62
56.583	0.00	0.14	0.267	o	|	|	|	|	0.62
56.667	0.00	0.14	0.266	o	|	|	|	|	0.62
56.750	0.00	0.14	0.265	o	|	|	|	|	0.61
56.833	0.00	0.14	0.264	o	|	|	|	|	0.61
56.917	0.00	0.14	0.263	o	|	|	|	|	0.61
57.000	0.00	0.14	0.262	o	|	|	|	|	0.61
57.083	0.00	0.14	0.261	o	|	|	|	|	0.61
57.167	0.00	0.14	0.260	o	|	|	|	|	0.60
57.250	0.00	0.14	0.259	o	|	|	|	|	0.60
57.333	0.00	0.13	0.258	o	|	|	|	|	0.60
57.417	0.00	0.13	0.257	o	|	|	|	|	0.60
57.500	0.00	0.13	0.256	o	|	|	|	|	0.59
57.583	0.00	0.13	0.255	o	|	|	|	|	0.59
57.667	0.00	0.13	0.254	o	|	|	|	|	0.59
57.750	0.00	0.13	0.254	o	|	|	|	|	0.59
57.833	0.00	0.13	0.253	o	|	|	|	|	0.59
57.917	0.00	0.13	0.252	o	|	|	|	|	0.58
58.000	0.00	0.13	0.251	o	|	|	|	|	0.58
58.083	0.00	0.13	0.250	o	|	|	|	|	0.58
58.167	0.00	0.13	0.249	o	|	|	|	|	0.58
58.250	0.00	0.13	0.248	o	|	|	|	|	0.58
58.333	0.00	0.13	0.247	o	|	|	|	|	0.57
58.417	0.00	0.13	0.246	o	|	|	|	|	0.57
58.500	0.00	0.13	0.245	o	|	|	|	|	0.57
58.583	0.00	0.13	0.245	o	|	|	|	|	0.57
58.667	0.00	0.13	0.244	o	|	|	|	|	0.57
58.750	0.00	0.13	0.243	o	|	|	|	|	0.56
58.833	0.00	0.13	0.242	o	|	|	|	|	0.56

58.917	0.00	0.13	0.241	o	|	|	|	|	0.56
59.000	0.00	0.13	0.240	o	|	|	|	|	0.56
59.083	0.00	0.12	0.239	o	|	|	|	|	0.56
59.167	0.00	0.12	0.239	o	|	|	|	|	0.55
59.250	0.00	0.12	0.238	o	|	|	|	|	0.55
59.333	0.00	0.12	0.237	o	|	|	|	|	0.55
59.417	0.00	0.12	0.236	o	|	|	|	|	0.55
59.500	0.00	0.12	0.235	o	|	|	|	|	0.55
59.583	0.00	0.12	0.234	o	|	|	|	|	0.54
59.667	0.00	0.12	0.233	o	|	|	|	|	0.54
59.750	0.00	0.12	0.233	o	|	|	|	|	0.54
59.833	0.00	0.12	0.232	o	|	|	|	|	0.54
59.917	0.00	0.12	0.231	o	|	|	|	|	0.54
60.000	0.00	0.12	0.230	o	|	|	|	|	0.53
60.083	0.00	0.12	0.229	o	|	|	|	|	0.53
60.167	0.00	0.12	0.228	o	|	|	|	|	0.53
60.250	0.00	0.12	0.228	o	|	|	|	|	0.53
60.333	0.00	0.12	0.227	o	|	|	|	|	0.53
60.417	0.00	0.12	0.226	o	|	|	|	|	0.52
60.500	0.00	0.12	0.225	o	|	|	|	|	0.52
60.583	0.00	0.12	0.224	o	|	|	|	|	0.52
60.667	0.00	0.12	0.224	o	|	|	|	|	0.52
60.750	0.00	0.12	0.223	o	|	|	|	|	0.52
60.833	0.00	0.12	0.222	o	|	|	|	|	0.52
60.917	0.00	0.12	0.221	o	|	|	|	|	0.51
61.000	0.00	0.12	0.220	o	|	|	|	|	0.51
61.083	0.00	0.11	0.220	o	|	|	|	|	0.51
61.167	0.00	0.11	0.219	o	|	|	|	|	0.51
61.250	0.00	0.11	0.218	o	|	|	|	|	0.51
61.333	0.00	0.11	0.217	o	|	|	|	|	0.50
61.417	0.00	0.11	0.216	o	|	|	|	|	0.50
61.500	0.00	0.11	0.216	o	|	|	|	|	0.50
61.583	0.00	0.11	0.215	o	|	|	|	|	0.50
61.667	0.00	0.11	0.214	o	|	|	|	|	0.50
61.750	0.00	0.11	0.213	o	|	|	|	|	0.50
61.833	0.00	0.11	0.213	o	|	|	|	|	0.49
61.917	0.00	0.11	0.212	o	|	|	|	|	0.49
62.000	0.00	0.11	0.211	o	|	|	|	|	0.49
62.083	0.00	0.11	0.210	o	|	|	|	|	0.49
62.167	0.00	0.11	0.210	o	|	|	|	|	0.49
62.250	0.00	0.11	0.209	o	|	|	|	|	0.48
62.333	0.00	0.11	0.208	o	|	|	|	|	0.48
62.417	0.00	0.11	0.207	o	|	|	|	|	0.48
62.500	0.00	0.11	0.207	o	|	|	|	|	0.48
62.583	0.00	0.11	0.206	o	|	|	|	|	0.48
62.667	0.00	0.11	0.205	o	|	|	|	|	0.48
62.750	0.00	0.11	0.204	o	|	|	|	|	0.47
62.833	0.00	0.11	0.204	o	|	|	|	|	0.47
62.917	0.00	0.11	0.203	o	|	|	|	|	0.47
63.000	0.00	0.11	0.202	o	|	|	|	|	0.47
63.083	0.00	0.11	0.201	o	|	|	|	|	0.47
63.167	0.00	0.10	0.201	o	|	|	|	|	0.47
63.250	0.00	0.10	0.200	o	|	|	|	|	0.46
63.333	0.00	0.10	0.199	o	|	|	|	|	0.46
63.417	0.00	0.10	0.199	o	|	|	|	|	0.46
63.500	0.00	0.10	0.198	o	|	|	|	|	0.46
63.583	0.00	0.10	0.197	o	|	|	|	|	0.46
63.667	0.00	0.10	0.196	o	|	|	|	|	0.46
63.750	0.00	0.10	0.196	o	|	|	|	|	0.45
63.833	0.00	0.10	0.195	o	|	|	|	|	0.45
63.917	0.00	0.10	0.194	o	|	|	|	|	0.45
64.000	0.00	0.10	0.194	o	|	|	|	|	0.45
64.083	0.00	0.10	0.193	o	|	|	|	|	0.45
64.167	0.00	0.10	0.192	o	|	|	|	|	0.45
64.250	0.00	0.10	0.192	o	|	|	|	|	0.44

Remaining water in basin = 0.19 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 771
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 125.746 (CFS)
Total volume = 4.533 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 06/03/24

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: pro21003100.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    41
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       79.045 (CFS)
               Total volume =       6.126 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
*************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
____________________________________________________________________________

User entry of depth-outflow-storage data
---------------------------------------------------------------------
Total number of inflow hydrograph intervals = 41
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
---------------------------------------------------------------------
---------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
---------------------------------------------------------------------
---------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
---------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.431      0.225      0.430        0.432
   2.000      0.914      0.344      0.913        0.915
   3.000      1.451      0.991      1.448        1.454
   4.000      2.049      1.417      2.044        2.054
   5.000      2.712      1.731      2.706        2.718
   5.250      2.888      1.801      2.882        2.894
   5.500      3.069     17.046      3.010        3.128
   6.000      3.443    225.078      2.668        4.218
---------------------------------------------------------------------
               Hydrograph Detention Basin Routing
---------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
---------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                  Depth
(Hours) (CFS)   (CFS)     (Ac.Ft) .0      19.8   39.52   59.28  79.05 (Ft.)
 0.083    2.38    0.00      0.008  O       |       |       |       |     0.02
 0.167    6.30    0.02      0.038  O I     |       |       |       |     0.09
 0.250    6.92    0.04      0.083  O I     |       |       |       |     0.19
 0.333    7.49    0.07      0.133  O  I    |       |       |       |     0.31
 0.417    8.78    0.10      0.188  O  I    |       |       |       |     0.44
 0.500    9.92    0.13      0.252  O   I   |       |       |       |     0.58
 0.583   10.48    0.17      0.321  O   I   |       |       |       |     0.74
 0.667   10.36    0.20      0.391  O   I   |       |       |       |     0.91
 0.750   11.43    0.23      0.465  O   I   |       |       |       |     1.07
 0.833   10.95    0.25      0.540  O   I   |       |       |       |     1.23
 0.917   10.07    0.27      0.611  O   I   |       |       |       |     1.37
 1.000   10.62    0.29      0.680  O   I   |       |       |       |     1.52
 1.083   12.96    0.31      0.759  O    I  |       |       |       |     1.68
 1.167   15.55    0.33      0.855  O     I |       |       |       |     1.88
 1.250   16.23    0.40      0.962  O     I |       |       |       |     2.09
 1.333   15.83    0.53      1.069  O     I |       |       |       |     2.29
 1.417   17.01    0.66      1.178  O     I |       |       |       |     2.49
 1.500   20.80    0.81      1.303  O       I       |       |       |     2.73
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1.583	21.08	0.98	1.442	O	I	|	|	|	2.98
1.667	20.86	1.08	1.579	O	I	|	|	|	3.21
1.750	24.64	1.19	1.728	O	I	|	|	|	3.46
1.833	27.98	1.31	1.900	O	I	|	|	|	3.75
1.917	27.08	1.43	2.080	O	I	|	|	|	4.05
2.000	26.37	1.51	2.254	O	I	|	|	|	4.31
2.083	27.20	1.60	2.428	O	I	|	|	|	4.57
2.167	31.94	1.69	2.620	O	I	|	|	|	4.86
2.250	41.59	1.79	2.862	O	|	I	|	|	5.21
2.333	42.63	20.44	3.075	|	O	I	|	|	5.51
2.417	47.73	52.95	3.134	|	|	I O	|	|	5.59
2.500	68.12	59.49	3.145	|	|	O I	|	|	5.60
2.583	79.05	78.01	3.179	|	|	|	|	OI	5.65
2.667	78.70	79.14	3.181	|	|	|	|	IO	5.65
2.750	53.07	61.72	3.149	|	|	I O	|	|	5.61
2.833	27.04	33.25	3.098	|	I O	|	|	|	5.54
2.917	18.80	19.68	3.074	|	O	|	|	|	5.51
3.000	12.89	16.22	3.059	|	IO	|	|	|	5.49
3.083	5.70	13.11	3.022	| I	O |	|	|	|	5.44
3.167	1.76	8.89	2.972	I	O |	|	|	|	5.37
3.250	0.81	5.47	2.932	I O	|	|	|	|	5.31
3.333	0.37	3.28	2.906	IO	|	|	|	|	5.27
3.417	0.08	1.90	2.889	O	|	|	|	|	5.25
3.500	0.00	1.80	2.877	O	|	|	|	|	5.23
3.583	0.00	1.79	2.864	O	|	|	|	|	5.22
3.667	0.00	1.79	2.852	O	|	|	|	|	5.20
3.750	0.00	1.78	2.840	O	|	|	|	|	5.18
3.833	0.00	1.78	2.828	O	|	|	|	|	5.16
3.917	0.00	1.77	2.815	O	|	|	|	|	5.15
4.000	0.00	1.77	2.803	O	|	|	|	|	5.13
4.083	0.00	1.76	2.791	O	|	|	|	|	5.11
4.167	0.00	1.76	2.779	O	|	|	|	|	5.09
4.250	0.00	1.75	2.767	O	|	|	|	|	5.08
4.333	0.00	1.75	2.755	O	|	|	|	|	5.06
4.417	0.00	1.74	2.743	O	|	|	|	|	5.04
4.500	0.00	1.74	2.731	O	|	|	|	|	5.03
4.583	0.00	1.73	2.719	O	|	|	|	|	5.01
4.667	0.00	1.73	2.707	O	|	|	|	|	4.99
4.750	0.00	1.72	2.695	O	|	|	|	|	4.97
4.833	0.00	1.72	2.683	O	|	|	|	|	4.96
4.917	0.00	1.71	2.671	O	|	|	|	|	4.94
5.000	0.00	1.71	2.660	O	|	|	|	|	4.92
5.083	0.00	1.70	2.648	O	|	|	|	|	4.90
5.167	0.00	1.70	2.636	O	|	|	|	|	4.89
5.250	0.00	1.69	2.624	O	|	|	|	|	4.87
5.333	0.00	1.68	2.613	O	|	|	|	|	4.85
5.417	0.00	1.68	2.601	O	|	|	|	|	4.83
5.500	0.00	1.67	2.590	O	|	|	|	|	4.82
5.583	0.00	1.67	2.578	O	|	|	|	|	4.80
5.667	0.00	1.66	2.567	O	|	|	|	|	4.78
5.750	0.00	1.66	2.555	O	|	|	|	|	4.76
5.833	0.00	1.65	2.544	O	|	|	|	|	4.75
5.917	0.00	1.65	2.533	O	|	|	|	|	4.73
6.000	0.00	1.64	2.521	O	|	|	|	|	4.71
6.083	0.00	1.64	2.510	O	|	|	|	|	4.70
6.167	0.00	1.63	2.499	O	|	|	|	|	4.68
6.250	0.00	1.62	2.488	O	|	|	|	|	4.66
6.333	0.00	1.62	2.476	O	|	|	|	|	4.64
6.417	0.00	1.61	2.465	O	|	|	|	|	4.63
6.500	0.00	1.61	2.454	O	|	|	|	|	4.61
6.583	0.00	1.60	2.443	O	|	|	|	|	4.59
6.667	0.00	1.60	2.432	O	|	|	|	|	4.58
6.750	0.00	1.59	2.421	O	|	|	|	|	4.56
6.833	0.00	1.59	2.410	O	|	|	|	|	4.54
6.917	0.00	1.58	2.399	O	|	|	|	|	4.53
7.000	0.00	1.58	2.388	O	|	|	|	|	4.51
7.083	0.00	1.57	2.377	O	|	|	|	|	4.50
7.167	0.00	1.57	2.367	O	|	|	|	|	4.48
7.250	0.00	1.56	2.356	O	|	|	|	|	4.46
7.333	0.00	1.56	2.345	O	|	|	|	|	4.45
7.417	0.00	1.55	2.334	O	|	|	|	|	4.43
7.500	0.00	1.55	2.324	O	|	|	|	|	4.41
7.583	0.00	1.54	2.313	O	|	|	|	|	4.40
7.667	0.00	1.54	2.302	O	|	|	|	|	4.38
7.750	0.00	1.53	2.292	O	|	|	|	|	4.37
7.833	0.00	1.53	2.281	O	|	|	|	|	4.35
7.917	0.00	1.52	2.271	O	|	|	|	|	4.33
8.000	0.00	1.52	2.260	O	|	|	|	|	4.32
8.083	0.00	1.51	2.250	O	|	|	|	|	4.30
8.167	0.00	1.51	2.240	O	|	|	|	|	4.29
8.250	0.00	1.50	2.229	O	|	|	|	|	4.27
8.333	0.00	1.50	2.219	O	|	|	|	|	4.26
8.417	0.00	1.49	2.209	O	|	|	|	|	4.24
8.500	0.00	1.49	2.198	O	|	|	|	|	4.23
8.583	0.00	1.48	2.188	O	|	|	|	|	4.21
8.667	0.00	1.48	2.178	O	|	|	|	|	4.19

8.750	0.00	1.47	2.168	o	|	|	|	|	4.18
8.833	0.00	1.47	2.158	o	|	|	|	|	4.16
8.917	0.00	1.46	2.148	o	|	|	|	|	4.15
9.000	0.00	1.46	2.137	o	|	|	|	|	4.13
9.083	0.00	1.45	2.127	o	|	|	|	|	4.12
9.167	0.00	1.45	2.117	o	|	|	|	|	4.10
9.250	0.00	1.44	2.107	o	|	|	|	|	4.09
9.333	0.00	1.44	2.098	o	|	|	|	|	4.07
9.417	0.00	1.44	2.088	o	|	|	|	|	4.06
9.500	0.00	1.43	2.078	o	|	|	|	|	4.04
9.583	0.00	1.43	2.068	o	|	|	|	|	4.03
9.667	0.00	1.42	2.058	o	|	|	|	|	4.01
9.750	0.00	1.42	2.048	o	|	|	|	|	4.00
9.833	0.00	1.41	2.039	o	|	|	|	|	3.98
9.917	0.00	1.40	2.029	o	|	|	|	|	3.97
10.000	0.00	1.40	2.019	o	|	|	|	|	3.95
10.083	0.00	1.39	2.010	o	|	|	|	|	3.93
10.167	0.00	1.38	2.000	o	|	|	|	|	3.92
10.250	0.00	1.38	1.991	o	|	|	|	|	3.90
10.333	0.00	1.37	1.981	o	|	|	|	|	3.89
10.417	0.00	1.36	1.972	o	|	|	|	|	3.87
10.500	0.00	1.36	1.962	o	|	|	|	|	3.86
10.583	0.00	1.35	1.953	o	|	|	|	|	3.84
10.667	0.00	1.34	1.944	o	|	|	|	|	3.82
10.750	0.00	1.34	1.935	o	|	|	|	|	3.81
10.833	0.00	1.33	1.925	o	|	|	|	|	3.79
10.917	0.00	1.32	1.916	o	|	|	|	|	3.78
11.000	0.00	1.32	1.907	o	|	|	|	|	3.76
11.083	0.00	1.31	1.898	o	|	|	|	|	3.75
11.167	0.00	1.30	1.889	o	|	|	|	|	3.73
11.250	0.00	1.30	1.880	o	|	|	|	|	3.72
11.333	0.00	1.29	1.871	o	|	|	|	|	3.70
11.417	0.00	1.28	1.862	o	|	|	|	|	3.69
11.500	0.00	1.28	1.854	o	|	|	|	|	3.67
11.583	0.00	1.27	1.845	o	|	|	|	|	3.66
11.667	0.00	1.27	1.836	o	|	|	|	|	3.64
11.750	0.00	1.26	1.827	o	|	|	|	|	3.63
11.833	0.00	1.25	1.819	o	|	|	|	|	3.62
11.917	0.00	1.25	1.810	o	|	|	|	|	3.60
12.000	0.00	1.24	1.802	o	|	|	|	|	3.59
12.083	0.00	1.23	1.793	o	|	|	|	|	3.57
12.167	0.00	1.23	1.785	o	|	|	|	|	3.56
12.250	0.00	1.22	1.776	o	|	|	|	|	3.54
12.333	0.00	1.22	1.768	o	|	|	|	|	3.53
12.417	0.00	1.21	1.759	o	|	|	|	|	3.52
12.500	0.00	1.20	1.751	o	|	|	|	|	3.50
12.583	0.00	1.20	1.743	o	|	|	|	|	3.49
12.667	0.00	1.19	1.735	o	|	|	|	|	3.47
12.750	0.00	1.19	1.726	o	|	|	|	|	3.46
12.833	0.00	1.18	1.718	o	|	|	|	|	3.45
12.917	0.00	1.18	1.710	o	|	|	|	|	3.43
13.000	0.00	1.17	1.702	o	|	|	|	|	3.42
13.083	0.00	1.16	1.694	o	|	|	|	|	3.41
13.167	0.00	1.16	1.686	o	|	|	|	|	3.39
13.250	0.00	1.15	1.678	o	|	|	|	|	3.38
13.333	0.00	1.15	1.670	o	|	|	|	|	3.37
13.417	0.00	1.14	1.662	o	|	|	|	|	3.35
13.500	0.00	1.14	1.654	o	|	|	|	|	3.34
13.583	0.00	1.13	1.647	o	|	|	|	|	3.33
13.667	0.00	1.12	1.639	o	|	|	|	|	3.31
13.750	0.00	1.12	1.631	o	|	|	|	|	3.30
13.833	0.00	1.11	1.623	o	|	|	|	|	3.29
13.917	0.00	1.11	1.616	o	|	|	|	|	3.28
14.000	0.00	1.10	1.608	o	|	|	|	|	3.26
14.083	0.00	1.10	1.601	o	|	|	|	|	3.25
14.167	0.00	1.09	1.593	o	|	|	|	|	3.24
14.250	0.00	1.09	1.586	o	|	|	|	|	3.22
14.333	0.00	1.08	1.578	o	|	|	|	|	3.21
14.417	0.00	1.08	1.571	o	|	|	|	|	3.20
14.500	0.00	1.07	1.563	o	|	|	|	|	3.19
14.583	0.00	1.07	1.556	o	|	|	|	|	3.18
14.667	0.00	1.06	1.549	o	|	|	|	|	3.16
14.750	0.00	1.06	1.541	o	|	|	|	|	3.15
14.833	0.00	1.05	1.534	o	|	|	|	|	3.14
14.917	0.00	1.05	1.527	o	|	|	|	|	3.13
15.000	0.00	1.04	1.520	o	|	|	|	|	3.11
15.083	0.00	1.03	1.512	o	|	|	|	|	3.10
15.167	0.00	1.03	1.505	o	|	|	|	|	3.09
15.250	0.00	1.02	1.498	o	|	|	|	|	3.08
15.333	0.00	1.02	1.491	o	|	|	|	|	3.07
15.417	0.00	1.01	1.484	o	|	|	|	|	3.06
15.500	0.00	1.01	1.477	o	|	|	|	|	3.04
15.583	0.00	1.00	1.470	o	|	|	|	|	3.03
15.667	0.00	1.00	1.463	o	|	|	|	|	3.02
15.750	0.00	0.99	1.457	o	|	|	|	|	3.01
15.833	0.00	0.99	1.450	o	|	|	|	|	3.00

15.917	0.00	0.98	1.443	o	|	|	|	|	2.99
16.000	0.00	0.97	1.436	o	|	|	|	|	2.97
16.083	0.00	0.97	1.430	o	|	|	|	|	2.96
16.167	0.00	0.96	1.423	o	|	|	|	|	2.95
16.250	0.00	0.95	1.416	o	|	|	|	|	2.94
16.333	0.00	0.94	1.410	o	|	|	|	|	2.92
16.417	0.00	0.93	1.403	o	|	|	|	|	2.91
16.500	0.00	0.93	1.397	o	|	|	|	|	2.90
16.583	0.00	0.92	1.391	o	|	|	|	|	2.89
16.667	0.00	0.91	1.384	o	|	|	|	|	2.88
16.750	0.00	0.90	1.378	o	|	|	|	|	2.86
16.833	0.00	0.90	1.372	o	|	|	|	|	2.85
16.917	0.00	0.89	1.366	o	|	|	|	|	2.84
17.000	0.00	0.88	1.360	o	|	|	|	|	2.83
17.083	0.00	0.87	1.354	o	|	|	|	|	2.82
17.167	0.00	0.87	1.348	o	|	|	|	|	2.81
17.250	0.00	0.86	1.342	o	|	|	|	|	2.80
17.333	0.00	0.85	1.336	o	|	|	|	|	2.79
17.417	0.00	0.85	1.330	o	|	|	|	|	2.77
17.500	0.00	0.84	1.324	o	|	|	|	|	2.76
17.583	0.00	0.83	1.318	o	|	|	|	|	2.75
17.667	0.00	0.82	1.313	o	|	|	|	|	2.74
17.750	0.00	0.82	1.307	o	|	|	|	|	2.73
17.833	0.00	0.81	1.301	o	|	|	|	|	2.72
17.917	0.00	0.80	1.296	o	|	|	|	|	2.71
18.000	0.00	0.80	1.290	o	|	|	|	|	2.70
18.083	0.00	0.79	1.285	o	|	|	|	|	2.69
18.167	0.00	0.78	1.279	o	|	|	|	|	2.68
18.250	0.00	0.78	1.274	o	|	|	|	|	2.67
18.333	0.00	0.77	1.269	o	|	|	|	|	2.66
18.417	0.00	0.77	1.263	o	|	|	|	|	2.65
18.500	0.00	0.76	1.258	o	|	|	|	|	2.64
18.583	0.00	0.75	1.253	o	|	|	|	|	2.63
18.667	0.00	0.75	1.248	o	|	|	|	|	2.62
18.750	0.00	0.74	1.243	o	|	|	|	|	2.61
18.833	0.00	0.73	1.238	o	|	|	|	|	2.60
18.917	0.00	0.73	1.233	o	|	|	|	|	2.59
19.000	0.00	0.72	1.228	o	|	|	|	|	2.58
19.083	0.00	0.72	1.223	o	|	|	|	|	2.57
19.167	0.00	0.71	1.218	o	|	|	|	|	2.57
19.250	0.00	0.70	1.213	o	|	|	|	|	2.56
19.333	0.00	0.70	1.208	o	|	|	|	|	2.55
19.417	0.00	0.69	1.203	o	|	|	|	|	2.54
19.500	0.00	0.69	1.199	o	|	|	|	|	2.53
19.583	0.00	0.68	1.194	o	|	|	|	|	2.52
19.667	0.00	0.68	1.189	o	|	|	|	|	2.51
19.750	0.00	0.67	1.185	o	|	|	|	|	2.50
19.833	0.00	0.66	1.180	o	|	|	|	|	2.50
19.917	0.00	0.66	1.175	o	|	|	|	|	2.49
20.000	0.00	0.65	1.171	o	|	|	|	|	2.48
20.083	0.00	0.65	1.166	o	|	|	|	|	2.47
20.167	0.00	0.64	1.162	o	|	|	|	|	2.46
20.250	0.00	0.64	1.158	o	|	|	|	|	2.45
20.333	0.00	0.63	1.153	o	|	|	|	|	2.45
20.417	0.00	0.63	1.149	o	|	|	|	|	2.44
20.500	0.00	0.62	1.145	o	|	|	|	|	2.43
20.583	0.00	0.62	1.140	o	|	|	|	|	2.42
20.667	0.00	0.61	1.136	o	|	|	|	|	2.41
20.750	0.00	0.61	1.132	o	|	|	|	|	2.41
20.833	0.00	0.60	1.128	o	|	|	|	|	2.40
20.917	0.00	0.60	1.124	o	|	|	|	|	2.39
21.000	0.00	0.59	1.119	o	|	|	|	|	2.38
21.083	0.00	0.59	1.115	o	|	|	|	|	2.38
21.167	0.00	0.58	1.111	o	|	|	|	|	2.37
21.250	0.00	0.58	1.107	o	|	|	|	|	2.36
21.333	0.00	0.57	1.103	o	|	|	|	|	2.35
21.417	0.00	0.57	1.099	o	|	|	|	|	2.35
21.500	0.00	0.56	1.096	o	|	|	|	|	2.34
21.583	0.00	0.56	1.092	o	|	|	|	|	2.33
21.667	0.00	0.55	1.088	o	|	|	|	|	2.32
21.750	0.00	0.55	1.084	o	|	|	|	|	2.32
21.833	0.00	0.54	1.080	o	|	|	|	|	2.31
21.917	0.00	0.54	1.077	o	|	|	|	|	2.30
22.000	0.00	0.54	1.073	o	|	|	|	|	2.30
22.083	0.00	0.53	1.069	o	|	|	|	|	2.29
22.167	0.00	0.53	1.066	o	|	|	|	|	2.28
22.250	0.00	0.52	1.062	o	|	|	|	|	2.28
22.333	0.00	0.52	1.058	o	|	|	|	|	2.27
22.417	0.00	0.51	1.055	o	|	|	|	|	2.26
22.500	0.00	0.51	1.051	o	|	|	|	|	2.26
22.583	0.00	0.51	1.048	o	|	|	|	|	2.25
22.667	0.00	0.50	1.044	o	|	|	|	|	2.24
22.750	0.00	0.50	1.041	o	|	|	|	|	2.24
22.833	0.00	0.49	1.038	o	|	|	|	|	2.23
22.917	0.00	0.49	1.034	o	|	|	|	|	2.22
23.000	0.00	0.48	1.031	o	|	|	|	|	2.22

23.083	0.00	0.48	1.027	o	|	|	|	|	2.21
23.167	0.00	0.48	1.024	o	|	|	|	|	2.21
23.250	0.00	0.47	1.021	o	|	|	|	|	2.20
23.333	0.00	0.47	1.018	o	|	|	|	|	2.19
23.417	0.00	0.47	1.014	o	|	|	|	|	2.19
23.500	0.00	0.46	1.011	o	|	|	|	|	2.18
23.583	0.00	0.46	1.008	o	|	|	|	|	2.18
23.667	0.00	0.45	1.005	o	|	|	|	|	2.17
23.750	0.00	0.45	1.002	o	|	|	|	|	2.16
23.833	0.00	0.45	0.999	o	|	|	|	|	2.16
23.917	0.00	0.44	0.996	o	|	|	|	|	2.15
24.000	0.00	0.44	0.993	o	|	|	|	|	2.15
24.083	0.00	0.44	0.990	o	|	|	|	|	2.14
24.167	0.00	0.43	0.987	o	|	|	|	|	2.14
24.250	0.00	0.43	0.984	o	|	|	|	|	2.13
24.333	0.00	0.42	0.981	o	|	|	|	|	2.12
24.417	0.00	0.42	0.978	o	|	|	|	|	2.12
24.500	0.00	0.42	0.975	o	|	|	|	|	2.11
24.583	0.00	0.41	0.972	o	|	|	|	|	2.11
24.667	0.00	0.41	0.969	o	|	|	|	|	2.10
24.750	0.00	0.41	0.966	o	|	|	|	|	2.10
24.833	0.00	0.40	0.964	o	|	|	|	|	2.09
24.917	0.00	0.40	0.961	o	|	|	|	|	2.09
25.000	0.00	0.40	0.958	o	|	|	|	|	2.08
25.083	0.00	0.39	0.955	o	|	|	|	|	2.08
25.167	0.00	0.39	0.953	o	|	|	|	|	2.07
25.250	0.00	0.39	0.950	o	|	|	|	|	2.07
25.333	0.00	0.38	0.947	o	|	|	|	|	2.06
25.417	0.00	0.38	0.945	o	|	|	|	|	2.06
25.500	0.00	0.38	0.942	o	|	|	|	|	2.05
25.583	0.00	0.37	0.940	o	|	|	|	|	2.05
25.667	0.00	0.37	0.937	o	|	|	|	|	2.04
25.750	0.00	0.37	0.934	o	|	|	|	|	2.04
25.833	0.00	0.37	0.932	o	|	|	|	|	2.03
25.917	0.00	0.36	0.929	o	|	|	|	|	2.03
26.000	0.00	0.36	0.927	o	|	|	|	|	2.02
26.083	0.00	0.36	0.924	o	|	|	|	|	2.02
26.167	0.00	0.35	0.922	o	|	|	|	|	2.01
26.250	0.00	0.35	0.920	o	|	|	|	|	2.01
26.333	0.00	0.35	0.917	o	|	|	|	|	2.01
26.417	0.00	0.34	0.915	o	|	|	|	|	2.00
26.500	0.00	0.34	0.912	o	|	|	|	|	2.00
26.583	0.00	0.34	0.910	o	|	|	|	|	1.99
26.667	0.00	0.34	0.908	o	|	|	|	|	1.99
26.750	0.00	0.34	0.905	o	|	|	|	|	1.98
26.833	0.00	0.34	0.903	o	|	|	|	|	1.98
26.917	0.00	0.34	0.901	o	|	|	|	|	1.97
27.000	0.00	0.34	0.898	o	|	|	|	|	1.97
27.083	0.00	0.34	0.896	o	|	|	|	|	1.96
27.167	0.00	0.34	0.894	o	|	|	|	|	1.96
27.250	0.00	0.34	0.891	o	|	|	|	|	1.95
27.333	0.00	0.34	0.889	o	|	|	|	|	1.95
27.417	0.00	0.34	0.887	o	|	|	|	|	1.94
27.500	0.00	0.34	0.884	o	|	|	|	|	1.94
27.583	0.00	0.34	0.882	o	|	|	|	|	1.93
27.667	0.00	0.34	0.880	o	|	|	|	|	1.93
27.750	0.00	0.33	0.877	o	|	|	|	|	1.92
27.833	0.00	0.33	0.875	o	|	|	|	|	1.92
27.917	0.00	0.33	0.873	o	|	|	|	|	1.91
28.000	0.00	0.33	0.870	o	|	|	|	|	1.91
28.083	0.00	0.33	0.868	o	|	|	|	|	1.91
28.167	0.00	0.33	0.866	o	|	|	|	|	1.90
28.250	0.00	0.33	0.864	o	|	|	|	|	1.90
28.333	0.00	0.33	0.861	o	|	|	|	|	1.89
28.417	0.00	0.33	0.859	o	|	|	|	|	1.89
28.500	0.00	0.33	0.857	o	|	|	|	|	1.88
28.583	0.00	0.33	0.854	o	|	|	|	|	1.88
28.667	0.00	0.33	0.852	o	|	|	|	|	1.87
28.750	0.00	0.33	0.850	o	|	|	|	|	1.87
28.833	0.00	0.33	0.848	o	|	|	|	|	1.86
28.917	0.00	0.33	0.845	o	|	|	|	|	1.86
29.000	0.00	0.33	0.843	o	|	|	|	|	1.85
29.083	0.00	0.33	0.841	o	|	|	|	|	1.85
29.167	0.00	0.33	0.839	o	|	|	|	|	1.84
29.250	0.00	0.32	0.836	o	|	|	|	|	1.84
29.333	0.00	0.32	0.834	o	|	|	|	|	1.83
29.417	0.00	0.32	0.832	o	|	|	|	|	1.83
29.500	0.00	0.32	0.830	o	|	|	|	|	1.83
29.583	0.00	0.32	0.828	o	|	|	|	|	1.82
29.667	0.00	0.32	0.825	o	|	|	|	|	1.82
29.750	0.00	0.32	0.823	o	|	|	|	|	1.81
29.833	0.00	0.32	0.821	o	|	|	|	|	1.81
29.917	0.00	0.32	0.819	o	|	|	|	|	1.80
30.000	0.00	0.32	0.816	o	|	|	|	|	1.80
30.083	0.00	0.32	0.814	o	|	|	|	|	1.79
30.167	0.00	0.32	0.812	o	|	|	|	|	1.79

30.250	0.00	0.32	0.810	o	|	|	|	|	1.78
30.333	0.00	0.32	0.808	o	|	|	|	|	1.78
30.417	0.00	0.32	0.806	o	|	|	|	|	1.78
30.500	0.00	0.32	0.803	o	|	|	|	|	1.77
30.583	0.00	0.32	0.801	o	|	|	|	|	1.77
30.667	0.00	0.32	0.799	o	|	|	|	|	1.76
30.750	0.00	0.32	0.797	o	|	|	|	|	1.76
30.833	0.00	0.31	0.795	o	|	|	|	|	1.75
30.917	0.00	0.31	0.792	o	|	|	|	|	1.75
31.000	0.00	0.31	0.790	o	|	|	|	|	1.74
31.083	0.00	0.31	0.788	o	|	|	|	|	1.74
31.167	0.00	0.31	0.786	o	|	|	|	|	1.73
31.250	0.00	0.31	0.784	o	|	|	|	|	1.73
31.333	0.00	0.31	0.782	o	|	|	|	|	1.73
31.417	0.00	0.31	0.780	o	|	|	|	|	1.72
31.500	0.00	0.31	0.777	o	|	|	|	|	1.72
31.583	0.00	0.31	0.775	o	|	|	|	|	1.71
31.667	0.00	0.31	0.773	o	|	|	|	|	1.71
31.750	0.00	0.31	0.771	o	|	|	|	|	1.70
31.833	0.00	0.31	0.769	o	|	|	|	|	1.70
31.917	0.00	0.31	0.767	o	|	|	|	|	1.70
32.000	0.00	0.31	0.765	o	|	|	|	|	1.69
32.083	0.00	0.31	0.763	o	|	|	|	|	1.69
32.167	0.00	0.31	0.760	o	|	|	|	|	1.68
32.250	0.00	0.31	0.758	o	|	|	|	|	1.68
32.333	0.00	0.31	0.756	o	|	|	|	|	1.67
32.417	0.00	0.30	0.754	o	|	|	|	|	1.67
32.500	0.00	0.30	0.752	o	|	|	|	|	1.66
32.583	0.00	0.30	0.750	o	|	|	|	|	1.66
32.667	0.00	0.30	0.748	o	|	|	|	|	1.66
32.750	0.00	0.30	0.746	o	|	|	|	|	1.65
32.833	0.00	0.30	0.744	o	|	|	|	|	1.65
32.917	0.00	0.30	0.742	o	|	|	|	|	1.64
33.000	0.00	0.30	0.740	o	|	|	|	|	1.64
33.083	0.00	0.30	0.737	o	|	|	|	|	1.63
33.167	0.00	0.30	0.735	o	|	|	|	|	1.63
33.250	0.00	0.30	0.733	o	|	|	|	|	1.63
33.333	0.00	0.30	0.731	o	|	|	|	|	1.62
33.417	0.00	0.30	0.729	o	|	|	|	|	1.62
33.500	0.00	0.30	0.727	o	|	|	|	|	1.61
33.583	0.00	0.30	0.725	o	|	|	|	|	1.61
33.667	0.00	0.30	0.723	o	|	|	|	|	1.60
33.750	0.00	0.30	0.721	o	|	|	|	|	1.60
33.833	0.00	0.30	0.719	o	|	|	|	|	1.60
33.917	0.00	0.30	0.717	o	|	|	|	|	1.59
34.000	0.00	0.29	0.715	o	|	|	|	|	1.59
34.083	0.00	0.29	0.713	o	|	|	|	|	1.58
34.167	0.00	0.29	0.711	o	|	|	|	|	1.58
34.250	0.00	0.29	0.709	o	|	|	|	|	1.58
34.333	0.00	0.29	0.707	o	|	|	|	|	1.57
34.417	0.00	0.29	0.705	o	|	|	|	|	1.57
34.500	0.00	0.29	0.703	o	|	|	|	|	1.56
34.583	0.00	0.29	0.701	o	|	|	|	|	1.56
34.667	0.00	0.29	0.699	o	|	|	|	|	1.55
34.750	0.00	0.29	0.697	o	|	|	|	|	1.55
34.833	0.00	0.29	0.695	o	|	|	|	|	1.55
34.917	0.00	0.29	0.693	o	|	|	|	|	1.54
35.000	0.00	0.29	0.691	o	|	|	|	|	1.54
35.083	0.00	0.29	0.689	o	|	|	|	|	1.53
35.167	0.00	0.29	0.687	o	|	|	|	|	1.53
35.250	0.00	0.29	0.685	o	|	|	|	|	1.53
35.333	0.00	0.29	0.683	o	|	|	|	|	1.52
35.417	0.00	0.29	0.681	o	|	|	|	|	1.52
35.500	0.00	0.29	0.679	o	|	|	|	|	1.51
35.583	0.00	0.29	0.677	o	|	|	|	|	1.51
35.667	0.00	0.29	0.675	o	|	|	|	|	1.51
35.750	0.00	0.28	0.673	o	|	|	|	|	1.50
35.833	0.00	0.28	0.671	o	|	|	|	|	1.50
35.917	0.00	0.28	0.669	o	|	|	|	|	1.49
36.000	0.00	0.28	0.667	o	|	|	|	|	1.49
36.083	0.00	0.28	0.665	o	|	|	|	|	1.48
36.167	0.00	0.28	0.663	o	|	|	|	|	1.48
36.250	0.00	0.28	0.661	o	|	|	|	|	1.48
36.333	0.00	0.28	0.659	o	|	|	|	|	1.47
36.417	0.00	0.28	0.657	o	|	|	|	|	1.47
36.500	0.00	0.28	0.655	o	|	|	|	|	1.46
36.583	0.00	0.28	0.654	o	|	|	|	|	1.46
36.667	0.00	0.28	0.652	o	|	|	|	|	1.46
36.750	0.00	0.28	0.650	o	|	|	|	|	1.45
36.833	0.00	0.28	0.648	o	|	|	|	|	1.45
36.917	0.00	0.28	0.646	o	|	|	|	|	1.44
37.000	0.00	0.28	0.644	o	|	|	|	|	1.44
37.083	0.00	0.28	0.642	o	|	|	|	|	1.44
37.167	0.00	0.28	0.640	o	|	|	|	|	1.43
37.250	0.00	0.28	0.638	o	|	|	|	|	1.43
37.333	0.00	0.28	0.636	o	|	|	|	|	1.43

37.417	0.00	0.28	0.634	o	|	|	|	|	1.42
37.500	0.00	0.27	0.633	o	|	|	|	|	1.42
37.583	0.00	0.27	0.631	o	|	|	|	|	1.41
37.667	0.00	0.27	0.629	o	|	|	|	|	1.41
37.750	0.00	0.27	0.627	o	|	|	|	|	1.41
37.833	0.00	0.27	0.625	o	|	|	|	|	1.40
37.917	0.00	0.27	0.623	o	|	|	|	|	1.40
38.000	0.00	0.27	0.621	o	|	|	|	|	1.39
38.083	0.00	0.27	0.619	o	|	|	|	|	1.39
38.167	0.00	0.27	0.618	o	|	|	|	|	1.39
38.250	0.00	0.27	0.616	o	|	|	|	|	1.38
38.333	0.00	0.27	0.614	o	|	|	|	|	1.38
38.417	0.00	0.27	0.612	o	|	|	|	|	1.37
38.500	0.00	0.27	0.610	o	|	|	|	|	1.37
38.583	0.00	0.27	0.608	o	|	|	|	|	1.37
38.667	0.00	0.27	0.606	o	|	|	|	|	1.36
38.750	0.00	0.27	0.605	o	|	|	|	|	1.36
38.833	0.00	0.27	0.603	o	|	|	|	|	1.36
38.917	0.00	0.27	0.601	o	|	|	|	|	1.35
39.000	0.00	0.27	0.599	o	|	|	|	|	1.35
39.083	0.00	0.27	0.597	o	|	|	|	|	1.34
39.167	0.00	0.27	0.595	o	|	|	|	|	1.34
39.250	0.00	0.27	0.594	o	|	|	|	|	1.34
39.333	0.00	0.26	0.592	o	|	|	|	|	1.33
39.417	0.00	0.26	0.590	o	|	|	|	|	1.33
39.500	0.00	0.26	0.588	o	|	|	|	|	1.33
39.583	0.00	0.26	0.586	o	|	|	|	|	1.32
39.667	0.00	0.26	0.584	o	|	|	|	|	1.32
39.750	0.00	0.26	0.583	o	|	|	|	|	1.31
39.833	0.00	0.26	0.581	o	|	|	|	|	1.31
39.917	0.00	0.26	0.579	o	|	|	|	|	1.31
40.000	0.00	0.26	0.577	o	|	|	|	|	1.30
40.083	0.00	0.26	0.575	o	|	|	|	|	1.30
40.167	0.00	0.26	0.574	o	|	|	|	|	1.30
40.250	0.00	0.26	0.572	o	|	|	|	|	1.29
40.333	0.00	0.26	0.570	o	|	|	|	|	1.29
40.417	0.00	0.26	0.568	o	|	|	|	|	1.28
40.500	0.00	0.26	0.566	o	|	|	|	|	1.28
40.583	0.00	0.26	0.565	o	|	|	|	|	1.28
40.667	0.00	0.26	0.563	o	|	|	|	|	1.27
40.750	0.00	0.26	0.561	o	|	|	|	|	1.27
40.833	0.00	0.26	0.559	o	|	|	|	|	1.27
40.917	0.00	0.26	0.558	o	|	|	|	|	1.26
41.000	0.00	0.26	0.556	o	|	|	|	|	1.26
41.083	0.00	0.26	0.554	o	|	|	|	|	1.25
41.167	0.00	0.25	0.552	o	|	|	|	|	1.25
41.250	0.00	0.25	0.551	o	|	|	|	|	1.25
41.333	0.00	0.25	0.549	o	|	|	|	|	1.24
41.417	0.00	0.25	0.547	o	|	|	|	|	1.24
41.500	0.00	0.25	0.545	o	|	|	|	|	1.24
41.583	0.00	0.25	0.544	o	|	|	|	|	1.23
41.667	0.00	0.25	0.542	o	|	|	|	|	1.23
41.750	0.00	0.25	0.540	o	|	|	|	|	1.23
41.833	0.00	0.25	0.538	o	|	|	|	|	1.22
41.917	0.00	0.25	0.537	o	|	|	|	|	1.22
42.000	0.00	0.25	0.535	o	|	|	|	|	1.22
42.083	0.00	0.25	0.533	o	|	|	|	|	1.21
42.167	0.00	0.25	0.531	o	|	|	|	|	1.21
42.250	0.00	0.25	0.530	o	|	|	|	|	1.20
42.333	0.00	0.25	0.528	o	|	|	|	|	1.20
42.417	0.00	0.25	0.526	o	|	|	|	|	1.20
42.500	0.00	0.25	0.525	o	|	|	|	|	1.19
42.583	0.00	0.25	0.523	o	|	|	|	|	1.19
42.667	0.00	0.25	0.521	o	|	|	|	|	1.19
42.750	0.00	0.25	0.520	o	|	|	|	|	1.18
42.833	0.00	0.25	0.518	o	|	|	|	|	1.18
42.917	0.00	0.25	0.516	o	|	|	|	|	1.18
43.000	0.00	0.25	0.514	o	|	|	|	|	1.17
43.083	0.00	0.25	0.513	o	|	|	|	|	1.17
43.167	0.00	0.24	0.511	o	|	|	|	|	1.17
43.250	0.00	0.24	0.509	o	|	|	|	|	1.16
43.333	0.00	0.24	0.508	o	|	|	|	|	1.16
43.417	0.00	0.24	0.506	o	|	|	|	|	1.16
43.500	0.00	0.24	0.504	o	|	|	|	|	1.15
43.583	0.00	0.24	0.503	o	|	|	|	|	1.15
43.667	0.00	0.24	0.501	o	|	|	|	|	1.14
43.750	0.00	0.24	0.499	o	|	|	|	|	1.14
43.833	0.00	0.24	0.498	o	|	|	|	|	1.14
43.917	0.00	0.24	0.496	o	|	|	|	|	1.13
44.000	0.00	0.24	0.494	o	|	|	|	|	1.13
44.083	0.00	0.24	0.493	o	|	|	|	|	1.13
44.167	0.00	0.24	0.491	o	|	|	|	|	1.12
44.250	0.00	0.24	0.489	o	|	|	|	|	1.12
44.333	0.00	0.24	0.488	o	|	|	|	|	1.12
44.417	0.00	0.24	0.486	o	|	|	|	|	1.11
44.500	0.00	0.24	0.484	o	|	|	|	|	1.11

44.583	0.00	0.24	0.483	o	|	|	|	|	1.11
44.667	0.00	0.24	0.481	o	|	|	|	|	1.10
44.750	0.00	0.24	0.480	o	|	|	|	|	1.10
44.833	0.00	0.24	0.478	o	|	|	|	|	1.10
44.917	0.00	0.24	0.476	o	|	|	|	|	1.09
45.000	0.00	0.24	0.475	o	|	|	|	|	1.09
45.083	0.00	0.24	0.473	o	|	|	|	|	1.09
45.167	0.00	0.23	0.471	o	|	|	|	|	1.08
45.250	0.00	0.23	0.470	o	|	|	|	|	1.08
45.333	0.00	0.23	0.468	o	|	|	|	|	1.08
45.417	0.00	0.23	0.467	o	|	|	|	|	1.07
45.500	0.00	0.23	0.465	o	|	|	|	|	1.07
45.583	0.00	0.23	0.463	o	|	|	|	|	1.07
45.667	0.00	0.23	0.462	o	|	|	|	|	1.06
45.750	0.00	0.23	0.460	o	|	|	|	|	1.06
45.833	0.00	0.23	0.459	o	|	|	|	|	1.06
45.917	0.00	0.23	0.457	o	|	|	|	|	1.05
46.000	0.00	0.23	0.455	o	|	|	|	|	1.05
46.083	0.00	0.23	0.454	o	|	|	|	|	1.05
46.167	0.00	0.23	0.452	o	|	|	|	|	1.04
46.250	0.00	0.23	0.451	o	|	|	|	|	1.04
46.333	0.00	0.23	0.449	o	|	|	|	|	1.04
46.417	0.00	0.23	0.447	o	|	|	|	|	1.03
46.500	0.00	0.23	0.446	o	|	|	|	|	1.03
46.583	0.00	0.23	0.444	o	|	|	|	|	1.03
46.667	0.00	0.23	0.443	o	|	|	|	|	1.02
46.750	0.00	0.23	0.441	o	|	|	|	|	1.02
46.833	0.00	0.23	0.440	o	|	|	|	|	1.02
46.917	0.00	0.23	0.438	o	|	|	|	|	1.01
47.000	0.00	0.23	0.436	o	|	|	|	|	1.01
47.083	0.00	0.23	0.435	o	|	|	|	|	1.01
47.167	0.00	0.23	0.433	o	|	|	|	|	1.00
47.250	0.00	0.23	0.432	o	|	|	|	|	1.00
47.333	0.00	0.22	0.430	o	|	|	|	|	1.00
47.417	0.00	0.22	0.429	o	|	|	|	|	0.99
47.500	0.00	0.22	0.427	o	|	|	|	|	0.99
47.583	0.00	0.22	0.426	o	|	|	|	|	0.99
47.667	0.00	0.22	0.424	o	|	|	|	|	0.98
47.750	0.00	0.22	0.423	o	|	|	|	|	0.98
47.833	0.00	0.22	0.421	o	|	|	|	|	0.98
47.917	0.00	0.22	0.420	o	|	|	|	|	0.97
48.000	0.00	0.22	0.418	o	|	|	|	|	0.97
48.083	0.00	0.22	0.417	o	|	|	|	|	0.97
48.167	0.00	0.22	0.415	o	|	|	|	|	0.96
48.250	0.00	0.22	0.414	o	|	|	|	|	0.96
48.333	0.00	0.22	0.412	o	|	|	|	|	0.96
48.417	0.00	0.21	0.411	o	|	|	|	|	0.95
48.500	0.00	0.21	0.409	o	|	|	|	|	0.95
48.583	0.00	0.21	0.408	o	|	|	|	|	0.95
48.667	0.00	0.21	0.406	o	|	|	|	|	0.94
48.750	0.00	0.21	0.405	o	|	|	|	|	0.94
48.833	0.00	0.21	0.403	o	|	|	|	|	0.94
48.917	0.00	0.21	0.402	o	|	|	|	|	0.93
49.000	0.00	0.21	0.400	o	|	|	|	|	0.93
49.083	0.00	0.21	0.399	o	|	|	|	|	0.93
49.167	0.00	0.21	0.398	o	|	|	|	|	0.92
49.250	0.00	0.21	0.396	o	|	|	|	|	0.92
49.333	0.00	0.21	0.395	o	|	|	|	|	0.92
49.417	0.00	0.21	0.393	o	|	|	|	|	0.91
49.500	0.00	0.20	0.392	o	|	|	|	|	0.91
49.583	0.00	0.20	0.390	o	|	|	|	|	0.91
49.667	0.00	0.20	0.389	o	|	|	|	|	0.90
49.750	0.00	0.20	0.388	o	|	|	|	|	0.90
49.833	0.00	0.20	0.386	o	|	|	|	|	0.90
49.917	0.00	0.20	0.385	o	|	|	|	|	0.89
50.000	0.00	0.20	0.384	o	|	|	|	|	0.89
50.083	0.00	0.20	0.382	o	|	|	|	|	0.89
50.167	0.00	0.20	0.381	o	|	|	|	|	0.88
50.250	0.00	0.20	0.379	o	|	|	|	|	0.88
50.333	0.00	0.20	0.378	o	|	|	|	|	0.88
50.417	0.00	0.20	0.377	o	|	|	|	|	0.87
50.500	0.00	0.20	0.375	o	|	|	|	|	0.87
50.583	0.00	0.20	0.374	o	|	|	|	|	0.87
50.667	0.00	0.19	0.373	o	|	|	|	|	0.86
50.750	0.00	0.19	0.371	o	|	|	|	|	0.86
50.833	0.00	0.19	0.370	o	|	|	|	|	0.86
50.917	0.00	0.19	0.369	o	|	|	|	|	0.86
51.000	0.00	0.19	0.367	o	|	|	|	|	0.85
51.083	0.00	0.19	0.366	o	|	|	|	|	0.85
51.167	0.00	0.19	0.365	o	|	|	|	|	0.85
51.250	0.00	0.19	0.363	o	|	|	|	|	0.84
51.333	0.00	0.19	0.362	o	|	|	|	|	0.84
51.417	0.00	0.19	0.361	o	|	|	|	|	0.84
51.500	0.00	0.19	0.359	o	|	|	|	|	0.83
51.583	0.00	0.19	0.358	o	|	|	|	|	0.83
51.667	0.00	0.19	0.357	o	|	|	|	|	0.83

51.750	0.00	0.19	0.356	o	|	|	|	0.83
51.833	0.00	0.18	0.354	o	|	|	|	0.82
51.917	0.00	0.18	0.353	o	|	|	|	0.82
52.000	0.00	0.18	0.352	o	|	|	|	0.82
52.083	0.00	0.18	0.351	o	|	|	|	0.81
52.167	0.00	0.18	0.349	o	|	|	|	0.81
52.250	0.00	0.18	0.348	o	|	|	|	0.81
52.333	0.00	0.18	0.347	o	|	|	|	0.80
52.417	0.00	0.18	0.346	o	|	|	|	0.80
52.500	0.00	0.18	0.344	o	|	|	|	0.80
52.583	0.00	0.18	0.343	o	|	|	|	0.80
52.667	0.00	0.18	0.342	o	|	|	|	0.79
52.750	0.00	0.18	0.341	o	|	|	|	0.79
52.833	0.00	0.18	0.339	o	|	|	|	0.79
52.917	0.00	0.18	0.338	o	|	|	|	0.78
53.000	0.00	0.18	0.337	o	|	|	|	0.78
53.083	0.00	0.18	0.336	o	|	|	|	0.78
53.167	0.00	0.17	0.335	o	|	|	|	0.78
53.250	0.00	0.17	0.333	o	|	|	|	0.77
53.333	0.00	0.17	0.332	o	|	|	|	0.77
53.417	0.00	0.17	0.331	o	|	|	|	0.77
53.500	0.00	0.17	0.330	o	|	|	|	0.77
53.583	0.00	0.17	0.329	o	|	|	|	0.76
53.667	0.00	0.17	0.327	o	|	|	|	0.76
53.750	0.00	0.17	0.326	o	|	|	|	0.76
53.833	0.00	0.17	0.325	o	|	|	|	0.75
53.917	0.00	0.17	0.324	o	|	|	|	0.75
54.000	0.00	0.17	0.323	o	|	|	|	0.75
54.083	0.00	0.17	0.322	o	|	|	|	0.75
54.167	0.00	0.17	0.320	o	|	|	|	0.74
54.250	0.00	0.17	0.319	o	|	|	|	0.74
54.333	0.00	0.17	0.318	o	|	|	|	0.74
54.417	0.00	0.17	0.317	o	|	|	|	0.74
54.500	0.00	0.16	0.316	o	|	|	|	0.73
54.583	0.00	0.16	0.315	o	|	|	|	0.73
54.667	0.00	0.16	0.314	o	|	|	|	0.73
54.750	0.00	0.16	0.312	o	|	|	|	0.72
54.833	0.00	0.16	0.311	o	|	|	|	0.72
54.917	0.00	0.16	0.310	o	|	|	|	0.72
55.000	0.00	0.16	0.309	o	|	|	|	0.72
55.083	0.00	0.16	0.308	o	|	|	|	0.71
55.167	0.00	0.16	0.307	o	|	|	|	0.71
55.250	0.00	0.16	0.306	o	|	|	|	0.71
55.333	0.00	0.16	0.305	o	|	|	|	0.71
55.417	0.00	0.16	0.304	o	|	|	|	0.70
55.500	0.00	0.16	0.302	o	|	|	|	0.70
55.583	0.00	0.16	0.301	o	|	|	|	0.70
55.667	0.00	0.16	0.300	o	|	|	|	0.70
55.750	0.00	0.16	0.299	o	|	|	|	0.69
55.833	0.00	0.16	0.298	o	|	|	|	0.69
55.917	0.00	0.16	0.297	o	|	|	|	0.69
56.000	0.00	0.15	0.296	o	|	|	|	0.69
56.083	0.00	0.15	0.295	o	|	|	|	0.68
56.167	0.00	0.15	0.294	o	|	|	|	0.68
56.250	0.00	0.15	0.293	o	|	|	|	0.68
56.333	0.00	0.15	0.292	o	|	|	|	0.68
56.417	0.00	0.15	0.291	o	|	|	|	0.67
56.500	0.00	0.15	0.290	o	|	|	|	0.67
56.583	0.00	0.15	0.289	o	|	|	|	0.67
56.667	0.00	0.15	0.288	o	|	|	|	0.67
56.750	0.00	0.15	0.287	o	|	|	|	0.66
56.833	0.00	0.15	0.286	o	|	|	|	0.66
56.917	0.00	0.15	0.285	o	|	|	|	0.66
57.000	0.00	0.15	0.284	o	|	|	|	0.66
57.083	0.00	0.15	0.283	o	|	|	|	0.66
57.167	0.00	0.15	0.282	o	|	|	|	0.65
57.250	0.00	0.15	0.280	o	|	|	|	0.65
57.333	0.00	0.15	0.279	o	|	|	|	0.65
57.417	0.00	0.15	0.278	o	|	|	|	0.65
57.500	0.00	0.14	0.277	o	|	|	|	0.64
57.583	0.00	0.14	0.276	o	|	|	|	0.64
57.667	0.00	0.14	0.275	o	|	|	|	0.64
57.750	0.00	0.14	0.275	o	|	|	|	0.64
57.833	0.00	0.14	0.274	o	|	|	|	0.63
57.917	0.00	0.14	0.273	o	|	|	|	0.63
58.000	0.00	0.14	0.272	o	|	|	|	0.63
58.083	0.00	0.14	0.271	o	|	|	|	0.63
58.167	0.00	0.14	0.270	o	|	|	|	0.63
58.250	0.00	0.14	0.269	o	|	|	|	0.62
58.333	0.00	0.14	0.268	o	|	|	|	0.62
58.417	0.00	0.14	0.267	o	|	|	|	0.62
58.500	0.00	0.14	0.266	o	|	|	|	0.62
58.583	0.00	0.14	0.265	o	|	|	|	0.61
58.667	0.00	0.14	0.264	o	|	|	|	0.61
58.750	0.00	0.14	0.263	o	|	|	|	0.61
58.833	0.00	0.14	0.262	o	|	|	|	0.61

