

# Appendix A

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VMT Analysis Memorandum



# ASSOCIATED TRANSPORTATION ENGINEERS

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Since 1978

Richard L. Pool, P.E.  
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December 13, 2023

22086.01L02

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## **VMT ANALYSIS MEMO FOR THE BELLECREST SENIOR RESIDENTIAL PROJECT – CITY OF SANTA MARIA**

Associated Transportation Engineers (ATE) has been retained to prepare a traffic and VMT study for the Bellecrest Senior Residential Project (the “Project”), located on the north side of East Main Street in the City of Santa Maria. The following memo outlines our comments on the initial VMT analysis provided by City staff for the Project.

### **PROJECT DESCRIPTION**

The Project site is located on the north side of East Main Street, west of Suey Road and east of Navara Way in the City of Santa Maria, as shown on Figure 1 (attached). Figure 2 presents the Project site plan. The Project is proposing to develop a senior residential housing complex with 102 detached units, 40 attached duplex units, and associated recreational amenities. The units would be compact in size (712 square feet to 1,413 SF) and thus would operate more like senior apartments than detached housing. Access to the Project is proposed via a new roadway connection to Main Street located approximately midway between Suey Road and Navara Way.

### **BACKGROUND**

The City’s VMT screening map (attached) shows that the Project is located in an area that generates up to the average VMT per capita (14.52 two-way trips). ATE asked City staff to utilize the City’s VMT calculator to develop VMT estimates for the Project (results attached). The City’s VMT calculator indicated that the Project would generate 17.60 VMT per Capita, which is 30% greater than the range shown on the VMT screening map. Thus, there is a significant discrepancy between the City’s VMT calculator and the VMT screening map which is presumably based on the same model as the calculator. *This discrepancy should be reviewed with the City traffic model consultant.*



## PROJECT TRAFFIC COMPARISON

As noted, the Project is proposing to develop small senior detached and attached units ranging in size from 712 SF square feet to 1,413 SF. These senior units would generate substantially less traffic than standard single family homes. The Project site is located in a traffic model zone that contains predominantly single family homes, thus the baseline VMT estimates produced by the model and shown on the VMT screening map for the Project site do not accurately reflect the type of senior housing proposed.

Table 2 provides a comparison of the trip generation rates for senior housing units and single-family housing units.

**Table 2**  
**Project Trip Generation – Senior Adult Housing vs Single-Family Housing**

Land use	ADT Rate	AM Peak Rate	PM Peak Rate
Senior Detached Housing	4.31/Unit	0.24/Unit	0.30/Unit
Single-Family Housing	9.43/Unit	0.70/Unit	0.94/Unit
<b>Percent Reduction</b>	<b>-54%</b>	<b>-66%</b>	<b>-68%</b>

The data presented in Table 2 show that the senior housing units are forecast to generate 54% less average daily traffic, 66% less AM peak hour traffic, and 68% less PM peak hour traffic than single-family housing units.

The City's VMT calculator and VMT screening map do not have the flexibility to account for the type of senior residential units proposed, instead they are based on the attributes of the existing single family houses located in the Project study area and model zone. The senior housing units generate significantly less traffic than single family units and the trip lengths associated with the senior housing units would be much lower than the adjacent single-family units, thus the resulting per capita VMT estimates would be much lower than forecast.

It is recommended that adjustments be applied to the VMT forecasts shown on the City's VMT screening map to account for the type of senior housing proposed. Given that the senior units would generate 54% less average traffic than single family units and the senior residents would have much shorter trip lengths, a VMT adjustment of 35% to 45% could be justified. *This would result in VMT estimates that would be less than the City's VMT impact thresholds.*

This concludes ATE's VMT analysis memo for the Bellecrest Senior Residential Project. We look forward to discussing these issues with City staff as we move forward with the Project. Feel free to call if you have any questions.

Associated Transportation Engineers,

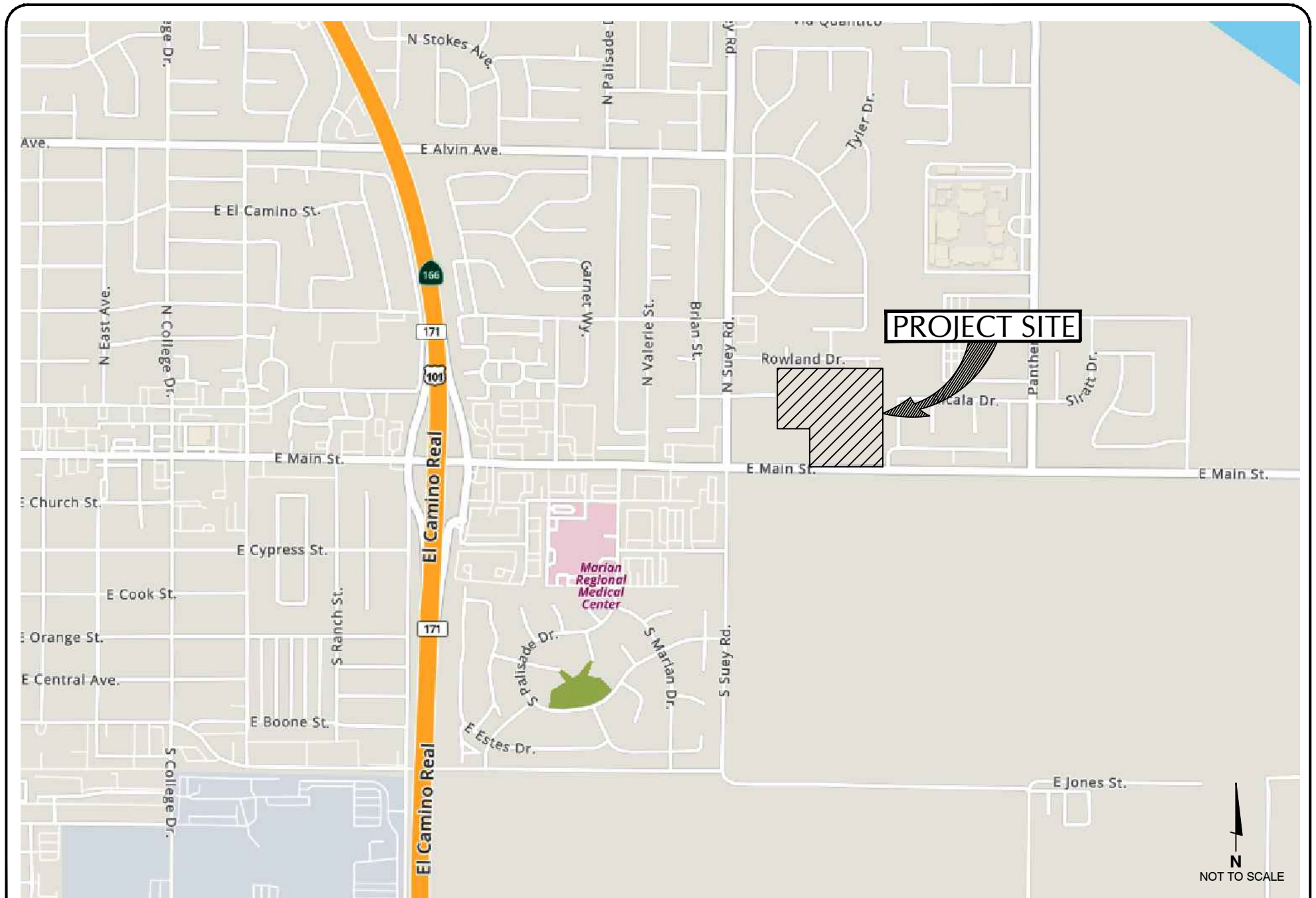
A handwritten signature in black ink, appearing to read "Scott Schell". The signature is fluid and cursive, with the first name "Scott" and last name "Schell" clearly distinguishable.

Scott Schell  
Principal Transportation Planner

SAS/GOM

Attachments

Cc: Brian Schwartz, UPC  
Laurie Tamura, UPC



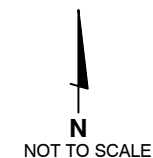
ASSOCIATED  
TRANSPORTATION  
ENGINEERS

## PROJECT SITE LOCATION

FIGURE

1

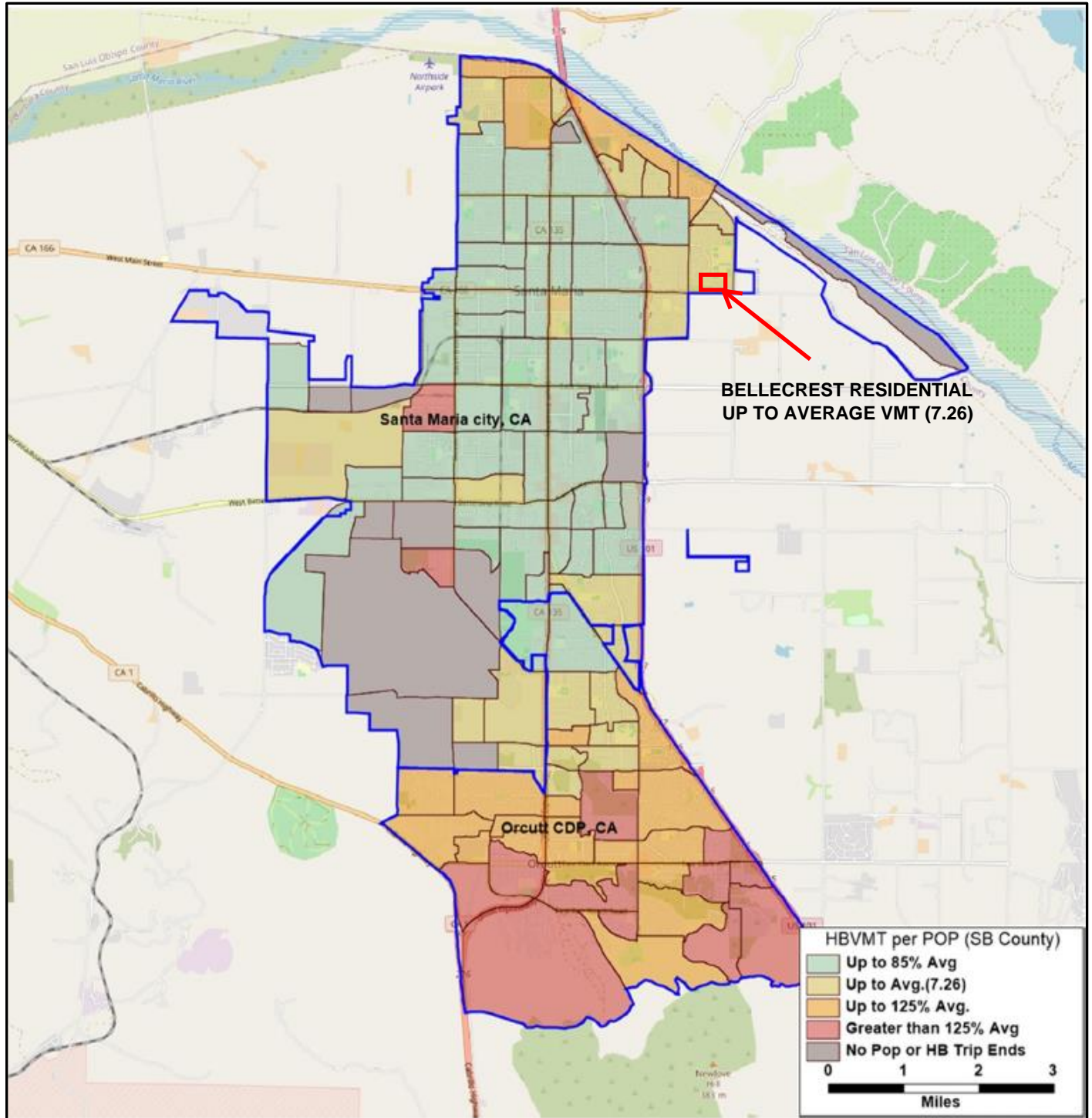






## Appendix B

### Countywide Average: Home-Based VMT per Population (Residential Land Uses)





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## Bellecrest Senior Residential Component City of Santa Maria VMT Calculator Results

### The VMT Screening Results

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Project Name: Bellecrest Residential  
Project Parcel: 128-052-014  
Daily Trips: 612  
Peak Hour Trips: 43

#### -----Proposed Development and Estimated VMT Impact-----

Residential: 142

The residential development is estimated to generate 17.6 VMT per person. The rate is higher than the adopted threshold. Please adjust the project parameters or propose mitigation.

Office:

This project does not include Office development.

Commercial:

This project does not include Commercial development.

Industrial:

This project does not include Industrial development.

# Appendix B

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# 1. Basic Project Information

## 1.1. Basic Project Information

Data Field	Value
Project Name	Bellecrest Residences
Construction Start Date	1/2/2025
Operational Year	2029
Lead Agency	—
Land Use Scale	Project/site
Analysis Level for Defaults	County
Windspeed (m/s)	2.90
Precipitation (days)	10.0
Location	1571 E Main St, Santa Maria, CA 93454, USA
County	Santa Barbara
City	Santa Maria
Air District	Santa Barbara County APCD
Air Basin	South Central Coast
TAZ	3385
EDFZ	6
Electric Utility	Pacific Gas & Electric Company
Gas Utility	Southern California Gas
App Version	2022.1.1.22

## 1.2. Land Use Types

Land Use Subtype	Size	Unit	Lot Acreage	Building Area (sq ft)	Landscape Area (sq ft)	Special Landscape Area (sq ft)	Population	Description
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Single Family Housing	142	Dwelling Unit	8.10	351,980	0.00	—	248	—
Parking Lot	126	Space	1.13	0.00	0.00	—	—	—
City Park	1.57	Acre	1.57	0.00	203,140	0.00	—	—

### 1.3. User-Selected Emission Reduction Measures by Emissions Sector

No measures selected

## 2. Emissions Summary

### 2.1. Construction Emissions Compared Against Thresholds

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Un/Mit.	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	1.81	4.40	13.4	72.8	0.18	0.33	10.1	10.4	0.30	4.43	4.73	—	18,033	18,033	0.82	0.83	9.86	18,311
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	2.94	4.55	22.4	72.9	0.18	0.92	10.1	10.4	0.85	4.43	4.73	—	18,028	18,028	0.82	0.83	0.26	18,297
Average Daily (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	0.88	3.03	6.28	22.1	0.05	0.17	2.17	2.34	0.16	0.92	1.07	—	5,000	5,000	0.23	0.19	1.28	5,062
Annual (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	0.16	0.55	1.15	4.03	0.01	0.03	0.40	0.43	0.03	0.17	0.20	—	828	828	0.04	0.03	0.21	838
Exceeds (Daily Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—



Threshold	—	25.0	25.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	—	No	No	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Exceeds (Average Daily)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Threshold	—	25.0	25.0	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	—	No	No	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

## 2.2. Construction Emissions by Year, Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Year	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily - Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2025	1.81	1.53	13.4	72.8	0.18	0.33	10.1	10.4	0.30	4.43	4.73	—	18,033	18,033	0.82	0.83	9.86	18,311
2026	0.86	4.40	5.80	17.2	0.03	0.04	0.96	1.00	0.04	0.23	0.27	—	3,727	3,727	0.17	0.13	4.70	3,775
2027	0.80	4.36	5.71	16.6	0.03	0.04	0.91	0.95	0.04	0.22	0.26	—	3,654	3,654	0.14	0.13	4.12	3,701
2028	0.45	4.03	2.93	9.60	0.02	0.02	0.53	0.55	0.02	0.13	0.15	—	2,091	2,091	0.08	0.07	2.13	2,115
Daily - Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2025	2.94	4.55	22.4	72.9	0.18	0.92	10.1	10.4	0.85	4.43	4.73	—	18,028	18,028	0.82	0.83	0.26	18,297
2026	0.93	4.53	5.87	28.6	0.05	0.08	0.96	1.00	0.08	0.23	0.27	—	5,722	5,722	0.23	0.13	0.12	5,760
2027	0.81	4.36	5.78	16.8	0.03	0.04	0.91	0.95	0.04	0.22	0.26	—	3,639	3,639	0.15	0.13	0.11	3,682
2028	0.45	4.03	2.96	9.67	0.02	0.02	0.53	0.55	0.02	0.13	0.15	—	2,082	2,082	0.08	0.07	0.06	2,105
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2025	0.88	1.43	6.28	22.1	0.05	0.17	2.17	2.34	0.16	0.92	1.07	—	5,000	5,000	0.23	0.19	1.28	5,062
2026	0.48	3.03	3.19	9.78	0.02	0.02	0.54	0.56	0.02	0.13	0.15	—	2,099	2,099	0.10	0.07	1.14	2,124

2027	0.45	3.00	3.14	9.43	0.02	0.02	0.51	0.54	0.02	0.12	0.15	—	2,053	2,053	0.08	0.07	1.00	2,078
2028	0.28	2.22	1.92	5.98	0.01	0.01	0.33	0.34	0.01	0.08	0.09	—	1,306	1,306	0.05	0.04	0.58	1,321
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
2025	0.16	0.26	1.15	4.03	0.01	0.03	0.40	0.43	0.03	0.17	0.20	—	828	828	0.04	0.03	0.21	838
2026	0.09	0.55	0.58	1.79	< 0.005	< 0.005	0.10	0.10	< 0.005	0.02	0.03	—	348	348	0.02	0.01	0.19	352
2027	0.08	0.55	0.57	1.72	< 0.005	< 0.005	0.09	0.10	< 0.005	0.02	0.03	—	340	340	0.01	0.01	0.17	344
2028	0.05	0.41	0.35	1.09	< 0.005	< 0.005	0.06	0.06	< 0.005	0.01	0.02	—	216	216	0.01	0.01	0.10	219

## 2.4. Operations Emissions Compared Against Thresholds

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Un/Mit.	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	3.02	11.3	2.53	17.4	0.03	0.13	1.60	1.73	0.13	0.41	0.54	44.2	4,112	4,156	3.77	0.14	7.70	4,299
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	2.30	10.6	2.55	10.2	0.03	0.13	1.60	1.73	0.13	0.41	0.53	44.2	4,066	4,110	3.78	0.14	2.66	4,250
Average Daily (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	2.63	10.9	2.57	13.7	0.03	0.13	1.58	1.71	0.13	0.40	0.53	44.2	4,071	4,116	3.78	0.14	4.75	4,257
Annual (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Unmit.	0.48	1.99	0.47	2.51	< 0.005	0.02	0.29	0.31	0.02	0.07	0.10	7.32	674	681	0.63	0.02	0.79	705

## 2.5. Operations Emissions by Sector, Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Sector	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	2.11	2.01	1.02	8.73	0.02	0.01	1.60	1.61	0.01	0.41	0.42	—	1,749	1,749	0.13	0.10	5.18	1,788
Area	0.74	9.19	0.08	8.08	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	0.00	21.5	21.5	< 0.005	< 0.005	—	21.6
Energy	0.17	0.08	1.43	0.61	0.01	0.12	—	0.12	0.12	—	0.12	—	2,321	2,321	0.24	0.01	—	2,331
Water	—	—	—	—	—	—	—	—	—	—	—	10.7	20.3	31.0	0.04	0.02	—	39.0
Waste	—	—	—	—	—	—	—	—	—	—	—	33.6	0.00	33.6	3.35	0.00	—	117
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	2.52	2.52
Total	3.02	11.3	2.53	17.4	0.03	0.13	1.60	1.73	0.13	0.41	0.54	44.2	4,112	4,156	3.77	0.14	7.70	4,299
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	2.13	2.02	1.12	9.58	0.02	0.01	1.60	1.61	0.01	0.41	0.42	—	1,725	1,725	0.14	0.11	0.13	1,760
Area	0.00	8.49	0.00	0.00	0.00	0.00	—	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00
Energy	0.17	0.08	1.43	0.61	0.01	0.12	—	0.12	0.12	—	0.12	—	2,321	2,321	0.24	0.01	—	2,331
Water	—	—	—	—	—	—	—	—	—	—	—	10.7	20.3	31.0	0.04	0.02	—	39.0
Waste	—	—	—	—	—	—	—	—	—	—	—	33.6	0.00	33.6	3.35	0.00	—	117
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	2.52	2.52
Total	2.30	10.6	2.55	10.2	0.03	0.13	1.60	1.73	0.13	0.41	0.53	44.2	4,066	4,110	3.78	0.14	2.66	4,250
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	2.10	1.99	1.10	9.14	0.02	0.01	1.58	1.60	0.01	0.40	0.41	—	1,719	1,719	0.14	0.10	2.23	1,756
Area	0.36	8.83	0.04	3.98	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	0.00	10.6	10.6	< 0.005	< 0.005	—	10.7
Energy	0.17	0.08	1.43	0.61	0.01	0.12	—	0.12	0.12	—	0.12	—	2,321	2,321	0.24	0.01	—	2,331
Water	—	—	—	—	—	—	—	—	—	—	—	10.7	20.3	31.0	0.04	0.02	—	39.0
Waste	—	—	—	—	—	—	—	—	—	—	—	33.6	0.00	33.6	3.35	0.00	—	117
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	2.52	2.52

Total	2.63	10.9	2.57	13.7	0.03	0.13	1.58	1.71	0.13	0.40	0.53	44.2	4,071	4,116	3.78	0.14	4.75	4,257
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Mobile	0.38	0.36	0.20	1.67	< 0.005	< 0.005	0.29	0.29	< 0.005	0.07	0.08	—	285	285	0.02	0.02	0.37	291
Area	0.07	1.61	0.01	0.73	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	0.00	1.76	1.76	< 0.005	< 0.005	—	1.76
Energy	0.03	0.02	0.26	0.11	< 0.005	0.02	—	0.02	0.02	—	0.02	—	384	384	0.04	< 0.005	—	386
Water	—	—	—	—	—	—	—	—	—	—	—	1.77	3.37	5.13	0.01	< 0.005	—	6.47
Waste	—	—	—	—	—	—	—	—	—	—	—	5.56	0.00	5.56	0.56	0.00	—	19.4
Refrig.	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.42	0.42
Total	0.48	1.99	0.47	2.51	< 0.005	0.02	0.29	0.31	0.02	0.07	0.10	7.32	674	681	0.63	0.02	0.79	705

## 3. Construction Emissions Details

### 3.1. Demolition (2025) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	2.86	2.40	22.2	19.9	0.03	0.92	—	0.92	0.84	—	0.84	—	3,425	3,425	0.14	0.03	—	3,437
Demolition	—	—	—	—	—	—	0.07	0.07	—	0.01	0.01	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Off-Road Equipment	0.17	0.14	1.34	1.20	< 0.005	0.06	—	0.06	0.05	—	0.05	—	206	206	0.01	< 0.005	—	207
Demolition	—	—	—	—	—	—	< 0.005	< 0.005	—	< 0.005	< 0.005	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.03	0.03	0.24	0.22	< 0.005	0.01	—	0.01	0.01	—	0.01	—	34.2	34.2	< 0.005	< 0.005	—	34.3
Demolition	—	—	—	—	—	—	< 0.005	< 0.005	—	< 0.005	< 0.005	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.07	0.07	0.06	0.57	0.00	0.00	0.09	0.09	0.00	0.02	0.02	—	92.4	92.4	0.01	< 0.005	0.01	93.9
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.01	< 0.005	0.14	0.05	< 0.005	< 0.005	0.02	0.03	< 0.005	0.01	0.01	—	97.1	97.1	0.01	0.02	< 0.005	102
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	< 0.005	< 0.005	< 0.005	0.03	0.00	0.00	0.01	0.01	0.00	< 0.005	< 0.005	—	5.58	5.58	< 0.005	< 0.005	0.01	5.67
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	< 0.005	< 0.005	0.01	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	—	5.85	5.85	< 0.005	< 0.005	< 0.005	6.14
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	< 0.005	< 0.005	< 0.005	0.01	0.00	0.00	< 0.005	< 0.005	0.00	< 0.005	< 0.005	—	0.92	0.92	< 0.005	< 0.005	< 0.005	0.94
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	—	0.97	0.97	< 0.005	< 0.005	< 0.005	1.02

### 3.3. Site Preparation (2025) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	2.11	1.77	16.0	17.8	0.03	0.67	—	0.67	0.61	—	0.61	—	2,950	2,950	0.12	0.02	—	2,960
Dust From Material Movement	—	—	—	—	—	—	2.56	2.56	—	1.31	1.31	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.12	0.10	0.88	0.98	< 0.005	0.04	—	0.04	0.03	—	0.03	—	162	162	0.01	< 0.005	—	162
Dust From Material Movement	—	—	—	—	—	—	0.14	0.14	—	0.07	0.07	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.02	0.02	0.16	0.18	< 0.005	0.01	—	0.01	0.01	—	0.01	—	26.8	26.8	< 0.005	< 0.005	—	26.9

Dust From Material Movement	—	—	—	—	—	—	0.03	0.03	—	0.01	0.01	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.09	0.08	0.06	0.67	0.00	0.00	0.11	0.11	0.00	0.03	0.03	—	108	108	0.01	< 0.005	0.01	110
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	< 0.005	< 0.005	< 0.005	0.04	0.00	0.00	0.01	0.01	0.00	< 0.005	< 0.005	—	5.92	5.92	< 0.005	< 0.005	0.01	6.02
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	< 0.005	< 0.005	< 0.005	0.01	0.00	0.00	< 0.005	< 0.005	0.00	< 0.005	< 0.005	—	0.98	0.98	< 0.005	< 0.005	< 0.005	1.00
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.5. Grading (2025) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.24	1.24	6.99	69.0	0.12	0.25	—	0.25	0.25	—	0.25	—	13,281	13,281	0.54	0.11	—	13,327
Dust From Material Movement	—	—	—	—	—	—	8.71	8.71	—	4.05	4.05	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	1.24	1.24	6.99	69.0	0.12	0.25	—	0.25	0.25	—	0.25	—	13,281	13,281	0.54	0.11	—	13,327
Dust From Material Movement	—	—	—	—	—	—	8.71	8.71	—	4.05	4.05	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.22	0.22	1.24	12.3	0.02	0.04	—	0.04	0.04	—	0.04	—	2,365	2,365	0.10	0.02	—	2,373
Dust From Material Movement	—	—	—	—	—	—	1.55	1.55	—	0.72	0.72	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.04	0.04	0.23	2.24	< 0.005	0.01	—	0.01	0.01	—	0.01	—	392	392	0.02	< 0.005	—	393



Dust From Material Movement:	—	—	—	—	—	—	0.28	0.28	—	0.13	0.13	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.22	0.20	0.14	1.69	0.00	0.00	0.28	0.28	0.00	0.07	0.07	—	283	283	0.02	0.01	1.25	289
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.36	0.09	6.23	2.16	0.05	0.08	1.10	1.18	0.05	0.31	0.36	—	4,469	4,469	0.26	0.71	8.61	4,696
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.22	0.20	0.17	1.72	0.00	0.00	0.28	0.28	0.00	0.07	0.07	—	277	277	0.02	0.01	0.03	282
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.35	0.09	6.40	2.18	0.05	0.08	1.10	1.18	0.05	0.31	0.36	—	4,470	4,470	0.26	0.71	0.22	4,688
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.04	0.04	0.03	0.30	0.00	0.00	0.05	0.05	0.00	0.01	0.01	—	49.4	49.4	< 0.005	< 0.005	0.10	50.3
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.06	0.02	1.15	0.39	0.01	0.01	0.19	0.21	0.01	0.05	0.06	—	796	796	0.05	0.13	0.66	835
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.01	0.01	0.01	0.05	0.00	0.00	0.01	0.01	0.00	< 0.005	< 0.005	—	8.18	8.18	< 0.005	< 0.005	0.02	8.33
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.01	< 0.005	0.21	0.07	< 0.005	< 0.005	0.04	0.04	< 0.005	0.01	0.01	—	132	132	0.01	0.02	0.11	138

### 3.7. Phase I Building Construction (2025) - Unmitigated

## Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.10	0.10	2.22	5.05	0.01	0.01	—	0.01	0.01	—	0.01	—	980	980	0.04	0.01	—	984
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.10	0.10	2.22	5.05	0.01	0.01	—	0.01	0.01	—	0.01	—	980	980	0.04	0.01	—	984
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.04	0.04	0.93	2.11	< 0.005	0.01	—	0.01	0.01	—	0.01	—	409	409	0.02	< 0.005	—	410
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01	0.01	0.17	0.38	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	67.7	67.7	< 0.005	< 0.005	—	67.9
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.24	0.23	0.16	1.92	0.00	0.00	0.32	0.32	0.00	0.07	0.07	—	322	322	0.02	0.01	1.42	328

Vendor	0.03	0.01	0.42	0.20	< 0.005	< 0.005	0.07	0.07	< 0.005	0.02	0.02	—	270	270	0.01	0.04	0.69	282
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.25	0.22	0.19	1.96	0.00	0.00	0.32	0.32	0.00	0.07	0.07	—	315	315	0.02	0.01	0.04	320
Vendor	0.02	0.01	0.44	0.21	< 0.005	< 0.005	0.07	0.07	< 0.005	0.02	0.02	—	270	270	0.01	0.04	0.02	281
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.10	0.10	0.07	0.79	0.00	0.00	0.13	0.13	0.00	0.03	0.03	—	131	131	0.01	0.01	0.26	134
Vendor	0.01	0.01	0.18	0.09	< 0.005	< 0.005	0.03	0.03	< 0.005	0.01	0.01	—	112	112	< 0.005	0.02	0.12	117
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.02	0.02	0.01	0.14	0.00	0.00	0.02	0.02	0.00	0.01	0.01	—	21.8	21.8	< 0.005	< 0.005	0.04	22.1
Vendor	< 0.005	< 0.005	0.03	0.02	< 0.005	< 0.005	0.01	0.01	< 0.005	< 0.005	< 0.005	—	18.6	18.6	< 0.005	< 0.005	0.02	19.4
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.9. Phase I Building Construction (2026) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.10	0.10	2.22	5.05	0.01	0.01	—	0.01	0.01	—	0.01	—	980	980	0.04	0.01	—	984
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.10	0.10	2.22	5.05	0.01	0.01	—	0.01	0.01	—	0.01	—	980	980	0.04	0.01	—	984
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.06	0.06	1.46	3.31	0.01	0.01	—	0.01	0.01	—	0.01	—	643	643	0.03	0.01	—	645
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01	0.01	0.27	0.60	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	106	106	< 0.005	< 0.005	—	107
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.23	0.21	0.15	1.76	0.00	0.00	0.32	0.32	0.00	0.07	0.07	—	315	315	0.02	0.01	1.32	321
Vendor	0.02	0.01	0.41	0.19	< 0.005	< 0.005	0.07	0.07	< 0.005	0.02	0.02	—	265	265	0.01	0.04	0.64	277
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.23	0.21	0.17	1.81	0.00	0.00	0.32	0.32	0.00	0.07	0.07	—	309	309	0.01	0.01	0.03	313
Vendor	0.02	0.01	0.42	0.20	< 0.005	< 0.005	0.07	0.07	< 0.005	0.02	0.02	—	265	265	0.01	0.04	0.02	276
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Worker	0.15	0.14	0.11	1.15	0.00	0.00	0.21	0.21	0.00	0.05	0.05	—	202	202	0.01	0.01	0.37	206
Vendor	0.01	0.01	0.28	0.13	< 0.005	< 0.005	0.04	0.05	< 0.005	0.01	0.01	—	174	174	0.01	0.02	0.18	181
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.03	0.03	0.02	0.21	0.00	0.00	0.04	0.04	0.00	0.01	0.01	—	33.5	33.5	< 0.005	< 0.005	0.06	34.1
Vendor	< 0.005	< 0.005	0.05	0.02	< 0.005	< 0.005	0.01	0.01	< 0.005	< 0.005	< 0.005	—	28.7	28.7	< 0.005	< 0.005	0.03	30.0
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.11. Phase II Building Construction (2026) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.10	0.10	2.22	5.05	0.01	0.01	—	0.01	0.01	—	0.01	—	980	980	0.04	0.01	—	984
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.10	0.10	2.22	5.05	0.01	0.01	—	0.01	0.01	—	0.01	—	980	980	0.04	0.01	—	984
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.04	0.04	0.93	2.12	< 0.005	0.01	—	0.01	0.01	—	0.01	—	411	411	0.02	< 0.005	—	412

Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01	0.01	0.17	0.39	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	68.0	68.0	< 0.005	< 0.005	—	68.2
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.23	0.21	0.15	1.76	0.00	0.00	0.32	0.32	0.00	0.07	0.07	—	315	315	0.02	0.01	1.32	321
Vendor	0.02	0.01	0.41	0.19	< 0.005	< 0.005	0.07	0.07	< 0.005	0.02	0.02	—	265	265	0.01	0.04	0.64	277
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.23	0.21	0.17	1.81	0.00	0.00	0.32	0.32	0.00	0.07	0.07	—	309	309	0.01	0.01	0.03	313
Vendor	0.02	0.01	0.42	0.20	< 0.005	< 0.005	0.07	0.07	< 0.005	0.02	0.02	—	265	265	0.01	0.04	0.02	276
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.10	0.09	0.07	0.73	0.00	0.00	0.13	0.13	0.00	0.03	0.03	—	129	129	0.01	0.01	0.24	132
Vendor	0.01	0.01	0.18	0.08	< 0.005	< 0.005	0.03	0.03	< 0.005	0.01	0.01	—	111	111	< 0.005	0.02	0.12	116
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.02	0.02	0.01	0.13	0.00	0.00	0.02	0.02	0.00	0.01	0.01	—	21.4	21.4	< 0.005	< 0.005	0.04	21.8
Vendor	< 0.005	< 0.005	0.03	0.01	< 0.005	< 0.005	0.01	0.01	< 0.005	< 0.005	< 0.005	—	18.4	18.4	< 0.005	< 0.005	0.02	19.2
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.13. Phase II Building Construction (2027) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.10	0.10	2.22	5.05	0.01	0.01	—	0.01	0.01	—	0.01	—	981	981	0.04	0.01	—	984
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.10	0.10	2.22	5.05	0.01	0.01	—	0.01	0.01	—	0.01	—	981	981	0.04	0.01	—	984
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.06	0.06	1.46	3.31	0.01	0.01	—	0.01	0.01	—	0.01	—	643	643	0.03	0.01	—	645
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01	0.01	0.27	0.60	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	106	106	< 0.005	< 0.005	—	107
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.22	0.20	0.14	1.64	0.00	0.00	0.32	0.32	0.00	0.07	0.07	—	309	309	0.01	0.01	1.21	315
Vendor	0.02	0.01	0.39	0.18	< 0.005	< 0.005	0.07	0.07	< 0.005	0.02	0.02	—	259	259	0.01	0.04	0.58	271
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.22	0.20	0.15	1.69	0.00	0.00	0.32	0.32	0.00	0.07	0.07	—	303	303	0.01	0.01	0.03	307
Vendor	0.02	0.01	0.40	0.18	< 0.005	< 0.005	0.07	0.07	< 0.005	0.02	0.02	—	259	259	0.01	0.04	0.01	271
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.14	0.13	0.10	1.07	0.00	0.00	0.21	0.21	0.00	0.05	0.05	—	199	199	0.01	0.01	0.34	202
Vendor	0.01	0.01	0.26	0.12	< 0.005	< 0.005	0.04	0.05	< 0.005	0.01	0.01	—	170	170	0.01	0.02	0.16	178
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.03	0.02	0.02	0.20	0.00	0.00	0.04	0.04	0.00	0.01	0.01	—	32.9	32.9	< 0.005	< 0.005	0.06	33.5
Vendor	< 0.005	< 0.005	0.05	0.02	< 0.005	< 0.005	0.01	0.01	< 0.005	< 0.005	< 0.005	—	28.1	28.1	< 0.005	< 0.005	0.03	29.4
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.15. Phase III Building Construction (2027) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—



Off-Road Equipment	0.10	0.10	2.22	5.05	0.01	0.01	—	0.01	0.01	—	0.01	—	981	981	0.04	0.01	—	984
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.10	0.10	2.22	5.05	0.01	0.01	—	0.01	0.01	—	0.01	—	981	981	0.04	0.01	—	984
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.04	0.04	0.93	2.12	< 0.005	0.01	—	0.01	0.01	—	0.01	—	411	411	0.02	< 0.005	—	412
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01	0.01	0.17	0.39	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	68.0	68.0	< 0.005	< 0.005	—	68.2
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.22	0.20	0.14	1.64	0.00	0.00	0.32	0.32	0.00	0.07	0.07	—	309	309	0.01	0.01	1.21	315
Vendor	0.02	0.01	0.39	0.18	< 0.005	< 0.005	0.07	0.07	< 0.005	0.02	0.02	—	259	259	0.01	0.04	0.58	271
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.22	0.20	0.15	1.69	0.00	0.00	0.32	0.32	0.00	0.07	0.07	—	303	303	0.01	0.01	0.03	307

Vendor	0.02	0.01	0.40	0.18	< 0.005	< 0.005	0.07	0.07	< 0.005	0.02	0.02	—	259	259	0.01	0.04	0.01	271
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.09	0.08	0.06	0.68	0.00	0.00	0.13	0.13	0.00	0.03	0.03	—	127	127	< 0.005	0.01	0.22	129
Vendor	0.01	< 0.005	0.17	0.08	< 0.005	< 0.005	0.03	0.03	< 0.005	0.01	0.01	—	109	109	< 0.005	0.02	0.10	113
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.02	0.02	0.01	0.12	0.00	0.00	0.02	0.02	0.00	0.01	0.01	—	21.0	21.0	< 0.005	< 0.005	0.04	21.4
Vendor	< 0.005	< 0.005	0.03	0.01	< 0.005	< 0.005	0.01	0.01	< 0.005	< 0.005	< 0.005	—	18.0	18.0	< 0.005	< 0.005	0.02	18.8
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.17. Phase III Building Construction (2028) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.10	0.10	2.22	5.05	0.01	0.01	—	0.01	0.01	—	0.01	—	981	981	0.04	0.01	—	984
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.10	0.10	2.22	5.05	0.01	0.01	—	0.01	0.01	—	0.01	—	981	981	0.04	0.01	—	984
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.06	0.06	1.46	3.32	0.01	0.01	—	0.01	0.01	—	0.01	—	645	645	0.03	0.01	—	647
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01	0.01	0.27	0.61	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	107	107	< 0.005	< 0.005	—	107
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.21	0.20	0.13	1.54	0.00	0.00	0.32	0.32	0.00	0.07	0.07	—	304	304	0.01	0.01	1.11	309
Vendor	0.02	0.01	0.37	0.17	< 0.005	< 0.005	0.07	0.07	< 0.005	0.02	0.02	—	253	253	0.01	0.04	0.51	264
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.21	0.20	0.14	1.59	0.00	0.00	0.32	0.32	0.00	0.07	0.07	—	297	297	0.01	0.01	0.03	302
Vendor	0.02	0.01	0.38	0.18	< 0.005	< 0.005	0.07	0.07	< 0.005	0.02	0.02	—	253	253	0.01	0.04	0.01	264
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.14	0.13	0.09	1.01	0.00	0.00	0.21	0.21	0.00	0.05	0.05	—	196	196	0.01	0.01	0.32	199
Vendor	0.01	0.01	0.25	0.11	< 0.005	< 0.005	0.04	0.05	< 0.005	0.01	0.01	—	166	166	0.01	0.02	0.15	174
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.03	0.02	0.02	0.18	0.00	0.00	0.04	0.04	0.00	0.01	0.01	—	32.4	32.4	< 0.005	< 0.005	0.05	33.0

Vendor	< 0.005	< 0.005	0.05	0.02	< 0.005	< 0.005	0.01	0.01	< 0.005	< 0.005	< 0.005	—	27.5	27.5	< 0.005	< 0.005	0.02	28.7
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.19. Paving (2025) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.31	0.31	2.19	17.5	0.03	0.06	—	0.06	0.06	—	0.06	—	3,428	3,428	0.14	0.03	—	3,440
Paving	—	0.04	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.06	0.06	0.39	3.15	0.01	0.01	—	0.01	0.01	—	0.01	—	617	617	0.03	0.01	—	619
Paving	—	0.01	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01	0.01	0.07	0.58	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	102	102	< 0.005	< 0.005	—	103
Paving	—	< 0.005	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.11	0.10	0.08	0.86	0.00	0.00	0.14	0.14	0.00	0.03	0.03	—	139	139	0.01	0.01	0.02	141
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.02	0.02	0.01	0.15	0.00	0.00	0.03	0.03	0.00	0.01	0.01	—	25.0	25.0	< 0.005	< 0.005	0.05	25.4
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	< 0.005	< 0.005	< 0.005	0.03	0.00	0.00	< 0.005	< 0.005	0.00	< 0.005	< 0.005	—	4.14	4.14	< 0.005	< 0.005	0.01	4.21
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.21. Paving (2026) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Off-Road Equipment	0.31	0.31	2.19	17.5	0.03	0.06	—	0.06	0.06	—	0.06	—	3,430	3,430	0.14	0.03	—	3,442
Paving	—	0.04	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	< 0.005	< 0.005	< 0.005	0.03	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	6.71	6.71	< 0.005	< 0.005	—	6.74
Paving	—	< 0.005	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	< 0.005	< 0.005	< 0.005	0.01	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	1.11	1.11	< 0.005	< 0.005	—	1.12
Paving	—	< 0.005	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.10	0.09	0.07	0.80	0.00	0.00	0.14	0.14	0.00	0.03	0.03	—	136	136	0.01	0.01	0.02	138
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	< 0.005	< 0.005	< 0.005	< 0.005	0.00	0.00	< 0.005	< 0.005	0.00	< 0.005	< 0.005	—	0.27	0.27	< 0.005	< 0.005	< 0.005	0.27
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	< 0.005	< 0.005	< 0.005	< 0.005	0.00	0.00	< 0.005	< 0.005	0.00	< 0.005	< 0.005	—	0.04	0.04	< 0.005	< 0.005	< 0.005	0.04
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.23. Phase I Architectural Coating (2025) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.03	0.03	0.15	2.14	< 0.005	0.01	—	0.01	0.01	—	0.01	—	418	418	0.02	< 0.005	—	419
Architect ural Coatings	—	3.60	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01	0.01	0.03	0.39	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	75.2	75.2	< 0.005	< 0.005	—	75.4
Architect ural Coatings	—	0.65	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	< 0.005	< 0.005	< 0.005	0.07	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	12.4	12.4	< 0.005	< 0.005	—	12.5
Architectural Coatings	—	0.12	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.15	0.13	0.11	1.17	0.00	0.00	0.19	0.19	0.00	0.04	0.04	—	189	189	0.01	0.01	0.02	192
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.03	0.02	0.02	0.21	0.00	0.00	0.03	0.03	0.00	0.01	0.01	—	34.1	34.1	< 0.005	< 0.005	0.07	34.7
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	< 0.005	< 0.005	< 0.005	0.04	0.00	0.00	0.01	0.01	0.00	< 0.005	< 0.005	—	5.64	5.64	< 0.005	< 0.005	0.01	5.74
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.25. Phase I Architectural Coating (2026) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)



Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.03	0.03	0.15	2.14	< 0.005	0.01	—	0.01	0.01	—	0.01	—	418	418	0.02	< 0.005	—	419
Architectural Coatings	—	3.60	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.03	0.03	0.15	2.14	< 0.005	0.01	—	0.01	0.01	—	0.01	—	418	418	0.02	< 0.005	—	419
Architectural Coatings	—	3.60	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.02	0.02	0.08	1.15	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	224	224	0.01	< 0.005	—	225
Architectural Coatings	—	1.93	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	< 0.005	< 0.005	0.01	0.21	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	37.1	37.1	< 0.005	< 0.005	—	37.2

Architect Coatings	—	0.35	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.14	0.13	0.09	1.05	0.00	0.00	0.19	0.19	0.00	0.04	0.04	—	189	189	0.01	0.01	0.79	193
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.14	0.13	0.10	1.08	0.00	0.00	0.19	0.19	0.00	0.04	0.04	—	185	185	0.01	0.01	0.02	188
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.07	0.07	0.05	0.56	0.00	0.00	0.10	0.10	0.00	0.02	0.02	—	99.4	99.4	0.01	< 0.005	0.18	101
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.01	0.01	0.01	0.10	0.00	0.00	0.02	0.02	0.00	< 0.005	< 0.005	—	16.4	16.4	< 0.005	< 0.005	0.03	16.7
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.27. Phase II Architectural Coating (2026) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
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Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.03	0.03	0.15	2.14	< 0.005	0.01	—	0.01	0.01	—	0.01	—	418	418	0.02	< 0.005	—	419
Architect ural Coatings	—	3.62	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01	0.01	0.03	0.38	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	74.4	74.4	< 0.005	< 0.005	—	74.6
Architect ural Coatings	—	0.64	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	< 0.005	< 0.005	< 0.005	0.07	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	12.3	12.3	< 0.005	< 0.005	—	12.4
Architect ural Coatings	—	0.12	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.10	0.10	0.07	0.81	0.00	0.00	0.14	0.14	0.00	0.03	0.03	—	139	139	0.01	0.01	0.02	141
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.02	0.02	0.01	0.14	0.00	0.00	0.03	0.03	0.00	0.01	0.01	—	24.7	24.7	< 0.005	< 0.005	0.05	25.2
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	< 0.005	< 0.005	< 0.005	0.03	0.00	0.00	< 0.005	< 0.005	0.00	< 0.005	< 0.005	—	4.10	4.10	< 0.005	< 0.005	0.01	4.17
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.29. Phase II Architectural Coating (2027) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.03	0.03	0.15	2.14	< 0.005	0.01	—	0.01	0.01	—	0.01	—	418	418	0.02	< 0.005	—	419
Architect ural Coatings	—	3.62	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.03	0.03	0.15	2.14	< 0.005	0.01	—	0.01	0.01	—	0.01	—	418	418	0.02	< 0.005	—	419
Architect ural Coatings	—	3.62	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.02	0.02	0.08	1.15	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	225	225	0.01	< 0.005	—	225
Architect ural Coatings	—	1.95	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	< 0.005	< 0.005	0.01	0.21	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	37.2	37.2	< 0.005	< 0.005	—	37.3
Architect ural Coatings	—	0.36	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.10	0.09	0.06	0.74	0.00	0.00	0.14	0.14	0.00	0.03	0.03	—	139	139	< 0.005	0.01	0.55	142
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.10	0.09	0.07	0.76	0.00	0.00	0.14	0.14	0.00	0.03	0.03	—	136	136	0.01	0.01	0.01	138
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.05	0.05	0.04	0.40	0.00	0.00	0.08	0.08	0.00	0.02	0.02	—	73.4	73.4	< 0.005	< 0.005	0.13	74.6
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.01	0.01	0.01	0.07	0.00	0.00	0.01	0.01	0.00	< 0.005	< 0.005	—	12.2	12.2	< 0.005	< 0.005	0.02	12.4
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.31. Phase III Architectural Coating (2027) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.03	0.03	0.15	2.14	< 0.005	0.01	—	0.01	0.01	—	0.01	—	418	418	0.02	< 0.005	—	419
Architect ural Coatings	—	3.61	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.01	0.01	0.03	0.38	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	73.5	73.5	< 0.005	< 0.005	—	73.8	
Architectural Coatings	—	0.64	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	< 0.005	< 0.005	< 0.005	0.07	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	12.2	12.2	< 0.005	< 0.005	—	12.2	
Architectural Coatings	—	0.12	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.10	0.09	0.07	0.76	0.00	0.00	0.14	0.14	0.00	0.03	0.03	—	136	136	0.01	0.01	0.01	138	
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.02	0.02	0.01	0.13	0.00	0.00	0.03	0.03	0.00	0.01	0.01	—	24.0	24.0	< 0.005	< 0.005	0.04	24.4	
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	< 0.005	< 0.005	< 0.005	0.02	0.00	0.00	< 0.005	< 0.005	0.00	< 0.005	< 0.005	—	3.98	3.98	< 0.005	< 0.005	0.01	4.04
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

### 3.33. Phase III Architectural Coating (2028) - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Location	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Onsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.03	0.03	0.15	2.14	< 0.005	0.01	—	0.01	0.01	—	0.01	—	418	418	0.02	< 0.005	—	419
Architect ural Coatings	—	3.61	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	0.03	0.03	0.15	2.14	< 0.005	0.01	—	0.01	0.01	—	0.01	—	418	418	0.02	< 0.005	—	419
Architect ural Coatings	—	3.61	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—



Off-Road Equipment	0.02	0.02	0.08	1.16	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	226	226	0.01	< 0.005	—	227
Architectural Coatings	—	1.96	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Off-Road Equipment	< 0.005	< 0.005	0.01	0.21	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	37.5	37.5	< 0.005	< 0.005	—	37.6
Architectural Coatings	—	0.36	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Onsite truck	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Offsite	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.10	0.09	0.06	0.69	0.00	0.00	0.14	0.14	0.00	0.03	0.03	—	137	137	< 0.005	0.01	0.50	139
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.10	0.09	0.06	0.71	0.00	0.00	0.14	0.14	0.00	0.03	0.03	—	134	134	0.01	0.01	0.01	136
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Average Daily	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.05	0.05	0.03	0.37	0.00	0.00	0.08	0.08	0.00	0.02	0.02	—	72.6	72.6	< 0.005	< 0.005	0.12	73.8
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Worker	0.01	0.01	0.01	0.07	0.00	0.00	0.01	0.01	0.00	< 0.005	< 0.005	—	12.0	12.0	< 0.005	< 0.005	0.02	12.2
Vendor	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
Hauling	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

## 4. Operations Emissions Details

### 4.1. Mobile Emissions by Land Use

#### 4.1.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	2.10	2.00	1.01	8.68	0.02	0.01	1.59	1.60	0.01	0.40	0.41	—	1,736	1,736	0.13	0.10	5.14	1,774
Parking Lot	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
City Park	0.01	0.01	0.01	0.06	< 0.005	< 0.005	0.01	0.01	< 0.005	< 0.005	< 0.005	—	13.1	13.1	< 0.005	< 0.005	0.04	13.3
Total	2.11	2.01	1.02	8.73	0.02	0.01	1.60	1.61	0.01	0.41	0.42	—	1,749	1,749	0.13	0.10	5.18	1,788
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	2.12	2.01	1.11	9.52	0.02	0.01	1.59	1.60	0.01	0.40	0.41	—	1,712	1,712	0.14	0.11	0.13	1,747
Parking Lot	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00

City Park	0.01	0.01	0.01	0.06	< 0.005	< 0.005	0.01	0.01	< 0.005	< 0.005	< 0.005	—	12.9	12.9	< 0.005	< 0.005	< 0.005	13.1
Total	2.13	2.02	1.12	9.58	0.02	0.01	1.60	1.61	0.01	0.41	0.42	—	1,725	1,725	0.14	0.11	0.13	1,760
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	0.38	0.36	0.20	1.66	< 0.005	< 0.005	0.29	0.29	< 0.005	0.07	0.08	—	284	284	0.02	0.02	0.37	290
Parking Lot	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00
City Park	< 0.005	< 0.005	< 0.005	0.01	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	—	1.12	1.12	< 0.005	< 0.005	< 0.005	1.14
Total	0.38	0.36	0.20	1.67	< 0.005	< 0.005	0.29	0.29	< 0.005	0.07	0.08	—	285	285	0.02	0.02	0.37	291

## 4.2. Energy

### 4.2.1. Electricity Emissions By Land Use - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	—	—	—	—	—	—	—	—	—	—	—	—	481	481	0.08	0.01	—	486
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	—	24.2	24.2	< 0.005	< 0.005	—	24.4
City Park	—	—	—	—	—	—	—	—	—	—	—	—	0.00	0.00	0.00	0.00	—	0.00
Total	—	—	—	—	—	—	—	—	—	—	—	—	505	505	0.08	0.01	—	510
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Single Family Housing	—	—	—	—	—	—	—	—	—	—	—	—	481	481	0.08	0.01	—	486
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	—	24.2	24.2	< 0.005	< 0.005	—	24.4
City Park	—	—	—	—	—	—	—	—	—	—	—	—	0.00	0.00	0.00	0.00	—	0.00
Total	—	—	—	—	—	—	—	—	—	—	—	—	505	505	0.08	0.01	—	510
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	—	—	—	—	—	—	—	—	—	—	—	—	79.7	79.7	0.01	< 0.005	—	80.5
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	—	4.00	4.00	< 0.005	< 0.005	—	4.04
City Park	—	—	—	—	—	—	—	—	—	—	—	—	0.00	0.00	0.00	0.00	—	0.00
Total	—	—	—	—	—	—	—	—	—	—	—	—	83.7	83.7	0.01	< 0.005	—	84.5

#### 4.2.3. Natural Gas Emissions By Land Use - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	0.17	0.08	1.43	0.61	0.01	0.12	—	0.12	0.12	—	0.12	—	1,816	1,816	0.16	< 0.005	—	1,821
Parking Lot	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	—	0.00	—	0.00	0.00	0.00	0.00	—	0.00
City Park	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	—	0.00	—	0.00	0.00	0.00	0.00	—	0.00
Total	0.17	0.08	1.43	0.61	0.01	0.12	—	0.12	0.12	—	0.12	—	1,816	1,816	0.16	< 0.005	—	1,821

Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	0.17	0.08	1.43	0.61	0.01	0.12	—	0.12	0.12	—	0.12	—	1,816	1,816	0.16	< 0.005	—	1,821
Parking Lot	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	—	0.00	—	0.00	0.00	0.00	0.00	—	0.00
City Park	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	—	0.00	—	0.00	0.00	0.00	0.00	—	0.00
Total	0.17	0.08	1.43	0.61	0.01	0.12	—	0.12	0.12	—	0.12	—	1,816	1,816	0.16	< 0.005	—	1,821
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	0.03	0.02	0.26	0.11	< 0.005	0.02	—	0.02	0.02	—	0.02	—	301	301	0.03	< 0.005	—	301
Parking Lot	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	—	0.00	—	0.00	0.00	0.00	0.00	—	0.00
City Park	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	—	0.00	—	0.00	0.00	0.00	0.00	—	0.00
Total	0.03	0.02	0.26	0.11	< 0.005	0.02	—	0.02	0.02	—	0.02	—	301	301	0.03	< 0.005	—	301

### 4.3. Area Emissions by Source

#### 4.3.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Source	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Hearths	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00
Consumer Products	—	7.71	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Architect ural	—	0.78	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Landscap e Equipme nt	0.74	0.70	0.08	8.08	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	21.5	21.5	< 0.005	< 0.005	—	21.6
Total	0.74	9.19	0.08	8.08	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	0.00	21.5	21.5	< 0.005	< 0.005	—	21.6
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Hearths	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00
Consum er Products	—	7.71	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Architect ural Coatings	—	0.78	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	0.00	8.49	0.00	0.00	0.00	0.00	—	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Hearths	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00	0.00	—	0.00	0.00	0.00	0.00	0.00	0.00	—	0.00
Consum er Products	—	1.41	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Architect ural Coatings	—	0.14	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Landscap e Equipme nt	0.07	0.06	0.01	0.73	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	—	1.76	1.76	< 0.005	< 0.005	—	1.76
Total	0.07	1.61	0.01	0.73	< 0.005	< 0.005	—	< 0.005	< 0.005	—	< 0.005	0.00	1.76	1.76	< 0.005	< 0.005	—	1.76

4.4. Water Emissions by Land Use

## 4.4.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	—	—	—	—	—	—	—	—	—	—	—	10.7	15.1	25.7	0.04	0.02	—	33.8
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00	0.00	0.00	0.00	0.00	—	0.00
City Park	—	—	—	—	—	—	—	—	—	—	—	0.00	5.25	5.25	< 0.005	< 0.005	—	5.30
Total	—	—	—	—	—	—	—	—	—	—	—	10.7	20.3	31.0	0.04	0.02	—	39.0
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	—	—	—	—	—	—	—	—	—	—	—	10.7	15.1	25.7	0.04	0.02	—	33.8
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00	0.00	0.00	0.00	0.00	—	0.00
City Park	—	—	—	—	—	—	—	—	—	—	—	0.00	5.25	5.25	< 0.005	< 0.005	—	5.30
Total	—	—	—	—	—	—	—	—	—	—	—	10.7	20.3	31.0	0.04	0.02	—	39.0
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	—	—	—	—	—	—	—	—	—	—	—	1.77	2.50	4.26	0.01	< 0.005	—	5.59
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00	0.00	0.00	0.00	0.00	—	0.00
City Park	—	—	—	—	—	—	—	—	—	—	—	0.00	0.87	0.87	< 0.005	< 0.005	—	0.88
Total	—	—	—	—	—	—	—	—	—	—	—	1.77	3.37	5.13	0.01	< 0.005	—	6.47

## 4.5. Waste Emissions by Land Use

### 4.5.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	—	—	—	—	—	—	—	—	—	—	—	33.5	0.00	33.5	3.35	0.00	—	117
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00	0.00	0.00	0.00	0.00	—	0.00
City Park	—	—	—	—	—	—	—	—	—	—	—	0.07	0.00	0.07	0.01	0.00	—	0.25
Total	—	—	—	—	—	—	—	—	—	—	—	33.6	0.00	33.6	3.35	0.00	—	117
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	—	—	—	—	—	—	—	—	—	—	—	33.5	0.00	33.5	3.35	0.00	—	117
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00	0.00	0.00	0.00	0.00	—	0.00
City Park	—	—	—	—	—	—	—	—	—	—	—	0.07	0.00	0.07	0.01	0.00	—	0.25
Total	—	—	—	—	—	—	—	—	—	—	—	33.6	0.00	33.6	3.35	0.00	—	117
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	—	—	—	—	—	—	—	—	—	—	—	5.54	0.00	5.54	0.55	0.00	—	19.4
Parking Lot	—	—	—	—	—	—	—	—	—	—	—	0.00	0.00	0.00	0.00	0.00	—	0.00



City Park	—	—	—	—	—	—	—	—	—	—	—	0.01	0.00	0.01	< 0.005	0.00	—	0.04
Total	—	—	—	—	—	—	—	—	—	—	—	5.56	0.00	5.56	0.56	0.00	—	19.4

## 4.6. Refrigerant Emissions by Land Use

### 4.6.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	2.52	2.52
City Park	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.00	0.00
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	2.52	2.52
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	2.52	2.52
City Park	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.00	0.00
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	2.52	2.52
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Single Family Housing	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.42	0.42
City Park	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.00	0.00
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	0.42	0.42

## 4.7. Offroad Emissions By Equipment Type

### 4.7.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Equipment Type	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

## 4.8. Stationary Emissions By Equipment Type

### 4.8.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Equipment Type	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

## 4.9. User Defined Emissions By Equipment Type

### 4.9.1. Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Equipment Type	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

## 4.10. Soil Carbon Accumulation By Vegetation Type

### 4.10.1. Soil Carbon Accumulation By Vegetation Type - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Vegetation	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

#### 4.10.2. Above and Belowground Carbon Accumulation by Land Use Type - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Land Use	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Total	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

#### 4.10.3. Avoided and Sequestered Emissions by Species - Unmitigated

Criteria Pollutants (lb/day for daily, ton/yr for annual) and GHGs (lb/day for daily, MT/yr for annual)

Species	TOG	ROG	NOx	CO	SO2	PM10E	PM10D	PM10T	PM2.5E	PM2.5D	PM2.5T	BCO2	NBCO2	CO2T	CH4	N2O	R	CO2e
Daily, Summer (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Avoided	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Sequestered	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Removed	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Daily, Winter (Max)	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Avoided	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Sequestered	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Removed	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Annual	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Avoided	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Sequestered	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Removed	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Subtotal	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

## 5. Activity Data

### 5.1. Construction Schedule

Phase Name	Phase Type	Start Date	End Date	Days Per Week	Work Days per Phase	Phase Description
Demolition	Demolition	1/2/2025	2/1/2025	5.00	22.0	—
Site Preparation	Site Preparation	2/2/2025	3/1/2025	5.00	20.0	—
Grading	Grading	3/2/2025	6/1/2025	5.00	65.0	—
Phase I Building Construction	Building Construction	6/2/2025	12/1/2026	5.00	392	—
Phase II Building Construction	Building Construction	6/1/2026	12/1/2027	5.00	393	—
Phase III Building Construction	Building Construction	6/1/2027	12/1/2028	5.00	394	—
Paving	Paving	10/1/2025	1/1/2026	5.00	67.0	—
Phase I Architectural Coating	Architectural Coating	10/1/2025	10/1/2026	5.00	262	—
Phase II Architectural Coating	Architectural Coating	10/2/2026	10/2/2027	5.00	261	—
Phase III Architectural Coating	Architectural Coating	10/3/2027	10/3/2028	5.00	262	—

### 5.2. Off-Road Equipment

#### 5.2.1. Unmitigated

Phase Name	Equipment Type	Fuel Type	Engine Tier	Number per Day	Hours Per Day	Horsepower	Load Factor
Demolition	Concrete/Industrial Saws	Diesel	Average	1.00	8.00	33.0	0.73
Demolition	Excavators	Diesel	Average	3.00	8.00	36.0	0.38
Demolition	Rubber Tired Dozers	Diesel	Average	2.00	8.00	367	0.40

Site Preparation	Tractors/Loaders/Backh	Diesel	Average	2.00	8.00	84.0	0.37
Site Preparation	Concrete/Industrial Saws	Diesel	Average	1.00	8.00	33.0	0.73
Site Preparation	Rubber Tired Dozers	Diesel	Average	1.00	8.00	367	0.40
Site Preparation	Excavators	Diesel	Average	1.00	8.00	36.0	0.38
Site Preparation	Generator Sets	Diesel	Average	1.00	8.00	14.0	0.74
Site Preparation	Rubber Tired Loaders	Diesel	Average	1.00	8.00	150	0.36
Grading	Tractors/Loaders/Backh oes	Diesel	Tier 4 Final	2.00	8.00	84.0	0.37
Grading	Rubber Tired Dozers	Diesel	Tier 4 Final	3.00	8.00	367	0.40
Grading	Excavators	Diesel	Tier 4 Final	1.00	8.00	36.0	0.38
Grading	Generator Sets	Diesel	Tier 4 Final	1.00	8.00	14.0	0.74
Grading	Graders	Diesel	Tier 4 Final	1.00	8.00	148	0.41
Grading	Rubber Tired Loaders	Diesel	Tier 4 Final	1.00	8.00	150	0.36
Grading	Off-Highway Trucks	Diesel	Tier 4 Final	2.00	8.00	376	0.38
Grading	Pumps	Diesel	Tier 4 Final	1.00	8.00	11.0	0.74
Grading	Rough Terrain Forklifts	Diesel	Tier 4 Final	1.00	8.00	96.0	0.40
Grading	Scrapers	Diesel	Tier 4 Final	2.00	8.00	423	0.48
Grading	Tractors/Loaders/Backh oes	Diesel	Tier 4 Final	1.00	8.00	84.0	0.37
Grading	Plate Compactors	Diesel	Tier 4 Final	2.00	8.00	8.00	0.43
Phase I Building Construction	Cement and Mortar Mixers	Diesel	Tier 4 Final	2.00	8.00	10.0	0.56
Phase I Building Construction	Forklifts	Diesel	Tier 4 Final	2.00	8.00	82.0	0.20
Phase I Building Construction	Generator Sets	Diesel	Tier 4 Final	1.00	8.00	14.0	0.74
Phase I Building Construction	Pressure Washers	Diesel	Tier 4 Final	1.00	8.00	14.0	0.30

Phase I Building Construction	Skid Steer Loaders	Diesel	Tier 4 Final	1.00	8.00	71.0	0.37
Phase I Building Construction	Sweepers/Scrubbers	Diesel	Tier 4 Final	1.00	8.00	36.0	0.46
Phase II Building Construction	Cement and Mortar Mixers	Diesel	Tier 4 Final	2.00	8.00	10.0	0.56
Phase II Building Construction	Forklifts	Diesel	Tier 4 Final	2.00	8.00	82.0	0.20
Phase II Building Construction	Generator Sets	Diesel	Tier 4 Final	1.00	8.00	14.0	0.74
Phase II Building Construction	Pressure Washers	Diesel	Tier 4 Final	1.00	8.00	14.0	0.30
Phase II Building Construction	Skid Steer Loaders	Diesel	Tier 4 Final	1.00	8.00	71.0	0.37
Phase II Building Construction	Sweepers/Scrubbers	Diesel	Tier 4 Final	1.00	8.00	36.0	0.46
Phase III Building Construction	Cement and Mortar Mixers	Diesel	Tier 4 Final	2.00	8.00	10.0	0.56
Phase III Building Construction	Forklifts	Diesel	Tier 4 Final	2.00	8.00	82.0	0.20
Phase III Building Construction	Generator Sets	Diesel	Tier 4 Final	1.00	8.00	14.0	0.74
Phase III Building Construction	Pressure Washers	Diesel	Tier 4 Final	1.00	8.00	14.0	0.30
Phase III Building Construction	Skid Steer Loaders	Diesel	Tier 4 Final	1.00	8.00	71.0	0.37
Phase III Building Construction	Sweepers/Scrubbers	Diesel	Tier 4 Final	1.00	8.00	36.0	0.46
Paving	Cement and Mortar Mixers	Diesel	Tier 4 Final	2.00	8.00	10.0	0.56
Paving	Plate Compactors	Diesel	Tier 4 Final	2.00	8.00	8.00	0.43
Paving	Rubber Tired Dozers	Diesel	Tier 4 Final	1.00	8.00	367	0.40
Paving	Pavers	Diesel	Tier 4 Final	1.00	8.00	81.0	0.42



Paving	Paving Equipment	Diesel	Tier 4 Final	1.00	8.00	89.0	0.36
Paving	Rollers	Diesel	Tier 4 Final	1.00	8.00	36.0	0.38
Paving	Surfacing Equipment	Diesel	Tier 4 Final	1.00	8.00	399	0.30
Phase I Architectural Coating	Cement and Mortar Mixers	Diesel	Tier 4 Final	2.00	8.00	10.0	0.56
Phase I Architectural Coating	Forklifts	Diesel	Tier 4 Final	2.00	8.00	82.0	0.20
Phase II Architectural Coating	Cement and Mortar Mixers	Diesel	Tier 4 Final	2.00	8.00	10.0	0.56
Phase II Architectural Coating	Forklifts	Diesel	Tier 4 Final	2.00	8.00	82.0	0.20
Phase III Architectural Coating	Cement and Mortar Mixers	Diesel	Tier 4 Final	2.00	8.00	10.0	0.56
Phase III Architectural Coating	Forklifts	Diesel	Tier 4 Final	2.00	8.00	82.0	0.20

## 5.3. Construction Vehicles

### 5.3.1. Unmitigated

Phase Name	Trip Type	One-Way Trips per Day	Miles per Trip	Vehicle Mix
Demolition	—	—	—	—
Demolition	Worker	15.0	8.80	LDA,LDT1,LDT2
Demolition	Vendor	—	5.30	HHDT,MHDT
Demolition	Hauling	1.32	20.0	HHDT
Demolition	Onsite truck	—	—	HHDT
Site Preparation	—	—	—	—
Site Preparation	Worker	17.5	8.80	LDA,LDT1,LDT2
Site Preparation	Vendor	—	5.30	HHDT,MHDT
Site Preparation	Hauling	0.00	20.0	HHDT
Site Preparation	Onsite truck	—	—	HHDT

Grading	—	—	—	—
Grading	Worker	45.0	8.80	LDA,LDT1,LDT2
Grading	Vendor	—	5.30	HHDT,MHDT
Grading	Hauling	60.7	20.0	HHDT
Grading	Onsite truck	—	—	HHDT
Phase I Building Construction	—	—	—	—
Phase I Building Construction	Worker	51.1	8.80	LDA,LDT1,LDT2
Phase I Building Construction	Vendor	15.2	5.30	HHDT,MHDT
Phase I Building Construction	Hauling	0.00	20.0	HHDT
Phase I Building Construction	Onsite truck	—	—	HHDT
Paving	—	—	—	—
Paving	Worker	22.5	8.80	LDA,LDT1,LDT2
Paving	Vendor	—	5.30	HHDT,MHDT
Paving	Hauling	0.00	20.0	HHDT
Paving	Onsite truck	—	—	HHDT
Phase I Architectural Coating	—	—	—	—
Phase I Architectural Coating	Worker	30.7	8.80	LDA,LDT1,LDT2
Phase I Architectural Coating	Vendor	—	5.30	HHDT,MHDT
Phase I Architectural Coating	Hauling	0.00	20.0	HHDT
Phase I Architectural Coating	Onsite truck	—	—	HHDT
Phase II Building Construction	—	—	—	—
Phase II Building Construction	Worker	51.1	8.80	LDA,LDT1,LDT2
Phase II Building Construction	Vendor	15.2	5.30	HHDT,MHDT
Phase II Building Construction	Hauling	0.00	20.0	HHDT
Phase II Building Construction	Onsite truck	—	—	HHDT
Phase III Building Construction	—	—	—	—
Phase III Building Construction	Worker	51.1	8.80	LDA,LDT1,LDT2

Phase III Building Construction	Vendor	15.2	5.30	HHDT,MHDT
Phase III Building Construction	Hauling	0.00	20.0	HHDT
Phase III Building Construction	Onsite truck	—	—	HHDT
Phase II Architectural Coating	—	—	—	—
Phase II Architectural Coating	Worker	23.0	8.80	LDA,LDT1,LDT2
Phase II Architectural Coating	Vendor	—	5.30	HHDT,MHDT
Phase II Architectural Coating	Hauling	0.00	20.0	HHDT
Phase II Architectural Coating	Onsite truck	—	—	HHDT
Phase III Architectural Coating	—	—	—	—
Phase III Architectural Coating	Worker	23.0	8.80	LDA,LDT1,LDT2
Phase III Architectural Coating	Vendor	—	5.30	HHDT,MHDT
Phase III Architectural Coating	Hauling	0.00	20.0	HHDT
Phase III Architectural Coating	Onsite truck	—	—	HHDT

5.4. Vehicles

5.4.1. Construction Vehicle Control Strategies

Non-applicable. No control strategies activated by user.

5.5. Architectural Coatings

Phase Name	Residential Interior Area Coated (sq ft)	Residential Exterior Area Coated (sq ft)	Non-Residential Interior Area Coated (sq ft)	Non-Residential Exterior Area Coated (sq ft)	Parking Area Coated (sq ft)
Phase I Architectural Coating	237,370	79,123	1,430	477	987
Phase II Architectural Coating	237,370	79,123	1,430	477	987
Phase III Architectural Coating	238,020	79,340	1,434	478	990

5.6. Dust Mitigation

### 5.6.1. Construction Earthmoving Activities

Phase Name	Material Imported (Cubic Yards)	Material Exported (Cubic Yards)	Acres Graded (acres)	Material Demolished (Building Square Footage)	Acres Paved (acres)
Demolition	0.00	0.00	0.00	2,500	—
Site Preparation	0.00	0.00	10.0	0.00	—
Grading	31,550	0.00	260	0.00	—
Paving	0.00	0.00	0.00	0.00	2.70

### 5.6.2. Construction Earthmoving Control Strategies

Control Strategies Applied	Frequency (per day)	PM10 Reduction	PM2.5 Reduction
Water Exposed Area	2	61%	61%
Water Demolished Area	2	36%	36%

### 5.7. Construction Paving

Land Use	Area Paved (acres)	% Asphalt
Single Family Housing	1.56	0%
Parking Lot	1.13	100%
City Park	0.00	0%

### 5.8. Construction Electricity Consumption and Emissions Factors

#### kWh per Year and Emission Factor (lb/MWh)

Year	kWh per Year	CO2	CH4	N2O
2025	0.00	204	0.03	< 0.005
2026	0.00	204	0.03	< 0.005
2027	0.00	204	0.03	< 0.005
2028	0.00	204	0.03	< 0.005

## 5.9. Operational Mobile Sources

### 5.9.1. Unmitigated

Land Use Type	Trips/Weekday	Trips/Saturday	Trips/Sunday	Trips/Year	VMT/Weekday	VMT/Saturday	VMT/Sunday	VMT/Year
Single Family Housing	612	612	612	223,387	2,249	2,249	2,249	821,018
Parking Lot	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
City Park	1.22	3.08	3.44	659	6.12	15.4	17.2	3,295

## 5.10. Operational Area Sources

### 5.10.1. Hearths

#### 5.10.1.1. Unmitigated

Hearth Type	Unmitigated (number)
Single Family Housing	—
Wood Fireplaces	0
Gas Fireplaces	0
Propane Fireplaces	0
Electric Fireplaces	0
No Fireplaces	142
Conventional Wood Stoves	0
Catalytic Wood Stoves	0
Non-Catalytic Wood Stoves	0
Pellet Wood Stoves	0

### 5.10.2. Architectural Coatings

Residential Interior Area Coated (sq ft)	Residential Exterior Area Coated (sq ft)	Non-Residential Interior Area Coated (sq ft)	Non-Residential Exterior Area Coated (sq ft)	Parking Area Coated (sq ft)
712759.5	237,587	4,293	1,431	2,964

### 5.10.3. Landscape Equipment

Season	Unit	Value
Snow Days	day/yr	0.00
Summer Days	day/yr	180

## 5.11. Operational Energy Consumption

### 5.11.1. Unmitigated

#### Electricity (kWh/yr) and CO2 and CH4 and N2O and Natural Gas (kBtu/yr)

Land Use	Electricity (kWh/yr)	CO2	CH4	N2O	Natural Gas (kBtu/yr)
Single Family Housing	860,996	204	0.0330	0.0040	5,665,817
Parking Lot	43,272	204	0.0330	0.0040	0.00
City Park	0.00	204	0.0330	0.0040	0.00

## 5.12. Operational Water and Wastewater Consumption

### 5.12.1. Unmitigated

Land Use	Indoor Water (gal/year)	Outdoor Water (gal/year)
Single Family Housing	4,988,897	0.00
Parking Lot	0.00	0.00
City Park	0.00	2,426,184

## 5.13. Operational Waste Generation

## 5.13.1. Unmitigated

Land Use	Waste (ton/year)	Cogeneration (kWh/year)
Single Family Housing	62.1	—
Parking Lot	0.00	—
City Park	0.14	—

## 5.14. Operational Refrigeration and Air Conditioning Equipment

## 5.14.1. Unmitigated

Land Use Type	Equipment Type	Refrigerant	GWP	Quantity (kg)	Operations Leak Rate	Service Leak Rate	Times Serviced
Single Family Housing	Average room A/C & Other residential A/C and heat pumps	R-410A	2,088	< 0.005	2.50	2.50	10.0
Single Family Housing	Household refrigerators and/or freezers	R-134a	1,430	0.12	0.60	0.00	1.00
City Park	Other commercial A/C and heat pumps	R-410A	2,088	< 0.005	4.00	4.00	18.0
City Park	Stand-alone retail refrigerators and freezers	R-134a	1,430	0.04	1.00	0.00	1.00

## 5.15. Operational Off-Road Equipment

## 5.15.1. Unmitigated

Equipment Type	Fuel Type	Engine Tier	Number per Day	Hours Per Day	Horsepower	Load Factor
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## 5.16. Stationary Sources

## 5.16.1. Emergency Generators and Fire Pumps

Equipment Type	Fuel Type	Number per Day	Hours per Day	Hours per Year	Horsepower	Load Factor
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5.16.2. Process Boilers

Equipment Type	Fuel Type	Number	Boiler Rating (MMBtu/hr)	Daily Heat Input (MMBtu/day)	Annual Heat Input (MMBtu/yr)
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5.17. User Defined

Equipment Type	Fuel Type
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5.18. Vegetation

5.18.1. Land Use Change

5.18.1.1. Unmitigated

Vegetation Land Use Type	Vegetation Soil Type	Initial Acres	Final Acres
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5.18.1. Biomass Cover Type

5.18.1.1. Unmitigated

Biomass Cover Type	Initial Acres	Final Acres
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5.18.2. Sequestration

5.18.2.1. Unmitigated

Tree Type	Number	Electricity Saved (kWh/year)	Natural Gas Saved (btu/year)
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6. Climate Risk Detailed Report



## 6.1. Climate Risk Summary

Cal-Adapt midcentury 2040–2059 average projections for four hazards are reported below for your project location. These are under Representation Concentration Pathway (RCP) 8.5 which assumes GHG emissions will continue to rise strongly through 2050 and then plateau around 2100.

Climate Hazard	Result for Project Location	Unit
Temperature and Extreme Heat	5.13	annual days of extreme heat
Extreme Precipitation	4.70	annual days with precipitation above 20 mm
Sea Level Rise	—	meters of inundation depth
Wildfire	47.0	annual hectares burned

Temperature and Extreme Heat data are for grid cell in which your project are located. The projection is based on the 98th historical percentile of daily maximum/minimum temperatures from observed historical data (32 climate model ensemble from Cal-Adapt, 2040–2059 average under RCP 8.5). Each grid cell is 6 kilometers (km) by 6 km, or 3.7 miles (mi) by 3.7 mi.

Extreme Precipitation data are for the grid cell in which your project are located. The threshold of 20 mm is equivalent to about  $\frac{3}{4}$  an inch of rain, which would be light to moderate rainfall if received over a full day or heavy rain if received over a period of 2 to 4 hours. Each grid cell is 6 kilometers (km) by 6 km, or 3.7 miles (mi) by 3.7 mi.

Sea Level Rise data are for the grid cell in which your project are located. The projections are from Radke et al. (2017), as reported in Cal-Adapt (Radke et al., 2017, CEC-500-2017-008), and consider inundation location and depth for the San Francisco Bay, the Sacramento-San Joaquin River Delta and California coast resulting different increments of sea level rise coupled with extreme storm events. Users may select from four scenarios to view the range in potential inundation depth for the grid cell. The four scenarios are: No rise, 0.5 meter, 1.0 meter, 1.41 meters

Wildfire data are for the grid cell in which your project are located. The projections are from UC Davis, as reported in Cal-Adapt (2040–2059 average under RCP 8.5), and consider historical data of climate, vegetation, population density, and large (> 400 ha) fire history. Users may select from four model simulations to view the range in potential wildfire probabilities for the grid cell. The four simulations make different assumptions about expected rainfall and temperature are: Warmer/drier (HadGEM2-ES), Cooler/wetter (CNRM-CM5), Average conditions (CanESM2), Range of different rainfall and temperature possibilities (MIROC5). Each grid cell is 6 kilometers (km) by 6 km, or 3.7 miles (mi) by 3.7 mi.

## 6.2. Initial Climate Risk Scores

Climate Hazard	Exposure Score	Sensitivity Score	Adaptive Capacity Score	Vulnerability Score
Temperature and Extreme Heat	N/A	N/A	N/A	N/A
Extreme Precipitation	N/A	N/A	N/A	N/A
Sea Level Rise	N/A	N/A	N/A	N/A
Wildfire	N/A	N/A	N/A	N/A
Flooding	N/A	N/A	N/A	N/A
Drought	N/A	N/A	N/A	N/A
Snowpack Reduction	N/A	N/A	N/A	N/A
Air Quality Degradation	N/A	N/A	N/A	N/A

The sensitivity score reflects the extent to which a project would be adversely affected by exposure to a climate hazard. Exposure is rated on a scale of 1 to 5, with a score of 5 representing the greatest exposure.

The adaptive capacity of a project refers to its ability to manage and reduce vulnerabilities from projected climate hazards. Adaptive capacity is rated on a scale of 1 to 5, with a score of 5 representing the greatest ability to adapt.

The overall vulnerability scores are calculated based on the potential impacts and adaptive capacity assessments for each hazard. Scores do not include implementation of climate risk reduction measures.

6.3. Adjusted Climate Risk Scores

Climate Hazard	Exposure Score	Sensitivity Score	Adaptive Capacity Score	Vulnerability Score
Temperature and Extreme Heat	N/A	N/A	N/A	N/A
Extreme Precipitation	N/A	N/A	N/A	N/A
Sea Level Rise	N/A	N/A	N/A	N/A
Wildfire	N/A	N/A	N/A	N/A
Flooding	N/A	N/A	N/A	N/A
Drought	N/A	N/A	N/A	N/A
Snowpack Reduction	N/A	N/A	N/A	N/A
Air Quality Degradation	N/A	N/A	N/A	N/A

The sensitivity score reflects the extent to which a project would be adversely affected by exposure to a climate hazard. Exposure is rated on a scale of 1 to 5, with a score of 5 representing the greatest exposure.

The adaptive capacity of a project refers to its ability to manage and reduce vulnerabilities from projected climate hazards. Adaptive capacity is rated on a scale of 1 to 5, with a score of 5 representing the greatest ability to adapt.

The overall vulnerability scores are calculated based on the potential impacts and adaptive capacity assessments for each hazard. Scores include implementation of climate risk reduction measures.

6.4. Climate Risk Reduction Measures

7. Health and Equity Details

7.1. CalEnviroScreen 4.0 Scores

The maximum CalEnviroScreen score is 100. A high score (i.e., greater than 50) reflects a higher pollution burden compared to other census tracts in the state.

Indicator	Result for Project Census Tract
Exposure Indicators	—
AQ-Ozone	10.6

AQ-PM	10.5
AQ-DPM	55.7
Drinking Water	17.6
Lead Risk Housing	24.7
Pesticides	99.7
Toxic Releases	17.0
Traffic	30.7
Effect Indicators	—
CleanUp Sites	0.00
Groundwater	44.3
Haz Waste Facilities/Generators	64.6
Impaired Water Bodies	98.1
Solid Waste	80.0
Sensitive Population	—
Asthma	86.7
Cardio-vascular	52.0
Low Birth Weights	43.8
Socioeconomic Factor Indicators	—
Education	38.5
Housing	17.9
Linguistic	22.9
Poverty	19.4
Unemployment	49.9

## 7.2. Healthy Places Index Scores

The maximum Health Places Index score is 100. A high score (i.e., greater than 50) reflects healthier community conditions compared to other census tracts in the state.

Indicator	Result for Project Census Tract
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Economic	—
Above Poverty	57.5003208
Employed	63.51854228
Median HI	60.74682407
Education	—
Bachelor's or higher	48.20993199
High school enrollment	100
Preschool enrollment	83.54933915
Transportation	—
Auto Access	49.51879892
Active commuting	6.403182343
Social	—
2-parent households	22.93083537
Voting	88.46400616
Neighborhood	—
Alcohol availability	97.0101373
Park access	58.11625818
Retail density	27.16540485
Supermarket access	20.74939048
Tree canopy	2.425253433
Housing	—
Homeownership	71.67971256
Housing habitability	73.4377005
Low-inc homeowner severe housing cost burden	43.50057744
Low-inc renter severe housing cost burden	85.53830361
Uncrowded housing	37.66200436
Health Outcomes	—

Insured adults	42.12755037
Arthritis	2.5
Asthma ER Admissions	32.8
High Blood Pressure	5.6
Cancer (excluding skin)	3.4
Asthma	51.9
Coronary Heart Disease	2.2
Chronic Obstructive Pulmonary Disease	13.3
Diagnosed Diabetes	25.3
Life Expectancy at Birth	48.9
Cognitively Disabled	64.4
Physically Disabled	24.6
Heart Attack ER Admissions	66.1
Mental Health Not Good	62.3
Chronic Kidney Disease	3.6
Obesity	57.4
Pedestrian Injuries	49.0
Physical Health Not Good	37.1
Stroke	8.8
Health Risk Behaviors	—
Binge Drinking	87.0
Current Smoker	70.9
No Leisure Time for Physical Activity	45.8
Climate Change Exposures	—
Wildfire Risk	0.0
SLR Inundation Area	0.0
Children	84.9

Elderly	6.9
English Speaking	86.4
Foreign-born	30.6
Outdoor Workers	52.0
Climate Change Adaptive Capacity	—
Impervious Surface Cover	71.7
Traffic Density	27.1
Traffic Access	0.0
Other Indices	—
Hardship	47.7
Other Decision Support	—
2016 Voting	65.8

7.3. Overall Health & Equity Scores

Metric	Result for Project Census Tract
CalEnviroScreen 4.0 Score for Project Location (a)	46.0
Healthy Places Index Score for Project Location (b)	64.0
Project Located in a Designated Disadvantaged Community (Senate Bill 535)	No
Project Located in a Low-Income Community (Assembly Bill 1550)	No
Project Located in a Community Air Protection Program Community (Assembly Bill 617)	No

a: The maximum CalEnviroScreen score is 100. A high score (i.e., greater than 50) reflects a higher pollution burden compared to other census tracts in the state.  
b: The maximum Health Places Index score is 100. A high score (i.e., greater than 50) reflects healthier community conditions compared to other census tracts in the state.

7.4. Health & Equity Measures

No Health & Equity Measures selected.

7.5. Evaluation Scorecard

Health & Equity Evaluation Scorecard not completed.

7.6. Health & Equity Custom Measures

No Health & Equity Custom Measures created.

8. User Changes to Default Data

Screen	Justification
Land Use	<p>Lot acreages for residences would encompass 8 acres. Parking lot includes only the guest spaces because the residential spaces are included within driveways the residential lots, accounted for in the single-family housing measurement.</p> <p>Population changed to 248 residents consistent with project description.</p> <p>2862 square feet encompasses the clubhouse building as designated in the design plan</p>
Construction: Construction Phases	<p>Applicant-provided schedule. CalEEMod only allows one paving phase, so the total amount of time for paving for the three phases (3 months) is shown as one phase.</p>
Construction: Off-Road Equipment	<p>Demolition utilizes CalEEMod defaults. All other phases include construction equipment provided by applicant. Applicant indicates all construction equipment would be Tier 4.</p>
Operations: Vehicle Data	<p>Single family housing trip rate changed based on the VMT Analysis Memo prepared for the project by Associated Transportation Engineers in December 2023. Memo concluded the Average Daily Trip rate for senior detached housing is 4.31 trips per unit</p>

# Appendix C

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Cultural Resources Assessment





**Rincon Consultants, Inc.**

1530 Monterey Street, Suite D  
San Luis Obispo, California 93401  
805-547-0900

July 8, 2024

Project No: 23-15551

Carol Ziesenhenné, Senior Planner  
City of Santa Maria  
Community Development Department  
110 South Pine Street, Suite 101  
Santa Maria, California 93458  
Via email: [cziesenhenné@cityofsantamaria.org](mailto:cziesenhenné@cityofsantamaria.org)

**Subject: Cultural Resources Assessment for the Bellecrest Residences Project at 1571 East Main Street, Santa Maria, California 93454**

Dear Ms. Ziesenhenné:

This letter report presents the findings of a cultural resources assessment completed in support of the Bellecrest Residences Project (proposed project) located at 1571 East Main Street in Santa Maria, Santa Barbara County, California. The City of Santa Maria retained Rincon Consultants, Inc. (Rincon) to support the proposed project's compliance with the California Environmental Quality Act (CEQA). This letter report documents the results of the tasks performed by Rincon, specifically a cultural resources records search, Sacred Lands File (SLF) search with the Native American Heritage Commission (NAHC), archival and background research, and field survey. All work was completed in accordance with CEQA.

This letter report was prepared to present the methods and results of the assessment conducted by Rincon. Rincon Archaeologist and Project Manager, Andrea Ogaz, MA, Registered Professional Archaeologist (RPA) provided cultural resource management oversight, served as a contributing author of the letter report, and completed the SLF search. Rincon Archaeologist Catherine Johnson, PhD, RPA, served as primary author of this letter report. Rincon Architectural Historian Josh Bevan, MSHP, American Institute of Certified Planners (AICP), served as contributing author of this letter report and prepared State of California Department of Parks and Recreation (DPR) 523 series forms; he conducted the historical evaluation presented herein. Principal Archaeologist Christopher Duran MA, RPA provided management oversight regarding archaeological resources. Cultural Resources Director and Senior Architectural Historian Steven Treffers, MHP, provided management oversight regarding built environment resources and reviewed for quality assurance/quality control. All of the professionals noted above meet the Secretary of the Interior's Professional Qualification Standards (PQS) in their respective fields (36 Code of Federal Regulations [CFR] Part 61) (National Park Service [NPS] 1983).

## **Project Site and Description**

The project site is located at 1571 East Main Street in Santa Maria, Santa Barbara County, California. Specifically, the proposed project encompasses portions of Section 12 of Township 10 North, Range 34 West on the *Santa Maria, California* United States Geological Survey (USGS) 7.5-minute topographic quadrangle (Attachment 1: Figure 1). The project site consists of 14.43 acres and encompasses Assessor's Parcel Numbers (APNs) 128-052-014 and 128-052-023. The surrounding vicinity consists of single-family residential developments to the north, west, and east, Pioneer Valley High School to the northeast, East Main Street to the south, and undeveloped land to the southwest.



(Attachment 1: Figure 2). Agricultural land is located to the south of the project site outside of the City limits in Santa Barbara County, adjacent to East Main Street

The proposed project involves the demolition of the existing single-family residence and associated structures and the development of a gated, 100 percent senior age-restricted residential community. The residential community would include 142 single-family residential lots; a community clubhouse with a pool, spa, and cabanas; an outdoor living and activity lawn; and a pet-friendly pocket park with a covered gazebo and outdoor seating. The single-family residences would all be one-story buildings with a maximum building height of 22 feet 9 inches. The community clubhouse would be located at the southwest portion of the project site. The community clubhouse building would include an assembly room, card room, kitchen, fitness gym, storage, janitor's closet, and restrooms. The community clubhouse would be constructed up to 25 feet 4 inches tall. The outdoor living and activity lawn, pool, spa, cabanas, pool equipment building, and barbecue area would be located adjacent to the community clubhouse building. The 7,737 square-foot pet friendly pocket park and pavilion would be located on the northern portion of the project site.

The project includes a General Plan Land Use Amendment and Zone Change to facilitate development of the proposed residential community. This would change the project site's land use classification from Lower-Density Residential (LWDR-4) to Medium Density Residential (MDR-12) and zoning from Single Family Residential with a Planned Development overlay (PD/R-1) to Medium Density Residential with a Planned Development overlay (PD/R-2).

## **Methods**

### **Background and Archival Research**

Rincon completed background and archival research in support of this assessment in June 2024. A variety of primary and secondary source materials were consulted. Sources included, but were not limited to, historical maps, aerial photographs, and written histories of the area. The following sources were utilized to develop an understanding of the project site and its context:

- Historical aerial photographs accessed via NETR Online (NETR)
- Historical aerial photographs accessed via University of California, Santa Barbara Library FrameFinder (UCSB)
- Historical USGS topographic maps (USGS)
- Historical plat maps via Bureau of Land Management General Land Office Records (BLM)
- City of Santa Maria Building Permits accessed via the City of Santa Maria Community Development Department, Planning Division
- Historical newspaper clippings obtained from Newspapers.com
- Various historical records via Ancestry.com
- Geologic Maps via USGS National Geologic Map Database
- Soil Data Explorer via California Soils Resource Lab

### **California Historical Resources Information System Records Search**

On April 11, 2024, Rincon requested California Historical Resources Information System (CHRIS) records search results (records search # 24-070) from the Central Coast Information Center (CCIC) (Attachment 2). The CCIC is the official state repository for cultural resources records and reports for the county in which the proposed project falls. The purpose of the records search was to identify



previously recorded cultural resources, as well as previously conducted cultural resources studies within the project site and a 0.5-mile radius surrounding it. Rincon also reviewed the National Register of Historic Places (NRHP), the California Register of Historical Resources (CRHR), the California Historical Landmarks list, and the Built Environment Resources Directory, as well as its predecessor the California State Historic Property Data File. Additionally, Rincon reviewed the Archaeological Determination of Eligibility list.

## **Sacred Lands File Search**

Rincon contacted the NAHC on April 18, 2024, to request a search of the SLF, as well as a CEQA Assembly Bill (AB) 52 and General Plan Senate Bill (SB) 18 contact list of Native Americans culturally affiliated with the project site vicinity (Attachment 3). The City of Santa Maria is conducting consultation under AB 52 and SB 18.

## **Field Survey**

Under the direction of Rincon Director and Senior Architectural Historian Steven Treffers, Rincon Archaeologist Catherine Johnson, PhD, RPA, conducted a built environment survey of the project site on June 14, 2024. The built environment resources within the project site, including buildings, structures, and associated tennis/basketball court and landscape elements, were visually inspected. Pursuant to OHP Guidelines (California OHP 1995: 2), properties over 45 years of age were evaluated for inclusion in the NRHP, CRHR, and local listing and recorded on DPR 523 series forms. The overall condition and integrity of these resources were documented and assessed. Site characteristics and conditions were documented using notes and digital photographs which are maintained at our Rincon San Luis Obispo office.

Catherine also conducted a pedestrian survey of the project site on June 14, 2024. The pedestrian survey was conducted using transect intervals spaced 15 meters and oriented generally from east to west. Exposed ground surfaces were examined for artifacts (e.g., flaked stone tools, tool-making debris, stone milling tools, ceramics, fire-affected rock), ecofacts (marine shell and bone), soil discoloration that might indicate the presence of a cultural midden, soil depressions, and features indicative of the former presence of structures or buildings (e.g., standing exterior walls, postholes, foundations) or historical debris (e.g., metal, glass, ceramics). Ground disturbances such as burrows and drainages were also visually inspected. Survey accuracy was maintained using a handheld Global Positioning Satellite unit and a georeferenced map of the project site. Site characteristics and survey conditions were documented using field records and a digital camera. Copies of the survey notes and digital photographs are maintained at our Rincon San Luis Obispo office. Representative photographs of the built environment and archaeological surveys are presented in Attachment 4.

## **Findings**

### **Background Research**

#### **California Historical Resources Information System**

The CHRIS records search and background research identified four cultural resources studies within 0.50 mile of the project site. Of these studies, none include a portion of the project site, and none include areas directly adjacent to the project site. Zero percent of the project site has been studied, and zero percent has been previously surveyed for cultural resources.



The CHRIS records search and background research identified zero cultural resources within a 0.50 mile of the project site.

### **Sacred Lands File Search**

On April 18, 2024, the NAHC responded to Rincon's AB 52/SB 18 contacts and SLF request, stating that the results of the SLF search were negative. See Attachment 3 for the NAHC response, including Tribal contacts list(s).

### **Aerial Imagery and Historical Topographic Maps Review**

Rincon completed a review of historical topographic maps and aerial imagery to ascertain the developmental history of the project site. A review of Bureau of Land Management (BLM) GLO Plat maps from 1861 and 1873 depict the project site as part of Suey Rancho lot number 37 (BLM 1861 and 1873). To the north of the project site is a road trending southeast titled "Road from San Luis Obispo to Santa Barbara." Historical topographic maps from 1905 depict the project site and surrounding area as undeveloped, situated between a major roadway to the west, a secondary road dotted with buildings to the south (East Main Street), and Santa Maria River approximately 0.75 mile northeast (USGS 1905). Historical aerial photography from 1938 and 1939 depict the project site as an agricultural field with a property within the southeastern corner along East Main Street (UCSB 1938, 1939). A second property consisting of main buildings and associated structures is located westerly adjacent to the southwestern-most corner of the project site along East Main Street. The surrounding areas are primarily agricultural fields with scattered residential properties. Aerial photography from 1943 shows development northwest of the project site westerly adjacent to present day Suey Road, with an access road running west to east through the northern part of the project site and an access road trending south towards East Main Street located to the southwest of the project site and the existing residential property (UCSB 1943).

Historical topographic maps from 1947 depict this access road leading north from East Main Street located just west of the present-day paved road within the project site (USGS 1947). Aerial photography from 1949 depicts the existing residential property southwest of the project site along East Main Street as extending east into the project site (UCSB 1949). The access roads in the northern portion of the project site have been graded over and an additional property appears along Suey Road west of the project site. Aerial photography from 1954 shows activity in the southeastern portion of the project site, which is depicted in aerial photography from 1956 as an extension of the southeastern property, which has expanded north and west (UCSB 1954, 1956). The field to the west of the property and within the project site appears overgrown, and the northern half of the project site appears evenly graded. By 1960 the property and access road to the southwest of the project site and the majority of the property within the southeastern corner of the project site had been removed, and by 1964 the only remnant of the southeastern property are ornamental trees (NETR Online 1964; UCSB 1960). Additionally, aerial photography from 1964 depicts an oval-shaped feature, an apparent track, dominating the northern portion of the project site and a small orchard and associated structures outside of the northeastern corner (NETR Online 1964). In aerial photography from 1966, this oval feature is expanded in size extending the full length of the northern portion of the project site (UCSB 1966).

Historical topographic maps from 1974 depict an access road trending north from East Main Street aligned with the present-day paved road as well as a building in the location of the extant single-family residence (USGS 1974). By 1981 the extant residential building and orchard fields had been developed along with the two ancillary structures south of the house (NETR Online 1981). The oval feature had been removed and the extant open grassy field is in its place. Aerial imagery from 1994

depicts the project site with the extant tree-lined border and by 2005 the extant basketball court had been constructed in the northwest corner of the project site (NETR Online 1994, 2005). The project site remains unchanged in aerial photography from 2005 to 2020 (NETR Online 2024).

## **Geologic and Soils Map Review**

Geologic mapping indicates Quaternary surficial sediments (map unit Qay) from alluvial fans and fluvial deposits are mapped at the surface within the project site (Sweetkind et al. 2021). This geologic unit was deposited during the Holocene (beginning approximately 11,700 years ago). The Holocene dates to human occupation of the region and is generally conducive to the natural burial and preservation of archaeological deposits. Soils mapping indicates the project site is underlain primarily by Sorrento sandy loam (StA) and Sorrento loam (SvA), a very deep, well-drained soil that forms in alluvium mostly from sedimentary rocks on alluvial fans and stabilized floodplains (California Soil Resource Lab 1999). The typical Sorrento series soil profile consists of topsoil (A-horizon) consisting of grayish brown to very dark grayish brown heavy loam from depths of 0 to 26 inches below the ground surface; grayish brown mixed with light brownish gray to dark grayish brown mixed with dark brown heavy loam from 26 to 37 inches below the ground surface; pale brown to dark yellowish brown heavy loam from 37 to 48 inches below the ground surface; light yellowish brown to yellowish brown fine sandy loam from 48 to 58 inches below the ground surface; and light yellowish brown to yellowish brown loamy fine sand from 58 to 74 inches below the ground surface (California Soil Resource Lab 1999). The soil profile does not contain subsurface topsoil, which would indicate potential for the presence of subsurface archaeological deposits.

## **Archaeological Sensitivity Summary**

The archival research indicates the sediments mapped at surface within the project site are generally conducive to the natural burial and preservation of archaeological resources given they were deposited during the Holocene, a period that dates to human occupation of the region. The soils map indicates the project site is underlain by Sorrento loam, which does not have documented buried A horizons. Given the age of the geologic unit and the absence of buried soil horizons as suggested by the geologic and soils maps, the project site has low to moderate sensitivity for the presence of subsurface archaeological deposits. However, the degree of previous disturbance within the project site associated with the construction of the extant single-family residence, ancillary structures and tennis/basketball court, and access road, orchard and agricultural activity, grading, and removal of previous structures within the project site, would reduce the likelihood for encountering intact subsurface archaeological deposits during project construction. Therefore, Rincon recommends a low sensitivity for the presence of subsurface archaeological deposits.

## **Survey Results**

### **Archaeological Resources**

Ground visibility was poor (0 to 35 percent) with approximately 25 percent exposure. Heavy vegetation including tall, thick grasses and weeds, unkempt trees and overgrowth, fallen tree branches, and leaf litter obscured surface visibility throughout the project site (Attachment 4: Photograph 1 through Photograph 4). Additionally, decorative rock, garden landscaping, imported gravel and wood chips, paved surfaces, and the extant residential building and associated structures supplied further limitations to surface visibility (Attachment 4: Photograph 5 through Photograph 9). Additional disturbances included frequent small animal burrows, which provided opportunities for inspection of exposed subsurface sediments. Where the ground was visible, the exposed soil consisted of light brown and greyish-brown silty loam (Attachment 4: Photograph 9 and Photograph 11). Some areas



were inaccessible due to vegetation including the northern half of the southeastern field, which consisted of knee-high and 5-foot-tall dried grasses and weeds (Attachment 4: Photograph 11) and the northeastern boundary of the project site, which consisted of thick mustard weeds and obstructed by the existing row of oak trees (Attachment 4: Photograph 13). Vegetation consisted of non-native ornamental trees and garden plants and flowers (including bamboo, oak, and pine), orchard trees, and seasonal grasses and weeds (including thistles and mustard). The project site was primarily flat, apart from raised earth features in the northern area of the project site. These features consisted of two half-circle-shaped mounds of earth in the northeast and northwest and a linear berm along the tree line north of the open field (Attachment 4: Photograph 14 and Photograph 15). No built environment features were observed associated with the earth features and their purposes are uncertain. The area has been heavily disturbed from construction of the extant single-family residence, garden area, and ancillary structures, landscaping, construction of the extant basketball court, orchard rows and irrigation infrastructure, paved roadway, and grading.

Two fragments of bottle glass were identified in the southeastern corner of the project site north of East Main Street. The fragments included one circular, colorless glass bottle base embossed with the Maywood Glass Company maker's mark, dating the fragment between 1930 and 1959 (Attachment 4: Photograph 16); and one amber glass bottle base embossed with the Owen's Illinois maker's mark dating the fragment between 1954 and present day (Attachment 4: Photograph 17). The fragments were observed within light brown silty loam surrounded by dried grasses and weeds. These isolates were recorded as part of the DPR 523 series forms of 1571 East Main Street, which are included in Attachment 5. No additional cultural resources were identified during the field survey.

## **Built Environment Resources**

The following section summarizes the results of all background research and fieldwork as they pertain to built environment resources that may qualify as historical resources. The fieldwork and background research resulted in the identification of one historic-age property within the project site: 1571 East Main Street. This property was recorded and evaluated for historical resources eligibility on DPR 523 series forms, which are included in Attachment 5 and summarized below.

### *1571 East Main Street*

## **PHYSICAL DESCRIPTION**

1571 East Main Street is an approximately 15.23-acre single-family residential property composed of two parcels, located on the eastern edge of the City of Santa Maria. The property, located on the north side of East Main Street to the east of E. Suey Road and west of Navarra Way, consists of a single-family residence, detached ancillary building, landscaping, a tennis/basketball court, a pasture, and orchard areas (See Attachment 4: Photograph 7 through Photograph 9). Parcel 128-052-023 is a vacant 3.48-acre rectangular parcel comprising the southeastern area of the site along East Main Street. Parcel 128-052-014 is an irregularly shaped parcel with a driveway extending northward from East Main Street to the site interior, terminating at a circular turnaround on the west side of the residence. The residence is oriented with its southwest façade toward East Main Street, northwest (primary) façade facing the driveway turnaround, and northeast and southeast façades oriented to interior areas of the property. To the east of the residence is a lawn, generally rectangular in shape, bordered by trees. The southern, eastern, northern perimeters and western third of the site are planted with orchards. A tennis/basketball court is in the northwest corner of the property. An ancillary building is located immediately east of the driveway, upon entering the property beyond the perimeter tree line; another ancillary shed is located to the north of the residence on the perimeter of the driveway.



## **PROPERTY HISTORY**

As of 1939, the subject property's site consisted of portions of two farmsteads or similar properties and agricultural land (UCSB 1938). One property was located approximately at the existing location of the driveway entrance on the north side of East Main Street. This property appears to have consisted of a residence and a barn, while only the barn appears to have been situated on land now within the subject property as part of parcel 128-052-014. The other farmstead was slightly smaller and located at the southeast corner of the existing property, at the northeast corner of East Main Street and Navarra Way. This farmstead appears to have consisted of three primary buildings, potentially with additional outbuildings. Review of GLO records, historical county maps and census records did not confirm ownership of the farmsteads that were present by 1939 (GLO 1861, 1873; Ancestry 2024).

The farmsteads described above appear to have been vacated by the 1950s and their associated buildings and structures were non-extant by 1967. During the mid-1960s, the present-day parcel 128-052-023 was vacant, while the land within the larger present-day parcel 128-052-014 featured an oval track by 1967 (NETR 2024). The track's origin is unknown, while its oval shape appears to generally align with the area now containing a lawn within the residential property. In 1974, Dr. and Mrs. Robert Ibsen received permits to construct a single-family residence and garage on the property at 1571 East Main Street (City of Santa Maria 2024). By 1981, the property featured the existing entrance driveway, two ancillary buildings to the east of the driveway and south of the residence, the oval-shaped area containing the residence and garage, a rectangular lawn area to the east of the residence, and orchard areas in the remainder of the larger of the two parcels. The second smaller parcel continued to be vacant land as of 1981. Review of historical aerial photography indicates the property has retained similar characteristics since 1981, with known alterations including the construction of a tennis court in the northwest corner of the property between 1994 and 2005 and the planting of a row of trees near to the east of the entrance driveway by 1994 (NETR 2024). During this same period, suburban development to the north and west of the property continued, including along Rowland Drive, to the immediate north of the property and along N. Suey Road and Jonathan Place, and to the immediate east on Navarra Way.

### Dr. Robert Louis Ibsen (1931-2016)

Dr. Robert Ibsen was born in Los Angeles in 1931 and died in 2016 at age 84 (Boston University 2016). He earned a degree in optometry from Southern California College in 1953 and a degree in dentistry from the University of Southern California in 1958 (Dudley Hoffman 2016). Ibsen married Marcia Ricks and the Ibsens settled in Santa Maria, where Dr. Ibsen practiced with Dr. Harold Case for seven years before establishing his own practice. Dr. Ibsen was known as a pioneer in the field of cosmetic dentistry and contributed to the development of over 30 patents during his career, in addition to serving as a Clinical Instructor at USC's School of Dentistry and as a Clinical Lecturer in the Department of Operative Dentistry at Boston University. His obituary notes:

He was awarded 9 Fellowships within the dental profession. He even co-authored the first book on adhesive dentistry and lectured to thousands of dentists around the world. He changed the face of cosmetic dentistry with his products and philosophies, eliminating the need for shots and drilling.

In 1974 he started Den Mat Corporation and hired Richard Glace as his chemist to translate his ideas into materials that solved a myriad of dental needs. What began as a small business with 10 employees in the confines of a house on West Cook Street, DenMat evolved into a business larger than anyone could have dreamed. Fifteen years, four moves and 600 employees later, DenMat became home to Rembrandt Toothpaste, the first ever whitening toothpaste, and began a

revolution in the world of dentistry. Rembrandt was purchased in 2004 by Gillette. Never one to sit still, Bob began on his next venture. He shifted his focus from toothpaste to minimally-invasive veneer placement, launching the Lumineers brand. After a long and successful run, the business was sold to a private equity group in 2007. With too much energy to retire at 74, Bob continued teaching and practicing cosmetic dentistry until the very last months of his life (Dudley Hoffman 2016).

Research of city directories identified the addresses 220 W. Cypress Street (ca. 1961 to ca. 1966, appears nonextant) and a medical-office building at 730 East Chapel Street (ca. 1967 to ca. 1983, extant) as Ibsen's business addresses in Santa Maria (Ancestry 2024). Research did not identify Ibsen's residence at 1571 East Main Street as a place of professional practice.

Dr. Robert Ibsen appears to have resided in the residence on the subject property between ca. 1974 and his death in 2016. As of this evaluation, the Ibsen-founded DenMat is headquartered in Lompoc, California.

## **HISTORICAL RESOURCES EVALUATION**

1571 East Main Street is recommended ineligible for listing in the NRHP, CRHR under all evaluative criteria due to a lack of architectural or historical significance.

1571 East Main Street was built in 1974 as a single-family residential property in the eastern region of the City of Santa Maria. Built on land that had contained an oval track by 1967, and as of 1939 two small farmsteads and agricultural land, the existing built environment resources are not associated with these no longer extant and earlier historic-period uses, but rather with a period of continued expansion of the city's limits after post-World War II. During this period, suburbanization became common in urbanized areas of Santa Barbara County, including Santa Maria. Built as the personal residence of prominent dentist Dr. Robert Ibsen and Marcia Ibsen, the property does not appear to be individually significant for having an association with ongoing development or suburbanization in the region in the 1970s. Research did not find that this property is associated with any other historic events of significance. Therefore, 1571 East Main Street is recommended ineligible under Criterion A/1 (Events).

Research into the property's ownership and occupancy found that it was owned and occupied ca. 1974 to ca. 2016 by Dr. Robert Ibsen and Marcia Ibsen. Dr. Ibsen led a career as a prominent and influential practitioner, technology developer, and lecturer in the field of cosmetic dentistry, and based his professional practice and business endeavors in Santa Maria for much of his career. It appears that the subject property was built in 1974, coinciding with Dr. Ibsen's establishment of the DenMat Corporation, which was eventually acquired by several parent corporations. Dr. Ibsen's professional work as a dentist was conducted at several business locations during his career, as well as on multiple university campuses. Although he resided on the subject property during the prime of his career, his places of work where he conducted business are more strongly associated with his contributions to the field of cosmetic dentistry. Therefore, 1571 East Main Street is recommended ineligible under Criterion B/2 (Persons).

Documentation relating to the building's original design and construction and associated design and building professionals was not found, beyond an original building permit listing Ibsen as the general contractor. Although Dr. Ibsen was a successful dentist, his primary profession was not as a general



contractor. Research of available historical newspapers failed to identify another contractor or an architect who may have participated in the design and construction of the Ibsen's residence in 1974. Thus, available documentation does not link the building to any builders or designers considered masters in their field. The subject building is representative of a contemporary, vernacular residence of the mid-1970s, but does appear to be an individually distinctive example of its type, period, or method of construction, or to possess high artistic values. The property is relatively large compared to the numerous suburban single-family properties in its immediate vicinity but does not appear to be significant based on its relative size alone. Overall, the property does not rise to level of significance. Therefore, 1571 East Main Street is recommended ineligible under Criterion C (Architecture/Design).

Research does not indicate the property has the potential to yield important information pertaining to prehistory or history under Criteria D (Information Potential). The isolates identified during the field survey were two isolated glass fragments, which have limited data potential and are typically not eligible for listing in the NRHP or CRHR.

#### City of Santa Maria Historical Landmark

Chapter 8-3 Historical Landmarks of the City of Santa Maria's Municipal authorizes the Recreation and Parks Commission to "receive and act upon applications from any interested persons to investigate and designate places, sites, buildings, structures, works of art and other objects within the incorporated limits of the City as having historic, cultural, aesthetic or other special character or interest, and being worthy of consideration for protection, enhancement or perpetuation as such." (City of Santa Maria 2024). "The Recreation and Parks Commission is further authorized and directed to locate and identify other places, sites, buildings, structures, and works of art as having historical merit which may satisfy the requirements for designation as an historical landmark or which may by the application of other standards, or by reason of a unique feature, have, in the opinion of the Recreation and Parks Commission, special historical, aesthetic or cultural value." Standards for designation and for removal of designation include:

The landmark designated shall have historical, cultural, aesthetic or special character or interest for the general public and not be limited only in interest to a special group of persons, and be at least 50 years of age. (Ord. 88-18 § 5, eff. 10/20/88; Ord. 2001-24, eff. 1/18/02; Ord. 2022-04, eff. 7/7/22)

The subject property does not appear qualify as a Historical Landmark. As explained above, the property does not appear to possess historical, cultural, aesthetic, or special character or interest. Although approximately 50 years old as of this evaluation, 1571 East Main Street has not been demonstrated to possess historical or architectural significance.

## **Conclusions and Recommendations**

The impact analysis included here is organized based on the cultural resources thresholds included in CEQA Guidelines Appendix G: Environmental Checklist Form:

- a. Would the project cause a substantial adverse change in the significance of a historical resource pursuant to Section 15064.5?
- b. Would the project cause a substantial adverse change in the significance of an archaeological resource pursuant to Section 15064.5?
- c. Would the project disturb any human remains, including those interred outside of dedicated cemeteries?



Threshold A broadly refers to historical resources. To more clearly differentiate between archaeological and built environment resources, we have chosen to limit analysis under Threshold A to built environment resources. Archaeological resources, including those that may be considered historical resources pursuant to Section 15064.5 and those that may be considered unique archaeological resources pursuant to Section 21083.2, are considered under Threshold B.

## Historical Built Environment Resources

The field survey and background research identified one built-environment historical resource in the project site, 1571 East Main Street. As detailed above under *Historical Resources Evaluation*, the resource was determined ineligible for the NRHP, CRHR and as City of Santa Maria Historical Landmark; therefore, the property therefore does not qualify as a historical resource as defined by CEQA. The proposed project would therefore result in **no impact to historical resources** under CEQA.

## Historical and Unique Archaeological Resources

The records search completed for the project did not identify any previously recorded cultural resources within the project site. The natural setting and soil conditions of the project site, in consideration with the degree of previous disturbance, suggest low sensitivity for archaeological resources. Results from the CHRIS search indicate there are no known prehistoric or historic archaeological resources within or adjacent to the project site. The field survey identified two isolates; however, these are glass fragments which date to the historic period and do not appear to have any significant associations or data potential. Furthermore, cultural resource studies performed within a 0.5-mile radius of the project site did not result in the identification or recording of any prehistoric or historic archaeological resources and the SLF results were negative. No archaeological resources were identified during the field survey. In addition, the project site has been heavily disturbed by landscaping and the development of the existing structure. For these reasons, the project site is not considered sensitive for archaeological resources. Rincon presents the following recommended mitigation measure for unanticipated discoveries during construction. With adherence to this measure, Rincon recommends a finding of **less than significant impact with mitigation for archaeological resources** under CEQA.

## Recommended Mitigation

### *Unanticipated Discovery of Cultural Resources*

If archaeological resources are unexpectedly encountered during ground-disturbing activities, work within 50 feet of the find shall halt and an archaeologist meeting the Secretary of the Interior's Professional Qualifications Standards for archaeology (National Park Service 1983) shall be contacted immediately to evaluate the resource. If the resource is determined by the qualified archaeologist to be prehistoric, then a Native American representative shall also be contacted to participate in the evaluation of the resource. If the qualified archaeologist and/or Native American representative determines it to be appropriate, archaeological testing for CRHR eligibility shall be completed. If the resource proves to be eligible for the CRHR and significant impacts to the resource cannot be avoided via project redesign, a qualified archaeologist shall prepare a data recovery plan tailored to the physical nature and characteristics of the resource, per the requirements of CCR Guidelines Section 15126.4(b)(3)(C). The data recovery plan shall identify data recovery excavation methods, measurable objectives, and data thresholds to reduce any significant impacts to cultural resources related to the resource. Pursuant to the data recovery plan, the qualified archaeologist and Native American representative, as appropriate, shall recover and document the scientifically consequential information that justifies the resource's significance. The City shall review and approve the treatment



plan and archaeological testing as appropriate, and the resulting documentation shall be submitted to the regional repository of the California Historical Resources Information System, per CCR Guidelines Section 15126.4(b)(3)(C).

## Human Remains

No human remains are known to be present within the project site. However, the discovery of human remains is always a possibility during ground disturbing activities. If human remains are found, the State of California Health and Safety Code Section 7050.5 states that no further disturbance shall occur until the County Coroner has made a determination of origin and disposition pursuant to Public Resources Code Section 5097.98. In the event of an unanticipated discovery of human remains, the County Coroner must be notified immediately. If the human remains are determined to be of Native American origin, the Coroner will notify the Native American Heritage Commission, which will determine and notify a most likely descendant (MLD). The MLD has 48 hours from being granted site access to make recommendations for the disposition of the remains. If the MLD does not make recommendations within 48 hours, the landowner shall reinter the remains in an area of the property secure from subsequent disturbance. With adherence to existing regulations, Rincon recommends a finding of **less than significant impact to human remains** under CEQA.

Should you have any questions concerning this study, please do not hesitate to contact the undersigned at 213-784-7550 or aogaz@rinconconsultants.com.

Sincerely,

**Rincon Consultants, Inc.**

A handwritten signature in black ink, appearing to read "Andrea Ogaz", with a stylized, cursive script.

Andrea Ogaz, MA, RPA  
Archaeologist/Project Manager

A handwritten signature in black ink, appearing to read "Josh Bevan", with a stylized, cursive script.

Josh Bevan, MSHP, AICP  
Architectural Historian

A handwritten signature in black ink, appearing to read "Catherine Johnson", with a stylized, cursive script.

Catherine Johnson, PhD, RPA  
Archaeologist

A handwritten signature in black ink, appearing to read "Steven Treffers", with a stylized, cursive script.