58.917	0.00	0.14	0.261	o	|	|	|	|	0.61
59.000	0.00	0.14	0.260	o	|	|	|	|	0.60
59.083	0.00	0.14	0.259	o	|	|	|	|	0.60
59.167	0.00	0.13	0.258	o	|	|	|	|	0.60
59.250	0.00	0.13	0.257	o	|	|	|	|	0.60
59.333	0.00	0.13	0.256	o	|	|	|	|	0.59
59.417	0.00	0.13	0.255	o	|	|	|	|	0.59
59.500	0.00	0.13	0.255	o	|	|	|	|	0.59
59.583	0.00	0.13	0.254	o	|	|	|	|	0.59
59.667	0.00	0.13	0.253	o	|	|	|	|	0.59
59.750	0.00	0.13	0.252	o	|	|	|	|	0.58
59.833	0.00	0.13	0.251	o	|	|	|	|	0.58
59.917	0.00	0.13	0.250	o	|	|	|	|	0.58
60.000	0.00	0.13	0.249	o	|	|	|	|	0.58
60.083	0.00	0.13	0.248	o	|	|	|	|	0.58
60.167	0.00	0.13	0.247	o	|	|	|	|	0.57
60.250	0.00	0.13	0.246	o	|	|	|	|	0.57
60.333	0.00	0.13	0.246	o	|	|	|	|	0.57
60.417	0.00	0.13	0.245	o	|	|	|	|	0.57
60.500	0.00	0.13	0.244	o	|	|	|	|	0.57
60.583	0.00	0.13	0.243	o	|	|	|	|	0.56
60.667	0.00	0.13	0.242	o	|	|	|	|	0.56
60.750	0.00	0.13	0.241	o	|	|	|	|	0.56
60.833	0.00	0.13	0.240	o	|	|	|	|	0.56
60.917	0.00	0.13	0.239	o	|	|	|	|	0.56
61.000	0.00	0.12	0.239	o	|	|	|	|	0.55
61.083	0.00	0.12	0.238	o	|	|	|	|	0.55
61.167	0.00	0.12	0.237	o	|	|	|	|	0.55
61.250	0.00	0.12	0.236	o	|	|	|	|	0.55
61.333	0.00	0.12	0.235	o	|	|	|	|	0.55
61.417	0.00	0.12	0.234	o	|	|	|	|	0.54
61.500	0.00	0.12	0.234	o	|	|	|	|	0.54
61.583	0.00	0.12	0.233	o	|	|	|	|	0.54
61.667	0.00	0.12	0.232	o	|	|	|	|	0.54
61.750	0.00	0.12	0.231	o	|	|	|	|	0.54
61.833	0.00	0.12	0.230	o	|	|	|	|	0.53
61.917	0.00	0.12	0.229	o	|	|	|	|	0.53
62.000	0.00	0.12	0.229	o	|	|	|	|	0.53
62.083	0.00	0.12	0.228	o	|	|	|	|	0.53
62.167	0.00	0.12	0.227	o	|	|	|	|	0.53
62.250	0.00	0.12	0.226	o	|	|	|	|	0.52
62.333	0.00	0.12	0.225	o	|	|	|	|	0.52
62.417	0.00	0.12	0.224	o	|	|	|	|	0.52
62.500	0.00	0.12	0.224	o	|	|	|	|	0.52
62.583	0.00	0.12	0.223	o	|	|	|	|	0.52
62.667	0.00	0.12	0.222	o	|	|	|	|	0.52
62.750	0.00	0.12	0.221	o	|	|	|	|	0.51
62.833	0.00	0.12	0.220	o	|	|	|	|	0.51
62.917	0.00	0.11	0.220	o	|	|	|	|	0.51
63.000	0.00	0.11	0.219	o	|	|	|	|	0.51
63.083	0.00	0.11	0.218	o	|	|	|	|	0.51
63.167	0.00	0.11	0.217	o	|	|	|	|	0.50
63.250	0.00	0.11	0.217	o	|	|	|	|	0.50
63.333	0.00	0.11	0.216	o	|	|	|	|	0.50
63.417	0.00	0.11	0.215	o	|	|	|	|	0.50
63.500	0.00	0.11	0.214	o	|	|	|	|	0.50
63.583	0.00	0.11	0.213	o	|	|	|	|	0.50
63.667	0.00	0.11	0.213	o	|	|	|	|	0.49
63.750	0.00	0.11	0.212	o	|	|	|	|	0.49
63.833	0.00	0.11	0.211	o	|	|	|	|	0.49
63.917	0.00	0.11	0.210	o	|	|	|	|	0.49
64.000	0.00	0.11	0.210	o	|	|	|	|	0.49
64.083	0.00	0.11	0.209	o	|	|	|	|	0.48
64.167	0.00	0.11	0.208	o	|	|	|	|	0.48
64.250	0.00	0.11	0.207	o	|	|	|	|	0.48
64.333	0.00	0.11	0.207	o	|	|	|	|	0.48
64.417	0.00	0.11	0.206	o	|	|	|	|	0.48
64.500	0.00	0.11	0.205	o	|	|	|	|	0.48
64.583	0.00	0.11	0.204	o	|	|	|	|	0.47
64.667	0.00	0.11	0.204	o	|	|	|	|	0.47
64.750	0.00	0.11	0.203	o	|	|	|	|	0.47
64.833	0.00	0.11	0.202	o	|	|	|	|	0.47
64.917	0.00	0.11	0.202	o	|	|	|	|	0.47
65.000	0.00	0.10	0.201	o	|	|	|	|	0.47
65.083	0.00	0.10	0.200	o	|	|	|	|	0.46
65.167	0.00	0.10	0.199	o	|	|	|	|	0.46
65.250	0.00	0.10	0.199	o	|	|	|	|	0.46
65.333	0.00	0.10	0.198	o	|	|	|	|	0.46
65.417	0.00	0.10	0.197	o	|	|	|	|	0.46
65.500	0.00	0.10	0.196	o	|	|	|	|	0.46
65.583	0.00	0.10	0.196	o	|	|	|	|	0.45
65.667	0.00	0.10	0.195	o	|	|	|	|	0.45
65.750	0.00	0.10	0.194	o	|	|	|	|	0.45
65.833	0.00	0.10	0.194	o	|	|	|	|	0.45
65.917	0.00	0.10	0.193	o	|	|	|	|	0.45
66.000	0.00	0.10	0.192	o	|	|	|	|	0.45

```
66.083    0.00    0.10      0.192  o       |       |       |       |     0.44
66.167    0.00    0.10      0.191  o       |       |       |       |     0.44

       Remaining water in basin =    0.19 (Ac.Ft)


       ****************************HYDROGRAPH DATA****************************
                     Number of intervals =   794
                     Time interval =    5.0 (Min.)
                     Maximum/Peak flow rate =       79.141 (CFS)
                     Total volume =       5.936 (Ac.Ft)
              Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
       ***********************************************************************

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FLOOD HYDROGRAPH ROUTING PROGRAM
Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro21006100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 77
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 79.376 (CFS)
Total volume = 8.658 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
_____

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 77
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

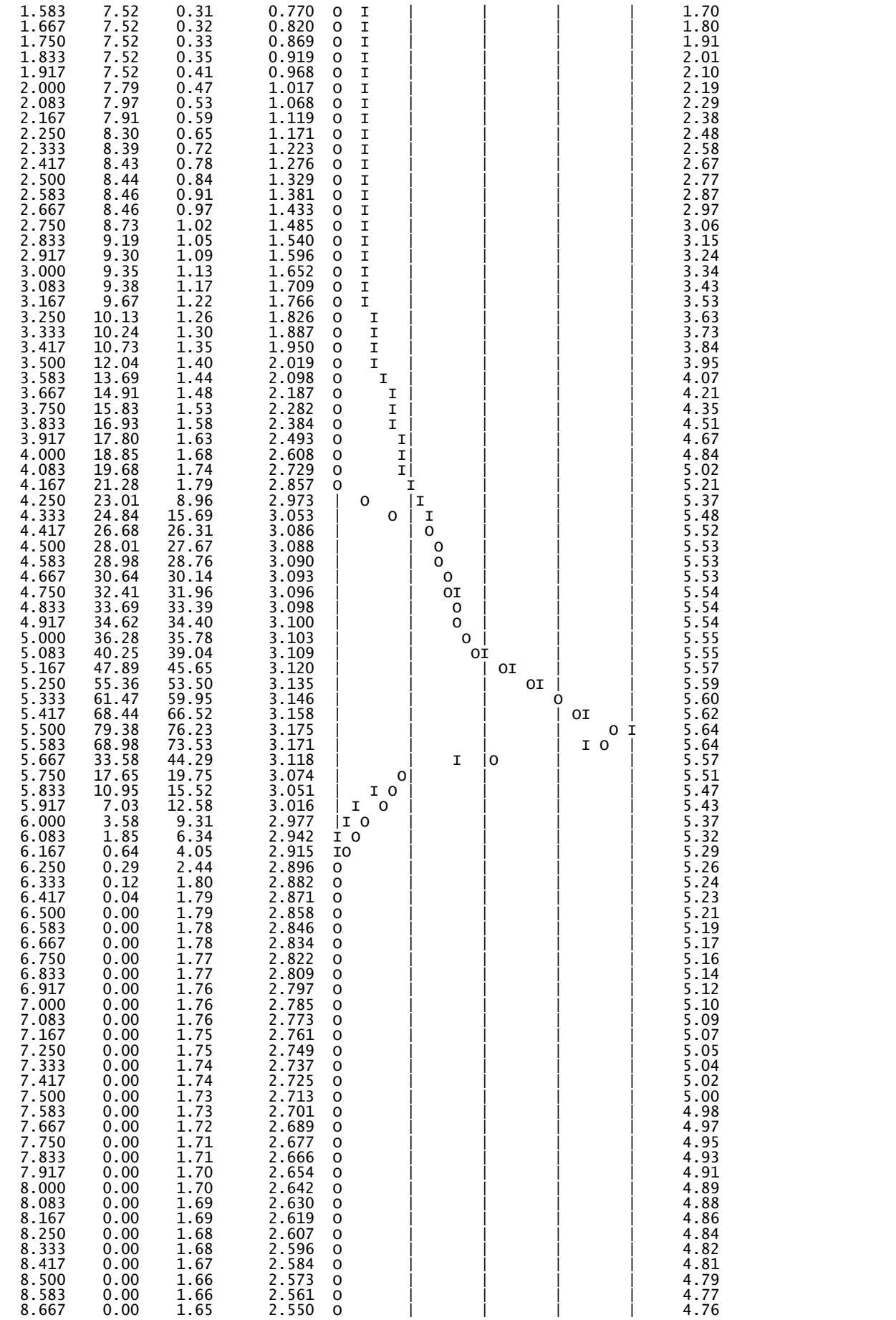
Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.431	0.225	0.430	0.432
2.000	0.914	0.344	0.913	0.915
3.000	1.451	0.991	1.448	1.454
4.000	2.049	1.417	2.044	2.054
5.000	2.712	1.731	2.706	2.718
5.250	2.888	1.801	2.882	2.894
5.500	3.069	17.046	3.010	3.128
6.000	3.443	225.078	2.668	4.218

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 19.8 39.69 59.53 79.38	Depth (Ft.)
0.083	1.37	0.00	0.005	O | | | |	0.01
0.167	3.91	0.01	0.023	OI | | | |	0.05
0.250	4.93	0.03	0.053	OI | | | |	0.12
0.333	5.30	0.05	0.088	O I | | | |	0.20
0.417	5.49	0.07	0.125	O I | | | |	0.29
0.500	5.89	0.09	0.164	O I | | | |	0.38
0.583	6.37	0.11	0.205	O I | | | |	0.48
0.667	6.48	0.13	0.249	O I | | | |	0.58
0.750	6.53	0.15	0.292	O I | | | |	0.68
0.833	6.56	0.18	0.336	O I | | | |	0.78
0.917	6.58	0.20	0.380	O I | | | |	0.88
1.000	6.85	0.22	0.425	O I | | | |	0.99
1.083	7.31	0.24	0.472	O I | | | |	1.09
1.167	7.42	0.25	0.521	O I | | | |	1.19
1.250	7.47	0.26	0.571	O I | | | |	1.29
1.333	7.50	0.27	0.621	O I | | | |	1.39
1.417	7.52	0.28	0.670	O I | | | |	1.50
1.500	7.52	0.30	0.720	O I | | | |	1.60



1.583	7.52	0.31	0.770	O I	1.70
1.667	7.52	0.32	0.820	O I	1.80
1.750	7.52	0.33	0.869	O I	1.91
1.833	7.52	0.35	0.919	O I	2.01
1.917	7.52	0.41	0.968	O I	2.10
2.000	7.79	0.47	1.017	O I	2.19
2.083	7.97	0.53	1.068	O I	2.29
2.167	7.91	0.59	1.119	O I	2.38
2.250	8.30	0.65	1.171	O I	2.48
2.333	8.39	0.72	1.223	O I	2.58
2.417	8.43	0.78	1.276	O I	2.67
2.500	8.44	0.84	1.329	O I	2.77
2.583	8.46	0.91	1.381	O I	2.87
2.667	8.46	0.97	1.433	O I	2.97
2.750	8.73	1.02	1.485	O I	3.06
2.833	9.19	1.05	1.540	O I	3.15
2.917	9.30	1.09	1.596	O I	3.24
3.000	9.35	1.13	1.652	O I	3.34
3.083	9.38	1.17	1.709	O I	3.43
3.167	9.67	1.22	1.766	O I	3.53
3.250	10.13	1.26	1.826	O I	3.63
3.333	10.24	1.30	1.887	O I	3.73
3.417	10.73	1.35	1.950	O I	3.84
3.500	12.04	1.40	2.019	O I	3.95
3.583	13.69	1.44	2.098	O I	4.07
3.667	14.91	1.48	2.187	O I	4.21
3.750	15.83	1.53	2.282	O I	4.35
3.833	16.93	1.58	2.384	O I	4.51
3.917	17.80	1.63	2.493	O I	4.67
4.000	18.85	1.68	2.608	O I	4.84
4.083	19.68	1.74	2.729	O I	5.02
4.167	21.28	1.79	2.857	O I	5.21
4.250	23.01	8.96	2.973	O I	5.37
4.333	24.84	15.69	3.053	O I	5.48
4.417	26.68	26.31	3.086	O	5.52
4.500	28.01	27.67	3.088	O	5.53
4.583	28.98	28.76	3.090	O	5.53
4.667	30.64	30.14	3.093	O	5.53
4.750	32.41	31.96	3.096	OI	5.54
4.833	33.69	33.39	3.098	O	5.54
4.917	34.62	34.40	3.100	O	5.54
5.000	36.28	35.78	3.103	O	5.55
5.083	40.25	39.04	3.109	OI	5.55
5.167	47.89	45.65	3.120	OI	5.57
5.250	55.36	53.50	3.135	OI	5.59
5.333	61.47	59.95	3.146	O	5.60
5.417	68.44	66.52	3.158	OI	5.62
5.500	79.38	76.23	3.175	O I	5.64
5.583	68.98	73.53	3.171	I O	5.64
5.667	33.58	44.29	3.118	I O	5.57
5.750	17.65	19.75	3.074	O	5.51
5.833	10.95	15.52	3.051	I O	5.47
5.917	7.03	12.58	3.016	I O	5.43
6.000	3.58	9.31	2.977	I O	5.37
6.083	1.85	6.34	2.942	I O	5.32
6.167	0.64	4.05	2.915	IO	5.29
6.250	0.29	2.44	2.896	O	5.26
6.333	0.12	1.80	2.882	O	5.24
6.417	0.04	1.79	2.871	O	5.23
6.500	0.00	1.79	2.858	O	5.21
6.583	0.00	1.78	2.846	O	5.19
6.667	0.00	1.78	2.834	O	5.17
6.750	0.00	1.77	2.822	O	5.16
6.833	0.00	1.77	2.809	O	5.14
6.917	0.00	1.76	2.797	O	5.12
7.000	0.00	1.76	2.785	O	5.10
7.083	0.00	1.76	2.773	O	5.09
7.167	0.00	1.75	2.761	O	5.07
7.250	0.00	1.75	2.749	O	5.05
7.333	0.00	1.74	2.737	O	5.04
7.417	0.00	1.74	2.725	O	5.02
7.500	0.00	1.73	2.713	O	5.00
7.583	0.00	1.73	2.701	O	4.98
7.667	0.00	1.72	2.689	O	4.97
7.750	0.00	1.71	2.677	O	4.95
7.833	0.00	1.71	2.666	O	4.93
7.917	0.00	1.70	2.654	O	4.91
8.000	0.00	1.70	2.642	O	4.89
8.083	0.00	1.69	2.630	O	4.88
8.167	0.00	1.69	2.619	O	4.86
8.250	0.00	1.68	2.607	O	4.84
8.333	0.00	1.68	2.596	O	4.82
8.417	0.00	1.67	2.584	O	4.81
8.500	0.00	1.66	2.573	O	4.79
8.583	0.00	1.66	2.561	O	4.77
8.667	0.00	1.65	2.550	O	4.76

8.750	0.00	1.65	2.538	o	|	|	|	|	4.74
8.833	0.00	1.64	2.527	o	|	|	|	|	4.72
8.917	0.00	1.64	2.516	o	|	|	|	|	4.70
9.000	0.00	1.63	2.504	o	|	|	|	|	4.69
9.083	0.00	1.63	2.493	o	|	|	|	|	4.67
9.167	0.00	1.62	2.482	o	|	|	|	|	4.65
9.250	0.00	1.62	2.471	o	|	|	|	|	4.64
9.333	0.00	1.61	2.460	o	|	|	|	|	4.62
9.417	0.00	1.61	2.449	o	|	|	|	|	4.60
9.500	0.00	1.60	2.438	o	|	|	|	|	4.59
9.583	0.00	1.60	2.427	o	|	|	|	|	4.57
9.667	0.00	1.59	2.416	o	|	|	|	|	4.55
9.750	0.00	1.59	2.405	o	|	|	|	|	4.54
9.833	0.00	1.58	2.394	o	|	|	|	|	4.52
9.917	0.00	1.58	2.383	o	|	|	|	|	4.50
10.000	0.00	1.57	2.372	o	|	|	|	|	4.49
10.083	0.00	1.56	2.361	o	|	|	|	|	4.47
10.167	0.00	1.56	2.351	o	|	|	|	|	4.45
10.250	0.00	1.55	2.340	o	|	|	|	|	4.44
10.333	0.00	1.55	2.329	o	|	|	|	|	4.42
10.417	0.00	1.54	2.318	o	|	|	|	|	4.41
10.500	0.00	1.54	2.308	o	|	|	|	|	4.39
10.583	0.00	1.53	2.297	o	|	|	|	|	4.37
10.667	0.00	1.53	2.287	o	|	|	|	|	4.36
10.750	0.00	1.52	2.276	o	|	|	|	|	4.34
10.833	0.00	1.52	2.266	o	|	|	|	|	4.33
10.917	0.00	1.51	2.255	o	|	|	|	|	4.31
11.000	0.00	1.51	2.245	o	|	|	|	|	4.30
11.083	0.00	1.50	2.234	o	|	|	|	|	4.28
11.167	0.00	1.50	2.224	o	|	|	|	|	4.26
11.250	0.00	1.50	2.214	o	|	|	|	|	4.25
11.333	0.00	1.49	2.204	o	|	|	|	|	4.23
11.417	0.00	1.49	2.193	o	|	|	|	|	4.22
11.500	0.00	1.48	2.183	o	|	|	|	|	4.20
11.583	0.00	1.48	2.173	o	|	|	|	|	4.19
11.667	0.00	1.47	2.163	o	|	|	|	|	4.17
11.750	0.00	1.47	2.153	o	|	|	|	|	4.16
11.833	0.00	1.46	2.143	o	|	|	|	|	4.14
11.917	0.00	1.46	2.133	o	|	|	|	|	4.13
12.000	0.00	1.45	2.122	o	|	|	|	|	4.11
12.083	0.00	1.45	2.113	o	|	|	|	|	4.10
12.167	0.00	1.44	2.103	o	|	|	|	|	4.08
12.250	0.00	1.44	2.093	o	|	|	|	|	4.07
12.333	0.00	1.43	2.083	o	|	|	|	|	4.05
12.417	0.00	1.43	2.073	o	|	|	|	|	4.04
12.500	0.00	1.42	2.063	o	|	|	|	|	4.02
12.583	0.00	1.42	2.053	o	|	|	|	|	4.01
12.667	0.00	1.41	2.044	o	|	|	|	|	3.99
12.750	0.00	1.41	2.034	o	|	|	|	|	3.97
12.833	0.00	1.40	2.024	o	|	|	|	|	3.96
12.917	0.00	1.39	2.015	o	|	|	|	|	3.94
13.000	0.00	1.39	2.005	o	|	|	|	|	3.93
13.083	0.00	1.38	1.995	o	|	|	|	|	3.91
13.167	0.00	1.37	1.986	o	|	|	|	|	3.89
13.250	0.00	1.37	1.977	o	|	|	|	|	3.88
13.333	0.00	1.36	1.967	o	|	|	|	|	3.86
13.417	0.00	1.35	1.958	o	|	|	|	|	3.85
13.500	0.00	1.35	1.949	o	|	|	|	|	3.83
13.583	0.00	1.34	1.939	o	|	|	|	|	3.82
13.667	0.00	1.33	1.930	o	|	|	|	|	3.80
13.750	0.00	1.33	1.921	o	|	|	|	|	3.79
13.833	0.00	1.32	1.912	o	|	|	|	|	3.77
13.917	0.00	1.31	1.903	o	|	|	|	|	3.76
14.000	0.00	1.31	1.894	o	|	|	|	|	3.74
14.083	0.00	1.30	1.885	o	|	|	|	|	3.73
14.167	0.00	1.29	1.876	o	|	|	|	|	3.71
14.250	0.00	1.29	1.867	o	|	|	|	|	3.70
14.333	0.00	1.28	1.858	o	|	|	|	|	3.68
14.417	0.00	1.27	1.849	o	|	|	|	|	3.67
14.500	0.00	1.27	1.841	o	|	|	|	|	3.65
14.583	0.00	1.26	1.832	o	|	|	|	|	3.64
14.667	0.00	1.26	1.823	o	|	|	|	|	3.62
14.750	0.00	1.25	1.815	o	|	|	|	|	3.61
14.833	0.00	1.24	1.806	o	|	|	|	|	3.59
14.917	0.00	1.24	1.797	o	|	|	|	|	3.58
15.000	0.00	1.23	1.789	o	|	|	|	|	3.57
15.083	0.00	1.23	1.780	o	|	|	|	|	3.55
15.167	0.00	1.22	1.772	o	|	|	|	|	3.54
15.250	0.00	1.21	1.764	o	|	|	|	|	3.52
15.333	0.00	1.21	1.755	o	|	|	|	|	3.51
15.417	0.00	1.20	1.747	o	|	|	|	|	3.50
15.500	0.00	1.20	1.739	o	|	|	|	|	3.48
15.583	0.00	1.19	1.731	o	|	|	|	|	3.47
15.667	0.00	1.18	1.722	o	|	|	|	|	3.45
15.750	0.00	1.18	1.714	o	|	|	|	|	3.44
15.833	0.00	1.17	1.706	o	|	|	|	|	3.43

15.917	0.00	1.17	1.698	o	|	|	|	|	3.41
16.000	0.00	1.16	1.690	o	|	|	|	|	3.40
16.083	0.00	1.16	1.682	o	|	|	|	|	3.39
16.167	0.00	1.15	1.674	o	|	|	|	|	3.37
16.250	0.00	1.14	1.666	o	|	|	|	|	3.36
16.333	0.00	1.14	1.658	o	|	|	|	|	3.35
16.417	0.00	1.13	1.651	o	|	|	|	|	3.33
16.500	0.00	1.13	1.643	o	|	|	|	|	3.32
16.583	0.00	1.12	1.635	o	|	|	|	|	3.31
16.667	0.00	1.12	1.627	o	|	|	|	|	3.29
16.750	0.00	1.11	1.620	o	|	|	|	|	3.28
16.833	0.00	1.11	1.612	o	|	|	|	|	3.27
16.917	0.00	1.10	1.604	o	|	|	|	|	3.26
17.000	0.00	1.09	1.597	o	|	|	|	|	3.24
17.083	0.00	1.09	1.589	o	|	|	|	|	3.23
17.167	0.00	1.08	1.582	o	|	|	|	|	3.22
17.250	0.00	1.08	1.574	o	|	|	|	|	3.21
17.333	0.00	1.07	1.567	o	|	|	|	|	3.19
17.417	0.00	1.07	1.560	o	|	|	|	|	3.18
17.500	0.00	1.06	1.552	o	|	|	|	|	3.17
17.583	0.00	1.06	1.545	o	|	|	|	|	3.16
17.667	0.00	1.05	1.538	o	|	|	|	|	3.14
17.750	0.00	1.05	1.530	o	|	|	|	|	3.13
17.833	0.00	1.04	1.523	o	|	|	|	|	3.12
17.917	0.00	1.04	1.516	o	|	|	|	|	3.11
18.000	0.00	1.03	1.509	o	|	|	|	|	3.10
18.083	0.00	1.03	1.502	o	|	|	|	|	3.09
18.167	0.00	1.02	1.495	o	|	|	|	|	3.07
18.250	0.00	1.02	1.488	o	|	|	|	|	3.06
18.333	0.00	1.01	1.481	o	|	|	|	|	3.05
18.417	0.00	1.01	1.474	o	|	|	|	|	3.04
18.500	0.00	1.00	1.467	o	|	|	|	|	3.03
18.583	0.00	1.00	1.460	o	|	|	|	|	3.02
18.667	0.00	0.99	1.453	o	|	|	|	|	3.00
18.750	0.00	0.99	1.446	o	|	|	|	|	2.99
18.833	0.00	0.98	1.440	o	|	|	|	|	2.98
18.917	0.00	0.97	1.433	o	|	|	|	|	2.97
19.000	0.00	0.96	1.426	o	|	|	|	|	2.95
19.083	0.00	0.95	1.420	o	|	|	|	|	2.94
19.167	0.00	0.95	1.413	o	|	|	|	|	2.93
19.250	0.00	0.94	1.407	o	|	|	|	|	2.92
19.333	0.00	0.93	1.400	o	|	|	|	|	2.91
19.417	0.00	0.92	1.394	o	|	|	|	|	2.89
19.500	0.00	0.91	1.388	o	|	|	|	|	2.88
19.583	0.00	0.91	1.381	o	|	|	|	|	2.87
19.667	0.00	0.90	1.375	o	|	|	|	|	2.86
19.750	0.00	0.89	1.369	o	|	|	|	|	2.85
19.833	0.00	0.88	1.363	o	|	|	|	|	2.84
19.917	0.00	0.88	1.357	o	|	|	|	|	2.82
20.000	0.00	0.87	1.351	o	|	|	|	|	2.81
20.083	0.00	0.86	1.345	o	|	|	|	|	2.80
20.167	0.00	0.86	1.339	o	|	|	|	|	2.79
20.250	0.00	0.85	1.333	o	|	|	|	|	2.78
20.333	0.00	0.84	1.327	o	|	|	|	|	2.77
20.417	0.00	0.83	1.321	o	|	|	|	|	2.76
20.500	0.00	0.83	1.316	o	|	|	|	|	2.75
20.583	0.00	0.82	1.310	o	|	|	|	|	2.74
20.667	0.00	0.81	1.304	o	|	|	|	|	2.73
20.750	0.00	0.81	1.299	o	|	|	|	|	2.72
20.833	0.00	0.80	1.293	o	|	|	|	|	2.71
20.917	0.00	0.79	1.288	o	|	|	|	|	2.70
21.000	0.00	0.79	1.282	o	|	|	|	|	2.69
21.083	0.00	0.78	1.277	o	|	|	|	|	2.68
21.167	0.00	0.77	1.271	o	|	|	|	|	2.67
21.250	0.00	0.77	1.266	o	|	|	|	|	2.66
21.333	0.00	0.76	1.261	o	|	|	|	|	2.65
21.417	0.00	0.76	1.256	o	|	|	|	|	2.64
21.500	0.00	0.75	1.250	o	|	|	|	|	2.63
21.583	0.00	0.74	1.245	o	|	|	|	|	2.62
21.667	0.00	0.74	1.240	o	|	|	|	|	2.61
21.750	0.00	0.73	1.235	o	|	|	|	|	2.60
21.833	0.00	0.72	1.230	o	|	|	|	|	2.59
21.917	0.00	0.72	1.225	o	|	|	|	|	2.58
22.000	0.00	0.71	1.220	o	|	|	|	|	2.57
22.083	0.00	0.71	1.215	o	|	|	|	|	2.56
22.167	0.00	0.70	1.211	o	|	|	|	|	2.55
22.250	0.00	0.70	1.206	o	|	|	|	|	2.54
22.333	0.00	0.69	1.201	o	|	|	|	|	2.53
22.417	0.00	0.68	1.196	o	|	|	|	|	2.53
22.500	0.00	0.68	1.192	o	|	|	|	|	2.52
22.583	0.00	0.67	1.187	o	|	|	|	|	2.51
22.667	0.00	0.67	1.182	o	|	|	|	|	2.50
22.750	0.00	0.66	1.178	o	|	|	|	|	2.49
22.833	0.00	0.66	1.173	o	|	|	|	|	2.48
22.917	0.00	0.65	1.169	o	|	|	|	|	2.47
23.000	0.00	0.65	1.164	o	|	|	|	|	2.47

23.083	0.00	0.64	1.160	o					2.46
23.167	0.00	0.63	1.155	o					2.45
23.250	0.00	0.63	1.151	o					2.44
23.333	0.00	0.62	1.147	o					2.43
23.417	0.00	0.62	1.142	o					2.43
23.500	0.00	0.61	1.138	o					2.42
23.583	0.00	0.61	1.134	o					2.41
23.667	0.00	0.60	1.130	o					2.40
23.750	0.00	0.60	1.126	o					2.39
23.833	0.00	0.59	1.122	o					2.39
23.917	0.00	0.59	1.117	o					2.38
24.000	0.00	0.58	1.113	o					2.37
24.083	0.00	0.58	1.109	o					2.36
24.167	0.00	0.57	1.105	o					2.36
24.250	0.00	0.57	1.101	o					2.35
24.333	0.00	0.57	1.098	o					2.34
24.417	0.00	0.56	1.094	o					2.33
24.500	0.00	0.56	1.090	o					2.33
24.583	0.00	0.55	1.086	o					2.32
24.667	0.00	0.55	1.082	o					2.31
24.750	0.00	0.54	1.079	o					2.31
24.833	0.00	0.54	1.075	o					2.30
24.917	0.00	0.53	1.071	o					2.29
25.000	0.00	0.53	1.067	o					2.29
25.083	0.00	0.52	1.064	o					2.28
25.167	0.00	0.52	1.060	o					2.27
25.250	0.00	0.52	1.057	o					2.27
25.333	0.00	0.51	1.053	o					2.26
25.417	0.00	0.51	1.050	o					2.25
25.500	0.00	0.50	1.046	o					2.25
25.583	0.00	0.50	1.043	o					2.24
25.667	0.00	0.49	1.039	o					2.23
25.750	0.00	0.49	1.036	o					2.23
25.833	0.00	0.49	1.032	o					2.22
25.917	0.00	0.48	1.029	o					2.21
26.000	0.00	0.48	1.026	o					2.21
26.083	0.00	0.47	1.023	o					2.20
26.167	0.00	0.47	1.019	o					2.20
26.250	0.00	0.47	1.016	o					2.19
26.333	0.00	0.46	1.013	o					2.18
26.417	0.00	0.46	1.010	o					2.18
26.500	0.00	0.46	1.007	o					2.17
26.583	0.00	0.45	1.003	o					2.17
26.667	0.00	0.45	1.000	o					2.16
26.750	0.00	0.44	0.997	o					2.16
26.833	0.00	0.44	0.994	o					2.15
26.917	0.00	0.44	0.991	o					2.14
27.000	0.00	0.43	0.988	o					2.14
27.083	0.00	0.43	0.985	o					2.13
27.167	0.00	0.43	0.982	o					2.13
27.250	0.00	0.42	0.979	o					2.12
27.333	0.00	0.42	0.976	o					2.12
27.417	0.00	0.42	0.974	o					2.11
27.500	0.00	0.41	0.971	o					2.11
27.583	0.00	0.41	0.968	o					2.10
27.667	0.00	0.41	0.965	o					2.10
27.750	0.00	0.40	0.962	o					2.09
27.833	0.00	0.40	0.960	o					2.08
27.917	0.00	0.40	0.957	o					2.08
28.000	0.00	0.39	0.954	o					2.07
28.083	0.00	0.39	0.951	o					2.07
28.167	0.00	0.39	0.949	o					2.06
28.250	0.00	0.38	0.946	o					2.06
28.333	0.00	0.38	0.943	o					2.05
28.417	0.00	0.38	0.941	o					2.05
28.500	0.00	0.37	0.938	o					2.05
28.583	0.00	0.37	0.936	o					2.04
28.667	0.00	0.37	0.933	o					2.04
28.750	0.00	0.36	0.931	o					2.03
28.833	0.00	0.36	0.928	o					2.03
28.917	0.00	0.36	0.926	o					2.02
29.000	0.00	0.36	0.923	o					2.02
29.083	0.00	0.35	0.921	o					2.01
29.167	0.00	0.35	0.918	o					2.01
29.250	0.00	0.35	0.916	o					2.00
29.333	0.00	0.34	0.914	o					2.00
29.417	0.00	0.34	0.911	o					1.99
29.500	0.00	0.34	0.909	o					1.99
29.583	0.00	0.34	0.907	o					1.98
29.667	0.00	0.34	0.904	o					1.98
29.750	0.00	0.34	0.902	o					1.97
29.833	0.00	0.34	0.899	o					1.97
29.917	0.00	0.34	0.897	o					1.97
30.000	0.00	0.34	0.895	o					1.96
30.083	0.00	0.34	0.892	o					1.96
30.167	0.00	0.34	0.890	o					1.95

30.250	0.00	0.34	0.888	o	|	|	|	|	1.95
30.333	0.00	0.34	0.885	o	|	|	|	|	1.94
30.417	0.00	0.34	0.883	o	|	|	|	|	1.94
30.500	0.00	0.34	0.881	o	|	|	|	|	1.93
30.583	0.00	0.34	0.879	o	|	|	|	|	1.93
30.667	0.00	0.33	0.876	o	|	|	|	|	1.92
30.750	0.00	0.33	0.874	o	|	|	|	|	1.92
30.833	0.00	0.33	0.872	o	|	|	|	|	1.91
30.917	0.00	0.33	0.869	o	|	|	|	|	1.91
31.000	0.00	0.33	0.867	o	|	|	|	|	1.90
31.083	0.00	0.33	0.865	o	|	|	|	|	1.90
31.167	0.00	0.33	0.862	o	|	|	|	|	1.89
31.250	0.00	0.33	0.860	o	|	|	|	|	1.89
31.333	0.00	0.33	0.858	o	|	|	|	|	1.88
31.417	0.00	0.33	0.856	o	|	|	|	|	1.88
31.500	0.00	0.33	0.853	o	|	|	|	|	1.87
31.583	0.00	0.33	0.851	o	|	|	|	|	1.87
31.667	0.00	0.33	0.849	o	|	|	|	|	1.87
31.750	0.00	0.33	0.847	o	|	|	|	|	1.86
31.833	0.00	0.33	0.844	o	|	|	|	|	1.86
31.917	0.00	0.33	0.842	o	|	|	|	|	1.85
32.000	0.00	0.33	0.840	o	|	|	|	|	1.85
32.083	0.00	0.33	0.838	o	|	|	|	|	1.84
32.167	0.00	0.32	0.835	o	|	|	|	|	1.84
32.250	0.00	0.32	0.833	o	|	|	|	|	1.83
32.333	0.00	0.32	0.831	o	|	|	|	|	1.83
32.417	0.00	0.32	0.829	o	|	|	|	|	1.82
32.500	0.00	0.32	0.826	o	|	|	|	|	1.82
32.583	0.00	0.32	0.824	o	|	|	|	|	1.81
32.667	0.00	0.32	0.822	o	|	|	|	|	1.81
32.750	0.00	0.32	0.820	o	|	|	|	|	1.80
32.833	0.00	0.32	0.818	o	|	|	|	|	1.80
32.917	0.00	0.32	0.815	o	|	|	|	|	1.80
33.000	0.00	0.32	0.813	o	|	|	|	|	1.79
33.083	0.00	0.32	0.811	o	|	|	|	|	1.79
33.167	0.00	0.32	0.809	o	|	|	|	|	1.78
33.250	0.00	0.32	0.807	o	|	|	|	|	1.78
33.333	0.00	0.32	0.804	o	|	|	|	|	1.77
33.417	0.00	0.32	0.802	o	|	|	|	|	1.77
33.500	0.00	0.32	0.800	o	|	|	|	|	1.76
33.583	0.00	0.32	0.798	o	|	|	|	|	1.76
33.667	0.00	0.31	0.796	o	|	|	|	|	1.76
33.750	0.00	0.31	0.794	o	|	|	|	|	1.75
33.833	0.00	0.31	0.791	o	|	|	|	|	1.75
33.917	0.00	0.31	0.789	o	|	|	|	|	1.74
34.000	0.00	0.31	0.787	o	|	|	|	|	1.74
34.083	0.00	0.31	0.785	o	|	|	|	|	1.73
34.167	0.00	0.31	0.783	o	|	|	|	|	1.73
34.250	0.00	0.31	0.781	o	|	|	|	|	1.72
34.333	0.00	0.31	0.778	o	|	|	|	|	1.72
34.417	0.00	0.31	0.776	o	|	|	|	|	1.72
34.500	0.00	0.31	0.774	o	|	|	|	|	1.71
34.583	0.00	0.31	0.772	o	|	|	|	|	1.71
34.667	0.00	0.31	0.770	o	|	|	|	|	1.70
34.750	0.00	0.31	0.768	o	|	|	|	|	1.70
34.833	0.00	0.31	0.766	o	|	|	|	|	1.69
34.917	0.00	0.31	0.764	o	|	|	|	|	1.69
35.000	0.00	0.31	0.761	o	|	|	|	|	1.68
35.083	0.00	0.31	0.759	o	|	|	|	|	1.68
35.167	0.00	0.31	0.757	o	|	|	|	|	1.68
35.250	0.00	0.30	0.755	o	|	|	|	|	1.67
35.333	0.00	0.30	0.753	o	|	|	|	|	1.67
35.417	0.00	0.30	0.751	o	|	|	|	|	1.66
35.500	0.00	0.30	0.749	o	|	|	|	|	1.66
35.583	0.00	0.30	0.747	o	|	|	|	|	1.65
35.667	0.00	0.30	0.745	o	|	|	|	|	1.65
35.750	0.00	0.30	0.743	o	|	|	|	|	1.65
35.833	0.00	0.30	0.741	o	|	|	|	|	1.64
35.917	0.00	0.30	0.738	o	|	|	|	|	1.64
36.000	0.00	0.30	0.736	o	|	|	|	|	1.63
36.083	0.00	0.30	0.734	o	|	|	|	|	1.63
36.167	0.00	0.30	0.732	o	|	|	|	|	1.62
36.250	0.00	0.30	0.730	o	|	|	|	|	1.62
36.333	0.00	0.30	0.728	o	|	|	|	|	1.62
36.417	0.00	0.30	0.726	o	|	|	|	|	1.61
36.500	0.00	0.30	0.724	o	|	|	|	|	1.61
36.583	0.00	0.30	0.722	o	|	|	|	|	1.60
36.667	0.00	0.30	0.720	o	|	|	|	|	1.60
36.750	0.00	0.30	0.718	o	|	|	|	|	1.59
36.833	0.00	0.30	0.716	o	|	|	|	|	1.59
36.917	0.00	0.29	0.714	o	|	|	|	|	1.59
37.000	0.00	0.29	0.712	o	|	|	|	|	1.58
37.083	0.00	0.29	0.710	o	|	|	|	|	1.58
37.167	0.00	0.29	0.708	o	|	|	|	|	1.57
37.250	0.00	0.29	0.706	o	|	|	|	|	1.57
37.333	0.00	0.29	0.704	o	|	|	|	|	1.56

37.417	0.00	0.29	0.702	o	|	|	|	|	1.56
37.500	0.00	0.29	0.700	o	|	|	|	|	1.56
37.583	0.00	0.29	0.698	o	|	|	|	|	1.55
37.667	0.00	0.29	0.696	o	|	|	|	|	1.55
37.750	0.00	0.29	0.694	o	|	|	|	|	1.54
37.833	0.00	0.29	0.692	o	|	|	|	|	1.54
37.917	0.00	0.29	0.690	o	|	|	|	|	1.54
38.000	0.00	0.29	0.688	o	|	|	|	|	1.53
38.083	0.00	0.29	0.686	o	|	|	|	|	1.53
38.167	0.00	0.29	0.684	o	|	|	|	|	1.52
38.250	0.00	0.29	0.682	o	|	|	|	|	1.52
38.333	0.00	0.29	0.680	o	|	|	|	|	1.52
38.417	0.00	0.29	0.678	o	|	|	|	|	1.51
38.500	0.00	0.29	0.676	o	|	|	|	|	1.51
38.583	0.00	0.28	0.674	o	|	|	|	|	1.50
38.667	0.00	0.28	0.672	o	|	|	|	|	1.50
38.750	0.00	0.28	0.670	o	|	|	|	|	1.49
38.833	0.00	0.28	0.668	o	|	|	|	|	1.49
38.917	0.00	0.28	0.666	o	|	|	|	|	1.49
39.000	0.00	0.28	0.664	o	|	|	|	|	1.48
39.083	0.00	0.28	0.662	o	|	|	|	|	1.48
39.167	0.00	0.28	0.660	o	|	|	|	|	1.47
39.250	0.00	0.28	0.658	o	|	|	|	|	1.47
39.333	0.00	0.28	0.656	o	|	|	|	|	1.47
39.417	0.00	0.28	0.655	o	|	|	|	|	1.46
39.500	0.00	0.28	0.653	o	|	|	|	|	1.46
39.583	0.00	0.28	0.651	o	|	|	|	|	1.45
39.667	0.00	0.28	0.649	o	|	|	|	|	1.45
39.750	0.00	0.28	0.647	o	|	|	|	|	1.45
39.833	0.00	0.28	0.645	o	|	|	|	|	1.44
39.917	0.00	0.28	0.643	o	|	|	|	|	1.44
40.000	0.00	0.28	0.641	o	|	|	|	|	1.44
40.083	0.00	0.28	0.639	o	|	|	|	|	1.43
40.167	0.00	0.28	0.637	o	|	|	|	|	1.43
40.250	0.00	0.28	0.635	o	|	|	|	|	1.42
40.333	0.00	0.27	0.634	o	|	|	|	|	1.42
40.417	0.00	0.27	0.632	o	|	|	|	|	1.42
40.500	0.00	0.27	0.630	o	|	|	|	|	1.41
40.583	0.00	0.27	0.628	o	|	|	|	|	1.41
40.667	0.00	0.27	0.626	o	|	|	|	|	1.40
40.750	0.00	0.27	0.624	o	|	|	|	|	1.40
40.833	0.00	0.27	0.622	o	|	|	|	|	1.40
40.917	0.00	0.27	0.620	o	|	|	|	|	1.39
41.000	0.00	0.27	0.618	o	|	|	|	|	1.39
41.083	0.00	0.27	0.617	o	|	|	|	|	1.38
41.167	0.00	0.27	0.615	o	|	|	|	|	1.38
41.250	0.00	0.27	0.613	o	|	|	|	|	1.38
41.333	0.00	0.27	0.611	o	|	|	|	|	1.37
41.417	0.00	0.27	0.609	o	|	|	|	|	1.37
41.500	0.00	0.27	0.607	o	|	|	|	|	1.37
41.583	0.00	0.27	0.605	o	|	|	|	|	1.36
41.667	0.00	0.27	0.604	o	|	|	|	|	1.36
41.750	0.00	0.27	0.602	o	|	|	|	|	1.35
41.833	0.00	0.27	0.600	o	|	|	|	|	1.35
41.917	0.00	0.27	0.598	o	|	|	|	|	1.35
42.000	0.00	0.27	0.596	o	|	|	|	|	1.34
42.083	0.00	0.27	0.594	o	|	|	|	|	1.34
42.167	0.00	0.26	0.593	o	|	|	|	|	1.33
42.250	0.00	0.26	0.591	o	|	|	|	|	1.33
42.333	0.00	0.26	0.589	o	|	|	|	|	1.33
42.417	0.00	0.26	0.587	o	|	|	|	|	1.32
42.500	0.00	0.26	0.585	o	|	|	|	|	1.32
42.583	0.00	0.26	0.584	o	|	|	|	|	1.32
42.667	0.00	0.26	0.582	o	|	|	|	|	1.31
42.750	0.00	0.26	0.580	o	|	|	|	|	1.31
42.833	0.00	0.26	0.578	o	|	|	|	|	1.30
42.917	0.00	0.26	0.576	o	|	|	|	|	1.30
43.000	0.00	0.26	0.575	o	|	|	|	|	1.30
43.083	0.00	0.26	0.573	o	|	|	|	|	1.29
43.167	0.00	0.26	0.571	o	|	|	|	|	1.29
43.250	0.00	0.26	0.569	o	|	|	|	|	1.29
43.333	0.00	0.26	0.567	o	|	|	|	|	1.28
43.417	0.00	0.26	0.566	o	|	|	|	|	1.28
43.500	0.00	0.26	0.564	o	|	|	|	|	1.28
43.583	0.00	0.26	0.562	o	|	|	|	|	1.27
43.667	0.00	0.26	0.560	o	|	|	|	|	1.27
43.750	0.00	0.26	0.559	o	|	|	|	|	1.26
43.833	0.00	0.26	0.557	o	|	|	|	|	1.26
43.917	0.00	0.26	0.555	o	|	|	|	|	1.26
44.000	0.00	0.26	0.553	o	|	|	|	|	1.25
44.083	0.00	0.25	0.551	o	|	|	|	|	1.25
44.167	0.00	0.25	0.550	o	|	|	|	|	1.25
44.250	0.00	0.25	0.548	o	|	|	|	|	1.24
44.333	0.00	0.25	0.546	o	|	|	|	|	1.24
44.417	0.00	0.25	0.544	o	|	|	|	|	1.23
44.500	0.00	0.25	0.543	o	|	|	|	|	1.23

44.583	0.00	0.25	0.541	o	|	|	|	|	1.23
44.667	0.00	0.25	0.539	o	|	|	|	|	1.22
44.750	0.00	0.25	0.538	o	|	|	|	|	1.22
44.833	0.00	0.25	0.536	o	|	|	|	|	1.22
44.917	0.00	0.25	0.534	o	|	|	|	|	1.21
45.000	0.00	0.25	0.532	o	|	|	|	|	1.21
45.083	0.00	0.25	0.531	o	|	|	|	|	1.21
45.167	0.00	0.25	0.529	o	|	|	|	|	1.20
45.250	0.00	0.25	0.527	o	|	|	|	|	1.20
45.333	0.00	0.25	0.526	o	|	|	|	|	1.20
45.417	0.00	0.25	0.524	o	|	|	|	|	1.19
45.500	0.00	0.25	0.522	o	|	|	|	|	1.19
45.583	0.00	0.25	0.520	o	|	|	|	|	1.19
45.667	0.00	0.25	0.519	o	|	|	|	|	1.18
45.750	0.00	0.25	0.517	o	|	|	|	|	1.18
45.833	0.00	0.25	0.515	o	|	|	|	|	1.17
45.917	0.00	0.25	0.514	o	|	|	|	|	1.17
46.000	0.00	0.24	0.512	o	|	|	|	|	1.17
46.083	0.00	0.24	0.510	o	|	|	|	|	1.16
46.167	0.00	0.24	0.509	o	|	|	|	|	1.16
46.250	0.00	0.24	0.507	o	|	|	|	|	1.16
46.333	0.00	0.24	0.505	o	|	|	|	|	1.15
46.417	0.00	0.24	0.504	o	|	|	|	|	1.15
46.500	0.00	0.24	0.502	o	|	|	|	|	1.15
46.583	0.00	0.24	0.500	o	|	|	|	|	1.14
46.667	0.00	0.24	0.499	o	|	|	|	|	1.14
46.750	0.00	0.24	0.497	o	|	|	|	|	1.14
46.833	0.00	0.24	0.495	o	|	|	|	|	1.13
46.917	0.00	0.24	0.494	o	|	|	|	|	1.13
47.000	0.00	0.24	0.492	o	|	|	|	|	1.13
47.083	0.00	0.24	0.490	o	|	|	|	|	1.12
47.167	0.00	0.24	0.489	o	|	|	|	|	1.12
47.250	0.00	0.24	0.487	o	|	|	|	|	1.12
47.333	0.00	0.24	0.485	o	|	|	|	|	1.11
47.417	0.00	0.24	0.484	o	|	|	|	|	1.11
47.500	0.00	0.24	0.482	o	|	|	|	|	1.11
47.583	0.00	0.24	0.480	o	|	|	|	|	1.10
47.667	0.00	0.24	0.479	o	|	|	|	|	1.10
47.750	0.00	0.24	0.477	o	|	|	|	|	1.10
47.833	0.00	0.24	0.475	o	|	|	|	|	1.09
47.917	0.00	0.24	0.474	o	|	|	|	|	1.09
48.000	0.00	0.24	0.472	o	|	|	|	|	1.09
48.083	0.00	0.23	0.471	o	|	|	|	|	1.08
48.167	0.00	0.23	0.469	o	|	|	|	|	1.08
48.250	0.00	0.23	0.467	o	|	|	|	|	1.08
48.333	0.00	0.23	0.466	o	|	|	|	|	1.07
48.417	0.00	0.23	0.464	o	|	|	|	|	1.07
48.500	0.00	0.23	0.463	o	|	|	|	|	1.07
48.583	0.00	0.23	0.461	o	|	|	|	|	1.06
48.667	0.00	0.23	0.459	o	|	|	|	|	1.06
48.750	0.00	0.23	0.458	o	|	|	|	|	1.06
48.833	0.00	0.23	0.456	o	|	|	|	|	1.05
48.917	0.00	0.23	0.455	o	|	|	|	|	1.05
49.000	0.00	0.23	0.453	o	|	|	|	|	1.05
49.083	0.00	0.23	0.451	o	|	|	|	|	1.04
49.167	0.00	0.23	0.450	o	|	|	|	|	1.04
49.250	0.00	0.23	0.448	o	|	|	|	|	1.04
49.333	0.00	0.23	0.447	o	|	|	|	|	1.03
49.417	0.00	0.23	0.445	o	|	|	|	|	1.03
49.500	0.00	0.23	0.444	o	|	|	|	|	1.03
49.583	0.00	0.23	0.442	o	|	|	|	|	1.02
49.667	0.00	0.23	0.440	o	|	|	|	|	1.02
49.750	0.00	0.23	0.439	o	|	|	|	|	1.02
49.833	0.00	0.23	0.437	o	|	|	|	|	1.01
49.917	0.00	0.23	0.436	o	|	|	|	|	1.01
50.000	0.00	0.23	0.434	o	|	|	|	|	1.01
50.083	0.00	0.23	0.433	o	|	|	|	|	1.00
50.167	0.00	0.23	0.431	o	|	|	|	|	1.00
50.250	0.00	0.22	0.430	o	|	|	|	|	1.00
50.333	0.00	0.22	0.428	o	|	|	|	|	0.99
50.417	0.00	0.22	0.426	o	|	|	|	|	0.99
50.500	0.00	0.22	0.425	o	|	|	|	|	0.99
50.583	0.00	0.22	0.423	o	|	|	|	|	0.98
50.667	0.00	0.22	0.422	o	|	|	|	|	0.98
50.750	0.00	0.22	0.420	o	|	|	|	|	0.98
50.833	0.00	0.22	0.419	o	|	|	|	|	0.97
50.917	0.00	0.22	0.417	o	|	|	|	|	0.97
51.000	0.00	0.22	0.416	o	|	|	|	|	0.96
51.083	0.00	0.22	0.414	o	|	|	|	|	0.96
51.167	0.00	0.22	0.413	o	|	|	|	|	0.96
51.250	0.00	0.21	0.411	o	|	|	|	|	0.95
51.333	0.00	0.21	0.410	o	|	|	|	|	0.95
51.417	0.00	0.21	0.408	o	|	|	|	|	0.95
51.500	0.00	0.21	0.407	o	|	|	|	|	0.94
51.583	0.00	0.21	0.405	o	|	|	|	|	0.94
51.667	0.00	0.21	0.404	o	|	|	|	|	0.94

51.750	0.00	0.21	0.403	o	|	|	|	0.93
51.833	0.00	0.21	0.401	o	|	|	|	0.93
51.917	0.00	0.21	0.400	o	|	|	|	0.93
52.000	0.00	0.21	0.398	o	|	|	|	0.92
52.083	0.00	0.21	0.397	o	|	|	|	0.92
52.167	0.00	0.21	0.395	o	|	|	|	0.92
52.250	0.00	0.21	0.394	o	|	|	|	0.91
52.333	0.00	0.20	0.393	o	|	|	|	0.91
52.417	0.00	0.20	0.391	o	|	|	|	0.91
52.500	0.00	0.20	0.390	o	|	|	|	0.90
52.583	0.00	0.20	0.388	o	|	|	|	0.90
52.667	0.00	0.20	0.387	o	|	|	|	0.90
52.750	0.00	0.20	0.386	o	|	|	|	0.89
52.833	0.00	0.20	0.384	o	|	|	|	0.89
52.917	0.00	0.20	0.383	o	|	|	|	0.89
53.000	0.00	0.20	0.381	o	|	|	|	0.89
53.083	0.00	0.20	0.380	o	|	|	|	0.88
53.167	0.00	0.20	0.379	o	|	|	|	0.88
53.250	0.00	0.20	0.377	o	|	|	|	0.88
53.333	0.00	0.20	0.376	o	|	|	|	0.87
53.417	0.00	0.20	0.375	o	|	|	|	0.87
53.500	0.00	0.19	0.373	o	|	|	|	0.87
53.583	0.00	0.19	0.372	o	|	|	|	0.86
53.667	0.00	0.19	0.371	o	|	|	|	0.86
53.750	0.00	0.19	0.369	o	|	|	|	0.86
53.833	0.00	0.19	0.368	o	|	|	|	0.85
53.917	0.00	0.19	0.367	o	|	|	|	0.85
54.000	0.00	0.19	0.365	o	|	|	|	0.85
54.083	0.00	0.19	0.364	o	|	|	|	0.84
54.167	0.00	0.19	0.363	o	|	|	|	0.84
54.250	0.00	0.19	0.361	o	|	|	|	0.84
54.333	0.00	0.19	0.360	o	|	|	|	0.84
54.417	0.00	0.19	0.359	o	|	|	|	0.83
54.500	0.00	0.19	0.358	o	|	|	|	0.83
54.583	0.00	0.19	0.356	o	|	|	|	0.83
54.667	0.00	0.19	0.355	o	|	|	|	0.82
54.750	0.00	0.18	0.354	o	|	|	|	0.82
54.833	0.00	0.18	0.352	o	|	|	|	0.82
54.917	0.00	0.18	0.351	o	|	|	|	0.81
55.000	0.00	0.18	0.350	o	|	|	|	0.81
55.083	0.00	0.18	0.349	o	|	|	|	0.81
55.167	0.00	0.18	0.347	o	|	|	|	0.81
55.250	0.00	0.18	0.346	o	|	|	|	0.80
55.333	0.00	0.18	0.345	o	|	|	|	0.80
55.417	0.00	0.18	0.344	o	|	|	|	0.80
55.500	0.00	0.18	0.342	o	|	|	|	0.79
55.583	0.00	0.18	0.341	o	|	|	|	0.79
55.667	0.00	0.18	0.340	o	|	|	|	0.79
55.750	0.00	0.18	0.339	o	|	|	|	0.79
55.833	0.00	0.18	0.338	o	|	|	|	0.78
55.917	0.00	0.18	0.336	o	|	|	|	0.78
56.000	0.00	0.17	0.335	o	|	|	|	0.78
56.083	0.00	0.17	0.334	o	|	|	|	0.77
56.167	0.00	0.17	0.333	o	|	|	|	0.77
56.250	0.00	0.17	0.332	o	|	|	|	0.77
56.333	0.00	0.17	0.330	o	|	|	|	0.77
56.417	0.00	0.17	0.329	o	|	|	|	0.76
56.500	0.00	0.17	0.328	o	|	|	|	0.76
56.583	0.00	0.17	0.327	o	|	|	|	0.76
56.667	0.00	0.17	0.326	o	|	|	|	0.76
56.750	0.00	0.17	0.324	o	|	|	|	0.75
56.833	0.00	0.17	0.323	o	|	|	|	0.75
56.917	0.00	0.17	0.322	o	|	|	|	0.75
57.000	0.00	0.17	0.321	o	|	|	|	0.74
57.083	0.00	0.17	0.320	o	|	|	|	0.74
57.167	0.00	0.17	0.319	o	|	|	|	0.74
57.250	0.00	0.17	0.318	o	|	|	|	0.74
57.333	0.00	0.17	0.316	o	|	|	|	0.73
57.417	0.00	0.16	0.315	o	|	|	|	0.73
57.500	0.00	0.16	0.314	o	|	|	|	0.73
57.583	0.00	0.16	0.313	o	|	|	|	0.73
57.667	0.00	0.16	0.312	o	|	|	|	0.72
57.750	0.00	0.16	0.311	o	|	|	|	0.72
57.833	0.00	0.16	0.310	o	|	|	|	0.72
57.917	0.00	0.16	0.309	o	|	|	|	0.72
58.000	0.00	0.16	0.307	o	|	|	|	0.71
58.083	0.00	0.16	0.306	o	|	|	|	0.71
58.167	0.00	0.16	0.305	o	|	|	|	0.71
58.250	0.00	0.16	0.304	o	|	|	|	0.71
58.333	0.00	0.16	0.303	o	|	|	|	0.70
58.417	0.00	0.16	0.302	o	|	|	|	0.70
58.500	0.00	0.16	0.301	o	|	|	|	0.70
58.583	0.00	0.16	0.300	o	|	|	|	0.70
58.667	0.00	0.16	0.299	o	|	|	|	0.69
58.750	0.00	0.16	0.298	o	|	|	|	0.69
58.833	0.00	0.15	0.297	o	|	|	|	0.69

58.917	0.00	0.15	0.296	o	|	|	|	0.69
59.000	0.00	0.15	0.294	o	|	|	|	0.68
59.083	0.00	0.15	0.293	o	|	|	|	0.68
59.167	0.00	0.15	0.292	o	|	|	|	0.68
59.250	0.00	0.15	0.291	o	|	|	|	0.68
59.333	0.00	0.15	0.290	o	|	|	|	0.67
59.417	0.00	0.15	0.289	o	|	|	|	0.67
59.500	0.00	0.15	0.288	o	|	|	|	0.67
59.583	0.00	0.15	0.287	o	|	|	|	0.67
59.667	0.00	0.15	0.286	o	|	|	|	0.66
59.750	0.00	0.15	0.285	o	|	|	|	0.66
59.833	0.00	0.15	0.284	o	|	|	|	0.66
59.917	0.00	0.15	0.283	o	|	|	|	0.66
60.000	0.00	0.15	0.282	o	|	|	|	0.65
60.083	0.00	0.15	0.281	o	|	|	|	0.65
60.167	0.00	0.15	0.280	o	|	|	|	0.65
60.250	0.00	0.15	0.279	o	|	|	|	0.65
60.333	0.00	0.15	0.278	o	|	|	|	0.65
60.417	0.00	0.14	0.277	o	|	|	|	0.64
60.500	0.00	0.14	0.276	o	|	|	|	0.64
60.583	0.00	0.14	0.275	o	|	|	|	0.64
60.667	0.00	0.14	0.274	o	|	|	|	0.64
60.750	0.00	0.14	0.273	o	|	|	|	0.63
60.833	0.00	0.14	0.272	o	|	|	|	0.63
60.917	0.00	0.14	0.271	o	|	|	|	0.63
61.000	0.00	0.14	0.270	o	|	|	|	0.63
61.083	0.00	0.14	0.269	o	|	|	|	0.62
61.167	0.00	0.14	0.268	o	|	|	|	0.62
61.250	0.00	0.14	0.267	o	|	|	|	0.62
61.333	0.00	0.14	0.266	o	|	|	|	0.62
61.417	0.00	0.14	0.265	o	|	|	|	0.62
61.500	0.00	0.14	0.264	o	|	|	|	0.61
61.583	0.00	0.14	0.263	o	|	|	|	0.61
61.667	0.00	0.14	0.262	o	|	|	|	0.61
61.750	0.00	0.14	0.262	o	|	|	|	0.61
61.833	0.00	0.14	0.261	o	|	|	|	0.60
61.917	0.00	0.14	0.260	o	|	|	|	0.60
62.000	0.00	0.14	0.259	o	|	|	|	0.60
62.083	0.00	0.13	0.258	o	|	|	|	0.60
62.167	0.00	0.13	0.257	o	|	|	|	0.60
62.250	0.00	0.13	0.256	o	|	|	|	0.59
62.333	0.00	0.13	0.255	o	|	|	|	0.59
62.417	0.00	0.13	0.254	o	|	|	|	0.59
62.500	0.00	0.13	0.253	o	|	|	|	0.59
62.583	0.00	0.13	0.252	o	|	|	|	0.59
62.667	0.00	0.13	0.251	o	|	|	|	0.58
62.750	0.00	0.13	0.250	o	|	|	|	0.58
62.833	0.00	0.13	0.250	o	|	|	|	0.58
62.917	0.00	0.13	0.249	o	|	|	|	0.58
63.000	0.00	0.13	0.248	o	|	|	|	0.57
63.083	0.00	0.13	0.247	o	|	|	|	0.57
63.167	0.00	0.13	0.246	o	|	|	|	0.57
63.250	0.00	0.13	0.245	o	|	|	|	0.57
63.333	0.00	0.13	0.244	o	|	|	|	0.57
63.417	0.00	0.13	0.243	o	|	|	|	0.56
63.500	0.00	0.13	0.242	o	|	|	|	0.56
63.583	0.00	0.13	0.242	o	|	|	|	0.56
63.667	0.00	0.13	0.241	o	|	|	|	0.56
63.750	0.00	0.13	0.240	o	|	|	|	0.56
63.833	0.00	0.12	0.239	o	|	|	|	0.55
63.917	0.00	0.12	0.238	o	|	|	|	0.55
64.000	0.00	0.12	0.237	o	|	|	|	0.55
64.083	0.00	0.12	0.236	o	|	|	|	0.55
64.167	0.00	0.12	0.236	o	|	|	|	0.55
64.250	0.00	0.12	0.235	o	|	|	|	0.54
64.333	0.00	0.12	0.234	o	|	|	|	0.54
64.417	0.00	0.12	0.233	o	|	|	|	0.54
64.500	0.00	0.12	0.232	o	|	|	|	0.54
64.583	0.00	0.12	0.231	o	|	|	|	0.54
64.667	0.00	0.12	0.231	o	|	|	|	0.54
64.750	0.00	0.12	0.230	o	|	|	|	0.53
64.833	0.00	0.12	0.229	o	|	|	|	0.53
64.917	0.00	0.12	0.228	o	|	|	|	0.53
65.000	0.00	0.12	0.227	o	|	|	|	0.53
65.083	0.00	0.12	0.226	o	|	|	|	0.53
65.167	0.00	0.12	0.226	o	|	|	|	0.52
65.250	0.00	0.12	0.225	o	|	|	|	0.52
65.333	0.00	0.12	0.224	o	|	|	|	0.52
65.417	0.00	0.12	0.223	o	|	|	|	0.52
65.500	0.00	0.12	0.222	o	|	|	|	0.52
65.583	0.00	0.12	0.222	o	|	|	|	0.51
65.667	0.00	0.12	0.221	o	|	|	|	0.51
65.750	0.00	0.11	0.220	o	|	|	|	0.51
65.833	0.00	0.11	0.219	o	|	|	|	0.51
65.917	0.00	0.11	0.218	o	|	|	|	0.51
66.000	0.00	0.11	0.218	o	|	|	|	0.51

66.083	0.00	0.11	0.217	o	|	|	|	|	0.50
66.167	0.00	0.11	0.216	o	|	|	|	|	0.50
66.250	0.00	0.11	0.215	o	|	|	|	|	0.50
66.333	0.00	0.11	0.215	o	|	|	|	|	0.50
66.417	0.00	0.11	0.214	o	|	|	|	|	0.50
66.500	0.00	0.11	0.213	o	|	|	|	|	0.49
66.583	0.00	0.11	0.212	o	|	|	|	|	0.49
66.667	0.00	0.11	0.212	o	|	|	|	|	0.49
66.750	0.00	0.11	0.211	o	|	|	|	|	0.49
66.833	0.00	0.11	0.210	o	|	|	|	|	0.49
66.917	0.00	0.11	0.209	o	|	|	|	|	0.49
67.000	0.00	0.11	0.209	o	|	|	|	|	0.48
67.083	0.00	0.11	0.208	o	|	|	|	|	0.48
67.167	0.00	0.11	0.207	o	|	|	|	|	0.48
67.250	0.00	0.11	0.206	o	|	|	|	|	0.48
67.333	0.00	0.11	0.206	o	|	|	|	|	0.48
67.417	0.00	0.11	0.205	o	|	|	|	|	0.48
67.500	0.00	0.11	0.204	o	|	|	|	|	0.47
67.583	0.00	0.11	0.203	o	|	|	|	|	0.47
67.667	0.00	0.11	0.203	o	|	|	|	|	0.47
67.750	0.00	0.11	0.202	o	|	|	|	|	0.47
67.833	0.00	0.11	0.201	o	|	|	|	|	0.47
67.917	0.00	0.10	0.200	o	|	|	|	|	0.47
68.000	0.00	0.10	0.200	o	|	|	|	|	0.46
68.083	0.00	0.10	0.199	o	|	|	|	|	0.46
68.167	0.00	0.10	0.198	o	|	|	|	|	0.46
68.250	0.00	0.10	0.198	o	|	|	|	|	0.46
68.333	0.00	0.10	0.197	o	|	|	|	|	0.46
68.417	0.00	0.10	0.196	o	|	|	|	|	0.46
68.500	0.00	0.10	0.195	o	|	|	|	|	0.45
68.583	0.00	0.10	0.195	o	|	|	|	|	0.45
68.667	0.00	0.10	0.194	o	|	|	|	|	0.45
68.750	0.00	0.10	0.193	o	|	|	|	|	0.45
68.833	0.00	0.10	0.193	o	|	|	|	|	0.45
68.917	0.00	0.10	0.192	o	|	|	|	|	0.45
69.000	0.00	0.10	0.191	o	|	|	|	|	0.44

Remaining water in basin = 0.19 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 828
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 76.226 (CFS)
Total volume = 8.467 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: pro210024100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 293
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 26.289 (CFS)
Total volume = 12.288 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 293
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.431	0.225	0.430	0.432
2.000	0.914	0.344	0.913	0.915
3.000	1.451	0.991	1.448	1.454
4.000	2.049	1.417	2.044	2.054
5.000	2.712	1.731	2.706	2.718
5.250	2.888	1.801	2.882	2.894
5.500	3.069	17.046	3.010	3.128
6.000	3.443	225.078	2.668	4.218

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	6.6	13.14	19.72	26.29	Depth (Ft.)
0.083	0.31	0.00	0.001	O	|	|	|	|	0.00
0.167	0.81	0.00	0.005	O	|	|	|	|	0.01
0.250	0.93	0.01	0.011	OI	|	|	|	|	0.03
0.333	1.14	0.01	0.018	OI	|	|	|	|	0.04
0.417	1.43	0.01	0.027	OI	|	|	|	|	0.06
0.500	1.51	0.02	0.037	OI	|	|	|	|	0.09
0.583	1.54	0.02	0.047	OI	|	|	|	|	0.11
0.667	1.56	0.03	0.058	OI	|	|	|	|	0.13
0.750	1.57	0.04	0.068	OI	|	|	|	|	0.16
0.833	1.72	0.04	0.079	O I	|	|	|	|	0.18
0.917	1.97	0.05	0.092	O I	|	|	|	|	0.21
1.000	2.03	0.05	0.105	O I	|	|	|	|	0.24
1.083	1.91	0.06	0.118	O I	|	|	|	|	0.27
1.167	1.67	0.07	0.130	O I	|	|	|	|	0.30
1.250	1.62	0.07	0.141	OI	|	|	|	|	0.33
1.333	1.59	0.08	0.151	OI	|	|	|	|	0.35
1.417	1.58	0.08	0.162	OI	|	|	|	|	0.38
1.500	1.57	0.09	0.172	OI	|	|	|	|	0.40

1.583	1.57	0.10	0.182	OI	|	|	|	|	0.42
1.667	1.57	0.10	0.192	OI	|	|	|	|	0.45
1.750	1.57	0.11	0.202	OI	|	|	|	|	0.47
1.833	1.72	0.11	0.213	O I	|	|	|	|	0.49
1.917	1.97	0.12	0.225	O I	|	|	|	|	0.52
2.000	2.03	0.12	0.238	O I	|	|	|	|	0.55
2.083	2.06	0.13	0.251	O I	|	|	|	|	0.58
2.167	2.08	0.14	0.264	O I	|	|	|	|	0.61
2.250	2.09	0.14	0.278	O I	|	|	|	|	0.64
2.333	2.09	0.15	0.291	O I	|	|	|	|	0.68
2.417	2.09	0.16	0.304	O I	|	|	|	|	0.71
2.500	2.09	0.17	0.318	O I	|	|	|	|	0.74
2.583	2.24	0.17	0.331	O I	|	|	|	|	0.77
2.667	2.49	0.18	0.347	O I	|	|	|	|	0.80
2.750	2.56	0.19	0.363	O I	|	|	|	|	0.84
2.833	2.58	0.20	0.379	O I	|	|	|	|	0.88
2.917	2.60	0.21	0.395	O I	|	|	|	|	0.92
3.000	2.61	0.22	0.412	O I	|	|	|	|	0.96
3.083	2.61	0.22	0.428	O I	|	|	|	|	0.99
3.167	2.61	0.23	0.445	O I	|	|	|	|	1.03
3.250	2.61	0.23	0.461	O I	|	|	|	|	1.06
3.333	2.61	0.24	0.478	O I	|	|	|	|	1.10
3.417	2.61	0.24	0.494	O I	|	|	|	|	1.13
3.500	2.61	0.24	0.510	O I	|	|	|	|	1.16
3.583	2.61	0.25	0.527	O I	|	|	|	|	1.20
3.667	2.61	0.25	0.543	O I	|	|	|	|	1.23
3.750	2.61	0.26	0.559	O I	|	|	|	|	1.27
3.833	2.76	0.26	0.576	O I	|	|	|	|	1.30
3.917	3.01	0.27	0.594	O I	|	|	|	|	1.34
4.000	3.08	0.27	0.613	O I	|	|	|	|	1.38
4.083	3.11	0.27	0.632	O I	|	|	|	|	1.42
4.167	3.12	0.28	0.652	O I	|	|	|	|	1.46
4.250	3.13	0.28	0.672	O I	|	|	|	|	1.50
4.333	3.29	0.29	0.692	O I	|	|	|	|	1.54
4.417	3.54	0.29	0.713	O I	|	|	|	|	1.58
4.500	3.60	0.30	0.736	O I	|	|	|	|	1.63
4.583	3.63	0.31	0.759	O I	|	|	|	|	1.68
4.667	3.64	0.31	0.781	O I	|	|	|	|	1.73
4.750	3.66	0.32	0.804	O I	|	|	|	|	1.77
4.833	3.81	0.32	0.828	O I	|	|	|	|	1.82
4.917	4.06	0.33	0.853	O I	|	|	|	|	1.87
5.000	4.12	0.34	0.879	O I	|	|	|	|	1.93
5.083	3.85	0.34	0.904	O I	|	|	|	|	1.98
5.167	3.36	0.36	0.926	O I	|	|	|	|	2.02
5.250	3.24	0.38	0.946	O I	|	|	|	|	2.06
5.333	3.34	0.41	0.966	O I	|	|	|	|	2.10
5.417	3.56	0.43	0.987	O I	|	|	|	|	2.14
5.500	3.60	0.46	1.009	O I	|	|	|	|	2.18
5.583	3.78	0.48	1.031	O I	|	|	|	|	2.22
5.667	4.05	0.51	1.055	O I	|	|	|	|	2.26
5.750	4.12	0.54	1.079	O I	|	|	|	|	2.31
5.833	4.15	0.57	1.104	O I	|	|	|	|	2.35
5.917	4.17	0.60	1.128	O I	|	|	|	|	2.40
6.000	4.18	0.63	1.153	O I	|	|	|	|	2.44
6.083	4.33	0.66	1.178	O I	|	|	|	|	2.49
6.167	4.58	0.69	1.204	O I	|	|	|	|	2.54
6.250	4.65	0.73	1.231	O I	|	|	|	|	2.59
6.333	4.67	0.76	1.257	O I	|	|	|	|	2.64
6.417	4.69	0.79	1.284	O I	|	|	|	|	2.69
6.500	4.70	0.82	1.311	|O I	|	|	|	|	2.74
6.583	4.85	0.86	1.338	|O I	|	|	|	|	2.79
6.667	5.10	0.89	1.367	|O I	|	|	|	|	2.84
6.750	5.17	0.92	1.396	|O I	|	|	|	|	2.90
6.833	5.20	0.96	1.425	|O I	|	|	|	|	2.95
6.917	5.21	0.99	1.454	|O I	|	|	|	|	3.01
7.000	5.22	1.01	1.483	|O I	|	|	|	|	3.05
7.083	5.22	1.03	1.512	|O I	|	|	|	|	3.10
7.167	5.22	1.05	1.541	|O I	|	|	|	|	3.15
7.250	5.22	1.08	1.569	|O I	|	|	|	|	3.20
7.333	5.38	1.10	1.598	|O I	|	|	|	|	3.25
7.417	5.63	1.12	1.629	|O I	|	|	|	|	3.30
7.500	5.69	1.14	1.660	|O I	|	|	|	|	3.35
7.583	5.87	1.16	1.692	|O I|	|	|	|	|	3.40
7.667	6.14	1.19	1.725	|O I|	|	|	|	|	3.46
7.750	6.21	1.21	1.759	|O I|	|	|	|	|	3.52
7.833	6.39	1.24	1.794	|O I|	|	|	|	|	3.57
7.917	6.66	1.26	1.831	|O I	|	|	|	|	3.63
8.000	6.73	1.29	1.868	|O I	|	|	|	|	3.70
8.083	7.07	1.32	1.906	|O I	|	|	|	|	3.76
8.167	7.59	1.34	1.948	|O |I	|	|	|	|	3.83
8.250	7.72	1.38	1.991	|O |I	|	|	|	|	3.90
8.333	7.78	1.41	2.035	|O |I	|	|	|	|	3.98
8.417	7.81	1.43	2.079	|O |I	|	|	|	|	4.05
8.500	7.83	1.45	2.123	|O |I	|	|	|	|	4.11
8.583	7.99	1.47	2.167	|O |I	|	|	|	|	4.18
8.667	8.24	1.49	2.213	|O | I	|	|	|	|	4.25

8.750	8.30	1.52	2.259	O	I			4.32
8.833	8.48	1.54	2.307	O	I			4.39
8.917	8.75	1.56	2.355	O	I			4.46
9.000	8.82	1.59	2.405	O	I			4.54
9.083	9.16	1.61	2.456	O	I			4.61
9.167	9.67	1.64	2.510	O	I			4.69
9.250	9.81	1.66	2.565	O	I			4.78
9.333	10.02	1.69	2.622	O	I			4.86
9.417	10.30	1.72	2.680	O	I			4.95
9.500	10.39	1.74	2.740	O	I			5.04
9.583	10.57	1.77	2.800	O	I			5.12
9.667	10.84	1.79	2.861	O	I			5.21
9.750	10.91	4.14	2.916	O	I			5.29
9.833	11.11	7.23	2.952	O	I			5.34
9.917	11.43	9.05	2.974	O I				5.37
10.000	11.56	10.15	2.987	O I				5.39
10.083	10.50	10.54	2.992	O				5.39
10.167	8.68	10.12	2.987	I O				5.39
10.250	8.23	9.37	2.978	IO				5.37
10.333	8.03	8.81	2.971	IO				5.36
10.417	7.92	8.44	2.967	IO				5.36
10.500	7.83	8.18	2.964	O				5.35
10.583	8.60	8.20	2.964	OI				5.35
10.667	9.85	8.66	2.969	OI				5.36
10.750	10.17	9.27	2.977	OI				5.37
10.833	10.31	9.71	2.982	OI				5.38
10.917	10.39	10.00	2.985	O				5.38
11.000	10.45	10.18	2.988	O				5.39
11.083	10.29	10.27	2.989	O				5.39
11.167	10.04	10.22	2.988	O				5.39
11.250	9.98	10.13	2.987	O				5.39
11.333	9.95	10.05	2.986	O				5.39
11.417	9.93	10.00	2.985	O				5.38
11.500	9.92	9.97	2.985	O				5.38
11.583	9.62	9.88	2.984	IO				5.38
11.667	9.12	9.65	2.981	O				5.38
11.750	8.99	9.38	2.978	IO				5.37
11.833	9.08	9.23	2.976	O				5.37
11.917	9.31	9.21	2.976	O				5.37
12.000	9.35	9.26	2.977	O				5.37
12.083	11.34	9.75	2.982	O I				5.38
12.167	14.59	11.20	3.000	O	I			5.40
12.250	15.46	12.92	3.020	O	I			5.43
12.333	16.17	14.22	3.035	O I				5.45
12.417	16.92	15.27	3.048	O I				5.47
12.500	17.24	16.08	3.058	OI				5.48
12.583	17.96	16.77	3.066	OI				5.50
12.667	19.04	18.51	3.072	OI				5.50
12.750	19.37	19.43	3.073	O				5.51
12.833	19.84	19.66	3.074	OI				5.51
12.917	20.45	20.30	3.075	O				5.51
13.000	20.67	20.64	3.075	O				5.51
13.083	22.30	21.75	3.077	OI				5.51
13.167	24.89	24.18	3.082	OI				5.52
13.250	25.60	25.58	3.084	O				5.52
13.333	25.93	25.82	3.085	O				5.52
13.417	26.13	26.09	3.085	O				5.52
13.500	26.29	26.24	3.086	OI				5.52
13.583	22.97	24.13	3.082	I O				5.52
13.667	17.50	19.02	3.073	I O				5.50
13.750	16.15	16.73	3.065	IO				5.49
13.833	15.57	16.34	3.061	IO				5.49
13.917	15.28	15.93	3.056	IO				5.48
14.000	15.08	15.59	3.052	O				5.48
14.083	16.35	15.65	3.052	O				5.48
14.167	18.40	16.42	3.062	O I				5.49
14.250	18.95	18.18	3.071	OI				5.50
14.333	18.92	19.17	3.073	O				5.51
14.417	18.58	18.62	3.072	O				5.50
14.500	18.59	18.58	3.072	O				5.50
14.583	18.58	18.59	3.072	O				5.50
14.667	18.59	18.59	3.072	O				5.50
14.750	18.61	18.61	3.072	O				5.50
14.833	18.35	18.44	3.072	O				5.50
14.917	17.89	18.02	3.071	O				5.50
15.000	17.81	17.80	3.070	O				5.50
15.083	17.49	17.60	3.070	O				5.50
15.167	17.00	17.13	3.069	O				5.50
15.250	16.89	16.99	3.068	O				5.50
15.333	16.58	16.88	3.067	O				5.50
15.417	16.08	16.63	3.064	IO				5.49
15.500	15.98	16.36	3.061	O				5.49
15.583	14.74	15.91	3.056	I O				5.48
15.667	12.74	14.94	3.044	I O				5.47
15.750	12.25	13.84	3.031	I O				5.45
15.833	12.07	13.09	3.022	IO				5.44

15.917	11.99	12.61	3.016	|	|	IO|	|	|	5.43
16.000	11.94	12.32	3.013	|	|	O |	|	|	5.42
16.083	9.07	11.50	3.003	|	| I O |	|	|	5.41
16.167	4.33	9.34	2.978	| I |	O |	|	|	5.37
16.250	3.13	6.82	2.948	| I O	|	|	|	5.33
16.333	2.60	5.04	2.926	| I O |	|	|	|	5.30
16.417	2.31	3.88	2.913	| I O	|	|	|	5.28
16.500	2.09	3.12	2.904	| IO	|	|	|	5.27
16.583	1.94	2.62	2.898	| IO	|	|	|	5.26
16.667	1.69	2.26	2.893	| O	|	|	|	5.26
16.750	1.62	1.99	2.890	|IO	|	|	|	5.25
16.833	1.59	1.82	2.888	|IO	|	|	|	5.25
16.917	1.58	1.80	2.887	|IO	|	|	|	5.25
17.000	1.57	1.80	2.885	|IO	|	|	|	5.25
17.083	1.87	1.80	2.885	| O	|	|	|	5.25
17.167	2.37	1.80	2.887	| O	|	|	|	5.25
17.250	2.50	2.01	2.890	| OI	|	|	|	5.25
17.333	2.56	2.24	2.893	| OI	|	|	|	5.26
17.417	2.59	2.39	2.895	| OI	|	|	|	5.26
17.500	2.61	2.48	2.896	| O	|	|	|	5.26
17.583	2.61	2.54	2.897	| O	|	|	|	5.26
17.667	2.61	2.57	2.897	| O	|	|	|	5.26
17.750	2.61	2.59	2.897	| O	|	|	|	5.26
17.833	2.46	2.57	2.897	| IO	|	|	|	5.26
17.917	2.21	2.46	2.896	| O	|	|	|	5.26
18.000	2.14	2.33	2.894	| O	|	|	|	5.26
18.083	2.12	2.24	2.893	| O	|	|	|	5.26
18.167	2.10	2.18	2.893	| O	|	|	|	5.26
18.250	2.09	2.14	2.892	| O	|	|	|	5.26
18.333	2.09	2.12	2.892	| O	|	|	|	5.26
18.417	2.09	2.11	2.892	| O	|	|	|	5.25
18.500	2.09	2.10	2.892	| O	|	|	|	5.25
18.583	1.94	2.06	2.891	| O	|	|	|	5.25
18.667	1.69	1.95	2.890	| O	|	|	|	5.25
18.750	1.62	1.82	2.888	|IO	|	|	|	5.25
18.833	1.44	1.80	2.886	|IO	|	|	|	5.25
18.917	1.17	1.80	2.883	|IO	|	|	|	5.24
19.000	1.10	1.80	2.878	|IO	|	|	|	5.24
19.083	1.22	1.80	2.874	|IO	|	|	|	5.23
19.167	1.46	1.79	2.871	|IO	|	|	|	5.23
19.250	1.51	1.79	2.869	|IO	|	|	|	5.22
19.333	1.69	1.79	2.867	| O	|	|	|	5.22
19.417	1.96	1.79	2.868	| O	|	|	|	5.22
19.500	2.03	1.79	2.869	| O	|	|	|	5.22
19.583	1.91	1.79	2.870	| O	|	|	|	5.22
19.667	1.67	1.79	2.870	| O	|	|	|	5.22
19.750	1.62	1.79	2.869	|IO	|	|	|	5.22
19.833	1.44	1.79	2.867	|IO	|	|	|	5.22
19.917	1.17	1.79	2.864	|IO	|	|	|	5.22
20.000	1.10	1.79	2.860	|IO	|	|	|	5.21
20.083	1.22	1.79	2.855	|IO	|	|	|	5.20
20.167	1.46	1.79	2.852	|IO	|	|	|	5.20
20.250	1.51	1.79	2.850	|IO	|	|	|	5.20
20.333	1.54	1.79	2.848	|IO	|	|	|	5.19
20.417	1.56	1.78	2.847	|IO	|	|	|	5.19
20.500	1.57	1.78	2.845	|IO	|	|	|	5.19
20.583	1.57	1.78	2.844	|IO	|	|	|	5.19
20.667	1.57	1.78	2.842	|IO	|	|	|	5.18
20.750	1.57	1.78	2.841	|IO	|	|	|	5.18
20.833	1.41	1.78	2.839	|IO	|	|	|	5.18
20.917	1.16	1.78	2.835	|IO	|	|	|	5.18
21.000	1.10	1.78	2.831	|IO	|	|	|	5.17
21.083	1.22	1.78	2.827	|IO	|	|	|	5.16
21.167	1.46	1.78	2.824	|IO	|	|	|	5.16
21.250	1.51	1.77	2.822	|IO	|	|	|	5.16
21.333	1.39	1.77	2.819	|IO	|	|	|	5.15
21.417	1.15	1.77	2.816	|IO	|	|	|	5.15
21.500	1.10	1.77	2.811	|IO	|	|	|	5.14
21.583	1.22	1.77	2.807	|IO	|	|	|	5.14
21.667	1.46	1.77	2.804	|IO	|	|	|	5.13
21.750	1.51	1.77	2.802	|IO	|	|	|	5.13
21.833	1.39	1.77	2.800	|IO	|	|	|	5.13
21.917	1.15	1.76	2.797	|IO	|	|	|	5.12
22.000	1.10	1.76	2.792	|IO	|	|	|	5.11
22.083	1.22	1.76	2.788	|IO	|	|	|	5.11
22.167	1.46	1.76	2.785	|IO	|	|	|	5.10
22.250	1.51	1.76	2.784	|IO	|	|	|	5.10
22.333	1.39	1.76	2.781	|IO	|	|	|	5.10
22.417	1.15	1.76	2.778	|IO	|	|	|	5.09
22.500	1.10	1.76	2.774	|IO	|	|	|	5.09
22.583	1.07	1.75	2.769	|IO	|	|	|	5.08
22.667	1.06	1.75	2.764	|IO	|	|	|	5.07
22.750	1.04	1.75	2.759	|IO	|	|	|	5.07
22.833	1.04	1.75	2.755	|IO	|	|	|	5.06
22.917	1.04	1.75	2.750	|IO	|	|	|	5.05
23.000	1.04	1.74	2.745	|IO	|	|	|	5.05

23.083	1.04	1.74	2.740	|IO				5.04
23.167	1.04	1.74	2.735	|IO				5.03
23.250	1.04	1.74	2.731	|IO				5.03
23.333	1.04	1.74	2.726	|IO				5.02
23.417	1.04	1.73	2.721	|IO				5.01
23.500	1.04	1.73	2.716	|IO				5.01
23.583	1.04	1.73	2.712	|IO				5.00
23.667	1.04	1.73	2.707	|IO				4.99
23.750	1.04	1.73	2.702	|IO				4.99
23.833	1.04	1.72	2.697	|IO				4.98
23.917	1.04	1.72	2.693	|IO				4.97
24.000	1.04	1.72	2.688	|IO				4.96
24.083	0.74	1.72	2.682	I O				4.96
24.167	0.24	1.71	2.674	I O				4.94
24.250	0.11	1.71	2.663	I O				4.93
24.333	0.05	1.70	2.652	I O				4.91
24.417	0.02	1.70	2.641	I O				4.89
24.500	0.00	1.69	2.629	I O				4.88
24.583	0.00	1.69	2.618	I O				4.86
24.667	0.00	1.68	2.606	I O				4.84
24.750	0.00	1.68	2.594	I O				4.82
24.833	0.00	1.67	2.583	I O				4.81
24.917	0.00	1.66	2.571	I O				4.79
25.000	0.00	1.66	2.560	I O				4.77
25.083	0.00	1.65	2.549	I O				4.75
25.167	0.00	1.65	2.537	I O				4.74
25.250	0.00	1.64	2.526	IO				4.72
25.333	0.00	1.64	2.515	IO				4.70
25.417	0.00	1.63	2.503	IO				4.69
25.500	0.00	1.63	2.492	IO				4.67
25.583	0.00	1.62	2.481	IO				4.65
25.667	0.00	1.62	2.470	IO				4.63
25.750	0.00	1.61	2.459	IO				4.62
25.833	0.00	1.61	2.448	IO				4.60
25.917	0.00	1.60	2.437	IO				4.58
26.000	0.00	1.60	2.426	IO				4.57
26.083	0.00	1.59	2.415	IO				4.55
26.167	0.00	1.58	2.404	IO				4.53
26.250	0.00	1.58	2.393	IO				4.52
26.333	0.00	1.57	2.382	IO				4.50
26.417	0.00	1.57	2.371	IO				4.49
26.500	0.00	1.56	2.360	IO				4.47
26.583	0.00	1.56	2.349	IO				4.45
26.667	0.00	1.55	2.339	IO				4.44
26.750	0.00	1.55	2.328	IO				4.42
26.833	0.00	1.54	2.317	IO				4.40
26.917	0.00	1.54	2.307	IO				4.39
27.000	0.00	1.53	2.296	IO				4.37
27.083	0.00	1.53	2.286	IO				4.36
27.167	0.00	1.52	2.275	IO				4.34
27.250	0.00	1.52	2.265	IO				4.33
27.333	0.00	1.51	2.254	IO				4.31
27.417	0.00	1.51	2.244	IO				4.29
27.500	0.00	1.50	2.233	IO				4.28
27.583	0.00	1.50	2.223	IO				4.26
27.667	0.00	1.49	2.213	IO				4.25
27.750	0.00	1.49	2.202	IO				4.23
27.833	0.00	1.48	2.192	IO				4.22
27.917	0.00	1.48	2.182	IO				4.20
28.000	0.00	1.48	2.172	IO				4.19
28.083	0.00	1.47	2.162	IO				4.17
28.167	0.00	1.47	2.152	IO				4.15
28.250	0.00	1.46	2.142	IO				4.14
28.333	0.00	1.46	2.131	IO				4.12
28.417	0.00	1.45	2.121	IO				4.11
28.500	0.00	1.45	2.112	IO				4.09
28.583	0.00	1.44	2.102	IO				4.08
28.667	0.00	1.44	2.092	IO				4.06
28.750	0.00	1.43	2.082	IO				4.05
28.833	0.00	1.43	2.072	IO				4.03
28.917	0.00	1.42	2.062	IO				4.02
29.000	0.00	1.42	2.052	IO				4.00
29.083	0.00	1.41	2.043	IO				3.99
29.167	0.00	1.41	2.033	IO				3.97
29.250	0.00	1.40	2.023	IO				3.96
29.333	0.00	1.39	2.014	IO				3.94
29.417	0.00	1.38	2.004	IO				3.92
29.500	0.00	1.38	1.995	IO				3.91
29.583	0.00	1.37	1.985	IO				3.89
29.667	0.00	1.36	1.976	IO				3.88
29.750	0.00	1.36	1.966	IO				3.86
29.833	0.00	1.35	1.957	IO				3.85
29.917	0.00	1.34	1.948	IO				3.83
30.000	0.00	1.34	1.938	IO				3.82
30.083	0.00	1.33	1.929	IO				3.80
30.167	0.00	1.33	1.920	IO				3.78

30.250	0.00	1.32	1.911	IO				3.77
30.333	0.00	1.31	1.902	IO				3.75
30.417	0.00	1.31	1.893	IO				3.74
30.500	0.00	1.30	1.884	IO				3.72
30.583	0.00	1.29	1.875	IO				3.71
30.667	0.00	1.29	1.866	IO				3.69
30.750	0.00	1.28	1.857	IO				3.68
30.833	0.00	1.27	1.848	IO				3.66
30.917	0.00	1.27	1.840	IO				3.65
31.000	0.00	1.26	1.831	IO				3.64
31.083	0.00	1.26	1.822	IO				3.62
31.167	0.00	1.25	1.814	IO				3.61
31.250	0.00	1.24	1.805	IO				3.59
31.333	0.00	1.24	1.797	IO				3.58
31.417	0.00	1.23	1.788	IO				3.56
31.500	0.00	1.23	1.780	IO				3.55
31.583	0.00	1.22	1.771	IO				3.54
31.667	0.00	1.21	1.763	IO				3.52
31.750	0.00	1.21	1.754	IO				3.51
31.833	0.00	1.20	1.746	IO				3.49
31.917	0.00	1.20	1.738	IO				3.48
32.000	0.00	1.19	1.730	IO				3.47
32.083	0.00	1.18	1.722	IO				3.45
32.167	0.00	1.18	1.713	IO				3.44
32.250	0.00	1.17	1.705	IO				3.43
32.333	0.00	1.17	1.697	IO				3.41
32.417	0.00	1.16	1.689	IO				3.40
32.500	0.00	1.16	1.681	IO				3.39
32.583	0.00	1.15	1.673	IO				3.37
32.667	0.00	1.14	1.665	IO				3.36
32.750	0.00	1.14	1.658	IO				3.35
32.833	0.00	1.13	1.650	IO				3.33
32.917	0.00	1.13	1.642	IO				3.32
33.000	0.00	1.12	1.634	IO				3.31
33.083	0.00	1.12	1.627	IO				3.29
33.167	0.00	1.11	1.619	IO				3.28
33.250	0.00	1.11	1.611	IO				3.27
33.333	0.00	1.10	1.604	IO				3.26
33.417	0.00	1.09	1.596	IO				3.24
33.500	0.00	1.09	1.589	IO				3.23
33.583	0.00	1.08	1.581	IO				3.22
33.667	0.00	1.08	1.574	IO				3.21
33.750	0.00	1.07	1.566	IO				3.19
33.833	0.00	1.07	1.559	IO				3.18
33.917	0.00	1.06	1.552	IO				3.17
34.000	0.00	1.06	1.544	IO				3.16
34.083	0.00	1.05	1.537	IO				3.14
34.167	0.00	1.05	1.530	IO				3.13
34.250	0.00	1.04	1.523	IO				3.12
34.333	0.00	1.04	1.515	IO				3.11
34.417	0.00	1.03	1.508	IO				3.10
34.500	0.00	1.03	1.501	IO				3.08
34.583	0.00	1.02	1.494	IO				3.07
34.667	0.00	1.02	1.487	IO				3.06
34.750	0.00	1.01	1.480	IO				3.05
34.833	0.00	1.01	1.473	IO				3.04
34.917	0.00	1.00	1.466	IO				3.03
35.000	0.00	1.00	1.459	IO				3.01
35.083	0.00	0.99	1.453	IO				3.00
35.167	0.00	0.98	1.446	IO				2.99
35.250	0.00	0.98	1.439	IO				2.98
35.333	0.00	0.97	1.432	IO				2.97
35.417	0.00	0.96	1.426	IO				2.95
35.500	0.00	0.95	1.419	IO				2.94
35.583	0.00	0.94	1.413	IO				2.93
35.667	0.00	0.94	1.406	IO				2.92
35.750	0.00	0.93	1.400	IO				2.90
35.833	0.00	0.92	1.393	IO				2.89
35.917	0.00	0.91	1.387	IO				2.88
36.000	0.00	0.91	1.381	IO				2.87
36.083	0.00	0.90	1.374	IO				2.86
36.167	0.00	0.89	1.368	IO				2.85
36.250	0.00	0.88	1.362	IO				2.83
36.333	0.00	0.88	1.356	IO				2.82
36.417	0.00	0.87	1.350	IO				2.81
36.500	0.00	0.86	1.344	IO				2.80
36.583	0.00	0.86	1.338	IO				2.79
36.667	0.00	0.85	1.332	IO				2.78
36.750	0.00	0.84	1.327	IO				2.77
36.833	0.00	0.83	1.321	IO				2.76
36.917	0.00	0.83	1.315	IO				2.75
37.000	0.00	0.82	1.309	O				2.74
37.083	0.00	0.81	1.304	O				2.73
37.167	0.00	0.81	1.298	O				2.72
37.250	0.00	0.80	1.293	O				2.71
37.333	0.00	0.79	1.287	O				2.69

37.417	0.00	0.79	1.282	o	|	|	|	|	2.68
37.500	0.00	0.78	1.276	o	|	|	|	|	2.67
37.583	0.00	0.77	1.271	o	|	|	|	|	2.66
37.667	0.00	0.77	1.266	o	|	|	|	|	2.65
37.750	0.00	0.76	1.260	o	|	|	|	|	2.64
37.833	0.00	0.76	1.255	o	|	|	|	|	2.64
37.917	0.00	0.75	1.250	o	|	|	|	|	2.63
38.000	0.00	0.74	1.245	o	|	|	|	|	2.62
38.083	0.00	0.74	1.240	o	|	|	|	|	2.61
38.167	0.00	0.73	1.235	o	|	|	|	|	2.60
38.250	0.00	0.72	1.230	o	|	|	|	|	2.59
38.333	0.00	0.72	1.225	o	|	|	|	|	2.58
38.417	0.00	0.71	1.220	o	|	|	|	|	2.57
38.500	0.00	0.71	1.215	o	|	|	|	|	2.56
38.583	0.00	0.70	1.210	o	|	|	|	|	2.55
38.667	0.00	0.69	1.205	o	|	|	|	|	2.54
38.750	0.00	0.69	1.200	o	|	|	|	|	2.53
38.833	0.00	0.68	1.196	o	|	|	|	|	2.52
38.917	0.00	0.68	1.191	o	|	|	|	|	2.52
39.000	0.00	0.67	1.186	o	|	|	|	|	2.51
39.083	0.00	0.67	1.182	o	|	|	|	|	2.50
39.167	0.00	0.66	1.177	o	|	|	|	|	2.49
39.250	0.00	0.66	1.173	o	|	|	|	|	2.48
39.333	0.00	0.65	1.168	o	|	|	|	|	2.47
39.417	0.00	0.64	1.164	o	|	|	|	|	2.47
39.500	0.00	0.64	1.159	o	|	|	|	|	2.46
39.583	0.00	0.63	1.155	o	|	|	|	|	2.45
39.667	0.00	0.63	1.151	o	|	|	|	|	2.44
39.750	0.00	0.62	1.146	o	|	|	|	|	2.43
39.833	0.00	0.62	1.142	o	|	|	|	|	2.42
39.917	0.00	0.61	1.138	o	|	|	|	|	2.42
40.000	0.00	0.61	1.134	o	|	|	|	|	2.41
40.083	0.00	0.60	1.129	o	|	|	|	|	2.40
40.167	0.00	0.60	1.125	o	|	|	|	|	2.39
40.250	0.00	0.59	1.121	o	|	|	|	|	2.39
40.333	0.00	0.59	1.117	o	|	|	|	|	2.38
40.417	0.00	0.58	1.113	o	|	|	|	|	2.37
40.500	0.00	0.58	1.109	o	|	|	|	|	2.36
40.583	0.00	0.57	1.105	o	|	|	|	|	2.36
40.667	0.00	0.57	1.101	o	|	|	|	|	2.35
40.750	0.00	0.56	1.097	o	|	|	|	|	2.34
40.833	0.00	0.56	1.093	o	|	|	|	|	2.33
40.917	0.00	0.56	1.089	o	|	|	|	|	2.33
41.000	0.00	0.55	1.086	o	|	|	|	|	2.32
41.083	0.00	0.55	1.082	o	|	|	|	|	2.31
41.167	0.00	0.54	1.078	o	|	|	|	|	2.31
41.250	0.00	0.54	1.074	o	|	|	|	|	2.30
41.333	0.00	0.53	1.071	o	|	|	|	|	2.29
41.417	0.00	0.53	1.067	o	|	|	|	|	2.29
41.500	0.00	0.52	1.063	o	|	|	|	|	2.28
41.583	0.00	0.52	1.060	o	|	|	|	|	2.27
41.667	0.00	0.52	1.056	o	|	|	|	|	2.26
41.750	0.00	0.51	1.053	o	|	|	|	|	2.26
41.833	0.00	0.51	1.049	o	|	|	|	|	2.25
41.917	0.00	0.50	1.046	o	|	|	|	|	2.25
42.000	0.00	0.50	1.042	o	|	|	|	|	2.24
42.083	0.00	0.49	1.039	o	|	|	|	|	2.23
42.167	0.00	0.49	1.036	o	|	|	|	|	2.23
42.250	0.00	0.49	1.032	o	|	|	|	|	2.22
42.333	0.00	0.48	1.029	o	|	|	|	|	2.21
42.417	0.00	0.48	1.026	o	|	|	|	|	2.21
42.500	0.00	0.47	1.022	o	|	|	|	|	2.20
42.583	0.00	0.47	1.019	o	|	|	|	|	2.20
42.667	0.00	0.47	1.016	o	|	|	|	|	2.19
42.750	0.00	0.46	1.013	o	|	|	|	|	2.18
42.833	0.00	0.46	1.009	o	|	|	|	|	2.18
42.917	0.00	0.46	1.006	o	|	|	|	|	2.17
43.000	0.00	0.45	1.003	o	|	|	|	|	2.17
43.083	0.00	0.45	1.000	o	|	|	|	|	2.16
43.167	0.00	0.44	0.997	o	|	|	|	|	2.15
43.250	0.00	0.44	0.994	o	|	|	|	|	2.15
43.333	0.00	0.44	0.991	o	|	|	|	|	2.14
43.417	0.00	0.43	0.988	o	|	|	|	|	2.14
43.500	0.00	0.43	0.985	o	|	|	|	|	2.13
43.583	0.00	0.43	0.982	o	|	|	|	|	2.13
43.667	0.00	0.42	0.979	o	|	|	|	|	2.12
43.750	0.00	0.42	0.976	o	|	|	|	|	2.12
43.833	0.00	0.42	0.973	o	|	|	|	|	2.11
43.917	0.00	0.41	0.970	o	|	|	|	|	2.11
44.000	0.00	0.41	0.968	o	|	|	|	|	2.10
44.083	0.00	0.41	0.965	o	|	|	|	|	2.09
44.167	0.00	0.40	0.962	o	|	|	|	|	2.09
44.250	0.00	0.40	0.959	o	|	|	|	|	2.08
44.333	0.00	0.40	0.957	o	|	|	|	|	2.08
44.417	0.00	0.39	0.954	o	|	|	|	|	2.07
44.500	0.00	0.39	0.951	o	|	|	|	|	2.07

44.583	0.00	0.39	0.948	o	|	|	|	|	2.06
44.667	0.00	0.38	0.946	o	|	|	|	|	2.06
44.750	0.00	0.38	0.943	o	|	|	|	|	2.05
44.833	0.00	0.38	0.941	o	|	|	|	|	2.05
44.917	0.00	0.37	0.938	o	|	|	|	|	2.04
45.000	0.00	0.37	0.935	o	|	|	|	|	2.04
45.083	0.00	0.37	0.933	o	|	|	|	|	2.04
45.167	0.00	0.36	0.930	o	|	|	|	|	2.03
45.250	0.00	0.36	0.928	o	|	|	|	|	2.03
45.333	0.00	0.36	0.925	o	|	|	|	|	2.02
45.417	0.00	0.35	0.923	o	|	|	|	|	2.02
45.500	0.00	0.35	0.921	o	|	|	|	|	2.01
45.583	0.00	0.35	0.918	o	|	|	|	|	2.01
45.667	0.00	0.35	0.916	o	|	|	|	|	2.00
45.750	0.00	0.34	0.913	o	|	|	|	|	2.00
45.833	0.00	0.34	0.911	o	|	|	|	|	1.99
45.917	0.00	0.34	0.909	o	|	|	|	|	1.99
46.000	0.00	0.34	0.906	o	|	|	|	|	1.98
46.083	0.00	0.34	0.904	o	|	|	|	|	1.98
46.167	0.00	0.34	0.902	o	|	|	|	|	1.97
46.250	0.00	0.34	0.899	o	|	|	|	|	1.97
46.333	0.00	0.34	0.897	o	|	|	|	|	1.96
46.417	0.00	0.34	0.895	o	|	|	|	|	1.96
46.500	0.00	0.34	0.892	o	|	|	|	|	1.95
46.583	0.00	0.34	0.890	o	|	|	|	|	1.95
46.667	0.00	0.34	0.888	o	|	|	|	|	1.95
46.750	0.00	0.34	0.885	o	|	|	|	|	1.94
46.833	0.00	0.34	0.883	o	|	|	|	|	1.94
46.917	0.00	0.34	0.881	o	|	|	|	|	1.93
47.000	0.00	0.34	0.878	o	|	|	|	|	1.93
47.083	0.00	0.33	0.876	o	|	|	|	|	1.92
47.167	0.00	0.33	0.874	o	|	|	|	|	1.92
47.250	0.00	0.33	0.871	o	|	|	|	|	1.91
47.333	0.00	0.33	0.869	o	|	|	|	|	1.91
47.417	0.00	0.33	0.867	o	|	|	|	|	1.90
47.500	0.00	0.33	0.865	o	|	|	|	|	1.90
47.583	0.00	0.33	0.862	o	|	|	|	|	1.89
47.667	0.00	0.33	0.860	o	|	|	|	|	1.89
47.750	0.00	0.33	0.858	o	|	|	|	|	1.88
47.833	0.00	0.33	0.855	o	|	|	|	|	1.88
47.917	0.00	0.33	0.853	o	|	|	|	|	1.87
48.000	0.00	0.33	0.851	o	|	|	|	|	1.87
48.083	0.00	0.33	0.849	o	|	|	|	|	1.86
48.167	0.00	0.33	0.846	o	|	|	|	|	1.86
48.250	0.00	0.33	0.844	o	|	|	|	|	1.86
48.333	0.00	0.33	0.842	o	|	|	|	|	1.85
48.417	0.00	0.33	0.840	o	|	|	|	|	1.85
48.500	0.00	0.33	0.837	o	|	|	|	|	1.84
48.583	0.00	0.32	0.835	o	|	|	|	|	1.84
48.667	0.00	0.32	0.833	o	|	|	|	|	1.83
48.750	0.00	0.32	0.831	o	|	|	|	|	1.83
48.833	0.00	0.32	0.828	o	|	|	|	|	1.82
48.917	0.00	0.32	0.826	o	|	|	|	|	1.82
49.000	0.00	0.32	0.824	o	|	|	|	|	1.81
49.083	0.00	0.32	0.822	o	|	|	|	|	1.81
49.167	0.00	0.32	0.820	o	|	|	|	|	1.80
49.250	0.00	0.32	0.817	o	|	|	|	|	1.80
49.333	0.00	0.32	0.815	o	|	|	|	|	1.80
49.417	0.00	0.32	0.813	o	|	|	|	|	1.79
49.500	0.00	0.32	0.811	o	|	|	|	|	1.79
49.583	0.00	0.32	0.809	o	|	|	|	|	1.78
49.667	0.00	0.32	0.806	o	|	|	|	|	1.78
49.750	0.00	0.32	0.804	o	|	|	|	|	1.77
49.833	0.00	0.32	0.802	o	|	|	|	|	1.77
49.917	0.00	0.32	0.800	o	|	|	|	|	1.76
50.000	0.00	0.32	0.798	o	|	|	|	|	1.76
50.083	0.00	0.31	0.796	o	|	|	|	|	1.75
50.167	0.00	0.31	0.793	o	|	|	|	|	1.75
50.250	0.00	0.31	0.791	o	|	|	|	|	1.75
50.333	0.00	0.31	0.789	o	|	|	|	|	1.74
50.417	0.00	0.31	0.787	o	|	|	|	|	1.74
50.500	0.00	0.31	0.785	o	|	|	|	|	1.73
50.583	0.00	0.31	0.783	o	|	|	|	|	1.73
50.667	0.00	0.31	0.780	o	|	|	|	|	1.72
50.750	0.00	0.31	0.778	o	|	|	|	|	1.72
50.833	0.00	0.31	0.776	o	|	|	|	|	1.71
50.917	0.00	0.31	0.774	o	|	|	|	|	1.71
51.000	0.00	0.31	0.772	o	|	|	|	|	1.71
51.083	0.00	0.31	0.770	o	|	|	|	|	1.70
51.167	0.00	0.31	0.768	o	|	|	|	|	1.70
51.250	0.00	0.31	0.766	o	|	|	|	|	1.69
51.333	0.00	0.31	0.763	o	|	|	|	|	1.69
51.417	0.00	0.31	0.761	o	|	|	|	|	1.68
51.500	0.00	0.31	0.759	o	|	|	|	|	1.68
51.583	0.00	0.31	0.757	o	|	|	|	|	1.68
51.667	0.00	0.30	0.755	o	|	|	|	|	1.67

51.750	0.00	0.30	0.753	o					1.67
51.833	0.00	0.30	0.751	o					1.66
51.917	0.00	0.30	0.749	o					1.66
52.000	0.00	0.30	0.747	o					1.65
52.083	0.00	0.30	0.745	o					1.65
52.167	0.00	0.30	0.742	o					1.64
52.250	0.00	0.30	0.740	o					1.64
52.333	0.00	0.30	0.738	o					1.64
52.417	0.00	0.30	0.736	o					1.63
52.500	0.00	0.30	0.734	o					1.63
52.583	0.00	0.30	0.732	o					1.62
52.667	0.00	0.30	0.730	o					1.62
52.750	0.00	0.30	0.728	o					1.61
52.833	0.00	0.30	0.726	o					1.61
52.917	0.00	0.30	0.724	o					1.61
53.000	0.00	0.30	0.722	o					1.60
53.083	0.00	0.30	0.720	o					1.60
53.167	0.00	0.30	0.718	o					1.59
53.250	0.00	0.30	0.716	o					1.59
53.333	0.00	0.29	0.714	o					1.59
53.417	0.00	0.29	0.712	o					1.58
53.500	0.00	0.29	0.710	o					1.58
53.583	0.00	0.29	0.708	o					1.57
53.667	0.00	0.29	0.706	o					1.57
53.750	0.00	0.29	0.704	o					1.56
53.833	0.00	0.29	0.702	o					1.56
53.917	0.00	0.29	0.700	o					1.56
54.000	0.00	0.29	0.698	o					1.55
54.083	0.00	0.29	0.696	o					1.55
54.167	0.00	0.29	0.694	o					1.54
54.250	0.00	0.29	0.692	o					1.54
54.333	0.00	0.29	0.690	o					1.54
54.417	0.00	0.29	0.688	o					1.53
54.500	0.00	0.29	0.686	o					1.53
54.583	0.00	0.29	0.684	o					1.52
54.667	0.00	0.29	0.682	o					1.52
54.750	0.00	0.29	0.680	o					1.51
54.833	0.00	0.29	0.678	o					1.51
54.917	0.00	0.29	0.676	o					1.51
55.000	0.00	0.28	0.674	o					1.50
55.083	0.00	0.28	0.672	o					1.50
55.167	0.00	0.28	0.670	o					1.49
55.250	0.00	0.28	0.668	o					1.49
55.333	0.00	0.28	0.666	o					1.49
55.417	0.00	0.28	0.664	o					1.48
55.500	0.00	0.28	0.662	o					1.48
55.583	0.00	0.28	0.660	o					1.47
55.667	0.00	0.28	0.658	o					1.47
55.750	0.00	0.28	0.656	o					1.47
55.833	0.00	0.28	0.654	o					1.46
55.917	0.00	0.28	0.652	o					1.46
56.000	0.00	0.28	0.650	o					1.45
56.083	0.00	0.28	0.649	o					1.45
56.167	0.00	0.28	0.647	o					1.45
56.250	0.00	0.28	0.645	o					1.44
56.333	0.00	0.28	0.643	o					1.44
56.417	0.00	0.28	0.641	o					1.43
56.500	0.00	0.28	0.639	o					1.43
56.583	0.00	0.28	0.637	o					1.43
56.667	0.00	0.28	0.635	o					1.42
56.750	0.00	0.27	0.633	o					1.42
56.833	0.00	0.27	0.631	o					1.41
56.917	0.00	0.27	0.630	o					1.41
57.000	0.00	0.27	0.628	o					1.41
57.083	0.00	0.27	0.626	o					1.40
57.167	0.00	0.27	0.624	o					1.40
57.250	0.00	0.27	0.622	o					1.40
57.333	0.00	0.27	0.620	o					1.39
57.417	0.00	0.27	0.618	o					1.39
57.500	0.00	0.27	0.616	o					1.38
57.583	0.00	0.27	0.615	o					1.38
57.667	0.00	0.27	0.613	o					1.38
57.750	0.00	0.27	0.611	o					1.37
57.833	0.00	0.27	0.609	o					1.37
57.917	0.00	0.27	0.607	o					1.36
58.000	0.00	0.27	0.605	o					1.36
58.083	0.00	0.27	0.603	o					1.36
58.167	0.00	0.27	0.602	o					1.35
58.250	0.00	0.27	0.600	o					1.35
58.333	0.00	0.27	0.598	o					1.35
58.417	0.00	0.27	0.596	o					1.34
58.500	0.00	0.27	0.594	o					1.34
58.583	0.00	0.26	0.592	o					1.33
58.667	0.00	0.26	0.591	o					1.33
58.750	0.00	0.26	0.589	o					1.33
58.833	0.00	0.26	0.587	o					1.32

58.917	0.00	0.26	0.585	o	|	|	|	|	1.32
59.000	0.00	0.26	0.583	o	|	|	|	|	1.32
59.083	0.00	0.26	0.582	o	|	|	|	|	1.31
59.167	0.00	0.26	0.580	o	|	|	|	|	1.31
59.250	0.00	0.26	0.578	o	|	|	|	|	1.30
59.333	0.00	0.26	0.576	o	|	|	|	|	1.30
59.417	0.00	0.26	0.574	o	|	|	|	|	1.30
59.500	0.00	0.26	0.573	o	|	|	|	|	1.29
59.583	0.00	0.26	0.571	o	|	|	|	|	1.29
59.667	0.00	0.26	0.569	o	|	|	|	|	1.29
59.750	0.00	0.26	0.567	o	|	|	|	|	1.28
59.833	0.00	0.26	0.565	o	|	|	|	|	1.28
59.917	0.00	0.26	0.564	o	|	|	|	|	1.27
60.000	0.00	0.26	0.562	o	|	|	|	|	1.27
60.083	0.00	0.26	0.560	o	|	|	|	|	1.27
60.167	0.00	0.26	0.558	o	|	|	|	|	1.26
60.250	0.00	0.26	0.557	o	|	|	|	|	1.26
60.333	0.00	0.26	0.555	o	|	|	|	|	1.26
60.417	0.00	0.26	0.553	o	|	|	|	|	1.25
60.500	0.00	0.25	0.551	o	|	|	|	|	1.25
60.583	0.00	0.25	0.550	o	|	|	|	|	1.25
60.667	0.00	0.25	0.548	o	|	|	|	|	1.24
60.750	0.00	0.25	0.546	o	|	|	|	|	1.24
60.833	0.00	0.25	0.544	o	|	|	|	|	1.23
60.917	0.00	0.25	0.543	o	|	|	|	|	1.23
61.000	0.00	0.25	0.541	o	|	|	|	|	1.23
61.083	0.00	0.25	0.539	o	|	|	|	|	1.22
61.167	0.00	0.25	0.537	o	|	|	|	|	1.22
61.250	0.00	0.25	0.536	o	|	|	|	|	1.22
61.333	0.00	0.25	0.534	o	|	|	|	|	1.21
61.417	0.00	0.25	0.532	o	|	|	|	|	1.21
61.500	0.00	0.25	0.530	o	|	|	|	|	1.21
61.583	0.00	0.25	0.529	o	|	|	|	|	1.20
61.667	0.00	0.25	0.527	o	|	|	|	|	1.20
61.750	0.00	0.25	0.525	o	|	|	|	|	1.20
61.833	0.00	0.25	0.524	o	|	|	|	|	1.19
61.917	0.00	0.25	0.522	o	|	|	|	|	1.19
62.000	0.00	0.25	0.520	o	|	|	|	|	1.18
62.083	0.00	0.25	0.519	o	|	|	|	|	1.18
62.167	0.00	0.25	0.517	o	|	|	|	|	1.18
62.250	0.00	0.25	0.515	o	|	|	|	|	1.17
62.333	0.00	0.25	0.513	o	|	|	|	|	1.17
62.417	0.00	0.24	0.512	o	|	|	|	|	1.17
62.500	0.00	0.24	0.510	o	|	|	|	|	1.16
62.583	0.00	0.24	0.508	o	|	|	|	|	1.16
62.667	0.00	0.24	0.507	o	|	|	|	|	1.16
62.750	0.00	0.24	0.505	o	|	|	|	|	1.15
62.833	0.00	0.24	0.503	o	|	|	|	|	1.15
62.917	0.00	0.24	0.502	o	|	|	|	|	1.15
63.000	0.00	0.24	0.500	o	|	|	|	|	1.14
63.083	0.00	0.24	0.498	o	|	|	|	|	1.14
63.167	0.00	0.24	0.497	o	|	|	|	|	1.14
63.250	0.00	0.24	0.495	o	|	|	|	|	1.13
63.333	0.00	0.24	0.493	o	|	|	|	|	1.13
63.417	0.00	0.24	0.492	o	|	|	|	|	1.13
63.500	0.00	0.24	0.490	o	|	|	|	|	1.12
63.583	0.00	0.24	0.488	o	|	|	|	|	1.12
63.667	0.00	0.24	0.487	o	|	|	|	|	1.12
63.750	0.00	0.24	0.485	o	|	|	|	|	1.11
63.833	0.00	0.24	0.483	o	|	|	|	|	1.11
63.917	0.00	0.24	0.482	o	|	|	|	|	1.11
64.000	0.00	0.24	0.480	o	|	|	|	|	1.10
64.083	0.00	0.24	0.479	o	|	|	|	|	1.10
64.167	0.00	0.24	0.477	o	|	|	|	|	1.10
64.250	0.00	0.24	0.475	o	|	|	|	|	1.09
64.333	0.00	0.24	0.474	o	|	|	|	|	1.09
64.417	0.00	0.24	0.472	o	|	|	|	|	1.09
64.500	0.00	0.23	0.470	o	|	|	|	|	1.08
64.583	0.00	0.23	0.469	o	|	|	|	|	1.08
64.667	0.00	0.23	0.467	o	|	|	|	|	1.08
64.750	0.00	0.23	0.466	o	|	|	|	|	1.07
64.833	0.00	0.23	0.464	o	|	|	|	|	1.07
64.917	0.00	0.23	0.462	o	|	|	|	|	1.07
65.000	0.00	0.23	0.461	o	|	|	|	|	1.06
65.083	0.00	0.23	0.459	o	|	|	|	|	1.06
65.167	0.00	0.23	0.458	o	|	|	|	|	1.06
65.250	0.00	0.23	0.456	o	|	|	|	|	1.05
65.333	0.00	0.23	0.454	o	|	|	|	|	1.05
65.417	0.00	0.23	0.453	o	|	|	|	|	1.05
65.500	0.00	0.23	0.451	o	|	|	|	|	1.04
65.583	0.00	0.23	0.450	o	|	|	|	|	1.04
65.667	0.00	0.23	0.448	o	|	|	|	|	1.04
65.750	0.00	0.23	0.447	o	|	|	|	|	1.03
65.833	0.00	0.23	0.445	o	|	|	|	|	1.03
65.917	0.00	0.23	0.443	o	|	|	|	|	1.03
66.000	0.00	0.23	0.442	o	|	|	|	|	1.02

66.083	0.00	0.23	0.440	o					1.02
66.167	0.00	0.23	0.439	o					1.02
66.250	0.00	0.23	0.437	o					1.01
66.333	0.00	0.23	0.436	o					1.01
66.417	0.00	0.23	0.434	o					1.01
66.500	0.00	0.23	0.432	o					1.00
66.583	0.00	0.22	0.431	o					1.00
66.667	0.00	0.22	0.429	o					1.00
66.750	0.00	0.22	0.428	o					0.99
66.833	0.00	0.22	0.426	o					0.99
66.917	0.00	0.22	0.425	o					0.99
67.000	0.00	0.22	0.423	o					0.98
67.083	0.00	0.22	0.422	o					0.98
67.167	0.00	0.22	0.420	o					0.97
67.250	0.00	0.22	0.419	o					0.97
67.333	0.00	0.22	0.417	o					0.97
67.417	0.00	0.22	0.416	o					0.96
67.500	0.00	0.22	0.414	o					0.96
67.583	0.00	0.22	0.413	o					0.96
67.667	0.00	0.21	0.411	o					0.95
67.750	0.00	0.21	0.410	o					0.95
67.833	0.00	0.21	0.408	o					0.95
67.917	0.00	0.21	0.407	o					0.94
68.000	0.00	0.21	0.405	o					0.94
68.083	0.00	0.21	0.404	o					0.94
68.167	0.00	0.21	0.402	o					0.93
68.250	0.00	0.21	0.401	o					0.93
68.333	0.00	0.21	0.400	o					0.93
68.417	0.00	0.21	0.398	o					0.92
68.500	0.00	0.21	0.397	o					0.92
68.583	0.00	0.21	0.395	o					0.92
68.667	0.00	0.21	0.394	o					0.91
68.750	0.00	0.20	0.392	o					0.91
68.833	0.00	0.20	0.391	o					0.91
68.917	0.00	0.20	0.390	o					0.90
69.000	0.00	0.20	0.388	o					0.90
69.083	0.00	0.20	0.387	o					0.90
69.167	0.00	0.20	0.385	o					0.89
69.250	0.00	0.20	0.384	o					0.89
69.333	0.00	0.20	0.383	o					0.89
69.417	0.00	0.20	0.381	o					0.88
69.500	0.00	0.20	0.380	o					0.88
69.583	0.00	0.20	0.379	o					0.88
69.667	0.00	0.20	0.377	o					0.88
69.750	0.00	0.20	0.376	o					0.87
69.833	0.00	0.20	0.375	o					0.87
69.917	0.00	0.19	0.373	o					0.87
70.000	0.00	0.19	0.372	o					0.86
70.083	0.00	0.19	0.371	o					0.86
70.167	0.00	0.19	0.369	o					0.86
70.250	0.00	0.19	0.368	o					0.85
70.333	0.00	0.19	0.367	o					0.85
70.417	0.00	0.19	0.365	o					0.85
70.500	0.00	0.19	0.364	o					0.84
70.583	0.00	0.19	0.363	o					0.84
70.667	0.00	0.19	0.361	o					0.84
70.750	0.00	0.19	0.360	o					0.84
70.833	0.00	0.19	0.359	o					0.83
70.917	0.00	0.19	0.357	o					0.83
71.000	0.00	0.19	0.356	o					0.83
71.083	0.00	0.19	0.355	o					0.82
71.167	0.00	0.18	0.354	o					0.82
71.250	0.00	0.18	0.352	o					0.82
71.333	0.00	0.18	0.351	o					0.81
71.417	0.00	0.18	0.350	o					0.81
71.500	0.00	0.18	0.349	o					0.81
71.583	0.00	0.18	0.347	o					0.81
71.667	0.00	0.18	0.346	o					0.80
71.750	0.00	0.18	0.345	o					0.80
71.833	0.00	0.18	0.344	o					0.80
71.917	0.00	0.18	0.342	o					0.79
72.000	0.00	0.18	0.341	o					0.79
72.083	0.00	0.18	0.340	o					0.79
72.167	0.00	0.18	0.339	o					0.79
72.250	0.00	0.18	0.337	o					0.78
72.333	0.00	0.18	0.336	o					0.78
72.417	0.00	0.17	0.335	o					0.78
72.500	0.00	0.17	0.334	o					0.77
72.583	0.00	0.17	0.333	o					0.77
72.667	0.00	0.17	0.331	o					0.77
72.750	0.00	0.17	0.330	o					0.77
72.833	0.00	0.17	0.329	o					0.76
72.917	0.00	0.17	0.328	o					0.76
73.000	0.00	0.17	0.327	o					0.76
73.083	0.00	0.17	0.326	o					0.76
73.167	0.00	0.17	0.324	o					0.75

73.250	0.00	0.17	0.323	o	|	|	|	|	0.75
73.333	0.00	0.17	0.322	o	|	|	|	|	0.75
73.417	0.00	0.17	0.321	o	|	|	|	|	0.74
73.500	0.00	0.17	0.320	o	|	|	|	|	0.74
73.583	0.00	0.17	0.319	o	|	|	|	|	0.74
73.667	0.00	0.17	0.317	o	|	|	|	|	0.74
73.750	0.00	0.17	0.316	o	|	|	|	|	0.73
73.833	0.00	0.16	0.315	o	|	|	|	|	0.73
73.917	0.00	0.16	0.314	o	|	|	|	|	0.73
74.000	0.00	0.16	0.313	o	|	|	|	|	0.73
74.083	0.00	0.16	0.312	o	|	|	|	|	0.72
74.167	0.00	0.16	0.311	o	|	|	|	|	0.72
74.250	0.00	0.16	0.310	o	|	|	|	|	0.72
74.333	0.00	0.16	0.308	o	|	|	|	|	0.72
74.417	0.00	0.16	0.307	o	|	|	|	|	0.71
74.500	0.00	0.16	0.306	o	|	|	|	|	0.71
74.583	0.00	0.16	0.305	o	|	|	|	|	0.71
74.667	0.00	0.16	0.304	o	|	|	|	|	0.71
74.750	0.00	0.16	0.303	o	|	|	|	|	0.70
74.833	0.00	0.16	0.302	o	|	|	|	|	0.70
74.917	0.00	0.16	0.301	o	|	|	|	|	0.70
75.000	0.00	0.16	0.300	o	|	|	|	|	0.70
75.083	0.00	0.16	0.299	o	|	|	|	|	0.69
75.167	0.00	0.16	0.298	o	|	|	|	|	0.69
75.250	0.00	0.15	0.296	o	|	|	|	|	0.69
75.333	0.00	0.15	0.295	o	|	|	|	|	0.69
75.417	0.00	0.15	0.294	o	|	|	|	|	0.68
75.500	0.00	0.15	0.293	o	|	|	|	|	0.68
75.583	0.00	0.15	0.292	o	|	|	|	|	0.68
75.667	0.00	0.15	0.291	o	|	|	|	|	0.68
75.750	0.00	0.15	0.290	o	|	|	|	|	0.67
75.833	0.00	0.15	0.289	o	|	|	|	|	0.67
75.917	0.00	0.15	0.288	o	|	|	|	|	0.67
76.000	0.00	0.15	0.287	o	|	|	|	|	0.67
76.083	0.00	0.15	0.286	o	|	|	|	|	0.66
76.167	0.00	0.15	0.285	o	|	|	|	|	0.66
76.250	0.00	0.15	0.284	o	|	|	|	|	0.66
76.333	0.00	0.15	0.283	o	|	|	|	|	0.66
76.417	0.00	0.15	0.282	o	|	|	|	|	0.65
76.500	0.00	0.15	0.281	o	|	|	|	|	0.65
76.583	0.00	0.15	0.280	o	|	|	|	|	0.65
76.667	0.00	0.15	0.279	o	|	|	|	|	0.65
76.750	0.00	0.15	0.278	o	|	|	|	|	0.64
76.833	0.00	0.14	0.277	o	|	|	|	|	0.64
76.917	0.00	0.14	0.276	o	|	|	|	|	0.64
77.000	0.00	0.14	0.275	o	|	|	|	|	0.64
77.083	0.00	0.14	0.274	o	|	|	|	|	0.64
77.167	0.00	0.14	0.273	o	|	|	|	|	0.63
77.250	0.00	0.14	0.272	o	|	|	|	|	0.63
77.333	0.00	0.14	0.271	o	|	|	|	|	0.63
77.417	0.00	0.14	0.270	o	|	|	|	|	0.63
77.500	0.00	0.14	0.269	o	|	|	|	|	0.62
77.583	0.00	0.14	0.268	o	|	|	|	|	0.62
77.667	0.00	0.14	0.267	o	|	|	|	|	0.62
77.750	0.00	0.14	0.266	o	|	|	|	|	0.62
77.833	0.00	0.14	0.265	o	|	|	|	|	0.62
77.917	0.00	0.14	0.264	o	|	|	|	|	0.61
78.000	0.00	0.14	0.263	o	|	|	|	|	0.61
78.083	0.00	0.14	0.262	o	|	|	|	|	0.61
78.167	0.00	0.14	0.261	o	|	|	|	|	0.61
78.250	0.00	0.14	0.260	o	|	|	|	|	0.60
78.333	0.00	0.14	0.260	o	|	|	|	|	0.60
78.417	0.00	0.14	0.259	o	|	|	|	|	0.60
78.500	0.00	0.13	0.258	o	|	|	|	|	0.60
78.583	0.00	0.13	0.257	o	|	|	|	|	0.60
78.667	0.00	0.13	0.256	o	|	|	|	|	0.59
78.750	0.00	0.13	0.255	o	|	|	|	|	0.59
78.833	0.00	0.13	0.254	o	|	|	|	|	0.59
78.917	0.00	0.13	0.253	o	|	|	|	|	0.59
79.000	0.00	0.13	0.252	o	|	|	|	|	0.59
79.083	0.00	0.13	0.251	o	|	|	|	|	0.58
79.167	0.00	0.13	0.250	o	|	|	|	|	0.58
79.250	0.00	0.13	0.249	o	|	|	|	|	0.58
79.333	0.00	0.13	0.249	o	|	|	|	|	0.58
79.417	0.00	0.13	0.248	o	|	|	|	|	0.57
79.500	0.00	0.13	0.247	o	|	|	|	|	0.57
79.583	0.00	0.13	0.246	o	|	|	|	|	0.57
79.667	0.00	0.13	0.245	o	|	|	|	|	0.57
79.750	0.00	0.13	0.244	o	|	|	|	|	0.57
79.833	0.00	0.13	0.243	o	|	|	|	|	0.56
79.917	0.00	0.13	0.242	o	|	|	|	|	0.56
80.000	0.00	0.13	0.242	o	|	|	|	|	0.56
80.083	0.00	0.13	0.241	o	|	|	|	|	0.56
80.167	0.00	0.13	0.240	o	|	|	|	|	0.56
80.250	0.00	0.12	0.239	o	|	|	|	|	0.55
80.333	0.00	0.12	0.238	o	|	|	|	|	0.55

80.417	0.00	0.12	0.237	o	|	|	|	|	0.55
80.500	0.00	0.12	0.236	o	|	|	|	|	0.55
80.583	0.00	0.12	0.236	o	|	|	|	|	0.55
80.667	0.00	0.12	0.235	o	|	|	|	|	0.54
80.750	0.00	0.12	0.234	o	|	|	|	|	0.54
80.833	0.00	0.12	0.233	o	|	|	|	|	0.54
80.917	0.00	0.12	0.232	o	|	|	|	|	0.54
81.000	0.00	0.12	0.231	o	|	|	|	|	0.54
81.083	0.00	0.12	0.231	o	|	|	|	|	0.53
81.167	0.00	0.12	0.230	o	|	|	|	|	0.53
81.250	0.00	0.12	0.229	o	|	|	|	|	0.53
81.333	0.00	0.12	0.228	o	|	|	|	|	0.53
81.417	0.00	0.12	0.227	o	|	|	|	|	0.53
81.500	0.00	0.12	0.226	o	|	|	|	|	0.53
81.583	0.00	0.12	0.226	o	|	|	|	|	0.52
81.667	0.00	0.12	0.225	o	|	|	|	|	0.52
81.750	0.00	0.12	0.224	o	|	|	|	|	0.52
81.833	0.00	0.12	0.223	o	|	|	|	|	0.52
81.917	0.00	0.12	0.222	o	|	|	|	|	0.52
82.000	0.00	0.12	0.222	o	|	|	|	|	0.51
82.083	0.00	0.12	0.221	o	|	|	|	|	0.51
82.167	0.00	0.11	0.220	o	|	|	|	|	0.51
82.250	0.00	0.11	0.219	o	|	|	|	|	0.51
82.333	0.00	0.11	0.218	o	|	|	|	|	0.51
82.417	0.00	0.11	0.218	o	|	|	|	|	0.50
82.500	0.00	0.11	0.217	o	|	|	|	|	0.50
82.583	0.00	0.11	0.216	o	|	|	|	|	0.50
82.667	0.00	0.11	0.215	o	|	|	|	|	0.50
82.750	0.00	0.11	0.215	o	|	|	|	|	0.50
82.833	0.00	0.11	0.214	o	|	|	|	|	0.50
82.917	0.00	0.11	0.213	o	|	|	|	|	0.49
83.000	0.00	0.11	0.212	o	|	|	|	|	0.49
83.083	0.00	0.11	0.211	o	|	|	|	|	0.49
83.167	0.00	0.11	0.211	o	|	|	|	|	0.49
83.250	0.00	0.11	0.210	o	|	|	|	|	0.49
83.333	0.00	0.11	0.209	o	|	|	|	|	0.49
83.417	0.00	0.11	0.208	o	|	|	|	|	0.48
83.500	0.00	0.11	0.208	o	|	|	|	|	0.48
83.583	0.00	0.11	0.207	o	|	|	|	|	0.48
83.667	0.00	0.11	0.206	o	|	|	|	|	0.48
83.750	0.00	0.11	0.205	o	|	|	|	|	0.48
83.833	0.00	0.11	0.205	o	|	|	|	|	0.47
83.917	0.00	0.11	0.204	o	|	|	|	|	0.47
84.000	0.00	0.11	0.203	o	|	|	|	|	0.47
84.083	0.00	0.11	0.203	o	|	|	|	|	0.47
84.167	0.00	0.11	0.202	o	|	|	|	|	0.47
84.250	0.00	0.10	0.201	o	|	|	|	|	0.47
84.333	0.00	0.10	0.200	o	|	|	|	|	0.46
84.417	0.00	0.10	0.200	o	|	|	|	|	0.46
84.500	0.00	0.10	0.199	o	|	|	|	|	0.46
84.583	0.00	0.10	0.198	o	|	|	|	|	0.46
84.667	0.00	0.10	0.197	o	|	|	|	|	0.46
84.750	0.00	0.10	0.197	o	|	|	|	|	0.46
84.833	0.00	0.10	0.196	o	|	|	|	|	0.45
84.917	0.00	0.10	0.195	o	|	|	|	|	0.45
85.000	0.00	0.10	0.195	o	|	|	|	|	0.45
85.083	0.00	0.10	0.194	o	|	|	|	|	0.45
85.167	0.00	0.10	0.193	o	|	|	|	|	0.45
85.250	0.00	0.10	0.193	o	|	|	|	|	0.45
85.333	0.00	0.10	0.192	o	|	|	|	|	0.45
85.417	0.00	0.10	0.191	o	|	|	|	|	0.44

Remaining water in basin = 0.19 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 1025
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 26.244 (CFS)
Total volume = 12.097 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

Extended Detention Basin No. 3

Drainage Areas	Storm Event	Existing Condition		Developed		Routed Basin			Ex (cfs) +10% Difference Max
		Flow (cfs)	Volume (ac.ft.)	Flow (cfs)	Volume (ac.ft.)	Routed Basin Out Flow (cfs)	Storage Volume (ac.ft.)	Depth (ft)	
BASIN 3	2 Year - 1 Hour	7.278	0.1721	6.894	0.2016	0.047	0.199	0.66	-0.994
	2 Year - 3 Hour	3.502	0.1551	3.105	0.2663	0.061	0.259	0.85	-0.983
	2 Year - 6 Hour	3.066	0.1657	2.682	0.3599	0.102	0.344	1.10	-0.967
	2 Year - 24 Hour	0.256	0.1190	0.961	0.5842	0.193	0.463	1.42	-0.246
	5 Year - 1 Hour	10.731	0.2863	10.025	0.2926	0.068	0.289	0.95	-0.994
	5 Year - 3 Hour	5.413	0.2799	5.001	0.3820	0.123	0.371	1.18	-0.977
	5 Year - 6 Hour	5.089	0.3281	4.638	0.5264	0.220	0.499	1.51	-0.957
	5 Year - 24 Hour	1.057	0.2494	1.362	0.8275	0.325	0.635	1.87	-0.693
	10 Year - 1 Hour	14.359	0.2623	13.398	0.4082	0.147	0.402	1.26	-0.990
	10 Year - 3 Hour	7.874	0.6137	7.299	0.5237	0.227	0.507	1.54	-0.971
	10 Year - 6 Hour	7.636	0.7746	7.055	0.7245	0.361	0.683	2.00	-0.953
	10 Year - 24 Hour	2.538	0.9033	1.943	1.0226	1.204	0.693	2.02	-0.526
	100 Year - 1 Hour	23.036	0.7679	21.922	0.7108	0.942	0.690	2.02	-0.959
	100 Year - 3 Hour	12.675	1.0704	12.163	0.9216	6.846	0.763	2.19	-0.460
	100 Year - 6 Hour	12.721	1.4956	12.206	1.3023	10.362	0.806	2.29	-0.185
	100 Year - 24 Hour	4.550	1.8552	3.955	1.8482	3.864	0.726	2.10	-0.151

Basin 3 Size and Flow Calculations

BASIN 3

Horiz. : Vert.

4 : 1 = Basin Side Slope

	BASIN PARAMETERS					OUTLET								
Basin Elevation	Depth	Area S.F.	Volume C.F.	Volume AC-FT	Effective Volume AC-FT	Q1 Orifice Plate (cfs)	Q2 Orifice Plate (cfs)	Q3 Orifice Plate (cfs)	Q4 Orifice Plate (cfs)	Q5Orifice Plate (cfs)	Q6 Orifice Plate (cfs)	Q7Orifice Plate (cfs)	Q Weir 1 (cfs)	Q Total (cfs)
1266.00	0.00	12,107.00	0.00	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
1267.00	1.00	14,361.00	13,234.00	0.304	0.304	0.072	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.072
1268.00	2.00	17,657.00	29,764.00	0.683	0.683	0.110	0.000	0.250	0.000	0.000	0.000	0.000	0.000	0.361
1268.50	2.50	18,942.50	38,913.88	0.893	0.893	0.125	0.000	0.354	0.000	0.000	0.000	0.000	16.971	17.450
1269.00	3.00	20,228.00	48,706.50	1.118	1.118	0.138	0.000	0.433	0.000	0.000	0.000	0.000	48.000	48.572

SUPPORTING DESIGN PARAMETERS

Orifice Coefficient	0.66	Dia of Orifice	1.70		3.50					
Gravimetric Constant	32.2 ft/s^2	Eff Dia of Orifice	0.1417	0.0000	0.2917	0.0000	0.0000	0.0000	0.0000	
Number of Rows		Area of Orifice	0.0158	0.0000	0.0668	0.0000	0.0000	0.0000	0.0000	
Minimum Orifice Plate Height		Number of Orifeces	1	1	1	1	1	1	1	
Minimum Orifice Plate Width		Elev	1266.25		1267.5					

Weir	Sharp Crest Weir Coefficient	4	
	Length of Weir	12.00	
	Elev. at Crest of Weir	1268	

Q100 Elevation Weir Calc		
Basin 3 Weir Calc		
Crest Wier Elev.	1268.00	
Q100	26.48	cfs
Weir Length	12	
Weir Coeff.	4	
H Weir	0.67264	
Q100 Elevation	**1268.67**	

FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: PRO3212.rte
**********HYDROGRAPH DATA**********
Number of intervals = 17
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 6.894 (CFS)
Total volume = 0.202 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

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Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 17
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.304	0.072	0.304	0.304
2.000	0.683	0.361	0.682	0.684
2.500	0.893	17.450	0.833	0.953
3.000	1.118	48.572	0.951	1.285

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.7 3.45 5.17 6.89	Depth (Ft.)
0.083	0.27	0.00	0.001	OI	0.00
0.167	0.71	0.00	0.004	O I	0.01
0.250	0.91	0.00	0.010	O I	0.03
0.333	1.02	0.00	0.016	O I	0.05
0.417	1.13	0.01	0.024	O I	0.08
0.500	1.28	0.01	0.032	O I	0.11
0.583	1.46	0.01	0.041	O I	0.14
0.667	1.72	0.01	0.052	O I	0.17
0.750	2.67	0.02	0.067	O I	0.22
0.833	6.55	0.02	0.099	O I	0.33
0.917	6.89	0.03	0.145	O I	0.48
1.000	2.67	0.04	0.178	O I	0.58
1.083	1.28	0.05	0.191	O I	0.63
1.167	0.49	0.05	0.197	O I	0.65
1.250	0.19	0.05	0.199	O	0.65
1.333	0.04	0.05	0.199	O	0.66
1.417	0.01	0.05	0.199	O	0.65
1.500	0.00	0.05	0.199	O	0.65

Remaining water in basin = 0.20 (Ac.Ft)

```
**************************HYDROGRAPH DATA**************************
               Number of intervals =    18
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =        0.047 (CFS)
               Total volume =       0.003 (Ac.Ft)
        Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
        Peak (CFS)      0.000     0.000     0.000     0.000     0.000
        Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
*******************************************************************************

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                            Study date: 06/03/24

      ---------------------------------------------------------------------



      Program License Serial Number 5006

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      ********************* HYDROGRAPH INFORMATION **********************

                  From study/file name: PRO3232.rte
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =    41
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =        3.105 (CFS)
                  Total volume =       0.266 (Ac.Ft)
            Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      *********************************************************************



      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
      Process from Point/Station        1.000 to Point/Station        2.000
      **** RETARDING BASIN ROUTING ****
      ____________________________________________________________________

      User entry of depth-outflow-storage data
      ---------------------------------------------------------------------
      Total number of inflow hydrograph intervals = 41
      Hydrograph time unit =  5.000 (Min.)
      Initial depth in storage basin =   0.00(Ft.)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Initial basin depth =   0.00 (Ft.)
      Initial basin storage =      0.00 (Ac.Ft)
      Initial basin outflow =   0.00 (CFS)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Depth vs. Storage and Depth vs. Discharge data:
       Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
            (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
      ---------------------------------------------------------------------
         0.000      0.000      0.000      0.000        0.000
         1.000      0.304      0.072      0.304        0.304
         2.000      0.683      0.361      0.682        0.684
         2.500      0.893     17.450      0.833        0.953
         3.000      1.118     48.572      0.951        1.285
      ---------------------------------------------------------------------
                     Hydrograph Detention Basin Routing
      ---------------------------------------------------------------------

      Graph values: 'I'= unit inflow; 'O'=outflow at time shown
      ---------------------------------------------------------------------
       Time   Inflow  Outflow    Storage                                  Depth
      (Hours)  (CFS)   (CFS)     (Ac.Ft) .0       0.8    1.55    2.33    3.11 (Ft.)
       0.083    0.17    0.00      0.001  OI      |       |       |       |     0.00
       0.167    0.40    0.00      0.003  O   I   |       |       |       |     0.01
       0.250    0.43    0.00      0.005  O   I   |       |       |       |     0.02
       0.333    0.47    0.00      0.008  O   I   |       |       |       |     0.03
       0.417    0.54    0.00      0.012  O    I  |       |       |       |     0.04
       0.500    0.60    0.00      0.016  O     I |       |       |       |     0.05
       0.583    0.61    0.00      0.020  O     I |       |       |       |     0.07
       0.667    0.62    0.01      0.024  O     I |       |       |       |     0.08
       0.750    0.66    0.01      0.028  O     I |       |       |       |     0.09
       0.833    0.63    0.01      0.033  O     I |       |       |       |     0.11
       0.917    0.60    0.01      0.037  O     I |       |       |       |     0.12
       1.000    0.63    0.01      0.041  O     I |       |       |       |     0.14
       1.083    0.72    0.01      0.046  O      I|       |       |       |     0.15
       1.167    0.80    0.01      0.051  O       I       |       |       |     0.17
       1.250    0.82    0.01      0.056  O       I       |       |       |     0.19
       1.333    0.80    0.01      0.062  O       I       |       |       |     0.20
       1.417    0.85    0.02      0.067  O       I       |       |       |     0.22
       1.500    0.96    0.02      0.074  O       |I      |       |       |     0.24
       1.583    0.96    0.02      0.080  O       |I      |       |       |     0.26
       1.667    0.96    0.02      0.086  O       |I      |       |       |     0.28
       1.750    1.08    0.02      0.093  O       |  I    |       |       |     0.31
       1.833    1.17    0.02      0.101  O       |   I   |       |       |     0.33
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1.917    1.14    0.03      0.109  O       |  I    |       |       |     0.36
2.000    1.12    0.03      0.116  O       |  I    |       |       |     0.38
2.083    1.14    0.03      0.124  O       |  I    |       |       |     0.41
2.167    1.31    0.03      0.132  O       |    I  |       |       |     0.43
2.250    1.61    0.03      0.142  O       |       I       |       |     0.47
2.333    1.60    0.04      0.153  O       |       I       |       |     0.50
2.417    1.85    0.04      0.164  O       |         |  I    |       |     0.54
2.500    2.57    0.04      0.179  O       |         |       | I     |     0.59
2.583    3.11    0.05      0.198  O       |         |       |       I     0.65
2.667    2.99    0.05      0.219  O       |         |       |     I |     0.72
2.750    1.91    0.06      0.236  O       |         |  I    |       |     0.78
2.833    1.09    0.06      0.246  O       |  I      |       |       |     0.81
2.917    0.85    0.06      0.252  O       I         |       |       |     0.83
3.000    0.59    0.06      0.256  O     I |         |       |       |     0.84
3.083    0.25    0.06      0.259  O I     |         |       |       |     0.85
3.167    0.08    0.06      0.259  O       |         |       |       |     0.85
3.250    0.03    0.06      0.259  O       |         |       |       |     0.85
3.333    0.01    0.06      0.259  O       |         |       |       |     0.85
3.417    0.00    0.06      0.259  O       |         |       |       |     0.85
3.500    0.00    0.06      0.258  O       |         |       |       |     0.85

Remaining water in basin =    0.26 (Ac.Ft)

****************************HYDROGRAPH DATA****************************
               Number of intervals =    42
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =        0.061 (CFS)
               Total volume =       0.008 (Ac.Ft)
       Status of hydrographs being held in storage
                   Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
***********************************************************************

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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: PRO3262.rte
**********HYDROGRAPH DATA**********
Number of intervals = 77
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 2.682 (CFS)
Total volume = 0.360 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 77
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.304	0.072	0.304	0.304
2.000	0.683	0.361	0.682	0.684
2.500	0.893	17.450	0.833	0.953
3.000	1.118	48.572	0.951	1.285

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.7	1.34	2.01	2.68	Depth (Ft.)
0.083	0.09	0.00	0.000	OI	|	|	|	|	0.00
0.167	0.23	0.00	0.001	O I	|	|	|	|	0.00
0.250	0.28	0.00	0.003	O I	|	|	|	|	0.01
0.333	0.30	0.00	0.005	O I	|	|	|	|	0.02
0.417	0.31	0.00	0.007	O I	|	|	|	|	0.02
0.500	0.33	0.00	0.009	O I	|	|	|	|	0.03
0.583	0.35	0.00	0.012	O I	|	|	|	|	0.04
0.667	0.36	0.00	0.014	O I	|	|	|	|	0.05
0.750	0.36	0.00	0.017	O I	|	|	|	|	0.05
0.833	0.36	0.00	0.019	O I	|	|	|	|	0.06
0.917	0.36	0.01	0.022	O I	|	|	|	|	0.07
1.000	0.38	0.01	0.024	O I	|	|	|	|	0.08
1.083	0.41	0.01	0.027	O I	|	|	|	|	0.09
1.167	0.41	0.01	0.030	O I	|	|	|	|	0.10
1.250	0.41	0.01	0.032	O I	|	|	|	|	0.11
1.333	0.41	0.01	0.035	O I	|	|	|	|	0.12
1.417	0.41	0.01	0.038	O I	|	|	|	|	0.12
1.500	0.41	0.01	0.041	O I	|	|	|	|	0.13
1.583	0.41	0.01	0.043	O I	|	|	|	|	0.14
1.667	0.41	0.01	0.046	O I	|	|	|	|	0.15
1.750	0.41	0.01	0.049	O I	|	|	|	|	0.16
1.833	0.41	0.01	0.052	O I	|	|	|	|	0.17

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1.917    0.41    0.01      0.055  O   I   |        |        |        |      0.18
2.000    0.43    0.01      0.057  O    I  |        |        |        |      0.19
2.083    0.44    0.01      0.060  O    I  |        |        |        |      0.20
2.167    0.44    0.01      0.063  O    I  |        |        |        |      0.21
2.250    0.46    0.02      0.066  O    I  |        |        |        |      0.22
2.333    0.46    0.02      0.069  O    I  |        |        |        |      0.23
2.417    0.47    0.02      0.072  O    I  |        |        |        |      0.24
2.500    0.47    0.02      0.075  O    I  |        |        |        |      0.25
2.583    0.47    0.02      0.079  O    I  |        |        |        |      0.26
2.667    0.47    0.02      0.082  O    I  |        |        |        |      0.27
2.750    0.48    0.02      0.085  O    I  |        |        |        |      0.28
2.833    0.51    0.02      0.088  O     I |        |        |        |      0.29
2.917    0.51    0.02      0.091  O     I |        |        |        |      0.30
3.000    0.52    0.02      0.095  O     I |        |        |        |      0.31
3.083    0.52    0.02      0.098  O     I |        |        |        |      0.32
3.167    0.54    0.02      0.102  O     I |        |        |        |      0.33
3.250    0.56    0.02      0.105  O     I |        |        |        |      0.35
3.333    0.57    0.03      0.109  O     I |        |        |        |      0.36
3.417    0.59    0.03      0.113  O      I|        |        |        |      0.37
3.500    0.63    0.03      0.117  O      I|        |        |        |      0.38
3.583    0.68    0.03      0.121  O       I        |        |        |      0.40
3.667    0.71    0.03      0.126  O       I        |        |        |      0.41
3.750    0.74    0.03      0.130  O       I        |        |        |      0.43
3.833    0.77    0.03      0.135  O       |I       |        |        |      0.45
3.917    0.79    0.03      0.141  O       |I       |        |        |      0.46
4.000    0.82    0.03      0.146  O       |I       |        |        |      0.48
4.083    0.84    0.04      0.151  O       | I      |        |        |      0.50
4.167    0.89    0.04      0.157  O       | I      |        |        |      0.52
4.250    0.94    0.04      0.163  O       |  I     |        |        |      0.54
4.333    0.99    0.04      0.169  O       |  I     |        |        |      0.56
4.417    1.04    0.04      0.176  O       |   I    |        |        |      0.58
4.500    1.07    0.04      0.183  O       |   I    |        |        |      0.60
4.583    1.10    0.05      0.190  O       |    I   |        |        |      0.63
4.667    1.15    0.05      0.198  O       |    I   |        |        |      0.65
4.750    1.20    0.05      0.205  O       |     I  |        |        |      0.68
4.833    1.23    0.05      0.213  O       |     I  |        |        |      0.70
4.917    1.26    0.05      0.222  O       |     I  |        |        |      0.73
5.000    1.30    0.05      0.230  O       |      I |        |        |      0.76
5.083    1.42    0.06      0.239  O       |        |I       |        |      0.79
5.167    1.64    0.06      0.249  O       |        |  I     |        |      0.82
5.250    1.85    0.06      0.261  O       |        |     I  |        |      0.86
5.333    2.02    0.06      0.274  O       |        |        I        |      0.90
5.417    2.22    0.07      0.288  O       |        |        | I      |      0.95
5.500    2.68    0.07      0.304  O       |        |        |       I|      1.00
5.583    2.31    0.08      0.321  |O      |        |        |  I     |      1.04
5.667    1.16    0.09      0.332  |O      |    I   |        |        |      1.07
5.750    0.66    0.10      0.338  |O     I|        |        |        |      1.09
5.833    0.43    0.10      0.341  |O   I  |        |        |        |      1.10
5.917    0.28    0.10      0.343  |O I    |        |        |        |      1.10
6.000    0.17    0.10      0.344  |OI     |        |        |        |      1.10
6.083    0.09    0.10      0.344  |O      |        |        |        |      1.10
6.167    0.03    0.10      0.343  IO      |        |        |        |      1.10
6.250    0.01    0.10      0.343  IO      |        |        |        |      1.10
6.333    0.00    0.10      0.342  IO      |        |        |        |      1.10
6.417    0.00    0.10      0.342  IO      |        |        |        |      1.10
6.500    0.00    0.10      0.341  IO      |        |        |        |      1.10
6.583    0.00    0.10      0.340  IO      |        |        |        |      1.10

 Remaining water in basin =    0.34 (Ac.Ft)

 ****************************HYDROGRAPH DATA****************************
               Number of intervals =    79
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =        0.102 (CFS)
               Total volume =       0.020 (Ac.Ft)
        Status of hydrographs being held in storage
                    Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
        Peak (CFS)      0.000     0.000     0.000     0.000     0.000
        Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: PRO32242.rte
**********HYDROGRAPH DATA**********
Number of intervals = 293
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.961 (CFS)
Total volume = 0.584 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****
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User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 293
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

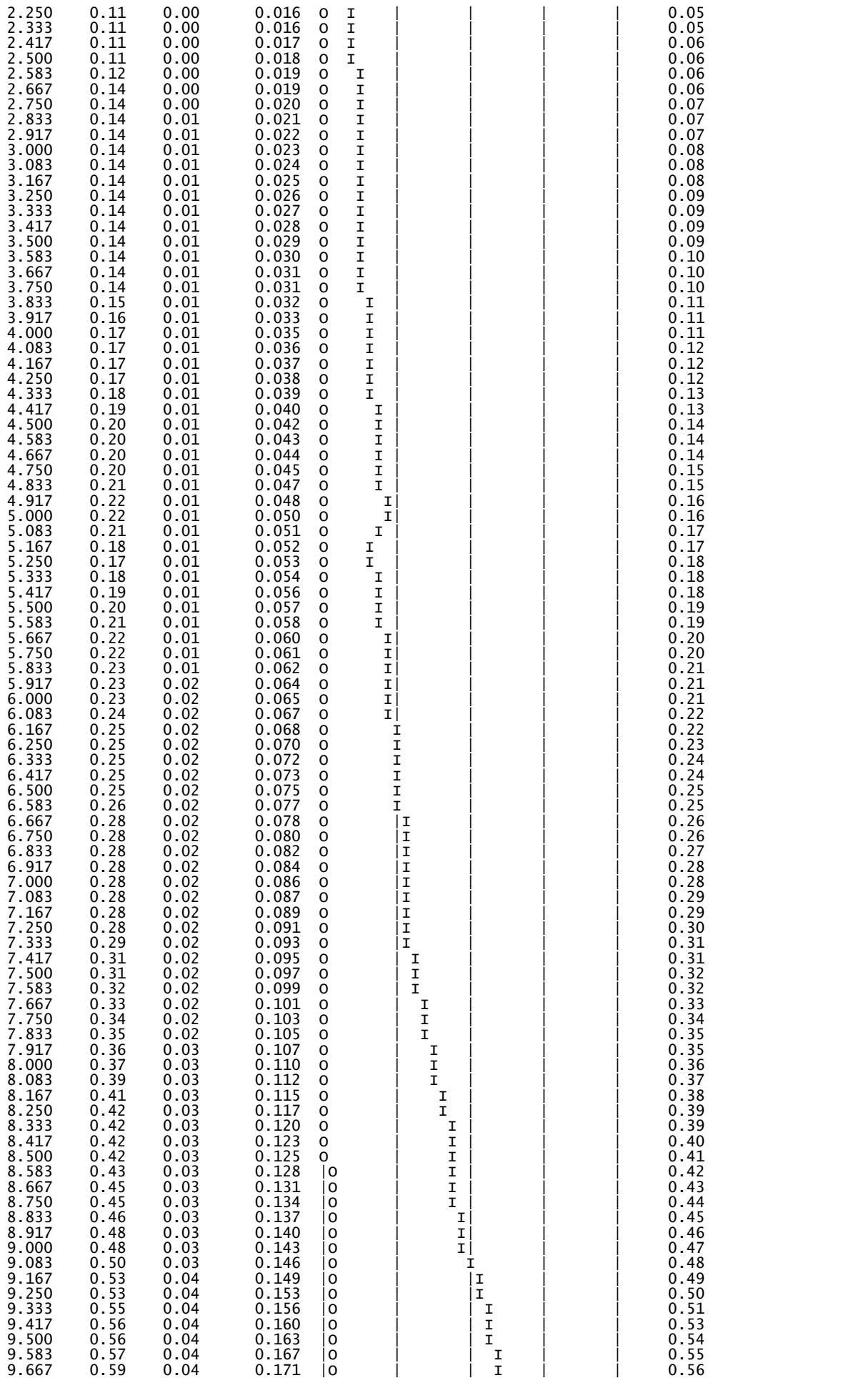
Depth vs. Storage and Depth vs. Discharge data:

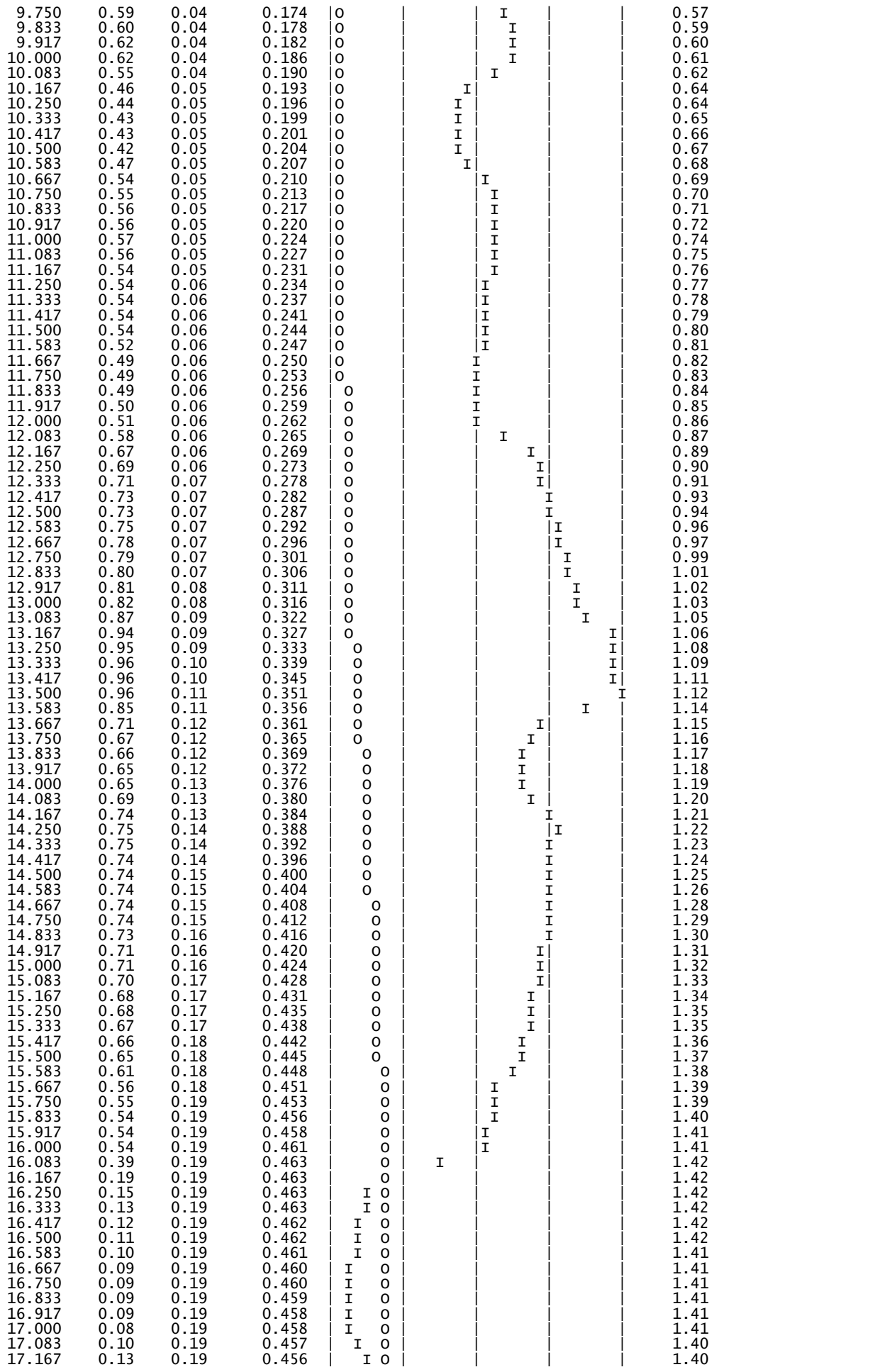
Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.304	0.072	0.304	0.304
2.000	0.683	0.361	0.682	0.684
2.500	0.893	17.450	0.833	0.953
3.000	1.118	48.572	0.951	1.285