Steven Treffers, MHP  
Cultural Resources Director

## Attachments

- Attachment 1 Figures
- Attachment 2 California Historical Resources Information System Results
- Attachment 3 Native American Heritage Commission Sacred Lands File Search Results
- Attachment 4 Photographs
- Attachment 5 California Department of Parks and Recreation 523 Series Forms

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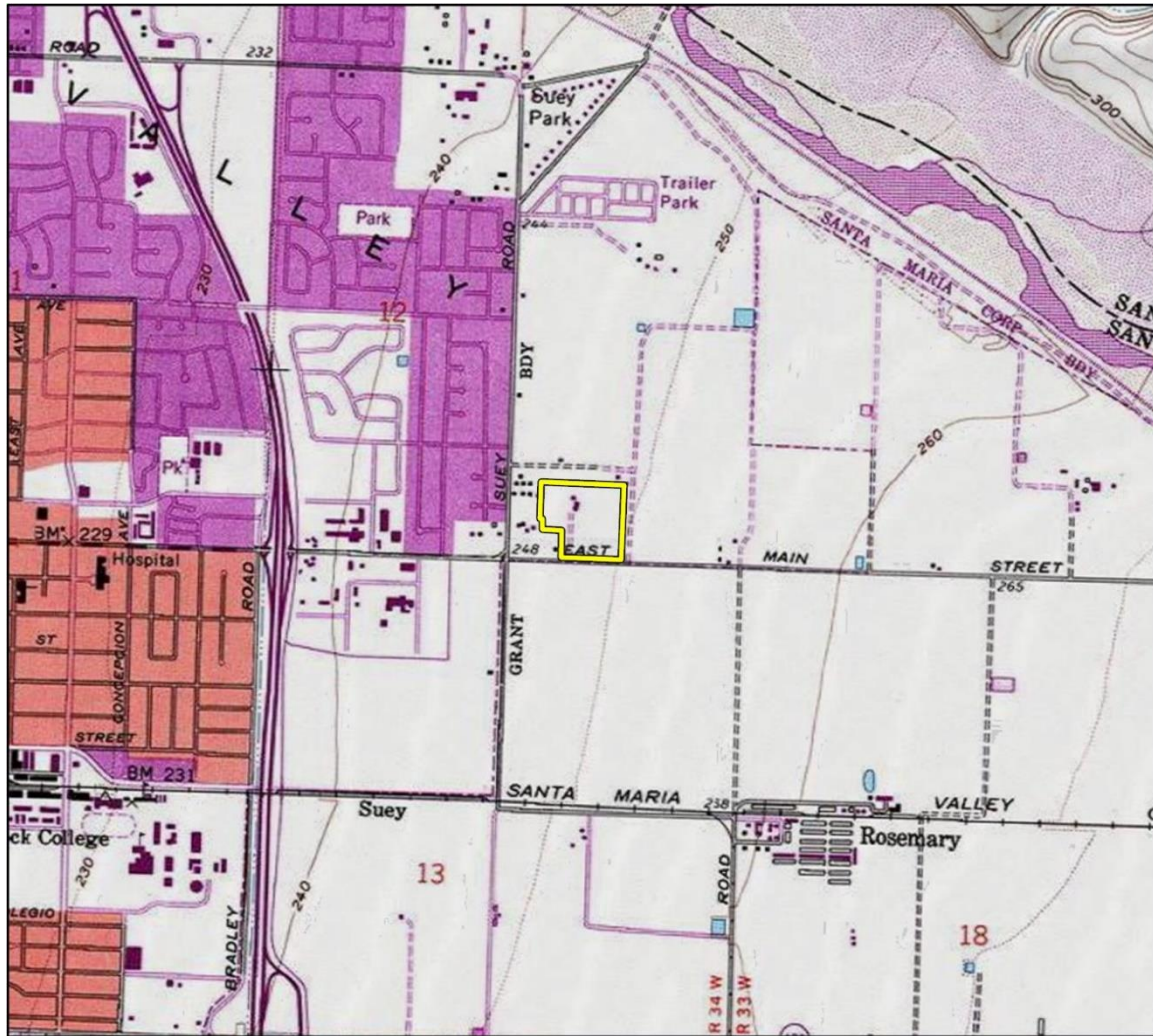
# Attachment 1

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Figures



**Figure 1 Regional Location Map**



Basemap provided by National Geographic Society, Esri and their licensors  
© 2024. Santa Maria Quadrangle. T10N R34W S12. The topographic representation depicted in this map may not portray all of the features currently found in the vicinity today and/or features depicted in this map may have changed since the original topographic map was assembled.

29-15551 CR  
CRFig 1 Proj Locn Map

 Project Location

0 1,000 2,000 Feet

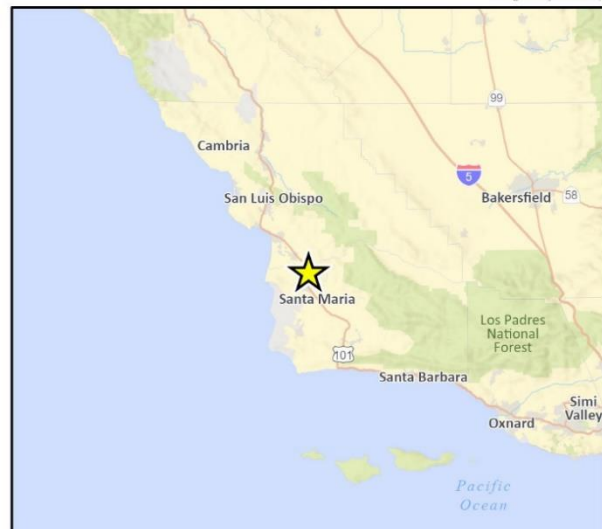
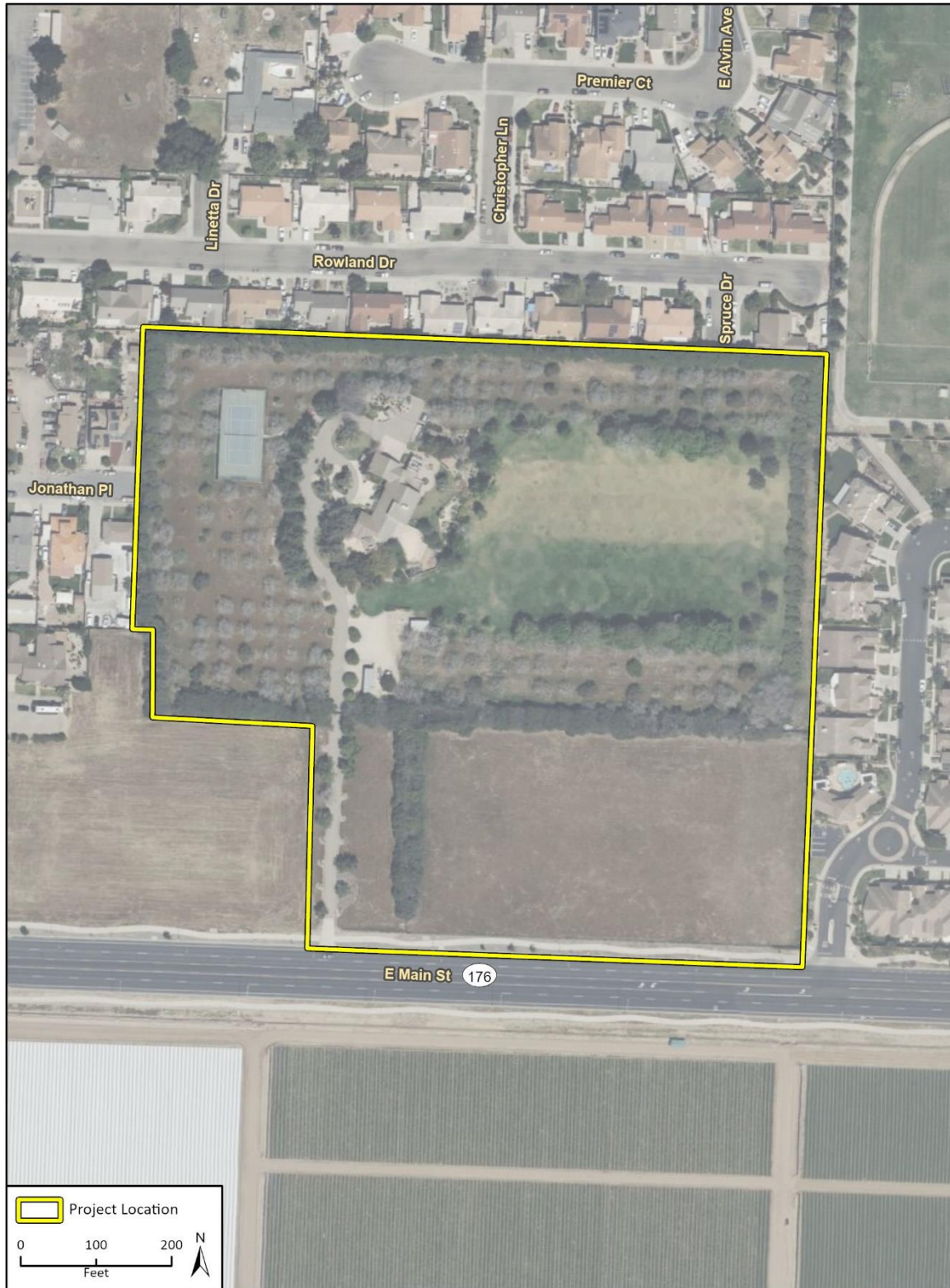




Figure 2 Project Location Map



Imagery provided by Microsoft Bing and its licensors © 2024.

23-15551 CR  
CRFig 2 Project Site

## **Attachment 2**

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California Historical Resources Information System Results



## Central Coast Information Center

Santa Barbara Museum of Natural History  
2559 Puesta del Sol  
Santa Barbara, CA 93105

PHONE (805) 682-4711 ext. 181

FAX (805) 682-3170

EMAIL [ccic@sbnature2.org](mailto:ccic@sbnature2.org)

4/17/2024

Records Search # 24-070

Andrea Ogaz  
Rincon Consultants, Inc.  
180 N. Ashwood Avenue  
Ventura, CA 93003

Re: 23-15551 Bellecrest Senior Residential Project

The Central Coast Information Center received your record search request for the project area referenced above, located on the Santa Maria USGS 7.5' quad(s). The following reflects the results of the records search for the project area and a One-Half Mile radius:

As indicated on the data request form, the locations of reports and resources are provided in the following format: ☒ custom GIS maps ☐ shapefiles ☐ hand-drawn maps ☐ none

Resources within project area:	None
Resources within ½ mile radius:	None
Reports within project area:	None
Reports within ½ mile radius:	Four; SR-01359, SR-04828, SR-05497, SR-05539

**Resource Database Printout (list):**

☐ enclosed ☐ not requested ☒ nothing listed

**Resource Database Printout (details):**

☐ enclosed ☒ not requested ☐ nothing listed

**Resource Digital Database Records:**

☐ enclosed ☐ not requested ☒ nothing listed

**Report Database Printout (list):**

☒ enclosed ☐ not requested ☐ nothing listed

**Report Database Printout (details):**

☐ enclosed ☒ not requested ☐ nothing listed

**Report Digital Database Records:**

☐ enclosed ☐ not requested ☒ nothing listed

**Resource Record Copies:**

☐ enclosed ☐ not requested ☒ nothing listed

**Report Copies:**

☐ enclosed ☒ not requested ☐ nothing listed

**OHP Historic Properties Directory:**

☐ enclosed ☐ not requested ☒ nothing listed (in project location)

**Archaeological Determinations of Eligibility:** ☐ enclosed ☐ not requested ☒ nothing listed

The following sources of information are available at [http://ohp.parks.ca.gov/?page\\_id=28065](http://ohp.parks.ca.gov/?page_id=28065). Some of these resources used to be available through the CHRIS but because they are now online, they can be accessed directly. The Office of Historic Preservation makes no guarantees about the availability, completeness, or accuracy of the information provided through the sources listed below.

<i>California State Lands Commission Shipwreck Database</i>	<i>Caltrans Historic Bridge Inventory</i>
<i>U.S. Geological Survey Historic Topographic Maps</i>	<i>Rancho Plat Maps</i>
<i>National Park Service National Register of Historic Places Nominations</i>	<i>Natural Resource Conservation Service Soil Survey Maps</i>
<i>US Bureau of Land Management General Land Office Records</i>	<i>California Historical Landmarks Listing (by county)</i>
<i>Five Views: An Ethnic Historic Site Survey for California (1988)</i>	<i>Historical Soil Survey Maps</i>

Please forward a copy of any resulting reports from this project to the office as soon as possible. Due to the sensitive nature of archaeological site location data, we ask that you do not include resource location maps and resource location descriptions in your report if the report is for public distribution. If you have any questions regarding the results presented herein, please contact the office at the phone number listed above.

The provision of California Historical Resources Information System (CHRIS) data via this records search response does not in any way constitute public disclosure of records otherwise exempt from disclosure under the California Public Records Act or any other law, including, but not limited to, records related to archeological site information maintained by or on behalf of, or in the possession of, the State of California, Department of Parks and Recreation, State Historic Preservation Officer, Office of Historic Preservation, or the State Historical Resources Commission.

Due to processing delays and other factors, not all of the historical resource reports and resource records that have been submitted to the Office of Historic Preservation are available via this records search. Additional information may be available through the federal, state, and local agencies that produced or paid for historical resource management work in the search area. Additionally, Native American tribes have historical resource information not in the CHRIS Inventory, and you should contact the California Native American Heritage Commission for information on local/regional tribal contacts.

Should you require any additional information for the above referenced project, reference the record search number listed above when making inquiries. Requests made after initial invoicing will result in the preparation of a separate invoice.

Thank you for using the CHRIS.

Sincerely,



Yoly Cohen  
Assistant Coordinator

## Report List

Report No.	Other IDs	Year	Author(s)	Title	Affiliation	Resources
SR-01359		1992	Breschini, G. and Haversat, T.	Preliminary Cultural Resources Reconnaissance for Revision of the Route 101/166 Interchange, Santa Maria, Santa Barbara County, California		
SR-01359A		1992	Breschini, G.	Negative Archaeological Survey Report for the Proposed Revision of the Route 101/166 interchange, P.M. 05-SB-101-88.6 Santa Maria, Santa Barbara County, California	Archaeological Consulting	
SR-01359B		1992	Breschini, G.	Historic Property Clearance Report for the Proposed Revision of the Route 101/166 Interchange, P.M. 05-SB-101-88.6 Santa Maria, Santa Barbara County, California	Archaeological Consulting	
SR-04828		2009	EarthTouch, Inc.	Collocation ("CO) Submission Packet, FCC Form 621, DSA Pioneer Valley SF-91510A	EarthTouch, Inc.	
SR-05497		1999	Jack Hunter	Historic Property Survey Report - 05 - SB - 101 - Post Mile 84 - Kilometer Post 135 - Charge Unit 05-250 - Expenditure Authorization 446010	Archaeological Information Center at University of California Santa Barbara	
SR-05539		2011	Carrie D. Wills	Cultural Resources Records Search and Site Visit for AT&T Mobility, LLC Candidate VN0052-01 (Pioneer Valley High School), 675 Panther Drive, Santa Maria, Santa Barbara County, California	Environmental Assessment Specialists	

## **Attachment 3**

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Native American Heritage Commission Sacred Lands File Search Results



## NATIVE AMERICAN HERITAGE COMMISSION

April 18, 2024

Andrea Ogaz  
Rincon Consultants, Inc.

Via Email to: [aogaz@rinconconsultants.com](mailto:aogaz@rinconconsultants.com)

CHAIRPERSON  
**Reginald Pagaling**  
Chumash

VICE-CHAIRPERSON  
**Buffy McQuillen**  
Yokayo Pomo, Yuki,  
Nomlaki

SECRETARY  
**Sara Dutschke**  
Miwok

PARLIAMENTARIAN  
**Wayne Nelson**  
Luiseño

COMMISSIONER  
**Isaac Bojorquez**  
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Luiseño Indians

EXECUTIVE SECRETARY  
**Raymond C.  
Hitchcock**  
Miwok, Nisenan

**NAHC HEADQUARTERS**  
1550 Harbor Boulevard  
Suite 100  
West Sacramento,  
California 95691  
(916) 373-3710  
[nahc@nahc.ca.gov](mailto:nahc@nahc.ca.gov)

**Re: Native American Consultation, Pursuant to Senate Bill 18 (SB18), Government Codes §65352.3 and §65352.4, as well as Assembly Bill 52 (AB52), Public Resources Codes §21080.1, §21080.3.1 and §21080.3.2, 23-154551 Bellecrest Senior Residential Project, Santa Barbara County**

To Whom It May Concern:

Attached is a consultation list of tribes with traditional lands or cultural places located within the boundaries of the above referenced counties or projects.

Government Codes §65352.3 and §65352.4 require local governments to consult with California Native American tribes identified by the Native American Heritage Commission (NAHC) for the purpose of avoiding, protecting, and/or mitigating impacts to cultural places when creating or amending General Plans, Specific Plans and Community Plans.

Public Resources Codes §21080.3.1 and §21080.3.2 requires public agencies to consult with California Native American tribes identified by the Native American Heritage Commission (NAHC) for the purpose of avoiding, protecting, and/or mitigating impacts to tribal cultural resources as defined, for California Environmental Quality Act (CEQA) projects.

The law does not preclude local governments and agencies from initiating consultation with the tribes that are culturally and traditionally affiliated within your jurisdiction. The NAHC believes that this is the best practice to ensure that tribes are consulted commensurate with the intent of the law.

Best practice for the AB52 process and in accordance with Public Resources Code §21080.3.1(d), is to do the following:

*Within 14 days of determining that an application for a project is complete or a decision by a public agency to undertake a project, the lead agency shall provide formal notification to the designated contact of, or a tribal representative of, traditionally and culturally affiliated California Native American tribes that have requested notice, which shall be accomplished by means of at least one written notification that includes a brief description of the proposed project and its location, the lead agency contact information, and a notification that the California Native American tribe has 30 days to request consultation pursuant to this section.*

The NAHC also recommends, but does not require that lead agencies include in their notification letters, information regarding any cultural resources assessment that has been completed on the area of potential affect (APE), such as:

1. The results of any record search that may have been conducted at an Information Center of the California Historical Resources Information System (CHRIS), including, but not limited to:
  - A listing of any and all known cultural resources have already been recorded on or adjacent to the APE, such as known archaeological sites;
  - Copies of any and all cultural resource records and study reports that may have been provided by the Information Center as part of the records search response;
  - Whether the records search indicates a low, moderate or high probability that unrecorded cultural resources are located in the APE; and
  - If a survey is recommended by the Information Center to determine whether previously unrecorded cultural resources are present.
2. The results of any archaeological inventory survey that was conducted, including:
  - Any report that may contain site forms, site significance, and suggested mitigation measures.

All information regarding site locations, Native American human remains, and associated funerary objects should be in a separate confidential addendum, and not be made available for public disclosure in accordance with Government Code Section 6254.10.
3. The result of the Sacred Lands File (SFL) check conducted through the Native American Heritage Commission was negative.
4. Any ethnographic studies conducted for any area including all or part of the potential APE; and
5. Any geotechnical reports regarding all or part of the potential APE.

Lead agencies should be aware that records maintained by the NAHC and CHRIS is not exhaustive, and a negative response to these searches does not preclude the existence of a tribal cultural resource. A tribe may be the only source of information regarding the existence of a tribal cultural resource.

This information will aid tribes in determining whether to request formal consultation. In the event, that they do, having the information beforehand will help to facilitate the consultation process.

If you receive notification of change of addresses and phone numbers from tribes, please notify the NAHC. With your assistance we can assure that our consultation list remains current.

If you have any questions, please contact me at my email address:

[Cody.Campagne@nahc.ca.gov](mailto:Cody.Campagne@nahc.ca.gov).

Sincerely,



Cody Campagne  
Cultural Resources Analyst

Attachment



Native American Heritage Commission  
Native American Contact List  
Santa Barbara County  
4/18/2024

County	Tribe Name	Fed (F) Non-Fed (N)	Contact Person	Contact Address	Phone #	Fax #	Email Address	Cultural Affiliation	Counties	Last Updated
Santa Barbara	Barbareño/Ventureño Band of Mission Indians	N	Cultural Resource Committee,	P.O. Box 364 Ojai, CA, 93024	(805) 746-6685		CR@bvbmi.com	Chumash	Kern,Los Angeles,San Luis Obispo,Santa Barbara,Ventura	6/19/2023
	Chumash Council of Bakersfield	N	Julio Quair, Chairperson	729 Texas Street Bakersfield, CA, 93307	(661) 322-0121		chumashtribe@sbcglobal.net	Chumash	Kern,Los Angeles,San Luis Obispo,Santa Barbara,Ventura	
	Coastal Band of the Chumash Nation	N	Gabe Frausto, Chairman	P.O. Box 40653 Santa Barbara, CA, 93140	(805) 568-8063		fraustogabriel28@gmail.com	Chumash	Kern,Los Angeles,San Luis Obispo,Santa Barbara,Ventura	8/28/2023
	Northern Chumash Tribal Council	N	Violet Walker, Chairperson	P.O. Box 6533 Los Osos, CA, 93412	(760) 549-3532		violetsagewalker@gmail.com	Chumash	Kern,Los Angeles,San Luis Obispo,Santa Barbara,Ventura	6/5/2023
	Santa Ynez Band of Chumash Indians	F	Wendy Teeter, Cultural Resources Archaeologist	100 Via Juana Road Santa Ynez, CA, 93460	(805) 325-8630		wteeter@chumash.gov	Chumash	Kern,Los Angeles,San Luis Obispo,Santa Barbara,Ventura	7/6/2023
	Santa Ynez Band of Chumash Indians	F	Sam Cohen, Government & Legal Affairs Director	100 Via Juana Road Santa Ynez, CA, 93460			scohen@chumash.gov	Chumash	Kern,Los Angeles,San Luis Obispo,Santa Barbara,Ventura	7/6/2023
	Santa Ynez Band of Chumash Indians	F	Kelsie Mendoza, Elders' Council Administrative Assistant	100 Via Juana Road Santa Ynez, CA, 93460	(805) 325-5537		cmendoza@chumash.gov	Chumash	Kern,Los Angeles,San Luis Obispo,Santa Barbara,Ventura	2/27/2024
	Santa Ynez Band of Chumash Indians	F	Nakia Zavalla, Tribal Historic Preservation Officer	100 Via Juana Road Santa Ynez, CA, 93460			nzavalla@chumash.gov	Chumash	Kern,Los Angeles,San Luis Obispo,Santa Barbara,Ventura	7/6/2023
	yak tityu tityu yak tilhini – Northern Chumash Tribe	N	Mona Tucker, Chairperson	660 Camino Del Rey Arroyo Grande, CA, 93420	(805) 748-2121		olivas.mona@gmail.com	Chumash	Kern,San Luis Obispo,Santa Barbara	5/30/2023

This list is current only as of the date of this document and is based on the information available to the Commission on the date it was produced. Distribution of this list does not relieve any person of statutory responsibility as defined in Section 7050.5 of the Health and Safety Code, Section 5097.94 of the Public Resources Code and Section 5097.98 of the Public Resources Code.

This list is applicable only for consultation with Native American tribes under Government Code Sections 65352.3, 65352.4 et seq. and Public Resources Code Sections 21080.3.1 for the proposed 23-15551 Bellcrest Senior Residential Project, Santa Barbara County.

Record: PROJ-2024-002083  
Report Type: AB52 SB18 Combo  
Counties: Santa Barbara  
NAHC Group: All

## **Attachment 4**

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Photographs

**Photograph 1 Southeastern Field within Project Site, View to the Northeast**



**Photograph 2 Southern Boundary of Western Orchard, View to the West**





**Photograph 3 Western Orchard, View to the North**



**Photograph 4 Eastern Field, View to the West**





**Photograph 5 Ancillary Structures and Garden Vegetation, View to the Northeast**



**Photograph 6 Paved Driveway and Southern Gate, View to the North**





**Photograph 7    Landscaped Surfaces at the House Entrance, View to the Northeast**



**Photograph 8    Residence, View to the East**





**Photograph 9 Tennis/Basketball Court in Western Area, View to the Northwest**



**Photograph 10 Exposed Soil in Southern Area, Plan View**





**Photograph 11 Exposed Soil in Southeastern Orchard, Plan View**



**Photograph 12 Inaccessible Area in Southeastern Area, View to the North**





**Photograph 13 Inaccessible Area on Northeastern Boundary, View to the North**



**Photograph 14 Earth Feature in Northeastern Corner, View to the Southwest**





**Photograph 15 Linear Earth Feature, View to the West**



**Photograph 16 Maywood Glass Company Glass Fragment, Plan View**





**Photograph 17 Owens Illinois Glass Fragment, Plan View**



## **Attachment 5**

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California Department of Parks and Recreation 523 Series Forms

State of California — The Resources Agency  
DEPARTMENT OF PARKS AND RECREATION  
**PRIMARY RECORD**

Primary #  
HRI #  
Trinomial  
NRHP Status Code 6Z

Other Listings  
Review Code

Reviewer

Date

Page 1 of 9

\*Resource Name or #: 1571 East Main Street

**P1. Other Identifier:** None

**\*P2. Location:** ☐ Not for Publication ☒ Unrestricted

**\*a. County:** Santa Barbara

**\*b. USGS 7.5' Quad:** *Santa Maria, California*

**Date:** 2023 **T** 10N; **R** 34W; **SW ¼ of SE ¼ of Sec 12; S.B.M B.M.**

c. Address: 1571 East Main Street City: Santa Maria Zip: 93454

d. UTM: Zone:, m E/m N

e. Other Locational Data: APN 128-052-014, 128-052-023

**\*P3a. Description:** 1571 East Main Street is an approximately 15.23-acre single-family residential property composed of two parcels, located on the eastern edge of the City of Santa Maria. The property, located on the north side of East Main Street to the east of E. Suey Road and west of Navarra Way, consists of a single-family residence, detached ancillary building, landscaping, a tennis court, a pasture, and orchard areas. (Two isolates were also identified on the property and are discussed in further detail below.) Parcel 128-052-023 is a vacant 3.48-acre rectangular parcel comprising the southeastern area of the site along East Main Street. Parcel 128-052-014 is an irregularly shaped parcel with a driveway extending northward from East Main Street to the site interior, terminating at a circular turnaround on the west side of the residence. To the east of the residence is a lawn, generally rectangular in shape and bordered by trees. The southern, eastern, northern perimeters and western third of the site are planted with orchards. A tennis court is located in the northwest corner of the property. An ancillary building is located immediately east of the driveway, upon entering the property beyond the perimeter tree line; another ancillary shed is located to the north of the residence on the perimeter of the driveway. The built environment features on the property appear to be in good condition.

A paved driveway trends north into the property's interior from the north side of East Main Street. The driveway is flanked by trees and enclosed with chain-link fencing along its western perimeter. It terminates on the west side of the residence (Photograph 1, Page 4).

**\*P3b. Resource Attributes:** HP2. Single-family residential property; HP4. Sheds; HP39. Tennis/Basketball Court

**\*P4. Resources Present:** ☒ Building ☒ Structure ☐ Object ☐ Site ☐ District ☐ Element of District ☒ Other (Isolates)



**P5b. Description of Photo:** Primary façade of residence, view to SE. June 14, 2024

**\*P6. Date Constructed/Age and Sources:**  
1974. City of Santa Maria building permit records (City of Santa Maria 2024).  
☒ Historic ☐ Prehistoric ☐ Both

**\*P7. Owner and Address:**  
Main Street Bungalows LLC  
330 James Way #270  
Pismo Beach, CA 93449-2892

**\*P8. Recorded by:**  
Catherine Johnson, PhD, RPA  
Josh Bevan, AICP, MSHP  
Rincon Consultants  
1530 Monterey Street, Suite D  
San Luis Obispo, California 93401

**\*P9. Date Recorded:** June 14, 2024

**\*P10. Survey Type:** Intensive.

**\*P11. Report Citation:** Rincon Consultants, Inc. Cultural Resources Assessment for the Bellecrest Residences Project at 1571 East Main Street, Santa Maria, California 93454. 2024

**\*Attachments:** ☐ NONE ☒ Location Map ☐ Sketch Map ☒ Continuation Sheet ☒ Building, Structure, and Object Record  
☐ Archaeological Record ☐ District Record ☐ Linear Feature Record ☐ Milling Station Record ☐ Rock Art Record  
☐ Artifact Record ☐ Photograph Record ☐ Other (List):



## LOCATION MAP

## Trinomial

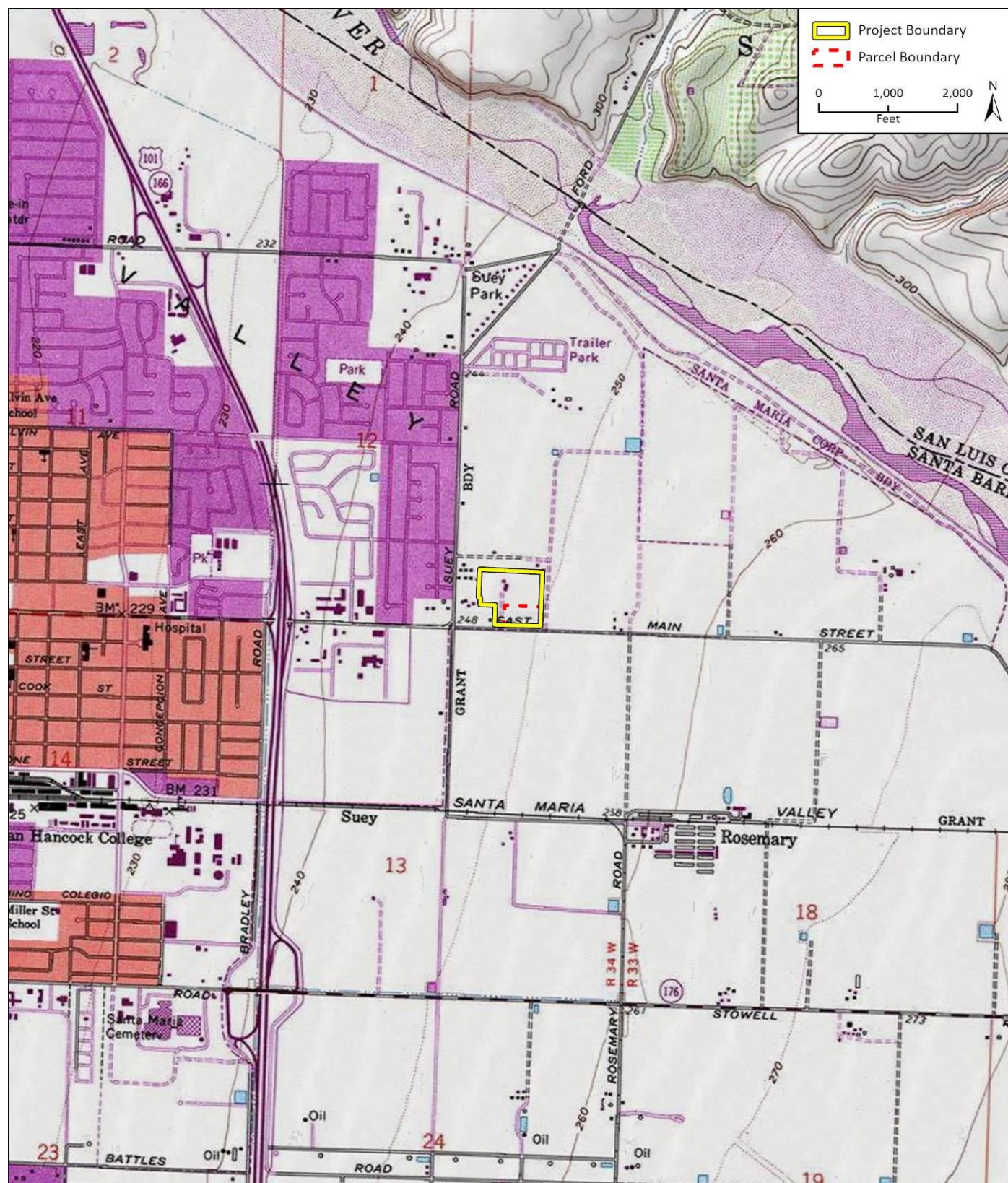
Page 2 of 9

**\*Resource Name or #:** 1571 East Main Street

**\*Map Name:** *Santa Maria Quadrangle*

**\*Scale: 1:24,000**

**\*Date of Map: 2023**



## BUILDING, STRUCTURE, AND OBJECT RECORD

Page 3 of 9

\*NRHP Status Code 6Z

\*Resource Name or # 1571 East Main Street

B1. Historic Name:

B2. Common Name: 1571 East Main Street

B3. Original Use: Single-family property

B4. Present Use: Single-family property

\*B5. Architectural Style: Contemporary (Vernacular)

\*B6. Construction History:

Building Permit Application Documentation on file with City of Santa Maria describes construction of single-family house and three-car garage for Dr. & Mrs. Robert Ibsen under Building Permit B-4553 in 1974. Owner listed as builder-general contractor. (City of Santa Maria 2024) Orchards in place by 1981 (NETR 2024); Tennis court constructed between 1994 and 2005 (NETR 2024).

\*B7. Moved? ☒No ☐Yes ☐Unknown Date:

Original Location:

\*B8. Related Features: None.

B9a. Architect: Unknown

b. Builder: Unknown

\*B10. Significance: Theme: None.

Area: City of Santa Maria

Period of Significance: None.

Property Type: Residential

Applicable Criteria: None.

(Discuss importance in terms of historical or architectural context as defined by theme, period, and geographic scope. Also address integrity.)

(See Continuation Sheets)

B11. Additional Resource Attributes: None.

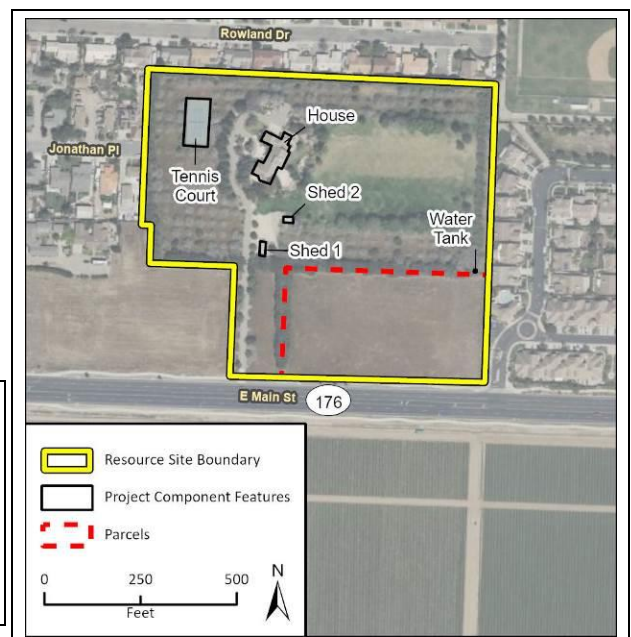
\*B12. References: See Continuation Sheet

B13. Remarks:

\*B14. Evaluator: Josh Bevan, MSHP – Rincon Consultants

\*Date of Evaluation: July 3, 2024

(This space reserved for official comments.)





Page 4 of 9

\*Resource Name or # 1571 East Main Street

Recorded By: Catherine Johnson, PhD, RPA and Josh Bevan, MSHP \*Date: April 24, 2024 ■ Continuation □ Update

**P3a. Description (Continued from Page 1)**

The residence has an irregular plan (roughly a backward C shape) composed of a primary gabled section oriented southwest-northeast and north and south wings, also with gable roofs. It is oriented slightly off the cardinal directions with its southwest façade toward East Main Street, northwest (primary) façade facing the driveway turnaround, and northeast and southeast façades oriented to interior areas of the property. The roof surfaces are finished with wood shingles and trimmed with flat wood fascia. The main roof also features a large dormer with a ribbon window, set above the front entrance (Photograph 2). The front entrance is flanked by brick wrapped columns that support a wood pergola that shades the front entrance steps. The entrance contains double wood doors with narrow vertical windows. The remainder of the exterior features smooth stucco. Fenestration includes horizontal tripartite and two-sash windows made of vinyl. To the north of the residence a rear deck is partially intact and is placed between the house and a steel-framed pergola that extends above an outdoor barbeque (Photograph 3). A paved patio area is located to the southeast of the house, and another to the southwest.



**Photograph 1. Driveway leading into property, view to northwest.**



**Photograph 2. Front entrance area of residence. View to the east.**



**Photograph 3. Rear of residence with partially intact deck and outdoor barbeque area. View to the NW.**

A prefabricated storage shed is situated to the immediate east of the driveway at the entrance to the residential area of the property. The shed has a concrete slab foundation, pressed wood siding exterior and a single-entry door of the same material on its south side, and a gable roof with corrugated metal sheeting (Photograph 4). A second ancillary building with an open west wall is situated further north and south of the residence. This ancillary building also has a concrete foundation, pressed wood siding exterior, and a shed roof covered with corrugated metal sheeting (Photograph 5). This building stands next to a concrete slab. Further to the east, at the southeast corner of the orchard area within parcel 128-052-014 is a cylindrical corrugated metal water tank and two adjacent small tanks, all of which appear to be of recent origin (Photograph 6 and Photograph 7). A tennis court/basketball court with a concrete playing surface and perimeter chain link fencing is located in the northwestern area of the property.





Photograph 4. Shed located immediate east of driveway within the property interior, view to the north.



Photograph 5. Storage shed with open wall. View to the southeast.



Photograph 6. Water tank situated at the southeast corner of the APN 128-052-014. View to the southwest.



Photograph 7. Small tanks of recent origin situated near the water tank. View to the northwest.



Photograph 8. Tennis and basketball court at northwest corner of property. View to the northwest.

Page 6 of 9

\*Resource Name or # 1571 East Main Street

Recorded By: Catherine Johnson, PhD, RPA and Josh Bevan, MSHP \*Date: April 24, 2024 ■ Continuation □ Update

#### Isolates

Two fragments of bottle glass were identified in the southeastern corner of the project site north of East Main Street. The fragments included one circular, colorless glass bottle base embossed with the Maywood Glass Company maker's mark, dating the fragment between 1930 and 1959; and one amber glass bottle base embossed with the Owen's Illinois maker's mark dating the fragment between 1954 and present day. The fragments were observed within light brown silty loam surrounded by dried grasses and weeds. No additional cultural resources were identified during the field survey.

#### **B10. Significance (Continued from Page 3):**

##### Santa Maria Historical Context

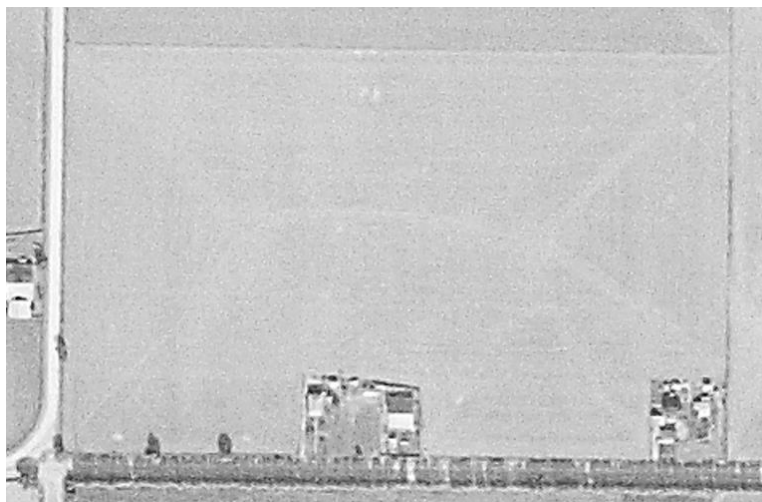
The following historical context is excerpted from the City of Santa Maria's Downtown Specific Plan:

The Santa Maria Valley first attracted European settlers in the late 1700's after the establishment of Mission San Luis Obispo and Mission La Purisima in Lompoc. Many settlers were the recipients of land for settlement from the government, and the area's rich soil available for various agricultural processes continued to attract settlers to the area through the mid 1800's. In the late 1870's, four of the valley's well-known settlers (Rudolph Cook, Isaac Fesler, Isaac Miller, and John Thornburg) each donated a section of their land to be used as the location for a new town known as Grangerville. Today's intersection of Broadway and Main Street marks the corners of these four pieces of land. Grangerville eventually took on the name Central City but was renamed Santa Maria in 1885. Oil exploration began in the valley in the late 1800's. By 1901, William Orcutt and his company, Union Oil, were leasing more than 70,000 acres of land for oil exploration and processing. The discovery of oil led to a population surge that finally resulted in Santa Maria becoming incorporated as a general law city in 1905. At the time of incorporation, the City population was estimated to be 1,000 persons. The first U.S. Census showed that the population more than doubled by the 1910 Census. In the 1950's the near simultaneous construction of U.S. 101, the Twitchell Reservoir, and the Santa Maria River levee were major historic milestone events for Santa Maria. The design of U.S. 101 bypassed the Downtown with a 4-lane highway that skirted down the eastern edge of the City's four-square mile boundary. The road gave travelers four interchanges, but the bypass became detrimental to many downtown businesses. The Reservoir, on the other hand, stabilized the groundwater basin to a point where the aquifer never felt serious damage from saltwater intrusion. Also, the levee prevented most of the flooding in the City and opened up areas to development that were regularly flooded by the Santa Maria River. These engineering marvels opened new land areas for development because they removed natural constraints (access and flooding) to the land located north of the City. In the 1970's, great deliberation and heated discussions led to the Redevelopment of the old Downtown. The U.S. 101 bypass of the City business districts of Main Street and Broadway had started a long decline in the central business districts. As the decline affected local businesses, the Urban Renewal policies of the 1960's enabled the City to form a Redevelopment Agency to work to stop the decline and transform a portion of downtown into an enclosed shopping mall. (City of Santa Maria 2015)

##### Property Development History

As of the 1939, the subject property's site consisted of portions of two farmsteads or similar properties and agricultural land (UCSB 1938, Figure 1). One property was located approximately at the existing location of the driveway entrance on the north side of East Main Street. This property appears to have consisted of a residence and a barn, while only the barn appears to have been situated on land now within the subject property as part of parcel 128-052-014. The other farmstead was slightly smaller and located at the southeast corner of the existing property, at the northeast corner of East Main Street and Navarra Way. This farmstead appears to have consisted of three primary buildings, potentially with additional outbuildings. Review of General Land Office (GLO) records, historical county maps and census records did not confirm ownership of the farmsteads that were present ca. 1938 (GLO 1861, 1873; Ancestry 2024). The farmsteads described above appear to have been vacated by the 1950s and their associated buildings and structures were non-extant by 1967. During the mid-1960s, the present-day parcel 128-052-023 was vacant, while the land within the larger present-day parcel 128-052-014 featured an oval track by 1967 (NETR 2024). The track's origin is unknown, while its oval shape appears to generally align with the area now containing a lawn within the residential property.

**CONTINUATION SHEET**



**Figure 1. Aerial view over future site of subject property, showing a farmstead or similar property in the southeast corner of the present-day property, 1938 (UCSB 1938).**

Dr. Robert Louis Ibsen (1931-2016)

Dr. Robert Ibsen was born in Los Angeles in 1931 and died in 2016 at age 84 (Boston University 2016). He earned a degree in optometry from Southern California College in 1953 and a degree in dentistry from the University of Southern California in 1958 (Dudley Hoffman 2016). Ibsen married Marcia Ricks and the Ibsens settled in Santa Maria, where Dr. Ibsen practiced with Dr. Harold Case for seven years before establishing his own practice. Dr. Ibsen was known as a pioneer in the field of cosmetic dentistry and contributed to the development of over 30 patents during his career, in addition to serving as a Clinical Instructor at USC's School of Dentistry and as a Clinical Lecturer in the Department of Operative Dentistry at Boston University. His obituary notes:

He was awarded 9 Fellowships within the dental profession. He even co-authored the first book on adhesive dentistry and lectured to thousands of dentists around the world. He changed the face of cosmetic dentistry with his products and philosophies, eliminating the need for shots and drilling.

In 1974 he started Den Mat Corporation and hired Richard Glace as his chemist to translate his ideas into materials that solved a myriad of dental needs. What began as a small business with 10 employees in the confines of a house on West Cook Street, DenMat evolved into a business larger than anyone could have dreamed. Fifteen years, four moves and 600 employees later, DenMat became home to Rembrandt Toothpaste, the first ever whitening toothpaste, and began a revolution in the world of dentistry. Rembrandt was purchased in 2004 by Gillette. Never one to sit still, Bob began on his next venture. He shifted his focus from toothpaste to minimally-invasive veneer placement, launching the Lumineers brand. After a long and successful run, the business was sold to a private equity group in 2007. With too much energy to retire at 74, Bob continued teaching and practicing cosmetic dentistry until the very last months of his life (Dudley Hoffman 2016).

Research of city directories identified the addresses 220 W. Cypress Street (ca. 1961 to ca. 1966, appears nonexistent) and a medical-office building at 730 E. Chapel Street (ca. 1967 to ca. 1983, extant) as Ibsen's business addresses in Santa Maria (Ancestry 2024). Research did not identify Ibsen's residence at 1571 East Main Street as a place of professional practice.

Dr. Robert Ibsen appears to have resided in the residence on the subject property between ca. 1974 and his death in 2016. As of this evaluation, the Ibsen-founded DenMat is headquartered in Lompoc, California.

**Evaluation for National Register of Historic Places and California Register of Historical Resources**

1571 East Main Street is recommended ineligible for listing in the National Register of Historic Places (NRHP), California Register of Historic Resources (CRHR) under all evaluative criteria due to a lack of architectural or historical significance.

1571 East Main Street was built in 1974 as a single-family residential property in the eastern region of the City of Santa Maria. Built on land that had contained an oval track by 1967, and as of 1939 two small farmsteads and agricultural land, the existing built environment resources are not associated with these no longer extant and earlier historic-period uses, but rather with a period of continued expansion of the city's limits after post-World War II. During this period, suburbanization became common in urbanized areas of Santa Barbara County, including Santa Maria. Built as the personal residence of prominent dentist Dr. Robert Ibsen and Marcia Ibsen, the property does not appear to be individually significant for having an association with ongoing development or suburbanization in the region in the 1970s. Research did not find that this property is associated with any other historic events of significance. Therefore, 1571 East Main Street is recommended ineligible under Criterion A/1 (Events).

Research into the property's ownership and occupancy found that it was owned and occupied ca. 1974 to ca. 2016 by Dr. Robert Ibsen and Marcia Ibsen. Dr. Ibsen led a career as a prominent and influential practitioner, technology developer, and lecturer in the field of cosmetic dentistry, and based his professional practice and business endeavors in Santa Maria for much of his career. It appears that the subject property was built in 1974, coinciding with Dr. Ibsen's establishment of the DenMat Corporation, which was eventually acquired by several parent corporations. Dr. Ibsen's professional work as a dentist was conducted at several business locations during his career, as well as on multiple university campuses. Although he resided on the subject property during the prime of his career, his places of work where he conducted business are more strongly associated with his contributions to the field of cosmetic dentistry. Therefore, 1571 East Main Street is recommended ineligible under Criterion B/2 (Persons).

Documentation relating to the building's original design and construction and associated design and building professionals was not found, beyond an original building permit listing Ibsen as the general contractor. Although Dr. Ibsen was a successful dentist, his primary profession was not as a general contractor. Research of available historical newspapers failed to identify another contractor or an architect who may have participated in the design and construction of the Ibsen's residence in 1974. Thus, available documentation does not link the building to any builders or designers considered masters in their field. The subject building is representative of a contemporary, vernacular residence of the mid-1970s, but does appear to be an individually distinctive example of its type, period, or method of construction, or to possess high artistic values. The property is relatively large compared to the numerous suburban single-family properties in its immediate vicinity but does not appear to be significant based on its relative size alone. Overall, the property does not rise to level of significance. Therefore, 1571 East Main Street is recommended ineligible under Criterion C (Architecture/Design).

Research does not indicate the property has the potential to yield important information pertaining to prehistory or history under Criteria D (Information Potential). The isolates identified during the field survey were two isolated glass fragments, which have limited data potential and are typically not eligible for listing in the NRHP or CRHR.

City of Santa Maria Historical Landmark

Chapter 8-3 Historical Landmarks of the City of Santa Maria's Municipal authorizes the Recreation and Parks Commission to "receive and act upon applications from any interested persons to investigate and designate places, sites, buildings, structures, works of art and other objects within the incorporated limits of the City as having historic, cultural, aesthetic or other special character or interest, and being worthy of consideration for protection, enhancement or perpetuation as such." (City of Santa Maria 2024). "The Recreation and Parks Commission is further authorized and directed to locate and identify other places, sites, buildings, structures, and works of art as having historical merit which may satisfy the requirements for designation as an historical landmark or which may by the application of other standards, or by reason of a unique feature, have, in the opinion of the Recreation and Parks Commission, special historical, aesthetic or cultural value." Standards for designation and for removal of designation include:

The landmark designated shall have historical, cultural, aesthetic or special character or interest for the general public and not be limited only in interest to a special group of persons, and be at least 50 years of age. (Ord. 88-18 § 5, eff. 10/20/88; Ord. 2001-24, eff. 1/18/02; Ord. 2022-04, eff. 7/7/22)



CONTINUATION SHEET

Page 9 of 9

\*Resource Name or # 1571 East Main Street

Recorded By: Catherine Johnson, PhD, RPA and Josh Bevan, MSHP \*Date: April 24, 2024 ■ Continuation □ Update

The subject property does not appear qualify as a Historical Landmark. As explained above, the property does not appear to possess historical, cultural, aesthetic, or special character or interest. Although approximately 50 years old as of this evaluation, 1571 East Main Street does has not been demonstrated to possess historical or architectural significance.

**B12. References (Continued):**

Ancestry.com

- 2024 Various genealogical databases and primary source documentation related to Dr. Robert Ibsen. Electronic resource. [https://www.ancestry.com/search/?name=robert+\\_ibsen&event=\\_santa+barbara-california-usa\\_2619&count=50](https://www.ancestry.com/search/?name=robert+_ibsen&event=_santa+barbara-california-usa_2619&count=50) (accessed June 2024).

Boston University

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# Appendix D

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Preliminary Drainage Study

**BETHEL ENGINEERING**  
2624 Airpark Drive  
Santa Maria, California 93455  
**(805) 934-5767    FAX (805) 934-3448**

JOB    **Bellecrest Residences**  
PAGE    **1 of 38**  
CALCULATED BY    **GC**    DATE    **2/13/2024**  
CHECKED BY    **RJG**    DATE    **2/13/2024**

# **PRELIMINARY**

## **DRAINAGE STUDY**

for

Bellecrest Residences  
SANTA MARIA, CA  
APN 128-052-014 AND 128-052-023  
February 13, 2024

**Contents**

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## BACKGROUND

The site is currently a single-family residence lot to the north of the site, along with a vacant lot to the south adjacent to E. Main Street totaling 15.23 acres. The address for the currently residences is 1571 E. main Street.

The proposed project consists of 142 individual single family residential lots. The proposed 142 lots consist of 4 typical lot types. One of these types will be condos and 3 will have single family lots. Along with the building the project proposes proposed sidewalks, drive aisles, parking, landscaping, and proposed stormwater management facilities to manage stormwater requirements are proposed on this site. The proposed development will be disturbed 14.50 of the 15.23 acres combined property. (see Vicinity Map, **Appendix C** attached).

**The proposed project is in its preliminary stages with possibilities modifications to the site that will alter the hydrology; therefore, this preliminary report is to show that intent and final project design will be in conformance with the Flood Control Standard Conditions for projects as identified in the 2011 Standard Conditions.**

## EXISTING SITE

The topography of the site is relatively flat. The site overall drains to the northwest of the entire site.

The USDA, Natural Resources Conservation Service and Web Soil Survey, determines that the site consists completely of Sorrento Sandy Loam (StA) and Sorrento Loam (SvA) having no significant clay component (see Appendix B). The definitions in the Stormwater Technical Guide helped determine the site's soil would fit into the HSG A/B (sandy soil). The site is located within an area of minimal flood hazard (see Appendix E).

Existing conditions:

- 1) **Predevelopment Overall** = 14.50 acres  
CN Selected = 85, Natural Western desert, HSG B  
Tc = 30 Mins.

Events for Subcatchment 127S: PRE-DEV				
Event	Rainfall (inches)	Runoff (cfs)	Volume (acre-feet)	Depth
1.40 95th Percentile	1.40	1.35	0.471	0.39
2 YEAR	1.81	2.70	0.796	0.66
5 YEAR	2.62	5.90	1.540	1.27
10 YEAR	3.15	8.21	2.072	1.72
25 YEAR	3.81	11.22	2.765	2.29
50 YEAR	4.29	13.48	3.284	2.72
100 YEAR	<b>4.76</b>	<b>15.71</b>	<b>3.802</b>	<b>3.15</b>

Storm Event	Predeveloped Flows (cfs)	Post-developed Flows (cfs)	Post developed SCM 1-15	
		SCM16		
<b>2-Year</b>	2.70	0.21	<b>0.0</b>	<b>YES</b>
<b>5-Year</b>	5.90	0.46	<b>0.0</b>	<b>YES</b>
<b>10-Year</b>	8.21	0.61	<b>0.0</b>	<b>YES</b>
<b>25-Year</b>	11.22	0.78	<b>0.0</b>	<b>YES</b>
<b>50- Year</b>	13.48	0.90	<b>0.0</b>	<b>YES</b>
<b>100-Year</b>	15.71	1.00	<b>0.0</b>	<b>YES</b>

### Existing conditions

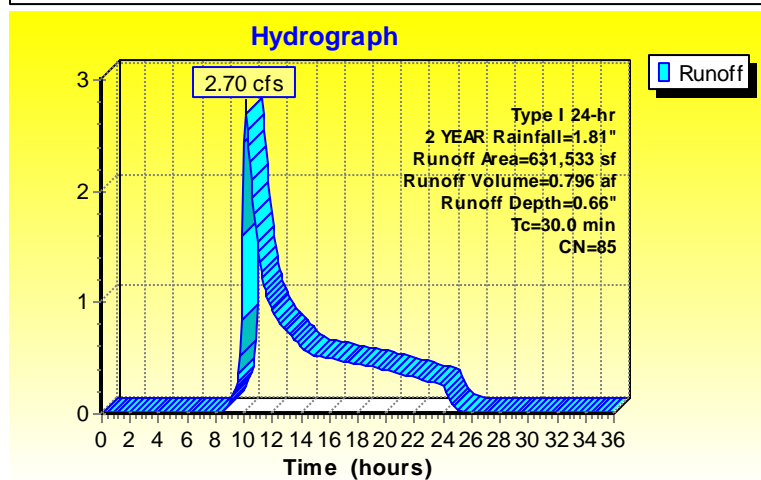
#### Summary for Subcatchment 127S: PRE-DEV

Runoff = 2.70 cfs @ 10.11 hrs, Volume= 0.796 af, Depth= 0.66"

Runoff by SBUH method, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Type I 24-hr 2 YEAR Rainfall=1.81"

Area (sf)	CN	Description
631,533	85	1/8 acre lots, 65% imp, HSG B
221,037		35.00% Pervious Area
410,496		65.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
30.0					Direct Entry,



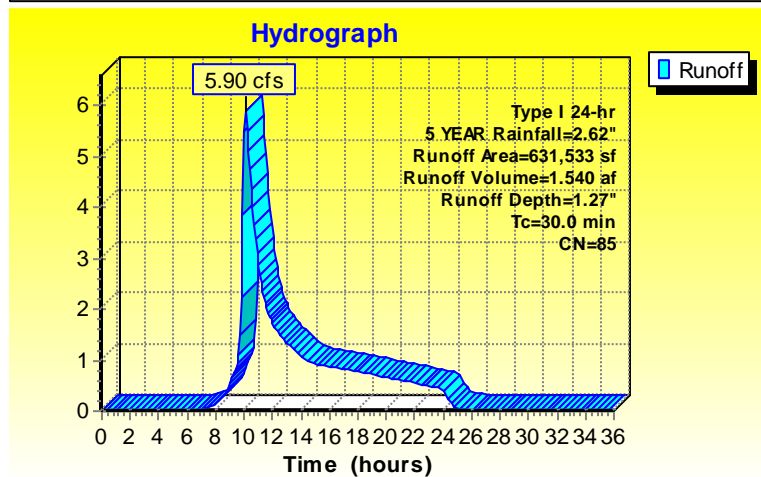
**Summary for Subcatchment 127S: PRE-DEV**

Runoff = 5.90 cfs @ 10.10 hrs, Volume= 1.540 af, Depth= 1.27"

Runoff by SBUH method, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Type I 24-hr 5 YEAR Rainfall=2.62"

Area (sf)	CN	Description
631,533	85	1/8 acre lots, 65% imp, HSG B
221,037		35.00% Pervious Area
410,496		65.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
30.0					Direct Entry,



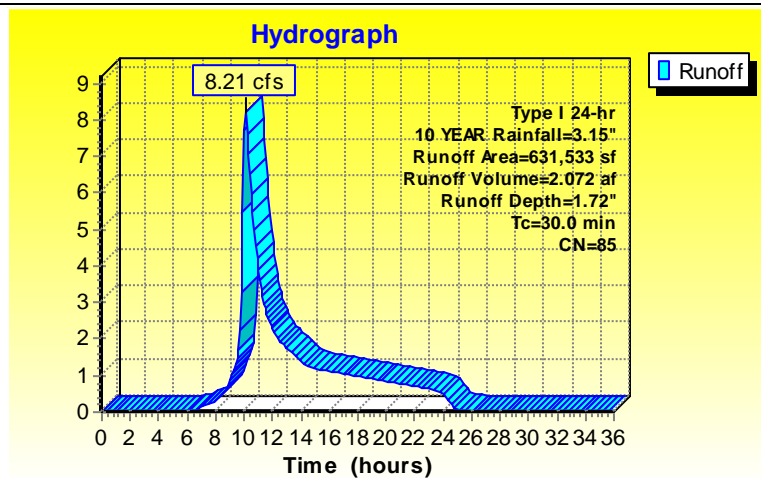
**Summary for Subcatchment 127S: PRE-DEV**

Runoff = 8.21 cfs @ 10.09 hrs, Volume= 2.072 af, Depth= 1.72"

Runoff by SBUH method, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Type I 24-hr 10 YEAR Rainfall=3.15"

Area (sf)	CN	Description
631,533	85	1/8 acre lots, 65% imp, HSG B
221,037		35.00% Pervious Area
410,496		65.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
30.0					Direct Entry,



**Summary for Subcatchment 127S: PRE-DEV**

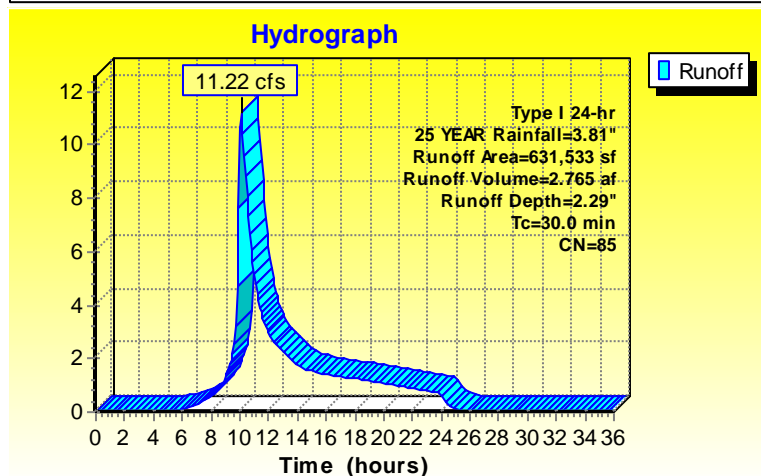
Runoff = 11.22 cfs @ 10.09 hrs, Volume= 2.765 af, Depth= 2.29"

Runoff by SBUH method, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Type I 24-hr 25 YEAR Rainfall=3.81"

Area (sf)	CN	Description
631,533	85	1/8 acre lots, 65% imp, HSG B
221,037		35.00% Pervious Area
410,496		65.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
30.0					Direct Entry,



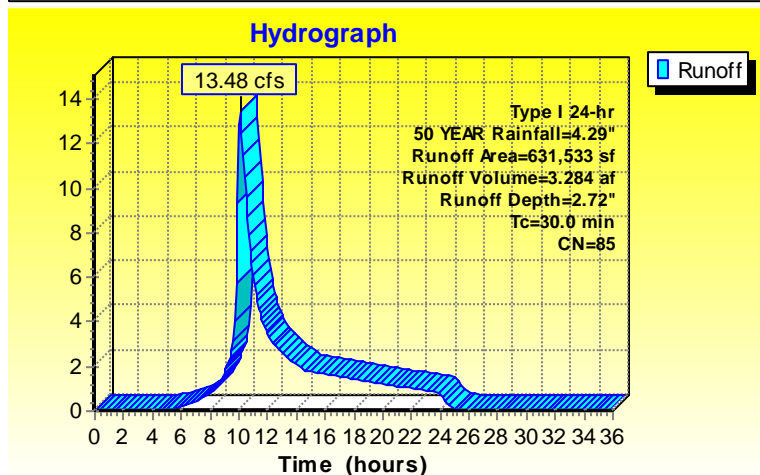
**Summary for Subcatchment 127S: PRE-DEV**

Runoff = 13.48 cfs @ 10.09 hrs, Volume= 3.284 af, Depth= 2.72"

Runoff by SBUH method, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Type I 24-hr 50 YEAR Rainfall=4.29"

Area (sf)	CN	Description
631,533	85	1/8 acre lots, 65% imp, HSG B
221,037		35.00% Pervious Area
410,496		65.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
30.0					Direct Entry,



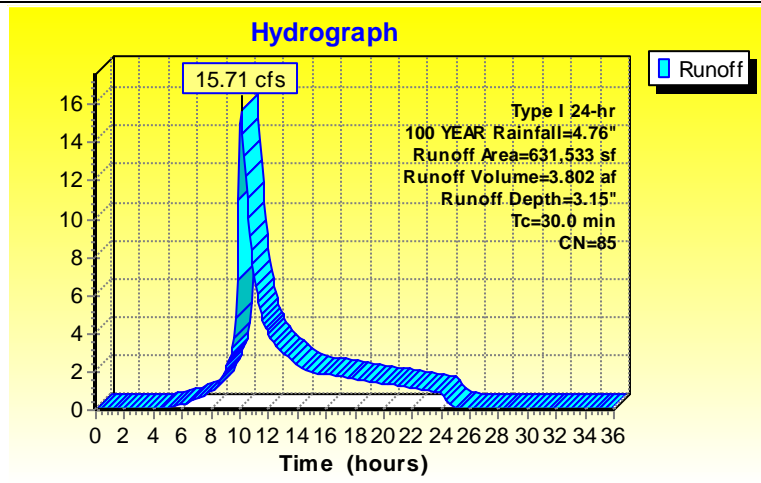
**Summary for Subcatchment 127S: PRE-DEV**

Runoff = 15.71 cfs @ 10.09 hrs, Volume= 3.802 af, Depth= 3.15"

Runoff by SBUH method, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Type I 24-hr 100 YEAR Rainfall=4.76"

Area (sf)	CN	Description
631,533	85	1/8 acre lots, 65% imp, HSG B
221,037		35.00% Pervious Area
410,496		65.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
30.0					Direct Entry,



## PROPOSED BASIN AND UNDERGROUND CHAMBERS DESIGN

### TRIBUTARY AREAS FOR SCM1

The developed on-site tributary areas are defined as follows: DMA 1 (roof and asphalt) will drain towards SCM1. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-1

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM1.

The Developed tributary area flows are as follows:

Area = 13,906 SF = 0.32-acres

### TRIBUTARY AREAS FOR SCM2

The developed on-site tributary areas are defined as follows: DMA 2 (roof and asphalt) will drain towards SCM2. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-2

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM2.

The Developed tributary area flows are as follows:

Area = 13,685 SF = 0.32-acres

### TRIBUTARY AREAS FOR SCM3

The developed on-site tributary areas are defined as follows: DMA 3 (roof and asphalt) will drain towards SCM3. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-3

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM3.

The Developed tributary area flows are as follows:

Area = 13,343 SF = 0.31-acres

### TRIBUTARY AREAS FOR SCM4

The developed on-site tributary areas are defined as follows: DMA 4 (roof and asphalt) will drain towards SCM4. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-4

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM4.

The Developed tributary area flows are as follows:

Area = 14,020 SF = 0.32-acres

### TRIBUTARY AREAS FOR SCM5

The developed on-site tributary areas are defined as follows: DMA 5 (roof and asphalt) will drain towards SCM5. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-5

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM5.

The Developed tributary area flows are as follows:

Area = 13,682 SF = 0.321-acres

### TRIBUTARY AREAS FOR SCM6

The developed on-site tributary areas are defined as follows: DMA 6 (roof and asphalt) will drain towards SCM6. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-6

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM6.

The Developed tributary area flows are as follows:

Area = 7,969 SF = 0.18-acres

#### TRIBUTARY AREAS FOR SCM7

The developed on-site tributary areas are defined as follows: DMA 7 (roof and asphalt) will drain towards SCM7. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-7

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM7.

The Developed tributary area flows are as follows:

Area = 13,750 SF = 0.32-acres

#### TRIBUTARY AREAS FOR SCM8

The developed on-site tributary areas are defined as follows: DMA 8 (roof and asphalt) will drain towards SCM8. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-8

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM8.

The Developed tributary area flows are as follows:

Area = 13,094 SF = 0.30-acres

#### TRIBUTARY AREAS FOR SCM9

The developed on-site tributary areas are defined as follows: DMA 9 (roof and asphalt) will drain towards SCM9. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-9

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM9.

The Developed tributary area flows are as follows:

Area = 11,397 SF = 0.26-acres

#### TRIBUTARY AREAS FOR SCM10

The developed on-site tributary areas are defined as follows: DMA 10 (roof and asphalt) will drain towards SCM10. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff



to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-10

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM10.

The Developed tributary area flows are as follows:

Area = 11,982 SF = 0.28-acres

#### TRIBUTARY AREAS FOR SCM12

The developed on-site tributary areas are defined as follows: DMA 12 (roof and asphalt) will drain towards SCM12. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-12

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM12.

The Developed tributary area flows are as follows:

Area = 10,491 SF = 0.24-acres

#### TRIBUTARY AREAS FOR SCM13

The developed on-site tributary areas are defined as follows: DMA 13 (roof and asphalt) will drain towards SCM13. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-13

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM13.

The Developed tributary area flows are as follows:

Area = 11,001 SF = 0.25-acres

#### TRIBUTARY AREAS FOR SCM14

The developed on-site tributary areas are defined as follows: DMA 14 (roof and asphalt) will drain towards SCM14. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-14

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM14.

The Developed tributary area flows are as follows:

Area = 8,941 SF = 0.21-acres

### TRIBUTARY AREAS FOR SCM15

The developed on-site tributary areas are defined as follows: DMA 15 (roof and asphalt) will drain towards SCM15. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the underground chambers and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-15

This tributary area represents the roofs of several residences . This runoff area will go through downspouts to storm drain pipe that will go directly towards the SCM15.

The Developed tributary area flows are as follows:

Area = 9,078 SF = 0.21-acres

### TRIBUTARY AREAS FOR BASIN RETENTION SCM16

The developed on-site tributary areas are defined as follows: DMA 16 and DMA 17 (roof, concrete, asphalt, and landscape) will drain towards SCM16. The purpose of subdividing the disturbed area into these areas is to calculate the total amount of runoff to the basin and to properly design an adequate outlet that will allow for an outflow that does not exceed the predeveloped flows of the proposed improvement areas.

#### Area DMA-16

This tributary area represents the proposed building's roof, concrete sidewalk and driveways, and asphalt road section. The roof's runoff will go through downspouts to a storm drain pipe directing it away from the building and onto valley gutters which drain into catch basins. The storm drain pipes will direct the runoff to SCM16. The concrete and asphalt surface runoff will also enter the catch basin and will direct it to SCM16 via storm drain pipes.

The Developed tributary area flows are as follows:

Area = 242,989 SF = 5.58-acres

#### Area DMA-17

This tributary area represents the entire proposed landscape. Even though this area is pervious, and the landscape area will mitigate some of the overall runoff high peak storm rain events will runoff to SCM16. This area was accounted for in this analysis.

The Developed tributary area flows are as follows:

Area = 175,144 SF = 4.02-acres

### SUMMARY PRELIMINARY DESIGN FOR EACH SCM

The retention basin and underground chambers are designed to accommodate a 100-year storm while allowing the proposed development runoff to conform to historical drainage patterns. The outflow discharge rates must not exceed predevelopment flows for the 2-year through 10-year storm event and has also been designed to meet Flood Control requirements of allowing runoff of 0.07cfs per acre for a 100-year storm event. Any runoff from the site is designed to flow into the proposed storm drain system that will be routed to the existing storm drain pipes in Main Street.

Underground Chamber (SCM1 to SCM15) receives flows as follows... SCM1 from DMA1, SCM2 from DMA2 and so on. Runoff will be directed to it's respected SCM via storm drain.

Retention basin (SCM 16) receives flows from DMA16, and DMA 17 via sheet flow through storm drain pipes from catch basin. SCM 16 has a 4.6" bleeder orifice below the soil media at a 36"x36" catch basin at a top of grate elevation of 244.00' which then ties into an 18" storm drain pipe which will tie-in to an existing storm drain pipe in Main Street.

Summary of results. See Appendix A for additional information.

Storm Event	Predeveloped Flows (cfs)	Post-developed Flows		TOTAL	
		SCM1-SCM15	SCM16		
<b>2-Year</b>	2.70	0.00	0.21	<b>0.21</b>	<b>YES</b>
<b>5-Year</b>	5.90	0.00	0.46	<b>0.46</b>	<b>YES</b>
<b>10-Year</b>	8.21	0.00	0.61	<b>0.61</b>	<b>YES</b>
<b>25-Year</b>	11.22	0.00	0.78	<b>0.78</b>	<b>YES</b>
<b>50- Year</b>	13.48	0.00	0.90	<b>0.90</b>	<b>YES</b>
<b>100-Year</b>	15.71	0.00	1.00	<b>1.00</b>	<b>YES</b>

#### **APPENDIX A:**

HydroCAD results for: Retention Basins (SCM 16)  
 And Underground Chambers (SCM 1 to SCM 15)  
 100-year rain event only

**Summary for Pond 143P: SCM-1**

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.346 ac, 100.00% Impervious, Inflow Depth = 4.52" for 100 YEAR event  
 Inflow = 0.79 cfs @ 10.00 hrs, Volume= 0.130 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 243.04' @ 29.70 hrs Surf.Area= 1,662 sf Storage= 5,682 cf

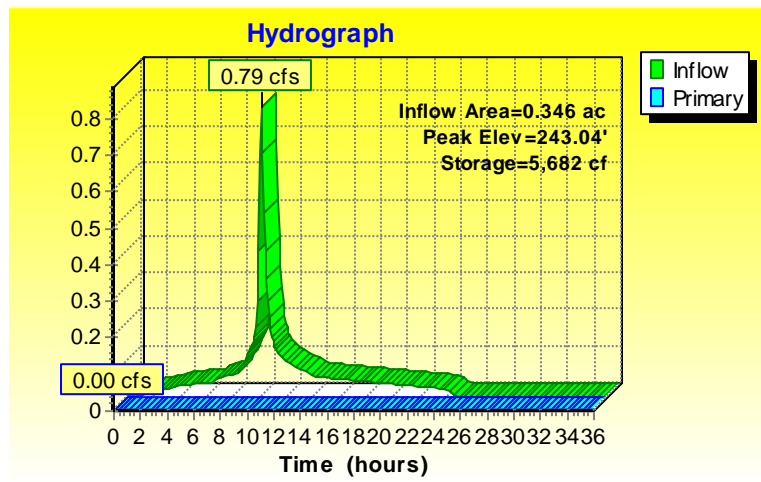
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	237.25'	3,265 cf	<b>22.75'W x 73.06'L x 6.75'H Field A</b> 11,220 cf Overall - 3,058 cf Embedded = 8,162 cf x 40.0% Voids
#2A	239.25'	3,058 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 27 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 27 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		6,323 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	244.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=237.25' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



### Summary for Pond 144P: SCM-2

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.334 ac, 100.00% Impervious, Inflow Depth = 4.52" for 100 YEAR event  
 Inflow = 0.76 cfs @ 10.00 hrs, Volume= 0.126 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 243.85' @ 29.50 hrs Surf.Area= 1,249 sf Storage= 5,484 cf

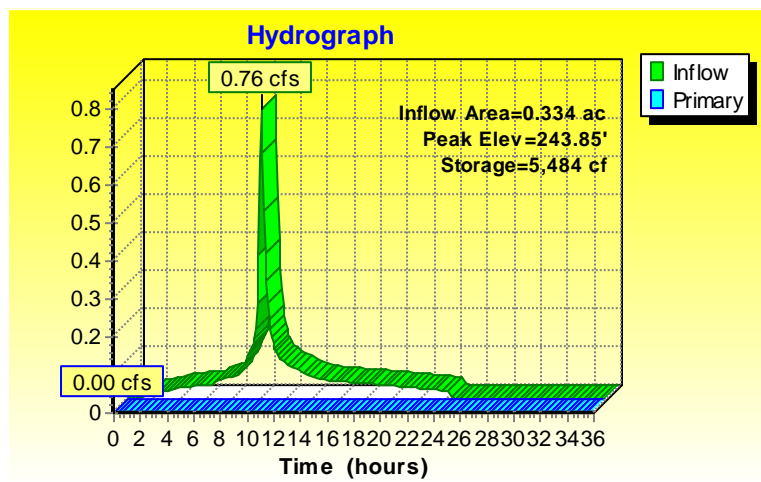
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	235.75'	3,162 cf	<b>22.75'W x 54.89'L x 8.25'H Field A</b> 10,302 cf Overall - 2,398 cf Embedded = 7,904 cf x 40.0% Voids
#2A	239.25'	2,398 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 21 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 21 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		5,560 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	244.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=235.75' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



### Summary for Pond 147P: SCM-3

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.326 ac, 100.00% Impervious, Inflow Depth = 4.52" for 100 YEAR event  
 Inflow = 0.75 cfs @ 10.00 hrs, Volume= 0.123 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 243.59' @ 29.60 hrs Surf.Area= 1,249 sf Storage= 5,356 cf

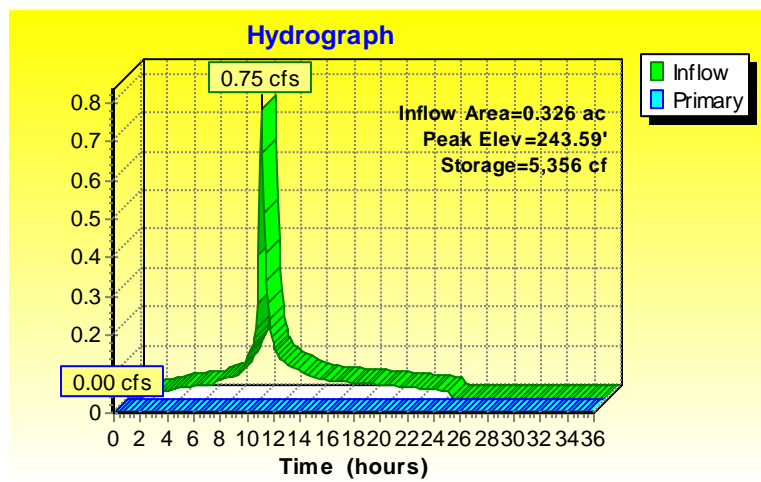
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	235.75'	3,162 cf	<b>22.75'W x 54.89'L x 8.25'H Field A</b> 10,302 cf Overall - 2,398 cf Embedded = 7,904 cf x 40.0% Voids
#2A	239.25'	2,398 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 21 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 21 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		5,560 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	244.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=235.75' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)





**Summary for Pond 148P: SCM-4**

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.342 ac, 100.00% Impervious, Inflow Depth = 4.52" for 100 YEAR event  
 Inflow = 0.78 cfs @ 10.01 hrs, Volume= 0.129 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 243.60' @ 29.60 hrs Surf.Area= 1,249 sf Storage= 5,611 cf

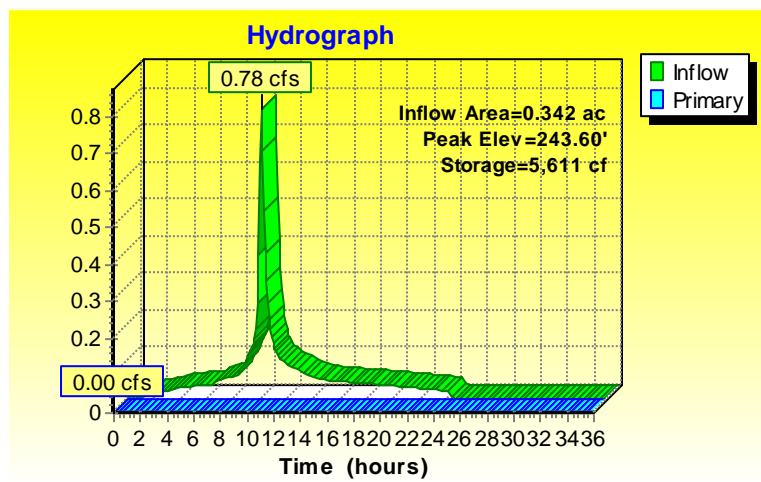
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	235.25'	3,411 cf	<b>22.75'W x 54.89'L x 8.75'H Field A</b> 10,927 cf Overall - 2,398 cf Embedded = 8,528 cf x 40.0% Voids
#2A	239.25'	2,398 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 21 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 21 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		5,810 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	244.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=235.25' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



**Summary for Pond 153P: SCM-5**

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.334 ac, 100.00% Impervious, Inflow Depth = 4.52" for 100 YEAR event  
 Inflow = 0.76 cfs @ 10.00 hrs, Volume= 0.126 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 243.85' @ 29.90 hrs Surf.Area= 1,249 sf Storage= 5,483 cf

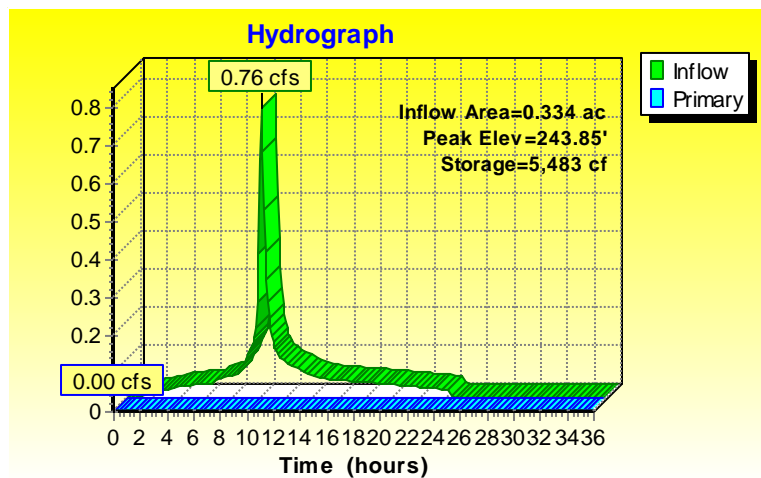
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail. Storage	Storage Description
#1A	235.75'	3,162 cf	<b>22.75'W x 54.89'L x 8.25'H Field A</b> 10,302 cf Overall - 2,398 cf Embedded = 7,904 cf x 40.0% Voids
#2A	239.25'	2,398 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 21 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 21 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		5,560 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	244.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=235.75' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



**Summary for Pond 154P: SCM-6**

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.196 ac, 100.00% Impervious, Inflow Depth = 4.52" for 100 YEAR event  
 Inflow = 0.45 cfs @ 10.00 hrs, Volume= 0.074 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 243.93' @ 29.70 hrs Surf.Area= 828 sf Storage= 3,221 cf

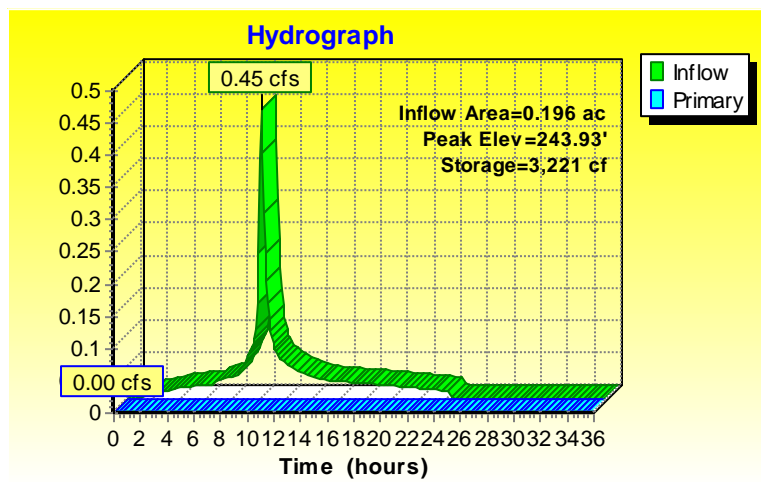
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	236.75'	1,837 cf	<b>22.75'W x 36.38'L x 7.25'H Field A</b> 6,000 cf Overall - 1,409 cf Embedded = 4,592 cf x 40.0% Voids
#2A	239.25'	1,409 cf	<b>ADS StormTech MC-3500 d +Cap x 12 Inside #1</b> Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 12 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		3,245 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	244.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=236.75' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



**Summary for Pond 155P: SCM-7**

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.347 ac, 100.00% Impervious, Inflow Depth = 4.52" for 100 YEAR event  
 Inflow = 0.80 cfs @ 10.00 hrs, Volume= 0.131 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 243.14' @ 29.50 hrs Surf.Area= 1,639 sf Storage= 5,699 cf

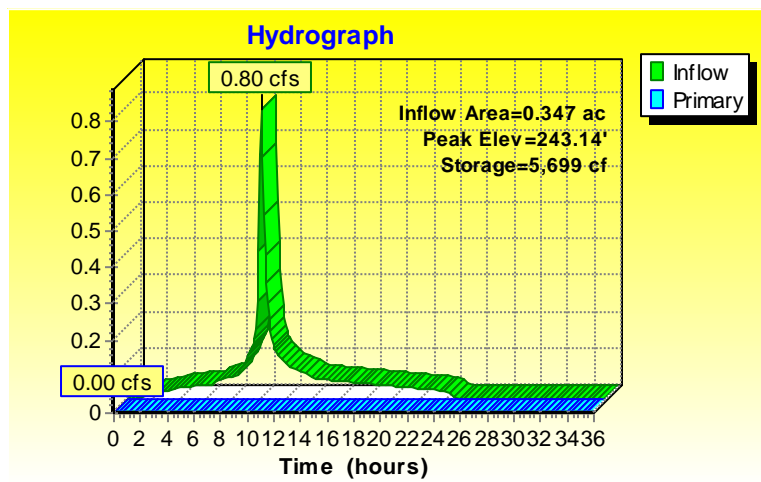
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail. Storage	Storage Description
#1A	237.25'	3,203 cf	<b>22.75'W x 72.06'L x 6.75'H Field A</b> 11,066 cf Overall - 3,058 cf Embedded = 8,008 cf x 40.0% Voids
#2A	239.25'	3,058 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 27 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 27 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		6,261 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	244.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=237.25' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



**Summary for Pond 156P: SCM-8**

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.324 ac, 100.00% Impervious, Inflow Depth = 4.52" for 100 YEAR event  
 Inflow = 0.74 cfs @ 10.00 hrs, Volume= 0.122 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 243.66' @ 29.70 hrs Surf.Area= 1,435 sf Storage= 5,316 cf

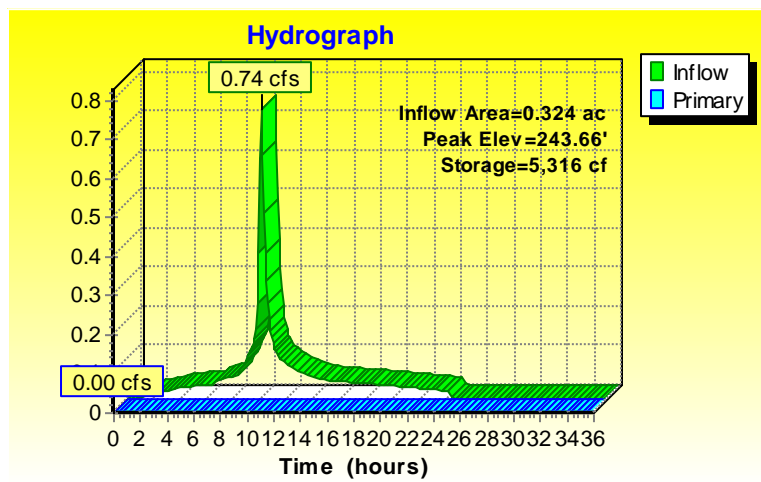
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	237.25'	2,782 cf	<b>22.75'W x 63.06'L x 6.75'H Field A</b> 9,684 cf Overall - 2,728 cf Embedded = 6,955 cf x 40.0% Voids
#2A	239.25'	2,728 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 24 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 24 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
5,510 cf			Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	244.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=237.25' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



### Summary for Pond 158P: SCM-9

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.285 ac, 100.00% Impervious, Inflow Depth = 4.52" for 100 YEAR event  
 Inflow = 0.65 cfs @ 10.00 hrs, Volume= 0.107 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 243.55' @ 29.60 hrs Surf.Area= 1,435 sf Storage= 4,676 cf

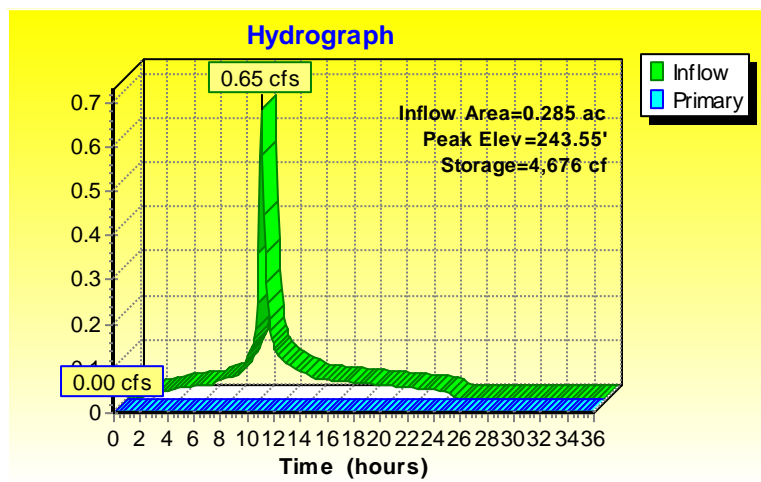
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	238.25'	2,208 cf	<b>22.75'W x 63.06'L x 5.75'H Field A</b> 8,249 cf Overall - 2,728 cf Embedded = 5,521 cf x 40.0% Voids
#2A	239.25'	2,728 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 24 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 24 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
			4,937 cf Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	244.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=238.25' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



### Summary for Pond 143P: SCM-10

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.298 ac, 100.00% Impervious, Inflow Depth > 4.51" for 100 YEAR event  
 Inflow = 0.68 cfs @ 10.00 hrs, Volume= 0.112 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 244.88' @ 24.00 hrs Surf.Area= 1,442 sf Storage= 4,884 cf

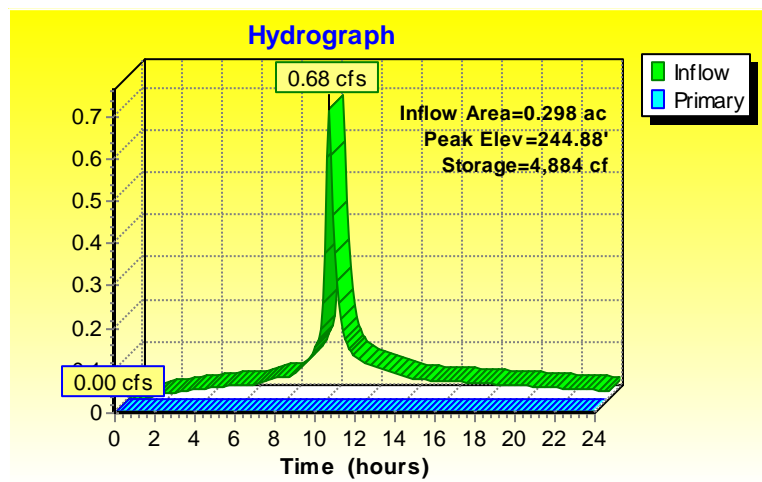
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	239.25'	2,226 cf	<b>22.75'W x 63.39'L x 5.75'H Field A</b> 8,293 cf Overall - 2,728 cf Embedded = 5,564 cf x 40.0% Voids
#2A	240.25'	2,728 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 24 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 24 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		4,954 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	245.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=239.25' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)





**Summary for Pond 144P: SCM-11**

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.296 ac, 100.00% Impervious, Inflow Depth > 4.51" for 100 YEAR event  
 Inflow = 0.68 cfs @ 10.00 hrs, Volume= 0.111 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 244.56' @ 24.00 hrs Surf.Area= 1,249 sf Storage= 4,841 cf

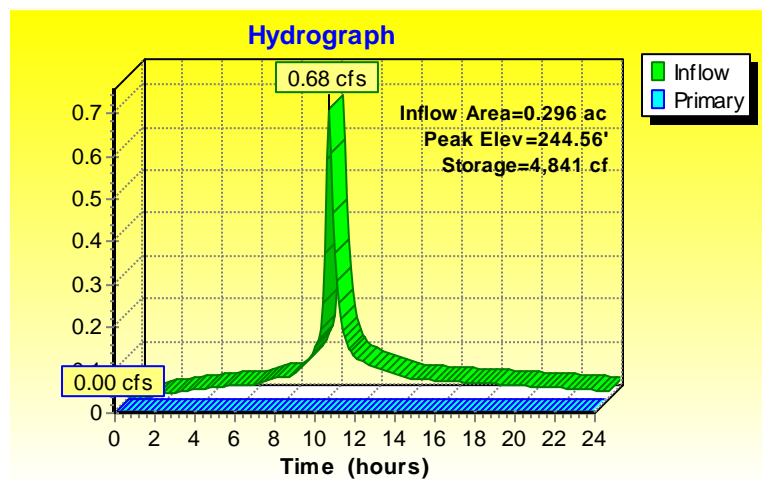
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	237.75'	2,662 cf	<b>22.75'W x 54.89'L x 7.25'H Field A</b> 9,053 cf Overall - 2,398 cf Embedded = 6,655 cf x 40.0% Voids
#2A	240.25'	2,398 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 21 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 21 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		5,060 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	245.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=237.75' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



**Summary for Pond 145P: SCM-12**

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.261 ac, 100.00% Impervious, Inflow Depth > 4.51" for 100 YEAR event  
 Inflow = 0.60 cfs @ 10.00 hrs, Volume= 0.098 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 244.41' @ 24.00 hrs Surf.Area= 1,249 sf Storage= 4,266 cf

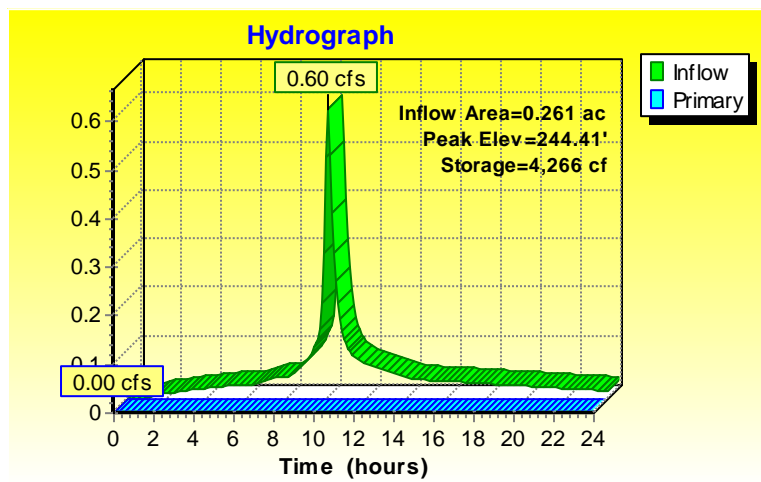
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	238.75'	2,163 cf	<b>22.75'W x 54.89'L x 6.25'H Field A</b> 7,805 cf Overall - 2,398 cf Embedded = 5,406 cf x 40.0% Voids
#2A	240.25'	2,398 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 21 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 21 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		4,561 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	245.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=238.75' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



**Summary for Pond 146P: SCM-13**

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.272 ac, 100.00% Impervious, Inflow Depth > 4.51" for 100 YEAR event  
 Inflow = 0.62 cfs @ 10.00 hrs, Volume= 0.102 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 244.79' @ 24.00 hrs Surf.Area= 1,249 sf Storage= 4,458 cf

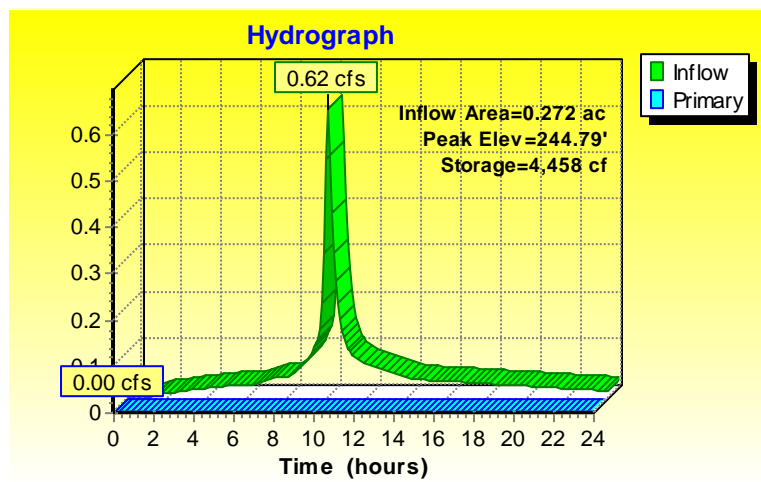
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	238.75'	2,163 cf	<b>22.75'W x 54.89'L x 6.25'H Field A</b> 7,805 cf Overall - 2,398 cf Embedded = 5,406 cf x 40.0% Voids
#2A	240.25'	2,398 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 21 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 21 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		4,561 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	245.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=238.75' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



**Summary for Pond 147P: SCM-14**

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.225 ac, 100.00% Impervious, Inflow Depth > 4.51" for 100 YEAR event  
 Inflow = 0.52 cfs @ 10.00 hrs, Volume= 0.085 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 243.76' @ 24.00 hrs Surf.Area= 1,249 sf Storage= 3,684 cf

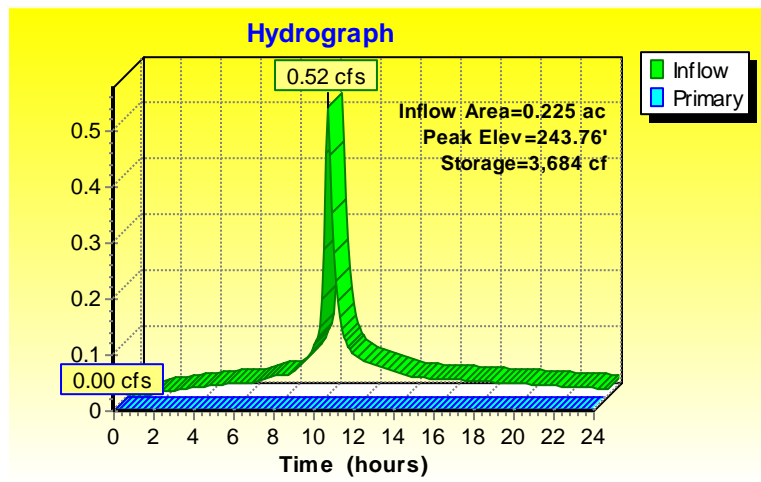
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	239.25'	1,913 cf	<b>22.75'W x 54.89'L x 5.75'H Field A</b> 7,180 cf Overall - 2,398 cf Embedded = 4,782 cf x 40.0% Voids
#2A	240.25'	2,398 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 21 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 21 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		4,311 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	245.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=239.25' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



**Summary for Pond 150P: SCM-15**

[92] Warning: Device #1 is above defined storage

Inflow Area = 0.228 ac, 100.00% Impervious, Inflow Depth > 4.51" for 100 YEAR event  
 Inflow = 0.52 cfs @ 10.00 hrs, Volume= 0.086 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.100000000 hrs  
 Peak Elev= 243.86' @ 24.00 hrs Surf.Area= 1,249 sf Storage= 3,738 cf

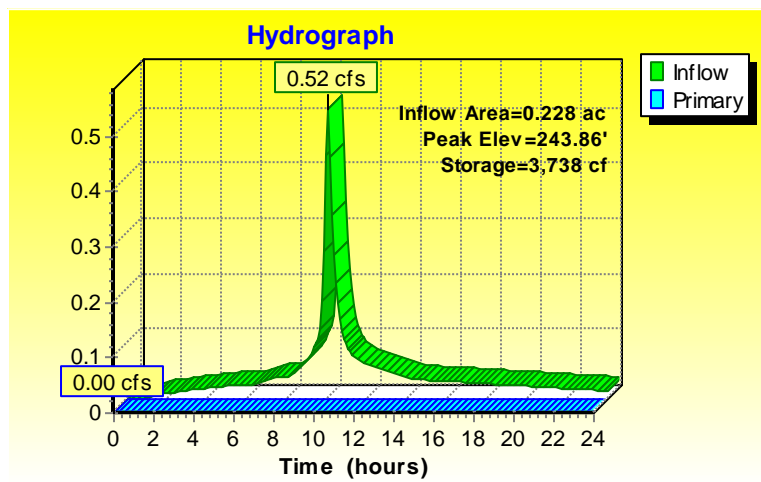
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)  
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1A	239.25'	1,913 cf	<b>22.75'W x 54.89'L x 5.75'H Field A</b> 7,180 cf Overall - 2,398 cf Embedded = 4,782 cf x 40.0% Voids
#2A	240.25'	2,398 cf	<b>ADS StormTech MC-3500 d +Cap</b> x 21 Inside #1 Effective Size= 70.4"W x 45.0"H => 15.33 sf x 7.17'L = 110.0 cf Overall Size= 77.0"W x 45.0"H x 7.50'L with 0.33' Overlap 21 Chambers in 3 Rows Cap Storage= +14.9 cf x 2 x 3 rows = 89.4 cf
		4,311 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	245.00'	<b>24.0" x 24.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=239.25' (Free Discharge)  
 ↑1=Orifice/Grate ( Controls 0.00 cfs)



**Summary for Pond 110P: SCM 16**

Inflow Area = 9.948 ac, 59.58% Impervious, Inflow Depth = 3.19" for 100 YEAR event  
 Inflow = 10.12 cfs @ 10.04 hrs, Volume= 2.646 af  
 Outflow = 1.00 cfs @ 18.06 hrs, Volume= 1.807 af, Atten= 90%, Lag= 481.1 min  
 Primary = 1.00 cfs @ 18.06 hrs, Volume= 1.807 af  
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.100000000 hrs / 2  
 Peak Elev= 243.67' @ 18.06 hrs Surf.Area= 14,338 sf Storage= 70,882 cf

Plug-Flow detention time= 731.2 min calculated for 1.807 af (68% of inflow)  
 Center-of-Mass det. time= 571.2 min ( 1,320.9 - 749.7 )

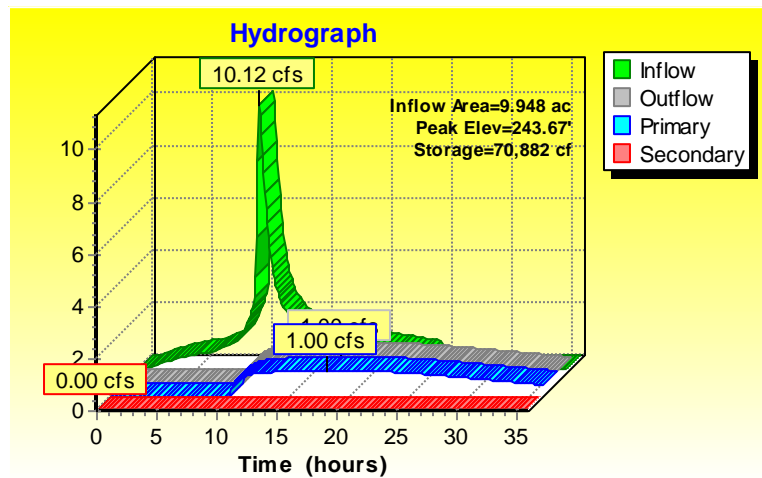
Volume	Invert	Avail.Storage	Storage Description
#1	238.00'	90,491 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
238.00	10,655	0	0
239.00	11,305	10,980	10,980
240.00	11,954	11,630	22,610
241.00	12,603	12,279	34,888
242.00	13,252	12,928	47,816
243.00	13,901	13,577	61,392
244.00	14,551	14,226	75,618
245.00	15,195	14,873	90,491

Device	Routing	Invert	Outlet Devices
#1	Primary	240.25'	<b>4.6" Vert. Orifice/Grate</b> C= 0.600
#2	Secondary	244.00'	<b>36.0" x 36.0" Horiz. Orifice/Grate</b> C= 0.600 Limited to weir flow at low heads

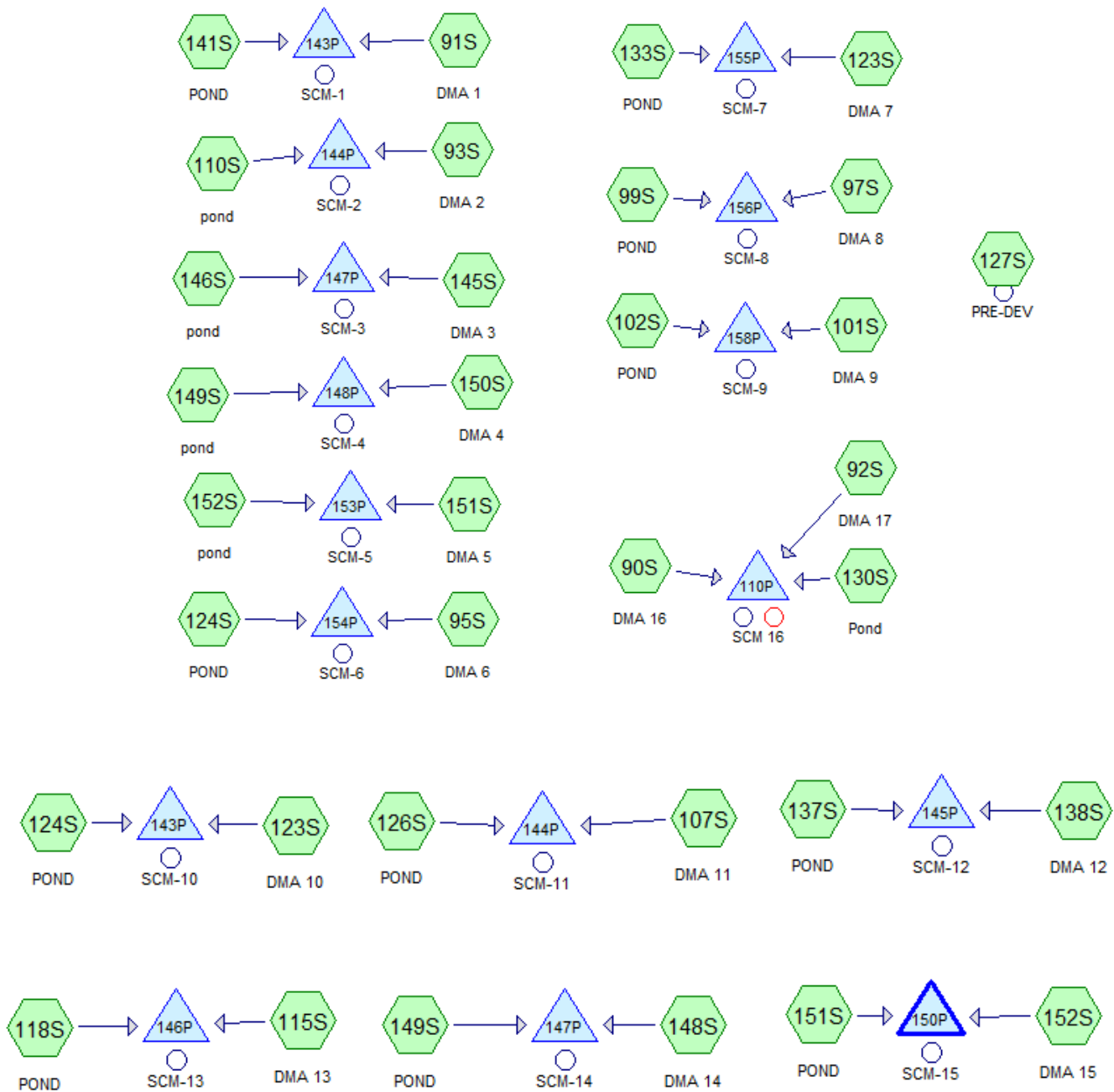
**Primary OutFlow** Max=1.00 cfs @ 18.06 hrs HW=243.67' (Free Discharge)  
 ↑1=Orifice/Grate (Orifice Controls 1.00 cfs @ 8.65 fps)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=238.00' (Free Discharge)  
 ↑2=Orifice/Grate ( Controls 0.00 cfs)



## APPENDIX B

### HydroCAD Routing Diagram





**APPENDIX C**  
**Vicinity Map**





**APPENDIX D**  
 Hydrologic Soil Group and Rating



## MAP LEGEND

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Area of Interest (AOI)	
	Area of Interest (AOI)
	Soil Map Unit Polygons
	Soil Map Unit Lines
	Soil Map Unit Points
Special Point Features	
	Blowout
	Borrow Pit
	Clay Spot
	Closed Depression
	Gravel Pit
	Gravelly Spot
	Landfill
	Lava Flow
	Marsh or swamp
	Mine or Quarry
	Miscellaneous Water
	Perennial Water
	Rock Outcrop
	Saline Spot
	Sandy Spot
	Severely Eroded Spot
	Sinkhole
	Slide or Slip
	Sodic Spot
Water Features	
	Streams and Canals
Transportation	
	Rails
	Interstate Highways
	US Routes
	Major Roads
	Local Roads
Background	
	Aerial Photography

Soil Map—Northern Santa Barbara Area, California

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## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
StA	Sorrento sandy loam, 0 to 2 percent slopes, MLRA 14	13.6	94.1%
SvA	Sorrento loam, 0 to 2 percent slopes, MLRA 14	0.9	5.9%
Totals for Area of Interest		14.5	100.0%

Map Unit Description: Sorrento sandy loam, 0 to 2 percent slopes, MLRA 14—Northern Santa Barbara Area, California

---

## **Northern Santa Barbara Area, California**

### **StA—Sorrento sandy loam, 0 to 2 percent slopes, MLRA 14**

#### **Map Unit Setting**

*National map unit symbol:* 2tyzx  
*Elevation:* 50 to 1,530 feet  
*Mean annual precipitation:* 15 to 20 inches  
*Mean annual air temperature:* 56 to 60 degrees F  
*Frost-free period:* 300 to 360 days  
*Farmland classification:* Prime farmland if irrigated

#### **Map Unit Composition**

*Sorrento and similar soils:* 85 percent  
*Minor components:* 15 percent  
*Estimates are based on observations, descriptions, and transects of the mapunit.*

#### **Description of Sorrento**

##### **Setting**

*Landform:* Flood plains  
*Landform position (two-dimensional):* Toeslope  
*Landform position (three-dimensional):* Talf  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Parent material:* Alluvium derived from sedimentary rock

##### **Typical profile**

*A - 0 to 26 inches:* sandy loam  
*C - 26 to 79 inches:* stratified sandy loam to loam

##### **Properties and qualities**

*Slope:* 0 to 2 percent  
*Depth to restrictive feature:* More than 80 inches  
*Drainage class:* Well drained  
*Runoff class:* Negligible  
*Capacity of the most limiting layer to transmit water (Ksat):* Moderately high to high (0.60 to 2.00 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Calcium carbonate, maximum content:* 10 percent  
*Maximum salinity:* Nonsaline to very slightly saline (0.0 to 2.0 mmhos/cm)  
*Available water supply, 0 to 60 inches:* Moderate (about 8.7 inches)

##### **Interpretive groups**

*Land capability classification (irrigated):* 1  
*Land capability classification (nonirrigated):* 3c  
*Hydrologic Soil Group:* B



Map Unit Description: Sorrento sandy loam, 0 to 2 percent slopes, MLRA 14—Northern Santa Barbara Area, California

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*Ecological site:* R014XG906CA - Dry Loamy Bottom  
*Hydric soil rating:* No

#### **Minor Components**

##### **Sorrento, loam**

*Percent of map unit:* 5 percent  
*Landform:* Flood plains  
*Landform position (two-dimensional):* Toeslope  
*Landform position (three-dimensional):* Talf  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Hydric soil rating:* No

##### **Mocho**

*Percent of map unit:* 5 percent  
*Landform:* Alluvial fans, flood plains  
*Landform position (two-dimensional):* Toeslope  
*Landform position (three-dimensional):* Tread, talf  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Hydric soil rating:* No

##### **Metz**

*Percent of map unit:* 5 percent  
*Landform:* Alluvial fans, flood plains  
*Landform position (two-dimensional):* Footslope, toeslope  
*Landform position (three-dimensional):* Talf  
*Down-slope shape:* Linear  
*Across-slope shape:* Linear  
*Hydric soil rating:* No

#### **Data Source Information**

Soil Survey Area: Northern Santa Barbara Area, California  
Survey Area Data: Version 16, Sep 9, 2021



**APPENDIX E**  
FEMA's National Flood Hazard Map

**National Flood Hazard Layer FIRMette**



**Legend**

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

<b>SPECIAL FLOOD HAZARD AREAS</b>	Without Base Flood Elevation (BFE) Zone A, V, AE, AH, VE, AR
	With BFE or Depth Zone AE, AO, AH, VE, AR
	Regulatory Floodway
<b>OTHER AREAS OF FLOOD HAZARD</b>	0.2% Annual chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile. Zone X
	Future Conditions 1% Annual chance Flood Hazard Zone X
	Area with Reduced Flood Risk due to Levee. See Notes, Zone X
	Area with Flood Risk due to Levee Zone D
<b>OTHER AREAS</b>	NO SCREEN Area of Minimal Flood Hazard Zone X
	Effective LOMRs
	Area of Undetermined Flood Hazard Zone D
<b>GENERAL STRUCTURES</b>	channel, culvert, or Storm Sewer
	Levee, Dike, or Floodwall
<b>CROSS SECTIONS</b>	20.2 Cross Sections with 1% Annual chance Water Surface Elevation
	17.6 Coastal Tract
	Base Flood Elevation Line (BFE)
	Limit of Study
	Jurisdiction Boundary
<b>OTHER FEATURES</b>	Coastal Tract Baseline
	Profile Baseline
	Hydrographic Feature
<b>MAP PANELS</b>	Digital Data Available
	No Digital Data Available
	Unmapped

The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 2/13/2024 at 4:54 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



APPENDIX F  
Drainage Map/ Post Developed map

BELLECREST RESIDENCES  
EXHIBIT 1: WATER QUALITY  
A.P.N. 128-052-014,  
128-052-023



LEGEND

DMA	AREA (SF)	DRAINS	DRAINS TO BASIN
1	13,906	ROOF	SCM1
2	13,685	ROOF	SCM2
3	13,343	ROOF	SCM3
4	14,020	ROOF	SCM4
5	13,682	ROOF	SCM5
6	7,969	ROOF	SCM6
7	13,750	ROOF	SCM7
8	13,094	ROOF	SCM8
9	11,397	ROOF	SCM9
10	11,982	ROOF	SCM10
11	12,021	ROOF	SCM11
12	10,491	ROOF	SCM12
13	11,001	ROOF	SCM13
14	8,941	ROOF	SCM14
15	9,078	ROOF	SCM15
16	242,989	ROOF/ROAD/CONC	SCM16
17	175,144	LANDSCAPE	SCM16
SCM1	1,168		
SCM2	864		
SCM3	864		
SCM4	864		
SCM5	864		
SCM6	576		
SCM7	7,286		
SCM8	1,008		
SCM9	1,008		
SCM10	1,016		
SCM11	864		
SCM12	864		
SCM13	864		
SCM14	864		
SCM15	871		
SCM16	15,195		
TOTAL	631,533		

NOTE: DRAWING NOT TO SCALE



2624 Airpark Dr., Santa Maria,  
California 93455 (805) 934-5767

# Appendix E

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Acoustical Analysis

**ACOUSTICAL ANALYSIS**

**1571 E. MAIN STREET RESIDENTIAL DEVELOPMENT  
SANTA MARIA, CALIFORNIA**

**WJVA Project No. 22-34**

**PREPARED FOR**

**COASTAL COMMUNITY BUILDERS  
330 JAMES WAY, SUITE 270  
SANTA MARIA, CALIFORNIA 93449**

**PREPARED BY**

**WJV ACOUSTICS, INC.  
VISALIA, CALIFORNIA**



**wjv acoustics**

**OCTOBER 11, 2023**

## INTRODUCTION

The project consists of a proposed senior residential development, to include 142 total units, including duplex units and cottage units, totaling 232 bedrooms. The overall project site consists of approximately 15.23 acres of land. The project is located at 1571 East Main Street, in Santa Maria.

The main access to the project site is from Main Street, via a gated entry point. Emergency access for the duplexes is through Spruce Drive. The project will also include a common use clubhouse area, with a pool, BBQ area, and an outdoor activity lawn area.

The City of Santa Maria has requested an acoustical analysis to assess project site noise exposure and determine if noise mitigation measures should be incorporated into the project design. This analysis, prepared by WJV Acoustics, Inc. (WJVA), is based upon a site visit and noise measurements conducted on April 29, 2022 and the project site plan prepared by EHD Studio, Inc. (dated 8/4/23).

Appendix A provides definitions of the acoustical terminology used in this report. Unless otherwise stated, all sound levels reported in this analysis are A-weighted sound pressure levels in decibels (dB). A-weighting de-emphasizes the very low and very high frequencies of sound in a manner similar to the human ear. Most community noise standards utilize A-weighted sound levels, as they correlate well with public reaction to noise. Appendix B provides typical A-weighted sound levels for common noise sources.

In terms of human perception, a 5 dB increase or decrease is considered to be a noticeable change in noise levels. Additionally, a 10 dB increase or decrease is perceived by the human ear as half as loud or twice as loud. In terms of perception, generally speaking the human ear cannot perceive an increase (or decrease) in noise levels less than 3 dB.



## **CRITERIA FOR ACCEPTABLE NOISE EXPOSURE**

The City of Santa Maria Noise Element of the General Plan establishes noise level criteria in terms of the CNEL metric. The CNEL (Community Noise Equivalent Level) is the time-weighted energy average noise level for a 24-hour day, with penalties of approximately 5 dB added to noise levels occurring during the evening hours (7:00 p.m.-10:00 p.m.) and 10 dB added to noise levels occurring during the nighttime hours (10:00 p.m.-7:00 a.m.). The CNEL represents cumulative exposure to noise over an extended period of time, and is therefore calculated based upon *annual average* conditions.

The Noise Element establishes a land use compatibility criterion of 60 dB CNEL for exterior noise exposure in outdoor activity areas of new residential developments. Outdoor activity areas generally include backyards of single-family residences and individual patios or balconies of multi-family developments. The intent of the exterior noise level requirement is to provide an acceptable noise environment for outdoor activities and recreation. The General Plan does provide an exception for patios and balconies of multi-family residential developments, allowing an exterior noise level up to 75 dB CNEL within individual unit patios and balconies.

The Noise Element also requires that interior noise exposure attributable to exterior noise sources not exceed 45 dB CNEL. The intent of the interior noise level standard is to provide an acceptable noise environment for indoor communication and sleep. Table I provides the City of Santa Maria exterior and interior noise level compatibility standards for specific land use designations.

<p style="text-align: center;"><b>TABLE I</b></p> <p style="text-align: center;"><b>CITY OF SANTA MARIA INTERIOR AND EXTERIOR NOISE STANDARDS</b></p> <p style="text-align: center;"><b>CITY OF SANTA MARIA GENERAL PLAN</b></p>			
Land Use Categories		Standard (dB, CNEL)	
Categories	Uses	Interior	Exterior
Residential	Single Family, Duplex, Multiple Family, Mobile Home	45	60 <sup>4</sup>
Commercial	Retail, Restaurant, Professional Offices	55	65 <sup>1,2</sup>
Industrial	Manufacturing, Utilities, Warehousing, Agriculture	65	70 <sup>3</sup>
Noise-Sensitive Land Uses	Motel, Hospital, School, Nursing Home, Church, Library	45	60
Open Space	Passive Outdoor Recreation		65

1 The Commercial Exterior Noise Standard is a noise level of 65 dB CNEL or less, or which does not interfere with normal business activity

2 Where commercial development proposes outside activities such as patio dining, outside play and picnic areas, the noise standards shall not apply to those outdoor areas.

3. The Industrial Exterior Noise Standard is a noise level of 70 dB CNEL or less or which does not interfere with normal business activity.

4. Exception to allow elevated noise levels in outdoor living areas. Outdoor living areas such as patios and balconies may be incorporated into multifamily development projects ("Duplex" and "Multiple Family", and mixed-use projects which incorporate these uses) in areas which experience elevated noise levels. These noise levels may not exceed the "Normally Unacceptable" Community Noise Exposure levels (75 dB and above) specified in Figure 2 of the "Noise Element Guidelines" (Appendix C of the California General Plan Guidelines). Furthermore, prospective buyers and future occupants of dwellings shall be provided the following notice:

This property is presently located in an urban area which periodically and regularly experiences elevated noise levels. Potential sources of this noise may be automobile traffic, railroad operations, flying aircraft, industrial/commercial uses and general human activity in an urban environment. You may wish to consider what noise level annoyances, if any, are associated with the property before you complete your purchase and/or rental agreement and determine whether they are acceptable to you.

Source: City of Santa Maria General Plan

The Santa Maria Noise Ordinance (Chapter 5, Sections 5-5.04 and 5-5.05) establishes noise level standards for noise sources that are *not* exempted from local control due to existing state or federal legislation. This includes noise produced by existing and potential commercial activities and vehicle movements off a public roadway. The noise ordinance standards are based upon the statistical distribution of noise over time, allow for progressively shorter exposure to noise levels of increasing magnitude, and are more restrictive during the nighttime hours. The noise ordinance standards for residential zones are summarized in Table II.

Section 5-5.10a of the City's noise ordinance states that the intent of the ordinance is *not* to enforce against the existing ambient or composite noise in any given area. However, it is reasonable to apply the ambient base levels of the ordinance to the design of appropriate noise mitigation measures for new noise-producing uses that are proposed for location near existing or planned noise-sensitive receptors.