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.2	0.48	0.72	0.96	Depth (Ft.)
0.083	0.02	0.00	0.000	O	|	|	|	|	0.00
0.167	0.05	0.00	0.000	OI	|	|	|	|	0.00
0.250	0.05	0.00	0.001	OI	|	|	|	|	0.00
0.333	0.06	0.00	0.001	O I	|	|	|	|	0.00
0.417	0.08	0.00	0.002	O I	|	|	|	|	0.01
0.500	0.08	0.00	0.002	O I	|	|	|	|	0.01
0.583	0.08	0.00	0.003	O I	|	|	|	|	0.01
0.667	0.08	0.00	0.003	O I	|	|	|	|	0.01
0.750	0.08	0.00	0.004	O I	|	|	|	|	0.01
0.833	0.09	0.00	0.004	O I	|	|	|	|	0.01
0.917	0.11	0.00	0.005	O I	|	|	|	|	0.02
1.000	0.11	0.00	0.006	O I	|	|	|	|	0.02
1.083	0.10	0.00	0.007	O I	|	|	|	|	0.02
1.167	0.09	0.00	0.007	O I	|	|	|	|	0.02
1.250	0.09	0.00	0.008	O I	|	|	|	|	0.03
1.333	0.09	0.00	0.008	O I	|	|	|	|	0.03
1.417	0.09	0.00	0.009	O I	|	|	|	|	0.03
1.500	0.08	0.00	0.010	O I	|	|	|	|	0.03
1.583	0.08	0.00	0.010	O I	|	|	|	|	0.03
1.667	0.08	0.00	0.011	O I	|	|	|	|	0.04
1.750	0.08	0.00	0.011	O I	|	|	|	|	0.04
1.833	0.09	0.00	0.012	O I	|	|	|	|	0.04
1.917	0.11	0.00	0.013	O I	|	|	|	|	0.04
2.000	0.11	0.00	0.013	O I	|	|	|	|	0.04
2.083	0.11	0.00	0.014	O I	|	|	|	|	0.05
2.167	0.11	0.00	0.015	O I	|	|	|	|	0.05





17.250	0.14	0.19	0.456	| I O |	|	|	|	1.40
17.333	0.14	0.19	0.456	| I O |	|	|	|	1.40
17.417	0.14	0.19	0.455	| I O |	|	|	|	1.40
17.500	0.14	0.19	0.455	| I O |	|	|	|	1.40
17.583	0.14	0.19	0.455	| I O |	|	|	|	1.40
17.667	0.14	0.19	0.454	| I O |	|	|	|	1.40
17.750	0.14	0.19	0.454	| I O |	|	|	|	1.40
17.833	0.13	0.19	0.454	| I O |	|	|	|	1.40
17.917	0.12	0.19	0.453	| I O |	|	|	|	1.39
18.000	0.12	0.19	0.453	| I O |	|	|	|	1.39
18.083	0.11	0.19	0.452	| I O |	|	|	|	1.39
18.167	0.11	0.18	0.452	| I O |	|	|	|	1.39
18.250	0.11	0.18	0.451	| I O |	|	|	|	1.39
18.333	0.11	0.18	0.451	| I O |	|	|	|	1.39
18.417	0.11	0.18	0.450	| I O |	|	|	|	1.39
18.500	0.11	0.18	0.450	| I O |	|	|	|	1.39
18.583	0.10	0.18	0.449	| I O |	|	|	|	1.38
18.667	0.09	0.18	0.449	| I O |	|	|	|	1.38
18.750	0.09	0.18	0.448	| I O |	|	|	|	1.38
18.833	0.08	0.18	0.447	| I O |	|	|	|	1.38
18.917	0.06	0.18	0.447	| I O |	|	|	|	1.38
19.000	0.06	0.18	0.446	| I O |	|	|	|	1.37
19.083	0.07	0.18	0.445	| I O |	|	|	|	1.37
19.167	0.08	0.18	0.444	| I O |	|	|	|	1.37
19.250	0.08	0.18	0.444	| I O |	|	|	|	1.37
19.333	0.09	0.18	0.443	| I O |	|	|	|	1.37
19.417	0.11	0.18	0.443	| I O |	|	|	|	1.37
19.500	0.11	0.18	0.442	| I O |	|	|	|	1.36
19.583	0.10	0.18	0.442	| I O |	|	|	|	1.36
19.667	0.09	0.18	0.441	| I O |	|	|	|	1.36
19.750	0.09	0.18	0.440	| I O |	|	|	|	1.36
19.833	0.08	0.18	0.440	| I O |	|	|	|	1.36
19.917	0.06	0.17	0.439	| I O |	|	|	|	1.36
20.000	0.06	0.17	0.438	| I O |	|	|	|	1.35
20.083	0.07	0.17	0.437	| I O |	|	|	|	1.35
20.167	0.08	0.17	0.437	| I O |	|	|	|	1.35
20.250	0.08	0.17	0.436	| I O |	|	|	|	1.35
20.333	0.08	0.17	0.436	| I O |	|	|	|	1.35
20.417	0.08	0.17	0.435	| I O |	|	|	|	1.35
20.500	0.08	0.17	0.434	| I O |	|	|	|	1.34
20.583	0.08	0.17	0.434	| I O |	|	|	|	1.34
20.667	0.08	0.17	0.433	| I O |	|	|	|	1.34
20.750	0.08	0.17	0.433	| I O |	|	|	|	1.34
20.833	0.07	0.17	0.432	| I O |	|	|	|	1.34
20.917	0.06	0.17	0.431	| I O |	|	|	|	1.34
21.000	0.06	0.17	0.430	| I O |	|	|	|	1.33
21.083	0.07	0.17	0.430	| I O |	|	|	|	1.33
21.167	0.08	0.17	0.429	| I O |	|	|	|	1.33
21.250	0.08	0.17	0.429	| I O |	|	|	|	1.33
21.333	0.07	0.17	0.428	| I O |	|	|	|	1.33
21.417	0.06	0.17	0.427	| I O |	|	|	|	1.33
21.500	0.06	0.17	0.427	| I O |	|	|	|	1.32
21.583	0.07	0.16	0.426	| I O |	|	|	|	1.32
21.667	0.08	0.16	0.425	| I O |	|	|	|	1.32
21.750	0.08	0.16	0.425	| I O |	|	|	|	1.32
21.833	0.07	0.16	0.424	| I O |	|	|	|	1.32
21.917	0.06	0.16	0.423	| I O |	|	|	|	1.31
22.000	0.06	0.16	0.423	| I O |	|	|	|	1.31
22.083	0.07	0.16	0.422	| I O |	|	|	|	1.31
22.167	0.08	0.16	0.421	| I O |	|	|	|	1.31
22.250	0.08	0.16	0.421	| I O |	|	|	|	1.31
22.333	0.07	0.16	0.420	| I O |	|	|	|	1.31
22.417	0.06	0.16	0.420	| I O |	|	|	|	1.31
22.500	0.06	0.16	0.419	| I O |	|	|	|	1.30
22.583	0.06	0.16	0.418	| I O |	|	|	|	1.30
22.667	0.06	0.16	0.418	| I O |	|	|	|	1.30
22.750	0.06	0.16	0.417	| I O |	|	|	|	1.30
22.833	0.06	0.16	0.416	| I O |	|	|	|	1.30
22.917	0.06	0.16	0.415	| I O |	|	|	|	1.29
23.000	0.06	0.16	0.415	| I O |	|	|	|	1.29
23.083	0.06	0.16	0.414	| I O |	|	|	|	1.29
23.167	0.06	0.16	0.413	| I O |	|	|	|	1.29
23.250	0.06	0.15	0.413	| I O |	|	|	|	1.29
23.333	0.06	0.15	0.412	| I O |	|	|	|	1.29
23.417	0.06	0.15	0.411	| I O |	|	|	|	1.28
23.500	0.06	0.15	0.411	| I O |	|	|	|	1.28
23.583	0.06	0.15	0.410	| I O |	|	|	|	1.28
23.667	0.06	0.15	0.409	| I O |	|	|	|	1.28
23.750	0.06	0.15	0.409	| I O |	|	|	|	1.28
23.833	0.06	0.15	0.408	| I O |	|	|	|	1.27
23.917	0.06	0.15	0.407	| I O |	|	|	|	1.27
24.000	0.06	0.15	0.407	| I O |	|	|	|	1.27
24.083	0.04	0.15	0.406	| I O |	|	|	|	1.27
24.167	0.01	0.15	0.405	I O |	|	|	|	1.27
24.250	0.00	0.15	0.404	I O |	|	|	|	1.26
24.333	0.00	0.15	0.403	I O |	|	|	|	1.26
24.417	0.00	0.15	0.402	I O |	|	|	|	1.26
24.500	0.00	0.15	0.401	I O |	|	|	|	1.26
24.583	0.00	0.15	0.400	I O |	|	|	|	1.25
24.667	0.00	0.14	0.399	I O |	|	|	|	1.25

24.750	0.00	0.14	0.398	I	O	|	|	|	|	1.25
24.833	0.00	0.14	0.397	I	O	|	|	|	|	1.25
24.917	0.00	0.14	0.396	I	O	|	|	|	|	1.24
25.000	0.00	0.14	0.395	I	O	|	|	|	|	1.24
25.083	0.00	0.14	0.394	I	O	|	|	|	|	1.24
25.167	0.00	0.14	0.393	I	O	|	|	|	|	1.24
25.250	0.00	0.14	0.392	I	O	|	|	|	|	1.23
25.333	0.00	0.14	0.391	I	O	|	|	|	|	1.23
25.417	0.00	0.14	0.390	I	O	|	|	|	|	1.23
25.500	0.00	0.14	0.389	I	O	|	|	|	|	1.23
25.583	0.00	0.14	0.389	I	O	|	|	|	|	1.22
25.667	0.00	0.14	0.388	I	O	|	|	|	|	1.22
25.750	0.00	0.14	0.387	I	O	|	|	|	|	1.22
25.833	0.00	0.13	0.386	I	O	|	|	|	|	1.22
25.917	0.00	0.13	0.385	I	O	|	|	|	|	1.21
26.000	0.00	0.13	0.384	I	O	|	|	|	|	1.21
26.083	0.00	0.13	0.383	I	O	|	|	|	|	1.21
26.167	0.00	0.13	0.382	I	O	|	|	|	|	1.21
26.250	0.00	0.13	0.381	I	O	|	|	|	|	1.20
26.333	0.00	0.13	0.380	I	O	|	|	|	|	1.20
26.417	0.00	0.13	0.379	I	O	|	|	|	|	1.20
26.500	0.00	0.13	0.378	I	O	|	|	|	|	1.20
26.583	0.00	0.13	0.378	I	O	|	|	|	|	1.19
26.667	0.00	0.13	0.377	I	O	|	|	|	|	1.19
26.750	0.00	0.13	0.376	I	O	|	|	|	|	1.19
26.833	0.00	0.13	0.375	I	O	|	|	|	|	1.19
26.917	0.00	0.13	0.374	I	O	|	|	|	|	1.19
27.000	0.00	0.12	0.373	I	O	|	|	|	|	1.18
27.083	0.00	0.12	0.372	I	O	|	|	|	|	1.18
27.167	0.00	0.12	0.372	I	O	|	|	|	|	1.18
27.250	0.00	0.12	0.371	I	O	|	|	|	|	1.18
27.333	0.00	0.12	0.370	I	O	|	|	|	|	1.17
27.417	0.00	0.12	0.369	I	O	|	|	|	|	1.17
27.500	0.00	0.12	0.368	I	O	|	|	|	|	1.17
27.583	0.00	0.12	0.367	I	O	|	|	|	|	1.17
27.667	0.00	0.12	0.367	I	O	|	|	|	|	1.16
27.750	0.00	0.12	0.366	I	O	|	|	|	|	1.16
27.833	0.00	0.12	0.365	I	O	|	|	|	|	1.16
27.917	0.00	0.12	0.364	I	O	|	|	|	|	1.16
28.000	0.00	0.12	0.363	I	O	|	|	|	|	1.16
28.083	0.00	0.12	0.362	I	O	|	|	|	|	1.15
28.167	0.00	0.12	0.362	I	O	|	|	|	|	1.15
28.250	0.00	0.12	0.361	I	O	|	|	|	|	1.15
28.333	0.00	0.11	0.360	I	O	|	|	|	|	1.15
28.417	0.00	0.11	0.359	I	O	|	|	|	|	1.15
28.500	0.00	0.11	0.358	I	O	|	|	|	|	1.14
28.583	0.00	0.11	0.358	I	O	|	|	|	|	1.14
28.667	0.00	0.11	0.357	I	O	|	|	|	|	1.14
28.750	0.00	0.11	0.356	I	O	|	|	|	|	1.14
28.833	0.00	0.11	0.355	I	O	|	|	|	|	1.14
28.917	0.00	0.11	0.355	I	O	|	|	|	|	1.13
29.000	0.00	0.11	0.354	I	O	|	|	|	|	1.13
29.083	0.00	0.11	0.353	I	O	|	|	|	|	1.13
29.167	0.00	0.11	0.352	I	O	|	|	|	|	1.13
29.250	0.00	0.11	0.352	I	O	|	|	|	|	1.13
29.333	0.00	0.11	0.351	I	O	|	|	|	|	1.12
29.417	0.00	0.11	0.350	I	O	|	|	|	|	1.12
29.500	0.00	0.11	0.349	I	O	|	|	|	|	1.12
29.583	0.00	0.11	0.349	I	O	|	|	|	|	1.12
29.667	0.00	0.11	0.348	I	O	|	|	|	|	1.12
29.750	0.00	0.10	0.347	I	O	|	|	|	|	1.11
29.833	0.00	0.10	0.346	I	O	|	|	|	|	1.11
29.917	0.00	0.10	0.346	I	O	|	|	|	|	1.11
30.000	0.00	0.10	0.345	I	O	|	|	|	|	1.11
30.083	0.00	0.10	0.344	I	O	|	|	|	|	1.11
30.167	0.00	0.10	0.344	I	O	|	|	|	|	1.10
30.250	0.00	0.10	0.343	I	O	|	|	|	|	1.10
30.333	0.00	0.10	0.342	I	O	|	|	|	|	1.10
30.417	0.00	0.10	0.342	I	O	|	|	|	|	1.10
30.500	0.00	0.10	0.341	I	O	|	|	|	|	1.10
30.583	0.00	0.10	0.340	I	O	|	|	|	|	1.10

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 367
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.193 (CFS)
Total volume = 0.244 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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FLOOD HYDROGRAPH ROUTING PROGRAM
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********** HYDROGRAPH INFORMATION **********

From study/file name: PRO3515.rte
**********HYDROGRAPH DATA**********
Number of intervals = 17
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 10.025 (CFS)
Total volume = 0.293 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 17
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.304	0.072	0.304	0.304
2.000	0.683	0.361	0.682	0.684
2.500	0.893	17.450	0.833	0.953
3.000	1.118	48.572	0.951	1.285

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 2.5 5.01 7.52 10.03	Depth (Ft.)
0.083	0.38	0.00	0.001	OI	0.00
0.167	0.97	0.00	0.006	O I	0.02
0.250	1.25	0.00	0.014	O I	0.04
0.333	1.40	0.01	0.023	O I	0.07
0.417	1.55	0.01	0.033	O I	0.11
0.500	1.76	0.01	0.044	O I	0.15
0.583	2.00	0.01	0.057	O I	0.19
0.667	2.49	0.02	0.072	O I	0.24
0.750	4.17	0.02	0.095	O I	0.31
0.833	9.80	0.03	0.143	O I	0.47
0.917	10.03	0.05	0.211	O I	0.69
1.000	3.83	0.06	0.258	O I	0.85
1.083	1.83	0.07	0.277	O I	0.91
1.167	0.70	0.07	0.286	O I	0.94
1.250	0.27	0.07	0.289	O	0.95
1.333	0.05	0.07	0.289	O	0.95
1.417	0.01	0.07	0.289	O	0.95
1.500	0.00	0.07	0.288	O	0.95

Remaining water in basin = 0.29 (Ac.Ft)

```
**************************HYDROGRAPH DATA**************************
               Number of intervals =    18
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =        0.068 (CFS)
               Total volume =       0.004 (Ac.Ft)
        Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
        Peak (CFS)      0.000     0.000     0.000     0.000     0.000
        Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
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                    FLOOD HYDROGRAPH ROUTING PROGRAM
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                            Study date: 06/03/24

      ---------------------------------------------------------------------



      Program License Serial Number 5006

      ---------------------------------------------------------------------
      ********************* HYDROGRAPH INFORMATION **********************

                  From study/file name: PRO3535.rte
      ****************************HYDROGRAPH DATA*****************************
                  Number of intervals =    41
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =        5.001 (CFS)
                  Total volume =       0.382 (Ac.Ft)
            Status of hydrographs being held in storage
                     Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
            Peak (CFS)      0.000     0.000     0.000     0.000     0.000
            Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      *************************************************************************



      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
      Process from Point/Station        1.000 to Point/Station        2.000
      **** RETARDING BASIN ROUTING ****
      _________________________________________________________________________

      User entry of depth-outflow-storage data
      ---------------------------------------------------------------------
      Total number of inflow hydrograph intervals = 41
      Hydrograph time unit =  5.000 (Min.)
      Initial depth in storage basin =   0.00(Ft.)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Initial basin depth =   0.00 (Ft.)
      Initial basin storage =      0.00 (Ac.Ft)
      Initial basin outflow =   0.00 (CFS)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Depth vs. Storage and Depth vs. Discharge data:
       Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
            (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
      ---------------------------------------------------------------------
        0.000      0.000      0.000      0.000        0.000
        1.000      0.304      0.072      0.304        0.304
        2.000      0.683      0.361      0.682        0.684
        2.500      0.893     17.450      0.833        0.953
        3.000      1.118     48.572      0.951        1.285
      ---------------------------------------------------------------------
                     Hydrograph Detention Basin Routing
      ---------------------------------------------------------------------

      Graph values: 'I'= unit inflow; 'O'=outflow at time shown
      ---------------------------------------------------------------------
       Time   Inflow  Outflow    Storage                                  Depth
      (Hours)  (CFS)   (CFS)     (Ac.Ft) .0       1.3    2.50    3.75    5.00 (Ft.)
       0.083    0.23    0.00      0.001  OI      |       |       |       |     0.00
       0.167    0.54    0.00      0.003  O  I    |       |       |       |     0.01
       0.250    0.58    0.00      0.007  O  I    |       |       |       |     0.02
       0.333    0.63    0.00      0.011  O   I   |       |       |       |     0.04
       0.417    0.73    0.00      0.016  O   I   |       |       |       |     0.05
       0.500    0.81    0.01      0.021  O    I  |       |       |       |     0.07
       0.583    0.83    0.01      0.027  O    I  |       |       |       |     0.09
       0.667    0.83    0.01      0.033  O    I  |       |       |       |     0.11
       0.750    0.90    0.01      0.038  O    I  |       |       |       |     0.13
       0.833    0.86    0.01      0.044  O    I  |       |       |       |     0.15
       0.917    0.81    0.01      0.050  O    I  |       |       |       |     0.16
       1.000    0.85    0.01      0.056  O    I  |       |       |       |     0.18
       1.083    0.97    0.01      0.062  O     I |       |       |       |     0.20
       1.167    1.07    0.02      0.069  O     I |       |       |       |     0.23
       1.250    1.10    0.02      0.076  O      I|       |       |       |     0.25
       1.333    1.08    0.02      0.084  O     I |       |       |       |     0.27
       1.417    1.14    0.02      0.091  O      I|       |       |       |     0.30
       1.500    1.29    0.02      0.099  O       I       |       |       |     0.33
       1.583    1.29    0.03      0.108  O       I       |       |       |     0.36
       1.667    1.29    0.03      0.117  O       I       |       |       |     0.38
       1.750    1.46    0.03      0.126  O       |I      |       |       |     0.41
       1.833    1.58    0.03      0.136  O       | I     |       |       |     0.45
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1.917	1.54	0.03	0.147	O	I					0.48
2.000	1.51	0.04	0.157	O	I					0.52
2.083	1.55	0.04	0.167	O	I					0.55
2.167	1.77	0.04	0.178	O	I					0.59
2.250	2.20	0.05	0.192	O	I					0.63
2.333	2.19	0.05	0.207	O	I					0.68
2.417	2.82	0.05	0.223	O	I					0.74
2.500	4.18	0.06	0.247	O	I					0.81
2.583	5.00	0.07	0.278	O	I					0.92
2.667	4.77	0.08	0.312	O	I					1.02
2.750	2.97	0.10	0.338	O	I					1.09
2.833	1.60	0.11	0.353	O	I					1.13
2.917	1.20	0.12	0.361	O	I					1.15
3.000	0.81	0.12	0.368	O	I					1.17
3.083	0.34	0.12	0.371	O I						1.18
3.167	0.11	0.12	0.371	O						1.18
3.250	0.04	0.12	0.371	O						1.18
3.333	0.02	0.12	0.370	O						1.18
3.417	0.00	0.12	0.370	O						1.17
3.500	0.00	0.12	0.369	O						1.17
3.583	0.00	0.12	0.368	O						1.17
3.667	0.00	0.12	0.367	O						1.17
3.750	0.00	0.12	0.366	O						1.16
3.833	0.00	0.12	0.365	O						1.16
3.917	0.00	0.12	0.365	O						1.16
4.000	0.00	0.12	0.364	O						1.16
4.083	0.00	0.12	0.363	O						1.16
4.167	0.00	0.12	0.362	O						1.15
4.250	0.00	0.12	0.361	O						1.15
4.333	0.00	0.12	0.361	O						1.15
4.417	0.00	0.11	0.360	O						1.15
4.500	0.00	0.11	0.359	O						1.15
4.583	0.00	0.11	0.358	O						1.14
4.667	0.00	0.11	0.357	O						1.14
4.750	0.00	0.11	0.357	O						1.14
4.833	0.00	0.11	0.356	O						1.14
4.917	0.00	0.11	0.355	O						1.13
5.000	0.00	0.11	0.354	O						1.13
5.083	0.00	0.11	0.354	O						1.13
5.167	0.00	0.11	0.353	O						1.13
5.250	0.00	0.11	0.352	O						1.13
5.333	0.00	0.11	0.351	O						1.13
5.417	0.00	0.11	0.351	O						1.12
5.500	0.00	0.11	0.350	O						1.12
5.583	0.00	0.11	0.349	O						1.12
5.667	0.00	0.11	0.348	O						1.12
5.750	0.00	0.11	0.348	O						1.12
5.833	0.00	0.10	0.347	O						1.11
5.917	0.00	0.10	0.346	O						1.11
6.000	0.00	0.10	0.346	O						1.11
6.083	0.00	0.10	0.345	O						1.11
6.167	0.00	0.10	0.344	O						1.11
6.250	0.00	0.10	0.343	O						1.10
6.333	0.00	0.10	0.343	O						1.10
6.417	0.00	0.10	0.342	O						1.10
6.500	0.00	0.10	0.341	O						1.10
6.583	0.00	0.10	0.341	O						1.10

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 79
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.123 (CFS)
Total volume = 0.042 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 06/03/24

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: PRO3565.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    77
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =        4.638 (CFS)
               Total volume =       0.526 (Ac.Ft)
       Status of hydrographs being held in storage
                 Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
*************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
____________________________________________________________________________

User entry of depth-outflow-storage data
---------------------------------------------------------------------
Total number of inflow hydrograph intervals = 77
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
---------------------------------------------------------------------
---------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
---------------------------------------------------------------------
---------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
---------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.304      0.072      0.304        0.304
   2.000      0.683      0.361      0.682        0.684
   2.500      0.893     17.450      0.833        0.953
   3.000      1.118     48.572      0.951        1.285
---------------------------------------------------------------------
               Hydrograph Detention Basin Routing
---------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
---------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                    Depth
(Hours)  (CFS)   (CFS)     (Ac.Ft) .0       1.2    2.32    3.48    4.64 (Ft.)
 0.083    0.13    0.00      0.000  O       |       |       |       |     0.00
 0.167    0.32    0.00      0.002  O I     |       |       |       |     0.01
 0.250    0.40    0.00      0.004  O I     |       |       |       |     0.01
 0.333    0.42    0.00      0.007  O I     |       |       |       |     0.02
 0.417    0.43    0.00      0.010  O I     |       |       |       |     0.03
 0.500    0.46    0.00      0.013  O  I    |       |       |       |     0.04
 0.583    0.50    0.00      0.016  O  I    |       |       |       |     0.05
 0.667    0.50    0.00      0.020  O  I    |       |       |       |     0.07
 0.750    0.51    0.01      0.023  O  I    |       |       |       |     0.08
 0.833    0.51    0.01      0.027  O  I    |       |       |       |     0.09
 0.917    0.51    0.01      0.030  O  I    |       |       |       |     0.10
 1.000    0.54    0.01      0.034  O  I    |       |       |       |     0.11
 1.083    0.57    0.01      0.038  O  I    |       |       |       |     0.12
 1.167    0.58    0.01      0.041  O  I    |       |       |       |     0.14
 1.250    0.58    0.01      0.045  O   I   |       |       |       |     0.15
 1.333    0.58    0.01      0.049  O   I   |       |       |       |     0.16
 1.417    0.58    0.01      0.053  O   I   |       |       |       |     0.18
 1.500    0.58    0.01      0.057  O   I   |       |       |       |     0.19
 1.583    0.58    0.01      0.061  O   I   |       |       |       |     0.20
 1.667    0.58    0.02      0.065  O   I   |       |       |       |     0.21
 1.750    0.58    0.02      0.069  O   I   |       |       |       |     0.23
 1.833    0.58    0.02      0.073  O   I   |       |       |       |     0.24
```

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1.917    0.58    0.02      0.077  O   I   |       |       |       |     0.25
2.000    0.61    0.02      0.081  O   I   |       |       |       |     0.27
2.083    0.62    0.02      0.085  O   I   |       |       |       |     0.28
2.167    0.62    0.02      0.089  O   I   |       |       |       |     0.29
2.250    0.65    0.02      0.093  O   I   |       |       |       |     0.31
2.333    0.65    0.02      0.097  O   I   |       |       |       |     0.32
2.417    0.65    0.02      0.102  O   I   |       |       |       |     0.33
2.500    0.65    0.03      0.106  O   I   |       |       |       |     0.35
2.583    0.66    0.03      0.110  O   I   |       |       |       |     0.36
2.667    0.66    0.03      0.115  O   I   |       |       |       |     0.38
2.750    0.68    0.03      0.119  O   I   |       |       |       |     0.39
2.833    0.71    0.03      0.124  O   I   |       |       |       |     0.41
2.917    0.72    0.03      0.128  O   I   |       |       |       |     0.42
3.000    0.73    0.03      0.133  O    I  |       |       |       |     0.44
3.083    0.73    0.03      0.138  O    I  |       |       |       |     0.45
3.167    0.75    0.03      0.143  O    I  |       |       |       |     0.47
3.250    0.79    0.04      0.148  O    I  |       |       |       |     0.49
3.333    0.80    0.04      0.153  O    I  |       |       |       |     0.50
3.417    0.82    0.04      0.158  O    I  |       |       |       |     0.52
3.500    0.89    0.04      0.164  O     I |       |       |       |     0.54
3.583    0.95    0.04      0.170  O     I |       |       |       |     0.56
3.667    1.00    0.04      0.177  O     I |       |       |       |     0.58
3.750    1.04    0.04      0.183  O      I|       |       |       |     0.60
3.833    1.08    0.05      0.190  O      I|       |       |       |     0.63
3.917    1.11    0.05      0.197  O      I|       |       |       |     0.65
4.000    1.15    0.05      0.205  O      I|       |       |       |     0.67
4.083    1.18    0.05      0.213  O       I       |       |       |     0.70
4.167    1.25    0.05      0.221  O       I       |       |       |     0.73
4.250    1.32    0.05      0.229  O       |I      |       |       |     0.75
4.333    1.39    0.06      0.238  O       |I      |       |       |     0.78
4.417    1.46    0.06      0.247  O       | I     |       |       |     0.81
4.500    1.51    0.06      0.257  O       | I     |       |       |     0.85
4.583    1.55    0.06      0.267  O       | I     |       |       |     0.88
4.667    1.61    0.07      0.278  O       |  I    |       |       |     0.91
4.750    1.68    0.07      0.289  O       |  I    |       |       |     0.95
4.833    1.73    0.07      0.300  O       |  I    |       |       |     0.99
4.917    1.76    0.08      0.311  O       |   I   |       |       |     1.02
5.000    1.83    0.09      0.323  O       |   I   |       |       |     1.05
5.083    2.00    0.10      0.336  O       |    I  |       |       |     1.08
5.167    2.36    0.11      0.350  O       |       I       |       |     1.12
5.250    2.79    0.12      0.367  O       |         I     |       |     1.17
5.333    3.22    0.14      0.387  O       |           I   |       |     1.22
5.417    3.76    0.15      0.410  |O      |           |   I       |     1.28
5.500    4.64    0.17      0.438  |O      |           |       I   |     1.35
5.583    3.85    0.20      0.466  |O      |           |    I      |     1.43
5.667    1.79    0.21      0.484  |O      |   I       |           |     1.47
5.750    1.00    0.22      0.492  |O    I |           |           |     1.50
5.833    0.63    0.22      0.496  |O  I   |           |           |     1.51
5.917    0.40    0.22      0.498  |OI     |           |           |     1.51
6.000    0.24    0.22      0.499  |O      |           |           |     1.51
6.083    0.12    0.22      0.498  IO      |           |           |     1.51
6.167    0.04    0.22      0.497  IO      |           |           |     1.51
6.250    0.01    0.22      0.496  IO      |           |           |     1.51
6.333    0.01    0.22      0.495  IO      |           |           |     1.50
6.417    0.00    0.22      0.493  IO      |           |           |     1.50
6.500    0.00    0.22      0.492  IO      |           |           |     1.50
6.583    0.00    0.21      0.490  IO      |           |           |     1.49
6.667    0.00    0.21      0.489  IO      |           |           |     1.49
6.750    0.00    0.21      0.487  IO      |           |           |     1.48
6.833    0.00    0.21      0.486  IO      |           |           |     1.48
6.917    0.00    0.21      0.484  IO      |           |           |     1.48
7.000    0.00    0.21      0.483  IO      |           |           |     1.47
7.083    0.00    0.21      0.482  IO      |           |           |     1.47
7.167    0.00    0.21      0.480  IO      |           |           |     1.46
7.250    0.00    0.21      0.479  IO      |           |           |     1.46
7.333    0.00    0.20      0.477  IO      |           |           |     1.46
7.417    0.00    0.20      0.476  IO      |           |           |     1.45
7.500    0.00    0.20      0.475  IO      |           |           |     1.45
7.583    0.00    0.20      0.473  IO      |           |           |     1.45
7.667    0.00    0.20      0.472  IO      |           |           |     1.44
7.750    0.00    0.20      0.470  IO      |           |           |     1.44
7.833    0.00    0.20      0.469  IO      |           |           |     1.44
7.917    0.00    0.20      0.468  IO      |           |           |     1.43
8.000    0.00    0.20      0.466  IO      |           |           |     1.43
8.083    0.00    0.19      0.465  IO      |           |           |     1.42
8.167    0.00    0.19      0.464  IO      |           |           |     1.42
8.250    0.00    0.19      0.462  IO      |           |           |     1.42
8.333    0.00    0.19      0.461  IO      |           |           |     1.41
8.417    0.00    0.19      0.460  IO      |           |           |     1.41
8.500    0.00    0.19      0.458  IO      |           |           |     1.41
8.583    0.00    0.19      0.457  IO      |           |           |     1.40
8.667    0.00    0.19      0.456  IO      |           |           |     1.40
8.750    0.00    0.19      0.454  IO      |           |           |     1.40
8.833    0.00    0.19      0.453  IO      |           |           |     1.39
8.917    0.00    0.18      0.452  IO      |           |           |     1.39
9.000    0.00    0.18      0.451  IO      |           |           |     1.39
```

9.083	0.00	0.18	0.449	IO				1.38
9.167	0.00	0.18	0.448	IO				1.38
9.250	0.00	0.18	0.447	IO				1.38
9.333	0.00	0.18	0.446	IO				1.37
9.417	0.00	0.18	0.444	IO				1.37
9.500	0.00	0.18	0.443	IO				1.37
9.583	0.00	0.18	0.442	IO				1.36
9.667	0.00	0.18	0.441	IO				1.36
9.750	0.00	0.18	0.440	IO				1.36
9.833	0.00	0.17	0.438	IO				1.35
9.917	0.00	0.17	0.437	IO				1.35
10.000	0.00	0.17	0.436	IO				1.35
10.083	0.00	0.17	0.435	IO				1.34
10.167	0.00	0.17	0.434	IO				1.34
10.250	0.00	0.17	0.432	IO				1.34
10.333	0.00	0.17	0.431	IO				1.34
10.417	0.00	0.17	0.430	IO				1.33
10.500	0.00	0.17	0.429	IO				1.33
10.583	0.00	0.17	0.428	IO				1.33
10.667	0.00	0.17	0.427	IO				1.32
10.750	0.00	0.16	0.425	IO				1.32
10.833	0.00	0.16	0.424	IO				1.32
10.917	0.00	0.16	0.423	IO				1.31
11.000	0.00	0.16	0.422	IO				1.31
11.083	0.00	0.16	0.421	IO				1.31
11.167	0.00	0.16	0.420	IO				1.31
11.250	0.00	0.16	0.419	IO				1.30
11.333	0.00	0.16	0.418	IO				1.30
11.417	0.00	0.16	0.417	IO				1.30
11.500	0.00	0.16	0.416	IO				1.29
11.583	0.00	0.16	0.414	IO				1.29
11.667	0.00	0.16	0.413	IO				1.29
11.750	0.00	0.15	0.412	IO				1.29
11.833	0.00	0.15	0.411	IO				1.28
11.917	0.00	0.15	0.410	IO				1.28
12.000	0.00	0.15	0.409	IO				1.28
12.083	0.00	0.15	0.408	IO				1.27
12.167	0.00	0.15	0.407	IO				1.27
12.250	0.00	0.15	0.406	IO				1.27
12.333	0.00	0.15	0.405	IO				1.27
12.417	0.00	0.15	0.404	IO				1.26
12.500	0.00	0.15	0.403	IO				1.26
12.583	0.00	0.15	0.402	IO				1.26
12.667	0.00	0.15	0.401	IO				1.26
12.750	0.00	0.15	0.400	IO				1.25
12.833	0.00	0.14	0.399	O				1.25
12.917	0.00	0.14	0.398	O				1.25
13.000	0.00	0.14	0.397	O				1.25
13.083	0.00	0.14	0.396	O				1.24
13.167	0.00	0.14	0.395	O				1.24
13.250	0.00	0.14	0.394	O				1.24
13.333	0.00	0.14	0.393	O				1.23
13.417	0.00	0.14	0.392	O				1.23
13.500	0.00	0.14	0.391	O				1.23
13.583	0.00	0.14	0.390	O				1.23
13.667	0.00	0.14	0.389	O				1.22
13.750	0.00	0.14	0.388	O				1.22
13.833	0.00	0.14	0.387	O				1.22
13.917	0.00	0.13	0.386	O				1.22
14.000	0.00	0.13	0.385	O				1.22
14.083	0.00	0.13	0.385	O				1.21
14.167	0.00	0.13	0.384	O				1.21
14.250	0.00	0.13	0.383	O				1.21
14.333	0.00	0.13	0.382	O				1.21
14.417	0.00	0.13	0.381	O				1.20
14.500	0.00	0.13	0.380	O				1.20
14.583	0.00	0.13	0.379	O				1.20
14.667	0.00	0.13	0.378	O				1.20
14.750	0.00	0.13	0.377	O				1.19
14.833	0.00	0.13	0.376	O				1.19
14.917	0.00	0.13	0.376	O				1.19
15.000	0.00	0.13	0.375	O				1.19
15.083	0.00	0.13	0.374	O				1.18
15.167	0.00	0.12	0.373	O				1.18
15.250	0.00	0.12	0.372	O				1.18
15.333	0.00	0.12	0.371	O				1.18
15.417	0.00	0.12	0.370	O				1.18
15.500	0.00	0.12	0.370	O				1.17
15.583	0.00	0.12	0.369	O				1.17
15.667	0.00	0.12	0.368	O				1.17
15.750	0.00	0.12	0.367	O				1.17
15.833	0.00	0.12	0.366	O				1.16
15.917	0.00	0.12	0.365	O				1.16
16.000	0.00	0.12	0.365	O				1.16
16.083	0.00	0.12	0.364	O				1.16
16.167	0.00	0.12	0.363	O				1.16

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16.250    0.00    0.12      0.362  o       |       |       |       |     1.15
16.333    0.00    0.12      0.361  o       |       |       |       |     1.15
16.417    0.00    0.12      0.361  o       |       |       |       |     1.15
16.500    0.00    0.11      0.360  o       |       |       |       |     1.15
16.583    0.00    0.11      0.359  o       |       |       |       |     1.15
16.667    0.00    0.11      0.358  o       |       |       |       |     1.14
16.750    0.00    0.11      0.357  o       |       |       |       |     1.14
16.833    0.00    0.11      0.357  o       |       |       |       |     1.14
16.917    0.00    0.11      0.356  o       |       |       |       |     1.14
17.000    0.00    0.11      0.355  o       |       |       |       |     1.14
17.083    0.00    0.11      0.354  o       |       |       |       |     1.13
17.167    0.00    0.11      0.354  o       |       |       |       |     1.13
17.250    0.00    0.11      0.353  o       |       |       |       |     1.13
17.333    0.00    0.11      0.352  o       |       |       |       |     1.13
17.417    0.00    0.11      0.351  o       |       |       |       |     1.13
17.500    0.00    0.11      0.351  o       |       |       |       |     1.12
17.583    0.00    0.11      0.350  o       |       |       |       |     1.12
17.667    0.00    0.11      0.349  o       |       |       |       |     1.12
17.750    0.00    0.11      0.348  o       |       |       |       |     1.12
17.833    0.00    0.11      0.348  o       |       |       |       |     1.12
17.917    0.00    0.10      0.347  o       |       |       |       |     1.11
18.000    0.00    0.10      0.346  o       |       |       |       |     1.11
18.083    0.00    0.10      0.346  o       |       |       |       |     1.11
18.167    0.00    0.10      0.345  o       |       |       |       |     1.11
18.250    0.00    0.10      0.344  o       |       |       |       |     1.11
18.333    0.00    0.10      0.343  o       |       |       |       |     1.10
18.417    0.00    0.10      0.343  o       |       |       |       |     1.10
18.500    0.00    0.10      0.342  o       |       |       |       |     1.10
18.583    0.00    0.10      0.341  o       |       |       |       |     1.10
18.667    0.00    0.10      0.341  o       |       |       |       |     1.10

 Remaining water in basin =    0.34 (Ac.Ft)

 ****************************HYDROGRAPH DATA****************************
                Number of intervals =   224
                Time interval =    5.0 (Min.)
                Maximum/Peak flow rate =        0.220 (CFS)
                Total volume =       0.186 (Ac.Ft)
         Status of hydrographs being held in storage
                    Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
         Peak (CFS)      0.000     0.000     0.000     0.000     0.000
         Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: PRO35245.rte
**********HYDROGRAPH DATA**********
Number of intervals = 293
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.362 (CFS)
Total volume = 0.828 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 293
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.304	0.072	0.304	0.304
2.000	0.683	0.361	0.682	0.684
2.500	0.893	17.450	0.833	0.953
3.000	1.118	48.572	0.951	1.285

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.3	0.68	1.02	1.36 (Ft.)	Depth
0.083	0.03	0.00	0.000	O	|	|	|	|	0.00
0.167	0.07	0.00	0.000	OI	|	|	|	|	0.00
0.250	0.07	0.00	0.001	OI	|	|	|	|	0.00
0.333	0.09	0.00	0.001	O I	|	|	|	|	0.00
0.417	0.11	0.00	0.002	O I	|	|	|	|	0.01
0.500	0.12	0.00	0.003	O I	|	|	|	|	0.01
0.583	0.12	0.00	0.004	O I	|	|	|	|	0.01
0.667	0.12	0.00	0.005	O I	|	|	|	|	0.02
0.750	0.12	0.00	0.005	O I	|	|	|	|	0.02
0.833	0.13	0.00	0.006	O I	|	|	|	|	0.02
0.917	0.15	0.00	0.007	O I	|	|	|	|	0.02
1.000	0.16	0.00	0.008	O I	|	|	|	|	0.03
1.083	0.14	0.00	0.009	O I	|	|	|	|	0.03
1.167	0.13	0.00	0.010	O I	|	|	|	|	0.03
1.250	0.12	0.00	0.011	O I	|	|	|	|	0.04
1.333	0.12	0.00	0.012	O I	|	|	|	|	0.04
1.417	0.12	0.00	0.013	O I	|	|	|	|	0.04
1.500	0.12	0.00	0.014	O I	|	|	|	|	0.04
1.583	0.12	0.00	0.014	O I	|	|	|	|	0.05
1.667	0.12	0.00	0.015	O I	|	|	|	|	0.05
1.750	0.12	0.00	0.016	O I	|	|	|	|	0.05
1.833	0.13	0.00	0.017	O I	|	|	|	|	0.06

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1.917    0.15    0.00      0.018  o  I    |       |       |       |      0.06
2.000    0.16    0.00      0.019  o  I    |       |       |       |      0.06
2.083    0.16    0.00      0.020  o  I    |       |       |       |      0.07
2.167    0.16    0.00      0.021  o  I    |       |       |       |      0.07
2.250    0.16    0.01      0.022  o  I    |       |       |       |      0.07
2.333    0.16    0.01      0.023  o  I    |       |       |       |      0.08
2.417    0.16    0.01      0.024  o  I    |       |       |       |      0.08
2.500    0.16    0.01      0.025  o  I    |       |       |       |      0.08
2.583    0.17    0.01      0.026  o   I   |       |       |       |      0.09
2.667    0.19    0.01      0.027  o   I   |       |       |       |      0.09
2.750    0.20    0.01      0.029  o   I   |       |       |       |      0.09
2.833    0.20    0.01      0.030  o   I   |       |       |       |      0.10
2.917    0.20    0.01      0.031  o   I   |       |       |       |      0.10
3.000    0.20    0.01      0.033  o   I   |       |       |       |      0.11
3.083    0.20    0.01      0.034  o   I   |       |       |       |      0.11
3.167    0.20    0.01      0.035  o   I   |       |       |       |      0.12
3.250    0.20    0.01      0.037  o   I   |       |       |       |      0.12
3.333    0.20    0.01      0.038  o   I   |       |       |       |      0.13
3.417    0.20    0.01      0.039  o   I   |       |       |       |      0.13
3.500    0.20    0.01      0.041  o   I   |       |       |       |      0.13
3.583    0.20    0.01      0.042  o   I   |       |       |       |      0.14
3.667    0.20    0.01      0.043  o   I   |       |       |       |      0.14
3.750    0.20    0.01      0.045  o   I   |       |       |       |      0.15
3.833    0.21    0.01      0.046  o    I  |       |       |       |      0.15
3.917    0.23    0.01      0.047  o    I  |       |       |       |      0.16
4.000    0.24    0.01      0.049  o    I  |       |       |       |      0.16
4.083    0.24    0.01      0.051  o    I  |       |       |       |      0.17
4.167    0.24    0.01      0.052  o    I  |       |       |       |      0.17
4.250    0.24    0.01      0.054  o    I  |       |       |       |      0.18
4.333    0.25    0.01      0.055  o    I  |       |       |       |      0.18
4.417    0.27    0.01      0.057  o     I |       |       |       |      0.19
4.500    0.28    0.01      0.059  o     I |       |       |       |      0.19
4.583    0.28    0.01      0.061  o     I |       |       |       |      0.20
4.667    0.28    0.01      0.062  o     I |       |       |       |      0.21
4.750    0.28    0.02      0.064  o     I |       |       |       |      0.21
4.833    0.29    0.02      0.066  o     I |       |       |       |      0.22
4.917    0.31    0.02      0.068  o      I|       |       |       |      0.22
5.000    0.32    0.02      0.070  o      I|       |       |       |      0.23
5.083    0.29    0.02      0.072  o     I |       |       |       |      0.24
5.167    0.25    0.02      0.074  o    I  |       |       |       |      0.24
5.250    0.25    0.02      0.076  o    I  |       |       |       |      0.25
5.333    0.26    0.02      0.077  o     I |       |       |       |      0.25
5.417    0.27    0.02      0.079  o     I |       |       |       |      0.26
5.500    0.28    0.02      0.081  o     I |       |       |       |      0.27
5.583    0.29    0.02      0.082  o     I |       |       |       |      0.27
5.667    0.31    0.02      0.084  o      I|       |       |       |      0.28
5.750    0.32    0.02      0.086  o      I|       |       |       |      0.28
5.833    0.32    0.02      0.088  o      I|       |       |       |      0.29
5.917    0.32    0.02      0.091  o      I|       |       |       |      0.30
6.000    0.32    0.02      0.093  o      I|       |       |       |      0.30
6.083    0.33    0.02      0.095  o      I|       |       |       |      0.31
6.167    0.35    0.02      0.097  o       I       |       |       |      0.32
6.250    0.36    0.02      0.099  o       I       |       |       |      0.33
6.333    0.36    0.02      0.101  o       I       |       |       |      0.33
6.417    0.36    0.02      0.104  o       I       |       |       |      0.34
6.500    0.36    0.03      0.106  o       I       |       |       |      0.35
6.583    0.37    0.03      0.108  o       I       |       |       |      0.36
6.667    0.39    0.03      0.111  o       |I      |       |       |      0.36
6.750    0.40    0.03      0.113  o       |I      |       |       |      0.37
6.833    0.40    0.03      0.116  o       |I      |       |       |      0.38
6.917    0.40    0.03      0.119  o       |I      |       |       |      0.39
7.000    0.40    0.03      0.121  o       |I      |       |       |      0.40
7.083    0.40    0.03      0.124  o       |I      |       |       |      0.41
7.167    0.40    0.03      0.126  o       |I      |       |       |      0.42
7.250    0.40    0.03      0.129  o       |I      |       |       |      0.42
7.333    0.41    0.03      0.131  o       |I      |       |       |      0.43
7.417    0.43    0.03      0.134  o       | I     |       |       |      0.44
7.500    0.44    0.03      0.137  o       | I     |       |       |      0.45
7.583    0.45    0.03      0.140  o       | I     |       |       |      0.46
7.667    0.47    0.03      0.143  o       |  I    |       |       |      0.47
7.750    0.48    0.03      0.146  o       |  I    |       |       |      0.48
7.833    0.49    0.04      0.149  o       |  I    |       |       |      0.49
7.917    0.51    0.04      0.152  o       |   I   |       |       |      0.50
8.000    0.52    0.04      0.155  o       |   I   |       |       |      0.51
8.083    0.55    0.04      0.159  o       |   I   |       |       |      0.52
8.167    0.59    0.04      0.162  o       |    I  |       |       |      0.53
8.250    0.59    0.04      0.166  o       |    I  |       |       |      0.55
8.333    0.60    0.04      0.170  o       |     I |       |       |      0.56
8.417    0.60    0.04      0.174  o       |     I |       |       |      0.57
8.500    0.60    0.04      0.178  o       |     I |       |       |      0.58
8.583    0.61    0.04      0.182  |o      |     I |       |       |      0.60
8.667    0.63    0.04      0.186  |o      |     I |       |       |      0.61
8.750    0.64    0.04      0.190  |o      |     I |       |       |      0.62
8.833    0.65    0.05      0.194  |o      |      I|       |       |      0.64
8.917    0.67    0.05      0.198  |o      |      I|       |       |      0.65
9.000    0.68    0.05      0.202  |o      |      I|       |       |      0.67
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 9.083    0.71    0.05      0.207  |O       |        I       |        |     0.68
 9.167    0.75    0.05      0.211  |O       |        |I      |        |     0.70
 9.250    0.75    0.05      0.216  |O       |        |I      |        |     0.71
 9.333    0.77    0.05      0.221  |O       |        | I     |        |     0.73
 9.417    0.79    0.05      0.226  |O       |        | I     |        |     0.74
 9.500    0.80    0.05      0.231  |O       |        | I     |        |     0.76
 9.583    0.81    0.06      0.236  |O       |        |  I    |        |     0.78
 9.667    0.83    0.06      0.242  |O       |        |  I    |        |     0.80
 9.750    0.84    0.06      0.247  |O       |        |  I    |        |     0.81
 9.833    0.85    0.06      0.253  |O       |        |   I   |        |     0.83
 9.917    0.87    0.06      0.258  |O       |        |   I   |        |     0.85
10.000    0.88    0.06      0.264  |O       |        |   I   |        |     0.87
10.083    0.78    0.06      0.269  |O       |        | I     |        |     0.88
10.167    0.65    0.06      0.273  |O       |       I|       |        |     0.90
10.250    0.62    0.07      0.277  |O       |      I |       |        |     0.91
10.333    0.61    0.07      0.281  |O       |      I |       |        |     0.92
10.417    0.60    0.07      0.285  |O       |      I |       |        |     0.94
10.500    0.60    0.07      0.289  |O       |      I |       |        |     0.95
10.583    0.67    0.07      0.292  |O       |       I|       |        |     0.96
10.667    0.76    0.07      0.297  |O       |        |I      |        |     0.98
10.750    0.79    0.07      0.302  |O       |        | I     |        |     0.99
10.833    0.79    0.07      0.307  |O       |        | I     |        |     1.01
10.917    0.80    0.08      0.312  |O       |        | I     |        |     1.02
11.000    0.80    0.08      0.317  |O       |        | I     |        |     1.03
11.083    0.79    0.09      0.322  | O      |        | I     |        |     1.05
11.167    0.77    0.09      0.326  | O      |        | I     |        |     1.06
11.250    0.76    0.09      0.331  | O      |        |I      |        |     1.07
11.333    0.76    0.10      0.336  | O      |        |I      |        |     1.08
11.417    0.76    0.10      0.340  | O      |        |I      |        |     1.10
11.500    0.76    0.10      0.345  | O      |        |I      |        |     1.11
11.583    0.73    0.11      0.349  | O      |        |I      |        |     1.12
11.667    0.70    0.11      0.353  | O      |        I       |        |     1.13
11.750    0.69    0.11      0.357  | O      |        I       |        |     1.14
11.833    0.70    0.12      0.361  | O      |        I       |        |     1.15
11.917    0.71    0.12      0.365  | O      |        I       |        |     1.16
12.000    0.72    0.12      0.369  | O      |        I       |        |     1.17
12.083    0.82    0.13      0.374  | O      |        |  I    |        |     1.18
12.167    0.95    0.13      0.379  |  O     |        |    I  |        |     1.20
12.250    0.98    0.13      0.385  |  O     |        |     I |        |     1.21
12.333    1.01    0.14      0.391  |  O     |        |     I |        |     1.23
12.417    1.03    0.14      0.397  |  O     |        |      I        |     1.24
12.500    1.04    0.15      0.403  |  O     |        |      I        |     1.26
12.583    1.07    0.15      0.409  |  O     |        |       |I      |     1.28
12.667    1.11    0.16      0.416  |  O     |        |       |I      |     1.29
12.750    1.12    0.16      0.422  |  O     |        |       | I     |     1.31
12.833    1.13    0.17      0.429  |  O     |        |       | I     |     1.33
12.917    1.15    0.17      0.435  |   O    |        |       |  I    |     1.35
13.000    1.16    0.18      0.442  |   O    |        |       |  I    |     1.36
13.083    1.23    0.18      0.449  |   O    |        |       |   I   |     1.38
13.167    1.32    0.19      0.457  |   O    |        |       |      I|     1.40
13.250    1.35    0.19      0.465  |   O    |        |       |      I|     1.42
13.333    1.36    0.20      0.472  |   O    |        |       |      I|     1.44
13.417    1.36    0.21      0.480  |   O    |        |       |      I|     1.47
13.500    1.36    0.21      0.488  |   O    |        |       |       I     1.49
13.583    1.21    0.22      0.496  |    O   |        |       |   I   |     1.51
13.667    1.00    0.22      0.502  |    O   |        |      I|       |     1.52
13.750    0.96    0.23      0.507  |    O   |        |     I |       |     1.54
13.833    0.94    0.23      0.512  |    O   |        |    I  |       |     1.55
13.917    0.93    0.23      0.517  |    O   |        |    I  |       |     1.56
14.000    0.92    0.24      0.521  |    O   |        |    I  |       |     1.57
14.083    0.98    0.24      0.526  |    O   |        |     I |       |     1.59
14.167    1.05    0.25      0.532  |    O   |        |       I       |     1.60
14.250    1.07    0.25      0.537  |    O   |        |       |I      |     1.62
14.333    1.06    0.25      0.543  |    O   |        |       I       |     1.63
14.417    1.05    0.26      0.548  |     O  |        |       I       |     1.64
14.500    1.04    0.26      0.554  |     O  |        |       I       |     1.66
14.583    1.04    0.27      0.559  |     O  |        |       I       |     1.67
14.667    1.04    0.27      0.564  |     O  |        |       I       |     1.69
14.750    1.04    0.27      0.570  |     O  |        |       I       |     1.70
14.833    1.03    0.28      0.575  |     O  |        |       I       |     1.72
14.917    1.01    0.28      0.580  |     O  |        |      I|       |     1.73
15.000    1.00    0.29      0.585  |     O  |        |      I|       |     1.74
15.083    0.99    0.29      0.590  |     O  |        |      I|       |     1.75
15.167    0.97    0.29      0.595  |     O  |        |     I |       |     1.77
15.250    0.96    0.30      0.599  |     O  |        |     I |       |     1.78
15.333    0.95    0.30      0.604  |      O |        |     I |       |     1.79
15.417    0.93    0.30      0.608  |      O |        |    I  |       |     1.80
15.500    0.92    0.31      0.612  |      O |        |    I  |       |     1.81
15.583    0.87    0.31      0.617  |      O |        |   I   |       |     1.82
15.667    0.79    0.31      0.620  |      O |        | I     |       |     1.83
15.750    0.77    0.32      0.623  |      O |        | I     |       |     1.84
15.833    0.77    0.32      0.626  |      O |        | I     |       |     1.85
15.917    0.76    0.32      0.629  |      O |        |I      |       |     1.86
16.000    0.76    0.32      0.633  |      O |        |I      |       |     1.87
16.083    0.55    0.32      0.635  |      O |   I    |       |       |     1.87
16.167    0.27    0.32      0.635  |     IO |        |       |       |     1.87
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16.250	0.21	0.32	0.635	| I O|	|	|	|	1.87
16.333	0.18	0.32	0.634	| I O|	|	|	|	1.87
16.417	0.17	0.32	0.633	| I O|	|	|	|	1.87
16.500	0.16	0.32	0.632	| I O|	|	|	|	1.86
16.583	0.15	0.32	0.631	| I O|	|	|	|	1.86
16.667	0.13	0.32	0.629	| I O|	|	|	|	1.86
16.750	0.12	0.32	0.628	| I O|	|	|	|	1.85
16.833	0.12	0.32	0.627	| I O|	|	|	|	1.85
16.917	0.12	0.32	0.625	| I O|	|	|	|	1.85
17.000	0.12	0.32	0.624	| I O|	|	|	|	1.84
17.083	0.15	0.32	0.623	| I O|	|	|	|	1.84
17.167	0.19	0.31	0.622	| I O|	|	|	|	1.84
17.250	0.19	0.31	0.621	| I O|	|	|	|	1.84
17.333	0.20	0.31	0.620	| I O|	|	|	|	1.83
17.417	0.20	0.31	0.619	| I O|	|	|	|	1.83
17.500	0.20	0.31	0.618	| I O|	|	|	|	1.83
17.583	0.20	0.31	0.618	| I O|	|	|	|	1.83
17.667	0.20	0.31	0.617	| I O|	|	|	|	1.83
17.750	0.20	0.31	0.616	| I O|	|	|	|	1.82
17.833	0.19	0.31	0.615	| I O|	|	|	|	1.82
17.917	0.17	0.31	0.614	| I O|	|	|	|	1.82
18.000	0.16	0.31	0.613	| I O|	|	|	|	1.82
18.083	0.16	0.31	0.612	| I O|	|	|	|	1.81
18.167	0.16	0.31	0.611	| I O|	|	|	|	1.81
18.250	0.16	0.31	0.610	| I O|	|	|	|	1.81
18.333	0.16	0.30	0.609	| I O|	|	|	|	1.81
18.417	0.16	0.30	0.608	| I O|	|	|	|	1.80
18.500	0.16	0.30	0.607	| I O|	|	|	|	1.80
18.583	0.15	0.30	0.606	| I O|	|	|	|	1.80
18.667	0.13	0.30	0.605	| I O|	|	|	|	1.80
18.750	0.12	0.30	0.604	| I O|	|	|	|	1.79
18.833	0.11	0.30	0.603	| I O|	|	|	|	1.79
18.917	0.09	0.30	0.601	| I O|	|	|	|	1.78
19.000	0.08	0.30	0.600	|I O |	|	|	|	1.78
19.083	0.10	0.30	0.599	| I O |	|	|	|	1.78
19.167	0.11	0.30	0.597	| I O |	|	|	|	1.77
19.250	0.12	0.29	0.596	| I O |	|	|	|	1.77
19.333	0.13	0.29	0.595	| I O |	|	|	|	1.77
19.417	0.15	0.29	0.594	| I O |	|	|	|	1.76
19.500	0.16	0.29	0.593	| I O |	|	|	|	1.76
19.583	0.14	0.29	0.592	| I O |	|	|	|	1.76
19.667	0.13	0.29	0.591	| I O |	|	|	|	1.76
19.750	0.12	0.29	0.590	| I O |	|	|	|	1.75
19.833	0.11	0.29	0.588	| I O |	|	|	|	1.75
19.917	0.09	0.29	0.587	| I O |	|	|	|	1.75
20.000	0.08	0.29	0.586	|I O |	|	|	|	1.74
20.083	0.10	0.29	0.584	| I O |	|	|	|	1.74
20.167	0.11	0.28	0.583	| I O |	|	|	|	1.74
20.250	0.12	0.28	0.582	| I O |	|	|	|	1.73
20.333	0.12	0.28	0.581	| I O |	|	|	|	1.73
20.417	0.12	0.28	0.580	| I O |	|	|	|	1.73
20.500	0.12	0.28	0.579	| I O |	|	|	|	1.72
20.583	0.12	0.28	0.577	| I O |	|	|	|	1.72
20.667	0.12	0.28	0.576	| I O |	|	|	|	1.72
20.750	0.12	0.28	0.575	| I O |	|	|	|	1.72
20.833	0.11	0.28	0.574	| I O |	|	|	|	1.71
20.917	0.09	0.28	0.573	| I O |	|	|	|	1.71
21.000	0.08	0.28	0.572	|I O |	|	|	|	1.71
21.083	0.10	0.28	0.570	| I O |	|	|	|	1.70
21.167	0.11	0.27	0.569	| I O |	|	|	|	1.70
21.250	0.12	0.27	0.568	| I O |	|	|	|	1.70
21.333	0.10	0.27	0.567	| I O |	|	|	|	1.69
21.417	0.09	0.27	0.566	| I O |	|	|	|	1.69
21.500	0.08	0.27	0.564	|I O |	|	|	|	1.69
21.583	0.10	0.27	0.563	| I O |	|	|	|	1.68
21.667	0.11	0.27	0.562	| I O |	|	|	|	1.68
21.750	0.12	0.27	0.561	| I O |	|	|	|	1.68
21.833	0.10	0.27	0.560	| I O |	|	|	|	1.68
21.917	0.09	0.27	0.559	| I O |	|	|	|	1.67
22.000	0.08	0.27	0.558	|I O |	|	|	|	1.67
22.083	0.10	0.26	0.556	| I O |	|	|	|	1.67
22.167	0.11	0.26	0.555	| I O |	|	|	|	1.66
22.250	0.12	0.26	0.554	| I O |	|	|	|	1.66
22.333	0.10	0.26	0.553	| I O |	|	|	|	1.66
22.417	0.09	0.26	0.552	| I O |	|	|	|	1.65
22.500	0.08	0.26	0.551	|I O |	|	|	|	1.65
22.583	0.08	0.26	0.550	|I O |	|	|	|	1.65
22.667	0.08	0.26	0.548	|I O |	|	|	|	1.64
22.750	0.08	0.26	0.547	|I O |	|	|	|	1.64
22.833	0.08	0.26	0.546	|I O |	|	|	|	1.64
22.917	0.08	0.26	0.545	|I O |	|	|	|	1.64
23.000	0.08	0.25	0.543	|I O |	|	|	|	1.63
23.083	0.08	0.25	0.542	|I O |	|	|	|	1.63
23.167	0.08	0.25	0.541	|I O |	|	|	|	1.63
23.250	0.08	0.25	0.540	|I O |	|	|	|	1.62
23.333	0.08	0.25	0.539	|I O |	|	|	|	1.62

23.417	0.08	0.25	0.538	|I o	|	|	|	|	1.62
23.500	0.08	0.25	0.536	|I o	|	|	|	|	1.61
23.583	0.08	0.25	0.535	|I o	|	|	|	|	1.61
23.667	0.08	0.25	0.534	|I o	|	|	|	|	1.61
23.750	0.08	0.25	0.533	|I o	|	|	|	|	1.60
23.833	0.08	0.25	0.532	|I o	|	|	|	|	1.60
23.917	0.08	0.24	0.531	|I o	|	|	|	|	1.60
24.000	0.08	0.24	0.530	|I o	|	|	|	|	1.59
24.083	0.05	0.24	0.528	|I o	|	|	|	|	1.59
24.167	0.01	0.24	0.527	I o	|	|	|	|	1.59
24.250	0.01	0.24	0.525	I o	|	|	|	|	1.58
24.333	0.00	0.24	0.524	I o	|	|	|	|	1.58
24.417	0.00	0.24	0.522	I o	|	|	|	|	1.58
24.500	0.00	0.24	0.520	I o	|	|	|	|	1.57
24.583	0.00	0.24	0.519	I o	|	|	|	|	1.57
24.667	0.00	0.23	0.517	I o	|	|	|	|	1.56
24.750	0.00	0.23	0.516	I o	|	|	|	|	1.56
24.833	0.00	0.23	0.514	I o	|	|	|	|	1.55
24.917	0.00	0.23	0.512	I o	|	|	|	|	1.55
25.000	0.00	0.23	0.511	I o	|	|	|	|	1.55
25.083	0.00	0.23	0.509	I o	|	|	|	|	1.54
25.167	0.00	0.23	0.508	I o	|	|	|	|	1.54
25.250	0.00	0.23	0.506	I o	|	|	|	|	1.53
25.333	0.00	0.22	0.504	I o	|	|	|	|	1.53
25.417	0.00	0.22	0.503	I o	|	|	|	|	1.52
25.500	0.00	0.22	0.501	I o	|	|	|	|	1.52
25.583	0.00	0.22	0.500	I o	|	|	|	|	1.52
25.667	0.00	0.22	0.498	I o	|	|	|	|	1.51
25.750	0.00	0.22	0.497	I o	|	|	|	|	1.51
25.833	0.00	0.22	0.495	I o	|	|	|	|	1.50
25.917	0.00	0.22	0.494	I o	|	|	|	|	1.50
26.000	0.00	0.22	0.492	I o	|	|	|	|	1.50
26.083	0.00	0.21	0.491	I o	|	|	|	|	1.49
26.167	0.00	0.21	0.489	I o	|	|	|	|	1.49
26.250	0.00	0.21	0.488	I o	|	|	|	|	1.49
26.333	0.00	0.21	0.486	I o	|	|	|	|	1.48
26.417	0.00	0.21	0.485	I o	|	|	|	|	1.48
26.500	0.00	0.21	0.484	I o	|	|	|	|	1.47
26.583	0.00	0.21	0.482	I o	|	|	|	|	1.47
26.667	0.00	0.21	0.481	I o	|	|	|	|	1.47
26.750	0.00	0.21	0.479	I o	|	|	|	|	1.46
26.833	0.00	0.20	0.478	I o	|	|	|	|	1.46
26.917	0.00	0.20	0.476	I o	|	|	|	|	1.46
27.000	0.00	0.20	0.475	I o	|	|	|	|	1.45
27.083	0.00	0.20	0.474	I o	|	|	|	|	1.45
27.167	0.00	0.20	0.472	I o	|	|	|	|	1.44
27.250	0.00	0.20	0.471	I o	|	|	|	|	1.44
27.333	0.00	0.20	0.470	I o	|	|	|	|	1.44
27.417	0.00	0.20	0.468	I o	|	|	|	|	1.43
27.500	0.00	0.20	0.467	I o	|	|	|	|	1.43
27.583	0.00	0.20	0.465	I o	|	|	|	|	1.43
27.667	0.00	0.19	0.464	I o	|	|	|	|	1.42
27.750	0.00	0.19	0.463	I o	|	|	|	|	1.42
27.833	0.00	0.19	0.461	I o	|	|	|	|	1.42
27.917	0.00	0.19	0.460	I o	|	|	|	|	1.41
28.000	0.00	0.19	0.459	I o	|	|	|	|	1.41
28.083	0.00	0.19	0.458	I o	|	|	|	|	1.41
28.167	0.00	0.19	0.456	I o	|	|	|	|	1.40
28.250	0.00	0.19	0.455	I o	|	|	|	|	1.40
28.333	0.00	0.19	0.454	I o	|	|	|	|	1.39
28.417	0.00	0.19	0.452	I o	|	|	|	|	1.39
28.500	0.00	0.18	0.451	I o	|	|	|	|	1.39
28.583	0.00	0.18	0.450	I o	|	|	|	|	1.38
28.667	0.00	0.18	0.449	I o	|	|	|	|	1.38
28.750	0.00	0.18	0.447	I o	|	|	|	|	1.38
28.833	0.00	0.18	0.446	I o	|	|	|	|	1.37
28.917	0.00	0.18	0.445	I o	|	|	|	|	1.37
29.000	0.00	0.18	0.444	I o	|	|	|	|	1.37
29.083	0.00	0.18	0.442	I o	|	|	|	|	1.37
29.167	0.00	0.18	0.441	I o	|	|	|	|	1.36
29.250	0.00	0.18	0.440	I o	|	|	|	|	1.36
29.333	0.00	0.17	0.439	I o	|	|	|	|	1.36
29.417	0.00	0.17	0.438	I o	|	|	|	|	1.35
29.500	0.00	0.17	0.436	I o	|	|	|	|	1.35
29.583	0.00	0.17	0.435	I o	|	|	|	|	1.35
29.667	0.00	0.17	0.434	I o	|	|	|	|	1.34
29.750	0.00	0.17	0.433	I o	|	|	|	|	1.34
29.833	0.00	0.17	0.432	I o	|	|	|	|	1.34
29.917	0.00	0.17	0.430	I o	|	|	|	|	1.33
30.000	0.00	0.17	0.429	I o	|	|	|	|	1.33
30.083	0.00	0.17	0.428	I o	|	|	|	|	1.33
30.167	0.00	0.17	0.427	I o	|	|	|	|	1.32
30.250	0.00	0.16	0.426	I o	|	|	|	|	1.32
30.333	0.00	0.16	0.425	I o	|	|	|	|	1.32
30.417	0.00	0.16	0.424	I o	|	|	|	|	1.32
30.500	0.00	0.16	0.423	I o	|	|	|	|	1.31

30.583	0.00	0.16	0.421	I	o	|	|	|	| 1.31
30.667	0.00	0.16	0.420	I	o	|	|	|	| 1.31
30.750	0.00	0.16	0.419	I	o	|	|	|	| 1.30
30.833	0.00	0.16	0.418	I	o	|	|	|	| 1.30
30.917	0.00	0.16	0.417	I	o	|	|	|	| 1.30
31.000	0.00	0.16	0.416	I	o	|	|	|	| 1.30
31.083	0.00	0.16	0.415	I	o	|	|	|	| 1.29
31.167	0.00	0.16	0.414	I	o	|	|	|	| 1.29
31.250	0.00	0.15	0.413	I	o	|	|	|	| 1.29
31.333	0.00	0.15	0.412	I	o	|	|	|	| 1.28
31.417	0.00	0.15	0.411	I	o	|	|	|	| 1.28
31.500	0.00	0.15	0.410	I	o	|	|	|	| 1.28
31.583	0.00	0.15	0.408	I	o	|	|	|	| 1.28
31.667	0.00	0.15	0.407	I	o	|	|	|	| 1.27
31.750	0.00	0.15	0.406	I	o	|	|	|	| 1.27
31.833	0.00	0.15	0.405	I	o	|	|	|	| 1.27
31.917	0.00	0.15	0.404	I	o	|	|	|	| 1.26
32.000	0.00	0.15	0.403	I	o	|	|	|	| 1.26
32.083	0.00	0.15	0.402	I	o	|	|	|	| 1.26
32.167	0.00	0.15	0.401	I	o	|	|	|	| 1.26
32.250	0.00	0.15	0.400	I	o	|	|	|	| 1.25
32.333	0.00	0.14	0.399	I	o	|	|	|	| 1.25
32.417	0.00	0.14	0.398	I	o	|	|	|	| 1.25
32.500	0.00	0.14	0.397	I	o	|	|	|	| 1.25
32.583	0.00	0.14	0.396	I	o	|	|	|	| 1.24
32.667	0.00	0.14	0.395	I	o	|	|	|	| 1.24
32.750	0.00	0.14	0.394	I	o	|	|	|	| 1.24
32.833	0.00	0.14	0.393	I	o	|	|	|	| 1.24
32.917	0.00	0.14	0.392	I	o	|	|	|	| 1.23
33.000	0.00	0.14	0.391	I	o	|	|	|	| 1.23
33.083	0.00	0.14	0.391	I	o	|	|	|	| 1.23
33.167	0.00	0.14	0.390	I	o	|	|	|	| 1.23
33.250	0.00	0.14	0.389	I	o	|	|	|	| 1.22
33.333	0.00	0.14	0.388	I	o	|	|	|	| 1.22
33.417	0.00	0.14	0.387	I	o	|	|	|	| 1.22
33.500	0.00	0.13	0.386	I	o	|	|	|	| 1.22
33.583	0.00	0.13	0.385	I	o	|	|	|	| 1.21
33.667	0.00	0.13	0.384	I	o	|	|	|	| 1.21
33.750	0.00	0.13	0.383	I	o	|	|	|	| 1.21
33.833	0.00	0.13	0.382	I	o	|	|	|	| 1.21
33.917	0.00	0.13	0.381	I	o	|	|	|	| 1.20
34.000	0.00	0.13	0.380	I	o	|	|	|	| 1.20
34.083	0.00	0.13	0.379	I	o	|	|	|	| 1.20
34.167	0.00	0.13	0.379	I	o	|	|	|	| 1.20
34.250	0.00	0.13	0.378	I	o	|	|	|	| 1.19
34.333	0.00	0.13	0.377	I	o	|	|	|	| 1.19
34.417	0.00	0.13	0.376	I	o	|	|	|	| 1.19
34.500	0.00	0.13	0.375	I	o	|	|	|	| 1.19
34.583	0.00	0.13	0.374	I	o	|	|	|	| 1.19
34.667	0.00	0.12	0.373	I	o	|	|	|	| 1.18
34.750	0.00	0.12	0.372	I	o	|	|	|	| 1.18
34.833	0.00	0.12	0.372	I	o	|	|	|	| 1.18
34.917	0.00	0.12	0.371	I	o	|	|	|	| 1.18
35.000	0.00	0.12	0.370	I	o	|	|	|	| 1.17
35.083	0.00	0.12	0.369	I	o	|	|	|	| 1.17
35.167	0.00	0.12	0.368	I	o	|	|	|	| 1.17
35.250	0.00	0.12	0.367	I	o	|	|	|	| 1.17
35.333	0.00	0.12	0.367	I	o	|	|	|	| 1.17
35.417	0.00	0.12	0.366	I	o	|	|	|	| 1.16
35.500	0.00	0.12	0.365	I	o	|	|	|	| 1.16
35.583	0.00	0.12	0.364	I	o	|	|	|	| 1.16
35.667	0.00	0.12	0.363	I	o	|	|	|	| 1.16
35.750	0.00	0.12	0.363	I	o	|	|	|	| 1.15
35.833	0.00	0.12	0.362	I	o	|	|	|	| 1.15
35.917	0.00	0.12	0.361	I	o	|	|	|	| 1.15
36.000	0.00	0.11	0.360	I	o	|	|	|	| 1.15
36.083	0.00	0.11	0.359	I	o	|	|	|	| 1.15
36.167	0.00	0.11	0.359	I	o	|	|	|	| 1.14
36.250	0.00	0.11	0.358	I	o	|	|	|	| 1.14
36.333	0.00	0.11	0.357	I	o	|	|	|	| 1.14
36.417	0.00	0.11	0.356	I	o	|	|	|	| 1.14
36.500	0.00	0.11	0.355	I	o	|	|	|	| 1.14
36.583	0.00	0.11	0.355	I	o	|	|	|	| 1.13
36.667	0.00	0.11	0.354	I	o	|	|	|	| 1.13
36.750	0.00	0.11	0.353	I	o	|	|	|	| 1.13
36.833	0.00	0.11	0.352	I	o	|	|	|	| 1.13
36.917	0.00	0.11	0.352	I	o	|	|	|	| 1.13
37.000	0.00	0.11	0.351	I	o	|	|	|	| 1.12
37.083	0.00	0.11	0.350	I	o	|	|	|	| 1.12
37.167	0.00	0.11	0.349	I	o	|	|	|	| 1.12
37.250	0.00	0.11	0.349	I	o	|	|	|	| 1.12
37.333	0.00	0.11	0.348	I	o	|	|	|	| 1.12
37.417	0.00	0.11	0.347	I	o	|	|	|	| 1.11
37.500	0.00	0.10	0.347	I	o	|	|	|	| 1.11
37.583	0.00	0.10	0.346	I	o	|	|	|	| 1.11
37.667	0.00	0.10	0.345	I	o	|	|	|	| 1.11

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37.750    0.00    0.10      0.344  I O     |       |       |       |     1.11
37.833    0.00    0.10      0.344  I O     |       |       |       |     1.10
37.917    0.00    0.10      0.343  I O     |       |       |       |     1.10
38.000    0.00    0.10      0.342  I O     |       |       |       |     1.10
38.083    0.00    0.10      0.342  I O     |       |       |       |     1.10
38.167    0.00    0.10      0.341  I O     |       |       |       |     1.10
38.250    0.00    0.10      0.340  I O     |       |       |       |     1.10

Remaining water in basin =    0.34 (Ac.Ft)

****************************HYDROGRAPH DATA****************************
               Number of intervals =   459
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =        0.325 (CFS)
               Total volume =       0.488 (Ac.Ft)
       Status of hydrographs being held in storage
                  Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
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                    FLOOD HYDROGRAPH ROUTING PROGRAM
                Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                            Study date: 06/03/24

      ---------------------------------------------------------------------



      Program License Serial Number 5006

      ---------------------------------------------------------------------
      ********************* HYDROGRAPH INFORMATION **********************

                  From study/file name: PRO310110.rte
      ****************************HYDROGRAPH DATA****************************
                  Number of intervals =    17
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =       13.398 (CFS)
                  Total volume =       0.408 (Ac.Ft)
             Status of hydrographs being held in storage
                       Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
             Peak (CFS)      0.000     0.000     0.000     0.000     0.000
             Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      *********************************************************************



      +++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
      Process from Point/Station        1.000 to Point/Station        2.000
      **** RETARDING BASIN ROUTING ****
      _____________________________________________________________________

      User entry of depth-outflow-storage data
      ---------------------------------------------------------------------
      Total number of inflow hydrograph intervals = 17
      Hydrograph time unit =  5.000 (Min.)
      Initial depth in storage basin =   0.00(Ft.)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Initial basin depth =   0.00 (Ft.)
      Initial basin storage =      0.00 (Ac.Ft)
      Initial basin outflow =   0.00 (CFS)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Depth vs. Storage and Depth vs. Discharge data:
       Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
            (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
      ---------------------------------------------------------------------
        0.000      0.000      0.000      0.000        0.000
        1.000      0.304      0.072      0.304        0.304
        2.000      0.683      0.361      0.682        0.684
        2.500      0.893     17.450      0.833        0.953
        3.000      1.118     48.572      0.951        1.285
      ---------------------------------------------------------------------
                     Hydrograph Detention Basin Routing
      ---------------------------------------------------------------------

      Graph values: 'I'= unit inflow; 'O'=outflow at time shown
      ---------------------------------------------------------------------
       Time   Inflow  Outflow    Storage                                  Depth
      (Hours)  (CFS)   (CFS)     (Ac.Ft) .0       3.3    6.70   10.05   13.40 (Ft.)
       0.083    0.45    0.00      0.002  OI      |       |       |       |     0.01
       0.167    1.18    0.00      0.007  O I     |       |       |       |     0.02
       0.250    1.56    0.00      0.017  O  I    |       |       |       |     0.05
       0.333    1.84    0.01      0.028  O   I   |       |       |       |     0.09
       0.417    2.16    0.01      0.042  O    I  |       |       |       |     0.14
       0.500    2.64    0.01      0.058  O     I |       |       |       |     0.19
       0.583    3.22    0.02      0.078  O      I|       |       |       |     0.26
       0.667    4.09    0.02      0.103  O       I       |       |       |     0.34
       0.750    6.31    0.03      0.139  O       |      I|       |       |     0.46
       0.833   13.17    0.05      0.206  O       |       |       |      I|     0.68
       0.917   13.40    0.07      0.297  O       |       |       |       I     0.98
       1.000    5.43    0.12      0.361  O       |   I   |       |       |     1.15
       1.083    2.44    0.14      0.387  O    I  |       |       |       |     1.22
       1.167    0.94    0.14      0.398  O I     |       |       |       |     1.25
       1.250    0.36    0.15      0.402  O       |       |       |       |     1.26
       1.333    0.07    0.15      0.402  O       |       |       |       |     1.26
       1.417    0.01    0.15      0.401  O       |       |       |       |     1.26
       1.500    0.00    0.15      0.400  O       |       |       |       |     1.25
       1.583    0.00    0.14      0.399  O       |       |       |       |     1.25
       1.667    0.00    0.14      0.398  O       |       |       |       |     1.25
       1.750    0.00    0.14      0.397  O       |       |       |       |     1.25
       1.833    0.00    0.14      0.396  O       |       |       |       |     1.24
```

1.917	0.00	0.14	0.395	o	|	|	|	1.24
2.000	0.00	0.14	0.394	o	|	|	|	1.24
2.083	0.00	0.14	0.393	o	|	|	|	1.24
2.167	0.00	0.14	0.392	o	|	|	|	1.23
2.250	0.00	0.14	0.392	o	|	|	|	1.23
2.333	0.00	0.14	0.391	o	|	|	|	1.23
2.417	0.00	0.14	0.390	o	|	|	|	1.23
2.500	0.00	0.14	0.389	o	|	|	|	1.22
2.583	0.00	0.14	0.388	o	|	|	|	1.22
2.667	0.00	0.14	0.387	o	|	|	|	1.22
2.750	0.00	0.13	0.386	o	|	|	|	1.22
2.833	0.00	0.13	0.385	o	|	|	|	1.21
2.917	0.00	0.13	0.384	o	|	|	|	1.21
3.000	0.00	0.13	0.383	o	|	|	|	1.21
3.083	0.00	0.13	0.382	o	|	|	|	1.21
3.167	0.00	0.13	0.381	o	|	|	|	1.20
3.250	0.00	0.13	0.380	o	|	|	|	1.20
3.333	0.00	0.13	0.380	o	|	|	|	1.20
3.417	0.00	0.13	0.379	o	|	|	|	1.20
3.500	0.00	0.13	0.378	o	|	|	|	1.19
3.583	0.00	0.13	0.377	o	|	|	|	1.19
3.667	0.00	0.13	0.376	o	|	|	|	1.19
3.750	0.00	0.13	0.375	o	|	|	|	1.19
3.833	0.00	0.13	0.374	o	|	|	|	1.19
3.917	0.00	0.12	0.373	o	|	|	|	1.18
4.000	0.00	0.12	0.373	o	|	|	|	1.18
4.083	0.00	0.12	0.372	o	|	|	|	1.18
4.167	0.00	0.12	0.371	o	|	|	|	1.18
4.250	0.00	0.12	0.370	o	|	|	|	1.17
4.333	0.00	0.12	0.369	o	|	|	|	1.17
4.417	0.00	0.12	0.368	o	|	|	|	1.17
4.500	0.00	0.12	0.367	o	|	|	|	1.17
4.583	0.00	0.12	0.367	o	|	|	|	1.17
4.667	0.00	0.12	0.366	o	|	|	|	1.16
4.750	0.00	0.12	0.365	o	|	|	|	1.16
4.833	0.00	0.12	0.364	o	|	|	|	1.16
4.917	0.00	0.12	0.363	o	|	|	|	1.16
5.000	0.00	0.12	0.363	o	|	|	|	1.15
5.083	0.00	0.12	0.362	o	|	|	|	1.15
5.167	0.00	0.12	0.361	o	|	|	|	1.15
5.250	0.00	0.11	0.360	o	|	|	|	1.15
5.333	0.00	0.11	0.359	o	|	|	|	1.15
5.417	0.00	0.11	0.359	o	|	|	|	1.14
5.500	0.00	0.11	0.358	o	|	|	|	1.14
5.583	0.00	0.11	0.357	o	|	|	|	1.14
5.667	0.00	0.11	0.356	o	|	|	|	1.14
5.750	0.00	0.11	0.356	o	|	|	|	1.14
5.833	0.00	0.11	0.355	o	|	|	|	1.13
5.917	0.00	0.11	0.354	o	|	|	|	1.13
6.000	0.00	0.11	0.353	o	|	|	|	1.13
6.083	0.00	0.11	0.352	o	|	|	|	1.13
6.167	0.00	0.11	0.352	o	|	|	|	1.13
6.250	0.00	0.11	0.351	o	|	|	|	1.12
6.333	0.00	0.11	0.350	o	|	|	|	1.12
6.417	0.00	0.11	0.350	o	|	|	|	1.12
6.500	0.00	0.11	0.349	o	|	|	|	1.12
6.583	0.00	0.11	0.348	o	|	|	|	1.12
6.667	0.00	0.11	0.347	o	|	|	|	1.11
6.750	0.00	0.10	0.347	o	|	|	|	1.11
6.833	0.00	0.10	0.346	o	|	|	|	1.11
6.917	0.00	0.10	0.345	o	|	|	|	1.11
7.000	0.00	0.10	0.344	o	|	|	|	1.11
7.083	0.00	0.10	0.344	o	|	|	|	1.10
7.167	0.00	0.10	0.343	o	|	|	|	1.10
7.250	0.00	0.10	0.342	o	|	|	|	1.10
7.333	0.00	0.10	0.342	o	|	|	|	1.10
7.417	0.00	0.10	0.341	o	|	|	|	1.10
7.500	0.00	0.10	0.340	o	|	|	|	1.10

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 90
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.147 (CFS)
Total volume = 0.068 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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                    FLOOD HYDROGRAPH ROUTING PROGRAM
                Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                            Study date: 06/03/24

      ---------------------------------------------------------------------



      Program License Serial Number 5006

      ---------------------------------------------------------------------
      ********************* HYDROGRAPH INFORMATION **********************

                  From study/file name: PRO310310.rte
      ******************************HYDROGRAPH DATA******************************
                  Number of intervals =    41
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =        7.299 (CFS)
                  Total volume =       0.524 (Ac.Ft)
             Status of hydrographs being held in storage
                       Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
             Peak (CFS)      0.000     0.000     0.000     0.000     0.000
             Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      ***************************************************************************



      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
      Process from Point/Station        1.000 to Point/Station        2.000
      **** RETARDING BASIN ROUTING ****
      _________________________________________________________________________

      User entry of depth-outflow-storage data
      ---------------------------------------------------------------------
      Total number of inflow hydrograph intervals = 41
      Hydrograph time unit =  5.000 (Min.)
      Initial depth in storage basin =   0.00(Ft.)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Initial basin depth =   0.00 (Ft.)
      Initial basin storage =      0.00 (Ac.Ft)
      Initial basin outflow =   0.00 (CFS)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Depth vs. Storage and Depth vs. Discharge data:
       Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
            (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
      ---------------------------------------------------------------------
        0.000      0.000      0.000      0.000        0.000
        1.000      0.304      0.072      0.304        0.304
        2.000      0.683      0.361      0.682        0.684
        2.500      0.893     17.450      0.833        0.953
        3.000      1.118     48.572      0.951        1.285
      ---------------------------------------------------------------------
                    Hydrograph Detention Basin Routing
      ---------------------------------------------------------------------

      Graph values: 'I'= unit inflow; 'O'=outflow at time shown
      ---------------------------------------------------------------------
       Time   Inflow  Outflow    Storage                                  Depth
      (Hours)  (CFS)   (CFS)     (Ac.Ft) .0       1.8    3.65    5.47    7.30 (Ft.)
       0.083    0.28    0.00      0.001  OI      |       |       |       |     0.00
       0.167    0.65    0.00      0.004  O I     |       |       |       |     0.01
       0.250    0.69    0.00      0.009  O  I    |       |       |       |     0.03
       0.333    0.75    0.00      0.014  O  I    |       |       |       |     0.04
       0.417    0.87    0.00      0.019  O  I    |       |       |       |     0.06
       0.500    0.96    0.01      0.026  O   I   |       |       |       |     0.08
       0.583    0.99    0.01      0.032  O   I   |       |       |       |     0.11
       0.667    1.00    0.01      0.039  O   I   |       |       |       |     0.13
       0.750    1.07    0.01      0.046  O   I   |       |       |       |     0.15
       0.833    1.02    0.01      0.053  O   I   |       |       |       |     0.17
       0.917    0.97    0.01      0.060  O   I   |       |       |       |     0.20
       1.000    1.02    0.02      0.067  O   I   |       |       |       |     0.22
       1.083    1.16    0.02      0.074  O    I  |       |       |       |     0.24
       1.167    1.29    0.02      0.082  O    I  |       |       |       |     0.27
       1.250    1.32    0.02      0.091  O    I  |       |       |       |     0.30
       1.333    1.29    0.02      0.100  O    I  |       |       |       |     0.33
       1.417    1.37    0.03      0.109  O    I  |       |       |       |     0.36
       1.500    1.56    0.03      0.119  O     I |       |       |       |     0.39
       1.583    1.56    0.03      0.129  O     I |       |       |       |     0.43
       1.667    1.56    0.03      0.140  O     I |       |       |       |     0.46
       1.750    1.91    0.04      0.152  O       I       |       |       |     0.50
       1.833    2.18    0.04      0.166  O       |I      |       |       |     0.54
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1.917	2.07	0.04	0.180	O	I	|	|	|	0.59
2.000	2.01	0.05	0.194	O	I	|	|	|	0.64
2.083	2.09	0.05	0.207	O	I	|	|	|	0.68
2.167	2.62	0.05	0.223	O	I	|	|	|	0.73
2.250	3.59	0.06	0.244	O	|	I	|	|	0.80
2.333	3.55	0.06	0.268	O	|	I	|	|	0.88
2.417	4.29	0.07	0.295	O	|	| I	|	|	0.97
2.500	6.25	0.09	0.331	O	|	|	I |	|	1.07
2.583	7.30	0.13	0.377	O	|	|	|	I	1.19
2.667	7.04	0.16	0.425	O	|	|	|	I |	1.32
2.750	4.43	0.19	0.463	O	|	| I	|	|	1.42
2.833	2.16	0.21	0.485	O	I	|	|	|	1.48
2.917	1.54	0.22	0.496	O	I	|	|	|	1.51
3.000	1.01	0.22	0.503	O	I	|	|	|	1.53
3.083	0.42	0.23	0.507	OI	|	|	|	|	1.53
3.167	0.13	0.23	0.507	O	|	|	|	|	1.54
3.250	0.05	0.23	0.506	O	|	|	|	|	1.53
3.333	0.02	0.22	0.505	O	|	|	|	|	1.53
3.417	0.00	0.22	0.503	O	|	|	|	|	1.53
3.500	0.00	0.22	0.502	O	|	|	|	|	1.52
3.583	0.00	0.22	0.500	O	|	|	|	|	1.52
3.667	0.00	0.22	0.499	O	|	|	|	|	1.51
3.750	0.00	0.22	0.497	O	|	|	|	|	1.51
3.833	0.00	0.22	0.495	O	|	|	|	|	1.51
3.917	0.00	0.22	0.494	O	|	|	|	|	1.50
4.000	0.00	0.22	0.492	O	|	|	|	|	1.50
4.083	0.00	0.21	0.491	O	|	|	|	|	1.49
4.167	0.00	0.21	0.490	O	|	|	|	|	1.49
4.250	0.00	0.21	0.488	O	|	|	|	|	1.49
4.333	0.00	0.21	0.487	O	|	|	|	|	1.48
4.417	0.00	0.21	0.485	O	|	|	|	|	1.48
4.500	0.00	0.21	0.484	O	|	|	|	|	1.47
4.583	0.00	0.21	0.482	O	|	|	|	|	1.47
4.667	0.00	0.21	0.481	O	|	|	|	|	1.47
4.750	0.00	0.21	0.479	O	|	|	|	|	1.46
4.833	0.00	0.20	0.478	O	|	|	|	|	1.46
4.917	0.00	0.20	0.477	O	|	|	|	|	1.46
5.000	0.00	0.20	0.475	O	|	|	|	|	1.45
5.083	0.00	0.20	0.474	O	|	|	|	|	1.45
5.167	0.00	0.20	0.472	O	|	|	|	|	1.44
5.250	0.00	0.20	0.471	O	|	|	|	|	1.44
5.333	0.00	0.20	0.470	O	|	|	|	|	1.44
5.417	0.00	0.20	0.468	O	|	|	|	|	1.43
5.500	0.00	0.20	0.467	O	|	|	|	|	1.43
5.583	0.00	0.20	0.466	O	|	|	|	|	1.43
5.667	0.00	0.19	0.464	O	|	|	|	|	1.42
5.750	0.00	0.19	0.463	O	|	|	|	|	1.42
5.833	0.00	0.19	0.462	O	|	|	|	|	1.42
5.917	0.00	0.19	0.460	O	|	|	|	|	1.41
6.000	0.00	0.19	0.459	O	|	|	|	|	1.41
6.083	0.00	0.19	0.458	O	|	|	|	|	1.41
6.167	0.00	0.19	0.456	O	|	|	|	|	1.40
6.250	0.00	0.19	0.455	O	|	|	|	|	1.40
6.333	0.00	0.19	0.454	O	|	|	|	|	1.40
6.417	0.00	0.19	0.453	O	|	|	|	|	1.39
6.500	0.00	0.18	0.451	O	|	|	|	|	1.39
6.583	0.00	0.18	0.450	O	|	|	|	|	1.39
6.667	0.00	0.18	0.449	O	|	|	|	|	1.38
6.750	0.00	0.18	0.447	O	|	|	|	|	1.38
6.833	0.00	0.18	0.446	O	|	|	|	|	1.38
6.917	0.00	0.18	0.445	O	|	|	|	|	1.37
7.000	0.00	0.18	0.444	O	|	|	|	|	1.37
7.083	0.00	0.18	0.443	O	|	|	|	|	1.37
7.167	0.00	0.18	0.441	O	|	|	|	|	1.36
7.250	0.00	0.18	0.440	O	|	|	|	|	1.36
7.333	0.00	0.17	0.439	O	|	|	|	|	1.36
7.417	0.00	0.17	0.438	O	|	|	|	|	1.35
7.500	0.00	0.17	0.436	O	|	|	|	|	1.35
7.583	0.00	0.17	0.435	O	|	|	|	|	1.35
7.667	0.00	0.17	0.434	O	|	|	|	|	1.34
7.750	0.00	0.17	0.433	O	|	|	|	|	1.34
7.833	0.00	0.17	0.432	O	|	|	|	|	1.34
7.917	0.00	0.17	0.431	O	|	|	|	|	1.33
8.000	0.00	0.17	0.429	O	|	|	|	|	1.33
8.083	0.00	0.17	0.428	O	|	|	|	|	1.33
8.167	0.00	0.17	0.427	O	|	|	|	|	1.32
8.250	0.00	0.17	0.426	O	|	|	|	|	1.32
8.333	0.00	0.16	0.425	O	|	|	|	|	1.32
8.417	0.00	0.16	0.424	O	|	|	|	|	1.32
8.500	0.00	0.16	0.423	O	|	|	|	|	1.31
8.583	0.00	0.16	0.422	O	|	|	|	|	1.31
8.667	0.00	0.16	0.420	O	|	|	|	|	1.31
8.750	0.00	0.16	0.419	O	|	|	|	|	1.30
8.833	0.00	0.16	0.418	O	|	|	|	|	1.30
8.917	0.00	0.16	0.417	O	|	|	|	|	1.30
9.000	0.00	0.16	0.416	O	|	|	|	|	1.30

9.083	0.00	0.16	0.415	o	|	|	|	|	1.29
9.167	0.00	0.16	0.414	o	|	|	|	|	1.29
9.250	0.00	0.15	0.413	o	|	|	|	|	1.29
9.333	0.00	0.15	0.412	o	|	|	|	|	1.28
9.417	0.00	0.15	0.411	o	|	|	|	|	1.28
9.500	0.00	0.15	0.410	o	|	|	|	|	1.28
9.583	0.00	0.15	0.409	o	|	|	|	|	1.28
9.667	0.00	0.15	0.408	o	|	|	|	|	1.27
9.750	0.00	0.15	0.406	o	|	|	|	|	1.27
9.833	0.00	0.15	0.405	o	|	|	|	|	1.27
9.917	0.00	0.15	0.404	o	|	|	|	|	1.27
10.000	0.00	0.15	0.403	o	|	|	|	|	1.26
10.083	0.00	0.15	0.402	o	|	|	|	|	1.26
10.167	0.00	0.15	0.401	o	|	|	|	|	1.26
10.250	0.00	0.15	0.400	o	|	|	|	|	1.25
10.333	0.00	0.14	0.399	o	|	|	|	|	1.25
10.417	0.00	0.14	0.398	o	|	|	|	|	1.25
10.500	0.00	0.14	0.397	o	|	|	|	|	1.25
10.583	0.00	0.14	0.396	o	|	|	|	|	1.24
10.667	0.00	0.14	0.395	o	|	|	|	|	1.24
10.750	0.00	0.14	0.394	o	|	|	|	|	1.24
10.833	0.00	0.14	0.394	o	|	|	|	|	1.24
10.917	0.00	0.14	0.393	o	|	|	|	|	1.23
11.000	0.00	0.14	0.392	o	|	|	|	|	1.23
11.083	0.00	0.14	0.391	o	|	|	|	|	1.23
11.167	0.00	0.14	0.390	o	|	|	|	|	1.23
11.250	0.00	0.14	0.389	o	|	|	|	|	1.22
11.333	0.00	0.14	0.388	o	|	|	|	|	1.22
11.417	0.00	0.14	0.387	o	|	|	|	|	1.22
11.500	0.00	0.13	0.386	o	|	|	|	|	1.22
11.583	0.00	0.13	0.385	o	|	|	|	|	1.21
11.667	0.00	0.13	0.384	o	|	|	|	|	1.21
11.750	0.00	0.13	0.383	o	|	|	|	|	1.21
11.833	0.00	0.13	0.382	o	|	|	|	|	1.21
11.917	0.00	0.13	0.381	o	|	|	|	|	1.20
12.000	0.00	0.13	0.380	o	|	|	|	|	1.20
12.083	0.00	0.13	0.380	o	|	|	|	|	1.20
12.167	0.00	0.13	0.379	o	|	|	|	|	1.20
12.250	0.00	0.13	0.378	o	|	|	|	|	1.19
12.333	0.00	0.13	0.377	o	|	|	|	|	1.19
12.417	0.00	0.13	0.376	o	|	|	|	|	1.19
12.500	0.00	0.13	0.375	o	|	|	|	|	1.19
12.583	0.00	0.13	0.374	o	|	|	|	|	1.19
12.667	0.00	0.12	0.373	o	|	|	|	|	1.18
12.750	0.00	0.12	0.373	o	|	|	|	|	1.18
12.833	0.00	0.12	0.372	o	|	|	|	|	1.18
12.917	0.00	0.12	0.371	o	|	|	|	|	1.18
13.000	0.00	0.12	0.370	o	|	|	|	|	1.17
13.083	0.00	0.12	0.369	o	|	|	|	|	1.17
13.167	0.00	0.12	0.368	o	|	|	|	|	1.17
13.250	0.00	0.12	0.368	o	|	|	|	|	1.17
13.333	0.00	0.12	0.367	o	|	|	|	|	1.17
13.417	0.00	0.12	0.366	o	|	|	|	|	1.16
13.500	0.00	0.12	0.365	o	|	|	|	|	1.16
13.583	0.00	0.12	0.364	o	|	|	|	|	1.16
13.667	0.00	0.12	0.363	o	|	|	|	|	1.16
13.750	0.00	0.12	0.363	o	|	|	|	|	1.15
13.833	0.00	0.12	0.362	o	|	|	|	|	1.15
13.917	0.00	0.12	0.361	o	|	|	|	|	1.15
14.000	0.00	0.11	0.360	o	|	|	|	|	1.15
14.083	0.00	0.11	0.359	o	|	|	|	|	1.15
14.167	0.00	0.11	0.359	o	|	|	|	|	1.14
14.250	0.00	0.11	0.358	o	|	|	|	|	1.14
14.333	0.00	0.11	0.357	o	|	|	|	|	1.14
14.417	0.00	0.11	0.356	o	|	|	|	|	1.14
14.500	0.00	0.11	0.356	o	|	|	|	|	1.14
14.583	0.00	0.11	0.355	o	|	|	|	|	1.13
14.667	0.00	0.11	0.354	o	|	|	|	|	1.13
14.750	0.00	0.11	0.353	o	|	|	|	|	1.13
14.833	0.00	0.11	0.353	o	|	|	|	|	1.13
14.917	0.00	0.11	0.352	o	|	|	|	|	1.13
15.000	0.00	0.11	0.351	o	|	|	|	|	1.12
15.083	0.00	0.11	0.350	o	|	|	|	|	1.12
15.167	0.00	0.11	0.350	o	|	|	|	|	1.12
15.250	0.00	0.11	0.349	o	|	|	|	|	1.12
15.333	0.00	0.11	0.348	o	|	|	|	|	1.12
15.417	0.00	0.11	0.347	o	|	|	|	|	1.11
15.500	0.00	0.10	0.347	o	|	|	|	|	1.11
15.583	0.00	0.10	0.346	o	|	|	|	|	1.11
15.667	0.00	0.10	0.345	o	|	|	|	|	1.11
15.750	0.00	0.10	0.344	o	|	|	|	|	1.11
15.833	0.00	0.10	0.344	o	|	|	|	|	1.10
15.917	0.00	0.10	0.343	o	|	|	|	|	1.10
16.000	0.00	0.10	0.342	o	|	|	|	|	1.10
16.083	0.00	0.10	0.342	o	|	|	|	|	1.10
16.167	0.00	0.10	0.341	o	|	|	|	|	1.10

```
16.250    0.00    0.10      0.340  o       |       |       |       |     1.10

       Remaining water in basin =    0.34 (Ac.Ft)


       ****************************HYDROGRAPH DATA****************************
                     Number of intervals =   195
                     Time interval =    5.0 (Min.)
                     Maximum/Peak flow rate =        0.227 (CFS)
                     Total volume =       0.184 (Ac.Ft)
              Status of hydrographs being held in storage
                        Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
              Peak (CFS)      0.000     0.000     0.000     0.000     0.000
              Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
       ***********************************************************************

       ----------------------------------------------------------------------
```

FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: PRO310610.rte
**********HYDROGRAPH DATA**********
Number of intervals = 77
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 7.055 (CFS)
Total volume = 0.724 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 77
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.304	0.072	0.304	0.304
2.000	0.683	0.361	0.682	0.684
2.500	0.893	17.450	0.833	0.953
3.000	1.118	48.572	0.951	1.285

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.8 3.53 5.29 7.06 Depth (Ft.)
0.083	0.16	0.00	0.001	O 0.00
0.167	0.39	0.00	0.002	OI 0.01
0.250	0.48	0.00	0.005	O I 0.02
0.333	0.51	0.00	0.009	O I 0.03
0.417	0.53	0.00	0.012	O I 0.04
0.500	0.56	0.00	0.016	O I 0.05
0.583	0.60	0.00	0.020	O I 0.07
0.667	0.61	0.01	0.024	O I 0.08
0.750	0.62	0.01	0.028	O I 0.09
0.833	0.62	0.01	0.033	O I 0.11
0.917	0.62	0.01	0.037	O I 0.12
1.000	0.65	0.01	0.041	O I 0.14
1.083	0.69	0.01	0.046	O I 0.15
1.167	0.70	0.01	0.050	O I 0.17
1.250	0.71	0.01	0.055	O I 0.18
1.333	0.71	0.01	0.060	O I 0.20
1.417	0.71	0.02	0.065	O I 0.21
1.500	0.71	0.02	0.070	O I 0.23
1.583	0.71	0.02	0.074	O I 0.24
1.667	0.71	0.02	0.079	O I 0.26
1.750	0.71	0.02	0.084	O I 0.28
1.833	0.71	0.02	0.089	O I 0.29

```
1.917    0.71    0.02      0.093  O  I    |        |        |        |     0.31
2.000    0.74    0.02      0.098  O  I    |        |        |        |     0.32
2.083    0.75    0.02      0.103  O  I    |        |        |        |     0.34
2.167    0.75    0.03      0.108  O  I    |        |        |        |     0.36
2.250    0.79    0.03      0.113  O  I    |        |        |        |     0.37
2.333    0.79    0.03      0.119  O  I    |        |        |        |     0.39
2.417    0.80    0.03      0.124  O  I    |        |        |        |     0.41
2.500    0.80    0.03      0.129  O  I    |        |        |        |     0.42
2.583    0.80    0.03      0.134  O  I    |        |        |        |     0.44
2.667    0.80    0.03      0.140  O  I    |        |        |        |     0.46
2.750    0.83    0.03      0.145  O  I    |        |        |        |     0.48
2.833    0.87    0.04      0.151  O  I    |        |        |        |     0.50
2.917    0.88    0.04      0.156  O  I    |        |        |        |     0.51
3.000    0.88    0.04      0.162  O   I   |        |        |        |     0.53
3.083    0.89    0.04      0.168  O   I   |        |        |        |     0.55
3.167    0.92    0.04      0.174  O   I   |        |        |        |     0.57
3.250    0.96    0.04      0.180  O   I   |        |        |        |     0.59
3.333    0.97    0.04      0.186  O   I   |        |        |        |     0.61
3.417    1.00    0.05      0.193  O   I   |        |        |        |     0.63
3.500    1.08    0.05      0.200  O   I   |        |        |        |     0.66
3.583    1.16    0.05      0.207  O    I  |        |        |        |     0.68
3.667    1.22    0.05      0.215  O    I  |        |        |        |     0.71
3.750    1.26    0.05      0.223  O    I  |        |        |        |     0.73
3.833    1.31    0.05      0.232  O    I  |        |        |        |     0.76
3.917    1.35    0.06      0.240  O     I |        |        |        |     0.79
4.000    1.40    0.06      0.250  O     I |        |        |        |     0.82
4.083    1.44    0.06      0.259  O     I |        |        |        |     0.85
4.167    1.52    0.06      0.269  O     I |        |        |        |     0.88
4.250    1.63    0.07      0.279  O      I|        |        |        |     0.92
4.333    1.78    0.07      0.290  O       I        |        |        |     0.96
4.417    1.95    0.07      0.303  O       I        |        |        |     1.00
4.500    2.06    0.08      0.316  O        I       |        |        |     1.03
4.583    2.16    0.09      0.330  O        I       |        |        |     1.07
4.667    2.31    0.10      0.345  O         I      |        |        |     1.11
4.750    2.48    0.12      0.360  O          I     |        |        |     1.15
4.833    2.59    0.13      0.377  O          I     |        |        |     1.19
4.917    2.69    0.14      0.394  O           I    |        |        |     1.24
5.000    2.85    0.15      0.412  O           I    |        |        |     1.29
5.083    3.26    0.17      0.432  O             I  |        |        |     1.34
5.167    4.02    0.19      0.456  O                | I      |        |     1.40
5.250    4.72    0.21      0.485  O                |    I   |        |     1.48
5.333    5.30    0.24      0.518  |O               |        I        |     1.56
5.417    5.97    0.26      0.555  |O               |        |  I     |     1.66
5.500    7.06    0.30      0.598  |O               |        |      I |     1.78
5.583    5.63    0.33      0.639  |O               |        I        |     1.88
5.667    2.48    0.35      0.665  |O          I    |        |        |     1.95
5.750    1.34    0.36      0.676  |O     I         |        |        |     1.98
5.833    0.82    0.36      0.681  |O I             |        |        |     1.99
5.917    0.51    0.36      0.683  |OI              |        |        |     2.00
6.000    0.29    0.36      0.683  |O               |        |        |     2.00
6.083    0.15    0.36      0.682  IO               |        |        |     2.00
6.167    0.05    0.36      0.680  IO               |        |        |     1.99
6.250    0.02    0.36      0.678  IO               |        |        |     1.99
6.333    0.01    0.36      0.676  IO               |        |        |     1.98
6.417    0.00    0.35      0.673  IO               |        |        |     1.97
6.500    0.00    0.35      0.671  IO               |        |        |     1.97
6.583    0.00    0.35      0.668  IO               |        |        |     1.96
6.667    0.00    0.35      0.666  IO               |        |        |     1.96
6.750    0.00    0.35      0.664  IO               |        |        |     1.95
6.833    0.00    0.34      0.661  IO               |        |        |     1.94
6.917    0.00    0.34      0.659  IO               |        |        |     1.94
7.000    0.00    0.34      0.656  IO               |        |        |     1.93
7.083    0.00    0.34      0.654  IO               |        |        |     1.92
7.167    0.00    0.34      0.652  IO               |        |        |     1.92
7.250    0.00    0.34      0.649  IO               |        |        |     1.91
7.333    0.00    0.33      0.647  IO               |        |        |     1.91
7.417    0.00    0.33      0.645  IO               |        |        |     1.90
7.500    0.00    0.33      0.643  IO               |        |        |     1.89
7.583    0.00    0.33      0.640  IO               |        |        |     1.89
7.667    0.00    0.33      0.638  IO               |        |        |     1.88
7.750    0.00    0.33      0.636  IO               |        |        |     1.88
7.833    0.00    0.32      0.634  IO               |        |        |     1.87
7.917    0.00    0.32      0.631  IO               |        |        |     1.86
8.000    0.00    0.32      0.629  IO               |        |        |     1.86
8.083    0.00    0.32      0.627  IO               |        |        |     1.85
8.167    0.00    0.32      0.625  IO               |        |        |     1.85
8.250    0.00    0.31      0.623  IO               |        |        |     1.84
8.333    0.00    0.31      0.620  IO               |        |        |     1.83
8.417    0.00    0.31      0.618  IO               |        |        |     1.83
8.500    0.00    0.31      0.616  IO               |        |        |     1.82
8.583    0.00    0.31      0.614  IO               |        |        |     1.82
8.667    0.00    0.31      0.612  IO               |        |        |     1.81
8.750    0.00    0.31      0.610  IO               |        |        |     1.81
8.833    0.00    0.30      0.608  IO               |        |        |     1.80
8.917    0.00    0.30      0.606  IO               |        |        |     1.80
9.000    0.00    0.30      0.604  IO               |        |        |     1.79
```

9.083	0.00	0.30	0.601	IO				1.78
9.167	0.00	0.30	0.599	IO				1.78
9.250	0.00	0.30	0.597	IO				1.77
9.333	0.00	0.29	0.595	IO				1.77
9.417	0.00	0.29	0.593	IO				1.76
9.500	0.00	0.29	0.591	IO				1.76
9.583	0.00	0.29	0.589	IO				1.75
9.667	0.00	0.29	0.587	IO				1.75
9.750	0.00	0.29	0.585	IO				1.74
9.833	0.00	0.29	0.583	IO				1.74
9.917	0.00	0.28	0.581	IO				1.73
10.000	0.00	0.28	0.579	IO				1.73
10.083	0.00	0.28	0.578	IO				1.72
10.167	0.00	0.28	0.576	IO				1.72
10.250	0.00	0.28	0.574	IO				1.71
10.333	0.00	0.28	0.572	IO				1.71
10.417	0.00	0.27	0.570	IO				1.70
10.500	0.00	0.27	0.568	IO				1.70
10.583	0.00	0.27	0.566	IO				1.69
10.667	0.00	0.27	0.564	IO				1.69
10.750	0.00	0.27	0.562	IO				1.68
10.833	0.00	0.27	0.561	IO				1.68
10.917	0.00	0.27	0.559	IO				1.67
11.000	0.00	0.26	0.557	IO				1.67
11.083	0.00	0.26	0.555	IO				1.66
11.167	0.00	0.26	0.553	IO				1.66
11.250	0.00	0.26	0.551	IO				1.65
11.333	0.00	0.26	0.550	IO				1.65
11.417	0.00	0.26	0.548	IO				1.64
11.500	0.00	0.26	0.546	IO				1.64
11.583	0.00	0.26	0.544	IO				1.63
11.667	0.00	0.25	0.543	IO				1.63
11.750	0.00	0.25	0.541	IO				1.62
11.833	0.00	0.25	0.539	IO				1.62
11.917	0.00	0.25	0.537	IO				1.62
12.000	0.00	0.25	0.536	IO				1.61
12.083	0.00	0.25	0.534	IO				1.61
12.167	0.00	0.25	0.532	IO				1.60
12.250	0.00	0.24	0.531	IO				1.60
12.333	0.00	0.24	0.529	IO				1.59
12.417	0.00	0.24	0.527	IO				1.59
12.500	0.00	0.24	0.526	IO				1.58
12.583	0.00	0.24	0.524	IO				1.58
12.667	0.00	0.24	0.522	IO				1.58
12.750	0.00	0.24	0.521	IO				1.57
12.833	0.00	0.24	0.519	IO				1.57
12.917	0.00	0.23	0.517	IO				1.56
13.000	0.00	0.23	0.516	IO				1.56
13.083	0.00	0.23	0.514	IO				1.55
13.167	0.00	0.23	0.513	IO				1.55
13.250	0.00	0.23	0.511	IO				1.55
13.333	0.00	0.23	0.509	IO				1.54
13.417	0.00	0.23	0.508	IO				1.54
13.500	0.00	0.23	0.506	IO				1.53
13.583	0.00	0.23	0.505	IO				1.53
13.667	0.00	0.22	0.503	IO				1.53
13.750	0.00	0.22	0.502	IO				1.52
13.833	0.00	0.22	0.500	IO				1.52
13.917	0.00	0.22	0.499	O				1.51
14.000	0.00	0.22	0.497	O				1.51
14.083	0.00	0.22	0.496	O				1.51
14.167	0.00	0.22	0.494	O				1.50
14.250	0.00	0.22	0.493	O				1.50
14.333	0.00	0.21	0.491	O				1.49
14.417	0.00	0.21	0.490	O				1.49
14.500	0.00	0.21	0.488	O				1.49
14.583	0.00	0.21	0.487	O				1.48
14.667	0.00	0.21	0.485	O				1.48
14.750	0.00	0.21	0.484	O				1.47
14.833	0.00	0.21	0.482	O				1.47
14.917	0.00	0.21	0.481	O				1.47
15.000	0.00	0.21	0.480	O				1.46
15.083	0.00	0.20	0.478	O				1.46
15.167	0.00	0.20	0.477	O				1.46
15.250	0.00	0.20	0.475	O				1.45
15.333	0.00	0.20	0.474	O				1.45
15.417	0.00	0.20	0.473	O				1.44
15.500	0.00	0.20	0.471	O				1.44
15.583	0.00	0.20	0.470	O				1.44
15.667	0.00	0.20	0.468	O				1.43
15.750	0.00	0.20	0.467	O				1.43
15.833	0.00	0.20	0.466	O				1.43
15.917	0.00	0.19	0.464	O				1.42
16.000	0.00	0.19	0.463	O				1.42
16.083	0.00	0.19	0.462	O				1.42
16.167	0.00	0.19	0.460	O				1.41

16.250	0.00	0.19	0.459	o	|	|	|	|	1.41
16.333	0.00	0.19	0.458	o	|	|	|	|	1.41
16.417	0.00	0.19	0.456	o	|	|	|	|	1.40
16.500	0.00	0.19	0.455	o	|	|	|	|	1.40
16.583	0.00	0.19	0.454	o	|	|	|	|	1.40
16.667	0.00	0.19	0.453	o	|	|	|	|	1.39
16.750	0.00	0.18	0.451	o	|	|	|	|	1.39
16.833	0.00	0.18	0.450	o	|	|	|	|	1.39
16.917	0.00	0.18	0.449	o	|	|	|	|	1.38
17.000	0.00	0.18	0.448	o	|	|	|	|	1.38
17.083	0.00	0.18	0.446	o	|	|	|	|	1.38
17.167	0.00	0.18	0.445	o	|	|	|	|	1.37
17.250	0.00	0.18	0.444	o	|	|	|	|	1.37
17.333	0.00	0.18	0.443	o	|	|	|	|	1.37
17.417	0.00	0.18	0.441	o	|	|	|	|	1.36
17.500	0.00	0.18	0.440	o	|	|	|	|	1.36
17.583	0.00	0.17	0.439	o	|	|	|	|	1.36
17.667	0.00	0.17	0.438	o	|	|	|	|	1.35
17.750	0.00	0.17	0.437	o	|	|	|	|	1.35
17.833	0.00	0.17	0.435	o	|	|	|	|	1.35
17.917	0.00	0.17	0.434	o	|	|	|	|	1.34
18.000	0.00	0.17	0.433	o	|	|	|	|	1.34
18.083	0.00	0.17	0.432	o	|	|	|	|	1.34
18.167	0.00	0.17	0.431	o	|	|	|	|	1.33
18.250	0.00	0.17	0.430	o	|	|	|	|	1.33
18.333	0.00	0.17	0.428	o	|	|	|	|	1.33
18.417	0.00	0.17	0.427	o	|	|	|	|	1.33
18.500	0.00	0.17	0.426	o	|	|	|	|	1.32
18.583	0.00	0.16	0.425	o	|	|	|	|	1.32
18.667	0.00	0.16	0.424	o	|	|	|	|	1.32
18.750	0.00	0.16	0.423	o	|	|	|	|	1.31
18.833	0.00	0.16	0.422	o	|	|	|	|	1.31
18.917	0.00	0.16	0.420	o	|	|	|	|	1.31
19.000	0.00	0.16	0.419	o	|	|	|	|	1.30
19.083	0.00	0.16	0.418	o	|	|	|	|	1.30
19.167	0.00	0.16	0.417	o	|	|	|	|	1.30
19.250	0.00	0.16	0.416	o	|	|	|	|	1.30
19.333	0.00	0.16	0.415	o	|	|	|	|	1.29
19.417	0.00	0.16	0.414	o	|	|	|	|	1.29
19.500	0.00	0.16	0.413	o	|	|	|	|	1.29
19.583	0.00	0.15	0.412	o	|	|	|	|	1.28
19.667	0.00	0.15	0.411	o	|	|	|	|	1.28
19.750	0.00	0.15	0.410	o	|	|	|	|	1.28
19.833	0.00	0.15	0.409	o	|	|	|	|	1.28
19.917	0.00	0.15	0.408	o	|	|	|	|	1.27
20.000	0.00	0.15	0.407	o	|	|	|	|	1.27
20.083	0.00	0.15	0.406	o	|	|	|	|	1.27
20.167	0.00	0.15	0.404	o	|	|	|	|	1.27
20.250	0.00	0.15	0.403	o	|	|	|	|	1.26
20.333	0.00	0.15	0.402	o	|	|	|	|	1.26
20.417	0.00	0.15	0.401	o	|	|	|	|	1.26
20.500	0.00	0.15	0.400	o	|	|	|	|	1.25
20.583	0.00	0.14	0.399	o	|	|	|	|	1.25
20.667	0.00	0.14	0.398	o	|	|	|	|	1.25
20.750	0.00	0.14	0.397	o	|	|	|	|	1.25
20.833	0.00	0.14	0.396	o	|	|	|	|	1.24
20.917	0.00	0.14	0.395	o	|	|	|	|	1.24
21.000	0.00	0.14	0.395	o	|	|	|	|	1.24
21.083	0.00	0.14	0.394	o	|	|	|	|	1.24
21.167	0.00	0.14	0.393	o	|	|	|	|	1.23
21.250	0.00	0.14	0.392	o	|	|	|	|	1.23
21.333	0.00	0.14	0.391	o	|	|	|	|	1.23
21.417	0.00	0.14	0.390	o	|	|	|	|	1.23
21.500	0.00	0.14	0.389	o	|	|	|	|	1.22
21.583	0.00	0.14	0.388	o	|	|	|	|	1.22
21.667	0.00	0.14	0.387	o	|	|	|	|	1.22
21.750	0.00	0.13	0.386	o	|	|	|	|	1.22
21.833	0.00	0.13	0.385	o	|	|	|	|	1.21
21.917	0.00	0.13	0.384	o	|	|	|	|	1.21
22.000	0.00	0.13	0.383	o	|	|	|	|	1.21
22.083	0.00	0.13	0.382	o	|	|	|	|	1.21
22.167	0.00	0.13	0.381	o	|	|	|	|	1.20
22.250	0.00	0.13	0.381	o	|	|	|	|	1.20
22.333	0.00	0.13	0.380	o	|	|	|	|	1.20
22.417	0.00	0.13	0.379	o	|	|	|	|	1.20
22.500	0.00	0.13	0.378	o	|	|	|	|	1.19
22.583	0.00	0.13	0.377	o	|	|	|	|	1.19
22.667	0.00	0.13	0.376	o	|	|	|	|	1.19
22.750	0.00	0.13	0.375	o	|	|	|	|	1.19
22.833	0.00	0.13	0.374	o	|	|	|	|	1.19
22.917	0.00	0.12	0.373	o	|	|	|	|	1.18
23.000	0.00	0.12	0.373	o	|	|	|	|	1.18
23.083	0.00	0.12	0.372	o	|	|	|	|	1.18
23.167	0.00	0.12	0.371	o	|	|	|	|	1.18
23.250	0.00	0.12	0.370	o	|	|	|	|	1.17
23.333	0.00	0.12	0.369	o	|	|	|	|	1.17

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23.417    0.00    0.12      0.368  o       |       |       |       |     1.17
23.500    0.00    0.12      0.368  o       |       |       |       |     1.17
23.583    0.00    0.12      0.367  o       |       |       |       |     1.17
23.667    0.00    0.12      0.366  o       |       |       |       |     1.16
23.750    0.00    0.12      0.365  o       |       |       |       |     1.16
23.833    0.00    0.12      0.364  o       |       |       |       |     1.16
23.917    0.00    0.12      0.363  o       |       |       |       |     1.16
24.000    0.00    0.12      0.363  o       |       |       |       |     1.15
24.083    0.00    0.12      0.362  o       |       |       |       |     1.15
24.167    0.00    0.12      0.361  o       |       |       |       |     1.15
24.250    0.00    0.11      0.360  o       |       |       |       |     1.15
24.333    0.00    0.11      0.359  o       |       |       |       |     1.15
24.417    0.00    0.11      0.359  o       |       |       |       |     1.14
24.500    0.00    0.11      0.358  o       |       |       |       |     1.14
24.583    0.00    0.11      0.357  o       |       |       |       |     1.14
24.667    0.00    0.11      0.356  o       |       |       |       |     1.14
24.750    0.00    0.11      0.356  o       |       |       |       |     1.14
24.833    0.00    0.11      0.355  o       |       |       |       |     1.13
24.917    0.00    0.11      0.354  o       |       |       |       |     1.13
25.000    0.00    0.11      0.353  o       |       |       |       |     1.13
25.083    0.00    0.11      0.353  o       |       |       |       |     1.13
25.167    0.00    0.11      0.352  o       |       |       |       |     1.13
25.250    0.00    0.11      0.351  o       |       |       |       |     1.12
25.333    0.00    0.11      0.350  o       |       |       |       |     1.12
25.417    0.00    0.11      0.350  o       |       |       |       |     1.12
25.500    0.00    0.11      0.349  o       |       |       |       |     1.12
25.583    0.00    0.11      0.348  o       |       |       |       |     1.12
25.667    0.00    0.11      0.347  o       |       |       |       |     1.11
25.750    0.00    0.10      0.347  o       |       |       |       |     1.11
25.833    0.00    0.10      0.346  o       |       |       |       |     1.11
25.917    0.00    0.10      0.345  o       |       |       |       |     1.11
26.000    0.00    0.10      0.345  o       |       |       |       |     1.11
26.083    0.00    0.10      0.344  o       |       |       |       |     1.11
26.167    0.00    0.10      0.343  o       |       |       |       |     1.10
26.250    0.00    0.10      0.342  o       |       |       |       |     1.10
26.333    0.00    0.10      0.342  o       |       |       |       |     1.10
26.417    0.00    0.10      0.341  o       |       |       |       |     1.10
26.500    0.00    0.10      0.340  o       |       |       |       |     1.10

 Remaining water in basin =    0.34 (Ac.Ft)

 ****************************HYDROGRAPH DATA****************************
                Number of intervals =   318
                Time interval =    5.0 (Min.)
                Maximum/Peak flow rate =        0.361 (CFS)
                Total volume =       0.384 (Ac.Ft)
         Status of hydrographs being held in storage
                    Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
         Peak (CFS)      0.000     0.000     0.000     0.000     0.000
         Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: PRO3102410.rte
**********HYDROGRAPH DATA**********
Number of intervals = 293
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.943 (CFS)
Total volume = 1.023 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 293
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.304	0.072	0.304	0.304
2.000	0.683	0.361	0.682	0.684
2.500	0.893	17.450	0.833	0.953
3.000	1.118	48.572	0.951	1.285

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0	0.5	0.97	1.46	1.94	Depth (Ft.)
0.083	0.03	0.00	0.000	O	|	|	|	|	0.00
0.167	0.08	0.00	0.001	OI	|	|	|	|	0.00
0.250	0.09	0.00	0.001	OI	|	|	|	|	0.00
0.333	0.11	0.00	0.002	OI	|	|	|	|	0.01
0.417	0.14	0.00	0.003	O I	|	|	|	|	0.01
0.500	0.14	0.00	0.004	O I	|	|	|	|	0.01
0.583	0.15	0.00	0.005	O I	|	|	|	|	0.02
0.667	0.15	0.00	0.006	O I	|	|	|	|	0.02
0.750	0.15	0.00	0.007	O I	|	|	|	|	0.02
0.833	0.16	0.00	0.008	O I	|	|	|	|	0.03
0.917	0.19	0.00	0.009	O I	|	|	|	|	0.03
1.000	0.19	0.00	0.010	O I	|	|	|	|	0.03
1.083	0.18	0.00	0.011	O I	|	|	|	|	0.04
1.167	0.16	0.00	0.013	O I	|	|	|	|	0.04
1.250	0.15	0.00	0.014	O I	|	|	|	|	0.04
1.333	0.15	0.00	0.015	O I	|	|	|	|	0.05
1.417	0.15	0.00	0.016	O I	|	|	|	|	0.05
1.500	0.15	0.00	0.017	O I	|	|	|	|	0.05
1.583	0.15	0.00	0.018	O I	|	|	|	|	0.06
1.667	0.15	0.00	0.018	O I	|	|	|	|	0.06
1.750	0.15	0.00	0.019	O I	|	|	|	|	0.06
1.833	0.16	0.00	0.021	O I	|	|	|	|	0.07

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1.917    0.19    0.01      0.022  o  I    |        |        |        |      0.07
2.000    0.19    0.01      0.023  o  I    |        |        |        |      0.08
2.083    0.19    0.01      0.024  o  I    |        |        |        |      0.08
2.167    0.20    0.01      0.026  o  I    |        |        |        |      0.08
2.250    0.20    0.01      0.027  o  I    |        |        |        |      0.09
2.333    0.20    0.01      0.028  o  I    |        |        |        |      0.09
2.417    0.20    0.01      0.029  o  I    |        |        |        |      0.10
2.500    0.20    0.01      0.031  o  I    |        |        |        |      0.10
2.583    0.21    0.01      0.032  o  I    |        |        |        |      0.11
2.667    0.24    0.01      0.034  o  I    |        |        |        |      0.11
2.750    0.24    0.01      0.035  o  I    |        |        |        |      0.12
2.833    0.24    0.01      0.037  o   I   |        |        |        |      0.12
2.917    0.24    0.01      0.038  o   I   |        |        |        |      0.13
3.000    0.24    0.01      0.040  o   I   |        |        |        |      0.13
3.083    0.24    0.01      0.042  o   I   |        |        |        |      0.14
3.167    0.24    0.01      0.043  o   I   |        |        |        |      0.14
3.250    0.24    0.01      0.045  o   I   |        |        |        |      0.15
3.333    0.24    0.01      0.046  o   I   |        |        |        |      0.15
3.417    0.24    0.01      0.048  o   I   |        |        |        |      0.16
3.500    0.24    0.01      0.050  o   I   |        |        |        |      0.16
3.583    0.24    0.01      0.051  o   I   |        |        |        |      0.17
3.667    0.24    0.01      0.053  o   I   |        |        |        |      0.17
3.750    0.24    0.01      0.055  o   I   |        |        |        |      0.18
3.833    0.26    0.01      0.056  o   I   |        |        |        |      0.18
3.917    0.28    0.01      0.058  o   I   |        |        |        |      0.19
4.000    0.29    0.01      0.060  o   I   |        |        |        |      0.20
4.083    0.29    0.01      0.062  o   I   |        |        |        |      0.20
4.167    0.29    0.02      0.064  o   I   |        |        |        |      0.21
4.250    0.29    0.02      0.066  o   I   |        |        |        |      0.22
4.333    0.31    0.02      0.068  o    I  |        |        |        |      0.22
4.417    0.33    0.02      0.070  o    I  |        |        |        |      0.23
4.500    0.34    0.02      0.072  o    I  |        |        |        |      0.24
4.583    0.34    0.02      0.074  o    I  |        |        |        |      0.24
4.667    0.34    0.02      0.076  o    I  |        |        |        |      0.25
4.750    0.34    0.02      0.079  o    I  |        |        |        |      0.26
4.833    0.36    0.02      0.081  o    I  |        |        |        |      0.27
4.917    0.38    0.02      0.083  o     I |        |        |        |      0.27
5.000    0.39    0.02      0.086  o     I |        |        |        |      0.28
5.083    0.36    0.02      0.088  o    I  |        |        |        |      0.29
5.167    0.31    0.02      0.090  o    I  |        |        |        |      0.30
5.250    0.30    0.02      0.092  o   I   |        |        |        |      0.30
5.333    0.31    0.02      0.094  o    I  |        |        |        |      0.31
5.417    0.33    0.02      0.096  o    I  |        |        |        |      0.32
5.500    0.34    0.02      0.099  o    I  |        |        |        |      0.32
5.583    0.36    0.02      0.101  o    I  |        |        |        |      0.33
5.667    0.38    0.02      0.103  o     I |        |        |        |      0.34
5.750    0.39    0.03      0.106  o     I |        |        |        |      0.35
5.833    0.39    0.03      0.108  o     I |        |        |        |      0.36
5.917    0.39    0.03      0.111  o     I |        |        |        |      0.36
6.000    0.39    0.03      0.113  o     I |        |        |        |      0.37
6.083    0.41    0.03      0.116  o     I |        |        |        |      0.38
6.167    0.43    0.03      0.118  o      I|        |        |        |      0.39
6.250    0.44    0.03      0.121  o      I|        |        |        |      0.40
6.333    0.44    0.03      0.124  o      I|        |        |        |      0.41
6.417    0.44    0.03      0.127  o      I|        |        |        |      0.42
6.500    0.44    0.03      0.130  o      I|        |        |        |      0.43
6.583    0.46    0.03      0.133  o      I|        |        |        |      0.44
6.667    0.48    0.03      0.136  o      I|        |        |        |      0.45
6.750    0.49    0.03      0.139  o       I        |        |        |      0.46
6.833    0.49    0.03      0.142  o       I        |        |        |      0.47
6.917    0.49    0.03      0.145  o       I        |        |        |      0.48
7.000    0.49    0.04      0.148  o       I        |        |        |      0.49
7.083    0.49    0.04      0.151  o       I        |        |        |      0.50
7.167    0.49    0.04      0.154  o       I        |        |        |      0.51
7.250    0.49    0.04      0.157  o       I        |        |        |      0.52
7.333    0.51    0.04      0.161  o       I        |        |        |      0.53
7.417    0.53    0.04      0.164  o       I        |        |        |      0.54
7.500    0.53    0.04      0.167  o       I        |        |        |      0.55
7.583    0.55    0.04      0.171  o       |I       |        |        |      0.56
7.667    0.58    0.04      0.174  o       |I       |        |        |      0.57
7.750    0.58    0.04      0.178  o       |I       |        |        |      0.59
7.833    0.60    0.04      0.182  o       |I       |        |        |      0.60
7.917    0.63    0.04      0.186  o       | I      |        |        |      0.61
8.000    0.63    0.04      0.190  o       | I      |        |        |      0.62
8.083    0.67    0.05      0.194  o       |  I     |        |        |      0.64
8.167    0.72    0.05      0.198  o       |  I     |        |        |      0.65
8.250    0.73    0.05      0.203  o       |  I     |        |        |      0.67
8.333    0.73    0.05      0.208  o       |   I    |        |        |      0.68
8.417    0.73    0.05      0.213  o       |   I    |        |        |      0.70
8.500    0.73    0.05      0.217  o       |   I    |        |        |      0.71
8.583    0.75    0.05      0.222  o       |   I    |        |        |      0.73
8.667    0.77    0.05      0.227  o       |   I    |        |        |      0.75
8.750    0.78    0.05      0.232  o       |   I    |        |        |      0.76
8.833    0.80    0.06      0.237  o       |    I   |        |        |      0.78
8.917    0.82    0.06      0.242  o       |    I   |        |        |      0.80
9.000    0.83    0.06      0.247  o       |    I   |        |        |      0.81
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 9.083    0.87    0.06      0.253  O       |      I |        |        |      0.83
 9.167    0.91    0.06      0.258  |O      |       I|        |        |      0.85
 9.250    0.92    0.06      0.264  |O      |       I|        |        |      0.87
 9.333    0.94    0.06      0.270  |O      |       I|        |        |      0.89
 9.417    0.97    0.07      0.277  |O      |       I|        |        |      0.91
 9.500    0.98    0.07      0.283  |O      |        I        |        |      0.93
 9.583    0.99    0.07      0.289  |O      |        I        |        |      0.95
 9.667    1.02    0.07      0.296  |O      |        I        |        |      0.97
 9.750    1.02    0.07      0.302  |O      |        I        |        |      0.99
 9.833    1.04    0.08      0.309  |O      |        |I       |        |      1.01
 9.917    1.07    0.08      0.315  |O      |        |I       |        |      1.03
10.000    1.07    0.09      0.322  |O      |        |I       |        |      1.05
10.083    0.96    0.09      0.329  |O      |       I|        |        |      1.06
10.167    0.80    0.09      0.334  |O      |     I  |        |        |      1.08
10.250    0.76    0.10      0.339  |O      |    I   |        |        |      1.09
10.333    0.75    0.10      0.343  |O      |    I   |        |        |      1.10
10.417    0.74    0.11      0.348  |O      |    I   |        |        |      1.12
10.500    0.73    0.11      0.352  |O      |    I   |        |        |      1.13
10.583    0.82    0.11      0.357  |O      |     I  |        |        |      1.14
10.667    0.93    0.12      0.362  |O      |       I|        |        |      1.15
10.750    0.96    0.12      0.367  |O      |       I|        |        |      1.17
10.833    0.97    0.12      0.373  | O     |       I|        |        |      1.18
10.917    0.98    0.13      0.379  | O     |        I        |        |      1.20
11.000    0.98    0.13      0.385  | O     |        I        |        |      1.21
11.083    0.96    0.14      0.391  | O     |       I|        |        |      1.23
11.167    0.94    0.14      0.396  | O     |       I|        |        |      1.24
11.250    0.93    0.15      0.402  | O     |       I|        |        |      1.26
11.333    0.93    0.15      0.407  | O     |       I|        |        |      1.27
11.417    0.93    0.15      0.413  | O     |       I|        |        |      1.29
11.500    0.93    0.16      0.418  | O     |       I|        |        |      1.30
11.583    0.90    0.16      0.423  | O     |      I |        |        |      1.31
11.667    0.85    0.17      0.428  | O     |      I |        |        |      1.33
11.750    0.84    0.17      0.433  | O     |     I  |        |        |      1.34
11.833    0.85    0.17      0.437  | O     |      I |        |        |      1.35
11.917    0.87    0.18      0.442  | O     |      I |        |        |      1.36
12.000    0.88    0.18      0.447  | O     |      I |        |        |      1.38
12.083    1.00    0.18      0.452  |  O    |        I        |        |      1.39
12.167    1.16    0.19      0.458  |  O    |        |  I     |        |      1.41
12.250    1.20    0.19      0.465  |  O    |        |  I     |        |      1.42
12.333    1.23    0.20      0.472  |  O    |        |   I    |        |      1.44
12.417    1.26    0.21      0.479  |  O    |        |   I    |        |      1.46
12.500    1.27    0.21      0.486  |  O    |        |   I    |        |      1.48
12.583    1.31    0.22      0.494  |  O    |        |    I   |        |      1.50
12.667    1.35    0.22      0.501  |  O    |        |     I  |        |      1.52
12.750    1.36    0.23      0.509  |  O    |        |     I  |        |      1.54
12.833    1.38    0.23      0.517  |  O    |        |     I  |        |      1.56
12.917    1.41    0.24      0.525  |  O    |        |      I|        |      1.58
13.000    1.42    0.25      0.533  |   O   |        |      I|        |      1.60
13.083    1.59    0.25      0.542  |   O   |        |        |  I     |      1.63
13.167    1.82    0.26      0.552  |   O   |        |        |     I  |      1.65
13.250    1.88    0.27      0.563  |   O   |        |        |      I|      1.68
13.333    1.91    0.28      0.574  |   O   |        |        |      I|      1.71
13.417    1.93    0.29      0.585  |   O   |        |        |      I|      1.74
13.500    1.94    0.30      0.596  |   O   |        |        |       I|     1.77
13.583    1.66    0.30      0.607  |   O   |        |        |  I     |      1.80
13.667    1.28    0.31      0.615  |    O  |        |    I   |        |      1.82
13.750    1.19    0.31      0.621  |    O  |        |  I     |        |      1.84
13.833    1.15    0.32      0.627  |    O  |        | I      |        |      1.85
13.917    1.13    0.32      0.633  |    O  |        | I      |        |      1.87
14.000    1.13    0.33      0.638  |    O  |        | I      |        |      1.88
14.083    1.19    0.33      0.644  |    O  |        |  I     |        |      1.90
14.167    1.29    0.34      0.650  |    O  |        |    I   |        |      1.91
14.250    1.31    0.34      0.657  |    O  |        |    I   |        |      1.93
14.333    1.30    0.35      0.663  |    O  |        |    I   |        |      1.95
14.417    1.28    0.35      0.670  |    O  |        |    I   |        |      1.97
14.500    1.28    0.36      0.676  |    O  |        |    I   |        |      1.98
14.583    1.27    0.36      0.683  |    O  |        |   I    |        |      2.00
14.667    1.27    0.74      0.688  |       |   O    |   I    |        |      2.01
14.750    1.27    0.97      0.691  |       |       O|   I    |        |      2.02
14.833    1.26    1.10      0.692  |       |        | O I    |        |      2.02
14.917    1.23    1.16      0.693  |       |        |  OI    |        |      2.02
15.000    1.23    1.19      0.693  |       |        |  OI    |        |      2.02
15.083    1.21    1.20      0.693  |       |        |  O     |        |      2.02
15.167    1.18    1.20      0.693  |       |        |  O     |        |      2.02
15.250    1.18    1.19      0.693  |       |        |  O     |        |      2.02
15.333    1.16    1.18      0.693  |       |        |  O     |        |      2.02
15.417    1.14    1.17      0.693  |       |        | IO     |        |      2.02
15.500    1.13    1.15      0.693  |       |        | O      |        |      2.02
15.583    1.06    1.13      0.692  |       |        |IO      |        |      2.02
15.667    0.97    1.08      0.692  |       |       I|O       |        |      2.02
15.750    0.95    1.02      0.691  |       |       IO       |        |      2.02
15.833    0.94    0.99      0.691  |       |       IO       |        |      2.02
15.917    0.93    0.96      0.690  |       |       O|       |        |      2.02
16.000    0.93    0.95      0.690  |       |       O|       |        |      2.02
16.083    0.67    0.88      0.689  |       |  I  O  |       |        |      2.02
16.167    0.33    0.72      0.687  |    I  |  O     |       |        |      2.01
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16.250	0.25	0.53	0.685	I o				2.00
16.333	0.22	0.40	0.684	I o				2.00
16.417	0.20	0.36	0.682	I o				2.00
16.500	0.20	0.36	0.681	I o				2.00
16.583	0.18	0.36	0.680	I o				1.99
16.667	0.16	0.36	0.679	I o				1.99
16.750	0.15	0.36	0.677	I o				1.99
16.833	0.15	0.36	0.676	I o				1.98
16.917	0.15	0.35	0.674	I o				1.98
17.000	0.15	0.35	0.673	I o				1.97
17.083	0.18	0.35	0.672	I o				1.97
17.167	0.23	0.35	0.671	I o				1.97
17.250	0.24	0.35	0.670	I o				1.97
17.333	0.24	0.35	0.669	I o				1.96
17.417	0.24	0.35	0.668	IO				1.96
17.500	0.24	0.35	0.668	IO				1.96
17.583	0.24	0.35	0.667	IO				1.96
17.667	0.24	0.35	0.666	IO				1.96
17.750	0.24	0.35	0.666	IO				1.95
17.833	0.23	0.35	0.665	I o				1.95
17.917	0.20	0.35	0.664	I o				1.95
18.000	0.20	0.35	0.663	I o				1.95
18.083	0.20	0.34	0.662	I o				1.94
18.167	0.20	0.34	0.661	I o				1.94
18.250	0.20	0.34	0.660	I o				1.94
18.333	0.20	0.34	0.659	I o				1.94
18.417	0.20	0.34	0.658	I o				1.93
18.500	0.20	0.34	0.657	I o				1.93
18.583	0.18	0.34	0.656	I o				1.93
18.667	0.16	0.34	0.655	I o				1.92
18.750	0.15	0.34	0.653	I o				1.92
18.833	0.13	0.34	0.652	I o				1.92
18.917	0.11	0.34	0.650	I o				1.91
19.000	0.10	0.33	0.649	I o				1.91
19.083	0.12	0.33	0.647	I o				1.91
19.167	0.14	0.33	0.646	I o				1.90
19.250	0.14	0.33	0.645	I o				1.90
19.333	0.16	0.33	0.643	I o				1.90
19.417	0.19	0.33	0.642	I o				1.89
19.500	0.19	0.33	0.641	I o				1.89
19.583	0.18	0.33	0.640	I o				1.89
19.667	0.16	0.33	0.639	I o				1.88
19.750	0.15	0.33	0.638	I o				1.88
19.833	0.13	0.33	0.637	I o				1.88
19.917	0.11	0.32	0.635	I o				1.87
20.000	0.10	0.32	0.634	I o				1.87
20.083	0.12	0.32	0.632	I o				1.87
20.167	0.14	0.32	0.631	I o				1.86
20.250	0.14	0.32	0.630	I o				1.86
20.333	0.15	0.32	0.629	I o				1.86
20.417	0.15	0.32	0.627	I o				1.85
20.500	0.15	0.32	0.626	I o				1.85
20.583	0.15	0.32	0.625	I o				1.85
20.667	0.15	0.32	0.624	I o				1.84
20.750	0.15	0.31	0.623	I o				1.84
20.833	0.13	0.31	0.621	I o				1.84
20.917	0.11	0.31	0.620	I o				1.83
21.000	0.10	0.31	0.619	I o				1.83
21.083	0.12	0.31	0.617	I o				1.83
21.167	0.14	0.31	0.616	I o				1.82
21.250	0.14	0.31	0.615	I o				1.82
21.333	0.13	0.31	0.614	I o				1.82
21.417	0.11	0.31	0.612	I o				1.81
21.500	0.10	0.31	0.611	I o				1.81
21.583	0.12	0.31	0.610	I o				1.81
21.667	0.14	0.30	0.608	I o				1.80
21.750	0.14	0.30	0.607	I o				1.80
21.833	0.13	0.30	0.606	I o				1.80
21.917	0.11	0.30	0.605	I o				1.79
22.000	0.10	0.30	0.603	I o				1.79
22.083	0.12	0.30	0.602	I o				1.79
22.167	0.14	0.30	0.601	I o				1.78
22.250	0.14	0.30	0.600	I o				1.78
22.333	0.13	0.30	0.599	I o				1.78
22.417	0.11	0.30	0.598	I o				1.77
22.500	0.10	0.29	0.596	I o				1.77
22.583	0.10	0.29	0.595	I o				1.77
22.667	0.10	0.29	0.594	I o				1.76
22.750	0.10	0.29	0.592	I o				1.76
22.833	0.10	0.29	0.591	I o				1.76
22.917	0.10	0.29	0.590	I o				1.75
23.000	0.10	0.29	0.588	I o				1.75
23.083	0.10	0.29	0.587	I o				1.75
23.167	0.10	0.29	0.586	I o				1.74
23.250	0.10	0.29	0.584	I o				1.74
23.333	0.10	0.28	0.583	I o				1.74