**TABLE II**  
**SANTA MARIA NOISE ORDINANCE STANDARDS**  
**AMBIENT BASE LEVELS - RESIDENTIAL ZONES<sup>1</sup>**

Time of Day	Cumulative Exposure (minutes/hour) <sup>2</sup>				
	30 (L <sub>50</sub> )	15 (L <sub>25</sub> )	5 (L <sub>8.3</sub> )	1 (L <sub>1.7</sub> )	0 (L <sub>Max</sub> )
Day (7a-10p)	55 dBA	60 dBA	65 dBA	70 dBA	75 dBA
Night (10p-7a)	45 dBA	50 dBA	55 dBA	60 dBA	65 dBA

<sup>1</sup>The noise level standards represented by this table are the “ambient base levels” shown by the City’s noise ordinance for residential zones. Potential violations of the ordinance occur when noise levels from the source of concern exceed the ambient noise level *or* the ambient base level, *whichever is higher*.

<sup>2</sup>In layman’s terms, the noise level standards shown may not be exceeded for more than the specified number of minutes within any one-hour time period. The L<sub>n</sub> value shown in parenthesis indicates the percent of the time during an hour that a particular noise level may not be exceeded. For example, the L<sub>50</sub> represents 50% of the hour, or 30 minutes.

Source: City of Santa Maria as interpreted by WJVA

## **PROJECT SITE NOISE EXPOSURE**

The project site is located at 1571 E. Main Street, along the north side of Main Street and east of N. Suey Road, in Santa Maria. The project site currently consists of one single-family residence, landscaped vegetation and undeveloped land. The project site is bordered to the north, west and east by existing residential land uses, and to the north by E. Main Street and agricultural lands. Additionally, Pioneer Valley High School is located northwest of the project site. The dominant sources of noise affecting the project site is vehicle traffic along E. Main Street. Other sources of noise observed during a project site visit include noise associated with nearby agricultural operations as well as occasional aircraft overflights.

### **AMBIENT NOISE SURVEY-**

Measurements of existing ambient noise levels in the project vicinity were conducted on April 29, 2022. Long-term (24-hour) ambient noise level measurements were conducted at one (1) location (site LT-1). Ambient noise levels were measured for a period of 24 continuous hours at site LT-1. Site LT-1 was located within the project site, approximately 75 feet from the centerline of E. Main Street. The noise monitor measured noise from all sources impacting the project site, for a continuous period of 24 hours. The location of 24-hour ambient noise measurement site LT-1 is provided on Figure 2.

Measured hourly energy average noise levels ( $L_{eq}$ ) at site LT-1 ranged from a low of 54.0 dB between 3:00 a.m. and 4:00 a.m. to a high of 66.4 dBA between 2:00 p.m. and 3:00 p.m. Hourly maximum ( $L_{max}$ ) noise levels at site LT-1 ranged from 72.1 to 93.2 dBA. Residual noise levels at the monitoring site, as defined by the  $L_{90}$ , ranged from 44.9 to 56.3 dBA. The  $L_{90}$  is a statistical descriptor that defines the noise level exceeded 90% of the time during each hour of the sample period. The  $L_{90}$  is generally considered to represent the residual (or background) noise level in the absence of identifiable single noise events from traffic, aircraft and other local noise sources. The measured 24-hour CNEL value at site LT-1 was 66.7 dB CNEL. Figure 3 graphically depicts hourly variations in ambient noise levels at site LT-1. Figure 4 provides a photograph of measurement site LT-1.

### **TRAFFIC NOISE EXPOSURE-**

The project site is exposed to traffic noise associated with vehicles along E. Main Street. The closest proposed residential setbacks to E. Main Street (units 1-12) are located at approximately 100 feet from the centerline of E. Main Street. Noise exposure from traffic on E. Main Street was calculated for existing conditions using the FHWA Traffic Noise Model and traffic data obtained from the City of Santa Maria.

WJVA utilized the Federal Highway Administration (FHWA) Highway Traffic Noise Prediction Model (FHWA-RD-77-108). The FHWA Model is a standard analytical method used for roadway traffic noise calculations. The model is based upon reference energy emission levels for automobiles, medium trucks (2 axles) and heavy trucks (3 or more axles), with consideration given to vehicle volume, speed, roadway configuration, distance to the receiver, and the

acoustical characteristics of the site. The FHWA Model was developed to predict hourly  $L_{eq}$  values for free-flowing traffic conditions, and is generally considered to be accurate within  $\pm 1.5$  dB. To predict CNEL values, it is necessary to determine the hourly distribution of traffic for a typical day and adjust the traffic volume input data to yield an equivalent hourly traffic volume.

Noise level measurements and concurrent traffic counts were conducted by WJVA staff within the project site on April 29, 2022. The purpose of the measurements was to evaluate the accuracy of the FHWA Model in describing traffic noise exposure within the project site. The measurement site was located adjacent to the project site at a distance of approximately 75 feet from the centerline of E. Main Street (approximate distance of the closest residential setbacks to the roadway). The speed limit posted in the project vicinity was 45 mph (miles per hour). The project vicinity and noise monitoring site location are provided as Figure 2. A photograph showing the E. Main Street noise measurement site is provided as Figure 3.

Noise monitoring equipment consisted of Larson-Davis Laboratories Model LDL-820 sound level analyzer equipped with a B&K Type 4176 1/2" microphone. The equipment complies with the specifications of the American National Standards Institute (ANSI) for Type I (Precision) sound level meters. The meter was calibrated in the field prior to use with a B&K Type 4230 acoustic calibrator to ensure the accuracy of the measurements. The microphone was located on a tripod at 5 feet above the ground.

Noise measurements were conducted in terms of the equivalent energy sound level ( $L_{eq}$ ). Measured  $L_{eq}$  values were compared to  $L_{eq}$  values calculated (predicted) by the FHWA Model using as inputs the traffic volumes, truck mix and vehicle speed observed during the noise measurements. The results of the comparison are shown in Table III.

<p><b>TABLE III</b></p> <p><b>COMPARISON OF MEASURED AND PREDICTED</b></p> <p><b>(FHWA MODEL) NOISE LEVELS</b></p> <p><b>1571 E. MAIN STREET RESIDENTIAL DEVELOPMENT, SANTA MARIA</b></p>	
	<b>E. Main Street</b>
Measurement Start Time	11:45 a.m.
Observed # Autos/Hr.	180
Observed # Medium Trucks/Hr.	36
Observed # Heavy Trucks/Hr.	0
Observed Speed (MPH)	45
Distance, ft. (from center of roadway)	80
$L_{eq}$ , dBA (Measured)	58.6
$L_{eq}$ , dBA (Predicted)	59.4
<b>Difference between Predicted and Measured <math>L_{eq}</math>, dBA</b>	<b>0.8</b>
<p>Note: FHWA "soft" site assumed for calculations.</p> <p>Source: WJV Acoustics, Inc.</p>	

From Table III it may be determined that the traffic noise levels predicted by the FHWA Model were 0.8 dB higher than those measured for the conditions observed at the time of the noise measurements for E. Main Street. This is considered to be reasonable agreement with the model and therefore no adjustments to the model are necessary. The slight overprediction of the model when compared to measured noise levels is likely the result of occasional traffic speeds below 45 mph, as there is an existing signalized intersection at N. Suey Road.

Annual Average Daily Traffic (AADT) data and the day/evening/night distribution of traffic for E. Main Street in the project vicinity was obtained from the City of Santa Maria. Truck percentages were estimated by WJVA, based upon project-site observations and previous studies prepared along similar roadways. A speed limit of 45 mph was applied for the traffic noise model calculations. Table IV summarizes annual average traffic data used to model noise exposure within the project site.

TABLE IV	
TRAFFIC NOISE MODELING ASSUMPTIONS	
1571 E. MAIN STREET RESIDENTIAL DEVELOPMENT, SANTA MARIA	
	E. Main Street
	Existing
Annual Avenue Daily Traffic (AADT)	6,399
Day/Evening/Night Split (%)	80/8/12
Assumed Vehicle Speed (mph)	45
% Medium Trucks (% AADT)	14
% Heavy Trucks (% AADT)	3
Sources: City of Santa Maria WJV Acoustics, Inc.	

Using data from Table IV, the FHWA Model, annual average traffic noise exposure was calculated for the closest proposed backyards from E. Main Street (approximately 100 feet from the roadway centerline). The calculated noise exposures for existing traffic conditions for the closest proposed setbacks to E. Main Street was approximately 63 dB CNEL. It should be noted, this calculated project site noise exposure is comparable to the 24-hour CNEL noise exposure level measured at ambient noise measurement site LT-1, when adjusted for distance to the roadway.

The City of Santa Maria exterior noise level standard is 60 dB CNEL, in outdoor activity areas of residential land uses. Outdoor activity areas generally include backyards of single-family residences (as well as duplex and cottage units) and individual patios or balconies of multi-family developments. The General Plan does provide an exception for patios and balconies of multi-family residential developments, allowing an exterior noise level up to 75 dB CNEL within individual unit patios and balconies.

The outdoor activity areas for units 1-12 face Main Street, and would not be acoustically shielded by the any buildings. Noise exposure levels within these backyards would be approximately 63

dB CNEL, and exterior noise mitigation must be included in project design. In regards to exterior noise levels at the common use clubhouse area, pool, BBQ area, and outdoor activity lawn areas, traffic noise exposure at these areas would be approximately 57 dB CNEL, and would not exceed the City's exterior noise level standard. Exterior noise levels within the backyards of Lots 1-12 represent the only proposed project areas at which exterior noise levels would be expected to exceed the City's 60 dB CNEL exterior noise level standard, and mitigation must be incorporated for these units.

#### **EXTERIOR NOISE MITIGATION-**

The City of Santa Maria establishes a 60 dB CNEL exterior noise criterion within outdoor activity areas (backyards) of single-family homes (including duplex and cottage units). The project site traffic noise exposure was calculated to be approximately 63 dB CNEL at the closest proposed residential setbacks to Main Street. Such levels exceed the City's applicable exterior noise level standards, and additional mitigation should be considered.

To mitigate exterior traffic noise exposure along E. Main Street it will be necessary to construct a sound wall along the roadway. The sound wall will provide acoustical shielding of backyards located closest to E. Main Street (Units 1-12).

A sound wall insertion loss program based on the FHWA Model was used to calculate the insertion loss (noise reduction) provided by the proposed sound walls. The model calculates the insertion loss of a wall of given height based on the effective height of the noise source, height of the receiver, distance from the receiver to the wall, and distance from the noise source to the wall. The standard assumptions used in the sound wall calculations are effective source heights of 8, 2 and 0 feet above the roadway for heavy trucks, medium trucks and automobiles, respectively. The standard height of a residential receiver is five feet above the ground elevation. For the purpose of this analysis, it was assumed that project site elevation would be comparable to the elevation of Main Street.

Based upon the above-described assumptions and method of analysis, the noise level insertion loss values for sound walls of various heights were calculated. The calculations indicated that a sound wall along the rear lot lines of units 1-12, constructed to a minimum height of six (6) feet above project site grade would result in exterior noise levels of approximately 58 dB CNEL within the closest proposed backyards to E. Main Street. In order for the sound wall to effectively shield backyards the sound walls will need to be turned inward (northward), for a minimum of twenty (20) feet at the backyards of Unit 1 (west side of backyard) and Unit 12 (east side of backyard).

With the incorporation of the above-described sound wall, the projected exterior noise exposure at the closest proposed setbacks along E. Main Street will comply with the City's 60 dB CNEL exterior noise standard within individual backyards of Units 1-12. It should be noted, the sound wall would be effective at first-floor elevation receivers only. The location of the required sound wall is provided on Figure 1.

### **INTERIOR NOISE EXPOSURE-**

The City of Santa Maria interior noise level standard is 45 dB CNEL. The worst-case exterior noise exposure within the proposed residential development would be approximately 63 dB CNEL. This means that the proposed residential construction must be capable of providing a minimum outdoor-to-indoor noise level reduction (NLR) of approximately 17 dB (63-45=17).

A specific analysis of interior noise levels was not performed. However, it may be assumed that residential construction methods complying with current building code requirements will reduce exterior noise levels by approximately 25 dB if windows and doors are closed. This will be sufficient for compliance with the City's 45 dB CNEL interior standard for all proposed units. Requiring that it be possible for windows and doors to remain closed for sound insulation means that air conditioning or mechanical ventilation will be required.

## **CONCLUSIONS AND RECOMMENDATIONS**

The proposed 1571 E. Main Street residential development will comply with all City of Santa Maria exterior and interior noise level standards, provided the following mitigation measures are incorporated into final project design.

### **Exterior Noise Compliance:**

1. A sound wall constructed to a minimum height of six (6) feet above project-side grade is constructed along the property line along E. Main Street at Units 1-12. In order for the sound wall to effectively shield backyards the sound wall will need to be turned inward (northward), for a minimum of twenty (20) feet at the backyard of Unit 1 (west side of backyard) and the backyard of Unit 12 (east side of backyard). Suitable construction materials include concrete blocks, masonry, or stucco on both sides of a wood or steel stud wall. The location of the required sound wall is provided on Figure 1.

### **Interior Noise Compliance:**

The proposed single-family residential development will comply with applicable City of Santa Maria interior noise level requirements provided the following mitigation measures are incorporated into final project design.

1. Mechanical ventilation or air conditioning must be provided for all homes so that windows and doors can remain closed for sound insulation purposes.



The conclusions and recommendations of this acoustical analysis are based upon the best information known to WJV Acoustics, Inc. (WJVA) at the time the analysis was prepared concerning the proposed project site, project construction and site plan, traffic volumes and vehicle speeds. Any significant changes to these factors may require revisions to the findings of this report. Additionally, any significant future changes in motor vehicle technology, noise regulations or other factors beyond WJVA's control may result in long-term noise results different from those described by this analysis.

Respectfully submitted,

A handwritten signature in blue ink, appearing to read "Walter J. Van Groningen", with a stylized flourish at the end.

Walter J. Van Groningen  
President

WJV:wjv

**FIGURE 1: PROJECT SITE PLAN**



**6-Foot Sound Wall**  
**BELLECREST RESIDENCES**  
 1571 E. MAIN ST., - SANTA MARIA, CA 93454

**ARCHITECTURAL SITE PLAN**

08/04/23

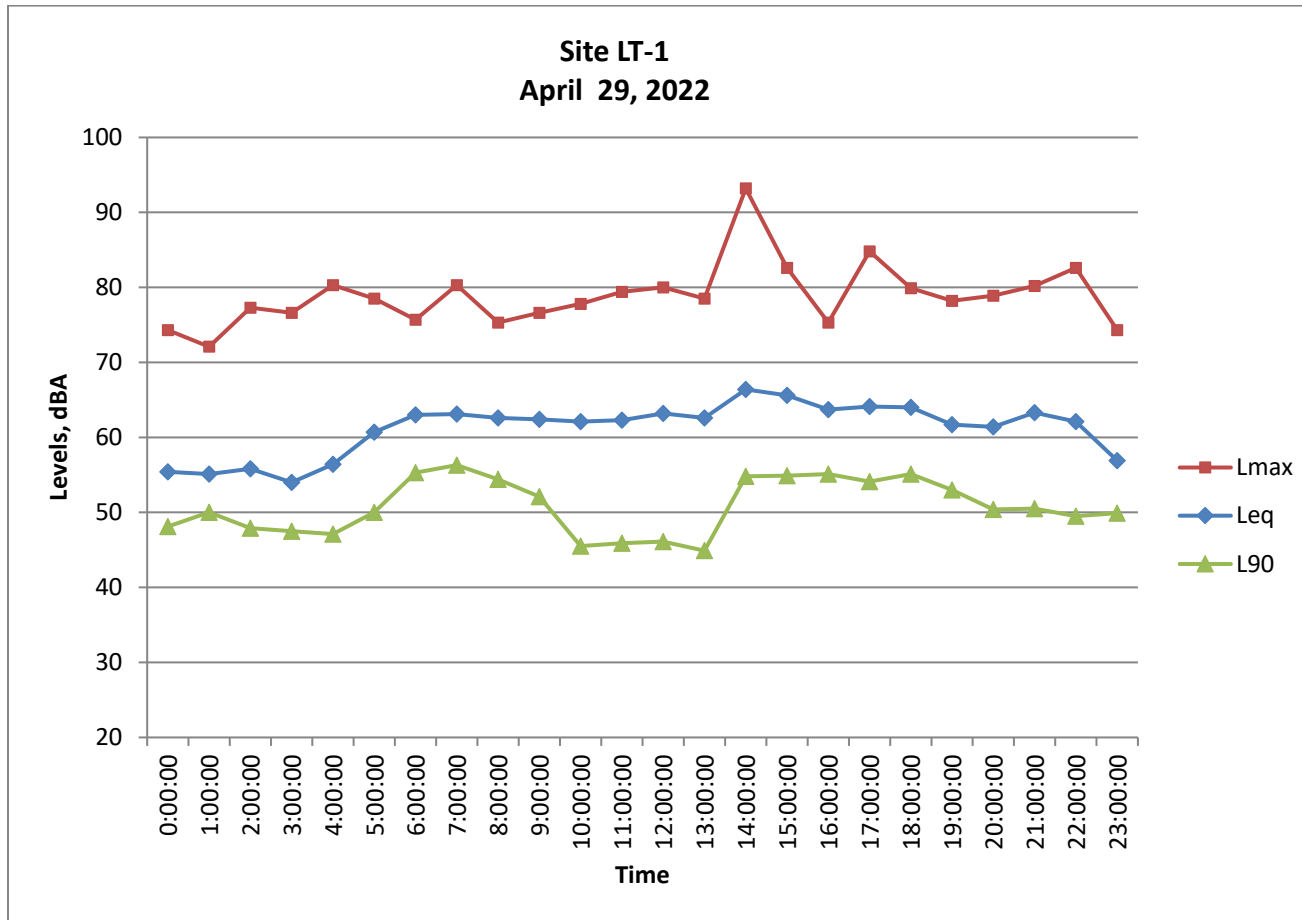
**A3**  
**PLANNING**  
**PACKAGE**



**FIGURE 2: PROJECT SITE VICINITY AND NOISE MONITORING SITE LOCATIONS**



**FIGURE 3: HOURLY NOISE LEVELS AT SITE LT-1**





**FIGURE 4: NOISE MONITORING SITE LT-1**



## APPENDIX A

### ACOUSTICAL TERMINOLOGY

<b>AMBIENT NOISE LEVEL:</b>	The composite of noise from all sources near and far. In this context, the ambient noise level constitutes the normal or existing level of environmental noise at a given location.
<b>CNEL:</b>	Community Noise Equivalent Level. The average equivalent sound level during a 24-hour day, obtained after addition of approximately five decibels to sound levels in the evening from 7:00 p.m. to 10:00 p.m. and ten decibels to sound levels in the night before 7:00 a.m. and after 10:00 p.m.
<b>DECIBEL, dB:</b>	A unit for describing the amplitude of sound, equal to 20 times the logarithm to the base 10 of the ratio of the pressure of the sound measured to the reference pressure, which is 20 micropascals (20 micronewtons per square meter).
<b>DNL/L<sub>dn</sub>:</b>	Day/Night Average Sound Level. The average equivalent sound level during a 24-hour day, obtained after addition of ten decibels to sound levels in the night after 10:00 p.m. and before 7:00 a.m.
<b>L<sub>eq</sub>:</b>	Equivalent Sound Level. The sound level containing the same total energy as a time varying signal over a given sample period. L <sub>eq</sub> is typically computed over 1, 8 and 24-hour sample periods.
<b>NOTE:</b>	The CNEL and DNL represent daily levels of noise exposure averaged on an annual basis, while L <sub>eq</sub> represents the average noise exposure for a shorter time period, typically one hour.
<b>L<sub>max</sub>:</b>	The maximum noise level recorded during a noise event.
<b>L<sub>n</sub>:</b>	The sound level exceeded "n" percent of the time during a sample interval (L <sub>90</sub> , L <sub>50</sub> , L <sub>10</sub> , etc.). For example, L <sub>10</sub> equals the level exceeded 10 percent of the time.



## ACOUSTICAL TERMINOLOGY

**NOISE EXPOSURE  
CONTOURS:**

Lines drawn about a noise source indicating constant levels of noise exposure. CNEL and DNL contours are frequently utilized to describe community exposure to noise.

**NOISE LEVEL  
REDUCTION (NLR):**

The noise reduction between indoor and outdoor environments or between two rooms that is the numerical difference, in decibels, of the average sound pressure levels in those areas or rooms. A measurement of a noise level reduction@ combines the effect of the transmission loss performance of the structure plus the effect of acoustic absorption present in the receiving room.

**SEL or SENEL:**

Sound Exposure Level or Single Event Noise Exposure Level. The level of noise accumulated during a single noise event, such as an aircraft overflight, with reference to a duration of one second. More specifically, it is the time-integrated A-weighted squared sound pressure for a stated time interval or event, based on a reference pressure of 20 micropascals and a reference duration of one second.

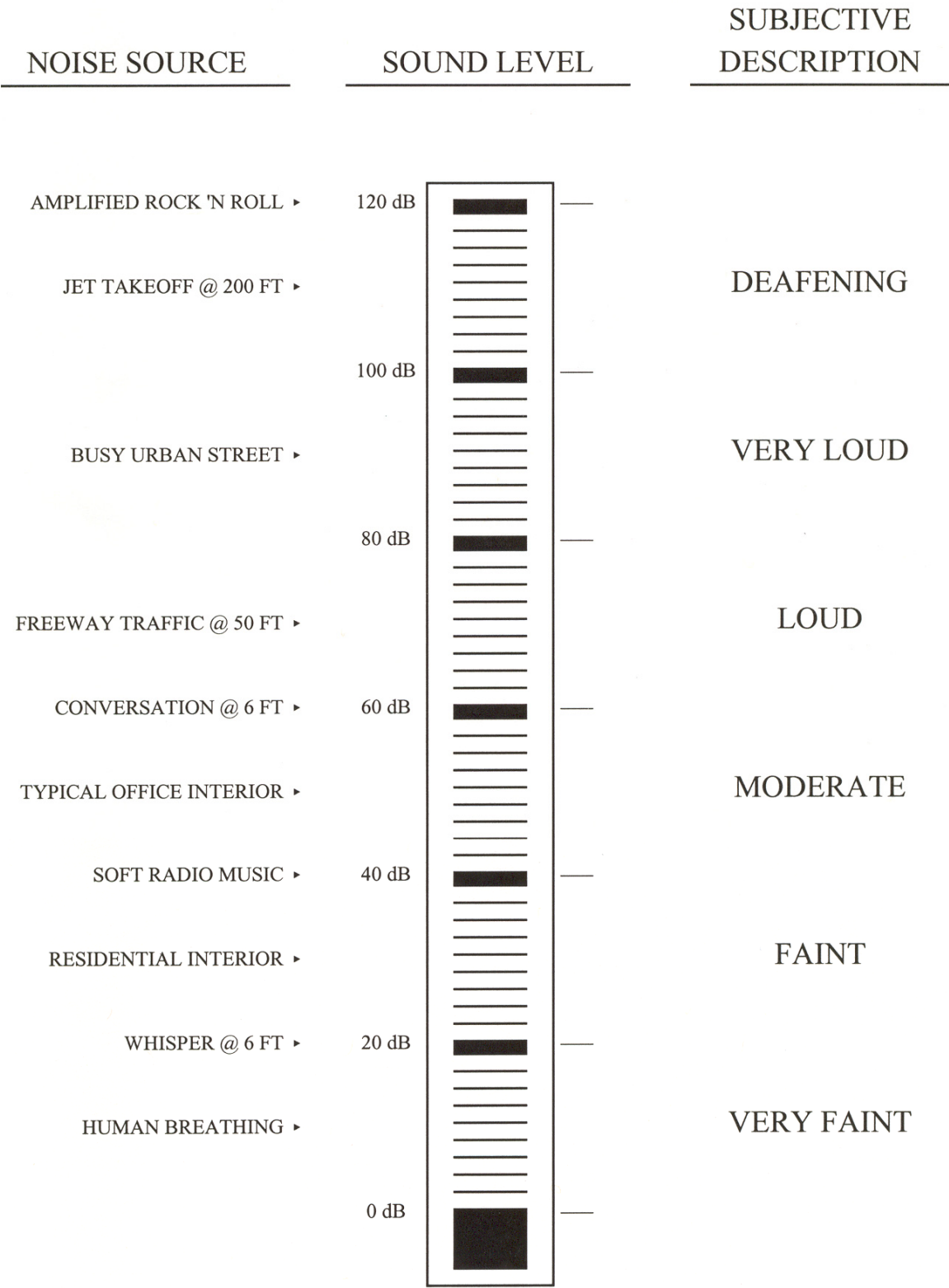
**SOUND LEVEL:**

The sound pressure level in decibels as measured on a sound level meter using the A-weighting filter network. The A-weighting filter de-emphasizes the very low and very high frequency components of the sound in a manner similar to the response of the human ear and gives good correlation with subjective reactions to noise.

**SOUND TRANSMISSION  
CLASS (STC):**

The single-number rating of sound transmission loss for a construction element (window, door, etc.) over a frequency range where speech intelligibility largely occurs.

APPENDIX B  
EXAMPLES OF SOUND LEVELS



# Appendix F

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Traffic and Circulation Study

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# **BELLECREST SENIOR HOUSING PROJECT**

## **CITY OF SANTA MARIA, CALIFORNIA**

---

### **TRAFFIC AND CIRCULATION STUDY**

---



**December 19, 2023**

**ATE #22086.01**

Coastal Community Builders  
330 James Way, Suite 270  
Pismo Beach, CA 93449



**ASSOCIATED TRANSPORTATION ENGINEERS**

100 N. Hope Avenue, Suite 4, Santa Barbara, CA 93110 • (805) 687-4418 • FAX (805) 682-8509



# ASSOCIATED TRANSPORTATION ENGINEERS

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Since 1978

Richard L. Pool, P.E.  
Scott A. Schell

December 19, 2023

22086.01.R01

Mr. Cam Boyd  
Coastal Community Builders  
330 James Way, Suite 270  
Pismo Beach, CA 93449

***TRAFFIC AND CIRCULATION STUDY FOR THE  
BELLECREST SENIOR HOUSING PROJECT - CITY OF SANTA MARIA***

Associated Transportation Engineers (ATE) has prepared the following traffic and circulation study for the Bellecrest Senior Housing Project, located in the City of Santa Maria.

We appreciate the opportunity to assist you with the project.

Associated Transportation Engineers

Scott A. Schell  
Principal Transportation Planner

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## INTRODUCTION

The following report contains an analysis of the potential traffic and circulation effects associated with the Bellecrest Senior Housing Project (the “Project”), proposed in the City of Santa Maria. The study evaluates existing and future traffic conditions in the Project study-area in order to determine the Project’s consistency with the City’s transportation policies. The intersections analyzed in the study were determined based on input provided by City of Santa Maria staff. An analysis of site access, circulation and queuing is also provided; and the study evaluates the Project’s potential CEQA traffic impacts based on the City’s adopted Vehicle Miles Traveled (VMT) impact criteria.

## PROJECT DESCRIPTION

The Project site is located on the north side of East Main Street, east of Suey Road and west of Navara Way in the City of Santa Maria. Figure 1 shows the location of the Project site within the City. The Project is proposing to develop a senior residential housing complex with 102 detached units, 40 attached duplex units, and associated recreational amenities. The units would be compact in size (712 square feet to 1,413 SF) and thus would operate more like senior apartments than detached housing. Figure 2 presents the Project site plan. As shown on the site plan, access to the Project site is proposed via a new roadway connection to Main Street located approximately midway between Suey Road and Navara Way.

## TRAFFIC ANALYSIS SCENARIOS

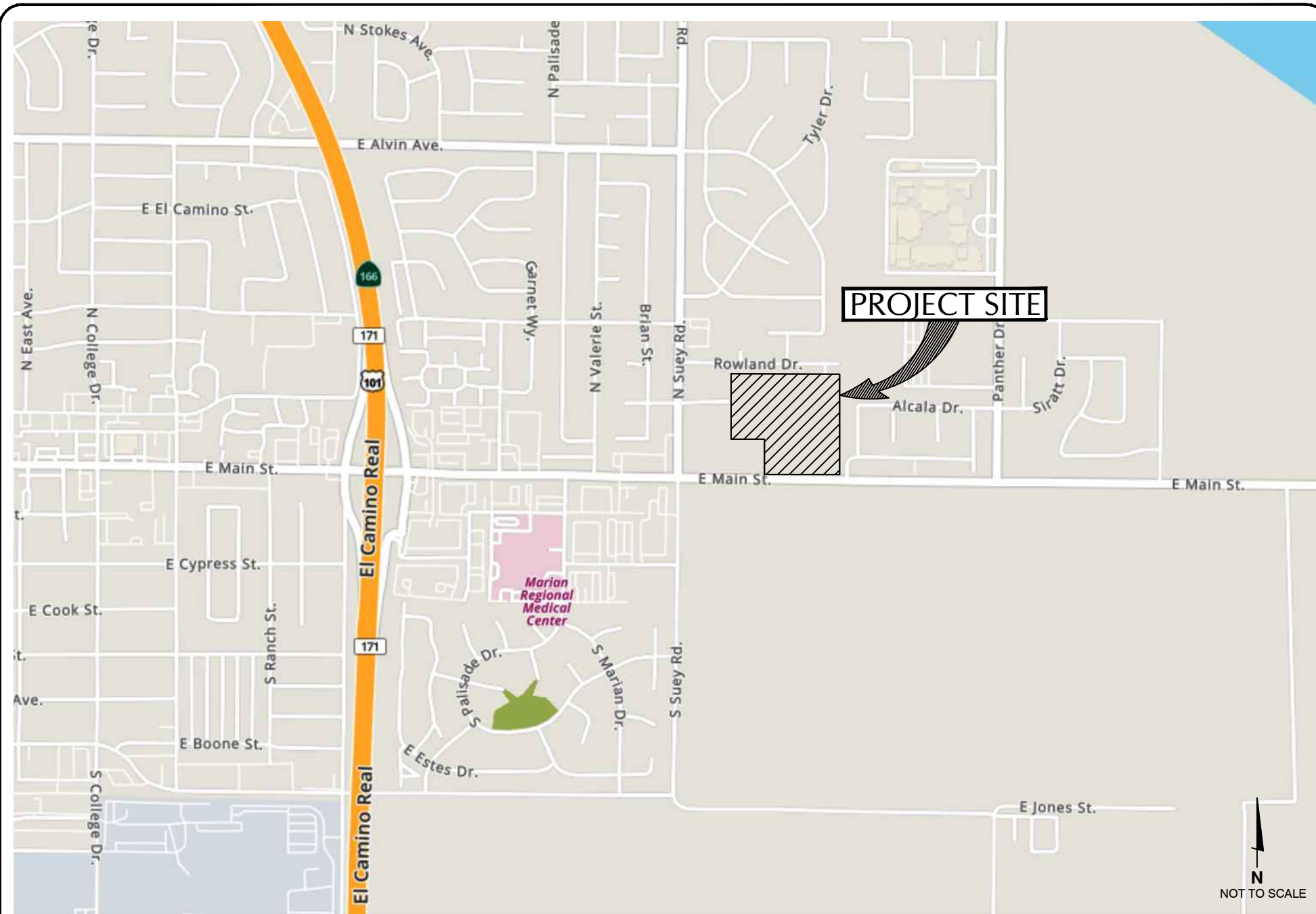
The following scenarios are included in the traffic analysis.

*Existing Conditions:* This scenario describes the existing street network and evaluates peak hour operations at the key study-area intersections identified for analyses.

*Existing + Project:* This scenario evaluates traffic operations assuming Existing + Project traffic forecasts. The Project’s consistency with the City’s transportation policies is evaluated for this scenario.

*Cumulative Conditions:* This scenario evaluates traffic operations assuming the additional traffic that will be generated by approved and pending developments located in the adjacent areas of the City. Traffic volumes generated by the approved and pending projects are layered onto the Existing baseline traffic forecasts for analyses.

*Cumulative + Project:* This scenario evaluates operations assuming the Cumulative conditions plus the traffic generated by the Project. The Project’s consistency with the City’s transportation policies is evaluated for this scenario.



PROJECT SITE LOCATION

FIGURE 1

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FIGURE 2

## EXISTING CONDITIONS

### Existing Street Network

The Project site is served by a network of highways, arterial, and collector streets, as shown on Figure 3. The following text provides a brief discussion of the major components of the study-area street network.

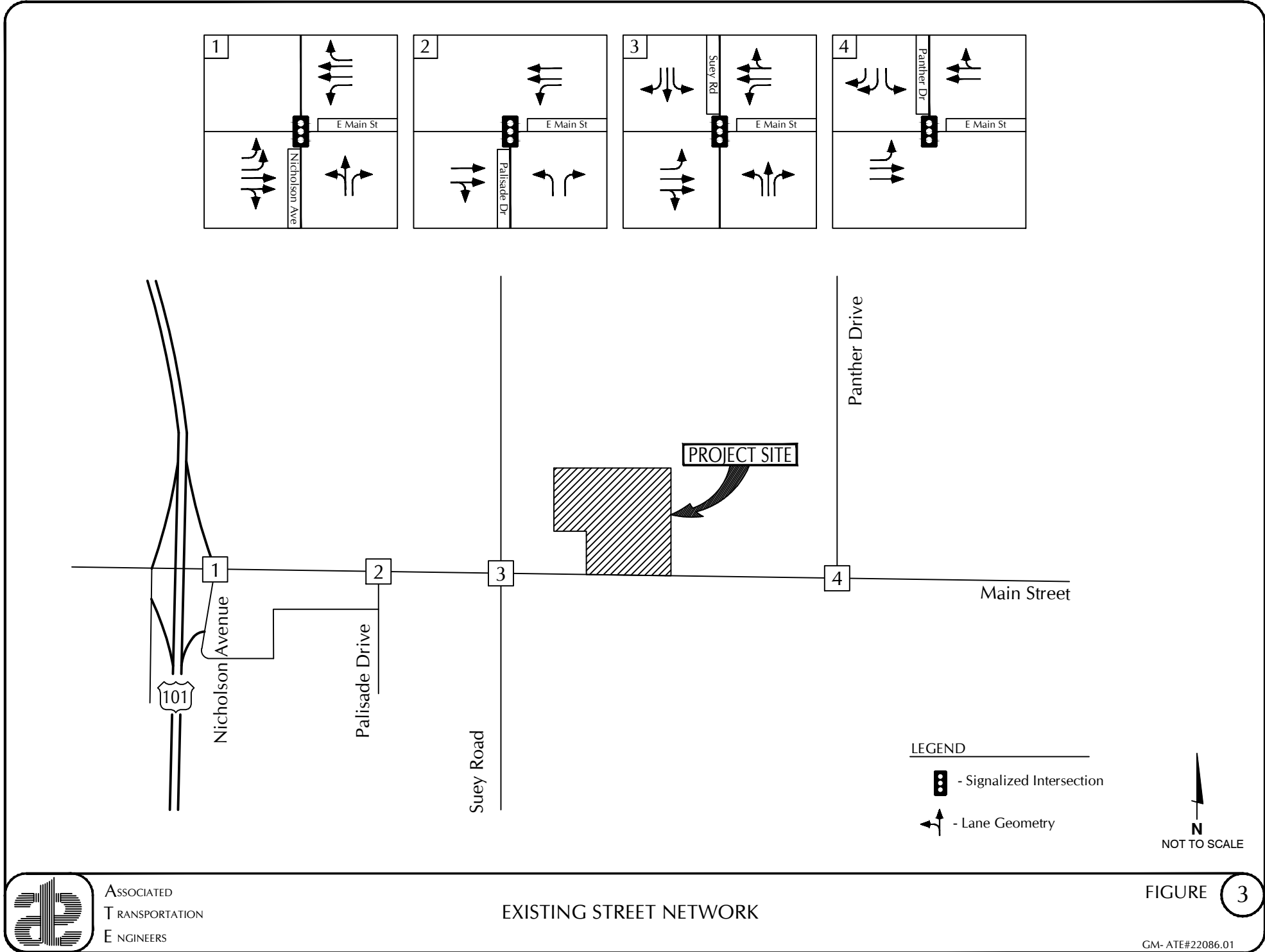
US 101, located west of the Project site, is a freeway that serves as the major north-south link through the Santa Maria Valley and is the principal inter-city route along the Pacific Coast. US 101 is a 6-lane freeway within the Santa Maria area, with 4 lanes provided north and south of the City. Access to the Project site from US 101 is provided via the Main Street interchange.

East Main Street, located on the southern boundary of the Project site, is a four-lane Primary Arterial roadway that extends west from US 101 as State Route (SR) 166 to the City of Guadalupe. East of US 101, Main Street extends to Stowell Road where it transitions to Philbric Road. Main Street provides access between the Project site and US 101 via a full access interchange. Within the Project study-area, Main Street contains Class II bike lanes. Access to the Project site would be provided via a new roadway connection to Main Street.

Palisade Drive, located west of the Project site, is a two lane Local Road that extends south of Main Street providing access to the Marian Regional Medical Center. No bike facilities are provided on Palisade Drive within the Project study-area.

Suey Road, located west of the Project site, is a two-lane Secondary Arterial that extends from Jones Street on the south to its terminus north of Donovan Road on the north. Within the Project study-area, Suey Road contains Class II bike lanes.

Panther Drive, located east of Project site, is a four-lane Secondary Arterial that extends north from Main Street providing access to the Pioneer Valley High School. Within the Project study-area, Panther Drive contains Class II bike lanes.





## **Existing Pedestrian Facilities**

Within the Project study area, sidewalks are currently provided on Main Street, Palisade Drive, and Panther Drive. Sidewalks are currently missing on the east side of Suey Road north and south of Main Street. ADA accessible crosswalks with pedestrian signals heads are provided on all four legs of the Main Street/Suey Road intersection.

## **Existing Transit Facilities**

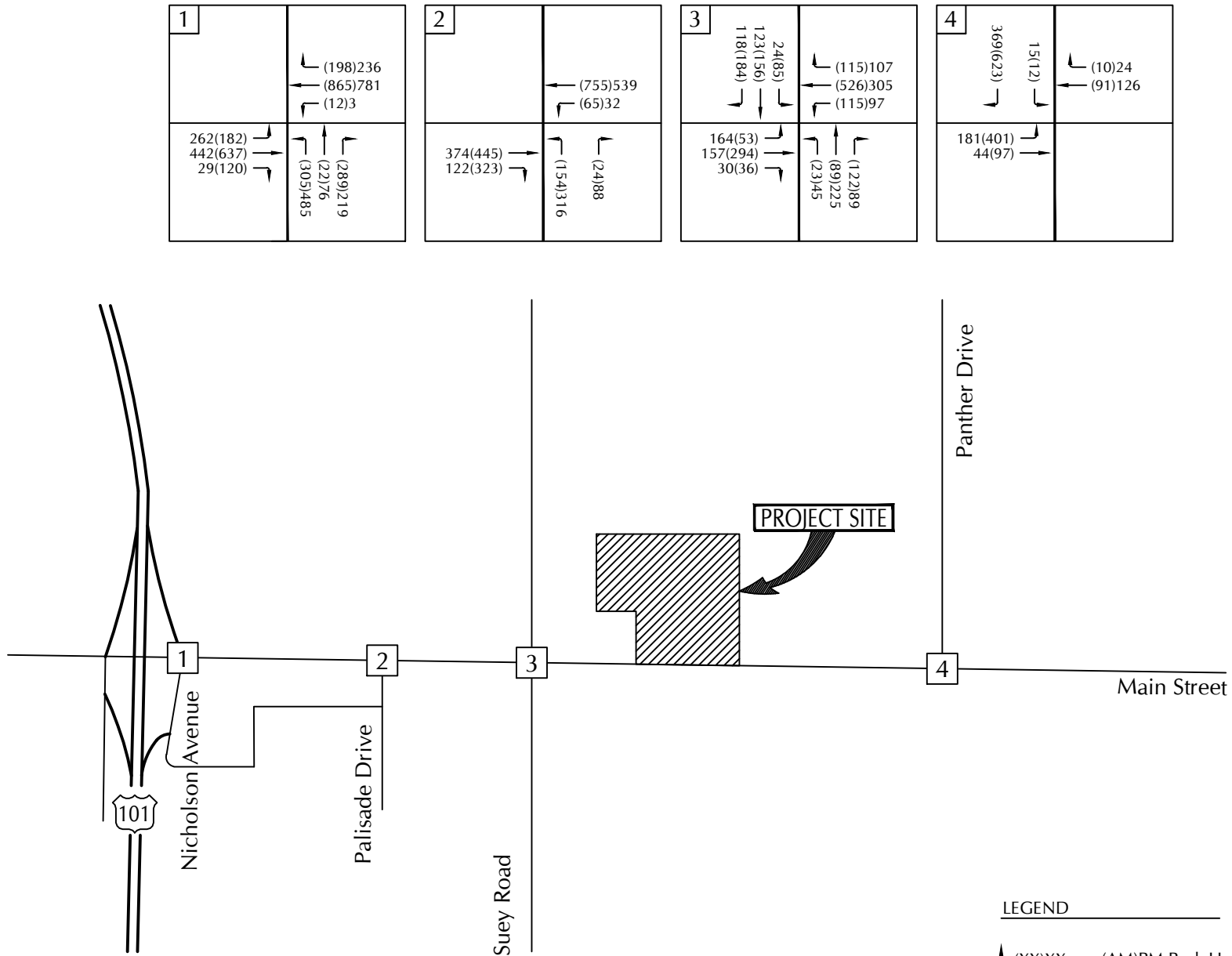
Transit service in the City of Santa Maria is provided by the Santa Maria Regional Transit (SMRT) service. Eastbound and westbound transit stops are located near the corner of the Main Street/Suey Road intersection west of the Project site. These stops are served by SMRT Route 3, which provides connections to the Marian Regional Medical Center on the west and the Santa Maria Transit Center to the southwest (see transit route map in Technical Appendix).

## **Intersection Operations**

Because traffic flow on urban arterials is most constrained at intersections, detailed traffic flow analyses focus on the operating conditions of critical intersections during peak travel periods. "Levels of Service" (LOS) A through F are used to rate intersection operations, with LOS A indicating very good operation and LOS F indicating poor operation (more complete definitions are contained in the Technical Appendix for reference). The City of Santa Maria considers LOS D as the performance standard for intersections (maintain LOS D or better).

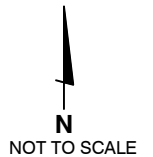
The existing traffic controls and lane geometry for the study-area intersections are presented on Figure 3. Existing intersection traffic volumes were obtained from traffic count data collected in November 2023 (see Technical Appendix for count data). Counts were conducted during the AM peak commuter period (7:00-9:00 AM) and PM peak commuter period (4:00-6:00 PM). The peak 1-hour volumes were then identified for the analysis. Figure 4 presents the existing peak hour traffic volumes for the study-area intersections.

Levels of service for the signalized intersections were calculated using the intersection capacity utilization (ICU) methodology adopted by the City of Santa Maria. Table 1 lists the existing traffic controls and levels of service for the study-area intersections identified for the analysis.



LEGEND

└(XX)XX - (AM)PM Peak Hour Volume



EXISTING TRAFFIC VOLUMES

FIGURE 4

GM- ATE#22086.01

**Table 1**  
**Existing Levels of Service**

Intersection	Control	AM Peak Hour		PM Peak Hour	
		ICU	LOS	ICU	LOS
Main Street/US 101 NB Ramps-Nicholson Road (a)	Signal	0.63	LOS B	0.78	LOS C
Main Street Palisade Drive	Signal	0.48	LOS A	0.47	LOS A
Main Street/Suey Road	Signal	0.44	LOS A	0.48	LOS A
Main Street/Panther Drive	Signal	0.58	LOS A	0.38	LOS A

(a) Intersection is under the jurisdiction of Caltrans.

The data presented in Table 1 show that the study-area intersections currently operate at LOS C or better during the AM and PM peak hours, which is consistent with the City's LOS D operating standard.

## TRAFFIC POLICY STANDARDS

The City of Santa Maria Circulation Element considers LOS D acceptable for roadway and intersection operations, with improvements required for LOS E and F. It is noted some of the study-area intersections are under Caltrans' jurisdiction. The current Caltrans traffic analysis guidelines are based on VMT and not LOS, thus the VMT section of this report addresses the Caltrans requirements.

## EXISTING + PROJECT CONDITIONS

### Project Trip Generation

Trip generation estimates were calculated for the Project using rates presented in the Institute of Transportation Engineers (ITE) Trip Generation Manual (11<sup>th</sup> Edition).<sup>1</sup> The rates for Senior Adult Housing – Single-Family (Land Use Code #251). To be conservative, the analysis used the senior single-family rates for both the detached units and the attached duplexes (senior adult housing - multifamily rates are approximately 17% to 25% lower than senior adult housing – single- family rates). Table 2 presents the results of the trip generation calculations.

**Table 2**  
**Project Trip Generation**

Land Use	Size	ADT		AM Peak Hour		PM Peak Hour	
		Rate	Trips	Rate	Trips	Rate	Trips
Senior Housing (a)	142 units	4.31	612	0.24	34 (11/23)	0.30	43 (26/17)

(a) Trip generation based on ITE Code #251 (Senior Adult Housing – Single-Family)

<sup>1</sup> Trip Generation, Institute of Transportation Engineers, 11th Edition, 2021.

The data presented in Table 2 indicate that the Project is forecast to generate 612 average daily trips (ADT), 34 AM peak hour trips and 43 PM peak hour trips.

### **Project Trip Distribution**

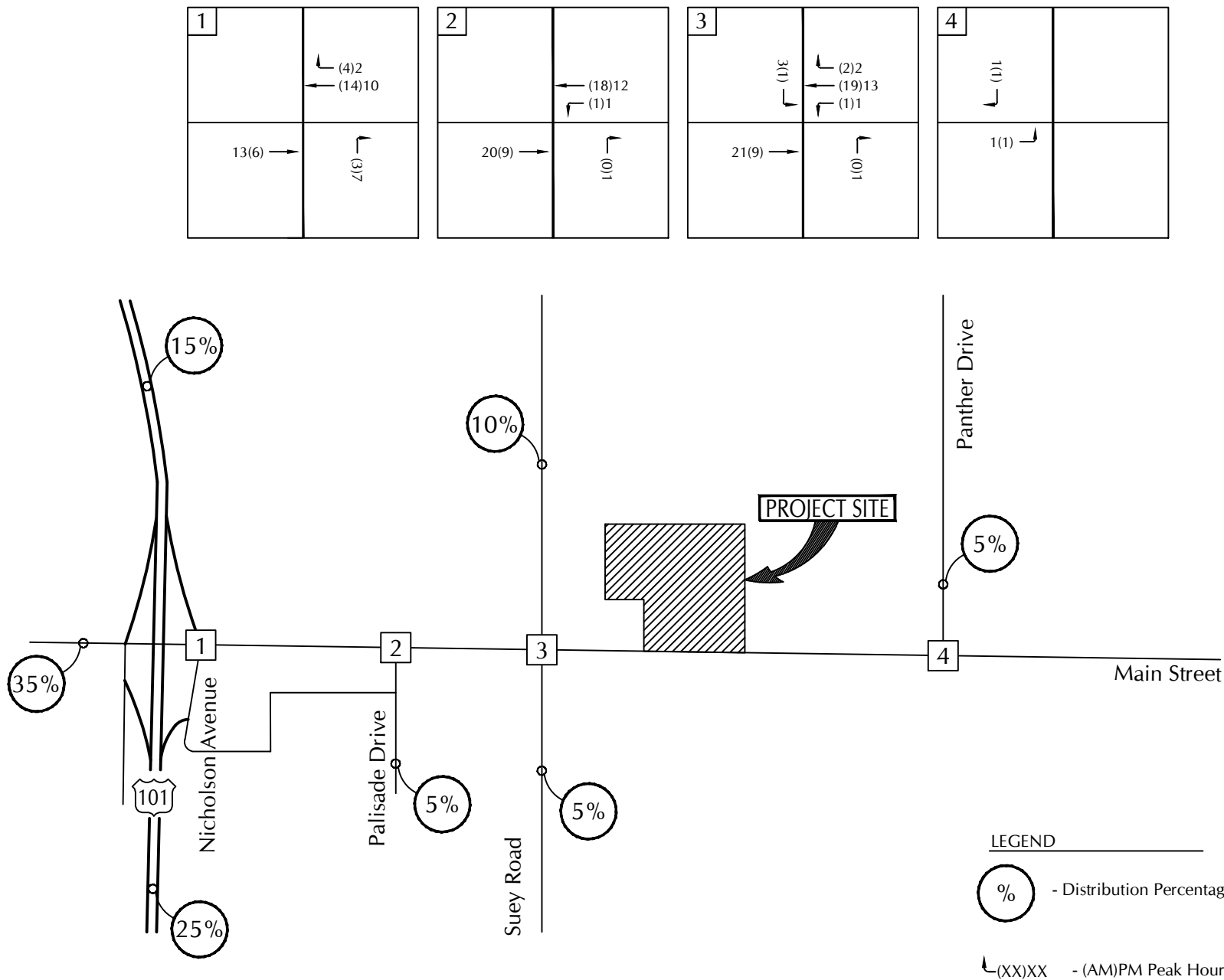
The trip distribution pattern for the Project was developed based on existing traffic patterns observed in the study-area, consideration of the land uses in the surrounding area, and the proposed Project site access system. Table 3 and Figure 5 present the trip distribution patterns developed for the Project.

**Table 3**  
**Project Trip Distribution Percentages**

<b>Origin/Destination</b>	<b>Direction</b>	<b>Distribution Percentage</b>
US 101	North South	15% 25%
Main Street (w/o US 101)	West	35%
Panther Drive	North	5%
Suey Road	North South	10% 5%
Palisade Drive	South	5%
<b>Totals</b>		<b>100%</b>

### **Existing + Project Intersection Operations**

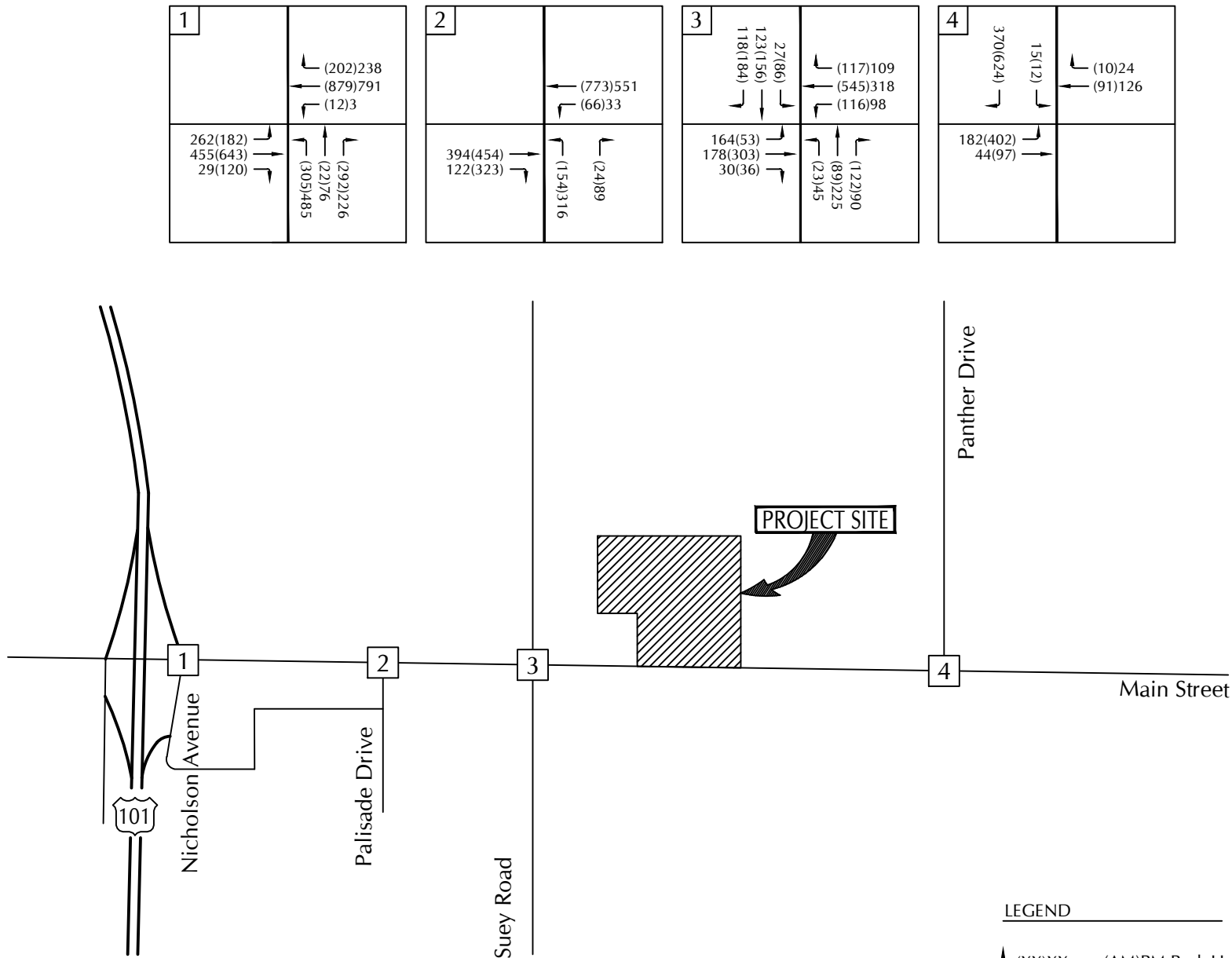
Levels of service were calculated for the study-area intersections assuming the Existing + Project traffic volumes shown on Figure 6. Tables 4 and 5 compare the Existing and Existing + Project level of service forecasts and identify the Project's consistency with the City's LOS D standard.



PROJECT TRIP DISTRIBUTION AND ASSIGNMENT

FIGURE 5





EXISTING + PROJECT TRAFFIC VOLUMES

FIGURE 6

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**Table 4**  
**Existing + Project Levels of Service – AM Peak Hour**

Intersection	Existing		Existing + Project		Consistent?
	ICU	LOS	ICU	LOS	
Main Street/US 101 NB Ramps-Nicholson Road	0.63	LOS B	0.64	LOS B	Yes
Main Street Palisade Drive	0.48	LOS A	0.48	LOS A	Yes
Main Street/Suey Road	0.44	LOS A	0.45	LOS A	Yes
Main Street/Panther Drive	0.58	LOS A	0.58	LOS A	Yes

**Table 5**  
**Existing + Project Levels of Service – PM Peak Hour**

Intersection	Existing		Existing + Project		Consistent?
	ICU	LOS	ICU	LOS	
Main Street/US 101 NB Ramps-Nicholson Road	0.78	LOS C	0.78	LOS C	Yes
Main Street Palisade Drive	0.47	LOS A	0.48	LOS A	Yes
Main Street/Suey Road	0.48	LOS A	0.49	LOS A	Yes
Main Street/Panther Drive	0.38	LOS A	0.38	LOS A	Yes

The data presented in Tables 4 and 5 show that the study-area intersections intersection are forecast to operate at LOS C or better during the AM and PM peak hours with Existing + Project traffic, which meet the City's LOS D operating standard. The Project would therefore be consistent with the City's Circulation Element transportation policies.

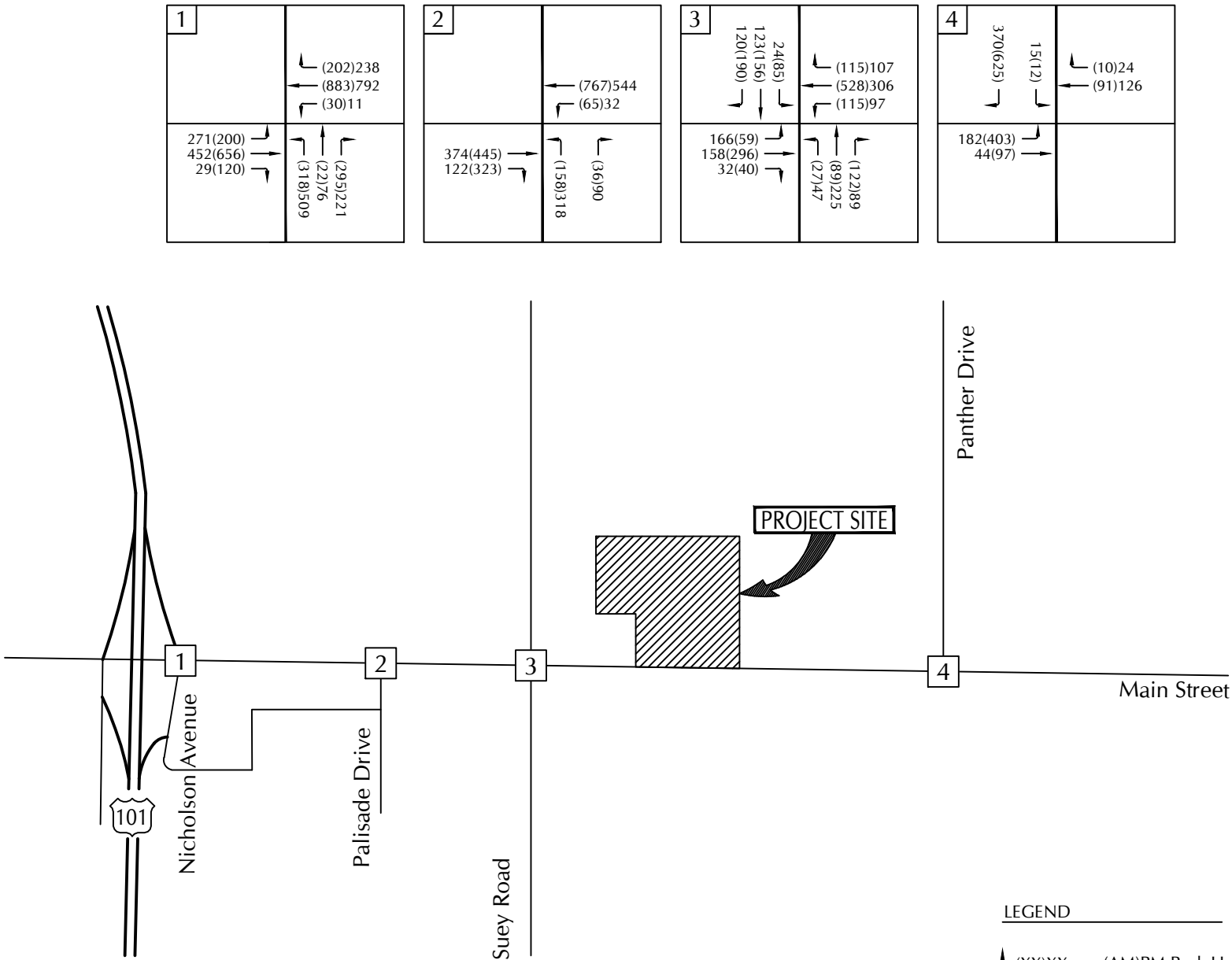
## CUMULATIVE ANALYSIS

### Cumulative Traffic Volumes

Cumulative traffic volumes were forecast for the study-area intersections assuming development of the approved and pending projects located in the adjacent portions of the City (list of cumulative projects is contained in the Technical Appendix). Trip generation estimates were developed for the cumulative projects using ITE rates or from traffic studies prepared for the cumulative projects (cumulative trip generation calculations are contained in the Technical Appendix). The traffic generated by the cumulative projects was then added to the Existing volumes to produce the Cumulative traffic forecasts. Figure 7 shows the Cumulative traffic volumes and Figure 8 shows the Cumulative + Project volumes.