23.417	0.10	0.28	0.582	|I o	|	|	|	1.73
23.500	0.10	0.28	0.580	|I o	|	|	|	1.73
23.583	0.10	0.28	0.579	|I o	|	|	|	1.73
23.667	0.10	0.28	0.578	|I o	|	|	|	1.72
23.750	0.10	0.28	0.577	|I o	|	|	|	1.72
23.833	0.10	0.28	0.575	|I o	|	|	|	1.72
23.917	0.10	0.28	0.574	|I o	|	|	|	1.71
24.000	0.10	0.28	0.573	|I o	|	|	|	1.71
24.083	0.06	0.28	0.572	|I o	|	|	|	1.71
24.167	0.02	0.27	0.570	I o	|	|	|	1.70
24.250	0.01	0.27	0.568	I o	|	|	|	1.70
24.333	0.00	0.27	0.566	I o	|	|	|	1.69
24.417	0.00	0.27	0.564	I o	|	|	|	1.69
24.500	0.00	0.27	0.563	I o	|	|	|	1.68
24.583	0.00	0.27	0.561	I o	|	|	|	1.68
24.667	0.00	0.27	0.559	I o	|	|	|	1.67
24.750	0.00	0.27	0.557	I o	|	|	|	1.67
24.833	0.00	0.26	0.555	I o	|	|	|	1.66
24.917	0.00	0.26	0.553	I o	|	|	|	1.66
25.000	0.00	0.26	0.552	I o	|	|	|	1.65
25.083	0.00	0.26	0.550	I o	|	|	|	1.65
25.167	0.00	0.26	0.548	I o	|	|	|	1.64
25.250	0.00	0.26	0.546	I o	|	|	|	1.64
25.333	0.00	0.26	0.545	I o	|	|	|	1.63
25.417	0.00	0.25	0.543	I o	|	|	|	1.63
25.500	0.00	0.25	0.541	I o	|	|	|	1.63
25.583	0.00	0.25	0.539	I o	|	|	|	1.62
25.667	0.00	0.25	0.538	I o	|	|	|	1.62
25.750	0.00	0.25	0.536	I o	|	|	|	1.61
25.833	0.00	0.25	0.534	I o	|	|	|	1.61
25.917	0.00	0.25	0.532	I o	|	|	|	1.60
26.000	0.00	0.24	0.531	I o	|	|	|	1.60
26.083	0.00	0.24	0.529	I o	|	|	|	1.59
26.167	0.00	0.24	0.527	I o	|	|	|	1.59
26.250	0.00	0.24	0.526	I o	|	|	|	1.59
26.333	0.00	0.24	0.524	I o	|	|	|	1.58
26.417	0.00	0.24	0.522	I o	|	|	|	1.58
26.500	0.00	0.24	0.521	I o	|	|	|	1.57
26.583	0.00	0.24	0.519	I o	|	|	|	1.57
26.667	0.00	0.23	0.518	I o	|	|	|	1.56
26.750	0.00	0.23	0.516	I o	|	|	|	1.56
26.833	0.00	0.23	0.514	I o	|	|	|	1.56
26.917	0.00	0.23	0.513	I o	|	|	|	1.55
27.000	0.00	0.23	0.511	I o	|	|	|	1.55
27.083	0.00	0.23	0.510	I o	|	|	|	1.54
27.167	0.00	0.23	0.508	I o	|	|	|	1.54
27.250	0.00	0.23	0.506	I o	|	|	|	1.53
27.333	0.00	0.23	0.505	I o	|	|	|	1.53
27.417	0.00	0.22	0.503	I o	|	|	|	1.53
27.500	0.00	0.22	0.502	I o	|	|	|	1.52
27.583	0.00	0.22	0.500	I o	|	|	|	1.52
27.667	0.00	0.22	0.499	I o	|	|	|	1.51
27.750	0.00	0.22	0.497	I o	|	|	|	1.51
27.833	0.00	0.22	0.496	I o	|	|	|	1.51
27.917	0.00	0.22	0.494	I o	|	|	|	1.50
28.000	0.00	0.22	0.493	I o	|	|	|	1.50
28.083	0.00	0.21	0.491	I o	|	|	|	1.49
28.167	0.00	0.21	0.490	I o	|	|	|	1.49
28.250	0.00	0.21	0.488	I o	|	|	|	1.49
28.333	0.00	0.21	0.487	I o	|	|	|	1.48
28.417	0.00	0.21	0.485	I o	|	|	|	1.48
28.500	0.00	0.21	0.484	I o	|	|	|	1.47
28.583	0.00	0.21	0.483	I o	|	|	|	1.47
28.667	0.00	0.21	0.481	I o	|	|	|	1.47
28.750	0.00	0.21	0.480	I o	|	|	|	1.46
28.833	0.00	0.20	0.478	I o	|	|	|	1.46
28.917	0.00	0.20	0.477	I o	|	|	|	1.46
29.000	0.00	0.20	0.475	I o	|	|	|	1.45
29.083	0.00	0.20	0.474	I o	|	|	|	1.45
29.167	0.00	0.20	0.473	I o	|	|	|	1.45
29.250	0.00	0.20	0.471	I o	|	|	|	1.44
29.333	0.00	0.20	0.470	I o	|	|	|	1.44
29.417	0.00	0.20	0.469	I o	|	|	|	1.43
29.500	0.00	0.20	0.467	I o	|	|	|	1.43
29.583	0.00	0.20	0.466	I o	|	|	|	1.43
29.667	0.00	0.19	0.465	I o	|	|	|	1.42
29.750	0.00	0.19	0.463	I o	|	|	|	1.42
29.833	0.00	0.19	0.462	I o	|	|	|	1.42
29.917	0.00	0.19	0.461	I o	|	|	|	1.41
30.000	0.00	0.19	0.459	I o	|	|	|	1.41
30.083	0.00	0.19	0.458	I o	|	|	|	1.41
30.167	0.00	0.19	0.457	I o	|	|	|	1.40
30.250	0.00	0.19	0.455	I o	|	|	|	1.40
30.333	0.00	0.19	0.454	I o	|	|	|	1.40
30.417	0.00	0.19	0.453	I o	|	|	|	1.39
30.500	0.00	0.18	0.451	I o	|	|	|	1.39

30.583	0.00	0.18	0.450	I o				1.39
30.667	0.00	0.18	0.449	I o				1.38
30.750	0.00	0.18	0.448	I o				1.38
30.833	0.00	0.18	0.446	I o				1.38
30.917	0.00	0.18	0.445	I o				1.37
31.000	0.00	0.18	0.444	I o				1.37
31.083	0.00	0.18	0.443	I o				1.37
31.167	0.00	0.18	0.442	I o				1.36
31.250	0.00	0.18	0.440	I o				1.36
31.333	0.00	0.18	0.439	I o				1.36
31.417	0.00	0.17	0.438	I o				1.35
31.500	0.00	0.17	0.437	I o				1.35
31.583	0.00	0.17	0.436	I o				1.35
31.667	0.00	0.17	0.434	I o				1.34
31.750	0.00	0.17	0.433	I o				1.34
31.833	0.00	0.17	0.432	I o				1.34
31.917	0.00	0.17	0.431	I o				1.33
32.000	0.00	0.17	0.430	I o				1.33
32.083	0.00	0.17	0.429	I o				1.33
32.167	0.00	0.17	0.427	I o				1.33
32.250	0.00	0.17	0.426	I o				1.32
32.333	0.00	0.16	0.425	I o				1.32
32.417	0.00	0.16	0.424	I o				1.32
32.500	0.00	0.16	0.423	I o				1.31
32.583	0.00	0.16	0.422	I o				1.31
32.667	0.00	0.16	0.421	I o				1.31
32.750	0.00	0.16	0.419	I o				1.30
32.833	0.00	0.16	0.418	I o				1.30
32.917	0.00	0.16	0.417	I o				1.30
33.000	0.00	0.16	0.416	I o				1.30
33.083	0.00	0.16	0.415	I o				1.29
33.167	0.00	0.16	0.414	I o				1.29
33.250	0.00	0.16	0.413	I o				1.29
33.333	0.00	0.15	0.412	I o				1.28
33.417	0.00	0.15	0.411	I o				1.28
33.500	0.00	0.15	0.410	I o				1.28
33.583	0.00	0.15	0.409	I o				1.28
33.667	0.00	0.15	0.408	I o				1.27
33.750	0.00	0.15	0.407	I o				1.27
33.833	0.00	0.15	0.406	I o				1.27
33.917	0.00	0.15	0.405	I o				1.27
34.000	0.00	0.15	0.404	I o				1.26
34.083	0.00	0.15	0.403	I o				1.26
34.167	0.00	0.15	0.402	I o				1.26
34.250	0.00	0.15	0.401	I o				1.25
34.333	0.00	0.14	0.400	I o				1.25
34.417	0.00	0.14	0.399	I o				1.25
34.500	0.00	0.14	0.398	I o				1.25
34.583	0.00	0.14	0.397	I o				1.24
34.667	0.00	0.14	0.396	I o				1.24
34.750	0.00	0.14	0.395	I o				1.24
34.833	0.00	0.14	0.394	I o				1.24
34.917	0.00	0.14	0.393	I o				1.23
35.000	0.00	0.14	0.392	I o				1.23
35.083	0.00	0.14	0.391	I o				1.23
35.167	0.00	0.14	0.390	I o				1.23
35.250	0.00	0.14	0.389	I o				1.22
35.333	0.00	0.14	0.388	I o				1.22
35.417	0.00	0.14	0.387	I o				1.22
35.500	0.00	0.13	0.386	I o				1.22
35.583	0.00	0.13	0.385	I o				1.21
35.667	0.00	0.13	0.384	I o				1.21
35.750	0.00	0.13	0.383	I o				1.21
35.833	0.00	0.13	0.382	I o				1.21
35.917	0.00	0.13	0.382	I o				1.20
36.000	0.00	0.13	0.381	I o				1.20
36.083	0.00	0.13	0.380	I o				1.20
36.167	0.00	0.13	0.379	I o				1.20
36.250	0.00	0.13	0.378	I o				1.20
36.333	0.00	0.13	0.377	I o				1.19
36.417	0.00	0.13	0.376	I o				1.19
36.500	0.00	0.13	0.375	I o				1.19
36.583	0.00	0.13	0.374	I o				1.19
36.667	0.00	0.13	0.374	I o				1.18
36.750	0.00	0.12	0.373	I o				1.18
36.833	0.00	0.12	0.372	I o				1.18
36.917	0.00	0.12	0.371	I o				1.18
37.000	0.00	0.12	0.370	I o				1.17
37.083	0.00	0.12	0.369	I o				1.17
37.167	0.00	0.12	0.368	IO				1.17
37.250	0.00	0.12	0.368	IO				1.17
37.333	0.00	0.12	0.367	IO				1.17
37.417	0.00	0.12	0.366	IO				1.16
37.500	0.00	0.12	0.365	IO				1.16
37.583	0.00	0.12	0.364	IO				1.16
37.667	0.00	0.12	0.364	IO				1.16

37.750	0.00	0.12	0.363	IO	|	|	|	|	1.16
37.833	0.00	0.12	0.362	IO	|	|	|	|	1.15
37.917	0.00	0.12	0.361	IO	|	|	|	|	1.15
38.000	0.00	0.11	0.360	IO	|	|	|	|	1.15
38.083	0.00	0.11	0.360	IO	|	|	|	|	1.15
38.167	0.00	0.11	0.359	IO	|	|	|	|	1.14
38.250	0.00	0.11	0.358	IO	|	|	|	|	1.14
38.333	0.00	0.11	0.357	IO	|	|	|	|	1.14
38.417	0.00	0.11	0.356	IO	|	|	|	|	1.14
38.500	0.00	0.11	0.356	IO	|	|	|	|	1.14
38.583	0.00	0.11	0.355	IO	|	|	|	|	1.13
38.667	0.00	0.11	0.354	IO	|	|	|	|	1.13
38.750	0.00	0.11	0.353	IO	|	|	|	|	1.13
38.833	0.00	0.11	0.353	IO	|	|	|	|	1.13
38.917	0.00	0.11	0.352	IO	|	|	|	|	1.13
39.000	0.00	0.11	0.351	IO	|	|	|	|	1.12
39.083	0.00	0.11	0.350	IO	|	|	|	|	1.12
39.167	0.00	0.11	0.350	IO	|	|	|	|	1.12
39.250	0.00	0.11	0.349	IO	|	|	|	|	1.12
39.333	0.00	0.11	0.348	IO	|	|	|	|	1.12
39.417	0.00	0.11	0.347	IO	|	|	|	|	1.11
39.500	0.00	0.10	0.347	IO	|	|	|	|	1.11
39.583	0.00	0.10	0.346	IO	|	|	|	|	1.11
39.667	0.00	0.10	0.345	IO	|	|	|	|	1.11
39.750	0.00	0.10	0.345	IO	|	|	|	|	1.11
39.833	0.00	0.10	0.344	IO	|	|	|	|	1.11
39.917	0.00	0.10	0.343	IO	|	|	|	|	1.10
40.000	0.00	0.10	0.343	IO	|	|	|	|	1.10
40.083	0.00	0.10	0.342	IO	|	|	|	|	1.10
40.167	0.00	0.10	0.341	IO	|	|	|	|	1.10
40.250	0.00	0.10	0.340	IO	|	|	|	|	1.10

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 483
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 1.204 (CFS)
Total volume = 0.683 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: PRO31001100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 17
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 21.922 (CFS)
Total volume = 0.711 (Ac.Ft)
Status of hydrographs being held in storage
Stream 1 Stream 2 Stream 3 Stream 4 Stream 5
Peak (CFS) 0.000 0.000 0.000 0.000 0.000
Vol (Ac.Ft) 0.000 0.000 0.000 0.000 0.000
****

++++++++++
Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 17
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.304	0.072	0.304	0.304
2.000	0.683	0.361	0.682	0.684
2.500	0.893	17.450	0.833	0.953
3.000	1.118	48.572	0.951	1.285

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 5.5 10.96 16.44 21.92	Depth (Ft.)
0.083	0.85	0.00	0.003	OI	0.01
0.167	2.37	0.00	0.014	O I	0.05
0.250	3.23	0.01	0.033	O I	0.11
0.333	3.75	0.01	0.057	O I	0.19
0.417	4.28	0.02	0.085	O I	0.28
0.500	5.04	0.03	0.117	O I	0.38
0.583	5.96	0.04	0.154	O I	0.51
0.667	7.33	0.05	0.200	O I	0.66
0.750	10.81	0.06	0.262	O I	0.86
0.833	21.56	0.12	0.373	O I	1.18
0.917	21.92	0.24	0.521	O I	1.57
1.000	9.35	0.32	0.627	O I	1.85
1.083	4.33	0.35	0.672	O I	1.97
1.167	1.63	0.80	0.688	OI	2.01
1.250	0.63	0.94	0.690	IO	2.02
1.333	0.13	0.70	0.687	IO	2.01
1.417	0.03	0.43	0.684	O	2.00
1.500	0.00	0.36	0.681	O	2.00
1.583	0.00	0.36	0.679	O	1.99
1.667	0.00	0.36	0.676	O	1.98
1.750	0.00	0.35	0.674	O	1.98
1.833	0.00	0.35	0.671	O	1.97

1.917	0.00	0.35	0.669	o	|	|	|	1.96
2.000	0.00	0.35	0.667	o	|	|	|	1.96
2.083	0.00	0.35	0.664	o	|	|	|	1.95
2.167	0.00	0.34	0.662	o	|	|	|	1.94
2.250	0.00	0.34	0.659	o	|	|	|	1.94
2.333	0.00	0.34	0.657	o	|	|	|	1.93
2.417	0.00	0.34	0.655	o	|	|	|	1.93
2.500	0.00	0.34	0.652	o	|	|	|	1.92
2.583	0.00	0.34	0.650	o	|	|	|	1.91
2.667	0.00	0.33	0.648	o	|	|	|	1.91
2.750	0.00	0.33	0.645	o	|	|	|	1.90
2.833	0.00	0.33	0.643	o	|	|	|	1.89
2.917	0.00	0.33	0.641	o	|	|	|	1.89
3.000	0.00	0.33	0.639	o	|	|	|	1.88
3.083	0.00	0.33	0.636	o	|	|	|	1.88
3.167	0.00	0.32	0.634	o	|	|	|	1.87
3.250	0.00	0.32	0.632	o	|	|	|	1.87
3.333	0.00	0.32	0.630	o	|	|	|	1.86
3.417	0.00	0.32	0.628	o	|	|	|	1.85
3.500	0.00	0.32	0.625	o	|	|	|	1.85
3.583	0.00	0.32	0.623	o	|	|	|	1.84
3.667	0.00	0.31	0.621	o	|	|	|	1.84
3.750	0.00	0.31	0.619	o	|	|	|	1.83
3.833	0.00	0.31	0.617	o	|	|	|	1.83
3.917	0.00	0.31	0.615	o	|	|	|	1.82
4.000	0.00	0.31	0.612	o	|	|	|	1.81
4.083	0.00	0.31	0.610	o	|	|	|	1.81
4.167	0.00	0.30	0.608	o	|	|	|	1.80
4.250	0.00	0.30	0.606	o	|	|	|	1.80
4.333	0.00	0.30	0.604	o	|	|	|	1.79
4.417	0.00	0.30	0.602	o	|	|	|	1.79
4.500	0.00	0.30	0.600	o	|	|	|	1.78
4.583	0.00	0.30	0.598	o	|	|	|	1.78
4.667	0.00	0.29	0.596	o	|	|	|	1.77
4.750	0.00	0.29	0.594	o	|	|	|	1.76
4.833	0.00	0.29	0.592	o	|	|	|	1.76
4.917	0.00	0.29	0.590	o	|	|	|	1.75
5.000	0.00	0.29	0.588	o	|	|	|	1.75
5.083	0.00	0.29	0.586	o	|	|	|	1.74
5.167	0.00	0.29	0.584	o	|	|	|	1.74
5.250	0.00	0.28	0.582	o	|	|	|	1.73
5.333	0.00	0.28	0.580	o	|	|	|	1.73
5.417	0.00	0.28	0.578	o	|	|	|	1.72
5.500	0.00	0.28	0.576	o	|	|	|	1.72
5.583	0.00	0.28	0.574	o	|	|	|	1.71
5.667	0.00	0.28	0.572	o	|	|	|	1.71
5.750	0.00	0.28	0.570	o	|	|	|	1.70
5.833	0.00	0.27	0.568	o	|	|	|	1.70
5.917	0.00	0.27	0.567	o	|	|	|	1.69
6.000	0.00	0.27	0.565	o	|	|	|	1.69
6.083	0.00	0.27	0.563	o	|	|	|	1.68
6.167	0.00	0.27	0.561	o	|	|	|	1.68
6.250	0.00	0.27	0.559	o	|	|	|	1.67
6.333	0.00	0.27	0.557	o	|	|	|	1.67
6.417	0.00	0.26	0.556	o	|	|	|	1.66
6.500	0.00	0.26	0.554	o	|	|	|	1.66
6.583	0.00	0.26	0.552	o	|	|	|	1.65
6.667	0.00	0.26	0.550	o	|	|	|	1.65
6.750	0.00	0.26	0.548	o	|	|	|	1.64
6.833	0.00	0.26	0.547	o	|	|	|	1.64
6.917	0.00	0.26	0.545	o	|	|	|	1.64
7.000	0.00	0.25	0.543	o	|	|	|	1.63
7.083	0.00	0.25	0.541	o	|	|	|	1.63
7.167	0.00	0.25	0.540	o	|	|	|	1.62
7.250	0.00	0.25	0.538	o	|	|	|	1.62
7.333	0.00	0.25	0.536	o	|	|	|	1.61
7.417	0.00	0.25	0.534	o	|	|	|	1.61
7.500	0.00	0.25	0.533	o	|	|	|	1.60
7.583	0.00	0.25	0.531	o	|	|	|	1.60
7.667	0.00	0.24	0.529	o	|	|	|	1.59
7.750	0.00	0.24	0.528	o	|	|	|	1.59
7.833	0.00	0.24	0.526	o	|	|	|	1.59
7.917	0.00	0.24	0.524	o	|	|	|	1.58
8.000	0.00	0.24	0.523	o	|	|	|	1.58
8.083	0.00	0.24	0.521	o	|	|	|	1.57
8.167	0.00	0.24	0.519	o	|	|	|	1.57
8.250	0.00	0.24	0.518	o	|	|	|	1.56
8.333	0.00	0.23	0.516	o	|	|	|	1.56
8.417	0.00	0.23	0.515	o	|	|	|	1.56
8.500	0.00	0.23	0.513	o	|	|	|	1.55
8.583	0.00	0.23	0.511	o	|	|	|	1.55
8.667	0.00	0.23	0.510	o	|	|	|	1.54
8.750	0.00	0.23	0.508	o	|	|	|	1.54
8.833	0.00	0.23	0.507	o	|	|	|	1.53
8.917	0.00	0.23	0.505	o	|	|	|	1.53
9.000	0.00	0.22	0.504	o	|	|	|	1.53

9.083	0.00	0.22	0.502	o	|	|	|	|	1.52
9.167	0.00	0.22	0.500	o	|	|	|	|	1.52
9.250	0.00	0.22	0.499	o	|	|	|	|	1.51
9.333	0.00	0.22	0.497	o	|	|	|	|	1.51
9.417	0.00	0.22	0.496	o	|	|	|	|	1.51
9.500	0.00	0.22	0.494	o	|	|	|	|	1.50
9.583	0.00	0.22	0.493	o	|	|	|	|	1.50
9.667	0.00	0.21	0.491	o	|	|	|	|	1.49
9.750	0.00	0.21	0.490	o	|	|	|	|	1.49
9.833	0.00	0.21	0.489	o	|	|	|	|	1.49
9.917	0.00	0.21	0.487	o	|	|	|	|	1.48
10.000	0.00	0.21	0.486	o	|	|	|	|	1.48
10.083	0.00	0.21	0.484	o	|	|	|	|	1.48
10.167	0.00	0.21	0.483	o	|	|	|	|	1.47
10.250	0.00	0.21	0.481	o	|	|	|	|	1.47
10.333	0.00	0.21	0.480	o	|	|	|	|	1.46
10.417	0.00	0.21	0.478	o	|	|	|	|	1.46
10.500	0.00	0.20	0.477	o	|	|	|	|	1.46
10.583	0.00	0.20	0.476	o	|	|	|	|	1.45
10.667	0.00	0.20	0.474	o	|	|	|	|	1.45
10.750	0.00	0.20	0.473	o	|	|	|	|	1.45
10.833	0.00	0.20	0.471	o	|	|	|	|	1.44
10.917	0.00	0.20	0.470	o	|	|	|	|	1.44
11.000	0.00	0.20	0.469	o	|	|	|	|	1.43
11.083	0.00	0.20	0.467	o	|	|	|	|	1.43
11.167	0.00	0.20	0.466	o	|	|	|	|	1.43
11.250	0.00	0.19	0.465	o	|	|	|	|	1.42
11.333	0.00	0.19	0.463	o	|	|	|	|	1.42
11.417	0.00	0.19	0.462	o	|	|	|	|	1.42
11.500	0.00	0.19	0.461	o	|	|	|	|	1.41
11.583	0.00	0.19	0.459	o	|	|	|	|	1.41
11.667	0.00	0.19	0.458	o	|	|	|	|	1.41
11.750	0.00	0.19	0.457	o	|	|	|	|	1.40
11.833	0.00	0.19	0.455	o	|	|	|	|	1.40
11.917	0.00	0.19	0.454	o	|	|	|	|	1.40
12.000	0.00	0.19	0.453	o	|	|	|	|	1.39
12.083	0.00	0.18	0.452	o	|	|	|	|	1.39
12.167	0.00	0.18	0.450	o	|	|	|	|	1.39
12.250	0.00	0.18	0.449	o	|	|	|	|	1.38
12.333	0.00	0.18	0.448	o	|	|	|	|	1.38
12.417	0.00	0.18	0.447	o	|	|	|	|	1.38
12.500	0.00	0.18	0.445	o	|	|	|	|	1.37
12.583	0.00	0.18	0.444	o	|	|	|	|	1.37
12.667	0.00	0.18	0.443	o	|	|	|	|	1.37
12.750	0.00	0.18	0.442	o	|	|	|	|	1.36
12.833	0.00	0.18	0.440	o	|	|	|	|	1.36
12.917	0.00	0.18	0.439	o	|	|	|	|	1.36
13.000	0.00	0.17	0.438	o	|	|	|	|	1.35
13.083	0.00	0.17	0.437	o	|	|	|	|	1.35
13.167	0.00	0.17	0.436	o	|	|	|	|	1.35
13.250	0.00	0.17	0.434	o	|	|	|	|	1.34
13.333	0.00	0.17	0.433	o	|	|	|	|	1.34
13.417	0.00	0.17	0.432	o	|	|	|	|	1.34
13.500	0.00	0.17	0.431	o	|	|	|	|	1.34
13.583	0.00	0.17	0.430	o	|	|	|	|	1.33
13.667	0.00	0.17	0.429	o	|	|	|	|	1.33
13.750	0.00	0.17	0.428	o	|	|	|	|	1.33
13.833	0.00	0.17	0.426	o	|	|	|	|	1.32
13.917	0.00	0.16	0.425	o	|	|	|	|	1.32
14.000	0.00	0.16	0.424	o	|	|	|	|	1.32
14.083	0.00	0.16	0.423	o	|	|	|	|	1.31
14.167	0.00	0.16	0.422	o	|	|	|	|	1.31
14.250	0.00	0.16	0.421	o	|	|	|	|	1.31
14.333	0.00	0.16	0.420	o	|	|	|	|	1.31
14.417	0.00	0.16	0.419	o	|	|	|	|	1.30
14.500	0.00	0.16	0.417	o	|	|	|	|	1.30
14.583	0.00	0.16	0.416	o	|	|	|	|	1.30
14.667	0.00	0.16	0.415	o	|	|	|	|	1.29
14.750	0.00	0.16	0.414	o	|	|	|	|	1.29
14.833	0.00	0.16	0.413	o	|	|	|	|	1.29
14.917	0.00	0.15	0.412	o	|	|	|	|	1.29
15.000	0.00	0.15	0.411	o	|	|	|	|	1.28
15.083	0.00	0.15	0.410	o	|	|	|	|	1.28
15.167	0.00	0.15	0.409	o	|	|	|	|	1.28
15.250	0.00	0.15	0.408	o	|	|	|	|	1.27
15.333	0.00	0.15	0.407	o	|	|	|	|	1.27
15.417	0.00	0.15	0.406	o	|	|	|	|	1.27
15.500	0.00	0.15	0.405	o	|	|	|	|	1.27
15.583	0.00	0.15	0.404	o	|	|	|	|	1.26
15.667	0.00	0.15	0.403	o	|	|	|	|	1.26
15.750	0.00	0.15	0.402	o	|	|	|	|	1.26
15.833	0.00	0.15	0.401	o	|	|	|	|	1.26
15.917	0.00	0.14	0.400	o	|	|	|	|	1.25
16.000	0.00	0.14	0.399	o	|	|	|	|	1.25
16.083	0.00	0.14	0.398	o	|	|	|	|	1.25
16.167	0.00	0.14	0.397	o	|	|	|	|	1.24

16.250	0.00	0.14	0.396	o	|	|	|	1.24
16.333	0.00	0.14	0.395	o	|	|	|	1.24
16.417	0.00	0.14	0.394	o	|	|	|	1.24
16.500	0.00	0.14	0.393	o	|	|	|	1.23
16.583	0.00	0.14	0.392	o	|	|	|	1.23
16.667	0.00	0.14	0.391	o	|	|	|	1.23
16.750	0.00	0.14	0.390	o	|	|	|	1.23
16.833	0.00	0.14	0.389	o	|	|	|	1.22
16.917	0.00	0.14	0.388	o	|	|	|	1.22
17.000	0.00	0.14	0.387	o	|	|	|	1.22
17.083	0.00	0.13	0.386	o	|	|	|	1.22
17.167	0.00	0.13	0.385	o	|	|	|	1.21
17.250	0.00	0.13	0.384	o	|	|	|	1.21
17.333	0.00	0.13	0.383	o	|	|	|	1.21
17.417	0.00	0.13	0.383	o	|	|	|	1.21
17.500	0.00	0.13	0.382	o	|	|	|	1.20
17.583	0.00	0.13	0.381	o	|	|	|	1.20
17.667	0.00	0.13	0.380	o	|	|	|	1.20
17.750	0.00	0.13	0.379	o	|	|	|	1.20
17.833	0.00	0.13	0.378	o	|	|	|	1.20
17.917	0.00	0.13	0.377	o	|	|	|	1.19
18.000	0.00	0.13	0.376	o	|	|	|	1.19
18.083	0.00	0.13	0.375	o	|	|	|	1.19
18.167	0.00	0.13	0.375	o	|	|	|	1.19
18.250	0.00	0.13	0.374	o	|	|	|	1.18
18.333	0.00	0.12	0.373	o	|	|	|	1.18
18.417	0.00	0.12	0.372	o	|	|	|	1.18
18.500	0.00	0.12	0.371	o	|	|	|	1.18
18.583	0.00	0.12	0.370	o	|	|	|	1.17
18.667	0.00	0.12	0.369	o	|	|	|	1.17
18.750	0.00	0.12	0.369	o	|	|	|	1.17
18.833	0.00	0.12	0.368	o	|	|	|	1.17
18.917	0.00	0.12	0.367	o	|	|	|	1.17
19.000	0.00	0.12	0.366	o	|	|	|	1.16
19.083	0.00	0.12	0.365	o	|	|	|	1.16
19.167	0.00	0.12	0.364	o	|	|	|	1.16
19.250	0.00	0.12	0.364	o	|	|	|	1.16
19.333	0.00	0.12	0.363	o	|	|	|	1.16
19.417	0.00	0.12	0.362	o	|	|	|	1.15
19.500	0.00	0.12	0.361	o	|	|	|	1.15
19.583	0.00	0.12	0.360	o	|	|	|	1.15
19.667	0.00	0.11	0.360	o	|	|	|	1.15
19.750	0.00	0.11	0.359	o	|	|	|	1.14
19.833	0.00	0.11	0.358	o	|	|	|	1.14
19.917	0.00	0.11	0.357	o	|	|	|	1.14
20.000	0.00	0.11	0.357	o	|	|	|	1.14
20.083	0.00	0.11	0.356	o	|	|	|	1.14
20.167	0.00	0.11	0.355	o	|	|	|	1.13
20.250	0.00	0.11	0.354	o	|	|	|	1.13
20.333	0.00	0.11	0.354	o	|	|	|	1.13
20.417	0.00	0.11	0.353	o	|	|	|	1.13
20.500	0.00	0.11	0.352	o	|	|	|	1.13
20.583	0.00	0.11	0.351	o	|	|	|	1.12
20.667	0.00	0.11	0.351	o	|	|	|	1.12
20.750	0.00	0.11	0.350	o	|	|	|	1.12
20.833	0.00	0.11	0.349	o	|	|	|	1.12
20.917	0.00	0.11	0.348	o	|	|	|	1.12
21.000	0.00	0.11	0.348	o	|	|	|	1.11
21.083	0.00	0.10	0.347	o	|	|	|	1.11
21.167	0.00	0.10	0.346	o	|	|	|	1.11
21.250	0.00	0.10	0.345	o	|	|	|	1.11
21.333	0.00	0.10	0.345	o	|	|	|	1.11
21.417	0.00	0.10	0.344	o	|	|	|	1.11
21.500	0.00	0.10	0.343	o	|	|	|	1.10
21.583	0.00	0.10	0.343	o	|	|	|	1.10
21.667	0.00	0.10	0.342	o	|	|	|	1.10
21.750	0.00	0.10	0.341	o	|	|	|	1.10
21.833	0.00	0.10	0.341	o	|	|	|	1.10

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 262
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 0.942 (CFS)
Total volume = 0.371 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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                    FLOOD HYDROGRAPH ROUTING PROGRAM
                Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                            Study date: 06/03/24

      ---------------------------------------------------------------------



      Program License Serial Number 5006

      ---------------------------------------------------------------------
      ********************* HYDROGRAPH INFORMATION **********************

                  From study/file name: PRO31003100.rte
      ******************************HYDROGRAPH DATA******************************
                  Number of intervals =    41
                  Time interval =    5.0 (Min.)
                  Maximum/Peak flow rate =       12.163 (CFS)
                  Total volume =       0.922 (Ac.Ft)
             Status of hydrographs being held in storage
                       Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
             Peak (CFS)      0.000     0.000     0.000     0.000     0.000
             Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
      ***************************************************************************



      ++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
      Process from Point/Station        1.000 to Point/Station        2.000
      **** RETARDING BASIN ROUTING ****
      ________________________________________________________________________

      User entry of depth-outflow-storage data
      ---------------------------------------------------------------------
      Total number of inflow hydrograph intervals = 41
      Hydrograph time unit =  5.000 (Min.)
      Initial depth in storage basin =   0.00(Ft.)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Initial basin depth =   0.00 (Ft.)
      Initial basin storage =      0.00 (Ac.Ft)
      Initial basin outflow =   0.00 (CFS)
      ---------------------------------------------------------------------
      ---------------------------------------------------------------------
      Depth vs. Storage and Depth vs. Discharge data:
       Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
            (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
      ---------------------------------------------------------------------
         0.000      0.000      0.000      0.000        0.000
         1.000      0.304      0.072      0.304        0.304
         2.000      0.683      0.361      0.682        0.684
         2.500      0.893     17.450      0.833        0.953
         3.000      1.118     48.572      0.951        1.285
      ---------------------------------------------------------------------
                     Hydrograph Detention Basin Routing
      ---------------------------------------------------------------------

      Graph values: 'I'= unit inflow; 'O'=outflow at time shown
      ---------------------------------------------------------------------
       Time   Inflow  Outflow    Storage                                  Depth
      (Hours)  (CFS)   (CFS)     (Ac.Ft) .0       3.0    6.08    9.12   12.16 (Ft.)
       0.083    0.43    0.00      0.001  OI      |       |       |       |     0.00
       0.167    1.00    0.00      0.006  O I     |       |       |       |     0.02
       0.250    1.06    0.00      0.013  O I     |       |       |       |     0.04
       0.333    1.17    0.01      0.021  O  I    |       |       |       |     0.07
       0.417    1.35    0.01      0.030  O  I    |       |       |       |     0.10
       0.500    1.52    0.01      0.040  O  I    |       |       |       |     0.13
       0.583    1.57    0.01      0.050  O   I   |       |       |       |     0.16
       0.667    1.58    0.01      0.061  O   I   |       |       |       |     0.20
       0.750    1.73    0.02      0.072  O   I   |       |       |       |     0.24
       0.833    1.63    0.02      0.084  O   I   |       |       |       |     0.28
       0.917    1.51    0.02      0.094  O  I    |       |       |       |     0.31
       1.000    1.61    0.02      0.105  O   I   |       |       |       |     0.35
       1.083    2.00    0.03      0.117  O    I  |       |       |       |     0.39
       1.167    2.38    0.03      0.132  O     I |       |       |       |     0.43
       1.250    2.47    0.04      0.148  O     I |       |       |       |     0.49
       1.333    2.38    0.04      0.165  O     I |       |       |       |     0.54
       1.417    2.62    0.04      0.182  O     I |       |       |       |     0.60
       1.500    3.18    0.05      0.202  O       I       |       |       |     0.66
       1.583    3.17    0.05      0.223  O       I       |       |       |     0.73
       1.667    3.17    0.06      0.244  O       I       |       |       |     0.80
       1.750    3.80    0.06      0.268  O       |I      |       |       |     0.88
       1.833    4.24    0.07      0.295  O       |  I    |       |       |     0.97
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1.917	4.07	0.09	0.323	O	I				1.05
2.000	3.98	0.11	0.350	O	I				1.12
2.083	4.11	0.13	0.377	O	I				1.19
2.167	4.93	0.15	0.408	O	I				1.27
2.250	6.44	0.18	0.446	O	I				1.37
2.333	6.37	0.21	0.488	O	I				1.49
2.417	7.51	0.25	0.535	O	I				1.61
2.500	10.54	0.29	0.595	O	I				1.77
2.583	12.16	0.35	0.671	O	I				1.97
2.667	11.77	4.67	0.736	I	O				2.13
2.750	7.52	6.85	0.763	I	OI				2.19
2.833	3.66	6.30	0.756	I	O				2.17
2.917	2.55	4.90	0.739	I	O				2.13
3.000	1.65	3.67	0.724	I	O				2.10
3.083	0.67	2.57	0.710	IO					2.06
3.167	0.20	1.64	0.699	IO					2.04
3.250	0.08	0.98	0.691	I O					2.02
3.333	0.03	0.58	0.686	IO					2.01
3.417	0.01	0.36	0.683	O					2.00
3.500	0.00	0.36	0.680	O					1.99
3.583	0.00	0.36	0.678	O					1.99
3.667	0.00	0.36	0.675	O					1.98
3.750	0.00	0.35	0.673	O					1.97
3.833	0.00	0.35	0.670	O					1.97
3.917	0.00	0.35	0.668	O					1.96
4.000	0.00	0.35	0.665	O					1.95
4.083	0.00	0.35	0.663	O					1.95
4.167	0.00	0.34	0.661	O					1.94
4.250	0.00	0.34	0.658	O					1.93
4.333	0.00	0.34	0.656	O					1.93
4.417	0.00	0.34	0.654	O					1.92
4.500	0.00	0.34	0.651	O					1.92
4.583	0.00	0.34	0.649	O					1.91
4.667	0.00	0.33	0.647	O					1.90
4.750	0.00	0.33	0.644	O					1.90
4.833	0.00	0.33	0.642	O					1.89
4.917	0.00	0.33	0.640	O					1.89
5.000	0.00	0.33	0.638	O					1.88
5.083	0.00	0.32	0.635	O					1.87
5.167	0.00	0.32	0.633	O					1.87
5.250	0.00	0.32	0.631	O					1.86
5.333	0.00	0.32	0.629	O					1.86
5.417	0.00	0.32	0.627	O					1.85
5.500	0.00	0.32	0.624	O					1.85
5.583	0.00	0.31	0.622	O					1.84
5.667	0.00	0.31	0.620	O					1.83
5.750	0.00	0.31	0.618	O					1.83
5.833	0.00	0.31	0.616	O					1.82
5.917	0.00	0.31	0.614	O					1.82
6.000	0.00	0.31	0.611	O					1.81
6.083	0.00	0.30	0.609	O					1.81
6.167	0.00	0.30	0.607	O					1.80
6.250	0.00	0.30	0.605	O					1.79
6.333	0.00	0.30	0.603	O					1.79
6.417	0.00	0.30	0.601	O					1.78
6.500	0.00	0.30	0.599	O					1.78
6.583	0.00	0.30	0.597	O					1.77
6.667	0.00	0.29	0.595	O					1.77
6.750	0.00	0.29	0.593	O					1.76
6.833	0.00	0.29	0.591	O					1.76
6.917	0.00	0.29	0.589	O					1.75
7.000	0.00	0.29	0.587	O					1.75
7.083	0.00	0.29	0.585	O					1.74
7.167	0.00	0.28	0.583	O					1.74
7.250	0.00	0.28	0.581	O					1.73
7.333	0.00	0.28	0.579	O					1.73
7.417	0.00	0.28	0.577	O					1.72
7.500	0.00	0.28	0.575	O					1.72
7.583	0.00	0.28	0.573	O					1.71
7.667	0.00	0.28	0.571	O					1.71
7.750	0.00	0.27	0.570	O					1.70
7.833	0.00	0.27	0.568	O					1.70
7.917	0.00	0.27	0.566	O					1.69
8.000	0.00	0.27	0.564	O					1.69
8.083	0.00	0.27	0.562	O					1.68
8.167	0.00	0.27	0.560	O					1.68
8.250	0.00	0.27	0.558	O					1.67
8.333	0.00	0.26	0.557	O					1.67
8.417	0.00	0.26	0.555	O					1.66
8.500	0.00	0.26	0.553	O					1.66
8.583	0.00	0.26	0.551	O					1.65
8.667	0.00	0.26	0.549	O					1.65
8.750	0.00	0.26	0.548	O					1.64
8.833	0.00	0.26	0.546	O					1.64
8.917	0.00	0.26	0.544	O					1.63
9.000	0.00	0.25	0.542	O					1.63

9.083	0.00	0.25	0.541	o	|	|	|	|	1.62
9.167	0.00	0.25	0.539	o	|	|	|	|	1.62
9.250	0.00	0.25	0.537	o	|	|	|	|	1.61
9.333	0.00	0.25	0.535	o	|	|	|	|	1.61
9.417	0.00	0.25	0.534	o	|	|	|	|	1.61
9.500	0.00	0.25	0.532	o	|	|	|	|	1.60
9.583	0.00	0.24	0.530	o	|	|	|	|	1.60
9.667	0.00	0.24	0.529	o	|	|	|	|	1.59
9.750	0.00	0.24	0.527	o	|	|	|	|	1.59
9.833	0.00	0.24	0.525	o	|	|	|	|	1.58
9.917	0.00	0.24	0.524	o	|	|	|	|	1.58
10.000	0.00	0.24	0.522	o	|	|	|	|	1.58
10.083	0.00	0.24	0.520	o	|	|	|	|	1.57
10.167	0.00	0.24	0.519	o	|	|	|	|	1.57
10.250	0.00	0.23	0.517	o	|	|	|	|	1.56
10.333	0.00	0.23	0.515	o	|	|	|	|	1.56
10.417	0.00	0.23	0.514	o	|	|	|	|	1.55
10.500	0.00	0.23	0.512	o	|	|	|	|	1.55
10.583	0.00	0.23	0.511	o	|	|	|	|	1.55
10.667	0.00	0.23	0.509	o	|	|	|	|	1.54
10.750	0.00	0.23	0.508	o	|	|	|	|	1.54
10.833	0.00	0.23	0.506	o	|	|	|	|	1.53
10.917	0.00	0.22	0.504	o	|	|	|	|	1.53
11.000	0.00	0.22	0.503	o	|	|	|	|	1.52
11.083	0.00	0.22	0.501	o	|	|	|	|	1.52
11.167	0.00	0.22	0.500	o	|	|	|	|	1.52
11.250	0.00	0.22	0.498	o	|	|	|	|	1.51
11.333	0.00	0.22	0.497	o	|	|	|	|	1.51
11.417	0.00	0.22	0.495	o	|	|	|	|	1.50
11.500	0.00	0.22	0.494	o	|	|	|	|	1.50
11.583	0.00	0.22	0.492	o	|	|	|	|	1.50
11.667	0.00	0.21	0.491	o	|	|	|	|	1.49
11.750	0.00	0.21	0.489	o	|	|	|	|	1.49
11.833	0.00	0.21	0.488	o	|	|	|	|	1.49
11.917	0.00	0.21	0.486	o	|	|	|	|	1.48
12.000	0.00	0.21	0.485	o	|	|	|	|	1.48
12.083	0.00	0.21	0.484	o	|	|	|	|	1.47
12.167	0.00	0.21	0.482	o	|	|	|	|	1.47
12.250	0.00	0.21	0.481	o	|	|	|	|	1.47
12.333	0.00	0.21	0.479	o	|	|	|	|	1.46
12.417	0.00	0.20	0.478	o	|	|	|	|	1.46
12.500	0.00	0.20	0.476	o	|	|	|	|	1.45
12.583	0.00	0.20	0.475	o	|	|	|	|	1.45
12.667	0.00	0.20	0.474	o	|	|	|	|	1.45
12.750	0.00	0.20	0.472	o	|	|	|	|	1.44
12.833	0.00	0.20	0.471	o	|	|	|	|	1.44
12.917	0.00	0.20	0.469	o	|	|	|	|	1.44
13.000	0.00	0.20	0.468	o	|	|	|	|	1.43
13.083	0.00	0.20	0.467	o	|	|	|	|	1.43
13.167	0.00	0.20	0.465	o	|	|	|	|	1.43
13.250	0.00	0.19	0.464	o	|	|	|	|	1.42
13.333	0.00	0.19	0.463	o	|	|	|	|	1.42
13.417	0.00	0.19	0.461	o	|	|	|	|	1.42
13.500	0.00	0.19	0.460	o	|	|	|	|	1.41
13.583	0.00	0.19	0.459	o	|	|	|	|	1.41
13.667	0.00	0.19	0.457	o	|	|	|	|	1.41
13.750	0.00	0.19	0.456	o	|	|	|	|	1.40
13.833	0.00	0.19	0.455	o	|	|	|	|	1.40
13.917	0.00	0.19	0.454	o	|	|	|	|	1.39
14.000	0.00	0.19	0.452	o	|	|	|	|	1.39
14.083	0.00	0.18	0.451	o	|	|	|	|	1.39
14.167	0.00	0.18	0.450	o	|	|	|	|	1.38
14.250	0.00	0.18	0.449	o	|	|	|	|	1.38
14.333	0.00	0.18	0.447	o	|	|	|	|	1.38
14.417	0.00	0.18	0.446	o	|	|	|	|	1.37
14.500	0.00	0.18	0.445	o	|	|	|	|	1.37
14.583	0.00	0.18	0.444	o	|	|	|	|	1.37
14.667	0.00	0.18	0.442	o	|	|	|	|	1.37
14.750	0.00	0.18	0.441	o	|	|	|	|	1.36
14.833	0.00	0.18	0.440	o	|	|	|	|	1.36
14.917	0.00	0.17	0.439	o	|	|	|	|	1.36
15.000	0.00	0.17	0.438	o	|	|	|	|	1.35
15.083	0.00	0.17	0.436	o	|	|	|	|	1.35
15.167	0.00	0.17	0.435	o	|	|	|	|	1.35
15.250	0.00	0.17	0.434	o	|	|	|	|	1.34
15.333	0.00	0.17	0.433	o	|	|	|	|	1.34
15.417	0.00	0.17	0.432	o	|	|	|	|	1.34
15.500	0.00	0.17	0.430	o	|	|	|	|	1.33
15.583	0.00	0.17	0.429	o	|	|	|	|	1.33
15.667	0.00	0.17	0.428	o	|	|	|	|	1.33
15.750	0.00	0.17	0.427	o	|	|	|	|	1.32
15.833	0.00	0.16	0.426	o	|	|	|	|	1.32
15.917	0.00	0.16	0.425	o	|	|	|	|	1.32
16.000	0.00	0.16	0.424	o	|	|	|	|	1.32
16.083	0.00	0.16	0.422	o	|	|	|	|	1.31
16.167	0.00	0.16	0.421	o	|	|	|	|	1.31