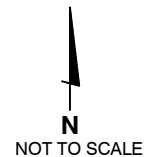
### Cumulative Intersection Operations

Levels of service were calculated for the study-area intersections assuming the Cumulative and Cumulative + Project traffic volumes presented on Figures 7 and 8. Tables 6 and 7 compare the Cumulative and Cumulative + Project levels of service forecasts and identify the Project's consistency with the City's LOS D standard.



LEGEND

└(XX)XX - (AM)PM Peak Hour Volume



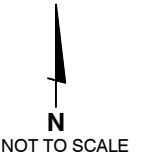
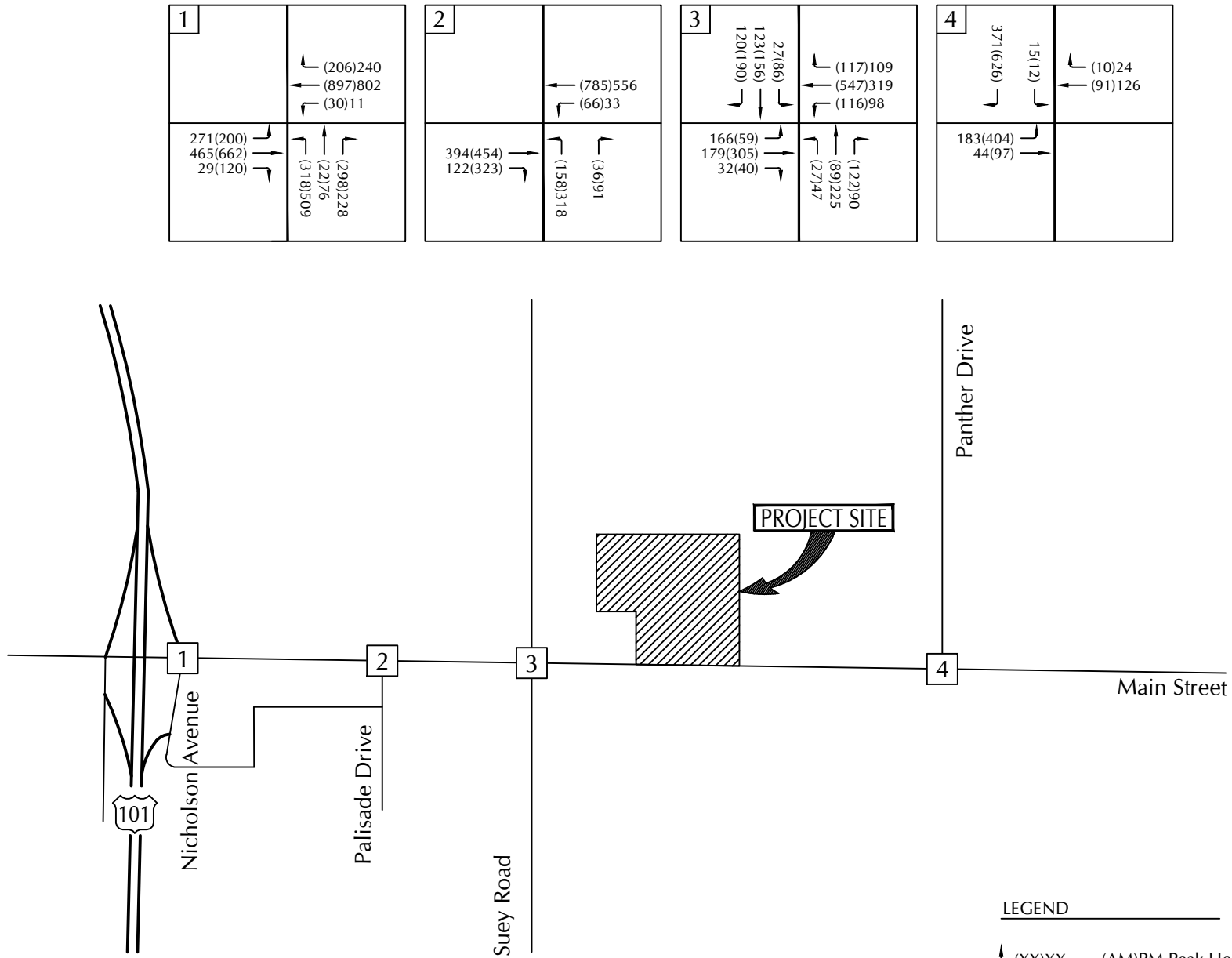
CUMULATIVE TRAFFIC VOLUMES

FIGURE 7

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CUMULATIVE + PROJECT TRAFFIC VOLUMES

FIGURE 8

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TRANSPORTATION  
ENGINEERS

**Table 6**  
**Cumulative + Project Levels of Service – AM Peak Hour**

Intersection	Cumulative		Cumulative + Project		Consistent?
	ICU	LOS	ICU	LOS	
Main Street/US 101 NB Ramps-Nicholson Road	0.65	LOS B	0.66	LOS B	Yes
Main Street Palisade Drive	0.48	LOS A	0.48	LOS A	Yes
Main Street/Suey Road	0.45	LOS A	0.45	LOS A	Yes
Main Street/Panther Drive	0.58	LOS A	0.58	LOS A	Yes

**Table 7**  
**Cumulative + Project Levels of Service – PM Peak Hour**

Intersection	Cumulative		Cumulative + Project		Consistent?
	ICU	LOS	ICU	LOS	
Main Street/US 101 NB Ramps-Nicholson Road	0.80	LOS C	0.80	LOS C	Yes
Main Street Palisade Drive	0.47	LOS A	0.48	LOS A	Yes
Main Street/Suey Road	0.49	LOS A	0.49	LOS A	Yes
Main Street/Panther Drive	0.38	LOS A	0.38	LOS A	Yes

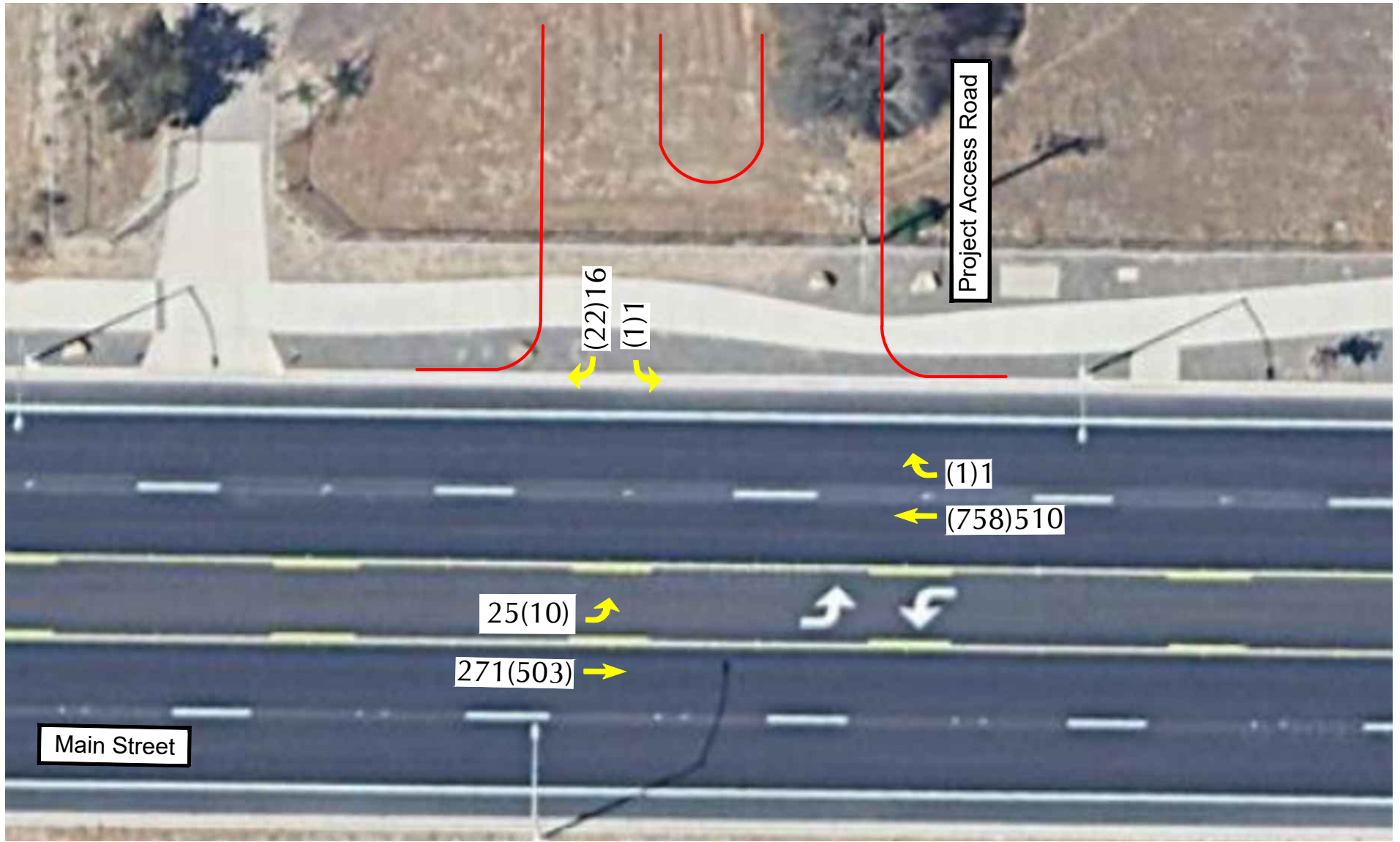
The data presented in Tables 6 and 7 show that the study-area intersections are forecast to operate at LOS C or better during the AM and PM peak hours with Cumulative and Cumulative + Project traffic, which meet the City's LOS D operating standard. The Project would therefore be consistent with the City's Circulation Element transportation policies under cumulative conditions.

## **SITE ACCESS AND CIRCULATION**

### **Main Street/Project Access Road Operations**

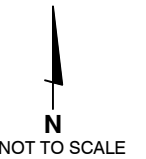
The following section reviews the operations of the Main Street/Project Access Road intersection. Cumulative + Project Volumes were forecast for the intersection in order complete the analysis, as presented on Figure 9. Levels of service were calculated for the Main Street/Project Access Road intersection using the Highway Capacity Manual (HCM)<sup>2</sup> methodology for 2-way stop-sign controlled intersections (level of service calculations are contained in the Technical Appendix). Table 8 presents the results of the LOS calculations.

<sup>2</sup> Highway Capacity Manual, Transportation Research Board, 7<sup>th</sup> Edition, 2022.



LEGEND

(XX)XX - (AM)PM Peak Hour Volume



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CUMULATIVE + PROJECT TRAFFIC VOLUMES -  
MAIN STREET/PROJECT ACCESS ROAD INTERSECTION

FIGURE 9

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**Table 8**  
**Main Street/Project Access Road LOS**

Intersection	Cumulative + Project		Consistent?
	AM Peak Delay / LOS	PM Peak Delay / LOS	
Main Street/Project Access Road			
Southbound Access Road Left + Right	11.9 Sec./LOS B	11.0 Sec./LOS B	Yes
EB Main Street Left	9.7 Sec./LOS A	9.2 Sec./LOS A	
Average Weighted Delay	11.2 Sec./LOS B	9.9 Sec./LOS A	

The data presented in Table 8 indicate that the Main Street/Project Access Road intersection would operate acceptably in the LOS A-B range with Cumulative + Project traffic volumes.

It is noted that the section of Main Street adjacent to the Project site is currently configured with a center two way left-turn lane (TWLTL). It is recommended that the striping be modified to provide a dedicated eastbound left-turn with a minimum of 150 feet of storage (see Recommended Improvements section). The left-turn lane would provide a storage area of approximately 150 feet and then transition to a two-way-center left-turn lane that provides an additional storage area of approximately 450 feet to the Main Street/Suey Road intersection.

### Driveway Queuing Analysis

A queuing analysis was completed for the Main Street/Project Access Road intersection to determine if the eastbound left-turn queues at the intersection would exceed the 150 feet of storage recommended (see Recommended Improvements section). The analysis also reviews the queues at the Project access road.

The queueing analysis was completed using the SYNCHRO software program. The SYNCHRO software implements the HCM operations methodology and predicts both "50th Percentile" and "95th Percentile" queue forecasts for the peak period. The 50th percentile queue forecasts represent the average queues during the peak period. The 95th percentile queue forecasts represent the peak queues during the peak period and are recommended for design purposes. Worksheets showing the queue forecasts are contained in the Technical Appendix. Table 9 summarizes the lane storage provided and the average (50<sup>th</sup>) and peak (95<sup>th</sup>) queue forecasts for the Project access road intersection.



**Table 9**  
**Cumulative + Project Queue Analysis Summary –**  
**Main Street/Project Access Road Intersection**

Peak Hour Period Intersection Approach	Storage Length	Cumulative + Project		Exceeds Storage?
		50 <sup>th</sup> % Queue	95 <sup>th</sup> % Queue	
AM Peak hour				
EB Left-Turn Lane	150 Feet	< 1 Vehicle	< 1 Vehicle	No
SB Left-Right Lane	100 Feet	18 Feet	42 Feet	No
PM Peak hour				
EB Left-Turn Lane	150 Feet	12 Feet	35 Feet	No
SB Left-Right Lane	100 Feet	12 Feet	38 Feet	No

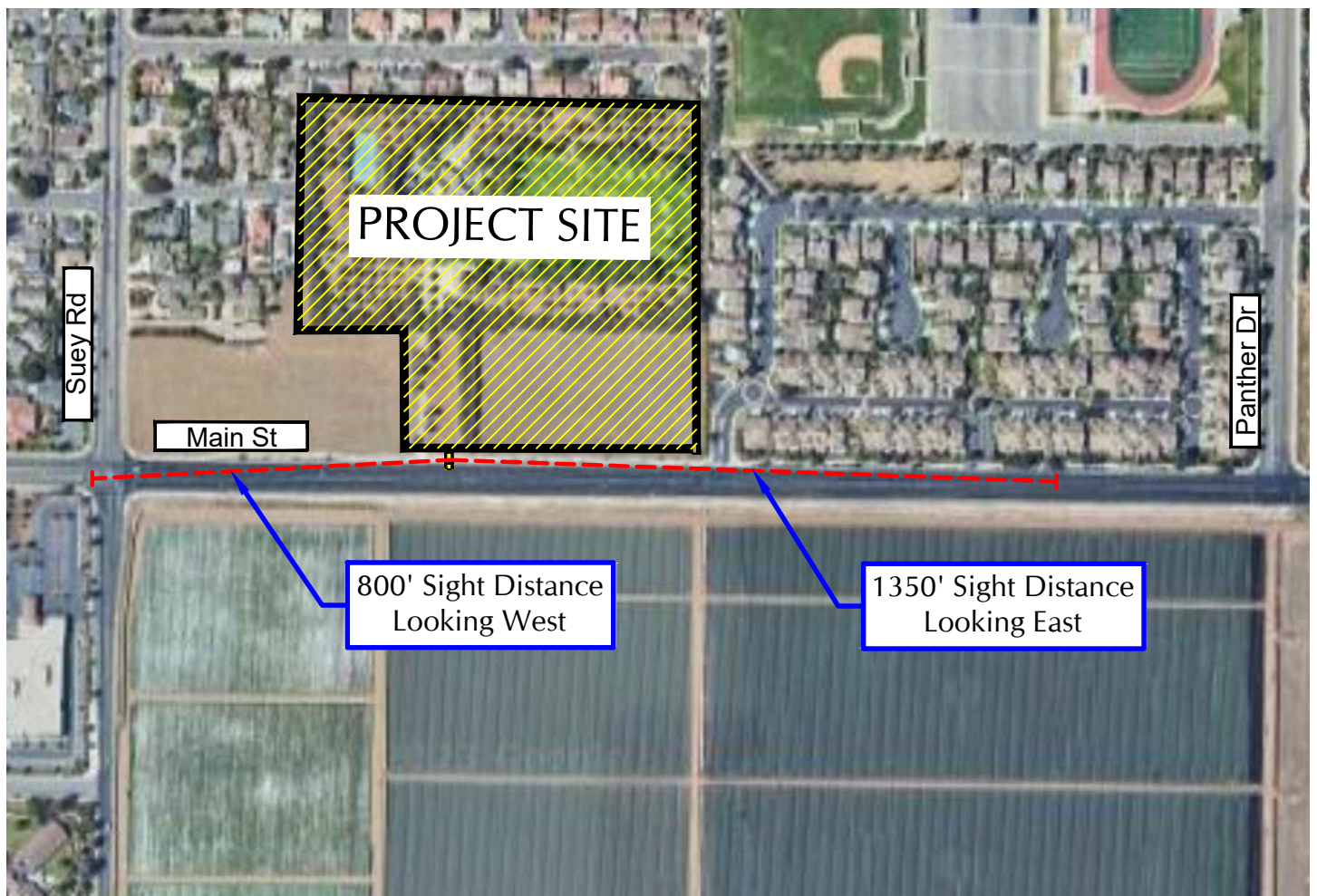
The data presented in Table 9 indicate that the storage provided at the Main Street/Project Access Road intersection would accommodate the peak queue forecasts.

### Sight Distance Evaluation

Sight distances were analyzed at the Main Street/Project Access Road intersection to determine if the sight lines along Main Street are sufficient in length to permit drivers to anticipate and avoid potential collisions when turning from the Project Access Road onto Main Street. The corner sight distance standards outlined in the Caltrans Highway Design Manual were used to determine the minimum sight distances requirements.<sup>3</sup> Main Street is posted within a 45 MPH speed limit adjacent to the Project site. Speed surveys found that vehicles travel in the 45-50 MPH range when approaching the Project Access Road. To be conservative, the Caltrans minimum corner sight distance standard for a 50 MPH design speed was applied in the analysis – which is a minimum of 550 feet of sight distance for drivers looking along Main Street from the Project Access Road.

Sight distances were measured from the Project Access Road looking to the east and west along Main Street. The sight distance to the east was measured at 1,350 feet and the sight distance to the west was measured at 800 feet, both of which exceed the Caltrans 550-foot minimum sight distance standard. The sight distances are illustrated on Figure 10.

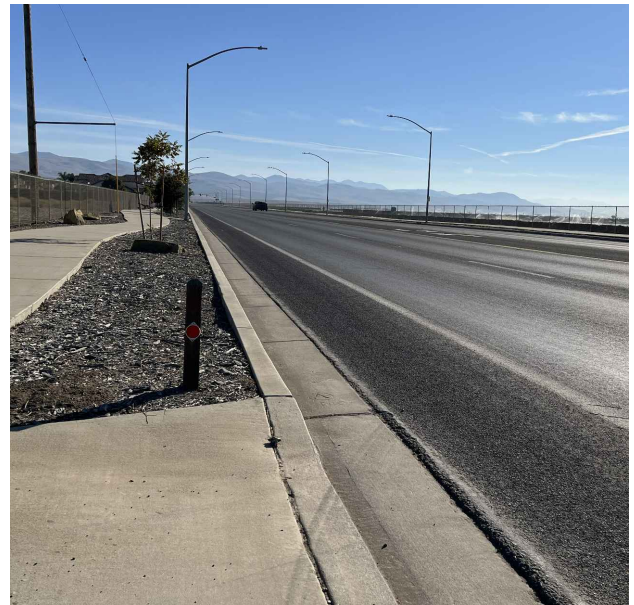
<sup>3</sup> Highway Design Manual, California Department of Transportation, July 2020.



Looking West



Looking East



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## MAIN STREET/PROJECT ACCESS ROAD SIGHT DISTANCES

FIGURE 10

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## ACCIDENT ANALYSIS

An accident analysis was completed to evaluate the accident rates for the study-area intersections. Accident data was obtained from the City of Santa Maria for the most current 3-year period of accident records available (November 2020 – November 2022).

It is important to note that accident data is used as a screening tool to identify potential safety problems. The rate of accidents was calculated for each intersection and then compared to California statewide averages for similar facilities to identify potential safety issues. By nature, accident rates experienced on a facility are often higher than the statewide average rate for similar facilities since the statewide averages are comprised of lower-than-average rates + higher-than-average rates (lower + higher = average).

If the accident rate experienced on a facility is higher than the statewide average, the Caltrans significance test is performed to determine if the number of accidents that occurred on the facility is statistically significant. If the number of accidents experienced is statistically significant, more detailed safety investigations are performed to determine if there are accident patterns that can be corrected by changing design features of the facility (e.g., widen traffic lanes, widen roadway shoulders, change roadway curvatures, add signs, install traffic signals, etc.).

Accident rates were calculated for the study-area intersections adjacent to the Project site using the 3-year accident history. The “area of influence” for each intersection is defined as within 250 feet of the intersection. The rate of accidents was calculated and then compared to the California statewide average for similar facilities. Table 10 lists the actual rate of accidents for the 3-year period and compares the rates to the California statewide averages for similar intersections (see attached accident rate calculations for more details).

**Table 10**  
**Study Area Intersections - Accident Rates**

Location	# Accidents	Accident Rate(a)	Statewide Average Rate(a)
Main Street/US 101 NB Ramps-Nicholson Road	6 Accidents	0.23 per mev	0.55 per mev
Main Street Palisade Drive	5 Accidents	0.33 per mev	0.43 per mev
Main Street/Suey Road	3 Accidents	0.20 per mev	0.55 per mev
Main Street/Panther Drive	2 Accidents	0.26 per mev	0.43 per mev

(a) Accident rates per million entering vehicles (mev).

Main Street/US 101 NB Ramps-Nicholson Road. As shown in Table 10, there were 6 accidents at this intersection within the 3-year period. The rate of accidents was 0.23 accidents per million entering vehicles and the California statewide average for similar intersections is 0.55 accidents per million entering vehicles. Thus, the rate of accidents is below the statewide average and further investigation is not required.

Main Street/Palisade Drive. As shown in Table 10, there were 5 accidents at this intersection within the 3-year period. The rate of accidents was 0.33 accidents per million entering vehicles and the California statewide average for similar intersections is 0.43 accidents per million entering vehicles. Thus, the rate of accidents is below the statewide average and further investigation is not required.

Main Street/Suey Road. As shown in Table 10, there were 3 accidents at this intersection within the 3-year period. The rate of accidents was 0.20 accidents per million entering vehicles and the California statewide average for similar intersections is 0.55 accidents per million entering vehicles. Thus, the rate of accidents is below the statewide average and further investigation is not required.

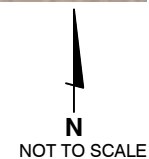
Main Street/Panther Drive. As shown in Table 10, there were 2 accidents at this intersection within the 3-year period. The rate of accidents was 0.26 accidents per million entering vehicles and the California statewide average for similar intersections is 0.43 accidents per million entering vehicles. Thus, the rate of accidents is below the statewide average and further investigation is not required.

## **RECOMMENDED IMPROVEMENT MEASURES**

### **Main Street/Project Access Road**

As discussed in the Site Access and Circulation section, the section of Main Street adjacent to the location of the proposed Project Access Road is currently configured with a center two way left-turn lane (TWLTL). It is recommended that the striping be modified to provide a dedicated eastbound left-turn with a minimum of 150 feet of storage (see Recommended Improvements section). The left-turn lane would provide a storage area of approximately 150 feet and then transition to a two-way-center left-turn lane that provides an additional storage area of approximately 450 feet to the Main Street/Suey Road intersection. Figure 11 illustrates the recommended improvement.





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## MAIN STREET/PROJECT ACCESS ROAD INTERSECTION IMPROVEMENT RECOMMENDATION

FIGURE

11

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## VMT ANALYSIS

Per the State's Natural Resource Agency Updated Guidelines for the Implementation of the CEQA adopted in 2018, Vehicle Miles Traveled (VMT) has been designated as the most appropriate measure of transportation impacts. "Vehicle Miles Traveled" refers to the amount and distance of automobile travel attributable to a project. Other relevant considerations may include the effects of the project on transit and non-motorized travel. For land use projects, vehicle miles traveled exceeding an applicable threshold of significance may indicate a significant impact. The Governor's Office of Planning and Research (OPR) published a Technical Advisory on Transportation that includes recommendations regarding assessment of VMT, thresholds of significance, and mitigation measures.<sup>4</sup> The Technical Advisory provides screening tools to determine when a project may have a significant VMT impacts.



The City of Santa Maria's adopted Environmental Procedures and Guidelines manual ("CEQA Guidelines")<sup>5</sup> contain thresholds and methodologies for assessing potential VMT impacts for Projects located in the City, which are reviewed below.

### Residential VMT Analysis

The potential VMT impacts associated with the residential portion of the Project are reviewed below.

#### *VMT Thresholds*

Consistent with CEQA Guidelines Section 15064.7, Thresholds of Significance, the City of Santa Maria has adopted the countywide baseline average of home-based VMT per population for residential projects and thresholds set at 85% of these countywide baseline averages for determining whether a project's VMT will be significant. The thresholds will be periodically updated as necessary during normal updates of the model baseline (approximately every five years).

New residential projects (single family, multi-family, mobile home) are required to generate less than 12.34 VMT per person (two-way trips). Projects that exceed this threshold may have a significant effect on the environment and will require project revisions and/or mitigation measures may be implemented to reduce the impact to less than significant. Mitigation strategies would be specific to the particular project and could include introducing mixed-use components, alternative transportation opportunities, pedestrian and/or transit network improvements, and traffic calming measures.

---

<sup>4</sup> Technical Advisory on Evaluating Transportation Impacts in CEQA, Governor's Office of Planning and Research, December 2018.

<sup>5</sup> City of Santa Maria Environmental Procedures and Guidelines, City of Santa Maria, Amended November 3, 2020.



## VTM Analysis

City staff utilized the City's VMT calculator to develop VMT estimates for the residential portion of the Project (results attached). The VMT calculator indicated that the residential portion of the Project would generate 17.60 VMT per person, which is more than the threshold of 12.34 VMT per person. The residential portion of the Project would therefore have a significant VMT impact based on City thresholds. It is noted that the City's VMT screening map, presented on Figure 12, shows that the Project is located in an area that generates up to the average VMT per capita (14.52 two-way trips), which is 30% less than the range in the City's VMT calculator. Thus, there is a significant discrepancy between the City's VMT calculator and the VMT screening map which is presumably based on the same model as the calculator. Table 11 presents the results of the VMT analysis based on the VMT calculator and the VMT screening map.

**Table 11**  
**Residential Component VMT Comparison to City Threshold**

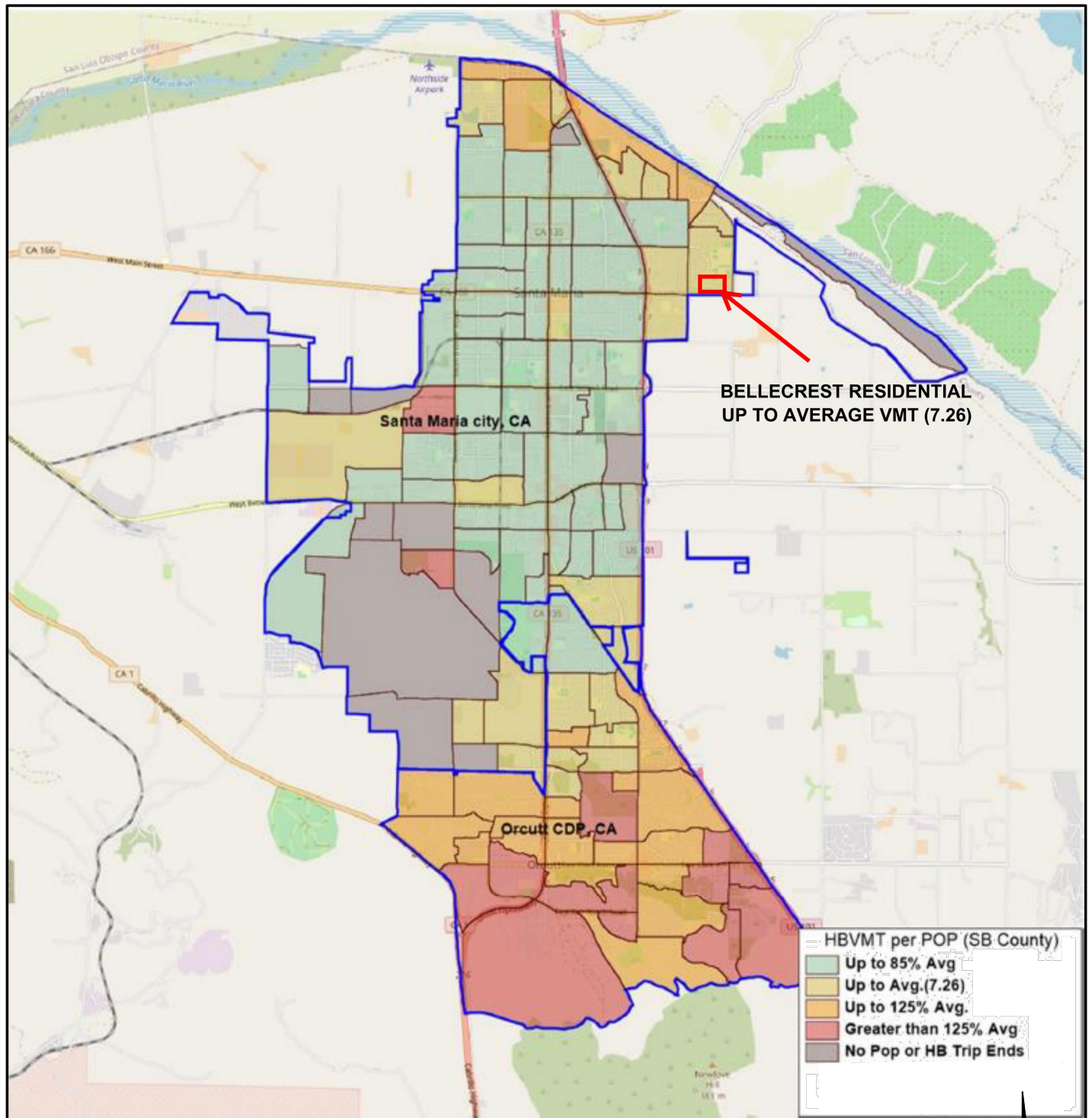
<b>VMT Estimate Source</b>	<b>VMT Estimate</b>	<b>City of Santa Maria VMT Threshold</b>	<b>Potential Impact?</b>
City of Santa Maria VMT Sketch Planning Tool	17.60 VMT Per Capita	12.34 VMT Per Capita	YES
VMT Screening Map	14.52 VMT Per Capita	12.34 VMT Per Capita	Yes

As noted, the Project is proposing to develop small senior detached and attached units ranging in size from 712 SF square feet to 1,413 SF which are more like apartments. These senior units would generate substantially less traffic than standard single family homes. The Project site is located in a traffic model zone that contains predominantly single family homes, thus the baseline VMT estimates produced by the model and shown on the VMT screening map for the Project site do not accurately reflect the type of senior housing proposed. Table 12 provides a comparison of the trip generation rates for senior housing units (single-family and multifamily) and single-family housing units.

**Table 12**  
**Project Trip Generation – Senior Adult Housing vs Single-Family Housing**

<b>Land use</b>	<b>ADT Rate</b>	<b>AM Peak Rate</b>	<b>PM Peak Rate</b>
Senior Adult Housing - Single-Family	4.31/Unit	0.24/Unit	0.30/Unit
Single-Family Housing	9.43/Unit	0.70/Unit	0.94/Unit
<b>Percent Reduction</b>	<b>-54%</b>	<b>-66%</b>	<b>-68%</b>
Senior Adult Housing - MultiFamily	3.24/Unit	0.20/Unit	0.25/Unit
Single-Family Housing	9.43/Unit	0.70/Unit	0.94/Unit
<b>Percent Reduction</b>	<b>-66%</b>	<b>-71%</b>	<b>-73%</b>

# Countywide Average: Home-Based VMT per Population (Residential Land Uses)



N  
NOT TO SCALE



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## CITY OF SANTA MARIA VMT SCREENING MAP

FIGURE 12

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The data presented in Table 12 show that the senior adult housing – single-family units are forecast to generate 54% less average daily traffic, 66% less AM peak hour traffic, and 68% less PM peak hour traffic than single-family housing units; and the senior adult housing – multifamily units are forecast to generate 66% less average daily traffic, 71% less AM peak hour traffic, and 73% less PM peak hour traffic than single-family housing units.

The City's VMT calculator and VMT screening map do not have the flexibility to account for the type of senior residential units proposed, instead they are based on the attributes of the existing single family houses located in the Project study area and model zone. The senior housing units generate significantly less traffic than single family units and the trip lengths associated with the senior housing units would be much lower than the adjacent single-family units, thus the resulting per capita VMT estimates would be much lower than forecast.

It is recommended that adjustments be applied to the VMT forecasts shown on the City's VMT screening map to account for the type of senior housing proposed. Given that the senior units would generate 54%-66% less average traffic than single family units and the senior residents would have much shorter trip lengths, a VMT adjustment of 35% to 45% could be justified. *This would result in VMT estimates that would be less than the City's VMT impact thresholds.* Table 13 summarizes the results of the VMT analysis with the adjustment.

**Table 13**  
**Residential Component VMT Comparison to City Threshold – With Adjustment**

<b>VMT Estimate Source</b>	<b>VMT Estimate</b>	<b>35% VMT Reduction Factor</b>	<b>City of Santa Maria VMT Threshold</b>	<b>Potential Impact?</b>
City of Santa Maria VMT Sketch Planning Tool	17.60 VMT Per Capita	11.44	12.34 VMT Per Capita	NO
VMT Screening Map	14.52 VMT Per Capita	9.44	12.34 VMT Per Capita	NO

■ ■ ■

## REFERENCES AND PERSONS CONTACTED

### Associated Transportation Engineers

Scott A. Schell, Principal Transportation Planner  
Glenn Manaois, Transportation Engineer I

### Persons Contacted

Mark Mueller, PE, City of Santa Maria  
Luis Magallon, PE, City of Santa Maria  
Dana Eady, Planning Division Manager, City of Santa Maria

### References

Trip Generation, Institute of Transportation Engineers, 11th Edition, 2021.

Highway Capacity Manual, Transportation Research Board, 7<sup>th</sup> Edition, 2022.

Highway Design Manual, California Department of Transportation, July 2020.

Technical Advisory on Evaluating Transportation Impacts in CEQA, Governor's Office of Planning and Research, December 2018.

City of Santa Maria Environmental Procedures and Guidelines, City of Santa Maria, Amended November 3, 2020

## TECHNICAL APPENDIX

### CONTENTS:

LEVEL OF SERVICE DEFINITIONS

SANTA MARIA TRANSIT ROUTE 3 MAP

TRAFFIC COUNT DATA

PROJECT TRIP GENERATION CALCULATION WORKSHEET

CITY OF SANTA MARIA APPROVED AND PENDING PROJECTS LIST

APPROVED AND PENDING PROJECT TRIP GENERATION WORKSHEET

ACCIDENT DATA AND CALCULATION WORKSHEETS

PROJECT DRIVEWAY QUEUING ANALYSIS WORKSHEETS

VMT CALCULATOR RESULTS

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PROJECT DRIVEWAY LEVEL OF SERVICE CALCULATION WORKSHEETS

- Reference 1 - Main Street/Project Driveway

## **LEVEL OF SERVICE DEFINITIONS**





# ASSOCIATED TRANSPORTATION ENGINEERS

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Richard L. Pool, P.E.  
Scott A. Schell

## Signalized Intersection Level of Service Definitions

LOS	Delay (a)	V/C Ratio	Definition
A	< 10.0	< 0.60	Progression is extremely favorable. Most vehicles arrive during the green phase. Many vehicles do not stop at all.
B	10.1 - 20.0	0.61 - 0.70	Good progression, short cycle lengths, or both. More vehicles stop than with LOS A, causing higher levels of delay.
C	20.1 - 35.0	0.71 - 0.80	Only fair progression, longer cycle lengths, or both, result in higher cycle lengths. Cycle lengths may fail to serve queued vehicles, and overflow occurs. Number of vehicles stopped is significant, though many still pass through intersection without stopping.
D	35.1 - 55.0	0.81 - 0.90	Congestion becomes more noticeable. Unfavorable progression, long cycle lengths and high v/c ratios result in longer delays. Many vehicles stop, and the proportion of vehicles not stopping declines. Individual cycle failures are noticeable.
E	55.1 - 80.0	0.91 - 1.00	High delay values indicate poor progression, long cycle lengths and high v/c ratios. Individual cycle failures are frequent
F	> 80.0	> 1.00	Considered unacceptable for most drivers, this level occurs when arrival flow rates exceed the capacity of lane groups, resulting in many individual cycle failures. Poor progression and long cycle lengths may also contribute to high delay levels.

(a) Average control delay per vehicle in seconds.

## Unsignalized Intersection Level of Service Definitions

The HCM<sup>1</sup> uses *control delay* to determine the level of service at unsignalized intersections. Control delay is the difference between the travel time actually experienced at the control device and the travel time that would occur in the absence of the traffic control device. Control delay includes deceleration from free flow speed, queue move-up time, stopped delay and acceleration back to free flow speed.

LOS	Control Delay Seconds per Vehicle
A	< 10.0
B	10.1 - 15.0
C	15.1 - 25.0
D	25.1 - 35.0
E	35.1 - 50.0
F	> 50.0

<sup>1</sup> Highway Capacity Manual, National Research Board, 2016.

## **SANTA MARIA TRANSIT ROUTE 3 MAP**

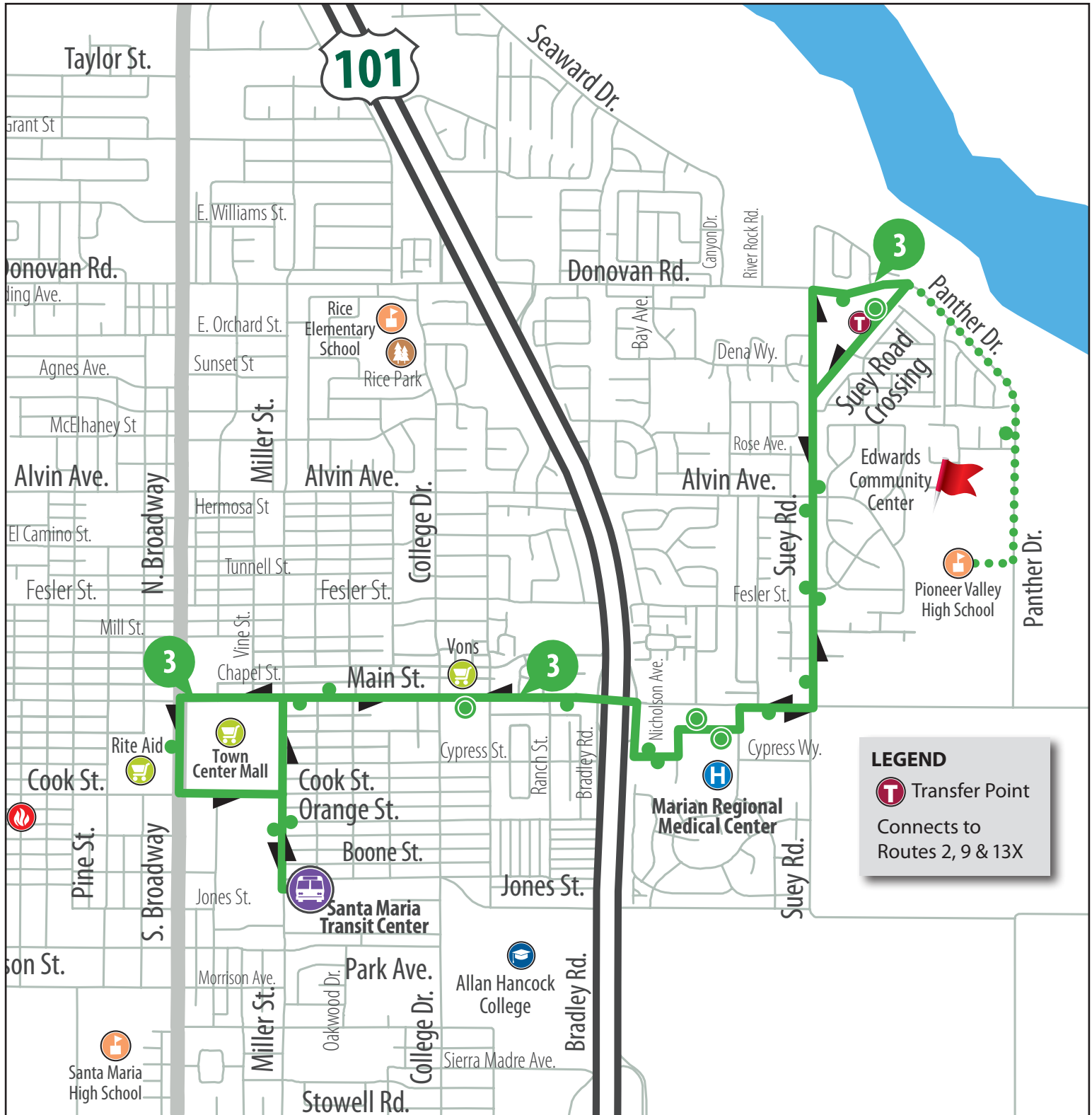


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**ROUTE 3**

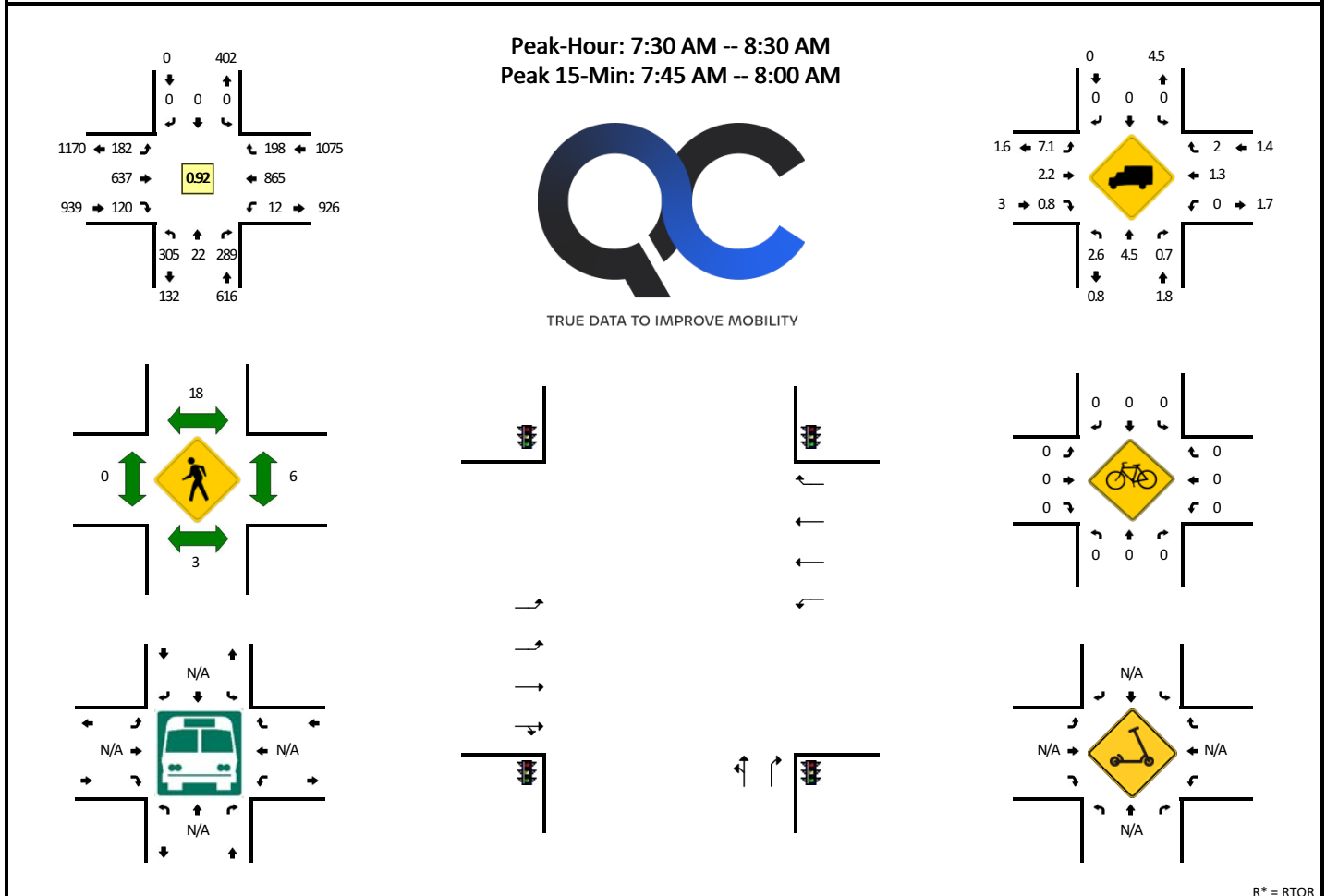
## Transit Center to Marian Hospital to PVH School, via E. Main, Suey Ln.



## TRAFFIC COUNT DATA

**LOCATION:** US 101 NB On Ramp/Nicholson Ave -- E Main St  
**CITY/STATE:** Santa Maria, CA

**QC JOB #:** 16382901  
**DATE:** Thu, Nov 9 2023



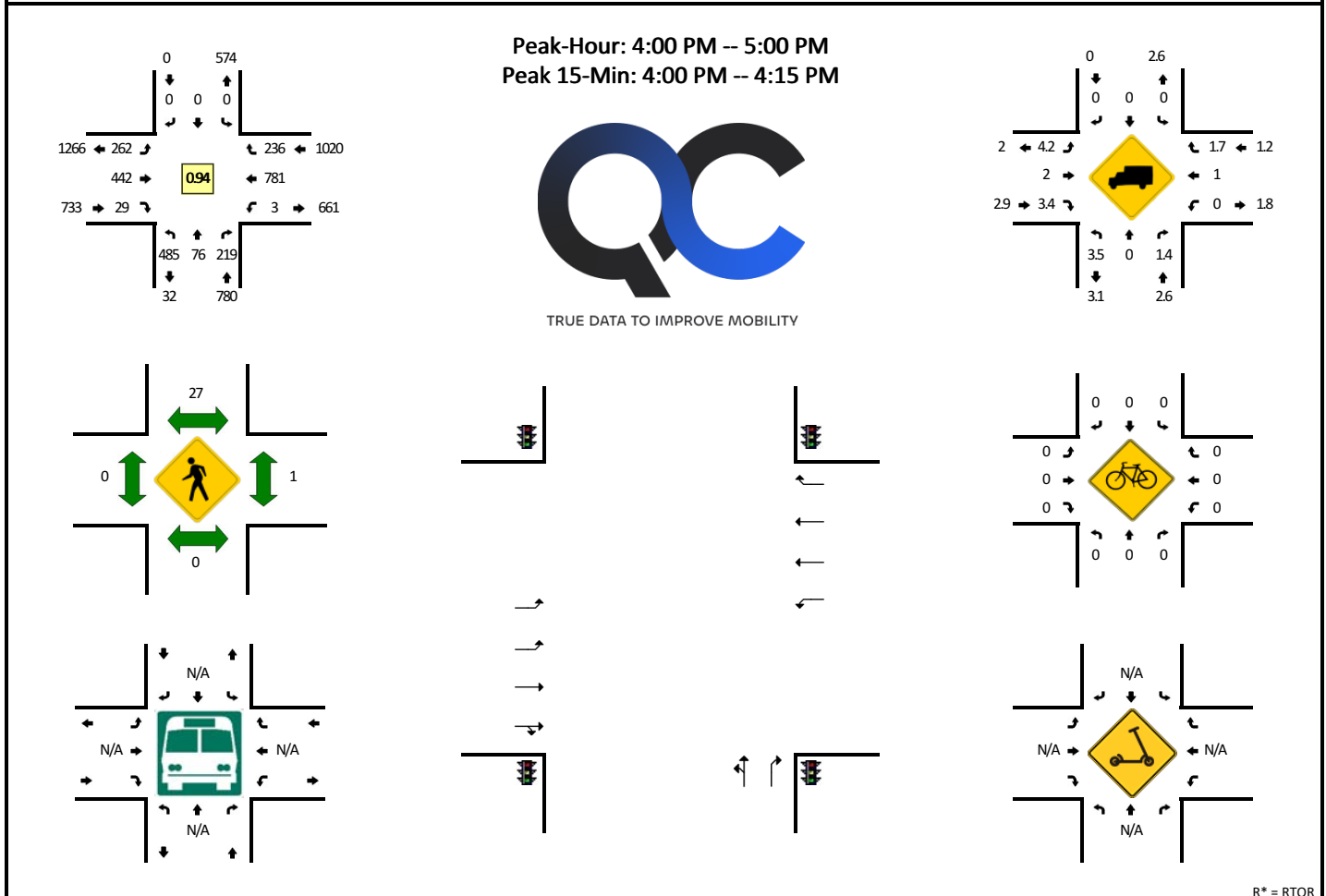
R\* = RTOR

15-Min Count Period Beginning At	US 101 NB On Ramp/Nicholson Ave (Northbound)					US 101 NB On Ramp/Nicholson Ave (Southbound)					E Main St (Eastbound)					E Main St (Westbound)					Total	Hourly Totals
	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*		
7:00 AM	41	3	5	0	20	0	0	0	0	0	56	66	10	0	0	0	75	16	0	25	317	
7:15 AM	47	3	12	0	23	0	0	0	0	0	55	86	18	0	2	1	118	36	0	24	425	
7:30 AM	65	9	36	0	30	0	0	0	0	0	65	137	20	0	4	5	170	30	0	28	599	
7:45 AM	83	4	54	0	23	0	0	0	0	0	36	183	34	0	3	3	244	20	0	29	716	2057
8:00 AM	87	2	52	0	28	0	0	0	0	0	34	166	20	0	5	3	233	22	0	21	673	2413
8:15 AM	70	7	36	0	30	0	0	0	0	0	47	151	31	0	3	1	218	30	0	18	642	2630
8:30 AM	70	9	37	0	31	0	0	0	0	0	49	112	20	0	1	0	210	25	0	28	592	2623
8:45 AM	78	10	23	0	23	0	0	0	0	0	40	130	23	0	2	2	123	13	0	19	486	2393
Peak 15-Min Flowrates	Northbound					Southbound					Eastbound					Westbound					Total	
	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*		
All Vehicles	332	16	308	0	92	0	0	0	0	0	144	732	148	0	12	12	976	196	0	116	3084	
Heavy Trucks	8	0	0			0	0	0			12	8	0			0	16	0			44	
Buses																						
Pedestrians		0					16					0					0				16	
Bicycles	0	0	0			0	0	0			0	0	0			0	0	0			0	
Scooters																						

**Comments:**

**LOCATION:** US 101 NB On Ramp/Nicholson Ave -- E Main St  
**CITY/STATE:** Santa Maria, CA

**QC JOB #:** 16382902  
**DATE:** Thu, Nov 9 2023



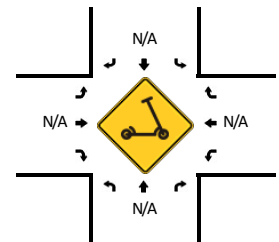
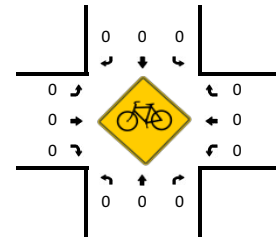
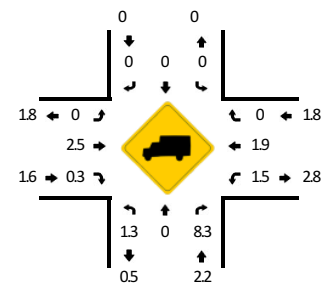
R\* = RTOR

15-Min Count Period Beginning At	US 101 NB On Ramp/Nicholson Ave (Northbound)					US 101 NB On Ramp/Nicholson Ave (Southbound)					E Main St (Eastbound)					E Main St (Westbound)					Total	Hourly Totals
	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*		
4:00 PM	130	15	35	0	30	0	0	0	0	0	65	126	10	0	0	1	195	38	0	28	673	
4:15 PM	117	20	15	0	19	0	0	0	0	0	52	94	8	0	1	1	206	20	0	31	584	
4:30 PM	115	22	37	0	27	0	0	0	0	0	78	114	2	0	1	0	195	35	0	36	662	
4:45 PM	123	19	28	0	28	0	0	0	0	0	67	108	7	0	0	1	185	25	0	23	614	2533
5:00 PM	120	33	32	0	28	0	0	0	0	0	78	91	8	0	3	0	185	45	0	30	653	2513
5:15 PM	119	11	45	0	26	0	0	0	0	0	85	101	9	0	3	0	132	29	0	22	582	2511
5:30 PM	101	12	49	0	29	0	0	0	0	0	116	103	8	0	3	1	158	19	0	22	621	2470
5:45 PM	87	9	37	0	28	0	0	0	0	0	65	119	8	0	1	1	152	18	0	19	544	2400
Peak 15-Min Flowrates	Northbound					Southbound					Eastbound					Westbound					Total	
	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*		
All Vehicles	520	60	260	0	120	0	0	0	0	0	260	504	40	0	0	4	780	264	0	112	2924	
Heavy Trucks	20	0	4			0	0	0			16	8	0			0	4	4			56	
Buses																						
Pedestrians		0					20					0					4				24	
Bicycles	0	0	0			0	0	0			0	0	0			0	0	0			0	
Scoters																						

**Comments:**

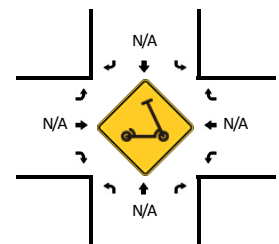
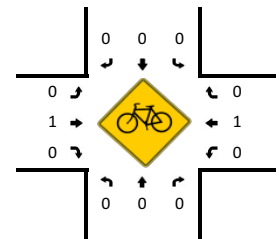
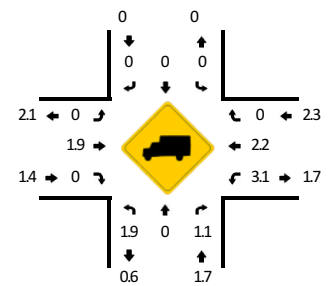


QC JOB #: 16382903  
DATE: Thu, Nov 9 2023

[illegible]

SOURCE: Quality Counts, LLC (<http://www.qualitycounts.net>) 1-877-580-2212

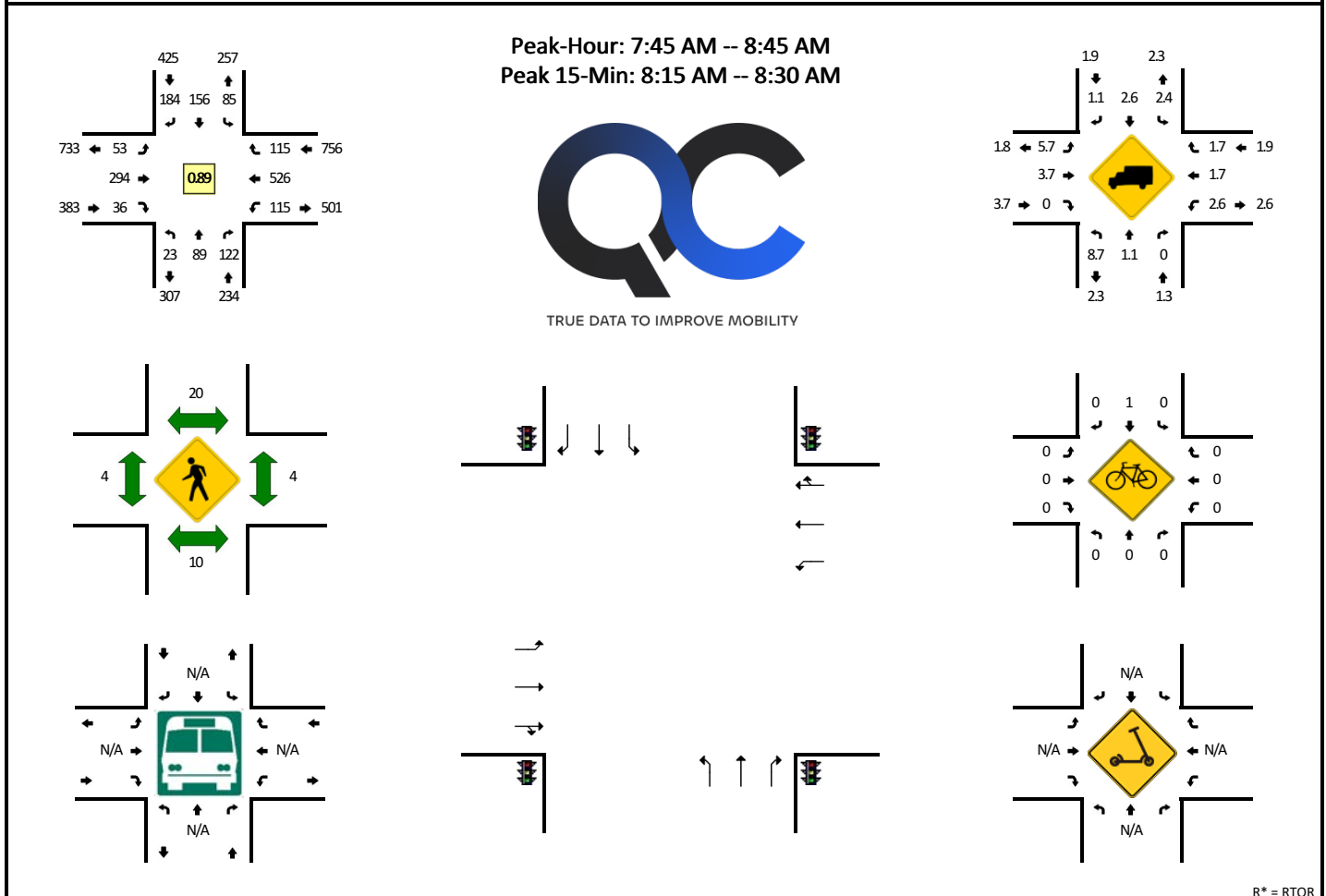
QC JOB #: 16382904  
DATE: Thu, Nov 9 2023