16.250	0.00	0.16	0.420	o	|	|	|	|	1.31
16.333	0.00	0.16	0.419	o	|	|	|	|	1.30
16.417	0.00	0.16	0.418	o	|	|	|	|	1.30
16.500	0.00	0.16	0.417	o	|	|	|	|	1.30
16.583	0.00	0.16	0.416	o	|	|	|	|	1.30
16.667	0.00	0.16	0.415	o	|	|	|	|	1.29
16.750	0.00	0.16	0.414	o	|	|	|	|	1.29
16.833	0.00	0.15	0.413	o	|	|	|	|	1.29
16.917	0.00	0.15	0.412	o	|	|	|	|	1.28
17.000	0.00	0.15	0.411	o	|	|	|	|	1.28
17.083	0.00	0.15	0.409	o	|	|	|	|	1.28
17.167	0.00	0.15	0.408	o	|	|	|	|	1.28
17.250	0.00	0.15	0.407	o	|	|	|	|	1.27
17.333	0.00	0.15	0.406	o	|	|	|	|	1.27
17.417	0.00	0.15	0.405	o	|	|	|	|	1.27
17.500	0.00	0.15	0.404	o	|	|	|	|	1.26
17.583	0.00	0.15	0.403	o	|	|	|	|	1.26
17.667	0.00	0.15	0.402	o	|	|	|	|	1.26
17.750	0.00	0.15	0.401	o	|	|	|	|	1.26
17.833	0.00	0.15	0.400	o	|	|	|	|	1.25
17.917	0.00	0.14	0.399	o	|	|	|	|	1.25
18.000	0.00	0.14	0.398	o	|	|	|	|	1.25
18.083	0.00	0.14	0.397	o	|	|	|	|	1.25
18.167	0.00	0.14	0.396	o	|	|	|	|	1.24
18.250	0.00	0.14	0.395	o	|	|	|	|	1.24
18.333	0.00	0.14	0.394	o	|	|	|	|	1.24
18.417	0.00	0.14	0.393	o	|	|	|	|	1.24
18.500	0.00	0.14	0.392	o	|	|	|	|	1.23
18.583	0.00	0.14	0.391	o	|	|	|	|	1.23
18.667	0.00	0.14	0.390	o	|	|	|	|	1.23
18.750	0.00	0.14	0.390	o	|	|	|	|	1.23
18.833	0.00	0.14	0.389	o	|	|	|	|	1.22
18.917	0.00	0.14	0.388	o	|	|	|	|	1.22
19.000	0.00	0.14	0.387	o	|	|	|	|	1.22
19.083	0.00	0.13	0.386	o	|	|	|	|	1.22
19.167	0.00	0.13	0.385	o	|	|	|	|	1.21
19.250	0.00	0.13	0.384	o	|	|	|	|	1.21
19.333	0.00	0.13	0.383	o	|	|	|	|	1.21
19.417	0.00	0.13	0.382	o	|	|	|	|	1.21
19.500	0.00	0.13	0.381	o	|	|	|	|	1.20
19.583	0.00	0.13	0.380	o	|	|	|	|	1.20
19.667	0.00	0.13	0.379	o	|	|	|	|	1.20
19.750	0.00	0.13	0.379	o	|	|	|	|	1.20
19.833	0.00	0.13	0.378	o	|	|	|	|	1.19
19.917	0.00	0.13	0.377	o	|	|	|	|	1.19
20.000	0.00	0.13	0.376	o	|	|	|	|	1.19
20.083	0.00	0.13	0.375	o	|	|	|	|	1.19
20.167	0.00	0.13	0.374	o	|	|	|	|	1.19
20.250	0.00	0.12	0.373	o	|	|	|	|	1.18
20.333	0.00	0.12	0.372	o	|	|	|	|	1.18
20.417	0.00	0.12	0.372	o	|	|	|	|	1.18
20.500	0.00	0.12	0.371	o	|	|	|	|	1.18
20.583	0.00	0.12	0.370	o	|	|	|	|	1.17
20.667	0.00	0.12	0.369	o	|	|	|	|	1.17
20.750	0.00	0.12	0.368	o	|	|	|	|	1.17
20.833	0.00	0.12	0.367	o	|	|	|	|	1.17
20.917	0.00	0.12	0.367	o	|	|	|	|	1.17
21.000	0.00	0.12	0.366	o	|	|	|	|	1.16
21.083	0.00	0.12	0.365	o	|	|	|	|	1.16
21.167	0.00	0.12	0.364	o	|	|	|	|	1.16
21.250	0.00	0.12	0.363	o	|	|	|	|	1.16
21.333	0.00	0.12	0.363	o	|	|	|	|	1.15
21.417	0.00	0.12	0.362	o	|	|	|	|	1.15
21.500	0.00	0.12	0.361	o	|	|	|	|	1.15
21.583	0.00	0.11	0.360	o	|	|	|	|	1.15
21.667	0.00	0.11	0.359	o	|	|	|	|	1.15
21.750	0.00	0.11	0.359	o	|	|	|	|	1.14
21.833	0.00	0.11	0.358	o	|	|	|	|	1.14
21.917	0.00	0.11	0.357	o	|	|	|	|	1.14
22.000	0.00	0.11	0.356	o	|	|	|	|	1.14
22.083	0.00	0.11	0.355	o	|	|	|	|	1.14
22.167	0.00	0.11	0.355	o	|	|	|	|	1.13
22.250	0.00	0.11	0.354	o	|	|	|	|	1.13
22.333	0.00	0.11	0.353	o	|	|	|	|	1.13
22.417	0.00	0.11	0.352	o	|	|	|	|	1.13
22.500	0.00	0.11	0.352	o	|	|	|	|	1.13
22.583	0.00	0.11	0.351	o	|	|	|	|	1.12
22.667	0.00	0.11	0.350	o	|	|	|	|	1.12
22.750	0.00	0.11	0.349	o	|	|	|	|	1.12
22.833	0.00	0.11	0.349	o	|	|	|	|	1.12
22.917	0.00	0.11	0.348	o	|	|	|	|	1.12
23.000	0.00	0.10	0.347	o	|	|	|	|	1.11
23.083	0.00	0.10	0.347	o	|	|	|	|	1.11
23.167	0.00	0.10	0.346	o	|	|	|	|	1.11
23.250	0.00	0.10	0.345	o	|	|	|	|	1.11
23.333	0.00	0.10	0.344	o	|	|	|	|	1.11

```
23.417    0.00    0.10      0.344  o       |       |       |       |     1.10
23.500    0.00    0.10      0.343  o       |       |       |       |     1.10
23.583    0.00    0.10      0.342  o       |       |       |       |     1.10
23.667    0.00    0.10      0.342  o       |       |       |       |     1.10
23.750    0.00    0.10      0.341  o       |       |       |       |     1.10
23.833    0.00    0.10      0.340  o       |       |       |       |     1.10

      Remaining water in basin =    0.34 (Ac.Ft)

      ****************************HYDROGRAPH DATA****************************
                    Number of intervals =   286
                    Time interval =    5.0 (Min.)
                    Maximum/Peak flow rate =        6.846 (CFS)
                    Total volume =       0.582 (Ac.Ft)
             Status of hydrographs being held in storage
                       Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
             Peak (CFS)      0.000     0.000     0.000     0.000     0.000
             Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
      ************************************************************************

      ------------------------------------------------------------------
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                FLOOD HYDROGRAPH ROUTING PROGRAM
          Copyright (c) CIVILCADD/CIVILDESIGN, 1989 - 2004
                      Study date: 06/03/24

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Program License Serial Number 5006

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********************* HYDROGRAPH INFORMATION **********************

               From study/file name: PRO31006100.rte
*****************************HYDROGRAPH DATA*****************************
               Number of intervals =    77
               Time interval =    5.0 (Min.)
               Maximum/Peak flow rate =       12.206 (CFS)
               Total volume =       1.302 (Ac.Ft)
       Status of hydrographs being held in storage
                  Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
       Peak (CFS)      0.000     0.000     0.000     0.000     0.000
       Vol (Ac.Ft)      0.000     0.000     0.000     0.000     0.000
************************************************************************



++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++++
Process from Point/Station        1.000 to Point/Station        2.000
**** RETARDING BASIN ROUTING ****
____________________________________________________________________________

User entry of depth-outflow-storage data
------------------------------------------------------------------------
Total number of inflow hydrograph intervals = 77
Hydrograph time unit =  5.000 (Min.)
Initial depth in storage basin =   0.00(Ft.)
------------------------------------------------------------------------
------------------------------------------------------------------------
Initial basin depth =   0.00 (Ft.)
Initial basin storage =      0.00 (Ac.Ft)
Initial basin outflow =   0.00 (CFS)
------------------------------------------------------------------------
------------------------------------------------------------------------
Depth vs. Storage and Depth vs. Discharge data:
 Basin Depth  Storage    Outflow   (S-O*dt/2)   (S+O*dt/2)
     (Ft.)    (Ac.Ft)    (CFS)     (Ac.Ft)    (Ac.Ft)
------------------------------------------------------------------------
   0.000      0.000      0.000      0.000        0.000
   1.000      0.304      0.072      0.304        0.304
   2.000      0.683      0.361      0.682        0.684
   2.500      0.893     17.450      0.833        0.953
   3.000      1.118     48.572      0.951        1.285
------------------------------------------------------------------------
               Hydrograph Detention Basin Routing
------------------------------------------------------------------------

Graph values: 'I'= unit inflow; 'O'=outflow at time shown
------------------------------------------------------------------------
 Time   Inflow  Outflow    Storage                                    Depth
(Hours) (CFS)   (CFS)     (Ac.Ft) .0       3.1    6.10    9.15   12.21 (Ft.)
 0.083    0.25    0.00      0.001  O       |       |       |       |     0.00
 0.167    0.63    0.00      0.004  OI      |       |       |       |     0.01
 0.250    0.77    0.00      0.009  O I     |       |       |       |     0.03
 0.333    0.82    0.00      0.014  O I     |       |       |       |     0.05
 0.417    0.84    0.00      0.020  O I     |       |       |       |     0.06
 0.500    0.90    0.01      0.026  O I     |       |       |       |     0.08
 0.583    0.96    0.01      0.032  O I     |       |       |       |     0.11
 0.667    0.98    0.01      0.039  O I     |       |       |       |     0.13
 0.750    0.99    0.01      0.045  O I     |       |       |       |     0.15
 0.833    0.99    0.01      0.052  O I     |       |       |       |     0.17
 0.917    0.99    0.01      0.059  O I     |       |       |       |     0.19
 1.000    1.04    0.02      0.066  O I     |       |       |       |     0.22
 1.083    1.10    0.02      0.073  O I     |       |       |       |     0.24
 1.167    1.12    0.02      0.080  O I     |       |       |       |     0.26
 1.250    1.13    0.02      0.088  O I     |       |       |       |     0.29
 1.333    1.13    0.02      0.096  O I     |       |       |       |     0.31
 1.417    1.13    0.02      0.103  O I     |       |       |       |     0.34
 1.500    1.13    0.03      0.111  O I     |       |       |       |     0.36
 1.583    1.13    0.03      0.119  O I     |       |       |       |     0.39
 1.667    1.13    0.03      0.126  O I     |       |       |       |     0.41
 1.750    1.13    0.03      0.134  O I     |       |       |       |     0.44
 1.833    1.13    0.03      0.141  O I     |       |       |       |     0.46
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1.917    1.13    0.04      0.149  o I     |       |       |       |     0.49
2.000    1.18    0.04      0.157  o  I    |       |       |       |     0.51
2.083    1.20    0.04      0.164  o  I    |       |       |       |     0.54
2.167    1.20    0.04      0.172  o  I    |       |       |       |     0.57
2.250    1.25    0.04      0.181  o  I    |       |       |       |     0.59
2.333    1.26    0.04      0.189  o  I    |       |       |       |     0.62
2.417    1.27    0.05      0.197  o  I    |       |       |       |     0.65
2.500    1.27    0.05      0.206  o  I    |       |       |       |     0.68
2.583    1.27    0.05      0.214  o  I    |       |       |       |     0.70
2.667    1.27    0.05      0.223  o  I    |       |       |       |     0.73
2.750    1.32    0.05      0.231  o  I    |       |       |       |     0.76
2.833    1.39    0.06      0.240  o  I    |       |       |       |     0.79
2.917    1.40    0.06      0.249  o  I    |       |       |       |     0.82
3.000    1.41    0.06      0.259  o  I    |       |       |       |     0.85
3.083    1.41    0.06      0.268  o  I    |       |       |       |     0.88
3.167    1.46    0.07      0.277  o  I    |       |       |       |     0.91
3.250    1.53    0.07      0.287  o   I   |       |       |       |     0.94
3.333    1.54    0.07      0.297  o   I   |       |       |       |     0.98
3.417    1.63    0.07      0.308  o   I   |       |       |       |     1.01
3.500    1.84    0.08      0.319  o   I   |       |       |       |     1.04
3.583    2.09    0.09      0.332  o    I  |       |       |       |     1.07
3.667    2.27    0.10      0.346  o    I  |       |       |       |     1.11
3.750    2.41    0.12      0.362  o     I |       |       |       |     1.15
3.833    2.57    0.13      0.378  o     I |       |       |       |     1.20
3.917    2.71    0.14      0.395  o      I|       |       |       |     1.24
4.000    2.85    0.16      0.413  o      I|       |       |       |     1.29
4.083    2.99    0.17      0.432  o      I|       |       |       |     1.34
4.167    3.23    0.19      0.453  o       I       |       |       |     1.39
4.250    3.50    0.20      0.474  o       |I      |       |       |     1.45
4.333    3.78    0.22      0.498  o       |I      |       |       |     1.51
4.417    4.06    0.24      0.523  o       | I     |       |       |     1.58
4.500    4.24    0.26      0.550  o       |  I    |       |       |     1.65
4.583    4.39    0.28      0.578  o       |  I    |       |       |     1.72
4.667    4.65    0.30      0.607  o       |   I   |       |       |     1.80
4.750    4.92    0.33      0.638  o       |   I   |       |       |     1.88
4.833    5.09    0.35      0.670  o       |    I  |       |       |     1.97
4.917    5.24    1.66      0.699  |   O   |    I  |       |       |     2.04
5.000    5.49    3.28      0.719  |       O    I  |       |       |     2.09
5.083    6.16    4.40      0.733  |       |  O   I        |       |     2.12
5.167    7.36    5.43      0.745  |       |    O |  I     |       |     2.15
5.250    8.48    6.52      0.759  |       |      |O   I   |       |     2.18
5.333    9.40    7.58      0.772  |       |      |  O   I |       |     2.21
5.417   10.48    8.61      0.784  |       |      |    O |  I    |     2.24
5.500   12.21    9.81      0.799  |       |      |      |O      I     2.28
5.583    9.94   10.36      0.806  |       |      |      | IO    |     2.29
5.667    4.58    9.00      0.789  |       |  I   |      O|       |     2.25
5.750    2.31    6.57      0.759  |     I |      |O      |       |     2.18
5.833    1.38    4.50      0.734  |  I    |  O   |       |       |     2.12
5.917    0.84    3.01      0.716  | I   O |      |       |       |     2.08
6.000    0.47    1.98      0.703  |I   O  |      |       |       |     2.05
6.083    0.24    1.27      0.694  I  O    |      |       |       |     2.03
6.167    0.07    0.78      0.688  I O     |      |       |       |     2.01
6.250    0.03    0.46      0.684  IO      |      |       |       |     2.00
6.333    0.01    0.36      0.682  O       |      |       |       |     2.00
6.417    0.00    0.36      0.679  O       |      |       |       |     1.99
6.500    0.00    0.36      0.677  O       |      |       |       |     1.98
6.583    0.00    0.35      0.674  O       |      |       |       |     1.98
6.667    0.00    0.35      0.672  O       |      |       |       |     1.97
6.750    0.00    0.35      0.669  O       |      |       |       |     1.96
6.833    0.00    0.35      0.667  O       |      |       |       |     1.96
6.917    0.00    0.35      0.665  O       |      |       |       |     1.95
7.000    0.00    0.35      0.662  O       |      |       |       |     1.95
7.083    0.00    0.34      0.660  O       |      |       |       |     1.94
7.167    0.00    0.34      0.657  O       |      |       |       |     1.93
7.250    0.00    0.34      0.655  O       |      |       |       |     1.93
7.333    0.00    0.34      0.653  O       |      |       |       |     1.92
7.417    0.00    0.34      0.650  O       |      |       |       |     1.91
7.500    0.00    0.33      0.648  O       |      |       |       |     1.91
7.583    0.00    0.33      0.646  O       |      |       |       |     1.90
7.667    0.00    0.33      0.644  O       |      |       |       |     1.90
7.750    0.00    0.33      0.641  O       |      |       |       |     1.89
7.833    0.00    0.33      0.639  O       |      |       |       |     1.88
7.917    0.00    0.33      0.637  O       |      |       |       |     1.88
8.000    0.00    0.32      0.635  O       |      |       |       |     1.87
8.083    0.00    0.32      0.632  O       |      |       |       |     1.87
8.167    0.00    0.32      0.630  O       |      |       |       |     1.86
8.250    0.00    0.32      0.628  O       |      |       |       |     1.85
8.333    0.00    0.32      0.626  O       |      |       |       |     1.85
8.417    0.00    0.32      0.624  O       |      |       |       |     1.84
8.500    0.00    0.31      0.621  O       |      |       |       |     1.84
8.583    0.00    0.31      0.619  O       |      |       |       |     1.83
8.667    0.00    0.31      0.617  O       |      |       |       |     1.83
8.750    0.00    0.31      0.615  O       |      |       |       |     1.82
8.833    0.00    0.31      0.613  O       |      |       |       |     1.81
8.917    0.00    0.31      0.611  O       |      |       |       |     1.81
9.000    0.00    0.30      0.609  O       |      |       |       |     1.80
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9.083	0.00	0.30	0.606	o	|	|	|	|	1.80
9.167	0.00	0.30	0.604	o	|	|	|	|	1.79
9.250	0.00	0.30	0.602	o	|	|	|	|	1.79
9.333	0.00	0.30	0.600	o	|	|	|	|	1.78
9.417	0.00	0.30	0.598	o	|	|	|	|	1.78
9.500	0.00	0.29	0.596	o	|	|	|	|	1.77
9.583	0.00	0.29	0.594	o	|	|	|	|	1.77
9.667	0.00	0.29	0.592	o	|	|	|	|	1.76
9.750	0.00	0.29	0.590	o	|	|	|	|	1.76
9.833	0.00	0.29	0.588	o	|	|	|	|	1.75
9.917	0.00	0.29	0.586	o	|	|	|	|	1.74
10.000	0.00	0.29	0.584	o	|	|	|	|	1.74
10.083	0.00	0.28	0.582	o	|	|	|	|	1.73
10.167	0.00	0.28	0.580	o	|	|	|	|	1.73
10.250	0.00	0.28	0.578	o	|	|	|	|	1.72
10.333	0.00	0.28	0.576	o	|	|	|	|	1.72
10.417	0.00	0.28	0.575	o	|	|	|	|	1.71
10.500	0.00	0.28	0.573	o	|	|	|	|	1.71
10.583	0.00	0.28	0.571	o	|	|	|	|	1.70
10.667	0.00	0.27	0.569	o	|	|	|	|	1.70
10.750	0.00	0.27	0.567	o	|	|	|	|	1.69
10.833	0.00	0.27	0.565	o	|	|	|	|	1.69
10.917	0.00	0.27	0.563	o	|	|	|	|	1.68
11.000	0.00	0.27	0.561	o	|	|	|	|	1.68
11.083	0.00	0.27	0.559	o	|	|	|	|	1.67
11.167	0.00	0.27	0.558	o	|	|	|	|	1.67
11.250	0.00	0.26	0.556	o	|	|	|	|	1.66
11.333	0.00	0.26	0.554	o	|	|	|	|	1.66
11.417	0.00	0.26	0.552	o	|	|	|	|	1.65
11.500	0.00	0.26	0.550	o	|	|	|	|	1.65
11.583	0.00	0.26	0.549	o	|	|	|	|	1.65
11.667	0.00	0.26	0.547	o	|	|	|	|	1.64
11.750	0.00	0.26	0.545	o	|	|	|	|	1.64
11.833	0.00	0.25	0.543	o	|	|	|	|	1.63
11.917	0.00	0.25	0.542	o	|	|	|	|	1.63
12.000	0.00	0.25	0.540	o	|	|	|	|	1.62
12.083	0.00	0.25	0.538	o	|	|	|	|	1.62
12.167	0.00	0.25	0.536	o	|	|	|	|	1.61
12.250	0.00	0.25	0.535	o	|	|	|	|	1.61
12.333	0.00	0.25	0.533	o	|	|	|	|	1.60
12.417	0.00	0.25	0.531	o	|	|	|	|	1.60
12.500	0.00	0.24	0.530	o	|	|	|	|	1.60
12.583	0.00	0.24	0.528	o	|	|	|	|	1.59
12.667	0.00	0.24	0.526	o	|	|	|	|	1.59
12.750	0.00	0.24	0.525	o	|	|	|	|	1.58
12.833	0.00	0.24	0.523	o	|	|	|	|	1.58
12.917	0.00	0.24	0.521	o	|	|	|	|	1.57
13.000	0.00	0.24	0.520	o	|	|	|	|	1.57
13.083	0.00	0.24	0.518	o	|	|	|	|	1.56
13.167	0.00	0.23	0.516	o	|	|	|	|	1.56
13.250	0.00	0.23	0.515	o	|	|	|	|	1.56
13.333	0.00	0.23	0.513	o	|	|	|	|	1.55
13.417	0.00	0.23	0.512	o	|	|	|	|	1.55
13.500	0.00	0.23	0.510	o	|	|	|	|	1.54
13.583	0.00	0.23	0.508	o	|	|	|	|	1.54
13.667	0.00	0.23	0.507	o	|	|	|	|	1.54
13.750	0.00	0.23	0.505	o	|	|	|	|	1.53
13.833	0.00	0.22	0.504	o	|	|	|	|	1.53
13.917	0.00	0.22	0.502	o	|	|	|	|	1.52
14.000	0.00	0.22	0.501	o	|	|	|	|	1.52
14.083	0.00	0.22	0.499	o	|	|	|	|	1.52
14.167	0.00	0.22	0.498	o	|	|	|	|	1.51
14.250	0.00	0.22	0.496	o	|	|	|	|	1.51
14.333	0.00	0.22	0.495	o	|	|	|	|	1.50
14.417	0.00	0.22	0.493	o	|	|	|	|	1.50
14.500	0.00	0.22	0.492	o	|	|	|	|	1.50
14.583	0.00	0.21	0.490	o	|	|	|	|	1.49
14.667	0.00	0.21	0.489	o	|	|	|	|	1.49
14.750	0.00	0.21	0.487	o	|	|	|	|	1.48
14.833	0.00	0.21	0.486	o	|	|	|	|	1.48
14.917	0.00	0.21	0.484	o	|	|	|	|	1.48
15.000	0.00	0.21	0.483	o	|	|	|	|	1.47
15.083	0.00	0.21	0.482	o	|	|	|	|	1.47
15.167	0.00	0.21	0.480	o	|	|	|	|	1.46
15.250	0.00	0.21	0.479	o	|	|	|	|	1.46
15.333	0.00	0.20	0.477	o	|	|	|	|	1.46
15.417	0.00	0.20	0.476	o	|	|	|	|	1.45
15.500	0.00	0.20	0.474	o	|	|	|	|	1.45
15.583	0.00	0.20	0.473	o	|	|	|	|	1.45
15.667	0.00	0.20	0.472	o	|	|	|	|	1.44
15.750	0.00	0.20	0.470	o	|	|	|	|	1.44
15.833	0.00	0.20	0.469	o	|	|	|	|	1.44
15.917	0.00	0.20	0.468	o	|	|	|	|	1.43
16.000	0.00	0.20	0.466	o	|	|	|	|	1.43
16.083	0.00	0.19	0.465	o	|	|	|	|	1.42
16.167	0.00	0.19	0.464	o	|	|	|	|	1.42

16.250	0.00	0.19	0.462	o	|	|	|	|	1.42
16.333	0.00	0.19	0.461	o	|	|	|	|	1.41
16.417	0.00	0.19	0.460	o	|	|	|	|	1.41
16.500	0.00	0.19	0.458	o	|	|	|	|	1.41
16.583	0.00	0.19	0.457	o	|	|	|	|	1.40
16.667	0.00	0.19	0.456	o	|	|	|	|	1.40
16.750	0.00	0.19	0.454	o	|	|	|	|	1.40
16.833	0.00	0.19	0.453	o	|	|	|	|	1.39
16.917	0.00	0.18	0.452	o	|	|	|	|	1.39
17.000	0.00	0.18	0.451	o	|	|	|	|	1.39
17.083	0.00	0.18	0.449	o	|	|	|	|	1.38
17.167	0.00	0.18	0.448	o	|	|	|	|	1.38
17.250	0.00	0.18	0.447	o	|	|	|	|	1.38
17.333	0.00	0.18	0.446	o	|	|	|	|	1.37
17.417	0.00	0.18	0.444	o	|	|	|	|	1.37
17.500	0.00	0.18	0.443	o	|	|	|	|	1.37
17.583	0.00	0.18	0.442	o	|	|	|	|	1.36
17.667	0.00	0.18	0.441	o	|	|	|	|	1.36
17.750	0.00	0.18	0.439	o	|	|	|	|	1.36
17.833	0.00	0.17	0.438	o	|	|	|	|	1.35
17.917	0.00	0.17	0.437	o	|	|	|	|	1.35
18.000	0.00	0.17	0.436	o	|	|	|	|	1.35
18.083	0.00	0.17	0.435	o	|	|	|	|	1.34
18.167	0.00	0.17	0.434	o	|	|	|	|	1.34
18.250	0.00	0.17	0.432	o	|	|	|	|	1.34
18.333	0.00	0.17	0.431	o	|	|	|	|	1.34
18.417	0.00	0.17	0.430	o	|	|	|	|	1.33
18.500	0.00	0.17	0.429	o	|	|	|	|	1.33
18.583	0.00	0.17	0.428	o	|	|	|	|	1.33
18.667	0.00	0.17	0.427	o	|	|	|	|	1.32
18.750	0.00	0.16	0.425	o	|	|	|	|	1.32
18.833	0.00	0.16	0.424	o	|	|	|	|	1.32
18.917	0.00	0.16	0.423	o	|	|	|	|	1.31
19.000	0.00	0.16	0.422	o	|	|	|	|	1.31
19.083	0.00	0.16	0.421	o	|	|	|	|	1.31
19.167	0.00	0.16	0.420	o	|	|	|	|	1.31
19.250	0.00	0.16	0.419	o	|	|	|	|	1.30
19.333	0.00	0.16	0.418	o	|	|	|	|	1.30
19.417	0.00	0.16	0.417	o	|	|	|	|	1.30
19.500	0.00	0.16	0.415	o	|	|	|	|	1.29
19.583	0.00	0.16	0.414	o	|	|	|	|	1.29
19.667	0.00	0.16	0.413	o	|	|	|	|	1.29
19.750	0.00	0.15	0.412	o	|	|	|	|	1.29
19.833	0.00	0.15	0.411	o	|	|	|	|	1.28
19.917	0.00	0.15	0.410	o	|	|	|	|	1.28
20.000	0.00	0.15	0.409	o	|	|	|	|	1.28
20.083	0.00	0.15	0.408	o	|	|	|	|	1.27
20.167	0.00	0.15	0.407	o	|	|	|	|	1.27
20.250	0.00	0.15	0.406	o	|	|	|	|	1.27
20.333	0.00	0.15	0.405	o	|	|	|	|	1.27
20.417	0.00	0.15	0.404	o	|	|	|	|	1.26
20.500	0.00	0.15	0.403	o	|	|	|	|	1.26
20.583	0.00	0.15	0.402	o	|	|	|	|	1.26
20.667	0.00	0.15	0.401	o	|	|	|	|	1.26
20.750	0.00	0.15	0.400	o	|	|	|	|	1.25
20.833	0.00	0.14	0.399	o	|	|	|	|	1.25
20.917	0.00	0.14	0.398	o	|	|	|	|	1.25
21.000	0.00	0.14	0.397	o	|	|	|	|	1.25
21.083	0.00	0.14	0.396	o	|	|	|	|	1.24
21.167	0.00	0.14	0.395	o	|	|	|	|	1.24
21.250	0.00	0.14	0.394	o	|	|	|	|	1.24
21.333	0.00	0.14	0.393	o	|	|	|	|	1.23
21.417	0.00	0.14	0.392	o	|	|	|	|	1.23
21.500	0.00	0.14	0.391	o	|	|	|	|	1.23
21.583	0.00	0.14	0.390	o	|	|	|	|	1.23
21.667	0.00	0.14	0.389	o	|	|	|	|	1.22
21.750	0.00	0.14	0.388	o	|	|	|	|	1.22
21.833	0.00	0.14	0.387	o	|	|	|	|	1.22
21.917	0.00	0.13	0.386	o	|	|	|	|	1.22
22.000	0.00	0.13	0.385	o	|	|	|	|	1.21
22.083	0.00	0.13	0.385	o	|	|	|	|	1.21
22.167	0.00	0.13	0.384	o	|	|	|	|	1.21
22.250	0.00	0.13	0.383	o	|	|	|	|	1.21
22.333	0.00	0.13	0.382	o	|	|	|	|	1.21
22.417	0.00	0.13	0.381	o	|	|	|	|	1.20
22.500	0.00	0.13	0.380	o	|	|	|	|	1.20
22.583	0.00	0.13	0.379	o	|	|	|	|	1.20
22.667	0.00	0.13	0.378	o	|	|	|	|	1.20
22.750	0.00	0.13	0.377	o	|	|	|	|	1.19
22.833	0.00	0.13	0.376	o	|	|	|	|	1.19
22.917	0.00	0.13	0.376	o	|	|	|	|	1.19
23.000	0.00	0.13	0.375	o	|	|	|	|	1.19
23.083	0.00	0.13	0.374	o	|	|	|	|	1.18
23.167	0.00	0.12	0.373	o	|	|	|	|	1.18
23.250	0.00	0.12	0.372	o	|	|	|	|	1.18
23.333	0.00	0.12	0.371	o	|	|	|	|	1.18

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23.417    0.00    0.12      0.370  o       |       |       |       |     1.18
23.500    0.00    0.12      0.370  o       |       |       |       |     1.17
23.583    0.00    0.12      0.369  o       |       |       |       |     1.17
23.667    0.00    0.12      0.368  o       |       |       |       |     1.17
23.750    0.00    0.12      0.367  o       |       |       |       |     1.17
23.833    0.00    0.12      0.366  o       |       |       |       |     1.16
23.917    0.00    0.12      0.365  o       |       |       |       |     1.16
24.000    0.00    0.12      0.365  o       |       |       |       |     1.16
24.083    0.00    0.12      0.364  o       |       |       |       |     1.16
24.167    0.00    0.12      0.363  o       |       |       |       |     1.16
24.250    0.00    0.12      0.362  o       |       |       |       |     1.15
24.333    0.00    0.12      0.361  o       |       |       |       |     1.15
24.417    0.00    0.12      0.361  o       |       |       |       |     1.15
24.500    0.00    0.11      0.360  o       |       |       |       |     1.15
24.583    0.00    0.11      0.359  o       |       |       |       |     1.15
24.667    0.00    0.11      0.358  o       |       |       |       |     1.14
24.750    0.00    0.11      0.357  o       |       |       |       |     1.14
24.833    0.00    0.11      0.357  o       |       |       |       |     1.14
24.917    0.00    0.11      0.356  o       |       |       |       |     1.14
25.000    0.00    0.11      0.355  o       |       |       |       |     1.13
25.083    0.00    0.11      0.354  o       |       |       |       |     1.13
25.167    0.00    0.11      0.354  o       |       |       |       |     1.13
25.250    0.00    0.11      0.353  o       |       |       |       |     1.13
25.333    0.00    0.11      0.352  o       |       |       |       |     1.13
25.417    0.00    0.11      0.351  o       |       |       |       |     1.13
25.500    0.00    0.11      0.351  o       |       |       |       |     1.12
25.583    0.00    0.11      0.350  o       |       |       |       |     1.12
25.667    0.00    0.11      0.349  o       |       |       |       |     1.12
25.750    0.00    0.11      0.348  o       |       |       |       |     1.12
25.833    0.00    0.11      0.348  o       |       |       |       |     1.12
25.917    0.00    0.10      0.347  o       |       |       |       |     1.11
26.000    0.00    0.10      0.346  o       |       |       |       |     1.11
26.083    0.00    0.10      0.346  o       |       |       |       |     1.11
26.167    0.00    0.10      0.345  o       |       |       |       |     1.11
26.250    0.00    0.10      0.344  o       |       |       |       |     1.11
26.333    0.00    0.10      0.343  o       |       |       |       |     1.10
26.417    0.00    0.10      0.343  o       |       |       |       |     1.10
26.500    0.00    0.10      0.342  o       |       |       |       |     1.10
26.583    0.00    0.10      0.341  o       |       |       |       |     1.10
26.667    0.00    0.10      0.341  o       |       |       |       |     1.10

 Remaining water in basin =    0.34 (Ac.Ft)

 ****************************HYDROGRAPH DATA****************************
                 Number of intervals =   320
                 Time interval =    5.0 (Min.)
                 Maximum/Peak flow rate =       10.362 (CFS)
                 Total volume =       0.962 (Ac.Ft)
         Status of hydrographs being held in storage
                    Stream 1  Stream 2  Stream 3  Stream 4  Stream 5
         Peak (CFS)      0.000     0.000     0.000     0.000     0.000
         Vol (Ac.Ft)     0.000     0.000     0.000     0.000     0.000
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FLOOD HYDROGRAPH ROUTING PROGRAM
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Study date: 06/03/24

Program License Serial Number 5006

********** HYDROGRAPH INFORMATION **********

From study/file name: PRO310024100.rte
**********HYDROGRAPH DATA**********
Number of intervals = 293
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 3.955 (CFS)
Total volume = 1.848 (Ac.Ft)
Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

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Process from Point/Station 1.000 to Point/Station 2.000
**** RETARDING BASIN ROUTING ****

User entry of depth-outflow-storage data

Total number of inflow hydrograph intervals = 293
Hydrograph time unit = 5.000 (Min.)
Initial depth in storage basin = 0.00(Ft.)

Initial basin depth = 0.00 (Ft.)
Initial basin storage = 0.00 (Ac.Ft)
Initial basin outflow = 0.00 (CFS)

Depth vs. Storage and Depth vs. Discharge data:

Basin Depth (Ft.)	Storage (Ac.Ft)	Outflow (CFS)	(S-O*dt/2) (Ac.Ft)	(S+O*dt/2) (Ac.Ft)
0.000	0.000	0.000	0.000	0.000
1.000	0.304	0.072	0.304	0.304
2.000	0.683	0.361	0.682	0.684
2.500	0.893	17.450	0.833	0.953
3.000	1.118	48.572	0.951	1.285

Hydrograph Detention Basin Routing

Graph values: 'I'= unit inflow; 'O'=outflow at time shown

Time (Hours)	Inflow (CFS)	Outflow (CFS)	Storage (Ac.Ft)	.0 1.0 1.98 2.97 3.96	Depth (Ft.)
0.083	0.06	0.00	0.000	O	0.00
0.167	0.13	0.00	0.001	OI	0.00
0.250	0.14	0.00	0.002	OI	0.01
0.333	0.18	0.00	0.003	OI	0.01
0.417	0.22	0.00	0.004	OI	0.01
0.500	0.23	0.00	0.006	OI	0.02
0.583	0.23	0.00	0.007	OI	0.02
0.667	0.23	0.00	0.009	OI	0.03
0.750	0.24	0.00	0.011	OI	0.03
0.833	0.26	0.00	0.012	O I	0.04
0.917	0.30	0.00	0.014	O I	0.05
1.000	0.31	0.00	0.016	O I	0.05
1.083	0.28	0.00	0.018	O I	0.06
1.167	0.25	0.00	0.020	O I	0.07
1.250	0.24	0.01	0.022	OI	0.07
1.333	0.24	0.01	0.023	OI	0.08
1.417	0.24	0.01	0.025	OI	0.08
1.500	0.24	0.01	0.027	OI	0.09
1.583	0.24	0.01	0.028	OI	0.09
1.667	0.24	0.01	0.030	OI	0.10
1.750	0.24	0.01	0.031	OI	0.10
1.833	0.26	0.01	0.033	O I	0.11

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1.917    0.30    0.01      0.035  o I     |       |       |       |      0.11
2.000    0.31    0.01      0.037  o I     |       |       |       |      0.12
2.083    0.31    0.01      0.039  o I     |       |       |       |      0.13
2.167    0.31    0.01      0.041  o I     |       |       |       |      0.13
2.250    0.31    0.01      0.043  o I     |       |       |       |      0.14
2.333    0.31    0.01      0.045  o I     |       |       |       |      0.15
2.417    0.31    0.01      0.047  o I     |       |       |       |      0.16
2.500    0.31    0.01      0.049  o I     |       |       |       |      0.16
2.583    0.34    0.01      0.052  o I     |       |       |       |      0.17
2.667    0.38    0.01      0.054  o  I    |       |       |       |      0.18
2.750    0.39    0.01      0.056  o  I    |       |       |       |      0.19
2.833    0.39    0.01      0.059  o  I    |       |       |       |      0.19
2.917    0.39    0.01      0.062  o  I    |       |       |       |      0.20
3.000    0.39    0.02      0.064  o  I    |       |       |       |      0.21
3.083    0.39    0.02      0.067  o  I    |       |       |       |      0.22
3.167    0.39    0.02      0.069  o  I    |       |       |       |      0.23
3.250    0.39    0.02      0.072  o  I    |       |       |       |      0.24
3.333    0.39    0.02      0.075  o  I    |       |       |       |      0.25
3.417    0.39    0.02      0.077  o  I    |       |       |       |      0.25
3.500    0.39    0.02      0.080  o  I    |       |       |       |      0.26
3.583    0.39    0.02      0.082  o  I    |       |       |       |      0.27
3.667    0.39    0.02      0.085  o  I    |       |       |       |      0.28
3.750    0.39    0.02      0.087  o  I    |       |       |       |      0.29
3.833    0.42    0.02      0.090  o  I    |       |       |       |      0.30
3.917    0.46    0.02      0.093  o  I    |       |       |       |      0.31
4.000    0.47    0.02      0.096  o  I    |       |       |       |      0.32
4.083    0.47    0.02      0.099  o  I    |       |       |       |      0.33
4.167    0.47    0.02      0.102  o  I    |       |       |       |      0.34
4.250    0.47    0.02      0.105  o  I    |       |       |       |      0.35
4.333    0.50    0.03      0.108  o   I   |       |       |       |      0.36
4.417    0.54    0.03      0.112  o   I   |       |       |       |      0.37
4.500    0.54    0.03      0.115  o   I   |       |       |       |      0.38
4.583    0.55    0.03      0.119  o   I   |       |       |       |      0.39
4.667    0.55    0.03      0.122  o   I   |       |       |       |      0.40
4.750    0.55    0.03      0.126  o   I   |       |       |       |      0.41
4.833    0.58    0.03      0.130  o   I   |       |       |       |      0.43
4.917    0.61    0.03      0.134  o   I   |       |       |       |      0.44
5.000    0.62    0.03      0.138  o    I  |       |       |       |      0.45
5.083    0.57    0.03      0.141  o   I   |       |       |       |      0.47
5.167    0.50    0.03      0.145  o   I   |       |       |       |      0.48
5.250    0.48    0.04      0.148  o  I    |       |       |       |      0.49
5.333    0.50    0.04      0.151  o   I   |       |       |       |      0.50
5.417    0.54    0.04      0.155  o   I   |       |       |       |      0.51
5.500    0.54    0.04      0.158  o   I   |       |       |       |      0.52
5.583    0.57    0.04      0.162  o   I   |       |       |       |      0.53
5.667    0.61    0.04      0.165  o   I   |       |       |       |      0.54
5.750    0.62    0.04      0.169  o    I  |       |       |       |      0.56
5.833    0.63    0.04      0.173  o    I  |       |       |       |      0.57
5.917    0.63    0.04      0.177  o    I  |       |       |       |      0.58
6.000    0.63    0.04      0.182  o    I  |       |       |       |      0.60
6.083    0.66    0.04      0.186  o    I  |       |       |       |      0.61
6.167    0.69    0.04      0.190  o    I  |       |       |       |      0.62
6.250    0.70    0.05      0.194  o    I  |       |       |       |      0.64
6.333    0.70    0.05      0.199  o    I  |       |       |       |      0.65
6.417    0.71    0.05      0.204  o    I  |       |       |       |      0.67
6.500    0.71    0.05      0.208  o    I  |       |       |       |      0.68
6.583    0.73    0.05      0.213  o    I  |       |       |       |      0.70
6.667    0.77    0.05      0.218  o     I |       |       |       |      0.72
6.750    0.78    0.05      0.222  o     I |       |       |       |      0.73
6.833    0.78    0.05      0.227  o     I |       |       |       |      0.75
6.917    0.78    0.06      0.233  o     I |       |       |       |      0.76
7.000    0.79    0.06      0.238  o     I |       |       |       |      0.78
7.083    0.79    0.06      0.243  o     I |       |       |       |      0.80
7.167    0.79    0.06      0.248  o     I |       |       |       |      0.81
7.250    0.79    0.06      0.253  o     I |       |       |       |      0.83
7.333    0.81    0.06      0.258  o     I |       |       |       |      0.85
7.417    0.85    0.06      0.263  o     I |       |       |       |      0.87
7.500    0.86    0.06      0.268  o     I |       |       |       |      0.88
7.583    0.89    0.06      0.274  o      I|       |       |       |      0.90
7.667    0.93    0.07      0.280  o      I|       |       |       |      0.92