[illegible]

SOURCE: Quality Counts, LLC (<http://www.qualitycounts.net>) 1-877-580-2212

**LOCATION:** Suey Rd -- E Main St  
**CITY/STATE:** Santa Maria, CA

**QC JOB #:** 16382905  
**DATE:** Thu, Nov 9 2023



R\* = RTOR

15-Min Count Period Beginning At	Suey Rd (Northbound)					Suey Rd (Southbound)					E Main St (Eastbound)					E Main St (Westbound)					Total	Hourly Totals
	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*		
7:00 AM	2	14	1	0	3	6	25	5	0	24	5	14	8	0	2	4	20	1	0	2	136	
7:15 AM	2	12	2	0	3	8	26	16	0	23	13	27	4	0	3	8	36	3	0	3	189	
7:30 AM	6	22	7	0	13	11	36	15	0	21	16	44	4	0	2	18	70	11	0	1	297	
7:45 AM	5	16	14	0	16	14	55	40	0	28	17	87	3	0	3	34	111	16	0	3	462	1084
8:00 AM	4	26	22	0	22	38	39	21	0	17	13	91	10	0	3	25	132	22	0	9	494	1442
8:15 AM	5	32	13	0	23	30	37	26	0	15	9	75	2	0	4	32	163	39	0	2	507	1760
8:30 AM	9	15	8	0	4	3	25	17	0	20	14	41	8	0	3	24	120	20	0	4	335	1798
8:45 AM	7	5	1	0	6	5	25	9	0	11	12	33	4	0	1	8	33	2	0	3	165	1501
Peak 15-Min Flowrates	Northbound					Southbound					Eastbound					Westbound					Total	
	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*		
All Vehicles	20	128	144	0	92	120	148	164	0	60	36	300	24	0	16	128	652	164	0	8	2204	
Heavy Trucks	0	0	0			4	0	8			4	16	0			4	8	4			48	
Buses																						
Pedestrians		4					28					4					0				36	
Bicycles	0	0	0			0	0	0			0	0	0			0	0	0			0	
Scoters																						

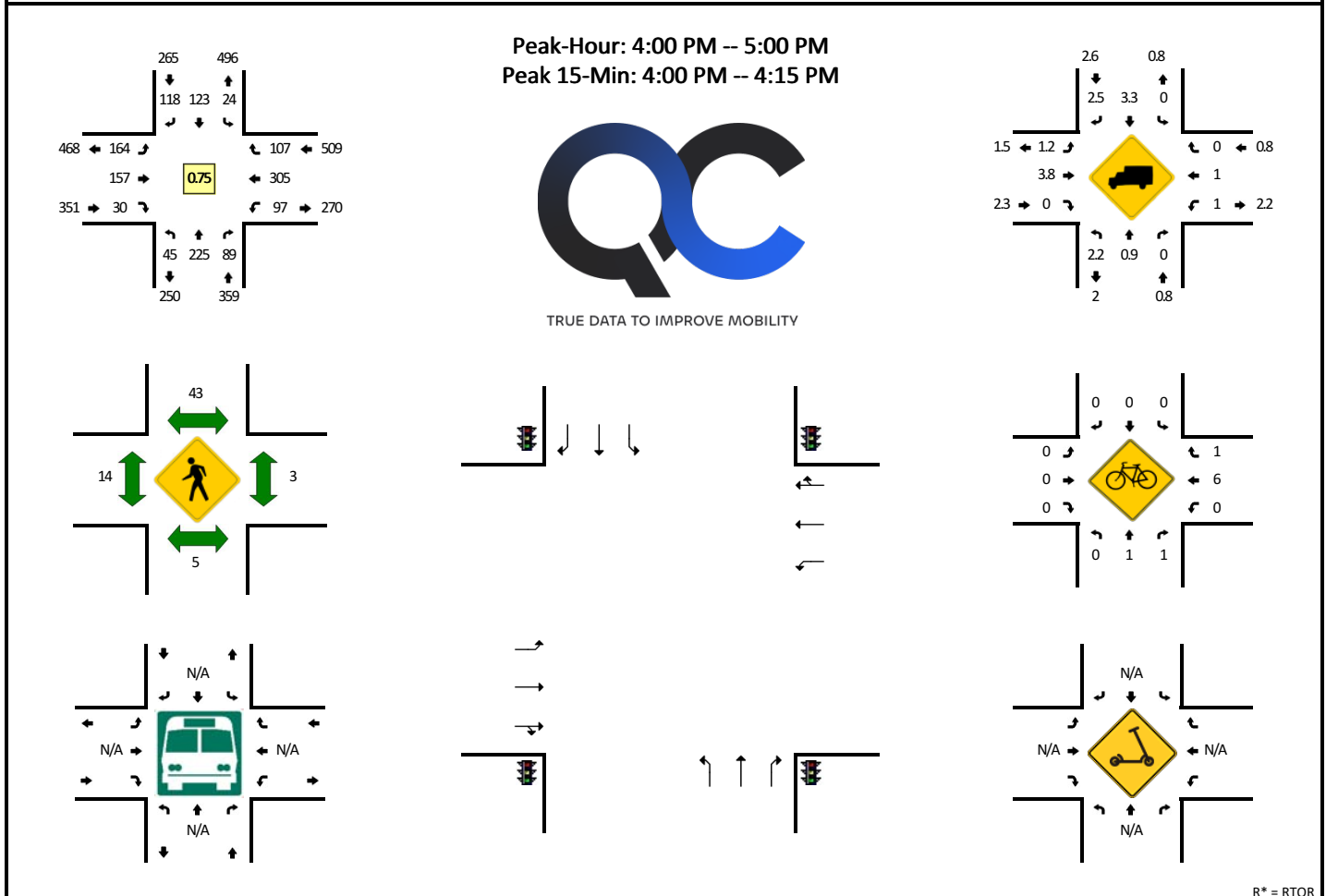
**Comments:**

Report generated on 11/27/2023 4:49 PM

SOURCE: Quality Counts, LLC (<http://www.qualitycounts.net>) 1-877-580-2212

**LOCATION:** Suey Rd -- E Main St  
**CITY/STATE:** Santa Maria, CA

**QC JOB #:** 16382906  
**DATE:** Thu, Nov 9 2023



R\* = RTOR

15-Min Count Period Beginning At	Suey Rd (Northbound)					Suey Rd (Southbound)					E Main St (Eastbound)					E Main St (Westbound)					Total	Hourly Totals
	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*		
4:00 PM	17	55	17	0	13	10	33	12	0	11	37	41	6	0	1	43	140	56	0	3	495	
4:15 PM	10	52	8	0	13	3	32	16	0	23	43	32	4	0	3	30	79	23	0	6	377	
4:30 PM	14	61	8	0	10	4	26	11	0	18	43	39	5	0	3	13	51	11	0	1	318	
4:45 PM	4	57	7	0	13	7	32	13	0	14	41	45	7	0	1	11	35	4	0	3	294	1484
5:00 PM	8	61	9	0	11	5	39	9	0	16	42	29	4	0	5	14	37	8	0	5	302	1291
5:15 PM	6	62	4	0	13	4	36	14	0	11	35	29	6	0	2	15	29	9	0	6	281	1195
5:30 PM	7	60	8	0	17	7	38	16	0	20	40	52	3	0	2	8	38	4	0	4	324	1201
5:45 PM	11	35	8	0	11	1	31	11	0	24	36	52	2	0	1	13	40	7	0	4	287	1194
Peak 15-Min Flowrates	Northbound					Southbound					Eastbound					Westbound					Total	
	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*		
All Vehicles	68	220	120	0	52	40	132	92	0	44	148	164	28	0	4	172	560	236	0	12	2092	
Heavy Trucks	0	0	0			0	4	0			4	0	0			0	0	0			8	
Buses																						
Pedestrians		0					40					20					0				60	
Bicycles	0	0	4			0	0	0			0	0	0			0	12	4			20	
Scoters																						

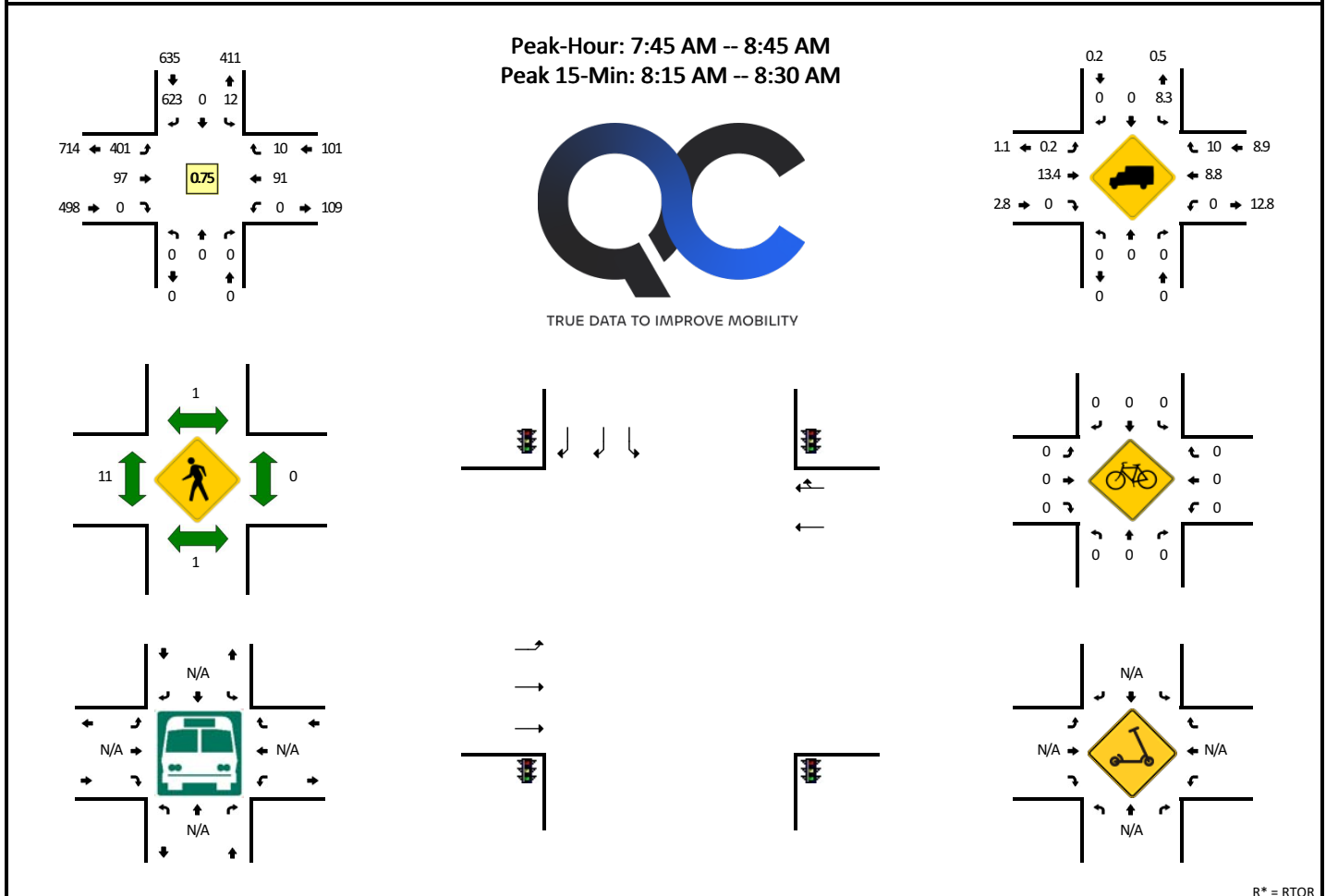
*Comments:*

Report generated on 11/27/2023 4:49 PM

SOURCE: Quality Counts, LLC (<http://www.qualitycounts.net>) 1-877-580-2212

**LOCATION:** Panther Dr -- E Main St  
**CITY/STATE:** Santa Maria, CA

**QC JOB #:** 16382907  
**DATE:** Thu, Nov 9 2023



R\* = RTOR

15-Min Count Period Beginning At	Panther Dr (Northbound)					Panther Dr (Southbound)					E Main St (Eastbound)					E Main St (Westbound)					Total	Hourly Totals
	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*		
7:00 AM	0	0	0	0	0	1	0	10	0	8	15	8	0	0	0	0	6	0	0	0	48	
7:15 AM	0	0	0	0	0	4	0	16	0	19	31	9	0	0	0	0	10	0	0	0	89	
7:30 AM	0	0	0	0	0	2	0	19	0	53	51	12	0	0	0	0	22	0	0	0	159	
7:45 AM	0	0	0	0	0	2	0	22	0	100	110	12	0	0	0	0	21	1	0	0	268	564
8:00 AM	0	0	0	0	0	2	0	40	0	130	142	36	0	0	0	0	12	3	0	0	365	881
8:15 AM	0	0	0	0	0	5	0	61	0	158	116	38	0	0	0	0	30	0	0	4	412	1204
8:30 AM	0	0	0	0	0	3	0	32	0	80	33	11	0	0	0	0	28	2	0	0	189	1234
8:45 AM	0	0	0	0	0	6	0	7	0	23	29	18	0	0	0	0	16	1	0	1	101	1067
Peak 15-Min Flowrates	Northbound					Southbound					Eastbound					Westbound					Total	
	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*		
All Vehicles	0	0	0	0	0	20	0	876	0	632	464	152	0	0	0	0	120	16	0	16	2296	
Heavy Trucks	0	0	0			0	0	0			0	16	0			0	16	0			32	
Buses																						
Pedestrians		4					0					16					0				20	
Bicycles	0	0	0			0	0	0			0	0	0			0	0	0			0	
Scoters																						

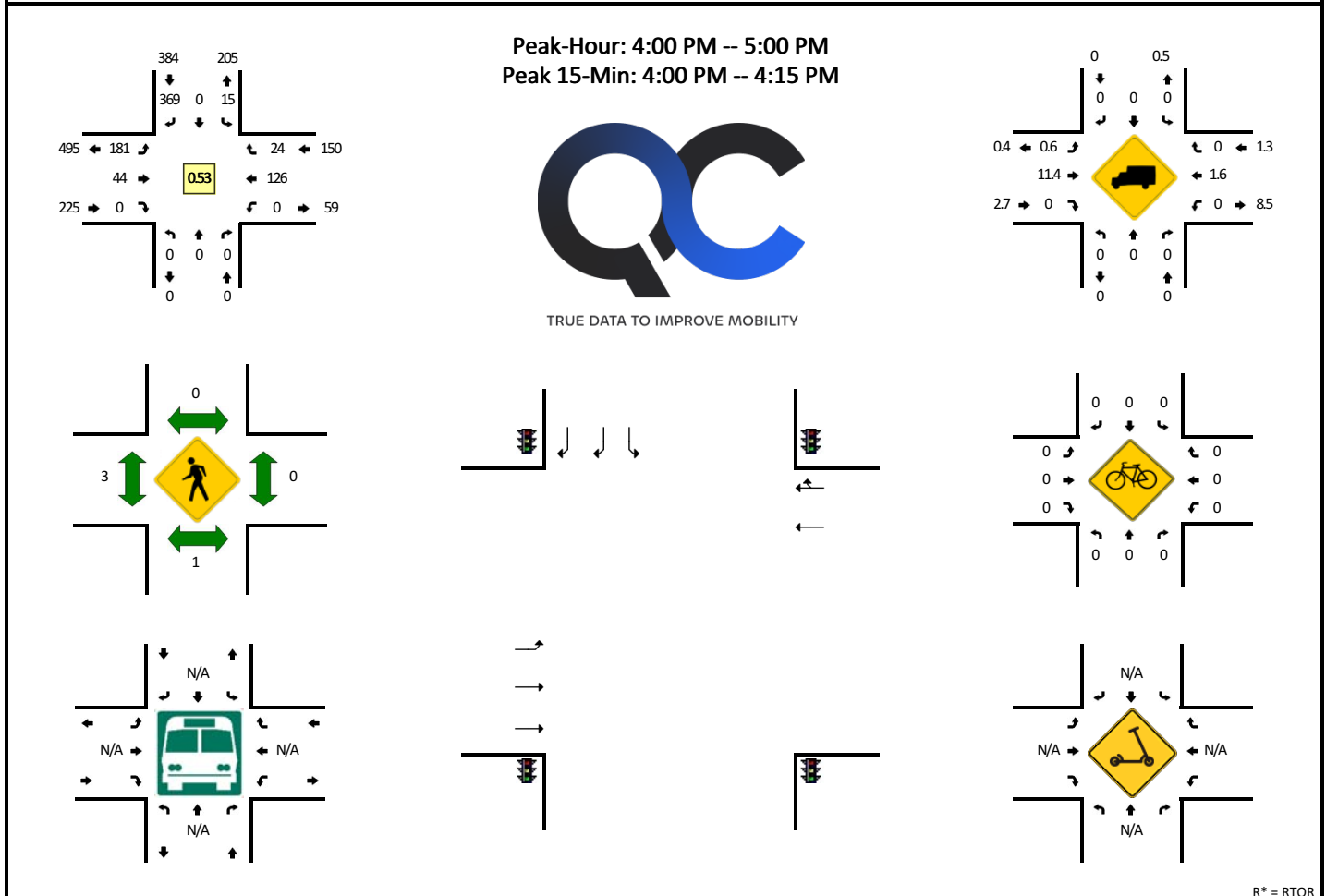
*Comments:*

Report generated on 11/27/2023 4:49 PM

SOURCE: Quality Counts, LLC (<http://www.qualitycounts.net>) 1-877-580-2212

**LOCATION:** Panther Dr -- E Main St  
**CITY/STATE:** Santa Maria, CA

**QC JOB #:** 16382908  
**DATE:** Thu, Nov 9 2023



R\* = RTOR

15-Min Count Period Beginning At	Panther Dr (Northbound)					Panther Dr (Southbound)					E Main St (Eastbound)					E Main St (Westbound)					Total	Hourly Totals
	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*		
4:00 PM	0	0	0	0	0	5	0	91	0	127	63	11	0	0	0	0	56	3	0	1	357	
4:15 PM	0	0	0	0	0	4	0	16	0	56	36	14	0	0	0	0	31	8	0	1	166	
4:30 PM	0	0	0	0	0	5	0	22	0	34	39	10	0	0	0	0	25	8	0	1	144	
4:45 PM	0	0	0	0	0	1	0	2	0	21	43	9	0	0	0	0	14	2	0	0	92	759
5:00 PM	0	0	0	0	0	1	0	12	0	27	30	16	0	0	0	0	23	6	0	1	116	518
5:15 PM	0	0	0	0	0	0	0	6	0	36	35	9	0	0	0	0	18	4	0	0	108	460
5:30 PM	0	0	0	0	0	1	0	2	0	33	47	14	0	0	0	0	16	3	0	0	116	432
5:45 PM	0	0	0	0	0	0	0	4	0	45	55	7	0	0	0	0	11	1	0	0	123	463
Peak 15-Min Flowrates	Northbound					Southbound					Eastbound					Westbound					Total	
	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*	Left	Thru	Right	U	R*		
All Vehicles	0	0	0	0	0	20	0	872	0	508	252	44	0	0	0	0	224	16	0	4	1940	
Heavy Trucks	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Buses	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Pedestrians	0	0	0	0	0	0	0	0	0	0	12	0	0	0	0	0	0	0	0	0	12	
Bicycles	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Scooters	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	

**Comments:**

Report generated on 11/27/2023 4:49 PM

SOURCE: Quality Counts, LLC (<http://www.qualitycounts.net>) 1-877-580-2212



## **PROJECT TRIP GENERATION CALCULATION WORKSHEET**

Associated Transportation Engineers #22086.01  
Trip Generation Worksheet

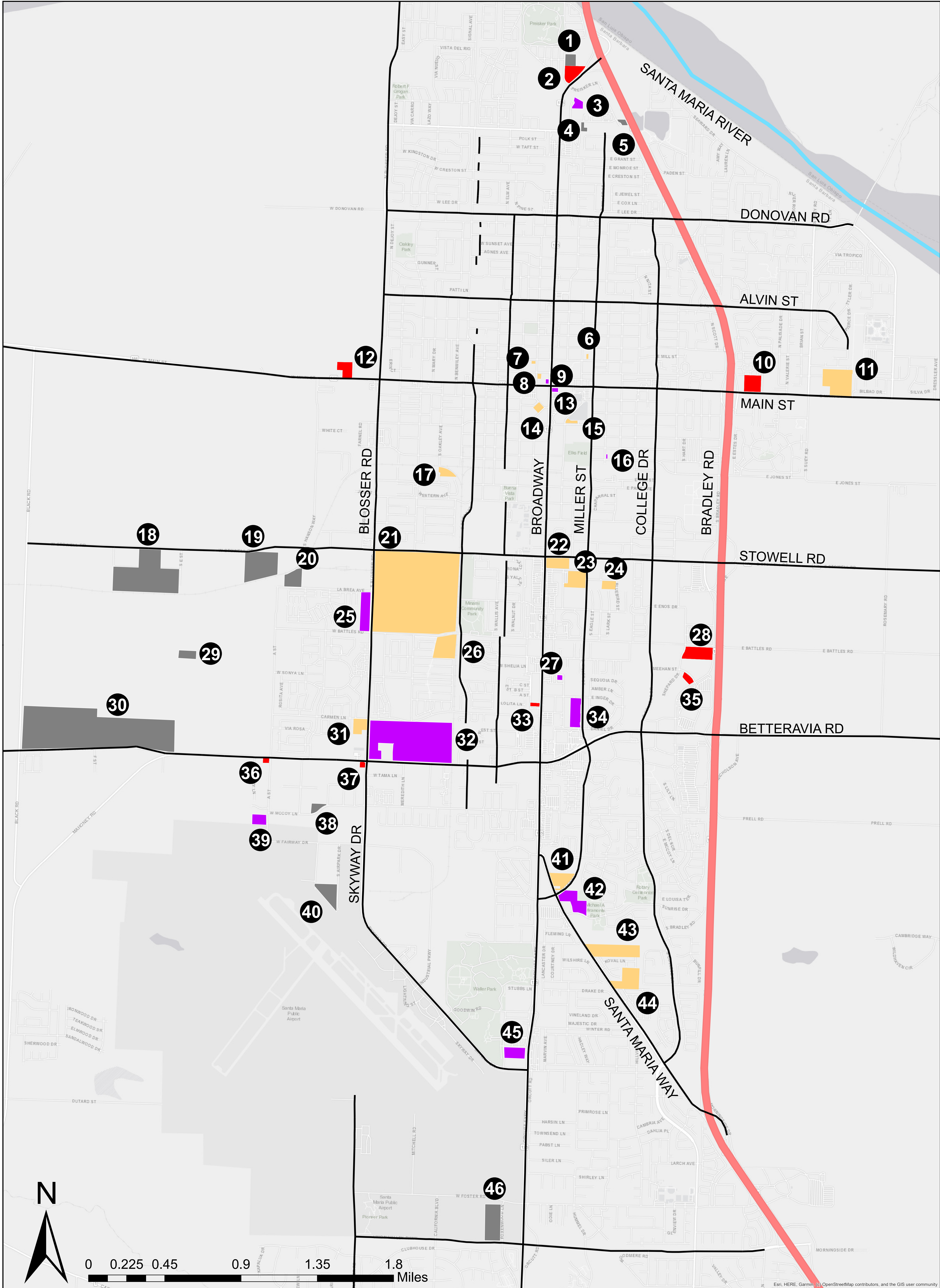
BELLECREST SENIOR RESIDENTIAL PROJECT

Use	Size	Internal-Trip Factor	ADT		AM PEAK HOUR						PM PEAK HOUR					
			Rate	Trips	Rate	Trips	In %	Trips	Out %	Trips	Rate	Trips	In %	Trips	Out %	Trips
PROPOSED																
Senior Apartments (a)	142 DU	1.00	4.31	612	0.24	34	33%	11	67%	23	0.30	43	61%	26	39%	17
Totals				612		34		11		23		43		26		17

(a) Trip generation based on ITE rates for Senior Adult Housing - Single-Family (ITE #251).

## **CITY OF SANTA MARIA APPROVED AND PENDING PROJECTS LIST**





Residential

- 6

309 Mill Apartments  
309 E Mill St  
23 unit apartments
- 7

200 Mill Apartments  
200 W Mill St  
20 unit apartments
- 8

Vino Bella Apartments  
120 W Chapel St  
32 unit apartments
- 11

Bellecrest Residences (Paradiso)  
1571 E Main St  
142 single family senior homes
- 14

Heritage Walk Lofts  
201 Town Center West  
102 residential units
- 15

Cook Street Apartments  
N of Cook & E of McClelland  
114 unit apartments
- 17

Oakley Court Apartments  
600 Block S Oackley Ct  
30 unit apartments
- 21

Blosser Ranch  
NE/c Blosser Rd & W Battles Rd  
338 "for rent" single family homes with 329 ADUs & 832 apartments
- 22

Vandenberg Senior Residence  
1314 S Broadway  
52 unit senior apartment addition
- 23

Centennial Square  
SW/c Miller St & Plaza Dr  
184 unit affordable apartments
- 24

Barcellus Senior Apartments  
502 E Barcellus Ave  
80 unit senior apartments
- 26

Centennial Gardens  
SW/c Battles St & Depot St  
160 unit affordable apartments
- 31

Avante Apartments  
SW/c of Carmen Ln & S Blosser Rd  
86 unit apartments
- 41

Santa Maria Studios  
2660 Santa Maria Way  
378 Senior Affordable Units
- 43

Northman Residential  
SM Way btw Sunrise Dr & E Dauphin St  
63 single family residences
- 44

Skylight Homes  
3170 Santa Maria Way  
49 single family homes

Commercial

- 2

Preisker Commercial Center  
N Broadway at Preisker Ln  
108 rm hotel, drive thru rest, retail
- 10

Starbucks at Home Motors  
1313 E Main St  
Coffee shop & drive-thru
- 12

Nutrien AG Solutions  
1300 block of West Main Street  
Outdoor storage & truck repair facility
- 28

Home Motors  
1004 E Battles Rd  
52,000 sq ft auto dealership
- 33

Mister Carwash  
1925 S Broadway  
Drive-thru carwash
- 35

Enos Auto Center South  
Lots 8-11 Enos Ranch  
Design/layout of auto center
- 35

Splash N Dash  
Lot 8 Enos Ranch  
8,200 sq ft car wash
- 36

A Street Deli  
W Betteravia Rd at A St  
4,420 sq ft retail bldg
- 37

Starbucks Drive-Thru Coffee  
1202 W. Betteravia  
Drive-thru only

Industrial

- 1

Preisker RV Storage  
2210 N Preisker Lane  
RV storage for 150 trailers
- 4

SMOOTH Bus Wash  
240 E Roemer Way  
1,134 sq ft bus wash building
- 5

Donahue Truck Center  
Preisker Lane  
Rental facility, truck sales & service
- 18

Bonita Packing Expansion  
1850 W Stowell Rd  
173,720 sq ft cooler addition
- 19

Maxco Box Facility  
1550 W Stowell Rd  
60,000 sq ft & outdoor storage
- 20

Seaside Warehouse  
La Brea Ave  
40,854 sq ft facility
- 29

SM Cooler & Box Facility  
1767 and 1795 A St  
130,000 sq ft cooler & box facility
- 30

Windset Farms Greenhouse  
1650 Black Rd  
4.3 mil sqft greenhouse & 93k bldg
- 38

Hardy Diagnostics  
1291 W McCoy Lane  
36,400 sq ft manufacturing, warehouse & office
- 40

2811 Center  
2811 Airpark Dr  
51,200 sq ft of office in 2 bldgs
- 46

SM Airport Foxenwood Self Storage  
3335 Corsair Circle  
101,450 sq ft mini-warehouse facility

Mixed Use/Other

- 3

Holiday Inn Express & Suites  
Roemer Court  
Four story hotel
- 9

Gateway Mixed Use  
101 N Broadway  
33,700 sq ft 4 story mixed use bldg
- 13

Alvin Newton Apartments  
SEC Main St and Broadway  
5 story mixed use bldg
- 16

Boone Street Market  
501 E Boone St  
2,280 sq ft add & 2 units
- 25

Westgate Village  
S Blosser Rd & W Battles Rd  
126 apts & 16k sq ft retail
- 27

Crucified Life Church  
NW/c S McClelland St  
11,700 sq ft church bldg
- 32

Betteravia Plaza  
W Betteravia Rd at SMVRR  
443 apts & 291,278 sq ft retail/office
- 34

Celebration I, II, III  
S Miller St at E Inger Dr  
56 homes/33 senior/7,000 sqft comm
- 34

Caring Hands Veterinary Clinic  
1995 S Miller St  
7,000 sq ft veterinary bldg
- 39

VTC Enterprises (Phase 2)  
2445 A St  
6,187 sq ft vocational training bldg
- 42

Park Edge Apartments  
SE/c Santa Maria Way & S Miller St  
140 apts & 5,435 sq ft comm
- 45

Elements Apartments (Lakeview Mixed Use Project)  
NW corner of Orcutt Expressway & Skyway Dr  
152 apartments & 9,800 sqft commercial



- RESIDENTIAL
- COMMERCIAL
- INDUSTRIAL
- MIXED USE/OTHER





## City of Santa Maria

### MAJOR DEVELOPMENTS (JULY 2023)

1	Project	<b>Preisker RV Storage</b>	Category	<b>Industrial</b>	File #s	Approved	Status
	Description	RV storage for 150 RV/trailers. Pumping site & modular unit for attendant	Acreage	3.3	<b>PD2022-0004</b>	<b>Pending</b>	Appeal of November 16, 2022
	Location	2210 N Preisker Lane	District	PD/C-2	<b>U2022-0004</b>	<b>Pending</b>	Planning Commission approval filed.
	APN(s)	128-002-035	Planner	<a href="#">Cody Graybehl</a>			Appeal in process.
	Contact	<a href="#">Jacob Weintraub, Applicant, 805-441-0332</a>					
2	Project	<b>Preisker Commercial Center</b>	Category	<b>Commercial</b>	File #s	Approved	Status
	Description	108 rm hotel and two drive-thru fast food restaurants totaling 8,300 sq. ft.	Acreage	5	<b>PD2015-0011</b>	<b>5/18/2016</b>	Planning permits for Chick-Fil-A under review (PD2023-0005).
	Location	NW/c N. Broadway and Preisker Ln	District	PD-f/C-2	<b>TR2016-0001</b>	<b>9/7/2016</b>	
	APN(s)	128-002-048, -049 & -050	Planner	<a href="#">Cody Graybehl</a>	<b>A2019-0004</b>	<b>2/18/2019</b>	
	Contact	<a href="#">Jody Walker Belsick, Applicant, 702-786-1829</a>			<b>PD2023-0005</b>	<b>Pending</b>	
3	Project	<b>Holiday Inn Express &amp; Suites</b>	Category	<b>Mixed/Other</b>	File #s	Approved	Status
	Description	New 4 story hotel, wood construction	Acreage	2.13	<b>PD2022-0001</b>	<b>Pending</b>	Planning permits under review.
	Location	Roemer Ct.	District	CM	<b>GPZ2022-0001</b>	<b>Pending</b>	
	APN(s)	128-003-047, -048	Planner	<a href="#">Cody Graybehl</a>			
	Contact	<a href="#">Prakash Patel, Applicant, 669-333-1880</a>					
4	Project	<b>SMOOTH Bus Wash</b>	Category	<b>Industrial</b>	File #s	Approved	Status
	Description	1,134 sq. ft. bus wash building	Acreage	1.2	<b>PD2017-0023</b>	<b>5/16/2018</b>	Planning permit expiration on 5/16/2023
	Location	240 E. Roemer Way	District	PD/M-1	<b>A2021-0004</b>	<b>8/4/2021</b>	
	APN(s)	128-003-046	Planner	<a href="#">Carol Ziesenhenn</a>			
	Contact	<a href="#">Tom Martinez, Architect, 805-934-5737</a>					
5	Project	<b>Donahue Truck Center</b>	Category	<b>Industrial</b>	File #s	Approved	Status
	Description	Rental facility, truck sales and service	Acreage	1.53	<b>PD2022-0016</b>	<b>Pending</b>	Planning permits under review.
	Location	Preisker Lane	District	PD-F/CM			
	APN(s)	128-003-008	Planner	<a href="#">Cody Graybehl</a>			
	Contact	<a href="#">Thele-Donahue, LLC</a>					
6	Project	<b>309 Mill Apartments</b>	Category	<b>Residential</b>	File #s	Approved	Status
	Description	Construct a 23 unit, 9750 sq. ft. apartment building	Acreage	0.2	<b>DT2020-0015</b>	<b>Pending</b>	Planning permits under review.
	Location	309 E Mill St	District	DTSP - Bungalow District			
	APN(s)	121-193-011	Planner	<a href="#">Greg Vine</a>			
	Contact	<a href="#">Jason Heyward, Consultant, 805-928-8948</a>					
7	Project	<b>200 Mill Apartments</b>	Category	<b>Residential</b>	File #s	Approved	Status
	Description	Construct a 20 unit, 3-story building	Acreage	0.17	<b>DT2022-0019</b>	<b>Pending</b>	Planning permits under review.
	Location	200 W Mill Street	District	DTSP- Bungalow			
	APN(s)	119-273-007	Planner	<a href="#">Frank Alb</a>			
	Contact	<a href="#">CHG South Pine, LLC, Applicant</a>					
8	Project	<b>Vino Bella Apartments</b>	Category	<b>Residential</b>	File #s	Approved	Status
	Description	Construct a 32 unit, 3-story apartment building	Acreage	0.3	<b>DT2020-0017</b>	<b>12/16/2020</b>	Building permits submitted. Planning permit expiration on 12/16/2023.
	Location	120 W Chapel St	District	DTSP - Bungalow District			
	APN(s)	119-276-015	Planner	<a href="#">Frank Alb</a>			
	Contact	<a href="#">Ben Nikfarjam, Applicant, 310-215-4882</a>					
9	Project	<b>Gateway Mixed Use</b>	Category	<b>Mixed/Other</b>	File #s	Approved	Status
	Description	33,700 sq. ft., four-story mixed use development	Acreage	0.3	<b>DT2017-0033</b>	<b>1/16/2018</b>	Under construction.
	Location	101 N. Broadway	District	DTSP - Gateway	<b>A2019-0032</b>	<b>9/4/2019</b>	
	APN(s)	119-276-019	Planner	<a href="#">Frank Alb</a>			
	Contact	<a href="#">Ben Nikfarjam, Developer, 310-251-4882</a>					
10	Project	<b>Starbucks at Home Motors</b>	Category	<b>Commercial</b>	File #s	Approved	Status
	Description	Coffee shop and drive-thru	Acreage	5.81	<b>PD2021-0011</b>	<b>11/16/2022</b>	Building permits submitted. Planning permit expiration on 11/16/2025.
	Location	1313 E Main St	District	PD/C-2	<b>U2021-0019</b>	<b>11/16/2022</b>	
	APN(s)	128-120-003	Planner	<a href="#">Carol Ziesenhenn</a>			
	Contact	<a href="#">Jacob Weintraub, Applicant, 805-441-0332</a>					

11	Project	<b>Bellecrest Residences (Paradiso)</b>	Category	<b>Residential</b>	File #s	Approved	Status
	Description	142 single-family senior residential homes	Acreage	14.58	GPZ 2022-0003	Pending	Planning permits under review.
	Location	1571 E Main Street	District	PD/R-1	PD2022-0008	Pending	
	APN(s)	128-052-014 & 023	Planner	<a href="#">Frank Albro</a>	PD2022-0009	Pending	
	Contact	<a href="#">Cam Boyd, Applicant, 805-556-3060x164</a>			TR2022-0007	Pending	
12	Project	<b>Nutrien AG Solutions</b>	Category	<b>Commercial</b>	File #s	Approved	Status
	Description	Phased Expansion (Phase 1 outdoor storage and property improvements, Phase 2 a new 6,7000 sqft truck repair facility)	Acreage	4.42	PD2023-0014	Pending	Planning permits under review.
	Location	1300 block of West Main Street	District	PD/CM	A2022-0013	Pending	
	APN(s)	117-180-030	Planner	<a href="#">Greg Vine</a>			
	Contact	<a href="#">Nutrien AG Solutions, Applicant, 805-922-5848</a>					
13	Project	<b>Alvin Newton Apartments</b>	Category	<b>Mixed Use/ Other</b>	File #s	Approved	Status
	Description	5 story mixed-use (1 floor commercial and 4 floors apartments)	Acreage	1.49	DT2022-0022	Pending	Planning permits under review.
	Location	SWC Main St. and Broadway	District	DTSP- Gateway			
	APN(s)	125-320-050	Planner	<a href="#">Carol Ziesenhennne</a>			
	Contact	<a href="#">The Vernon Group, Applicant, 805-963-1244</a>					
14	Project	<b>Heritage Walk Lofts</b>	Category	<b>Residential</b>	File #s	Approved	Status
	Description	Re-purpose structure for 102 residential units	Acreage	1.29	DT2022-0018	3/7/2023	Planning permit expiration on 3/7/2026.
	Location	201 Town Center West	District	DTSP- Town Center			
	APN(s)	123-280-003	Planner	<a href="#">Carol Ziesenhennne</a>			
	Contact	<a href="#">Vernon Property Group, LLC, Applicant</a>					
15	Project	<b>Cook Street Apartments</b>	Category	<b>Residential</b>	File #s	Approved	Status
	Description	Six story building to accommodate up to 114 residential apartment units	Acreage	0.44	DT2022-0017	Pending	Planning permits under review.
	Location	N of Cook Street and E of McClelland Street	District	DTSP - Gateway			
	APN(s)	125-320-018, -019	Planner	<a href="#">Frank Albro</a>			
	Contact	<a href="#">Brian Schwartz, Principal Planner, 805-934-5760</a>					
16	Project	<b>Boone Street Market</b>	Category	<b>Mixed/Other</b>	File #s	Approved	Status
	Description	2,280 sq. ft. addition to market, and 2 new units	Acreage	0.2	GPZ2016-0004	5/2/2017	Building permits issued. Planning permit expiration on 3/20/2022.
	Location	501 E. Boone St	District	DTSP - Railroad Loft	SPZ2016-0003	5/2/2017	
	APN(s)	125-114-015	Planner	<a href="#">Carol Ziesenhennne</a>	DT2016-0040	8/21/2017	
	Contact	<a href="#">Brian Schwartz, Consultant, 805-934-5760</a>			A2019-0006	3/4/2019	
17	Project	<b>Oakley Court Apartments</b>	Category	<b>Residential</b>	File #s	Approved	Status
	Description	30 apartment units with on-site manager's unit	Acreage	2.1	GPZ2019-0001	10/1/2019	Planning permit expiration on 7/17/2024.
	Location	600 Block S. Oakley Ct	District	PD/R-3	PD2019-0002	7/17/2019	
	APN(s)	123-140-036	Planner	<a href="#">Frank Albro</a>	A2022-0010	1/18/2023	
	Contact	<a href="#">Lupe &amp; Gustavo, Applicant, 805-937-1108</a>					
18	Project	<b>Bonita Packing Expansion</b>	Category	<b>Industrial</b>	File #s	Approved	Status
	Description	173,270 sq. ft. cooler addition in 4 phases	Acreage	45.4	PD2012-0007	5/1/2013	Phase 1 (45,935 sq. ft.) is completed.
	Location	1850 W. Stowell Rd	District	PD/CM			
	APN(s)	117-820-028	Planner	<a href="#">Dana Eady</a>			
	Contact	<a href="#">John Smith, Engineer, 805-466-5660</a>					
19	Project	<b>Maxco Box Facility</b>	Category	<b>Industrial</b>	File #s	Approved	Status
	Description	Construct a new 60,000 sq. ft. box facility and outdoor storage yard	Acreage	19.8	PD2021-0007	9/21/2022	Building permits submitted. Planning permit expiration on 9/21/2025.
	Location	1550 W Stowell Rd	District	PD/CM-AG	U2021-0020	9/21/2022	
	APN(s)	117-820-015	Planner	<a href="#">Cody Graybehl</a>			
	Contact	<a href="#">Steve Rigor, Applicant, (503) 477-8328 x 112</a>					
20	Project	<b>Seaside Packaging Warehouse</b>	Category	<b>Industrial</b>	File #s	Approved	Status
	Description	40, 854 square-foot packaging warehouse	Acreage	6.18	U2021-0002	3/16/2022	Building permits approved. Planning permit expiration on 3/16/2025.
	Location	La Brea Avenue	District	M-2			
	APN(s)	117-240-034	Planner	<a href="#">Cody Graybehl</a>			
	Contact	<a href="#">Suzanne D. Winslow, Applicant, (805) 544-9700</a>					



21	<b>Project</b>	<b>Blosser Ranch</b>	<b>Category</b>	<b>Mixed/Other</b>	<b>File #s</b>	<b>Approved</b>	<b>Status</b>
	<b>Description</b>	Construct 338 "for rent" single-family residences with 329 ADUs as well as 832 apartments totalling 1,499 units	<b>Acreage</b>	155.5	<b>PD2023-0002</b>	<b>Pending</b>	Planning permits under review.
	<b>Location</b>	NE/c of S. Blosser Rd and W. Battles Rd	<b>District</b>	Blosser SE SP	<b>TR2023-0001</b>	<b>Pending</b>	
	<b>APN(s)</b>	117-240-028	<b>Planner</b>	<a href="#">Carol Ziesenhenn</a>	<b>PD2023-0006</b>	<b>Pending</b>	
	<b>Contact</b>	<a href="#">Laurie Tamura, Consultant, 805-934-5760</a>			<b>TR2023-0002</b>	<b>Pending</b>	
					<b>PD2023-0007</b>	<b>Pending</b>	
					<b>PD2023-0011</b>	<b>Pending</b>	
					<b>PD2022-0013</b>	<b>6/7/2023</b>	
					<b>PD2022-0007</b>	<b>5/3/2023</b>	
					<b>PD2022-0006</b>	<b>5/3/2023</b>	
22	<b>Project</b>	<b>Vandenberg Senior Residences</b>	<b>Category</b>	<b>Residential</b>	<b>File #s</b>	<b>Approved</b>	<b>Status</b>
	<b>Description</b>	52 unit senior apartment addition	<b>Acreage</b>	4.9	<b>PD2017-0002</b>	<b>7/18/2018</b>	Building permit approved. Planning permit expiration on 7/18/2023.
	<b>Location</b>	1314 S. Broadway	<b>District</b>	PD/C-1	<b>A2021-0008</b>	<b>11/17/2021</b>	
	<b>APN(s)</b>	128-065-008	<b>Planner</b>	<a href="#">Carol Ziesenhenn</a>			
	<b>Contact</b>	<a href="#">Barry Williams, Architect, 805-459-7353</a>					
23	<b>Project</b>	<b>Centennial Square Apartments</b>	<b>Category</b>	<b>Residential</b>	<b>File #s</b>	<b>Approved</b>	<b>Status</b>
	<b>Description</b>	184 affordable apartments	<b>Acreage</b>	6.35	<b>PD2020-0009</b>	<b>8/4/2021</b>	Under construction.
	<b>Location</b>	SW/c Miller St and Plaza Dr	<b>District</b>	PD/R-3			
	<b>APN(s)</b>	128-066-003	<b>Planner</b>	<a href="#">Carol Ziesenhenn</a>			
	<b>Contact</b>	<a href="#">Brian Schwartz, Consultant, 805-934-5760</a>					
24	<b>Project</b>	<b>Barcellus Senior Apartments</b>	<b>Category</b>	<b>Residential</b>	<b>File #s</b>	<b>Approved</b>	<b>Status</b>
	<b>Description</b>	80 unit senior apartments	<b>Acreage</b>	2.3	<b>GPZ2016-0002</b>	<b>12/7/2016</b>	Planning permit expiration on 2/1/2026.
	<b>Location</b>	502 E. Barcellus Ave	<b>District</b>	PD/R-3	<b>PD2022-0015</b>	<b>2/1/2023</b>	
	<b>APN(s)</b>	128-067-032, -033, -034	<b>Planner</b>	<a href="#">Cody Graybehl</a>			
	<b>Contact</b>	<a href="#">Brian Schwartz, Consultant, 805-934-5760</a>					
25	<b>Project</b>	<b>Westgate Village</b>	<b>Category</b>	<b>Mixed/Other</b>	<b>File #s</b>	<b>Approved</b>	<b>Status</b>
	<b>Description</b>	126 multifamily units and 16,000 sq. ft. retail (including gas station)	<b>Acreage</b>	7.6	<b>PD2007-012</b>	<b>7/2/2008</b>	Planning permit under review.
	<b>Location</b>	NW/c S. Blosser Rd and W. Battles Rd	<b>District</b>	PD/CC	<b>A2017-0029</b>	<b>2/7/2018</b>	
	<b>APN(s)</b>	117-240-046, -045	<b>Planner</b>	<a href="#">Carol Ziesenhenn</a>	<b>A2018-0023</b>	<b>1/16/2019</b>	
	<b>Contact</b>	<a href="#">Craig Minus, Developer, 805-962-2121</a>			<b>A2020-0003</b>	<b>5/20/2020</b>	
					<b>A2021-0013</b>	<b>3/14/2022</b>	
					<b>GPZ2022-0002</b>	<b>Pending</b>	
					<b>PD2022-0005</b>	<b>Pending</b>	
					<b>U2022-0007</b>	<b>Pending</b>	
					<b>TR2022-0004</b>	<b>Pending</b>	
26	<b>Project</b>	<b>Centennial Gardens</b>	<b>Category</b>	<b>Residential</b>	<b>File #s</b>	<b>Approved</b>	<b>Status</b>
	<b>Description</b>	Construct 160 affordable apartment units	<b>Acreage</b>	8.36	<b>PD2020-0006</b>	<b>11/18/2020</b>	Under construction.
	<b>Location</b>	SW/c Battles and Depot	<b>District</b>	PD/R-3			
	<b>APN(s)</b>	118-010-058	<b>Planner</b>	<a href="#">Frank Albro</a>			
	<b>Contact</b>	<a href="#">Brian Schwartz, Consultant, 805-934-5760</a>					
27	<b>Project</b>	<b>Crucified Life Church</b>	<b>Category</b>	<b>Mixed/Other</b>	<b>File #s</b>	<b>Approved</b>	<b>Status</b>
	<b>Description</b>	11,700 sq. ft. building	<b>Acreage</b>	0.6	<b>PD2017-0017</b>	<b>2/21/2018</b>	Building permits submitted. Planning permit expiration on 2/21/2023.
	<b>Location</b>	NW/c S. McClelland St	<b>District</b>	PD/C-2	<b>A2019-0041</b>	<b>12/18/2019</b>	
	<b>APN(s)</b>	128-114-069	<b>Planner</b>	<a href="#">Frank Albro</a>	<b>A2020-0017</b>	<b>2/3/2021</b>	
	<b>Contact</b>	<a href="#">Cordelia Raymond, Architect, 805-786-4391</a>					
28	<b>Project</b>	<b>Enos Auto Center North Campus</b>	<b>Category</b>	<b>Commercial</b>	<b>File #s</b>	<b>Approved</b>	<b>Status</b>
	<b>Description</b>	Overall site design and layout of an auto center	<b>Acreage</b>	17.7	<b>PD2018-0006</b>	<b>5/16/2018</b>	Under construction.
	<b>Location</b>	Lots 2-7 of Enos Ranchos Specific Plan	<b>District</b>	Enos Ranchos SP	<b>TU2019-0153</b>	<b>6/17/2020</b>	
	<b>APN(s)</b>	128-189-002, 003, 004, 005, 006, 007	<b>Planner</b>	<a href="#">Carol Ziesenhenn</a>			
	<b>Contact</b>	<a href="#">Jacob Weintraub, Consultant, 805-441-0332</a>					

28(a)	Project	<b>Home Motors</b>	Category	<b>Commercial</b>	File #s	Approved	Status
	Description	52,000 sq. ft. auto dealership	Acreage	7.2	PD2018-0004	5/16/2018	Building permits submitted.
	Location	1004 E. Battles Rd	District	Enos Ranchos SP			
	APN(s)	128-189-002	Planner	<a href="#">Carol Ziesenhenne</a>			
	Contact	<a href="#">Jacob Weintraub, Consultant, 805-441-0332</a>					
29	Project	<b>Santa Maria Cooler and Box Facility</b>	Category	<b>Industrial</b>	File #s	Approved	Status
	Description	Multi-phased 130,000 sq. ft. AG cooler and box facility	Acreage	11.48	PD2023-0013	Pending	Planning permit under review.
	Location	1767 and 1795 A St	District	PD/M-1 - Area 9 SP			
	APN(s)	117-820-022 & 117-820-036	Planner	<a href="#">Cody Graybehl</a>			
	Contact	<a href="#">Gil Palacios, Architect, 805-928-8008</a>					
30	Project	<b>Windset Farms Greenhouses 7-9</b>	Category	<b>Industrial</b>	File #s	Approved	Status
	Description	4.3 mil sq. ft. greenhouse and 93,000 sq. ft. bldg.	Acreage	49	PD2017-0009	Pending	Planning permit under review.
	Location	1650 Black Rd	District	Area 9 SP			
	APN(s)	117-310-018	Planner	<a href="#">Dana Eady</a>			
	Contact	<a href="#">Brian Schwartz, Consultant, 805-934-5760</a>					
31	Project	<b>Avante Apartments</b>	Category	<b>Residential</b>	File #s	Approved	Status
	Description	86 unit apartment complex	Acreage	3.91	PD2021-0013	11/16/2022	Building permits submitted. Planning permit expiration 11/16/2025.
	Location	SW/c of Carmen Lane and South Blosser Road	District	PD/R-3	TR2022-0002	11/16/2022	
	APN(s)	117-770-047	Planner	<a href="#">Cody Graybehl</a>			
	Contact	<a href="#">Steve Simoulis, Applicant, 805-440-9876</a>					
32	Project	<b>Betteravia Plaza</b>	Category	<b>Mixed/Other</b>	File #s	Approved	Status
	Description	Up to 443 units and 291,278 sq. ft. of retail/office	Acreage	55.2	DA2015-0001	2/2/2016	Planning permit expiration on 2/7/2026
	Location	NW/c of W. Betteravia Rd & SMVRR tracks	District	Multiple	TR2016-0007	11/21/2018	
	APN(s)	117-990-001	Planner	<a href="#">Carol Ziesenhenne</a>	GPZ2021-0002	2/21/2023	
	Contact	<a href="#">Dan Blough, Consultant, 805-680-9666</a>			PD2021-0006	2/7/2023	
33	Project	<b>Mister Carwash</b>	Category	<b>Commercial</b>	File #s	Approved	Status
	Description	Drive-thru carwash with on-site office and storage	Acreage	0.92	PD2023-0008	Pending	Planning permit under review
	Location	1925 S. Broadway	District	PD/C-2 - Entrada SP			
	APN(s)	117-500-029 and 117-500-012	Planner	<a href="#">Greg Vine</a>			
	Contact	<a href="#">Lauren Smith, Applicant, 713-449-9447</a>					
34	Project	<b>Celebration I, II, III</b>	Category	<b>Mixed/Other</b>	File #s	Approved	Status
	Description	56 single family units, 33 unit senior apt, 7,000 sq. ft. office bldg, 1 mixed use bldg	Acreage	6.8	Tract 5893, 5921	Recorded	Phase III (rooftop gardens) building permits submitted and planning permits expiration on 8/15/2021.
	Location	NW/c S. Miller St and E. Inger Dr	District	PD/R-2	PD2005-023	12/21/2005	
	APN(s)	128-177 (all) and 128-178 (all)	Planner	<a href="#">Cody Graybehl</a>	PD2006-019	9/20/2006	
	Contact	<a href="#">Frances Romero, Agent, 805-469-9510</a>			PD2013-0010	7/1/2014	
34(a)	Project	<b>Caring Hands Veterinary Clinic</b>	Category	<b>Mixed/Other</b>	File #s	Approved	Status
	Description	Establishment of a Veterinary Clinic	Acreage	0.17	U2021-0006	6/15/2022	Planning permit expiration 6/15/2025
	Location	1995 S. Miller St Suite 103	District	PD/R-2	A2021-0010	6/15/2022	
	APN(s)	128-185-005	Planner	<a href="#">Carol Ziesenhenne</a>			
	Contact	<a href="#">Tom Martinez, Architect, 805-934-5737</a>					
35	Project	<b>Enos Auto Center South Campus</b>	Category	<b>Commercial</b>	File #s	Approved	Status
	Description	Overall site design and layout of an auto center	Acreage	15.2	PD2018-0007	5/16/2018	Under construction.
	Location	Lots 8-11 of the Enos Ranch Specific Plan	District	Enos Ranchos SP			
	APN(s)	128-189-008, 009, 010, 011	Planner	<a href="#">Carol Ziesenhenne</a>			
	Contact	<a href="#">Jacob Weintraub, Consultant, 805-441-0332</a>					
35(a)	Project	<b>Splash N Dash</b>	Category	<b>Commercial</b>	File #s	Approved	Status
	Description	8,200 sq ft carwash	Acreage	1.6	PD2018-0005	9/4/2019	Grading permits submitted. Planning permit expiration on 9/4/2022.
	Location	Lot 8	District	Enos Ranchos SP			
	APN(s)	128-189-008	Planner	<a href="#">Carol Ziesenhenne</a>			
	Contact	<a href="#">Jacob Weintraub, Consultant, 805-441-0332</a>					

36	Project	<b>A Street Deli</b>	Category	<b>Commercial</b>	File #s	Approved	Status
	Description	4,420 sq. ft. retail building	Acreage	0.5	GPZ2015-0005	9/20/2016	Building permits issued.
	Location	1500 W. Betteravia	District	PD/C-2	PD2015-0019	9/21/2016	
	APN(s)	111-040-006	Planner	<a href="#">Carol Ziesenhenne</a>	A2018-0002	3/21/2018	
	Contact	<a href="#">Gil Rodriguez, Applicant, 805-478-1674</a>			A2019-0025	9/4/2019	
37	Project	<b>Starbucks Drive-Thru Coffee</b>	Category	<b>Commercial</b>	File #s	Approved	Status
	Description	1,300 sq. ft. drive-thru only	Acreage	0.51	PD2023-0009	Pending	Planning permit under review
	Location	1202 W. Betteravia	District	PD/C-2	U2023-0007	Pending	
	APN(s)	111-400-032	Planner	<a href="#">Cody Graybehl</a>			
	Contact	<a href="#">Jane Collete, Architect, 805-648-1234 ext. 20</a>					
38	Project	<b>Hardy Diagnostics</b>	Category	<b>Industrial</b>	File #s	Approved	Status
	Description	36,400 sq. ft. manufacutring, warehouse and office building	Acreage	1.96	PD2023-0003	6/21/2023	Planning permit expiration 6/21/2026.
	Location	1291 W. McCoy Lane	District	PD/M-1			
	APN(s)	111-051-011	Planner	<a href="#">Frank Albro</a>			
	Contact	<a href="#">Pamela Ricci, Applicant, 805-543-1794</a>					
39	Project	<b>VTC Enterprises (Phase 2)</b>	Category	<b>Mixed/Other</b>	File #s	Approved	Status
	Description	6,187 sq. ft. vocational training buildings	Acreage	3.3	U2008-0004	7/2/2008	Classroom building built (12,023 sq. ft.). Building permits submitted for Phase 2 (5,277 sq. ft. office)
	Location	2445 A St	TAZ	30091			
	APN(s)	111-040-043, -044	District	PF			
	Contact	<a href="#">Gil Palacios, Architect, 805-928-8008</a>	Planner	<a href="#">Cody Graybehl</a>			
40	Project	<b>2811 Center</b>	Category	<b>Industrial</b>	File #s	Approved	Status
	Description	51,200 sq. ft. of office in 2 buildings	Acreage	7	PD2017-0003	6/7/2017	One 25,600 sq. ft. building constructed. Second building pending.
	Location	2815 Airpark Dr	District	PD/M-1	TR2017-0002	3/21/2018	
	APN(s)	111-231-003	Planner	<a href="#">Carol Ziesenhenne</a>	A2022-0001	1/25/2022	
	Contact	<a href="#">Steve Simoulis, Developer, 805-541-9004</a>					
41	Project	<b>Santa Maria Studios</b>	Category	<b>Residential</b>	Files #s	Approved	Status
	Description	358 senior, affordable & market rate units (Phase 1= 160 + Phase 2 = 19	Acreage	5.5	PD2020-0001	N/A	Phase 1 is under construction.
	Location	2660 Santa Maria Way, Santa Maria, CA	District	PD/C-2	PD2023-0004	Pending	Planning permit under review.
	APN(s)	128-090-011	Planner	<a href="#">Cody Graybehl</a>			
	Contact	<a href="#">AMG &amp; Associates, LLC, 818-380-2600</a>					
42	Project	<b>Park Edge Apartments</b>	Category	<b>Mixed Use/Other</b>	File #s	Approved	Status
	Description	140 apt units, clubhouse and 5,435 sq. ft. multi-tenant commercial	Acreage	7.45	PD2020-0008	6/16/2022	Building permits submitted. Planning permits expiration on 6/16/2025.
	Location	2770 Santa Maria Way	District	PD/C-2 & PD/R-3	U2020-0012	6/16/2022	
	APN(s)	128-090-022, -023 & 109-010-039	Planner	<a href="#">Cody Graybehl</a>			
	Contact	<a href="#">Brian Schwartz, Consultant, 805-934-5760</a>					
43	Project	<b>Northman Residential</b>	Category	<b>Residential</b>	File #s	Approved	Status
	Description	63 single family residences	Acreage	13.2	GPZ2018-0004	8/6/2019	Under construction.
	Location	Santa Maria Wy btw Sunrise Dr & E Dauphin St	District	PD/R-1	TR2018-0003	7/16/2019	
	APN(s)	109-010-005, -006	Planner	<a href="#">Dana Eady</a>	PD2018-0013	6/19/2019	
	Contact	<a href="#">Brian Schwartz, Consultant</a>			A2021-0012	4/28/2022	
44	Project	<b>Skylight Homes</b>	Category	<b>Residential</b>	File #s	Approved	Status
	Description	49 single family homes in 50 parcels	Acreage	8.89	GPZ2021-0001	1/4/2022	Planning permits expiration 1/17/2026.
	Location	3170 Santa Maria Way	District	PD/R-1	PD2022-0006	1/17/2023	Building permits submitted.
	APN(s)	109-010-012	Planner	<a href="#">Cody Graybehl</a>	TR2022-0005	1/17/2023	
	Contact	<a href="#">Sheryl Flores, Applicant, 805-540-2465</a>					

<b>45</b>	<i>Project</i>	<b>Elements Apartments (Lakeview Mixed Use Project)</b>	<i>Category</i>	<b>Mixed Use</b>	<i>File #s</i>	<i>Approved</i>	<i>Status</i>
	<i>Description</i>	152 apartment units and approx. 9,800 sqft of commercial space	<i>Acreage</i>	4	<b>PD2018-0008</b>	<b>4/2/2019</b>	Under construction
	<i>Location</i>	NW corner of Orcutt Expressway & Skyway Drive	<i>District</i>	PD/R-3			
	<i>APN(s)</i>	111-100-008 & 111-100-009	<i>Planner</i>	<a href="#">Frank Albro</a>			
	<i>Contact</i>	<a href="#">Urban Planning Concepts, Applicant, 805-934-5760</a>					
<b>46</b>	<i>Project</i>	<b>Santa Maria Airport Foxenwood Self Storage</b>	<i>Category</i>	<b>Industrial</b>	<i>File #s</i>	<i>Approved</i>	<i>Status</i>
	<i>Description</i>	Mini-warehouse facility	<i>Acreage</i>	608.01	<b>PD2022-0017</b>	<b>Pending</b>	Planning permits under review
	<i>Location</i>	3335 Corsair Circle	<i>District</i>	AA,PD/AS-1	<b>SPZ2022-0001</b>	<b>Pending</b>	
	<i>APN(s)</i>	111-231-011	<i>Planner</i>	<a href="#">Frank Albro</a>			
	<i>Contact</i>	<a href="#">Santa Maria Public Airport District, 805-922-1726</a>					

**APPROVED AND PENDING PROJECT TRIP GENERATION SPREADSHEET**

Associated Transportation Engineers  
Pending and Approved Projects - Trip Generation Worksheet

BELLECREST SENIOR RESIDENTIAL PROJECT - CUMULATIVE CITY LIST (#22086.01)																
Land-Use		Size		Pass-By Factor	AM Peak						PM Peak					
					Rate	Trips	In %	Trips	Out %	Trips	Rate	Trips	In %	Trips	Out %	Trips
6	309 Mill Aparments (a)	23	DU	1.00	0.40	9	24%	2	76%	7	0.51	12	63%	8	37%	4
7	200 Mill Aparments (a)	20	DU	1.00	0.40	8	24%	2	76%	6	0.51	10	63%	6	37%	4
8	Vino Bella Apartments (a)	32	DU	1.00	0.40	13	24%	3	76%	10	0.51	16	63%	10	37%	6
9	Gateway Mixed Use (b)	27	DU	1.00	0.37	10	23%	2	77%	8	0.39	11	61%	7	39%	4
9	Gateway Mixed Use (c)	3,300	SF	1.00	2.36	8	60%	5	40%	3	6.59	22	50%	11	50%	11
10	Starbucks at Home Motors (d)	1,800	SF	0.50	85.88	77	51%	39	49%	38	38.99	35	50%	18	50%	17
13	Alvin Newton Apartments (e)	-	-	1.00	-	64	-	25	-	39	-	64	-	39	-	25
14	Heritage Walk Lofts (a)	102	DU	1.00	0.40	41	24%	10	76%	31	0.51	52	63%	33	37%	19
15	Cook Street Apartments (f)	-	-	1.00	-	62	-	21	-	41	-	72	-	45	-	27
16	Boone Street Market (g)	2,280	SF	1.00	0.59	1	79%	1	21%	0	16.62	38	50%	19	50%	19
16	Boone Street Market (a)	2	DU	1.00	0.40	1	24%	0	76%	1	0.51	1	63%	1	37%	0
	Sisters of Saint Francis Residential Project (h)	-	-	1.00	-	50	-	16	-	34	-	48	-	28	-	20

(a) Trip generation based on rates for Multifamily Housing Low-Rise (#220).

(b) Trip generation based on rates for Multifamily Housing Mid-Rise (#221).

(c) Trip generation based on rates for Strip Retail Plaza (<40k) (#822).

(d) Trip generation based on rates for Coffee/Donut Shop with Drive-Through Window (#937).

(e) Traffic Study, ATE, March 2023.

(f) Traffic Study, ATE, February 2023.

(g) Trip generation based on rates for Liquor Store (#899).

(h) Traffic Study, ATE, May 2023.



## **ACCIDENT DATA AND CALCULATION WORKSHEETS**



## ASSOCIATED TRANSPORTATION ENGINEERS

100 N. Hope Avenue, Suite 4, Santa Barbara, CA 93110 • (805) 687-4418 • (805) 682-8509-F

### ACCIDENT RATE CALCULATION SHEET - FOR INTERSECTIONS

**Project:** Bellecrest Senior Residential **File Name:** Accident Rate Worksheet 3 Year  
**Project #:** 22086.01  
**Analyst:** GOM  
**Date:** 11/22/2023

**N/S Street:** Nicholson Road-US 101 NB  
**E/W Street:** Main Street

**Weekday:**  
PM Peak Hour Entering Volume: 2533  
Peak Hour Factor: 10  
-----OR-----  
Total Approach ADT: N/A

**Weekend:**  
PM Peak Hour Entering Volume OR ADT: 75% (as a percentage of Weekday PM Peak Hour Entering Volume OR ADT)

**Period Analyzed (years):** 3

**Number of Accidents:** 6

**Million Entering Vehicle Miles:** 25.76 million entering vehicle miles (mevm)

**Accident Rate:** .23 accidents per million entering vehicle miles (mevm)

**Intersection Rate Group:** 109  
**California State Average Collision Rate:** 0.55



## ASSOCIATED TRANSPORTATION ENGINEERS

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### ACCIDENT RATE CALCULATION SHEET - FOR INTERSECTIONS

**Project:** Bellecrest Senior Residential **File Name:** Accident Rate Worksheet 3 Year  
**Project #:** 22086.01  
**Analyst:** GOM  
**Date:** 11/22/2023

**N/S Street:** Palisade Drive  
**E/W Street:** Main Street

**Weekday:**  
PM Peak Hour Entering Volume: 1471  
Peak Hour Factor: 10  
-----OR-----  
Total Approach ADT: N/A

**Weekend:**  
PM Peak Hour Entering Volume OR ADT: 75% (as a percentage of Weekday PM Peak Hour Entering Volume OR ADT)

**Period Analyzed (years):** 3

**Number of Accidents:** 5

**Million Entering Vehicle Miles:** 14.96 million entering vehicle miles (mevm)

**Accident Rate:** .33 accidents per million entering vehicle miles (mevm)

**Intersection Rate Group:** 124  
**California State Average Collision Rate:** 0.43



## ASSOCIATED TRANSPORTATION ENGINEERS

100 N. Hope Avenue, Suite 4, Santa Barbara, CA 93110 • (805) 687-4418 • (805) 682-8509-F

### ACCIDENT RATE CALCULATION SHEET - FOR INTERSECTIONS

**Project:** Bellecrest Senior Residential **File Name:** Accident Rate Worksheet 3 Year  
**Project #:** 22086.01  
**Analyst:** GOM  
**Date:** 11/22/2023

**N/S Street:** Suey Road  
**E/W Street:** Main Street

**Weekday:**  
PM Peak Hour Entering Volume: 1484  
Peak Hour Factor: 10  
-----OR-----  
Total Approach ADT: N/A

**Weekend:**  
PM Peak Hour Entering Volume OR ADT: 75% (as a percentage of Weekday PM Peak Hour Entering Volume OR ADT)

**Period Analyzed (years):** 3

**Number of Accidents:** 3

**Million Entering Vehicle Miles:** 15.09 million entering vehicle miles (mevm)

**Accident Rate:** .2 accidents per million entering vehicle miles (mevm)

**Intersection Rate Group:** 109  
**California State Average Collision Rate:** 0.55



## ASSOCIATED TRANSPORTATION ENGINEERS

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### ACCIDENT RATE CALCULATION SHEET - FOR INTERSECTIONS

**Project:** Bellecrest Senior Residential **File Name:** Accident Rate Worksheet 3 Year  
**Project #:** 22086.01  
**Analyst:** GOM  
**Date:** 11/22/2023

**N/S Street:** Panther Drive  
**E/W Street:** Main Street

**Weekday:**  
PM Peak Hour Entering Volume: 759  
Peak Hour Factor: 10  
-----OR-----  
Total Approach ADT: N/A

**Weekend:**  
PM Peak Hour Entering Volume OR ADT: 75% (as a percentage of Weekday PM Peak Hour Entering Volume OR ADT)

**Period Analyzed (years):** 3

**Number of Accidents:** 2

**Million Entering Vehicle Miles:** 7.72 million entering vehicle miles (mevm)

**Accident Rate:** .26 accidents per million entering vehicle miles (mevm)

**Intersection Rate Group:** 124  
**California State Average Collision Rate:** 0.43

## **PROJECT DRIVEWAY QUEUING ANALYSIS WORKSHEETS**

## Queuing and Blocking Report

### CUMULATIVE + PROJECT AM PEAK HOUR

---

#### Intersection: 3: Main Street & Project Driveway

---

Movement	SB
Directions Served	LR
Maximum Queue (ft)	31
Average Queue (ft)	18
95th Queue (ft)	42
Link Distance (ft)	249
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

#### Network Summary

---

Network wide Queuing Penalty: 0
---------------------------------



## Queuing and Blocking Report

### CUMULATIVE + PROJECT PM PEAK HOUR

---

#### Intersection: 3: Main Street & Project Driveway

---

Movement	EB	SB
Directions Served	L	LR
Maximum Queue (ft)	29	31
Average Queue (ft)	12	12
95th Queue (ft)	35	38
Link Distance (ft)	249	
Upstream Blk Time (%)		
Queuing Penalty (veh)		
Storage Bay Dist (ft)	150	
Storage Blk Time (%)		
Queuing Penalty (veh)		

#### Network Summary

---

Network wide Queuing Penalty: 0

## **VMT CALCULATOR RESULTS**



# ASSOCIATED TRANSPORTATION ENGINEERS

100 N. Hope Avenue, Suite 4, Santa Barbara, CA 93110 • (805)687-4418 • FAX (805)682-8509 • [main@atesb.com](mailto:main@atesb.com)

Since 1978

Richard L. Pool, P.E.  
Scott A. Schell

## Bellecrest Senior Residential Component City of Santa Maria VMT Calculator Results

### The VMT Screening Results

---

Project Name: Bellecrest Residential  
Project Parcel: 128-052-014  
Daily Trips: 612  
Peak Hour Trips: 43

#### -----Proposed Development and Estimated VMT Impact-----

Residential: 142

The residential development is estimated to generate 17.6 VMT per person. The rate is higher than the adopted threshold. Please adjust the project parameters or propose mitigation.

Office:

This project does not include Office development.

Commercial:

This project does not include Commercial development.

Industrial:

This project does not include Industrial development.

## **INTERSECTION LEVEL OF SERVICE CALCULATION WORKSHEETS**

- Reference 1 - Main Street/US 101 NB Ramps-Nicholson Road**
- Reference 2 - Main Street/Palisade Drive**
- Reference 3 - Main Street/Suey Road**
- Reference 4 - Main Street/Panther Drive**

## #22086.01 BELLECREST SENIOR HOUSING PROJECT

REF: 01\_AM

## INTERSECTION CAPACITY UTILIZATION WORKSHEET

COUNT DATE: 11/09/2023

TIME PERIOD: AM PEAK HOUR

N/S STREET: US 101 NB RAMPS-NICHOLSON ROAD

E/W STREET: MAIN STREET

CONTROL TYPE: SIGNAL

## TRAFFIC VOLUME SUMMARY

VOLUMES		NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
		L	T	R	L	T	R	L	T	R	L	T	R
(A)	EXISTING:	305	22	289	0	0	0	182	637	120	12	865	198
(B)	PROJECT-ADDED:	0	0	3	0	0	0	0	6	0	0	14	4
(C)	CUMULATIVE:	318	22	295	0	0	0	200	656	120	30	883	202

## GEOMETRICS

LANE GEOMETRICS	NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
	L	T	R	L	T	R	LL	T	TR	L	T	TR

## TRAFFIC SCENARIOS

SCENARIO 1 = EXISTING VOLUMES (A)

SCENARIO 2 = EXISTING + PROJECT VOLUMES(A+B)

SCENARIO 3 = SHORT-TERM CUMULATIVE (C)

SCENARIO 4 = SHORT-TERM CUMULATIVE + PROJECT VOLUMES (B+C)

## LEVEL OF SERVICE CALCULATIONS

MOVE- MENTS	# OF LANES	CAPACITY	SCENARIO VOLUMES				SCENARIO V/C RATIOS					
			1	2	3	4	1	2	3	4		
NBL	0	0	305	305	318	318	-	-	-	-		
NBT	1	1600	22	22	22	22	0.204 *	0.204 *	0.213 *	0.213 *		
NBR (a)	1	1600	289	292	295	298	0.181	0.183	0.184	0.186		
SBL	0	0	0	0	0	0	-	-	-	-		
SBT	0	0	0	0	0	0	-	-	-	-		
SBR (b)	0	0	0	0	0	0	-	-	-	-		
EBL	2	3200	182	182	200	200	0.057 *	0.057 *	0.063 *	0.063 *		
EBT	2	3200	637	643	656	662	0.237	0.238	0.243	0.244		
EBR (c)	0	0	120	120	120	120	-	-	-	-		
WBL	1	1600	12	12	30	30	0.008	0.008	0.019	0.019		
WBT	2	3200	865	879	883	897	0.270 *	0.275 *	0.276 *	0.280 *		
WBR (d)	1	1600	198	202	202	206	0.124	0.126	0.126	0.129		
LOST TIME:							0.100 *	0.100 *	0.100 *	0.100 *		
TOTAL INTERSECTION CAPACITY UTILIZATION:							0.631	0.636	0.652	0.656		
SCENARIO LEVEL OF SERVICE:							B	B	B	B		

## NOTES:

RTOR: (a) 0%

(b) 0%

(c) 0%

(d) 0%

Printed: 11/28/23

## #22086.01 BELLECREST SENIOR HOUSING PROJECT

REF: 01\_PM

## INTERSECTION CAPACITY UTILIZATION WORKSHEET

COUNT DATE: 11/09/2023

TIME PERIOD: PM PEAK HOUR

N/S STREET: US 101 NB RAMPS-NICHOLSON ROAD

E/W STREET: MAIN STREET

CONTROL TYPE: SIGNAL

## TRAFFIC VOLUME SUMMARY

VOLUMES		NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
		L	T	R	L	T	R	L	T	R	L	T	R
(A)	EXISTING:	485	76	219	0	0	0	262	442	29	3	781	236
(B)	PROJECT-ADDED:	0	0	7	0	0	0	0	13	0	0	10	2
(C)	CUMULATIVE:	509	76	221	0	0	0	271	452	29	11	792	238

## GEOMETRICS

LANE GEOMETRICS		NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
		L	T	R	L	T	R	L	T	R	L	T	R

## TRAFFIC SCENARIOS

SCENARIO 1 = EXISTING VOLUMES (A)

SCENARIO 2 = EXISTING + PROJECT VOLUMES(A+B)

SCENARIO 3 = SHORT-TERM CUMULATIVE (C)

SCENARIO 4 = SHORT-TERM CUMULATIVE + PROJECT VOLUMES (B+C)

## LEVEL OF SERVICE CALCULATIONS

MOVE- MENTS	# OF LANES	CAPACITY	SCENARIO VOLUMES				SCENARIO V/C RATIOS					
			1	2	3	4	1	2	3	4		
NBL	0	0	485	485	509	509	-	-	-	-		
NBT	1	1600	76	76	76	76	0.351 *	0.351 *	0.366 *	0.366 *		
NBR (a)	1	1600	219	226	221	228	0.137	0.141	0.138	0.143		
SBL	0	0	0	0	0	0	-	-	-	-		
SBT	0	0	0	0	0	0	-	-	-	-		
SBR (b)	0	0	0	0	0	0	-	-	-	-		
EBL	2	3200	262	262	271	271	0.082 *	0.082 *	0.085 *	0.085 *		
EBT	2	3200	442	455	452	465	0.147	0.151	0.150	0.154		
EBR (c)	0	0	29	29	29	29	-	-	-	-		
WBL	1	1600	3	3	11	11	0.002	0.002	0.007	0.007		
WBT	2	3200	781	791	792	802	0.244 *	0.247 *	0.248 *	0.251 *		
WBR (d)	1	1600	236	238	238	240	0.148	0.149	0.149	0.150		
LOST TIME:							0.100 *	0.100 *	0.100 *	0.100 *		
TOTAL INTERSECTION CAPACITY UTILIZATION:							0.777	0.780	0.799	0.802		
SCENARIO LEVEL OF SERVICE:							C	C	C	C		

## NOTES:

RTOR: (a) 0%

(b) 0%

(c) 0%

(d) 0%

Printed: 11/28/23

## #22086.01 BELLECREST SENIOR HOUSING PROJECT

REF: 02\_AM

## INTERSECTION CAPACITY UTILIZATION WORKSHEET

COUNT DATE: 11/09/2023

TIME PERIOD: AM PEAK HOUR

N/S STREET: PALISADE DRIVE

E/W STREET: MAIN STREET

CONTROL TYPE: SIGNAL

## TRAFFIC VOLUME SUMMARY

VOLUMES		NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
		L	T	R	L	T	R	L	T	R	L	T	R
(A)	EXISTING:	154	0	24	0	0	0	0	445	323	65	755	0
(B)	PROJECT-ADDED:	0	0	0	0	0	0	0	9	0	1	18	0
(C)	CUMULATIVE:	158	0	36	0	0	0	0	445	323	65	767	0

## GEOMETRICS

LANE GEOMETRICS	NORTH BOUND		SOUTH BOUND		EAST BOUND		WEST BOUND	
	L	R	L	R	T	TR	L	TT

## TRAFFIC SCENARIOS

SCENARIO 1 = EXISTING VOLUMES (A)

SCENARIO 2 = EXISTING + PROJECT VOLUMES(A+B)

SCENARIO 3 = SHORT-TERM CUMULATIVE (C)

SCENARIO 4 = SHORT-TERM CUMULATIVE + PROJECT VOLUMES (B+C)

## LEVEL OF SERVICE CALCULATIONS

MOVE- MENTS	# OF LANES	CAPACITY	SCENARIO VOLUMES				SCENARIO V/C RATIOS					
			1	2	3	4	1	2	3	4		
NBL	1	1600	154	154	158	158	0.096 *	0.096 *	0.099 *	0.099 *		
NBT	0	0	0	0	0	0	-	-	-	-		
NBR (a)	1	1600	24	24	36	36	0.015	0.015	0.023	0.023		
SBL	0	0	0	0	0	0	-	-	-	-		
SBT	0	0	0	0	0	0	-	-	-	-		
SBR (b)	0	0	0	0	0	0	-	-	-	-		
EBL	0	0	0	0	0	0	-	-	-	-		
EBT	2	3200	445	454	445	454	0.240 *	0.243 *	0.240 *	0.243 *		
EBR (c)	0	0	323	323	323	323	-	-	-	-		
WBL	1	1600	65	66	65	66	0.041 *	0.041 *	0.041 *	0.041 *		
WBT	2	3200	755	773	767	785	0.236	0.242	0.240	0.245		
WBR (d)	0	0	0	0	0	0	-	-	-	-		
LOST TIME:							0.100 *	0.100 *	0.100 *	0.100 *		
TOTAL INTERSECTION CAPACITY UTILIZATION:							0.477	0.480	0.480	0.483		
SCENARIO LEVEL OF SERVICE:							A	A	A	A		

## NOTES:

RTOR: (a) 0%

(b) 0%

(c) 0%

(d) 0%

Printed: 11/28/23



## #22086.01 BELLECREST SENIOR HOUSING PROJECT

REF: 02\_PM

## INTERSECTION CAPACITY UTILIZATION WORKSHEET

COUNT DATE: 11/09/2023

TIME PERIOD: PM PEAK HOUR

N/S STREET: PALISADE DRIVE

E/W STREET: MAIN STREET

CONTROL TYPE: SIGNAL

## TRAFFIC VOLUME SUMMARY

VOLUMES		NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
		L	T	R	L	T	R	L	T	R	L	T	R
(A)	EXISTING:	316	0	88	0	0	0	0	374	122	32	539	0
(B)	PROJECT-ADDED:	0	0	1	0	0	0	0	20	0	1	12	0
(C)	CUMULATIVE:	318	0	90	0	0	0	0	374	122	32	544	0

## GEOMETRICS

LANE GEOMETRICS		NORTH BOUND		SOUTH BOUND		EAST BOUND		WEST BOUND	
		L	R	L	R	T	TR	L	TT

## TRAFFIC SCENARIOS

SCENARIO 1 = EXISTING VOLUMES (A)

SCENARIO 2 = EXISTING + PROJECT VOLUMES(A+B)

SCENARIO 3 = SHORT-TERM CUMULATIVE (C)

SCENARIO 4 = SHORT-TERM CUMULATIVE + PROJECT VOLUMES (B+C)

## LEVEL OF SERVICE CALCULATIONS

MOVE- MENTS	# OF LANES	CAPACITY	SCENARIO VOLUMES				SCENARIO V/C RATIOS					
			1	2	3	4	1	2	3	4		
NBL	1	1600	316	316	318	318	0.198 *	0.198 *	0.199 *	0.199 *		
NBT	0	0	0	0	0	0	-	-	-	-		
NBR (a)	1	1600	88	89	90	91	0.055	0.056	0.056	0.057		
SBL	0	0	0	0	0	0	-	-	-	-		
SBT	0	0	0	0	0	0	-	-	-	-		
SBR (b)	0	0	0	0	0	0	-	-	-	-		
EBL	0	0	0	0	0	0	-	-	-	-		
EBT	2	3200	374	394	374	394	0.155 *	0.161 *	0.155 *	0.161 *		
EBR (c)	0	0	122	122	122	122	-	-	-	-		
WBL	1	1600	32	33	32	33	0.020 *	0.021 *	0.020 *	0.021 *		
WBT	2	3200	539	551	544	556	0.168	0.172	0.170	0.174		
WBR (d)	0	0	0	0	0	0	-	-	-	-		
LOST TIME:							0.100 *	0.100 *	0.100 *	0.100 *		
TOTAL INTERSECTION CAPACITY UTILIZATION:							0.473	0.480	0.474	0.481		
SCENARIO LEVEL OF SERVICE:							A	A	A	A		

## NOTES:

RTOR: (a) 0%

(b) 0%

(c) 0%

(d) 0%

Printed: 11/28/23

## #22086.01 BELLECREST SENIOR HOUSING PROJECT

REF: 03\_AM

## INTERSECTION CAPACITY UTILIZATION WORKSHEET

COUNT DATE: 11/09/2023

TIME PERIOD: AM PEAK HOUR

N/S STREET: SUEY ROAD

E/W STREET: MAIN STREET

CONTROL TYPE: SIGNAL

## TRAFFIC VOLUME SUMMARY

VOLUMES		NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
		L	T	R	L	T	R	L	T	R	L	T	R
(A)	EXISTING:	23	89	122	85	156	184	53	294	36	115	526	115
(B)	PROJECT-ADDED:	0	0	0	1	0	0	0	9	0	1	19	2
(C)	CUMULATIVE:	27	89	122	85	156	190	59	296	40	115	528	115

## GEOMETRICS

LANE GEOMETRICS	NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
	L	T	R	L	T	R	L	T	R	L	T	R

## TRAFFIC SCENARIOS

SCENARIO 1 = EXISTING VOLUMES (A)

SCENARIO 2 = EXISTING + PROJECT VOLUMES(A+B)

SCENARIO 3 = SHORT-TERM CUMULATIVE (C)

SCENARIO 4 = SHORT-TERM CUMULATIVE + PROJECT VOLUMES (B+C)

## LEVEL OF SERVICE CALCULATIONS

MOVE- MENTS	# OF LANES	CAPACITY	SCENARIO VOLUMES				SCENARIO V/C RATIOS					
			1	2	3	4	1	2	3	4		
NBL	1	1600	23	23	27	27	0.014 *	0.014 *	0.017 *	0.017 *		
NBT	1	1600	89	89	89	89	0.056	0.056	0.056	0.056		
NBR (a)	1	1600	57	57	57	57	0.036	0.036	0.036	0.036		
SBL	1	1600	85	86	85	86	0.053	0.054	0.053	0.054		
SBT	1	1600	156	156	156	156	0.098 *	0.098 *	0.098 *	0.098 *		
SBR (b)	1	1600	105	105	108	108	0.066	0.066	0.068	0.068		
EBL	1	1600	53	53	59	59	0.033 *	0.033 *	0.037 *	0.037 *		
EBT	2	3200	294	303	296	305	0.099	0.102	0.101	0.103		
EBR (c)	0	0	23	23	26	26	-	-	-	-		
WBL	1	1600	115	116	115	116	0.072	0.073	0.072	0.073		
WBT	2	3200	526	545	528	547	0.195 *	0.201 *	0.195 *	0.202 *		
WBR (d)	0	0	97	98	97	98	-	-	-	-		
LOST TIME:							0.100 *	0.100 *	0.100 *	0.100 *		
TOTAL INTERSECTION CAPACITY UTILIZATION:							0.440	0.446	0.447	0.454		
SCENARIO LEVEL OF SERVICE:							A	A	A	A		

## NOTES:

RTOR: (a) 53%

(b) 43%

(c) 36%

(d) 16%

Printed: 11/28/23

## #22086.01 BELLECREST SENIOR HOUSING PROJECT

REF: 03\_PM

## INTERSECTION CAPACITY UTILIZATION WORKSHEET

COUNT DATE: 11/09/2023

TIME PERIOD: PM PEAK HOUR

N/S STREET: SUEY ROAD

E/W STREET: MAIN STREET

CONTROL TYPE: SIGNAL

## TRAFFIC VOLUME SUMMARY

VOLUMES		NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
		L	T	R	L	T	R	L	T	R	L	T	R
(A)	EXISTING:	45	225	89	24	123	118	164	157	30	97	305	107
(B)	PROJECT-ADDED:	0	0	1	3	0	0	0	21	0	1	13	2
(C)	CUMULATIVE:	47	225	89	24	123	120	166	158	32	97	306	107

## GEOMETRICS

LANE GEOMETRICS		NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
		L	T	R	L	T	R	L	T	R	L	T	R

## TRAFFIC SCENARIOS

SCENARIO 1 = EXISTING VOLUMES (A)

SCENARIO 2 = EXISTING + PROJECT VOLUMES(A+B)

SCENARIO 3 = SHORT-TERM CUMULATIVE (C)

SCENARIO 4 = SHORT-TERM CUMULATIVE + PROJECT VOLUMES (B+C)

## LEVEL OF SERVICE CALCULATIONS

MOVE- MENTS	# OF LANES	CAPACITY	SCENARIO VOLUMES				SCENARIO V/C RATIOS					
			1	2	3	4	1	2	3	4		
NBL	1	1600	45	45	47	47	0.028	0.028	0.029	0.029		
NBT	1	1600	225	225	225	225	0.141 *	0.141 *	0.141 *	0.141 *		
NBR (a)	1	1600	40	41	40	41	0.025	0.026	0.025	0.026		
SBL	1	1600	24	27	24	27	0.015 *	0.017 *	0.015 *	0.017 *		
SBT	1	1600	123	123	123	123	0.077	0.077	0.077	0.077		
SBR (b)	1	1600	52	52	53	53	0.033	0.033	0.033	0.033		
EBL	1	1600	164	164	166	166	0.103 *	0.103 *	0.104 *	0.104 *		
EBT	2	3200	157	178	158	179	0.056	0.063	0.057	0.063		
EBR (c)	0	0	22	22	23	23	-	-	-	-		
WBL	1	1600	97	98	97	98	0.061	0.061	0.061	0.061		
WBT	2	3200	305	318	306	319	0.125 *	0.129 *	0.125 *	0.130 *		
WBR (d)	0	0	94	96	94	96	-	-	-	-		
LOST TIME:							0.100 *	0.100 *	0.100 *	0.100 *		
TOTAL INTERSECTION CAPACITY UTILIZATION:							0.484	0.490	0.485	0.492		
SCENARIO LEVEL OF SERVICE:							A	A	A	A		

## NOTES:

RTOR: (a) 55%

(b) 56%

(c) 27%

(d) 12%

Printed: 11/28/23

## #22086.01 BELLECREST SENIOR HOUSING PROJECT

REF: 04\_AM

## INTERSECTION CAPACITY UTILIZATION WORKSHEET

COUNT DATE: 11/09/2023

TIME PERIOD: AM PEAK HOUR

N/S STREET: PANTHER DRIVE

E/W STREET: MAIN STREET

CONTROL TYPE: SIGNAL

## TRAFFIC VOLUME SUMMARY

VOLUMES		NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
		L	T	R	L	T	R	L	T	R	L	T	R
(A)	EXISTING:	0	0	0	12	0	623	401	97	0	0	91	10
(B)	PROJECT-ADDED:	0	0	0	0	0	1	1	0	0	0	0	0
(C)	CUMULATIVE:	0	0	0	12	0	625	403	97	0	0	91	10

## GEOMETRICS

LANE GEOMETRICS		NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
		L T R			L R R			L T T			T T R		

## TRAFFIC SCENARIOS

SCENARIO 1 = EXISTING VOLUMES (A)

SCENARIO 2 = EXISTING + PROJECT VOLUMES(A+B)

SCENARIO 3 = SHORT-TERM CUMULATIVE (C)

SCENARIO 4 = SHORT-TERM CUMULATIVE + PROJECT VOLUMES (B+C)

## LEVEL OF SERVICE CALCULATIONS

MOVE- MENTS	# OF LANES	CAPACITY	SCENARIO VOLUMES				SCENARIO V/C RATIOS					
			1	2	3	4	1	2	3	4		
NBL	0	0	0	0	0	0	-	-	-	-		
NBT	0	0	0	0	0	0	-	-	-	-		
NBR (a)	0	0	0	0	0	0	-	-	-	-		
SBL	1	1600	12	12	12	12	0.008	0.008	0.008	0.008		
SBT	0	0	0	0	0	0	-	-	-	-		
SBR (b)	2	3200	623	624	625	626	0.195 *	0.195 *	0.195 *	0.196 *		
EBL	1	1600	401	402	403	404	0.251 *	0.251 *	0.252 *	0.253 *		
EBT	2	3200	97	97	97	97	0.030	0.030	0.030	0.030		
EBR (c)	0	0	0	0	0	0	-	-	-	-		
WBL	0	0	0	0	0	0	-	-	-	-		
WBT	2	3200	91	91	91	91	0.032 *	0.032 *	0.032 *	0.032 *		
WBR (d)	0	0	10	10	10	10	-	-	-	-		
LOST TIME:							0.100 *	0.100 *	0.100 *	0.100 *		
TOTAL INTERSECTION CAPACITY UTILIZATION:							0.578	0.578	0.579	0.581		
SCENARIO LEVEL OF SERVICE:							A	A	A	A		

## NOTES:

RTOR: (a) 0%

(b) 0%

(c) 0%

(d) 0%

Printed: 11/28/23

## #22086.01 BELLECREST SENIOR HOUSING PROJECT

REF: 04\_PM

## INTERSECTION CAPACITY UTILIZATION WORKSHEET

COUNT DATE: 11/09/2023

TIME PERIOD: PM PEAK HOUR

N/S STREET: PANTHER DRIVE

E/W STREET: MAIN STREET

CONTROL TYPE: SIGNAL

## TRAFFIC VOLUME SUMMARY

VOLUMES		NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
		L	T	R	L	T	R	L	T	R	L	T	R
(A)	EXISTING:	0	0	0	15	0	369	181	44	0	0	126	24
(B)	PROJECT-ADDED:	0	0	0	0	0	1	1	0	0	0	0	0
(C)	CUMULATIVE:	0	0	0	15	0	370	182	44	0	0	126	24

## GEOMETRICS

LANE GEOMETRICS		NORTH BOUND			SOUTH BOUND			EAST BOUND			WEST BOUND		
		L T R			L R R			L T T			T T R		

## TRAFFIC SCENARIOS

SCENARIO 1 = EXISTING VOLUMES (A)

SCENARIO 2 = EXISTING + PROJECT VOLUMES(A+B)

SCENARIO 3 = SHORT-TERM CUMULATIVE (C)

SCENARIO 4 = SHORT-TERM CUMULATIVE + PROJECT VOLUMES (B+C)

## LEVEL OF SERVICE CALCULATIONS

MOVE- MENTS	# OF LANES	CAPACITY	SCENARIO VOLUMES				SCENARIO V/C RATIOS					
			1	2	3	4	1	2	3	4		
NBL	0	0	0	0	0	0	-	-	-	-		
NBT	0	0	0	0	0	0	-	-	-	-		
NBR (a)	0	0	0	0	0	0	-	-	-	-		
SBL	1	1600	15	15	15	15	0.009	0.009	0.009	0.009		
SBT	0	0	0	0	0	0	-	-	-	-		
SBR (b)	2	3200	369	370	370	371	0.115 *	0.116 *	0.116 *	0.116 *		
EBL	1	1600	181	182	182	183	0.113 *	0.114 *	0.114 *	0.114 *		
EBT	2	3200	44	44	44	44	0.014	0.014	0.014	0.014		
EBR (c)	0	0	0	0	0	0	-	-	-	-		
WBL	0	0	0	0	0	0	-	-	-	-		
WBT	2	3200	126	126	126	126	0.047 *	0.047 *	0.047 *	0.047 *		
WBR (d)	0	0	24	24	24	24	-	-	-	-		
LOST TIME:							0.100 *	0.100 *	0.100 *	0.100 *		
TOTAL INTERSECTION CAPACITY UTILIZATION:							0.375	0.377	0.377	0.377		
SCENARIO LEVEL OF SERVICE:							A	A	A	A		

## NOTES:

RTOR: (a) 0%

(b) 0%

(c) 0%

(d) 0%

Printed: 11/28/23

## **PROJECT DRIVEWAY LEVEL OF SERVICE CALCULATION WORKSHEETS**

**Reference 1 - Main Street/Project Driveway**

# HCS Two-Way Stop-Control Report

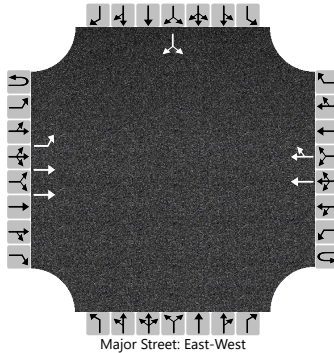
## General Information

Analyst	GOM
Agency/Co.	ATE
Date Performed	11/29/2023
Analysis Year	2023
Time Analyzed	AM PEAK HOUR
Intersection Orientation	East-West
Project Description	CUMULATIVE + PROJECT

## Site Information

Intersection	MAIN STREET/PROJECT DRIVEWAY
Jurisdiction	SANTA MARIA
East/West Street	MAIN STREET
North/South Street	PROJECT DRIVEWAY
Peak Hour Factor	0.89
Analysis Time Period (hrs)	0.25

## Lanes



## Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
Movement	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Priority	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Number of Lanes	0	1	2	0	0	0	2	0		0	0	0		0	1	0
Configuration		L	T				T	TR							LR	
Volume (veh/h)	0	10	503				758	1						1		22
Percent Heavy Vehicles (%)	3	3												3		3
Proportion Time Blocked																
Percent Grade (%)													0			
Right Turn Channelized																
Median Type   Storage					Left Only								1			

## Critical and Follow-up Headways

Base Critical Headway (sec)		4.1												7.5		6.9
Critical Headway (sec)		4.16												6.86		6.96
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.23												3.53		3.33

## Delay, Queue Length, and Level of Service

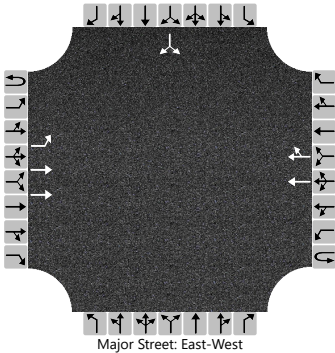
Flow Rate, v (veh/h)		11											26	
Capacity, c (veh/h)		776											551	
v/c Ratio		0.01											0.05	
95% Queue Length, Q <sub>95</sub> (veh)		0.0											0.1	
Control Delay (s/veh)		9.7											11.9	
Level of Service (LOS)		A											B	
Approach Delay (s/veh)	0.2									11.9				
Approach LOS	A									B				



HCS Two-Way Stop-Control Report

General Information		Site Information	
Analyst	GOM	Intersection	MAIN STREET/PROJECT DRIVEWAY
Agency/Co.	ATE	Jurisdiction	SANTA MARIA
Date Performed	11/29/2023	East/West Street	MAIN STREET
Analysis Year	2023	North/South Street	PROJECT DRIVEWAY
Time Analyzed	PM PEAK HOUR	Peak Hour Factor	0.75
Intersection Orientation	East-West	Analysis Time Period (hrs)	0.25
Project Description	CUMULATIVE + PROJECT		

Lanes



Vehicle Volumes and Adjustments

Approach	Eastbound				Westbound				Northbound				Southbound			
Movement	U	L	T	R	U	L	T	R	U	L	T	R	U	L	T	R
Priority	1U	1	2	3	4U	4	5	6		7	8	9		10	11	12
Number of Lanes	0	1	2	0	0	0	2	0		0	0	0		0	1	0
Configuration		L	T				T	TR							LR	
Volume (veh/h)	0	25	271				510	1						1		16
Percent Heavy Vehicles (%)	3	3												3		3
Proportion Time Blocked																
Percent Grade (%)													0			
Right Turn Channelized																
Median Type   Storage	Left Only								1							

Critical and Follow-up Headways

Base Critical Headway (sec)		4.1												7.5		6.9
Critical Headway (sec)		4.16												6.86		6.96
Base Follow-Up Headway (sec)		2.2												3.5		3.3
Follow-Up Headway (sec)		2.23												3.53		3.33

Delay, Queue Length, and Level of Service

Flow Rate, v (veh/h)		33													23	
Capacity, c (veh/h)		901													623	
v/c Ratio		0.04													0.04	
95% Queue Length, Q <sub>95</sub> (veh)		0.1													0.1	
Control Delay (s/veh)		9.2													11.0	
Level of Service (LOS)		A													B	
Approach Delay (s/veh)		0.8												11.0		
Approach LOS		A												B		

AWD = 9.9 sec. (LOS A)

# Appendix G

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Sewer Study

# Technical Memorandum

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<b>Date:</b>	7/26/2024
<b>To:</b>	Mark Mueller, PE; Shad Springer, PE
<b>Prepared By:</b>	Isabella Campbell, EIT
<b>Reviewed By:</b>	Stephanie Ard, PE; Joshua Reynolds, PE
<b>Project:</b>	Bellecrest Sewer Impact Analysis and Flow Monitoring
<b>Subject:</b>	Sewer Impact Analysis

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## 1.0 Summary

The City of Santa Maria (City) received a development request for the Bellecrest Residences, which proposes to develop one parcel into an age restricted community with 142 residential lots and a community clubhouse space. This proposed development was not accounted for in the 2012 Utilities Capacity Study (UCS), so the City requested an evaluation of its impacts on the existing wastewater system. This Technical Memorandum (TM) assesses whether the City's existing wastewater system can sufficiently serve the additional flow posed by the project.

The study also deployed a wastewater flow meter to check flow volume in the existing wastewater collection system near the proposed project location. The flow volume was used to check if the wastewater model, developed as part of the 2012 UCS, accurately reflects the current system flows. WSC understands that the City's sewage flows decreased after the 2012 UCS because of significant water conservation efforts triggered by the 2011 to 2017 drought.

### 1.1 Flow Monitoring

The wastewater hydraulic model was updated, and its accuracy verified against gravity wastewater flow monitoring data. Model infrastructure was compared to the City's GIS layers and pipe alignment and sizing were updated as necessary. Pipe connectivity, flow directions, and invert elevations were also checked and updated where needed. It is recommended that the City survey the manholes along East Fesler Way to ensure the model is updated with the most accurate information.

In addition to these model updates, the model was validated against flow monitoring data from one site in the vicinity of the proposed development. Figure 1 provides a map showing this location.

No. 1 - 10-in Pipe  
Upstream of of MH  
SM00887-N5B

Planned connection point  
for Bellecrest loads

**Legend**

 Sewer Pipes

 Sewer Manhole

 Bellecrest

**basins**

 Blosser Basin

 Cook-Orange Basin

 Enos Basin

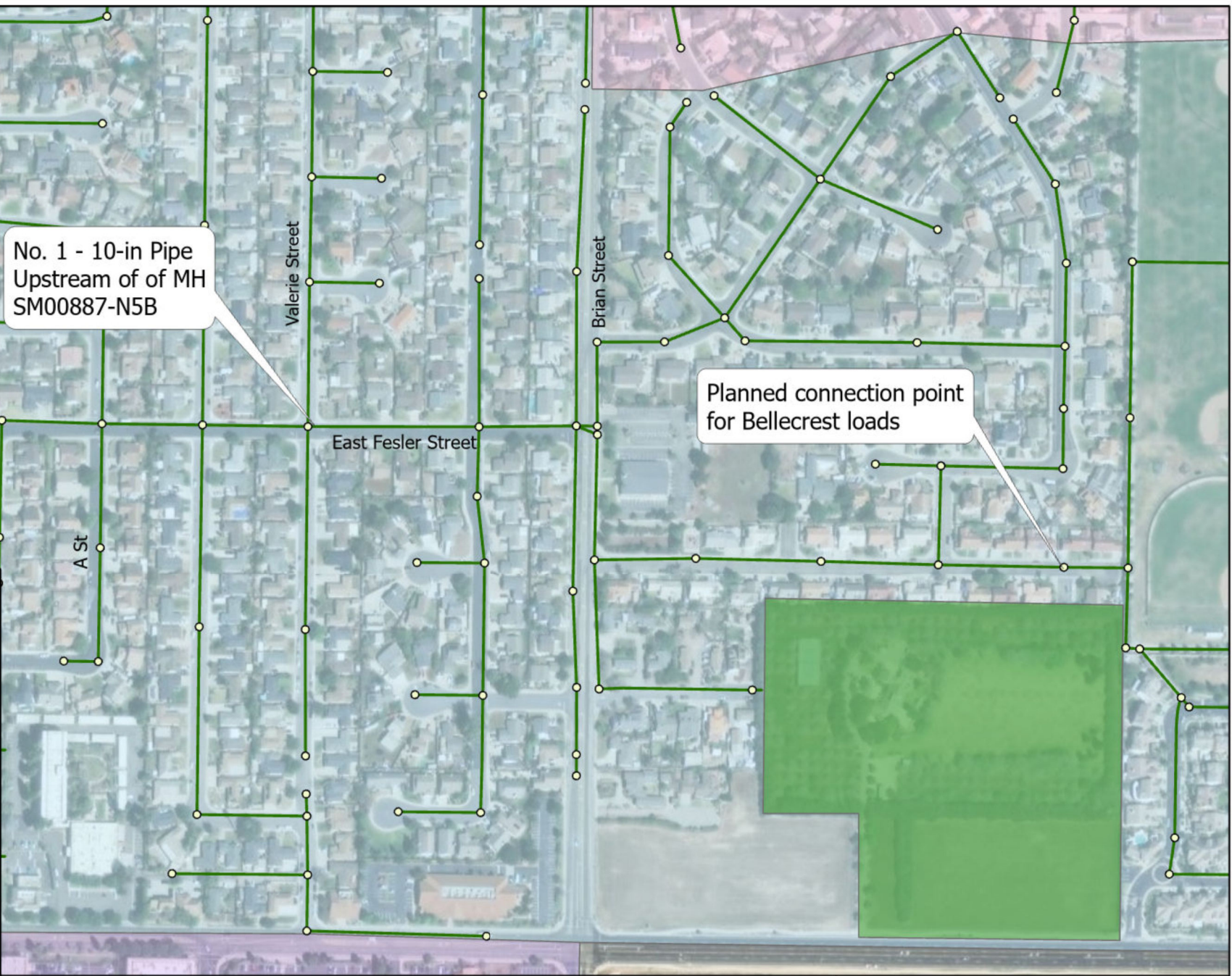
 Fesler Basin

 Inger Basin

 McCoy Basin

 McElhaney Basin


 Morrison Basin




City of Santa Maria  
Bellecrest Sewer Impact Analysis  
Figure 1 - Sewer Flow Monitoring Locations

0 150 300 600

Feet







The flow monitoring data was compared to the hydraulic model predicted flow at the same location under 2013 “current” flow loading conditions. A summary of this comparison is shown in Table 1.

**Table 1. Average Velocity, Level, and Flow Data from Flow Monitoring Period**

Site	Description	Average Flow (MGD)				Peak Hour Flow (MGD)			
		Field	Model	Delta	% Delta	Field	Model	Delta	% Delta
1	Valerie St	0.076	0.09	0.01	11.78%	0.15	0.18	0.03	18.30%

The data obtained from flow monitoring was compared to the loading in the existing model for the Average Daily Flow (ADF) and Peak Hour Flow (PHF) scenarios. At the location the model predicted greater flow than the flow monitoring data under both scenarios, which makes the model a conservative predictor of the system. Based on these results, no changes were made to the model for the purpose of this study.

## 1.2 Flow Projection

Wastewater flow projections were determined using generation factors specific to residential wastewater flows calculated from the UCS. Although the UCS outlines a wastewater factor for R-2 residential zoning, the character of this development along with the age restriction, doesn’t fit that land use. Therefore, we recommend using the method detailed below.

Residential demands vary by community and housing density. On the Central Coast, water conservation measures are strict and most residential units are equipped with water efficient fixtures and appliances. A representative value for high density residential use of 172-gpd per dwelling unit was assumed based on professional judgment and evaluation of multiple similar water suppliers’ demand factors derived from actual water use as summarized in the City of Ventura’s Water Demand Factor Study (Wood Rodgers, April 8, 2020) and the Water Research Foundation’s report on Water Use in the Multi-Family Housing Sector (Krentz, 2018). Based on the UCS water to wastewater return factor of 88% for residential small lot districts, the resulting wastewater generation factor is 150 gpd/dwelling unit. For the clubhouse, a wastewater generation factor of 25 gpd/person was assumed.

A summary of the wastewater flow projections is provided in Table 2.

**Table 2. Wastewater Flow Projections by Development**

Type	Dwelling Units	Acres	Residential Square Footage	Total Projection (gpd)
SFD	142	15.23	351,980	21,300
Clubhouse			2,862	1,517
<b>Total</b>	<b>142</b>	<b>15.23</b>	<b>354,842</b>	<b>22,817</b>

Wastewater peaking factor was pulled from the UCS to develop peak hour loads. This factor is summarized in Table 3.

**Table 3. Peaking Factors**

Demand Type	Peaking Factor	Source
<b>Peak Hour Wet Weather Flow</b>	2.0	UCS Section 5.2.2

The preliminary development plans show the proposed sewer connection point to the 10-in pipe in Rowland Drive, directly north of Spruce Drive. Therefore, the projected loads were added to the manhole shown in Figure 1, with flows going west towards North Suey Road and then West along East Fesler Street.

## 2.0 Evaluation Criteria

The new flow from the proposed development was added to the wastewater system at anticipated point of connection and evaluated using the evaluation criteria described below. Capacity was evaluated under Peak Hour Flow (PHF) conditions. This flow generation of the proposed project was added to the existing City model for this analysis.

WSC used the same evaluation criteria in this analysis as was used in the City's UCS. The evaluation criteria for the wastewater system is summarized in Table 4.

**Table 4. Wastewater System Evaluation Criteria**

Purpose	Criteria
Pipe Velocities (Gravity)	Minimum of <b>2 fps</b> at Average Annual Daily Flow (AAF) and a maximum of <b>10 fps</b> at Peak Hour Wet Weather Flow (PHWWF)
d/D	Maximum d/D at PHWWF or <b>0.60</b> for pipes with diameter 10" or less and <b>0.75</b> for pipes with diameter greater than 10".

## 2.1 Scenarios

The capacity of the City's wastewater collection system was evaluated under a peak flow simulation. Peak flows in a sewer system model signify the maximum expected volume of wastewater and stormwater within the system. These simulations encapsulate the standard wastewater flows originating from service connections, supplemented by the additional inflow and infiltration resulting from a storm event. They provide a comprehensive assessment of the system's capacity to manage the demanding conditions, aiding in the effective design and management of the wastewater infrastructure.

This scenario was assessed under three demand conditions:

- Existing (2024) flows (to be used as a baseline).
- Existing (2024) flows plus the projected development flows.
- Buildout demands (adjusted from the UCS) plus the projected development flows.
- Note that existing flows are assumed to be representative of 2024 wastewater flows because the model was validated using 2024 flow monitoring data.

A summary of all scenarios evaluated is provided in Table 5.

**Table 5. Wastewater Distribution Capacity Analysis Scenarios**

Scenario	System Demands	System Facilities	Criteria
Peak Flow	Existing Peak Flows	Existing System (as of December 2023)	Max d/D = <b>0.60</b> (10" or less) & <b>0.75</b> (greater than 10")
	Existing Peak Flows + Development Flows		
	Buildout Flows (including development flows)		Max velocity = 10 fps

## 3.0 Results

The proposed project was modeled in the City's hydraulic model under the existing PHF and buildout PHF conditions. Under existing PHF conditions, the hydraulic model simulation did not predict that the flows from the proposed developments will cause existing pipes to reach or exceed their d/D limits, with just one pipe segment shown to approach the limit. The d/D results of this analysis are displayed in Figure 2, demonstrating that the proposed development does not cause capacity issues in the sections of the main along East Fesler Street.

Under buildout flow projections, the Bellecrest loads add additional flow to a section of the main along East Fesler Street, making the capacity issues already caused from other buildout loads worse. Bellecrest is not the only development which cause it to exceed d/D limits, shown in Figure 3. One 10-inch pipe segment approaches the capacity limits, along East Fesler Street.



Two additional pipe segments are shown as surcharged and therefore d/D limits could not be calculated by the model and are represented as zero in the figure.

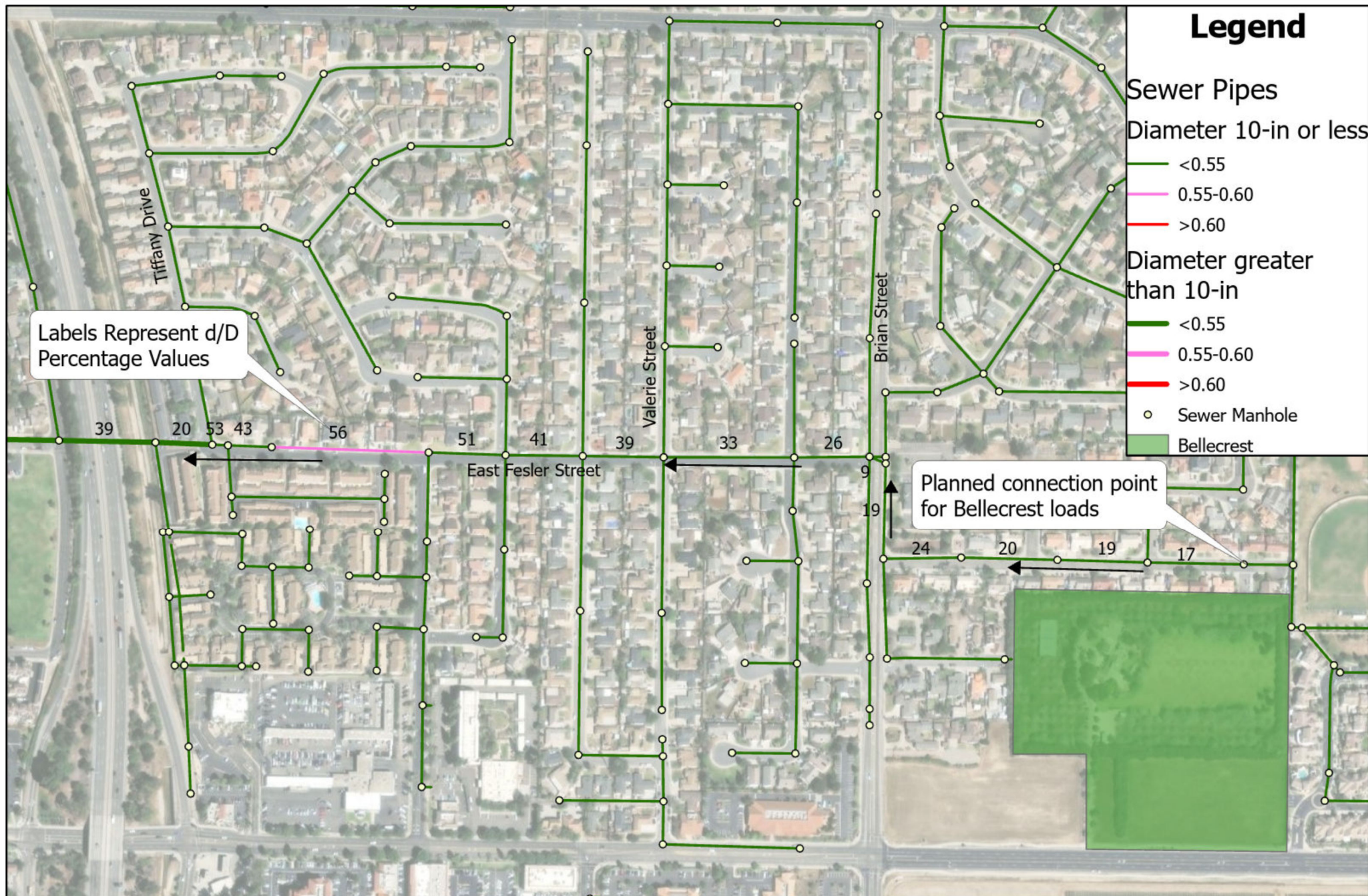
These buildout results are consistent with those predicted in the 2012 UCS. A capital improvement project (CIP) was recommended that entailed replacing the existing 10-inch pipeline along East Fesler Street, from Tiffany Drive to Valerie Street, with a 15-inch pipeline. The results from this analysis show enough capacity exceedances to require the full CIP initially proposed, as described in the following section.

### 3.1 Conclusion and Recommendations

The Bellecrest development will not cause immediate capacity issues for the City's existing wastewater collection system, however, will make future capacity issues worse. After building the Bellecrest development, there will be about 17,787 gallons per minute (in average day flow) of capacity left in the 10-inch pipeline along Fesler Street. This leftover capacity means the pipeline can support the flow from roughly 118 more dwelling units before it is full. It is recommended that the City continue to monitor the available capacity of this wastewater main as the City progresses toward buildout.

Once the pipe reaches its capacity, it is recommended that the City upgrade the section of the 10-inch pipe along Fesler Street, between Tiffany Drive and Valerie drive, in accordance with the UCS, as shown in Figure 4. This will help relieve future capacity issues at buildout and include the pipe segment that is shown to be approaching capacity.

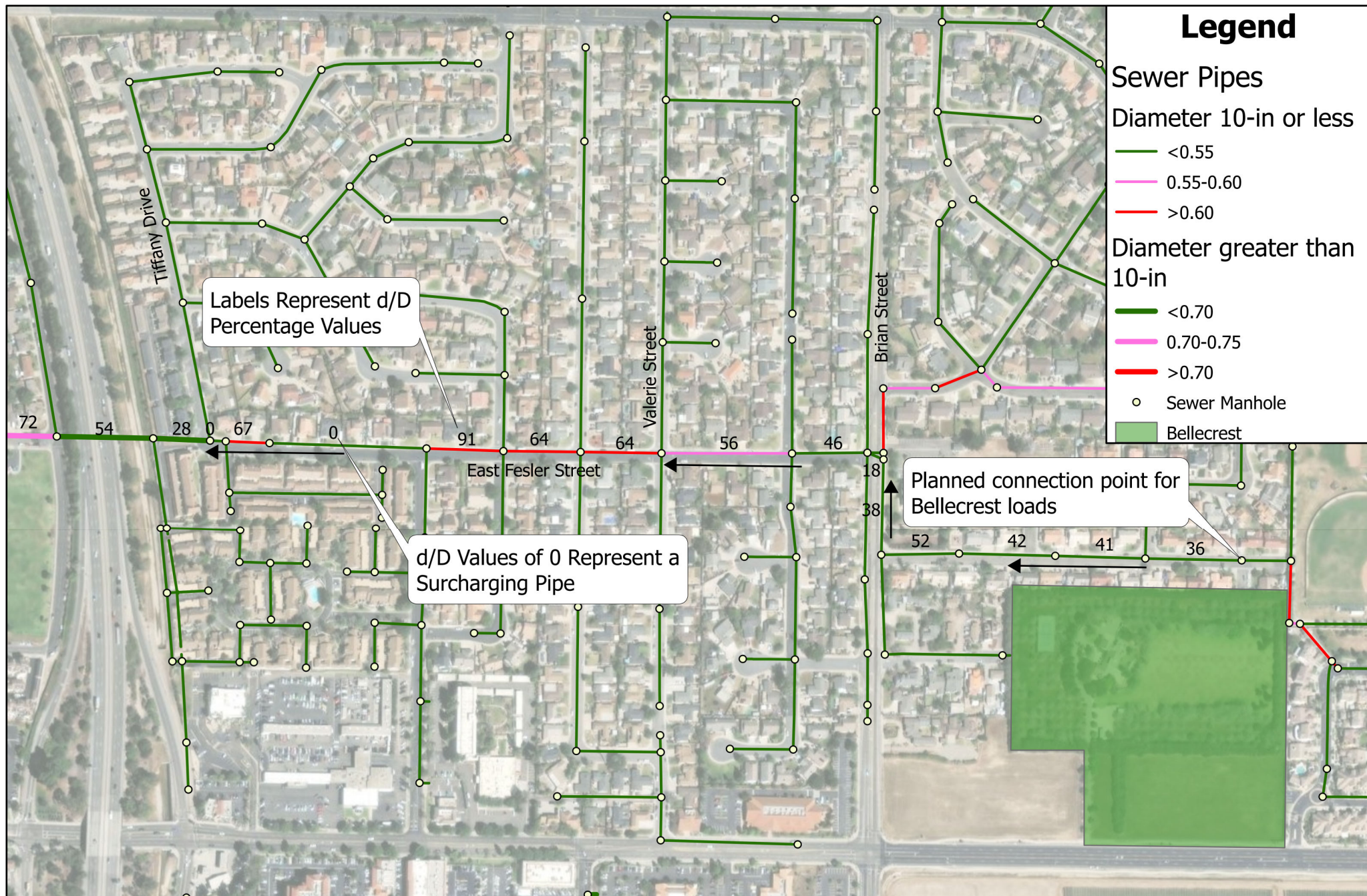
It is also recommended that the City continue to monitor the 27-inch line heading west along Main Street, from Depot Street to the wastewater treatment plant, as the addition of Bellecrest will also exacerbate capacity issues in that line at buildout.



City of Santa Maria  
 Bellecrest Sewer Impact Analysis  
 Figure 2 - d/D Results During PHF Simulation  
 Existing + Future Developments







City of Santa Maria  
 Bellecrest Sewer Impact Analysis  
 Figure 3 - d/D Results During BO Simulation  
 Existing + Future Developments







City of Santa Maria  
Bellecrest Sewer Impact Analysis  
Figure 4 - BO Pipeline Improvements