7.750    0.94    0.07      0.286  o      I|       |       |       |      0.94
7.833    0.97    0.07      0.292  o      I|       |       |       |      0.96
7.917    1.01    0.07      0.298  o       I       |       |       |      0.98
8.000    1.02    0.07      0.305  o       I       |       |       |      1.00
8.083    1.07    0.08      0.311  o       I       |       |       |      1.02
8.167    1.15    0.08      0.318  o       |I      |       |       |      1.04
8.250    1.17    0.09      0.326  o       |I      |       |       |      1.06
8.333    1.17    0.09      0.333  o       |I      |       |       |      1.08
8.417    1.18    0.10      0.341  o       |I      |       |       |      1.10
8.500    1.18    0.11      0.348  o       |I      |       |       |      1.12
8.583    1.21    0.11      0.355  o       |I      |       |       |      1.14
8.667    1.24    0.12      0.363  o       | I     |       |       |      1.16
8.750    1.25    0.12      0.371  o       | I     |       |       |      1.18
8.833    1.28    0.13      0.379  |o      | I     |       |       |      1.20
8.917    1.32    0.14      0.387  |o      | I     |       |       |      1.22
9.000    1.33    0.14      0.395  |o      | I     |       |       |      1.24
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9.083	1.39	0.15	0.403	O	I			1.26
9.167	1.46	0.15	0.412	O	I			1.29
9.250	1.48	0.16	0.421	O	I			1.31
9.333	1.52	0.17	0.430	O	I			1.33
9.417	1.56	0.18	0.440	O	I			1.36
9.500	1.56	0.18	0.449	O	I			1.38
9.583	1.60	0.19	0.459	O	I			1.41
9.667	1.63	0.20	0.469	O	I			1.43
9.750	1.64	0.21	0.479	O	I			1.46
9.833	1.68	0.21	0.489	O	I			1.49
9.917	1.72	0.22	0.499	O	I			1.51
10.000	1.74	0.23	0.509	O	I			1.54
10.083	1.55	0.24	0.519	O	I			1.57
10.167	1.28	0.24	0.527	O	I			1.59
10.250	1.22	0.25	0.534	O	I			1.61
10.333	1.20	0.25	0.541	O	I			1.62
10.417	1.18	0.26	0.547	O	I			1.64
10.500	1.18	0.26	0.553	O	I			1.66
10.583	1.32	0.27	0.560	O	I			1.68
10.667	1.50	0.27	0.568	O	I			1.70
10.750	1.54	0.28	0.576	O	I			1.72
10.833	1.56	0.29	0.585	O	I			1.74
10.917	1.57	0.29	0.594	O	I			1.77
11.000	1.57	0.30	0.603	O	I			1.79
11.083	1.54	0.31	0.611	O	I			1.81
11.167	1.51	0.31	0.620	O	I			1.83
11.250	1.50	0.32	0.628	O	I			1.85
11.333	1.49	0.33	0.636	O	I			1.88
11.417	1.49	0.33	0.644	O	I			1.90
11.500	1.49	0.34	0.652	O	I			1.92
11.583	1.44	0.34	0.660	O	I			1.94
11.667	1.36	0.35	0.667	O	I			1.96
11.750	1.35	0.35	0.674	O	I			1.98
11.833	1.37	0.36	0.681	O	I			1.99
11.917	1.40	0.67	0.687	O	I			2.01
12.000	1.41	0.99	0.691	O	I			2.02
12.083	1.77	1.25	0.694	O	I			2.03
12.167	2.24	1.58	0.698	O	I			2.04
12.250	2.35	1.89	0.702	O	I			2.04
12.333	2.46	2.12	0.705	O	I			2.05
12.417	2.57	2.29	0.707	O	I			2.06
12.500	2.60	2.42	0.708	O	I			2.06
12.583	2.72	2.53	0.710	O	I			2.06
12.667	2.88	2.65	0.711	O	I			2.07
12.750	2.92	2.76	0.712	O	I			2.07
12.833	3.00	2.85	0.714	O	I			2.07
12.917	3.09	2.93	0.715	O	I			2.08
13.000	3.11	3.01	0.716	O	I			2.08
13.083	3.40	3.12	0.717	O	I			2.08
13.167	3.78	3.33	0.719	O	I			2.09
13.250	3.87	3.54	0.722	O	I			2.09
13.333	3.92	3.70	0.724	O	I			2.10
13.417	3.94	3.80	0.725	O	I			2.10
13.500	3.96	3.86	0.726	O	I			2.10
13.583	3.36	3.77	0.725	O	I			2.10
13.667	2.56	3.42	0.721	O	I			2.09
13.750	2.38	3.00	0.715	O	I			2.08
13.833	2.31	2.72	0.712	O	I			2.07
13.917	2.28	2.53	0.710	O	I			2.06
14.000	2.27	2.42	0.708	O	I			2.06
14.083	2.50	2.40	0.708	O	I			2.06
14.167	2.79	2.51	0.709	O	I			2.06
14.250	2.87	2.65	0.711	O	I			2.07
14.333	2.85	2.74	0.712	O	I			2.07
14.417	2.80	2.78	0.713	O	I			2.07
14.500	2.79	2.79	0.713	O	I			2.07
14.583	2.79	2.79	0.713	O	I			2.07
14.667	2.80	2.79	0.713	O	I			2.07
14.750	2.80	2.79	0.713	O	I			2.07
14.833	2.75	2.79	0.713	O	I			2.07
14.917	2.69	2.76	0.712	O	I			2.07
15.000	2.68	2.72	0.712	O	I			2.07
15.083	2.62	2.69	0.712	O	I			2.07
15.167	2.55	2.64	0.711	O	I			2.07
15.250	2.54	2.60	0.711	O	I			2.07
15.333	2.48	2.56	0.710	O	I			2.06
15.417	2.41	2.51	0.709	O	I			2.06
15.500	2.40	2.46	0.709	O	I			2.06
15.583	2.18	2.39	0.708	O	I			2.06
15.667	1.89	2.23	0.706	O	I			2.05
15.750	1.83	2.07	0.704	O	I			2.05
15.833	1.80	1.96	0.703	O	I			2.05
15.917	1.80	1.89	0.702	O	I			2.04
16.000	1.80	1.85	0.701	O	I			2.04
16.083	1.28	1.71	0.700	O	I			2.04
16.167	0.59	1.37	0.695	O	I			2.03

16.250	0.43	0.99	0.691	I O				2.02
16.333	0.36	0.73	0.688	I O				2.01
16.417	0.33	0.56	0.685	I O				2.01
16.500	0.31	0.46	0.684	IO				2.00
16.583	0.29	0.39	0.683	IO				2.00
16.667	0.25	0.36	0.683	O				2.00
16.750	0.24	0.36	0.682	IO				2.00
16.833	0.24	0.36	0.681	IO				1.99
16.917	0.24	0.36	0.680	IO				1.99
17.000	0.24	0.36	0.679	IO				1.99
17.083	0.29	0.36	0.679	O				1.99
17.167	0.36	0.36	0.678	O				1.99
17.250	0.38	0.36	0.679	OI				1.99
17.333	0.39	0.36	0.679	OI				1.99
17.417	0.39	0.36	0.679	OI				1.99
17.500	0.39	0.36	0.679	OI				1.99
17.583	0.39	0.36	0.679	OI				1.99
17.667	0.39	0.36	0.680	OI				1.99
17.750	0.39	0.36	0.680	OI				1.99
17.833	0.37	0.36	0.680	O				1.99
17.917	0.33	0.36	0.680	O				1.99
18.000	0.32	0.36	0.680	O				1.99
18.083	0.32	0.36	0.679	O				1.99
18.167	0.31	0.36	0.679	O				1.99
18.250	0.31	0.36	0.679	O				1.99
18.333	0.31	0.36	0.679	O				1.99
18.417	0.31	0.36	0.678	O				1.99
18.500	0.31	0.36	0.678	O				1.99
18.583	0.29	0.36	0.678	O				1.99
18.667	0.25	0.36	0.677	O				1.98
18.750	0.24	0.36	0.676	IO				1.98
18.833	0.21	0.36	0.675	IO				1.98
18.917	0.17	0.35	0.674	IO				1.98
19.000	0.16	0.35	0.673	IO				1.97
19.083	0.19	0.35	0.672	IO				1.97
19.167	0.22	0.35	0.671	IO				1.97
19.250	0.23	0.35	0.670	IO				1.97
19.333	0.26	0.35	0.669	O				1.96
19.417	0.30	0.35	0.669	O				1.96
19.500	0.31	0.35	0.668	O				1.96
19.583	0.28	0.35	0.668	O				1.96
19.667	0.25	0.35	0.667	O				1.96
19.750	0.24	0.35	0.667	IO				1.96
19.833	0.21	0.35	0.666	IO				1.95
19.917	0.17	0.35	0.665	IO				1.95
20.000	0.16	0.35	0.663	IO				1.95
20.083	0.19	0.35	0.662	IO				1.95
20.167	0.22	0.34	0.661	IO				1.94
20.250	0.23	0.34	0.661	IO				1.94
20.333	0.23	0.34	0.660	IO				1.94
20.417	0.23	0.34	0.659	IO				1.94
20.500	0.24	0.34	0.658	IO				1.93
20.583	0.24	0.34	0.658	IO				1.93
20.667	0.24	0.34	0.657	IO				1.93
20.750	0.24	0.34	0.656	IO				1.93
20.833	0.21	0.34	0.655	IO				1.93
20.917	0.17	0.34	0.654	IO				1.92
21.000	0.16	0.34	0.653	IO				1.92
21.083	0.19	0.34	0.652	IO				1.92
21.167	0.22	0.34	0.651	IO				1.92
21.250	0.23	0.34	0.650	IO				1.91
21.333	0.21	0.34	0.649	IO				1.91
21.417	0.17	0.33	0.648	IO				1.91
21.500	0.16	0.33	0.647	IO				1.91
21.583	0.19	0.33	0.646	IO				1.90
21.667	0.22	0.33	0.645	IO				1.90
21.750	0.23	0.33	0.645	IO				1.90
21.833	0.21	0.33	0.644	IO				1.90
21.917	0.17	0.33	0.643	IO				1.89
22.000	0.16	0.33	0.642	IO				1.89
22.083	0.19	0.33	0.641	IO				1.89
22.167	0.22	0.33	0.640	IO				1.89
22.250	0.23	0.33	0.639	IO				1.88
22.333	0.21	0.33	0.638	IO				1.88
22.417	0.17	0.33	0.637	IO				1.88
22.500	0.16	0.33	0.636	IO				1.88
22.583	0.16	0.32	0.635	IO				1.87
22.667	0.16	0.32	0.634	IO				1.87
22.750	0.16	0.32	0.633	IO				1.87
22.833	0.16	0.32	0.632	IO				1.86
22.917	0.16	0.32	0.631	IO				1.86
23.000	0.16	0.32	0.629	IO				1.86
23.083	0.16	0.32	0.628	IO				1.86
23.167	0.16	0.32	0.627	IO				1.85
23.250	0.16	0.32	0.626	IO				1.85
23.333	0.16	0.32	0.625	IO				1.85

23.417	0.16	0.32	0.624	|IO	|	|	|	|	1.84
23.500	0.16	0.32	0.623	|IO	|	|	|	|	1.84
23.583	0.16	0.31	0.622	|IO	|	|	|	|	1.84
23.667	0.16	0.31	0.621	|IO	|	|	|	|	1.84
23.750	0.16	0.31	0.620	|IO	|	|	|	|	1.83
23.833	0.16	0.31	0.619	|IO	|	|	|	|	1.83
23.917	0.16	0.31	0.617	|IO	|	|	|	|	1.83
24.000	0.16	0.31	0.616	|IO	|	|	|	|	1.82
24.083	0.10	0.31	0.615	I O	|	|	|	|	1.82
24.167	0.03	0.31	0.613	I O	|	|	|	|	1.82
24.250	0.01	0.31	0.612	I O	|	|	|	|	1.81
24.333	0.00	0.30	0.609	I O	|	|	|	|	1.81
24.417	0.00	0.30	0.607	I O	|	|	|	|	1.80
24.500	0.00	0.30	0.605	I O	|	|	|	|	1.80
24.583	0.00	0.30	0.603	I O	|	|	|	|	1.79
24.667	0.00	0.30	0.601	I O	|	|	|	|	1.78
24.750	0.00	0.30	0.599	I O	|	|	|	|	1.78
24.833	0.00	0.30	0.597	I O	|	|	|	|	1.77
24.917	0.00	0.29	0.595	I O	|	|	|	|	1.77
25.000	0.00	0.29	0.593	I O	|	|	|	|	1.76
25.083	0.00	0.29	0.591	I O	|	|	|	|	1.76
25.167	0.00	0.29	0.589	I O	|	|	|	|	1.75
25.250	0.00	0.29	0.587	I O	|	|	|	|	1.75
25.333	0.00	0.29	0.585	I O	|	|	|	|	1.74
25.417	0.00	0.28	0.583	I O	|	|	|	|	1.74
25.500	0.00	0.28	0.581	I O	|	|	|	|	1.73
25.583	0.00	0.28	0.579	I O	|	|	|	|	1.73
25.667	0.00	0.28	0.577	I O	|	|	|	|	1.72
25.750	0.00	0.28	0.575	I O	|	|	|	|	1.72
25.833	0.00	0.28	0.573	I O	|	|	|	|	1.71
25.917	0.00	0.28	0.572	I O	|	|	|	|	1.71
26.000	0.00	0.27	0.570	I O	|	|	|	|	1.70
26.083	0.00	0.27	0.568	I O	|	|	|	|	1.70
26.167	0.00	0.27	0.566	I O	|	|	|	|	1.69
26.250	0.00	0.27	0.564	I O	|	|	|	|	1.69
26.333	0.00	0.27	0.562	I O	|	|	|	|	1.68
26.417	0.00	0.27	0.560	I O	|	|	|	|	1.68
26.500	0.00	0.27	0.558	I O	|	|	|	|	1.67
26.583	0.00	0.26	0.557	I O	|	|	|	|	1.67
26.667	0.00	0.26	0.555	I O	|	|	|	|	1.66
26.750	0.00	0.26	0.553	I O	|	|	|	|	1.66
26.833	0.00	0.26	0.551	I O	|	|	|	|	1.65
26.917	0.00	0.26	0.549	I O	|	|	|	|	1.65
27.000	0.00	0.26	0.548	I O	|	|	|	|	1.64
27.083	0.00	0.26	0.546	I O	|	|	|	|	1.64
27.167	0.00	0.26	0.544	I O	|	|	|	|	1.63
27.250	0.00	0.25	0.542	I O	|	|	|	|	1.63
27.333	0.00	0.25	0.541	I O	|	|	|	|	1.62
27.417	0.00	0.25	0.539	I O	|	|	|	|	1.62
27.500	0.00	0.25	0.537	I O	|	|	|	|	1.62
27.583	0.00	0.25	0.535	I O	|	|	|	|	1.61
27.667	0.00	0.25	0.534	IO	|	|	|	|	1.61
27.750	0.00	0.25	0.532	IO	|	|	|	|	1.60
27.833	0.00	0.24	0.530	IO	|	|	|	|	1.60
27.917	0.00	0.24	0.529	IO	|	|	|	|	1.59
28.000	0.00	0.24	0.527	IO	|	|	|	|	1.59
28.083	0.00	0.24	0.525	IO	|	|	|	|	1.58
28.167	0.00	0.24	0.524	IO	|	|	|	|	1.58
28.250	0.00	0.24	0.522	IO	|	|	|	|	1.58
28.333	0.00	0.24	0.520	IO	|	|	|	|	1.57
28.417	0.00	0.24	0.519	IO	|	|	|	|	1.57
28.500	0.00	0.23	0.517	IO	|	|	|	|	1.56
28.583	0.00	0.23	0.516	IO	|	|	|	|	1.56
28.667	0.00	0.23	0.514	IO	|	|	|	|	1.55
28.750	0.00	0.23	0.512	IO	|	|	|	|	1.55
28.833	0.00	0.23	0.511	IO	|	|	|	|	1.55
28.917	0.00	0.23	0.509	IO	|	|	|	|	1.54
29.000	0.00	0.23	0.508	IO	|	|	|	|	1.54
29.083	0.00	0.23	0.506	IO	|	|	|	|	1.53
29.167	0.00	0.22	0.504	IO	|	|	|	|	1.53
29.250	0.00	0.22	0.503	IO	|	|	|	|	1.52
29.333	0.00	0.22	0.501	IO	|	|	|	|	1.52
29.417	0.00	0.22	0.500	IO	|	|	|	|	1.52
29.500	0.00	0.22	0.498	IO	|	|	|	|	1.51
29.583	0.00	0.22	0.497	IO	|	|	|	|	1.51
29.667	0.00	0.22	0.495	IO	|	|	|	|	1.50
29.750	0.00	0.22	0.494	IO	|	|	|	|	1.50
29.833	0.00	0.22	0.492	IO	|	|	|	|	1.50
29.917	0.00	0.21	0.491	IO	|	|	|	|	1.49
30.000	0.00	0.21	0.489	IO	|	|	|	|	1.49
30.083	0.00	0.21	0.488	IO	|	|	|	|	1.49
30.167	0.00	0.21	0.486	IO	|	|	|	|	1.48
30.250	0.00	0.21	0.485	IO	|	|	|	|	1.48
30.333	0.00	0.21	0.484	IO	|	|	|	|	1.47
30.417	0.00	0.21	0.482	IO	|	|	|	|	1.47
30.500	0.00	0.21	0.481	IO	|	|	|	|	1.47

30.583	0.00	0.21	0.479	IO					1.46
30.667	0.00	0.20	0.478	IO					1.46
30.750	0.00	0.20	0.476	IO					1.46
30.833	0.00	0.20	0.475	IO					1.45
30.917	0.00	0.20	0.474	IO					1.45
31.000	0.00	0.20	0.472	IO					1.44
31.083	0.00	0.20	0.471	IO					1.44
31.167	0.00	0.20	0.470	IO					1.44
31.250	0.00	0.20	0.468	IO					1.43
31.333	0.00	0.20	0.467	IO					1.43
31.417	0.00	0.20	0.466	IO					1.43
31.500	0.00	0.19	0.464	IO					1.42
31.583	0.00	0.19	0.463	IO					1.42
31.667	0.00	0.19	0.462	IO					1.42
31.750	0.00	0.19	0.460	IO					1.41
31.833	0.00	0.19	0.459	IO					1.41
31.917	0.00	0.19	0.458	IO					1.41
32.000	0.00	0.19	0.456	IO					1.40
32.083	0.00	0.19	0.455	IO					1.40
32.167	0.00	0.19	0.454	IO					1.39
32.250	0.00	0.19	0.452	IO					1.39
32.333	0.00	0.18	0.451	IO					1.39
32.417	0.00	0.18	0.450	IO					1.38
32.500	0.00	0.18	0.449	IO					1.38
32.583	0.00	0.18	0.447	IO					1.38
32.667	0.00	0.18	0.446	IO					1.37
32.750	0.00	0.18	0.445	IO					1.37
32.833	0.00	0.18	0.444	IO					1.37
32.917	0.00	0.18	0.442	IO					1.37
33.000	0.00	0.18	0.441	IO					1.36
33.083	0.00	0.18	0.440	IO					1.36
33.167	0.00	0.17	0.439	IO					1.36
33.250	0.00	0.17	0.438	IO					1.35
33.333	0.00	0.17	0.436	IO					1.35
33.417	0.00	0.17	0.435	IO					1.35
33.500	0.00	0.17	0.434	IO					1.34
33.583	0.00	0.17	0.433	IO					1.34
33.667	0.00	0.17	0.432	IO					1.34
33.750	0.00	0.17	0.431	IO					1.33
33.833	0.00	0.17	0.429	IO					1.33
33.917	0.00	0.17	0.428	IO					1.33
34.000	0.00	0.17	0.427	IO					1.32
34.083	0.00	0.16	0.426	IO					1.32
34.167	0.00	0.16	0.425	IO					1.32
34.250	0.00	0.16	0.424	IO					1.32
34.333	0.00	0.16	0.423	IO					1.31
34.417	0.00	0.16	0.421	IO					1.31
34.500	0.00	0.16	0.420	IO					1.31
34.583	0.00	0.16	0.419	IO					1.30
34.667	0.00	0.16	0.418	IO					1.30
34.750	0.00	0.16	0.417	IO					1.30
34.833	0.00	0.16	0.416	IO					1.30
34.917	0.00	0.16	0.415	IO					1.29
35.000	0.00	0.16	0.414	IO					1.29
35.083	0.00	0.15	0.413	IO					1.29
35.167	0.00	0.15	0.412	IO					1.28
35.250	0.00	0.15	0.411	IO					1.28
35.333	0.00	0.15	0.410	IO					1.28
35.417	0.00	0.15	0.408	IO					1.28
35.500	0.00	0.15	0.407	IO					1.27
35.583	0.00	0.15	0.406	IO					1.27
35.667	0.00	0.15	0.405	IO					1.27
35.750	0.00	0.15	0.404	IO					1.26
35.833	0.00	0.15	0.403	IO					1.26
35.917	0.00	0.15	0.402	IO					1.26
36.000	0.00	0.15	0.401	IO					1.26
36.083	0.00	0.15	0.400	IO					1.25
36.167	0.00	0.14	0.399	IO					1.25
36.250	0.00	0.14	0.398	IO					1.25
36.333	0.00	0.14	0.397	IO					1.25
36.417	0.00	0.14	0.396	IO					1.24
36.500	0.00	0.14	0.395	IO					1.24
36.583	0.00	0.14	0.394	IO					1.24
36.667	0.00	0.14	0.393	IO					1.24
36.750	0.00	0.14	0.392	IO					1.23
36.833	0.00	0.14	0.391	IO					1.23
36.917	0.00	0.14	0.391	IO					1.23
37.000	0.00	0.14	0.390	IO					1.23
37.083	0.00	0.14	0.389	IO					1.22
37.167	0.00	0.14	0.388	IO					1.22
37.250	0.00	0.14	0.387	IO					1.22
37.333	0.00	0.13	0.386	IO					1.22
37.417	0.00	0.13	0.385	IO					1.21
37.500	0.00	0.13	0.384	IO					1.21
37.583	0.00	0.13	0.383	IO					1.21
37.667	0.00	0.13	0.382	IO					1.21

37.750	0.00	0.13	0.381	IO	|	|	|	|	1.20
37.833	0.00	0.13	0.380	IO	|	|	|	|	1.20
37.917	0.00	0.13	0.379	IO	|	|	|	|	1.20
38.000	0.00	0.13	0.379	IO	|	|	|	|	1.20
38.083	0.00	0.13	0.378	IO	|	|	|	|	1.19
38.167	0.00	0.13	0.377	IO	|	|	|	|	1.19
38.250	0.00	0.13	0.376	IO	|	|	|	|	1.19
38.333	0.00	0.13	0.375	IO	|	|	|	|	1.19
38.417	0.00	0.13	0.374	IO	|	|	|	|	1.19
38.500	0.00	0.12	0.373	IO	|	|	|	|	1.18
38.583	0.00	0.12	0.372	IO	|	|	|	|	1.18
38.667	0.00	0.12	0.372	O	|	|	|	|	1.18
38.750	0.00	0.12	0.371	O	|	|	|	|	1.18
38.833	0.00	0.12	0.370	O	|	|	|	|	1.17
38.917	0.00	0.12	0.369	O	|	|	|	|	1.17
39.000	0.00	0.12	0.368	O	|	|	|	|	1.17
39.083	0.00	0.12	0.367	O	|	|	|	|	1.17
39.167	0.00	0.12	0.367	O	|	|	|	|	1.17
39.250	0.00	0.12	0.366	O	|	|	|	|	1.16
39.333	0.00	0.12	0.365	O	|	|	|	|	1.16
39.417	0.00	0.12	0.364	O	|	|	|	|	1.16
39.500	0.00	0.12	0.363	O	|	|	|	|	1.16
39.583	0.00	0.12	0.363	O	|	|	|	|	1.15
39.667	0.00	0.12	0.362	O	|	|	|	|	1.15
39.750	0.00	0.12	0.361	O	|	|	|	|	1.15
39.833	0.00	0.11	0.360	O	|	|	|	|	1.15
39.917	0.00	0.11	0.359	O	|	|	|	|	1.15
40.000	0.00	0.11	0.359	O	|	|	|	|	1.14
40.083	0.00	0.11	0.358	O	|	|	|	|	1.14
40.167	0.00	0.11	0.357	O	|	|	|	|	1.14
40.250	0.00	0.11	0.356	O	|	|	|	|	1.14
40.333	0.00	0.11	0.355	O	|	|	|	|	1.14
40.417	0.00	0.11	0.355	O	|	|	|	|	1.13
40.500	0.00	0.11	0.354	O	|	|	|	|	1.13
40.583	0.00	0.11	0.353	O	|	|	|	|	1.13
40.667	0.00	0.11	0.352	O	|	|	|	|	1.13
40.750	0.00	0.11	0.352	O	|	|	|	|	1.13
40.833	0.00	0.11	0.351	O	|	|	|	|	1.12
40.917	0.00	0.11	0.350	O	|	|	|	|	1.12
41.000	0.00	0.11	0.349	O	|	|	|	|	1.12
41.083	0.00	0.11	0.349	O	|	|	|	|	1.12
41.167	0.00	0.11	0.348	O	|	|	|	|	1.12
41.250	0.00	0.11	0.347	O	|	|	|	|	1.11
41.333	0.00	0.10	0.347	O	|	|	|	|	1.11
41.417	0.00	0.10	0.346	O	|	|	|	|	1.11
41.500	0.00	0.10	0.345	O	|	|	|	|	1.11
41.583	0.00	0.10	0.344	O	|	|	|	|	1.11
41.667	0.00	0.10	0.344	O	|	|	|	|	1.10
41.750	0.00	0.10	0.343	O	|	|	|	|	1.10
41.833	0.00	0.10	0.342	O	|	|	|	|	1.10
41.917	0.00	0.10	0.342	O	|	|	|	|	1.10
42.000	0.00	0.10	0.341	O	|	|	|	|	1.10
42.083	0.00	0.10	0.340	O	|	|	|	|	1.10

Remaining water in basin = 0.34 (Ac.Ft)

**********HYDROGRAPH DATA**********

Number of intervals = 505
Time interval = 5.0 (Min.)
Maximum/Peak flow rate = 3.864 (CFS)
Total volume = 1.508 (Ac.Ft)

Status of hydrographs being held in storage

	Stream 1	Stream 2	Stream 3	Stream 4	Stream 5
Peak (CFS)	0.000	0.000	0.000	0.000	0.000
Vol (Ac.Ft)	0.000	0.000	0.000	0.000	0.000

****

Appendix E – Catch Basin and Streert Capacity Calculations

Inlet Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Friday, May 31 2024

Node 3 On Grade Inlet

Curb Inlet

Location	=	On grade
Curb Length (ft)	=	21.00
Throat Height (in)	=	6.00
Grate Area (sqft)	=	-0-
Grate Width (ft)	=	-0-
Grate Length (ft)	=	-0-

Gutter

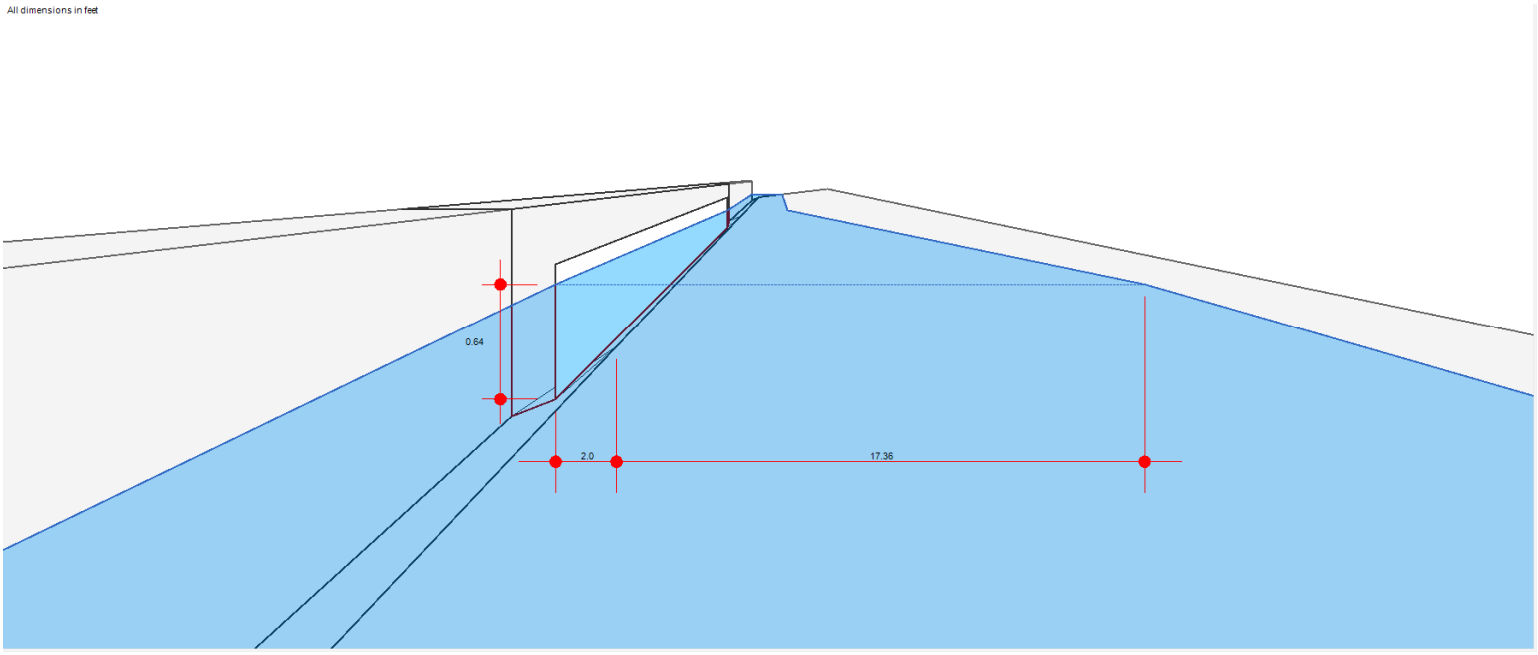
Slope, Sw (ft/ft)	=	0.083
Slope, Sx (ft/ft)	=	0.020
Local Depr (in)	=	1.50
Gutter Width (ft)	=	2.00
Gutter Slope (%)	=	1.00
Gutter n-value	=	0.015

Calculations

Compute by:		Known Q
Q (cfs)	=	16.02

Highlighted

Q Total (cfs)	=	16.02
Q Capt (cfs)	=	13.43
Q Bypass (cfs)	=	2.59
Depth at Inlet (in)	=	7.66
Efficiency (%)	=	84
Gutter Spread (ft)	=	19.36
Gutter Vel (ft/s)	=	4.14
Bypass Spread (ft)	=	8.88
Bypass Depth (in)	=	3.64



Inlet Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Friday, May 31 2024

Node 7 On Grade Inlet

Curb Inlet

Location	=	On grade
Curb Length (ft)	=	21.00
Throat Height (in)	=	6.00
Grate Area (sqft)	=	-0-
Grate Width (ft)	=	-0-
Grate Length (ft)	=	-0-

Gutter

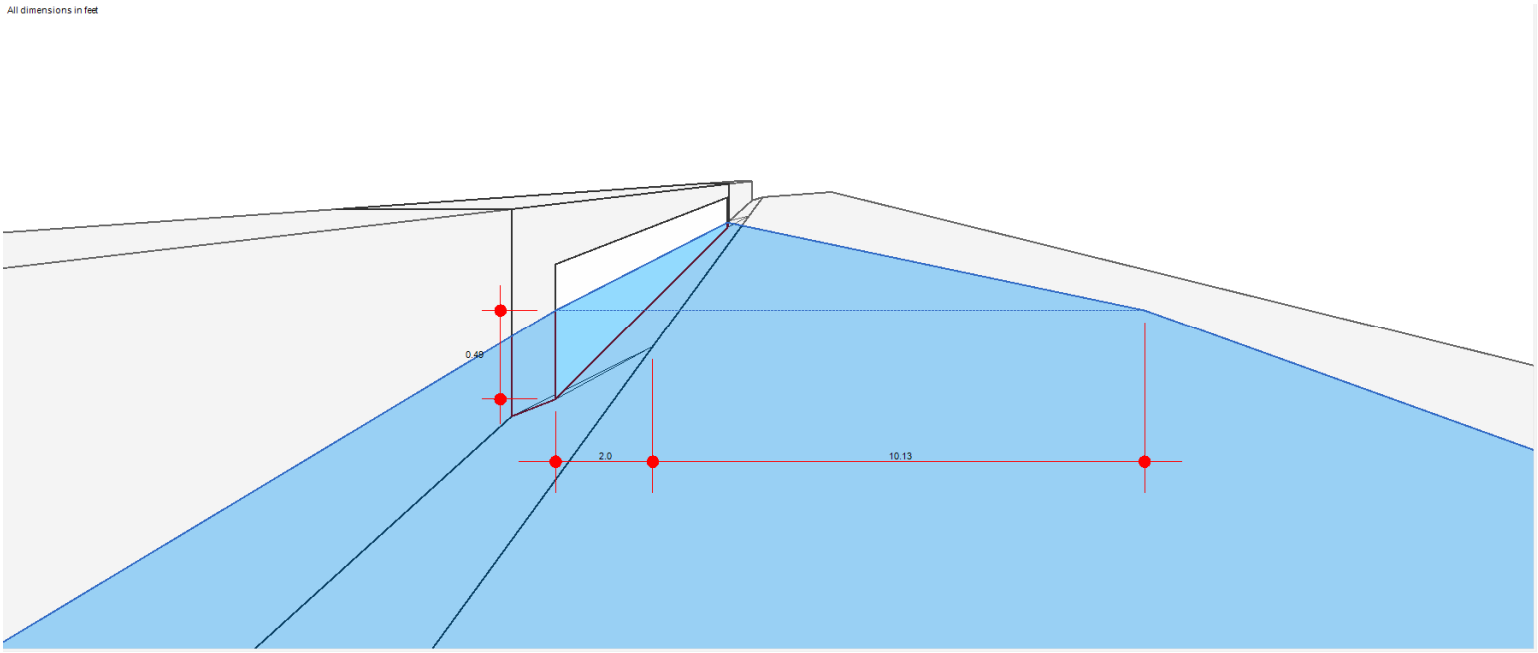
Slope, Sw (ft/ft)	=	0.083
Slope, Sx (ft/ft)	=	0.020
Local Depr (in)	=	1.50
Gutter Width (ft)	=	2.00
Gutter Slope (%)	=	1.00
Gutter n-value	=	0.015

Calculations

Compute by:		Known Q
Q (cfs)	=	5.14

Highlighted

Q Total (cfs)	=	5.14
Q Capt (cfs)	=	5.14
Q Bypass (cfs)	=	-0-
Depth at Inlet (in)	=	5.92
Efficiency (%)	=	100
Gutter Spread (ft)	=	12.13
Gutter Vel (ft/s)	=	3.22
Bypass Spread (ft)	=	-0-
Bypass Depth (in)	=	-0-



Inlet Report

Node 9 On Grade Inlet (2.59CFS Bypass from Node 3)

Combination Inlet

Location	=	On grade
Curb Length (ft)	=	21.00
Throat Height (in)	=	6.00
Grate Area (sqft)	=	-0-
Grate Width (ft)	=	2.00
Grate Length (ft)	=	6.00

Gutter

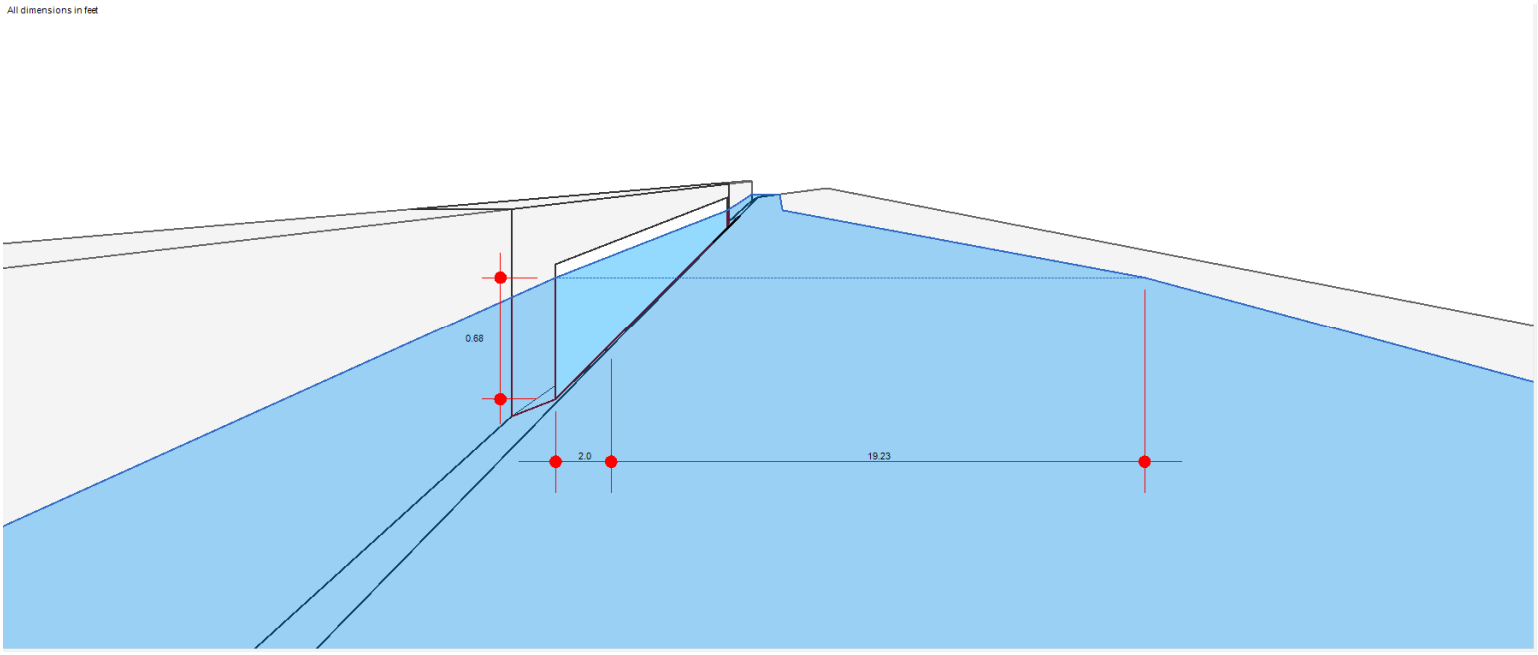
Slope, Sw (ft/ft)	=	0.083
Slope, Sx (ft/ft)	=	0.020
Local Depr (in)	=	1.50
Gutter Width (ft)	=	2.00
Gutter Slope (%)	=	1.00
Gutter n-value	=	0.015

Calculations

Compute by:		Known Q
Q (cfs)	=	20.22

Highlighted

Q Total (cfs)	=	20.22
Q Capt (cfs)	=	17.60
Q Bypass (cfs)	=	2.62
Depth at Inlet (in)	=	8.11
Efficiency (%)	=	87
Gutter Spread (ft)	=	21.23
Gutter Vel (ft/s)	=	4.37
Bypass Spread (ft)	=	8.94
Bypass Depth (in)	=	3.66



Inlet Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Friday, May 31 2024

Node 13 Sag Inlet (2.62CFS Bypass from Node 9)

Combination Inlet

Location	= Sag
Curb Length (ft)	= 7.00
Throat Height (in)	= 6.00
Grate Area (sqft)	= 12.00
Grate Width (ft)	= 2.00
Grate Length (ft)	= 6.00

Gutter

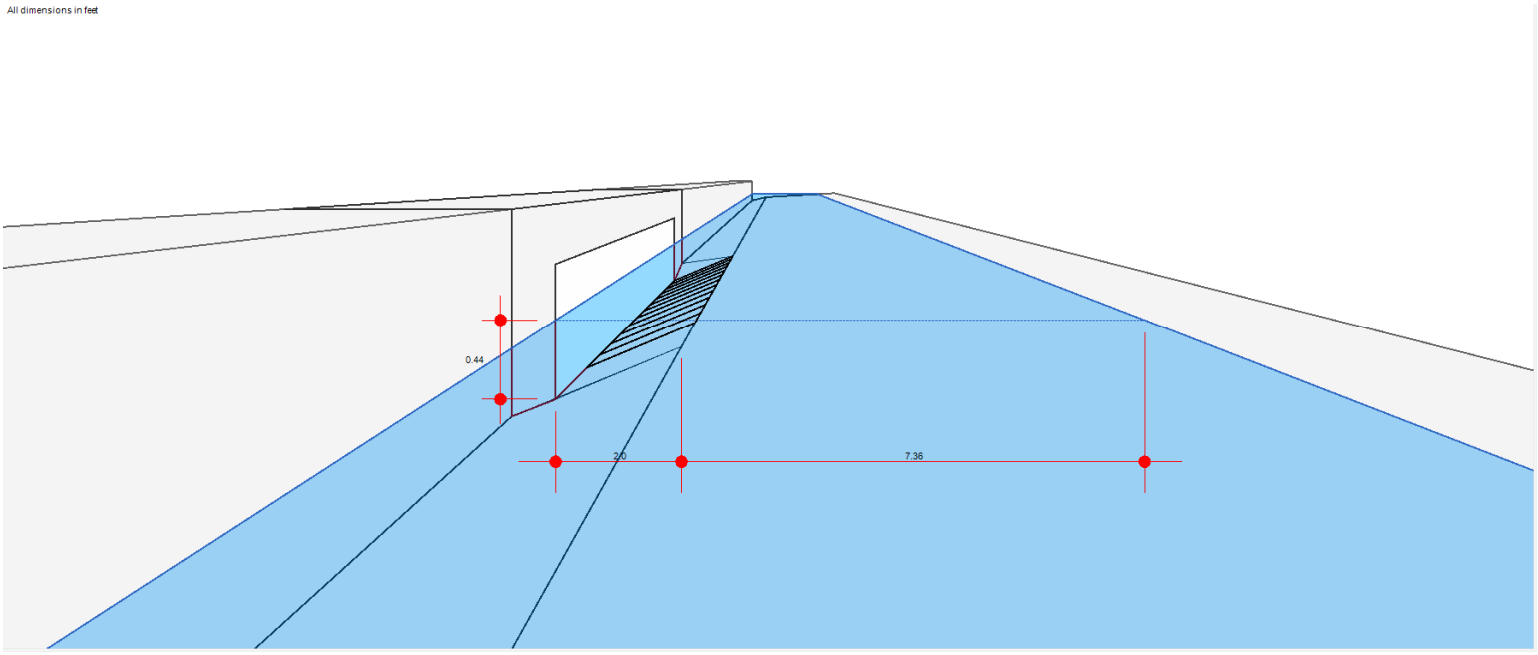
Slope, Sw (ft/ft)	= 0.083
Slope, Sx (ft/ft)	= 0.020
Local Depr (in)	= 1.50
Gutter Width (ft)	= 2.00
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

Calculations

Compute by:	Known Q
Q (cfs)	= 5.61

Highlighted

Q Total (cfs)	= 5.61
Q Capt (cfs)	= 5.61
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 5.26
Efficiency (%)	= 100
Gutter Spread (ft)	= 9.36
Gutter Vel (ft/s)	= 4.37
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-



Inlet Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Friday, May 31 2024

Node 17 Sag Inlet

Curb Inlet

Location	= Sag
Curb Length (ft)	= 7.00
Throat Height (in)	= 6.00
Grate Area (sqft)	= -0-
Grate Width (ft)	= -0-
Grate Length (ft)	= -0-

Gutter

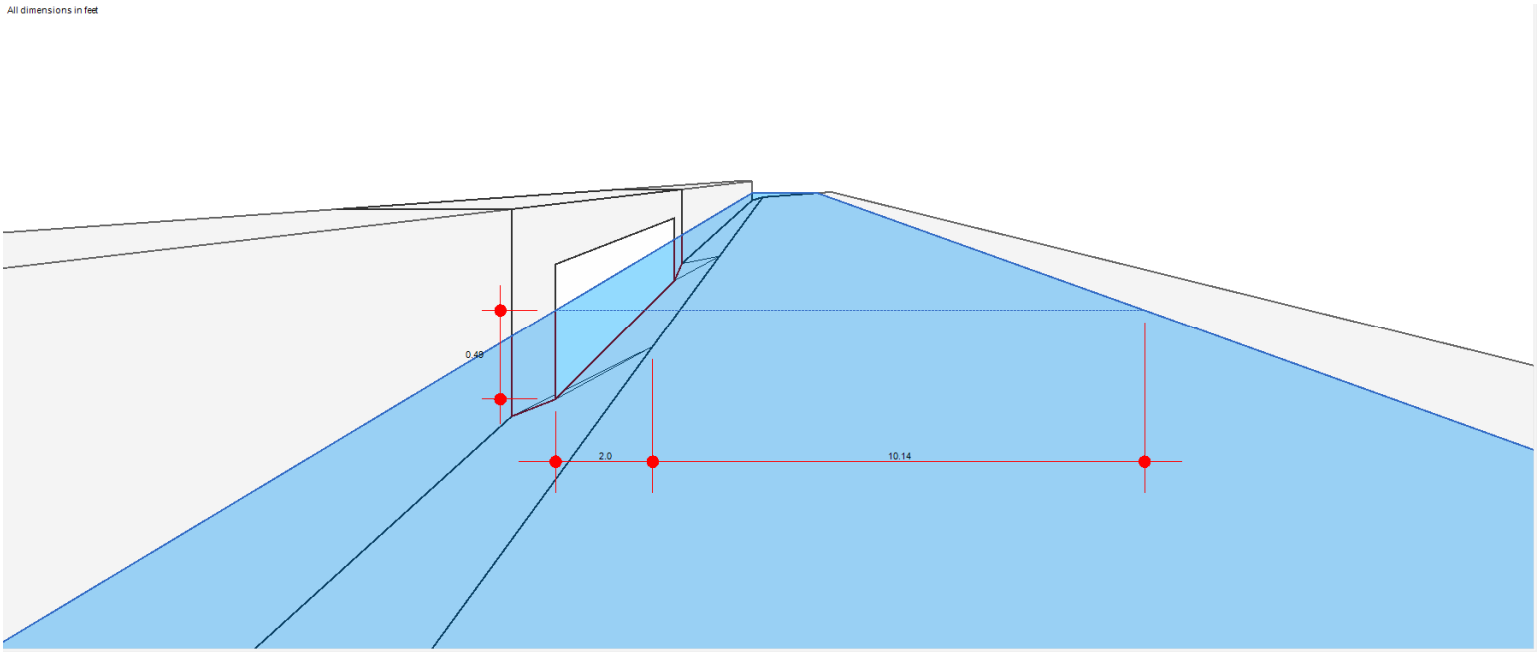
Slope, Sw (ft/ft)	= 0.083
Slope, Sx (ft/ft)	= 0.020
Local Depr (in)	= 1.50
Gutter Width (ft)	= 2.00
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

Calculations

Compute by:	Known Q
Q (cfs)	= 2.92

Highlighted

Q Total (cfs)	= 2.92
Q Capt (cfs)	= 2.92
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 5.93
Efficiency (%)	= 100
Gutter Spread (ft)	= 12.14
Gutter Vel (ft/s)	= 4.37
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-



Inlet Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Friday, May 31 2024

Node 21 Sag Inlet

Curb Inlet

Location	= Sag
Curb Length (ft)	= 21.00
Throat Height (in)	= 6.00
Grate Area (sqft)	= -0-
Grate Width (ft)	= -0-
Grate Length (ft)	= -0-

Gutter

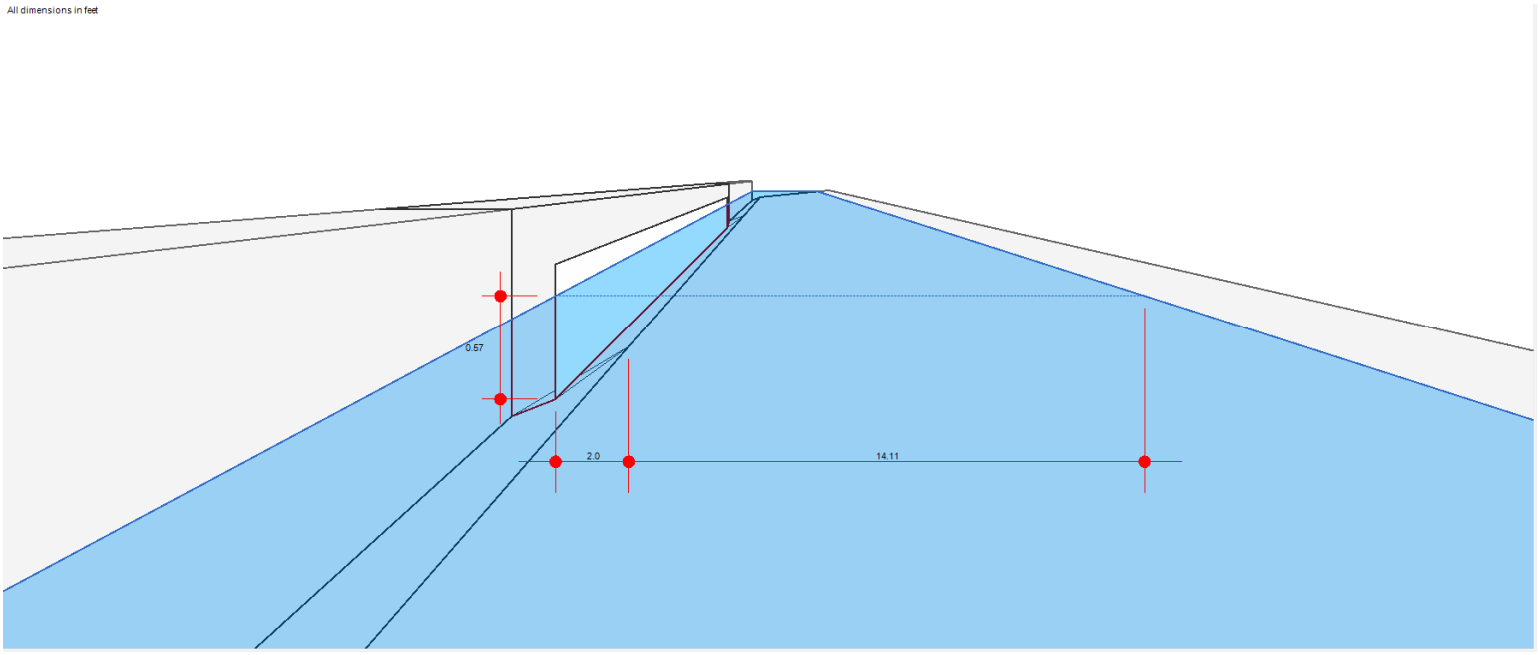
Slope, Sw (ft/ft)	= 0.083
Slope, Sx (ft/ft)	= 0.020
Local Depr (in)	= 1.50
Gutter Width (ft)	= 2.00
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

Calculations

Compute by:	Known Q
Q (cfs)	= 10.36

Highlighted

Q Total (cfs)	= 10.36
Q Capt (cfs)	= 10.36
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 6.88
Efficiency (%)	= 100
Gutter Spread (ft)	= 16.11
Gutter Vel (ft/s)	= 4.37
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-



Inlet Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Friday, May 31 2024

Node 25 Sag Inlet

Curb Inlet

Location	= Sag
Curb Length (ft)	= 14.00
Throat Height (in)	= 6.00
Grate Area (sqft)	= -0-
Grate Width (ft)	= -0-
Grate Length (ft)	= -0-

Gutter

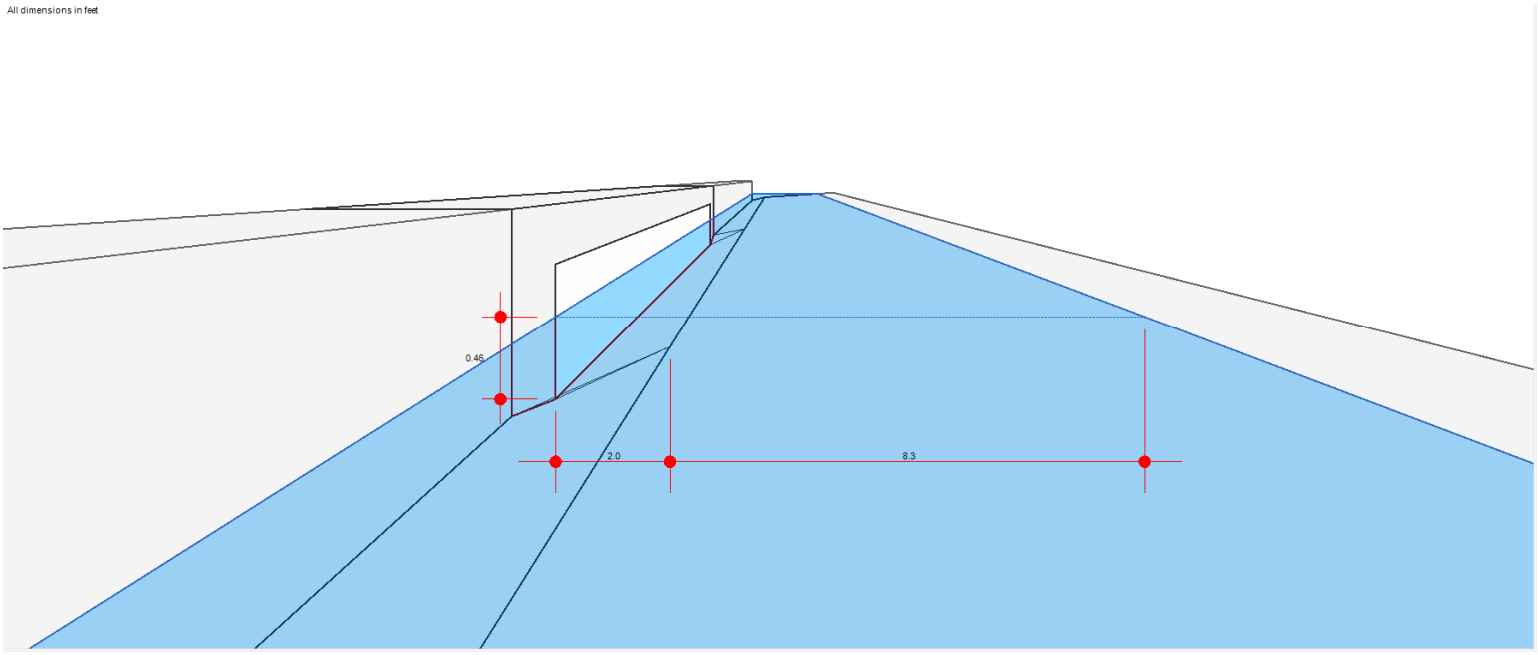
Slope, Sw (ft/ft)	= 0.083
Slope, Sx (ft/ft)	= 0.020
Local Depr (in)	= 1.50
Gutter Width (ft)	= 2.00
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

Calculations

Compute by:	Known Q
Q (cfs)	= 3.79

Highlighted

Q Total (cfs)	= 3.79
Q Capt (cfs)	= 3.79
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 5.48
Efficiency (%)	= 100
Gutter Spread (ft)	= 10.30
Gutter Vel (ft/s)	= 4.37
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-



Inlet Report

Node 101.1 Grade Inlet

Combination Inlet

Location	= On grade
Curb Length (ft)	= 21.00
Throat Height (in)	= 6.00
Grate Area (sqft)	= -0-
Grate Width (ft)	= 2.00
Grate Length (ft)	= 9.00

Gutter

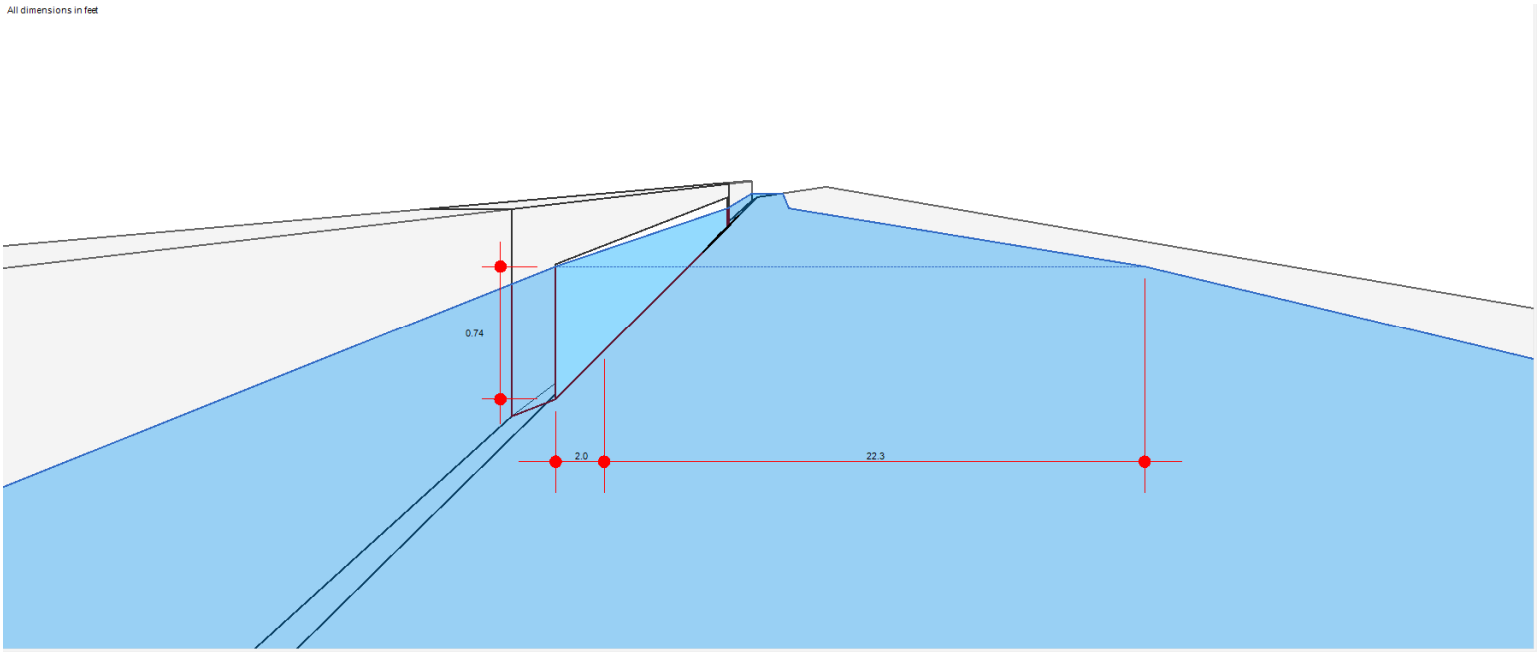
Slope, Sw (ft/ft)	= 0.083
Slope, Sx (ft/ft)	= 0.020
Local Depr (in)	= 1.50
Gutter Width (ft)	= 2.00
Gutter Slope (%)	= 1.00
Gutter n-value	= 0.015

Calculations

Compute by:	Known Q
Q (cfs)	= 28.59

Highlighted

Q Total (cfs)	= 28.59
Q Capt (cfs)	= 24.13
Q Bypass (cfs)	= 4.46
Depth at Inlet (in)	= 8.84
Efficiency (%)	= 84
Gutter Spread (ft)	= 24.30
Gutter Vel (ft/s)	= 4.74
Bypass Spread (ft)	= 11.40
Bypass Depth (in)	= 4.25



Inlet Report

Node 101.4 Grade Inlet

Combination Inlet

Location	=	On grade
Curb Length (ft)	=	21.00
Throat Height (in)	=	6.00
Grate Area (sqft)	=	-0-
Grate Width (ft)	=	2.00
Grate Length (ft)	=	6.00

Gutter

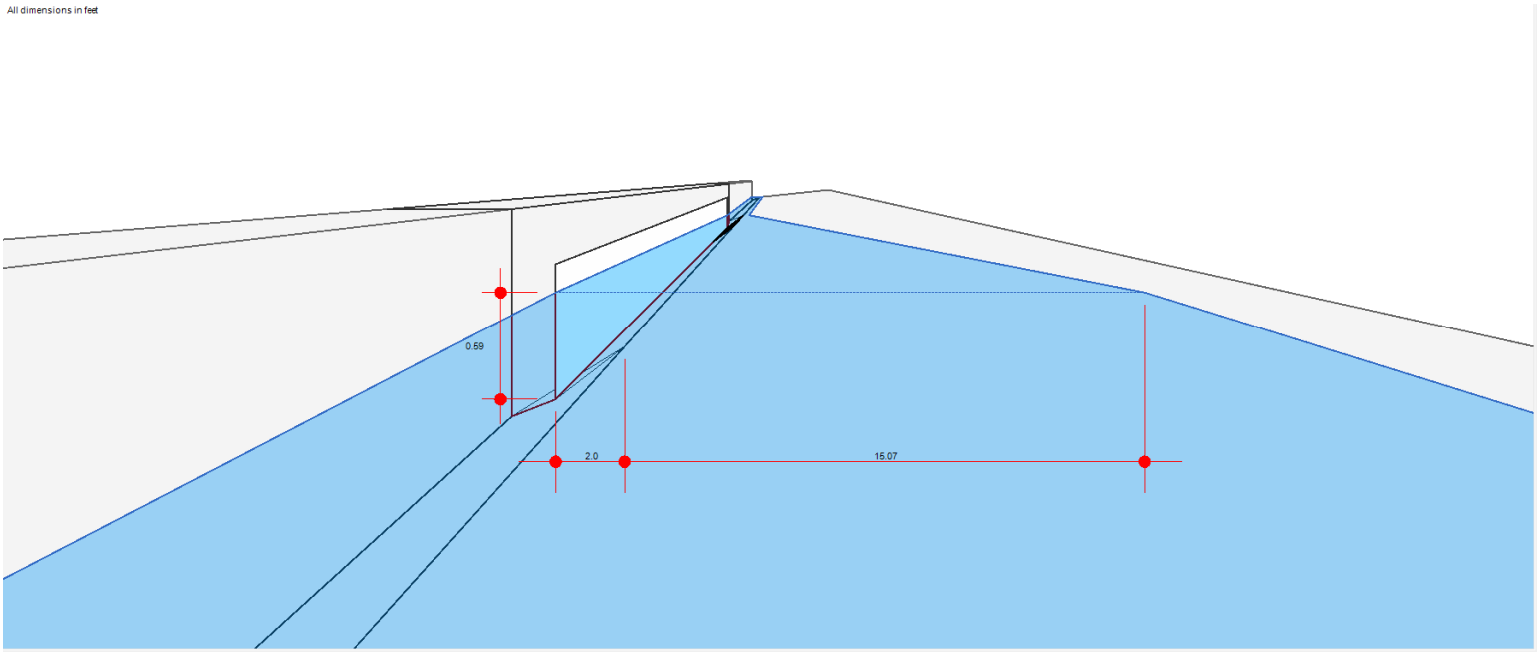
Slope, Sw (ft/ft)	=	0.083
Slope, Sx (ft/ft)	=	0.020
Local Depr (in)	=	1.50
Gutter Width (ft)	=	2.00
Gutter Slope (%)	=	1.00
Gutter n-value	=	0.015

Calculations

Compute by:		Known Q
Q (cfs)	=	11.70

Highlighted

Q Total (cfs)	=	11.70
Q Capt (cfs)	=	11.22
Q Bypass (cfs)	=	0.48
Depth at Inlet (in)	=	7.11
Efficiency (%)	=	96
Gutter Spread (ft)	=	17.07
Gutter Vel (ft/s)	=	3.85
Bypass Spread (ft)	=	2.82
Bypass Depth (in)	=	2.19



Inlet Report

Node 104 On Grade Inlet (4.94 CFS Bypass from Node 101.1 and 101.4)

Combination Inlet

Location	=	On grade
Curb Length (ft)	=	21.00
Throat Height (in)	=	6.00
Grate Area (sqft)	=	-0-
Grate Width (ft)	=	2.00
Grate Length (ft)	=	9.00

Gutter

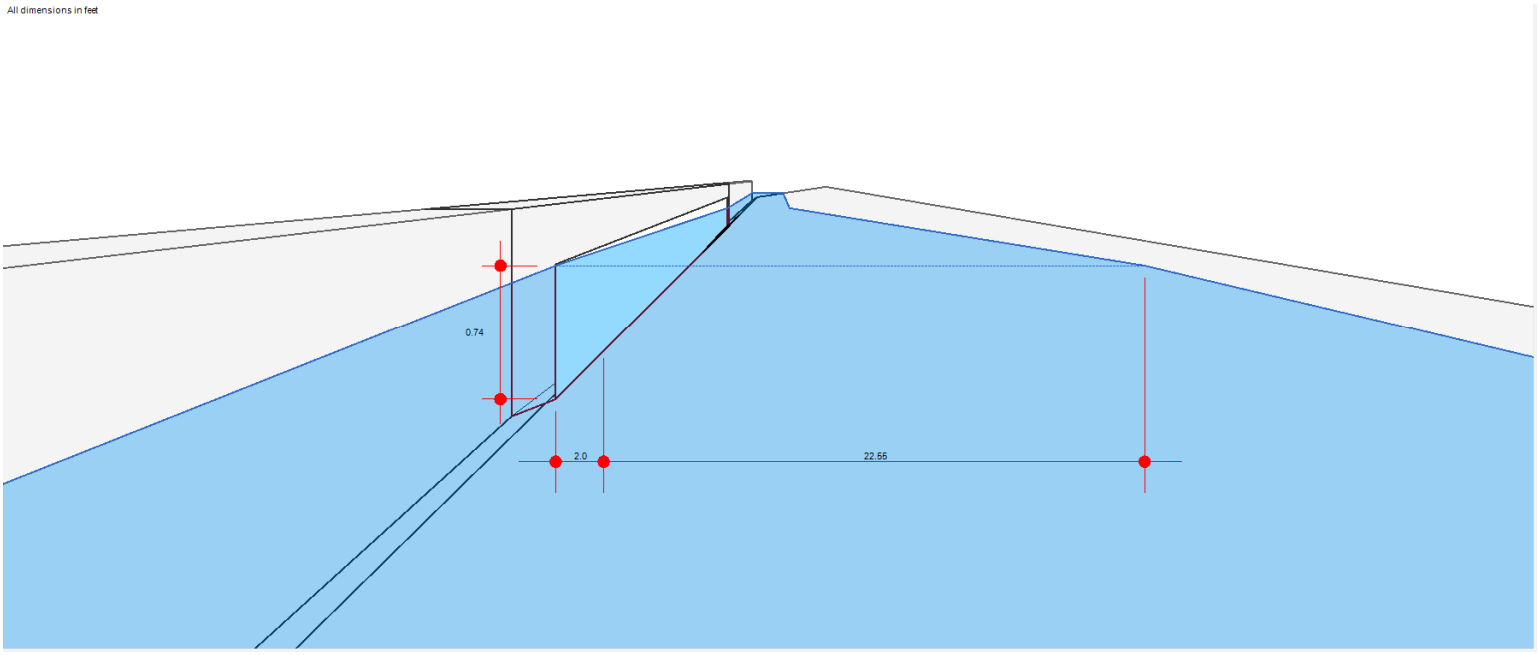
Slope, Sw (ft/ft)	=	0.083
Slope, Sx (ft/ft)	=	0.020
Local Depr (in)	=	1.50
Gutter Width (ft)	=	2.00
Gutter Slope (%)	=	1.00
Gutter n-value	=	0.015

Calculations

Compute by:		Known Q
Q (cfs)	=	29.34

Highlighted

Q Total (cfs)	=	29.34
Q Capt (cfs)	=	24.65
Q Bypass (cfs)	=	4.69
Depth at Inlet (in)	=	8.90
Efficiency (%)	=	84
Gutter Spread (ft)	=	24.55
Gutter Vel (ft/s)	=	4.77
Bypass Spread (ft)	=	11.65
Bypass Depth (in)	=	4.31



Inlet Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Friday, May 31 2024

Node 108 On Grade Inlet

Curb Inlet

Location	=	On grade
Curb Length (ft)	=	21.00
Throat Height (in)	=	6.00
Grate Area (sqft)	=	-0-
Grate Width (ft)	=	-0-
Grate Length (ft)	=	-0-

Gutter

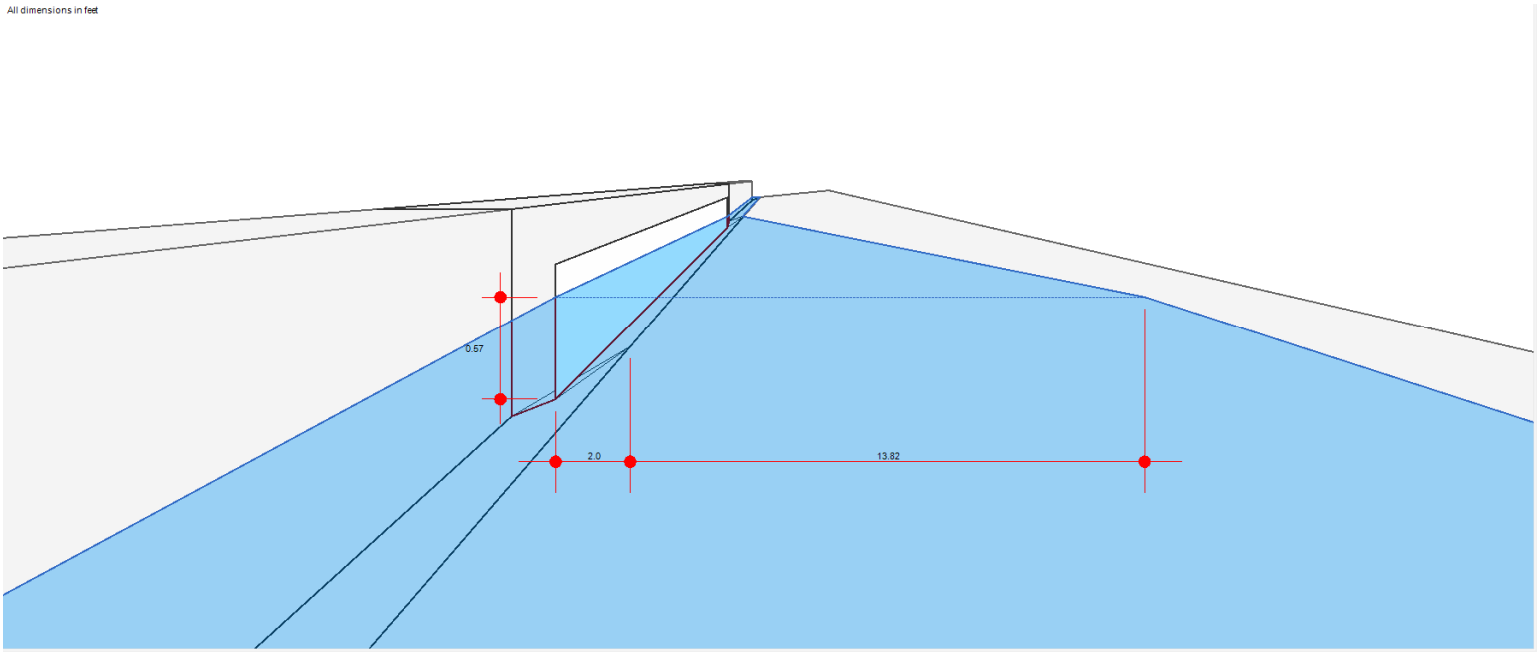
Slope, Sw (ft/ft)	=	0.083
Slope, Sx (ft/ft)	=	0.020
Local Depr (in)	=	1.50
Gutter Width (ft)	=	2.00
Gutter Slope (%)	=	1.00
Gutter n-value	=	0.015

Calculations

Compute by:		Known Q
Q (cfs)	=	9.69

Highlighted

Q Total (cfs)	=	9.69
Q Capt (cfs)	=	9.39
Q Bypass (cfs)	=	0.30
Depth at Inlet (in)	=	6.81
Efficiency (%)	=	97
Gutter Spread (ft)	=	15.82
Gutter Vel (ft/s)	=	3.69
Bypass Spread (ft)	=	1.84
Bypass Depth (in)	=	1.83



Inlet Report

Node 112 Sag Inlet (4.69CFS Bypass from Node 104)

Curb Inlet

Location	= Sag
Curb Length (ft)	= 28.00
Throat Height (in)	= 6.00
Grate Area (sqft)	= -0-
Grate Width (ft)	= -0-
Grate Length (ft)	= -0-

Gutter

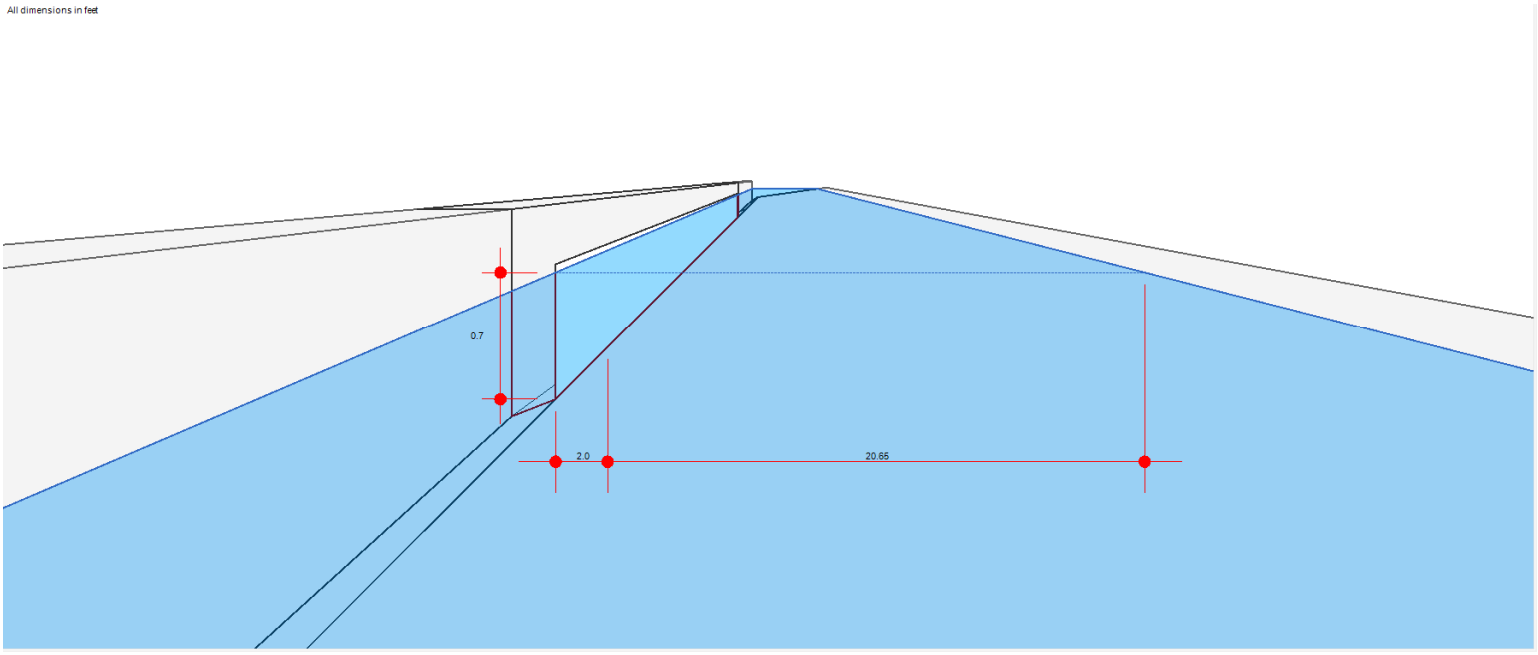
Slope, Sw (ft/ft)	= 0.083
Slope, Sx (ft/ft)	= 0.020
Local Depr (in)	= 1.50
Gutter Width (ft)	= 2.00
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

Calculations

Compute by:	Known Q
Q (cfs)	= 22.18

Highlighted

Q Total (cfs)	= 22.18
Q Capt (cfs)	= 22.18
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 8.45
Efficiency (%)	= 100
Gutter Spread (ft)	= 22.65
Gutter Vel (ft/s)	= 4.37
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-



Inlet Report

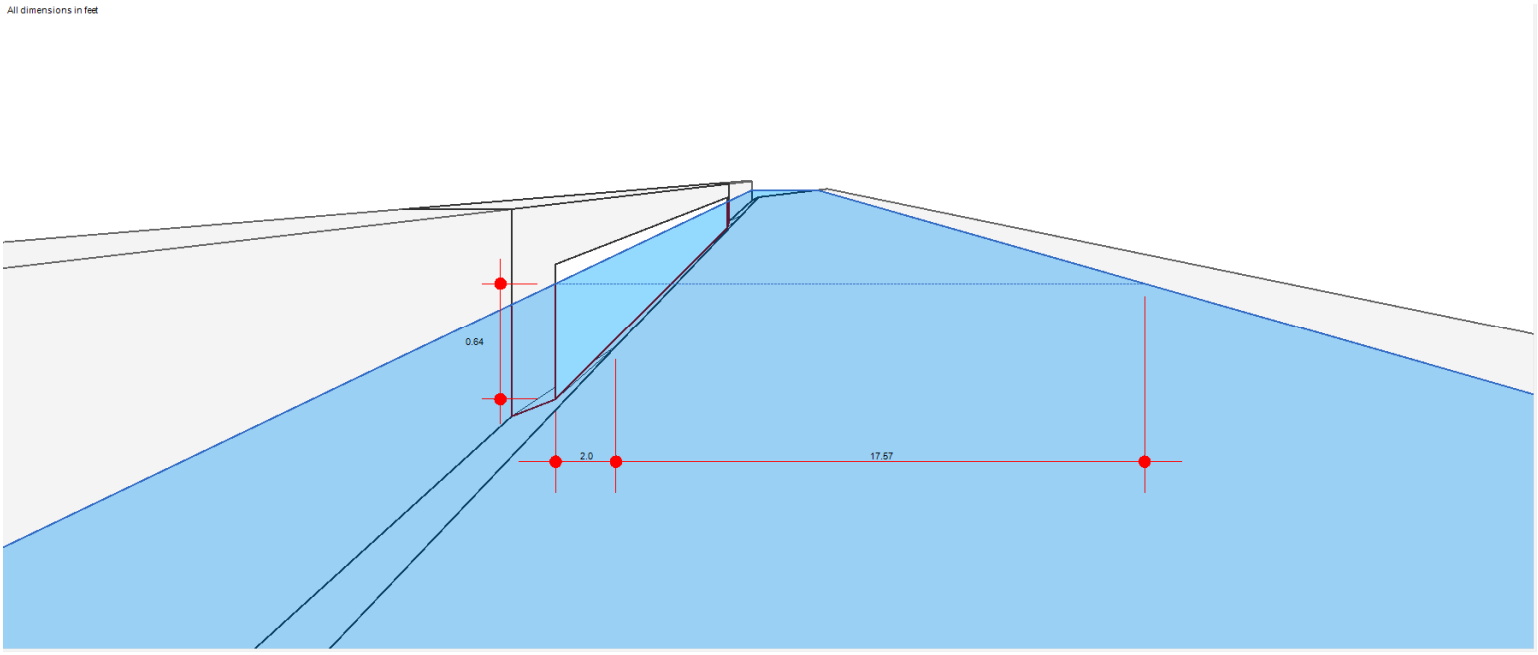
Node 115 Sag Inlet (0.30CFS Bypass from Node 108)

Curb Inlet	
Location	= Sag
Curb Length (ft)	= 21.00
Throat Height (in)	= 6.00
Grate Area (sqft)	= -0-
Grate Width (ft)	= -0-
Grate Length (ft)	= -0-

Gutter	
Slope, Sw (ft/ft)	= 0.083
Slope, Sx (ft/ft)	= 0.020
Local Depr (in)	= 1.50
Gutter Width (ft)	= 2.00
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

Calculations	
Compute by:	Known Q
Q (cfs)	= 13.86

Highlighted	
Q Total (cfs)	= 13.86
Q Capt (cfs)	= 13.86
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 7.71
Efficiency (%)	= 100
Gutter Spread (ft)	= 19.57
Gutter Vel (ft/s)	= 3.69
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-



Inlet Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Friday, May 31 2024

Node 202 Sag Inlet (0.66CFS Bypass from Node 205)

Curb Inlet

Location	= Sag
Curb Length (ft)	= 14.00
Throat Height (in)	= 6.00
Grate Area (sqft)	= -0-
Grate Width (ft)	= -0-
Grate Length (ft)	= -0-

Gutter

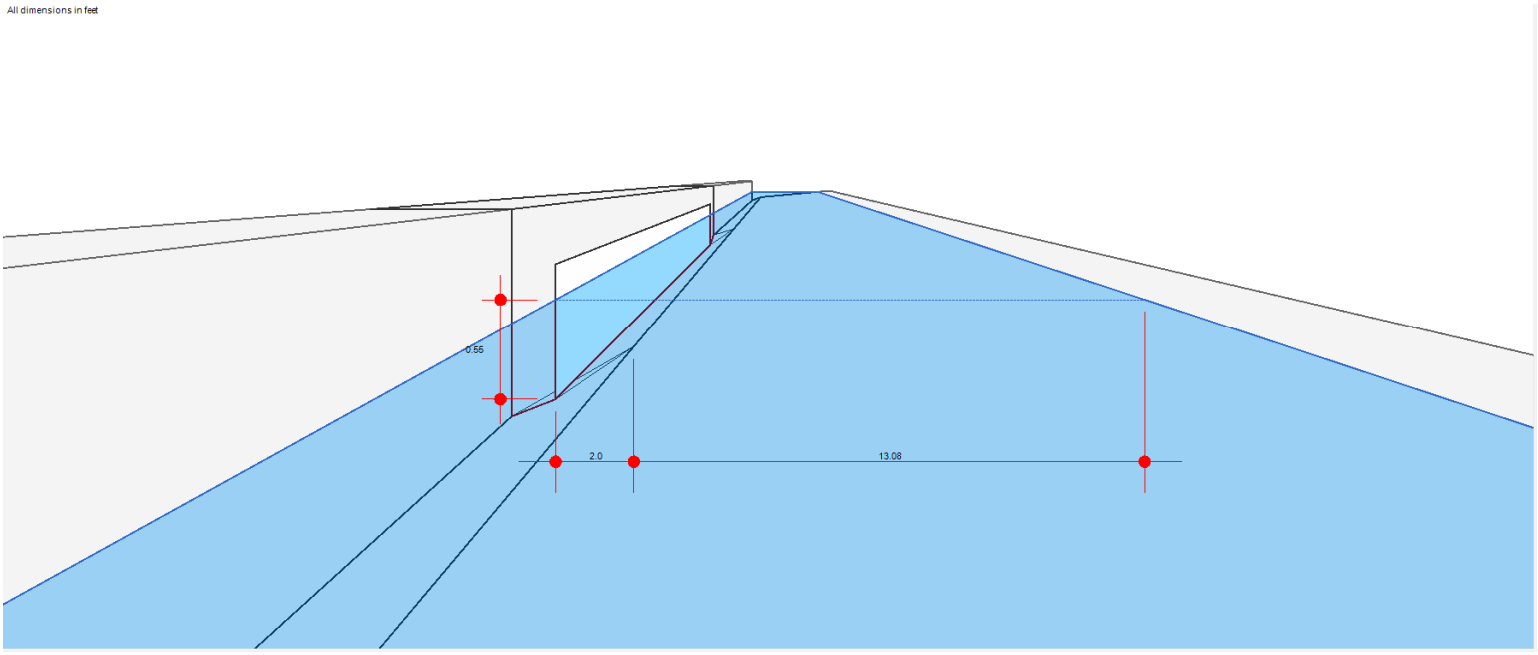
Slope, Sw (ft/ft)	= 0.083
Slope, Sx (ft/ft)	= 0.020
Local Depr (in)	= 1.50
Gutter Width (ft)	= 2.00
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

Calculations

Compute by:	Known Q
Q (cfs)	= 6.71

Highlighted

Q Total (cfs)	= 6.71
Q Capt (cfs)	= 6.71
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 6.63
Efficiency (%)	= 100
Gutter Spread (ft)	= 15.08
Gutter Vel (ft/s)	= 4.37
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-



Inlet Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc. Friday, May 31 2024

Node 205 On Grade Inlet

Curb Inlet

Location	=	On grade
Curb Length (ft)	=	21.00
Throat Height (in)	=	6.00
Grate Area (sqft)	=	-0-
Grate Width (ft)	=	-0-
Grate Length (ft)	=	-0-

Gutter

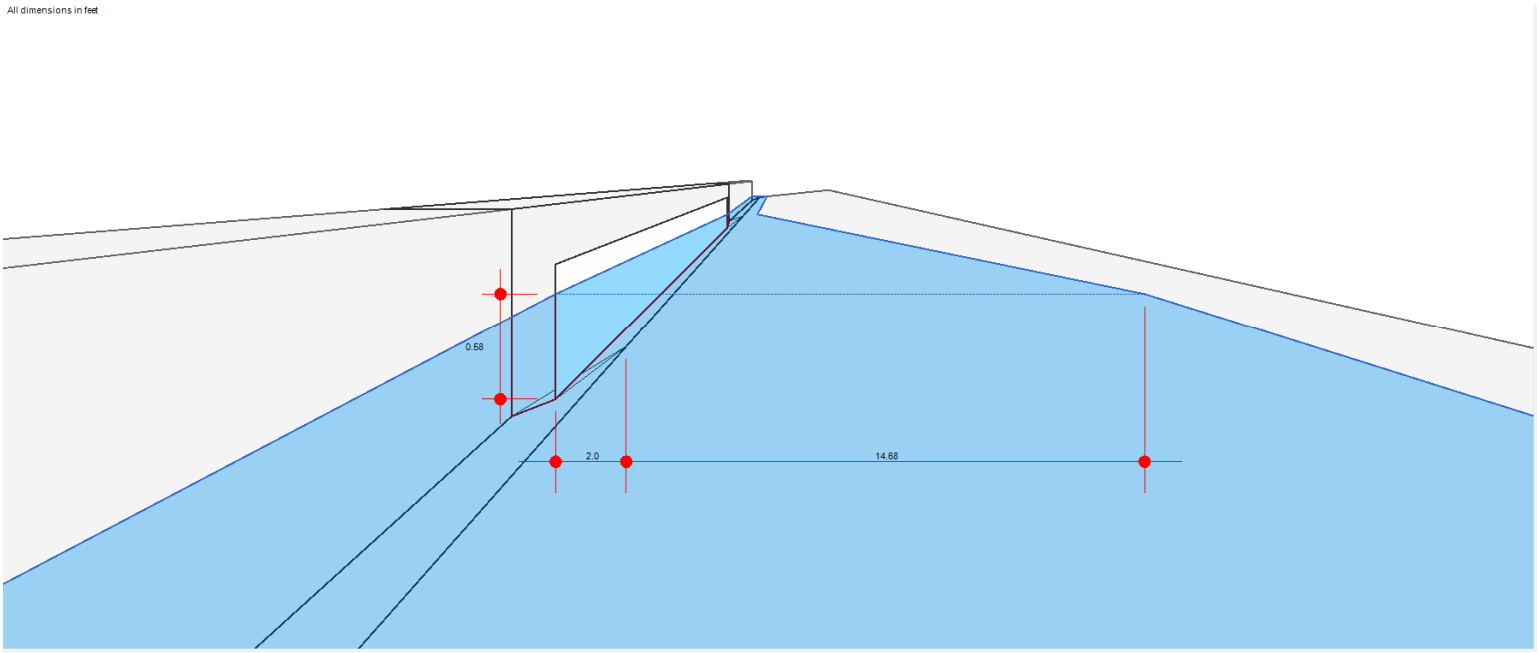
Slope, Sw (ft/ft)	=	0.083
Slope, Sx (ft/ft)	=	0.020
Local Depr (in)	=	1.50
Gutter Width (ft)	=	2.00
Gutter Slope (%)	=	1.00
Gutter n-value	=	0.015

Calculations

Compute by:		Known Q
Q (cfs)	=	11.05

Highlighted

Q Total (cfs)	=	11.05
Q Capt (cfs)	=	10.39
Q Bypass (cfs)	=	0.66
Depth at Inlet (in)	=	7.02
Efficiency (%)	=	94
Gutter Spread (ft)	=	16.68
Gutter Vel (ft/s)	=	3.80
Bypass Spread (ft)	=	3.83
Bypass Depth (in)	=	2.43



60’ Street
Worksheet for Irregular Channel

Project Description	
Worksheet	60' Street
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data		
Slope	0.010000	ft/ft
Water Surface Elevation	0.50	ft

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

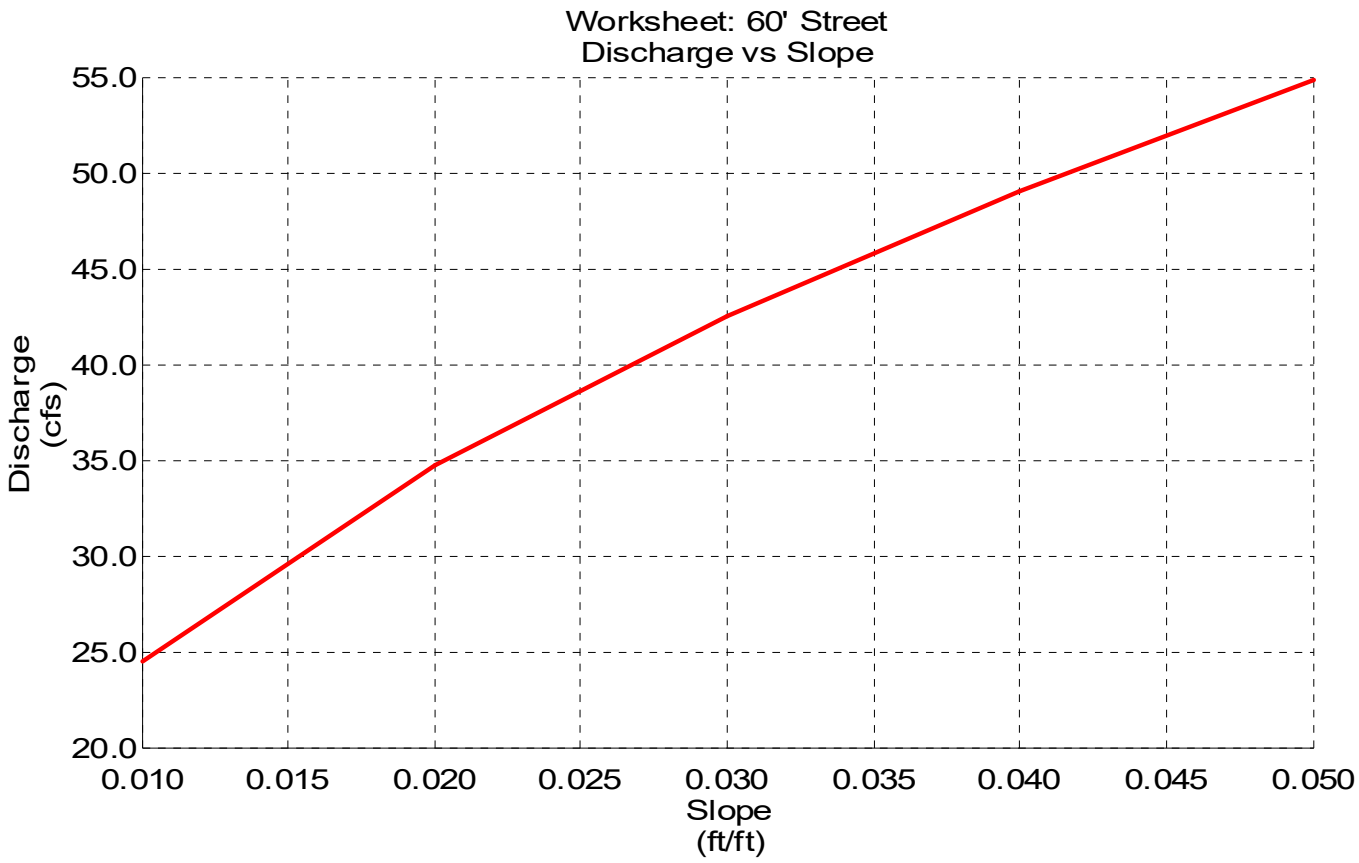
Results		
Mannings Coefficient	0.015	
Elevation Range	0.00 to 0.70	
Discharge	24.53	cfs
Flow Area	7.5	ft²
Wetted Perimeter	39.02	ft
Top Width	38.00	ft
Actual Depth	0.50	ft
Critical Elevation	0.55	ft
Critical Slope	0.005677	ft/ft
Velocity	3.29	ft/s
Velocity Head	0.17	ft
Specific Energy	0.67	ft
Froude Number	1.31	
Flow Type	Supercritical	

Calculation Messages:
Flow is divided.

Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00	0+60	0.015

Natural Channel Points	
Station (ft)	Elevation (ft)
0+00	0.70
0+10	0.50
0+10	0.00
0+12	0.16
0+30	0.52
0+48	0.16
0+50	0.00
0+50	0.50
0+60	0.70

60’ Street
Worksheet for Irregular Channel



66’ Street
Worksheet for Irregular Channel

Project Description	
Worksheet	66' Street
Flow Element	Irregular Channel
Method	Manning's Formula
Solve For	Discharge

Input Data		
Slope	0.010000	ft/ft
Water Surface Elevation	0.50	ft

Options	
Current Roughness Method	Improved Lotter's Method
Open Channel Weighting Method	Improved Lotter's Method
Closed Channel Weighting Method	Horton's Method

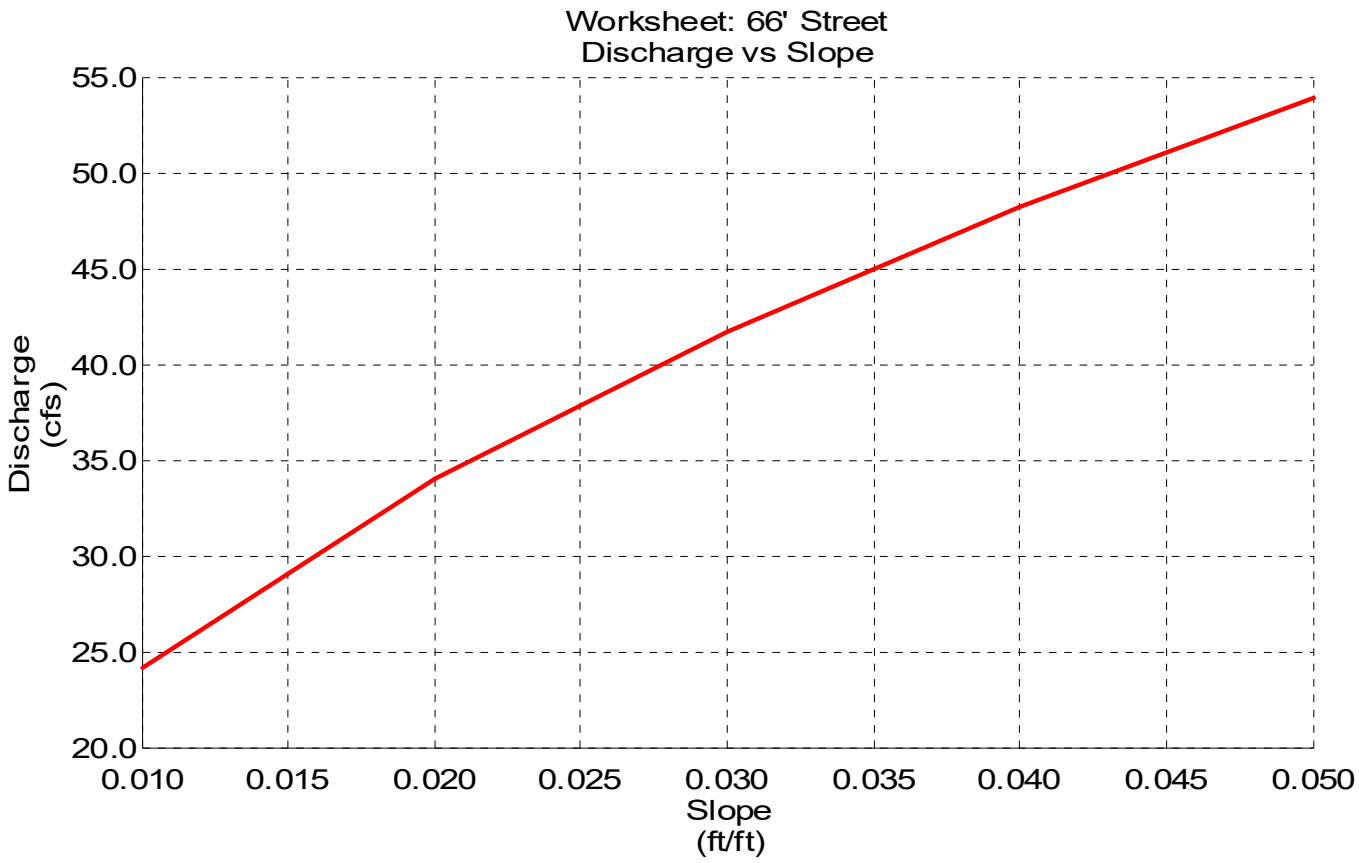
Results		
Mannings Coefficient	0.015	
Elevation Range	0.00 to 0.72	
Discharge	24.09	cfs
Flow Area	7.3	ft²
Wetted Perimeter	38.17	ft
Top Width	37.15	ft
Actual Depth	0.50	ft
Critical Elevation	0.55	ft
Critical Slope	0.005770	ft/ft
Velocity	3.29	ft/s
Velocity Head	0.17	ft
Specific Energy	0.67	ft
Froude Number	1.31	
Flow Type	Supercritical	

Calculation Messages:
Flow is divided.

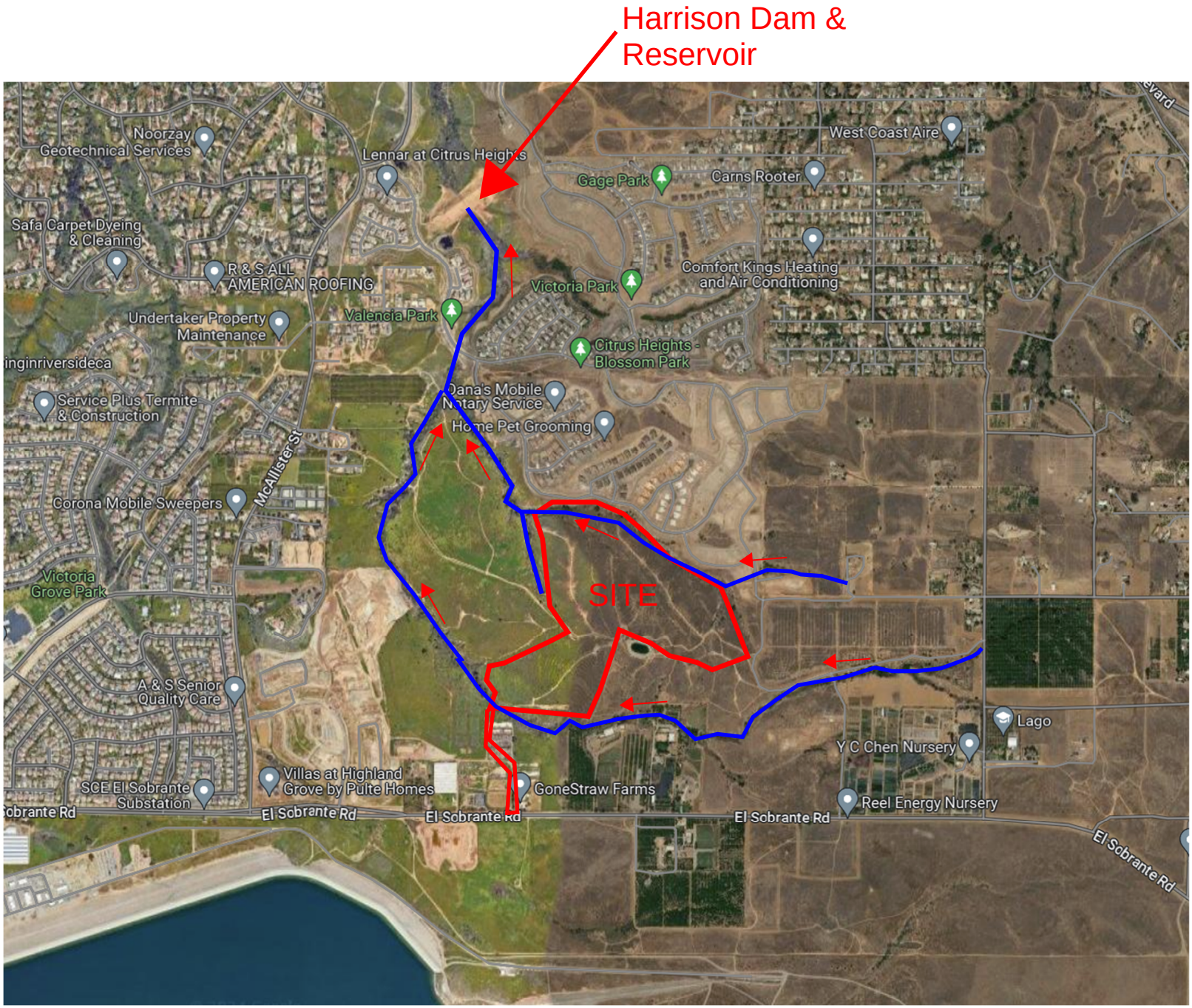
Roughness Segments		
Start Station	End Station	Mannings Coefficient
0+00	0+66	0.015

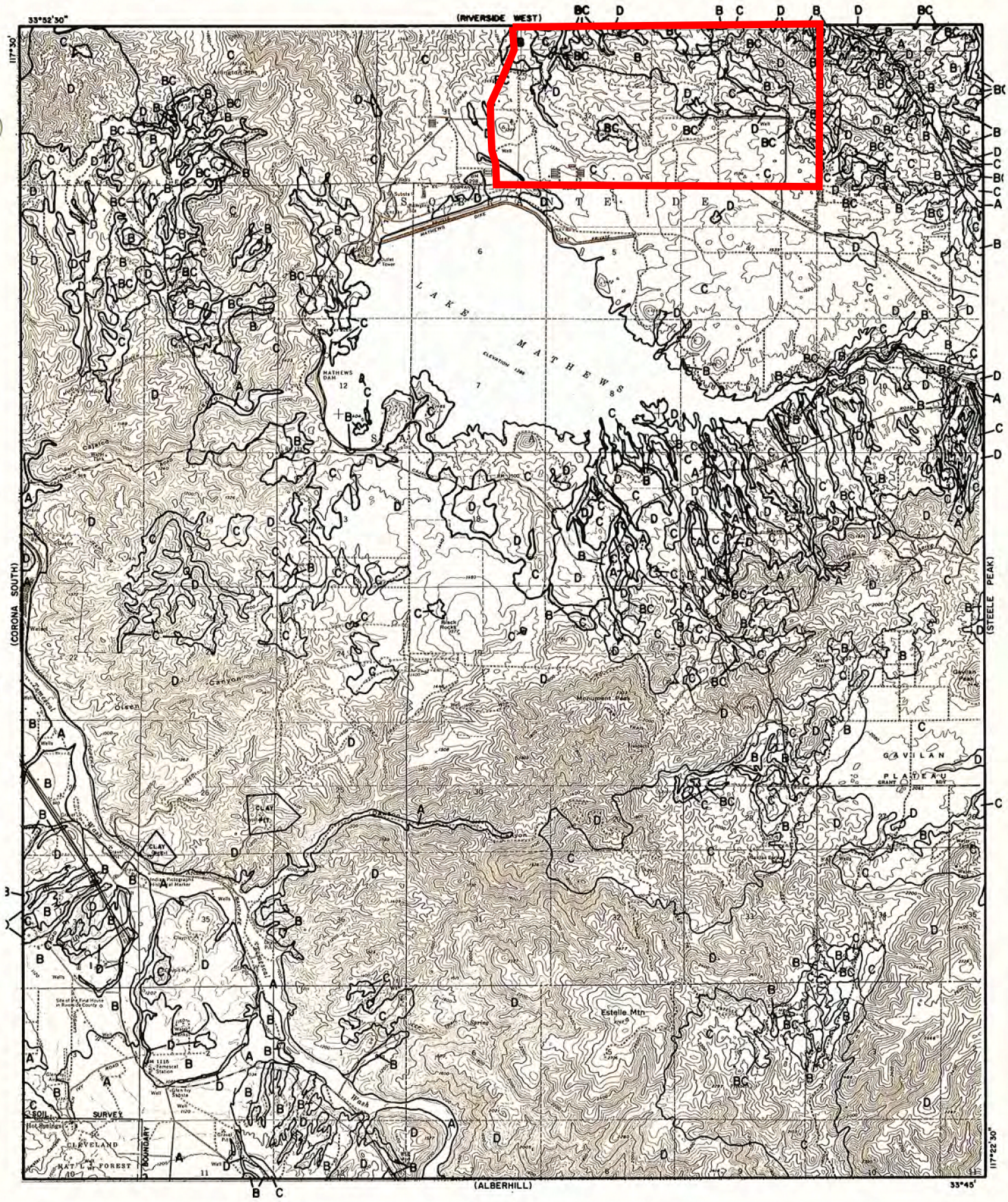
Natural Channel Points	
Station (ft)	Elevation (ft)
0+00	0.72
0+12	0.50
0+12	0.00
0+14	0.16
0+33	0.56
0+53	0.16
0+55	0.00
0+55	0.50
0+66	0.72

66’ Street
Worksheet for Irregular Channel



Appendix G – Riverside County Flood Control Hydology Manual Plates


Harrison Dam &
Reservoir
Noorzay
Geotechnical Services
Lennar at Citrus Heights
West Coast Aire
Gage Park
Carns Rooter
Safa Carpet Dyeing
& Cleaning
R & S ALL
AMERICAN ROOFING
Comfort Kings Heating
and Air Conditioning
Victoria Park
Undertaker Property
Maintenance
Valencia Park
Citrus Heights -
Blossom Park
Service Plus Termite
& Construction
Dana's Mobile
Notary Service
Home Pet Grooming
McAllister St
Corona Mobile Sweepers
SITE
Victoria
Grove Park
A & S Senior
Quality Care
Lago
Y C Chen Nursery
SCE El Sobrante
Substation
Villas at Highland
Grove by Pulte Homes
GoneStraw Farms
Reel Energy Nursery
El Sobrante Rd
El Sobrante Rd
El Sobrante Rd
El Sobrante Rd



LEGEND

—— SOILS GROUP BOUNDARY

A SOILS GROUP DESIGNATION

RCFC&WCD

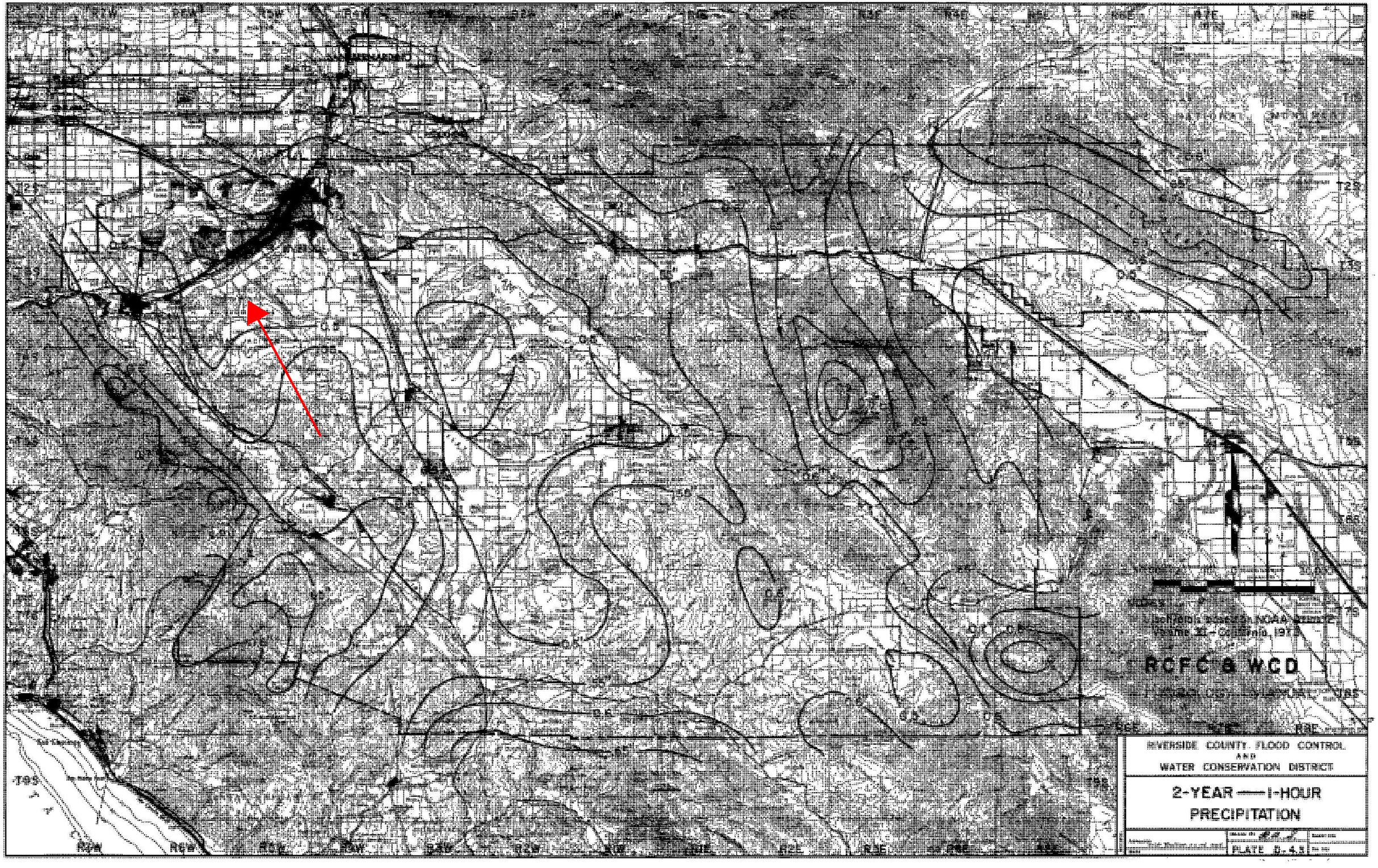
HYDROLOGY MANUAL

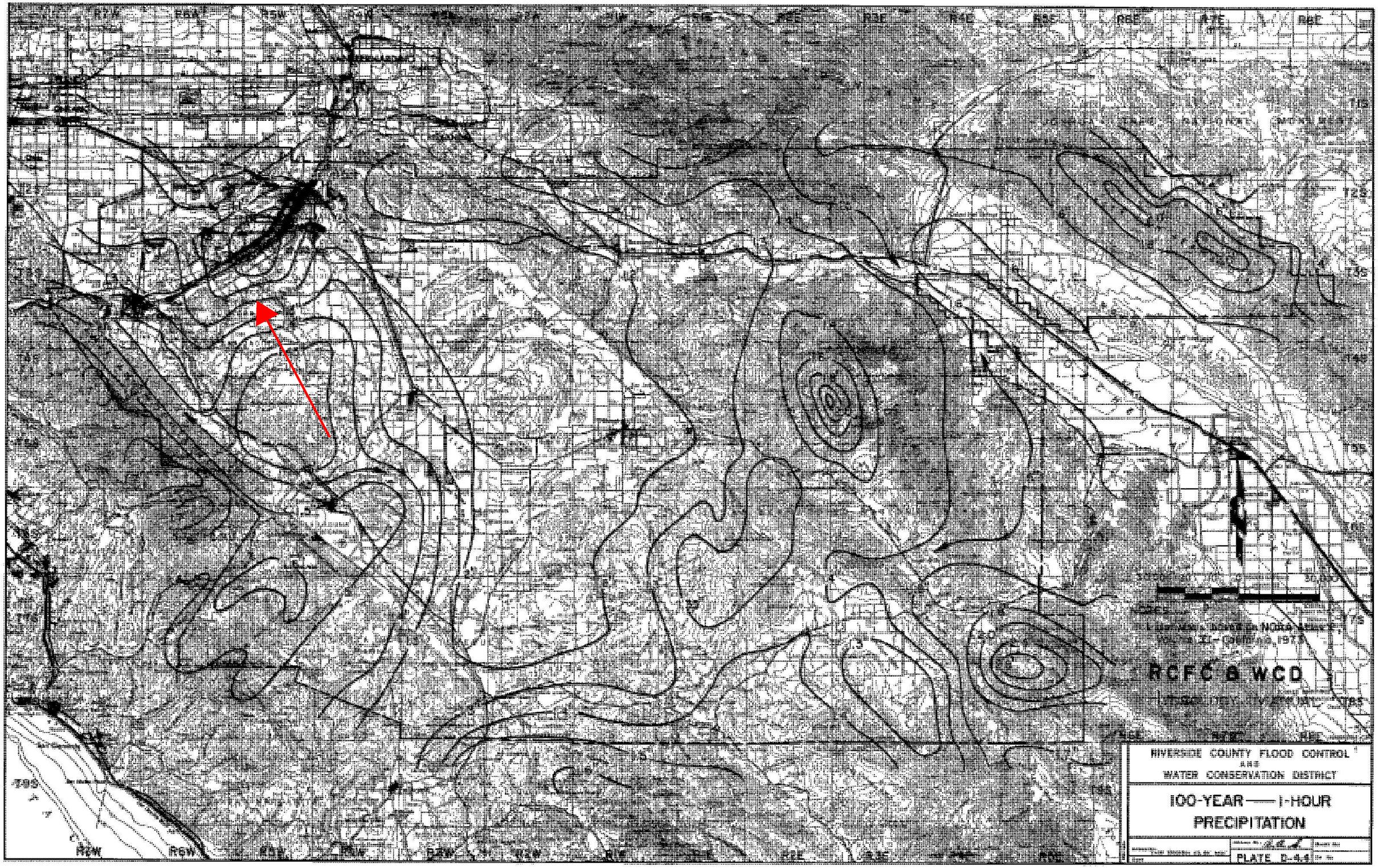
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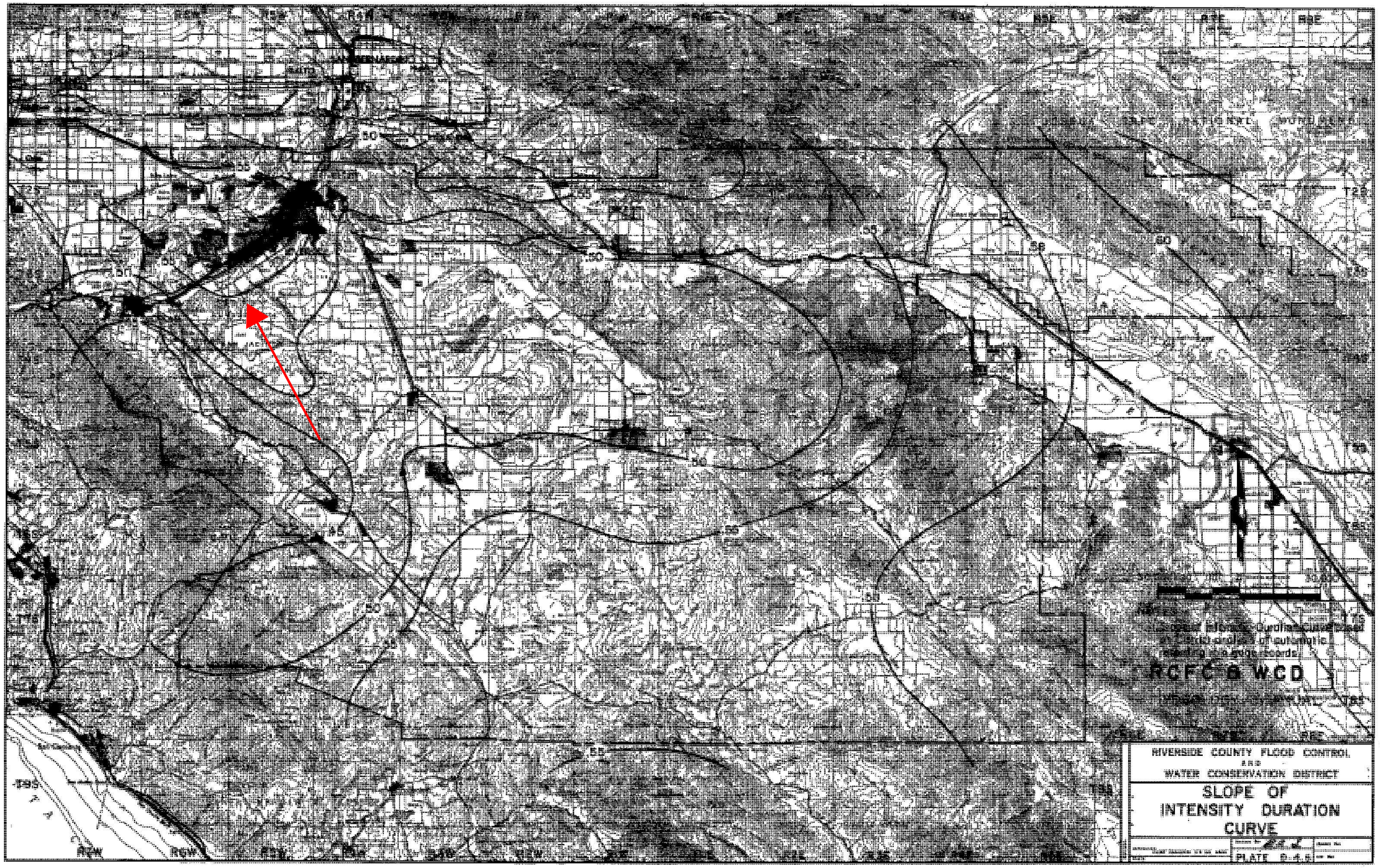
0 FEET 5000

HYDROLOGIC SOILS GROUP MAP FOR LAKE MATHEWS

PLATE C-1.28


RCFC & WCD
RIVERSIDE COUNTY FLOOD CONTROL
AND
WATER CONSERVATION DISTRICT
2-YEAR — 1-HOUR
PRECIPITATION
PLATE D-4.3


RCFC & WCD
RIVERSIDE COUNTY FLOOD CONTROL AND WATER CONSERVATION DISTRICT
100-YEAR — 1-HOUR PRECIPITATION
PLATE D-4.4


RIVERSIDE COUNTY FLOOD CONTROL
AND
WATER CONSERVATION DISTRICT
SLOPE OF
INTENSITY DURATION
CURVE
PLATE D-4.6
RCFC & WCD

ACTUAL IMPERVIOUS COVER

Land Use (1)	Range-Percent	Recommended Value For Average Conditions-Percent(2)
Natural or Agriculture	0 - 10	0
Single Family Residential: (3)		
40,000 S. F. (1 Acre) Lots	10 - 25	20
20,000 S. F. (½ Acre) Lots	30 - 45	40
7,200 - 10,000 S. F. Lots	45 - 55	50
Multiple Family Residential:		
Condominiums	45 - 70	65
Apartments	65 - 90	80
Mobile Home Park	60 - 85	75
Commercial, Downtown Business or Industrial	80 -100	90

Notes:

1. Land use should be based on ultimate development of the watershed. Long range master plans for the County and incorporated cities should be reviewed to insure reasonable land use assumptions.

2. Recommended values are based on average conditions which may not apply to a particular study area. The percentage impervious may vary greatly even on comparable sized lots due to differences in dwelling size, improvements, etc. Landscape practices should also be considered as it is common in some areas to use ornamental gravels underlain by impervious plastic materials in place of lawns and shrubs. A field investigation of a study area should always be made, and a review of aerial photos, where available may assist in estimating the percentage of impervious cover in developed areas.

3. For typical horse ranch subdivisions increase impervious area 5 percent over the values recommended in the table above.

RCFC & WCD
HYDROLOGY MANUAL

IMPERVIOUS COVER FOR DEVELOPED AREAS

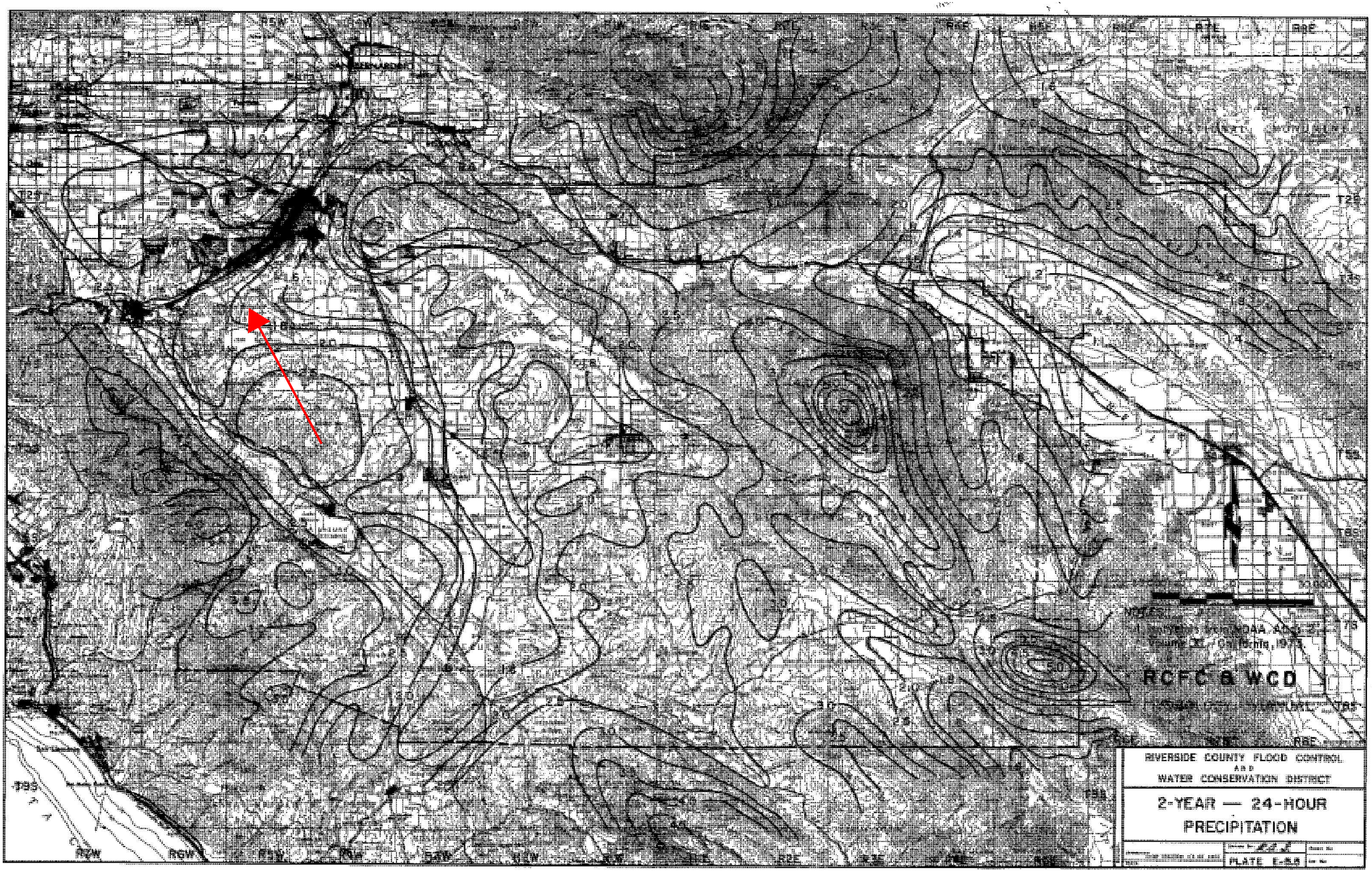
RUNOFF INDEX NUMBERS OF HYDROLOGIC SOIL-COVER COMPLEXES FOR PERVIOUS AREAS-AMC II

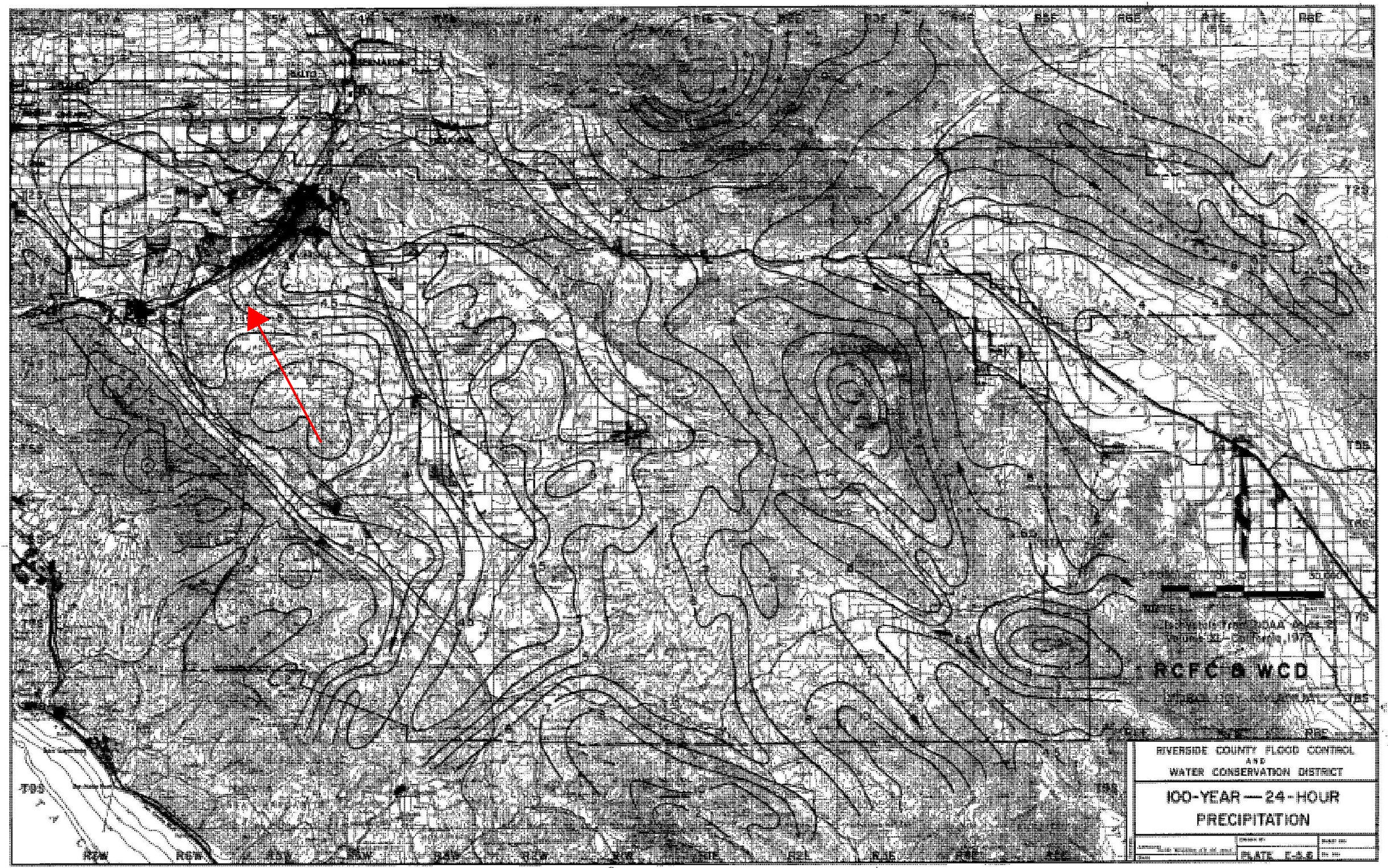
Cover Type (3)	Quality of Cover (2)	Soil Group A	B	C	D
NATURAL COVERS -					
Barren (Rockland, eroded and graded land)		78	86	91	93
Chaparrel, Broadleaf (Manzonita, ceanothus and scrub oak)	Poor	53	70	80	85
	Fair	40	63	75	81
	Good	31	57	71	78
Chaparrel, Narrowleaf (Chamise and redshank)	Poor	71	82	88	91
	Fair	55	72	81	86
Grass, Annual or Perennial	Poor	67	78	86	89
	Fair	50	69	79	84
	Good	38	61	74	80
Meadows or Cienegas (Areas with seasonally high water table, principal vegetation is sod forming grass)	Poor	63	77	85	88
	Fair	51	70	80	84
	Good	30	58	72	78
Open Brush (Soft wood shrubs - buckwheat, sage, etc.)	Poor	62	76	84	88
	Fair	46	66	77	83
	Good	41	63	75	81
Woodland (Coniferous or broadleaf trees predominate. Canopy density is at least 50 percent)	Poor	45	66	77	83
	Fair	36	60	73	79
	Good	28	55	70	77
Woodland, Grass (Coniferous or broadleaf trees with canopy density from 20 to 50 percent)	Poor	57	73	82	86
	Fair	44	65	77	82
	Good	33	58	72	79
URBAN COVERS -					
Residential or Commercial Landscaping (Lawn, shrubs, etc.)	Good	32	56	69	75
Turf (Irrigated and mowed grass)	Poor	58	74	83	87
	Fair	44	65	77	82
	Good	33	58	72	79
AGRICULTURAL COVERS -					
Fallow (Land plowed but not tilled or seeded)		76	85	90	92

RCFC & WCD
HYDROLOGY MANUAL

RUNOFF INDEX NUMBERS FOR PERVIOUS AREA

PLATE D-5.5 (1 of 2)


RIVERSIDE COUNTY FLOOD CONTROL
AND
WATER CONSERVATION DISTRICT
2-YEAR — 24-HOUR
PRECIPITATION
PLATE E-5.6
RCFC & WCD



RIVERSIDE COUNTY FLOOD CONTROL
AND
WATER CONSERVATION DISTRICT

100-YEAR — 24-HOUR PRECIPITATION

PLATE E-4.8